



Aaron Meyers, Site Acquisition
c/o New Cingular Wireless, PCS LLC (AT&T)
Centerline Communications, LLC
750 W. Center St., Floor 3
West Bridgewater, MA 02379
Mobile: (774) 420-4202
ameyers@clinellc.com

DATE June 18, 2019

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

**RE: Notice of Exempt Modification // Site Number: CT5432
151 Berkshire Rd, Newton, CT 06482 (Site Name: Newton)
N 41.397375 // W -73.236069**

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC (“AT&T”) currently maintains six (6) antennas at the 118.5-foot level of the existing 148-foot Monopole tower at 151 Berkshire Rd., Newton, CT 06482. The tower is owned by Eversource. The property is owned by SBA Infrastructure, LLC. AT&T now intends to add three (3) antennas, replace three (3) Antennas, and replace six (6) RRUS for its LTE upgrade. This equipment would be installed at the 118.5-foot level of the tower.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Daniel C. Rosenthal, First Selectman, as well as the tower and ground owner, SBA Infrastructure, LLC.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

Attached to accommodate this filing are construction drawings dated May 14, 2019 by Hudson Design Group, LLC, a structural analysis dated June 14, 2019 by Tower Engineering Solutions, a mount analysis dated April 22, 2018 by Hudson Design Group, LLC, a mount modification design dated May 14, 2019 by Hudson Design Group, LLC, and an Emissions Analysis Report dated June 28, 2019 by Centerline Communications, LLC.

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading as shown in the attached structural analysis by Tower Engineering Solutions, dated June 14, 2019.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Aaron Meyers, Site Acquisition
c/o New Cingular Wireless, PCS LLC (AT&T)
Centerline Communications, LLC
750 W. Center St., Floor 3
West Bridgewater, MA 02379
Mobile: (774) 420-4202
ameyers@centerlincommunications.com

Attachments

cc: Daniel C. Rosenthal, First Selectman - as elected official
SBA Infrastructure, LLC – as tower and property owner
John Poeltl – as Chief Building Official



Tower Engineering Solutions

Phone (972) 483-0607, Fax (972) 975-9615
1320 Greenway Drive, Suite 600, Irving, Texas 75038

Structural Analysis Report

Existing 148 ft Pennsummit Monopole
Customer Name: SBA Communications Corp
Customer Site Number: CT13057-A
Customer Site Name: Newtown
Carrier Name: AT&T(App#: 116066, V#2)
Carrier Site ID / Name: CT5432 / Sandy Hook
Site Location: 151 Berkshire Road

Newtown, Connecticut

Exp.01/31/2020

Fairfield County

Latitude: 41.397375

Longitude: -73.236069



Analysis Result:

Max Structural Usage: 61.6% [Pass] 06/14/2019

Max Foundation Usage: 43.0% [Pass]

Additional Usage Caused by New Mount/Mount Modification: +1.6%

Report Prepared By : Uma S Atluri

Introduction

The purpose of this report is to summarize the analysis results on the 148 ft Pennsummit Monopole to support the proposed antennas and transmission lines in addition to those currently installed. Any modification listed under Sources of Information was assumed completed and was included in this analysis.

Sources of Information

Tower Drawings	PennSummit/PJF, Job # 29203-0081, dated 4/22/2003:
Foundation Drawing	PennSummit/PJF, Job # 29203-0081, dated 4/28/2003:
Geotechnical Report	N/A
Modification Drawings	N/A

Analysis Criteria

The rigorous analysis was performed in accordance with the requirements and stipulations of the ANSI/TIA/EIA 222-G. In accordance with this standard, the structure was analyzed using **TESPoles**, a proprietary analysis software. The program considers the structure as an elastic 3-D model with second-order effects and temperature effects incorporated in the analysis. The analysis was performed using multiple wind directions.

Wind Speed Used in the Analysis:	Ultimate Design Wind Speed $V_{ult} = 120.0$ mph (3-Sec. Gust)/ Nominal Design Wind Speed $V_{asd} = 93.0$ mph (3-Sec. Gust)
Wind Speed with Ice:	50 mph (3-Sec. Gust) with 3/4" radial ice concurrent
Operational Wind Speed:	60 mph + 0" Radial ice
Standard/Codes:	ANSI/TIA/EIA 222-G / 2015 IBC / 2018 Connecticut State Building Code
Exposure Category:	C
Structure Class:	II
Topographic Category:	1
Crest Height:	0 ft
Seismic Parameters:	$S_S = 0.203$, $S_1 = 0.065$

This structural analysis is based upon the tower being classified as a Structure Class II; however, if a different classification is required subsequent to the date hereof, the tower classification will be changed to meet such requirement and a new structural analysis will be run.

Existing Antennas, Mounts and Transmission Lines

The table below summarizes the antennas, mounts and transmission lines that were considered in the analysis as existing on the tower.

Items	Elevation (ft.)	Qty.	Antenna Descriptions	Mount Type & Qty.	Transmission Lines	Owner
1	153.0	1	Decibel - DB-TDD6492A-A - Omni	(1) 2 ft. Standoff	(1) 7/8"	Town of Newtown
2	147.0	1	Trombone		(1) 7/8"	
3	137.5	3	Antel - BXA-171063-8BF - Panel	(1)Low Profile Platform	(12) 1 5/8"	Verizon
4		3	Swedcom - SLCP2x6014 - Panel			
5		6	Swedcom - SC-E 6014 Rev2W - Panel			
6		6	RFS - FD9R6004/2C-3L - Diplexer			
-	118.5	3	Allgon - 7770 - Panel	(1)Low Profile Platform + (1) RRH Collar Mount	(6) 1 5/8" (1) 3/8" (2) 5/8"	AT&T
-		3	Allgon - P65-16 - Panel			
-		6	Powerwave - LGP 21401 - TMA			
-		6	Ericsson - RRUS-11 - RRU			
-		1	Raycap - DC6-48-60-18-8F - SP			
13	109.0	3	RFS - APXVSP18-C-A20 - Panel	(3) T-Arms w/ Working Platforms	(4) 1 1/4"	Sprint
14		3	RFS - APXVTM14-C-I20 - Panel			
15		3	ALU - 800 MHz RRH - RRU			
16		3	ALU - 1900MHz RRH - RRU			
17		3	ALU - TD-RRH8x20 - RRU			
18		3	ALU - 800MHz RRH Filter			
19		4	RFS - ACU-A20-N - RET			
20	99.5	6	Andrew - RR65-18-00DPL2 - Panel	Platform w/ Hand Rails (Commscope MT-195-12)	(12) 1 1/4"	T-Mobile
21		3	RFS - APXV18-206513-C-A20 - Panel			
22		3	Commscope - LNX-6515DS-A1M - Panel			
23		3	RFS - ATMAA1412D-1A2 - TMA			
24		3	Kathrein - 782 11054 - Bias Ts			
25	50.5	1	Decibel - 260B - GPS	(1) 3 ft. Standoff	(1) 1/2"	Sprint

Proposed Carrier’s Final Configuration of Antennas, Mounts and Transmission Lines

Information pertaining to the proposed carrier’s final configuration of antennas and transmission lines was provided by SBA Communications Corp. The proposed antennas and lines are listed below.

Items	Elevation (ft)	Qty.	Antenna Descriptions	Mount Type & Qty.	Transmission Lines	Owner
7	118.5	3	Powerwave 7770 - Panel	Low Profile Platform + (1) RRH Collar Mount w/SitePro Sitepro 1 P/N HRK12-Handrail Kit/3 2-1/2" std. (2.88" O.D.)- Pipe Mast	(6) 1 5/8" (4) 3/4" DC Power (2) 1/2" Fiber	AT&T
8		6	Kathrein 800-10965 - Panel			
9		6	Powerwave LGP21401 TMA			
10		3	Ericsson 4449 B5/B12			
11		3	Ericsson RRUS 8843 B2 B66A			
12		2	Raycap DC6-48-60-18-8F (24x11" 32.8 lbs))			

See the attached coax layout for the line placement considered in the analysis.

Analysis Results

The results of the structural analysis, performed for the wind and ice loading and antenna equipment as defined above, are summarized as the following:

	Pole shafts	Anchor Bolts	Base Plate	Flange @120'
Max. Usage:	60.3%	56.5%	61.6%	31.0%
Pass/Fail	Pass	Pass	Pass	Pass

Foundations

	Moment (Kip-Ft)	Shear (Kips)
Original Design Reactions	3750.0	35.0
Analysis Reactions	2872.8	29.3
Factored Reactions*	5062.5	47.3
% of Design Reactions	56.7%	61.9%

* Per section 15.5.1 of the TIA-222-G standard, factored reactions were obtained by multiplying a 1.35 factor to the original design reactions.

The foundation has been analyzed using the supplied documents and was found adequate. Therefore, no modification to the foundation will be required. Geotechnical soil parameters were obtained from the original foundation calculations included with the referenced tower and foundation design drawings.

Operational Condition (Rigidity):

Operational characteristics of the tower are found to be within the limits prescribed by ANSI/TIA/EIA 222-G for the installed antennas. The maximum twist/sway at the elevation of the proposed equipment is 0.8894 degrees under the operational wind speed as specified in the Analysis Criteria.

Conclusions

Based on the analysis results, the existing structure and its foundation were found to be adequate to safely support the existing and proposed equipment and meet the minimum requirements per the ANSI/TIA/EIA 222-G Standard under the design basic wind speed as specified in the Analysis Criteria.

Standard Conditions

1. This analysis was performed based on the information supplied to **(TES) Tower Engineering Solutions, LLC**. Verification of the information provided was not included in the Scope of Work for **TES**. The accuracy of the analysis is dependent on the accuracy of the information provided.
2. The structural analysis was performance based upon the evidence available at the time of this report. All information provided by the client is considered to be accurate.
3. The analyses will be performed based on the codes as specified by the client or based on the best knowledge of the engineering staff of **TES**. In the absence of information to the contrary, all work will be performed in accordance with the latest relevant revision of ANSI/TIA-222. If wind speed and/or ice loads are different from the minimum values recommended by the EIA/TIA-222 standard or other codes, **TES** should be notified in writing and the applicable minimum values provided by the client.
4. The configuration of the existing mounts, antennas, coax and other appurtenances were supplied by the customer for the current structural analysis. **TES** has not visited the tower site to verify the adequacy of the information provided. If there is any discrepancy found in the report regarding the existing conditions, **TES** should be notified immediately to evaluate the effect of the discrepancy on the analysis results.
5. The client will assume responsibility for rework associated with the differences in initially provided information, including tower and foundation information, existing and/or proposed equipment and transmission lines.
6. If a feasibility analysis was performed, final acceptance of changed conditions shall be based upon a rigorous structural analysis.

Usage Diagram - Max Ratio 60.32% at 0.0ft

Structure: ÔVFHÉÍ ÌÈËÓÉ
Site Name: P^, q, }
Height: FÌ ÌÈÁÇ
Base Elev: ÈÈÈÁÇ

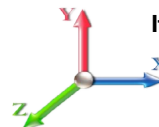
Code: ÒÖEVÖÈGGÉÖ
Exposure: Ô
Gh: FÈ

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 Úæ ^ ÌÆ



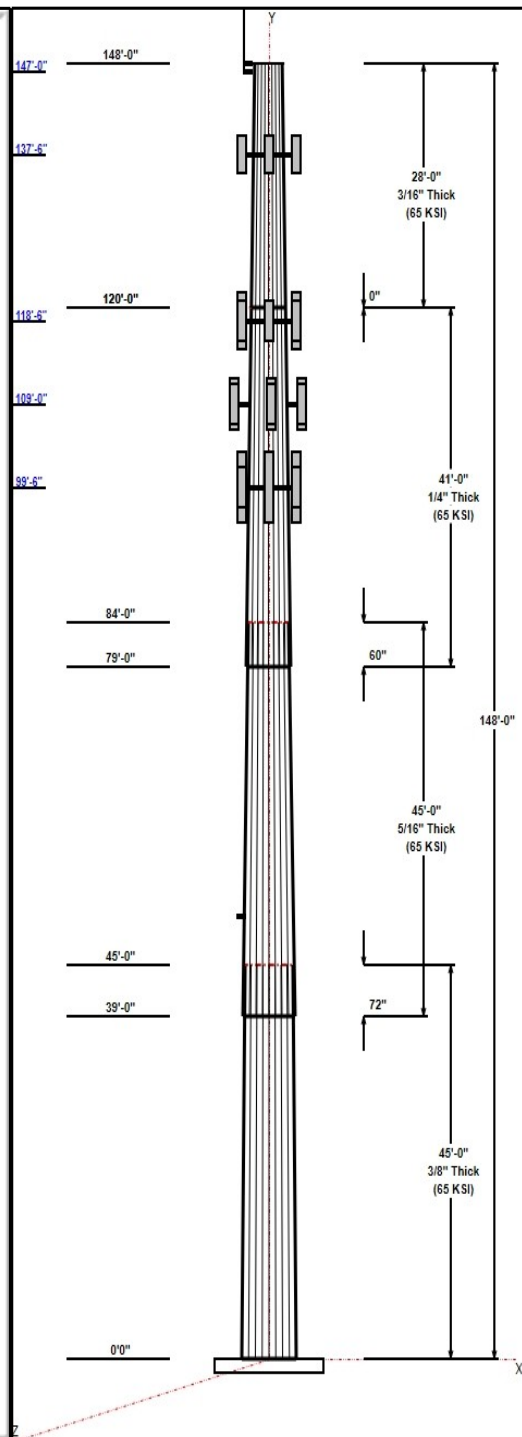
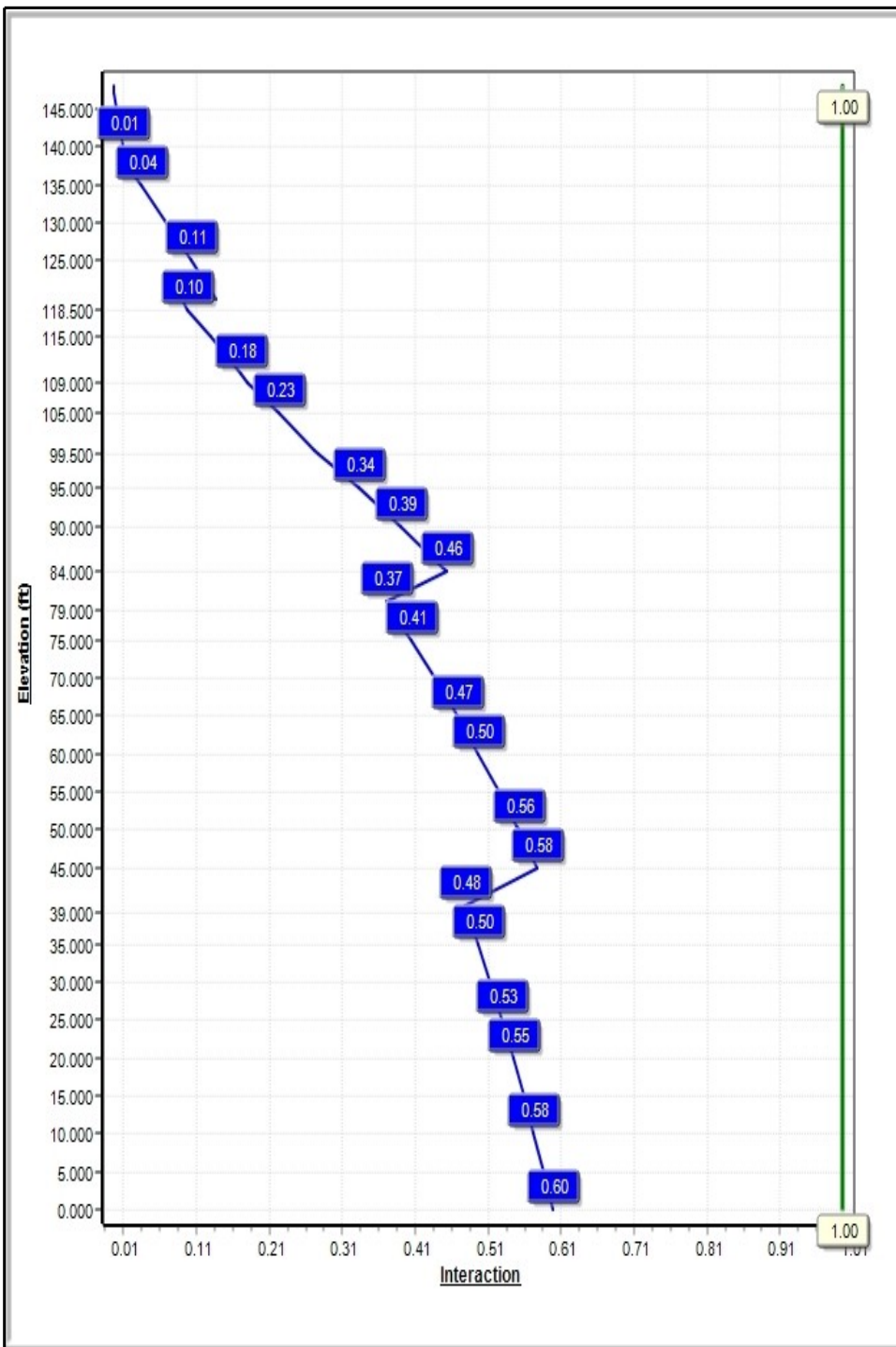
Ô^áÁÏ ááÁÇÏK FÈÈ
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Load Case : 1.2D + 1.6W 93 mph Wind



Iterations: GH

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Structure: CT13057-A-SBA

Type: Væ^i^å
 Site Name: P^, q, }
 Height: FI Ì ÈÉÁÇC
 Base Elev: ÈÈÉÁÇD

Base Shape: FÌ ÆÛå^å
 Taper: ÈÈÈÛÌ H

Í ÆI ÈÈÈFJ
 Úæ^åH



ÈÈÈ	FÈJÈÈ	Q•å^	FÁÈÁÛÓ[æ	Û]!å c
ÈÈÈ	JJÈÈ	Q•å^	FÁÈÁÛÓ[æ	VÈ[åå^
ÈÈÈ	íÈÈ	U^•å^	FÈÁÛÓ[æ	Û]!å c

Anchor Bolts

Úç	Û] ^ååååå	Ö:åå^	Ç•D	ÈÈ:å *^ ^} c
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Base Plate

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ÇD	ÇD	Ç•D	Õ^[{ ^d^	
ÈÈíÈÈ	ííÈÈ	ííÈÈ	Ò]å]å^	

Reactions

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FÈÖÁÈÈY ÁÈÁ] @Y å å	ÇVÈSå•D	Så•D	Så•D
FÈÖÁÈÈY ÁÈÁ] @Y å å	GÍÈÈ	GJÈÈ	IFÈÈ
ÈÈÖÁÈÈY ÁÈÁ] @Y å å	GÍÈÈ	GJÈÈ	HFÈÈ
FÈÖÁÈÈÈÈÖÁÈÈY ÁÈÁ] @Y å å	JIJÈÈ	JÈÈÈ	ííÈÈ
FÈÖÁÈÈÈÈ	FÈÈÈÈ	FÈÈÈÈ	IFÈÈÈ
ÈÈÖÁÈÈÈÈ	FÈÈÈÈ	FÈÈÈÈ	HFÈÈÈ
FÈÖÁÈÈÈÈY ÁÈÁ] @Y å å	íííÈÈÈ	íÈÈÈÈÈ	HÈÈÈÈÈ

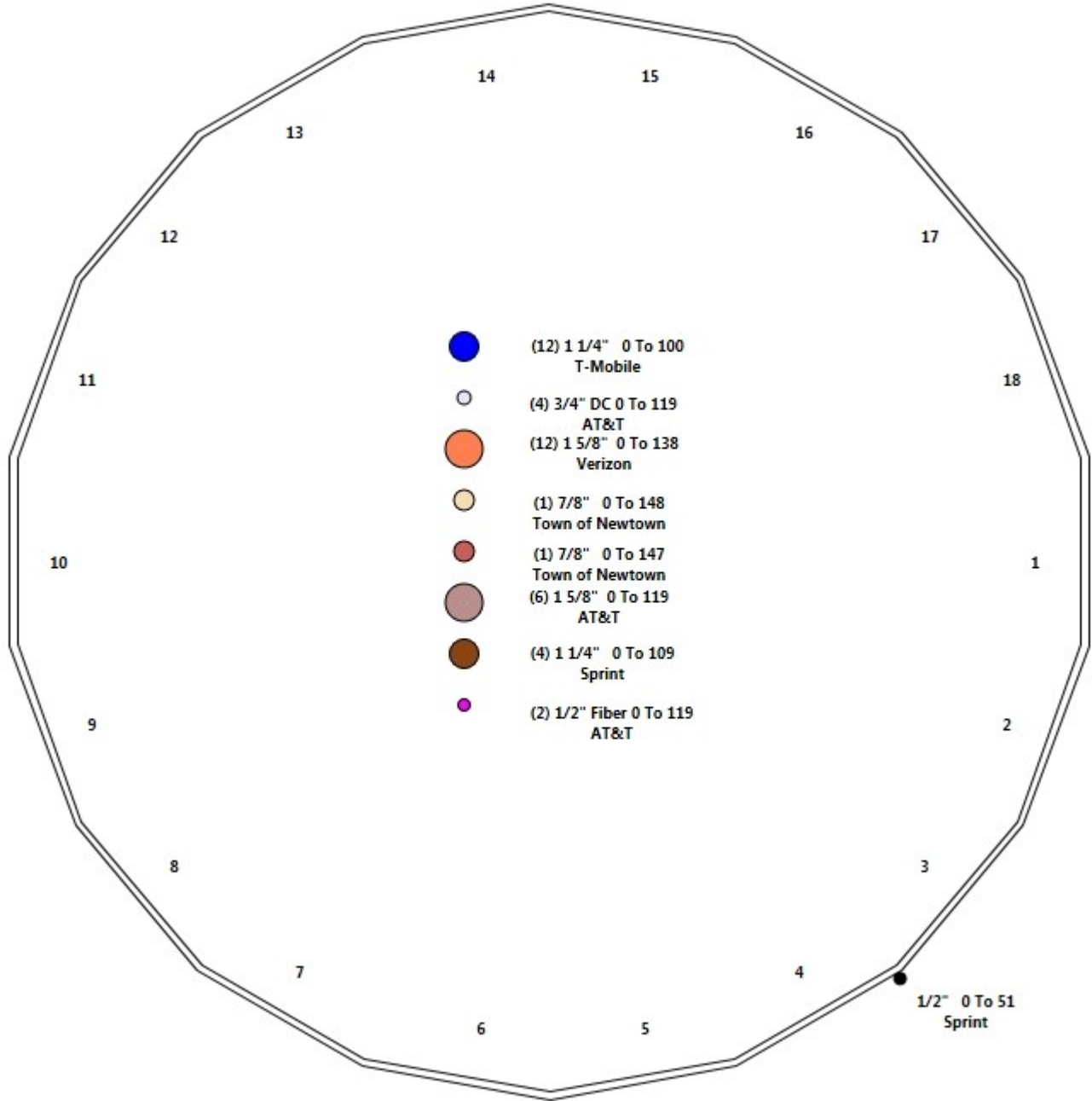
Structure: CT13057-A-SBA - Coax Line Placement

Type: T [] [] [] [] ^
Site Name: P ^, q, }
Height: F i [] [] [] [] C

Í Æ J B Æ F J



Ú æ ^ Á



Shaft Properties

Structure: ÔVFHÍ í ÈÛÓÇÈ Site Name: Þ^, ç, } Height: Fì ÌÈÁÇ Base Elev: ÈÈÈÁÇD Gh: FÈ	Code: ÒÇÈVÇÈÈÇÇÈÖ Ì ÈI ÈÈFJ Exposure: Ò Crest Height: ÈÈÈ Site Class: ÖÁÛÇ-ÁÛ ç Struct Class: Ç
Topography: F	Úæ^KÁ



Sec. No.	Shape	Length (ft)	Thick (in)	Fy (ksi)	Joint Type	Overlap (in)	Weight (lb)
F	Fì	Í ÌÈÈÈ	ÈÈÍ ÌÈ	ÍÍ		ÈÈÈ	JÈÍ H
G	Fì	Í ÌÈÈÈ	ÈÈFGÍ	ÍÍ	Ùjç	ì ÇÈÈ	ì ÈÈ
H	Fì	Í FÈÈÈ	ÈÈÍ ÈÈ	ÍÍ	Ùjç	ì ÈÈÈ	HÈÇÇ
I	Fì	Ç ÌÈÈÈ	ÈÈÍ ÌÍ	ÍÍ	Øæ*^	ÈÈÈ	FÈÈÇ
Total Shaft Weight:							21,203

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V}]

Sec. No.	Dia (in)	Elev (ft)	Area (sqin)	Ix (in^4)	W/t Ratio	D/t Ratio	Dia (in)	Elev (ft)	Area (sqin)	Ix (in^4)	W/t Ratio	D/t Ratio	Taper
F	Í ÌÈH	ÈÈÈ	Í ÌÈÈ	Ç ÈJÈÈ	Ç ÈÈ	Fì ÌÈÈ	Í ÌÈJ	Í ÌÈÈ	Í ÌÈÇ	Fì Ç ÈÈ	Ç ÈÈ	FÇÈÈ	ÈÈÈJ ÌÈ
G	Í ÌÈÌ	HJÈÈ	Í ÌÈÈ	FHì ÈÈÈ	Ç ÈÈ	Fì HÈÈ	H ÌÈH	ì ÌÈÈ	H ÌÈÈ	Ì JHJÈÈ	Ç ÈÈ	FÇÈÈ	ÈÈÈJ ÌÈ
H	HJÈÌ	ì JÈÈ	HÈÈÇ	Ì Ç ÌÈÈ	Ç ÈÈ	Fì JÈÈ	HÈÈ	FÇÈÈÈ	Ç ÈÈÈ	HÈÇÈÈÈ	Ç ÈÈÈ	FÇÈÈ	ÈÈÈJ ÌÈ
I	HÈÈÌ	FÇÈÈ	Fì ÈÈÈ	Ç ÈÈÈ	Ç ÈÈÈ	Fì ÌÈÈ	Ç ÈÈÈ	Fì ÌÈÈÈ	Fì ÈÈÈ	FÇÈÈÈÈÈ	Ç ÈÈÈ	FHì ÈÈÈ	ÈÈÈJ ÌÈ

8]gWYhY'5 ddi fhYbUbWYg

b[A^

Q^

No.	Elev (ft)	Description	Qty	Weight (lb)	CaAa (sf)	CaAa Factor	Weight (lb)	CaAa (sf)	CaAa Factor	Hor. Ecc. (ft)	Vert Ecc (ft)
€€€	FFi €€	Q D A B A A O O		€€€		Q • a ^					
€€€	F€J €€	Q D A F A B A A O [a a		€€€		Q • a ^					
€€€	JJ€€	Q C D F A F D A A O [a a		€€€		Q • a ^					
€€€	i €€€	Q D A F B A A O [a a		€€i		U • a ^					

Linear Appurtenance Segment Forces (Factored)

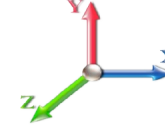
Structure: ÓV F H É Í Ì È Ò É Ú Ó È	Code: Ò Q È V Q È È G G È Ò	Í Ì È Ì È È F J
Site Name: P ^ , q , }	Exposure: Ò	
Height: F Í Ì È È Á G C	Crest Height: È È È	
Base Elev: È È È È Á G D	Site Class: Ò Á Ú G Á Ú Ì á	
Gh: F È È	Topography: F	Struct Class: Q



Load Case: F È Ò Á È Á È Y Á H Á] @ Y á á

Dead Load Factor F È È

Wind Load Factor F È È



Iterations GH

Top Elev (ft)	Description	Wind Exposed	Length (ft)	Ca	Exposed Width (in)	Area (sqft)	CaAa (sqft)	Ra	Cf Adjust Factor	qz (psf)	F X (lb)	Dead Load (lb)
Í È È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F G	È È È È	F Í È Ì J	È È È	È È Í
F È È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F G	È È È È	F Í È Ì J	È È È	È È Í
F Í È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F G	È È È È	F Í È Ì J	È È È	È È Í
G È È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F G	È È È È	F Í È Ì F	È È È	È È Í
G Í È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F H	È È È È	F J È Ì H	È È È	È È Í
H È È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F H	È È È È	G È È Í F	È È È	È È Í
H Í È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F H	È È È È	G È È Í H	È È È	È È Í
H Ú È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì G	È È È	È È È F H	È È È È	G È È Í H	È È È	È È Í
I È È	F È Ò Á È Á È] @ Y á á	Y ^	F È È	È È È È	È È Í	È È Ì	È È È	È È È F I	È È È È	G È È Í F	È È È	È È J
I Í È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F I	È È È È	G È È Í G	È È È	È È Í
Í È È	F È Ò Á È Á È] @ Y á á	Y ^	Í È È	È È È È	È È Í	È È Ì	È È È	È È È F I	È È È È	G È È Í	È È È	È È Í
Í È È	F È Ò Á È Á È] @ Y á á	Y ^	È È È	È È È È	È È Í	È È H	È È È	È È È F I	È È È È	G È È Í	È È È	È È È
Totals:											0.0	9.7

Calculated Forces

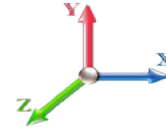
Structure: $\hat{O}\hat{V}\hat{F}\hat{H}\hat{E}\hat{I}\hat{I}\hat{E}\hat{E}\hat{U}\hat{O}\hat{C}\hat{E}$
 Site Name: $\hat{P}\hat{A}, \hat{Q}, \hat{J}$
 Height: $\hat{F}\hat{I}\hat{I}\hat{E}\hat{E}\hat{A}\hat{G}\hat{C}$
 Base Elev: $\hat{E}\hat{E}\hat{E}\hat{E}\hat{A}\hat{G}\hat{D}$
 Gh: $\hat{F}\hat{E}$ Topography: \hat{F}

Code: $\hat{O}\hat{Q}\hat{E}\hat{V}\hat{Q}\hat{H}\hat{E}\hat{G}\hat{G}\hat{E}\hat{O}$ $\hat{I}\hat{H}\hat{I}\hat{E}\hat{E}\hat{F}\hat{J}$
 Exposure: \hat{O}
 Crest Height: $\hat{E}\hat{E}\hat{E}$
 Site Class: $\hat{O}\hat{A}\hat{U}\hat{G}\hat{A}\hat{U}\hat{J}\hat{a}$
 Struct Class: \hat{Q}



Load Case: $\hat{F}\hat{E}\hat{O}\hat{A}\hat{E}\hat{F}\hat{E}\hat{Y}\hat{A}\hat{H}\hat{A}\hat{J}\hat{a}\hat{V}\hat{a}\hat{a}$

Dead Load Factor $\hat{F}\hat{E}\hat{E}$
 Wind Load Factor $\hat{F}\hat{E}\hat{E}$



