

QC Development
PO Box 916
Storrs, CT 06268
860-670-9068
Mark.Roberts@QCDevelopment.net

September 14, 2018

Melanie A. Bachman Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Notice of Exempt Modification – New Cingular Wireless PCS, LLC (AT&T) – CT1160 35 Wildwood Street, New Britain, CT 06051 N 41.66861111 W 72.75583333

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the 114-foot level of the existing 110-foot Monopole Tower at 35 Wildwood Street, New Britain, CT. The tower is owned by AT&T and the property is owned by The City of New Britain. AT&T now intends to remove (3) existing Powerwave antennas and replace them with (3) new Kathrein 800-10798 antennas. AT&T will also install (3) Ericsson RRUS-32 and (3) 4426-B66 Remote Radio Units (RRU). These Antennas and Remote Radio Units (RRU) will also be installed at the 114-foot level of the tower.

This facility was proposed as a 110' monopole replacement of an existing 60' light stanchion and was approved by the City of New Britain on August 11, 2004. The Siting Council acknowledged the City's jurisdiction in Petition # 703 on March 3, 2005. Since no change is proposed to the overall tower height, this modification complies with the aforementioned approval.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Honorable Erin E. Stewart, Mayor of the City of New Britain, as elected official and property owner and to the new Britain Zoning Staff.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Please feel free to call me at (860) 670-9068 with any questions regarding this matter. Thank you for your consideration.

Sincerely,

Mark Roberts

QC Development

Consultant for AT&T

Attachments

cc: Mayor Erin E. Stewart - as Elected Official & Property Owner David Zajac- Zoning Enforcement Officer

Power Density

Existing Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%МРЕ
Other Carriers*							12.81%
AT&T GSM	1	283	114	0.0087	880	0.5867	0.15%
AT&T GSM	2	875	114	0.0540	1900	1.0000	0.54%
AT&T UMTS	2	565	114	0.0348	880	0.5867	0.59%
AT&T UMTS	4	525	114	0.0647	1900	1.0000	0.65%
AT&T LTE	1	1313	114	0.0412	734	0.4893	0.84%
Site Total							15.58%

^{*}Per CSC Records (available upon request, includes calculation formulas)

Proposed Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%МРЕ
Other Carriers*							12.81%
AT&T UMTS	1	270	114	0.0083	850	0.5867	0.15%
AT&T UMTS	1	411	114	0.0127	1900	1.0000	0.13%
AT&T LTE	1	1476	114	0.0455	700	0.4667	0.98%
AT&T LTE / 5G	2	1000	114	0.0617	850	0.5667	1.09%
AT&T LTE	2	3664	114	0.2259	1900	1.0000	2.26%
AT&T LTE	1	3837	114	0.1183	2100	1.0000	1.18%
AT&T LTE	1	1285	114	0.0396	2300	1.0000	0.40%
Site Total							18.99%

^{*}Per CSC Records (available upon request, includes calculation formulas)

^{**} If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

^{**} If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

PROJECT INFORMATION

ITEMS TO BE MOUNTED ON THE EXISTING MONOPOLE

- NEW AT&T ANTENNAS: (800-10798) MOUNTED @ POSITION 3 (TYP. OF 1 PER SECTOR, TOTAL OF 3)
- NEW AT&T RRUS 32 (WCS) MOUNTED @ POSITION 3 (TYP. OF 1 PER SECTOR, TOTAL
- NEW AT&T RRUS 4426 B66 (AWS) MOUNTED @ POSITION 3 (TYP. OF 1 PER SECTOR,
- EXISTING AT&T ANTENNAS: (AM-X-CD-17-65-00T-RET) MOUNTED @ POSITION 3 (TYP. OF 1 PER SECTOR, TOTAL OF 3) TO BE RELOCATED @ POSITION 4.
- EXISTING AT&T ANTENNAS: (7000) MOUNTED @ POSITION 4 (TYP. OF 1 PER SECTOR, TOTAL OF 3) TO BE REMOVED
- INSTALL (1) SQUID
- INSTALL (1) FIBER CABLE
- INSTALL (2) DC CABLES
- INSTALL (6) LOW BAND COMBINERS (DBC0061F1V51-2)

ITEMS TO BE MOUNTED AT EQUIPMENT LOCATION:

- ADD (3) 850 4478 B5 RRH'S. WITH (12) SURGE PROTECTORS.
- SWAP BBU WITH RBS5216.
- ADD NEW POWER PLANT.
- REPLACE GSM COMPONENTS WITH (DBC0061F1V51-2) LOW BAND COMBINERS.

•(6) ANTENNAS, (6) RRU'S, (6) TMA'S, (1) SURGE ARRESTOR, (12) COAX CABLES, (2) DC POWER & (1) FIBER.

SQUID ALARMING (NOT TO BE DAISY CHAINED).

- •THE 1ST SQUID INSTALLED WILL BE ALARMED TO THE LOWEST BAND (OR FIRST INSTALLED RRH/RRU ON THE ALPHA SECTOR, IN THE EVENT THE ALARM CABLE CANNOT BE CONNECTED TO ALPHA IT WILL BE ACCEPTABLE TO ALARM TO THE CLOSEST PHYSICAL SECTOR ON AN EXCEPTION BASIS.
- 2ND SQUID INSTALLED WILL BE ALARMED TO THE LOWEST BAND (OR FIRST INSTALLED) RRH/RRU ON THE BETA SECTOR.
- 3RD SQUID INSTALLED WILL BE ALARMED TO THE LOWEST BAND (OR FIRST INSTALLED) RRH/RRU ON THE GAMMA SECTOR.

SITE ADDRESS:

WILDWOOD ST

NEW BRITAIN, CT 06051

LATITUDE: 41.668186 N, 41° 40′ 05.46″ N LONGITUDE: 72.755198 W, 72° 45' 18.71" W TYPE OF SITE: MONOPOLE / INDOOR EQUIPMENT

STRUCTURE HEIGHT: 111'±

RAD CENTER: 113'± & 114'±

CURRENT USE: TELECOMMUNICATIONS FACILITY PROPOSED USE: TELECOMMUNICATIONS FACILITY

DRAWING INDEX

SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	1
GN-1	GENERAL NOTES	1
A-1	COMPOUND & EQUIPMENT PLAN	1
A-2	ANTENNA LAYOUTS & ELEVATION	1
A-3	DETAILS	1
SN-1	STRUCTURAL NOTES	1
S-1	STRUCTURAL DETAILS	1
G-1	GROUNDING DETAILS	1
RF-1	RF PLUMBING DIAGRAM	1



SITE NUMBER: CT1160

SITE NAME: NEW BRITAIN WILDWOOD ST

FA CODE:10050945

PACE ID: MRCTB031100, MRCTB031559, MRCTB031241

PROJECT: LTE 3C/4C/5C 2018 UPGRADE

VICINITY MAP

DIRECTIONS TO SITE:

START OUT GOING NORTHEAST ON ENTERPRISE DR TOWARD CAPITAL BLVD 0.3 MI. TURN LEFT ONTO CAPITAL BLVD 0.3 MI. TURN LEFT ONTO WEST ST 0.3 MI. TURN LEFT TO MERGE ONTO I-91 S TOWARD NEW HAVEN 1.8 MI. TAKE EXIT 22N TO MERGE ONTO CT-9 N TOWARD NEW BRITAIN 5.5 MI TAKE EXIT 25 FOR ELLIS ST 0.3 MI. TURN RIGHT ONTO ELLIS ST 0.3 MI. TAKE THE 3RD LEFT ONTO EAST ST 0.6 MI. TURN RIGHT ONTO BELDEN ST 0.5 MI. TAKE THE 2ND LEFT ONTO WILDWOOD ST. DESTINATION WILL BE ON THE RIGHT



GENERAL NOTES

- THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
- 2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
- CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
- CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

72 HOURS

BEFORE YOU DIG CALL TOLL FREE 1 - 800 - 922 - 4455or call 811

UNDERGROUND SERVICE ALERT



NORTH ANDOVER, MA 01845

TEL: (978) 557-5553 FAX: (978) 336-5586

12 INDUSTRIAL WAY SALEM, NH 03079

SITE NUMBER: CT1160 SITE NAME: NEW BRITAIN WILDWOOD ST

> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY



1							DE STATE OF		
						*		*======================================	AT&T
1	08/28/18	ISSUED FOR	CONSTRUCTION	M	R AT		ulf C	con	TITLE SHEET
Α	06/28/18	ISSUED FOR	REVIEW	CI	- AT	DJC	POPLENSY		(LTE 3C/4C/5C)
Ю.	DATE		REVISIONS	B,	CHI	APP'D	11,55/ONAL END	SITE NUMBER	DRAWING NUMBER
SCA	LE: AS SH	HOWN	DESIGNED BY: AT	DRAWN B	Y: CF	•	"Millinn"	CT1160	T-1

GROUNDING NOTES

- 1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
- 2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- 4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS FOUIPMENT
- 5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
- 6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- 7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- 8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR
- 9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS
- 10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- 11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- 12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250,50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) OWNER - AT&T MOBILITY

- 2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
- 3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE
- 4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE
- 5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON
- 6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
- 7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
- 9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
- 10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
- 11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
- 13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

- 14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
- 15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
- 16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
- 17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS
- 19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
- 20. APPLICABLE BUILDING CODES:

SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

BUILDING CODE: IBC 2012 WITH 2016 CT STATE BUILDING CODE AMENDMENTS ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE:

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-G, STRUCTURAL STANDARDS FOR STEEL

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL. METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

			ABBREVIATIONS		
AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
втсм	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	Р	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD J. CR
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		E SO SE ECT TO



NORTH ANDOVER, MA 01845



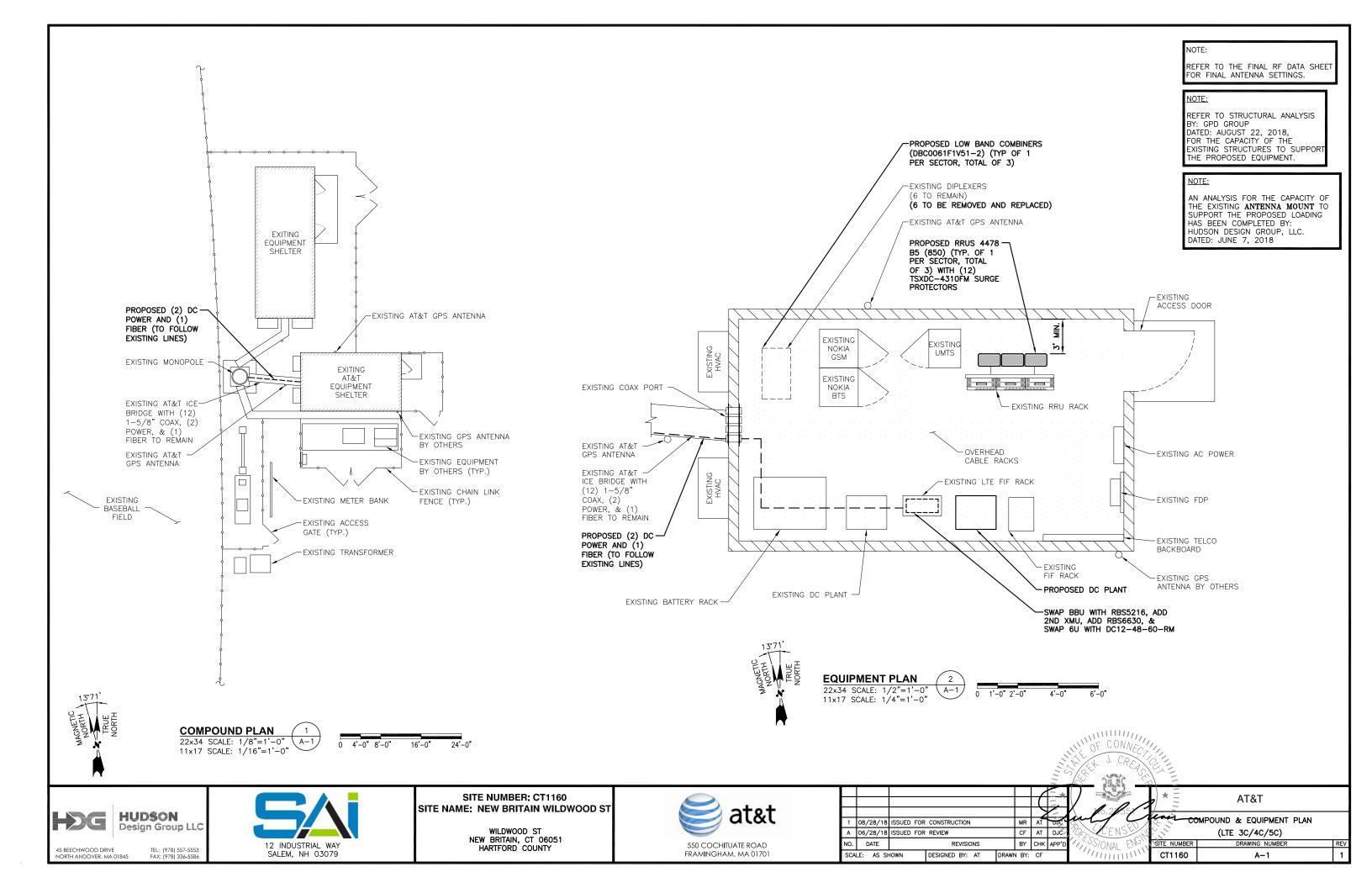
SITE NUMBER: CT1160 SITE NAME: NEW BRITAIN WILDWOOD ST

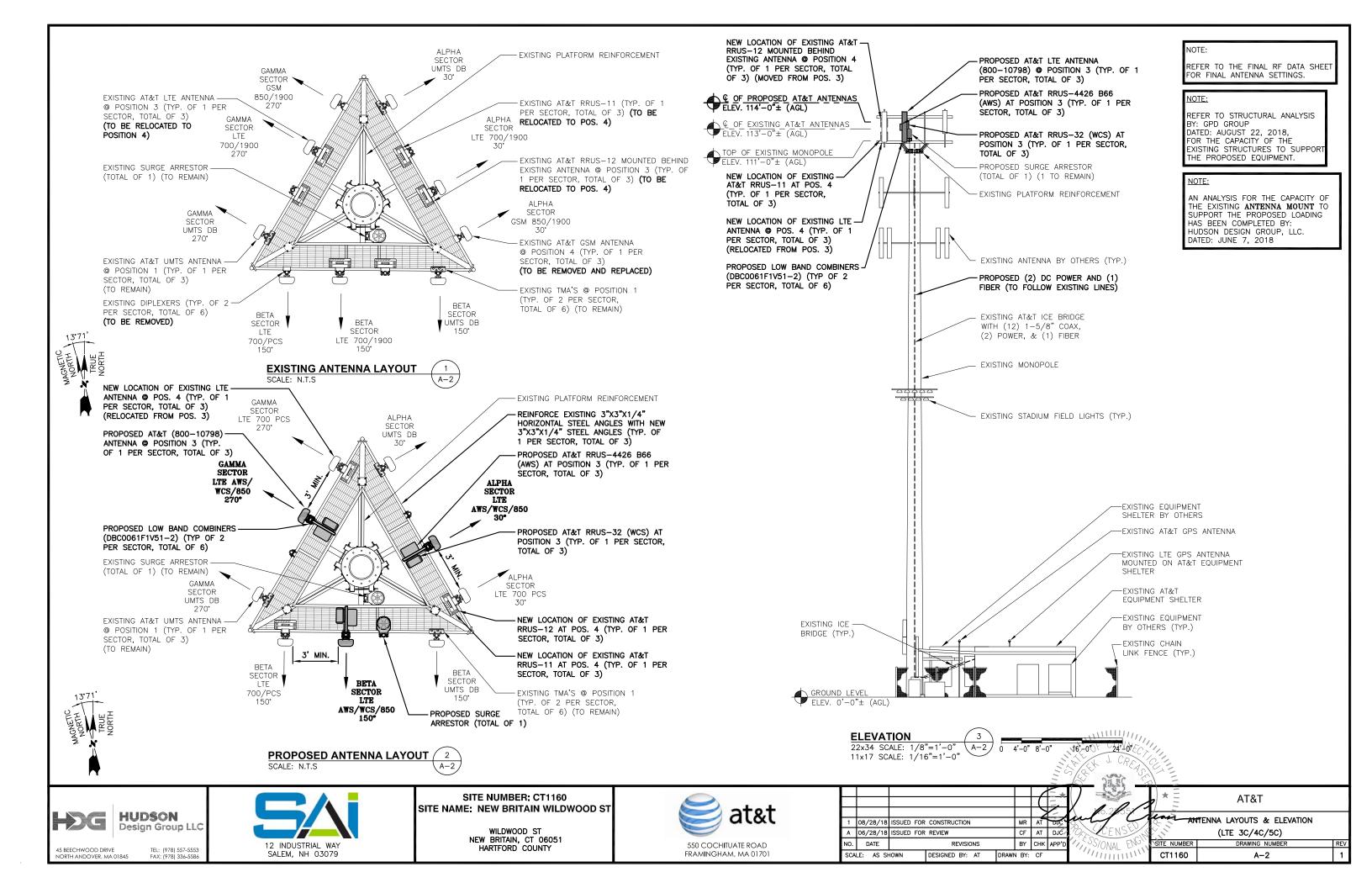
> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY



FRAMINGHAM, MA 0170

KEF	REF	ERENCE					1	18	Dr. EC	70	\ =	
						(*	\mathcal{I}	1.05		*==	AT&T
1	08/28/18	ISSUED FOR	CONSTRUCTION		MR	AT	DOC	in		5/	ear _	- GENERAL NOTES
Α	06/28/18	ISSUED FOR	REVIEW		CF	AT	DJC	19/2	CENS			(LTE 3C/4C/5C)
NO.	DATE		REVISIONS		BY	СНК	APP'D	11,5	S/ONAL EN	10), [SITE NUMBER	DRAWING NUMBER
SCA	LE: AS SI	HOWN	DESIGNED BY: AT	DRAWN	N BY:	CF	•	'//	minn's	111,	CT1160	GN-1





NOTE

REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

REFER TO STRUCTURAL ANALYSIS BY: GPD GROUP DATED: AUGUST 22, 2018, FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT.

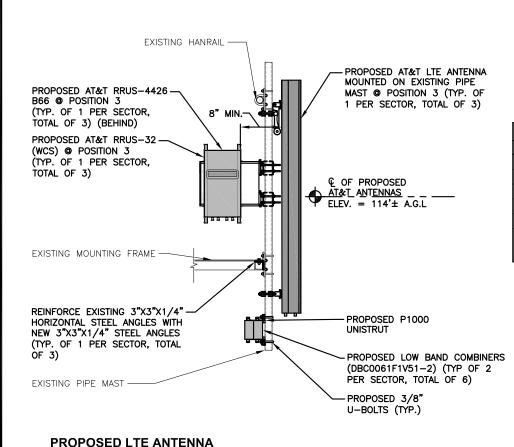
NOTE:

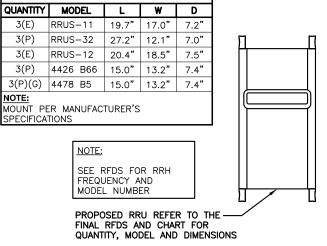
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING **ANTENNA MOUNT** TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JUNE 7, 2018

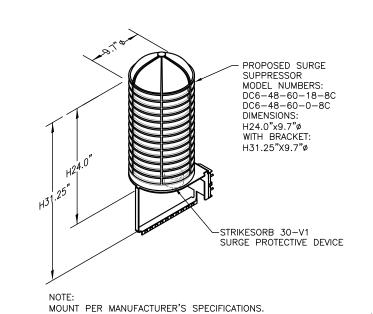
	ANTENNA SCHEDULE													
SECTOR	EXISTING/ PROPOSED	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA & HEIGHT	AZIMUTH	TMA/ DIPLEXER	RRU	SIZE (INCHES) (L x W x D)	FEEDER	RAYCAP			
A1	EXISTING	UMTS DB	7770	55X11X5	±114'	30°	(E) (2) POWERWAVE LGP21401	-	-	(2) 1-5/8 COAX (LENGTH 170 FT ±)	9 - 8 -			
A2	-	-	_	-	-	-	-	-	-	-	\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \			
АЗ	PROPOSED LTE AWS/WCS/850 800-10798 78.5X14.8X6.7 ±114' 30° (P)(2) KAELUS DBC0061F1V51-2 (P) (1) (G) 4478 B5 (P) (1) (G) KAELUS DBC0061F1V51-2 (P) (1) RRUS-32		15X13.2X7.4 15X13.2X7.4 27.2X12.1X7.0	(2) 1-5/8 COAX (LENGTH 170 FT ±)	.) (1) RAYCAP -48-60-18-8F									
A4	EXISTING	LTE 700 PCS	AM-X-CD-16-65-00T-RET	72X11.8X5.9	±113'	30°		(E) (1) RRUS-11 (E) (1) RRUS-12	-	-	(E) DC6-			
B1	EXISTING	UMTS 850	7770	55X11X5	±114'	150°	(E) (2) POWERWAVE LGP21401	-	_	(2) 1-5/8 COAX (LENGTH 170 FT ±)	LP −8℃			
B2	_	_	_	_	_	-	-	_	_	-	1 5 E			
В3	PROPOSED	LTE AWS/WCS/850	800-10798	78.5X14.8X6.7	±114'	150°	(P)(2) KAELUS DBC0061F1V51-2 (P)(1)(G) KAELUS DBC0061F1V51-2	(P) (1) (G) 4478 B5 (P) (1) 4426 B66 (P) (1) RRUS-32	15X13.2X7.4 15X13.2X7.4 27.2X12.1X7.0	(2) 1-5/8 COAX (LENGTH 170 FT ±)) (1) RAYCAP -48-60-18-8C			
B4	EXISTING	LTE 700 PCS	AM-X-CD-16-65-00T-RET	72X11.8X5.9	±113'	150°	-	(E) (1) RRUS-11 (E) (1) RRUS-12	-	-	(P) DC6-			
C1	EXISTING	UMTS 850	7770	55X11X5	±114'	270°	(E) (2) POWERWAVE LGP21401	-	_	(2) 1-5/8 COAX (LENGTH 170 FT ±)				
C2	-	-	_	-	-	-	-	-	-	-				
СЗ	PROPOSED	LTE AWS/WCS/850	800-10798	78.5X14.8X6.7	±114'	270°	(P)(2) KAELUS DBC0061F1V51-2 (P)(1)(G) KAELUS DBC0061F1V51-2	(P) (1) (G) 4478 B5 (P) (1) 4426 B66 (P) (1) RRUS-32	15X13.2X7.4 15X13.2X7.4 27.2X12.1X7.0	(2) 1-5/8 COAX (LENGTH 170 FT ±)	SHARED			
C4	EXISTING	LTE 700 PCS	AM-X-CD-16-65-00T-RET	72X11.8X5.9	±113'	270°	_	(E) (1) RRUS-11 (E) (1) RRUS-12	_	_				

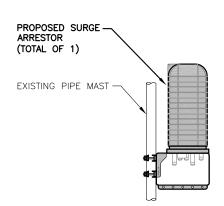
FINAL ANTENNA SCHEDULE /

SCALE: N.T.S









MOUNT PER MANUFACTURER'S SPECIFICATIONS.

RRU CHART

PROPOSED RRUS DETAIL 2
SCALE: N.T.S A-3

DC SURGE SUPPRESSOR DETAIL

SCALE: N.T.S

A-.

OPROPOSED SURGE ARRESTOR MOUNTING DETAIL SCALE: N.T.S

HUDSON Design Group LLC

45 BEECHWOOD DRIVE NORTH ANDOVER, MA 01845

& RRH MOUNTING DETAIL

TEL: (978) 557-5553 FAX: (978) 336-5586

22x34 SCALE: 3/4"=1'-0"

11x17 SCALE: 3/8"=1'-0"

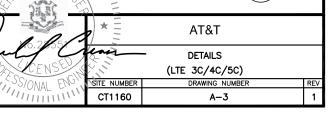


SITE NUMBER: CT1160 SITE NAME: NEW BRITAIN WILDWOOD ST

> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY



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Α	06/28/18	ISSUED FOR	REVIEW			Ī	CF	AT	DJC	,77
NO.	DATE		RE	VISIO	NS		BY	СНК	APP'D	
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STRUCTURAL NOTES:

- DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE SUPPLEMENTS, INTERNATIONAL BUILDING CODE, EIA/TIA-222-G STRUCTURAL STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- 2. CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. ANY UNUSUAL CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- 3. DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS".
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A36 UNLESS OTHERWISE INDICATED.
- 5. STEEL PIPE SHALL CONFORM TO ASTM A500 "COLD-FORMED WELDED & SEAMLESS CARBON STEEL STRUCTURAL TUBING", GRADE B, OR ASTM A53 PIPE STEEL BLACK AND HOT-DIPPED ZINC-COATED WELDED AND SEAMLESS TYPE E OR S, GRADE B. PIPE SIZES INDICATED ARE NOMINAL. ACTUAL OUTSIDE DIAMETER IS LARGER.
- 6. STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS
- 8. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS
- FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT COMPLYING WITH REQUIREMENTS OF ASTM A780. GALVANIZING REPAIR PAINT SHALL HAVE 65 PERCENT ZINC BY WEIGHT, ZIRP BY DUNCAN GALVANIZING, GALVA BRIGHT PREMIUM BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 OR A153
- 10. CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND DI.I. WHERE FILLET WELD SIZES ARE NOT SHOWN. PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "STEEL CONSTRUCTION MANUAL". 14TH EDITION.
- . INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON-CONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL
- 12. UNISTRUT SHALL BE FORMED STEEL CHANNEL STRUT FRAMING AS MANUFACTURED BY UNISTRUT CORP., WAYNE, MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA, UNLESS OTHERWISE NOTED, AND SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION.
- 13. EPOXY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS & WASHERS. AN INTERNALLY THREADED INSERT, A SCREEN TUBE AND A EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HILTI-HIT HY-270 AND OR HY-200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- 14. EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS I, HILTI KWIK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- 15. LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- 16. WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERTIGHT
- 17. ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- 18. NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- 19. SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE.

THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE PROJECT ARE PERMITTED TO ACT AS THE APPROVED AGENCY AND THEIR PERSONNEL ARE PERMITTED TO ACT AS THE SPECIAL INSPECTOR FOR THE WORK DESIGNED BY THEM, PROVIDED THOSE PERSONNEL MEET THE QUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. REPORTS SHALL INDICATE THAT WORK INSPECTED WAS OR WAS NOT COMPLETED IN CONFORMANCE TO APPROVED CONSTRUCTION DOCUMENTS. DISCREPANCIES SHALL BE BROUGHT TO THE IMMEDIATE ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE, A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED

SPECIAL INSPE	CTION CHECKLIST
BEFORE C	ONSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	ENGINEER OF RECORD APPROVED SHOP DRAWINGS ¹
N/A	MATERIAL SPECIFICATIONS REPORT
N/A	FABRICATOR NDE INSPECTION
N/A	PACKING SLIPS ³
ADDITIONAL TESTING AND INSP	ECTIONS:
DURING C	ONSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	STEEL INSPECTIONS
N/A	HIGH STRENGTH BOLT INSPECTIONS
N/A	HIGH WIND ZONE INSPECTIONS 4
N/A	FOUNDATION INSPECTIONS
N/A	CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT
N/A	POST INSTALLED ANCHOR VERIFICATION ⁵
N/A	GROUT VERIFICATION
N/A	CERTIFIED WELD INSPECTION
N/A	EARTHWORK: LIFT AND DENSITY
N/A	ON SITE COLD GALVANIZING VERIFICATION
N/A	GUY WIRE TENSION REPORT
ADDITIONAL TESTING AND INSP	ECTIONS:
AFTER CO	ONSTRUCTION
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	MODIFICATION INSPECTOR REDLINE OR RECORD DRAWINGS ⁶
N/A	POST INSTALLED ANCHOR PULL-OUT TESTING
REQUIRED	PHOTOGRAPHS
ADDITIONAL TESTING AND INSP	FOTIONS

NOTES:

- REQUIRED FOR ANY NEW SHOP FABRICATED FRP OR STEEL PROVIDED BY MANUFACTURER, REQUIRED IF HIGH STRENGTH BOLTS OR STEEL
- PROVIDED BY GENERAL CONTRACTOR; PROOF OF MATERIALS HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C,D 110MPH INSPECT FRAMING OF WALLS, ANCHORING,
- FASTENING SCHEDULE.
 ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ACI 355.4 AND ICC-ES AC308 FOR CRACKED CONCRETE AND SEISMIC APPLICATIONS. DESIGN ADHESIVE BOND STRENGTH HAS BEEN BASED ON ACI 355.4 TEMPERATURE CATEGORY B WITH INSTALLATIONS INTO DRY HOLES DRILLED LISING A CARBIDE BIT INTO CRACKED CONCRETE THAT HAS CURED FOR AT LEAST 21 DAYS. ADHESIVE ANCHORS REQUIRING CERTIFIED INSTALLATIONS SHALL BE INSTALLED BY A CERTIFIED ADHESIVE ANCHOR INSTALLER PER ACI 318-11 D.9.2.2. INSTALLATIONS REQUIRING CERTIFIED INSTALLERS SHALL BE INSPECTED PER ACI 318-11 D.8.2.4.
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

NOTES:

- 1. ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4" A325-X BOLTS, UNLESS OTHERWISE NOTIFIED
- 2. SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED BEFORE ORDERING MATERIAL.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
- VERIFICATION OF EXISTING ROOF CONSTRUCTION IS REQUIRED PRIOR TO THE INSTALLATION OF THE ROOF PLATFORM. ENGINEER OF RECORD IS TO APPROVE EXISTING CONDITIONS IN ORDER TO MOVE FORWARD.
- 5. CENTERLINE OF PROPOSED STEEL PLATFORM SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- 6. EXISTING BRICK MASONRY COLUMNS/BEARING TO BE REPAIRED/REPLACED AT ALL PROPOSED PLATFORM SUPPORT POINTS. ENGINEER OF RECORD TO REVIEW AND APPROVE.

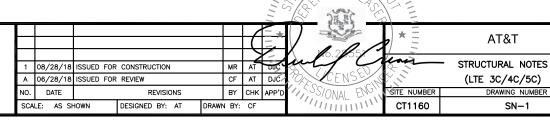
AT&T

SN-1

SITE NUMBER: CT1160 SITE NAME: NEW BRITAIN WILDWOOD ST

> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY







NORTH ANDOVER, MA 01845



NOTE:

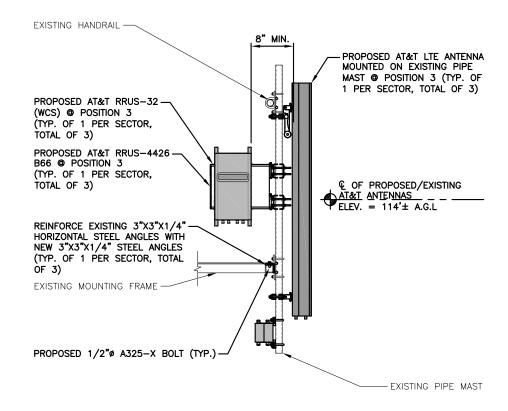
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

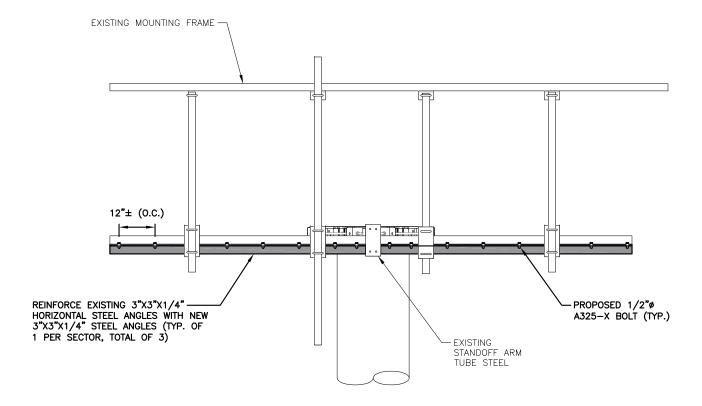
REFER TO STRUCTURAL ANALYSIS BY: GPD GROUP DATED: AUGUST 22, 2018, FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT.

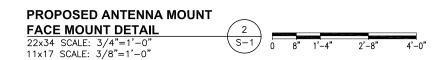
NOTE:

AN ANALYSIS FOR THE CAPACITY OF THE EXISTING ANTENNA MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY: HUDSON DESIGN GROUP, LLC. DATED: JUNE 7, 2018











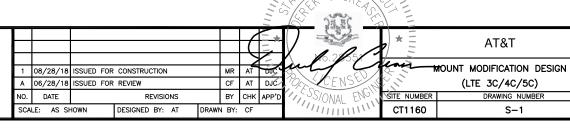
45 BEECHWOOD DRIVE TEL: (978) 557-5553 NORTH ANDOVER, MA 01845 FAX: (978) 336-5586

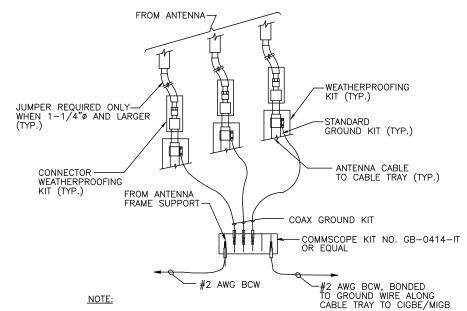


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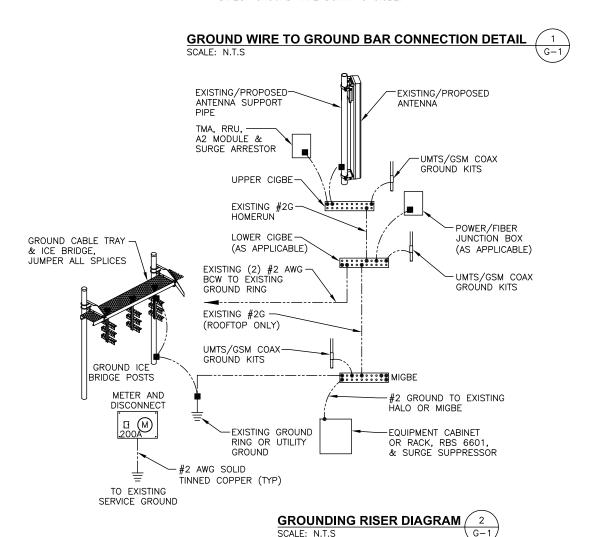
> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY

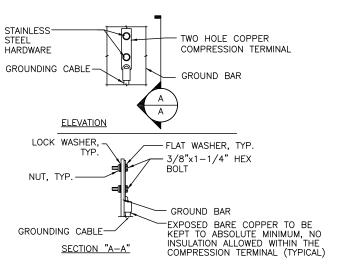






1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.





NOTE:

- 1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
- 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
- 3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL
SCALE: N.T.S



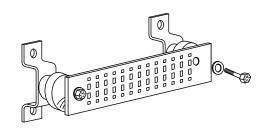
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

CABLE ENTRY PORTS (HATCH PLATES) (#2)
GENERATOR FRAMEWORK (IF AVAILABLE) (#2)
TELCO GROUND BAR
COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2)
+24V POWER SUPPLY RETURN BAR (#2)
-48V POWER SUPPLY RETURN BAR (#2)
RECTIFIER FRAMES.

SECTION "A" - SURGE ABSORBERS

INTERIOR GROUND RING (#2)
EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)
METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)
BUILDING STEEL (IF AVAILABLE) (#2)







AT&T

GROUNDING DETAILS

(LTE 3C/4C/5C)

G-1



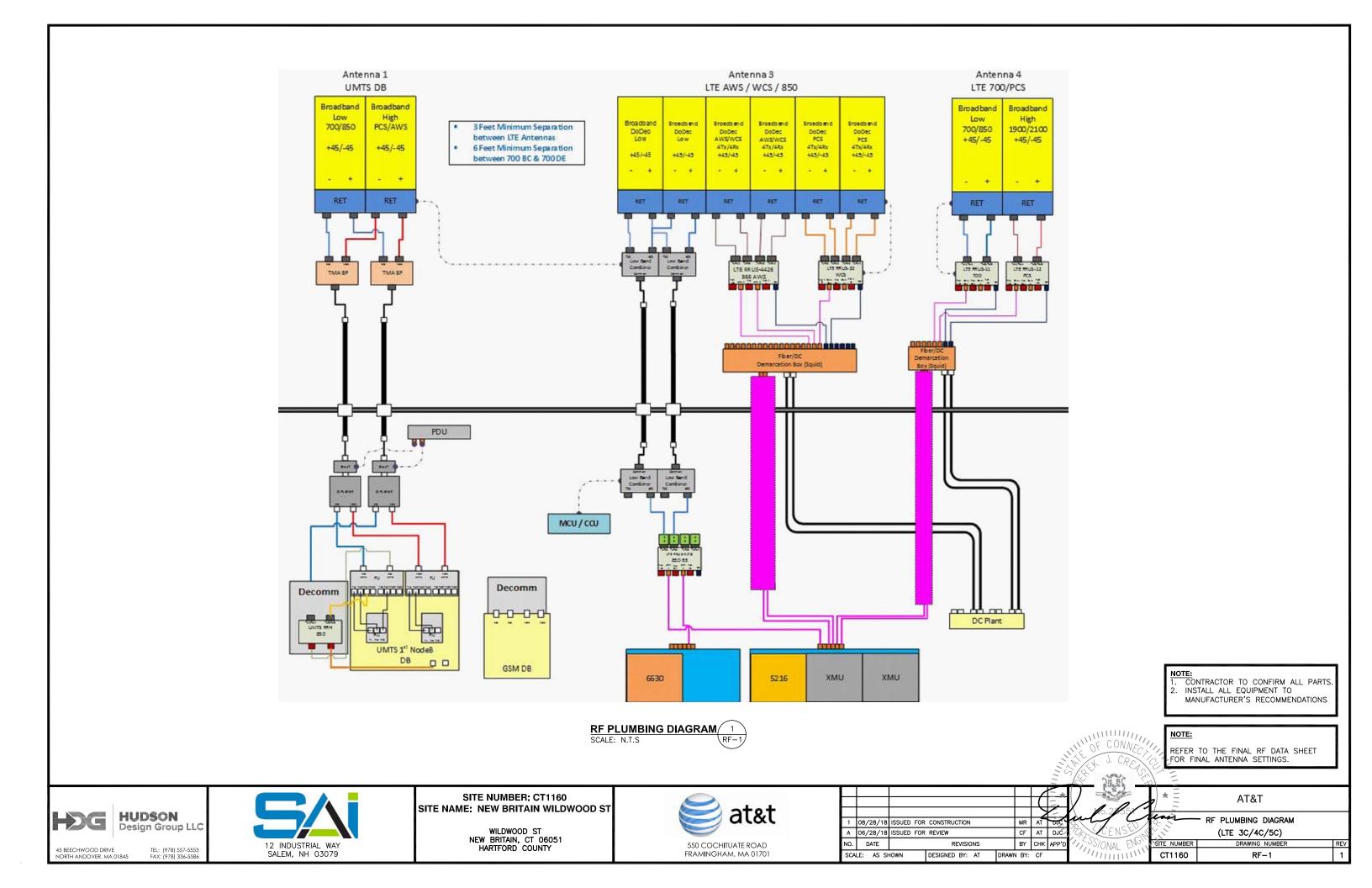


SITE NUMBER: CT1160 SITE NAME: NEW BRITAIN WILDWOOD ST

> WILDWOOD ST NEW BRITAIN, CT 06051 HARTFORD COUNTY



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GPD# 2018723.13.88241.03

August 22, 2018

RIGOROUS STRUCTURAL ANALYSIS REPORT

AT&T DESIGNATION: Site USID: 88241

Site FA: 10050945 Client #: CT1160

Site Name: NEW BRITAIN WILDWOOD STREET

ANALYSIS CRITERIA: Codes: TIA-222-G, 2012 IBC & 2016 CSBC

125-mph Ultimate (3-second gust) with 0" ice 97-mph Nominal (3-second gust) with 0" ice

40-mph (3-second gust) with 1" ice

SITE DATA: Wildwood Street, New Britain, CT 06051, Hartford County

Latitude 41° 40′ 5.47″ N, Longitude 72° 45′ 18.72″ W

Market: New England

110' Penn Summit Monopole

Mr. Tim Burks,

GPD is pleased to submit this Rigorous Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

Analysis Results

Tower Stress Level with Proposed Equipment: 98.2% Pass Foundation Ratio with Proposed Equipment: 63.2% Pass

We at GPD appreciate the opportunity of providing our continuing professional services to you and SAI Communications, Inc. If you have any questions or need further assistance on this or any other projects please do not he sitate to call.

Respectfully submitted

Christopher J. Scheks, P.E. Connecticut #: 0030026

8/22/2018

SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT&T Mobility to SAI Communications, Inc. This report was commissioned by Mr. Tim Burks of SAI Communications, Inc.

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 125 mph converted to a nominal 3-second gust wind speed of 97 mph per Section 1609.3 and Appendix N as required for use in the TIA-222-G Standard per Exception #5 of Section 1609.1.1. Exposure Category C and Risk Category II were used in this analysis.

The mount modifications recommended in the mount analysis by Hudson Design Group (Project #: CT1160, dated 6/7/2018) are assumed to be installed with this project, and have been considered in this analysis.

The proposed coax shall be installed internal to the monopole in order for the analysis to be valid.

Member	Capacity	Results
Monopole	98.2%	Pass
Anchor Rods	74.5%	Pass
Base Plate	84.0%	Pass
Foundation	63.2%	Pass

TOWER SUMMARY AND RESULTS

ANALYSIS METHOD

tnxTower (Version 8.0.2.1), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is based solely on this information and is being completed without the benefit of a detailed site visit.

DOCUMENTS PROVIDED

Document	Remarks	Source
Construction Drawings	SAI Site #: CT1160 Rev. A, dated 6/28/2018	SAI
RF Data Sheet	RFDS Name: CT1160 v1.00, dated 5/24/2018	SAI
Tower Design	PJF Job #: 29205-0027, dated 4/29/2005	AT&T
Foundation Design	Not Provided	N/A
Geotechnical Report	Not Provided	N/A
Previous Structural Analysis	GPD Project #: 2018723.01.88241.02, dated 6/21/2018	AT&T
Mount Analysis	Hudson Design Group Project #: CT1160, dated 6/7/2018	SAI

8/22/2018 Page 2 of 4

ASSUMPTIONS

This rigorous structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

- 1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
- 2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
- 3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
- 4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
- 5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
- 6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
- 7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
- 8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
- 9. All prior structural modifications are assumed to be as per data supplied/available and to have been properly installed.
- 10. Loading interpreted from photos is accurate to $\pm 5'$ AGL, antenna size accurate to ± 3.3 sf, and coax equal to the number of existing antennas without reserve.
- 11. All existing loading was obtained from the previous structural analysis by GPD (Project #: 2018723.01.88241.02, dated 6/21/2018), the provided construction drawings, the RF Data Sheet and site photos and is assumed to be accurate.
- 12. The final loading configuration has been modeled to reflect that of the provided construction drawings and is assumed to be accurate.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD should be allowed to review any new information to determine its effect on the structural integrity of the tower.

8/22/2018 Page 3 of 4

DISCLAIMER OF WARRANTIES

GPD has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD in connection with this Rigorous Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

This analysis is limited to the designated maximum wind and seismic conditions per the governing tower standards and code. Wind forces resulting in tower vibrations near the structure's resonant frequencies were not considered in this analysis and are outside the scope of this analysis. Lateral loading from any dynamic response was not evaluated under a time-domain based fatigue analysis.

GPD does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the capability of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the code specified amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

GPD makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD pursuant to this report will be limited to the total fee received for preparation of this report.

