

STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
www.ct.gov/csc

March 1, 2013

Jennifer Palumbo
Sprint
48 Spruce Street
Oakland, NJ 07436

RE: **EM-SPRINT-108-130215** - Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 20 Great Oak Road, Oxford, Connecticut.

Dear Ms. Palumbo:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Prior to antenna installation, the modifications identified in the Structural Modification Report prepared by Paul J. Ford and Company dated October 23, 2012, and stamped by Joseph Jacobs shall be implemented;
- Within 45 days following completion of the antenna installation, a signed letter from a Professional Engineer duly licensed in the State of Connecticut shall be submitted to the Council to certify that the recommended modifications have been completed and the structure and foundation do not exceed 100 percent of the post-construction structural rating.
- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Within 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated February 15, 2013. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency

emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

Very truly yours,



Linda Roberts
Executive Director

LR/CDM/cm

c: The Honorable George R. Temple, First Selectman, Town of Oxford
Vincent Vizzo, Planning & Zoning Chairman, Town of Oxford



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February 20, 2013

The Honorable George R. Temple
First Selectman
Town of Oxford
486 Oxford Road
Oxford, CT 06478-1298

RE: **EM-SPRINT-108-130215** - Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 20 Great Oak Road, Oxford, Connecticut.

Dear First Selectman Temple:

The Connecticut Siting Council (Council) received a request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72, a copy of which has already been provided to you.

If you have any questions or comments regarding the proposal, please call me or inform the Council by March 6, 2013.

Thank you for your cooperation and consideration.

Very truly yours,

Linda Roberts
Executive Director

LR/cm

c: Vincent Vizzo, Planning & Zoning Chairman, Town of Oxford

EM-SPRINT-108-130215



Together with Nextel

48 Spruce Street
Oakland, NJ 07436
Phone: (845) 499-4712
Jennifer Palumbo

ORIGINAL

RECEIVED
FEB 15 2013

CONNECTICUT
SITING COUNCIL

September 19, 2012

Hand Delivered

Ms. Linda Roberts
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 20 Great Oak Road, Oxford, CT 06478. Known to Sprint Spectrum L.P. as site CT23XC507.

Dear Ms. Roberts:

In order to accommodate technological changes, implement Code Division Multiple Access ("CDMA") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs Spread-Spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel. LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

As part of the project the new multi-mode 800/1900 antenna will replace existing antennas. These antennas will provide more flexibility for optimization by allowing fast and easy electrical tilt adjustment from remote location and will enable the transmission of multiple technologies from a single antenna. As Sprint Nextel's network evolves to meet the demands of its customers, it is essential for Sprint Nextel to install modern equipment and antennas in order to provide reliable wireless voice and data services. The

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September 19, 2012

Hand Delivery

Ms. Linda Roberts
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 20 Great Oak Road, Oxford, CT 06478. Known to Sprint Spectrum L.P. as site CT23XC207.

Dear Ms. Roberts:

In order to accommodate technological changes, implement Code Division Multiple Access ("CDMA") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-20j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-20j-73(b)(2). In compliance with R.C.S.A. Section 16-20j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs spread-spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel. LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

As part of the project the new multi-mode 800/1900 antenna will replace existing antennas. These antennas will provide more flexibility for optimization by allowing fast and easy electrical tilt adjustment from remote location and will enable the transmission of multiple technologies from a single antenna. As Sprint Nextel's network evolves to meet the demands of its customers, it is essential for Sprint Nextel to install modern equipment and antennas in order to provide reliable wireless voice and data services. The

proposed equipment will include multi-mode radios that will allow Sprint Nextel to transmit at different frequencies using different technologies, including LTE technology. Likewise, the proposed antennas are quad-pole multi-band high gain antennas that will allow Sprint to operate using its multiple frequency bands and technologies, including LTE technology. The proposed equipment and antennas will improve the reliability, coverage and capacity of Sprint Nextel's voice and data networks across Sprint Nextel's various FCC licensed frequency bands and significantly increase the data speeds of Sprint Nextel's network by utilizing the latest LTE technology. Without the proposed modifications Sprint Nextel will be unable to provide reliable wireless voice and data service using the latest technologies.

Sprint Spectrum L.P. will have an interim (testing) period during the modification/installation prior to the final configuration. This antenna configuration is shown on the attached drawings of the planned modifications. Also included is the power density calculation reflecting the change in Sprint's operations at the site and documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

The changes to the facility do not constitute modification as defined Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for the R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will not be affected.
2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound.
3. The proposed changes will not increase the noise level at the existing facility by 6 decibels or more.
4. Radio Frequency power density may increase due to the use of one or more CDMA transmissions. Moreover, LTE will utilize additional radio frequencies newly licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons Sprint Spectrum L.P. respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (845)-499-4712 or email JPalumbo@Transcendwireless.com with questions concerning this matter. Thank you for your consideration.

Sincerely,

Jennifer Palumbo
Real Estate Consultant



EBI Consulting

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RADIO FREQUENCY EMISSIONS ANALYSIS REPORT
EVALUATION OF HUMAN EXPOSURE POTENTIAL
TO NON-IONIZING EMISSIONS

Sprint Existing Facility

Site ID: CT23XC507

Seymour / Oxford Town Garage
20 Great Oak Road
Oxford, CT 06478

August 28, 2012



EBI Consulting

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August 28, 2012

Sprint

Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495

Re: Emissions Values for Site **CT23XC507 – Seymour / Oxford Town Garage**

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 20 Great Oak Road, Oxford, CT, for the purpose of determining whether the emissions from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limit for the cellular band is approximately 567 $\mu\text{W}/\text{cm}^2$, and the general population exposure limit for the PCS band is 1000 $\mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 20 Great Oak Road, Oxford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario. Actual values seen from this site will be dramatically less than those shown in this report. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 2 CDMA Carriers (1900 MHz) were considered for each sector of the proposed installation.
- 2) 1 CDMA Carrier (850 MHz) was considered for each sector of the proposed installation
- 3) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 4) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The actual gain in this direction was used per the manufactures supplied specifications.
- 5) The antenna used in this modeling is the RFS APXVSP18-C-A20. This is based on feedback from the carrier with regards to anticipated antenna selection. This antenna has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario.



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- 6) The antenna mounting height centerline of the proposed antennas is **150 feet** above ground level (AGL)
- 7) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits



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Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public exposure to RF Emissions.

The anticipated Maximum Composite contributions from the Sprint facility are **10.791% (3.597% from each sector)** of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **24.401%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government

Scott Heffernan
RF Engineering Director

EBI Consulting
21 B Street
Burlington, MA 01803



PAUL J. FORD AND COMPANY
 STRUCTURAL ENGINEERS
 250 East Broad Street • Suite 1500 • Columbus, Ohio 43215-3708

Date: **October 23, 2012**

Ben Goodhart
 Crown Castle USA Inc.
 3530 Toringdon Way, Suite 300
 Charlotte, NC 28277

Paul J Ford and Company
 250 E. Broad Street, Suite 1500
 Columbus, OH 43215
 614.221.6679
 cmccartney@pjfweb.com

Subject: Structural Modification Report

Carrier Designation: *Sprint PCS Co-Locate*
Carrier Site Number: CT23XC507
Carrier Site Name: N/A

Crown Castle Designation:
Crown Castle BU Number: 876361
Crown Castle Site Name: Seymour 2 / Oxford Town Garage
Crown Castle JDE Job Number: 183553
Crown Castle Work Order Number: 544952
Crown Castle Application Number: 151567 Rev. 0

Engineering Firm Designation: **Paul J Ford and Company Project Number:** 37512-1818 R1 Aero

Site Data: **20 Great Oak Rd., OXFORD, New Haven County, CT**
Latitude 41° 25' 34.91", Longitude -73° 8' 39.33"
150 Foot - Monopole Tower

Dear Ben Goodhart,

Paul J Ford and Company is pleased to submit this "Structural Modification Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 497643, in accordance with application 151567, revision 0.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure w/ Existing + Reserved + Proposed **Sufficient Capacity**
 Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

The analysis has been performed in accordance with the TIA/EIA-222-F standard and the 2005 CT State Building Code based upon a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at Paul J Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle USA Inc. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

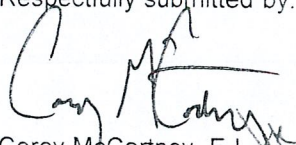

 Corey McCartney, E.I.
 Structural Engineer





TABLE OF CONTENTS

1) INTRODUCTION

2) ANALYSIS CRITERIA

Table 1 - Proposed Antenna and Cable Information

Table 2 - Existing and Reserved Antenna and Cable Information

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

3.1) Analysis Method

3.2) Assumptions

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Table 5 - Tower Component Stresses vs. Capacity

4.1) Recommendations

5) APPENDIX A

tnxTower Output

6) APPENDIX B

Base Level Drawing

7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 150-ft Monopole tower designed by ENGINEERED ENDEAVORS, INC. in October of 1999. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
152.0	147.0	3	alcatel lucent	1900MHz RRH (65MHz)	3	1-1/4	-
		3	alcatel lucent	800 EXTERNAL NOTCH FILTER			
		3	alcatel lucent	800MHZ RRH			
		9	rfs celwave	ACU-A20-N			
		3	rfs celwave	APXVSP18-C-A20 w/ Mount Pipe			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
152.0	152.0	1	crown mounts	Platform Mount [LP 602-1]	-	-	1
	148.0	6	decibel	980H90T3R-M w/ Mount Pipe	6	1-5/8	3
138.0	140.0	6	antel	LPA-185080/12CF w/ Mount Pipe	6	1-5/8	2
		6	antel	LPA-80080/8CF w/ Mount Pipe			
		3	antel	BXA-171063-12BF w/ Mount Pipe			
		3	antel	BXA-70063-6CF-2 w/ Mount Pipe			
		6	antel	LPA-80063-6CF-EDIN-2 w/ Mount Pipe			
	138.0	1	crown mounts	Platform Mount [LP 601-1]	12	1-5/8	1
129.0	129.0	1	crown mounts	Side Arm Mount [SO 102-3]	-	-	2
		6	ericsson	RRUS-11			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note	
127.0	128.0	3	powerwave	7770.00 w/ Mount Pipe	-	-	3	
		6	powerwave	LGP21401				
		6	andrew	SBNH-1D6565C w/ Mount Pipe	1 2	3/8 3/4	2	
		6	cci	DTMABP7819VG12A				
	3	kmw communications	AM-X-CD-16-65-00T-RET w/ Mount Pipe					
	1	raycap	DC6-48-60-18-8F					
	127.0	1	1	crown mounts	T-Arm Mount [TA 601-3]	-	-	3
			1	crown mounts	Pipe Mount [PM 601-3]			
85.0	86.0	1	lucent	KS24019-L112A	6	1-1/4	1	
	85.0	1	crown mounts	Side Arm Mount [SO 701-1]	1	1/2	1	

- Notes:
 1) Existing Equipment
 2) Reserved Equipment
 3) Equipment To Be Removed

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
GEOTECHNICAL REPORTS	Dr. Clarence Welti, CT23XC507, 09/22/99	1532984	CCISITES
TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	EEl, CT23XC507, 06/23/00	1447042	CCISITES
TOWER MANUFACTURER DRAWINGS	EEl, 5723, 10/01/99	1446979	CCISITES
TOWER STRUCTURAL ANALYSIS REPORTS	FDH, 12-04574E S4, 06/18/12	3241229	CCISITES
TOWER PROPOSED MODIFICATION DRAWINGS	PJF, 37512-1818 R1, 10/23/12	-	PJF

3.1) Analysis Method

tnxTower (version 6.0.3.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole will be reinforced in conformance with the attached proposed modification drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	150 - 123.423	Pole	TP20.66x15x0.1875	1	-4.73	612.53	82.7	Pass
L2	123.423 - 118.25	Pole	TP21.3901x19.6105x0.25	2	-5.61	872.06	94.9	Pass
L3	118.25 - 90.5	Pole	TP27.3113x21.3901x0.483	3	-10.10	1864.63	89.4	Pass
L4	90.5 - 60.5	Pole	TP33.2114x27.3113x0.5991	4	-17.09	2820.72	85.1	Pass
L5	60.5 - 42.413	Pole	TP37.07x33.2114x0.5727	5	-20.37	2937.40	90.3	Pass
L6	42.413 - 30.5	Pole	TP38.9889x34.8222x0.6222	6	-22.92	3204.97	88.5	Pass
L7	30.5 - 0	Pole	TP45.5x38.9889x0.5742	7	-28.60	3366.18	93.4	Pass
							Summary	
						Pole (L2)	94.9	Pass
						Rating =	94.9	Pass

Table 5 - Tower Component Stresses vs. Capacity - LC4.7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	95.8	Pass
1	Base Plate	0	95.0	Pass
1	Base Foundation Steel	0	80.5	Pass
1	Base Foundation Soil Interaction	0	92.0	Pass

Structure Rating (max from all components) =	95.8%
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Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

4.1) Recommendations

- 1) See attached modification drawings

APPENDIX A
TNXTOWER OUTPUT

Tower Input Data

There is a pole section.
 This tower is designed using the TIA/EIA-222-F standard.
 The following design criteria apply:

- 1) Tower is located in New Haven County, Connecticut.
- 2) Basic wind speed of 85 mph.
- 3) Nominal ice thickness of 0.7500 in.
- 4) Ice thickness is considered to increase with height.
- 5) Ice density of 56.00 pcf.
- 6) A wind speed of 38 mph is used in combination with ice.
- 7) Temperature drop of 50 °F.
- 8) Deflections calculated using a wind speed of 50 mph.
- 9) A non-linear (P-delta) analysis was used.
- 10) Pressures are calculated at each section.
- 11) Stress ratio used in pole design is 1.333.
- 12) Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

Options

- | | | |
|-------------------------------------|------------------------------------|--------------------------------------|
| Consider Moments - Legs | Distribute Leg Loads As Uniform | √ Treat Feedline Bundles As Cylinder |
| Consider Moments - Horizontals | Assume Legs Pinned | Use ASCE 10 X-Brace Ly Rules |
| Consider Moments - Diagonals | √ Assume Rigid Index Plate | Calculate Redundant Bracing Forces |
| Use Moment Magnification | √ Use Clear Spans For Wind Area | Ignore Redundant Members in FEA |
| √ Use Code Stress Ratios | Use Clear Spans For KL/r | SR Leg Bolts Resist Compression |
| √ Use Code Safety Factors - Guys | Retension Guys To Initial Tension | All Leg Panels Have Same Allowable |
| √ Escalate Ice | √ Bypass Mast Stability Checks | Offset Girt At Foundation |
| Always Use Max Kz | √ Use Azimuth Dish Coefficients | √ Consider Feedline Torque |
| Use Special Wind Profile | √ Project Wind Area of Appurt. | Include Angle Block Shear Check |
| Include Bolts In Member Capacity | √ Autocalc Torque Arm Areas | Poles |
| Leg Bolts Are At Top Of Section | SR Members Have Cut Ends | √ Include Shear-Torsion Interaction |
| Secondary Horizontal Braces Leg | Sort Capacity Reports By Component | Always Use Sub-Critical Flow |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing | Use Top Mounted Sockets |
| Add IBC .6D+W Combination | | |

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	150.0000- 123.4230	26.5770	3.17	18	15.0000	20.6600	0.1875	0.7500	A572-65 (65 ksi)
L2	123.4230- 118.2500	8.3400	0.00	18	19.6105	21.3901	0.2500	1.0000	A572-65 (65 ksi)
L3	118.2500- 90.5000	27.7500	0.00	18	21.3901	27.3113	0.4830	1.9322	Reinf 56.68 ksi (57 ksi)
L4	90.5000- 60.5000	30.0000	0.00	18	27.3113	33.2114	0.5991	2.3964	Reinf 56.87 ksi (57 ksi)
L5	60.5000- 42.4130	18.0870	5.17	18	33.2114	37.0700	0.5727	2.2909	Reinf 57.08 ksi (57 ksi)
L6	42.4130- 30.5000	17.0800	0.00	18	34.8222	38.9889	0.6222	2.4889	Reinf 57.22 ksi (57 ksi)
L7	30.5000- 0.0000	30.5000		18	38.9889	45.5000	0.5742	2.2969	Reinf 57.67 ksi (58 ksi)

Tapered Pole Properties

Section	Tip Dia. in	Area in ²	I in ⁴	r in	C in	I/C in ³	J in ⁴	I/Q in ²	w in	w/t
L1	15.2314	8.8153	244.3603	5.2584	7.6200	32.0683	489.0422	4.4085	2.3100	12.32
	20.9787	12.1837	645.1464	7.2677	10.4953	61.4701	1291.1417	6.0930	3.3062	17.633
L2	20.5992	15.3626	727.5059	6.8730	9.9622	73.0270	1455.9690	7.6828	3.0115	12.046
	21.7200	16.7746	947.1157	7.5047	10.8662	87.1620	1895.4776	8.3889	3.3247	13.299
L3	21.7200	32.0540	1770.1247	7.4220	10.8662	162.9027	3542.5787	16.0300	2.9145	6.034
	27.7326	41.1322	3740.2750	9.5240	13.8741	269.5864	7485.4715	20.5700	3.9566	8.191
L4	27.7326	50.7952	4579.0772	9.4828	13.8741	330.0444	9164.1796	25.4024	3.7523	6.263
	33.7237	62.0147	8332.8666	11.5774	16.8714	493.9053	16676.6978	31.0132	4.7908	7.996
L5	33.7237	59.3320	7985.3005	11.5867	16.8714	473.3044	15981.1083	29.6717	4.8372	8.446
	37.6419	66.3464	11165.4298	12.9565	18.8316	592.9105	22345.5514	33.1795	5.5163	9.632
L6	36.6394	67.5425	9980.8405	12.1410	17.6897	564.2178	19974.8140	33.7777	5.0336	8.09
	39.5904	75.7714	14091.3090	13.6202	19.8064	711.4535	28201.1597	37.8929	5.7669	9.268
L7	39.5904	70.0136	13053.1307	13.6372	19.8064	659.0371	26123.4370	35.0135	5.8514	10.19
	46.2019	81.8806	20878.9938	15.9487	23.1140	903.3051	41785.4607	40.9481	6.9974	12.186

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C _A A _A ft ² /ft	Weight klf
HB114-1-0813U4-M5J(1 1/4")	C	No	CaAa (Out Of Face)	150.0000 - 0.0000	1	No Ice	0.1540	0.00
						1/2" Ice	0.2540	0.00
						1" Ice	0.3540	0.00
						2" Ice	0.5540	0.01
						4" Ice	0.9540	0.03
HB114-1-0813U4-M5J(1 1/4")	C	No	Inside Pole	150.0000 - 0.0000	2	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
**								
LDF7-50A(1-5/8")	C	No	Inside Pole	138.0000 - 0.0000	12	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
LDF7-50A(1-5/8")	C	No	CaAa (Out Of Face)	138.0000 - 0.0000	1	No Ice	0.1980	0.00
						1/2" Ice	0.2980	0.00
						1" Ice	0.3980	0.00
						2" Ice	0.5980	0.01
						4" Ice	0.9980	0.03
LDF7-50A(1-5/8")	C	No	Inside Pole	138.0000 - 0.0000	5	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
**								
LDF6-50A(1-1/4")	C	No	Inside Pole	127.0000 - 0.0000	6	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
FB-L98B-002-75000(3/8")	C	No	Inside Pole	127.0000 - 0.0000	1	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
WR-VG86ST-BRD(C	No	Inside Pole	127.0000 - 0.0000	2	No Ice	0.0000	0.00

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C _A A _A ft ² /ft	Weight klf
3/4)						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.00
						4" Ice	0.0000	0.00
** LDF4-50A(1/2")	C	No	CaAa (Out Of Face)	85.0000 - 0.0000	1	No Ice	0.0000	0.00
						1/2" Ice	0.0000	0.00
						1" Ice	0.0000	0.00
						2" Ice	0.0000	0.01
						4" Ice	0.0000	0.02
** Aero MP3-06	C	No	CaAa (Out Of Face)	92.0000 - 0.0000	1	No Ice	0.4343	0.00
						1/2" Ice	0.5454	0.00
						1" Ice	0.6566	0.00
						2" Ice	0.8788	0.00
						4" Ice	1.3232	0.00
Aero MP3-05	C	No	CaAa (Out Of Face)	122.0000 - 92.0000	1	No Ice	0.3478	0.00
						1/2" Ice	0.4001	0.00
						1" Ice	0.6566	0.00
						2" Ice	0.8788	0.00
						4" Ice	1.3232	0.00

Feed Line/Linear Appurtenances Section Areas

Tower Sectio n	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
L1	150.0000-123.4230	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	6.979	0.33
L2	123.4230-118.2500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	3.125	0.12
L3	118.2500-90.5000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	19.549	0.65
L4	90.5000-60.5000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	23.590	0.71
L5	60.5000-42.4130	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	14.222	0.43
L6	42.4130-30.5000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	9.367	0.28
L7	30.5000-0.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	23.983	0.72

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Sectio n	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
L1	150.0000-123.4230	A	0.889	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	14.296	0.45
L2	123.4230-118.2500	A	0.876	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	5.909	0.15
L3	118.2500-90.5000	A	0.861	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	35.616	0.81
L4	90.5000-60.5000	A	0.828	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
L5	60.5000-42.4130	C	0.791	0.000	0.000	0.000	39.040	0.91
		A		0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
L6	42.4130-30.5000	C	0.759	0.000	0.000	0.000	23.122	0.55
		A		0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
L7	30.5000-0.0000	C	0.750	0.000	0.000	0.000	15.229	0.36
		A		0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	38.217	0.91

Feed Line Center of Pressure

Section	Elevation ft	CP _x in	CP _z in	CP _x Ice in	CP _z Ice in
L1	150.0000-123.4230	-0.2985	0.1723	-0.4912	0.2836
L2	123.4230-118.2500	-0.5840	0.3372	-0.8536	0.4928
L3	118.2500-90.5000	-0.6798	0.3925	-0.9791	0.5653
L4	90.5000-60.5000	-0.7787	0.4496	-1.0762	0.6214
L5	60.5000-42.4130	-0.8052	0.4649	-1.1209	0.6471
L6	42.4130-30.5000	-0.8163	0.4713	-1.1446	0.6608
L7	30.5000-0.0000	-0.8350	0.4821	-1.1698	0.6754

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K	
1900MHz RRH (65MHz)	A	From Face	4.0000 0.00 -5.00	0.00	152.0000	No Ice	2.6979	2.7708	0.06
						1/2" Ice	2.9362	3.0111	0.08
						Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
800 EXTERNAL NOTCH FILTER	A	From Face	4.0000 0.00 -5.00	0.00	152.0000	No Ice	0.7701	0.3747	0.01
						1/2" Ice	0.8898	0.4647	0.02
						Ice	1.0181	0.5634	0.02
						1" Ice	1.3007	0.7868	0.04
						2" Ice	1.9696	1.3372	0.11
800MHZ RRH	A	From Face	4.0000 0.00 -5.00	0.00	152.0000	No Ice	2.4899	2.0685	0.05
						1/2" Ice	2.7061	2.2705	0.07
						Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
(3) ACU-A20-N	A	From Face	4.0000 0.00 -5.00	0.00	152.0000	No Ice	0.0778	0.1361	0.00
						1/2" Ice	0.1210	0.1890	0.00
						Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
APXVSPP18-C-A20 w/ Mount Pipe	A	From Face	4.0000 0.00 -5.00	0.00	152.0000	No Ice	8.4975	6.9458	0.08
						1/2" Ice	9.1490	8.1266	0.15
						Ice	9.7672	9.0212	0.22
						1" Ice	11.0311	10.8440	0.41
						2" Ice	13.6786	14.8507	0.91
1900MHz RRH (65MHz)	B	From Face	4.0000	0.00	152.0000	No Ice	2.6979	2.7708	0.06

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustmen t °	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K	
			0.00			1/2"	2.9362	3.0111	0.08
			-5.00			Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
						4" Ice			
800 EXTERNAL NOTCH FILTER	B	From Face	4.0000	0.00	152.0000	No Ice	0.7701	0.3747	0.01
			0.00			1/2"	0.8898	0.4647	0.02
			-5.00			Ice	1.0181	0.5634	0.02
						1" Ice	1.3007	0.7868	0.04
						2" Ice	1.9696	1.3372	0.11
						4" Ice			
800MHZ RRH	B	From Face	4.0000	0.00	152.0000	No Ice	2.4899	2.0685	0.05
			0.00			1/2"	2.7061	2.2705	0.07
			-5.00			Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
						4" Ice			
(3) ACU-A20-N	B	From Face	4.0000	0.00	152.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2"	0.1210	0.1890	0.00
			-5.00			Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
						4" Ice			
APXVSPP18-C-A20 w/ Mount Pipe	B	From Face	4.0000	0.00	152.0000	No Ice	8.4975	6.9458	0.08
			0.00			1/2"	9.1490	8.1266	0.15
			-5.00			Ice	9.7672	9.0212	0.22
						1" Ice	11.0311	10.8440	0.41
						2" Ice	13.6786	14.8507	0.91
						4" Ice			
1900MHz RRH (65MHz)	C	From Face	4.0000	0.00	152.0000	No Ice	2.6979	2.7708	0.06
			0.00			1/2"	2.9362	3.0111	0.08
			-5.00			Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
						4" Ice			
800 EXTERNAL NOTCH FILTER	C	From Face	4.0000	0.00	152.0000	No Ice	0.7701	0.3747	0.01
			0.00			1/2"	0.8898	0.4647	0.02
			-5.00			Ice	1.0181	0.5634	0.02
						1" Ice	1.3007	0.7868	0.04
						2" Ice	1.9696	1.3372	0.11
						4" Ice			
800MHZ RRH	C	From Face	4.0000	0.00	152.0000	No Ice	2.4899	2.0685	0.05
			0.00			1/2"	2.7061	2.2705	0.07
			-5.00			Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
						4" Ice			
(3) ACU-A20-N	C	From Face	4.0000	0.00	152.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2"	0.1210	0.1890	0.00
			-5.00			Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
						4" Ice			
APXVSPP18-C-A20 w/ Mount Pipe	C	From Face	4.0000	0.00	152.0000	No Ice	8.4975	6.9458	0.08
			0.00			1/2"	9.1490	8.1266	0.15
			-5.00			Ice	9.7672	9.0212	0.22
						1" Ice	11.0311	10.8440	0.41
						2" Ice	13.6786	14.8507	0.91
						4" Ice			
Platform Mount [LP 602-1]	C	None		0.00	152.0000	No Ice	32.0300	32.0300	1.34
						1/2"	38.7100	38.7100	1.80
						Ice	45.3900	45.3900	2.26
						1" Ice	58.7500	58.7500	3.17
						2" Ice	85.4700	85.4700	5.00
						4" Ice			

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement		C _{AA} A _{Front}	C _{AA} A _{Side}	Weight
			Horz	Lateral				ft ²	ft ²	
			ft	ft	°	ft				K
(3) 6' x 2.375" Pipe Mount	A	From Face	4.0000	0.00	0.00	152.0000	No Ice	1.4250	1.4250	0.02
							1/2" Ice	1.9250	1.9250	0.03
							Ice	2.2939	2.2939	0.05
							1" Ice	3.0596	3.0596	0.09
							2" Ice	4.7022	4.7022	0.23
(3) 6' x 2.375" Pipe Mount	B	From Face	4.0000	0.00	0.00	152.0000	No Ice	1.4250	1.4250	0.02
							1/2" Ice	1.9250	1.9250	0.03
							Ice	2.2939	2.2939	0.05
							1" Ice	3.0596	3.0596	0.09
							2" Ice	4.7022	4.7022	0.23
(3) 6' x 2.375" Pipe Mount	C	From Face	4.0000	0.00	0.00	152.0000	No Ice	1.4250	1.4250	0.02
							1/2" Ice	1.9250	1.9250	0.03
							Ice	2.2939	2.2939	0.05
							1" Ice	3.0596	3.0596	0.09
							2" Ice	4.7022	4.7022	0.23

