December 2, 2014

## VIA EMAIL AND OVERNIGHT DELIVERY

Ms. Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

## RE: Sprint Spectrum, L.P. - Notice of Exempt Modification 302 Ball Pond Road, New Fairfield, CT

Dear Ms. Bachman:
This letter and attachments are submitted on behalf of Sprint Spectrum, L.P. ("Sprint"). Sprint is undertaking modifications to certain existing sites in its Connecticut network in order to implement updated technology. In order to do so, Sprint will modify antenna and equipment configurations at a number of existing sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the First Selectman of the Town of New Fairfield.

Sprint plans to modify the existing facility at 302 Ball Pond Road owned by the Town of New Fairfield (coordinates $41^{\circ} 27^{\prime} 53.2^{\prime \prime} \mathrm{N},-73^{\circ} 29^{\prime} 49^{\prime \prime} \mathrm{W}$ ). Attached are drawings depicting the planned changes, and documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration. Also included is a power density calculation reflecting the modification to Sprint's operations at the site.

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will be unaffected. Sprint proposes to replace three (3) existing CDMA antennas with three (3) new NV antennas, add three (3) new 2.5 GHz antennas and nine (9) new remote radio heads, all at a centerline height of approximately $70^{\prime}$ above the tower base. Additionally, Sprint will remove all existing CDMA coax cables and install three (3) hybriflex cables and one (1) fiber cable.
2. The proposed changes will not extend the site boundaries. Sprint will replace existing CDMA cabinets with two (2) BBU cabinets, and install one (1) new BTS cabinet and one (1) new fiber distribution box inside the existing equipment shelter. Thus, there will be no effect on the site compound or Sprint's leased area.
3. The proposed changes will not increase the noise level at the existing facility by six decibels or more. The incremental effect of the proposed changes will be negligible.
4. The changes to the facility will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site. As indicated in the attached power density calculations, Sprint's operations at the site will result in a power density of $2.53 \%$; the combined site operations will result in a total power density of $56.92 \%$.

Please feel free to call me with any questions or concerns regarding this matter. Thank you for your consideration.

Respectfully submitted,


## Attachments

cc: Susan Chapman, First Selectman, Town of New Fairfield



environmental | engineering | due diligence

# RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT 

Sprint Existing Facility

Site ID: CT72XC045
Ball Pond Road
302 Ball Pond Road
New Fairfield, CT 06812
August 12, 2014

EBI Project Number: 62144194

August 12, 2014

Sprint
Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495
Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:
CT72XC045-Ball Pond Road
Site Total: $\mathbf{5 6 . 9 2 \%}$ - MPE \% in full compliance
EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 302 Ball Pond Road, New Fairfield, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm} 2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limit for the cellular band ( 850 MHz Band) is approximately $567 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the 1900 MHz and 2500 MHz bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 302 Ball Pond Road, New Fairfield, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

1) 3 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
6) The antennas used in this modeling are the RFS APXVSPP18-C-A20, The POWERWAVE P40-16-XLPP-RR-A and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The POWERWAVE P40-16-XLPP-RR-A has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz . The RFS APXVTM14-C-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz . The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antenna mounting height centerline for the proposed antennas is $\mathbf{1 5 5}$ feet above ground level (AGL).
8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

