

Northeast Site Solutions Denise Sabo 4 Angela's Way, Burlington CT 06013 203-435-3640 denise@northeastsitesolutions.com

March 31, 2021

Members of the Siting Council Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification

25 Lower Boulevard, New London CT 06320

Latitude: 41.32247500 Longitude: -72.09370000

T-Mobile Site#: CTNL041A\_L600\_Anchor\_L1900

## Dear Ms. Bachman:

T-Mobile currently maintains six (6) antennas at the 59-foot level of the existing 60-foot self-support tower at 25 Lower Boulevard, New London CT 06320. The 60-foot self-support tower and property are both owned by The City of New London. T-Mobile now intends to replace six (6) of its existing antennas with three (3) new antenna 1900/2100 MHz antenna, and three (3) new 2500 MHz antenna. T-Mobile also intends to add three (3) new 600/700/1900 MHz antenna. The new antennas would be installed at the 59-foot and 57-foot level of the tower. T-Mobile is also proposing tower mount reinforcements, and tower modifications from the 5-ft -25-ft level of the support tower. See attached modification plan.

## Planned Modifications:

Remove:

- (12) 7/8" Coax
- (1) Hybrid Line
- (3) Twin Style 1B- AWS

# Remove and Replace:

- (3) Air21 B2P B4A Antenna (Remove) (3) Air32 B66A B2A- 1900/2100 MHz Antenna (Replace)
- (3) Air21 B2A B12P (Remove) (3) Air6449 B41- 2500 MHz 5G Antenna (Replace)
- (3) RRUS11 B12 (Remove) (3) Radio 4449 B71+B85 (Replace)

## Install New:

- $(3) \ RFS \ APXVAALL24\_43-U-NA20-600/700/1900/2100 \ MHz \ 5G \ Antenna$
- (2) Hybrid Line
- (3) Radio 4415 B25

Mount Stiff Arm Kit (STK-U)

## Existing to Remain:

(1) Hybrid line



Ground Work:

- (1) AAV Cabinet
- (1) BBU
- (1) 6160 Radio Cabinet

This facility was approved by the CT Siting Council TS- T-MOBILE-095-060929—on October 17, 2006. T-Mobile tower share was approved to install three (3) antenna on the existing tower. Please see attached.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16- SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-SOj-73, a copy of this letter is being sent to Mayor Michael Passero, Steven Fields, Chief Administrative Officer, Felix J. Reyes, Director of the Office of Development & Planning, Thomas J. Curcio, Fire Chief.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Victoria Masse

Mobile: 860-306-2326 Fax: 413-521-0558

Office: 420 Main Street, Unit 2, Sturbridge MA 01566

Email: victoria@northeastsitesolutions.com



Attachments cc: Mayor Michael Passero New London City Hall 181 State Street New London, CT 06320

Steven Fields- Chief Administrative Officer New London City Hall 181 State Street New London, CT 06320

Felix J. Reyes- Director of the Office of Development & Planning New London City Hall 181 State Street New London, CT 06320

Thomas J. Curcio- Fire Chief New London Fire Department Headquarters 289 Bank Street New London, CT 06320

# Exhibit A



Daniel F. Caruso
Chairman
October 17, 2006

# STATE OF CONNECTICUT

# CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov Internet: ct.gov/csc

Karina Fournier Zoning Dept. T-Mobile 30 Cold Springs Road Rocky Hill, CT 06067

RE:

TS-T-MOBILE-095-060929 - Omnipoint Communications, Inc. request for an order to approve tower sharing at an approved telecommunications facility located at 25 Lower Boulevard, New London, Connecticut.

## Dear Ms. Fournier:

At a public meeting held October 10, 2006, the Connecticut Siting Council (Council) ruled that the shared use of this tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility to avoid the unnecessary proliferation of tower structures. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Any additional change to this facility may require an explicit request to this agency pursuant to General Statutes § 16-50a or notice pursuant to Regulations of Connecticut State Agencies Section 16-50j-73, as applicable. Such request or notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

This decision applies only to this request for tower sharing and is not applicable to any other request or construction. Please be advised that the validity of this action shall expire one year from the date of this letter.

The proposed shared use is to be implemented as specified in your letter dated September 29, 2006, including the placement of all necessary equipment and shelters within the tower compound.

Thank you for your attention and cooperation.

Very truly yours,

Daniel F. Caruso

Chairman

DFC/MP/laf

c: The Honorable Elizabeth Sabilia, Mayor, City of New London Michelle J. Greiner, Zoning Enforcement Officer, City of New London



# Exhibit B

# **LOWER BLVD**

Location LOWER BLVD City, State, Zip

**Mblu** G23/41/36// **Acct#** G23 0041 0036

Owner NEW LONDON CITY OF-LOW Assessment \$794,080

**Appraisal** \$1,134,400 **PID** 1088

**Building Count** 1

## **Current Value**

Appraisal					
Valuation Year Improvements Land Total					
2018	\$956,900	\$177,500	\$1,134,400		
	Assessment				
Valuation Year Improvements Land Total					
2018	\$669,830	\$124,250	\$794,080		

# **Owner of Record**

 Owner
 NEW LONDON CITY OF-LOW
 Sale Price
 \$0

 Co-Owner
 Certificate

Address 181 STATE ST Book & Page 0446/0303

NEW LONDON, CT 06320 Sale Date 01/01/1700

Instrument

# **Ownership History**

Ownership History					
Owner Sale Price Certificate Book & Page Instrument Sale Date					
NEW LONDON CITY OF-LOW	\$0		0446/0303		01/01/1700

# **Building Information**

# **Building 1: Section 1**

 Year Built:
 1979

 Living Area:
 7,206

 Replacement Cost:
 \$1,230,946

**Building Percent Good:** 77

# **Replacement Cost**

Less Depreciation: \$947,800

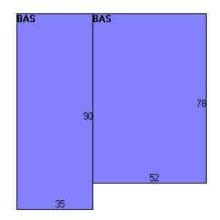
Less Depreciation:	Less Depreciation: \$947,800			
	Building Attributes			
Field	Description			
STYLE	Fire Station			
MODEL	Ind/Lg UnfinCM			
Grade	Above Ave			
Stories:	1			
Occupancy	1.00			
Exterior Wall 1	Brick/Masonry			
Exterior Wall 2				
Roof Structure	Steel Frm/Trus			
Roof Cover	Tar & Gravel			
Interior Wall 1	Minim/Masonry			
Interior Wall 2	Drywall/Sheet			
Interior Floor 1	Concr-Finished			
Interior Floor 2	Vinyl/Asphalt			
Heating Fuel	Gas			
Heating Type	Hot Water			
AC Type	None			
Struct Class				
Bldg Use	MUN FIRE MDL-96			
Total Rooms				
Total Bedrms	00			
Total Baths	0			
Conv Type				
Usrfld 219				
1st Floor Use:	903K			
Heat/AC	NONE			
Frame Type	STEEL			
Baths/Plumbing	AVERAGE			
Ceiling/Wall	CEIL & WALLS			
Rooms/Prtns	AVERAGE			
Wall Height	16.00			
% Comn Wall	0.00			

# **Building Photo**



(http://images.vgsi.com/photos/NewLondonCTPhotos/\\00\\01\18\37.jpg)

# **Building Layout**



 $(http://images.vgsi.com/photos/NewLondonCTPhotos//Sketches/1088\_110) \\$ 

Building Sub-Areas (sq ft)			<u>Legend</u>
Code Description		Gross Area	Living Area
BAS	First Floor	7,206	7,206
		7,206	7,206

# **Extra Features**

Extra Features	Legend
No Data for Extra Features	

## Land

## Land Use Land Line Valuation

Use Code 903K

Description MUN FIRE MDL-96

Zone R-1 Neighborhood EX1 Alt Land Appr No

Category

and Line valuation

 Size (Acres)
 0.36

 Frontage
 0

 Depth
 0

**Assessed Value** \$124,250 **Appraised Value** \$177,500

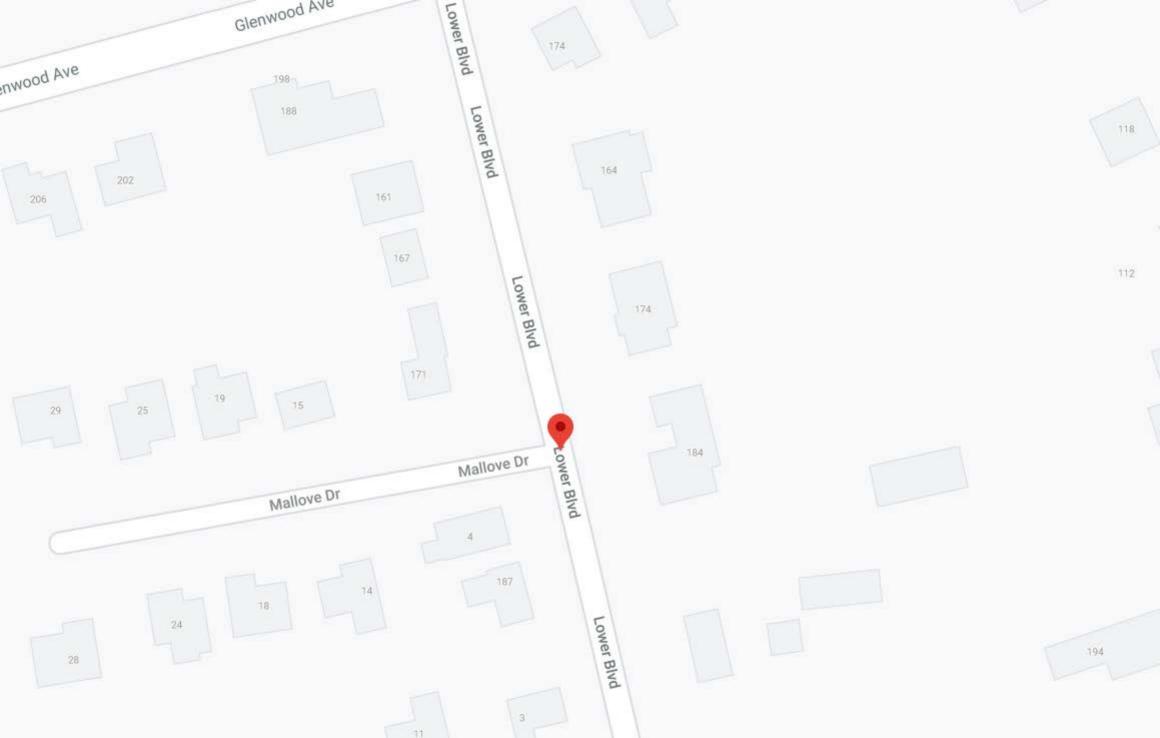
# Outbuildings

	Outbuildings <u>I</u>					
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
PAV1	PAVING-ASPHALT			3000.00 S.F.	\$4,500	1
SHD1	SHED FRAME			48.00 S.F.	\$400	1
PAV2	PAVING-CONC			1850.00 S.F.	\$4,200	1

# **Valuation History**

Appraisal				
Valuation Year	Land	Total		
2019	\$956,900	\$177,500	\$1,134,400	
2018	\$956,900	\$177,500	\$1,134,400	
2017	\$870,600	\$177,500	\$1,048,100	

Assessment				
Valuation Year Improvements Land Total				
2019	\$669,830	\$124,250	\$794,080	
2018	\$669,830	\$124,250	\$794,080	
2017	\$609,420	\$124,250	\$733,670	



# Exhibit C

# T··Mobile·

# T-MOBILE NORTHEAST LLC

PROJECT TITLE: ANCHOR

SITE NUMBER: CTNL041A

SITE NAME: NL041GARDNER-NEW LONDON

SITE ADDRESS: 25 LOWER BLVD.

NEW LONDON, CT 06230

67D5997DB\_2XAIR+1OP (U21 MARKET)

# **PROJECT NOTES:**

THIS IS AN UNMANNED TELECOMMUNICATION FACILITY AND NOT FOR HUMAN HABITATION:

HANDICAPPED ACCESS IS NOT REQUIRED. POTABLE WATER OR SANITARY SERVICE IS NOT REQUIRED. NO OUTDOOR STORAGE OR ANY SOLID WASTE RECEPTACLES REQUIRED

DEVELOPMENT AND USE OF THE SITE WILL CONFORM TO ALL APPLICABLE CODES ORDINANCES AND SPECIFICATIONS.

## CODE COMPLIANCE:

ALL WORK SHALL COMPLY WITH THE CURRENT NATIONAL AND CONNECTICUT STATE BUILDING AND LIFE SAFETY CODES, SUPPLEMENTS AND AMENDMENTS INCLUDING BUT NOT LIMITED TO THE LATEST EDITION OF

CONNECTICUT STATE BUILDING CODE (CSBC)

ANSI/TIA-222-G STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS

NATIONAL ELECTRICAL CODE (NEC) FOR POWER AND GROUNDING

OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA).

NFPA - NATIONAL FIRE PROTECTION ASSOCIATION.



1-800-922-4455

Minimum of 2 working days in advance, no more than 30 days in advance

DATE

SITE VICINITY:

SITE

G24-41-39

G24-41-40

LOCATION

# **CONTRACTOR'S NOTES:**

CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, AND CONDITIONS ON THE JOB SITE. CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ARCHITECT/ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING

WITH THE WORK. FAILURE TO NOTIFY THE ARCHITECT/ENGINEER PLACES THE RESPONSIBILITY ON THE CONTRACTOR TO CORRECT THE DISCREPANCIES AT THE CONTRACTOR'S EXPENSE.

REFER TO STRUCTURAL REPORTS / DRAWINGS:

TOWER ANALYSIS REPORT - UPGRADES, DATED 03/05/2021 BY EFI GLOBAL INC. MOUNT STRUCTURAL ANALYSIS REPORT, DATED 10/26/2020 BY EFI GLOBAL INC.

# **APPROVALS:**

FSA CM	DATE
RF ENGINEER	DATE
FOPS	DATE
T-MOBILE ENGINEERING AND DEVELOPMENT	DATE
	DATE



# PROJECT SCOPE:

THE PROPOSED PROJECT SCOPE WILL INCLUDE THE FOLLOWING EQUIPMENT MODIFICATIONS: UPGRADE EXISTING RBS 6102 CABINET INTERNALLY. REPLACE EXISTING ANTENNA MOUNTS. REPLACE (6) OF (6) EXISTING AND ADD (3) FOR TOTAL OF (9) ANTENNAS. REPLACE (3) OF (3) EXISTING AND ADD (3) FOR TOTAL OF (6) RRU. REMOVE (3) OF (3) EXISTING TMA AT ANTENNAS. ADD (1) 6160 AND (1) B160 CABINETS ON EXISTING CONCRETE PAD

REMOVE (12) OF (12) EXISTING COAX, ADD (2) 6X12 HCS, FOR FINAL

# CONFIGURATION OF (3) 6X12 HCS CABLES PROJECT INFORMATION:

ADDRESS: 25 LOWER BLVD. NEW LONDON CT 06230

SELF SUPPORT TOWER STRUCTURE TYPE:

PARCEL ID: ZONING DISTRICT 95-G23-41-36

COORDINATES: 41° 19' 22.35" N, 72° 05' 37.51" W APPROX. GROUND ELEV:

# **PROJECT TEAM:**

APPLICANT:

T-MOBILE NORTHEAST, LLC. 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

PROPERTY OWNER:

CITY OF NEW LONDON, CT 181 STATE STREET NEW LONDON, CT 6320

FORESITE LLC

PROJECT MANAGER:

NORTHEAST SITE SOLUTIONS 420 MAIN STREET, BLDG 4 STURBRIDGE MA 01566 SHELDON FREINCLE

SHELDON@NORTHEASTSITESOLUTIONS.COM

ENGINEERING CONSULTANTS:

462 WALNUT ST SAFED MOSSAVAT SMOSSAVAT@FORESITELLC.COM

## **SHEET INDEX:**

TITLE SHEET A-1: A-2: A-3: SITE PLAN EQUIPMENT LAYOUT

ELEVATION ANTENNA LAYOUT

EQUIPMENT SPECIFICATIONS ELECTRICAL AND GROUNDING DETAILS

STRUCTURAL DETAILS STRUCTURAL DETAILS STRUCTURAL DETAILS STRUCTURAL DETAILS

APPLICANT:

# T · · Mobile · T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

## PROJECT MANAGER

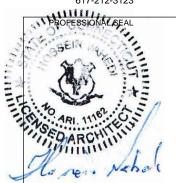


STURBRIDGE MA 01566 203-275-6669

## **CONSULTANT:**



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123



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ı	REV	DESCRIPTION	DATE
ı	Α	PRELIMINARY	03/18/21
ı	0	FINAL ISSUED	03/27/21
1	1	REVISED CABLE COUNTS	03/30/21
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SITE NUMBER: CTNL041A SITE NAME: NL041GARDNER-NEW LONDON

> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

SHEET TITLE: T-1: TITLE SHEET

## **GENERAL NOTES:**

- 1. THE CONTRACTOR SHALL GIVE ALL NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY, MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS, AND LOCAL AND STATE JURISDICTIONAL CODES BEARING ON THE PERFORMANCE OF THE WORK. THE WORK PERFORMED ON THE PROJECT AND THE MATERIALS INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES.
- 2. THE ARCHITECT/ENGINEER HAS MADE EVERY EFFORT TO SET FORTH IN THE CONSTRUCTION AND CONTRACT DOCUMENTS THE COMPLETE SCOPE OF WORK. THE CONTRACTOR BIDDING THE JOB IS NEVERTHELESS CAUTIONED THAT MINOR OMISSIONS OR ERRORS IN THE DRAWINGS AND OR SPECIFICATIONS SHALL NOT EXCUSE SAID CONTRACTOR FROM COMPLETING THE PROJECT AND IMPROVEMENTS IN ACCORDANCE WITH THE INTENT OF THESE DOCUMENTS.
- 3. THE CONTRACTOR OR BIDDER SHALL BEAR THE RESPONSIBILITY OF NOTIFYING (IN WRITING) THE CLIENT'S REPRESENTATIVE OF ANY CONFLICTS, ERRORS, OR OMISSIONS PRIOR TO THE SUBMISSION OF CONTRACTOR'S PROPOSAL OR PERFORMANCE OF WORK.
- 5. THE CONTRACTOR SHALL VISIT THE JOB SITE PRIOR TO THE SUBMISSION OF BIDS OR PERFORMING WORK TO FAMILIARIZE HIMSELF WITH THE FIELD CONDITIONS AND TO VERIFY THAT THE PROJECT CAN BE CONSTRUCTED IN ACCORDANCE WITH THE CONSTRUCTION DOCUMENTS.
- 6. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS ACCORDING TO THE MANUFACTURER'S / VENDOR'S SPECIFICATIONS UNLESS NOTED OTHERWISE OR WHERE LOCAL CODES OR ORDINANCES TAKE PRECEDENCE.
- 7. THE CONTRACTOR SHALL MAKE NECESSARY PROVISIONS TO PROTECT EXISTING IMPROVEMENTS DURING CONSTRUCTION
- 8. THE CONTRACTOR SHALL COMPLY WITH ALL PERTINENT SECTIONS OF THE BASIC STATE BUILDING CODE, LATEST EDITION, AND ALL OSHA REQUIREMENTS AS THEY APPLY TO THIS PROJEC
- 9. THE CONTRACTOR SHALL NOTIFY THE CLIENT'S REPRESENTATIVE IN WRITING WHERE A CONFLICT OCCURS ON ANY OF THE CONTRACT DOCUMENTS. THE CONTRACTOR IS NOT TO ORDER MATERIAL OR CONSTRUCT ANY PORTION OF THE WORK THAT IS IN CONFLICT UNTIL CONFLICT IS RESOLVED BY THE CLIENT'S REPRESENTATIVE.
- $10. \hspace{0.1in}$  THE WORK SHALL CONFORM TO THE CODES AND STANDARDS OF THE FOLLOWING AGENCIES AS FURTHER CITED HEREIN:
- A. ASTM: AMERICAN SOCIETY FOR TESTING AND MATERIALS, AS PUBLISHED IN "COMPILATION OF ASTM STANDARDS BUILDING CODES" OR LATEST EDITION.
- B. AWS: AMERICAN WELDING SOCIETY INC. AS PUBLISHED IN "STANDARD D1.1-08, STRUCTURAL WELDING CODE" OR LATEST EDITION.
- C. AISC: AMERICAN INSTITUTE FOR STEEL CONSTRUCTION AS PUBLISHED IN "CODE FOR STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES"; "SPECIFICATIONS FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS" (LATEST EDITION).
- 11. BOLTING:
- A. BOLTS SHALL BE CONFORMING TO ASTM A325 HIGH STRENGTH, HOT DIP GALVANIZED WITH ASTM A153 HEAVY HEX TYPE NUTS.
- B. BOLTS SHALL BE 3/4" $\phi$  MINIMUM (UNLESS OTHERWISE NOTED)
- C. ALL CONNECTIONS SHALL BE 2 BOLTS MINIMUM.
- 12. FABRICATION:
- . FABRICATION OF STEEL SHALL CONFORM TO THE AISC AND AWS STANDARDS AND CODES (LATEST EDITION).
- B. ALL STRUCTURAL STEEL SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 (LATEST EDITION), UNLESS OTHERWISE NOTED.
- 13. ERECTION OF STEEL:
- A. PROVIDE ALL ERECTION EQUIPMENT, BRACING, PLANKING, FIELD BOLTS, NUTS, WASHERS, DRIFT PINS, AND SIMILAR MATERIALS WHICH DO NOT FORM A PART OF THE COMPLETED CONSTRUCTION BUT ARE NECESSARY FOR ITS PROPER ERECTION.
- B. ERECT AND ANCHOR ALL STRUCTURAL STEEL IN ACCORDANCE WITH AISC REFERENCE STANDARDS. ALL WORK SHALL BE ACCURATELY SET TO ESTABLISHED LINES AND ELEVATIONS AND RIGIDLY FASTENED IN PLACE WITH SUITABLE ATTACHMENTS TO THE CONSTRUCTION OF THE BUILDING.
- C. TEMPORARY BRACING, GUYING AND SUPPORT SHALL BE PROVIDED TO KEEP THE STRUCTURE SAFE AND ALIGNED AT ALL TIMES DURING CONSTRUCTION, AND TO PREVENT DANGER TO PERSONS AND PROPERTY. CHECK ALL TEMPORARY LOADS AND STAY WITHIN SAFE CAPACITY OF ALL BUILDING COMPONENTS.
- 14. RELATED WORK, FURNISH THE FOLLOWING WORK AS SPECIFIED UNDER CONSTRUCTION DOCUMENTS, BUT COORDINATE WITH OTHER TRADES PRIOR TO BID:
- A. FLASHING OF OPENING INTO OUTSIDE WALLS

- B. SEALING AND CAULKING ALL OPENINGS
- C. PAINTING
- D. CUTTING AND PATCHING
- 15. REQUIREMENTS OF REGULATORY AGENCIES:
- A. FURNISH U.L. LISTED EQUIPMENT WHERE SUCH LABEL IS AVAILABLE. INSTALL IN CONFORMANCE WITH U.L. STANDARDS WHERE APPLICABLE.
- B. INSTALL ANTENNA, ANTENNA CABLES, GROUNDING SYSTEM IN ACCORDANCE WITH DRAWINGS AND SPECIFICATION IN EFFECT AT PROJECT LOCATION AND RECOMMENDATIONS OF STATE AND LOCAL BUILDING CODES, AND SPECIAL CODES HAVING JURISDICTION OVER SPECIFIC PORTIONS OF WORK. THIS WORK INCLUDES BUT IS NOT LIMITED TO THE FOLLOWING:
- C. TIA-EIA 222 (LATEST EDITION). STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- D. FAA FEDERAL AVIATION ADMINISTRATION ADVISORY CIRCULAR AC 70/7460-IH, OBSTRUCTION MARKING AND LIGHTING.
- E. FCC FEDERAL COMMUNICATIONS COMMISSION RULES AND REGULATIONS FORM 715, OBSTRUCTION MARKING AND LIGHTING SPECIFICATION FOR ANTENNA STRUCTURES AND FORM 715A, HIGH INTENSITY OBSTRUCTION LIGHTING SPECIFICATIONS FOR ANTENNA STRUCTURES.
- F. AISC AMERICAN INSTITUTE OF STEEL CONSTRUCTION SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM A325 BOLTS (LATEST EDITION).
- G. NEC NATIONAL ELECTRICAL CODE ON TOWER LIGHTING KITS.
- H. UL UNDERWRITER'S LABORATORIES APPROVED ELECTRICAL PRODUCTS.
- I. IN ALL CASES, PART 77 OF THE FAA RULES AND PARTS 17 AND 22 OF THE FCC RULES ARE APPLICABLE AND IN THE EVENT OF CONFLICT, SUPERSEDE ANY OTHER STANDARDS OR SPECIFICATIONS.
- J. 2018 LIFE SAFETY CODE NFPA 101.

## APPLICANT:

# T - Mobile - T-Mobile -

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

## PROJECT MANAGER

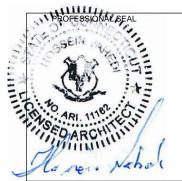


420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

## **CONSULTANT:**



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123



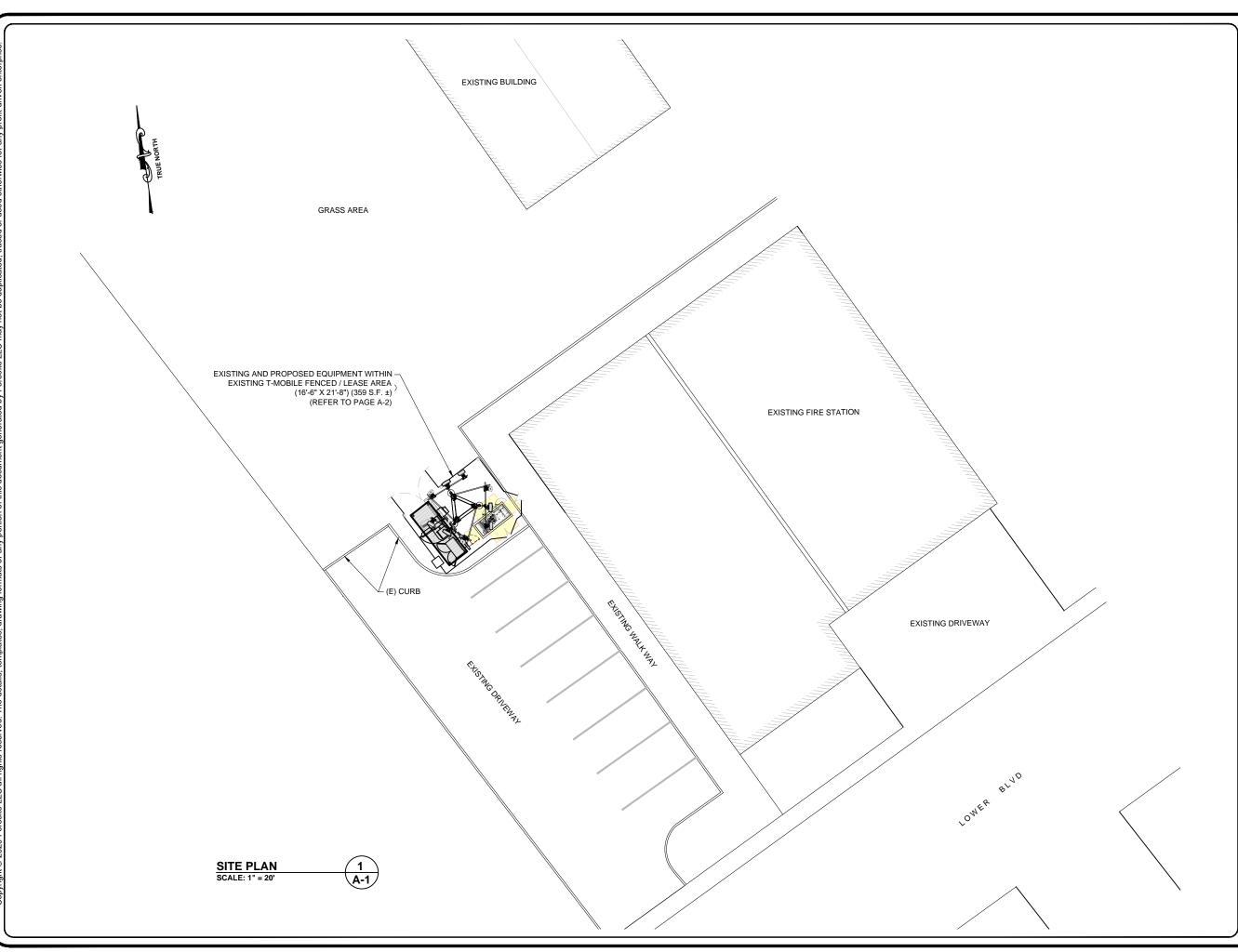
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Ш	REV	DESCRIPTION	DATE
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SITE NUMBER: CTNL041A SITE NAME: NL041GARDNER-NEW LONDON

> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

SHEET TITLE: N-1: NOTES AND DISCLAIMERS



# T - Mobile -

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER



420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

# CONSULTANT:



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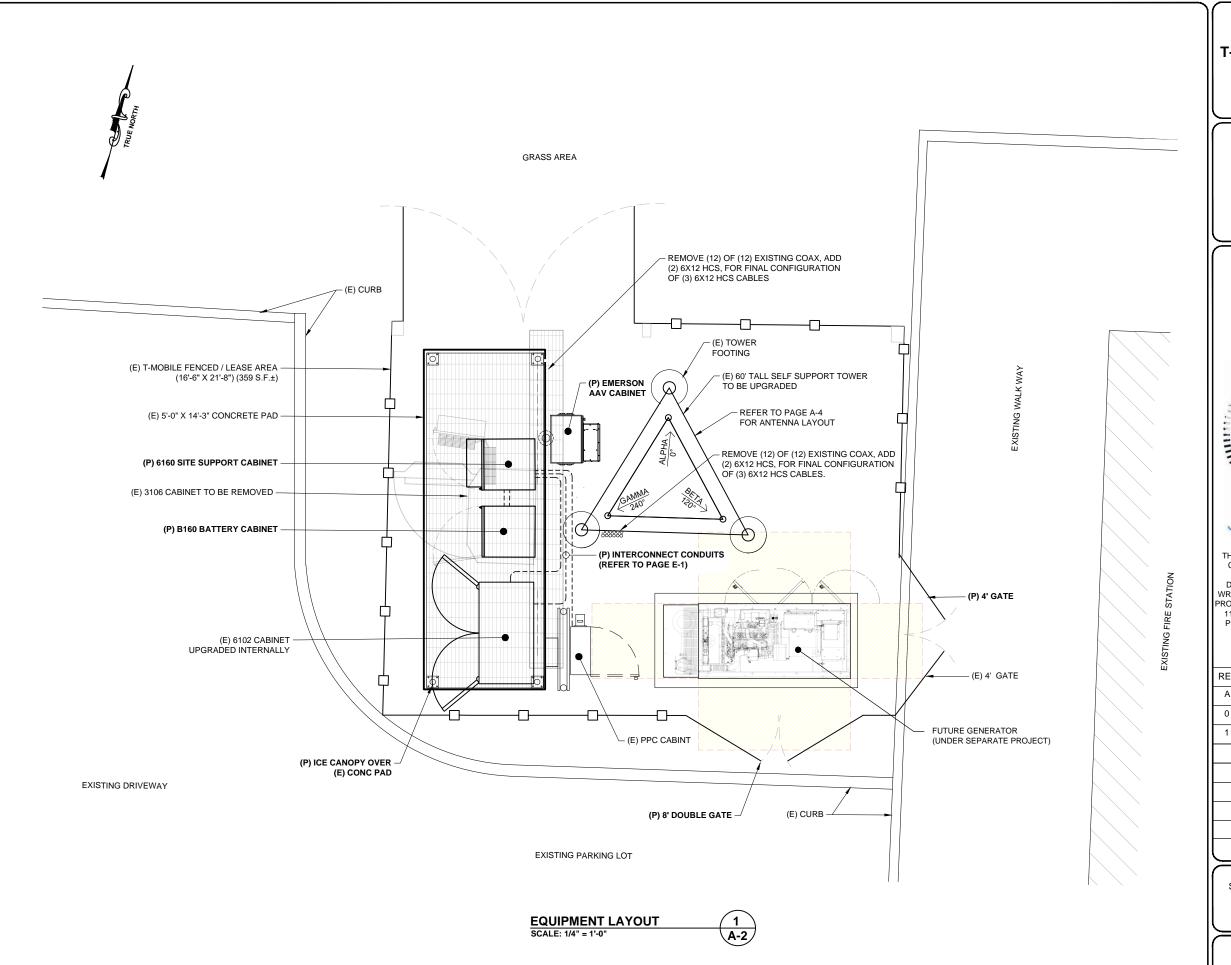
REV	DESCRIPTION	DATE
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0	FINAL ISSUED	03/27/21
1	REVISED CABLE COUNTS	03/30/21
		J

SITE NUMBER: CTNL041A
SITE NAME: NL041GARDNER-NEW LONDON

SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

SHEET TITLE:

A-1: PLAN



# T - Mobile - T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

## PROJECT MANAGER



420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

## CONSULTANT:



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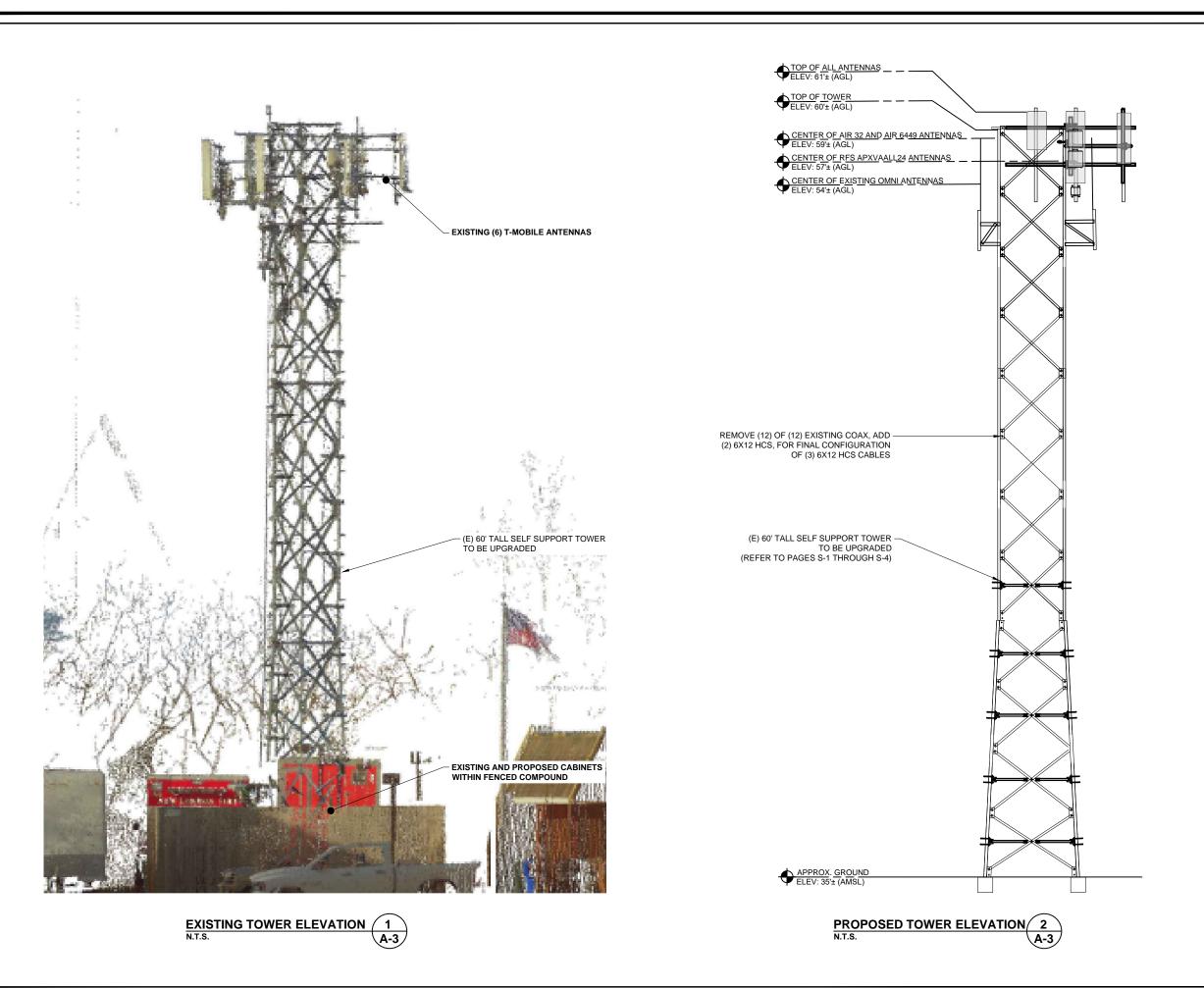
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1	REVISED CABLE COUNTS	03/30/21

SITE NUMBER: CTNL041A
SITE NAME: NL041GARDNER-NEW LONDON

SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

SHEET TITLE:

A-2: EQUIPMENT LAYOUT



# T - Mobile - T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER

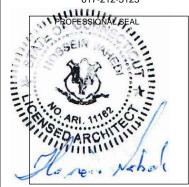


420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

# CONSULTANT:



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123



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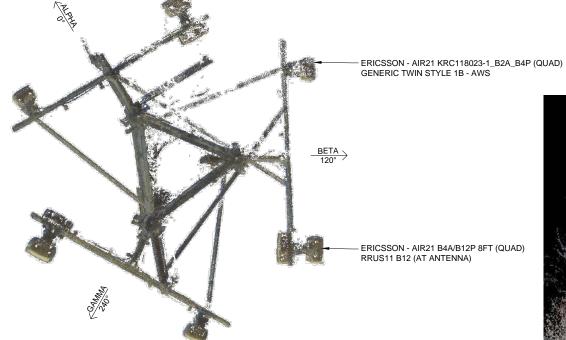
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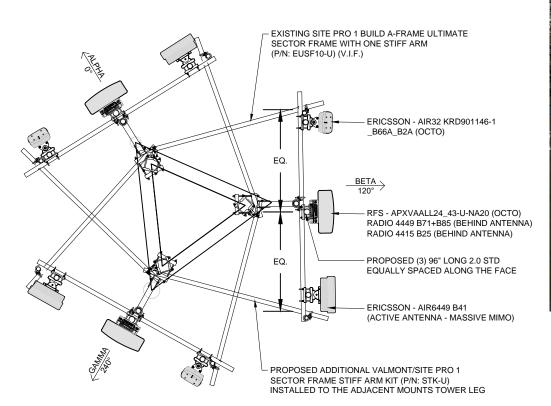
SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

> SHEET TITLE: A-3: ELEVATION





# EXISTING ANTENNA PLAN N.T.S. 1 A-4





EXISTING SITE CONDITIONS N.T.S.

 $\frac{3}{A-4}$ 

PROPOSED ANTENNA PLAN



APPLICANT:

# T - Mobile - T-Mobile - T-Mobile NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER



420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

# CONSULTANT:



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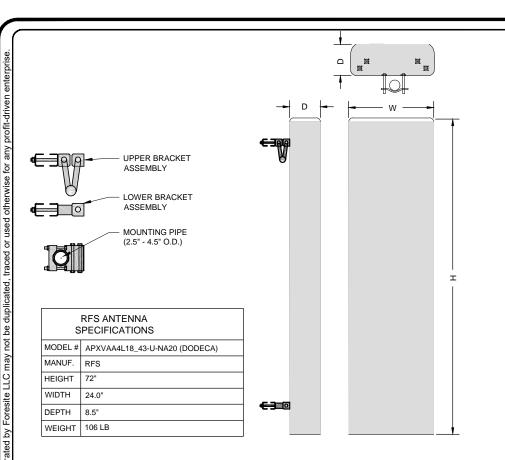
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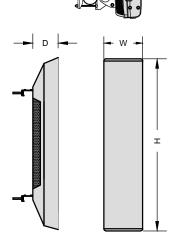
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SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

SHEET TITLE:

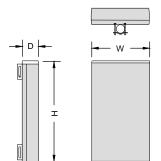
A-4: ANTENNA PLANS





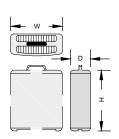
ERICSON ANTENNA SPECIFICATIONS		
MODEL#	AIR32 KRD901146-1_ B66A_B2A (OCTO)	
MANUF.	ERICSSON	
HEIGHT	56.6"	
WIDTH	12.9"	
DEPTH	8.7"	
WEIGHT	132.2 LB	





ERICSON ANTENNA SPECIFICATIONS		
MODEL#	AIR6449 B41	
MANUF.	ERICSSON	
HEIGHT	33.1"	
WIDTH	20.5"	
DEPTH	8.3"	
WEIGHT	103 LB	
	MODEL # MANUF. HEIGHT WIDTH DEPTH	



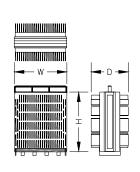


**RFS ANTENNA** 

N.T.S

REMOTE RADIO UNIT SPECIFICATIONS			
MODEL # RADIO 4415 B25			
MANUF.	ERICSSON		
HEIGHT	14.9"		
WIDTH	13.2"		
DEPTH	5.4"		
WEIGHT	46.3 LB		





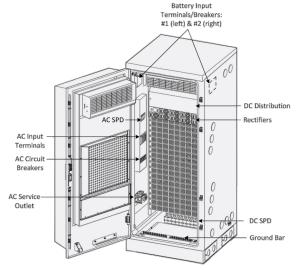
REMOTE RADIO UNIT SPECIFICATIONS		
MODEL # RADIO 4449 B71+B85		
MANUF. ERICSSON		
HEIGHT 14.9"		
WIDTH 13.2"		
DEPTH 10.4"		
WEIGHT 74 LB		





BATTERY CABINET SPECIFICATIONS		
MODEL#	B160	
MANUF.	ERICSSON	
HEIGHT	63"	
WIDTH	26"	
DEPTH	26"	
WEIGHT	1883 lbs	





SITE SUPPORT CABINET SPECIFICATIONS		
MODEL#	6160	
MANUF.	ERICSSON	
HEIGHT	63"	
WIDTH	25.6"	
DEPTH	33.5"	
WEIGHT	605 lbs	

SITE SUPPORT CABINET 7 N.T.S. A-5

# APPLICANT:

# T - Mobile - T-Mobile - T-Mobile NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

## PROJECT MANAGER

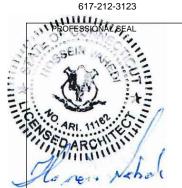


420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

## **CONSULTANT:**



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460



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> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

> > SHEET TITLE:

A-5: ANTENNA AND EQUIPMENT SPECS

2. ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED AND PRODUCED PER SPECIFICATION REQUIREMENTS.

- 3. THE ELECTRICAL WORK INCLUDES ALL LABOR AND MATERIAL DESCRIBED BY DRAWINGS AND SPECIFICATION INCLUDING INCIDENTAL WORK TO PROVIDE COMPLETE OPERATING AND APPROVED ELECTRICAL SYSTEM.
- 4. GENERAL CONTRACTOR SHALL PAY FEES FOR PERMITS, AND RESPONSIBLE FOR OBTAINING SAID PERMITS AND COORDINATION OF INSPECTIONS
- 5. ELECTRICAL AND TELCO WIRING OUTSIDE A BUILDING AND EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUITS OR SCHEDULE 80 PVC (AS PERMITTED BY CODE) ND WHERE REQUIRED IN LIQUID TIGHT FLEXIBLE METAL OR NONMETALLIC CONDUITS
- 6. RIGID STEEL CONDUITS SHALL BE GROUNDED AT BOTH ENDS.
- 7. ELECTRICAL WIRING SHALL BE COPPER WITH TYPE XHHW, THWN, OR THIN INSULATION.

8 RUN ELECTRICAL CONDUIT OR CABLING BETWEEN ELECTRICAL ROOM AND PROPOSED. CELL SITE ARE PEDESTAL AS INDICATED ON THIS DRAWING, PROVIDE FULL LENGTH PULL ROPE. COORDINATE INSTALLATION WITH UTILITY COMPANY.

9. RUN TELCO CONDUIT OR CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT AND PROPOSED CELL SITE TELECOM CABINET AND RBS CABINET AS INDICATED ON DRAWING A -1. PROVIDE FULL LENGTH PULL ROPE INSTALLED TELCO CONDUIT. PROVIDE GREENLEE CONDUIT MEASURING TAPE AT EACH END.

10. ALL EQUIPMENT LOCATED OUTSIDE SHALL HAVE NAME 3R ENCLOSURE.

- 11. GROUNDING SHALL COMPLY WITH NEC ART. 250.
- 12. GROUNDING COAX CABLE SHIELDS MINIMUM AT BOTH ENDS USING MANUFACTURES COAX CABLE GROUNDING KITS SUPPLIED BY PROJECT OWNER

13. USE #6 COPPER STRANDED WIRE WITH GREEN COLOR INSTALLATION FOR ABOVE GRADE GROUNDING (UNLESS OTHERWISE SPECIFIED) AND #2 SOLID TINNED BARE COPPER WIRE FOR BELOW GRADE GROUNDING AS INDICATED ON THE GROUND.

14. ALL GROUND CONNECTION TO BE BURNDY HYGROUND COMPRESSION TYPE CONNECTORS OR CADWELD EXOTHERMIC WELD. DO NOT ALLOW BARE COPPER WIRE TO BE IN CONTACT WITH GALVANIZED STEEL.

15. ROUTE GROUNDING CONDUCTORS ALONG THE SHORTEST AND STRAIGHTEST PATH POSSIBLE, EXCEPT AS OTHERWISE INDICATED. GROUNDING LEADS SHOULD NEVER BE BENT AS RIGHT ANGLE AL WAYS MAKE AT LEAST 12" RADIUS BENDS #6 WIRE CAN BE BENT AT 6" RADIUS WHEN NECESSARY BOND ANY METER OBJECTS WITHIN 7 FEET OF PROPOSED EQUIPMENT OR CABINET TO MASTER GROUND BAR.

16. CONNECTIONS TO MGB SHALL BE ARRANGED IN THREE MAIN GROUPS: SURGE PROCEDURES (COAXIAL CABLE GROUND KITS, TELCO AND POWER PANEL GROUND); (GROUNDING ELECTRODE RING OR BUILDING STEEL); NON-SURGING OBJECTS (EGB

17. CONNECTIONS TO GROUND BARS SHALL BE MADE WITH TWO HOLE COMPRESSION TYPE COPPER LUGS. APPLY OXIDE INHIBITING COMPOUND TO ALL LOCATIONS.

18. APPLY OXIDE INHIBITING COMPOUND TO ALL COMPRESSION TYPE GROUND CONNECTION

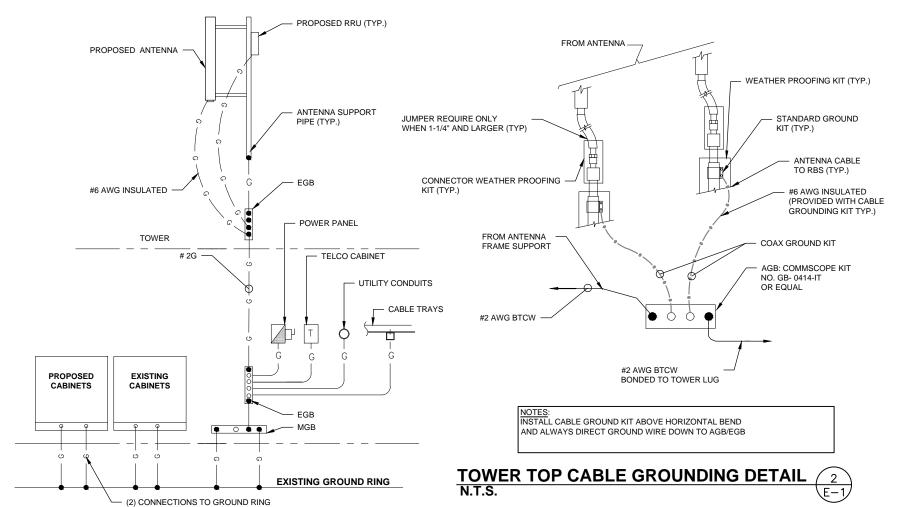
19. BOND ANTENNA MOUNTING BRACKETS, COAXIAL CABLE GROUND KITS, AND ALNA TO EGB PLACED NEAR THE ANTENNA LOCATION.

20 BOND ANTENNA EGB'S AND MGB TO WATER MAIN.

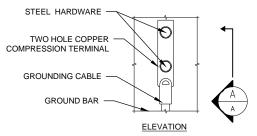
21. TEST COMPLETED GROUND SYSTEM AND RECORD RESULTS FOR PROJECT CLOSE-OUT DOCUMENTATION.

22. BOND ANY METAL OBJECTS WITHIN 7 FEET OF PROPOSED EQUIPMENT OR CABINET TO MASTER GROUND BAR.

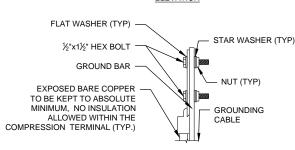
23. VERIFY PROPOSED SERVICE UPGRADE WITH LOCAL UTILITY COMPANY PRIOR TO CONSTRUCTION







PER CABINET



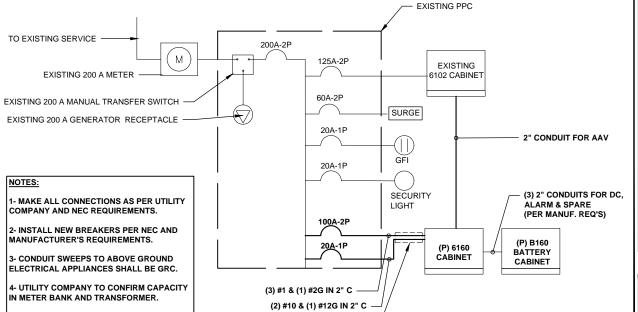
SECTION A-A

1. "DOUBLING UP" OR "STACKING " OF CONNECTION IS NOT PERMITTED

TYPICAL GROUND BAR CONNECTIONS DETAIL

#### SPECIAL CONTRACTOR'S NOTES:

CONTRACTOR TO VERIFY THE POWER FEED & PHASE OF METER BANK AND THAT THE EXISTING AND PROPOSED CONDUITS AND WIRE SIZES ARE ADEQUATE FOR THE PROPOSED LOADING IN ACCORDANCE WITH NEC AND INCLUDE ELECTRICAL UPGRADES IN THE SCOPE OF WORK AS



2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

TYPICAL ONE LINE DIAGRAM N.T.S.

(1) 2" CONDUIT

**APPLICANT:** 

# T - Mobile-T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

## PROJECT MANAGER

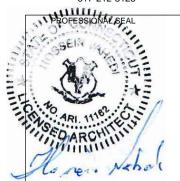


420 MAIN STREET BLDG 4 STURBRIDGE MA 01566 203-275-6669

## **CONSULTANT:**



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123



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SITE NUMBER: CTNL041A SITE NAME: NL041GARDNER-NEW LONDON

> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

> > SHEET TITLE:

E-1: ELECTRICAL & GROUNDING DETAIL

N.T.S.

# P2.0x0. P2.0x0.21 2 5x0.203 LEGS

80'-0" AGL

40'-0" AGL

20'-0" AGL

0'-0" AGL

#### NOTES:

- 1. UPGRADE DESIGN VALID FOR APPURTENANCES LISTED IN EFI ANALYSIS REPORT DATED 03/05/2021. CONTRACTOR TO REVIEW AND SHOULD
- 2. CONTRACTOR TO REMOVE AND REATTACH EXISTING APPURTENANCES AS
- 3. ALL DIMENSIONS ARE BASED ON STRUCTURAL ANALYSIS REPORT PREPARED BY EBI CONSULTING, DATED 02/13/2015.
- 4. CONTRACTOR TO FIELD VERIFY EXISTING TOWER MEMBER SIZES AND TOWER DIMENSIONS IN THE VICINITY OF THE UPGRADE, BEFORE FABRICATION OF STEEL AND COMMENCEMENT OF WORK. ANY DISCREPANCY SHOULD BE REPORTED TO EFI IMMEDIATELY FOR FURTHER EVALUATION.
- 5. DO NOT PERFORM THE WORK ON THE TOWER WHEN WINDS GUST MORE THAN 15 MPH AT THE GROUND LEVEL.

54 KIPS

6. NEW TOWER REACTIONS:

LEG UPLIFT: LEG COMPRESSION:

61 KIPS LEG SHEAR: 6 KIPS

- 7. CONTRACTOR TO HAVE THE SAFETY CLIMB INTACT AND FUNCTIONAL AFTER
- 8. TOWER WILL BECOME UNSTABLE WHEN MEMBERS ARE DISCONNECTED OR BEING REPLACED. CONTRACTOR IS FULLY RESPONSIBLE TO MAINTAIN STABILITY OF THE TOWER DURING WORK AND SHOULD CONSULT WITH AN
- 9. EFI DISCLAIMS ANY LIABILITY ARISING FROM THE ORIGINAL MATERIAL, FABRICATION OR ERECTION OF THE TOWER.
- 10. ALL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN AND SHALL MEET ANSI/ASSE A10.48 (LATEST EDITION), OSHA, AND GENERAL INDUSTRY STANDARDS. ALL RIGGING PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION) INCLUDING THE REQUIRED INVOLVEMENT OF A QUALIFIED ENGINEER FOR CLASS IV CONSTRUCTION.

[B] ADD L2X2X/4 SECONDARY HORIZONTALS TOWER MODIFICATION SCHEDULE REFERENCE FROM (FT) TO (FT) MODIFICATION SHFFT 0'-0" 25'-0" ADD L2x2x1/4 SECONDARY HORIZONTALS S2 20'-0" 20'-0" ADD NEW KNIFE PLATES S2 NOTE: APPLY INDICATED MODIFICATIONS TO ALL 3 TOWER FACES

[A] ADD L2X2X1/4 SECONDARY HORIZONTALS SEE 1/S2

SEE 2/S2

SEE 4/S2

[C] ADD KNIFE PLATE

# **TOWER ELEVATION** S1 /

#### 1. DESIGN INFORMATION AND GENERAL REQUIREMENTS

#### 1.1 CODES

a. 2018 CONNECTICUT BUILDING CODE (2015 IBC). b. MINIMUM DESIGN LOADS AND ASSOCIATED CRITÉRIA FOR BUILDINGS AND OTHER STRUCTURES, ASCE/SEI 7-10, AMERICAN SOCIETY OF CIVIL **ENGINEERS** 

c. STEEL CONSTRUCTION MANUAL, 14TH EDITION, AMERICAN INSTITUTE OF STEEL CONSTRUCTION

d. STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, ANSI/TIA-222-G TELECOMMUNICATIONS INDUSTRY ASSOCIATION

1.2 GENERAL a. PRIOR TO PURCHASE OR FABRICATION OF MATERIAL, THE CONTRACTOR SHALL PERFORM AN INSPECTION VERIFYING MEMBER DIMENSIONS AND BOLT SIZES. SHOULD THE CONTRACTOR DISCOVER ANY DAMAGED OR MISSING MEMBERS OR THE MEMBER OR BOLT SIZES DO NOT MATCH THOSE LISTED, EFI SHALL BE NOTIFIED IMMEDIATELY.

b. CONTRACTOR TO REPLACE ALL BOLTS REMOVED WITH NEW BOLTS OF SAME TYPE, UNLESS NOTED OTHERWISE.

## 1.3 LOADS & DESIGN CRITERIA

a. WIND LOADING: V=135MPH (ULTIMATE DESIGN WIND SPEED), EXPOSURE CATEGORY C. RISK CATEGORY

#### 2. STRUCTURAL STEEL

a. STRUCTURAL STEEL . . . . . ASTM A992
ANGLE & PLATE . . . . . ASTM A56 U.N.O.

PIPE . . . . . . . . . . . . . . . . ASTM A53 GRADE B (OR Fy>35KSI)

HSS ROUND . . . . . ASTM A500 GRADE B (OR Fy>42KSI) BARS (SOLID RODS) . . . ASTM A572 GRADE 50

b. BOLTS . . . . . . . . . . . . . . . . . ASTM A325N U.N.O.
c. WELDING ELECTRODES . . . . . AWS A5.1 (E70XX)
d. STEEL CONSTRUCTION SHALL CONFORM TO "SPECIFICATION FOR

STRUCTURAL STEEL BUILDINGS, ANSI/AISC 360-10"

e. WELDING SHALL CONFORM TO AWS D1.1/D1.3/D1.7 AS APPLICABLE. f. THE FABRICATOR SHALL FURNISH CHECKED SHOP AND ERECTION DRAWINGS TO THE ENGINEER, AND OBTAIN APPROVAL PRIOR TO

FABRICATING ANY STRUCTURAL STEEL. SHOP DRAWINGS SHALL CONFORM TO "DETAILING FOR STEEL CONSTRUCTION, 2ND EDITION" g. POOR MATCHING OF HOLES SHALL BE CORRECTED BY DRILLING TO THE NEXT LARGER SIZE. WELDING FOR RE-DRILLING WILL NOT BE PERMITTED.

# 2.2 CONNECTIONS

a. SHOP CONNECTIONS MAY BE BOLTED OR WELDED

b. FIELD CONNECTIONS BOLTED WITH A325-N BOLTS, (INSTALLED SNUG TIGHT) UNLESS OTHERWISE SPECIFIED OR IF WELDED CONNECTIONS ARE NOTED ON DRAWINGS

c. FIELD CONNECTIONS SHALL BE MADE WITH A325-N BOLTS AND

HARDENED WASHERS EXCEPT AS INDICATED ON THE DESIGN DRAWINGS d. CONNECTIONS NOT SHOWN ON DRAWINGS SHALL BE DESIGNED BY THE STEEL FABRICATOR. CONNECTIONS SHALL BE DESIGNED IN ACCORDANCE WITH AISC "SPECIFICATIONS FOR STRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS" AND "AISC CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES"

e. DO NOT FIELD CUT OR ALTER STRUCTURAL MEMBERS WITHOUT PRIOR

WRITTEN APPROVAL OF ENGINEER.

f. BOLT HOLES SHALL BE CUT, DRILLED OR PUNCHED AT RIGHT ANGLES
TO THE SURFACE OF THE METAL AND SHALL NOT BE MADE OR ENLARGED BY BURNING. HOLES SHALL BE CLEAN CUT WITHOUT TORN OR RAGGED EDGES. OUTSIDE BURRS RESULTING FROM DRILLING OR REAMING OPERATION SHALL BE REMOVED WITH A TOOL MAKING A 1/16 INCH BEVEL. BOLT HOLES SHALL BE 1/16 INCH OVERSIZE.

#### 2.3 FINISHES

a. STRUCTURAL STEEL SHALL BE HOT DIP GALVANIZED AFTER FABRICATION

b. BOLTS AND NUTS SHALL BE HOT DIP GALVANIZED PER ASTM A153.
c. ALL SURFACES DAMAGED DURING THE WORK SHALL BE PAINTED WITH COLD GALVANIZING COMPOUND TWICE. THE PAINT SHOULD BE AT LEAST 93% PURE ZINC. RUST-OLEUM PROFESSIONAL, (MODEL# 7585838) OR

#### 2.4 WELDING

a. CONTRACTOR TO TAKE ALL NECESSARY PRECAUTIONS FOR FIRE PREVENTION DURING WELDING, SUCH AS; INSTALLING 3000 (NFPA 701) FIRE BLANKET AROUND COAX. MORE SPLATTER AND SPARKS SHOULD BE ANTICIPATED WHILE WELDING ON GALVANIZED SURFACE, COAX IS FLAMMABLE AND SHALL CATCH FIRE IF NOT PROTECTED. WATER SHALL BE ON SITE OF ADEQUATE AMOUNT AND AVAILABLE AT SHORT NOTICE AT ALL TIMES DURING WELDING ACTIVITY. CONTRACTOR SHOULD BE ABLE TO TRANSPORT THE WATER TO THE HEIGHT WELDING BEING PERFORMED.

b. WELDING ON GALVANIZED SURFACE SHOULD BE DONE WITH EXTREME CAUTION. IF THE WELD MATERIAL IS CONTAMINATED WITH ZINC, IT DOES

NOT PROVIDE A STRUCTURAL WELD. GRIND GALVANIZING BEFORE WELDING.

c. WELDING CERTIFICATE MUST BE PROVIDED PRIOR TO WELDING. ALL
WELDING SHALL BE PERFORMED BY AWS QUALIFIED WELDER WHO HAS EXPERIENCE WITH GALVANIZED SURFACES.

