




(1)

## BURNDY GROUNDING DETAILS

 sCale: N.t.s

| BURNDY GROUNDING PRODUCTS 2 |
| :--- |
| SCALE: N.t.s |
| E-2 |



CADWELD GROUNDING CONNECTION PRODUCTS SCALE: N.t.s


 2 FOR GROUND BOND TO STEEL ONLY: USER A TOOTH WASHER BETWEEN LUG AND


TYPICAL GROUND BAR CONNECTIONS DETAIL Scale N.t.S


GROWN
SCALE: N.T.S

LUG NOTES:

1. ALL HAROWARE IS $18-8$ STAINLESS

CT EEL INCL ENG LOCK WAAHEEESS.

3. FOR GROUND BOND TO STEEL ONLY: NSERT A DRAGON TOOTH WASHER
BETWEEN LUG AND TEL. COAT ALL SCREEN
SURACE WITH ANTIOEXIDIZATIO
COMPUND PRIOR TO MAINE.

| GROUND BAR DETAIL | 6 |
| :--- | :--- |
| SCALE: N.T.s |  |
| -2 |  |




T-Mobile Towers
12920 SE 38th Street
Bellevue, WA 98006
(425) 383-3978

## REVIEWED

By JACKIE DONAHUE at 10:09 am, Aug 28, 2015

GPD Engineering and Architecture Professional Corporation
Chris Scheks
520 South Main Street, Suite 2531
Akron, OH 44311
(614) 588-8973
cschecks@gpdgroup.com

GPD\# 2015791.16
August 28, 2015

## STRUCTURAL ANALYSIS REPORT

| T-MOBILE DESIGNATION: | Site Number: | CTNL804B |
| :---: | :---: | :---: |
|  | Site Name: | AMTRAK_OldLyme5 |
|  | T-Mobile Project: | Network Modification |
| ANALYSIS CRITERIA: | Codes: | TIA/EIA-222-F, 2003 IBC \& 2005 CTBC |
|  |  | $104-\mathrm{mph}$ fastest-mile (equivalent 120 mph 3 second gust) with 0 " ice |
|  |  |  |
| SITE DATA: |  | 387 Shore Road, Old Lyme, CT 06371, New London County |
|  |  |  |
|  |  | 80' Sabre Monopole |

Mr. John Warzecha,

GPD is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

## Analysis Results

| Tower Stress Level with Proposed Equipment: | $51.9 \%$ | Pass |
| :--- | :--- | :--- |
| Foundation Ratio with Proposed Equipment: | $48.6 \%$ | Pass |

We at GPD appreciate the opportunity of providing our continuing professional services to you and T-Mobile Towers. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.


## SUMMARY \& RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by T-Mobile Towers. This report was commissioned by Mr. John Warzecha of T-Mobile Towers.

The proposed coax shall be installed inside the monopole in order for the results of this analysis to be valid. Please see Appendix C for feedline plan.

TOWER SUMMARY AND RESULTS

| Member | Capacity | Results |
| :--- | :---: | :---: |
| Monopole | $47.6 \%$ | Pass |
| Anchor Rods | $31.2 \%$ | Pass |
| Base Plate | $34.4 \%$ | Pass |
| Flange Plates | $29.0 \%$ | Pass |
| Flange Bolts | $51.9 \%$ | Pass |
|  |  |  |
| Foundation | $48.6 \%$ | Pass |

## ANALYSIS METHOD

tnxTower (Version 6.1.4.1), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a detailed site visit.

## DOCUMENTS PROVIDED

| Document | Remarks | Source |
| :--- | :--- | :---: |
| Structrual Analysis Worksheet | CTNL804B TMO L700, dated 8/24/2015 | T-Mobile |
| Tower Design | Sabre Job \#: 40204, dated 2/7/2011 | T-Mobile |
| Foundation Design | Sabre Job \#: 40204, dated 2/7/2011 | T-Mobile |
| Geotechnical Report | Terracon Project \#: J2105225, dated 11/11/2010 | T-Mobile |
| Previous Structural Analysis | GPD Project \#: 2014790.25 Rev 2, dated 3/19/2014 | GPD |

## ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. Loading interpreted from photos is accurate to $\pm 5^{\prime} \mathrm{AGL}$, antenna size accurate to $\pm 3.3 \mathrm{sf}$, and coax equal to the number of existing antennas without reserve.
10. The proposed loading is taken from the provided Structural Analysis Worksheet titled: CTNL804B TMO L700, dated $8 / 24 / 2015$, and is assumed to be accurate.
11. Appurtenance azimuths have not been provided and have been assumed.
12. The proposed coax shall be installed inside the monopole in order for the results of this analysis to be valid.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD should be allowed to review any new information to determine its effect on the structural integrity of the tower.