|  | Site ID | CT72XC045-Ball Pond Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Site Addresss | 302 Ball Pond Road, New Fairfield, CT, 06812 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Site Type | Monopole |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Sector 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Antenna Number | Antenna Make | Antenna Model | Radio Type | Frequency Band | Technology | Power Out Per Channel (Watts) | Number of Channels | Composite Power | $\begin{array}{\|c} \text { Antenna Gain } \\ \text { (10 db } \\ \text { reduction) } \end{array}$ | Antenna Height (ft) | analysis height | Cable Size | $\begin{array}{\|c\|} \hline \text { Cable Loss } \\ \text { (dB) } \end{array}$ | Additional Loss (dB) | ERP | Power <br> Density <br> Percentage |
| 1a | RFS | APXVSPP18-C-A20 | RRH | 1900 MHz | CDMA / LTE | 20 | 3 | 60 | 5.9 | 155 | 149 | $1 / 2^{\prime \prime}$ | 0.5 | 0 | 208.04 | 0.34\% |
| 1a | RFS | APXVSPP18-C-A20 | RRH | 850 MHz | CDMA / LTE | 20 | 1 | 20 | 3.4 | 155 | 149 | $1 / 2{ }^{\prime \prime}$ | 0.5 | 0 | 39.00 | 0.11\% |
| 1B | RFS | APXVTMM14-C-120 | RRH | 2500 MHz | CDMA / LTE | 20 | 2 | 40 | 5.9 | 155 | 149 | 1/2" | 0.5 | 0 | 138.69 | 0.40\% |
| Sector total Power Density Value: $0.84 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Sector 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Antenna Number | Antenna Make | Antenna Model | Radio Type | Frequency Band | Technology | Power Out Per Channel (Watts) | Number of Channels | Composite Power | $\begin{array}{\|c} \text { Antenna Gain } \\ (10 \mathrm{db} \\ \text { reduction }) \end{array}$ | Antenna Height (ft) | analysis height | Cable Size | Cable Loss <br> (dB) | Additional Loss (dB) | ERP |  |
| 2a | Powerwave | P40-16-XLPP-RR-A | RRH | 1900 MHz | CDMA / LTE | 20 | 3 | 60 | 5.9 | 155 | 149 | 1/2" | 0.5 | 0 | 208.04 | 0.34\% |
| 2 a | Powerwave | P40-16-XLPP-RR-A | RRH | 850 MHz | CDMA / LTE | 20 | 1 | 20 | 3.4 | 155 | 149 | $1 / 2{ }^{\prime \prime}$ | 0.5 | 0 | 39.00 | 0.11\% |
| 2 B | RFS | APXVTMM14-C-120 | RRH | 2500 MHz | CDMA / LTE | 20 | 2 | 40 | 5.9 | 155 | 149 | 1/2" | 0.5 | 0 | 138.69 | 0.40\% |
| Sector total Power Density Value: $0.84 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Sector 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Antenna Number | Antenna Make | Antenna Model | Radio Type | Frequency Band | Technology | Power <br> Out Per <br> Channel <br> (Watts) | Number of Channels | Composite Power | $\begin{array}{\|c} \text { Antenna Gain } \\ (10 \mathrm{db} \\ \text { reduction }) \end{array}$ | Antenna Height (ft) | analysis height | Cable Size | Cable Loss <br> (dB) | Additional Loss (dB) | ERP | Power <br> Density <br> Percentage |
| 3 a | Powerwave | P40-16-XLPP-RR-A | RRH | 1900 MHz | CDMA / LTE | 20 | 3 | 60 | 5.9 | 155 | 149 | $1 / 2^{\prime \prime}$ | 0.5 | 0 | 208.04 | 0.34\% |
| 3 a | Powerwave | P40-16-XLPP-RR-A | RRH | 850 MHz | CDMA / LTE | 20 | 1 | 20 | 3.4 | 155 | 149 | 1/2" | 0.5 | 0 | 39.00 | 0.11\% |
| 3B | RFS | APXVTMM14-C-120 | RRH | 2500 MHz | CDMA / LTE | 20 | 2 | 40 | 5.9 | 155 | 149 | 1/2 " | 0.5 | 0 | 138.69 | 0.40\% |
|  |  |  |  |  |  |  |  |  |  |  |  | Sector to | tal Power D | ensity Value: | 0.84\% |  |


| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| Sprint | $2.53 \%$ |
| Town | $2.16 \%$ |
| Town PD | $1.37 \%$ |
| Town FD | $2.10 \%$ |
| Nextel | $3.17 \%$ |
| Clearwire | $1.08 \%$ |
| AT\&T | $18.14 \%$ |
| T-Mobile | $0.16 \%$ |
| Verizon Wireless | $26.21 \%$ |
|  |  |
| Total Site MPE \% | $\mathbf{5 6 . 9 2 \%}$ |

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## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are $\mathbf{2 . 5 3 \%}$ ( $\mathbf{0 . 8 4 \%}$ from sector $\mathbf{1 , 0 . 8 4 \%}$ from sector $\mathbf{2}$ and $\mathbf{0 . 8 4 \%}$ from sector 3) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{5 6 . 9 2 \%}$ of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

RF Engineering Director

EBI Consulting
21 B Street
Burlington, MA 01803

# STRUCTURAL ANALYSIS REPORT 175’ MONOPOLE TOWER NEW FAIRFIELD, CONNECTICUT 

Prepared for<br>HPC Wireless Services

## Sprint Site \#CT72XC045

July 30, 2014


APT Project \#CT255852

# STRUCTURAL ANALYSIS REPORT <br> 175' MONOPOLE TOWER NEW FAIRFIELD, CONNECTICUT <br> prepared for <br> HPC Wireless Services 

## EXECUTIVE SUMMARY:

All-Points Technology Corporation, P.C. (APT) performed a structural analysis of this 175foot monopole tower located in New Fairfield, Connecticut. The analysis was performed for Sprint's proposed removal of nine existing DB844H90 panel antennas and addition of six panel antennas and nine remote radio heads (RRHs) on the existing mounts at 155 ', fed by four 11/4" hybrid fiber/power cables.

Our analysis indicates the tower meets the requirements of the Connecticut State Building Code and EIA/TIA-222 with the proposed equipment changes.