Iterations $\hat{G}\hat{H}$

Seg Elev (ft)	Pu (kips)	Vu (kips)	Tu (ft-kips)	Mu MZ (ft-kips)	Mu MX (ft-kips)	Resultant Moment (ft-kips)	phi Pn (kips)	phi Vn (kips)	phi Tn (ft-kips)	phi Mn (ft-kips)	Total Deflect (in)	Rotation Sway (deg)	Rotation Twist (deg)	Stress Ratio
1	100	200	300	400	500	600	700	800	900	1000	1100	1200	1300	1400
2	200	400	600	800	1000	1200	1400	1600	1800	2000	2200	2400	2600	2800
3	300	600	900	1200	1600	2000	2400	2800	3200	3600	4000	4400	4800	5200
4	400	800	1200	1600	2100	2600	3100	3600	4100	4600	5100	5600	6100	6600
5	500	1000	1600	2100	2700	3300	3900	4500	5100	5700	6300	6900	7500	8100
6	600	1200	2000	2700	3400	4100	4800	5500	6200	6900	7600	8300	9000	9700
7	700	1400	2400	3200	4000	4800	5600	6400	7200	8000	8800	9600	10400	11200
8	800	1600	2800	3700	4600	5500	6400	7300	8200	9100	10000	10900	11800	12700
9	900	1800	3200	4200	5100	6100	7000	7900	8800	9700	10600	11500	12400	13300
10	1000	2000	3600	4600	5600	6600	7500	8400	9300	10200	11100	12000	12900	13800
11	1100	2200	4000	5000	6000	7000	7900	8800	9700	10600	11500	12400	13300	14200
12	1200	2400	4400	5400	6400	7400	8300	9200	10100	11000	11900	12800	13700	14600
13	1300	2600	4800	5800	6800	7800	8700	9600	10500	11400	12300	13200	14100	15000
14	1400	2800	5200	6200	7200	8200	9100	10000	10900	11800	12700	13600	14500	15400
15	1500	3000	5600	6600	7600	8600	9500	10400	11300	12200	13100	14000	14900	15800
16	1600	3200	6000	7000	8000	9000	9900	10800	11700	12600	13500	14400	15300	16200
17	1700	3400	6400	7400	8400	9400	10300	11200	12100	13000	13900	14800	15700	16600
18	1800	3600	6800	7800	8800	9800	10700	11600	12500	13400	14300	15200	16100	17000
19	1900	3800	7200	8200	9200	10200	11100	12000	12900	13800	14700	15600	16500	17400
20	2000	4000	7600	8600	9600	10600	11500	12400	13300	14200	15100	16000	16900	17800
21	2100	4200	8000	9000	10000	11000	11900	12800	13700	14600	15500	16400	17300	18200
22	2200	4400	8400	9400	10400	11400	12300	13200	14100	15000	15900	16800	17700	18600
23	2300	4600	8800	9800	10800	11800	12700	13600	14500	15400	16300	17200	18100	19000
24	2400	4800	9200	10200	11200	12200	13100	14000	14900	15800	16700	17600	18500	19400
25	2500	5000	9600	10600	11600	12600	13500	14400	15300	16200	17100	18000	18900	19800
26	2600	5200	10000	11000	12000	13000	13900	14800	15700	16600	17500	18400	19300	20200
27	2700	5400	10400	11400	12400	13400	14300	15200	16100	17000	17900	18800	19700	20600
28	2800	5600	10800	11800	12800	13800	14700	15600	16500	17400	18300	19200	20100	21000
29	2900	5800	11200	12200	13200	14200	15100	16000	16900	17800	18700	19600	20500	21400
30	3000	6000	11600	12600	13600	14600	15500	16400	17300	18200	19100	20000	20900	21800
31	3100	6200	12000	13000	14000	15000	15900	16800	17700	18600	19500	20400	21300	22200
32	3200	6400	12400	13400	14400	15400	16300	17200	18100	19000	19900	20800	21700	22600
33	3300	6600	12800	13800	14800	15800	16700	17600	18500	19400	20300	21200	22100	23000
34	3400	6800	13200	14200	15200	16200	17100	18000	18900	19800	20700	21600	22500	23400
35	3500	7000	13600	14600	15600	16600	17500	18400	19300	20200	21100	22000	22900	23800
36	3600	7200	14000	15000	16000	17000	17900	18800	19700	20600	21500	22400	23300	24200
37	3700	7400	14400	15400	16400	17400	18300	19200	20100	21000	21900	22800	23700	24600
38	3800	7600	14800	15800	16800	17800	18700	19600	20500	21400	22300	23200	24100	25000
39	3900	7800	15200	16200	17200	18200	19100	20000	20900	21800	22700	23600	24500	25400
40	4000	8000	15600	16600	17600	18600	19500	20400	21300	22200	23100	24000	24900	25800
41	4100	8200	16000	17000	18000	19000	19900	20800	21700	22600	23500	24400	25300	26200
42	4200	8400	16400	17400	18400	19400	20300	21200	22100	23000	23900	24800	25700	26600
43	4300	8600	16800	17800	18800	19800	20700	21600	22500	23400	24300	25200	26100	27000
44	4400	8800	17200	18200	19200	20200	21100	22000	22900	23800	24700	25600	26500	27400
45	4500	9000	17600	18600	19600	20600	21500	22400	23300	24200	25100	26000	26900	27800
46	4600	9200	18000	19000	20000	21000	21900	22800	23700	24600	25500	26400	27300	28200
47	4700	9400	18400	19400	20400	21400	22300	23200	24100	25000	25900	26800	27700	28600
48	4800	9600	18800	19800	20800	21800	22700	23600	24500	25400	26300	27200	28100	29000
49	4900	9800	19200	20200	21200	22200	23100	24000	24900	25800	26700	27600	28500	29400
50	5000	10000	19600	20600	21600	22600	23500	24400	25300	26200	27100	28000	28900	29800

Discrete Appurtenance Forces

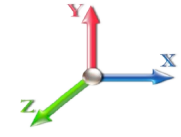
Structure: $\hat{\sigma} \nu \phi \eta \epsilon \iota \dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 Site Name: $\rho \wedge, \rho, \}$
 Height: $\phi \dot{\iota} \dot{\iota} \epsilon \epsilon \wedge \rho \epsilon$
 Base Elev: $\epsilon \dot{\iota} \epsilon \epsilon \epsilon \wedge \rho \epsilon$
 Gh: $\phi \dot{\iota} \dot{\iota}$ Topography: F

Code: $\hat{\sigma} \nu \phi \eta \epsilon \iota \dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 Exposure: $\hat{\sigma}$
 Crest Height: $\epsilon \dot{\iota} \epsilon \epsilon$
 Site Class: $\hat{\sigma} \nu \phi \eta \epsilon \iota \dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 Struct Class: ω

$\dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 $\dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 $\dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 $\dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$



Load Case: $\epsilon \dot{\iota} \epsilon \epsilon \wedge \rho \epsilon \phi \eta \epsilon \iota \dot{\iota} \epsilon \mu \dot{\iota} \omega \epsilon \epsilon$
 Dead Load Factor $\epsilon \dot{\iota} \epsilon \epsilon$
 Wind Load Factor $\phi \dot{\iota} \dot{\iota} \epsilon \epsilon$



Iterations GH

No.	Elev (ft)	Description	Qty	qz (psf)	qzGh (psf)	Orient Factor x Ka	Ka	Total CaAa (sf)	Dead Load (lb)	Horiz Ecc (ft)	Vert Ecc (ft)	Wind FX (lb)	Mom Y (lb-ft)	Mom Z (lb-ft)
AF	11.00	ÖÖB/ÖÖI JCOÖE	AF	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
AG	11.00	ÏËà @ ä * Ä[ä	AG	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
AH	11.00	Üä ^Ä[~ } c	AH	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	V[{ ä[^	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	Ücä ä[~	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	ÜÖBÄ ÆI Ä^çGY	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	ÖÝÖEÏ FÉ HÉ ÖÖ	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	ÜSÖÜçI ÆI	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ä	11.00	ÖJÜÏ ÆI ÖÖBÄ	Ä	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FE	11.00	Ï, Ä[{ Ä[] {	FE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FF	11.00	ÜÜPÄ[] {	FF	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FG	11.00	Üä &ä ÖÖI ÉI É ÉÉI É Ö	FG	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FH	11.00	Üä ^Ä[~ c	FH	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FI	11.00	Üä Ü[Ä[] { ÄÄ	FI	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FÍ	11.00	Öä • [] ÄÜWÄI I HÖG	FÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FÍ	11.00	Öä • [] ÄI I JÄI ÖFG	FÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FÍ	11.00	Sä @ ä Ä ÉÉÉÉI	FÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FÍ	11.00	Ï, Ä[{ Ä[] {	FÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
FJ	11.00	Ü, ^, ä^SÖÜçI Æ	FJ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ÖE	11.00	Ü, ^, ä^ÄI É	ÖE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ÖF	11.00	ÏÉÄ P: ÄÜPÄÜW	ÖF	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ÖG	11.00	ÖÜYXVT FI ÖÖE	ÖG	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ÖH	11.00	FJÉET P: ÄÜPÄÜW	ÖH	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
G	11.00	ÖÜYXÜÜFI ÖÖE	G	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
GÍ	11.00	VÖEÜPI çÖÄÜW	GÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
GÍ	11.00	ÖVÖEÉÄÜÖV	GÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
GÍ	11.00	VÖE { • Ä Ä [] ä *	GÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
GÍ	11.00	ÏÉÄ P: ÄÜPÄÜW	GÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
GJ	11.00	ÏYÉI FI ÖÜEFT	GJ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HE	11.00	ÜÜI ÉI ÉÉÖÜSG	HE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HF	11.00	ÖÜYXF I ÉÉI F HÖEÖE	HF	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HG	11.00	ÏI ÇÄFÉI ÄÖä Ä•	HG	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HH	11.00	ÖVT ÖE FI ÇÖEÖÇÄVT ÖE	HH	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
H	11.00	Üä { } Ä Ä ä Ää	H	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HÍ	11.00	ÏÉÉ HÄÜcä ä[~	HÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HÍ	11.00	ÏÉÉ Ç ÉÖ	HÍ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Totals:									8,458.03					
										15,429.53				

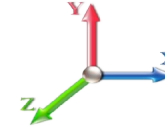
Linear Appurtenance Segment Forces (Factored)

Structure: ÔVFHEÍ Ì ÈËËÚÓË	Code: ÒQËVQËÈGGËÖ	Í ËË ËËFJ
Site Name: Þ^, ç, }	Exposure: Ò	
Height: FÌ Ì ÈÈÁÇ	Crest Height: ÈÈÈ	
Base Elev: ÈÈÈÈÁÇD	Site Class: ÖÁËÜç-ÁË ã	
Gh: FÈ	Topography: F	Struct Class: Q



Load Case: FÈÖÁÈ FÈÖÁÈ FÈY ã ÈÁ] ÖY ã á

Dead Load Factor FÈÈ
Wind Load Factor FÈÈ



Iterations GH

Top Elev (ft)	Description	Wind Exposed	Length (ft)	Ca	Exposed Width (in)	Area (sqft)	CaAa (sqft)	Ra	Cf Adjust Factor	qz (psf)	F X (lb)	Dead Load (lb)
Í ÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ F	ÈÈÈ	ÈÈÈFG	ÈÈÈÈ	Í ÈÈ Í	ÈÈÈ	F ÈÈ È
F ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ Ì	ÈÈÈ	ÈÈÈFG	ÈÈÈÈ	Í ÈÈ Í	ÈÈÈ	F Í ÈÈ H
F Í ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ H	ÈÈÈ	ÈÈÈFG	ÈÈÈÈ	Í ÈÈ Í	ÈÈÈ	F Í ÈÈ Ì
G ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ Í	ÈÈÈ	ÈÈÈFG	ÈÈÈÈ	Í ÈÈ Ì H	ÈÈÈ	F Í ÈÈ Ì
G Í ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ J	ÈÈÈ	ÈÈÈFH	ÈÈÈÈ	Í ÈÈ Ì Í	ÈÈÈ	F Í ÈÈ H
H ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ F	ÈÈÈ	ÈÈÈFH	ÈÈÈÈ	Í ÈÈ Ì G	ÈÈÈ	F Í ÈÈ Ì
H Í ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ H	ÈÈÈ	ÈÈÈFH	ÈÈÈÈ	Í ÈÈ Ì J	ÈÈÈ	F Í ÈÈ Ì
HJ ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ ÇH	ÈÈÈ	ÈÈÈFH	ÈÈÈÈ	Í ÈÈ Ì FF	ÈÈÈ	F Í ÈÈ Ì
I ÈÈÈ	FÈÁÁÖ	ÿ^	F ÈÈÈ	ÈÈÈÈ	ÈÈ Í	ÈÈ F	ÈÈÈ	ÈÈÈF	ÈÈÈÈ	Í ÈÈ Ì Í	ÈÈÈ	H ÈÈ Ì
I Í ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ Í	ÈÈÈ	ÈÈÈF	ÈÈÈÈ	Í ÈÈ Ì È	ÈÈÈ	FJ ÈÈ Ì
Í ÈÈÈ	FÈÁÁÖ	ÿ^	Í ÈÈ	ÈÈÈÈ	ÈÈ Í	FÈ Ì	ÈÈÈ	ÈÈÈF	ÈÈÈÈ	Í ÈÈ Ì È	ÈÈÈ	G ÈÈÈ G
Í ÈÈ È	FÈÁÁÖ	ÿ^	ÈÈ È	ÈÈÈÈ	ÈÈ Í	ÈÈ Ì	ÈÈÈ	ÈÈÈF	ÈÈÈÈ	Í ÈÈ Ì I	ÈÈÈ	G ÈÈ F
Totals:											0.0	178.6

Calculated Forces

Structure: ÔÛFHÉÍ Ì ÊÛÛÓÇÈ
Site Name: Ð^, Ç, }
Height: FÌ Ì ÊÇÁÇÇ
Base Elev: ÊÇÇÇÁÇÇ
Gh: FÈÈ

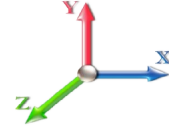
Code: ÒÇÛÛVÇÛÈÇÇÇÇÇ
Exposure: Ò
Crest Height: ÊÇÈÈ
Site Class: ÒËËÛÇÁÛÌ Ç
Struct Class: Ç

Iterations: 10
GH: 10



Load Case: FÈÇÇÁÇÇ FÈÇÇÁÇÇ FÈÈ Ì ÊÇÁ Ç] ÇÁ Ç à

Dead Load Factor: FÈÈÈ
Wind Load Factor: FÈÈÈ



Seg Elev (ft)	Pu FY (-) (kips)	Vu FX (-) (kips)	Tu MY (-) (ft-kips)	Mu MZ (ft-kips)	Mu MX (ft-kips)	Resultant Moment (ft-kips)	phi Pn (kips)	phi Vn (kips)	phi Tn (ft-kips)	phi Mn (ft-kips)	Total Deflect (in)	Rotation Sway (deg)	Rotation Twist (deg)	Stress Ratio
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
7.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
9.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
11.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
12.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
13.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
14.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
16.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
17.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
18.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
22.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
23.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
24.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
26.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
27.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
29.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
31.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
33.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
34.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
36.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
37.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
38.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
39.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
40.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
41.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
43.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
44.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
45.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
46.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
47.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
49.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Calculated Forces

Structure: $\hat{O}V F H \acute{E} \acute{I} \acute{I} \acute{E} \acute{U} \acute{O} \acute{C} \acute{E}$
Site Name: $P \wedge, \acute{C}, \}$
Height: $F \acute{I} \acute{I} \acute{E} \acute{C} \acute{A} \acute{C}$
Base Elev: $\acute{E} \acute{E} \acute{C} \acute{C} \acute{A} \acute{C}$
Gh: $F \acute{E}$

Code: $\acute{O} \acute{C} \acute{E} V \acute{O} \acute{E} \acute{G} \acute{G} \acute{E} \acute{O}$
Exposure: \acute{O}
Crest Height: $\acute{E} \acute{E} \acute{E}$
Site Class: $\acute{O} \acute{A} \acute{U} \acute{G} \acute{A} \acute{U} \acute{I} \acute{q}$
Struct Class: \acute{O}

Iterations $\acute{I} \acute{E} \acute{I} \acute{E} \acute{E} \acute{F} \acute{J}$
Ss $\acute{E} \acute{E} \acute{E}$
S1 $\acute{E} \acute{E} \acute{I}$
SA $\acute{E} \acute{E} \acute{I}$
Seismic Importance Factor $F \acute{E} \acute{E}$



Topography: F

$\acute{U} \acute{a} \acute{e} \wedge \acute{K} \acute{G}$

Load Case: $F \acute{E} \acute{O} \acute{A} \acute{E} \acute{F} \acute{E} \acute{O}$

Gust Response Factor $F \acute{E} \acute{E}$

Sds $\acute{E} \acute{E} \acute{G}$

Iterations GF

Dead Load Factor $F \acute{E} \acute{E}$

Seismic Load Factor $F \acute{E} \acute{E}$

Sd1 $\acute{E} \acute{E} \acute{E}$

Ss $\acute{E} \acute{E} \acute{E}$

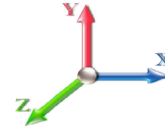
S1 $\acute{E} \acute{E} \acute{I}$

Wind Load Factor $\acute{E} \acute{E} \acute{E}$

Structure Frequency (f1) $\acute{E} \acute{E} \acute{I}$

SA $\acute{E} \acute{E} \acute{I}$

Seismic Importance Factor $F \acute{E} \acute{E}$



Seg Elev (ft)	Pu FY (-) (kips)	Vu FX (-) (kips)	Tu MY (-) (ft-kips)	Mu MZ (ft-kips)	Mu MX (ft-kips)	Resultant Moment (ft-kips)	phi Pn (kips)	phi Vn (kips)	phi Tn (ft-kips)	phi Mn (ft-kips)	Total Deflect (in)	Rotation Sway (deg)	Rotation Twist (deg)	Stress Ratio
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
7.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
9.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
11.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
12.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
13.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
14.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
16.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
17.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
18.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
22.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
23.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
24.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
26.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
27.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
29.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
31.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
33.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
34.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
36.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
37.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
38.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
39.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
40.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
41.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
43.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
44.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
45.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
46.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
47.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
49.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Calculated Forces

Structure: $\hat{O}V F H \acute{E} \acute{I} \acute{I} \acute{E} \acute{U} \acute{O} \acute{C} \acute{E}$
Site Name: $P \wedge, \acute{C}, \}$
Height: $F \acute{I} \acute{I} \acute{E} \acute{C} \acute{A} \acute{C}$
Base Elev: $\acute{E} \acute{E} \acute{C} \acute{C} \acute{A} \acute{C}$
Gh: $F \acute{E}$

Code: $\acute{O} \acute{Q} \acute{E} \acute{V} \acute{Q} \acute{E} \acute{G} \acute{G} \acute{E} \acute{O}$
Exposure: \acute{O}
Crest Height: $\acute{E} \acute{E} \acute{E}$
Site Class: $\acute{O} \acute{A} \acute{U} \acute{G} \acute{A} \acute{U} \acute{I} \acute{q}$
Struct Class: \acute{Q}

Iterations $\acute{I} \acute{E} \acute{I} \acute{E} \acute{E} \acute{F} \acute{J}$
Ss $\acute{E} \acute{E} \acute{E}$
S1 $\acute{E} \acute{E} \acute{I}$
SA $\acute{E} \acute{E} \acute{I}$
Seismic Importance Factor $F \acute{E} \acute{E}$



Load Case: $\acute{E} \acute{I} \acute{O} \acute{A} \acute{E} \acute{A} \acute{E} \acute{O}$

Gust Response Factor $F \acute{E} \acute{E}$

Dead Load Factor $\acute{E} \acute{I} \acute{E}$

Wind Load Factor $\acute{E} \acute{E} \acute{E}$

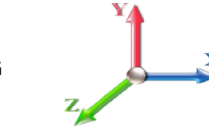
Seismic Load Factor $F \acute{E} \acute{E}$

Structure Frequency (f1) $\acute{E} \acute{E} \acute{I}$

Sds $\acute{E} \acute{E} \acute{G}$

Sd1 $\acute{E} \acute{E} \acute{E}$

SA $\acute{E} \acute{E} \acute{I}$



Iterations

GF

Ss $\acute{E} \acute{E} \acute{E}$

S1 $\acute{E} \acute{E} \acute{I}$

Seismic Importance Factor $F \acute{E} \acute{E}$

Seg Elev (ft)	Pu FY (-) (kips)	Vu FX (-) (kips)	Tu MY (-) (ft-kips)	Mu MZ (ft-kips)	Mu MX (ft-kips)	Resultant Moment (ft-kips)	phi Pn (kips)	phi Vn (kips)	phi Tn (ft-kips)	phi Mn (ft-kips)	Total Deflect (in)	Rotation Sway (deg)	Rotation Twist (deg)	Stress Ratio
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
7.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
9.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
11.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
12.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
13.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
14.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
15.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
16.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
17.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
18.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
22.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
23.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
24.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
26.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
27.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
29.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
31.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
33.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
34.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
36.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
37.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
38.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
39.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
40.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
41.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
43.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
44.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
45.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
46.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
47.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
49.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Total Applied Force Summary

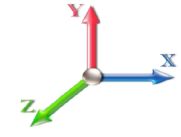
Structure: ÔVFHÉÍ ÌÈÈÚÓÈ	Code: ÒQÈVQÈÈGGÈÖ	Í ÆI ÈÈFJ
Site Name: Þ^, ç, }	Exposure: Ò	
Height: FÌ ÌÈÈÁÇ	Crest Height: ÈÈÈ	
Base Elev: ÈÈÈÈÁÇ	Site Class: ÖÄÚÇ-ÁÚ ç	
Gh: FÈ	Topography: F	Struct Class: Q
		Úæ^ÁÈÈ



Load Case: FÈÖÁÈÈÈY Á ÈÁ] @Y ç à

Dead Load Factor FÈÈ

Wind Load Factor FÈÈ



Iterations GG

Elev (ft)	Description	Lateral FX (-) (lb)	Axial FY (-) (lb)	Torsion MY (lb-ft)	Moment MZ (lb-ft)
ÈÈÈ		ÈÈÈ	ÈÈÈ	ÈÈÈ	ÈÈÈ
Í ÈÈ		FGÈÈ F	FG Í ÈÇ	ÈÈÈ	ÈÈÈ
FÈÈÈ		FGÈÈ Í	FG Í ÈÈÈ	ÈÈÈ	ÈÈÈ
FÌ ÈÈ		FFÌ ÈÈ Ì	FGGÈÈ Ì	ÈÈÈ	ÈÈÈ
GÈÈÈ		FGÈÈ H	FGGÈÈ F	ÈÈÈ	ÈÈÈ
G ÈÈ		FG ÈÈ Ì	FFÌ FÈÇ	ÈÈÈ	ÈÈÈ
HÈÈÈ		FGÈÈ J	FFÌ ÈÈG	ÈÈÈ	ÈÈÈ
H ÈÈ		FHÈÈ H	FFHÌ ÈÈ Ì	ÈÈÈ	ÈÈÈ
HUÈÈ		FÈÈ ÈÈ Ì	Ì JÌ ÈÈ G	ÈÈÈ	ÈÈÈ
I ÈÈÈ		G ÈÈ F	HÌ FÈÌ	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		FHÈÈ Ì	FÌ Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì ÈÈÈ		FHÈÈ F	JHÌ ÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì ÈÈ È	(ÇDÁææ@ ^) ø	Ì FÈÈG	FHÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		FFJÈÈ Ì	Ì GÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì ÈÈÈ		FHÈÈ G	Ì JÌ ÈÈ	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		FHÈÈ Ì	Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì ÈÈÈ		FHÈÈ Ç	Ì Ì GÈ Ì	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		FG ÈÈ Ì	Ì Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
Ì JÈÈ		FÈÈÈ F	Ì Ì HÈ Ì	ÈÈÈ	ÈÈÈ
Ì ÈÈÈ		G ÈÈ È	GÌ FÈÈ	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		FÈÈÈ G	FÈÌ FÈ Ì	ÈÈÈ	ÈÈÈ
Ì Ì ÈÈ		G ÈÈ Ì	FHÌ ÈÈ U	ÈÈÈ	ÈÈÈ
JÈÈÈ		FG ÈÈG	Ì Ì HÈ Ì	ÈÈÈ	ÈÈÈ
JÌ ÈÈ		FGÈÈ Ì	Ì Ì JÈÈ	ÈÈÈ	ÈÈÈ
JJÈÈ È	(FJDÁææ@ ^) ø	FFHUÈÈ Ì	GÌ HÌ ÈÈ Ì	ÈÈÈ	ÈÈÈ
FÈÈÈÈ		FFÈÈ Ì	Ì JÈÈG	ÈÈÈ	ÈÈÈ
FÈÌ ÈÈ		FFÌ ÈÈ J	Ì JFÈÈ Ì	ÈÈÈ	ÈÈÈ
FÈJÈÈ	(ÇDÁææ@ ^) ø	JG ÈÈ F	GÌ HÈÈ	ÈÈÈ	ÈÈÈ
FFÈÈÈ		GGÈÈ Ì	FFFÈÈ Ì	ÈÈÈ	ÈÈÈ
FFÌ ÈÈ		FFHÈÈ Ì	Ì Ì JÈÈ Ì	ÈÈÈ	ÈÈÈ
FFÌ ÈÈ È	(ÇDÁææ@ ^) ø	FHÌ GÈ Ç	Ì ÈÈ GÈ Ì	ÈÈÈ	ÈÈÈ
FGÈÈÈ		HGÈÈ Ì	FÌ Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
FG ÈÈ		FÈÈ ÈÈ U	HÌ Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
FHÈÈÈ		FÈÈ ÈÈ Ì	HÌ Ì ÈÈ Ì	ÈÈÈ	ÈÈÈ
FHÌ ÈÈ		FÈÈÈ Ì	HÌ Ì ÈÈ G	ÈÈÈ	ÈÈÈ
FHÌ ÈÈ È	(FJDÁææ@ ^) ø	Ì Ì Ì ÈÈ	FÌ Ì ÈÈ H	ÈÈÈ	ÈÈÈ
FÌ ÈÈÈ		Ì JÈÈ Ì	FÌ ÈÈ Ì	ÈÈÈ	ÈÈÈ
FÌ Ì ÈÈ		JÌ ÈÈ G	GÌ HÈ Ì	ÈÈÈ	ÈÈÈ
FÌ Ì ÈÈ È	(ÇDÁææ@ ^) ø	Ì Ì ÈÈ È	FÌ GÈÈ È	ÈÈÈ	FJÈÈG
FÌ Ì ÈÈ È	(FJDÁææ@ ^) ø	JÈÈ Ì	FFJÈÈ J	ÈÈÈ	FGJÈÈÈ
	Totals:	7,594.25	34,520.97	0.00	148.32

Linear Appurtenance Segment Forces (Factored)

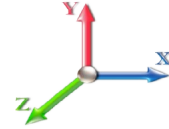
Structure: ÔV F H É Í Ì È Ò Ü Ó È Site Name: P ^, q, } Height: F Ì Ì È Á Ç C Base Elev: È È È È Á Ç D Gh: F È	Code: Ô Ç È V Ç È È Ç Ç È Ö Exposure: Ô Crest Height: È È È Site Class: Ô Ä Ü ç - Ä Ü ç Struct Class: Ç
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Load Case: F È Ö Ä È F È Y Ä È Á] Ç Y ç à

Dead Load Factor F È È

Wind Load Factor F È È



Iterations GG

Top Elev (ft)	Description	Wind Exposed	Length (ft)	Ca	Exposed Width (in)	Area (sqft)	CaAa (sqft)	Ra	Cf Adjust Factor	qz (psf)	F X (lb)	Dead Load (lb)
1.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FG	0.000	1.0 G	0.000	0.000
2.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FG	0.000	1.0 G	0.000	0.000
3.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FG	0.000	1.0 G	0.000	0.000
4.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FG	0.000	1.0 G	0.000	0.000
5.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
6.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
7.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
8.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
9.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
10.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
11.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
12.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
13.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
14.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
15.0	FRAM[] 2P	Y^	1.0	0.000	0.0	0.0	0.000	0.0FH	0.000	1.0 G	0.000	0.000
Totals:											0.0	8.1

Final Analysis Summary

Structure: ÓV F H É Í Ì È Û Ó È Site Name: P ^, q, } Height: F Ì È Á Ç D Base Elev: È È È Á Ç D Gh: F È	Code: Ò Ç È V Ç È È Ç Ç È Ò Exposure: Ò Crest Height: È È È Site Class: Ò Á Û ç Á Û ç Struct Class: Ç
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F Y U W Ç b g

Load Case	Shear FX (kips)	Shear FZ (kips)	Axial FY (kips)	Moment MX (ft-kips)	Moment MY (ft-kips)	Moment MZ (ft-kips)
F È Ç Ò Á È Á È Y Á H Á } @ V ç á á	G J È H	È È È	I F È Ì	È È È	È È È	G Ì Ç È I
È È Ç Ò Á È Á È Y Á H Á } @ V ç á á	G J È G	È È È	H F È H	È È È	È È È	G Ì F È Ì
F È Ç Ò Á È Á È Ç Ò Á È Á È Y Á È Á } @ V ç á á	J È	È È È	Ì Í È J	È È È	È È È	J I J È È
F È Ç Ò Á È Á È Ç Ò	F È	È È È	I F È H	È È È	È È È	F È F È Í
È È Ç Ò Á È Á È Ç Ò	F È	È È È	H F È Ì	È È È	È È È	F È È È Í
F È Ç Ò Á È Á È Y Á È Á } @ V ç á á	Ì È	È È È	H È È G	È È È	È È È	Ì I H È Ì

A U Ç G f Y g g Y g

Load Case	Pu FY (-) (kips)	Vu FX (-) (kips)	Tu MY (-) (ft-kips)	Mu MZ (ft-kips)	Mu MX (ft-kips)	Resultant Moment (ft-kips)	phi Pn (kips)	phi Vn (kips)	phi Tn (ft-kips)	phi Mn (ft-kips)	Elev (ft)	Stress Ratio
F È Ç Ò Á È Á È Y Á H Á } @ V ç á á	È F È Ì	È Ç J È Ì	È È È	È Ç Ì Ç È	È È È	È Ç Ì Ç È	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È H
È È Ç Ò Á È Á È Y Á H Á } @ V ç á á	È F È H	È Ç J È G	È È È	È Ç Ì F È H	È È È	È Ç Ì F È H	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È J
F È Ç Ò Á È Á È Ç Ò Á È Á È Y Á È Á } @ V ç á á	È Í È J	È Ç È Ì	È È È	È J I J È È	È È È	È J I J È È	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È F F
F È Ç Ò Á È Á È Ç Ò	È F È H	È F È J	È È È	È F È F È Í	È È È	È F È F È Í	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È F
È È Ç Ò Á È Á È Ç Ò	È F È Ì	È F È J	È È È	È F È È È Ì	È È È	È F È È È Ì	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È G
F È Ç Ò Á È Á È Y Á È Á } @ V ç á á	È H È È G	È È È F	È È È	È I H È Ì	È È È	È I H È Ì	I G È È È	Ç F H È È	J Í J È È	Ì Ì Ç È Ì	È È È	È È È G

Base Plate Summary

Structure: 0VFHEÍ Ì ÈÈÚÓ	Code: 0QEV0ÈÈGGËÖ	Site Name: P^, q, }
Site Name: P^, q, }	Exposure: 0	Height: FI Ì ÈÈÁÇC
Height: FI Ì ÈÈÁÇC	Crest Height: ÈÈÈ	Base Elev: ÈÈÈÈÁÇD
Base Elev: ÈÈÈÈÁÇD	Site Class: 0ÁÚá-ÁÚ[q	Gh: ÈÈ
Gh: ÈÈ	Struct Class: Q	Topography: F



Reactions	Base Plate	Anchor Bolts
U!ã q } 0^•ã }	Yield (ksi): Í Ì ÈÈ	Bolt Circle: Í GÈÈ
Moment (kip-ft): H Í ÈÈÈ	Width (in): Í FÈÈ	Number Bolts: FÍ ÈÈÈ
Axial (kip): H ÈÈÈ	Style: 0ã] ^á	Bolt Type: GÈ ÁÈ Ì R
Shear (kip): H ÈÈÈ	Polygon Sides: ÈÈÈ	Bolt Diameter (in): GÈÍ
0ã } •ã }	Clip Length (in): FÈÈÈ	Yield (ksi): Í Ì ÈÈÈ
Moment (kip-ft): G Í GÈÍ	Effective Len (in): Ì ÈÈ	Ultimate (ksi): FÈÈÈÈ
Axial (kip): Í Ì ÈÈJ	Moment (kip-in): Ì Ì ÈÈH	Arrangement: 0~ •ç!^á
Shear (kip): G ÈÈ	Allow Stress (ksi): Í Ì ÈÈ	Cluster Dist (in): Í ÈÈÈ
Moment Design %: Í Ì ÈÈF	Applied Stress (ksi): ÈÈÈ	Start Angle (deg): Í Ì ÈÈÈ
	Stress Ratio: ÈÈ G	0[{ } !^••ã }
		Force (kip): FI ÈÈF
		Allowable (kip): G ÈÈÈ
		Ratio: ÈÈ Í
		V^} •ã }
		Force (kip): FI ÈÈÈ
		Allowable (kip): G ÈÈÈ
		Ratio: ÈÈ H



Monopole Mat Foundation Design

Date	
6/14/2019	
Customer Name:	AT&T
EIA/TIA Standard:	EIA-222-G
Site Name:	
Structure Height (Ft.):	148
Site Number:	CT13057-A-SBA
Engineer Name:	U. Atluri
Engr. Number:	77764
Engineer Login ID:	

Foundation Info Obtained from:

Drawings/Calculations
Monopole
Analysis

Structure Type:

Analysis or Design?