BXA-171063-12BF w/ Mount Pipe	A	From Face	4.0000	0.00	0.00	138.0000	No Ice	4.9710	5.2283	0.04
							1/2" Ice	5.5211	6.3892	0.08
							Ice	6.0361	7.2610	0.14
							1" Ice	7.0911	9.0462	0.27
							2" Ice	9.3593	12.8165	0.67
BXA-70063-6CF-2 w/ Mount Pipe	A	From Face	4.0000	0.00	0.00	138.0000	No Ice	7.9686	5.8008	0.04
							1/2" Ice	8.6091	6.9529	0.10
							Ice	9.2158	7.8191	0.17
							1" Ice	10.4591	9.6015	0.34
							2" Ice	13.0655	13.3662	0.80
(2) LPA-80063-6CF-EDIN- 2 w/ Mount Pipe	A	From Face	4.0000	0.00	0.00	138.0000	No Ice	10.7445	10.7001	0.05
							1/2" Ice	11.4117	11.9672	0.14
							Ice	12.0450	12.9479	0.25
							1" Ice	13.3414	14.9632	0.48
							2" Ice	16.0541	19.2085	1.09
BXA-171063-12BF w/ Mount Pipe	B	From Face	4.0000	0.00	0.00	138.0000	No Ice	4.9710	5.2283	0.04
							1/2" Ice	5.5211	6.3892	0.08
							Ice	6.0361	7.2610	0.14
							1" Ice	7.0911	9.0462	0.27
							2" Ice	9.3593	12.8165	0.67
BXA-70063-6CF-2 w/ Mount Pipe	B	From Face	4.0000	0.00	0.00	138.0000	No Ice	7.9686	5.8008	0.04
							1/2" Ice	8.6091	6.9529	0.10
							Ice	9.2158	7.8191	0.17
							1" Ice	10.4591	9.6015	0.34
							2" Ice	13.0655	13.3662	0.80
(2) LPA-80063-6CF-EDIN- 2 w/ Mount Pipe	B	From Face	4.0000	0.00	0.00	138.0000	No Ice	10.7445	10.7001	0.05
							1/2" Ice	11.4117	11.9672	0.14
							Ice	12.0450	12.9479	0.25
							1" Ice	13.3414	14.9632	0.48
							2" Ice	16.0541	19.2085	1.09
BXA-70063-6CF-2 w/ Mount Pipe	C	From Face	4.0000	0.00	0.00	138.0000	No Ice	7.9686	5.8008	0.04
							1/2" Ice	8.6091	6.9529	0.10
							Ice	9.2158	7.8191	0.17
							1" Ice	10.4591	9.6015	0.34
							2" Ice	13.0655	13.3662	0.80
(2) LPA-80063-6CF-EDIN- 2 w/ Mount Pipe	C	From Face	4.0000	0.00	0.00	138.0000	No Ice	10.7445	10.7001	0.05
							1/2" Ice	11.4117	11.9672	0.14
							Ice	12.0450	12.9479	0.25
							1" Ice	13.3414	14.9632	0.48
							2" Ice	16.0541	19.2085	1.09

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustmen t	Placement	C _A A _A Front	C _A A _A Side	Weight	
			Horz	Lateral						ft
							ft ²	ft ²	K	
BXA-171063-12BF w/ Mount Pipe	C	From Face	4.0000	0.00	0.00	138.0000	2" Ice	16.0541	19.2085	1.09
							4" Ice			
							No Ice	4.9710	5.2283	0.04
							1/2" Ice	5.5211	6.3892	0.08
							Ice	6.0361	7.2610	0.14
							1" Ice	7.0911	9.0462	0.27
Platform Mount [LP 601-1]	C	None			0.00	138.0000	2" Ice	9.3593	12.8165	0.67
							4" Ice			
							No Ice	28.4700	28.4700	1.12
							1/2" Ice	33.5900	33.5900	1.51
							Ice	38.7100	38.7100	1.91
							1" Ice	48.9500	48.9500	2.69
*** (3) SBNH-1D6565C w/ Mount Pipe	A	From Face	4.0000	0.00	0.00	127.0000	2" Ice	69.4300	69.4300	4.26
							4" Ice			
							No Ice	11.5561	9.7151	0.09
							1/2" Ice	12.2227	11.1857	0.18
							Ice	12.8929	12.5942	0.28
							1" Ice	14.2911	14.8689	0.51
(2) DTMABP7819VG12A	A	From Face	4.0000	0.00	0.00	127.0000	2" Ice	17.4280	19.6184	1.14
							4" Ice			
							No Ice	1.1389	0.3907	0.02
							1/2" Ice	1.2835	0.4884	0.03
							Ice	1.4368	0.5947	0.04
							1" Ice	1.7693	0.8334	0.06
(2) RRUS-11	A	From Face	4.0000	0.00	0.00	129.0000	2" Ice	2.5380	1.4144	0.14
							4" Ice			
							No Ice	3.2486	1.3726	0.05
							1/2" Ice	3.4905	1.5510	0.07
							Ice	3.7411	1.7380	0.09
							1" Ice	4.2682	2.1381	0.15
DC6-48-60-18-8F	A	From Face	4.0000	0.00	0.00	127.0000	2" Ice	5.4260	3.0418	0.31
							4" Ice			
							No Ice	2.5667	4.3167	0.02
							1/2" Ice	2.7978	4.5965	0.05
							Ice	3.0377	4.8849	0.09
							1" Ice	3.5432	5.4877	0.17
(2) DTMABP7819VG12A	B	From Face	4.0000	0.00	0.00	127.0000	2" Ice	4.6580	6.7969	0.38
							4" Ice			
							No Ice	1.1389	0.3907	0.02
							1/2" Ice	1.2835	0.4884	0.03
							Ice	1.4368	0.5947	0.04
							1" Ice	1.7693	0.8334	0.06
(2) RRUS-11	B	From Face	4.0000	0.00	0.00	129.0000	2" Ice	5.4260	3.0418	0.31
							4" Ice			
							No Ice	3.2486	1.3726	0.05
							1/2" Ice	3.4905	1.5510	0.07
							Ice	3.7411	1.7380	0.09
							1" Ice	4.2682	2.1381	0.15
(3) AM-X-CD-16-65-00T-RET w/ Mount Pipe	B	From Face	4.0000	0.00	0.00	127.0000	2" Ice	5.4260	3.0418	0.31
							4" Ice			
							No Ice	8.4975	6.3042	0.07
							1/2" Ice	9.1490	7.4790	0.14
							Ice	9.7672	8.3676	0.21
							1" Ice	11.0311	10.1785	0.38
(3) SBNH-1D6565C w/ Mount Pipe	C	From Face	4.0000	0.00	0.00	127.0000	2" Ice	13.6786	14.0237	0.87
							4" Ice			
							No Ice	11.5561	9.7151	0.09
							1/2" Ice	12.2227	11.1857	0.18
							Ice	12.8929	12.5942	0.28
							1" Ice	14.2911	14.8689	0.51
(2) DTMABP7819VG12A	C	From Face	4.0000	0.00	0.00	127.0000	2" Ice	17.4280	19.6184	1.14
							4" Ice			
							No Ice	1.1389	0.3907	0.02
							1/2" Ice	1.2835	0.4884	0.03

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustmen t	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K	
			Horz Lateral ft ft ft	Vert ft						
				1.00						
(2) RRUS-11	C	From Face	4.0000 0.00 0.00	0.00	0.00	129.0000	Ice	1.4368	0.5947	0.04
							1" Ice	1.7693	0.8334	0.06
							2" Ice	2.5380	1.4144	0.14
							4" Ice			
							No Ice	3.2486	1.3726	0.05
							1/2" Ice	3.4905	1.5510	0.07
							Ice	3.7411	1.7380	0.09
T-Arm Mount [TA 601-3]	C	None			0.00	127.0000	1" Ice	4.2682	2.1381	0.15
							2" Ice	5.4260	3.0418	0.31
							4" Ice			
							No Ice	10.9000	10.9000	0.73
							1/2"	14.6500	14.6500	0.93
							Ice	18.4000	18.4000	1.13
							1" Ice	25.9000	25.9000	1.52
Side Arm Mount [SO 102-3]	C	None			0.00	129.0000	2" Ice	40.9000	40.9000	2.32
							4" Ice			
							No Ice	3.0000	3.0000	0.08
							1/2"	3.4800	3.4800	0.11
							Ice	3.9600	3.9600	0.14
							1" Ice	4.9200	4.9200	0.20
							2" Ice	6.8400	6.8400	0.32
*** KS24019-L112A	A	From Face	4.0000 0.00 1.00	0.00	0.00	85.0000	4" Ice			
							No Ice	0.1556	0.1556	0.01
							1/2"	0.2247	0.2247	0.01
							Ice	0.3025	0.3025	0.01
							1" Ice	0.4840	0.4840	0.02
							2" Ice	0.9506	0.9506	0.06
							4" Ice			
Side Arm Mount [SO 701-1]	A	None			0.00	85.0000	No Ice	0.8500	1.6700	0.07
							1/2"	1.1400	2.3400	0.08
							Ice	1.4300	3.0100	0.09
							1" Ice	2.0100	4.3500	0.12
							2" Ice	3.1700	7.0300	0.18
							4" Ice			

Tower Pressures - No Ice

$G_H = 1.690$

Section Elevation ft	z ft	K _Z	q _Z ksf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L1 150.0000-123.4230	136.0084	1.499	0.03	39.489	A	0.000	39.489	39.489	100.00	0.000	0.000
					B	0.000	39.489		100.00	0.000	0.000
					C	0.000	39.489		100.00	0.000	6.979
L2 123.4230-118.2500	120.8137	1.449	0.03	8.983	A	0.000	8.983	8.983	100.00	0.000	0.000
					B	0.000	8.983		100.00	0.000	0.000
					C	0.000	8.983		100.00	0.000	3.125
L3 118.2500-90.5000	103.8127	1.387	0.03	56.311	A	0.000	56.311	56.311	100.00	0.000	0.000
					B	0.000	56.311		100.00	0.000	0.000
					C	0.000	56.311		100.00	0.000	19.549
L4 90.5000-60.5000	75.0126	1.264	0.02	75.653	A	0.000	75.653	75.653	100.00	0.000	0.000
					B	0.000	75.653		100.00	0.000	0.000
					C	0.000	75.653		100.00	0.000	23.590
L5 60.5000-42.4130	51.2910	1.134	0.02	52.966	A	0.000	52.966	52.966	100.00	0.000	0.000
					B	0.000	52.966		100.00	0.000	0.000
					C	0.000	52.966		100.00	0.000	14.222
L6 42.4130-30.5000	36.3796	1.028	0.02	37.264	A	0.000	37.264	37.264	100.00	0.000	0.000
					B	0.000	37.264		100.00	0.000	0.000
					C	0.000	37.264		100.00	0.000	9.367
L7 30.5000-	14.8583	1	0.02	107.37	A	0.000	107.371	107.371	100.00	0.000	0.000

Section Elevation	z	K _Z	q _Z	A _G	Face	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		ksf	ft ²		ft ²	ft ²	ft ²		ft ²	ft ²
0.0000				1	B	0.000	107.371		100.00	0.000	0.000
					C	0.000	107.371		100.00	0.000	23.983

Tower Pressure - With Ice

$G_H = 1.690$

Section Elevation	z	K _Z	q _Z	t _Z	A _G	Face	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		ksf	in	ft ²		ft ²	ft ²	ft ²		ft ²	ft ²
L1 150.0000-123.4230	136.0084	1.499	0.01	0.8889	43.427	A	0.000	43.427	43.427	100.00	0.000	0.000
						B	0.000	43.427	100.00	0.000	0.000	
						C	0.000	43.427	100.00	0.000	14.296	
L2 123.4230-118.2500	120.8137	1.449	0.01	0.8764	9.749	A	0.000	9.749	9.749	100.00	0.000	0.000
						B	0.000	9.749	100.00	0.000	0.000	
						C	0.000	9.749	100.00	0.000	5.909	
L3 118.2500-90.5000	103.8127	1.387	0.01	0.8606	60.291	A	0.000	60.291	60.291	100.00	0.000	0.000
						B	0.000	60.291	100.00	0.000	0.000	
						C	0.000	60.291	100.00	0.000	35.616	
L4 90.5000-60.5000	75.0126	1.264	0.00	0.8277	79.792	A	0.000	79.792	79.792	100.00	0.000	0.000
						B	0.000	79.792	100.00	0.000	0.000	
						C	0.000	79.792	100.00	0.000	39.040	
L5 60.5000-42.4130	51.2910	1.134	0.00	0.7908	55.350	A	0.000	55.350	55.350	100.00	0.000	0.000
						B	0.000	55.350	100.00	0.000	0.000	
						C	0.000	55.350	100.00	0.000	23.122	
L6 42.4130-30.5000	36.3796	1.028	0.00	0.7588	38.834	A	0.000	38.834	38.834	100.00	0.000	0.000
						B	0.000	38.834	100.00	0.000	0.000	
						C	0.000	38.834	100.00	0.000	15.229	
L7 30.5000-0.0000	14.8583	1	0.00	0.7500	111.184	A	0.000	111.184	111.184	100.00	0.000	0.000
						B	0.000	111.184	100.00	0.000	0.000	
						C	0.000	111.184	100.00	0.000	38.217	

Tower Pressure - Service

$G_H = 1.690$

Section Elevation	z	K _Z	q _Z	A _G	Face	A _F	A _R	A _{leg}	Leg %	C _A A _A In Face	C _A A _A Out Face
ft	ft		ksf	ft ²		ft ²	ft ²	ft ²		ft ²	ft ²
L1 150.0000-123.4230	136.0084	1.499	0.01	39.489	A	0.000	39.489	39.489	100.00	0.000	0.000
					B	0.000	39.489	100.00	0.000	0.000	
					C	0.000	39.489	100.00	0.000	6.979	
L2 123.4230-118.2500	120.8137	1.449	0.01	8.983	A	0.000	8.983	8.983	100.00	0.000	0.000
					B	0.000	8.983	100.00	0.000	0.000	
					C	0.000	8.983	100.00	0.000	3.125	
L3 118.2500-90.5000	103.8127	1.387	0.01	56.311	A	0.000	56.311	56.311	100.00	0.000	0.000
					B	0.000	56.311	100.00	0.000	0.000	
					C	0.000	56.311	100.00	0.000	19.549	
L4 90.5000-60.5000	75.0126	1.264	0.01	75.653	A	0.000	75.653	75.653	100.00	0.000	0.000
					B	0.000	75.653	100.00	0.000	0.000	
					C	0.000	75.653	100.00	0.000	23.590	
L5 60.5000-42.4130	51.2910	1.134	0.01	52.966	A	0.000	52.966	52.966	100.00	0.000	0.000
					B	0.000	52.966	100.00	0.000	0.000	
					C	0.000	52.966	100.00	0.000	14.222	
L6 42.4130-30.5000	36.3796	1.028	0.01	37.264	A	0.000	37.264	37.264	100.00	0.000	0.000
					B	0.000	37.264	100.00	0.000	0.000	
					C	0.000	37.264	100.00	0.000	9.367	
L7 30.5000-0.0000	14.8583	1	0.01	107.371	A	0.000	107.371	107.371	100.00	0.000	0.000
					B	0.000	107.371	100.00	0.000	0.000	
					C	0.000	107.371	100.00	0.000	23.983	

Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	150 - 123.423	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-13.70	1.21	-0.32
			Max. Mx	11	-4.74	203.23	-0.15
			Max. My	8	-4.74	0.22	-203.01
			Max. Vy	11	-17.84	203.23	-0.15
			Max. Vx	8	17.86	0.22	-203.01
			Max. Torque	8			-2.80
L2	123.423 - 118.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-14.75	1.27	-0.35
			Max. Mx	11	-5.62	354.61	-0.66
			Max. My	8	-5.62	0.77	-354.51
			Max. Vy	11	-18.48	354.61	-0.66
			Max. Vx	8	18.49	0.77	-354.51
			Max. Torque	2			2.82
L3	118.25 - 90.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-19.76	1.51	-0.47
			Max. Mx	11	-10.11	901.98	-2.32
			Max. My	8	-10.11	2.54	-902.31

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L4	90.5 - 60.5	Pole	Max. Vy	11	-21.04	901.98	-2.32
			Max. Vx	8	21.06	2.54	-902.31
			Max. Torque	2			2.94
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-27.48	1.84	-0.62
			Max. Mx	11	-17.10	1577.80	-4.11
			Max. My	8	-17.10	4.43	-1578.56
			Max. Vy	11	-24.02	1577.80	-4.11
L5	60.5 - 42.413	Pole	Max. Vx	8	24.03	4.43	-1578.56
			Max. Torque	13			3.15
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-31.04	1.98	-0.70
			Max. Mx	11	-20.38	1895.15	-4.88
			Max. My	8	-20.38	5.23	-1896.10
			Max. Vy	11	-25.13	1895.15	-4.88
			Max. Vx	8	25.15	5.23	-1896.10
L6	42.413 - 30.5	Pole	Max. Torque	13			3.24
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-37.66	2.18	-0.81
			Max. Mx	11	-26.37	2337.68	-5.90
			Max. My	8	-26.37	6.28	-2338.90
			Max. Vy	5	26.61	-2336.44	5.44
			Max. Vx	8	26.62	6.28	-2338.90
			Max. Torque	13			3.36
L7	30.5 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-47.67	2.56	-1.04
			Max. Mx	11	-35.63	3183.04	-7.69
			Max. My	8	-35.63	8.10	-3184.71
			Max. Vy	11	-28.88	3183.04	-7.69
			Max. Vx	8	28.89	8.10	-3184.71
			Max. Torque	13			3.59

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	24	47.67	7.05	-0.02
	Max. H _x	11	35.64	28.86	-0.06
	Max. H _z	2	35.64	-0.06	28.87
	Max. M _x	2	3184.13	-0.06	28.87
	Max. M _z	5	3181.59	-28.86	0.06
	Max. Torsion	13	3.59	14.38	24.98
	Min. Vert	1	35.64	0.00	0.00
	Min. H _x	5	35.64	-28.86	0.06
	Min. H _z	8	35.64	0.06	-28.87
	Min. M _x	8	-3184.71	0.06	-28.87
	Min. M _z	11	-3183.04	28.86	-0.06
	Min. Torsion	7	-3.59	-14.38	-24.98

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturing Moment, M _x kip-ft	Overturing Moment, M _z kip-ft	Torque kip-ft
Dead Only	35.64	0.00	0.00	0.28	0.70	0.00
Dead+Wind 0 deg - No Ice	35.64	0.06	-28.87	-3184.13	-6.70	-3.53
Dead+Wind 30 deg - No Ice	35.64	14.48	-25.03	-2761.16	-1596.84	-2.52
Dead+Wind 60 deg - No Ice	35.64	25.02	-14.48	-1598.31	-2758.92	-0.84
Dead+Wind 90 deg - No Ice	35.64	28.86	-0.06	-7.12	-3181.59	1.07
Dead+Wind 120 deg - No Ice	35.64	24.96	14.39	1586.09	-2751.58	2.69
Dead+Wind 150 deg - No Ice	35.64	14.38	24.98	2754.39	-1584.06	3.59

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 180 deg - No Ice	35.64	-0.06	28.87	3184.71	8.10	3.53
Dead+Wind 210 deg - No Ice	35.64	-14.48	25.03	2761.76	1598.26	2.52
Dead+Wind 240 deg - No Ice	35.64	-25.02	14.48	1598.90	2760.36	0.84
Dead+Wind 270 deg - No Ice	35.64	-28.86	0.06	7.69	3183.04	-1.07
Dead+Wind 300 deg - No Ice	35.64	-24.96	-14.39	-1585.54	2753.01	-2.69
Dead+Wind 330 deg - No Ice	35.64	-14.38	-24.98	-2753.84	1585.46	-3.59
Dead+Ice+Temp	47.67	-0.00	0.00	1.04	2.56	-0.00
Dead+Wind 0 deg+Ice+Temp	47.67	0.02	-7.05	-802.43	0.11	-0.91
Dead+Wind 30 deg+Ice+Temp	47.67	3.54	-6.11	-696.05	-401.64	-0.63
Dead+Wind 60 deg+Ice+Temp	47.67	6.12	-3.54	-402.88	-695.07	-0.19
Dead+Wind 90 deg+Ice+Temp	47.67	7.05	-0.02	-1.47	-801.54	0.31
Dead+Wind 120 deg+Ice+Temp	47.67	6.10	3.51	400.62	-692.52	0.72
Dead+Wind 150 deg+Ice+Temp	47.67	3.51	6.09	695.65	-397.24	0.94
Dead+Wind 180 deg+Ice+Temp	47.67	-0.02	7.05	804.57	5.20	0.91
Dead+Wind 210 deg+Ice+Temp	47.67	-3.54	6.11	698.20	406.96	0.63
Dead+Wind 240 deg+Ice+Temp	47.67	-6.12	3.54	405.03	700.38	0.19
Dead+Wind 270 deg+Ice+Temp	47.67	-7.05	0.02	3.62	806.85	-0.31
Dead+Wind 300 deg+Ice+Temp	47.67	-6.10	-3.51	-398.48	697.84	-0.72
Dead+Wind 330 deg+Ice+Temp	47.67	-3.51	-6.09	-693.51	402.55	-0.94
Dead+Wind 0 deg - Service	35.64	0.02	-9.99	-1103.91	-1.84	-1.24
Dead+Wind 30 deg - Service	35.64	5.01	-8.66	-957.26	-553.23	-0.89
Dead+Wind 60 deg - Service	35.64	8.66	-5.01	-554.03	-956.18	-0.30
Dead+Wind 90 deg - Service	35.64	9.98	-0.02	-2.27	-1102.74	0.37
Dead+Wind 120 deg - Service	35.64	8.64	4.98	550.17	-953.62	0.94
Dead+Wind 150 deg - Service	35.64	4.98	8.64	955.28	-548.78	1.26
Dead+Wind 180 deg - Service	35.64	-0.02	9.99	1104.49	3.30	1.24
Dead+Wind 210 deg - Service	35.64	-5.01	8.66	957.85	554.69	0.89
Dead+Wind 240 deg - Service	35.64	-8.66	5.01	554.62	957.65	0.30
Dead+Wind 270 deg - Service	35.64	-9.98	0.02	2.86	1104.20	-0.37
Dead+Wind 300 deg - Service	35.64	-8.64	-4.98	-549.59	955.09	-0.94
Dead+Wind 330 deg - Service	35.64	-4.98	-8.64	-954.70	550.25	-1.26

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-35.64	0.00	0.00	35.64	0.00	0.000%
2	0.06	-35.64	-28.87	-0.06	35.64	28.87	0.000%
3	14.48	-35.64	-25.03	-14.48	35.64	25.03	0.000%
4	25.02	-35.64	-14.48	-25.02	35.64	14.48	0.000%
5	28.86	-35.64	-0.06	-28.86	35.64	0.06	0.000%
6	24.96	-35.64	14.39	-24.96	35.64	-14.39	0.000%
7	14.38	-35.64	24.96	-14.38	35.64	-24.98	0.000%
8	-0.06	-35.64	28.87	0.06	35.64	-28.87	0.000%
9	-14.48	-35.64	25.03	14.48	35.64	-25.03	0.000%
10	-25.02	-35.64	14.48	25.02	35.64	-14.48	0.000%

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
11	-28.86	-35.64	0.06	28.86	35.64	-0.06	0.000%
12	-24.96	-35.64	-14.39	24.96	35.64	14.39	0.000%
13	-14.38	-35.64	-24.98	14.38	35.64	24.98	0.000%
14	0.00	-47.67	0.00	0.00	47.67	-0.00	0.000%
15	0.02	-47.67	-7.05	-0.02	47.67	7.05	0.000%
16	3.54	-47.67	-6.11	-3.54	47.67	6.11	0.000%
17	6.12	-47.67	-3.54	-6.12	47.67	3.54	0.000%
18	7.05	-47.67	-0.02	-7.05	47.67	0.02	0.000%
19	6.10	-47.67	3.51	-6.10	47.67	-3.51	0.000%
20	3.51	-47.67	6.09	-3.51	47.67	-6.09	0.000%
21	-0.02	-47.67	7.05	0.02	47.67	-7.05	0.000%
22	-3.54	-47.67	6.11	3.54	47.67	-6.11	0.000%
23	-6.12	-47.67	3.54	6.12	47.67	-3.54	0.000%
24	-7.05	-47.67	0.02	7.05	47.67	-0.02	0.000%
25	-6.10	-47.67	-3.51	6.10	47.67	3.51	0.000%
26	-3.51	-47.67	-6.09	3.51	47.67	6.09	0.000%
27	0.02	-35.64	-9.99	-0.02	35.64	9.99	0.000%
28	5.01	-35.64	-8.66	-5.01	35.64	8.66	0.000%
29	8.66	-35.64	-5.01	-8.66	35.64	5.01	0.000%
30	9.98	-35.64	-0.02	-9.98	35.64	0.02	0.000%
31	8.64	-35.64	4.98	-8.64	35.64	-4.98	0.000%
32	4.98	-35.64	8.64	-4.98	35.64	-8.64	0.000%
33	-0.02	-35.64	9.99	0.02	35.64	-9.99	0.000%
34	-5.01	-35.64	8.66	5.01	35.64	-8.66	0.000%
35	-8.66	-35.64	5.01	8.66	35.64	-5.01	0.000%
36	-9.98	-35.64	0.02	9.98	35.64	-0.02	0.000%
37	-8.64	-35.64	-4.98	8.64	35.64	4.98	0.000%
38	-4.98	-35.64	-8.64	4.98	35.64	8.64	0.000%

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 123.423	42.69	34	2.82	0.01
L2	126.59 - 118.25	29.44	34	2.45	0.01
L3	118.25 - 90.5	25.34	34	2.21	0.01
L4	90.5 - 60.5	14.27	34	1.58	0.00
L5	60.5 - 42.413	6.20	34	1.00	0.00
L6	47.58 - 30.5	3.84	34	0.75	0.00
L7	30.5 - 0	1.55	34	0.50	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
152.0000	1900MHz RRH (65MHz)	34	42.69	2.82	0.01	8942
138.0000	BXA-171063-12BF w/ Mount Pipe	34	35.68	2.67	0.01	3725
129.0000	(2) RRUS-11	34	30.70	2.50	0.01	2145
127.0000	(3) SBNH-1D5565C w/ Mount Pipe	34	29.65	2.46	0.01	2024
85.0000	KS24019-L112A	34	12.51	1.47	0.00	2775

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 123.423	122.48	9	8.10	0.03
L2	126.59 - 118.25	84.59	9	7.03	0.03
L3	118.25 - 90.5	72.84	9	6.37	0.02

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L4	90.5 - 60.5	41.08	9	4.54	0.01
L5	60.5 - 42.413	17.86	9	2.87	0.01
L6	47.58 - 30.5	11.05	9	2.17	0.00
L7	30.5 - 0	4.47	9	1.44	0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
152.0000	1900MHz RRH (65MHz)	9	122.48	8.10	0.03	3228
138.0000	BXA-171063-12BF w/ Mount Pipe	9	102.44	7.67	0.03	1343
129.0000	(2) RRUS-11	9	88.20	7.20	0.03	771
127.0000	(3) SBNH-1D6565C w/ Mount Pipe	9	85.19	7.06	0.03	726
85.0000	KS24019-L112A	9	36.00	4.23	0.01	977

