Jennifer Iliades

From:

UPS Quantum View <pkginfo@ups.com>

Sent:

Friday, September 21, 2018 11:23 AM

To:

Jennifer Iliades

Subject:

UPS Delivery Notification, Tracking Number 1Z9Y45031311256789



Your package has been delivered.

Delivery Date: Friday, 09/21/2018

Delivery Time: 11:15 AM

At the request of Centerline Communications, LLC this notice alerts you that the status of the shipment listed below has changed.

Shipment Detail

Tracking Number:

1Z9Y45031311256789

Daniel V. Jerram, First Selectman

Town of New Hartford

Ship To: 530 MAIN ST

NEW HARTFORD, CT 06057

UPS Service:

UPS NEXT DAY AIR SAVER

Number of Packages:

1

Shipment Type:

Letter

Delivery Location:

OFFICE

HAYWARD

Reference Number 1:

CT1121 - CSC to First Selectman

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Help and Support Center

Jennifer Iliades

From: Sent:

UPS Quantum View <pkginfo@ups.com> Friday, September 21, 2018 11:23 AM

Jennifer Iliades

To: Subject:

UPS Delivery Notification, Tracking Number 1Z9Y45031311299779



Your package has been delivered.

Delivery Date: Friday, 09/21/2018

Delivery Time: 11:15 AM

At the request of Centerline Communications, LLC this notice alerts you that the status of the shipment listed below has changed.

Shipment Detail

Tracking Number:

1Z9Y45031311299779

Ruth Mulcahy, ZEO Town of New Hartford

530 MAIN ST Ship To:

NEW HARTFORD, CT 06057

US

UPS Service:

UPS NEXT DAY AIR SAVER

Number of Packages:

Shipment Type:

Letter

Delivery Location:

OFFICE

HAYWARD

Reference Number 1:

CT1121 - CSC to ZEO

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Help and Support Center

Jennifer Iliades

From: Sent:

UPS Quantum View < pkginfo@ups.com> Monday, September 24, 2018 10:12 AM

To:

Subject:

Jennifer Iliades

UPS Delivery Notification, Tracking Number 1Z9Y45031302344763

×

Your package has been delivered.

Delivery Date: Monday, 09/24/2018

Delivery Time: 10:09 AM

At the request of Centerline Communications, LLC this notice alerts you that the status of the shipment listed below has changed.

Shipment Detail

Tracking Number:

1Z9Y45031302344763

Paul Pedicone Crown Castle

Ship To:

3 CORPORATE DR CLIFTON PARK, NY 12065

UPS Service:

UPS NEXT DAY AIR SAVER

Number of Packages:

Shipment Type:

Letter

Delivery Location:

MET CUSTOMER WOMAN

RHOADES

Reference Number 1:

CT1121 - CSC to Crown

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Jennifer Iliades

From: Sent:

UPS Quantum View <pkginfo@ups.com> Friday, September 21, 2018 12:13 PM

To:

Subject:

Jennifer Iliades

UPS Delivery Notification, Tracking Number 1Z9Y45031331171323



Your package has been delivered.

Delivery Date: Friday, 09/21/2018

Delivery Time: 12:08 PM

At the request of Centerline Communications, LLC this notice alerts you that the status of the shipment listed below has changed.

Shipment Detail

Tracking Number:

1Z9Y45031331171323

Framingham Commons LLC 705 N MOUNTAIN RD NEWINGTON, CT 06111

Ship To:

US

UPS Service:

UPS NEXT DAY AIR SAVER

Number of Packages:

Shipment Type:

Letter

Delivery Location:

RECEIVER

LORI

Reference Number 1:

CT1121 - Ground LL

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Help and Support Center





September 20, 2018

Melanie A. Bachman Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Regarding: Notice of Exempt Modification – AT&T Site CT1121

Address: 115 Industrial Park Road, New Hartford, CT 06057 (a/k/a 115 Industrial

Park Access Road, 115 Greenwoods Industrial Park)

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC ("AT&T") currently maintains a wireless telecommunications facility on an existing 168-foot monopole tower at the above-referenced address, latitude 41.8862400, longitude -72.9661400. Said monopole is operated by Crown Castle.

AT&T desires to modify its existing telecommunications facility by swapping (3) antennas and adding (3) remote-radio heads. The centerline height of the existing antennas is and will remain at 119 feet.

Please accept this letter as notification pursuant to R.C.S.A §16-50j-73 for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Daniel V. Jerram, First Selectman of the Town of New Britain, Ruth Mulcahy, Zoning Enforcement Officer of the Town of New Britain, Crown Castle as tower owner and Framingham Commons, LLC, as property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Specifically:

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require an extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the modified facility will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety





standard. Please see the RF emissions calculation for AT&T's modified facility enclosed herewith.

- 5. The proposed modifications will not cause an ineligible change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading. *Please see the structural analysis dated August 29, 2018 by Hudson Design Group LLC enclosed herewith.*

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Jennifer Iliades

Site Acquisition Consultant Centerline Communications, LLC 750 West Center Street, Suite 301 West Bridgewater, MA 02379

jiliades@clinellc.com

Enclosures: Exhibit 1 – Field Card and GIS Map

Exhibit 2 – Construction Drawings Exhibit 3 – Structural Analysis

Exhibit 4 – RF Emissions Analysis Report Evaluation

Exhibit 5 – Mount Analysis

cc: Daniel V. Jerram, First Selectman, Town of New Britain

Ruth Mulcahy, Zoning Enforcement Officer, Town of New Britain

Crown Castle. Tower Operator

Framingham Commons, LLC, Property Owner

EXHIBIT 1

Map Block Lot 038-134-15C-1

Account

00284401

Property Information

		The state of the s		
115 INDUSTRIAL PARK ROAD				
FRAMINGHAM COMMONS LLC				
C/O GLOBAL SIGNAL ACQUISITION PME 331				
4017 WASH	INGTON	ROAD		
MCMURRA	Y	PA	15317	
4400	IND VA	CANT		
I				
	C/O GLOBA 331 4017 WASH MCMURRA	FRAMINGHAM COM C/O GLOBAL SIGNA 331 4017 WASHINGTON MCMURRAY	FRAMINGHAM COMMONS L C/O GLOBAL SIGNAL ACQU 331 4017 WASHINGTON ROAD MCMURRAY PA	

Fire District	1			
Census Tract				
Neighborhood	С			
Zoning Code	IP			
Acreage	0.23			
Utilities	Well, Septic			
Lot Setting/Desc	Rural	Level		

Photo

Sketch



Primary Construction Details

Year Built	
Stories	
Building Style	
Building Use	Attended to the second
Building Condition	A STATE OF THE STA
Floors	
Total Rooms	

Bedrooms	0	
Full Bathrooms		
Half Bathrooms		13-177
Bath Style		5577976
Kitchen Style		10000
Roof Style		
Roof Cover		

Exterior Walls	
Interior Walls	
Heating Type	
Heating Fuel	
AC Type	
Gross Bldg Area	
Total Living Area	0

Map Block Lot 038-134-15C-1

Account

00284401

Valuation Summary (Assessed value = 70% of Appraised Value)

Item	Appraised	Assessed		
Buildings	0	0		
Outbuildings	98700	69090		
Improvements	98700	69090		
Extras	0	0		
Land	660000	462000		
Total	758700	531090		

Sub Areas

Subarea Type	Gross Area (sq ft)	Living Area (sq ft)
e transcent de la companyant de la companya		
To	otal Area	0

Outbuilding and Extra Items

Туре	Description
Fence-8' Chain	400.00 L.F.
Pre Cast Cell	300.00 S.F.
Pre Cast Cell	240.00 S.F.
Malauri Ma	

Sales History

Owner of Record	Book/ Page	Sale Date	Sale Price	
FRAMINGHAM COMMONS LLC	234/ 515	5/10/2005		

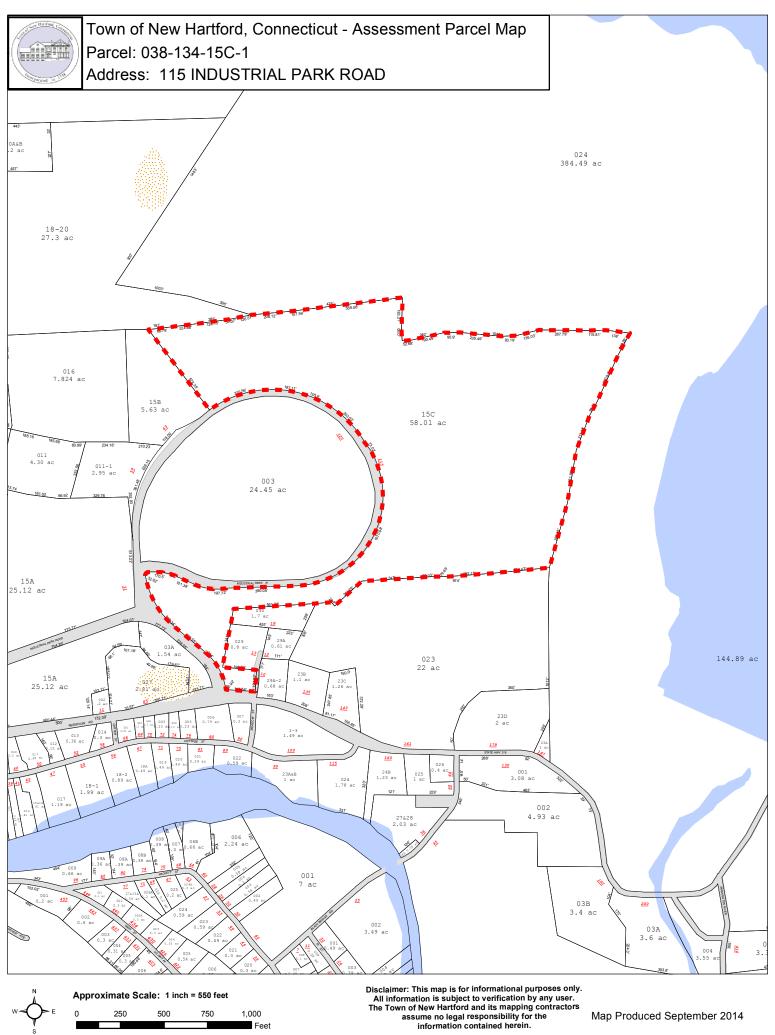


EXHIBIT 2

PROJECT INFORMATION

- ITEMS TO BE MOUNTED ON THE EXISTING MONOPOLE:

 NEW AT&T ANTENNA (HPA-65R-BUU-H6) (TOTAL OF 1 FOR ALPHA SECTOR).

 NEW AT&T ANTENNAS (SBNHH-1D65A) (TYP. OF 1 FOR BETA & GAMMA SECTOR,
- NEW AT&T RRUS 4415 B25 (PCS) (TYP. OF 1 PER SECTOR, TOTAL OF 3).

ITEMS TO BE MOUNTED AT EQUIPMENT LOCATION:

- SWAP BBU WITH (1) 5216 AND ADD (1) XMU.
- NEW AT&T RRUS 4478 B5 (850) (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T RRUS B14 4478 (850) (TOTAL OF 2).
- NEW DIPLEXERS (LPG21401) (TYP. OF 2 PER SECTOR, TOTAL OF 6).
- NEW SURGE ARRESTOR (TSXDC-43/OFM) (TOTAL OF 20).

• (6) ANTENNAS, (3) RRU'S, (6) TMA'S, (1) SURGE ARRESTOR

(12) COAX CABLES, (2) DC POWER & (1) FIBER.

SITE ADDRESS:

INDUSTRIAL ROAD

NEW HARTFORD, CT 06057

LATITUDE:

41.886240° N 41° 53' 10.46" N 72.966140° W 72° 57' 58.10" W

LONGITUDE: TYPE OF SITE:

MONOPOLE/INDOOR EQUIPMENT

TOWER HEIGHT:

166'-0"± 119'-0"±

RAD CENTER: CURRENT USE:

TELECOMMUNICATIONS FACILITY

PROPOSED USE:

TELECOMMUNICATIONS FACILITY



SITE NUMBER: CT1121

SITE NAME: NEW HARTFORD-INDUSTRIAL PARK

FA CODE: 10071155

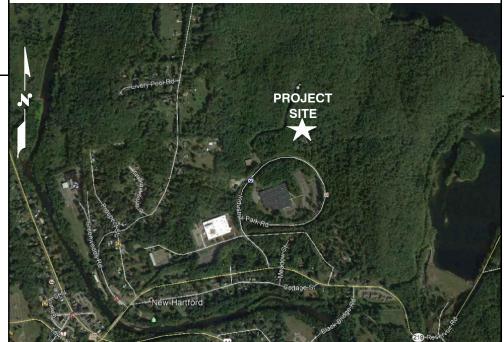
PACE ID: MRCTB032151, MRCTB032154, MRCTB032158

PROJECT: LTE 2C/3C/4C 2018 UPGRADE

DRAWING INDEX					
SHEET NO.	DESCRIPTION	REV.			
T-1	TITLE SHEET	1			
GN-1	GENERAL NOTES	1			
A-1	COMPOUND PLAN AND EQUIPMENT PLAN	1			
A-2	ANTENNA LAYOUTS & ELEVATION	1			
A-3	DETAILS	1			
A-4	SCHEMATIC AND NOTES	1			
G-1	GROUNDING DETAILS	1			
RF-1	RF PLUMBING DIAGRAM	1			

DIRECTIONS TO SITE: HEAD EAST TOWARD MA-106 E. TURN RIGHT ONTO MA-106 E. MARGE ONTO MA-24 S VIA THE RAMP TO FALL RIVER. MERGE ONTO MA-24 S. TAKE EXIT 14B TO MERGE ONTO 1-495 TOWARD WORCESTER TAKE EXIT 22 FOR I-90 TOWARD MASS/PIKE/BOSTON/ALBANY NY. KEEP LEFT AT THE FORK, FOLLOW SIGNS FOR I-90 W/SPRINGFIELD/ALBANY AND MERGE ONTO I-90 W. TAKE 9 FOR I-84 TOWARD US-20/HARTFORD/NEW YORK CITY. CONTINUE ONTO I-84. KEEP RIGHT STAY ON I-84. KEEP LEFT TO STAY I-84. TAKE EXIT 39 TOWARD FARMINGTON/CT-4 CONTINUE ONTO STATE HWY 508. STATE HWY 508 TURNS SLIGHTLY RIGHT AND BECOMES CT-4 W. CONTINUE STRAIGHT TO STAY ON CT-4 W. SLIGHT RIGHT TO STAY ON CT-4 W. CONTINUE ONTO CT-179 N. TURN RIGHT ONTO BRIDGE ST. TURN LEFT ONTO CT-179 N/RIVER RD. TURN LEFT ONTO US-44 W. TURN RIGHT ONTO RESERVOIR RD. TURN LEFT ONTO GREENWOOD INDUSTRIAL PARK.

VICINITY MAP



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- DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
- 2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
- 3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
- 4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OR RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

72 HOURS

BEFORE YOU DIG

CALL TOLL FREE 1-800-922-4455

OR CALL 811

WILLIAM TO UNDERGROUND SERVICE ALERT

CCI SITE NAME: NEW HARTFORD INDUSTRIAL PARK RD. CCI SITE #: 876392

Design Group LLC 750 WEST CENTER STREET, SUITE #301

TEL: (978) 557-5553 FAX: (978) 336-5586

NORTH ANDOVER, MA 01845

CENTERLINE

WEST BRIDGEWATER, MA 02379"

SITE NUMBER: CT1121 SITE NAME: NEW HARTFORD-INDUSTRIAL PARK CCI STE #: 876392

> INDUSTRIAL RD NEW HARTFORD, CT 06057 LITCHFIELD COUNTY



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	08/27/18	ISSUED FOR	REVIEW			MR	AT	DUC	0/2/	SCF N	13/1	$\langle \hat{\mathcal{C}} \rangle$
١.	DATE		REVISIO	ONS		BY	СНК	APP'D	155	S/ONAI	EMP,	11
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AT&T TITLE SHEET (LTE 2C/3C/4C) CT1121

GROUNDING NOTES

- 1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE—SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
- 2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- 3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL—OF—POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- 4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
- 5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
- 6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- 7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- 8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
- ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- 10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- 11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- 12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE. PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

CONTRACTOR - CENTERLINE SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) OWNER - AT&T MOBILITY

- PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
- 3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- 4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
- UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
- 7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
- 9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
- 10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
- 11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
- 13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

- 14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR—ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
- 15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
- 16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
- 17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT
- 19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMACNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
- 20. APPLICABLE BUILDING CODES:

SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

BUILDING CODE: IBC 2012 WITH 2016 CT STATE BUILDING CODE AMENDMENTS ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS LIGHTENING CODE: REFER TO ELECTRICAL DRAWINGS

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)

MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G, STRUCTURAL STANDARDS FOR STEEL

EQUIPMENT AND ANTENNA SUPPORTING STRUCTURES; REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

			ABBREVIATIONS		
AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
втсм	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	Р	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD J. CR.
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		



NORTH ANDOVER, MA 01845

TEL: (978) 557-5553 FAX: (978) 336-5586



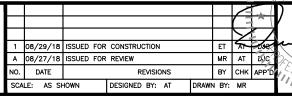
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT1121
SITE NAME: NEW HARTFORD-INDUSTRIAL PARK
CCI STE #: 876392

INDUSTRIAL RD
NEW HARTFORD, CT 06057
LITCHFIELD COUNTY

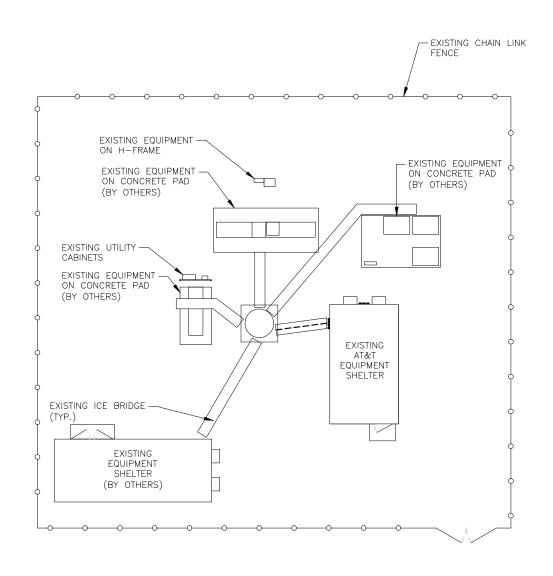


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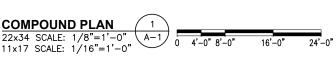


GENERAL NOTES
(LTE 2C/3C/4C)

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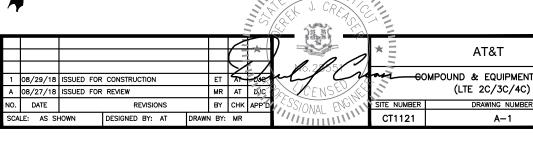
COMPOUND PLAN 22x34 SCALE: 1/8"=1'-0" 11x17 SCALE: 1/16"=1'-0"

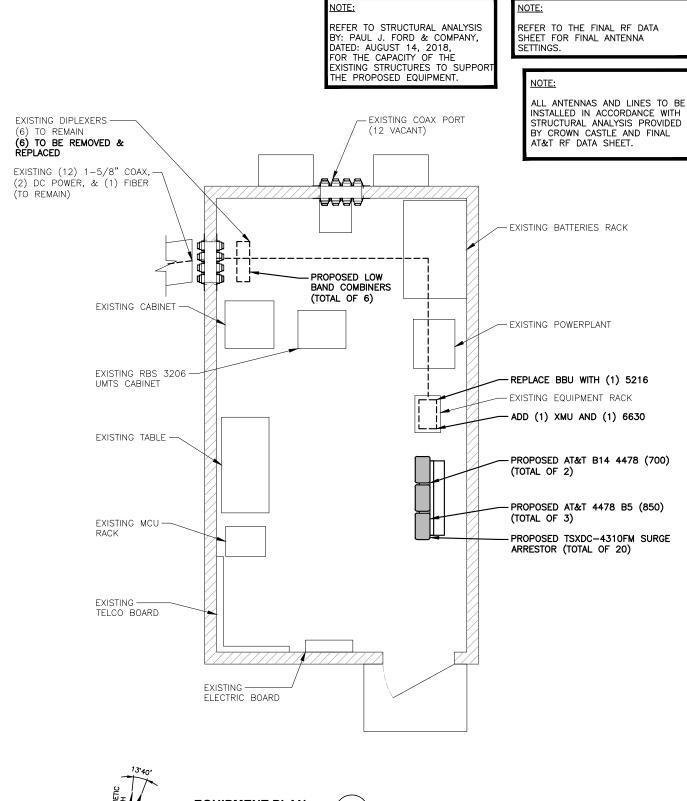
CENTERLINE

SITE NUMBER: CT1121 SITE NAME: NEW HARTFORD-INDUSTRIAL PARK CCI STE #: 876392

> INDUSTRIAL RD NEW HARTFORD, CT 06057 LITCHFIELD COUNTY











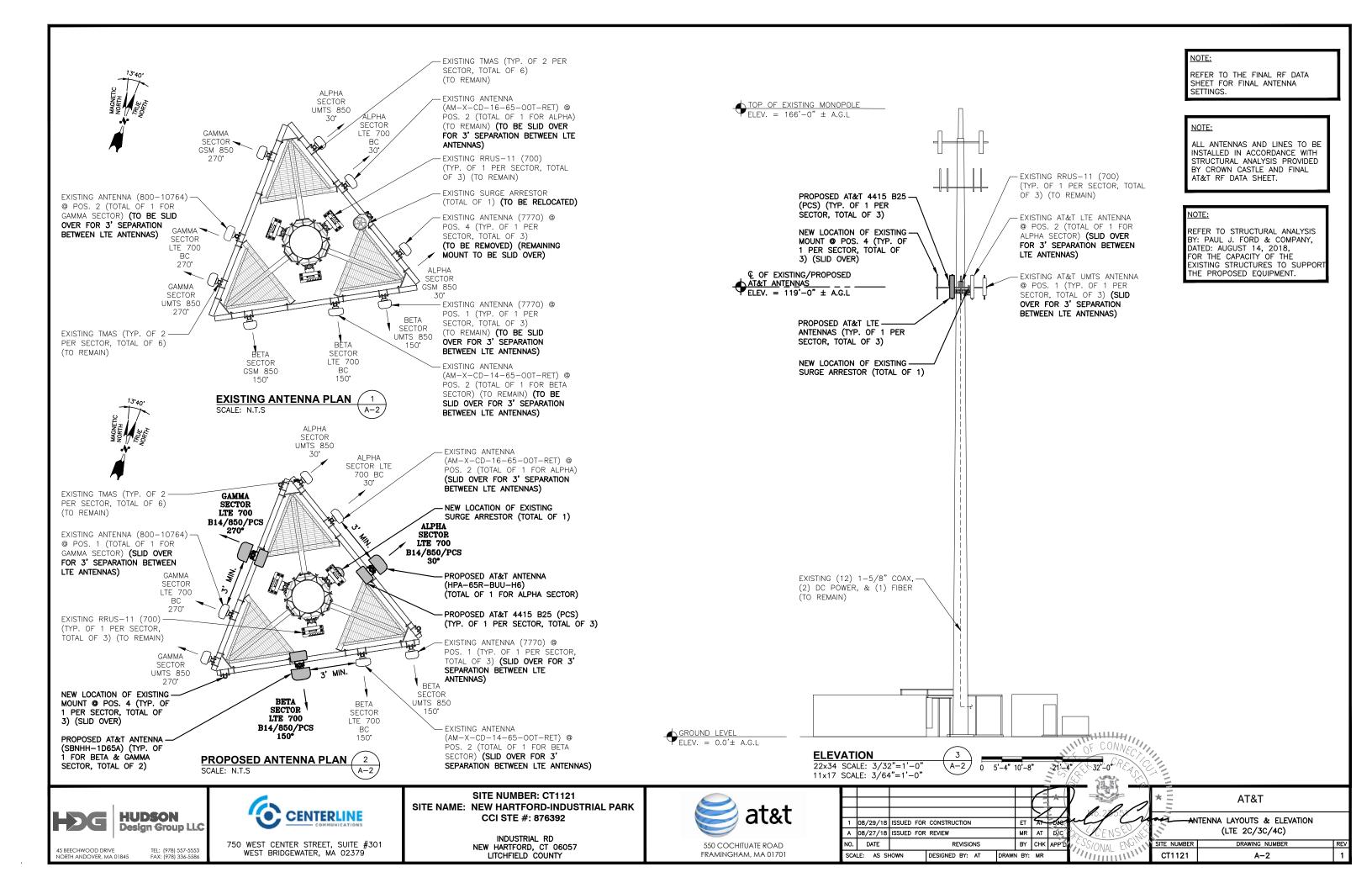


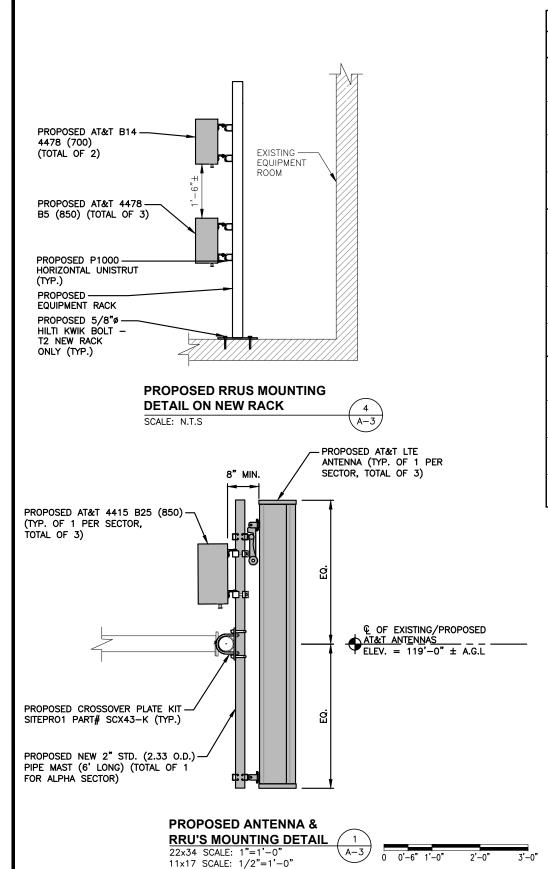
45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845

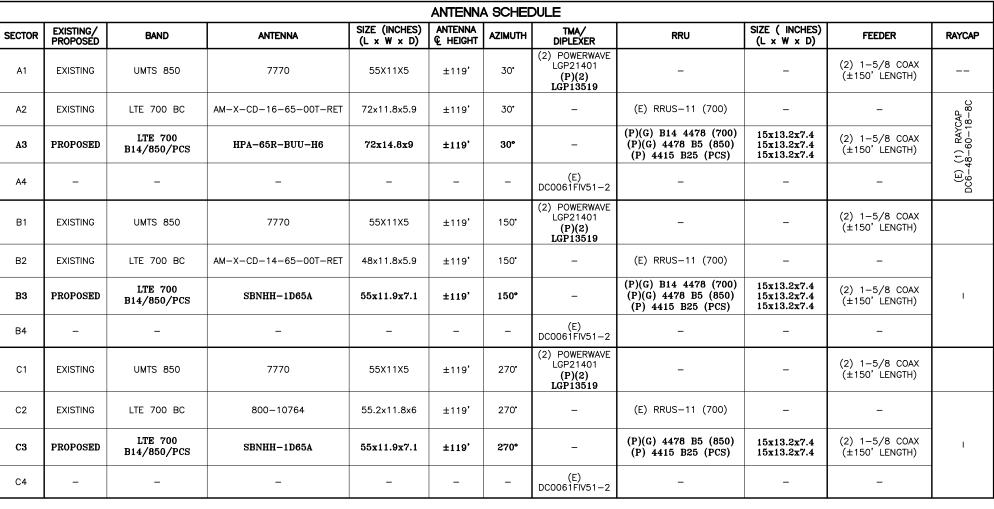
TEL: (978) 557-5553 FAX: (978) 336-5586

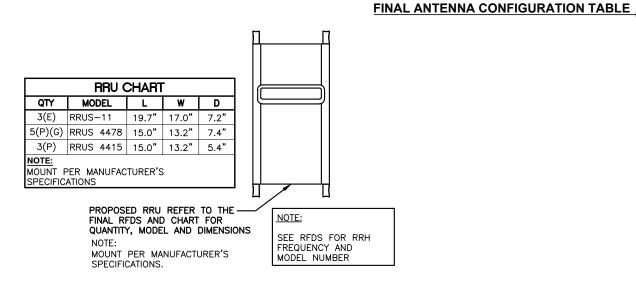
750 WEST CENTER STREET, SUITE #301 WEST BRIDGEWATER, MA 02379

-COMPOUND & EQUIPMENT PLAN









NOTE:

REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

REFER TO STRUCTURAL ANALYSIS BY: PAUL J. FORD & COMPANY, DATED: AUGUST 14, 2018, FOR THE CAPACITY OF THE THE STRUCTURES TO SUPPORTHE PROPOSED EQUIPMENT.

NOTE:

ALL ANTENNAS AND LINES TO BE INSTALLED IN ACCORDANCE WITH STRUCTURAL ANALYSIS PROVIDED BY CROWN CASTLE AND FINAL AT&T RF DATA SHEET.

