T-Mobile<br>Ryan Clark<br>Real Estate Consultant<br>750 W. Center St, Suite 301<br>W. Bridgewater, MA 02379<br>Phone: (203) 300-7310<br>rclark@clinellc.com

TS-T-MOBILE-086-210921

September 10, 2021

Members of the Connecticut Siting Council
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

## Re: Request for Tower Share <br> T-Mobile Northeast, LLC ("T-Mobile") Request for Approval of the Shared Use of an Existing Tower at 689 Old Colchester Road Uncasville/Montville, CT 06382 T-Mobile site: CTNL024A

## Dear Members of the Council:



T-Mobile proposes to share an existing telecommunications tower located at 689 Old Colchester Road Uncasville/Montville, CT 06382 (the facility). The subject parcel is identified by the Town of Uncasville/Montville, CT as Map 030, Block 089 and lot 00A. The property and tower is owned by Atlantic Broadband (CT), LLC. The property is roughly $8.3 \pm$ acres and accommodates an existing telecommunication compound with five shelters and one concrete pad with telecommunications carriers' cabinets as well as the guyed tower within the fenced compound. The facility is and will continue to be owned and operated by Atlantic Broadband (CT), LLC.

Pursuant to Connecticut General Statues Section 16-50aa (the Statute), T-Mobile requests a finding from the Connecticut Siting Council that the shared use of this facility is technically, legally, environmentally and economically feasible, will meet safety concerns, will avoid the unnecessary proliferation of towers and is in the public interest. It further requests an order approving the shared use of this facility.

The purpose of this request is to use an existing tower to develop T-Mobile's wireless network to provide high speed wireless data and wireless service within the State of Connecticut and in this part of Uncasville/Montville: avoiding the need for an additional tower in Coventry.

T-Mobile is licensed by the Federal Communications Commission ("FCC") to provide multiple technologies, including LTE, NR, 5G and GSM including ( $600,700,1900,2100,2500 \mathrm{MHz}$ frequencies) in New London County. T-Mobile is building and enhancing its network to take advantage of its licensed spectrum, and improve its broadband high speed wireless voice and data services

## Existing Facility \& Proposed Modification

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COMMUNICATIONS

The existing facility is and will continue to be a $370^{\prime}$ guyed tower located at 689 Old Colchester Road Uncasville/Montville, CT 06382. Site coordinates (NAD83) are N 41.45311000 and W 72.15403000. Currently there are two other major commercial wireless carriers located on this tower along with other users, whereby T-Mobile now intends to use the vacant space on the lowest part of the tower, beneath Verizon and AT\&T. The site plan of the facility is included in the proposed Modifications drawings and Construction drawings, prepared by Centerline
Communications dated August 11, 2021 respectively, and enclosed herewith.
T-Mobile intends to install three (3) RFS-APX16DWV-S-E-A20, three (3) RFS-APXVAALL24_43-U-NA20, (3) AIR6449 B41 antennas, three (3) 4460 B25+B66 and three (3) $4480 \mathrm{~B} 71+\mathrm{B} 85$ RRUs, as shown in the construction drawing, to be attached to the guyed tower at the 230 ' mount level. T-Mobile will also install three (3) $6 \times 24$ hybrid fiber cables on the tower. TMobile will add a 15 ' $\times 15$ ' leased area with one (1) concrete pad and one (1) H-frame. T-Mobile intends to enter into a new agreement, at this tower height, in order to license the portion of space within the existing and proposed compound for the new $15^{\prime}-0^{\prime \prime} \times 15^{\prime}-0^{\prime \prime}$ concrete pad with three (3) new cabinets and (1) 35 KW diesel generator.

Consistent with the requirements of the Statute, it is feasible for T-Mobile to collocate at this facility. T-Mobile is proposing to collocate on the existing monopole tower that will continue to remain in the ownership of Atlantic Broadband (CT), LLC. Included with this application is a Structural Analysis Report from Centerline Communications dated August 12, 2021 that shows that the existing tower can support T-Mobile's proposed equipment once modified.

## The Proposal is Legally Feasible.

The Council has authority, pursuant to statute, to issue an order approving of the shared use of this tower. By issuing an order approving T-Mobile's shared use of this tower, T-Mobile will be able to proceed with obtaining a building permit for the proposed installation. Wireless Solutions, LLC has executed a Letter of Authorization that approved T-Mobile's Request for Tower Share filing, which approval is included with this application. T-Mobile's proposal is legally feasible.

T-Mobile is a telecommunication provider licensed by the FCC to provide service in the State of Connecticut, including but not limited to Tolland County. T-Mobile will enter into an agreement with the owner of this facility, Wireless Solutions, LLC, for the location of this proposed equipment on the existing tower so that it may provide telecommunications services to the surrounding community. Consequently, the proposal is legally feasible.

## The Proposal is Environmentally Feasible.

Pursuant to the Statute, the proposal will be environmentally feasible for the following reasons:

- The overall impact on the Uncasville/Montville area will be decreased with the sharing of a single tower versus the proliferation of multiple towers.
- There will be no material increase in the visibility of the tower with the addition of the

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- COMMUNICATIONS
antennas and associated equipment on the tower.
- There will be no increased impact on air quality because no air pollutants will be generated during normal operation of the facility.
- There will only be a brief, slight increase in noise pollution while the site is under construction.
- During construction, the proposed project will generate a small amount of traffic as construction takes place. Upon completion, traffic will be limited to an average of one trip per month for maintenance and inspections.
- There will be no adverse impact to the health and safety of the surrounding community or workers at the facility due to the addition of T-Mobile's new antennas to the tower. TMobile has performed an analysis of the radio frequency field emanating from the transmitting antennas on the tower to ensure compliance with the National Council on Radiation Protection and measurements (NCRP) standard for maximum permissible exposure (MPE) adopted by the FCC. The analysis indicates that T-Mobile and other antennas on the tower will cumulatively emit $.16 \%$ of the NCRP standard for maximum permissible exposure. The report indicates that maximum level of exposure will be well below the FCC's mandated radio frequency exposure limits. The report is enclosed herewith.
- T-Mobile expects to enhance safety in this portion of by improving wireless telecommunications for local residents and travelers. T-Mobile is currently developing its network to provide its customers with quality and reliable coverage to comply with their FCC license, the site is a necessary part of T-Mobile's network development.
- Specifically, this proposal is designed to provide reliable wireless coverage for this section of Coventry.


## Conclusions:

For the reasons stated above, the attachment of T-Mobile's antennas and associated equipment to the tower would meet all the requirements set forth in the Statute. The proposal is legally, technically, economically and environmentally feasible and meets all public safety concerns. Therefore, T-Mobile respectfully requests that the Council approve this request for the shared use of this tower located at 689 Old Colchester Road Uncasville/Montville, CT 06382.

Respectfully yours,

Ryan Clark<br>Real Estate Consultant - Site Acquisition<br>c/o T-Mobile<br>Centerline Communications, LLC<br>750 West Center Street, Floor 3 / Suite 301<br>West Bridgewater, MA 02379<br>Mobile: (203) 300-7310<br>rclark@,clinellc.com

cc: Atlantic Broadband (CT), LLC - property and tower owner Ronald K. McDaniel, chief elected official, Town of Montville Marcia A. Vlaun, Town Planner, Town of Montville.

## Exhibit A

Letter of Authorization

## ATLANTIC ${ }^{\circ}$

broadband
a Cogeco company

## LETTER OF AUTHORIZATION

## SITE No.: CTNL024A

SITE NAME: CTNL024A
ADDRESS: 689 Old Colchester Road Montville, CT

Atlantic Broadband (CT), LLC, owner of the above-described property, hereby authorizes T-Mobile Northeast, LLC ("T-Mobile") and/or their agent, to file any land use or building permit application(s) necessary to obtain approval of the applicable jurisdiction for T-Mobile's installation of the antennas and related telecommunications equipment on the above-described property.

| Sean | Sean Calnan <br> 2021.09.10 <br> Calnan <br> ArLa $14: 14: 01-04^{\prime} 00^{\prime}$ |
| :---: | :---: |

Print Name: Sean Calnan

Title: Director, Carrier Sales

Date: 9/10/2021

## Exhibit B

Original Facility Approval


The Montville Zoning and Planning Cormission at its meeting held on September 19, 1989, took the following action:

APPROVED WITH MDOIFICATION the application of SNET CELUAR, INC. for a zoning pernit to construct a one-story equipment building on property located at Old Colchester Road, Montville, Ct. Shom on Assessor's Map 30, Lot 89 A.

APPROVED THE APPLICATION OF ANDPEN A. MTES to renew a termorary trailer permit on property located at 211 Chapel Hill Road, Montville, Ct. Shown on Assessor's Map 28, Lot 8.

APPROVED WITH CONDITIONS the application of PNUL TINE for a Special Permit to construct a hardware store on property located on Route 32, Montville, Ct. Shown on Assessor's Map 83, Lot 298. Coastạl Site Plan was also approved.

APPROVED WITH CONDITION the application of TIM CONROY for a Special Permit to grade property located at Route 32 Rest Home, Montville, Ct. Shown on Assessor's Map 83, Lot 34. Coastal Site Plan was also approved.

APPROVED AENOMENS TO SUBOIVISION REGUATIONS PREATIVE TO SECTION 4.6 effective 10/7/89, as follows:
4.6 Subsurface Sewage Disposal. Any subdivision or part thereof for which a public sewage disposal system is not available shall submit a plan which carplies with the following requirenents:
4.6.1 Plans must be on a scale no smaller than 1:40.
4.6.2 A minimu of 4 test holes must be dug on each lot, which meet minimum Public Health Code requirements. 2 holes must be located in the proposed primary area, and 2 holes in the proposed reserve area.
4.6.3 2 percolation tests must be perfomed on each lot, one in the proposed primary area, and one in the proposed reserve area, as required by the Public Health Code.
4.6.4 All septic systems must be located a rinimum of $50^{\prime}$ from any watercourse, pond or wetlands.
4.6.5 All drainage, existing and proposed, must be shown in relation to the septic systens.
4.6.6 Any wells and septic systens on adjacent properties must be located on the plan.
4.6.7 All wetlands and watercourse within $50^{\prime}$ of the property must be located on the plan.
4.6.8 Original seal and signature of surveyor and/or engineer must appear on the plan.
4.6.9 All easements and rights of ways are to be shown on the plan
4.6.10 For sites which require an engineered septic system the location of the proposed house or structure and the location of the primary and reserve must be shown.

APPROVED the application of EVE YN \& HENRY W. MLINOWSKY, SR. for a zone change from M to RA-20 on property located at 79 Haley Rd., Montville, Ct. Shown on Assessor's Map 10, Lot 2. Eff. 10/7/89.

APPROVED WITH CONDITIONS the application of PFUL SMITH for a Special Permit for a recreational carpground on property located at 695 Doyle Rd., Montville, Ct. Shown on Assessor's Map 57, Lots 10 and 30A.

APPROVED WITH CONDITIONS the application of SEWOUR NEEMN for a Special Permit to excavate gravel on property located at the intersection of Nobel Hill and Leffingwell Roads, Montville, Ct. Shown on Assessor's Map 61, Lot 4.
denied The Application of rocer \& Lima philuips for a Special Permit to excavate gravel on property located at Map 11, Lot 2A, Route 85, Montville, Ct.

APPROVED WITH MODIFICATION the application of DAVID A. KING for a zoning permit to construct a professional office building on property located at Map 72, Lot 33, Pequat Rd., Nontville, Ct. Shown on Assessor's Map 72, Lot 33.

Maps and documentation concerning the above applications are on file in the office of the Tow Planner
Town Hall Annex, Montville, Ct.
Dated at Montville, Ct. this 20th day of Septenber, 1989.
NONTVILLE ZONING AND PLANNING COMMISSION
Joseph E. Sheffey, Jr., Chaiman
TO BE PUBLISHED IN THE DAY Septeriber $\stackrel{23}{23}, 1989$

# NOTICE OF INTENT TO MODIFY AN EXEMPT TOWER AND ASSOCIATED EQUIPMENT 

Pursuant to Section 16-50i(a) (5) of the Connecticut General Statutes and pursuant to Section 16-50j-73 of the Regulations of Connecticut state Agencies, SNET Cellular, Inc. (SNET) a company which provides cellular radio telecommunications service in the state of Connecticut hereby notifies the Connecticut siting council that it intends to modify an existing telecommunications tower. The site is is located at Old Colchester Road, Montville, Connecticut.

The location will be leased in part from its current owner and operator, Eastern Connecticut Cable Television, Inc. (Owner), and will be used in part as a cell site to provide cellular mobile telecommunications service in New London County. The proposed modification would contain both transmit and receive antennas.

## DISCUSSION

The tower is located on the Owner's Land on Old Colchester Road, Montville. The proposed addition is needed to supply additional channel capacity and improved transmission for cellular service to the Montville area by SNET Cellular, Inc. This cell site has been designed to properly interface with the adjacent cell sites in Waterford and Norwich.

The proposed antenna addition consists of up to six (6) antennas. The antennas to be used will be mounted on brackets at the 225 foot level i of the existing 385 foot guyed community television tower. From the ground the antennas will appear smaller and be difficult to see. The existing tower has various cable television antennas and the cellular antennas of Metro Mobile CTS.

The maxium power density of the cellular facility is set forth below. It has been calculated in Milliwatts per square centimeter.

Location Power Density Power Density
(all existing antennas) (including SNET Antennas)

| Tower Base | 0.0602 | 0.1113 |
| :--- | :--- | :--- |
| Fence | 0.0509 | 0.1110 |
| Nearest Building | 0.0599 | 0.1106 |

This addition does not increase the total power density measured at the tower site boundary to or above 2.933 milliwatts $/ \mathrm{cm} .^{2}$

In 1984 the Connecticut Legislature adopted the safety levels of the American National Standards Institute ("ANSI") in CGS Section 22a-162. The current ANSI power density level standard (for the cellular service band ) for non-ionizing radition is 2.933 milliwatts $/ \mathrm{cm}^{2}$ (See ANSI Standard C95.1-1982). In this case the cellular power density figures are more than twenty-five times less than the applicable standard.
a The levels shown indicated the total power density in milliwatts per sq. cm. from all cellular antennas measured simultaneously.
b The nearest building is the owner's cable television building.

The proposed addition does not constitute a "Modification" of an existing facility as defined in Connecticut General statutes, section 16-50i(d). This is because there is no change in the tower's height. There is no extension of the boundaries of the tower site. There will be no increase in noise levels at the tower's boundary by six decibels or more. The additional SNET antennas will not increase the power density at this site to or above 2.933 milliwatts/cm? This addition will not have a substantially adverse enviromental effect.

For the reasons discussed above, SNET Cellular, Inc. requests the Council to acknowledge that the Notice of modification meets the Council's exemption criteria.
sincerely,

peter J. Tyrrell


# STATE OF CONNECTICUT 

connecticut siting council
136 Main Street, Suite 401
New Britain, Connecticut 06051
Phone: 827-7682
Gloria Dibble Pond
uirperson
CUMMISSIONERS
Energy / Telecommunications
Peter G. Boucher
Leslie Carothers
Hazardous Waste / Low-level
Radioactive Waste
Frederick G. Adams
Lester J. Forst
COUNCIL. MEMBERS
Harry E. Covey
Mortimer A. Gelston
Daniel P. Lynch, Jr.
Paulann H. Sheets
William H. Smith
Colin C. Tait
Joel M. Rinebold
Executive Director
Stanley J. Modzelesky
Executive Assistant

Peter J. Tyrrell
July 11, 1989
Page Two
The Council is pleased to note that the shared use of an existing tower meets the Council's long-term goal and the public interest to avoid proliferation of additional tower structures.

Please notify the Council upon completion of construction.

Very truly yours,
Sharia Dibble Pond ra
Gloria Dibble Pond Chairperson

GDP/JMR/go
3252 E

## Exhibit C

Property Card

## 689 OLD COLCHESTER RD

| Location | 689 OLD COLCHESTER RD | Mblu | $030 / 089 / 00 \mathrm{~A} / /$ |
| ---: | :--- | ---: | :--- |
| Acct\# | Z 20252300 | Owner | ATLANTIC BROADBAND (CT) <br> LLC |
| Assessment | $\$ 545,650$ | Appraisal | $\$ 779,490$ |
| PID | 1790 | Building Count | 1 |

## Current Value

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$661,920 | \$117,570 | \$779,490 |
| Assessment |  |  |  |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$463,350 | \$82,300 | \$545,650 |

## Owner of Record

| Owner | ATLANTIC BROADBAND (CT) LLC | Sale Price | $\$ 777,060$ |
| :--- | :--- | :--- | :--- |
| Co-Owner |  | Certificate |  |
| Address | TWO BATTERYMARCH PARK STE 205 | Book \& Page | $0608 / 0350$ |
|  |  | Sale Date | $08 / 24 / 2015$ |
|  | QUINCY, MA 02169 | Instrument | 03 |

## Ownership History

| Ownership History |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Owner | Sale Price | Certificate | Book \& Page | Instrument | Sale Date |
| ATLANTIC BROADBAND (CT) LLC | \$777,060 |  | 0608/0350 | 03 | 08/24/2015 |
| METROCAST COMMUNICATIONS OF CT LLC | \$660,000 |  | 0497/0220 | 22 | 09/20/2006 |
| EASTERN CONN CABLE TELEVISION INC | \$5,000 | 1 | 0120/0149 |  | 08/16/1973 |

Building Information

Building 1 : Section 1

| Year Built: | 2008 |
| :--- | :--- |
| Living Area: | 1,600 |
| Replacement Cost: | $\$ 349,760$ |


| Building Percent Good: |  |
| :---: | :---: |
| Replacement Cost |  |
| Less Depreciation: | 320 |
|  | Attributes |
| Field | Description |
| STYLE | Telephone Bldg |
| MODEL | Industrial |
| Grade | C |
| Stories: | 1 |
| Occupancy | 1.00 |
| Exterior Wall A | Pre-cast Concr |
| Exterior Wall B |  |
| Roof Structure | Flat |
| Roof Cover | Concrete Tile |
| Interior Wall A | Minimum |
| Interior Wall B |  |
| Interior Floor A | Concrete |
| Interior Floor B |  |
| Heating Fuel | Electric |
| Heating Type | Forced Air |
| AC Type | Central |
| Prim Bldg Use | Industrial Bldg |
| 1st Floor Use: |  |
| Heat/AC | HEAT/AC PKGS |
| Frame Type | REINF. CONCR |
| Baths/Plumbing | AVERAGE |
| Ceiling/Walls | CEIL \& WALLS |
| Rooms/Prtns | AVERAGE |
| Wall Height | 10.00 |
| \% Comn Wall |  |

## Building Photo

- Building Photo
(http://images.vgsi.com/photos2/montvilleCTPhotos//00102154/48.jpg)
Building Layout


| Building Sub-Areas (sq ft) |  |  | Legend |
| :--- | :--- | ---: | ---: |
| Code | Description | Gross <br> Area | Living <br> Area |
| BAS | First Floor | 1,600 | 1,600 |
| CPD | Concrete Pad | 729 | 0 |
|  |  | 2,329 | 1,600 |

## Extra Features

| Extra Features Legend |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Code | Description | Size | Value | Bldg \# |
| SPR3 | Sprinklers- Dry/Chem | 1600.00 S.F. | \$1,850 | 1 |

Land

## Land Use

| Use Code | 4022 | Size (Acres) | 8.3 |
| :--- | :--- | :--- | :--- |
| Description | Industrial Bldg | Frontage |  |
| Zone | R40 | Depth |  |

Size (Acres) 8.3

Depth

| Neighborhood | Assessed Value $\$ 82,300$ |
| :--- | :--- |
| Alt Land Appr No | Appraised Value $\$ 117,570$ |
| Category |  |

## Outbuildings

| Outbuildings | Legend |
| :--- | :--- |
| No Data for Outbuildings |  |

## Valuation History

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$661,920 | \$117,570 | \$779,490 |
| 2015 | \$636,180 | \$140,880 | \$777,060 |
| 2014 | \$636,180 | \$140,880 | \$777,060 |


| Assessment |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
|  | Valuation Year | Improvements | Land |  |  |  |  |
|  |  |  | $\$ 463,350$ | $\$ 82,300$ | Total |  |  |
| 2016 |  | $\$ 445,330$ | $\$ 98,620$ |  |  |  |  |
| 2015 |  | $\$ 445,330$ | $\$ 945,650$ |  |  |  |  |
| 2014 |  |  | $\$ 98,620$ | $\$ 543,950$ |  |  |  |

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## Exhibit D

Construction Drawings




|  |  |  |  |  |  | $\begin{aligned} \\ \hline \end{aligned}$ |  |  |  |  |  |  |  | 4 <br> 2 <br> 2 <br> 2 <br> 2 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


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 GENERAC


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## Exhibit E

Structural Analysis Report

# Structural Analysis Report 

Site ID: CTNL024A
Site Name: CTNL024A
Project Name: Coverage Strategy
Address: 689 Old Colchester Rd
Uncasville, CT 06382

## Client:

Date: 8/12/2021

## Scope of Work:

Centerline Communications was authorized by T-Mobile Northeast LLC to perform an analysis of the existing structure to determine its capacity to support the proposed and existing T-Mobile equipment/appurtenances listed in this report.

