# JULIE D. KOHLER 

please reply to: Bridgeport WRITER'S DIRECT DIAL: (203) 337-4157 E-Mail Address: jkohler@cohenandwolf.com

September 3, 2014

Attorney Melanie Bachman<br>Acting Executive Director<br>Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051

## Re: Notice of Exempt Modification <br> Florida Tower Partners/ T-Mobile co-location <br> Site ID CTNH522A <br> 50 Devine Street, North Haven CT

Dear Attorney Bachman:
This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, Florida Tower Partners owns the existing monopole telecommunications tower and related facility at 50 Devine Street, North Haven, Connecticut (Latitude: 41.377810, Longitude: -72.8762). T-Mobile intends to add three antennas and related equipment at this existing telecommunications facility in North Haven ("North Haven Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the First Selectman Michael J. Freda, and the property owner, 424 Chapel Street LLC.

The existing North Haven Facility consists of a 130 foot monopole tower. ${ }^{1}$ T-Mobile plans to add three antennas and three remote radio units ("RRU") on T-arm mounts at a centerline of 117 feet. (See the plans revised to August 14, 2014 attached hereto as Exhibit A). T-Mobile will also add an equipment cabinet mounted to an existing railing within the compound and reuse existing coax cables. The existing North Haven Facility is structurally capable of supporting T-Mobile's proposed modifications, as indicated in the structural analysis dated August 25, 2014 and attached hereto as Exhibit B.

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Site ID CTNH522A
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The planned modifications to the North Haven Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the height of the tower. T-Mobile's additional antennas and PRUs will be installed at a centerline of 117 feet. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.
2. The proposed modifications will not require an extension of the site boundaries or lease area, as depicted on Sheets 4 of Exhibit A. T-Mobile's equipment will be located entirely within the existing compound area.
3. The proposed modification to the North Haven Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the replacement antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated September 2, 2014, T-Mobile's operations would add $9.79 \%$ of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be $48.12 \%$ of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, T-Mobile respectfully submits that the proposed replacement antennas and equipment at the North Haven Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,

cc: Town of North Haven, First Selectman Michael J. Freda
424 Chapel Street LLC
Florida Tower Partners
Sheldon Freincle, NSS



KEY PLAN
N.T.S.

## CONFIGURATION 704CU

| SUBMITTALS |  |
| :--- | :--- |
| LE REVA | 08.14 .14 |
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|  |  |

- tlantis

G R O U P
1340 Centre Street Suite 212
Newton, MA 02459 Office: 617-965-0789 Fax: 617-213-5056

LEASE EXHIBIT
SITE NUMBER:
CTNH522A
SITE NAME:
FLORIDA PARTNERS NORTH HAVEN
MONOPOLE
SITE ADDRESS:
50 DEVINE ST, NORTH HAVEN, CT

NORTHEAST SITE SOLUTIONS
54 MAIN STREET, UNIT 3 STURBRIDGE, MA 01566
(508) 434-5237
for
T-MOBILE NORTHEAST, LLC
35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 OFFICE: (860) 692-7100 FAX: (860) 692-7159




## EXISTING EQUIPMENT



| SUBMITTALS |  | 1340 Centre Street Suite 212 <br> Newton, MA 02459 <br> Office: 617-965-0789 <br> Fax: 617-213-5056 | LEASE EXXHIBITSTE NUMBER:CTNH522ASTE NAME:FLORIDA PARTNERS NORTH HAVENMONOPOLESITE ADDRESS:5ODEVINE ST,NORTH HAVEN, CT |  | NORTHEAST SITE SOLUTIONS 54 MAIN STREET, UNIT 3 STURBRIDGE, MA 01566 <br> (508) 434-5237 <br> FOR <br> T-MOBILE NORTHEAST, LLC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LE REV A | 08.14.14 |  |  |  |  |
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|  |  |  |  |  |  |
|  |  |  |  |  | 35 GRIFFIN ROAD SOUTH |
|  |  |  |  |  | BLOOMFIELD, CT 06002 |
|  |  |  |  |  | OFFICE: (860) 692-7100 <br> FAX: (860) 692-7159 |
|  |  |  | DRAWN BY: MB | CHECKED BY:SM | PAGE 4OF 5 |




# Structural Analysis 130-ft Monopole 

Prepared For:<br>Florida Tower Partners, LLC<br>$10013^{\text {rd }}$ Ave. West, Suite 420<br>Bradenton, FL 34205<br>MFP Project \#40914-090<br>Site Location:<br>CT1003 North Haven<br>New Haven Co., Connecticut<br>Lat/Long: $41^{\circ} 22^{\prime} 40.1^{\prime \prime},-72^{\circ} 52$ '34.1"

Analysis Type:<br>ANSI/TIA-222-G<br>Structure Rating: 85.5\% Passing

August 25, 2014


Michael F , Plahovinsak, P.E.
18301 State Route I61 W, Plain City, OH 43064
614-398-6250-mike@mfpena, com

Project Summary:

We have completed a structural analysis of the existing monopole for the proposed configuration:

> MetroPCS/T-Mobile - 117' -

- (6) Ericsson AIR-21 Panel + (3) Andrew LNX-6515DS Panel
- (3) Ericsson RRUS11-B-12 RRU
- \& (12) $15 / 8$ " on T-Arm Mounts

The pole has been analyzed in accordance with the requirements of the 2006-2012 International Building Code, and the recommendations of the Telecommunications Industry Association "Structural Standard for Steel Antenna Supporting Structures" ANSI/TIA-222-G.

This analysis may be considered a "Rigorous Structural Analysis" as defined in ANSI/TIA-222-G 15.5.2.

As indicated in the conclusions of this analysis, we have determined that the existing pole and foundation have sufficient capacity to support the existing, reserved and proposed antenna loads as detailed herein. Based on the results of our analysis, structural modifications are not required at this time.