AT&T

DETAILS

(LTE 2C/3C/4C)

DRAWING NUMBER

A-3

RRU DETAIL

SCALE: N.T.S

2
A-3



NORTH ANDOVER, MA 01845

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750 WEST CENTER STREET, SUITE #301

WEST BRIDGEWATER, MA 02379"

SITE NUMBER: CT1121
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CCI STE #: 876392

INDUSTRIAL RD
NEW HARTFORD, CT 06057
LITCHFIELD COUNTY



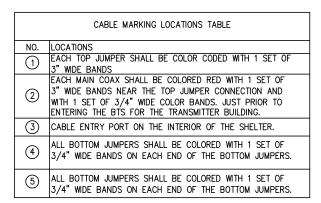
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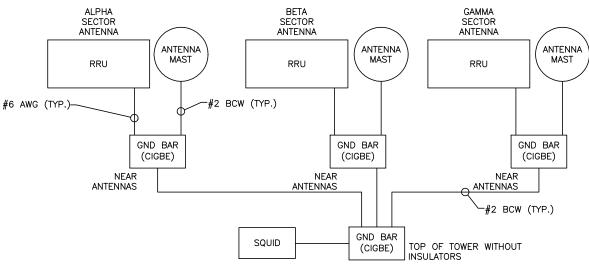
COAX COLOR CODING AND IDENTIFICATION NOTES

- 1. SECTOR ORIENTATION/AZIMUTH WILL VARY FROM REGION TO REGION AND IS SITE SPECIFIC. REFER TO RF REPORT FOR EACH SITE TO DETERMINE THE ANTENNA LOCATION AND FUNCTION OF EACH TOWER SECTOR FACE.
- 2. THE ANTENNA SYSTEM COAX SHALL BE LABELED WITH VINYL TAPE EXCEPT IN LOCATIONS WHERE ENVIRONMENTAL CONDITIONS CAUSE PHYSICAL DAMAGE, THE PHYSICAL TAGS ARE PREFERRED.
- 3. THE STANDARD IS BASED ON 8 COLORED TAPES—RED, BLUE, GREEN, YELLOW, ORANGE, BROWN, WHITE, AND VIOLET. THESE TAPES MUST BE 3/4" WIDE & UV RESISTANT SUCH AS SCOTCH 35 VINYL ELECTIRCAL COLOR CODING TAPE AND SHOULD BE READILY AVALIBLE TO THE ELECTRICIAN OR SUBCONTRACTOR ON SITE.
- 4. USING COLOR BANDS ON THE CABLES, MARK ALL RF CABLE BY SECTOR AND CABLE NUMBER AS SHOWN ON "CABLE MARKING COLOR CONVENTION TABLE".
- 5. WHEN AN EXISTING COAXIAL LINE THAT IS INTENDED TO BE A SHARED LINE BETWEEN GSM/3G AND IS-136/TDMA IS ENCOUNTERED, THE SUBCONTRACTOR SHALL REMOVE THE EXISTING COLOR CODING SCHEME AND REPLACE IT WITH THE COLOR CODING AND TAGGING STANDARD THAT IS OUTLINED IN THE CURRENT VERSION OF ND-00027. IN THE ABSENCE OF AN EXISTING COLOR CODING AND TAGGING SCHEME, OR WHEN INSTALLING PROPOSED COAXIAL CABLES, THE GUIDELINE SHALL BE IMPLEMENTED AT THE SITE REGARDLESS OF TECHNOLOGY.
- 6. ALL COLOR CODE TAPE SHALL BE 3M-35 AND SHALL BE INSTALLED USING A MINIMUM OF 3 WRAPS OF TAPE AND SHALL BE NEATLY TRIMMED AND SMOOTHED OUT SI AS TO AVOID UNRAVELING.
- 7. ALL COLOR BANDS INSTALLED AT THE TOP OF THE TOWER SHALL BE A MINIMUM OF 3" WIDE, AND SHALL HAVE A MINIMUM OF 3/4" OF SPACE BETWEEN EACH COLOR.
- 8. ALL COLOR CODES SHALL BE INSTALLED SO AS TO ALIGN NEATLY WITH ONE ANOTHER FROM SIDE TO SIDE.
- 9. IF EXISTING CABLES AT THE SITE ALREADY HAVE A COLOR CODING SCHEME AND THEY ARE NOT INTENDED TO BE REUSED OR SHARED WITH THE GSM TECHNOLOGY, THE EXISTING COLOR CODING SCHEME SHALL REMAIN UNTOUCHED.

CABLE MARKING TAGS

WHEN USING THE ALTERNATIVE LABELING METHOD, EACH RF CABLE SHALL BE IDENTIFIED WITH A METAL ID TAG MADE OF STAINLESS STEEL OR BRASS, THE TAG SHALL BE 1 1/2" IN DIAMETER WITH 1/4" STAMPED LETTERS AND NUMBERS INDICATING THE SECTOR, ANTENNA POSITION, AND CABLE NUMBER. THE ID MARKING LOCATIONS SHOULD BE AS PER CABLING MARKING LOCATIONS TABLE. THE TAG SHOULD BE ATTACHED WITH CORROSION PROOF WIRE AROUND THE CABLE AT THE SAME LOCATION AS DEFINED ABOVE. THE TAG SHOULD BE LABELED AS SHOWN ON THE GSM AND UMTS LINE TAG DETAIL.





SCHEMATIC DIAGRAM GROUNDING SYSTEM



FAX: (978) 336-5586

NORTH ANDOVER, MA 01845



WEST BRIDGEWATER, MA 02379"

SITE NUMBER: CT1121
SITE NAME: NEW HARTFORD-INDUSTRIAL PARK
CCI STE #: 876392

INDUSTRIAL RD NEW HARTFORD, CT 06057 LITCHFIELD COUNTY



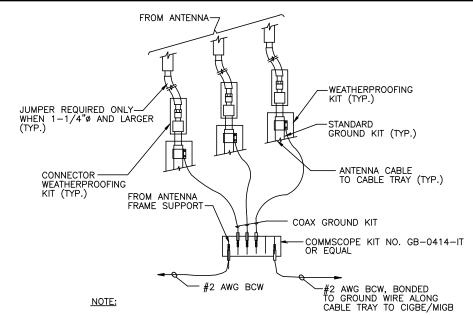
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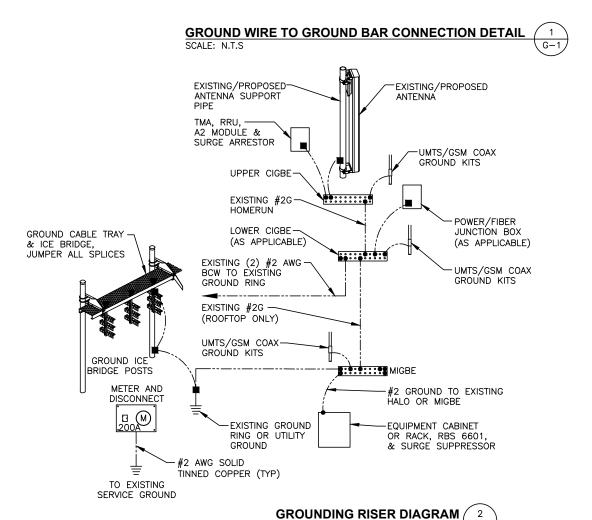
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(LTE 2C/3C/4C)

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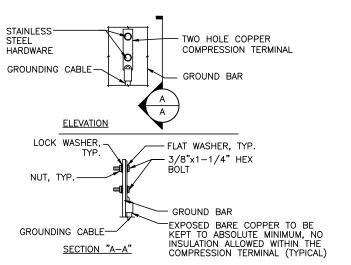
CT1121 A-4 1



1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.



SCALE: N.T.S



NOTE:

- 1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
- 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
- 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB



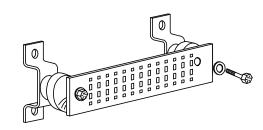
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

CABLE ENTRY PORTS (HATCH PLATES) (#2)
GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
TELCO GROUND BAR
COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
+24V POWER SUPPLY RETURN BAR (#2)
-48V POWER SUPPLY RETURN BAR (#2)
RECTIFIER FRAMES.

SECTION "A" - SURGE ABSORBERS

INTERIOR GROUND RING (#2)
EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
BUILDING STEEL (IF AVAILABLE) (#2)









NORTH ANDOVER, MA 01845

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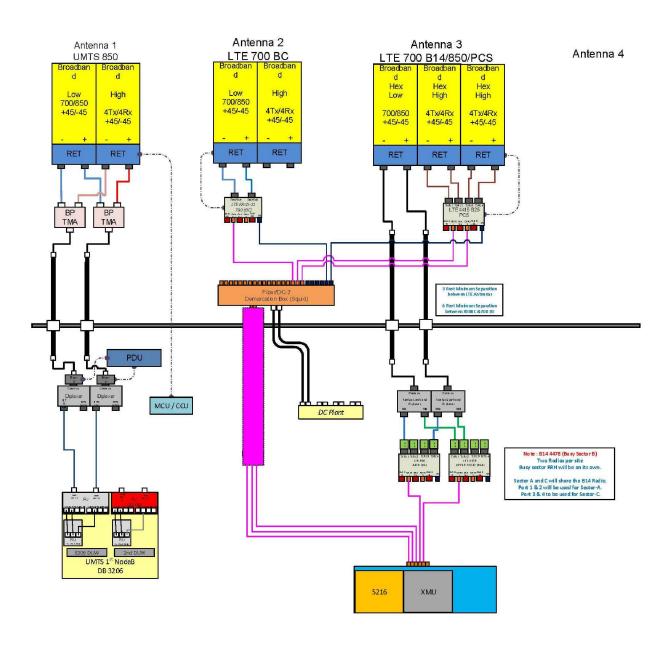
WEST BRIDGEWATER, MA 02379"

SITE NUMBER: CT1121
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INDUSTRIAL RD
NEW HARTFORD, CT 06057
LITCHFIELD COUNTY



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NOTE:

1. CONTRACTOR TO CONFIRM ALL PARTS
2. INSTALL ALL EQUIPMENT TO

MANUFACTURER'S RECOMMENDATIONS

NOTE: REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

HUDSONDesign Group LLC TEL: (978) 557-5553 FAX: (978) 336-5586

45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845



SITE NUMBER: CT1121 SITE NAME: NEW HARTFORD-INDUSTRIAL PARK CCI STE #: 876392

INDUSTRIAL RD NEW HARTFORD, CT 06057 LITCHFIELD COUNTY



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AT&T RF PLUMBING DIAGRAM (LTE 2C/3C/4C) SITE NUMBER CT1121 RF-1

EXHIBIT 3

PE PAUL J. FORD & COMPANY

Date: August 14, 2018

Winnie Japardi Crown Castle 2055 S. Stearman Drive Chandler, AZ 85286

Paul J. Ford and Company 250 East Broad st., Suite 600 Columbus, OH 43215 (614) 221-6679

Subject:

Structural Analysis Report

Carrier Designation:

AT&T Mobility Co-Locate

Carrier Site Number:

CT1121

Carrier Site Name:

NEW HARTFORD INDUSTRIAL PARK ROAD

Crown Castle Designation:

Crown Castle BU Number:

876392

Crown Castle Site Name: NEW HARTFORD / EXECUTIVE GREET

Crown Castle JDE Job Number: **Crown Castle Work Order Number:**

523211 1613794

Crown Castle Order Number:

453742 Rev. 1

Engineering Firm Designation:

Paul J. Ford and Company Project Number: 37518-1341.004.7805

Site Data:

115 Industrial Park RD, New Hartford, Litchfield County, CT

Latitude 41° 53' 10.48", Longitude -72° 57' 58.1"

168 Foot - Monopole Tower

Dear Winnie Japardi,

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1233936, in accordance with order 453742, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Existing + Reserved + Proposed Equipment

Sufficient Capacity

èssiona)

Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 120 mph converted to a nominal 3-second gust wind speed of 93 mph per Section 1609.3 and Appendix N as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1. Risk Category II, Exposure Category C and Topographic Category 1 with a maximum Topographic Factor, Kzt, of 1.0 were used in this analysis.

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

\$tructural Designer acuna@pauljford.com

tnxTower Report - version 8.0.2.1

TABLE OF CONTENTS

1) INTRODUCTION

2) ANALYSIS CRITERIA

Table 1 - Proposed Antenna and Cable Information

Table 2 - Existing and Reserved Antenna and Cable Information

Table 3 - Design Antenna and Cable Information

3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

3.1) Analysis Method

3.2) Assumptions

4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Table 6 - Tower Components vs. Capacity

4.1) Recommendations

5) APPENDIX A

tnxTower Output

6) APPENDIX B

Base Level Drawing

7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 168 ft Monopole tower designed by SUMMIT in September of 2000. The tower was originally designed for a wind speed of 90 mph per TIA/EIA-222-F.

2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 120 mph converted to a nominal 3-second gust wind speed of 93 mph per Section 1609.3 and Appendix N as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1. Risk Category II, Exposure Category C and Topographic Category 1 with a maximum Topographic Factor, Kzt, of 1.0 were used in this analysis.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		2	andrew	SBNHH-1D65A w/ Mount Pipe			
118.0	119.0	1	cci antennas	HPA-65R-BUU-H6 w/ Mount Pipe	-	-	_
		3	ericsson	RRUS 4415 B25			
	6		powerwave technologies	7020.00			

Table 2 - Existing and Reserved Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
400.0	168.0	3	communication components inc.	DTMA-1819-DD-12	40	4.5/0	
166.0	166.0		rfs celwave	APX16PV-16PVL-E	12	1-5/8	1
	166.0		tower mounts	Pipe Mount [PM 601-3]			
	3		alcatel lucent	RRH2X50-800			
	3		alcatel lucent	TD-RRH8X20-25			
157.0	157.0	3	commscope	DT465B-2XR w/ Mount Pipe	1	5/8	2
157.0	157.0	3	rfs celwave APXVTM14-C-120 w/ Mount Pipe				
		9	rfs celwave	ACU-A20-N	3	1 1/1	1
		1	tower mounts	Platform Mount [LP 712-1]	ა	1-1/4	ı
156.0		3	alcatel lucent	800 EXTERNAL NOTCH FILTER			
		3	alcatel lucent	800MHZ RRH			
155.0		1	tower mounts	Side Arm Mount [SO 102-3]	-	-	1
	154.0	3	alcatel lucent	1900MHz RRH (65MHz) w/ Mount Pipe			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note	
		3	antel	BXA-171085-12BF-2 w/ Mount Pipe				
1	147.0		antel	BXA-70063-6CF-2 w/ Mount Pipe	-	-	2	
145.0		6	rfs celwave	FD9R6004/2C-3L				
		6	antel	LPA-80080/6CF w/ Mount Pipe	12	1-5/8	1	
	145.0	1	tower mounts	Platform Mount [LP 403-1]				
120.0			tower mounts	Side Arm Mount [SO 102-3]	-	-	1	
	119.0	3	ericsson	RRUS 11				
	3 powerwave technologies 7770.00 w/ Mount Pipe		-	-	3			
		1	kathrein	800 10764 w/ Mount Pipe				
	119.0	1	kmw communications	AM-X-CD-14-65-00T-RET w/ Mount Pipe				
118.0		1	kmw communications	AM-X-CD-16-65-00T-RET w/ Mount Pipe	12	1-5/8		
		3	powerwave technologies	7770.00 w/ Mount Pipe	1 2	3/8 7/16	1	
	440.0	12	powerwave technologies	LGP2140X				
	118.0	1	raycap	DC6-48-60-18-8F				
		1	tower mounts	Platform Mount [LP 303-1]				
102.0	102.0	3	rfs celwave	APXV18-206517S-C w/ Mount Pipe	6	1-5/8	1	
		1	tower mounts	Pipe Mount [PM 601-3]				
	75.0	1	lucent	KS24019-L112A				
74.0	74.0	1	tower mounts	Side Arm Mount [SO 702-1]	1	1/2	1	

Notes:

Existing Equipment

1) 2) 3)

Reserved Equipment
Equipment To Be Removed

Table 3 - Design Antenna and Cable Information

Mounting Level (ft	 Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)

3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Criscuolo Shepard Associates, 2000.910, 03/10/2000	1532994	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Summit, 11428, 09/19/2000	1616556	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Summit, 11428, 09/19/2000	1441325	CCISITES
4-POST-MODIFICATION INSPECTION	GPD, 2010177.92, 01/04/2011	2808249	CCISITES
4-POST-MODIFICATION INSPECTION	TEP, 131001.876392, 04/10/2013	3839078	CCISITES

3.1) Analysis Method

tnxTower (version 8.0.2.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole was modified in conformance with the referenced modification drawings.
- 5) The existing monopole shaft has been reinforced using a Crown-approved system in accordance with the above referenced documents. However, in this analysis we found that due to the change from the EIA/TIA-222-F Standard (the Standard used in the original reinforcing design) to the TIA-222-G-2 Standard (the most current Standard) the shaft reinforcing was found to be ineffective and, therefore, not considered in this analysis.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	168 - 158.5	Pole	TP14x14x0.25	1	-0.76	340.18	9.0	Pass
L2	158.5 - 158	Pole	TP22x14x0.25	2	-0.76	340.18	9.0	Pass
L3	158 - 116.5	Pole	TP29.139x22x0.1875	3	-8.18	1091.80	71.9	Pass
L4	116.5 - 80.25	Pole	TP35x28.1189x0.25	4	-16.72	1822.96	96.0	Pass
L5	80.25 - 39.75	Pole	TP41.467x33.7259x0.3125	5	-26.21	2752.39	99.9	Pass
L6	39.75 - 0	Pole	TP47.68x39.9389x0.375	6	-40.33	3909.54	96.4	Pass
							Summary	
						Pole (L5)	99.9	Pass
						Rating =	99.9	Pass

Table 6 - Tower Component Stresses vs. Capacity - LC7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	79.9	Pass
1	Base Plate	0	83.6	Pass
1	Base Foundation Structural Steel	0	66.0	Pass
1	Base Foundation Soil Interaction	0	61.4	Pass
1	Flange Connection	68	9.9	Pass

Structure Rating (max from all components) =	99.9%
----------------------------------------------	-------

Notes:

4.1) Recommendations

The monopole and its foundation have sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

¹⁾ See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

APPENDIX A TNXTOWER OUTPUT

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- 1) Tower is located in Litchfield County, Connecticut.
- 2) ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
- 3) Basic wind speed of 93.00 mph.
- 4) Structure Class II.
- 5) Exposure Category C.
- 6) Topographic Category 1.
- 7) Crest Height 0.0000 ft.
- 8) Nominal ice thickness of 1.0000 in.
- 9) Ice thickness is considered to increase with height.
- 10) Ice density of 56.00 pcf.
- 11) A wind speed of 40.00 mph is used in combination with ice.
- 12) Temperature drop of 50.00 °F.
- 13) Deflections calculated using a wind speed of 60.00 mph.
- 14) A non-linear (P-delta) analysis was used.
- 15) Pressures are calculated at each section.
- 16) Stress ratio used in pole design is 1.
- 17) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- √ Use Code Stress Ratios
- √ Use Code Safety Factors Guys Escalate Ice
 Always Use Max Kz
 Use Special Wind Profile

Include Bolts In Member Capacity

Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric Distribute Leg Loads As Uniform Assume Legs Pinned

- √ Assume Rigid Index Plate
- √ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension
- √ Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt.

Autocalc Torque Arm Areas

Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

 ✓ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption

Poles

✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft	Sides	in	in	in	in	
L1	168.0000- 158.5000	9.5000	0.00	Round	14.0000	14.0000	0.2500		A53-B-35 (35 ksi)

Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	fť	fť	Sides	in	in	in	in	
L2	158.5000-	0.5000	0.00	Round	14.0000	22.0000	0.2500		A53-B-35
	158.0000								(35 ksi)
L3	158.0000-	41.5000	3.75	18	22.0000	29.1390	0.1875	0.7500	A607-65
	116.5000								(65 ksi)
L4	116.5000-	40.0000	4.50	18	28.1189	35.0000	0.2500	1.0000	A607-65
	80.2500								(65 ksi)
L5	80.2500-	45.0000	5.25	18	33.7259	41.4670	0.3125	1.2500	A607-65
	39.7500								(65 ksi)
L6	39.7500-	45.0000		18	39.9389	47.6800	0.3750	1.5000	A607-65
	0.0000								(65 ksi)

Tapered Pole Properties

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	W	w/t
	in	in²	in⁴	in	in	in³	in⁴	in²	in	
L1	14.0000	10.7992	255.3004	4.8622	7.0000	36.4715	510.6008	5.3964	0.0000	0
	14.0000	10.7992	255.3004	4.8622	7.0000	36.4715	510.6008	5.3964	0.0000	0
L2	14.0000	10.7992	255.3004	4.8622	7.0000	36.4715	510.6008	5.3964	0.0000	0
	22.0000	17.0824	1010.2644	7.6903	11.0000	91.8422	2020.5288	8.5361	0.0000	0
L3	22.3105	12.9812	780.3007	7.7434	11.1760	69.8193	1561.6281	6.4918	3.5420	18.891
	29.5596	17.2298	1824.5630	10.2778	14.8026	123.2595	3651.5267	8.6165	4.7985	25.592
L4	29.1692	22.1140	2169.9230	9.8935	14.2844	151.9085	4342.7013	11.0591	4.5089	18.036
	35.5014	27.5741	4206.7704	12.3363	17.7800	236.6013	8419.0762	13.7897	5.7200	22.88
L5	34.9840	33.1419	4674.7190	11.8617	17.1327	272.8529	9355.5890	16.5741	5.3858	17.234
	42.0585	40.8201	8734.6676	14.6098	21.0652	414.6485	17480.828	20.4139	6.7482	21.594
							5			
L6	41.4142	47.0909	9312.6205	14.0452	20.2889	458.9997	18637.494	23.5499	6.3692	16.985
							8			
	48.3577	56.3048	15918.303	16.7933	24.2214	657.1989	31857.552	28.1577	7.7317	20.618
			5				7			

Tower	Gusset	Gusset	Gusset Grade Adjust. Factor	Adjust.	Weight Mult.	Double Angle	Double Angle	Double Angle
Elevation	Area (per face)	Thickness	A_f	Factor A _r	-	Stitch Bolt Spacing	Stitch Bolt Spacing	Stitch Bolt Spacing
						Diagonals	Horizontals	Redundants
ft	ft ²	in				in	in	in
L1 168.0000-			1	1	1			
158.5000								
L2 158.5000-			1	1	1			
158.0000								
L3 158.0000-			1	1	1			
116.5000								
L4 116.5000-			1	1	1			
80.2500								
L5 80.2500-			1	1	1			
39.7500								
L6 39.7500-			1	1	1			
0.0000								

Feed Line/Linear Appurtenances - Entered As Area

Description	Face	Allow	Component	Placement	Total		C_AA_A	Weight
	or	Shield	Type		Number			
	Leg			ft			ft²/ft	plf
561(1-5/8")	С	No	CaAa (Out Of	166.0000 - 0.0000	10	No Ice	0.0000	1.35
			Face)			1/2" Ice	0.0000	2.65
			ŕ			1" Ice	0.0000	4.56
561(1-5/8")	С	No	CaAa (Out Of	102.0000 - 0.0000	2	No Ice	0.0000	1.35
,			Face)			1/2" Ice	0.0000	2.65
			,			1" Ice	0.0000	4 56

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg	Ornora	1,400	ft	rvarribor		ft²/ft	plf
561(1-5/8'')	С	No	CaAa (Out Of	166.0000 -	2	No Ice	0.1625	1.35
			Face)	102.0000		1/2" Ice	0.2625	2.65
						1" Ice	0.3625	4.56

HB114-1-0813U4-M5J(С	No	CaAa (Out Of	157.0000 - 0.0000	3	No Ice	0.0000	1.20
1 1/4")			Face)			1/2" Ice	0.0000	2.45
,			,			1" Ice	0.0000	4.30
HB058-M12-	С	No	CaAa (Out Of	157.0000 - 0.0000	1	No Ice	0.0000	0.24
XXXF(5/8'')	_		Face)			1/2" Ice	0.0000	1.06
(5, 5)			,			1" Ice	0.0000	2.49
*****							0.000	
LDF7-50A(1-5/8")	С	No	Inside Pole	145.0000 - 0.0000	12	No Ice	0.0000	0.82
	Ū					1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82
******						1 100	0.0000	0.02
LDF7-50A(1-5/8")	С	No	Inside Pole	118.0000 - 0.0000	12	No Ice	0.0000	0.82
_5 55/1(10/0)	9	0	1110100 1 010	. 10.0000 0.0000		1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82
FB-L98B-002-	С	No	Inside Pole	118.0000 - 0.0000	1	No Ice	0.0000	0.06
75000(3/8)	C	INO	iliside i die	110.0000 - 0.0000	'	1/2" Ice	0.0000	0.06
73000(3/8)						1" Ice	0.0000	0.06
WR-VG122ST-	С	No	Inside Pole	118.0000 - 0.0000	2	No Ice	0.0000	0.00
	C	INO	Iliside Fole	116.0000 - 0.0000	2	1/2" Ice		
BRDA(7/16)						1/2 ice 1" lce	0.0000	0.14
2" (Nominal) Canduit	0	No	CoAo (Out Of	102.0000 0.0000	4	No Ice	0.0000	0.14
2" (Nominal) Conduit	С	No	CaAa (Out Of	102.0000 - 0.0000	1		0.2375	0.72
			Face)			1/2" Ice	0.3375	2.48
011 (N)	_	NI.	0-1-10-101	440.0000		1" Ice	0.4375	4.84
2" (Nominal) Conduit	С	No	CaAa (Out Of	118.0000 -	1	No Ice	0.0000	0.72
			Face)	102.0000		1/2" Ice	0.0000	2.48
******						1" Ice	0.0000	4.84
	_		0 4 (0 , 0)	400 0000 0 0000	_		0.0000	0.50
LCF158-50JL(1-5/8")	С	No	CaAa (Out Of	102.0000 - 0.0000	5	No Ice	0.0000	0.52
			Face)			1/2" Ice	0.0000	2.03
	_					1" Ice	0.0000	4.16
LCF158-50JL(1-5/8")	С	No	CaAa (Out Of	102.0000 - 0.0000	1	No Ice	0.1980	0.52
			Face)			1/2" Ice	0.2980	2.03
******						1" Ice	0.3980	4.16
	_		In add 15 1	74.0000 0.0000	,	NI- I	0.0000	0.45
LDF4-50A(1/2")	С	No	Inside Pole	74.0000 - 0.0000	1	No Ice	0.0000	0.15
						1/2" Ice	0.0000	0.15
*******						1" Ice	0.0000	0.15
	_		0 4 (0 : 0:	00 5000 0 0000			0.0000	0.05
1 1/4" Flat	С	No	CaAa (Out Of	30.5000 - 0.0000	1	No Ice	0.2083	0.00
Reinforcement			Face)			1/2" Ice	0.3194	0.00
						1" Ice	0.4306	0.00
1" Flat Reinforcement	С	No		71.7500 - 30.5000	1	No Ice	0.1667	0.00
			Face)			1/2" Ice	0.2778	0.00
						1" Ice	0.3889	0.00
1" Flat Reinforcement	С	No	CaAa (Out Of	93.0000 - 83.0000	1	No Ice	0.1667	0.00
			Face)			1/2" Ice	0.2778	0.00
						1" Ice	0.3889	0.00

Feed Line/Linear Appurtenances Section Areas

Tower Sectio	Tower Elevation	Face	A_R	A_F	C _A A _A In Face	C _A A _A Out Face	Weight
n	ft		ft ²	ft ²	ft ²	ft ²	K
L1	168.0000-	Α	0.000	0.000	0.000	0.000	0.00
	158.5000	В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	2.438	0.12
L2	158.5000-	Α	0.000	0.000	0.000	0.000	0.00
	158.0000	В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	0.163	0.01
L3	158.0000-	Α	0.000	0.000	0.000	0.000	0.00
	116.5000	В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	13.488	1.12

Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Sectio	Elevation				In Face	Out Face	
n	ft		ft ²	ft ²	ft ²	ft ²	K
L4	116.5000-	Α	0.000	0.000	0.000	0.000	0.00
	80.2500	В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	15.852	1.55
L5	80.2500-39.7500	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	22.971	1.78
L6	39.7500-0.0000	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	25.207	1.75

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Sectio	Elevation	or	Thickness			In Face	Out Face	•
n	ft	Leg	in	ft²	ft ²	ft ²	ft ²	K
L1	168.0000-	Α	2.347	0.000	0.000	0.000	0.000	0.00
	158.5000	В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	9.478	1.21
L2	158.5000-	Α	2.339	0.000	0.000	0.000	0.000	0.00
	158.0000	В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	0.630	0.08
L3	158.0000-	Α	2.305	0.000	0.000	0.000	0.000	0.00
	116.5000	В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	51.751	8.75
L4	116.5000-	Α	2.230	0.000	0.000	0.000	0.000	0.00
	80.2500	В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	54.396	10.38
L5	80.2500-39.7500	Α	2.122	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	74.952	12.23
L6	39.7500-0.0000	Α	1.903	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	77.699	11.08

Feed Line Center of Pressure

Section	Elevation	CPx	CP _Z	CPx	CP _Z
Gootion	Liovation	OI X	Or Z	lce	lce
	ft	in	in	in	in
L1	168.0000-	-1.3747	0.7937	-2.1095	1.2179
	158.5000				
L2	158.5000-	-1.7561	1.0139	-2.7848	1.6078
	158.0000				
L3	158.0000-	-1.9594	1.1313	-3.2097	1.8531
	116.5000				
L4	116.5000-80.2500	-2.5730	1.4855	-4.0224	2.3223
L5	80.2500-39.7500	-3.1770	1.8342	-4.9773	2.8736
L6	39.7500-0.0000	-3.6134	2.0862	-5.4565	3.1503

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

Shielding Factor Ka

Tower	Feed Line	Description	Feed Line	K _a	K _a
Section	Record No.	-	Segment	No Ice	Ice
			Ĕlev.		

