Together with Nextel

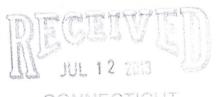
48 Spruce Street Oakland, NJ 07436 Phone: (201)-951-3869

May 20, 2013

Hand Delivered

Ms. Linda Roberts
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051





CONNECTICUT SITING COUNCIL

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 338 Oxford Road, Oxford, CT 06478. Known to Sprint Spectrum L.P. as site CT23XC508.

Dear Ms. Roberts:

In order to accommodate technological changes, implement Code Division Multiple Access ("CDMA") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs Spread-Spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel. LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

As part of the project the new multi-mode 800/1900 antenna will replace existing antennas. These antennas will provide more flexibility for optimization by allowing fast and easy electrical tilt adjustment from remote location and will enable the transmission of multiple technologies from a single antenna. As Sprint Nextel's network evolves to meet the demands of its customers, it is essential for Sprint Nextel to install modern equipment and antennas in order to provide reliable wireless voice and data services. The proposed equipment will include multi-mode radios that will allow Sprint Nextel to

transmit at different frequencies using different technologies, including LTE technology. Likewise, the proposed antennas are quad-pole multi-band high gain antennas that will allow Sprint to operate using its multiple frequency bands and technologies, including LTE technology. The proposed equipment and antennas will improve the reliability, coverage and capacity of Sprint Nextel's voice and data networks across Sprint Nextel's various FCC licensed frequency bands and significantly increase the data speeds of Sprint Nextel's network by utilizing the latest LTE technology. Without the proposed modifications Sprint Nextel will be unable to provide reliable wireless voice and data service using the latest technologies.

Sprint Spectrum L.P. will have an interim (testing) period during the modification/installation prior to the final configuration. This antenna configuration is shown on the attached drawings of the planned modifications. Also included is the power density calculation reflecting the change in Sprint's operations at the site and documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

The changes to the facility do not constitute modification as defined Connecticut General Statues ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for the R.C.S.A. Section 16-50i-72(b)(2).

- 1. The height of the overall structure will not be affected.
- 2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound.
- 3. The proposed changes will not increase the noise level at the existing facility by 6 decibels or more.
- 4. Radio Frequency power density may increase due to the use of one or more CDMA transmissions. Moreover, LTE will utilize additional radio frequencies newly licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons Sprint Spectrum L.P. respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (845)-499-4712 or email Notaro@Transcendwireless.com with questions concerning this matter. Thank you for your consideration.

Sincerely,

Jennifer Palumbo Real Estate Consultant



Date: July 23, 2012

Jason Rouse Crown Castle USA Inc. 3530 Toringdon Way, Suite 300 Charlotte, NC 28277 704.405.6605

Paul J. Ford and Company 250 East Broad St, Suite 1500 Columbus, OH 43215 614.221.6679 tdehnke@pjfweb.com

Subject:

Structural Modification Report

Carrier Designation:

Sprint PCS Co-Locate Carrier Site Number: Carrier Site Name:

CT223XC508

Crown Castle Designation:

Crown Castle BU Number:

876362

N/A

Crown Castle Site Name:

OXFORD / FRITZ PROPERTY

Crown Castle JDE Job Number: Crown Castle Work Order Number:

183460 512743

Engineering Firm Designation:

Paul J. Ford and Company Project Number: 37512-1027 BP R2

Aero Solutions

Site Data:

338 Oxford Rd., OXFORD, New Haven County, CT Latitude 41° 25′ 40.77″, Longitude -73° 6′ 30.75″

150 Foot - Monopole Tower

Dear Jason Rouse,

Paul J. Ford and Company is pleased to submit this "Structural Modification Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 476988, in accordance with application 151572, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure w/ Existing + Reserved + Proposed Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

Sufficient Capacity

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 1.25 inch ice thickness and 50 mph under service loads.

All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle USA Inc. If you have any questions or need further assistance on this or any other

Respectfully submitted

Phomas J. Dehnke. Project Engineer

tnxTower Report - version 6.0.3.0



Date: July 23, 2012

Jason Rouse Crown Castle USA Inc. 3530 Toringdon Way, Suite 300 Charlotte, NC 28277 704.405.6605

Paul J. Ford and Company 250 East Broad St, Suite 1500 Columbus, OH 43215

614.221.6679 tdehnke@pjfweb.com

Subject:

Structural Modification Report

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Sprint PCS Co-Locate

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Respectfully submitted by:

Thomas J. Dehnke, E.I.T. **Project Engineer**

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1) INTRODUCTION

This tower is a 150 ft Monopole tower designed by ENGINEERED ENDEAVORS, INC. in September of 1999. The tower was originally designed for a wind speed of 89.25 mph per TIA/EIA-222-F.

2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 1.25 inch ice thickness and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
	152	1	tower mounts	Miscellaneous [NA 507-1]	<u> </u>	<u> </u>	
		3	RFS/CELWAVE	APXVSPP18-C-A20			
		9	RFS/CELWAVE	ACU-A20-N			
152	150	3	ALCATEL	1900MHz RRH (65MHz)	3	1-1/4	_
	130	3	ALCATEL	800MHz RRH			
		3	ALCATEL	800 EXTERNAL NOTCH FILTER			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
152.0	152.0	6	decibel	DB980H90E-M w/ Mount Pipe	6	1 5/8	3
102.0	102.0	1	tower mounts	Platform Mount [LP 601-1]	-	-	1
		6	adc	DD1900 FULL BAND w/850 BY-PASS MASTHEAD	10		
		3	powerwave	7770.00 w/ Mount Pipe	12	1 1/4	1
		6	powerwave	LGP21901			
		4	andrew	SBNH-1D6565C w/ Mount Pipe			
137.0	139.0	6	communication components inc.	DTMABP7819VG12A			
		3	ericsson	RRUS-11	1	3/8	
		2	kmw communications	AM-X-CD-16-65-00T-RET w/ Mount Pipe	2	3/4	2
		3	powerwave	7020.00			
		1	raycap	DC6-48-60-18-8F			
	137.0	1	tower mounts	Collar Mount (MTC3335)			
	137.0	1	tower mounts	Platform Mount [LP 712-1]	-	-	1
	130.0	1	gps	GPS_A			
		3	antel	BXA-171063-12BF w/ Mount Pipe			
127.0	129.0	3	antel	BXA-70063-4CF-EDIN-X w/ Mount Pipe	1 12	1/2 1 5/8	1
		6	rfs celwave	APL866513-42T0 w/ Pipe			
		6	rfs celwave	FD9R6004/2C-3L			
	127.0	1	tower mounts	Platform Mount [LP 712-1]			
117.0	117.0	3	andrew	HBX-6516DS-VTM w/ Mount Pipe	6	1 5/8	1
		1	tower mounts	T-Arm Mount [TA 601-3]	1	3/8	
75.0	76.0	1	kathrein	OG-860/1920/GPS-A		4.00	
13.0	75.0	1	tower mounts	Side Arm Mount [SO 701-1]	1	1/2	1

Notes:

Existing equipment
Reserved equipment
Existing Equipment to be removed. 1) 2) 3)

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Clarence Welti Assoc., Sprint Site CT23xC508, 9/15/1999	1531939	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	EEI, 5724,1/26/2000	1440552	CCISITES
4-TOWER MANUFACTURER DRAWINGS	EEI, 99-1188, 9/21/1999	1441271	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	Vertical Solutions, 080876.07, 12/01/2008	2364904	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA (PROPOSED #1)	PJF 37511-1194 BP, 12/21/2011	3041498	CCISITES
4-TOWER STRUCTURAL ANALYSIS REPORTS	PJF, 37512-1027R1 B, 06/06/2012	3232137	CCISITES

3.1) Analysis Method

tnxTower (version 6.0.3.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Existing pier vertical reinforcing is assumed carry pole base shear across the interface between the pier and mat. The existing anchors are assumed to transfer the pole base moment directly into the mat portion of the foundation.
- 5) For the existing reinforcing, the monopole was reinforced in conformance with the referenced modification drawings.
- Monopole will be reinforced in conformance to the referenced PJF proposed modification documents.
- 7) Monopole will be reinforced in conformance to the attached proposed modification documents.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	150 - 123.42	Pole	TP20.74x15x0.1875	1	-5.59	614.69	78.5	Pass
L2	123.42 - 115.25	Pole	TP22.0918x19.6804x0.25	2	-7.46	901.01	94.5	Pass
L3	115.25 - 105.25	Pole	TP24.2182x22.0918x0.3845	3	-8.83	1293.52	88.9	Pass
L4	105.25 - 101.9	Pole	TP24.9305x24.2182x0.5774	4	-9.45	1426.64	88.2	Pass
L5	101.9 - 101.25	Pole	TP25.0687x24.9305x0.6054	5	-9.59	1621.83	78.8	Pass
L6	101.25 - 85.96	Pole	TP28.32x25.0687x0.5671	6	-11.77	1677.43	92.4	Pass
L7	85.96 - 76.25	Pole	TP29.8904x26.3182x0.6021	7	-15.43	1945.93	97.0	Pass
L8	76.25 - 75	Pole	TP30.1567x29.8904x0.599	8	-15.71	1954.55	97.8	Pass
L9	75 - 72.15	Pole	TP30.7639x30.1567x0.7005	9	-16.52	2327.11	85.3	Pass
L10	72.15 - 42.41	Pole	TP37.1x30.7639x0.6479	10	-23.13	2657.54	91.6	Pass
L11	42.41 - 31.25	Pole	TP38.849x34.7028x0.5358	11	-25.67	2781.17	93.0	Pass
L12	31.25 - 18.75	Pole	TP41.5094x38.849x0.5216	12	-30.23	3035.21	93.2	Pass
L13	18.75 - 0	Pole	TP45.5x41.5094x0.4491	13	-31.94	2925.92	99.6	Pass
							Summary	
						Pole (L13)	99.6	Pass
						RATING =	99.6	Pass

Table 5 - Tower Component Stresses vs. Capacity

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail	
1,2	Anchor Rods	0	99.4	Pass	
1	Base Plate	0	72.8	Pass	
1	Base Foundation Soil Interaction	0	92.4	Pass	
1	Base Foundation Structural Steel	0	52.8	Pass	

Structure Rating (max from all components) =	99.6%
	t

Notes:

4.1) Recommendations

- 1) See attached proposed modification drawings
- 2) Existing empty pipe mounts at the 150-Ft elevation are to be removed upon installation of the proposed equipment.

See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

²⁾ Worst case scenario between existing and post installed anchors.

APPENDIX A TNXTOWER OUTPUT

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in New Haven County, Connecticut.
- 2) Basic wind speed of 85 mph.
- Nominal ice thickness of 1.2500 in. 3)
- Ice thickness is considered to increase with height. 4)
- Ice density of 56.00 pcf. 5)
- A wind speed of 38 mph is used in combination with ice. 6)
- Temperature drop of 50 °F. 7)
- Deflections calculated using a wind speed of 50 mph. 8)
- A non-linear (P-delta) analysis was used. 9)
- 10) Pressures are calculated at each section.
- 11) Stress ratio used in pole design is 1.333.
- Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are 12) not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification Use Code Stress Ratios

- Use Code Safety Factors Guys
 - Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- Bypass Mast Stability Checks Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- √ Consider Feedline Torque Include Angle Block Shear Check Poles
- √ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	150.00-123.42	26.58	3.17	18	15.0000	20.7400	0.1875	0.7500	A572-65
L2	123.42-115.25	11.34	0.00	18	19.6804	22.0918	0.2500	1.0000	(65 ksi) A572-65
L3	115.25-105.25	10.00	0.00	18	22.0918	24.2182	0.3845	1.5378	(65 ksi) Reinf 55.61 ksi
L4	105.25-101.90	3.35	0.00	18	24.2182	24.9305	0.5774	2.3094	(56 ksi) Reinf 39.97 ksi
L5	101.90-101.25	0.65	0.00	18	24.9305	25.0687	0.6054	2.4215	(40 ksi) Reinf 43.14 ksi
L6	101.25-85.96	15.29	4.08	18	25.0687	28.3200	0.5671	2.2684	(43 ksi) Reinf 43.34 ksi
L7	85.96-76.25	13.79	0.00	18	26.3182	29.8904	0.6021	2.4083	(43 ksi) Reinf 43.47 ksi
L8	76.25-75.00	1.25	0.00	18	29.8904	30.1567	0.5990	2.3958	(43 ksi) Reinf 43.49 ksi
L9	75.00-72.15	2.85	0.00	18	30.1567	30.7639	0.7005	2.8020	(43 ksi) Reinf 43.53 ksi

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
		n	ft	Sides	in	in	in	in	
L10	72.15-42.41	29.74	E 47	40	00 7000	07.4000			(44 ksi)
LIU	72.15-42.41	29.74	5.17	18	30.7639	37.1000	0.6479	2.5914	Reinf 45.71 ksi
L11	40 44 04 05	40.00							(46 ksi)
Lii	42.41-31.25	16.33	0.00	18	34.7028	38.8490	0.5358	2.1432	Reinf 57.63 ksi
1.40	04.05.40.77	4							(58 ksi)
L12	31.25-18.75	12.50	0.00	18	38.8490	41.5094	0.5216	2.0864	Reinf 57.80 ksi
									(58 ksi)
L13	18.75-0.00	18.75		18	41.5094	45.5000	0.4491	1.7965	Reinf 62.50 ksi
NATIONAL AND SELECTION AND SELECTION OF SELECTION AND SELECTION AND SELECTION ASSESSMENT OF SELECTION	Barner de como de a colonia altorio par		DT NE S (SWEAT), CONTRACTO TOTAL THROUGH						(63 ksi)

				Tape	red Po	le Prop	perties			
Section	Tip Dia. in	Area in²	in ⁴	r in	C in	I/C in³	J in⁴	lt∕Q in²	w in	w/t
L1	15.2314	8.8153	244.3603	5.2584	7.6200	32.0683	489.0422	4.4085	2.310	0 12.32
	21.0599	12.2313	652.7391	7.2961	10.5359	61.9537	1306.3371	6.1168	3.320	
L2	20.6685	15.4180	735.4139		9.9977	73.5586	1471.7954	7.7105	3.023	
	22.4326	17.3314	1044.5920		11.2226	93.0792	2090.5584	8.6674	3.448	
L3	22.4326	26.4882	1576.8910		11.2226	140.5102	3155.8568	13.2466	3.211	
	24.5918	29.0829	2087.1766		12.3028	169.6502	4177.0995	14.5442	3.585	
L4	24.5918	43.3220	3058.9375		12.3028	248.6370	6121.9000	21.6651	3.246	
	25.3151	44.6274	3343.8668		12.6647	264.0306	6692.1336	22.3179	3.371	
L5	25.3151	46.7394	3494.0634		12.6647	275.8901	6992.7243	23.3741	3.322	
	25.4554	47.0050	3553.9642		12.7349	279.0726	7112.6049	23.5069	3.346	
L6	25.4554	44.1016	3344.8858		12.7349	262.6548	6694.1729	22.0550	3.414	
. ~	28.7569	49.9537	4860.9588		14.3866	337.8819	9728.3139	24.9816	3.986	
L7	27.7974	49.1436	4105.9834		13.3697	307.1118	8217.3695	24.5765	3.572	
	30.3515	55.9700	6065.6957	10.3973	15.1843	399.4713		27.9903	4.201	
L8	30.3515	55.6859	6036.1917	10.3985	15.1843	397.5283	9 12080.326 0	27.8482	4.206	5 7.023
	30.6219	56.1922	6202.3316	10.4930	15.3196	404.8627	12412.824 5	28.1014	4.253	4 7.101
L9	30.6219	65.4916	7179.1996	10.4569	15.3196	468.6286	14367.845	32.7520	4.074	7 5.817
	31.2385	66.8416	7632.3832	10.6725	15.6281	488.3772	15274.809 2	33.4271	4.181	6 5.97
L10	31.2385	61.9278	7096.0762	10.6912	15.6281	454.0602	14201.489 6	30.9698	4.274	2 6.597
	37.6723	74.9568	12583.302 2	12.9405	18.8468	667.6625	25183.161 9	37.4855	5.389	4 8.319
L11	36.5711	58.1065	8569.8988	12.1293	17.6290	486.1243	17151.074 0	29.0588	5.164	7 9.639
1.40	39.4483	65.1578	12083.733 7	13.6012	19.7353	612.2901	24183.367 6	32.5851	5.894	4 11.001
L12	39.4483	63.4545	11776.576 0	13.6062	19.7353	596.7263	23568.647 9	31.7333	5.919	4 11.348
1 12	42.1498	67.8590	14403.048	14.5507	21.0868	683.0367	28825.049 0	33.9360	6.3876	6 12.246
L13	42.1498	58.5330	12467.588	14.5764	21.0868		24951.583 0	29.2721	6.5152	2 14.506
content decide habe	46.2019	64.2218	16467.436 0	15.9931	23.1140	712.4442	32956.540 3	32.1170	7.217	5 16.07
Tower Elevation	(per fa	ea Thi ace)	usset Gud ickness	sset Grade A	Adjust. Factor Ar	Adjust. Factor A _r	Weight M	ult. Double Stitch Spac Diago	Bolt . cing	ouble Angle Stitch Bolt Spacing Horizontals
<i>ft</i> ∟1 150.00	ft²		in		1		1	in		in
123.42 -2 123.42	2-				1	1	, 1			
							1			

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade Adjust. Factor Ar	Adjust. Factor Ar	Weight Mult.	Double Angle Stitch Bolt	Double Angle Stitch Bolt
ft 105.25	ft ²	in		77		Spacing Diagonals	Spacing Horizontals
L4 105.25-			The state of the s		en commence de la co	in	in
101.90			1	4			
L5 101.90-			·	,	1		
101.25			1	1	4		
L6 101.25-				•	1		
85.96			1	1	4		
L7 85.96-				•	ı		
76.25			1	1	4		
L8 76.25-					•		
75.00			1	1	1		
L9 75.00-					1		
72.15			1	1	1		
L10 72.15-					•		
42.41			1	1	1		
L11 42.41-			_		•		
31.25			1	1	1		
L12 31.25-			•				
18.75			1	1	1		
L13 18.75- 0.00			4				
U,UU			1	1	1		

		<u>u</u> L	ing/Linea	r Appurten	ance	s - Ente	ered Ae	Aron
Description	Face or Leg	Allov Shiel	V Component	Placement ft	Tota Numbe	e chapter is also many any and any	C _A A _A	Weight
LDF6-50A(1-1/4")	С	No		PART PROPERTY OF THE PARTY OF T	The second second second		ft²/ft	klf
FB-L98B-002-75000(С	No	Inside Pole CaAa (Out Of	137.00 - 0.00 137.00 - 0.00	12	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice No Ice	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
WR-VG86ST-BRD(С	No	Face) CaAa (Out Of	137.00 - 0.00		1/2" Ice 1" Ice 2" Ice 4" Ice	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.01 0.02
WR-VG86ST-BRD(С	No	Face) CaAa (Out Of		1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.01
3/4)		110	Face)	46.00 - 0.00	1	No Ice 1/2" Ice 1" Ice 2" Ice	0.00 0.08 0.18 0.28 0.48	0.02 0.00 0.00 0.00
VR-VG86ST-BRD(3/4)	С	No	CaAa (Out Of Face)	76.00 - 46.00	1	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.88 0.00 0.00 0.00	0.01 0.02 0.00 0.00 0.00
VR-VG86ST-BRD(3/4)	С	No :	CaAa (Out Of Face)	137.00 - 76.00	1	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.00 0.00 0.08 0.18 0.28 0.48	0.01 0.02 0.00 0.00 0.00
LDE4 = A A A A A A A A A A A A A A A A A A	C N	1 0	Inside Pole	127.00 - 0.00		4" Ice No Ice 1/2" Ice 1" Ice	0.88 0.00 0.00 0.00	0.01 0.02 0.00 0.00

Description		e Allo	w Componen	t Placement	Tot		menta estagan general.	الرازار وراجدون وجاداتها والرازار والمعادات
	or		eld Type	· · · · · · · · · · · · · · · · · · ·	Numi		$C_A A_A$	Weight
The state of the second	Leg	<i>.</i>	ere se a la l	ft.			ft²/ft	klf
LDF7-50A(1-5/8")	С	No	Incido Data	40= 40		4" Ice	0.00	0.00
, - ,	•	140	Inside Pole	127.00 - 0.00	12		0.00	0.00
						1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" Ice	0.00	
**						4" Ice	0.00	0.00
FXL-1873(1 5/8")	С	N.					0.00	0.00
(, 6,6)	Ü	No	Inside Pole	117.00 - 0.00	6	No ice	0.00	0.00
						1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" ice	0.00	0.00
860 10033(3/8)	С	Nio	lands on a			4" Ice	0.00	0.00
	C	No	Inside Pole	117.00 - 0.00	1	No Ice	0.00	0.00
						1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" lce	0.00	0.00
**						4" lce	0.00	0.00
LDF4-50A(1/2")	^					7 100	0.00	0.00
LDI 4-30A(1/2)	С	No	CaAa (Out Of	75.00 - 0.00	1	No Ice	0.00	
			Face)		,	1/2" Ice	0.00	0.00
			-			1/2" ice 1" ice	0.00	0.00
						2" Ice	0.00	0.00
**							0.00	0.01
						4" Ice	0.00	0.02
LDF4-50A(1/2")	С	No	Inside Pole	60.00 - 0.00	2	A1- 1	_	
				0.00	2	No Ice	0.00	0.00
						1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" Ice	0.00	0.00
**						4" Ice	0.00	0.00
**								
Aero MP3-03	С	No	CaAa (Out Of	76.00 - 46.00				
			Face)	70.00 - 46.00	1	No Ice	0.26	0.00
			. 400)			1/2" Ice	0.37	0.00
						1" Ice	0.48	0.00
						2" Ice	0.71	0.00
**						4" lce	1.15	0.00
Aero MP3-05	Α	No	CaAa (Out Of	46.05 0.00				0.00
			Face)	46.25 - 0.00	1	No Ice	0.35	0.00
			r doe)			1/2" ice	0.40	0.00
						1" Ice	0.66	0.00
						2" Ice	0.88	0.00
Aero MP3-03	Α	No	CaAa (Out Of	70.00 10.00		4" ice	1.32	0.00
			Face)	76.00 - 46.25	1	No Ice	0.26	0.00
			race)			1/2" Ice	0.37	0.00
						1" Ice	0.48	0.00
						2" Ice	0.71	
Aero MP3-03	Α	No	C=A= (O + O			4" Ice	1.15	0.00 0.00
	, ·	140	CaAa (Out Of	116.25 - 76.00	1	No Ice	0.26	
			Face)			1/2" Ice	0.37	0.00
						1" ice	0.48	0.00
						2" Ice	0.71	0.00
114-1-0813U4-M5J(۸	N	.			4" ice	1.15	0.00
1 1/4")	Α	No (CaAa (Out Of	116.25 - 0.00	1	No Ice		0.00
1 174)			Face)		•	1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" Ice	0.00	0.00
114-1-0813U4-M5J(_			4" Ice	0.00	0.01
1 1/4")	A I	No (CaAa (Out Of	150.00 - 116.25	1	No Ice	0.00	0.03
1 1/4)			Face)		,		0.15	0.00
			•			1/2" Ice	0.25	0.00
						1" Ice	0.35	0.00
114.4.0040044						2" Ice	0.55	0.01
114-1-0813U4-M5J(A N	No C	CaAa (Out Of	150.00 - 0.00	2	4" ice	0.95	0.03
1 1/4")			Face)	. 50.00 - 0,00	2	No Ice	0.00	0.00
			,			1/2" Ice	0.00	0.00
						1" Ice	0.00	0.00
						2" Ice	0.00	0.01
The State of the Control of the Cont						4" Ice		

Feed Line/Linear	A /		
Toda Line/Linear	Appurtenances	Section	Areas
		<u> </u>	MI Cas

Tower Sectio	Tower Elevation	Face	A _R	A F	C _A A _A	CAAA	The second se
<i>n</i> L1	ft	er ee oo aan a	ft ²	ft²	In Face ft²	Out Face ft²	Weight
LI	150.00-123.42	Α	0.000	0.000	0.000	the company of the contract of	K
		В	0.000	0.000	0.000	4.093	0.10
1.0		С	0.000	0.000		0.000	0.00
L2	123.42-115.25	Α	0.000	0.000	0.000	1.051	0.16
		В	0.000	0.000	0.000	1.367	0.03
		С	0.000	0.000	0.000	0.000	0.00
L3	115.25-105.25	Α	0.000	0.000	0.000	0.632	0.16
		В	0.000		0.000	2.625	0.04
		č	0.000	0.000	0.000	0.000	0.00
L4	105.25-101.90	Ä	0.000	0.000	0.000	0.774	0.23
		B	0.000	0.000	0.000	0.879	0.01
		č		0.000	0.000	0.000	0.00
L5	101.90-101.25	Ä	0.000	0.000	0.000	0.259	0.08
	701.20	B	0.000	0.000	0.000	0.171	0.00
		Č	0.000	0.000	0.000	0.000	
L6	101.25-85.96		0.000	0.000	0.000	0.050	0.00
	701.20-00.90	A	0.000	0.000	0.000	4.013	0.02
		В	0.000	0.000	0.000	0.000	0.06
L7	85.96-76.25	Ç	0.000	0.000	0.000	1.183	0.00
	00.90-76.25	A	0.000	0.000	0.000	2.549	0.35
		В	0.000	0.000	0.000		0.03
L8	70 00 75 00	С	0.000	0.000	0.000	0.000	0.00
	76.25-75.00	Α	0.000	0.000	0.000	0.752	0.23
		В	0.000	0.000	0.000	0.328	0.00
_9	75.00 ==	С	0.000	0.000	0.000	0.000	0.00
_ 0	75.00-72.15	Α	0.000	0.000	0.000	0.282	0.03
		В	0.000	0.000		0.748	0.01
10		С	0.000	0.000	0.000 0.000	0.000	0.00
10	72.15-42.41	Α	0.000	0.000		0.748	0.07
		В	0.000	0.000	0.000	8.133	0.11
		С	0.000	0.000	0.000	0.000	0.00
11	42.41-31.25	Α	0.000	0.000	0.000	7.141	0.70
		В	0.000	0.000	0.000	3.881	0.04
		Ċ	0.000		0.000	0.000	0.00
2	31.25-18.75	Ä	0.000	0.000	0.000	0.864	0.26
		В	0.000	0.000	0.000	4.347	0.04
		č	0.000	0.000	0.000	0.000	0.00
3	18.75-0.00	Ă	0.000	0.000	0.000	0.968	0.30
		B	0.000	0.000	0.000	6.521	0.07
		Č	0.000	0.000	0.000	0.000	0.00
n ar de de merger y	parties of the partie	**************	U.UUU	0.000	0.000	1.451	0.44

Feed Line/Linear Appurtenances Section Areas - With Ice

the second second second second	Contraction and the second second second second second second						7 1.7 0 40	. AAICII !(
Tower Sectio n	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft²	A _F	C _A A _A In Face	C _A A _A Out Face	Weight
L1	150.00-123.42	Α	1.482	A R. A. Charles and Appear of the con-	ft²	ft ²	ft ²	κ
L2	123.42-115.25	B C A	1.458	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000	11.969 0.000 5.075	0.56 0.00 0.33
L3	115.25-105.25	B C A B	1.445	0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000 0.000	3.820 0.000 3.053 5.835	0.17 0.00 0.27
L4	105.25-101.90	C A B	1.434	0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000	0.000 3.663 1.947	0.20 0.00 0.35 0.07
L5	101.90-101.25	C A B	1.431	0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000	0.000 1.220 0.377	0.07 0.00 0.12 0.01
L6	101.25-85.96	C A B	1.416	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.236 8.825	0.00 0.02 0.30
tovTowor	Poport					0.000	0.000	0.00

Tower Sectio n	Tower Elevation ft	Face or Leg	lce Thickness in	A _R ft ²	A _F ft²	C _A A _A In Face ft²	C _A A _A Out Face ff ²	Weight K
	rente transcer Teaching	C	<mark>***</mark>	0.000	0.000	0.000	5.515	e e e centraliste a la companya de la
L7	85.96-76.25	Ã	1.392	0.000	0.000	0.000	5.605	0.53
		В	1.002	0.000	0.000	0.000		0.19
		Č		0.000	0.000		0.000	0.00
L8	76.25-75.00	Ă	1.381	0.000	0.000	0.000	3.502	0.34
		В	1.001	0.000	0.000	0.000	0.712	0.02
		č		0.000		0.000	0.000	0.00
L9	75.00-72.15	Ä	1.376		0.000	0.000	0.658	0.04
LO	70.00-72.10	B	1.370	0.000	0.000	0.000	1.620	0.05
		Č		0.000	0.000	0.000	0.000	0.00
L10	72.15-42.41		4.004	0.000	0.000	0.000	1.620	0.11
LIU	72.10-42.41	A	1.334	0.000	0.000	0.000	17.283	0.55
		В		0.000	0.000	0.000	0.000	0.00
1.4.4	40 44 04 05	Ç		0.000	0.000	0.000	15.853	1.11
L11	42.41-31.25	A	1.266	0.000	0.000	0.000	8.156	0.21
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	3.842	0.42
L12	31.25-18.75	Α	1.250	0.000	0.000	0.000	8.901	0.21
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	4.093	0.45
L13	18.75-0.00	Α	1.250	0.000	0.000	0.000	13.352	0.32
		В		0.000	0.000	0.000	0.000	0.00
TO STANK AND THE TRANSPORTS THE TRANSPORTS	en partie commente en fact autocourse de les responsibles	C	TOTAL SEASON AND STREET AND SERVICES AND	0.000	0.000	0.000	6.139	0.68

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reea	Line	center o	f Pressure	ļ

