Crown Castle 3530 Toringdon Way, Suite 300 Charlotte, NC 28277



November 24, 2014

Melanie A. Bachman Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Sprint PCS-Exempt Modification – Crown Site BU: 826222

Sprint PCS Site ID: CT54XC716

Located at: 201 South Main Street, Newtown, CT 06470

Dear Ms. Bachman:

This letter and exhibits are submitted on behalf of Sprint PCS (Sprint). Sprint is making modifications to certain existing sites in its Connecticut system in order to implement their 2.5GHz LTE technology. Please accept this letter and exhibits as notification, pursuant to § 16-50j-73 of the Regulations of Connecticut State Agencies ("R.C.S.A."), of construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In compliance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Mrs. E. Patricia Llodra, First Selectman for the City of Newtown, and Bluelinx Corp., Property Owner.

Sprint plans to modify the existing wireless communications facility owned by Crown Castle and located at **201 South Main Street, Newtown, CT 06470.** Attached are a compound plan and elevation depicting the planned changes (Exhibit-1), and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration (Exhibit-2). Also included is a power density table report reflecting the modification to Sprint's operations at the site (Exhibit-3).

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") § 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in the R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing tower. Sprint's additional antennas will be located at the same elevation on the existing tower.
- 2. There will be no proposed modifications to the ground and no extension of boundaries.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more.

- 4. A Structural Modification Report confirming that the tower and foundation can support Sprint's proposed modifications is included as Exhibit-2.
- 5. The operation of the additional antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table report for Sprint's modified facility is included as Exhibit-3.

For the foregoing reasons, Sprint respectfully submits the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Donna Neal.

Sincerely,

Susan Vale

Real Estate Specialist

Enclosures

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc: Mrs. E. Patricia Llodra, First Selectman for the Town of Newtown

Newtown Municipal Center

3 Primrose Street Newtown CT 06470

cc: Bluelinx Corp

4300 Wildwood Pkwy Atlanta, GA 30339



CT54XC716

SITE NAME:

NEWTOWN GEORGIA PACIFIC/VS

201 SOUTH MAIN STREET NEWTOWN, CT 06470

CROWN ID#: 826222

CROWN SITE NAME: NEWTOWN/RT-25

SHEET INFORMATION VICINITY MAP (NOT TO SCALE) CROWN CASTLE USA 2000 CORPORATE DRIVE CANONSBURG, PA LANDLORD: SITE NUMBER: CT54XC716 SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470 LOCAL POWER COMPANY: CONNECTICUT LIGHT AND POWER CONTACT CUSTOMER SERVICE SITE NAME: NEWTOWN GEORGIA PACIFIC/VS (800) 286-2000 COUNTY: FAIRFIELD APPLICANT: COORDINATES: 41° 22' 41.32" N 6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (NAD 83) 73° 16' 26.94" W GROUND ELEV: 377'± AMSL ENGINEER: JAMES QUICKSELL (845) 567-6656 EXT. 2835 STRUCTURE TYPE: MONOPOLE SPRINT CM: PETER CULBERT Peter.Culbert@sprint.com STRUCTURE HEIGHT: 150'-0"± AGL STRUCTURE CROWN CM: 140'-0"± AGL JASON D'AMICO RAD CENTER: (860) 209-0104 jason.d'amico@crowncastle.com ZONING



APPROVALS

THE FOLLOWING PARTIES HEREBY APPROVE AND ACCEPT THESE DOCUMENTS AND AUTHORIZE THE CONTRACTOR TO PROCEED WITH THE CONSTRUCTION DESCRIBED HEREIN. ALL DOCUMENTS ARE SUBJECT TO REVIEW BY THE LOCAL BUILDING DEPARTMENT AND MAY IMPOSE CHANGES OR MODIFICATIONS.

SHEET INDEX

SHEET DESCRIPTION

SHT. NO.

T-1

A-1

A-2

A-3

A-5

A-6

S-1

E-2

SP-1

TITLE SHEET

GENERAL NOTES

GENERAL NOTES

ANTENNA LAYOUT PLANS

RAN WIRING DIAGRAM

EQUIPMENT DETAILS

EQUIPMENT SCHEMATIC DETAILS

GROUNDING DETAILS & NOTES

ELECTRICAL & GROUNDING PLANS

CABLE DETAILS

ENLARGED EQUIPMENT LAYOUT PLANS

SITE PLAN

ELEVATION

CONSTRUCTION:	DATE:	
LEASING/ SITE ACQUISITION:	DATE:	
LANDLORD/ PROPERTY OWNER:	DATE:	
R.F. ENGINEER:	DATE:	



2.5 EOUIPMENT DEPLOYMENT 6580 SPRINT PARKWAY **OVERLAND PARK, KANSAS 66251**



TECTONIC Engineering & Surveying Consultants P.C.

1279 Route 300 Newburgh, NY 12550 Phone: (845) 567-6656 Fax: (845) 567-8703 www.tectonicengineering.com

	SL	JBMITTALS	
PRO	DJECT NO	7225.CT54XC7I6	
NO	DATE	DESCRIPTION	BY
0	07/14/14	FOR COMMENT	MF
Ì	11/21/14	FOR CONSTRUCTION	MF

DATE	REVIEWED BY
00000	A GENTANCE

SITE WARER

CT54XC716 SITE NAME:

NEWTOWN GEORGIA PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET

NEWTOWN, CT 06470

SHEET TITLE:

TITLE SHEET

SHEET NO:

T-1

CLASSIFICATION: M-1 MAP-BLOCK-LOT: 36/12/10/C/	Pool atack Hiller Pool atack Hiller Furnble Jungle A Your Healthy Pet
GENERAL NOTES	AERIAL VIEW (NOT TO SCALE)
1. THIS IS AN UNMANNED TELECOMMUNICATION FACILITY AND NOT FOR HUMAN HABITATION: HANDICAP ACCESS REQUIREMENTS ARE NOT REQUIRED. FACILITY HAS NO PLUMBING OR REFRIGERANTS. THIS FACILITY SHALL MEET OR EXCEED ALL FAA AND FCC REGULATOR REQUIREMENTS.	
2. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE PROJECT OWNER'S REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.	
 DEVELOPMENT AND USE OF THIS SITE WILL CONFORM TO ALL APPLICABLE CODES AND ORDINANCES. 	
 2005 STATE OF CONNECTICUT BUILDING CODE. ANSI/TIA/EIA-222-F-1996. NATIONAL ELECTRICAL CODE, LATEST EDITION. 	SITE
PROJECT DESCRIPTION	
1. (1) NEW 2.5 EQUIPMENT RACK INSIDE EXIST MMBTS CABINET.	
2. (3) NEW RFS APXVTM14-C-120 ANTENNAS.	
3. (3) NEW TD-RRH8x20-25 RRH.	
4. (1) NEW 1-1/4" HYBRID CABLE.	
5. (3) NEW RFS APXVSPP18C-A2O ANTENNAS.	

DIVISION 01000-GENERAL NOTES

- 1. THE CONTRACTOR SHALL GIVE ALL NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY, MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS, AND LOCAL AND STATE JURISDICTIONAL CODES BEARING ON THE PERFORMANCE OF THE WORK. THE WORK PERFORMED ON THE PROJECT AND THE MATERIALS INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES.
- 2. THE ARCHITECT/ENGINEER HAVE MADE EVERY EFFORT TO SET FORTH IN THE CONSTRUCTION AND CONTRACT DOCUMENTS THE COMPLETE SCOPE OF WORK. THE CONTRACTOR BIDDING THE JOB IS NEVERTHELESS CAUTIONED THAT MINOR OMISSIONS OR ERRORS IN THE DRAWINGS AND OR SPECIFICATIONS SHALL NOT EXCUSE SAID CONTRACTOR FROM COMPLETING THE PROJECT AND IMPROVEMENTS IN ACCORDANCE WITH THE INTENT OF THEFE POOLIMENTS. THESE DOCUMENTS.
- 3. THE CONTRACTOR OR BIDDER SHALL BEAR THE RESPONSIBILITY OF NOTIFYING (IN WRITING) THE PROJECT OWNER'S REPRESENTATIVE OF ANY CONFLICTS, ERRORS, OR OMISSIONS PRIOR TO THE SUBMISSION OF CONTRACTOR'S PROPOSAL OR PERFORMANCE OF WORK.
- 4. THE SCOPE OF WORK SHALL INCLUDE FURNISHING ALL MATERIALS. FOUIPMENT LABOR AND ALL OTHER MATERIALS AND LABOR DEEMED NECESSARY TO COMPLETE THE WORK/PROJECT AS DESCRIBED HEREIN.
- 5. THE CONTRACTOR SHALL VISIT THE JOB SITE PRIOR TO THE SUBMISSION OF BIDS OR PERFORMING WORK TO FAMILIARIZE HIMSELF WITH THE FIELD CONDITIONS AND TO VERIFY THAT THE PROJECT CAN BE CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- 6. ONCE THE CONTRACTOR HAS RECEIVED AND ACCEPTED THE NOTICE TO PROCEED, CONTRACTOR WILL CONTACT THE CROWN CASTLE CONSTRUCTION MANAGER OF RECORD (NOTED ON THE FIRST PAGE ON THIS CONSTRUCTION DRAWING) A MINIMUM OF 48 HOURS PRIOR TO WORK
 START. UPON ARRIVAL TO THE JOB SITE, CONTRACTOR CREW IS REQUIRED
 CALL 1-800-788-7011 TO NOTIFY THE CROWN CASTLE NOC WORK HAS
- 7. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS ACCORDING TO THE MANUFACTURER'S/VENDOR'S SPECIFICATIONS UNLESS NOTED OTHERWISE OR WHERE LOCAL CODES OR ORDINANCES TAKE
- 8. THE CONTRACTOR SHALL PROVIDE A FULL SET OF CONSTRUCTION DOCUMENTS AT THE SITE UPDATED WITH THE LATEST REVISIONS AND ADDENDUMS OR CLARIFICATIONS AVAILABLE FOR THE USE BY ALL PERSONNEL INVOLVED WITH THE PROJECT
- 9. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE PROJECT DESCRIBED HEREIN. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER
- 10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS WHICH MAY BE REQUIRED FOR THE WORK BY THE ARCHITECT/ENGINEER, THE STATE, COUNTY OR LOCAL GOVERNMENT
- 11. THE CONTRACTOR SHALL MAKE NECESSARY PROVISIONS TO PROTECT EXISTING IMPROVEMENTS, EASEMENTS, PAVING, CURBING, ETC. DURING CONSTRUCTION. UPON COMPLETION OF WORK, THE CONTRACTOR SHALL REPAIR ANY DAMAGE THAT MAY HAVE OCCURRED DUE TO CONSTRUCTION ON OR ABOUT THE PROPERTY.
- 12. THE CONTRACTOR SHALL KEEP THE GENERAL WORK AREA CLEAN AND HAZARD FREE DURING CONSTRUCTION AND DISPOSE OF ALL DIRT, DEBRIS, RUBBISH AND REMOVE EQUIPMENT NOT SPECIFIED AS REMAINING ON THE PROPERTY. PREMISES SHALL BE LEFT IN CLEAN CONDITION AND FREE FROM PAINT SPOTS, DUST, OR SMUDGES OF ANY NATURE.
- 13. THE CONTRACTOR SHALL COMPLY WITH ALL PERTINENT SECTIONS OF THE BASIC STATE BUILDING CODE, LATEST EDITION, AND ALL OSHA REQUIREMENTS AS THEY APPLY TO THIS PROJECT. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK SHALL BE DEFINED. RELOCATED AS DIRECTED BY THE ARCHITECT/ENGINEER. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR PIER DRILLING AROUND OR NEAR UTILITIES. THE CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT LIMITED TO A) FALL PROTECTION, B) CONFINED SPACE, C) FLECTRICAL SAFETY, D) TRENCHING AND EXCAVATION OF ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES WHICH INTERFERE WITH THE EXECUTION OF THE WORK SHALL BE REMOVED AND OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT THE POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK SUBJECT TO THE APPROVAL OF THE ARCHITECT/ENGINEER.
- 14. THE CONTRACTOR SHALL NOTIFY THE PROJECT OWNER'S REPRESENTATIVE IN WRITING WHERE A CONFLICT OCCURS ON ANY OF THE CONTRACT DOCUMENTS. THE CONTRACTOR IS NOT TO ORDER MATERIAL OR CONSTRUCT ANY PORTION OF THE WORK THAT IS IN CONFLICT UNTIL CONFLICT IS RESOLVED BY THE LESSEE/LICENSEE REPRESENTATIVE.
- 15. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS, ELEVATIONS, PROPERTY LINES, ETC. ON THE JOB.
- 16. THE CONTRACTOR SHALL NOTIFY THE THE RF ENGINEER FOR ANTENNA AZIMUTH VERIFICATION (DURING ANTENNA INSTALLATION) PRIOR TO CONDUCTING SWEEP TESTS.
- 17. THE CONTRACTOR SHALL SUBMIT AT THE END OF THE PROJECT A COMPLETE SET OF AS-BUILT DRAWINGS TO THE CLIENT REPRESENTATIVE

- 18 REFER TO: CONSTRUCTION STANDARDS-SPRINT DOCUMENT FYHIRE A—STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES REV. 4.0— 02.15.2011.DOCM.
- REFER TO: WEATHER PROOFING SPECS: EXCERPT EXH A-WIHRPRF-STD CONSTR SPECS._157201110421855492.DOCM.
- 20. REFER TO: COLOR CODING-SPRINT NEXTEL ANT AND LINE COLOR CODING (DRAFT) V3 09-08-11.PDF
- 21. REFER TO LATEST DOCUMENTATION REVISION.

DIVISION 03000-CONCRETE

- 1.03 APPLICABLE STANDARDS (USE LATEST EDITIONS)
- $\mbox{AC1-301}$ SPECIFICATIONS FOR STRUCTURAL CONCRETE FOR BUILDINGS. $\mbox{AC1-347}$ GUIDE TO FORM WORK FOR CONCRETE.
- ASTM C33- CONCRETE AGGREGATE
- ASTM C94 READY MIXED CONCRETE e. ASTM C150 PORTLAND CEMENT.
- ASTM C260 AIR—ENTRAINING ADMIXTURES FOR CONCRETE
 ASTM C309— LIQUID MEMBRANE FORMING COMPOUNDS FOR CURING CONCRETE.
- ASTM C494 CHEMICAL ADMIXTURES FOR CONCRETE
 ASTM A615— DEFORMED AND PLAIN BILLET—STEEL BARS FOR CONCRETE REINFORCEMENT
 ASTM A185— STEEL WELDED WIRE FABRIC (PLAIN) FOR CONCRETE REINFORCEMENT
- 1.04 QUALITY ASSURANCE

CONCRETE MATERIALS AND OPERATIONS SHALL BE TESTED AND INSPECTED BY THE ARCHITECT/ENGINEER AS DIRECTED BY THE CLIENT'S REPRESENTATIVE.

3.04 SURFACE FINISHES

SURFACES AGAINST WHICH BACKFILL OR CONCRETE SHALL BE PLACED REQUIRE NO TREATMENT EXCEPT REPAIR OF DEFECTIVE

B. SURFACES THAT WILL BE PERMANENTLY EXPOSED SHALL PRESENT A UNIFORM FINISH PROVIDED BY THE REMOVAL OF FINS AND THE FILLING HOLES AND OTHER IRREGULARITIES WITH DRY PACK GROUT, OR BY SACKING WITH UTILITY OR ORDINARY GROUT.

- SURFACES THAT WOULD NORMALLY BE LEVEL AND WHICH WILL BE PERMANENTLY EXPOSED TO THE WEATHER SHALL BE SLOPED FOR DRAINAGE. UNLESS ENGINEER'S DESIGN DRAWING SPECIFIES A HORIZONTAL SURFACE OR SURFACES SUCH AS STAIR TREADS, WALLS, CURBS, AND PARAPETS SHALL BE SLOPED APPROXIMATELY 1/4" PER FOOT
- D. SURFACES THAT WILL BE COVERED BY BACKFILL OR CONCRETE SHALL BE SMOOTH SCREENED
- E. EXPOSED SLAB SURFACES SHALL BE CONSOLIDATED, SCREENED, FLOATED, AND STEEL TROWELED. HAND OR POWER-DRIVEN EQUIPMENT MAY BE USED FOR FLOATING. FLOATING SHALL BE STARTED AS SOON AS THE SCREENED SURFACE HAS ATTAINED A STIFFNESS TO PERMIT FINISHING OPERATIONS. OPERATIONS. ALL EDGES MUST HAVE A 3/4" CHAMFER.
- 1.04 QUALITY ASSURANCE CONCRETE MATERIALS AND OPERATIONS SHALL BE TESTED AND INSPECTED BY THE ENGINEER

THE CONTRACTOR SHALL NOTIFY THE ENGINEER IMMEDIATELY UPON REMOVAL OF THE FORMS TO OBSERVE CONCRETE SURFACE CONDITIONS IMPERFECTIONS SHALL BE PATCHED ACCORDING TO THE ENGINEER'S

THE CONTRACTOR SHALL NOTIFY OR REPLACE CONCRETE NOT CONFORMING TO REQUIRED LEVELS AND LINES, DETAILS, AND ELEVATIONS AS SPECIFIED IN ACI 301.

3.07 PROTECTION

A. IMMEDIATELY AFTER PLACEMENT. THE CONTRACTOR SHALL PROTECT THE CONCRETE FROM PREMATURE DRYING, EXCESSIVELY HOT OR COLD TEMPERATURES, AND MECHANICAL INJURY. FINISHED WORK

- B. CONCRETE SHALL BE MAINTAINED WITH MINIMAL MOISTURE LOSS AT RELATIVELY CONSTANT TEMPERATURE FOR PERIOD NECESSARY FOR HYDRATION OF CEMENT AND HARDENING OF CONCRETE.
- C. ALL CONCRETE SHALL BE WATER CURED PER ACCEPTABLE PRACTICES SPECIFIED BY ACI CODE (LATEST EDITION)

DIVISION 05000 - METALS

PART 1 - GENERAL

1.01 WORK INCLUDED

- THE WORK CONSISTS OF THE FABRICATION AND INSTALLATION OF ALL MATERIALS TO BE FURNISHED. AND WITHOUT LIMITING THE GENERALITY THEREOF, INCLUDING ALL EQUIPMENT, LABOR AND SERVICES REQUIRED FOR ALL STRUCTURAL STEEL WORK AND ALL ITEMS INCIDENTAL AS SPECIFIED AND AS SHOWN ON THE DRAWINGS:
- STEEL FRAMING INCLUDING BEAMS, ANGLES, CHANNELS AND PLATES. WELDING AND BOLTING OF ATTACHMENTS.

1.02 REFERENCE STANDARDS

- THE WORK SHALL CONFORM TO THE CODES AND STANDARDS OF THE FOLLOWING AGENCIES AS FURTHER CITED HEREIN.
- ASTM: AMERICAN SOCIETY FOR TESTING AND MATERIALS AS PUBLISHED IN "COMPILATION OF ASTM STANDARDS IN BUILDING CODES"
 OR LATEST EDITION.
 AWS: AMERICAN WELDING SOCIETY CODE OR LATEST EDITION.
- AISC: AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS" (LATEST EDITION).

PART 2 - PRODUCTS

2.01 MATERIALS

A. STRUCTURAL STEEL: SHALL COMPLY WITH THE REQUIREMENTS OF ASTM A36 AND A992 FOR STRUCTURAL STEEL.

ALL PROPOSED STRUCTURAL STEEL SHALL BE FABRICATED AND ERECTED IN ACCORDANCE WITH AISC CODE AND ASTM SPECIFICATIONS (LATEST EDITION) ALL NEW STEEL SHALL CONFORM TO THE FOLLOWING.

- STRUCTURAL WIDE FLANGE: ASTM A992 Fy=50KSI.
 MISCELLANEOUS STEEL (PLATES), CHANNELS, ANGLES, ETC): ASTM A36 (Fy=36KSI).

 3.STRUCTURAL TUBING: ASTM A500 Gr. B (Fy=46KSI).
- 4. STEEL PIPE: ASTM A53 Gr B (Fy=35KSI)

2.02 WELDING

- ALL WELDING SHALL BE DONE BY CERTIFIED WELDERS. CERTIFICATION DOCUMENTS SHALL BE MADE AVAILABLE FOR ENGINEER'S AND/OR OWNER'S REVIEW IF REQUESTED.
- WELDING ELECTRODES FOR MANUAL SHIELDED METAL ARC WELDING SHALL CONFORM TO ASTM 1-233, E70 SERIES. BARE ELECTRODES AND GRANULAR FLUX USED IN THE SUBMERGED ARC PROCESS SHALL CONFORM TO AISC SPECIFICATIONS.
- FIELD WELDING SHALL BE DONE AS PER AWS D1.1 REQUIREMENTS VISUAL INSPECTION IS ACCEPTABLE.
- STUD WELDING SHALL BE ACCOMPLISHED BY CAPACITOR DISCHARGE (CD) WELDING TECHNIQUE USING CAPACITOR DISCHARGE STUD WELDER.
- PROVIDE STUD FASTENERS OF MATERIALS AND SIZES SHOWN ON DRAWINGS OR AS RECOMMENDED BY THE MANUFACTURER FOR STRUCTURAL LOADINGS REQUIRED.
- FOLLOW MANUFACTURERS SPECIFICATIONS AND INSTRUCTIONS TO PROPERLY SELECT AND INSTALL STUD WELDS.