## INTRODUCTION:

A structural analysis of this communications tower was performed by APT for HPC Wireless Services. The tower is located at 302 Ball Pond Road in New Fairfield, Connecticut. This analysis relied on information provided by others, which included a tower mapping by WesTower Communications dated July 18, 2014, equipment changes proposed by Sprint, Fred A. Nudd Corporation tower drawings, and base plate reinforcement drawings prepared by Vertical Structures, Inc.

The analysis was conducted with the following antenna inventory (proposed equipment shown in bold text):

| Carrier | Antenna | Elev. | Mount | Coax. |
| :---: | :---: | :---: | :---: | :---: |
| Town | (4) PD-220 omnidirectional whips, 1' square panel, 2.5 ' dish with radome | 175' | 13' low-profile platform | (4) 1-5/8", (2) 1/2" |
| Sprint | (2) RR65-18-02DTR, (1) RR45-19-02DPL, <br> (1) APXVSPP18-C-A20, (2) P40-16-XLPP-RR, <br> (3) APXVTM14-G120 panels, (9) RRHs | 155' | 13' low-profile platform | (4) 1-1/4" hybrid |
| T-Mobile | (6) AIR21 B2A-B4P panels, (3) TMAs ${ }^{2}$ | 145’ | (3) 10' T-arms | (18) 1-5/8", <br> (1) hybrid |
| AT\&T | (6) 7770.00, (3) P65-17-XLH-RR, (6) TMAs, (6) Diplexers, (6) RCU, (6) RRHs, (1) surge suppressor | 135' | (3) 10' T-arms | (12) 1-5/8", fiber \& (2) power in conduit |
| Verizon | (6) BXA-171085/12, (6) LPA-80080/6, <br> (3) BXA-70063/6, (3) RRHs, (1) surge suppressor ${ }^{3}$ | 125' | 13' low-profile platform | (18) $1-5 / 8^{\prime \prime}$, <br> (1) hybrid |
| Unknown | PD-220 omnidirectional whip | 100' | 4' standoff | 1-5/8" |
| Unknown | GPS antenna | 85' | (3) 2' standoffs | (3) $1 / 2$ " |

All-Points Technology Corporation, P.C.
${ }^{1}$ Two RR65-18-02DTR, one RR45-19-02DPL, and nine DB844H90 panels currently installed, fed by nine $7 / 8$ " and six $1-5 / 8^{\prime \prime}$ lines.
${ }^{2}$ Three APX16DWV-16DWV panels, three RR65-18-02DPL panels, and nine TMAs currently installed. Larger AIR21 B2A-B4P panels used for analysis.
${ }^{3}$ Six LPA-80080/6 panels, three BXA-171085/12 panels, three BXA-70063/6 panels, three RRHs, and one surge suppressor currently installed, fed by twelve 1-5/8" lines.

## STRUCTURAL ANALYSIS:

## Methodology:

The structural analysis was done in accordance with the Connecticut State Building Code and TIA/EIA-222, Revision F (TIA), Structural Standards for Steel Antenna Towers and Antenna Supporting Structures.

The analysis was conducted using a fastest mile wind speed of 85 mph (equivalent to 100 mph 3 -second gust) and one-half inch of radial ice over the structure and associated appurtenances. The TIA Standard requires a basic wind speed of 85 miles per hour for Fairfield County, Connecticut.

Two loading conditions were evaluated in accordance with TIA/EIA-222-F to determine tower capacity. The more demanding of the two cases is used to calculate tower capacity:

- Case $1=$ Wind Load (without ice) + Tower Dead Load
- Case $2=0.75$ Wind Load (with ice) + Ice Load + Tower Dead Load

The TIA/EIA standard permits a one-third increase in allowable stresses for towers less than 700 -feet tall. Allowable stresses of tower members were increased by one-third when computing the tower capacity values shown below.

## Analysis Results:

The following table summarizes the usage capacity of the pole:

| Elevation | Capacity |
| :---: | :---: |
| $130^{\prime}-175^{\prime}$ | $32 \%$ |
| $85^{\prime}-130^{\prime}$ | $65 \%$ |
| $41^{\prime}-85^{\prime}$ | $70 \%$ |
| $0^{\prime}-41^{\prime}$ | $82 \%$ |

The existing base plate was evaluated from Vertical Structures, Inc. base plate reinforcement drawings. Base plate reinforcement was conducted in 2005 for an overturning moment

## All-Points Technology Corporation, P.C.

reaction of 4370 ft -kips; calculated overturning moment with the proposed equipment changes is only 3920 ft -kips. The existing base plate is adequate to support the proposed loads.

The existing reinforced concrete mat and pier foundation was evaluated from Fred A. Nudd Corporation design drawings. We found the existing foundation is adequately sized to support the proposed equipment changes. Base reactions imposed with the proposed changes were calculated to be as follows:

Compression: $\quad 48.0$ kips
Total Shear:
Overturning Moment:
33.7 kips
$3920 \mathrm{ft}-\mathrm{kips}$

## CONCLUSIONS AND SUGGESTIONS:

As detailed above, our analysis indicates that the existing 175' Nudd monopole tower and foundation in New Fairfield, Connecticut meet the requirements of the Connecticut State Building Code and EIA/TIA-222 with the equipment changes proposed by Sprint.