Compression Checks

Pole Design Data

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	F_a ksi	A in^2	Actual P K	Allow. P_a K	Ratio $\frac{P}{P_a}$
L1	150 - 123.423 (1)	TP20.66x15x0.1875	26.5770	0.0000	0.0	39.00	11.7823	-4.73	459.51	0.010
L2	123.423 - 118.25 (2)	TP21.3901x19.6105x0.25	8.3400	0.0000	0.0	39.00	16.7746	-5.61	654.21	0.009
L3	118.25 - 90.5 (3)	TP27.3113x21.3901x0.483	27.7500	0.0000	0.0	34.01	41.1322	-10.10	1398.82	0.007
L4	90.5 - 60.5 (4)	TP33.2114x27.3113x0.599 1	30.0000	0.0000	0.0	34.12	62.0147	-17.09	2116.07	0.008
L5	60.5 - 42.413 (5)	TP37.07x33.2114x0.5727	18.0870	0.0000	0.0	34.25	64.3426	-20.37	2203.60	0.009
L6	42.413 - 30.5 (6)	TP38.9889x34.8222x0.622 2	17.0800	0.0000	0.0	34.33	70.0319	-22.92	2404.33	0.010
L7	30.5 - 0 (7)	TP45.5x38.9889x0.5742	30.5000	0.0000	0.0	34.60	72.9804	-28.60	2525.27	0.011

Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M_x kip-ft	Actual f_{bx} ksi	Allow. F_{bx} ksi	Ratio $\frac{f_{bx}}{F_{bx}}$	Actual M_y kip-ft	Actual f_{by} ksi	Allow. F_{by} ksi	Ratio $\frac{f_{by}}{F_{by}}$
L1	150 - 123.423 (1)	TP20.66x15x0.1875	203.24	42.44	39.00	1.088	0.00	0.00	39.00	0.000
L2	123.423 - 118.25 (2)	TP21.3901x19.6105x0.25	355.14	48.89	39.00	1.254	0.00	0.00	39.00	0.000
L3	118.25 - 90.5 (3)	TP27.3113x21.3901x0.48 3	904.23	40.25	34.01	1.184	0.00	0.00	34.01	0.000
L4	90.5 - 60.5 (4)	TP33.2114x27.3113x0.59 91 1	1581.9	38.43	34.12	1.126	0.00	0.00	34.12	0.000
L5	60.5 - 42.413 (5)	TP37.07x33.2114x0.5727 6	1900.0	40.91	34.25	1.194	0.00	0.00	34.25	0.000
L6	42.413 - 30.5 (6)	TP38.9889x34.8222x0.62 22 1	2031.6	40.17	34.33	1.170	0.00	0.00	34.33	0.000
L7	30.5 - 0 (7)	TP45.5x38.9889x0.5742 3	2549.0	42.69	34.60	1.234	0.00	0.00	34.60	0.000

Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f_v ksi	Allow. F_v ksi	Ratio $\frac{f_v}{F_v}$	Actual T kip-ft	Actual f_{vt} ksi	Allow. F_{vt} ksi	Ratio $\frac{f_{vt}}{F_{vt}}$
L1	150 - 123.423 (1)	TP20.66x15x0.1875	17.90	1.52	26.00	0.117	2.09	0.21	26.00	0.008
L2	123.423 - 118.25 (2)	TP21.3901x19.6105x0.25	18.54	1.11	26.00	0.085	2.10	0.14	26.00	0.005
L3	118.25 - 90.5 (3)	TP27.3113x21.3901x0.48 3	21.11	0.51	22.67	0.045	2.17	0.05	22.67	0.002
L4	90.5 - 60.5 (4)	TP33.2114x27.3113x0.59 91	24.08	0.39	22.75	0.034	2.30	0.03	22.75	0.001
L5	60.5 - 42.413 (5)	TP37.07x33.2114x0.5727	25.19	0.39	22.83	0.034	2.35	0.02	22.83	0.001
L6	42.413 - 30.5 (6)	TP38.9889x34.8222x0.62 22	25.83	0.37	22.89	0.032	2.37	0.02	22.89	0.001
L7	30.5 - 0 (7)	TP45.5x38.9889x0.5742	27.34	0.37	23.07	0.032	2.44	0.02	23.07	0.001

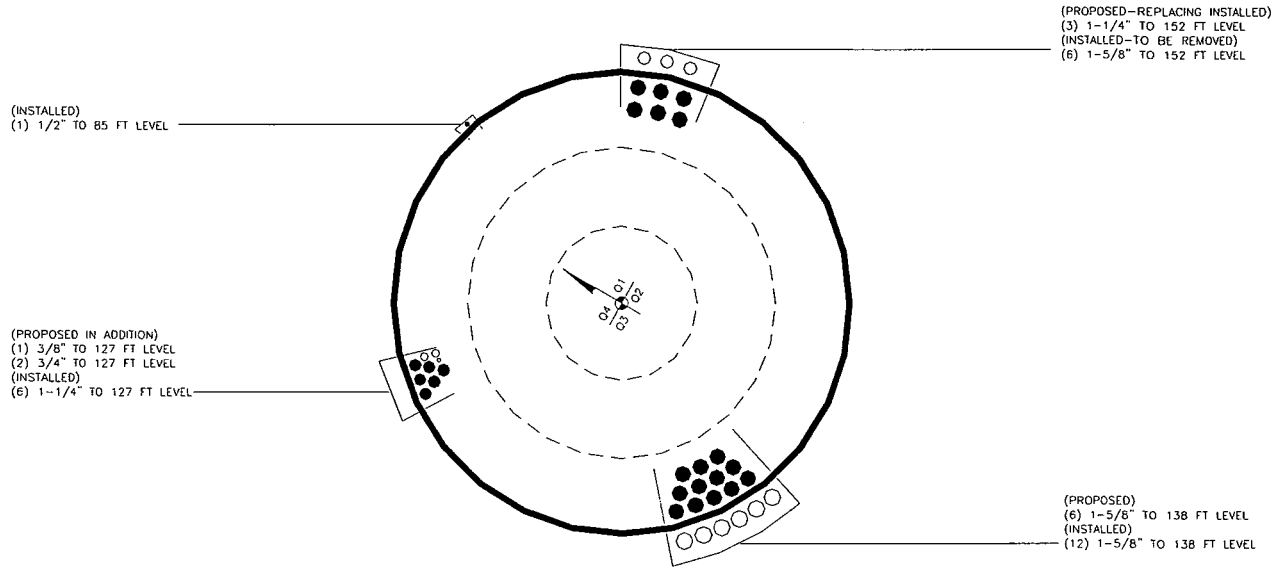
Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P}{P_a}$	Ratio $\frac{f_{bx}}{F_{bx}}$	Ratio $\frac{f_{by}}{F_{by}}$	Ratio $\frac{f_v}{F_v}$	Ratio $\frac{f_{vt}}{F_{vt}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	150 - 123.423 (1)	0.010	1.088	0.000	0.117	0.008	1.103	1.333	H1-3+VT ✓
L2	123.423 - 118.25 (2)	0.009	1.254	0.000	0.085	0.005	1.265	1.333	H1-3+VT ✓
L3	118.25 - 90.5 (3)	0.007	1.184	0.000	0.045	0.002	1.191	1.333	H1-3+VT ✓
L4	90.5 - 60.5 (4)	0.008	1.126	0.000	0.034	0.001	1.135	1.333	H1-3+VT ✓
L5	60.5 - 42.413 (5)	0.009	1.194	0.000	0.034	0.001	1.204	1.333	H1-3+VT ✓
L6	42.413 - 30.5 (6)	0.010	1.170	0.000	0.032	0.001	1.180	1.333	H1-3+VT ✓
L7	30.5 - 0 (7)	0.011	1.234	0.000	0.032	0.001	1.245	1.333	H1-3+VT ✓

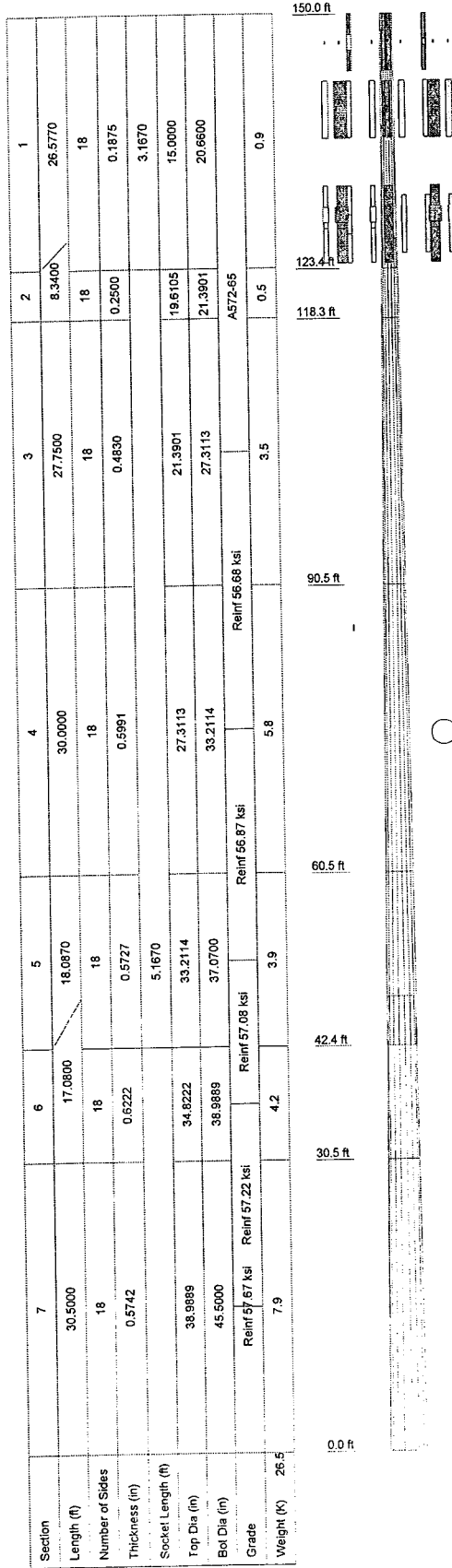
Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF* P_{allow} K	% Capacity	Pass Fail
L1	150 - 123.423	Pole	TP20.66x15x0.1875	1	-4.73	612.53	82.7	Pass
L2	123.423 - 118.25	Pole	TP21.3901x19.6105x0.25	2	-5.61	872.06	94.9	Pass
L3	118.25 - 90.5	Pole	TP27.3113x21.3901x0.483	3	-10.10	1864.63	89.4	Pass
L4	90.5 - 60.5	Pole	TP33.2114x27.3113x0.5991	4	-17.09	2820.72	85.1	Pass
L5	60.5 - 42.413	Pole	TP37.07x33.2114x0.5727	5	-20.37	2937.40	90.3	Pass
L6	42.413 - 30.5	Pole	TP38.9889x34.8222x0.6222	6	-22.92	3204.97	88.5	Pass
L7	30.5 - 0	Pole	TP45.5x38.9889x0.5742	7	-28.60	3366.18	93.4	Pass
Summary								
Pole (L2)							94.9	Pass
RATING =							94.9	Pass

APPENDIX B BASE LEVEL DRAWING



APPENDIX C
ADDITIONAL CALCULATIONS



DESIGNED APPURTENANCE LOADING

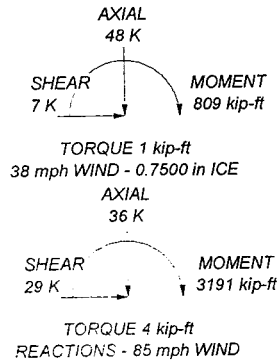
TYPE	ELEVATION	TYPE	ELEVATION
1900MHz RRH (65MHz)	152	BXA-70063-6CF-2 w/ Mount Pipe	138
800 EXTERNAL NOTCH FILTER	152	(2) LPA-80063-6CF-EDIN-2 w/ Mount Pipe	138
800MHz RRH	152		
(3) ACU-A20-N	152	BXA-70063-6CF-2 w/ Mount Pipe	138
APXVSP18-C-A20 w/ Mount Pipe	152	(2) LPA-80063-6CF-EDIN-2 w/ Mount Pipe	138
1900MHz RRH (65MHz)	152		
800 EXTERNAL NOTCH FILTER	152	BXA-171063-12BF w/ Mount Pipe	138
800MHz RRH	152	Platform Mount [LP 601-1]	138
(3) ACU-A20-N	152	(2) RRUS-11	129
APXVSP18-C-A20 w/ Mount Pipe	152	(2) RRUS-11	129
1900MHz RRH (65MHz)	152	(2) RRUS-11	129
800 EXTERNAL NOTCH FILTER	152	Side Arm Mount [SO 102-3]	129
800MHz RRH	152	(2) DTMAPB7819VG12A	127
(3) ACU-A20-N	152	(2) DTMAPB7819VG12A	127
APXVSP18-C-A20 w/ Mount Pipe	152	(3) AM-X-CD-16-65-00T-RET w/ Mount Pipe	127
Platform Mount [LP 602-1]	152	(3) SBNH-1D6565C w/ Mount Pipe	127
(3) 6' x 2.375" Pipe Mount	152	(2) DTMAPB7819VG12A	127
(3) 6' x 2.375" Pipe Mount	152	(3) SBNH-1D6565C w/ Mount Pipe	127
BXA-171063-12BF w/ Mount Pipe	138	T-Arm Mount [TA 601-3]	127
BXA-70063-6CF-2 w/ Mount Pipe	138	DCS-48-60-18-8F	127
(2) LPA-80063-6CF-EDIN-2 w/ Mount Pipe	138	KS24019-L112A	85
BXA-171063-12BF w/ Mount Pipe	138	Side Arm Mount [SO 701-1]	85

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi	Reinf 57.08 ksi	57 ksi	72 ksi
Reinf 56.68 ksi	57 ksi	71 ksi	Reinf 57.22 ksi	57 ksi	72 ksi
Reinf 56.87 ksi	57 ksi	72 ksi	Reinf 57.67 ksi	58 ksi	73 ksi

TOWER DESIGN NOTES

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 94.9%



Paul J Ford and Company
 250 E. Broad Street Suite 1500
 Columbus, OH 43215
 Phone: 614.221.6679
 FAX: 614.448.4105

Project: 150' MP; Seymour 2/ Oxford Town Garage; Oxford, CT	
Client: P/JF# 37512-1818 (BU# 876361)	
Client: CCI	Drawn by: Corey McCartney
Code: TIA/EIA-222-F	Date: 07/10/12
Path:	Scale: N.T.S.
	Dwg No: E-1



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STRUCTURAL ENGINEERS
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 Phone: 614-223-6679 • Fax: 614-448-1105 • www.PJFwd.com

Date: 7/10/2012
 PJF Project: 37512-1818
 Client Ref. # BU 876361
 Site Name: Seymour 2/ Oxford Town Garage
 Description: 150' MP
 Owner: CCI
 Engineer: CMM

v4.0 - Effective 1-12-12

Asymmetric Anchor Rod Analysis

Moment =	3191	k-ft	TIA Ref.	F	Location =	Base Plate	
Axial =	36.0	kips	ASIF =	1.3333	η =	N/A	for BP, Rev. G Sect. 4.9.9
Shear =	29.0	kips	Max Ratio =	105.0%	Threads =	N/A	for FP, Rev. G
Anchor Qty =	15						

**** For Post Installed Anchors: Check anchors for embedment, epoxy/grout bond, and capacity based on proof load. ****

Item	Nominal Anchor Dia, in	Anchor Spec	Fy, ksi	Fu, ksi	Location, degrees	Anchor Circle, in	Area Override, in ²	Area, in ²	Max Net Compression, kips	Max Net Tension, kips	Load for Capacity Calc, kips	Capacity Override, kips	Capacity, kips	Capacity Ratio
1	2.250	#18J A615 Gr 75	75	100	0.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
2	2.250	#18J A615 Gr 75	75	100	30.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
3	2.250	#18J A615 Gr 75	75	100	60.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
4	2.250	#18J A615 Gr 75	75	100	90.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
5	2.250	#18J A615 Gr 75	75	100	120.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
6	2.250	#18J A615 Gr 75	75	100	150.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
7	2.250	#18J A615 Gr 75	75	100	180.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
8	2.250	#18J A615 Gr 75	75	100	210.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
9	2.250	#18J A615 Gr 75	75	100	240.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
10	2.250	#18J A615 Gr 75	75	100	270.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
11	2.250	#18J A615 Gr 75	75	100	300.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
12	2.250	#18J A615 Gr 75	75	100	330.0	54.00	0.00	3.98	191.53	186.73	186.73	0.00	195.00	95.8%
13	2.250	A193 Gr B7	105	125	85.0	54.00	0.00	3.98	191.35	186.55	186.55	0.00	218.68	85.3%
14	2.250	A193 Gr B7	105	125	205.0	54.00	0.00	3.98	191.35	186.55	186.55	0.00	218.68	85.3%
15	2.250	A193 Gr B7	105	125	325.0	54.00	0.00	3.98	191.35	186.55	186.55	0.00	218.68	85.3%

59.69

Stiffened or Unstiffened, UngROUTed, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data	
BU#:	
Site Name:	
App #:	
Pole Manufacturer:	Other

Reactions		
Moment:	2553.3	ft-kips
Axial:	28.8	kips
Shear:	23.2	kips

Anchor Rod Data		
Qty:	12	
Diam:	2.25	in
Rod Material:	A615-J	
Strength (Fu):	100	ksi
Yield (Fy):	75	ksi
Bolt Circle:	54	in

If No stiffeners, Criteria: **AISC ASD** <-Only Applicable to Unstiffened Cases

Anchor Rod Results	
Maximum Rod Tension:	186.7 Kips
Allowable Tension:	195.0 Kips
Anchor Rod Stress Ratio:	95.8% Pass

Stiffened
Service, ASD
Fty*ASIF

Plate Data		
Diam:	60	in
Thick:	1.75	in
Grade:	60	ksi
Single-Rod B-eff:	12.03	in

Base Plate Results		Flexural Check
Base Plate Stress:	57.0 ksi	
Allowable Plate Stress:	60.0 ksi	
Base Plate Stress Ratio:	95.0% Pass	

Stiffened
Service, ASD
0.75*Fy*ASIF
Y.L. Length:
N/A, Roark

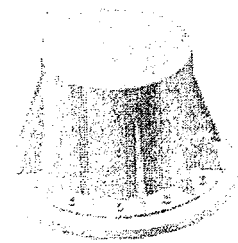
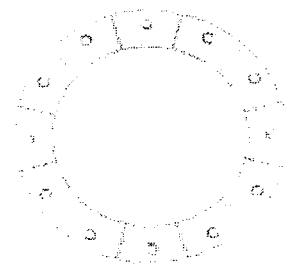
Stiffener Data (Welding at both sides)		
Config:	1	*
Weld Type:	Both	
Groove Depth:	0.5	in **
Groove Angle:	45	degrees
Fillet H. Weld:	0.5	in
Fillet V. Weld:	0.375	in
Width:	6	in
Height:	18	in
Thick:	1	in
Notch:	0.75	in
Grade:	65	ksi
Weld str.:	80	ksi

Stiffener Results	
Horizontal Weld :	48.0% Pass
Vertical Weld:	46.6% Pass
Plate Flex+Shear, fb/Fb+(fv/Fv)^2:	11.2% Pass
Plate Tension+Shear, f/Ft+(fv/Fv)^2:	47.4% Pass
Plate Comp. (AISC Bracket):	48.8% Pass

Pole Results	
Pole Punching Shear Check:	14.4% Pass

Pole Data		
Diam:	45.5	in
Thick:	0.375	in
Grade:	65	ksi
# of Sides:	18	"0" IF Round
Fu	80	ksi
Reinf. Fillet Weld	0	"0" if None

Stress Increase Factor		
ASIF:	1.333	



* 0 = none. 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt
 ** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes



PAUL J. FORD AND COMPANY
STRUCTURAL ENGINEERS
 250 East Broad Street • Suite 1500 • Columbus, Ohio 43215-3708
 Phone 614-221-6679 • Fax 614-448-1103 • www.PJFweb.com

Date: 7/10/2012
 PJF Project: 37512-1818
 Client Ref. # BU 876361
 Site Name: Seymour 2/ Oxford Town Garage
 Description: 150' MP
 Owner: CCI
 Engineer: CMM

v4.0 - Effective 1-12-12

Micropiles

Moment =	500	k-ft	TIA Ref.	F	Location =	Base Plate
Axial =	0.0	kips	ASIF =	1.3333	η =	N/A for BP, Rev. G Sect. 4.9.9
Shear =	0.0	kips	Max Ratio =	105.0%	Threads =	N/A for FP, Rev. G
Anchor Qty =	3					

**** For Post Installed Anchors: Check anchors for embedment, epoxy/grout bond, and capacity based on proof load. ****

Item	Nominal Anchor Dia, in	Anchor Spec	Fy, ksi	Fu, ksi	Location, degrees	Anchor Circle, in	Area Override, in ²	Area, in ²	Max Net Compression, kips	Max Net Tension, kips	Load for Capacity Calc, kips	Capacity Override, kips	Capacity, kips	Capacity Ratio
1	0.000		109	87	0.0	186.00	1.36	1.36	45.62	45.62	45.62	75.60	75.60	60.3%
2	0.000		109	87	90.0	186.00	1.36	1.36	64.52	64.52	64.52	75.60	75.60	85.3%
3	0.000		109	87	180.0	186.00	1.36	1.36	45.62	45.62	45.62	75.60	75.60	60.3%

4.08

Foundation Loads:

Tower leg compression = 36 (kips)
 Horizontal load at top of pier = 29 (kips)
 Overturning moment at top of pier = 2691 (ft-kips)

Design criteria:

Safety factor against overturning = 1.5

Soil Properties:

Soil density = 120 (pcf)
 Allowable soil bearing = 6 (ksf)
 Depth to water table = 99 (ft)

Dimensions:

Pier shape (round or square) S ("R" or "S")
 Pier width = 6 (ft)
 Pier height above grade = 1 (ft)
 depth to bottom of footing = 6 (ft)
 Footing thickness = 3 (ft)
 Footing width = 21.5 (ft)
 Footing length = 21.5 (ft)

Concrete:

Concrete strength = 3 (ksi)
 Rebar strength = 60 (ksi)
 ultimate load factor = 1.3

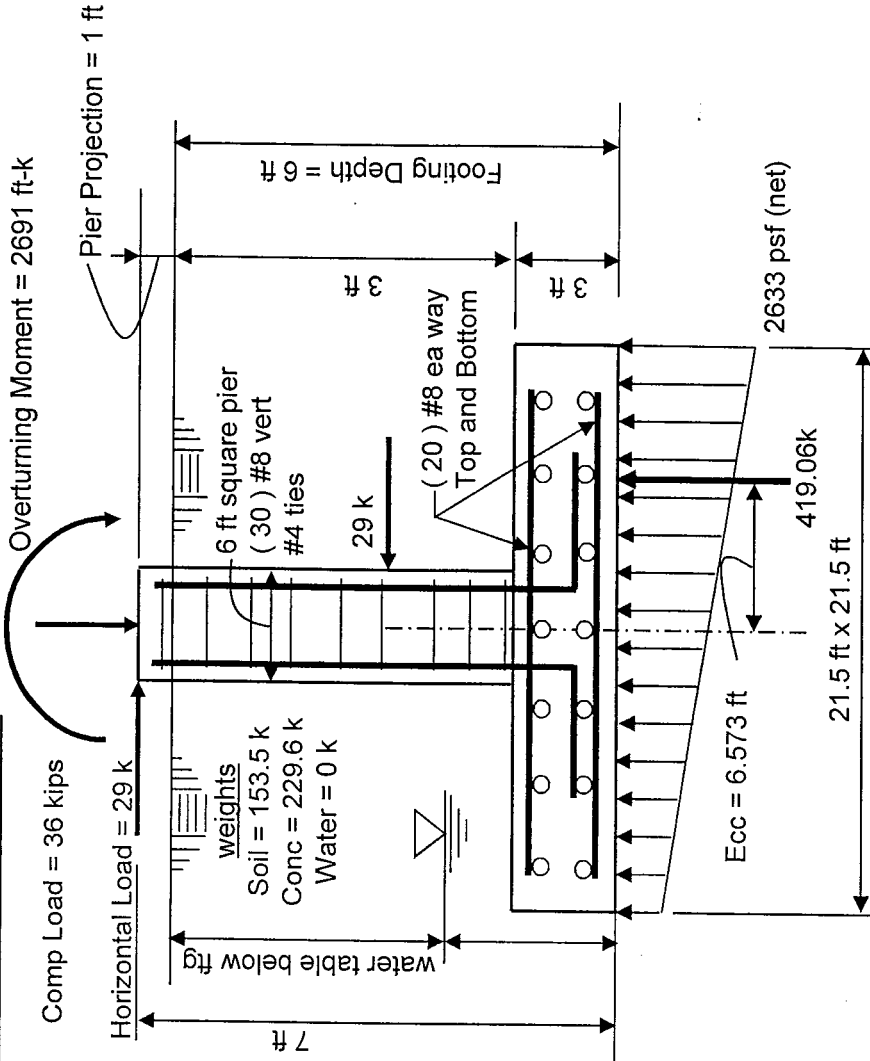
Reinforcing Steel:

minimum cover over rebar = 3 inches
 size of pad rebar = #8 bar
 quantity of pad rebar = 20 (ea direction)

Reinforcing Steel:

size of vert rebar in pier = #8 bar
 vertical rebar quantity = 30
 size of pier ties = #4 bar
 minimum cover over rebar = 3 inches

Total volume of concrete = 56.7 cu yd



Summary of analysis results

Maximum Net Soil Bearing = 2.633 ksf
 Allowable Net Soil Bearing = 6 ksf
Soil Bearing Stress Ratio = 0.44 Okay

Ult Bending Shear Capacity = 110 psi
 Ult Bending Shear Stress = 39 psi
Bending Shear Stress Ratio = 0.36 Okay

Fig Overturning Resistance = 4505 ft-kips
 Overturning Moment = 2755 ft-kips
 Required Overturning Safety Factor = 1.5
 Overturning Safety Factor = 1.635
Ratio = 0.92 Okay

Pad Bending Moment Capacity = 2188 ft-k
 Pad Bending Moment = 1393 ft-k
Bending Moment Stress Ratio = 0.64 OK

STRUCTUREPOINT - spColumn v4.80 (TM)
 Licensed to: Paul J. Ford and Company - Columbus. License ID: 58800-1028985-4-1E6CD-22701
 g:\tower\375_crown_castle\2012\37512-1818 bu 876361\37512-1818.col

General Information:

File Name: g:\tower\375_crown_castle\2012\37512-1818 bu 876361\37512-1818.col
 Project: 37512-1818
 Column: ACI 318-02
 Code: ACI 318-02
 Engineer: CMM
 Units: English

Run Option: Investigation
 Run Axis: X-axis
 Slenderness: Not considered
 Column Type: Structural

Material Properties:

$f_y = 60$ ksi
 $E_s = 29000$ ksi
 $f'_c = 3$ ksi
 $E_c = 3122.02$ ksi
 Ultimate strain = 0.003 in/in
 Beta1 = 0.85

Section:

Rectangular: Width = 72 in Depth = 72 in
 Gross section area, $A_g = 5184$ in²
 $I_x = 2.23949e1006$ in⁴
 $I_y = 2.23949e+006$ in⁴
 $r_x = 20.7846$ in
 $r_y = 20.7846$ in
 $X_o = 0$ in
 $Y_o = 0$ in

Reinforcement:

Bar Set: ASTM A615

Size	Diam (in)	Area (in ²)	Size	Diam (in)	Area (in ²)
# 3	0.38	0.11	# 4	0.50	0.20
# 6	0.75	0.44	# 7	0.88	0.60
# 9	1.13	1.00	# 10	1.27	1.27
# 14	1.69	2.25	# 18	2.26	4.00
			# 5	0.63	0.31
			# 8	1.00	0.79
			# 11	1.41	1.56