- A. BOLTS SHALL BE CONFORMING TO ASTM A35 HIGH STRENGTH HOT DIP GALVANIZED WITH ASTM A153 HEAVY HEX TYPE NUTS
- BOLTS SHALL BE 3/4" (MINIMUM) CONFORMING TO ASTM A325, HOT DIP GALVANIZED, ASTM A153 NUTS SHALL BE HEAVY HEX TYPE.
- ALL CONNECTIONS SHALL BE 2 BOLTS MINIMUM
- EXCEPT WHERE SHOWN, ALL BEAM TO BEAM AND BEAM TO COLUMN CONNECTIONS TO BE DOUBLE ANGLED CONNECTIONS WITH HIGH STRENGTH BOLTS (THREADS EXCLUDED FROM SHEAR PLANE) AND
- E. STANDARD, OVERSIZED OR HORIZONTAL SHORT SLOTTED HOLES.
- SNUG-TIGHT STRENGTH BEARING BOLTS MAY BE USED IN STANDARD HOLES CONFORMING TO ACIS, USING THE TURN OF THE NUT METHOD
- H. FULLY-TENSIONED HIGH STRENGTH (SLIP CRITICAL) SHALL BE USED IN OVERSIZED SLOT HOLES (RESPECTIVE OF SLOT ORIENTATION).
- ALL BRACED CONNECTION, MOMENT CONNECTION AND CONNECTIONS NOTED AS "SLIP CRITICAL" SHALL BE BE SLIP CRITICAL JOINTS WITH CLASS A SURFACE CONDITIONS, UNLESS OTHERWISE NOTED.
- EPOXY ANCHOR ASSEMBLIES SHALL BE AS MANUFACTURED BY HILTI OR ENGINEER APPROVED EQUAL, AS FOLLOWS:

BASE MATERIAL

ANCHOR SYSTEM

HOLLOW & GROUTED CMU OR BRICK

2.04 FABRICATION

A. FABRICATION OF STEEL SHALL CONFORM TO THE AISC AND AWS

2.05 FINISH

A. STRUCTURAL STEEL EXPOSED TO WEATHER SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123. (LATEST EDITION) UNLESS OTHERWISE NOTED.

2.06 PROTECTION

A. UPON COMPLETION OF ERECTION INSPECT ALL GALVANIZED STEEL AND PAINT ANY FIELD CUTS, WELDS OR GALVANIZED BREAKS WITH (2) COATS OF ZINC-RICH COLD GALVANIZING PAINT.

PART 3 - ERECTION

- A. PROVIDE ALL ERECTION, EQUIPMENT, BRACING, PLANKING, FIELD BOLTS, NUTS, WASHERS, DRIFT PINS, AND SIMILAR MATERIALS WHICH DO NOT FORM A PART OF THE COMPLETED
 CONSTRUCTION, BUT ARE NECESSARY FOR ITS
 PROPER ERECTION.
- B. ERECT AND ANCHOR ALL STRUCTURAL STEEL IN ACCORDANCE WITH AISC REFERENCE STANDARDS.
 ALL WORK SHALL BE ACCURATELY SET TO
 ESTABLISHED SUITABLE ATTACHMENTS TO THE
 CONSTRUCTION OF THE BUILDING
- C. TEMPORARY BRACING, GUYING, AND SUPPORT SHALL BE PROVIDED TO KEEP THE STRUCTURE SET AND ALIGNED AT ALL TIMES DURING CONSTRUCTION, AND TO PREVENT DANGER TO PERSONS AND PROPERTY, CHECK ALL TEMPORARY LOADS AND STAY WITHIN SAFE CAPACITY OF ALL BUILDING COMPONENTS.



OVERLAND PARK, KANSAS 66251



TECTONIC

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DATE	REVIEWED BY



State White 600 CT54XC716

SITE NAME: NEWTOWN GEORGIA PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

GENERAL NOTES

SHEET NO:

SP-1

DIVISION 13000-SPECIAL CONSTRUCTION ANTENNA INSTALLATION

PART 1 - GENERAL

1.01 WORK INCLUDED

ANTENNAS AND HYBRIFLEX CABLES ARE FURNISHED BY CLIENT'S REPRESENTATIVE UNDER SEPARATE CONTRACT. THE CONTRACTOR SHALL ASSIST ANTENNA INSTALLATION CONTRACTOR IN TERMS OF COORDINATION AND SITE ACCESS. ERECTION SUBCONTRACTOR SHALL BE RESPONSIBLE FOR THE PROPERTY.

- B. INSTALL ANTENNAS AS INDICATED ON DRAWINGS AND CLIENT'S REPRESENTATIVE SPECIFICATIONS.
- INSTALL GALVANIZED STEEL ANTENNA MOUNTS AS INDICATED ON
- D. INSTALL FURNISHED GALVANIZED STEEL OR ALUMINUM WAVEGUIDE AND PROVIDE PRINTOUT OF THAT RESULT
- F. INSTALL HYBRIFLEX CABLES AND TERMINATIONS BETWEEN ANTENNAS AND EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS. WEATHERPROOF ALL CONNECTORS BETWEEN THE ANTENNA AND EQUIPMENT PER MANUFACTURER'S REQUIREMENTS.
- G. ANTENNA AND HYBRIFLEX CABLE GROUNDING:
- ALL EXTERIOR #6 GREEN GROUND WIRE DAISY CHAIN CONNECTIONS ARE TO BE WEATHER SEALED WITH ANDREWS CONNECTOR/SPLICE WEATHERPROOFING KIT TYPE 3221213 OR
- ALL HYBRIFLEX CABLE GROUNDING KITS ARE TO BE INSTALLED ON STRAIGHT RUNS OF HYBRIFLEX CABLE (NOT WITHIN BENDS).

 1.02 RELATED WORK FURNISH THE FOLLOWING WORK AS SPECIFIED UNDER CONSTRUCTION DOCUMENTS, BUT COORDINATE WITH QOTHER TRADES PRIOR TO BID:
- FLASHING OF OPENING INTO OUTSIDE WALLS. SEALING AND CAULKING ALL OPENINGS. PAINTING.
- PAINTING.
 CUTTING AND PATCHING.
- 1.03 REQUIREMENTS OF REGULATOR AGENCIES
- A. FURNISH U.L. LISTED EQUIPMENT WHERE SUCH LABEL IS
- FURNISH U.L. ISTED EQUIPMENT WHERE SUCH LABEL IS AVAILABLE. INSTALL IN CONFORMANCE WITH U.L. STANDARDS WHERE APPLICABLE. INSTALL ANTENNA, ANTENNA CABLES, GROUNDING SYSTEM IN ACCORDANCE WITH DRAWINGS AND SPECIFICATIONS IN EFFECT AT PROJECT LOCATION AND RECOMMENDATIONS OF STATE AND LOCAL BUILDING CODES HAVING JURISDICTION OVER SPECIFIC PORTIONS OF WORK. THIS WORK INCLUDES, BUT IS NOT LIMITED TO THE
- EIA ELECTRONIC INDUSTRIES ASSOCIATION RS-22. STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES
- 2. FAA FEDERAL AVIATION ADMINISTRATION ADVISORY CIRCULAR AC 70/7480-IH. CONSTRUCTION MARKING AND LIGHTING.
- FCC FEDERAL COMMUNICATION COMMISSION RULES AND REGULATIONS FORM 715, OBSTRUCTION MARKING AND LIGHTING SPECIFICATION FOR ANTENNA STRUCTURES
- AISC AMERICAN INSTITUTE OF STEEL CONSTRUCTION FOR STRUCTURAL JOINTS USING ASTM 1325 OR A490 BOLTS.
- 5. NEC NATIONAL ELECTRIC CODE ON TOWER LIGHTING KITS.
- UL UNDERWRITER'S LABORATORIES APPROVED ELECTRICAL
- IN ALL CASES, PART 77 OF THE FAA RULES AND PARTS 17 AND 22 OF THE FCC RULES ARE APPLICABLE AND IN THE EVENT OF CONFLICT, SUPERSEDE ANY OTHER STANDARDS OR
- 8. LIFE SAFETY CODE NFPA, LATEST EDITION.

DIVISION 13000-EARTHWORK

PART 1 GENERAL

- WORK INCLUDED: REFER TO SURVEY AND SITE PLAN FOR WORK INCLUDED.
- RELATED WORK
- CONSTRUCTION OF EQUIPMENT FOUNDATIONS

PART 2 PRODUCTS

2.01 MATERIALS

- ROAD AND SITE MATERIALS; FILL MATERIAL SHALL BE ACCEPTABLE, SELECT FILL SHALL BE IN ACCORDANCE WITH LOCAL DEPARTMENT OF HIGHWAY AND PUBLIC TRANSPORTATION STANDARD SPECIFICATIONS.
- SOIL STERILIZER SHALL BE EPA REGISTERED OF LIQUID COMPOSITION AND OF PRE-EMERGENCE DESIGN.
- SOIL STABILIZER FABRIC SHALL BE MIRAFI OR EQUAL 600X AT C. ACCESS ROAD AND COMPOUND
- GRAVEL FILL; WELL GRADED, HARD, DURABLE, NATURAL SAND AND GRAVEL, FREE FROM ICE AND SNOW, ROOTS, SOD RUBBISH, AND OTHER DELETERIOUS OR ORGANIC MATTER.

MATERIAL SHALL CONFORM TO THE FOLLOWING GRADATION

GRAVEL FILL TO BE PLACED IN LIFTS OF 9" MAXIMUM THICKNESS AND 90 % DENSITY. COMPACTED TO 95

E. NO FILL OR EMBANKMENT MATERIALS SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OF EMBANKMENT

2.02 FOUIPMENT

- COMPACTION SHALL BE ACCOMPLISHED BY MECHANICAL MEANS. LARGER AREAS SHALL BE COMPACTED BY MEEPS FOOT, VIBRATORY OR RUBBER TIED ROLLERS WEIGHING AT LEAST FIVE TONS. SMALLER AREAS SHALL BE COMPACTED BY POWER-DRIVER, HAND HELD TAMPERS.
- PRIOR TO OTHER EXCAVATION AND CONSTRUCTION EFFORTS GRUB ORGANIC MATERIAL TO A MINIMUM OF 6" BELOW ORIGINAL GROUND
- UNLESS OTHERWISE INSTRUCTED BY CLIENT'S REPRESENTATIVE. REMOVE TREES, BRUSH AND DEBRIS FROM THE PROPERTY TO AN AUTHORIZED DISPOSAL LOCATION. C.
- PRIOR TO PLACEMENT OF FILL OR BASE MATERIALS, ROLL THE SOIL.
- WHERE UNSTABLE SOIL CONDITIONS ARE ENCOUNTERED, LINE THE GRUBBED AREAS WITH STABILIZER MAT PRIOR TO PLACEMENT OF FILL OR BASE MATERIAL.

3.03 INSTALLATION

- THE SITE AND TURNAROUND AREAS SHALL BE AT THE SUB-BASE COURSE ELEVATION PRIOR TO FORMING FOUNDATIONS. GRADE OR FILL THE SITE AND ACCESS ROAD AS REQUIRED TO PRODUCE EVEN DISTRIBUTION OF SPOILS RESULTING FROM FOUNDATION EXCAVATIONS. THE RESULTING GRADE SHALL CORRESPOND WITH SAID SUB-BASE COURSE, ELEVATIONS ARE TO BE CALCULATED FORM FINISHED GRADES OR SLOPES INDICATED.
- THE ACCESS ROAD SHALL BE BROUGHT TO BASE COURSE ELEVATION PRIOR TO FOUNDATION CONSTRUCTION
- DO NOT CREATE DEPRESSIONS WHERE WATER MAY POND.
- THE CONTRACT INCLUDES ALL NECESSARY GRADING, BANKING, DITCHING AND COMPLETE SURFACE COURSE FOR ACCESS ROAD.
 ALL ROADS OR ROUTES UTILIZED FOR ACCESS TO PUBLIC
 THOROUGHFARE IS INCLUDED IN SCOPE OF WORK UNLESS OTHERWISE INDICATED.
- WHEN IMPROVING AN EXISTING ACCESS ROAD, GRADE THE EXISTING ROAD TO REMOVE ANY ORGANIC MATTER AND SMOOTH THE SURFACE BEFORE PLACING FILL OR STONE.
- F. PLACE FILL OR STONE IN 3" MAXIMUM LIFTS AND COMPACT BEFORE PLACING NEXT LIFT.
- THE FINISH GRADE, INCLUDING TOP SURFACE COURSE SHALL EXTEND A MINIMUM OF 12" BEYOND THE SITE FENCE AND SHALL COVER THE AREA AS INDICATED.
- RIPRAP SHALL BE APPLIED TO THE SIDE SLOPES OF ALL FENCED AREAS, PARKING AREAS AND TO ALL OTHER SLOPES GREATER THAN H. 2.1
- RIPRAP SHALL BE APPLIED TO THE SIDES OF DITCHES OR DRAINAGE SWALES AS INDICATED ON PLANS.
- RIPRAP ENTIRE DITCH FOR 6'-0" IN ALL DIRECTIONS AT CULVERT

- SEED, FERTILIZER AND STRAW COVER SHALL BE APPLIED TO ALL OTHER DISTURBED AREAS AND DITCHES, DRAINAGE, SWALES, NOT OTHERWISE RIP—RAPPED.
- UNDER NO CIRCUMSTANCES SHALL DITCHES, SWALES OR CULVERTS BE PLACED SO THEY DIRECT WATER TOWARDS, OR PERMIT STANDING WATER IMMEDIATELY ADJACENT TO SITE. OWNER DESIGNS OR IF DESIGN ELEVATIONS CONFLICT WITH THIS GUIDANCE ADVISE THE OWNER IMMEDIATELY.
- IF A DITCH LIES WITH SLOPE GREATER THAN TEN PERCENT, MOUND DIVERSIONARY HEADWALL IN THE DITCH AT CULVERT ENTRANCES. RIP—RAP THE UPSTREAM SIDE OF THE HEADWALL AS WELL AS THE DITCH FOR 6'-0" ABOVE THE CULVERT
- IF A DITCH LIFS WITH SLOPES GREATER THAN TEN PERCENT MOUND DIVERSIONARY HEADWALLS IN THE DITCH FOR 6'-0" ABOVE THE CULVERT ENTRANCE.
- SEED AND FERTILIZER SHALL BE APPLIED TO SURFACE CONDITIONS WHICH WILL ENCOURAGE ROOTING, RAKE AREAS TO BE SEEDED TO EVEN THE SURFACE AND TO LOOSEN THE SOIL.
- SOW SEED IN TWO DIRECTIONS IN TWICE THE QUANTITY RECOMMENDED BY THE SEED PRODUCER
- IT IS THE CONTRACTOR'S RESPONSIBILITY TO ENSURE GROWTH OF SEEDED AND LANDSCAPED AREAS BY WATERING UP TO THE POINT OF RELEASE FROM THE CONTRACT. CONTINUE TO REWORK BARE AREAS UNTIL COMPLETE COVERAGE IS OBTAINED.

3.04 FIELD QUALITY CONTROL

- COMPACTION SHALL BE D-1557 FOR SITE WORK AND 95 % MAXIMUM DENSITY UNDER SLAB AREAS. AREAS OF SETTLEMENT WILL BE EXCAVATED AND REFILLED AT CONTRACTOR'S EXPENSE. REQUIRED. USE OF EROSION CONTROL MESH OR MULCH NET SHALL BE AN ACCEPTABLE ALTERNATIVE.
- B. THE COMPACTION TEST RESULTS SHALL BE AVAILABLE PRIOR TO THE CONCRETE POUR.

3.05 PROTECTION

- PROTECT SEEDED AREAS FORM EROSION BY SPREADING STRAW TO A UNIFORM LOOSE DEPTH OF 1"-2". STAKE AND TIE DOWN AS REQUIRED. USE OF EROSION CONTROL MESH OR MULCH NET SHALL BE AN ACCEPTABLE ALTERNATIVE.
- ALL TREES PLACED IN CONJUNCTION WITH A LANDSCAPE CONTRACT SHALL BE WRAPPED, TIED WITH HOSE PROTECTED WIRE AND SECURED TO STAKES EXTENDING 2'-0" INTO THE GROUND ON FOUR SIDES OF THE TREE.
- C. ALL EXPOSED AREAS SHALL BE PROTECTED AGAINST WASHOUTS AND SOIL EROSION. STRAW BALES SHALL BE PLACED AT THE INLET APPROACH TO ALL NEW OR EXISTING CULVERTS. REFER TO

SYMBOLS	ABBREVIATIONS
	GROUND WIRE
———е———е—	ELECTRIC
· — — - I — — I —	TELEPHONE
CHIM —— CHIM —	OVERHEAD WIRE
	PROPERTY LINE
_xx	CHAIN LINK FENCE
A-1	ANTENNA MARK
(E)	EXISTING
(P)	PROPOSED DETAIL
DET #	REFERENCE
•	SURFACE ELEVATION





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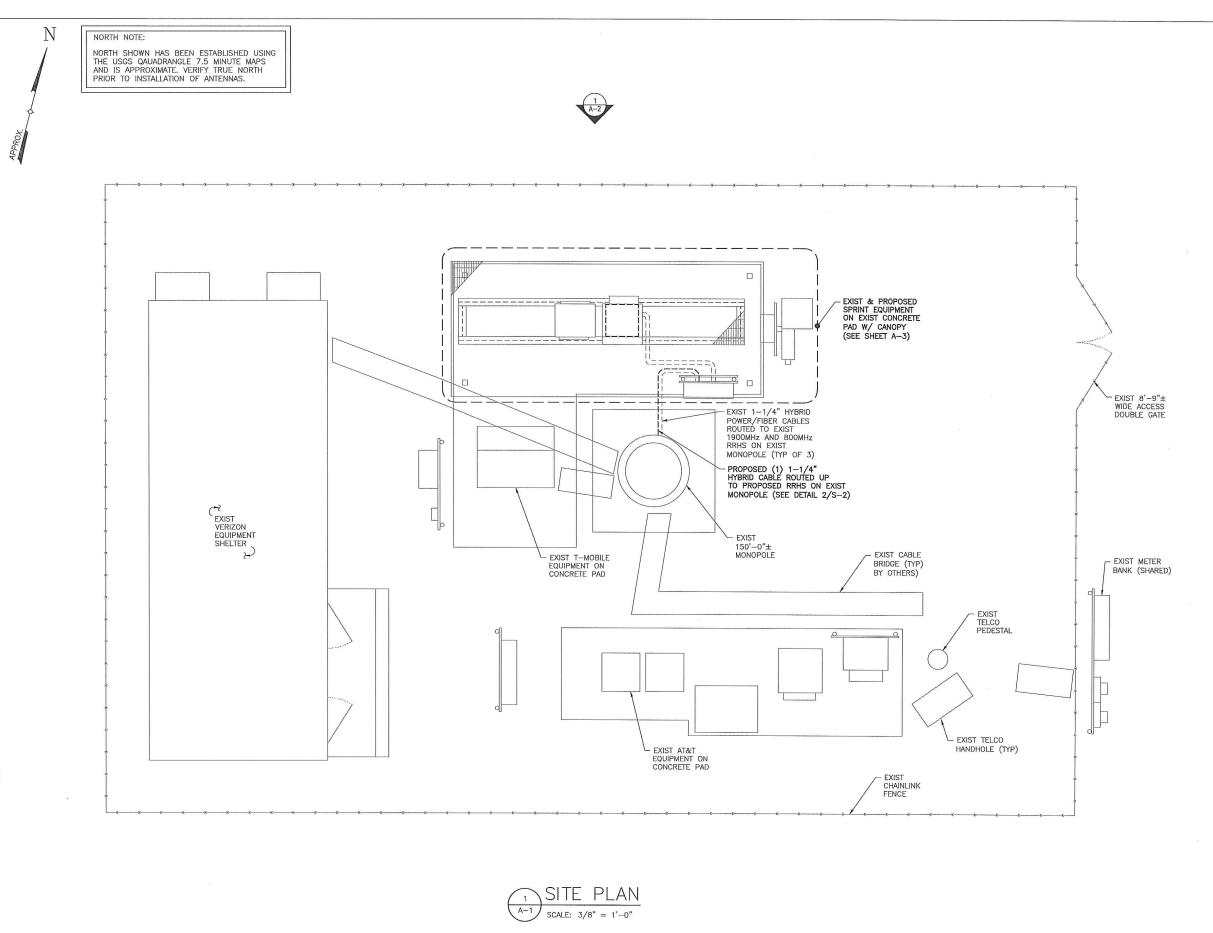
201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

GENERAL NOTES

SHEET NO:

SP-2





2.5 EQUIPMENT DEPLOYMENT 6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251

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SITE NAME:

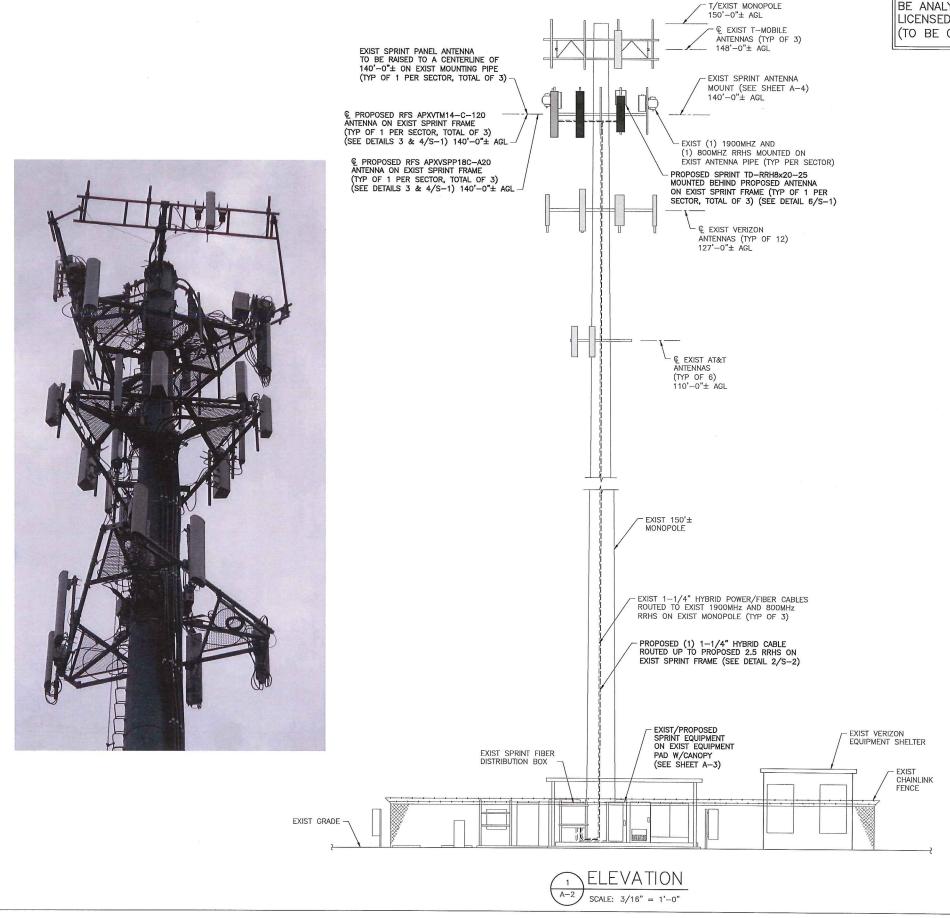
NEWTOWN GEORGIA PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

SITE PLAN

SHEET NO:



THE EXISTING MONOPOLE SHALL
BE ANALYZED BY A PROFESSIONAL ENGINEER
LICENSED IN THE STATE OF CONNECTICUT
(TO BE COORDINATED BY OTHERS).