## DISCLAIMER OF WARRANTIES

GPD has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the specified code recommended amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD, but are beyond the scope of this report.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD pursuant to this report will be limited to the total fee received for preparation of this report.

## APPENDIX A

Tower Analysis Summary Form

## Tower Analysis Summary Form

General Info

| Site Name | AMTRAK_OldLyme5 |
| :--- | :---: |
| Site Number | CTNL804B |
| Proposed Carrier | T-Mobile |
| Date of Analysis | August 28,2015 |
| Company Performing Analysis | GPD |

The information contained in this summary report is not to be used independently from the PE stamped tower analysis

| Tower Info | Description | Date |
| :---: | :---: | :---: |
| Tower Type (G, SST, MP) | MP |  |
| Tower Height (top of steel AGL) | $80^{\prime}$ |  |
| Tower Manufacturer | Sabre |  |
| Tower Model | n/a |  |
| Tower Design | Sabre Job \#: 40204 | 2/7/2011 |
| Foundation Design | Sabre Job \#: 40204 | 2/7/2011 |
| Geotech Report | Terracon Project \#: J2105225 | 11/11/2010 |
| Tower Mapping | n/a |  |
| Previous Structural Analysis | GPD Project \#: 2014790.25 Rev 2 | 3/19/2014 |
| Foundation Mapping | n/a |  |

Design Parameters

| Design Code Used | TIA/EIA-222-F, |
| :--- | :---: |
|  | 2003 IBC \& 2005 CTBC |
| Location of Tower (County, State) | New London, CT |
| Basic Wind Speed (mph) | 104 (fastest-mile) |
| Ice Thickness (in) | 0.75 |
| Structure Classification (I, II, III) |  |
| Exposure Category (B, C, D) |  |
| Topographic Category (1 to 5) |  |



Steel Yield Strength (ksi)

| Steel Yield Strength (ksi) |  |
| :--- | :--- |
| Pole | 65 |
| Base Plate | 50 |
| Anchor Rods | 75 |
| Flange Plate | 60 |
| Flange Bolts | A325 |

Existing / Reserved Loading

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | $\begin{gathered} \text { Antenna } \\ \text { CL ( } \mathrm{ft} \text { ) } \end{gathered}$ | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Int./Ext. |
| T-Mobile | 77 | 77 | 3 | Panel | Ericsson | AIR 21 |  | 3 | Unknown | 12' T-Arms | 12 | Unknown | 7/8" | Internal |
| T-Mobile | 77 | 77 | 3 | Panel | Ericsson | AIR 33 |  |  |  | on the existing mounts | 1 | Hybrid | 1-5/8" | Internal |
| T-Mobile | 77 | 77 | 1 | covp | Raycap | DC4-48-60-8-20F |  |  |  | on the existing mounts |  |  |  |  |
| T-Mobile | 77 | 77 | 1 | Dish | Unknown | 2' HP Dish |  |  |  | on the existing mounts |  |  |  |  |


| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | Antenna CL (ft) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Int./Ext. |
| T-Mobile | 77 | 78 | 6 | Panel | Ericsson | AIR 21 |  | 3 | Unknown | 12' T-Arms | 12 | Unknown | 7/8" | Internal |
| T-Mobile | 77 | 76 | 3 | Panel | Commscope | LNX-6515DS-VTM |  |  |  | on the existing mounts | 1 | Hybrid | 1-5/8" | Internal |
| T-Mobile | 77 | 78 | 3 | TMA | Ericsson | KRY11271 |  |  |  | on the existing mounts |  |  |  |  |
| T-Mobile | 77 | 78 | 3 | RRUS | Ericsson | RRUS 11 B12 |  |  |  | on the existing mounts |  |  |  |  |

Note: The proposed coax shall be installed inside the monopole in order for the results of this analysis to be valid. Please see Appendix C for feedline plan.