Confinement: Tied; #4 ties with #8 bars, #4 with larger bars.
 $\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Layout: Circular
 Pattern: All Sides Equal (Cover to transverse reinforcement)
 Total steel area: $A_s = 23.70$ in² at $\rho = 0.46\%$ (Note: $\rho < 0.50\%$)
 Minimum clear spacing = 4.96 in

30 #8 Cover = 6.5 in

Factored Loads and Moments with Corresponding Capacities:

No.	P_u kip	M_{ux} k-ft	ϕM_{nx} k-ft	$\phi M_n/\mu$	NA depth in	Dt depth in	eps_t	ϕ
1	36.00	2807.00	3489.36	1.243	7.99	64.50	0.02121	0.900

*** End of output ***



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

August 10, 2015

Camille M. Mulligan
Alcatel-Lucent
1 Robbins Road
Westford, MA 01886

RE: Compliance Extension Request

EM-SPRINT-008-130130	93 Old Amity Road	Bethany
EM-SPRINT-009-131008	8 Sky Edge Drive	Bethel
EM-SPRINT-017-131008	371 Terryville Avenue	Bristol
EM-SPRINT-018-130322	39 Carmen Hill Road	Brookfield
EM-SPRINT-033-130920	179 Shunpike Road	Cromwell
EM-SPRINT-034-130920	41 Padanaram Road	Danbury
EM-SPRINT-069-130409	246 East Franklin Street	Danielson
EM-SPRINT-035-130322	126 Ledge Road	Darien
EM-SPRINT-043-130311	310 Prestige Park Road	East Hartford
EM-SPRINT-047-131008	232 South Main Street	East Windsor
EM-SPRINT-051-130606	280 Morehouse Drive	Fairfield
EM-SPRINT-052-130606	45 Maple Ridge Road	Farmington
EM-SPRINT-057-120122	363 Riversville Road	Greenwich
EM-SPRINT-057-131127	9 Sound Shore Dr., a/k/a 12 Sound Shore Drive	Greenwich
EM-SPRINT-059-130819	99 Briar Road	Groton
EM-SPRINT-062-130509	Talmadge Road	Hamden
EM-SPRINT-068-121226	136 Bulls Bridge Road	Kent
EM-SPRINT-076-130819	135 New Road	Madison
EM-SPRINT-077-130828	Olcott Street a/k/a 250 Olcott Street	Manchester
EM-SPRINT-080-131024	21 West Peak Drive	Meriden
EM-SPRINT-081-130716	1 Service Road	Middlebury
EM-SPRINT-084-130124	528 Wheeler's Farm Rd.	Milford
EM-SPRINT-091-130606	302 Ball Pond Road	New Fairfield
EM-SPRINT-095-131008	26 Washinton Street	New London
EM-SPRINT-097-131008	8 Ferris Road	Newtown
EM-SPRINT-097-131129	201 South Main St.	Newtown
EM-SPRINT-103-121226	173/177 West Rocks Road	Norwalk
EM-SPRINT-104-131112	2 Hinkley Hill Road	Norwich
EM-SPRINT-108-130215	20 Great Oak Road	Oxford
EM-SPRINT-108-130401	133 Coppermine Road	Oxford
EM-SPRINT-108-130712	338 Oxford Road	Oxford
EM-SPRINT-119-130314	47 Inwood Road	Rocky Hill



EM-SPRINT-119-130819	52 New Britain Avenue	Rocky Hill
EM-SPRINT-120-130828	Lower County Road a/k/a 35 Lower County Road	Roxbury
EM-SPRINT-126-130325	219 Nells Rock Road	Shelton
EM-SPRINT-126-130515	70 Platt Road	Shelton
EM-SPRINT-128-131112	22 Wintonbury Road (aka 49a and 53 Wintonbury Road)	Simsbury
EM-SPRINT-130-130531	1432 Old Waterbury Road	Southbury
EM-SPRINT-135-130128	69 Guinea Road	Stamford
EM-SPRINT-135-131112	366 Old Long Ridge Road	Stamford
EM-SPRINT-143-130712	350 Burr Mountain Road	Torrington
EM-SPRINT-151-131209	184 Garden Circle	Waterbury
EM-SPRINT-155-130828	345 North Main Street a/k/a 333 North Main Street	West Hartford
EM-SPRINT-157-130701	56 Norfield Road	Weston
EM-SPRINT-164-130920	Windsor Avenue a/k/a 494 Windsor Avenue	Windsor
EM-SPRINT-NEXTEL-166-130116	164 County Road	Wolcott

Dear Ms. Mulligan:

The Connecticut Siting Council (Council) is in receipt of your letter dated August 10, 2015, submitted on behalf of Sprint, requesting an extension of time to submit notices of completion of construction and associated post modification inspection reports for the above-referenced exempt modifications that were approved in 2013.

Please be advised that Council approval of these exempt modifications has expired. Therefore, any additional changes to these facilities will require explicit notice to the Council pursuant to Regulations of Connecticut State Agencies Section 16-50j-73 and a filing fee.

Thank you for your attention to this matter.

Sincerely,



Melanie A. Bachman
Acting Executive Director

MAB/cm

Site ID	CT23XC507 - Seymour / Oxford Town Garage																
Site Address	20 Great Oak Road, Oxford, CT 06478																
Site Type	Monopole																
Sector 1																	
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
1a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150	144	1/2 "	0.5	0	1386.9474	24.0459	2.40459%
1a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	150	144	1/2 "	0.5	0	389.96892	6.761001	1.19242%
Sector total Power Density Value:																3.597%	
Sector 2																	
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
2a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150	144	1/2 "	0.5	0	1386.9474	24.0459	2.40459%
2a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	150	144	1/2 "	0.5	0	389.96892	6.761001	1.19242%
Sector total Power Density Value:																3.597%	
Sector 3																	
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBd)	Antenna Height (ft)	analysis height	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
3a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	150	144	1/2 "	0.5	0	1386.9474	24.0459	2.40459%
3a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	150	144	1/2 "	0.5	0	389.96892	6.761001	1.19242%
Sector total Power Density Value:																3.597%	

Site Composite MPE %	
Carrier	MPE %
Sprint	10.791%
AT&T	7.980%
Verizon Wireless	5.630%
Total Site MPE %	24.401%

CROWN CASTLE PROJECT: BU #876361; SEYMOUR 2/OXFORD TOWN GARAGE; OXFORD, CT
MONOPOLE RETROFIT PROJECT MASTER NOTES DOCUMENT (REV. 2, 1/22/2009)

UPON THE SUCCESSFUL AND COMPLETE INSTALLATION OF THE REINFORCING SYSTEM SPECIFIED IN THESE PLANS, THE REINFORCED POLE MEETS THE WIND DESIGN RECOMMENDATIONS OF THE TIA/EIA-222-F-1996 STANDARD FOR WIND SPEEDS OF 85 MPH AND 38 MPH + 3/4" RADIAL ICE

A. GENERAL NOTES

- IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO FABRICATION AND CONSTRUCTION. THESE DRAWINGS WERE PREPARED FROM INFORMATION AND DOCUMENTS PROVIDED TO PAUL J. FORD & COMPANY BY CROWN CASTLE. THIS INFORMATION PROVIDED HAS NOT BEEN FIELD VERIFIED BY PAUL J. FORD & COMPANY FOR ACCURACY AND THEREFORE DISCREPANCIES BETWEEN THESE DRAWINGS AND ACTUAL SITE CONDITIONS SHOULD BE ANTICIPATED. ANY DISCREPANCIES AND/OR CHANGES BETWEEN THE INFORMATION CONTAINED IN THESE DRAWINGS AND THE ACTUAL VERIFIED SITE CONDITIONS SHALL BE IMMEDIATELY BROUGHT TO THE ATTENTION OF CROWN CASTLE AND PAUL J. FORD & COMPANY SO THAT ANY CHANGES AND/OR ADJUSTMENTS, IF NECESSARY, CAN BE MADE TO THE DESIGN AND DRAWINGS.
- THE EXISTING UNREINFORCED MONOPOLE STRUCTURE DOES NOT HAVE THE STRUCTURAL CAPACITY TO CARRY ALL OF THE ANTENNA AND PLATFORM LOADS SHOWN ON THESE DRAWINGS AT THE REQUIRED MINIMUM TIA/EIA-222-F BASIC WIND SPEEDS. DO NOT INSTALL ANY ADDITIONAL OR NEW ANTENNA AND PLATFORM LOADS UNTIL THE MONOPOLE REINFORCING SYSTEM IS COMPLETELY AND SUCCESSFULLY INSTALLED.
- IF MATERIALS, QUANTITIES, STRENGTHS OR SIZES INDICATED BY THE DRAWINGS OR SPECIFICATIONS ARE NOT IN AGREEMENT WITH THESE NOTES, THE BETTER QUALITY AND/OR GREATER QUANTITY, STRENGTH OR SIZE INDICATED, SPECIFIED OR NOTED SHALL BE PROVIDED.
- THIS STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER THE INSTALLATION OF THE REINFORCING REPAIR SYSTEM HAS BEEN PROPERLY AND ADEQUATELY COMPLETED. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY TO INSURE THE SAFETY AND STABILITY OF THE MONOPOLE AND ITS COMPONENT PARTS DURING FIELD MODIFICATIONS. THIS INCLUDES, BUT IS NOT LIMITED TO, THE ADDITION OF WHATEVER TEMPORARY BRACING, GUYS OR TIE DOWNS THAT MAY BE NECESSARY. SUCH MATERIAL SHALL BE REMOVED AND SHALL REMAIN THE PROPERTY OF THE CONTRACTOR AFTER THE COMPLETION OF THE PROJECT. IMPORTANT CUTTING, WELDING AND SAFETY GUIDELINES: THE CONTRACTOR SHALL FOLLOW ALL CROWN CASTLE CUTTING, WELDING, FIRE PREVENTION AND SAFETY GUIDELINES. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL OBTAIN A COPY OF THE CURRENT CROWN CASTLE GUIDELINES FROM CROWN CASTLE PER THE 12-01-2005 CROWN CASTLE DIRECTIVE. "ALL CUTTING AND WELDING ACTIVITIES SHALL BE CONDUCTED IN ACCORDANCE WITH CROWN CASTLE POLICY CUTTING AND WELDING PLAN" (DOC # ENG-PLN-10015) ON AN ONGOING BASIS THROUGHOUT THE ENTIRE LIFE OF THE PROJECT.
- THE STRUCTURAL CONTRACT DOCUMENTS DO NOT INDICATE THE METHOD OR MEANS OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES. OBSERVATION VISITS TO THE SITE BY THE OWNER AND/OR THE ENGINEER SHALL NOT INCLUDE INSPECTIONS OF THE PROTECTIVE MEASURES OR THE CONSTRUCTION PROCEDURES.
- ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE FURNISHED BY THE INSPECTING/TESTING AGENCY. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE SOLELY FOR THE PURPOSE OF ASSISTING IN QUALITY CONTROL AND IN ACHIEVING CONFORMANCE WITH CONTRACT DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE CONSTRUED AS SUPERVISION OF CONSTRUCTION.
- ALL MATERIALS AND EQUIPMENT FURNISHED WILL BE NEW AND OF GOOD QUALITY, FREE FROM FAULTS AND DEFECTS AND IN CONFORMANCE WITH THE CONTRACT DOCUMENTS. ANY AND ALL SUBSTITUTIONS MUST BE PROPERLY APPROVED AND AUTHORIZED IN WRITING BY THE OWNER AND ENGINEER PRIOR TO INSTALLATION. THE CONTRACTOR SHALL FURNISH SATISFACTORY EVIDENCE AS TO THE KIND AND QUALITY OF MATERIALS AND EQUIPMENT BEING SUBSTITUTED.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR INITIATING, MAINTAINING, AND SUPERVISING ALL SAFETY PRECAUTIONS AND PROGRAMS IN CONNECTION WITH THE WORK. THE CONTRACTOR IS RESPONSIBLE TO INSURE THAT THIS PROJECT AND RELATED WORK COMPLIES WITH ALL APPLICABLE LOCAL, STATE, AND FEDERAL SAFETY CODES AND REGULATIONS GOVERNING THIS WORK AS WELL AS CROWN CASTLE SAFETY GUIDELINES.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING AND NEW COAXIAL CABLES AND OTHER EQUIPMENT DURING CONSTRUCTION.
- ANY EXISTING ATTACHMENTS AND/OR PROJECTIONS ON THE POLE THAT MAY INTERFERE WITH THE INSTALLATION OF THE REINFORCING SYSTEM WILL HAVE TO BE REMOVED, AND/OR RELOCATED, AND/OR REPLACED AND RE-INSTALLED AFTER THE REINFORCING IS SUCCESSFULLY COMPLETED. THE CONTRACTOR SHALL IDENTIFY AND COORDINATE THESE ITEMS PRIOR TO CONSTRUCTION WITH THE OWNER, TESTING AGENCY, AND ENGINEER.
- ANY AND ALL EXISTING PLATFORMS THAT ARE LOCATED IN AREAS OF THE POLE SHAFT WHERE SHAFT REINFORCING MUST BE APPLIED SHALL BE TEMPORARILY REMOVED OR OTHERWISE SUPPORTED TO PERMIT NEW CONTINUOUS REINFORCEMENT TO BE ATTACHED. AFTER THE CONTRACTOR HAS SUCCESSFULLY INSTALLED THE MONOPOLE REINFORCEMENT SYSTEM, THE CONTRACTOR SHALL RE-INSTALL THE PLATFORMS. IN NO CASE SHALL ANY NEW AND/OR ADDITIONAL PLATFORMS AND/OR ANTENNAS AND/OR COAX CABLES AND/OR OTHER EQUIPMENT BE INSTALLED ON THE MONOPOLE UNTIL THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF ALL OF THE REQUIRED STRUCTURAL REINFORCING SYSTEM COMPONENTS.
- "LOW HEAT" WELDING PROCEDURES:
A. ANY AND ALL FIELD WELDING REQUIRED ON THIS PROJECT SHALL BE PERFORMED BY AWS CERTIFIED WELDERS USING "LOW HEAT" WELDING TECHNIQUES.
FOR THE PURPOSES OF THIS PROJECT, "LOW HEAT" WELDING IS DEFINED AS A CAREFUL AND CONTROLLED WELDING PROCESS, PERFORMED BY EXPERIENCED AWS CERTIFIED WELDERS, SUCH THAT THE CORRECT AMOUNT OF WELD METAL IS DEPOSITED AND IS PROPERLY FUSED IN SUCH A WAY THAT EXCESSIVE AMOUNTS OF HEAT BUILD UP AT THE WELDED JOINT, DUE TO EXCESSIVE MOLTEN WELD METAL POOLING, IS AVOIDED.
- THE "LOW HEAT" WELDING PROCESS SHALL BE SET UP SO THAT ANY FIELD WELDING ACTIVITY ON THE INSIDE OF THE POLE SHAFT OR OTHERWISE DAMAGE THE EXISTING GALVANIZED SURFACE PROTECTION AND FIRE SAFETY GUIDELINES, SHALL BE SET UP SO THAT ANY FIELD WELDING ACTIVITY ON THE POLE STRUCTURE DOES NOT SCORCH AND/OR OTHERWISE DAMAGE THE EXISTING COAX CABLES THAT RUN ON THE INSIDE AND/OR OUTSIDE OF THE POLE SHAFT IN AND AROUND THE REGION OF THE WELD.
- "LOW HEAT" WELD DEMONSTRATION REQUIRED: PRIOR TO BEGINNING THE FIELD WELDING FOR THE REINFORCEMENT WORK, THE CONTRACTOR'S AWS CERTIFIED WELDER SHALL DEMONSTRATE THE "LOW HEAT" WELDING PROCESS THAT WILL BE USED ON THIS PROJECT SO THAT CROWN CASTLE REPRESENTATIVES CAN OBSERVE AND VERIFY THAT THE PROPOSED PROCESS DOES NOT DAMAGE THE EXISTING GALVANIZED SURFACE ON THE BACK SIDE OF THE SAMPLE PLATE THAT IS BEING WELDED. THE CONTRACTOR SHALL USE TEMPERATURE MONITORING DEVICES SUCH AS THERMOCOUPLE, HEAT CRAYON, AND/OR INFRARED SENSOR TO MEASURE AND DEMONSTRATE THE TEMPERATURE OF THE STEEL ON THE BACK SURFACE IN THE REGION OF THE WELD. THE "LOW HEAT" WELD DEMONSTRATION SHALL BE CARRIED OUT ON-SITE AND USING A GALVANIZED STEEL PLATE SAMPLE WITH A THICKNESS EQUAL TO THE MINIMUM SHAFT THICKNESS THAT WILL BE REINFORCED. ONLY AFTER THE "LOW HEAT" TECHNIQUES HAVE BEEN SUCCESSFULLY DEMONSTRATED AND ARE APPROVED BY CROWN CASTLE REPRESENTATIVES, CAN THE CONTRACTOR PROCEED WITH THE FIELD WELDING ON THE STRUCTURE. CAUTION: THE CONTRACTOR SHALL CAREFULLY FOLLOW ALL CROWN CASTLE CUTTING, WELDING, FIRE SAFETY, AND ALL OTHER SAFETY GUIDELINES WHICH ALSO INCLUDE "LOW HEAT" WELDING TECHNIQUES. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR MAINTAINING THE SAFETY AND STABILITY OF THE STRUCTURE DURING CONSTRUCTION. THE CONTRACTOR SHALL BE HELD FULLY LIABLE FOR ANY DAMAGE (INCLUDING HEAT AND FIRE DAMAGE CAUSED BY FIELD WELDING) TO THE STRUCTURE AND ANY OF ITS COMPONENTS WHICH OCCURS DURING CONSTRUCTION.

- SPECIAL INSPECTION AND TESTING
ALL WORK SHALL BE SUBJECT TO REVIEW AND OBSERVATION BY THE OWNER'S REPRESENTATIVE AND THE OWNER'S AUTHORIZED INDEPENDENT INSPECTION AND TESTING AGENCY. REFER TO CROWN CASTLE DOCUMENT ENG-SOW-10066 FOR SPECIFICATION.
- ANY SUPPORT SERVICES PERFORMED BY THE ENGINEER DURING CONSTRUCTION SHALL BE DISTINGUISHED FROM CONTINUOUS AND DETAILED INSPECTION SERVICES WHICH ARE FURNISHED BY OTHERS. THESE SUPPORT SERVICES PERFORMED BY THE ENGINEER ARE PERFORMED SOLELY FOR THE PURPOSE OF ASSISTING IN QUALITY CONTROL AND IN ACHIEVING CONFORMANCE WITH CONTRACT DOCUMENTS. THEY DO NOT GUARANTEE CONTRACTOR'S PERFORMANCE AND SHALL NOT BE CONSTRUED AS SUPERVISION OF CONSTRUCTION.
- OBSERVED DISCREPANCIES BETWEEN THE WORK AND THE CONTRACT DOCUMENTS SHALL BE CORRECTED BY THE CONTRACTOR AT NO ADDITIONAL COST.
- AN INDEPENDENT QUALIFIED INSPECTING/TESTING AGENCY SHALL BE SELECTED, RETAINED AND PAID FOR BY THE OWNER FOR THE SOLE PURPOSE OF INSPECTING, TESTING, DOCUMENTING, AND APPROVING ALL WELDING AND FIELD WORK PERFORMED BY THE CONTRACTOR.

- ACCESS TO ANY PLACE WHERE WORK IS BEING DONE SHALL BE PERMITTED AT ALL TIMES. THE INSPECTION AGENCY SHALL SO SCHEDULE THIS WORK AS TO CAUSE A MINIMUM OF INTERRUPTION TO, AND COORDINATE WITH, THE WORK IN PROGRESS. IT IS THE CONTRACTOR'S RESPONSIBILITY TO COORDINATE THE WORK SCHEDULE WITH THE TESTING AGENCY. THE CONTRACTOR SHALL ALLOW FOR ADEQUATE TIME AND ACCESS FOR THE TESTING AGENCY TO PERFORM THEIR DUTIES.
- THE INSPECTOR AND TESTING AGENCY SHALL BE RESPONSIBLE TO PERFORM THE FOLLOWING SERVICES FOR THE OWNER. THE TESTING AGENCY SHALL INSPECT THE FOLLOWING ITEMS IN ACCORDANCE WITH THE CONSTRUCTION DRAWINGS. THE TESTING AGENCY SHALL INSPECT ITEMS ON THIS LIST AND OTHER ITEMS AS NECESSARY TO FULFILL THEIR RESPONSIBILITY. THE TESTING AGENCY SHALL UTILIZE EXPERIENCED, TRAINED INSPECTORS INCLUDING AWS CERTIFIED WELDING INSPECTORS (CWI) INSPECTORS SHALL HAVE THE TRAINING, CREDENTIALS, AND EXPERIENCE APPROPRIATE FOR AND COMMENSURATE WITH THE SCOPE AND TYPE OF INSPECTION WORK TO BE PERFORMED.

- PERFORM CONTINUOUS ON-SITE OBSERVATION, INSPECTION, VERIFICATION, AND TESTING DURING THE TIME THE CONTRACTOR IS WORKING ON-SITE. AGENCY SHALL NOTIFY OWNER IMMEDIATELY WHEN FIELD PROBLEMS OR DISCREPANCIES OCCUR.
- FOUNDATIONS, CONCRETE, AND SOIL PREPARATION - (NOT REQUIRED)
- CONCRETE TESTING PER AGI - (NOT REQUIRED)

- CHECK THE STEEL ON THE JOB WITH THE PLANS.
- CHECK MILL CERTIFICATIONS.
- CHECK GRADE OF STEEL MEMBERS, AND BOLTS FOR CONFORMANCE WITH DRAWINGS.
- INSPECT STEEL MEMBERS FOR DISTORTION, EXCESSIVE RUST, FLAWS AND BURNED HOLES.
- CALL FOR LABORATORY TEST REPORTS WHEN IN DOUBT.
- CHECK STEEL MEMBERS FOR SIZES, SWEEP AND DIMENSIONAL TOLERANCES.
- CHECK FOR SURFACE FINISH SPECIFIED, GALVANIZED.
- CHECK BOLT TIGHTENING ACCORDING TO AISC "TURN OF THE NUT" METHOD.

- VERIFY FIELD WELDING PROCEDURES, WELDERS, AND WELDING OPERATORS, NOT DEEMED PREQUALIFIED, IN ACCORDANCE WITH AWS D1.1.
- INSPECT FIELD WELDED CONNECTIONS IN ACCORDANCE WITH THE REQUIREMENTS SPECIFIED AND IN ACCORDANCE WITH AWS D1.1.
- APPROVE FIELD WELDING SEQUENCE.
 - A PROGRAM OF THE APPROVED SEQUENCES SHALL BE SUBMITTED TO THE OWNER BEFORE WELDING BEGINS. NO CHANGE IN APPROVED SEQUENCES MAY BE MADE WITHOUT PERMISSION FROM THE OWNER.

- INSPECT WELDED CONNECTIONS AS FOLLOWS AND IN ACCORDANCE WITH AWS D1.1:
 - INSPECT WELDING EQUIPMENT FOR CAPACITY, MAINTENANCE AND WORKING CONDITIONS. VERIFY SPECIFIED ELECTRODES AND HANDLING AND STORAGE OF ELECTRODES FOR CONFORMANCE TO SPECIFICATIONS.
 - INSPECT PREHEATING AND INTERPASS TEMPERATURES FOR CONFORMANCE WITH AWS D1.1.

- VISUALLY INSPECT ALL WELDS AND VERIFY THAT QUALITY OF WELDS MEETS THE REQUIREMENTS OF AWS D1.1.
- SPOT TEST AT LEAST ONE FILLET WELD OF EACH MEMBER USING MAGNETIC PARTICLE OR DYE PENETRANT.
- VERIFY THAT THE BASE METAL CONFORMS TO THE DRAWINGS.
- REVIEW THE REPORTS BY TESTING LABS.
- CHECK TO SEE THAT WELDS ARE CLEAN AND FREE FROM SLAG.
- INSPECT RUST PROTECTION OF WELDS AS PER SPECIFICATIONS.
- CHECK THAT DEFECTIVE WELDS ARE CLEARLY MARKED AND HAVE BEEN ADEQUATELY REPAIRED.

- SPECIAL INSPECTION OF EXISTING SHAFT-TO-FLANGE WELD CONNECTIONS:
(1) PRIOR TO CONSTRUCTION, TESTING AGENCY SHALL INSPECT CONDITION OF EXISTING SHAFT-TO-BASE-PLATE WELD CONNECTION. ALSO INSPECT EXISTING STIFFENERS IF PRESENT. THE INSPECTOR SHALL USE THE FOLLOWING INSPECTION METHODS, OR COMBINATION OF METHODS, AS REQUIRED TO IDENTIFY ANY CRACKS: VISUAL, MAGNETIC PARTICLE, AND/OR ULTRASONIC. IN ADDITION, OTHER TEST METHODS MAY ALSO BE USED AT THE RECOMMENDATION OF THE TESTING AGENCY AND UPON THE APPROVAL OF THE OWNER AND THE ENGINEER. THE TESTING AGENCY SHALL PROVIDE CAREFUL AND THOROUGH DOCUMENTATION OF THIS INSPECTION TO THE OWNER AND THE ENGINEER. TESTING AGENCY SHALL COORDINATE THESE INSPECTION ACTIVITIES WITH THE OWNER'S REQUIRED PROCESSES AND PROCEDURES. IMPORTANT: THE TESTING AGENCY SHALL IMMEDIATELY REPORT ANY INDICATIONS OF CRACKS, FRACTURES, DISTRESS, AND/OR CORROSION TO THE OWNER AND ENGINEER.
- AFTER CONSTRUCTION, TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD REPAIRS IMPLEMENTED AS REQUIRED BY THE OWNER FROM THE RESULTS OF THE INSPECTION IN THE PREVIOUS NOTE 5.F.(1), ABOVE.
- REFER TO CROWN CASTLE DOCUMENTS ENG-SOW-10033 AND ENG-BUL-10051 FOR SPECIFICATIONS.

- REPORTS:
(1) COMPLETE AND PERIODICALLY SUBMIT DAILY INSPECTION REPORTS TO THE OWNER.

- THE INSPECTION PLAN OUTLINED HEREIN IS INTENDED AS A DESCRIPTION OF GENERAL AND SPECIFIC ITEMS OF CONCERN. IT IS NOT INTENDED TO BE ALL-INCLUSIVE. IT DOES NOT LIMIT THE TESTING AND INSPECTION AGENCY TO THE ITEMS LISTED. ADDITIONAL TESTING, INSPECTION, AND CHECKING MAY BE REQUIRED AND SHOULD BE ANTICIPATED. THE TESTING AGENCY SHALL USE THEIR PROFESSIONAL JUDGMENT AND KNOWLEDGE OF THE JOB SITE CONDITIONS AND THE CONTRACTOR'S PERFORMANCE TO DECIDE WHAT OTHER ITEMS REQUIRE ADDITIONAL ATTENTION. THE TESTING AGENCY'S JUDGMENT MUST PREVAIL ON ITEMS NOT SPECIFICALLY COVERED. ANY DISCREPANCIES AND PROBLEMS SHALL BE BROUGHT IMMEDIATELY TO THE OWNER'S ATTENTION. RESOLUTIONS ARE NOT TO BE MADE WITHOUT THE OWNER'S REVIEW AND SPECIFIC WRITTEN CONSENT. THE OWNER RESERVES THE RIGHT TO DETERMINE WHAT IS AN ACCEPTABLE RESOLUTION OF DISCREPANCIES AND PROBLEMS.
- AFTER EACH INSPECTION, THE TESTING AGENCY WILL PREPARE A WRITTEN ACCEPTANCE OR REJECTION WHICH WILL BE GIVEN TO THE CONTRACTOR AND FILED AS DAILY REPORTS TO THE OWNER. THIS WRITTEN ACTION WILL GIVE THE CONTRACTOR A LIST OF ITEMS TO BE CORRECTED, PRIOR TO CONTINUING CONSTRUCTION, AND/OR LOADING OF STRUCTURAL ITEMS.
- THE TESTING AGENCY DOES NOT RELIEVE THE CONTRACTOR'S CONTRACTUAL OR STATUTORY OBLIGATIONS. THE CONTRACTOR HAS THE SOLE RESPONSIBILITY FOR ANY DEVIATIONS FROM THE OFFICIAL CONTRACT DOCUMENTS. THE TESTING AGENCY WILL NOT REPLACE THE CONTRACTOR'S QUALITY CONTROL PERSONNEL.