Discrete Tower Loads Offset Offsets: Azimuth C_AA_A C_AA_A Weight Description Face Placement Horz Adjustmen **Front** Side or Type Leg Lateral t Vert ft ft² ft² Κ ft ft ft Lightning Rod 5/8x4' С None 0.0000 170.0000 No Ice 0.2500 0.2500 0.03 1/2" 0.6635 0.6635 0.03 0.9732 0.9732 0.04 Ice 1" Ice APX16PV-16PVL-E 1.0000 0.0000 166.0000 6.0770 2.0028 0.04 Α From Leg No Ice 0.00 2.3262 0.07 1/2" 6.4350 2.00 Ice 6.8001 2.6569 0.11 1" Ice APX16PV-16PVL-E В 1.0000 0.0000 2.0028 0.04 From Leg 166.0000 No Ice 6.0770 0.00 1/2" 6.4350 2.3262 0.07 6.8001 2.6569 2.00 Ice 0.11 1" Ice APX16PV-16PVL-E 1.0000 0.04 С From Leg 0.0000 166.0000 No Ice 6.0770 2.0028 0.00 1/2" 6.4350 2.3262 0.07 6.8001 2.6569 2.00 0.11 Ice 1" Ice DTMA-1819-DD-12 1.0000 0.0000 166.0000 0.6050 0.3732 0.01 Α From Leg No Ice 0.00 1/2" 0.7126 0.4648 0.02 2.00 Ice 0.8276 0.5634 0.03 1" Ice DTMA-1819-DD-12 В 1.0000 0.0000 166.0000 No Ice 0.6050 0.3732 0.01 From Leg 0.00 1/2" 0.7126 0.4648 0.02 2.00 0.8276 0.5634 0.03 Ice 1" Ice DTMA-1819-DD-12 С From Leg 1.0000 0.0000 166.0000 No Ice 0.6050 0.3732 0.01 0.00 1/2" 0.7126 0.4648 0.02 2.00 Ice 0.8276 0.5634 0.03 1" Ice 0.0000 Pipe Mount [PM 601-3] С None 166.0000 No Ice 4.3900 4.3900 0.20 5.4800 1/2" 5.4800 0.24 Ice 6.5700 6.5700 0.28 1" Ice ****** APXVTM14-C-120 w/ 4.0000 0.0000 157.0000 No Ice 6.5799 4.9591 0.08 From Leg 7.0306 Mount Pipe 0.00 1/2" 5.7544 0.13 0.00 6.4723 0.19 Ice 7.4733 1" Ice APXVTM14-C-120 w/ 4.0000 157.0000 В From Leg 0.0000 No Ice 6.5799 4.9591 0.08 Mount Pipe 0.00 7.0306 5.7544 1/2" 0.13 6.4723 0.00 Ice 7.4733 0.19 1" Ice 6.5799 APXVTM14-C-120 w/ С 4.0000 4.9591 0.08 From Leg 0.0000 157.0000 No Ice Mount Pipe 0.00 7.0306 5.7544 0.13 1/2" 0.00 Ice 7.4733 6.4723 0.19 1" Ice DT465B-2XR w/ Mount 4.0000 0.08 0.0000 157.0000 9.3360 7.6339 Α No Ice From Leg 0.00 1/2" 9.9051 8.8197 0.16 Pipe 10.4391 0.00 9.7184 0.24 Ice 1" Ice DT465B-2XR w/ Mount 4.0000 9.3360 0.08 В From Leg 0.0000 157.0000 No Ice 7.6339 Pipe 0.00 1/2" 9.9051 8.8197 0.16 10.4391 9.7184 0.24 0.00 Ice 1" Ice DT465B-2XR w/ Mount С 4.0000 0.0000 157.0000 No Ice 9.3360 7.6339 0.08 From Leg Pipe 0.00 1/2" 9.9051 8.8197 0.16 0.00 10.4391 9.7184 0.24 Ice 1" Ice

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	0	ft		ft²	ft²	K
(3) ACU-A20-N	Α	From Leg	4.0000	0.0000	157.0000	No Ice	0.0667	0.1167	0.00
			0.00 0.00			1/2" Ice 1" Ice	0.1037 0.1481	0.1620 0.2148	0.00 0.00
(3) ACU-A20-N	В	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice	0.0667 0.1037 0.1481	0.1167 0.1620 0.2148	0.00 0.00 0.00
(3) ACU-A20-N	С	From Leg	4.0000 0.00 0.00	0.0000	157.0000	1" Ice No Ice 1/2" Ice	0.0667 0.1037 0.1481	0.1167 0.1620 0.2148	0.00 0.00 0.00
TD-RRH8X20-25	С	From Leg	4.0000 0.00	0.0000	157.0000	1" Ice No Ice 1/2"	4.0455 4.2975	1.5345 1.7142	0.07 0.10
(a) TD DDU(a) (a) as	0		0.00	0.0000	457.0000	Ice 1" Ice	4.5570	1.9008	0.13
(2) TD-RRH8X20-25	С	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice 1" Ice	4.0455 4.2975 4.5570	1.5345 1.7142 1.9008	0.07 0.10 0.13
(2) RRH2X50-800	В	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice 1" Ice	1.7008 1.8640 2.0345	1.2822 1.4275 1.5803	0.05 0.07 0.09
RRH2X50-800	С	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice	1.7008 1.8640 2.0345	1.2822 1.4275 1.5803	0.05 0.07 0.09
Platform Mount [LP 712-1]	С	None		0.0000	157.0000	1" Ice No Ice 1/2" Ice 1" Ice	24.5300 29.9400 35.3500	24.5300 29.9400 35.3500	1.34 1.65 1.96
2.375" OD x 4' Mount Pipe	Α	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice 1" Ice	0.8657 1.1106 1.3648	0.8657 1.1106 1.3648	0.02 0.03 0.04
2.375" OD x 4' Mount Pipe	В	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice 1" Ice	0.8657 1.1106 1.3648	0.8657 1.1106 1.3648	0.02 0.03 0.04
2.375" OD x 4' Mount Pipe	С	From Leg	4.0000 0.00 0.00	0.0000	157.0000	No Ice 1/2" Ice 1" Ice	0.8657 1.1106 1.3648	0.8657 1.1106 1.3648	0.02 0.03 0.04
800 EXTERNAL NOTCH FILTER	Α	From Leg	2.0000 0.00 1.00	0.0000	155.0000	No Ice 1/2" Ice 1" Ice	0.6601 0.7627 0.8727	0.3211 0.3983 0.4830	0.01 0.02 0.02
800 EXTERNAL NOTCH FILTER	В	From Leg	2.0000 0.00 1.00	0.0000	155.0000	No Ice 1/2" Ice 1" Ice	0.6601 0.7627 0.8727	0.3211 0.3983 0.4830	0.01 0.02 0.02
800 EXTERNAL NOTCH FILTER	С	From Leg	2.0000 0.00 1.00	0.0000	155.0000	No Ice 1/2" Ice 1" Ice	0.6601 0.7627 0.8727	0.3211 0.3983 0.4830	0.01 0.02 0.02
1900MHz RRH (65MHz) w/ Mount Pipe	Α	From Leg	2.0000 0.00 -1.00	0.0000	155.0000	No Ice 1/2" Ice 1" Ice	2.7273 3.0489 3.3824	3.2407 3.6916 4.1590	0.07 0.11 0.15
1900MHz RRH (65MHz) w/ Mount Pipe	В	From Leg	2.0000 0.00 -1.00	0.0000	155.0000	No Ice 1/2" Ice 1" Ice	2.7273 3.0489 3.3824	3.2407 3.6916 4.1590	0.07 0.11 0.15

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	٥	ft		ft²	ft²	K
1900MHz RRH (65MHz) w/	С	From Leg	2.0000	0.0000	155.0000	No Ice	2.7273	3.2407	0.07
Mount Pipe			0.00 -1.00			1/2" Ice 1" Ice	3.0489 3.3824	3.6916 4.1590	0.11 0.15
800MHZ RRH	Α	From Leg	2.0000	0.0000	155.0000	No Ice 1/2"	2.1342 2.3195	1.7730 1.9461	0.05 0.07
			1.00			Ice 1" Ice	2.5123	2.1267	0.10
800MHZ RRH	В	From Leg	2.0000 0.00 1.00	0.0000	155.0000	No Ice 1/2" Ice	2.1342 2.3195 2.5123	1.7730 1.9461 2.1267	0.05 0.07 0.10
800MHZ RRH	С	From Leg	2.0000	0.0000	155.0000	1" Ice No Ice	2.1342	1.7730	0.05
	J		0.00	0.0000	.00.000	1/2" Ice	2.3195 2.5123	1.9461 2.1267	0.07 0.10
Side Arm Mount [SO 102-	С	None		0.0000	155.0000	1" Ice No Ice	3.0000	3.0000	0.08
3]						1/2" Ice 1" Ice	3.4800 3.9600	3.4800 3.9600	0.11 0.14
******						i ice			
(2) LPA-80080/6CF w/ Mount Pipe	Α	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice	4.5639 5.1051 5.6116	10.2588 11.4274 12.3118	0.05 0.11 0.19
(0) 54 00000 (005 /	_					1" Ice			
(2) LPA-80080/6CF w/ Mount Pipe	В	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice	4.5639 5.1051 5.6116	10.2588 11.4274 12.3118	0.05 0.11 0.19
(2) LPA-80080/6CF w/ Mount Pipe	С	From Leg	4.0000 0.00 2.00	0.0000	145.0000	1" Ice No Ice 1/2" Ice	4.5639 5.1051 5.6116	10.2588 11.4274 12.3118	0.05 0.11 0.19
BXA-70063-6CF-2 w/ Mount Pipe	Α	From Leg	4.0000 0.00 2.00	0.0000	145.0000	1" Ice No Ice 1/2" Ice	7.8065 8.3569 8.8720	5.8008 6.9529 7.8191	0.04 0.10 0.17
	_					1" Ice			
BXA-70063-6CF-2 w/ Mount Pipe	В	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice 1" Ice	7.8065 8.3569 8.8720	5.8008 6.9529 7.8191	0.04 0.10 0.17
BXA-70063-6CF-2 w/ Mount Pipe	С	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice	7.8065 8.3569 8.8720	5.8008 6.9529 7.8191	0.04 0.10 0.17
BXA-171085-12BF-2 w/	Α	From Leg	4.0000	0.0000	145.0000	1" Ice No Ice	4.9710	5.2283	0.04
Mount Pipe	Λ,	r rom Log	0.00	0.0000	140.0000	1/2" Ice	5.5211 6.0361	6.3892 7.2610	0.09 0.14
BXA-171085-12BF-2 w/ Mount Pipe	В	From Leg	4.0000 0.00 2.00	0.0000	145.0000	1" Ice No Ice 1/2" Ice	4.9710 5.5211 6.0361	5.2283 6.3892 7.2610	0.04 0.09 0.14
	_					1" Ice			
BXA-171085-12BF-2 w/ Mount Pipe	С	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice	4.9710 5.5211 6.0361	5.2283 6.3892 7.2610	0.04 0.09 0.14
(2) FD9R6004/2C-3L	Α	From Leg	4.0000	0.0000	145.0000	1" Ice No Ice	0.3142	0.0762	0.00
,, 		9	0.00			1/2" Ice 1" Ice	0.3862 0.4656	0.1189 0.1685	0.01 0.01
(2) FD9R6004/2C-3L	В	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice 1" Ice	0.3142 0.3862 0.4656	0.0762 0.1189 0.1685	0.00 0.01 0.01

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	۰	ft		ft ²	ft²	K
(2) FD9R6004/2C-3L	С	From Leg	4.0000 0.00 2.00	0.0000	145.0000	No Ice 1/2" Ice	0.3142 0.3862 0.4656	0.0762 0.1189 0.1685	0.00 0.01 0.01
Platform Mount [LP 403-1]	С	None		0.0000	145.0000	1" Ice No Ice 1/2" Ice 1" Ice	18.8500 24.3000 29.7500	18.8500 24.3000 29.7500	1.50 1.80 2.09
**************************************	Α	From Leg	2.0000 0.00 -1.00	0.0000	120.0000	No Ice 1/2" Ice	2.7908 2.9984 3.2134	1.1923 1.3395 1.4957	0.05 0.07 0.10
RRUS 11	В	From Leg	2.0000 0.00 -1.00	0.0000	120.0000	1" Ice No Ice 1/2" Ice 1" Ice	2.7908 2.9984 3.2134	1.1923 1.3395 1.4957	0.05 0.07 0.10
RRUS 11	С	From Leg	2.0000 0.00 -1.00	0.0000	120.0000	No Ice 1/2" Ice 1" Ice	2.7908 2.9984 3.2134	1.1923 1.3395 1.4957	0.05 0.07 0.10
Side Arm Mount [SO 102-3]	С	None		0.0000	120.0000	No Ice 1/2" Ice 1" Ice	3.0000 3.4800 3.9600	3.0000 3.4800 3.9600	0.08 0.11 0.14
7770.00 w/ Mount Pipe	Α	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice	5.7460 6.1791 6.6067	4.2543 5.0137 5.7109	0.06 0.10 0.16
7770.00 w/ Mount Pipe	В	From Leg	4.0000 0.00 1.00	0.0000	118.0000	1" Ice No Ice 1/2" Ice 1" Ice	5.7460 6.1791 6.6067	4.2543 5.0137 5.7109	0.06 0.10 0.16
7770.00 w/ Mount Pipe	С	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	5.7460 6.1791 6.6067	4.2543 5.0137 5.7109	0.06 0.10 0.16
AM-X-CD-16-65-00T-RET w/ Mount Pipe	Α	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	8.2619 8.8215 9.3462	6.3042 7.4790 8.3676	0.07 0.14 0.21
AM-X-CD-14-65-00T-RET w/ Mount Pipe	В	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	5.2316 5.6179 6.0119	4.0153 4.6330 5.2567	0.05 0.10 0.15
800 10764 w/ Mount Pipe	С	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	5.7119 6.1273 6.5428	4.2940 4.9925 5.6620	0.06 0.11 0.17
HPA-65R-BUU-H6 w/ Mount Pipe	Α	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	9.8953 10.4700 11.0098	8.1125 9.3041 10.2095	0.08 0.16 0.25
SBNHH-1D65A w/ Mount Pipe	В	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	5.8154 6.2024 6.5968	5.0515 5.7157 6.3790	0.06 0.11 0.17
SBNHH-1D65A w/ Mount Pipe	С	From Leg	4.0000 0.00 1.00	0.0000	118.0000	No Ice 1/2" Ice 1" Ice	5.8154 6.2024 6.5968	5.0515 5.7157 6.3790	0.06 0.11 0.17
(4) LGP2140X	Α	From Leg	4.0000 0.00 0.00	0.0000	118.0000	No Ice 1/2" Ice	1.0800 1.2137 1.3548	0.3580 0.4536 0.5563	0.01 0.02 0.03

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	C _A A _A Side	Weight
			Vert ft ft ft	٥	ft		f€	ft²	K
(4) LGP2140X	В	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	1.0800	0.3580	0.01
(4) LGF2140X	ь	r toill Leg	0.00	0.0000	110.0000	1/2"	1.2137	0.3560	0.01
			0.00			Ice	1.3548	0.5563	0.03
(4) LGP2140X	С	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	1.0800	0.3580	0.01
(1) 201 21 10/	Ü	1 10111 209	0.00	0.0000	110.0000	1/2"	1.2137	0.4536	0.02
			0.00			lce 1" lce	1.3548	0.5563	0.03
DC6-48-60-18-8F	В	From Leg	4.0000	0.0000	118.0000	No Ice	0.9167	0.9167	0.02
200 10 00 10 01	_		0.00	0.000		1/2"	1.4583	1.4583	0.04
			0.00			Ice	1.6431	1.6431	0.06
(2) 7020.00	Α	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	0.1021	0.1750	0.00
(=) . 0=0.00	, ,		0.00	0.000		1/2"	0.1469	0.2393	0.01
			1.00			Ice	0.1991	0.3109	0.01
(2) 7020.00	В	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	0.1021	0.1750	0.00
(2) 7020.00		r rom Log	0.00	0.0000	110.0000	1/2"	0.1469	0.2393	0.01
			1.00			Ice	0.1991	0.3109	0.01
(2) 7020.00	С	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	0.1021	0.1750	0.00
(2) 7020.00	O	r rom Log	0.00	0.0000	110.0000	1/2"	0.1469	0.2393	0.01
			1.00			Ice	0.1991	0.3109	0.01
RRUS 4415 B25	Α	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	1.6444	0.6788	0.04
11100 4410 020	^	1 Tom Log	0.00	0.0000	110.0000	1/2"	1.8044	0.7911	0.06
			1.00			Ice	1.9719	0.9129	0.07
RRUS 4415 B25	В	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	1.6444	0.6788	0.04
11100 4410 B20		r rom Log	0.00	0.0000	110.0000	1/2"	1.8044	0.7911	0.06
			1.00			Ice	1.9719	0.9129	0.07
RRUS 4415 B25	С	From Leg	4.0000	0.0000	118.0000	1" Ice No Ice	1.6444	0.6788	0.04
1110 520	Ü	1 10111 209	0.00	0.0000	110.0000	1/2"	1.8044	0.7911	0.06
			1.00			Ice	1.9719	0.9129	0.07
Platform Mount [LP 303-1]	С	None		0.0000	118.0000	1" Ice No Ice	14.6600	14.6600	1.25
						1/2"	18.8700	18.8700	1.48
						lce 1" lce	23.0800	23.0800	1.71
******						1 100			
APXV18-206517S-C w/	Α	From Leg	1.0000	0.0000	102.0000	No Ice	5.4042	4.7000	0.05
Mount Pipe			0.00 0.00			1/2" Ice	5.9597 6.4808	5.8600 6.7338	0.10 0.15
			0.00			1" Ice	0.1000	0.7000	0.10
APXV18-206517S-C w/	В	From Leg	1.0000	0.0000	102.0000	No Ice	5.4042	4.7000	0.05
Mount Pipe			0.00 0.00			1/2" Ice	5.9597 6.4808	5.8600 6.7338	0.10 0.15
			0.00			1" Ice	0.4000	0.7550	0.15
APXV18-206517S-C w/	С	From Leg	1.0000	0.0000	102.0000	No Ice	5.4042	4.7000	0.05
Mount Pipe			0.00 0.00			1/2" Ice	5.9597 6.4808	5.8600 6.7338	0.10 0.15
			0.00			1" Ice	0.4000	0.7550	0.15
Pipe Mount [PM 601-3]	С	None		0.0000	102.0000	No Ice	4.3900	4.3900	0.20
						1/2" Ice	5.4800 6.5700	5.4800 6.5700	0.24 0.28
						1" Ice	0.5700	0.5700	0.20
*************	_		0.0000	0.0000	746000		0.4.0=	0.4.0=	0.01
KS24019-L112A	С	From Leg	3.0000 0.00	0.0000	74.0000	No Ice 1/2"	0.1407 0.1979	0.1407 0.1979	0.01 0.01
			1.00			Ice	0.1979	0.1979	0.01
Side Arm Mount [SO 702-	_			0.005	7/22==	1" Ice			
Sign Arm Mount (SO 702	С	None		0.0000	74.0000	No Ice	1.0000	1.4300	0.03

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement		C _A A _A Front	$C_A A_A$ Side	Weight
	J		Vert ft ft ft	0	ft		fℓ²	ft²	К
						1/2" Ice 1" Ice	1.0000	2.6700	0.05

Tower Pressures - No Ice

 $G_H = 1.100$

Section	Z	Kz	qz	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					а				%	_In	Out
				• • •	С	6.2	•0	6.0		Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 168.0000-	163.2500	1.403	29.52	11.083	Α	0.000	11.083	11.083	100.00	0.000	0.000
158.5000					В	0.000	11.083		100.00	0.000	0.000
					С	0.000	11.083		100.00	0.000	2.438
L2 158.5000-	158.2315	1.394	29.32	0.750	Α	0.000	0.750	0.750	100.00	0.000	0.000
158.0000					В	0.000	0.750		100.00	0.000	0.000
					С	0.000	0.750		100.00	0.000	0.163
L3 158.0000-	136.4479	1.351	28.40	89.692	Α	0.000	89.692	89.692	100.00	0.000	0.000
116.5000					В	0.000	89.692		100.00	0.000	0.000
					С	0.000	89.692		100.00	0.000	13.488
L4 116.5000-	97.9594	1.26	26.48	97.679	Α	0.000	97.679	97.679	100.00	0.000	0.000
80.2500					В	0.000	97.679		100.00	0.000	0.000
					С	0.000	97.679		100.00	0.000	15.852
L5 80.2500-	59.7435	1.136	23.80	130.00	Α	0.000	130.009	130.009	100.00	0.000	0.000
39.7500				9	В	0.000	130.009		100.00	0.000	0.000
					С	0.000	130.009		100.00	0.000	22.971
L6 39.7500-	20.0692	0.903	19.19	148.68	Α	0.000	148.685	148.685	100.00	0.000	0.000
0.0000	_			5	В	0.000	148.685		100.00	0.000	0.000
					С	0.000	148.685		100.00	0.000	25.207

Tower Pressure - With Ice

 $G_H = 1.100$

Section	Z	K₂	q_z	t_Z	A_{G}	F	A_F	A_R	A_{leg}	Leg	C_AA_A	C_AA_A
Elevation						а				%	In	Out
						С					Face	Face
ft	ft		psf	in	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 168.0000-	163.2500	1.403	5.46	2.3467	14.799	Α	0.000	14.799	14.799	100.00	0.000	0.000
158.5000						В	0.000	14.799		100.00	0.000	0.000
						С	0.000	14.799		100.00	0.000	9.478
L2 158.5000-	158.2315	1.394	5.42	2.3394	0.945	Α	0.000	0.945	0.945	100.00	0.000	0.000
158.0000						В	0.000	0.945		100.00	0.000	0.000
						С	0.000	0.945		100.00	0.000	0.630
L3 158.0000-	136.4479	1.351	5.25	2.3050	105.635	Α	0.000	105.635	105.635	100.00	0.000	0.000
116.5000						В	0.000	105.635		100.00	0.000	0.000
						С	0.000	105.635		100.00	0.000	51.751
L4 116.5000-	97.9594	1.26	4.90	2.2299	111.606	Α	0.000	111.606	111.606	100.00	0.000	0.000
80.2500						В	0.000	111.606		100.00	0.000	0.000
						С	0.000	111.606		100.00	0.000	54.396
L5 80.2500-	59.7435	1.136	4.40	2.1223	145.061	Α	0.000	145.061	145.061	100.00	0.000	0.000
39.7500						В	0.000	145.061		100.00	0.000	0.000
						С	0.000	145.061		100.00	0.000	74.952

Section	Z	K_Z	q_z	t_Z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation						а			_	%	In	Out
						С					Face	Face
ft	ft		psf	in	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L6 39.7500-	20.0692	0.903	3.55	1.9030	162.745	Α	0.000	162.745	162.745	100.00	0.000	0.000
0.0000						В	0.000	162.745		100.00	0.000	0.000
						С	0.000	162.745		100.00	0.000	77.699

Tower Pressure - Service

 $G_H = 1.100$

Section	Z	Kz	q_z	A_G	F	A_F	A_R	A_{leg}	Leg	$C_A A_A$	$C_A A_A$
Elevation					а				%	In	Out
					С					Face	Face
ft	ft		psf	ft ²	е	ft ²	ft ²	ft ²		ft ²	ft ²
L1 168.0000-	163.2500	1.403	10.99	11.083	Α	0.000	11.083	11.083	100.00	0.000	0.000
158.5000					В	0.000	11.083		100.00	0.000	0.000
					С	0.000	11.083		100.00	0.000	2.438
L2 158.5000-	158.2315	1.394	10.92	0.750	Α	0.000	0.750	0.750	100.00	0.000	0.000
158.0000					В	0.000	0.750		100.00	0.000	0.000
					С	0.000	0.750		100.00	0.000	0.163
L3 158.0000-	136.4479	1.351	10.58	89.692	Α	0.000	89.692	89.692	100.00	0.000	0.000
116.5000					В	0.000	89.692		100.00	0.000	0.000
					С	0.000	89.692		100.00	0.000	13.488
L4 116.5000-	97.9594	1.26	9.86	97.679	Α	0.000	97.679	97.679	100.00	0.000	0.000
80.2500					В	0.000	97.679		100.00	0.000	0.000
					С	0.000	97.679		100.00	0.000	15.852
L5 80.2500-	59.7435	1.136	8.86	130.00	Α	0.000	130.009	130.009	100.00	0.000	0.000
39.7500				9	В	0.000	130.009		100.00	0.000	0.000
					С	0.000	130.009		100.00	0.000	22.971
L6 39.7500-	20.0692	0.903	7.15	148.68	Α	0.000	148.685	148.685	100.00	0.000	0.000
0.0000				5	В	0.000	148.685		100.00	0.000	0.000
					С	0.000	148.685		100.00	0.000	25.207

Load Combinations

Comb.	Description
No.	·
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
tovTow	or Papart - vargion 8.0.2.1

Comb.	Description
No.	·
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 lce+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 lce+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 lce+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n	ft	Type		Load		Moment	Moment
No.				Comb.	K	kip-ft	kip-ft
L1	168 - 158.5	Pole	Max Tension	8	0.00	0.00	0.00
			Max. Compression	26	-3.52	0.72	-0.42
			Max. Mx	20	-0.76	10.90	-0.05
			Max. My	14	-0.77	0.08	-10.86
			Max. Vy	20	-1.52	10.90	-0.05
			Max. Vx	14	1.52	0.08	-10.86
			Max. Torque	13			-0.07
L2	158.5 - 158	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-3.66	0.78	-0.46
			Max. Mx	20	-0.80	11.68	-0.06
			Max. My	14	-0.80	0.10	-11.64
			Max. Vy	20	-1.57	11.68	-0.06
			Max. Vx	14	1.56	0.10	-11.64
			Max. Torque	13			-0.08
L3	158 - 116.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-35.00	14.24	-10.12
			Max. Mx	20	-8.20	448.96	-6.54
			Max. My	14	-8.24	6.78	-441.88
			Max. Vý	20	-15.06	448.96	-6.54
			Max. Vx	14	14.87	6.78	-441.88
			Max. Torque	23			1.56
L4	116.5 -	Pole	Max Tension	1	0.00	0.00	0.00
	80.25		Max. Compression	26	-62.42	29.71	-18.26
			Max. Mx	20	-02.42 -16.74	1203.78	-10.20
				20 14	-16.74 -16.77	13.09	-12.34 -1191.46
			Max. My				
			Max. Vy	20	-23.77	1203.78	-12.34
			Max. Vx	14	23.64	13.09	-1191.46
	00.05	Б.	Max. Torque	25	0.00	0.00	1.90
L5	80.25 - 39.75	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-85.83	49.83	-29.99
			Max. Mx	20	-26.22	2242.24	-18.95
			Max. My	14	-26.24	20.40	-2224.14
			Max. Vy	20	-28.26	2242.24	-18.95
			Max. Vx	14	28.13	20.40	-2224.14
			Max. Torque	25			3.36
			•				

Sectio n	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
No.				Comb.	K	kip-ft	kip-ft
L6	39.75 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-114.69	70.87	-42.18
			Max. Mx	20	-40.33	3610.08	-26.24
			Max. My	14	-40.33	28.56	-3585.63
			Max. Vy	20	-32.12	3610.08	-26.24
			Max. Vx	14	32.01	28.56	-3585.63
			Max. Torque	25			5.12

Maximum Reactions

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, 2
		Load	K	K	K
		Comb.			
Pole	Max. Vert	26	114.69	-0.00	0.00
	Max. H _x	20	40.37	32.08	-0.13
	Max. H _z	2	40.37	-0.13	31.96
	Max. M _x	2	3576.71	-0.13	31.96
	Max. M _z	8	3595.92	-32.07	0.13
	Max. Torsion	25	5.12	15.93	27.61
	Min. Vert	9	30.28	-32.07	0.13
	Min. H _x	9	30.28	-32.07	0.13
	Min. H _z	15	30.28	0.13	-31.96
	Min. M _x	14	-3585.63	0.13	-31.96
	$Min. M_z$	20	-3610.08	32.08	-0.13
	Min. Torsion	13	-5.12	-15.93	-27.61

Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	33.64	0.00	-0.00	3.58	5.48	0.00
1.2 Dead+1.6 Wind 0 deg -	40.37	0.13	-31.96	-3576.71	-15.11	-4.58
No Ice						
0.9 Dead+1.6 Wind 0 deg -	30.28	0.13	-31.96	-3519.65	-16.46	-4.60
No Ice						
1.2 Dead+1.6 Wind 30 deg -	40.37	16.15	-27.74	-3107.92	-1813.99	-2.85
No Ice						
0.9 Dead+1.6 Wind 30 deg -	30.28	16.15	-27.74	-3058.46	-1786.06	-2.85
No Ice						
1.2 Dead+1.6 Wind 60 deg -	40.37	27.84	-16.09	-1805.03	-3124.88	-0.35
No Ice						
0.9 Dead+1.6 Wind 60 deg -	30.28	27.84	-16.09	-1776.73	-3075.64	-0.34
No Ice						
1.2 Dead+1.6 Wind 90 deg -	40.37	32.07	-0.13	-17.42	-3595.92	2.23
No Ice						
0.9 Dead+1.6 Wind 90 deg -	30.28	32.07	-0.13	-18.17	-3539.38	2.25
No Ice						
1.2 Dead+1.6 Wind 120 deg	40.37	27.71	15.87	1776.23	-3103.39	4.22
- No Ice						
0.9 Dead+1.6 Wind 120 deg	30.28	27.71	15.87	1746.31	-3054.55	4.25
- No Ice						
1.2 Dead+1.6 Wind 150 deg	40.37	15.93	27.61	3095.23	-1776.36	5.09
- No Ice						
0.9 Dead+1.6 Wind 150 deg	30.28	15.93	27.61	3043.84	-1749.15	5.12
- No Ice						
1.2 Dead+1.6 Wind 180 deg	40.37	-0.13	31.96	3585.63	28.56	4.60
- No Ice						
0.9 Dead+1.6 Wind 180 deg	30.28	-0.13	31.96	3526.33	26.36	4.62
- No Ice						