THE EXISTING MOUNT HAS BEEN ANALYZED BY TECTONIC ENGINEERING AND FOUND TO BE ADEQUATE TO SUPPORT THE PROPOSED SPRINT UPGRADE AS DETAILED IN THE STRUCTURAL ANALYSIS EVALUATION LETTER DATED 11/21/14.



2.5 EQUIPMENT DEPLOYMENT 6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251



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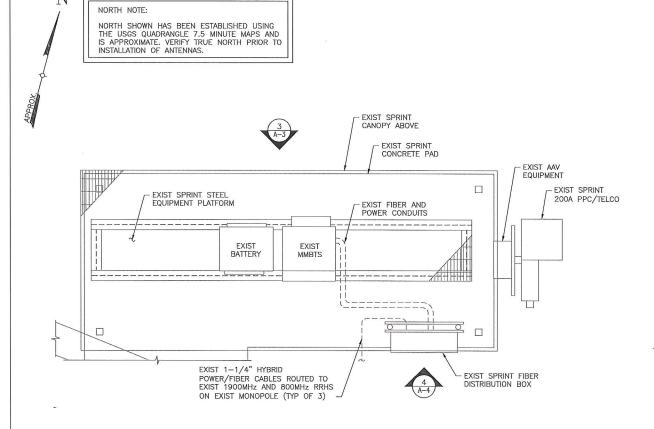
site name: NEWTOWN GEORGIA PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470

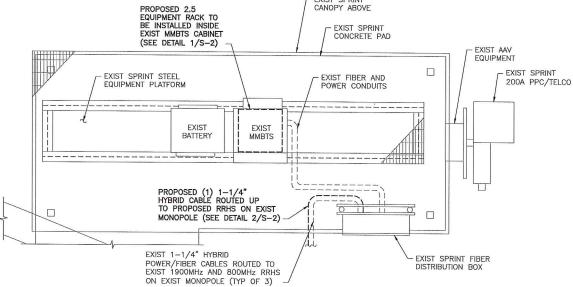
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ELEVATION

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NENLARGED EQUIPMENT LAYOUT PLAN (EXIST)



- EXIST SPRINT CANOPY ABOVE

SCALE: NTS

EXIST FIBER DISTRIBUTION BOX SCALE: NTS







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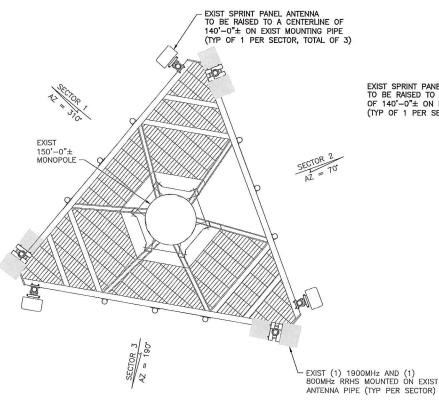
SHEET TITLE:

ENLARGED EQUIPMENT LAYOUT PLANS

SHEET NO:



PPROX. \diamond



EXIST SPRINT PANEL ANTENNA
TO BE RAISED TO A CENTERLINE
OF 140'-0"± ON EXIST MOUNTING PIPE
(TYP OF 1 PER SECTOR, TOTAL OF 3)

EXIST (1) 1900MHz AND (1) 800MHz RRH MOUNTIED ON EXIST ANIENNA MOUNTING PIPE (TYP PER SECTOR)

THE EXISTING MONOPOLE SHALL
BE ANALYZED BY A PROFESSIONAL ENGINEER
LICENSED IN THE STATE OF CONNECTICUT
(TO BE COORDINATED BY OTHERS).

THE EXISTING MOUNT HAS BEEN ANALYZED BY TECTONIC ENGINEERING AND FOUND TO BE ADEQUATE TO SUPPORT THE PROPOSED SPRINT UPGRADE AS DETAILED IN THE STRUCTURAL ANALYSIS EVALUATION LETTER DATED 11/21/14.





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PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

ANTENNA LAYOUT PLANS

SHEET NO: A-4

EXIST MOUNTING PIPE

EXIST MOUNTING BRACKET

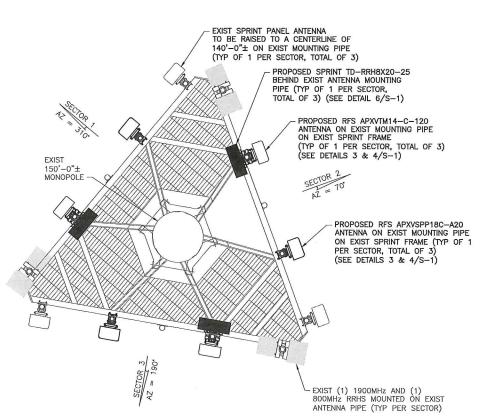
PROPOSED SPRINT TD—RRH8x20—25



ANTENNA DATA

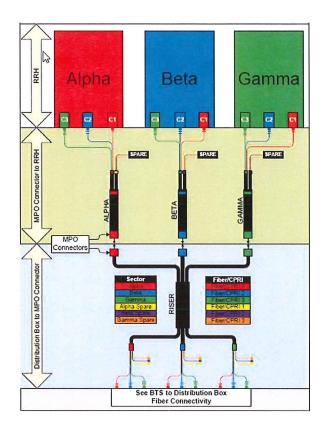
Status	Exist (Proposed)	Proposed
Antenna Manufacturer	RFS-CEL WAVE	RFS-CEL WAVE
Antenna Model Number	APXVSPP18C-A20	APXVTM14-C-120
Number of Antennas	3 (3)	3
Antenna RAD Center	140'	140'
Antenna Azimuth	310/70/190	310/70/190
Antenna RRH Model Number	1900MHz/800MHz RRHS	2.5GHz RRH-V3
Number of RRH	6	3

ANTENNA LAYOUT PLAN (EXIST)



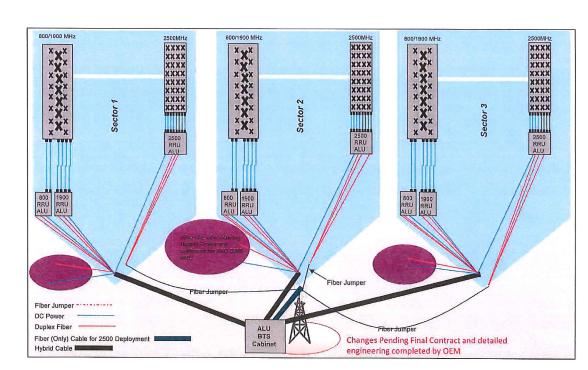
ANTENNA LAYOUT PLAN (FINAL)

SCALE: 1/2" = 1'-0"

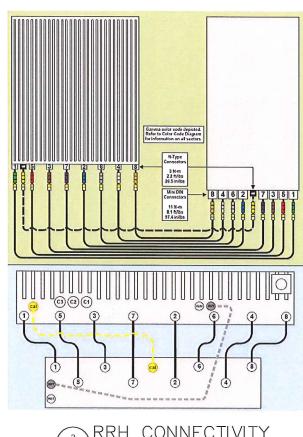


2.5 CABLE COLOR CODING

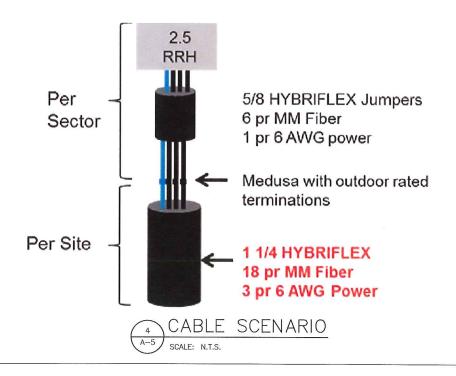
SCALE: N.T.S.















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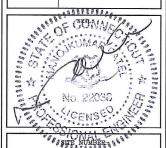
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SITE NAME:
NEWTOWN GEORGIA

PACIFIC/VS

SITE ADDRESS:
201 SOUTH MAIN STREET

NEWTOWN, CT 06470

SHEET TITLE:

RAN WIRING DIAGRAM

SHEET NO:

IMPORTANTII LINE UP WHITE
MARKINGS ON JUMPER AND RISER
IP—MPO CONNECTOR. PUSH THE
WHITE MARK ON THE JUMPER
CONNECTOR FLUSH AGAINST THE RED
SEAL ON THE RISER CONNECTION



IMPORTANTI! ROTATE THE BAYONET HOUSING CLOCKWISE UNTIL A CLICK SOUND IS HEARD TO ENSURE A GOOD CONNECTION



CONNECTION (MPQ) TO BE
INSTALLE PER MANUFACTURER
REQUIREMENTS. SEE DETAIL.

FIBER BREAKOUT

DC POWER BREAKOUT

BREAKOUTS TO RRH

CABLE TERMINATION
ENCLOSURE FURNISHED

USE EXIST NV
SPARE HYBRIFLEX
DC CONDUCTORS

EXIST RRU

INSTALL (1) 1-1/4"6
HYBRID CABLE

INSTALL (1) 3/4"6

2.5 HYBRID CABLE W/FIBER & DC FEEDERS

FIBER ONLY TRUNK LINES

HYBRIFLEX RISER/JUMPER CONNECTION DETAILS

TRUNK LINE DETAILS (TYPICAL)

SPECIAL NOTES: CABLE MARKINGS AT RAD CENTER AND ALL WALL/BLDG, PENETRATIONS

 \bullet ALL COLOR CODE TAPE SHALL BE 3M-35 AND SHALL BE INSTALLED USING A MINIMUM OF (3) WRAPS OF TAPE.

TRUNK-LINE TO JUMPER

- \bullet ALL COLOR BANDS INSTALLED AT THE TOWER TOP SHALL BE A MINIMUM OF 3" WIDE AND SHALL HAVE A MINIMUM OF 3/4" OF SPACING BETWEEN EACH COLOR.
- ALL COLOR BANDS INSTALLED AT OR NEAR THE GROUND MAY BE ONLY 3/4" WIDE. EACH TOP-JUMPER SHALL BE COLOR CORDED WITH (1) SET OF 3" WIDE BANDS.
- EACH MAIN COAX SHALL BE COLOR CODED WITH (1) SET OF 3" BANDS NEAR THE TOP-JUMPER CONNECTION AND WITH 3/4" COLOR BANDS JUST PRIOR TO ENTERING THE BTS OR TRANSMITTER BUILDING.
- ALL BOTTOM JUMPERS SHALL BE COLOR CODED WITH (1) SET OF 3/4" BANDS ON EACH END OF THE BOTTOM JUMPER.
- \bullet ALL COLOR CODES SHALL BE INSTALLED SO AS TO ALIGN NEATLY WITH ONE ANOTHER FROM SIDE—TO—SIDE.
- \bullet EACH COLOR BAND SHALL HAVE A MINIMUM OF (3) WRAPS AND SHALL BE NEATLY TRIMMED AND SMOOTHED OUT AS TO AVOID UNRAYELING.
- X-POLE ANTENNAS SHOULD USE "XX-1" FOR THE "+45" PORT, "XX-2" FOR THE "-45" PORT.
- COLOR BAND #4 REFERS TO THE FREQUENCY BAND: ORANGE=850, VIOLET=1900. USED ON JUMPERS ONLY.
- RF FEEDLINE SHALL BE IDENTIFIED WITH A METAL TAG (STAINLESS OR BRASS) AND STAMPED WITH THE SECTOR, ANTENNA POSITION, AND CABLE NUMBER.
- ANTENNAS MUST BE IDENTIFIED, USING THE SECTOR LETTER AND ANTENNA NUMBER, WITH A BLACK MARKER PRIOR TO INSTALLATION.



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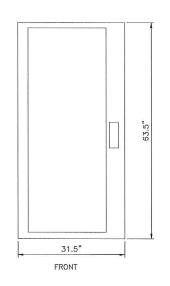
SITE NAME:
NEWTOWN GEORGIA
PACIFIC/VS

SITE ADDRESS:
201 SOUTH MAIN STREET
NEWTOWN, CT 06470

SHEET TITLE:

CABLE DETAILS

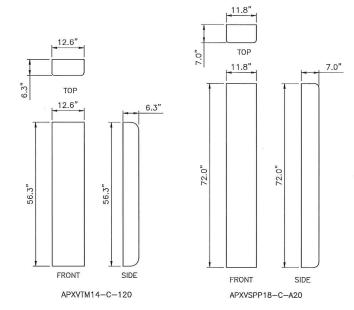
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9927 MMBTS MODULAR CELL SPECIFICATIONS:

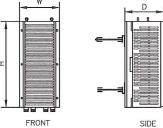
WIDTH: 31.5" DEPTH: 38.0"

(EXIST) MMBTS CABINET SCALE: 1" = 1'-0"

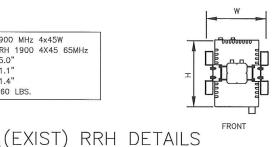


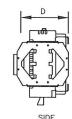
ANTENNA DETAILS SCALE: 3/4" = 1'-0"

SCALE: $1 \frac{1}{2}$ " = 1'-0"

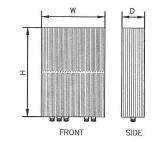


1900 MHz 4x45W MODEL #: RRH 1900 4X45 65MHz HEIGHT: " 25.0" WIDTH: 11.1" DEPTH: WEIGHT: ±60 LBS.





TYPE: 800 MHz 2x50W MODEL #: FD-RRH-2x50-800 HEIGHT: 19.7" WIDTH: 13" DEPTH: 10.8" WEIGHT: ±53 LBS

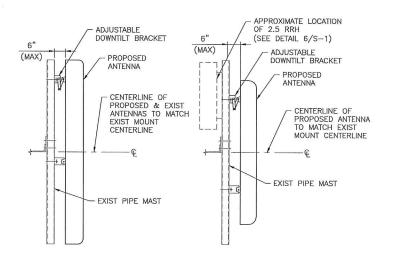


TYPE: 2.5 RRH MODEL #: TD-RRH8x20-25 HEIGHT: 26.1" WIDTH: 18.6" DEPTH: 6.7" WEIGHT: ±70 LBS

(PROPOSED) RRH DETAIL SCALE: 1" = 1'-0"

BATTERY SPECIFICATIONS: HEIGHT: 63.5" WIDTH: 31.5" DEPTH: 28.0" 31.5"

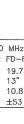
(EXIST) BATTERY CABINET



APXVSPP18-C-A20

APXVTM14-C-120

ANTENNA MOUNTING DETAILS SCALE: 3/4" = 1'-0"









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SITE NAME: NEWTOWN GEORGIA

PACIFIC/VS SITE ADDRESS:

201 SOUTH MAIN STREET NEWTOWN, CT 06470

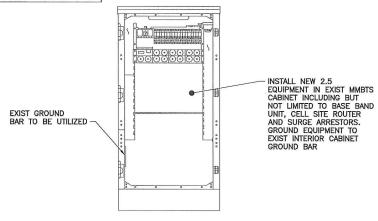
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EQUIPMENT DETAILS

SHEET NO:

S-1

NOTE: LOCATIONS SHOWN FOR INSTALLATION OF NEW INSTALLATION OF NEW EQUIPMENT IN EXISTING CABINET ARE APPROXIMATE ACTUAL SPACE AVAILABLE TO BE VERIFIED IN FIELD ON A SITE BY SITE BASIS.



FRONT ELEVATION (CABINET INTERIOR)

MMBTS INTERIOR DETAIL

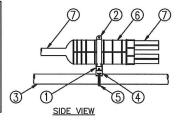
SCALE: N.T.S.

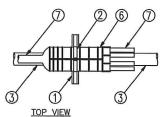
LEGEND: 1. P1000T-HG UNISTRUT,

12" LONG.
2. 6" PIPE HANGER.
3. EXISTING SUPPORT PIPE.
4. NEW STANDOFF BRACKET, ANDREW PART# 30848-4.
5. NEW ROUND MEMBER

ADAPTER SIZED FOR EXISTING PIPE SUPPORT. BREAKOUT UNIT.