Base Reactions (Factored):

Axial Load (Kips):	65.6	Shear Force (Kips):	29.2
Uplift Force (Kips):	0.0	Moment (Kips-ft):	2869.6

Allowable overstress %: 5.0%

Foundation Geometries:

Diameter of Pier (ft.):	7.0	Depth of Base BG (ft.):	7.5	Mods required -Yes/No ?:	No
Pier Height A. G. (ft.):	0.50	Thickness of Pad (ft):	4.00		
Length of Pad (ft.):	23.5	Width of Pad (ft.):	23.5		
Final Length of pad (ft)	23.5	Final width of pad (ft):	23.5		

Material Properties and Rebar Info:

Concrete Strength (psi):	3000	Steel Elastic Modulus:	29000	ksi
Vertical bar yield (ksi)	60	Tie steel yield (ksi):	60	
Vertical Rebar Size #:	11	Tie / Stirrup Size #:	4	
Qty. of Vertical Rebars:	36	Tie Spacing (in):	12.0	
Pad Rebar Yield (Ksi):	60	Pad Steel Rebar Size (#):	11	
Concrete Cover (in.):	3	Unit Weight of Concrete:	150.0	pcf
Rebar at the bottom of the concrete pad:				
Qty. of Rebar in Pad (L):	24	Qty. of Rebar in Pad (W):	24	
Rebar at the top of the concrete pad:				
Qty. of Rebar in Pad (L):	24	Qty. of Rebar in Pad (W):	24	

Apply 1.35 factor for e/w Per G: 1.35

Soil Design Parameters:

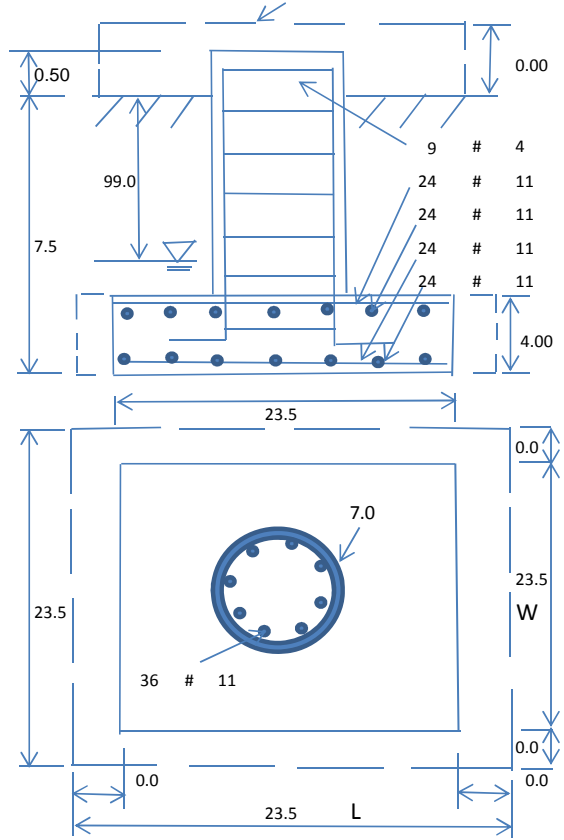
Soil Unit Weight (pcf):	110.0	Soil Buoyant Weight:	50.0	Pcf
Water Table B.G.S. (ft):	99.0	Unit Weight of Water:	62.4	pcf
Ultimate Bearing Pressure (psf):	8000	Ultimate Skin Friction:	425	Psf
Consider Friction for O.T.M. (Y/N):	No	Consider Friction for bearing (Y/N):	Yes	
Consider soil hor. resist. for OTM.:	Yes	Reduction factor on the maximum soil bearing pressure:	1.00	
		Angle from Top of Pad:	30	
		Angle from Bottm of Pad:	25	
		Angle from Bottm of Pad:	25	

Foundation Analysis and Design:

Uplift Strength Reduction Factor:	0.75	Compression Strength Reduction Factor:	0.75
Total Dry Soil Volume (cu. Ft.):	1798.18	Total Dry Soil Weight (Kips):	197.80
Total Buoyant Soil Volume (cu. Ft.):	0.00	Total Buoyant Soil Weight (Kips):	0.00
Total Effective Soil Weight (Kips):	197.80	Weight from the Concrete Block at Top (K):	0.00
Total Dry Concrete Volume (cu. Ft.):	2362.94	Total Dry Concrete Weight (Kips):	354.44
Total Buoyant Concrete Volume (cu. Ft.):	0.00	Total Buoyant Concrete Weight (Kips):	0.00
Total Effective Concrete Weight (Kips):	354.44	Total Vertical Load on Base (Kips):	617.84

Check Soil Capacities:

Calculated Maxium Net Soil Pressure under the base (psf):	2045	<	Allowable Factored Soil Bearing (psf):	6000	0.34	OK!
Allowable Foundation Overturning Resistance (kips-ft.):	6610.7	>	Design Factored Momont (kips-ft):	2835	0.43	OK!
Factor of Safety Against Overturning (O. R. Moment/Design Moment):	2.33					OK!



Check the capacities of Reinforcing Concrete:

Strength reduction factor (Flexure and axial tension):	0.90	Strength reduction factor (Shear):	0.75
Strength reduction factor (Axial compression):	0.65	Wind Load Factor on Concrete Design:	1.00

(1) Concrete Pier:

Vertical Steel Rebar Area (sq. in./each):	1.56	Tie / Stirrup Area (sq. in./each):	0.20			
Calculated Moment Capacity (Mn,Kips-Ft):	8832.5	> Design Factored Moment (Mu, Kips-F	2986.4	0.34	OK!	
Calculated Shear Capacity (Kips):	589.7	> Design Factored Shear (Kips):	29.2	0.05	OK!	
Calculated Tension Capacity (Tn, Kips):	3032.6	> Design Factored Tension (Tu Kips):	0.0	0.00	OK!	
Calculated Compression Capacity (Pn, Kips):	7273.9	> Design Factored Axial Load (Pu Kips):	65.6	0.01	OK!	
Moment & Axial Strength Combination:	0.34	OK! Check Tie Spacing (Design/Required):		1	OK!	
Pier Reinforcement Ratio:	0.010	Reinforcement Ratio is satisfied per ACI				

(2).Concrete Pad:

One-Way Design Shear Capacity (L-Direction, Kips):	1026.7	> One-Way Factored Shear (L-D. Kips):	173.4	0.17	OK!	
One-Way Design Shear Capacity (W-Direction, Kips):	1026.7	> One-Way Factored Shear (W-D., Kips)	173.4	0.17	OK!	
One-Way Design Shear Capacity (Corner-Corner. Kips):	823.5	> One-Way Factored Shear (C-C, Kips):	161.9	0.20	OK!	
Lower Steel Pad Reinforcement Ratio (L-Direct.):	0.0030	OK! Lower Steel Pad Reinf. Ratio (W-Direc	0.0030			
Lower Steel Pad Moment Capacity (L-Direction. Kips-ft):	7202.6	> Moment at Bottom (L-Dir. K-Ft):	1078.2	0.15	OK!	
Lower Steel Pad Moment Capacity (W-Direction. Kips-ft):	7202.6	> Moment at Bottom (W-Dir. K-Ft):	1078.2	0.15	OK!	
Lower Steel Pad Moment Capacity (Corner-Corner,K-ft):	10086.7	> Moment at Bottom (C-C Dir. K-Ft):	1524.8	0.15	OK!	
Upper Steel Pad Reinforcement Ratio (L-Direct.):	0.0030	OK! Upper Steel Reinf. Ratio (W-Dir.):	0.0030			
Upper Steel Pad Moment Capacity (L-Direc. Kips-ft):	7202.6	> Moment at the top (L-Dir K-Ft):	405.3	0.06	OK!	
Upper Steel Pad Moment Capacity (W-Direc. Kips-ft):	7202.6	> Moment at the top (W-Dir K-Ft):	405.3	0.06	OK!	
Upper Steel Pad Moment Capacity (Corner-Corner. K-ft):	10086.7	> Moment at the top (C-C Dir. K-Ft):	381.3	0.04	OK!	

(3).Check Punching Shear Capacity due to Moment in the Pier:

Moment transferred by punching shear:	1147.8	k-ft.	Max. factored shear stress v_{u_CD} :	1.4	Psi
Max. factored shear stress v_{u_AB} :	6.8	Psi	Factored shear Strength ϕv_n :	164.3	Psi
Max. factored shear stress v_u :	6.8	Psi	Check Usage of Punching Shear Capacity:	0.04	OK!

April 22, 2019



Centerline Communications
750 West Center Street, Suite #301
West Bridgewater, MA 02379

RE: Site Number: CT5432 (LTE 2C/3C/4C)
 FA Number: 10071168
 PACE Number: MRCTB037970
 PT Number: -
 Site Name: NEWTOWN EAST CENTRAL
 Site Address: 151 Berkshire Road
 Sandy Hook, CT 06482

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by Centerline Communications to perform a mount analysis on the existing AT&T antenna/RRH mount to determine their capability of supporting the following additional loading:

- (3) 7770 Antennas (55.0"x11.0"x5.0" - Wt. = 35 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7" Φ - Wt. = 33 lbs. /each) (Tower Mount)
- **(6) 800-10965 Antennas (78.7"x20.0"x6.9" - Wt. = 109 lbs. /each)**
- **(3) B5/B12 4449 RRH's (14.9"x13.2"x10.4" - Wt. = 73 lbs. /each)**
- **(3) B2/B66A 8843 RRH's (14.9"x13.2"x10.9" - Wt. = 72 lbs. /each)**
- **(1) Squid Surge Arrestor (24.0"x9.7" Φ - Wt. = 33 lbs. /each)**

**Proposed equipment shown in bold*

No original structural design documents or fabrication drawings were available for the existing mount. HDG's subconsultant, ProVertic LLC, conducted a survey climb and mapping of the existing AT&T antenna mount on April 16, 2019.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-H, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2015 with 2018 Connecticut State Building Code, and AT&T Mount Technical Directive – R12.
- HDG considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all around the mount. Per TIA-222-H and Appendix N of the Connecticut State Building Code, the max basic wind speed for this site is equal to 120 mph with a max basic wind speed with ice of 50 mph and a max ice thickness of 1.0 in. An escalated ice thickness of 1.13 in was used for this analysis.
- HDG considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.
- HDG considers this site to be topographic category 1; tower is located on flat terrain or the bottom of a hill or ridge.
- The mount has been analyzed with load combinations consisting of 250 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 2.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst case location on the mount.
- The existing mount is secured to the existing monopole with ring mount. The connection is considered OK by visual inspection.

Based on our evaluation, we have determined that the existing mount **IS NOT CAPABLE** of supporting the proposed installation. HDG recommends the following modifications:

- **Install new handrall kit, SitePro1 P/N HRK12 (or approved equal).**
- **Remove existing pipe mast and install new 2-1/2" std. (2.88" O.D.) pipe mast behind new 800-10965 antennas secured to existing mount (typ. of 1 per sector, total of 3).**

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Existing (LTE 2C/3C/4C) Mount Rating	29	LC1	103%	FAIL
Modified (LTE 2C/3C/4C) Mount Rating	1	LC16	97%	PASS

Reference Documents:

- Mount mapping report prepared by ProVertic LLC.

This determination was based on the following limitations and assumptions:

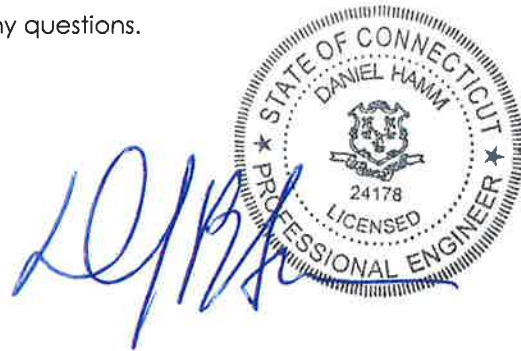
1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,
Hudson Design Group LLC



Michael Cabral
Structural Dept. Head



Daniel P. Hamm, PE
Principal

FIELD PHOTOS:







HUDSON
Design Group LLC

Wind & Ice Calculations

Date: 4/23/2019
 Project Name: NEWTOWN EAST CENTRAL
 Project No.: CT5432
 Designed By: LBW Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$K_z = 1.041$ $z = 120$ (ft)
 $z_g = 1200$ (ft)
 $\alpha = 7.0$

$K_{zmin} \leq K_z \leq 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_c
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.2 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_c K_t / K_h)]^2$$

$$K_h = e^{(fz/H)}$$

$K_{zt} = \text{\#DIV/0!}$

$K_h = \text{\#DIV/0!}$

$K_c = 0.9$ (from Table 2-4)

$K_t = 0$ (from Table 2-5)

$f = 0$ (from Table 2-5)

$z = 120$

$z_s = 1500$ (Mean elevation of base of structure above se)

$H = 0$ (Ht. of the crest above surrounding terrain)

$K_{zt} = 1.00$ (from 2.6.6.2.1)

$K_e = 0.95$ (from 2.6.8)

(If Category 1 then $K_{zt} = 1.0$)

Category = 1

2.6.10 Design Ice Thickness

Max Ice Thickness =

$t_i = 1.00$ in

Importance Factor =

$I = 1.0$ (from Table 2-3)

$K_{iz} = 1.14$ (from Sec. 2.6.10)

$t_{iz} = t_i * I * K_{iz} * (K_{zt})^{0.35}$

$t_{iz} = 1.14$ in

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2.6.9 Gust Effect Factor

2.6.9.1 Self Supporting Lattice Structures

$G_h = 1.0$ Latticed Structures > 600 ft

$G_h = 0.85$ Latticed Structures 450 ft or less

$G_h = 0.85 + 0.15 [h/150 - 3.0]$ h= ht. of structure

h= 149 $G_h = 0.85$

2.6.9.2 Guyed Masts $G_h = 0.85$

2.6.9.3 Pole Structures $G_h = 1.1$

2.6.9 Appurtenances $G_h = 1.0$

2.6.9.4 Structures Supported on Other Structures

(Cantilevered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5))

$G_h = 1.35$ $G_h = 1.00$

2.6.11.2 Design Wind Force on Appurtenances

$F = q_z * G_h * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_s * K_e * K_d * V_{max}^2$

$q_z = 34.20$
 $q_z (ice) = 5.94$
 $q_z (30) = 2.14$

$K_z = 1.031$ (from 2.6.5.2)
 $K_{zt} = 1.0$ (from 2.6.6.2.1)
 $K_s = 1.0$ (from 2.6.7)
 $K_e = 0.95$ (from 2.6.8)
 $K_d = 0.95$ (from Table 2-2)
 $V_{max} = 120$ mph (Ultimate Wind Speed)
 $V_{max (ice)} = 50$ mph
 $V_{30} = 30$ mph

Table 2-2

Structure Type	Wind Direction Probability Factor, K_d
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95
Tubular pole structures supporting antennas enclosed within a cylindrical shroud	1.00

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Determine Ca:

Table 2-9

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Square/Rectangular HSS		$1.2 - 2.8(r_s) \geq 0.85$	$1.4 - 4.0(r_s) \geq 0.90$	$2.0 - 6.0(r_s) \geq 1.25$
Round	C < 39 (Subcritical)	0.7	0.8	1.2
	$39 \leq C \leq 78$ (Transitional)	$4.14/(C^{0.485})$	$3.66/(C^{0.415})$	$46.8/(C^{1.0})$
	C > 78 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
 (Aspect ratio is independent of the spacing between support points of a linear appurtenance.)

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = **1.14 in** Angle = **0 (deg)** Equivalent Angle = **180 (deg)**

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	190	42	12
800-10965 Antenna	78.7	20.0	6.9	10.93	3.94	1.26	477	95	30
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.43	1.20	45	11	3
B5/B12 4449 RRH (Shielded)	14.9	6.6	13.2	0.68	2.26	1.20	28	8	2
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.20	47	11	3
B2/B66A 8843 RRH (Shielded)	14.9	6.6	13.2	0.68	2.26	1.20	28	8	2
Surge Arrestor	24.0	9.7	9.7	1.62	2.47	0.70	39	9	2
2" Pipe	2.4	12.0		0.20	0.20	1.20	8	3	1
3" Pipe	3.5	12.0		0.29	0.29	1.20	12	4	1
2x2 Angle	2.0	12.0		0.17	0.17	2.00	12	5	1
3-1/2x3 Channel	3.5	12.0		0.29	0.29	2.00	20	7	1
6x3/8 Plate	6.0	12.0		0.50	0.50	2.00	35	10	2

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WIND LOADS

Angle = 30 (deg)

Ice Thickness = 1.14 in.

Equivalent Angle = 210 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	190	101	168
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	477	201	408
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	45	57	48
B5/B12 4449 RRH (Shield)	14.9	5.2	13.2	0.54	1.37	2.87	1.13	1.22	1.20	23	57	31
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	47	57	49
B2/B66A 8843 RRH (Shield)	14.9	5.5	13.2	0.56	1.37	2.73	1.13	1.21	1.20	24	57	32

WIND LOADS WITH ICE:

7770 Antenna	57.3	13.3	7.3	5.28	2.89	4.31	7.87	1.28	1.43	41	25	37
800-10965 Antenna	81.0	22.3	9.2	12.53	5.16	3.64	8.83	1.25	1.46	94	45	82
B5/B12 4449 RRH	17.2	12.7	15.5	1.51	1.85	1.36	1.11	1.20	1.20	11	13	11
B5/B12 4449 RRH (Shield)	17.2	6.3	15.5	0.76	1.85	2.71	1.11	1.21	1.20	5	13	7
B2/B66A 8843 RRH	17.2	13.2	15.5	1.57	1.85	1.30	1.11	1.20	1.20	11	13	12
B2/B66A 8843 RRH (Shield)	17.2	6.6	15.5	0.79	1.85	2.61	1.11	1.20	1.20	6	13	8

WIND LOADS AT 30 MPH:

7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	12	6	10
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	30	13	26
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	3	4	3
B5/B12 4449 RRH (Shield)	14.9	5.2	13.2	0.54	1.37	2.87	1.13	1.22	1.20	1	4	2
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	3	4	3
B2/B66A 8843 RRH (Shield)	14.9	5.5	13.2	0.56	1.37	2.73	1.13	1.21	1.20	1	4	2

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WIND LOADS

Angle = 60 (deg)

Ice Thickness = 1.14 in.

Equivalent Angle = 240 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	190	101	123
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	477	201	270
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	45	57	54
B5/B12 4449 RRH (Shield)	14.9	7.8	13.2	0.81	1.37	1.91	1.13	1.20	1.20	33	57	51
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	47	57	54
B2/B66A 8843 RRH (Shield)	14.9	8.2	13.2	0.85	1.37	1.82	1.13	1.20	1.20	35	57	51

WIND LOADS WITH ICE:

7770 Antenna	57.3	13.3	7.3	5.28	2.89	4.31	7.87	1.28	1.43	41	25	29
800-10965 Antenna	81.0	22.3	9.2	12.53	5.16	3.64	8.83	1.25	1.46	94	45	57
B5/B12 4449 RRH	17.2	12.7	15.5	1.51	1.85	1.36	1.11	1.20	1.20	11	13	13
B5/B12 4449 RRH (Shield)	17.2	9.5	15.5	1.13	1.85	1.81	1.11	1.20	1.20	8	13	12
B2/B66A 8843 RRH	17.2	13.2	15.5	1.57	1.85	1.30	1.11	1.20	1.20	11	13	13
B2/B66A 8843 RRH (Shield)	17.2	9.9	15.5	1.18	1.85	1.74	1.11	1.20	1.20	8	13	12

WIND LOADS AT 30 MPH:

7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	12	6	8
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	30	13	17
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	3	4	3
B5/B12 4449 RRH (Shield)	14.9	7.8	13.2	0.81	1.37	1.91	1.13	1.20	1.20	2	4	3
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	3	4	3
B2/B66A 8843 RRH (Shield)	14.9	8.2	13.2	0.85	1.37	1.82	1.13	1.20	1.20	2	4	3

Date: 4/23/2019
 Project Name: NEWTOWN EAST CENTRAL
 Project No.: CT5432
 Designed By: LBW Checked By: MSC



WIND LOADS

Angle = 90 (deg)

Ice Thickness = 1.14 in.

Equivalent Angle = 270 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	190	101	101
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	477	201	201
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	45	57	57
B5/B12 4449 RRH (Shielc	14.9	6.6	13.2	0.68	1.37	2.26	1.13	1.20	1.20	28	57	57
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	47	57	57
B2/B66A 8843 RRH (Shie	14.9	6.6	13.2	0.68	1.37	2.26	1.13	1.20	1.20	28	57	57

WIND LOADS WITH ICE:

7770 Antenna	57.3	13.3	7.3	5.28	2.89	4.31	7.87	1.28	1.43	41	25	25
800-10965 Antenna	81.0	22.3	9.2	12.53	5.16	3.64	8.83	1.25	1.46	94	45	45
B5/B12 4449 RRH	17.2	12.7	15.5	1.51	1.85	1.36	1.11	1.20	1.20	11	13	13
B5/B12 4449 RRH (Shielc	17.2	8.9	15.5	1.06	1.85	1.94	1.11	1.20	1.20	8	13	13
B2/B66A 8843 RRH	17.2	13.2	15.5	1.57	1.85	1.30	1.11	1.20	1.20	11	13	13
B2/B66A 8843 RRH (Shie	17.2	8.9	15.5	1.06	1.85	1.94	1.11	1.20	1.20	8	13	13

WIND LOADS AT 30 MPH:

7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	12	6	6
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	30	13	13
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	3	4	4
B5/B12 4449 RRH (Shielc	14.9	6.6	13.2	0.68	1.37	2.26	1.13	1.20	1.20	2	4	4
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	3	4	4
B2/B66A 8843 RRH (Shie	14.9	6.6	13.2	0.68	1.37	2.26	1.13	1.20	1.20	2	4	4

Date: 4/23/2019
 Project Name: NEWTOWN EAST CENTRAL
 Project No.: CT5432
 Designed By: LBW Checked By: MSC



WIND LOADS

Angle = 120 (deg)

Ice Thickness = 1.14 in.

Equivalent Angle = 300 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	190	101	123
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	477	201	270
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	45	57	54
B5/B12 4449 RRH (Shield)	14.9	7.8	13.2	0.81	1.37	1.91	1.13	1.20	1.20	33	57	51
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	47	57	54
B2/B66A 8843 RRH (Shie)	14.9	8.2	13.2	0.85	1.37	1.82	1.13	1.20	1.20	35	57	51

WIND LOADS WITH ICE:

7770 Antenna	57.3	13.3	7.3	5.28	2.89	4.31	7.87	1.28	1.43	41	25	29
800-10965 Antenna	81.0	22.3	9.2	12.53	5.16	3.64	8.83	1.25	1.46	94	45	57
B5/B12 4449 RRH	17.2	12.7	15.5	1.51	1.85	1.36	1.11	1.20	1.20	11	13	13
B5/B12 4449 RRH (Shield)	17.2	9.5	15.5	1.13	1.85	1.81	1.11	1.20	1.20	8	13	12
B2/B66A 8843 RRH	17.2	13.2	15.5	1.57	1.85	1.30	1.11	1.20	1.20	11	13	13
B2/B66A 8843 RRH (Shie)	17.2	9.9	15.5	1.18	1.85	1.74	1.11	1.20	1.20	8	13	12

WIND LOADS AT 30 MPH:

7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	12	6	8
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	30	13	17
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	3	4	3
B5/B12 4449 RRH (Shield)	14.9	7.8	13.2	0.81	1.37	1.91	1.13	1.20	1.20	2	4	3
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	3	4	3
B2/B66A 8843 RRH (Shie)	14.9	8.2	13.2	0.85	1.37	1.82	1.13	1.20	1.20	2	4	3

Date: 4/23/2019
 Project Name: NEWTOWN EAST CENTRAL
 Project No.: CT5432
 Designed By: LBW Checked By: MSC



WIND LOADS

Angle = 150 (deg)

Ice Thickness = 1.14 in.