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
4.0 Dec. de 4.0 Wheel 040 de se	K 40.07	K 10.15	K 07.74	kip-ft	kip-ft	kip-ft
1.2 Dead+1.6 Wind 210 deg - No Ice	40.37	-16.15	27.74	3116.69	1827.40	2.86
0.9 Dead+1.6 Wind 210 deg	30.28	-16.15	27.74	3064.91	1795.93	2.87
- No Ice						
1.2 Dead+1.6 Wind 240 deg - No Ice	40.37	-27.84	16.09	1813.82	3138.29	0.36
0.9 Dead+1.6 Wind 240 deg	30.28	-27.84	16.09	1783.20	3085.51	0.35
- No Ice 1.2 Dead+1.6 Wind 270 deg	40.37	-32.08	0.13	26.24	3610.08	-2.24
- No Ice 0.9 Dead+1.6 Wind 270 deg	30.28	-32.08	0.13	24.65	3549.64	-2.27
- No Ice						
1.2 Dead+1.6 Wind 300 deg - No Ice	40.37	-27.71	-15.87	-1767.41	3116.84	-4.24
0.9 Dead+1.6 Wind 300 deg	30.28	-27.71	-15.87	-1739.84	3064.45	-4.27
- No Ice 1.2 Dead+1.6 Wind 330 deg	40.37	-15.93	-27.61	-3086.43	1789.82	-5.10
- No Ice 0.9 Dead+1.6 Wind 330 deg	30.28	-15.93	-27.61	-3037.38	1759.06	-5.12
- No Ice						
1.2 Dead+1.0 Ice+1.0 Temp	114.69	0.00	-0.00	42.18	70.87	0.00
1.2 Dead+1.0 Wind 0	114.69	0.02	-7.30	-913.48	67.39	-1.66
deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 30	114.69	3.67	-6.33	-787.19	-412.39	-0.99
deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 60	114.69	6.35	-3.66	-438.67	-762.69	-0.06
deg+1.0 Ice+1.0 Temp		5.55				
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	114.69	7.32	-0.02	38.70	-889.63	0.89
1.2 Dead+1.0 Wind 120	114.69	6.33	3.63	516.99	-759.20	1.61
deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 150	114.69	3.65	6.31	868.04	-406.36	1.89
deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 180	114.69	-0.02	7.30	997.77	74.33	1.67
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	114.69	-3.67	6.33	871.58	554.14	1.00
1.2 Dead+1.0 Wind 240	114.69	-6.35	3.66	522.97	904.33	0.06
deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 270	114.69	-7.32	0.02	45.65	1031.27	-0.89
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	114.69	-6.33	-3.63	-432.62	900.89	-1.60
1.2 Dead+1.0 Wind 330	114.69	-3.65	-6.31	-783.69	548.09	-1.89
deg+1.0 Ice+1.0 Temp Dead+Wind 0 deg - Service	33.64	0.03	-7.44	-823.93	0.57	-1.09
Dead+Wind 30 deg - Service	33.64	3.76	-6.46	-715.63	-415.17	-0.68
Dead+Wind 60 deg - Service	33.64	6.48	-3.75	-414.53	-718.17	-0.08
Dead+Wind 90 deg - Service	33.64	7.46	-0.03	-1.36	-827.16	0.53
Dead+Wind 120 deg -	33.64	6.45	3.69	413.15	-713.13	1.01
Service Dead+Wind 150 deg -	33.64	3.71	6.43	717.88	-406.41	1.21
Service						
Dead+Wind 180 deg - Service	33.64	-0.03	7.44	831.28	10.66	1.09
Dead+Wind 210 deg - Service	33.64	-3.76	6.46	722.98	426.41	0.68
Dead+Wind 240 deg -	33.64	-6.48	3.75	421.88	729.40	0.08
Service Dead+Wind 270 deg -	33.64	-7.46	0.03	8.72	838.39	-0.53
Service Dead+Wind 300 deg -	33.64	-6.45	-3.69	-405.76	724.30	-1.01
Service						
Dead+Wind 330 deg - Service	33.64	-3.71	-6.43	-710.59	417.68	-1.21

Solution Summary

	Sur	n of Applied Force	25		Sum of Reaction	ns	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	ĸ	ĸ	K	K	ĸ	70 =
1	0.00	-33.64	0.00	-0.00	33.64	0.00	0.002%
2	0.13	-40.37	-31.96	-0.13	40.37	31.96	0.005%
3	0.13	-30.28	-31.96	-0.13	30.28	31.96	0.006%
4	16.15	-40.37	-27.74	-16.15	40.37	27.74	0.000%
5	16.15	-30.28	-27.74	-16.15	30.28	27.74	0.000%
6	27.84	-40.37	-16.09	-27.84	40.37	16.09	0.000%
7	27.84	-30.28	-16.09	-27.84	30.28	16.09	0.000%
8	32.08	-40.37	-0.13	-32.07	40.37	0.13	0.013%
9	32.08	-30.28	-0.13	-32.07	30.28	0.13	0.010%
10	27.71	-40.37	15.87	-27.71	40.37	-15.87	0.000%
11	27.71	-30.28	15.87	-27.71	30.28	-15.87	0.000%
12	15.93	-40.37	27.61	-15.93	40.37	-27.61	0.000%
13	15.93	-30.28	27.61	-15.93	30.28	-27.61	0.000%
14	-0.13	-40.37	31.96	0.13	40.37	-31.96	0.003%
15	-0.13	-30.28	31.96	0.13	30.28	-31.96	0.002%
16	-16.15	-40.37	27.74	16.15	40.37	-27.74	0.000%
17	-16.15	-30.28	27.74	16.15	30.28	-27.74	0.000%
18	-27.84	-40.37	16.09	27.84	40.37	-16.09	0.000%
19	-27.84	-30.28	16.09	27.84	30.28	-16.09	0.000%
20	-32.08	-40.37	0.13	32.08	40.37	-0.13	0.003%
21	-32.08	-30.28	0.13	32.08	30.28	-0.13	0.004%
22	-27.71	-40.37	-15.87	27.71	40.37	15.87	0.000%
23	-27.71	-30.28	-15.87	27.71	30.28	15.87	0.000%
24	-15.93	-40.37	-27.61	15.93	40.37	27.61	0.000%
25	-15.93	-30.28	-27.61	15.93	30.28	27.61	0.000%
26	0.00	-114.69	0.00	-0.00	114.69	0.00	0.000%
27	0.02	-114.69	-7.30	-0.02	114.69	7.30	0.001%
28	3.68	-114.69	-6.33	-3.67	114.69	6.33	0.001%
29	6.35	-114.69	-3.66	-6.35	114.69	3.66	0.001%
30	7.32	-114.69	-0.02	-7.32	114.69	0.02	0.001%
31	6.33	-114.69	3.64	-6.33	114.69	-3.63	0.001%
32	3.65	-114.69	6.31	-3.65	114.69	-6.31	0.002%
33	-0.02	-114.69	7.30	0.02	114.69	-7.30	0.002%
34	-3.68	-114.69	6.33	3.67	114.69	-6.33	0.001%
35	-6.35	-114.69	3.66	6.35	114.69	-3.66	0.002%
36	-7.32	-114.69	0.02	7.32	114.69	-0.02	0.002%
37	-6.33	-114.69	-3.64	6.33	114.69	3.63	0.002%
38	-3.65	-114.69	-6.31	3.65	114.69	6.31	0.002%
39	0.03	-33.64	-7.44	-0.03	33.64	7.44	0.004%
40	3.76	-33.64	-6.46	-3.76	33.64	6.46	0.002%
41	6.48	-33.64	-3.75	-6.48	33.64	3.75	0.002%
42	7.47	-33.64	-0.03	-7.46	33.64	0.03	0.002 %
43	6.45	-33.64	3.69	-6.45	33.64	-3.69	0.002%
44	3.71	-33.64	6.43	-3.71	33.64	-6.43	0.002%
45	-0.03	-33.64	7.44	0.03	33.64	-7.44	0.004%
46	-3.76	-33.64	6.46	3.76	33.64	-6.46	0.002%
47	-6.48	-33.64	3.75	6.48	33.64	-3.75	0.002%
48	-7.47	-33.64	0.03	7.46	33.64	-0.03	0.004%
49	-7.47 -6.45	-33.64	-3.69	6.45	33.64	3.69	0.004%
50	-3.71	-33.64	-6.43	3.71	33.64	6.43	0.004%
	-0.11	-00.04	-0.43	J./ I	JJ.U4	0.40	0.002 /0

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination	_	of Cycles	Tolerance	Tolerance
1	Yes	11	0.0000001	0.00001461
2	Yes	22	0.00004343	0.00009905
3	Yes	21	0.00004545	0.00011853
4	Yes	29	0.0000001	0.00011810
5	Yes	28	0.0000001	0.00012589
6	Yes	29	0.00000001	0.00011978
7	Yes	28	0.00000001	0.00012769
8	Yes	20	0.00011419	0.00013952
9	Yes	20	0.00077445	0.00010818
10	Yes	29	0.000007440	0.000110110
11	Yes	28	0.00000001	0.00011302
12	Yes	29	0.0000001	0.00012741
13	Yes	28	0.0000001	0.00011328
14	Yes	23	0.0000001	0.00012037
15	Yes	23	0.00002634	0.00014143
16	Yes	29 29	0.00001660	0.00010022
17		28		
18	Yes	26 29	0.00000001	0.00013061
	Yes	-	0.00000001	0.00012205
19	Yes	28	0.0000001	0.00012962
20	Yes	23	0.00002645	0.00010885
21	Yes	22	0.00002741	0.00012606
22	Yes	29	0.00000001	0.00011420
23	Yes	28	0.0000001	0.00012145
24	Yes	29	0.0000001	0.00011941
25	Yes	28	0.0000001	0.00012749
26	Yes	24	0.0000001	0.00000625
27	Yes	26	0.00014590	0.00003979
28	Yes	26	0.00014562	0.00008289
29	Yes	26	0.00014561	0.00008728
30	Yes	26	0.00014597	0.00003201
31	Yes	26	0.00014539	0.00011190
32	Yes	26	0.00014543	0.00009457
33	Yes	26	0.00014565	0.00004746
34	Yes	27	0.00010036	0.00010709
35	Yes	26	0.00014493	0.00014902
36	Yes	26	0.00014556	0.00004002
37	Yes	26	0.00014527	0.00010898
38	Yes	26	0.00014523	0.00012581
39	Yes	20	0.00009901	0.00004323
40	Yes	21	0.00006091	0.00009790
41	Yes	21	0.00006091	0.00010270
42	Yes	20	0.00009902	0.00003778
43	Yes	21	0.00006091	0.00011195
44	Yes	20	0.00009871	0.00014490
45	Yes	20	0.00009901	0.00004767
46	Yes	21	0.00006089	0.00011626
47	Yes	21	0.00006089	0.00011231
48	Yes	20	0.00009901	0.000011201
49	Yes	20	0.00009901	0.00004140
50	Yes	21	0.00009071	0.00014831

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	168 - 158.5	46.372	47	2.3350	0.0071
L2	158.5 - 158	41.735	47	2.3234	0.0069
L3	158 - 116.5	41.492	47	2.3230	0.0069
L4	120.25 - 80.25	24.187	47	1.9453	0.0040
L5	84.75 - 39.75	11.754	47	1.3402	0.0026
L6	45 - 0	3.255	47	0.6631	0.0013

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
170.0000	Lightning Rod 5/8x4'	47	46.372	2.3350	0.0071	44262
166.0000	APX16PV-16PVL-E	47	45.394	2.3321	0.0070	44262
157.0000	APXVTM14-C-120 w/ Mount Pipe	47	41.006	2.3218	0.0069	20443
155.0000	800 EXTERNAL NOTCH FILTER	47	40.036	2.3175	0.0069	16634
145.0000	(2) LPA-80080/6CF w/ Mount Pipe	47	35.241	2.2608	0.0063	7989
120.0000	RRUS 11	47	24.084	1.9413	0.0040	3536
118.0000	7770.00 w/ Mount Pipe	47	23.269	1.9097	0.0038	3486
102.0000	APXV18-206517S-C w/ Mount Pipe	47	17.246	1.6428	0.0031	3445
74.0000	KS24019-L112A	47	8.863	1.1512	0.0023	3247

Maximum Tower Deflections - Design Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	168 - 158.5	198.184	18	10.0007	0.0304
L2	158.5 - 158	178.488	18	9.9519	0.0300
L3	158 - 116.5	177.455	18	9.9503	0.0299
L4	120.25 - 80.25	103.748	18	8.3610	0.0169
L5	84.75 - 39.75	50.516	18	5.7675	0.0110
L6	45 - 0	14.005	18	2.8544	0.0054

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
170.0000	Lightning Rod 5/8x4'	18	198.184	10.0007	0.0304	11088
166.0000	APX16PV-16PVL-E	18	194.031	9.9885	0.0303	11088
157.0000	APXVTM14-C-120 w/ Mount	18	175.391	9.9453	0.0299	5515
	Pipe					
155.0000	800 EXTERNAL NOTCH FILTER	18	171.268	9.9273	0.0297	4482
145.0000	(2) LPA-80080/6CF w/ Mount	18	150.874	9.6902	0.0272	2041
	Pipe					
120.0000	RRUS 11	18	103.308	8.3443	0.0169	868
118.0000	7770.00 w/ Mount Pipe	18	99.825	8.2097	0.0162	855
102.0000	APXV18-206517S-C w/ Mount	18	74.062	7.0687	0.0129	833
	Pipe					
74.0000	KS24019-L112A	18	38.107	4.9542	0.0097	768

Compression Checks

Pole Design Data

Section No.	Elevation	Size	L	Lu	KI/r	Α	P_u	ϕP_n	Ratio Pu
	ft		ft	ft		in²	K	K	$\overline{\phi P_n}$
L1	168 - 158.5 (1)	TP14x14x0.25	9.5000	0.0000	0.0	10.799 2	-0.76	340.18	0.002
L2	158.5 - 158 (2)	TP22x14x0.25	0.5000	0.0000	0.0	10.799 2	-0.76	340.18	0.002
L3	158 - 116.5 (3)	TP29.139x22x0.1875	41.500 0	0.0000	0.0	16.845 9	-8.18	1091.80	0.007
L4	116.5 - 80.25 (4)	TP35x28.1189x0.25	40.000 0	0.0000	0.0	26.959 9	-16.72	1822.96	0.009
L5	80.25 - 39.75 (5)	TP41.467x33.7259x0.312	45.000 0	0.0000	0.0	39.924 3	-26.21	2752.39	0.010
L6	39.75 - 0 (6)	TP47.68x39.9389x0.375	45.000 0	0.0000	0.0	56.304 8	-40.33	3909.54	0.010

	Pole Bending Design Data									
Section No.	Elevation	Size	M _{ux}	ф <i>М</i> _{пх}	Ratio M _{ux}	M _{uy}	φM _{ny}	Ratio M _{uy}		
	ft		kip-ft	kip-ft	ϕM_{nx}	kip-ft	kip-ft	ϕM_{ny}		
L1	168 - 158.5 (1)	TP14x14x0.25	10.92	124.09	0.088	0.00	124.09	0.000		
L2	158.5 - 158 (2)	TP22x14x0.25	10.91	124.09	0.088	0.00	124.09	0.000		
L3	158 - 116.5 (3)	TP29.139x22x0.1875	452.08	636.29	0.710	0.00	636.29	0.000		
L4	116.5 - 80.25 (4)	TP35x28.1189x0.25	1210.25	1274.26	0.950	0.00	1274.26	0.000		
L5	80.25 - 39.75 (5)	TP41.467x33.7259x0.312 5	2252.61	2278.38	0.989	0.00	2278.38	0.000		
L6	39.75 - 0 (6)	TP47.68x39.9389x0.375	3624.75	3802.74	0.953	0.00	3802.74	0.000		

Section No.	Elevation	Size	Actual V _u	ϕV_n	Ratio V _u	Actual T _u	ϕT_n	Ratio T _u
	ft		K	K	ϕV_n	kip-ft	kip-ft	ϕT_n
L1	168 - 158.5 (1)	TP14x14x0.25	1.53	170.09	0.009	0.00	191.47	0.000
L2	158.5 - 158 (2)	TP22x14x0.25	1.61	269.05	0.006	0.00	191.47	0.000
L3	158 - 116.5 (3)	TP29.139x22x0.1875	15.14	545.90	0.028	0.40	1275.41	0.000
L4	116.5 - 80.25 (4)	TP35x28.1189x0.25	23.87	911.48	0.026	0.36	2554.47	0.000
L5	80.25 - 39.75 (5)	TP41.467x33.7259x0.312 5	28.35	1376.20	0.021	0.36	4567.67	0.000
L6	39.75 - 0 (6)	TP47.68x39.9389x0.375	32.21	1954.77	0.016	0.36	7623.88	0.000

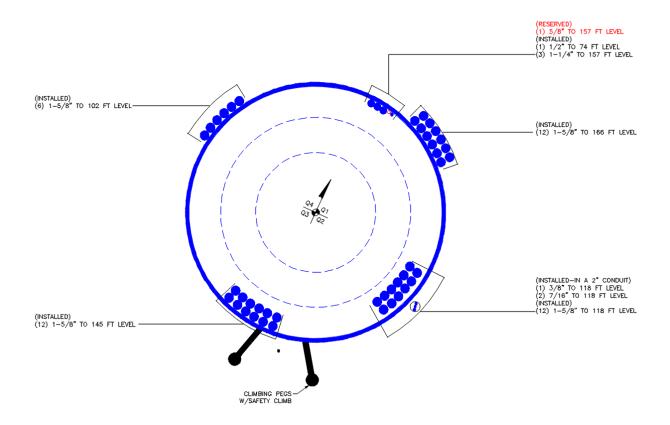
			Pol	e Inter	action	Desig	n Data			
Section No.	Elevation	Ratio P _u	Ratio M _{ux}	Ratio M _{uv}	Ratio V,,	Ratio T,,	Comb. Stress	Allow. Stress	Criteria	-
	ft	ϕP_n	φ <i>M</i> _{nx}	ϕM_{ny}	φ V _n	φ <i>T</i> _n	Ratio	Ratio		
L1	168 - 158.5 (1)	0.002	0.088	0.000	0.009	0.000	0.090	1.000	4.8.2	-

Section No.	Elevation	Ratio P _u	Ratio M _{ux}	Ratio M _{uy}	Ratio V _u	Ratio T _u	Comb. Stress	Allow. Stress	Criteria
	ft	ϕP_n	φ <i>M</i> _{nx}	ϕM_{ny}	$\overline{\phi V_n}$	ϕT_n	Ratio	Ratio	
L2	158.5 - 158 (2)	0.002	0.088	0.000	0.006	0.000	0.090	1.000	4.8.2
L3	158 - 116.5 (3)	0.007	0.710	0.000	0.028	0.000	0.719	1.000	4.8.2
L4	116.5 - 80.25 (4)	0.009	0.950	0.000	0.026	0.000	0.960	1.000	4.8.2
L5	80.25 - 39.75 (5)	0.010	0.989	0.000	0.021	0.000	0.999	1.000	4.8.2
L6	39.75 - 0 (6)	0.010	0.953	0.000	0.016	0.000	0.964	1.000	4.8.2

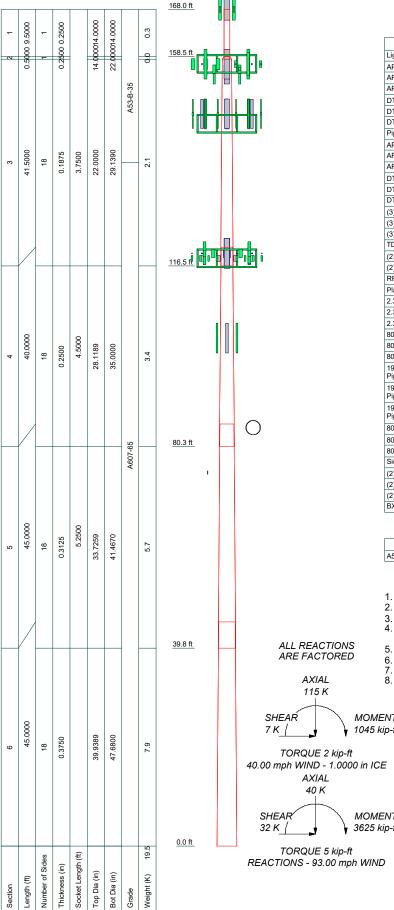
Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	øP _{allow} K	% Capacity	Pass Fail
L1	168 - 158.5	Pole	TP14x14x0.25	1	-0.76	340.18	9.0	Pass
L2	158.5 - 158	Pole	TP22x14x0.25	2	-0.76	340.18	9.0	Pass
L3	158 - 116.5	Pole	TP29.139x22x0.1875	3	-8.18	1091.80	71.9	Pass
L4	116.5 - 80.25	Pole	TP35x28.1189x0.25	4	-16.72	1822.96	96.0	Pass
L5	80.25 - 39.75	Pole	TP41.467x33.7259x0.3125	5	-26.21	2752.39	99.9	Pass
L6	39.75 - 0	Pole	TP47.68x39.9389x0.375	6	-40.33	3909.54	96.4	Pass
							Summary	
						Pole (L5)	99.9	Pass
						RATING =	99.9	Pass

APPENDIX B BASE LEVEL DRAWING



APPENDIX C ADDITIONAL CALCULATIONS



DESIGNED APPURTENANCE LOADING

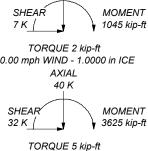
TYPE	ELEVATION	TYPE	ELEVATION
Lightning Rod 5/8x4'	170	BXA-70063-6CF-2 w/ Mount Pipe	145
APX16PV-16PVL-E	166	BXA-70063-6CF-2 w/ Mount Pipe	145
APX16PV-16PVL-E	166	BXA-171085-12BF-2 w/ Mount Pipe	145
APX16PV-16PVL-E	166	BXA-171085-12BF-2 w/ Mount Pipe	145
DTMA-1819-DD-12	166	BXA-171085-12BF-2 w/ Mount Pipe	145
DTMA-1819-DD-12	166	(2) FD9R6004/2C-3L	145
DTMA-1819-DD-12	166	(2) FD9R6004/2C-3L	145
Pipe Mount [PM 601-3]	166	(2) FD9R6004/2C-3L	145
APXVTM14-C-120 w/ Mount Pipe	157	Platform Mount [LP 403-1]	145
APXVTM14-C-120 w/ Mount Pipe	157	RRUS 11	120
APXVTM14-C-120 w/ Mount Pipe	157	RRUS 11	120
DT465B-2XR w/ Mount Pipe	157	RRUS 11	120
DT465B-2XR w/ Mount Pipe	157	Side Arm Mount [SO 102-3]	120
DT465B-2XR w/ Mount Pipe	157	7770.00 w/ Mount Pipe	118
(3) ACU-A20-N	157	7770.00 w/ Mount Pipe	118
(3) ACU-A20-N	157	7770.00 w/ Mount Pipe	118
(3) ACU-A20-N	157	AM-X-CD-16-65-00T-RET w/ Mount	118
TD-RRH8X20-25	157	Pipe	
(2) TD-RRH8X20-25	157	AM-X-CD-14-65-00T-RET w/ Mount	118
(2) RRH2X50-800	157	Pipe	
RRH2X50-800	157	800 10764 w/ Mount Pipe	118
Platform Mount [LP 712-1]	157	HPA-65R-BUU-H6 w/ Mount Pipe	118
2.375" OD x 4' Mount Pipe	157	SBNHH-1D65A w/ Mount Pipe	118
2.375" OD x 4' Mount Pipe	157	SBNHH-1D65A w/ Mount Pipe	118
2.375" OD x 4' Mount Pipe	157	(4) LGP2140X	118
800 EXTERNAL NOTCH FILTER	155	(4) LGP2140X	118
800 EXTERNAL NOTCH FILTER	155	(4) LGP2140X	118
800 EXTERNAL NOTCH FILTER	155	DC6-48-60-18-8F	118
1900MHz RRH (65MHz) w/ Mount	155	(2) 7020.00	118
Pipe		(2) 7020.00	118
1900MHz RRH (65MHz) w/ Mount	155	(2) 7020.00	118
Pipe		RRUS 4415 B25	118
1900MHz RRH (65MHz) w/ Mount	155	RRUS 4415 B25	118
Pipe		RRUS 4415 B25	118
800MHZ RRH	155	Platform Mount [LP 303-1]	118
800MHZ RRH	155	APXV18-206517S-C w/ Mount Pipe	102
800MHZ RRH	155	APXV18-206517S-C w/ Mount Pipe	102
Side Arm Mount [SO 102-3]	155	APXV18-206517S-C w/ Mount Pipe	102
(2) LPA-80080/6CF w/ Mount Pipe	145	Pipe Mount [PM 601-3]	102
(2) LPA-80080/6CF w/ Mount Pipe	145	KS24019-L112A	74
(2) LPA-80080/6CF w/ Mount Pipe BXA-70063-6CF-2 w/ Mount Pipe	145	Side Arm Mount [SO 702-1]	74

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A53-B-35	35 ksi	60 ksi	A607-65	65 ksi	80 ksi

TOWER DESIGN NOTES

- 1. Tower is located in Litchfield County, Connecticut.
- 2. Tower designed for Exposure C to the TIA-222-G Standard.
- Tower designed for a 93.00 mph basic wind in accordance with the TIA-222-G Standard. Tower is also designed for a 40.00 mph basic wind with 1.00 in ice. Ice is considered to
- increase in thickness with height.
- 5. Deflections are based upon a 60.00 mph wind.
- 6. Tower Structure Class II.7. Topographic Category 1 with Crest Height of 0.0000 ft8. TOWER RATING: 99.9%





^{Job:} 168 ft Monopole / N	ew Hartford / Executiv	ve Greet
Project: PJF# 37518-1341.004.	7805 / BU# 876392	
Client: CCI	Drawn by: jacuna	App'd:
Code: TIA-222-G	Date: 08/14/18	Scale: NTS
Path: G:TOWER:375 Crown Castle:2018:37518-1341 876392 New H	artford - Executiv/37518-1341.004.7805 SA 1613794\37518-1341.004.780	Dwg No. E-1

PAUL J. FORD & COMPANY 250 E Broad St, Ste 600 • Columbus, OH 43215

Phone 614.221.6679 www.pauljford.com

v4.4 - Effective 7-12-13

Date: 8/14/2018

PJF Project: 37518-1341.004.7805

Client Ref. # BU 876392

Site Name: New Hartford / Executive Greet

Description: 158-ft Pole w/ 10-ft Ext

Owner: Crown Castle Engineer: JAB

Asymmetric Bolt Analysis

Moment = 10.92 k-ft Axial = 0.76 kips 1.53 Shear = kips Anchor Qty = 18

TIA Ref. G ASIF = N/A Max Ratio = 100.0% Location = η=

Flange Plate

N/A for BP, Rev. G Sect. 4.9.9

N-Included for FP, Rev. G Threads =

** For Flange Plates: Prying action is not considered in the bolt loads. **

Item	Nominal Bolt Dia, in	Spec	Fy, ksi	Fu, ksi	Location, degrees	Bolt Circle,	Area Override, in ²	Area, in ²	Max Net Compressi on, kips	Max Net Tension, kips	Load for Capacity Calc, kips	Capacity Override, kips	Capacity, kips	Capacity Ratio
1					0.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
2					20.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
3	0.750	A325	92	120	40.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
4	0.750	A325	92	120	60.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
5	0.750	A325	92	120	80.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
6					100.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
7					120.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
8					140.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
9	0.750	A325	92	120	160.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
10	0.750	A325	92	120	180.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
11	0.750	A325	92	120	200.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
12					220.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
13					240.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
14					260.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
15	0.750	A325	92	120	280.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
16	0.750	A325	92	120	300.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
17	0.750	A325	92	120	320.0	19.00	0.00	0.44	3.15	2.98	2.98	0.00	30.06	9.9%
18					340.0	19.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0%
			-			-		3.98						

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 876392 Site Name: New Hartford / Executive

App #:

Bolt quanitity
djust to account
for extension
mouse hole

120

92

Reactions								
Mu	21.52009	ft-kips						
Axial, Pu:	0.8	kips						
Shear, Vu:	1.5	kips						
Elevation:	158	feet						

TIA G

Bolt Threads:
X-Excluded
φVn=φ(0.55*Ab*Fu)
φ=0.75, φ*Vn (kips):
21.87

Non-Rigid

φ*Tn

30.06 kips $\varphi Tn[(1-(Vu/\varphi Vn)^2]^0.5]$

<-Only Applcable to Unstiffened Cases

30.06 kips

2.98 Kips

1.205 in

0.293 in

0.379 in

Pole Manufacturer:	Other
--------------------	-------

Bolt Data		
Qty:	18	
Diameter (in.):	0.75	Bolt Fu:
Bolt Material:	A325	Bolt Fy:
N/A:		< Disregard
N/A:		< Disregard
Circle (in.):	19	

Plate Data		
Diam:	24	in
Thick, t:	1.25	in
Grade (Fy):	65	ksi
Strength, Fu:	80	ksi
Single-Rod B-eff:	2.44	in

Stiffener Data (Welding at Both Sides)			
Config:	0	*	
Weld Type:			
Groove Depth:		in **	
Groove Angle:		degrees	
Fillet H. Weld:		< Disregard	
Fillet V. Weld:		in	
Width:		in	
Height:		in	
Thick:		in	
Notch:		in	
Grade:		ksi	
Weld str.:		ksi	

Pole Data			
Diam:	14	in	
Thick:	0.25	in	
Grade:	35	ksi	
# of Sides:	0	"0" IF Round	
Fu	58	ksi	
Reinf. Fillet Weld	0	"0" if None	

If No stiffeners, Criteria:	
Flange Bolt Results	s

Bolt Tension Capacity, φ*Tn,**B1**:
Adjusted φ*Tn (due to Vu=Vu/Qty), **B**:

Max Bolt <u>directly</u> applied Tu:

<u>Min. PL "tc" for **B** cap. **w/o** Pry:

Min PL "treq" for actual **T w/ Pry**:

<u>Min PL "t1" for actual **T w/o Pry**:</u></u>

T allowable w/o Prying: 30.06 kips α '<0 case

Prying Force, q: 0.00 kips
Total Bolt Tension=Tu+q: 2.98 kips
Non-Prying Bolt Stress Ratio, Tu/B: 9.9% Pass

Exterior Flange Plate Results Flexural Check
Compression Side Plate Stress: 4.1 ksi
Allowable Plate Stress: 58.5 ksi

Compression Plate Stress Ratio: 7.1% Pass
No Prying

Tension Side Stress Ratio, (treq/t)^2: 5.5% Pass

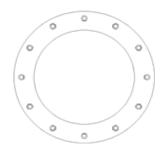
<u>n/a</u>

Stiffener Results

Horizontal Weld: n/a
Vertical Weld: n/a
Plate Flex+Shear, fb/Fb+(fv/Fv)^2: n/a
Plate Tension+Shear, ft/Ft+(fv/Fv)^2: n/a
Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check:





n/a

^{* 0 =} none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

^{**} Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

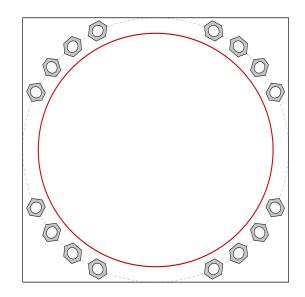
Monopole Base Plate Connection



Site Info		
	BU#	876392
	Site Name	/ Haftford / Executive G
	Order#	

Analysis Considerations		
TIA-222 Revision	G	
l _{ar} (in)	0	
Eta Factor, η	0.5	

Applied Loads		
Moment (kip-ft)	3624.75	
Axial Force (kips)	40.33	
Shear Force (kips)	32.21	