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APPENDIX A

Tower Analysis Summary Form

Tower Analysis Summary Form

General Info

Site Name	NEW BRITAIN WILDWOOD STREET
Site Number	88241 (CT1160)
FA Number	10050945
Date of Analysis	8/22/2018
Company Performing Analysis	GPD

Tower Info Description Date Tower Type (G, SST, MP) Tower Height (top of steel AGL) Tower Manufacturer 2005 Penn Summit Tower Model 4/29/2005 Tower Design PJF Job # 29205-0027 Foundation Design Geotech Report Tower Mapping Previous Structural Analysis GPD Project #: 2018723.01.88241.02 6/21/2018 Mount Analysis Hudson Design Group Project #: CT1160 6/7/2018

Steel Yield Strength (ksi)

Pole	65
Base Plate	50
Anchor Rods	75

The information contained in this summary report is not to be used independently from the PE stamped tower analysis.

Design Parameters

Design Codes Used	TIA-222-G, 2012 IBC & 2016 CSBC
Location of Tower (County, State)	Hartford, CT
Nominal Wind Speed (mph)	97 (3-second gust)
Ice Thickness (in)	1
Risk Category (I, II, III)	II
Exposure Category (B, C, D)	С
Topographic Category (1 to 5)	1

The mount modifications recommended in the mount analysis by Hudson Design Group (Project #: CT1160, dated 6/7/2018) are issumed to be installed with this project, and have been considered in this analysis.

Analysis Results (% Maximum Usage)

Existing/Reserved + Future + Proposed Condition								
Tower (%)	98.2%							
Tower Base (%)	84.0%							
Foundation (%)	63.2%							
Foundation Adequate?	Yes							

Existing / Reserved Loading

			F	Antenna					Mou	nt		Transm	ission Line	
Antenna Owner	Mount Height (ft)	Antenna CL (ft)	Quantity	Туре	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Туре	Quantity	Model	Size	Attachment Int/Ext
AT&T Mobility	110	114	6	Panel	Powerwave	7770.00	30/150/270	1	Unknown	LP Platform w/ Rails	12	Unknown	1-5/8"	Internal
AT&T Mobility	110	113	3	Panel	KMW	AM-X-CD-16-65-00T-RET	30/150/270			On The Same Mount	2	DC Power	3/4"	Internal
AT&T Mobility	110	113	6	TMA	Powerwave	LGP 21401				On The Same Mount	1	Fiber Cable	1/2"	Internal
AT&T Mobility	110	113	6	Diplexer	Powerwave	LGP 13519				On The Same Mount				
AT&T Mobility	110	113	3	RRU	Ericsson	RRUS 11				On The Same Mount				
AT&T Mobility	110	113	3	RRU	Ericsson	RRUS 12				On The Same Mount				
AT&T Mobility	110	110	1	Surge	Raycap	DC6-48-60-18-8F				Tower Mounted				
T-Mobile	100	100	3	Panel	Ericsson	AIR 21 B2A B4P	60/160/310	1	Unknown	Platform w/ Rails	11	Unknown	1-5/8"	Internal
T-Mobile	100	100	3	Panel	RFS	APXVARR24_43 U-NA20	60/160/310			On The Same Mount	3	Hybrid Cable	1-1/4"	Internal
T-Mobile	100	100	3	Panel	Ericsson	AIR 32 B66AaB2a				On The Same Mount				
T-Mobile	100	100	3	RRU	Ericsson	4449-B12+71				On The Same Mount				
Verizon	90	90	3	Panel	Antel	BXA-80063/4CF	0/120/240	3	Unknown	T-Arms	12	Unknown	1-5/8"	Internal
Verizon	90	90	3	Panel	Antel	BXA-171063-8BF	0/120/240			On The Same Mounts	6	Unknown	1-5/8"	External
Verizon	90	90	3	Panel	Antel	BXA-70063-6CF_2	0/120/240			On The Same Mounts				
·														
Township	60	60	10	Lights	Unknown	Stadium Lights		1	Unknown	Stadium Light Rack				

Note: The existing (3) 7770.00 and (6) LGP 13519 at 110' shall be removed prior to the installation of the proposed loading. All remaining equipment shall be reused.

Proposed Loading

			A	ntenna			Mour	nt	Transmission Line					
Antenna Owner	Mount Height (ft)	Antenna CL (ft)	Quantity	Туре	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Туре	Quantity	Model	Size	Attachment Int/Ext
AT&T Mobility	110	114	3	Panel	Kathrein	800 10798	30/150/270	3	Unknown	Toe Rail Reinforcement	2	DC Power	3/4"	Internal
AT&T Mobility	110	113	6	Diplexer	Kaelus	DBC0061F1V51-2				On The Existing Mount	1	Fiber Cable	1/2"	Internal
AT&T Mobility	110	113	3	RRU	Ericsson	RRUS 4478 B5				On The Existing Mount				
AT&T Mobility	110	113	3	RRU	Ericsson	RRUS 4426 B66				On The Existing Mount				
AT&T Mobility	110	113	3	RRU	Ericsson	RRUS 32				On The Existing Mount				
AT&T Mobility	110	110	1	Surge	Raycap	DC6-48-60-18-8C				Tower Mounted				

Note: The proposed loading is in addition to the remaining loading at the same elevation.

The proposed coax shall be installed internal to the monopole in order for the analysis to be valid.

Future Loading

	Antenna								Mou	nt	Transmission Line			
Antenna Owner	Mount Height (ft)	Antenna CL (ft)	Quantity	Туре	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Туре	Quantity	Model	Size	Attachment Int/Ext
						_								

APPENDIX B

tnxTower Output File

4	7
tnvi	'ower
	UIVEI

GPD

520 South Main Street Suite 2531 Akron, Ohio 44311 Phone: (555) 555-1234 FAX: (555) 555-1235

Job	Page
88241 (CT1160) NEW BRITAIN WILDWOOD STREET	1 of 7
Project	Date
2018723.13.88241.03	12:43:41 08/20/18
Client	Designed by
SAI Communications, Inc.	mschooley

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Hartford County, Connecticut.

ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).

Basic wind speed of 97 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 40 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Component Type	Placement	Total Number	Number Per Row		Width or Diameter	Perimeter	Weight
			ft				in	in	plf
Climbing Pegs	В	Surface Ar	110.00 - 8.00	1	1	0.000	0.1500		0.31
		(CaAa)				0.000			
LDF7-50A (1-5/8 FOAM)	C	Surface Ar	90.00 - 8.00	6	6	0.000	1.9800		0.82
		(CaAa)				0.000			

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg	Smeia	Туре	ft	rumber		ft²/ft	plf
Safety Line (3/8")	В	No	CaAa (Out Of	110.00 - 8.00	1	No Ice	0.04	0.22
• , , ,			Face)			1/2" Ice	0.14	0.75
						1" Ice	0.24	1.28
LDF7-50A (1-5/8	В	No	Inside Pole	110.00 - 8.00	12	No Ice	0.00	0.82
FOAM)						1/2" Ice	0.00	0.82
						1" Ice	0.00	0.82
3/4" DC Power Line	В	No	Inside Pole	110.00 - 8.00	4	No Ice	0.00	0.33
						1/2" Ice	0.00	0.33
						1" Ice	0.00	0.33
1/2" Fiber Cable	В	No	Inside Pole	110.00 - 8.00	2	No Ice	0.00	0.15
						1/2" Ice	0.00	0.15
						1" Ice	0.00	0.15
LDF7-50A (1-5/8	Α	No	Inside Pole	100.00 - 8.00	11	No Ice	0.00	0.82
FOAM)						1/2" Ice	0.00	0.82
,						1" Ice	0.00	0.82
1-1/4" Hybrid Cable	Α	No	Inside Pole	100.00 - 8.00	3	No Ice	0.00	1.00

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	88241 (CT1160) NEW BRITAIN WILDWOOD STREET	2 of 7
Ī	Project	Date
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	Client SAI Communications, Inc.	Designed by
	or a communications, me.	mschooley

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg		71	ft			ft²/ft	plf
						1/2" Ice	0.00	1.00
						1" Ice	0.00	1.00
LDF7-50A (1-5/8	C	No	Inside Pole	90.00 - 8.00	12	No Ice	0.00	0.82
FOAM)						1/2" Ice	0.00	0.82
						1" Ice	0.00	0.82

D : 4		
Discrete	IOWAR	I Vade
D 1301 616		LUUUS

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C_AA_A Side	Weight
			Vert ft ft ft	0	ft		ft²	ft²	K
Platform w/ Handrails	С	None	Ji	0.0000	110.00	No Ice	33.04	33.04	2.17
						1/2" Ice	43.38	43.38	2.68
						1" Ice	53.72	53.72	3.19
Kicker Kit	C	None		0.0000	109.00	No Ice	11.84	11.84	0.28
						1/2" Ice	16.96	16.96	0.30
		_				1" Ice	22.08	22.08	0.32
Toe Rail Reinforcement	A	From	4.00	30.0000	110.00	No Ice	3.99	0.07	0.07
(L3x3x1/4)		Centroid-Le	0.00			1/2" Ice	4.90	0.11	0.10
	_	_ g	0.00			1" Ice	5.81	0.16	0.15
Toe Rail Reinforcement	В	From	4.00	30.0000	110.00	No Ice	3.99	0.07	0.07
(L3x3x1/4)		Centroid-Le	0.00			1/2" Ice	4.90	0.11	0.10
	~	g	0.00	• • • • • •		1" Ice	5.81	0.16	0.15
Toe Rail Reinforcement	C	From	4.00	30.0000	110.00	No Ice	3.99	0.07	0.07
(L3x3x1/4)		Centroid-Le	0.00			1/2" Ice	4.90	0.11	0.10
D: 14 (C) 2.2751		g	0.00	20.0000	110.00	1" Ice	5.81	0.16	0.15
Pipe Mount 6'x2.375"	Α	From	4.00	30.0000	110.00	No Ice	1.43	1.43	0.03
		Centroid-Le	0.00			1/2" Ice	1.92	1.92	0.04
D: M (C) 2.27511	D	g	3.00	20,0000	110.00	1" Ice	2.29	2.29	0.05
Pipe Mount 6'x2.375"	В	From Centroid-Le	4.00	30.0000	110.00	No Ice 1/2" Ice	1.43 1.92	1.43 1.92	0.03
			0.00			1" Ice	2.29	2.29	0.04
Pipe Mount 6'x2.375"	С	g From	3.00 4.00	30.0000	110.00		1.43	1.43	0.05 0.03
Pipe Mount 6 x2.373	C	Centroid-Le	0.00	30.0000	110.00	No Ice 1/2" Ice	1.43	1.43	0.03
			3.00			1" Ice	2.29	2.29	0.04
7770.00 w/Mount Pipe	A	g From	4.00	30.0000	110.00	No Ice	5.51	4.10	0.03
///0.00 w/Mount Fipe	А	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	5.87	4.73	0.00
			4.00			1" Ice	6.23	5.37	0.11
7770.00 w/Mount Pipe	В	g From	4.00	30.0000	110.00	No Ice	5.51	4.10	0.16
7770.00 W/Wount Tipe	ь	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	5.87	4.73	0.00
		g g	4.00			1" Ice	6.23	5.37	0.11
7770.00 w/Mount Pipe	C	From	4.00	30.0000	110.00	No Ice	5.51	4.10	0.16
7770.00 W/Would Tipe	C	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	5.87	4.73	0.00
		g g	4.00			1" Ice	6.23	5.37	0.16
M-X-CD-16-65-00T-RET	Α	From	4.00	30.0000	110.00	No Ice	8.31	6.65	0.10
w/ Mount Pipe	7.1	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	8.85	7.68	0.16
w would app		g	3.00			1" Ice	9.37	8.56	0.23
M-X-CD-16-65-00T-RET	В	From	4.00	30.0000	110.00	No Ice	8.31	6.65	0.09
w/ Mount Pipe	2	Centroid-Le	0.00	20.0000	110.00	1/2" Ice	8.85	7.68	0.16
mount 1 pe		g	3.00			1" Ice	9.37	8.56	0.23
M-X-CD-16-65-00T-RET	C	From	4.00	30.0000	110.00	No Ice	8.31	6.65	0.09
w/ Mount Pipe	Ü	Centroid-Le	0.00	2 2.2000		1/2" Ice	8.85	7.68	0.16
unt 1 ipe		g g	3.00			1" Ice	9.37	8.56	0.23
800 10798 w/ Mount Pipe	Α	From	4.00	30.0000	110.00	No Ice	10.69	5.69	0.08

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Project	Date
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Client	Designed by
SAI Communications, Inc.	mschooley

Description	Face or	Offset Type	Offsets: Horz	Azimuth Adjustment	Placement		C_AA_A Front	$C_A A_A$ Side	Weigh
	Leg	71	Lateral Vert	,					
			ft	0	ft		ft^2	ft^2	K
			ft ft		J.		J	J	
		Centroid-Le	0.00			1/2" Ice	11.19	6.18	0.14
	_	_ g	4.00			1" Ice	11.71	6.67	0.21
800 10798 w/ Mount Pipe	В	From	4.00	30.0000	110.00	No Ice	10.69	5.69	0.08
		Centroid-Le	0.00			1/2" Ice	11.19	6.18	0.14
200 10709 m/ Mount Ding	С	g From	4.00 4.00	30.0000	110.00	1" Ice No Ice	11.71 10.69	6.67 5.69	0.21 0.08
800 10798 w/ Mount Pipe	C	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	11.19	6.18	0.08
		g	4.00			1" Ice	11.71	6.67	0.14
(2) LGP21401	Α	From	4.00	30.0000	110.00	No Ice	1.10	0.21	0.01
(2) 20121 101	• •	Centroid-Le	0.00	20.000	110.00	1/2" Ice	1.24	0.27	0.02
		g	3.00			1" Ice	1.38	0.35	0.03
(2) LGP21401	В	From	4.00	30.0000	110.00	No Ice	1.10	0.21	0.01
		Centroid-Le	0.00			1/2" Ice	1.24	0.27	0.02
		g	3.00			1" Ice	1.38	0.35	0.03
(2) LGP21401	C	From	4.00	30.0000	110.00	No Ice	1.10	0.21	0.01
		Centroid-Le	0.00			1/2" Ice	1.24	0.27	0.02
		g	3.00			1" Ice	1.38	0.35	0.03
(2) DBC0061F1V51-2	A	From	4.00	30.0000	110.00	No Ice	0.43	0.41	0.03
		Centroid-Le	0.00			1/2" Ice	0.51	0.50	0.03
(a) pp. (1511151 a		g	3.00	20.0000	110.00	1" Ice	0.61	0.59	0.04
(2) DBC0061F1V51-2	В	From	4.00	30.0000	110.00	No Ice	0.43	0.41	0.03
		Centroid-Le	0.00			1/2" Ice	0.51	0.50	0.03
(2) DDC00(1E11/51 2	0	g	3.00	20,0000	110.00	1" Ice	0.61	0.59	0.04
(2) DBC0061F1V51-2	C	From	4.00	30.0000	110.00	No Ice 1/2" Ice	0.43	0.41	0.03
		Centroid-Le	0.00 3.00			1" Ice	0.51 0.61	0.50 0.59	0.03 0.04
RRUS 11	Α	g From	4.00	30.0000	110.00	No Ice	2.78	1.19	0.04
KKUS II	Α	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	2.78	1.19	0.03
			3.00			1" Ice	3.21	1.33	0.07
RRUS 11	В	g From	4.00	30.0000	110.00	No Ice	2.78	1.19	0.10
KKC5 11	Ь	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	2.99	1.33	0.03
		g	3.00			1" Ice	3.21	1.49	0.10
RRUS 11	C	From	4.00	30.0000	110.00	No Ice	2.78	1.19	0.05
1410511	Č	Centroid-Le	0.00	20.000	110.00	1/2" Ice	2.99	1.33	0.07
		g	3.00			1" Ice	3.21	1.49	0.10
RRUS 12	Α	From	4.00	30.0000	110.00	No Ice	3.15	1.29	0.06
		Centroid-Le	0.00			1/2" Ice	3.36	1.44	0.08
		g	3.00			1" Ice	3.59	1.60	0.11
RRUS 12	В	From	4.00	30.0000	110.00	No Ice	3.15	1.29	0.06
		Centroid-Le	0.00			1/2" Ice	3.36	1.44	0.08
		g	3.00			1" Ice	3.59	1.60	0.11
RRUS 12	C	From	4.00	30.0000	110.00	No Ice	3.15	1.29	0.06
		Centroid-Le	0.00			1/2" Ice	3.36	1.44	0.08
		_ g	3.00			1" Ice	3.59	1.60	0.11
RRUS 4478 B5	Α	From	4.00	30.0000	110.00	No Ice	1.84	1.06	0.06
		Centroid-Le	0.00			1/2" Ice	2.01	1.20	0.08
DD11G 4450 D5	-	g	3.00	20.0000	110.00	1" Ice	2.19	1.34	0.09
RRUS 4478 B5	В	From	4.00	30.0000	110.00	No Ice	1.84	1.06	0.06
		Centroid-Le	0.00			1/2" Ice	2.01	1.20	0.08
RRUS 4478 B5	С	g From	3.00	30.0000	110.00	1" Ice No Ice	2.19 1.84	1.34 1.06	0.09 0.06
KKUS 44/8 B3	C	From Centroid-Le	4.00 0.00	30.0000	110.00	1/2" Ice	2.01	1.06	0.08
			3.00			1/2" Ice 1" Ice	2.01	1.20	0.08
RRUS 4426 B66	Α	g From	4.00	30.0000	110.00	No Ice	1.64	0.73	0.09
ANUS 4420 D00	А	Centroid-Le	0.00	30.0000	110.00	1/2" Ice	1.80	0.73	0.05
		g	3.00			1" Ice	1.97	0.97	0.08

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88241 (CT1160) NEW BRITAIN WILDWOOD STREET	4 of 7
Project	Date
2018723.13.88241.03	12:43:41 08/20/18
Client	Designed by
SAI Communications, Inc.	mschooley

Leg			$C_AA_A Weig$ Side
RRUS 4426 B66			
RRUS 4426 B66	ft	22	ft² K
RRUS 4426 B66	Ji	,	ji K
RRUS 4426 B66	'Ice 1.8	80 0	0.84 0.00
RRUS 32			0.08
RRUS 32			0.73 0.05
RRUS 32			0.00
RRUS 32 B From 4.00 30.000 110.00 No Centroid-Le 0.00 2 3.00 110.00 No Centroid-Le 0.00 11/2" RRUS 32 C From 4.00 30.0000 110.00 No Centroid-Le 0.00 11/2" B G 3.00			0.08
RRUS 32 B From 4.00 30.0000 110.00 No Centroid-Le 0.00			2.42 0.08 2.64 0.10
RRUS 32 B Centroid-Le 0.00 Centroid-Le			2.86 0.14
RRUS 32			2.42 0.08
RRUS 32			2.64 0.10
RRUS 32	Ice 3.8	81 2	2.86 0.14
DC6-48-60-18-8F Surge C From Leg 0.50 0.0000 110.00 No 1/2"	Ice 3.3	31 2	2.42 0.08
DC6-48-60-18-8F Surge Suppression Unit O.00		56 2	2.64 0.10
Suppression Unit			2.86 0.14
DC6-48-60-18-8C Surge Suppression Unit			0.02
DC6-48-60-18-8C Surge Suppression Unit			.46 0.04
Suppression Unit **** Platform w/ Handrails C None Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le Centroid-Le 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le Centroid-Le 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le Centroid-Le 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le Centroid-Le 0.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le Centroid-Le 0.00 APXVARR24_43 U-NA20 W/ Mount Pipe Centroid-Le Centroid-Le 0.00 APXVARR24_43 U-NA20 W/ Mount Pipe Centroid-Le Centroid-Le Q 0.00 APXVARR24_43 U-NA20 W/ Mount Pipe Centroid-Le Centroid-Le Q 0.00 APXVARR24_43 U-NA20 Centroid-Le Q 0.00 APXVARR24_43 U-NA20 W/ Mount Pipe Centroid-Le Centroid-Le Q 0.00 APXVARR24_43 U-NA20 W/ Mount Pipe Centroid-Le Centroid-Le Q 0.00 APXVARR24_43 U-NA20 Centroid-Le Q 0.00 APXVARR24_43 U-NA20 Centroid-Le Q 0.00 APXVARR24_43 U-NA20 APXVARR24_43 U-NA20 Centroid-Le Q 0.00 APXVARR24_43 U-NA20 APXV			64 0.00
Platform w/ Handrails C None			
Platform w/ Handrails C None 0.0000 100.00 No 1/2" AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le 0.00 g 0.00 100.00 No 1/2" AIR 21 B2A/B4P w/ Mount B From 4.00 30.0000 100.00 No 1/2" BY FOM 4.00 30.0000 100.00 No 1/2" AIR 21 B2A/B4P w/ Mount C From 4.00 30.0000 100.00 No 1/2" AIR 21 B2A/B4P w/ Mount C From 4.00 30.0000 100.00 No 1/2" BY FOM 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" B From 4.00 30.0000 100.00 No 1/2" BY FOM 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2" AIR 32 B66Aa/B2A w/ 60" A From 4.00 30.0000 100.00 No 1/2"			2.00 0.00
AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le S S S S S S S S S S S S S S S S S S S			
AIR 21 B2A/B4P w/ Mount Pipe APXVARR24_43 U-NA20 w/ Mount Pipe Centroid-Le 0.00			2.03 1.34
AIR 21 B2A/B4P w/ Mount Pipe AIR 21 B2A/B4P w/ Mount Controid-Le O.00 AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le O.00 APXVARR24 43 U-NA20 A From 4.00 APXVARR24 43 U-NA20 Centroid-Le O.00 APXVARR24 43 U-NA20 A From 4.00 APXVARR24 43 U-NA20 A From 4.00 APXVARR24 43 U-NA20 Centroid-Le O.00 APXVARR24 43 U-NA20 A From 4.00 APXVARR24 43 U-NA20 A From 4.00 APXVARR24 43 U-NA20 A From 4.00 Centroid-Le O.00 APXVARR24 43 U-NA20 A From 4.00 A From 4.			8.71 1.80
Pipe Centroid-Le 0.00 1/2" 1" 1 1 1 1 1 1 1 1			5.39 2.20
AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le 0.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 B From 4.00 Centroid-Le 0.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 Centroid-Le 0.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 Centroid-Le 0.00 APXVARR24_43 U-NA20 Centroid-Le 0.00 APXVARR24_43 U-NA20 Centroid-Le 0.00 APXVARR24_43 U-NA20 A From 4.00 APXVARR24_43 U-NA20 Centroid-Le 0.00 APXVARR24_43 U-NA20 A From 4.00 A FROM A.00 A F			0.10
AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le 0.00			5.30 0.16 7.00 0.22
Pipe			5.55 0.10
Section Sect			5.30 0.10
AIR 21 B2A/B4P w/ Mount Pipe Centroid-Le g 0.00 AIR 30.0000 Pipe Centroid-Le g 0.00 AIR 30.0000 AIR 30.0000 100.00 No Mount Pipe Centroid-Le g 0.00 AIR 30.0000 100.00 No Mount Pipe Centroid-Le g 0.00 AIR 30.0000 100.00 No Mount Pipe Centroid-Le g 0.00 AIR 30.0000 AIR 30.0000 100.00 No Mount Pipe Centroid-Le g 0.00 AIR 30.0000 AI			7.00 0.22
Pipe			5.55 0.10
AIR32 B66Aa/B2A w/ 60"			5.30 0.10
AIR32 B66Aa/B2A w/ 60"	Ice 7.0	03 7	7.00 0.22
Section Sect		58 5	5.90 0.15
AIR32 B66Aa/B2A w/ 60" B From 4.00 30.0000 100.00 No Mount Pipe g 0.00 11/2" AIR32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No Mount Pipe g 0.00 11/2" APXVARR24_43 U-NA20 A From 4.00 30.0000 100.00 No w/ Mount Pipe g 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_13 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 11/2"		97 6	0.2
Mount Pipe Centroid-Le 0.00 1/2" 1" 1 1 2 2 3 3 3 3 3 3 3 3			7.24 0.28
Section Sect			5.90 0.13
AIR32 B66Aa/B2A w/ 60" C From 4.00 30.0000 100.00 No Mount Pipe g 0.00 11/2" APXVARR24_43 U-NA20 A From 4.00 30.0000 100.00 No w/ Mount Pipe g 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 11/2"			0.56
Mount Pipe Centroid-Le 0.00 1/2" 3 1" 3 1" 3 1 1 1 1 1 1 1 1 1			7.24 0.28
Section Property			5.90 0.15
APXVARR24_43 U-NA20 A From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 11/2"			0.56 0.23 7.24 0.28
w/ Mount Pipe Centroid-Le 0.00 1/2" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 1/2" 1"1 1"1 APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 1/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 1/2" 1"1			0.64 0.12
g 0.00 1"1" APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 11/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 11/2"			2.07 0.12
APXVARR24_43 U-NA20 B From 4.00 30.0000 100.00 No w/ Mount Pipe	Ice 18.		3.35 0.37
w/ Mount Pipe Centroid-Le 0.00 1/2" APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 1/2" g 0.00 1"1 RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 1/2"			0.64 0.12
Section Sect			2.07 0.24
APXVARR24_43 U-NA20 C From 4.00 30.0000 100.00 No w/ Mount Pipe Centroid-Le 0.00 1/2" RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 1/2"			3.35 0.37
RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 1/2"			0.64 0.12
RRUS 4449-B12+71 A From 4.00 30.0000 100.00 No Centroid-Le 0.00 1/2"			2.07 0.24
Centroid-Le 0.00 1/2"			3.35 0.37
			.16 0.07
σ ΛΛΛ			.30 0.09
			.45 0.10
RRUS 4449-B12+71 B From 4.00 30.0000 100.00 No			.16 0.07
Centroid-Le 0.00 1/2" g 0.00 1"1"			30 0.09 45 0.10

GPD

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88241 (CT1160) NEW BRITAIN WILDWOOD STREET	5 of 7
Project	Date
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Client	Designed by
SAI Communications, Inc.	mschooley

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C_AA_A Front	C_AA_A Side	Weight
	Leg		Vert						
			ft ft	o	ft		ft²	ft ²	K
RRUS 4449-B12+71	С	From	ft4.00	30.0000	100.00	No Ice	1.65	1.16	0.07
KKUS 4449-B12+71	C	Centroid-Le	0.00	30.0000	100.00	1/2" Ice	1.81	1.30	0.09
***		g	0.00			1" Ice	1.98	1.45	0.10
10' T-Arm - Round (GPD)	Α	From Leg	1.50	0.0000	90.00	No Ice	3.90	2.33	0.25
10 1 71111 Round (GLD)	71	Trom Leg	0.00	0.0000	70.00	1/2" Ice	4.30	2.96	0.30
			0.00			1" Ice	4.70	3.60	0.35
10' T-Arm - Round (GPD)	В	From Leg	1.50	0.0000	90.00	No Ice	3.90	2.33	0.25
(0.2)			0.00			1/2" Ice	4.30	2.96	0.30
			0.00			1" Ice	4.70	3.60	0.35
10' T-Arm - Round (GPD)	С	From Leg	1.50	0.0000	90.00	No Ice	3.90	2.33	0.25
, ,			0.00			1/2" Ice	4.30	2.96	0.30
			0.00			1" Ice	4.70	3.60	0.35
BXA-80063-4CF w/ mount	Α	From Leg	3.00	0.0000	90.00	No Ice	3.58	3.66	0.03
pipe		J	0.00			1/2" Ice	3.88	4.21	0.06
1 1			0.00			1" Ice	4.20	4.77	0.10
BXA-80063-4CF w/ mount	В	From Leg	3.00	0.0000	90.00	No Ice	3.58	3.66	0.03
pipe		C	0.00			1/2" Ice	3.88	4.21	0.06
1 1			0.00			1" Ice	4.20	4.77	0.10
BXA-80063-4CF w/ mount	C	From Leg	5.00	0.0000	90.00	No Ice	3.58	3.66	0.03
pipe		Č	0.00			1/2" Ice	3.88	4.21	0.06
1 1			0.00			1" Ice	4.20	4.77	0.10
3XA-171063-8BF w/ Mount	Α	From Leg	3.00	0.0000	90.00	No Ice	3.18	3.35	0.03
Pipe		•	0.00			1/2" Ice	3.56	3.97	0.06
•			0.00			1" Ice	3.93	4.60	0.10
3XA-171063-8BF w/ Mount	В	From Leg	3.00	0.0000	90.00	No Ice	3.18	3.35	0.03
Pipe		_	0.00			1/2" Ice	3.56	3.97	0.06
•			0.00			1" Ice	3.93	4.60	0.10
3XA-171063-8BF w/ Mount	C	From Leg	3.00	0.0000	90.00	No Ice	3.18	3.35	0.03
Pipe			0.00			1/2" Ice	3.56	3.97	0.06
			0.00			1" Ice	3.93	4.60	0.10
3XA-70063-6CF-2 w/ Mount	Α	From Leg	3.00	0.0000	90.00	No Ice	7.81	5.80	0.04
Pipe			0.00			1/2" Ice	8.36	6.95	0.10
			0.00			1" Ice	8.87	7.82	0.17
XA-70063-6CF-2 w/ Mount	В	From Leg	3.00	0.0000	90.00	No Ice	7.81	5.80	0.04
Pipe			0.00			1/2" Ice	8.36	6.95	0.10
			0.00			1" Ice	8.87	7.82	0.17
3XA-70063-6CF-2 w/ Mount	C	From Leg	3.00	0.0000	90.00	No Ice	7.81	5.80	0.04
Pipe			0.00			1/2" Ice	8.36	6.95	0.10
			0.00			1" Ice	8.87	7.82	0.17

10' T-Arm - Round (GPD)	C	From Face	1.50	0.0000	60.00	No Ice	3.90	2.33	0.25
			0.00			1/2" Ice	4.30	2.96	0.30
			1.50			1" Ice	4.70	3.60	0.35
10' T-Arm - Round (GPD)	C	From Face	1.50	0.0000	60.00	No Ice	3.90	2.33	0.25
			0.00			1/2" Ice	4.30	2.96	0.30
			-1.50			1" Ice	4.70	3.60	0.35

GPD

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88241 (CT1160) NEW BRITAIN WILDWOOD STREET	6 of 7
Project	Date
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Client	Designed by
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					Dis	shes					
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	0	0	ft	ft		ft^2	K
Stadium Light (2')	С	Paraboloid w/o Radome	From Face	3.00 -6.00	0.0000		60.00	2.00	No Ice 1/2" Ice	3.14 3.41	0.08 0.02
Stadium Light (2')	C	Paraboloid w/o Radome	From Face	1.50 3.00 -3.00	0.0000		60.00	2.00	1" Ice No Ice 1/2" Ice	3.68 3.14 3.41	0.00 0.08 0.02
Stadium Light (2')	C	Paraboloid w/o Radome	From Face	1.50 3.00 0.00	0.0000		60.00	2.00	1" Ice No Ice 1/2" Ice	3.68 3.14 3.41	0.00 0.08 0.02
Stadium Light (2')	С	Paraboloid w/o	From	1.50 3.00	0.0000		60.00	2.00	1" Ice No Ice	3.68 3.14	0.02 0.00 0.08
G. 1	a	Radome	Face	3.00 1.50	0.0000		60.00	2.00	1/2" Ice 1" Ice	3.41 3.68	0.02
Stadium Light (2')	С	Paraboloid w/o Radome	From Face	3.00 6.00 1.50	0.0000		60.00	2.00	No Ice 1/2" Ice 1" Ice	3.14 3.41 3.68	0.08 0.02 0.00
Stadium Light (2')	C	Paraboloid w/o Radome	From Face	3.00 -6.00	0.0000		60.00	2.00	No Ice 1/2" Ice	3.14 3.41	0.08 0.02
Stadium Light (2')	C	Paraboloid w/o Radome	From Face	-1.50 3.00 -3.00	0.0000		60.00	2.00	1" Ice No Ice 1/2" Ice	3.68 3.14 3.41	0.00 0.08 0.02
Stadium Light (2')	C	Paraboloid w/o	From	-1.50 3.00	0.0000		60.00	2.00	1" Ice No Ice	3.68 3.14	0.00 0.08
Stadium Light (2')	С	Radome Paraboloid w/o	Face From	0.00 -1.50 3.00	0.0000		60.00	2.00	1/2" Ice 1" Ice No Ice	3.41 3.68 3.14	0.02 0.00 0.08
Stautum Eight (2)	C	Radome	Face	3.00 3.00 -1.50	0.0000		00.00	2.00	1/2" Ice 1" Ice	3.41 3.68	0.08 0.02 0.00
Stadium Light (2')	C	Paraboloid w/o Radome	From Face	3.00 6.00	0.0000		60.00	2.00	No Ice 1/2" Ice	3.14 3.41	0.08 0.02
				-1.50					1" Ice	3.68	0.0

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	0	0	ft
110.00	Platform w/ Handrails	45	20.830	1.6005	0.0046	20057
109.00	Kicker Kit	45	20.498	1.5953	0.0046	20057
100.00	Platform w/ Handrails	45	17.527	1.5440	0.0046	10028
90.00	10' T-Arm - Round (GPD)	45	14.341	1.4609	0.0045	5304
61.50	Stadium Light (2')	45	6.699	1.0313	0.0035	2935
60.00	10' T-Arm - Round (GPD)	45	6.375	1.0044	0.0034	2867
58.50	Stadium Light (2')	45	6.062	0.9774	0.0033	2802

GPD

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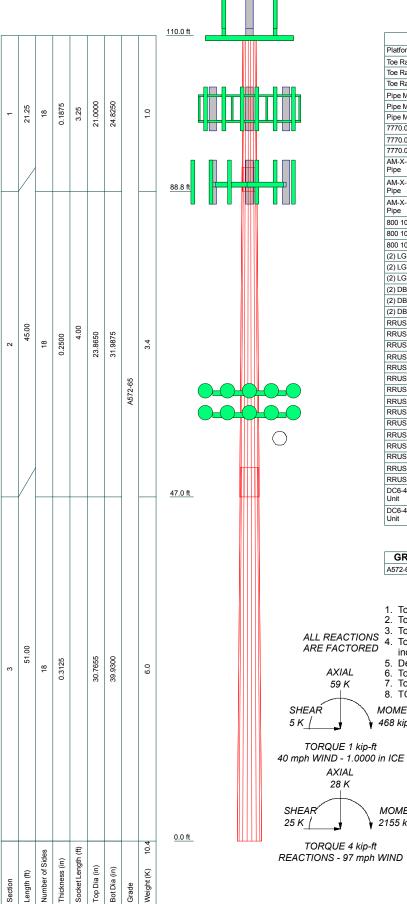
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Project	Date
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Client	Designed by
SAI Communications, Inc.	mschooley

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$ onumber egin{array}{c} $	% Capacity	Pass Fail
L1	110 - 88.75	Pole	TP24.825x21x0.1875	1	-8.47	988.23	43.8	Pass
L2	88.75 - 47	Pole	TP31.9875x23.865x0.25	2	-17.16	1718.42	89.0	Pass
L3	47 - 0	Pole	TP39.93x30.7655x0.3125	3	-28.21	2723.90	98.2	Pass
							Summary	
						Pole (L3)	98.2	Pass
						RATING =	98.2	Pass

APPENDIX C

Tower Elevation Drawing



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Platform w/ Handrails	110	Kicker Kit	109
Toe Rail Reinforcement (L3x3x1/4)	110	Platform w/ Handrails	100
Toe Rail Reinforcement (L3x3x1/4)	110	AIR 21 B2A/B4P w/ Mount Pipe	100
Toe Rail Reinforcement (L3x3x1/4)	110	AIR 21 B2A/B4P w/ Mount Pipe	100
Pipe Mount 6'x2.375"	110	AIR 21 B2A/B4P w/ Mount Pipe	100
Pipe Mount 6'x2.375"	110	AIR32 B66Aa/B2A w/ 60" Mount Pipe	100
Pipe Mount 6'x2.375"	110	AIR32 B66Aa/B2A w/ 60" Mount Pipe	100
7770.00 w/Mount Pipe	110	AIR32 B66Aa/B2A w/ 60" Mount Pipe	100
7770.00 w/Mount Pipe	110	APXVARR24 43 U-NA20 w/ Mount	100
7770.00 w/Mount Pipe	110	Pipe	
AM-X-CD-16-65-00T-RET w/ Mount Pipe	110	APXVARR24_43 U-NA20 w/ Mount Pipe	100
AM-X-CD-16-65-00T-RET w/ Mount Pipe	110	APXVARR24_43 U-NA20 w/ Mount Pipe	100
AM-X-CD-16-65-00T-RET w/ Mount	110	RRUS 4449-B12+71	100
Pipe		RRUS 4449-B12+71	100
800 10798 w/ Mount Pipe	110	RRUS 4449-B12+71	100
800 10798 w/ Mount Pipe	110	10' T-Arm - Round (GPD)	90
800 10798 w/ Mount Pipe	110	10' T-Arm - Round (GPD)	90
(2) LGP21401	110	10' T-Arm - Round (GPD)	90
(2) LGP21401	110	BXA-80063-4CF w/ mount pipe	90
(2) LGP21401	110	BXA-80063-4CF w/ mount pipe	90
(2) DBC0061F1V51-2	110	BXA-80063-4CF w/ mount pipe	90
(2) DBC0061F1V51-2	110	BXA-171063-8BF w/ Mount Pipe	90
(2) DBC0061F1V51-2	110	BXA-171063-8BF w/ Mount Pipe	90
RRUS 11	110	BXA-171063-8BF w/ Mount Pipe	90
RRUS 11	110	BXA-70063-6CF-2 w/ Mount Pipe	90
RRUS 11	110	BXA-70063-6CF-2 w/ Mount Pipe	90
RRUS 12	110	BXA-70063-6CF-2 w/ Mount Pipe	90
RRUS 12	110	10' T-Arm - Round (GPD)	60
RRUS 12	110	10' T-Arm - Round (GPD)	60
RRUS 4478 B5	110	Stadium Light (2')	60
RRUS 4478 B5	110	Stadium Light (2')	60
RRUS 4478 B5	110	Stadium Light (2')	60
RRUS 4426 B66	110	Stadium Light (2')	60
RRUS 4426 B66	110	Stadium Light (2')	60
RRUS 4426 B66	110	Stadium Light (2')	60
RRUS 32	110	Stadium Light (2')	60
RRUS 32	110	Stadium Light (2')	60
RRUS 32	110	Stadium Light (2')	60
DC6-48-60-18-8F Surge Suppression Unit	110	Stadium Light (2')	60
DC6-48-60-18-8C Surge Suppression Unit	110	1	

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
Δ572-65	65 kei	8∩ ksi			

TOWER DESIGN NOTES

- 1. Tower is located in Hartford County, Connecticut.
- 2. Tower designed for Exposure C to the TIA-222-G Standard.
- ALL REACTIONS
 ARE FACTORED

 3. Tower is also designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
 4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with basicht. increase in thickness with height.
 - 5. Deflections are based upon a 60 mph wind.
 - Tower Structure Class II.
 Topographic Category 1
 - Topographic Category 1 with Crest Height of 0.00 ft
 - 8. TOWER RATING: 98.2%

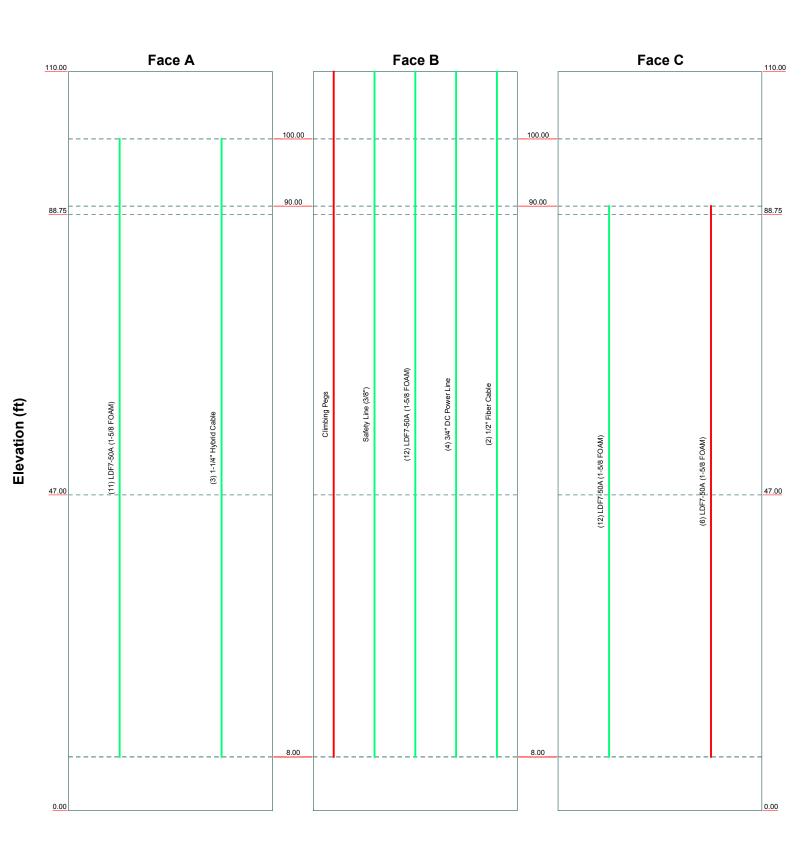
MOMENT 468 kip-ft

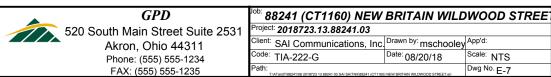
MOMENT 2155 kip-ft

GPD

	^{lob:} 88241 (CT1160) NEW	BRITAIN WILD	WOOD STREE
31	Project: 2018723.13.88241.03		
-	Client: SAI Communications, Inc.	Drawn by: mschooley	App'd:
	Code: TIA-222-G	Date: 08/20/18	Scale: NTS
	Path:		Dwg No. ⊏_1

Round Flat App Out Face Truss Leg

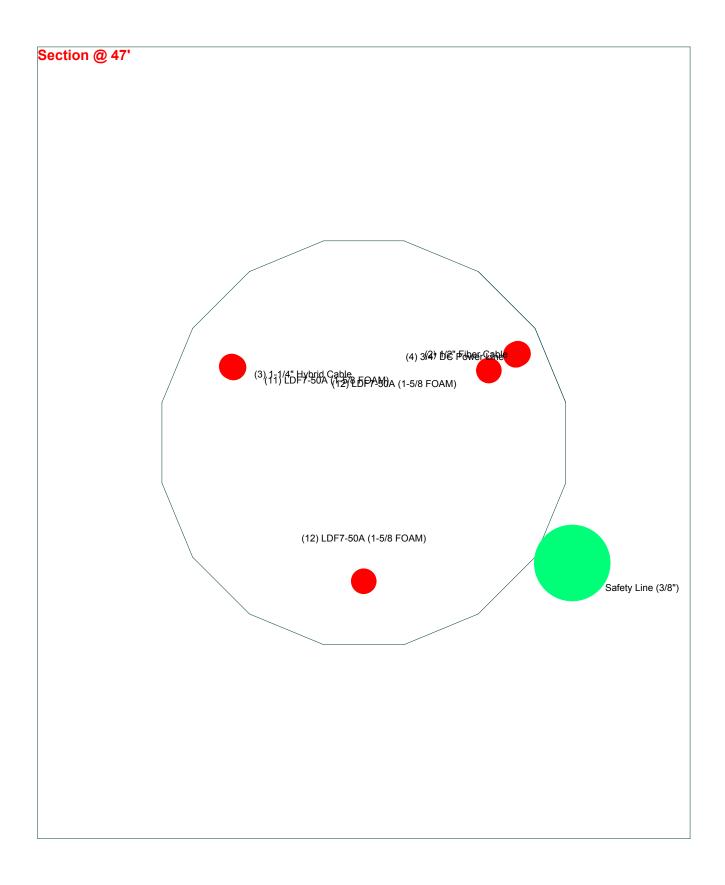




Scale: NTS

Dwg No. E-7

Round _____ Flat ____ App In Face ____ App Out Face



GPD
520 South Main Street Suite 2531
Akron, Ohio 44311
Phone: (555) 555-1234
FAX: (555) 555-1235

^{Job:} 88241 (CT1160) NEW	BRITAIN WILD	WOOD STREE
Project: 2018723.13.88241.03		
Client: SAI Communications, Inc.	Drawn by: mschooley	App'd:
^{Code:} TIA-222-G	Date: 08/20/18	Scale: NTS
Path:	NATIVE PRITAIN WILDWOOD CTREET	Dwg No. E-7

APPENDIX D

Anchor Rod and Base Plate Analysis



Anchor Rod and Base Plate Stresses, TIA-222-G-1 88241 (CT1160) NEW BRITAIN WILDWOOD STREET 2018723.13.88241.03

Overturning Moment =	2155.00	k*ft
Axial Force =	28.00	k
Shear Force =	25.00	k

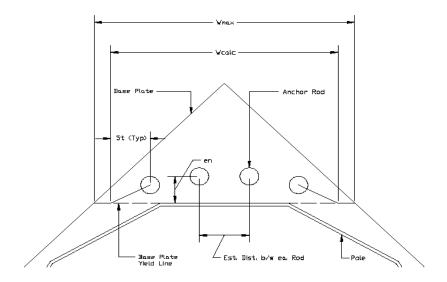


Anchor Rods				
Pole Diameter =	39.93	in		
Number of Rods =	12			
φ =	0.8			
Rod Ultimate Strength (F_u) =	100	ksi		
Base Plate Detail Type* =	d			
Rod Circle =	46	in		
Rod Diameter =	2.25	in		
Net Tensile Area =	3.25	in ²		
Max Tension on Rod =	184.83	kips		
Max Compression on Rod =	189.50	kips		
$P_u =$	189.50	kips		
$V_u =$	2.08	kips		
η =	0.50			
$P_u + V_u / \eta =$	193.67	kips		
$\varphi R_{nt} =$	260.00	kips		
Anchor Rod Capacity =	74.5%	OK		

50	ksi
0.9	
2.5	in
45	in
6	in
36.90	in
23.71	in
23.71	in
37.05	in ³
1400.11	k-in
1667.08	k-in
84.0%	OK
	0.9 2.5 45 6 36.90 23.71 23.71 37.05 1400.11 1667.08

(Section 4.9.9, TIA-222-G-1)

*This analysis assumes the clear distance from the top of the concrete to the bottom of the leveling nut is less than the diameter of the anchor rod. Notify GPD Group immediately if existing field conditions do not meet this assumption.