## APPENDIX B

## tnxTower Output File

| tnxTower <br> GPD <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-3709 | Job CTNL804B AMTRAK_OldLyme5 |  | $\text { Page } 1 \text { of } 4$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2015791.16 | $\begin{aligned} & \text { Date } \\ & \text { 08:19:12 08/28/15 } \end{aligned}$ |
|  | Client | T-Mobile Towers | Designed by tbeltz |

## Tower Input Data

There is a pole section.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in New London County, Connecticut.
Basic wind speed of 104 mph .
Nominal ice thickness of 0.7500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf .
A wind speed of 38 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Feed Line/Linear Appurtenances - Entered As Area

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Allow \\
Shield
\end{tabular} \& Component Type \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& Total Number \& \& \(C_{A} A_{A}\)

$f t^{2} / f t$ \& Weight
plf <br>
\hline \multirow[t]{5}{*}{Step Pegs} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{80.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.08 \& 2.72 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.18 \& 3.51 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.28 \& 4.92 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.48 \& 9.56 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.88 \& 26.18 <br>
\hline \multirow[t]{5}{*}{Safety Line (3/8")} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{80.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.04 \& 0.22 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.14 \& 0.75 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.24 \& 1.28 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 0.44 \& 2.34 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.84 \& 4.46 <br>
\hline \multirow[t]{5}{*}{LDF5-50A (7/8 FOAM)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{77.00-8.00} \& \multirow[t]{5}{*}{12} \& No Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.00 \& 0.33 <br>
\hline \multirow[t]{5}{*}{1-5/8" Hybrid Cable} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{77.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.00 \& 0.82 <br>
\hline
\end{tabular}

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight

$l b$ <br>
\hline \multirow[t]{2}{*}{12' T-Arm - Round (GPD)} \& A \& From Leg \& 2.00 \& 0.0000 \& 77.00 \& No Ice \& 4.70 \& 2.33 \& 333.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.33 \& 2.96 \& 400.00 <br>
\hline
\end{tabular}

| tnxTower <br> GPD <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-3709 | Job CTNL804B AMTRAK_OldLyme5 |  | $\begin{aligned} & \text { Page } \\ & \\ & 2 \text { of } 4 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2015791.16 | $\begin{aligned} & \text { Date } \\ & \text { 08:19:12 08/28/15 } \end{aligned}$ |
|  | Client | T-Mobile Towers | Designed by tbeltz |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight

$l b$ <br>
\hline \multirow{7}{*}{$12^{\prime}$ T-Arm - Round (GPD)} \& \multirow{7}{*}{B} \& \multirow{7}{*}{From Leg} \& 0.00 \& \multirow{6}{*}{0.0000} \& \multirow{6}{*}{77.00} \& 1" Ice \& 6.00 \& 3.60 \& 467.00 <br>
\hline \& \& \& \& \& \& 2" Ice \& 6.67 \& 4.87 \& 533.00 <br>
\hline \& \& \& \& \& \& 4" Ice \& 8.33 \& 7.41 \& 600.00 <br>
\hline \& \& \& \& \& \& No Ice \& 4.70 \& 2.33 \& 333.00 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice
\] \& 5.33 \& 2.96 \& 400.00 <br>

\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 6.00 \& 3.60 \& 467.00 <br>
\hline \& \& \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 6.67 \& 4.87 \& 533.00 <br>
\hline \multirow{5}{*}{$12^{\prime}$ T-Arm - Round (GPD)} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \& \& 4 " Ice \& 8.33 \& 7.41 \& 600.00 <br>
\hline \& \& \& \& \& \& No Ice \& 4.70 \& 2.33 \& 333.00 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice
\] \& 5.33 \& 2.96 \& 400.00 <br>

\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 6.00 \& 3.60 \& 467.00 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 6.67 \& 4.87 \& 533.00 <br>
\hline \multirow{5}{*}{(2) AIR 21 w/ Mount Pipe} \& \& \& \& \& \& 4" Ice \& 8.33 \& 7.41 \& 600.00 <br>
\hline \& \& \& \& \& \& No Ice \& 6.85 \& 5.78 \& 112.90 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice
\] \& 7.41 \& 6.70 \& 170.69 <br>