Connection Properties	Analysis Results		
Anchor Rod Data	Anchor Rod Summary		(units of kips, kip-ft)
(16) 2-1/4" ø bolts (A615-75; Fy=75 ksi, Fu=100 ksi) on 54" BC	Pu = 203.75	φPn = 260	Stress Rating
pos. (deg): 25.9, 38.6, 51.4, 64.1, 115.9, 128.6, 141.4, 154.1, 205.9, 2.	Vu = 2.01	φVn = n/a	79.9%
	Mu = n/a	φMn = n/a	Pass
Base Plate Data			
54" OD x 2.5" Plate (A572-55; Fy=55 ksi, Fu=70 ksi)	Base Plate Summary		
	Max Stress (ksi):	41.38	
Stiffener Data	Allowable Stress (ksi):	49.5	
N/A	Stress Ratio:	83.6%	Pass

Pole Data

47.68" x 0.375" 18-sided pole (A607-65; Fy=65 ksi, Fu=80 ksi)

CCIplate - version 3.0.1 Analysis Date: 8/14/2018

Pier and Pad Foundation

BU # : 76392
Site Name: New Hartford / Exe
App. Number:



TIA-222 Revision: G
Tower Type: Monopole

Block Foundation?:	

Superstructure Analysis Reactions		
Compression, P _{comp} :	40	kips
Base Shear, Vu_comp:	32	kips
Moment, M _u :	3625	ft-kips
Tower Height, H:	168	ft
BP Dist. Above Fdn, bp _{dist} :	6	in

Pier Properties				
Pier Shape:	Square			
Pier Diameter, dpier :	7.0	ft		
Ext. Above Grade, E:	0.50	ft		
Pier Rebar Size, Sc :	11			
Pier Rebar Quantity, mc:	24			
Pier Tie/Spiral Size, St :	5			
Pier Tie/Spiral Quantity, mt:	21			
Pier Reinforcement Type:	Spiral			
Pier Clear Cover, cc _{pier} :	3	in		

Pad Properties		
Depth, D:	10.0	ft
Pad Width, W :	21.0	ft
Pad Thickness, T :	3.0	ft
Pad Rebar Size, Sp :	9	
Pad Rebar Quantity, mp :	25	
Pad Clear Cover, cc _{pad} :	3	in

Material Properties			
Rebar Grade, Fy :	60000	psi	
Concrete Compressive Strength, F'c:	3000	psi	
Dry Concrete Density, δ c :	150	pcf	

Soil Properties		
Total Soil Unit Weight, γ :	Total Soil Unit Weight, γ: 125 pcf	
Ultimate Gross Bearing, Qult:	12.000	ksf
Cohesion, Cu :		ksf
Friction Angle, $oldsymbol{arphi}$:	30	degrees
SPT Blow Count, Noblows:	21	
Base Friction, μ :		
Neglected Depth, N:	3.50	ft
Foundation Bearing on Rock?	No	
Groundwater Depth, gw :	12	ft

Foundation Analysis Checks				
	Capacity	Demand	Rating	Check
Lateral (Sliding) (kips)	341.54	32.00	9.4%	Pass
Bearing Pressure (ksf)	9.00	3.49	38.8%	Pass
Overturning (kip*ft)	6478.15	3977.00	61.4%	Pass
Pier Flexure (Comp.) (kip*ft)	5854.22	3865.00	66.0%	Pass
Pier Compression (kip)	25189.92	106.15	0.4%	Pass
Pad Flexure (kip*ft)	3390.85	1450.53	42.8%	Pass
Pad Shear - 1-way (kips)	648.20	266.25	41.1%	Pass
Pad Shear - 2-way (ksi)	0.16	0.04	23.8%	Pass

Soil Rating:	61.4%
Structural Rating:	66.0%

<--Toggle between Gross and Net

EXHIBIT 4



Radio Frequency Emissions Analysis Report

AT&T Existing Facility

Site ID: CT1121

FA#: 10071155

New Hartford - Inductrial Pk 115 Industrial Park Rd New Hartford, CT 06057

September 11, 2018

Centerline Communications Project Number: 950012-159

Site Compliance Summary		
Compliance Status:	COMPLIANT	
Site total MPE% of FCC general population allowable limit:	9.04 %	



September 11, 2018

AT&T Mobility – New England Attn: John Benedetto, RF Manager 550 Cochituate Road Suite 550 – 13&14 Framingham, MA 06040

Emissions Analysis for Site: **CT1121 – New Hartford - Inductrial Pk**

Centerline Communications, LLC ("Centerline") was directed to analyze the proposed AT&T facility located at **115 Industrial Park Rd, New Hartford, CT**, for the purpose of determining whether the emissions from the Proposed AT&T Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm2). The number of μ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

<u>General population/uncontrolled exposure</u> limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limits for the 700 and 850 MHz Bands are approximately 467 μ W/cm² and 567 μ W/cm² respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 2300 MHz (WCS) bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.



CALCULATIONS

Calculations were performed for the proposed AT&T Wireless antenna facility located at **115 Industrial Park Rd, New Hartford, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since AT&T is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
UMTS	850 MHz	2	30
LTE	700 MHz	2	40
LTE	700 MHz (Band 14)	2	40
LTE	850 MHz	2	40
LTE	1900 MHz (PCS)	4	40

Table 1: Channel Data Table



The following antennas listed in *Table 2* were used in the modeling for transmission in the 700 MHz, 850 MHz and 1900 MHz (PCS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

			Antenna
	Antenna		Centerline
Sector	Number	Antenna Make / Model	(ft)
A	1	Powerwave 7770	119
A	2	KMW AM-X-CD-16-65-00T-RET	119
A	3	CCI HPA-65R-BUU-H6	119
В	1	Powerwave 7770	119
В	2	KMW AM-X-CD-14-65-00T-RET	119
В	3	CCI SBNHH-1D65A	119
С	1	Powerwave 7770	119
С	2	KMW 800-10764	119
C	3	CCI SBNHH-1D65A	119

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.



RESULTS

Per the calculations completed for the proposed AT&T configurations *Table 3* shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

			Antenna		Total TX		
			Gain	Channel	Power		
Antenna ID	Antenna Make / Model	Frequency Bands	(dBd)	Count	(W)	ERP (W)	MPE %
Antenna A1	Powerwave 7770	850 MHz	11.4	2	60	828.23	0.41
	KMW						
Antenna A2	AM-X-CD-16-65-00T-RET	700 MHz	13.35	2	80	1,730.17	1.04
		700 MHz (Band 14) /	11.95 /				
	CCI	850 MHz /	12.65 /				
Antenna A3	HPA-65R-BUU-H6	1900 MHz (PCS)	14.75	8	320	7,502.63	2.83
	Sector A Composite MPE%			4.29			
Antenna B1	Powerwave 7770	850 MHz	11.4	2	60	828.23	0.41
	KMW						
Antenna B2	AM-X-CD-14-65-00T-RET	700 MHz	11.85	2	80	1,224.87	0.74
		700 MHz (Band 14) /	10.85 /				
	Commscope	850 MHz /	10.65 /				
Antenna B3	SBNHH-1D65A	1900 MHz (PCS)	14.55	8	320	6,463.74	2.33
				Sec	tor B Compo	site MPE%	3.48
Antenna C1	Powerwave 7770	850 MHz	11.4	2	60	828.23	0.41
Antenna C2	Kathrein 800-10764	700 MHz	12.15	2	80	1,312.47	0.79
		700 MHz (Band 14) /	10.85 /				
	Commscope	850 MHz /	10.65 /				
Antenna C3	SBNHH-1D65A	1900 MHz (PCS)	14.55	8	320	6,463.74	2.33
Sector C Composite MPE%					3.53		

Table 3: AT&T Emissions Levels



The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum AT&T MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, the sector with the largest calculated MPE% is Sector A. *Table 5* below shows a summary for each AT&T Sector as well as the composite MPE value for the site.

Site Composite MPE%		
Carrier	MPE%	
AT&T – Sector A	4.29 %	
Sprint	2.33 %	
T-Mobile	0.16 %	
MetroPCS	0.61 %	
Verizon Wireless	1.65 %	
Site Total MPE %:	9.04 %	

Table 4: All Carrier MPE Contributions

AT&T Sector A Total:	4.29 %
AT&T Sector B Total:	3.48 %
AT&T Sector C Total:	3.53 %
Site Total:	9.04 %

Table 5: Site MPE Summary



FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated AT&T sector(s). For this site, the sector with the largest calculated MPE% is Sector A.

AT&T _ Frequency Band / Technology Max Power Values (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (µW/cm²)	Calculated % MPE
AT&T 850 MHz UMTS – Antenna 1	2	414.12	119	2.33	850 MHz	567	0.41%
AT&T 700 MHz LTE – Antenna 2	2	865.09	119	4.87	700 MHz	467	1.04%
AT&T 700 MHz LTE (Band 14) – Antenna 3	2	626.70	119	3.53	700 MHz	467	0.76%
AT&T 850 MHz LTE – Antenna 3	2	736.31	119	4.15	850 MHz	567	0.73%
AT&T 1900 MHz (PCS) LTE – Antenna 3	4	1,194.15	119	13.45	1900 MHz (PCS)	1000	1.34%
						Total:	4.29%

Table 6: AT&T Maximum Sector MPE Power Values



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the AT&T facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

AT&T Sector	Power Density Value (%)		
Sector A:	4.29 %		
Sector B:	3.48 %		
Sector C:	3.53 %		
AT&T Maximum Total	4.29 %		
(Sector A):	4.29 %		
Site Total:	9.04 %		
Site Compliance Status:	COMPLIANT		

The anticipated composite MPE value for this site assuming all carriers present is **9.04** % of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Scott Heffernan

RF Engineering Director

Centerline Communications, LLC

95 Ryan Drive, Suite 1 Raynham, MA 02767

EXHIBIT 5



August 30, 2018



Centerline Communications 95 Ryan Drive Raynham, MA 02767

RE: Site Number:

CT1121 (LTE 2C/3C/4C)

FA Number: PACE Number:

10071155 MRCTB032151

PTN Number:

2051 A0GQK6

Site Name:

New Hartford-Industrial Park

Site Address:

Industrial Road

New Hartford, CT 06057

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by Centerline Communications to perform a mount analysis on the existing AT&T antenna/RRH mount to determine its capability of supporting the following additional loading:

- (3) 7770 Antennas (55.0"x11.0"x5.0" Wt. = 35 lbs. /each)
- (1) AM-X-CD-16-65-00T-RET Antenna (72"x11.8"x5.9" Wt. = 49 lbs. /each)
- (1) AM-X-CD-14-65-00T-RET Antenna (48.0"x11.8"x9.0" Wt. = 36.4 lbs. /each)
- (1) 800-10764 Antenna (55.2"x11.8"x6" Wt. = 41 lbs. /each)
- (3) RRUS-11 RRH's (19.7"x17.0"x7.2" Wt. = 51 lbs. /each) (Tower Mount)
- (6) LGP21401 TMA's (14.4"x9.0"x2.7" Wt. = 19 lbs. /each)
- (3) DBC0061F1V51-2 Diplexers (8.0"x6.2"x6.5" Wt. = 19 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7" Φ Wt. = 33 lbs. /each) (Tower Mount)
- (1) HPA-65R-BUU-H6 Antenna (72.0"x14.8"x9.0" Wt. = 51 lbs. /each)
- (2) \$BNHH-1D65A Antennas (55"x11.9"x7.1" Wt. = 34 lbs. /each)
- (3) 4415 B25 RRH's (14.96"x13.19"x5.39" Wt. = 44 lbs. /each)

No original structural design documents or fabrication drawings were available for the existing mounts. HDG's subconsultant, ProVertic LLC, conducted a survey climb and mapping of the existing AT&T antenna mounts on August 16, 2018.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2012 with 2016 Connecticut State Building Code, and AT&T Mount Technical Directive – R9.
- HDG considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all around the mount. Per TIA-222-G Annex B, the max basic wind speed for this site is equal to 100 mph with a max basic wind speed with ice of 40 mph. Per the AT&T Mount Technical Directive and Appendix N of the Connecticut State Building Code, an ultimate wind speed of 120 mph converted to a nominal wind speed of 93 mph was used for this analysis.
- HDG considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.

^{*}Proposed equipment shown in bold

Page 2 of 4 Re: CT1121 August 30, 2018

- HDG considers this site to be topographic category 3; tower is located at the upper half of a hill.
- The mount has been analyzed with load combinations consisting of 250 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 2.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst case location on the mount.
- The existing mount is secured to the existing monopole with a ring mount. The connection is considered OK by visual inspection.

Based on our evaluation, we have determined that the existing mount **IS CAPABLE** of supporting the proposed installation. HDG recommends the following modification:

 Install new handrail kit, SitePro1 P/N HRK14 (or approved equal). Handrail kit is required per AT&T Technical Directive to stabilize existing cantilevered antennas.

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Existing 2C/3C/4C Mount Rating	57	LC2	74%	PASS
Modified 2C/3C/4C Mount Rating	5/12/58	LC12/9/2	61%	PASS

Reference Documents:

Mount mapping report prepared by ProVertic LLC.

This determination was based on the following limitations and assumptions:

- 1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
- 2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
- 3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
- 4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
- 5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
- 6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted, Hudson Design Group LLC

Pular Cll

Michael Cabral Structural Dept. Head Daniel P. Hamm, PE Principal

MINIMUM INTERNAL

Page 2 of 4 Re: CT1121 August 30, 2018

- HDG considers this site to be topographic category 3; tower is located at the upper half of a hill.
- The mount has been analyzed with load combinations consisting of 250 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 2.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst case location on the mount.
- The existing mount is secured to the existing monopole with a ring mount. The connection is considered OK by visual inspection.

Based on our evaluation, we have determined that the existing mount **IS CAPABLE** of supporting the proposed installation. HDG recommends the following modification:

 Install new handrail kit, SitePro1 P/N HRK14 (or approved equal). Handrail kit is required per AT&T Technical Directive to stabilize existing cantilevered antennas.

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Existing 2C/3C/4C Mount Rating	57	LC2	74%	PASS
Modified 2C/3C/4C Mount Rating	5/12/58	LC12/9/2	61%	PASS

Reference Documents:

Mount mapping report prepared by ProVertic LLC.

This determination was based on the following limitations and assumptions:

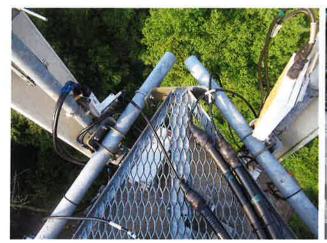
- HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
- 2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
- 3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
- 4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
- 5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
- 6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

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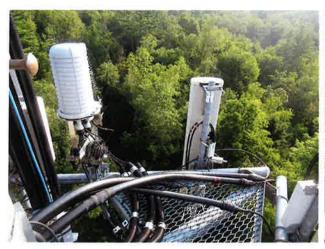
FIELD PHOTOS:



























Wind & Ice Calculations

8/30/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121

Designed By: AK Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$K_z = 2.01 (z/z_g)^{2/\alpha}$		z=	119 (ft)
		z _g =	1200 (ft)
K _z =	1.039	α=	7.0

 $Kzmin \le Kz \le 2.01$

Table 2-4

Exposure	Z _g	α	K _{zmin}	K _e
В	1200 ft	7.0	0.70	0.9
С	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.4 Topographic Factor:

Table 2-5

Topo. Category	K _t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} {=} \; [1 {+} (K_e \; K_t / K_{h)}]^2 \qquad \qquad K_h {=} \; e^{\; (f^*z/H)} \label{eq:Kzt}$$

$$K_{zt}$$
 1.282965901
 K_h
 3.60

 K_e
 0.9 (from Table 2-4)

 (If Category 1 then K_{zt} = 1.0)
 K_t
 0.53 (from Table 2-5)

 f
 2 (from Table 2-5)

 f
 1.19

 f
 1.28

 f
 1.28

 f
 1.14 (from Sec. 2.6.8)

2.6.8 Design Ice Thickness

Max Ice Thickness = t_i = 1.00 in $t_{iz} = 2.0*t_i*l*K_{iz}*(Kzt)^{0.35}$ t_{iz} = 2.48 in

8/30/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121

Designed By: AK Checked By: MSC



2.6.7 Gust Effect Factor

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0]

h= ht. of structure

h= 166

Gh= 0.85

2.6.7.2 Guyed Masts

Gh= 0.85

2.6.7.3 Pole Structures

Gh= 1.1

2.6.9 Appurtenances

Gh= 1.0

2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht.: width ratio > 5)

Gh=

1.35

Gh=

1.00

2.6.9.2 Design Wind Force on Appurtenances

State Code Ultimate Design Wind Speed:

 $V_{ult} = 120 \text{ mph}$

Nomial Design Wind Speed,

 $V_{asd} = V_{ult} V(0.6)$

93 mph

 V_{asd} per the AT&T Mount Technical Directive and Connecticut State Building Code, Latest Edition.

Per TIA-222-G,

 $q_{z(30)} =$

V_{min} =

90 mph

V_{max} = 100 mph

F= qz*Gh*(EPA)A

 $q_z = 0.00256*K_z*K_{zt}*K_d*V_{max}^2*I$

 $K_z = 1.039$

K_{zt}= 1.3

 $\begin{array}{ccc} q_z = & 28.00 \\ q_{z \text{ (lce)}} = & 5.18 \end{array}$

 $K_d = 0.95$ $V_{asd} = 93 \text{ mph}$

V_{max (ice)}= 40 mph

V₃₀= 30 mph |= 1.0

Table 2-2

2.92

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

8/30/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121

Designed By: AK Checked By: MSC



Determine Ca:

Table 2-8

	F	orce Coefficients (Ca) for	Appurtenances	
	ambas Turas	Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
M	ember Type	Ca	Ca	Ca
	Flat	1.2	1.4	2.0
Round	C < 32	0.7	0.8	1.2
	(Subcritical)	0.7	0.8	1.2
	32 ≤ C ≤ 64	44 - 0 485	44-0.415	10.
	(Transitional)	3.76/(C ^{0.485})	3.37/(C ^{0.415})	38.4/(C ^{-1.0})
	C > 64	0.5	0.0	0.6
	(Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.

(Aspect ratio is independent of the spacing between support points of a linear appurtenance,

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness =	2.48	in	Angle =	0 (deg)		Equival	ent Angle =	180 (deg)	
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	154	45	16
AM-X-CD-16-65-00T-RET Antenr	72.0	11.8	5.9	5.90	6.10	1.36	225	63	23
AM-X-CD-14-65-00T-RET Antenr	48.0	11.8	9.0	3.93	4.07	1.27	140	41	15
800-10764 Antenna	55.2	11.8	6.0	4.52	4.68	1.30	164	47	17
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.86	1.31	270	71	28
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	4.62	1.29	165	47	17
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 2.2	5.4 5.4	1.37 0.23	1.13 6.83	1.20 1.39		16 7	5 1
3" Pipe	3.5	12.0		0.29	0.29	1.20	10	6	1
2" Pipe	2.4	12.0		0.20	0.20	1.20	7	5	1

Dale: 8/31/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121



Angle = 30	(deg)		Ice Thick	ness =	2.48	ìn.			Equiva	fent Angle =	210	(deg)
			-				111	7.				
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
7770 Antenna	55.0	11.0	5.0	4,20	1.91	5.00	11.00	1.31	1.53	154	82	136
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	225	130	201
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	140	111	133
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	164	95	147
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	270	181	248
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	165	108	151
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 6.6	5.4 5.4	1.37 0.69	0.56 0.56	1.13 2.27	2.78 2.78	1.20 1.20	1.21 1.21	46 23	19 19	39 22
WIND LOADS WITH ICE:												
7770 Antenna	60.0	16.0	10.0	6.65	4.15	3,76	6.02	1.26	1,36	43	29	40
AM-X-CD-16-65-00T-RET Antenna	77.0	16.8	10.9	8.96	5.81	4.59	7.09	1.29	1.40	60	42	56
AM-X-CD-14-65-00T-RET Antenna	53.0	16.8	14.0	6.16	5.14	3.16	3.79	1.23	1.26	39	33	38
800-10764 Antenna	60.2	16.8	11.0	7.00	4.58	3.59	5.49	1.25	1.33	45	32	42
HPA-65R-BUU-H6 Antenna	77.0	19.8	14.0	10.56	7.46	3.89	5.51	1.26	1.33	69	52	65
SBNHH-1D65A Antenna	60.0	16.9	12.1	7.02	5.02	3.56	4.97	1,25	1,31	45	34	43
4415 B25 RRH 4415 B25 RRH (Shleided)	19.9 19.9	18.2 9.1	10.4 10.4	2.51 1.26	1.43 1.43	1.10 2.20	1.92 1.92	1.20 1.20	1.20 1.20	16 8	9	14 8
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	16	9	14
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	23	14	21
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	15	12	14
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	17	10	15
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	28	19	26
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	17	11	16
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 6.6	5.4 5.4	1.37 0.69	0.56 0.56	1.13 2.27	2.78 2.78	1.20 1.20	1.21 1.21	5 2	2 2	4 2

8/31/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121



Angle = 60	(deal)		Ina Think		2.48	-		î	Faulus	lant Amela -	240	(40-0)
Angle = 60	(deg)		Ice Thick	ness =	2.48	in.		ļ	Equiva	lent Angle =	240	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	100
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	225	130	154
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	140	111	118
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	164	95	112
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	270	181	203
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	165	108	122
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 9.9	5.4 5.4	1.37 1.03	0.56 0.56	1,13 1.51	2.78 2.78	1.20 1.20	1,21 1.21	46 35	19 19	26 23
WIND LOADS WITH ICE:												
7770 Antenna	60.0	16.0	10.0	6.65	4.15	3.76	6.02	1.26	1.36	43	29	33
AM-X-CD-16-65-00T-RET Antenna	77.0	16.8	10.9	8.96	5.81	4.59	7.09	1.29	1.40	60	42	47
AM-X-CD-14-65-00T-RET Antenna	53.0	16.8	14.0	6.16	5.14	3.16	3.79	1.23	1.26	39	33	35
800-10764 Antenna	60.2	16.8	11.0	7.00	4.58	3.59	5.49	1.25	1.33	45	32	35
HPA-65R-BUU-H6 Antenna	77.0	19.8	14.0	10.56	7.46	3.89	5,51	1.26	1.33	69	52	56
SBNHH-1D65A Antenna	60.0	16.9	12.1	7.02	5.02	3.56	4.97	1.25	1.31	45	34	37
4415 B25 RRH 4415 B25 RRH (Shielded)	19.9 19.9	18.2 13.6	10.4 10.4	2.51 1.88	1.43 1.43	1.10 1.46	1.92 1.92	1.20 1.20	1.20 1.20	16 12	9	11 10
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	16	9	10
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	23	14	16
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	15	12	12
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	17	10	12
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	28	19	21
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	17	11	13
4415 B25 RRH	15.0	13.2	5.4	1.37	0.56	1.13	2.78	1.20	1.21	5	2 2	3

Date: 8/31/2018

Project Name: New Hartford-Industrial Park

Project Number: C11121



Angle = 90	(deg)		Ice Thick	ness =	2.48	ln.		I	Equiva	lent Angle =	270	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs (side)) Force (lbs (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1,31	1.53	154	82	82
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	225	130	130
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	140	111	111
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1,47	164	95	95
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	270	181	181
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	165	108	108
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 2.2	5.4 5.4	1,37 0.23	0.56 0.56	1.13 6.83	2.78 2.78	1.20 1.39	1.21 1.21	46 9	19 19	19 19
WIND LOADS WITH ICE:												
7770 Antenna	60.0	16.0	10.0	6.65	4.15	3,76	6.02	1.26	1.36	43	29	29
AM-X-CD-16-65-00T-RET Antenna	77.0	16.8	10.9	8.96	5.81	4.59	7.09	1.29	1.40	60	42	42
AM-X-CD-14-65-00T-RET Antenna	53.0	16.8	14.0	6.16	5.14	3.16	3.79	1.23	1.26	39	33	33
800-10764 Antenna	60.2	16.8	11.0	7.00	4.58	3.59	5.49	1.25	1.33	45	32	32
HPA-65R-BUU-H6 Antenna	77.0	19.8	14.0	10.56	7.46	3.89	5.51	1.26	1.33	69	52	52
SBNHH-1D65A Antenna	60.0	16.9	12.1	7.02	5.02	3.56	4.97	1.25	1.31	45	34	34
4415 B25 RRH 4415 B25 RRH (Shielded)	19.9 19.9	18.2 7.2	10.4 10.4	2.51 0.99	1.43 1.43	1.10 2.79	1.92 1.92	1.20 1.21	1.20 1.20	16 6	9	9
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	16	9	9
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2,95	6.10	12,20	1.36	1.57	23	14	14
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	15	12	12
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4,68	9.20	1.30	1.47	17	10	10
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1,31	1.43	28	19	19
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	17	11	11
4415 B25 RRH	15.0	13.2	5.4	1.37	0.56	1.13	2.78	1.20	1.21	5	2	2

8/31/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121



Angle = 120	(deg)		Ice Thick	ness =	2.48	in,		1	Equiva	lent Angle =	300	(deg)
	(6/											10/
WIND LOADS WITH NO ICE:												
Appurtenances	Height	<u>Width</u>	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	100
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	225	130	154
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	140	111	118
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	164	95	112
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	270	181	203
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	165	108	122
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 9.9	5.4 5.4	1.37 1.03	0.56 0.56	1.13 1.51	2.78 2,78	1.20 1.20	1.21 1.21	46 35	19 19	26 23
WIND LOADS WITH ICE:												
7770 Antenna	60.0	16.0	10.0	6.65	4.15	3.76	6.02	1.26	1.36	43	29	33
AM-X-CD-16-65-00T-RET Antenna	77.0	16.8	10.9	8.96	5.81	4.59	7.09	1.29	1.40	60	42	47
AM-X-CD-14-65-00T-RET Antenna	53.0	16.8	14.0	6.16	5.14	3.16	3.79	1.23	1.26	39	33	35
800-10764 Antenna	60.2	16.8	11.0	7.00	4.58	3.59	5.49	1.25	1.33	45	32	35
HPA-65R-BUU-H6 Antenna	77.0	19.8	14.0	10.56	7.46	3.89	5.51	1.26	1.33	69	52	56
SBNHH-1D65A Antenna	60.0	16.9	12.1	7.02	5.02	3.56	4.97	1.25	1.31	45	34	37
4415 B25 RRH 4415 B25 RRH (Shielded)	19.9 19.9	18.2 13.6	10.4 10.4	2.51 1.88	1.43 1.43	1.10 1.46	1.92 1.92	1.20 1.20	1.20 1.20	16 12	9	11 10
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	16	9	10
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	23	14	16
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	15	12	12
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	17	10	12
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	28	19	21
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	17	11	13
4415 B25 RRH	15.0 15.0	13.2	5.4	1.37	0.56	1.13	2.78	1.20	1.21	5	2	3

8/31/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121



Angle = 150	(deg)		Ice Thick	ness =	2.48	in.			Equiva	lent Angle =	330	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	Height	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs (angle)
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	154	82	136
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12,20	1.36	1.57	225	130	201
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	140	111	133
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	164	95	147
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	270	181	248
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	165	108	151
4415 B25 RRH 4415 B25 RRH (Shielded)	15.0 15.0	13.2 6.6	5.4 5.4	1.37 0.69	0.56 0.56	1.13 2.27	2.78 2.78	1.20 1.20	1.21 1.21	46 23	19 19	39 22
WIND LOADS WITH ICE:												
7770 Antenna	60.0	16.0	10.0	6.65	4.15	3.76	6.02	1.26	1.36	43	29	40
AM-X-CD-16-65-00T-RET Antenna	77.0	16.8	10.9	8.96	5.81	4.59	7.09	1.29	1.40	60	42	56
AM-X-CD-14-65-00T-RET Antenna	53.0	16.8	14.0	6.16	5.14	3.16	3.79	1.23	1.26	39	33	38
800-10764 Antenna	60.2	16.8	11.0	7.00	4.58	3.59	5.49	1.25	1.33	45	32	42
HPA-65R-BUU-H6 Antenna	77.0	19.8	14.0	10.56	7.46	3.89	5.51	1.26	1.33	69	52	65
SBNHH-1D65A Antenna	60.0	16.9	12.1	7.02	5.02	3.56	4.97	1.25	1.31	45	34	43
4415 B25 RRH 4415 B25 RRH (Shielded)	19.9 19.9	18.2 9.1	10.4 10.4	2.51 1.26	1.43 1.43	1.10 2.20	1.92 1.92	1.20 1.20	1.20 1.20	16 8	9	14 8
WIND LOADS AT 30 MPH:												
7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1.53	16	9	14
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1,57	23	14	21
AM-X-CD-14-65-00T-RET Antenna	48.0	11.8	9.0	3.93	3.00	4.07	5.33	1.27	1.33	15	12	14
800-10764 Antenna	55.2	11.8	6.0	4.52	2.30	4.68	9.20	1.30	1.47	17	10	15
HPA-65R-BUU-H6 Antenna	72.0	14.8	9.0	7.40	4.50	4.86	8.00	1.31	1.43	28	19	26
SBNHH-1D65A Antenna	55.0	11.9	7.1	4.55	2.71	4.62	7.75	1.29	1.42	17	11	16
4415 B25 RRH	15.0	13.2	5.4	1.37	0.56	1.13	2.78	1.20	1.21	5	2	4

Date: 8/30/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121

Designed By: AK Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice: 2.48 in.