Source of Data:

| Resource | Source | Job Number | Date |
| :---: | :---: | :---: | :---: |
| Pole and Foundation Drawings | Sabre Towers | $11-05062$ | $05 / 12 / 10$ |
| Geotechnical Report | Terracon | J2105136 | $04 / 20 / 10$ |

## Analysis Criteria:

International Building Code (All Versions) Section 3108.4
Structural Standards for Steel Antenna Supporting Structures ANSI/TIA-222-G 2

- Basic Wind Speed
- Basic Wind Speed w/ 3/4" Ice
- Operational Wind Speed

115 mph (3-Sec Gust)
50 mph (3-Sec Gust)
60 mph (3-Sec Gust)

| Structure Class | Exposure Category | Topographic Category |
| :---: | :---: | :---: |
| $\mathrm{II}(\mathrm{I}=1.0)$ | C | I |

Michael F, Plahovinsak, P.E. - 2014

Appurtenance Listing:

| Status | Elev. | Antenna / Mounting | Coax | Owner |
| :---: | :---: | :---: | :---: | :---: |
| Existing | $130^{\prime}$ | (1) Antel BXA-70080/6CF + (1) BXA-80080/6CF <br> (4) Antel BXA-70063/6CF + (6) BXA-171063/12CF <br> (6) Lucent 2x40 RRH's \& (1) Distribution Box 12' Low Profile Platform | (12) $15 / 8^{\prime \prime}$ | Verizon |
| Proposed | $117^{\prime}$ | (6) Ericsson AIR-21 + (3) Andrew LNX-6515DS Panel <br> (3) Ericsson RRUS11-B12 RRU <br> 12' T-Arm Mounts | (12) $15 / 8^{\prime \prime}$ | MetroPCS |
| Existing | $107^{\prime}$ | (12) CCI HPA-65R-BUU-H8 Panel <br> (9) RRUS-11 + (6) RRUS-12 + (6) RRUS-32 + (6) RRUS-A2 <br> (4) Raycap DC6-48-60-18-8F Suppressor <br> 12' T-Arm Mounts | (8) $3 / 4^{\prime \prime}+$ <br> (2) $1 / 2^{\prime \prime}+$ <br> (3) $3 / 8^{\prime \prime}$ | AT\&T |

All antenna lines assumed internally mounted, not exposed to the wind.

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Foundation Analysis:
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The existing monopole foundation design was analyzed in conjunction with site specific geotechnical report. The existing foundation has sufficient capacity to support the pole with the proposed antenna configuration.

## Conclusion:

We have completed a structural analysis of the existing monopole and foundation in accordance with the project specifics outlined above. Our analysis indicates that the existing monopole and foundation is stressed to a maximum of $85.5 \%$ of its usable capacity when considering the existing plus proposed loading. Please refer to the attached calculations for an itemized listing of all member stress ratios. The existing pole is safe and adequate to support the proposed loads, and no structural reinforcing is required to support the above loading.

If you have any questions about the contents of this structural report or require any additional information, please feel free to contact my office.

Sincerely,

## Michael F. Plahovinsak, P.E.



Michael F, Plahovinsak, P.E. -2014

## Standard Conditions for Providing Structural Consulting Services on Existing Structures

1. The following standard conditions are a general overview of key issues regarding the work product supplied.
2. If the existing conditions are not as represented in this structural report or attached sketches, we should be contacted to evaluate the significance of the deviation and revise the structural assessment accordingly.
3. The structural analysis has been performed assuming that the structure is in "like new" condition. No allowance was made for excessive corrosion, damaged or missing structural members, loose bolts, etc. If there are any known deficiencies in the structure that potentially compromise structural integrity, we should be made aware of the deficiencies. If we are aware of a deficiency that exists in a structure at the time of our analysis, a general explanation of the structural concern due to the deficiency will be included in the structural report, but the deficiency will not be reflected in capacity calculations.
4. The structural analysis provided is an assessment of the primary load carrying capacity of the structure. We provide a limited scope of service in that we have not verified the capacity of every weld, plate, connection detail, etc. In most cases, structural fabrication details are unknown at the time of our analysis, and the detailed field measurement of this information is beyond the scope of our services. In instances where we have not performed connection capacity calculations, it is assumed that existing manufactured connections develop the full capacity of the primary members being connected.
5. The structural integrity of the existing foundation system can only be verified if exact foundation sizes and soils conditions are known. We will not accept any responsibility for the adequacy of the existing foundations unless this site-specific data is supplied.
6. Miscellaneous items such as antenna mounts, coax supports, etc. have not been designed, detailed, or specified as part of our work. It is assumed that material of adequate size and strength will be purchased from a reputable component manufacturer. The attached report and sketches are schematic in nature and should not be used to fabricate or purchase hardware and accessories to be attached to the structure. We recommend field measurement of the structure before fabricating or purchasing new hardware and accessories. We are not responsible for proper fit and clearance of hardware and accessory items in the field.
7. The structural analysis has been performed considering minimum code requirements or recommendations. If alternate wind, ice, or deflection criteria are to be considered, then We shall be made aware of the alternate criteria.