Existing \& Proposed Equipment:

| Carrier | Mounting <br> Level (ft) | Center Line Elevation (ft) | Number of Appurtenances | Antenna Manufacturer | Appurtenance Model | Feed Lines (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WGBH | 370.0 | 370.0 | 1 | - | Search Antenna | (1) $7 / 8$ |
| - | 355.0 | 355.0 | 1 | - | 8' Dish | (1) $7 / 8$ |
|  |  | 355.0 | 1 | - | 10'6"x4" Pipe Mount |  |
|  |  | 355.0 | 1 | - | $6^{\prime}$ Side Arm Mount |  |
| - | 350.0 | 350.0 | 1 | - | $20^{\prime} \times 3^{\prime \prime}$ Dia Omni | (2) $7 / 8$ |
|  |  | 350.0 | 1 | - | $6^{\prime} \times 4^{\prime \prime}$ Pipe Mount |  |
| - | 325.0 | 325.0 | 1 | - | $10^{\prime} \times 3^{\prime \prime}$ Dia Omni | (1) 1-5/8 |
|  |  | 325.0 | 1 | - | $3^{\prime}$ Side Arm Mount |  |
| Verizon <br> Wireless | 305.0 | 305.0 | 3 | Antel | QUAD656C0000 Panel Antenna | (12) $1-5 / 8$ <br> (2) $1-5 / 8$ Hybriflex |
|  |  | 305.0 | 6 | Commscope | HBXX-6517DS Panel Antenna |  |
|  |  | 305.0 | 3 | Commscope | LNX-6514DS-T4M Panel Antenna |  |
|  |  | 305.0 | 3 | Alcatel-Lucent | RRH $4 \times 45 / 2 \times 90-A W S$ |  |
|  |  | 305.0 | 3 | Alcatel-Lucent | RRH4×30-B13 |  |
|  |  | 305.0 | 2 | RFS | DB-T1-6Z-8AB-0Z |  |
|  |  | 305.0 | 6 | RFS | FD9R6004/2C-3L |  |
|  |  | 305.0 | 3 | - | $6^{\prime} \times 12^{\prime}$ Boom Gate |  |
| Secret Service | 250.0 | 250.0 | 1 | - | $20^{\prime} \times 3^{\prime \prime}$ Dia Omni |  |
|  |  | 250.0 | 1 | - | $6^{\prime} \times 4^{\prime \prime}$ Pipe Mount |  |
| AT\&T | 242.5 | 242.5 | 3 | Powerwave | 7770.00 Panel Antenna | (12) 1-5/8 <br> (2) Fiber Trunk <br> (6) $D C$ <br> Trunk <br> (3) $0.3^{\prime \prime}$ <br> RET |
|  |  | 242.5 | 2 | CCI | HPA-65R-BUU-H8 Panel Antenna |  |
|  |  | 242.5 | 1 | CCI | HPA-65R-BUU-H6 Panel Antenna |  |
|  |  | 242.5 | 4 | Kathrein | 800-10966 Panel Antenna |  |
|  |  | 242.5 | 2 | Kathrein | $\begin{gathered} \text { 800-10965 Panel } \\ \text { Antenna } \\ \hline \end{gathered}$ |  |
|  |  | 242.5 | 3 | Ericsson | 8843 B2/B66A RRH |  |
|  |  | 242.5 | 3 | Ericsson | 4449 B5/B12 RRH |  |
|  |  | 242.5 | 3 | Ericsson | B14 4478 RRH |  |
|  |  | 242.5 | 6 | Powerwave | LPG21401 TMA |  |
|  |  | 242.5 | 3 | Raycap | DC6-48-60-18-8F Surge <br> Arrestor |  |
|  |  | 242.5 | 3 | - | 12' T-Frame Mount |  |
|  |  | 242.5 | 3 | Site Pro 1 | SFS-H Stabilizer |  |


| T-Mobile | 230.0 | 230.0 | 3 | RFS | APX16DWV-16DWV-S-E-A20 Antenna | (3) $6 \times 24$ Hybrid |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 3 | RFS | APXVAALL24_43-U- <br> NA20 Antenna |  |
|  |  |  | 3 | Ericsson | AIR6449 B41 Antenna |  |
|  |  |  | 3 | Ericsson | 4460 B25+B66 RRH |  |
|  |  |  | 3 | Ericsson | 4489 B71+B85 RRH |  |
|  |  |  | 3 | Site Pro 1 | VFA12-HD Sector Mount |  |
| - | 200.0 | 200.0 | 1 | - | Yagi Antenna | (1) $7 / 8$ |
| - | 180.0 | 180.0 | 4 | - | Yagi Antenna | (1) $7 / 8$ |
|  |  | 180.0 | 2 | - | 5'3"x4" Pipe Mount |  |
| - | 148.0 | 148.0 | 1 | - | Yagi Antenna | (1) $1 / 2$ |
| - | 140.0 | 140.0 | 1 | - | Yagi Antenna | (1) $7 / 8$ |
| - | 125.0 | 125.0 | 1 | - | Yagi Antenna | (1) $1 / 2$ |
| - | 88.0 | 88.0 | 4 | - | X-Style Antenna | (4) $1 / 2$ |
| - | 62.0 | 62.0 | 1 | - | Yagi Antenna | (1) $7 / 8$ |
| - | 40.0 | 40.0 | 1 | - | Yagi Antenna | (1) $7 / 8$ |

Note: Proposed equipment shown in bold.

## Design Criteria:

## Design Codes:

2018 Connecticut State Building Code
2015 International Building Code
ASCE 7-10
TIA-222-G Standards

| Ultimate Design Wind Speed (V ${ }_{\text {utt }}$ ) | 135 mph |
| :--- | :---: |
| Wind Speed with Ice | 50 mph |
| Ice Thickness | 0.75 in. |
| Exposure Category | B |
| Topographic Category | 1 |
| Risk Category | II |
| Site Soil Class (Assumed) | $\mathrm{D}-$ Stiff Soil |
| Seismic Design Category | B |
| Spectral Response Acceleration Parameter at a Short Periods, $\mathrm{S}_{\mathrm{s}}$ | 0.165 g |
| Spectral Response Acceleration Parameter at a Period of 1 Second, $\mathrm{S}_{1}$ | 0.059 g |
| Short Period Site Coefficient, $\mathrm{F}_{\mathrm{a}}$ | 1.60 |
| Long Period Site Coefficient, $\mathrm{F}_{\mathrm{v}}$ | 2.40 |

*Refer to calculations for additional design criteria.

Conclusion:
Section Capacity (Summary)

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & \hline p \\ & l b \end{aligned}$ | $\begin{gathered} \emptyset P_{\text {allow }} \\ l b \end{gathered}$ | \% Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 368.75-362.5 | Leg | $23 / 4$ | 1 | -1648 | 102851 | 1.6 | Pass |
| T2 | 362.5-356.25 | Leg | $23 / 4$ | 13 | -2308 | 102851 | 2.2 | Pass |
| T3 | 356.25-350 | Leg | $23 / 4$ | 27 | -7365 | 102851 | 7.2 | Pass |
| T4 | 350-343.75 | Leg | 3 | 38 | -5644 | 135284 | 4.2 | Pass |
| T5 | 343.75-337.5 | Leg | 3 | 49 | -40355 | 135284 | 29.8 | Pass |
| T6 | 337.5-331.25 | Leg | 3 | 61 | -41273 | 135284 | 30.5 | Pass |
| T7 | 331.25-325 | Leg | 3 | 73 | -42145 | 135284 | 31.2 | Pass |
| T8 | 325-318.75 | Leg | $31 / 4$ | 86 | -44311 | 171629 | 25.8 | Pass |
| T9 | 318.75-312.5 | Leg | $31 / 4$ | 98 | -46133 | 171629 | 26.9 | Pass |
| T10 | 312.5-306.25 | Leg | $31 / 4$ | 110 | -48318 | 171629 | 28.2 | Pass |
| T11 | 306.25-300 | Leg | $31 / 4$ | 122 | -50010 | 171629 | 29.1 | Pass |
| T12 | 300-293.75 | Leg | $31 / 4$ | 134 | -41772 | 171629 | 24.3 | Pass |
| T13 | 293.75-287.5 | Leg | $31 / 4$ | 145 | -87458 | 171629 | 51.0 | Pass |
| T14 | 287.5-281.25 | Leg | $31 / 4$ | 157 | -93175 | 171629 | 54.3 | Pass |
| T15 | 281.25-275 | Leg | $31 / 4$ | 169 | -98618 | 171629 | 57.5 | Pass |
| T16 | 275-268.75 | Leg | $31 / 4$ | 181 | -102881 | 171629 | 59.9 | Pass |
| T17 | 268.75-262.5 | Leg | $31 / 4$ | 193 | -106219 | 171629 | 61.9 | Pass |
| T18 | 262.5-256.25 | Leg | $31 / 4$ | 205 | -108310 | 171629 | 63.1 | Pass |
| T19 | 256.25-250 | Leg | $31 / 4$ | 217 | -110446 | 171629 | 64.4 | Pass |
| T20 | 250-243.75 | Leg | $31 / 4$ | 229 | -110670 | 171629 | 64.5 | Pass |
| T21 | 243.75-237.5 | Leg | $31 / 4$ | 241 | -107859 | 171629 | 62.8 | Pass |
| T22 | 237.5-231.25 | Leg | $31 / 4$ | 253 | -98956 | 171629 | 57.7 | Pass |
| T23 | 231.25-225 | Leg | $31 / 4$ | 266 | -98309 | 171629 | 57.3 | Pass |
| T24 | 225-218.75 | Leg | 3 | 278 | -74499 | 135284 | 55.1 | Pass |
| T25 | 218.75-212.5 | Leg | 3 | 290 | -119480 | 135284 | 88.3 | Pass |
| T26 | 212.5-206.25 | Leg | 3 | 302 | -121146 | 135284 | 89.5 | Pass |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | Leg | 3 | 314 | -123424 | 135284 | 91.2 | Pass |
| T28 | 181.25-175 | Leg | 3 | 353 | -121904 | 200780 | 60.7 | Pass |
| T29 | 175-168.75 | Leg | $31 / 4$ | 368 | -120844 | 171629 | 70.4 | Pass |
| T30 | 168.75-162.5 | Leg | $31 / 4$ | 380 | -119558 | 171629 | 69.7 | Pass |
| T31 | 162.5-156.25 | Leg | $31 / 4$ | 392 | -126905 | 171629 | 73.9 | Pass |
| T32 | 156.25-150 | Leg | $31 / 4$ | 404 | -128316 | 171629 | 74.8 | Pass |
| T33 | 150-125 | Leg | $31 / 4$ | 416 | -130492 | 171629 | 76.0 | Pass |
| T34 | 125-100 | Leg | $31 / 4$ | 454 | -132847 | 171629 | 77.4 | Pass |
| T35 | 100-93.75 | Leg | $31 / 4$ | 493 | -109593 | 171629 | 63.9 | Pass |
| T36 | 93.75-87.5 | Leg | $31 / 4$ | 505 | -141823 | 171629 | 82.6 | Pass |
| T37 | 87.5-81.25 | Leg | $31 / 4$ | 517 | -142184 | 171629 | 82.8 | Pass |
| T38 | 81.25-75 | Leg | $31 / 4$ | 529 | -143347 | 171629 | 83.5 | Pass |
| T39 | 75-50 | Leg | $31 / 4$ | 541 | -148670 | 171629 | 86.6 | Pass |
| T40 | 50-25 | Leg | $31 / 4$ | 580 | -154278 | 171629 | 89.9 | Pass |
| T41 | 25-0 | Leg | $31 / 4$ | 619 | -156670 | 171629 | 91.3 | Pass |
| T1 | 368.75-362.5 | Diagonal | $\begin{gathered} \hline 121 / 2 \times 2 \\ 1 / 2 \times 1 / 4 \\ \hline \end{gathered}$ | 11 | -389 | 23510 | $\begin{gathered} 1.7 \\ 2.4(b) \\ \hline \end{gathered}$ | Pass |
| T2 | 362.5-356.25 | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 20 | -1171 | 102123 | $\begin{gathered} 1.1 \\ 3.7(b) \end{gathered}$ | Pass |
| T3 | 356.25-350 | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 34 | 3108 | 103075 | $\begin{gathered} 3.0 \\ 9.8(b) \\ \hline \end{gathered}$ | Pass |
| T4 | 350-343.75 | Diagonal | L3 $\times 21 / 2 \times 1 / 4$ | 46 | -3341 | 27333 | $\begin{gathered} 12.2 \\ 14.7(b) \end{gathered}$ | Pass |
| T5 | 343.75-337.5 | Diagonal | 5/8 | 55 | 4317 | 9940 | 43.4 | Pass |
| T6 | 337.5-331.25 | Diagonal | 5/8 | 70 | 4109 | 9940 | 41.3 | Pass |
| T7 | 331.25-325 | Diagonal | 5/8 | 82 | 3899 | 9940 | 39.2 | Pass |
| T8 | 325-318.75 | Diagonal | 3/4 | 94 | 4427 | 14314 | 30.9 | Pass |
| T9 | 318.75-312.5 | Diagonal | 3/4 | 106 | 4157 | 14314 | 29.0 | Pass |
| T10 | 312.5-306.25 | Diagonal | 3/4 | 118 | 4423 | 14314 | 30.9 | Pass |
| T11 | 306.25-300 | Diagonal | 3/4 | 132 | 7065 | 14314 | 49.4 | Pass |
| T12 | 300-293.75 | Diagonal | L3x2 1/2x1/4 | 142 | -7478 | 27408 | 27.3 | Pass |


|  |  |  |  |  |  |  | 30.1 (b) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T13 | 293.75-287.5 | Diagonal | 3/4 | 152 | 7436 | 14314 | 52.0 | Pass |
| T14 | 287.5-281.25 | Diagonal | 5/8 | 164 | 6569 | 9940 | 66.1 | Pass |
| T15 | 281.25-275 | Diagonal | 5/8 | 176 | 5816 | 9940 | 58.5 | Pass |
| T16 | 275-268.75 | Diagonal | 5/8 | 188 | 4908 | 9940 | 49.4 | Pass |
| T17 | 268.75-262.5 | Diagonal | 5/8 | 200 | 4057 | 9940 | 40.8 | Pass |
| T18 | 262.5-256.25 | Diagonal | 5/8 | 212 | 3580 | 9940 | 36.0 | Pass |
| T19 | 256.25-250 | Diagonal | 3/4 | 227 | 4259 | 14314 | 29.8 | Pass |
| T20 | 250-243.75 | Diagonal | 3/4 | 239 | 4275 | 14314 | 29.9 | Pass |
| T21 | 243.75-237.5 | Diagonal | 3/4 | 249 | 8591 | 14314 | 60.0 | Pass |
| T22 | 237.5-231.25 | Diagonal | 3/4 | 261 | 10770 | 14314 | 75.2 | Pass |
| T23 | 231.25-225 | Diagonal | 1 | 273 | 15422 | 25447 | $\begin{gathered} 60.6 \\ 97.0(\mathrm{~b}) \end{gathered}$ | Pass |
| T24 | 225-218.75 | Diagonal | $\begin{gathered} \hline \text { L2 } 1 / 2 \times 2 \\ 1 / 2 \times 1 / 4 \\ \hline \end{gathered}$ | 287 | -13948 | 65285 | $\begin{gathered} 21.4 \\ 28.1(\mathrm{~b}) \\ \hline \end{gathered}$ | Pass |
| T25 | 218.75-212.5 | Diagonal | 5/8 | 295 | 5664 | 9940 | 57.0 | Pass |
| T26 | 212.5-206.25 | Diagonal | 5/8 | 307 | 4278 | 9940 | 43.0 | Pass |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | Diagonal | 5/8 | 321 | 6222 | 9940 | 62.6 | Pass |
| T28 | 181.25-175 | Diagonal | 5/8 | 363 | 7038 | 9940 | 70.8 | Pass |
| T29 | 175-168.75 | Diagonal | 1 | 378 | 8623 | 25447 | $\begin{gathered} 33.9 \\ 54.2(\mathrm{~b}) \end{gathered}$ | Pass |
| T30 | 168.75-162.5 | Diagonal | 1 | 385 | 9611 | 25447 | $\begin{gathered} 37.8 \\ 60.4(b) \\ \hline \end{gathered}$ | Pass |
| T31 | 162.5-156.25 | Diagonal | 5/8 | 400 | 3401 | 9940 | 34.2 | Pass |
| T32 | 156.25-150 | Diagonal | 5/8 | 412 | 3004 | 9940 | 30.2 | Pass |
| T33 | 150-125 | Diagonal | 5/8 | 421 | 6901 | 9940 | 69.4 | Pass |
| T34 | 125-100 | Diagonal | $\begin{aligned} & \text { L2 } 1 / 2 \times 2 \\ & 1 / 2 \times 3 / 16 \end{aligned}$ | 460 | 12658 | 24840 | $\begin{gathered} 51.0 \\ 88.1(b) \end{gathered}$ | Pass |
| T35 | 100-93.75 | Diagonal | $\begin{gathered} 2 \mathrm{~L} 21 / 2 \times 2 \\ 1 / 2 \times 1 / 4 \end{gathered}$ | 502 | -15518 | 65385 | $\begin{gathered} 23.7 \\ 31.2(b) \end{gathered}$ | Pass |
| T36 | 93.75-87.5 | Diagonal | 3/4 | 511 | 4334 | 14314 | 30.3 | Pass |
| T37 | 87.5-81.25 | Diagonal | 5/8 | 523 | 2986 | 9940 | 30.0 | Pass |
| T38 | 81.25-75 | Diagonal | 5/8 | 535 | 2143 | 9940 | 21.6 | Pass |
| T39 | 75-50 | Diagonal | 5/8 | 547 | 3511 | 9940 | 35.3 | Pass |
| T40 | 50-25 | Diagonal | 5/8 | 615 | 4654 | 9940 | 46.8 | Pass |
| T41 | 25-0 | Diagonal | 5/8 | 625 | 3743 | 9940 | 37.7 | Pass |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | Horizontal | P1.25x. 14 | 326 | -3563 | 12040 | 29.6 | Pass |
| T33 | 150-125 | Horizontal | P1.25x. 14 | 427 | -4057 | 12102 | 33.5 | Pass |
| T34 | 125-100 | Horizontal | P1.25x. 14 | 466 | -7615 | 12102 | 62.9 | Pass |
| T39 | 75-50 | Horizontal | P1.25x. 14 | 564 | -2575 | 12102 | 21.3 | Pass |
| T40 | 50-25 | Horizontal | P1.25x. 14 | 612 | -2740 | 12102 | 22.6 | Pass |
| T41 | 25-0 | Horizontal | P1.25x. 14 | 633 | -2714 | 12102 | 22.4 | Pass |
| T28 | 181.25-175 | Secondary <br> Horizontal | P1.25x. 14 | 364 | -2111 | 12040 | $\begin{gathered} 17.5 \\ 34.0(\mathrm{~b}) \\ \hline \end{gathered}$ | Pass |
| T1 | 368.75-362.5 | Top Girt | 2L2 1/2×2×1/4 | 4 | 94 | 57257 | 0.3 | Pass |
| T2 | 362.5-356.25 | Top Girt | 2L2 1/2x3×1/4 | 16 | 282 | 75608 | $\begin{gathered} 0.4 \\ 0.9(b) \end{gathered}$ | Pass |
| T3 | 356.25-350 | Top Girt | 2L2 1/2x3×1/4 | 28 | -970 | 65488 | $\begin{gathered} 1.5 \\ 3.0(b) \\ \hline \end{gathered}$ | Pass |
| T4 | 350-343.75 | Top Girt | 2L2 1/2×2×1/4 | 40 | 8437 | 57257 | $\begin{gathered} 14.7 \\ 22.0(b) \\ \hline \end{gathered}$ | Pass |
| T5 | 343.75-337.5 | Top Girt | 2L2 1/2×2×1/4 | 52 | -3850 | 54623 | $\begin{gathered} 7.0 \\ 7.7 \text { (b) } \\ \hline \end{gathered}$ | Pass |
| T6 | 337.5-331.25 | Top Girt | P1.25x. 14 | 65 | -3149 | 12040 | 26.2 | Pass |
| T7 | 331.25-325 | Top Girt | P1.25x. 14 | 77 | -3060 | 12040 | 25.4 | Pass |
| T8 | 325-318.75 | Top Girt | P1.25x. 14 | 89 | -3674 | 12102 | 30.4 | Pass |
| T9 | 318.75-312.5 | Top Girt | P1.25x. 14 | 101 | -4207 | 12102 | 34.8 | Pass |
| T10 | 312.5-306.25 | Top Girt | P1.25x. 14 | 113 | -4313 | 12102 | 35.6 | Pass |
| T11 | 306.25-300 | Top Girt | 2L2 1/2×2×1/4 | 126 | -5825 | 54745 | $\begin{gathered} 10.6 \\ 11.7(b) \end{gathered}$ | Pass |
| T12 | 300-293.75 | Top Girt | 2L2 1/2x2x1/4 | 136 | 10151 | 57257 | $\begin{gathered} 17.7 \\ 26.5(b) \end{gathered}$ | Pass |
| T13 | 293.75-287.5 | Top Girt | 2L2 1/2×2×1/4 | 148 | -2723 | 54745 | 5.0 | Pass |