Section	Elevation	CP_X	CP₂	CP _X Ice	CP _z Ice
	ft	in	in	in	in
L1	150.00-123.42	-0.0490	-0.1761	-0.1676	-0.3264
L2	123.42-115.25	-0.0883	-0.1700	-0.3005	-0.2613
L3	115.25-105.25	-0.0855	-0.2854	-0.2943	-0.3714
L4	105.25-101.90	-0.0862	-0.2879	-0.2997	-0.3792
L5	101.90-101.25	-0.0864	-0.2886	-0.3013	-0.3814
L6	101.25-85.96	-0.0872	-0.2912	-0.3067	-0.3897
L7	85.96-76.25	-0.0880	-0.2938	-0.3140	-0.3990
L8	76.25-75.00	-0.2452	-0.1879	-0.4469	-0.3002
L9	75.00-72.15	-0.2825	-0.1631	-0.4800	-0.2771
L10	72.15-42.41	-0.2620	-0.1971	-0.4683	-0.3234
L11	42.41-31.25	-0.0885	-0.4080	-0.3158	-0.5919
L12	31.25-18.75	-0.0892	-0.4114	-0.3098	-0.5993
L13	18.75-0.00	-0.0900	-0.4150	-0.3164	-0.6120

Discrete Tower Loads											
Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement	state before the second of the second	C _A A _A Front	C _A A _A Side	Weigh		
·			ft ft ft	o	ft		ft²	ft²	7a		
Side Arm Mount [SO 701-	С	None		0.00	75.00	No Ice 1/2" Ice 1" Ice	0.85 1.14 1.43	1.67 2.34 3.01	0.07 0.08 0.09		
OG-860/1920/GPS-A	В	From Face	2.00	0.00	75.00	2" Ice 4" Ice No Ice	2.01 3.17 0.33	4.35 7.03 0.40	0.12 0.18 0.00		
xTower Report - versio			0.00 1.00			1/2" Ice	0.43 0.55	0.51 0.63	0.01 0.01		

Description	. (ace Offset or Type eg	Offsets: Horz Lateral Vert ft	Azimuth Adjustmen t	Placeme ft	nt	C_AA_A Front	C_AA_A Side	Weight
And the second of the second o		n and an area of the second property of	ft ft		514 W.E. (1)				
***						1" lce 2" lce 4" lce		0.89 1.52	0.02 0.08
T-Arm Mount [TA 601-3]	C	None		0.00	117.00	No Ice 1/2" Ice 1" Ice 2" Ice	10.90 14.65 18.40 25.90 40.90	10.90 14.65 18.40 25.90 40.90	0.73 0.93 1.13 1.52 2.32
HBX-6516DS-VTM w/ Mount Pipe	А	From Face	4.00 0.00 0.00	0.00	117.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	3.60 4.00 4.43 5.37 7.36	3.24 3.91 4.56 5.91 8.88	0.03 0.06 0.10 0.20 0.50
HBX-6516DS-VTM w/ Mount Pipe	В	From Face	4.00 0.00 0.00	0.00	117.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	3.60 4.00 4.43 5.37 7.36	3.24 3.91 4.56 5.91 8.88	0.03 0.06 0.10 0.20 0.50
HBX-6516DS-VTM w/ Mount Pipe	С	From Face	4.00 0.00 0.00	0.00	117.00	4" ice No ice 1/2" Ice 1" ice 2" ice 4" ice	3.60 4.00 4.43 5.37 7.36	3.24 3.91 4.56 5.91 8.88	0.03 0.06 0.10 0.20 0.50
Platform Mount [LP 712-1]	С	None		0.00	127.00	No Ice 1/2" Ice 1" Ice 2" Ice	24.53 29.94 35.35 46.17 67.81	24.53 29.94 35.35 46.17 67.81	1.34 1.65 1.96 2.58 3.82
GPS_A ***	В	From Face	4.00 0.00 3.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.30 0.37 0.46 0.65 1.15	0.30 0.37 0.46 0.65 1.15	0.00 0.00 0.01 0.02 0.08
7770.00 w/ Mount Pipe	A	From Face	4.00 0.00 2.00	0.00	137.00	No Ice 1/2" Ice 1" Ice 2" Ice	6.12 6.63 7.13 8.16 10.36	4.25 5.01 5.71 7.16 10.41	0.06 0.10 0.16 0.29 0.66
7770.00 w/ Mount Pipe	В	From Face	4.00 0.00 2.00	0.00	137.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	6.12 6.63 7.13 8.16 10.36	4.25 5.01 5.71 7.16 10.41	0.06 0.10 0.16 0.29 0.66
7770.00 w/ Mount Pipe	С	From Face	4.00 0.00 2.00	0.00	137.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	6.12 6.63 7.13 8.16 10.36	4.25 5.01 5.71 7.16 10.41	0.06 0.10 0.16 0.29 0.66
(2) LGP21901	Α	From Face	4.00 0.00 2.00	0.00	137.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.27 0.34 0.43 0.62 1.10	0.18 0.25 0.32 0.49 0.94	0.01 0.01 0.01 0.02 0.07

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Description		Fac oi Le	r Ty	set pe	Offse Horn Later Vert ft ft	z Adjustn al t	nen	ement ft	C _A , Fro	ent Sid	
(0) 1 000 100			terror and a second of		ft	to and an experience	9 m - 5 m - 1 - 1 - 1 - 1 - 1				^
(2) LGP21901		В	From f	Face	4.00 0.00 2.00	0.00	137	7.00 No 1/2 Ic 1" I 2" I	2" 0.34 e 0.43 ce 0.62	0.25 0.32 0.49	0.01 0.01 0.02
(2) LGP21901		С	From F	ace	4.00 0.00 2.00	0.00	137.	4"	ce ce 0.27 " 0.34 9 0.43	0.18 0.25 0.32	0.07 0.01 0.01 0.01
(2) DD1900 FULL BAND W/850 BY-PASS MASTHEAD)	Α	From Fa	ace	4.00 0.00 2.00	0.00	137.(2" lo 4" lo 00 No lo 1/2' lce 1" lo	te 1.10 te 1.29 ' 1.44 1.60	0.94 0.32 0.42 0.52	0.02 0.07 0.02 0.02 0.03
(2) DD1900 FULL BAND w/850 BY-PASS MASTHEAD		В	From Fa	ce	4.00 0.00 2.00	0.00	137.0	2" lca 4" lca 0 No lca 1/2" ice	2.75 9 1.29 1.44 1.60	0.76 1.35 0.32 0.42 0.52	0.06 0.14 0.02 0.02 0.03
(2) DD1900 FULL BAND W/850 BY-PASS MASTHEAD	•	С	From Fac	æ	4.00 0.00 2.00	0.00	137.00	1/2"	2.75 1.29 1.44	0.76 1.35 0.32 0.42	0.06 0.14 0.02 0.02
Platform Mount [LP 712-1]	C	3	None			0.00	137.00	. 10 100	1.60 1.95 2.75 24.53	0.52 0.76 1.35 24.53	0.03 0.06 0.14
Collar Mount (MTC3335)	С		None			0.00		1/2" Ice 1" Ice 2" Ice 4" Ice	29.94 35.35 46.17 67.81	29.94 35.35 46.17 67.81	1.65 1.96 2.58 3.82
(2) SDNIL 4D05000						0.00	137.00	No Ice 1/2" Ice 1" Ice 2" Ice	6.00 7.22 8.44 10.88 15.76	6.00 7.22 8.44 10.88	0.15 0.19 0.23 0.32
(2) SBNH-1D6565C w/ Mount Pipe	Α	Fr	om Face	0	1.00 0.00 0.00	0.00	137.00	4" Ice No Ice 1/2" Ice 1" Ice	11.56 12.22 12.89 14.29	9.72 11.19 12.59 14.87	0.50 0.09 0.18 0.28 0.51
(2) SBNH-1D6565C w/ Mount Pipe	В	Fro	m Face	0.	.00 .00 .00	0.00	137.00	2" Ice 4" Ice No Ice 1/2" Ice 1" Ice	17.43 11.56 12.22 12.89 14.29	9.72 11.19 12.59	1.14 0.09 0.18 0.28
2) AM-X-CD-16-65-00T- RET w/ Mount Pipe	С	Fro	m Face	4.0 0.0 2.0	00	0.00	137.00	2" Ice 4" Ice No Ice 1/2"	17.43 8.50 9.15	14.87 19.62 6.30 7.48	0.51 1.14 0.07
) DTMABP7819VG12A	A	Fron	n Face	4.0		0.00	407.00	Ice 1" Ice 2" Ice 4" Ice	9.77 11.03 13.68	7.48 8.37 10.18 14.02	0.14 0.21 0.38 0.87
				0.0 2.0	0	0.00	137.00	No Ice 1/2" Ice 1" Ice	1.14 1.28 1.44	0.39 0.49 0.59	0.02 0.03 0.04

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement	ARTON MORE TO THE	C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٥	ft		ft²	ft²	κ
(2) DTMARD77040\(0.40.4	_					2" Ice 4" Ice	2.54	1.41	0.14
(2) DTMABP7819VG12A	В	From Face	4.00	0.00	137.00	No Ice	1.14	0.39	0.02
			0.00 2.00			1/2"	1.28	0.49	0.03
			2.00			Ice 1" Ice	1.44 1.77	0.59	0.04
						2" Ice 4" Ice	2.54	0.83 1.41	0.06 0.14
(2) DTMABP7819VG12A	С	From Face	4.00	0.00	137.00	No Ice	1.14	0.39	0.02
			0.00			1/2"	1.28	0.49	0.03
			2.00			ice	1.44	0.59	0.04
						1" ice	1.77	0.83	0.06
						2" Ice 4" Ice	2.54	1.41	0.14
7020.00	Α	From Face	4.00	0.00	137.00	No ice	0.12	0.20	0.00
			0.00	0.00	107.00	1/2"	0.12	0.28	0.00 0.01
			2.00			Ice	0.23	0.36	0.01
						1" Ice	0.38	0.56	0.02
						2" Ice	0.78	1.05	0.07
7020.00	В	From Face	4.00	0.00	427.00	4" ice	0.40		
7020.00	D	Tromrace	0.00	0.00	137.00	No Ice 1/2"	0.12 0.17	0.20 0.28	0.00
			2.00			Ice	0.17	0.26	0.01 0.01
						1" Ice	0.38	0.56	0.02
						2" Ice	0.78	1.05	0.07
7020.00	С	From Face	4.00	0.00	407.00	4" Ice			
7020.00	C	riom race	4.00 0.00	0.00	137.00	No Ice 1/2"	0.12	0.20	0.00
			2.00			lce	0.17 0.23	0.28 0.36	0.01 0.01
						1" Ice	0.23	0.56	0.01
						2" Ice 4" Ice	0.78	1.05	0.07
RRUS-11	Α	From Face	4.00	0.00	137.00	No Ice	4.42	1.19	0.05
			0.00 2.00			1/2"	4.71	1.35	0.07
			2.00			Ice 1" Ice	5.00 5.61	1.53	0.10
						2" Ice	6.94	1.90 2.75	0.17 0.36
						4" Ice	0.04	2.70	0.50
RRUS-11	В	From Face	4.00	0.00	137.00	No Ice	4.42	1.19	0.05
			0.00			1/2"	4.71	1.35	0.07
			2.00			ice	5.00	1.53	0.10
						1" Ice 2" Ice	5.61 6.94	1.90 2.75	0.17
						4" Ice	U.J-4	2.75	0.36
RRUS-11	С	From Face	4.00	0.00	137.00	No Ice	4.42	1.19	0.05
			0.00			1/2"	4.71	1.35	0.07
			2.00			Ice	5.00	1.53	0.10
						1" Ice 2" Ice	5.61 6.94	1.90 2.75	0.17
						4" Ice	0.54	2.73	0.36
DC6-48-60-18-8F	Α	From Face	4.00	0.00	137.00	No Ice	2.57	4.32	0.02
			0.00			1/2"	2.80	4.60	0.05
			2.00			Ice	3.04	4.88	0.09
						1" Ice	3.54	5.49	0.17
						2" Ice 4" Ice	4.66	6.80	0.38

(2) APL866513-42T0 w/	۸	Fram F	4.00	0.05					
Mount Pipe	Α	From Face	4.00 0.00	0.00	127.00	No Ice	4.53	4.92	0.03
			2.00			1/2" Ice	4.97 5.41	5.60 6.28	0.08
						1" Ice	6.34	6.28 7.71	0.13 0.25
								, .	ں۔جی
						2" Ice	8.32	10.83	0.60
(2) APL866513-42T0 w/	В	From Face	4.00	0.00	127.00	2" Ice 4" Ice No Ice	8.32 4.53	10.83 4.92	0.60 0.03

Description		ace Offset or Type .eg	Offsets: Horz Lateral Vert ft	Azimuth Adjustmen t	Placeme ft	ent	C _A A _A Front	C _A A _A Side	Weigh
Mount Pipe		The second s	ft ft	0	п		ft²	ft ²	κ
·			0.00 2.00			1/2" Ice 1" Ice 2" Ice 4" Ice	8.32	5.60 6.28 7.71 10.83	0.08 0.13 0.25 0.60
(2) APL866513-42T0 w/ Mount Pipe	(C From Face	9 4.00 0.00 2.00	0.00	127.00	No Ice 1/2" Ice 1" Ice 2" Ice		4.92 5.60 6.28 7.71 10.83	0.03 0.08 0.13 0.25 0.60
(2) FD9R6004/2C-3L	A	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.37 0.45 0.54 0.75 1.28	0.08 0.14 0.20 0.34	0.00 0.01 0.01 0.02
(2) FD9R6004/2C-3L	В	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.37 0.45 0.54 0.75 1.28	0.74 0.08 0.14 0.20 0.34 0.74	0.06 0.00 0.01 0.01 0.02
(2) FD9R6004/2C-3L	С	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	0.37 0.45 0.54 0.75 1.28	0.74 0.08 0.14 0.20 0.34 0.74	0.06 0.00 0.01 0.01 0.02 0.06
BXA-171063-12BF w/ Mount Pipe	Α	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	4.97 5.52 6.04 7.09 9.36	5.23 6.39 7.26 9.05 12.82	0.04 0.08 0.14 0.27 0.67
BXA-70063-4CF-EDIN-X w/ Mount Pipe	Α	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.40 5.84 6.30 7.24 9.26	3.69 4.29 4.91 6.26 9.29	0.03 0.07 0.12 0.23 0.58
BXA-171063-12BF w/ Mount Pipe	В	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	4.97 5.52 6.04 7.09 9.36	5.23 6.39 7.26 9.05 12.82	0.04 0.08 0.14 0.27 0.67
3XA-70063-4CF-EDIN-X w/ Mount Pipe	В	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.40 5.84 6.30 7.24 9.26	3.69 4.29 4.91 6.26	0.03 0.07 0.12 0.23
BXA-171063-12BF w/ Mount Pipe	С	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice	4.97 5.52 6.04 7.09 9.36	9.29 5.23 6.39 7.26 9.05	0.58 0.04 0.08 0.14 0.27
XA-70063-4CF-EDIN-X w/ Mount Pipe	С	From Face	4.00 0.00 2.00	0.00	127.00	4" Ice No Ice 1/2" Ice 1" Ice	5.40 5.84 6.30 7.24 9.26	3.69 4.29 4.91 6.26 9.29	0.67 0.03 0.07 0.12 0.23 0.58

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	0	ft		ft²	ft²	K
1900MHz RRH (65MHz)	Α	From Face	4.00	0.00	152.00	No Ice	2.70	2.77	0.06
			0.00			1/2"	2.94	3.01	0.08
			-2.00			Ice	3.18	3.26	0.11
						1" Ice 2" Ice 4" Ice	3.70 4.85	3.78 4.93	0.18 0.35
800 EXTERNAL NOTCH	Α	From Face	4.00	0.00	152.00	No ice	0.77	0.37	0.01
FILTER			0.00			1/2"	0.89	0.46	0.02
			-2.00			Ice	1.02	0.56	0.02
						1" lce	1.30	0.79	0.04
						2" Ice 4" Ice	1.97	1.34	0.11
800MHZ RRH	Α	From Face	4.00	0.00	152.00	No Ice	2.49	2.07	0.05
			0.00			1/2"	2.71	2.27	0.07
			-2.00			tce	2.93	2.48	0.10
						1" Ice	3.41	2.93	0.16
						2" Ice	4.46	3.93	0.32
(3) ACU-A20-N	Α	From Face	4.00	0.00	152.00	4" Ice No Ice	0.08	0.14	0.00
(0) / 100 / 120 / 1	,,	1 TOTAL ACC	0.00	0.00	132.00	1/2"	0.08	0.14	0.00
			-2.00			ice	0.17	0.15	0.00
						1" Ice	0.30	0.40	0.01
						2" Ice	0.67	0.80	0.04
APXVSPP18-C-A20 w/	۸	Fram Face	4.00	0.00	450.00	4" ice	0.50		2.22
Mount Pipe	Α	From Face	4.00 0.00	0.00	152.00	No Ice	8.50	6.95	0.08
would the			-2.00			1/2" Ice	9.15 9.77	8.13 9.02	0.15 0.22
			2.00			1" Ice	11.03	10.84	0.22
						2" Ice	13.68	14.85	0.91
40004411	_					4" Ice			
1900MHz RRH (65MHz)	В	From Face	4.00	0.00	152.00	No Ice	2.70	2.77	0.06
			0.00 -2.00			1/2"	2.94	3.01	0.08
			-2.00			lce 1" lce	3.18 3.70	3.26 3.78	0.11 0.18
						2" Ice	4.85	4.93	0.15
						4" Ice			0.00
800 EXTERNAL NOTCH	В	From Face	4.00	0.00	152.00	No Ice	0.77	0.37	0.01
FILTER			0.00			1/2"	0.89	0.46	0.02
			-2.00			lce	1.02	0.56	0.02
						1" Ice 2" Ice	1.30 1.97	0.79 1.34	0.0 4 0.11
						4" Ice	1.07	1.04	0.11
800MHZ RRH	В	From Face	4.00	0.00	152.00	No Ice	2.49	2.07	0.05
			0.00			1/2"	2.71	2.27	0.07
			-2.00			Ice	2.93	2.48	0.10
						1" Ice 2" Ice	3.41	2.93	0.16
						4" Ice	4.46	3.93	0.32
(3) ACU-A20-N	В	From Face	4.00	0.00	152.00	No Ice	0.08	0.14	0.00
			0.00			1/2"	0.12	0.19	0.00
			-2.00			Ice	0.17	0.25	0.00
						1" Ice	0.30	0.40	0.01
						2" Ice 4" Ice	0.67	0.80	0.04
APXVSPP18-C-A20 w/	В	From Face	4.00	0.00	152.00	No ice	8.50	6.95	0.08
Mount Pipe			0.00			1/2"	9.15	8.13	0.15
			-2.00			Ice	9.77	9.02	0.22
						1" Ice	11.03	10.84	0.41
						2" Ice	13.68	14.85	0.91
1900MHz RRH (65MHz)	С	From Face	4.00	0.00	152.00	4" Ice No Ice	2.70	2.77	0.06
	9		0.00	0.00	102.00	1/2"	2.70	3.01	0.06 0.08
			-2.00			Ice	3.18	3.26	0.00
						1" Ice	3.70	3.78	0.18

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement	Property of the Control	C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	0	ft		ft²	ft ²	Κ
						2" Ice 4" Ice	4.85	4.93	0.35
800 EXTERNAL NOTCH	С	From Face	4.00	0.00	152.00	No Ice	0.77	0.37	0.01
FILTER			0.00			1/2"	0.89	0.46	0.02
			-2.00			Ice	1.02	0.56	0.02
						1" Ice	1.30	0.79	0.04
						2" Ice	1.97	1.34	0.11
						4" Ice			
800MHZ RRH	С	From Face	4.00	0.00	152.00	No Ice	2.49	2.07	0.05
			0.00			1/2"	2.71	2.27	0.07
			-2.00			Ice	2.93	2.48	0.10
						1" Ice	3.41	2.93	0.16
						2" Ice	4.46	3.93	0.32
						4" Ice			
(3) ACU-A20-N	С	From Face	4.00	0.00	152.00	No Ice	0.08	0.14	0.00
			0.00			1/2"	0.12	0.19	0.00
			-2.00			ice	0.17	0.25	0.00
						1" Ice	0.30	0.40	0.01
						2" Ice	0.67	0.80	0.04
						4" Ice			
APXVSPP18-C-A20 w/	С	From Face	4.00	0.00	152.00	No Ice	8.50	6.95	0.08
Mount Pipe			0.00			1/2"	9.15	8.13	0.15
			-2.00			Ice	9.77	9.02	0.22
						1" Ice	11.03	10.84	0.41
						2" Ice	13.68	14.85	0.91
						4" Ice			
Platform Mount [LP 602-1]	С	None		0.00	152.00	No Ice	32.03	32.03	1.34
						1/2"	38.71	38.71	1.80
						Ice	45.39	45.39	2.26
						1" Ice	58.75	58.75	3.17
						2" Ice	85.47	85.47	5.00
						4" Ice			0.00
8-ft Ladder	С	None		0.00	152.00	No Ice	5.00	5.00	0.04
						1/2"	6.00	6.00	0.07
						ice	7.00	7.00	0.08
						1" Ice	9.00	9.00	0.11
						2" Ice	13.00	13.00	0.11
						4" Ice	10.00	10.00	0.10

Tower Pressures - No Ice

 $G_{H} = 1.690$

Section Elevation	Z	Kz	q_z	A_G	F a	A_F	A_R	A _{leg}	Leg %	C _A A _A In	C _A A _A Out
ft	ft		ksf	ft²	c e	ft²	ft²	ft²	-	Face ft²	Face ft ²
L1 150.00-	136.00	1.499	0.03	39.582	Α	0.000	39.582	39.582	100.00	0.000	4.093
123.42					В	0.000	39.582		100.00	0.000	0.000
Į					С	0.000	39.582	ł	100.00	0.000	1.051
L2 123.42-	119.28	1.444	0.03	14.449	Α	0.000	14.449	14.449	100.00	0.000	1,367
115.25					В	0.000	14.449		100.00	0.000	0.000
					С	0.000	14.449		100.00	0.000	0.632
L3 115.25-	110.17	1.411	0.03	19.296	Α	0.000	19.296	19.296	100.00	0.000	2.625
105.25			- 1		В	0.000	19.296	j	100.00	0.000	0.000
					C	0.000	19.296		100.00	0.000	0.774
L4 105.25-	103.57	1.386	0.03	6.860	Α	0.000	6.860	6.860	100.00	0.000	0.879
101.90			İ		В	0.000	6.860		100.00	0.000	0.000
					С	0.000	6.860		100.00	0.000	0.259

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Section	Z	Kz	qz	A _G	F	A _F	A _R	Α.	100	I 0.4	
Elevation		1	"-	1.0	a] ''	78	A _{leg}	Leg %	CAAA	$C_A A_A$
j		ļ]		C	ì			70	In Face	Out
ft	ft	l	ksf	ft ²	e	ft²	ft ²	ft ²		Face ff ²	Face ft ²
L5 101.90-	101.57	1.379	0.03	1.354	Α	0.000	1.354	1.354	100.00	0.000	0,171
101.25		l	ļ		В	0.000	1.354	1.004	100.00	0.000	
					C	0.000	1.354		100.00	0.000	0.000 0.050
L6 101.25-	93.45	1.346	0.02	34.013	Α	0.000	34.013	34.013	100.00	0.000	4.013
85.96		ŀ			В	0.000	34.013	01.010	100.00	0.000	0.000
					С	0.000	34.013		100.00	0.000	1.183
L7 85.96-	81.03	1.293	0.02	23.169	Α	0.000	23.169	23.169	100.00	0.000	2.549
76.25					В	0.000	23.169		100.00	0.000	0.000
10 70 07					С	0.000	23.169		100.00	0.000	0.752
L8 76.25-	75.62	1.267	0.02	3.127	Α	0.000	3.127	3.127	100.00	0.000	0.328
75.00					В	0.000	3.127		100.00	0.000	0.000
10.75.00	70.57				С	0.000	3.127		100.00	0.000	0.282
L9 75.00-	73.57	1.257	0.02	7.234	Α	0.000	7.234	7.234	100.00	0.000	0.748
72.15	i		- 1		В	0.000	7.234		100.00	0.000	0.000
L10 72.15-	50.00	4 400			Ç	0.000	7.234		100.00	0.000	0.748
42.41	56.82	1.168	0.02	84.095	Α	0.000	84.095	84.095	100.00	0.000	8.133
42.41		ĺ	1		В	0.000	84.095		100.00	0.000	0.000
L11 42.41-	36.76	4 004	0.00		C	0.000	84.095		100.00	0.000	7.141
31,25	30.70	1.031	0.02	34.812	Α	0.000	34.812	34.812	100.00	0.000	3.881
31.23	ļ	- 1	1		В	0.000	34.812		100.00	0.000	0.000
L12 31.25-	24.93	1	0.00	44 050	c	0.000	34.812		100.00	0.000	0.864
18.75	24.83	1	0.02	41.853	A	0.000	41.853	41.853	100.00	0.000	4.347
10.73	l	-		İ	В	0.000	41.853	- 1	100.00	0.000	0.000
L13 18.75-	9.23	1	0.00	67.070	Ċ	0.000	41.853		100.00	0.000	0.968
0.00	9.23	'	0.02	67.976	A	0.000	67.976	67.976	100.00	0.000	6.521
0.00	ŀ	İ		į	B	0.000	67.976	ľ	100.00	0.000	0.000
				<u> </u>	С	0.000	67.976		100.00	0.000	1.451

Tower Pressure - With Ice

 $G_H = 1.690$

Section	Z	Kz	q _z	tz	A_{G}	F	AF	AR	A _{leg}	Leg	C _A A _A	C.A.
Elevation						а		- '''	, neg	20g	In	C _A A _A Out
					_	C	1 1			,,	Face	Face
ft	ft		ksf	in	ft ²	е	ft ²	ft²	ft ²		ft ²	ft ²
L1 150.00-	136.00	1.499	0.01	1.4815	46.145	A	0.000	46.145	46,145	100.00	0.000	11.969
123.42						В	0.000	46.145		100.00	0.000	0.000
1040040	اءء مدد					С	0.000	46.145		100.00	0.000	5.075
L2 123.42-	119.28	1.444	0.01	1.4584	16.467	Α	0.000	16.467	16.467	100.00	0.000	3.820
115.25						В	0.000	16.467		100.00	0.000	0.000
1244505	440.47					С	0.000	16.467		100.00	0.000	3.053
L3 115.25-	110.17	1.411	0.01	1.4446	21.703	Α	0.000	21.703	21.703	100.00	0.000	5.835
105.25		- 1	1			В	0.000	21.703		100.00	0.000	0.000
L4 105.25-	400 57	4 000				С	0.000	21.703		100.00	0.000	3.663
101.90	103.57	1.386	0.01	1.4339	7.661	Α	0.000	7.661	7.661	100.00	0.000	1.947
101.90	l	- 1	1	1		В	0.000	7.661		100.00	0.000	0.000
L5 101.90-	101 57	4 070	ا م م ما			С	0.000	7.661	ľ	100.00	0.000	1.220
101.25	101.57	1.379	0.00	1.4305	1.509	Α	0.000	1.509	1.509	100.00	0.000	0.377
101.23	-	ł		ŀ	1	В	0.000	1.509	I	100.00	0.000	0.000
L6 101.25-	93.45	1.346	0.00	4 4400	07.000	Ċ	0.000	1.509	i	100.00	0.000	0.236
85.96	95.45	1.340	0.00	1.4163	37.622	Α	0.000	37.622	37.622	100.00	0.000	8.825
00.50	1	l		i		В	0.000	37.622		100.00	0.000	0.000
L7 85.96-76.25	81.03	1.293	0.00	4 2022	05.404	С	0.000	37.622		100.00	0.000	5.515
00.00 70.20	01.03	1.233	0.00	1.3923	25.461	A	0.000	25.461	25.461	100.00	0.000	5.605
	ļ	- 1	- 1	ŀ	i	В	0.000	25.461	1	100.00	0.000	0.000
L8 76.25-75.00	75.62	1.267	0.00	1.3808		С	0.000	25.461	1	100.00	0.000	3.502
	75.02	1.207	0.00	1.3606	3.415	Ā	0.000	3.415	3.415	100.00	0.000	0.712
i	- 1	- 1		1	1	В	0.000	3.415	ŀ	100.00	0.000	0.000
L9 75.00-72.15	73.57	1.257	0.00	1.3762	7 000	Ċ	0.000	3.415	- 1	100.00	0.000	0.658
1 - 1 - 1 - 1	. 3.01	1.20/	0.00	1.3702	7.888	A	0.000	7.888	7.888	100.00	0.000	1.620
]	j		ļ		В	0.000	7.888	ļ	100.00	0.000	0.000
L10 72.15-	56.82	1.168	0.00	1.3342	90.708	Č	0.000	7.888		100.00	0.000	1.620
42.41	00.02		0.00	1.3342	30.708	A	0.000	90.708	90.708	100.00	0.000	17.283
1	,	1	1	- 1	ŀ	В	0.000	90.708	Į.	100.00	0.000	0.000

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Section Elevation	Z	Kz	q_z	tz	A_G	F a	A _F	A _R	A _{leg}	Leg	$C_A A_A$	$C_A A_A$
ft	ft		ksf	in	ft²	c e	ft²	ft²	ft²	%	In Face ft²	Out Face ft²
L11 42.41- 31.25	36.76	1.031	0.00	1.2663	37.294	C A B	0.000 0.000 0.000	90.708 37.294 37.294	37.294	100.00 100.00	0.000 0.000	15.85 8.15
L12 31.25- 18.75	24.93	1	0.00	1.2500	44.458	C A B	0.000	37.294 44.458	44.458	100.00 100.00 100.00	0.000 0.000 0.000	0.00 3.84 8.90
.13 18.75-0.00	9.23	1	0.00	1.2500	71.882	C A	0.000 0.000 0.000	44.458 44.458 71.882	71.882	100.00 100.00 100.00	0.000 0.000 0.000	0.00 4.09 13.35
						B C	0.000 0.000	71.882 71.882		100.00 100.00	0.000	0.00 6.13