Equivalent Angle = 330 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	190	101	168
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	477	201	408
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	45	57	48
B5/B12 4449 RRH (Shield)	14.9	5.2	13.2	0.54	1.37	2.87	1.13	1.22	1.20	23	57	31
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	47	57	49
B2/B66A 8843 RRH (Shield)	14.9	5.5	13.2	0.56	1.37	2.73	1.13	1.21	1.20	24	57	32

WIND LOADS WITH ICE:

7770 Antenna	57.3	13.3	7.3	5.28	2.89	4.31	7.87	1.28	1.43	41	25	37
800-10965 Antenna	81.0	22.3	9.2	12.53	5.16	3.64	8.83	1.25	1.46	94	45	82
B5/B12 4449 RRH	17.2	12.7	15.5	1.51	1.85	1.36	1.11	1.20	1.20	11	13	11
B5/B12 4449 RRH (Shield)	17.2	6.3	15.5	0.76	1.85	2.71	1.11	1.21	1.20	5	13	7
B2/B66A 8843 RRH	17.2	13.2	15.5	1.57	1.85	1.30	1.11	1.20	1.20	11	13	12
B2/B66A 8843 RRH (Shield)	17.2	6.6	15.5	0.79	1.85	2.61	1.11	1.20	1.20	6	13	8

WIND LOADS AT 30 MPH:

7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	12	6	10
800-10965 Antenna	78.7	20.0	6.9	10.93	3.77	3.94	11.41	1.26	1.55	30	13	26
B5/B12 4449 RRH	14.9	10.4	13.2	1.08	1.37	1.43	1.13	1.20	1.20	3	4	3
B5/B12 4449 RRH (Shield)	14.9	5.2	13.2	0.54	1.37	2.87	1.13	1.22	1.20	1	4	2
B2/B66A 8843 RRH	14.9	10.9	13.2	1.13	1.37	1.37	1.13	1.20	1.20	3	4	3
B2/B66A 8843 RRH (Shield)	14.9	5.5	13.2	0.56	1.37	2.73	1.13	1.21	1.20	1	4	2

Date: 4/22/2019

Project Name: NEWTOWN EAST CENTRAL

Project No.: CT5432

Designed By: LBW Checked By: MSC



HUDSON
Design Group LLC

ICE WEIGHT CALCULATIONS

Thickness of ice: 1.14 in.
Density of ice: 56 pcf

7770 Antenna

Weight of ice based on total radial SF area:
Height (in): 55.0
Width (in): 11.0
Depth (in): 5.0
Total weight of ice on object: 84 lbs
Weight of object: 35.0 lbs
Combined weight of ice and object: 119 lbs

B5/B12 4449 RRH

Weight of ice based on total radial SF area:
Height (in): 14.9
Width (in): 13.2
Depth (in): 10.4
Total weight of ice on object: 31 lbs
Weight of object: 73.0 lbs
Combined weight of ice and object: 104 lbs

Squid Surge Arrestor

Weight of ice based on total radial SF area:
Depth (in): 24.0
Diameter(in): 9.7
Total weight of ice on object: 30 lbs
Weight of object: 33 lbs
Combined weight of ice and object: 63 lbs

L 2x2 Angles

Weight of ice based on total radial SF area:
Height (in): 2
Width (in): 2
Per foot weight of ice on object: 6 plf

PL 6x3/8

Weight of ice based on total radial SF area:
Height (in): 6
Width (in): 0.375
Per foot weight of ice on object: 10 plf

800-10965 Antenna

Weight of ice based on total radial SF area:
Height (in): 78.7
Width (in): 20.0
Depth (in): 6.9
Total weight of ice on object: 204 lbs
Weight of object: 109.0 lbs
Combined weight of ice and object: 313 lbs

B2/B66A 8843 RRH

Weight of ice based on total radial SF area:
Height (in): 14.9
Width (in): 13.2
Depth (in): 10.9
Total weight of ice on object: 32 lbs
Weight of object: 72.0 lbs
Combined weight of ice and object: 104 lbs

2" pipe

Per foot weight of ice:
diameter (in): 2.38
Per foot weight of ice on object: 5 plf

3" Pipe

Per foot weight of ice:
diameter (in): 3.5
Per foot weight of ice on object: 6 plf

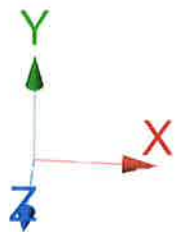
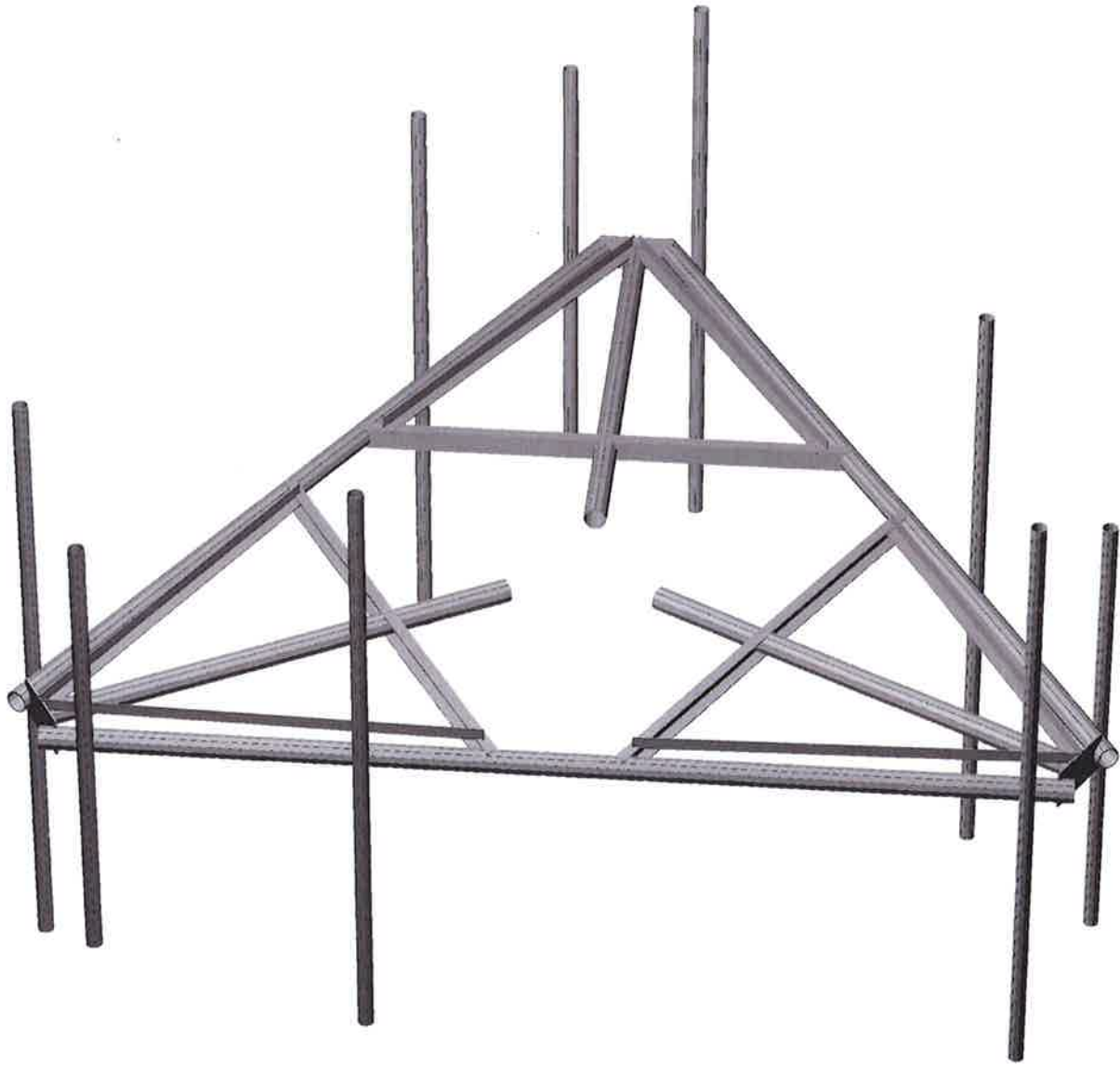
C 3-1/2x2

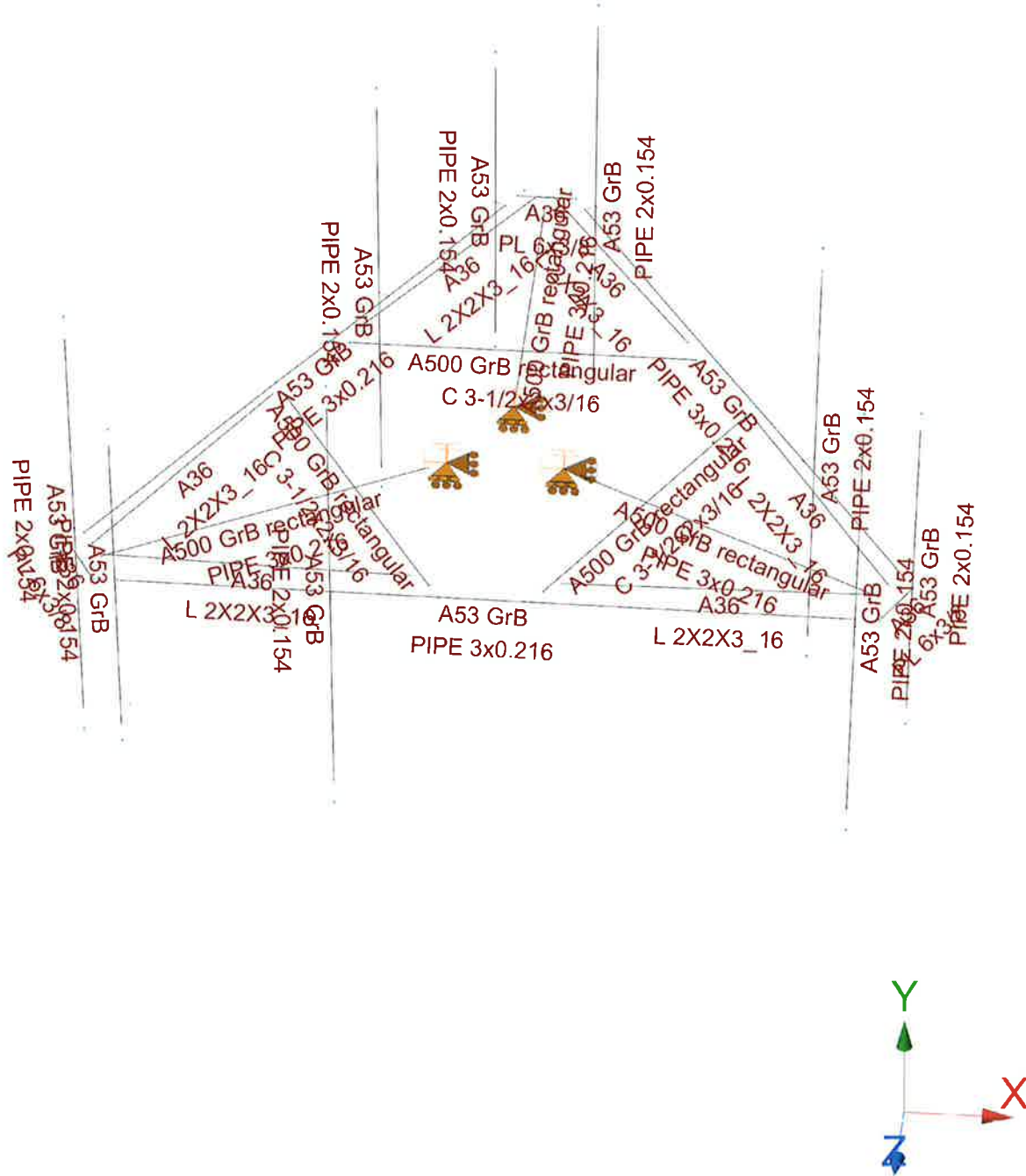
Weight of ice based on total radial SF area:
Height (in): 3.5
Width (in): 2
Per foot weight of ice on object: 7 plf







HUDSON
Design Group LLC

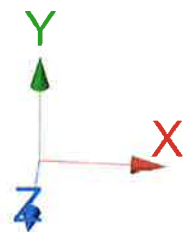
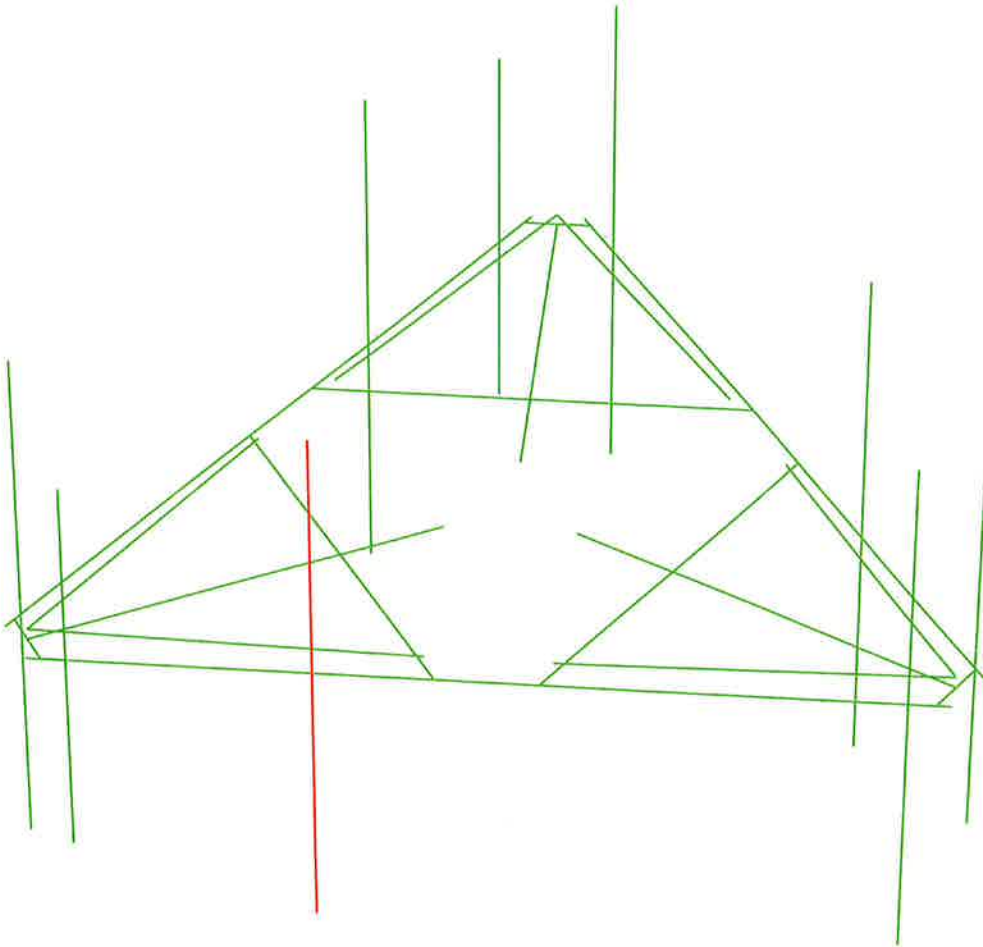
**Mount Calculations
(Existing Conditions)**

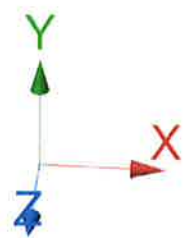
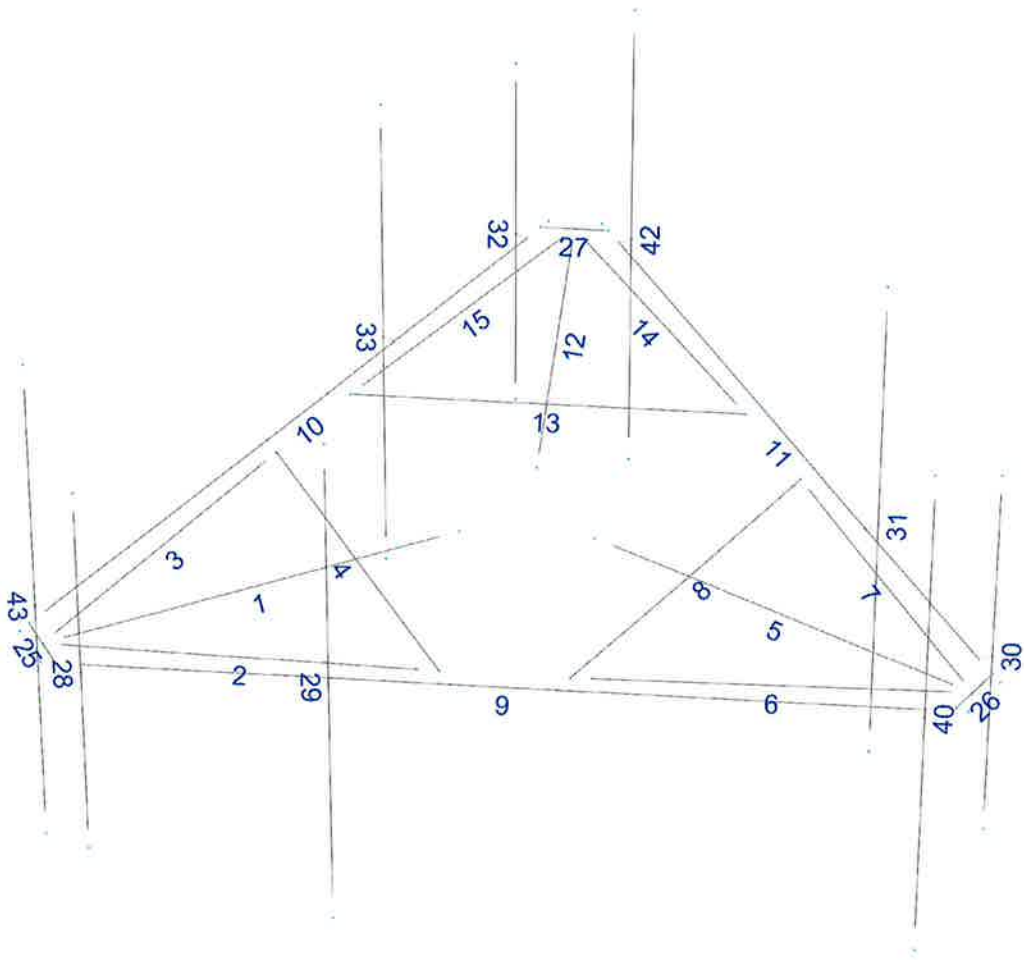




Design status

-  Not designed
-  Error on design
-  Design O.K.
-  With warnings





Current Date: 4/22/2019 2:48 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT5432\LTE 2C-3C-4C\CT5432 (LTE 2C-3C-4C).etx

Load data

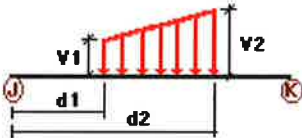
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
DL	Dead Load	No	DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
Wi0	Ice Wind Load 0/60/120 deg	No	WIND
Wi30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load End of Mount	No	LL
LLa1	250 lb Live Load Antenna 1	No	LL
LLa2	250 lb Live Load Antenna 2	No	LL
LLa3	250 lb Live Load Antenna 3	No	LL

Distributed force on members

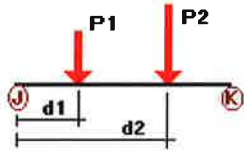


Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	2	y	-0.01	0.00	0.00	No	0.00	No
	3	y	-0.01	0.00	0.00	No	0.00	No
	4	y	-0.01	0.00	0.00	No	0.00	No
	6	y	-0.01	0.00	0.00	No	0.00	No
	7	y	-0.01	0.00	0.00	No	0.00	No
	8	y	-0.01	0.00	0.00	No	0.00	No
	13	y	-0.01	0.00	0.00	No	0.00	No
	14	y	-0.01	0.00	0.00	No	0.00	No
W0	15	y	-0.01	0.00	0.00	No	0.00	No
	1	z	-0.012	0.00	0.00	No	0.00	No
	2	z	-0.011	0.00	0.00	No	0.00	No
	3	z	-0.011	0.00	0.00	No	0.00	No
	4	z	-0.02	0.00	0.00	No	0.00	No
	5	z	-0.012	0.00	0.00	No	0.00	No
	6	z	-0.011	0.00	0.00	No	0.00	No

	7	z	-0.011	0.00	0.00	No	0.00	No
	8	z	-0.02	0.00	0.00	No	0.00	No
	9	z	-0.012	0.00	0.00	No	0.00	No
	10	z	-0.012	0.00	0.00	No	0.00	No
	11	z	-0.012	0.00	0.00	No	0.00	No
	12	z	-0.012	0.00	0.00	No	0.00	No
	13	z	-0.02	0.00	0.00	No	0.00	No
	14	z	-0.011	0.00	0.00	No	0.00	No
	15	z	-0.011	0.00	0.00	No	0.00	No
	25	z	-0.034	0.00	0.00	No	0.00	No
	26	z	-0.034	0.00	0.00	No	0.00	No
	27	z	-0.034	0.00	0.00	No	0.00	No
W30	1	x	-0.012	0.00	0.00	No	0.00	No
	2	x	-0.011	0.00	0.00	No	0.00	No
	3	x	-0.011	0.00	0.00	No	0.00	No
	4	x	-0.02	0.00	0.00	No	0.00	No
	5	x	-0.012	0.00	0.00	No	0.00	No
	6	x	-0.011	0.00	0.00	No	0.00	No
	7	x	-0.011	0.00	0.00	No	0.00	No
	8	x	-0.02	0.00	0.00	No	0.00	No
	9	x	-0.012	0.00	0.00	No	0.00	No
	10	x	-0.012	0.00	0.00	No	0.00	No
	11	x	-0.012	0.00	0.00	No	0.00	No
	12	x	-0.012	0.00	0.00	No	0.00	No
	13	x	-0.02	0.00	0.00	No	0.00	No
	14	x	-0.011	0.00	0.00	No	0.00	No
	15	x	-0.011	0.00	0.00	No	0.00	No
	25	x	-0.034	0.00	0.00	No	0.00	No
	26	x	-0.034	0.00	0.00	No	0.00	No
	27	x	-0.034	0.00	0.00	No	0.00	No
	28	x	-0.008	0.00	0.00	No	0.00	No
	29	x	-0.008	0.00	0.00	No	0.00	No
	30	x	-0.008	0.00	0.00	No	0.00	No
	31	x	-0.008	0.00	0.00	No	0.00	No
	32	x	-0.008	0.00	0.00	No	0.00	No
	33	x	-0.008	0.00	0.00	No	0.00	No
	40	x	-0.008	0.00	0.00	No	0.00	No
	42	x	-0.008	0.00	0.00	No	0.00	No
	43	x	-0.008	0.00	0.00	No	0.00	No
Di	1	y	-0.006	0.00	0.00	No	0.00	No
	2	y	-0.005	0.00	0.00	No	0.00	No
	3	y	-0.005	0.00	0.00	No	0.00	No
	4	y	-0.007	0.00	0.00	No	0.00	No
	5	y	-0.006	0.00	0.00	No	0.00	No
	6	y	-0.005	0.00	0.00	No	0.00	No
	7	y	-0.005	0.00	0.00	No	0.00	No
	8	y	-0.007	0.00	0.00	No	0.00	No
	9	y	-0.006	0.00	0.00	No	0.00	No
	10	y	-0.006	0.00	0.00	No	0.00	No
	11	y	-0.006	0.00	0.00	No	0.00	No
	12	y	-0.006	0.00	0.00	No	0.00	No
	13	y	-0.007	0.00	0.00	No	0.00	No
	14	y	-0.005	0.00	0.00	No	0.00	No
	15	y	-0.005	0.00	0.00	No	0.00	No
	25	y	-0.01	0.00	0.00	No	0.00	No
	26	y	-0.01	0.00	0.00	No	0.00	No
	27	y	-0.01	0.00	0.00	No	0.00	No
	28	y	-0.005	0.00	0.00	No	0.00	No
	29	y	-0.005	0.00	0.00	No	0.00	No
	30	y	-0.005	0.00	0.00	No	0.00	No

31	y	-0.005	0.00	0.00	No	0.00	No
32	y	-0.005	0.00	0.00	No	0.00	No
33	y	-0.005	0.00	0.00	No	0.00	No
40	y	-0.005	0.00	0.00	No	0.00	No
42	y	-0.005	0.00	0.00	No	0.00	No
43	y	-0.005	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%	
DL	28	y	-0.018	0.50	No	
		y	-0.018	4.50	No	
	29	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
		y	-0.145	1.50	No	
	30	y	-0.018	0.50	No	
		y	-0.018	4.50	No	
	31	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
		y	-0.145	1.50	No	
	32	y	-0.018	0.50	No	
		y	-0.018	4.50	No	
	33	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
		y	-0.145	1.50	No	
	40	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
	42	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
	43	y	-0.055	0.50	No	
		y	-0.055	7.50	No	
	W0	28	z	-0.095	0.50	No
			z	-0.095	4.50	No
		29	z	-0.237	0.50	No
z			-0.237	7.50	No	
z			-0.056	1.50	No	
30		z	-0.062	0.50	No	
		z	-0.062	4.50	No	
31		z	-0.134	0.50	No	
		z	-0.134	7.50	No	
		z	-0.051	1.50	No	
32		z	-0.062	0.50	No	
		z	-0.062	4.50	No	
33	z	-0.134	0.50	No		
	z	-0.134	7.50	No		
	z	-0.051	1.50	No		
40	z	-0.237	0.50	No		
	z	-0.237	7.50	No		
42	z	-0.134	0.50	No		
	z	-0.134	7.50	No		

		z	-0.134	7.50	No
	43	z	-0.134	0.50	No
		z	-0.134	7.50	No
W30	28	x	-0.051	0.50	No
		x	-0.051	4.50	No
	29	x	-0.10	0.50	No
		x	-0.10	7.50	No
		x	-0.056	1.50	No
	30	x	-0.084	0.50	No
		x	-0.084	4.50	No
	31	x	-0.203	0.50	No
		x	-0.203	7.50	No
		x	-0.032	1.50	No
	32	x	-0.084	0.50	No
		x	-0.084	4.50	No
	33	x	-0.203	0.50	No
		x	-0.203	7.50	No
		x	-0.032	1.50	No
	40	x	-0.10	0.50	No
		x	-0.10	7.50	No
	42	x	-0.203	0.50	No
		x	-0.203	7.50	No
	43	x	-0.203	0.50	No
		x	-0.203	7.50	No
Di	28	y	-0.042	0.50	No
		y	-0.042	4.50	No
	29	y	-0.101	0.50	No
		y	-0.101	7.50	No
		y	-0.062	1.50	No
	30	y	-0.042	0.50	No
		y	-0.042	4.50	No
	31	y	-0.101	0.50	No
		y	-0.101	7.50	No
		y	-0.062	1.50	No
	32	y	-0.042	0.50	No
		y	-0.042	4.50	No
	33	y	-0.101	0.50	No
		y	-0.101	7.50	No
		y	-0.062	1.50	No
	40	y	-0.101	0.50	No
		y	-0.101	7.50	No
	42	y	-0.101	0.50	No
		y	-0.101	7.50	No
	43	y	-0.101	0.50	No
		y	-0.101	7.50	No
Wi0	28	z	-0.021	0.50	No
		z	-0.021	4.50	No
	29	z	-0.047	0.50	No
		z	-0.047	7.50	No
		z	-0.016	1.50	No
	30	z	-0.015	0.50	No
		z	-0.015	4.50	No
	31	z	-0.029	0.50	No
		z	-0.029	7.50	No
		z	-0.012	1.50	No
	32	z	-0.015	0.50	No
		z	-0.015	4.50	No
	33	z	-0.029	0.50	No
		z	-0.029	7.50	No
		z	-0.012	1.50	No

	40	z	-0.047	0.50	No
		z	-0.047	7.50	No
	42	z	-0.029	0.50	No
		z	-0.029	7.50	No
	43	z	-0.029	0.50	No
		z	-0.029	7.50	No
W130	28	x	-0.013	0.50	No
		x	-0.013	4.50	No
	29	x	-0.023	0.50	No
		x	-0.023	7.50	No
		x	-0.013	1.50	No
	30	x	-0.019	0.50	No
		x	-0.019	4.50	No
	31	x	-0.041	0.50	No
		x	-0.041	7.50	No
		x	-0.007	1.50	No
	32	x	-0.019	0.50	No
		x	-0.019	4.50	No
	33	x	-0.041	0.50	No
		x	-0.041	7.50	No
		x	-0.007	1.50	No
	40	x	-0.023	0.50	No
		x	-0.023	7.50	No
	42	x	-0.041	0.50	No
		x	-0.041	7.50	No
	43	x	-0.041	0.50	No
		x	-0.041	7.50	No
WLO	28	z	-0.006	0.50	No
		z	-0.006	4.50	No
	29	z	-0.015	0.50	No
		z	-0.015	7.50	No
		z	-0.004	1.50	No
	30	z	-0.004	0.50	No
		z	-0.004	4.50	No
	31	z	-0.009	0.50	No
		z	-0.009	7.50	No
		z	-0.003	1.50	No
	32	z	-0.004	0.50	No
		z	-0.004	4.50	No
	33	z	-0.009	0.50	No
		z	-0.009	7.50	No
		z	-0.003	1.50	No
	40	z	-0.015	0.50	No
		z	-0.015	7.50	No
	42	z	-0.009	0.50	No
		z	-0.009	7.50	No
	43	z	-0.009	0.50	No
		z	-0.009	7.50	No
WL30	28	x	-0.004	0.50	No
		x	-0.004	4.50	No
	29	x	-0.007	0.50	No
		x	-0.007	7.50	No
		x	-0.004	1.50	No
	30	x	-0.006	0.50	No
		x	-0.006	4.50	No
	31	x	-0.013	0.50	No
		x	-0.013	7.50	No
		x	-0.002	1.50	No
	32	x	-0.006	0.50	No
		x	-0.006	4.50	No

	33	x	-0.013	0.50	No
		x	-0.013	7.50	No
		x	-0.002	1.50	No
	40	x	-0.007	0.50	No
		x	-0.007	7.50	No
	42	x	-0.013	0.50	No
		x	-0.013	7.50	No
	43	x	-0.013	0.50	No
		x	-0.013	7.50	No
LL1	9	y	-0.25	6.29	No
LL2	9	y	-0.25	0.00	No
LLa1	40	y	-0.25	4.00	No
LLa2	29	y	-0.25	3.00	No
LLa3	28	y	-0.25	3.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00
LLa1	250 lb Live Load Antenna 1	No	0.00	0.00	0.00
LLa2	250 lb Live Load Antenna 2	No	0.00	0.00	0.00
LLa3	250 lb Live Load Antenna 3	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
W0	0.00	0.00	0.00
W30	0.00	0.00	0.00
Di	0.00	0.00	0.00
Wi0	0.00	0.00	0.00
Wi30	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
LL1	0.00	0.00	0.00
LL2	0.00	0.00	0.00
LLa1	0.00	0.00	0.00
LLa2	0.00	0.00	0.00
LLa3	0.00	0.00	0.00

Current Date: 4/22/2019 2:49 PM

Units system: English

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Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2DL+W0
 LC2=1.2DL+W30
 LC3=1.2DL-W0
 LC4=1.2DL-W30
 LC5=0.9DL+W0
 LC6=0.9DL+W30
 LC7=0.9DL-W0
 LC8=0.9DL-W30
 LC9=1.2DL+Di+W0
 LC10=1.2DL+Di+W30
 LC11=1.2DL+Di-W0
 LC12=1.2DL+Di-W30
 LC13=1.2DL
 LC15=1.2DL+1.5LL1
 LC16=1.2DL+1.5LL2
 LC17=1.2DL+W0+1.5LLa1
 LC18=1.2DL+W30+1.5LLa1
 LC19=1.2DL-W0+1.5LLa1
 LC20=1.2DL-W30+1.5LLa1
 LC21=1.2DL+W0+1.5LLa2
 LC22=1.2DL+W30+1.5LLa2
 LC23=1.2DL-W0+1.5LLa2
 LC24=1.2DL-W30+1.5LLa2
 LC25=1.2DL+W0+1.5LLa3
 LC26=1.2DL+W30+1.5LLa3
 LC27=1.2DL-W0+1.5LLa3
 LC28=1.2DL-W30+1.5LLa3

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
C 3-1/2x2x3/16		4	LC11 at 50.00%	0.53	OK	Eq. H1-1b
		8	LC11 at 50.00%	0.51	OK	Eq. H1-1b
		13	LC9 at 50.00%	0.51	OK	Eq. H1-1b
L 2X2X3_16		2	LC9 at 0.00%	0.43	OK	Eq. H2-1
		3	LC12 at 0.00%	0.43	OK	Eq. H2-1
		6	LC9 at 0.00%	0.43	OK	Eq. H2-1
		7	LC8 at 100.00%	0.45	OK	Eq. H2-1
		14	LC10 at 100.00%	0.43	OK	Eq. H2-1
		15	LC12 at 100.00%	0.42	OK	Eq. H2-1
PIPE 2x0.154		28	LC3 at 46.88%	0.25	OK	Eq. H1-1b
		29	LC1 at 46.88%	1.03	N.G.	Eq. H1-1b
		30	LC4 at 46.88%	0.26	OK	Eq. H1-1b
		31	LC4 at 46.88%	0.91	OK	Eq. H1-1b
		32	LC2 at 46.88%	0.26	OK	Eq. H1-1b
		33	LC2 at 46.88%	0.91	OK	Eq. H1-1b
		40	LC1 at 50.00%	0.94	OK	Eq. H1-1b
		42	LC2 at 50.00%	0.62	OK	Eq. H1-1b
		43	LC4 at 50.00%	0.62	OK	Eq. H1-1b

PIPE 3x0.216	1	LC11 at 100.00%	0.85	OK	Eq. H1-1b
	5	LC11 at 100.00%	0.85	OK	Eq. H1-1b
	9	LC11 at 55.47%	0.51	OK	Eq. H1-1b
	10	LC12 at 44.53%	0.50	OK	Eq. H1-1b
	11	LC12 at 44.53%	0.51	OK	Eq. H1-1b
	12	LC12 at 0.00%	0.86	OK	Eq. H1-1b
<hr/>					
PL 6x3/8	25	LC2 at 0.00%	0.32	OK	Eq. H1-1b
	26	LC4 at 50.00%	0.31	OK	Eq. H1-1b
	27	LC1 at 0.00%	0.28	OK	Eq. H1-1b

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
2	-0.7253	0.00	4.0896	0
3	-6.0833	0.00	4.0896	0
4	-6.292	0.00	4.0896	0
5	-6.3333	0.00	3.6566	0
6	-6.5833	0.00	3.2236	0
7	-3.7376	0.00	-1.128	0
8	-3.9043	0.00	-1.4166	0
9	-0.892	0.00	3.8009	0
10	-6.6877	0.00	3.4042	0
11	-3.179	0.00	-2.6729	0
12	-2.8457	0.00	-2.6729	0
13	-0.50	0.00	-7.3131	0
14	-0.3957	0.00	-7.4938	0
17	0.7253	0.00	4.0896	0
18	6.0833	0.00	4.0896	0
19	6.292	0.00	4.0896	0
20	6.3333	0.00	3.6566	0
21	6.5833	0.00	3.2236	0
22	3.7376	0.00	-1.128	0
23	3.9043	0.00	-1.4166	0
24	0.892	0.00	3.8009	0