## LIMITATIONS:

This report is based on the following:

1. Tower is properly installed and maintained.
2. All members are in an undeteriorated condition.
3. All bolts are in place and are properly tightened.
4. Tower is in plumb condition.
5. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
6. Record drawings accurately reflect tower dimensions and height.

All-Points Technology Corporation, P.C. (APT) is not responsible for any modifications completed prior to or hereafter which APT is not or was not directly involved. Modifications include but are not limited to:

1. Adding or relocating antennas.
2. Installing antenna mounting gates or side arms.
3. Extending tower.

APT hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon the information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact APT. APT disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

## All-Points Technology Corporation, P.C.

## Appendix A

Tower Schematic

|  |
| ---: | :--- |



## Appendix B

Photographs


Overview photo of $175^{\prime}$ monopole tower.


Photo showing existing antennas on upper tower.


Photos of existing Sprint platform \& antennas from above.


Photos taken by WesTower Communications on July 18, 2014.


Photos of existing Sprint antennas on platform at 155'.


## Appendix C

Calculations

| tnxTower <br> All-Points Technology Corporation <br> 116 Grandview Road <br> Conway, NH 03818 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Job | 175' Monopole Tower | $\begin{array}{ll} \text { Page } \\ & 1 \text { of } 7 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | CT255802 New Fairfield | $\begin{aligned} & \text { Date } \\ & \text { 14:48:41 07/30/14 } \end{aligned}$ |
|  | Client | HPC; Sprint Site \#CT72XC045 | Designed by Rob Adair |

## Tower Input Data

This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in Fairfield County, Connecticut.
Basic wind speed of 85 mph .
Nominal ice thickness of 0.5000 in.
Ice density of 56 pcf
A wind speed of 74 mph is used in combination with ice.
Deflections calculated using a wind speed of 50 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.
Tapered Pole Section Geometry

| Section | Elevation <br> ft | Section Length $f t$ | Splice <br> Length <br> ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175.00-130.00 | 45.00 | 5.00 | 18 | 24.0000 | 34.9000 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | 130.00-85.00 | 50.00 | 6.00 | 18 | 33.1889 | 45.3000 | 0.3125 | 1.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | 85.00-41.00 | 50.00 | 7.00 | 18 | 43.2217 | 55.3328 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 41.00-0.00 | 48.00 |  | 18 | 52.8872 | 64.5139 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

Feed Line/Linear Appurtenances

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& Allow Shield \& Component Type \& Placement
ft \& \multicolumn{2}{|l|}{Total Number} \& \(C_{A} A_{A}\)

$f t^{2} / f t$ \& Weight
plf <br>
\hline \multirow[t]{2}{*}{$15 / 8$} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{175.00-6.00} \& \multirow[t]{2}{*}{4} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{2}{*}{1/2} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{175.00-6.00} \& \multirow[t]{2}{*}{2} \& No Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.25 <br>
\hline \multirow[t]{2}{*}{$15 / 8$} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{145.00-6.00} \& \multirow[t]{2}{*}{18} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{4}{*}{1.57" Hybrid fiber-power cable $15 / 8$} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{145.00-6.00} \& \multirow[t]{2}{*}{1} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{135.00-6.00} \& \multirow[t]{2}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{2}{*}{1.34" fiber cable} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{135.00-6.00} \& \multirow[t]{2}{*}{1} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline \multirow[t]{2}{*}{5/8 power} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{135.00-6.00} \& \multirow[t]{2}{*}{2} \& No Ice \& 0.00 \& 0.40 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.40 <br>
\hline \multirow[t]{2}{*}{$15 / 8$} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{125.00-6.00} \& \multirow[t]{2}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{2}{*}{$15 / 8$} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{125.00-8.00} \& \multirow[t]{2}{*}{6} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{2}{*}{1.57" Hybrid fiber-power cable} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{No} \& \multirow[t]{2}{*}{Inside Pole} \& \multirow[t]{2}{*}{125.00-6.00} \& \multirow[t]{2}{*}{1} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline Safety Line 3/8 \& C \& No \& CaAa (Out Of \& 175.00-0.00 \& 1 \& No Ice \& 0.04 \& 0.22 <br>
\hline \& \& \& Face) \& \& \& 1/2" Ice \& 0.14 \& 0.75 <br>
\hline 1/2 \& C \& No \& Inside Pole \& 85.00-6.00 \& 3 \& No Ice \& 0.00 \& 0.25 <br>
\hline
\end{tabular}

| tnxTower <br> All-Points Technology Corporation <br> 116 Grandview Road Conway, NH 03818 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Job | 175' Monopole Tower | $\begin{array}{ll} \text { Page } \\ & 2 \text { of } 7 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Client | HPC; Sprint Site \#CT72XC045 | Designed by Rob Adair |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Allow Shield \& Component Type \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& Total Number \& \& \(C_{A} A_{A}\)