RFS HYBRIFLEX RISER CABLES SCHEDULE

Fiber Only (Existing DC Power)	Hybrid cable MN: H8058-M12-050F 12x multi-mode fiber pairs, Top: Outdoor protected connectors, Bottom:LC Connectors, 5/8 cable, 50ft	50 ft
	MN: HB058-M12-075F	75 ft
	MN: HB058-M12-100F	100 ft
	MN:HB058-M12-125F	125 ft
	MN:HB058-M12-150F	150 ft
	MN:HB058-M12-175F	175 ft
	MN:HB058-M12-200F	200 ft

ær	Hybrid cable MN: H8114-08U3M12-050F 3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors. 1 1/4 cable. 50ft	50 ft
8 AWG Power	MN: HB114-08U3M12-075F	75 ft
Š	MN: HB114-08U3M12-100F	100 ft
¥.	MN: HB114-08U3M12-125F	125 ft
	MN: HB114-08U3M12-150F	150 ft
	MN: HB114-08U3M12-175F	175 ft
	MN: HB114-08U3M12-200F	200 ft

AWG Power	Hybrid cable MN: HB114-13U3M12-225F 3x 6 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 11/4 cable, 225ft	225 ft
₹	MN: HB114-13U3M12-250F	250 ft
9	MN: HB114-13U3M12-275F	275 ft
	MN: HB114-13U3M12-300F	300 ft

AWG Power	Hybrid cable MN: HB114-21U3M12-225F 3x 6 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 225ft	325 ft
4 A	MN: HB114-21U3M12-350F	350 ft
	MN: HB114-21U3M12-375F	375 ft

RFS HYBRIFLEX JUMPER CABLE SCHEDULE

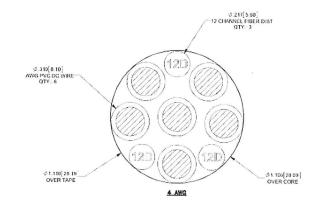
	Hybrid Jumper cable	
1	MN: HBF012-M3-5F1	5 ft
	5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable	
Fiber Only	MN: HBF012-M3-10F1	10 ft
per l	MN: HBF012-M3-15F1	15 ft
ᄄ	MN: HBF012-M3-20F1	20 ft
	MN: HBF012-M3-25F1	25 ft
	MN: HBF012-M3-30F1	30 ft

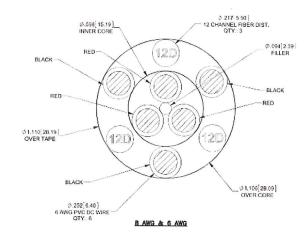
8 AWG Power	Hybrid Jumper cable MN: HBF058-08U1M3-5F1 5ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
9	MN: HBF058-08U1M3-10F1	10 ft
§ §	MN: HBF058-08U1M3-15F1	15 ft
∞ .	MN: HBF058-08U1M3-20F1	20 ft
	MN: HBF058-08U1M3-25F1	25 ft
	MN: HBF058-08U1M3-30F1	30 ft

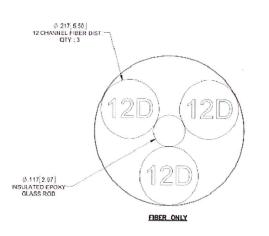
6 AWG Power	Hybrid Jumper cable MN: HBF058-13UJIM3-5F1 5ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
g g	MN: HBF058-13U1M3-10F1	10 ft
₹	MN: HBF058-13U1M3-15F1	15 ft
9	MN: HBF058-13U1M3-20F1	20 ft
	MN: HBF058-13U1M3-25F1	25 ft
	MN: HBF058-13U1M3-30F1	30 ft

Power	Hybrid Jumper cable MN: HBF078-21UJIM3-SF1 Sft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 7/8 cable	5 ft
9	MN: HBF078-21U1M3-10F1	10 ft
AWG	MN: HBF078-21U1M3-15F1	15 ft
4	MN: HBF078-21U1M3-20F1	20 ft
	MN: HBF078-21U1M3-25F1	25 ft
	MN: HBF078-21U1M3-30F1	20 ft

HYBRID CABLE	DC CONDUCTO	R SIZE GUIDELINE	
MANUF:	RFS	A .	
CABLE	LENGTH	DC CONDUCTOR	CABLE DIAMETER
FIBER ONLY	VARIES	USE NV HYBRIFLEX	7/8"
HYBRIFLEX	<200'	8 AWG	1-1/4"
HYBRIFLEX	225-300'	6 AWG	1-1/4"
HYBRIFLEX	325-375'	4 AWG	1-1/4"













TECTONIC Engineering & Surveying Consultants P.C.

1279 Route 300 Newburgh, NY 12550 Phone: (845) 567-6656 Fax: (845) 567-8703 www.tectonicengineering.com

	SL	JBMITTALS					
PRO	DJECT NO	: 7225.CT54XC7I6					
NO DATE DESCRIPTION							
0	07/14/14	FOR COMMENT	M				
Î.	11/21/14	FOR CONSTRUCTION	М				

DATE REVIEWED BY



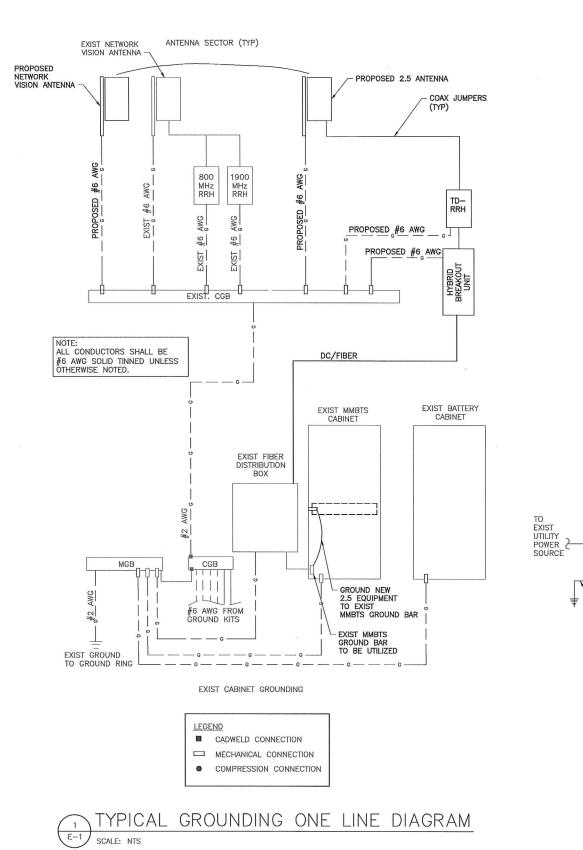
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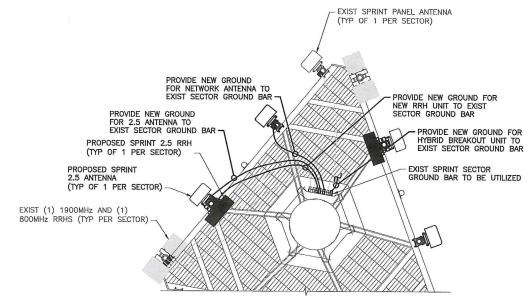
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SHEET TITLE: EQUIPMENT SCHEMATIC DETAILS

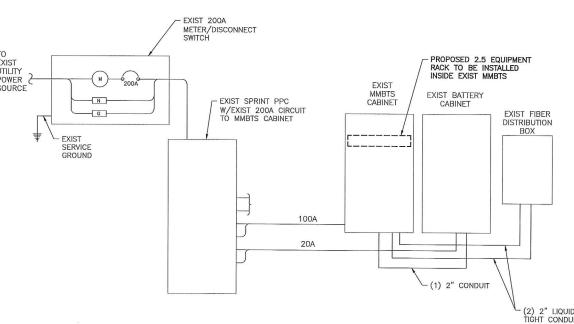
SHEET NO:

S-2





TYPICAL ANTENNA GROUNDING PLAN



SCALE: NTS





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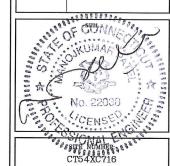
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SUBMITTALS PROJECT NO: 7225.CT54XC716 NO DATE DESCRIPTION BY 0 07/14/14 FOR COMMENT MP 1 11/21/14 FOR CONSTRUCTION MP

DATE REVIEWED BY



SITE NAME: NEWTOWN GEORGIA

PACIFIC/VS
SITE ADDRESS:

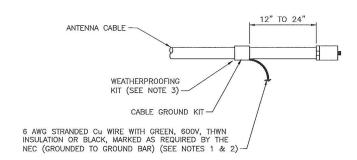
201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

ELECTRICAL & GROUNDING PLANS

SHEET NO:

E-1



CONNECTION OF CABLE GROUND KIT TO ANTENNA CABLE

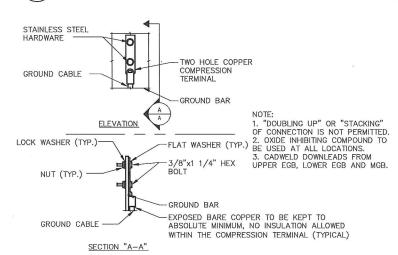
DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO

GROUNDING KIT SHALL BE TYPE AND PART NUMBER AS SUPPLIED OR RECOMMENDED BY CABLE

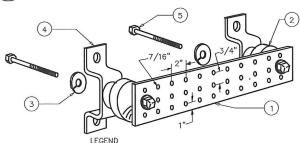
WEATHER PROOFING SHALL BE (TYPE AND PART NUMBER) AS SUPPLIED OR RECOMMENDED BY CABLE MANUFACTURER AND APPROVED BY CONTRACTOR.

CABLE GROUNDING KIT DETAIL

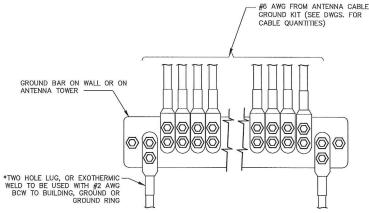
SCALE: N.T.S.



GROUNDING BAR CONN. DETAIL E-2



- INSULATORS, NEWTON INSTRUMENT CAT. NO. 3061-4 OR EQUAL
- 5/8" LOCKWASHERS OR EQUAL
- 4- WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT NO. A-6056 OR EQUAL
- 5- 5/8-11 X 1" H.H.C.S.BOLTS



- \star GROUND BARS AT THE BOTTOM OF TOWERS/MONOPOLES SHALL ONLY USE EXOTHERMIC WELDS.
- ATTACH "DO NOT DISCONNECT" LABELS TO GROUND BARS, CAN USE BRASS TAG "DO NOT DISCONDECT" AT EACH HYBRID GROUND POINT OR BACK-A-LITE PLATE LABEL ON GROUND BAR.
- CONNECT SEQUENCE- BOLT/WASHER/NO-OX/GROUND BAR/NO-OX/WASHER/LOCK-WASHER/NUT. THIS IS REPEATED FOR EACH

ANTENNA GROUND BAR DETAIL SCALE: NTS

GROUNDING NOTES:

- 1. GROUNDING SHALL BE IN ACCORDANCE WITH NEC ARTICLE 250-GROUNDING AND BONDING.
- 2. ALL GROUND WIRES SHALL BE #2 AWG UNLESS NOTED OTHERWISE.
- 3. ALL GROUNDING WIRES SHALL PROVIDE A STRAIGHT, DOWNWARD PATH TO GROUND WITH GRADUAL BENDS AS REQUIRED. GROUND WIRES SHALL NOT BE LOOPED OR SHARPLY BENT.
- 4. EACH EQUIPMENT CABINET SHALL BE CONNECTED TO THE MASTER ISOLATION GROUND BAR (MGB) WITH #2 AWG INSULATED STRANDED COPPER WIRE. EQUIPMENT CABINETS WALL HAVE (2)
- PROVIDE DEDICATED #2 AWG COPPER GROUND WIRE FROM EACH ANTENNA MOUNTING PIPE
- 6. THE CONTRACTOR SHALL VERIFY THAT THE EXISTING GROUND BARS HAVE ENOUGH SPACE/HOLES FOR ADDITIONAL TWO HOLE LUGS.
- 7. ALL CONDUITS SHALL BE RIGID GALVANIZED STEEL AND SHALL BE PROVIDED WITH
- 8. PROVIDE GROUND CONNECTIONS FOR ALL METALLIC STRUCTURES, ENCLOSURES, RACEWAYS AND OTHER CONDUCTIVE ITEMS ASSOCIATED WITH THE INSTALLATION OF CARRIER'S EQUIPMENT.
- 9. WHEN CABLE LENGTH IS OVER 20' THE MANUFACTURERS GROUND KIT MUST BE INSTALLED PER THE MANUFACTURERS SPECIFICATIONS.
- 10. REFER TO "ANTI-THEFT UPDATE TO SPRINT GROUNDING 082412.PDF" FOR GUIDELINE TO SUSPECTED OR ACTUAL THEFT OF GROUNDING
- 11. HOME RUN GROUNDS ARE NOT APPROVED BY CROWN CASTLE CONSTRUCTION STANDARDS AND THAT ANTENNA BUSS BARS SHOULD BE INSTALLED DIRECTLY TO TOWER STEEL WITHOUT INSULATORS OR DOWN CONDUCTORS.

PROTECTIVE GROUNDING SYSTEM GENERAL NOTES:

- 1. AT ALL TERMINATIONS AT EQUIPMENT ENCLOSURES, PANEL, AND FRAMES OF EQUIPMENT AND WHERE EXPOSED FOR GROUNDING. CONDUCTOR TERMINATION SHALL BE PERFORMED UTILIZING TWO HOLE BOLTED TONGUE COMPRESSION TYPE LUGS WITH STAINLESS STEEL SELF—TAPPING SCREWS.
- 2. ALL CLAMPS AND SUPPORTS USED TO SUPPORT THE GROUNDING SYSTEM CONDUCTORS AND PVC CONDUITS SHALL BE PVC TYPE (NON CONDUCTIVE). DO NOT USE METAL BRACKETS OR SUPPORTS WHICH WOULD FORM A COMPLETE RING AROUND ANY GROUNDING CONDUCTOR.
- 3. ALL GROUNDING CONNECTIONS SHALL BE COATED WITH A COPPER SHIELD ANTI-CORROSIVE AGENT SUCH AS T&B KOPR SHIELD. VERIFY PRODUCT WITH PROJECT MANAGER.
- 4. ALL BOLTS, WASHERS, AND NUTS USED ON GROUNDING CONNECTIONS SHALL BE STAINLESS STEEL.
- 5. INSTALL GROUND BUSHING ON ALL METALLIC CONDUITS AND BOND TO THE EQUIPMENT GROUND BUS IN THE PANEL BOARD.
- 6. GROUND ANTENNA BASES, FRAMES, CABLE RACKS, AND OTHER METALLIC COMPONENTS WITH #2 INSULATED TINNED STRANDED COPPER GROUNDING CONDUCTORS AND CONNECT TO INSULATED SURFACE MOUNTED GROUND BARS. CONNECTION DETAILS SHALL FOLLOW MANUFACTURER'S
- 7. GROUND HYBRID CABLE SHIELD AT BOTH ENDS USING MANUFACTURER'S GUIDELINES.

ELECTRICAL AND GROUNDING NOTES

- 1. ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) AS WELL AS APPLICABLE STATE AND LOCAL CODES.
- 2. ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED AND PROCURED PER SPECIFICATION REQUIREMENTS.
- 3. ELECTRICAL AND TELCO WIRING OUTSIDE A BUILDING AND EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUITS OR SCHEDULE 80 PVC (AS PERMITTED BY CODE) AND WHERE REQUIRED IN LIQUID TIGHT FLEXIBLE METAL OR NONMETALLIC CONDUITS.
- 4. BURIED CONDUIT SHALL BE SCHEDULE 40 PVC.
- 5. ELECTRICAL WIRING SHALL BE COPPER WITH TYPE XHHW, THWN, OR THNN
- 6. RUN TELCO CONDUIT OR CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT AND PROJECT OWNER CELL SITE TELCO CABINET AND BTS CABINET AS INDICATED ON THIS DRAWING PROVIDE FULL LENGTH PULL ROPE IN INSTALLED TELCO
- 7. WHERE CONDUIT BETWEEN BTS AND PROJECT OWNER CELL SITE PPC AND BETWEEN BTS AND PROJECT OWNER CELL SITE TELCO SERVICE CABINET ARE UNDERGROUND USE PVC, SCHEDULE 40 CONDUIT. ABOVE THE GROUND PORTION OF THESE CONDUITS SHALL BE PVC CONDUIT.
- 8. ALL EQUIPMENT LOCATED OUTSIDE SHALL HAVE NEMA 3R ENCLOSURE.
- 9. GROUNDING SHALL COMPLY WITH NEC ART, 250.
- 10. GROUND HYBRID CABLE SHIELDS AT 3 LOCATIONS USING MANUFACTURER'S HYBRID CABLE GROUNDING KITS SUPPLIED BY PROJECT OWNER.
- 11. USE #2 COPPER STRANDED WIRE WITH GREEN COLOR INSULATION FOR ABOVE GRADE GROUNDING (UNLESS OTHERWISE SPECIFIED) AND #2 SOLID TINNED BARE COPPER WIRE FOR BELOW GRADE GROUNDING AS INDICATED ON THE DRAWING.
- 12. ALL GROUND CONNECTIONS TO BE BURNDY HYGROUND COMPRESSION TYPE CONNECTORS OR CADWELD EXOTHERMIC WELD. DO NOT ALLOW BARE COPPER WIRE TO BE IN CONTACT WITH GALVANIZED STEEL.
- 13. ROUTE GROUNDING CONDUCTORS ALONG THE SHORTEST AND STRAIGHTEST PATH POSSIBLE, EXCEPT AS OTHERWISE INDICATED. GROUNDING LEADS SHOULD NEVER BE BENT AT RIGHT ANGLE. ALWAYS MAKE AT LEAST 12" RADIUS BENDS. #2 WIRE CAN BE BENT AT 6" RADIUS WHEN NECESSARY. BOND ANY METAL OBJECTS WITHIN 6 FEET OF PROJECT OWNER EQUIPMENT OR CABINET TO MASTER GROUND BAR OR
- 14. CONNECTIONS TO GROUND BARS SHALL BE MADE WITH TWO HOLE COMPRESSION TYPE COPPER LUGS. APPLY OXIDE INHIBITING COMPOUND TO ALL LOCATIONS.
- 15. APPLY OXIDE INHIBITING COMPOUND TO ALL COMPRESSION TYPE GROUND
- 16. BOND ANTENNA MOUNTING BRACKETS, HYBRID CABLE GROUND KITS, AND RRHs TO EGB PLACED NEAR THE ANTENNA LOCATION.
- 17. BOND ANTENNA EGB'S AND MGB TO GROUND RING.
- 18. CONTRACTOR SHALL TEST COMPLETED GROUND SYSTEM AND RECORD RESULT FOR PROJECT CLOSE-OUT DOCUMENTATION. 5 OHMS MINIMUM RESISTANCE REQUIRED
- 19. CONTRACTOR SHALL CONDUCT ANTENNA, HYBRID CABLES, GPS COAX AND RRH RETURN-LOSS AND DISTANCE- TO-FAULT MEASUREMENTS (SWEEP TESTS) AND RECORD RESULTS FOR PROJECT CLOSE OUT.
- 20. CONTRACTOR SHALL CHECK CAPACITY OF EXISTING SERVICE & PANEL ON SITE TO DETERMINE IF CAPACITY EXISTS TO ACCOMMODATE THE ADDED LOAD OF THIS PROJECT. ADVISE ENGINEER OF ANY DISCREPANCY.
- 21. LOCATION OF ALL OUTLET, BOXES, ETC, AND THE TYPE OF CONNECTION (PLUG OR DIRECT) SHALL BE CONFIRMED WITH THE OWNER'S REPRESENTATIVE PRIOR TO ROUGH-IN.
- 22. ELECTRICAL CHARACTERISTICS OF ALL EQUIPMENT (NEW AND EXISTING) SHALL BE FIELD VERIFIED WITH THE OWNERS REPRESENTATIVE AND EQUIPMENT SUPPLIER PRIOR TO ROUGH—IN OF CONDUIT AND WIRE. ALL EQUIPMENT SHALL BE PROPERLY CONNECTED ACCORDING TO THE NAMEPLATE DATA FURNISHED ON THE EQUIPMENT.





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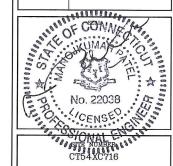
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	SL	JBMITTALS	
PRO	DJECT NO	7225.CT54XC7I6	
NO	DATE	DESCRIPTION	В
0	07/14/14	FOR COMMENT	М
1	11/21/14	FOR CONSTRUCTION	٢

DATE REVIEWED BY



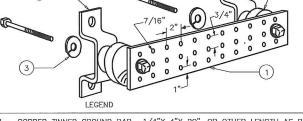
SITE NAME: NEWTOWN GEORGIA PACIFIC/VS

SITE ADDRESS: 201 SOUTH MAIN STREET NEWTOWN, CT 06470

SHEET TITLE:

GROUNDING DETAILS & NOTES

SHEET NO:



1- COPPER TINNED GROUND BAR, 1/4"X 4"X 20", OR OTHER LENGTH AS REQUIRED, HOLE CENTERS TO MATCH NEMA DOUBLE LUG CONFIGURATION

SCALE: NTS

ALL BOLTS, NUTS, WASHERS AND LOCK WASHERS SHALL BE 18-8

GROUNDING BAR DETAIL E-2 SCALE: NTS



Date: June 19, 2014

Darcy Tarr Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277

Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215 614.221.6679

Subject:

Structural Analysis Report

Carrier Designation:

Sprint PCS Co-Locate Carrier Site Number:

2.5 SCENARIO B

Carrier Site Name:

CT54XC716 N/A

Crown Castle BU Number:

826222

Crown Castle Site Name:

Newtown/RT-25

Crown Castle JDE Job Number: Crown Castle Work Order Number: 290762 781681

Crown Castle Application Number:

246082 Rev. 1

Engineering Firm Designation:

Crown Castle Designation:

Paul J Ford and Company Project Number: 37513-1642.002.7805

Site Data:

201 Main Street, Newtown, Fairfield County, CT Latitude 41° 22' 41.32", Longitude -73° 16' 26.94"

150 Foot - Monopole Tower

Dear Darcy Tarr,

Paul J Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 659210, in accordance with application 246082, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Existing + Reserved + Proposed Equipment & Modifications Note: See Table I and Table II for the proposed and existing/reserved loading, respectively. **Sufficient Capacity**

The structural analysis was performed for this tower in accordance with the requirements of the 2005 Connecticut Building Code and the TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

All modifications and equipment proposed in this report shall be installed in accordance with the proposed modifications drawings, referenced in Table 3 of this report, for the determined available structural capacity to be effective.