25	6.6877	0.00	3.4042	0
26	3.179	0.00	-2.6729	0
27	2.8457	0.00	-2.6729	0
28	0.50	0.00	-7.3131	0
29	0.3957	0.00	-7.4938	0
32	0.00	0.00	-7.3131	0
69	0.9427	0.00	0.5443	0
70	0.00	0.00	-1.0885	0
71	-0.9427	0.00	0.5443	0
76	-5.709	-3.00	4.2896	0
77	-2.355	-4.00	4.2896	0
78	-5.709	3.00	4.2896	0
79	-2.355	4.00	4.2896	0
84	-0.8604	-3.00	-7.0889	0
85	-2.5374	-4.00	-4.1843	0
86	-0.8604	3.00	-7.0889	0
87	-2.5374	4.00	-4.1843	0
92	6.5694	-3.00	2.7994	0
93	4.8924	-4.00	-0.1053	0
94	6.5694	3.00	2.7994	0
95	4.8924	4.00	-0.1053	0
98	5.712	-4.00	4.2896	0
99	5.712	4.00	4.2896	0
102	-6.5709	-4.00	2.802	0
103	-6.5709	4.00	2.802	0
106	0.8589	-4.00	-7.0915	0
107	0.8589	4.00	-7.0915	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
69	1	1	1	1	1	1
70	1	1	1	1	1	1
71	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	5	71		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00
2	5	9		L 2X2X3_16	A36	0.00	0.00	0.00
3	5	7		L 2X2X3_16	A36	0.00	0.00	0.00
4	8	2		C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
5	20	69		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00
6	20	24		L 2X2X3_16	A36	0.00	0.00	0.00
7	20	22		L 2X2X3_16	A36	0.00	0.00	0.00
8	23	17		C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
9	4	19		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
10	10	14		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
11	29	25		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
12	70	32		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00

13	11	26	C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
14	27	32	L 2X2X3_16	A36	0.00	0.00	0.00
15	12	32	L 2X2X3_16	A36	0.00	0.00	0.00
25	6	3	PL 6x3/8	A36	0.00	0.00	0.00
26	18	21	PL 6x3/8	A36	0.00	0.00	0.00
27	28	13	PL 6x3/8	A36	0.00	0.00	0.00
28	78	76	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
29	79	77	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
30	94	92	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
31	95	93	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
32	86	84	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
33	87	85	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
40	99	98	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
42	107	106	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	103	102	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
2	270.00	0	0.00	0.00	0.00
7	270.00	0	0.00	0.00	0.00
8	180.00	0	0.00	0.00	0.00
13	180.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
28	0.00	2	0.7071	0.00	-0.7071
29	0.00	2	0.7071	0.00	-0.7071
30	0.00	2	0.7071	0.00	-0.7071
31	0.00	2	0.7071	0.00	-0.7071
32	0.00	2	0.7071	0.00	-0.7071
33	0.00	2	0.7071	0.00	-0.7071
40	0.00	2	0.7071	0.00	-0.7071

Rigid end offsets

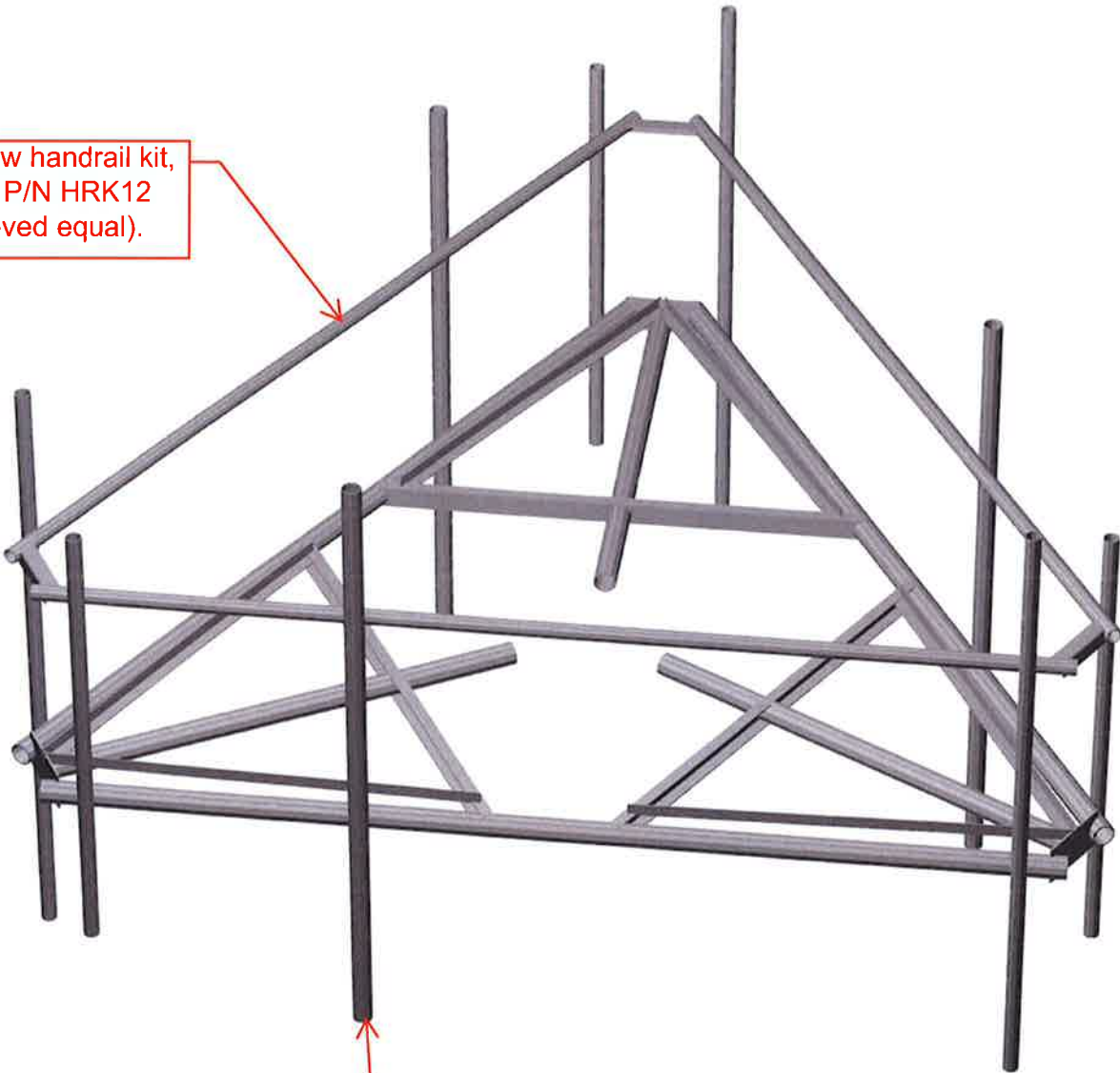
Member	DJX [in]	DJY [in]	DJZ [in]	DKX [in]	DKY [in]	DKZ [in]
2	0.00	2.00	0.00	0.00	2.00	0.00
3	0.00	2.00	0.00	0.00	2.00	0.00
6	0.00	2.00	0.00	0.00	2.00	0.00
7	0.00	2.00	0.00	0.00	2.00	0.00
14	0.00	2.00	0.00	0.00	2.00	0.00
15	0.00	2.00	0.00	0.00	2.00	0.00



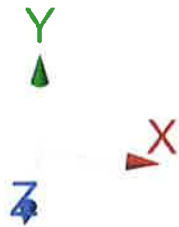
HUDSON
Design Group LLC

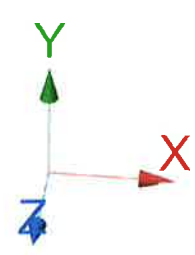
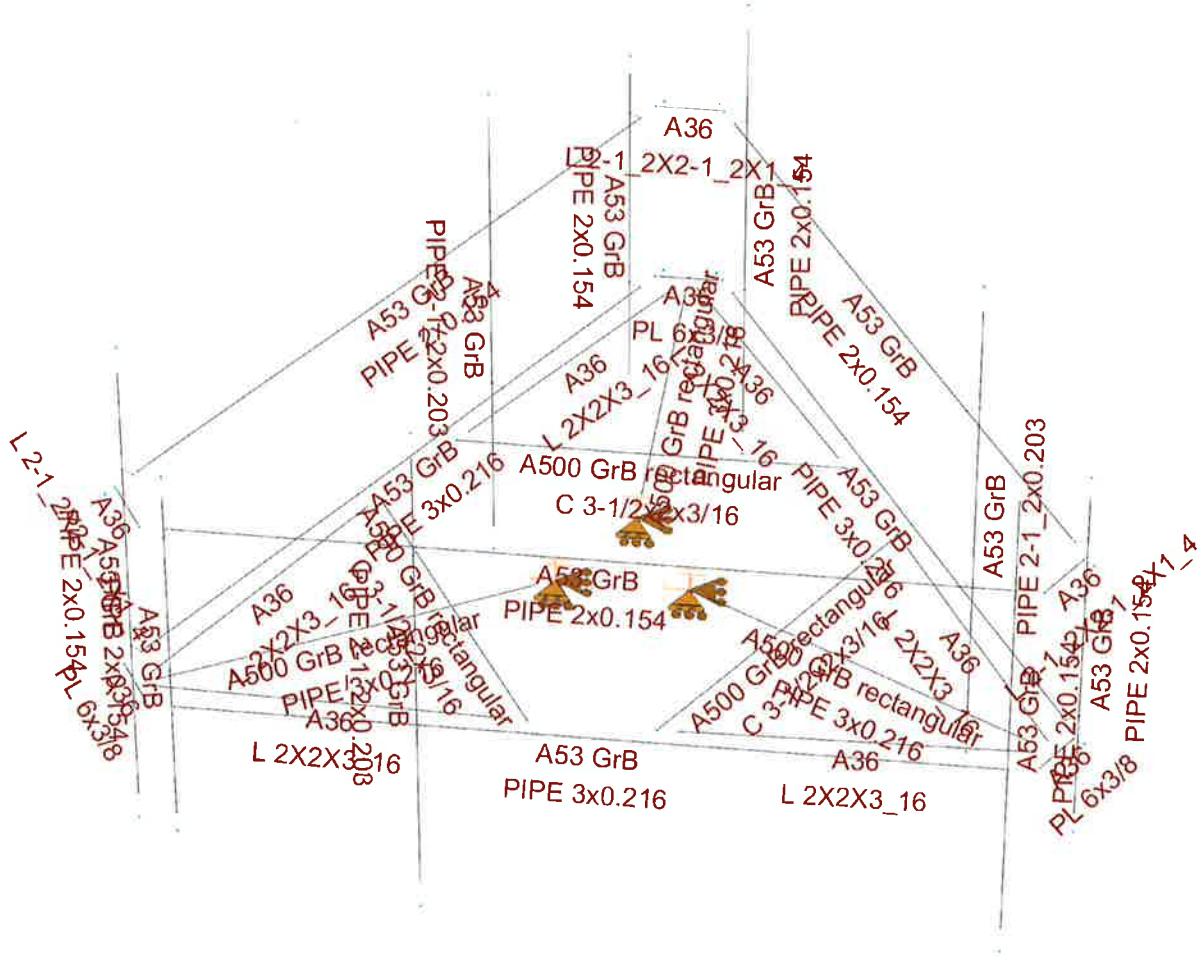
**Mount Calculations
(Modified Conditions)**

Install new handrail kit,
SitePro1 P/N HRK12
(or approved equal).







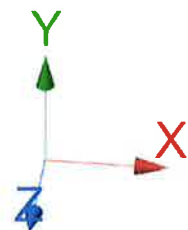
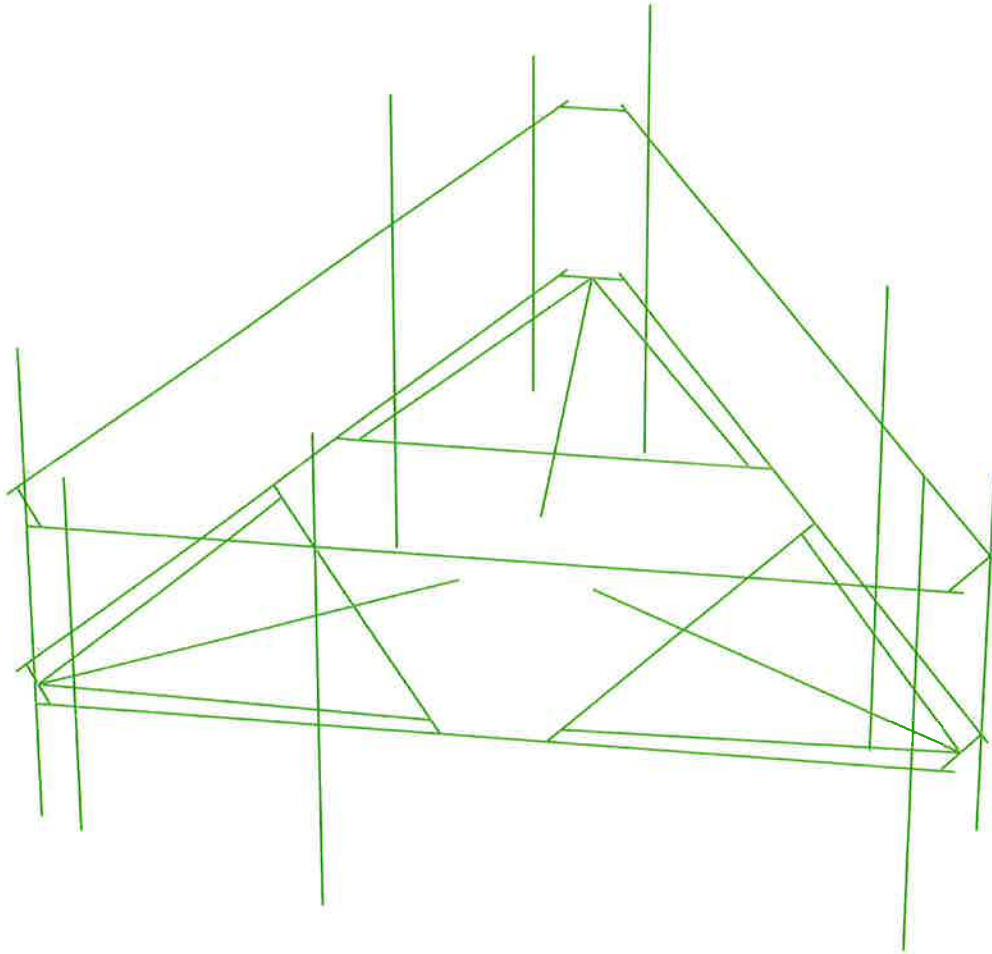
Remove existing pipe mast and install
new 2-1/2" std. (2.88" O.D.) pipe mast
behind new 800-10965 antennas
secured to existing mount (typ. of 1
per sector, total of 3).

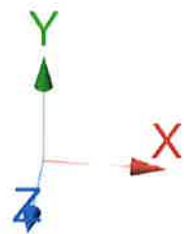
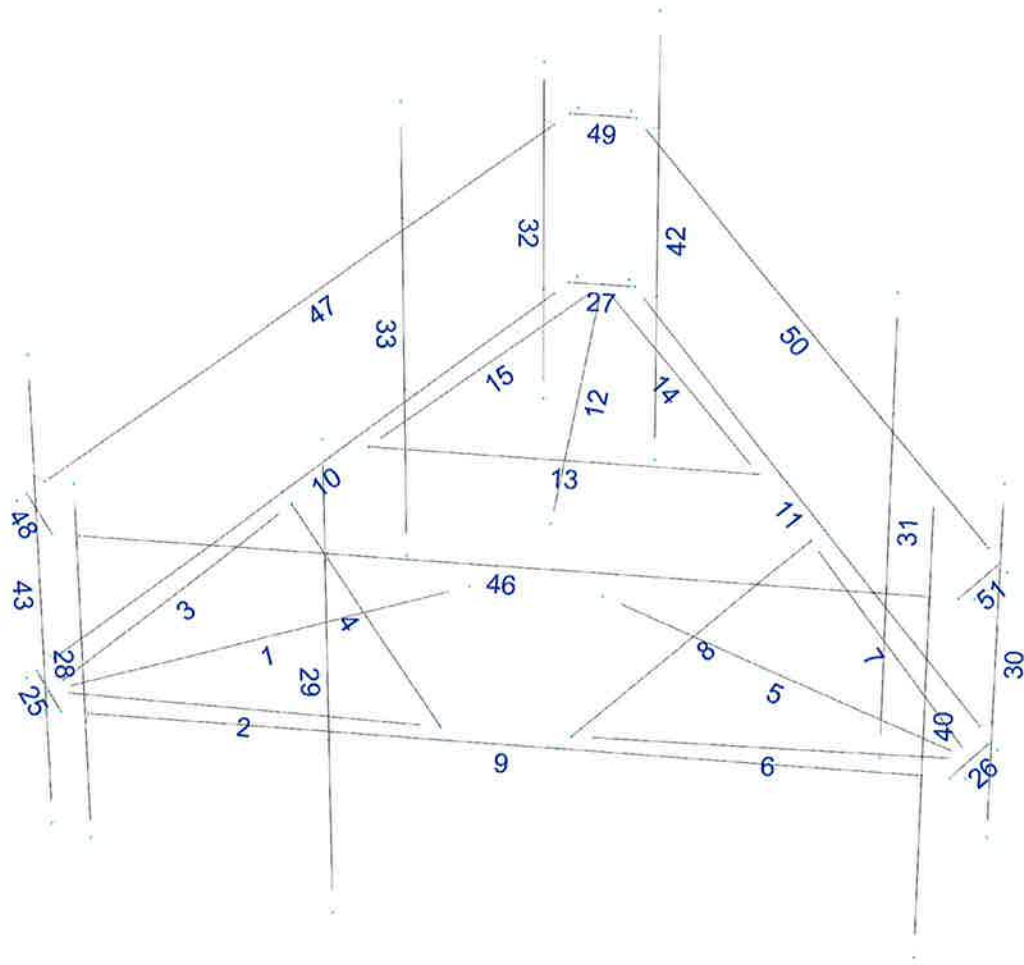




Design status

-  Not designed
-  Error on design
-  Design O.K.
-  With warnings





Current Date: 4/22/2019 2:50 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT5432\LTE 2C-3C-4C\CT5432 (LTE 2C-3C-4C)(MODS).etx

Load data

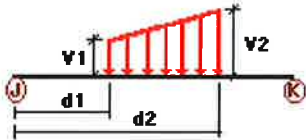
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
DL	Dead Load	No	DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
Wi0	Ice Wind Load 0/60/120 deg	No	WIND
Wi30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load End of Mount	No	LL
LLa1	250 lb Live Load Antenna 1	No	LL
LLa2	250 lb Live Load Antenna 2	No	LL
LLa3	250 lb Live Load Antenna 3	No	LL

Distributed force on members

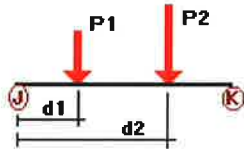


Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	2	y	-0.01	0.00	0.00	No	0.00	No
	3	y	-0.01	0.00	0.00	No	0.00	No
	4	y	-0.01	0.00	0.00	No	0.00	No
	6	y	-0.01	0.00	0.00	No	0.00	No
	7	y	-0.01	0.00	0.00	No	0.00	No
	8	y	-0.01	0.00	0.00	No	0.00	No
	13	y	-0.01	0.00	0.00	No	0.00	No
	14	y	-0.01	0.00	0.00	No	0.00	No
W0	1	z	-0.012	0.00	0.00	No	0.00	No
	2	z	-0.011	0.00	0.00	No	0.00	No
	3	z	-0.011	0.00	0.00	No	0.00	No
	4	z	-0.02	0.00	0.00	No	0.00	No
	5	z	-0.012	0.00	0.00	No	0.00	No
	6	z	-0.011	0.00	0.00	No	0.00	No

	7	z	-0.011	0.00	0.00	No	0.00	No
	8	z	-0.02	0.00	0.00	No	0.00	No
	9	z	-0.012	0.00	0.00	No	0.00	No
	10	z	-0.012	0.00	0.00	No	0.00	No
	11	z	-0.012	0.00	0.00	No	0.00	No
	12	z	-0.012	0.00	0.00	No	0.00	No
	13	z	-0.02	0.00	0.00	No	0.00	No
	14	z	-0.011	0.00	0.00	No	0.00	No
	15	z	-0.011	0.00	0.00	No	0.00	No
	25	z	-0.034	0.00	0.00	No	0.00	No
	26	z	-0.034	0.00	0.00	No	0.00	No
	27	z	-0.034	0.00	0.00	No	0.00	No
	46	z	-0.012	0.00	0.00	No	0.00	No
	47	z	-0.012	0.00	0.00	No	0.00	No
	48	z	-0.034	0.00	0.00	No	0.00	No
	49	z	-0.034	0.00	0.00	No	0.00	No
	50	z	-0.012	0.00	0.00	No	0.00	No
	51	z	-0.034	0.00	0.00	No	0.00	No
W30	1	x	-0.012	0.00	0.00	No	0.00	No
	2	x	-0.011	0.00	0.00	No	0.00	No
	3	x	-0.011	0.00	0.00	No	0.00	No
	4	x	-0.02	0.00	0.00	No	0.00	No
	5	x	-0.012	0.00	0.00	No	0.00	No
	6	x	-0.011	0.00	0.00	No	0.00	No
	7	x	-0.011	0.00	0.00	No	0.00	No
	8	x	-0.02	0.00	0.00	No	0.00	No
	9	x	-0.012	0.00	0.00	No	0.00	No
	10	x	-0.012	0.00	0.00	No	0.00	No
	11	x	-0.012	0.00	0.00	No	0.00	No
	12	x	-0.012	0.00	0.00	No	0.00	No
	13	x	-0.02	0.00	0.00	No	0.00	No
	14	x	-0.011	0.00	0.00	No	0.00	No
	15	x	-0.011	0.00	0.00	No	0.00	No
	25	x	-0.034	0.00	0.00	No	0.00	No
	26	x	-0.034	0.00	0.00	No	0.00	No
	27	x	-0.034	0.00	0.00	No	0.00	No
	28	x	-0.008	0.00	0.00	No	0.00	No
	29	x	-0.008	0.00	0.00	No	0.00	No
	30	x	-0.008	0.00	0.00	No	0.00	No
	31	x	-0.008	0.00	0.00	No	0.00	No
	32	x	-0.008	0.00	0.00	No	0.00	No
	33	x	-0.008	0.00	0.00	No	0.00	No
	40	x	-0.008	0.00	0.00	No	0.00	No
	42	x	-0.008	0.00	0.00	No	0.00	No
	43	x	-0.008	0.00	0.00	No	0.00	No
	46	x	-0.012	0.00	0.00	No	0.00	No
	47	x	-0.012	0.00	0.00	No	0.00	No
	48	x	-0.034	0.00	0.00	No	0.00	No
	49	x	-0.034	0.00	0.00	No	0.00	No
	50	x	-0.012	0.00	0.00	No	0.00	No
	51	x	-0.034	0.00	0.00	No	0.00	No
Di	1	y	-0.006	0.00	0.00	No	0.00	No
	2	y	-0.005	0.00	0.00	No	0.00	No
	3	y	-0.005	0.00	0.00	No	0.00	No
	4	y	-0.007	0.00	0.00	No	0.00	No
	5	y	-0.006	0.00	0.00	No	0.00	No
	6	y	-0.005	0.00	0.00	No	0.00	No
	7	y	-0.005	0.00	0.00	No	0.00	No
	8	y	-0.007	0.00	0.00	No	0.00	No
	9	y	-0.006	0.00	0.00	No	0.00	No

10	y	-0.006	0.00	0.00	No	0.00	No
11	y	-0.006	0.00	0.00	No	0.00	No
12	y	-0.006	0.00	0.00	No	0.00	No
13	y	-0.007	0.00	0.00	No	0.00	No
14	y	-0.005	0.00	0.00	No	0.00	No
15	y	-0.005	0.00	0.00	No	0.00	No
25	y	-0.01	0.00	0.00	No	0.00	No
26	y	-0.01	0.00	0.00	No	0.00	No
27	y	-0.01	0.00	0.00	No	0.00	No
28	y	-0.005	0.00	0.00	No	0.00	No
29	y	-0.005	0.00	0.00	No	0.00	No
30	y	-0.005	0.00	0.00	No	0.00	No
31	y	-0.005	0.00	0.00	No	0.00	No
32	y	-0.005	0.00	0.00	No	0.00	No
33	y	-0.005	0.00	0.00	No	0.00	No
40	y	-0.005	0.00	0.00	No	0.00	No
42	y	-0.005	0.00	0.00	No	0.00	No
43	y	-0.005	0.00	0.00	No	0.00	No
46	y	-0.006	0.00	0.00	No	0.00	No
47	y	-0.006	0.00	0.00	No	0.00	No
48	y	-0.01	0.00	0.00	No	0.00	No
49	y	-0.01	0.00	0.00	No	0.00	No
50	y	-0.006	0.00	0.00	No	0.00	No
51	y	-0.01	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
DL	28	y	-0.018	0.50	No
		y	-0.018	4.50	No
	29	y	-0.055	0.50	No
		y	-0.055	7.50	No
		y	-0.145	1.50	No
	30	y	-0.018	0.50	No
		y	-0.018	4.50	No
	31	y	-0.055	0.50	No
		y	-0.055	7.50	No
		y	-0.145	1.50	No
	32	y	-0.018	0.50	No
		y	-0.018	4.50	No
	33	y	-0.055	0.50	No
		y	-0.055	7.50	No
		y	-0.145	1.50	No
	40	y	-0.055	0.50	No
		y	-0.055	7.50	No
	42	y	-0.055	0.50	No
		y	-0.055	7.50	No
	43	y	-0.055	0.50	No
		y	-0.055	7.50	No

W0	28	z	-0.095	0.50	No
		z	-0.095	4.50	No
	29	z	-0.237	0.50	No
		z	-0.237	7.50	No
	30	z	-0.056	1.50	No
		z	-0.062	0.50	No
	31	z	-0.062	4.50	No
		z	-0.134	0.50	No
	32	z	-0.134	7.50	No
		z	-0.051	1.50	No
	33	z	-0.062	0.50	No
		z	-0.062	4.50	No
	40	z	-0.134	0.50	No
		z	-0.134	7.50	No
	42	z	-0.051	1.50	No
z		-0.237	0.50	No	
W30	28	x	-0.237	7.50	No
		x	-0.134	0.50	No
	29	x	-0.134	7.50	No
		x	-0.134	0.50	No
	30	x	-0.134	7.50	No
		x	-0.051	1.50	No
	31	x	-0.051	4.50	No
		x	-0.10	0.50	No
	32	x	-0.10	7.50	No
		x	-0.056	1.50	No
	33	x	-0.084	0.50	No
		x	-0.084	4.50	No
	40	x	-0.084	0.50	No
		x	-0.084	4.50	No
	42	x	-0.203	0.50	No
x		-0.203	7.50	No	
43	x	-0.032	1.50	No	
	x	-0.084	0.50	No	
Di	28	y	-0.084	4.50	No
		y	-0.203	0.50	No
	29	y	-0.203	7.50	No
		y	-0.032	1.50	No
	30	y	-0.10	0.50	No
		y	-0.10	7.50	No
	31	y	-0.203	0.50	No
		y	-0.203	7.50	No
	32	y	-0.032	1.50	No
		y	-0.042	0.50	No
	33	y	-0.042	4.50	No
		y	-0.101	0.50	No
	40	y	-0.101	7.50	No
		y	-0.062	1.50	No
	42	y	-0.062	0.50	No
y		-0.101	7.50	No	

		y	-0.101	7.50	No
	43	y	-0.101	0.50	No
		y	-0.101	7.50	No
Wi0	28	z	-0.021	0.50	No
		z	-0.021	4.50	No
	29	z	-0.047	0.50	No
		z	-0.047	7.50	No
		z	-0.016	1.50	No
	30	z	-0.015	0.50	No
		z	-0.015	4.50	No
	31	z	-0.029	0.50	No
		z	-0.029	7.50	No
		z	-0.012	1.50	No
	32	z	-0.015	0.50	No
		z	-0.015	4.50	No
	33	z	-0.029	0.50	No
		z	-0.029	7.50	No
		z	-0.012	1.50	No
	40	z	-0.047	0.50	No
		z	-0.047	7.50	No
	42	z	-0.029	0.50	No
		z	-0.029	7.50	No
	43	z	-0.029	0.50	No
		z	-0.029	7.50	No
Wi30	28	x	-0.013	0.50	No
		x	-0.013	4.50	No
	29	x	-0.023	0.50	No
		x	-0.023	7.50	No
		x	-0.013	1.50	No
	30	x	-0.019	0.50	No
		x	-0.019	4.50	No
	31	x	-0.041	0.50	No
		x	-0.041	7.50	No
		x	-0.007	1.50	No
	32	x	-0.019	0.50	No
		x	-0.019	4.50	No
	33	x	-0.041	0.50	No
		x	-0.041	7.50	No
		x	-0.007	1.50	No
	40	x	-0.023	0.50	No
		x	-0.023	7.50	No
	42	x	-0.041	0.50	No
		x	-0.041	7.50	No
	43	x	-0.041	0.50	No
		x	-0.041	7.50	No
WLO	28	z	-0.006	0.50	No
		z	-0.006	4.50	No
	29	z	-0.015	0.50	No
		z	-0.015	7.50	No
		z	-0.004	1.50	No
	30	z	-0.004	0.50	No
		z	-0.004	4.50	No
	31	z	-0.009	0.50	No
		z	-0.009	7.50	No
		z	-0.003	1.50	No
	32	z	-0.004	0.50	No
		z	-0.004	4.50	No
	33	z	-0.009	0.50	No
		z	-0.009	7.50	No
		z	-0.003	1.50	No

	40	z	-0.015	0.50	No
		z	-0.015	7.50	No
	42	z	-0.009	0.50	No
		z	-0.009	7.50	No
	43	z	-0.009	0.50	No
		z	-0.009	7.50	No
WL30	28	x	-0.004	0.50	No
		x	-0.004	4.50	No
	29	x	-0.007	0.50	No
		x	-0.007	7.50	No
		x	-0.004	1.50	No
	30	x	-0.006	0.50	No
		x	-0.006	4.50	No
	31	x	-0.013	0.50	No
		x	-0.013	7.50	No
		x	-0.002	1.50	No
	32	x	-0.006	0.50	No
		x	-0.006	4.50	No
	33	x	-0.013	0.50	No
		x	-0.013	7.50	No
		x	-0.002	1.50	No
	40	x	-0.007	0.50	No
		x	-0.007	7.50	No
	42	x	-0.013	0.50	No
		x	-0.013	7.50	No
	43	x	-0.013	0.50	No
		x	-0.013	7.50	No
LL1	9	y	-0.25	6.29	No
	46	y	-0.25	6.29	No
LL2	9	y	-0.25	0.00	No
	46	y	-0.25	0.00	No
LLa1	40	y	-0.25	4.00	No
LLa2	29	y	-0.25	4.00	No
LLa3	28	y	-0.25	3.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00
LLa1	250 lb Live Load Antenna 1	No	0.00	0.00	0.00
LLa2	250 lb Live Load Antenna 2	No	0.00	0.00	0.00
LLa3	250 lb Live Load Antenna 3	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
W0	0.00	0.00	0.00
W30	0.00	0.00	0.00
Di	0.00	0.00	0.00
Wi0	0.00	0.00	0.00
Wi30	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
LL1	0.00	0.00	0.00
LL2	0.00	0.00	0.00
LLa1	0.00	0.00	0.00
LLa2	0.00	0.00	0.00
LLa3	0.00	0.00	0.00