FEB 0 8 2013

10-23-2012



AEROSOLUTIONS SHAFT REINFORCING OPTION

BU #876361; SEYMOUR 2/OXFORD TOWN GARAGE
OXFORD, CT

MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

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PROJECT No:
37512-1818

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CHECKED BY:
C.M.M.

APPROVED BY:

DATE:
6-28-2012

ISSUE DATE OF
PERMIT: 6-28-2012

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- D. STRUCTURAL STEEL**
STRUCTURAL STEEL MATERIALS, FABRICATION, DETAILING, AND WORKMANSHIP SHALL CONFORM TO THE LATEST EDITION OF THE FOLLOWING REFERENCE STANDARDS:
BY THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC):
(A) "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL BUILDINGS."
(B) "SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS," AS APPROVED BY THE RESEARCH COUNCIL ON STRUCTURAL CONNECTIONS OF THE ENGINEERING FOUNDATION.
(C) "CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES" (PARAGRAPH 4.2.1 SPECIFICALLY EXCLUDED).
- E. STRUCTURAL WELDING:**
(A) "STRUCTURAL WELDING CODE - STEEL D11."
(B) "SYMBOLS FOR WELDING AND NON-DESTRUCTIVE TESTING"
ANY MATERIAL OR WORKMANSHIP WHICH IS OBSERVED TO BE DEFECTIVE OR INCONSISTENT WITH THE CONTRACT DOCUMENTS SHALL BE CORRECTED, MODIFIED, OR REPLACED AT THE CONTRACTOR'S EXPENSE.
- F. TIGHTEN ALL STRUCTURAL BOLTS, INCLUDING THE AJAX M20 BOLTS WITH SHEAR SLEEVES, ACCORDING TO THE REQUIREMENTS OF THE AISC "TURN OF THE NUT" METHOD. TIGHTEN BOLTS 1/3 TURN PAST THE SNUG TIGHT CONDITION AS DEFINED BY AISC.**
WELDED CONNECTIONS SHALL CONFORM TO THE LATEST REVISED CODE OF THE AMERICAN WELDING SOCIETY, AWS D1.1. ALL WELD ELECTRODES SHALL BE E80XX UNLESS NOTED OTHERWISE ON THE DRAWINGS.
- G. ALL WELDED CONNECTIONS SHALL BE MADE BY WELDERS CERTIFIED BY AWS. CONTRACTOR SHALL SUBMIT WELDERS' CERTIFICATION AND QUALIFICATION DOCUMENTATION TO THE OWNER'S TESTING AGENCY FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.**
STRUCTURAL STEEL PLATES SHALL CONFORM TO ASTM A572 GRADE 65 (FY = 65 KSI MIN.) UNLESS NOTED OTHERWISE ON THE DRAWINGS.
SURFACES OF EXISTING STEEL SHALL BE PREPARED AS REQUIRED FOR FIELD WELDING PER AWS. SEE SECTION J NOTES REGARDING TOUCH-UP OF GALVANIZED SURFACES DAMAGED DURING TRANSPORTATION OR ERECTION AND ASSEMBLY AS WELL AS FIELD WELDING.
UNLESS OTHERWISE NOTED, ALL STEEL MEMBERS SHALL BE HOT-DIP GALVANIZED, AFTER FABRICATION, IN ACCORDANCE WITH ASTM A123. SEE SECTION J FOR FURTHER NOTES AND FOR EXCEPTIONS (IF ANY).
ALL WELDS SHALL BE VISUALLY INSPECTED BY THE OWNER'S APPROVED TESTING AGENCY. OTHER TESTS MAY ALSO BE PERFORMED ON THE WELDS BY THE TESTING AGENCY IN ORDER FOR THEM TO PERFORM THEIR DUTIES FOR THIS PROJECT. THE CONTRACTOR SHALL COOPERATE WITH THE TESTING AGENCY IN THEIR TESTING EFFORTS.
NO WELDING SHALL BE DONE TO THE EXISTING STRUCTURE WITHOUT THE PRIOR APPROVAL AND SUPERVISION OF THE TESTING AGENCY.
- H. FIELD CUTTING OF STEEL**
(A) PRIOR TO ANY FIELD CUTTING, THE CONTRACTOR SHALL MARK THE CUT OUTLINES ON THE STEEL AND THE INSPECTION/TESTING AGENCY SHALL VERIFY PROPOSED LAYOUT, LOCATION, AND DIMENSIONS.
(B) ANY REQUIRED CUTS IN THE STEEL SHALL BE CAREFULLY CUT BY MECHANICAL METHODS SUCH AS DRILLING, SAW CUTTING, AND GRINDING. THE CONTRACTOR IS RESPONSIBLE TO PREVENT ANY DAMAGE TO THE COAX CABLES, AND/OR OTHER EQUIPMENT AND/OR THE STRUCTURE, DURING THE CUTTING WORK. ANY DAMAGE TO THE COAX CABLES, AND/OR OTHER EQUIPMENT AND/OR THE STRUCTURE, RESULTING FROM THE CONTRACTOR'S ACTIVITIES SHALL BE REPAIRED AT THE CONTRACTOR'S EXPENSE. THE INSPECTION/TESTING AGENCY SHALL CLOSELY AND CONTINUOUSLY MONITOR THIS ACTIVITY.
(C) ALL REQUIRED CUTS SHALL BE CUT WITHIN THE DIMENSIONS SHOWN ON THE DRAWINGS. NO CUTS SHALL EXTEND BEYOND THE OUTLINE OF THE DIMENSIONS SHOWN ON THE DRAWINGS. ALL CUT EDGES SHALL BE GROUND SMOOTH AND DE-BURRED. CUT EDGES THAT ARE TO BE FIELD WELDED SHALL BE PREPARED FOR FIELD WELDING PER AWS D1.1 AND AS SHOWN ON THE DRAWINGS. IT MAY BE NECESSARY TO DRILL STARTER HOLES AS REQUIRED TO MAKE THE CUTS. THE INSPECTION/TESTING AGENCY SHALL CLOSELY AND CONTINUOUSLY MONITOR THIS ACTIVITY.
- I. BASE PLATE GROUT**
NEW GROUT FOR THE POLE BASE SHALL BE NON-SHRINK, NON-METALLIC, GROUT (EUCO NS GROUT BY EUCLID, OR APPROVED EQUAL) WITH A 7500 PSI MINIMUM COMPRESSIVE STRENGTH. PVC DRAINAGE PIPES SHALL BE PROVIDED FROM INSIDE THE POLE SHAFT OUT THROUGH THE GROUT SPACE UNDER THE BASE PLATE IN ORDER TO ALLOW MOISTURE TO ADEQUATELY DRAIN FROM THE INTERIOR OF THE POLE SHAFT. CONTRACTOR SHALL SUBMIT PROPOSED GROUT SPECIFICATION INFORMATION TO THE OWNER FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION.
CONTRACTOR SHALL FOLLOW GROUT MANUFACTURER'S SPECIFICATIONS FOR COLD WEATHER GROUTING PROCEDURES (IF NECESSARY) AND THE TESTING AGENCY SHALL PREPARE GROUT SAMPLE SPECIMENS FOR COMPRESSIVE STRENGTH TESTING AND VERIFICATION.
GROUT SHALL BE INSTALLED TIGHT UNDER BASE PLATE WITH NO VOIDS REMAINING BETWEEN TOP OF EXISTING CONCRETE AND UNDERSIDE OF EXISTING BASE PLATE (EXCEPT FOR DRAIN PIPES). GROUT COMPLETELY SOLID (EXCEPT FOR DRAIN PIPES) UNDER ENTIRE SURFACE OF BASE PLATE FROM OUTSIDE EDGE TO INSIDE EDGE.
- J. FOUNDATION WORK**
THE CONTRACTOR SHALL PROTECT THE EXISTING MONOPOLE STRUCTURE, AS WELL AS ANY OTHER NEARBY EXISTING FOUNDATIONS FOR OTHER STRUCTURES OR EQUIPMENT, FROM LOSS OF SOIL AROUND AND/OR BENEATH FOOTINGS DURING ANY REQUIRED EXCAVATION. THE CONTRACTOR SHALL BRACE THE SIDES OF THE OPEN EXCAVATION AS REQUIRED.
THE EFFECT OF ADDITIONAL EXCAVATION (WHERE REQUIRED) FOR THE NEW MAT FOOTING (WHERE REQUIRED) OR OTHER FOUNDATION AUGMENTATION AND REINFORCING (WHERE REQUIRED) MAY HAVE IMPACT ON EXISTING EQUIPMENT AND/OR OTHER EXISTING STRUCTURES NEAR THE EXCAVATION. (ENGINEER-OF-RECORD) HAS NOT BEEN PROVIDED WITH ANY SPECIFIC INFORMATION OR DETAILS REGARDING EXISTING EQUIPMENT OR OTHER EXISTING STRUCTURES ON THE SITE. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO DETERMINE THE IMPACT OR EFFECT THAT ANY REQUIRED EXCAVATION WORK HAS ON ANY EXISTING NEARBY EQUIPMENT AND/OR STRUCTURES. CONTRACTOR SHALL COORDINATE THIS SITE-SPECIFIC INFORMATION WITH THE OWNER AND TESTING AGENCY PRIOR TO CONSTRUCTION AND FOUNDATION WORK. THE CONTRACTOR SHALL ADEQUATELY BRACE, SHORE, AND/OR RELOCATE (AFTER OBTAINING THE PRIOR WRITTEN PERMISSION OF THE OWNER), AS NECESSARY, THE INTERFERING EXISTING NEARBY EQUIPMENT AND/OR STRUCTURES.

CAST-IN-PLACE CONCRETE - (NOT REQUIRED)

EPOXY GROUTED REINFORCING ANCHOR RODS
UNLESS OTHERWISE NOTED, REINFORCING ANCHOR RODS SHALL BE 150 KSI ALL-THREAD BAR CONFORMING TO ASTM A722. RECOMMENDED MANUFACTURERS/SUPPLIERS OF 150 KSI ALL-THREAD BAR ARE WILLIAMS FORM ENGINEERING CORPORATION AND D'VIDAG SYSTEMS INTERNATIONAL. ALL REINFORCING ANCHOR RODS SHALL BE HOT DIP GALVANIZED PER ASTM A153. ALTERNATIVELY, ALL REINFORCING ANCHOR RODS MAY BE EPOXY COATED PER ASTM A775.
THE CORE-DRILLED HOLES IN THE CONCRETE FOR THE ANCHOR RODS SHALL BE CLEAN AND DRY, AND OTHERWISE PROPERLY PREPARED ACCORDING TO THE ANCHOR ROD AND EPOXY MANUFACTURERS' INSTRUCTIONS, PRIOR TO PLACEMENT OF ANCHOR RODS AND EPOXY. CONTRACTOR SHALL FOLLOW ALL ANCHOR ROD AND EPOXY MANUFACTURER RECOMMENDATIONS REGARDING HANDLING OF RODS, EPOXY, ACCEPTABLE AMBIENT TEMPERATURE RANGE DURING INSTALLATION AND POST-INSTALLATION CURING, THE EFFECT OF TEMPERATURE ON EPOXY CURING TIME, PREPARATION OF HOLE, ETC.
ULTRABOND 1, HILTI HIT RE-500 OR ANCHORTITE EPOXY SHALL BE USED TO ANCHOR THE 150 KSI ALL-THREAD BAR IN THE DRILL HOLES. IF CONTRACTOR WISHES TO USE A DIFFERENT EPOXY, A REQUEST INCLUDING THE EPOXY TECHNICAL DATA SHEET(S) SHALL BE SUBMITTED TO PAUL J FORD AND COMPANY FOR REVIEW PRIOR TO CONSTRUCTION. AS NOTED ABOVE, FOLLOW ALL EPOXY MANUFACTURER RECOMMENDATIONS REGARDING HANDLING OF EPOXY, ACCEPTABLE AMBIENT TEMPERATURE RANGE DURING INSTALLATION AND POST-INSTALLATION CURING, THE EFFECT OF TEMPERATURE ON EPOXY CURING TIME, PREPARATION OF HOLE, ETC.
ONCE THE REINFORCING ANCHOR RODS HAVE BEEN INSTALLED AND ALL EPOXY AND GROUT HAVE CURED (IF BASE PLATE AND/OR BEARING PLATES HAVE BEEN GROUTED PRIOR TO TESTING), ALL REINFORCING ANCHOR RODS SHALL BE LOAD TESTED PER CROWN CASTLE ENGINEERING DOCUMENT #ENG-PRC-10119. REFER TO THE NEW ANCHOR & BRACKET DETAIL ON FOLLOWING DRAWING SHEETS FOR SPECIFIED ANCHOR ROD PROOF LOAD.
ONCE THE REINFORCING ANCHOR RODS HAVE BEEN SUCCESSFULLY LOAD TESTED AND APPROVED AND BASE PLATE/BEARING PLATE GROUT HAS CURED (IF BASE PLATE AND/OR BEARING PLATES HAVE BEEN GROUTED AFTER TESTING), CONTRACTOR SHALL TIGHTEN ALL HEAVY HEX ANCHOR NUTS TO SNUG TIGHT PLUS 1/4 TURN OF NUT.

TOUCH UP OF GALVANIZING

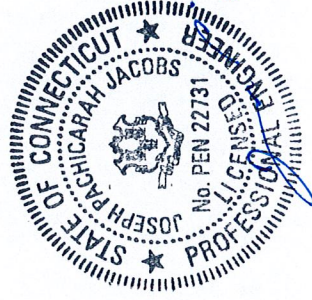
THE CONTRACTOR SHALL TOUCH UP ANY AND/OR ALL AREAS OF GALVANIZING ON THE EXISTING STRUCTURE OR NEW COMPONENTS THAT ARE DAMAGED OR ABRADED DURING CONSTRUCTION. GALVANIZED SURFACES DAMAGED DURING TRANSPORTATION OR ERECTION AND ASSEMBLY AS WELL AS ANY AND ALL ABRASIONS, CUTS, FIELD DRILLING, AND ALL FIELD WELDING SHALL BE TOUCHED UP WITH TWO (2) COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND. FILM THICKNESS PER COAT SHALL BE: WET 3.0 MILS; DRY 1.5 MILS. APPLY PER ZRC (MANUFACTURER) RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-800-831-3275 FOR PRODUCT INFORMATION.
CONTRACTOR SHALL CLEAN AND PREPARE ALL FIELD WELDS ON GALVANIZED AND PRIME PAINTED SURFACES FOR TOUCH-UP COATING IN ACCORDANCE WITH AWS D1.1. THE OWNER'S TESTING AGENCY SHALL VERIFY THE PREPARED SURFACE PRIOR TO APPLICATION OF THE TOUCH-UP COATING.
THE OWNER'S TESTING AGENCY SHALL TEST AND VERIFY THE COATING THICKNESS AFTER THE CONTRACTOR HAS APPLIED THE ZRC COLD GALVANIZING COMPOUND AND IT HAS SUFFICIENTLY DRIED. AREAS FOUND TO BE INADEQUATELY COATED, SHALL BE RE-COATED BY THE CONTRACTOR AND RE-TESTED BY THE TESTING AGENCY.

HOT DIP GALVANIZING
ALL STRUCTURAL STEEL MEMBERS AND ALL STEEL ACCESSORIES, BOLTS, WASHERS, ETC., PER ASTM A123 OR PER ASTM A153, AS APPROPRIATE.
PROPERLY PREPARE STEEL ITEMS FOR GALVANIZING.
DRILL OR PUNCH WEEP AND/OR DRAINAGE HOLES AS REQUIRED.
ALL GALVANIZING SHALL BE DONE AFTER FABRICATION IS COMPLETED AND PRIOR TO FIELD INSTALLATION.

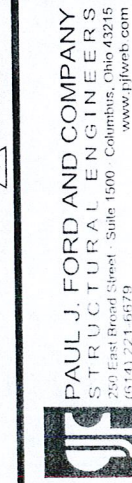
PERPETUAL INSPECTION AND MAINTENANCE BY THE OWNER

AFTER THE CONTRACTOR HAS SUCCESSFULLY COMPLETED THE INSTALLATION OF THE MONOPOLE REINFORCING SYSTEM AND THE WORK HAS BEEN ACCEPTED BY THE OWNER, THE OWNER WILL BE RESPONSIBLE FOR THE LONG TERM AND PERPETUAL INSPECTION AND MAINTENANCE OF THE POLE AND REINFORCING SYSTEM.
THE MONOPOLE REINFORCING SYSTEM INDICATED IN THESE DOCUMENTS USES REINFORCING COMPONENTS THAT INVOLVE FIELD WELDING STEEL MEMBERS TO THE EXISTING GALVANIZED STEEL POLE STRUCTURE. THESE FIELD WELDED CONNECTIONS ARE SUBJECT TO CORROSION DAMAGE AND DETERIORATION IF THEY ARE NOT PROPERLY MAINTAINED AND COVERED WITH CORROSION PREVENTIVE COATING SUCH AS THE ZRC GALVANIZING COMPOUND SPECIFIED PREVIOUSLY. THE STRUCTURAL LOAD CARRYING CAPACITY OF THE REINFORCED POLE SYSTEM IS DEPENDENT UPON THE INSTALLED SIZE AND QUALITY, MAINTAINED SOUND CONDITION AND STRENGTH OF THESE FIELD WELDED CONNECTIONS. ANY CORROSION OF, DAMAGE TO, FATIGUE, FRACTURE, AND/OR DETERIORATION OF THESE WELDS AND/OR THE CONNECTED COMPONENTS WILL RESULT IN THE LOSS OF STRUCTURAL LOAD CARRYING CAPACITY AND MAY LEAD TO FAILURE OF THE STRUCTURAL SYSTEM. THEREFORE, IT IS IMPERATIVE THAT THE OWNER REGULARLY INSPECTS, MAINTAINS, AND REPAIRS AS NECESSARY, ALL OF THESE WELDS, CONNECTIONS, AND COMPONENTS FOR THE LIFE OF THE STRUCTURE.
THE OWNER SHALL REFER TO TIA/EIA-222-F-1996, SECTION 14 AND ANNEX E FOR RECOMMENDATIONS FOR MAINTENANCE AND INSPECTION. THE FREQUENCY OF THE INSPECTION AND MAINTENANCE INTERVALS IS TO BE DETERMINED BY THE OWNER BASED UPON ACTUAL SITE AND ENVIRONMENTAL CONDITIONS. PAUL J. FORD & COMPANY RECOMMENDS THAT A COMPLETE AND THOROUGH INSPECTION OF THE ENTIRE REINFORCED MONOPOLE STRUCTURAL SYSTEM BE PERFORMED YEARLY AND/OR AS FREQUENTLY AS CONDITIONS WARRANT. ACCORDING TO TIA/EIA-222-F-1996 SECTION 14.1, NOTE 1, "IT IS RECOMMENDED THAT THE STRUCTURE BE INSPECTED AFTER SEVERE WIND AND/OR ICE STORMS OR OTHER EXTREME LOADING CONDITIONS".

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BU #876361; SEYMOUR 2/OXFORD TOWN GARAGE
OXFORD, CT
MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

ISSUE DATE OF
PERMIT: 6-28-2012

S-2A

AJAX BOLT NOTE SHEET: REV. 1.2, 01-23-2012

- NOTES:
- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
 - ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009.
 - ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL BELOW FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
 - ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTI'S) AND HARDENED WASHERS. DTI'S SHALL BE THE SQUIRTER® STYLE, MADE TO ASTM F959 LATEST REVISION; AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.

NOTES FOR AJAX M20 'ONE-SIDE' BOLTS WITH DIRECT TENSION INDICATORS (DTI'S):

DTI'S REQUIRED: DTI'S SHALL BE "SELF-INDICATING" SQUIRTER® STYLE DTI'S MADE WITH SILICONE EMBEDDED IN THEM, INSPECTED BY MEANS OF THE VISUAL EJECTION OF SILICONE AS THE DTI PROTRUSIONS COMPRESS. SQUIRTER® DTI'S SHALL BE CALIBRATED PER MANUFACTURER'S INSTRUCTIONS PRIOR TO USE.

THE DIRECT TENSION INDICATOR (DTI) WASHERS SHALL BE THE "SQUIRTER® STYLE" AS MANUFACTURED BY:

APPLIED BOLTING TECHNOLOGY PRODUCTS, INC.
1413 ROCKINGHAM ROAD BELLOW'S FALLS, VERMONT, USA 05101
PHONE 1-800-552-1999
WEBSITE: WWW.APPLIEDBOLTING.COM

DISTRIBUTORS OF SQUIRTER® DTI'S:
[HTTP://WWW.APPLIEDBOLTING.COM/APPLIED-BOLTING-DISTRIBUTORS.HTML](http://WWW.APPLIEDBOLTING.COM/APPLIED-BOLTING-DISTRIBUTORS.HTML)

DTI: USE DIRECT TENSION INDICATOR (DTI) WASHERS COMPATIBLE WITH 3/4" NOMINAL A325 BOLTS FOR THE AJAX M20 BOLTS. DTI'S SHALL NOT BE HOT-DIP GALVANIZED. DTI'S SHALL BE MECHANICALLY GALVANIZED (MG) BY THE COLD MECHANICAL PROCESS ONLY AS PROVIDED BY THE DTI MANUFACTURER.

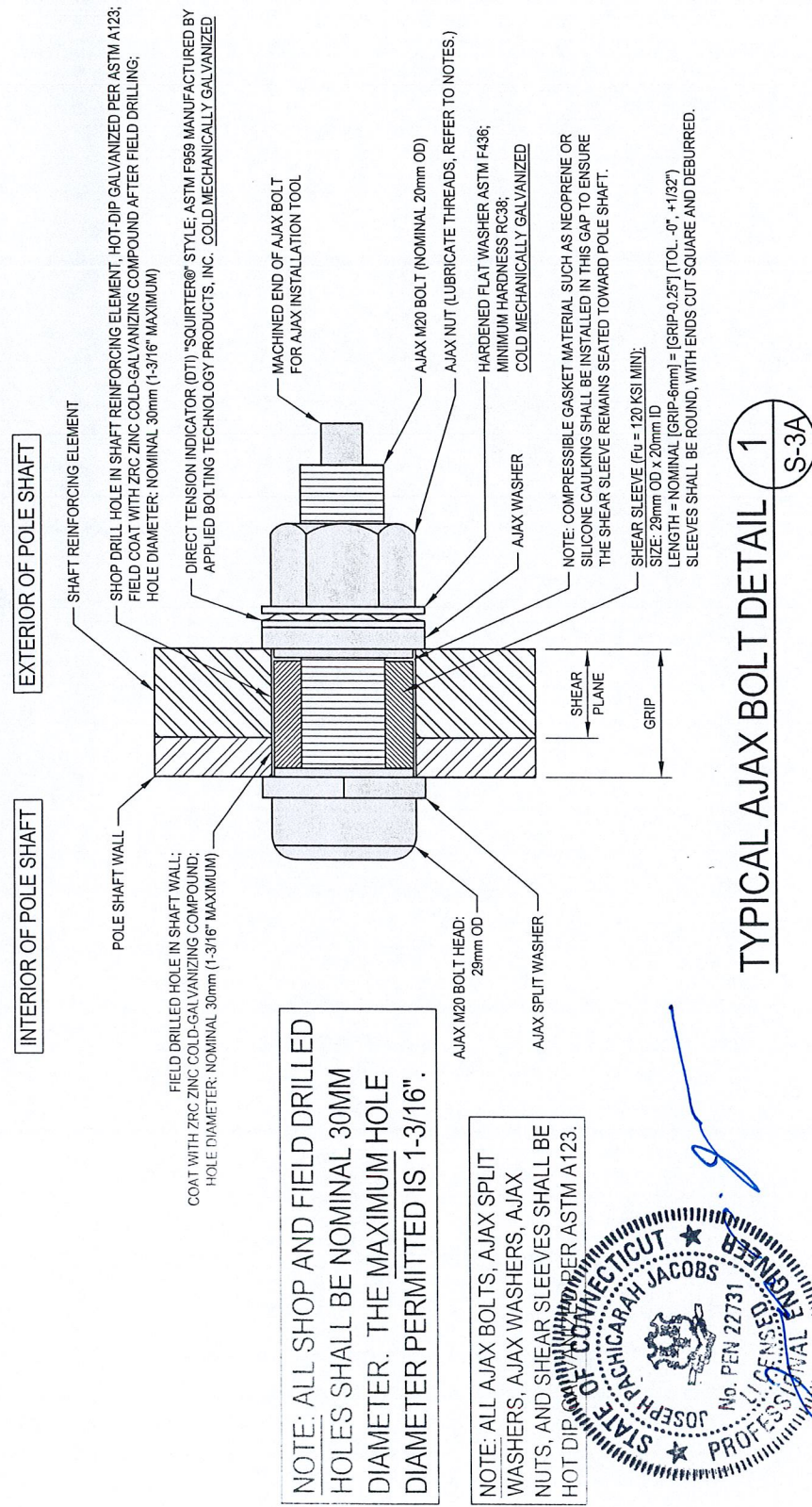
HARDENED WASHERS REQUIRED: USE A HARDENED WASHER FOR A 3/4" NOMINAL BOLT BETWEEN THE TOP OF THE DIRECT TENSION INDICATOR (DTI) WASHER AND THE NUT OF THE AJAX M20 BOLTS. HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A MINIMUM HARDNESS OF RC 38 OR HIGHER. THE HARDENED WASHERS SHALL BE MECHANICALLY GALVANIZED BY THE COLD MECHANICAL PROCESS. ALTERNATIVELY, CORRECTLY MADE HOT DIP GALVANIZED HARDENED FLAT WASHERS HAVING A MINIMUM HARDNESS OF RC 38 CAN BE USED; CONTRACTOR SHALL PROVIDE DOCUMENTATION OF WASHER SPECIFICATION AND HARDNESS.

NUT LUBRICATION REQUIRED: PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SHALL FOLLOW DTI MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING.

NOTE: COMPLETELY COMPRESSED DTI'S SHOWING NO VISIBLE REMAINING GAP ARE ACCEPTABLE. DTI WASHERS SHALL BE PLACED DIRECTLY AGAINST THE OUTER AJAX WASHER WITH THE DTI BUMPS FACING AWAY FROM THE AJAX WASHER. PLACE A HARDENED WASHER BETWEEN THE DTI AND THE AJAX NUT. THE DTI BUMPS SHALL BEAR AGAINST THE UNDERSIDE OF A HARDENED FLAT WASHER, NEVER DIRECTLY AGAINST THE NUT.

CONTRACTOR SHALL FOLLOW DTI MANUFACTURER'S INSTRUCTIONS FOR INSTALLATION, LUBRICATION, TIGHTENING AND INSPECTION.

INSPECTION REQUIRED: ALL AJAX BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC 'SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS', DEC. 31, 2009, BY A QUALIFIED BOLT INSPECTOR. DURING INSTALLATION, THE BOLT INSPECTOR SHALL VERIFY AND DOCUMENT: THE SHOP-DRILLED AND FIELD-DRILLED HOLE SIZES; THE INSTALLATION OF THE AJAX BOLT ASSEMBLY, INCLUDING THE SHEAR SLEEVE PLACEMENT AND NUT LUBRICATION; AND THE CONTRACTOR'S TENSIONING PROCEDURE. IN ADDITION, ALL AJAX BOLTS AND DTI'S SHALL BE VISUALLY INSPECTED ACCORDING TO THE DTI MANUFACTURER'S INSTRUCTIONS. THE BOLT INSPECTOR SHALL PROVIDE COMPLETE PHOTO DOCUMENTATION OF ALL BOLTS AFTER TIGHTENING CLEARLY SHOWING THE CONDITION OF THE DTI'S.