Density of ice: 56 pcf

7770 Antenna

Weight of ice based on total radial SF area:

 Height (in):
 55.0

 Width (in):
 11.0

 Depth (in):
 5.0

Total weight of ice on object: 202 lbs

Weight of object: 35 lbs

Combined weight of ice and object: 237 lbs

AM-X-CD-14-65-00T-RET Antenna

Weight of ice based on total radial SF area:

 Height (in):
 48.0

 Width (in):
 11.8

 Depth (in):
 9.0

Total weight of ice on object: 210 lbs

Weight of object: 37 lbs

Combined weight of ice and object: 247 lbs

HPA-65R-BUU-H6 Antenna

Weight of ice based on total radial SF area:

 Height (in):
 72.0

 Width (in):
 14.8

 Depth (in):
 9.0

Total weight of ice on object: 360 lbs

Weight of object:

Combined weight of ice and object: 411 lbs

51 lbs

4415 B25 RRH

Weight of ice based on total radial SF area:

 Height (in):
 15.0

 Width (in):
 13.2

 Depth (in):
 5.4

Total weight of ice on object: 63 lbs

Weight of object: 44 lbs

Combined weight of ice and object: 107 lbs

DBC0061F1V51-2 Diplexer

Weight of ice based on total radial SF area:

 Height (in):
 8.0

 Width (in):
 6.2

 Depth (in):
 6.5

Total weight of ice on object: 23 lbs

Weight of object: 19 lbs

Combined weight of ice and object: 42 lbs

AM-X-CD-16-65-00T-RET Antenna

Weight of ice based on total radial SF area: Height (in): 72.0

Width (in): 11.8
Depth (in): 5.9

Total weight of ice on object: 285 lbs

Weight of object: 49 lbs

Combined weight of ice and object: 334 lbs

800-10764 Antenna

Weight of ice based on total radial SF area:

 Height (in):
 55.2

 Width (in):
 11.8

 Depth (in):
 6.0

Total weight of ice on object: 219 lbs

Weight of object: 41 lbs

Combined weight of ice and object: 260 lbs

SBNHH-1D65A Antenna

Weight of ice based on total radial SF area:

 Height (in):
 55.0

 Width (in):
 11.9

 Depth (in):
 7.1

Total weight of ice on object: 227 lbs
Weight of object: 34 lbs

Combined with a fire and able at

Combined weight of ice and object: 261 lbs

800-10764 Antenna

Weight of ice based on total radial SF area:

 Height (in):
 55.2

 Width (in):
 11.8

 Depth (in):
 6.0

Total weight of ice on object: 219 lbs

Weight of object: 41 lbs

Combined weight of ice and object: 260 lbs

LGP21401 TMA

Weight of ice based on total radial SF area:

 Height (in):
 14.4

 Width (in):
 9.0

 Depth (in):
 2.7

Total weight of ice on object: 43 lbs

Weight of object: 19 lbs

Combined weight of ice and object: 62 lbs

Date: 8/30/2018

Project Name: New Hartford-Industrial Park

Project Number: CT1121

Designed By: AK Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice: 2.48 in. Density of ice: 56 pcf

7770 Antenna

Weight of ice based on total radial SF area: Height (in): 55.0 Width (in): 11.0 Depth (in): 5.0

Total weight of ice on object: 202 lbs

Weight of object:

35 lbs Combined weight of ice and object: 237 lbs

AM-X-CD-14-65-00T-RET Antenna

Weight of ice based on total radial SF area:

Height (in): Width (in): 11.8 Depth (in): 9.0

Total weight of ice on object: 210 lbs

Weight of object:

37 lbs 247 lbs Combined weight of ice and object:

HPA-65R-BUU-H6 Antenna

Weight of ice based on total radial SF area:

Height (in): 72.0 Width (in): 14.8 Depth (in): 9.0

Total weight of ice on object: 360 lbs

Weight of object: 51 lbs

Combined weight of ice and object: 411 lbs

4415 B25 RRH

Weight of ice based on total radial SF area:

Height (in): Width (in): 13.2 Depth (in): 5.4

Total weight of ice on object:

Weight of object: 44 lbs

Combined weight of ice and object: 107 lbs

63 lbs

23 lbs

DBC0061F1V51-2 Diplexer

Weight of ice based on total radial SF area:

Height (in): 8.0 Width (in): 6.2 Depth (in):

Total weight of ice on object:

Weight of object: 19 lbs

Combined weight of ice and object: 42 lbs

PL 6x1/2

Weight of ice based on total radial SF area:

Height (in): 6 Width (in):

Per foot weight of ice on object: 26 plf

L 2x2x3/16 Angles

Weight of ice based on total radial SF area: Height (in):

Width (in): Per foot weight of ice on object: 16 plf

L 2-1/2x2-1/2x3/6

Weight of ice based on total radial SF area:

Height (in): 2.5 Width (in):

Per foot weight of ice on object: 18 plf AM-X-CD-16-65-00T-RET Antenna

Weight of ice based on total radial SF area: Height (in): 72.0 Width (in): 11.8 Depth (in): 5.9

Total weight of ice on object: 285 lbs

Weight of object:

Combined weight of ice and object: 334 lbs

800-10764 Antenna

Weight of ice based on total radial SF area: Height (in): 55.2 Width (in): 11.8

Depth (in): 6.0

Total weight of ice on object: 219 lbs Weight of object:

Combined weight of ice and object: 260 lbs

SBNHH-1D65A Antenna

Weight of ice based on total radial SF area: Height (in): 55.0

Width (in): 11.9 Depth (in): 7.1

Total weight of ice on object: 227 lbs

Weight of object:

Combined weight of ice and object: 261 lbs

800-10764 Antenna

Weight of ice based on total radial SF area:

Height (in): Width (in): 11.8 Depth (in): 6.0 Total weight of ice on object:

219 lbs Weight of object:

Combined weight of ice and object:

LGP21401 TMA

Weight of ice based on total radial SF area:

Height (in): Width (in): 9.0 Depth (in):

Total weight of ice on object: 43 lbs

Weight of object:

62 lbs Combined weight of ice and object:

2" pipe

Per foot weight of ice:

diameter (in): 2.38

Per foot weight of ice on object: 15 plf

3" Pipe

Per foot weight of ice:

diameter (in):

Per foot weight of ice on object: 18 plf

HSS 4x4

Weight of ice based on total radial SF area:

Height (in): Width (in):

Per foot weight of ice on object: 25 plf



Mount Calculations (Modified 2C/3C/4C Configuration)



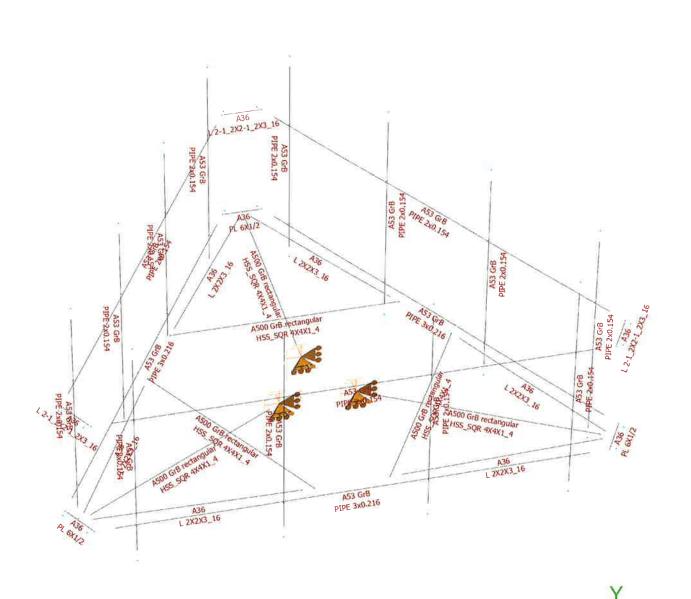
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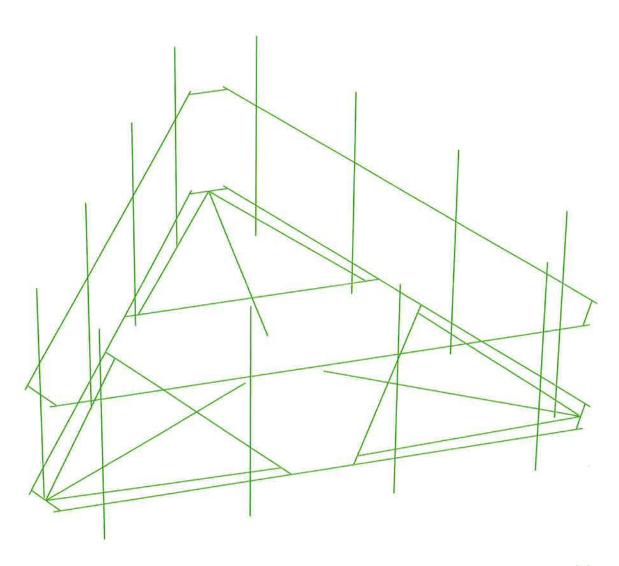


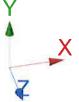


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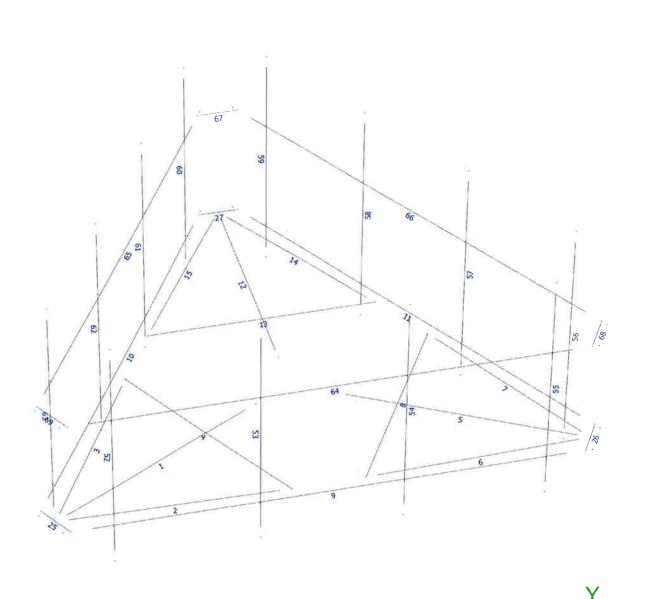








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Load data

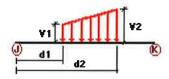
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
 DL	Dead Load	No	DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
∕Vi0	Ice Wind Load 0/60/120 deg	No	WIND
Ni30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
_L1	250 lb Live Load Center of Mount	No	LL
_L2	250 lb Live Load End of Mount	No	LL
_La1	500 lb Live Load on Antenna 1	No	LL
_La2	500 lb Live Load on Antenna 2	No	LL
La3	500 lb Live Load on Antenna 3	No	LL
La4	500 lb Live Load on Antenna 4	No	LL
W180	-W0	Yes	
N210	-W30	Yes	
Vi180	-Wi0	Yes	
Vi210	-Wi30	Yes	
VL180	-WL0	Yes	
VL210	-WL30	Yes	

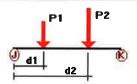
Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	1	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	2	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	3	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	5	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	6	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	7	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	12	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	14	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	15	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes

wo	10	7	-0.01	-0.01	0.00	Yes	100.00	Yes
****	11	Z Z	-0.01	-0.01	0.00	Yes	100.00	Yes
	64	7	-0.007	-0.007	0.00	Yes	100.00	Yes
	65	Z Z	-0.007	-0.007	0.00	Yes	100.00	Yes
	66	7	-0.007	-0.007	0.00	Yes	100.00	Yes
	9	Z Z	-0.01	-0.01	0.00	Yes	100.00	Yes
W30	10	X	-0.01	-0.01	0.00	Yes	100.00	Yes
	11	X	-0.01	-0.01	0.00	Yes	100.00	Yes
	64	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	65	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	66	X	-0.007	-0.007	0.00	Yes	100.00	Yes
	9	Х	-0.01	-0.01	0.00	Yes	100.00	Yes
Di	1	Υ	-0.025	-0.025	0.00	Yes	100.00	Yes
	2	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	3	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	4	Υ	-0.025	-0.025	0.00	Yes	100.00	Yes
	5	Y	-0.025	-0.025	0.00	Yes	100.00	Yes
	6	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	7	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	8	Υ	-0.025	-0.025	0.00	Yes	100.00	Yes
	10	Y	-0.018	-0.018	0.00	Yes	100.00	Yes
	11	Υ	-0.018	-0.018	0.00	Yes	100.00	Yes
	12	Υ	-0.025	-0.025	0.00	Yes	100.00	Yes
	13	Υ	-0.025	-0.025	0.00	Yes	100.00	Yes
	14	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	15	Υ	-0.016	-0.016	0.00	Yes	100.00	Yes
	25	Υ	-0.026	-0.026	0.00	Yes	100.00	Yes
	26	Υ	-0.026	-0.026	0.00	Yes	100.00	Yes
	27	Υ	-0.026	-0.026	0.00	Yes	100.00	Yes
	52	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	53	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	54	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	55	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	56	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	57	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	58	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	59	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	60	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	61	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	62	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	63	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	64	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	65	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	66	Υ	-0.015	-0.015	0.00	Yes	100.00	Yes
	67	Υ	-0.018	-0.018	0.00	Yes	100.00	Yes
	68	Υ	-0.018	-0.018	0.00	Yes	100.00	Yes
	69	Υ	-0.018	-0.018	0.00	Yes	100.00	Yes
	9	Y	-0.018	-0.018	0.00	Yes	100.00	Yes

Concentrated forces on members



Condition	Member	Dir1	Value1	Dist1	%
STREET WOULD BE DANNED	zawwas zoosuneun	2200000-000	[Kip]	[ft]	
DL	53	у	-0.017	4.54	No
		У	-0.017	1.46	No
	997315	У	-0.044	3.00	No
	54	У	-0.019	4.25	No
		y	-0.019 -0.019	1.75 3.00	No No
	55	y y	-0.019	4.54	No
		y	-0.018	1.46	No
		ý	-0.038	4.00	No
	57	У	-0.026	5.25	No
		У	-0.026	0.75	No
	50	У	-0.044	2.00	No
	58	У	-0.025	5.25	No
		y y	-0.025 -0.019	0.75 4.00	No No
	59	y	-0.018	4.54	No
		y	-0.018	1.46	No
		y	-0.038	4.00	No
	61	у	-0.017	4.54	No
		У	-0.017	1.46	No
	12420	У	-0.044	2.00	No
	62	У	-0.021	4.55	No
		У	-0.021	1.45	No
	63	У	-0.019	3.00 4.54	No No
	03	y y	-0.018 -0.018	1.46	No
		y	-0.038	4.00	No
W0	53	z	-0.083	4.54	No
		z	-0.083	1.46	No
		z	-0.009	3.00	No
	54	Z	-0.07	4.25	No
		Z	-0.07	1.75	No
	55	z	-0.078	4.54	No
	67	Z	-0.078	1.46	No
	57	z z	-0.102 -0.102	5.25 0.75	No No
		z	-0.023	2.00	No
	58	z	-0.077	5.25	No
	52	z	-0.077	0.75	No
	59	Z	-0.051	4.54	No
		Z	-0.051	1.46	No
	61	Z	-0.062	4.54	No
		Z	-0.062	1.46	No
	60	Z	-0.023	2.00	No
	62	z z	-0.057 -0.057	4.55 1.45	No No
	63	z	-0.051	4.54	No
	00	z	-0.051	1.46	No
W30	53	x	-0.055	4.54	No
		x	-0.055	1.46	No
		x	-0.019	2.00	No
	54	X	-0.056	4.25	No
		x	-0.056	1.75	No
	55	X	-0.041	4.54	No
	57	X	-0.041	1.46	No
	o i	×	-0.124 -0.124	5.25 0.75	No No
		x	-0.022	2.00	No
	58	x	-0.101	5.25	No
	m.540	х	-0.101	0.75	No

	59	×	-0.069	4.54	No
		x	-0.069	1.46	No
	61	×	-0.076	4.54	No
		x	-0.076	1.46	No
		x	-0.022	2.00	No
	62	×	-0.074	4.55	No
		×	-0.074	1.45	No
	63	x	-0.069	4.54	No
		X	-0.069	1.46	No
Di	53	У	-0.114	4.54	No
		У	-0.114	1.46	No
		У	-0.063	3.00	No
	54	У	-0.105	4.25	No
		У	-0.105	1.75	No
		У	-0.023	3.00	No
	55	У	-0.101	4.54	No
		У	-0.101	1.46	No
		У	-0.086	4.00	No
	57	У	-0.18	5.25	No
		У	-0.18	0.75	No
		У	-0.063	2.00	No
	58	У	-0.143	5.25	No
		У	-0.143	0.75	No
	=0	У	-0.023	4.00	No
	59	У	-0.101	4.54	No
		У	-0.101	1.46	No
	0.4	У	-0.086	4.00	No
	61	У	-0.114	4.54	No
		У	-0.114	1.46	No
		У	-0.063	2.00	No
	62	У	-0.11	4.55	No
		У	-0.11	1.45	No
		У	-0.023	3.00	No
	63	У	-0.101	4.54	No
		У	-0.101	1.46	No
14/10	50	У	-0.086	4.00	No
Wi0	53	Z	-0.024	4.54	No
		z	-0.024	1.46	No
	E 4	z	-0.007	3.00	No
	54	z	-0.021	4.25	No
	55	z	-0.021	1.75	No
	55	Z	-0.023	4.54	No
	57	z	-0.023	1.46	No
	57	z	-0.028	5.25	No
		z	-0.028	0.75	No
	50	z	-0.01	2.00	No
	58	Z	-0.024	5.25	No
	50	z	-0.024	0.75	No
	59	z	-0.017	4.54	No
	61	Z	-0.017 0.019	1.46 4.54	No No
	ΟI	Z	-0.019 -0.019	4.54 1.46	No No
		Z	-0.019	2.00	No
	62	z	-0.01 -0.018	4.55	No
	UZ	Z		4.55 1.45	
	63	Z	-0.018 -0.017		No No
	US	Z	-0.017 -0.017	4.54 1.46	No No
Wi30	53	Z	-0.017 -0.018	4.54	No No
VVIOU	55	×	-0.018	1.46	No
		×	-0.009	2.00	No
			-0.008	2.00	140

	54	×	-0.017	4.25	No
		×	-0.017	1.75	No
	55	×	-0.015	4.54	No
		×	-0.015	1.46	No
	57	×	-0.033	5.25	No
		×	-0.033	0.75	No
		×	-0.008	2.00	No
	58	×	-0.028	5.25	No
		×	-0.028	0.75	No
	59	×	-0.02	4.54	No
		×	-0.02	1.46	No
	61	×	-0.022	4.54	No
		×	-0.022	1.46	No
		×	-0.008	2.00	No
	62	×	-0.021	4.55	No
		x	-0.021	1.45	No
	63	×	-0.02	4.54	No
		×	-0.02	1.46	No
WL0	53	z	-0.009	4.54	No
		z	-0.009	1.46	No
		z	-0.001	3.00	No
	54	z	-0.008	4.25	No
		z	-0.008	1.75	No
	55	z	-0.009	4.54	No
		z	-0.009	1.46	No
	57	z	-0.011	5.25	No
		z	-0.011	0.75	No
		z	-0.003	2.00	No
	58	z	-0.009	5.25	No
	•••	z	-0.009	0.75	No
	59	z	-0.006	4.54	No
	•	z	-0.006	1.46	No
	61	z	-0.007	4.54	No
	Ψ.	z	-0.007	1.46	No
		z	-0.003	2.00	No
	62	z	-0.006	4.55	No
	02	z	-0.006	1.45	No
	63	z	-0.006	4.54	No
	00	z	-0.006	1.46	No
WL30	53	X	-0.006	4.54	No
VVLOU	00	x	-0.006	1.46	No
		x	-0.002	2.00	No
	54		-0.002	4.25	No
	J4	X	-0.006	1.75	
	55	×			No
	55	×	-0.005 -0.005	4.54	No
	E7	×		1.46	No
	57	X	-0.013	5.25	No
		×	-0.013	0.75	No
		×	-0.003	2.00	No
	58	x	-0.011	5.25	No
	50	X	-0.011	0.75	No
	59	X	-0.008	4.54	No
	04	X	-0.008	1.46	No
	61	×	-0.008	4.54	No
		x	-0.008	1.46	No
		x	-0.003	2.00	No
	62	×	-0.008	4.55	No
		×	-0.008	1.45	No
	63	x	-0.008	4.54	No
		x	-0.008	1.46	No

LL1	64	у	-0.25	6.25	No
	9	у	-0.25	6.25	No
LL2	64	У	-0.25	0.00	No
	9	У	-0.25	0.00	No
LLa1	55	у	-0.25	3.00	No
LLa2	54	у	-0.25	3.00	No
LLa3	53	У	-0.25	3.00	No
LLa4	52	у	-0.25	3.00	No

Self weight multipliers for load conditions

			Self weight multiplier				
Condition	Description	Comb.	MultX	MultY	MultZ		
 DL	Dead Load	No	0.00	-1.00	0.00		
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00		
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00		
Di	Ice Load	No	0.00	0.00	0.00		
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00		
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00		
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00		
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00		
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00		
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00		
LLa1	500 lb Live Load on Antenna 1	No	0.00	0.00	0.00		
LLa2	500 lb Live Load on Antenna 2	No	0.00	0.00	0.00		
LLa3	500 lb Live Load on Antenna 3	No	0.00	0.00	0.00		
LLa4	500 lb Live Load on Antenna 4	No	0.00	0.00	0.00		
W180	-W0	Yes	0.00	0.00	0.00		
W210	-W30	Yes	0.00	0.00	0.00		
Wi180	-Wi0	Yes	0.00	0.00	0.00		
Ni210	-Wi30	Yes	0.00	0.00	0.00		
VL180	-WL0	Yes	0.00	0.00	0.00		
WL210	-WL30	Yes	0.00	0.00	0.00		

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]	
DL	0.00	0.00	0.00	
W0	0.00	0.00	0.00	
W30	0.00	0.00	0.00	
Di	0.00	0.00	0.00	
Wi0	0.00	0.00	0.00	
Wi30	0.00	0.00	0.00	
WL0	0.00	0.00	0.00	
WL30	0.00	0.00	0.00	
LL1	0.00	0.00	0.00	
LL2	0.00	0.00	0.00	
LLa1	0.00	0.00	0.00	
LLa2	0.00	0.00	0.00	
LLa3	0.00	0.00	0.00	

LLa4	0.00	0.00	0.00	
W180	0.00	0.00	0.00	
W210	0.00	0.00	0.00	
Wi180	0.00	0.00	0.00	
Wi210	0.00	0.00	0.00	
WL180	0.00	0.00	0.00	
WL210	0.00	0.00	0.00	



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Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design:

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

LC4=1.2DL-1.6W30

1.05 0.001 1.01100

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30

LC7=0.9DL-1.6W0

LC8=0.9DL-1.6W30

LC9=1.2DL+Di+Wi0

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LC12=1.2DL+Di-Wi30

LC12=1.2DL11 LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.6LL1

LC16=1.2DL+1.6LL2

LC17=1.2DL+WL0+LLa1

LC 17 = 1.2DL+VVLU+LLa I

LC18=1.2DL+WL30+LLa1

LC19=1.2DL-WL0+LLa1

LC20=1.2DL-WL30+LLa1 LC21=1.2DL+WL0+LLa2

LC22=1.2DL+WL30+LLa2

LC23=1.2DL-WL0+LLa2

LC24=1.2DL-WL30+LLa2

LC25=1.2DL+WL0+LLa3

LC26=1.2DL+WL30+LLa3

LC27=1.2DL+WL0+LLa3

LC28=1.2DL-WL30+LLa3

LC29=1.2DL+WL0+LLa4

LC30=1.2DL+WL30+LLa4

LC31=1.2DL-WL0+LLa4

LC32=1.2DL-WL30+LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS_SQR 4X4X1_4	1	LC1 at 100.00%	0.10	 ОК	
			LC10 at 100.00%	0.56	ОК	Eq. H1-1b
			LC11 at 100.00%	0.56	OK	
			LC12 at 100.00%	0.51	OK	
			LC13 at 100.00%	0.17	OK	
			LC14 at 100.00%	0.12	ОК	
			LC15 at 100.00%	0.25	OK	
			LC16 at 100.00%	0.47	OK	
			LC17 at 100.00%	0.15	OK	
			LC18 at 100.00%	0.17	OK	
			LC19 at 100.00%	0.16	OK	
			LC2 at 100.00%	0.36	ОК	
			LC20 at 100.00%	0.15	OK	
			LC21 at 100.00%	0.17	ok	
			LC22 at 100.00%	0.19	OK	
			LC23 at 100.00%	0.19	OK	
			LC24 at 100.00%	0.17	OK	

Page1

	LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC3 at 100.00% LC3 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 75.00% LC5 at 75.00% LC6 at 100.00% LC7 at 100.00% LC7 at 100.00% LC8 at 75.00% LC9 at 100.00%	0.21 0.22 0.22 0.20 0.24 0.30 0.26 0.26 0.06 0.32 0.26 0.07 0.53	OK OK OK OK OK OK OK OK OK OK OK OK	
4	LC1 at 100.00% LC10 at 50.00% LC11 at 50.00% LC12 at 50.00% LC13 at 50.00% LC14 at 50.00% LC15 at 50.00% LC16 at 50.00% LC17 at 50.00% LC18 at 50.00% LC19 at 50.00% LC2 at 48.44% LC20 at 50.00% LC21 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 50.00% LC25 at 50.00% LC26 at 50.00% LC27 at 50.00% LC28 at 50.00% LC29 at 50.00% LC29 at 50.00% LC21 at 50.00% LC21 at 50.00% LC21 at 50.00% LC21 at 50.00% LC23 at 50.00% LC23 at 50.00% LC23 at 50.00% LC31 at 50.00% LC31 at 50.00% LC31 at 50.00%	0.07 0.33 0.33 0.31 0.09 0.07 0.18 0.18 0.10 0.11 0.11 0.12 0.12 0.11 0.12 0.13 0.13 0.13 0.12 0.17 0.12 0.12 0.17	OK	Eq. H1-1b Eq. H1-1b
	LC32 at 50.00% LC4 at 0.00% LC5 at 100.00% LC6 at 48.44% LC7 at 50.00% LC8 at 0.00%	0.12 0.06 0.07 0.17 0.15 0.06 0.31	OK OK OK OK OK OK	Eq. H1-1b
5	LC1 at 100.00% LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 75.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00%	0.15 0.56 0.61 0.61 0.17 0.13 0.26 0.13 0.25 0.25 0.26 0.06 0.27 0.21	OK O	Eq. H1-1b

	LC23 at 100.00%	0.23	OK	
	LC24 at 100.00%	0.23	OK	
			OK	
	LC25 at 100.00%	0.18		
	LC26 at 100.00%	0.18	OK	
	LC27 at 100.00%	0.20	OK	
	LC28 at 100.00%	0.20	OK	
	LC29 at 100.00%	0.16	OK	
	LC3 at 100.00%	0.35	OK	
	LC30 at 100.00%	0.15	OK	
	LC31 at 100.00%	0.17	OK	
	LC32 at 100.00%	0.17	OK	
	LC4 at 100.00%	0.37	OK	
	LC5 at 100.00%	0.11	OK	
	LC6 at 75.00%	0.07	OK	
	LC7 at 100.00%	0.31	OK	
	LC8 at 100.00%	0.33	OK	
	LC9 at 100.00%	0.58	OK	
8	LC1 at 48.44%	0.08	OK	
0				
	LC10 at 48.44%	0.33	OK	
	LC11 at 48.44%	0.35	OK	
	LC12 at 48.44%	0.35	OK	Eq. H1-1b
	LC13 at 50.00%	0.09	OK	
	LC14 at 50.00%	0.07	OK	
	LC15 at 50.00%	0.18	OK	
	LC16 at 50.00%	0.11	OK	
			OK	
	LC17 at 50.00%	0.12		
	LC18 at 50.00%	0.12	OK	
	LC19 at 50.00%	0.12	OK	
	LC2 at 0.00%	0.07	OK	Eq. H1-1b
	LC20 at 50.00%	0.13	OK	
	LC21 at 50.00%	0.13	OK	
	LC22 at 50.00%	0.12	OK	
	LC23 at 50.00%	0.13	OK	
	LC24 at 50.00%	0.13	OK	
	LC25 at 50.00%	0.12	OK	
	LC26 at 50.00%	0.11	OK	
	LC27 at 50.00%	0.12	OK	
	LC28 at 50.00%		OK	
		0.12		
	LC29 at 50.00%	0.10	OK	
	LC3 at 50.00%	0.18	OK	
	LC30 at 50.00%	0.10	ОК	
	LC31 at 50.00%	0.11	OK	
	LC32 at 50.00%	0.11	OK	
	LC4 at 48.44%	0.20	OK	
	LC5 at 100.00%	0.08	OK	
	LC6 at 0.00%	0.06	OK	
	LC7 at 50.00%	0.15	OK	
	LC8 at 48.44%	0.17	OK	
	LC9 at 48.44%	0.34	OK	
	200 01 10.1170	0.01		
40	1.04 -4.0.000/	0.00	OV	
12	LC1 at 0.00%	0.39	OK	
	LC10 at 0.00%	0.59	OK	
	LC11 at 0.00%	0.55	OK	
	LC12 at 0.00%	0.59	OK	
	LC13 at 0.00%	0.17	OK	
	LC14 at 0.00%	0.13	OK	
	LC15 at 0.00%	0.12	ОК	
	LC16 at 0.00%	0.11	OK	
	LC17 at 0.00%	0.16	OK	
	LC18 at 0.00%	0.16	OK	
	LC19 at 0.00%	0.14	OK	
	LC2 at 0.00%	0.26	OK	
	LC20 at 0.00%	0.16	OK	

	LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 25.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00%	0.16 0.14 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.20 0.22 0.09 0.22 0.61	OK O	Eq. H1-1b
13	LC1 at 50.00% LC10 at 50.00%	0.19 0.35	OK OK	
	LC11 at 50.00%	0.34	OK OK	
	LC12 at 50.00%	0.35	OK	
	LC13 at 50.00%	0.10	OK	
	LC14 at 50.00%	0.07	OK	
	LC15 at 50.00%	0.06	OK	
	LC16 at 48.44%	0.10	OK	
	LC17 at 50.00%	0.10	OK	
	LC18 at 50.00%	0.09	OK	
	LC19 at 50.00%	0.09	OK	
	LC2 at 48.44%	0.13	OK OK	
	LC20 at 50.00% LC21 at 50.00%	0.10 0.09	OK	
	LC22 at 50.00%	0.09	OK	
	LC23 at 50.00%	0.08	OK	
	LC24 at 50.00%	0.09	OK	
	LC25 at 50.00%	0.09	OK	
	LC26 at 50.00%	0.09	OK	
	LC27 at 50.00%	0.08	OK	
	LC28 at 50.00%	0.09	OK	
	LC29 at 48.44%	0.09	OK	
	LC3 at 100.00%	0.03	OK	
	LC30 at 48.44%	0.09	OK	
	LC31 at 48.44%	0.09	OK	
	LC32 at 48.44% LC4 at 50.00%	0.09 0.14	OK OK	
	LC5 at 50.00%	0.14	OK OK	
	LC6 at 48.44%	0.11	OK	
	LC7 at 100.00%	0.03	OK	
	LC8 at 50.00%	0.12	OK	
	LC9 at 50.00%	0.36	ОК	Eq. H1-1b
67	LC1 at 100.00%	0.26	 ОК	
O1	LC10 at 100.00%	0.25	OK	
	LC11 at 100.00%	0.23	OK OK	
	LC12 at 100.00%	0.29	ok	
	LC13 at 100.00%	0.08	OK	
	LC14 at 100.00%	0.06	OK	
	LC15 at 100.00%	0.08	ok	
	LC16 at 100.00%	0.15	OK	
	LC17 at 0.00%	0.09	OK	
	LC18 at 0.00%	0.08	ОК	
	LC19 at 0.00%	0.08	ОК	

L 2-1_2X2-1_2X3_16

	LC2 at 100.00% LC20 at 0.00% LC21 at 100.00% LC22 at 0.00% LC23 at 0.00% LC24 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.30 0.09 0.08 0.07 0.07 0.08 0.09 0.07 0.09 0.10 0.11 0.09 0.08 0.10 0.29 0.24	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H3-8
	LC6 at 100.00%	0.30	OK	
	LC7 at 100.00%	0.13	OK	
	LC8 at 0.00%	0.29	OK	
	LC9 at 100.00%	0.30	OK	Sec. F1
68	LC1 at 100.00%	0.25	 ОК	Eq. H3-8
00	LC10 at 100.00%	0.23	OK OK	Lq. 113-6
	LC11 at 100.00%	0.28	OK	Sec. F1
	LC12 at 100.00%	0.28	OK	
	LC13 at 100.00%	0.07	OK	
	LC14 at 100.00%	0.06	OK	
	LC15 at 100.00%	0.11	OK	
	LC16 at 0.00%	0.15	OK	
	LC17 at 100.00%	0.09	OK	
	LC18 at 100.00%	0.09	OK	
	LC19 at 100.00%	0.11	OK	
	LC2 at 0.00%	0.14	OK OK	
	LC20 at 100.00% LC21 at 100.00%	0.11 0.09	OK OK	
	LC22 at 100.00%	0.09	OK OK	
	LC23 at 100.00%	0.10	OK	
	LC24 at 100.00%	0.10	OK	
	LC25 at 0.00%	0.08	OK	
	LC26 at 100.00%	0.08	OK	
	LC27 at 100.00%	0.09	OK	
	LC28 at 100.00%	0.09	OK	
	LC29 at 0.00%	0.09	OK	
	LC3 at 0.00%	0.24	OK	
	LC30 at 0.00% LC31 at 0.00%	0.08 0.09	OK OK	
	LC32 at 0.00%	0.10	OK	
	LC4 at 0.00%	0.17	ok	
	LC5 at 100.00%	0.25	OK	
	LC6 at 0.00%	0.15	OK	
	LC7 at 0.00%	0.24	OK	
	LC8 at 0.00%	0.25	OK	
	LC9 at 0.00%	0.25	OK	
60	I C1 at 0 000/	0.40	OK	
69	LC1 at 0.00% LC10 at 100.00%	0.19 0.29	ок ок	Sec. F1
	LC10 at 100.00%	0.29	OK	360.11
	LC12 at 100.00%	0.23	OK	
	LC13 at 100.00%	0.07	OK	
	LC14 at 100.00%	0.06	OK	
	LC15 at 0.00%	0.10	OK	
	LC16 at 100.00%	0.26	OK	Sec. F1
	LC17 at 100.00%	0.09	OK	

		LC18 at 100.00%	0.10	ОК	
		LC19 at 100.00%	0.10	OK	
		LC2 at 100.00%	0.27	OK	
		LC20 at 100.00%	80.0	OK	
		LC21 at 100.00%	0.08	OK	
		LC22 at 100.00%	0.09	OK	
		LC23 at 0.00%	0.08	OK	
		LC24 at 0.00%	0.07	OK	
		LC25 at 0.00%	0.08	OK	
		LC26 at 0.00%	0.09	OK	
		LC27 at 0.00%	0.09	OK	
		LC28 at 0.00%	0.08	OK	
		LC29 at 0.00%	0.09	OK	
		LC3 at 100.00%	0.21	OK	Eq. H3-8
		LC30 at 0.00%	0.10	OK	. = =
		LC31 at 0.00%	0.10	OK	
		LC32 at 0.00%	0.09	OK	
		LC4 at 100.00%	0.14	OK	
		LC5 at 0.00%	0.19	OK	
		LC6 at 100.00%	0.26	ОК	
		LC7 at 100.00%	0.20	OK	
		LC8 at 100.00%	0.15	OK	
		LC9 at 100.00%	0.25	OK	
L 2X2X3_16	2	LC1 at 0.00%	0.17	OK	
	_	LC10 at 100.00%	0.29	OK	
					F= 110.4
		LC11 at 100.00%	0.30	OK	Eq. H2-1
		LC12 at 100.00%	0.28	OK	
		LC13 at 100.00%	0.13	OK	
		LC14 at 100.00%	0.09	OK	
		LC15 at 0.00%	0.14	OK	
		LC16 at 100.00%	0.21	OK	
		LC17 at 100.00%	0.13	OK	
		LC18 at 100.00%	0.13	OK	
		LC19 at 100.00%	0.13	OK	
		LC2 at 0.00%	0.22	OK	
		LC20 at 100.00%	0.13	OK	
		LC21 at 100.00%	0.13	OK	
		LC22 at 100.00%	0.13	OK	
		LC23 at 100.00%	0.13	OK	
		LC24 at 100.00%	0.13	OK	
		LC25 at 0.00%	0.13	OK	
		LC26 at 0.00%	0.13	OK	
		LC27 at 0.00%	0.12	OK	
		LC28 at 0.00%	0.12	OK	
		LC29 at 100.00%	0.14	OK	
		LC3 at 100.00%	0.24	ОК	
		LC30 at 100.00%	0.15	OK	
		LC31 at 100.00%	0.14	OK	
		LC32 at 100.00%	0.14	OK	
		LC4 at 100.00%	0.11	OK	
		LC5 at 0.00%	0.14	OK	
		LC6 at 0.00%	0.19	OK	
		LC7 at 100.00%	0.21	OK	
		LC8 at 50.00%	0.08	OK	
		LC9 at 100.00%	0.29	OK	
	3	LC1 at 100.00%	0.11	ОК	
	•			OK	Eq. H2-1
		LC10 at 100.00%	0.30		∟q. 112-1
		LC11 at 100.00%	0.29	OK	
		LC12 at 100.00%	0.29	OK	
		LC13 at 100.00%	0.13	OK	
		LC14 at 100.00%	0.10	OK	
		LC15 at 100.00%	0.15	OK	
			00		

	LC16 at 100.00%	0.20	OK	
	LC17 at 100.00%	0.13	OK	
	LC18 at 100.00%	0.13	OK	
	LC19 at 100.00%	0.13	OK	
	LC2 at 100.00%	0.29	OK	
	LC20 at 100.00%	0.13	OK	
	LC21 at 100.00%	0.13	OK	
	LC22 at 100.00%	0.14	OK	
	LC23 at 100.00%	0.13	OK	
	LC24 at 100.00%	0.13	OK	
	LC25 at 100.00%	0.14	OK	
	LC26 at 100.00%	0.14	OK	
	LC27 at 100.00%	0.14	OK	
	LC28 at 100.00%	0.14	OK	
	LC29 at 100.00%	0.14	OK	
	LC3 at 0.00%	0.16	OK	
	LC30 at 100.00%	0.15	OK	
	LC31 at 100.00%	0.15	OK	
	LC32 at 100.00%	0.15	OK	
	LC4 at 0.00%	0.16	OK	
	LC5 at 100.00%	0.08	OK	
	LC6 at 100.00%	0.26	OK	
	LC7 at 0.00%	0.14	OK	
	LC8 at 0.00%	0.13	OK	
	LC9 at 100.00%	0.29	ok	
	LC3 at 100.0070	0.29	OK	
	1.04.4.0.000/	0.40	014	
6	LC1 at 0.00%	0.18	OK	
	LC10 at 100.00%	0.30	OK	
	LC11 at 100.00%	0.31	OK	Eq. H2-1
	LC12 at 100.00%	0.30	OK	
	LC13 at 100.00%	0.13	OK	
	LC14 at 100.00%	0.10	OK	
	LC15 at 0.00%	0.13	OK	
	LC16 at 100.00%	0.14	OK	
	LC17 at 100.00%	0.15	OK	
	LC18 at 100.00%	0.15	ОК	
	LC18 at 100.00% LC19 at 100.00%	0.15 0.15	OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00%	0.15 0.15 0.12	OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00%	0.15 0.15 0.12 0.15	OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00%	0.15 0.15 0.12	OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00%	0.15 0.15 0.12 0.15	OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00%	0.15 0.15 0.12 0.15 0.12 0.12	OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12	OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12	OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13	OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC25 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13	OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13	OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC25 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13	OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14	OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13	OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13 0.26	OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC30 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13 0.26 0.13	OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC3 at 100.00% LC3 at 100.00% LC3 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13 0.14 0.13	OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC30 at 100.00% LC31 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13 0.26 0.13	OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC3 at 100.00% LC3 at 100.00% LC3 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.13 0.14 0.13	OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.14	OK OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC35 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.13	OK OK OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC21 at 0.00% LC21 at 0.00% LC23 at 100.00% LC24 at 0.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC31 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.13 0.15 0.09	OK OK OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.14 0.26 0.15 0.09 0.23	OK OK OK OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 0.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.13 0.15 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.14 0.26 0.15 0.09 0.23	OK OK OK OK OK OK OK OK OK OK OK OK OK	
	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 0.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.14 0.23 0.15 0.09 0.23 0.20	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC3 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 0.00% LC9 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.26 0.13 0.14 0.14 0.23 0.15 0.09 0.23 0.20 0.30	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% LC9 at 100.00% LC1 at 100.00% LC1 at 100.00% LC3 at 100.00% LC3 at 100.00% LC4 at 100.00% LC5 at 0.00% LC5 at 100.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.14 0.13 0.15 0.09 0.23 0.20 0.30	OK OK OK OK OK OK OK OK OK OK OK OK OK O	
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% LC1 at 100.00% LC1 at 100.00% LC3 at 100.00% LC3 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 0.00% LC9 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.15 0.19 0.23 0.20 0.30 0.11 0.29	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Ea ∐2 1
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% LC1 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.15 0.19 0.23 0.20 0.30 0.11 0.29 0.29	OK O	Eq. H2-1
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC4 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% LC1 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.15 0.19 0.23 0.20 0.30 0.11 0.29 0.29 0.30	OK O	Eq. H2-1 Eq. H2-1
7	LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC4 at 100.00% LC5 at 0.00% LC6 at 43.75% LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% LC1 at 100.00%	0.15 0.15 0.12 0.15 0.12 0.12 0.12 0.12 0.13 0.13 0.14 0.13 0.15 0.19 0.23 0.20 0.30 0.11 0.29 0.29	OK O	

	LC14 at 100.00%	0.09	OK	
	LC15 at 100.00%	0.15	OK	
	LC16 at 0.00%	0.13	OK	
	LC17 at 100.00%	0.14	OK	
	LC18 at 100.00%	0.14	OK	
	LC19 at 100.00%	0.15	OK	
	LC2 at 0.00%	0.16	OK	
	LC20 at 100.00%	0.15	OK	
	LC21 at 100.00%	0.13	OK	
	LC22 at 100.00%	0.13	OK	
	LC23 at 100.00%	0.14	OK	
	LC24 at 100.00%	0.14	OK	
	LC25 at 100.00%	0.14	OK OK	
	LC26 at 100.00%	0.13	OK OK	
	LC27 at 100.00%	0.13	OK	
	LC28 at 100.00%	0.13	OK	
	LC29 at 100.00%	0.12	OK	
	LC3 at 0.00%	0.18	OK	
	LC30 at 100.00%	0.12	OK	
	LC31 at 100.00%	0.13	OK	
	LC32 at 100.00%	0.13	OK	
	LC4 at 100.00%	0.28	OK	
	LC5 at 100.00%	0.08	OK	
	LC6 at 0.00%	0.13	OK	
	LC7 at 0.00%	0.15	OK	
	LC8 at 100.00%	0.25	OK	
	LC9 at 100.00%	0.28	OK	
14	LC1 at 0 000/	Λ 20	OK	
14	LC1 at 0.00%	0.28	OK	
	LC10 at 0.00%	0.29	OK	
	LC11 at 0.00% LC12 at 0.00%	0.29	OK OK	
		0.29	OK	
	LC13 at 0.00%	0.13		
	LC14 at 0.00%	0.10	OK	
	LC15 at 0.00%	0.12	OK	
	LC16 at 100.00%	0.12	OK	
	LC17 at 0.00%	0.13	OK	
	LC18 at 0.00%	0.13	OK	
	LC19 at 0.00%	0.13	OK	
	LC2 at 100.00%	0.18	OK	
	LC20 at 0.00%	0.13	OK	
	LC21 at 0.00%	0.13	OK	
	LC22 at 0.00%	0.13	OK	
	LC23 at 0.00%	0.12	OK	
	LC24 at 0.00%	0.13	OK	
	LC25 at 0.00%	0.13	OK	
	LC26 at 0.00%	0.13	OK	
	LC27 at 0.00%	0.12	OK	
	LC28 at 0.00%	0.12	OK	
	LC29 at 0.00%	0.12	OK	
	LC3 at 100.00%	0.13	OK	
	LC30 at 0.00%	0.12	OK	
	LC31 at 0.00%	0.12	OK	
	LC32 at 0.00%	0.12	OK	
	LC4 at 0.00%	0.18	OK	
	LC5 at 0.00%	0.25	OK	
	LC6 at 100.00%	0.15	OK	
	LC7 at 100.00%	0.10	OK	
	LC8 at 0.00%	0.15	OK	
	LC9 at 0.00%	0.30	OK	Eq. H2-1
15	L C1 at 0 000/	0.07		HISSOCORPOGRAPHICA CATANIP SHEEVASIARE ROU
15	LC10 at 0.00%	0.27	OK	
	LC10 at 0.00%	0.30	OK	
	LC11 at 0.00%	0.29	OK	

		LC12 at 0.00%	0.29	OK	
		LC13 at 0.00%	0.13	OK	
		LC14 at 0.00%	0.10	OK	
		LC15 at 0.00%	0.12	OK	
		LC16 at 0.00%	0.14	OK	
		LC17 at 0.00%	0.12	OK	
		LC18 at 0.00%	0.12	OK	
		LC19 at 0.00%	0.12	OK	
		LC2 at 0.00%	0.18	OK	
		LC20 at 0.00%	0.12	OK	
		LC21 at 0.00%	0.13	OK	
		LC22 at 0.00%	0.12	OK	
		LC23 at 0.00%	0.12	OK	
		LC24 at 0.00%	0.12	OK	
		LC25 at 0.00%	0.13	OK	
		LC26 at 0.00%	0.13	OK	
		LC27 at 0.00%	0.12	OK	
		LC28 at 0.00%	0.12	OK OK	
		LC29 at 0.00%	0.13	OK	
		LC3 at 100.00%	0.12	OK	
		LC30 at 0.00%	0.13	OK OK	
		LC31 at 0.00%	0.13	OK	
		LC32 at 0.00%	0.13	OK	
		LC4 at 100.00%	0.19	OK	
		LC5 at 0.00%	0.24	OK	
		LC6 at 0.00%	0.15	OK	
		LC7 at 100.00%	0.09	OK	
		LC8 at 100.00%	0.16	OK	
		LC9 at 0.00%	0.31	ОК	Eq. H2-1
5.55 6 6 45 4	=0	1.04 1.04.050/		TERESPONSIONAL CONCENSIONAL CON	
PIPE 2x0.154	52	LC1 at 81.25%	0.20	OK	
		LC10 at 81.25%	0.47	OK	
		LC11 at 81.25%	0.48	OK	
		LC12 at 81.25%	0.50	OK	Eq. H1-1b
		LC13 at 81.25%	0.15	OK	
		LC14 at 81.25%	0.11	OK	
		LC15 at 81.25%	0.13	OK	
		LC16 at 81.25%	0.43	OK	
		LC17 at 81.25%	0.17	OK	
		LC18 at 81.25%	0.16	OK	
		LC19 at 81.25%	0.16	OK	
		LC2 at 81.25%	0.13	OK	
		LC20 at 81.25%	0.17	OK	
		LC21 at 81.25%	0.15	OK	
		LC22 at 81.25%	0.14	OK	
		LC23 at 81.25%	0.14	OK	
		LC24 at 81.25%	0.15	OK	
		LC25 at 81.25%	0.14	OK	
		LC26 at 81.25%	0.13	OK	
		LC27 at 81.25%	0.14	OK	
		LC28 at 81.25%	0.14	OK	
		LC29 at 81.25%	0.21	OK	
		LC3 at 81.25%	0.22	OK	
		LC30 at 81.25%	0.20	OK	
		LC31 at 81.25%	0.21	ОК	
		LC32 at 81.25%	0.21	OK	
		LC32 at 81.25% LC4 at 81.25%	0.21 0.26	OK OK	
		LC4 at 81.25%	0.26	OK	
		LC4 at 81.25% LC5 at 81.25%	0.26 0.16	OK OK	
		LC4 at 81.25% LC5 at 81.25% LC6 at 81.25%	0.26 0.16 0.14	OK OK OK	
		LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25%	0.26 0.16 0.14 0.21	OK OK OK	
		LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25% LC8 at 81.25%	0.26 0.16 0.14 0.21 0.23	OK OK OK OK	
		LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25%	0.26 0.16 0.14 0.21	OK OK OK	
	53	LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25% LC8 at 81.25%	0.26 0.16 0.14 0.21 0.23	OK OK OK OK	

	LC10 at 81.25%	0.41	OK	
	LC11 at 81.25%	0.39	OK	
	LC12 at 81.25%	0.47	OK	
	LC13 at 81.25%	0.12	OK	
	LC14 at 81.25%	0.09	OK	
	LC15 at 81.25%	0.13	OK	
	LC16 at 81.25%	0.24	OK	
	LC17 at 81.25%	0.15	OK	
	LC18 at 81.25%	0.12	OK	
	LC19 at 81.25%	0.12	OK	
	LC2 at 81.25%	0.25	OK	
	LC20 at 81.25%	0.14	OK	
	LC21 at 81.25%	0.13	OK	
	LC22 at 81.25%	0.10	OK	
	LC23 at 81.25%	0.09	OK	
	LC24 at 81.25%	0.12	OK	
	LC25 at 81.25%	0.18	OK	
	LC26 at 81.25% LC27 at 81.25%	0.15	OK OK	
	LC27 at 81.25% LC28 at 81.25%	0.13	OK	
	LC29 at 81.25%	0.16 0.19	OK	
	LC3 at 81.25%	0.19	OK	
	LC30 at 81.25%	0.16	OK	
	LC31 at 81.25%	0.15	OK	
	LC32 at 81.25%	0.18	OK	
	LC4 at 81.25%	0.34	OK	
	LC5 at 81.25%	0.41	OK	
	LC6 at 81.25%	0.26	OK	
	LC7 at 81.25%	0.41	OK	
	LC8 at 81.25%	0.33	OK	
	LC9 at 81.25%	0.49	ОК	Eq. H1-1b
54	LC1 at 81.25%	0.47	OK	
J-1				
J-1	LC10 at 81.25%	0.51	OK	
34	LC10 at 81.25% LC11 at 81.25%	0.51 0.42	OK OK	
J 4	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25%	0.51 0.42 0.44	OK OK OK	
34	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25%	0.51 0.42 0.44 0.13	OK OK OK	
J-1	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25%	0.51 0.42 0.44 0.13 0.10	OK OK OK OK	
J-4	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14	OK OK OK OK OK	
J.	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21	OK OK OK OK OK OK	
J.	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21	OK OK OK OK OK OK OK	
J.	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC17 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19	OK OK OK OK OK OK OK OK	
J.	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC16 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16	OK OK OK OK OK OK OK OK	Ea. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC16 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC16 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC24 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC2 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC27 at 81.25% LC27 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16 0.14	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC28 at 81.25% LC28 at 81.25% LC28 at 81.25% LC28 at 81.25% LC29 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC28 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16 0.14 0.13 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC29 at 81.25% LC29 at 81.25% LC29 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16 0.14 0.13 0.10 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25% LC3 at 81.25% LC3 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16 0.14 0.13 0.10 0.11 0.17 0.47	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC29 at 81.25% LC29 at 81.25% LC29 at 81.25% LC30 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.16 0.14 0.13 0.10 0.11 0.17	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC30 at 81.25% LC31 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.47 0.15 0.12	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC30 at 81.25% LC31 at 81.25% LC32 at 81.25% LC31 at 81.25% LC32 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.47 0.15 0.12 0.13	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC30 at 81.25% LC31 at 81.25% LC30 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.15 0.12 0.13 0.25	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC33 at 81.25% LC33 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25% LC34 at 81.25% LC35 at 81.25% LC35 at 81.25% LC36 at 81.25% LC37 at 81.25% LC38 at 81.25% LC39 at 81.25% LC39 at 81.25% LC39 at 81.25% LC30 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.15 0.12 0.13 0.25 0.44	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC30 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC33 at 81.25% LC34 at 81.25% LC35 at 81.25% LC36 at 81.25% LC37 at 81.25% LC38 at 81.25% LC39 at 81.25% LC39 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC34 at 81.25% LC35 at 81.25% LC4 at 81.25% LC5 at 81.25% LC5 at 81.25% LC5 at 81.25% LC5 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.15 0.12 0.13 0.25 0.44 0.34	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC16 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC3 at 81.25% LC30 at 81.25% LC31 at 81.25% LC32 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC34 at 81.25% LC35 at 81.25% LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC6 at 81.25% LC7 at 81.25% LC7 at 81.25% LC7 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.19 0.17 0.14 0.16 0.14 0.13 0.10 0.11 0.17 0.47 0.15 0.12 0.13 0.25 0.44 0.34 0.45	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC20 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC30 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC33 at 81.25% LC34 at 81.25% LC35 at 81.25% LC36 at 81.25% LC37 at 81.25% LC38 at 81.25% LC39 at 81.25% LC39 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC34 at 81.25% LC35 at 81.25% LC4 at 81.25% LC5 at 81.25% LC5 at 81.25% LC5 at 81.25% LC5 at 81.25%	0.51 0.42 0.44 0.13 0.10 0.14 0.21 0.20 0.19 0.16 0.35 0.16 0.19 0.17 0.14 0.13 0.10 0.11 0.17 0.47 0.15 0.12 0.13 0.25 0.44 0.34	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

55	LC1 at 81.25%	0.23	OK	
			OK	Eq. H1-1b
	LC10 at 81.25%	0.53		Eq. m 1-1b
	LC11 at 81.25%	0.50	OK	
	LC12 at 81.25%	0.50	OK	
	LC13 at 81.25%	0.15	OK	
	LC14 at 81.25%	0.11	OK	
	LC15 at 81.25%	0.13	OK	
	LC16 at 81.25%	0.25	OK	
	LC17 at 81.25%	0.22	OK	
	LC18 at 81.25%	0.22	OK	
	LC19 at 81.25%	0.21	OK	
	LC2 at 81.25%	0.27	OK	
	LC20 at 81.25%	0.21	OK	
	LC21 at 81.25%	0.15	OK	
	LC22 at 81.25%	0.15	OK	
	LC23 at 81.25%	0.14	OK	
	LC24 at 81.25%	0.14	OK	
	LC25 at 81.25%	0.16	OK	
	LC26 at 81.25%	0.16	OK	
	LC27 at 81.25%	0.14	OK	
	LC28 at 81.25%	0.15	OK	
	LC29 at 81.25%	0.18	OK	
	LC3 at 81.25%	0.26	OK	
	LC30 at 81.25%	0.18	OK	
	LC31 at 81.25%	0.17	OK	
	LC32 at 81.25%	0.17	OK	
	LC4 at 81.25%	0.13	OK	
	LC5 at 81.25%	0.20	OK	
	LC6 at 81.25%	0.23	OK	
	LC7 at 81.25%	0.25	OK	
	LC8 at 81.25%	0.15	OK	
	LC9 at 81.25%	0.53	OK	
56	LC1 at 33.33%	0.41	OK	
	LC10 at 81.25%	0.51	OK	
	LC11 at 81.25%	0.46	OK	
	LC12 at 81.25%	0.48	OK	
	LC13 at 81.25%	0.15	OK	
	LC14 at 81.25%	0.11	OK	
	LC15 at 81.25%	0.20	OK	
	LC16 at 81.25%	0.11	OK	
	LC17 at 81.25%			
		0.23	OK	
	LC18 at 81.25%	0.23	OK	
	LC18 at 81.25% LC19 at 81.25%	0.23 0.21	OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25%	0.23 0.21 0.27	OK OK OK	
	LC18 at 81.25% LC19 at 81.25%	0.23 0.21	OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25%	0.23 0.21 0.27	OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25%	0.23 0.21 0.27 0.22 0.19	OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19	OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17	OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19	OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC23 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17	OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17	OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.17	OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.17	OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.17	OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.17	OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.17 0.17 0.17 0.16 0.15 0.15	OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.17 0.17 0.17 0.16 0.15 0.15 0.15	OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC29 at 81.25% LC29 at 81.25% LC30 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.17 0.17 0.17 0.16 0.15 0.15 0.23 0.15	OK OK OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.17 0.17 0.17 0.16 0.15 0.15 0.15	OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC29 at 81.25% LC29 at 81.25% LC30 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.16 0.15 0.15 0.15 0.23 0.15 0.13	OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.15 0.15 0.15 0.15 0.15 0.13 0.14	OK OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.16 0.15 0.15 0.15 0.15 0.13 0.14 0.13	OK OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.35% LC32 at 81.35% LC32 at 81.35% LC4 at 33.33% LC5 at 33.33%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.16 0.15 0.15 0.15 0.15 0.23 0.15 0.13 0.14 0.13 0.38	OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.16 0.15 0.15 0.15 0.15 0.13 0.14 0.13	OK OK OK OK OK OK OK OK OK	
	LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC29 at 81.25% LC30 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.35% LC32 at 81.35% LC32 at 81.35% LC4 at 33.33% LC5 at 33.33%	0.23 0.21 0.27 0.22 0.19 0.19 0.17 0.17 0.16 0.15 0.15 0.15 0.15 0.23 0.15 0.13 0.14 0.13 0.38	OK	

	LC8 at 33.33% LC9 at 81.25%	0.10 0.52	OK OK	Eq. H1-1b
57	LC1 at 81.25% LC10 at 81.25%	0.41 0.50	OK OK	
	LC11 at 81.25%	0.42	OK	
	LC12 at 81.25%	0.41	OK	
	LC13 at 81.25%	0.13	OK	
	LC14 at 81.25%	0.09	OK OK	
	LC15 at 81.25%	0.14	OK	
	LC16 at 81.25% LC17 at 81.25%	0.09 0.17	OK OK	
	LC18 at 81.25%	0.17	OK	
	LC19 at 81.25%	0.15	OK	
	LC2 at 81.25%	0.50	ОК	Eq. H1-1b
	LC20 at 81.25%	0.14	OK	
	LC21 at 81.25%	0.15	OK	
	LC22 at 81.25%	0.16	OK	
	LC23 at 81.25% LC24 at 81.25%	0.13 0.12	OK OK	
	LC25 at 81.25%	0.14	OK	
	LC26 at 81.25%	0.14	OK	
	LC27 at 81.25%	0.12	OK	
	LC28 at 81.25%	0.11	OK	
	LC29 at 81.25%	0.13	OK	
	LC3 at 81.25% LC30 at 81.25%	0.46 0.14	OK OK	
	LC30 at 81.25%	0.14	OK	
	LC32 at 81.25%	0.11	OK	
	LC4 at 81.25%	0.47	OK	
	LC5 at 81.25%	0.41	OK	
	LC6 at 81.25%	0.50	OK	
	LC7 at 81.25%	0.45	OK	
	LC8 at 81.25% LC9 at 81.25%	0.47 0.48	OK OK	
58	LC1 at 81.25%	0.24	OK	
	LC10 at 81.25%	0.39	OK	
	LC11 at 81.25% LC12 at 81.25%	0.44 0.45	OK OK	
	LC13 at 81.25%	0.43	OK	
	LC14 at 81.25%	0.09	OK	
	LC15 at 81.25%	0.17	OK	
	LC16 at 81.25%	0.09	OK	
	LC17 at 81.25%	0.15	OK	
	LC18 at 33.33% LC19 at 81.25%	0.15 0.18	OK OK	
	LC2 at 81.25%	0.10	OK OK	Eg. H1-1b
	LC20 at 81.25%	0.19	OK	
	LC21 at 81.25%	0.13	OK	
	LC22 at 33.33%	0.13	OK	
	LC23 at 81.25%	0.15	OK	
	LC24 at 81.25%	0.16	OK	
	LC25 at 81.25% LC26 at 81.25%	0.11 0.12	OK OK	
	LC27 at 81.25%	0.12	OK	
	LC28 at 81.25%	0.15	OK	
	LC29 at 81.25%	0.10	OK	
	LC3 at 81.25%	0.40	OK	
	LC30 at 81.25%	0.12	OK OK	
	LC31 at 81.25% LC32 at 81.25%	0.12 0.13	OK OK	
	LC4 at 81.25%	0.13	OK	
	LC5 at 81.25%	0.26	ОК	