|  |  |  |  |  |  |  | 5.5 (b) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T14 | 287.5-281.25 | Top Girt | P1.25x. 14 | 160 | -4351 | 12102 | 36.0 | Pass |
| T15 | 281.25-275 | Top Girt | P1.25x. 14 | 172 | -3901 | 12102 | 32.2 | Pass |
| T16 | 275-268.75 | Top Girt | P1.25x. 14 | 184 | -3386 | 12102 | 28.0 | Pass |
| T17 | 268.75-262.5 | Top Girt | P1.25x. 14 | 197 | -3136 | 12102 | 25.9 | Pass |
| T18 | 262.5-256.25 | Top Girt | P1.25x. 14 | 209 | -3125 | 12102 | 25.8 | Pass |
| T19 | 256.25-250 | Top Girt | P1.25x. 14 | 221 | -3852 | 12102 | 31.8 | Pass |
| T20 | 250-243.75 | Top Girt | 2L2 1/2×2×1/4 | 233 | -4708 | 54378 | $\begin{gathered} 8.7 \\ 14.8 \text { (b) } \end{gathered}$ | Pass |
| T21 | 243.75-237.5 | Top Girt | 2L2 1/2×2x1/4 | 245 | -5842 | 54745 | $\begin{gathered} 10.7 \\ 11.8 \text { (b) } \end{gathered}$ | Pass |
| T22 | 237.5-231.25 | Top Girt | 2L2 1/2x2x1/4 | 257 | -6091 | 54745 | $\begin{gathered} 11.1 \\ 12.3(b) \end{gathered}$ | Pass |
| T23 | 231.25-225 | Top Girt | 2L2 1/2×2x1/4 | 269 | -8163 | 54745 | $\begin{gathered} 14.9 \\ 16.4 \text { (b) } \end{gathered}$ | Pass |
| T24 | 225-218.75 | Top Girt | 2L2 1/2x2x1/4 | 280 | 13332 | 57257 | $\begin{gathered} 23.3 \\ 34.8(b) \end{gathered}$ | Pass |
| T25 | 218.75-212.5 | Top Girt | 2L2 1/2×2×1/4 | 292 | 6194 | 57257 | $\begin{gathered} 10.8 \\ 16.2(b) \end{gathered}$ | Pass |
| T26 | 212.5-206.25 | Top Girt | P1.25x. 14 | 304 | -2995 | 12040 | 24.9 | Pass |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | Top Girt | P1.25x. 14 | 317 | -2393 | 12040 | 19.9 | Pass |
| T28 | 181.25-175 | Top Girt | P1.25x. 14 | 356 | -4002 | 12040 | 33.2 | Pass |
| T29 | 175-168.75 | Top Girt | P1.25x. 14 | 372 | -4796 | 12102 | 39.6 | Pass |
| T30 | 168.75-162.5 | Top Girt | P1.25x. 14 | 382 | -5678 | 12102 | 46.9 | Pass |
| T31 | 162.5-156.25 | Top Girt | 2L2 1/2×2×1/4 | 396 | 4944 | 59296 | $\begin{gathered} 8.3 \\ 15.5(b) \\ \hline \end{gathered}$ | Pass |
| T32 | 156.25-150 | Top Girt | P1.25x. 14 | 406 | -2223 | 12102 | 18.4 | Pass |
| T33 | 150-125 | Top Girt | P1.25x. 14 | 418 | -2260 | 12102 | 18.7 | Pass |
| T34 | 125-100 | Top Girt | P1.25x. 14 | 457 | -4962 | 12102 | 41.0 | Pass |
| T35 | 100-93.75 | Top Girt | 2L2 1/2×2×1/4 | 498 | 12915 | 57257 | $\begin{gathered} 22.6 \\ 33.7(b) \end{gathered}$ | Pass |
| T36 | 93.75-87.5 | Top Girt | $2 \mathrm{~L} 21 / 2 \times 2 \times 1 / 4$ | 508 | 8487 | 59296 | $\begin{gathered} 14.3 \\ 26.7(b) \end{gathered}$ | Pass |
| T37 | 87.5-81.25 | Top Girt | P1.25x. 14 | 522 | -2463 | 12102 | 20.3 | Pass |
| T38 | 81.25-75 | Top Girt | P1.25x. 14 | 534 | -2483 | 12102 | 20.5 | Pass |
| T39 | 75-50 | Top Girt | P1.25x. 14 | 546 | -2575 | 12102 | 21.3 | Pass |
| T40 | 50-25 | Top Girt | L2 1/2×2×1/4 | 585 | -2672 | 15544 | $\begin{gathered} 17.2 \\ 19.8(\mathrm{~b}) \end{gathered}$ | Pass |
| T41 | 25-0 | Top Girt | P1.25x. 14 | 624 | -2714 | 12102 | 22.4 | Pass |
| T4 | 350-343.75 | Guy A@350 | 7/8 | 670 | 20577 | 47820 | 43.0 | Pass |
| T12 | 300-293.75 | Guy A@300 | 7/8 | 688 | 23402 | 47820 | 48.9 | Pass |
| T24 | 225-218.75 | Guy A@225 | 3/4 | 706 | 20607 | 34980 | 58.9 | Pass |
| T31 | 162.5-156.25 | Guy A@162.5 | 3/4 | 714 | 19985 | 34980 | 57.1 | Pass |
| T35 | 100-93.75 | Guy A@100 | 9/16 | 728 | 10756 | 21000 | 51.2 | Pass |
| T40 | 50-25 | Guy A@50 | 9/16 | 735 | 9484 | 21000 | 45.2 | Pass |
| T4 | 350-343.75 | Guy B@350 | 7/8 | 665 | 19105 | 47820 | 40.0 | Pass |
| T12 | 300-293.75 | Guy B@300 | 7/8 | 682 | 22135 | 47820 | 46.3 | Pass |
| T24 | 225-218.75 | Guy B@225 | 3/4 | 700 | 21077 | 34980 | 60.3 | Pass |
| T31 | 162.5-156.25 | Guy B@162.5 | 3/4 | 713 | 20629 | 34980 | 59.0 | Pass |
| T35 | 100-93.75 | Guy B@100 | 9/16 | 721 | 11389 | 21000 | 54.2 | Pass |
| T40 | 50-25 | Guy B@50 | 9/16 | 734 | 9361 | 21000 | 44.6 | Pass |
| T4 | 350-343.75 | Guy C@350 | 7/8 | 658 | 19080 | 47820 | 39.9 | Pass |
| T12 | 300-293.75 | Guy C@300 | 7/8 | 677 | 22289 | 47820 | 46.6 | Pass |
| T24 | 225-218.75 | Guy C@225 | 3/4 | 695 | 20691 | 34980 | 59.1 | Pass |
| T31 | 162.5-156.25 | Guy C@162.5 | 3/4 | 712 | 20259 | 34980 | 57.9 | Pass |
| T35 | 100-93.75 | Guy C@100 | 9/16 | 716 | 10823 | 21000 | 51.5 | Pass |
| T40 | 50-25 | Guy C@50 | 9/16 | 733 | 9655 | 21000 | 46.0 | Pass |
| T4 | 350-343.75 | Torque Arm Top@350 | $2 \mathrm{~L} 3 \times 2$ 1/2×1/4 | 660 | 18530 | 85212 | 21.7 | Pass |
| T12 | 300-293.75 | $\begin{gathered} \text { Torque Arm } \\ \text { Top@300 } \\ \hline \end{gathered}$ | 2L3x2 1/2x1/4 | 690 | 20534 | 85212 | 24.1 | Pass |
| T24 | 225-218.75 | Torque Arm Top@225 | $2 \mathrm{~L} 3 \times 2$ 1/2×1/4 | 708 | 19991 | 85212 | 23.5 | Pass |


| T35 | 100-93.75 | Torque Arm Top@100 | 2L3x2 1/2x1/4 | 723 | 12339 | 85212 | 14.5 | Pass |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | 350-343.75 | Torque Arm Bottom@350 | 2L3x2 1/2x1/4 | 675 | -21838 | 46126 | 47.3 | Pass |
| T12 | 300-293.75 | Torque Arm Bottom@300 | 2L3x2 1/2x1/4 | 693 | -25675 | 46226 | 55.5 | Pass |
| T24 | 225-218.75 | Torque Arm Bottom@225 | 2L3x2 1/2x1/4 | 705 | -21487 | 46126 | 46.6 | Pass |
| T35 | 100-93.75 | Torque Arm Bottom@100 | 2L3x2 1/2x1/4 | 725 | -8318 | 46226 | 18.0 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T41) | 91.3 | Pass |
|  |  |  |  |  |  | Diagonal (T23) | 97.0 | Pass |
|  |  |  |  |  |  | Horizontal (T34) | 62.9 | Pass |
|  |  |  |  |  |  | Secondary Horizontal (T28) | 34.0 | Pass |
|  |  |  |  |  |  | Top Girt (T30) | 46.9 | Pass |
|  |  |  |  |  |  | Guy A (T24) | 58.9 | Pass |
|  |  |  |  |  |  | Guy B (T24) | 60.3 | Pass |
|  |  |  |  |  |  | Guy C (T24) | 59.1 | Pass |
|  |  |  |  |  |  | Torque Arm Top (T12) | 24.1 | Pass |
|  |  |  |  |  |  | Torque Arm Bottom (T12) | 55.5 | Pass |
|  |  |  |  |  |  | Bolt Checks | 97.0 | Pass |
|  |  |  |  |  |  | RATING = | 97.0 | Pass |


| Structure Rating (max from all components) $=$ | $\mathbf{9 7 . 0 \%}$ |
| :--- | :--- |

Foundation Capacity (Summary)

| Component | Capacity $\%$ | Pass/Fail |
| :---: | :---: | :---: |
| Base Foundation - Soil Rating | 96.5 | Pass |
| Anchor Block at 114.41 ft. Radius - Soil Rating | 16.1 | Pass |
| Anchor Block at 193.65 ft. Radius - Soil Rating | 31.9 | Pass |
| Anchor Block at 224.79 ft. Radius - Soil Rating | 30.4 | Pass |
| Anchor Block at 247.15 ft. Radius - Soil Rating | 23.4 | Pass |

Foundation Rating (max from all components) $=\quad \mathbf{9 6 . 5 \%}$

## Recommendations:

The existing tower and foundations have adequate capacity to support the existing and proposed loading for the final loading configuration. Modifications to the tower structure are not required.

## Reference Documents:

- T-Mobile RFDS CTNLO24A_Coverage Strategy_1, dated June 16, 2021
- Site Photos and Notes by Centerline Communications, dated May 20, 2021
- Structural Analysis by Centek Engineering, dated March 6, 2019
- Construction Drawings by SAI Communications, dated February 11, 2019
- Mount Analysis by SAI Communications, dated December 18, 2018


## Assumptions and Limitations:

- The tower and structures were built and maintained with the manufacturer's specifications.
- The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in this report and the referenced drawings.

Design Calculations

Address:
689 Old Colchester Rd Uncasville, Connecticut 06382

## ASCE 7 Hazards Report

Standard: ASCE/SEI 7-10 Elevation: 449.23 ft (NAVD 88)<br>Risk Category: ॥ Soil Class: D - Stiff Soil<br>Latitude: 41.452616<br>Longitude: -72.155704



## Wind

## Results:

| Wind Speed: | 132 Vmph |
| :--- | :--- |
| 10-year MRI | 79 Vmph |
| 25 -year MRI | 89 Vmph |
| 50 -year MRI | 98 Vmph |
| 100 -year MRI | 108 Vmph |

## Date Socessed:

ACEAK日U200, 1Fig. 26.5-1A and Figs. CC-1-CC-4, and Section 26.5.2, incorporating errata of March 12, 2014
Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Seismic

## Site Soil Class: <br> D - Stiff Soil

## Results:

| $\mathrm{S}_{\mathrm{s}}:$ | 0.166 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.06 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{v}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.266 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.143 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.177 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.095 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.083 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.133 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category

B



Data Accessed:
Date Source:

Tue Aug 032021
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2.
Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

Ice

## Results:

| Ice Thickness: | 0.75 in. |
| :--- | :--- |
| Concurrent Temperature: | 15 F |
| Gust Speed: | 50 mph |
| Source: | Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8 |
| e Accessed: | Tue Aug 03 2021 |

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

## Snow

## Results:

Ground Snow Load, $\mathrm{p}_{\mathrm{g}}$ :
$30 \mathrm{lb} / \mathrm{ft}^{2}$
Elevation:
Data Source:
Date Accessed:
449.2 ft

ASCE/SEI 7-10, Fig. 7-1.
Tue Aug 032021
Values provided are ground snow loads. In areas designated "case study required," extreme local variations in ground snow loads preclude mapping at this scale. Site-specific case studies are required to establish ground snow loads at elevations not covered.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.



PLAN

SYMBOL LIST

| MARK |  | SIZE | MARK |  | SIZE |
| :---: | :--- | :---: | :--- | :--- | :--- |
| A | L2 $1 / 2 \times 21 / 2 \times 1 / 4$ | F | $2 \mathrm{~L} 21 / 2 \times 21 / 2 \times 1 / 4$ |  |  |
| B | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | G | $\mathrm{L} 21 / 2 \times 21 / 2 \times 3 / 16$ |  |  |
| C | $\mathrm{L} 3 \times 21 / 2 \times 1 / 4$ | H | $2 \mathrm{~L} 21 / 2 \times 2 \times 1 / 4$ |  |  |
| D | SR $3 / 4$ | I | $2 \mathrm{~L} 21 / 2 \times 3 \times 1 / 4$ |  |  |
| E | SR 1 |  | J | $\mathrm{P} 1.25 \times .14$ |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :--- | :--- | :--- | :--- | :--- | :--- |
| A36 | 36 ksi |  | 58 ksi |  |  |

TOWER DESIGN NOTES

1. Tower is located in New London County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 105 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $97 \%$

| Centerline Communications | lob: | CTNLO24A |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- |
| 750 West Center Street, Suite 301 | Project: ANCHOR |  |  |  |  |
| West Bridgewater, MA 02379 | Client: T-MOBILE | Drawn by: Arielle Novak | App'd: |  |  |
| Phone: $7811-713-4725$ | Code: | TIA-222-G | Date: 08/12/21 | Scale: |  |
| FAX: | Pat: |  |  |  | Dwg No. |



| DESIGNED APPURTENANCE LOADING |  |  |  |
| :---: | :---: | :---: | :---: |
| TYPE | ELEVATION | TYPE | ELEVATION |
| Search Antenna | 370 | Site Pro Horizontal Stabilizer SFS-H | 242.5 |
| $10^{\prime} 6{ }^{\prime \prime} \times 4$ ' Pipe Mount | 355 | 7770.00 | 242.5 |
| Rohn 6' Side-Arm | 355 | HPA-65R-BUU-H6 | 242.5 |
| 8' Dish | 355 | HPA-65R-BUU-H8 | 242.5 |
| $6^{\prime} \times 4^{\prime \prime}$ Pipe Mount | 350 | HPA-65R-BUU-H8 | 242.5 |
| $20^{\prime} \times 3^{\prime \prime}$ Dia Omni | 350 | 80010965 | 242.5 |
| ROHN 3-ft Side Arm | 325 | 80010966 | 242.5 |
| $10^{\prime} \times 3^{\prime \prime}$ Dia Omni | 325 | 80010966 | 242.5 |
| QUAD656C0000 | 305 | 80010965 | 242.5 |
| HBXX-6517DS | 305 | 80010966 | 242.5 |
| LNX-6514DS-T4M | 305 | 80010966 | 242.5 |
| HBXX-6517DS | 305 | 7770.00 | 242.5 |
| QUAD656C0000 | 305 | 7770.00 | 242.5 |
| HBXX-6517DS | 305 | (2) LPG21401 TMA | 242.5 |
| LNX-6514DS-T4M | 305 | APX16DWV-16DWV-S-E-A20 | 230 |
| HBXX-6517DS | 305 | (T-MOBILE) |  |
| QUAD656C0000 | 305 | APX16DWV-16DWV-S-E-A20 | 230 |
| HBXX-6517DS | 305 | (T-MOBILE) |  |
| LNX-6514DS-T4M | 305 | APX16DWV-16DWV-S-E-A20 (T-MOBILE) | 230 |
| HBXX-6517DS | 305 | APXVAALL24 43-U-NA20 (T-MOBILE) | 230 |
| RRH4×45/2x90-AWS | 305 | APXVAALL24 43-U-NA20 (T-MOBILE) | 230 |
| RRH4 $4 \times 45 / 2 \times 90-A W S$ | 305 | APXVAALL24_43-U-NA20 (T-MOBILE) | 230 |
| RRH4×45/2x90-AWS | 305 | AIR 6449 B41 (T-MOBILE) | 230 |
| RRH4×30-B13 | 305 | AIR 6449 B41 (T-MOBILE) | 230 |
| RRH4×30-B13 | 305 | AIR 6449 B41 (T-MOBILE) | 230 |
| RRH4×30-B13 | 305 | RADIO 4460 B25_B66 (T-MOBILE) | 230 |
| DB-T1-6Z-8AB-0Z | 305 | RADIO 4460 B25_B66 (T-MOBILE) | 230 |
| DB-T1-6Z-8AB-0Z | 305 | RADIO 4460 B25_B66 (T-MOBILE) | 230 |
| Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate | 305 | RADIO 4480 B71+B85 (T-MOBILE) | 230 |
| Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate | 305 | RADIO 4480 B71+B85 (T-MOBILE) | 230 |
| Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate | 305 | RADIO 4480 B71+B85 (T-MOBILE) | 230 |
| $6^{\prime} \times 4^{\prime \prime}$ Pipe Mount $20^{\prime} \times 3^{\prime \prime}$ Dia Omni | 250 | Site Pro 1 VFA12-HD (T-MOBILE) | 230 |
| $20^{\circ} \times 3^{\prime \prime}$ Dia Omni | 250 | Site Pro 1 VFA12-HD (T-MOBILE) | 230 |
| (2) LPG21401 TMA | 242.5 | Site Pro 1 VFA12-HD (T-MOBILE) | 230 |
| (2) LPG21401 TMA | 242.5 | (4) $7^{\prime} \times 22^{\prime \prime}$ Antenna Mount Pipe | 230 |
| 8843 B2/B66A | 242.5 | (T-MOBILE) | 230 |
| 8843 B2/B66A | 242.5 | (4) $7^{\prime} \times 2^{\prime \prime}$ Antenna Mount Pipe | 230 |
| 8843 B2/B66A | 242.5 | (T-MOBILE) |  |
| 4449 B5/B12 | 242.5 | (4) 7 ' $\times 2^{\prime \prime}$ Antenna Mount Pipe | 230 |
| 4449 B5/B12 | 242.5 | (T-MOBILE) |  |
| 4449 B5/B12 | 242.5 | Yagi | 200 |
| B14 4478 | 242.5 | (4) Yagi | 180 |
| B14 4478 | 242.5 | (2) $5^{\prime} 3^{\prime \prime} \times 4^{\prime \prime}$ Pipe Mount | 180 |
| B14 4478 | 242.5 | Yagi | 148 |
| DC6-48-60-18-8F Surge Arrestor | 242.5 | Yagi | 140 |
| DC6-48-60-18-8F Surge Arrestor | 242.5 | Yagi | 125 |
| DC6-48-60-18-8F Surge Arrestor | 242.5 | $X$-Style | 88 |
| Pirod 12' T-Frame Sector Mount | 242.5 | (2) X-Style | 88 |
| Pirod 12' T-Frame Sector Mount | 242.5 | X-Style | 88 |
| Pirod 12' T-Frame Sector Mount | 242.5 | Yagi | 62 |
| Site Pro Horizontal Stabilizer SFS-H | 242.5 | Yagi | 40 |
| Site Pro Horizontal Stabilizer SFS-H | 242.5 |  |  |