\hline \& \& \& 1.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.94 \& 7.50 \& 235.28 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 9.05 \& 9.14 \& 388.12 <br>
\hline \multirow{4}{*}{(2) AIR 21 w/ Mount Pipe} \& \& \& \& \& \& 4" Ice \& 11.38 \& 12.65 \& 819.05 <br>
\hline \& \& \& \& \& \& No Ice \& 6.85 \& 5.78 \& 112.90 <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \[

1 / 2^{\prime \prime} Ice
\] \& 7.41 \& 6.70 \& 170.69 <br>

\hline \& \& \& 1.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 7.94 \& 7.50 \& 235.28 <br>
\hline \multirow{5}{*}{(2) AIR 21 w/ Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 9.05 \& 9.14 \& 388.12 <br>
\hline \& \& \& \& \& \& 4" Ice \& 11.38 \& 12.65 \& 819.05 <br>
\hline \& \& \& \& \& \& No Ice \& 6.85 \& 5.78 \& 112.90 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 7.41 \& 6.70 \& 170.69 <br>

\hline \& \& \& 1.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.94 \& 7.50 \& 235.28 <br>
\hline \multirow{5}{*}{LNX-6515DS-VTM w/ Mount Pipe} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 9.05 \& 9.14 \& 388.12 <br>
\hline \& \& \& \& \& \& 4" Ice \& 11.38 \& 12.65 \& 819.05 <br>

\hline \& \& \& \& \& \& No Ice \& 11.64 \& 9.79 \& $$
82.54
$$ <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 12.34 \& \[

11.30

\] \& \[

171.68
\] <br>

\hline \& \& \& -1.00 \& \& \& $1^{\prime \prime}$ Ice \& 13.04 \& 12.80 \& 270.74 <br>
\hline \multirow{6}{*}{LNX-6515DS-VTM w/ Mount Pipe} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 14.48 \& 15.12 \& 502.93 <br>
\hline \& \& \& \& \& \& 4" Ice \& 17.71 \& 19.94 \& 1143.89 <br>

\hline \& \& \& \& \& \& No Ice \& 11.64 \& 9.79 \& $$
82.54
$$ <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 12.34 \& 11.30 \& \[

171.68
\] <br>

\hline \& \& \& -1.00 \& \& \& 1" Ice \& 13.04 \& 12.80 \& 270.74 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& $2^{\prime \prime}$ Ice \& 14.48 \& 15.12 \& 502.93 <br>
\hline \multirow{6}{*}{LNX-6515DS-VTM w/ Mount Pipe} \& \& \& \& \& \& 4" Ice \& 17.71 \& 19.94 \& 1143.89 <br>

\hline \& \& \& \& \& \& No Ice \& 11.64 \& 9.79 \& $$
82.54
$$ <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 12.34 \& 11.30 \& $$
171.68
$$ <br>

\hline \& \& \& -1.00 \& \& \& 1" Ice \& 13.04 \& 12.80 \& 270.74 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& $2^{\prime \prime}$ Ice \& 14.48 \& 15.12 \& 502.93 <br>
\hline \& \& \& \& \& \& 4" Ice \& 17.71 \& 19.94 \& 1143.89 <br>
\hline \multirow[t]{4}{*}{KRY 11271} \& \& \& \& \& \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 0.80 \& 0.56 \& 18.38 <br>

\hline \& \& \& 1.00 \& \& \& 1" Ice \& 0.93 \& 0.68 \& 25.16 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{77.00} \& 2" Ice \& 1.22 \& 0.94 \& 44.33 <br>
\hline \multirow{4}{*}{KRY 11271} \& \& \& \& \& \& 4" Ice \& 1.90 \& 1.57 \& 110.52 <br>
\hline \& \& \& \& \& \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.80 \& 0.56 \& 18.38 <br>
\hline \& \& \& 1.00 \& \& \& 1" Ice \& 0.93 \& 0.68 \& 25.16 <br>
\hline \multirow{6}{*}{KRY 11271} \& \multirow{6}{*}{C} \& \multirow{6}{*}{From Leg} \& \& \multirow{6}{*}{0.0000} \& \multirow{6}{*}{77.00} \& 2" Ice \& 1.22 \& 0.94 \& 44.33 <br>
\hline \& \& \& \& \& \& 4" Ice \& 1.90 \& 1.57 \& 110.52 <br>
\hline \& \& \& \& \& \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.80 \& 0.56 \& 18.38 <br>
\hline \& \& \& 1.00 \& \& \& 1" Ice \& 0.93 \& 0.68 \& 25.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& 1.22 \& 0.94 \& 44.33 <br>
\hline
\end{tabular}

| tnxTower <br> GPD <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-3709 | Job $\quad$ CTNL804B AMTRAK_OldLyme5 |  | $\text { Page } 3 \text { of } 4$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2015791.16 | $\begin{aligned} & \hline \text { Date } \\ & \text { 08:19:12 08/28/15 } \\ & \hline \end{aligned}$ |
|  | Client | T-Mobile Towers | Designed by tbeltz |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& $C_{A} A_{A}$
Front