Michael F, Plahovirsak, P., , -2014
mike@mfpeng.com

1.0 ft

ALL REACTIONS ARE FACTORED


TORQUE 0 kip-ft 50 mph WIND - 0.7500 in ICE


TORQUE 1 kip-ft
REACTIONS - 115 mph WIND

DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| (2) Antel BXA-70063/0CF w/mount pipe (Verizon) | 130 | (2) Ericsson AlR 21 w/ mount pipe (MetropCS /T-Mobile) | 117 |
| (2) Antel BXA-171063/12CF w/mount pipe (Verizon) | 130 | Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS./T-Mobile) | 117 |
| (2) Lucent $2 \times 40$ RRH (Verizon) | 130 | Ericsson RRUS11 B12 (MetroPCS /T-Mobile) | 117 |
| (2) Antel BXA-70063/6CF w/ mount pipe (Verizon) | 130 |  |  |
|  |  | 12 T-Arm Mounts (MetropCS/T-Mobile) | 117 |
| (2) Antel BXA-171063/12CF w/ mount pipe (Verizon) | 130 |  |  |
| (2) Lucent $2 \times 40$ RRH (Verizon) | 130 | (4) CCI HPA-65R-BLUU-H8 w/ mount pipe (ATT) | 107 |
| Antel BXA-70080-6CF w/ mount pipe (Verizon) | 130 | (3) Ericsson RRUS-11 (ATT) | 107 |
|  |  | (2) Ericsson RRUS 12 (ATT) | 107 |
| Antel BXA-80080/6CF w/ mount pipe (Verizon) | 130 | (2) Ericsson RRUS-32 (ATT) | 107 |
|  |  | (2) Ericsson RRUS A2 (ATT) | 107 |
| (2) Antel BXA-171063/12CF w/ mount pipe (Verizon) | 130 | (4) CCI HPA-65R-BUU-H8 w/ mount pipe (ATT) | 107 |
| (2) Lucent $2 \times 40$ RRH (Verizon) | 130 | (3) Ericsson RRUS-11 (ATT) | 107 |
| RFS DB-T1-6Z-8AB-OZ Box (Verizon) | 130 | (2) Ericsson RRUS 12 (ATT) | 107 |
| 12' Low Profile Platform (Verizon) | 130 | (2) Ericsson RRUS-32 (ATT) | 107 |
| (2) Ericsson AIR 21 w/ mount pipe (MetroPCS / T-Mobile) | 117 | (2) Ericsson RRUS A2 (ATT) | 107 |
| Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS /T-Mobile) | 117 | (4) CCl HPA-65R-BUU-H8 w/ mount pipe (ATT) | 107 |
|  |  | (3) Ericsson RRUS-11 (ATT) | 107 |
| Ericsson RRUS11 B12 (MetroPCS / | 117 | (2) Ericsson RRUS 12 (ATT) | 107 |
| (2) Eriosson AIR 21 w/ mount pipe | 117 | (2) Ericsson RRUS-32 (ATT) | 107 |
| (MetroPCS / T-Mobile) |  | (2) Ericsson RRUS A2 (ATT) | 107 |
| Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS /T-Mobile) | 117 | (4) Raycap DC6-48-60-18-8F Supressor (ATT) | 107 |
| Ericsson RRUS11 B12 (MetroPCS / | 117 | 12' T-Arm Mounts (ATT) | 107 |

MATERIAL STRENGTH
MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A $572-65$ | 65 ksi | 80 ksi |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 115 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $80.8 \%$

Michael F. Plahovinsak, P.E.
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Phone: 614-398-6250 FAX: mike@mfpeng.com


## Tower Input Data

This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in New Haven County, Connecticut.
Basic wind speed of 115 mph .
Structure Class II.
Exposure Category C.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 0.7500 in .
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

| Tapered Pole Section Geometry |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation $f t$ $\qquad$ | Section Length $f t$ | Splice Length $f t$ | Number of Sides | Top <br> Diameter <br> in | Bottom Diameter in | Wall Thickness in | Bend <br> Radius <br> in | Pole Grade |
| L1 | 130.00-120.00 | 10.00 | 0.00 | 18 | 20.9000 | 23.1600 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | 120.00-91.50 | 28.50 | 4.25 | 18 | 23.1600 | 29.6000 | 0.2500 | 1.0000 | A572-65 $(65 \mathrm{ksi})$ |
| L3 | 91.50-48.25 | 47.50 | 5.50 | 18 | 28.1396 | 38.8700 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 48.25-1.00 | 52.75 |  | 18 | 36.8775 | 48.8000 | 0.4375 | 1.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

Tapered Pole Properties

| Section | Tip Dia. <br> in | Area <br> $i n^{2}$ | $I$ <br> $\mathrm{~m}^{4}$ | $r$ <br> in | $C$ <br> in | $I / C$ <br> $i n^{3}$ | $J$ <br> $i n^{4}$ | $I t / Q$ <br> $i n^{2}$ | $w$ <br> in | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 21.2224 | 12.3265 | 668.1027 | 7.3529 | 10.6172 | 62.9264 | 1337.0845 | 6.1644 | 3.3484 | 17.858 |
|  | 23.5173 | 13.6715 | 911.5289 | 8.1552 | 11.7653 | 77.4762 | 1824.2571 | 6.8371 | 3.7462 | 19.98 |
| L2 | 23.5173 | 18.1791 | 1205.4790 | 8.1331 | 11.7653 | 102.4607 | 2412.5442 | 9.0913 | 3.6362 | 14.545 |
|  | 30.0566 | 23.2892 | 2534.5957 | 10.4193 | 15.0368 | 168.5595 | 5072.5265 | 11.6468 | 4.7696 | 19.078 |
| L3 | 29.5486 | 33.0469 | 3218.4903 | 9.8565 | 14.2949 | 225.1489 | 6441.2155 | 16.5266 | 4.2926 | 11.447 |
|  | 39.4696 | 45.8187 | 8578.0508 | 13.6657 | 19.7460 | 434.4205 | 17167.3888 | 22.9137 | 6.1811 | 16.483 |
| L4 | 38.7087 | 50.6015 | 8489.0461 | 12.9362 | 18.7338 | 453.1409 | 16989.2624 | 25.3056 | 5.7204 | 13.075 |
|  | 49.5528 | 67.1574 | 19844.8883 | 17.1687 | 24.7904 | 800.5070 | 39715.8890 | 33.5851 | 7.8188 | 17.872 |



## Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Component Type | $f$ | Total <br> Number |  | $C_{A} A_{A}$ $f^{2} / f t$ | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $15 / 8^{\prime \prime}$ | C | No | Inside Pole | 130.00-1.00 | 12 | No Ice | 0.00 | 0.92 |
| (Verizon) |  |  |  |  |  | 1/2" Ice | 0.00 | 0.92 |
|  |  |  |  |  |  | 1" Ice | 0.00 | 0.92 |
| *** |  |  |  |  |  |  |  |  |
| $15 / 8^{\prime \prime}$ | C | No | Inside Pole | 117.00-1.00 | 12 | No Ice | 0.00 | 0.92 |
| (MetroPCS / T-Mobile) |  |  |  |  |  | $1 / 2^{\prime \prime}$ Ice | 0.00 | 0.92 |
|  |  |  |  |  |  | 1 " Ice | 0.00 | 0.92 |
| ** |  |  |  |  |  |  |  |  |
| 3/4" | C | No | Inside Pole | 107.00-1.00 | 8 |  | 0.00 | 0.33 |
| (ATT) |  |  |  |  |  | $1 / 2^{\prime \prime} \text { Ice }$ | 0.00 | 0.33 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.33 |
| 1/2" | C | No | Inside Pole | 107.00-1.00 | 2 | No Ice | 0.00 | 0.15 |
| (ATT) |  |  |  |  |  | $1 / 2^{\prime \prime}$ Ice | 0.00 | 0.15 |
|  |  |  |  |  |  | 1" Ice | 0.00 | 0.15 |
| $3 / 8^{\prime \prime}$ | C | No | Inside Pole | 107.00-1.00 | 3 | No Ice | 0.00 | 0.08 |
| (ATT) |  |  |  |  |  | $1 / 2^{\prime \prime}$ Ice | 0.00 | 0.08 |
|  |  |  |  |  |  | 1" Ice | 0.00 | 0.08 |


| Discrete Tower Loads |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Off sets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f_{t}$ | Azimuth Adjustment <br> 0 | Placement <br> $f t$ |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A} A_{A}$ Side <br> $f t^{2}$ | Weight K |
| (2) Antel BXA-70063/6CF w/ mount pipe (Verizon) | A | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\prime \prime}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 7.75 \\ & 8.29 \\ & 8.85 \end{aligned}$ | $\begin{aligned} & 5.18 \\ & 6.11 \\ & 6.92 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.09 \\ & 0.16 \end{aligned}$ |
| (2) Antel BXA-171063/12CF <br> $\mathrm{w} /$ mount pipe (Verizon) | A | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice 1/2" Ice $1^{\prime \prime}$ Ice | $\begin{array}{r} 4.98 \\ 5.43 \\ 5.89 \end{array}$ | $\begin{aligned} & 5.93 \\ & 6.87 \\ & 7.69 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.08 \\ & 0.14 \end{aligned}$ |
| (2) Lucent $2 \times 40$ RRH (Verizon) | A | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\text {" }}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 1.20 \\ & 1.35 \\ & 1.51 \end{aligned}$ | $\begin{aligned} & 2.25 \\ & 2.45 \\ & 2.66 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \\ & 0.05 \end{aligned}$ |
| (2) Antel BXA-70063/6CF w/ mount pipe (Verizon) | B | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\prime \prime}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 7.75 \\ & 8.29 \\ & 8.85 \end{aligned}$ | $\begin{aligned} & 5.18 \\ & 6.11 \\ & 6.92 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.09 \\ & 0.16 \end{aligned}$ |
| (2) Antel BXA-171063/12CF w/ mount pipe (Verizon) | B | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\prime \prime}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 4.98 \\ & 5.43 \\ & 5.89 \end{aligned}$ | $\begin{aligned} & 5.93 \\ & 6.87 \\ & 7.69 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.08 \\ & 0.14 \end{aligned}$ |
| (2) Lucent $2 \times 40$ RRH (Verizon) | B | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice <br> $1 / 2^{2}$ Ice <br> " Ice | $\begin{aligned} & 1.20 \\ & 1.35 \\ & 1.51 \end{aligned}$ | $\begin{aligned} & 2.25 \\ & 2.45 \\ & 2.66 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \\ & 0.05 \end{aligned}$ |
| Antel BXA-70080-6CF w/ mount pipe (Verizon) | C | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\text {" }}$ Ice 1" Ice | $\begin{aligned} & 5.79 \\ & 6.25 \\ & 6.71 \end{aligned}$ | $\begin{aligned} & 5.99 \\ & 6.93 \\ & 7.74 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.09 \\ & 0.15 \end{aligned}$ |
| Antel BXA-80080/6CF w/ mount pipe (Verizon) | C | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\prime \prime}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 5.79 \\ & 6.25 \\ & 6.71 \end{aligned}$ | $\begin{aligned} & 5.99 \\ & 6.93 \\ & 7.74 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.13 \\ & 0.19 \end{aligned}$ |
| (2) Antel BXA-171063/12CF w/ mount pipe (Verizon) | C | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice $1 / 2^{\text {" }}$ Ice $1^{\prime \prime}$ Ice | $\begin{aligned} & 4.98 \\ & 5.43 \\ & 5.89 \end{aligned}$ | $\begin{aligned} & 5.93 \\ & 6.87 \\ & 7.69 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.08 \\ & 0.14 \end{aligned}$ |
| (2) Lucent $2 \times 40$ RRH (Verizon) | C | From Face | $\begin{aligned} & 3.00 \\ & 0.00 \end{aligned}$ | 0.0000 | 130.00 | No Ice <br> $1 / 2^{1}$ Ice | $\begin{aligned} & 1.20 \\ & 1.35 \end{aligned}$ | $\begin{aligned} & 2.25 \\ & 2.45 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |


| tnxTower | 130-ft Monopole - MFP \#40914-090 |  | $\begin{aligned} & \text { Page } 3 \text { of } 7 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Michael F. Plahovinsak, P.E. <br> 18301 State Route 161 W | Project | CT1003, North Haven | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 16:34:06 08/25/14 } \end{array}$ |
| Plain City, OH 43064 <br> Phone: 614-398-6250 <br> FAX: mike@mfpeng.com | Client | Florida Tower Partners | Designed by Mike |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

ft \& \& | $C_{A} A_{A}$ Front |
| :--- |
| $f t^{2}$ | \& CAAA

Side \& Weight

$K$ <br>
\hline \multirow{4}{*}{RFS DB-T1-6Z-8AB-OZ Box
(Verizon)} \& \multirow{4}{*}{C} \& \multirow{4}{*}{None} \& 0.00 \& \multirow{4}{*}{0.0000} \& \multirow{3}{*}{130.00} \& 1" Ice \& 1.51 \& 2.66 \& 0.05 <br>
\hline \& \& \& \& \& \& No Ice \& 5.60 \& 2.33 \& 0.04 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 5.92 \& 2.56 \& 0.08 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 6.24 \& 2.79 \& 0.12 <br>
\hline \multirow[t]{3}{*}{12' Low Profile Platform (Verizon)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{None} \& \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{130.00} \& No Ice \& 14.00 \& 14.00 \& 1.10 <br>
\hline \& \& \& \& \& \& $1 / 2^{\text {1 }}$ Ice \& 16.00 \& 16.00 \& 1.70 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 18.00 \& 18.00 \& 2.30 <br>
\hline \multicolumn{10}{|l|}{***} <br>