Tower Pressure - Service

 $G_H=1.690$

Section Elevation	z	Kz	qz	A_G	F	A _F	A_R	A _{leg}	100	C 4	
Elevation					a	İ .	1 ""	\ \tag{}	Leg %	$C_A A_A$ In	$C_A A_A$
ft			1		C	1	i	1	/ "		Out
	ft		ksf	ft ²	е	ft ²	ft ²	ft ²	1	Face ft²	Face
L1 150.00-	136.00	1.499	0.01	39.582	A	0.000	39.582	39.582	100.00		ft ²
123.42		1	1		В	0.000	39.582	39.362	100.00	0.000	4.0
1040040		1.	1		C	0.000	39.582	İ	100.00	0.000	0.00
L2 123.42-	119.28	1.444	0.01	14.449	A	0.000	14,449	14,449		0.000	1.0
115.25					В	0.000	14,449	14.448	100.00	0.000	1.3
1044505		i	1		l c	0.000	14,449	[100.00	0.000	0.0
L3 115.25-	110.17	1.411	0.01	19.296	A	0.000	19.296	19.296	100.00	0.000	0.6
105.25		1	f	I	В	0.000	19.296	13.230		0.000	2.6
14405.05			ĺ	İ	l c	0.000	19.296		100.00	0.000	0.0
L4 105.25-	103.57	1.386	0.01	6.860	Α	0.000	6.860	6.860	100.00 100.00	0.000	0.7
101.90			l	1	В	0.000	6.860	0.000		0.000	0.8
15 404 00		1	1	1	C	0.000	6.860		100.00	0.000	0.00
L5 101.90-	101.57	1.379	0.01	1.354	A	0.000	1.354	1.354		0.000	0.25
101.25			!	ĺ	В	0.000	1.354	1.334	100.00	0.000	0.17
1040405	_	i	1		C	0.000	1.354		100.00	0.000	0.00
L6 101.25-	93.45	1.346	0.01	34.013	Α	0.000	34.013	24.042	100.00	0.000	0.05
85.96		l i			В	0.000	34.013	34.013	100.00	0.000	4.01
170700		1			C	0.000	34.013		100.00	0.000	0.00
L7 85.96-	81.03	1.293	0.01	23,169	A	0.000	23.169	23.169	100.00	0.000	1.18
76.25		ŀ			В	0.000	23.169	23.169	100.00	0.000	2.54
					Ċ	0.000	23.169		100.00	0.000	0.00
L8 76.25-	75.62	1.267	0.01	3.127	Ă	0.000	3.127	2.407	100.00	0.000	0.75
75.00					в	0.000	3.127	3.127	100.00	0.000	0.32
				l	čΙ	0.000	3.127		100.00	0.000	0.00
L9 75.00-	73.57	1.257	0.01	7.234	Ă	0.000	7.234	7.004	100.00	0.000	0.28
72.15		- 1	1		В	0.000		7.234	100.00	0.000	0.74
140		- 1	- 1		č l	0.000	7.234 7.234		100.00	0.000	0.00
L10 72.15-	56.82	1.168	0.01	84.095	Ă	0.000	84.095	04.00-	100.00	0.000	0.74
42.41	l				в	0.000	84.095	84.095	100.00	0.000	8.13
	ı]		- 1	čΙ	0.000	84.095	[100.00	0.000	0.00
L11 42.41-	36.76	1.031	0.01	34.812	Ă	0.000		04.045	100.00	0.000	7.14
31.25	- 1	[, 2	вI	0.000	34.812	34.812	100.00	0.000	3.88
	1	i	- 1	İ	c l	0.000	34.812	}	100.00	0.000	0.000
L12 31.25-	24.93	1	0.01	41.853	Ă	0.000	34.812		100.00	0.000	0.864
18.75					B	0.000	41.853	41.853	100.00	0.000	4.347
1	- 1	}	- 1	- 1	č	0.000	41.853	i	100.00	0.000	0.000
L13 18.75-	9.23	1	0.01	67.976	Ă	0.000	41.853	[100.00	0.000	0.968
0.00]		2.0.	57.575	B	0.000	67.976	67.976	100.00	0.000	6.521
	ŀ	1		l	Ĉ l		67.976	1	100.00	0.000	0.000
					Ų.	0.000	67.976		100.00	0.000	1.451

Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 50 deg - No ice Dead+Wind 60 deg - No ice
5	
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice Dead+Wind 150 deg - No Ice
8	
9	Dead+Wind 180 deg - No Ice
10	Dead+Wind 210 deg - No Ice
11	Dead+Wind 240 deg - No Ice
12	Dead+Wind 270 deg - No Ice Dead+Wind 300 deg - No Ice
13	
14	Dead+Wind 330 deg - No Ice Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 50 deg+lce+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 30 deg+lce+Temp
20	Dead+Wind 150 deg+lce+Temp
21	Dead+Wind 180 deg+lce+Temp
22	Dead+Wind 210 deg+lce+Temp
23	Dead+Wind 240 deg+lce+Temp
24	Dead+Wind 270 deg+lce+Temp
25	Dead+Wind 300 deg+lce+Temp
26	Dead+Wind 330 deg+lce+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service
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Maximum Member Forces

Sectio n No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	150 - 123.42	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-18.32	0.60	1.61
			Max. Mx	11	-5.61	192.70	-0.33
			Max. My	2	-5.59	-0.44	193.86
			Max. Vý	11	-15.54	192.70	-0.33
			Max. Vx	2	-15.62	-0.44	193.86
			Max. Torque	10			-2.14
L2	123.42 - 115.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-21.94	0.73	1.82
			Max. Mx	11	-7.48	374.87	-0.67
			Max. My	2	-7.46	-0.83	376.93
			Max. Vý	11	-17.29	374.87	-0.67
			Max. Vx	2	-17.36	-0.83	376.93
			Max. Torque	10		2,00	-2.15
L3	115.25 - 105.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-23.88	0.87	2.00
			Max. Mx	11	-8.84	551.22	-0.99
			Max. My	2	-8.83	-1.19	554.07
			Max. Vý	11	-18.00	551.22	-0.99
			Max. Vx	2	-18.08	-1.19	554.07
			Max. Torque	10			-2.16

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Force	Major Axis Moment	Minor Axis Moment
No.		<u></u>	tota in tipiparamen meganisasas	Comb.	<i>K</i>	kip-ft	kip-ft
L4	105.25 - 101.9	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-24.72	0.91	2.06
			Max. Mx	11	-9.47	611.94	-1.10
			Max. My	2	-9.46	-1.30	615.05
			Max. Vy	11	-18.26	611.94	-1.10
			Max. Vx	2	-18.34	-1.30	615.05
			Max. Torque	10			-2.17
L5	101.9 - 101.25	Pole	Max Tension	1	0.00	0.00	0.00
	,		Max. Compression	14	-24.89	0.92	2.07
			Max. Mx	11	-9.60	623.82	-1.12
			Max. My	2	-9.59	-1.33	626.99
			Max. Vý	11	-18.31	623.82	-1.12
			Max. Vx	2	-18.39	-1.33	626.99
			Max. Torque	10	10.00	1.00	-2.17
L6	101.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	85.96						
			Max. Compression	14	-27.81	1.09	2.28
			Max. Mx	11	-11.78	833.96	-1.48
			Max. My	2	-11.77	-1.73	838.03
			Max. Vy	11	-19.19	833.96	-1.48
			Max. Vx	2	-19.27	-1.73	838.03
L7	05.00	0.1	Max. Torque	10	_		-2.19
L7	85.96 - 76.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-32.63	1.29	2.55
			Max. Mx	11	-15.44	1106.89	-1.92
			Max. My	2	-15.43	-2.22	1112.07
			Max. Vy	11	-20.34	1106.89	-1.92
			Max. Vx	2	-20.42	-2.22	1112.07
			Max. Torque	10			-2.21
L8	76.25 <i>-</i> 75	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-33.00	1.31	2.57
			Max. Mx	11	-15.73	1132.38	-1.96
			Max. My	2	-15.72	-2.26	1137.66
			Max. Vý	11	-20.45	1132.38	-1.96
			Max. Vx	2	-20.53	-2.26	1137.66
			Max. Torque	10			-2.21
L9	75 - 72.15	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-34.08	1.33	2.65
			Max. Mx	11	-16.54	1191.25	-2.05
			Max. My	2	-16.53	-2.36	1196.77
			Max. Vý	11	-20.78	1191.25	-2.05
			Max. Vx	2	-20.86	-2.36	1196.77
			Max. Torque	10		2.00	-2.22
L10	72.15 - 42.41	Pole	Max Tension	1	0.00	0.00	0.00
	1m.T)		Max. Compression	14	12 51	4.04	2.05
			Max. Mx	11	-42.51 33.44	1.81	3.05
			Max. My		-23.14	1725.98	-2.81
			Max. Vv	2	-23.14	-3.20	1733.52
			Max. Vx	11	-22.79	1725.98	-2.81
				2	-22.87	-3.20	1733.52
L11	42.41 -	Pole	Max. Torque	10	0.00		-2.26
L11	31.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-49.43	2.13	3.31
			Max. Mx	11	-28.55	2108.96	-3.32
			Max. My	2	-28.54	-3.76	2117.84
			Max. Vy	11	-24.01	2108.96	-3.32
			Max. Vx	2	-24.09	-3.76	2117.84
		_	Max. Torque	10			-2.30
L12	31.25 - 18.75	Pole	Max Tension	1	0.00	0.00	0.00
	-		Max. Compression	14	-53.69	2.39	3.53
			Max. Mx	11	-31.92	2413.63	-3.70
			Max. My	2	-31.92	-4.18	2423.54
			Max. Vý	11	-24.77	2413.63	-3.70
			Max. Vx	2	-24.85	-4.18	2423.54

Sectio n No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
			Max. Torque	10	* • • • · · · · · · · · · · · · · ·		-2.34
L13	18.75 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-59.90	2.79	3.87
			Max. Mx	11	-36.77	2887.86	-4.27
			Max. My	2	-36.77	-4.80	2899.27
			Max. Vy	11	-25.85	2887.86	-4.27
			Max. Vx	2	-25.93	-4.80	2899.27
			Max. Torque	10			-2.39

			Maximun	n Reactions	
Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	15	59.90	-0.01	7.25
	Max. H _x	11	36.78	25.83	-0.03
	Max. H _z	2	36.78	-0.03	25.91
	Max. M _x	2	2899.27	-0.03	25.91
	Max. M _z	5	2887.27	-25.83	0.03
	Max. Torsion	4	2.38	-22.39	12.98
	Min. Vert	1	36.78	0.00	0.00
	Min. H _x	5	36.78	-25.83	0.03
	Min. H _z	8	36.78	0.03	-25.91
	Min. M _x	8	-2897.60	0.03	-25.91
	Min. M _z	11	-2887.86	25.83	-0.03
	Min. Torsion	10	-2.39	22.39	-12.98

Load Combination	Vertical	Shear _x	Shear₂	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	36.78	0.00	0.00	-0.80	0.28	0.00
Dead+Wind 0 deg - No Ice	36.78	0.03	-25.91	-2899.27	-4.80	-0.83
Dead+Wind 30 deg - No Ice	36.78	12.95	-22.46	-2513.48	-1447.87	-1.85
Dead+Wind 60 deg - No Ice	36.78	22.39	-12.98	-1454.44	-2502.93	-2.38
Dead+Wind 90 deg - No Ice	36.78	25.83	-0.03	-5.90	-2887.27	-2.27
Dead+Wind 120 deg - No Ice	36.78	22.36	12.92	1444.02	-2497.87	-1.56
Dead+Wind 150 deg - No Ice	36.78	12.89	22.42	2506.77	-1439.08	-0.42
Dead+Wind 180 deg - No Ice	36.78	-0.03	25.91	2897.60	5.37	0.83
Dead+Wind 210 deg - No Ice	36.78	-12.95	22.46	2511.82	1448.43	1.86
Dead+Wind 240 deg - No Ice	36.78	-22.39	12.98	1452.81	2503.50	2.39
Dead+Wind 270 deg - No Ice	36.78	-25.83	0.03	4.27	2887.86	2.28
Dead+Wind 300 deg - No Ice	36.78	-22.36	-12.92	-1445.67	2498.47	1.55
Dead+Wind 330 deg - No Ice	36.78	-12.89	-22.42	-2508.44	1439.67	0.41
Dead+Ice+Temp	59.90	-0.00	-0.00	-3.87	2.79	-0.00
Dead+Wind 0	59.90	0.01	-7.25	-870.49	1.74	-0.23
deg+lce+Temp					,	0.20
Dead+Wind 30	59.90	3.61	-6.28	-754.97	-428.89	-0.50
deg+lce+Temp					,20.00	0.00
Dead+Wind 60	59.90	6.25	-3.63	-438.22	-743.84	-0.64
deg+lce+Temp						0.01
Dead+Wind 90	59.90	7.22	-0.01	-5.13	-858.70	-0.61
deg+lce+Temp					000.10	0.01
Dead+Wind 120	59.90	6.25	3.62	428.27	-742.70	-0.41
leg+lce+Temp					7 12.70	0.41
Dead+Wind 150	59.90	3.60	6.27	745.85	-426.93	-0.10
leg+lce+Temp					120.00	0.10
Dead+Wind 180	59.90	-0.01	7.25	862.50	4.01	0.23
leg+lce+Temp		Ţ.J.	0	332.00	7.01	0.20
Dead+Wind 210	59.90	-3.61	6.28	746.98	434.64	0.50

Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shear₂	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	Κ	K	K	kip-ft	kip-ft	kip-ft
deg+lce+Temp						
Dead+Wind 240	59.90	-6.25	3.63	430.24	749.59	0.64
deg+lce+Temp						
Dead+Wind 270	59.90	-7.22	0.01	-2.86	864.45	0.61
deg+lce+Temp						
Dead+Wind 300	59.90	-6.25	-3.62	-436.26	748.45	0.41
deg+lce+Temp						
Dead+Wind 330	59.90	-3.60	-6.27	-753.83	432.68	0.10
deg+lce+Temp						
Dead+Wind 0 deg - Service	36.78	0.01	-8.97	-1005.73	-1.47	-0.29
Dead+Wind 30 deg - Service	36.78	4.48	-7.77	-871.99	-501.78	-0.65
Dead+Wind 60 deg - Service	36.78	7.75	-4.49	-504.82	-867.57	-0.84
Dead+Wind 90 deg - Service	36.78	8.94	-0.01	-2.61	-1000.81	-0.80
Dead+Wind 120 deg -	36.78	7.74	4.47	500.08	-865.81	-0.55
Service						
Dead+Wind 150 deg -	36.78	4.46	7.76	868.54	-498.73	-0.15
Service						
Dead+Wind 180 deg -	36.78	-0.01	8.97	1004.04	2.06	0.29
Service						
Dead+Wind 210 deg -	36.78	-4.48	7.77	870.30	502.37	0.65
Service						
Dead+Wind 240 deg -	36.78	-7.75	4.49	503.13	868.16	0.84
Service						
Dead+Wind 270 deg -	36.78	-8.94	0.01	0.92	1001.40	0.80
Service						
Dead+Wind 300 deg -	36.78	-7.74	-4.47	-501.77	866.40	0.55
Service						
Dead+Wind 330 deg - Service	36.78	-4.46	-7.76	-870.23	499.32	0.15

Solution	Summary
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Comb. K <th>N</th> <th>Sun</th> <th>n of Applied Force</th> <th>9S</th> <th>the state of the s</th> <th>Sum of Reactio</th> <th>ns</th> <th>in anne men an anna an an an an an an an an an an</th>	N	Sun	n of Applied Force	9S	the state of the s	Sum of Reactio	ns	in anne men an anna an an an an an an an an an an
1 0.00 -36.78 0.00 0.00 36.78 0.00 0.0009 2 0.03 -36.78 -25.91 -0.03 36.78 22.46 0.0009 3 12.95 -36.78 -22.46 -12.95 36.78 22.46 0.0009 4 22.39 -36.78 -12.98 -22.39 36.78 12.98 0.003 5 25.83 -36.78 -0.03 -25.83 36.78 0.03 0.0009 6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.0009 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 25.91 0.03 36.78 -22.46 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 <th>Load</th> <th>PX</th> <th>PY</th> <th>PZ</th> <th>PX</th> <th>PY</th> <th>PZ</th> <th>% Error</th>	Load	PX	PY	PZ	PX	PY	PZ	% Error
2 0.03 -36.78 -25.91 -0.03 36.78 25.91 0.0009 3 12.95 -36.78 -22.46 -12.95 36.78 22.46 0.0009 4 22.39 -36.78 -12.98 -22.39 36.78 12.98 0.0009 5 25.83 -36.78 -0.03 -25.83 36.78 12.92 0.0009 6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.0009 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 22.42 -12.89 36.78 -22.42 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.29 23.6 36.78 12.98 0.0009 <	Comb.	K	K	<i>K</i>		K		
3 12.95 -36.78 -22.46 -12.95 36.78 22.46 0.0009 4 22.39 -36.78 -12.98 -22.39 36.78 12.98 0.0009 5 25.83 -36.78 -0.03 -25.83 36.78 0.03 0.0009 6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.0009 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 22.42 -12.89 36.78 -22.42 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.03 25.83 36.78 12.92 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009	1		-36.78	0.00	0.00	36.78	0.00	0.000%
4 22.39 -36.78 -12.98 -22.39 36.78 12.98 0.000 5 25.83 -36.78 -0.03 -25.83 36.78 0.03 0.000 6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.000 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.000 8 -0.03 -36.78 22.46 12.95 36.78 -25.91 0.000 9 -12.95 -36.78 22.46 12.95 36.78 -25.91 0.000 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.000 11 -25.83 -36.78 12.92 22.36 36.78 12.92 0.000 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.000 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.000 14<		0.03	-36.78	-25.91	-0.03	36.78	25.91	0.000%
5 25.83 -36.78 -0.03 -25.83 36.78 0.03 0.0009 6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.0009 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 22.46 12.95 36.78 -25.91 0.000 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 12.98 22.39 36.78 -12.98 0.0009 12 -22.36 -36.78 12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.00 1	3		-36.78	-22.46	-12.95	36.78	22.46	0.000%
6 22.36 -36.78 12.92 -22.36 36.78 -12.92 0.0009 7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 25.91 0.03 36.78 -25.91 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.03 25.83 36.78 -12.92 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.00 1.00 0.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1			-36.78	-12.98	-22.39	36.78	12.98	0.000%
7 12.89 -36.78 22.42 -12.89 36.78 -22.42 0.0009 8 -0.03 -36.78 25.91 0.003 36.78 -25.91 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.03 25.83 36.78 -12.98 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.00 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.000 16 3.61 -59.90 -3.63 -6.25 59.90 3.63 0.0009 17 <td></td> <td></td> <td>-36.78</td> <td>-0.03</td> <td>-25.83</td> <td>36.78</td> <td>0.03</td> <td>0.000%</td>			-36.78	-0.03	-25.83	36.78	0.03	0.000%
8 -0.03 -36.78 25.91 0.03 36.78 -25.91 0.0009 9 -12.95 -36.78 22.46 12.95 36.78 -22.46 0.0009 10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.03 25.83 36.78 -0.03 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.0009 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -3.63 -6.25 59.90 3.63 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18			-36.78	12.92	-22.36	36.78	-12.92	0.000%
9				22.42	-12.89	36.78	-22.42	0.000%
10 -22.39 -36.78 12.98 22.39 36.78 -12.98 0.0009 11 -25.83 -36.78 0.03 25.83 36.78 -0.03 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.00 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 20 3.60 -59.90 3.62 -6.25 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009			-36.78	25.91	0.03	36.78	-25.91	0.000%
11 -25.83 -36.78 0.03 25.83 36.78 -0.03 0.0009 12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.009 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 20 3.60 -59.90 3.62 -6.25 59.90 -3.62 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 3.63 6.25 59.90 -3.63 0.0009			-36.78	22.46	12.95	36.78	-22.46	0.000%
12 -22.36 -36.78 -12.92 22.36 36.78 12.92 0.0009 13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.009 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 3.63 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -3.63 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 3.62 -6.25 59.90 -3.62 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 3.63 6.25 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009		-22.39	-36.78	12.98	22.39	36.78	-12.98	0.000%
13 -12.89 -36.78 -22.42 12.89 36.78 22.42 0.0009 14 0.00 -59.90 0.00 0.00 59.90 0.00 0.009 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 3.63 6.25 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009				0.03		36.78	-0.03	0.000%
14 0.00 -59.90 0.00 0.00 59.90 0.00 0.0009 15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22		-22.36	-36.78	-12.92	22.36	36.78	12.92	0.000%
15 0.01 -59.90 -7.25 -0.01 59.90 7.25 0.0009 16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.		-12.89	-36.78	-22.42	12.89	36.78	22.42	0.000%
16 3.61 -59.90 -6.28 -3.61 59.90 6.28 0.0009 17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009		0.00	-59.90	0.00	0.00	59.90	0.00	0.000%
17 6.25 -59.90 -3.63 -6.25 59.90 3.63 0.0009 18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -3.63 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 7.77 0.0009			-59.90		-0.01	59.90	7.25	0.000%
18 7.22 -59.90 -0.01 -7.22 59.90 0.01 0.0009 19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -6.28 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.4		3.61	-59.90	-6.28	-3.61	59.90	6.28	0.000%
19 6.25 -59.90 3.62 -6.25 59.90 -3.62 0.0009 20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -6.28 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90	-3.63		59.90	3.63	0.000%
20 3.60 -59.90 6.27 -3.60 59.90 -6.27 0.0009 21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -6.28 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90			59.90	0.01	0.000%
21 -0.01 -59.90 7.25 0.01 59.90 -7.25 0.0009 22 -3.61 -59.90 6.28 3.61 59.90 -6.28 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90		-6.25	59.90	-3.62	0.000%
22 -3.61 -59.90 6.28 3.61 59.90 -6.28 0.0009 23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90		-3.60	59.90	-6.27	0.000%
23 -6.25 -59.90 3.63 6.25 59.90 -3.63 0.0009 24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90	7.25	0.01	59.90	-7.25	0.000%
24 -7.22 -59.90 0.01 7.22 59.90 -0.01 0.0009 25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009						59.90	-6.28	0.000%
25 -6.25 -59.90 -3.62 6.25 59.90 3.62 0.0009 26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009					6.25	59.90	-3.63	0.000%
26 -3.60 -59.90 -6.27 3.60 59.90 6.27 0.0009 27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009			-59.90	0.01		59.90	-0.01	0.000%
27 0.01 -36.78 -8.97 -0.01 36.78 8.97 0.0009 28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009					6.25	59.90	3.62	0.000%
28 4.48 -36.78 -7.77 -4.48 36.78 7.77 0.0009 29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009				-6.27	3.60	59.90	6.27	0.000%
29 7.75 -36.78 -4.49 -7.75 36.78 4.49 0.0009				-8.97	-0.01	36.78	8.97	0.000%
				-7.77	-4.48	36.78	7.77	0.000%
30 8.94 -36.78 -0.01 -8.94 36.78 0.01 0.000				· · · · •			4.49	0.000%
	30	8.94	-36.78	-0.01	-8.94	36.78	0.01	0.000%
31 7.74 -36.78 4.47 -7.74 36.78 -4.47 0.0009	31	7.74	-36.78	4.47	-7.74	36.78	-4.47	0.000%

The second of th	Sur	n of Applied Force)S	an managarina ang katalong di Baling Ang katalong	Sum of Reaction		estri e di en redecimentalità del presidenti i di petri
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K K	Κ	K	K	K	
32	4.46	-36.78	7.76	-4.46	36.78	-7.76	0.000%
33	-0.01	-36.78	8.97	0.01	36.78	-8.97	0.000%
34	-4.48	-36.78	7.77	4.48	36.78	-7.77	0.000%
35	-7.75	-36.78	4.49	7.75	36.78	-4.49	0.000%
36	-8.94	-36.78	0.01	8.94	36.78	-0.01	0.000%
37	-7.74	-36.78	-4.47	7.74	36.78	4.47	0.000%
38	-4.46	-36.78	-7.76	4.46	36.78	7.76	0.000%

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	_Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00005624
3	Yes	6	0.0000001	0.00010859
4	Yes	6	0.0000001	0.00011754
5	Yes	5	0.0000001	0.00019467
6	Yes	6	0.0000001	0.00010860
7	Yes	6	0.00000001	0.00011260
8	Yes	5	0.00000001	0.00008226
9	Yes	6	0.00000001	0.00011640
10	Yes	6	0.00000001	0.00010760
11	Yes	5	0.00000001	0.00016803
12	Yes	6	0.00000001	0.00011511
13	Yes	6	0.0000001	0.00011096
14	Yes	4	0.0000001	0.00011724
15	Yes	6	0.00000001	0.00015600
16	Yes	6	0.0000001	0.00022561
17	Yes	6	0.0000001	0.00023103
18	Yes	6	0.0000001	0.00015412
19	Yes	6	0.0000001	0.00022077
20	Yes	6	0.0000001	0.00022349
21	Yes	6	0.0000001	0.00015384
22	Yes	6	0.0000001	0.00022892
23	Yes	6	0.0000001	0.00022306
24	Yes	6	0.0000001	0.00015523
25	Yes	6	0.0000001	0.00023067
26	Yes	6	0.0000001	0.00022837
27	Yes	4	0.0000001	0.00034387
28	Yes	5	0.0000001	0.00021835
29	Yes	5	0.0000001	0.00025331
30	Yes	4	0.0000001	0.00082439
31	Yes	5	0.00000001	0.00021642
32	Yes	5	0.0000001	0.00023159
33	Yes	4	0.0000001	0.00037501
34	Yes	5	0.0000001	0.00024808
35	Yes	5	0.0000001	0.00021436
36	Yes	4	0.0000001	0.00078710
37	Yes	5	0.00000001	0.00024281
38	Yes	5	0.0000001	0.00022641

Maximum Tower Deflections - Service Wind

Section No.	Elevation	Elevation Horz. Deflection		Tilt	Twist
	ft	in	Comb.	•	•
L1	150 - 123.42	41.41	28	2.71	0.01
L2	126.59 - 115.25	28.74	28	2.34	0.01
L3	115.25 - 105.25	23.52	28	2.02	0.01
L4	105.25 - 101.9	19.56	28	1.76	0.00

Section No.	Elevation	Horz. Deflection	Gov. Load	Tilt	Twist
	ft	in	Comb.	o ·	۰
L5	101.9 - 101.25	18.34	28	1.70	0.00
L6	101.25 - 85.96	18.11	28	1.69	0.00
L7	90.04 - 76.25	14.38	28	1.48	0.00
L8	76.25 - 75	10.39	28	1.26	0.00
L9	75 - 72.15	10.06	28	1.24	0.00
L10	72.15 - 42.41	9.34	28	1.19	0.00
L11	47.58 - 31.25	4.22	28	0.80	0.00
L12	31.25 - 18.75	1.84	28	0.56	0.00
L13	18.75 - 0	0.66	28	0.34	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ππ		Comb.	in	0	•	ft
152.00	1900MHz RRH (65MHz)	28	41.41	2.71	0.01	9490
137.00	7770.00 w/ Mount Pipe	28	34.16	2.54	0.01	3649
127.00	Platform Mount [LP 712-1]	28	28.94	2.35		
117.00	T-Arm Mount [TA 601-3]	28	24.27		0.01	2112
75.00				2.07	0.01	1926
75.00	Side Arm Mount [SO 701-1]	28	10.06	1.24	0.00	3287

Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load	Tilt	Twist
	ft	in	Comb.	0	0
L1	150 - 123.42	118.96	2	7.80	0.04
L2	126.59 - 115.25	82.65	2	6.72	0.02
L3	115.25 - 105.25	67.66	2	5.80	0.02
L4	105.25 - 101.9	56.28	3	5.08	0.02
L5	101.9 - 101.25	52.79	3	4.90	0.01
L6	101.25 - 85.96	52.12	3	4.87	0.01
L7	90.04 - 76.25	41.41	3	4.27	0.01
L8	76.25 - 75	29.92	3	3.63	0.01
L9	75 - 72.15	28.98	3	3.56	0.01
L10	72,15 - 42,41	26.89	3	3.44	0.01
L11	47.58 - 31.25	12.16	3	2.32	0.00
L12	31,25 - 18,75	5.29	š	1.61	
L13	18.75 - 0	1.91	3	0.99	0.00 0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	o	•	Curvature fi
152.00	1900MHz RRH (65MHz)	2	118.96	7.80	0.04	3421
137.00	7770.00 w/ Mount Pipe	2	98.20	7.31	0.03	1314
127.00	Platform Mount [LP 712-1]	2	83.23	6.75	0.02	757
117.00	T-Arm Mount [TA 601-3]	2	69.83	5.95	0.02	685
75.00	Side Arm Mount [SO 701-1]	3	28.98	3.56	0.02	1151

Compression Checks

			Pole	Desig	n Dat	а				
Section No.	Elevation	en en verta intra de la transposita de sporte de la compansión de compansión de la compansi	L	Lu	Kl/r	Fa	A	Actual P	Allow. Pa	Ratio P
	ft		ft	ft		ksi	in²	K	ĸ	Pa
L1	150 - 123.42 (1)	TP20.74x15x0.1875	26.58	0.00	0.0	39.00	11.8239	-5.59	461.13	0.012
L2	123.42 - 115.25 (2)	TP22.0918x19.6804x0.25	11.34	0.00	0.0	39.00	17.3314	-7.46	675.93	0.011
L3	115.25 - ´ 105.25 (3)	TP24.2182x22.0918x0.384	10.00	0.00	0.0	33.37	29.0829	-8.83	970.38	0.009
L4		TP24.9305x24.2182x0.577	3.35	0.00	0.0	23.98	44.6274	-9.45	1070.25	0.009
L5		TP25.0687x24.9305x0.605	0.65	0.00	0.0	25.88	47.0050	-9.59	1216.68	0.008
L6	101.25 - 85.96 (6)	TP28.32x25.0687x0.5671	15.29	0.00	0.0	26.00	48.3921	-11.77	1258.39	0.009
L7	85.96 - 76.25 (7)	TP29.8904x26.3182x0.602	13.79	0.00	0.0	26.08	55.9700	-15.43	1459.81	0.011
L8		TP30.1567x29.8904x0.599	1.25	0.00	0.0	26.09	56.1922	-15.71	1466.28	0.011
L9	75 - 72.15 (9)	TP30.7639x30.1567x0.700	2.85	0.00	0.0	26.12	66.8416	-16.52	1745.77	0.009
L10	72.15 - 42.41 (10)	TP37.1x30.7639x0.6479	29.74	0.00	0.0	27.43	72.6918	-23.13	1993.65	0.012
L11	42.41 - 31.25 (11)	TP38.849x34.7028x0.5358	16.33	0.00	0.0	34.58	60.3389	-25.67	2086.40	0.012
L12	31.25 - 18.75 (12)	TP41.5094x38.849x0.5216	12.50	0.00	0.0	34.68	65.6568	-30.23	2276.98	0.013
L13	18.75 - 0 (13)	TP45.5x41.5094x0.4491	18.75	0.00	0.0	37.50	58.5330	-31.94	2194.99	0.015