$f t^{2}$ \& $C_{A} A_{A}$
Side

$f t^{2}$ \& Weight

$l b$ <br>
\hline \multirow{6}{*}{RRUS 11 B12} \& \multirow{6}{*}{A} \& \multirow{6}{*}{From Leg} \& \& \& \& 4" Ice \& 1.90 \& 1.57 \& 110.52 <br>
\hline \& \& \& 4.00 \& 0.0000 \& 77.00 \& No Ice \& 3.31 \& 1.36 \& 50.70 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.55 \& 1.54 \& 71.57 <br>
\hline \& \& \& 1.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 95.49 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 4.33 \& 2.13 \& 153.24 <br>
\hline \& \& \& \& \& \& $4{ }^{\text {" Ice }}$ \& 5.50 \& 3.04 \& 313.85 <br>
\hline \multirow[t]{5}{*}{RRUS 11 B12} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& 0.0000 \& 77.00 \& No Ice \& 3.31 \& 1.36 \& 50.70 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.55 \& 1.54 \& 71.57 <br>
\hline \& \& \& 1.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 95.49 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 4.33 \& 2.13 \& 153.24 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 5.50 \& 3.04 \& 313.85 <br>
\hline \multirow[t]{5}{*}{RRUS 11 B12} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& 0.0000 \& 77.00 \& No Ice \& 3.31 \& 1.36 \& 50.70 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.55 \& 1.54 \& 71.57 <br>
\hline \& \& \& 1.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 95.49 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 4.33 \& 2.13 \& 153.24 <br>
\hline \& \& \& \& \& \& 4" Ice \& 5.50 \& 3.04 \& 313.85 <br>
\hline
\end{tabular}

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation <br> ft |  | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist |  | Radius of Curvature $f t$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 77.00 |  | 12' T-Arm - Round (GPD) | 35 | 4.128 | 0.4680 |  | 0.0001 | 34994 |  |
| Compression Checks |  |  |  |  |  |  |  |  |  |
| Pole Design Data |  |  |  |  |  |  |  |  |  |
| Section <br> No. | Elevation <br> ft | Size | $L$ $L_{u}$ <br> $f t$ $f t$ | $K l / r$ | $\begin{aligned} & F_{a} \\ & k s i \end{aligned}$ | A $i n^{2}$ | $\begin{gathered} \text { Actual } \\ P \\ l b \end{gathered}$ | $\begin{gathered} \text { Allow. } \\ P_{a} \\ l b \end{gathered}$ | Ratio $P$ $P_{a}$ |
| $\begin{aligned} & \text { L1 } \\ & \text { L2 } \\ & \text { L3 } \end{aligned}$ | $\begin{gathered} 80-55(1) \\ 55-43(2) \\ 43-1(3) \end{gathered}$ | TP25.42x20x0.1875 TP28.03x25.42x0.1875 TP36.77x26.8938x0.3125 | 25.00 79.00 <br> 12.00 79.00 <br> 45.50 79.00 | $\begin{gathered} 105.8 \\ 98.6 \\ 73.2 \end{gathered}$ | $\begin{aligned} & 13.333 \\ & 15.358 \\ & 23.791 \end{aligned}$ |  | $\begin{aligned} & -3226.59 \\ & -3766.74 \\ & -9275.65 \end{aligned}$ | $\begin{aligned} & 200207.00 \\ & 247517.00 \\ & 860301.00 \end{aligned}$ | $\begin{aligned} & 0.016 \\ & 0.015 \\ & 0.011 \end{aligned}$ |
| Pole Bending Design Data |  |  |  |  |  |  |  |  |  |
| Section No. | Elevation <br> ft | Size | $\begin{gathered} \text { Actual } \\ M_{x} \\ l b-f t \end{gathered}$ | Actual <br> $f_{b x}$ <br> ksi | Allow. Ratio <br> $F_{b x}$ $f_{b x}$ <br>  $F_{b x}$ | Actual $M_{y}$ $l b-f t$ | Actual <br> $f_{\text {by }}$ <br> ksi | Allow. <br> $F_{b y}$ <br> ksi | Ratio $\frac{f_{b y}}{F_{b y}}$ |
| L1 | 80-55 (1) | TP25.42x20x0.1875 | 143232.50 | 18.375 | $39.000 \quad 0.471$ | 0.00 | 0.000 | 39.000 | 0.000 |
| L2 | 55-43 (2) | TP28.03x25.42x0.1875 | 208588.33 | 23.219 | $39.000 \quad 0.595$ | 0.00 | 0.000 | 39.000 | 0.000 |
| L3 | 43-1 (3) | TP36.77x26.8938x0.3125 | 658614.17 | 24.312 | $39.000 \quad 0.623$ | 0.00 | 0.000 | 39.000 | 0.000 |