**APPLICANT:** 

# T - Mobile-T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER

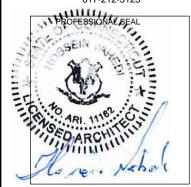


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## **CONSULTANT:**



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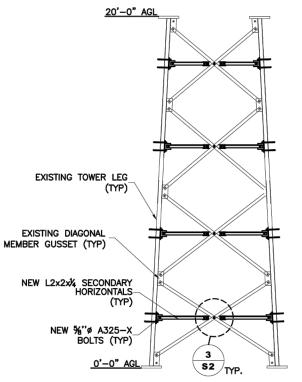


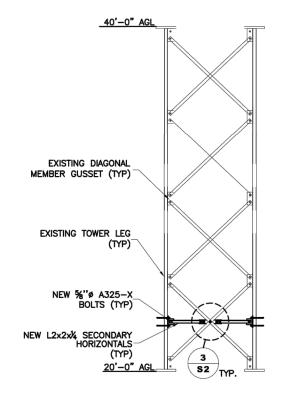
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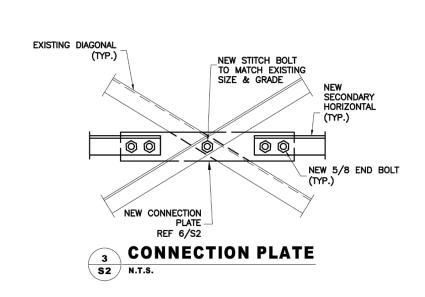
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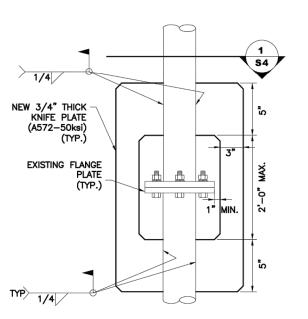


S2 N.T.S.

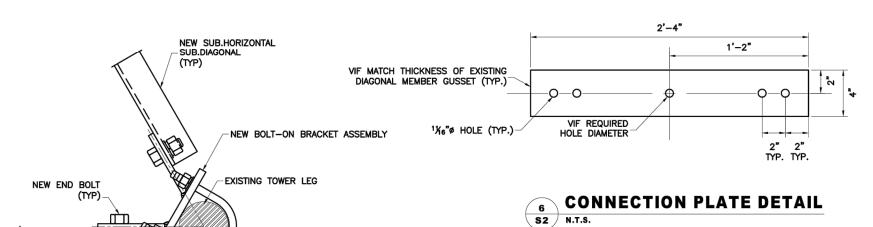
**ELEVATION VIEW: 20' - 40'** 



ELEVATION VIEW: 0' - 20'



KNIFE PLATE DETAIL @ 20'



5 BOLT-ON BRACKET s2 N.T.S.

APPLICANT:

# T - Mobile - T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER

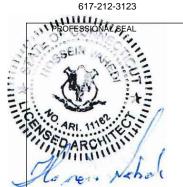


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462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123

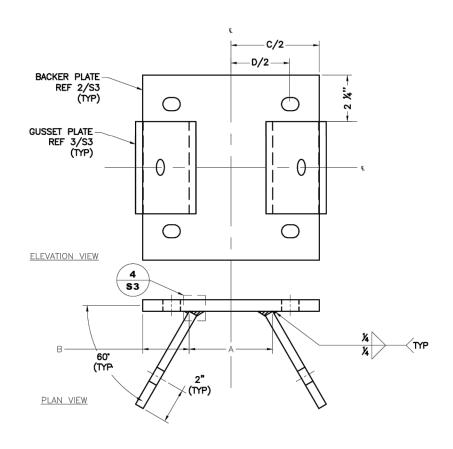


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REV	REV DESCRIPTION	
Α	PRELIMINARY	03/18/21
0	FINAL ISSUED	03/27/21
1	REVISED CABLE COUNTS	03/30/21

SITE NUMBER: CTNL041A
SITE NAME: NL041GARDNER-NEW LONDON

SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230



**BOLT-ON BRACKET ASSEMBLY** S3 N.T.S.

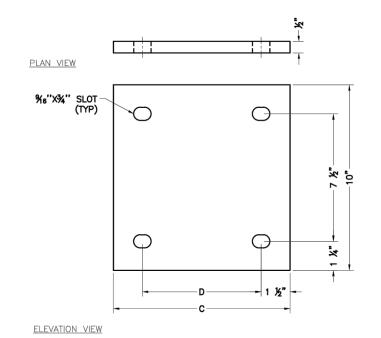
PIPE2.5STD+HSS3.5X0.203 SPLIT PIPE

LEG	OUTER	ASSE	MBLY	BACKER	PLATE		U-BOLT	
LEG	DIAMETER	A (in)	B (in)	C (in)	D (in)	E (in)	F (in)	G (in)
PIPE2.5STD	27/8	2 <sup>1</sup> / <sub>16</sub>	1 <sup>2</sup> / <sub>32</sub>	6	3½	4%	3	1/2
PIPE2.0X STD	2¾	2¾	1¹¾6	6	3	4%	2½	1/2

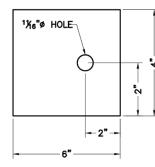
- NOTES:
  1. ALL HOLES TO BE SHOP FABRICATED, UNLESS NOTED OTHERWISE.
- 2. TOLERANCES UNLESS NOTED OTHERWISE: FRACTIONS ± 1/6"
- ANGLES ± ½°
  DECIMALS ± 0.010" 3. U-BOLTS SHALL MEET REQUIREMENTS OF ASME B18.31.5-2011 BENT BOLTS.
- 4. U-BOLTS TO BE ASTM A36/A307, SAE 429 GR 2. PLATES TO BE ASTM A572 GRADE 50.
- 5. USE 2 U-BOLTS PER ASSEMBLY, COMPLETE W/ NUTS, WASHERS AND LOCK WASHERS.
- 6. FOR WELDING, WELD TO BE E70xx ELECTRODES.
  7. FULL ASSEMBLY TO BE HOT DIP GALVANIZED PER ASTM 153/ A153M OR A123, AS
- APPLICABLE

  8. STANDARD %6" HOLES IN PLACE OF SLOTTED HORIZONTAL HOLES ON THE BACKER PLATE ARE PERMITTED

  9. NO FIELD FABRICATION PERMITTED ON THIS PART



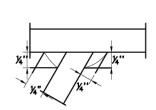




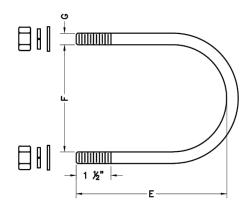
ELEVATION VIEW

**BACKER PLATE** S3 N.T.S.











**APPLICANT:** 

# T - Mobile T-MOBILE NORTHEAST LLC

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER

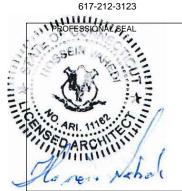


420 MAIN STREET. BLDG 4 STURBRIDGE, MA 01566 203-275-6669

## **CONSULTANT:**



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460

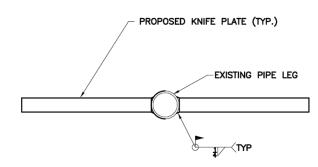


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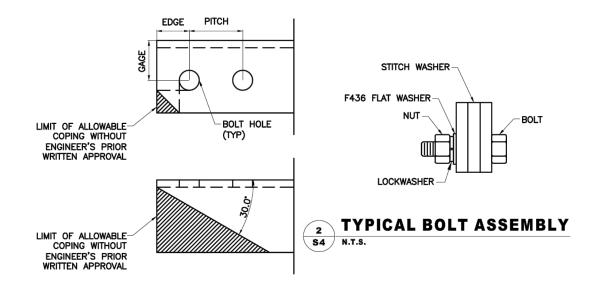
REV	DESCRIPTION	DATE
Α	PRELIMINARY	03/18/21
0	FINAL ISSUED	03/27/21
1	REVISED CABLE COUNTS	03/30/21

SITE NUMBER: CTNL041A SITE NAME: NL041GARDNER-NEW LONDON

> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230







BOLT SCHEDULE						
MEMBER SIZE CONNECTION TYPE BOLT SIZE MIN EDGE DISTANCE PITCH DISTANCE GAGE DISTANCE BOLT HOLE						
L2X2X1/4	L2X2X¼ END 56"ø X 2" LONG 76" 11%" 11%" 11/16"					
NOTE: ALL BOLTS TO BE A325—X						

# T - • Mobile • T-Mobile • T-Mobil

35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860-692-7100

# PROJECT MANAGER

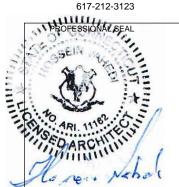


420 MAIN STREET, BLDG 4 STURBRIDGE, MA 01566 203-275-6669

# CONSULTANT:



462 WALNUT STREET, SUITE 1 NEWTON, MA 02460 617-212-3123



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REV	DESCRIPTION	DATE
Α	PRELIMINARY	03/18/21
0	FINAL ISSUED	03/27/21
1	REVISED CABLE COUNTS	03/30/21

SITE NUMBER: CTNL041A SITE NAME: NL041GARDNER-NEW LONDON

> SITE ADDRESS: 25 LOWER BLVD. NEW LONDON, CT 06230

# Exhibit D

# STRUCTURAL ANALYSIS REPORT - UPGRADE SELF-SUPPORT TOWER



# Prepared For:

# ·· T··Mobile·

T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002



# **Structure Rating**

Self-Support Tower: 85.3% (Pass) Anchor bolts: 57.7% (Pass) Foundation: 65.7% (Pass)

Sincerely, EFI Global, Inc.

License No: PEC0001245



Ahmet Colakoglu, PE Connecticut Professional Engineer

License No: 27057

Site ID: CTNL041A
Site Name: NL041/Gardner-NewLondon
25 Lower Boulevard,
New London, CT 06320

EFI Global Job No: 049.00940 - 2075089

# **CONTENTS**

- 1.0 SUBJECT AND REFERENCES
- 1.1 STRUCTURE
- 2.0 EXISTING AND PROPOSED APPURTENANCES
- 3.0 CODES AND LOADING
- 4.0 STANDARD CONDITIONS FOR ENGINEERING SERVICES ON EXISTING STRUCTURES
- 5.0 ANALYSIS AND ASSUMPTIONS
- 6.0 RESULTS AND CONCLUSION

# **APPENDIX**

A - PICTURES AND CALCULATIONS

Page | 0 EFI GLOBAL, INC.

# 1.0 SUBJECT AND REFERENCES

The purpose of this analysis is to evaluate the structural capacity of the existing 60 feet tall self-support tower, located at 25 Lower Boulevard, New London, CT 06320 for the additions and alterations proposed by T-Mobile.

The structural analysis is based on the following information provided to EFI Global, Inc. (EFI):

- Geotechnical Report prepared by HighTower Solutions, Inc., dated 02/07/2021.
- RFDS prepared by T-Mobile, dated 10/09/2020.
- Construction Drawings prepared by EBI Consulting, dated 03/23/2015.
- Structural Analysis Report prepared by EBI Consulting, dated 02/13/2015.
- Structural Design Report prepared by Saber Communication Corporation, dated 12/27/2006.

# 1.1 STRUCTURE

The subject structure is a 3-sided 60 feet tall self-support tower formed by three (3) sections which are X-braced with single angle diagonals. The tower tapers from 7.0 feet wide at the base to 5.0 feet wide at elevation 20 feet. Between elevations 20 feet and 60 feet, the tower is 5.00 feet wide. Please refer to the software output in Appendix A for tower geometry, member sizes, and other details.

# 2.0 EXISTING AND PROPOSED APPURTENANCES

**Existing Configuration of T-Mobile Appurtenances:** 

RAD Center (ft.)	Antennas and Equipment	Соах	Mount
59	(3) Ericsson AIR21 B2A B4P (3) Ericsson AIR21 B4A B12P (4) RRUS 11 B12 (4) Generic Style 1B – Twin AWS	(12) 7/8" (1) 6x12 HCS	(3) Sector Mounts

**Proposed and Final Configuration of T-Mobile Appurtenances:** 

RAD Center (ft.)	Antennas and Equipment	Coax	Mount
59	(3) Ericsson AIR32 B66A B2A (3) AIR6449 B41		(3) Sector
57	(3) RFS APXVAALL24_43-U-NA20 (3) Radio 4449 B71+B85* (3) Radio 4415 B25*	(3) 6x12 HCS	Mounts

<sup>\*</sup> To be mounted behind antennas.

# **Existing and Remaining Appurtenances by Others:**

RAD Center (ft.)	Antennas and Equipment	Coax	Mount
56	26T-2400 (4' Grid Dish)	(1) 7/8"	(1) Standoff
54	7' Omni 6' Dipole	(2) 7/8"	(2) Standoff

#### 3.0 **CODES AND LOADING**

This analysis has been performed in accordance with the 2018 Connecticut State Building Code (2015 IBC) based upon an ultimate 3-second gust wind speed of 135 mph (Risk Category II) converted to a nominal 3-second gust wind speed of 105 mph per section 1609.3.1 as required for use in the ANSI/TIA-222-G Standard per Exception #5 of Section 1609.1.1. The following loading criteria were used in the analysis:

- Basic wind speed 105 mph without ice (V)
- Basic wind speed 50 mph concurrent with design ice thickness 3/4" (V<sub>i</sub> and t<sub>i</sub>)
- Exposure Category C, Structural Class II, I=1.0
- Topographic Category 1, K<sub>zt</sub>=1.0

The following load combinations were used with wind blowing at 30° increment measured from a line normal to the face of the smokestack.

- 1.2 D + 1.6 W<sub>0</sub>
- 0.9 D + 1.6 W<sub>0</sub>
- 1.2 D + 1.0 D<sub>i</sub> + 1.0 W<sub>i</sub>

D: Dead Load of structure and appurtenances

W<sub>0</sub>: Wind Load, without ice W<sub>i</sub>: Wind Load, with ice

D<sub>i</sub>: Weight of Ice

# 4.0 STANDARD CONDITIONS FOR ENGINEERING SERVICES ON EXISTING STRUCTURES

The analysis is based on the information provided to EFI and is assumed to be current and correct. Unless otherwise noted, the structure and the foundation system are assumed to be in good condition, free of defects and can achieve theoretical strength.

It is assumed that the structure has been maintained and shall be maintained during its service. The superstructure and the foundation system are assumed to be designed with proper engineering practice and fabricated, constructed and erected in accordance with the design documents. EFI will accept no liability which may arise due to any existing deficiency in design, material, fabrication, erection, construction, etc. or lack of maintenance.

The analysis does not include a qualification of the mounts attached on the structure or their connections. The analysis is performed to verify the capacity of the main structural members, which is the current practice in the tower industry.

The analysis results presented in this report are only applicable for the previously mentioned existing and proposed additions and alterations. Any deviation of the proposed equipment and placement, etc., will require EFI to generate an additional structural analysis.

# 5.0 **ANALYSIS AND ASSUMPTIONS**

The tower was analyzed by utilizing tnxTower, a non-linear, three-dimensional, finite elementanalysis software package, a product of Tower Numerics, Inc. Software output for this analysis is provided in Appendix A of this report.

Tower Leg connections are considered designed to meet the full capacity of the adjoining leg members.

Page | 3 EFI GLOBAL, INC.

# 6.0 RESULTS AND CONCLUSION

Based on a structural analysis per ANSI/TIA-222-G, the existing self-support tower will have adequate structural capacity for the proposed changes by T-Mobile, once it has been upgraded in accordance with the upgrade drawings attached with this report, dated 03/05/2021. For the code specified load combinations and as a maximum, the tower legs are stressed to 85.3% of their structural capacities. The tower diagonals, anchor bolts and horizontals are stressed to 72.4%, 57.7% & 8.0% of their structural capacities, respectively.

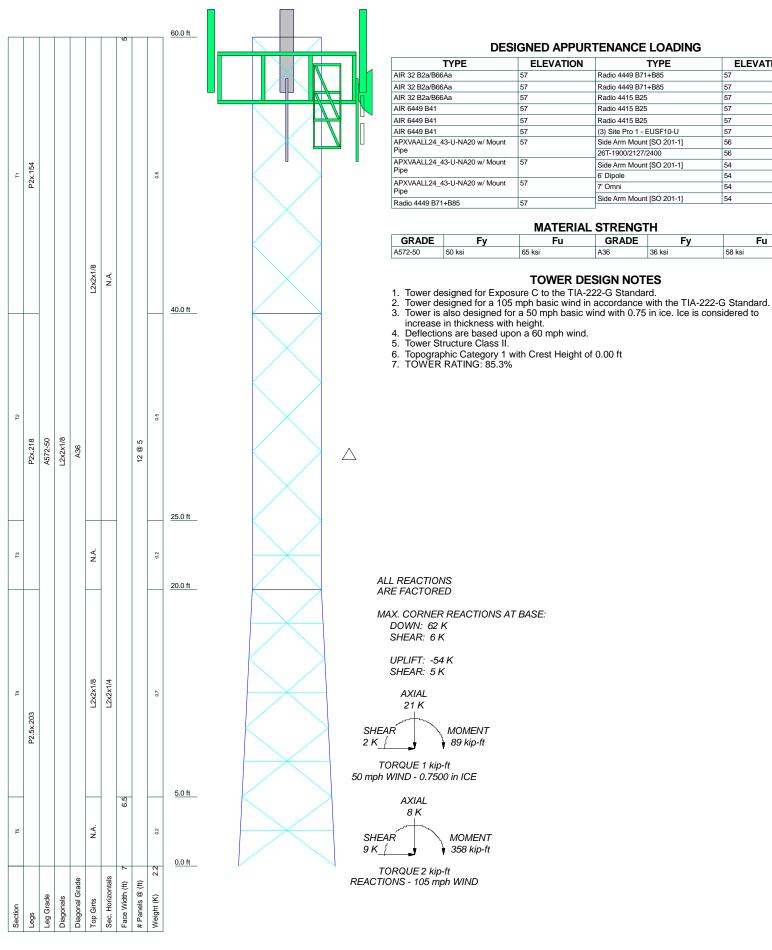
The existing base foundation has **adequate** structural capacity for the proposed changes by T-Mobile. For the code specified load combinations and as a maximum, the base foundation is stressed to **65.7%** of its structural capacity.

Therefore, the additions and alterations proposed by T-Mobile **can** be implemented as intended and with the conditions outlined in this report.

Should you need any clarifications or have any questions about this report, please contact EFI at <a href="mailto:telecom@efiglobal.com">telecom@efiglobal.com</a>.

Page | 4 EFI GLOBAL, INC.

# APPENDIX A SOFTWARE OUTPUT



Job: CTNL041A		
Project: <b>049.00940</b>		
Client: T-Mobile	Drawn by: Ahmet Colakoglu	App'd:
Code: TIA-222-G	Date: 03/05/21	Scale: NT
Path:	company Strategy (1995). Control   Child (1996), 1996, CTM (1996) Charles (1997) (1994), Lorente	Dwg No. E

EFI Global, INC

Atlanta, GA Phone: 770-693-0835 FAX:

one efi global 1117 Perimeter Center West, Ste E500

**ELEVATION** 

Fu

57

57

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56

56

54

54

54

54

Fy

Radio 4449 B71+B85

Radio 4449 B71+B85

(3) Site Pro 1 - EUSF10-U

26T-1900/2127/2400

Side Arm Mount [SO 201-1]

Side Arm Mount [SO 201-1]

Side Arm Mount [SO 201-1]

Radio 4415 B25

Radio 4415 B25

Radio 4415 B25

6' Dipole

7' Omni

GRADE

4			
tnx1	n	142	or
	U		

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FAX:

Job		Page
	CTNL041A	1 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

# **Tower Input Data**

The main tower is a 3x free standing tower with an overall height of 60.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 5.00 ft at the top and 7.00 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Basic wind speed of 105 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

# **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

√ Use Code Stress Ratios

√ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz

Use Special Wind Profile

√ Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section

√ Secondary Horizontal Braces Leg
 Use Diamond Inner Bracing (4 Sided)
 SR Members Have Cut Ends
 SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned

√ Assume Rigid Index Plate

√ Use Clear Spans For Wind Area

√ Use Clear Spans For KL/r
Retension Guys To Initial Tension

√ Bypass Mast Stability Checks

√ Use Azimuth Dish Coefficients

✓ Project Wind Area of Appurt.
 Autocalc Torque Arm Areas
 Add IBC .6D+W Combination

√ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs Use ASCE 10 X-Brace Ly Rules

√ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA

√ SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation

√ Consider Feed Line Torque

√ Include Angle Block Shear Check
Use TIA-222-G Bracing Resist. Exemption
Use TIA-222-G Tension Splice Exemption
Poles

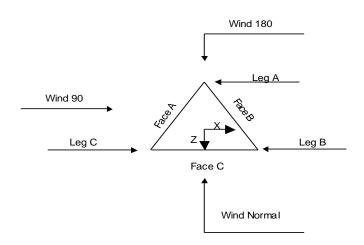
Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

# tnxTower

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1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	2 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu



Triangular Tower

	Tower Section Geometry										
Tower	Tower	Assembly	Description	Section	Number	Section					
Section	Elevation	Database	•	Width	of	Length					
					Sections						
	ft			ft		ft					
T1	60.00-40.00			5.00	1	20.00					
T2	40.00-25.00			5.00	1	15.00					
T3	25.00-20.00			5.00	1	5.00					
T4	20.00-5.00			5.00	1	15.00					
T5	5.00-0.00			6.50	1	5.00					

	Tower Section Geometry (cont'd)												
Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt						
Section	Elevation	Spacing	Type	K Brace	Horizontals	Offset	Offset						
				End									
	ft	ft		Panels		in	in						
T1	60.00-40.00	5.00	X Brace	No	Steps	0.0000	0.0000						
T2	40.00-25.00	5.00	X Brace	No	Yes	0.0000	0.0000						
T3	25.00-20.00	5.00	X Brace	No	Yes	0.0000	0.0000						
T4	20.00-5.00	5.00	X Brace	No	Yes	0.0000	0.0000						
T5	5.00-0.00	5.00	X Brace	No	Yes	0.0000	0.0000						

# Tower Section Geometry (cont'd)

# tnxTower

**EFI Global, INC** 1117 Perimeter Center West, Ste E500

Atlanta, GA Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	3 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 60.00-40.00	Pipe	P2x.154	A572-50 (50 ksi)	Single Angle	L2x2x1/8	A36 (36 ksi)
T2 40.00-25.00	Pipe	P2x.218	A572-50 (50 ksi)	Single Angle	L2x2x1/8	A36 (36 ksi)
T3 25.00-20.00	Pipe	P2x.218	A572-50 (50 ksi)	Single Angle	L2x2x1/8	A36 (36 ksi)
T4 20.00-5.00	Pipe	P2.5x.203	A572-50 (50 ksi)	Single Angle	L2x2x1/8	A36 (36 ksi)
T5 5.00-0.00	Pipe	P2.5x.203	A572-50 (50 ksi)	Single Angle	L2x2x1/8	A36 (36 ksi)

		Tower	Section C	Seometry (	(cont'd)	
Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
Г1 60.00-40.00	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A36 (36 ksi)
T2 40.00-25.00	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A36 (36 ksi)
T4 20.00-5.00	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A36 (36 ksi)

	Tower Section Geometry (cont'd)										
Tower Elevation	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade					
<u>π</u> T3 25.00-20.00	Equal Angle	L2x2x1/4	A36	Solid Round		A572-50					
T4 20 00 5 00	F 14 1	10014	(36 ksi)	0.11.1.0		(50 ksi)					
T4 20.00-5.00	Equal Angle	L2x2x1/4	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)					
T5 5.00-0.00	Equal Angle	L2x2x1/4	A36	Solid Round		A572-50					
			(36 ksi)			(50 ksi)					

ngle Double Angle
Solt Stitch Bolt
ig Spacing
tals Redundants
in
36.0000
36.0000
3

# *tnxTower*

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> Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	4 of 20
Project	049.00940 - 2075089	<b>Date</b> 16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	$Adjust.\ Factor \ A_f$	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing	Double Angle Stitch Bolt Spacing	Double Angle Stitch Bolt Spacing
ft	$ft^2$	in			•		Diagonals in	Horizontals in	Redundants in
T3 25.00-20.00	0.00	0.0000	(36 ksi) A36 (36 ksi)	1.03	1	1.05	36.0000	36.0000	36.0000
T4 20.00-5.00	0.00	0.0000	A36 (36 ksi)	1.03	1	1.05	36.0000	36.0000	36.0000
T5 5.00-0.00	0.00	0.0000	A36 (36 ksi)	1.03	1	1.05	36.0000	36.0000	36.0000

# **Tower Section Geometry** (cont'd)

						K Fac	ctors <sup>1</sup>			
Tower	Calc	Calc	Legs	X	K	Single	Girts	Horiz.	Sec.	Inner
Elevation	K	K	_	Brace	Brace	Diags			Horiz.	Brace
	Single	Solid		Diags	Diags					
	Angles	Rounds		X	X	X	X	X	X	X
ft				Y	Y	Y	Y	Y	Y	Y
T1	No	No	1	1	1	1	1	1	1	1
60.00-40.00				1	1	1	1	1	1	1
T2	No	No	1	1	1	1	1	1	1	1
40.00-25.00				1	1	1	1	1	1	1
T3	No	No	1	1	1	1	1	1	1	1
25.00-20.00				1	1	1	1	1	0.5	1
T4 20.00-5.00	No	No	1	1	1	1	1	1	1	1
				1	1	1	1	1	0.5	1
Γ5 5.00-0.00	No	No	1	1	1	1	1	1	1	1
				1	1	1	1	1	0.5	1

<sup>&</sup>lt;sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

# **Tower Section Geometry** (cont'd)

Tower Elevation ft	Leg		Diago	nal	Top G	irt	Botton	ı Girt	Mid	Girt	Long Ho	rizontal	Short Ho	rizontal
J.	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 60.00-40.00		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 40.00-25.00 T3 25.00-20.00		1	0.0000	0.75 0.75	0.0000	0.75 0.75	0.0000	0.75 0.75	0.0000	0.75 0.75	0.0000	0.75 0.75	0.0000	0.75 0.75
T4 20.00-5.00		1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 5.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

# **Tower Section Geometry** (cont'd)

**EFI Global, INC**1117 Perimeter Center West, Ste E500

Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	5 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T Makila	Designed by
	T-Mobile	Ahmet Colakoglu

Tower	Leg	Leg		Diagon	ıal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hori	zontal	Short Hori	izontal
Elevation	Connection														
ft	Type														
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T1 60.00-40.00	Sleeve DS	0.0000	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325N		A325N		A325N		A325N	
T2 40.00-25.00	Flange	0.5000	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325N		A325N		A325N		A325N	
T3 25.00-20.00	Flange	0.5000	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325N		A325N		A325N		A325N	
T4 20.00-5.00	Flange	0.5000	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325N		A325N		A325N		A325N	
T5 5.00-0.00	Flange	0.5000	0	0.6250	1	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325N		A325N		A325N		A325N	

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or	Allow Shield	Exclude From	Component Type	Placement	Face Offset	Lateral Offset	#	# Per	Clear Spacing	Width or Diameter	Perimeter	Weight
	Leg		Torque Calculation		ft	in	(Frac FW)		Row	in	in	in	plf
RFS HYBRIFLEX 1 1/4	С	No	No	Ar (CaAa)	59.00 - 0.00	-1.0000	0.45	3	3	0.5000 1.5400	1.5400		1.30
Feedline Ladder (Af) ***	С	No	No	Af (CaAa)	59.00 - 0.00	-1.0000	0.45	1	1	3.0000	3.0000		8.40
VXL5-50(7/8)	В	No	No	Ar (CaAa)	54.00 - 0.00	-1.0000	0.45	3	3	0.5000 1.0800	1.0800		0.29
VXL5-50(7/8)	В	No	No	Ar (CaAa)	56.00 - 54.00	-1.0000	0.45	1	1	0.5000 1.0800	1.0800		0.29
Feedline Ladder (Af) ****	В	No	No	Af (CaAa)	56.00 - 0.00	-1.0000	0.45	1	1	3.0000	3.0000		8.40

## Feed Line/Linear Appurtenances - Entered As Area

Description	Face	Allow	Exclude	Component	Placement	Total	$C_A A_A$	Weight
	or	Shield	From	Type		Number		
	Leg		Torque		ft		ft <sup>2</sup> /ft	plf
			Calculation					
****								

## Feed Line/Linear Appurtenances Section Areas

Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft <sup>2</sup>	ft <sup>2</sup>	€t²	ft <sup>2</sup>	V
	Ji		jι	jι	jι	jι	A

EFI Global, INC 1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835

FAX:

	Job		Page
		CTNL041A	6 of 20
	Project		Date
)		049.00940 - 2075089	16:48:44 03/05/21
	Client	T-Mobile	Designed by Ahmet Colakoglu

Tower Section	Tower Elevation	Face	$A_R$	$A_F$	$C_AA_A$ In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
section	ft Elevation		ft²	$ft^2$	ft <sup>2</sup>	ft <sup>2</sup>	K
		В	0.000	0.000	12.741	0.000	0.15
		C	0.000	0.000	18.278	0.000	0.23
T2	40.00-25.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	12.360	0.000	0.14
		C	0.000	0.000	14.430	0.000	0.18
T3	25.00-20.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	4.120	0.000	0.05
		C	0.000	0.000	4.810	0.000	0.06
T4	20.00-5.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	12.360	0.000	0.14
		C	0.000	0.000	14.430	0.000	0.18
T5	5.00-0.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	4.120	0.000	0.05
		C	0.000	0.000	4.810	0.000	0.06

## Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	$ft^2$	$ft^2$	ft <sup>2</sup>	ft <sup>2</sup>	K
T1	60.00-40.00	A	1.564	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	28.403	0.000	0.46
		C		0.000	0.000	38.989	0.000	0.67
T2	40.00-25.00	A	1.498	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	27.564	0.000	0.43
		C		0.000	0.000	30.249	0.000	0.51
T3	25.00-20.00	A	1.444	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	9.042	0.000	0.14
		C		0.000	0.000	9.938	0.000	0.16
T4	20.00-5.00	A	1.361	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	26.458	0.000	0.40
		C		0.000	0.000	29.149	0.000	0.47
T5	5.00-0.00	A	1.159	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	8.275	0.000	0.12
		C		0.000	0.000	9.175	0.000	0.14