APPENDIX E

Foundation Analysis



Mat Foundation Analysis 88241 (CT1160) NEW BRITAIN WILDWOOD STREET 2018723.13.88241.03

General Info				
Foundation Criteria	GPD			
TIA Code	TIA-222-G			
Soil Code	AASHTO 2012			
Concrete Code	ACI 318-11			
Seismic Design Category	В			
Tower Height	110 ft			
Bearing On	Soil			
Foundation Type	Monopole Pad			
Pier Type	Square			
Reinforcing Known	Yes			
Max Bearing Capacity	105%			
Max Overturning Capacity	105%			

Tower Reactions					
Moment, M	2155 k-ft				
Axial, P	28 k				
Shear, V	25 k				

Pad & Pier Geometry					
Pier Width, ø	6 ft				
Pad Length, L [y]	21.5 ft				
Pad Width, W [x]	21.5 ft				
Pad Thickness, t	3 ft				
Depth, D	6 ft				
Height Above Grade, HG	0.5 ft				
Tower Centroid, X	10.75 ft				
Tower Centroid, Y	10.75 ft				
Tower Eccentricity	0.0000 ft				

Pad & Pier Reinforcing						
Rebar Fy	60 ksi					
Concrete F'c	3 ksi					
Pier Reinforcing Clear Cover	3 in					
Shear Rebar Type	Tie					
Shear Rebar Size	# 4					
Pad Reinforcing Clear Cover	3 in					
Reinforced Top & Bottom?	Yes					
Pad Reinforcing Size	#8					
Pad Quantity Per Layer	22					
Pier Rebar Size	#8					
Pier Quantity of Rebar	36					

Soil Properties							
Soil Type	Cohesive						
Soil Unit Weight	100 pcf						
Cohesion, Cu (ksf)	0						
Base Friction Coeff. Provided in Geo?	Yes						
Base Friction Coefficient, $\boldsymbol{\mu}$	0.3						
Bearing Type	Gross						
Ultimate Bearing	6 ksf						
Water Table Depth	99 ft						
Frost Depth	3.333 ft						

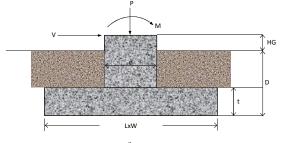
GPD Mat Foundation Analysis - V3.2

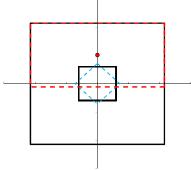
Bearing Summary							
Case Demand/Limits Capacity/Availability Check Eccentricity Load Case							
Qxmax	2.49 ksf	4.50 ksf	OK, <= 105%	L/4.2	1.2D+1.6W		
Qymax	2.49 ksf	4.50 ksf	OK, <= 105%	W/4.2	1.2D+1.6W		
Qmax @ 45°	Qmax @ 45° 2.41 ksf 4.50 ksf OK, <= 105%		W/4.5	0.9D+1.6W			
Controlling C	Controlling Capacity 55.3% Pass		Pass				

Overturning Summary							
Case Demand/Limits Capacity/Availability Check Load Case							
Ovtx	2310.5 k-ft	4877.8 k-ft	63.2%	OK	0.9D+1.6W		
Ovty	2310.5 k-ft	4877.8 k-ft	63.2%	ОК	0.9D+1.6W		
Ovtxy	1634.8 k-ft	3658.3 k-ft	44.7%	ОК	0.9D+1.6W		
Controlling Capacity		63.2%	63.2% Pass				

Sliding Summary						
Case Demand/Limits Capacity/Availability Check Load Case						
Slidingx	25.0 k	83.7 k	29.9%	OK	0.9D+1.6W	
Slidingy	25.0 k	83.7 k	29.9%	ОК	0.9D+1.6W	
Controlling	Controlling Capacity 29.9%		Pas	ss		

Reinforcement Summary									
Component	Demand/Limits	Capacity/Availability	Che	ck	Load Case				
Pad Flexural Bending	42.3 k-ft	111.7 k-ft	37.9% OK		37.9% OK		37.9% OK		0.9D+1.6W
One-Way Shear in Pad	155.9 k	667.7 k	23.3%	ОК	0.9D+1.6W				
Two-Way Shear in Pad	367.1 k	2142.9 k	17.1%	ОК	0.9D+1.6W				
Compression on Pier	50.7 k	17185.0 k	0.3% OK		1.2D+1.6W				
Moment on Pier	2242.5 k-ft	3784.1 k-ft	59.3%	ОК	1.2D+1.6W				
As Min Pad Met?	1.62 sq. in.	0.32 sq. in.	Yes						
As Min Pier Met?	28.44 sq. in.	25.92 sq. in.	Yes]				
Controlling Capacity 59.3%		59.3%	Pas	ss	1				







June 7, 2018



SAI Communications 12 Industrial Way Salem NH, 03079

RE: Site Number: CT1160 (LTE 3C/4C/5C)

 FA Number:
 10050945

 PACE Number:
 MRCTB031100

 PT Number:
 2051A0GJ8C

Site Name: New Britain Wildwood Street

Site Address: Wildwood Street
New Britain, CT 06051

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by SAI Communications to perform a mount analysis on the existing AT&T antenna/RRH mount to determine its capability of supporting the following additional loading:

- (3) Powerwave 7770 Antennas (55.0"x11.0"x5.0" Wt. = 35 lbs. /each)
- (3) AM-X-CD-16-65-00T-RET Antennas (72"x11.8"x5.9" Wt. = 49 lbs. /each)
- (3) RRUS-11 RRH's (19.7"x17.0"x7.2" Wt. = 51 lbs. /each)
- (3) RRUS-12 RRH's (20.4"x18.5"x7.5" Wt. = 58 lbs. /each)
- (6) LGP21401 TMA's (14.4"x9.0"x2.7" Wt. = 19 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7" Φ Wt. = 33 lbs. /each)
- (3) 800-10798 Antennas (86.5"x15.6"x8.3" Wt. = 87 lbs. /each)
- (3) RRUS-32 RRH's (27.2"x12.1"x7.0" Wt. = 60 lbs. /each)
- (3) 4478 B5 RRH's (18.1"x13.4"x8.26" Wt. = 60 lbs. /each)
- (3) 4426 B66 RRH's (15"x13.2"x7.4" Wt. = 49 lbs. /each)
- (1) Squid Surge Arrestor (24.0"x9.7" Φ Wt. = 33 lbs. /each)
- (6) DBC0061F1V51-2 Combiners (8.0"x6.2"x6.5" Wt. = 19 lbs. /each)

No original structural design documents or fabrication drawings were available for the existing mounts. Mount mapping data was provided by SAI Communications.

^{*}Proposed equipment shown in bold

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2012 with 2005 Connecticut Supplement with 2016 Amendments, and AT&T Mount Technical Directive R7.
- HDG considers this mount to be asymmetrical and has applied wind loads in 30 degree increments
 all around the mount. Per TIA-222-G Annex B, the max basic wind speed for this site is equal to 105
 mph with a max basic wind speed with ice of 50 mph. Per the AT&T Mount Technical Directive and
 Appendix N of the Connecticut State Building Code, an ultimate wind speed of 125 mph
 converted to a nominal wind speed of 97 mph was used for this analysis.
- HDG considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.
- HDG considers this site to be topographic category 1; tower is located on flat terrain or the bottom of a hill or ridge.
- The mount has been analyzed with load combinations consisting of 500 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 4.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst
 case location on the mount.

Based on our evaluation, we have determined that the existing mount **IS NOT CAPABLE** of supporting the proposed installation. HDG recommends the following modifications:

• Reinforce existing 3"x3"x1/4" horizontal steel angles with new 3"x3"x1/4" steel angles (typ. of 1 per sector, total of 3).

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Existing 3C/4C/5C Mount Rating	3	IC1	101%	FAIL
Modified 3C/4C/5C Mount Rating	10	LC2	74%	PASS

Reference Documents:

Mount mapping data was provided by SAI Communications.

This determination was based on the following limitations and assumptions:

- 1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
- 2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
- 3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
- 4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
- 5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
- 6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted, Hudson Design Group LLC

Michael Cabral Structural Dept. Head Daniel P. Hamm, PE Principal

FIELD PHOTOS:



























Wind & Ice Calculations

Project Name: New Britain Wildwood Street

Project Number: CT1160

Designed By: AK Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

 $Kzmin \le Kz \le 2.01$

Table 2-4

Exposure	Z _g	α	K _{zmin}	K _e
В	1200 ft	7.0	0.70	0.9
С	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.4 Topographic Factor:

Table 2-5

Topo. Category	K _t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t/K_h)]^2$$
 $K_h = e^{(f^*z/H)}$

K _{zt} = #DIV/0!	$K_h =$	#DIV/0!
	K _e =	0 (from Table 2-4)
(If Category 1 then $K_{zt} = 1.0$)	K _t =	0 (from Table 2-5)
	f=	0 (from Table 2-5)
Category= 1	z=	114
1	H=	0 (Ht. of the crest above surrounding terrain)
	K _{zt} =	1.00
	$K_{iz} =$	1.13 (from Sec. 2.6.8)

2.6.8 Design Ice Thickness

 $\label{eq:max_loss} \text{Max Ice Thickness} = & t_i = & 1.00 \text{ in} \\ \\ t_{iz} = 2.0^* t_i^* l^* K_{iz}^* (Kzt)^{0.35} & t_{iz} = & 2.26 \text{ in} \\ \\ \end{cases}$

Project Name: New Britain Wildwood Street

Project Number: CT1160

Designed By: AK Checked By: MSC



2.6.7 Gust Effect Factor

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

Gh = 0.85 + 0.15 [h/150 - 3.0]

h= ht. of structure

 h=
 115
 Gh=
 0.85

 2.6.7.2 Guyed Masts
 Gh=
 0.85

 2.6.7.3 Pole Structures
 Gh=
 1.1

 2.6.9 Appurtenances
 Gh=
 1.0

2.6.7.4 Structures Supported on Other Structures

(Cantilivered tubular or latticed spines, pole, structures on buildings (ht.: width ratio > 5)

Gh= 1.35 Gh= 1.00

2.6.9.2 Design Wind Force on Appurtenances

State Code Ultimate Design Wind Speed: V_{ult} =

Nomial Design Wind Speed, $V_{asd} = V_{ult} V(0.6)$ $V_{asd} = 97 \text{ mph}$

 $V_{asd} \ per \ the \ AT\&T \ Mount \ Technical \ Directive \ and \ Connecticut \ State \ Building \ Code, \ Latest \ Edition.$

Per TIA-222-G, $V_{min} = 90 \text{ mph}$ $V_{max} = 105 \text{ mph}$

F= qz*Gh*(EPA)A

> $K_{zt} = 1.0$ $K_{d} = 0.95$

 q_z = 23.39 K_d = 0.95 q_z (ice) = 6.24 V_{asd} = 97 mph q_z (30) = 2.25 V_{max} (ice) = 50 mph

V₃₀= 30 mph l= 1.0

125 mph

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95

Project Name: New Britain Wildwood Street

Project Number: CT1160

Designed By: AK Checked By: MSC



Determine Ca:

Table 2-8

	F	orce Coefficients (Ca) for	Appurtenances	
		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
M	ember Type	Ca	Ca	Ca
	Flat	1.2	1.4	2.0
Round	C < 32	0.7	0.8	1.2
	(Subcritical)	0.7	0.8	1.2
	32 ≤ C ≤ 64	4 -0 485	0.0-1/00.415	00.4451.0
	(Transitional)	3.76/(C ^{0,485})	3.37/(C ^{0,415})	38.4/(C ^{.1.0})
	C > 64	0.5	0.6	0.6
	(Supercritical)	0.5	0.6	0.0

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.

(Aspect ratio is independent of the spacing between support points of a linear appurtenance,

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness =	2.26	in	Angle =	0 (deg)		Equival	ent Angle =	180 (deg)	
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area	Aspect Ratio	<u>Ca</u>	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	5.00	1.31	129	52	12
800-10798 Antenna	86.5	15.6	8.3	9.37	5.54	1.34	293	106	28
AM-X-CD-16-65-00T-RET Antenr	72.0	11.8	5.9	5.90	6.10	1.36	188	74	18
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 1.1	7.0 7.0	2.29 0.21	2.25 24.73	1.20 1.99		27 15	6 1
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.35 7.54	1.20 1.42		21 10	5 1
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.35 7.54	1.20 1.42		21 10	5 1
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 6.0	7.2 7.2	2.33 0.82	1.16 3.28	1.20 1.23		27 14	6 2
RRUS-12 RRH RRUS-12 RRH	20.4 20.4	18.5 7.5	7.5 7.5	2.62 1.06	1.10 2.72	1.20 1.21		30 16	7 3
2" Pipe	2.4	12.0		0.20	0.20	1.20	6	6	. 1
3x3 Angle	3.0	12.0		0.25	0.25	2.00	12	11	1

Project Name: New Britain Wildwood Street

Project Number: CT1160



Angle = 30	(deg)	ř.	Ice Thick	1955 =	2.26	in.	i	1	Eouiva	lent Angle =	210	(deg)
Aligie – 30	(uce)	h	ice micki	11233 -			ı		-4			10/
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	Depth	(normal)	flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	<u>Ca</u> (side)	(normal)	Force (lbs) (side)	Force (lbs) (angle)
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1.31	1,53	129	68	114
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5.54	10.42	1,34	1.51	293	177	264
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5,9	5.90	2.95	6.10	12.20	1.36	1.57	188	109	168
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3,89	1.20	1.26	64	39	58
RRUS-32 RRH (Shielded)	27.2	6.1	7.0	1.14	1.32	4.50	3,89	1.29	1.26	34	39	36
4478 B5 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2,19	1,20	1.20	47	29	43
4478 B5 RRH (Shielded)	18.1	6.7	8,3	0.84	1.04	2.70	2.19	1,21	1.20	24	29	25
4426 B66 RRH	18.1	13.4	8,3	1.68	1.04	1.35	2.19	1.20	1.20	47	29	43
4426 B66 RRH (Shielded)	18.1	6.7	8,3	0.84	1.04	2.70	2,19	1,21	1.20	24	29	25
RRUS-11 RRH	19.7	17.0	7.2	2.93	0.99	1.16	2,74	1.20	1,21	65	28	56
RRUS-11 RRH (Shielded)	19.7	8.5	7.2	1.16	0.99	2.32	2.74	1,20	1.21	33	28	31
RRUS-12 RRH	20.4	18.5	7.5	2,62	1.06	1,10	2.72	1,20	1.21	74	30	63
RRUS-12 RRH WIND LOADS WITH ICE:	20.4	7.5	7.5	1.06	1,06	2.72	2.72	1.21	1.21	30	30	30
Powerwave 7770 Antenna	59.5	15.5	9.5	6.42	3.94	3,83	6.25	1,26	1.37	50	34	46
800-10798 Antenna	91.0	20.1	12.8	12.72	8.11	4.52	7,10	1.29	1.40	102	71	95
AM-X-CD-16-65-00T-RET Antenna	76.5	16,3	10.4	8.68	5.54	4.69	7,34	1.30	1.41	70	49	65
RRUS-32 RRH	31.7	16.6	11.5	3,66	2.54	1,91	2.75	1,20	1.21	27	19	25
RRUS-32 RRH (Shielded)	31.7	8.3	11.5	1.83	2.54	3,82	2.75	1,26	1.21	14	19	16
4478 B5 RRH	22.6	17.9	12.8	2.82	2,01	1.26	1.77	1.20	1.20	21	15	20
4478 B5 RRH (Shielded)	22.6	9.0	12.8	1.41	2.01	2.52	1.77	1.20	1.20	11	15	12
4426 B66 RRH	22.6	17.9	12.8	2.82	2.01	1,26	1.77	1.20	1.20	21	15	20
4426 B66 RRH (Shielded)	22.6	9.0	12.8	1.41	2.01	2.52	1.77	1,20	1.20	11	15	12
RRU5-11 RRH	24.2	21.5	11.7	3.62	1.97	1,13	2,07	1.20	1,20	27	15	24
RRUS-11 RRH (Shielded)	24.2	10.8	11.7	1.81	1.97	2.25	2,07	1.20	1.20	14	15	14
RRUS-12 RRH	24.9	23.0	12.0	3.99	2.08	1.08	2.07	1.20	1.20	30	16	26
RRUS-12 RRH #REF!	24.9 #REF!	12.0 #REF	12.0 #REF!	2.08 #REFI	2.08 #REF!	2.07 #REF!	2.07 #REF!	1,20 #REF!	1.20 #REF!	16 #REF!	16 #REF!	16 #REF!
WIND LOADS AT 30 MPH:												
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1,91	5.00	11.00	1.31	1.53	12	7	11
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5.54	10.42	1,34	1.51	28	17	25
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5,9	5.90	2.95	6.10	12.20	1.36	1,57	18	10	16
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3,89	1.20	1.26	6	4	6
RRUS-32 RRH (Shielded)	27.2	6.1	7.0	1.14	1,32	4.50	3,89	1.29	1.26	3	4	3
4478 B5 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.19	1,20	1.20	5	3	4
4478 B5 RRH (Shielded)	18.1	6.7	8.3	0.84	1.04	2.70	2.19	1.21	1.20	2	3	2
4426 B66 RRH	18.1	13.4	8.3	1.68	1.04	1,35	2.19	1,20	1.20	5	3	4
4426 B66 RRH (Shielded)	18.1	6.7	8,3	0.84	1.04	2.70	2.19	1.21	1.20	2	3	2
RRUS-11 RRH	19.7	17.0	7.2	2,33	0.99	1.16	2.74	1.20	1.21	6	3	5 3
RRUS-11 RRH (Shielded)	19.7	8.5	7.2	1,16	0.99	2.32	2.74	1.20	1.21	3	3	3
RRUS-12 RRH	20.4	18.5	7.5	2.62	1.06	1.10	2.72	1.20	1,21	7	3	6

Project Name: New Britain Wildwood Street

Project Number: CT1160



Angle = 60	(deg)		Ice Thick	ness =	2.26	in.		[Equiva	lent Angle =	240	(deg)
WIND LOADS WITH NO ICE:												
<u>Appurtenances</u>	<u>Height</u>	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
Powerwave 7770 Antenna	55.0	11.0	5,0	4.20	1.91	5.00	11,00	1.31	1,53	129	68	84
800-10798 Antenna	86.5	15.6	8,3	9.37	4.99	5.54	10.42	1.34	1,51	293	177	206
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1,36	1.57	188	109	128
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3,89	1.20	1,26	64	39	45
RRUS-32 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3.89	1.22	1,26	49	39	42
4478 B5 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.19	1,20	1.20	47	29	34
4478 B5 RRH (Shielded)	18.1	10.1	8,3	1.26	1.04	1.80	2,19	1.20	1.20	35	29	31
4426 B66 RRH	18.1	13.4	8.3	1.68	1.04	1,35	2.19	1,20	1.20	47	29 29	34 31
4426 B66 RRH (Shielded)	18.1	10.1	8.3	1.26	1.04	1.80	2.19	1,20	1.20	35		
RRUS-11 RRH	19.7	17.0	7.2	2.33 1.74	0.99	1.16 1.55	2.74 2.74	1,20 1,20	1.21 1.21	65 49	28 28	37 33
RRUS-11 RRH (Shielded)	19.7	12.8	7.2									
RRUS-12 RRH RRUS-12 RRH	20.4 20.4	18.5 7.5	7.5 7.5	2.62 1.06	1.06 1.06	1.10 2.72	2.72 2.72	1.20 1.21	1,21 1,21	74 30	30 30	41 30
WIND LOADS WITH ICE:	20,4	7.5		2,00	2.00							
Powerwave 7770 Antenna	59.5	15.5	9.5	6.42	3.94	3,83	6.25	1.26	1.37	50	34	38
800-10798 Antenna	91.0	20.1	12.8	12.72	8.11	4.52	7,10	1.29	1.40	102	71	79
AM-X-CD-16-65-00T-RET Antenna	76.5	16.3	10.4	8.68	5.54	4,69	7.34	1.30	1.41	70	49	54
RRUS-32 RRH	31.7	16.6	11.5	3.66	2.54	1.91	2.75	1.20	1,21	27	19	21
RRUS-32 RRH (Shielded)	31.7	12.5	11.5	2.75	2.54	2.54	2.75	1,20	1.21	21	19	20
4478 B5 RRH	22.6	17.9	12.8	2.82	2.01	1:26	1.77	1.20	1.20	21	15	17
4478 B5 RRH (Shielded)	22.6	13.4	12.8	2.11	2.01	1.68	1.77	1.20	1.20	16	15	15
4426 B66 RRH	22.6	17.9	12.8	2.82 2.11	2.01 2.01	1,26 1,68	1.77 1.77	1.20 1.20	1.20 1.20	21 16	15 15	17 15
4426 B66 RRH (Shielded)	22.6	13.4	12.8	2.11	2.01	1,00	1,77	1,20	1.20			
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.2 24.2	21.5 16.1	11.7 11.7	3.62 2.72	1.97 1.97	1.13 1.50	2.07 2.07	1.20 1.20	1.20 1.20	27 20	15 15	18 16
NNO3-11 NNN (Sillelded)	24.2	10,1										
RRUS-12 RRH RRUS-12 RRH	24.9 24.9	23.0 12.0	12.0 12.0	3.99 2.08	2.08	1.08 2.07	2.07 2.07	1,20 1,20	1.20 1.20	30 16	16 16	19 16
#REF!	#REFI	#REFI		#REF!	#REFI	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!
WIND LOADS AT 30 MPH:												
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1,31	1.53	12	7	8
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5.54	10.42	1.34	1.51	28	17	20
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5,9	5.90	2.95	6.10	12.20	1.36	1.57	18	10	12
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	6	4	4
RRUS-32 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3.89	1.22	1,26	5	4	
4478 B5 RRH	18.1	13.4 10.1	8.3 8.3	1.68 1.26	1.04 1.04	1.35 1.80	2.19 2.19	1.20 1.20	1.20 1.20	5 3	3	3
4478 B5 RRH (Shielded)	18.1	10.1										
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 10.1	8.3 8.3	1.68 1.26	1.04 1.04	1.35 1.80	2.19 2.19	1.20 1.20	1.20 1.20	5 3	3	3
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1,20	1.21	6	3	4
RRUS-11 RRH (Shielded)	19.7	12.8	7.2	1.74	0.99	1.55	2.74	1.20	1.21	5	3	3
RRUS-12 RRH	20.4	18.5	7.5	2,62	1.06	1.10	2.72	1.20	1-21	7	3	4

Project Name: New Britain Wildwood Street

Project Number: C11160



Angle = 90	(deg)		Ice Thick	ness =	2.26	in.		1	Equiva	lent Angle =	270	(deg)
All Bic -	14-8/				3758							
WIND LOADS WITH NO ICE:												
Appurtenances	<u>Height</u>	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs (angle)
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1,31	1,53	129	68	68
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5,54	10.42	1.34	1.51	293	177	177
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12,20	1.36	1.57	188	109	109
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 1.1	7.0 7.0	2.29 0.21	1.32 1.32	2.25 24.73	3.89 3.89	1.20 1.99	1,26 1,26	64 10	39 39	39 39
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.04 1.04	1.35 7.54	2.19 2.19	1,20 1,42	1,20 1,20	47 10	29 29	29 29
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.04 1.04	1.35 7.54	2.19 2.19	1.20 1.42	1.20 1.20	47 10	29 29	29 29
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 6.0	7.2 7.2	2.33 0.82	0.99 0.99	1,16 3.28	2.74 2.74	1.20 1.23	1.21 1.21	65 24	28 28	28 28
RRUS-12 RRH RRUS-12 RRH WIND LOADS WITH ICE:	20.4 20.4	18.5 7.5	7.5 7.5	2.62 1.06	1.06 1.06	1.10 2.72	2.72 2.72	1.20 1.21	1.21 1.21	74 30	30 30	30 30
Powerwave 7770 Antenna	59.5	15.5	9.5	6.42	3.94	3.83	6.25	1.26	1.37	50	34	34
800-10798 Antenna	91.0	20.1	12.8	12.72	8.11	4,52	7.10	1.29	1.40	102	71	71
AM-X-CD-16-65-00T-RET Antenna	76.5	16.3	10.4	8.68	5.54	4.69	7,34	1,30	1.41	70	49	49
RRUS-32 RRH RRUS-32 RRH (Shielded)	31.7 31.7	16.6 5.6	11.5 11.5	3.66 1.24	2.54 2.54	1.91 5.64	2.75 2.75	1.20 1,34	1.21 1.21	27 10	19 19	19 19
4478 B5 RRH 4478 B5 RRH (Shielded)	22.6 22.6	17.9 6.9	12.8 12.8	2.82 1.09	2.01 2.01	1.26 3.27	1.77 1.77	1.20 1.23	1.20 1.20	21 8	15 15	15 15
4426 B66 RRH 4426 B66 RRH (Shielded)	22.6 22.6	17.9 6.9	12.8 12.8	2.82 1.09	2.01	1.26 3.27	1.77 1.77	1.20 1.23	1.20 1.20	21 8	15 15	15 15
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.2 24.2	21.5 10.5	11.7 11.7	3.62 1.77	1.97 1.97	1.13 2.30	2,07 2.07	1.20 1.20	1.20 1.20	27 13	15 15	15 15
RRUS-12 RRH RRUS-12 RRH #REF!	24.9 24.9 #REFI	23.0 12.0 #REF!	12.0 12.0 #REF!	3.99 2.08 #REF!	2.08 2.08 #REFI	1.08 2.07 #REF!	2,07 2.07 #REF!	1,20 1,20 #REF!	1.20 1.20 #REF!	30 16 #REF!	16 16 #REFI	16 16 #REFI
WIND LOADS AT 30 MPH:												
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11,00	1,31	1.53	12	7	7
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5.54	10.42	1.34	1.51	28	17	17
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1.36	1.57	18	10	10
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 1.1	7.0 7.0	2.29 0.21	1.32 1.32	2.25 24.73	3.89 3.89	1.20 1.99	1.26 1.26	6 1	4	4
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.04 1.04	1.35 7.54	2.19 2.19	1.20 1.42	1.20 1.20	5 1	3	3
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 2.4	8.3 8.3	1.68 0.30	1.04 1.04	1,35 7.54	2.19 2.19	1.20 1.42	1.20 1.20	5 1	3	3
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 6.0	7.2 7.2	2.33 0.82	0.99 0.99	1.16 3,28	2.74 2.74	1.20 1.23	1.21 1.21	6 2	3	3
	20.4	18.5	7.5	2,62	1.06	1.10	2.72	1.20	1,21	7	3	3

Date:

Project Name: New Britain Wildwood Street

Project Number: CT1160
Designed By: AK Checked By: MSC



Angle = 120	(deg)		Ice Thick	ness =	2.26	in.		Г	Equiva	lent Angle =	300	(deg)
								•				
WIND LOADS WITH NO ICE:												
Appurtenances	Height	Width	<u>Depth</u>	Flat Area (normal)	(side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	(normal)	Force (lbs) (side)	Force (lbs) (angle)
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11.00	1,31	1.53	129	68	84
800-10798 Antenna	86.5	15.6	8,3	9.37	4.99	5.54	10.42	1,34	1,51	293	177	206
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12,20	1.36	1,57	188	109	128
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1,20	1.26	64	39	45
RRUS-32 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3.89	1.22	1,26	49	39	42
4478 B5 RRH	18.1	13.4	8,3	1.68	1.04	1,35	2.19	1.20	1.20	47	29	34
4478 85 RRH (Shielded)	18.1	10.1	8.3	1.26	1.04	1.80	2.19	1,20	1.20	35	29	31
4426 B66 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.19	1.20	1.20	47	29	34
4426 B66 RRH (Shielded)	18.1	10.1	8,3	1.26	1.04	1.80	2.19	1,20	1.20	35	29	31
RRUS-11 RRH	19.7	17.0	7.2	2.33	0,99	1.16	2,74	1.20	1,21	65	28	37
RRUS-11 RRH (Shielded)	19.7	12.8	7.2	1.74	0.99	1,55	2.74	1.20	1,21	49	28	33
RRUS-12 RRH	20.4	18.5	7.5	2.62	1.06	1.10	2.72	1.20	1.21	74	30	41
RRUS-12 RRH WIND LOADS WITH ICE:	20.4	7.5	7.5	1.06	1.06	2.72	2.72	1,21	1.21	30	30	30
Powerwave 7770 Antenna	59.5	15.5	9.5	6,42	3.94	3,83	6,25	1.26	1,37	50	34	38
800-10798 Antenna	91.0	20.1	12.8	12.72	8.11	4.52	7.10	1.29	1.40	102	71	79
AM-X-CD-16-65-00T-RET Antenna	76.5	16,3	10.4	8.68	5.54	4.69	7.34	1.30	1.41	70	49	54
RRUS-32 RRH	31.7	16.6	11.5	3.66	2.54	1,91	2.75	1.20	1.21	27	19	21
RRUS-32 RRH (Shielded)	31.7	12.5	11.5	2.75	2.54	2,54	2.75	1.20	1.21	21	19	20
4478 B5 RRH	22.6	17.9	12.8	2.82	2.01	1.26	1.77	1,20	1.20	21 16	15 15	17 15
4478 B5 RRH (Shielded)	22.6	13.4	12.8	2.11	2,01	1.68	1,77	1.20	1.20			
4426 B66 RRH	22.5	17.9	12.8	2.82	2.01	1.26	1.77	1.20	1,20	21	15 15	17 15
4426 B66 RRH (Shielded)	22.6	13.4	12.8	2.11	2.01	1.68	1.77	1.20	1,20	16	12	15
RRUS-11 RRH	24.2	21.5	11.7	3.62	1.97	1.13	2.07	1.20	1.20	27 20	15 15	18 16
RRUS-11 RRH (Shielded)	24.2	16.1	11.7	2.72	1.97	1.50	2,07	1,20	1.20			
RRUS-12 RRH	24.9	23.0	12.0	3.99	2.08	1.08 2.07	2,07 2.07	1.20 1.20	1,20 1,20	30 16	16 16	19 16
RRU5-12 RRH #REF!	24.9 #REFI	12.0 #REFI	12.0 #REF!	2.08 #REF!	#REFI	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!
WIND LOADS AT 30 MPH:												
Powerwave 7770 Antenna	55.0	11.0	5.0	4.20	1.91	5.00	11,00	1.31	1,53	12	7	
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5,54	10.42	1.34	1.51	28	17	20
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12.20	1,36	1.57	18	10	12
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	6	4	4
RRUS-32 RRH (Shielded)	27.2	9.1	7.0	1.71	1.32	3.00	3,89	1.22	1.26	5	4	4
4478 B5 RRH	18.1	13.4	8,3	1.68	1.04	1.35	2.19	1.20	1,20	5	3	3
4478 B5 RRH (Shielded)	18.1	10.1	8.3	1.26	1.04	1.80	2.19	1.20	1,20	3	3	3
4426 B66 RRH	18.1	13.4	8,3	1.68	1.04	1.35	2.19	1.20	1.20	5	3	3
4426 B66 RRH (Shielded)	18.1	10.1	8.3	1.26	1.04	1.80	2.19	1.20	1.20	3	3	
RRUS-11 RRH	19.7	17.0	7.2	2.33	0.99	1.16	2.74	1.20	1.21 1.21	6 5	3	4
RRUS-11 RRH (Shielded)	19.7	12.8	7.2	1.74	0.99	1.55	2,74	1.20	1.21	•	•	•
RRUS-12 RRH	20.4	18.5	7.5	2.62	1.06	1.10	2.72	1.20	1.21	7	3	4

Date:

6/7/2018

Project Name: New Britain Wildwood Street

Project Number: CT1160



Angle = 150	(deg)		Ice Thick	noss =	2.26	in.		г	Fanises	lent Angle =	330	(deg)
Angle = 150	(deg)		ice inicki	ness =	2.20	in.		L	Equiva	ient Angle –	330	(deg)
WIND LOADS WITH NO ICE:												
Appurtenances	Height	Width	<u>Depth</u>	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	<u>Ca</u> (normal)	<u>Ca</u> (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs)
Powerwave 7770 Antenna	55.0	11.0	5,0	4.20	1.91	5,00	11.00	1.31	1,53	129	68	114
800-10798 Antenna	86.5	15.6	8,3	9.37	4.99	5.54	10.42	1.34	1.51	293	177	264
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5.9	5.90	2.95	6.10	12,20	1.36	1,57	188	109	168
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 5.1	7.0 7.0	2.29 1.14	1.32 1.32	2.25 4.50	3.89 3.89	1.20 1.29	1,26 1,26	64 34	39 39	58 36
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 6.7	8,3 8,3	1.68 0.84	1.04 1.04	1.35 2.70	2.19 2.19	1.20 1.21	1.20 1,20	47 24	29 29	43 25
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 6.7	8,3 8.3	1.68 0.84	1.04 1.04	1.35 2.70	2.19 2.19	1.20 1.21	1.20 1.20	47 24	29 29	43 25
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 8.5	7.2 7.2	2.33 1.16	0.99 0.99	1.16 2.32	2,74 2.74	1.20 1.20	1,21 1.21	65 33	28 28	56 31
RRUS-12 RRH RRUS-12 RRH	20.4 20.4	18.5 7.5	7.5 7.5	2,62 1.05	1.06 1.06	1.10 2.72	2.72 2.72	1.20 1.21	1,21 1,21	74 30	30 30	63 30
WIND LOADS WITH ICE: Powerwave 7770 Antenna	59.5	15.5	9.5	6.42	3.94	3.83	6,25	1.26	1.37	50	34	46
800-10798 Antenna	91.0	20.1	12.8	12.72	8.11	4.52	7.10	1.29	1,40	102	71	95
AM-X-CD-16-65-00T-RET Antenna	76.5	16.3	10.4	8.68	5.54	4.69	7.34	1.30	1.41	70	49	65
RRUS-32 RRH RRUS-32 RRH (Shielded)	31.7 31.7	16.6 8.3	11.5 11.5	3.66 1.83	2.54 2.54	1.91 3.82	2.75 2.75	1.20 1.26	1.21 1.21	27 14	19 19	25 16
4478 B5 RRH 4478 B5 RRH (Shielded)	22.6 22.6	17.9 9.0	12.8 12.8	2.82 1.41	2.01 2.01	1.26 2.52	1.77 1.77	1.20 1.20	1,20 1.20	21 11	15 15	20 12
4426 B66 RRH 4426 B66 RRH (Shielded)	22.6 22.6	17.9 9.0	12.8 12.8	2.82 1.41	2.01 2.01	1.26 2.52	1.77 1.77	1.20 1.20	1.20 1.20	21 11	15 15	20 12
RRUS-11 RRH RRUS-11 RRH (Shielded)	24.2 24.2	21.5 10.8	11.7 11.7	3.62 1.81	1.97 1.97	1.13 2.25	2.07 2.07	1.20 1.20	1.20 1,20	27 14	15 15	24 14
RRUS-12 RRH RRUS-12 RRH #REF!	24.9 24.9 #REFI	23.0 12.0 #REFI	12.0 12.0 #REFI	3.99 2.08 #REFI	2.08 2.08 #REFI	1.08 2.07 #REF!	2.07 2.07 #REF!	1.20 1.20 #REF!	1.20 1.20 #REF!	30 16 #REF!	16 16 #REF!	26 16 #REFI
WIND LOADS AT 30 MPH:												
Powerwave 7770 Antenna	55,0	11.0	5,0	4,20	1.91	5.00	11,00	1.31	1.53	12	7	11
800-10798 Antenna	86.5	15.6	8.3	9.37	4.99	5.54	10.42	1.34	1.51	28	17	25
AM-X-CD-16-65-00T-RET Antenna	72.0	11.8	5,9	5,90	2.95	6.10	12.20	1.36	1.57	18	10	16
RRUS-32 RRH RRUS-32 RRH (Shielded)	27.2 27.2	12.1 6.1	7.0 7.0	2.29 1.14	1.32 1.32	2.25 4.50	3.89 3.89	1.20 1.29	1.26 1.26	6 3	4	6 3
4478 B5 RRH 4478 B5 RRH (Shielded)	18.1 18.1	13.4 6.7	8.3 8.3	1.68 0,84	1.04 1.04	1.35 2.70	2.19 2.19	1.20 1.21	1.20 1.20	5 2	3	4 2
4426 B66 RRH 4426 B66 RRH (Shielded)	18.1 18.1	13.4 6.7	8.3 8.3	1.68 0.84	1.04 1.04	1.35 2,70	2.19 2.19	1.20 1.21	1,20 1,20	5 2	3 3	4 2
RRUS-11 RRH RRUS-11 RRH (Shielded)	19.7 19.7	17.0 8.5	7.2 7.2	2.33 1.16	0.99 0.99	1,16 2,32	2.74 2.74	1.20 1.20	1.21 1,21	6 3	3	5 3
RRUS-12 RRH	20.4	18.5	7.5	2.62	1.06	1.10	2.72	1.20	1.21	7 3	3	6

Project Name: New Britain Wildwood Street

Project Number: CT1160

Designed By: AK Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice: 1 in. Density of ice: 56 pcf

7770 Antenna

Weight of ice based on total radial SF area: Height (in): Width (in): 11.0 Depth (in): 5.0

Total weight of ice on object: 70 lbs

Weight of object:

Combined weight of ice and object: 105 lbs

800-10798 Antenna

Weight of ice based on total radial SF area:

Height (in): Width (in): Depth (in):

15.6 8.3

18.5

7.5

35 lbs

Total weight of ice on object:

157 lbs

Weight of object:

87 lbs

Combined weight of ice and object:

244 lbs

RRUS-12 RRH

Weight of ice based on total radial SF area:

Height (in): Width (in): Depth (in):

Total weight of ice on object:

50 lbs

Weight of object:

58 lbs Combined weight of ice and object: 108 lbs

4478 B5 RRH

Weight of ice based on total radial SF area:

Height (in): 18.1 Width (in): 13.4 Depth (in):

Total weight of ice on object: 38 lbs

Weight of object:

60 lbs Combined weight of ice and object: 98 lbs

LGP21401 TMA

Weight of ice based on total radial SF area:

Height (in): 14.4 Width (in): 9.0 Depth (in): 2.7

Total weight of ice on object:

16 lbs

Weight of object:

19 lbs Combined weight of ice and object: 35 lbs

DBC0061F1V51-2 Combiner

Weight of ice based on total radial SF area:

8.0 Height (in): Width (in): 6.2 6.5 Depth (in):

Total weight of ice on object:

12 lbs

Weight of object:

19 lbs

Combined weight of ice and object:

31 lbs

HSS 4x4

Weight of ice based on total radial SF area:

Height (in): Width (in):

Per foot weight of ice on object: 8 plf AM-X-CD-14-65-OOT-RET Antenna

Weight of ice based on total radial SF area: Height (in): 72.0 Width (in): 11.8 5.9 Depth (in):

Total weight of ice on object: 99 lbs

Weight of object: 49 lbs

Combined weight of ice and object: 148 lbs

RRUS-11 RRH

Weight of ice based on total radial SF area: Height (in):

Width (in): Depth (in):

7.2

17.0

Total weight of ice on object:

45 lbs

45 lbs

105 lbs

Weight of object:

51 lbs 96 lbs

Combined weight of ice and object:

RRUS-32 RRH

Weight of ice based on total radial SF area:

Height (in): 27.2 12.1 Width (in): 7.0

Depth (in): Total weight of ice on object:

60 lbs Weight of object:

Combined weight of ice and object:

4426 B66 RRH

Weight of ice based on total radial SF area:

15.0 Height (in): 13.2 Width (in):

Depth (in): 7.4

Total weight of ice on object: 31 lbs

49 lbs Weight of object:

Combined weight of ice and object: 80 lbs

Squid Surge Arrestor

Weight of ice based on total radial SF area:

Depth (in): Diameter(in): 24.0 9.7

Total weight of ice on object:

35 lbs

Weight of object:

33 lbs Combined weight of ice and object:

2" pipe

Per foot weight of ice:

diameter (in):

4 plf Per foot weight of ice on object:

L3x3x1/4 Angles

Weight of ice based on total radial SF area:

Thickness (in):

0.25

Height (in): Width (in):

3

Per foot weight of ice on object: 7 plf



Mount Calculations (Unmodified 3C/4C/5C Configuration)

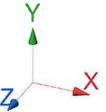


Bentley

Current Date: 6/7/2018 12:15 PM

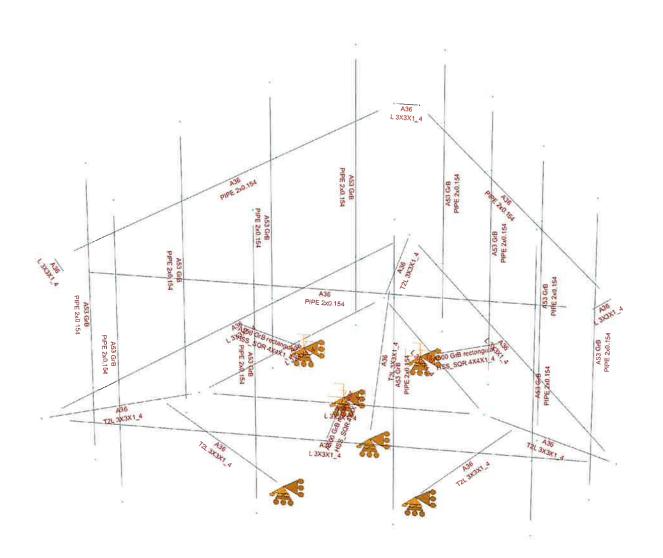
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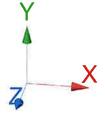