| tnxTower <br> GPD <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-3709 | Job CTNL804B AMTRAK_OldLyme5 |  | $\begin{aligned} & \text { Page } \\ & \\ & 4 \text { of } 4 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2015791.16 | $\begin{aligned} & \text { Date } \\ & \text { 08:19:12 08/28/15 } \end{aligned}$ |
|  | Client | T-Mobile Towers | Designed by tbeltz |

## Pole Shear Design Data

| Section No. | Elevation <br> $f t$ | Size | Actual V $l b$ | Actual $f_{v}$ ksi | Allow. $F_{v}$ ksi | $\begin{gathered} \hline \text { Ratio } \\ f_{v} \\ \hline F_{v} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Actual } \\ T \\ l b-f t \\ \hline \end{gathered}$ | Actual $f_{v t}$ ksi | Allow. <br> $F_{v t}$ <br> ksi | $\begin{gathered} \hline \text { Ratio } \\ f_{v t} \\ \hline F_{v t} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 80-55 (1) | TP25.42x20x0.1875 | 7350.02 | 0.489 | 26.000 | 0.038 | 0.00 | 0.000 | 26.000 | 0.000 |
| L2 | 55-43 (2) | TP28.03x25.42x0.1875 | 8030.56 | 0.498 | 26.000 | 0.038 | 0.00 | 0.000 | 26.000 | 0.000 |
| L3 | 43-1 (3) | TP36.77x26.8938x0.3125 | 11865.70 | 0.328 | 26.000 | 0.025 | 0.00 | 0.000 | 26.000 | 0.000 |

## Pole Interaction Design Data



## Section Capacity Table

| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F * P_{\text {allow }} \\ l b \end{gathered}$ | \% Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 80-55 | Pole | TP25.42x20x0.1875 | 1 | -3226.59 | 266875.92 | 36.6 | Pass |
| L2 | 55-43 | Pole | TP28.03x25.42x0.1875 | 2 | -3766.74 | 329940.15 | 45.8 | Pass |
| L3 | 43-1 | Pole | TP36.77x26.8938x0.3125 | 3 | -9275.65 | 1146781.19 | 47.6 | Pass |
|  |  |  |  |  |  | $\begin{aligned} & \text { Pole (L3) } \\ & \text { RATING = } \end{aligned}$ | $\begin{gathered} \text { Summary } \\ 47.6 \\ \mathbf{4 7 . 6} \end{gathered}$ | Pass Pass |

## APPENDIX C

## Tower Elevation Drawing

DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| 12' T-Arm - Round (GPD) | 77 | LNX-6515DS-VTM w/ Mount Pipe | 77 |  |  |
| 12' T-Arm - Round (GPD) | 77 | KRY 112 71 | 77 |  |  |
| 12' T-Arm - Round (GPD) | 77 | KRY 112 71 | 77 |  |  |
| (2) AIR 21 w/ Mount Pipe | 77 | KRY 112 71 | 77 |  |  |
| (2) AIR 21 w/ Mount Pipe | 77 | RRUS 11 B12 | 77 |  |  |
| (2) AIR 21 w/ Mount Pipe | 77 | RRUS 11 B12 | 77 |  |  |
| LNX-6515DS-VTM w/ Mount Pipe | 77 | RRUS 11 B12 | 77 |  |  |
| LNX-6515DS-VTM w/ Mount Pipe | 77 |  |  |  |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A572-65 | 65 ksi | 80 ksi |  |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in New London County, Connecticut.
2. Tower designed for a 104 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: $47.6 \%$