## **Feed Line Center of Pressure**

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
T1	60.00-40.00	-1.9433	4.1283	-2.2811	5.0117
T2	40.00-25.00	-1.3336	4.6014	-1.5183	5.5359
T3	25.00-20.00	-1.2324	4.2696	-1.3776	4.9354
T4	20.00-5.00	-1.2256	4.3572	-1.4555	5.2154
T5	5.00-0.00	-1.3408	4.9033	-1.7611	6.0394

## **Shielding Factor Ka**

**EFI Global, INC** 1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	7 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu

Tower	Feed Line	Description	Feed Line	$K_a$	$K_a$
Section	Record No.	•	Segment Elev.	No Ice	Ice
T1	1	RFS HYBRIFLEX 1 1/4	40.00 - 59.00	0.6000	0.5979
T1	2	Feedline Ladder (Af)	40.00 - 59.00	0.6000	0.5979
T1	4	VXL5-50(7/8)	40.00 - 54.00	0.6000	0.5979
T1	5	VXL5-50(7/8)	54.00 - 56.00	0.6000	0.5979
T1	6	Feedline Ladder (Af)	40.00 - 56.00	0.6000	0.5979
T2	1	RFS HYBRIFLEX 1 1/4	25.00 - 40.00	0.6000	0.6000
T2	2	Feedline Ladder (Af)	25.00 - 40.00	0.6000	0.6000
T2	4	VXL5-50(7/8)	25.00 - 40.00	0.6000	0.6000
T2	6	Feedline Ladder (Af)	25.00 - 40.00	0.6000	0.6000
T3	1	RFS HYBRIFLEX 1 1/4	20.00 - 25.00	0.6000	0.5600
T3	2	Feedline Ladder (Af)	20.00 - 25.00	0.6000	0.5600
T3	4	VXL5-50(7/8)	20.00 - 25.00	0.6000	0.5600
T3	6	Feedline Ladder (Af)	20.00 - 25.00	0.6000	0.5600
T4	1	RFS HYBRIFLEX 1 1/4	5.00 - 20.00	0.6000	0.5710
T4	2	Feedline Ladder (Af)	5.00 - 20.00	0.6000	0.5710
T4	4	VXL5-50(7/8)	5.00 - 20.00	0.6000	0.5710
T4	6	Feedline Ladder (Af)	5.00 - 20.00	0.6000	0.5710
T5	1	RFS HYBRIFLEX 1 1/4	0.00 - 5.00	0.6000	0.6000
T5	2	Feedline Ladder (Af)	0.00 - 5.00	0.6000	0.6000
T5	4	VXL5-50(7/8)	0.00 - 5.00	0.6000	0.6000
T5	6	Feedline Ladder (Af)	0.00 - 5.00	0.6000	0.6000

<b>D</b> :	_	
Licerata	IOWAR	I ASAC
Discrete	iowei	LUAUS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	$C_AA_A$ Side	Weight
			ft ft ft	0	ft		ft <sup>2</sup>	ft <sup>2</sup>	K
AIR 32 B2a/B66Aa	A	From Leg	3.50 0.00 2.00	0.0000	57.00	No Ice 1/2" Ice 1" Ice	3.86 4.23 4.61	2.51 2.86 3.22	0.17 0.22 0.27
AIR 32 B2a/B66Aa	В	From Leg	3.50 0.00	0.0000	57.00	No Ice 1/2" Ice	3.86 4.23	2.51 2.86	0.17 0.22
AIR 32 B2a/B66Aa	C	From Leg	2.00 3.50 0.00	0.0000	57.00	1" Ice No Ice 1/2" Ice	4.61 3.86 4.23	3.22 2.51 2.86	0.27 0.17 0.22
AIR 6449 B41	A	From Leg	2.00 3.50 0.00	0.0000	57.00	1" Ice No Ice 1/2" Ice	4.61 5.65 5.96	3.22 2.42 2.64	0.27 0.10 0.14
AIR 6449 B41	В	From Leg	2.00 3.50 0.00	0.0000	57.00	1" Ice No Ice 1/2" Ice	6.26 5.65 5.96	2.87 2.42 2.64	0.18 0.10 0.14
AIR 6449 B41	C	From Leg	2.00 3.50 0.00	0.0000	57.00	1" Ice No Ice 1/2" Ice	6.26 5.65 5.96	2.87 2.42 2.64	0.18 0.10 0.14
APXVAALL24_43-U-NA20 w/ Mount Pipe	A	From Leg	2.00 3.50 0.00 0.00	0.0000	57.00	1" Ice No Ice 1/2" Ice 1" Ice	6.26 14.69 15.46 16.23	2.87 6.87 7.55	0.18 0.18 0.31 0.45
APXVAALL24_43-U-NA20 w/ Mount Pipe	В	From Leg	3.50 0.00	0.0000	57.00	No Ice 1/2" Ice	14.69 15.46	8.25 6.87 7.55	0.45 0.18 0.31

**EFI Global, INC** 1117 Perimeter Center West, Ste E500

Atlanta, GA Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	8 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	0	ft		ft²	ft <sup>2</sup>	K
			0.00			1" Ice	16.23	8.25	0.45
APXVAALL24_43-U-NA20	C	From Leg	3.50	0.0000	57.00	No Ice	14.69	6.87	0.18
w/ Mount Pipe			0.00			1/2" Ice	15.46	7.55	0.31
•			0.00			1" Ice	16.23	8.25	0.45
Radio 4449 B71+B85	A	From Leg	3.50	0.0000	57.00	No Ice	1.97	1.59	0.07
		· ·	0.00			1/2" Ice	2.15	1.75	0.09
			2.00			1" Ice	2.33	1.92	0.12
Radio 4449 B71+B85	В	From Leg	3.50	0.0000	57.00	No Ice	1.97	1.59	0.07
			0.00			1/2" Ice	2.15	1.75	0.09
			2.00			1" Ice	2.33	1.92	0.12
Radio 4449 B71+B85	C	From Leg	3.50	0.0000	57.00	No Ice	1.97	1.59	0.07
			0.00			1/2" Ice	2.15	1.75	0.09
			2.00			1" Ice	2.33	1.92	0.12
Radio 4415 B25	A	From Leg	3.50	0.0000	57.00	No Ice	1.64	0.68	0.05
114410 1110 220		Trom Leg	0.00	0.0000	27.00	1/2" Ice	1.80	0.79	0.06
			2.00			1" Ice	1.97	0.91	0.07
Radio 4415 B25	В	From Leg	3.50	0.0000	57.00	No Ice	1.64	0.68	0.05
Radio 1113 B23	Ь	Troin Leg	0.00	0.0000	37.00	1/2" Ice	1.80	0.79	0.06
			2.00			1" Ice	1.97	0.91	0.07
Radio 4415 B25	C	From Leg	3.50	0.0000	57.00	No Ice	1.64	0.68	0.05
Radio 4413 B23	C	1 Tolli Leg	0.00	0.0000	37.00	1/2" Ice	1.80	0.79	0.06
			0.00			1" Ice	1.97	0.75	0.07
(3) Site Pro 1 - EUSF10-U	C	None	0.00	0.0000	57.00	No Ice	17.82	17.82	0.80
(3) Site 110 1 - EUSI-10-U	C	None		0.0000	37.00	1/2" Ice	25.01	25.01	1.14
						1" Ice	32.11	32.11	1.60
*** 56 ft ***						1 100	32.11	32.11	1.00
Side Arm Mount [SO 201-1]	В	From Leg	0.50	0.0000	56.00	No Ice	1.78	2.61	0.10
Side Aiii Would [SO 201-1]	ь	Fioni Leg	0.00	0.0000	30.00	1/2" Ice	2.24	3.15	0.10
			0.00			1" Ice	2.75	3.73	0.12
*** 54 ft ***			0.00			1 Ice	2.73	3.73	0.14
Side Arm Mount [SO 201-1]	A	Enom I ao	0.50	0.0000	54.00	No Ice	1.78	2.61	0.10
Side Ariii Mount [SO 201-1]	Α	From Leg		0.0000	34.00				
			0.00			1/2" Ice	2.24	3.15	0.12
G' 1 A M + FGO 201 11	D	г т	0.00	0.0000	54.00	1" Ice	2.75	3.73	0.14
Side Arm Mount [SO 201-1]	В	From Leg	0.50	0.0000	54.00	No Ice	1.78	2.61	0.10
			0.00			1/2" Ice	2.24	3.15	0.12
CID: 1	D	г т	0.00	0.0000	54.00	1" Ice	2.75	3.73	0.14
6' Dipole	В	From Leg	3.00	0.0000	54.00	No Ice	1.20	1.20	0.02
			0.00			1/2" Ice	1.80	1.80	0.03
<b>5</b> 1.0 ·			0.00	0.0000	74.00	1" Ice	2.40	2.40	0.04
7' Omni	A	From Leg	3.00	0.0000	54.00	No Ice	1.74	1.74	0.04
			0.00			1/2" Ice	2.60	2.60	0.05
			0.00			1" Ice	3.46	3.46	0.07

Dishes											
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				Vert ft	٥	٥	ft	ft		ft²	K
26T-1900/2127/2400	В	Grid	From	3.00	0.0000		56.00	3.27	No Ice	8.40	0.00

### EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835

FAX:

Job		Page
	CTNL041A	9 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	۰	0	ft	ft		$ft^2$	K
			Leg	0.00					1/2" Ice	8.84	0.05
				0.00					1" Ice	9.27	0.10

## **Load Combinations**

Comb.	Description
No.	·
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36 37	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
38 39	Dead+Wind 0 deg - Service
40	Dead+Wind 0 deg - Service  Dead+Wind 30 deg - Service
41	Dead+Wind 50 deg - Service  Dead+Wind 60 deg - Service
42	Dead+Wind 00 deg - Service  Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service  Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service  Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
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### EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	10 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T 84 1 11	Designed by
	T-Mobile	Ahmet Colakoglu

Comb.		Description	
No.			
50	Dead+Wind 330 deg - Service		

## **Maximum Member Forces**

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
	v			Comb.	K	kip-ft	kip-ft
T1	60 - 40	Leg	Max Tension	7	12.81	-0.06	0.02
		C	Max. Compression	10	-15.76	-0.06	-0.02
			Max. Mx	20	-1.74	-0.88	0.01
			Max. My	14	-1.63	0.02	0.88
			Max. Vy	20	-0.79	0.55	0.01
			Max. Vx	2	-0.81	-0.01	0.58
		Diagonal	Max Tension	7	2.40	0.00	0.00
		Ü	Max. Compression	18	-2.57	0.00	0.00
			Max. Mx	31	0.32	0.02	0.00
			Max. My	24	-2.19	0.00	-0.00
			Max. Vy	31	-0.02	0.02	0.00
			Max. Vx	24	0.00	0.00	-0.00
		Top Girt	Max Tension	23	0.11	0.00	0.00
		1	Max. Compression	18	-0.15	0.00	0.00
			Max. Mx	27	-0.11	-0.03	0.00
			Max. My	18	0.04	0.00	-0.00
			Max. Vy	27	0.03	0.00	0.00
		Max. Vx	18	0.00	0.00	0.00	
T2	40 - 25	Leg	Max Tension	15	31.90	0.00	0.05
12 10 2		- 8	Max. Compression	10	-36.24	0.06	0.04
			Max. Mx	8	-1.63	-0.21	-0.02
			Max. My	24	-1.82	0.09	0.20
			Max. Vy	8	0.06	-0.21	-0.02
			Max. Vx	24	-0.07	0.09	0.20
		Diagonal	Max Tension	20	3.03	0.00	0.00
		8	Max. Compression	20	-3.06	0.00	0.00
			Max. Mx	10	-2.52	-0.03	-0.01
			Max. My	20	-3.03	-0.02	0.01
			Max. Vy	31	-0.02	0.02	0.00
			Max. Vx	20	-0.00	-0.02	0.01
		Top Girt	Max Tension	6	0.36	0.00	0.00
		1	Max. Compression	11	-0.35	0.00	0.00
			Max. Mx	26	0.10	-0.03	0.00
			Max. My	18	0.21	0.00	-0.00
			Max. Vy	26	0.02	0.00	0.00
			Max. Vx	18	0.00	0.00	0.00
T3	25 - 20	Leg	Max Tension	15	38.40	0.00	-0.25
		8	Max. Compression	10	-43.17	0.11	0.07
			Max. Mx	10	-43.15	-0.25	-0.14
			Max. My	2	-42.82	-0.00	0.28
			Max. Vy	10	-0.15	-0.25	-0.14
			Max. Vx	2	0.17	-0.00	0.28
		Diagonal	Max Tension	21	3.30	0.02	-0.00
			Max. Compression	18	-3.55	0.00	0.00
			Max. Mx	18	2.69	0.05	-0.01
			Max. My	7	-2.00	-0.03	-0.02
			Max. Vy	31	-0.02	0.03	0.00
			Max. Vx	7	0.00	-0.03	-0.02
		Secondary Horizontal	Max Tension	10	0.75	0.00	0.00
			Max. Compression	10	-0.75	0.01	-0.01
			Max. Mx	16	-0.04	0.04	-0.00

EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	11 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
			Man Ma	Comb.	K 0.75	kip-ft 0.02	kip-ft
			Max. My	18 34	-0.75 -0.02	0.02	-0.02 -0.00
			Max. Vy Max. Vx		0.02	0.03	
T4	20 - 5	Leg	Max Tension	18 15	49.98	-0.46	0.00 -0.00
14	20 - 3	Leg	Max. Compression	18	-56.21	-0.40	0.00
			Max. Mx	10	-52.86	0.56	-0.00
			Max. My	16	-2.28	-0.05	0.49
			Max. Vy	10	-0.42	0.56	-0.00
			Max. Vx	16	0.42	-0.05	0.49
		Diagonal	Max Tension	7	1.88	0.03	-0.01
		Diagonai	Max. Compression	18	-2.10	0.00	0.00
			Max. Mx	18	1.40	0.04	-0.01
			Max. My	18	-2.10	-0.03	0.02
			Max. Vy	33	0.02	0.02	-0.00
			Max. Vx	18	0.00	0.00	0.00
		Secondary Horizontal	Max Tension	18	0.97	0.00	0.00
			Max. Compression	18	-0.97	-0.01	-0.01
			Max. Mx	6	0.49	0.03	-0.01
			Max. My	4	-0.41	0.02	0.01
			Max. Vy	31	0.03	0.03	0.00
			Max. Vx	16	-0.00	0.00	0.00
		Top Girt	Max Tension	33	0.14	0.00	0.00
			Max. Compression	10	-0.14	0.00	0.00
			Max. Mx	26	0.13	-0.03	0.00
			Max. My	29	0.12	0.00	0.00
			Max. Vy	26	0.02	0.00	0.00
			Max. Vx	29	-0.00	0.00	0.00
T5	5 - 0	Leg	Max Tension	15	52.81	-0.39	-0.00
			Max. Compression	18	-59.53	0.00	0.00
			Max. Mx	18	-59.52	0.46	0.00
			Max. My	16	-2.67	-0.04	0.47
			Max. Vy	18	-0.37	0.46	0.00
			Max. Vx	16	0.23	-0.04	0.47
		Diagonal	Max Tension	7	1.77	0.02	-0.00
			Max. Compression	18	-2.00	0.00	0.00
			Max. Mx	18	1.28	0.03	-0.01
			Max. My	18	0.77	0.03	0.01
			Max. Vy	31	-0.02	0.02	0.00
		G 1	Max. Vx	18	-0.00	0.00	0.00
		Secondary Horizontal	Max Tension	18	1.03	0.00	0.00
			Max. Compression	18	-1.03	0.02	-0.01
			Max. Mx	6	0.52	0.03	-0.00
			Max. My	16	-0.37	-0.01	0.01
			Max. Vy	31	0.02	0.00	0.00
			Max. Vx	16	-0.00	0.00	0.00

## **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	K	K	K
		Comb.			
Leg C	Max. Vert	18	61.54	5.09	-2.70
_	Max. H <sub>x</sub>	18	61.54	5.09	-2.70
	Max. H <sub>z</sub>	7	-53.96	-4.49	2.36
	Min. Vert	7	-53.96	-4.49	2.36

**EFI Global, INC** 1117 Perimeter Center West, Ste E500

Atlanta, GA
Phone: 770-693-0835
FAX:

Job		Page
	CTNL041A	12 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	K	K	K
		Comb.			
	Min. H <sub>x</sub>	7	-53.96	-4.49	2.36
	Min. H <sub>z</sub>	18	61.54	5.09	-2.70
Leg B	Max. Vert	10	61.41	-5.01	-2.77
•	Max. H <sub>x</sub>	23	-53.53	4.39	2.42
	Max. H <sub>z</sub>	23	-53.53	4.39	2.42
	Min. Vert	23	-53.53	4.39	2.42
	Min. H <sub>x</sub>	10	61.41	-5.01	-2.77
	Min. H <sub>z</sub>	10	61.41	-5.01	-2.77
Leg A	Max. Vert	2	61.29	0.05	5.77
•	Max. H <sub>x</sub>	23	29.34	0.21	2.68
	Max. H <sub>z</sub>	2	61.29	0.05	5.77
	Min. Vert	15	-54.48	-0.05	-5.10
	Min. H <sub>x</sub>	11	-27.55	-0.21	-2.65
	Min. Hz	15	-54.48	-0.05	-5.10

## **Tower Mast Reaction Summary**

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, $M_x$	Overturning Moment, $M_z$	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	6.31	-0.00	-0.00	1.56	-0.16	-0.00
1.2 Dead+1.6 Wind 0 deg - No	7.58	0.01	-8.98	-356.27	-0.53	0.62
Ice						
0.9 Dead+1.6 Wind 0 deg - No	5.68	0.01	-8.98	-356.18	-0.48	0.62
Ice						
1.2 Dead+1.6 Wind 30 deg - No Ice	7.58	4.33	-7.44	-297.74	-174.99	1.76
0.9 Dead+1.6 Wind 30 deg - No	5.68	4.33	-7.44	-297.75	-174.67	1.75
Ice						
1.2 Dead+1.6 Wind 60 deg - No	7.58	7.23	-4.16	-167.23	-294.81	2.48
Ice						
0.9 Dead+1.6 Wind 60 deg - No	5.68	7.23	-4.16	-167.44	-294.30	2.47
Ice						
1.2 Dead+1.6 Wind 90 deg - No	7.58	8.37	-0.01	1.55	-340.96	2.04
Ice						
0.9 Dead+1.6 Wind 90 deg - No	5.68	8.37	-0.01	1.08	-340.37	2.04
Ice						
1.2 Dead+1.6 Wind 120 deg -	7.58	7.69	4.42	179.24	-308.72	1.26
No Ice				.=		
0.9 Dead+1.6 Wind 120 deg -	5.68	7.69	4.42	178.49	-308.19	1.26
No Ice	<b>7.</b> 50	4.00	<b>7.00</b>	200.46	172.22	0.55
1.2 Dead+1.6 Wind 150 deg -	7.58	4.23	7.32	299.16	-172.22	0.65
No Ice	5.68	4.23	7.32	298.22	-171.90	0.65
0.9 Dead+1.6 Wind 150 deg - No Ice	3.08	4.23	7.32	298.22	-1/1.90	0.03
1.2 Dead+1.6 Wind 180 deg -	7.58	0.00	8.38	342.73	-0.36	-0.61
No Ice	7.56	0.00	0.50	342.73	-0.50	-0.01
0.9 Dead+1.6 Wind 180 deg -	5.68	0.00	8.38	341.73	-0.31	-0.61
No Ice	5.00	0.00	0.50	341.73	0.51	0.01
1.2 Dead+1.6 Wind 210 deg -	7.58	-4.30	7.46	302.40	173.06	-1.76
No Ice						
0.9 Dead+1.6 Wind 210 deg -	5.68	-4.30	7.46	301.46	172.84	-1.75
No Ice						
1.2 Dead+1.6 Wind 240 deg -	7.58	-7.74	4.46	180.10	309.14	-2.49
No Ice						
0.9 Dead+1.6 Wind 240 deg -	5.68	-7.74	4.46	179.35	308.71	-2.48
No Ice						

### EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	13 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning Moment, M <sub>x</sub>	Overturning Moment, Mz	Torque
Como unamon	K	K	K	kip-ft	kip-ft	kip-ft
1.2 Dead+1.6 Wind 270 deg -	7.58	-8.37	0.02	2.77	340.57	-2.09
No Ice						
0.9 Dead+1.6 Wind 270 deg -	5.68	-8.37	0.02	2.30	340.09	-2.09
No Ice						
1.2 Dead+1.6 Wind 300 deg -	7.58	-7.15	-4.11	-166.20	292.29	-1.26
No Ice						
0.9 Dead+1.6 Wind 300 deg -	5.68	-7.15	-4.11	-166.41	291.88	-1.26
No Ice						
1.2 Dead+1.6 Wind 330 deg -	7.58	-4.22	-7.32	-295.67	171.36	-0.60
No Ice						
0.9 Dead+1.6 Wind 330 deg -	5.68	-4.22	-7.32	-295.68	171.14	-0.60
No Ice						
1.2 Dead+1.0 Ice+1.0 Temp	20.79	-0.00	-0.00	5.30	-1.25	-0.00
1.2 Dead+1.0 Wind 0 deg+1.0	20.79	-0.06	-2.16	-81.69	2.26	0.07
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 30 deg+1.0	20.79	1.04	-1.80	-67.34	-43.38	0.52
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 60 deg+1.0	20.79	1.78	-1.02	-36.11	-73.69	0.76
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 90 deg+1.0	20.79	2.05	-0.00	5.19	-84.59	0.64
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 120	20.79	1.81	1.04	47.65	-74.85	0.35
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 150	20.79	1.03	1.78	77.86	-43.15	0.11
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 180	20.79	0.00	2.07	89.20	-1.48	-0.17
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 210	20.79	-1.04	1.80	77.99	40.81	-0.52
deg+1.0 Ice+1.0 Temp	20.50	4.00	4.00	45.40	77. TO	0.55
1.2 Dead+1.0 Wind 240	20.79	-1.89	1.02	45.43	75.52	-0.66
deg+1.0 Ice+1.0 Temp	20.50	2.05	0.04	2.24	02.42	0.40
1.2 Dead+1.0 Wind 270	20.79	-2.07	-0.04	3.24	83.43	-0.49
deg+1.0 Ice+1.0 Temp	20.70	1.70	1.00	26.70	71.01	0.25
1.2 Dead+1.0 Wind 300	20.79	-1.78	-1.02	-36.79	71.91	-0.35
deg+1.0 Ice+1.0 Temp	20.70	1.00	1.70	(7.22	42.21	0.26
1.2 Dead+1.0 Wind 330	20.79	-1.08	-1.79	-67.32	43.21	-0.26
deg+1.0 Ice+1.0 Temp	c 21	0.00	1.02	-71.45	0.22	0.12
Dead+Wind 0 deg - Service	6.31	0.00	-1.83		-0.23	0.13
Dead+Wind 30 deg - Service	6.31	0.88	-1.52	-59.52	-35.80	0.36
Dead+Wind 60 deg - Service	6.31	1.48	-0.85	-32.91	-60.22	0.50
Dead+Wind 90 deg - Service	6.31	1.71	-0.00	1.50	-69.63	0.42
Dead+Wind 120 deg - Service	6.31 6.31	1.57 0.86	0.90	37.73 62.17	-63.06 -35.23	0.26 0.13
Dead+Wind 150 deg - Service	6.31	0.00	1.49 1.71	62.17 71.06	-35.25 -0.20	-0.12
Dead+Wind 180 deg - Service	6.31	-0.88	1.71	62.83	-0.20 35.16	-0.12 -0.36
Dead+Wind 210 deg - Service Dead+Wind 240 deg - Service	6.31	-0.88 -1.58	0.91	62.83 37.90	62.91	-0.50
Dead+Wind 270 deg - Service	6.31	-1.58 -1.71	0.91	1.75	69.31	-0.51
	6.31	-1.71 -1.46	-0.84	-32.70	59.47	-0.45
Dead+Wind 300 deg - Service	6.31	-1.46 -0.86	-0.84 -1.49	-32.70 -59.09	34.81	-0.26
Dead+Wind 330 deg - Service	0.31	-0.00	-1.49	-53.09	34.81	-0.12

## **Solution Summary**

	Sui	n of Applied Force:	s		Sum of Reaction	S	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-6.31	0.00	0.00	6.31	0.00	0.000%
2	0.01	-7.58	-8.98	-0.01	7.58	8.98	0.001%
3	0.01	-5.68	-8.98	-0.01	5.68	8.98	0.001%

EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	14 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

	Sur	n of Applied Forces	Š		Sum of Reaction	S	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
4	4.33	-7.58	-7.44	-4.33	7.58	7.44	0.001%
5	4.33	-5.68	-7.44	-4.33	5.68	7.44	0.001%
6	7.23	-7.58	-4.16	-7.23	7.58	4.16	0.001%
7	7.23	-5.68	-4.16	-7.23	5.68	4.16	0.001%
8	8.37	-7.58	-0.01	-8.37	7.58	0.01	0.001%
9	8.37	-5.68	-0.01	-8.37	5.68	0.01	0.001%
10	7.69	-7.58	4.42	-7.69	7.58	-4.42	0.001%
11	7.69	-5.68	4.42	-7.69	5.68	-4.42	0.001%
12	4.23	-7.58	7.32	-4.23	7.58	-7.32	0.001%
13	4.23	-5.68	7.32	-4.23	5.68	-7.32	0.001%
14	0.00	-7.58	8.38	-0.00	7.58	-8.38	0.001%
15	0.00	-5.68	8.38	-0.00	5.68	-8.38	0.001%
16	-4.30	-7.58	7.46	4.30	7.58	-7.46	0.001%
17	-4.30	-5.68	7.46	4.30	5.68	-7.46	0.001%
18	-7.74	-7.58	4.46	7.74	7.58	-4.46	0.001%
19	-7.74	-5.68	4.46	7.74	5.68	-4.46	0.001%
20	-8.37	-7.58	0.02	8.37	7.58	-0.02	0.001%
21	-8.37	-5.68	0.02	8.37	5.68	-0.02	0.001%
22	-7.15	-7.58	-4.11	7.15	7.58	4.11	0.001%
23	-7.15	-5.68	-4.11	7.15	5.68	4.11	0.001%
24	-4.22	-7.58	-7.32	4.22	7.58	7.32	0.001%
25	-4.22	-5.68	-7.32	4.22	5.68	7.32	0.001%
26	0.00	-20.79	0.00	0.00	20.79	0.00	0.000%
27	-0.06	-20.79	-2.16	0.06	20.79	2.16	0.000%
28	1.04	-20.79	-1.80	-1.04	20.79	1.80	0.000%
29	1.78	-20.79	-1.02	-1.78	20.79	1.02	0.000%
30	2.05	-20.79	-0.00	-2.05	20.79	0.00	0.000%
31	1.81	-20.79	1.04	-2.03 -1.81	20.79	-1.04	0.000%
32	1.03	-20.79	1.78	-1.03	20.79	-1.78	0.000%
33	0.00	-20.79	2.07	-0.00	20.79	-2.07	0.000%
34	-1.04	-20.79	1.80	1.04	20.79	-1.80	0.000%
34 35	-1.04	-20.79	1.02	1.89	20.79	-1.02	0.000%
35 36		-20.79 -20.79	-0.04			0.04	
30 37	-2.07 -1.78	-20.79 -20.79	-0.04 -1.02	2.07 1.78	20.79 20.79	1.02	0.000%
38	-1.78 -1.08	-20.79	-1.02 -1.79	1.78	20.79	1.02	0.000% 0.000%
38 39	0.00	-20.79 -6.31	-1.79 -1.83	-0.00	6.31	1.79	0.000%
39 40	0.88	-6.31		-0.00 -0.88		1.83	
			-1.52		6.31		0.000%
41	1.48	-6.31	-0.85	-1.48	6.31	0.85	0.000%
42	1.71	-6.31	-0.00	-1.71	6.31	0.00	0.000%
43	1.57	-6.31	0.90	-1.57	6.31	-0.90	0.000%
44	0.86	-6.31	1.49	-0.86	6.31	-1.49	0.000%
45	0.00	-6.31	1.71	-0.00	6.31	-1.71	0.000%
46	-0.88	-6.31	1.52	0.88	6.31	-1.52	0.000%
47	-1.58	-6.31	0.91	1.58	6.31	-0.91	0.000%
48	-1.71	-6.31	0.00	1.71	6.31	-0.00	0.000%
49	-1.46	-6.31	-0.84	1.46	6.31	0.84	0.000%
50	-0.86	-6.31	-1.49	0.86	6.31	1.49	0.000%

## **Non-Linear Convergence Results**

_					
	Load	Converged?	Number	Displacement	Force
	Combination		of Cycles	Tolerance	Tolerance
_	1	Yes	6	0.00000001	0.00000001
	2	Yes	9	0.00000001	0.00005422
	3	Yes	9	0.00000001	0.00003896
	4	Yes	9	0.00000001	0.00005956

#### EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page	
	CTNL041A	15 of 20	
Project	049.00940 - 2075089	Date 16:48:44 03/05/21	
	040.00040 2070000	10.40.44 00/00/21	
Client	T-Mobile	Designed by Ahmet Colakoglu	

5	Yes	9	0.00000001	0.00004412
6	Yes	9	0.00000001	0.00006411
7	Yes	9	0.00000001	0.00004843
8	Yes	9	0.00000001	0.00005951
9	Yes	9	0.00000001	0.00004408
10	Yes	9	0.00000001	0.00005428
11	Yes	9	0.00000001	0.00003900
12	Yes	9	0.00000001	0.00005948
13	Yes	9	0.00000001	0.00004405
14	Yes	9	0.00000001	0.00006403
15	Yes	9	0.00000001	0.00004839
16	Yes	9	0.0000001	0.00005946
17	Yes	9	0.0000001	0.00004404
18	Yes	9	0.00000001	0.00005423
19	Yes	9	0.00000001	0.00003898
20	Yes	9	0.00000001	0.00005936
21	Yes	9	0.00000001	0.00004397
22	Yes	9	0.00000001	0.00006398
23	Yes	9	0.00000001	0.00004836
24	Yes	9	0.00000001	0.00005944
25	Yes	9	0.00000001	0.00004403
26	Yes	8	0.00000001	0.00009966
27	Yes	9	0.00000001	0.00013339
28	Yes	9	0.00000001	0.00013493
29	Yes	9	0.00000001	0.00013837
30	Yes	9	0.00000001	0.00013929
31	Yes	9	0.00000001	0.00014029
32	Yes	9	0.00000001	0.00014133
33	Yes	9	0.00000001	0.00014182
34	Yes	9	0.00000001	0.00013908
35	Yes	9	0.0000001	0.00013691
36	Yes	9	0.00000001	0.00013498
37	Yes	9	0.00000001	0.00013436
38	Yes	9	0.00000001	0.00013302
39	Yes	9	0.00000001	0.00004616
40	Yes	9	0.00000001	0.00004725
41	Yes	9	0.00000001	0.00004820
42	Yes	9	0.00000001	0.00004731
43	Yes	9	0.00000001	0.00004641
44	Yes	9 9	0.00000001	0.00004732
45	Yes	9	0.00000001	0.00004815
46 47	Yes Yes	9	0.00000001 0.00000001	0.00004720 0.00004616
48	Yes	9	0.0000001	0.00004616
48 49	Yes	9	0.0000001	0.00004697
49 50	Yes Yes	9	0.0000001	0.00004787
30	res	9	0.0000001	0.00004703