SYMBOL LIST

| SYMBOL LIST |  |  |  |
| :---: | :---: | :---: | :---: |
| MARK | SIZE | MARK | SIZE |
| A | L2 1/2x2 1/2×1/4 | F | 2 L2 1/2×2 1/2×1/4 |
| B | $213 \times 3 \times 5 / 16$ | G | L2 1/2x2 1/2×3/16 |
| c | L3×2 1/2x1/4 | H | 2 L 1/2×2×1/4 |
| D | SR 3/4 | 1 | $2 \mathrm{~L} 21 / 2 \times 3 \times 1 / 4$ |
| E | SR 1 | J | P1.25x. 14 |

MATERIAL STRENGTH
GRADE $\qquad$ Fy $\qquad$ Fu GRADE $\qquad$ Fy $\qquad$ Fu

| Centerline Communications | ${ }^{\text {Lob }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Project: ANCHOR |  |  |
| West Bridgewater, MA 02379 | Client T-MOBILE | Drawn by: Arielle Novak | App |
| Phone: 781-713-4725 | Code: TIA-222-G | Date: 08/12/21 | Scale: |
| FAX: | Path: |  | Dwg No. |

TIA-222-G - $105 \mathrm{mph} / 50 \mathrm{mph} 0.7500$ in Ice Exposure B


| Centerline Communications | ${ }^{\text {1ob }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Priject ANCHOR |  |  |
| West Bridgewater, MA 02379 | Client t-MOBILE | Orawn by Arielle Novak | Appid |
| Phone: 781-713-4725 | Code: TIA-222-G | Dale 08/12/21 | Scale: N |
| FAX: | Path: |  | Dwg No. |



| Centerline Commmnications | ${ }^{\text {Pob: }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Project: $A N C H O R$ |  |  |
| West Bridgewater, MA 02379 | Client T-MOBILE | Drawn by: Arielle Novak | App'd: |
| Phone: 781-713-4725 | Code: TIA-222-G | Date: 08/12/21 | Scale: $\Lambda$ |
| FAX: | Path: |  | Dwg No. |



| Centerline Communications | ${ }^{\text {Iob }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Project ANCHOR |  |  |
| West Bridgewater, MA 02379 | ${ }^{\text {Client }}$ T-MOBILE | Drawn by Arielle Novak | Appód. |
| Phone: 781-713-4725 | Code: TIA-222-G | Dale: 08/12/21 | Scale: |
| FAX: | Path: |  | Dwg No. |



| Centerline Comimunications | Pob: CTNLO24A |  |  |  |
| :---: | :--- | :--- | :--- | :--- |
| 750 West Center Street, Suite 301 | Project: ANCHOR |  |  |  |
| West Bridgewater, MA 02379 | Client: T-MOBILE | Drawn by: Arielle Novak | App'd: |  |
| Phone: $781-713-4725$ | Code: | TIA-222-G | Date: $08 / 12 / 21$ | Scale: $\wedge$ |
| FAX: | Path: |  |  |  |


(3) $6 \times 24$ HYBRID (T-MOBILF)


| Centerline Communications | ${ }^{\text {Lob: }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Project: ANCHOR |  |  |
| West Bridgewater, MA 02379 | ${ }^{\text {Client: }}$ T-MOBILE | Drawn by: Arielle Novak | App'd |
| Phone: 781-713-4725 | Code: TIA-222-G | Date: 08/12/21 | Scale: $\Lambda$ |
| FAX: | Path: |  | Owg No. |

Face A


Face B


Face C

## 

| Centerline Communications | ${ }^{\text {ob: }}$ CTNLO24A |  |  |
| :---: | :---: | :---: | :---: |
| 750 West Center Street, Suite 301 | Project ANCHOR |  |  |
| West Bridgewater, MA 02379 | Client T-MOBILE | Drawn by: Arielle Novak | ppid: |
| Phone: 781-713-4725 | Code: TIA-222-G | Date 08/12/21 | Scale: $\wedge$ |
| FAX: | Path: |  | Dwg No. |

Wind Pressures and Ice Thickness
TIA-222-G - $105 \mathrm{mph} / 50 \mathrm{mph} 0.7500$ in Ice Exposure B


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{array}{ll} \hline \text { Page } & \\ & 1 \text { of } 69 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

## Tower Input Data

The main tower is a $3 x$ guyed tower with an overall height of 368.75 ft above the ground line.
The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 5.00 ft at the top and 5.00 ft at the base.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in New London County, Connecticut.
ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
Basic wind speed of 105 mph .
Structure Class II.
Exposure Category B.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 0.7500 in .
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
Tension only take-up is 0.0313 in .
Pressures are calculated at each section.
Stress ratio used in tower member design is 1 .
Safety factor used in guy design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
$\checkmark$ Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
$\sqrt{ }$ Include Bolts In Member Capacity
$\sqrt{ }$ Leg Bolts Are At Top Of Section
$\sqrt{ }$ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided)
SR Members Have Cut Ends
SR Members Are Concentric

Distribute Leg Loads As Uniform
Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r
$\sqrt{ }$ Retension Guys To Initial Tension Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
$\sqrt{ }$ Autocalc Torque Arm Areas Add IBC .6D+W Combination
$\sqrt{ }$ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
$\sqrt{ }$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA
$\sqrt{ }$ SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\sqrt{ }$ Consider Feed Line Torque
$\sqrt{ }$ Include Angle Block Shear Check
Use TIA-222-G Bracing Resist. Exemption
Use TIA-222-G Tension Splice Exemption Poles
Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & \\ & 2 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |



Corner \& Starmount Guyed Tower

| tnxTMOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
|  | Croject | Client | ANCHOR |



Face Guyed

Tower Section Geometry

| Tower Section | Tower Elevation | Assembly Database | Description | Section Width | Number of Sections | Section Length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  |  | $f t$ |  | $f t$ |
| TI | 368.75-362.50 |  |  | 5.00 | 1 | 6.25 |
| T2 | 362.50-356.25 |  |  | 5.00 | 1 | 6.25 |
| T3 | 356.25-350.00 |  |  | 5.00 | 1 | 6.25 |
| T4 | 350.00-343.75 |  |  | 5.00 | 1 | 6.25 |
| T5 | 343.75-337.50 |  |  | 5.00 | 1 | 6.25 |
| T6 | 337.50-331.25 |  |  | 5.00 | 1 | 6.25 |
| T7 | 331.25-325.00 |  |  | 5.00 | 1 | 6.25 |
| T8 | 325.00-318.75 |  |  | 5.00 | 1 | 6.25 |
| T9 | 318.75-312.50 |  |  | 5.00 | 1 | 6.25 |
| T10 | 312.50-306.25 |  |  | 5.00 | I | 6.25 |
| T11 | 306.25-300.00 |  |  | 5.00 | 1 | 6.25 |
| T12 | 300.00-293.75 |  |  | 5.00 | 1 | 6.25 |
| T13 | 293.75-287.50 |  |  | 5.00 | 1 | 6.25 |
| T14 | 287.50-281.25 |  |  | 5.00 | 1 | 6.25 |
| T15 | 281.25-275.00 |  |  | 5.00 | 1 | 6.25 |
| T16 | 275.00-268.75 |  |  | 5.00 | 1 | 6.25 |


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| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower | Tower |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Assembly <br> Database | Description |  |
|  | ft | Section <br> Width | Number <br> of | Section <br> Length |
| T17 | $268.75-262.50$ |  | $5 t$ | Sections |

## Tower Section Geometry (cont'd)

| Tower Section | Tower Elevation $f t$ | Diagonal Spacing $\qquad$ | Bracing Type | $\begin{gathered} \text { Has } \\ \text { K Brace } \\ \text { End } \\ \text { Panels } \\ \hline \end{gathered}$ | Has <br> Horizontals | Top Girt Offset in | Bottom Girt Offset $\qquad$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 368.75-362.50 | 6.25 | X Brace | No | No | 0.0000 | 0.0000 |
| T2 | 362.50-356.25 | 6.25 | X Brace | No | No | 0.0000 | 0.0000 |
| T3 | 356.25-350.00 | 6.25 | X Brace | No | No | 0.0000 | 0.0000 |
| T4 | 350.00-343.75 | 6.25 | X Brace | No | Yes | 0.0000 | 0.0000 |
| T5 | 343.75-337.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T6 | 337.50-331.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T7 | 331.25-325.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T8 | 325.00-318.75 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T9 | 318.75-312.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T10 | 312.50-306.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| TII | 306.25-300.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T12 | 300.00-293.75 | 6.25 | X Brace | No | Yes | 0.0000 | 0.0000 |
| T13 | 293.75-287.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T14 | 287.50-281.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T15 | 281.25-275.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T16 | 275.00-268.75 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T17 | 268.75-262.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T18 | 262.50-256.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T19 | 256.25-250.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T20 | 250.00-243.75 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T21 | 243.75-237.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T22 | 237.50-231.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T23 | 231.25-225.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & \\ & 5 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Section | Tower Elevation $f t$ | Diagonal Spacing $f t$ | Bracing Type | Has K Brace End Panels | Has <br> Horizontals | Top Girt Offset in | Bottom Girt Offset in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T24 | 225.00-218.75 | 6.25 | X Brace | No | Yes | 0.0000 | 0.0000 |
| T25 | 218.75-212.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T26 | 212.50-206.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T27 | 206.25-181.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T28 | 181.25-175.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T29 | 175.00-168.75 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T30 | 168.75-162.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T31 | 162.50-156.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T32 | 156.25-150.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T33 | 150.00-125.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T34 | 125.00-100.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T35 | 100.00-93.75 | 6.25 | X Brace | No | Yes | 0.0000 | 0.0000 |
| T36 | 93.75-87.50 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T37 | 87.50-81.25 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T38 | 81.25-75.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T39 | 75.00-50.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T40 | 50.00-25.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |
| T41 | 25.00-0.00 | 6.25 | TX Brace | No | Yes | 0.0000 | 0.0000 |

## Tower Section Geometry (cont'd)

| Tower Elevation $f t$ | Leg <br> Type | Leg <br> Size | Leg Grade | Diagonal Type | Diagonal Size | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 368.75-362.50 | Solid Round | $23 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Single Angle | L2 1/2x2 1/2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T2 362.50-356.25 | Solid Round | $23 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T3 356.25-350.00 | Solid Round | $23 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T4 350.00-343.75 | Solid Round | 3 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Single Angle | L3x2 1/2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T5 343.75-337.50 | Solid Round | 3 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T6 337.50-331.25 | Solid Round | 3 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T7 331.25-325.00 | Solid Round | 3 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T8 325.00-318.75 | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 3/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T9 318.75-312.50 | Solid Round | $31 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 3/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T10 } \\ 312.50-306.25 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 3/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T11 } \\ 306.25-300.00 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 3/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T12 } \\ 300.00-293.75 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Single Angle | L3x2 1/2xI/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \mathrm{T} 13 \\ 293.75-287.50 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 3/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T14 } \\ 287.50-281.25 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T15 } \\ 281.25-275.00 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T16 } \\ 275.00-268.75 \end{gathered}$ | Solid Round | $31 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Solid Round | 5/8 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T17 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & \\ & 6 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Elevation <br> ft | Leg <br> Type | Leg Size | Leg Grade | Diagonal Type | Diagonal Size | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 268.75-262.50 | Solid Round | $31 / 4$ | (36 ksi) | Solid Round | 5/8 | (36 ksi) |
| T18 |  |  | A36 |  |  | A36 |
| 262.50-256.25 |  |  | ( 36 ksi ) |  |  | (36 ksi) |
| T19 | Solid Round | $31 / 4$ | A36 | Solid Round | 3/4 | A36 |
| 256.25-250.00 | Solid Round | $31 / 4$ | ( 36 ksi ) | Solid Round | 3/4 | (36 ksi) |
| T20 |  |  | A36 |  |  | A36 |
| 250.00-243.75 |  |  | (36 ksi) |  |  | (36 ksi) |
| T21 | Solid Round | $31 / 4$ | A36 | Solid Round | 3/4 | A36 |
| 243.75-237.50 |  |  | (36 ksi) |  |  | (36 ksi) |
| T22 | Solid Round | $31 / 4$ | A36 | Solid Round | 3/4 | A36 |
| 237.50-231.25 |  |  | (36 ksi) |  |  | (36 ksi) |
| T23 | Solid Round | $31 / 4$ | A36 | Solid Round | 1 | A36 |
| 231.25-225.00 |  |  | (36 ksi) |  |  | (36 ksi) |
| T24 | Solid Round | 3 | A36 | Double Angle | $2 \mathrm{~L} 21 / 2 \times 21 / 2 \times 1 / 4$ | A36 |
| 225.00-218.75 |  |  | (36 ksi) |  |  | (36 ksi) |
| T25 | Solid Round | 3 | A36 | Solid Round | 5/8 | A36 |
| 218.75-212.50 |  |  | (36 ksi) |  |  | (36 ksi) |
| T26 | Solid Round | 3 | A36 | Solid Round | 5/8 | A36 |
| 212.50-206.25 |  |  | (36 ksi) |  |  | (36 ksi) |
| T27 | Solid Round | 3 | A36 | Solid Round | 5/8 | A36 |
| 206.25-181.25 |  |  | (36 ksi) |  |  | (36 ksi) |
| T28 | Solid Round | 3 | A36 | Solid Round | 5/8 | A36 |
| 181.25-175.00 |  |  | (36 ksi) |  |  | (36 ksi) |
| T29 | Solid Round | $31 / 4$ | A36 | Solid Round | 1 | A36 |
| 175.00-168.75 |  |  | (36 ksi) |  |  | (36 ksi) |
| T30 | Solid Round | $31 / 4$ | A36 | Solid Round | 1 | A36 |
| 168.75-162.50 |  |  | (36 ksi) |  |  | (36 ksi) |
| T31 | Solid Round | $31 / 4$ |  | Solid Round | 5/8 | A36 |
| $162.50-156.25$ |  |  | (36 ksi) |  |  | (36 ksi) |
| T32 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
| $156.25-150.00$ |  |  | (36 ksi) |  |  | (36 ksi) |
| T33 $150.00-125.00$ | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
| 150.00-125.00 |  |  | (36 ksi) |  |  | (36 ksi) |
| T34 | Solid Round | $31 / 4$ | A36 | Single Angle | L2 $1 / 2 \times 21 / 2 \times 3 / 16$ | A36 |
| 125.00-100.00 |  |  | (36 ksi) |  |  | (36 ksi) |
| T35 100.00-93.75 | Solid Round | $31 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | 2L2 1/2x2 1/2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T36 93.75-87.50 | Solid Round | $31 / 4$ | A36 | Solid Round | 3/4 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T37 87.50-81.25 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T38 81.25-75.00 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T39 75.00-50.00 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T40 50.00-25.00 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T41 25.00-0.00 | Solid Round | $31 / 4$ | A36 | Solid Round | 5/8 | A36 |
|  |  |  | (36 ksi) |  |  | (36 ksi) |

Tower Section Geometry (cont'd)

| Tower <br> Elevation <br> $f t$ | Top Girt <br> Type |  | Top Girt <br> Size | Top Girt <br> Grade | Bottom Girt <br> Type | Bottom Girt <br> Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 $368.75-362.50$ | Double Angle | $2 \mathrm{~L} 21 / 2 \times 2 \times 1 / 4$ | A36 | Flat Bar | Bottom Girt <br> Grade |  |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | CTNL024A |  | $\text { Page } 7 \text { of } 69$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \\ \hline \end{array}$ |
| $\begin{aligned} & \text { West Bridgevater, MA } 02379 \\ & \text { Phone: } 71-1113-4725 \\ & \text { FAX: } \end{aligned}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Elevation $\qquad$ | Top Girt Type | Top Girt Size | Top Girt Grade | Bottom Girt Type | Bottom Girt Size | Bottom Girt Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (36 ksi) |  |  | (36 ksi) |
| T2 362.50-356.25 | Double Angle | 2L2 1/2×3x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T3 356.25-350.00 | Double Angle | 2L2 $1 / 2 \times 3 \times 1 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T4 350.00-343.75 | Double Angle | 2L2 $1 / 2 \times 2 \times 1 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T5 343.75-337.50 | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T6 337.50-331.25 | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T7 331.25-325.00 | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T8 325.00-318.75 | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T9 318.75-312.50 | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \mathrm{T} 10 \\ 312.50-306.25 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T11 } \\ 306.25-300.00 \end{gathered}$ | Double Angle | 2L2 $1 / 2 \times 2 \times 1 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T12 } \\ 300.00-293.75 \end{gathered}$ | Double Angle | 2L2 $1 / 2 \times 2 \times 1 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T13 } \\ 293.75-287.50 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T14 } \\ 287.50-281.25 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T15 } \\ 281.25-275.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T16 } \\ 275.00-268.75 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T17 } \\ 268.75-262.50 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T18 } \\ 262.50-256.25 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T19 } \\ 256.25-250.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T20 } \\ 250.00-243.75 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T21 } \\ 243.75-237.50 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \mathrm{T} 22 \\ 237.50-231.25 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \mathrm{T} 23 \\ 231.25-225.00 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T24 } \\ 225.00-218.75 \end{gathered}$ | Double Angle | 2L2 1/2×2×1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T25 } \\ 218.75-212.50 \end{gathered}$ | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T26 } \\ 212.50-206.25 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T27 } \\ 206.25-181.25 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T28 } \\ 181.25-175.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T29 } \\ 175.00-168.75 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T30 } \\ 168.75-162.50 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T31 } \\ 162.50-156.25 \end{gathered}$ | Double Angle | 2L2 $1 / 2 \times 2 \times 1 / 4$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 | Job CTNL024A |  | Page 8 of 69 |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
| West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Elevation $\qquad$ | Top Girt Type | Top Girt Size | Top Girt Grade | Bottom Girt Type | Bottom Girt Size | Bottom Girt Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T32 } \\ 156.25-150.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T33 } \\ 150.00-125.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T34 } \\ 125.00-100.00 \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T35 100.00-93.75 | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T36 93.75-87.50 | Double Angle | 2L2 1/2x2x1/4 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T37 87.50-81.25 | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T38 81.25-75.00 | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T39 75.00-50.00 | Pipe | P1.25x. 14 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T40 50.00-25.00 | Single Angle | L2 $1 / 2 \times 2 \mathrm{xl} / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T41 25.00-0.00 | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \\ \hline \end{gathered}$ | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \\ \hline \end{gathered}$ |