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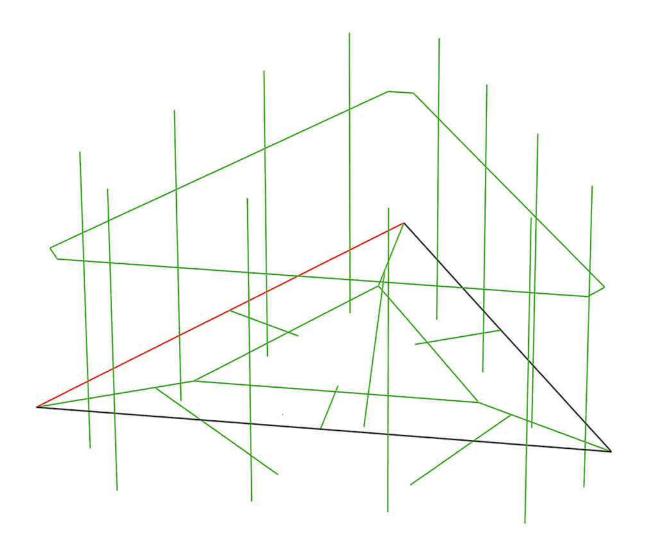


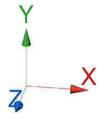


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Design status

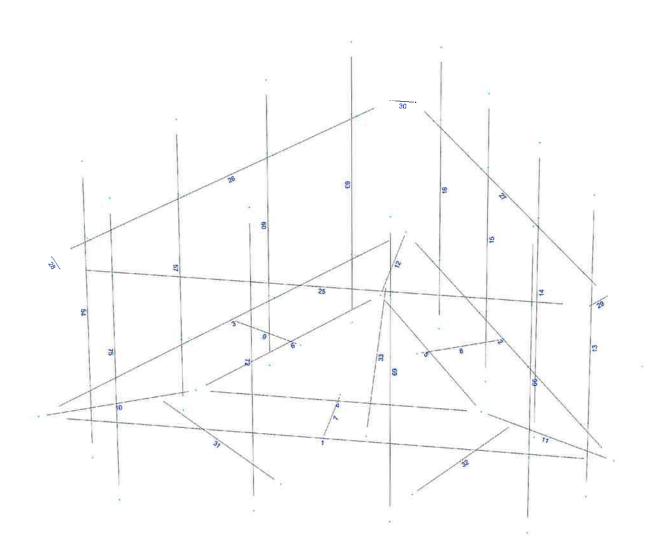


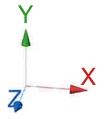






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Units system: English

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Load data

GLOSSARY

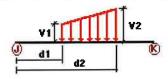
Comb

Indicates if load condition is a load combination

Load conditions

Condition	Description	Comb.	Category
DL	Dead Load	No	DL
W0	Wind Load 0/60/120 deg	No	WIND
W30	Wind Load 30/90/150 deg	No	WIND
Di	Ice Load	No	LL
Wi0	Ice Wind Load 0/60/120 deg	No	WIND
Wi30	Ice Wind Load 30/90/150 deg	No	WIND
WL0	WL 30 mph 0/60/120 deg	No	WIND
WL30	WL 30 mph 30/90/150 deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load End of Mount	No	LL
LLa1	500 lb Live Load on Antenna 1	No	LL
LLa2	500 lb Live Load on Antenna 2	No	LL
LLa3	500 lb Live Load on Antenna 3	No	LL
LLa4	500 lb Live Load on Antenna 4	No	LL
W180	-W0	Yes	
W210	-W30	Yes	
Wi180	-Wi0	Yes	
Wi210	-Wi30	Yes	
WL180	-WL0	Yes	
WL210	-WL30	Yes	

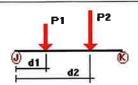
Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
DL	4	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	5	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	6	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	7	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	8	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
	9	Υ	-0.01	-0.01	0.00	Yes	100.00	Yes
W0	1	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	2	Z	-0.012	-0.012	0.00	Yes	100.00	Yes
	3	Z	-0.012	-0.012	0.00	Yes	100.00	Yes

	25	Z	-0.006	-0.006	0.00	Yes	100.00	Yes
	26	Z	-0.006	-0.006	0.00	Yes	100.00	Yes
	27	Z	-0.006	-0.006	0.00	Yes	100.00	Yes
W30	2	X	-0.012	-0.012	0.00	Yes	100.00	Yes
	3	X	-0.012	-0.012	0.00	Yes	100.00	Yes
	26	X	-0.006	-0.006	0.00	Yes	100.00	Yes
	27	X	-0.006	-0.006	0.00	Yes	100.00	Yes
	66	X	-0.006	-0.006	0.00	Yes	100.00	Yes
	69	X	-0.006	-0.006	0.00	Yes	100.00	Yes
	72	X	-0.006	-0.006	0.00	Yes	100.00	Yes
	75	X	-0.006	-0.006	0.00	Yes	100.00	Yes
Di	1	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	2	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	3	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	4	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	5	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	6	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	7	Υ	-0.008	-0.008	0.00	Yes	100.00	Yes
	8	Υ	-0.008	-0.008	0.00	Yes	100.00	Yes
	9	Υ	-0.008	-0.008	0.00	Yes	100.00	Yes
	10	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	11	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	12	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	13	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	14	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	16	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	25	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	26	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	27	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	28	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	29	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	30	Υ	-0.007	-0.007	0.00	Yes	100.00	Yes
	31	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	32	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	33	Υ	-0.014	-0.014	0.00	Yes	100.00	Yes
	54	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	57	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	15	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	60	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	63	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	66	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	69	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	72	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes
	75	Υ	-0.004	-0.004	0.00	Yes	100.00	Yes

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
DL	13	у	-0.025	6.25	No
		У	-0.025	1.75	No
		У	-0.051	5.00	No
	4.4	У	-0.058	2.00	No
	14	У	-0.044	6.85 1.15	No
		У	-0.044 -0.06	3.00	No No
		y y	-0.06	1.00	No
		У	-0.049	5.00	No
		ý	-0.019	3.00	No
	16	у	-0.018	5.54	No
		У	-0.018	2.46	No
		У	-0.019	4.00	No
	54	У	-0.018	5.54	No
		У	-0.018	2.46	No
		У	-0.019	4.00	No
	60	У	-0.044	6.85	No
		У	-0.044	1.15	No
		У	-0.06 -0.06	3.00 1.00	No No
		У	-0.049	5.00	No
		y y	-0.019	3.00	No
	63	y	-0.025	6.25	No
	••	y	-0.025	1.75	No
		ý	-0.051	5.00	No
		ý	-0.058	2.00	No
	66	У	-0.018	5.54	No
		У	-0.018	2.46	No
		У	-0.019	2.00	No
	72	У	-0.044	6.85	No
		У	-0.044	1.15	No
		У	-0.06	3.00	No
		У	-0.06 -0.049	1.00 5.00	No No
		У	-0.033	4.00	No
	75	y y	-0.049	6.25	No
	70	y	-0.049	1.75	No
		y	-0.051	5.00	No
		ý	-0.058	5.00	No
		ý	-0.033	4.00	No
W0	13	z	-0.065	6.25	No
		Z	-0.065	1.75	No
		Z	-0.033	5.00	No
		Z	-0.03	2.00	No
	14	Z	-0.103	6.85	No
		Z	-0.103	1.15	No
		z	-0.042	3.00	No
		z	-0.031 -0.031	1.00 5.00	No No
	16	z z	-0.042	5.54	No
	10	Z	-0.042	2.46	No
	54	z	-0.042	5.54	No
		z	-0.042	2.46	No
	60	z	-0.103	6.85	No
		z	-0.103	1.15	No
		z	-0.042	3.00	No
		z	-0.031	1.00	No
		Z	-0.031	5.00	No
	63	Z	-0.065	6.25	No
		Z	-0.065	1.75	No

		z	-0.033	5.00	No
		z	-0.03	2.00	No
	66	z	-0.065	5.54	No
		z	-0.065	2.46	No
	72	z	-0.147	6.85	No
		z	-0.147	1.15	No
		Z	-0.01	3.00	No
		Z	-0.01	1.00	No
		z	-0.01	5.00	No
	75	z	-0.094	6.25	No
		z	-0.094	1.75	No
		z	-0.024	5.00	No
		z	-0.03	5.00	No
W30	13	x	-0.084	6.25	No
		x	-0.084	1.75	No
		×	-0.031	5.00	No
		×	-0.03	2.00	No
	14	×	-0.132	6.85	No
		x	-0.132	1.15	No
		x	-0.036	3.00	No
		x	-0.025	1.00	No
		×	-0.025	5.00	No
	16	x	-0.057	5.54	No
		x	-0.057	2.46	No
	54	x	-0.057	5.54	No
	0 1	×	-0.057	2.46	No
	60	×	-0.132	6.85	No
	00	X	-0.132	1.15	No
		x	-0.036	3.00	No
		x	-0.025	1.00	No
		×	-0.025	5.00	No
	63	×	-0.084	6.25	No
	05	×	-0.084	1.75	No
		x	-0.031	5.00	No
		×	-0.03	2.00	No
	66	×	-0.035	5.54	No
	00	x	-0.035	2.46	No
	72	x	-0.089	6.85	No
	12		-0.089	1.15	No
		X	-0.039	3.00	No
		×	-0.029	3.00	No
		×	-0.029	3.00	No
	75		-0.055	6.25	No
	75	X		1.75	No
		×	-0.055 0.039	3.00	No
		×	-0.028	2.00	No
Di:	12		-0.03 0.05	6.25	No
Di	13	У	-0.05	1.75	No
		У	-0.05		No
		У	-0.045	5.00	
	4.4	У	-0.05 0.070	2.00	No
	14	У	-0.079 0.070	6.85 1.15	No No
		У	-0.079 0.045	1.15	No
		У	-0.045	3.00	No
		У	-0.038	1.00	No
		У	-0.031	5.00	No
	40	У	-0.012	3.00	No
	16	У	-0.035	5.54	No
		У	-0.035	2.46	No
		У	-0.016	4.00	No
	54	У	-0.035	5.54	No

		199	-0.035	2.46	No
		У	-0.035	4.00	No
	60	У	-0.079	6.85	No
	00	У	-0.079	1.15	No
		y y	-0.045	3.00	No
		y	-0.038	1.00	No
		y	-0.031	5.00	No
		ý	-0.012	3.00	No
	63	y	-0.05	6.25	No
	00	y	-0.05	1.75	No
		y	-0.045	5.00	No
		y	-0.05	2.00	No
	66	ý	-0.035	5.54	No
		ý	-0.035	2.46	No
		y	-0.016	2.00	No
	72	y	-0.079	6.85	No
		ý	-0.079	1.15	No
		ý	-0.045	3.00	No
		ý	-0.038	1.00	No
		ý	-0.031	5.00	No
		ý	-0.035	4.00	No
	75	ý	-0.05	6.25	No
		у	-0.05	1.75	No
		ý	-0.045	5.00	No
		у	-0.05	5.00	No
		ý	-0.035	4.00	No
Wi0	13	z	-0.028	6.25	No
		z	-0.028	1.75	No
		z	-0.016	5.00	No
		z	-0.016	2.00	No
	14	z	-0.04	6.85	No
		Z	-0.04	1.15	No
		z	-0.02	3.00	No
		z	-0.015	1.00	No
		z	-0.015	1.00	No
	16	z	-0.019	5.54	No
		z	-0.019	2.46	No
	54	z	-0.019	5.54	No
		z	-0.019	2.46	No
	60	Z	-0.04	6.85	No
		z	-0.04	1.15	No
		z	-0.02	3.00	No
		Z	-0.015	1.00	No
		Z	-0.015	1.00	No
	63	Z	-0.028	6.25	No
		z	-0.028	1.75	No
		z	-0.016	5.00	No
		Z	-0.016	2.00	No
	66	Z	-0.027	5.54	No
		Z	-0.027	2.46	No
	72	z	-0.053	6.85	No
		Z	-0.053	1.15	No
		z	-0.015	3.00	No
		z	-0.01	1.00	No
		Z	-0.01	5.00	No
	75	z	-0.037	6.25	No
		z	-0.037	1.75	No
		z	-0.014	5.00	No
		Z	-0.016	5.00	No
Wi30	13	x	-0.033	6.25	No

		×	-0.033	1.75	No
		×	-0.014	5.00	No
		×	-0.016	2.00	No
	14	x	-0.048	6.85	No
		×	-0.048	1.15	No
		×	-0.016	3.00	No
		×	-0.012	1.00	No
		x	-0.012	1.00	No
	16	×	-0.024	5.54	No
		x	-0.024	2.46	No
	54	x	-0.024	5.54	No
		x	-0.024	2.46	No
	60	x	-0.048	6.85	No
		×	-0.048	1.15	No
		×	-0.016	3.00	No
		×	-0.012	1.00	No
		x	-0.012	1.00	No
	63	x	-0.033	6.25	No
		×	-0.033	1.75	No
		x	-0.014	5.00	No
		x	-0.016	2.00	No
	66	×	-0.017	5.54	No
		×	-0.017	2.46	No
	72	×	-0.036	6.85	No
		x	-0.036	1.15	No
		x	-0.019	2.00	No No
		×	-0.015 0.015	2.00 2.00	No
	75	×	-0.015 -0.025	6.25	No
	75	x	-0.025	1.75	No
		X	-0.025	2.00	No
		x	-0.016	2.00	No
WL0	13	x z	-0.007	6.25	No
VVLO	15	z	-0.007	1.75	No
		z	-0.004	5.00	No
		z	-0.003	2.00	No
	14	z	-0.01	6.85	No
		z	-0.01	1.15	No
		z	-0.004	3.00	No
		z	-0.003	1.00	No
		z	-0.003	1.00	No
	16	z	-0.005	5.54	No
		z	-0.005	2.46	No
	54	Z	-0.005	5.54	No
		z	-0.005	2.46	No
	60	z	-0.01	6.85	No
		z	-0.01	1.15	No
		Z	-0.004	3.00	No
		Z	-0.003	1.00	No
		z	-0.003	1.00	No
	63	z	-0.007	6.25	No
		z	-0.007	1.75	No
		Z	-0.004	5.00	No
		z	-0.003	2.00	No
	66	z	-0.007	5.54	No
		Z	-0.007	2.46	No
	72	Z	-0.015	6.85	No
		z	-0.015	1.15	No
		z	-0.001	3.00	No
		z	-0.001	1.00	No

		z	-0.001	5.00	No
	75	z	-0.01	6.25	No
		z	-0.01	1.75	No
		z	-0.003	5.00	No
		z	-0.003	5.00	No
WL30	13	×	-0.009	6.25	No
		x	-0.009	1.75	No
		x	-0.004	5.00	No
		x	-0.003	2.00	No
	14	x	-0.013	6.85	No
		x	-0.013	1.15	No
		x	-0.004	3.00	No
		x	-0.003	1.00	No
		x	-0.003	1.00	No
	16	x	-0.006	5.54	No
		x	-0.006	2.46	No
	54	x	-0.006	5.54	No
		x	-0.006	2.46	No
	60	x	-0.013	6.85	No
		x	-0.013	1.15	No
		x	-0.004	3.00	No
		x	-0.003	1.00	No
		x	-0.003	1.00	No
	63	x	-0.009	6.25	No
A		x	-0.009	1.75	No
		x	-0.004	5.00	No
		x	-0.003	2.00	No
	66	x	-0.004	5.54	No
		x	-0.004	2.46	No
	72	x	-0.009	6.85	No
		x	-0.009	1.15	No
		X	-0.004	2.00	No
		x	-0.003	2.00	No
		x	-0.003	2.00	No
	75	x	-0.006	6.25	No
		x	-0.006	1.75	No
		x	-0.003	2.00	No
		x	-0.003	2.00	No
LL1	1	у	-0.25	7.00	No
	2 3	У	-0.25	7.00	No
		У	-0.25	7.00	No
LL2	1	У	-0.25	0.00	No
	2	У	-0.25	0.00	No
	3	У	-0.25	0.00	No
LLa1	16	у	-0.50	4.00	No
	54	У	-0.50	4.00	No
	66	У	-0.50	4.00	No
LLa2	57	У	-0.50	4.00	No
	15	y	-0.50	4.00	No No
	69	y	-0.50	4.00	No No
LLa3	14	у	-0.50	4.00	No No
	60	у	-0.50	4.00	No No
11 - 4	72	у	-0.50	4.00	No No
LLa4	13	y	-0.50	4.00	No No
	63	у	-0.50	4.00	No No
	75	У	-0.50	4.00	No

Self weight multipliers for load conditions

			Self weight multiplier				
Condition	Description	Comb.	MultX	MultY	MultZ		
 DL	Dead Load	No	0.00	-1.00	0.00		
W0	Wind Load 0/60/120 deg	No	0.00	0.00	0.00		
W30	Wind Load 30/90/150 deg	No	0.00	0.00	0.00		
Di	Ice Load	No	0.00	0.00	0.00		
Wi0	Ice Wind Load 0/60/120 deg	No	0.00	0.00	0.00		
Wi30	Ice Wind Load 30/90/150 deg	No	0.00	0.00	0.00		
WL0	WL 30 mph 0/60/120 deg	No	0.00	0.00	0.00		
WL30	WL 30 mph 30/90/150 deg	No	0.00	0.00	0.00		
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00		
LL2	250 lb Live Load End of Mount	No	0.00	0.00	0.00		
LLa1	500 lb Live Load on Antenna 1	No	0.00	0.00	0.00		
LLa2	500 lb Live Load on Antenna 2	No	0.00	0.00	0.00		
LLa3	500 lb Live Load on Antenna 3	No	0.00	0.00	0.00		
LLa4	500 lb Live Load on Antenna 4	No	0.00	0.00	0.00		
W180	-W0	Yes	0.00	0.00	0.00		
W210	-W30	Yes	0.00	0.00	0.00		
Wi180	-Wi0	Yes	0.00	0.00	0.00		
Wi210	-Wi30	Yes	0.00	0.00	0.00		
WL180	-WL0	Yes	0.00	0.00	0.00		
WL210	-WL30	Yes	0.00	0.00	0.00		

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
W0	0.00	0.00	0.00
W30	0.00	0.00	0.00
Di	0.00	0.00	0.00
Wi0	0.00	0.00	0.00
Wi30	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
LL1	0.00	0.00	0.00
LL2	0.00	0.00	0.00
LLa1	0.00	0.00	0.00
LLa2	0.00	0.00	0.00
LLa3	0.00	0.00	0.00
LLa4	0.00	0.00	0.00
W180	0.00	0.00	0.00
W210	0.00	0.00	0.00
Wi180	0.00	0.00	0.00
Wi210	0.00	0.00	0.00
WL180	0.00	0.00	0.00
WL210	0.00	0.00	0.00



Current Date: 6/7/2018 12:17 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1160\CT1160 (3C-4C-5C).etz\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design:

W180=-W0

W210=-W30

Wi180=-Wi0

Wi210=-Wi30

WL180=-WL0

WL210=-WL30

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

LC4=1.2DL-1.6W30

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30

LC7=0.9DL-1.6W0 LC8=0.9DL-1.6W30

LC9=1.2DL+Di+Wi0

040 4 001 -01-1400

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LC12=1.2DL+Di-Wi30

LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.6LL1

LC16=1.2DL+1.6LL2

LC17=1.2DL+WL0+LLa1

LC18=1.2DL+WL30+LLa1

LC19=1.2DL-WL0+LLa1

LC20=1.2DL-WL30+LLa1

LC21=1.2DL+WL0+LLa2

LC22=1.2DL+WL30+LLa2

LC23=1.2DL-WL0+LLa2

LC24=1.2DL-WL30+LLa2

LC25=1.2DL+WL0+LLa3

LC26=1.2DL+WL30+LLa3

LC27=1.2DL-WL0+LLa3

LC28=1.2DL-WL30+LLa3 LC29=1.2DL+WL0+LLa4

LC30=1.2DL+WL30+LLa4

LC31=1.2DL-WL0+LLa4

LC32=1.2DL-WL30+LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS SQR 4X4X1_4	7	LC1 at 0.00%	0.11	 ОК	Eq. H1-1b
			LC10 at 0.00%	0.27	OK	Eq. H1-1b
			LC11 at 0.00%	0.25	OK	Eq. H1-1b
			LC12 at 0.00%	0.25	OK	Eq. H1-1b
			LC13 at 0.00%	0.13	OK	Eq. H1-1b
			LC14 at 0.00%	0.10	OK	Eq. H1-1b
			LC15 at 0.00%	0.21	OK	Eq. H1-1b
			LC16 at 0.00%	0.14	OK	Eq. H1-1b
			LC17 at 0.00%	0.16	OK	Eq. H1-1b
			LC18 at 0.00%	0.17	OK	Eq. H1-1b
			LC19 at 0.00%	0.16	OK	Eq. H1-1b

	L GO =t 0 000/	0.24	OK	Ea U1 1h
	LC2 at 0.00%	0.24	OK	Eq. H1-1b
	LC20 at 0.00%	0.17	OK	Eq. H1-1b
	LC21 at 0.00%	0.22	ОК	Eq. H1-1b
	LC22 at 0.00%	0.22	OK	Eq. H1-1b
	LC23 at 0.00%	0.22	OK	Eq. H1-1b
	LC24 at 0.00%	0.21	OK	Eq. H1-1b
	LC25 at 0.00%	0.22	OK	Eq. H1-1b
	LC26 at 0.00%	0.23	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC27 at 0.00%	0.22		•
	LC28 at 0.00%	0.22	OK	Eq. H1-1b
	LC29 at 0.00%	0.17	OK	Eq. H1-1b
	LC3 at 0.00%	0.16	OK	Eq. H1-1b
	LC30 at 0.00%	0.18	OK	Eq. H1-1b
	LC31 at 0.00%	0.17	OK	Eq. H1-1b
	LC32 at 0.00%	0.17	OK	Eq. H1-1b
	LC4 at 0.00%	0.22	OK	Eq. H1-1b
	LC5 at 0.00%	0.08	OK	Eq. H1-1b
	LC6 at 0.00%	0.20	OK	Eq. H1-1b
	LC7 at 0.00%	0.12	OK	Eq. H1-1b
	LC8 at 0.00%	0.19	OK	Eq. H1-1b
	LC9 at 0.00%	0.24	OK	Eq. H1-1b
	W180 at 100.00%	0.02	OK	Eq. H1-1b
	W210 at 0.00%	0.08	OK	
	Wi180 at 100.00%	0.01	OK	Eq. H1-1b
	Wi210 at 0.00%	0.03	OK	-4
	WL180 at 100.00%	0.00	OK	Eq. H1-1b
				Eq. 111-10
	WL210 at 0.00%	0.01	ОК	
8	LC1 at 0.00%	0.22	OK	Eg. H1-1b
O				Eq. H1-1b
	LC10 at 0.00%	0.23	OK OK	•
	LC11 at 0.00%	0.25	OK	Eq. H1-1b
	LC12 at 0.00%	0.25	OK	Eq. H1-1b
	LC13 at 0.00%	0.12	OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00%	0.12	OK	Eq. H1-1b Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00%	0.12 0.09 0.20	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.12 0.09 0.20 0.13	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00%	0.12 0.09 0.20 0.13 0.16	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15	OK OK OK OK OK OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15	OK OK OK OK OK OK OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19 0.15	OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19 0.15	OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC21 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21	OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21	OK	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC24 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.21 0.20 0.20	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.22 0.20 0.20	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.22 0.20 0.20 0.21 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC29 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.22 0.20 0.20 0.21 0.21 0.21 0.21	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.22 0.21 0.20 0.20 0.21 0.15 0.15 0.16 0.16	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC21 at 0.00% LC22 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.22 0.20 0.21 0.15 0.21 0.15 0.21 0.22 0.21 0.22 0.24 0.25 0.26	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC35 at 0.00% LC35 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.22 0.20 0.21 0.15 0.21 0.15 0.21 0.20 0.21 0.15 0.21 0.20 0.21 0.15 0.21 0.21 0.20 0.21 0.21 0.21 0.21 0.21 0.22 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.22 0.20 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.22 0.20 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.22 0.21 0.22 0.21 0.21 0.21 0.21 0.21 0.21 0.22 0.22 0.22 0.22 0.22 0.23 0.24 0.25 0.26	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC35 at 0.00% LC36 at 0.00% LC36 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.15 0.21 0.15 0.16 0.16 0.16 0.16 0.22 0.20 0.16	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC29 at 0.00% LC20 at 0.00% LC21 at 0.00% LC21 at 0.00% LC21 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.15 0.15 0.16 0.16 0.16 0.16 0.18	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.21 0.15 0.21 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.19	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC33 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.21 0.15 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.22 0.20 0.16 0.18 0.19 0.24	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.15 0.16 0.16 0.16 0.16 0.16 0.19 0.16 0.18 0.19 0.24 0.07	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC33 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.21 0.15 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.22 0.20 0.16 0.18 0.19 0.24	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC34 at 0.00% LC35 at 0.00% LC36 at 0.00% LC37 at 0.00% LC38 at 0.00% LC39 at 0.00% LC39 at 0.00% LC30 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.15 0.16 0.16 0.16 0.16 0.16 0.19 0.16 0.18 0.19 0.24 0.07	OK O	Eq. H1-1b
	LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC34 at 0.00% LC35 at 0.00% LC36 at 0.00% LC37 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% LC9 at 0.00% LC9 at 0.00%	0.12 0.09 0.20 0.13 0.16 0.15 0.19 0.15 0.21 0.21 0.21 0.20 0.20 0.21 0.15 0.16 0.16 0.16 0.12 0.10 0.10 0.10 0.10 0.10 0.10 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

		0.04	014	
	WL180 at 0.00%	0.01	OK OK	E- 114.45
	WL210 at 0.00%	0.01	OK	Eq. H1-1b
•	L O4 = 1 0 000/	0.00	OK	
9	LC1 at 0.00%	0.23	OK	Eq. H1-1b
	LC10 at 0.00%	0.24	OK	Eq. H1-1b
	LC11 at 0.00%	0.24	OK	Eq. H1-1b
	LC12 at 0.00%	0.23	OK	Eq. H1-1b
	LC13 at 0.00%	0.12	OK	Eq. H1-1b
	LC14 at 0.00%	0.09	OK	Eq. H1-1b
	LC15 at 0.00%	0.20	OK	Eq. H1-1b
	LC16 at 0.00%	0.13	OK	Eq. H1-1b
	LC17 at 0.00%	0.15	OK	Eq. H1-1b
	LC18 at 0.00%	0.16	OK	Eq. H1-1b
	LC19 at 0.00%	0.16	OK	Eq. H1-1b
	LC2 at 0.00%	0.21	OK	Eq. H1-1b
	LC20 at 0.00%	0.15	OK	Eq. H1-1b
	LC21 at 0.00%	0.21	OK	Eq. H1-1b
	LC22 at 0.00%	0.21	OK	Eq. H1-1b
	LC23 at 0.00%	0.21	OK	Eq. H1-1b
	LC24 at 0.00%	0.20	OK	Eq. H1-1b
	LC25 at 0.00%	0.21	OK	Eq. H1-1b
	LC26 at 0.00%	0.21	OK	Eq. H1-1b
	LC27 at 0.00%	0.21	OK	Eq. H1-1b
	LC28 at 0.00%	0.21	OK	Eq. H1-1b
	LC29 at 0.00%	0.16	OK	Eq. H1-1b
	LC3 at 0.00%	0.22	OK	Eq. H1-1b
	LC30 at 0.00%	0.15	OK	Eq. H1-1b
	LC31 at 0.00%	0.15	OK	Eq. H1-1b
	LC32 at 0.00%	0.16	OK	Eq. H1-1b
	LC4 at 0.00%	0.18	OK	Eq. H1-1b
	LC5 at 0.00%	0.21	OK	Eq. H1-1b
	LC6 at 0.00%	0.18	OK	Eq. H1-1b
	LC7 at 0.00%	0.19	OK	Eq. H1-1b
	LC8 at 0.00%	0.15	OK	Eq. H1-1b
	LC9 at 0.00%	0.25	ок	Eq. H1-1b
	W180 at 0.00%	0.07	OK	
	W210 at 0.00%	0.06	OK	Eq. H1-1b
	Wi180 at 0.00%	0.03	OK	Eq. H1-1b
	Wi210 at 0.00%	0.02	OK	Eq. H1-1b
	WL180 at 0.00%	0.01	OK	Eq. H1-1b
	WL210 at 0.00%	0.00	OK	Eq. H1-1b
	I C1 at 49 069/	0.56	\A/ith warnings	Eq. H3-8
1	LC1 at 48.96% LC10 at 48.96%	0.56 0.78	With warnings With warnings	Eq. H3-6 Eq. H2-1
	LC10 at 48.96%	0.78	With warnings	Eq. H2-1
	LC11 at 48.96%	0.75	With warnings	Eq. H2-1
	LC12 at 48.96%	0.40	With warnings	Eq. H2-1
	LC13 at 48.96%	0.40	With warnings	Eq. H2-1
	LC14 at 48.96%	0.38	With warnings	Eq. H2-1
	LC16 at 48.96%	0.38	With warnings	Eq. H2-1
	LC17 at 0.00%	0.48	With warnings With warnings	Eq. H2-1
	LC17 at 0.00%	0.57	With warnings	Eq. H2-1
	LC19 at 0.00%	0.56	With warnings	Eq. H2-1
	LC19 at 0.00%	0.96	With warnings	Eq. H2-1
		0.53	With warnings	Eq. H2-1
	LC20 at 0.00%		•	•
	LC21 at 50.00%	0.54	With warnings With warnings	Eq. H2-1
	LC22 at 50.00%	0.55	_	Eq. H2-1
	LC23 at 50.00%	0.56	With warnings	Eq. H2-1
	LC24 at 50.00%	0.55	With warnings	Eq. H2-1
	LC25 at 48.96%	0.66	With warnings With warnings	Eq. H2-1 Eq. H2-1
	LC26 at 48.96%	0.68	With warnings	Eq. H2-1
	LC27 at 48.96%	0.68	With warnings With warnings	
	LC28 at 48.96%	0.67	With warnings	Eq. H2-1 Eq. H2-1
	LC29 at 48.96%	0.60	vvitii vvaiiiiigs	E4.112-1

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				E 110.4
	LC3 at 48.96%	0.75	With warnings	Eq. H2-1
	LC30 at 48.96%	0.62	With warnings	Eq. H2-1
	LC31 at 48.96%	0.62	With warnings	Eq. H2-1
			•	•
	LC32 at 48.96%	0.61	With warnings	Eq. H2-1
	LC4 at 100.00%	0.87	With warnings	Eq. H2-1
	LC5 at 48.96%	0.49	With warnings	Eq. H3-8
	LC6 at 0.00%	0.89	With warnings	Eq. H2-1
	LC7 at 48.96%	0.66	With warnings	Eq. H2-1
			•	
	LC8 at 100.00%	0.82	With warnings	Eq. H2-1
	LC9 at 48.96%	0.73	With warnings	Eq. H2-1
	W180 at 48.96%	0.41	With warnings	Eq. H2-1
	W210 at 100.00%	0.41	With warnings	Eq. H2-1
		0.13		
	Wi180 at 48.96%		With warnings	Eq. H2-1
	Wi210 at 100.00%	0.15	With warnings	Eq. H2-1
	WL180 at 48.96%	0.03	With warnings	Eq. H2-1
	WL210 at 100.00%	0.04	With warnings	Eq. H2-1
2	LC1 at 100.00%	0.99	With warnings	Eq. H2-1
_	LC10 at 50.00%	0.75	With warnings	Eq. H2-1
			•	•
	LC11 at 50.00%	0.78	With warnings	Eq. H2-1
	LC12 at 50.00%	0.83	With warnings	Eq. H2-1
	LC13 at 50.00%	0.41	With warnings	Eq. H2-1
	LC14 at 50.00%	0.30	With warnings	Eq. H2-1
	LC15 at 50.00%	0.38	With warnings	Eq. H2-1
	LC16 at 50.00%	0.49	With warnings	Eq. H2-1
			•	
	LC17 at 100.00%	0.52	With warnings	Eq. H2-1
	LC18 at 100.00%	0.50	With warnings	Eq. H2-1
	LC19 at 0.00%	0.50	With warnings	Eq. H2-1
	LC2 at 50.00%	0.60	With warnings	Eq. H3-8
	LC20 at 0.00%	0.51	With warnings	Eq. H2-1
	LC21 at 50.00%	0.50	With warnings	Eq. H2-1
		0.48	With warnings	
	LC22 at 50.00%			Eq. H2-1
	LC23 at 50.00%	0.49	With warnings	Eq. H2-1
	LC24 at 50.00%	0.50	With warnings	Eq. H2-1
	LC25 at 50.00%	0.73	With warnings	Eq. H2-1
	LC26 at 50.00%	0.71	With warnings	Eq. H2-1
	LC27 at 50.00%	0.72	With warnings	Eq. H2-1
	LC28 at 50.00%	0.73	With warnings	Eq. H2-1
			•	
	LC29 at 50.00%	0.64	With warnings	Eq. H2-1
	LC3 at 0.00%	0.59	With warnings	Eq. H2-1
	LC30 at 50.00%	0.63	With warnings	Eq. H2-1
	LC31 at 50.00%	0.63	With warnings	Eq. H2-1
	LC32 at 50.00%	0.65	With warnings	Eq. H2-1
	LC4 at 0.00%	0.94	With warnings	Eq. H2-1
	LC5 at 100.00%	0.94	With warnings	Eq. H2-1
			_	
	LC6 at 50.00%	0.53	With warnings	Eq. H3-8
	LC7 at 0.00%	0.54	With warnings	Eq. H2-1
	LC8 at 0.00%	0.88	With warnings	Eq. H2-1
	LC9 at 50.00%	0.81	With warnings	Eq. H2-1
	W180 at 100.00%	0.28	With warnings	Eq. H2-1
	W210 at 0.00%	0.45	With warnings	Eq. H2-1
	Wi180 at 100.00%	0.10	With warnings	Eq. H2-1
	Wi210 at 0.00%	0.15	.	
			With warnings	Eq. H2-1
	WL180 at 100.00%	0.02	With warnings	Eq. H2-1
	WL210 at 0.00%	0.04	With warnings	Eq. H2-1
3	LC1 at 0.00%	1.01	N.G.	Eq. H2-1
	LC10 at 50.00%	0.83	With warnings	Eq. H2-1
	LC11 at 50.00%	0.77	With warnings	Eq. H2-1
	LC12 at 50.00%	0.76	With warnings	Eq. H2-1
	LC13 at 50.00%	0.70	With warnings	Eq. H2-1
			•	
	LC14 at 50.00%	0.31	With warnings	Eq. H2-1
	LC15 at 50.00%	0.38	With warnings	Eq. H2-1
	LC16 at 50.00%	0.49	With warnings	Eq. H2-1

	LC17 at 100.00%	0.55	With warnings	Eq. H2-1
			•	
	LC18 at 100.00%	0.58	With warnings	Eq. H2-1
	LC19 at 100.00%	0.57	With warnings	Eq. H2-1
	LC2 at 100.00%	0.99	With warnings	Eq. H2-1
	LC20 at 100.00%	0.54	With warnings	Eq. H2-1
	LC21 at 50.00%	0.50	With warnings	Eq. H2-1
				•
	LC22 at 50.00%	0.50	With warnings	Eq. H2-1
	LC23 at 50.00%	0.49	With warnings	Eq. H2-1
	LC24 at 50.00%	0.49	With warnings	Eq. H2-1
	LC25 at 50.00%	0.73	With warnings	Eq. H2-1
			_	Eq. H2-1
	LC26 at 50.00%	0.73	With warnings	•
	LC27 at 50.00%	0.72	With warnings	Eq. H2-1
	LC28 at 50.00%	0.72	With warnings	Eq. H2-1
	LC29 at 50.00%	0.64	With warnings	Eq. H2-1
	LC3 at 100.00%	0.59	With warnings	Eq. H2-1
			•	•
	LC30 at 50.00%	0.65	With warnings	Eq. H2-1
	LC31 at 50.00%	0.63	With warnings	Eq. H2-1
	LC32 at 50.00%	0.63	With warnings	Eq. H2-1
	LC4 at 50.00%	0.45	With warnings	Eq. H3-8
		0.96	With warnings	Eq. H2-1
	LC5 at 0.00%		_	•
	LC6 at 100.00%	0.92	With warnings	Eq. H2-1
	LC7 at 100.00%	0.53	With warnings	Eq. H2-1
	LC8 at 50.00%	0.40	With warnings	Eq. H2-1
	LC9 at 50.00%	0.82	With warnings	Eq. H2-1
			•	•
	W180 at 0.00%	0.29	With warnings	Eq. H2-1
	W210 at 50.00%	0.27	With warnings	Eq. H2-1
	Wi180 at 0.00%	0.11	With warnings	Eq. H2-1
	Wi210 at 100.00%	0.09	With warnings	Eq. H2-1
	WL180 at 0.00%	0.02	With warnings	Eq. H2-1
			_	
	WL210 at 100.00%	0.02	With warnings	Eq. H2-1
	200000000000000000000000000000000000000			
			A14	E 110.4
4	LC1 at 100.00%	0.09	OK	Eq. H2-1
4				
4	LC10 at 0.00%	0.28	OK	Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00%	0.28 0.25	OK OK	Eq. H2-1 Eq. H2-1
4	LC10 at 0.00%	0.28 0.25 0.25	OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00%	0.28 0.25	OK OK	Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00%	0.28 0.25 0.25	OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00%	0.28 0.25 0.25 0.12 0.09	OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12	ОК ОК ОК ОК ОК	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12 0.25	OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12 0.25 0.20	OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12 0.25 0.20	OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12 0.25 0.20	OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00%	0.28 0.25 0.25 0.12 0.09 0.12 0.25 0.20 0.22	OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00%	0.28 0.25 0.12 0.09 0.12 0.25 0.20 0.22 0.21 0.36	OK OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC16 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC2 at 100.00%	0.28 0.25 0.12 0.09 0.12 0.25 0.20 0.22 0.21 0.36	OK OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
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4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC16 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC2 at 100.00%	0.28 0.25 0.12 0.09 0.12 0.25 0.20 0.22 0.21 0.36	OK OK OK OK OK OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
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4	LC10 at 0.00% LC11 at 0.00% LC12 at 100.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 0.00% LC23 at 0.00%	0.28 0.25 0.12 0.09 0.12 0.25 0.20 0.22 0.21 0.36 0.20 0.13 0.15 0.14 0.13 0.13	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1
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	W210 at 0.00% Wi180 at 100.00% Wi210 at 0.00% WL180 at 100.00% WL210 at 0.00%	0.21 0.03 0.08 0.01 0.02	OK OK OK OK	Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
5	LC1 at 100.00% LC10 at 100.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 100.00% LC19 at 0.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 0.00% LC26 at 100.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00%	0.36 0.20 0.23 0.25 0.09 0.07 0.10 0.22 0.20 0.18 0.19 0.21 0.20 0.13 0.12 0.12 0.13 0.12 0.13 0.12 0.12 0.13	ОК ОК ОК ОК ОК ОК ОК ОК ОК ОК	Eq. H2-1
	LC30 at 100.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 100.00% LC6 at 0.00% LC7 at 100.00% LC8 at 0.00% W180 at 100.00% Wi180 at 100.00% Wi210 at 0.00% Wi210 at 0.00% WL180 at 100.00% WL210 at 0.00%	0.19 0.20 0.33 0.23 0.29 0.30 0.25 0.23 0.15 0.08 0.05 0.02 0.01	OK OK OK OK OK OK OK OK OK OK OK	Eq. H2-1
6	LC1 at 0.00% LC10 at 100.00% LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.35 0.28 0.26 0.19 0.12 0.09 0.12 0.25 0.20 0.22 0.22 0.35 0.19 0.13 0.15 0.13 0.15	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1

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	LC27 at 100.00%	0.15	OK	Eq. H2-1
	LC28 at 100.00%	0.13	OK	Eq. H2-1
	LC29 at 100.00%	0.20	OK	Eq. H2-1
	LC3 at 100.00%	0.26	OK	Eq. H2-1
	LC30 at 100.00%	0.22	OK	Eq. H2-1
	LC31 at 100.00%	0.22	OK	Eq. H2-1
	LC32 at 100.00%	0.20	OK	Eq. H2-1
	LC4 at 100.00%	0.19	OK	Eq. H2-1
	LC5 at 0.00%	0.33	ОК	Eq. H2-1
	LC6 at 100.00%	0.32	OK	Eq. H2-1
	LC7 at 0.00%	0.28	OK	Eq. H2-1
	LC8 at 100.00%	0.22	OK	Eq. H2-1
	LC9 at 0.00%	0.25	OK	Eq. H2-1
				•
	W180 at 0.00%	0.23	OK	Eq. H2-1
	W210 at 100.00%	0.20	OK	Eq. H2-1
	Wi180 at 0.00%	80.0	OK	Eq. H2-1
	Wi210 at 100.00%	0.07	OK	Eq. H2-1
	WL180 at 0.00%	0.02	OK	Eq. H2-1
	WL210 at 100.00%	0.02	OK	Eq. H2-1
28	LC1 at 100.00%	0.67	OK	Eq. H3-8
	LC10 at 100.00%	0.19	OK	Eq. H3-8
	LC11 at 100.00%	0.16	OK	Eq. H2-1
	LC12 at 0.00%	80.0	OK	Sec. F1
	LC13 at 100.00%	0.07	OK	Eq. H3-8
	LC14 at 100.00%	0.05	OK	Eq. H3-8
	LC15 at 100.00%	0.07	OK	Eq. H3-8
	LC16 at 100.00%	0.07	OK	Eq. H3-8
	LC17 at 0.00%	0.06	OK	Eq. H2-1
	LC18 at 0.00%	0.09	OK	Eq. H2-1
	LC19 at 100.00%	0.09	OK	Eq. H2-1
	LC2 at 0.00%	0.40	OK	Sec. F1
	LC20 at 100.00%	0.07	OK	Eq. H2-1
	LC21 at 0.00%	0.06	OK	Eq. H2-1
	LC22 at 0.00%	0.09	OK	Eq. H2-1
	LC23 at 100.00%	0.09	OK	Eq. H2-1
	LC24 at 100.00%	0.05	OK	Eq. H2-1
	LC25 at 100.00%	0.14	OK	Eq. H3-8
	LC26 at 100.00%	0.13	OK	Eq. H3-8
	LC27 at 100.00%	0.09	OK	Eq. H2-1
	LC28 at 100.00%	0.09	OK	Eq. H3-8
				Eq. H3-8
	LC29 at 100.00%	0.20	OK	Eq. H3-8
	LC3 at 0.00%	0.56	OK	
	LC30 at 100.00%	0.18	OK	Eq. H3-8
	LC31 at 100.00%	0.13	OK	Eq. H3-8
	LC32 at 100.00%	0.15	OK	Eq. H3-8
	LC4 at 0.00%	0.33	OK	Sec. F1
	LC5 at 100.00%	0.66	OK	Eq. H3-8
	LC6 at 0.00%	0.39	OK	Sec. F1
	LC7 at 0.00%	0.57	OK	Eq. H3-8
	LC8 at 0.00%	0.34	OK	Sec. F1
	LC9 at 100.00%	0.26	OK	Eq. H3-8
	W180 at 0.00%	0.38	OK	Eq. H3-8
	W210 at 0.00%	0.23	OK	Sec. F1
	Wi180 at 0.00%	0.15	OK	Eq. H3-8
	Wi210 at 0.00%	80.0	OK	Sec. F1
	WL180 at 0.00%	0.03	OK	Eq. H3-8
	WL210 at 0.00%	0.02	OK	Sec. F1
29	LC1 at 100.00%	0.23	OK	Eq. H3-8
	LC10 at 0.00%	0.10	OK	Eq. H3-8
	LC11 at 100.00%	0.13	OK	Eq. H2-1
	LC12 at 0.00%	0.19	OK	Eq. H2-1
	LC13 at 100.00%	0.04	OK	Eq. H2-1