TORQUE $43 \mathrm{lb}-\mathrm{ft}$ 38 mph WIND - 0.7500 in ICE

AXIAL
9283 lb


TORQUE $82 \mathrm{lb}-\mathrm{ft}$ REACTIONS - 104 mph WIND

GPD
520 South Main Street, Suite 2531
Akron, OH 44311
Phone: (330) 572-2100
FAX: (330) 572-3709
${ }^{\text {Iob: }}$ CTNL804B AMTRAK_OIdLyme5 Project: 2015791.16

| Client: T-Mobile Towers | Drawn by: tbeltz | App'd: |
| :--- | :--- | :--- |
| Code: TIA/EIA-222-F | Date: $08 / 28 / 15$ | Scale: NTS |
| Path: |  | Dwg No. E-1 |



FEEDLINE PLAN
NOT TO SCALE


## APPENDIX D

Flange Plate Analysis


| Acceptable Stress Ratio |  |
| ---: | ---: |
|  | $=100.0 \%$ |
|  |  |



| UpperStiffeners |  |  |  |
| :---: | :--- | :---: | :---: |
| Configuration $=1 \quad$ None |  |  |  |


| Lower Flange Plate |  |
| :---: | :---: |
| Location = | External |
| Plate Strength $\left(\mathrm{F}_{\mathrm{y}}\right)=$ | 60 ksi |
| Plate Thickness = | 1 in |
| Outer Diameter $=$ | 32.625 in |
| wcalc = | 12.61 in |
| wmax = | 18.77 in |
| w = | 12.61 in |
| $S=$ | 2.10 in^3 |
| $\mathrm{f}_{\mathrm{b}}=$ | 17.41 ksi |
| $\mathrm{F}_{\mathrm{b}}=$ | 60 ksi |
| LP Capacity = | 29.0\% OK |


| Lower Stiffeners |  |  |
| :---: | :---: | :---: |
| Configuration $=1 \quad$ None |  |  |

GPD Flange Plate Stress (Rev F) - V1.08

## APPENDIX E

Anchor Rod \& Base Plate Analysis



Anchor Rod and Base Plate Stresses CTNL804B AMTRAK _ Old Lyme5
2015791.16

GPD GROUP


GPD Unstiffened Square Base Plate Stress (Rev F) - V2.07

## APPENDIX F

Foundation Analysis

Mat Foundation Analysis
CTNL804B AMTRAK _ Old Lyme5
2015791.16

| General Info |  |
| :---: | :---: |
| Code | TIA/EIA-222-F (ASD) |
| Bearing On | Soil |
| Foundation Type | Mono Pad |
| Pier Type | Round |
| Reinforcing Known | Yes |
| Max Capacity | 1 |


| Bearing Summary |  |  | Load Case |
| :---: | :---: | :---: | :---: |
| Qxmax | 1.31 | ksf | 1D+1W |
| Qymax | 1.31 | ksf | 1D+1W |
| Qmax @ 45 | 1.62 | ksf | 1D+1W |
| $\mathrm{Q}_{\text {(all) Gross }}$ | 3.34 | ksf |  |
| trolling Capacity | 48.6\% | Pass |  |


| Tower Reactions |  |
| :---: | :---: |
| Moment, M | $658.61 \mathrm{k}-\mathrm{ft}$ |
| Axial, P | 9.28 k |
| Shear, V | 11.86 k |


| Overturning Summary (Required $\mathbf{F S}=\mathbf{1 . 5}$ ) |  | Load Case |  |  |
| :---: | :---: | :---: | :---: | :---: |
| FS(ot)x | 4.18 | $\geq 1.5$ | $1 \mathrm{D}+1 \mathrm{~W}$ |  |
| $\mathrm{FS}(\mathrm{ot}) \mathrm{y}$ | 4.18 | $\geq 1.5$ | 1D+1W |  |
| Controlling Capacity | $\mathbf{3 5 . 9 \%}$ | Pass |  |  |