		Pole	Ben	Pole Bending Design Data											
Section No.	Elevation ft	Size	Actual M _x kip-ft	Actual f _{bx} ksi	Allow. F _{bx} ksi	Ratio f _{bx} F _{bx}	Actual M _y kip-ft	Actual f _{by} ksi	Allow. F _{by} ksi	Ratio f _{by} F _{by}					
L1	150 - 123.42 (1)	TP20.74x15x0.1875	193.94	40.21	39.00	1.031	0.00	0.00	39.00	0.000					
L2	123.42 - 115.25 (2)	TP22.0918x19.6804x0.25	377.13	48.62	39.00	1.247	0.00	0.00	39.00	0.000					
L3	115.25 - 105.25 (3)	TP24.2182x22.0918x0.38 45	554.39	39.21	33.37	1.175	0.00	0.00	33.37	0.000					
L4	105.25 - 101.9 (4)	TP24.9305x24.2182x0.57	615.42	27.97	23.98	1.166	0.00	0.00	23.98	0.000					
L5	101.9 - 101.25 (5)	TP25.0687x24.9305x0.60 54	627.36	26.98	25.88	1.042	0.00	0.00	25.88	0.000					
L6	101.25 - 85.96 (6)	TP28.32x25.0687x0.5671	838.53	31.75	26.00	1.221	0.00	0.00	26.00	0.000					
L7	85.96 - 76.25 (7)	TP29.8904x26.3182x0.60	1112.7 3	33.43	26.08	1.282	0.00	0.00	26.08	0.000					
L8	76.25 - 75 (8)	TP30.1567x29.8904x0.59	1138.3 4	33.74	26.09	1.293	0.00	0.00	26.09	0.000					
L9	75 - 72.15 (9)	TP30.7639x30.1567x0.70 05	1197.4 7	29.42	26.12	1.127	0.00	0.00	26.12	0.000					
L10	72.15 - 42.41 (10)	TP37.1x30.7639x0.6479	1734.4 7	33.16	27.43	1.209	0.00	0.00	27.43	0.000					
L11	42.41 - 31.25 (11)	TP38.849x34.7028x0.535	1854.0 7	42.42	34.58	1.227	0.00	0.00	34.58	0.000					
L12	31.25 - 18.75 (12)	TP41.5094x38.849x0.521	2270.6 8	42.63	34.68	1.229	0.00	0.00	34.68	0.000					
L13	18.75 - 0 (13)	TP45.5x41.5094x0.4491	2424.7 8	49.21	37.50	1.312	0.00	0.00	37.50	0.000					

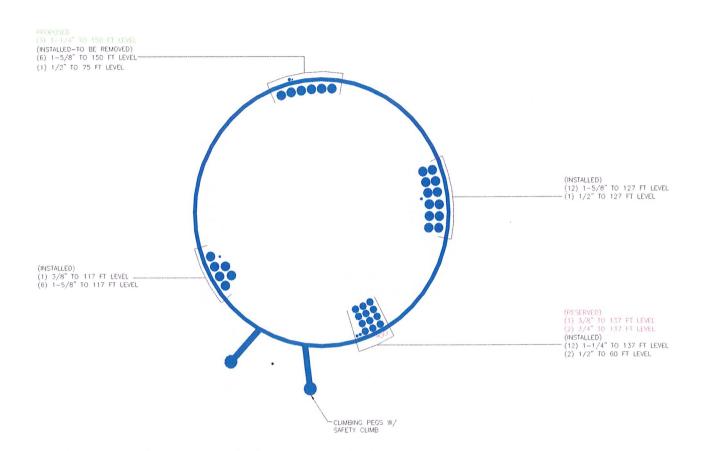
	ran ara di kirintan ya wa kana angista a ta di Garandia ya sa sa	Pole Shear Design Data										
Section No.	Elevation ft	Size	Actual V K	Actual f _v ksi	Allow. F _v ksi	Ratio f _v F _v	Actual T kip-ft	Actual f _{vt} ksi	Allow. F _{vt} ksi	Ratio f _{vt}		
L1	150 - 123.42 (1)	TP20.74x15x0.1875	15.63	1.32	26.00	0.102	1.71	0.17	26.00	0.007		
L2	123.42 - 115.25 (2)	TP22.0918x19.6804x0.25	17.38	1.00	26.00	0.077	1.68	0.11	26.00	0.004		
L3	115.25 - 105.25 (3)	TP24.2182x22.0918x0.38 45	18.09	0.62	22.24	0.056	1.69	0.06	22.24	0.003		
L4	105.25 - 1 101.9 (4)	TP24.9305x24.2182x0.57 74	18.35	0.41	15.99	0.051	1.70	0.04	15.99	0.002		
L5	101.9 - 101.25 (5)	TP25.0687x24.9305x0.60 54	18.40	0.39	17.26	0.045	1.70	0.04	17.26	0.002		
L6	101.25 - 85.96 (6)	TP28.32x25.0687x0.5671	19.28	0.40	17.34	0.046	1.71	0.03	17.34	0.002		
L7	85.96 - 76.25 (7)	TP29.8904x26.3182x0.60 21	20.44	0.37	17.39	0.042	1.73	0.02	17.39	0.001		
L8	76.25 - 75 (8)	TP30.1567x29.8904x0.59	20.54	0.37	17.40	0.042	1.73	0.02	17.40	0.001		
L9	75 - 72.15 (9)	TP30.7639x30.1567x0.70 05	20.88	0.31	17.41	0.036	1.71	0.02	17.41	0.001		
L10	72.15 - 42.41 (10)	TP37.1x30.7639x0.6479	22.88	0.31	18.28	0.034	1.76	0.02	18.28	0.001		
L11	42.41 - 31.25 (11)	TP38.849x34.7028x0.535 8	23.46	0.39	23.05	0.033	1.78	0.02	23.05	0.001		
L12	31.25 - 18.75 (12)	TP41.5094x38.849x0.521 6	24.54	0.37	23.12	0.032	1.81	0.02	23.12	0.001		
L13	18.75 - Ó (13)	TP45.5x41.5094x0.4491	24.92	0.43	25.00	0.034	1.82	0.02	25.00	0.001		

			Pol	le Inter	action	Desig	n Data		
Section No.	Elevation ft	Ratio P P _a	Ratio f _{bx} F _{bx}	Ratio f _{by}	Ratio f _v	Ratio f _{vt}	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	150 - 123.42 (1)	0.012	1.031	F _{by} 0.000	0.102	0.007	1.046	1.333	H1-3+VT 🗸
L2	123.42 - 115.25 (2)	0.011	1.247	0.000	0.077	0.004	1.260	1.333	H1-3+VT 🗸
L3	115.25 - 105.25 (3)	0.009	1.175	0.000	0.056	0.003	1.185	1.333	H1-3+VT 🗸
L4	105.25 - 101.9 (4)	0.009	1.166	0.000	0.051	0.002	1.176	1.333	H1-3+VT 🗸
L5	101.9 - 101.25 (5)	0.008	1.042	0.000	0.045	0.002	1.051	1.333	H1-3+VT 🗸
L6	101.25 - 85.96 (6)	0.009	1.221	0.000	0.046	0.002	1.231	1.333	H1-3+VT 🗸
L7	85.96 - 76.25 (7)	0.011	1.282	0.000	0.042	0.001	1.293	1.333	H1-3+VT 🗸
L8	76.25 - 75 (8)	0.011	1.293	0.000	0.042	0.001	1.304	1.333	H1-3+VT 🖊
L9	75 - 72.15 (9)	0.009	1.127	0.000	0.036	0.001	1.136	1.333	H1-3+VT 🗸
L10	72.15 - 42.41 (10)	0.012	1.209	0.000	0.034	0.001	1.221	1.333	H1-3+VT 🗸
L11	42.41 - 31.25 (11)	0.012	1.227	0.000	0.033	0.001	1.239	1.333	H1-3+VT 🗸
L12	31.25 - 18.75 (12)	0.013	1.229	0.000	0.032	0.001	1.243	1.333	H1-3+VT 🗸
L13	18.75 - 0 (13)	0.015	1.312	0.000	0.034	0.001	1.327	1.333	H1-3+VT 🗸

Section	Elevation	Ratio	Ratio	Ratio	Ratio	Ratio	Comb.	Allow.	Criteria
No.	ft				<u>f_v</u>	- t _{vt}	Stress Ratio	Stress Ratio	
			, bx	ГБУ			1		

	Section Capacity Table										
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail			
L1	150 - 123.42	Pole	TP20.74x15x0.1875	1	-5.59	614.69	78.5	Pass			
L2	123.42 - 115.25	Pole	TP22.0918x19.6804x0.25	2	-7.46	901.01	94.5	Pass			
L3	115.25 - 105.25	Pole	TP24.2182x22.0918x0.3845	3	-8.83	1293.52	88.9	Pass			
L4	105.25 - 101.9	Pole	TP24.9305x24.2182x0.5774	4	-9.45	1426.64	88.2	Pass			
L5	101.9 - 101.25	Pole	TP25.0687x24.9305x0.6054	5	-9.59	1621.83	78.8	Pass			
L6	101.25 - 85.96	Pole	TP28.32x25.0687x0.5671	6	-11.77	1677.43	92.4	Pass			
L7	85.96 - 76.25	Pole	TP29.8904x26.3182x0.6021	7	-15.43	1945.93	97.0	Pass			
L8	76.25 - 75	Pole	TP30.1567x29.8904x0.599	8	-15.71	1954.55	97.8	Pass			
L9	75 - 72.15	Pole	TP30.7639x30.1567x0.7005	9	-16.52	2327.11	85.3	Pass			
L10	72.15 - 42.41	Pole	TP37.1x30.7639x0.6479	10	-23.13	2657.54	91.6	Pass			
L11	42.41 - 31.25	Pole	TP38.849x34.7028x0.5358	11	-25.67	2781.17	93.0	Pass			
L12	31.25 - 18.75	Pole	TP41.5094x38.849x0.5216	12	-30.23	3035.21	93.2	Pass			
L13	18.75 - 0	Pole	TP45.5x41.5094x0.4491	13	-31.94	2925.92	99.6	Pass			
							Summary				
						Pole (L13)	99.6	Pass			
						RATING =	99.6	Pass			

APPENDIX B BASE LEVEL DRAWING



APPENDIX C

ADDITIONAL CALCULATIONS

 $Program\ Version\ 6.0.3.0\ -\ 12/7/2011\ File: T:/375_Crown_Castle/2012/37512-1027\ BU\ 876362/37512-1027\ BP\ R2\ -\ WO512743\ BU\ 876362/Aero/37512-1027\ Reinforced\ -\ Aero\ -\ Check.eri$

Program Version 6.0.3.0 - 12/7/2011 File:T:/375_Crown_Castle/2012/37512-1027 BU 876362/37512-1027 BP R2 - WO512743 BU 876362/Aero/37512-1027 Reinforced - Aero - Check.eri

0.1875 3.17 1.0 4 123.4 ft 22.0918 0.2500 9.0 18 0.3845 10.00 0.9 48 43.ReinsBSBTanks5.61 ksi 105.3 ft 0.65.35 8 101.9 ft 8 Reinf 25.0687 0.5671 15.29 2.4 18 4.08 Reinf 43.34 ksi 86.0 ft 13.79 26.3182 Reinf 43e46f k83.47 ksi 0.6021 2.5 9 **ZSE8904** 30.7889567 76.3 ft 0.6 0.2 2.851.25 18 9 72.2 ft 30 Reinf 43.53 ksi 0.6479 29.74 5.17 6.9 18 Reinf 45.71 ksi 42.4 ft 38.8490 0.5358 3.4 18 Reinf 57.63 ksi 31.3 ft 41.5094 12.50 2.8 12 18 18.8 ft Reinf 62.50 ksReinf 57.80 45.5000 0.4491 3.9 13 18 0.0 ft 26.0 Number of Sides Socket Length Thickness (in) Top Dia (in) Bot Dia (in) Weight (K)

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
1900MHz RRH (65MHz)	152	7770.00 w/ Mount Pipe	137
300 EXTERNAL NOTCH FILTER	152	7770.00 w/ Mount Pipe	137
BOOMHZ RRH	152	(2) LGP21901	137
(3) ACU-A20-N	152	(2) LGP21901	137
APXVSPP18-C-A20 w/ Mount Pipe	152	(2) LGP21901	137
1900MHz RRH (65MHz)	152	(2) DD1900 FULL BAND w/850	137
300 EXTERNAL NOTCH FILTER	152	BY-PASS MASTHEAD	
BOOMHZ RRH	152	(2) DD1900 FULL BAND w/850	137
(3) ACU-A20-N	152	BÝ-PASS MASTHEAD	137
APXVSPP18-C-A20 w/ Mount Pipe	152	(2) DD1900 FULL BAND w/850 BY-PASS MASTHEAD	137
1900MHz RRH (65MHz)	152	BXA-70063-4CF-EDIN-X w/ Mount	127
800 EXTERNAL NOTCH FILTER	152	Pipe	1
800MHZ RRH	152	BXA-171063-12BF w/ Mount Pipe	127
(3) ACU-A20-N	152	BXA-70063-4CF-EDIN-X w/ Mount	127
APXVSPP18-C-A20 w/ Mount Pipe	152	Pipe	
Platform Mount [LP 602-1]	152	Platform Mount [LP 712-1]	127
8-ft Ladder	152	GPS_A	127
Platform Mount [LP 712-1]	137	(2) APL866513-42T0 w/ Mount Pipe	127
Collar Mount (MTC3335)	137	(2) APL866513-42T0 w/ Mount Pipe	127
(2) SBNH-1D6565C w/ Mount Pipe	137	(2) APL866513-42T0 w/ Mount Pipe	127
(2) SBNH-1D6565C w/ Mount Pipe	137	(2) FD9R6004/2C-3L	127
(2) AM-X-CD-16-65-00T-RET w/ Mount	137	(2) FD9R6004/2C-3L	127
Pipe		(2) FD9R6004/2C-3L	127
(2) DTMABP7819VG12A	137	BXA-171063-12BF w/ Mount Pipe	127
(2) DTMABP7819VG12A	137	BXA-70063-4CF-EDIN-X w/ Mount	127
(2) DTMABP7819VG12A	137	Pipe	
7020.00	137	BXA-171063-12BF w/ Mount Pipe	127
7020.00	137	HBX-6516DS-VTM w/ Mount Pipe	117
7020.00	137	T-Arm Mount [TA 601-3]	117
RRUS-11	137	HBX-6516DS-VTM w/ Mount Pipe	117
RRUS-11	137	HBX-6516DS-VTM w/ Mount Pipe	117
RRUS-11	137	OG-860/1920/GPS-A	75
DC6-48-60-18-8F	137	Side Arm Mount [SO 701-1]	75
7770.00 w/ Mount Pipe	137		

MATERIAL STRENGTH

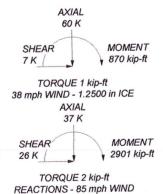
		1007 1 1 1001 117			-
GRADE	Fv	Fu	GRADE	Fy	ru
A572-65	65 ksi	80 ksi	Reinf 43.49 ksi	43 ksi	65 ksi
Reinf 55.61 ksi	56 ksi	70 ksi	Reinf 43.53 ksi	44 ksi	65 ksi
Reinf 39.97 ksi		65 ksi	Reinf 45.71 ksi	46 ksi	58 ksi
Reinf 43.14 ksi		65 ksi	Reinf 57.63 ksi	58 ksi	73 ksi
Reinf 43.34 ksi		55 ksi	Reinf 57.80 ksi	58 ksi	73 ksi
Reinf 43.47 ksi		55 ksi	Reinf 62.50 ksi	63 ksi	79 ksi

TOWER DESIGN NOTES

 Tower is located in New Haven County, Connecticut.
 Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 Tower is also designed for a 38 mph basic wind with 1.25 in ice. Ice is considered to increase in thickness with height.

Deflections are based upon a 50 mph wind.

TOWER RATING: 99.6%



Paul J. Ford and Company 250 East Broad St, Suite 150 Columbus, OH 43215

Phone: 614.221.6679

FAX:

v	Project: PJF 37512-102	ord, CT; Oxford	/ Fritz Property
10	Project: PJF 37512-102	27 Rev (BU 87636)	2)
,,,	Client: Crown Castle	Drawn by: TDehnke	App'd:
	Code: TIA/EIA-222-F	Date: 07/23/12	Scale: NTS
	Path:		Dwg No. E-1

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data

BU#: Site Name:

App #:

Qty:

Diam:

Diam:

Thick:

Grade:

Thick:

Single-Rod B-eff:

Rod Material:

Strength (Fu):

Yield (Fy):

Bolt Circle:

Pole Manufacturer: Other

Anchor Rod Data

12 2.25

A615-J

100

75

54

Plate Data

60

1.75

60

12.03

in

ksi

ksi

in

in

in

ksi

in

in

in

Reactions		
Moment:	2332.44	ft-kips
Axial:	37	kips
Shear:	26	kips

If No stiffeners, Criteria:

AISC ASD <-Only Applicable to Unstiffened Cases

Anchor Rod Results

Maximum Rod Tension: 169.7 Kips 195.0 Kips Allowable Tension: 87.0% Pass

Anchor Rod Stress Ratio:

Stiffened Service, ASD Fty*ASIF

Base Plate Results

Base Plate Stress: 7.4 ksi

Base Plate Stress Ratio: 23.3% Pass

Stiffened Service, ASD 0.75*Fy*ASIF Y.L. Length:

Stiffener Data (Welding at both sides)

Config: 3 Weld Type: Both in ** Groove Depth: 0.25 Groove Angle: 45 degrees Fillet H. Weld: 0.375

in Fillet V. Weld: 0.375 in Width: 6.75 in Height: 13.75 in

0.5

Notch: 0.75 Grade: 50 ksi Weld str. 80 ksi

Clear Space between 5.5 in Stiffeners (b):

Axial:	37	kips
Shear:	26	kips

Shear Check Only

Allowable Plate Stress: 32.0 ksi

N/A, Roark

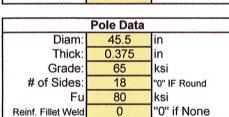
Analysis Date: 7/23/2012

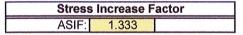
Stiffener Results

Horizontal Weld: 54.1% Pass 33.0% Pass Vertical Weld: 28.2% Pass Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 56.7% Pass Plate Tension+Shear, ft/Ft+(fv/Fv)^2: Plate Comp. (AISC Bracket): 72.8% Pass

Pole Results

13.2% Pass Pole Punching Shear Check:









^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes



Date: 7/23/2012 PJF Project: 37512-1027 Client Ref. # 876362

Site Name:
Description:
Owner:

v4.1 - Effective 7-3-12

Engineer: TJD
Asymmetric Anchor Rod Analysis

 Moment =
 2901
 k-ft
 TIA Ref.

 Axial =
 37.0
 kips
 ASIF =

 Shear =
 26.0
 kips
 Max Ratio =

 Anchor Qty =
 15
 Max Ratio =

Location = η = Threads = Base Plate
N/A f

for BP, Rev. G Sect. 4.9.9

for FP, Rev. G

** For Post Installed Anchors: Check anchors for embedment, epoxy/grout bond, and capacity based on proof load. **

1.3333

100.0%

	Nominal Anchor Dia,				Location,	Anchor	Area Override,	-	Max Net Compressi	Max Net Tension,	Load for Capacity	Capacity Override,	Capacity,	Capacity
Item	in	Spec	Fy, ksi	Fu, ksi	degrees	Circle, in	in ²	Area, in ²	on, kips	kips	Calc, kips	kips	kips	Ratio
1	2.250	#18J A615 Gr 75	75	100	0.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
2	2.250	#18J A615 Gr 75	75	100	30.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
3	2.250	#18J A615 Gr 75	75	100	60.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
4	2.250	#18J A615 Gr 75	75	100	90.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
5	2.250	#18J A615 Gr 75	75	100	120.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
6	2.250	#18J A615 Gr 75	75	100	150.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
7	2.250	#18J A615 Gr 75	75	100	180.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
8	2.250	#18J A615 Gr 75	75	100	210.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
9	2.250	#18J A615 Gr 75	75	100	240.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
10	2.250	#18J A615 Gr 75	75	100	270.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
11	2.250	#18J A615 Gr 75	75	100	300.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
12	2.250	#18J A615 Gr 75	75	100	330.0	54.00	0.00	3.98	175.05	169.69	169.69	0.00	195.00	87.0%
13	1.750	A193 Gr B7	105	125	15.0	69.00	0.00	2.41	134.72	131.49	131.49	0.00	132.29	99.4%
14	1.750	A193 Gr B7	105	125	135.0	69.00	0.00	2.41	134.72	131.49	131.49	0.00	132.29	99.4%
15	1.750	A193 Gr B7	105	125	255.0	69.00	0.00	2.41	134.72	131.49	131.49	0.00	132.29	99.4%
								54.98						

Pier Projection = 1 ft

Overturning Moment = 2901 ft-k

Comp Load = 37 kips

Horizontal Load = 26 k

Foundation Loads:

(kips)	(kips)	2901 (ft-kips)
37	26	ļ
Pole weight or tower leg compression =	Horizontal load at top of pier =	Overturning moment at top of pier=

1.5 <u>Design criteria:</u>
Safety factor against overturning =

Soil Properties:

(bct)	(ksf)	(#)
100	16	66
Soil density =	Allowable soil bearing =	Depth to water table =

Footing Depth = 5 ft

Top and Bottom (31)#8 ea way

6.0

26 k

6 ft square pier (26) #8 vert

#4 ties

Conc = 357.5 kWater ≈ 0 k

water table below ftg

#9

Soil = $24.1 \, \text{k}$

weights

H 3.4

Dimensions:

S ("R" or "S")	(tf)	1 (ft)	5 (Ħ)	4.5 (ft)	22.75 (ft)	22.75 (ft)
Pier shape (round or square)	Pier width =	Pier height above grade =	depth to bottom of footing =	Footing thickness =	Footing width =	Footing length =

Concrete:

2511 psf (net)

418.53k

Ecc = 7.006 ft

22.75 ft x 22.75 ft

Reinforcing Steel:

Pad	3 inches	#8 bar	31 (ea direction	
	minimum cover over rebar =	size of pad rebar =	quantity of pad rebar =	

Reinforcing Steel:

Pier	#8 bar	26	# 4 bar	4.5 inches
	size of vert rebar in pier=	vertical rebar quantity =	size of pier ties =	minimum cover over rebar =

Total volume of concrete = 88.3 cu yd

	Summary of analysis results	lalysis results
fion)	tion) Maximum Net Soil Bearing = 2.511 ksf	Ult Bending Shear Capacity = 126 psi
,		Ult Bending Shear Stress = 23 psi
	kay	Bending Shear Stress Ratio = 0.18 Okay
	Eta Overturning Resistance = 4761 ff-kips	Pad Bending Moment Capacity= 5368 ft-k
		Dod Donding Moment = 1530 ft-k
	Overturning Moment = 2932 II-Rips	rad belighing mornent - 1999 ich
	= 1.5	Bending Moment Stress Ratio = 0.29 OK
	Overturning Safety Factor = 1.624	
	Ratio = 0.92 Okay	

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spColumn v4.80 (TM)

Computer program for the Strength Design of Reinforced Concrete Sections

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General Information:

File Name: T:\375 Crown Castle\2012\37512-1027 BU 876362\...\37512-1027R1_B_anchor fully develop.col

Project: 37512-1027

Column: Engineer: lgr ACI 318-08 Units: English Code:

Slenderness: Not considered Run Option: Investigation Run Axis: X-axis Column Type: Structural

Material Properties:

f'c = 4 ksifγ = 60 ksi = 3605 ksi = 29000 ksi Es

Ultimate strain = 0.003 in/in

Beta1 = 0.85

Section:

Rectangular: Width = 72 in

Depth = 72 in

Gross section area, $Ag = 5184 \text{ in}^2$

 $Iy = 2.23949e+006 in^4$

ry = 20.7846 in Yo = 0 in

Ix = 2.23949e+006 in^4 rx = 20.7846 in Xo = 0 in

Reinforcement: _____

Bar Set: ASTM A615

S	ize	Diam (in)	Area (in^2)	S:	ize	Diam (in)	Area (in^	(2) S:	Lze	Diam (in)	Area (in^2)
_											
#	3	0.38	0.11	#	4	0.50	0.	20 #	5	0.63	0.31
#	6	0.75	0.44	#	7	0.88	0.	60 #	8	1.00	0.79
#	9	1.13	1.00	#	10	1.27	1.	27 #	11	1.41	1.56
#	14	1.69	2 25	#	18	2 26	4	00			

Confinement: Tied; #4 ties with #10 bars, #4 with larger bars. phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.65

Layout: Circular

Pattern: All Sides Equal (Cover to transverse reinforcement)
Total steel area: As = 54.61 in^2 at rho = 1.05%

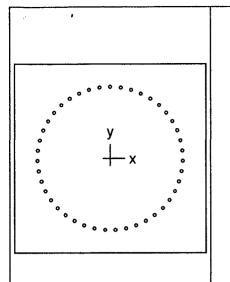
Minimum clear spacing = 2.72 in

43 #10 Cover = 7.56 in

Factored Loads and Moments with Corresponding Capacities:

	Pu	Mux	PhiMnx	PhiMn/Mu	NA depth	Dt depth	eps_t	Phi
No.	kip	k-ft	k-ft		in	in	***	
1	0.00	3822.00	7245.47	1.896	11.65	63.23	0.01330	0.900

*** End of output ***



72 x 72 in

Code: ACI 318-08

Units: English

Run axis: About X-axis

Run option: Investigation

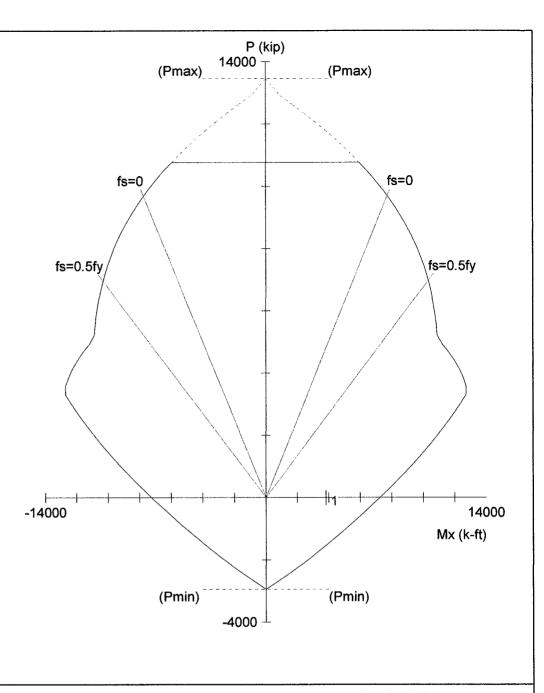
Slenderness: Not considered

Column type: Structural

Bars: ASTM A615

Date: 07/24/12

Time: 10:32:07



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File: T:\375_Crown_Castle\2012\37512-1027 BU 876362\37512-1027 BP R2...\37512-1027R1_B_anchor fully develop.col

Project: 37512-1027

Column:

fc = 4 ksi

fy = 60 ksi

Ec = 3605 ksi

Es = 29000 ksi

fc = 3.4 ksi

e_u = 0.003 in/in

Beta1 = 0.85

Confinement: Tied

phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.65

Engineer: Igr

 $Ag = 5184 \text{ in}^2$

43 #10 bars

 $As = 54.61 \text{ in}^2$

rho = 1.05%

Xo = 0.00 in

 $1x = 2.23949e + 006 in^4$

Yo = 0.00 in

 $ly = 2.23949e+006 in^4$

Min clear spacing = 2.72 in

Clear cover = 8.06 in

CROWN CASTLE PROJECT: BU #876362; OXFORD / FRITZ PROPERTY; OXFORD, CT MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

UPON THE SUCCESSFUL AND COMPLETE INSTALLATION OF THE REINFORCING SYSTEM SPECIFIED IN THESE PLANS, THE REINFORCED FOLE MEETS THE WIND DESIGN RECOMMENDATIONS OF THE TILAFELA-222-F-1998 STANDARD FOR WIND SPECES OF 85 MPH AND 37.5 MPH + 1 M* FADIAL ICE

PON THE SUCCESSFUL AND COMPLETE INSTALLATION OF THE REINFORCING SYSTEM SPECIFIED IN THESE PLANS. THE REINFORCED POLE MEETS THE WIND DESIGN RECOMMENDATIONS OF THE TAYER AZZZF-1999 STANDARD FOR WIND SPEEDS OF SEMPH AND 37.6 MPH + 1 TAY FADIAL ICE.

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STRUCTORAL REPROVINCIAND STREET CORN STREET OF THE POLICE SHALL BE PERFORMED BY AWS CERTIFIED WELDERS REQUIRED ON THIS PROJECT SHALL BE PERFORMED BY AWS CERTIFIED WELDERS USING TWO HEAT WELDING TECHNIQUES.