LC14 at 100.00% 0.03 OK	Eq. H2-1
LC15 at 100.00% 0.04 OK	Eq. H2-1
	Eq. H2-1
	Sec. F1
	Eq. H2-1
	Eq. H2-1
LC22 at 100.00% 0.05 OK	Eq. H2-1
LC23 at 100.00% 0.08 OK	Eq. H2-1
LC24 at 0.00% 0.09 OK	Eq. H2-1
LC25 at 0.00% 0.07 OK	Eq. H2-1
LC26 at 0.00% 0.07 OK	Eq. H3-8
	Eq. H2-1
	Eg. H2-1
	Eq. H2-1
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	Eq. H3-8
	Eq. H3-8
	Eq. H3-8
	Eq. H2-1
LC4 at 0.00% 0.50 OK	Sec. F1
LC5 at 100.00% 0.24 OK	Eq. H3-8
LC6 at 0.00% 0.44 OK	Sec. F1
LC7 at 0.00% 0.29 OK	Eq. H3-8
LC8 at 0.00% 0.49 OK	Sec. F1
	Eq. H2-1
	Eq. H3-8
	Sec. F1
	Eq. H3-8
	Sec. F1
	Eq. H3-8
WL210 at 0.00% 0.03 OK	Sec. F1
	Sec. F1
LC10 at 0.00% 0.13 OK	 Sec. F1 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK	Sec. F1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK	 Sec. F1 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK	Sec. F1 Eq. H2-1 Sec. F1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK LC16 at 100.00% 0.05 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK LC16 at 100.00% 0.05 OK LC17 at 0.00% 0.09 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK LC16 at 100.00% 0.05 OK LC17 at 0.00% 0.09 OK LC18 at 0.00% 0.08 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK LC16 at 100.00% 0.05 OK LC17 at 0.00% 0.09 OK LC18 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.04 OK LC16 at 100.00% 0.05 OK LC17 at 0.00% 0.09 OK LC18 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.32 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC17 at 0.00% 0.09 OK LC18 at 0.00% 0.08 OK LC19 at 100.00% 0.08 OK LC19 at 100.00% 0.06 OK LC20 at 100.00% 0.07 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H2-1
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LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC18 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.06 OK LC22 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H2-1
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.06 OK LC20 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H2-1
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LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.32 OK LC20 at 100.00% 0.07 OK LC23 at 100.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC24 at 100.00% 0.08 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.07 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1
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LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.32 OK LC20 at 100.00% 0.07 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK LC24 at 100.00% 0.08 OK LC25 at 56.25% 0.08 OK LC27 at 0.00% 0.07 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8
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LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.05 OK LC24 at 100.00% 0.05 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.07 OK LC27 at 0.00% 0.06 OK LC28 at 0.00% 0.08 OK LC29 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 0.00% 0.08 OK LC24 at 100.00% 0.07 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.08 OK LC27 at 0.00% 0.08 OK LC28 at 0.00% 0.08 OK LC29 at 100.00% 0.08 OK LC31 at 0.00% 0.08 OK LC32 at 0.00% 0.08 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.05 OK LC24 at 100.00% 0.05 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.07 OK LC27 at 0.00% 0.06 OK LC28 at 0.00% 0.08 OK LC29 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC23 at 0.00% 0.08 OK LC31 at 0.00% 0.08 OK LC32 at 0.00% 0.08 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC18 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.08 OK LC23 at 100.00% 0.08 OK LC24 at 100.00% 0.08 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.07 OK LC27 at 0.00% 0.08 OK LC29 at 100.00% 0.07 OK LC21 at 0.00% 0.07 OK LC21 at 0.00% 0.08 OK LC23 at 0.00% 0.08 OK LC24 at 100.00% 0.07 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.08 OK LC27 at 0.00% 0.08 OK LC27 at 0.00% 0.08 OK LC29 at 100.00% 0.08 OK LC29 at 100.00% 0.08 OK LC29 at 100.00% 0.08 OK LC31 at 0.00% 0.08 OK LC32 at 0.00% 0.008 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8
LC10 at 0.00% 0.13 OK LC11 at 100.00% 0.08 OK LC12 at 0.00% 0.13 OK LC13 at 100.00% 0.04 OK LC14 at 100.00% 0.03 OK LC15 at 100.00% 0.05 OK LC16 at 100.00% 0.09 OK LC17 at 0.00% 0.08 OK LC19 at 0.00% 0.06 OK LC2 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 100.00% 0.05 OK LC24 at 100.00% 0.05 OK LC25 at 56.25% 0.08 OK LC25 at 56.25% 0.08 OK LC27 at 0.00% 0.06 OK LC27 at 0.00% 0.06 OK LC29 at 100.00% 0.07 OK LC21 at 0.00% 0.08 OK LC22 at 0.00% 0.08 OK LC23 at 0.00% 0.08 OK LC24 at 100.00% 0.07 OK LC25 at 56.25% 0.08 OK LC25 at 56.25% 0.08 OK LC26 at 0.00% 0.06 OK LC27 at 0.00% 0.08 OK LC29 at 100.00% 0.08 OK LC29 at 100.00% 0.08 OK LC31 at 0.00% 0.08 OK LC31 at 0.00% 0.08 OK LC32 at 0.00% 0.09 OK LC32 at 0.00% 0.08 OK LC32 at 0.00% 0.042 OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8

		1 C9 at 0 000/	0.36	ок	Eq. H3-8
		LC8 at 0.00%	0.30	OK	Eq. H2-1
		LC9 at 0.00% W180 at 0.00%	0.17	OK OK	Sec. F1
			0.23	OK	Eq. H3-8
		W210 at 0.00% Wi180 at 0.00%	0.10	OK	Sec. F1
		Wi210 at 0.00%	0.10	OK	Eq. H3-8
		WL180 at 0.00%	0.02	OK	Sec. F1
		WL210 at 0.00%	0.02	OK	Eq. H3-8
		**L210 at 0.0070	0.02		
PIPE 2x0.154	13	LC1 at 25.00%	0.44	OK	Eq. H1-1b
		LC10 at 72.92%	0.09	OK	Eq. H1-1b
		LC11 at 72.92%	0.20	OK	Eq. H1-1b
		LC12 at 72.92%	0.17	OK	Eq. H1-1b
		LC13 at 72.92%	0.06	OK	Eq. H1-1b
		LC14 at 72.92%	0.04	OK	Eq. H1-1b
		LC15 at 72.92%	0.06	OK	Eq. H1-1b
		LC16 at 72.92%	0.07	OK	Eq. H1-1b
		LC17 at 25.00%	0.07	OK	Eq. H1-1b
		LC18 at 72.92%	0.06	OK	Eq. H1-1b
		LC19 at 72.92%	0.07	OK	Eq. H1-1b
		LC2 at 72.92%	0.26	OK	Eq. H1-1b
		LC20 at 72.92%	0.06	OK	Eq. H1-1b
		LC21 at 25.00%	0.04	OK	Eq. H1-1b
		LC22 at 72.92%	0.04	OK	Eq. H1-1b
		LC23 at 72.92%	0.07	OK	Eq. H1-1b
		LC24 at 72.92%	0.07	OK	Eq. H1-1b
		LC25 at 72.92%	0.06	OK	Eq. H1-1b
		LC26 at 72.92%	0.07	OK	Eq. H1-1b
		LC27 at 72.92%	0.11	OK	Eq. H1-1b
		LC28 at 72.92%	0.10	OK	Eq. H1-1b
		LC29 at 72.92%	0.11	OK	Eq. H1-1b
		LC3 at 72.92%	0.45	OK	Eq. H1-1b
		LC30 at 72.92%	0.10	OK	Eq. H1-1b
		LC31 at 72.92%	0.14	OK	Eq. H1-1b
		LC32 at 72.92%	0.14	OK OK	Eq. H1-1b
		LC4 at 72.92%	0.34	OK	Eq. H1-1b
		LC5 at 25.00%	0.44	OK OK	Eq. H1-1b Eq. H1-1b
		LC6 at 72.92% LC7 at 72.92%	0.25 0.44	OK	Eq. H1-1b
		LC8 at 72.92%	0.33	OK	Eq. H1-1b
		LC9 at 25.00%	0.35	OK	Eq. H1-1b
		W180 at 25.00%	0.13	OK	Eq. H1-1b
		W210 at 72.92%	0.17	OK	Eq. H1-1b
		Wi180 at 25.00%	0.10	OK	Eq. H1-1b
		Wi210 at 72.92%	0.06	OK	Eq. H1-1b
		WL180 at 25.00%	0.02	OK	Eq. H1-1b
		WL210 at 72.92%	0.02	ок	Eq. H1-1b
				A.	— 114.41
	14	LC1 at 72.92%	0.59	OK	Eq. H1-1b
		LC10 at 72.92%	0.36	OK	Eq. H1-1b
		LC11 at 72.92%	0.16	OK OK	Eq. H1-1b
		LC12 at 72.92%	0.17 0.14	OK OK	Eq. H1-1b Eq. H1-1b
		LC13 at 72.92% LC14 at 72.92%	0.14	OK OK	Eq. H1-1b
		LC14 at 72.92%	0.09	OK OK	Eq. H1-1b
		LC16 at 72.92%	0.13	OK	Eq. H1-1b
		LC17 at 72.92%	0.17	ок	Eq. H1-1b
		LC18 at 72.92%	0.16	OK	Eq. H1-1b
		LC19 at 72.92%	0.11	ОК	Eq. H1-1b
		LC2 at 72.92%	0.54	OK	Eq. H1-1b
		LC20 at 72.92%	0.10	OK	Eq. H1-1b
		LC21 at 72.92%	0.16	OK	Eq. H1-1b
		LC22 at 72.92%	0.16	OK	Eq. H1-1b
		LC23 at 72.92%	0.11	OK	Eq. H1-1b

	LC24 at 72 02%	0.11	OK	Eg. H1-1b
	LC24 at 72.92%			•
	LC25 at 72.92%	0.29	OK	Eq. H1-1b
	LC26 at 72.92%	0.29	OK	Eq. H1-1b
				•
	LC27 at 72.92%	0.24	OK	Eq. H1-1b
	LC28 at 72.92%	0.24	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC29 at 72.92%	0.25		_ '
	LC3 at 72.92%	0.56	OK	Eq. H1-1b
	LC30 at 72.92%	0.25	OK	Eq. H1-1b
				•
	LC31 at 72.92%	0.20	OK	Eq. H1-1b
	LC32 at 72.92%	0.20	OK	Eq. H1-1b
	LC4 at 72.92%	0.29	OK	Eq. H1-1b
	LC5 at 72.92%	0.58	OK	Eg. H1-1b
	LC6 at 72.92%	0.50	ок	Eg. H1-1b
				•
	LC7 at 72.92%	0.56	OK	Eq. H1-1b
	LC8 at 72.92%	0.31	OK	Eq. H1-1b
				•
	LC9 at 72.92%	0.36	OK	Eq. H1-1b
	W180 at 72.92%	0.35	OK	Eq. H1-1b
		0.25	OK	Eq. H1-1b
	W210 at 72.92%			•
	Wi180 at 72.92%	0.13	OK	Eq. H1-1b
	Wi210 at 72.92%	0.09	OK	Eq. H1-1b
				•
	WL180 at 72.92%	0.03	OK	Eq. H1-1b
	WL210 at 72.92%	0.02	OK	Eq. H1-1b
				wearn and and renewaless.
16	LC1 at 72.92%	0.43	OK	Eq. H1-1b
	LC10 at 72.92%	0.08	OK	Eq. H1-1b
	LC11 at 25.00%	0.15	OK	Eq. H1-1b
	LC12 at 25.00%	0.14	OK	Eq. H1-1b
		0.03	OK	Eq. H1-1b
	LC13 at 25.00%			
	LC14 at 25.00%	0.02	OK	Eq. H1-1b
	LC15 at 25.00%	0.03	OK	Eq. H1-1b
				•
	LC16 at 72.92%	0.09	OK	Eq. H1-1b
	LC17 at 72.92%	0.10	OK	Eq. H1-1b
	LC18 at 72.92%	0.09	OK	Eq. H1-1b
				_ '
	LC19 at 72.92%	0.13	OK	Eq. H1-1b
	LC2 at 25.00%	0.30	OK	Eq. H1-1b
		0.12	OK	Eq. H1-1b
	LC20 at 72.92%			
	LC21 at 72.92%	0.07	OK	Eq. H1-1b
	LC22 at 72.92%	0.06	OK	Eq. H1-1b
				•
	LC23 at 72.92%	0.03	OK	Eq. H1-1b
	LC24 at 70.83%	0.04	OK	Eq. H1-1b
	LC25 at 72.92%	0.04	OK	Eq. H1-1b
	LC26 at 72.92%	0.03	OK	Eq. H1-1b
	LC27 at 25.00%	0.06	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC28 at 25.00%	0.06		
	LC29 at 25.00%	0.07	OK	Eq. H1-1b
	LC3 at 72.92%	0.39	OK	Eq. H1-1b
				Eg. H1-1b
	LC30 at 25.00%	0.07	OK	•
	LC31 at 25.00%	0.10	OK	Eq. H1-1b
	LC32 at 25.00%	0.10	OK	Eq. H1-1b
				•
	LC4 at 25.00%	0.37	OK	Eq. H1-1b
	LC5 at 72.92%	0.43	OK	Eq. H1-1b
	LC6 at 25.00%	0.31	OK	Eq. H1-1b
	LC7 at 72.92%	0.40	OK	Eq. H1-1b
	LC8 at 25.00%	0.35	OK	Eq. H1-1b
				•
	LC9 at 72.92%	0.12	OK	Eq. H1-1b
	W180 at 72.92%	0.25	OK	Eq. H1-1b
	W210 at 25.00%	0.20	ок	Eq. H1-1b
				•
	Wi180 at 72.92%	0.10	OK	Eq. H1-1b
	Wi210 at 25.00%	80.0	OK	Eg. H1-1b
	WL180 at 72.92%	0.02	OK	Eq. H1-1b
				· · · · · · · · · · · · · · · · · · ·
	WL210 at 25.00%	0.02	OK	Eq. H1-1b

25	LC1 at 10.00%	0.47	ОК	Eq. H1-1b
25				•
	LC10 at 63.75%	0.22	OK	Eq. H1-1b

	LC11 at 36.25%	0.21	OK	Eq. H1-1b
	LC12 at 11.25%	0.26	OK	Eq. H1-1b
	LC13 at 63.75%	0.07	OK	Eq. H1-1b
	LC14 at 63.75%	0.05	OK	Eq. H1-1b
	LC15 at 62.50%	0.07	OK	Eg. H1-1b
	LC16 at 63.75%	0.13	OK	Eq. H1-1b
	LC17 at 63.75%	0.13	ОК	Eg. H1-1b
	LC18 at 63.75%	0.17	OK	Eq. H1-1b
	LC19 at 63.75%	0.16	OK	Eq. H1-1b
	LC2 at 88.75%	0.68	OK	Eq. H1-1b
	LC20 at 63.75%	0.13	OK	Eq. H1-1b
	LC21 at 10.00%	0.07	OK	Eq. H1-1b
	LC22 at 0.00%	0.08	OK	Eq. H1-1b
	LC23 at 36.25%	0.11	OK	Eq. H1-1b
	LC24 at 36.25%	0.10	OK	Eq. H1-1b
	LC25 at 37.50%	0.14	OK	Eq. H1-1b
	LC26 at 37.50%	0.14	OK	Eq. H1-1b
	LC27 at 37.50%	0.18	OK	Eq. H1-1b
	LC28 at 37.50%	0.18	OK	Eq. H1-1b
	LC29 at 11.25%	0.19	OK	Eq. H1-1b
	LC3 at 36.25%	0.55	OK	Eq. H1-1b
	LC30 at 10.00%	0.16	OK	Eq. H1-1b
	LC31 at 11.25%	0.20	OK	Eq. H1-1b
	LC32 at 11.25%	0.23	OK	Eq. H1-1b
	LC4 at 88.75%	0.71	OK	Eq. H1-1b
	LC5 at 10.00%	0.46	OK	Eq. H1-1b
	LC6 at 88.75%	0.68	OK	Eq. H1-1b
	LC7 at 36.25%	0.54	OK	Eq. H1-1b
	LC8 at 88.75%	0.71	OK OK	Eq. H1-1b
	LC9 at 10.00%	0.20	OK	Eq. H1-1b
	W180 at 36.25%	0.32	OK OK	Eq. H1-1b Eq. H1-1b
	W210 at 88.75%	0.43 0.12	OK OK	Eq. H1-1b
	Wi180 at 36.25%			
	Wi210 at 88.75%	0.16	OK	Eq. H1-1b
	Wi210 at 88.75% WL180 at 36.25%	0.16 0.03	OK OK	Eq. H1-1b Eq. H1-1b
	Wi210 at 88.75%	0.16	OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25%	0.16 0.03	OK OK	Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75% LC1 at 90.00%	0.16 0.03 0.04 0.54	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12 0.17	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12 0.17 0.57	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12 0.17 0.57 0.20	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
26	Wi210 at 88.75% WL180 at 36.25% WL210 at 88.75%	0.16 0.03 0.04 0.54 0.24 0.22 0.21 0.08 0.06 0.08 0.12 0.16 0.15 0.12 0.69 0.14 0.07 0.11 0.08 0.07 0.15 0.19 0.16 0.12 0.17 0.57 0.20 0.21	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	LC5 at 90.00%	0.53	OK	Eq. H1-1b
				•
	LC6 at 36.25%	0.68	OK	Eq. H1-1b
	LC7 at 11.25%	0.56	OK	Eq. H1-1b
				•
	LC8 at 36.25%	0.60	OK	Eq. H1-1b
	LC9 at 63.75%	0.22	OK	Eq. H1-1b
	W180 at 11.25%	0.33	OK	Eq. H1-1b
				•
	W210 at 36.25%	0.39	OK	Eq. H1-1b
	Wi180 at 11.25%	0.12	OK	Eq. H1-1b
				•
	Wi210 at 36.25%	0.15	OK	Eq. H1-1b
	WL180 at 11.25%	0.03	OK	Eq. H1-1b
	WL210 at 36.25%	0.04	OK	Eq. H1-1b
			www.neorali.com.com.com.com.com	Marting Co.
27	LC1 at 88.75%	0.62	OK	Eq. H1-1b
	LC10 at 62.50%	0.19	OK	Eq. H1-1b
	LC11 at 10.00%	0.19	OK	Eq. H1-1b
	LC12 at 63.75%	0.22	OK	Eq. H1-1b
	LC13 at 63.75%	0.07	OK	Eq. H1-1b
	LC14 at 63.75%	0.05	OK	Eq. H1-1b
	LC15 at 37.50%	0.06	OK	Eg. H1-1b
				_ '
	LC16 at 63.75%	0.12	OK	Eq. H1-1b
	LC17 at 63.75%	0.13	OK	Eq. H1-1b
	LC18 at 63.75%	0.12	OK	Eq. H1-1b
				•
	LC19 at 63.75%	0.15	OK	Eq. H1-1b
	LC2 at 36.25%	0.52	OK	Eq. H1-1b
			OK	•
	LC20 at 63.75%	0.16		Eq. H1-1b
	LC21 at 36.25%	0.10	OK	Eq. H1-1b
	LC22 at 100.00%	0.07	OK	Eq. H1-1b
	LC23 at 0.00%	0.07	OK	Eq. H1-1b
	LC24 at 36.25%	0.09	OK	Eq. H1-1b
	LC25 at 37.50%	0.18	OK	Eq. H1-1b
				•
	LC26 at 37.50%	0.14	OK	Eq. H1-1b
	LC27 at 37.50%	0.13	OK	Eq. H1-1b
				•
	LC28 at 37.50%	0.17	OK	Eq. H1-1b
	LC29 at 11.25%	0.20	OK	Eq. H1-1b
				Ea U4 45
	LC3 at 88 75%	0.57	OK	EO 11-10
	LC3 at 88.75%	0.57	OK	Eq. H1-1b
	LC3 at 88.75% LC30 at 11.25%	0.57 0.19	OK	Eq. H1-1b
			OK	•
	LC30 at 11.25% LC31 at 10.00%	0.19 0.16	OK OK	Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25%	0.19 0.16 0.15	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00%	0.19 0.16	OK OK	Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25%	0.19 0.16 0.15 0.58	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75%	0.19 0.16 0.15 0.58 0.61	ОК ОК ОК ОК	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75%	0.19 0.16 0.15 0.58 0.61	ОК ОК ОК ОК	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% Wi210 at 36.25% WL180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% Wi210 at 36.25% WL180 at 88.75%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% WL210 at 36.25% UL310 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% WL210 at 36.25% UL180 at 88.75% WL210 at 36.25% UL10 at 36.25% LC1 at 25.00% LC10 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% UL180 at 88.75% LC1 at 25.00% LC1 at 72.92% LC11 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% UL180 at 88.75% LC1 at 25.00% LC1 at 72.92% LC11 at 72.92% LC12 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% UL180 at 88.75% LC1 at 25.00% LC1 at 72.92% LC11 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% WL10 at 72.92% LC1 at 72.92% LC12 at 72.92% LC13 at 25.00%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% WL10 at 72.92% LC1 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% WL10 at 72.92% LC1 at 72.92% LC12 at 72.92% LC13 at 25.00%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% LC9 at 37.50% W180 at 88.75% W210 at 36.25% Wi180 at 88.75% Wi210 at 36.25% WL180 at 88.75% WL210 at 36.25% WL10 at 72.92% LC1 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W1210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03 0.04 0.09	ОК ОК ОК ОК ОК ОК ОК ОК ОК ОК	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W1210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03 0.04 0.09 0.14	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W1210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03 0.04 0.09 0.14 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W1210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03 0.04 0.09 0.14 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W180 at 88.75% W1210 at 36.25% WL180 at 88.75% WL210 at 36.25% WL180 at 88.75% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC14 at 25.00% LC16 at 72.92% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC18 at 72.92% LC19 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.01 0.01 0.01 0.01 0.01 0.0	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
54	LC30 at 11.25% LC31 at 10.00% LC32 at 11.25% LC4 at 36.25% LC5 at 88.75% LC6 at 36.25% LC7 at 88.75% LC8 at 36.25% W180 at 88.75% W210 at 36.25% W180 at 88.75% W1210 at 36.25% W1180 at 88.75% W1210 at 36.25% WL180 at 88.75% LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92%	0.19 0.16 0.15 0.58 0.61 0.53 0.58 0.57 0.23 0.37 0.35 0.15 0.14 0.03 0.03 0.46 0.10 0.11 0.11 0.04 0.03 0.04 0.09 0.14 0.11	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	LC21 at 25.00%	0.03	OK	Eq. H1-1b
	LC22 at 72.92%	0.06	OK	Eq. H1-1b
	LC23 at 72.92%	0.07	OK	Eq. H1-1b
	LC24 at 72.92%	0.04	OK	Eq. H1-1b
	LC25 at 25.00%	0.07	OK	Eq. H1-1b
	LC26 at 25.00%	0.05	OK	Eq. H1-1b
	LC27 at 72.92%	0.04	OK	Eq. H1-1b
	LC28 at 25.00%	0.06	OK	Eq. H1-1b
		0.11	ok	Eq. H1-1b
	LC29 at 25.00%			•
	LC3 at 25.00%	0.40	OK	Eq. H1-1b
	LC30 at 25.00%	0.09	OK	Eq. H1-1b
	LC31 at 25.00%	0.08	OK	Eq. H1-1b
	LC32 at 25.00%	0.10	OK	Eq. H1-1b
	LC4 at 72.92%	0.26	OK	Eq. H1-1b
	LC5 at 25.00%	0.45	OK	Eq. H1-1b
	LC6 at 72.92%	0.30	OK	Eq. H1-1b
	LC7 at 25.00%	0.40	OK	Eq. H1-1b
	LC8 at 72.92%	0.27	OK	Eq. H1-1b
	LC9 at 25.00%	0.17	OK	Eq. H1-1b
	W180 at 25.00%	0.27	OK	Eq. H1-1b
	W210 at 72.92%	0.17	OK	Eq. H1-1b
	Wi180 at 25.00%	0.10	OK	Eq. H1-1b
	Wi210 at 72.92%	0.06	OK	Eq. H1-1b
	WL180 at 25.00%	0.02	OK	Eq. H1-1b
	WL210 at 72.92%	0.02	OK	Eq. H1-1b
	VVL210 at 72.3270	0.02	OR .	_q;;;;;;
57	LC1 at 25.00%	0.52	OK	Eq. H1-1b
31			OK	Eq. H1-1b
	LC10 at 25.00%	0.12		
	LC11 at 25.00%	0.13	OK	Eq. H1-1b
	LC12 at 72.92%	0.12	OK	Eq. H1-1b
	LC13 at 72.92%	0.03	OK	Eq. H1-1b
	LC14 at 72.92%	0.02	OK	Eq. H1-1b
	LC15 at 25.00%	0.03	OK	Eq. H1-1b
	LC16 at 72.92%	0.05	OK	Eq. H1-1b
	LC17 at 72.92%	0.13	OK	Eq. H1-1b
	LC18 at 72.92%	0.09	ОК	Eq. H1-1b
	LC19 at 72.92%	0.09	OK	Eq. H1-1b
	LO 13 at 12.32 /0	0.00		Eq. H1-1b
	LC2 at 25 00%	U 30	ΩK	
	LC2 at 25.00%	0.39	OK	•
	LC20 at 72.92%	0.12	OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92%	0.12 0.18	OK OK	Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.12	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92%	0.12 0.18	OK OK	Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.12 0.18 0.14	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92%	0.12 0.18 0.14 0.14 0.17	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.12 0.18 0.14 0.14 0.17 0.05	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00%	0.12 0.18 0.14 0.14 0.17 0.05 0.09	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00%	0.12 0.18 0.14 0.14 0.17 0.05 0.09	OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 25.00% LC29 at 72.92%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05	OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 25.00% LC29 at 72.92% LC3 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC3 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 25.00% LC29 at 72.92% LC3 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC3 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC32 at 72.92%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05 0.05 0.05	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.05 0.05 0.06 0.06 0.04 0.34	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.05 0.05 0.05 0.06 0.06 0.04 0.34 0.52 0.38	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC28 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.06 0.06 0.04 0.34 0.52 0.38 0.52	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00% LC8 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.05 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC29 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.05 0.05 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32	OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC4 at 25.00% LC5 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00% W210 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.52 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32 0.23	OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00% W210 at 25.00% W180 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.52 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32 0.23 0.12	OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC4 at 25.00% LC5 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00% W210 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.52 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32 0.23	OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC3 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00% W210 at 25.00% W180 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.52 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32 0.23 0.12	OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC30 at 25.00% LC30 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 72.92% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00% W210 at 25.00% W1180 at 25.00% W1180 at 25.00%	0.12 0.18 0.14 0.17 0.05 0.09 0.09 0.05 0.52 0.06 0.06 0.04 0.34 0.52 0.38 0.52 0.35 0.16 0.32 0.23 0.12 0.08	OK O	Eq. H1-1b

	2442224242422244			
15	LC1 at 25.00%	0.50	OK	Eq. H1-1b
	LC10 at 25.00%	0.09	OK	Eq. H1-1b
	LC11 at 72.92%	0.17	OK	Eg. H1-1b
	LC12 at 72.92%	0.13	OK	Eq. H1-1b
	LC13 at 72.92%	0.04	OK	Eq. H1-1b
	LC14 at 72.92%	0.03	OK	Eq. H1-1b
	LC15 at 72.92%	0.03	OK	Eq. H1-1b
	LC16 at 72.92%	0.06	OK	Eq. H1-1b
	LC17 at 72.92%	0.09	OK	Eq. H1-1b
	LC18 at 72.92%	0.10	OK	Eq. H1-1b
	LC19 at 72.92%	0.14	OK	Eq. H1-1b
	LC2 at 25.00%	0.41	OK	Eg. H1-1b
	LC20 at 72.92%	0.13	OK	Eg. H1-1b
	LC21 at 72.92%	0.14	ok	Eg. H1-1b
			ok	Eq. H1-1b
	LC22 at 72.92%	0.15		•
	LC23 at 72.92%	0.19	OK	Eq. H1-1b
	LC24 at 72.92%	0.18	OK	Eq. H1-1b
	LC25 at 25.00%	0.09	OK	Eq. H1-1b
	LC26 at 25.00%	0.07	OK	Eq. H1-1b
	LC27 at 72.92%	0.06	OK	Eq. H1-1b
	LC28 at 25.00%	0.06	OK	Eq. H1-1b
	LC29 at 25.00%	0.06	OK	Eq. H1-1b
	LC3 at 25.00%	0.46	OK	Eg. H1-1b
	LC30 at 25.00%	0.05	OK	Eq. H1-1b
		0.05	ok	Eq. H1-1b
	LC31 at 72.92%			Eq. H1-1b
	LC32 at 72.92%	0.04	OK	·
	LC4 at 25.00%	0.41	OK	Eq. H1-1b
	LC5 at 25.00%	0.50	OK	Eq. H1-1b
	LC6 at 25.00%	0.41	OK	Eq. H1-1b
	LC7 at 25.00%	0.47	OK	Eq. H1-1b
	LC8 at 25.00%	0.41	OK	Eq. H1-1b
	LC9 at 25.00%	0.15	OK	Eq. H1-1b
51	W180 at 25.00%	0.30	OK	Eq. H1-1b
	W210 at 25.00%	0.25	OK	Eg. H1-1b
	Wi180 at 25.00%	0.12	OK	Eq. H1-1b
			OK	Eq. H1-1b
	Wi210 at 25.00%	0.09		
	WL180 at 25.00%	0.03	OK	Eq. H1-1b
	WL210 at 25.00%	0.02	OK 	Eq. H1-1b
60	LC1 at 72.92%	0.39	OK	Eq. H1-1b
	LC10 at 72.92%	0.32	OK	Eq. H1-1b
	LC11 at 72.92%	0.39	OK	Eq. H1-1b
	LC12 at 72.92%	0.23	OK	Eq. H1-1b
	LC13 at 72.92%	0.14	OK	Eq. H1-1b
	LC14 at 72.92%	0.10	OK	Eq. H1-1b
	LC15 at 72.92%	0.14	OK	Eq. H1-1b
	LC16 at 72.92%	0.17	OK	Eq. H1-1b
	LC17 at 72.92%	0.11	OK	Eq. H1-1b
	LC18 at 72.92%	0.14	OK	Eq. H1-1b
	LC19 at 72.92%	0.17	OK	Eg. H1-1b
	LC2 at 72.92%	0.53	OK	Eq. H1-1b
			OK OK	Eq. H1-1b
	LC20 at 72.92%	0.13		
	LC21 at 72.92%	0.12	OK	Eq. H1-1b
	LC22 at 72.92%	0.15	OK	Eq. H1-1b
	LC23 at 72.92%	0.17	OK	Eq. H1-1b
	LC24 at 72.92%	0.13	OK	Eq. H1-1b
	LC25 at 72.92%	0.24	OK	Eq. H1-1b
	LC26 at 72.92%	0.28	OK	Eq. H1-1b
	LC27 at 72.92%	0.30	OK	Eq. H1-1b
	LC28 at 72.92%	0.26	OK	Eq. H1-1b
ef	LC29 at 72.92%	0.20	OK	Eq. H1-1b
	LC3 at 72.92%	0.65	OK	Eg. H1-1b
	LC30 at 72.92%	0.24	OK	Eg. H1-1b
	E000 at 12.02/0	J	5.1	-4

	LC31 at 72.92%	0.26	OK	Eq. H1-1b
	LC32 at 72.92%	0.22	OK	Eq. H1-1b
	LC4 at 72.92%	0.49	OK	Eq. H1-1b
	LC5 at 72.92%	0.42	OK	Eq. H1-1b
	LC6 at 72.92%	0.52	OK	Eq. H1-1b
	LC7 at 72.92%	0.62	OK	Eq. H1-1b
	LC8 at 72.92%	0.49	OK	Eq. H1-1b
	LC9 at 72.92%	0.15	OK	Eq. H1-1b
	W180 at 72.92%	0.32	OK	Eq. H1-1b
	W210 at 72.92%	0.31	ОК	Eq. H1-1b
	Wi180 at 72.92%	0.12	OK	Eq. H1-1b
				•
	Wi210 at 72.92%	0.11	OK	Eq. H1-1b
	WL180 at 72.92%	0.03	OK	Eq. H1-1b
	WL210 at 72.92%	0.03	OK	Eq. H1-1b
63	LC1 at 72.92%	0.47	OK	Eq. H1-1b
	LC10 at 25.00%	0.13	OK	Eq. H1-1b
	LC11 at 72.92%	0.13	OK	Eq. H1-1b
				Eq. H1-1b
	LC12 at 72.92%	0.15	OK	_ '
	LC13 at 72.92%	0.05	OK	Eq. H1-1b
	LC14 at 72.92%	0.04	OK	Eq. H1-1b
	LC15 at 72.92%	0.06	OK	Eq. H1-1b
	LC16 at 72.92%	0.07	OK	Eq. H1-1b
	LC17 at 72.92%	0.06	OK	Eq. H1-1b
	LC18 at 25.00%	0.08	OK	Eq. H1-1b
	LC19 at 72.92%	0.07	OK	Eq. H1-1b
	LC2 at 25.00%	0.35	OK	Eq. H1-1b
	LC20 at 72.92%	0.05	OK	Eq. H1-1b
	LC21 at 72.92%	0.07	OK	Eq. H1-1b
	LC22 at 25.00%	0.05	OK	Eq. H1-1b
	LC23 at 72.92%	0.05	ОК	Eq. H1-1b
		0.07	OK	Eq. H1-1b
	LC24 at 72.92%			
	LC25 at 72.92%	0.10	OK	Eq. H1-1b
	LC26 at 72.92%	0.06	OK	Eq. H1-1b
	LC27 at 72.92%	0.06	OK	Eq. H1-1b
	LC28 at 72.92%	0.09	OK	Eq. H1-1b
	LC29 at 72.92%	0.14	OK	Eq. H1-1b
	LC3 at 72.92%	0.38	ОК	Eq. H1-1b
		0.11	OK	Eq. H1-1b
	LC30 at 72.92%			•
	LC31 at 72.92%	0.12	OK	Eq. H1-1b
	LC32 at 72.92%	0.13	OK	Eq. H1-1b
	LC4 at 25.00%	0.31	OK	Eq. H1-1b
	LC5 at 72.92%	0.46	OK	Eq. H1-1b
	LC6 at 25.00%	0.34	OK	Eq. H1-1b
	LC7 at 72.92%	0.38	ОК	Eq. H1-1b
	LC8 at 25.00%	0.31	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC9 at 72.92%	0.19		· · · · · · · · · · · · · · · · · · ·
	W180 at 72.92%	0.26	OK	Eq. H1-1b
	W210 at 25.00%	0.21	OK	Eq. H1-1b
	Wi180 at 72.92%	0.10	OK	Eq. H1-1b
	Wi210 at 25.00%	0.08	OK	Eq. H1-1b
	WL180 at 72.92%	0.02	OK	Eq. H1-1b
	WL210 at 25.00%	0.02	OK	Eq. H1-1b

66	I C1 at 25 00%	0.14	OK	
66	LC1 at 25.00%			Ea H1 1h
	LC10 at 25.00%	0.18	OK OK	Eq. H1-1b
	LC11 at 31.25%	0.10	OK	Eq. H1-1b
		0.13	OK	Eq. H1-1b
	LC12 at 72.92%	0.10		•
	LC12 at 72.92% LC13 at 25.00%	0.04	OK	Eq. H1-1b
	LC13 at 25.00%	0.04	OK	•
	LC13 at 25.00% LC14 at 25.00%	0.04 0.03	OK OK	Eq. H1-1b Eq. H1-1b
	LC13 at 25.00% LC14 at 25.00% LC15 at 25.00%	0.04 0.03 0.03	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 25.00% LC14 at 25.00% LC15 at 25.00% LC16 at 72.92%	0.04 0.03 0.03 0.09	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC13 at 25.00% LC14 at 25.00% LC15 at 25.00%	0.04 0.03 0.03	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b

	LC19 at 72.92%	0.11	OK	Eg. H1-1b
	LC2 at 25.00%	0.50	OK	Eg. H1-1b
	LC20 at 72.92%	0.11	OK	Eg. H1-1b
	LC21 at 72.92%	0.04	OK	Eq. H1-1b
	LC22 at 25.00%	0.03	OK	Eq. H1-1b
	LC23 at 72.92%	0.05	OK	Eq. H1-1b
	LC24 at 72.92%	0.07	OK	Eq. H1-1b
	LC25 at 25.00%	0.04	OK	Eq. H1-1b
	LC26 at 25.00%	0.07	OK	Eq. H1-1b
	LC27 at 25.00%	0.05	OK	Eq. H1-1b
	LC28 at 72.92%	0.05	OK	Eq. H1-1b
	LC29 at 25.00%	0.08	OK	Eq. H1-1b
	LC3 at 31.25%	0.17	OK	Eq. H1-1b
	LC30 at 25.00%	0.11	OK	Eq. H1-1b
	LC31 at 25.00%	0.09	OK	Eq. H1-1b
	LC32 at 25.00%	0.07	OK	Eq. H1-1b
	LC4 at 72.92%	0.50	OK	Eq. H1-1b
	LC5 at 25.00%	0.14	OK	
	LC6 at 25.00%	0.49	OK	Eq. H1-1b
	LC7 at 31.25%	0.17	OK	Eq. H1-1b
	LC8 at 72.92%	0.50	OK	Eq. H1-1b
	LC9 at 72.92%	0.05	OK	Eq. H1-1b
	W180 at 25.00%	0.09	OK	
	W210 at 72.92%	0.30	OK	Eq. H1-1b
	Wi180 at 31.25%	0.03	OK	Eq. H1-1b
	Wi210 at 25.00%	0.11	OK	Eq. H1-1b
	WL180 at 31.25%	0.01	OK	Eq. H1-1b
	WL210 at 25.00%	0.03	OK	Eq. H1-1b
69	LC1 at 25.00%	0.12	OK	Eg. H1-1b
03	LC10 at 72.92%	0.12	OK	Eq. H1-1b
	LC11 at 72.92%	0.08	OK	Eq. H1-1b
	LC12 at 25.00%	0.16	OK	Eg. H1-1b
	LC13 at 72.92%	0.04	OK	Eq. H1-1b
	LC14 at 72.92%	0.03	OK	Eg. H1-1b
	LC15 at 25.00%	0.03	OK	Eq. H1-1b
	LC16 at 72.92%	0.06	OK	Eq. H1-1b
	LC17 at 72.92%	0.11	OK	Eq. H1-1b
	LC18 at 72.92%	0.14	OK	Eq. H1-1b
	LC19 at 72.92%	0.11	OK	Eq. H1-1b
		O EC	OK	
	LC2 at 25.00%	0.56	OIL	Eq. H1-1b
	LC2 at 25.00% LC20 at 72.92%	0.09	OK	Eq. H1-1b Eq. H1-1b
				·
	LC20 at 72.92%	0.09	OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92%	0.09 0.16	OK OK	Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.09 0.16 0.19	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92%	0.09 0.16 0.19 0.16	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92%	0.09 0.16 0.19 0.16 0.14 0.06	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.06 0.07	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC27 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.06 0.07	OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC28 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.06 0.07 0.09 0.04	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC3 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.06 0.07 0.09 0.04 0.13	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC30 at 72.92%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC29 at 25.00% LC3 at 25.00% LC3 at 25.00% LC30 at 72.92% LC31 at 25.00% LC32 at 25.00%	0.09 0.16 0.19 0.16 0.04 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00% LC30 at 72.92% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC32 at 25.00% LC32 at 25.00%	0.09 0.16 0.19 0.16 0.014 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00% LC30 at 72.92% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC36 at 25.00% LC4 at 25.00% LC5 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00% LC30 at 72.92% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00%	0.09 0.16 0.19 0.16 0.014 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56 0.12	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC30 at 72.92% LC31 at 25.00% LC31 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56 0.12 0.55	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC29 at 25.00% LC3 at 25.00% LC3 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56 0.12 0.55 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC28 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00% LC3 at 25.00% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92% W180 at 25.00%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56 0.12 0.55 0.07 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 25.00% LC26 at 72.92% LC27 at 25.00% LC29 at 25.00% LC3 at 25.00% LC3 at 25.00% LC31 at 25.00% LC31 at 25.00% LC32 at 25.00% LC32 at 25.00% LC4 at 25.00% LC5 at 25.00% LC5 at 25.00% LC6 at 25.00% LC6 at 25.00% LC7 at 25.00% LC7 at 25.00% LC9 at 72.92%	0.09 0.16 0.19 0.16 0.14 0.06 0.07 0.09 0.04 0.13 0.06 0.05 0.07 0.55 0.12 0.56 0.12 0.55 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	Wi210 at 25.00%	0.13	OK	Eq. H1-1b
	WL180 at 25.00%	0.01	OK	Eq. H1-1b
				Eq. H1-1b
	WL210 at 25.00%	0.03	OK	Eq. H1-1b
				= 114.41
72	LC1 at 72.92%	0.29	OK	Eq. H1-1b
	LC10 at 72.92%	0.16	OK	Eq. H1-1b
	LC11 at 72.92%	0.26	OK	Eq. H1-1b
	LC12 at 72.92%	0.42	OK	Eq. H1-1b
	LC13 at 72.92%	0.15	OK	Eq. H1-1b
	LC14 at 72.92%	0.10	OK	Eq. H1-1b
	LC15 at 72.92%	0.15	OK	Eq. H1-1b
	LC16 at 72.92%	0.18	ok	Eq. H1-1b
				·
	LC17 at 72.92%	0.16	OK	Eq. H1-1b
	LC18 at 72.92%	0.12	OK	Eq. H1-1b
	LC19 at 72.92%	0.13	OK	Eq. H1-1b
	LC2 at 72.92%	0.56	OK	Eq. H1-1b
	LC20 at 72.92%	0.18	OK	Eq. H1-1b
	LC21 at 72.92%	0.16	OK	Eq. H1-1b
	LC22 at 72.92%	0.12	OK	Eq. H1-1b
	LC23 at 72.92%	0.15	OK	Eq. H1-1b
	LC24 at 72.92%	0.19	ok	Eq. H1-1b
		0.29	ok	Eq. H1-1b
	LC25 at 72.92%			· ·
	LC26 at 72.92%	0.25	OK	Eq. H1-1b
	LC27 at 72.92%	0.27	OK	Eq. H1-1b
	LC28 at 72.92%	0.31	OK	Eq. H1-1b
	LC29 at 72.92%	0.25	OK	Eq. H1-1b
	LC3 at 72.92%	0.28	OK	Eq. H1-1b
	LC30 at 72.92%	0.21	OK	Eq. H1-1b
	LC31 at 72.92%	0.23	OK	Eq. H1-1b
	LC32 at 72.92%	0.27	OK	Eq. H1-1b
	LC4 at 72.92%	0.74	OK	Eq. H1-1b
				·
	LC5 at 72.92%	0.25	OK	Eq. H1-1b
	LC6 at 72.92%	0.55	OK	Eq. H1-1b
	LC7 at 72.92%	0.27	OK	Eq. H1-1b
	LC8 at 72.92%	0.69	OK	Eq. H1-1b
	LC9 at 72.92%	0.32	OK	Eq. H1-1b
	W180 at 72.92%	0.15	OK	Eq. H1-1b
	W210 at 72.92%	0.36	OK	Eq. H1-1b
	Wi180 at 72.92%	0.05	OK	Eq. H1-1b
	Wi210 at 72.92%	0.13	ok	Eq. H1-1b
			OK	Eq. H1-1b
	WL180 at 72.92%	0.01		
	WL210 at 72.92%	0.03	OK	Eq. H1-1b