TYPICAL AJAX BOLT DETAIL 1
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10-23-2012

AEROSOLUTIONS SHAFT REINFORCING OPTION

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BU #876361; SEYMOUR 2/OXFORD TOWN GARAGE
OXFORD, CT
MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

PROJECT No:
37512-1818
DRAWN BY:
B.M.S.
CHECKED BY:
C.M.M.
APPROVED BY:
DATE:
6-28-2012

ISSUE DATE OF
PERMIT: 6-28-2012

S-3A

NOTE: NO DETAILED INFORMATION REGARDING INTERFERENCES WAS PROVIDED. THEREFORE, CONTRACTOR SHALL FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS BEFORE PROCEEDING WITH THE WORK. REPORT ANY AND ALL DISCREPANCIES TO PAUL J. FORD AND COMPANY AND CROWN CASTLE FIELD PERSONNEL IMMEDIATELY.

THIS POLE REINFORCEMENT DRAWING IS FOR THE POLE DESIGN AND ANTENNA LOADING DOCUMENTED IN THE PJF CO-LOCATION ANALYSIS FOR THIS SITE (PJF#37512-1818), DATED 6-28-2012.

POLE SPECIFICATIONS	
POLE SHAPE TYPE:	18-SHRED POLYGRH
TAPER:	0.2143329 IN/FT
SHAFT STEEL:	ASTM A572 GRADE 65
BASE PL. STEEL:	ASTM A633 GR. E (60 KSI)
ANCHOR BOLDS:	2 1/4" Ø #15 ASTM A615 GRADE 75

SHAFT SECTION DATA					
SHAFT SECTION	SECTION LENGTH (FT)	PLATE THICKNESS (IN)	LAP SPLICE (IN)	DIAMETER ACROSS FLATS (IN)	
				@ TOP	@ BOTTOM
1	26.58	0.1875	38.00	15.000	20.660
2	40.63	0.2500	49.00	19.611	28.280
3	47.63	0.3125	62.00	26.909	37.070
4	47.59	0.3750		35.343	45.500

NOTE: DIMENSIONS SHOWN DO NOT INCLUDE GALVANIZING TOLERANCES

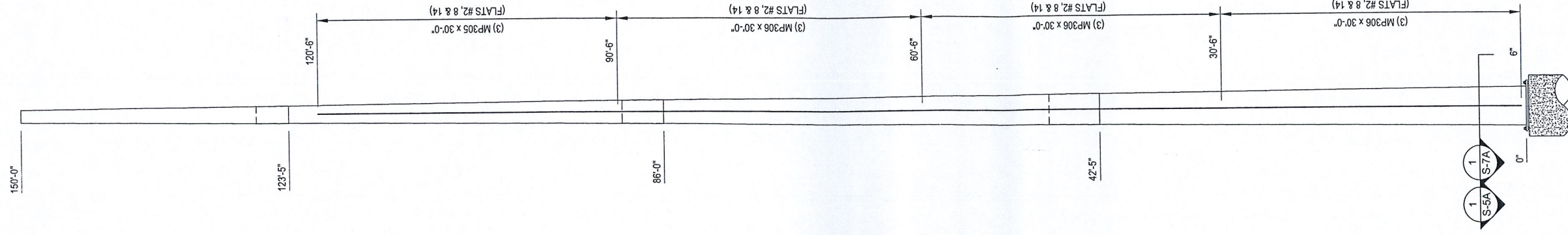
CONTRACTOR SHALL PROVIDE ASTM A36 SHIM PLATES BELOW SLIP JOINTS. THE SHIM PLATES SHALL BE PLACED BETWEEN THE NEW SHAFT REINFORCEMENT AND THE EXISTING POLE SHAFT FROM THE SLIP JOINT TO THE NEW SHAFT REINFORCEMENT SPLICE PLATE LOCATION AND AN EXTRA LONG "SPLICE SHIM" SHALL BE PLACED BETWEEN THE NEW UPPER AND LOWER SHAFT REINFORCEMENT PLATES AT THE SHAFT REINFORCEMENT SPLICE PLATE LOCATION.

NOTES:

- ALL STRUCTURAL BOLTS SHALL BE INSTALLED AND TIGHTENED TO THE PRETENSIONED CONDITION ACCORDING TO THE REQUIREMENTS OF THE AISC "SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS", DEC. 31, 2009.
- ALL STRUCTURAL BOLTS SHALL BE INSPECTED ACCORDING TO THE REQUIREMENTS OF THE AISC "SPECIFICATION FOR STRUCTURAL JOINTS USING HIGH-STRENGTH BOLTS", DEC. 31, 2009.
- ALL AJAX M20 BOLTS WITH SHEAR SLEEVES SHALL BE PRETENSIONED AND TIGHTENED UNTIL THE DIRECT TENSION INDICATOR (DTI) WASHERS SHOW THAT THE PROPER BOLT TENSION HAS BEEN REACHED. SEE NOTES AND DETAIL ON SHEET S-3 FOR THE USE OF DIRECT TENSION INDICATOR (DTI) WASHERS WITH THE AJAX M20 BOLTS.
- DTIS REQUIRED: * ALL AJAX BOLTS SHALL BE INSTALLED USING DIRECT TENSION INDICATORS (DTIS) AND HARDENED WASHERS. DTIS SHALL BE THE SOURITE® STYLE, MADE TO ASTM F959 LATEST REVISION, AND HARDENED WASHERS SHALL CONFORM TO ASTM F436 AND HAVE A HARDNESS OF RC 38 OR HIGHER.
- NUT LUBRICATION REQUIRED: * PROPERLY LUBRICATE THE THREADS OF THE NUT OF THE AJAX BOLT SO THAT IT CAN BE PROPERLY TIGHTENED WITHOUT GALLING AND/OR LOCKING UP ON THE BOLT THREADS. CONTRACTOR SHALL FOLLOW OEM MANUFACTURER INSTRUCTIONS FOR PROPER LUBRICATION AND TIGHTENING. REFER TO SHEET S-3.
- AJAX BOLT HOLE SIZE: ALL SHOP- AND FIELD-DRILLED HOLES SHALL BE NOMINAL 30MM DIAMETER. THE MAXIMUM HOLE DIAMETER PERMITTED IS 1.3/16". REFER TO SHEET S-3.

* AS OF 5/30/2012, UNTIL FURTHER NOTICE, CROWN CASTLE WILL ACCEPT AJAX BOLTS TIGHTENED USING AISC "TURN-OF-THE-NUT" METHODOLOGY. INSTALLERS SHALL FOLLOW CROWN GUIDELINES FOR AISC "TURN-OF-THE-NUT" METHOD AND ALSO PROVIDE COMPLETE INSPECTION DOCUMENTATION IN THE PMI.

NDE OF THE CIRCUMFERENTIAL WELD OF THE BASE PLATE TO SHAFT CONNECTION IS REQUIRED. PLEASE SEE ENG-SOW-1033 - TOWER BASE PLATE NDE AND ENG-RUL-10051 - NDE REQUIREMENTS FOR MONOPOLE BASE PLATE TO PREVENT CONNECTION FAILURE. NOTIFY THE EOR AND CROWN ENGINEERING IMMEDIATELY IF ANY CRACKS ARE SUSPECTED OR HAVE BEEN IDENTIFIED. THE NDE SHALL INCLUDE ALL EXISTING REINFORCEMENTS THAT HAVE BEEN WELDED TO THE BASE PLATE. FULL PENETRATION WELDING TO THE BASE PLATE REQUIRED AS PART OF THIS ACTIVE REINFORCEMENT DESIGN SHALL BE INCLUDED IN THE NDE SCOPE OF WORK.



POLE ELEVATION 1
S-4A

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10-23-2012

AEROSOLUTIONS SHAFT REINFORCING OPTION

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- SPECIAL INSPECTION OF EXISTING SHAFT TO FLANGE WELD CONNECTIONS:
- PRIOR TO CONSTRUCTION, CONTRACTOR'S INSPECTION AGENCY SHALL INSPECT CONDITION OF EXISTING SHAFT TO BASE PLATE WELD CONNECTION. ALSO INSPECT EXISTING STIFFENERS IF PRESENT. THE CONTRACTOR'S INSPECTION AGENCY SHALL USE THE FOLLOWING INSPECTION METHODS, OR COMBINATION OF METHODS, AS REQUIRED TO DETERMINE ANY CRACKS, VISUAL, MAGNETIC PARTICLE, AND/OR ULTRASONIC. IN ADDITION, OTHER TEST METHODS MAY ALSO BE USED AT THE RECOMMENDATION OF THE TESTING AGENCY AND UPON THE APPROVAL OF THE OWNER AND THE ENGINEER. CONTRACTOR SHALL PROVIDE CAREFUL AND THOROUGH DOCUMENTATION OF THIS INSPECTION TO THE OWNER AND THE ENGINEER BEFORE PROCEEDING WITH WORK. CONTRACTOR SHALL COORDINATE THESE INSPECTION ACTIVITIES WITH THE OWNER'S REQUIRED PROCESSES AND PROCEDURES. IMPORTANT: THE TESTING AGENCY SHALL IMMEDIATELY REPORT ANY INDICATIONS OF CRACKS, FRACTURES, DISTRESS, AND/OR CORROSION TO THE OWNER AND ENGINEER.
 - AFTER CONSTRUCTION, TESTING AGENCY SHALL INSPECT ANY AND ALL FIELD WELDS AND FIELD REPAIRS IMPLEMENTED AS REQUIRED BY THE OWNER FROM THE RESULTS OF THE INSPECTION IN THE PREVIOUS NOTE (1) ABOVE.

PROVIDE NON-SHRINK GROUT (NS GROUT BY EUCLID OR APPROVED, EQUAL: 7500 PSI MIN.) BELOW EXIST. BASE PLATE AND NEW BEARING PLATES. PRIOR TO GROUTING, INSTALL FOUR 1-INCH DIAMETER PVC DRAIN PIPES AT APPROXIMATELY NINETY (90) DEGREES APART THROUGH GROUT SPACE. GROUT SHALL BE INSTALLED TIGHT UNDER BASE PLATE WITH NO VOIDS REMAINING BETWEEN TOP OF EXISTING CONCRETE AND UNDERSIDE OF EXISTING BASE PLATE (EXCEPT FOR DRAIN PIPES). GROUT COMPLETELY SOLID UNDER ENTIRE SURFACE OF BASE PLATE FROM OUTSIDE EDGE TO INSIDE EDGE.

CONTRACTOR TO PROVIDE PVC PIPE (TOTAL OF 4) TO ALLOW FOR FREE DRAINAGE FROM INTERIOR OF POLE THROUGH GROUT SPACE.

** REMOVE (1) EXISTING STIFFENER (3 TOTAL LOCATIONS) TO ALLOW FOR INSTALLATION OF NEW SHAFT REINFORCING AND NEW TRANSITION STIFFENERS

** NEW MP3 SHAFT REINFORCING (TYP.)

EXISTING PORT (TYP.)

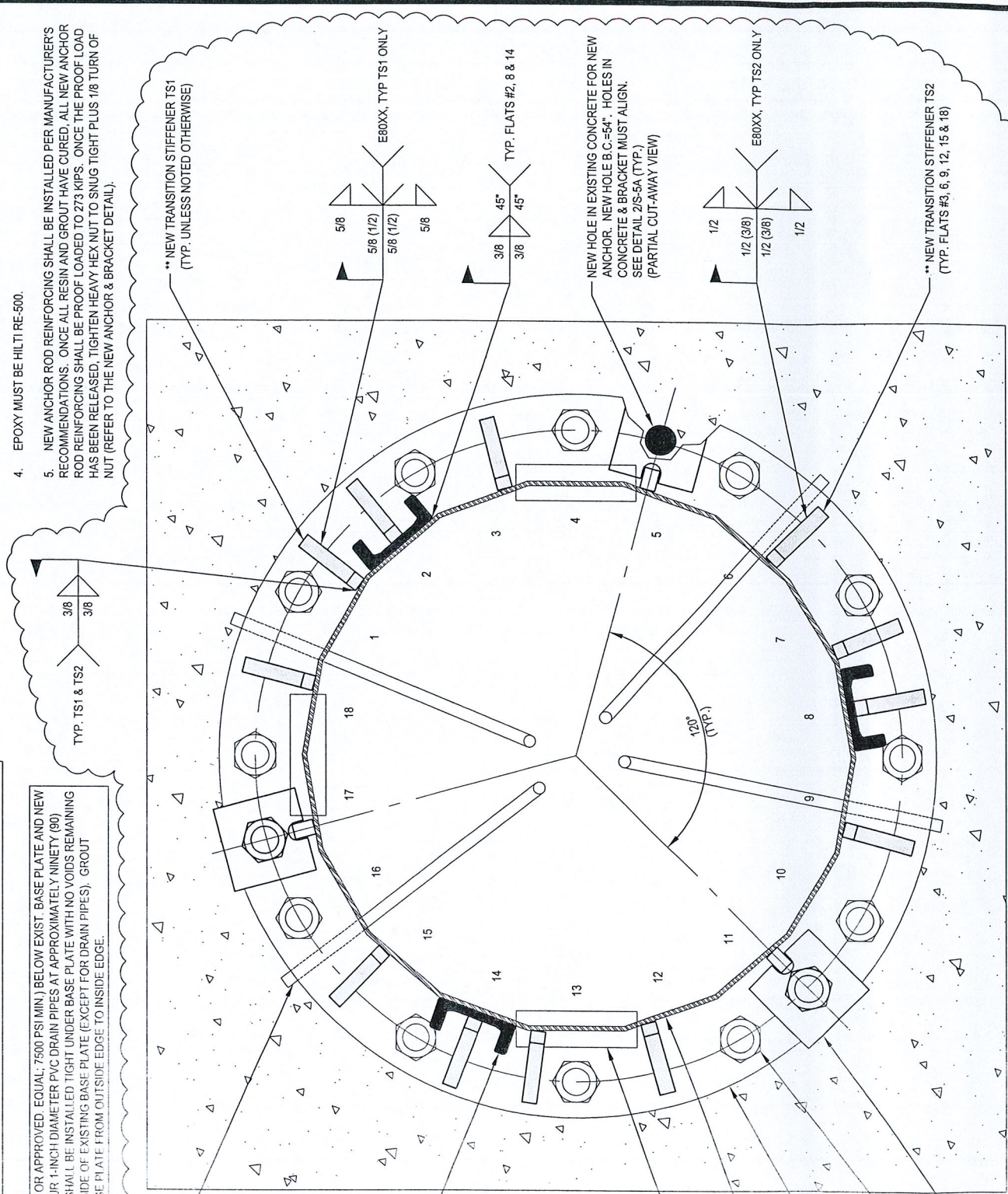
EXISTING POLE SHAFT

EXISTING 60% GR-60 BASE PLATE

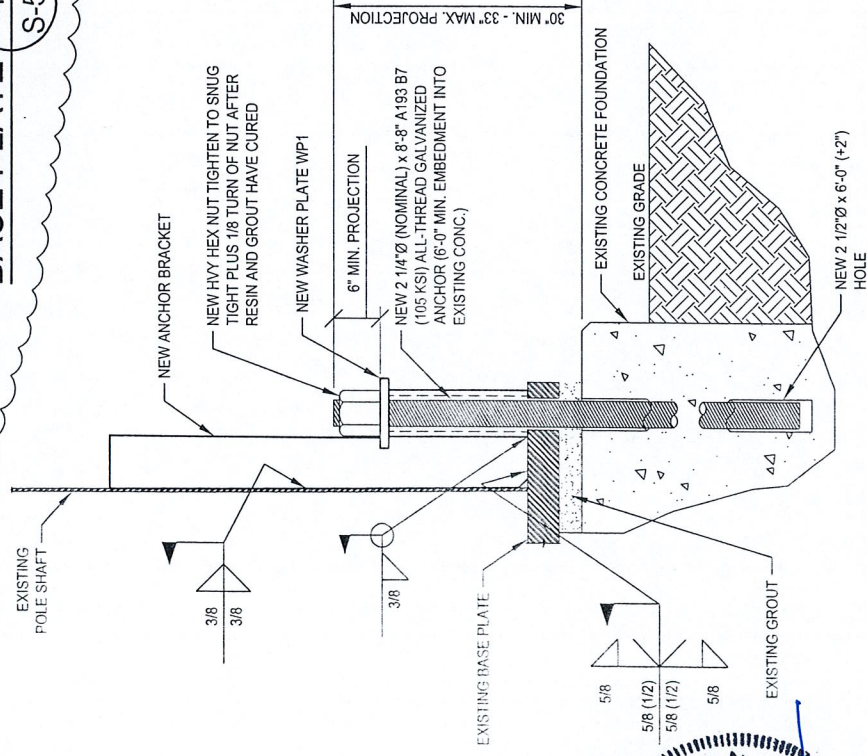
EXISTING 2 1/4" ANCHOR RODS ON A 54" B.C. (TYP. 12 LOCATIONS)
REMOVE EXISTING STIFFENER AND REPLACE WITH NEW FIELD WELDED STEEL BRACKET. SEE AB1 & WP1. (TYP. AT ALL (3) NEW ANCHOR HOLE LOCATIONS)

GENERAL NOTES:

- ALAX BOLTS ARE TO BE 20 mm Ø WITH CORRESPONDING 20 mm Ø SHEAR SLEEVE WITH MATCHING STEEL GRADE. DRILLED HOLE DIAMETERS IN REINFORCING STEEL AND EXISTING SHAFT SHALL BE 1/32" Ø MAX.
- ALL STEEL SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123. ALTERNATIVELY, ALL NEW STIFFENER PLATE STEEL REINFORCING MAY BE COLD GALVANIZED AS FOLLOWS: APPLY A MINIMUM OF TWO COATS OF ZRC-BRAND ZINC-RICH COLD GALVANIZING COMPOUND. FILM THICKNESS PER COAT SHALL BE: WET 3.0 MILS, DRY 1.5 MILS. APPLY PER ZRC (MANUFACTURER) RECOMMENDED PROCEDURES. CONTACT ZRC AT 1-800-831-3275 FOR PRODUCT INFORMATION.
- ALL SHAFT REINFORCING IS A572 GR 65.
- EPOXY MUST BE HILTI RE-500.
- NEW ANCHOR ROD REINFORCING SHALL BE INSTALLED PER MANUFACTURER'S RECOMMENDATIONS. ONCE ALL RESIN AND GROUT HAVE CURED, ALL NEW ANCHOR ROD REINFORCING SHALL BE PROOF LOADED TO 273 KIPS. ONCE THE PROOF LOAD HAS BEEN RELEASED, TIGHTEN HEAVY HEX NUT TO SNUG TIGHT PLUS 1/8 TURN OF NUT (REFER TO THE NEW ANCHOR & BRACKET DETAIL).



BASE PLATE 1 S-5A



NEW ANCHOR & BRACKET DETAIL 2 S-5A



FEB 08 2013

10-23-2012; ADDED NEW BASE STIFFENERS

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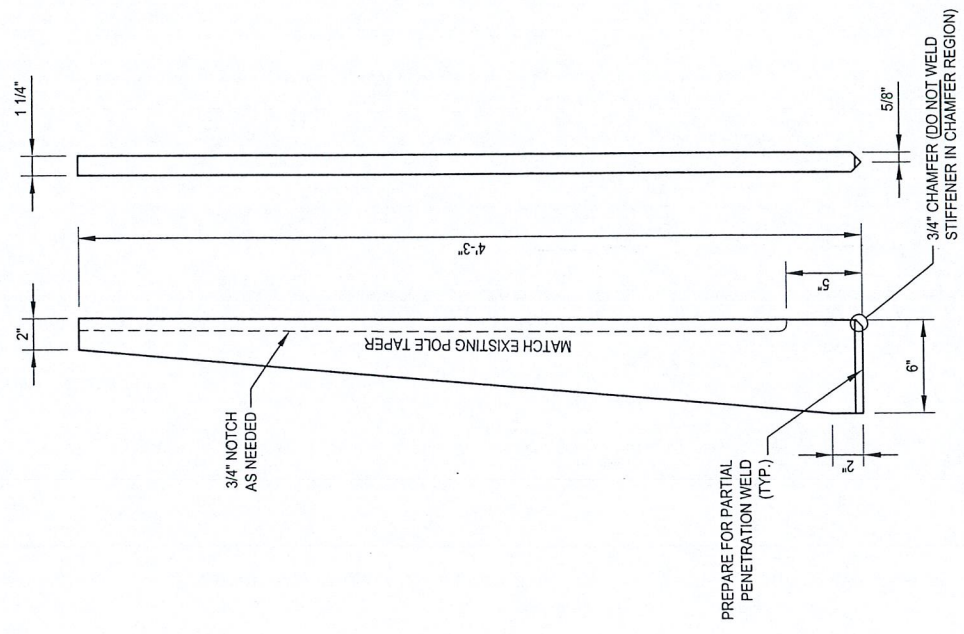
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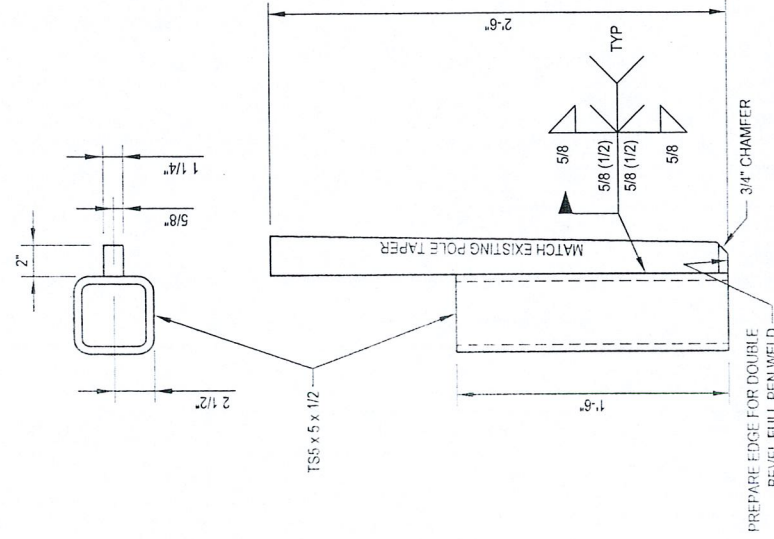
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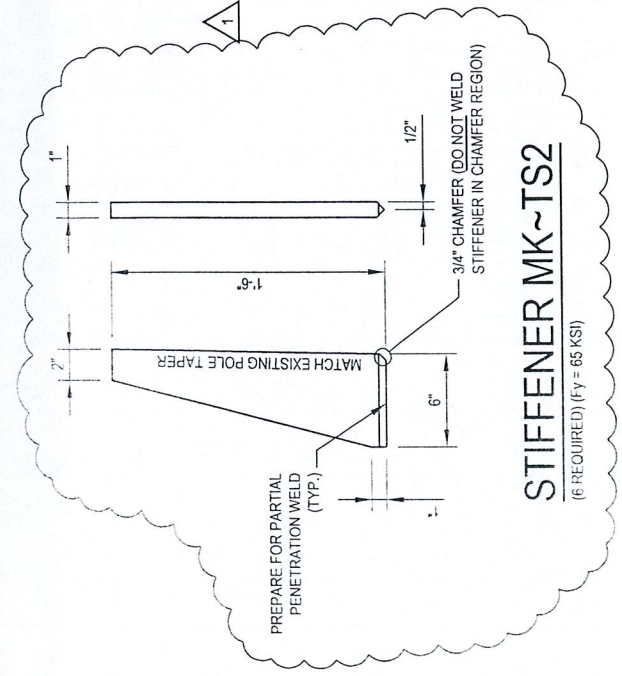
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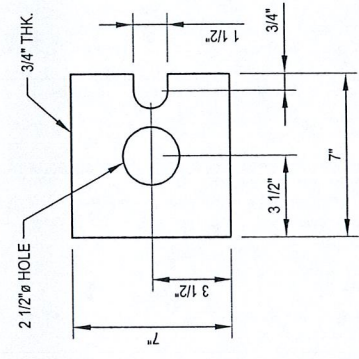
TRANSITION STIFFENER MK~TS1
 (6 TOTAL REQUIRED; 3 NOTCHED) (Fy = 65 KSI)



ANCHOR BRACKET MK~AB1
 (3 REQUIRED) (TUBE Fy = 46 KSI) (STIFFENER Fy = 65 KSI)



STIFFENER MK~TS2
 (6 REQUIRED) (Fy = 65 KSI)



WASHER PLATE MK~WP1
 (3 REQUIRED) (Fy = 50 KSI)



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1 10-23-2012; ADDED STIFFENER DETAIL

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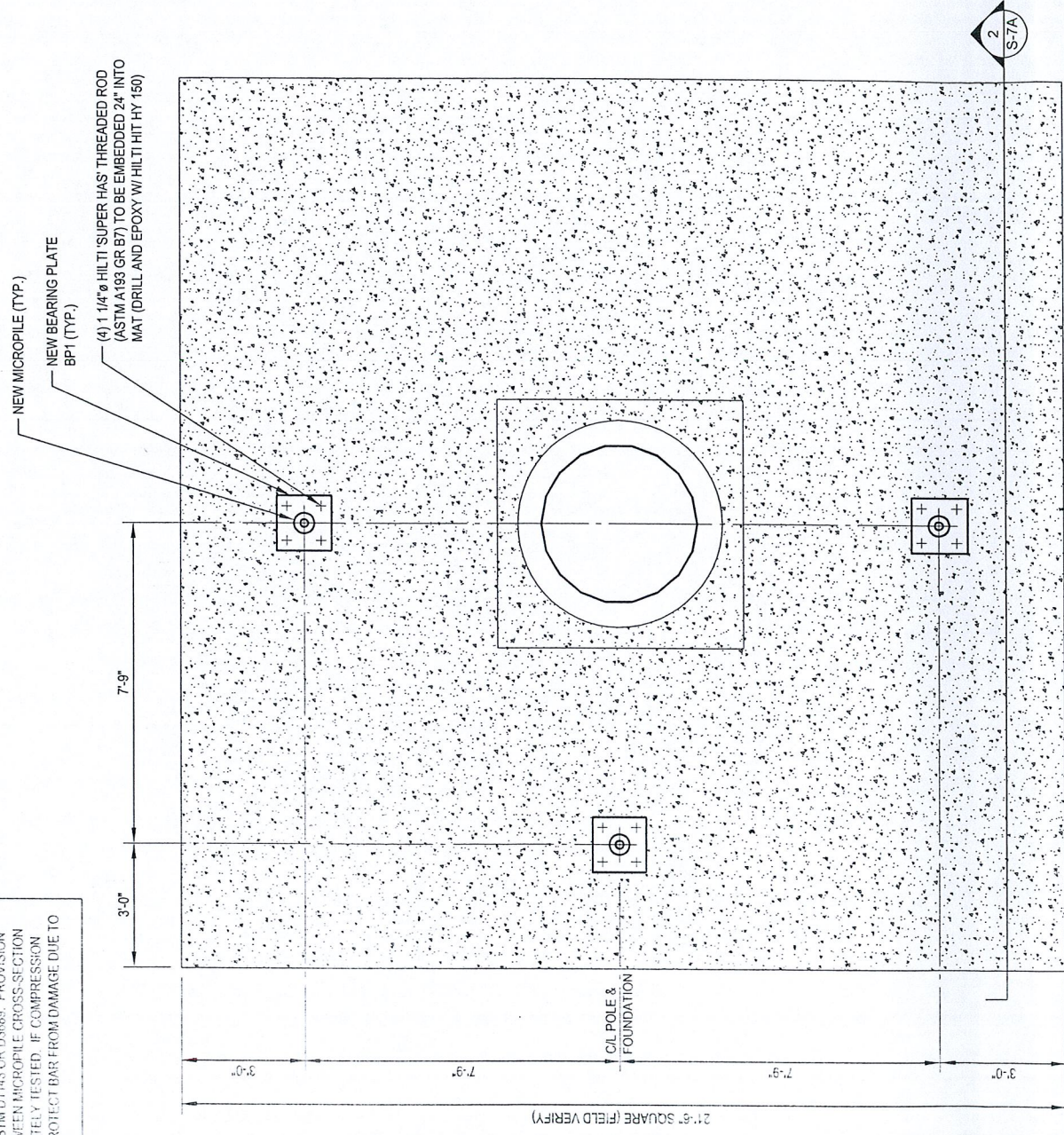
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MICROPILE TESTING REQUIREMENTS