ORTHER PURPOSES OF THIS PROJECT. TOW HEAT WELDING IS DEFINED AS A CAREFUL AND CONTROLLED WELDING PROCESS, PERFORMED BY EXPERIENCED AWS CERTIFIED WELDERS, SUCH THAT THE CORRECT AMOUNTS OF HEAT BUILDUP AT THE WELDED JOINT, DUE TO EXCESSIVE AMOUNTS OF HEAT BUILDUP AT THE WELDED JOINT, DUE TO EXCESSIVE MOUNTS OF HEAT BUILDUP AT THE WELDED JOINT, DUE TO EXCESSIVE MOUNTS OF HEAT BUILDUP AT THE WELDED JOINT, DUE TO EXCESSIVE MOINT AND FREID WELDING ACTIVITY ON THE POLE STRUCTURE DOES NOT SCORCH OR OTHERWISE DAMAGE THE EXISTING GALVANIZED SURFACE ON THE INSIDE OF THE POLE SHAFT IN AND AROUND THE REGION OF THE WELD.

THE TOW HEAT WELDING PROCESS, USED IN CONJUNCTION WITH THE CROWN CASTLE COAX PROTECTION AND FIRE SAFETY GUIDELINES, SHALL BE SET UP SO THAT ANY FIELD WELDING ACTIVITY ON THE COUNT CASTLE COAX PROTECTION AND FIRE SAFETY GUIDELINES, SHALL BE SET UP SO THAT ANY FIELD WELDING ACTIVITY ON THE POLE STRUCTURE DOES NOT SOORCH ANDOR OTHERWISE DAMAGE THE EXISTING COAX CABLES THAT RUN ON THE INSIDE ANDOR OUTSIDE OF THE POLE SHAFT IN AND AROUND THE REGION OF THE WELD.

ON THE POLE STRUCTURE DUES NOT SCORAT MADERS OF THE POLE SHAPT. IN AND AROUND THE REGION OF THE WELD.

CRAILES THAT RUN ON THE INSIDE ANDORO OUTSIDE OF THE POLE SHAPT. IN AND AROUND THE REGION OF THE WELD.

WHEAT WELD DEMONSTRATION REQUIRED. PRIOR TO BEGINNING THE FIELD WELDING FOR THE RENFORCEMENT WORK, THE CONTRACTORS AND SCENTED BY WELD WELD BY MAD LE BEINGSTRATE THE "LOW HEAT" WELDING PROCESS THAT WILL BE USED ON THIS PROJECT SO THAT GROWN CASTLE REPRESENTATIVES AND OSERVEY WELP THAT THE PROPOSED PROCESS DOES NOT DAMAGE THE EXISTING BALVANIZED SURFACE ON HE BLCK SIDE OF THE SAMPLE PLATE THAT IS BEING WELDED THE CONTRACTOR SHALL USE TEMPERATURE BLCK SIDE OF THE SAMPLE PLATE THAT IS BEING WELDED CRAYON, ANDIOR INFRARED SENSOR TO MEASURE AND DEMONSTRATE HE TEMPERATURE OF THE STEEL ON THE BACK SURFACE IN THE REGION OF THE WELD. THE TOWN HEAT WELD DEMONSTRATION STEEL ON THE BACK SURFACE IN THE REGION OF THE WELD. THE TWENT DEMONSTRATION STEEL ON THE BACK SURFACE IN THE REGION OF THE WELD. THE TABLE WITH A THICKNESS SHALL BE CARRIED OUT ON SITE AND USES THAT WILL BE REPROVED BY GROWN CASTLE FECHNIQUES AND BECKERS SUCK, AND THE CONTRACTOR SHALL BE CARRIED OUT ON SITE AND USES THAT WILL BE REPROVED BY GROWN CASTLE CONTROL OF THE WELD. THE THAT SHAPE WITH A THICKNESS COULD THE CONTRACTOR SHAPE WELD DEMONSTRATION AND THE PLATE SHAPE BE DONE OF THE WELD DEMONSTRATION OF THE WELD THAT SHAPE WITH A THICKNESS COULD SHAPE SHAPE BE DONE OF THE SHAPE SHAPE BE DONE OF THE SHAPE SHAPE BE DONE OF THE SHAPE SHAPE BE DONE OF THE THE SHAPE S

C. SPECIAL INSPECTION AND TESTING
ALT WORK SPALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND
THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY. REFER TO GROWN
THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY. REFER TO GROWN
ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE
DISTINGUISHED FROM CONTRIVENCES PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR
THE PURPOSE OF ASSISTING HOUSE PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR
THE PURPOSE OF ASSISTING AUGUST CONTROL
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THE PURPOSE OF ASSISTING AUGUST CONTROL
TO CONTRICE A SISTING HOUSE OF CONSTRUCTION.
CONTRICED AND THE PURPOSE OF THE CONTRACTOR.

APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.

A PURPOSE OF THE CONTRACTOR AND AND FOR THE PURPOSE OF THE CONTRACTOR.

A PURPOSE OF THE OWNER OF THE SOLE PURPOSE OF THE CONTRACTOR.

BY THE INSPECTION AGENCY SHALL SO SCHEDULE THIS WORK AS TO CAUSE A MINIMUM OF INTERNETING AGENCY. THE CONTRACTOR RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TITLE AGE THE THE THE PURPOSE OF THE TESTING AGENCY. THE CONTRACTOR RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TITLE AGE THE AGENCY SHALL ALLOW FOR ADEQUATE THE AND OTHER TESTING AGENCY SHALL ALLOW FOR ADEQUATE THE FOLLOWING TERMS ON THIS USE THAT AND OTHER TESMS AS RECESSARY TO FULFILL THER RESPONSIBLE TO PERFORM THE FOLLOWIN

AND COMMENSURALE WHITE THE COLOR TO THE MATERIAL WHITE THE CONTRACTOR AND TESTING GENERAL.

(II.) PERFORM CONTINUOUS ON-SITE OBSERVATION, INSPECTION, VERIFICATION, AND TESTING DURING THE TIME THE CONTRACTOR IS WORKING ON-SITE. AGENCY SHALL NOTIFY OWNER IMMEDIATELY WHICH FIELD PROBLEMS OR DISCREPANCIES OCCUR.

(I.) VERHY MATERIALS AT BOTTOM OF EXCAVATION ARE ADEQUATE TO ACHIEVE THE DESIGN BARNING CAPACITY.

(2.) VERHY THAT EXCAVATIONS HAVE EXTENDED TO PROPER DEPTH AND HAVE REACHED PROPER MATERIAL.

BEANING LOWARD.

(2.) VERRY THAT EXCAVATIONS HAVE EXTENDED TO PROPER DEPTH AND DAYLOW AND TRIAL.

(3.) PERFORM CLASSIFICATION AND TESTING OF COMPACTED FILL MATERIALS.

(4.) VERIFY USE OF PROPER MATERIALS, DENSITIES AND LIFT THICKNESS DURING PLACEMENT AND COMPACTION OF COMPACTED HILL, OBSERVE SUBGRADE AND VERIFY SITE HAS BEEN PROPERLY.

(5.) PRICAT OF PLACEMENT OF COMPACTED HILL, OBSERVE SUBGRADE AND VERIFY SITE HAS BEEN PLACEMENT OF REINFORCING STEEL.

(7.) THE PROPERTY OF PLACEMENT OF REINFORCING STEEL.

(8.) VERIFYING USE OF REQUIRED MIX DESIGN.

(9.) VERIFYING USE OF REQUIRED MIX DESIGN.

(14.) AT THE TIME FRESH CONCRETE IS SAMPLED TO FABRICATE SPECIMENS FOR STRENGTH TESTS, PERFORM SLUMP AND AIR CONTINUENT TEST AND DETERMINE TEMPERATURE OF THE CONCRETE.

(6.) INSPECTION OF EXCELLED LANGUAGE AND PROPER APPLICATION TECHNIQUE.

(6) INSPECTION OF SPECIFIED CURING AND TEMPERATURE TECHNIQUES.

O. STRUCTURAL STEEL

T. CRECK THE STEEL ON THE JOB WITH THE PLANS.

C. CRECK THE STEEL ON THE JOB WITH THE PLANS.

C. CRECK WILL CERTIFICATIONS.

C. CRECK GRADE OF STEEL MEMBERS, AND BOLTS FOR CONFORMANCE WITH DRAWINGS.

MSPECT STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.

S. CALL FOR LABORATORY TEST REPORTS WHEN IN DOUBT.

C. CRECK STEEL MEMBERS FOR SIZES, SWEEP AND DIMENSIONAL TOLERANCES.

T. CRECK FOR SURFACE FINISH SPECIFIED, GALVANIZED.

B. CRECK BOLT TIGHTENING ACCORDING TO AISC "TURN OF THE NUT" METHOD.

E. WELDING.

(8) CHECK BOLT TIGHTENING ACCURDING TO ADD TOTAL OF THE WELDING:

(1,1) VERIFY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, NOT DEEMED PREQUALIFIED, IN ACCORDANCE WITH AWB D1.1.

(2) INSPECT FIELD WELDED CONNECTIONS IN ACCORDANCE WITH THE REQUIREMENTS SPECIFIED AND IN ACCORDANCE WITH AWB D1.1.

(3) APPROVE FIELD WELDING SEQUENCE.

(A) A PROGRAM OF THE APPROVED SEQUENCES SHALL BE SUBMITTED TO THE OWNER BEFORE WELDING BEDINS. NO CHANGE IN APPROVED SEQUENCES MAY BE MADE WITHOUT PERMISSION FROM THE OWNER.

OWNER.

(4.) INSPECT WELDED CONNECTIONS AS FOLLOWS AND IN ACCORDANCE WITH AWS D1.1:

(A) INSPECT WELDING EQUIPMENT FOR CAPACITY, MAINTENANCE AND WORKING CONDITIONS.

(B) VERIETY SPECIFIED ELECTRODES AND HANDLING AND STORAGE OF ELECTRODES FOR CONFORMANCE TO SPECIFICATIONS.

(C) INSPECT PREHEATING AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS D1.1:

CONTOMNANCE 10 SPECIFICATIONS.

(C.) INSPECT PREHEATING AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS D.1.

(D.) VISUALLY INSPECT ALL WELDS AND VERIFY THAT QUALITY OF WELDS MEETS THE REQUIREMENTS OF AWS D.1.

(E.) SPOT TEST AT LEAST ONE FILLET WELD OF EACH MEMBER USING MAGNETIC PARTICLE OR DYE PENETRANT.

(F.) INSPECT FOR SIZE, SPACING, TYPE AND LOCATION AS PER APPROVED PLANS.

(Q.) VERIFY THAT THE BASE METAL CONFORMS TO THE DRAWINGS.

(H.) CHECK TO SEE THAT WELDS ARE CLEAN AND FREE FROM SLAG.

(J.) MISPECT RUST PROTECTION OF WELDS AS PER SPECIFICATIONS.

(K.) CHECK THAT DEFECTIVE WELDS ARE CLEANLY MARKED AND HAVE BEEN ADEQUATELY REPAIRED.

F. SPECIAL INSPECTION OF EXISTING SHAFT-TO-FLANGE WELD CONNECTIONS.

(T.) PRIOR TO CONSTRUCTION, TESTING AGENCY SHALL INSPECT CONDITION OF EXISTING SHAFT-TO-BASE-PLATE WELD CONNECTION. ALSO INSPECT CONDITION OF EXISTING SHAFT-TO-BASE-PLATE WELD CONNECTION. ALSO INSPECT CONDITION OF EXISTING SHAFT-TO-BASE-PLATE WELD CONNECTION. ALSO INSPECT CONDITION OF EXISTING METHODS, AS REQUIRED TO IDENTIFY ANY CRACKS: VISUAL, MAGNETIC PARTICLE, ANDIOR ULTRA-SONIC, IN ADDITION, OTHER TEST METHODS MAY ALSO BE USED AT HE OWNER AND THE REGIONE METHOD SHAP ALSO BE USED AT HE OWNER AND THE RESULTS OF ROVIDE CAREFURCH OF HIS WAY AND AND OF THE COMMENDATION OF THE TESTING AGENCY AND UPON THE APPROVAL OF THE OWNER AND THE ENGINEER. THE TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD REPAIRS AND PROCEDURES. IMPORTANT: THE TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD REPAIRS IMPLEMENTED AS REQUIRED PROCESSES AND PROCEDURES. IMPORTANT: THE TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD REPAIRS IMPLEMENTED AS REQUIRED BY THE OWNER FROM THE RESULTS OF THE INSPECTION IN THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROPORT ANY INDICATIONS OF CRACKS, "TYPICHES," INSTERS AND/OR CONSIGN TO THE OWNER AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND THE PROVINCE AND TH

G. REPORTS: (1.) COMPILE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

(T) COMPILE AND PERIODICALLY SUBMIT DAILY MSPECTION REPORTS TO THE OWNER.

THE INSPECTION PLAN OUTLINED HEREIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC HEMS OF CONCERN. IT IS NOT INTENDED TO BE ALL-INCLUSIVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE ITEMS LISTED. ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTICHATED. THE TESTING AGENCY SHALL USE THEIR PREPERSHANCE JUDGMENT AND KNOWLEDGE OF THE JOB SITE CONDITIONS AND ITEMS TESTING AGENCY SUBCRIENT TO DEDDE WHAT OTHER THE JOB SITE CONDITIONS AND ITEMS TESTING AGENCY SUBCRIENT MUST PREVAILE WHAT OTHER INSPECTION ADDITIONS AND ITEMS TO THE OWNERS ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNERS REVIEW AND SPECIFIC WITHTEN CONSENT. THE OWNER RESERVES THE RIGHT TO DETERMINE WHAT IS AN ACCEPTABLE RESOLUTION OF DISCREPANCIES AND PROBLEMS. AFTER EACH INSPECTION, THE TESTING AGENCY WILL PREPARE A WITHTEN ACCEPTANCE OR REJECTION WHILD AND SPECIFIC WITHTEN CONSENT. THE OWNER RESERVES THE RIGHT TO DETERMINE WHAT IS AN ACCEPTABLE RESOLUTION OF DISCREPANCIES AND PROBLEMS. AFTER EACH INSPECTION, THE TESTING AGENCY WILL PREPARE A WITHTEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WITHTEN ACCIDENT TO THE OWNER. THIS WITHTEN ACCIDENT TO THE OWNER. THIS WITHTEN ACCIDENT OF PRIOR TO CONTRIBUTION, ANDORIC LODDING OF STRUCTURAL TIEMS.

RESPONSIBILITY: THE TESTING AGENCY ODES NOT RELIEVE THE CONTRACTOR'S CONTRACTUAL OR STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR ANY DEVARTOR OF PROMITIES. THE TESTING AGENCY ODES NOT RELIEVE THE CONTRACTOR'S CONTRACTOR'

AEROSOLUTIONS SHAFT REINFORCING OPTION

SUMMERS 7/24/201

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street - Suite 1500 - Columbus, Oha 43216 (614) 221-6879

CROWN CASTLE 3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NC 28277 PH: (908) 258-7010

BU #876362; OXFORD / FRITZ PROPERTY OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

37512-1027 DRAWN BY: B.M.S. CHECKED BY T.J.D.

APPROVED BY

DATE:

ISSUE DATE OF PERMIT: 7-6-2012

S-1A

STRUCTURAL STEEL
STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM
TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

TO THE LATEST EDITION OF THE FOLLOWING REPEALANTS.

BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):

"SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL

(A.)

TO THE LAYEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:

BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (ASC):

(A.) "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL

FOR BUILDINGS."

(B.) "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL

FOR BUILDINGS."

(C.) "CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1

SPECIFICATLY EXCLUDED).

BY THE AMERICAN WELDING SOCIETY (AWS):

(A.) "STRUCTURAL WELDING SOCIETY (AWS):

(A.) "STRUCTURAL WELDING SOCIETY (AWS):

(B.) "SYMBOLS FOR WELDING SOCIETY (AWS):

(B.) "SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING"

(B.) "SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING"

(B.) "SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING"

(B.) "SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING"

ANY MATERIAL OR WORKMANSHIP WHICH IS DRISERVED TO BE DEFECTIVE OR INCONSISTENT WITH

THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE

CONTRACTOR'S EXPENSE.

TIGHTEN ALL STRUCTURAL BOLTS, INCLUDING THE AJAX M20 BOLTS WITH SHEAR SLEEVES,

ACCORDING TO THE REQUIREMENTS OF THE AJAX M20 BOLTS WITH SHEAR SLEEVES,

ACCORDING TO THE REQUIREMENTS OF THE AJAX M20 BOLTS WITH SHEAR SLEEVES,

TIGHTEN ALL STRUCTURAL BOLTS, INCLUDING THE AJAX M20 BOLTS WITH SHEAR SLEEVES,

WELDED CONNECTIONS SHALL CONFORM TO THE AJAX M20 BOLTS WITH SHEAR SLEEVES,

TOWN WELDING SOCIETY, ANN DIT. ALL WELD ELECTRODES SHALL BE EBOX UNLESS NOTED

OTHERWISE ON THE DRAWMINGS.

ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS. CONTRACTOR SHALL

SUBMIT WELDERS' CERTIFICATION AND QUALIFICATION DOCUMENTATION TO THE OWNER'S TESTING

AGENCY FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.

STRUCTURAL STEEL PLATES SHALL CONFORM TO ASTIN ARZO GRADE 65 (FY = 85 KSI MIN) UNLESS

SURFACES OF EXISTING STEEL SHOWLD SHALL BE ADDED BY AWS. CONTRACTOR SHALL BY A SHALL BY A SHALL BY A SHALL BY A SHALL BY SHALL BY SHALL BY SHALL BY A SHALL BY A SHALL BY A SHALL BY A SHALL BY A SHALL BY A SHALL BY SHALL BY SHALL BY SHALL BY A SHALL BY SIELL AND THE INSPECTION/TESTING AGENCY SHALL VERIEFY PROPOSED LAYOUT, LOCATION, AND DIMENSIONS.

ANY REQUIRED CUTS IN THE STEEL SHALL BE CAREFULLY CUT BY MECHANICAL METHODS SUCH AS DRILLING, SAW CUTTING, AND GRINDING. THE CONTRACTOR IS RESPONSIBLE TO PREVENT ANY DAMAGE TO THE COAK CABLES, ANDIOR OTHER EQUIPMENT AND ORTHER STRUCTURE, RESULTING FROM THE COAK CABLES, ANDOR OTHER EQUIPMENT ANDIOR THE STRUCTURE, RESULTING FROM THE CONTRACTOR'S EXPENSE. THE INSPECTION/TESTING AGENCY SHALL CLOSELY AND CONTINUOUSLY MONITOR THIS ACTIVITY.

ALR REQUIRED CUTS SHALL BE CUT WITHIN THE DIMENSIONS SHOWN ON THE DRAWNINGS. NO CUTS SHALL EXTEND BEYOND THE OUTLINE OF THE DIMENSIONS SHOWN ON THE DRAWNINGS. ALL CUT EDGES SHALL BE GROUND SMOOTH AND DE-BURRED. CUT EDGES THAT ARE THE PROPERTIES OF FIELD WELDED SHALL BE PREPARED FOR FIELD WELDED SHALL BE REPREPARED FOR FIELD WELDED SHALL BE TREPREPARED FOR FIELD WELDED SHALL BE REPREPARED FOR FIELD WELDED SHALL BE TREPREPARED FOR FIELD WELDED SHALL BE TREPREPARED FOR FIELD WELDED SHALL BE REPREPARED FOR FIELD WELDED SHALL BE TREPREPARED FOR FIELD WELDED.

BASE PLATE GROUT
NEW STROUT FOR THE POLE BASE SHALL BE NON-SHRINK, NON-METALLIC, GROUT (EUCO NS GROUT
NEW STROUT FOR THE POLE BASE SHALL BE NON-SHRINK, NON-METALLIC, GROUT (EUCO NS GROUT
SPECLEURO, OR APPROVED EQUAL) WITH A 7500 PSI MINIMUM COMPRESSIVE STRENGTH. PVC
DRAINAGE PIPES SHALL BE PROVIDED FROM INSIDE THE POLE SHAFT OUT THROUGH THE GROUT
SPACE UNDER THE BASE PLATE IN ORDER TO ALLOW MISSITURE TO ADEQUATELY DRAIN FROM THE
INTERIOR OF THE POLE SHAFT. CONTRACTOR SHALL SUBMIT PROPOSED GROUT SPECIFICATION
INFORMATION TO THE OWNER FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.
CONTRACTOR SHALL FOLLOW GROUT MANUFACTURER'S SPECIFICATIONS FOR COLD WEATHER
GROUTING PROCEDURES (IF NECESSARY) AND THE TESTING AGENCY SHALL PREPARE GROUT
SAMPLE SPECIMENS FOR COMPRESSIVE STRENGTH TESTING AND VERIFICATION.
SAMPLE SPECIMENS FOR COMPRESSIVE STRENGTH TESTING AND VERIFICATION.
GROUT SHALL BE INSTALLED TIGHT UNDER BASE PLATE WITH NO YOURS REMAINING BETWEEN TOP
OF EXISTING CONCRETE AND UNDERSIDE OF EXISTING BASE PLATE (EXCEPT FOR DRAIN PIPES).
GROUT COMPLETELY SOLD (EXCEPT FOR DRAIN PIPES) UNDER ENTIRE SURFACE OF BASE PLATE
FROM OUTSIDE EDGE TO INSIDE EDGE.

FOUNDATION WORK - (NOT REQUIRED)

CAST-IM-PLACE CONCRETE
CONCRETE SHALL RAVE A NIMIMUM COMPRESSIVE STRENGTH OF 4000 PSI AT 28 DAYS.
(A) CONCRETE EXPOSED TO WEATHER SHALL BE AIR ENTRAINED (6% +* 1.5%).
(B) WATER CEMENT RATIO = 0.52 (MAXIMUM).
ALL REINFORCING STEEL SHALL BE NEW DOMESTIC DEFORMED BILLET STEEL CONFORMING TO ASTIM ABIS GRADE 60.
ASTIM ABIS GRADE 60.
ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH "THE BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE" ACI 318, LATEST EDITION.
CONTRACTOR SHALL FOLLOW ALL APPLICABLE ACI PROCEDURES FOR COLD WEATHER CONCRETE PLACEMENT.
ALL REINFORCING DETAILS SHALL CONFORM TO "MANUAL OF STANDARD PRACTICE FOR DETAILING REINFORCED CONCRETE STRUCTURES" ACI 315, ON THE STRUCTURAL DRAWNIGS.
LATEST EDITION, UNLESS DETAILED OTHERWISE ON THE STRUCTURAL DRAWNIGS.
CONTRACTOR SHALL VERIFY LOCATIONS OF ALL OPENINGS, SLEEVES, ANCHOR RODS, INSERTS, ETC., AS REQUIRED BEFORE CONCRETE IS PLACED.
WHERE BAR LENGTHS ARE GIVEN ON THE DRAWNINGS, THE LENGTH OF ANY HOOK, IF REQUIRED, IS NOT INSLIBED.

ETC., AS REQUIRED BEFORE CONCRETE IS PLACED.

WHERE BAR LENGTHS ARE GIVEN ON THE DRAWINGS, THE LENGTH OF ANY HOOK, IF REQUIRED, IS

WIS BE BAR LENGTHS ARE GIVEN ON THE DRAWINGS, THE LENGTH OF ANY HOOK, IF REQUIRED, IS

NOT INCLUDED.

CONTRACTOR SHALL, PROVIDE SPACERS, CHAIRS, BOLSTERS, ETC., NECESSARY TO SUPPORT

REINFORCING STEEL. CHAIRS WHICH BEAR ON EXPOSED

CONCRETE SUPFACES SHALL HAVE ENDS WHICH ARE PLASTIC TIPPED OR STAINLESS STEEL.

ALL STRUCTURAL MEMBERS SHALL BE POURED MONOLTHICALLY, EXCEPT FOR REQUIRED

CONSTRUCTION JOINTS. CONTRACTOR SHALL SUBMIT

PROPOSED CONSTRUCTION JOINT LOCATIONS AND DETAILS TO THE ENGINEER FOR REVIEW.

CONTRACTOR SHALL PROVIDE 3/4-INCH CHAMFER ON ALL EXPOSED CORNERS UNLESS OTHERWISE

MIDICATED ON THE DRAWINGS. MINIMUM

CLEARANCES FOR REINFORCING STEELS SHALL BE PROVIDED FOR REINFORCEMENT:

THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCEMENT:

11-1/2" CONCRETE CAST AGAINST AND PERMANETHE, BS THROUGH #18 BARS.

2" CONCRETE CAST AGAINST AND PERMANETHE, BS THROUGH #18 BARS.

2" CONCRETE CAST OF THE CONCRETE CAST OF THE PROVIDED FOR REINFORCEMENT:

1-1/2" CONCRETE CAST OF THE CONCRETE CAST OF THE CONCRETE BARS WITH A 2"-0" LAP

ON EACH LEG.

FOOTING BARS SHALL BE BENT THE AND CONPORT OF FIELD OFFICE.

FOOTING BARS SHALL BE BENT THE AND CONPORT OF THE PROVIDED FOR SHALL SHAL

11.

12.

PEORY OROUTED REINFORCING ANCHOR RODS

INLESS OTHERWISE NOTED, REINFORCING ANCHOR ROOS SHALL BE 150 KSI ALL-THREAD BAR

INLESS OTHERWISE NOTED, REINFORCING ANCHOR ROOS SHALL BE 150 KSI ALL-THREAD BAR

INLESS OTHERWISE NOTED, REINFORCING ANCHOR ROOS SHALL BE 150 KSI ALL-THREAD

BAR ARE WILLMAS FORME RIGINEERING CORPORATION AND DYWIDIAG SYSTEMS INTERNATIONAL.

ALL REINFORCING ANCHOR ROOS SHALL BE HOT IDIP GALVANIZED PER ASTIM ATS. ALTERNATIONAL.

ALL REINFORCING ANCHOR ROOS SHALL BE HOT IDIP GALVANIZED PER ASTIM ATS. ALTERNATIVELY,

ALL REINFORCING ANCHOR ROOS SHALL BE HOT IDIP GALVANIZED PER ASTIM ATS. ALTERNATIVELY,

ALL REINFORCING ANCHOR ROOS SHALL BE HOT IDIP GALVANIZED PER ASTIM ATS. ALTERNATIVELY,

ALL REINFORCING ANCHOR ROOS SHALL BE FOOXY CAREED

THE CORE-DRILLED HOLES IN THE CONCRETE FOR THE ANCHOR ROOS SHALL BE CLEAN AND DIPPORY,

MANUFACTURERS INSTRUCTIONS, PRICET TO PLACEMENT OF ANCHOR ROOD AND POOY,

MANUFACTURERS INSTRUCTIONS, PRICET TO PLACEMENT OF ANCHOR ROOD AND POOY,

MANUFACTURER RECOMMENTALIZATION CURING, THE EFFECT OF TEMPERATURE ON EPOXY, CURING

TIME, PREPARATION OF HOLE ETC MICHORITIES EPOXY SHALL BE USED TO ANCHOR THE 160 KSI

ULTRAGOND I, HILT HIT RESTALLATION CURING, THE EFFECT OF TEMPERATURE ON EPOXY, CURING

THE PREPARATION OF HOLE ETC MICHORITIES EPOXY SHALL BE USED TO ANCHOR THE 160 KSI

ULTRAGOND IN HILT HIT SHALL DIVIDE TO THE TOWN SHEST TO USE A DIFFERENT EPOXY, A

ALL THREAD BAR IN JULIES OF THE SHORL THE SHALL BROOMER FOR THE ASSENCE AND THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER FOR THE SHALL BROOMER

TOUCH UP OF GALVANIZING
THE CONTRACTOR SHALL TOUCH UP ANY AND/OR ALL AREAS OF GALVANIZING ON THE EXISTING
STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED OR ABRADED DURING CONSTRUCTION.
GALVANIZED SURFACES DAMAGED DURING TRANSPORTATION OR ERECTION AND ASSEMBLY AS
WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FIELD WELDING SHALL BE
TOUCHED UP WITH TWO (2) COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND. FLM
THICKNESS PER COAT SHALL BE: WET 3.0 MILS; DRY 15 MILS, APPLY PER ZRC (MANDFACTURER)
CONTRACTOR SHALL CLEAN AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PAINTED
SURFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS DI.1. THE OWNER'S TESTING
AGENCY SHALL VERIFY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUCH-UP

COATING.
THE OWNERS TESTING AGENCY SHALL TEST AND VERIEY THE COATING THICKNESS AFTER THE CONTRACTOR HAS APPLIED THE ZEC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY DRIED. AREAS FOUND TO BE INADEQUATELY COATED, SHALL BE RE-COATED BY THE CONTRACTOR AND RE-TESTED BY THE TESTING AGENCY.

HOT DIP GALVANIZING
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PERPETUAL INSPECTION AND MANTENANCE BY THE OWNER
AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPETED THE INSTALLATION OF THE MONOPOLE
REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE
RESPONSIBLE FOR STEEL AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE
RESPONSIBLE FOR STEEL
THE MONOPOLE REINFORCING SYSTEM INDICATED IN THESE DOCUMENTS USES REINFORCING
COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
POLE STRUCTURE. THESE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
POLE STRUCTURE. THESE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL
POLE STRUCTURE. THESE FIELD WELDING CONNECTIONS ARE SUBJECT TO CORROSION DAMAGE
AND DETERIORATION IF THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION
PREVENTIVE COATING SUCH AS THE ZRG GALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE
STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON
THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD
WELDED CONNECTIONS. ANY CORROSION OF, DAMAGET OF, FATIGUE, FRACTURE, ANDIOR
DETERIORATION OF THESE WELDS ANDIOR THE CONNECTED COMPONENTS WILL RESULT IN THE
LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FALURE OF THE
STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REGULARLY MSPECTS,
MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND
COMPONENTS FOR THE LIFE OF THE STRUCTURE.
THE OWNER SHALL REFER TO TUALEL-222-F1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS
FOR MAINTENANCE AND INSPECTION. THE FREQUENCY OF THE INSPECTION AND MAINTENANCE
INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL STRE AND ENVIRONMENTAL
CONDITIONS. PAUL J. FORD & COMPANY RECOMMENDS THAT A COMPITIONS THAT A SOON ENTER AND ENVIRONMENTAL
CONDITIONS. PAUL J. FORD & COMPANY RECOMMENDS THAT A COMPITEE HE AND THOROUGH
INSPECTION OF THE STRUCTURE. THIS RECOMMENDED THAT THE STRUCTURE BE MISPECTED AFTER SEVERE
WIND AND/OR ICE STORMS OR OTHER EXTREME LOA



AEROSOLUTIONS SHAFT REINFORCING OPTION

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street - Surle 1500 - Columbus, Ohio 43216 www.pikesb.com

CROWN CASTLE 3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NO PH: (906) 256-7010

BU #876362; OXFORD / FRITZ PROPERTY OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

T.J.D.