$f t^{2} / f t$ \& | Weight |
| :--- |
| plf | <br>

\hline \multirow{3}{*}{$15 / 8$} \& \multirow{3}{*}{C} \& \multirow{3}{*}{No} \& \multirow{3}{*}{Inside Pole} \& \multirow{3}{*}{100.00-6.00} \& \multirow{3}{*}{1} \& 1/2" Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline 1-1/4" Hybrid \& C \& No \& Inside Pole \& 155.00-6.00 \& 4 \& No Ice \& 0.00 \& 0.66 <br>
\hline fiber-power cable \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline
\end{tabular}

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
o
\end{tabular} \& Placement

$f t$ \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight <br>

\hline \multirow[t]{3}{*}{1' square panel} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{175.00} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& 1.40 \& 0.35 \& 15.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \multirow[t]{2}{*}{1.56} \& \multirow[t]{2}{*}{0.45} \& \multirow[t]{2}{*}{22.91} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5$ ' omni whip} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{175.00} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& 5.00 \& 5.00 \& 50.00 <br>

\hline \& \& \& -4.50 \& \& \& \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{86.96} <br>
\hline \& \& \& 10.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5$ ' omni whip} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{175.00} \& \multirow[t]{3}{*}{No Ice
1/2" Ice} \& 5.00 \& 5.00 \& 50.00 <br>
\hline \& \& \& 3.00 \& \& \& \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{86.96} <br>
\hline \& \& \& 10.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5$ " omni whip} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{175.00} \& \multirow[t]{3}{*}{No Ice 1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 5.00 \\
& 7.03
\end{aligned}
$$} \& 5.00 \& 50.00 <br>

\hline \& \& \& -4.50 \& \& \& \& \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{86.96} <br>
\hline \& \& \& 10.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{$20^{\prime} \times 2.5$ " omni whip} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{175.00} \& No Ice \& 5.00 \& 5.00 \& 50.00 <br>

\hline \& \& \& 4.50 \& \& \& \multirow[t]{2}{*}{1/2" Ice} \& \multirow[t]{2}{*}{$$
7.03
$$} \& \multirow[t]{2}{*}{7.03} \& \multirow[t]{2}{*}{86.96} <br>

\hline \& \& \& 10.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{2}{*}{15' low-profile platform} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{None} \& \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{175.00} \& \multirow[t]{2}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 10.50 \\
& 11.71
\end{aligned}
$$

\]} \& 9.10 \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 1400.00 \\
& 2386.45
\end{aligned}
$$
\]} <br>

\hline \& \& \& \& \& \& \& \& 10.15 \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14-ALU-120} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& No Ice \& 6.90 \& 3.61 \& 60.00 <br>
\hline \& \& \& 0.00 \& \& \& \multirow[t]{2}{*}{1/2" Ice} \& \multirow[t]{2}{*}{7.35} \& \multirow[t]{2}{*}{3.97} \& \multirow[t]{2}{*}{99.53} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14-ALU-120} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice

1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 6.90 \\
& 7.35
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 3.61 \\
& 3.97
\end{aligned}
$$
\]} \& 60.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{99.53} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14-ALU-120} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice
1/2'Ice} \& 6.90 \& 3.61 \& 60.00 <br>
\hline \& \& \& 0.00 \& \& \& \& \multirow[t]{2}{*}{7.35} \& \multirow[t]{2}{*}{3.97} \& \multirow[t]{2}{*}{99.53} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{APXVSPP18-C-A20} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice $1 / 2$ " Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 8.26 \\
& 8.81
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 5.28 \\
& 5.74
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 107.00 \\
& 156.52
\end{aligned}
$$
\]} <br>

\hline \& \& \& $$
0.00
$$ \& \& \& \& \& \& <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{P40-16-XLPP-RR-A} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice $1 / 2$ " Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 10.50 \\
& 10.98
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 3.52 \\
& 3.87
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{gathered}
48.00 \\
101.23
\end{gathered}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{P40-16-XLPP-RR-A} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice

1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 10.50 \\
& 10.98
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 3.52 \\
& 3.87
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{gathered}
48.00 \\
101.23
\end{gathered}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{RR65-18-02DP} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 4.36 \\
& 4.77
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 1.97 \\
& 2.31
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 18.00 \\
& 40.42
\end{aligned}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RR65-18-02DP} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 4.36 \\
& 4.77
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 1.97 \\
& 2.31
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 18.00 \\
& 40.42
\end{aligned}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RR45-19-02DPL4} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{No Ice