Tower Section Geometry (cont'd)

| Tower Elevation $\qquad$ | No. of Mid Girts | Mid Girt Type | Mid Girt Size | Mid Girt Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 350.00-343.75 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T5 343.75-337.50 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T6 337.50-331.25 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T7 331.25-325.00 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T8 325.00-318.75 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T9 318.75-312.50 | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T10 } \\ 312.50-306.25 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T11 } \\ 306.25-300.00 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T12 } \\ 300.00-293.75 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T13 } \\ 293.75-287.50 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T14 } \\ 287.50-281.25 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T15 } \\ 281.25-275.00 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T16 } \\ 275.00-268.75 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x. 14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T17 } \\ 268.75-262.50 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | P1.25x.14 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T18 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |


| tnxTower | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | Date $14: 28: 2008 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation <br> ft | No. of Mid Girts | Mid Girt Type | Mid Girt Size | Mid Girt Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 262.50-256.25 | None | Flat Bar |  | (36 ksi) | Pipe | P1.25x. 14 | (36 ksi) |
| T19 |  |  |  | A36 |  |  | A36 |
| 256.25-250.00 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T20 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 250.00-243.75 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T21 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 243.75-237.50 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T22 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 237.50-231.25 |  |  |  | $(36 \mathrm{ksi})$ |  |  | (36 ksi) |
| T23 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 231.25-225.00 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T24 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 225.00-218.75 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T25 | None | Flat Bar |  | A36 | Pipe | P1.25x.14 | A36 |
| 218.75-212.50 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T26 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 212.50-206.25 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| $\mathrm{T} 27$ | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 206.25-181.25 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T28 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 181.25-175.00 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T29 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 175.00-168.75 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T30 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 168.75-162.50 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T31 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 162.50-156.25 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T32 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| $156.25-150.00$ |  |  |  | $(36 \mathrm{ksi})$ |  |  | (36 ksi) |
| T33 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 150.00-125.00 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T34 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
| 125.00-100.00 |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T35 100.00-93.75 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | $(36 \mathrm{ksi})$ |  |  | (36 ksi) |
| T36 93.75-87.50 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T37 87.50-81.25 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T38 81.25-75.00 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T39 75.00-50.00 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T40 50.00-25.00 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | A36 |
|  |  |  |  | (36 ksi) |  |  | (36 ksi) |
| T41 25.00-0.00 | None | Flat Bar |  | A36 | Pipe | P1.25x. 14 | $\mathrm{A} 36$ |
|  |  |  |  | $(36 \mathrm{ksi})$ |  |  | $(36 \mathrm{ksi})$ |

## Tower Section Geometry (cont'd)

| Tower <br> Elevation | Secondary <br> Horizontal Type | Secondary Horizontal <br> Size | Secondary <br> Horizontal <br> Grade | Inner Bracing <br> Type | Inner Bracing Size | Inner Bracing |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grade |  |  |  |  |  |  |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | Job |  | $\begin{array}{ll} \hline \text { Page } & \\ & 10 \text { of } 69 \end{array}$ |
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|  | CTNL024A |  |  |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| $\begin{gathered} \text { West Bridgewater, MA } 02379 \\ \text { Phone: } ; 78 I-713-4725 \\ \text { FAX: } \end{gathered}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Tower | Secondary <br> Elevation <br> Horizontal Type | Secondary Horizontal <br> Size | Secondary <br> Horizontal <br> Grade | Inner Bracing <br> Type | Inner Bracing Size |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inner Bracing |  |  |  |  |  |  |
| Grade |  |  |  |  |  |  |

## Tower Section Geometry (cont'd)

| Tower Elevation <br> ft | Gusset Area (perface) $f t^{2}$ | Gusset Thickness <br> in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TI | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 368.75-362.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T2 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 362.50-356.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T3 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 356.25-350.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T4 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 350.00-343.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T5 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 343.75-337.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T6 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 337.50-331.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T7 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 331.25-325.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T8 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 325.00-318.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T9 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 318.75-312.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T10 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 312.50-306.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T11 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 306.25-300.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T12 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 300.00-293.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T13 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 293.75-287.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T14 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 287.50-281.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T15 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 281.25-275.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T16 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 275.00-268.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T17 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 268.75-262.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T18 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 262.50-256.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T19 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 256.25-250.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T20 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 250.00-243.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T21 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 243.75-237.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T22 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 237.50-231.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T23 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 231.25-225.00 |  |  | (36 ksi) |  |  |  |  |  |  |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 $F A X:$ | Job | CTNL024A | Page 11 of 69 |
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|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation <br> $f t$ | Gusset Area (per face) $\qquad$ | Gusset Thickness in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T24 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 225.00-218.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T25 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 218.75-212.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T26 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 212.50-206.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T27 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 206.25-181.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T28 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 181.25-175.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T29 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 175.00-168.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T30 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 168.75-162.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T31 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 162.50-156.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T32 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 156.25-150.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T33 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 150.00-125.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T34 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 125.00-100.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T35 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 100.00-93.75 |  |  | (36 ksi) |  |  |  |  |  |  |
| T36 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 93.75-87.50 |  |  | (36 ksi) |  |  |  |  |  |  |
| T37 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 87.50-81.25 |  |  | (36 ksi) |  |  |  |  |  |  |
| T38 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 81.25-75.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T39 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 75.00-50.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T40 | 0.00 | 0.0000 | A36 | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |
| 50.00-25.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| T41 25.00-0.00 | 0.00 | 0.0000 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.05 | 1 | 1 | 36.0000 | 36.0000 | 36.0000 |

Tower Section Geometry (cont'd)

| Tower <br> Elevation | Calc <br> K <br> Single <br> Angles | Calc <br> K Solid Rounds | K Factors ${ }^{\prime}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Legs | $X$ | K | Single Diags | Girts | Horiz. | Sec. Horiz. | Inner <br> Brace |
|  |  |  |  | Brace | Brace |  |  |  |  |  |
|  |  |  |  | Diags | Diags |  |  |  |  |  |
|  |  |  |  | $X$ | $X$ | $X$ | $X$ | $x$ | $x$ | X |
| $f t$ |  |  |  | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ |
| T1 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 368.75-362.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | , |
| T2 | Yes | Yes | 1 | 1 | 1 | 1 | , | 1 | 1 | I |
| 362.50-356.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T3 | Yes | Yes | 1 | I | 1 | I | 1 | 1 | 1 | 1 |
| 356.25-350.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T4 | Yes | Yes | 1 | 1 | , | 1 | 1 | 1 | 1 | 1 |
| 350.00-343.75 |  |  |  | , | 1 | , | 1 | 1 | 1 | 1 |
| T5 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 343.75-337.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | I |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{array}{ll} \text { Page } \\ & \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Elevation | Calc <br> K <br> Single <br> Angles | Calc K Solid Rounds | $K$ Factors ${ }^{\prime}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Legs | $X$ <br> Brace | K Brace | Single <br> Diags | Girts | Horiz. | Sec. Horiz. | Inner <br> Brace |
|  |  |  |  | Diags | Diags |  |  |  |  |  |
|  |  |  |  | X | $X$ | X | X | X | $X$ | $X$ |
| $f t$ |  |  |  | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ |
| T6 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 337.50-331.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T7 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 331.25-325.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T8 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 325.00-318.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T9 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 318.75-312.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T10 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 312.50-306.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| TII | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 306.25-300.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T12 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 300.00-293.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T13 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 293.75-287.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T14 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 287.50-281.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{T} 15$ | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 281.25-275.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T16 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 275.00-268.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T17 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 268.75-262.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T18 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 262.50-256.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T19 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $256.25-250.00$ |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{T} 20$ | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 250.00-243.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T21 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 243.75-237.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{T} 22$ | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 237.50-231.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T23 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 231.25-225.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T24 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 225.00-218.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{T} 25$ | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 218.75-212.50 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T26 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 212.50-206.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T27 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 206.25-181.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T28 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 181.25-175.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T29 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 175.00-168.75 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T30 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $168.75-162.50$ |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T31 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 162.50-156.25 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T32 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 156.25-150.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T33 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 150.00-125.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T34 | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 125.00-100.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | CTNL024A |  | Page 13 of 69 |
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|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \\ \hline \end{array}$ |
| $\begin{aligned} & \text { West Bridgewater; MA } 02379 \\ & \text { Phone: } 71-1113-4725 \\ & \text { FAX: } \end{aligned}$ | Client | T-MOBILE | Designed by Arielle Novak |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

[^1]Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in | $U$ | Net Width Deduct in |  | $\begin{aligned} & \text { Net Width } \\ & \text { Deduct } \\ & \text { in } \end{aligned}$ |  | Net Width Deduct in | $U$ | Net <br> Width <br> Deduct in | $U$ | Net <br> Width <br> Deduct in | $U$ | Net <br> Width <br> Deduct in | $U$ |
| $\begin{gathered} \mathrm{Tl} \\ 368.75-362.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 2 \\ 362.50-356.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T3 } \\ 356.25-350.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 4 \\ 350.00-343.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T5 } \\ 343.75-337.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T6 } \\ 337.50-331.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T7 } \\ 331.25-325.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T8 } \\ 325.00-318.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T9 } \\ 318.75-312.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T10 } \\ 312.50-306.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T11 } \\ 306.25-300.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T12 $300.00-293.75$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 13 \\ 293.75-287.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T14 } \\ 287.50-281.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |


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|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
| ```West Bridgewater, MA 02379 Phone: 781-713-4725 FAX:``` | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation $f t$ | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in | $U$ | Net Width Deduct in |  | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net <br> Width <br> Deduct in | $U$ | Net Width Deduct in | $U$ |
| $\begin{gathered} \mathrm{T} 15 \\ 281.25-275.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T16 } \\ 275.00-268.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 17 \\ 268.75-262.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T18 } \\ 262.50-256.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T19 } \\ 256.25-250.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T20 } \\ 250.00-243.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T21 } \\ 243.75-237.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 22 \\ 237.50-231.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T23 } \\ 231.25-225.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 24 \\ 225.00-218.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T25 } \\ 218.75-212.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T26 } \\ 212.50-206.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T27 } \\ 206.25-181.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T28 } \\ 181.25-175.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 29 \\ 175.00-168.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T30 } \\ 168.75-162.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T31 } \\ 162.50-156.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T32 } \\ 156.25-150.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T33 } \\ 150.00-125.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T34 } \\ 125.00-100.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T35 } \\ 100.00-93.75 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T36 } \\ 93.75-87.50 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T37 } \\ 87.50-81.25 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T38 } \\ 81.25-75.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T39 } \\ 75.00-50.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T40 } \\ 50.00-25.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T41 25.00-0.00 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & \\ & 15 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation | Redundant Horizontal |  | Redundant Diagonal |  | Redundant Sub-Diagonal |  | Redundant Sub-Horizontal |  | Redundant Vertical |  | Redundant Hip |  | Redundant Hip Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in |  | Net Width Deduct in |  | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net <br> Width <br> Deduct <br> in | $U$ |
| $\begin{gathered} \hline \mathrm{Tl} \\ 368.75-362.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 2 \\ 362.50-356.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 3 \\ 356.25-350.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 4 \\ 350.00-343.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T5 } \\ 343.75-337.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T6 } \\ 337.50-331.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 7 \\ 331.25-325.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T8 } \\ 325.00-318.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T9 } \\ 318.75-312.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T10 } \\ 312.50-306.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T11 } \\ 306.25-300.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T12 } \\ 300.00-293.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T13 } \\ 293.75-287.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T14 } \\ 287.50-281.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T15 } \\ 281.25-275.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T16 } \\ 275.00-268.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 17 \\ 268.75-262.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T18 } \\ 262.50-256.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T19 } \\ 256.25-250.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T20 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T21 } \\ 243.75-237.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 22 \\ 237.50-231.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| 231.25-225.00 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T24 $225.00-218.75$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \mathrm{T} 25 \\ 218.75-212.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T26 } \\ 212.50-206.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T27 206.25-181.25 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T28 } \\ 181.25-175.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 | Job |  | $\begin{aligned} & \text { Page } \\ & \\ & 16 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | CTNL024A |  |  |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| $\begin{gathered} \text { West Bridgevater; MA } 02379 \\ \text { Phone: } 781-7 / 3-4725 \\ \text { FAX: } \end{gathered}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation $f t$ | Redundant <br> Horizontal |  | Redundant <br> Diagonal |  | Redundant Sub-Diagonal |  | Redundant Sub-Horizontal |  | Redundant Vertical |  | Redundant Hip |  | Redundant Hip Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in |  | Net Width Deduct in |  | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net <br> Width <br> Deduct in | $U$ | Net <br> Width <br> Deduct <br> in | $U$ | Net <br> Width <br> Deduct <br> in | U |
| $\begin{gathered} \hline \text { T29 } \\ 175.00-168.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T30 } \\ \text { 168.75-162.50 } \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T31 } \\ 162.50-156.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T32 156.25-150.00 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T33 } \\ 150.00-125.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T34 } \\ 125.00-100.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T35 } \\ 100.00-93.75 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T36 } \\ 93.75-87.50 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T37 } \\ 87.50-81.25 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T38 } \\ 81.25-75.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T39 } \\ 75.00-50.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T40 } \\ 50.00-25.00 \end{gathered}$ | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T41 25.00-0.00 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |

Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg Connection Type | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. |
| TI | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 368.75-362.50 |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  |
| T2 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 362.50-356.25 |  | A325N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A 325 N |  |
| T3 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 356.25-350.00 |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  |
| T4 | Flange | 0.7500 | 6 | 0.6250 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 350.00-343.75 |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  |
| T5 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 343.75-337.50 |  | A325N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  |
| T6 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 0 |
| 337.50-331.25 |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  |
| T7 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 331.25-325.00 |  | A 325 N |  | A325N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A307 |  |
| T8 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 325.00-318.75 |  | A325N |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A307 |  |
| T9 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 318.75-312.50 |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |


| tnxTower | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & \\ & 17 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by <br> Arielle Novak |


| Tower <br> Elevation <br> ft | Leg Connection Type | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bolt Size in | No. | Bolt Size in |  | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | $\begin{gathered} \text { Bolt Size } \\ \text { in } \end{gathered}$ | No. |
| T10 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 312.50-306.25 |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T11 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 306.25-300.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T12 | Flange | 0.7500 | 6 | 0.6250 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 300.00-293.75 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T13 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 293.75-287.50 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T14 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 287.50-281.25 |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A 307 |  |
| T15 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 281.25-275.00 |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T16 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 275.00-268.75 |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A 325 N |  | A 325 N |  | A307 |  |
| T17 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 268.75-262.50 |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T18 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 262.50-256.25 |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A307 |  |
| T19 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 256.25-250.00 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T20 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 250.00-243.75 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T21 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 243.75-237.50 |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T22 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 237.50-231.25 |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A307 |  |
| T23 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 231.25-225.00 |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T24 | Flange | 0.7500 | 6 | 0.6250 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 225.00-218.75 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T25 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 218.75-212.50 |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T26 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 212.50-206.25 |  | A325N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A307 |  |
| T27 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | I |
| 206.25-181.25 |  | A325N |  | A325N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A307 |  |
| T28 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 181.25-175.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T29 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 175.00-168.75 |  | A325N |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A307 |  |
| T30 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 168.75-162.50 |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A325N |  | A 325 N |  | A307 |  |
| T31 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 162.50-156.25 |  | A325N |  | A325N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A307 |  |
| T32 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 156.25-150.00 |  | A 325 N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A307 |  |
| T33 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 150.00-125.00 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T34 | Flange | 0.7500 | 6 | 0.6250 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 125.00-100.00 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T35 | Flange | 0.7500 | 6 | 0.6250 | 2 | 0.6250 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 100.00-93.75 |  | A325N |  | A 325 N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A307 |  |
| T36 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 93.75-87.50 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T37 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 87.50-81.25 |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A307 |  |
| T38 | Flange | 0.7500 | 0 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 81.25-75.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A307 |  |


| tnxTower <br> Centerline Contmunications 750 West Center Street, Suite 301 West Bridgewater, MA 02379 Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } 18 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \\ \hline \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Elevation $f t$ | $\begin{gathered} \text { Leg } \\ \text { Connection } \\ \text { Type } \end{gathered}$ | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bolt Size in | No. | Bolt Size in |  | Bolt Size in | No. | Bolt Size $\qquad$ in |  | $\begin{gathered} \text { Bolt Size } \\ \text { in } \\ \hline \end{gathered}$ |  | $\begin{array}{\|c} \begin{array}{c} \text { Bolt Size } \\ \text { in } \end{array} \\ \hline \end{array}$ | No. | $\begin{array}{\|c} \hline \begin{array}{c} \text { Bolt Size } \\ \text { in } \end{array} \\ \hline \end{array}$ | No. |
| T39 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| 75.00-50.00 |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | $\begin{gathered} \text { A307 } \\ 06250 \end{gathered}$ | 1 |
| T40 | Flange | 0.7500 | 6 | 0.5000 | 2 | 0.5000 | 2 | 0.6250 | 0 | 0.6250 | 0 | A 325 N |  | A307 |  |
| 50.00-25.00 |  | A325N |  | A 32.5 N |  | A 325 N |  | A325 |  | A32 | 0 | 0.6250 | 2 | 0.6250 | 1 |
| T41 25.00-0.00 | Flange | $0.7500$ | 6 | $\begin{aligned} & 0.5000 \\ & \mathrm{~A} 325 \mathrm{~N} \end{aligned}$ | 2 | 0.5000 A 325 N | 2 | 0.6250 A 325 N | 0 | A 325 N | 0 | A 325 N |  | A307 |  |

## Guy Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Guy Elevation \& Guy Grade \& \& Guy Size \& \begin{tabular}{l}
Initial \\
Tension
\end{tabular} \& \% \& Guy Modulus \& \begin{tabular}{l}
Guy \\
Weight
\end{tabular} \& \(L_{17}\)

ft \& \begin{tabular}{l}
Anchor <br>
Radius

 \& 

Anchor <br>
Azimuth Adj.