ISSUE DATE OF PERMIT: 7-6-2012

S-2A

AJAX BOLT NOTE SHEET: REV. 1.2, 01-23-2012

- NOTES: 1. ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
 - 2. ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH
 - 3. ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED, SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
 - 4. ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 36 OR HIGHER.

NOTES FOR AJAX M20 'ONE-SIDE' BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH SILICONE EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY:

APPLIED BOLTING TECHNOLOGY PRODUCTS, INC. 1413 ROCKINGHAM ROAD BELLOWS FALLS, VERMONT, USA 05101 PHONE 1-800-552-1999

CROWN CASTLE

3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NC 2827

WEBSITE: WWW.APPLIEDBOLTING.COM

DISTRIBUTORS OF SQUIRTER® DTI'S: HTTP://WWW.APPLIEDBOLTING.COM/APPLIED-BOLTING-DISTRIBUTORS.HTML

DTI: USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 3/4" NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS. DTI'S SHALL NOT BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

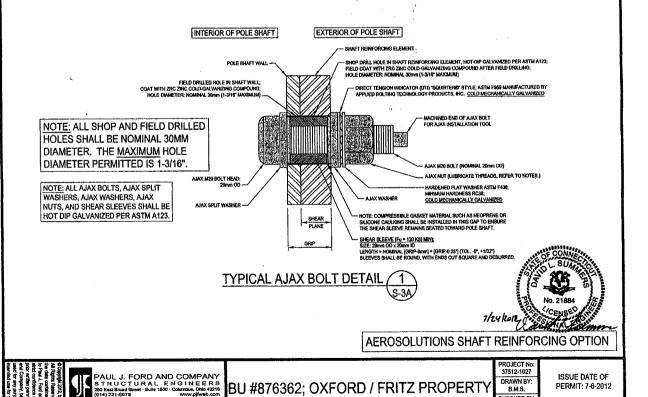
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 314" NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F438 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE <u>THREADS OF THE NUT</u> OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER, NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE SHOP DRIVEN BY AND ALL ADDRESS OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE SHOP DRIVEN BY AND ALL ADDRESS OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION. TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTTS SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTTS.



BU #876362; OXFORD / FRITZ PROPERTY

OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

B.M.S. CHECKED BY

T.J.D.

APPROVED BY

S-3A

NOTE: NO DETAILED INFORMATION REGARDING INTERFERENCES WAS PROVIDED. THEREFORE, CONTRACTOR SHALL FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS BEFORE PROCEEDING WITH THE WORK. REPORT ANY AND ALL DISCREPANCIES TO PAUL J. FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL IMMEDIATELY.

THIS POLE REINFORCEMENT DRAWING IS FOR THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF CO-LOCATION ANALYSIS FOR THIS SITE (PJF#37512-1027), DATED 7-23-2012.

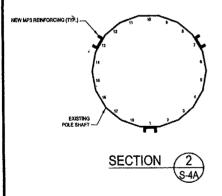
ſ	POLE SPECIFICATIONS
POLE SHAPE TYPE:	18-SIDED POLYGON
TAPER:	0.2033 IN/FT
SHAFT STEEL:	ASTN A572 GRADE 65
BASE PL STEEL:	ASTM A833 GR. E (60 KSI)
ANCHOR RODS:	2140
	#183 ASTM A615 GRADE 76

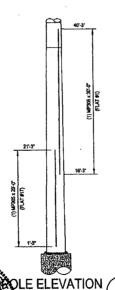
SHAFT	SECTION LENGTH	PLATE THICKNESS	LAP SPLICE	DIAMETER ACROSS FLATS (IN)			
SECTION	(FI)	fisal	1 100	€ TÓP	@ BOTTON		
1	26,5600	0.1875	447	15.000	20,740		
2	40.6300	8,2500	3.17	19.680	28.320		
3	47.6300	0.3125	4.08	26.952	37.100		
4	47,6800	0.3750	5.17	35.374	45.500		

S. <u>NUT LUBRICATION REQUIRED.</u> "PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT ON HE PROPERLY TIGHTENED WITHOUT CALLING ANDIOR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SINLE, FOLLOW DIT MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTEN REFER TO SHEET 5-3.

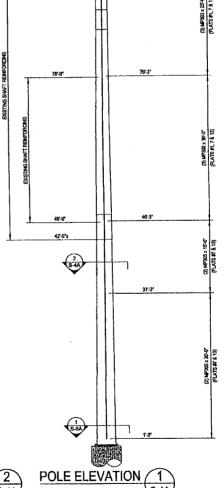
'AS OF 8/8/2012, UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AUX BOLTS TIGHTENED USING AISC "TURN-OF-THE-HUT" METHODOLOGY, INSTALLERS SHALL FOLLOW GROWN GUIDELINES FOR AISC "TURN-OF-THE-HUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PML

INDE OF THE CIRCUMFERENTIAL WELD OF THE BASE PLATE TO SHAFT CONNECTION IS REQUIRED. PLEASE SEE END-SOW, 1003: TOWER BASE PLATE NOE AND END-SHAFTON INDERECURELENTS FOR MONOPOLE BASE PLATE TO REPREVAT CONNECTION FAULTE. HOWEVER FER OR AND CROWN FROMERENENS HEMBERTALEY IN ANY CRACKS ARE SUSPECTED OR HAVE BEEN BOTTIFFED. THE NOE SHALL INCLUDE ALL EDSTING REMOTECHEN HAVE HAVE HAVE AND FOR THE PLATE ROQUER OF THE NOETHERN SHAFT OF THIS ACTIVE REMOTROBLENT OF SHAFT OF THIS ACTIVE REMOTROBLENT OF SHAFT OF THIS ACTIVE REMOTROBLENT OF SHAFT OF THIS ACTIVE REMOTROBLENT OF SHAFT OF THIS ACTIVE REMOTROBLENT OSSION SHALL BE INCLIDED IN THE NOE SOOPE OF WORK.





7/24/2012



116'-3'



PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Broad Street - Sulte 1500 - Columbus, Ohio 43218 (614) 221-8879 www.phwsb.com

PROJECT No 37512-1027 DRAWN BY: B.M.S. CHECKED BY T.J.D. PROVED BY

DATE:

AEROSOLUTIONS SHAFT REINFORCING OPTION

ISSUE DATE OF PERMIT: 7-6-2012

S-4A

CROWN CASTLE 3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NC 28277 PH: (908) 256-7010 FAX: (301) 789-5849

OXFORD, CT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

BU #876362; OXFORD / FRITZ PROPERTY

SPECIAL INSPECTION OF EXISTING SHAFT-TO-FLANGE WELD CONNECTIONS:

(1) PRIOR TO CONSTRUCTION, CONTRACTOR'S MISPECTION AGENCY SHALL INSPECT CONDITION OF EXISTING SHAFT-TO-BASE-PLATE WELD CONNECTION. ALSO INSPECT EXISTING STIFFENERS IF PRESENT. THE CONTRACTOR'S INSPECTION AGENCY SHALL USE THE PLOCUMING INSPECTION METHODS, OR COMBINATION OF METHODS, AS REQUIRED TO IDENTEY ANY CRACKS: VISUAL, MAGNETIC PARTICLE, AND CITALSONIC. IN ADDITION OF METHODS MAY ALSO BE USED AT THE RECOMMENDATION OF THE ESTIMA AGENCY AND EXPENSIVE OF THE OWNER AND THE RECOMMENDATION SHALL PROVIDE CAMERIA, AND THIS APPROVAL OF THE OWNER AND THE ENGINEER CONTRACTOR SHALL PROVIDE CAMERIA, AND THIS INSPECTION ACTIVITIES WITH THE OWNERS REQUIRED PROCESSES AND PROCESSES, BURDETIANT. THE ESTIMA AGENCY SHALL MAGNETIAN PROPART AND PROCLAINES, CHRISES, AND THE CONTRACTOR SHALL CONDITION TO THE OWNER AND THIS PROVIDED PROCESSES AND PROCESSES, AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES AND PROCESSES.

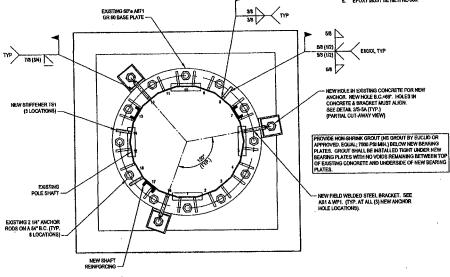
[2] AFER CONSTRUCTION, TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD WELDS AND FIELD REPARTS IMPLEMENTED AS RECOURSED BY THE OWNER FROM THE RESULTS OF THE INSPECTION IN THE PREVIOUS NOTE (1) ABOVE.

GENERAL NOTES

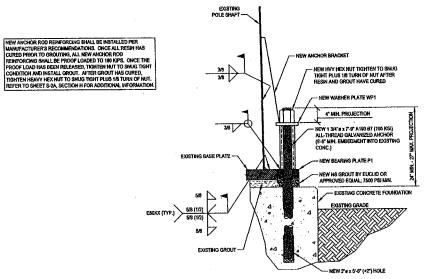
1. AUX BOLTS ARE TO BE 20 mm & WITH CORRESPONDING 29 mm & SHEAR SLEEVE
MITH MATCHING STEEL GRADE: DIRILLED HOLE DAMETERS IN REINFORCING STEEL
AND EXISTING SHAFT SHALL BE 1 3/16"s MAX.

2. AL STEEL SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ADDIT A 123. ALTERNATIVELY, ALL NEW STREENER PLATE STEEL REINFORCING MAY SE COLD GALVANIZED AS FOLKOWS, PLAY A NAMILAN OF TWO CATS GO CARRAD ZUG-RICH COLD GALVANIZING COMPOUND. PLAT INCOMESS PER COAT SHALL BE: WET 33 MAIS. JOY 15 MGS. PREY PER ZIG (ANMAFACTURES) PER COATECOMMERCING DIP TO CONTRACT ZRG AT 1-800-831-3276 FOR PRODUCT

- 3. ALL SHAFT REINFORCING IS A572 GR 65.
- 4. PRELIM DESIGN BASED ON FAILING SA BY PAUL J FORD & COMPANY, DATED JUNE 6, 2012.
- 5. EPOXY MUST BE HILTI RE-500.



BASE PLATE



NEW ANCHOR & BRACKET DETAIL



CENSOLUTIONS SHAFT REINFORCING OPTION

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS BU #876362; OXFORD / FRITZ PROPERTY 200 End Board State 1500 - Columbia, Otto 4215 BU #876362; OXFORD / FRITZ PROPERTY

CROWN CASTLE 3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NC 28277 PH: (908) 258-7010 FAX: (301) 789-6649

OXFORD, CT

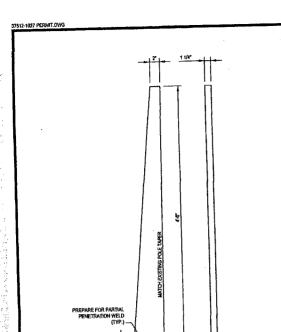
MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

37512-1027 DRAWN BY: B.M.S. CHECKED BY

ISSUE DATE OF PERMIT: 7-6-2012

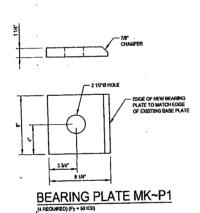
PPROVED BY

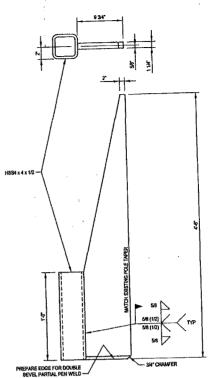
S-5A



TRANSITION STIFFENER MK~TS1

3/4" CHAMFER (DO NOT WELD STIFFENER IN CHAMFER REGION)





ANCHOR BRACKET MK~AB1





AEROSOLUTIONS SHAFT REINFORCING OPTION

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 806 Easi Broad Givert - Bute 1500 - Columbia, Drie 43216 441) 221-4678 - www.phveb.com

CROWN CASTLE 3530 TORINGDON WAY, SUITE 300, CHARLOTTE, NC 28277 PH: (908) 258-7010 FAX: (301) 789-5849

BU #876362; OXFORD / FRITZ PROPERTY OXFORD, CT MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

ISSUE DATE OF PERMIT: 7-8-2012 DRAWN BY: B.M.S. CHECKED BY: T.J.D.

S-6A



AEROSOLUTIONS SHAFT REINFORCING OPTION

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 250 East Brand Strian: - Suite 1500 - Columbus, Office 1216 www.ys/wab.com

CROWN CASTLE

BU #876362; OXFORD / FRITZ PROPERTY OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT No: 37512-1027 DRAWN BY: B.M.S. CHECKED BY:

ISSUE DATE OF PERMIT: 7-6-2012

APPROVED BY S-7A

MODIFICATION INSPECTION NOTES:

GENERAL
THE MODIFICATION INSPECTION (MI) IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS
AND OTHER REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, INJURY THE
MODIFICATION DRAWNIGS, AS DESIGNED BY THE ENGINEER OF RECORD (EOR).

THE MILES TO COMPIRM RISTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN TIBBLE, NOR DOES THE MI MISPECTOR TAKE COMMERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIVENESS AND INTEGRITY RESIDES WITH THE EOR AT ALL TIMES.

ALL WIS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (MEN) OR ENGINEERING SERVICE VENDOR (MESY) THAT IS APPROVED TO PERFORM ELEVATED WORK FOR CROWN. SEE ENGIBUL-10171 LIST OF APPROVED MI VENDORS.

TO ENSINE THAT THE REQUIREMENTS OF THE MI ARE NET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MINISPECTOR BEGIN COMMUNICATING AND COORDINATING AS 500M AS A POIS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE FROACTIVE IN REACHING OUT TO THE OTHER PARTY. IF CONTACT HEFORMATION IS NOT KNOWN, CONTACT YOUR CROWN POINT OF CONTACT (POC).

REFER TO ENG-SOW-10007: MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS

IA MISPECTOR THE MI INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEMING A PO FOR THE MITO, AT A MINIMAN.

- REVIEW THE REQUIREMENTS OF THE MICHECRUST
 WORK WITH THE GO TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOLINDATION INSPECTIONS

THE IN INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR AMERICANCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE RI-FIELD INSPECTIONS, AND SUBMITTING THE MI REPORT

GENERAL CONTRACTOR
THE GG BEQUIRED TO CONTACT THE MINSPECTOR AS SOON AS RECEIVING A POFOR THE NODIFICATION INSTALLATION OR TURNNEY
PROJECT TO, AT ANNIQUAL:

- PRIVEW THE REQUIREMENTS OF THE MICHEOGLIST
 WORK WITH THE MI INSPECTIOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOLIADATION INSPECTIONS
 SETTER UNDERSTAND ALL INSPECTION AND TESTING RECURREMENTS

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REGULARMENTS OF THE MI CHECKLIST AN DENG-SOW-10007.

RECOMMENDATIONS
THE FOLLOWING RECONQUENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING

- If is suggested that the GC provide a minimum of 5 business days notice, preferable 19, to the IM inspectior as to when the SITE will be ready for the IM to be computed.
 The SITE will be ready for the IM to be computed.
 The SITE will be ready for the IM to be computed to the IM to be site of the IM to select

CAMPELLATION OR DELAYS IN SCHEDIALED IN

IF THE GO AND IN INSPECTIOR AGREET O. A DITE ON WHICH THE MI WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, CHOWN

IF THE GO AND IN INSPECTIOR AGREET O. A DITE ON WHICH THE MI WILL BE CONDUCTED, AND EITHER PARTY CANCELLATION OR

SHALL NOT BE RESPONSIBLE FOR CONTROL THE E.B. THAVEL AND LODGING, COSTS OF RESPHOLEDIRED IN OHISTE, ETC., IF CROWN

CONTROLS DEEDLY FOR A THIRD PARTY ME, EXCEPTIONS MAY BE MADE IN THE EVENT THAT THE DELAY/CANCELLATION IS CAUSED BY

WRITTEN OR OTHER CONDITIONS THAT MAY COUPPROMISE THE BAPETY OF THE PARTIES INVOLVED.

CORRECTION OF FAILING NOS

F THE MODIFICATION WISTALIATION WOULD FAIL THE MI ("FAILED MI"), THE GC SHALL WORK WITH CROWN TO COORDINATE A REMEDIATION

- CORRECT FAILING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND
 COORDINATE. A SUPPLEMENT IM.
 OR, MITH CORPINAS APPROVAL, THE GC MAY WORK WITH THE EOR TO RE-AMALYZE THE MODIFICATION PERIFORCEMENT USING THE
 AS-BURLT CONDITION

MUVERFICATION INSPECTIONS
CROWN RESERVES THE ROYIT TO COMPUTET AN VERIFICATION INSPECTION TO VERBY THE ACCURACY AND COMPLETENESS OF PREMIOUSLY COMPLETED MIS SPECTION(S) ON TOWER MODIFICATION PROJECTS.

ALL VERFICATION INSPECTIONS SHALL BE HELD TO THE SAME SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS AND IN ACCORDANCE WITH EINS SOM-1997.

VERIFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT AEVIAEBY FIRM AFTER A MODIFICATION PROJECT IS COMPLETED, AS MARKED BY THE DATE OF AN ACCEPTED "PASSING M" ON "PASS AS NOTED M".

REPORT FOR THE ORIGINAL PROJECT.

PHOTOGRAPHS
BETWEEN THE GO AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A LIMITABLE AND TO BE TAKEN AND INCLUDED IN THE MI
REPORT: PRE-CONSTRUCTION CENERAL SITE CONDITION
PHOTOGRAPHS DURNING THE REINFORCEMENT MODIFICATION CONSTRUCTION FRECTION AND INSPECTION
RAW MATERIALS
PHOTOS OF ALL CRITICAL DETAILS
FOUNDATION MODIFICATIONS
WELD PREPARATION
BOLT RISTALLATION AND TORQUE
FINAL INSTALLED CONDITION
SURFACE CONTROL REPARA
POST CONSTRUCTION PROTOGRAPHS
POST CONSTRUCTION PROTOGRAPHS
FINAL INFELID CONDITION
FINAL INFELID CONDITION

PHOTOS OF ELEVATED MODIFICATIONS TAXEN FROM THE GROUND SHALL BE CONSIDERED MADEQUI

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS, PLEASE REFER TO ENG-SOW-10007

	MI CHECKLIST							
INSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM							
	PRE-CONSTRUCTION							
×	MI CHECKLIST DRAWINGS							
×	EOR APPROVED SHOP DRAWINGS							
×	FABRICATION INSPECTION							
- X	FABRICATOR CERTIFIED WELD INSPECTION							
×	MATERIAL TEST REPORT (MTR)							
NA NA	FABRICATOR NOE INSPECTION							
x	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)							
x	PACKING SLIPS							
ODITIONAL TESTING AND INSPECTIONS:								
	CONSTRUCTION							
x	CONSTRUCTION INSPECTIONS							
	FOUNDATION INSPECTIONS							
x	CONCRETE COMP. STRENGTH AND SLUMP TESTS							
x	POST INSTALLED ANCHOR ROD VERIFICATION							
x	BASE PLATE GROUT VERIFICATION							
x	CONTRACTOR'S CERTIFIED WELD INSPECTION							
NA NA	EARTHWORK: LIFT AND DENSITY							
X	ON SITE COLD GALVANIZING VERIFICATION							
	GUY WIRE TENSION REPORT							
NA NA	GC AS-BUILT DOCUMENTS							
x .	INSPECTION OF BOLT PRETENSION PER AISC BOLT SPEC.							
	INSPECTION OF AJAX BOLTS AND DITS PER REQUIREMENTS ON SHEET S-3							
X X								
ADDITIONAL TESTING AND INSPECTIONS:								
	POST-CONSTRUCTION							
x	MI INSPECTOR REDLINE OR RECORD DRAWING(S)							
×	POST INSTALLED ANCHOR ROD PULL-OUT TESTING							
x	PHOTOGRAPHS							
ADDITIONAL TESTING AND INSPECTIONS:								
F								

NOTE: X DENOTES A DOCUMENT NEEDED FOR THE PM REPORT
NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE PMI REPORT



7/24/2017

AEROSOLUTIONS SHAFT REINFORCING OPTION

CROWN CASTLE

PAUL J. FORD AND COMPANY STRUCTURAL ENGINEERS 200 East Bred Struct Students, Chie 1900 - Columbia, Chie 4078 BU #876362; OXFORD / FRITZ PROPERTY 200 East Bred Struct Students, Chie 1900 - Columbia, Chie 4078 BU #876362; OXFORD / FRITZ PROPERTY OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT No 37512-1027 DRAWN BY: CHECKED BY T.J.D.

ISSUE DATE OF PERMIT: 7-6-2012

PROVED BY

S-8A



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

Sprint Existing Facility

Site ID: CT23XC508

Oxford / Fritz Property 338 Oxford Road Oxford, CT 06478

August 28, 2012

Tel: (781) 273.2500

Fax: (781) 273.3311



August 28, 2012

Sprint Attn: RF Engineering Manager 1 International Boulevard, Suite 800 Mahwah, NJ 07495

Re: Emissions Values for Site CT23XC508 – Oxford / Fritz Property

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 338 Oxford Road, Oxford, CT, for the purpose of determining whether the emissions from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm2). The number of μ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limit for the cellular band is approximately 567 μ W/cm², and the general population exposure limit for the PCS band is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 338 Oxford Road, Oxford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario. Actual values seen from this site will be dramatically less than those shown in this report. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 2 CDMA Carriers (1900 MHz) were considered for each sector of the proposed installation.
- 2) 1 CDMA Carrier (850 MHz) was considered for each sector of the proposed installation
- 3) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 4) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The actual gain in this direction was used per the manufactures supplied specifications.
- 5) The antenna used in this modeling is the RFS APXVSPP18-C-A20. This is based on feedback from the carrier with regards to anticipated antenna selection. This antenna has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario.

Tel: (781) 273.2500 Fax: (781) 273.3311



- 6) The antenna mounting height centerline of the proposed antennas is **150.4 feet** above ground level (AGL)
- 7) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public exposure to RF Emissions.

The anticipated Maximum Composite contributions from the Sprint facility are 10.731% (3.577% from each sector) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **38.521%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government

Scott Heffernan

RF Engineering Director

EBI Consulting

21 B Street

Burlington, MA 01803

Fax: (781) 273.3311

STATE OF THE PARTY

STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

July 12, 2013

The Honorable George R. Temple First Selectman Town of Oxford 486 Oxford Road Oxford, CT 06478-1298

RE: **EM-SPRINT-108-130712** – Sprint Spectrum, L.P. notice of intent to modify an existing telecommunications facility located at 338 Oxford Road, Oxford, Connecticut.

Dear First Selectman Temple:

The Connecticut Siting Council (Council) received a request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72, a copy of which has already been provided to you.

If you have any questions or comments regarding the proposal, please call me or inform the Council by July 26, 2013.

Thank you for your cooperation and consideration.

Very truly yours,

Melanie Bachman

Acting Executive Director

MB/cm

c: Vincent Vizzo, Planning & Zoning Chairman, Town of Oxford



STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

August 10, 2015

Camille M. Mulligan Alcatel-Lucent 1 Robbins Road Westford, MA 01886

RE: Compliance Extension Request

EM-SPRINT-008-130130	93 Old Amity Road	Bethany
EM-SPRINT-009-131008	8 Sky Edge Drive	Bethel
EM-SPRINT-017-131008	371 Terryville Avenue	Bristol
EM-SPRINT-018-130322	39 Carmen Hill Road	Brookfield
EM-SPRINT-033-130920	179 Shunpike Road	Cromwell
EM-SPRINT-034-130920	41 Padanaram Road	Danbury
EM-SPRINT-069-130409	246 East Franklin Street	Danielson
EM-SPRINT-035-130322	126 Ledge Road	Darien
EM-SPRINT-043-130311	310 Prestige Park Road	East Hartford
EM-SPRINT-047-131008	232 South Main Street	East Windsor
EM-SPRINT-051-130606	280 Morehouse Drive	Fairfield
EM-SPRINT-052-130606	45 Maple Ridge Road	Farmington
EM-SPRINT-057-120122	363 Riversville Road	Greenwich
EM-SPRINT-057-131127	9 Sound Shore Dr., a/k/a 12 Sound Shore Drive	Greenwich
EM-SPRINT-059-130819	99 Briar Road	Groton
EM-SPRINT-062-130509	Talmadge Road	Hamden
EM-SPRINT-068-121226	136 Bulls Bridge Road	Kent
EM-SPRINT-076-130819	135 New Road	Madison
EM-SPRINT-077-130828	Olcott Street a/k/a 250 Olcott Street	Manchester
EM-SPRINT-080-131024	21 West Peak Drive	Meriden
EM-SPRINT-081-130716	1 Service Road	Middlebury
EM-SPRINT-084-130124	528 Wheeler's Farm Rd.	Milford
EM-SPRINT-091-130606	302 Ball Pond Road	New Fairfield
EM-SPRINT-095-131008	26 Washinton Street	New London
EM-SPRINT-097-131008	8 Ferris Road	Newtown
EM-SPRINT-097-131129	201 South Main St.	Newtown
EM-SPRINT-103-121226	173/177 West Rocks Road	Norwalk
EM-SPRINT-104-131112	2 Hinkley Hill Road	Norwich
EM-SPRINT-108-130215	20 Great Oak Road	Oxford
EM-SPRINT-108-130401	133 Coppermine Road	Oxford
LM-SPRINT-108-130712	338 Oxford Road	Oxford
EM-SPRINT-119-130314	47 Inwood Road	Rocky Hill



											Carrier Hardy	A SIGNAL AND A					
	Site ID	CT23XC5	08 - Oxford / Fr	itz Property	1												
	Site Addresss		rd Road, Oxford														
	Site Type		Monopole														
							Secto	or 1									
Antenna Number 1a	Antenna Make RFS	Antenna Model APXVSPP18-C-A20	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Power	Antenna Gair in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size		Additional Loss	ERP	Power Density Value	Power Density Percentage
1a 1a	RFS	APXVSPP18-C-A20 APXVSPP18-C-A20	RRH RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150.4	144.4	1/2 "	0.5	0	1386.9474	23.91286	2.39129%
14	I KF3	APAV3PP16-C-AZU	_ ккн	850 MHz	CDMA / LTE	20	1	20	13.4	150.4	144.4	1/2 "	0.5	0		6.723596	1.18582%
	Sector total Power Density Value: 3.577%																
	Sector 2																
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size	PRODUCTION OF THE PROPERTY OF	Additional	ERP	Power Density	Power Density
2a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150.4	144.4	1/2 "	0.5	Loss	1386.9474	Value 23.91286	Percentage
2a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	150.4	144.4	1/2 "	0.5	0	THE PARTY OF THE P	6.723596	2.39129% 1.18582%
														ensity Value:	3.577%	0.723330	1.10302%
							Secto	r 3							3.37770		
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size	1973/01/17/2014/01/01	Additional Loss	ERP	Power Density Value	Power Density
3a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150.4	144.4	1/2 "	0.5	0	NE so and street parties and a finish a fill	23.91286	Percentage 2.39129%
3a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	150.4	144.4	1/2 "	0.5	0		6.723596	1.18582%
														nsity Value:	3.577%	0.723330	1.10302/0

	osite MPE %
Carrier	MPE %
Sprint	10.731%
AT&T	6.830%
Verizon Wireless	20.960%
Fotal Site MPE %	

* Combin his compared to the limited in



APPRO	VALS			
SPRINT REPRESENTATIVES	DATE	APPROVED	APPROVED AS NOTED	DISAPPROVED
SI KINT KEI KESENTATIVES	DATE			
SPRINT RF ENGINEER	DATE		Ш	
SITE OWNER	DATE			
	DATE			

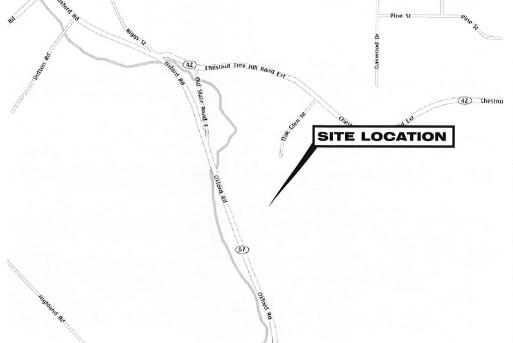
Sprint®

SITE ID: CT23XC508 CROWN CASTLE #876362 SITE NAME: OXFORD / FRITZ PROPERTY

THE STRUCTURAL ENGINEERING CONCERNING THE STRUCTURAL STABILITY OF THE TOWER/POLE, FOUNDATION, ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT IS BEING COMPLETED BY OTHERS. KMB DESIGN GROUP, LLC HAS NOT BEEN REQUESTED TO PERFORM ANY STRUCTURAL ANALYSIS SERVICES TO VERIFY THAT THE TOWER/POLE AND/OR FOLINDATION IS CAPABLE OF SUPPORTING THE PROPOSED FOLIDMENT DEPICTED WITHIN THESE SIGNED AND SEALED DRAWINGS. FURTHERMORE KMB DESIGN GROUP, LLC HAS NOT BEEN REQUESTED TO PHYSICALLY CONFIRM THE EXISTING MOUNT CONFIGURATION AND PERFORM A STRUCTURAL ANALYSIS TO VERIFY THAT THE EXISTING, INTERIM AND PROPOSED ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT CAN BE SAFELY SUPPORTED. SIGNED AND SEALED DRAWINGS REVISED TO STATE "ISSUED FOR CONSTRUCTION" SHALL BE PROVIDED TO THE PROFESSIONAL ENGINEERS RESPONSIBLE FOR THE STRUCTURAL ANALYSIS OF THE TOWER/POLE, ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT. KMB ESIGN GROUP, LLC SHALL BE NOTIFIED SHOULD THE STRUCTURAL ANALYSIS RESULT IN SOME ELEMENTS NOT BEING STRUCTURALLY CAPABLE OF SUPPORTING THE PROPOSED DESIGN DEPICTED. THE CONTRACTOR SHALL NOT COMMENCE CONSTRUCTION WITHOUT OBTAINING (A) A SIGNED AND SEALED COPY OF THE PLANS "ISSUED FOR CONSTRUCTION"; (B) STRUCTURAL ANALYSIS REPORT STATING THAT THE TOWER/POLE/FOUNDATION IS CAPABLE OF SUPPORTING THE PROPOSED LOADING REFERENCING THE SIGNED AND SEALED PLANS BY KMB DESIGN GROUP, LLC: (C) SPRINT PLATFORM ANALYSIS STATING THAT THE SPRINT PLATFORM IS CAPABLE OF SUPPORTING THE PROPOSED DESIGN AS REFERENCED WITHIN THE SIGNED AND SEALED PLANS BY KMB DESIGN GROUP, LLC.