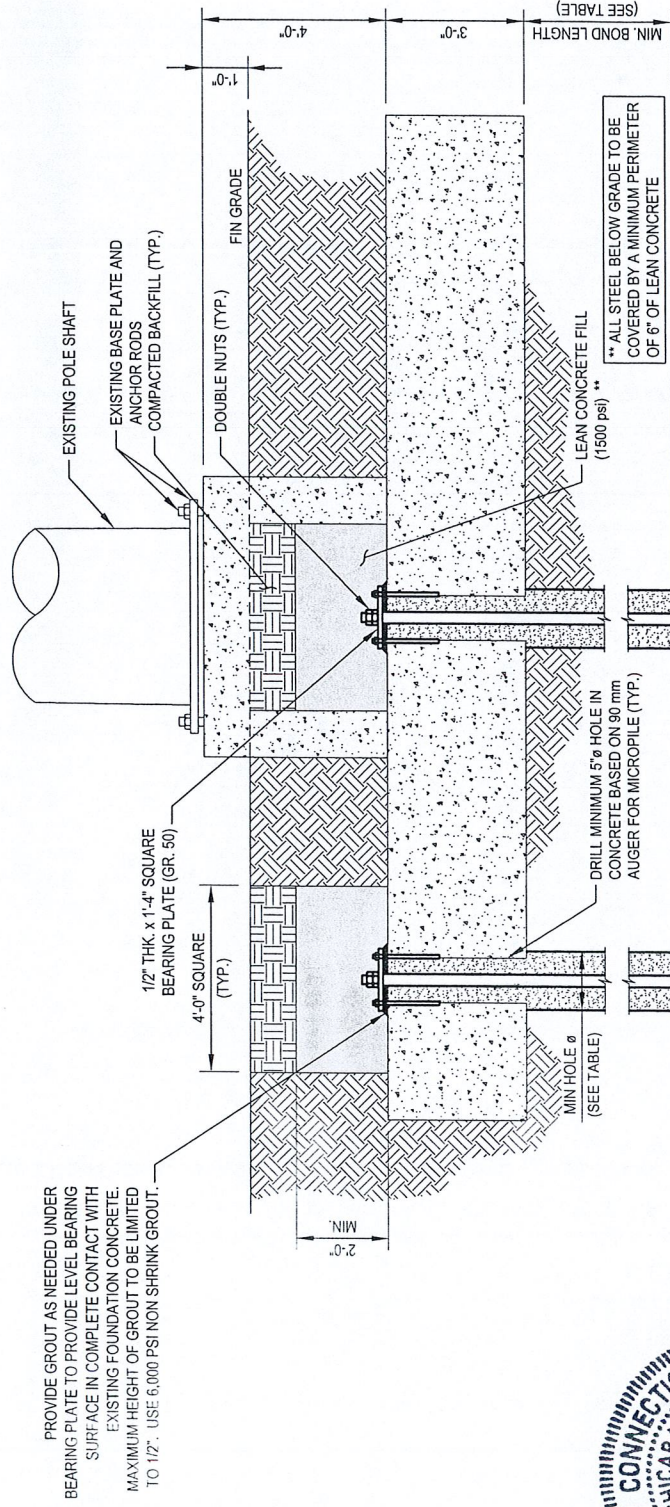
A MINIMUM OF 2 IN PLACE MICROPILES (TEST PILES SHALL BE IN OPPOSITE CORNERS OF FOUNDATION) ARE TO BE TESTED TO 94.5k IN TENSION. PROVIDE REPORT OF TEST RESULTS TO STRUCTURAL ENGINEER AND GEOTECHNICAL ENGINEER ALONG WITH RECOMMENDATIONS (IF ANY) FOR PRODUCTION PILE LENGTHS TO ACHIEVE THE 94.5k PILE WORKING CAPACITIES. (SF-27.0)

ALL PILE TESTING SHALL BE CARRIED OUT PER ASTM D1143 OR D3689. PROVISION SHALL BE MADE TO ALLOW FOR MOVEMENT BETWEEN MICROPILE CROSS-SECTION AND SOIL SO THAT GROUT BOND LINE IS ADEQUATELY TESTED. IF COMPRESSION TESTING IS PERFORMED, CONTRACTOR SHALL PROTECT BAR FROM DAMAGE DUE TO BUCKLING FOR LENGTH WITHIN MAT THICKNESS.

CONTECH'S 40/16 HOLLOW BAR MICROPILE OR EQUIVALENT SYSTEM.



FOUNDATION REINFORCING PLAN 1 S-7A



FOUNDATION REINFORCING 2 S-7A

PROVIDE GROUT AS NEEDED UNDER BEARING PLATE TO PROVIDE LEVEL BEARING SURFACE IN COMPLETE CONTACT WITH EXISTING FOUNDATION CONCRETE. MAXIMUM HEIGHT OF GROUT TO BE LIMITED TO 1/2\".



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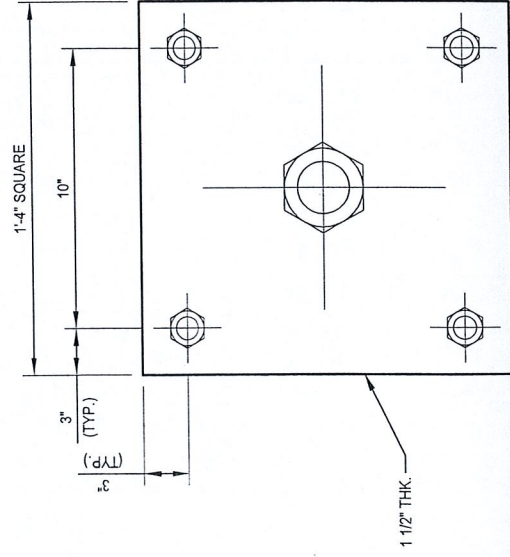
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- MICROPILE NOTES:
1. ALL BEARING PLATE STEEL SHALL CONFORM TO ASTM A572 (FY=50 KSI).
 2. WELDED CONNECTIONS SHALL CONFORM TO THE LAST REVISED CODE OF THE AMERICAN WELDING SOCIETY A.W.S. D1.1.
 3. FOUNDATION DESIGN IS BASED ON GEOTECHNICAL REPORT PREPARED BY DR. CLARENCE WELTI, P.E., P.C. DATED SEPTEMBER 22 1999, PROJECT NAME CT23XC507
 4. MICROPILE DESIGN BASED ON (3) 4"Ø DRILLED/GROUTED MICROPILES (MICROPILES MUST PROVIDE A 94.5 KIPS WORKING LOAD CAPACITY @ 25' MIN. ROCK EMBEDMENT) OR EQUIVALENT.
 5. GROUT TO BE 4,000 PSI MIN COMPRESSION STRENGTH WITH 0.5 (MAXIMUM WATER/CEMENT) W/C RATIO (TO BE COLLOIDALLY MIXED FOR MICROPILE).
 6. ALL THREADED RODS TO BE GALVANIZED PER ASTM A163, PLATES GALVANIZED PER ASTM A123.

PILE DESIGN PARAMETER SCHEDULE							
PARAMETER	Ø STEEL AREA	PILE CAPACITY (kips)	ULTIMATE SKIN FRICTION (PSF)	PRESTRESSING LENGTH	FRICTION DEVELOPMENT LENGTH/BOND LENGTH	ROCK SOCKET/PLUNGE LENGTH	TOTAL EMBEDMENT LENGTH
OPTIONS	4"Ø	94.5K	10000 PSF	0	20' MIN.	N.A.	25'
MICROPILE	1.36 IN ² MIN.						

*INSTALLED GROUT COLUMN IS BASED ON A 90MM ANGER W/ 5/2 ADAPTOR FOR ROCK



NEW BEARING PLATE MK~BP1

(FY=50 KSI) (TYP. 3 LOCATIONS)



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S-8A

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MODIFICATION INSPECTION NOTES:

GENERAL
 THE MODIFICATION INSPECTION (MI) IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND OTHER REPORTS TO ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, NAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF RECORD (EOR).

THE MI IS TO CONFIRM INSTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN ITSELF. WORKDOLS THE MI INSPECTOR TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIVENESS AND INTEGRITY REMAINS WITH THE EOR AT ALL TIMES.

ALL MFS SHALL BE CONDUCTED BY A CROWN ENGINEERING VENDOR (AEV) OR ENGINEERING SERVICE VENDOR (AESV) THAT IS APPROVED TO PERFORM ELEVATED WORK FOR CROWN. SEE ENG-BUL-1017/LIST OF APPROVED MI VENDORS.

TO ENSURE THAT THE REQUIREMENTS OF THE MI ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MI INSPECTOR BEGIN COMMUNICATING AND COORDINATING AS SOON AS A PO IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY. IF CONTACT INFORMATION IS NOT KNOWN, CONTACT YOUR CROWN POINT OF CONTACT (POC).

REFER TO ENG-SOW-10007 MODIFICATION INSPECTION SOW FOR FURTHER DETAILS AND REQUIREMENTS.

MI INSPECTOR
 THE MI INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO FOR THE MI TO, AT A MINIMUM:

- REVIEW THE REQUIREMENTS OF THE MI CHECKLIST
- WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

THE MI INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE MI REPORT TO CROWN.

GENERAL CONTRACTOR
 THE GC IS REQUIRED TO CONTACT THE MI INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURKEY PROJECT TO, AT A MINIMUM:

- REVIEW THE REQUIREMENTS OF THE MI CHECKLIST
- WORK WITH THE MI INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
- BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH THE REQUIREMENTS OF THE MI CHECKLIST AN ENG-SOW-10007.

RECOMMENDATIONS
 THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A MI REPORT:

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE MI INSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE MI TO BE CONDUCTED.
- THE GC AND MI INSPECTOR COORDINATE CLOSELY THROUGHOUT THE ENTIRE PROJECT.
- WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MI INSPECTOR ON-SITE SIMULTANEOUSLY FOR ANY GUY WIRE TENSIONING OR RE-TENSIONING OPERATIONS
- IT MAY BE BENEFICIAL TO INST ALL TOWER MODIFICATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND MI INSPECTIONS TO COMMENCE WITH ONE SITE VISIT.
- WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MI INSPECTOR ON-SITE DURING THE MI TO HAVE ANY DEFICIENCIES CORRECTED DURING THE INITIAL MI. THEREFORE, THE GC MAY CHOOSE TO COORDINATE THE MI CAREFULLY TO ENSURE ALL CONSTRUCTION FACILITIES ARE AT THEIR DISPOSAL WHEN THE MI INSPECTOR IS ON-SITE.

CANCELLATION OR DELAYS IN SCHEDULED MI
 IF THE GC AND MI INSPECTOR AGREE TO A DATE ON WHICH THE MI WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, CROWN SHALL NOT BE RESPONSIBLE FOR ANY COSTS, FEES, LOSS OF DEPOSITS AND/OR OTHER PENALTIES RELATED TO THE CANCELLATION OR DELAY INCURRED BY EITHER PARTY FOR ANY TIME (E.G. TRAVEL AND LODGING, COSTS OF KEEPING EQUIPMENT ON-SITE, ETC.). IF CROWN CONTACTS DIRECTLY FOR A THIRD PARTY, MI EXCEPTIONS MAY BE MADE IN THE EVENT THAT THE DELAY/CANCELLATION IS CAUSED BY WEATHER OR OTHER CIRCUMSTANCES THAT MAY COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

CORRECTION OF FAILING MI S
 IF THE MODIFICATION INSTALLATION WOULD FAIL THE MI ("FAILED MI"), THE GC SHALL WORK WITH CROWN TO COORDINATE A REMEDIATION PLAN IN ONE OF TWO WAYS:

- CORRECT FAILING ISSUES TO COMPLY WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND COORDINATE A SUPPLEMENT MI
- OR, WITH CROWN'S APPROVAL, THE GC MAY WORK WITH THE EOR TO RE-ANALYZE THE MODIFICATION/REINFORCEMENT USING THE AS-BUILT CONDITION

MI VERIFICATION INSPECTIONS
 CROWN RESERVES THE RIGHT TO CONDUCT A MI VERIFICATION INSPECTION TO VERIFY THE ACCURACY AND COMPLETENESS OF PREVIOUSLY COMPLETED MI INSPECTIONS ON TOWER MODIFICATION PROJECTS.

ALL VERIFICATION INSPECTIONS SHALL BE HELD TO THE SAME SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS AND IN ACCORDANCE WITH ENG-SOW-10007.

VERIFICATION INSPECTION MAY BE CONDUCTED BY AN INDEPENDENT AEA/AESV FIRM AFTER A MODIFICATION PROJECT IS COMPLETED, AS MARKED BY THE DATE OF AN ACCEPTED "PASSING MI" OR "PASS AS NOTED MI" REPORT FOR THE ORIGINAL PROJECT.

PHOTOGRAPHS
 BETWEEN THE GC AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE MI REPORT:

- PRE-CONSTRUCTION GENERAL SITE CONDITION
- PHOTOGRAPHS DURING THE REINFORCEMENT MODIFICATION CONSTRUCTION/RECTION AND INSPECTION
- RAW MATERIALS
- PHOTOS OF ALL CRITICAL DETAILS
- FOUNDATION MODIFICATIONS
- WELD PREPARATION
- BOLT INSTALLATION AND TORQUE
- FINAL INSTALLED CONDITION
- SURFACE COATING REPAIR
- POST CONSTRUCTION PHOTOGRAPHS
- FINAL INFIELD CONDITION

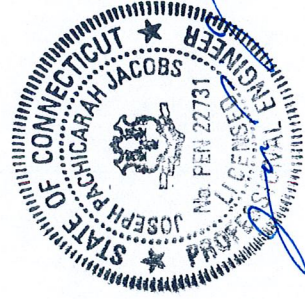
PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE.

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS, PLEASE REFER TO ENG-SOW-10007.

MI CHECKLIST	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY EOR)	REPORT ITEM
PRE-CONSTRUCTION	
X	MI CHECKLIST DRAWINGS
X	EOR APPROVED SHOP DRAWINGS
X	FABRICATION INSPECTION
NA	FABRICATOR CERTIFIED WELD INSPECTION
X	MATERIAL TEST REPORT (MTR)
X	FABRICATOR NDE INSPECTION
X	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)
X	PACKING SLIPS
ADDITIONAL TESTING AND INSPECTIONS: _____	
CONSTRUCTION	
X	CONSTRUCTION INSPECTIONS
X	FOUNDATION INSPECTIONS
NA	CONCRETE COMP. STRENGTH AND SLUMP TESTS
X	POST INSTALLED ANCHOR ROD VERIFICATION
X	BASE PLATE GROUT VERIFICATION
X	CONTRACTOR'S CERTIFIED WELD INSPECTION
NA	EARTHWORK: LIFT AND DENSITY
X	ON SITE COLD GALVANIZING VERIFICATION
NA	GUY WIRE TENSION REPORT
X	GC AS-BUILT DOCUMENTS
X	INSPECTION OF BOLT PRETENSION PER AISC BOLT SPEC.
X	INSPECTION OF ALAX BOLTS AND DTI'S PER REQUIREMENTS ON SHEET S-3
ADDITIONAL TESTING AND INSPECTIONS: _____	
POST-CONSTRUCTION	
X	MI INSPECTOR REDLINE OR RECORD DRAWING(S)
X	POST INSTALLED ANCHOR ROD PULL-OUT TESTING
X	PHOTOGRAPHS
ADDITIONAL TESTING AND INSPECTIONS: _____	

NOTE: X DENOTES A DOCUMENT NEEDED FOR THE PMI REPORT
 NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE PMI REPORT

FEB 08 2013



1 10-23-2012

AEROSOLUTIONS SHAFT REINFORCING OPTION

PAUL J. FORD AND COMPANY
 STRUCTURAL ENGINEERS
 250 East Broad Street, Suite 1500 Columbus, Ohio 43215
 (614) 221-6679 www.pjfweb.com

CROWN CASTLE
 3530 FORBIDDON WAY, SUITE 300, CHARLOTTE, NC 28277
 PH: (704) 371-3945 FAX: (704) 416-6950

BU #876361; SEYMOUR 2/OXFORD TOWN GARAGE
OXFORD, CT
 MONOPOLE REINFORCEMENT AND RETROFIT PROJECT

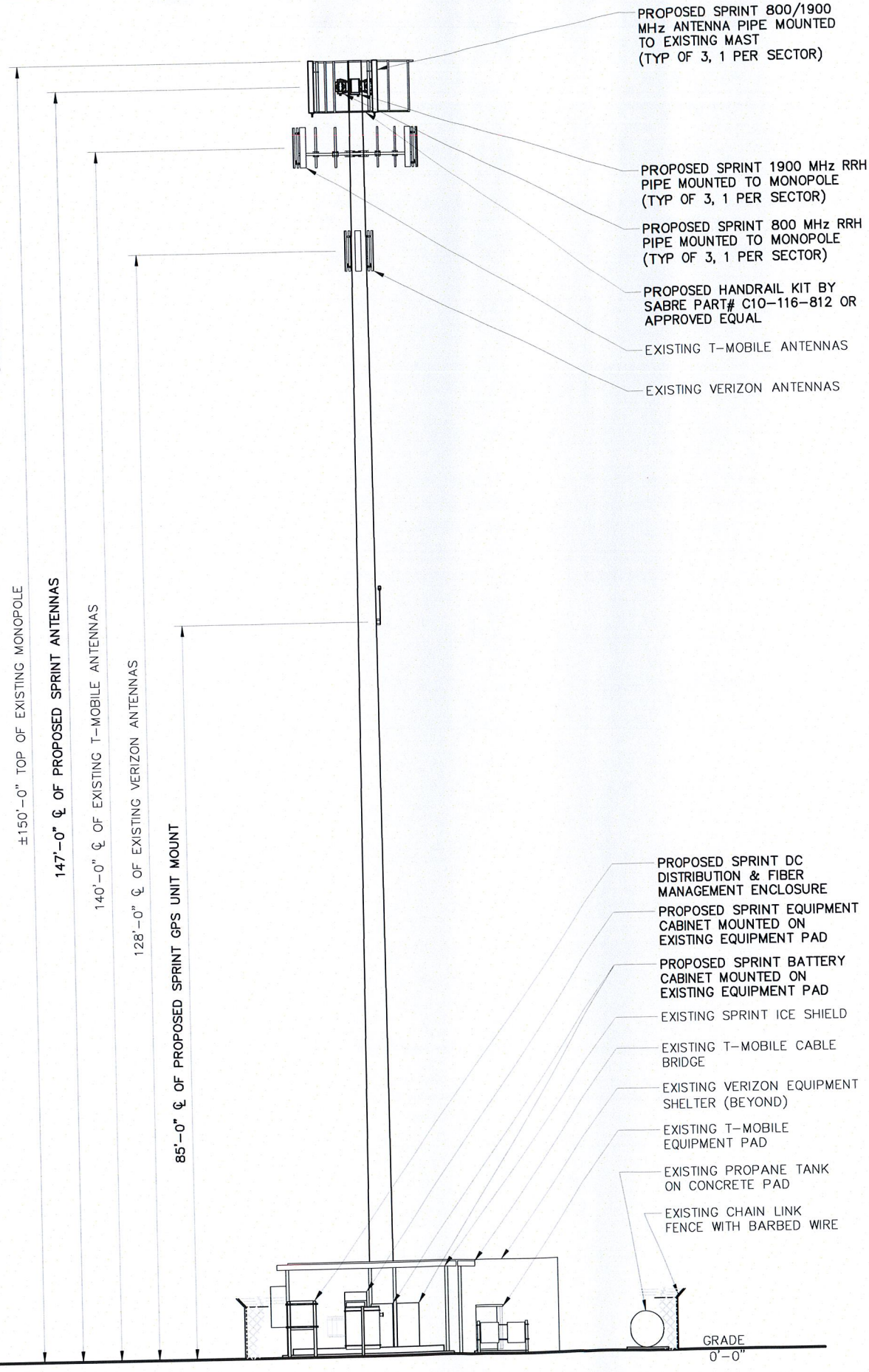
PROJECT No: 37512-1818
 DRAWN BY: B.M.S.
 CHECKED BY: C.M.M.
 APPROVED BY:
 DATE: 6-28-2012

ISSUE DATE OF PERMIT: 6-28-2012

S-9A

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THE STRUCTURAL ENGINEERING CONCERNING THE STRUCTURAL STABILITY OF THE TOWER/POLE, FOUNDATION, ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT IS BEING COMPLETED BY OTHERS. KMB DESIGN GROUP, LLC HAS NOT BEEN REQUESTED TO PERFORM ANY STRUCTURAL ANALYSIS SERVICES TO VERIFY THAT THE TOWER/POLE AND/OR FOUNDATION IS CAPABLE OF SUPPORTING THE PROPOSED EQUIPMENT DEPICTED WITHIN THESE SIGNED AND SEALED DRAWINGS. FURTHERMORE KMB DESIGN GROUP, LLC HAS NOT BEEN REQUESTED TO PHYSICALLY CONFIRM THE EXISTING MOUNT CONFIGURATION AND PERFORM A STRUCTURAL ANALYSIS TO VERIFY THAT THE EXISTING, INTERIM AND PROPOSED ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT CAN BE SAFELY SUPPORTED. SIGNED AND SEALED DRAWINGS REVISED TO STATE "ISSUED FOR CONSTRUCTION" SHALL BE PROVIDED TO THE PROFESSIONAL ENGINEERS RESPONSIBLE FOR THE STRUCTURAL ANALYSIS OF THE TOWER/POLE, ANTENNAS, MOUNTS AND ALL ASSOCIATED ANCILLARY RADIO EQUIPMENT. KMB DESIGN GROUP, LLC SHALL BE NOTIFIED SHOULD THE STRUCTURAL ANALYSIS RESULT IN SOME ELEMENTS NOT BEING STRUCTURALLY CAPABLE OF SUPPORTING THE PROPOSED DESIGN DEPICTED. THE CONTRACTOR SHALL NOT COMMENCE CONSTRUCTION WITHOUT OBTAINING (A) A SIGNED AND SEALED COPY OF THE PLANS "ISSUED FOR CONSTRUCTION"; (B) STRUCTURAL ANALYSIS REPORT STATING THAT THE TOWER/POLE/FOUNDATION IS CAPABLE OF SUPPORTING THE PROPOSED LOADING REFERENCING THE SIGNED AND SEALED PLANS BY KMB DESIGN GROUP, LLC; (C) SPRINT PLATFORM ANALYSIS STATING THAT THE SPRINT PLATFORM IS CAPABLE OF SUPPORTING THE PROPOSED DESIGN AS REFERENCED WITHIN THE SIGNED AND SEALED PLANS BY KMB DESIGN GROUP, LLC.



NOTES:
 1. NO CONSTRUCTION TO COMMENCE PRIOR TO CROWN CASTLE APPROVAL.
 2. FINAL ANTENNA & EQUIPMENT CONFIGURATION SHOWN ON THIS PLAN. SEE EQUIPMENT & ANTENNA PLAN SHEETS FOR EXISTING AND INTERIM CONFIGURATION.
 3. CONTRACTOR TO VERIFY ALL TOWER MODIFICATIONS HAVE BEEN COMPLETED AS PER CROWN CASTLE STRUCTURAL ANALYSIS REPORT PRIOR TO CONSTRUCTION.

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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



CT LICENSE: 26657 2/12/13

PROJECT NUMBER: **332.1484**

SITE INFORMATION:
 20 GREAT OAK ROAD
 OXFORD, CT 06478
 FAIRFIELD COUNTY
 CROWN CASTLE SITE: 876361
CT23XC507

PROJECT TYPE: **NETWORK VISION**

DRAWN BY: **JLS** CHECKED BY: DATE: **03-13-12**

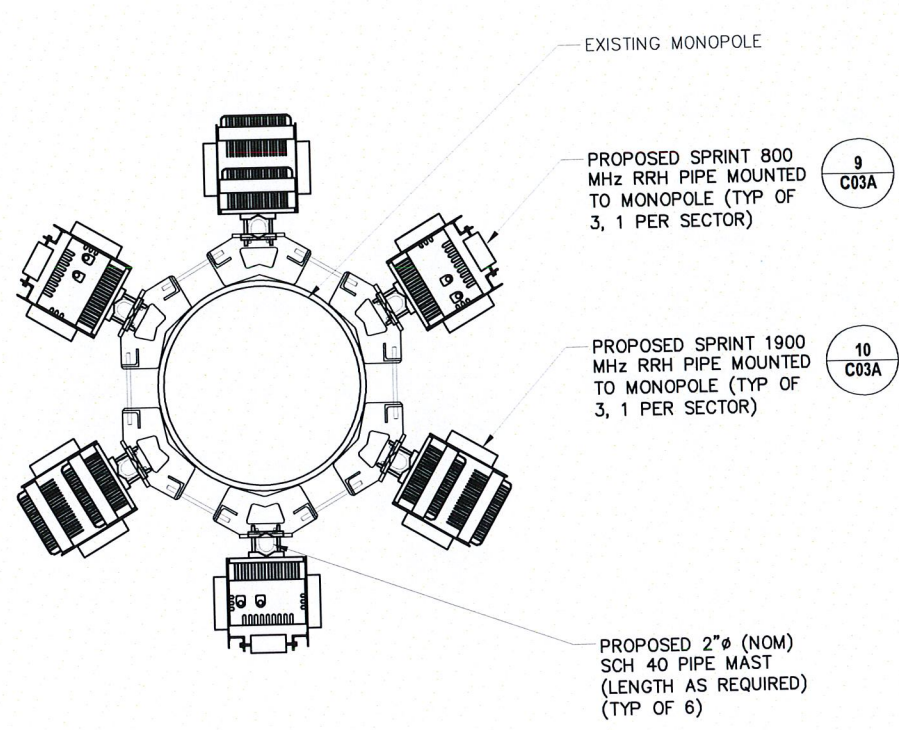
SHEET TITLE: **ELEVATION**

SHEET NUMBER: **C02A** REV: **0**

1 **NORTHEAST ELEVATION**
 11x17 SCALE: 1/16" = 1'-0" 24x36 SCALE: 1/8" = 1'-0"

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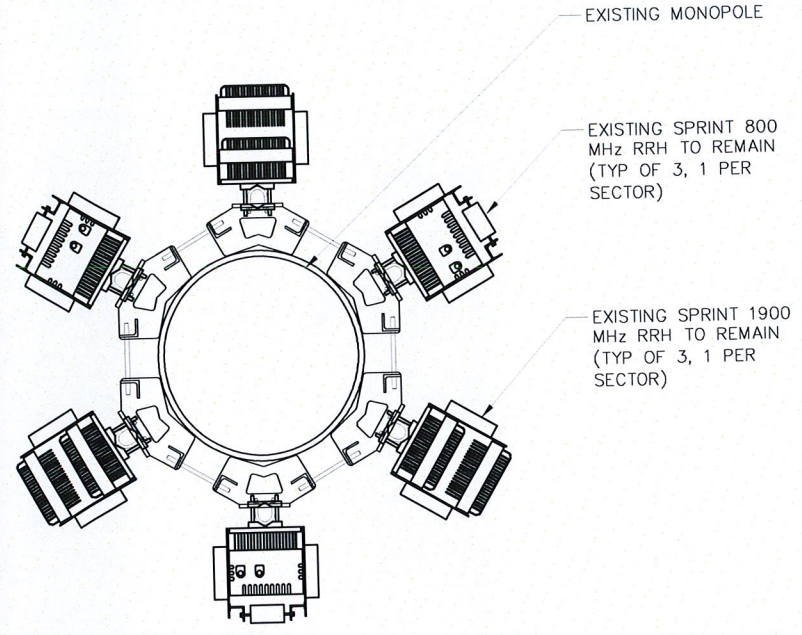
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1 INTERIM RRH PLAN @ ±146'-0" AGL (ALL SECTORS)

11x17 SCALE: 3/8" = 1'-0"

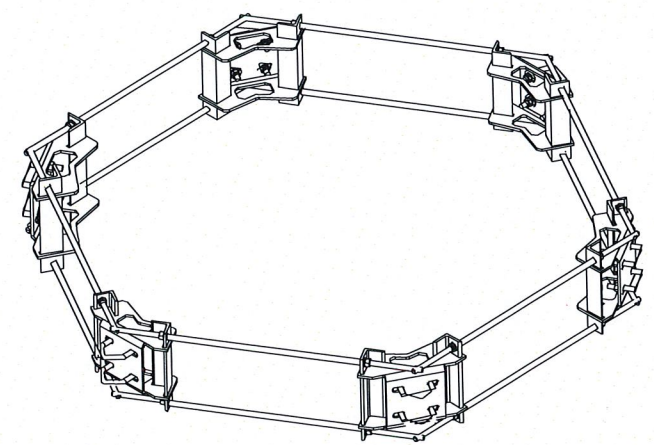
24x36 SCALE: 3/4" = 1'-0"



2 FINAL RRH PLAN @ ±146'-0" AGL (ALL SECTORS)

11x17 SCALE: 3/8" = 1'-0"

24x36 SCALE: 3/4" = 1'-0"



3 RRH MOUNT DETAIL

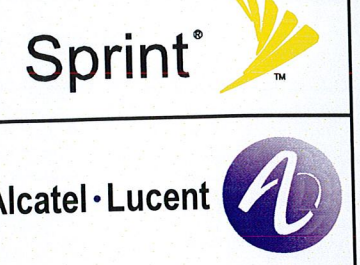
SCALE: NTS

NOTE:
RRHs NOT SHOWN FOR CLARITY.