| Pad \& Pier Geometry |  |  |
| :---: | :---: | :---: |
| Pier Diameter, $\varnothing$ | 5.5 | ft |
| Pad Length, L | 18.5 | ft |
| Pad Width, W | 18.5 | ft |
| Pad Thickness, t | 1.5 | ft |
| Depth, D | 5.6 | ft |
| Height Above Grade, HG | 1 | ft |



| Pad \& Pier Reinforcing |  |  |
| :---: | :---: | :--- |
| Rebar Fy | 60 | ksi |
| Concrete Fc' | 4 | ksi |
| Clear Cover | 3 | in |
| Reinforced Top \& Bottom? | Yes |  |
| Pad Reinforcing Size | $\# 8$ |  |
| Pad Quantity Per Layer | 20 |  |
| Pier Rebar Size | $\# 7$ |  |
| Pier Quantity of Rebar | 30 |  |


| Soil Properties |  |
| :---: | :---: |
| Soil Type | Granular |
| Soil Unit Weight | 120 pcf |
| Angle of Friction, $\varnothing$ | $30^{\circ}$ |
| Bearing Type | Net |
| Ultimate Bearing | 6 ksf |
| Water Table Depth | 99 ft |
| Frost Depth | 3.5 ft |



GPD Mat Foundation Analysis - V1.02

Base Foundation Reinforcement Check CTNL804B AMTRAK _ Old Lyme5
2015791.16

| Tower Reactions |  |
| :---: | :---: |
| Moment | $658.61 \mathrm{k}-\mathrm{ft}$ |
| Axial | 9.28 k |
| Shear | 11.86 k |


| Pad \& Pier Geometry |  |
| :---: | ---: |
| Height | 5.6 ft |
| Height above Grade | 1 ft |
| Pad Length, L | 18.5 ft |
| Pad Width, W | 18.5 ft |
| Pad Thickness | 1.5 ft |
| Pier Shape | Round |
| Round Pier Diameter | 5.5 ft |


| Pad \& Pier Reinforcing |  |
| :---: | :---: |
| Reinforcing Known | Yes |
| $\mathrm{f}_{\mathrm{c}}{ }^{\prime}$ | 4 ksi |
| Clear Cover | 3 in |
| Rebar Fy | 60 ksi |
| Reinforced Top \& Bottom? | Yes |
| Pad Rebar Size | $\# 8$ |
| Pad Rebar Quantity | 20 |
| Pier Rebar Size | $\# 7$ |
| Pier Rebar Quantity | 30 |


| Unit Weights |  |
| :---: | :--- |
| Concrete Unit Weight | 150 pcf |
| Soil Unit Weight | 120 pcf |


| Orthogonal Bearing |  |
| :---: | :---: |
| $\mathrm{Q}_{\max }$ | 1.53 ksf |
| $\mathrm{Q}_{\min }$ | 0.01 ksf |


| Pad Moment Capacity |  |  |
| :---: | :---: | :---: |
| $\mathrm{M}_{\mathrm{u}}=$ | $8.87 \mathrm{k}-\mathrm{ft}$ |  |
| $\phi \mathrm{M}_{\mathrm{n}}=$ | $49.47 \mathrm{k}-\mathrm{ft}$ |  |
| Moment Capacity | $17.9 \%$ | OK |
| One-Way (Wide-Beam) Shear |  |  |
| $\mathrm{V}_{\mathrm{u}}=$ | 37.50 kips |  |
| $\phi \mathrm{V}_{\mathrm{n}}=$ | 284.32 kips |  |
| Shear Capacity | $13.2 \%$ | OK |
| $T$ wo-Way (Punching) Shear |  |  |
| $\mathrm{V}_{\mathrm{u}}=$ | 196.15 kips |  |
| $\phi \mathrm{V}_{\mathrm{n}}=$ | 714.60 kips |  |
| Shear Capacity | $27.4 \%$ | OK |
| Pier Compression |  |  |
| $\mathrm{P}_{\mathrm{u}}=$ | 12.06 kips |  |
| $\phi \mathrm{P}_{\mathrm{n}}=$ | 6578.45 kips |  |
| Compression Capacity | $0.2 \%$ | OK |


| Overall Capacities |  |  |
| :---: | :---: | :---: |
| Reinforcement Capacity | $27.4 \%$ | OK |
| As Min Met? | Yes |  |
| Controlling Capacity | $\mathbf{2 7 . 4 \%}$ | OK |




Base Foundation Reinforcement - V1.09