NETWORK VISION CONSTRUCTION DRAWINGS





AERIAL VIEW

CODES & STANDARDS

A SE	DWG#	DRAWING TITLES	These
H S	A01	COVER SHEET	111636
ATE(C01	GENERAL NOTES 1 OF 2	State
POR	C01A	GENERAL NOTES 2 OF 2	
UP.	C02	COMPOUND PLAN	2003
SING	C02A	ELEVATION	2003
IGN	C03	EQUIPMENT PLANS	2003
DES	C03A	EQUIPMENT & ANTENNA SPECIFICATIONS	2003
AND	C04	EXISTING ANTENNA PLAN (ALL SECTORS)	2003
OF P	C04A	INTERIM ANTENNA PLAN (ALL SECTORS)	ICC/A
E ID	C04B	FINAL ANTENNA PLAN (ALL SECTORS)	2005
IZAT	C05	SITE DETAILS	2000
AN P	C06	RF SCHEDULE	
AUT	C06A	RF DATA SHEET	
CUM	C07	AAV DRAWINGS - COVER SHEET	1. [
8 E	C07A	AAV DRAWINGS - SITE PHOTOS	2. 7
E N	C07B	AAV DRAWINGS - COMPOUND PLAN	E
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OWNERSHIP OF DOCUMENTS. THIS DOCUMENT AND THE IDEAS AND DESIGNS INCORPORATED HERE! OTHER PROJECTS WITHOUT THE WRITTEN AUTHORIZATION OF KMB DESIGN GROUP, LLC. IT IS UNLAM			(
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DRAWING INDEX

se documents are in compliance & all construction to be in accordance with the following codes & standards as applicable:

LOCATION MAP

te Building Code: 2005 Connecticut Supplement

3 International Building Code

3 International Residential Code 3 International Existing Building Code

3 International Mechanic Code

3 International Plumbing Code

3 International Energy Conservation Code (re-adopted with changes)

ANSI A117.1-2003 Assessible and Usable Buildings and Facilities

5 National Electrical Code (NFPA-70)

DRIVING DIRECTIONS

- DEPART 1 INTERNATIONAL BLVD, MAHWAH, NJ 07495 TAKE 3RD EXIT FROM ROUNDABOUT INTERNATIONAL BLVD ONTO LEISURE LN
- TAKE RAMP ONTO STATE HIGHWAY 17 (RT-17 N).
- CONTINUE ON I-287 N. TAKE THE I-87 S/I-287/NEW YORK STATE THRUWAY SOUTH/TAPPAN ZEE BR/NEW YORK CITY EXIT ONTO NEW YORK STATE THRUWAY SOUTH (I-287 E, I-87 S) (PARTIAL
- KEEP RIGHT ONTO NEW YORK STATE THRUWAY SOUTH (I-87 S) TOWARD RT-119/SAW MILL PKWY NORTH/SAW MILL PKWY SOUTH/NEW YORK CITY/ELMSFORD
- TAKE EXIT #8A/RT-119/SAW MILL PKWY NORTH/ELMSFORD ONTO SAW MILL PKY NORTH, SAW MILL RIVER PKY N TOWARD SAW MILL RIVER PKWY NORTH/KATONAH.
- TAKE LEFT RAMP ONTO I-684 N TOWARD BREWSTER.
- TAKE EXIT #9E/I-84 E/DANBURY ONTO I-84 E. TAKE EXIT #15/US-6 E/CT-67/SOUTHBURY TOWARD US-6 E/CT-67 N/WOODBURY/ROXBURY.
- TURN RIGHT ONTO CT-67, YOUR DESTINATION ON OXFORD RD (CT-67) IS ON THE LEFT

SITE INFORMATION

BLOCK: 9 LOT: 34A ZONING CLASSIFICATION: TBD ZONING JURISDICTION: TBD

PROJECT INFORMATION:

SITE ADDRESS: 338 OXFORD ROAD OXFORD CT, 06478 NEW HAVEN COUNTY

COORDINATES:

N 41° 25' 40.98" W 73° 06' 30.92" DATUM: NAD 83 LATITUDE: LONGITUDE:

STRUCTURE HEIGHT: ±150'-0" (TOP OF EXISTING MONOPOLE) PROJECT DIRECTORY

PROPERTY OWNER:

CROWN CASTLE USA 2000 CORPORATE DRIVE CANONSBURG, PA 15317

APPLICANT: SPRINT-NEXTEL 6200 SPRINT PARKWAY OVERLAND PARK, KS 66251

ENGINEER: KMB DESIGN GROUP, LLC 1800 ROUTE 34, SUITE 209 WALL, NJ 07719 KEITH DRENNAN - PROJECT MANAGER

(732) 280-5623 POWER COMPANY CONNECTICUT LIGHT & POWER P.O. BOX 270

HARTFORD, CT 06141-0270 (800) 286-2000

CONSTRUCTION MANAGER: TODD AMANN (914) 715-9363

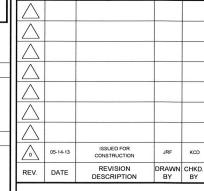
CROWN CASTLE CONSTRUCTION MANAGER: MIKE CALLAHAN (860) 919-7278

NO CONSTRUCTION IS TO COMMENCE

PRIOR TO CROWN CASTLE APPROVAL

Sprint'







Stephen A. Bray



CT LICENSE: 26657

5/16/13

332.1485

338 OXFORD ROAD

OXFORD, CT 06478 **NEW HAVEN COUNTY**

CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

04-19-12 JLS

> COVER SHEET

A01

GENERAL CONSTRUCTION NOTES:

- 1. This set of plans has been prepared for the purposes of municipal and agency review and approval. This set of plans shall not be utilized as construction documents until all drawings have been revised to indicate "ISSUED FOR CONSTRUCTION." Contractor shall e-mail plans@kmbdg.com to ensure that they have the latest set of construction drawings prior to commencing any work whatsoever.
- ADA compliance: The facility is a normally unoccupied mobile radio facility
- These plans are intended to be used to direct the proposed layout. Drawings should not be scaled unless
 otherwise noted. Plans, elevations and details are intended to show the end result of design. Minor
 modifications may be required to suit job dimensions or conditions.
- The contractor shall verify all dimensions and conditions and notify the Project Manager of any discrepancies before starting any work.
- 5. These plans are designed to reflect observed field conditions. Certain conditions are assumed to comply with general standard construction design methods and principles, and the Contractor shall note that not all areas of structural attachment have been opened or specifically verified. The Contractor is therefore requested to notify the Engineer immediately should encountered field conditions vary from those depicted on the drawings. KMB Design Group, LLC will issue field change direction if required. The Project Manager is referenced on the cover sheet.
- All equipment and materials shall be installed in accordance with the manufacturer's recommendations
 unless otherwise noted by the Engineer of Record.
- 7. The Contractor shall be responsible for all work performed and materials installed to be in strict conformance, as a minimum standard, with all applicable codes, regulations and ordinances having jurisdiction. Electrical systems shall be installed in conformance with the National Electrical Code, and all other local and state jurisdictional codes, ordinances, and with local utility company specifications, whichever is more stringent.
- 8. The Contractor shall keep contract area clean, hazard free and dispose of all dirt, stumps, stones, rubbish or debris in accordance with all local and environmental laws. No materials or equipment shall be placed anywhere on or in the structure without making adequate provisions to protect existing property. Upon completion, repair any damage that may have occurred during construction. Repair all existing wall surfaces damaged during construction such that they match and blend with adjacent surfaces.
- The Contractor shall be solely responsible and have control over construction means, methods techniques, sequences, and procedures.

SPRINT SPECIFICATIONS:

- . Contractor shall ensure that they obtain the latest copy of the following documents from ALU:
- A. Cell Site Installation & De-Installation Services Attachment G-1
- B. Sprint Integrated Construction Standards for Wireless Sites
- C. Standard Construction Specifications for Wireless Sites
- Contractor shall notify the Engineer immediately if any of the Sprint standards contradict the standards provided by KMB Design Group, LLC so that the Engineer can provide direction.
- B. State, Federal and Local codes prevail.

DIVISION 1 - GENERAL REQUIREMENTS SECTION 01010 SUMMARY OF WORK:

- The Contractor shall review and become familiar with specifications contained in the bid package
 prepared by KMB Design Group, LLC and the client. The Contractor shall e-mail plans@kmbdg.com to
 ensure that they have the latest set of construction drawings prior to commencing any work whatsoever.
- In the event of a conflict between the bid package specifications and these notes, the provisions of the clients specifications shall take precedence.
- 3. The Contractor shall visit the site of the proposed work and fully acquaint themselves with the conditions as they exist in order that any restrictions pertaining to the work are understood. All areas and dimensions are indicated on the drawings as accurately as possible, but all conditions shall be verified by each contractor and/or subcontractor at the site. The failure of the contractor to examine or receive any form, instrument or document, or to visit the site shall not relieve the Contractor from any obligation with respect to their quoted price. The submission of a quotation shall acknowledge that the Contractor and their Subcontractors have fully examined the site and know the existing conditions and have made provisions for operating under the conditions as they exist at the site and have included all necessary items.
- The General Contractor's responsibilities shall include, but not be limited to, construction of the
 equipment foundation, including electrical service, telephone conduits, grounding system and
 coordination with local utility companies.
- 5. The antenna installers responsibilities shall include, but not be limited to, cable tray installation, routing of cables from radio equipment to antennas, associated hardware for securing antenna cables, antenna mounts, determining supplier of antennas, grounding of antennas to grounding system, installing antennas and verifying with Radio Frequency Engineers, the alignment, location, and proper orientation of antennas.
- The Contractors shall coordinate construction activities with the Crown Castle Construction Manager in order to avoid conflicts with current use of the site.
- The Contractor shall conform to all applicable local, county, state, and federal codes, laws and requirements, including OSHA.
- The Contractor shall apply and pay for the construction permit, certificate of occupancy and all other required permits or licenses. The Contractor is responsible for obtaining all inspections.
- 9. Safety procedures: Attention is directed to federal, state, and local laws, rules and regulations concerning construction safety and health standards. The construction company awarded this project shall ensure all working surroundings and conditions are sanitary, and are not hazardous or dangerous to the health or safety of the work crews or building occupants. Precaution shall be exercised at all times for the protection of persons and property. It is mandatory that the safety provisions of applicable local laws, OSHA regulations and building and construction codes, be observed for all contractors and antenna ringers.

SECTION 01613 - DELIVERY, STORAGE AND HANDLING:

- The Contractor shall be responsible for all procedures and scheduling associated with hoisting, staging, and erecting of materials and equipment to and/or upon the site.
- All elements of the existing site, i.e. structures, site plantings, etc. shall be protected as necessary from said actions. This work must be done in a safe, secure nondestructive manner for protecting personnel and property.

SECTION 01740 WARRANTIES AND BONDS:

- The Contractor shall guarantee all labor and materials used in this project for a minimum period of one

 (1) year commencing from the date of final acceptance by the client. The Contractor is not required to guarantee material supplied by the Owner.
- Final date of acceptance is deemed as the date that all required state and federal approval have been obtained including, but not limited to:
 - A. Final inspection
 - B. Certificate of Occupancy
- 3. Any deficiencies that come evident during this one (1) year period shall be corrected by the Contractor at the Contractor's expense

Sprint Sprint

Icatel·Lucent

CONSTRUCTION

REV. DATE

REVISION

DESCRIPTION

BY

BY

BY



Stephen A. Bray



332.1485

SITE INFORMATION:

338 OXFORD ROAD OXFORD, CT 06478 NEW HAVEN COUNTY

CROWN CASTLE # 876362 CT23XC508

SIGN TYPE:

NETWORK VISION

CHECKED BY: DATE: 04-19-12

JLS SHEET TITLE:

GENERAL NOTES 1 OF 2

SHEET NUMBER:

C01

0

- 1. The Contractor shall call utilities prior to the start of construction
- All existing active sewer, water, gas, electric, and other utilities where encountered in the work, shall be
 protected at all times, and where required for the proper execution of the work, shall be relocated as
 directed by Engineers. Extreme caution should be used by the Contractor when excavating or pier drilling
 around or near utilities. The Contractor shall provide safety training for the working crew. This will include
 but not limited to:
- A. Fall protection
- B. Confined spaceC. Electrical safety
- D. Trenching & excavation
- . All site work shall be as indicated on the drawing and stipulated in the specification project summary.
- If necessary, rubbish, stumps, debris, sticks, stones, and other refuse shall be removed from the site and disposed of legally.
- The site shall be graded to cause surface water flow away from the equipment shelter and monopole areas.
- No fill or embankment material shall be placed on frozen ground. Frozen materials, snow or ice shall not be placed in any fill or embankment.
- The sub grade shall be compacted and brought to a smooth uniform grade prior to finished surface application.
- All existing inactive sewer, water, gas, electric and other utilities, which interfere with the execution of the
 work, shall be removed and/or capped, plugged or otherwise discontinued at points which will not
 interfere with the execution of the work, subject to the approval of engineering.
- The areas of the Owners property disturbed by the work and not covered by the building or driveway, shall be graded to a uniform slope, fertilized, seeded, and covered with mulch as specified in the specification of landscape work.
- The Contractor shall minimize disturbance to existing site during construction. Erosion control measures, shall be in conformance with the local guidelines for erosion and sediment control.
- All back fill shall be compacted to 95% modified proctor density as determined by ASTM standard test procedures.

DIVISION 3 - CONCRETE

- Design and construction of all concrete elements shall conform to the latest editions of the following applicable codes: ACI 301 "Specifications for Structural Concrete for Buildings", ACI 318 "Building Code Requirements for Reinforced Concrete".
- 2. Mix design shall be approved by Owner's representative prior to placing concrete
- Concrete shall be normal weight, 6% air entrained (±1.5%) with a maximum 4" slump, and have a minimum 28-day compressive strength of 3000 psi unless otherwise noted.
- 4. Maximum aggregate size shall be 1".
- 5. The following materials shall be used:

Portland cement: ASTM C 150, TYPE I
Reinforcement: ASTM A 185
Normal weight aggregate: ASTM C 33

mal weight aggregate: ASTM C 33 er: Drinkable

Admixtures: Non-chloride containing

- 6. Reinforcing details shall be in accordance with the latest edition of ACI 315.
- Reinforcing steel shall conform to ASTM A 615, grade 60, deformed unless noted otherwise. Welded wire fabric shall conform to ASTM A 185 welded steel wire fabric unless noted otherwise. Splices shall be class "B" and all hooks shall be standard, unless otherwise noted.
- The following minimum concrete cover shall be provided for reinforcing steel unless shown otherwise on drawings:
- A 1" chamfer shall be provided at all exposed edges of concrete, unless otherwise noted, in accordance with ACI 30 section 4.2.4
- 10. Installation of concrete anchor, shall be per manufacturers written recommended procedure, the anchor bolt, dowel or rod shall conform to manufacturer's recommendation for embedment depth or as shown on the drawing. No rebar shall be cut without prior engineering approval when drilling holes in concrete.
- 11. Curing compounds shall conform to ASTM C-309.
- 12. Admixtures shall conform to the appropriate ASTM standard as referenced in ACI-301
- 13. Do not weld or tack weld reinforcing steel.

Beams and columns

- 14. All dowels, anchor bolts, embedded steel, electrical conduits, pipe sleeves, grounds and all other embedded items and formed details shall be in place before start of concrete placement.
- Locate additional construction joints required to facilitate construction as acceptable to Engineer. Place reinforcement continuously through joint.
- Reinforcement shall be cold bent whenever bending is required.
- 17. Place concrete in a uniform manner to prevent the formation of cold joints and other planes of weakness. Vibrate the concrete to fully embed reinforcing. Do not use vibrators to transport concrete thorough chutes or formwork.
- 18. Do not place concrete in water, ice, or on frozen ground.
- Do not allow concrete sub base to freeze during concrete curing and setting period, or a minimum of 14 days after placement.
- For cold -weather and hot-weather concrete placement, conform to applicable ACI codes and
 recommendations. In either case, materials containing chloride, calcium, salts, etc. shall not be used.
 Protect fresh concrete from weather for 7 davs minimum.

DIVISION 5 - METALS

SECTION 05120 - STRUCTURAL STEEL

Codes and specifications:

- A. The fabrication/erection shall conform to the requirements of the following codes and specifications, latest edition, unless otherwise noted:
- The local building code.
- AISC-specification for structural steel buildings, allowable stress design, 1989.
- ASTM A992 structural steel (for all w sections only).
- ASTM A36 structural steel (all other sections).
- ASTM A53, type E, grade B, electric resistance welded steel pipe.
- ASTM 123 zinc (hot-dip galvanized) coatings on iron and steel products.
- ASTM 153 zinc coated (hot-dip) iron and steel hardware.
- AWS D1.1 structural welding code.
- EIA/TIA-222 structural standards for steel antenna towers and antenna supporting structures.

Design parameters:

A. The structural steel antenna mounting frames are designed to provide support for antennas and all hardware and accessories associated with antennas

3. Fabrication and installation requirements:

- A. The antenna supports, antennas and mounting hardware shall be constructed plumb, level and true.
- B. All structural elements and fasteners shall be galvanized in accordance with ASTM A123 and A153.
- C. Welds should be shop made wherever possible, conforming to AISC specification and AWS requirements. All welds are to be of the size and type indicated. Contractor shall employ a licensed welder and shall provide the engineer with their name and a copy of their license prior to commencing any field welding.
- D. Contractor shall provide fire watch during all welding operations, brazing and soldering and other work requiring the use of an open flame. Two (2) hand held 30 lb fire extinguishers and adequate water supply shall be maintained on site. Fire watch plan shall be submitted to the client for approval prior to welding.
- E. All bolted connections shall be A325 high strength bolts 5/8" diameter minimum size unless otherwise noted. Bolts shall be supplied with flat washers. Bolts shall be tightened in accordance with the AISC snug tight condition, unless otherwise noted.
- F. Protective galvanized coatings which were damaged or removed during erection or transportation shall be restored by painting with zinc-rich primer.
- G. All threaded rods shall be 1/2" diameter A36 steel unless otherwise noted.
- H. Temporary structures for staging and construction shall be capable of withstanding forces specified by the local building code current edition.

Inspections:

- A. All structural steel antenna frames, and connections shall be inspected prior to installation of antennas
- B. All antenna cable trays, supports, channels and clamps shall be inspected prior to installation of antenna cables.
- C. Coordinate all inspections with the client's Construction Manager.
 D. Contractor to make notifications 72 hours prior to any required inspections.

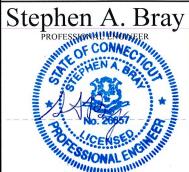
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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY
\triangle	05-14-13	ISSUED FOR CONSTRUCTION	JRF	KCD
\triangle				



1800 ROUTE 34, SUITE 209 WALL, NJ 07719 (732) 280-5623



CI	LICENS	E: 26657

332.1485

338 OXFORD ROAD OXFORD, CT 06478 NEW HAVEN COUNTY

CROWN CASTLE # 876362 CT23XC508

DESIGN TYPE:

NETWORK VISION

N BY: CHECKED BY: DATE: 04-19-12

JLS

GENERAL NOTES 2 OF 2

SHEET NUMBER:

 $C01\Lambda$

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5/16/13

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Stephen A. Bray PROFESSIONAL ENGINEER

CT LICENSE: 26657 5/16/13

332.1485

338 OXFORD ROAD OXFORD, CT 06478 NEW HAVEN COUNTY

CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

JLS

04-19-12

COMPOUND PLAN

SHEET NUMBER

C02

HOME RUN GROUNDS NOT APPROVED. ALL ANTENNA BUSS BARS SHOULD BE INSTALLED DIRECTLY TO TOWER STEEL WITHOUT INSULATORS OR DOWN CONDUCTORS.

GROUNDING NOTES:

- CABLING NOTES:

 1. PROPOSED CABLING TO FOLLOW EXISTING ROUTE AND METHOD OF ATTACHMENT AT INTERIM.

 2. EXISTING COAXIAL CABLES TO BE REMOVED AT FINAL.
- CONTRACTOR TO REPAIR/REPLACE ANY MISSING/DAMAGED CABLE TRAY AND ADD HURRICANE STRAPS AS REQUIRED IF APPLICABLE.

- GENERAL NOTES:

 1. FINAL ANTENNA & EQUIPMENT CONFIGURATION SHOWN ON THIS PLAN. SEE EQUIPMENT & ANTENNA PLAN SHEETS FOR EXISTING AND INTERIM CONFIGURATION.

 2. CONTRACTOR TO REPLACE ALL MISSING GROUND BARS AND GROUNDING CONNECTIONS AS REQUIRED WITH GALVANIZED GROUND BARS. CONTRACTOR SHALL PROVIDE BEFORE & AFTER PHOTOS.
- CONTRACTOR TO RESTORE ANY RUST AREA TO ORIGINAL CONDITION AND PROTECTIVE COATING TO BE APPLIED. STRUCTURAL ANALYSIS PROVIDED UNDER SEPARATE COVER. PROPOSED SPRINT 1600 MHz GPS UNIT TO REPLACE EXISTING GPS AT FINAL.

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■ PROFESSIONAL ENGINEER



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5/16/13

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338 OXFORD ROAD OXFORD, CT 06478 **NEW HAVEN COUNTY**

CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

JLS SHEET TITLE

ELEVATION

C₀₂A

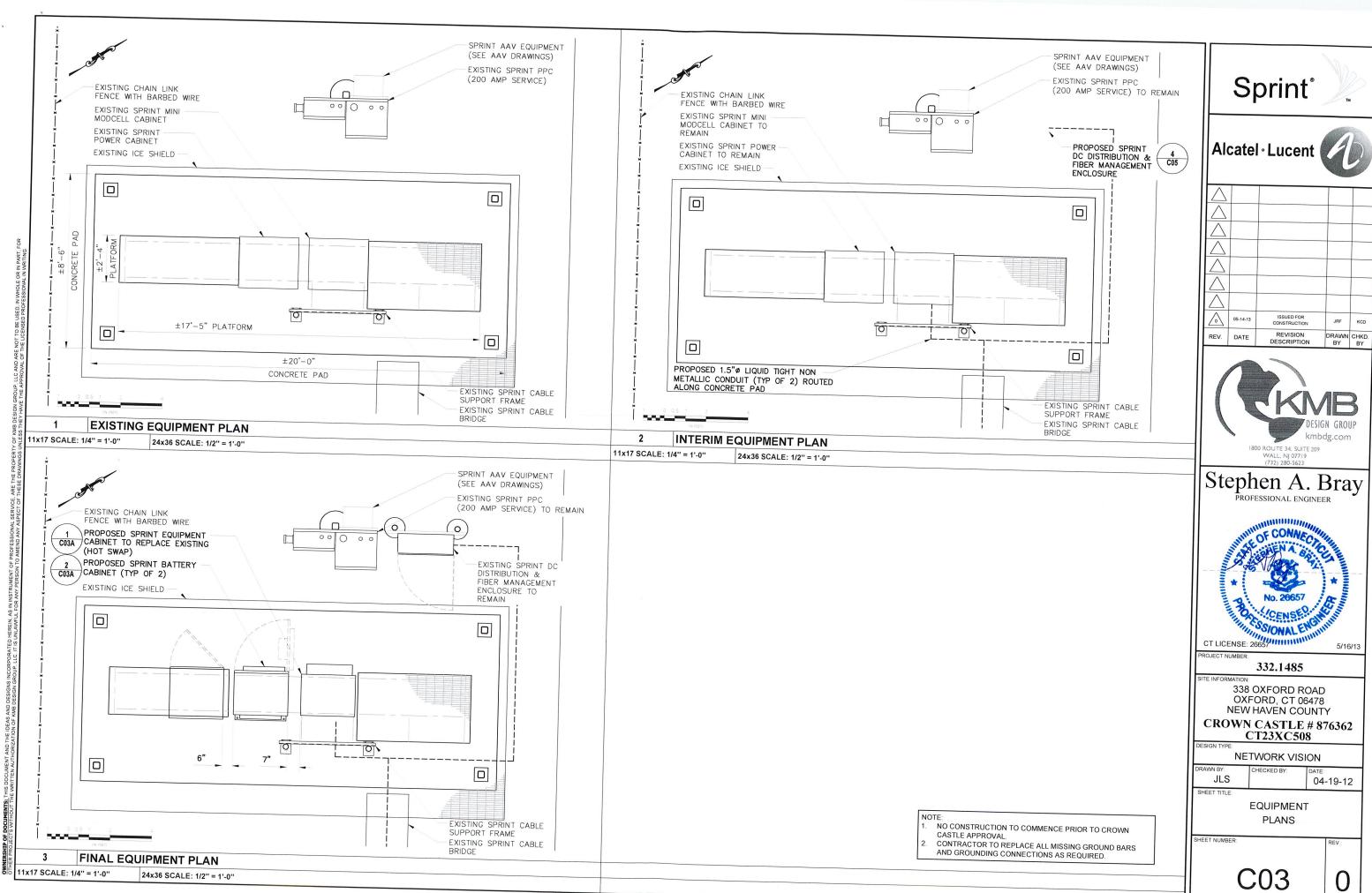
04-19-12

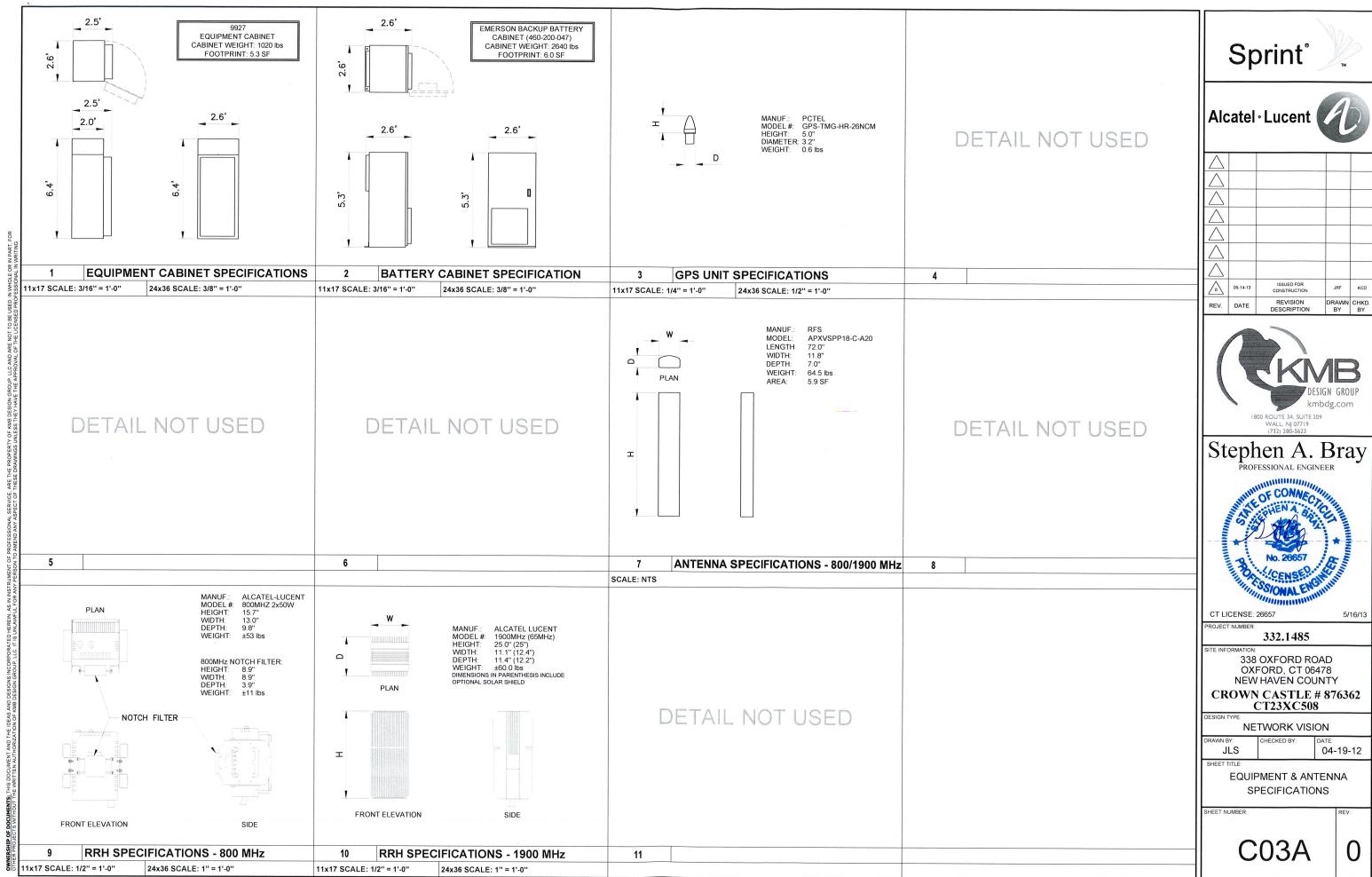
NO CONSTRUCTION TO COMMENCE PRIOR TO CROWN CASTLE APPROVAL.