 \& Anchor Elevation \& 

End <br>
Fitting Efficiency $\%$
\end{tabular} <br>

\hline $f t$ \& \& \& \& $l b$ \& \& ksi \& plf \& ft \& $f t$ \& \& \& \% <br>
\hline \multirow[t]{3}{*}{350} \& \multirow[t]{3}{*}{EHS} \& A \& 7/8 \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 430.92 \& 247.15 \& 0.00 \& 1.81 \& 100\% <br>
\hline \& \& B \& 7/8 \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 424.88 \& 247.51 \& 0.0000 \& 1.81 \& 100\% <br>
\hline \& \& C \& $7 / 8$ \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 438.63 \& 251.45 \& 0.0000 \& -12.20 \& 100\% <br>
\hline \multirow[t]{3}{*}{300} \& \multirow[t]{2}{*}{EHS} \& A \& 7/8 \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 376.90 \& 224.79 \& 0.0000 \& -5.41
1.23 \& 100\% <br>
\hline \& \& B \& 7/8 \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 368.38 \& 219.43 \& 0.0000 \& -1.23 \& 100\% <br>
\hline \& \multirow{3}{*}{EHS} \& C \& $7 / 8$ \& 7970.00 \& 10\% \& 19000 \& 1.581 \& 382.21 \& 227.42 \& 0.0000
0.0000 \& -10.07 \& 100\% <br>
\hline \multirow[t]{3}{*}{225} \& \& A \& 3/4 \& 5830.00 \& 10\% \& 19000 \& 1.155 \& 319.27 \& 224.79 \& 0.0000 \& - 1.23 \& 100\% <br>
\hline \& \& B \& 3/4 \& 5830.00 \& 10\% \& 19000 \& 1.155 \& 310.78 \& 219.43
227.42 \& 0.0000 \& -10.07 \& 100\% <br>
\hline \& \multirow{3}{*}{EHS} \& C \& $3 / 4$ \& 5830.00 \& 10\% \& 19000 \& 1.155 \& 324.45 \& 227.42
201.41 \& 0.0000 \& -4.96 \& 100\% <br>
\hline \multirow[t]{3}{*}{162.5} \& \& A \& $3 / 4$ \& 5830.00 \& 10\% \& 19000 \& 1.155 \& 259.49
249.91 \& 201.41 \& 0.0000 \& -4.72 \& 100\% <br>
\hline \& \& B \& 3/4 \& 5830.00 \& 10\% \& 19000 \& 1.155
1.155 \& 249.91
266.15 \& 193.65
206.73 \& 0.0000 \& -8.98 \& 100\% <br>
\hline \& \& C \& 3/4 \& 5830.00 \& 10\% \& 19000 \& 1.155
0.671 \& 266.15 \& 201.41 \& 0.0000 \& -4.96 \& 100\% <br>
\hline \multirow[t]{3}{*}{100} \& \multirow[t]{2}{*}{EHS} \& A \& 9/16 \& 3500.00
3500.00 \& 10\% \& 21000
21000 \& 0.671
0.671 \& 214.45 \& 193.65 \& 0.0000 \& 0.72 \& 100\% <br>
\hline \& \& B \& 9/16 \& 3500.00
3500.00 \& $10 \%$
$10 \%$ \& 21000
21000 \& 0.671 \& 214.45
230.53 \& 206.73 \& 0.0000 \& -8.98 \& 100\% <br>
\hline \& \multirow{3}{*}{EHS} \& C \& $9 / 16$ \& 3500.00
3500.00 \& $10 \%$
$10 \%$ \& 21000 \& 0.671 \& 123.30 \& 114.04 \& 0.0000 \& -3.60 \& 100\% <br>
\hline \multirow[t]{2}{*}{50} \& \& A \& $9 / 16$
$9 / 16$ \& 3500.00
3500.00 \& $10 \%$
$10 \%$ \& 21000 \& 0.671 \& 123.03 \& 115.63 \& 0.0000 \& 0.50 \& 100\% <br>
\hline \& \& B \& $9 / 16$
$9 / 16$ \& 3500.00
3500.00 \& 10\% \& 21000 \& 0.671 \& 124.42 \& 114.41 \& 0.0000 \& -5.40 \& 100\% <br>
\hline
\end{tabular}

Guy Data(cont'd)

| Guy Elevation $f t$ | $\begin{aligned} & \text { Mount } \\ & \text { Type } \end{aligned}$ | Torque-Arm Spread <br> $f t$ | Torque-Arm Leg Angle <br> - | Torque-Arm Style | Torque-Arm Grade | Torque-Arm Type | Torque-Arm Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 350 | Torque Arm | 12.00 | 49.0000 | Bat Ear | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 2 \mathrm{l} / 2 \times 1 / 4$ |
| 300 | Torque Arm | 12.00 | 49.0000 | Bat Ear | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ |
| 225 | Torque Arm | 12.00 | 49.0000 | Bat Ear | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 2$ 1/2x1/4 |
| $\begin{gathered} 162.5^{4} \\ 100 \end{gathered}$ | Corner <br> Torque Arm | 12.00 | 49.0000 | Bat Ear | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | Double Angle | 2L3x2 1/2x1/4 |
| 50 | Corner |  |  |  |  |  |  |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } 19 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

## Guy Data (cont'd)

| Guty <br> Elevation <br> $f t$ | Diagonal <br> Grade | Diagonal <br> Type | Upper Diagonal <br> Size | Lower Diagonal <br> Size | Is <br> Strap. | Pull-Off <br> Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 350.00 | A572-50 | Solid Round |  |  | A572-50 | Solid Round |
|  | $(50 \mathrm{ksi})$ |  |  | $(50 \mathrm{ksi})$ |  |  |
| 300.00 | A572-50 | Solid Round |  |  | A572-50 | Solid Round |
|  | $(50 \mathrm{ksi})$ |  |  | $(50 \mathrm{ksi})$ |  |  |
| 225.00 | A572-50 | Solid Round |  | A572-50 | Solid Round |  |
|  | $(50 \mathrm{ksi})$ |  | $(50 \mathrm{ksi})$ |  |  |  |
| 162.50 | A572-50 | Solid Round |  | A572-50 | Solid Round |  |
|  | $(50 \mathrm{ksi})$ |  | $(50 \mathrm{ksi})$ |  |  |  |
| 100.00 | A572-50 | Solid Round |  | A572-50 | Solid Round |  |
|  | $(50 \mathrm{ksi})$ |  | $(50 \mathrm{ksi})$ |  |  |  |
| 50.00 | A572-50 | Solid Round |  | A572-50 | Solid Round |  |
|  | $(50 \mathrm{ksi})$ |  |  | $(50 \mathrm{ksi})$ |  |  |

Guy Data (cont'd)

| Guy | Cable | Cable | Cable | Cable | Tower | Tower | Tower | Tower |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation | Weight <br> A | Weight <br> B | Weight <br> C | Weight <br> D | Intercept <br> A | Intercept <br> B | Intercept C | Intercept D |
| $f t$ | $1 b$ | $1 b$ | $l b$ | $l b$ | $f t$ | $f t$ | $f t$ | $f t$ |
| 350 | 681.29 | 671.73 | 693.47 |  | 17.81 | 17.33 | 18.44 |  |
|  |  |  |  |  | $7.3 \mathrm{sec} / \mathrm{pulse}$ | $7.2 \mathrm{sec} /$ pulse | $7.4 \mathrm{sec} /$ pulse |  |
| 300 | 595.87 | 582.41 | 604.27 |  | 13.69 | 13.09 | 14.07 |  |
|  |  |  |  |  | $6.4 \mathrm{sec} / \mathrm{pulse}$ | $6.2 \mathrm{sec} / \mathrm{pulse}$ | $6.5 \mathrm{sec} / \mathrm{pulse}$ |  |
| 225 | 368.76 | 358.95 | 374.74 |  | 9.88 | 9.37 | 10.20 |  |
|  |  |  |  |  | $5.4 \mathrm{sec} / \mathrm{pulse}$ | $5.3 \mathrm{sec} / \mathrm{pulse}$ | $5.5 \mathrm{sec} / \mathrm{pulse}$ |  |
| 162.5 | 299.72 | 288.65 | 307.40 |  | 6.57 | 6.10 | 6.91 |  |
|  |  |  |  |  | $4.4 \mathrm{sec} /$ pulse | $4.3 \mathrm{sec} / \mathrm{pulse}$ | $4.5 \mathrm{sec} / \mathrm{pulse}$ |  |
| 100 | 150.27 | 143.90 | 154.69 |  | 4.76 | 4.37 | 5.05 |  |
|  |  |  |  |  | $3.8 \mathrm{sec} / \mathrm{pulse}$ | $3.6 \mathrm{sec} / \mathrm{pulse}$ | $3.9 \mathrm{sec} / \mathrm{pulse}$ |  |
| 50 | 82.73 | 82.55 | 83.49 |  | 1.45 | 1.45 | 1.48 |  |
|  |  |  |  |  | $2.1 \mathrm{sec} / \mathrm{pulse}$ | 2.1 sec/pulse | $2.1 \mathrm{sec} / \mathrm{pulse}$ |  |

## Guy Data (cont'd)

| Guy Elevation ft | Calc K Single Angles | Calc K <br> Solid <br> Rounds | Torque Arm |  | Pull Off |  | Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $K_{\text {r }}$ | $K_{y}$ | $K_{x}$ | $K_{y}$ | $K_{x}$ | $K_{y}$ |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| 350 | No | No | 1 | 1 | 1 | 1 | 1 | 1 |
| 300 | No | No | 1 | 1 | 1 | 1 | 1 | 1 |
| 225 | No | No | 1 | 1 | 1 | 1 | 1 | 1 |
| 162.5 | No | No |  |  | 1 | 1 | 1 | 1 |
| 100 | No | No | 1 | 1 | 1 | 1 | 1 | 1 |
| 50 | No | No |  |  | 1 | 1 | 1 | 1 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } 20 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

## Guy Data (cont'd)

| $\begin{gathered} \text { Guy } \\ \text { Elevation } \\ f t \\ \hline \end{gathered}$ | Torque-Arm |  |  |  | Pull Off |  |  |  | Diagonal |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bolt Size in | Number | Net Width Deduct in | $U$ | Bolt Size in | Number | Net Width Deduct in | $U$ | Bolt Size in | Number | Net Width Deduct in | $U$ |
| 350 | 0.0000 | 0 | 0.0000 | 1 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A 325 N |  |  |  | A 325 N |  |  |  | A 325 N |  |  |  |
| 300 | 0.0000 | 0 | 0.0000 | 1 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A 325 N |  |  |  | A 325 N |  |  |  | A 325 N |  |  |  |
| 225 | 0.0000 | 0 | 0.0000 | 1 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A 325 N |  |  |  | A 325 N |  |  |  | A 325 N |  |  |  |
| 162.5 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A 325 N |  |  |  | A 325 N |  |  |  | A 325 N |  |  |  |
| 100 | 0.0000 | 0 | 0.0000 | 1 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A 325 N |  |  |  | A 325 N |  |  |  | A325N |  |  |  |
| 50 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 | 0.6250 | 0 | 0.0000 | 0.75 |
|  | A325N |  |  |  | A325N |  |  |  | A 325 N |  |  |  |

## Guy Pressures

| $\begin{gathered} \text { Guy } \\ \text { Elevation } \\ f t \end{gathered}$ | Guy Location | $z$ $f t$ | $q=$ $p s f$ | $q=$ Ice $p s f$ | Ice Thickness in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 350 | A | 172.10 | 28 | 6 | 1.7694 |
|  | B | 175.91 | 28 | 6 | 1.7732 |
|  | C | 168.90 | 28 | 6 | 1.7660 |
| 300 | A | 147.30 | 26 | 6 | 1.7420 |
|  | B | 150.62 | 27 | 6 | 1.7459 |
|  | C | 144.97 | 26 | 6 | 1.7393 |
| 225 | A | 109.80 | 24 | 6 | 1.6916 |
|  | B | 113.12 | 25 | 6 | 1.6966 |
|  | C | 107.47 | 24 | 5 | 1.6880 |
| 162.5 | A | 78.77 | 22 | 5 | 1.6363 |
|  | B | 81.61 | 22 | 5 | 1.6422 |
|  | C | 76.76 | 22 | 5 | 1.6321 |
| 100 | A | 47.52 | 19 | 4 | 1.5557 |
|  | B | 50.36 | 19 | 4 | 1.5648 |
|  | C | 45.51 | 19 | 4 | 1.5490 |
| 50 | A | 23.20 | 17 | 4 | 1.4481 |
|  | B | 25.25 | 17 | 4 | 1.4604 |
|  | C | 22.30 | 17 | 4 | 1.4423 |

Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow <br> Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement $f t$ | Face Offset in | Lateral Offset (Frac FW) | \# | $\#$ Per Row | Clear <br> Spacing in | Width or Diameter. in | Perimeter in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7/8 | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | 40.00-3.00 | $-1.0000$ | 0.46 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 7/8 | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | 62.00-3.00 | -0.5000 | 0.47 | 1 | 1 | 1.1100 | 1.1100 |  | 0.54 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | 88.00-3.00 | -2.0000 | 0.46 | 4 | 4 | 0.5800 | 0.5800 |  | 0.25 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | 125.00 - | -1.0000 | 0.45 | 1 | 1 | 0.5800 | 0.5800 |  | 0.25 |


| tnxTower | Job |  | $\begin{aligned} & \text { Page } 21 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  |  | CTNL024A |  |
| Centerline Communications 750 West Center Street, Suite 301 | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \\ \hline \end{array}$ |
| West Bridgevater, MA 02379 Phone: $781-713-4725$ <br> FAX: | Client | T-MOBILE | Designed by Arielle Novak |


| Description | Face or Leg | Allow <br> Shield | Exclude <br> From <br> Torque <br> Calculation | Component Type | Placement <br> ft | Face Offset in | Lateral Offset (Frac FW) | \# |  | Clear <br> Spacing in | Width or Perimeter Diameter. in in | Weight <br> $p l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7/8 | C | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 140.00- \\ 3.00 \end{gathered}$ | $-1.0000$ | 0.47 | 1 | 1 | 1.1100 | 1.1100 | 0.54 |
| 1/2 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 148.00- \\ 3.00 \end{gathered}$ | $-3.0000$ | 0.47 | 1 | 1 | 0.5800 | 0.5800 | 0.25 |
| 7/8 | A | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 180.00- \\ 3.00 \end{gathered}$ | -2.0000 | 0.44 | 1 | 1 | 1.1100 | 1.1100 | 0.54 |
| 7/8 | C | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 200.00- \\ 3.00 \end{gathered}$ | $-1.0000$ | 0.45 | 1 | 1 | 1.1100 | 1.1100 | 0.54 |
| $15 / 8$ | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 325.00- \\ 3.00 \end{gathered}$ | $-2.0000$ | 0.45 | 1 | 1 | 1.9800 | 1.9800 | 1.04 |
| 7/8 | B | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 350.00- \\ 3.00 \end{gathered}$ | $-1.0000$ | 0.44 | 2 | 2 | 1.1100 | 1.1100 | 0.54 |
| 7/8 | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 355.00- \\ 3.00 \end{gathered}$ | $-2.0000$ | 0.44 | 1 | 1 | 1.1100 | 1.1100 | 0.54 |
| 7/8 | C | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 365.00- \\ 3.00 \end{gathered}$ | $-2.0000$ | 0.46 | 1 | 1 | 1.1100 | 1.1100 | 0.54 |
| $15 / 8$ | C | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 300.00- \\ 3.00 \end{gathered}$ | 1.0000 | -0.3 | 12 | 6 | 1.9800 | 1.9800 | 1.04 |
| $\begin{gathered} \text { HYBRIFLEX } \\ 15 / 8 \\ \text { (VERIZON) } \end{gathered}$ | B | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 300.00- \\ 3.00 \end{gathered}$ | 1.0000 | 0.46 | 2 | 2 | 1.9800 | 1.9800 | 1.04 |
| $\begin{gathered} 15 / 8 \\ \text { (AT\&T) } \end{gathered}$ | C | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 2.0000 | 0.5 | 12 | 2 | 1.9800 | 1.9800 | 1.04 |
| Fiber Trunk (AT\&T) | A | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 0.0000 | -0.4 | 1 | 1 | 0.4000 | 0.4000 | 1.00 |
| DC Trunk <br> (AT\&T) | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 0.0000 | -0.4 | 2 | 2 | 0.4000 | 0.4000 | 0.11 |
| Fiber Trunk (AT\&T) | A | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 0.0000 | -0.4 | 1 | 1 | 0.4000 | 0.4000 | 1.00 |
| DC Trunk <br> (AT\&T) | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 0.0000 | -0.4 | 4 | 4 | 0.4000 | 0.4000 | 0.11 |
| $0.3^{\prime \prime}$ dia. RET <br> (AT\&T) <br> *** | A | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 240.00- \\ 3.00 \end{gathered}$ | 0.0000 | -0.37 | 3 | 3 | 0.3000 | 0.3000 | 0.00 |
| $\begin{gathered} 6 \times 24 \\ \text { HYBRID } \\ \text { (T-MOBILE) } \\ \hline \end{gathered}$ | A | No | No | $\mathrm{Ar}(\mathrm{CaAa})$ | $\begin{gathered} 230.00- \\ 3.00 \end{gathered}$ | $-1.0000$ | 0.35 | 3 | 3 | 1.9800 | 1.9800 | 1.04 |

Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation $f t$ \& Face \& $A_{R}$

$f t^{2}$ \& $A_{F}$
$f t^{2}$ \& $C_{A} A_{A}$ In Face $\mathrm{ft}^{2}$ \& $C_{A} A_{A}$ Out Face $\mathrm{ft}^{2}$ \& Weight
lb <br>
\hline \multirow[t]{3}{*}{TI} \& \multirow[t]{3}{*}{368.75-362.50} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.278 \& 0.000 \& 1.35 <br>
\hline \multirow[t]{3}{*}{T2} \& \multirow[t]{3}{*}{362.50-356.25} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \multirow[t]{3}{*}{T3} \& \multirow[t]{3}{*}{356.25-350.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.555 \& 0.000 \& 2.70 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \multirow[t]{3}{*}{T4} \& \multirow[t]{3}{*}{350.00-343.75} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline T5 \& 343.75-337.50 \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline
\end{tabular}

| thxTOWer | Job | PTNL024A | Page |
| :---: | :--- | :--- | :--- |
|  | Project | Client | ANCHOR |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower \\
Section
\end{tabular} \& \begin{tabular}{l}
Tower \\
Elevation \\
ft
\end{tabular} \& Face \& \(A_{R}\)

$j t^{2}$ \& $A_{F}$
$\mathrm{ft}^{2}$ \& $C_{A} A_{A}$ In Face $\mathrm{ft}^{2}$ \& $C_{A} A_{A}$ Out Face $\mathrm{ft}^{2}$ \& Weight
$l b$ <br>
\hline \multirow{4}{*}{T6} \& \multirow{4}{*}{337.50-331.25} \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T7} \& \multirow{3}{*}{331.25-325.00} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T8} \& \multirow{3}{*}{325.00-318.75} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T9} \& \multirow{3}{*}{318.75-312.50} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T10} \& \multirow{3}{*}{312.50-306.25} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T11} \& \multirow{3}{*}{306.25-300.00} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.081 \& 0.000 \& 10.13 <br>
\hline \multirow{3}{*}{T12} \& \multirow{3}{*}{300.00-293.75} \& C \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 3.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T13} \& \multirow{3}{*}{293.75-287.50} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T14} \& \multirow{3}{*}{287.50-281.25} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T15} \& \multirow{3}{*}{281.25-275.00} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T16} \& \multirow{3}{*}{275.00-268.75} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T17} \& \multirow{3}{*}{268.75-262.50} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T18} \& \multirow{3}{*}{262.50-256.25} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T19} \& \multirow{3}{*}{256.25-250.00} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T20} \& \multirow{3}{*}{250.00-243.75} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.238 \& 0.000 \& 6.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T21} \& \multirow{3}{*}{243.75-237.50} \& C \& 0.000 \& 0.000 \& 15.544 \& 0.000 \& 81.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 2.263 \& 0.000 \& 13.15 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T22} \& \multirow{3}{*}{237.50-231.25} \& C \& 0.000 \& 0.000 \& 21.484 \& 0.000 \& 112.58 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 3.800 \& 0.000 \& 23.13 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T23} \& \multirow{3}{*}{231.25-225.00} \& C \& 0.000 \& 0.000 \& 30.394 \& 0.000 \& 159.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 6.770 \& 0.000 \& 38.73 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T24} \& \multirow{3}{*}{225.00-218.75} \& C \& 0.000 \& 0.000 \& 30.394 \& 0.000 \& 159.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 7.512 \& 0.000 \& 42.63 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T25} \& \multirow{3}{*}{218.75-212.50} \& C \& 0.000 \& 0.000 \& 30.394 \& 0.000 \& 159.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 7.512 \& 0.000 \& 42.63 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline
\end{tabular}

| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } 23 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation $f t$ \& Face \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& | Weight |
| :---: |
| lb | <br>