\hline \multirow[t]{3}{*}{| (2) Ericsson AIR $21 \mathrm{w} /$ mount pipe |
| :--- |
| (MetroPCS / T-Mobile) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 6.61 \& 5.50 \& 0.11 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.08 \& 6.22 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.55 \& 6.95 \& 0.22 <br>
\hline \multirow[t]{3}{*}{Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS / T-Mobile)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 11.45 \& 9.60 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 12.06 \& 11.02 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 12.69 \& 12.29 \& 0.26 <br>
\hline Ericsson RRUS11 B12 \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 3.31 \& 1.36 \& 0.06 <br>
\hline \multirow[t]{2}{*}{(MetroPCS / T-Mabile)} \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.55 \& 1.54 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 0.10 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson AIR 21 w/ mount pipe (MetroPCS / T-Mobile)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 6.61 \& 5.50 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.08 \& 6.22 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 7.55 \& 6.95 \& 0.22 <br>
\hline \multirow[t]{3}{*}{Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS / T-Mobile)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 11.45 \& 9.60 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 12.06 \& 11.02 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 12.69 \& 12.29 \& 0.26 <br>
\hline Ericsson RRUS11 B12 \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 3.31 \& 1.36 \& 0.06 <br>
\hline \multirow[t]{2}{*}{(MetroPCS / T-Mobile)} \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.55 \& 1.54 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 0.10 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson AIR 21 w/ mount pipe (MetroPCS / T-Mobile)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 6.61 \& 5.50 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.08 \& 6.22 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.55 \& 6.95 \& 0.22 <br>
\hline \multirow[t]{3}{*}{Andrew LNX-6515DS-VTM w/ mount pipe (MetroPCS / T-Mobile)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 11.45 \& 9.60 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' Ice \& 12.06 \& 11.02 \& 0.16 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 12.69 \& 12.29 \& 0.26 <br>
\hline Ericsson RRUS11 B12 \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 3.31 \& 1.36 \& 0.06 <br>
\hline \multirow[t]{2}{*}{(MetroPCS / T-Mobile)} \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.55 \& 1.54 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.80 \& 1.73 \& 0.10 <br>
\hline \multirow[t]{3}{*}{$12^{\prime}$ T-Arm Mounts (MetroPCS / T-Mobile)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{117.00} \& No Ice \& 12.00 \& 12.00 \& 1.14 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 18.00 \& 18.00 \& 1.27 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 24.00 \& 24.00 \& 0.47 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{6}{*}{| (4) CCI HPA-65R-BUU-H8 |
| :--- |
| w/ mount pipe (ATT) |
| (3) Ericsson RRUS-11 (ATT) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No Ice \& 13.62 \& 9.18 \& 0.10 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2^{11}$ Ice \& 14.35 \& 10.58 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 15.09 \& 11.83 \& 0.29 <br>
\hline \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No Ice \& 2.55 \& 0.92 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.77 \& 1.07 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.99 \& 1.23 \& 0.08 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS 12 (ATT)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No Ice \& 3.67 \& 1.46 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.92 \& 1.64 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 4.19 \& 1.84 \& 0.11 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS-32 (ATT)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No lce \& 3.87 \& 2.76 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 4.15 \& 3.02 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 4.44 \& 3.29 \& 0.14 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS A2 (ATT)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No Ice \& 1.87 \& 0.50 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.05 \& 0.62 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.24 \& 0.75 \& 0.05 <br>
\hline \multirow[t]{3}{*}{(4) CCI HPA-65R-BUU-H8 w/ mount pipe (ATT)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{107.00} \& No Ice \& 13.62 \& 9.18 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 14.35 \& 10.58 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 15.09 \& 11.83 \& 0.29 <br>
\hline
\end{tabular}



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{(3) Ericsson RRUS-11 (ATT)} \& B \& From Face \& 3.00 \& 0.0000 \& 107.00 \& No Ice \& 2.55 \& 0.92 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.77 \& 1.07 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1 Ice \& 2.99 \& 1.23 \& 0.08 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS 12 (ATT)} \& B \& From Face \& 2.50 \& 0.0000 \& 107.00 \& No Ice \& 3.67 \& 1.46 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.92 \& 1.64 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1 ' Ice \& 4.19 \& 1.84 \& 0.11 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS-32 (ATT)} \& B \& From Face \& 2.00 \& 0.0000 \& 107.00 \& No Ice \& 3.87 \& 2.76 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 4.15 \& 3.02 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 4.44 \& 3.29 \& 0.14 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS A2 (ATT)} \& B \& From Face \& 1.50 \& 0.0000 \& 107.00 \& No Ice \& 1.87 \& 0.50 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.05 \& 0.62 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.24 \& 0.75 \& 0.05 <br>
\hline \multirow[t]{3}{*}{(4) $\mathrm{CCIHPA}-65 \mathrm{R}-\mathrm{BUU}-\mathrm{H} 8$ $\mathrm{w} /$ mount pipe (ATT)} \& C \& From Face \& 3.00 \& 0.0000 \& 107.00 \& No Ice \& 13.62 \& 9.18 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 14.35 \& 10.58 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 15.09 \& 11.83 \& 0.29 <br>

\hline \multirow[t]{3}{*}{| (3) Ericsson RRUS-11 |
| :--- |
| (ATT) |} \& C \& From Face \& 3.00 \& 0.0000 \& 107.00 \& No Ice \& 2.55 \& 0.92 \& 0.05 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.77 \& 1.07 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.99 \& 1.23 \& 0.08 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS 12 (ATT)} \& C \& From Face \& 2.50 \& 0.0000 \& 107.00 \& No Ice \& 3.67 \& 1.46 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.92 \& 1.64 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 4.19 \& 1.84 \& 0.11 <br>