## **Maximum Tower Deflections - Service Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	60 - 40	1.236	43	0.1504	0.0145
T2	40 - 25	0.618	43	0.1310	0.0112
T3	25 - 20	0.245	43	0.0914	0.0071
T4	20 - 5	0.157	43	0.0716	0.0054
T5	5 - 0	0.009	47	0.0172	0.0011

tnxTowe	er
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EFI Global, INC 1117 Perimeter Center West, Ste E500 Atlanta, GA

Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	16 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu

## **Critical Deflections and Radius of Curvature - Service Wind**

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
57.00	AIR 32 B2a/B66Aa	43	1.140	0.1485	0.0141	146032
56.00	26T-1900/2127/2400	43	1.108	0.1479	0.0139	146032
54.00	Side Arm Mount [SO 201-1]	43	1.045	0.1465	0.0137	121693

## **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	٥	٥
T1	60 - 40	5.976	10	0.7238	0.0710
T2	40 - 25	2.996	10	0.6331	0.0552
T3	25 - 20	1.191	18	0.4426	0.0347
T4	20 - 5	0.763	18	0.3470	0.0265
T5	5 - 0	0.045	2	0.0834	0.0056

## Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	٥	٥	ft
57.00	AIR 32 B2a/B66Aa	10	5.514	0.7153	0.0691	31021
56.00	26T-1900/2127/2400	10	5.360	0.7124	0.0684	31021
54.00	Side Arm Mount [SO 201-1]	10	5.054	0.7062	0.0671	25851

## **Bolt Design Data**

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	60	Diagonal	A325X	0.6250	1	2.40	4.55	0.527	1	Member Block Shear
		Top Girt	A325X	0.6250	1	0.11	4.55	0.024	1	Member Block Shear
T2	40	Diagonal	A325X	0.6250	1	3.03	4.55	0.665	1	Member Block Shear
		Top Girt	A325X	0.6250	1	0.36	4.55	0.080	1	Member Block Shear
Т3	25	Diagonal	A325X	0.6250	1	3.30	4.55	0.724	1	Member Block Shear
T4	20	Diagonal	A325X	0.6250	1	1.88	4.55	0.414	1	Member Block Shear
		Top Girt	A325X	0.6250	1	0.14	4.55	0.030	1	Member Block Shear

EFI Global, INC 1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job	Page
CTNL041A	17 of 20
Project	Date
049.00940 - 2075089	16:48:44 03/05/21
Client T-Mobile	Designed by Ahmet Colakoglu

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T5	5	Diagonal	A325X	0.6250	1	1.77	4.55	0.388	1	Member Block Shear

## Compression Checks

K=1.00

Leg Design Data (Compression)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	60 - 40	P2x.154	20.00	5.00	76.2 K=1.00	1.0745	-15.76	31.62	0.498 1
T2	40 - 25	P2x.218	15.00	5.00	78.3 K=1.00	1.4773	-36.24	42.47	0.853 1
T3	25 - 20	P2x.218	5.00	2.50	39.1 K=1.00	1.4773	-43.17	59.43	0.726 1
T4	20 - 5	P2.5x.203	15.03	2.60	33.0 K=1.00	1.7040	-56.21	70.82	0.794 1
Т5	5 - 0	P2 5x 203	5.01	2 60	32.9	1 7040	-59 53	70.85	$0.840^{-1}$

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

Diagonal Design Data (Compression)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	60 - 40	L2x2x1/8	7.07	3.40	102.5 K=1.00	0.4844	-2.57	8.89	0.289 1
T2	40 - 25	L2x2x1/8	7.07	3.40	102.5 K=1.00	0.4844	-3.06	8.89	0.344 1
Т3	25 - 20	L2x2x1/8	7.07	3.40	102.5 K=1.00	0.4844	-3.55	8.89	0.399 1
T4	20 - 5	L2x2x1/8	7.25	3.64	110.0 K=1.00	0.4844	-2.10	8.19	0.257 1
T5	5 - 0	L2x2x1/8	8.40	4.21	127.0 K=1.00	0.4844	-2.00	6.68	0.300 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

## **Secondary Horizontal Design Data (Compression)**

#### EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
	CTNL041A	18 of 20
Project		Date
	049.00940 - 2075089	16:48:44 03/05/21
Client	T-Mobile	Designed by Ahmet Colakoglu

Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	$Ratio$ $P_u$
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
Т3	25 - 20	L2x2x1/4	5.00	2.40	73.7 K=1.00	0.9380	-0.75	22.83	0.033 1
T4	20 - 5	L2x2x1/4	6.24	3.00	92.1 K=1.00	0.9380	-0.97	19.45	0.050 1
T5	5 - 0	L2x2x1/4	6.74	3.25	99.8 K=1.00	0.9380	-1.03	18.00	0.057 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

	Top Girt Design Data (Compression)								
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	60 - 40	L2x2x1/8	5.00	4.80	145.0 K=1.00	0.4844	-0.15	5.21	0.030 1
T2	40 - 25	L2x2x1/8	5.00	4.80	145.0 K-1.00	0.4844	-0.35	5.21	$0.067^{-1}$

4.80

5.00

20 - 5

L2x2x1/8

T4

## Tension Checks

145.0

K=1.00

0.4844

-0.14

5.21

 $0.027^{-1}$ 

					•				
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	60 - 40	P2x.154	20.00	5.00	76.2	1.0745	12.81	48.35	0.265
T2	40 - 25	P2x.218	15.00	5.00	78.3	1.4773	31.90	66.48	0.480
T3	25 - 20	P2x.218	5.00	2.50	39.1	1.4773	38.40	66.48	$0.578^{-1}$
T4	20 - 5	P2.5x.203	15.03	2.40	30.4	1.7040	49.98	76.68	0.652
T5	5 - 0	P2.5x.203	5.01	2.41	30.5	1.7040	52.81	76.68	0.689

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

	Diagonal Design Data (Tension)								
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	60 - 40	L2x2x1/8	7.07	3.40	65.1	0.2930	2.40	12.74	0.188 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

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1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

,	Job		Page
		CTNL041A	19 of 20
	Project		Date
		049.00940 - 2075089	16:48:44 03/05/21
	Client	T-Mobile	Designed by Ahmet Colakoglu

Section	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio
No.									$P_u$
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T2	40 - 25	L2x2x1/8	7.07	3.40	65.1	0.2930	3.03	12.74	0.238 1
T3	25 - 20	L2x2x1/8	7.07	3.40	65.1	0.2930	3.30	12.74	$0.259^{-1}$
T4	20 - 5	L2x2x1/8	7.25	3.64	69.8	0.2930	1.88	12.74	$0.148^{-1}$
T5	5 - 0	L2x2x1/8	8.40	4.21	80.6	0.2930	1.77	12.74	$0.139^{-1}$

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

		Secondar	ry Horiz	ontai	Desig	gn Dat	a (Tens	sion)	
Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T3	25 - 20	L2x2x1/4	5.00	2.40	94.6	0.9380	0.75	30.39	0.025 1
T4 T5	20 - 5 5 - 0	L2x2x1/4 L2x2x1/4	6.24 6.74	3.00 3.25	118.2 128.1	0.9380 0.9380	0.97 1.03	30.39 30.39	$0.032^{-1} \\ 0.034^{-1}$

	Top Girt Design Data (Tension)								
Section	Elevation	Size	L	$L_u$	Kl/r	A	$P_u$	$\phi P_n$	Ratio
No.	ft		ft	ft		$in^2$	K	K	$\frac{P_u}{\phi P_n}$
T1	60 - 40	L2x2x1/8	5.00	4.80	92.0	0.2930	0.11	12.74	0.009 1
T2	40 - 25	L2x2x1/8	5.00	4.80	92.0	0.2930	0.36	12.74	$0.028^{-1}$
T4	20 - 5	L2x2x1/8	5.00	4.80	92.0	0.2930	0.14	12.74	0.011 1

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

## **Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$egin{aligned} \phi P_{allow} \ K \end{aligned}$	% Capacity	Pass Fail
T1	60 - 40	Leg	P2x.154	2	-15.76	31.62	49.8	Pass
T2	40 - 25	Leg	P2x.218	32	-36.24	42.47	85.3	Pass
T3	25 - 20	Leg	P2x.218	56	-43.17	59.43	72.6	Pass
T4	20 - 5	Leg	P2.5x.203	67	-56.21	70.82	79.4	Pass
T5	5 - 0	Leg	P2.5x.203	100	-59.53	70.85	84.0	Pass
T1	60 - 40	Diagonal	L2x2x1/8	7	-2.57	8.89	28.9 52.7 (b)	Pass
T2	40 - 25	Diagonal	L2x2x1/8	37	-3.06	8.89	34.4 66.5 (b)	Pass
Т3	25 - 20	Diagonal	L2x2x1/8	58	-3.55	8.89	39.9 72.4 (b)	Pass
T4	20 - 5	Diagonal	L2x2x1/8	91	-2.10	8.19	25.7 41.4 (b)	Pass
T5	5 - 0	Diagonal	L2x2x1/8	103	-2.00	6.68	30.0	Pass

<sup>&</sup>lt;sup>1</sup>  $P_u$  /  $\phi P_n$  controls

EFI Global, INC

1117 Perimeter Center West, Ste E500 Atlanta, GA Phone: 770-693-0835 FAX:

Job		Page
СТ	NL041A	20 of 20
Project		Date
049.009	940 - 2075089	16:48:44 03/05/21
Client		Designed by
	-Mobile	Ahmet Colakoglu

Section	Elevation	Component	Size	Critical	P	$\phi P_{allow}$	%	Pass
No.	ft	Type		Element	K	K	Capacity	Fail
							38.8 (b)	
T3	25 - 20	Secondary Horizontal	L2x2x1/4	64	-0.75	22.83	3.3	Pass
T4	20 - 5	Secondary Horizontal	L2x2x1/4	79	-0.97	19.45	5.0	Pass
T5	5 - 0	Secondary Horizontal	L2x2x1/4	111	-1.03	18.00	5.7	Pass
T1	60 - 40	Top Girt	L2x2x1/8	5	-0.15	5.21	3.0	Pass
T2	40 - 25	Top Girt	L2x2x1/8	36	-0.35	5.21	6.7 8.0 (b)	Pass
T4	20 - 5	Top Girt	L2x2x1/8	72	-0.14	5.21	2.7 3.0 (b)	Pass
							Summary	
						Leg (T2)	85.3	Pass
						Diagonal (T3)	72.4	Pass
						Secondary Horizontal (T5)	5.7	Pass
						Top Girt (T2)	8.0	Pass
						Bolt Checks	72.4	Pass
						RATING =	85.3	Pass

# Client: Foresite LLC Site ID: CTNL041A

#### **CALCULATION SHEET**



### Jump Plate Reinforcement Check (Plate, typ)

#### Jump Plate

Number of jump plates N := 3

Yield strength of plate  $F_y := 50 \text{ksi}$ 

Ultimate strength of plate  $F_u := 65ksi$ 

Thickness of plate  $t_{plate} := 0.75in$ 

Effective width of plate Weffective := 3in

Applied Compression (Tnx)  $P_{tnx} := 43.17 \cdot kip$ 

Applied Tension (Tnx)  $T_{tnx} := 0kip$ 

#### Determine the force distribution

#### **EXISTING PIPE LEG INPUTS**

Outside Diameter:  $D_{L_out} := 2.375in$ 

Thickness:  $t_{leg} := 0.218in$ 

Inside Diameter:  $D_{L\_in} := D_{L\_out} - 2 \cdot t_{leg} = 1.939 \cdot in$ 

Area:  $A_{L} := \frac{\pi}{4} \cdot \left( D_{L\_out}^{2} - D_{L\_in}^{2} \right) = 1.477 \cdot in^{2}$ 

 $A_{\text{mod}} := 2.1917 \cdot \text{in}^2$ 

gross area of the plate  $A_g := t_{plate} \cdot w_{effective} = 2.25 \cdot in^2$  cross section

Total Area:  $A_{\text{tot}} := A_{L} + A_{\text{mod}} + NA_{g}$ 

Tensile load carried  $P_{TLeg} := \frac{A_L + A_{mod}}{A_{tot}} \cdot T_{tnx} = 0 \cdot \text{kip}$  through the tower leg

Tensile load carried  $P_{TP1} := \frac{N \cdot A_g}{A_{tot}} \cdot T_{tnx} = 0 \cdot \text{kip}$  through the Knife Plates

Tensile load carried  $P_{\text{CLeg}} := \frac{A_L + A_{\text{mod}}}{A_{\text{tot}}} \cdot P_{\text{tnx}} = 19.389 \cdot \text{kip}$  through the tower leg

Compressive load carried  $P_{CPl} := \frac{N \cdot A_g}{A_{tot}} \cdot P_{tnx} = 23.781 \cdot \text{kip}$  through the Knife Plates

# Client: Foresite LLC Site ID: CTNL041A

#### **CALCULATION SHEET**



#### Tensile Strength of the Jump Plate

AISC 13th Edition Chapter D Equation (D2-1)

Safety Factor  $\phi_t := 0.9$ 

Tensile strength in the gross cross section  $P_{n.plate} := F_y \cdot A_g = 112.5 \cdot kip$ 

Tensile force needed to be resisted by each jump plate  $P_{t} := \frac{P_{TP1}}{N} = 0 \cdot \text{kip}$ 

#### Tension Check

#### Gross Section Yield

$$\label{eq:Check_ten_yieldhss} \text{Check}_{\text{ten}\_\text{yieldhss}} \coloneqq \left| \begin{array}{ccc} \text{"OK"} & \text{if } \varphi P_{\text{n.tension}} \geq \frac{P_{\text{TPl}}}{N} \\ \\ \text{"N/G"} & \text{otherwise} \end{array} \right|$$

 $Check_{ten\_yieldHSS} = "OK"$ 

 $Check_{tension} := \frac{P_t}{\phi P_{n.tension}} = 0.\%$ 

#### Client: Foresite LLC Site ID: CTNL041A

#### **CALCULATION SHEET**



AISC 13th Edition Chapter E *Equation (E3-1 to E3-4)* 

#### Compression Check of the Jump Plate

Unbraced Length

K Factor

Radius of gyration (calculated from AutoCAD)

Modulus of elasticity

compression force needed to be resisted by each jump plate

$$r_x := \frac{t_{plate}}{\sqrt{12}} = 0.217 \cdot in$$

E:= 29000ksi

$$P_{C} := \frac{P_{CP1}}{N} = 11.89 \cdot kip$$

#### Compression Strength of Jump Plate

Safety Factor

$$\phi_{\rm C} := 0.9$$

$$\Phi P_{n\_comp} = \Phi_c \cdot F_{cr} \cdot A_g$$

$$F_{e} := \frac{\pi^{2} \cdot 29000 \text{ksi}}{\left(\frac{\text{K} \cdot l_{u}}{r_{x}}\right)^{2}} = 36.395 \cdot \text{ksi}$$

$$\frac{\text{K} \cdot \text{l}_{\text{u}}}{\text{r}_{\text{x}}} = 88.681 < 4.71 \cdot \sqrt{\frac{29000 \cdot \text{ksi}}{\text{F}_{\text{y}}}} = 113.432$$

$$F_{cr} := 0.658 \frac{F_{y}}{F_{e}}$$

$$F_{cr} := 0.658 \cdot F_{y} = 28.135 \cdot ksi$$

AISC 13th Edition Chapter J Equation (J4-6)

$$\begin{split} \varphi P_{n\_comp} := & \left| \begin{array}{l} \varphi_c \cdot F_y \cdot A_g & \text{if } \frac{K \cdot l_u}{r_x} \leq 25 \\ \\ \varphi_c \cdot F_{cr} \cdot A_g & \text{otherwise} \end{array} \right| \end{split}$$

$$\phi P_{n\_comp} = 56.973 \cdot \text{kip}$$

Check<sub>comp</sub> = "OK"

$$Check_{compression} := \frac{P_{c}}{\phi P_{n\_comp}} = 20.87 \cdot 9$$

# Client: Foresite LLC Site ID: CTNL041A

#### CALCULATION SHEET



#### WELD CONNECTION

#### Weld Sizing

Length of vertical weld

Electrode Strength

Vertical fillet weld size - jump plate to leg (in sixteenths of an inch):

Horizontal component of eccentricity with respect to centroid of the weld group

Load Not in Plane with Weld Group

Electrode Strength Coefficient

Coefficient for eccentrically Loaded Weld Groups

 $l_{weld} := 5 \cdot in$ 

 $F_{EXX} := 70 \cdot ksi$ 

 $D_{vplate} := 4$ 

Weldsize :=  $\frac{D_{\text{vplate}}}{16} = 0.25$ 

 $e_x := 5.5 \cdot in$ 

k := 0

 $a := \frac{e_x}{l_{weld}} = 1.1$ 

 $C_1 = 1$ 

C := 1.175

(Linearly interpolated from AISC, 13th Edition, Table 8-4)

#### Weld Capacity

#### Design Strength

$$\phi_{w} := 0.75$$

$$\mathtt{D}_{\texttt{min}} \coloneqq \texttt{ceil} \left( \frac{\texttt{max} \big( \mathtt{P}_{\texttt{t}} \,,\, \mathtt{P}_{\texttt{c}} \big) \cdot \texttt{in}}{ \varphi_{\texttt{w}} \cdot \mathtt{CC}_{1} \cdot \mathtt{l}_{\texttt{weld}} \cdot \texttt{kip}} \right) = 3$$

minweldsize := 
$$\frac{D_{\text{min}}}{16} = \frac{3}{16}$$

$$\label{eq:checkweld} \mbox{Check}_{\mbox{weld}} := \begin{tabular}{ll} "OK" & if $D_{\mbox{vplate}} \geq D_{\mbox{min}} \wedge D_{\mbox{vplate}} \geq \mbox{Min}_{\mbox{weldsize}} \wedge D_{\mbox{vplate}} \leq \mbox{Max}_{\mbox{weldsize}} \\ "N/G" & otherwise \\ \end{tabular}$$

Checkweld = "N/G"

 $\phi \text{Rn}_{\text{weld2}} := \phi_{\text{w}} \cdot \text{Cksi} \cdot \text{in} \cdot \text{C}_1 \cdot \text{D}_{\text{vplate}} \cdot \text{l}_{\text{weld}} = 17.625 \cdot \text{kip}$ 

$$\label{eq:checkweld3} \begin{array}{ll} \text{Check}_{\text{weld3}} \coloneqq & \text{"OK"} & \text{if } \varphi \text{Rn}_{\text{weld2}} \geq P_t \\ & \text{"N/G"} & \text{otherwise} \\ \\ \hline \\ \text{Check}_{\text{weld3}} = \text{"OK"} \end{array}$$

$$\frac{\max(P_t, P_c)}{\phi Rn_{weld2}} = 67.463 \cdot \%$$

<b>Project Info</b>	<b>Project Information</b>					
BU#						
Site Name	CTNL041A					
Order #						

Tower Information		
Tower Type	Self Support	
TIA-222 Rev	G	

☐ Load Z Normalization

Applied Loads				
Comp. Uplift				
Axial (k)	62.00	54.00		
Shear (k)	6.00	5.00		

Anchor Rod Data		
Quantity:	4	
Diameter (in):	0.75	
Material Grade:	A449	
Grout Considered:	No	
I <sub>ar</sub> (in):	0	
Eta Factor, η:	0.5	
Thread Type:	N-Included	
Configuration:	Symmetrical	

Fy=92 ksi Fu=120 ksi

Anchor Rod Results		
Axial, Pu_c (kips)	15.50	
Shear, Vu (kips)	1.50	
Moment, Mu (kip-in)	ı	
Axial Cap., φPn_t (kips)	32.06	
Shear Cap., φVn (kips)	-	
Moment Cap., фМп (kip-in)	-	
Stress Rating	57.7%	

**Pass** 

## **SST Unit Base Foundation**

BU # : Site Name: CTNL041A App. Number:

TIA-222 Revision: G

Top & Bot. Pad Rein. Different?:	
Tower Centroid Offset?:	
Block Foundation?:	

Superstructure Analysis Reactions		
Global Moment, M:	358	ft-kips
Global Axial, P:	8	kips
Global Shear, V:	9	kips
Leg Compression, P <sub>comp</sub> :	62	kips
Leg Comp. Shear, $V_{u\_comp}$ :	6	kips
Leg Uplift, <b>P</b> <sub>uplift</sub> :	54	kips
Leg Uplift. Shear, <b>V</b> <sub>u_uplift</sub> :	5	kips
Tower Height, <b>H</b> :	60	ft
Base Face Width, BW:	7	ft
BP Dist. Above Fdn, <b>bp</b> <sub>dist</sub> :	3	in

Foundation Analysis Checks				
	Capacity	Demand	Rating	Check
Lateral (Sliding) (kips)	36.54	9.00	24.6%	Pass
Bearing Pressure (ksf)	5.94	1.49	25.0%	Pass
Overturning (kip*ft)	610.42	400.75	65.7%	Pass
Pier Flexure (Comp.) (kip*ft)	236.06	18.00	7.6%	Pass
Pier Flexure (Tension) (kip*ft)	146.24	15.00	10.3%	Pass
Pier Compression (kip)	2343.24	64.65	2.8%	Pass
Pad Flexure (kip*ft)	631.92	103.97	16.5%	Pass
Pad Shear - 1-way (kips)	179.68	40.24	22.4%	Pass
Pad Shear - Comp 2-way (ksi)	0.164	0.036	21.8%	Pass

Pier Properties		
Pier Shape:	Circular	
Pier Diameter, <b>dpier</b> :	2.5	ft
Ext. Above Grade, E:	0.50	ft
Pier Rebar Size, <b>Sc</b> :	7	
Pier Rebar Quantity, <b>mc</b> :	6	
Pier Tie/Spiral Size, <b>St</b> :	4	
Pier Tie/Spiral Quantity, mt:	6	
Pier Reinforcement Type:	Tie	
Pier Clear Cover, <b>cc</b> <sub>pier</sub> :	3	in

Soil Rating:	65.7%
Structural Rating:	22.4%

Pad Properties		
Depth, <b>D</b> :	4.00	ft
Pad Width, <b>W</b> :	13.50	ft
Pad Thickness, <b>T</b> :	1.50	ft
Pad Rebar Size (Bottom), Sp:	8	
Pad Rebar Quantity (Bottom), mp:	14	
Pad Clear Cover, <b>cc</b> <sub>pad</sub> :	3	in

Material Properties		
Rebar Grade, <b>Fy</b> :	60	ksi
Concrete Compressive Strength, F'c:	3	ksi
Dry Concrete Density, δ <b>c</b> :	150	pcf

Soil Properties		
Total Soil Unit Weight, $\gamma$ :	120	pcf
Ultimate Net Bearing, Qnet:	7.500	ksf
Cohesion, <b>Cu</b> :	0.000	ksf
Friction Angle, $oldsymbol{arphi}$ :	35	degrees
SPT Blow Count, N <sub>blows</sub> :	22	
Base Friction, $\mu$ :	0.35	
Neglected Depth, N:	3.0	ft
Foundation Bearing on Rock?	No	
Groundwater Depth, <b>gw</b> :	3	ft

<-- Toggle between Gross and Net



#### Address:

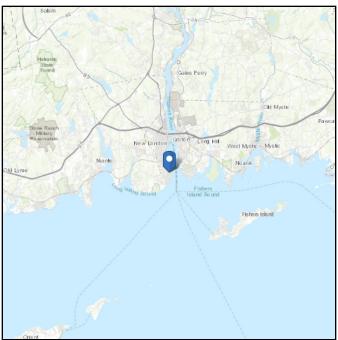
No Address at This Location

## **ASCE 7 Hazards Report**

Standard: ASCE/SEI 7-10 Elevation: 33.93 ft (NAVD 88)

Risk Category: || Latitude: 41.322475 Soil Class: D - Stiff Soil Longitude: -72.0937





### Wind

#### Results:

Wind Speed: 135 Vmph
10-year MRI 80 Vmph
25-year MRI 90 Vmph
50-year MRI 99 Vmph
100-year MRI 110 Vmph

Data Source: ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of

March 12, 2014

Date Accessed: Thu Oct 22 2020

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings shall be protected against wind-borne debris as specified in Section 26.10.3.

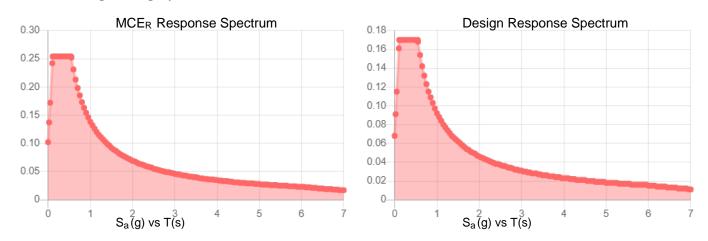
Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



### **Seismic**

Site Soil Class: Results:	D - Stiff Soil			
S <sub>S</sub> :	0.159	S <sub>DS</sub> :	0.17	
$S_1$ :	0.058	$S_{D1}$ :	0.092	
F <sub>a</sub> :	1.6	T <sub>L</sub> :	6	
F <sub>v</sub> :	2.4	PGA:	0.079	
$S_{MS}$ :	0.254	PGA <sub>M</sub> :	0.126	
S <sub>M1</sub> :	0.138	F <sub>PGA</sub> :	1.6	
		l <sub>o</sub> :	1	

#### Seismic Design Category B



Data Accessed: Thu Oct 22 2020

Date Source: USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating

Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with

ASCE/SEI 7-10 Ch. 21 are available from USGS.



#### **Ice**

#### Results:

Ice Thickness: 0.75 in.

Concurrent Temperature: 15 F

Gust Speed: 50 mph

**Data Source:** Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8

Date Accessed: Thu Oct 22 2020

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

#### NOTES:

- 1. UPGRADE DESIGN VALID FOR APPURTENANCES LISTED IN EFI ANALYSIS REPORT DATED 03/05/2021. CONTRACTOR TO REVIEW AND SHOULD ADHERE TO THE REPORT.
- 2. CONTRACTOR TO REMOVE AND REATTACH EXISTING APPURTENANCES AS
- 3. ALL DIMENSIONS ARE BASED ON STRUCTURAL ANALYSIS REPORT PREPARED BY EBI CONSULTING, DATED 02/13/2015.
- 4. CONTRACTOR TO FIELD VERIFY EXISTING TOWER MEMBER SIZES AND TOWER DIMENSIONS IN THE VICINITY OF THE UPGRADE, BEFORE FABRICATION OF STEEL AND COMMENCEMENT OF WORK. ANY DISCREPANCY SHOULD BE REPORTED TO EFI IMMEDIATELY FOR FURTHER EVALUATION.
- 5. DO NOT PERFORM THE WORK ON THE TOWER WHEN WINDS GUST MORE THAN 15 MPH AT THE GROUND LEVEL.
- 6. NEW TOWER REACTIONS:

LEG UPLIFT: LEG COMPRESSION: 61 KIPS

6 KIPS LEG SHEAR:

- 7. CONTRACTOR TO HAVE THE SAFETY CLIMB INTACT AND FUNCTIONAL AFTER WORK IS COMPLETE.
- 8. TOWER WILL BECOME UNSTABLE WHEN MEMBERS ARE DISCONNECTED OR BEING REPLACED. CONTRACTOR IS FULLY RESPONSIBLE TO MAINTAIN STABILITY OF THE TOWER DURING WORK AND SHOULD CONSULT WITH AN
- 9. EFI DISCLAIMS ANY LIABILITY ARISING FROM THE ORIGINAL MATERIAL, FABRICATION OR ERECTION OF THE TOWER.
- 10. ALL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN AND SHALL MEET ANSI/ASSE A10.48 (LATEST EDITION), OSHA, AND GENERAL INDUSTRY STANDARDS. ALL RIGGING PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION) INCLUDING THE REQUIRED INVOLVEMENT OF A QUALIFIED ÈNGINEER FOR CLASS IV CONSTRUCTION.

[B] ADD L2X2X4 - SECONDARY HORIZONTALS		TOWER MODIFICATION SCHEDULE					
SEE 2/S2		FROM (FT)	TO (FT)	MODIFICATION	REFERENCE SHEET		
[C] ADD KNIFE PLATE SEE 4/S2	A	0'-0"	25'-0"	ADD L2x2x1/4 SECONDARY HORIZONTALS	S2		
	В	20'-0"	20'-0"	ADD NEW KNIFE PLATES	S2		
		NC	TE: APPLY	INDICATED MODIFICATIONS TO ALL 3 TOWER FACES			

#### **TOWER ELEVATION** S1 / 1/8" = 1'-0"

SECONDARY HORIZONTALS

SEE 1/S2

80'-0" AGL

40'-0" AGL

20'-0" AGL

0'-0" AGL

P2.0x0.21

SIZES

**EXISTING** 

TOWER

SUP

SCALE ON 11x17 SHEETS

#### 1. DESIGN INFORMATION AND GENERAL REQUIREMENTS

#### 1.1 CODES

a. 2018 CONNECTICUT BUILDING CODE (2015 IBC)

b. MINIMUM DESIGN LOADS AND ASSOCIATED CRITERIA FOR BUILDINGS AND OTHER STRUCTURES, ASCE/SEI 7-10, AMERICAN SOCIETY OF CIVIL

c. STEEL CONSTRUCTION MANUAL, 14TH EDITION, AMERICAN INSTITUTE OF STEEL CONSTRUCTION

d. STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES AND ANTENNAS, ANSI/TIA-222-G TELECOMMUNICATIONS INDUSTRY ASSOCIATION

1.2 GENERAL
a. PRIOR TO PURCHASE OR FABRICATION OF MATERIAL, THE CONTRACTOR SHALL PERFORM AN INSPECTION VERIFYING MEMBER DIMENSIONS AND BOLT SIZES. SHOULD THE CONTRACTOR DISCOVER ANY DAMAGED OR MISSING MEMBERS OR THE MEMBER OR BOLT SIZES DO NOT MATCH THOSE LISTED, EFI SHALL BE NOTIFIED IMMEDIATELY.

b. CONTRACTOR TO REPLACE ALL BOLTS REMOVED WITH NEW BOLTS OF SAME TYPE, UNLESS NOTED OTHERWISE.