We at Paul J Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Seth Treaming Seth Tschanen Structural Designer

tnxTower Report - version 6.1.4.1

JUN 2 0 2014



Date: June 19, 2014

Darcy Tarr Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277 Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215

614.221.6679

Subject: Structural Analysis Report

Carrier Designation: Sprint PCS Co-Locate 2.5 SCENARIO B

Carrier Site Number: CT54XC716

Carrier Site Name: N/A

Crown Castle Designation: Crown Castle BU Number: 826222

Crown Castle Site Name: Newtown/RT-25

Crown Castle JDE Job Number: 290762
Crown Castle Work Order Number: 781681
Crown Castle Application Number: 246082 Rev. 1

Engineering Firm Designation: Paul J Ford and Company Project Number: 37513-1642.002.7805

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Respectfully submitted by:

Seth Tschanen Structural Designer

tnxTower Report - version 6.1.4.1

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tnxTower Output

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7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 150 ft Monopole tower designed by PIROD MANUFACTURES INC. in October of 2000. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of the 2005 Connecticut Building Code and the TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Flevation	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
	140.0	3	alcatel lucent	1900MHz RRH			
		3	alcatel lucent	800MHZ RRH			
	137.0	3	alcatel lucent	TD-RRH8x20-25			
140.0		137.0	6	rfs celwave	APXVSPP18-C-A20 w/ Mount Pipe	4	1 1/4
		3	rfs celwave	APXVTM14-C-120 w/ Mount Pipe			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note				
150.0		andrew	HP4-102			3					
			3	ericsson	ERICSSON AIR 21 B2A B4P w/ Mount Pipe						
148.0	148.0	3	ericsson	ERICSSON AIR 21 B4A B2P w/ Mount Pipe	7	1 5/8	2				
		3	ericsson	KRY 112 144/1			İ				
		1	1 tower mounts Sector Mount [SM 408-3]		18	1 5/8	1				
	140.0	140.0 3			6	decibel	DB980F90E-M w/ Mount Pipe	6	1 5/8	3	
140.0			3	decibel	DB980F90T2E-M w/ Mount Pipe	0	1 3/6	3			
		1	tower mounts	Platform Mount [LP 303-1]			1				
				3	alcatel lucent	RRH2x40-AWS					
									1	antel	BXA-70063/4CF w/ Mount Pipe
		3	kathrein	742 213 w/ Mount Pipe							
127.0	127.0	1	rfs celwave	DB-B1-6C-8AB-0Z							
			1	antel	BXA-171063-12BF w/ Mount Pipe	12	1 5/8	1			
		2	antel	BXA-171063/8CF w/ Mount Pipe	12	1 3/6	1				

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note		
127.0		6	rfs celwave	APL866513-42T0 w/ Mount Pipe					
	127.0	6	rfs celwave	FD9R6004/2C-3L			1		
	127.0	127.0	127.0	2	swedcom	SLCP 2x6014 w/ Mount Pipe			
		1	tower mounts	Platform Mount [LP 304-1]					
			6	ericsson	RRUS-11				
		3	powerwave technologies	7770.00 w/ Mount Pipe	1	3/4			
110.0	110.0	6 powerwave LGP21401	2	7/0	1				
		3	powerwave technologies	P65-16-XLH-RR w/ Mount Pipe	2	7/8			
		1	raycap	DC6-48-60-18-8F	6	1 1/4			
		1	tower mounts	Platform Mount [LP 303-1]	U				

Notes:

- 1) Existing Equipment
- 2) Reserved Equipment
 3) Equipment To Be Ren
- 3) Equipment To Be Removed Not Considered in this Analysis

Table 3 - Design Antenna and Cable Information

Mount Level	(64)	Number of Antennas	Antenna Manufacturer	Number of Feed Lines	

3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Dr. Clarence Welti Geotechnica Engineering, 10/16/2000	3536527	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Pirod, A-117711-F-1001206, 10/17/2000	3536528	CCISITES
PROPOSED MODIFICATION DRAWINGS	PJF, 37513-1642 BP, 8/20/2013	3963744	CCISITES

3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- Monopole will be reinforced in conformance with the reference modification drawings by PJF dated 8/20/2013.
- 5) Micropile will be relocated in conformance with Rich Hoffman's requested location in email to Rich Taschek on 4/16/2013.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	PINI	SF*P_allow (K)	% Capacity	Pass / Fail
L1	150 - 133	Pole	TP26x21.83x0.25	1	-4.66	1032.38	10.5	Pass
L2	133 - 98.45	Pole	TP34.0625x24.7764x0.3125	2	-12.83	1691.15	49.8	Pass
L3	98.45 - 64.8	Pole	TP41.75x32.4841x0.375	3	-19.67	2488.32	63.2	Pass
L4	64.8 - 32	Pole	TP49.0625x39.8387x0.375	4	-27.80	2928.95	74.3	Pass
L5	32 - 0	Pole	TP56.125x46.9597x0.375	5	-38.78	3394.28	82.0	Pass
							Summary	
						Pole (L5)	82.0	Pass
						Rating =	82.0	Pass

Table 6 - Tower Component Stresses vs. Capacity - LC4.7

auto o Torrei Compension Curación Cupación, 10 m									
Notes	Component	Elevation (ft)	% Capacity	Pass / Fail					
1	Anchor Rods	0	77.2	Pass					
1	Base Plate	0	82.0	Pass					
1	Base Foundation Steel	0	99.6	Pass					
1,2	Base Foundation Soil Interaction	0	19.0	Pass					
1	Micropile	0	87.1	Pass					

Structure Rating (max from all components) =	99.6%
--	-------

Notes:

4.1) Recommendations

- Reinforce the monopole in conformance with the referenced proposed modification drawings by PJF dated 8/20/2013.
- Relocate micropile in conformance with Rich Hoffman's requested location in email to Rich Taschek on 4/16/2013.

¹⁾ See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity

²⁾ Foundation capacity determined by comparing analysis reactions to original design reactions.

APPENDIX A TNXTOWER OUTPUT

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in Fairfield County, Connecticut.
- Basic wind speed of 85 mph.
- Nominal ice thickness of 0.7500 in. 3)
- Ice thickness is considered to increase with height.
- 5) Ice density of 56.00 pcf.
- 6) A wind speed of 38 mph is used in combination with ice.
- 7) Deflections calculated using a wind speed of 50 mph.
- 8) A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- 10) Stress ratio used in pole design is 1.333.
- 11) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- Use Code Stress Ratios
- Use Code Safety Factors Guys
 - Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- Consider Feedline Torque Include Angle Block Shear Check Poles
- Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft	Sides	in	in	in	in	
L1	150.0000- 133.0000	17.0000	2.95	18	21.8300	26.0000	0.2500	1.0000	A572-65 (65 ksi)
L2	133.0000- 98.4500	37.5000	3.85	18	24.7764	34.0625	0.3125	0.1250	A572-65 (65 ksi)
L3	98.4500- 64.8000	37.5000	4.70	18	32.4841	41.7500	0.3750	1.5000	A572-65 (65 ksi)
L4	64.8000- 32.0000	37.5000	5.50	18	39.8387	49.0625	0.3750	0.1875	A572-65 (65 ksi)
L5	32.0000-0.0000	37.5000		18	46.9597	56.1250	0.3750	0.1875	A572-65 (65 ksi)

Tapered Pole Properties

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	w	w/t
	in	in^2	in^4	in	in	in^3	in^4	in^2	in	
L1	22.1668	17.1237	1007.4853	7.6609	11.0896	90.8492	2016.2962	8.5635	3.4021	13.608
	26.4011	20.4326	1711.6544	9.1412	13.2080	129.5922	3425.5610	10.2183	4.1360	16.544
L2	25.9004	24.2651	1834.7230	8.6847	12.5864	145.7703	3671.8603	12.1349	4.2066	13.461
	34.5880	33.4758	4817.4335	11.9812	17.3038	278.4040	9641.2058	16.7411	5.8410	18.691
L3	33.9512	38.2179	4978.0706	11.3987	16.5019	301.6659	9962.6915	19.1126	5.0572	13.486
	42.3941	49.2466	10650.9822	14.6881	21.2090	502.1916	21315.9793	24.6280	6.6880	17.835
1.4	41.6271	46.9716	9242.0494	14.0096	20.2380	456.6670	18496.2597	23,4903	6.8136	18.17

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	w	w/t
	in	in^2	in^4	in	in	in^3	in^4	in^2	in	
	49.8194	57.9503	17355.1378	17.2841	24.9238	696.3293	34733.1119	28.9807	8.4370	22.499
L5	49.0491	55.4474	15202.1423	16.5376	23.8555	637.2591	30424.2880	27.7290	8.0669	21.512
	56.9908	66.3564	26056.1506	19.7913	28.5115	913.8821	52146.5865	33.1845	9.6800	25.813

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade Adjus	st. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing	Stitch Bolt Spacing
ft	ft^2	in					Diagonals in	Horizontals in
L1 150.0000-	J			1	1	1		
133.0000								
L2 133.0000-				1	1	1		
98.4500								
L3 98.4500-				1	1	1		
64.8000								
L4 64.8000-				1	1	1		
32.0000								
L5 32.0000-				1	1	1		
0.0000								

Feed Line/Linear Appurtenances - Entered As Area

Description		Allow Shield	Component	Placement	Total		$C_A A_A$	Weight
	or Leg	Shield	Type	ft	Number		ft²/ft	plf
LDF7-50A(1-5/8")	C	No	Inside Pole	148.0000 - 0.0000	18	No Ice	0.0000	$\frac{p_{ij}}{0.82}$
LDI 1-30A(1-3/6)	C	NO	Hiside Fole	146.0000 - 0.0000	10	1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82
						2" Ice	0.0000	0.82
						4" Ice	0.0000	0.82
LDF7-50A(1-5/8")	С	No	Inside Pole	148.0000 - 0.0000	6	No Ice	0.0000	0.82
LDI 7-30A(1-3/6)	C	NO	Hiside Fole	146.0000 - 0.0000	U	1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82
						2" Ice	0.0000	0.82
						4" Ice	0.0000	0.82
MITHE	C	NI-	Inside Pole	148.0000 - 0.0000	1	No Ice	0.0000	1.07
MLE Hybrid	C	No	inside Pole	148.0000 - 0.0000	1			
Power/18Fiber RL 2(1						1/2" Ice	0.0000	1.07
5/8)						1" Ice	0.0000	1.07
						2" Ice	0.0000	1.07
***						4" Ice	0.0000	1.07
HB114-1-0813U4-M5J(С	No	Inside Pole	140.0000 - 0.0000	4	No Ice	0.0000	1.20
1 1/4")						1/2" Ice	0.0000	1.20
,						1" Ice	0.0000	1.20
						2" Ice	0.0000	1.20
						4" Ice	0.0000	1.20
***			G + (0 + 0)	127 0000 0 0000		N. 1	0.1000	0.02
LDF7-50A(1-5/8")	C	No	CaAa (Out Of	127.0000 - 0.0000	2	No Ice	0.1980	0.82
			Face)			1/2" Ice	0.2980	2.33
						1" Ice	0.3980	4.46
						2" Ice	0.5980	10.54
	_					4" Ice	0.9980	30.04
LDF7-50A(1-5/8")	C	No	CaAa (Out Of	127.0000 - 0.0000	10	No Ice	0.0000	0.82
			Face)			1/2" Ice	0.0000	2.33
						1" Ice	0.0000	4.46
						2" Ice	0.0000	10.54
						4" Ice	0.0000	30.04
HB158-1-08U8-S8J18(C	No	CaAa (Out Of	127.0000 - 0.0000	1	No Ice	0.0000	1.30
1-5/8)			Face)			1/2" Ice	0.0000	2.81
						1" Ice	0.0000	4.94
						2" Ice	0.0000	11.02
***						4" Ice	0.0000	30.52
LDF5-50A(7/8")	С	No	Inside Pole	110.0000 - 0.0000	2	No Ice	0.0000	0.33
LDI 3-30A(1/0)	C	140	maide i oie	110.0000 - 0.0000	2	1/2" Ice	0.0000	0.33
						1" Ice	0.0000	0.33
						2" Ice	0.0000	0.33
						4" Ice	0.0000	0.33
						+ 100	0.0000	0.55

Description	Face	Allow	Component	Placement	Total		$C_A A_A$	Weight
	or	Shield	Type		Number			
	Leg			ft			ft²/ft	plf
LDF6-50A(1-1/4")	С	No	Inside Pole	110.0000 - 0.0000	6	No Ice	0.0000	0.66
						1/2" Ice	0.0000	0.66
						1" Ice	0.0000	0.66
						2" Ice	0.0000	0.66
						4" Ice	0.0000	0.66
9776(3/4")	C	No	Inside Pole	110.0000 - 0.0000	1	No Ice	0.0000	0.31
						1/2" Ice	0.0000	0.31
						1" Ice	0.0000	0.31
						2" Ice	0.0000	0.31
						4" Ice	0.0000	0.31

Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft^2	ft^2	ft^2	ft^2	K
L1	150.0000-	A	0.000	0.000	0.000	0.000	0.00
	133.0000	В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.34
L2	133.0000-98.4500	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	11.306	1.26
L3	98.4500-64.8000	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	13.325	1.40
L4	64.8000-32.0000	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	12.989	1.37
L5	32.0000-0.0000	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	12.672	1.33

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	ft^2	ft^2	ft^2	ft^2	K
L1	150.0000-	A	0.893	0.000	0.000	0.000	0.000	0.00
	133.0000	В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.34
L2	133.0000-98.4500	A	0.871	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	21.504	2.44
L3	98.4500-64.8000	A	0.836	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	25.053	2.75
L4	64.8000-32.0000	A	0.785	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	23.953	2.62
L5	32.0000-0.0000	A	0.750	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	22.721	2.47

Feed Line Center of Pressure

Section	Elevation	CP_X	CP_Z	CP_X	CP_Z
				Ice	Ice
	ft	in	in	in	in
L1	150.0000-133.0000	0.0000	0.0000	0.0000	0.0000
L2	133.0000-98.4500	-0.3849	0.2222	-0.6322	0.3650
L3	98.4500-64.8000	-0.4567	0.2637	-0.7532	0.4349
L4	64.8000-32.0000	-0.4653	0.2686	-0.7702	0.4447
L5	32.0000-0.0000	-0.4715	0.2722	-0.7730	0.4463

Discrete Tower Loads

Description	Face	Offset	Offsets:	Azimuth	Placement		$C_A A_A$	$C_A A_A$	Weight
	or	Type	Horz	Adjustment			Front	Side	
	Leg		Lateral						
			Vert ft	0	ft		ft^2	ft^2	K
			ft		Ji		Ji	Ji	n
			ft						
ERICSSON AIR 21 B2A	A	From Leg	4.0000	0.00	148.0000	No Ice	6.8253	5.6424	0.11
B4P w/ Mount Pipe			0.00			1/2" Ice	7.3471	6.4800	0.17
			0.00			1" Ice	7.8631	7.2567	0.23
						2" Ice 4" Ice	8.9261 11.1755	8.8640 12.2932	0.38 0.81
ERICSSON AIR 21 B2A	В	From Leg	4.0000	0.00	148.0000	No Ice	6.8253	5.6424	0.81
B4P w/ Mount Pipe	Б	Trom Leg	0.00	0.00	110.0000	1/2" Ice	7.3471	6.4800	0.17
1			0.00			1" Ice	7.8631	7.2567	0.23
						2" Ice	8.9261	8.8640	0.38
EDIGGGGOV ATD AL DO L	~		4.0000	0.00	4.40.0000	4" Ice	11.1755	12.2932	0.81
ERICSSON AIR 21 B2A	C	From Leg	4.0000	0.00	148.0000	No Ice	6.8253	5.6424	0.11
B4P w/ Mount Pipe			0.00 0.00			1/2" Ice 1" Ice	7.3471 7.8631	6.4800 7.2567	0.17 0.23
			0.00			2" Ice	8.9261	8.8640	0.23
						4" Ice	11.1755	12.2932	0.81
ERICSSON AIR 21 B4A	A	From Leg	4.0000	0.00	148.0000	No Ice	6.8155	5.6334	0.11
B2P w/ Mount Pipe			0.00			1/2" Ice	7.3373	6.4717	0.17
			0.00			1" Ice	7.8532	7.2478	0.23
						2" Ice	8.9160	8.8537	0.38
ERICSSON AIR 21 B4A	В	From Leg	4.0000	0.00	148.0000	4" Ice No Ice	11.1650 6.8155	12.2804 5.6334	0.81 0.11
B2P w/ Mount Pipe	D	From Leg	0.00	0.00	146.0000	1/2" Ice	7.3373	5.0554 6.4717	0.11
B21 W/ Would Tipe			0.00			1" Ice	7.8532	7.2478	0.23
						2" Ice	8.9160	8.8537	0.38
						4" Ice	11.1650	12.2804	0.81
ERICSSON AIR 21 B4A	C	From Leg	4.0000	0.00	148.0000	No Ice	6.8155	5.6334	0.11
B2P w/ Mount Pipe			0.00			1/2" Ice	7.3373	6.4717	0.17
			0.00			1" Ice 2" Ice	7.8532 8.9160	7.2478 8.8537	0.23 0.38
						4" Ice	11.1650	12.2804	0.38
KRY 112 144/1	A	From Leg	4.0000	0.00	148.0000	No Ice	0.4083	0.2042	0.01
			0.00			1/2" Ice	0.4969	0.2733	0.01
			0.00			1" Ice	0.5941	0.3511	0.02
						2" Ice	0.8145	0.5326	0.03
VDV 110 144/1	ъ	г т	4.0000	0.00	1.40.0000	4" Ice	1.3590	0.9992	0.08
KRY 112 144/1	В	From Leg	4.0000 0.00	0.00	148.0000	No Ice 1/2" Ice	0.4083 0.4969	0.2042 0.2733	0.01 0.01
			0.00			1" Ice	0.5941	0.2733	0.01
			0.00			2" Ice	0.8145	0.5326	0.03
						4" Ice	1.3590	0.9992	0.08
KRY 112 144/1	C	From Leg	4.0000	0.00	148.0000	No Ice	0.4083	0.2042	0.01
			0.00			1/2" Ice	0.4969	0.2733	0.01
			0.00			1" Ice	0.5941	0.3511	0.02
						2" Ice 4" Ice	0.8145 1.3590	0.5326 0.9992	0.03 0.08
Sector Mount [SM 408-3]	C	None		0.00	148.0000	No Ice	22.4500	22.4500	1.02
Sector Mount [SM 100 3]	C	Tione		0.00	110.0000	1/2" Ice	33.5000	33.5000	1.47
						1" Ice	44.5500	44.5500	1.93
						2" Ice	66.6500	66.6500	2.84
						4" Ice	110.8500	110.8500	4.66
*** (2) ADVICED 19 C A20/	A	Enone I	4 0000	0.00	140,0000	No I	9.4075	6.0450	0.00
(2) APXVSPP18-C-A20 w/ Mount Pipe	A	From Leg	4.0000 0.00	0.00	140.0000	No Ice 1/2" Ice	8.4975 9.1490	6.9458 8.1266	0.08 0.15
Would I ipc			-3.00			1" Ice	9.7672	9.0212	0.13
			2.00			2" Ice	11.0311	10.8440	0.41
						4" Ice	13.6786	14.8507	0.91
(2) APXVSPP18-C-A20 w/	В	From Leg	4.0000	0.00	140.0000	No Ice	8.4975	6.9458	0.08
Mount Pipe			0.00			1/2" Ice	9.1490	8.1266	0.15
			-3.00			1" Ice	9.7672	9.0212	0.23
						2" Ice 4" Ice	11.0311 13.6786	10.8440 14.8507	0.41 0.91
(2) APXVSPP18-C-A20 w/	C	From Leg	4.0000	0.00	140.0000	No Ice	8.4975	6.9458	0.91
· /	~	200		2.00					