	LC6 at 81.25%	0.58	OK	
	LC7 at 81.25%	0.38	OK	
	LC8 at 81.25%	0.46	OK	
	LC9 at 81.25%	0.37	OK	

59	LC1 at 33.33%	0.09	OK	
	LC10 at 81.25%	0.39	OK	
	LC11 at 81.25%	0.40	OK	
	LC12 at 81.25%	0.41	OK	Eq. H1-1b
	LC13 at 81.25%	0.12	OK	·
	LC14 at 81.25%	0.09	ОK	
	LC15 at 81.25%	0.14	OK	
	LC16 at 81.25%	0.15	OK	
	LC17 at 81.25%	0.16	OK	
	LC18 at 81.25%	0.15	OK	
	LC19 at 81.25%	0.18	OK	
	LC2 at 81.25%	0.25	OK	
	LC20 at 81.25%	0.18	OK	
	LC21 at 81.25%	0.13	OK	
	LC22 at 81.25%	0.12	OK	
	LC23 at 81.25%	0.15	OK	
	LC24 at 81.25%	0.15	OK	
	LC25 at 81.25%	0.11	OK	
	LC26 at 81.25%	0.12	OK	
	LC27 at 81.25%	0.13	OK	
	LC28 at 81.25%	0.13	OK	
	LC29 at 81.25%	0.11	OK	
	LC3 at 81.25%	0.30	OK	
	LC30 at 81.25%	0.13	OK	
	LC31 at 81.25%	0.12	OK	
	LC32 at 81.25%	0.11	OK	
	LC4 at 81.25%	0.37	ОК	
	LC5 at 81.25%	0.10	OK	
	LC6 at 81.25%	0.23	OK	
	LC7 at 81.25%	0.27	OK	
	LOT at 01.25%	0.27		
	LC8 at 81.25%	0.34	OK	
			OK OK	
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35	OK	
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33%	0.34 0.35 	OK OK	Es U4.4h
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45	OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43	OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43 0.38	OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43	OK OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43 0.38	OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09	OK OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15	OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% 	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31	OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11	OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11	OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11	OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11	OK	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC19 at 81.25% LC19 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC19 at 81.25% LC19 at 81.25% LC21 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.12	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.12 0.14	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.12 0.14 0.13	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC16 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.12 0.14 0.13 0.11	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.12 0.14 0.13 0.11	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC21 at 81.25% LC22 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.13	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC28 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.15	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC29 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.15 0.13	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC9 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC28 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.15	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC21 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25% LC29 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.15 0.13	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC18 at 81.25% LC19 at 81.25% LC2 at 81.25% LC2 at 81.25% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC26 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC28 at 81.25% LC29 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.12 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.15 0.17	OK O	Eq. H1-1b
60	LC8 at 81.25% LC9 at 81.25% LC1 at 33.33% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC17 at 81.25% LC19 at 81.25% LC19 at 81.25% LC21 at 81.25% LC22 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC29 at 81.25% LC29 at 81.25% LC20 at 81.25% LC21 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC28 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25% LC30 at 81.25%	0.34 0.35 0.04 0.45 0.43 0.38 0.13 0.09 0.15 0.31 0.11 0.37 0.12 0.14 0.13 0.11 0.14 0.15 0.13 0.17 0.12	OK O	Eq. H1-1b

	LC4 at 81.25% LC5 at 33.33% LC6 at 81.25%	0.23 0.03 0.34	OK OK OK	
	LC7 at 81.25%	0.21	ОК	
	LC8 at 81.25% LC9 at 81.25%	0.21	OK OK	
	LC9 at 61.25%	0.40		
61	LC1 at 81.25%	0.15	OK	
	LC10 at 81.25%	0.40	OK	
	LC11 at 81.25%	0.38	OK	
	LC12 at 81.25%	0.37	OK	
	LC13 at 81.25%	0.11	OK	
	LC14 at 81.25% LC15 at 81.25%	0.08 0.15	OK OK	
	LC16 at 81.25%	0.73	OK	
	LC17 at 81.25%	0.09	OK	
	LC18 at 81.25%	0.12	OK	
	LC19 at 81.25%	0.11	OK	
	LC2 at 81.25%	0.46	OK	
	LC20 at 81.25%	0.11	OK	
	LC21 at 81.25%	0.10	OK	
	LC22 at 81.25%	0.13	OK	
	LC23 at 81.25%	0.13	OK	
	LC24 at 81.25%	0.11	OK	
	LC25 at 81.25%	0.12	OK	
	LC26 at 81.25% LC27 at 81.25%	0.15	OK OK	
	LC27 at 81.25%	0.14 0.12	OK	
	LC29 at 81.25%	0.12	OK	
	LC3 at 81.25%	0.32	OK	
	LC30 at 81.25%	0.17	OK	
	LC31 at 81.25%	0.16	OK	
	LC32 at 81.25%	0.13	OK	
	LC4 at 81.25%	0.51	OK	Eq. H1-1b
	LC5 at 81.25%	0.17	OK	
	LC6 at 81.25%	0.44	OK	
	LC7 at 81.25%	0.29	OK OK	
	LC8 at 81.25%	0.48	OK	
	LC9 at 81.25%	0.32	OK	*********************
62	LC1 at 81.25%	0.38	OK OK	
	LC10 at 81.25% LC11 at 81.25%	0.48 0.49	OK OK	
	LC12 at 81.25%	0.56	OK	Eq. H1-1b
	LC13 at 81.25%	0.15	OK	_4
	LC14 at 81.25%	0.11	OK	
	LC15 at 81.25%	0.15	OK	
	LC16 at 81.25%	0.25	OK	
	LC17 at 81.25%	0.15	OK	
	LC18 at 81.25%	0.12	OK	
	LC19 at 81.25%	0.12	OK	
	LC2 at 81.25%	0.36	OK	
	LC20 at 81.25% LC21 at 81.25%	0.15 0.16	OK OK	
	LC21 at 81.25%	0.10	OK OK	
	LC23 at 81.25%	0.13	OK	
	LC24 at 81.25%	0.16	OK	
	LC25 at 81.25%	0.17	OK	
	LC26 at 81.25%	0.14	ОК	
	LC27 at 81.25%	0.14	OK	
	LO27 at 01.2070			
	LC28 at 81.25%	0.17	ОК	
	LC28 at 81.25% LC29 at 81.25%	0.17 0.19	OK	
	LC28 at 81.25%	0.17		

	LC31 at 81.25% LC32 at 81.25% LC4 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25% LC8 at 81.25% LC9 at 81.25%	0.16 0.19 0.43 0.35 0.37 0.34 0.39	OK OK OK OK OK OK	
63	LC1 at 81.25% LC10 at 81.25% LC11 at 81.25% LC12 at 81.25% LC13 at 81.25% LC14 at 81.25% LC15 at 81.25% LC16 at 81.25% LC16 at 81.25% LC19 at 81.25% LC2 at 33.33% LC20 at 81.25% LC21 at 81.25% LC22 at 81.25% LC23 at 81.25% LC24 at 81.25% LC25 at 81.25% LC25 at 81.25% LC26 at 81.25% LC27 at 81.25% LC27 at 81.25% LC26 at 81.25% LC27 at 81.25% LC28 at 81.25% LC30 at 81.25% LC30 at 81.25% LC4 at 81.25% LC5 at 81.25% LC5 at 81.25% LC6 at 81.25% LC7 at 81.25% LC31 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC31 at 81.25% LC32 at 81.25% LC32 at 81.25% LC32 at 81.25% LC34 at 81.25% LC55 at 81.25% LC56 at 81.25%	0.35 0.50 0.49 0.53 0.16 0.12 0.20 0.42 0.15 0.14 0.13 0.15 0.17 0.15 0.17 0.19 0.18 0.17 0.19 0.24 0.20 0.22 0.23 0.26 0.31 0.12 0.20 0.22 0.25	OK O	Eq. H1-1b
64	LC1 at 91.07% LC10 at 64.29% LC11 at 64.29% LC12 at 64.29% LC13 at 64.29% LC14 at 64.29% LC15 at 50.00% LC16 at 35.71% LC17 at 64.29% LC19 at 64.29% LC2 at 90.18% LC20 at 64.29% LC21 at 64.29% LC22 at 64.29% LC22 at 64.29% LC24 at 35.71% LC25 at 64.29% LC25 at 64.29% LC25 at 64.29% LC25 at 64.29% LC26 at 64.29% LC27 at 64.29% LC28 at 64.29% LC29 at 35.71%	0.24 0.38 0.38 0.36 0.11 0.08 0.18 0.22 0.15 0.16 0.23 0.15 0.10 0.11 0.11 0.11 0.11 0.11 0.11	OK O	Eq. H1-1b Eq. H1-1b

	LC3 at 91.07%	0.21	OK	
	LC30 at 35.71%	0.14	OK	
	LC31 at 35.71%	0.15	OK	
	LC32 at 35.71%	0.15	OK	
	LC4 at 9.82%	0.23	OK	
	LC5 at 91.07%	0.24	OK	
	LC6 at 90.18%	0.21	OK	
	LC7 at 91.07%	0.22	OK	
	LC8 at 9.82%	0.21	OK	
	LC9 at 64.29%	0.36	OK	
	LO9 at 04.29 /6	0.50	OK	
65	LC1 at 62 200/	0.24	OK	Ea U1 1b
00	LC1 at 63.39%	0.21	OK	Eq. H1-1b
	LC10 at 35.71%	0.37	OK	
	LC11 at 35.71%	0.35	OK	
	LC12 at 35.71%	0.36	OK	
	LC13 at 35.71%	0.11	OK	
	LC14 at 35.71%	0.08	OK	
	LC15 at 35.71%	0.13	OK	
	LC16 at 35.71%	0.23	OK	
	LC17 at 35.71%	0.11	OK	
	LC18 at 64.29%	0.11	OK	
	LC19 at 64.29%	0.10	OK	
	LC2 at 64.29%	0.24	OK	
	LG2 at 04.29 /0		OK	
	LC20 at 35.71%	0.10	OK	
	LC21 at 35.71%	0.12	OK	
	LC22 at 35.71%	0.11	OK	
	LC23 at 35.71%	0.10	OK	
	LC24 at 35.71%	0.11	OK	
	LC25 at 35.71%	0.13	OK	
	LC26 at 35.71%	0.12	OK	
	LC27 at 35.71%	0.11	OK	
	LC28 at 35.71%	0.12	OK	
	LO20 at 33.7 170	0.12	OK	
	LC29 at 35.71%	0.15	OK	
	LC29 at 35.71%	0.15	OK	
	LC29 at 35.71% LC3 at 90.18%	0.15 0.21	OK OK	
	LC3 at 90.18%	0.21	ОК	
	LC3 at 90.18% LC30 at 35.71%	0.21 0.14	OK OK	
	LC3 at 90.18%	0.21	ОК	
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71%	0.21 0.14 0.14	OK OK OK	
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71%	0.21 0.14 0.14 0.14	OK OK OK	
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71%	0.21 0.14 0.14	OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07%	0.21 0.14 0.14 0.14 0.21	OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39%	0.21 0.14 0.14 0.14 0.21 0.20	OK OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07%	0.21 0.14 0.14 0.14 0.21 0.20	OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29%	0.21 0.14 0.14 0.14 0.21 0.20 0.21	OK OK OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39%	0.21 0.14 0.14 0.14 0.21 0.20	OK OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20	OK OK OK OK OK OK	Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20	OK OK OK OK OK OK OK	·
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b
	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20	OK OK OK OK OK OK OK	·
££	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38	OK OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20	OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38	OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38	OK OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38	OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71% 	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39	OK OK OK OK OK OK OK OK OK OK	·
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71% 	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11 0.08	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11 0.08 0.12	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11 0.08 0.12 0.10	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11 0.08 0.12	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.37 0.39 0.11 0.08 0.12 0.10 0.15	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.37 0.39 0.11 0.08 0.12 0.10 0.15	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13	OK	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25	OK	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.28 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.25 0.14	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25	OK	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.28 0.38 0.28 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13 0.11	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13 0.11 0.12	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.13 0.25 0.14 0.13 0.11 0.12 0.12 0.12	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13 0.11 0.12	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.15 0.13 0.11 0.12 0.12 0.12 0.12 0.12	OK OK OK <	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.25 0.14 0.13 0.11 0.12 0.12 0.10 0.12 0.10 0.11	OK O	Eq. H1-1b Eq. H1-1b
66	LC3 at 90.18% LC30 at 35.71% LC31 at 35.71% LC32 at 35.71% LC4 at 91.07% LC5 at 63.39% LC6 at 64.29% LC7 at 90.18% LC8 at 91.07% LC9 at 35.71%	0.21 0.14 0.14 0.14 0.21 0.20 0.21 0.20 0.21 0.38 0.33 0.37 0.39 0.11 0.08 0.12 0.10 0.15 0.13 0.13 0.15 0.13 0.11 0.12 0.12 0.12 0.12 0.12	OK OK OK <	Eq. H1-1b Eq. H1-1b

		LC28 at 35.71%	0.12	OK	
		LC29 at 64.29%	0.11	OK	
		LC3 at 63.39%	0.24	OK	
		LC30 at 35.71%	0.09	OK	
		LC31 at 35.71%	0.11	OK	
		LC32 at 35.71%	0.12	OK	
		LC4 at 35.71%	0.29	OK	
		LC5 at 64.29%	0.26	OK	
		LC6 at 8.93%	0.25	OK	
		LC7 at 63.39%	0.24	OK	
		LC8 at 63.39%	0.27	OK	
		LC9 at 64.29%	0.37	OK	Eq. H1-1b
	_				anno de la companya
PIPE 3x0.216	9	LC1 at 56.25%	0.16	OK	Eq. H3-1
		LC10 at 44.44%	0.31	OK	Eq. H1-1b
		LC11 at 55.56%	0.31	OK	
		LC12 at 55.56%	0.32	ок	Eq. H1-1b
					Eq. 111 15
		LC13 at 55.56%	0.09	OK	
		LC14 at 55.56%	0.07	OK	
		LC15 at 56.25%	0.10	OK	
		LC16 at 43.75%	0.22	OK	
		LC17 at 56.25%			
			0.13	OK	
		LC18 at 56.25%	0.12	OK	
		LC19 at 56.25%	0.13	OK	
		LC2 at 43.75%	0.16	OK	
		LC20 at 56.25%	0.13	ОK	
		LC21 at 56.25%	0.10	OK	
		LC22 at 44.44%	0.10	OK	
		LC23 at 44.44%	0.10	OK	
		LC24 at 56.25%	0.10	OK	
		LC25 at 55.56%	0.10	OK	
		LC26 at 43.75%	0.10	OK	
		LC27 at 55.56%	0.10	OK	
		LC28 at 55.56%	0.10	OK	
		LC29 at 43.75%	0.12	OK	
					Fo. 114.45
		LC3 at 56.25%	0.18	OK	Eq. H1-1b
		LC30 at 43.75%	0.12	OK	
		LC31 at 43.75%	0.12	OK	
		LC32 at 43.75%	0.12	OK	
		LC4 at 56.25%	0.17	ОK	
		LC5 at 56.25%	0.16	OK	
		LC6 at 43.75%	0.15	OK	
		LC7 at 56.25%	0.17	OK	
		LC8 at 56.25%	0.15	OK	
		LC9 at 55.56%	0.30	OK	

	10	LC1 at 56.25%	0.19	OK	
		LC10 at 55.56%	0.31	OK	
		LC11 at 55.56%	0.30	OK	
		LC12 at 55.56%	0.31	OK	
		LC13 at 55.56%	0.09	OK	
		LC14 at 55.56%	0.07	OK	
		LC15 at 44.44%	0.13	OK	
		LC16 at 43.75%	0.22	OK	
		LC17 at 55.56%	0.09	OK	
		LC18 at 44.44%	0.09	OK	
		LC19 at 44.44%	0.09	OK	
		LC2 at 43.75%	0.20	OK	
		LC20 at 55.56%	0.08	OK	
		LC21 at 44.44%	0.09	OK	
		LC22 at 44.44%	0.10	OK	
		LC23 at 44.44%	0.10	OK	
		LC24 at 44.44%	0.09	OK	
		LC25 at 44.44%	0.11	OK	
		LUZU at 44.4470	V. 1 I	OK.	

		LC26 at 44.44%	0.11	OK	
		LC27 at 44.44%	0.11	OK	
		LC28 at 44.44%	0.10	OK	
		LC29 at 44.44%	0.12	OK	
		LC3 at 43.75%	0.17	OK	
		LC30 at 44.44%	0.12	OK	
		LC31 at 44.44%	0.12	OK	
		LC32 at 44.44%	0.12	OK	
		LC4 at 56.25%	0.18	OK	
		LC5 at 56.25%	0.17	OK	
		LC6 at 43.75%	0.18	OK	
		LC7 at 43.75%	0.15	OK	
		LC8 at 56.25%	0.16	OK	
		LC9 at 55.56%	0.32	OK	Eq. H1-1b

	11	LC1 at 43.75%	0.19	OK	
	• •				Fo. 114.4b
		LC10 at 43.75%	0.30	OK	Eq. H1-1b
		LC11 at 56.25%	0.30	OK	Eq. H1-1b
		LC12 at 55.56%	0.30	OK	Eq. H1-1b
		LC13 at 44.44%	0.09	OK	-4
		LC14 at 44.44%	0.07	OK	
		LC15 at 55.56%	0.13	OK	
		LC16 at 55.56%	0.07	OK	
		LC17 at 55.56%	0.12	OK	
		LC18 at 55.56%	0.12	OK	
		LC19 at 55.56%	0.12	OK	
		LC2 at 43.75%	0.19	ОК	
		LC20 at 55.56%	0.12	OK	
		LC21 at 55.56%	0.11	OK	
		LC22 at 55.56%	0.10	OK	
		LC23 at 55.56%	0.11	OK	
		LC24 at 55.56%	0.11	OK	
		LC25 at 55.56%	0.09	OK	
		LC26 at 55.56%	0.09		
		LUZD AL DOLDOM	0.09	OK	
		LC27 at 55.56%	0.10	OK	
		LC27 at 55.56%	0.10		
		LC27 at 55.56% LC28 at 55.56%	0.10 0.10	OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44%	0.10 0.10 0.08	OK OK	
		LC27 at 55.56% LC28 at 55.56%	0.10 0.10	OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44%	0.10 0.10 0.08	OK OK OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56%	0.10 0.10 0.08 0.19 0.08	OK OK OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56%	0.10 0.10 0.08 0.19 0.08 0.09	OK OK OK OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56%	0.10 0.10 0.08 0.19 0.08 0.09	OK OK OK OK OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56%	0.10 0.10 0.08 0.19 0.08 0.09	OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25%	0.10 0.10 0.08 0.19 0.08 0.09 0.09	OK OK OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17	OK OK OK OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17	OK OK OK OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17	OK OK OK OK OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17	OK OK OK OK OK OK OK	Eq. H1-1b
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC8 at 56.25%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.17	OK OK OK OK OK OK OK OK	
		LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b
DI 6Y1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC8 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK	
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC8 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK	Eq. H1-1b
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC8 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK	
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC8 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03 0.03 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03 0.03 0.09 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03 0.03 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03 0.03 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1
PL 6X1/2	25	LC27 at 55.56% LC28 at 55.56% LC29 at 44.44% LC3 at 56.25% LC30 at 55.56% LC31 at 55.56% LC32 at 55.56% LC4 at 56.25% LC5 at 43.75% LC6 at 43.75% LC7 at 56.25% LC9 at 44.44%	0.10 0.10 0.08 0.19 0.08 0.09 0.20 0.17 0.17 0.18 0.31 0.06 0.12 0.13 0.12 0.03 0.02 0.05 0.10 0.03 0.03 0.03 0.03 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b Eq. H3-1 Eq. H3-1

	LC24 at 0.00% LC25 at 50.00% LC26 at 50.00% LC27 at 50.00% LC28 at 50.00% LC29 at 50.00% LC3 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 46.88% LC5 at 50.00% LC6 at 46.88% LC7 at 0.00% LC8 at 46.88% LC7 at 0.00%	0.03 0.04 0.04 0.04 0.05 0.08 0.05 0.05 0.05 0.09 0.06 0.09 0.08 0.09 0.12	OK OK OK OK OK OK OK OK OK OK OK	
26	LC1 at 0.00%	0.07	OK	
	LC10 at 50.00% LC11 at 50.00%	0.13 0.14	ок ок	Eq. H3-1
	LC12 at 0.00%	0.14	OK	Eq. H3-1
	LC13 at 0.00%	0.03	OK	Eq. 110-1
	LC14 at 0.00%	0.02	OK	
	LC15 at 0.00%	0.05	OK	
	LC16 at 50.00%	0.04	OK	
	LC17 at 0.00%	0.05	OK	
	LC18 at 50.00%	0.05	OK	
	LC19 at 50.00%	0.05	OK	
	LC2 at 50.00%	0.09	OK	
	LC20 at 0.00%	0.05	OK	
	LC21 at 0.00% LC22 at 0.00%	0.05 0.04	OK OK	
	LC23 at 50.00%	0.04	OK	
	LC24 at 0.00%	0.05	OK	
	LC25 at 0.00%	0.04	OK	
	LC26 at 50.00%	0.03	OK	
	LC27 at 50.00%	0.04	OK	
	LC28 at 0.00%	0.04	OK	
	LC29 at 0.00%	0.03	OK	
	LC3 at 50.00%	0.09	OK	
	LC30 at 50.00%	0.03	OK	
	LC31 at 50.00% LC32 at 50.00%	0.04	OK OK	
	LC4 at 50.00%	0.03 0.09	OK	Eq. H1-1b
	LC5 at 46.88%	0.03	OK	Eq. (11-16
	LC6 at 50.00%	0.09	ок	
	LC7 at 50.00%	0.09	OK	
	LC8 at 50.00%	0.09	OK	
	LC9 at 0.00%	0.13	OK	
27	LC1 at 50.00%	0.09	OK	Eq. H1-1b
	LC10 at 0.00%	0.14	OK	Eq. H3-1
	LC11 at 0.00%	0.12	OK	
	LC12 at 50.00%	0.13	OK	Eq. H3-1
	LC13 at 0.00%	0.03	OK	
	LC14 at 0.00%	0.02	OK	
	LC15 at 0.00%	0.02	OK	
	LC16 at 0.00%	0.03	OK	
	LC17 at 50.00% LC18 at 0.00%	0.03 0.03	OK OK	
	LC18 at 0.00%	0.03 0.03	OK	
	LC2 at 0.00%	0.03	OK	
	LC20 at 50.00%	0.03	OK	
	LC21 at 50.00%	0.03	OK	

LC22 at 0.00%	0.03	OK
LC23 at 0.00%	0.03	OK
LC24 at 50.00%	0.03	OK
LC25 at 0.00%	0.03	OK
LC26 at 0.00%	0.03	OK
LC27 at 0.00%	0.03	OK
LC28 at 50.00%	0.03	OK
LC29 at 0.00%	0.03	OK
LC3 at 50.00%	0.09	OK
LC30 at 0.00%	0.03	OK
LC31 at 0.00%	0.03	OK
LC32 at 50.00%	0.03	OK
LC4 at 50.00%	0.09	OK
LC5 at 50.00%	0.09	OK
LC6 at 0.00%	0.09	OK
LC7 at 50.00%	0.09	OK
LC8 at 50.00%	0.09	OK
LC9 at 0.00%	0.13	OK



Current Date: 8/30/2018 5:35 PM

Units system: English

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Geometry data

GLOSSARY

Cb22, Cb33 Moment gradient coefficients

Cm22, Cm33 Coefficients applied to bending term in interaction formula d0 Tapered member section depth at J end of member DJX Rigid end offset distance measured from J node in axis X DJY Rigid end offset distance measured from J node in axis Y DJZ Rigid end offset distance measured from J node in axis Z DKX Rigid end offset distance measured from K node in axis X DKY Rigid end offset distance measured from K node in axis Y DKZ : Rigid end offset distance measured from K node in axis Z dL Tapered member section depth at K end of member

Ig factor : Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members

K22 : Effective length factor about axis 2
K33 : Effective length factor about axis 3

L22 : Member length for calculation of axial capacity
L33 : Member length for calculation of axial capacity

LB pos : Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg : Lateral unbraced length of the compression flange in the negative side of local axis 2

RX : Rotation about X
RY : Rotation about Y
RZ : Rotation about Z

TO :1 = Tension only member 0 = Normal member

TX : Translation in X
TY : Translation in Y
TZ : Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
2	-0.7253	0.00	0.00	0
3	-6.0833	0.00	0.00	0
4	-6.25	0.00	0.00	0
5	-6.3333	0.00	-0.433	0
6	-6.5833	0.00	-0.866	0
7	-3.7376	0.00	-5.2176	0
8	-3.9043	0.00	-5.5062	0
9	-0.892	0.00	-0.2887	0
10	-6.6667	0.00	-0.7217	0
11	-3.179	0.00	-6.7625	0
12	-2.8457	0.00	-6.7625	0
13	-0.50	0.00	-11.4027	0
14	-0.4167	0.00	-11.547	0
17	0.7253	0.00	0.00	0
18	6.0833	0.00	0.00	0
19	6.25	0.00	0.00	0
20	6.3333	0.00	-0.433	0
21	6.5833	0.00	-0.866	0
22	3.7376	0.00	-5.2176	0
23	3.9043	0.00	-5.5062	0
24	0.892	0.00	-0.2887	0
25	6.6667	0.00	-0.7217	0

26	3.179	0.00	-6.7625	0
28	0.50	0.00	-11.4027	0
29	0.4167	0.00	-11.547	0
32	0.00	0.00	-11.4027	0
51	5.1136	5.00	0.05	0
53	-5.1136	5.00	0.05	0
63	5.1136	-1.00	0.05	0
67	-5.1136	-1.00	0.05	0
69	0.9427	0.00	-3.5453	0
70	0.00	0.00	-5.1781	0
72	1.7046	5.00	0.05	0
73	-1.7046	5.00	0.05	0
82	1.7046	-1.00	0.05	0
83	-1.7046	-1.00	0.05	0
122	6.1428	5.00	-1.7318	0
123	4.4383	5.00	-4.6842	0
124	2.7337	5.00	-7.6365	0
125	1.0292	5.00	-10.5889	0
126	6.1428	-1.00	-1.7318	0
127	4.4383	-1.00	-4.6842	0
128	2.7337	-1.00	-7.6365	0
130	-6.1428	5.00	-1.7318	0
131	-4.4383	5.00	-4.6842	0
132	-2.7337	5.00	-7.6365	0
133	-1.0292	5.00	-10.5889	0
134	-6.1428	-1.00	-1.7318	0
135	-4.4383	-1.00	-4.6842	0
136	-2.7337	-1.00	-7.6365	0
137	-1.0292	-1.00	-10.5889	0
170	-6.25	3.00	0.00	0
171	6.25	3.00	0.00	0
172	-6.6667	3.00	-0.7217	0
173	-0.4167	3.00	-11.547	0
174	0.4167	3.00	-11.547	0
175	6.6667	3.00	-0.7217	0
176	0.50	3.00	-11.4027	0
177	-0.50	3.00	-11.4027	0
178	6.0833	3.00	0.00	0
179	6.5833	3.00	-0.866	0
180	-6.5833	3.00	-0.866	0
181	-6.0833	3.00	0.00	0
71	-0.9427	0.00	-3.5453	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
69	1	1		1		1
70	1	1	1	1	1	1
71	1	1	1	1	1	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	5	71		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
2	5	9		L 2X2X3_16	A36	0.00	0.00	0.00
3	5	7		L 2X2X3_16	A36	0.00	0.00	0.00
4	8	2		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
5	20	69		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
6	20	24		L 2X2X3_16	A36	0.00	0.00	0.00
7	20	22		L 2X2X3_16	A36	0.00	0.00	0.00
8	23	17		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
10	10	14		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
11	29	25		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
12	70	32		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
13	11	26		HSS_SQR 4X4X1_4	A500 GrB rectangular		0.00	0.00
14	27	32		L 2X2X3_16	A36	0.00	0.00	0.00
15	12	32		L 2X2X3_16	A36	0.00	0.00	0.00
25	6	3		PL 6X1/2	A36	0.00	0.00	0.00
26	18	21		PL 6X1/2	A36	0.00	0.00	0.00
27	28	13		PL 6X1/2	A36	0.00	0.00	0.00
52	53	67		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
53	73	83		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
54	72	82		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
55	51	63		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
56	122	126		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	123	127		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
58	124	128		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
59	125	129		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	133	137		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
61	132	136		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
62	131	135		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
63	130	134		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
64	170	171		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
65	172	173		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
66	174	175		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
67	176	177		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
68	178	179		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
69	180	181		L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
9	4	19		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
2	270.00	0	0.00	0.00	0.00
4	180.00	0	0.00	0.00	0.00
7	270.00	0	0.00	0.00	0.00
8	90.00	0	0.00	0.00	0.00
13	90.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
67	270.00	0	0.00	0.00	0.00
68	270.00	0	0.00	0.00	0.00
69	270.00	0	0.00	0.00	0.00

Rigid end offsets

Member	DJX	DJY	DJZ	DKX	DKY	DKZ
	[in]	[in]	[in]	[in]	[in]	[in]
52	0.00	0.00	2.00	0.00	0.00	2.00
53	0.00	0.00	2.00	0.00	0.00	2.00
54	0.00	0.00	2.00	0.00	0.00	2.00
55	0.00	0.00	2.00	0.00	0.00	2.00
56	1.7188	0.00	-1.00	1.7188	0.00	-1.00
57	1.7188	0.00	-1.00	1.7188	0.00	-1.00
58	1.7188	0.00	-1.00	1.7188	0.00	-1.00
59	1.7188	0.00	-1.00	1.7188	0.00	-1.00
60	-1.7188	0.00	-1.00	-1.7188	0.00	-1.00
61	-1.7188	0.00	-1.00	-1.7188	0.00	-1.00
62	-1.7188	0.00	-1.00	-1.7188	0.00	-1.00
63	-1.7188	0.00	-1.00	-1.7188	0.00	-1.00