#### 1.3 LOADS & DESIGN CRITERIA

a. WIND LOADING: V=135MPH (ULTIMATE DESIGN WIND SPEED), EXPOSURE CATEGORY C, RISK CATEGORY II

#### 2. STRUCTURAL STEEL

2.1 MATERIALS

a. STRUCTURAL STEEL ANGLE & PLATE . . . . . . . ASTM A36 U.N.O. HSS ROUND . . . . . . . . . . . ASTM A500 GRADE B (OR Fy>42KSI)

BARS (SOLID RODS) . . . . . ASTM A572 GRADE 50

b. BOLTS . . . . . . . . . . . ASTM A325N U.N.O.
c. WELDING ELECTRODES . . . . AWS A5.1 (E70XX)
d. STEEL CONSTRUCTION SHALL CONFORM TO "SPECIFICATION FOR

STRUCTURAL STEEL BUILDINGS, ANSI/AISC 360-10" e. WELDING SHALL CONFORM TO AWS D1.1/D1.3/D1.7 AS APPLICABLE.

THE FABRICATOR SHALL FURNISH CHECKED SHOP AND ERECTION DRAWINGS TO THE ENGINEER, AND OBTAIN APPROVAL PRIOR TO FABRICATING ANY STRUCTURAL STEEL. SHOP DRAWINGS SHALL CONFORM TO "DETAILING FOR STEEL CONSTRUCTION, 2ND EDITION"

g. POOR MATCHING OF HOLES SHALL BE CORRECTED BY DRILLING TO THE NEXT LARGER SIZE. WELDING FOR RE-DRILLING WILL NOT BE PERMITTED.

#### 2.2 CONNECTIONS

a. SHOP CONNECTIONS MAY BE BOLTED OR WELDED

b. FIELD CONNECTIONS BOLTED WITH A325-N BOLTS, (INSTALLED SNUG TIGHT) UNLESS OTHERWISE SPECIFIED OR IF WELDED CONNECTIONS ARE NOTED ON DRAWINGS

c. FIELD CONNECTIONS SHALL BE MADE WITH A325—N BOLTS AND HARDENED WASHERS EXCEPT AS INDICATED ON THE DESIGN DRAWINGS d. CONNECTIONS NOT SHOWN ON DRAWINGS SHALL BE DESIGNED BY THE STEEL FABRICATOR. CONNECTIONS SHALL BE DESIGNED IN ACCORDANCE WITH AISC "SPECIFICATIONS FOR STRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS" AND "AISC CODE OF STANDARD PRACTICE FOR STEEL BUILDINGS AND BRIDGES"

e. DO NOT FIELD CUT OR ALTER STRUCTURAL MEMBERS WITHOUT PRIOR WRITTEN APPROVAL OF ENGINEER.

TO THE SURFACE OF THE METAL AND SHALL NOT BE MADE OR ENLARGED BY BURNING. HOLES SHALL BE CLEAN CUT WITHOUT TORN OR RAGGED EDGES. OUTSIDE BURRS RESULTING FROM DRILLING OR REAMING OPERATION SHALL BE REMOVED WITH A TOOL MAKING A 1/16 INCH BEVEL. BOLT HOLES SHALL BE 1/16 INCH OVERSIZE.

a. STRUCTURAL STEEL SHALL BE HOT DIP GALVANIZED AFTER FABRICATION PER ASTM A123

b. BOLTS AND NUTS SHALL BE HOT DIP GALVANIZED PER ASTM A153.
c. ALL SURFACES DAMAGED DURING THE WORK SHALL BE PAINTED WITH COLD GALVANIZING COMPOUND TWICE. THE PAINT SHOULD BE AT LEAST 93% PURE ZINC. RUST-OLEUM PROFESSIONAL, (MODEL# 7585838) OR

a. CONTRACTOR TO TAKE ALL NECESSARY PRECAUTIONS FOR FIRE PREVENTION DURING WELDING, SUCH AS; INSTALLING 3000 (NFPA 701) FIRE BLANKET AROUND COAX. MORE SPLATTER AND SPARKS SHOULD BE ANTICIPATED WHILE WELDING ON GALVANIZED SURFACE. COAX IS FLAMMABLE AND SHALL CATCH FIRE IF NOT PROTECTED. WATER SHALL BE ON SITE OF ADEQUATE AMOUNT AND AVAILABLE AT SHORT NOTICE AT ALL TIMES DURING WELDING ACTIVITY. CONTRACTOR SHOULD BE ABLE TO TRANSPORT THE WATER TO THE HEIGHT WELDING BEING PERFORMED.

b. WELDING ON GALVANIZED SURFACE SHOULD BE DONE WITH EXTREME CAUTION. IF THE WELD MATERIAL IS CONTAMINATED WITH ZINC, IT DOES NOT PROVIDE A STRUCTURAL WELD. GRIND GALVANIZING BEFORE WELDING. c. WELDING CERTIFICATE MUST BE PROVIDED PRIOR TO WELDING. ALL WELDING SHALL BE PERFORMED BY AWS QUALIFIED WELDER WHO HAS EXPERIENCE WITH GALVANIZED SURFACES.



2075089

Ahmet Colakoglu, PE CT License No: PEN 27057

efi globa

EFI GLOBAL, INC. 117 PERIMETER CENTER SUITE E500 ATLANTA, GA 30338 TEL NO: 770-693-0835 TELECOM@EFIGLOBAL.COM

T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002

FOR

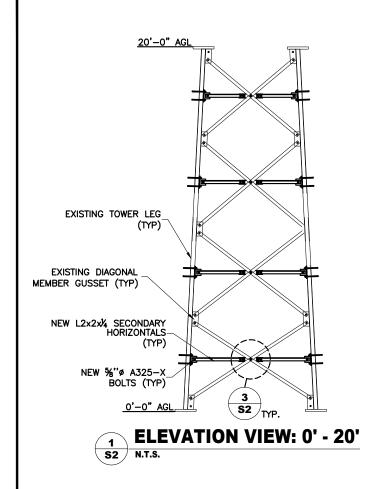
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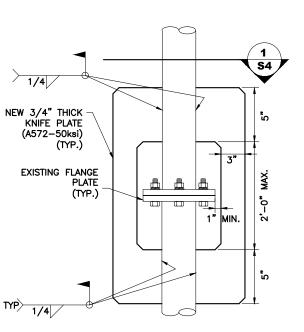
DATE 03/05/21

**≱** | ∢ | CTNL041A 25 New

DRAWN: SK CHECKED: AC OB #: 049.00940-

**S1 SCOPE OF MODIFICATION** 

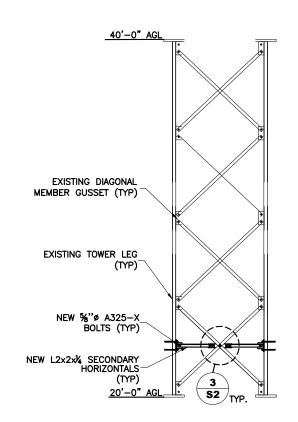




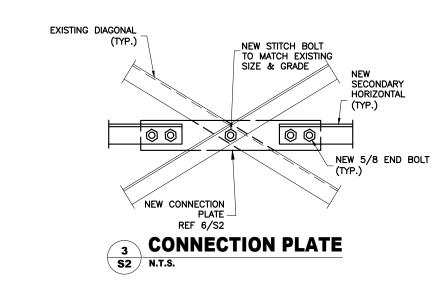
4 N.T.S.

**KNIFE PLATE DETAIL @ 20'** 

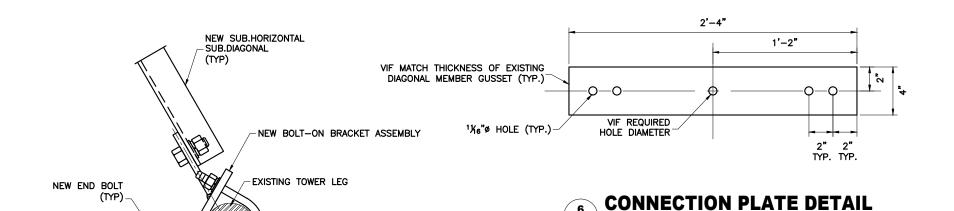
DRAWINGS PLOTTED TO SCALE ON 11x17 SHEETS







S2 N.T.S.







Ahmet Colakoglu, PE CT License No: PEN 27057 EFI GLOBAL, INC.
1117 PERIMETER CENTER W
SUITE E500
ATLANTA, GA 30338
TEL NO: 770-693-0835
TELECOM@EFIGLOBAL.COM

(%) efi global

T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002

NUM DATE DESCRIPTION:
A 03/05/21 ISSUED FOR CONSTRUCT

CTNL041A

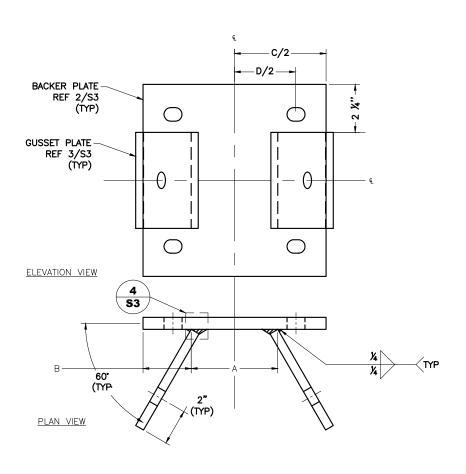
EESS: 25 Lower Boulevard,

New London, CT 06320

DESIGNED: SK
DRAWN: SK
CHECKED: AC

JOB #:049.00940— 2075089

S2 STRUCTURAL DETAILS



**BOLT-ON BRACKET ASSEMBLY** S3 N.T.S.

PIPE2.5STD+HSS3.5X0.203 SPLIT PIPE

LEG	OUTER	ASSEMBLY		BACKER PLATE		U-BOLT		
LEG	DIAMETER	A (in)	B (in)	C (in)	D (in)	E (in)	F (in)	G (in)
PIPE2.5STD	27/8	2 <sup>1</sup> 1/ <sub>6</sub>	1 <sup>2</sup> / <sub>32</sub>	6	3½	4%	3	1/2
PIPE2.0X STD	23%	2¾	1 <sup>1</sup> 3⁄16	6	3	4%	21/2	1/2

- NOTES:
  1. ALL HOLES TO BE SHOP FABRICATED, UNLESS NOTED OTHERWISE.

- 2. TOLERANCES UNLESS NOTED OTHERWISE: FRACTIONS ± 1/6"

  ANGLES ± 1/2"
  DECIMALS ± 0.010"

  3. U-BOLTS SHALL MEET REQUIREMENTS OF ASME B18.31.5-2011 BENT BOLTS.

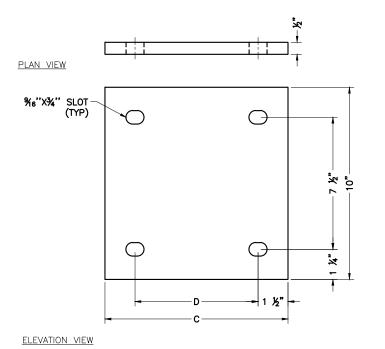
  4. U-BOLTS TO BE ASTM A36/A307, SAE 429 GR 2. PLATES TO BE ASTM A572 GRADE 50.

  5. USE 2 U-BOLTS PER ASSEMBLY, COMPLETE W/ NUTS, WASHERS AND LOCK WASHERS.

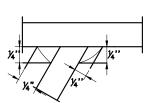
  6. FOR WELDING, WELD TO BE E70xx ELECTRODES.

  7. FULL ASSEMBLY TO BE HOT DIP GALVANIZED PER ASTM 153/ A153M OR A123, AS APPLICABLE
- 8. STANDARD %6" HOLES IN PLACE OF SLOTTED HORIZONTAL HOLES ON THE BACKER PLATE ARE PERMITTED

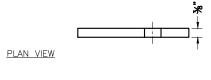
  9. NO FIELD FABRICATION PERMITTED ON THIS PART

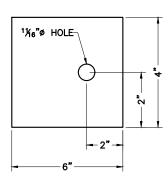






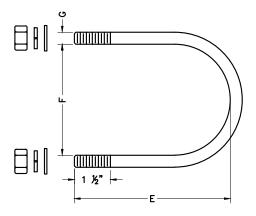






ELEVATION VIEW









CHECKED: AC IOB #:049.00940-2075089

DESIGNED: SK DRAWN: SK

Lower Boulevard, London, CT 06320

25 New

( efi global

EFI GLOBAL, INC. 1117 PERIMETER CENTER V SUITE E500 ATLANTA, GA 30338 TEL NO: 770—693—0835 TELECOM@EFIGLOBAL.COM

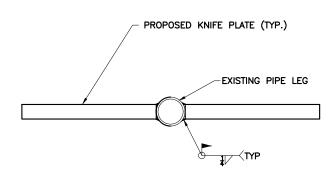
T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002

DATE 03/05/21

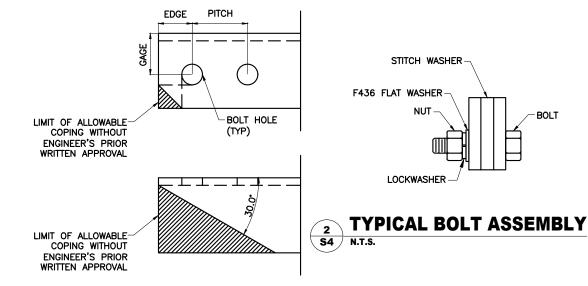
CTNL041A

**S3 STRUCTURAL DETAILS** Ahmet Colakoglu, PE CT License No: PEN 27057

PLOTTED TO SCALE ON 11x17 SHEETS



**KNIFE PLATE CONNECTION** 1 \$4



	BOLT SCHEDULE							
MEMBER SIZE	MEMBER SIZE CONNECTION TYPE BOLT SIZE MIN EDGE DISTANCE PITCH DISTANCE GAGE DISTANCE BOLT HOLE							
L2X2X1/4	L2X2X¼ END 56"ø X 2" LONG 76" 11/6" 11/6"							
	NOTE: ALL BOLTS TO BE A325-X							

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T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002

NUM DATE DESCRIPTION:
A 03/05/21 ISSUED FOR CONSTRUCTION

25 Lower Boulevard, New London, CT 06320

DESIGNED: SK DRAWN: SK CHECKED: AC JOB #:049.00940-2075089

CTNL041A

S4 STRUCTURAL DETAILS

Ahmet Colakoglu, PE CT License No: PEN 27057

# Exhibit E

# ·· T··Mobile·



Date: 10/26/2020

To: T-Mobile Northeast, LLC 35 Griffin Road South Bloomfield, CT 06002

Subject: Mount Structural Analysis Report

**T-Mobile Designation:** Site Name: NL041/Gardner-NewLondon

Site ID: CTNL041A

**EFI Designation:** Project Number: 049.00940 - 2075089

Site Data: 25 Lower Boulevard, New London, CT 06320

Latitude 41.322475°, Longitude -72.093700°

*EFI Global, Inc.* is pleased to submit this **"Mount Structural Analysis Report"** to determine the structural capacity of the antenna mounts utilized by T-Mobile at the above referenced site.

The purpose of the analysis is to determine acceptability of the mount stress level for the changes proposed by T-Mobile. Under the following load case we have determined the mounts to have:

Existing + Proposed Equipment Adequate Capacity w/ Mods (85.8%)

Note: See Analysis Criteria for loading configuration

The analysis has been performed in accordance with the TIA-222-G Standard and 2018 Connecticut State Building Code (2015 IBC).

We at *EFI Global, Inc.* appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance on this or any other projects, please give us a call.

Sincerely, EFI Global, Inc.

License No: PEC0001245

Ahmet Colakoglu, PE Connecticut Professional Engineer

License No: 27057



#### 1) ANALYSIS CRITERIA

The analysis was performed for the existing and proposed appurtenances as specified in the loading information referenced below, and per the following loading criteria of Table 1.

Table 1 - Loading and Analysis Criteria

	<u> </u>	
Rad Center	59' & 57'	
Structure Type	Self-Support Tower	
<b>Exposure Category</b>	С	
Basic Wind Speed	125 * 1/0 6 - 105 mmh /Nomina	
(3-Second Gust)	135 * √0.6 = 105 mph (Nominal)	
Ice Loading	0.75" with 50 mph Wind	
Risk Category	II	
Topographic Factor	Kzt = 1.0	

Table 1.1 – Existing Appurtenance Configuration

	 8
Qty	Model
3	Ericsson AIR21 B2A B4P – Antennas
3	Ericsson AIR21 B4A B12P – Antennas
3	RRUS 11 B12 – RRHs
3	Generic Twin Style 1B – AWS – TMAs

Table 1.2 – Proposed and Final Appurtenance Configuration

Qty	Model
3	Ericsson AIR32 B66A B2A – Antennas
3	RFS APXVAALL24_43-U-NA20 – Antennas
3	Ericsson AIR6449 B41 – Antennas
3	Radio 4449 B71 + B85 – RRHs*
3	Radio 4415 B25 – RRHs*

<sup>\*</sup> To be mounted behind antennas

Table 1.3 – Assumed Material Properties

	and the state of t					
Member Type	<b>ASTM Material Designation</b>	Fy (ksi)	Fu (ksi)			
Pipes	A53 Gr. B	35	60			
Angles/Channels	A36	36	58			
Rectangular HSS	A500 Gr. B - 46	46	58			
Round HSS	A500 Gr. B - 42	42	58			
Others (UNO)	A572 Gr. 50	50	65			

Page 2 of 5 EFI Global, Inc.

#### 2) ANALYSIS PROCEDURE

The analysis is based on the following information:

Table 2 - Documents

Document	Provided By	Date
RFDS	T-Mobile	10/14/2020
Construction Drawings	EBI Consulting	04/01/2015
Structural Analysis Report	EBI Consulting	02/13/2015

#### 2.1) Analysis Method

Risa-3D, a commercially available analysis software package, was used to create a threedimensional model of the mount and calculate member stresses for various loading cases. Selected output from the analysis is included in the Appendix.

#### 2.2) Analysis Conditions and Assumptions

- 1) The mount was built and installed in accordance with the manufacturer's specifications.
- The mount has been maintained and will be maintained in accordance with the manufacturer's specifications. All structural members and connections of the mount are in good condition and can achieve theoretical strength.
- 3) The configuration of antennas is as specified in "1) Analysis Criteria".
- 4) The analysis was performed for the subject mount only. It does not include an evaluation of the other mounts or the tower, which should be analyzed by others.
- 5) The evaluation does not include any antenna rigging loads. The equipment should not be rigged using the subject antenna mount as the support.
- 6) The analysis includes a minimum 250 lbf maintenance point load at the worst-case location on the mount, as well as a minimum 500 lbf maintenance point load at each antenna location in conjunction with a 30 mph wind load.
- 7) Any steel grating represented in this model is for loading purposes only and it is not considered to provide any structural restraint or support.
- 8) Member sizes per the available mount specifications and assumed based on our experience with similar structures. Please refer to calculation output in the appendix of this report for sizes and lengths assumed.
- 9) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.

EFI Global, Inc. (EFI), must be notified immediately if any of these assumptions are discovered to be incorrect. The results of this analysis may be affected if any of the assumptions are not valid or have been made in error.

Page 3 of 5 EFI Global, Inc.

#### 3) ANALYSIS RESULTS AND CONCLUSION

The analysis results are shown on the table below.

Table 3.1 – Mount Component Stresses vs. Capacity

Component	% Capacity	Pass / Fail
Horizontal Face Pipe	85.8	Pass
Standoff Tube	28.5	Pass
Vertical Standoff Pipe	43.4	Pass
Antenna Mount Pipe	60.8	Pass
Pipe Stiffener	< 20	Pass

Sector Mounts: The existing sector mounts will have adequate capacity for the proposed changes by T-Mobile, once an additional Valmont/Site Pro 1 Sector Frame Stiff Arm Kit (P/N: STK-U) is attached directly to the outside mount pipe on the opposite side of the existing tie back and equally spaced between the horizontal face members at each sector. The existing stiff arm (tie back) is assumed to be installed to the outer mount pipe and equally spaced between the horizontal face members at each sector. For the code specified load combinations and as a maximum, the mount members will be stressed to 85.8% of their structural capacity.

EFI Global Inc., assumes that a Valmont/Site Pro 1 Build A-Frame Ultimate Sector Frame with one Stiff Arm (P/N: EUSF10-U) has been installed at each sector per the construction drawings prepared by EBI Consulting, dated 04/01/2015. This analysis also assumes the following:

- The mount centerline is equal to 57' AGL (above grade level), to be verified at field.
- The two (2) stiff arms are installed to the adjacent mounts tower legs.
- Three (3) 96" long 2.0 STD mount pipes are equally spaced along the face.

#### **APPENDIX**

INPUT LOADS
ANALYSIS OUTPUT

CLIENT: ForeSite / T-Mobile PROJECT: Antenna Loads - G Code with Sections 16 Revisions SUBJECT:

Tower Height Basic Wind Speed, V Type of Mount Sector mph (=Ultimate Speed\*Sqrt(0.6)) Basic Wind Speed mph with Ice,  $V_i$ Load Factor for Maint. Load Cases (Basic Wind Speed=30 mph) Maintanence Load Factor, L<sub>FM</sub> Design Ice Thickness, t<sub>i</sub>

Table 2-3 Importance Factors

Structure Classification	Wind Load Without Ice	Wind Load With Ice	Ice Thicknes s	Earthquake
	1	1	1	1

Table 2-4 Exposure Category Coefficients

Exposure Category	Zg	α	Kzmin	Ke	m
c -	900	9.5	0.85	1	0.6

Table 2-5 Topographic Categories **Kzt** 

1.000

Table 2-2 Wind Direction	ality Factor, Kd	
Structure Type	Kd	
1	0.95	DOES NOT CHANGE
Lattice Tower		
Gust Effect Factor G	h	
Structure Type	Gh	
1	1.00	DOES NOT CHANGE
Lattice Tower		
Shielding Factor, Ka		
Structure Type	Ka	
	0.90	DOES NOT CHANGE
Lattice Tower ▼		

CLIENT:

ForeSite / T-Mobile

PROJECT:

SUBJECT:

Antenna Loads - G Code with Sections 16 Revisions

Rad Center

ntenna AND	Mount With	out Ice																	Pound	ls		
Mounting Pole	Height (ft)	Model Number	#	Weight (lbs)	H (in)	*W (in)	D (in)	Ka	**A <sub>N</sub> (ft2)	***A <sub>T</sub> (ft2)	Aspect (FRONT)	Aspect (SIDE)	Ca (FRONT)	Ca (SIDE)	K <sub>z</sub>	q <sub>z</sub> (psf)	Wind Load (Front)	Wind Load (Side)	Dead Load	Total Wind Load (Front)	Total Wind Load (Side)	Total Dead Load
Pos. 1	59.00	Ericsson AIR 32 B66A B2A	1	172.0	59.3	12.9	8.7	0.90	5.30	3.58	4.60	6.81	1.29	1.39	1.133	30.4	187.2	136.1	171.96	187	136	1
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
																				94	69	
Pos. 2	59.00	RFS APXVAALL24_43-U-NA20	1	149.9	95.9	24.0	8.5	0.90	15.98	5.66	4.00	11.28	1.27	1.54	1.133	30.4	553.2	238.7	149.9	553	301	20
	59.00	Radio 4449 B71+B85	1	73.2	17.9	N/A	10.6	0.90	-	1.32	-	1.68	-	1.20	1.133	30.4	0.0	43.4	73.21			
	59.00	Radio 4415 B25	1	44.0	15.0	N/A	5.4	0.90	-	0.56	-	2.78	-	1.21	1.133	30.4	0.0	18.6	44			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
																				277	151	13
Pos. 3	59.00	Ericsson AIR6449 B41	1	115.0	33.1	20.6	8.6	0.90	4.74	1.98	1.61	3.85	1.20	1.26	1.133	30.4	155.3	68.1	115	155	68	11
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	_	-	-	0.0	0.0	0			
		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
																				78	35	
Pos. 4		Empty		0.0	-	-	-	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0	0	0	
		Empty Empty		0.0	-	-	-	0.90	-	_	-	-	-	-	-	-	0.0	0.0	0			
		Empty		0.0	-	-	_	0.90	-	-	-	-	-	-	-	-	0.0	0.0	0			
		Empty Empty		0.0	-	-	_	0.90	_		_	_	-	_	_	-	0.0	0.0	0			
		Empty		0.0	_	-	_	0.90	_	_	_	_	_	_	_		0.0	0.0	0			
		2		0.0				0.00									0.0	0.0	ŭ	0	0	ı

DL

#REF!

\* Enter N/A in the W column for front sheilded apurtanances.

\*\*\*  $A_T$  is the product of H and D

Mount	Height (ft)	Member	*L (in)	**W (in)	D (in)	*** Ca	K <sub>z</sub>	q <sub>z</sub> (psf)	Wind Load (PLF)
	59.00	3.0 STD Pipe	12.00	3.50	0.00	1.20	1.133	27.3	1
	59.00	2.5 STD Pipe	0.00	2.88	0.00	-	-	-	
	59.00	2.0 STD Pipe	12.00	2.38	0.00	1.20	1.133	27.3	
	59.00	3/4" SR	0.00	0.75	0.00	-	-	-	
	59.00	L2.5x2.5	0.00	2.50	2.50	-	-	-	
	59.00	L2x2	0.00	2.00	2.00	-	-	-	
	59.00	Angle Diagonal	0.00	0.00	0.00	-	-	-	
	59.00	Plate Horizontal (P6x5/8)	0.00	6.00	0.63	-	-	-	
	59.00	Tube Radial (3x3)	12.00	3.00	3.00	2.00	1.133	27.3	1
	59.00	Tube Radial (4.5x4.5)	0.00	4.50	4.50	-	-	-	
	59.00	Double Angle (LL2x2x3x0)	0.00	2.00	2.00	-	-	-	
	59.00	Double Angle (LL2.5x2.5x3x0)	0.00	5.00	2.50	-	-	-	
	59.00	Channel (Weak Axis Bending)	0.00	0.00	0.00	-	-	-	
	59.00	Invert U 5.375x3.625x.375	0.00	3.63	5.38	-	-	-	
		naion of the member							

 $<sup>^{\</sup>star\star}$   ${\rm A}_{\rm N}$  is the product of H and W

<sup>\*</sup>The dimension L is the longest dimension of the member

\*\* The dimension W is the height or width of the member that resists wind load

\*\*\* Ca will equal 1.2 for round members and 2.0 for flat members

CLIENT: ForeSite / T-Mobile

PROJECT:

Antenna Loads - G Code with Sections 16 Revisions SUBJECT:

> Kiz 1.0598241 reduction 0.22676 ti (in) 1.589736

#### Antenna AND Mount With Ice

ntenna AND	Mount With	ICE																	Pounds				
Mounting	Height		.,	н	w	D	14	*A <sub>N</sub>	*A <sub>T</sub>	*Volume	*Weight	**Ca	**Ca	14	$q_z$	Ice Wind	Ice Wind	Combined Wind	Combined Wind	Ice	**Total	**Total	Tota
Pole	(ft)	Model Number	#	(in)	(in)	(in)	Ka	(ft2)	(ft2)	(ft3)	Ice (lbs)	(FRONT)	(SIDE)	Kz	(psf)	Load (Front)	Load (Side)	Load (Front)	Load (Side)	Dead Load	Wind Load (Front)	Wind Load (Side)	lce Load
Pos. 1	59.00	Ericsson AIR 32 B66A B2A	1	59.3	12.9	8.7	0.90	1.66	1.57	3.05	170.74	0.73	0.76	1.133	6.9	7.5	7.4	50.0		171	50		
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	0			
Pos. 2	F0 00	DEC ADVIANTIQA 42 II NA20	1	05.0	24.0	0.5	0.00	0.70	2.20	6.00	205.27	0.70	0.00	1 100	6.0	10.0	10.0	107.7	66.4	205	25		
Pos. 2	59.00 59.00	RFS APXVAALL24_43-U-NA20 Radio 4449 B71+B85	1	95.9 17.9	24.0 13.2	8.5 10.6		2.72	2.38 0.70	6.88 1.31	385.27 73.15	0.73 0.70	0.83 0.70	1.133 1.133	6.9	12.2	12.3 3.0			385 73		86	
	59.00 59.00	Radio 4415 B25	1				0.90	-			48.00	0.70	0.70		6.9	0.0				13			
	59.00	Empty	'	15.0	13.2	5.4	0.90	-	0.52	0.86				1.133	6.9	0.0	2.3			40			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	U	69	43	Ł
Pos. 3	59.00	Ericsson AIR6449 B41	1	33.1	20.6	8.6	0.90	1.26	0.99	2.49	139.33	0.70	0.71	1.133	6.9	5.4	4.4	40.7	19.8	139		20	,
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0		0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
																					21	10	<u> </u>
Pos. 4		Empty		-	-	-	0.90	-	-	-	0.00		-	-	-	0.0	0.0			0	0	0	į.
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0			0			
		Empty		-	-	-	0.90	-	-	-	0.00	-	-	-	-	0.0	0.0	0.0	0.0	0		_	
																					0	0	1