\hline \multirow[t]{3}{*}{| (2) Ericsson RRUS-32 |
| :--- |
| (ATT) |} \& C \& From Face \& 2.00 \& 0.0000 \& 107.00 \& No Ice \& 3.87 \& 2.76 \& 0.08 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 4.15 \& 3.02 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 4.44 \& 3.29 \& 0.14 <br>
\hline \multirow[t]{3}{*}{(2) Ericsson RRUS A2 (ATT)} \& C \& From Face \& 1.50 \& 0.0000 \& 107.00 \& No Ice \& 1.87 \& 0.50 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.05 \& 0.62 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.24 \& 0.75 \& 0.05 <br>
\hline (4) Raycap DC6-48-60-18-8F \& C \& None \& \& 0.0000 \& 107.00 \& No Ice \& 1.47 \& 1.47 \& 0.03 <br>
\hline Supressor \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.67 \& 1.67 \& 0.05 <br>
\hline (ATT) \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 1.88 \& 1.88 \& 0.07 <br>
\hline \multirow[t]{3}{*}{$12^{\prime}$ T-Arm Mounts (ATT)} \& C \& None \& \& 0.0000 \& 107.00 \& No Ice \& 12.00 \& 12.00 \& 1.14 <br>
\hline \& \& \& \& \& \& 1/2 ${ }^{11}$ Ice \& 18.00 \& 18.00 \& 1.27 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 24.00 \& 24.00 \& 0.47 <br>
\hline
\end{tabular}

## Load Combinations

| Comb. <br> No. |  |
| :--- | :--- |
| 1 | Dead Only |
| 2 | 1.2 Dead 1.6 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.6 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.6 Wind 90 deg - No Ice |
| 5 | 0.9 Dead +1.6 Wind 90 deg - No Ice |
| 6 | 1.2 Dead+1.6 Wind 180 deg - No Ice |
| 7 | 0.9 Dead+1.6 Wind 180 deg - No Ice |
| 8 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 9 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 10 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 11 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 12 | Dead+Wind 0 deg - Service |
| 13 | Dead+Wind 90 deg - Service |
| 14 | Dead+Wind 180 deg - Service |



| Maxímum Member Forces |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Condition | Gov. Load Comb. | Axial <br> $K$ | Major Axis Moment lap-ft | $\begin{gathered} \text { Minor Axis } \\ \text { Moment } \\ \text { Kip-ft } \end{gathered}$ |
| L1 | 130-120 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 8 | -8.42 | 0.00 | -0.08 |
|  |  |  | Max. Mx | 4 | -1.83 | -73.97 | -0.08 |
|  |  |  | Max. My | 6 | -1.88 | 0.00 | -70.73 |
|  |  |  | Max. Vy | 4 | 7.89 | -73.97 | -0.08 |
|  |  |  | Max. Vx | 6 | 7.55 | 0.00 | -70.73 |
|  |  |  | Max. Torque | 4 |  |  | -1.09 |
| L2 | 120-91.5 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 8 | -27.89 | 0.00 | -0.08 |
|  |  |  | Max. Mx | 4 | -9.95 | -562.79 | -0.13 |
|  |  |  | Max. My | 6 | -10.03 | 0.00 | -551.04 |
|  |  |  | Max. Vy | 4 | 29.20 | -562.79 | -0.13 |
|  |  |  | Max. Vx | 6 | 28.85 | 0.00 | -551.04 |
|  |  |  | Max. Torque | 4 |  |  | -1.09 |
| L3 | 91.5-48.25 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 8 | -39.41 | 0.00 | -0.08 |
|  |  |  | Max. Mx | 4 | -19.26 | -1895.78 | $-0.18$ |
|  |  |  | Max. My | 6 | -19.30 | $0.00$ | -1869.05 |
|  |  |  | Max. Vy | 4 | 34.26 | $-1895.78$ | $-0.18$ |
|  |  |  | Max. Vx | 6 | 33.91 | 0.00 | -1869.05 |
|  |  |  | Max. Torque | 4 |  |  | -1.09 |
| L4 | 48.25-1 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 8 | -59.35 | 0.00 | -0.08 |
|  |  |  | Max. Mx | 4 | -36.31 | $-3860.53$ | $-0.19$ |
|  |  |  | Max. My | 6 | -36.31 | 0.00 | -3815.27 |
|  |  |  | Max. Vy | 4 | 39.91 | -3860.53 | -0.19 |
|  |  |  | Max. Vx | 6 | 39.56 | 0.00 | -3815.27 |
|  |  |  | Max. Torque | 4 |  |  | -1.08 |


| Maximum |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Horz. | Gov. | Tilt | Twist |
| No. |  | Deflection | Load |  |  |
|  | $f t$ | in | Comb. | - | - |
| L1 | 130-120 | 15.383 | 13 | 1.0220 | 0.0024 |
| L2 | 120-91.5 | 13.257 | 13 | 1.0029 | 0.0016 |
| L3 | 95.75-48.25 | 8.465 | 13 | 0.8504 | 0.0007 |
| L4 | 53.75-1 | 2.581 | 13 | 0.4558 | 0.0002 |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load <br> Comb. | in | Deflection | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |



## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. <br> Load <br> Comb. | Deflection | in | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Pole Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - $f t$ |  |  | $f t$ | $f t$ |  | $i n^{2}$ | K | $K$ | фP $P_{n}$ |
| L1 | 130-120 (1) | TP23.16x20.9x0.1875 | 10.00 | 0.00 | 0.0 | 13.6715 | -1.83 | 958.52 | 0.002 |
| L2 | 120-91.5 (2) | TP29.6x23.16x0.25 | 28.50 | 0.00 | 0.0 | 22.5272 | -9.95 | 1617.01 | 0.006 |
| L3 | 91.5-48.25 (3) | TP38.87x28.1396x0.375 | 47.50 | 0.00 | 0.0 | 44.3398 | -19.26 | 3294.23 | 0.006 |
| L4 | 48.25-1 (4) | TP48.8×36.8775 $\times 0.4375$ | 52.75 | 0.00 | 0.0 | 67.1574 | -36.31 | 4858.33 | 0.007 |


|  | Pole Bendíng Design Data |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{r x}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \end{gathered}$ | $M_{u y}$ | $\phi M_{n y}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \end{gathered}$ |
|  | $f t$ |  | kip-ft | kip-ft | $\phi M_{n x}$ | $k i p-f t$ | kip-ft | $\phi M_{m p}$ |
| LI | 130-120 (1) | TP23.16×20.9×0.1875 | 73.97 | 452.66 | 0.163 | 0.00 | 452.66 | 0.000 |
| L2 | 120-91.5 (2) | TP29.6x23.16x0.25 | 562.79 | 943.10 | 0.597 | 0.00 | 943.10 | 0.000 |
| L3 | 91.5-48.25 (3) | TP38.87×28.1396x0.375 | 1895.78 | 2517.97 | 0.753 | 0.00 | 2517.97 | 0.000 |
| LA | 48.25-1 (4) | TP48.8×36.8775x0.4375 | 3860.53 | 4825.88 | 0.800 | 0.00 | 4825.88 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | K | $K$ | $\phi V_{n}$ | kip-ft | $k i p-f t$ | $\phi T_{n}$ |
| L1 | 130-120(1) | TP23.16x20.9x0.1875 | 7.89 | 479.26 | 0.016 | 1.09 | 906.43 | 0.001 |
| L2 | 120-91.5 (2) | TP29.6x23.16x0.25 | 29.20 | 808.51 | 0.036 | 1.09 | 1888.51 | 0.001 |
| L3 | 91.5-48.25 (3) | TP38.87×28.1396x0.375 | 34.26 | 1647.11 | 0.021 | 1.09 | 5042.12 | 0.000 |
| L4 | 48.25-1 (4) | TP48.8×36.8775×0.4375 | 39.91 | 2429.16 | 0.016 | 1.08 | 9663.58 | 0.000 |


| tnxTower <br> Michael F. Plahovinsak, P.E. <br> 18301 State Route 161 W | Job 130-ft Monopole - MFP \#40914-090 |  | Page <br> 7 of 7 |
| :---: | :---: | :---: | :---: |
|  | Project | CT1003, North Haven | $\begin{array}{\|l\|} \hline \text { Date } \\ 16: 34: 06 \quad 08 / 25 / 14 \end{array}$ |
| Plain City, OH 43064 <br> Phone: 614-398-6250 <br> FAX: mike@mfpeng.com | Client | Florida Tower Partners | Designed by Mike |

## Pole Interaction Design Data



## Section Capacity Table

$\left.\begin{array}{cccccccc}\hline \begin{array}{c}\text { Section } \\ \text { No. }\end{array} & \begin{array}{c}\text { Elevation } \\ f t\end{array} & \begin{array}{c}\text { Component } \\ \text { Type }\end{array} & & \text { Size } & & \text { Critical } \\ \text { Element }\end{array}\right)$

| Michael F. Plahovinsak, P.E. <br> 18301 State Route 161 W <br> Plain City, OH 43064 <br> Phone: 614-398-6250 <br> email: mike@mfpeng.com | Job 130-ft monopole - MFP \#40914-090 |  | Page $\quad$ BP-G |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Project |  | 8/25/2014 |  |
|  | Client |  | Designed by |  |

## Anchor Rod and Base Plate Calculation

## ANSI/TIA-222-G-2

| Factored Base Reactions: | Pole Shape: | Anchor Rods: | Base Plate: |  |
| ---: | :---: | :--- | :--- | :--- |
| Moment: | 3861 ft -kips | 18-Sided | (20) $2.25 \mathrm{in} . \mathrm{A} 615 \mathrm{GR} .75$ | $2.75 \mathrm{in} . \times 58 \mathrm{in}$. Round |
| Shear: | 40 kips | Pole Dia. $\left(D_{f}\right):$ | Anchor Rods Evenly Spaced | fy $=50 \mathrm{ksi}$ |
| Axial: | 36 kips | 48.80 in | On a 55.25 in Bolt Circle |  |

Anchor Rod Calculation According to TLA-222-G section 4.9.9


## Base Plate Calculation According to TlA-222-G

| $\phi=$ | 0.90 tia 4.7 |  |  |
| :---: | :---: | :---: | :---: |
| $\mathbf{M}_{\text {PL }}=$ | 356.0 in-kip Plate Moment |  |  |
| $\mathrm{L}=$ | 7.7 in Section Length | Calculated Moment vs Factored Resistance |  |
| $\mathbf{Z}=$ | 14.5 Plastic Section Modulus | 355.99 in-kip $\leq$ | 652 in-kip |
| $\mathbf{M}_{\mathbf{P}}=$ | 724.6 in-kip ${ }_{\text {Plastic Moment }}$ |  |  |
| $\phi \mathbf{M}_{\mathrm{n}}=$ | 652.2 in-kip Factored Resistance |  |  |


| Anchor Rods Are Adequate | $\mathbf{6 6 . 0 \%}$ | $\square$ |
| :--- | :--- | :--- |
| Base Plate is Adequate | $\mathbf{5 4 . 6 \%}$ | $\square$ |

## Monopole Spread Footing Calculation

## ANSI/TIA-222-G-2

| Factored Base Reactions: |  | Footing Dimensions: |  | Concrete: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Moment: | 3861 ft-kips | 24 ft x 24 ft | 7 ft Square Pier | $\mathrm{fc}=4000 \mathrm{psi}$ |  |
| Shear: | 40 kips | x 2 ft thick | w/6 in Reveal | Steel fy $=60 \mathrm{ksi}$ |  |
| Axial: | 36 kips | Bearing $8 \mathrm{ft} \mathrm{B.G}$. | 54.5 Yd3 Concrete | $\mathrm{f}=0.75$ |  |
| Soil Backfill | 120 pcf | Ultimate Bearing: | 6000 psf | Water Table | 5.5 |

## Foundation Weight

| Weight of Pole | 36.0 kips |
| :---: | ---: |
| Weight of Concrete | 220.575 kips |
| Weight of Soil | 379.44 kips |
| Bouyancy of Water | -89.9 kips |
| Total | 546.2 kips |