1/2" Ice} \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 5.60 \\
& 5.99
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 2.09 \\
& 2.39
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 23.00 \\
& 51.55
\end{aligned}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{2}{*}{TD-RRH8x20-25} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{From Face} \& 4.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{$$
155.00
$$} \& \multirow[t]{2}{*}{No Ice 1/2" Ice} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 4.72 \\
& 5.01
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 1.70 \\
& 1.92
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{gathered}
75.00 \\
102.14
\end{gathered}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline
\end{tabular}

| tnxTower <br> All-Points Technology Corporation 116 Grandview Road Conway, NH 03818 Phone: (603) 496-5853 FAX: (603) 447-2124 | Job | 175' Monopole Tower | Page 3 of 7 |
| :---: | :---: | :---: | :---: |
|  | Project | CT255802 New Fairfield | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:48:41 07/30/14 } \end{array}$ |
|  | Client | HPC; Sprint Site \#CT72XC045 | Designed by Rob Adair |



| tnxTower <br> All-Points Technology Corporation 116 Grandview Road Conway, NH 03818 Phone: (603) 496-5853 FAX: (603) 447-2124 | Job | 175' Monopole Tower | $\begin{array}{ll} \hline \text { Page } & \\ & 4 \text { of } 7 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | CT255802 New Fairfield | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:48:41 07/30/14 } \end{array}$ |
|  | Client | HPC; Sprint Site \#CT72XC045 | Designed by Rob Adair |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\) Side
\[
f t^{2}
\] \& Weight

$l b$ <br>

\hline \multirow{4}{*}{P65-17-XLH-RR panel} \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Face} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{135.00} \& \multirow[b]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& \multirow[b]{3}{*}{\[

$$
\begin{aligned}
& 11.47 \\
& 12.08
\end{aligned}
$$

\]} \& \multirow[b]{3}{*}{\[

$$
\begin{aligned}
& 6.80 \\
& 7.38
\end{aligned}
$$

\]} \& \multirow[b]{3}{*}{\[

$$
\begin{gathered}
60.00 \\
122.06
\end{gathered}
$$
\]} <br>

\hline \& \& \& 4.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Face} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{135.00} \& \multirow[b]{3}{*}{| No Ice |
| :--- |
| 1/2" Ice |} \& \multirow[b]{3}{*}{11.47

12.08} \& \multirow[b]{3}{*}{6.80

7.38} \& \multirow{4}{*}{$$
\begin{gathered}
60.00 \\
122.06
\end{gathered}
$$} <br>

\hline \multirow[t]{3}{*}{P65-17-XLH-RR panel} \& \& \& 4.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{135.00} \& \multirow{4}{*}{No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$} \& \multirow{4}{*}{\[

$$
\begin{aligned}
& 2.94 \\
& 3.17
\end{aligned}
$$

\]} \& \multirow{4}{*}{\[

$$
\begin{aligned}
& 1.19 \\
& 1.35
\end{aligned}
$$
\]} \& <br>

\hline \multirow[t]{3}{*}{(2) Ericsson RRUS-11} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \& \& \& \& \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 55.00 \\
& 74.32
\end{aligned}
$$} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) Ericsson RRUS-11} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 2.94 \\
& 3.17
\end{aligned}
$$
\]} \& \multirow[t]{3}{*}{1.19

1.35} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 55.00 \\
& 74.32
\end{aligned}
$$} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) Ericsson RRUS-11} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice 1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 2.94 \\
& 3.17
\end{aligned}
$$} \& 1.19 \& 55.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \multirow[t]{2}{*}{1.35} \& \multirow[t]{2}{*}{74.32} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Raycap DC6-48 surge suppressor} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$} \& \multirow[t]{3}{*}{1.19

1.37} \& \multirow[t]{3}{*}{1.19
1.37} \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{44.34} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(2) 7770.00} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2$ " Ice} \& \multirow[t]{3}{*}{5.88
6.31} \& \multirow[t]{3}{*}{2.93
3.27} \& 35.00 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{67.63} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) 7770.00} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& \multirow[t]{3}{*}{$$
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& 5.88 \\
& 6.31
\end{aligned}
$$} \& \multirow{3}{*}{2.93

3.27} \& 35.00 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{67.63} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) 7770.00} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice 1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 5.88 \\
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\begin{aligned}
& 35.00 \\
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\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) LGP2140X TMA} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice 1/2" Ice} \& $$
1.26
$$ \& 0.38 \& 20.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \multirow[t]{2}{*}{$$
1.42
$$} \& \multirow[t]{2}{*}{0.49} \& \multirow[t]{2}{*}{27.13} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) LGP2140X TMA} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& \multirow[t]{3}{*}{\[
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\begin{aligned}
& 1.26 \\
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\begin{aligned}
& 20.00 \\
& 27.13
\end{aligned}
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\hline \multirow[t]{3}{*}{(2) LGP2140X TMA} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice

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1 / 2^{\prime \prime} \text { Ice }
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\]} \& 20.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{27.13} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{Dual band TMA} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 0.71 \\
& 0.83
\end{aligned}
$$

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$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 15.00 \\
& 20.03
\end{aligned}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{Dual band TMA} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 0.71 \\
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\begin{aligned}
& 15.00 \\
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\hline \multirow[t]{3}{*}{Dual band TMA} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice 1/2" Ice} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& 0.71 \\
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& 0.41 \\
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\begin{aligned}
& 15.00 \\
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\]} <br>

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\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(2) 7020.00 RET-RCU} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 0.40 \\
& 0.49
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 0.12 \\
& 0.17
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 5.00 \\
& 7.94
\end{aligned}
$$
\]} <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) 7020.00 RET-RCU} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2$ " Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 0.40 \\
& 0.49
\end{aligned}
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\begin{aligned}
& 0.12 \\
& 0.17
\end{aligned}
$$
\]} \& 5.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{7.94} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) 7020.00 RET-RCU} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{135.00} \& \multirow[t]{3}{*}{No Ice $1 / 2$ " Ice} \& \multirow[t]{3}{*}{\[
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\begin{aligned}
& 0.40 \\
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\begin{aligned}
& 0.12 \\
& 0.17
\end{aligned}
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\]} \& 5.00 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& \multirow[t]{2}{*}{7.94} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{2}{*}{$10^{\prime} \mathrm{T}$-arm} \& \multirow[t]{2}{*}{A} \& None \& \& 0.0000 \& 135.00 \& No Ice \& 2.67 \& 2.67 \& 150.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 3.36 \& 3.36 \& 547.19 <br>
\hline 10' T-arm \& B \& None \& \& 0.0000 \& 135.00 \& No Ice \& 2.67 \& 2.67 \& 150.00 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 3.36 \& 3.36 \& 547.19 <br>
\hline
\end{tabular}

| tnxTOWer | Job | Page | 175' Monopole Tower |
| :---: | :--- | :---: | :--- |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ | Azimuth Adjustment <br> 0 | Placement |  | $C_{A} A_{A}$ Front <br> $f t^{2}$ | $C_{A} A_{A}$ Side $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $10^{\prime}$ T-arm | C | None |  | 0.0000 | 135.00 | No Ice | 2.67 | 2.67 | 150.00 |
|  |  |  |  |  |  | 1/2" Ice | 3.36 | 3.36 | 547.19 |
| (2) LPA-80080/6 | A | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.32 | 9.10 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 4.76 | 9.65 | 73.26 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) LPA-80080/6 | B | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.32 | 9.10 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 4.76 | 9.65 | 73.26 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) LPA-80080/6 | C | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.32 | 9.10 | 25.00 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime} \text { Ice }$ | $4.76$ | 9.65 | 73.26 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) BXA-171085/12 | A | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.79 | 3.62 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.24 | 4.06 | 52.45 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) BXA-171085/12 | B | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.79 | 3.62 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.24 | 4.06 | 52.45 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) BXA-171085/12 | C | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 4.79 | 3.62 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.24 | 4.06 | 52.45 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| BXA-70063/6 | A | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 7.73 | 3.76 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 8.27 | 4.19 | 65.60 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| BXA-70063/6 | B | From Face | 4.00 | 0.0000 | 125.00 |  | 7.73 | 3.76 | $25.00$ |
|  |  |  | 0.00 |  |  | 1/2" Ice | 8.27 | 4.19 | $65.60$ |
|  |  |  | 0.00 |  |  |  |  |  |  |
| BXA-70063/6 | C | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 7.73 | 3.76 | 25.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 8.27 | 4.19 | 65.60 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| ALU RRH2x40-AWS | A | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 2.52 | 1.59 | 45.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.75 | 1.80 | 62.40 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| ALU RRH2x40-AWS | B | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 2.52 | 1.59 | 45.00 |
|  |  |  | 0.00 |  |  | 1/2' Ice | 2.75 | 1.80 | 62.40 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| ALU RRH2x40-AWS | C | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 2.52 | 1.59 | 45.00 |
|  |  |  | 0.00 |  |  | 1/2' Ice | 2.75 | 1.80 | 62.40 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) RFS FD9R6004_2C-3L diplexer | A | From Face | 4.00 | 0.0000 | 125.00 | No Ice | $0.37$ | $0.08$ | $5.00$ |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime} \text { Ice }$ | $0.45$ | $0.14$ | $7.30$ |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) RFS FD9R6004_2C-3L diplexer | B | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 0.37 | 0.08 | 5.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.45 | 0.14 | 7.30 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| (2) RFS FD9R6004_2C-3L diplexer | C | From Face | 4.00 | 0.0000 | 125.00 | No Ice | 0.37 | 0.08 | 5.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.45 | 0.14 | 7.30 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| Raycap RDC-4276-PF-48 <br> J-box | C | None |  | 0.0000 | 125.00 | No Ice | 6.69 | 2.70 | 35.00 |
|  |  |  |  |  |  | 1/2" Ice | 7.03 | 2.95 | 76.97 |
| 13' low-profile platform | C | None |  | 0.0000 | 125.00 | No Ice | 9.10 | 7.88 | 1100.00 |
|  |  |  |  |  |  | 1/2" Ice | 10.15 | 8.79 | 1848.74 |
| $20^{\prime} \times 2.5{ }^{\prime \prime}$ omni whip | A | From Face | 3.00 | 0.0000 | 120.00-100.00 | No Ice | 5.00 | 5.00 | 50.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 7.03 | 7.03 | 86.96 |
|  |  |  | 0.00 |  |  |  |  |  |  |
| 3' x 4" standoff | A | None | 2.00 | 0.0000 | 100.00 | No Ice | 1.40 | 0.16 | 40.00 |
|  |  |  |  |  |  | 1/2" Ice | 1.66 | 0.21 | 51.31 |
| GPS on 2' standoff | A | From Leg |  | 0.0000 | 85.00 | No Ice | 0.60 | 0.60 | 50.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.79 | 0.79 | 55.81 |
|  |  |  | 0.00 |  |  |  |  |  |  |