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		C_AA_A Front	C_AA_A Side	Weight
	Leg		Lateral Vert						
			ft ft	0	ft		ft^2	ft^2	K
Mount Pipe			ft 0.00			1/2" Ice	9.1490	8.1266	0.15
Would Tipe			-3.00			1" Ice	9.7672	9.0212	0.23
						2" Ice	11.0311	10.8440	0.41
APXVTM14-C-120 w/	A	From Leg	4.0000	0.00	140.0000	4" Ice No Ice	13.6786 7.1342	14.8507 4.9591	0.91 0.08
Mount Pipe	А	From Leg	0.00	0.00	140.0000	1/2" Ice	7.1342	5.7544	0.08
Troum Tipe			-3.00			1" Ice	8.1830	6.4723	0.19
						2" Ice	9.2563	8.0099	0.34
ADVI/TM14 C 120/	D	F I	4.0000	0.00	1.40.0000	4" Ice	11.5262	11.4120	0.75
APXVTM14-C-120 w/ Mount Pipe	В	From Leg	4.0000 0.00	0.00	140.0000	No Ice 1/2" Ice	7.1342 7.6618	4.9591 5.7544	0.08 0.13
Would Tipe			-3.00			1" Ice	8.1830	6.4723	0.19
						2" Ice	9.2563	8.0099	0.34
						4" Ice	11.5262	11.4120	0.75
APXVTM14-C-120 w/	C	From Leg	4.0000	0.00	140.0000	No Ice	7.1342	4.9591	0.08
Mount Pipe			0.00 -3.00			1/2" Ice 1" Ice	7.6618 8.1830	5.7544 6.4723	0.13 0.19
			-3.00			2" Ice	9.2563	8.0099	0.13
						4" Ice	11.5262	11.4120	0.75
1900MHz RRH	Α	From Leg	4.0000	0.00	140.0000	No Ice	2.9069	3.8014	0.04
			0.00			1/2" Ice	3.1446	4.0650	0.08
			0.00			1" Ice 2" Ice	3.3909 3.9094	4.3372 4.9076	0.11 0.19
						4" Ice	5.0502	6.1520	0.19
1900MHz RRH	В	From Leg	4.0000	0.00	140.0000	No Ice	2.9069	3.8014	0.04
			0.00			1/2" Ice	3.1446	4.0650	0.08
			0.00			1" Ice	3.3909	4.3372	0.11
						2" Ice 4" Ice	3.9094 5.0502	4.9076 6.1520	0.19 0.41
1900MHz RRH	C	From Leg	4.0000	0.00	140.0000	No Ice	2.9069	3.8014	0.41
170011112 1441	C	Trom Leg	0.00	0.00	110.0000	1/2" Ice	3.1446	4.0650	0.08
			0.00			1" Ice	3.3909	4.3372	0.11
						2" Ice	3.9094	4.9076	0.19
800MHZ RRH	A	From Leg	4.0000	0.00	140.0000	4" Ice No Ice	5.0502 2.4899	6.1520 2.0685	0.41 0.05
OUUVITIZ KKII	А	110III Leg	0.00	0.00	140.0000	1/2" Ice	2.7061	2.2705	0.03
			0.00			1" Ice	2.9310	2.4812	0.10
						2" Ice	3.4068	2.9284	0.16
0000 4117 PP11	ъ.	Б. т	4.0000	0.00	1.40.0000	4" Ice	4.4620	3.9265	0.32
800MHZ RRH	В	From Leg	4.0000 0.00	0.00	140.0000	No Ice 1/2" Ice	2.4899 2.7061	2.0685 2.2705	0.05 0.07
			0.00			1" Ice	2.9310	2.4812	0.07
						2" Ice	3.4068	2.9284	0.16
						4" Ice	4.4620	3.9265	0.32
800MHZ RRH	C	From Leg	4.0000	0.00	140.0000	No Ice	2.4899	2.0685	0.05
			0.00 0.00			1/2" Ice 1" Ice	2.7061 2.9310	2.2705 2.4812	0.07 0.10
			0.00			2" Ice	3.4068	2.9284	0.16
						4" Ice	4.4620	3.9265	0.32
TD-RRH8x20-25	A	From Leg	4.0000	0.00	140.0000	No Ice	4.7198	1.7027	0.07
			0.00			1/2" Ice	5.0138	1.9196	0.10
			-3.00			1" Ice 2" Ice	5.3165 5.9478	2.1453 2.6224	0.13 0.20
						4" Ice	7.3141	3.6805	0.40
TD-RRH8x20-25	В	From Leg	4.0000	0.00	140.0000	No Ice	4.7198	1.7027	0.07
		-	0.00			1/2" Ice	5.0138	1.9196	0.10
			-3.00			1" Ice	5.3165	2.1453	0.13
						2" Ice 4" Ice	5.9478 7.3141	2.6224 3.6805	0.20 0.40
TD-RRH8x20-25	С	From Leg	4.0000	0.00	140.0000	No Ice	4.7198	1.7027	0.40
	-	- 0	0.00			1/2" Ice	5.0138	1.9196	0.10
			-3.00			1" Ice	5.3165	2.1453	0.13
			-3.00			1" Ice 2" Ice 4" Ice	5.3165 5.9478 7.3141	2.1453 2.6224 3.6805	0.13 0.20 0.40

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C_AA_A Front	C_AA_A Side	Weight
			Vert ft ft ft	o	ft		ft ²	ft^2	K
			J.			1/2" Ice	18.8700	18.8700	1.48
						1" Ice	23.0800	23.0800	1.71
						2" Ice 4" Ice	31.5000 48.3400	31.5000 48.3400	2.18 3.10
***						4 100	40.3400	40.5400	3.10
(2) APL866513-42T0 w/	Α	From Leg	4.0000	0.00	127.0000	No Ice	4.5308	4.9208	0.03
Mount Pipe			0.00			1/2" Ice	4.9675	5.5962	0.08
			0.00			1" Ice 2" Ice	5.4135 6.3370	6.2837 7.7123	0.13 0.25
						4" Ice	8.3197	10.8330	0.23
(2) APL866513-42T0 w/	В	From Leg	4.0000	0.00	127.0000	No Ice	4.5308	4.9208	0.03
Mount Pipe		Č	0.00			1/2" Ice	4.9675	5.5962	0.08
			0.00			1" Ice	5.4135	6.2837	0.13
						2" Ice	6.3370	7.7123	0.25
(2) APL866513-42T0 w/	С	From Leg	4.0000	0.00	127.0000	4" Ice No Ice	8.3197 4.5308	10.8330 4.9208	0.60 0.03
Mount Pipe	C	110III Leg	0.00	0.00	127.0000	1/2" Ice	4.9675	5.5962	0.03
Troum Tipo			0.00			1" Ice	5.4135	6.2837	0.13
						2" Ice	6.3370	7.7123	0.25
(2) 2311 1510 (2) 257			4.0000	0.00	127 0000	4" Ice	8.3197	10.8330	0.60
(2) BXA-171063/8CF w/	A	From Leg	4.0000 0.00	0.00	127.0000	No Ice 1/2" Ice	3.1574 3.5312	3.3303 3.9423	0.03 0.06
Mount Pipe			0.00			1" Ice	3.9415	4.5633	0.00
			0.00			2" Ice	4.8273	5.8553	0.19
						4" Ice	6.7342	8.8407	0.48
(2) SLCP 2x6014 w/ Mount	В	From Leg	4.0000	0.00	127.0000	No Ice	7.4514	6.9545	0.04
Pipe			0.00 0.00			1/2" Ice 1" Ice	7.9606 8.4698	7.7563	0.10 0.18
			0.00			2" Ice	9.5191	8.5195 10.0997	0.18
						4" Ice	11.7421	13.4750	0.80
BXA-171063-12BF w/	C	From Leg	4.0000	0.00	127.0000	No Ice	4.9710	5.2283	0.04
Mount Pipe			0.00			1/2" Ice	5.5211	6.3892	0.09
			0.00			1" Ice 2" Ice	6.0361 7.0911	7.2610	0.14 0.27
						4" Ice	9.3593	9.0462 12.8165	0.27
(2) FD9R6004/2C-3L	Α	From Leg	4.0000	0.00	127.0000	No Ice	0.3665	0.0846	0.00
•		C	0.00			1/2" Ice	0.4506	0.1362	0.01
			0.00			1" Ice	0.5433	0.1965	0.01
						2" Ice 4" Ice	0.7546 1.2808	0.3430 0.7396	0.02 0.06
(2) FD9R6004/2C-3L	В	From Leg	4.0000	0.00	127.0000	No Ice	0.3665	0.7396	0.00
(2) 12 311000 1,20 32	-	Trom Log	0.00	0.00	127.0000	1/2" Ice	0.4506	0.1362	0.01
			0.00			1" Ice	0.5433	0.1965	0.01
						2" Ice	0.7546	0.3430	0.02
(2) FD9R6004/2C-3L	C	From Leg	4.0000	0.00	127.0000	4" Ice No Ice	1.2808 0.3665	0.7396 0.0846	0.06 0.00
(2) FD9K0004/2C-3L	C	Fiolii Leg	0.00	0.00	127.0000	1/2" Ice	0.3663	0.0846	0.00
			0.00			1" Ice	0.5433	0.1965	0.01
						2" Ice	0.7546	0.3430	0.02
						4" Ice	1.2808	0.7396	0.06
742 213 w/ Mount Pipe	A	From Leg	4.0000	0.00	127.0000	No Ice	5.3729 5.9502	4.6203	0.05 0.09
			0.00			1/2" Ice 1" Ice	6.5014	6.0004 6.9816	0.09
			0.00			2" Ice	7.6106	8.8524	0.13
						4" Ice	9.9329	12.7940	0.68
742 213 w/ Mount Pipe	В	From Leg	4.0000	0.00	127.0000	No Ice	5.3729	4.6203	0.05
			0.00 0.00			1/2" Ice 1" Ice	5.9502 6.5014	6.0004	0.09
			0.00			2" Ice	7.6106	6.9816 8.8524	0.15 0.28
						4" Ice	9.9329	12.7940	0.68
742 213 w/ Mount Pipe	C	From Leg	4.0000	0.00	127.0000	No Ice	5.3729	4.6203	0.05
			0.00			1/2" Ice	5.9502	6.0004	0.09
			0.00			1" Ice	6.5014	6.9816	0.15
						2" Ice	7.6106	8.8524	0.28

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft	o	ft		ft^2	ft ²	K
BXA-70063/4CF w/ Mount	C	From Leg	4.0000	0.00	127.0000	No Ice	5.3988	3.6158	0.03
Pipe			0.00			1/2" Ice	5.8435	4.2169	0.07
			0.00			1" Ice	6.2986	4.8343	0.12
						2" Ice	7.2405	6.1609	0.23
DDIIA 40 ANIG		Б. Т	4.0000	0.00	127 0000	4" Ice	9.2612	9.1826	0.57
RRH2x40-AWS	Α	From Leg	4.0000	0.00	127.0000	No Ice	2.5217	1.5894 1.7953	0.04
			0.00 0.00			1/2" Ice 1" Ice	2.7530 2.9930	2.0098	0.06 0.08
			0.00			2" Ice	3.4990	2.4648	0.08
						4" Ice	4.6146	3.4785	0.28
RRH2x40-AWS	В	From Leg	4.0000	0.00	127.0000	No Ice	2.5217	1.5894	0.04
		Ç	0.00			1/2" Ice	2.7530	1.7953	0.06
			0.00			1" Ice	2.9930	2.0098	0.08
						2" Ice	3.4990	2.4648	0.13
	_					4" Ice	4.6146	3.4785	0.28
RRH2x40-AWS	C	From Leg	4.0000	0.00	127.0000	No Ice	2.5217	1.5894	0.04
			0.00			1/2" Ice 1" Ice	2.7530 2.9930	1.7953 2.0098	0.06 0.08
			0.00			2" Ice	3.4990	2.4648	0.08
						4" Ice	4.6146	3.4785	0.28
DB-B1-6C-8AB-0Z	C	From Leg	4.0000	0.00	127.0000	No Ice	5.6000	2.3333	0.04
		Ç	0.00			1/2" Ice	5.9154	2.5580	0.08
			0.00			1" Ice	6.2395	2.7914	0.12
						2" Ice	6.9136	3.2840	0.21
DI . 6	~			0.00	127 0000	4" Ice	8.3654	4.3728	0.45
Platform Mount [LP 304-1]	С	None		0.00	127.0000	No Ice	17.4600	17.4600	1.35
						1/2" Ice 1" Ice	22.4400 27.4200	22.4400 27.4200	1.62 1.90
						2" Ice	37.3800	37.3800	2.45
***						4" Ice	57.3000	57.3000	3.55
7770.00 w/ Mount Pipe	A	From Leg	4.0000	0.00	110.0000	No Ice	6.1194	4.2543	0.06
. , , , , , , , , , , , , , , , , , , ,			0.00			1/2" Ice	6.6258	5.0137	0.10
			0.00			1" Ice	7.1283	5.7109	0.16
						2" Ice	8.1643	7.1553	0.29
						4" Ice	10.3599	10.4117	0.66
7770.00 w/ Mount Pipe	В	From Leg	4.0000	0.00	110.0000	No Ice	6.1194	4.2543	0.06
			0.00 0.00			1/2" Ice 1" Ice	6.6258 7.1283	5.0137	0.10 0.16
			0.00			2" Ice	8.1643	5.7109 7.1553	0.16
						4" Ice	10.3599	10.4117	0.66
7770.00 w/ Mount Pipe	C	From Leg	4.0000	0.00	110.0000	No Ice	6.1194	4.2543	0.06
1		Ç	0.00			1/2" Ice	6.6258	5.0137	0.10
			0.00			1" Ice	7.1283	5.7109	0.16
						2" Ice	8.1643	7.1553	0.29
Dec 16 WHI DD /M			4.0000	0.00	110 0000	4" Ice	10.3599	10.4117	0.66
P65-16-XLH-RR w/ Mount	A	From Leg	4.0000	0.00	110.0000	No Ice	8.6375	6.3625	0.08
Pipe			0.00			1/2" Ice 1" Ice	9.2903 9.9098	7.5378 8.4270	0.14 0.22
			0.00			2" Ice	11.1763	10.2390	0.22
						4" Ice	13.8289	14.0988	0.89
P65-16-XLH-RR w/ Mount	В	From Leg	4.0000	0.00	110.0000	No Ice	8.6375	6.3625	0.08
Pipe		Ç	0.00			1/2" Ice	9.2903	7.5378	0.14
-			0.00			1" Ice	9.9098	8.4270	0.22
						2" Ice	11.1763	10.2390	0.39
Def 16 MH H DD 134	~		4.0000	0.00	110 0000	4" Ice	13.8289	14.0988	0.89
P65-16-XLH-RR w/ Mount	С	From Leg	4.0000	0.00	110.0000	No Ice	8.6375	6.3625	0.08
Pipe			0.00			1/2" Ice 1" Ice	9.2903 9.9098	7.5378	0.14
			0.00			2" Ice	9.9098	8.4270 10.2390	0.22 0.39
						4" Ice	13.8289	14.0988	0.89
(2) LGP21401	A	From Leg	4.0000	0.00	110.0000	No Ice	1.2880	0.2326	0.01
()	• =		0.00			1/2" Ice	1.4453	0.3134	0.02
			0.00			1" Ice	1.6112	0.4028	0.03
						2" Ice	1.9690	0.6076	0.05

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
			Vert ft ft ft	0	ft		ft ²	ft^2	K
						4" Ice	2.7882	1.1210	0.14
(2) LGP21401	В	From Leg	4.0000	0.00	110.0000	No Ice	1.2880	0.2326	0.01
			0.00			1/2" Ice	1.4453	0.3134	0.02
			0.00			1" Ice	1.6112	0.4028	0.03
						2" Ice	1.9690	0.6076	0.05
						4" Ice	2.7882	1.1210	0.14
(2) LGP21401	C	From Leg	4.0000	0.00	110.0000	No Ice	1.2880	0.2326	0.01
			0.00			1/2" Ice	1.4453	0.3134	0.02
			0.00			1" Ice	1.6112	0.4028	0.03
						2" Ice	1.9690	0.6076	0.05
						4" Ice	2.7882	1.1210	0.14
(2) RRUS-11	A	From Leg	4.0000	0.00	110.0000	No Ice	3.2486	1.3726	0.05
		_	0.00			1/2" Ice	3.4905	1.5510	0.07
			0.00			1" Ice	3.7411	1.7380	0.09
						2" Ice	4.2682	2.1381	0.15
						4" Ice	5.4260	3.0418	0.31
(2) RRUS-11	В	From Leg	4.0000	0.00	110.0000	No Ice	3.2486	1.3726	0.05
		_	0.00			1/2" Ice	3.4905	1.5510	0.07
			0.00			1" Ice	3.7411	1.7380	0.09
						2" Ice	4.2682	2.1381	0.15
						4" Ice	5.4260	3.0418	0.31
(2) RRUS-11	C	From Leg	4.0000	0.00	110.0000	No Ice	3.2486	1.3726	0.05
		_	0.00			1/2" Ice	3.4905	1.5510	0.07
			0.00			1" Ice	3.7411	1.7380	0.09
						2" Ice	4.2682	2.1381	0.15
						4" Ice	5.4260	3.0418	0.31
DC6-48-60-18-8F	A	From Leg	4.0000	0.00	110.0000	No Ice	2.5667	2.5667	0.02
		C	0.00			1/2" Ice	2.7978	2.7978	0.04
			0.00			1" Ice	3.0377	3.0377	0.07
						2" Ice	3.5432	3.5432	0.13
						4" Ice	4.6580	4.6580	0.30
Platform Mount [LP 303-1]	C	None		0.00	110.0000	No Ice	14.6600	14.6600	1.25
	-					1/2" Ice	18.8700	18.8700	1.48
						1" Ice	23.0800	23.0800	1.71
						2" Ice	31.5000	31.5000	2.18
						4" Ice	48.3400	48.3400	3.10

Tower Pressures - No Ice

 $G_H = 1.690$

Section	z	K_Z	q_z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					a				%	In	Out
					c					Face	Face
ft	ft		psf	ft^2	e	ft^2	ft^2	ft^2		ft^2	ft^2
L1 150.0000-	141.2530	1.515	28.02	33.880	A	0.000	33.880	33.880	100.00	0.000	0.000
133.0000			2		В	0.000	33.880		100.00	0.000	0.000
					C	0.000	33.880		100.00	0.000	0.000
L2 133.0000-	115.0815	1.429	26.40	85.755	Α	0.000	85.755	85.755	100.00	0.000	0.000
98.4500			2		В	0.000	85.755		100.00	0.000	0.000
					C	0.000	85.755		100.00	0.000	11.306
L3 98.4500-	81.2529	1.294	23.88	105.416	Α	0.000	105.416	105.416	100.00	0.000	0.000
64.8000			0		В	0.000	105.416		100.00	0.000	0.000
					C	0.000	105.416		100.00	0.000	13.325
L4 64.8000-	48.3113	1.115	20.51	123.078	Α	0.000	123.078	123.078	100.00	0.000	0.000
32.0000			4		В	0.000	123.078		100.00	0.000	0.000
					C	0.000	123.078		100.00	0.000	12.989
L5 32.0000-	15.6006	1	18.49	139.239	Α	0.000	139.239	139.239	100.00	0.000	0.000
0.0000			6		В	0.000	139.239		100.00	0.000	0.000
					C	0.000	139.239		100.00	0.000	12.672

Tower Pressure - With Ice

 $G_H = 1.690$

Section	Z	K_Z	q_z	t_Z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation						a				%	In	Out
						c					Face	Face
ft	ft		psf	in	ft^2	e	ft^2	ft^2	ft^2		ft^2	ft^2
L1 150.0000-	141.2530	1.515	5.483	0.8930	36.410	A	0.000	36.410	36.410	100.00	0.000	0.000
133.0000						В	0.000	36.410		100.00	0.000	0.000
						C	0.000	36.410		100.00	0.000	0.000
L2 133.0000-	115.0815	1.429	5.166	0.8713	90.897	A	0.000	90.897	90.897	100.00	0.000	0.000
98.4500						В	0.000	90.897		100.00	0.000	0.000
						C	0.000	90.897		100.00	0.000	21.504
L3 98.4500-	81.2529	1.294	4.673	0.8356	110.303	Α	0.000	110.303	110.303	100.00	0.000	0.000
64.8000						В	0.000	110.303		100.00	0.000	0.000
						C	0.000	110.303		100.00	0.000	25.053
L4 64.8000-	48.3113	1.115	4.014	0.7851	127.646	A	0.000	127.646	127.646	100.00	0.000	0.000
32.0000						В	0.000	127.646		100.00	0.000	0.000
						C	0.000	127.646		100.00	0.000	23.953
L5 32.0000-	15.6006	1	3.619	0.7500	143.426	A	0.000	143.426	143.426	100.00	0.000	0.000
0.0000						В	0.000	143.426		100.00	0.000	0.000
						C	0.000	143.426		100.00	0.000	22.721

Tower Pressure - Service

 $G_H = 1.690$

Section		ν		4	F	4	4	4	1	C 1	C 1
	Z	K_Z	q_z	A_G	Г	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					а				%	In	Out
					c					Face	Face
ft	ft		psf	ft^2	e	ft^2	ft^2	ft^2		ft^2	ft^2
L1 150.0000-	141.2530	1.515	9.696	33.880	Α	0.000	33.880	33.880	100.00	0.000	0.000
133.0000					В	0.000	33.880		100.00	0.000	0.000
					C	0.000	33.880		100.00	0.000	0.000
L2 133.0000-	115.0815	1.429	9.135	85.755	Α	0.000	85.755	85.755	100.00	0.000	0.000
98.4500					В	0.000	85.755		100.00	0.000	0.000
					C	0.000	85.755		100.00	0.000	11.306
L3 98.4500-	81.2529	1.294	8.263	105.416	Α	0.000	105.416	105.416	100.00	0.000	0.000
64.8000					В	0.000	105.416		100.00	0.000	0.000
					C	0.000	105.416		100.00	0.000	13.325
L4 64.8000-	48.3113	1.115	7.098	123.078	A	0.000	123.078	123.078	100.00	0.000	0.000
32.0000					В	0.000	123.078		100.00	0.000	0.000
					C	0.000	123.078		100.00	0.000	12.989
L5 32.0000-	15.6006	1	6.400	139.239	A	0.000	139.239	139.239	100.00	0.000	0.000
0.0000					В	0.000	139.239		100.00	0.000	0.000
					C	0.000	139.239		100.00	0.000	12.672

Load Combinations

Comb.	Description
No.	·
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice
tnyTow/	or Poport, version 6.1.4.1