75	LC1 at 25.00%	0.16	OK	
	LC10 at 72.92%	0.24	OK	Eq. H1-1b
	LC11 at 72.92%	0.14	OK	Eq. H1-1b
	LC12 at 25.00%	0.16	OK	Eq. H1-1b
	LC13 at 72.92%	0.07	OK	Eq. H1-1b
	LC14 at 72.92%	0.05	OK	Eq. H1-1b
	LC15 at 72.92%	0.08	OK	Eq. H1-1b
	LC16 at 25.00%	0.08	OK	Eq. H1-1b
	LC17 at 72.92%	0.07	OK	Eq. H1-1b
	LC18 at 72.92%	0.09	OK	Eq. H1-1b
	LC19 at 25.00%	0.07	OK	Eq. H1-1b
	LC2 at 72.92%	0.58	OK	Eq. H1-1b
	LC20 at 72.92%	0.09	OK	Eq. H1-1b
	LC21 at 72.92%	0.08	OK	Eq. H1-1b
	LC22 at 72.92%	0.09	OK	Eq. H1-1b
	LC23 at 72.92%	80.0	OK	Eq. H1-1b
	LC24 at 72.92%	0.05	OK	Eq. H1-1b
	LC25 at 72.92%	0.10	ОК	Eq. H1-1b
	LC25 at 72.92%	0.10	OK OK	Eq. H1-1b
	LC27 at 72.92%	0.10	OK	Eq. H1-1b
	LC28 at 72.92%	80.0	OK	Eq. H1-1b

		LC29 at 72.92%	0.14	ок	Eq. H1-1b
		LC3 at 25.00%	0.16	OK	
		LC30 at 72.92%	0.17	OK	Eq. H1-1b
		LC31 at 72.92%	0.14	OK	Eq. H1-1b
		LC32 at 72.92%	0.12	OK	Eq. H1-1b
		LC4 at 25.00%	0.47	OK	Eq. H1-1b
		LC5 at 25.00%	0.16	OK	
		LC6 at 72.92%	0.56	OK	Eq. H1-1b
		LC7 at 25.00%	0.16	OK	
		LC8 at 25.00%	0.47	OK	Eq. H1-1b
		LC9 at 72.92%	0.12	OK	Eq. H1-1b
		W180 at 25.00%	0.10	OK	•
		W210 at 72.92%	0.31	OK	Eq. H1-1b
		Wi180 at 25.00%	0.04	OK	-4
		Wi210 at 72.92%	0.12	OK	Eq. H1-1b
		WL180 at 25.00%	0.01	OK	-4
		WL210 at 72.92%	0.03	ок	Eq. H1-1b
T21 2V2V4 4	10	L C1 at 100 00%	0.21	OK	Eq. H1-1b
T2L 3X3X1_4	10	LC1 at 100.00% LC10 at 100.00%	0.21 0.64	OK OK	Eq. H1-1b
				OK	Eq. H1-1b
		LC11 at 100.00%	0.63		
		LC12 at 100.00%	0.50	OK -	Eq. H1-1b
		LC13 at 100.00%	0.30	OK	Eq. H1-1b
		LC14 at 100.00%	0.22	OK	Eq. H1-1b
		LC15 at 100.00%	0.32	OK	Eq. H1-1b
		LC16 at 25.00%	0.43	OK	Eq. H1-1b
		LC17 at 100.00%	0.50	OK	Eq. H1-1b
		LC18 at 100.00%	0.52	OK	Eq. H1-1b
		LC19 at 100.00%	0.50	OK	Eq. H1-1b
		LC2 at 100.00%	0.65	ок	Eq. H1-1b
		LC20 at 100.00%	0.48	OK	Eq. H1-1b
		LC21 at 100.00%	0.36	OK	Eq. H1-1b
		LC22 at 100.00%	0.39	OK	Eq. H1-1b
		LC23 at 100.00%	0.39	OK	Eq. H1-1b
		LC24 at 100.00%	0.36	OK	Eq. H1-1b
		LC25 at 100.00%	0.37	OK	Eq. H1-1b
		LC26 at 100.00%	0.40	OK	Eq. H1-1b
		LC27 at 100.00%	0.40	OK	Eq. H1-1b
		LC28 at 100.00%	0.37	OK	Eq. H1-1b
		LC29 at 100.00%	0.51	OK	Eq. H1-1b
		LC3 at 100.00%	0.58	OK	Eq. H1-1b
		LC30 at 100.00%	0.54	OK	Eq. H1-1b
		LC31 at 100.00%	0.54	OK	Eq. H1-1b
		LC32 at 100.00%	0.51	OK	Eq. H1-1b
		LC4 at 25.00%	0.25	OK	Eq. H1-1b
		LC5 at 100.00%	0.14	OK	Eq. H1-1b
		LC6 at 100.00%	0.58	OK	Eq. H1-1b
		LC7 at 100.00%	0.51	OK	Eq. H1-1b
		LC8 at 25.00%	0.34	OK	Eq. H1-1b
		LC9 at 100.00%	0.51	OK	Eq. H1-1b
		W180 at 100.00%	0.18	OK	Eq. H1-1b
		W210 at 25.00%	0.38	OK	Eq. H1-1b
		Wi180 at 100.00%	0.06	OK	Eg. H1-1b
		Wi210 at 25.00%	0.14	ОК	Eq. H1-1b
		WL180 at 100.00%	0.02	ОК	Eq. H1-1b
		WL210 at 25.00%	0.03	ок	Eq. H1-1b
	11	LC1 at 100.00%	 0.16	ок	Eq. H1-1b
		LC10 at 100.00%	0.41	OK OK	Eq. H1-1b
		LC11 at 100.00%	0.52	ОК	Eq. H1-1b
		LC12 at 100.00%	0.58	OK	Eq. H1-1b
		LC12 at 100.00%	0.35	OK OK	Eq. H1-1b
		LC14 at 100.00%	0.23	OK	Eq. H1-1b
		LC15 at 100.00%	0.18	OK	Eq. H1-1b
		LO 10 dt 100.00%	0.27	OK.	Eq. 111-10

	LC16 at 25.00%	0.40	OK	Eq. H1-1b
	LC17 at 100.00%	0.44	OK	Eq. H1-1b
	LC18 at 100.00%	0.44	OK	Eq. H1-1b
	LC19 at 100.00%	0.47	OK	Eq. H1-1b
	LC2 at 25.00%	0.32	OK	Eq. H1-1b
	LC20 at 100.00%	0.47	OK	Eq. H1-1b
	LC21 at 100.00%	0.31	OK	Eq. H1-1b
	LC22 at 100.00%	0.30	OK	Eq. H1-1b
	LC23 at 100.00%	0.33	OK	Eq. H1-1b
	LC24 at 100.00%	0.34	OK	Eq. H1-1b
	LC25 at 100.00%	0.32	OK	Eq. H1-1b
	LC26 at 100.00%	0.31	OK	Eq. H1-1b
	LC27 at 100.00%	0.34	OK	Eq. H1-1b
	LC28 at 100.00%	0.35	OK	Eq. H1-1b
	LC29 at 100.00%	0.47	OK	Eq. H1-1b
	LC3 at 100.00%	0.50	OK	Eq. H1-1b
	LC30 at 100.00%	0.45	OK OK	Eq. H1-1b Eq. H1-1b
	LC31 at 100.00%	0.48 0.49	OK OK	Eq. H1-1b
	LC32 at 100.00% LC4 at 100.00%	0.49	OK OK	Eq. H1-1b
	LC5 at 34.38%	0.11	OK	Eg. H1-1b
	LC6 at 25.00%	0.39	OK	Eq. H1-1b
	LC7 at 100.00%	0.44	OK	Eq. H1-1b
	LC8 at 100.00%	0.59	OK	Eg. H1-1b
	LC9 at 100.00%	0.47	OK	Eq. H1-1b
	W180 at 100.00%	0.17	OK	Eq. H1-1b
	W210 at 100.00%	0.25	OK	Eq. H1-1b
	Wi180 at 100.00%	0.06	OK	Eq. H1-1b
	Wi210 at 100.00%	0.09	OK	Eq. H1-1b
	WL180 at 100.00%	0.01	OK	Eq. H1-1b
	WL210 at 100.00%	0.02	OK	Eq. H1-1b
40	L O4 = 1400 000/	0.63	OK	Eq. H1-1b
12	LC1 at 100.00% LC10 at 100.00%	0.63 0.51	ок ок	Eq. H1-1b
	LC11 at 100 00%	() 41	()K	Fa. H1-10
	LC11 at 100.00%	0.41 0.48	OK OK	Eq. H1-1b Ea. H1-1b
	LC12 at 100.00%	0.48	ОК	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00%	0.48 0.25	OK OK	Eq. H1-1b
	LC12 at 100.00%	0.48	ОК	Eq. H1-1b Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00%	0.48 0.25 0.18	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00%	0.48 0.25 0.18 0.27	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00%	0.48 0.25 0.18 0.27 0.40	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47	OK OK OK OK OK OK OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45	OK OK OK OK OK OK OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35	OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34	OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34	OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC21 at 100.00% LC22 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32	OK	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.35	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC27 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC17 at 100.00% LC18 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC29 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49 0.37	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 25.00% LC30 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 25.00% LC30 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48 0.45	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48 0.45 0.47	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC21 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC28 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.32 0.32 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48 0.45	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 100.00% LC6 at 100.00% LC6 at 100.00% LC6 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.34 0.32 0.30 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48 0.45 0.47 0.49	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC18 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 100.00% LC6 at 100.00% LC7 at 25.00% LC8 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.32 0.32 0.32 0.32 0.32 0.35 0.33 0.31 0.32 0.49 0.37 0.48 0.45 0.47 0.49 0.47	OK O	Eq. H1-1b
	LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC16 at 25.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 100.00% LC6 at 100.00% LC6 at 100.00% LC6 at 100.00%	0.48 0.25 0.18 0.27 0.40 0.47 0.45 0.44 0.35 0.46 0.32 0.32 0.32 0.33 0.31 0.32 0.49 0.37 0.48 0.45 0.47 0.48 0.47 0.49 0.49 0.49 0.49 0.31	OK O	Eq. H1-1b

			014	E 114.45
	W180 at 25.00%	0.41	OK	Eq. H1-1b
	W210 at 100.00%	0.07	OK	Eq. H1-1b
	Wi180 at 25.00%	0.16	OK	Eq. H1-1b
	Wi210 at 100.00%	0.02	OK	Eq. H1-1b
	WL180 at 25.00%	0.04	OK	Eq. H1-1b
	WL210 at 100.00%	0.01	OK	Eq. H1-1b
	VVL210 Bt 100.0070			_q
31	LC1 at 0.00%	0.01	ОК	Eq. H1-1b
31				Eq. H1-1b
	LC10 at 0.00%	0.41	OK	•
	LC11 at 0.00%	0.38	OK	Eq. H1-1b
	LC12 at 0.00%	0.27	OK	Eq. H1-1b
	LC13 at 0.00%	0.17	OK	Eq. H1-1b
	LC14 at 0.00%	0.13	OK	Eq. H1-1b
	LC15 at 0.00%	0.18	OK	Eq. H1-1b
	LC16 at 0.00%	0.36	OK	Eq. H1-1b
	LC17 at 0.00%	0.29	OK	Eq. H1-1b
	LC18 at 0.00%	0.32	OK	Eq. H1-1b
	LC19 at 0.00%	0.31	ОК	Eq. H1-1b
	LC2 at 0.00%	0.46	OK	Eg. H1-1b
		0.29	ок	Eq. H1-1b
	LC20 at 0.00%			Eq. H1-1b
	LC21 at 0.00%	0.19	OK	•
	LC22 at 0.00%	0.22	OK	Eq. H1-1b
	LC23 at 0.00%	0.21	OK	Eq. H1-1b
	LC24 at 0.00%	0.18	OK	Eq. H1-1b
	LC25 at 0.00%	0.19	OK	Eq. H1-1b
	LC26 at 0.00%	0.22	OK	Eq. H1-1b
	LC27 at 0.00%	0.21	OK	Eq. H1-1b
	LC28 at 0.00%	0.18	OK	Eq. H1-1b
	LC29 at 0.00%	0.30	ОК	Eq. H1-1b
	LC3 at 0.00%	0.33	ОК	Eq. H1-1b
	LC30 at 0.00%	0.32	OK	Eq. H1-1b
	LC31 at 0.00%	0.31	OK	Eq. H1-1b
	LC32 at 0.00%	0.29	OK	Eq. H1-1b
	LC4 at 0.00%	0.07	OK	Eq. H1-1b
	LC5 at 0.00%	0.02	OK	Eq. H1-1b
	LC6 at 0.00%	0.42	OK	Eq. H1-1b
	LC7 at 0.00%	0.29	OK	Eq. H1-1b
	LC8 at 0.00%	0.09	OK	Eq. H1-1b
	LC9 at 0.00%	0.30	OK	Eq. H1-1b
	W180 at 0.00%	0.10	OK	Eq. H1-1b
	W210 at 0.00%	0.10	ОК	Eq. H1-1b
	Wi180 at 0.00%	0.04	ОК	Eq. H1-1b
	Wi210 at 0.00%	0.04	OK	Eq. H1-1b
	WL180 at 0.00%	0.01	ОК	Eq. H1-1b
	WL210 at 0.00%	0.01	OK	Eq. H1-1b
	VVL2.10 at 0.0070	0.01		
20	L C4 at 04 050/	0.00	OK	Eg. H1-1b
32	LC1 at 81.25%	0.02	OK	•
	LC10 at 100.00%	0.22	OK	Eq. H1-1b
	LC11 at 100.00%	0.33	OK	Eq. H1-1b
	LC12 at 100.00%	0.36	OK	Eq. H1-1b
	LC13 at 100.00%	0.14	OK	Eq. H1-1b
	LC14 at 100.00%	0.10	OK	Eq. H1-1b
	LC15 at 100.00%	0.15	OK	Eq. H1-1b
	LC16 at 100.00%	0.33	OK	Eq. H1-1b
	LC17 at 100.00%	0.26	OK	Eq. H1-1b
	LC18 at 100.00%	0.25	OK	Eq. H1-1b
	LC19 at 100.00%	0.28	OK	Eq. H1-1b
	LC2 at 100.00%	0.09	OK	Eq. H1-1b
				Eq. H1-1b
	LC20 at 100.00%	0.29	OK OK	
	LC21 at 100.00%	0.16	OK	Eq. H1-1b
	LC22 at 100.00%	0.15	OK	Eq. H1-1b
	LC23 at 100.00%	0.18	OK	Eq. H1-1b
	LC24 at 100.00%	0.18	OK	Eq. H1-1b
	LC25 at 100.00%	0.16	OK	Eq. H1-1b

	LC26 at 100.00%	0.15	OK	Eq. H1-1b
				•
	LC27 at 100.00%	0.18	OK	Eq. H1-1b
	LC28 at 100.00%	0.19	OK	Eq. H1-1b
	LC29 at 100.00%	0.26	OK	Eq. H1-1b
		0.30	OK	Eq. H1-1b
	LC3 at 100.00%			•
	LC30 at 100.00%	0.26	OK	Eq. H1-1b
	LC31 at 100.00%	0.28	OK	Eq. H1-1b
	LC32 at 100.00%	0.29	OK	Eq. H1-1b
				•
	LC4 at 100.00%	0.43	OK	Eq. H1-1b
	LC5 at 100.00%	0.03	OK	Eq. H1-1b
	LC6 at 100.00%	0.11	OK	Eq. H1-1b
		0.26		Eq. H1-1b
	LC7 at 100.00%		OK	•
	LC8 at 100.00%	0.40	OK	Eq. H1-1b
	LC9 at 100.00%	0.26	OK	Eq. H1-1b
	W180 at 100.00%	0.10	OK	Eq. H1-1b
	W210 at 100.00%	0.18	OK	Eq. H1-1b
	Wi180 at 100.00%	0.04	OK	Eq. H1-1b
	Wi210 at 100.00%	0.07	OK	Eq. H1-1b
				•
	WL180 at 100.00%	0.01	OK	Eq. H1-1b
	WL210 at 100.00%	0.02	OK	Eq. H1-1b
33	LC1 at 0.00%	0.45	OK	Eg. H1-1b
33				Eq. H1-1b
	LC10 at 0.00%	0.29	OK	
	LC11 at 0.00%	0.21	OK	Eq. H1-1b
	LC12 at 0.00%	0.29	OK	Eq. H1-1b
	LC13 at 0.00%	0.14	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC14 at 0.00%	0.10		
	LC15 at 0.00%	0.14	OK	Eq. H1-1b
	LC16 at 0.00%	0.33	OK	Eq. H1-1b
	LC17 at 0.00%	0.29	OK	Eq. H1-1b
	LC18 at 0.00%	0.27	OK	Eq. H1-1b
				•
	LC19 at 0.00%	0.25	OK	Eq. H1-1b
	LC2 at 0.00%	0.14	OK	Eq. H1-1b
	LC20 at 0.00%	0.27	OK	Eq. H1-1b
	LC21 at 0.00%	0.18	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC22 at 0.00%	0.17		•
	LC23 at 0.00%	0.15	OK	Eq. H1-1b
	LC24 at 0.00%	0.17	OK	Eq. H1-1b
	LC25 at 0.00%	0.18	OK	Eq. H1-1b
	LC26 at 0.00%	0.17	OK	Eg. H1-1b
	LC27 at 0.00%	0.15	OK	Eq. H1-1b
	LC28 at 0.00%	0.17	OK	Eq. H1-1b
	LC29 at 0.00%	0.29	OK	Eq. H1-1b
	LC3 at 0.00%	0.10	OK	Eq. H1-1b
		0.27	OK	Eg. H1-1b
	LC30 at 0.00%			•
	LC31 at 0.00%	0.25	OK	Eq. H1-1b
	LC32 at 0.00%	0.27	OK	Eq. H1-1b
	LC4 at 0.00%	0.14	OK	Eq. H1-1b
		0.42	OK	Eq. H1-1b
	LC5 at 0.00%			•
	LC6 at 0.00%	0.11	OK	Eq. H1-1b
	LC7 at 0.00%	0.12	OK	Eq. H1-1b
	LC8 at 0.00%	0.10	OK	Eq. H1-1b
	LC9 at 0.00%	0.37	OK	Eq. H1-1b
	W180 at 0.00%	0.11	OK	Eq. H1-1b
	W210 at 0.00%	0.00	OK	Eq. H1-1b
	Wi180 at 0.00%	0.04	OK	Eq. H1-1b
	Wi210 at 0.00%	0.00	OK	Eq. H1-1b
	WL180 at 0.00%	0.01	OK	Eq. H1-1b
				Eq. H1-1b
	WL210 at 0.00%	0.00	OK	mannament

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Geometry data

GLOSSARY

Cb22, Cb33 Moment gradient coefficients

: Coefficients applied to bending term in interaction formula Cm22, Cm33 : Tapered member section depth at J end of member d0 : Rigid end offset distance measured from J node in axis X DJX Rigid end offset distance measured from J node in axis Y DJY Rigid end offset distance measured from J node in axis Z DJZ : Rigid end offset distance measured from K node in axis X DKX : Rigid end offset distance measured from K node in axis Y DKY DKZ : Rigid end offset distance measured from K node in axis Z Tapered member section depth at K end of member dL

Ig factor : Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members

K22 : Effective length factor about axis 2 K33 : Effective length factor about axis 3

L22 : Member length for calculation of axial capacity
L33 : Member length for calculation of axial capacity

LB pos : Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg : Lateral unbraced length of the compression flange in the negative side of local axis 2

RX : Rotation about X
RY : Rotation about Y
RZ : Rotation about Z

TO \$1 = Tension only member 0 = Normal member

TX : Translation in X
TY : Translation in Y
TZ : Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
2	0.00	0.00	-2.3333	0
3	-3.5359	0.00	-2.00	0
4	-7.00	0.00	0.00	0
5	-1.4793	0.00	-4.8955	0
6	-3.50	0.00	-6.0622	0
7	0.00	0.00	-8.1244	0
8	0.00	0.00	-12.1244	0
9	3.5359	0.00	-2.00	0
10	7.00	0.00	0.00	0
11	1.4793	0.00	-4.8955	0
12	3.50	0.00	-6.0622	0
14	6.1705	6.00	-1.8274	0
19	1.1705	6.00	-10.4876	0
41	1.1705	-2.00	-10.4876	0
44	6.1705	-2.00	-1.8274	0
53	4.5038	6.00	-4.7141	0
54	2.8372	6.00	-7.6009	0
63	2.8372	-2.00	-7.6009	0
64	4.5038	-2.00	-4.7141	0
69	-6.3333	4.00	0.00	0
71	-6.6667	4.00	-0.5774	0
73	6.3333	4.00	0.00	0

75	6.6667	4.00	-0.5774	0
77	0.3333	4.00	-11.547	0
79	-0.3333	4.00	-11.547	0
83	-1.6717	-3.00	-3.0763	0
84	1.6717	-3.00	-3.0763	0
86	0.00	-3.00	-5.9718	ő
87	-4.4019	0.00	-1.50	0
88	4.4019	0.00	-1.50	o
		0.00	-9.1244	0
89	0.00	0.00	0.00	0
91	0.00 5.9973		-1.7274	0
93		4.00		0
94	0.9973	4.00	-10.3876	
95	4.3306	4.00	-4.6141	0
96	2.664	4.00	-7.5009	0
97	6.1705	4.00	-1.8274	0
98	1.1705	4.00	-10.4876	0
99	4.5038	4.00	-4.7141	0
100	2.8372	4.00	-7.6009	0
101	5.9973	0.00	-1.7274	0
102	6.1705	0.00	-1.8274	0
103	4.3306	0.00	-4.6141	0
104	4.5038	0.00	-4.7141	0
105	2.664	0.00	-7.5009	0
106	2.8372	0.00	-7.6009	0
107	0.9973	0.00	-10.3876	0
108	1.1705	0.00	-10.4876	0
133	-6.1705	6.00	-1.8274	0
134	-6.1705	-2.00	-1.8274	0
135	-5.9973	4.00	-1.7274	0
136	-6.1705	4.00	-1.8274	0
137	-5.9973	0.00	-1.7274	0
138	-6.1705	0.00	-1.8274	0
139	-4.5038	6.00	-4.7141	0
140	-4.5038	-2.00	-4.7141	0
141	-4.3306	4.00	-4.6141	0
142	-4.5038	4.00	-4.7141	0
143	-4.3306	0.00	-4.6141	o o
144	-4.5038	0.00	-4.7141	0
		6.00	-7.6009	0
145	-2.8372		-7.6009	ő
146	-2.8372	-2.00 4.00	-7.5009 -7.5009	0
147	-2.664			0
148	-2.8372	4.00	-7.6009 -7.5000	-
149	-2.664	0.00	-7.5009	0
150	-2.8372	0.00	-7.6009	0
151	-1.1705	6.00	-10.4876	0
152	-1.1705	-2.00	-10.4876	0
153	-0.9973	4.00	-10.3876	0
154	-1.1705	4.00	-10.4876	0
155	-0.9973	0.00	-10.3876	0
156	-1.1705	0.00	-10.4876	0
157	5.00	6.00	0.20	0
158	5.00	-2.00	0.20	0
159	5.00	4.00	0.00	0
160	5.00	4.00	0.20	0
161	5.00	0.00	0.00	0
162	5.00	0.00	0.20	0
163	1.6667	6.00	0.20	0
164	1.6667	-2.00	0.20	0
165	1.6667	4.00	0.00	0
166	1.6667	4.00	0.20	0

180	-5.00	0.00	0.20	0
179	-5.00	0.00	0.00	0
178	-5.00	4.00	0.20	0
177	-5.00	4.00	0.00	0
176	-5.00	-2.00	0.20	0
175	-5.00	6.00	0.20	0
174	-1.6667	0.00	0.20	0
173	-1.6667	0.00	0.00	0
172	-1.6667	4.00	0.20	0
171	-1.6667	4.00	0.00	0
170	-1.6667	-2.00	0.20	0
169	-1.6667	6.00	0.20	0
168	1.6667	0.00	0.20	0
167	1.6667	0.00	0.00	0

Restraints

Node	тх	TY	TZ	RX	RY	RZ
2	1	1		**************************************	1	1
5	1	1	1	1	1	1
11	1	1	1	1	1	1
83	1	1	1	0	0	0
84	1	1	1	0	0	0
86	1	1	1	0	0	0

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	4	10		L 3X3X1_4	A36	0.00	0.00	0.00
2	10	8		L 3X3X1_4	A36	0.00	0.00	0.00
3	8	4		L 3X3X1_4	A36	0.00	0.00	0.00
4	3	9		L 3X3X1_4	A36	0.00	0.00	0.00
5	9	7		L 3X3X1_4	A36	0.00	0.00	0.00
6	7	3		L 3X3X1_4	A36	0.00	0.00	0.00
7	2	91		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
8	11	12		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
9	5	6		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
10	3	4		T2L 3X3X1_4	A36	0.00	0.00	0.00
11	9	10		T2L 3X3X1_4	A36	0.00	0.00	0.00
12	7	8		T2L 3X3X1_4	A36	0.00	0.00	0.00
13	14	44		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
14	53	64		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
16	19	41		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
25	69	73		PIPE 2x0.154	A36	0.00	0.00	0.00
26	79	71		PIPE 2x0.154	A36	0.00	0.00	0.00
27	75	77		PIPE 2x0.154	A36	0.00	0.00	0.00
28	69	71		L 3X3X1_4	A36	0.00	0.00	0.00
29	73	75		L 3X3X1_4	A36	0.00	0.00	0.00
30	77	79		L 3X3X1_4	A36	0.00	0.00	0.00
31	87	83		T2L 3X3X1_4	A36	0.00	0.00	0.00

32	84	88	T2L 3X3X1_4	A36	0.00	0.00	0.00
33	89	86	T2L 3X3X1_4	A36	0.00	0.00	0.00
54	133	134	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	139	140	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
15	54	63	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	145	146	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
63	151	152	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
66	157	158	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
69	163	164	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
72	169	170	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
75	175	176	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

Member	Rotation	Axes23	NX	NY	NZ
	[Deg]				
1	270.00	0	0.00	0.00	0.00
2	270.00	0	0.00	0.00	0.00
3	270.00	0	0.00	0.00	0.00
7	90.00	0	0.00	0.00	0.00
8	90.00	0	0.00	0.00	0.00
9	90.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	180.00	0	0.00	0.00	0.00
12	180.00	0	0.00	0.00	0.00
13	0.00	2	-0.50	0.00	-0.866
14	0.00	2	-0.50	0.00	-0.866
16	0.00	2	-0.50	0.00	-0.866
25	270.00	0	0.00	0.00	0.00
26	270.00	0	0.00	0.00	0.00
27	270.00	0	0.00	0.00	0.00
28	90.00	0	0.00	0.00	0.00
29	180.00	0	0.00	0.00	0.00
30	180.00	0	0.00	0.00	0.00
54	0.00	2	-0.50	0.00	0.866
57	0.00	2	-0.50	0.00	0.866
15	0.00	2	-0.50	0.00	-0.866
60	0.00	2	-0.50	0.00	0.866
63	0.00	2	-0.50	0.00	0.866



Mount Calculations (Modified 3C/4C/5C Configuration)

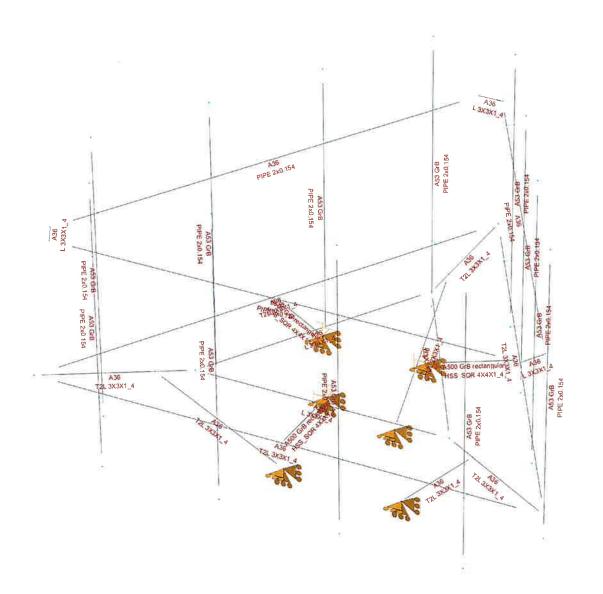


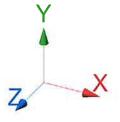
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Units system: English
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Current Date: 6/7/2018 12:19 PM
Units system: English
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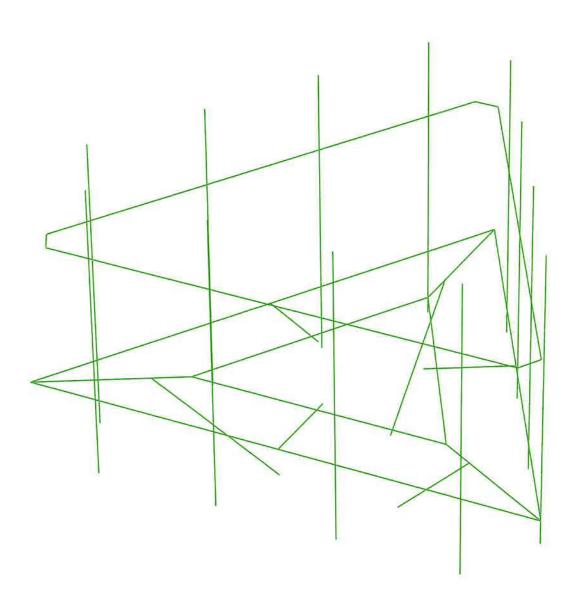


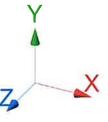


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Design status

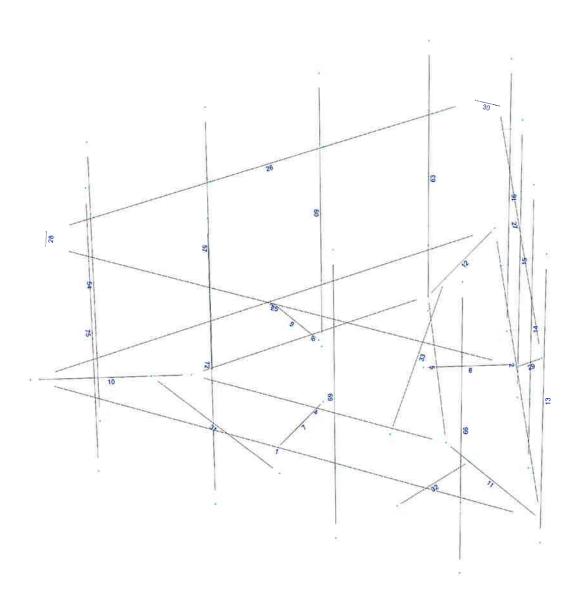


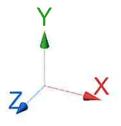






Bentley
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Current Date: 6/7/2018 12:20 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\AT&T\CT\CT1160\CT1160 (3C-4C-5C) (mod).etz\

Steel Code Check

Report: Summary - For all selected load conditions

Load conditions to be included in design :

W180=-W0

W210=-W30

Wi180=-Wi0

Wi210=-Wi30

WL180=-WL0

WL210=-WL30

LC1=1.2DL+1.6W0

LC2=1.2DL+1.6W30

LC3=1.2DL-1.6W0

LC4=1.2DL-1.6W30

LC5=0.9DL+1.6W0

LC6=0.9DL+1.6W30 LC7=0.9DL-1.6W0

LC8=0.9DL-1.6W30

LC9=1.2DL+Di+Wi0

LC10=1.2DL+Di+Wi30

LC11=1.2DL+Di-Wi0

LC12=1.2DL+Di-Wi30

LC13=1.2DL

LC14=0.9DL

LC15=1.2DL+1.6LL1

LC16=1.2DL+1.6LL2

LC17=1.2DL+WL0+LLa1

LC18=1.2DL+WL30+LLa1

LC19=1.2DL-WL0+LLa1

LC20=1.2DL-WL30+LLa1

LC21=1.2DL+WL0+LLa2

LC22=1.2DL+WL30+LLa2

LC23=1.2DL-WL0+LLa2

LC24=1.2DL-WL30+LLa2 LC25=1.2DL+WL0+LLa3

LC26=1.2DL+WL30+LLa3

LC27=1.2DL-WL0+LLa3

LC28=1.2DL-WL30+LLa3

LC29=1.2DL+WL0+LLa4

LC30=1.2DL+WL30+LLa4 LC31=1.2DL-WL0+LLa4

LC32=1.2DL-WL30+LLa4

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS SQR 4X4X1_4	7	LC1 at 0.00%	0.11	 ОК	Eq. H1-1b
	_		LC10 at 0.00%	0.28	OK	Eq. H1-1b
			LC11 at 0.00%	0.27	OK	Eq. H1-1b
			LC12 at 0.00%	0.27	OK	Eq. H1-1b
			LC13 at 0.00%	0.14	OK	Eq. H1-1b
			LC14 at 0.00%	0.11	OK	Eq. H1-1b
			LC15 at 0.00%	0.22	OK	Eq. H1-1b
			LC16 at 0.00%	0.15	OK	Eq. H1-1b
			LC17 at 0.00%	0.18	OK	Eq. H1-1b
			LC18 at 0.00%	0.19	OK	Eq. H1-1b
			LC19 at 0.00%	0.18	OK	Eq. H1-1b

	LC2 at 0.00%	0.24	OK	Eq. H1-1b
	LC20 at 0.00%	0.18	OK	Eq. H1-1b
	LC21 at 0.00%	0.23	OK	Eq. H1-1b
	LC22 at 0.00%	0.23	OK	Eq. H1-1b
	LC23 at 0.00%	0.23	OK	Eq. H1-1b
				Eq. H1-1b
	LC24 at 0.00%	0.23	OK	
	LC25 at 0.00%	0.23	OK	Eq. H1-1b
	LC26 at 0.00%	0.23	OK	Eq. H1-1b
	LC27 at 0.00%	0.23	OK	Eq. H1-1b
	LC28 at 0.00%	0.22	OK	Eq. H1-1b
	LC29 at 0.00%	0.18	OK	Eq. H1-1b
	LC3 at 0.00%	0.19	OK	Eq. H1-1b
	LC30 at 0.00%	0.19	OK	Eq. H1-1b
	LC31 at 0.00%	0.18	OK	Eq. H1-1b
		0.18	ok	Eg. H1-1b
	LC32 at 0.00%			Eq. H1-1b
	LC4 at 0.00%	0.23	OK	
	LC5 at 0.00%	0.07	OK	Eq. H1-1b
	LC6 at 0.00%	0.21	OK	Eq. H1-1b
	LC7 at 0.00%	0.15	OK	Eq. H1-1b
	LC8 at 0.00%	0.19	OK	Eq. H1-1b
	LC9 at 0.00%	0.25	OK	Eq. H1-1b
	W180 at 0.00%	0.03	OK	Eq. H1-1b
	W210 at 0.00%	0.08	OK	·
	Wi180 at 0.00%	0.01	OK	Eq. H1-1b
	Wi210 at 0.00%	0.03	OK	—
		0.00	OK	Eg. H1-1b
	WL180 at 0.00%			Eq. 111-16
	WL210 at 0.00%	0.01	OK 	***************************************
8	LC1 at 0.00%	0.24	ОК	Eq. H1-1b
	LC10 at 0.00%	0.24	OK	Eq. H1-1b
	LC11 at 0.00%	0.25	OK	Eq. H1-1b
	LC12 at 0.00%	0.26	ОК	Eq. H1-1b
	LC13 at 0.00%	0.13	OK	Eq. H1-1b
		0.10	OK	Eq. H1-1b
	LC14 at 0.00%			Eq. H1-1b
	LC15 at 0.00%	0.20	OK	
	LC16 at 0.00%	0.14	OK	Eq. H1-1b
	LC17 at 0.00%	0.17	OK	Eq. H1-1b
	LC18 at 0.00%	0.17	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC19 at 0.00%	0.17	OK	
		0.17 0.18	OK	Eq. H1-1b
	LC19 at 0.00%			Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00%	0.18 0.17	OK	
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00%	0.18 0.17 0.22	OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00%	0.18 0.17 0.22 0.22	OK OK OK	Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00%	0.18 0.17 0.22 0.22 0.22	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.22	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC25 at 0.00% LC26 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.22	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.22	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC27 at 0.00% LC28 at 0.00% LC28 at 0.00% LC29 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.22	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.22	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.22 0.17 0.21 0.17 0.17	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.27 0.21 0.17 0.17 0.17 0.17	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.17 0.25 0.21	OK	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.17 0.15	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.17 0.17 0.17 0.15 0.21 0.15	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC7 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.17 0.15 0.21 0.18 0.21	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC9 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.17 0.15 0.21 0.18 0.21 0.26	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC9 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.17 0.17 0.17 0.15 0.18 0.21 0.26 0.07	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC9 at 0.00% LC9 at 0.00% V180 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.15 0.21 0.18 0.21 0.26 0.07 0.07	OK O	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC29 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC9 at 0.00% LC9 at 0.00% UC9 at 0.00% UC9 at 0.00% W180 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.17 0.17 0.17 0.15 0.18 0.21 0.26 0.07 0.07	OK O O K O K K K K K K K K K K K K K K	Eq. H1-1b
	LC19 at 0.00% LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00% LC30 at 0.00% LC30 at 0.00% LC31 at 0.00% LC31 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC32 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC30 at 0.00% LC4 at 0.00% LC5 at 0.00% LC5 at 0.00% LC6 at 0.00% LC7 at 0.00% LC9 at 0.00% LC9 at 0.00% V180 at 0.00%	0.18 0.17 0.22 0.22 0.22 0.22 0.22 0.21 0.22 0.17 0.21 0.17 0.17 0.15 0.21 0.18 0.21 0.26 0.07 0.07	OK O	Eq. H1-1b

	WL180 at 0.00%	0.01	OK	Eq. H1-1b
	WL210 at 0.00%	0.01	OK	Eq. H1-1b
	VVLZ 10 Ut 0.0070	0.01		
9	LC1 at 0.00%	0.25	OK	Eq. H1-1b
3	LC10 at 0.00%	0.26	OK	Eq. H1-1b
	LC11 at 0.00%	0.26	OK	Eq. H1-1b
	LC12 at 0.00%	0.24	OK	Eq. H1-1b
	LC13 at 0.00%	0.13	OK	Eq. H1-1b
	LC14 at 0.00%	0.10	OK	Eq. H1-1b
	LC15 at 0.00%	0.21	OK	Eq. H1-1b
	LC16 at 0.00%	0.14	OK	Eq. H1-1b
	LC17 at 0.00%	0.17	OK	Eq. H1-1b
	LC18 at 0.00%	0.17	OK	Eq. H1-1b
	LC19 at 0.00%	0.17	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC2 at 0.00%	0.23		•
	LC20 at 0.00%	0.17	OK	Eq. H1-1b
	LC21 at 0.00%	0.22	OK	Eq. H1-1b
	LC22 at 0.00%	0.22	OK	Eq. H1-1b
	LC23 at 0.00%	0.22	OK	Eq. H1-1b
	LC24 at 0.00%	0.21	OK	Eq. H1-1b
	LC25 at 0.00%	0.22	OK	Eq. H1-1b
	LC26 at 0.00%	0.22	OK	Eq. H1-1b
	LC27 at 0.00%	0.22	OK	Eq. H1-1b
	LC28 at 0.00%	0.21	OK	Eq. H1-1b
	LC29 at 0.00%	0.17	OK	Eq. H1-1b
	LC3 at 0.00%	0.22	OK	Eq. H1-1b
	LC30 at 0.00%	0.17	OK	Eq. H1-1b
	LC31 at 0.00%	0.17	OK	Eq. H1-1b
	LC32 at 0.00%	0.17	OK	Eq. H1-1b
	LC4 at 0.00%	0.17	OK	Eq. H1-1b
	LC5 at 0.00%	0.22	OK	Eq. H1-1b
		0.20	OK	Eq. H1-1b
	LC6 at 0.00%			· · · · · · · · · · · · · · · · · · ·
	LC7 at 0.00%	0.18	OK	Eq. H1-1b
	LC8 at 0.00%	0.14	OK	Eq. H1-1b
	LC9 at 0.00%	0.26	OK	Eq. H1-1b
	W180 at 0.00%	0.08	OK	Eq. H1-1b
	W210 at 0.00%	0.06	OK	Eq. H1-1b
	Wi180 at 0.00%	0.03	OK	Eq. H1-1b
	Wi210 at 0.00%	0.02	ΟK	Eq. H1-1b
	WL180 at 0.00%	0.01	OK	Eq. H1-1b
	WL210 at 0.00%	0.01	OK	Eq. H1-1b
	VVL2 10 at 0.00 /6	0.01	TOTAL TOTAL	Eq. III-Ib
4	LC1 at 100.00%	0.08	OK	Eq. H2-1
4				Eq. H2-1
	LC10 at 0.00%	0.25	OK	
	LC11 at 0.00%	0.23	OK	Eq. H2-1
	LC12 at 100.00%	0.22	OK	Eq. H2-1
	LC13 at 0.00%	0.11	OK	Eq. H2-1
	LC14 at 0.00%	0.08	OK	Eq. H2-1
	LC15 at 0.00%	0.12	OK	Eq. H2-1
	LC16 at 0.00%	0.22	OK	Eq. H2-1
	LC17 at 0.00%	0.18	OK	Eq. H2-1
	LC18 at 0.00%	0.20	ОК	Eq. H2-1
		0.20	OK	Eq. H2-1
	LC19 at 0.00%			•
	LC2 at 0.00%	0.32	OK	Eq. H2-1
	LC20 at 100.00%	0.18	OK	Eq. H2-1
	LC21 at 0.00%	0.13	OK	Eq. H2-1
	LC22 at 0.00%	0.14	OK	Eq. H2-1
	LC23 at 0.00%	0.14	OK	Eq. H2-1
	LC24 at 100.00%	0.12	OK	Eq. H2-1
	LC25 at 0.00%	0.13	ok	Eq. H2-1
	LC26 at 0.00%	0.14	OK	Eq. H2-1
		0.14	ok	Eq. H2-1
	LC27 at 0.00%			- ·
	LC28 at 0.00%	0.12	OK	Eq. H2-1
	LC29 at 0.00%	0.19	OK	Eq. H2-1