Current Date: 4/22/2019 2:50 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT5432\LTE 2C-3C-4C\CT5432 (LTE 2C-3C-4C)(MODS).etx

Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

- LC1=1.2DL+W0
- LC2=1.2DL+W30
- LC3=1.2DL-W0
- LC4=1.2DL-W30
- LC5=0.9DL+W0
- LC6=0.9DL+W30
- LC7=0.9DL-W0
- LC8=0.9DL-W30
- LC9=1.2DL+Di+Wi0
- LC10=1.2DL+Di+Wi30
- LC11=1.2DL+Di-Wi0
- LC12=1.2DL+Di-Wi30
- LC13=1.2DL
- LC15=1.2DL+1.5LL1
- LC16=1.2DL+1.5LL2
- LC17=1.2DL+WL0+1.5LLa1
- LC18=1.2DL+WL30+1.5LLa1
- LC19=1.2DL-WL0+1.5LLa1
- LC20=1.2DL-WL30+1.5LLa1
- LC21=1.2DL+WL0+1.5LLa2
- LC22=1.2DL+WL30+1.5LLa2
- LC23=1.2DL-WL0+1.5LLa2
- LC24=1.2DL-WL30+1.5LLa2
- LC25=1.2DL+WL0+1.5LLa3
- LC26=1.2DL+WL30+1.5LLa3
- LC27=1.2DL-WL0+1.5LLa3
- LC28=1.2DL-WL30+1.5LLa3

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
C 3-1/2x2x3/16		4	LC11 at 50.00%	0.60	OK	Eq. H1-1b
		8	LC12 at 48.44%	0.58	OK	Eq. H1-1b
		13	LC9 at 48.44%	0.57	OK	Eq. H1-1b
L 2-1_2X2-1_2X1_4		48	LC3 at 0.00%	0.36	OK	Eq. H2-1
		49	LC2 at 0.00%	0.46	OK	Eq. H2-1
		51	LC1 at 0.00%	0.41	OK	Eq. H2-1
L 2X2X3_16		2	LC7 at 100.00%	0.47	OK	Eq. H2-1
		3	LC2 at 100.00%	0.43	OK	Eq. H2-1
		6	LC3 at 100.00%	0.41	OK	Eq. H2-1
		7	LC8 at 100.00%	0.48	OK	Eq. H2-1
		14	LC2 at 100.00%	0.40	OK	Eq. H2-1
		15	LC4 at 100.00%	0.48	OK	Eq. H2-1
PIPE 2-1_2x0.203		29	LC1 at 60.42%	0.69	OK	Eq. H1-1b
		31	LC2 at 60.42%	0.67	OK	Eq. H1-1b
		33	LC4 at 60.42%	0.60	OK	Eq. H1-1b
PIPE 2x0.154		28	LC4 at 64.58%	0.45	OK	Eq. H1-1b
		30	LC2 at 64.58%	0.41	OK	Eq. H1-1b

32	LC3 at 64.58%	0.42	OK	Eq. H1-1b
40	LC2 at 60.42%	0.68	OK	Eq. H1-1b
42	LC4 at 60.42%	0.69	OK	Eq. H1-1b
43	LC1 at 60.42%	0.65	OK	Eq. H1-1b
46	LC11 at 31.25%	0.50	OK	Eq. H1-1b
47	LC10 at 68.75%	0.50	OK	Eq. H1-1b
50	LC9 at 68.75%	0.51	OK	Eq. H1-1b

PIPE 3x0.216

1	LC16 at 100.00%	0.97	OK	Eq. H1-1b
5	LC11 at 100.00%	0.78	OK	Eq. H1-1b
9	LC16 at 43.75%	0.42	OK	Eq. H1-1b
10	LC16 at 43.75%	0.43	OK	Eq. H1-1b
11	LC11 at 56.25%	0.38	OK	Eq. H1-1b
12	LC9 at 0.00%	0.80	OK	Eq. H1-1b

PL 6x3/8

25	LC2 at 46.88%	0.32	OK	Eq. H1-1b
26	LC4 at 50.00%	0.35	OK	Eq. H1-1b
27	LC1 at 0.00%	0.34	OK	Eq. H1-1b

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
2	-0.7253	0.00	4.0896	0
3	-6.0833	0.00	4.0896	0
4	-6.292	0.00	4.0896	0
5	-6.3333	0.00	3.6566	0
6	-6.5833	0.00	3.2236	0
7	-3.7376	0.00	-1.128	0
8	-3.9043	0.00	-1.4166	0
9	-0.892	0.00	3.8009	0
10	-6.6877	0.00	3.4042	0
11	-3.179	0.00	-2.6729	0
12	-2.8457	0.00	-2.6729	0
13	-0.50	0.00	-7.3131	0
14	-0.3957	0.00	-7.4938	0
17	0.7253	0.00	4.0896	0
18	6.0833	0.00	4.0896	0
19	6.292	0.00	4.0896	0
20	6.3333	0.00	3.6566	0
21	6.5833	0.00	3.2236	0
22	3.7376	0.00	-1.128	0
23	3.9043	0.00	-1.4166	0
24	0.892	0.00	3.8009	0

25	6.6877	0.00	3.4042	0
26	3.179	0.00	-2.6729	0
27	2.8457	0.00	-2.6729	0
28	0.50	0.00	-7.3131	0
29	0.3957	0.00	-7.4938	0
32	0.00	0.00	-7.3131	0
69	0.9427	0.00	0.5443	0
70	0.00	0.00	-1.0885	0
71	-0.9427	0.00	0.5443	0
76	-5.709	-2.00	4.2896	0
77	-2.355	-3.00	4.2896	0
78	-5.709	4.00	4.2896	0
79	-2.355	5.00	4.2896	0
84	-0.8604	-2.00	-7.0889	0
85	-2.5374	-3.00	-4.1843	0
86	-0.8604	4.00	-7.0889	0
87	-2.5374	5.00	-4.1843	0
92	6.5694	-2.00	2.7994	0
93	4.8924	-3.00	-0.1053	0
94	6.5694	4.00	2.7994	0
95	4.8924	5.00	-0.1053	0
98	5.712	-3.00	4.2896	0
99	5.712	5.00	4.2896	0
102	-6.5709	-3.00	2.802	0
103	-6.5709	5.00	2.802	0
106	0.8589	-3.00	-7.0915	0
107	0.8589	5.00	-7.0915	0
108	-6.292	3.00	4.0896	0
109	6.292	3.00	4.0896	0
110	-6.6877	3.00	3.4042	0
111	-0.3957	3.00	-7.4938	0
112	-6.5833	3.00	3.2236	0
113	-6.0833	3.00	4.0896	0
114	0.50	3.00	-7.3131	0
115	-0.50	3.00	-7.3131	0
116	0.3957	3.00	-7.4938	0
117	6.6877	3.00	3.4042	0
118	6.0833	3.00	4.0896	0
119	6.5833	3.00	3.2236	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
69	1	1	1	1	1	1
70	1	1	1	1	1	1
71	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	5	71		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00
2	5	9		L 2X2X3_16	A36	0.00	0.00	0.00
3	5	7		L 2X2X3_16	A36	0.00	0.00	0.00
4	8	2		C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
5	20	69		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00
6	20	24		L 2X2X3_16	A36	0.00	0.00	0.00
7	20	22		L 2X2X3_16	A36	0.00	0.00	0.00
8	23	17		C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
9	4	19		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
10	10	14		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
11	29	25		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
12	70	32		PIPE 3x0.216	A500 GrB rectangular	0.00	0.00	0.00
13	11	26		C 3-1/2x2x3/16	A500 GrB rectangular	0.00	0.00	0.00
14	27	32		L 2X2X3_16	A36	0.00	0.00	0.00
15	12	32		L 2X2X3_16	A36	0.00	0.00	0.00
25	6	3		PL 6x3/8	A36	0.00	0.00	0.00
26	18	21		PL 6x3/8	A36	0.00	0.00	0.00
27	28	13		PL 6x3/8	A36	0.00	0.00	0.00
28	78	76		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
29	79	77		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
30	94	92		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
31	95	93		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
32	86	84		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
33	87	85		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
40	99	98		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
42	107	106		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	103	102		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
46	108	109		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
47	110	111		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
48	112	113		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
49	114	115		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
50	116	117		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
51	118	119		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
2	270.00	0	0.00	0.00	0.00
7	270.00	0	0.00	0.00	0.00
8	180.00	0	0.00	0.00	0.00
13	180.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
28	0.00	2	0.7071	0.00	-0.7071
29	0.00	2	0.7071	0.00	-0.7071
30	0.00	2	0.7071	0.00	-0.7071
31	0.00	2	0.7071	0.00	-0.7071
32	0.00	2	0.7071	0.00	-0.7071
33	0.00	2	0.7071	0.00	-0.7071
40	0.00	2	0.7071	0.00	-0.7071
48	180.00	0	0.00	0.00	0.00
49	180.00	0	0.00	0.00	0.00
51	180.00	0	0.00	0.00	0.00

Rigid end offsets

Member	DJX [in]	DJY [in]	DJZ [in]	DKX [in]	DKY [in]	DKZ [in]
2	0.00	2.00	0.00	0.00	2.00	0.00
3	0.00	2.00	0.00	0.00	2.00	0.00
6	0.00	2.00	0.00	0.00	2.00	0.00
7	0.00	2.00	0.00	0.00	2.00	0.00
14	0.00	2.00	0.00	0.00	2.00	0.00
15	0.00	2.00	0.00	0.00	2.00	0.00

STRUCTURAL NOTES:

- DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE SUPPLEMENTS, INTERNATIONAL BUILDING CODE, EIA/TIA-222-G STRUCTURAL STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. ANY UNUSUAL CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS".
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A36 UNLESS OTHERWISE INDICATED.
- STEEL PIPE SHALL CONFORM TO ASTM A500 "COLD-FORMED WELDED & SEAMLESS CARBON STEEL STRUCTURAL TUBING", GRADE B, OR ASTM A53 PIPE STEEL BLACK AND HOT-DIPPED ZINC-COATED WELDED AND SEAMLESS TYPE E OR S, GRADE B. PIPE SIZES INDICATED ARE NOMINAL. ACTUAL OUTSIDE DIAMETER IS LARGER.
- STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA UON.
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS OTHERWISE NOTED.
- ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS OTHERWISE NOTED.
- FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT COMPLYING WITH REQUIREMENTS OF ASTM A780. GALVANIZING REPAIR PAINT SHALL HAVE 65 PERCENT ZINC BY WEIGHT, ZIRP BY DUNCAN GALVANIZING, GALVA BRIGHT PREMIUM BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 OR A153 AS APPLICABLE.
- CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D.I. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "STEEL CONSTRUCTION MANUAL". 14TH EDITION.
- INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON-CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL.
- UNISTRUT SHALL BE FORMED STEEL CHANNEL STRUT FRAMING AS MANUFACTURED BY UNISTRUT CORP., WAYNE, MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA, UNLESS OTHERWISE NOTED, AND SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION.
- EPOXY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS & WASHERS. AN INTERNALLY THREADED INSERT, A SCREEN TUBE AND A EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HILTI-HIT HY-270 AND OR HY-200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS I, HILTI KWIK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT.
- ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL. ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE.

THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE PROJECT ARE PERMITTED TO ACT AS THE APPROVED AGENCY AND THEIR PERSONNEL ARE PERMITTED TO ACT AS THE SPECIAL INSPECTOR FOR THE WORK DESIGNED BY THEM, PROVIDED THOSE PERSONNEL MEET THE QUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE. THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705.

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. REPORTS SHALL INDICATE THAT WORK INSPECTED WAS OR WAS NOT COMPLETED IN CONFORMANCE TO APPROVED CONSTRUCTION DOCUMENTS. DISCREPANCIES SHALL BE BROUGHT TO THE IMMEDIATE ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED.

SPECIAL INSPECTION CHECKLIST	
BEFORE CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	ENGINEER OF RECORD APPROVED SHOP DRAWINGS ¹
N/A	MATERIAL SPECIFICATIONS REPORT ²
N/A	FABRICATOR NDE INSPECTION
N/A	PACKING SLIPS ³
ADDITIONAL TESTING AND INSPECTIONS:	
DURING CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	STEEL INSPECTIONS
N/A	HIGH STRENGTH BOLT INSPECTIONS
N/A	HIGH WIND ZONE INSPECTIONS ⁴
N/A	FOUNDATION INSPECTIONS
N/A	CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT
N/A	POST INSTALLED ANCHOR VERIFICATION ⁵
N/A	GROUT VERIFICATION
N/A	CERTIFIED WELD INSPECTION
N/A	EARTHWORK: LIFT AND DENSITY
N/A	ON SITE COLD GALVANIZING VERIFICATION
N/A	GUY WIRE TENSION REPORT
ADDITIONAL TESTING AND INSPECTIONS:	
AFTER CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	MODIFICATION INSPECTOR REDLINE OR RECORD DRAWINGS ⁶
N/A	POST INSTALLED ANCHOR PULL-OUT TESTING
REQUIRED	PHOTOGRAPHS
ADDITIONAL TESTING AND INSPECTIONS:	

NOTES:

- REQUIRED FOR ANY NEW SHOP FABRICATED FRP OR STEEL.
- PROVIDED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH BOLTS OR STEEL.
- PROVIDED BY GENERAL CONTRACTOR; PROOF OF MATERIALS.
- HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C,D 110MPH INSPECT FRAMING OF WALLS, ANCHORING, FASTENING SCHEDULE.
- ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ACI 308.4 AND ICC-ES AC308 FOR CRACKED CONCRETE AND SEISMIC APPLICATIONS. DESIGN ADHESIVE BOND STRENGTH HAS BEEN BASED ON ACI 308.4 TEMPERATURE CATEGORY B WITH INSTALLATIONS INTO DRY HOLES DRILLED USING A CARBIDE BIT INTO CRACKED CONCRETE THAT HAS CURED FOR AT LEAST 21 DAYS. ADHESIVE ANCHORS REQUIRING CERTIFIED INSTALLATIONS SHALL BE INSTALLED BY A CERTIFIED ADHESIVE ANCHOR INSTALLER PER ACI 318-11 D.9.2.2. INSTALLATIONS REQUIRING CERTIFIED INSTALLERS SHALL BE INSPECTED PER ACI 318-11 D.8.2.4.
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

NOTES:

- ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4" A325-X BOLTS, UNLESS OTHERWISE NOTIFIED.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED BEFORE ORDERING MATERIAL.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
- VERIFICATION OF EXISTING ROOF CONSTRUCTION IS REQUIRED PRIOR TO THE INSTALLATION OF THE ROOF PLATFORM. ENGINEER OF RECORD IS TO APPROVE EXISTING CONDITIONS IN ORDER TO MOVE FORWARD.
- CENTERLINE OF PROPOSED STEEL PLATFORM SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- EXISTING BRICK MASONRY COLUMNS/BEARING TO BE REPAIRED/REPLACED AT ALL PROPOSED PLATFORM SUPPORT POINTS. ENGINEER OF RECORD TO REVIEW AND APPROVE.

HGD HUDSON Design Group LLC
 45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845
 TEL: (978) 557-5553 FAX: (978) 336-5586

CENTERLINE COMMUNICATIONS
 750 WEST CENTER STREET., SUITE #301 WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT5432
SITE NAME: NEWTOWN EAST CENTRAL
SBA SITE ID: CT13057
 151 BERKSHIRE ROAD SANDY HOOK, CT 06482 FAIRFIELD COUNTY

at&t
 500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067

2	05/14/19	ISSUED FOR CONSTRUCTION	HC	A	DJC
1	04/24/19	ISSUED FOR REVIEW	RP	AT	DJC
A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: JM		



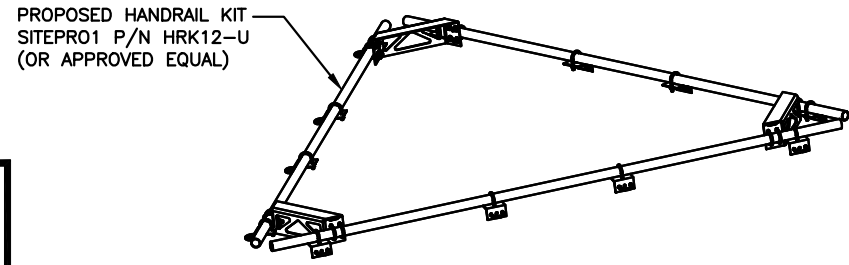
AT&T
STRUCTURAL NOTES
 (LTE 2C/3C/4C/4TX4RX)
 SITE NUMBER: CT5432
 DRAWING NUMBER: SN-1
 REV: 2

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION

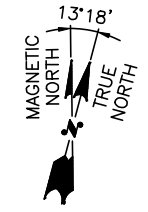
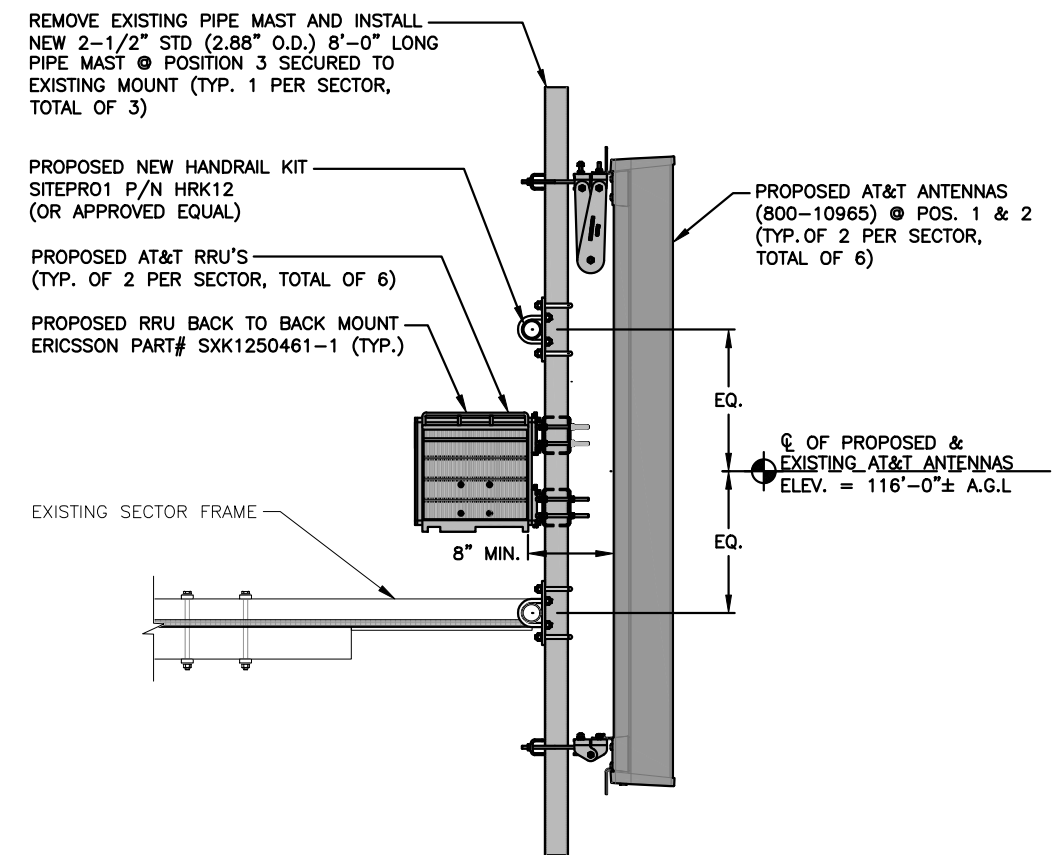
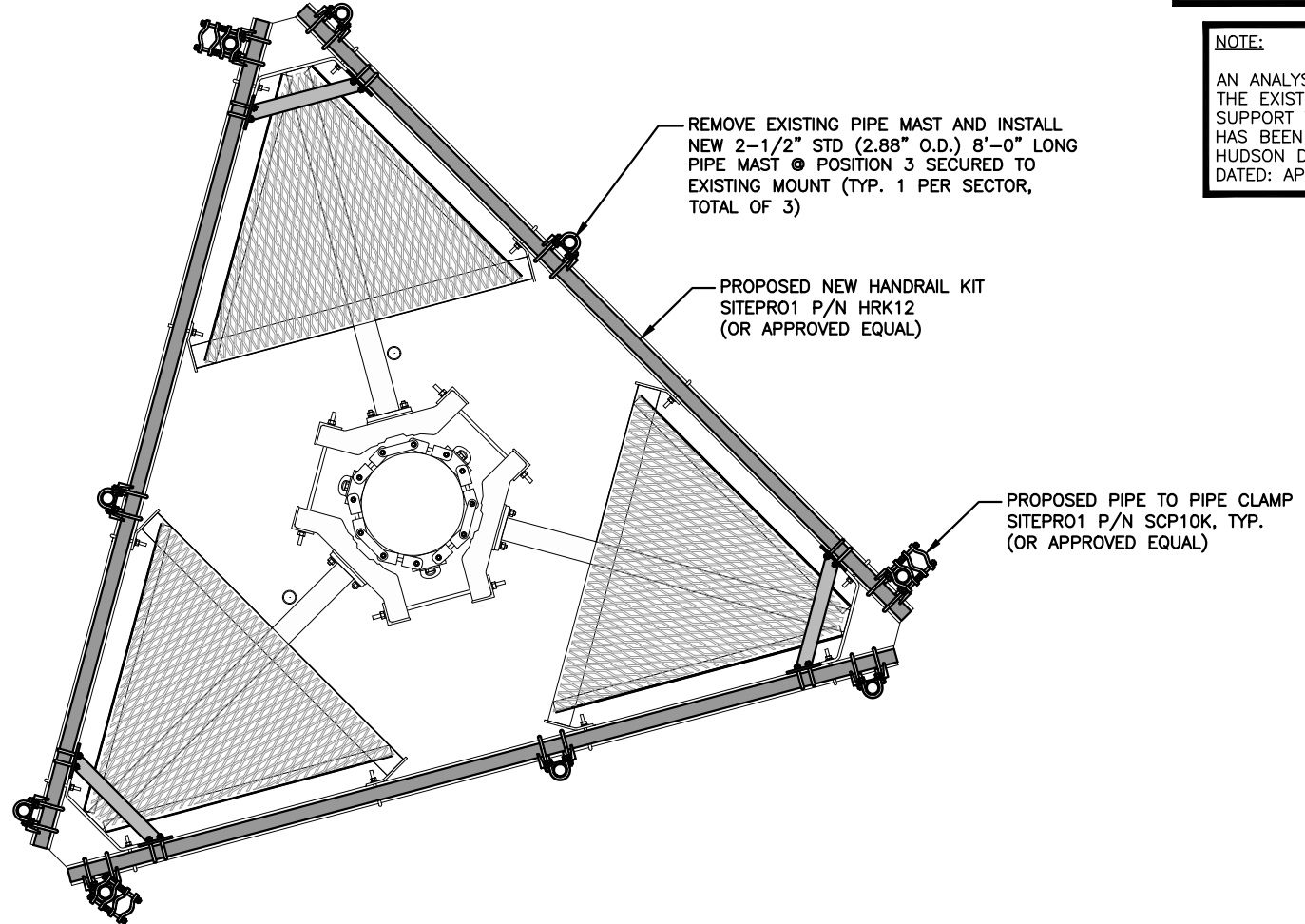
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
ROTATION OF MOUNTS OR INSTALLATION OF MOUNT MODS MUST NOT ADVERSELY AFFECT, OBSTRUCT, BEND OR PINCH EXISTING SAFETY CABLE IN ANY WAY. GC, C/O AT&T, WILL PURCHASE AND INSTALL CABLE RE-ROUTING BRACKETS AS REQUIRED.

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING **ANTENNA MOUNT** TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: APRIL 22, 2019



PROPOSED HANDRAIL KIT
SCALE: N.T.S.



PROPOSED MOUNT MODIFICATIONS PLAN
22x34 SCALE: 3/4"=1'-0"
11x17 SCALE: 3/8"=1'-0"



PROPOSED LTE ANTENNA & RRH MOUNTING DETAIL
22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"



				AT&T			
				MOUNT MODIFICATION DESIGN (LTE 2C/3C/4C/4TX4RX)			
NO.	DATE	REVISIONS	BY	CHK	APP'D	SITE NUMBER	DRAWING NUMBER
2	05/14/19	ISSUED FOR CONSTRUCTION	HC	AT	DJC	CT5432	S-1
1	04/24/19	ISSUED FOR REVIEW	RP	AT	DJC		
A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC		
SCALE: AS SHOWN				DESIGNED BY: AT		DRAWN BY: JM	
						REV	2

PROJECT INFORMATION

SCOPE OF WORK: ITEMS TO BE MOUNTED ON THE EXISTING MONOPOLE:

- NEW AT&T ANTENNAS (800-10965) @ POS. 1 (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T ANTENNAS (800-10965) @ POS. 2 (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T AT&T RRUS B2/B66A 8843 (AWS/PCS) (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T RRUS B5/B12 4449 (850/700) (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T SURGE ARRESTOR DC6-48-60-18-8C (TOTAL OF 1) WITH (2) DC POWER, (1) FIBER RUN WITHIN (P) 3"Ø FLEX CONDUIT.
- INSTALL (1) HANDRAIL KIT.

ITEMS TO BE MOUNTED AT EQUIPMENT LOCATION:

- SWAP BBU FOR 6630.
- ADD 2ND 6630 FOR 5G.

ITEMS TO REMAIN:

- (3) ANTENNAS, (6) TWIN TMA'S, (1) SURGE ARRESTOR, (6) COAX CABLES, (2) DC POWER & (1) FIBER.

SITE ADDRESS: 151 BERKSHIRE ROAD
SANDY HOOK, CT 06482

LATITUDE: 41.397491° N 41° 23' 50.97" N

LONGITUDE: 73.235798° W 73° 14' 8.88" W

TYPE OF SITE: MONOPOLE / OUTDOOR EQUIPMENT

TOWER HEIGHT: 149'-0"±

RAD CENTER: 116'-0"±

CURRENT USE: TELECOMMUNICATIONS FACILITY

PROPOSED USE: TELECOMMUNICATIONS FACILITY



SITE NUMBER: CT5432

SITE NAME: NEWTOWN EAST CENTRAL

FA CODE: 10071168

PACE ID: MRCTB037970, MRCTB037935, MRCTB038091, MRCTB038093,

PROJECT: LTE 2C/3C/4C/4TX4RX 2019 LTE NEXT CARRIER

VICINITY MAP

GENERAL NOTES

DIRECTIONS TO SITE:

DEPART W CENTER ST. HEAD EAST ON MA-106 E. TURN RIGHT ONTO MA-106 E. USE RIGHT LANE TO MERGE ONTO MA-24 S VIA THE RAMP TO FALL RIVER. MERGE ONTO MA-24 S. TAKE EXIT 14B TO MERGE ONTO I-495 N TOWARD WORCESTER. TAKE EXIT 22 FOR I-90 TOWARD MASSPIKE/BOSTON/ALBANY NY. KEEP LEFT AT THE FORK, FOLLOW SIGNS FOR I-90 W/SPRINGFIELD/ALBANY AND MERGE ONTO I-90 W. USE THE RIGHT TWO LANES TO TAKE EXIT 9 FOR I-84 TOWARD US-20/HARTFORD/NEW YORK CITY. CONTINUE ONTO I-84. CONTINUE STRAIGHT TO STAY ON I-84 (SIGNS FOR I-91 N/HARTFORD). TAKE EXIT 11 TOWARD CT-34/DERBY/NEW HAVEN. DRIVE TO CT-34 E. TURN RIGHT ONTO WASSERMAN WAY. TURN RIGHT ONTO CT-34 E. ADDRESS WILL BE ON THE LEFT.

1. THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

DRAWING INDEX

SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	2
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A-1	COMPOUND & EQUIPMENT PLANS	2
A-2	ANTENNA LAYOUTS & ELEVATION	2
A-3	DETAILS	2
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RF-1	RF PLUMBING DIAGRAM	2
G-1	GROUNDING DETAILS	2



72 HOURS



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750 WEST CENTER STREET., SUITE #301
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT5432
SITE NAME: NEWTOWN EAST CENTRAL
SBA SITE ID: CT13057

151 BERKSHIRE ROAD
SANDY HOOK, CT 06482
FAIRFIELD COUNTY

500 ENTERPRISE DRIVE, SUITE 3A
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NO.	DATE	REVISIONS	BY	CHK	APP'D
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A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: JM

AT&T

TITLE SHEET
(LTE 2C/3C/4C/4TX4RX)

SITE NUMBER	DRAWING NUMBER	REV
CT5432	T-1	2

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:
 CONTRACTOR – CENTERLINE
 SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)
 OWNER – AT&T MOBILITY
2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
20. APPLICABLE BUILDING CODES:
 SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

BUILDING CODE: IBC 2015 WITH 2018 CT STATE BUILDING CODE AMENDMENTS
 ELECTRICAL CODE: 2017 NATIONAL ELECTRICAL CODE (NFPA 70-2017)

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G, STRUCTURAL STANDARDS FOR STEEL

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS					
AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
BTCW	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	P	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		

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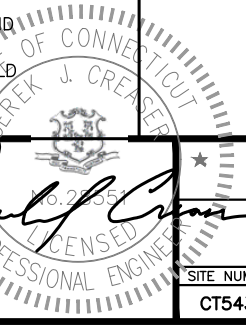
750 WEST CENTER STREET., SUITE #301
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SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: JM



AT&T
 GENERAL NOTES
 (LTE 2C/3C/4C/4TX4RX)

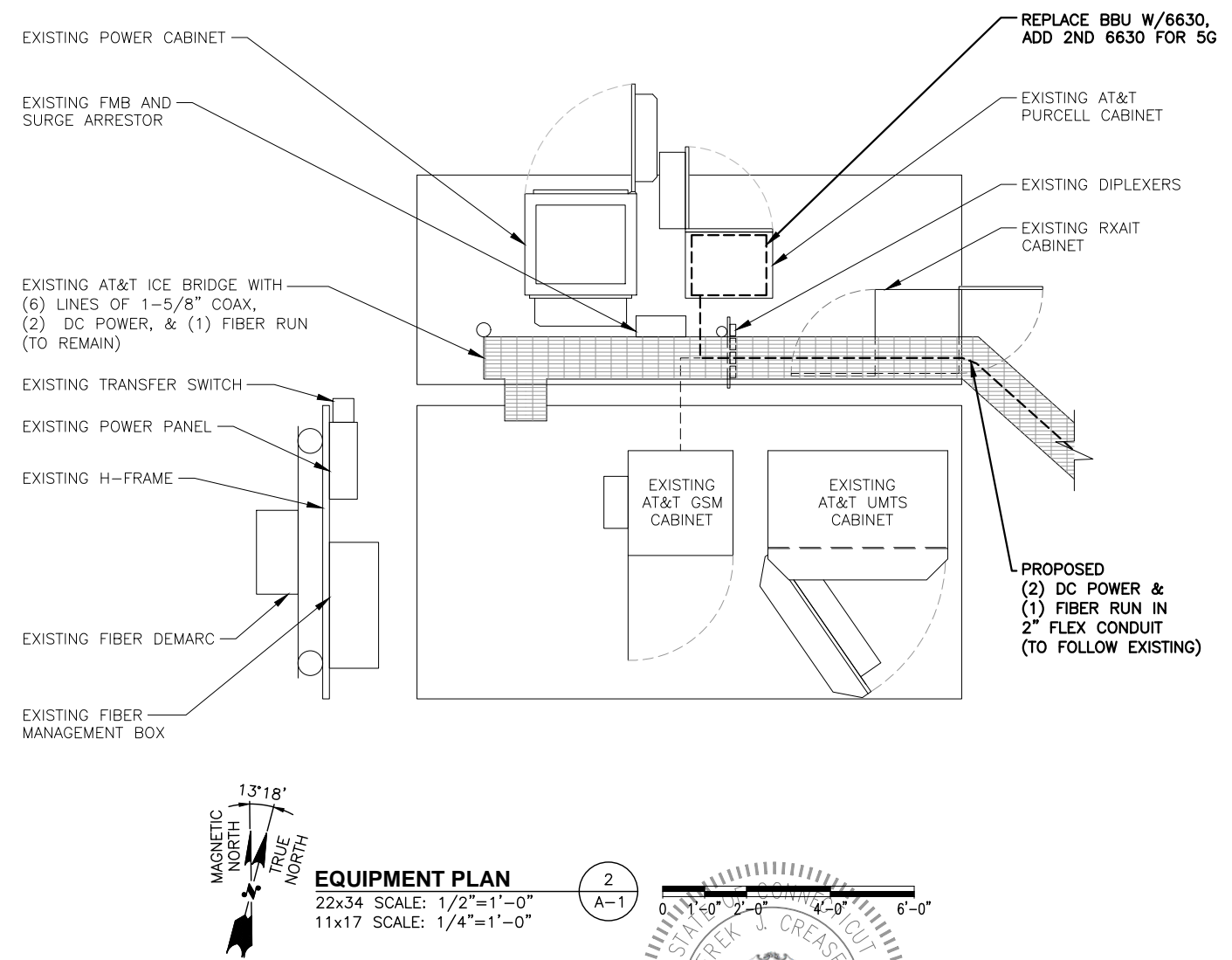
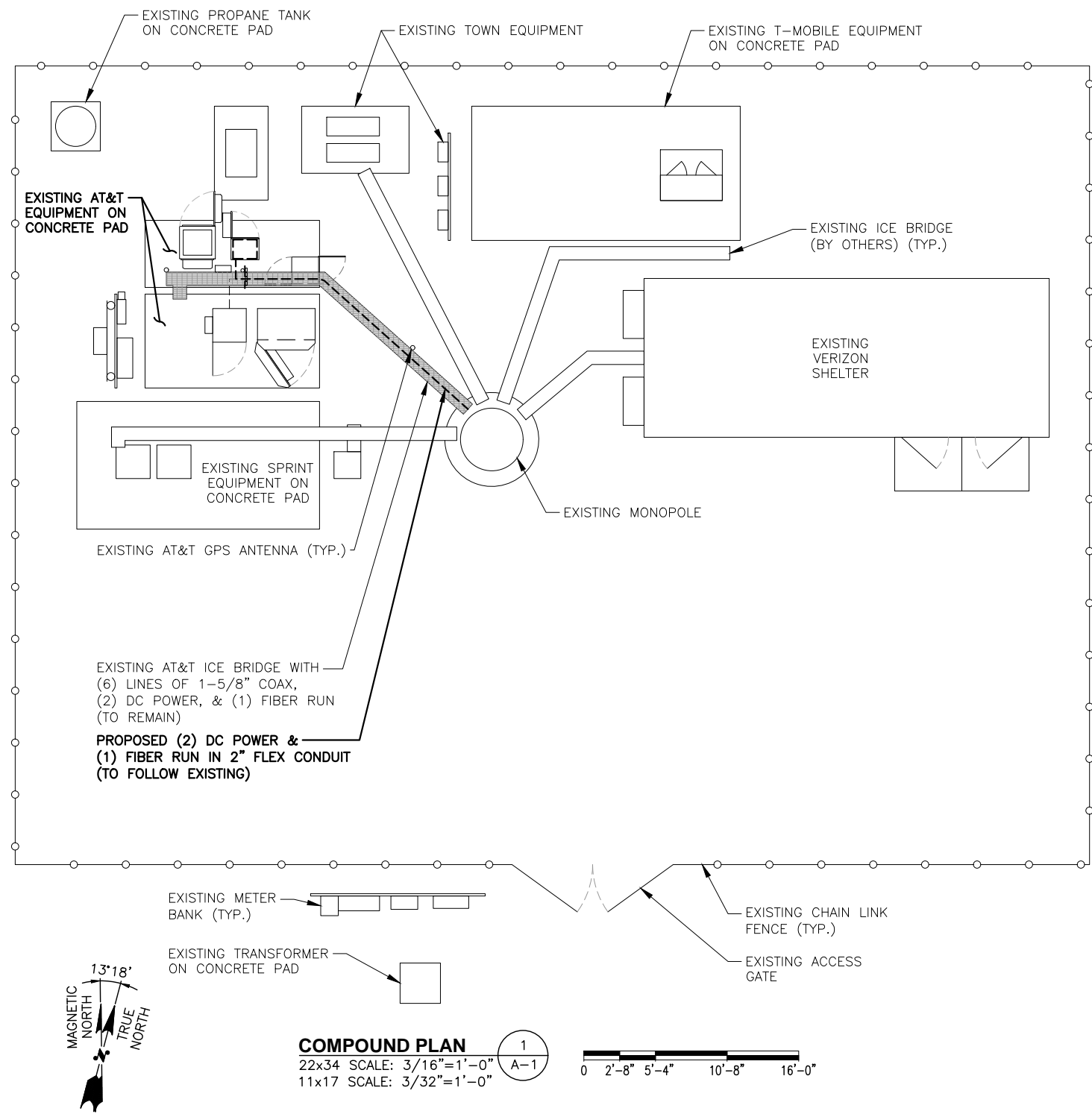
SITE NUMBER	DRAWING NUMBER	REV
CT5432	GN-1	2

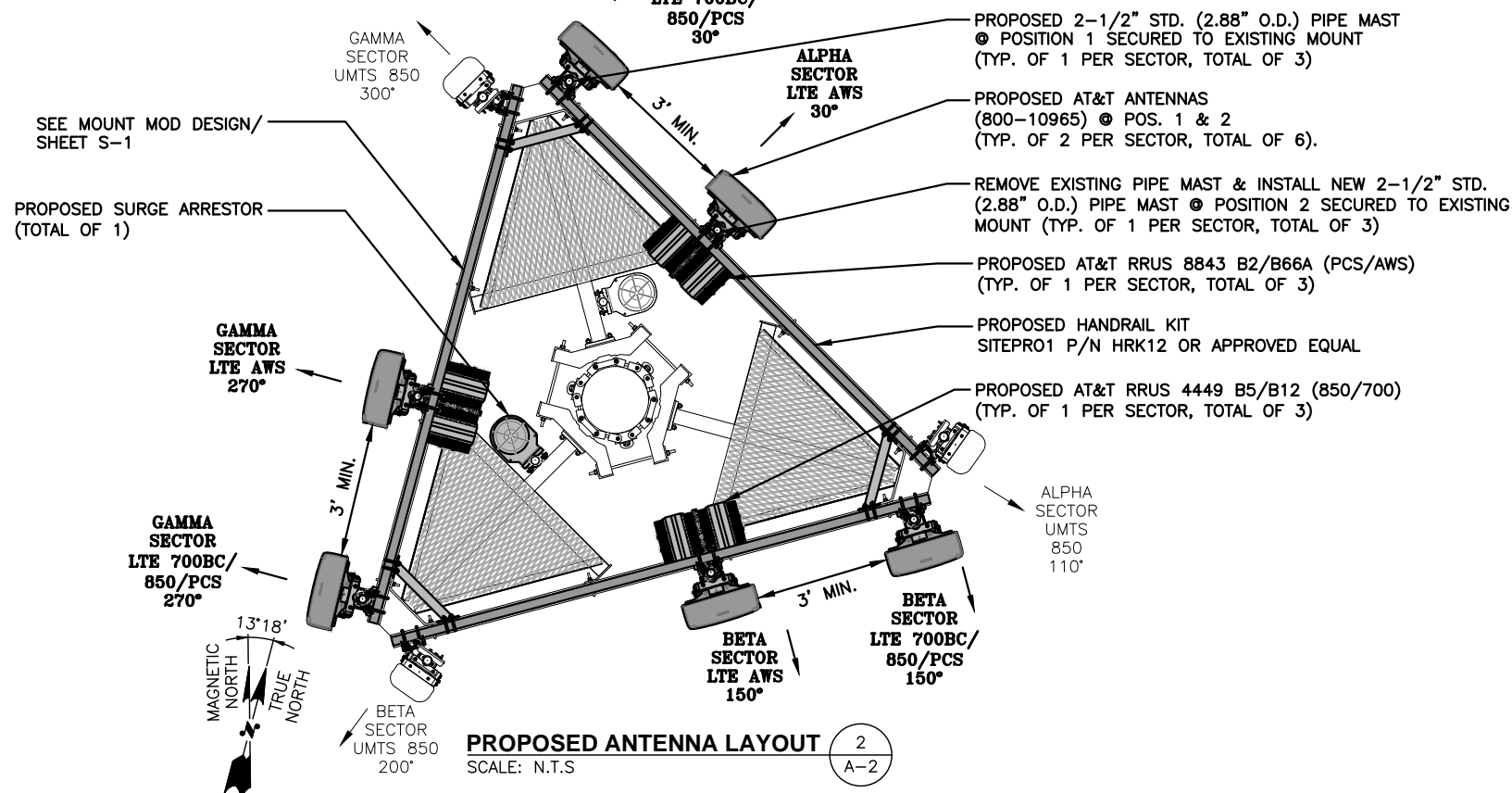
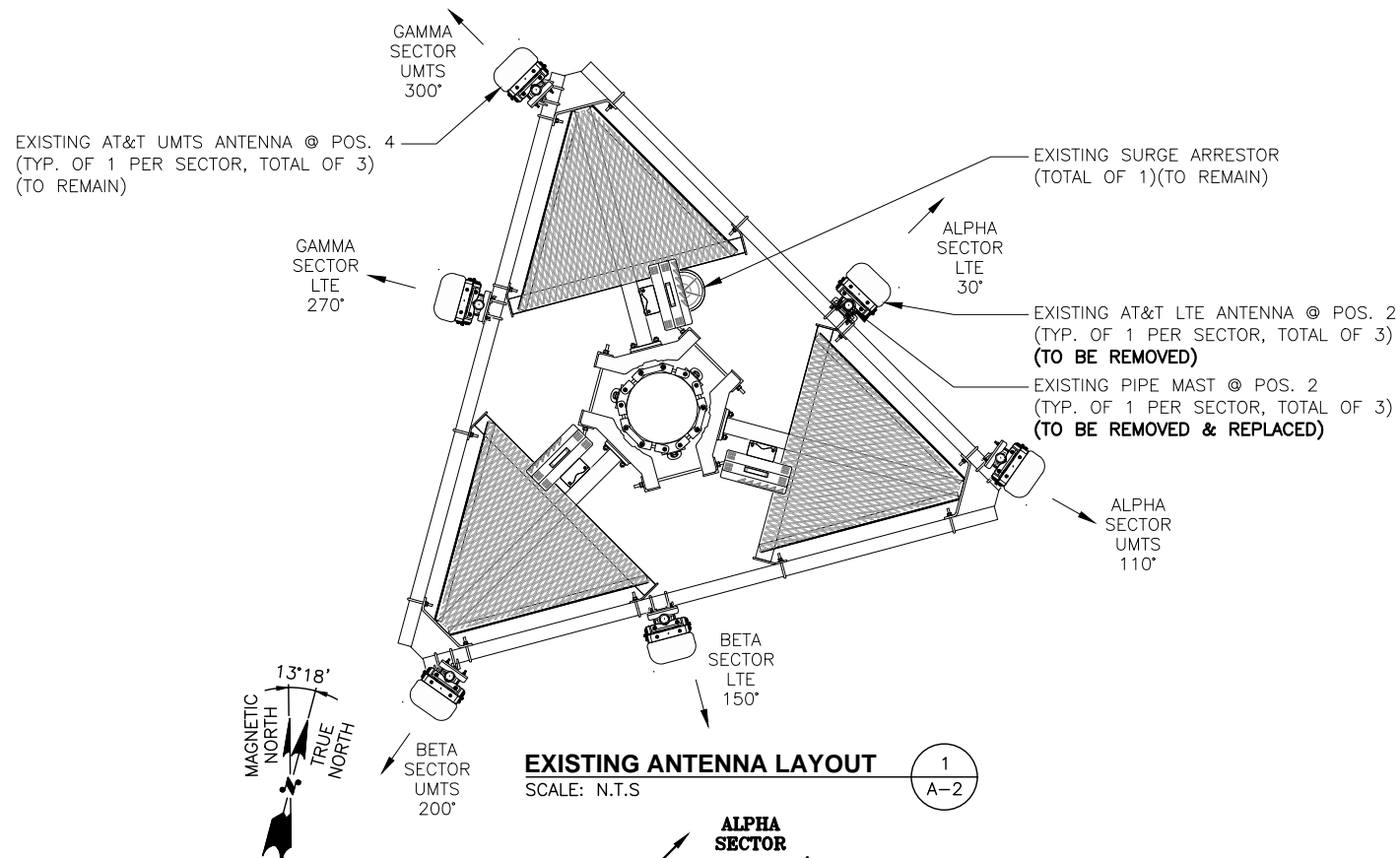
NOTE:
 ROTATION OF MOUNTS OR INSTALLATION OF MOUNT MODS MUST NOT ADVERSELY AFFECT, OBSTRUCT, BEND OR PINCH EXISTING SAFETY CABLE IN ANY WAY. GC, C/O AT&T, WILL PURCHASE AND INSTALL CABLE RE-ROUTING BRACKETS AS REQUIRED.

NOTE:
 REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
 AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION

NOTE:
 AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: APRIL 22, 2019



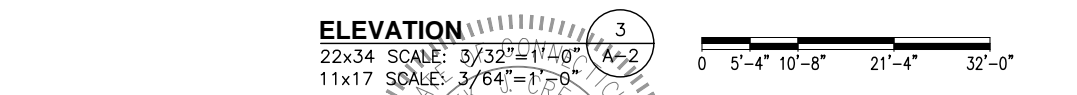
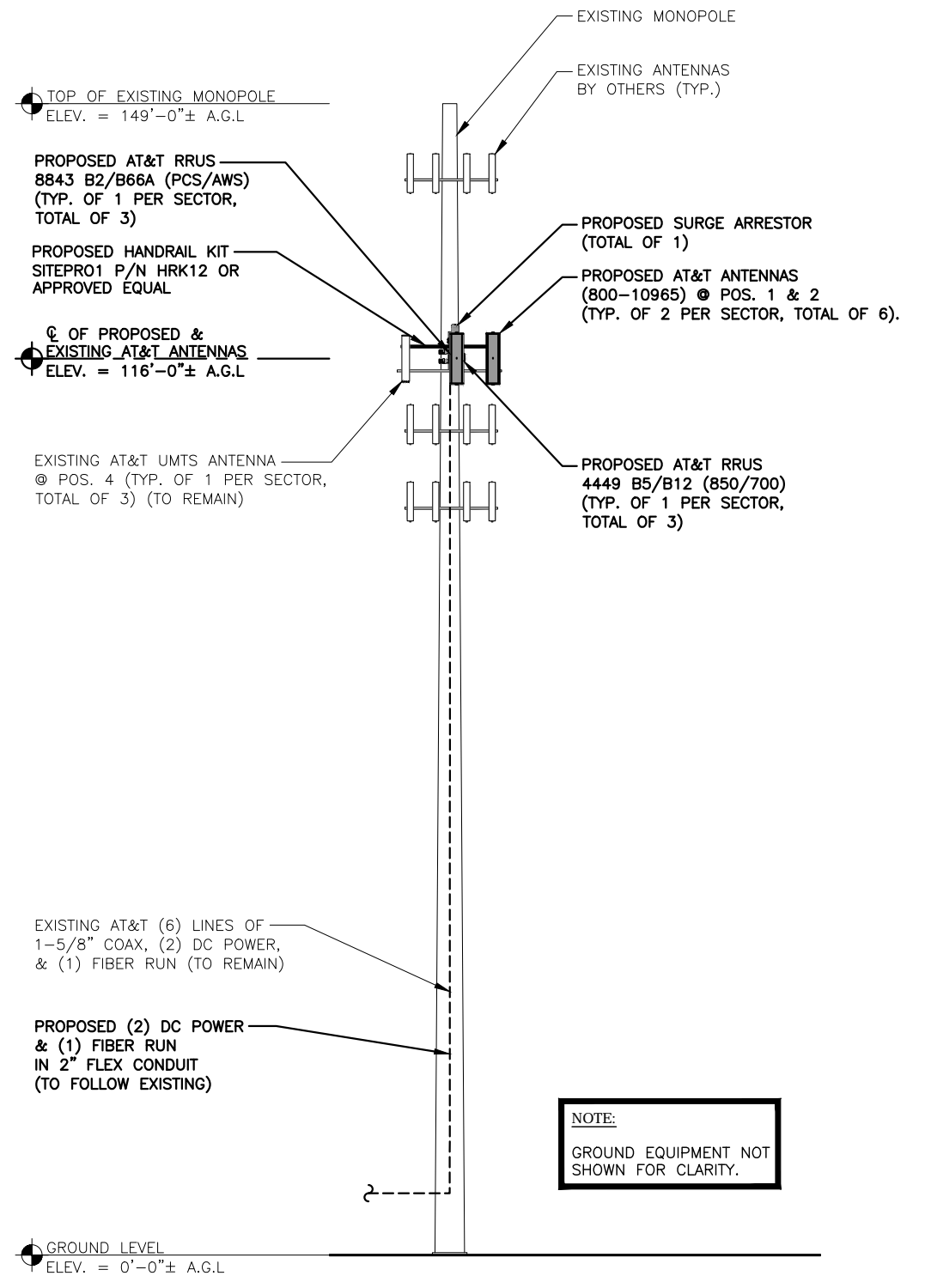


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SBA SITE ID: CT13057
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SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: JM		

AT&T
ANTENNA LAYOUTS & ELEVATION
(LTE 2C/3C/4C/4TX4RX)
SITE NUMBER: CT5432
DRAWING NUMBER: A-2
REV: 2

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ANTENNA SCHEDULE

SECTOR	EXISTING/PROPOSED	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA Q HEIGHT	AZIMUTH	TMA/DIPLEXER	RRU	SIZE (INCHES) (L x W x D)	FEEDER	RAYCAP
A1	PROPOSED	LTE 850/ /700 BC/PCS	800-10965	78.7X20X6.9	±116'-0"	30°	-	(P)(1) 8843 B2/B66A (AWS/PCS)	14.9X13.2X10.9	(2) 1-5/8 COAX (LENGTH 160' ±)	(E)(1) RAYCAP DC6-48-60-18-8C
A2	PROPOSED	LTE AWS	800-10965	78.7X20X6.9	±116'-0"	30°	-	(P)(1) 4449 B5/B12 (850/700BC)	14.9X13.2X10.4	(2) DC POWER, 1 FIBER	
A3	-	-	-	-	-	-	-	-	-	-	
A4	EXISTING	UMTS 850	7770	72X12X6	±116'-0"	110°	E)(G)(2) POWERWAVE LGP21901 E)(2) POWERWAVE LGP21401	-	-	-	
B1	PROPOSED	LTE 850/ /700 BC/PCS	800-10965	78.7X20X6.9	±116'-0"	150°	-	(P)(1) 8843 B2/B66A (AWS/PCS)	14.9X13.2X10.9	(2) 1-5/8 COAX (LENGTH 160' ±)	(P)(1) RAYCAP DC6-48-60-18-8C
B2	PROPOSED	LTE AWS	800-10965	78.7X20X6.9	±116'-0"	150°	-	(P)(1) 4449 B5/B12 (850/700BC)	14.9X13.2X10.4	(2) DC POWER, 1 FIBER	
B3	-	-	-	-	-	-	-	-	-	-	
B4	EXISTING	UMTS 850	7770	72X12X6	±116'-0"	200°	E)(G)(2) POWERWAVE LGP21901 E)(2) POWERWAVE LGP21401	-	-	-	
C1	PROPOSED	LTE 850/ /700 BC/PCS	800-10965	78.7X20X6.9	±116'-0"	270°	-	(P)(1) 8843 B2/B66A (AWS/PCS)	14.9X13.2X10.9	(2) 1-5/8 COAX (LENGTH 160' ±)	SHARED
C2	PROPOSED	LTE AWS	800-10965	78.7X20X6.9	±116'-0"	270°	-	(P)(1) 4449 B5/B12 (850/700BC)	14.9X13.2X10.4	(2) DC POWER, 1 FIBER	
C3	-	-	-	-	-	-	-	-	-	-	
C4	EXISTING	UMTS 850	7770	72X12X6	±116'-0"	300°	E)(G)(2) POWERWAVE LGP21901 E)(2) POWERWAVE LGP21401	-	-	-	

REMOVE EXISTING PIPE MAST AND INSTALL NEW 2-1/2" STD (2.88" O.D.) 8'-0" LONG PIPE MAST @ POSITION 3 SECURED TO EXISTING MOUNT (TYP. 1 PER SECTOR, TOTAL OF 3)

PROPOSED HANDRAIL KIT SITEPRO1 P/N HRK12 (OR APPROVED EQUAL)

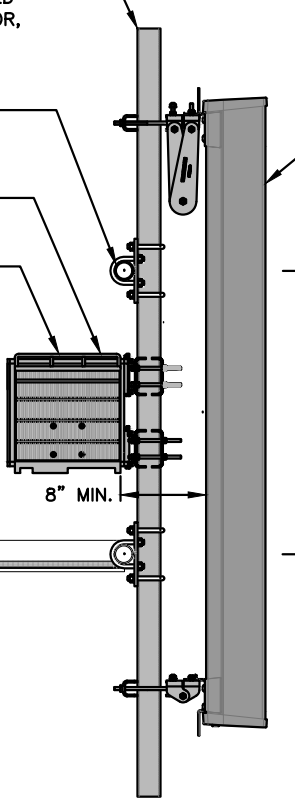
PROPOSED AT&T RRU'S (TYP. OF 2 PER SECTOR, TOTAL OF 6)

PROPOSED RRU BACK TO BACK MOUNT ERICSSON PART# SXK1250461-1 (TYP.)

PROPOSED AT&T ANTENNAS (800-10965) @ POS. 1 & 2 (TYP. OF 2 PER SECTOR, TOTAL OF 6)

Q OF PROPOSED & EXISTING AT&T ANTENNAS ELEV. = 116'-0"± A.G.L.

EXISTING SECTOR FRAME



PROPOSED LTE ANTENNA & RRH MOUNTING DETAIL

22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"

2
A-3



RRU CHART				
QUANTITY	MODEL	L	W	D
3(P)	4449	14.9"	13.2"	10.4"
3(P)	8843	14.9"	13.2"	10.9"

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS

NOTE:

SEE RFDS FOR RRH FREQUENCY AND MODEL NUMBER

PROPOSED RRU REFER TO THE FINAL RFDS AND CHART FOR QUANTITY, MODEL AND DIMENSIONS

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

PROPOSED RRUS DETAIL

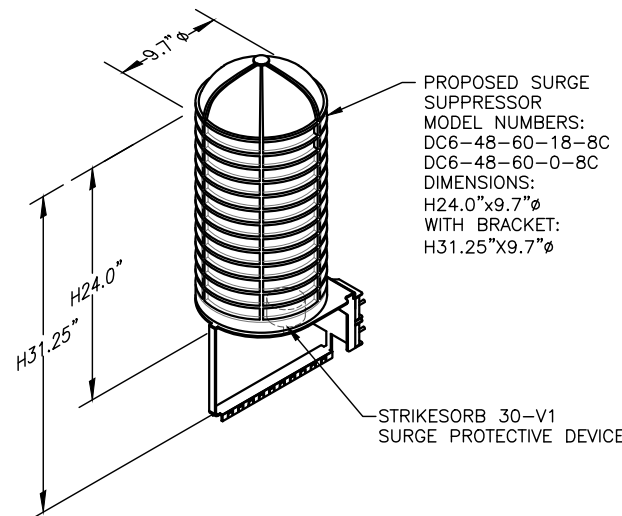
SCALE: N.T.S

3
A-3

FINAL ANTENNA SCHEDULE

SCALE: N.T.S

1
A-3



PROPOSED SURGE SUPPRESSOR MODEL NUMBERS: DC6-48-60-18-8C DC6-48-60-0-8C DIMENSIONS: H24.0"x9.7"φ WITH BRACKET: H31.25"x9.7"φ

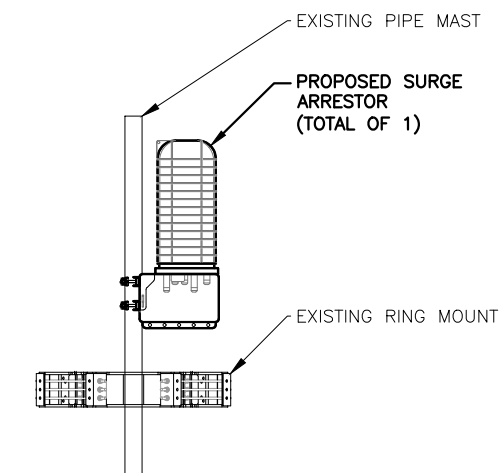
STRIKESORB 30-V1 SURGE PROTECTIVE DEVICE

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

DC SURGE SUPPRESSOR DETAIL

SCALE: N.T.S

4
A-3



PROPOSED SURGE ARRESTOR MOUNTING DETAIL

SCALE: N.T.S

5
A-3



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500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067

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2	05/14/19	ISSUED FOR CONSTRUCTION	HC	A	DJC
1	04/24/19	ISSUED FOR REVIEW	RP	AT	DJC
A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: JM



AT&T

DETAILS (LTE 2C/3C/4C/4TX4RX)

SITE NUMBER: CT5432 DRAWING NUMBER: A-3 REV: 2

STRUCTURAL NOTES:

- DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE SUPPLEMENTS, INTERNATIONAL BUILDING CODE, EIA/TIA-222-G STRUCTURAL STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. ANY UNUSUAL CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS".
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A36 UNLESS OTHERWISE INDICATED.
- STEEL PIPE SHALL CONFORM TO ASTM A500 "COLD-FORMED WELDED & SEAMLESS CARBON STEEL STRUCTURAL TUBING", GRADE B, OR ASTM A53 PIPE STEEL BLACK AND HOT-DIPPED ZINC-COATED WELDED AND SEAMLESS TYPE E OR S, GRADE B. PIPE SIZES INDICATED ARE NOMINAL. ACTUAL OUTSIDE DIAMETER IS LARGER.
- STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA UON.
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS OTHERWISE NOTED.
- ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS OTHERWISE NOTED.
- FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT COMPLYING WITH REQUIREMENTS OF ASTM A780. GALVANIZING REPAIR PAINT SHALL HAVE 65 PERCENT ZINC BY WEIGHT, ZIRP BY DUNCAN GALVANIZING, GALVA BRIGHT PREMIUM BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 OR A153 AS APPLICABLE.
- CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D.I. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "STEEL CONSTRUCTION MANUAL". 14TH EDITION.
- INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON-CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL.
- UNISTRUT SHALL BE FORMED STEEL CHANNEL STRUT FRAMING AS MANUFACTURED BY UNISTRUT CORP., WAYNE, MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA, UNLESS OTHERWISE NOTED, AND SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION.
- EPOXY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS & WASHERS. AN INTERNALLY THREADED INSERT, A SCREEN TUBE AND A EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HILTI-HIT HY-270 AND OR HY-200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS I, HILTI KWIK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT.
- ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL. ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE.

THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE PROJECT ARE PERMITTED TO ACT AS THE APPROVED AGENCY AND THEIR PERSONNEL ARE PERMITTED TO ACT AS THE SPECIAL INSPECTOR FOR THE WORK DESIGNED BY THEM, PROVIDED THOSE PERSONNEL MEET THE QUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE. THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705.

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. REPORTS SHALL INDICATE THAT WORK INSPECTED WAS OR WAS NOT COMPLETED IN CONFORMANCE TO APPROVED CONSTRUCTION DOCUMENTS. DISCREPANCIES SHALL BE BROUGHT TO THE IMMEDIATE ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED.

SPECIAL INSPECTION CHECKLIST	
BEFORE CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	ENGINEER OF RECORD APPROVED SHOP DRAWINGS ¹
N/A	MATERIAL SPECIFICATIONS REPORT ²
N/A	FABRICATOR NDE INSPECTION
N/A	PACKING SLIPS ³
ADDITIONAL TESTING AND INSPECTIONS:	
DURING CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	STEEL INSPECTIONS
N/A	HIGH STRENGTH BOLT INSPECTIONS
N/A	HIGH WIND ZONE INSPECTIONS ⁴
N/A	FOUNDATION INSPECTIONS
N/A	CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT
N/A	POST INSTALLED ANCHOR VERIFICATION ⁵
N/A	GROUT VERIFICATION
N/A	CERTIFIED WELD INSPECTION
N/A	EARTHWORK: LIFT AND DENSITY
N/A	ON SITE COLD GALVANIZING VERIFICATION
N/A	GUY WIRE TENSION REPORT
ADDITIONAL TESTING AND INSPECTIONS:	
AFTER CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	MODIFICATION INSPECTOR REDLINE OR RECORD DRAWINGS ⁶
N/A	POST INSTALLED ANCHOR PULL-OUT TESTING
REQUIRED	PHOTOGRAPHS
ADDITIONAL TESTING AND INSPECTIONS:	

NOTES:

- REQUIRED FOR ANY NEW SHOP FABRICATED FRP OR STEEL.
- PROVIDED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH BOLTS OR STEEL.
- PROVIDED BY GENERAL CONTRACTOR; PROOF OF MATERIALS.
- HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C,D 110MPH INSPECT FRAMING OF WALLS, ANCHORING, FASTENING SCHEDULE.
- ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ACI 355.4 AND ICC-ES AC308 FOR CRACKED CONCRETE AND SEISMIC APPLICATIONS. DESIGN ADHESIVE BOND STRENGTH HAS BEEN BASED ON ACI 355.4 TEMPERATURE CATEGORY B WITH INSTALLATIONS INTO DRY HOLES DRILLED USING A CARBIDE BIT INTO CRACKED CONCRETE THAT HAS CURED FOR AT LEAST 21 DAYS. ADHESIVE ANCHORS REQUIRING CERTIFIED INSTALLATIONS SHALL BE INSTALLED BY A CERTIFIED ADHESIVE ANCHOR INSTALLER PER ACI 318-11 D.9.2.2. INSTALLATIONS REQUIRING CERTIFIED INSTALLERS SHALL BE INSPECTED PER ACI 318-11 D.8.2.4.
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

NOTES:

- ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4"Ø A325-X BOLTS, UNLESS OTHERWISE NOTIFIED.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED BEFORE ORDERING MATERIAL.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
- VERIFICATION OF EXISTING ROOF CONSTRUCTION IS REQUIRED PRIOR TO THE INSTALLATION OF THE ROOF PLATFORM. ENGINEER OF RECORD IS TO APPROVE EXISTING CONDITIONS IN ORDER TO MOVE FORWARD.
- CENTERLINE OF PROPOSED STEEL PLATFORM SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- EXISTING BRICK MASONRY COLUMNS/BEARING TO BE REPAIRED/REPLACED AT ALL PROPOSED PLATFORM SUPPORT POINTS. ENGINEER OF RECORD TO REVIEW AND APPROVE.