<sup>\*</sup> A<sub>N</sub> ,A<sub>T</sub>, Volume Ice and Weight Ice are calculated per unit
\*\* Ca will equal 1.2 for all ice load calculations

lount	Height (ft)	Member	*L (in)	**W (in)	D (in)	***A <sub>N</sub> (ft2)	Volume Ice (ft3)	Weight Ice (lbs)	****Ca (FRONT)	Kz	q <sub>z</sub> (psf)	lce Wind Load (Front)	Combined Wind Load (Front)	lce Dea Loa
	59.00	3.0 STD Pipe	12.00	3.50	0.00	0.41	0.18	9.89	1.20	1.133	6.2	3.1	5.2	
	59.00	2.5 STD Pipe	0.00	2.88	0.00	-	-	-	-	-	-	-	-	
	59.00	2.0 STD Pipe	12.00	2.38	0.00	0.39	0.14	7.70	1.20	1.133	6.2	2.9	4.4	
	59.00	3/4" SR	0.00	0.75	0.00	-	-	-	-	-	-	-	-	
	59.00	L2.5x2.5	0.00	2.50	2.50	-	-	-	-	-	-	-	-	
	59.00	L2x2	0.00	2.00	2.00	-	-	-	-	-	-	-	-	
	59.00	Angle Diagonal	0.00	0.00	0.00	-	-	-	-	-	-	-	-	
	59.00	Plate Horizontal (P6x5/8)	0.00	6.00	0.63	-	-	-	-	-	-	-	-	
	59.00	Tube Radial (3x3)	12.00	3.00	3.00	0.40	0.27	15.28	1.20	1.133	6.2	3.0	6.1	
	59.00	Tube Radial (4.5x4.5)	0.00	4.50	4.50	-	-	-	-	-	-	-	-	
	59.00	Double Angle (LL2x2x3x0)	0.00	2.00	2.00	-	-	-	-	-	-	-	-	
	59.00	Double Angle (LL2.5x2.5x3x0)	0.00	5.00	2.50	-	-	-	-	-	-	-	-	
	59.00	Channel (Weak Axis Bending)	0.00	0.00	0.00	-	-	-	-	-	-	-	-	
	59.00	Invert U 5.375x3.625x.375	0.00	3.63	5.38	-	-	-	-	-	-	-	-	

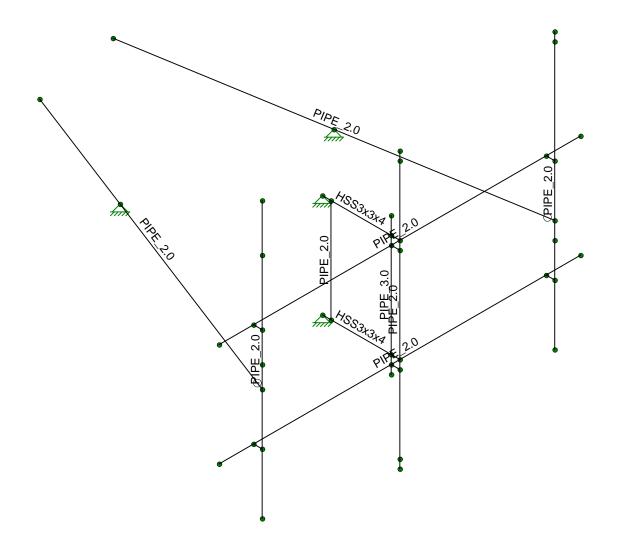
<sup>\*</sup>The dimension L is the longest dimension of the member

\*The dimension W is the height or width of the member that resists wind load

\*\*\*\* A<sub>N</sub> is the area of ice built up on the LW plane

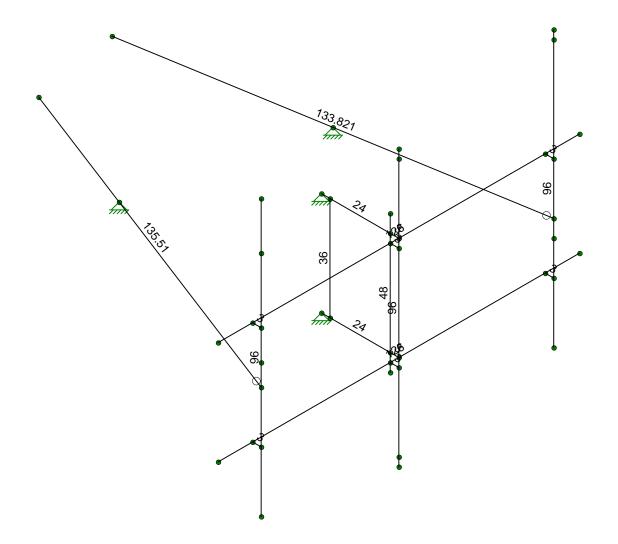
\*\*\*\* Ca will equal 1.2 for all ice load calculations





EFI Global, Inc/ ForeSite,		SK - 1
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049.00940 - 2075089		CTNL041A.R3D

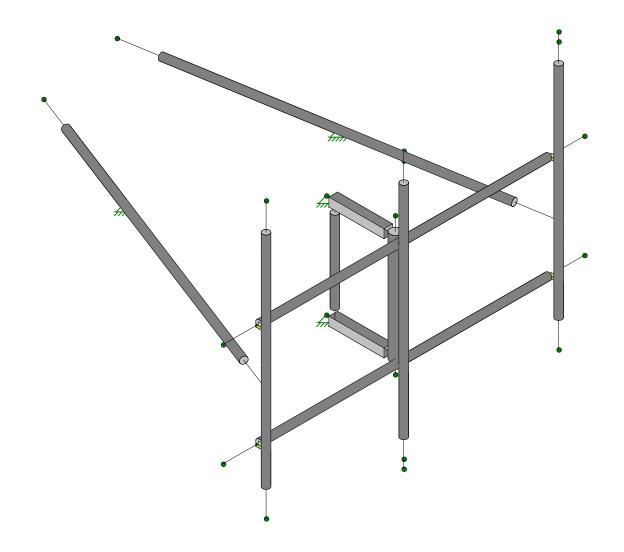




Member Length (in) Displayed Envelope Only Solution

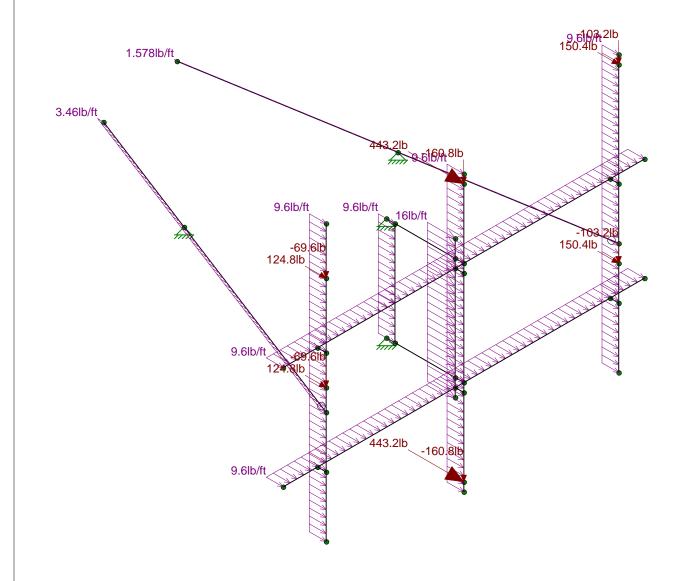
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AG	CTNL041A	Oct 26, 2020 at 3:32 PM
049.00940 - 2075089		CTNL041A.R3D





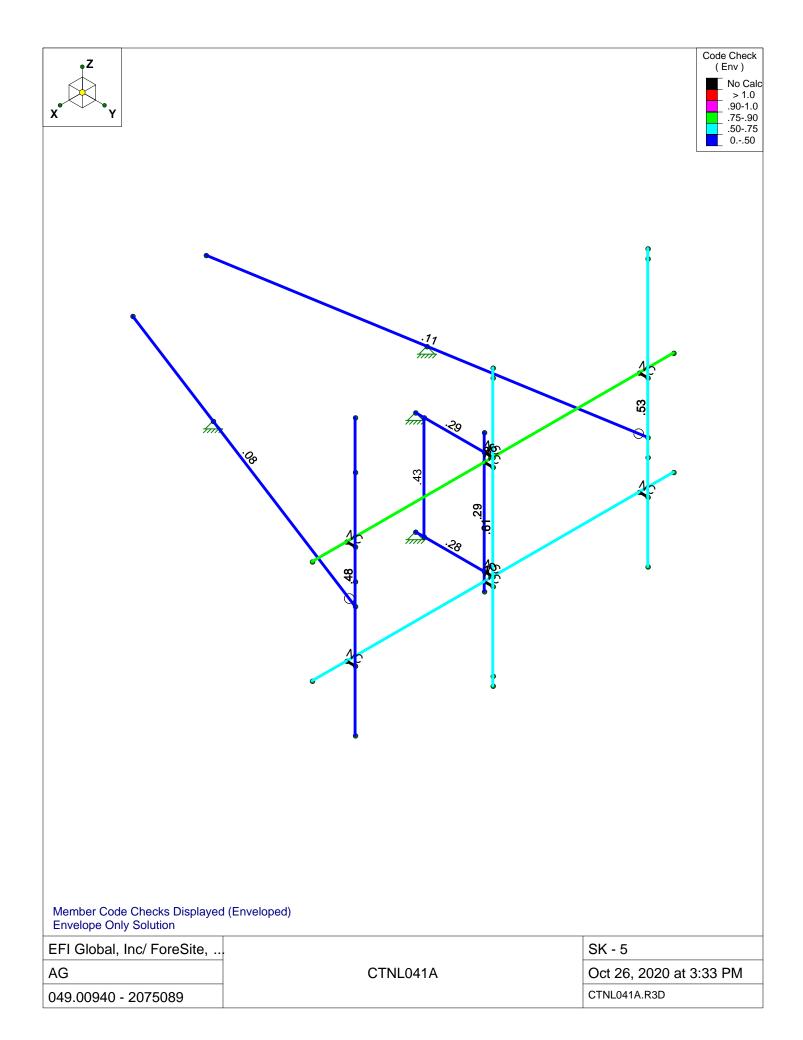
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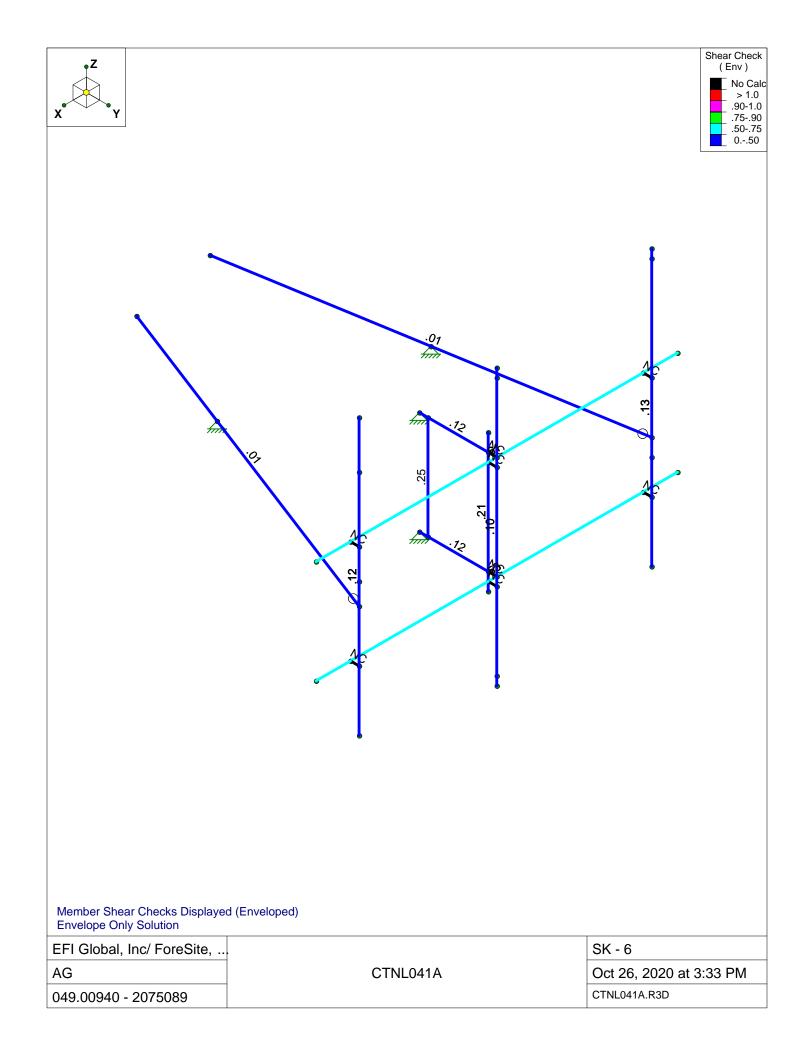




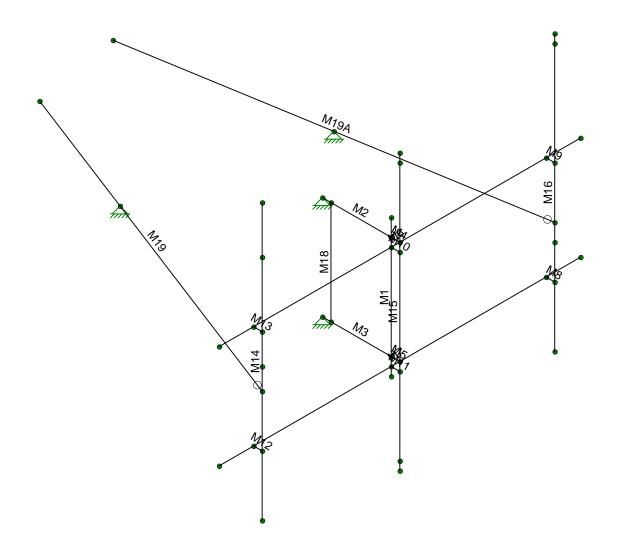
Loads: LC 1, DL + WL (NO ICE) 0 Degree Envelope Only Solution

EFI Global, Inc/ ForeSite,		SK - 4
AG	CTNL041A	Oct 26, 2020 at 3:32 PM
049.00940 - 2075089		CTNL041A.R3D



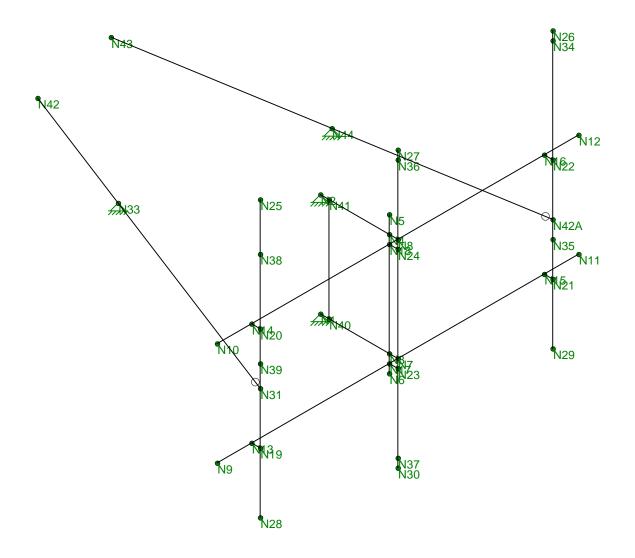






EFI Global, Inc/ ForeSite,		SK - 7
AG	CTNL041A	Oct 26, 2020 at 3:33 PM
049.00940 - 2075089		CTNL041A.R3D





EFI Global, Inc/ ForeSite,		SK - 8	
AG	CTNL041A	Oct 26, 2020 at 3:33 PM	
049.00940 - 2075089		CTNL041A.R3D	



Company : EFI Global, Inc/ ForeSite, LLC
Designer : AG
Job Number : 049.00940 - 2075089
Model Name : CTNL041A

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## (Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Z
Global Member Orientation Plane	XY
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 14th(360-10): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): LRFD
Cold Formed Steel Code	AISI NAS-01: ASD
Wood Code	AF&PA NDS-05/08: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-05
Masonry Code	ACI 530-05: ASD
Aluminum Code	AA ADM1-05: ASD - Building
	AISC 14th(360-10); ASD

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8



: EFI Global, Inc/ ForeSite, LLC : AG

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# (Global) Model Settings, Continued

Seismic Code	ASCE 7-05
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.035
Ct Z	.035
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	8.5
R Z	8.5
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	Not Entered
Occupancy Cat	I or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1

# **Project Grid Lines**

 Label	Start X [in]	End X [in]	Start Y [in]	End Y [in]	Start Bubble	End Bubble
		No Data to	Print			

## **Hot Rolled Steel Properties**

	Label	E [ksi]	G [ksi]	Nu	Therm (\1E	.Density[k/ft	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	1.1
3	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	.3	.65	.527	42	1.4	58	1.3
5	A500 Gr.B Rect	29000	11154	.3	.65	.527	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	.3	.65	.49	35	1.6	60	1.2
7	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3

## **Hot Rolled Steel Section Sets**

	Label	Shape	Type	Design List	Material	Design Rules	A [in2]	lyy [in4]	Izz [in4]	J [in4]
1	HR1	W4x13	Beam	Wide Flange	A36 Gr.36	Typical	3.83	3.86	11.3	.151

## **Member Primary Data**

	Label	I Joint	J Joint	Rotate	Section/Shape	Type	Design List	Material	Design
1	M4	N4	N8		RIGID	None	None	RIGID	Typical
2	M5	N3	N7		RIGID	None	None	RIGID	Typical
3	M8	N15	N21		RIGID	None	None	RIGID	Typical
4	M9	N16	N22		RIGID	None	None	RIGID	Typical
5	M10	N18	N24		RIGID	None	None	RIGID	Typical
6	M11	N17	N23		RIGID	None	None	RIGID	Typical
7	M12	N13	N19		RIGID	None	None	RIGID	Typical
8	M13	N14	N20		RIGID	None	None	RIGID	Typical



Company : EFI Global, Inc/ ForeS Designer : AG Job Number : 049.00940 - 2075089

: EFI Global, Inc/ ForeSite, LLC : AG

Model Name : CTNL041A

Oct 26, 2020 3:34 PM Checked By:\_

## Member Primary Data (Continued)

	Label	I Joint	J Joint	Rotate	Section/Shape	Type	Design List	Material	Design
9	M1	N5	N6				Wide Flan		Typical
10	M6	N10	N12		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
11	M7	N9	N11		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
12	M14	N25	N28		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
13	M15	N27	N30		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
14	M16	N26	N29		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
15	M2	N2	N4		HSS3x3x4	Beam	Wide Flan	A500 Gr.B Rect	
16	M3	N1	N3		HSS3x3x4	Beam	Wide Flan	A500 Gr.B Rect	Typical
17	M18	N41	N40		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
18	M19	N42	N31		PIPE 2.0	Beam	Wide Flan	A53 Gr.B	Typical
19	M19A	N43	N42A		PIPE_2.0	Beam	Wide Flan	A53 Gr.B	Typical

## Member Advanced Data

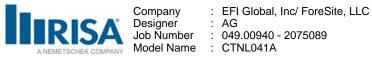
	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Analysis	Inactive	Seismic Design
1	M4					•	Yes			None
2	M5						Yes			None
3	M8						Yes			None
4	M9						Yes			None
5	M10						Yes			None
6	M11						Yes			None
7	M12						Yes			None
8	M13						Yes			None
9	M1						Yes			None
10	M6						Yes			None
11	M7						Yes			None
12	M14						Yes			None
13	M15						Yes			None
14	M16						Yes			None
15	M2						Yes			None
16	M3						Yes			None
17	M18						Yes			None
18	M19		BenPIN				Yes			None
19	M19A		BenPIN				Yes			None

# Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torq	Kyy	Kzz	Cb	<b>Function</b>
1	M1	PIPE 3.0	48	77.		Lbyy			•			Lateral
2	M6	PIPE 2.0	126			Lbyy						Lateral
3	M7	PIPE 2.0	126			Lbyy						Lateral
4	M14	PIPE 2.0	96			Lbyy						Lateral
5	M15	PIPE 2.0	96			Lbyy						Lateral
6	M16	PIPE 2.0	96			Lbyy						Lateral
7	M2	HSS3x3x4	24			Lbyy						Lateral
8	M3	HSS3x3x4	24			Lbyy						Lateral
9	M18	PIPE 2.0	36			Lbyy						Lateral
10	M19	PIPE 2.0	135.51			Lbyy						Lateral
11	M19A	PIPE_2.0	133.821			Lbyy						Lateral

# Joint Coordinates and Temperatures

	Label	X [in]	Y [in]	Z [in]	Temp [F]	Detach From Diap
1	N1	0	0	0	0	·
2	N2	0	0	36	0	



Oct 26, 2020 3:34 PM Checked By:\_

# Joint Coordinates and Temperatures (Continued)

	Label	X [in]	Y [in]	Z [in]	Temp [F]	Detach From Diap
3	N3	0	24	Ō	0	·
4	N4	0	24	36	0	
5	N5	0	24	42	0	
6	N6	0	24	-6	0	
7	N7	0	27	0	0	
8	N8	0	27	36	0	
9	N9	63	27	0	0	
10	N10	63	27	36	0	
11	N11	-63	27	0	0	
12	N12	-63	27	36	0	
13	N13	51	27	0	0	
14	N14	51	27	36	0	
15	N15	-51	27	0	0	
16	N16	-51	27	36	0	
17	N17	3	27	0	0	
18	N18	3	27	36	0	
19	N19	51	30	0	0	
20	N20	51	30	36	0	
21	N21	-51	30	0	0	
22	N22	-51	30	36	0	
23	N23	3	30	0	0	
24	N24	3	30	36	0	
25	N25	51	30	75	0	
26	N26	-51	30	75	0	
27	N27	3	30	66	0	
28	N28	51	30	-21	0	
29	N29	-51	30	-21	0	
30	N30	3	30	-30	0	
31	N31	51	30	18	0	
32	N33	19.82196	-50.696103	18	0	
33	N34	-51	30	72	0	
34	N35	-51	30	12	0	
35	N36	3	30	63	0	
36	N37	3	30	-27	0	
37	N38	51	30	58.5	0	
38	N39	51	30	25.5	0	
39	N40	0	3	0	0	
40	N41	0	3	36	0	
41	N42	2.162396	-96.403211	18	0	
42	N42A	-51	30	18	0	
43	N43	-29	-102	18	0	
44	N44	-40	-36	18	0	

# **Joint Boundary Conditions**

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N2	Reaction	Reaction	Reaction	_		
2	N1	Reaction	Reaction	Reaction			
3	N3						
4	N4						
5	N5						
6	N6						
7	N7						
8	N8						
9	N9						
10	N10						



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# Joint Boundary Conditions (Continued)

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
11	N11						
12	N12						
13	N13						
14	N14						
15	N15						
16	N16						
17	N17						
18	N18						
19	N19						
20	N20						
21	N21						
22	N22						
23	N23						
24	N24						
25	N25						
26	N26						
27	N27						
28	N28						
29	N29						
30	N30						
31	N33	Reaction	Reaction	Reaction			
32	N34						
33	N35						
34	N36						
35	N37						
36	N38						
37	N39						
38	N40						
39	N41						
40	N43						
41	N44	Reaction	Reaction	Reaction			

# **Basic Load Cases**

	BLC Description	Category	X Gravi	Y Gravi	Z Gravity	Joint	Point	Distrib	Area(M	.Surfac
1	DEAD LOAD	None			-1	6			,	
2	DEAD LOAD ICE	None				6		11		
3	WIND LOAD (NO ICE) FRONT	None				6		11		
4	WIND LOAD (NO ICE) SIDE	None				6		11		
5	WIND LOAD (ICE) FRONT	None				6		11		
6	WIND LOAD (ICE) SIDE	None				6		11		
7	LIVE LOAD 1	None				1				
8	LIVE LOAD 2	None				1				
9	LIVE LOAD 3	None								
10	MAINTENANCE LOAD 1	None				1				
11	MAINTENANCE LOAD 2	None				1				
12	MAINTENANCE LOAD 3	None				1				
13	MAINTENANCE LOAD 4	None								

## Joint Loads and Enforced Displacements (BLC 1 : DEAD LOAD)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	Z	-86
2	N35	L	Z	-86
3	N36	L	Z	-134
4	N37	L	Z	-134



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Joint Loads and Enforced Displacements (BLC 1 : DEAD LOAD) (Continued)
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	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
5	N38	L	Z	-58
6	N39	L	Z	-58

## Joint Loads and Enforced Displacements (BLC 2 : DEAD LOAD ICE)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	Z	-86
2	N35	L	Z	-86
3	N36	L	Z	-254
4	N37	L	Z	-254
5	N38	L	Z	-70
6	N39	L	Z	-70

## Joint Loads and Enforced Displacements (BLC 3: WIND LOAD (NO ICE) FRONT)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	Υ	94
2	N35	L	Υ	94
3	N36	L	Υ	277
4	N37	L	Υ	277
5	N38	L	Υ	78
6	N39	L	Υ	78

## Joint Loads and Enforced Displacements (BLC 4: WIND LOAD (NO ICE) SIDE)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	X	69
2	N35	L	X	69
3	N36	L	X	151
4	N37	L	X	151
5	N38	L	X	35
6	N39	L	X	35

## Joint Loads and Enforced Displacements (BLC 5: WIND LOAD (ICE) FRONT)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	Υ	26
2	N35	L	Υ	26
3	N36	L	Υ	69
4	N37	L	Υ	69
5	N38	L	Y	21
6	N39	L	Y	21

## Joint Loads and Enforced Displacements (BLC 6: WIND LOAD (ICE) SIDE)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N34	L	X	20
2	N35	L	X	20
3	N36	L	X	43
4	N37	L	X	43
5	N38		X	10
6	N39	L	X	10

## Joint Loads and Enforced Displacements (BLC 7 : LIVE LOAD 1)

	Joint Label	L,D,M	Direction	Magnitude[(lb,k-ft), (in,rad), (lb*s^2
1	N11		7	-250

## Joint Loads and Enforced Displacements (BLC 8 : LIVE LOAD 2)

Joint Label	L.D.M	Direction	Magnitude[(lb.k-ft), (in.rad), (lb*s^2



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: EFI Global, Inc/ ForeSite, LLC

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: 049.00940 - 2075089

CTNL041A

Member Distributed Loads (BLC 4: WIND LOAD (NO ICE) SIDE)

Direction

PX

PX

PX

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Joint	Loads and Enforc	ed Displace	ements (BLC 8 :	LIVE LOAD 2)	(Continued)	
	Joint Label		L,D,M	Direction	Magnitude[(lb	,k-ft), (in,rad), (lb*s^2
1	N9		L	Z		-250
Joint	Loads and Enforc	ed Displace	ements (BLC 10	: MAINTENANO	CE LOAD 1)	
	Joint Label		L,D,M	Direction	Magnitude[(lb	,k-ft), (in,rad), (lb*s^2
1	N29		L	Z		-500
Joint	Loads and Enforc	ed Displace	ements (BLC 11	: MAINTENANO	CE LOAD 2)	
	Joint Label		L,D,M	Direction	Magnitude[(lb	,k-ft), (in,rad), (lb*s^2
1	N30		L	Z		-500
Joint	Loads and Enforc	ed Displace	ements (BLC 12	: MAINTENANO	CE LOAD 3)	
	Joint Label		L,D,M	Direction	Magnitude[(lb	,k-ft), (in,rad), (lb*s^2
1	N28		L	Z		-500
<u>Memt</u>	ber Point Loads  Member Label		Direction	Magnitudellh	K-ft] L	ocation[in %]
	Wichiber Laber		No Data to		<u> </u>	.ocation[in, 70]
<u>Memt</u>	ber Distributed Loa				Ctart Location [in 0/1	End Looption(in 0/1
1	Member Label M1	Direction Z	Start Magnitude[lb/ft,	-10	O Start Location[in,%]	End Location[in,%] 0
2	M6	Z	-8	-8	0	0
3	M7	Z	-8	-8	0	0
4	M14	Z	-8	-8	0	0
5	M15	Z	-8	-8	0	0
6	M16	Z	-8	-8	0	0
7	M18	Z	-8	-8	0	0
8	M2	Z	-15	-15	0	0
9	<u>M3</u>	<u>Z</u>	-15	-15	0	0
10	M19	<u>Z</u>	-8	-8	0	0
11	M19A	Z	-8	-8	0	0
Memb	ber Distributed Loa	ads (BLC 3	: WIND LOAD (I	NO ICE) FRONT	)	
	Member Label	Direction	Start Magnitude[lb/ft,	End Magnitude[lb/ft,		End Location[in,%]
1	M1	PY	10	10	0	0
2	<u>M6</u>	PY	6	6	0	0
3	M7	PY	6	6	0	0
4	M14	PY	6	6	0	0
5	M15	PY	6	6	0	0
6	M16	PY	6	6	0	0
8	M18 M2	PY PY	6 14	6 14	0	0
9	M3	PY PY	14	14	0	0
10	M19	PY	6	6	0	0
11	M19A	PY	6	6	0	0
	WITOA		·	<u> </u>	<u> </u>	<u> </u>

3

Member Label

M1

M6

M7

10

6

6

Start Magnitude[lb/ft,...End Magnitude[lb/ft,...