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	LC3 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 100.00% LC5 at 50.00% LC6 at 0.00% LC7 at 0.00% LC8 at 100.00% LC9 at 0.00% W180 at 100.00% W210 at 0.00% W1210 at 0.00% WL180 at 100.00% WL210 at 0.00%	0.21 0.20 0.20 0.18 0.30 0.09 0.29 0.18 0.28 0.18 0.06 0.18 0.02 0.07 0.01 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1
5	LC1 at 100.00%	0.32	OK	Eq. H2-1
	LC10 at 100.00%	0.18	OK	Eq. H2-1
	LC11 at 0.00%	0.21	OK	Eq. H2-1
	LC12 at 0.00%	0.22	OK	Eq. H2-1
	LC13 at 0.00%	0.09	OK	Eq. H2-1
	LC14 at 0.00%	0.07	OK	Eq. H2-1
	LC15 at 0.00%	0.10	OK	Eq. H2-1
	LC16 at 0.00%	0.20	OK	Sec. F1
	LC17 at 100.00%	0.18	OK	Eq. H2-1
	LC18 at 100.00%	0.17	OK	Eq. H2-1
	LC19 at 0.00%	0.17	OK	Eq. H2-1
	LC2 at 0.00%	0.18	OK	Eq. H2-1
	LC20 at 0.00%	0.18	OK	Eq. H2-1
	LC21 at 100.00%	0.12	OK	Eq. H2-1
	LC22 at 100.00%	0.11	OK	Eq. H2-1 Eq. H2-1
	LC23 at 0.00%	0.12	OK	Eq. H2-1
	LC24 at 0.00%	0.12	OK OK	Eq. H2-1
	LC25 at 100.00%	0.12	OK	Eq. H2-1
	LC26 at 100.00% LC27 at 0.00%	0.11 0.12	OK OK	Eq. H2-1
	LC28 at 0.00%	0.12	OK	Eq. H2-1
	LC29 at 100.00%	0.12	OK	Eq. H2-1
	LC3 at 100.00%	0.22	OK	Eq. H2-1
	LC30 at 100.00%	0.17	OK	Eq. H2-1
	LC31 at 0.00%	0.18	OK	Eq. H2-1
	LC32 at 0.00%	0.18	OK	Eq. H2-1
	LC4 at 0.00%	0.29	OK	Eq. H2-1
	LC5 at 100.00%	0.29	OK	Eq. H2-1
	LC6 at 0.00%	0.21	ОК	Eq. H2-1
	LC7 at 100.00%	0.25	OK	Eq. H2-1
	LC8 at 0.00%	0.27	OK	Eq. H2-1
	LC9 at 100.00%	0.23	OK	Eq. H2-1
	W180 at 100.00%	0.20	OK	Eq. H2-1
	W210 at 0.00%	0.13	OK	Eq. H2-1
	Wi180 at 100.00%	0.07	OK	Eq. H2-1
	Wi210 at 0.00%	0.05	OK	Eq. H2-1
	WL180 at 100.00%	0.02	OK	Eq. H2-1
	WL210 at 0.00%	0.01	OK	Eq. H2-1
				m 15 1
6	LC1 at 0.00%	0.32	OK	Eq. H2-1
	LC10 at 100.00%	0.25	OK	Eq. H2-1
	LC11 at 100.00%	0.23	OK	Eq. H2-1
	LC12 at 0.00%	0.18	OK	Eq. H2-1
	LC13 at 100.00%	0.11	OK	Eq. H2-1
	LC14 at 100.00%	80.0	OK	Eq. H2-1
	LC15 at 100.00%	0.12	OK	Eq. H2-1
	LC16 at 100.00%	0.22	OK	Sec. F1

LC17 at 100.00%	0.18	OK	Sec. F1
LC18 at 100.00%	0.20	OK	Eq. H2-1
LC19 at 100.00%	0.20	OK	Eq. H2-1
LC2 at 100.00%	0.32	OK	Eq. H2-1
LC20 at 100.00%	0.18	OK	Sec. F1
LC21 at 100.00%	0.13	OK	Eq. H2-1
LC22 at 100.00%	0.14	OK	Eq. H2-1
LC23 at 100.00%	0.14	OK	Eq. H2-1
LC24 at 100.00%	0.12	OK	Eq. H2-1
LC25 at 100.00%	0.12	OK	Eq. H2-1
LC26 at 100.00%	0.14	OK	Eq. H2-1
LC27 at 100.00%	0.14	OK	Eq. H2-1
LC28 at 100.00%	0.12	OK	Eq. H2-1
LC29 at 100.00%	0.18	OK	Sec. F1
LC3 at 100.00%	0.23	OK	Eq. H2-1
LC30 at 100.00%	0.20	OK OK	Eq. H2-1
LC31 at 100.00%	0.20	OK OK	Eq. H2-1
LC32 at 100.00%	0.18	OK OK	Sec. F1
LC4 at 100.00%	0.16	OK	Eq. H2-1 Eq. H2-1
LC5 at 0.00%	0.29	OK	Eq. H2-1
LC6 at 100.00%	0.29 0.24	OK OK	Eq. H2-1
LC7 at 0.00%		OK	Eq. H2-1
LC8 at 100.00%	0.20 0.23	OK	Eq. H2-1
LC9 at 0.00%	0.23	OK	Eq. H2-1
W180 at 0.00% W210 at 100.00%	0.20	OK	Eq. H2-1
Wi180 at 0.00%	0.18	OK	Eq. H2-1
Wi210 at 100.00%	0.07	OK	Eq. H2-1
WL180 at 0.00%	0.02	OK	Eq. H2-1
WL210 at 100.00%	0.02	OK	Eq. H2-1
LC1 at 100.00%	0.68	ок	Eq. H3-8
LC10 at 0.00%	0.14		E~ U2 4
		OK	Eq. H2-1
LC11 at 100.00%	0.15	OK	Eq. H2-1
LC11 at 100.00% LC12 at 0.00%	0.15 0.05	OK OK	Eq. H2-1 Sec. F1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00%	0.15 0.05 0.04	OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00%	0.15 0.05 0.04 0.03	OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00%	0.15 0.05 0.04 0.03 0.04	OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05	OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05	OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05	OK OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07	OK OK OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00% LC19 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07	OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37	OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05	OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08	OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08	OK OK OK OK OK OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 100.00% LC22 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC25 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 100.00% LC23 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.09 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H3-8 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.09 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 100.00% LC25 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.09 0.08	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05 0.09 0.08	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05 0.09 0.08 0.08	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.09 0.08 0.08 0.05 0.09	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC21 at 0.00% LC22 at 0.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05 0.09 0.08 0.05 0.09 0.01 0.05	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H2-1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 0.00% LC18 at 0.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC21 at 0.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC29 at 100.00% LC30 at 100.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.05 0.09 0.08 0.05 0.01 0.05	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC22 at 0.00% LC21 at 0.00% LC22 at 100.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.08 0.08 0.05 0.11 0.63 0.09 0.07	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.08 0.09 0.08 0.05 0.11 0.63 0.09 0.07 0.07 0.07 0.08	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC22 at 0.00% LC22 at 100.00% LC22 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 100.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.08 0.08 0.05 0.11 0.63 0.09 0.07 0.07 0.07 0.08	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC22 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 100.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC6 at 0.00% LC7 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.08 0.05 0.11 0.63 0.09 0.07 0.06 0.31 0.67 0.36 0.63 0.32 0.21	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Eq. H2-1 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8
LC11 at 100.00% LC12 at 0.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC18 at 0.00% LC19 at 100.00% LC2 at 0.00% LC22 at 0.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC26 at 0.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 100.00% LC4 at 0.00% LC5 at 100.00% LC5 at 100.00% LC5 at 100.00% LC6 at 0.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00%	0.15 0.05 0.04 0.03 0.04 0.05 0.07 0.07 0.37 0.04 0.05 0.08 0.08 0.08 0.05 0.11 0.63 0.09 0.07 0.07 0.07 0.06 0.31 0.67 0.36 0.63 0.32	OK O	Eq. H2-1 Sec. F1 Eq. H2-1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1

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	W210 at 0.00% Wi180 at 0.00% Wi210 at 0.00% WL180 at 0.00% WL210 at 0.00%	0.21 0.15 0.08 0.04 0.02	OK OK OK OK OK	Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1
29	LC1 at 100.00% LC10 at 0.00% LC11 at 100.00% LC12 at 0.00% LC13 at 12.50% LC14 at 12.50% LC15 at 12.50% LC16 at 0.00% LC17 at 0.00% LC18 at 100.00% LC19 at 100.00%	0.25 0.07 0.11 0.17 0.03 0.03 0.03 0.04 0.05 0.04	OK OK OK OK OK OK OK OK	Eq. H3-8 Eq. H3-8 Eq. H2-1
	LC2 at 0.00% LC20 at 0.00% LC21 at 0.00% LC22 at 100.00% LC23 at 100.00% LC24 at 0.00% LC25 at 0.00% LC26 at 0.00% LC27 at 100.00% LC28 at 0.00% LC29 at 0.00%	0.40 0.08 0.06 0.04 0.07 0.08 0.06 0.04 0.07 0.08	OK OK OK OK OK OK OK OK	Sec. F1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H2-1 Eq. H3-8 Eq. H2-1 Eq. H2-1
	LC3 at 0.00% LC30 at 0.00% LC31 at 0.00% LC32 at 0.00% LC4 at 0.00% LC5 at 100.00% LC6 at 0.00% LC7 at 0.00% LC8 at 0.00% UC8 at 0.00% UC9 at 0.00%	0.28 0.06 0.06 0.08 0.47 0.26 0.41 0.28 0.46 0.07	OK OK OK OK OK OK OK OK OK	Eq. H3-8 Eq. H3-8 Eq. H3-8 Eq. H2-1 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8
	W210 at 0.00% Wi180 at 0.00% Wi210 at 0.00% WL180 at 0.00% WL210 at 0.00%	0.27 0.07 0.10 0.01 0.03	OK OK OK OK	Sec. F1 Eq. H3-8 Sec. F1 Eq. H3-8 Sec. F1
30	LC1 at 0.00% LC10 at 0.00% LC11 at 100.00% LC12 at 0.00% LC13 at 0.00% LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00% LC18 at 0.00% LC18 at 0.00%	0.39 0.11 0.06 0.11 0.03 0.02 0.03 0.04 0.07 0.06 0.04	OK OK OK OK OK OK OK OK OK	Sec. F1 Eq. H2-1 Sec. F1 Eq. H3-8 Eq. H2-1
	LC19 at 100.00% LC20 at 100.00% LC21 at 0.00% LC22 at 0.00% LC23 at 100.00% LC24 at 100.00% LC25 at 0.00% LC26 at 0.00%	0.34 0.06 0.07 0.07 0.04 0.06 0.07	OK OK OK OK OK OK OK	Eq. H3-8 Eq. H2-1

		LC27 at 100.00%	0.04	OK	Eq. H2-1
		LC28 at 100.00%	0.06	ОК	Eq. H2-1
					Eq. H2-1
		LC29 at 0.00%	0.07	OK	•
		LC3 at 0.00%	0.34	OK	Sec. F1
		LC30 at 0.00%	0.07	OK	Eq. H2-1
		LC31 at 100.00%	0.05	OK	Eq. H2-1
		LC32 at 0.00%	0.06	OK	Eq. H3-8
		LC4 at 0.00%	0.36	OK	Eq. H3-8
		LC5 at 0.00%	0.39	OK	Sec. F1
		LC6 at 100.00%	0.34	OK	Eq. H3-8
		LC7 at 0.00%	0.35	OK	Sec. F1
		LC8 at 0.00%	0.36	OK	Eq. H3-8
		LC9 at 0.00%	0.15	OK	Sec. F1
		W180 at 0.00%	0.23	OK	Sec. F1
				OK	
		W210 at 0.00%	0.22		Eq. H3-8
		Wi180 at 0.00%	0.09	OK	Sec. F1
		Wi210 at 0.00%	0.08	OK	Eq. H3-8
		WL180 at 0.00%	0.02	OK	Sec. F1
		WL210 at 0.00%	0.02	OK	Eq. H3-8
DIDE 240 454	13	LC1 at 72.92%	0.43	OK	Eg. H1-1b
PIPE 2x0.154	13				•
		LC10 at 72.92%	0.14	OK	Eq. H1-1b
		LC11 at 72.92%	0.16	OK	Eq. H1-1b
		LC12 at 72.92%	0.12	OK	Eq. H1-1b
		LC13 at 72.92%	0.05	OK	Eq. H1-1b
		LC14 at 72.92%	0.04	ок	Eq. H1-1b
		LC15 at 72.92%	0.04	OK	Eq. H1-1b
				OK	Eq. H1-1b
		LC16 at 72.92%	0.09		
		LC17 at 72.92%	0.09	OK	Eq. H1-1b
		LC18 at 72.92%	0.08	OK	Eq. H1-1b
		LC19 at 72.92%	0.06	OK	Eq. H1-1b
		LC2 at 72.92%	0.25	OK	Eq. H1-1b
		LC20 at 72.92%	0.07	ОК	Eq. H1-1b
		LC21 at 72.92%	0.07	OK	Eq. H1-1b
		LC22 at 72.92%	0.06	OK	Eq. H1-1b
		LC23 at 72.92%	0.06	OK	Eq. H1-1b
		LC24 at 72.92%	0.05	OK	Eq. H1-1b
		LC25 at 72.92%	0.06	OK	Eq. H1-1b
		LC26 at 72.92%	0.05	OK	Eq. H1-1b
		LC27 at 72.92%	0.07	OK	Eq. H1-1b
		LC28 at 72.92%	0.07	OK	Eq. H1-1b
		LC29 at 72.92%	0.17	OK OK	Eq. H1-1b
		LC3 at 72.92%	0.44	OK	Eq. H1-1b
		LC30 at 72.92%	0.16	OK	Eq. H1-1b
		LC31 at 72.92%	0.13	OK	Eq. H1-1b
		LC32 at 72.92%	0.14	OK	Eq. H1-1b
		LC4 at 72.92%	0.29	ОК	Eq. H1-1b
		LC5 at 72.92%	0.42	OK	Eq. H1-1b
		LC6 at 72.92%	0.24	OK	Eq. H1-1b
		LC7 at 72.92%	0.43	OK	Eq. H1-1b
		LC8 at 72.92%	0.28	OK	Eq. H1-1b
		LC9 at 72.92%	0.19	OK	Eq. H1-1b
		W180 at 72.92%	0.26	OK	Eq. H1-1b
		W210 at 72.92%	0.15	OK	Eq. H1-1b
		Wi180 at 72.92%	0.10	ОК	Eq. H1-1b
			0.06	OK	Eq. H1-1b
		Wi210 at 72.92%			
		WL180 at 72.92%	0.02	OK	Eq. H1-1b
		WL210 at 72.92%	0.01	OK	Eq. H1-1b
		S инера клива пед сопсов съсъти изв ес			
	14	LC1 at 72.92%	0.54	OK	Eq. H1-1b
		LC10 at 72.92%	0.30	OK	Eq. H1-1b
		LC11 at 72.92%	0.20	OK	Eq. H1-1b
		LC12 at 72.92%	0.09	OK	Eq. H1-1b
		LC13 at 72.92%	0.10	OK	Eq. H1-1b

	1.044 -1.70.000/	0.00	OK	F~ U4.4b
	LC14 at 72.92%	0.08	OK	Eq. H1-1b
	LC15 at 72.92%	0.10	OK	Eq. H1-1b
	LC16 at 72.92%	0.13	OK	Eq. H1-1b
	LC17 at 72.92%	0.12	OK	Eq. H1-1b
	LC18 at 72.92%	0.13	OK	Eq. H1-1b
	LC19 at 72.92%	0.08	OK	Eq. H1-1b
	LC2 at 72.92%	0.56	OK	Eq. H1-1b
	LC20 at 72.92%	0.07	OK	Eq. H1-1b
	LC21 at 72.92%	0.12	OK	Eq. H1-1b
				· ·
	LC22 at 72.92%	0.12	OK	Eq. H1-1b
	LC23 at 72.92%	0.09	OK	Eq. H1-1b
	LC24 at 72.92%	0.07	OK	Eq. H1-1b
	LC25 at 72.92%	0.23	OK	Eq. H1-1b
	LC26 at 72.92%	0.23	OK	Eq. H1-1b
	LC27 at 72.92%	0.19	OK	Eq. H1-1b
	LC28 at 72.92%	0.18	OK	Eq. H1-1b
	LC29 at 72.92%	0.17	OK	Eq. H1-1b
	LC3 at 72.92%	0.58	ОК	Eq. H1-1b
	LC30 at 72.92%	0.18	OK	Eq. H1-1b
	LC31 at 72.92%	0.13	OK	Eq. H1-1b
				Eq. H1-1b
	LC32 at 72.92%	0.12	OK	·
	LC4 at 72.92%	0.38	OK	Eq. H1-1b
	LC5 at 72.92%	0.54	OK	Eq. H1-1b
	LC6 at 72.92%	0.54	OK	Eq. H1-1b
	LC7 at 72.92%	0.57	OK	Eq. H1-1b
	LC8 at 72.92%	0.40	OK	Eq. H1-1b
	LC9 at 72.92%	0.28	OK	Eq. H1-1b
	W180 at 72.92%	0.34	OK	Eq. H1-1b
	W210 at 72.92%	0.29	OK	Eq. H1-1b
	Wi180 at 72.92%	0.13	OK	Eq. H1-1b
	Wi210 at 72.92%	0.11	OK	Eq. H1-1b
		0.03	OK	Eq. H1-1b
	WL180 at 72.92%			_ ·
	WL210 at 72.92%	0.03	OK	Eq. H1-1b
40	LO4 - 4 70 000/	0.40	OK	
16	LC1 at 72.92%	0.40	OK	Eq. H1-1b
16	LC10 at 72.92%	0.06	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92%	0.06 0.16	OK OK	Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92%	0.06	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92%	0.06 0.16	OK OK	Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92%	0.06 0.16 0.14	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92%	0.06 0.16 0.14 0.04	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92%	0.06 0.16 0.14 0.04 0.03	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC18 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC19 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13 0.16 0.30	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13 0.16 0.30 0.16	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13 0.16 0.30 0.16	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.13 0.16 0.30 0.16 0.04	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04	OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04	OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.04	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.04 0.03 0.04 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.04 0.03 0.06 0.05 0.39	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.04 0.03 0.06 0.05 0.39 0.05	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.06 0.05 0.39 0.05 0.09	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC27 at 72.92% LC29 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.04 0.03 0.05 0.06 0.05 0.39 0.05 0.09 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC30 at 72.92% LC31 at 72.92% LC32 at 72.92% LC34 at 25.00%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.06 0.05 0.39 0.05 0.09 0.08 0.35	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC30 at 72.92% LC31 at 72.92% LC32 at 72.92% LC35 at 72.92% LC35 at 72.92% LC36 at 72.92% LC37 at 72.92% LC38 at 72.92% LC39 at 72.92% LC39 at 72.92% LC30 at 72.92% LC31 at 72.92% LC32 at 72.92%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.06 0.05 0.39 0.05 0.09 0.08 0.35 0.40	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
16	LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC30 at 72.92% LC31 at 72.92% LC32 at 72.92% LC34 at 25.00%	0.06 0.16 0.14 0.04 0.03 0.04 0.08 0.13 0.16 0.30 0.16 0.04 0.03 0.04 0.03 0.06 0.05 0.39 0.05 0.09 0.08 0.35	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

	LC8 at 25.00%	0.34	OK	Eq. H1-1b
	LC9 at 72.92%	0.09	OK	Eq. H1-1b
	W180 at 72.92%	0.25	OK	Eq. H1-1b
	W210 at 25.00%	0.20	OK	Eq. H1-1b
	Wi180 at 72.92%	0.10	OK	Eq. H1-1b
	Wi210 at 25.00%	0.07	OK	Eq. H1-1b
	WL180 at 72.92%	0.02	OK	Eq. H1-1b
	WL210 at 25.00%	0.02	OK	Eq. H1-1b
25	LC1 at 10.00%	0.50	OK	Eq. H1-1b
	LC10 at 63.75%	0.16	OK	Eg. H1-1b
	LC11 at 36.25%	0.18	OK	Eq. H1-1b
	LC12 at 11.25%	0.19	ок	Eq. H1-1b
	LC13 at 63.75%	0.05	OK	Eq. H1-1b
	LC14 at 63.75%	0.04	OK	Eq. H1-1b
	LC15 at 37.50%	0.04	OK	Eq. H1-1b
	LC16 at 63.75%	0.10	OK	Eq. H1-1b
	LC17 at 63.75%	0.09	OK	Eq. H1-1b
	LC18 at 63.75%	0.11	OK	Eq. H1-1b
	LC19 at 63.75%	0.10	OK	Eq. H1-1b
	LC2 at 88.75%	0.61	OK	Eq. H1-1b
	LC20 at 36.25%	0.08	OK	Eq. H1-1b
	LC21 at 11.25%	0.05	OK	Eq. H1-1b
	LC22 at 0.00%	0.07	OK	Eq. H1-1b
	LC23 at 36.25%	0.08	OK	Eq. H1-1b
	LC24 at 100.00%	0.08	OK	Eq. H1-1b
	LC25 at 37.50%	0.09	OK	Eq. H1-1b
	LC26 at 37.50%	0.09	OK	Eq. H1-1b
	LC27 at 37.50%	0.13	OK	Eq. H1-1b
	LC28 at 37.50%	0.13	OK	Eq. H1-1b
	LC29 at 11.25%	0.12	OK	Eq. H1-1b
	LC3 at 36.25%	0.48	OK OK	Eq. H1-1b Eq. H1-1b
	LC30 at 63.75%	0.09	OK OK	Eq. H1-1b
	LC31 at 11.25% LC32 at 11.25%	0.11 0.15	OK	Eq. H1-1b
	LC4 at 88.75%	0.13	OK	Eq. H1-1b
	LC5 at 10.00%	0.49	OK	Eg. H1-1b
	LC6 at 88.75%	0.61	OK	Eg. H1-1b
	LC7 at 10.00%	0.48	OK	Eq. H1-1b
	LC8 at 88.75%	0.62	OK	Eg. H1-1b
	LC9 at 10.00%	0.15	OK	Eq. H1-1b
	W180 at 10.00%	0.31	OK	Eq. H1-1b
	W210 at 88.75%	0.38	OK	Eq. H1-1b
7.0	Wi180 at 10.00%	0.12	OK	Eq. H1-1b
	Wi210 at 88.75%	0.14	OK	Eq. H1-1b
	WL180 at 10.00%	0.03	OK	Eq. H1-1b
	WL210 at 88.75%	0.04	OK	Eq. H1-1b
26	L C1 at 00 000/	0.56	OK	Ea U1_1h
26	LC1 at 90.00%	0.56	OK	Eq. H1-1b Eq. H1-1b
	LC10 at 36.25%	0.21 0.17	OK OK	Eq. H1-1b
	LC11 at 62.50% LC12 at 10.00%	0.17	OK OK	Eq. H1-1b
	LC13 at 62.50%	0.05	OK	Eq. H1-1b
	LC14 at 62.50%	0.04	OK	Eq. H1-1b
	LC15 at 90.00%	0.05	OK	Eq. H1-1b
	LC16 at 63.75%	0.09	OK	Eq. H1-1b
	LC17 at 63.75%	0.11	OK	Eq. H1-1b
	LC18 at 36.25%	0.10	OK	Eq. H1-1b
	LC19 at 63.75%	0.07	OK	Eq. H1-1b
	LC2 at 36.25%	0.63	OK	Eq. H1-1b
	LC20 at 63.75%	0.09	ОК	Eq. H1-1b
	LC21 at 0.00%	0.07	OK	Eq. H1-1b
	LC22 at 36.25%	0.09	OK	Eq. H1-1b
	LC23 at 100.00%	0.07	ОК	Eq. H1-1b

	LC24 at 10.00% LC25 at 37.50% LC26 at 37.50% LC27 at 37.50% LC28 at 37.50% LC29 at 63.75% LC3 at 11.25% LC30 at 11.25% LC31 at 11.25% LC32 at 11.25% LC4 at 10.00% LC5 at 90.00% LC6 at 10.00% LC7 at 11.25% LC8 at 10.00% LC9 at 63.75% W180 at 90.00% W210 at 10.00% W1180 at 11.25% W180 at 90.00% W1180 at 90.00% WL180 at 90.00% WL180 at 90.00%	0.05 0.10 0.14 0.11 0.07 0.09 0.53 0.12 0.13 0.09 0.63 0.56 0.63 0.53 0.62 0.17 0.32 0.38 0.12 0.14 0.03 0.04	OK O	Eq. H1-1b
27	LC1 at 88.75% LC10 at 62.50% LC11 at 10.00% LC12 at 63.75% LC13 at 63.75% LC14 at 63.75% LC15 at 37.50% LC16 at 63.75% LC16 at 63.75% LC19 at 63.75% LC19 at 63.75% LC19 at 63.75% LC2 at 90.00% LC20 at 63.75% LC21 at 36.25% LC22 at 100.00% LC23 at 0.00% LC24 at 37.50% LC25 at 37.50% LC26 at 37.50% LC26 at 37.50% LC29 at 11.25% LC3 at 88.75% LC30 at 11.25% LC3 at 88.75% LC30 at 11.25% LC31 at 63.75% LC32 at 36.25% LC4 at 90.00% LC5 at 88.75% LC30 at 11.25% LC3 at 88.75% LC30 at 17.50% LC30 at 17.50% LC30 at 37.50% LC30 at 88.75% LC30 at 90.00% LC5 at 88.75% LC4 at 90.00% LC5 at 88.75% LC6 at 90.00% LC7 at 88.75% LC8 at 90.00% LC9 at 37.50% W180 at 88.75% W210 at 90.00% W1180 at 88.75% W1210 at 90.00% WL180 at 88.75% WL210 at 36.25%	0.58 0.15 0.16 0.05 0.03 0.04 0.09 0.09 0.07 0.10 0.57 0.11 0.08 0.06 0.07 0.13 0.09 0.08 0.12 0.12 0.55 0.12 0.08 0.09 0.62 0.58 0.57 0.55 0.61 0.19 0.35 0.38 0.14 0.14 0.03 0.03	OK OK	Eq. H1-1b
54	LC1 at 25.00% LC10 at 70.83%	0.43 0.07	ОК ОК	Eq. H1-1b Eq. H1-1b

	LC11 at 72.92%	0.09	OK	Eq. H1-1b
	LC12 at 72.92%	0.12	OK	Eq. H1-1b
	LC13 at 72.92%	0.04	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC14 at 72.92%	0.03		·
	LC15 at 72.92%	0.04	OK	Eq. H1-1b
	LC16 at 72.92%	0.09	OK	Eq. H1-1b
	LC17 at 72.92%	0.17	OK	Eq. H1-1b
	LC18 at 72.92%	0.14	OK	Eg. H1-1b
	LC19 at 72.92%	0.13	OK	Eq. H1-1b
	LC2 at 72.92%	0.27	OK	Eq. H1-1b
	LC20 at 72.92%	0.16	OK	Eq. H1-1b
	LC21 at 72.92%	0.05	OK	Eg. H1-1b
	LC22 at 72.92%	0.04	OK	Eq. H1-1b
		0.04	OK	Eq. H1-1b
	LC23 at 72.92%			100
	LC24 at 72.92%	0.04	OK	Eq. H1-1b
	LC25 at 72.92%	0.06	OK	Eq. H1-1b
	LC26 at 72.92%	0.04	OK	Eq. H1-1b
	LC27 at 72.92%	0.03	OK	Eq. H1-1b
	LC28 at 72.92%	0.05	OK	Eg. H1-1b
			OK	Eq. H1-1b
	LC29 at 72.92%	0.09		•
	LC3 at 25.00%	0.38	OK	Eq. H1-1b
	LC30 at 72.92%	0.06	OK	Eq. H1-1b
	LC31 at 72.92%	0.05	OK	Eq. H1-1b
	LC32 at 72.92%	0.08	OK	Eq. H1-1b
	LC4 at 72.92%	0.26	OK	Eq. H1-1b
	LC5 at 25.00%	0.42	OK	Eq. H1-1b
	LC6 at 72.92%	0.27	OK	Eq. H1-1b
	LC7 at 25.00%	0.39	OK	Eq. H1-1b
	LC8 at 72.92%	0.26	OK	Eq. H1-1b
	LC9 at 72.92%	0.18	OK	Eg. H1-1b
	W180 at 25.00%	0.26	OK	Eq. H1-1b
		0.16	OK	Eq. H1-1b
	W210 at 72.92%			<u>'</u>
		0.10	OK	Eq. H1-1b
	Wi180 at 25.00%	00		
	Wi210 at 72.92%	0.06	OK	Eq. H1-1b
	Wi210 at 72.92% WL180 at 25.00%	0.06 0.02	OK	Eq. H1-1b
	Wi210 at 72.92%	0.06	OK OK	Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02	OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC14 at 25.00% LC15 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC14 at 25.00% LC16 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC16 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC18 at 72.92% LC19 at 72.92% LC19 at 72.92%	0.06 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC10 at 72.92% LC20 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC19 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC10 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC19 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92%	0.06 0.02 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC10 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC19 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92%	0.06 0.02 0.02 0.02 0.48 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC10 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC15 at 72.92% LC16 at 72.92% LC16 at 72.92% LC19 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC11 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06	OK O	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC11 at 25.00% LC11 at 25.00% LC11 at 72.92% LC12 at 72.92% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00%	0.06 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC11 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC26 at 25.00% LC27 at 25.00% LC27 at 25.00% LC28 at 72.92%	0.06 0.02 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 72.92% LC29 at 72.92%	0.06 0.02 0.02 0.02 0.04 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC11 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92% LC2 at 25.00% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 72.92% LC29 at 72.92% LC3 at 25.00% LC3 at 25.00%	0.06 0.02 0.02 0.02 0.04 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.03 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 72.92% LC29 at 72.92%	0.06 0.02 0.02 0.02 0.04 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC11 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC17 at 72.92% LC18 at 72.92% LC2 at 25.00% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 72.92% LC29 at 72.92% LC3 at 25.00% LC3 at 25.00%	0.06 0.02 0.02 0.02 0.04 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.03 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC29 at 72.92% LC30 at 25.00% LC31 at 72.92%	0.06 0.02 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06 0.03 0.03 0.03 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC28 at 72.92% LC30 at 25.00% LC30 at 25.00% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92% LC30 at 25.00% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92%	0.06 0.02 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06 0.03 0.03 0.03 0.03 0.03	OK OK OK <	Eq. H1-1b
57	Wi210 at 72.92% WL180 at 25.00% WL210 at 72.92% LC1 at 25.00% LC10 at 25.00% LC11 at 72.92% LC12 at 72.92% LC13 at 25.00% LC14 at 25.00% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 25.00% LC27 at 25.00% LC29 at 72.92% LC29 at 72.92% LC30 at 25.00% LC31 at 72.92%	0.06 0.02 0.02 0.02 0.048 0.11 0.13 0.10 0.02 0.01 0.02 0.04 0.08 0.04 0.05 0.37 0.08 0.14 0.10 0.12 0.14 0.03 0.06 0.06 0.03 0.03 0.03 0.03 0.03	OK OK OK <	Eq. H1-1b

	1.05 1.05 000/	0.40	OV	Ea U1 1b
	LC5 at 25.00%	0.48	OK	Eq. H1-1b
	LC6 at 25.00%	0.36	OK	Eq. H1-1b
	LC7 at 25.00%	0.48	OK	Eq. H1-1b
	LC8 at 25.00%	0.34	OK	Eq. H1-1b
	LC9 at 25.00%	0.12	OK	Eq. H1-1b Eq. H1-1b
	W180 at 25.00%	0.30	OK	•
	W210 at 25.00%	0.22	OK	Eq. H1-1b Eq. H1-1b
	Wi180 at 25.00%	0.11	OK OK	Eq. H1-1b
	Wi210 at 25.00%	0.08	OK OK	Eq. H1-1b
	WL180 at 25.00% WL210 at 25.00%	0.03 0.02	OK	Eq. H1-1b
	VVL2 10 at 25.0070			
15	LC1 at 25.00%	0.47	ОК	Eq. H1-1b
	LC10 at 72.92%	0.10	ОК	Eq. H1-1b
	LC11 at 72.92%	0.14	OK	Eq. H1-1b
	LC12 at 25.00%	0.09	OK	Eq. H1-1b
	LC13 at 72.92%	0.02	OK	Eq. H1-1b
	LC14 at 72.92%	0.01	OK	Eq. H1-1b
	LC15 at 72.92%	0.02	OK	Eq. H1-1b
	LC16 at 72.92%	0.04	OK	Eq. H1-1b
	LC17 at 72.92%	0.04	OK	Eq. H1-1b
	LC18 at 72.92%	0.05	OK	Eq. H1-1b
	LC19 at 72.92%	0.09	OK	Eq. H1-1b
	LC2 at 25.00%	0.37	OK	Eq. H1-1b
	LC20 at 72.92%	0.08	OK	Eq. H1-1b
	LC21 at 72.92%	0.11	OK	Eq. H1-1b
	LC22 at 72.92%	0.11	OK	Eq. H1-1b
	LC23 at 72.92%	0.15	OK	Eq. H1-1b
	LC24 at 72.92%	0.14	OK	Eq. H1-1b
	LC25 at 25.00%	0.07	OK	Eq. H1-1b
	LC26 at 72.92%	0.05	OK	Eq. H1-1b
	LC27 at 72.92%	0.04	OK	Eq. H1-1b
	LC28 at 25.00%	0.04	OK	Eq. H1-1b
	LC29 at 25.00%	0.05	OK	Eq. H1-1b
	LC3 at 72.92%	0.45	OK	Eq. H1-1b
	LC30 at 72.92%	0.04	OK	Eq. H1-1b
	LC31 at 72.92%	0.04	OK	Eq. H1-1b
	LC32 at 72.92%	0.03	OK	Eq. H1-1b
	LC4 at 25.00%	0.37	OK	Eg. H1-1b Eg. H1-1b
	LC5 at 25.00%	0.47	OK	Eq. H1-1b
	LC6 at 25.00%	0.37	OK OK	Eq. H1-1b
	LC7 at 25.00% LC8 at 25.00%	0.45 0.37	OK OK	Eq. H1-1b
	LC9 at 25.00%	0.13	OK	Eq. H1-1b
	W180 at 25.00%	0.19	OK	Eq. H1-1b
	W210 at 25.00%	0.23	OK	Eg. H1-1b
	Wi180 at 25.00%	0.11	OK	Eq. H1-1b
	Wi210 at 25.00%	0.08	OK	Eq. H1-1b
	WL180 at 25.00%	0.03	OK	Eq. H1-1b
	WL210 at 25.00%	0.02	ОК	Eq. H1-1b
60	LC1 at 72.92%	0.45	OK	Eq. H1-1b
	LC10 at 72.92%	0.23	OK	Eq. H1-1b
	LC11 at 72.92%	0.33	OK	Eq. H1-1b
	LC12 at 72.92%	0.17	OK	Eq. H1-1b
	LC13 at 72.92%	0.11	OK	Eq. H1-1b
	LC14 at 72.92%	0.08	OK	Eq. H1-1b
	LC15 at 72.92%	0.10	OK	Eq. H1-1b
	LC16 at 72.92%	0.13	OK	Eq. H1-1b
	LC17 at 72.92%	0.08	OK	Eq. H1-1b
	LC18 at 72.92%	0.10	OK	Eq. H1-1b
	LC19 at 72.92%	0.14	OK	Eq. H1-1b
	LC2 at 72.92%	0.47	OK	Eq. H1-1b
	LC20 at 72.92%	0.10	OK	Eq. H1-1b

	1 C24 of 72 029/	0.07	OK	Eq. H1-1b
	LC21 at 72.92%	0.07		•
	LC22 at 72.92%	0.11	OK	Eq. H1-1b
	LC23 at 72.92%	0.13	OK	Eq. H1-1b
	LC24 at 72.92%	0.09	OK	Eq. H1-1b
	LC25 at 72.92%	0.18	ok	Eq. H1-1b
	LC26 at 72.92%	0.22	OK	Eq. H1-1b
	LC27 at 72.92%	0.24	OK	Eq. H1-1b
	LC28 at 72.92%	0.21	OK	Eq. H1-1b
	LC29 at 72.92%	0.13	OK	Eq. H1-1b
	LC3 at 72.92%	0.64	ОК	Eq. H1-1b
	LC30 at 72.92%	0.16	OK	Eq. H1-1b
	LC31 at 72.92%	0.19	OK	Eq. H1-1b
	LC32 at 72.92%	0.15	OK	Eq. H1-1b
	LC4 at 72.92%	0.51	OK	Eq. H1-1b
	LC5 at 72.92%	0.47	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC6 at 72.92%	0.47		Eq. H1-1b
	LC7 at 72.92%	0.61	OK	
	LC8 at 72.92%	0.50	OK	Eq. H1-1b
	LC9 at 72.92%	0.14	OK	Eq. H1-1b
	W180 at 72.92%	0.33	OK	Eq. H1-1b
	W210 at 72.92%	0.30	OK	Eq. H1-1b
	Wi180 at 72.92%	0.13	OK	Eq. H1-1b
	Wi210 at 72.92%	0.11	OK	Eq. H1-1b
	WL180 at 72.92%	0.03	OK	Eq. H1-1b
	WL210 at 72.92%	0.03	OK	Eq. H1-1b
63	LC1 at 72.92%	0.43	OK	Eq. H1-1b
03	LC10 at 72.92%	0.17	OK	Eq. H1-1b
	The second second	0.17	OK	Eq. H1-1b
	LC11 at 72.92%			
	LC12 at 72.92%	0.12	OK	Eq. H1-1b
	LC13 at 72.92%	0.05	OK	Eq. H1-1b
	LC14 at 72.92%	0.04	OK	Eq. H1-1b
	LC15 at 72.92%	0.05	OK	Eq. H1-1b
	LC15 at 72.92% LC16 at 72.92%	0.09	OK	Eq. H1-1b
			OK OK	Eq. H1-1b Eq. H1-1b
	LC16 at 72.92%	0.09	OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92%	0.09 0.07	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92%	0.09 0.07 0.09	OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92%	0.09 0.07 0.09 0.10	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00%	0.09 0.07 0.09 0.10 0.34	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07	OK OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04	OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC24 at 72.92% LC25 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07	OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06	OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06	OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.06 0.06	OK	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC3 at 72.92% LC3 at 72.92% LC3 at 72.92% LC3 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.06 0.14 0.39	OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC30 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.06 0.14 0.39 0.17	OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC27 at 72.92% LC30 at 72.92% LC31 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.06 0.14 0.39 0.17 0.18	OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14	OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC31 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC29 at 72.92% LC3 at 72.92% LC3 at 72.92% LC4 at 72.92% LC5 at 72.92% LC5 at 72.92% LC3 at 72.92% LC3 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC4 at 25.00% LC5 at 72.92% LC5 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34	OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% LC8 at 25.00%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.38 0.32	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC30 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% LC8 at 25.00% LC9 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.32 0.32 0.32	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 25.00% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC3 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% LC8 at 25.00% LC9 at 72.92% LC8 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.32 0.35 0.32 0.15 0.25	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC30 at 72.92% LC3 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% LC8 at 25.00% LC9 at 72.92% W180 at 72.92% W180 at 72.92% W180 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.32 0.42 0.34 0.35 0.25 0.20	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC28 at 72.92% LC30 at 72.92% LC31 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% W180 at 72.92% W180 at 72.92% W1180 at 72.92% W1180 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.32 0.42 0.34 0.35 0.15 0.25 0.20 0.10	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC23 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC30 at 72.92% LC3 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% LC8 at 25.00% LC9 at 72.92% W180 at 72.92% W180 at 72.92% W180 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.32 0.42 0.34 0.35 0.25 0.20	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC23 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC28 at 72.92% LC30 at 72.92% LC31 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% W180 at 72.92% W180 at 72.92% W1180 at 72.92% W1180 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.38 0.32 0.15 0.25 0.20 0.10 0.07 0.02	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
	LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC20 at 25.00% LC20 at 72.92% LC21 at 72.92% LC22 at 72.92% LC24 at 72.92% LC25 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC30 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC4 at 25.00% LC5 at 72.92% LC6 at 25.00% LC7 at 72.92% W180 at 72.92% W180 at 72.92% W180 at 72.92% W1180 at 72.92% W1180 at 72.92% W1180 at 72.92%	0.09 0.07 0.09 0.10 0.34 0.07 0.05 0.06 0.07 0.04 0.07 0.06 0.06 0.14 0.39 0.17 0.18 0.14 0.32 0.42 0.34 0.38 0.32 0.15 0.25 0.20 0.10 0.07	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b

66	LC1 at 31.25%	0.14	OK	Eq. H1-1b
	LC10 at 72.92%	0.18	OK	Eq. H1-1b
	LC11 at 72.92%	0.10	OK	Eq. H1-1b
	LC12 at 72.92%	0.11	OK	Eq. H1-1b
	LC13 at 72.92%	0.04	OK	Eq. H1-1b
	LC14 at 72.92%	0.03	OK	Eg. H1-1b
	LC15 at 72.92%	0.04	OK	Eq. H1-1b
	LC16 at 72.92%	0.08	OK	Eg. H1-1b
	LC17 at 72.92%	0.14	OK	Eq. H1-1b
	LC18 at 72.92%	0.17	OK	Eq. H1-1b
	LC19 at 72.92%	0.15	OK	Eq. H1-1b
	LC2 at 72.92%	0.48	ок	Eq. H1-1b
	LC20 at 72.92%	0.12	OK	Eq. H1-1b
	LC21 at 72.92%	0.03	OK	Eq. H1-1b
	LC22 at 72.92%	0.05	OK	Eq. H1-1b
	LC23 at 72.92%	0.04	OK	Eq. H1-1b
	LC24 at 72.92%	0.05	OK	Eq. H1-1b
	LC25 at 72.92%	0.04	OK	Eq. H1-1b
	LC26 at 72.92%	0.06	OK	Eq. H1-1b
	LC27 at 72.92%	0.04	OK	Eq. H1-1b
	LC28 at 72.92%	0.03	OK	Eq. H1-1b
	LC29 at 72.92%	0.06	OK	Eq. H1-1b
	LC3 at 31.25%	0.19	OK	Eq. H1-1b
	LC30 at 72.92%	0.09	OK	Eq. H1-1b
	LC31 at 72.92%	0.07	OK	Eq. H1-1b
	LC32 at 72.92%	0.04	OK	Eq. H1-1b
	LC4 at 72.92%	0.47	OK	Eq. H1-1b
	LC5 at 31.25%	0.14	OK	Eq. H1-1b
	LC6 at 72.92%	0.48	OK	Eq. H1-1b
	LC7 at 31.25%	0.18	OK	Eq. H1-1b
	LC8 at 72.92%	0.47	OK	Eq. H1-1b
	LC9 at 72.92%	0.06	OK	Eq. H1-1b
	W180 at 31.25%	0.09	OK	Eq. H1-1b
	W210 at 72.92%	0.30	OK	Eq. H1-1b
	Wi180 at 31.25%	0.04	OK	Eq. H1-1b
	Wi210 at 72.92%	0.11	OK	Eq. H1-1b
	WL180 at 31.25%	0.01	OK	Eq. H1-1b
	WL210 at 72.92%	0.03	OK	Eq. H1-1b
00	L O4 -+ 05 000/	0.40	OV	
69	LC1 at 25.00%	0.10	OK OK	Eq. H1-1b Eq. H1-1b
	LC10 at 72.92%	0.15	OK	Eq. H1-1b
	LC11 at 25.00% LC12 at 72.92%	0.05 0.14	OK	Eq. H1-1b
	LC12 at 72.92 %	0.14	OK	Eq. H1-1b
	LC14 at 25.00%	0.01	OK	Eq. H1-1b
	LC15 at 25.00%	0.02	OK	Eq. H1-1b
	LC16 at 72.92%	0.04	OK	Eq. H1-1b
	LC17 at 72.92%	0.06	ок	Eq. H1-1b
	LC18 at 72.92%	0.09	ok	Eq. H1-1b
	LC19 at 72.92%	0.06	OK	Eq. H1-1b
	LC2 at 25.00%	0.52	ОК	Eq. H1-1b
	LC20 at 72.92%	0.04	OK	Eq. H1-1b
	LC21 at 72.92%	0.13	OK	Eq. H1-1b
	LC22 at 72.92%	0.15	OK	Eq. H1-1b
	LC23 at 72.92%	0.12	ОК	Eq. H1-1b
	LC24 at 72.92%	0.12	ОК	Eq. H1-1b
	LC25 at 25.00%	0.04	ОК	Eq. H1-1b
	LC26 at 72.92%	0.04	OK	Eq. H1-1b
	LC27 at 25.00%	0.05	OK	Eq. H1-1b
	LC28 at 25.00%	0.07	OK	Eq. H1-1b
	LC29 at 72.92%	0.03	OK	Eq. H1-1b
	LC3 at 25.00%	0.11	OK	Eq. H1-1b
	LC30 at 72.92%	0.04	OK	Eq. H1-1b