## Solution Summary

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection | Gov. <br> Load | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | in | Comb. | $\circ$ | $\circ$ |
| L1 | $175-130$ | 18.167 | 11 | 1.4103 | 0.0081 |
| L2 | $135-85$ | 8.558 | 11 | 1.2755 | 0.0033 |
| L3 | $91-41$ | 2.421 | 11 | 0.8790 | 0.0015 |
| L4 | $48-0$ |  | 11 | 0.4577 | 0.0006 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 175.00 | 2.5' dish with radome | 11 | 30.167 | 1.4103 | 0.0081 | 69407 |
| 155.00 | APXV9TM14-ALU-120 | 11 | 24.318 | 1.3637 | 0.0052 | 17351 |
| 145.00 | (2) AIR 21 B2A B4P panel | 11 | 21.480 | 1.3274 | 0.0040 | 11567 |
| 135.00 | P65-17-XLH-RR panel | 11 | 18.745 | 1.2755 | 0.0033 | 8774 |
| 125.00 | (2) LPA-80080/6 | 11 | 16.146 | 1.2045 | 0.0028 | 7782 |
| 120.00 | $20^{\prime} \times 2.5$ " omni whip | 11 | 14.903 | 1.1629 | 0.0025 | 7402 |
| 115.00 | $20^{\prime} \times 2.5$ " omni whip | 11 | 13.701 | 1.1181 | 0.0023 | 7057 |
| 110.00 | $20^{\prime}$ x 2.5 " omni whip | 11 | 12.542 | 1.0707 | 0.0021 | 6742 |
| 105.00 | $20^{\prime} \times 2.5$ " omni whip | 11 | 11.426 | 1.0214 | 0.0019 | 6455 |
| 100.00 | $20^{\prime} \times 2.5$ " omni whip | 11 | 10.358 | 0.9709 | 0.0017 | 6190 |
| 85.00 | GPS on 2' standoff | 11 | 7.451 | 0.8184 | 0.0013 | 5590 |


| tnxTower <br> All-Points Technology Corporation <br> 116 Grandview Road Conway, NH 03818 <br> Phone: (603) 496-5853 <br> FAX: (603) 447-2124 | Job | 175' Monopole Tower | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | CT255802 New Fairfield | $\begin{array}{\|l\|l\|} \hline \text { Date } \\ \text { 14:48:41 07/30/14 } \end{array}$ |
|  | Client | HPC; Sprint Site \#CT72XC045 | Designed by Rob Adair |

## Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ \quad l b \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 175-130 | Pole | TP34.9x24x0.25 | 1 | -12854.80 | 168772.46 | 32.1 | Pass |
| L2 | 130-85 | Pole | TP45.3x33.1889x0.3125 | 2 | -19322.00 | 465528.90 | 64.7 | Pass |
| L3 | 85-41 | Pole | TP55.3328x43.2217x0.375 | 3 | -31806.30 | 1023046.80 | 69.5 | 晉 阁 |
| L4 | 41-0 | Pole | TP64.5139x52.8872x0.375 | 4 | -47943.20 | 1784513.69 | 82.2 | Pass |
|  |  |  |  |  |  | Pole (L4) RATING = | $\begin{gathered} \text { Summary } \\ 82.2 \\ \mathbf{8 2 . 2} \\ \hline \end{gathered}$ | Pass <br> Pass |