10

6

6

End Location[in,%]

0

0

0

Start Location[in,%]

0

0

0



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## Member Distributed Loads (BLC 4: WIND LOAD (NO ICE) SIDE) (Continued)

	Member Label	Direction	Start Magnitude[lb/ft,	.End Magnitude[lb/ft,	Start Location[in,%]	End Location[in,%]
4	M14	PX	6	6	0	0
5	M15	PX	6	6	0	0
6	M16	PX	6	6	0	0
7	M18	PX	6	6	0	0
8	M2	PX	14	14	0	0
9	M3	PX	14	14	0	0
10	M19	PX	6	6	0	0
11	M19A	PX	6	6	0	0

## Member Distributed Loads (BLC 5: WIND LOAD (ICE) FRONT)

	Member Label	Direction	Start Magnitude[lb/ft,	.End Magnitude[lb/ft,	Start Location[in,%]	End Location[in,%]
1	M1	PY	5.2	5.2	0	0
2	M6	PY	4.4	4.4	0	0
3	M7	PY	4.4	4.4	0	0
4	M14	PY	4.4	4.4	0	0
5	M15	PY	4.4	4.4	0	0
6	M16	PY	4.4	4.4	0	0
7	M18	PY	4.4	4.4	0	0
8	M2	PY	6.1	6.1	0	0
9	M3	PY	6.1	6.1	0	0
10	M19	PY	4.4	4.4	0	0
11	M19A	PY	4.4	4.4	0	0

## Member Distributed Loads (BLC 6: WIND LOAD (ICE) SIDE)

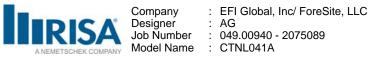
	Member Label	Direction	Start Magnitude[lb/ft,	End Magnitude[lb/ft,	Start Location[in,%]	End Location[in,%]
1	M1	PX	5.2	5.2	0	0
2	M6	PX	4.4	4.4	0	0
3	M7	PX	4.4	4.4	0	0
4	M14	PX	4.4	4.4	0	0
5	M15	PX	4.4	4.4	0	0
6	M16	PX	4.4	4.4	0	0
7	M18	PX	4.4	4.4	0	0
8	M2	PX	6.1	6.1	0	0
9	M3	PX	6.1	6.1	0	0
10	M19	PX	4.4	4.4	0	0
11	M19A	PX	4.4	4.4	0	0

## **Member Area Loads**

Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[psf]
			No Data to Pri	int		

## **Load Combinations**

	Description	S	P	S B		Fa E	3 F	-а	В	Fa	В	Fa	В	Fa	В	Fa	В	Fa	В	Fa	В	Fa	В	Fa
1	DL + WL (NO ICE) 0 Degree	Yes				1.2			3	1.6														
2	DL + WL (NO ICE) 30 Degree	Yes	Υ		1	1.2			3	1.3	4	.8												
3	DL + WL (NO ICE) 60 Degree	Yes	Υ		1	1.2			3	.8	4	1.3												
4	DL + WL (NO ICE) 90 Degree	Yes	Υ		1	1.2					4	1.6												
5	DL + WL (NO ICE) 120 Degree	Yes	Υ		1	1.2			3	8	4	1.3												
6	DL + WL (NO ICE) 150 Degree				1	1.2			3	-1	4	.8												
7	DL + WL (NO ICE) 180 Degree				1	1.2			3	-1.6														
8	DL + WL (NO ICE) 210 Degree				1	1.2			3	-1	4	8												
9	DL + WL (NO ICE) 240 Degree				1	1.2			3	8	4	-1												
10	DL + WL (NO ICE) 270 Degree	Yes	Υ		1	1.2					4	-1.6												



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# **Load Combinations (Continued)**

	Description	S P	S.	B	Fa	В	Fa	В	Fa	В	Fa	В	Fa	. В	Fa	В	Fa	В	Fa	В	Fa	В	Fa
11	DL + WL (NO ICE) 300 Degree	Yes \	(	1	1.2			3	.8	4	-1												
12	DL + WL (NO ICE) 330 Degree	Yes \	1	1	1.2			3	1.3	4	8												
13	DL + DL ICE + WL (ICE) 0 Degr	Yes \	/	1	1.2	2	1	5	1														
14	DL + DL ICE + WL (ICE) 30 De	Yes \	/	1	1.2	2	1	5	.866	6	.5												
15	DL + DL ICE + WL (ICE) 60 De	Yes \	1	1	1.2	2	1	5	.5	6	.866												
16	DL + DL ICE + WL (ICE) 90 De	Yes \	1	1	1.2	2	1			6	1												
17	DL + DL ICE + WL (ICE) 120 D	Yes \	/	1	1.2	2	1	5	5	6	.866												
18	DL + DL ICE + WL (ICE) 150 D	Yes \	1	1	1.2	2	1	5	8	6	.5												
19	DL + DL ICE + WL (ICE) 180 D	Yes \	/	1	1.2	2	1	5	-1														
20	DL + DL ICE + WL (ICE) 210 D	Yes \	1	1	1.2	2	1	5	8	6	5												
21	DL + DL ICE + WL (ICE) 240 D	Yes \	/	1	1.2	2	1	5	5		8												
22	DL + DL ICE + WL (ICE) 270 D	Yes \	1	1	1.2		1			6	-1												
23	DL + DL ICE + WL (ICE) 300 D	Yes \	/	1	1.2	2	1	5	.5	6	8												
24	DL + DL ICE + WL (ICE) 330 D	Yes \	/	1	1.2	2	1	5	.866	6	5												
25	DEAD LOAD + LIVE LOAD1	Yes \	1	1	1.2					7	1.5												
26	DEAD LOAD + LIVE LOAD2	Yes \	1	1	1.2					8	1.5												
27	DEAD LOAD + LIVE LOAD3	Yes \	/	1	1.2						1.5												
28	DL + MAIN L1+30MPH WL FR	Yes \	/	1	1.2	10	1.5	3	.082														
29	DL + MAIN L2+30MPH WL FR	Yes \	/	1	1.2	11	1.5	3	.082														
30	DL + MAIN L3+30MPH WL FR	Yes \	1	1	1.2		1.5		.082														
31	DL + MAIN L4+30MPH WL FR	Yes \	1	1	1.2	13	1.5	3	.082														
	DL + MAIN L1+30MPH WL SIDE			1	1.2	10	1.5	4	.082														
	DL + MAIN L2+30MPH WL SIDE			1	1.2	11	1.5	4	.082														
34	DL + MAIN L3+30MPH WL SIDE	Yes \	/	1	1.2	12	1.5	4	.082														
35	DL + MAIN L4+30MPH WL SIDE	Yes \	1	1	1.2	13	1.5	4	.082														
36	DL + MAIN L1+30MPH WL FR	Yes \	1	1	1.2	10	1.5	3	0														
37	DL + MAIN L2+30MPH WL FR	Yes \	1	1	1.2	11	1.5	3	0														
38	DL + MAIN L3+30MPH WL FR	Yes \	/	1	1.2	12	1.5	3	0														
39	DL + MAIN L4+30MPH WL FR	Yes \	/	1	1.2	13	1.5	3	0														
40	DL + MAIN L1+30MPH WL SID	Yes \	/	1	1.2		1.5																
41	DL + MAIN L2+30MPH WL SID	Yes \	/	1	1.2		1.5																
42	DL + MAIN L3+30MPH WL SID	Yes \	1	1	1.2		1.5																
43	DL + MAIN L4+30MPH WL SID	Yes \	/	1	1.2	12	1.5	4	0														

# **Envelope Joint Reactions**

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N2	max	1158.5222	40	250.9164	7	1170.5473	24	0	1	0	1	0	1
2		min	-1055.9243	34	-1997.7331	13	350.2089	6	0	1	0	1	0	1
3	N1	max	1030.9506	42	1835.1087	19	1159.1439	18	0	1	0	1	0	1
4		min	-1133.3479	32	565.0129	1	346.8708	12	0	1	0	1	0	1
5	N33	max	180.0268	6	589.2531	6	108.1672	24	0	1	0	1	0	1
6		min	-173.4356	12	-583.3376	12	35.5594	5	0	1	0	1	0	1
7	N44	max	68.5338	12	562.7177	9	136.4225	15	0	1	0	1	0	1
8		min	-66.5701	6	-557.2985	3	44.2045	9	0	1	0	1	0	1
9	Totals:	max	1435.5228	10	2018.2331	7	2520.8568	22						
10		min	-1435.5225	4	-2018.2266	1	1037.2854	4						

## **Envelope Joint Displacements**

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation	LC	Y Rotation	LC	Z Rotation [	LC
1	N1	max	0	32	Ö	1	0	12	-1.368e-03	7	3.4418e-03	30	1.5274e-02	10
2		min	0	42	0	19	0	18	-3.803e-03	13	-3.8301e-03	36	-1.5673e-02	4
3	N2	max	0	34	0	13	0	6	-1.4908e-03	8	3.4717e-03	34	1.8164e-02	10
4		min	0	40	0	7	0	24	-3.7784e-03	14	-3.8579e-03	40	-1.7737e-02	4
5	N3	max	.3564	4	0002	1	0296	7	-5.8098e-04	9	5.7565e-03	34	1.2961e-02	10

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Oct 26, 2020 3:34 PM Checked By:\_

# **Envelope Joint Displacements (Continued)**

	JOPE COIIIE					,								
	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation	LC	Y Rotation		Z Rotation [	LC
6		min	3483	10	0006	19	0842	13	-1.8635e-03	15	-6.4437e-03	40	-1.3154e-02	4
7	N4	max	.4011	4	.0007	13	0308	7	-3.2501e-04	6	5.8045e-03	34	1.4663e-02	10
8		min	4099	10	0002	7	084	13	-1.9134e-03	24	-6.4888e-03	40	-1.444e-02	4
9	N5	max	.4106	4	.0121	24	0308	7	-3.2438e-04	6	5.8045e-03	34	1.4663e-02	10
10	140	min	4233	10	.0018	6	084	13	-1.9137e-03	24	-6.4888e-03		-1.444e-02	4
11	N6	max	.3528	4	0038	9	0296	7	-5.8134e-04	9	5.7564e-03	34		10
12	INO			10	0038 0117	15	0842	13	-1.8634e-03		-6.4436e-03		-1.3154e-02	4
	N7	min	<u>3409</u>					7	-5.8098e-04	9	5.7565e-03	34		
13	IN7	max	.3959	4	0002	1	0316						-1.3154e-02	10
14	NO	min	3871	10	0006	19	0897	13	-1.8635e-03	<u>15</u>	-6.4437e-03			4
15	N8	max	.4444	4	.0007	13	0319	7	-3.2501e-04	6_	5.8045e-03	34		10
16		min	4 <u>539</u>	10	0002	7	0897	13		24	-6.4888e-03		-1.444e-02	4
17	<u>N9</u>	max	.3959	4	1647	9	.229	40	2.539e-03	8	1.069e-02	34	1.5784e-03	6
18		min	3877	10	1848	3	969	34	-4.009e-03	2	-5.5007e-03			12
19	N10	max	.4453	4	.2946	12	.229	40	9.0013e-03	7_	1.0739e-02	34	3.0252e-03	1
20		min	4542	10	275	6	9694	34	-1.0486e-02	1	-5.4718e-03	40	-3.0639e-03	7
21	N11	max	.3963	4	.1072	7	.1608	34		7	4.8325e-03	34	3.899e-03	4
22		min	3869	10	1304	1	-1.0506	40	-5.3808e-03	1	-1.1339e-02	40	-3.943e-03	10
23	N12	max	.4448	4	.2393	2	.1623	34	1.1125e-02	7	4.9163e-03	34	5.3811e-03	6
24		min	455	10	216	8	-1.0526	40	-1.2763e-02	1	-1.1517e-02	40	-5.2329e-03	12
25	N13	max	.3959	4	.1692	9	.1629	40	2.539e-03	8	1.0684e-02	34	1.5922e-03	6
26	1110	min	3877	10	1895	3	8407	34	-4.009e-03	2	-5.5076e-03			12
27	N14	max	.4453	4	.2755	11	.1633	40	9.0013e-03	7	1.0732e-02	34		1
28	1117	min	4542	10	2549	5	8405	34	-1.0486e-02	1	-5.4786e-03	<u> </u>	-3.048e-03	7
	N15			<del></del>				34	3.7612e-03	7	4.8393e-03	34		4
29	CIVI	max	.3963	4	.1238	6	.1028		-5.3808e-03	1	-1.1332e-02			
30	NAC	min	<u>3869</u>	10	14 <u>58</u>	12	9146	40	1.1125e-02	7	4.9232e-02	40	-3.943e-03 5.3673e-03	10
31	N16	max	.4448	4	.2152	2	.1033	34		7				6
32		min	<u>455</u>	10	192	8	9144	40	-1.2763e-02	1_	-1.151e-02	40		12
33	N17	max	.3959	4	.0363	10	0279	8	5.6517e-04	12	7.8438e-03	30		10
34		min	3872	10	0375	4	092	14	-1.7722e-03	6	-6.1108e-03		-1.1732e-02	4
35	<u>N18</u>	max	<u>.4445</u>	4	<u>.0415</u>	10	0308	9	1.4059e-03	_7_	7.9321e-03	34		10
36		min	454	10	0401	4	0916	15	-2.6103e-03	1_	-6.2065e-03		-1.2595e-02	4
37	N19	max	.3925	4	.1692	9	.1542	40	2.539e-03	8	1.0684e-02	34	1.5922e-03	6
38		min	3844	10	1895	3	8418	34	-4.009e-03	2	-5.5076e-03	40	-1.5323e-03	12
39	N20	max	.4431	4	.2755	11	.1541	40	9.0013e-03	7	1.0732e-02	34	3.0093e-03	1
40		min	4519	10	2549	5	8413	34	-1.0486e-02	1	-5.4786e-03	40	-3.048e-03	7
41	N21	max	.3846	4	.1238	6	.0927	34	3.7612e-03	7	4.8393e-03	34	3.899e-03	4
42		min	375	10	1458	12	9162	40	-5.3808e-03	1	-1.1332e-02	40		10
43	N22	max	.4348	4	.2152	2	.0927	34	1.1125e-02	7	4.9232e-03	34	5.3673e-03	6
44		min	4452	10	192	8	9156	40	-1.2763e-02	1	-1.151e-02	40		12
45	N23	max	.4311	4	.0363	10	032	8	5.6517e-04	12	7.8438e-03			10
46	1120	min	4217	10	0375	4	0959		-1.7722e-03	6				4
47	N24	max	.4823	4	.0415	10	0295	8	1.4059e-03	7	7.9321e-03			10
48	INZT	min	4926	10	0401	4	0964		-2.6103e-03	1				4
	NOE										1.0826e-02		3.0093e-03	4
49	N25	max	.5801	4	.7468	12	.1541	40		7_				7
50	NIOC	min	5328	10	669	6	8414	34		1	-5.5643e-03		-3.048e-03	7
51	N26	max	.6525	4	.8814	1	.0925	34		7	7.2215e-03	4		6
52		min	783	10	7 <u>928</u>	7	9158	40	-2.0094e-02	<u>1</u>			-5.2192e-03	
53	<u>N27</u>	max	.7052	4	.3276	1	0297	8	1.2797e-02	<u> 7</u>	9.2809e-03	_4_		10
54		min	7073	10	2903	7	0969	14		1_	-9.0067e-03	10	-1.2595e-02	4
55	N28	max	.3316	4	.2058	9	.1542		2.4654e-03	8	1.0558e-02	34		6
56		min	354	10	257	3	8425	34	-3.9353e-03	2			-1.5323e-03	12
57	N29	max	.3807	4	.1997	6	.0927	34		7	4.8347e-03	34	3.899e-03	4
58		min	3062	10	2551	12	9168	40	-5.2956e-03	1	-1.1199e-02	40	-3.943e-03	10
59	N30	max	.5534	4	.2606	1	0322	8	1.1843e-02	1				10
60		min	5521	10	2982	7	0964		-1.3044e-02	7	-6.3469e-03			4
61	N31	max	.4247	4	.1657	10	.1542		6.0917e-03	7	4.181e-03			2
62	.,,,,,	min	4249	10	1657	4	8416		-7.2961e-03				-1.2871e-03	
UZ		111111	. <del>1</del> 213	IU	.1007	7	.0410	l UT	55.6 65		3.53255 50	TU	5, 15 00	J



: EFI Global, Inc/ ForeSite, LLC: AG: 049.00940 - 2075089

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# **Envelope Joint Displacements (Continued)**

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation	LC	Y Rotation	LC	Z Rotation [	. LC
63	N33	max	Ō	12	Ō	12	Ō	5	-3.1609e-04	7	7.3144e-03	38	4.9037e-03	10
64		min	0	6	0	6	0	24	-7.4606e-03	30	-7.7541e-03	28	-4.9063e-03	4
65	N34	max	.6309	4	.8212	1	.0925	34	1.8447e-02	7	7.2213e-03	4	5.3673e-03	6
66		min	7521	10	7382	8	9158	40	-2.0094e-02	1	-1.1846e-02	40	-5.2192e-03	12
67	N35	max	.397	4	.0791	5	.0927	34	5.5654e-03	7	6.4992e-03	34	3.7362e-03	5
68		min	4008	10	0851	11	916	40	-6.8069e-03	1	-5.0536e-03	40	-3.7195e-03	10
69	N36	max	.6774	4	.2856	1	0297	8	1.2797e-02	7	9.2807e-03	4	1.2876e-02	10
70		min	6803	10	2519	7	0969	14	-1.4006e-02	1	-9.0064e-03	10	-1.2595e-02	4
71	N37	max	.5356	4	.2251	1	0322	8	1.1843e-02	1	8.0745e-03	42	1.1484e-02	10
72		min	5335	10	259	7	0964	14	-1.3043e-02	7	-6.3469e-03	32	-1.1732e-02	4
73	N38	max	.5171	4	.5365	12	.1541	40	1.1691e-02	7	1.0823e-02	34	3.0093e-03	1
74		min	4935	10	4832	6	8414	34	-1.3178e-02	1	-5.562e-03	40	-3.048e-03	7
75	N39	max	.4297	4	.1987	11	.1541	40	7.8105e-03	7	5.3088e-03	34	1.9742e-03	2
76		min	4393	10	1924	5	8415	34	-9.0592e-03	1	-6.6042e-03	40	-2.0136e-03	8
77	N40	max	.0471	4	0	1	0042	7	-1.3296e-03	7	3.4418e-03	30	1.5246e-02	10
78		min	0459	10	0	19	0116	13	-3.7316e-03	13	-3.8301e-03	36	-1.5639e-02	4
79	N41	max	.0534	4	.0001	13	0045	8	-1.4653e-03	8	3.4717e-03	34	1.8098e-02	10
80		min	0547	10	0	7	0115	14	-3.7044e-03	14	-3.8579e-03	40	-1.7677e-02	4
81	N42	max	.1918	10	.0742	4	.4505	34	1.2067e-04	7	7.1456e-03	38	3.9631e-03	10
82		min	192	4	0741	10	1135	40	-7.0244e-03	30	-7.9227e-03	28	-3.9702e-03	4
83	N42A	max	.4061	4	.0689	4	.0927	34	6.9955e-03	7	6.7041e-03	34	4.0594e-03	5
84		min	4066	10	069	10	9159	40	-8.1949e-03	1	-4.2781e-03	40	-3.981e-03	11
85	N43	max	.1481	11	.0247	11	.7962	40	2.2395e-03	34	7.6865e-03	30	1.6783e-03	11
86		min	1548	5	0258	5	2124	34	-1.0736e-02	40	-6.1766e-03	36	-1.7799e-03	5
87	N44	max	0	6	0	3	0	9	1.0645e-03	34	7.4906e-03	30	4.1584e-03	10
88		min	0	12	0	9	0	15	-1.191e-02	40	-6.3725e-03	36	-4.1476e-03	4

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

	Member	Shape	Code Check	Loc[in]	LC	Shear	Loc[in]	Dir L	C phi*Pnc	.phi*Pnt [	phi*Mn	phi*Mn	Cb Egn
1	M1	PIPE 3.0	.287	6	13	.209	6	4	59852.6	65205	5.7487	5.7487	1 H1-1b
2	M6	PIPE 2.0	.858	63	6	.615	63		7 8922.08	32130	1.8716	1.8716	1 H3-6
3	M7	PIPE 2.0	.699	63	32	.525	63		1 8922.08	32130	1.8716	1.8716	1H1-1b
4	M14	PIPE 2.0	.485	39	34	.117	57		6 14916.0	32130	1.8716	1.8716	1H1-1b
5	M15	PIPE 2.0	.608	66	1	.102	66	4	<mark>14916.0</mark>	32130	1.8716	1.8716	1H1-1b
6	M16	PIPE 2.0	.531	39	40	.129	57		1 14916.0	32130	1.8716	1.8716	1H1-1b
7	M2	HSS3x3x4	.285	24	40	.123	3	z	4 <mark>0</mark> 97902.6	101016	8.556	8.556	2H1-1b
8	M3	HSS3x3x4	.285	24	32	.121	3	z	3 <mark>6</mark> 97902.6	101016	8.556	8.556	2H1-1b
9	M18	PIPE 2.0	.434	0	40	.250	0	4	4 <mark>0</mark> 28843.4	32130	1.8716	1.8716	2H1-1b
10	M19	PIPE 2.0	.079	49.4	6	.006	49.4	2	7713.76	32130	1.8716	1.8716	2H1-1b*
11	M19A	PIPE 2.0	.115	66.9	21	.007	66.9		<mark>16</mark> 7909.70	32130	1.8716	1.8716	1H1-1b

# Exhibit F



# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CTNL041A

NL041/Gardner-NewLondon 25 Lower Boulevard New London, Connecticut 06320

December 6, 2020

EBI Project Number: 6220006133

Site Compliance Summary			
Compliance Status:	COMPLIANT		
Site total MPE% of FCC general population allowable limit:	70.92%		



December 6, 2020

T-Mobile Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, Connecticut 06002

Emissions Analysis for Site: CTNL041A - NL041/Gardner-NewLondon

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **25 Lower Boulevard** in **New London, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm²). The number of  $\mu$ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400  $\mu$ W/cm² and 467  $\mu$ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000  $\mu$ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 25 Lower Boulevard in New London, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) I NR channel (600 MHz Band) was considered for each sector of the proposed installation. This Channel has a transmit power of 80 Watts.
- 3) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 4 GSM channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 2 UMTS channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.



- 6) 4 LTE channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 7) 2 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 8) I LTE channel (BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of I20 Watts.
- 9) I NR channel (BRS Band 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of I20 Watts.
- 10) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 11) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 12) The antennas used in this modeling are the Ericsson AIR 32 for the 1900 MHz / 1900 MHz / 2100 MHz channel(s), the RFS APXVAALL24\_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s) in Sector A, the Ericsson AIR 32 for the 1900 MHz / 1900 MHz / 2100 MHz channel(s), the RFS APXVAALL24\_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 1900 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s) in Sector B, the Ericsson AIR 32 for the 1900 MHz / 1900 MHz / 2100 MHz channel(s), the RFS APXVAALL24\_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative



estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 13) The antenna mounting height centerline of the proposed antennas is 59 feet above ground level (AGL).
- 14) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 15) All calculations were done with respect to uncontrolled / general population threshold limits.



# **T-Mobile Site Inventory and Power Data**

Sector:	Α	Sector:	В	Sector:	C	
Antenna #:	l I	Antenna #:	ı	Antenna #:		
Make / Model:	Ericsson AIR 32	Make / Model:	Ericsson AIR 32	Make / Model:	Ericsson AIR 32	
Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz	
Gain:	15.35 dBd / 15.35 dBd / 15.85 dBd	Gain:	15.35 dBd / 15.35 dBd / 15.85 dBd	Gain:	15.35 dBd / 15.35 dBd / 15.85 dBd	
Height (AGL):	59 feet	Height (AGL):	59 feet	Height (AGL):	59 feet	
Channel Count:	8	Channel Count:	8	Channel Count:	8	
Total TX Power (W):	360 Watts	Total TX Power (W):	360 Watts	Total TX Power (W):	360 Watts	
ERP (W):	12,841.53	ERP (W):	12,841.53	ERP (W):	12,841.53	
Antenna A1 MPE %:	13.26%	Antenna B1 MPE %:	13.26%	Antenna C1 MPE %:	13.26%	
Antenna #:	2	Antenna #:	2	Antenna #:	2	
Make / Model:	RFS APXVAALL24_43-U- NA20	Make / Model:	RFS APXVAALL24_43-U- NA20	Make / Model:	RFS APXVAALL24_43-U- NA20	
Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz	
Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd / 15.45 dBd / 15.45 dBd	
Height (AGL):	57 feet	Height (AGL):	57 feet	Height (AGL):	57 feet	
Channel Count:	9	Channel Count:	9	Channel Count:	9	
Total TX Power (W):	380 Watts	Total TX Power (W):	380 Watts	Total TX Power (W):	380 Watts	
ERP (W):	10,465.36	ERP (W):	10,465.36	ERP (W):	10,465.36	
Antenna A2 MPE %:	17.92%	Antenna B2 MPE %:	17.92%	Antenna C2 MPE %:	17.92%	
Antenna #:	3	Antenna #:	3	Antenna #:	3	
Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449	
Frequency Bands:	2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz	
Gain:	22.05 dBd / 22.05 dBd	Gain:	22.05 dBd / 22.05 dBd	Gain:	22.05 dBd / 22.05 dBd	
Height (AGL):	59 feet	Height (AGL):	59 feet	Height (AGL):	59 feet	
Channel Count:	2	Channel Count:	2	Channel Count:	2	
Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts	
ERP (W):	38,477.89	ERP (W):	38,477.89	ERP (W):	38,477.89	
Antenna A3 MPE %:	39.74%	Antenna B3 MPE %:	39.74%	Antenna C3 MPE %:	39.74%	

# environmental | engineering | due diligence

Site Composite MPE %				
Carrier	MPE %			
T-Mobile (Max at Sector A):	70.92%			
Police	0%			
Fire	0%			
Tactical Channel	0%			
Site Total MPE %:	70.92%			

T-Mobile MPE % Per Sector				
T-Mobile Sector A Total:	70.92%			
T-Mobile Sector B Total:	70.92%			
T-Mobile Sector C Total:	70.92%			
Site Total MPE % :	70.92%			

T-Mobile Maximum MPE Power Values (Sector A)							
T-Mobile Frequency Band / Technology (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (μW/cm²)	Calculated % MPE
T-Mobile 1900 MHz GSM	4	1028.30	59.0	42.48	1900 MHz GSM	1000	4.25%
T-Mobile 1900 MHz LTE	2	2056.61	59.0	42.48	1900 MHz LTE	1000	4.25%
T-Mobile 2100 MHz LTE	2	2307.55	59.0	47.66	2100 MHz LTE	1000	4.77%
T-Mobile 600 MHz LTE	2	591.73	57.0	13.10	600 MHz LTE	400	3.27%
T-Mobile 600 MHz NR	Ţ	1577.94	57.0	17.46	600 MHz NR	400	4.37%
T-Mobile 700 MHz LTE	2	695.22	57.0	15.39	700 MHz LTE	467	3.29%
T-Mobile 1900 MHz UMTS	2	1052.26	57.0	23.29	1900 MHz UMTS	1000	2.33%
T-Mobile 1900 MHz LTE	2	2104.51	57.0	46.57	1900 MHz LTE	1000	4.66%
T-Mobile 2500 MHz LTE	I	19238.94	59.0	198.70	2500 MHz LTE	1000	19.87%
T-Mobile 2500 MHz NR	1	19238.94	59.0	198.70	2500 MHz NR	1000	19.87%
					Total:	70.92%	

<sup>•</sup> NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



# **Summary**

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	70.92%
Sector B:	70.92%
Sector C:	70.92%
T-Mobile Maximum	70.92%
MPE % (Sector A):	70.72%
Site Total:	70.92%
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **70.92**% of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

# Exhibit G

## **Deborah Chase**

**From:** Deborah Chase

**Sent:** Friday, April 2, 2021 5:38 PM **To:** 'pzw@newlondonct.org'

**Subject:** 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-ANCHOR)

Attachments: 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-

Anchor).pdf

#### Dear Mr. Reyes

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council today, April 2, 2021.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable.

If you could kindly confirm receipt.

Thank you.

#### **Deborah Chase**

Senior Project Coordinator & Analyst

Mobile: 860-490-8839



Save a tree. Refuse. Reduce. Reuse. Recycle.

## **Deborah Chase**

**From:** Deborah Chase

**Sent:** Friday, April 2, 2021 5:35 PM **To:** 'sfields@newlondonct.org'

**Subject:** 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-ANCHOR)

Attachments: 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-

Anchor).pdf

Dear Mr. Fields

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council today, April 2, 2021.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable.

If you could kindly confirm receipt.

Thank you.

#### **Deborah Chase**

Senior Project Coordinator & Analyst

Mobile: 860-490-8839



Save a tree. Refuse.Reduce. Reuse. Recycle.

## **Deborah Chase**

**From:** Deborah Chase

**Sent:** Friday, April 2, 2021 5:33 PM **To:** 'mpassero@newlondonct.org'

**Subject:** 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-ANCHOR)

Attachments: 25 LOWER BOULEVARD NEW LONDON CT 06320 T-MOBILE EM APPLICATION (CTNL041A-

Anchor).pdf

#### Dear

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council today, April 2, 2021.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable.

If you could kindly confirm receipt. Thank you.

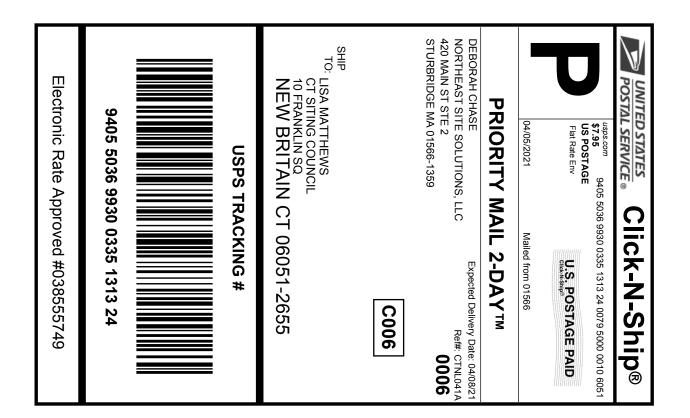
#### **Deborah Chase**

Senior Project Coordinator & Analyst

Mobile: 860-490-8839



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Cut on dotted line.

## Instructions

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- 2. Place your label so it does not wrap around the edge of the package.
- 3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
- 4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
- 5. Mail your package on the "Ship Date" you selected when creating this label.

# Click-N-Ship® Label Record

## **USPS TRACKING #:** 9405 5036 9930 0335 1313 24

529599668 04/02/2021 Trans. #: Print Date: Ship Date: 04/05/2021 04/08/2021 Delivery Date:

Priority Mail® Postage: Total:

\$7.95 \$7.95

From: DEBORAH CHASE Ref#: CTNL041A

NORTHEAST SITE SOLUTIONS, LLC

420 MAIN ST STF 2

STURBRIDGE MA 01566-1359

LISA MATTHEWS

CT SITING COUNCIL 10 FRANKLIN SQ

NEW BRITAIN CT 06051-2655

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## Instructions

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- 2. Place your label so it does not wrap around the edge of the package.
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- 4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
- 5. Mail your package on the "Ship Date" you selected when creating this label.

# Click-N-Ship® Label Record

## **USPS TRACKING #:** 9405 5036 9930 0335 1313 31

529599668 04/02/2021 Trans. #: Print Date: Ship Date: 04/05/2021 04/08/2021 Delivery Date:

Priority Mail® Postage: Total:

\$7.95 \$7.95

From: DEBORAH CHASE Ref#: CTNL041

NORTHEAST SITE SOLUTIONS, LLC

420 MAIN ST STE 2

STURBRIDGE MA 01566-1359

THOMAS J CURCIO

FIRE CHIEF-NEW LONDON FIRE DEPT.

289 BANK ST

NEW LONDON CT 06320-5521

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