FINAL ANTENNA & EQUIPMENT CONFIGURATION SHOWN ON THIS PLAN. SEE EQUIPMENT & ANTENNA PLAN SHEETS FOR EXISTING AND INTERIM CONFIGURATION.

NORTHWEST ELEVATION 1x17 SCALE: 1" = 20'

24x36 SCALE: 1" = 10'





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. Akatel-Lucent(332.1485_CT23XC508_338 Oxford Road(332.1485_CAD)(332.1485_Construction)(332.1485_C03A.chvg_5/16/2013 9

NOTES:
1. NO CONSTRUCTION TO COMMENCE PRIOR TO CROWN CASTLE APPROVAL.

EXISTING ANTENNA PLAN (ALL SECTORS)

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ISSUED FOR CONSTRUCTION

REVISION DESCRIPTION

Stephen A. Bray

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338 OXFORD ROAD OXFORD, CT 06478 **NEW HAVEN COUNTY** CROWN CASTLE # 876362 CT23XC508 NETWORK VISION

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REV.

05-14-13

DATE

CT LICENSE: 26657

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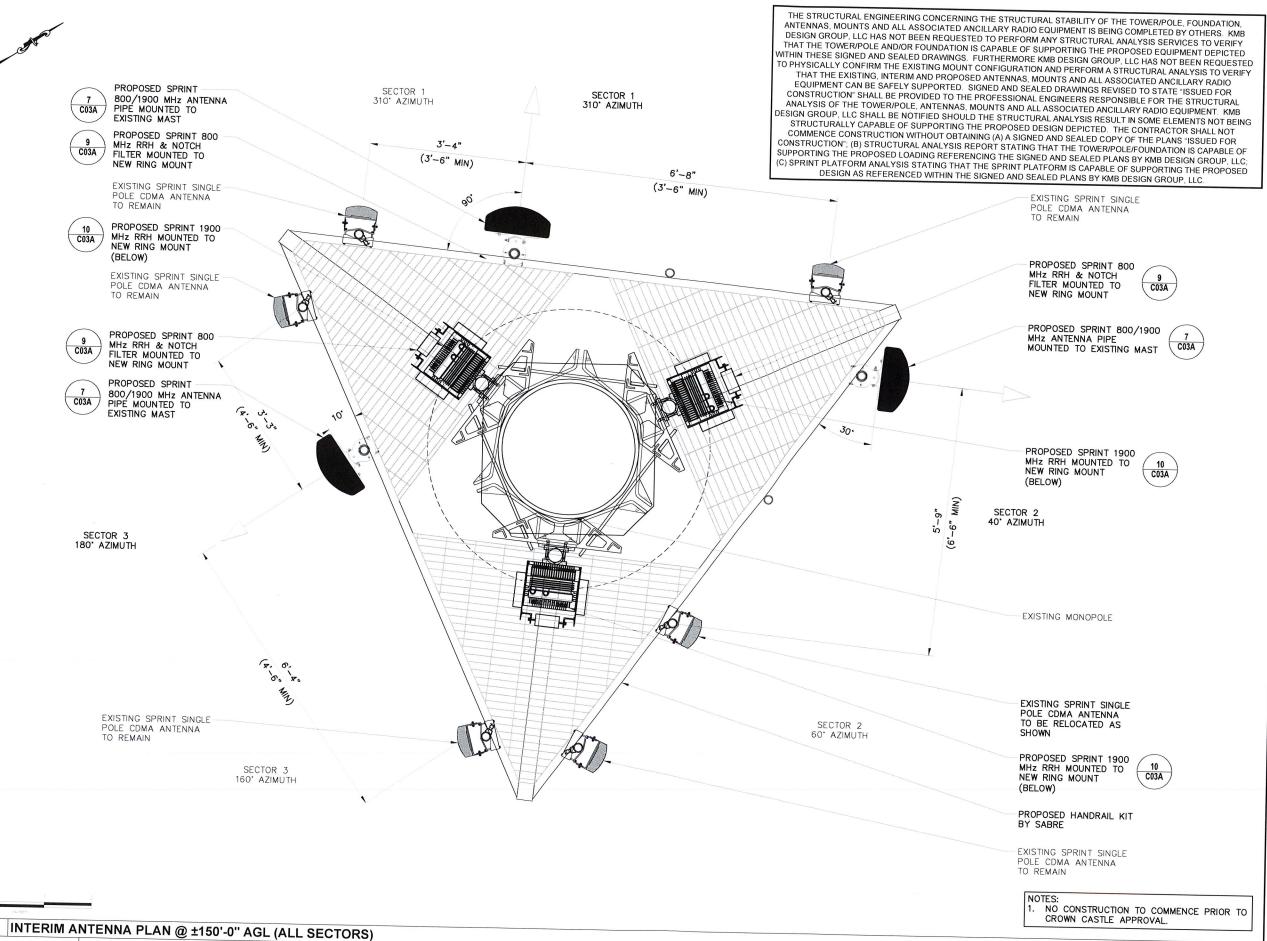
C04

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04-19-12

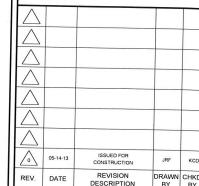
EXISTING ANTENNA PLAN @ ±150'-0" AGL (ALL SECTORS) 11x17 SCALE: 1/2" = 1'-0"

24x36 SCALE: 1" = 1'-0"





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Stephen A. Bray PROFESSIONAL ENGINEER



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338 OXFORD ROAD

OXFORD, CT 06478 **NEW HAVEN COUNTY**

CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

JLS

04-19-12

5/16/13

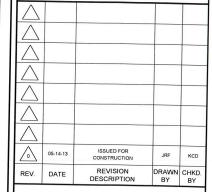
INTERIM ANTENNA PLAN (ALL SECTORS)

C04A

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CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

JLS

04-19-12

FINAL ANTENNA PLAN (ALL SECTORS)

C04B

11x17 SCALE: 1/2" = 1'-0"

24x36 SCALE: 1" = 1'-0"

11x17 SCALE: 3/4" = 1'-0"

24x36 SCALE: 1 1/2" = 1'-0"

1x17 SCALE: 3/4" = 1'-0"

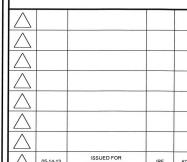
24x36 SCALE: 1 1/2" = 1'-0"

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THE STRUCTURAL ENGINEERING CONCERNING THE STRUCTURAL STABILITY OF THE TOWER/POLE, FOUNDATION, ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT IS BEING COMPLETED BY OTHERS. KMB



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REVISION

DESCRIPTION

DATE

DRAWN CHKD

Stephen A. Bray

WALL, NJ 07719

PROFESSIONAL ENGINEER



CT LICENSE: 26657

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338 OXFORD ROAD OXFORD, CT 06478 **NEW HAVEN COUNTY**

CROWN CASTLE # 876362 CT23XC508

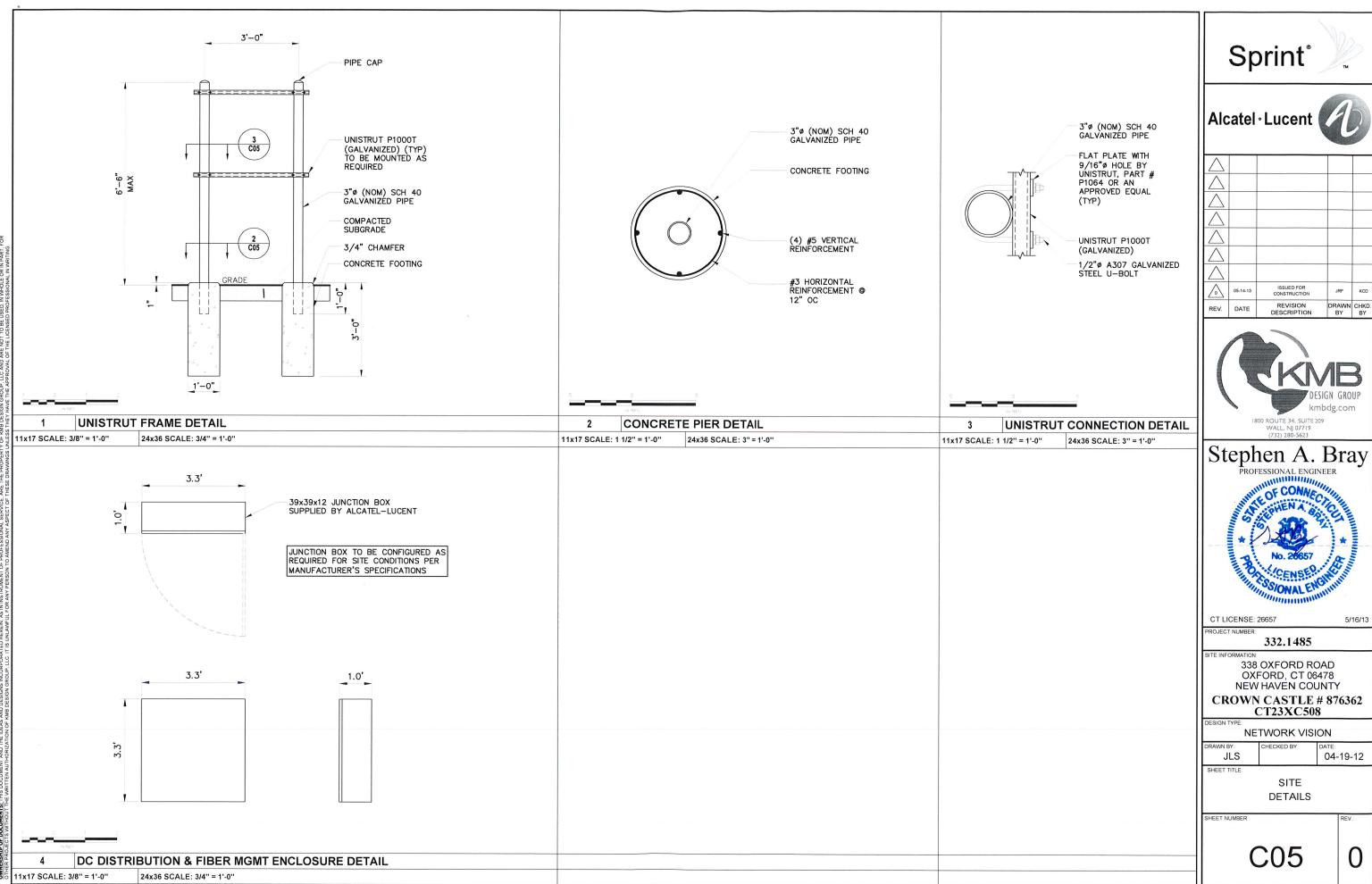
NETWORK VISION

JLS 04-19-12

ANTENNA & RRH MOUNT DETAILS (ALL SECTORS)

C04C

5/16/13





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Stephen A. Bray



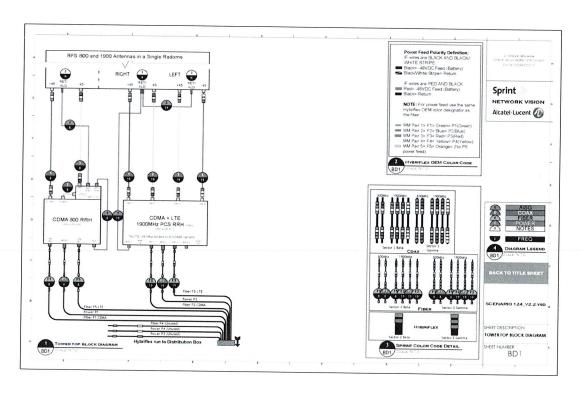
04-19-12

_	FINIAL ANTENNA AND THE															CASCAMA I
_			_			FIN	NAL ANTENNA AN	D C	ABL	E SC	CHEDULE					
SECTOR	AZIMUTH (DEGREES)		(DEGREES) MECHANICAL DT (DEGREES)	ELECTRICAL DT (DEGREES)	RAD CENTER AGL		ANTENNA	R	RH		P COAX UMPER	COM	IBINER MPER	NOTCH JUI	H FILTER MPER	HYBRIFLEX
SE		AZ (DE	MEC DT (0	ELEC DT (D	(FT)	MAKE	MODEL	Q	TY	QTY	LENGTH (FT)	QTY	LENGTH (FT)	QTY	LENGTH (FT)	LENGTH (FT)
	_															
1	800/1900	310	0	800 1900 -8 -4	150	RFS	APXVSPP18-C-A20	800	1900	6	10	_	_	1	3	
	_															200
_	_															
	800/1900	40	0	800 1900 0 0	150	RFS	APXVSPP18-C-A20	800	1900	6	10	-	_	1	3	
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NO	-															

- DUE TO FIELD MEASUREMENTS AND THE INSTALLATION OF NEW ANTENNAS THAT VARY IN SIZE FROM THE EXISTING ANTENNAS, THE ANTENNA RAD CENTER HAS CHANGED FROM WHAT IS ON RECORD. THE DATABASE MAY NEED TO BE UPDATED TO MATCH THESE PLANS.

 SOME CABLING MAY CHANGE AT THE TIME OF CONSTRUCTION. CONTRACTOR TO CONFIRM ALL CABLE LENGTHS, TYPE, QUANTITIES, AND CONFIGURATION PRIOR TO CONSTRUCTION. ALL UNUSED POWER AND FIBER MUST BE PROPERLY TERMINATED AND WEATHERPROOFED.

CONTRACTOR TO VERIFY & USE THE LATEST TOWER TOP SCENARIO AS PROVIDED BY ALCATEL-LUCENT CONSTRUCTION MANAGER



Sprint[®] Alcatel · Lucent REVISION DESCRIPTION REV. DATE 1800 ROUTE 34, SUITE 209 WALL, NJ 07719 (732) 280-5623 Stephen A. Bray CT LICENSE: 26657 5/16/13 332.1485 338 OXFORD ROAD OXFORD, CT 06478 NEW HAVEN COUNTY CROWN CASTLE # 876362 CT23XC508 **NETWORK VISION** JLS 04-19-12 RF SCHEDULE C06

4	Cascade ID	CT23XC508		
		SECTOR 1	SECTOR 2	SECTOR 3
	Split sector present	No	No	No
I	1900MHz_Azimuth	310	40	180
[1900MHz_No_of_Antennas	1	1	1
Γ	1900MHz_RADCenter(ft)	150	150	150
Γ	1900MHz_Antenna Make	RFS	RFS	RFS
777	1900MHz_Antenna Model	APXVSPP18-C-A20	APXV5PP18-C-A20	APXVSPP18-C-A20
	1900MHz_Horizontal_Beamwidth	65	65	65
9	1900MHz_Vertical_Beam width	5.5	5.5	5.5
	1900MHz_AntennaHeight (ft)	6	6	6
	1900MHz_AntennaGain(dBd)	15.9	15.9	15.9
-	1900MHz_E_Tilt	-4	0	0
,	1900MHz _M_Tilt	0	0	0
,	1900MHz_Carrier_Forecast_Year_2013	2	2	2
-	1900MHz RRH Manufacturer	ALU	ALU	ALU
-	1900MHz_RRH Model	RRH 1900 4X45 65MHz	RRH 1900 4X45 65MHz	RRH 1900 4X45 65MHz
-	1900MHz_RRH Count	1	1	1
-	1900MHz_RRH Location	Top of the Pale/Tower	Top of the Pole/Tower	Top of the Pale/Tower
	1900MHz Com biner Model	No Combiner Required	No Combiner Required	No Com biner Required
-	1900MHz_Top_Jumper #1_Length (RRH or Combiner-to-Antenna for TT or Main Coax to	10	10	10
-	1900MHz_Top_Jumper #1_Cable_Model (RRH or Combiner-to-Antenna for TT or Main Coax	LCF12-50J	LCF12-50J	LCF12-50J
-	1900MHz_Top_Jumper #2_Length (RRH to Combiner for TT if applicable, ft)	N/A	N/A	
	1900MHz_Top_Jumper #2_Cable_Model (RRH to Combiner for TT if applicable)			N/A
_	1900MHz_Main_Coax_Cable_Length (ft)			N/A
-	1900MHz_Main_Coax_Cable_Model			N/A
-		N/A N/A N/A del N/A N/A ength (Ground based RRH to Combiner-OR-Main Coax, ft) N/A N/A able_Model (Ground based RRH to Combiner-OR-Main Coax) N/A N/A ength (Ground based-Combiner to Main Coax, ft) N/A N/A	N/A	
1				N/A
_				N/A
	1900MHz_Bottom_Jumper #2_Cable_Model (Ground based-Combiner to Main Coax)	N/A N/A	N/A N/A	N/A N/A
_	800MHz Azimuth			
-	800MHz_No_of_Antennas	310	40	180
_	800MHz_RADCenter(ft)	0	0	0
-	800MHz_AntennaMake	150	150	150
•	bounitz_Airteilliamake	RFS	RFS	RFS
,	900killa Antononikodol	APXVSPP18-C-A20 (Shared	PRODUCT STATES COME TO THE PARTY MADE AT ADDRESS OF THE PARTY AND THE PA	APXVSPP18-C-A20 (Share
-	800MHz_AntennaModel	w/1900)	w/1900)	w/1900)
-	800MHz_Horizontal_Beamwidth	65	65	65
_	800MHz_Vertical_Beamwidth	11.5	11.5	11.5
-	800MHz_AntennaHeight (ft) 800MHz_AntennaGain (dBd)	6	6	6
-	-	13.4	13.4	13.4
-	800MHz_E_Tit	-8	0	-1
-	800MHz_M_Tilt	0	0	0
-	800MHz_RRH Manufacturer	ALU	ALU	ALU
-	800MHz_RRH Model	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W	RRH 800 MHz 2x50W
_	800MHz_RRH Count	1	1	1
-	800MHz_RRH Location	Top of the Pale/Tower	Top of the Pole/Tower	Top of the Pole/Tower
	800_Top_Jumper #1_Length (RRH to Antenna for TT or Main Coax to Antenna for GM)	10	10	10
_	800_Top_Jumper_Cable_Model (RRH to Antenna for TT or Main Coax to Antenna for GM)	LCF12-50J	LCF12-50J	LCF12-50J
-	800MHz_Main_Coax_Cable_Length (ft)	N/A	N/A	N/A
	BOOMHz_Main_Coax_Cable_Model	N/A	N/A	N/A
	800_Bottom_Jum per #1_Length (Ground based RRH to Main Coax)	N/A	N/A	N/A
	BOO_Bottom_Jum per #1_Cable_Model (Ground based RRH to Main Coax)	N/A	N/A	N/A
-	Plumbing Scenario *	124	124	124
1	f plumbing scenario does not match the material received, please contact your Construction	n Manager		

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	REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



Stephen A. Bray

CT LICENSE: 26657

332.1485

338 OXFORD ROAD OXFORD, CT 06478 NEW HAVEN COUNTY

CROWN CASTLE # 876362 CT23XC508

NETWORK VISION

JLS

04-19-12

5/16/13

RF DATA SHEET

DUE TO FIELD MEASUREMENTS AND THE INSTALLATION OF NEW ANTENNAS THAT VARY IN SIZE FROM THE EXISTING ANTENNAS, THE ANTENNA RAD CENTER HAS CHANGED FROM WHAT IS ON RECORD. THE DATABASE NEEDS TO BE UPDATED TO MATCH THESE PLANS.

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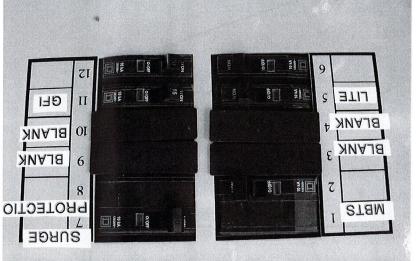
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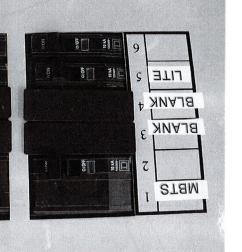
CT LICENSE: 26657

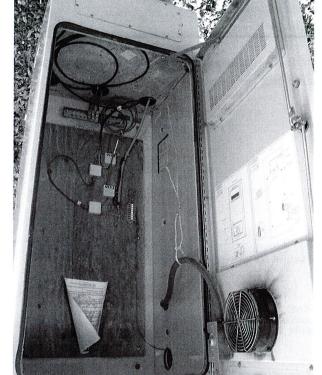
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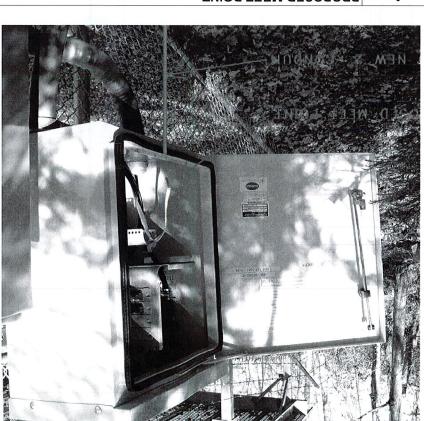




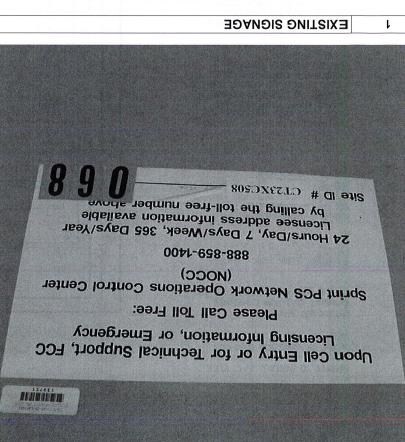
PROPOSED MEET POINT

EXISTING EQUIPMENT AREA









EXISTING TELCO CABINET

PROPOSED NID EQUIPMENT LOCATION

EXISTING POWER SOURCE

5/16/13

21-61-40

C01

SITE PHOTOS **SDNIWAAD VAA**

NETWORK VISION

CL73XC208 CBOMN CV2LFE # 816362

21-61-40

5/16/13

ELECTRICAL

NETWORK VISION

CT23XC508

CBOMN CYSLIFE # 816362

ИЕМ НАУЕИ СОПИТУ

OXFORD, CT 06478 338 OXFORD ROAD

332.1485

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800 KOOLE 34, SUITE 209

DESCRIPTION

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CT LICENSE: 26657

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11	cation Pol	mar	an a	ebyoue	I GI	

* New Utility Meter Location

emained consistent with the contractor documents: construction. In this is necessary to reconfirm that the utility points have The contractor is required to contact the utility companies prior to starting

- B. Transformers shall be as manufactured by Square D, General Electric, or Siemens.
- A. Transformers shall be dry type with average temperature rise not to exceed 150° C (115° C)(80° C)
 - I ransformers:
 - A. Lighting fixtures shall be furnished complete with necessary hardware and lamps
 - righting fixtures and lamps:
- All work requiring an outage or interruption of service (power, telephone) shall be scheduled only at such time permitted by owner.
 - A. The electrical contractor shall furnish and install all power and control wring for equipment contained in contract documents.
 - C Special Requirements:
 - contractor to provide all safety disconnects.
- A. Switches shall be quick-make, quick-break NEMA 1 for indoor use and NEMA 3R for outdoor use as manufactured by General Electric, Square D or equal. Electrical

 - A. Switches, receptacles and other wiring devices shall be specification grade of type, size and rating indicated on the drawings.
 - Wiring Devices:
- be utilized when connecting to equipment cabinets and vibrating equipment. The maximum length for flexible conduit shall be 6'-0". All feeders in "damp" or "wet" locations shall consist of individual conductor in rigid galvanized steel or rigid aluminum conduit. Liquid-tight flexible metallic conduit shall
- vehicular traffic, conduits shall be encased in concrete. All sweeps below grade shall be schedule 80 PVC. will be required at time punchilat is performed. Feeders shall be individual conductors in schedule 40 PVC, direct burial conduit. When buried conduits are subject to
- Underground conduits shall be a minimum of 24" below finished grade. All underground work shall be documented by photograph before any backfill is begun. Photos
 - G. Seal all exterior wall penetrations as required.
 - Provide fire stopping around all conduits at wall and floor penetrations.
 - C. All conductor terminals shall be U.L. listed for minimum of 75° C.
 - clearly specified, no conduits shall be routed on exterior surface of buildings.
- D. The contractor shall conceal all conduit routing passing through finished areas. Conduit routing through unfinished shall be supported as specified in drawings. Unless
 - C. Equipment ground conductors shall be provided for all feeders and branch circuits.
 - connectors in Junction boxes.
- P. Conductors shall be continuous from origin to panel or equipment without splices. Where tap splices are necessary and approved, they shall be made with suitable
 - Connections to communications cabinets and vibrating equipment shall consist of pulled conductors in LFMC, maximum 6' in length.
- receptacles, miscellaneous branch circuits concealed above suspended ceilings or within dry walls shall consist of type MC metal clad cable it allowed by code. F. All feeders shall consist of pulled conductors in conduit. All branch circuits shall consist of pulled conduit. Except 15 and 20 Ampere 1 pole lighting
 - t. Wiring Methods:
 - Conduit routings are schematic. Sub contractor shall install conduits so that access to equipment is not blocked.
 - Exposed raceways shall be run true, plumb, and parallel or perpendicular to building lines.
 - A. Minimum conduit size shall be 3/4" unless otherwise noted on the drawings.
 - 3. Васемауя:
- white letters on black background unless noted otherwise. All panel boards, switches and other equipment enclosures shall bear engraved nameplates as manufactured by Seton Nameplate Corp., or equal lettering to be 1/2"
 - Provide typewritten directories for panels, indicating use of each branch circuit and designating spare circuits. Handwritten directories are not acceptable.
 - responsibility of the contractor to meet with utility company prior to construction to verify source of electric service, tap and meter location. When a utility company meter is specified, the contractor shall obtain all associated cut-in cards, inspections, etc., necessary to have the meter set. It is the
 - D. All work shall conform to the adopted edition of the National Electrical Code and local, state and applicable codes.
 - engineer to make minor changes in locations and arrangements when required by job development without additional compensation to the confractor. Unless otherwise indicated, the arrangement, position, connections, etc. shown on the drawings shall be taken on a diagram basis. The right is reserved by the
 - B. Service equipment shall be 120/240 VAC, 100 Amp, single phase, unless otherwise directed by the Sprint Construction Manager.
 - source of electric power to the final connection, tested and made ready for salisfactory operation.
- nstallation of all electrical work. All fixtures, devices, and equipment shown, noted or required on these drawings, and/or contained herein shall be connected from the The electrical contractor shall furnish all labor, materials, tools, transportation equipment, services and facilities required for the complete, proper and substantial

J. General:

ELECTRICAL SPECIFICATIONS

- CONDUIT RUNNING UNDER GROUND CONDULI RUNNING ABOVE GRADE 84 PULL BOX DUNCTION BOX ar CONDUIT TURNING UP 0-TYPICAL CONDUIT TURNING DOWN qYT **KACEWAY** екопир кор \otimes RWY RIGID GALVANIZED STEEL SOZ CHEMICAL GROUND ROD \boxtimes RIGID (2CH 40) PVC CONDUIT DΛC CKOOND KOD MITH ACCESS MASTER GROUND BAR WCB COMPRESSION TYPE CONNECTION **ВЕИЕВАТОЯ** CEN CADWELD TYPE CONNECTION ELECTRICAL METALLIC TUBING CIRCUIT BREAKER LME DMG **METER** BARE COPPER WIRE $\overline{}$ DISCONNECT SWITCH AMERICAN WIRE GAUGE **DWA** WIRING SYMBOLS **SNOITAIV3A88A** ELECTRICAL SYMBOLS
- 10. Home run grounds not approved. All antenna buss bars should be installed directly to tower steel without insulators or down conductors.
 - Ground depth shall be 30" minimum below finished grade, or 6" below frost line, whichever is greater.
- Where grounding connections are made to painted metal surfaces shall be scraped clean to bear metal to ensure proper contact. Surfaces shall be restored to match
- naing tall potential method. Maximum resistance of the completed ground system shall not exceed 5 Ohms. Lesting shall be performed in accordance with technical specification for facility grounding,
 - Connections to equipment and enclosures shall be made utilizing two-hole ground lugs with an antioxidant compound.

Ose of 90° bends in the protection grounding conductors shall be avoided when 45° bends can be adequately supported.

- All ground connections below grade shall be exothermic (Cadweld).
- All ground connections above grade (interior & exterior) shall be formed using high press crimps.
- All exterior ground conductors shall be #2 AWG solid tinned copper unless otherwise indicated.
- The subcontractor is responsible for properly sequencing grounding and underground conduit installation as to prevent any loss of continuity in the grounding system or

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- The equipment/protections must be rated for standard of AIC rate higher than incoming equipment and/or utility company AIC rate.
 - 10. Redlined As-Builts are to be delivered to a Sprint representative.
 - 9. Contractor to provide and install engraved label on the Sprint meter socket enclosure.
 - 8. Label all equipment served from Sprint panelboard with phenolic labels sized in relation to usage.
 - Obtain all permits and approvals from authorities having jurisdiction and paying all fees required.
 - location of existing conditions to make a complete and operable system without additional cost to the carrier or the engineer.
- Before submitting this bid, the contractor shall visit the Job site to examine and fully acquaint himself with the existing Job conditions, paying particular attention to the
 - Provide all required temporary utilities and pay all associated fees and operating costs.
 - Contractor shall inform the engineer immediately of any conflict discovered before performing any work related to such conflict
 - adnibusent furnished by carrier or other trades involved in this contract.
- All work shall be carefully coordinated with the landlord and all trades involved, and the contractor shall provide proper intings, valves, piping, etc. for all

All work should be done in a neat workmanlike manner, left clean and free from defects, and completely operable. The contractor shall provide all equipment as scheduled

load added to the compound as per NEC Article # 230-2(B) fuls value, contractor must coordinate with the utility company and authority having jurisquence. Run an additional exclusive and dedicated service lateral set for the new Contractor shall verify that the total number of service entrance alsoonnects in the existing utility company pedestal must not exceed six, if the new service added exceeds

on the drawings. All materials shall be new and all work and materials shall be guaranteed by the contractor for a period of one (1) year from the date of acceptance by the

GENERAL SPECIFICATIONS

Alcatel · Lucent Sprint

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SCALE: NTS

SCALE: NTS