SIX SECTOR PIPE RING MOUNT KIT BY COMMSCOPE, PART # RR-RM1560 OR AN APPROVED EQUAL KIT INCLUDES:
MOUNT, THREADED ROD & (12)
2-3/8" U-BOLTS

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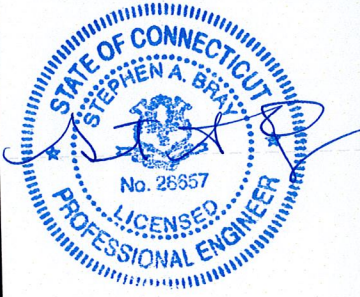
NOTE:
1. CONTRACTOR TO VERIFY ALL TOWER MODIFICATIONS HAVE BEEN COMPLETED AS PER CROWN CASTLE STRUCTURAL ANALYSIS REPORT PRIOR TO CONSTRUCTION.
2. NO CONSTRUCTION IS TO COMMENCE PRIOR TO CROWN CASTLE APPROVAL



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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY	



Stephen A. Bray
PROFESSIONAL ENGINEER



CT LICENSE: 26657 2/12/13

PROJECT NUMBER: **332.1484**

SITE INFORMATION:
20 GREAT OAK ROAD
OXFORD, CT 06478
FAIRFIELD COUNTY
CROWN CASTLE SITE: 876361
CT23XC507

PROJECT TYPE: **NETWORK VISION**

DRAWN BY: **JLS** CHECKED BY: DATE: **03-13-12**

SHEET TITLE: **RRH PLANS (ALL SECTORS)**

SHEET NUMBER: **C04C** REV: **0**

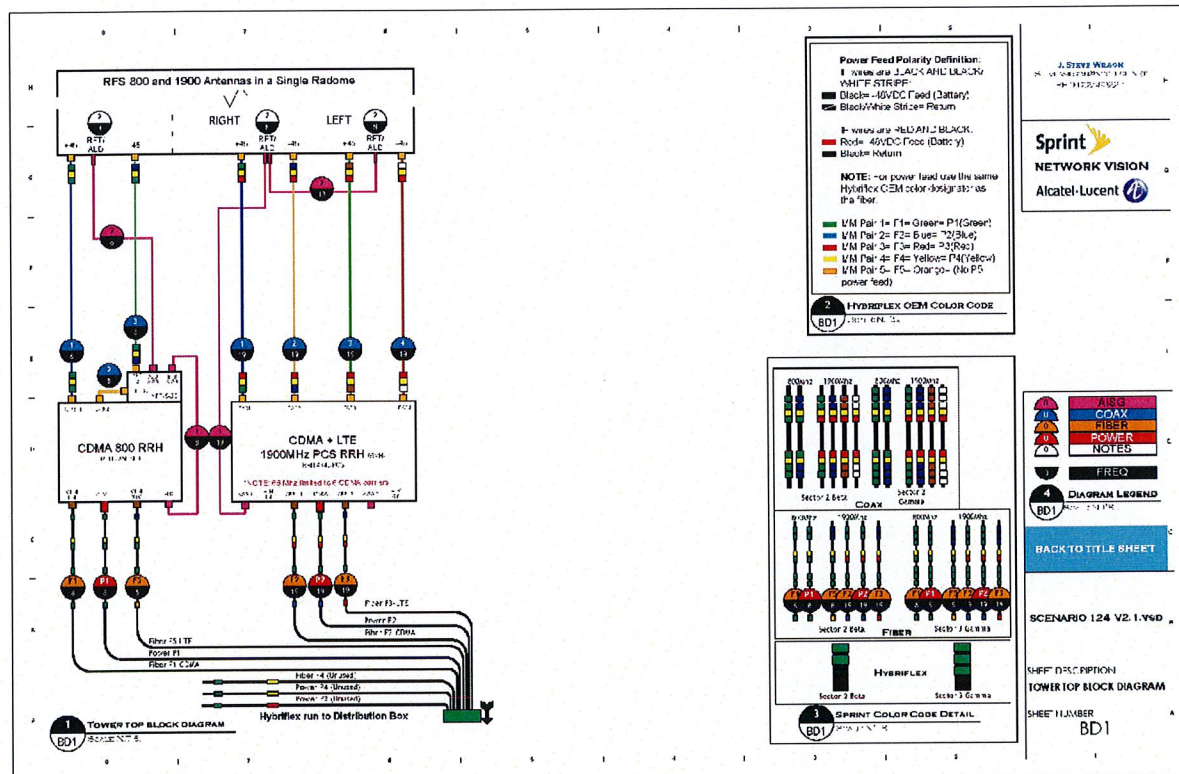
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FINAL ANTENNA AND CABLE SCHEDULE

SECTOR	ANTENNA	AZIMUTH (DEGREES)	MECHANICAL DT (DEGREES)	ELECTRICAL DT (DEGREES)	RAD CENTER AGL (FT)	ANTENNA		RRH		TOP COAX JUMPER		COMBINER JUMPER		NOTCH FILTER JUMPER		HYBRIFLEX LENGTH (FT)
						MAKE	MODEL	QTY	QTY	LENGTH (FT)	QTY	LENGTH (FT)	QTY	LENGTH (FT)		
1	800/1900	310	0	800 -8 1900 -5	147.0	RFS	APXVSP18-C-A20	800 1 1900 1	6	10	-	-	1	3	210	
2	800/1900	70	0	800 -7 1900 -1	147.0	RFS	APXVSP18-C-A20	800 1 1900 1	6	10	-	-	1	3	210	
3	800/1900	220	0	800 -5 1900 -2	147.0	RFS	APXVSP18-C-A20	800 1 1900 1	6	10	-	-	1	3	210	

- NOTES:
- DUE TO FIELD MEASUREMENTS AND THE INSTALLATION OF NEW ANTENNAS THAT VARY IN SIZE FROM THE EXISTING ANTENNAS, THE ANTENNA RAD CENTER HAS CHANGED FROM WHAT IS ON RECORD. THE DATABASE MAY NEED TO BE UPDATED TO MATCH THESE PLANS.
 - SOME CABLING MAY CHANGE AT THE TIME OF CONSTRUCTION. CONTRACTOR TO CONFIRM ALL CABLE LENGTHS, TYPE, QUANTITIES, AND CONFIGURATION PRIOR TO CONSTRUCTION.
 - ALL UNUSED POWER AND FIBER MUST BE PROPERLY TERMINATED AND WEATHERPROOFED.

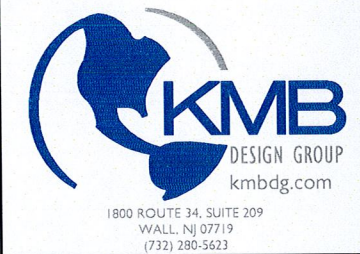
CONTRACTOR TO VERIFY & USE THE LATEST TOWER TOP SCENARIO AS PROVIDED BY ALCATEL-LUCENT CONSTRUCTION MANAGER



ALL SECTORS



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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



Stephen A. Bray
PROFESSIONAL ENGINEER



CT LICENSE: 26657 2/12/13

PROJECT NUMBER: 332.1484

SITE INFORMATION:
20 GREAT OAK ROAD
OXFORD, CT 06478
FAIRFIELD COUNTY
CROWN CASTLE SITE: 876361
CT23XC507

PROJECT TYPE: NETWORK VISION

DRAWN BY: JLS CHECKED BY: DATE: 03-13-12

SHEET TITLE: RF SCHEDULE

SHEET NUMBER: C06 REV: 0

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GENERAL SPECIFICATIONS

- Contractor shall verify that the total number of service entrance disconnects in the existing utility company pedestal must not exceed six. If the new service added exceeds this value, contractor must coordinate with the utility company and authority having jurisdiction. Run an additional exclusive and dedicated service lateral set for the new load added to the compound as per NEC Article # 230-2(B)
- All work should be done in a neat workmanlike manner, left clean and free from defects, and completely operable. The contractor shall provide all equipment as scheduled on the drawings. All materials shall be new and all work and materials shall be guaranteed by the contractor for a period of one (1) year from the date of acceptance by the owner.
- All work shall be carefully coordinated with the landlord and all trades involved, and the contractor shall provide proper connections, fittings, valves, piping, etc. for all equipment furnished by carrier or other trades involved in this contract.
- Contractor shall inform the engineer immediately of any conflict discovered before performing any work related to such conflict.
- Provide all required temporary utilities and pay all associated fees and operating costs.
- Before submitting this bid, the contractor shall visit the job site to examine and fully acquaint himself with the existing job conditions, paying particular attention to the location of existing conditions to make a complete and operable system without additional cost to the carrier or the engineer.
- Obtain all permits and approvals from authorities having jurisdiction and paying all fees required.
- Label all equipment served from Sprint panelboard with phenolic labels sized in relation to usage.
- Contractor to provide and install engraved label on the Sprint meter socket enclosure.
- Redlined As-Builts are to be delivered to a Sprint representative.
- The equipment/protections must be rated for standard of AIC rate higher than incoming equipment and/or utility company AIC rate.

GROUNDING NOTES

- The subcontractor is responsible for properly sequencing grounding and underground conduit installation as to prevent any loss of continuity in the grounding system or damage to the conduit.
- All exterior ground conductors shall be #2 AWG solid tinned copper unless otherwise indicated.
- All ground connections above grade (interior & exterior) shall be formed using high press crimps.
- All ground connections below grade shall be exothermic (Cadweld).
- Connections to equipment and enclosures shall be made utilizing two-hole ground lugs with an antioxidant compound.
- Maximum resistance of the completed ground system shall not exceed 5 Ohms. Testing shall be performed in accordance with technical specification for facility grounding, using fall potential method.
- Where grounding connections are made to painted metal surfaces shall be scraped clean to bear metal to ensure proper contact. Surfaces shall be restored to match original finishes.
- Use of 90° bends in the protection grounding conductors shall be avoided when 45° bends can be adequately supported.
- Ground depth shall be 30" minimum below finished grade, or 6" below frost line, whichever is greater.
- Home run grounds not approved. All antenna buss bars should be installed directly to tower steel without insulators or down conductors.

ELECTRICAL SYMBOLS		ABBREVIATIONS	
WIRING SYMBOLS		AWG	AMERICAN WIRE GAUGE
	DISCONNECT SWITCH	BCW	BARE COPPER WIRE
	METER	DWG	DRAWING
	CIRCUIT BREAKER	EMT	ELECTRICAL METALLIC TUBING
	CADWELD TYPE CONNECTION	GEN	GENERATOR
	COMPRESSION TYPE CONNECTION	MGB	MASTER GROUND BAR
	GROUND ROD WITH ACCESS	PVC	RIGID (SCH 40) PVC CONDUIT
	CHEMICAL GROUND ROD	RGS	RIGID GALVANIZED STEEL
	GROUND ROD	RWY	RACEWAY
	CONDUIT TURNING DOWN	TYP	TYPICAL
	CONDUIT TURNING UP		
	JUNCTION BOX		
	PULL BOX		
	CONDUIT RUNNING ABOVE GRADE		
	CONDUIT RUNNING UNDER GROUND		

ELECTRICAL SPECIFICATIONS

- General:
 - The electrical contractor shall furnish all labor, materials, tools, transportation equipment, services and facilities required for the complete, proper and substantial installation of all electrical work. All fixtures, devices, and equipment shown, noted or required on these drawings, and/or contained herein shall be connected from the source of electric power to the final connection, tested and made ready for satisfactory operation.
 - Service equipment shall be 120/240 VAC, 100 Amp, single phase, unless otherwise directed by the Sprint Construction Manager.
 - Unless otherwise indicated, the arrangement, position, connections, etc. shown on the drawings shall be taken on a diagram basis. The right is reserved by the engineer to make minor changes in locations and arrangements when required by job development without additional compensation to the contractor.
 - All work shall conform to the adopted edition of the National Electrical Code and local, state and applicable codes.
 - When a utility company meter is specified, the contractor shall obtain all associated cut-in cards, inspections, etc., necessary to have the meter set. It is the responsibility of the contractor to meet with utility company prior to construction to verify source of electric service, tap and meter location.
- Identification:
 - Provide typewritten directories for panels, indicating use of each branch circuit and designating spare circuits. Handwritten directories are not acceptable.
 - All panel boards, switches and other equipment enclosures shall bear engraved nameplates as manufactured by Seton Nameplate Corp., or equal lettering to be 1/2" white letters on black background unless noted otherwise.
- Raceways:
 - Minimum conduit size shall be 3/4" unless otherwise noted on the drawings.
 - Exposed raceways shall be run true, plumb, and parallel or perpendicular to building lines.
 - Conduit routings are schematic. Sub contractor shall install conduits so that access to equipment is not blocked.
- Wiring Methods:
 - All feeders shall consist of pulled conductors in conduit. All branch circuits shall consist of pulled conductors in conduit. Except 15 and 20 Ampere 1 pole lighting receptacles, miscellaneous branch circuits concealed above suspended ceilings or within dry walls shall consist of type MC metal clad cable if allowed by code. Connections to communications cabinets and vibrating equipment shall consist of pulled conductors in LFMC, maximum 6' in length.
 - Conductors shall be continuous from origin to panel or equipment without splices. Where tap splices are necessary and approved, they shall be made with suitable connectors in junction boxes.
 - Equipment ground conductors shall be provided for all feeders and branch circuits.
 - The contractor shall conceal all conduit routing passing through finished areas. Conduit routing through unfinished shall be supported as specified in drawings. Unless clearly specified, no conduits shall be routed on exterior surface of buildings.
 - All conductor terminals shall be U.L. listed for minimum of 75° C.
 - Provide fire stopping around all conduits at wall and floor penetrations.
 - Seal all exterior wall penetrations as required.
 - Underground conduits shall be a minimum of 24" below finished grade. All underground work shall be documented by photograph before any backfill is begun. Photos will be required at time punchlist is performed. Feeders shall be individual conductors in schedule 40 PVC, direct burial conduit. When buried conduits are subject to vehicular traffic, conduits shall be encased in concrete. All sweeps below grade shall be schedule 80 PVC.
 - All feeders in "damp" or "wet" locations shall consist of individual conductor in rigid galvanized steel or rigid aluminum conduit. Liquid-tight flexible metallic conduit shall be utilized when connecting to equipment cabinets and vibrating equipment. The maximum length for flexible conduit shall be 6'-0".
- Wiring Devices:
 - Switches, receptacles and other wiring devices shall be specification grade of type, size and rating indicated on the drawings.
- Disconnect Switches:
 - Switches shall be quick-make, quick-break NEMA 1 for indoor use and NEMA 3R for outdoor use as manufactured by General Electric, Square D or equal. Electrical contractor to provide all safety disconnects.
- Special Requirements:
 - The electrical contractor shall furnish and install all power and control wiring for equipment contained in contract documents.
 - All work requiring an outage or interruption of service (power, telephone) shall be scheduled only at such time permitted by owner.
- Lighting fixtures and lamps:
 - Lighting fixtures shall be furnished complete with necessary hardware and lamps.
- Transformers:
 - Transformers shall be dry type with average temperature rise not to exceed 150° C (115° C)(80° C)
 - Transformers shall be as manufactured by Square D, General Electric, or Siemens.

The contractor is required to contact the utility companies prior to starting construction. This is necessary to reconfirm that the utility points have remained consistent with the contractor documents:

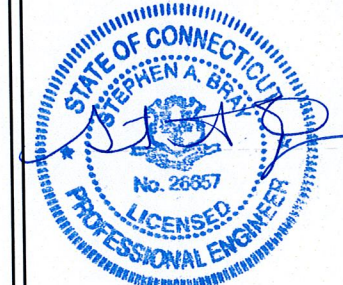
- * Telephone Demarcation Point
- * Electrical Service Tap Point
- * New Utility Meter Location



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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



Stephen A. Bray
PROFESSIONAL ENGINEER



CT LICENSE: 26657 2/12/13

PROJECT NUMBER: **332.1484**

SITE INFORMATION:
20 GREAT OAK ROAD
OXFORD, CT 06478
FAIRFIELD COUNTY
CROWN CASTLE SITE: 876361
CT23XC507

PROJECT TYPE: **NETWORK VISION**

DRAWN BY: JLS	CHECKED BY:	DATE: 03-13-12
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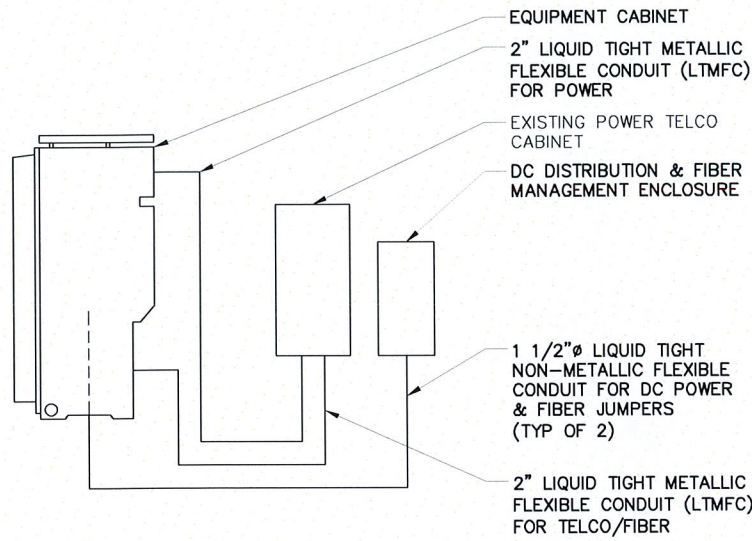
SHEET TITLE: **ELECTRICAL NOTES**

SHEET NUMBER: E01	REV.: 0
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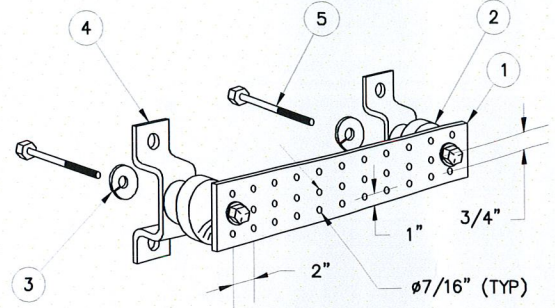
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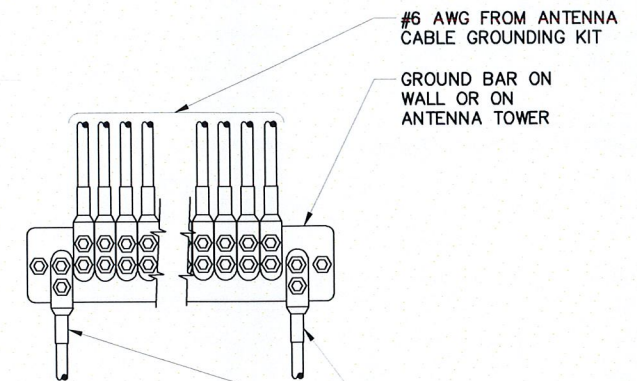


1 PLUMBING SCHEMATIC (IF REQUIRED)



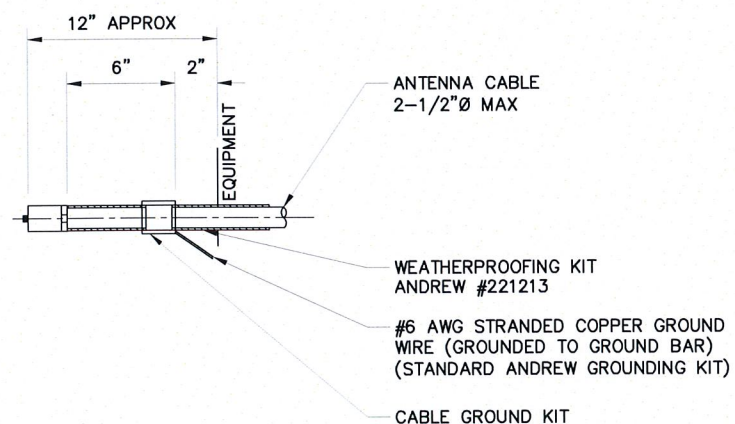
1. GALVANIZED STEEL GROUND BAR, 1/4" x 4" x 20", HAGER PART NO TGBI-14420C OR A.L.T. PART NO. 382227. HOLE CENTERS TO MATCH NEMA DOUBLE LUG CONFIGURATION.
2. INSULATORS, NEWTON INSTRUMENT CAT. NO. 3061-4.
3. 5/8" LOCKWASHERS, NEWTON INSTRUMENT CO. CAT. NO. 3015-8.
4. WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT NO. A-6056.
5. 5/8-11 X 1" H.H.C.S.BOLTS, NEWTON INSTRUMENT CO. CAT NO. 3012-1

2 GROUND BAR DETAIL



NOTE:
CONTRACTOR TO UTILIZE KOPR-SHIELD (THOMAS & BETTS) ON ALL LUG CONNECTIONS

3 GROUND LUG TO GROUND BAR CONNECTION DETAIL



NOTE:
DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.

4 CABLE GROUND KIT CONNECTION DETAIL

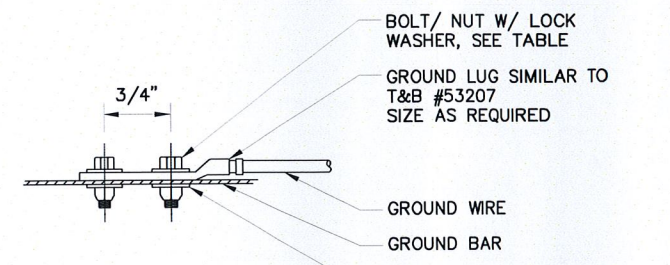
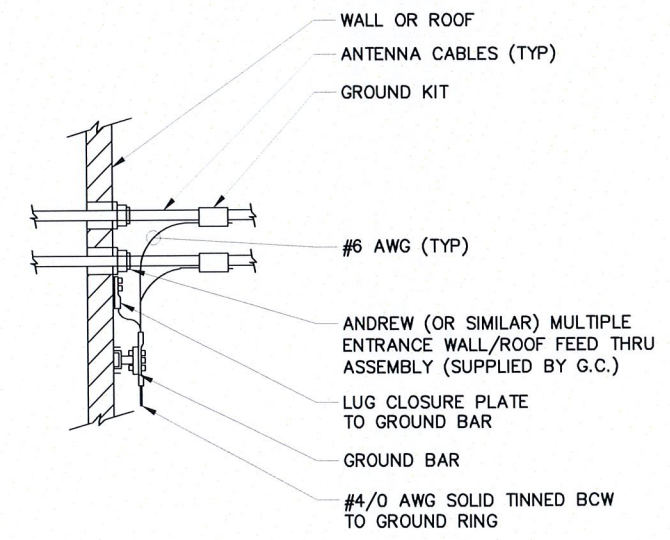
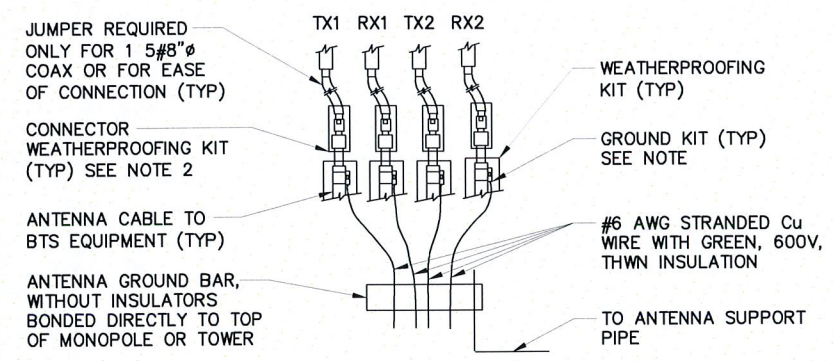


TABLE		
WIRE SIZE	LUG #	BOLT SIZE
#4/0	53212	1/2" - 20 NC x 1/2" S.S. BOLT & NUT W/ LOCK WASHERS
#2	53207	1/4" - 20 NC x 1/2" S.S. BOLT & NUT W/ LOCK WASHERS
#6	53205	

5 GROUND LUG CONNECTION DETAIL



6 CABLE GROUNDING DETAIL



- NOTES:**
1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO ANTENNA GROUND BAR.
 2. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT. COLD SHRINK SHALL NOT BE USED.
 3. ATTACH "DO NOT DISCONNECT" LABELS TO GROUND BARS. CAN USE BRASS TAG "DO NOT DISCONNECT" AT EACH COAX GROUND POINT OR BACK-A-LITE PLATE ON GROUND BAR.

7 GROUND BAR TO GROUND WIRE CONNECTION DETAIL



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△	02-12-13	ISSUED FOR CONSTRUCTION	DTP	KCD
REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



Stephen A. Bray
PROFESSIONAL ENGINEER



CT LICENSE: 26657 2/12/13

PROJECT NUMBER: **332.1484**

SITE INFORMATION:
20 GREAT OAK ROAD
OXFORD, CT 06478
FAIRFIELD COUNTY
CROWN CASTLE SITE: 876361
CT23XC507

PROJECT TYPE:
NETWORK VISION

DRAWN BY: JLS	CHECKED BY:	DATE: 03-13-12
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SHEET TITLE:
ELECTRICAL & GROUNDING DETAILS

SHEET NUMBER: E02	REV: 0
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