## Overturning Resistance:

| Overturning Moment $\left(M_{u}\right)$ | 4201 ft -kips |
| :---: | ---: |
| Resisting Moment $\left(\mathrm{R}_{\mathrm{s}}\right)$ | 6553.908 ft -kips |
| $\phi$ x $\mathrm{R}_{\mathrm{s}}>\mathrm{M}_{\mathrm{u}}$ | $\mathrm{M}_{\text {overtuming }} / \mathrm{fM}_{\text {resist }}$ |

ft -kips $+(1.05$ kips $\times 0 \mathrm{ft})$
$546.159 \mathrm{kips} \times 24 \mathrm{ft} / 2$
85.5\% OK

## Soil Bearing Pressure:

| Eccentricity (e) | 7.69 ft | $4201 \mathrm{ft}-\mathrm{kips} / 546.159 \mathrm{kips}$ |
| :---: | :---: | :--- |
| $6(\mathrm{e})$ | $46.2 \mathrm{ft}>$ | $24.0 \mathrm{ft} \quad 6 \mathrm{e}>24$ |
| Maximum Soil Bearing | 3676.4242 psf | Calculated across corners |
| Soil Overburden | -804 psf | Overburden - Bouyancy |
| Net Soil Bearing | 2872.4242 psf |  |
| Resisting Soil Bearing $\left(\mathrm{R}_{\mathrm{s}}\right)$ | 6000 psf |  |
| Net Soil Bearing $<\phi \times \mathrm{R}_{\mathrm{s}}$ | Net Bearing $/ \mathrm{fR}_{\mathrm{s}}$ | $\mathbf{6 3 . 8} \% \quad \mathbf{O K}$ |

## Bending Moment in Pier:

Bending Moment
$4121 \mathrm{ft}-\mathrm{kips}$
$3861 \mathrm{ft}-\mathrm{kips}+(40 \mathrm{kips} \times 6.5 \mathrm{ft})$

## Bending Moment in Footing:

Max Bending Moment
2383.8318 ft-kips
$\Sigma$ Moments about pier face

Min. Footing Steel
$0.52 \mathrm{in}^{2} / \mathrm{ft}$
$0.18 \%$


# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility
Site ID: CTNH522A
Florida Partners North Haven Monopole
50 Devine Street
North Haven, CT 06473
September 2, 2014

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general public <br> allowable limit: | $\mathbf{4 8 . 1 2 \%}$ |

environmental | engineering | due diligence

September 2, 2014

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

## Emissions Analysis for Site: CTNH522A - Florida Partners North Haven Monopole

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 50 Devine Street, North Haven, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(\mathrm{~b})(1)$ - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limit for the 700 MHz Band is $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the PCS and AWS bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.
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Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 50 Devine Street, North Haven, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels (PCS Band -1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
2) $\mathbf{2}$ UMTS channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 1 LTE channel ( 700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
environmental | engineering | due diligence
6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antennas used in this modeling are the Ericsson AIR21 B4A/B2P for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the Commscope LNX-6515DS-VTM for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The Ericsson AIR21 B4A/B2P has a maximum gain of $\mathbf{1 5 . 9} \mathbf{~ d B d}$ at its main lobe. The Commscope LNX-6515DS-VTM has a maximum gain of $\mathbf{1 4 . 6} \mathbf{~ d B d}$ at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antenna mounting height centerline of the proposed antennas is $\mathbf{1 1 7}$ feet above ground level (AGL).
9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

## EBI Consulting <br> environmental | engineering | due diligence

T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | 1 | Antenna \#: | 1 | Antenna \#: | 1 |
| Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson ATR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 117 | Height (AGL): | 117 | Height (AGL): | 117 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 2 | Channel Count | 2 | \# PCS Channels: | 2 |
| Total TX Power: | 120 | Total TX Power: | 120 | \# AWS Channels: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna AI MPE\% | 1.36 | Antenna Bl MPE\% | 1.36 | Antenaa C1 MPE\% | 1.36 |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| Make / Model: | $\begin{gathered} \text { Ericsson AR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AlR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 117 | Height (AGL): | 117 | Height (AGL): | 117 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \\ & \hline \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 4 | Channel Count | 4 | Channel Count | 4 |
| Total TX Power: | 120 | Total TX Power: | 120 | Total TX Power: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna A2 MPE\% | 1.36 | Antenna B2 MPE\% | 1.36 | Antenna C2 MPE\% | 1.36 |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna \#: | 3 |
| Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 117 | Height (AGL): | 117 | Height (AGL): | 117 |
| Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz |
| Chamel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power: | 30 | Total TX Power: | 30 |
| ERP (W): | 445.37 | ERP (W): | 445.37 | ERP (W): | 445.37 |
| Antenna A3 MPE\% | 0.54 | Antenna B3 MPE\% | 0.54 | Antenna C3 MPE\% | 0.54 |
|  | Site Composite MPE\% |  |  | T-Mobile Sector 1 Total: | l $\quad 3.26 \%$ |
|  | Carrier | MPE\% |  | T-Mobile Sector 2 Total: | $1: 33.26 \%$ |
|  | T-Mobile | 9.79 |  | T-Mobile Sector 3 Total: | 1: $3.26 \%$ |
|  | Verizon Wireless | 24.90 \% |  | Site Total: | I: 48.12 \% |

environmental | engineering | due diligence

## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector 1: | $3.26 \%$ |
| Sector 2: | $3.26 \%$ |
| Sector 3: | $3.26 \%$ |
| T-Mobile Total: | $9.79 \%$ |
|  |  |
| Site Total: | $48.12 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{4 8 . 1 2 \%}$ of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

RF Engineering Director

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21 B Street
Burlington, MA 01803


[^0]:    ${ }^{1}$ The North Haven Facility was approved at a height of 120 feet (Docket 384), and subsequently the subject of a Petition to increase the height of the Facility to 130 feet (Petition 1089). The existing/proposed antenna height and configuration is consistent with the February 25, 2010 Docket 384 Decision and Order.