Comb.	Description
No.	
15	Dead+Wind 0 deg+Ice
16	Dead+Wind 30 deg+Ice
17	Dead+Wind 60 deg+Ice
18	Dead+Wind 90 deg+Ice
19	Dead+Wind 120 deg+Ice
20	Dead+Wind 150 deg+Ice
21	Dead+Wind 180 deg+Ice
22	Dead+Wind 210 deg+Ice
23	Dead+Wind 240 deg+Ice
24	Dead+Wind 270 deg+Ice
25	Dead+Wind 300 deg+Ice
26	Dead+Wind 330 deg+Ice
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

Maximum Member Forces

Section	Elevation	Component	Condition	Gov.	Force	Major Axis	Minor Axis
No.	ft	Туре		Load		Moment	Moment
				Comb.	K	kip-ft	kip-ft
L1	150 - 133	Pole	Max Tension	5	0.00	0.00	0.00
			Max. Compression	14	-9.17	0.02	-0.01
			Max. Mx	11	-4.66	53.38	-0.02
			Max. My	8	-4.66	0.01	-53.36
			Max. Vy	11	-9.11	53.38	-0.02
			Max. Vx	8	9.11	0.01	-53.36
			Max. Torque	12			0.00
L2	133 - 98.45	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-23.52	1.71	-1.41
			Max. Mx	11	-12.84	557.44	-2.18
			Max. My	8	-12.86	2.43	-553.39
			Max. Vy	11	-20.43	557.44	-2.18
			Max. Vx	8	20.28	2.43	-553.39
			Max. Torque	4			-1.47
L3	98.45 - 64.8	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-32.82	4.06	-2.78
			Max. Mx	11	-19.67	1280.74	-5.06
			Max. My	8	-19.68	5.49	-1271.38
			Max. Vy	11	-23.64	1280.74	-5.06
			Max. Vx	8	23.48	5.49	-1271.38
			Max. Torque	4			-0.95
L4	64.8 - 32	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-43.39	6.67	-4.29
			Max. Mx	11	-27.80	2086.17	-7.91
			Max. My	8	-27.81	8.57	-2071.60
			Max. Vy	11	-26.58	2086.17	-7.91
			Max. Vx	8	26.43	8.57	-2071.60
			Max. Torque	11			0.97
L5	32 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-57.22	9.91	-6.16
			Max. Mx	11	-38.78	3143.18	-11.24
			Max. My	8	-38.78	12.23	-3122.56
			Max. Vy	11	-29.74	3143.18	-11.24
			Max. Vx	8	29.59	12.23	-3122.56
			Max. Torque	11	27.07	12.20	1.05

Maximum Reaction	
	9

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	K	K	K
		Comb.			
Pole	Max. Vert	14	57.22	-0.00	0.00
	Max. H _x	11	38.79	29.72	-0.08
	Max. H _z	2	38.79	-0.08	29.57
	Max. M _x	2	3119.89	-0.08	29.57
	Max. M _z	5	3138.36	-29.72	0.08
	Max. Torsion	11	1.05	29.72	-0.08
	Min. Vert	5	38.79	-29.72	0.08
	Min. H _x	5	38.79	-29.72	0.08
	Min. Hz	8	38.79	0.08	-29.57
	Min. M _x	8	-3122.56	0.08	-29.57
	Min. M _z	11	-3143.18	29.72	-0.08
	Min. Torsion	5	-1.05	-29.72	0.08

Tower Mast Reaction Summary

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, M _x	Overturning Moment, Mz	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	38.79	-0.00	0.00	1.30	2.26	0.00
Dead+Wind 0 deg - No Ice	38.79	0.08	-29.57	-3119.89	-7.57	0.09
Dead+Wind 30 deg - No Ice	38.79	14.92	-25.65	-2706.90	-1576.73	0.60
Dead+Wind 60 deg - No Ice	38.79	25.77	-14.85	-1567.97	-2722.77	0.95
Dead+Wind 90 deg - No Ice	38.79	29.72	-0.08	-8.57	-3138.36	1.05
Dead+Wind 120 deg - No Ice	38.79	25.70	14.72	1553.51	-2712.90	0.86
Dead+Wind 150 deg - No Ice	38.79	14.79	25.57	2699.70	-1559.60	0.45
Dead+Wind 180 deg - No Ice	38.79	-0.08	29.57	3122.56	12.23	-0.08
Dead+Wind 210 deg - No Ice	38.79	-14.92	25.65	2709.56	1581.39	-0.60
Dead+Wind 240 deg - No Ice	38.79	-25.77	14.85	1570.64	2727.42	-0.95
Dead+Wind 270 deg - No Ice	38.79	-29.72	0.08	11.24	3143.18	-1.05
Dead+Wind 300 deg - No Ice	38.79	-25.70	-14.72	-1550.83	2717.55	-0.87
Dead+Wind 330 deg - No Ice	38.79	-14.79	-25.57	-2697.02	1564.25	-0.45
Dead+Ice	57.22	0.00	-0.00	6.16	9.91	0.00
Dead+Wind 0 deg+Ice	57.22	0.01	-7.10	-774.68	8.07	-0.09
Dead+Wind 30 deg+Ice	57.22	3.58	-6.16	-671.04	-383.96	0.06
Dead+Wind 60 deg+Ice	57.22	6.18	-3.56	-385.92	-670.42	0.19
Dead+Wind 90 deg+Ice	57.22	7.13	-0.01	4.28	-774.55	0.27
Dead+Wind 120 deg+Ice	57.22	6.17	3.54	395.00	-668.46	0.28
Dead+Wind 150 deg+Ice	57.22	3.55	6.14	681.55	-380.56	0.21
Dead+Wind 180 deg+Ice	57.22	-0.01	7.10	787.15	12.00	0.09
Dead+Wind 210 deg+Ice	57.22	-3.58	6.16	683.51	404.02	-0.06
Dead+Wind 240 deg+Ice	57.22	-6.18	3.56	398.40	690.48	-0.19
Dead+Wind 270 deg+Ice	57.22	-7.13	0.01	8.20	794.61	-0.27
Dead+Wind 300 deg+Ice	57.22	-6.17	-3.54	-382.52	688.52	-0.28
Dead+Wind 330 deg+Ice	57.22	-3.55	-6.14	-669.07	400.62	-0.21
Dead+Wind 0 deg - Service	38.79	0.03	-10.23	-1079.54	-1.10	0.03
Dead+Wind 30 deg - Service	38.79	5.16	-8.87	-936.50	-544.49	0.21
Dead+Wind 60 deg - Service	38.79	8.92	-5.14	-542.10	-941.36	0.33
Dead+Wind 90 deg - Service	38.79	10.28	-0.03	-2.09	-1085.31	0.36
Dead+Wind 120 deg - Service	38.79	8.89	5.09	538.85	-937.94	0.30
Dead+Wind 150 deg - Service	38.79	5.12	8.85	935.76	-538.55	0.16
Dead+Wind 180 deg - Service	38.79	-0.03	10.23	1082.23	5.76	-0.03
Dead+Wind 210 deg - Service	38.79	-5.16	8.87	939.18	549.15	-0.21
Dead+Wind 240 deg - Service	38.79	-8.92	5.14	544.78	946.02	-0.33
Dead+Wind 270 deg - Service	38.79	-10.28	0.03	4.77	1089.96	-0.37
Dead+Wind 300 deg - Service	38.79	-8.89	-5.09	-536.16	942.59	-0.30
Dead+Wind 330 deg - Service	38.79	-5.12	-8.85	-933.07	543.21	-0.16

Solution	Summary
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	Sui	n of Applied Force	s		Sum of Reaction	ıs	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-38.79	0.00	0.00	38.79	0.00	0.000%
2	0.08	-38.79	-29.57	-0.08	38.79	29.57	0.005%
3	14.92	-38.79	-25.65	-14.92	38.79	25.65	0.000%
4	25.77	-38.79	-14.85	-25.77	38.79	14.85	0.000%
5	29.72	-38.79	-0.08	-29.72	38.79	0.08	0.005%
6	25.70	-38.79	14.72	-25.70	38.79	-14.72	0.000%
7	14.79	-38.79	25.57	-14.79	38.79	-25.57	0.000%
8	-0.08	-38.79	29.57	0.08	38.79	-29.57	0.005%
9	-14.92	-38.79	25.65	14.92	38.79	-25.65	0.000%
10	-25.77	-38.79	14.85	25.77	38.79	-14.85	0.000%
11	-29.72	-38.79	0.08	29.72	38.79	-0.08	0.002%
12	-25.70	-38.79	-14.72	25.70	38.79	14.72	0.000%
13	-14.79	-38.79	-25.57	14.79	38.79	25.57	0.000%
14	0.00	-57.22	0.00	-0.00	57.22	0.00	0.000%
15	0.01	-57.22	-7.10	-0.01	57.22	7.10	0.002%
16	3.58	-57.22	-6.16	-3.58	57.22	6.16	0.002%
17	6.18	-57.22	-3.56	-6.18	57.22	3.56	0.002%
18	7.13	-57.22	-0.01	-7.13	57.22	0.01	0.002%
19	6.17	-57.22	3.54	-6.17	57.22	-3.54	0.002%
20	3.55	-57.22	6.15	-3.55	57.22	-6.14	0.002%
21	-0.01	-57.22	7.10	0.01	57.22	-7.10	0.002%
22	-3.58	-57.22	6.16	3.58	57.22	-6.16	0.002%
23	-6.18	-57.22	3.56	6.18	57.22	-3.56	0.002%
24	-7.13	-57.22	0.01	7.13	57.22	-0.01	0.002%
25	-6.17	-57.22	-3.54	6.17	57.22	3.54	0.002%
26	-3.55	-57.22	-6.15	3.55	57.22	6.14	0.002%
27	0.03	-38.79	-10.23	-0.03	38.79	10.23	0.002%
28	5.16	-38.79	-8.87	-5.16	38.79	8.87	0.001%
29	8.92	-38.79	-5.14	-8.92	38.79	5.14	0.001%
30	10.28	-38.79	-0.03	-10.28	38.79	0.03	0.002%
31	8.89	-38.79	5.09	-8.89	38.79	-5.09	0.001%
32	5.12	-38.79	8.85	-5.12	38.79	-8.85	0.001%
33	-0.03	-38.79	10.23	0.03	38.79	-10.23	0.002%
34	-5.16	-38.79	8.87	5.16	38.79	-8.87	0.001%
35	-8.92	-38.79	5.14	8.92	38.79	-5.14	0.001%
36	-10.28	-38.79	0.03	10.28	38.79	-0.03	0.002%
37	-8.89	-38.79	-5.09	8.89	38.79	5.09	0.001%
38	-5.12	-38.79	-8.85	5.12	38.79	8.85	0.001%

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	7	0.00006031	0.00009986
3	Yes	11	0.00000001	0.00005832
4	Yes	11	0.00000001	0.00005619
5	Yes	7	0.00006027	0.00012972
6	Yes	11	0.00000001	0.00005739
7	Yes	11	0.00000001	0.00005620
8	Yes	7	0.00006030	0.00007767
9	Yes	11	0.00000001	0.00005669
10	Yes	11	0.00000001	0.00005903
11	Yes	8	0.00000001	0.00006373
12	Yes	11	0.00000001	0.00005576
13	Yes	11	0.00000001	0.00005675
14	Yes	4	0.00000001	0.00000644
15	Yes	7	0.00012992	0.00002633
16	Yes	7	0.00012980	0.00008092
17	Yes	7	0.00012981	0.00007134
18	Yes	7	0.00012993	0.00002979
19	Yes	7	0.00012981	0.00008530
20	Yes	7	0.00012981	0.00007530

21	Yes	7	0.00012993	0.00002683
22	Yes	7	0.00012979	0.00008116
23	Yes	7	0.00012978	0.00009197
24	Yes	7	0.00012991	0.00003109
25	Yes	7	0.00012979	0.00007426
26	Yes	7	0.00012979	0.00008335
27	Yes	7	0.00000001	0.00003565
28	Yes	8	0.00000001	0.00006401
29	Yes	8	0.00000001	0.00005674
30	Yes	7	0.00000001	0.00004012
31	Yes	8	0.00000001	0.00006281
32	Yes	8	0.00000001	0.00005877
33	Yes	7	0.00000001	0.00003521
34	Yes	8	0.00000001	0.00005840
35	Yes	8	0.00000001	0.00006641
36	Yes	7	0.0000001	0.00004173
37	Yes	8	0.00000001	0.00005726
38	Yes	8	0.00000001	0.00006060

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	150 - 133	27.56	35	1.51	0.00
L2	135.95 - 98.45	23.13	35	1.50	0.00
L3	102.3 - 64.8	13.34	35	1.22	0.00
L4	69.5 - 32	6.17	35	0.84	0.00
L5	37.5 - 0	1.82	35	0.44	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
148.0000	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	35	26.93	1.51	0.00	48963
140.0000	(2) APXVSPP18-C-A20 w/ Mount Pipe	35	24.40	1.51	0.00	24480
127.0000	(2) APL866513-42T0 w/ Mount Pipe	35	20.36	1.45	0.00	10264
110.0000	7770.00 w/ Mount Pipe	35	15.41	1.31	0.00	5757

Maximum Tower Deflections - Design Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	150 - 133	79.34	10	4.36	0.01
L2	135.95 - 98.45	66.58	10	4.31	0.01
L3	102.3 - 64.8	38.43	10	3.52	0.00
L4	69.5 - 32	17.79	10	2.41	0.00
L5	37.5 - 0	5.23	10	1.27	0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
148.0000	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	10	77.52	4.36	0.01	17195
140.0000	(2) APXVSPP18-C-A20 w/ Mount Pipe	10	70.24	4.34	0.01	8596
127.0000	(2) APL866513-42T0 w/ Mount Pipe	10	58.64	4.18	0.01	3603
110.0000	7770.00 w/ Mount Pipe	10	44.37	3.76	0.00	2018

Compression Checks

	Pole Design Data									
Section	Elevation	Size	L	L_u	Kl/r	F_a	A	Actual	Allow.	Ratio
No.	ft		ft	ft		ksi	in^2	K	$egin{aligned} P_a \ K \end{aligned}$	$\frac{P}{P_a}$
L1	150 - 133 (1)	TP26x21.83x0.25	17.0000	0.0000	0.0	39.00	19.8584	-4.66	774.48	0.006
L2	133 - 98.45 (2)	TP34.0625x24.7764x0.3125	37.5000	0.0000	0.0	39.00	32.5302	-12.83	1268.68	0.010
L3	98.45 - 64.8 (3)	TP41.75x32.4841x0.375	37.5000	0.0000	0.0	39.00	47.8643	-19.67	1866.71	0.011
L4	64.8 - 32 (4)	TP49.0625x39.8387x0.375	37.5000	0.0000	0.0	39.00	56.3401	-27.80	2197.26	0.013
L5	32 - 0 (5)	TP56.125x46.9597x0.375	37.5000	0.0000	0.0	38.37	66.3564	-38.78	2546.35	0.015

Pole Bending Design Data

Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			M_x	f_{bx}	F_{bx}	f_{bx}	M_y	f_{by}	F_{by}	f_{by}
	ft		kip-ft	ksi	ksi	F_{bx}	kip-ft	ksi	ksi	F_{by}
L1	150 - 133 (1)	TP26x21.83x0.25	53.39	5.23	39.00	0.134	0.00	0.00	39.00	0.000
L2	133 - 98.45 (2)	TP34.0625x24.7764x0.3125	558.26	25.49	39.00	0.654	0.00	0.00	39.00	0.000
L3	98.45 - 64.8 (3)	TP41.75x32.4841x0.375	1282.62	32.45	39.00	0.832	0.00	0.00	39.00	0.000
L4	64.8 - 32 (4)	TP49.0625x39.8387x0.375	2089.09	38.10	39.00	0.977	0.00	0.00	39.00	0.000
L5	32 - 0 (5)	TP56.125x46.9597x0.375	3147.33	41.33	38.37	1.077	0.00	0.00	38.37	0.000

Pole Shear Design Data

Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			V	f_{v}	F_{v}	f_{v}	T	f_{vt}	F_{vt}	f_{vt}
	ft		K	ksi	ksi	F_{v}	kip-ft	ksi	ksi	F_{vt}
L1	150 - 133 (1)	TP26x21.83x0.25	9.11	0.46	26.00	0.035	0.00	0.00	26.00	0.000
L2	133 - 98.45 (2)	TP34.0625x24.7764x0.3125	20.46	0.63	26.00	0.048	0.95	0.02	26.00	0.001
L3	98.45 - 64.8 (3)	TP41.75x32.4841x0.375	23.67	0.49	26.00	0.038	0.95	0.01	26.00	0.000
L4	64.8 - 32 (4)	TP49.0625x39.8387x0.375	26.61	0.47	26.00	0.036	0.95	0.01	26.00	0.000
L5	32 - 0 (5)	TP56.125x46.9597x0.375	29.77	0.45	26.00	0.034	0.95	0.01	26.00	0.000

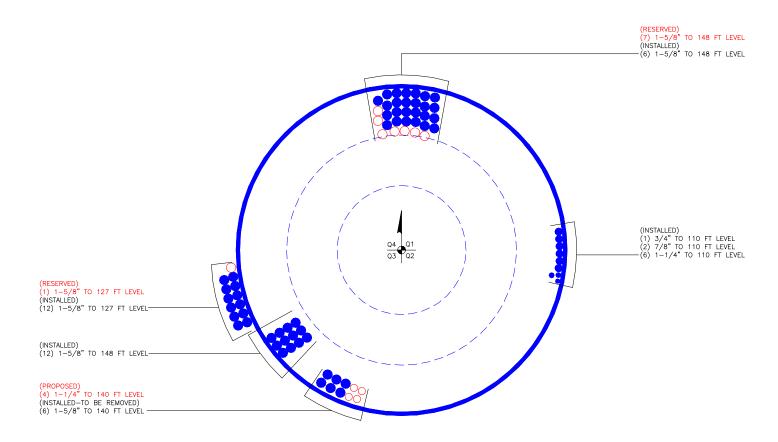
Pole Interaction Design Data

Section No.	Elevation	Ratio P	Ratio f_{bx}	$Ratio$ f_{by}	Ratio f_v	$Ratio \ f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	P_a	F_{bx}	F_{by}	F_{v}	F_{vt}	Ratio	Ratio	
L1	150 - 133 (1)	0.006	0.134	0.000	0.035	0.000	0.141	1.333	H1-3+VT 🗸
L2	133 - 98.45 (2)	0.010	0.654	0.000	0.048	0.001	0.664 🖊	1.333	H1-3+VT 🗸
L3	98.45 - 64.8 (3)	0.011	0.832	0.000	0.038	0.000	0.843 🖊	1.333	H1-3+VT 🖊
L4	64.8 - 32 (4)	0.013	0.977	0.000	0.036	0.000	0.990 🗸	1.333	H1-3+VT ✔
L5	32 - 0 (5)	0.015	1.077	0.000	0.034	0.000	1.092	1.333	H1-3+VT 🗸

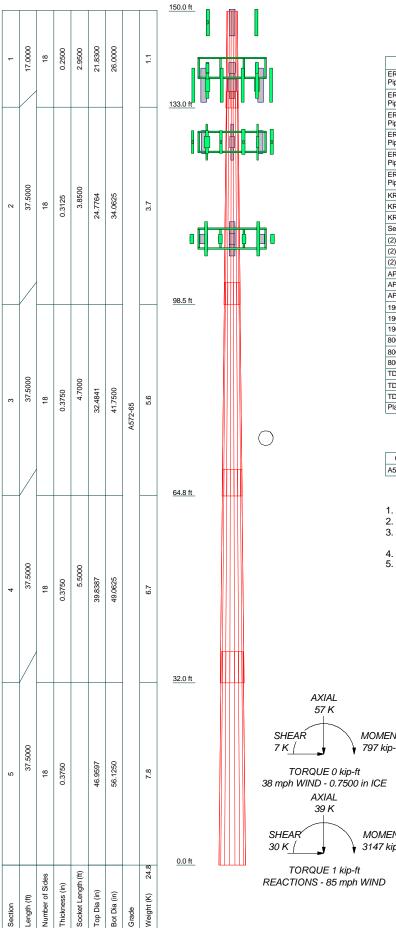
Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$SF^*P_{\mathit{allow}} \ K$	% Capacity	Pass Fail
L1	150 - 133	Pole	TP26x21.83x0.25	1	-4.66	1032.38	10.5	Pass
L2	133 - 98.45	Pole	TP34.0625x24.7764x0.3125	2	-12.83	1691.15	49.8	Pass
L3	98.45 - 64.8	Pole	TP41.75x32.4841x0.375	3	-19.67	2488.32	63.2	Pass
L4	64.8 - 32	Pole	TP49.0625x39.8387x0.375	4	-27.80	2928.95	74.3	Pass
L5	32 - 0	Pole	TP56.125x46.9597x0.375	5	-38.78	3394.28	82.0	Pass
							Summary	
						Pole (L5)	82.0	Pass
						RATING =	82.0	Pass