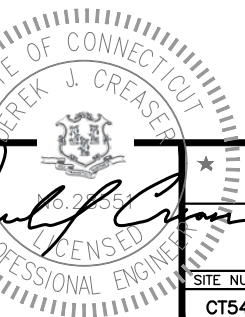
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

750 WEST CENTER STREET., SUITE #301
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT5432
SITE NAME: NEWTOWN EAST CENTRAL
SBA SITE ID: CT13057
151 BERKSHIRE ROAD
SANDY HOOK, CT 06482
FAIRFIELD COUNTY

500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06067

2	05/14/19	ISSUED FOR CONSTRUCTION	HC	A	DJC
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A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: JM		



AT&T
STRUCTURAL NOTES
(LTE 2C/3C/4C/4TX4RX)

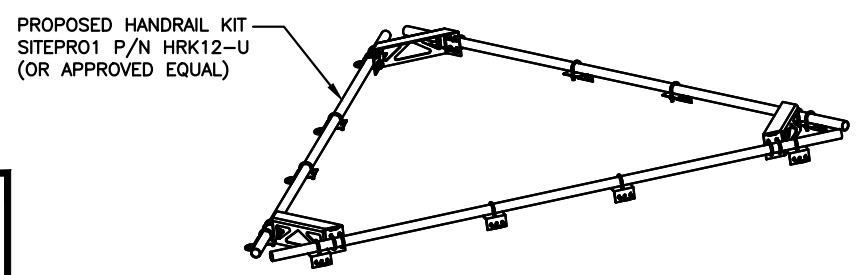
SITE NUMBER	DRAWING NUMBER	REV
CT5432	SN-1	2

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION

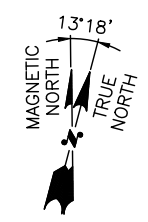
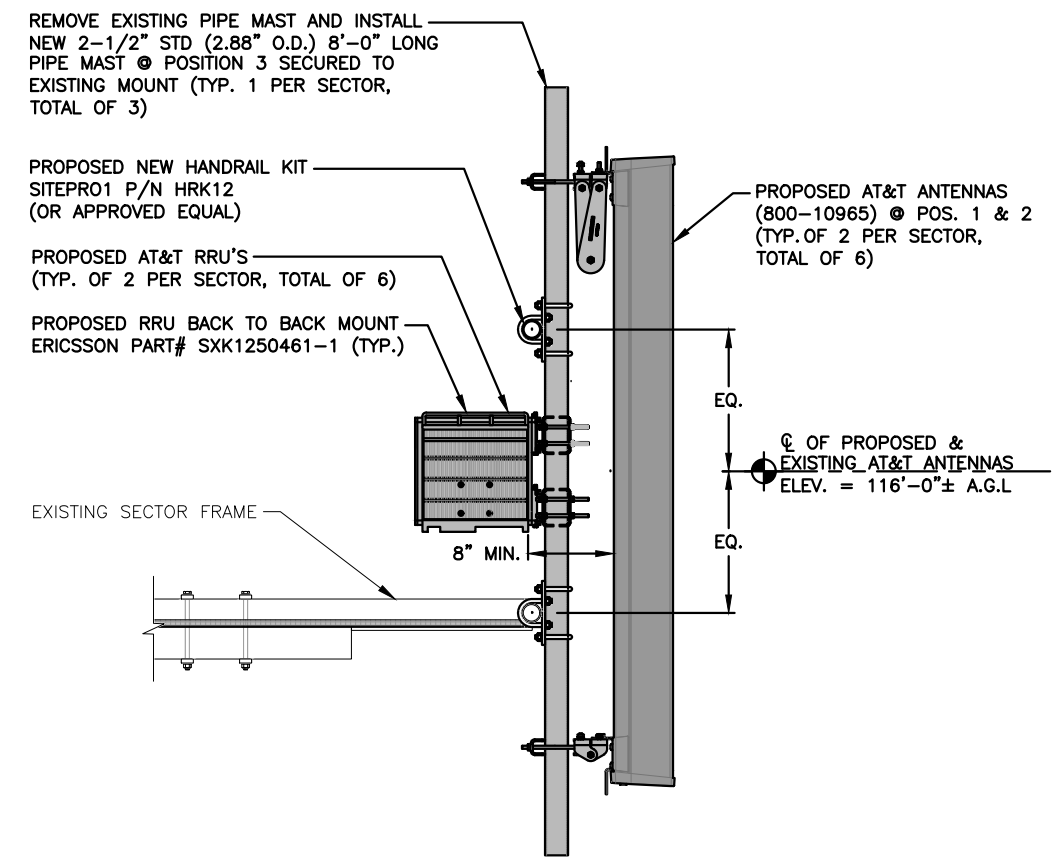
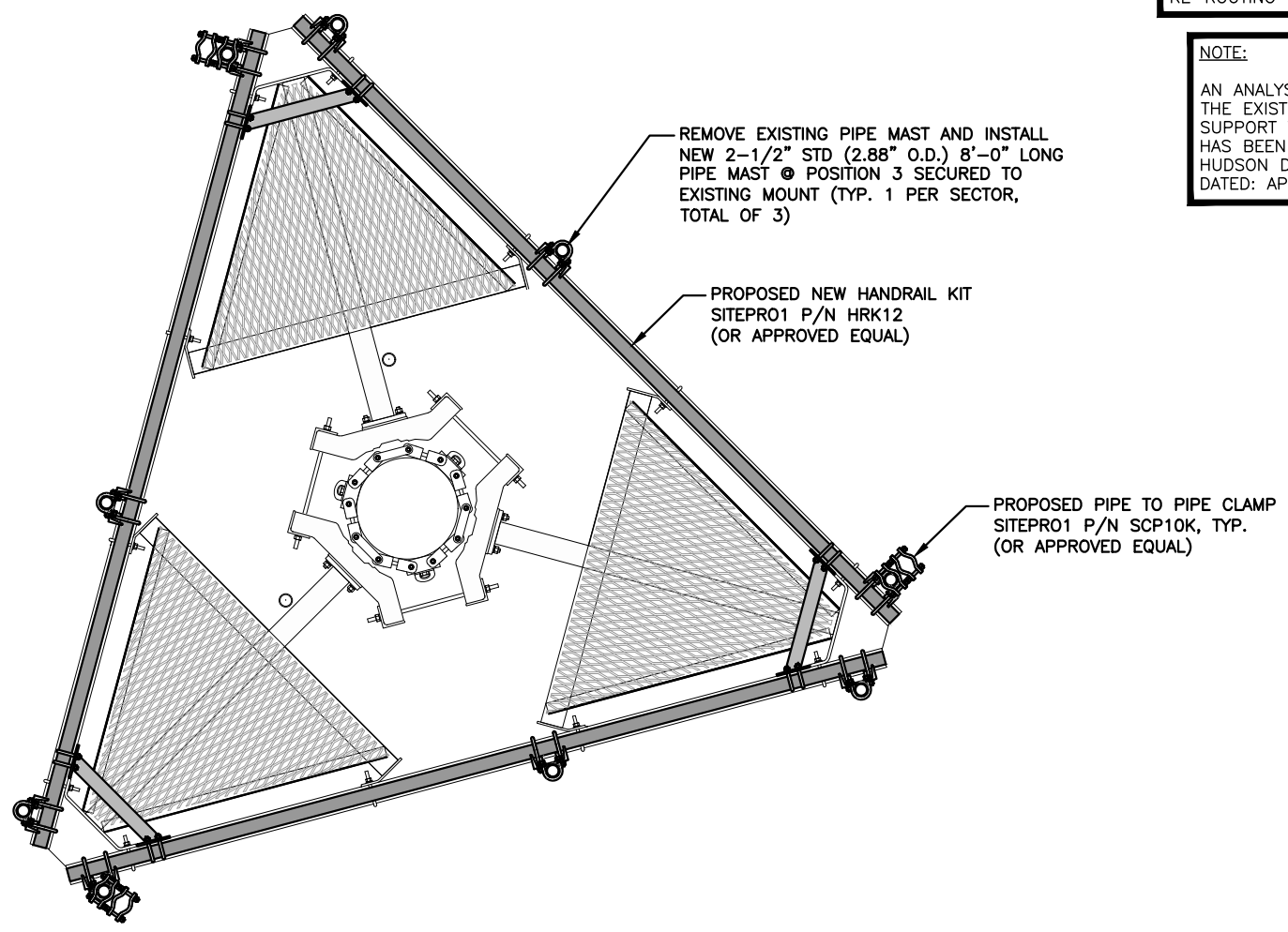
NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
ROTATION OF MOUNTS OR INSTALLATION OF MOUNT MODS MUST NOT ADVERSELY AFFECT, OBSTRUCT, BEND OR PINCH EXISTING SAFETY CABLE IN ANY WAY. GC, C/O AT&T, WILL PURCHASE AND INSTALL CABLE RE-ROUTING BRACKETS AS REQUIRED.

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: APRIL 22, 2019



PROPOSED HANDRAIL KIT
SCALE: N.T.S. 3
S-1



PROPOSED MOUNT MODIFICATIONS PLAN 1
S-1
22x34 SCALE: 3/4"=1'-0"
11x17 SCALE: 3/8"=1'-0"



PROPOSED LTE ANTENNA & RRH MOUNTING DETAIL 2
S-1
22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"



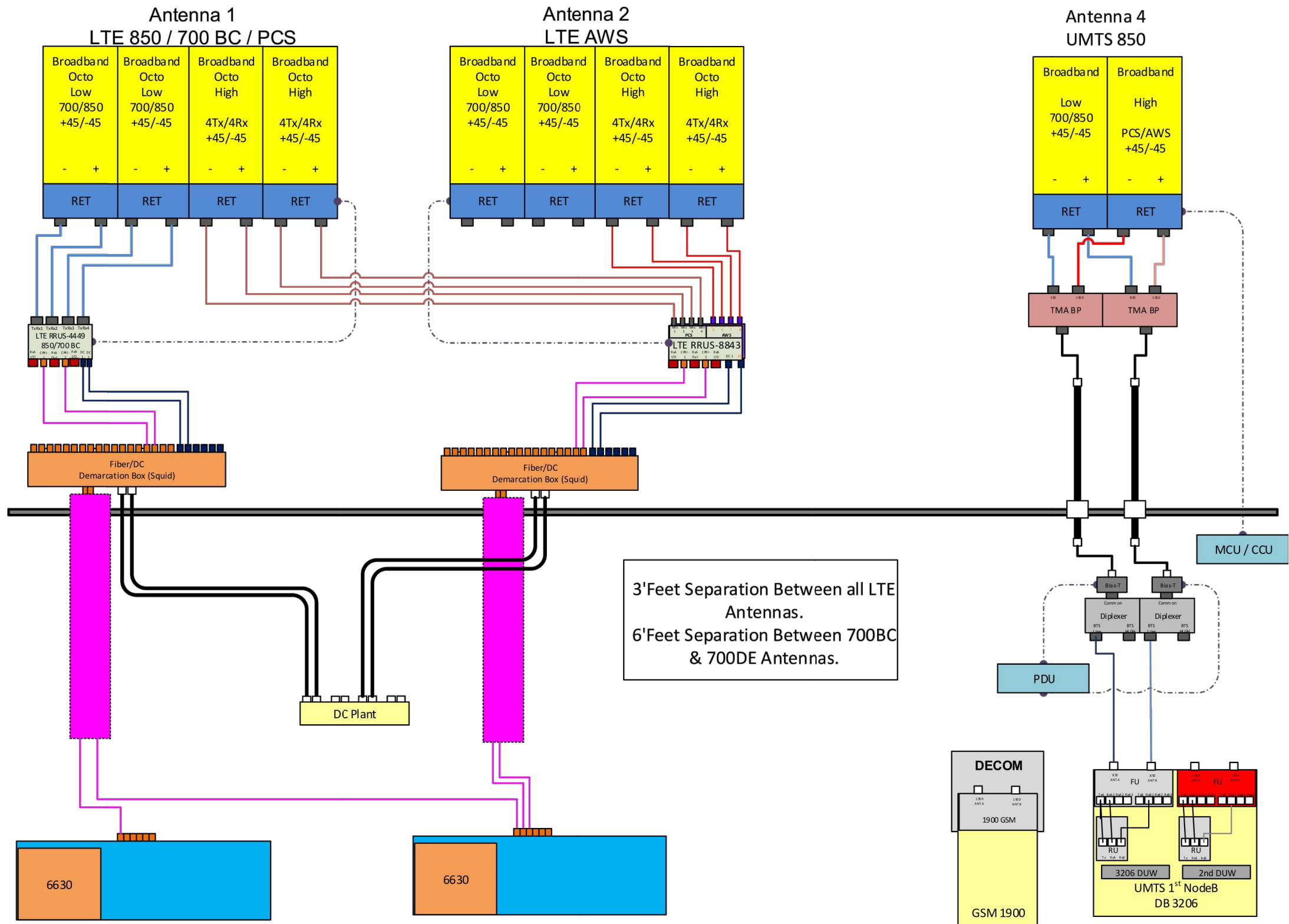
HG HUDSON
Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

CENTERLINE
COMMUNICATIONS
750 WEST CENTER STREET., SUITE #301
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT5432
SITE NAME: NEWTOWN EAST CENTRAL
SBA SITE ID: CT13057
151 BERKSHIRE ROAD
SANDY HOOK, CT 06482
FAIRFIELD COUNTY

at&t
500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06067

				AT&T			
				MOUNT MODIFICATION DESIGN (LTE 2C/3C/4C/4TX4RX)			
NO.	DATE	REVISIONS	BY	CHK	APP'D	SITE NUMBER	DRAWING NUMBER
2	05/14/19	ISSUED FOR CONSTRUCTION	HC	AT	DJC	CT5432	S-1
1	04/24/19	ISSUED FOR REVIEW	RP	AT	DJC		
A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC		
SCALE: AS SHOWN				DESIGNED BY: AT		DRAWN BY: JM	
							2



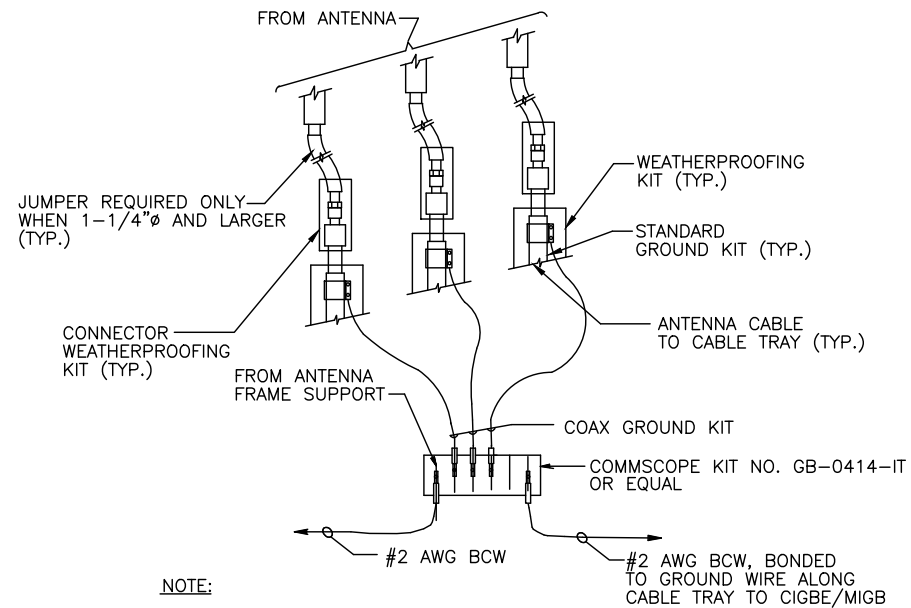
3' Feet Separation Between all LTE Antennas.
6' Feet Separation Between 700BC & 700DE Antennas.

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS.
2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS

NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

RF PLUMBING DIAGRAM 1
SCALE: N.T.S. RF-1

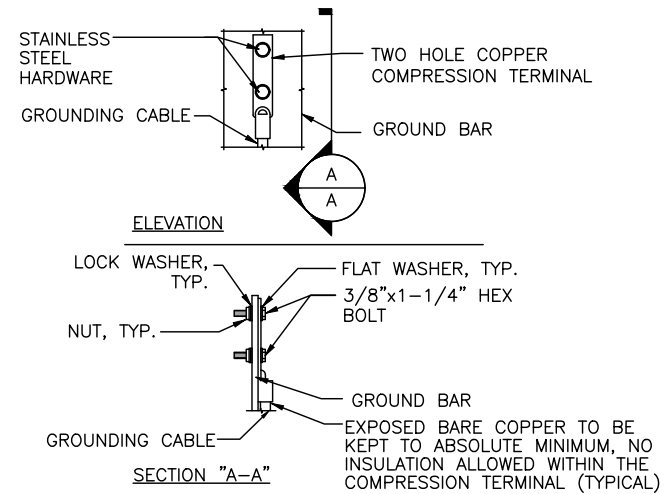
<p>45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845 TEL: (978) 557-5553 FAX: (978) 336-5586</p>	<p>750 WEST CENTER STREET., SUITE #301 WEST BRIDGEWATER, MA 02379</p>	<p>SITE NUMBER: CT5432 SITE NAME: NEWTOWN EAST CENTRAL SBA SITE ID: CT13057</p> <p>151 BERKSHIRE ROAD SANDY HOOK, CT 06482 FAIRFIELD COUNTY</p>	<p>500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067</p>	<table border="1"> <tr> <th>NO.</th> <th>DATE</th> <th>REVISIONS</th> <th>BY</th> <th>CHK</th> <th>APP'D</th> </tr> <tr> <td>2</td> <td>05/14/19</td> <td>ISSUED FOR CONSTRUCTION</td> <td>HC</td> <td>AT</td> <td>DJC</td> </tr> <tr> <td>1</td> <td>04/24/19</td> <td>ISSUED FOR REVIEW</td> <td>RP</td> <td>AT</td> <td>DJC</td> </tr> <tr> <td>A</td> <td>04/12/19</td> <td>ISSUED FOR REVIEW</td> <td>JM</td> <td>AT</td> <td>DJC</td> </tr> </table>	NO.	DATE	REVISIONS	BY	CHK	APP'D	2	05/14/19	ISSUED FOR CONSTRUCTION	HC	AT	DJC	1	04/24/19	ISSUED FOR REVIEW	RP	AT	DJC	A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC		<p>AT&T</p> <p>RF PLUMBING DIAGRAM (LTE 2C/3C/4C/4TX4RX)</p>	<p>SITE NUMBER</p> <p>CT5432</p>	<p>DRAWING NUMBER</p> <p>RF-1</p>	<p>REV</p> <p>2</p>
					NO.	DATE	REVISIONS	BY	CHK	APP'D																							
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A	04/12/19	ISSUED FOR REVIEW	JM	AT	DJC																												
<p>SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: JM</p>																																	



NOTE:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

GROUND WIRE TO GROUND BAR CONNECTION DETAIL

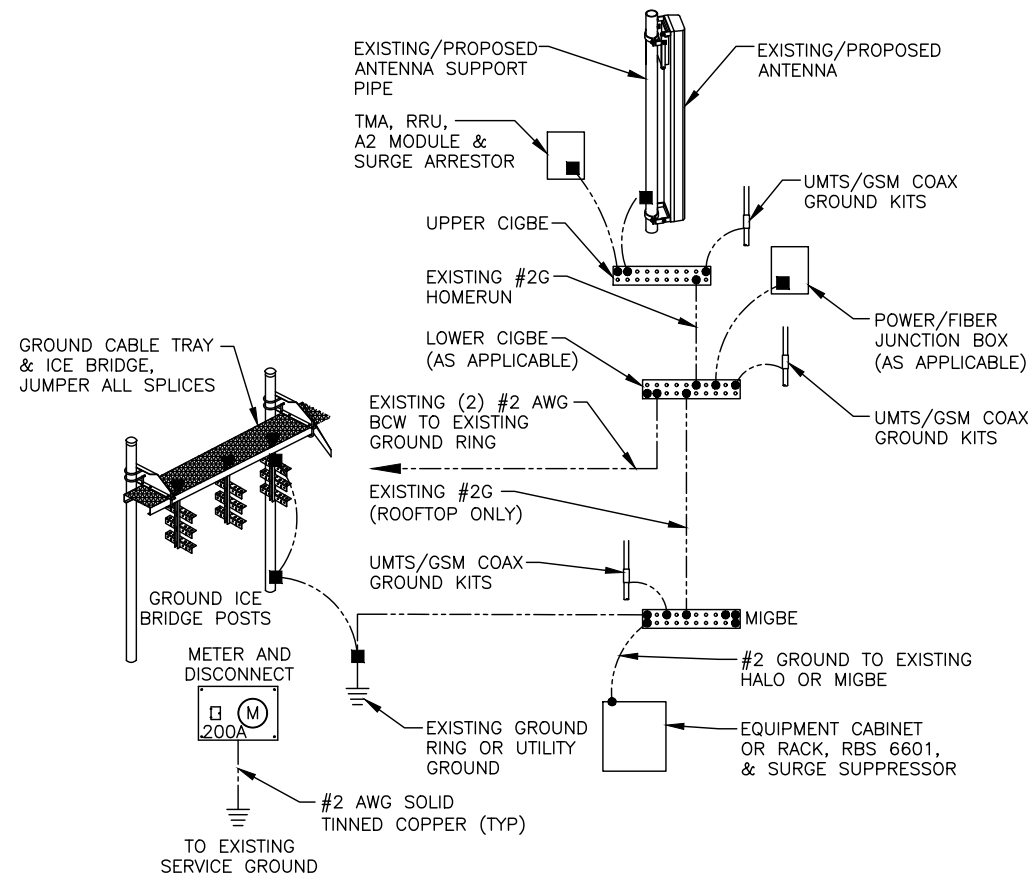
SCALE: N.T.S



NOTE:
 1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL

SCALE: N.T.S



GROUNDING RISER DIAGRAM

SCALE: N.T.S



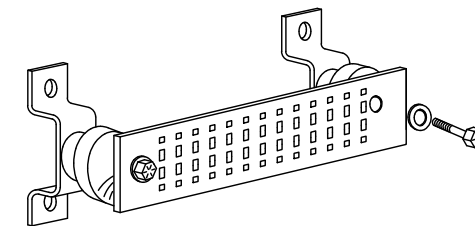
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

- CABLE ENTRY PORTS (HATCH PLATES) (#2)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
- +24V POWER SUPPLY RETURN BAR (#2)
- 48V POWER SUPPLY RETURN BAR (#2)
- RECTIFIER FRAMES.

SECTION "A" - SURGE ABSORBERS

- INTERIOR GROUND RING (#2)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
- BUILDING STEEL (IF AVAILABLE) (#2)



GROUND BAR - DETAIL

SCALE: N.T.S



				AT&T	
				GROUNDING DETAILS (LTE 2C/3C/4C/4TX4RX)	
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SCALE: AS SHOWN		DESIGNED BY: AT		DRAWN BY: JM	
SITE NUMBER			DRAWING NUMBER		REV
CT5432			G-1		2



Radio Frequency Emissions Analysis Report

AT&T Existing Facility

Site ID: CT5432

Newtown East Central
151 Berkshire Road

Sandy Hook, CT 06482

June 28, 2019

Centerline Communications Project Number: 950012-229

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	9.56 %



June 28, 2019

AT&T Mobility – New England
Attn: John Benedetto, RF Manager
550 Cochituate Road
Suite 550 – 13&14
Framingham, MA 06040

Emissions Analysis for Site: **CT5432 – Newtown East Central**

Centerline Communications, LLC (“Centerline”) was directed to analyze the proposed AT&T facility located at **151 Berkshire Road in Sandy Hook, Connecticut** for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 700 and 850 MHz Bands are approximately $467 \mu\text{W}/\text{cm}^2$ and $567 \mu\text{W}/\text{cm}^2$ respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



CALCULATIONS

Calculations were performed for the proposed AT&T Wireless antenna facility located at **151 Berkshire Road in Sandy Hook, Connecticut**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
UMTS	850 MHz	2	30
5G	850 MHz	2	25
LTE	850 MHz	2	40
LTE	700 MHz	2	40
LTE	2100 MHz (AWS)	4	30
LTE	1900 MHz (PCS)	4	40

Table 1: Channel Data Table



The following antennas listed in Table 2 were used in the modeling for transmission in the 700 MHz, 850 MHz, 1900 MHz (PCS), and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

Sector	Antenna Number	Antenna Make / Model	Antenna Centerline (ft)
A	1	Kathrein 800-10965	116
A	2	Kathrein 800-10965	116
A	3	Powerwave 7770	116
B	1	Kathrein 800-10965	116
B	2	Kathrein 800-10965	116
B	3	Powerwave 7770	116
C	1	Kathrein 800-10965	116
C	2	Kathrein 800-10965	116
C	3	Powerwave 7770	116

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.



RESULTS

Per the calculations completed for the proposed AT&T configurations *Table 3* shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

Antenna ID	Antenna Make / Model	Frequency Bands	Antenna Gain (dBd)	Channel Count	Total TX Power	ERP (W)	MPE %
Antenna A1	Kathrein 800-10965	700 MHz / 850 MHz / 1900 MHz / 1900 MHz / 850 MHz	12.65 dBd / 13.45 dBd / 15.65 dBd / 15.65 dBd / 13.45 dBd	14	530	16,102.67	5.34
Antenna A2	Kathrein 800-10965	2100 MHz	15.95 dBd	4	120	4,722.60	1.26
Antenna A3	Powerwave 7770	850 MHz	11.5 dBd	2	60	847.52	0.40
Sector A Composite MPE%							7.00
Antenna B1	Kathrein 800-10965	700 MHz / 850 MHz / 1900 MHz / 1900 MHz / 850 MHz	12.65 dBd / 13.45 dBd / 15.65 dBd / 15.65 dBd / 13.45 dBd	14	530	16,102.67	5.34
Antenna B2	Kathrein 800-10965	2100 MHz	15.95 dBd	4	120	4,722.60	1.26
Antenna B3	Powerwave 7770	850 MHz	11.5 dBd	2	60	847.52	0.40
Sector B Composite MPE%							7.00
Antenna C1	Kathrein 800-10965	700 MHz / 850 MHz / 1900 MHz / 1900 MHz / 850 MHz	12.65 dBd / 13.45 dBd / 15.65 dBd / 15.65 dBd / 13.45 dBd	14	530	16,102.67	5.34
Antenna C2	Kathrein 800-10965	2100 MHz	15.95 dBd	4	120	4,722.60	1.26
Antenna C3	Powerwave 7770	850 MHz	11.5 dBd	2	60	847.52	0.40
Sector C Composite MPE%							7.00

Table 3: AT&T Emissions Levels



The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. *Table 5* below shows a summary for each AT&T Sector as well as the composite MPE value for the site.

Site Composite MPE%	
Carrier	MPE%
AT&T – Max Per Sector Value	7.00%
Sprint	0.02%
T-Mobile	1.18%
Town	0.17%
Verizon	1.19%
Site Total MPE %:	9.56 %

Table 4: All Carrier MPE Contributions

AT&T Sector A Total:	7.00	%
AT&T Sector B Total:	7.00	%
AT&T Sector C Total:	7.00	%
Site Total:	9.56	%

Table 5: Site MPE Summary



FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT&T sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

AT&T _ Frequency Band / Technology Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (i.tW/cm ²)	Frequency (MHz)	Allowable MPE (i.tW/cm ²)	Calculated % MPE
AT&T 700 MHz LTE	2	736.31	116.0	3.93	700 MHz LTE	467	0.84%
AT&T 850 MHz LTE	2	885.24	116.0	4.73	850 MHz LTE	567	0.83%
AT&T 1900 MHz LTE	4	1469.13	116.0	15.70	1900 MHz LTE	1000	1.57%
AT&T 1900 MHz LTE	4	1469.13	116.0	15.70	1900 MHz LTE	1000	1.57%
AT&T 850 MHz 5G	2	553.27	116.0	2.96	850 MHz 5G	567	0.52%
AT&T 2100 MHz LTE AWS	4	1180.65	116.0	12.62	2100 MHz LTE AWS	1000	1.26%
AT&T 850 MHz UMTS	2	423.76	116.0	2.26	850 MHz UMTS	567	0.40%
						Total:	7.00%

Table 6: AT&T Maximum Sector MPE Power Values



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

AT&T Sector	Power Density Value (%)
Sector A:	7.00 %
Sector B:	7.00 %
Sector C:	7.00 %
AT&T Maximum Total (per sector):	7.00 %
Site Total:	9.56 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **9.56 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

A handwritten signature in black ink that reads 'Ryan B. McManus'.

Ryan McManus
Senior RF EME Compliance Manager
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767

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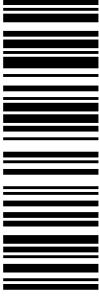
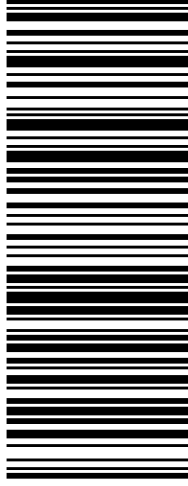

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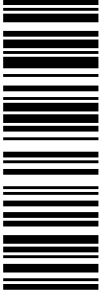
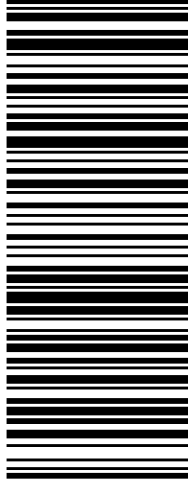

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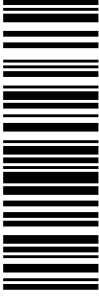


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