	LC31 at 25.00% LC32 at 25.00% LC4 at 72.92% LC5 at 25.00% LC6 at 25.00% LC7 at 25.00% LC8 at 72.92% LC9 at 72.92% W180 at 25.00% W210 at 25.00% Wi210 at 25.00% WL180 at 25.00% WL180 at 25.00% WL210 at 25.00%	0.03 0.05 0.53 0.10 0.52 0.10 0.52 0.05 0.06 0.32 0.02 0.13 0.01 0.03	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
72	LC1 at 72.92% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92% LC19 at 72.92% LC2 at 72.92% LC20 at 72.92% LC21 at 72.92% LC21 at 72.92% LC22 at 72.92% LC24 at 72.92% LC25 at 72.92% LC25 at 72.92% LC26 at 72.92% LC26 at 72.92% LC27 at 72.92% LC27 at 72.92% LC28 at 72.92% LC29 at 72.92% LC30 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at 72.92% LC31 at 72.92% LC32 at	0.32 0.20 0.16 0.34 0.11 0.08 0.11 0.14 0.12 0.08 0.10 0.59 0.14 0.12 0.09 0.09 0.14 0.23 0.19 0.21 0.25 0.17 0.21 0.13 0.15 0.19 0.68 0.29 0.57 0.21 0.64 0.26 0.14 0.36 0.05 0.13 0.01 0.03	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
75	LC1 at 25.00% LC10 at 72.92% LC11 at 72.92% LC12 at 72.92% LC13 at 72.92% LC14 at 72.92% LC15 at 72.92% LC16 at 72.92% LC17 at 72.92% LC18 at 72.92%	0.16 0.20 0.13 0.23 0.07 0.05 0.06 0.10 0.10	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b

LC40 et 72 029/	0.40	OK	Eg. H1-1b
LC19 at 72.92%	0.10	OK	•
LC2 at 72.92%	0.55	ok	Eq. H1-1b
LC20 at 72.92%	0.11	OK	Eq. H1-1b
LC21 at 72.92%	0.07	OK	Eq. H1-1b
			•
LC22 at 72.92%	0.08	OK	Eq. H1-1b
LC23 at 72.92%	0.07	OK	Eg. H1-1b
			Eq. H1-1b
LC24 at 72.92%	0.09	OK	•
LC25 at 72.92%	0.06	OK	Eq. H1-1b
LC26 at 72.92%	0.09	OK	Eq. H1-1b
			Eq. H1-1b
LC27 at 72.92%	0.06	OK	•
LC28 at 72.92%	0.08	OK	Eq. H1-1b
LC29 at 72.92%	0.17	OK	Eq. H1-1b
LC3 at 25.00%	0.18	OK	
LC30 at 72.92%	0.15	OK	Eq. H1-1b
LC31 at 72.92%	0.17	OK	Eq. H1-1b
LC32 at 72.92%	0.20	OK	Eq. H1-1b
LC4 at 72.92%	0.51	OK	Eq. H1-1b
LC5 at 25.00%	0.16	ok	
			le. maras
LC6 at 72.92%	0.54	ok	Eq. H1-1b
LC7 at 25.00%	0.17	OK	
		OK	Eq. H1-1b
LC8 at 72.92%	0.49		•
LC9 at 72.92%	0.11	OK	Eq. H1-1b
W180 at 25.00%	0.11	OK	
			Eg. H1-1b
W210 at 72.92%	0.31	OK	Eq. 111-10
Wi180 at 25.00%	0.04	OK	
Wi210 at 72.92%	0.12	OK	Eq. H1-1b
			24
WL180 at 25.00%	0.01	OK	
WL210 at 72.92%	0.03	OK	Eq. H1-1b
LC4 at 49 069/	0.30	OK	Eg. H1-1b
LC1 at 48.96%	0.30	OK	· ·
LC10 at 48.96%	0.25	OK	Eq. H1-1b
LC11 at 48.96%	0.26	OK	Eq. H1-1b
			· ·
LC12 at 48.96%	0.24	OK	Eq. H1-1b
		OK OK	· ·
LC12 at 48.96% LC13 at 48.96%	0.24 0.13	OK OK	Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96%	0.24 0.13 0.10	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00%	0.24 0.13 0.10 0.12	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96%	0.24 0.13 0.10	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96%	0.24 0.13 0.10 0.12 0.19	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25	OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25	OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC23 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC18 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC23 at 50.00% LC23 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17	OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC23 at 50.00% LC24 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC25 at 48.96% LC25 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.17	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC23 at 50.00% LC24 at 50.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.17 0.19	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.17 0.19 0.19	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96% LC29 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.17 0.19 0.19	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.17 0.19 0.19	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96% LC29 at 48.96% LC29 at 48.96% LC3 at 48.96% LC3 at 48.96% LC3 at 48.96% LC3 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.19 0.18 0.19 0.19	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC26 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC28 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96% LC8 at 100.00%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32 0.20	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC28 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC29 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96% LC8 at 100.00% LC9 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32 0.20 0.28	OK O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96% LC8 at 100.00% LC9 at 48.96% LC8 at 100.00% LC9 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32 0.20 0.28 0.15	OK O O O O O O O O O O O O O O O O O O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96% LC8 at 100.00% LC9 at 48.96% V310 at 48.96% V310 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.19 0.18 0.25 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32 0.20 0.28 0.15 0.09	OK O O O O O O O O O O O O O O O O O O	Eq. H1-1b
LC12 at 48.96% LC13 at 48.96% LC14 at 48.96% LC15 at 0.00% LC16 at 48.96% LC17 at 48.96% LC19 at 50.00% LC2 at 0.00% LC20 at 50.00% LC21 at 50.00% LC22 at 50.00% LC22 at 50.00% LC23 at 50.00% LC24 at 50.00% LC25 at 48.96% LC26 at 48.96% LC27 at 48.96% LC30 at 48.96% LC30 at 48.96% LC30 at 48.96% LC31 at 48.96% LC31 at 48.96% LC31 at 48.96% LC32 at 48.96% LC32 at 48.96% LC31 at 48.96% LC32 at 48.96% LC4 at 100.00% LC5 at 48.96% LC6 at 0.00% LC7 at 48.96% LC8 at 100.00% LC9 at 48.96% LC8 at 100.00% LC9 at 48.96%	0.24 0.13 0.10 0.12 0.19 0.19 0.18 0.25 0.19 0.17 0.17 0.17 0.17 0.20 0.19 0.18 0.19 0.22 0.35 0.21 0.20 0.21 0.22 0.27 0.23 0.32 0.20 0.28 0.15	OK O O O O O O O O O O O O O O O O O O	Eq. H1-1b

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			2	
	Wi210 at 85.42%	0.04	OK	Eq. H1-1b
	WL180 at 48.96%	0.01	OK	Eq. H1-1b
	WL210 at 85.42%	0.01	OK	Eq. H1-1b
2	LC1 at 100.00%	0.23	OK	Eq. H1-1b
	LC10 at 50.00%	0.27	OK	Eq. H1-1b
	LC11 at 50.00%	0.26	OK	Eq. H1-1b
	LC12 at 50.00%	0.26	ОК	Eq. H1-1b
	LC13 at 50.00%	0.13	OK	Eq. H1-1b
	LC14 at 50.00%	0.10	ok	Eq. H1-1b
		0.11	OK	Eq. H1-1b
	LC15 at 50.00%			Eq. H1-1b
	LC16 at 50.00%	0.18	OK	
	LC17 at 50.00%	0.18	OK	Eq. H1-1b
	LC18 at 50.00%	0.19	OK	Eq. H1-1b
	LC19 at 50.00%	0.19	OK	Eq. H1-1b
	LC2 at 50.00%	0.30	OK	Eq. H1-1b
	LC20 at 50.00%	0.18	OK	Eq. H1-1b
	LC21 at 50.00%	0.15	OK	Eq. H1-1b
	LC22 at 50.00%	0.16	OK	Eq. H1-1b
	LC23 at 50.00%	0.16	OK	Eq. H1-1b
	LC24 at 50.00%	0.15	OK	Eq. H1-1b
	LC25 at 50.00%	0.20	OK	Eq. H1-1b
	LC26 at 50.00%	0.21	OK	Eq. H1-1b
	LC27 at 50.00%	0.20	OK	Eq. H1-1b
	LC28 at 50.00%	0.19	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC29 at 50.00%	0.21		
	LC3 at 0.00%	0.24	OK	Eq. H1-1b
	LC30 at 50.00%	0.22	OK	Eq. H1-1b
	LC31 at 50.00%	0.22	OK	Eq. H1-1b
	LC32 at 50.00%	0.21	OK	Eq. H1-1b
	LC4 at 50.00%	0.35	OK	Eq. H1-1b
	LC5 at 100.00%	0.21	OK	Eq. H1-1b
	LC6 at 50.00%	0.27	OK	Eq. H1-1b
	LC7 at 0.00%	0.22	OK	Eq. H1-1b
	LC8 at 50.00%	0.32	OK	Eq. H1-1b
	LC9 at 50.00%	0.23	OK	Eq. H1-1b
	W180 at 0.00%	0.10	OK	Eq. H1-1b
	W210 at 50.00%	0.15	OK	Eq. H1-1b
	Wi180 at 0.00%	0.04	OK	Eq. H1-1b
	Wi210 at 50.00%	0.05	OK	Eq. H1-1b
	WL180 at 0.00%	0.03	OK	Eq. H1-1b
	WL210 at 50.00%	0.01	OK	Eq. H1-1b
2	L C4 =4 50 000/	0.2E	OK	Eq. H1-1b
3	LC1 at 50.00%	0.25	OK	Eq. H1-1b
	LC10 at 50.00%	0.26	OK	-
	LC11 at 50.00%	0.26	OK	Eq. H1-1b
	LC12 at 50.00%	0.28	OK	Eq. H1-1b
	LC13 at 50.00%	0.13	OK	Eq. H1-1b
	LC14 at 50.00%	0.10	OK	Eq. H1-1b
	LC15 at 50.00%	0.11	OK	Eq. H1-1b
	LC16 at 50.00%	0.19	OK	Eq. H1-1b
	LC17 at 50.00%	0.18	OK	Eq. H1-1b
	LC18 at 50.00%	0.18	OK	Eq. H1-1b
	LC19 at 50.00%	0.19	OK	Eq. H1-1b
	LC2 at 50.00%	0.31	ОК	Eq. H1-1b
	LC20 at 50.00%	0.19	OK	Eq. H1-1b
	LC21 at 50.00%	0.16	ОК	Eq. H1-1b
	LC22 at 50.00%	0.15	OK	Eg. H1-1b
	LC23 at 50.00%	0.16	OK	Eq. H1-1b
	LC24 at 50.00%	0.10	OK	Eq. H1-1b
			OK	Eq. H1-1b
	LC25 at 50.00%	0.20		•
	LC26 at 50.00%	0.20	OK	Eq. H1-1b
	LC27 at 50.00%	0.21	OK OK	Eq. H1-1b
	LC28 at 50.00%	0.21	ОК	Eq. H1-1b

	LC29 at 50.00%	0.21	OK	Eq. H1-1b
	LC3 at 50.00%	0.21	OK	Eq. H1-1b
	LC30 at 50.00%	0.21	ОК	Eq. H1-1b
	LC31 at 50.00%	0.22	OK	Eq. H1-1b
	LC32 at 50.00%	0.23	OK	Eq. H1-1b
	LC4 at 50.00%	0.30	OK	Eq. H1-1b
	LC5 at 50.00%	0.23	OK	Eq. H1-1b
	LC6 at 50.00%	0.29	OK	Eq. H1-1b
				•
	LC7 at 50.00%	0.17	OK	Eq. H1-1b
	LC8 at 50.00%	0.26	OK	Eq. H1-1b
	LC9 at 50.00%	0.25	OK	Eq. H1-1b
	W180 at 50.00%	0.12	OK	Eq. H1-1b
			OK	Eq. H1-1b
	W210 at 50.00%	0.18		•
	Wi180 at 50.00%	0.04	OK	Eq. H1-1b
	Wi210 at 50.00%	0.05	OK	Eq. H1-1b
	WL180 at 50.00%	0.01	OK	Eq. H1-1b
	WL210 at 50.00%	0.01	OK	Eq. H1-1b
	Technological Control Control Control	an commence		namana arau menganan ang atawa
40	1.04 -4.400.000/	0.00	OK	Ea U1 1b
10	LC1 at 100.00%	0.22	OK	Eq. H1-1b
	LC10 at 100.00%	0.72	OK	Eq. H1-1b
	LC11 at 100.00%	0.68	OK	Eq. H1-1b
	LC12 at 100.00%	0.54	OK	Eq. H1-1b
	LC13 at 100.00%	0.34	OK	Eq. H1-1b
				· ·
	LC14 at 100.00%	0.26	OK	Eq. H1-1b
	LC15 at 100.00%	0.39	OK	Eq. H1-1b
	LC16 at 100.00%	0.51	OK	Eq. H1-1b
	LC17 at 100.00%	0.55	OK	Eq. H1-1b
	LC18 at 100.00%	0.57	OK	Eq. H1-1b
		0.57	OK	Eq. H1-1b
	LC19 at 100.00%			•
	LC2 at 100.00%	0.74	ОК	Eq. H1-1b
	LC20 at 100.00%	0.53	OK	Eq. H1-1b
	LC21 at 100.00%	0.43	OK	Eq. H1-1b
	LC22 at 100.00%	0.45	OK	Eq. H1-1b
	LC23 at 100.00%	0.45	OK	Eq. H1-1b
				Eq. H1-1b
	LC24 at 100.00%	0.41	OK	•
	LC25 at 100.00%	0.43	OK	Eq. H1-1b
	LC26 at 100.00%	0.46	OK	Eq. H1-1b
	LC27 at 100.00%	0.44	OK	Eq. H1-1b
	LC28 at 100.00%	0.42	OK	Eq. H1-1b
	LC29 at 100.00%	0.55	OK	Eq. H1-1b
	LC3 at 100.00%	0.61	OK	Eq. H1-1b
	LC30 at 100.00%	0.58	OK	Eq. H1-1b
	LC31 at 100.00%	0.57	OK	Eq. H1-1b
	LC32 at 100.00%	0.54	OK	Eq. H1-1b
	LC4 at 25.00%	0.16	ОК	Eq. H1-1b
				Eg. H1-1b
	LC5 at 100.00%	0.13	OK OK	•
	LC6 at 100.00%	0.65	OK	Eq. H1-1b
	LC7 at 100.00%	0.53	OK	Eq. H1-1b
	LC8 at 25.00%	0.25	OK	Eq. H1-1b
	LC9 at 100.00%	0.60	OK	Eq. H1-1b
	W180 at 100.00%	0.18	ОК	Eq. H1-1b
	W210 at 25.00%	0.32	OK	Eq. H1-1b
	Wi180 at 100.00%	0.06	OK	Eq. H1-1b
	Wi210 at 25.00%	0.12	OK	Eq. H1-1b
	WL180 at 100.00%	0.02	OK	Eq. H1-1b
	WL210 at 25.00%	0.03	OK	Eq. H1-1b
11	LC1 at 100.00%	0.15	OK	Eq. H1-1b
• •				•
	LC10 at 100.00%	0.47	OK	Eq. H1-1b
	LC11 at 100.00%	0.61	OK	Eq. H1-1b
	LC12 at 100.00%	0.64	OK	Eq. H1-1b
	LC13 at 100.00%	0.29	OK	Eq. H1-1b
	LC14 at 100.00%	0.22	OK	Eq. H1-1b
	LC15 at 100.00%	0.33	ОК	Eq. H1-1b
	_O 10 Gt 100.00 /0	0.00	J.,	-4

	LC16 at 100.00%	0.45	ОК	Eq. H1-1b
	LC17 at 100.00%	0.49	OK	Eq. H1-1b
	LC18 at 100.00%	0.48	OK	Eq. H1-1b
	LC19 at 100.00%	0.51	OK	Eq. H1-1b
	LC2 at 25.00%	0.23	OK	Eq. H1-1b
	LC20 at 100.00%	0.52	OK	Eq. H1-1b
	LC21 at 100.00%	0.37	OK	Eq. H1-1b
	LC22 at 100.00%	0.36	OK	Eq. H1-1b
	LC23 at 100.00%	0.39	OK	Eq. H1-1b
	LC24 at 100.00%	0.40	OK	Eq. H1-1b
	LC25 at 100.00%	0.37	OK	Eq. H1-1b
	LC26 at 100.00%	0.36	OK	Eq. H1-1b
	LC27 at 100.00%	0.39	OK	Eq. H1-1b
	LC28 at 100.00%	0.40	OK	Eq. H1-1b
	LC29 at 100.00%	0.49	OK	Eq. H1-1b
	LC3 at 100.00%	0.54	OK	Eq. H1-1b
	LC30 at 100.00%	0.49	OK	Eq. H1-1b
	LC31 at 100.00%	0.52	OK OK	Eq. H1-1b Eq. H1-1b
	LC32 at 100.00%	0.52	OK	Eq. H1-1b
	LC4 at 100.00%	0.70	OK OK	Eq. H1-1b
	LC5 at 93.75% LC6 at 25.00%	0.08 0.30	OK	Eq. H1-1b
		0.30	OK	Eq. H1-1b
	LC7 at 100.00% LC8 at 100.00%	0.47	OK	Eq. H1-1b
	LC9 at 100.00%	0.53	OK	Eq. H1-1b
	W180 at 100.00%	0.16	OK	Eq. H1-1b
	W210 at 100.00%	0.27	OK	Eq. H1-1b
	Wi180 at 100.00%	0.06	OK	Eq. H1-1b
	Wi210 at 100.00%	0.10	OK	Eq. H1-1b
	WL180 at 100.00%	0.01	OK	Eg. H1-1b
	WL210 at 100.00%	0.02	ОК	Eq. H1-1b
12	LC1 at 100.00%	0.71	OK	Eq. H1-1b
12	LC10 at 100.00%	0.56	OK	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00%	0.56 0.46	OK OK	Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00%	0.56 0.46 0.56	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00%	0.56 0.46 0.56 0.29	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00%	0.56 0.46 0.56 0.29 0.21	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33	OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45	OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45	OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50	OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48	OK OK OK OK OK OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40	OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC18 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40 0.38	OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40 0.38 0.36	OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40 0.38 0.36 0.38	OK OK OK OK OK OK OK OK OK OK OK OK OK	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC25 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40 0.38 0.36 0.38 0.40	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC2 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.50 0.40 0.38 0.36 0.38 0.40 0.38	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.36	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.40 0.38	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.40 0.38 0.36 0.37 0.52 0.50	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.40 0.38 0.40 0.38 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.4	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC29 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.52 0.27 0.50 0.48 0.51	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.38 0.36 0.38 0.40 0.38 0.36 0.38 0.52 0.27 0.50 0.48 0.51 0.36	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.30 0.38 0.36 0.38 0.36 0.38 0.52 0.27 0.50 0.48 0.51 0.36 0.64	OK OK OK OK OK OK OK OK OK OK OK OK OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.30 0.38 0.36 0.38 0.36 0.38 0.52 0.27 0.50 0.48 0.51 0.36 0.64 0.29	OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.30 0.40 0.38 0.36 0.38 0.40 0.38 0.52 0.27 0.50 0.48 0.51 0.36 0.64 0.29 0.34	OK O	Eq. H1-1b
12	LC10 at 100.00% LC11 at 100.00% LC12 at 100.00% LC13 at 100.00% LC14 at 100.00% LC15 at 100.00% LC15 at 100.00% LC16 at 100.00% LC17 at 100.00% LC19 at 100.00% LC20 at 100.00% LC21 at 100.00% LC22 at 100.00% LC22 at 100.00% LC23 at 100.00% LC24 at 100.00% LC25 at 100.00% LC25 at 100.00% LC26 at 100.00% LC27 at 100.00% LC29 at 100.00% LC3 at 25.00% LC30 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC32 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC5 at 100.00%	0.56 0.46 0.56 0.29 0.21 0.33 0.45 0.52 0.50 0.48 0.36 0.30 0.38 0.36 0.38 0.36 0.38 0.52 0.27 0.50 0.48 0.51 0.36 0.64 0.29	OK O	Eq. H1-1b

	W180 at 25.00%	0.35	OK	Eq. H1-1b
	W210 at 100.00%	0.05	OK	Eq. H1-1b
	Wi180 at 25.00%	0.13	OK	Eq. H1-1b
	Wi210 at 100.00%	0.01	OK	Eq. H1-1b
	WL180 at 25.00%	0.03	OK	Eg. H1-1b
				Eq. H1-1b
	WL210 at 100.00%	0.00	OK	Eq. 171-10
				- 114 45
31	LC1 at 0.00%	0.03	OK	Eq. H1-1b
	LC10 at 0.00%	0.37	OK	Eq. H1-1b
	LC11 at 0.00%	0.34	OK	Eq. H1-1b
	LC12 at 0.00%	0.26	OK	Eq. H1-1b
	LC13 at 0.00%	0.17	OK	Eg. H1-1b
	LC14 at 0.00%	0.12	OK	Eq. H1-1b
	LC15 at 0.00%	0.18	OK	Eq. H1-1b
				•
	LC16 at 0.00%	0.32	OK	Eq. H1-1b
	LC17 at 0.00%	0.27	OK	Eq. H1-1b
	LC18 at 0.00%	0.29	OK	Eq. H1-1b
	LC19 at 0.00%	0.29	OK	Eq. H1-1b
	LC2 at 0.00%	0.41	OK	Eq. H1-1b
	LC20 at 0.00%	0.27	OK	Eq. H1-1b
	LC21 at 0.00%	0.19	OK	Eg. H1-1b
		0.21	ОК	Eq. H1-1b
	LC22 at 0.00%			Eq. H1-1b
	LC23 at 0.00%	0.20	OK	•
	LC24 at 0.00%	0.18	OK	Eq. H1-1b
	LC25 at 0.00%	0.19	OK	Eq. H1-1b
	LC26 at 0.00%	0.21	OK	Eq. H1-1b
	LC27 at 0.00%	0.20	OK	Eq. H1-1b
	LC28 at 0.00%	0.18	OK	Eq. H1-1b
	LC29 at 0.00%	0.27	OK	Eq. H1-1b
	LC3 at 0.00%	0.30	OK	Eq. H1-1b
	LC30 at 0.00%	0.30	ok	Eq. H1-1b
		0.30	OK	Eq. H1-1b
	LC31 at 0.00%			•
	LC32 at 0.00%	0.27	OK	Eq. H1-1b
	LC4 at 0.00%	0.04	OK	Eq. H1-1b
	LC5 at 31.25%	0.01	OK	Eq. H1-1b
	LC6 at 0.00%	0.37	OK	Eq. H1-1b
	LC7 at 0.00%	0.26	OK	Eq. H1-1b
	LC8 at 0.00%	0.07	OK	Eq. H1-1b
	LC9 at 0.00%	0.28	OK	Eq. H1-1b
	W180 at 0.00%	0.08	OK	Eq. H1-1b
	W210 at 0.00%	0.09	OK	Eq. H1-1b
		0.03	ОК	Eq. H1-1b
	Wi180 at 0.00%			Eq. H1-1b
	Wi210 at 0.00%	0.03	OK	
	WL180 at 0.00%	0.01	OK	Eq. H1-1b
	WL210 at 0.00%	0.01	OK	Eq. H1-1b
32	LC1 at 50.00%	0.01	OK	Eq. H1-1b
	LC10 at 100.00%	0.21	OK	Eq. H1-1b
	LC11 at 100.00%	0.30	OK	Eq. H1-1b
	LC12 at 100.00%	0.33	OK	Eq. H1-1b
	LC13 at 100.00%	0.14	OK	Eq. H1-1b
	LC14 at 100.00%	0.10	OK	Eq. H1-1b
	LC15 at 100.00%	0.15	OK	Eq. H1-1b
	LC16 at 100.00%	0.29	OK	Eq. H1-1b
	LC17 at 100.00%	0.24	OK	Eq. H1-1b
	LC18 at 100.00%	0.24	OK	Eq. H1-1b
	LC19 at 100.00%	0.26	OK	Eq. H1-1b
	LC2 at 100.00%	0.06	OK	Eq. H1-1b
	LC20 at 100.00%	0.26	OK	Eq. H1-1b
	LC21 at 100.00%	0.16	OK	Eq. H1-1b
	LC22 at 100.00%	0.15	OK	Eg. H1-1b
	LC23 at 100.00%	0.17	OK	Eq. H1-1b
	LC24 at 100.00%	0.17	OK	Eq. H1-1b
	LUZ4 at 100.0070		OK OK	
	LC25 at 100.00%	0.16		Eq. H1-1b

	LC26 at 100.00% LC27 at 100.00% LC28 at 100.00% LC29 at 100.00% LC3 at 100.00% LC31 at 100.00% LC31 at 100.00% LC32 at 100.00% LC4 at 100.00% LC5 at 100.00% LC6 at 100.00%	0.15 0.17 0.18 0.24 0.27 0.24 0.26 0.27 0.38 0.02 0.08	OK OK OK OK OK OK OK OK	Eq. H1-1b
	LC7 at 100.00% LC8 at 100.00% LC9 at 100.00% W180 at 100.00%	0.23 0.35 0.24 0.08	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	W210 at 100.00% Wi180 at 100.00% Wi210 at 100.00%	0.15 0.03 0.06	OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	WL180 at 100.00% WL210 at 100.00%	0.01 0.01	OK OK 	Eq. H1-1b
33	LC1 at 0.00% LC10 at 0.00% LC11 at 0.00% LC12 at 0.00% LC13 at 0.00%	0.40 0.27 0.21 0.27 0.14	ок ок ок ок ок	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC14 at 0.00% LC15 at 0.00% LC16 at 0.00% LC17 at 0.00%	0.10 0.15 0.29 0.26	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC18 at 0.00% LC19 at 0.00% LC2 at 0.00% LC20 at 0.00%	0.25 0.24 0.14 0.25	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC21 at 0.00% LC22 at 0.00% LC23 at 0.00% LC24 at 0.00%	0.18 0.16 0.15 0.16	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC25 at 0.00% LC26 at 0.00% LC27 at 0.00% LC28 at 0.00%	0.18 0.16 0.15 0.16	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC29 at 0.00% LC3 at 0.00% LC30 at 0.00% LC31 at 0.00%	0.27 0.07 0.25 0.24	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC32 at 0.00% LC4 at 0.00% LC5 at 0.00% LC6 at 0.00%	0.25 0.13 0.37 0.10	OK OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	LC7 at 0.00% LC8 at 0.00% LC9 at 0.00%	0.09 0.10 0.33	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b
	W180 at 0.00% W210 at 0.00% Wi180 at 0.00% Wi210 at 0.00%	0.10 0.00 0.04 0.00	OK OK OK	Eq. H1-1b Eq. H1-1b Eq. H1-1b Eq. H1-1b
	WL180 at 0.00% WL210 at 0.00%	0.01 0.00	OK OK	Eq. H1-1b Eq. H1-1b



Current Date: 6/7/2018 12:20 PM

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Geometry data

GLOSSARY

Cb22, Cb33 Moment gradient coefficients

* Coefficients applied to bending term in interaction formula Cm22, Cm33 : Tapered member section depth at J end of member d0 Rigid end offset distance measured from J node in axis X DJX Rigid end offset distance measured from J node in axis Y DJY Rigid end offset distance measured from J node in axis Z DJZ Rigid end offset distance measured from K node in axis X DKX : Rigid end offset distance measured from K node in axis Y DKY : Rigid end offset distance measured from K node in axis Z DKZ * Tapered member section depth at K end of member dL

Ig factor : Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members

K22 : Effective length factor about axis 2 K33 : Effective length factor about axis 3

L22 : Member length for calculation of axial capacity
L33 : Member length for calculation of axial capacity

LB pos : Lateral unbraced length of the compression flange in the positive side of local axis 2

LB neg : Lateral unbraced length of the compression flange in the negative side of local axis 2

RX : Rotation about X
RY : Rotation about Y
RZ : Rotation about Z

TO 1 = Tension only member 0 = Normal member

TX : Translation in X TY : Translation in Y TZ : Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
2	0.00	0.00	-2.3333	0
3	-3.5359	0.00	-2.00	0
4	-7.00	0.00	0.00	0
5	-1.4793	0.00	-4.8955	0
6	-3.50	0.00	-6.0622	0
7	0.00	0.00	-8.1244	0
8	0.00	0.00	-12.1244	0
9	3.5359	0.00	-2.00	0
10	7.00	0.00	0.00	0
11	1.4793	0.00	-4.8955	0
12	3.50	0.00	-6.0622	0
14	6.1705	6.00	-1.8274	0
19	1.1705	6.00	-10.4876	0
41	1.1705	-2.00	-10.4876	0
44	6.1705	-2.00	-1.8274	0
53	4.5038	6.00	-4.7141	0
54	2.8372	6.00	-7.6009	0
63	2.8372	-2.00	-7.6009	0
64	4.5038	-2.00	-4.7141	0
69	-6.3333	4.00	0.00	0
71	-6.6667	4.00	-0.5774	0
73	6.3333	4.00	0.00	0

75	6.6667	4.00	-0.5774	0
77	0.3333	4.00	-11.547	0
79	-0.3333	4.00	-11.547	0
83	-1.6717	-3.00	-3.0763	0
84	1.6717	-3.00	-3.0763	0
86	0.00	-3.00	-5.9718	0
87	-4.4019	0.00	-1.50	0
88	4.4019	0.00	-1.50	0
89	0.00	0.00	-9.1244	0
91	0.00	0.00	0.00	0
93	5.9973	4.00	-1.7274	0
94	0.9973	4.00	-10.3876	0
95	4.3306	4.00	-4.6141	0
96	2.664	4.00	-7.5009	0
97	6.1705	4.00	-1.8274	0
98	1.1705	4.00	-10.4876	0
99	4.5038	4.00	-4.7141	0
100	2.8372	4.00	-7.6009	0
101	5.9973	0.00	-1.7274	0
102	6.1705	0.00	-1.8274	0
103	4.3306	0.00	-4.6141	0
104	4.5038	0.00	-4.7141	0
105	2.664	0.00	-7.5009	0
106	2.8372	0.00	-7.6009	0
107	0.9973	0.00	-10.3876	0
108	1.1705	0.00	-10.4876	0
133	-6.1705	6.00	-1.8274	0
134	-6.1705	-2.00	-1.8274	0
135	-5.9973	4.00	-1.7274	0
136	-6.1705	4.00	-1.8274	0
137	-5.9973	0.00	-1.7274	0
138	-6.1705	0.00	-1.8274	0
139	-4.5038	6.00	-4.7141	0
140	-4.5038	-2.00	-4.7141	0
141	-4.3306	4.00	-4.6141	0
142	-4.5038	4.00	-4.7141	0
143	-4.3306	0.00	-4.6141	0
144	-4.5038	0.00	-4.7141	0
145	-2.8372	6.00	-7.6009	0
146	-2.8372	-2.00	-7.6009	0
147	-2.664	4.00	-7.5009	0
148	-2.8372	4.00	-7.6009	0
149	-2.664	0.00	-7.5009	0
150	-2.8372	0.00	-7.6009	0
151	-1.1705	6.00	-10.4876	0
152	-1.1705	-2.00	-10.4876	0
153	-0.9973	4.00	-10.3876	0
154	-1.1705	4.00	-10.4876	0
155	-0.9973	0.00	-10.3876	0
156	-1.1705	0.00	-10.4876	0
157	5.00	6.00	0.20	0
158	5.00	-2.00	0.20	0
159	5.00	4.00	0.00	0
160	5.00	4.00	0.20	0
161	5.00	0.00	0.00	0
162	5.00	0.00	0.20	0
163	1.6667	6.00	0.20	0
164	1.6667	-2.00	0.20	0
165	1.6667	4.00	0.00	0
166	1.6667	4.00	0.20	0

167	1.6667	0.00	0.00	0
168	1.6667	0.00	0.20	0
169	-1.6667	6.00	0.20	0
170	-1.6667	-2.00	0.20	0
171	-1.6667	4.00	0.00	0
172	-1.6667	4.00	0.20	0
173	-1.6667	0.00	0.00	0
174	-1.6667	0.00	0.20	0
175	-5.00	6.00	0.20	0
176	-5.00	-2.00	0.20	0
177	-5.00	4.00	0.00	0
178	-5.00	4.00	0.20	0
179	-5.00	0.00	0.00	0
180	-5.00	0.00	0.20	0
		000000000000000000000000000000000000000		

Restraints

Node	TX	TY	TZ	RX	RY	RZ
2	ининения 1	1	1	1	1	 1
5	1	1	1	1	1	1
11	1	1	1	1	1	1
83	1	1	1	0	0	0
84	1	1	1	0	0	0
86	1	1	1	0	0	0

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	4	10		T2L 3X3X1_4	A36	0.00	0.00	0.00
2	10	8		T2L 3X3X1_4	A36	0.00	0.00	0.00
3	8	4		T2L 3X3X1_4	A36	0.00	0.00	0.00
4	3	9		L 3X3X1_4	A36	0.00	0.00	0.00
5	9	7		L 3X3X1_4	A36	0.00	0.00	0.00
6	7	3		L 3X3X1_4	A36	0.00	0.00	0.00
7	2	91		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
8	11	12		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
9	5	6		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
10	3	4		T2L 3X3X1_4	A36	0.00	0.00	0.00
11	9	10		T2L 3X3X1_4	A36	0.00	0.00	0.00
12	7	8		T2L 3X3X1_4	A36	0.00	0.00	0.00
13	14	44		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
14	53	64		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
16	19	41		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
25	69	73		PIPE 2x0.154	A36	0.00	0.00	0.00
26	79	71		PIPE 2x0.154	A36	0.00	0.00	0.00
27	75	77		PIPE 2x0.154	A36	0.00	0.00	0.00
28	69	71		L 3X3X1_4	A36	0.00	0.00	0.00
29	73	75		L 3X3X1_4	A36	0.00	0.00	0.00
30	77	79		L 3X3X1_4	A36	0.00	0.00	0.00
31	87	83		T2L 3X3X1 4	A36	0.00	0.00	0.00

32	84	88	T2L 3X3X1_4	A36	0.00	0.00	0.00
33	89	86	T2L 3X3X1_4	A36	0.00	0.00	0.00
54	133	134	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	139	140	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
15	54	63	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	145	146	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
63	151	152	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
66	157	158	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
69	163	164	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
72	169	170	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
75	175	176	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
	[= 09]				
1	90.00	0	0.00	0.00	0.00
2	90.00	0	0.00	0.00	0.00
3	90.00	0	0.00	0.00	0.00
7	90.00	0	0.00	0.00	0.00
8	90.00	0	0.00	0.00	0.00
9	90.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	180.00	0	0.00	0.00	0.00
12	180.00	0	0.00	0.00	0.00
13	0.00	2	-0.50	0.00	-0.866
14	0.00	2	-0.50	0.00	-0.866
16	0.00	2	-0.50	0.00	-0.866
25	270.00	0	0.00	0.00	0.00
26	270.00	0	0.00	0.00	0.00
27	270.00	0	0.00	0.00	0.00
28	90.00	0	0.00	0.00	0.00
29	180.00	0	0.00	0.00	0.00
30	180.00	0	0.00	0.00	0.00
54	0.00	2	-0.50	0.00	0.866
57	0.00	2	-0.50	0.00	0.866
15	0.00	2	-0.50	0.00	-0.866
60	0.00	2	-0.50	0.00	0.866
63	0.00	2	-0.50	0.00	0.866

35 WILDWOOD ST

Location 35 WILDWOOD ST **Mblu** A8B/ 1///

Acct# 91200035 Owner NEW BRITAIN CITY OF -

PARK

Assessment \$1,128,330 **Appraisal** \$1,611,900

PID 1830 Building Count 1

Current Value

Appraisal					
Valuation Year Improvements Land Total					
2012	\$926,900	\$685,000	\$1,611,900		
Assessment					
Valuation Year	Improvements	Land	Total		
2012	\$648,830	\$479,500	\$1,128,330		

Owner of Record

OwnerNEW BRITAIN CITY OF - PARKSale Price\$0Co-OwnerCHESLEY PARKCertificateAddress27 WEST MAIN STBook & Page

NEW BRITAIN, CT 06051 Sale Date 01/01/1900

Ownership History

Ownership History				
Owner	Sale Price	Certificate	Book & Page	Sale Date
NEW BRITAIN CITY OF - PARK	\$0			01/01/1900

Building Information

Building 1 : Section 1

Year Built:
Living Area: 0

Building Photo

Replacement Cost: \$0

Building Percent

Good:

Replacement Cost

Less Depreciation: \$0

Building Attributes			
Field Description			
Style	Outbuildings		
Model			

Grade Stories Occupancy Exterior Wall 1 Exterior Wall 2 Roof Structure Roof Cover Interior Wall 1 Interior Wall 2 Interior Fir 1 Interior Fir 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages Bldg Nbhd		
Occupancy Exterior Wall 1 Exterior Wall 2 Roof Structure Roof Cover Interior Wall 1 Interior Wall 2 Interior Fir 1 Interior Fir 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Attra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Grade	
Exterior Wall 2 Roof Structure Roof Cover Interior Wall 1 Interior Wall 2 Interior Flr 1 Interior Flr 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Alf Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Stories	
Exterior Wall 2 Roof Structure Roof Cover Interior Wall 1 Interior Wall 2 Interior Fir 1 Interior Fir 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Occupancy	
Roof Structure Roof Cover Interior Wall 1 Interior Wall 2 Interior Flr 1 Interior Flr 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Exterior Wall 1	
Roof Cover Interior Wall 1 Interior Wall 2 Interior Fir 1 Interior Fir 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Exterior Wall 2	
Interior Wall 1 Interior Wall 2 Interior Fir 1 Interior Fir 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Roof Structure	
Interior Wall 2 Interior FIr 1 Interior FIr 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Roof Cover	
Interior Flr 1 Interior Flr 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Interior Wall 1	
Interior FIr 2 Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Atra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Interior Wall 2	
Central Heat Sys AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Interior Flr 1	
AC Type Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Interior Flr 2	
Total Bedrooms Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Central Heat Sys	
Total Full Baths Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	AC Type	
Total Half Baths Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Total Bedrooms	
Total Xtra Fixtrs Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Total Full Baths	
Total Rooms Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Total Half Baths	
Bath Style Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Total Xtra Fixtrs	
Kitchen Style Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Total Rooms	
Whirlpool Tub Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Bath Style	
Fireplaces Rec Room Finish Rec Room Qual Bsmt Garages	Kitchen Style	
Rec Room Finish Rec Room Qual Bsmt Garages	Whirlpool Tub	
Rec Room Qual Bsmt Garages	Fireplaces	
Bsmt Garages	Rec Room Finish	
	Rec Room Qual	
Bldg Nbhd	Bsmt Garages	
	Bldg Nbhd	



(http://images.vgsi.com/photos/NewBritainCTPhotos// $\00\$ $\14/61.JPG$)

Building Layout

■ Building Layout

Building Sub-Areas (sq ft) <u>Legend</u>

No Data for Building Sub-Areas

Extra Features

Extra Features	<u>Legend</u>
No Data for Extra Features	

Land

Land Use		Land Line Valuation	
Use Code	903A	Size (Acres)	11.85
Description	Mun Park MDL-00	Depth	
Zone	Т	Assessed Value	\$479,500
Neighborhood	107	Appraised Value	\$685,000
Alt Land Appr	No		
Category			

Outbuildings

Outbuildings <u>Legend</u>

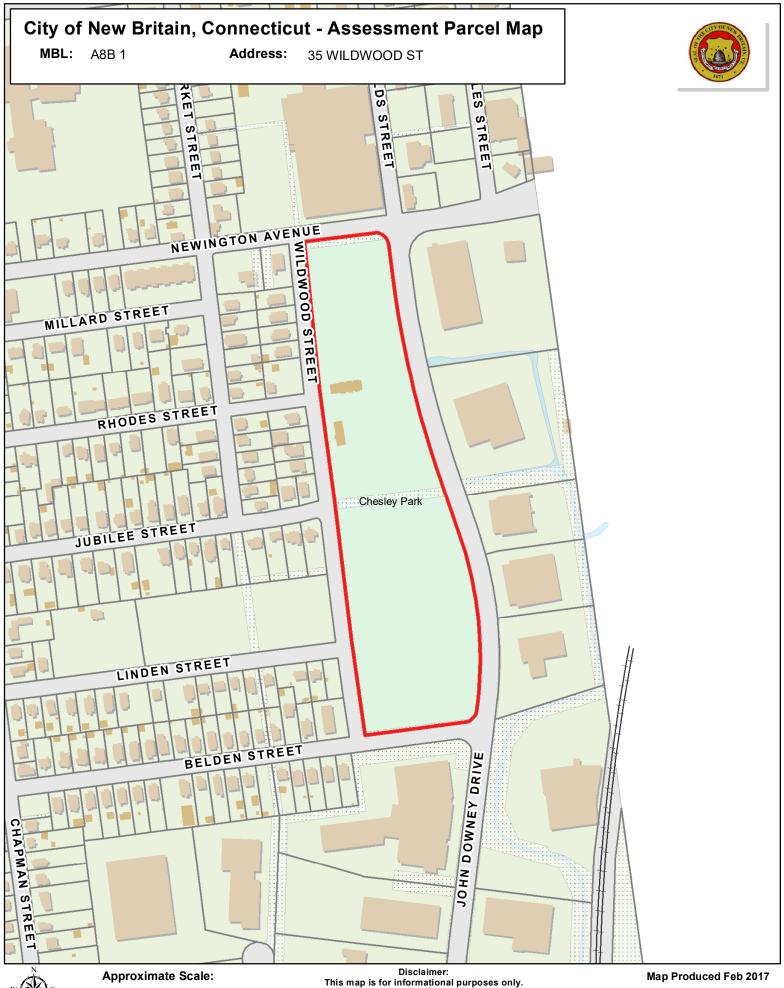
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
TEN1	Tennis Crt Asp			4 Units	\$96,600	1
PAV1	Paving Asphalt			50000 S.F.	\$48,000	1
FN5	Fence-10' Chai			888 L.F.	\$13,600	1
TR2	RestRoom stone			2697 S.F.	\$354,000	1
TR2	RestRoom stone			1875 S.F.	\$246,100	1
FN1	Fence - Chain			4000 L.F.	\$28,600	1
CAN4	Canopy rf/slb			800 S.F.	\$9,600	1
СВЗ	PreCastConcCel			240 S.F.	\$55,400	1
FN1	Fence - Chain			100 L.F.	\$700	1
CB4	PreCastConcCel			360 S.F.	\$74,300	1

Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2015	\$1,646,900	\$685,000	\$2,331,900
2014	\$1,646,900	\$685,000	\$2,331,900
2013	\$1,646,900	\$685,000	\$2,331,900

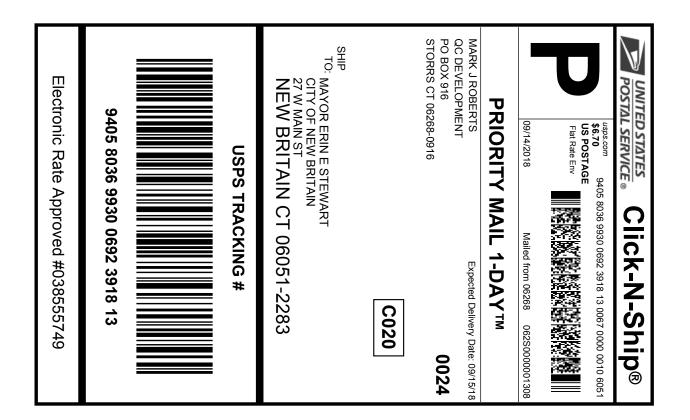
Assessment				
Valuation Year	Improvements	Land	Total	
2015	\$1,152,830	\$479,500	\$1,632,330	
2014	\$1,152,830	\$479,500	\$1,632,330	
2013	\$1,152,830	\$479,500	\$1,632,330	

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- 2. Place your label so it does not wrap around the edge of the package.
- 3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
- 4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
- 5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

USPS TRACKING # / Insurance Number: 9405 8036 9930 0692 3918 13

Trans. #: 443940284 Print Date: 09/12/2018 Ship Date: 09/14/2018 Expected Delivery Date: Insured Value: 09/15/2018 Priority Mail® Postage: Insurance Fee \$0.00 Total \$6.70

From: MARK J ROBERTS

> QC DEVELOPMENT PO BOX 916

\$50.00

STORRS CT 06268-0916

MAYOR ERIN E STEWART

CITY OF NEW BRITAIN

27 W MAIN ST

NEW BRITAIN CT 06051-2283

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