APPENDIX B BASE LEVEL DRAWING



APPENDIX C ADDITIONAL CALCULATIONS



DESIGNED APPURTENANCE LOADING

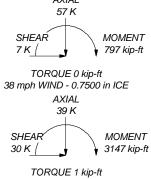
TYPE	ELEVATION	TYPE	ELEVATION
ERICSSON AIR 21 B2A B4P w/ Mount	148	(2) APL866513-42T0 w/ Mount Pipe	127
Pipe		(2) APL866513-42T0 w/ Mount Pipe	127 127 127 127 127 127 127 127
ERICSSON AIR 21 B2A B4P w/ Mount	148	(2) APL866513-42T0 w/ Mount Pipe	127
Pipe		(2) BXA-171063/8CF w/ Mount Pipe	127
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	148	(2) SLCP 2x6014 w/ Mount Pipe	127
ERICSSON AIR 21 B4A B2P w/ Mount	148	BXA-171063-12BF w/ Mount Pipe	127
Pipe	140	(2) FD9R6004/2C-3L	127
ERICSSON AIR 21 B4A B2P w/ Mount	148	(2) FD9R6004/2C-3L	127
Pipe		(2) FD9R6004/2C-3L	127
ERICSSON AIR 21 B4A B2P w/ Mount	148	742 213 w/ Mount Pipe	127
Pipe		742 213 w/ Mount Pipe	127
KRY 112 144/1	148	742 213 w/ Mount Pipe	127
KRY 112 144/1	148	BXA-70063/4CF w/ Mount Pipe	127
KRY 112 144/1	148	RRH2x40-AWS	127
Sector Mount [SM 408-3]	148	RRH2x40-AWS	127
(2) APXVSPP18-C-A20 w/ Mount Pipe	140	RRH2x40-AWS	127
(2) APXVSPP18-C-A20 w/ Mount Pipe	140	DB-B1-6C-8AB-0Z	127
(2) APXVSPP18-C-A20 w/ Mount Pipe	140	Platform Mount [LP 304-1]	127
APXVTM14-C-120 w/ Mount Pipe	140	7770.00 w/ Mount Pipe	110
APXVTM14-C-120 w/ Mount Pipe	140	7770.00 w/ Mount Pipe	110
APXVTM14-C-120 w/ Mount Pipe	140	7770.00 w/ Mount Pipe	110
1900MHz RRH	140	P65-16-XLH-RR w/ Mount Pipe	110
1900MHz RRH	140	P65-16-XLH-RR w/ Mount Pipe	110
1900MHz RRH	140	P65-16-XLH-RR w/ Mount Pipe	110
800MHZ RRH	140	(2) LGP21401	110
800MHZ RRH	140	(2) LGP21401	110
800MHZ RRH	140	(2) LGP21401	110
TD-RRH8x20-25	140	(2) RRUS-11	110
TD-RRH8x20-25	140	(2) RRUS-11	110
TD-RRH8x20-25	140	(2) RRUS-11	110
Platform Mount [LP 303-1]	140	DC6-48-60-18-8F	110
		Platform Mount [LP 303-1]	110

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

- 1. Tower is located in Fairfield County, Connecticut.
- 2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
- Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
- 4. Deflections are based upon a 50 mph wind.5. TOWER RATING: 82%





Paul J Ford and Company 250 E. Broad Street Suite 600 Columbus, OH 43215 Phone: 614.221.6679 FAX: 614.448.4105

ob: 150' Monopole / Newtown					
Project: 37513-1642.002	/BU 8256222				
Client: Crown Castle	Drawn by: Seth Tschanen	App'd:			
Code: TIA/EIA-222-F	Date: 06/20/14	Scale: NTS			
Path:	DIT 925727W/0 T94694 DIT 925727 . nn2 \$4/27642.4642 nn2 7906 ed	Dwg No. E-1			

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev F

Site Data

BU#: 826222

Site Name: Newtown/RT-25

App #:

πρρ π.	
Pole Manufacturer:	Pirod

Anchor Rod Data					
Qty:					
Diam:	1.25	in			
Rod Material:	Other				
Strength (Fu):	150	ksi			
Yield (Fy):	105	ksi			
Bolt Circle:	61	in			

Plate Data						
Diam: 65 in						
Thick:	1.5	in				
Grade:	50	ksi				
Single-Rod B-eff:	4.57	in				

Stiffener Data (Welding at both sides)				
Config:	1	*		
Weld Type:	Fillet			
Groove Depth:		< Disregard		
Groove Angle:		< Disregard		
Fillet H. Weld:	0.5	in		
Fillet V. Weld:	0.5	in		
Width:	4.5	in		
Height:	8	in		
Thick:	0.75	in		
Notch:	0.5	in		
Grade:	36	ksi		
Weld str.:	70	ksi		

Pole Data				
Diam:	56.125	in		
Thick:	0.375	in		
Grade:	65	ksi		
# of Sides:	18	"0" IF Round		
Fu	80	ksi		
Reinf. Fillet Weld	0	"0" if None		

Stress Increase Factor			
ASIF:	1.333		

Reactions			
Moment:	3147	ft-kips	
Axial:	39	kips	
Shear:	30	kips	

If No stiffeners, Criteria: AISC	ASD <-Only Applcable to Unstiffened Cases
----------------------------------	---

Anchor Rod ResultsMaximum Rod Tension:62.5 KipsAllowable Tension:81.0 Kips

Anchor Rod Stress Ratio: 77.2% Pass

Base Plate Results	Shear Check Only
Base Plate Stress:	Rohn/Pirod, OK
Allowable Plate Stress:	26.7 ksi
Base Plate Stress Ratio:	Rohn/Pirod, OK

Stiffened
Service, ASD
0.75*Fy*ASIF
Y.L. Length:
N/A, Roark

Stiffened

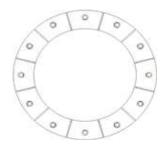
Service, ASD

Fty*ASIF

Stiffener ResultsN/A for Rohn / PirodHorizontal Weld :N/AVertical Weld:N/APlate Flex+Shear, fb/Fb+(fv/Fv)^2:N/APlate Tension+Shear, ft/Ft+(fv/Fv)^2:N/APlate Comp. (AISC Bracket):N/A

Pole Results

Pole Punching Shear Check: N/A





^{*} 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Foundation Loads:

Pole weight or tower leg compression = 39 (kips)

Horizontal load at top of pier = 30 (kips)

Overturning moment at top of pier = 2570 (ft-kips)

Design criteria:

Safety factor against overturning = 1.5

Soil Properties:

Dimensions:

Pier shape (round or square) ("R" or "S") Pier width = 7 (ft) 0.5 (ft) Pier height above grade = depth to bottom of footing = 6 (ft) Footing thickness = 2 (ft) Footing width = 21 (ft) Footing length = (ft) 21

Concrete:

Concrete strength = 4 (ksi) Rebar strength = 60 (ksi) ultimate load factor = 1.3

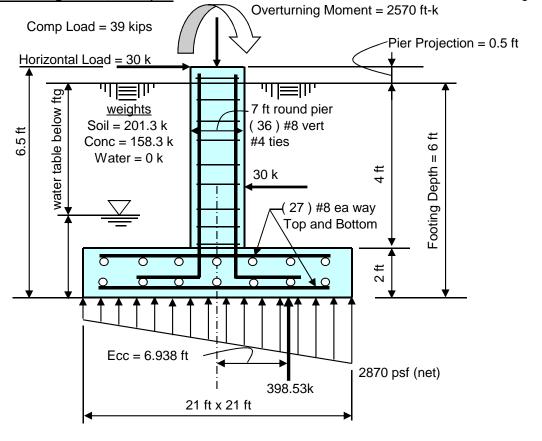
Reinforcing Steel:

minimum cover over rebar = $\frac{\underline{Pad}}{3}$ inches size of pad rebar = $\frac{\#8}{27}$ (ea direction)

Reinforcing Steel:

size of vert rebar in pier=
vertical rebar quantity =
size of pier ties =
minimum cover over rebar =

Total volume of concrete = 39.1 cu yd



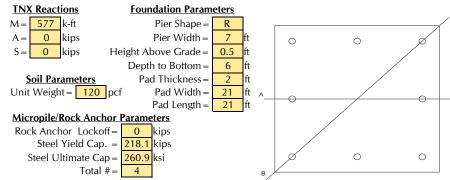
Summary of analysis results		
Maximum Net Soil Bearing = 2.87 ksf Allowable Net Soil Bearing = 15 ksf Soil Bearing Stress Ratio = 0.19 Okay	Ult Bending Shear Capacity = 126 psi Ult Bending Shear Stress = 70 psi Bending Shear Stress Ratio = 0.55 Okay	
SEE "CHECK OF OVERTURNING CAPACITY" PAGE FOR OVERTURNING CALCUALATIONS & CAPACITY	Pad Bending Moment Capacity= 1800 ft-k Pad Bending Moment = 1322 ft-k Bending Moment Stress Ratio = 0 SEE "MICROPILE/ROCK ANCHOR DESIGNFOR MAT OR PAD PIER" PAGE	



Page: By: Date: 6/20/2014 Project: 826222 Client: Crown PROJ#: 37513-1642.002

6/17/2013

Micropile/Rock Anchor Design for Mat or Pad Pier



Wind Side (About A)

Bolt #	<u>#</u>	Area, in ²	Ybar, in
1	3	3.07	62.2254
2	1	3.07	39

$$f_{1A} = M^* y_{bar1} / I_{boltsA} = 10.7 \text{ ksi}$$

 $f_{2A} = M^* y_{bar2} / I_{boltsA} = 6.7 \text{ ksi}$

$$I_{boltsA} = \varepsilon NAy^2 = 40331 \text{ in}^4$$

 $M = 6924 \text{ k-in}$

$$C_{1A} = 120.7 \text{ kips}$$
 $T_{1A} = 0.0 \text{ kips}$ $C_{2A} = 108.4 \text{ kips}$ $T_{2A} = 0.0 \text{ kips}$

7.87 kips	
Capacity,k	
156.54	
156.54	

Wind Into Corner (About B)

Bolt #	<u>#</u>	Area, in ²	Ybar, in
1	1	3.07	88.0625
2	1	3.07	72.125
3	0		
4	0		
£ 1.4	* /!	1.0	2 kgi

$$f_{1B} = M^* y_{bar1} / I_{boltsB} = 15.3 \text{ ksi}$$
 $f_{2B} = M^* y_{bar2} / I_{boltsB} = 12.6 \text{ ksi}$
 $f_{3B} = M^* y_{bar3} / I_{boltsB} = 0.0 \text{ ksi}$
 $f_{4B} = M^* y_{bar4} / I_{boltsB} = 0.0 \text{ ksi}$

		Capacity,k
$C_{1B} = 134.9 \text{ kips}$	$T_{1B} = 0.0$ kips	156.54
$C_{2B} = 126.4 \text{ kips}$	$T_{2B} = 0.0$ kips	156.54
$C_{3B} = 0.0 \text{ kips}$	$T_{3B} = 0.0$ kips	156.54
$C_{3B} = 0.0$ kips	$T_{3B} = 0.0$ kips	156.54

Steel Check

Revision = Actual Load

Max Tension/Compression Load = 134.9 kips

Capacity

Capacity = 0.6*Steel Ultimate Capacity = 156.5 kips Stress Ratio = 86.2%

Bending Check (Wind into side)

Distance from center to end of pier = 42.0 in. Bending Moment = \sum [# of Bolts * (ybar- 42.0 in.)*Tension] = 291.5 k-ft Additional Pad Bending Moment from Pad & Pier Spreadsheet = 1336.0 k-ft Use 1715.0 k-ft to analyze bending in pad $a = \frac{A_s * f_y}{0.85 * f'_c * b}$ Bottom Clear Dist. = 4 in. 4 ksi $As = 21.33 \text{ in}^2$ $\emptyset M_n = 0.9 * A_s * f_y * \left(d - \frac{a}{2}\right)$ a = 4.48 in. Number of Bars = d = 19.5 in. 27 Bar #= Bar Area = 0.790 in. 1.000 in.² $\emptyset Mn = 1969.7 \text{ k-ft}$ Capacity = 87.1% Bar Diameter =

(Overrided from SPColumn)

Micropile Embedment Check

Required Embedment = 22.7 ft Ratio = 84.2%

STRUCTUREPOINT - spColumn v4.80 (TM) Page 1 Licensed to: Paul J. Ford and Company. License ID: 60478-1036166-4-1E6CD-2369D 06/20/14 g:\tower\375_crown_castle\2013\37513-1642 bu 826222\wo $78...\37513-1642.002$ - pier steel check.col 02:47 PM

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000	200	00		000	000	000	200	00	0	000	200	00	00	00	00	00 ((TM)

spColumn v4.80 (TM)

Computer program for the Strength Design of Reinforced Concrete Sections Copyright © 1988-2011, STRUCTUREPOINT, LLC. All rights reserved

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General Information:

=============

File Name: q:\tower\375_crown_castle\2013\37513-1642 bu 826...\37513-1642.002 - pier steel check.col

Project: Column:

Engineer:
ACI 318-05 Units: English

Code: ACI 318-05 Units:

Run Option: Investigation Slenderness: Not considered Run Axis: X-axis Column Type: Architectural

Material Properties:

f'c = 4 ksi

Ultimate strain = 0.003 in/in

Beta1 = 0.85

Section:

Circular: Diameter = 84 in

Gross section area, Ag = 5541.77 in^2

 $Ix = 2.44392e+006 in^4$ $Iy = 2.44392e+006 in^4$ rx = 21 in ry = 21 in

Reinforcement:

=========

Bar Set: ASTM A615

Size Diam (in) Area (in^2) Size Diam (in) Area (in^2) Size Diam (in) Area (in^2) # 5 0.63 0.31 0.88 0.44 # 7 1.00 # 10 0.79 1.56 # 6 0.75 0.60 # 8 1.00 # 9 1.13 1.27 1.27 # 11 1.41 2.25 # 18 # 14 1.69 2.26 4.00

Confinement: Tied; #4 ties with #10 bars, #4 with larger bars.

phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.65

Layout: Circular

Pattern: All Sides Equal (Cover to transverse reinforcement)

Total steel area: As = 28.44 in^2 at rho = 0.51% (Note: rho < 1.0%)

Minimum clear spacing = 5.62 in

36 #8 Cover = 3 in

Factored Loads and Moments with Corresponding Capacities:

No.	Pu kip	Mux k-ft	PhiMnx k-ft		NA depth in	Dt depth in	eps_t	Phi
1	0.00	4344.60	4360.09	1.004	14.82	80.00	0.01320	0.900

*** End of output ***

Check Overturning Capacity of Foundation System

PJF job no. <u>37513-1642.002</u>

Assumptions: 1) Micropile reinforcing has been installed

2) Wind into side of foundation is worst case scenario

Pole base moment =	<u>3147</u>	ft-k	
Pole base shear =	<u>30</u>	kips	
Pole axial load =	<u>39</u>	kips	
Total foundation thickness / height =	<u>6.5</u>	feet	
Distance from center of pole to edge of fdn =	<u>10.5</u>	feet	
Foundation weight =	<u>158.3</u>	kips	
Soil weight (abv fdn) =	201.3	kips	
Quantity of piles =	<u>2</u>		
Pile yield strength =	<u>=</u> 218.1	kips	
Pile distance to edge of fdn =	14.75	feet	(Average of two worst case pile locations)
Overturning resistance (pole/fdn/soil) =	4185.3	ft-k	
Overturning resistance (piles) =	6434.0	ft-k	
Total overturning resistance =	<u>10619.3</u>	ft-k	
Overturning moment at base of foundation =	<u>3342.0</u>	ft-k	
_		IL-K	
Required safety factor against overturning = % Capacity =	1.5 47.2%	<u>OK</u>	
% Capacity =	T/.Z/0	$\frac{\mathbf{C}\mathbf{K}}{\mathbf{C}}$	



RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

Sprint Existing Facility

Site ID: CT54XC716

Newtown Georgia Pacific VS

201 South Main Street Newtown, CT 06470

September 7, 2014

EBI Project Number: 62144516

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



September 7, 2014

Sprint Attn: RF Engineering Manager 1 International Boulevard, Suite 800 Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:

CT54XC716 - Newtown Georgia Pacific VS

Site Total: 45.36% - MPE% in full compliance

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at **201 South Main Street, Newtown, CT**, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm2). The number of μ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limit for the cellular band (850 MHz Band) is approximately 567 μ W/cm², and the general population exposure limit for the 1900 MHz and 2500 MHz bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at **201 South Main Street, Newtown, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 2 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation.
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.



- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20 and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXVTM14-C-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antenna mounting height centerline for the proposed antennas is **137 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

Site D						=											
Sector 1	Site ID CT54XC716 - Newtown Georgia Pacific VS																
Sector 1 Sector 2 Sector 2 Sector 2 Sector 3 Sector 4 Sector 5 Sector 5 Sector 5 Sector 5 Sector 5 Sector 5 Sector 6																	
Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction) Height (ft) height (2able Loss Additional Power Density Value: Cable Size (Bill Loss Additional Cable Size (Bill Loss (Bil		Site Type	ype Monopole														
Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction) Height (ft) height (2able Loss Additional Power Density Value: Cable Size (Bill Loss Additional Cable Size (Bill Loss (Bil																	
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Number Antenna Make Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction Height (th) h	Antenna						Channel	Number of	Composite	(10 db	Antenna	analysis		Cable Loss	Additional		Density
13		Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology				,			Cable Size			ERP	
The color of the	1a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	5.9	137	131	1/2 "	0.5	0	138.69	0.29%
Sector 2	1a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	137	131	1/2 "	0.5	0	39.00	0.14%
Sector 2 Sector 2 Sector 2 Sector 2 Sector 3 Sector 2 Sector 3	1B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	137	131	1/2 "	0.5	0	138.69	0.51%
Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power Cut Processed RFS APXVSPP18-C-A20 RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.51% Representation of Composite Composite Club Antenna analysis Cable Loss (dB) Los													Sector to	otal Power D	Density Value:	0.95%	
Antenna Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channel Radio Type Frequency Band Technology (Watts) RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 2 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 Antenna Gain (10 db Antenna Gain (Sector 2															
Antenna Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channel Radio Type Frequency Band Technology (Watts) RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 2 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 Antenna Gain (10 db Antenna Gain (
Antenna Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channel Radio Type Frequency Band Technology (Watts) RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 2 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.29% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 137 131 1/2" 0.5 0 138.69 0.51% 2 8 RFS APXVSPP18-C-A20 RRH 2500 MHz CDMA/LTE 20 1 1 20 3.4 Antenna Gain (10 db Antenna Gain (
Antenna Number Antenna Make Antenna Antenna Make Antenna Make Antenna Make Antenna Make Antenna Make Antenna Anten							Power										
Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction Height (ft) height Cable Size (dB) Loss (dB) ERP Percentage							Out Per			Antenna Gain							Power
2a	Antenna						Channel	Number of	Composite	,							Density
2a RFS APXVSPP18-C-A20 RRH 850 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2 0.5 0 39.00 0.14% 2B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 0.5 0 138.69 0.51% Sector 3 Sector total Power Density Value: 0.95% Sector 13 Antenna Make An							. ,					_			, ,		
28																	
Sector total Power Density Value: 0.95% Sector 3 Sector 4 Sector 3 Sector 4 Sector 4 Sector 5 Sector 6 Sector 6 Sector 5 Sector 6																	
Power	2B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	137	131		***			0.51%
Power		Sector total Power Density Value:									0.95%						
Antenna Make								Sector 3									
Antenna Make																	
Antenna Make							Dowo-										
Antenna Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction) Height (ft) Cable Loss Additional Loss (dB) ERP Percentage 3a RFS APXVSPP18-C-A20 RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.29% 3a RFS APXVSPP18-C-A20 RRH 850 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2 " 0.5 0 39.00 0.14% 3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 39.00 0.14% 3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.51%										Antenna Gain							Power
Number Antenna Make Antenna Model Radio Type Frequency Band Technology (Watts) Channels Power reduction Height (ft) height (ft) height (able Size) (dB) Loss (dB) ERP Percentage 3a RFS APXVSPP18-C-A20 RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.29% 3a RFS APXVSPP18-C-A20 RRH 850 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2 " 0.5 0 39.00 0.14% 3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 39.00 0.14%	Antenna							Number of	Composite			analysis		Cable Loss	Additional		
3a RFS APXVSPP18-C-A20 RRH 1900 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.29% 3a RFS APXVSPP18-C-A20 RRH 850 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2 " 0.5 0 39.00 0.14% 3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.51%		Antenna Make	Antenna Model	Radio Tyne	Frequency Band	Technology			-				Cable Size			FRP	-
3a RFS APXVSPP18-C-A20 RRH 850 MHz CDMA/LTE 20 1 20 3.4 137 131 1/2 " 0.5 0 39.00 0.14% 3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.51%							. ,							, ,			
3B RFS APXVTMM14-C-120 RRH 2500 MHz CDMA/LTE 20 2 40 5.9 137 131 1/2 " 0.5 0 138.69 0.51%																	
								_									
													Sector to	otal Power D	Density Value:	0.95%	•

Site Composite MPE %									
Carrier	MPE %								
Sprint	2.84%								
AT&T	14.64%								
T-Mobile	0.16%								
Verizon Wireless	27.72%								
Total Site MPE %	45.36%								



Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are 2.84% (0.95% from sector 1, 0.95% from sector 2 and 0.95% from sector 3) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **45.36**% of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

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