\hline \multirow{3}{*}{T26} \& \multirow{3}{*}{212.50-206.25} \& C \& 0.000 \& 0.000 \& 30.394 \& 0.000 \& 159.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 7.512 \& 0.000 \& 42.63 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T27} \& \multirow{3}{*}{206.25-181.25} \& C \& 0.000 \& 0.000 \& 30.394 \& 0.000 \& 159.38 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 30.050 \& 0.000 \& 170.50 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 18.225 \& 0.000 \& 92.50 <br>
\hline \multirow{3}{*}{T28} \& \multirow{3}{*}{181.25-175.00} \& C \& 0.000 \& 0.000 \& 123.656 \& 0.000 \& 647.63 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.068 \& 0.000 \& 45.33 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T29} \& \multirow{3}{*}{175.00-168.75} \& C \& 0.000 \& 0.000 \& 31.087 \& 0.000 \& 162.75 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T30} \& \multirow{3}{*}{168.75-162.50} \& C \& 0.000 \& 0.000 \& 31.087 \& 0.000 \& 162.75 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T31} \& \multirow{3}{*}{162.50-156.25} \& C \& 0.000 \& 0.000 \& 31.087 \& 0.000 \& 162.75 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T32} \& \multirow{3}{*}{156.25-150.00} \& C \& 0.000 \& 0.000 \& 31.087 \& 0.000 \& 162.75 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.556 \& 0.000 \& 23.13 <br>
\hline \multirow{3}{*}{T33} \& \multirow{3}{*}{150.00-125.00} \& C \& 0.000 \& 0.000 \& 31.087 \& 0.000 \& 162.75 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 32.825 \& 0.000 \& 184.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 19.559 \& 0.000 \& 98.25 <br>
\hline \multirow{3}{*}{T34} \& \multirow{3}{*}{125.00-100.00} \& C \& 0.000 \& 0.000 \& 126.015 \& 0.000 \& 659.10 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 32.825 \& 0.000 \& 184.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 21.125 \& 0.000 \& 105.00 <br>
\hline \multirow{3}{*}{T35} \& \multirow{3}{*}{100.00-93.75} \& C \& 0.000 \& 0.000 \& 127.125 \& 0.000 \& 664.50 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.281 \& 0.000 \& 26.25 <br>
\hline \multirow{3}{*}{T36} \& \multirow{3}{*}{93.75-87.50} \& C \& 0.000 \& 0.000 \& 31.781 \& 0.000 \& 166.13 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.397 \& 0.000 \& 26.75 <br>
\hline \multirow{3}{*}{T37} \& \multirow{3}{*}{87.50-81.25} \& C \& 0.000 \& 0.000 \& 31.781 \& 0.000 \& 166.13 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 6.731 \& 0.000 \& 32.50 <br>
\hline \multirow{3}{*}{T38} \& \multirow{3}{*}{81.25-75.00} \& C \& 0.000 \& 0.000 \& 31.781 \& 0.000 \& 166.13 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.206 \& 0.000 \& 46.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 6.731 \& 0.000 \& 32.50 <br>
\hline \multirow{3}{*}{T39} \& \multirow{3}{*}{75.00-50.00} \& C \& 0.000 \& 0.000 \& 31.781 \& 0.000 \& 166.13 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 34.157 \& 0.000 \& 190.48 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 26.925 \& 0.000 \& 130.00 <br>
\hline \multirow{3}{*}{T40} \& \multirow{3}{*}{50.00-25.00} \& C \& 0.000 \& 0.000 \& 127.125 \& 0.000 \& 664.50 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 37.265 \& 0.000 \& 205.60 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 26.925 \& 0.000 \& 130.00 <br>
\hline \multirow{4}{*}{T41} \& \multirow{4}{*}{25.00-0.00} \& C \& 0.000 \& 0.000 \& 127.125 \& 0.000 \& 664.50 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 33.770 \& 0.000 \& 185.68 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 23.694 \& 0.000 \& 114.40 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 111.870 \& 0.000 \& 584.76 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower <br> Section | Tower <br> Elevation <br> ft | Face <br> or <br> Leg | Ice <br> Thickness <br> in | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face | $C_{A} A_{A}$ <br> Out Face | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f^{2}$ | $\mathrm{ft}^{2}$ | $f^{2}$ | $\mathrm{ft}^{2}$ | lb |  |  |  |
| $\mathrm{T1}$ | $368.75-362.50$ | A | 1.908 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 1.231 | 0.000 | 18.94 |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } 24 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation $f t$ \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Ice Thickness in \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $C_{A} A_{A}$ Out Face $f t^{2}$ \& | Weight |
| :--- |
| lb | <br>

\hline \multirow[t]{3}{*}{T2} \& \multirow[t]{3}{*}{362.50-356.25} \& A \& \multirow[t]{3}{*}{1.905} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.074 \& 0.000 \& 47.22 <br>
\hline \multirow[t]{3}{*}{T3} \& \multirow[t]{3}{*}{356.25-350.00} \& A \& \multirow[t]{3}{*}{1.901} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.456 \& 0.000 \& 37.67 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.070 \& 0.000 \& 47.09 <br>
\hline \multirow[t]{3}{*}{T4} \& \multirow[t]{3}{*}{350.00-343.75} \& A \& \multirow[t]{3}{*}{1.898} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.825 \& 0.000 \& 121.42 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.066 \& 0.000 \& 46.96 <br>
\hline \multirow[t]{3}{*}{T5} \& \multirow[t]{3}{*}{343.75-337.50} \& A \& \multirow[t]{3}{*}{1.894} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.813 \& 0.000 \& 121.12 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.062 \& 0.000 \& 46.83 <br>
\hline \multirow[t]{3}{*}{T6} \& \multirow[t]{3}{*}{337.50-331.25} \& A \& \multirow[t]{3}{*}{1.891} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.801 \& 0.000 \& 120.82 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.057 \& 0.000 \& 46.70 <br>
\hline \multirow[t]{3}{*}{T7} \& \multirow[t]{3}{*}{331.25-325.00} \& A \& \multirow[t]{3}{*}{1.887} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.789 \& 0.000 \& 120.52 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.053 \& 0.000 \& 46.57 <br>
\hline \multirow[t]{3}{*}{T8} \& \multirow[t]{3}{*}{325.00-318.75} \& A \& \multirow[t]{3}{*}{1.884} \& 0.000 \& 0.000 \& 3.592 \& 0.000 \& 62.07 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.776 \& 0.000 \& 120.21 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.048 \& 0.000 \& 46.43 <br>
\hline \multirow[t]{3}{*}{T9} \& \multirow[t]{3}{*}{318.75-312.50} \& A \& \multirow[t]{3}{*}{1.880} \& 0.000 \& 0.000 \& 3.587 \& 0.000 \& 61.91 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.764 \& 0.000 \& 119.90 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.044 \& 0.000 \& 46.30 <br>
\hline \multirow[t]{3}{*}{T10} \& \multirow[t]{3}{*}{312.50-306.25} \& A \& \multirow[t]{3}{*}{1.876} \& 0.000 \& 0.000 \& 3.583 \& 0.000 \& 61.75 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.751 \& 0.000 \& 119.58 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.039 \& 0.000 \& 46.16 <br>
\hline \multirow[t]{3}{*}{TII} \& \multirow[t]{3}{*}{306.25-300.00} \& A \& \multirow[t]{3}{*}{1.872} \& 0.000 \& 0.000 \& 3.578 \& 0.000 \& 61.58 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 9.738 \& 0.000 \& 119.25 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 3.034 \& 0.000 \& 46.02 <br>
\hline \multirow[t]{3}{*}{T12} \& \multirow[t]{3}{*}{300.00-293.75} \& A \& \multirow[t]{3}{*}{1.869} \& 0.000 \& 0.000 \& 3.573 \& 0.000 \& 61.41 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.505 \& 0.000 \& 234.37 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.350 \& 0.000 \& 617.19 <br>
\hline \multirow[t]{3}{*}{T13} \& \multirow[t]{3}{*}{293.75-287.50} \& A \& \multirow[t]{3}{*}{1.865} \& 0.000 \& 0.000 \& 3.568 \& 0.000 \& 61.24 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.483 \& 0.000 \& 233.79 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.337 \& 0.000 \& 616.41 <br>
\hline \multirow[t]{3}{*}{T14} \& \multirow[t]{3}{*}{287.50-281.25} \& A \& \multirow[t]{3}{*}{1.860} \& 0.000 \& 0.000 \& 3.563 \& 0.000 \& 61.06 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.461 \& 0.000 \& 233.19 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.324 \& 0.000 \& 615.62 <br>
\hline \multirow[t]{3}{*}{T15} \& \multirow[t]{3}{*}{281.25-275.00} \& A \& \multirow[t]{3}{*}{1.856} \& 0.000 \& 0.000 \& 3.558 \& 0.000 \& 60.88 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.438 \& 0.000 \& 232.58 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.310 \& 0.000 \& 614.81 <br>
\hline \multirow[t]{3}{*}{T16} \& \multirow[t]{3}{*}{275.00-268.75} \& A \& \multirow[t]{3}{*}{1.852} \& 0.000 \& 0.000 \& 3.553 \& 0.000 \& 60.70 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.414 \& 0.000 \& 231.96 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.297 \& 0.000 \& 613.99 <br>
\hline \multirow[t]{3}{*}{T17} \& \multirow[t]{3}{*}{268.75-262.50} \& A \& \multirow[t]{3}{*}{1.848} \& 0.000 \& 0.000 \& 3.547 \& 0.000 \& 60.51 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.390 \& 0.000 \& 231.33 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.283 \& 0.000 \& 613.14 <br>
\hline \multirow[t]{3}{*}{T18} \& \multirow[t]{3}{*}{262.50-256.25} \& A \& \multirow[t]{3}{*}{1.843} \& 0.000 \& 0.000 \& 3.542 \& 0.000 \& 60.32 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.366 \& 0.000 \& 230.68 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.268 \& 0.000 \& 612.29 <br>
\hline \multirow[t]{3}{*}{T19} \& \multirow[t]{3}{*}{256.25-250.00} \& A \& \multirow[t]{3}{*}{1.839} \& 0.000 \& 0.000 \& 3.536 \& 0.000 \& 60.13 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.341 \& 0.000 \& 230.03 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.254 \& 0.000 \& 611.41 <br>
\hline \multirow[t]{3}{*}{T20} \& \multirow[t]{3}{*}{250.00-243.75} \& A \& \multirow[t]{3}{*}{1.834} \& 0.000 \& 0.000 \& 3.530 \& 0.000 \& 59.93 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.315 \& 0.000 \& 229.35 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 24.239 \& 0.000 \& 610.51 <br>
\hline \multirow[t]{3}{*}{T21} \& \multirow[t]{3}{*}{243.75-237.50} \& A \& \multirow[t]{3}{*}{1.830} \& 0.000 \& 0.000 \& 11.949 \& 0.000 \& 144.74 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.289 \& 0.000 \& 228.67 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 32.720 \& 0.000 \& 835.66 <br>
\hline T22 \& 237.50-231.25 \& A \& 1.825 \& 0.000 \& 0.000 \& 24.537 \& 0.000 \& 271.21 <br>
\hline
\end{tabular}

| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } 25 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation $f t$ \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Ice
Thickness
in \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
\text { ft }^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& | Weight |
| :--- |
| $l b$ | <br>

\hline \multirow{4}{*}{T23} \& \multirow{4}{*}{231.25-225.00} \& B \& \multirow{4}{*}{1.820} \& 0.000 \& 0.000 \& 18.263 \& 0.000 \& 227.97 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 45.440 \& 0.000 \& 1173.05 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 33.649 \& 0.000 \& 402.56 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.235 \& 0.000 \& 227.25 <br>
\hline \multirow{3}{*}{T24} \& \multirow{3}{*}{225.00-218.75} \& C \& \multirow{3}{*}{1.815} \& 0.000 \& 0.000 \& 45.414 \& 0.000 \& 1171.31 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 35.877 \& 0.000 \& 434.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.207 \& 0.000 \& 226.52 <br>
\hline \multirow{3}{*}{T25} \& \multirow{3}{*}{218.75-212.50} \& C \& \multirow{3}{*}{1.810} \& 0.000 \& 0.000 \& 45.388 \& 0.000 \& 1169.52 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 35.813 \& 0.000 \& 432.61 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.178 \& 0.000 \& 225.76 <br>
\hline \multirow{3}{*}{T26} \& \multirow{3}{*}{212.50-206.25} \& C \& \multirow{3}{*}{1.804} \& 0.000 \& 0.000 \& 45.360 \& 0.000 \& 1167.70 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 35.748 \& 0.000 \& 431.02 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 18.149 \& 0.000 \& 224.99 <br>
\hline \multirow{3}{*}{T27} \& \multirow{3}{*}{206.25-181.25} \& C \& \multirow{3}{*}{1.790} \& 0.000 \& 0.000 \& 45.332 \& 0.000 \& 1165.82 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 142.302 \& 0.000 \& 1707.54 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 72.285 \& 0.000 \& 891.92 <br>
\hline \multirow{3}{*}{T28} \& \multirow{3}{*}{181.25-175.00} \& C \& \multirow{3}{*}{1.775} \& 0.000 \& 0.000 \& 189.830 \& 0.000 \& 4772.75 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 37.721 \& 0.000 \& 456.45 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.988 \& 0.000 \& 220.82 <br>
\hline \multirow{3}{*}{T29} \& \multirow{3}{*}{175.00-168.75} \& C \& \multirow{3}{*}{1.769} \& 0.000 \& 0.000 \& 48.093 \& 0.000 \& 1198.14 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 38.218 \& 0.000 \& 462.87 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.953 \& 0.000 \& 219.92 <br>
\hline \multirow{3}{*}{T30} \& \multirow{3}{*}{168.75-162.50} \& C \& \multirow{3}{*}{1.763} \& 0.000 \& 0.000 \& 48.051 \& 0.000 \& 1195.70 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 38.129 \& 0.000 \& 460.72 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.916 \& 0.000 \& 218.98 <br>
\hline \multirow{3}{*}{T31} \& \multirow{3}{*}{162.50-156.25} \& C \& \multirow{3}{*}{1.756} \& 0.000 \& 0.000 \& 48.009 \& 0.000 \& 1193.17 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 38.037 \& 0.000 \& 458.50 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.879 \& 0.000 \& 218.02 <br>
\hline \multirow{3}{*}{T32} \& \multirow{3}{*}{156.25-150.00} \& C \& \multirow{3}{*}{1.749} \& 0.000 \& 0.000 \& 47.965 \& 0.000 \& 1190.56 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 37.942 \& 0.000 \& 456.20 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.840 \& 0.000 \& 217.02 <br>
\hline \multirow{3}{*}{T33} \& \multirow{3}{*}{150.00-125.00} \& C \& \multirow{3}{*}{1.730} \& 0.000 \& 0.000 \& 47.919 \& 0.000 \& 1187.86 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 150.751 \& 0.000 \& 1800.42 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 80.236 \& 0.000 \& 975.51 <br>
\hline \multirow{3}{*}{T34} \& \multirow{3}{*}{125.00-100.00} \& C \& \multirow{3}{*}{1.696} \& 0.000 \& 0.000 \& 198.043 \& 0.000 \& 4820.80 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 148.885 \& 0.000 \& 1756.10 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 90.038 \& 0.000 \& 1086.36 <br>
\hline \multirow{3}{*}{T35} \& \multirow{3}{*}{100.00-93.75} \& C \& \multirow{3}{*}{1.671} \& 0.000 \& 0.000 \& 201.545 \& 0.000 \& 4828.83 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 36.880 \& 0.000 \& 431.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 22.307 \& 0.000 \& 266.57 <br>
\hline \multirow{3}{*}{T36} \& \multirow{3}{*}{93.75-87.50} \& C \& \multirow{3}{*}{1.659} \& 0.000 \& 0.000 \& 50.191 \& 0.000 \& 1196.76 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 36.729 \& 0.000 \& 427.49 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 22.739 \& 0.000 \& 269.62 <br>
\hline \multirow{3}{*}{T37} \& \multirow{3}{*}{87.50-81.25} \& C \& \multirow{3}{*}{1.648} \& 0.000 \& 0.000 \& 50.105 \& 0.000 \& 1192.16 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 36.569 \& 0.000 \& 423.76 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 28.617 \& 0.000 \& 327.17 <br>
\hline \multirow{3}{*}{T38} \& \multirow{3}{*}{81.25-75.00} \& C \& \multirow{3}{*}{1.635} \& 0.000 \& 0.000 \& 50.013 \& 0.000 \& 1187.28 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 36.397 \& 0.000 \& 419.80 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 28.489 \& 0.000 \& 324.10 <br>
\hline \multirow{3}{*}{T39} \& \multirow{3}{*}{75.00-50.00} \& C \& \multirow{3}{*}{1.599} \& 0.000 \& 0.000 \& 49.915 \& 0.000 \& 1182.08 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 148.802 \& 0.000 \& 1704.36 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 112.491 \& 0.000 \& 1261.69 <br>
\hline \multirow{3}{*}{T40} \& \multirow{3}{*}{50.00-25.00} \& C \& \multirow{3}{*}{1.519} \& 0.000 \& 0.000 \& 198.539 \& 0.000 \& 4669.13 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 155.912 \& 0.000 \& 1754.50 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 109.259 \& 0.000 \& 1186.79 <br>
\hline \multirow{4}{*}{T41} \& \multirow{4}{*}{25.00-0.00} \& C \& \multirow{4}{*}{1.361} \& 0.000 \& 0.000 \& 196.069 \& 0.000 \& 4539.91 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 131.934 \& 0.000 \& 1396.91 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 90.513 \& 0.000 \& 919.58 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 168.232 \& 0.000 \& 3774.43 <br>
\hline
\end{tabular}

| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } 26 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by <br> Arielle Novak |

Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ | $C P_{Z}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  |  | Ice | Ice |
|  | in | in | in | in |  |
| T1 | $368.75-362.50$ | -0.2980 | 0.1786 | -0.6410 | 0.3601 |
| T2 | $362.50-356.25$ | -0.6773 | 0.4071 | -1.4281 | 0.8045 |
| T3 | $356.25-350.00$ | -0.1639 | 0.7324 | -0.3385 | 1.4182 |
| T4 | $350.00-343.75$ | 1.1050 | 1.5126 | 1.6224 | 2.5922 |
| T5 | $343.75-337.50$ | 1.9062 | 2.4418 | 2.3365 | 3.5918 |
| T6 | $337.50-331.25$ | 2.2801 | 2.8003 | 2.4843 | 3.7703 |
| T7 | $331.25-325.00$ | 2.2801 | 2.8003 | 2.4858 | 3.7725 |
| T8 | $325.00-318.75$ | 2.0836 | 0.2338 | 2.3138 | 1.1881 |
| T9 | $318.75-312.50$ | 2.0827 | 0.2337 | 2.3152 | 1.1887 |
| T10 | $312.50-306.25$ | 2.0819 | 0.2336 | 2.3166 | 1.1892 |
| T11 | $306.25-300.00$ | 1.7813 | 0.2074 | 2.1922 | 1.1384 |
| T12 | $300.00-293.75$ | 7.5728 | 3.8034 | 6.5528 | 3.7943 |
| T13 | $293.75-287.50$ | 10.1100 | 5.2583 | 8.2684 | 4.8059 |
| T14 | $287.50-281.25$ | 11.0625 | 5.8055 | 8.6591 | 5.0260 |
| T15 | $281.25-275.00$ | 11.0600 | 5.8037 | 8.6663 | 5.0302 |
| T16 | $275.00-268.75$ | 11.0574 | 5.8018 | 8.6737 | 5.0344 |
| T17 | $268.75-262.50$ | 11.0548 | 5.7998 | 8.6812 | 5.0388 |
| T18 | $262.50-256.25$ | 11.0521 | 5.7978 | 8.6889 | 5.0432 |
| T19 | $256.25-250.00$ | 10.9382 | 5.7134 | 8.6255 | 4.9998 |
| T20 | $250.00-243.75$ | 10.0957 | 5.2479 | 8.3184 | 4.8346 |
| T21 | $243.75-237.50$ | 7.3920 | 9.9011 | 4.3930 | 7.9636 |
| T22 | $237.50-231.25$ | 3.9734 | 14.1016 | -0.1259 | 10.9567 |
| T23 | $231.25-225.00$ | 3.5642 | 11.4041 | -0.2401 | 8.4185 |
| T24 | $225.00-218.75$ | 2.9141 | 9.4136 | -0.2348 | 7.1795 |
| T25 | $218.75-212.50$ | 3.5929 | 11.1762 | -0.2640 | 8.0679 |
| T26 | $212.50-206.25$ | 3.8349 | 11.7276 | -0.2648 | 8.2375 |
| T27 | $206.25-181.25$ | 3.4678 | 11.7743 | -0.8323 | 8.4089 |
| T28 | $181.25-175.00$ | 3.2077 | 10.9364 | -0.8990 | 7.1253 |
| T29 | $175.00-168.75$ | 3.1882 | 10.7791 | -0.9335 | 7.3055 |
| T30 | $168.75-162.50$ | 3.1882 | 10.7791 | -0.9259 | 7.3141 |
| T31 | $162.50-156.25$ | 3.0659 | 10.5272 | -0.9099 | 7.2977 |
| T32 | $156.25-150.00$ | 3.2602 | 11.0162 | -0.9249 | 7.4466 |
| T33 | $150.00-125.00$ | 3.1420 | 11.1034 | -0.7496 | 7.7985 |
| T34 | $125.00-100.00$ | 2.5535 | 9.4059 | -0.2703 | 7.3180 |
| T35 | $100.00-93.75$ | 2.4510 | 9.1171 | -0.2404 | 7.2083 |
| T36 | $93.75-87.50$ | 2.9997 | 10.6294 | -0.1860 | 7.9849 |
| T37 | $87.50-81.25$ | 3.7202 | 11.3205 | 0.6515 | 8.4859 |
| T38 | $81.25-75.00$ | 3.7202 | 11.3205 | 0.6643 | 8.4941 |
| T39 | $75.00-50.00$ | 3.6945 | 11.0256 | 0.6933 | 8.0719 |
|  | $50.00-25.00$ | 3.5838 | 10.2482 | 0.7556 | 7.1244 |
| $25.00-0.00$ | 3.4939 | 9.7927 | 0.8977 | 6.7460 |  |

## Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{gathered} \hline K_{a} \\ I c e \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 12 | 7/8 | $362.50-$ 365.00 | 0.6000 | 0.4924 |
| T2 | 12 | 7/8 | $356.25-$ 362.50 | 0.6000 | 0.4736 |


| tnxTOWer | Job | PTNL024A | Page |
| :---: | :--- | :--- | :--- |
|  | Project | Client | ANCHOR |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{gathered} K_{a} \\ I c e \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T3 | 11 | 7/8 | $350.00-$ 355.00 | 0.6000 | 0.4741 |
| T3 | 12 | 7/8 | $350.00-$ 356.25 | 0.6000 | 0.4741 |
| T4 | 10 | 7/8 | $343.75-$ 350.00 3 | 0.6000 | 0.4705 |
| T4 | 11 | 7/8 | $343.75-$ 350.00 | 0.6000 | 0.4705 |
| T4 | 12 | 7/8 | $343.75-$ 350.00 | 0.6000 | 0.4705 |
| T5 | 10 | 7/8 | $337.50-$ 343.75 | 0.6000 | 0.5629 |
| T5 | 11 | 7/8 | $337.50-$ 343.75 | 0.6000 | 0.5629 |
| T5 | 12 | 7/8 | $337.50-$ 343.75 | 0.6000 | 0.5629 |
| T6 | 10 | 7/8 | $331.25-$ 337.50 331.25 | 0.6000 | 0.5744 |
| T6 | 11 | 7/8 | $331.25-$ 337.50 | 0.6000 | 0.5744 |
| T6 | 12 | 7/8 | $331.25-$ 337.50 | 0.6000 | 0.5744 |
| T7 | 10 | 7/8 | $325.00-1$. | 0.6000 | 0.5749 |
| T7 | 11 | 7/8 | $325.00-$ 331.25 | 0.6000 | 0.5749 |
| T7 | 12 | 7/8 | $325.00-$ 331.25 | 0.6000 | 0.5749 |
| T8 | 9 | $15 / 8$ | $318.75-$ 325.00 | 0.6000 | 0.5660 |
| T8 | 10 | 7/8 | $318.75-$ 325.00 | 0.6000 | 0.5660 |
| T8 | 11 | 7/8 | $318.75-$ 325.00 | 0.6000 | 0.5660 |
| T8 | 12 | 7/8 | $318.75-$ 325.00 | 0.6000 | 0.5660 |
| T9 | 9 | $15 / 8$ | $312.50-$ 318.75 312.50 | 0.6000 | 0.5665 |
| T9 | 10 | 7/8 | $312.50-$ 318.75 | 0.6000 | 0.5665 |
| T9 | 11 | 7/8 | 312.50 318.75 318. | 0.6000 | 0.5665 |
| T9 | 12 | 7/8 | $312.50-$ 318.75 | 0.6000 | 0.5665 |
| T10 | 9 | $15 / 8$ | $306.25-$ 312.50 306 | 0.6000 | 0.5671 |
| T10 | 10 | 7/8 | $306.25-$ 312.50 | 0.6000 | 0.5671 |
| T10 | 11 | 7/8 | $306.25-$ 312.50 | 0.6000 | 0.5671 |
| T10 | 12 | 7/8 | $306.25-$ 312.50 | 0.6000 | 0.5671 |
| T11 | 9 | $15 / 8$ | $300.00-$ 306.25 | 0.6000 | 0.5567 |
| T11 | 10 | 7/8 | $300.00-$ 306.25 | 0.6000 | 0.5567 |
| TII | 11 | 7/8 | $\begin{array}{r} 300.00- \\ 306.25 \end{array}$ | 0.6000 | 0.5567 |
| T11 | 12 | 7/8 | $300.00-$ 306.25 | 0.6000 | 0.5567 |
| T12 | 9 | $15 / 8$ | $\begin{array}{r} 293.75- \\ 300.00 \end{array}$ | 0.6000 | 0.4705 |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 28 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | Date $14: 28: 2008 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T12 | 10 | 7/8 | $293.75-$ 300.00 | 0.6000 | 0.4705 |
| T12 | 11 | 7/8 | $293.75-$ 300.00 | 0.6000 | 0.4705 |
| T12 | 12 | 7/8 | $293.75-$ 300.00 | 0.6000 | 0.4705 |
| T12 | 13 | $15 / 8$ | $293.75-$ 300.00 | 0.6000 | 0.4705 |
| T12 | 14 | HYBRIFLEX $15 / 8$ | $293.75-$ 300.00 | 0.6000 | 0.4705 |
| T13 | 9 | $15 / 8$ | $287.50-$ 293.75 | 0.6000 | 0.5578 |
| T13 | 10 | 7/8 | $287.50-$ 293.75 | 0.6000 | 0.5578 |
| T13 | 11 | 7/8 | $287.50-$ 293.75 | 0.6000 | 0.5578 |
| T13 | 12 | 7/8 | $287.50-$ 293.75 | 0.6000 | 0.5578 |
| T13 | 13 | $15 / 8$ | $287.50-1$ | 0.6000 | 0.5578 |
| T13 | 14 | HYBRIFLEX $15 / 8$ | $287.50-$ 293.75 | 0.6000 | 0.5578 |
| T14 | 9 | $15 / 8$ | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T14 | 10 | 7/8 | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T14 | 11 | 7/8 | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T14 | 12 | 7/8 | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T14 | 13 | $15 / 8$ | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T14 | 14 | HYBRIFLEX $15 / 8$ | $281.25-$ 287.50 | 0.6000 | 0.5738 |
| T15 | 9 | $15 / 8$ | $275.00-$ 281.25 | 0.6000 | 0.5744 |
| T15 | 10 | 7/8 | $275.00-$ 281.25 | 0.6000 | 0.5744 |
| T15 | 11 | 7/8 | $275.00-$ 281.25 | 0.6000 | 0.5744 |
| T15 | 12 | 7/8 | $275.00-1$. | 0.6000 | 0.5744 |
| T15 | 13 | $15 / 8$ | $275.00-$ 281.25 | 0.6000 | 0.5744 |
| T15 | 14 | HYBRIFLEX $15 / 8$ | $275.00-$ 281.25 | 0.6000 | 0.5744 |
| T16 | 9 | $15 / 8$ | $268.75-$ 275.00 | 0.6000 | 0.5750 |
| T16 | 10 | 7/8 | $268.75-$ 275.00 | 0.6000 | 0.5750 |
| T16 | 11 | 7/8 | 268.75- | 0.6000 | 0.5750 |
| T16 | 12 | 7/8 | $268.75-$ 275.00 | 0.6000 | 0.5750 |
| T16 | 13 | $15 / 8$ | 268.75- | 0.6000 | 0.5750 |
| T16 | 14 | HYBRIFLEX $15 / 8$ | $\begin{array}{r} 268.75 \\ 275.00 \end{array}$ | 0.6000 | 0.5750 |
| T17 | 9 | $15 / 8$ | $\begin{array}{r} 262.50- \\ 268.75 \end{array}$ | 0.6000 | 0.5756 |
| T17 | 10 | 7/8 | $\begin{array}{r} 262.50- \\ 268.75 \end{array}$ | 0.6000 | 0.5756 |


| tnxTMOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
|  | CTNL024A | Project | ANCHOR |


| Tower <br> Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T17 | 11 | 7/8 | $\begin{array}{r} 262.50- \\ 268.75 \end{array}$ | 0.6000 | 0.5756 |
| T17 | 12 | 7/8 | $262.50-$ 268.75 | 0.6000 | 0.5756 |
| T17 | 13 | $15 / 8$ | $262.50-1$ | 0.6000 | 0.5756 |
| T17 | 14 | HYBRIFLEX $15 / 8$ | $\begin{array}{r} 262.50- \\ 268.75 \end{array}$ | 0.6000 | 0.5756 |
| T18 | 9 | $15 / 8$ | $256.25-$ 262.50 | 0.6000 | 0.5762 |
| T18 | 10 | 7/8 | $\begin{array}{r} 256.25- \\ 262.50 \end{array}$ | 0.6000 | 0.5762 |
| T18 | 11 | 7/8 | $256.25-$ 262.50 | 0.6000 | 0.5762 |
| T18 | 12 | 7/8 | 256.25- | 0.6000 | 0.5762 |
| T18 | 13 | $15 / 8$ | $256.25-$ 262.50 | 0.6000 | 0.5762 |
| T18 | 14 | HYBRIFLEX $15 / 8$ | $\begin{array}{r} 256.25- \\ 262.50 \end{array}$ | 0.6000 | 0.5762 |
| T19 | 9 | $15 / 8$ | $\begin{array}{r} 250.00- \\ 256.25 \end{array}$ | 0.6000 | 0.5724 |
| T19 | 10 | 7/8 | $250.00-1$ | 0.6000 | 0.5724 |
| T19 | 11 | 7/8 | $\begin{array}{r} 250.00- \\ 256.25 \end{array}$ | 0.6000 | 0.5724 |
| T19 | 12 | 7/8 | $\begin{array}{r} 250.00- \\ 256.25 \end{array}$ | 0.6000 | 0.5724 |
| T19 | 13 | $15 / 8$ | $250.00-1$ | 0.6000 | 0.5724 |
| T19 | 14 | HYBRIFLEX $15 / 8$ | $\begin{array}{r} 250.00- \\ 256.25 \end{array}$ | 0.6000 | 0.5724 |
| T20 | 9 | $15 / 8$ | $243.75-$ 250.00 | 0.6000 | 0.5621 |
| T20 | 10 | 7/8 | $\begin{array}{r} 243.75- \\ 250.00 \end{array}$ | 0.6000 | 0.5621 |
| T20 | 11 | 7/8 | $243.75-$ 250.00 | 0.6000 | 0.5621 |
| T20 | 12 | 7/8 | $243.75-$ 250.00 | 0.6000 | 0.5621 |
| T20 | 13 | $15 / 8$ | $\begin{array}{r} 243.75- \\ 250.00 \end{array}$ | 0.6000 | 0.5621 |
| T20 | 14 | HYBRIFLEX $15 / 8$ | $243.75-$ 250.00 | 0.6000 | 0.5621 |
| T21 | 9 | $15 / 8$ | $\begin{array}{r} 237.50- \\ 243.75 \end{array}$ | 0.6000 | 0.5628 |
| T21 | 10 | 7/8 | $\begin{array}{r} 237.50- \\ 243.75 \end{array}$ | 0.6000 | 0.5628 |
| T21 | 11 | 7/8 | $237.50-$ 243.75 | 0.6000 | 0.5628 |
| T21 | 12 | 7/8 | $237.50-$ 243.75 | 0.6000 | 0.5628 |
| T21 | 13 | $15 / 8$ | $237.50-$ 243.75 | 0.6000 | 0.5628 |
| T21 | 14 | HYBRIFLEX $15 / 8$ | $237.50-$ 243.75 | 0.6000 | 0.5628 |
| T21 | 15 | $15 / 8$ | $237.50-$ 240.00 | 0.6000 | 0.5628 |
| T21 | 16 | Fiber Trunk | $237.50-$ 240.00 | 0.6000 | 0.5628 |
| T21 | 17 | DC Trunk | $\begin{array}{r} 237.50- \\ 240.00 \end{array}$ | 0.6000 | 0.5628 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 30 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{gathered} K_{a} \\ \text { Ice } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T21 | 18 | Fiber Trunk | $237.50-$ 240.00 | 0.6000 | 0.5628 |
| T21 | 19 | DC Trunk | $237.50-$ 240.00 | 0.6000 | 0.5628 |
| T21 | 20 | 0.3" dia. RET | $237.50-$ 240.00 | 0.6000 | 0.5628 |
| T22 | 9 | $15 / 8$ | 231.25- | 0.6000 | 0.5634 |
| T22 | 10 | 7/8 | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T22 | 11 | 7/8 | 231.25- 237.50 | 0.6000 | 0.5634 |
| T22 | 12 | 7/8 | 231.25- | 0.6000 | 0.5634 |
| T22 | 13 | $15 / 8$ | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T22 | 14 | HYBRIFLEX $15 / 8$ | 231.25- | 0.6000 | 0.5634 |
| T22 | 15 | $15 / 8$ | 231.25- | 0.6000 | 0.5634 |
| T22 | 16 | Fiber Trunk | $\begin{array}{r} 231.25- \\ 237.50 \end{array}$ | 0.6000 | 0.5634 |
| T22 | 17 | DC Trunk | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T22 | 18 | Fiber Trunk | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T22 | 19 | DC Trunk | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T22 | 20 | 0.3' dia. RET | $231.25-$ 237.50 | 0.6000 | 0.5634 |
| T23 | 9 | $15 / 8$ | $225.00-$ 231.25 | 0.6000 | 0.5551 |
| T23 | 10 | 7/8 | $225.00-$ 231.25 | 0.6000 | 0.5551 |
| T23 | 11 | 7/8 | 225.00- | 0.6000 | 0.5551 |
| T23 | 12 | 7/8 | $225.00-1$ | 0.6000 | 0.5551 |
| T23 | 13 | $15 / 8$ | $225.00-1$ | 0.6000 | 0.5551 |
| T23 | 14 | HYBRIFLEX $15 / 8$ | $225.00-1$. | 0.6000 | 0.5551 |
| T23 | 15 | $15 / 8$ | $225.00-$ 231.25 | 0.6000 | 0.5551 |
| T23 | 16 | Fiber Trunk | $225.00-1$. | 0.6000 | 0.5551 |
| T23 | 17 | DC Trunk | $225.00-1$. | 0.6000 | 0.5551 |
| T23 | 18 | Fiber Trunk | 225.00- | 0.6000 | 0.5551 |
| T23 | 19 | DC Trunk | $225.00-$ | 0.6000 | 0.5551 |
| T23 | 20 | 0.3" dia. RET | $225.00-1$ | 0.6000 | 0.5551 |
| T23 | 22 | $6 \times 24$ HYBRID | $225.00-$ 230.00 | 0.6000 | 0.5551 |
| T24 | 9 | $15 / 8$ | 218.75- | 0.6000 | 0.5012 |
| T24 | 10 | 7/8 | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 11 | 7/8 | 218.75- | 0.6000 | 0.5012 |


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|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by <br> Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{gathered} K_{a} \\ I c e \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T24 | 12 | 7/8 | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 13 | $15 / 8$ | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 14 | HYBRIFLEX $15 / 8$ | 218.75- | 0.6000 | 0.5012 |
| T24 | 15 | $15 / 8$ | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 16 | Fiber Trunk | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 17 | DC Trunk | $218.75-$ 225.00 | 0.6000 | 0.5012 |
| T24 | 18 | Fiber Trunk | 218.75- | 0.6000 | 0.5012 |
| T24 | 19 | DC Trunk | 218.75- | 0.6000 | 0.5012 |
| T24 | 20 | 0.3 " dia. RET | 218.75- | 0.6000 | 0.5012 |
| T24 | 22 | $6 \times 24$ HYBRID | 218.75- | 0.6000 | 0.5012 |
| T25 | 9 | $15 / 8$ | $\begin{array}{r} 212.50- \\ 218.75 \end{array}$ | 0.6000 | 0.5750 |
| T25 | 10 | 7/8 | $\begin{array}{r} 212.50- \\ 218.75 \end{array}$ | 0.6000 | 0.5750 |
| T25 | 11 | 7/8 | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 12 | 7/8 | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 13 | $15 / 8$ | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 14 | HYBRIFLEX $15 / 8$ | $212.50-18$ | 0.6000 | 0.5750 |
| T25 | 15 | $15 / 8$ | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 16 | Fiber Trunk | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 17 | DC Trunk | $212.50-$ | 0.6000 | 0.5750 |
| T25 | 18 | Fiber Trunk | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 19 | DC Trunk | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 20 | 0.3 " dia. RET | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T25 | 22 | $6 \times 24$ HYBRID | $212.50-$ 218.75 | 0.6000 | 0.5750 |
| T26 | 9 | $15 / 8$ | 206.25- | 0.6000 | 0.5868 |
| T26 | 10 | 7/8 | 206.25- | 0.6000 | 0.5868 |
| T26 | 11 | 7/8 | 206.25- | 0.6000 | 0.5868 |
| T26 | 12 | 7/8 | 206.25- | 0.6000 | 0.5868 |
| T26 | 13 | $15 / 8$ | 206.25- | 0.6000 | 0.5868 |
| T26 | 14 | HYBRIFLEX $15 / 8$ | 206.25- | 0.6000 | 0.5868 |
| T26 | 15 | $15 / 8$ | 206.25- | 0.6000 | 0.5868 |
| T26 | 16 | Fiber Trunk | $\begin{array}{r} 206.25- \\ 212.50 \end{array}$ | 0.6000 | 0.5868 |


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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{gathered} K_{a} \\ I c e \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T26 | 17 | DC Trunk | $\begin{array}{r} 206.25- \\ 212.50 \end{array}$ | 0.6000 | 0.5868 |
| T26 | 18 | Fiber Trunk | 206.25- | 0.6000 | 0.5868 |
| T26 | 19 | DC Trunk | 206.25- | 0.6000 | 0.5868 |
| T26 | 20 | 0.3 " dia. RET | 206.25- | 0.6000 | 0.5868 |
| T26 | 22 | $6 \times 24$ HYBRID | 206.25- | 0.6000 | 0.5868 |
| T27 | 8 | 7/8 | $181.25-$ 200.00 | 0.6000 | 0.5888 |
| T27 | 9 | $15 / 8$ | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 10 | 7/8 | $181.25-$ 206.25 | 0.6000 | 0.5888 |
| T27 | 11 | 7/8 | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 12 | 7/8 | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 13 | $15 / 8$ | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 14 | HYBRIFLEX $15 / 8$ | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 15 | 15/8 | $181.25-$ 206.25 | 0.6000 | 0.5888 |
| T27 | 16 | Fiber Trunk | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 17 | DC Trunk | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 18 | Fiber Trunk | $181.25-$ 206.25 | 0.6000 | 0.5888 |
| T27 | 19 | DC Trunk | $\begin{array}{r} 181.25- \\ 206.25 \end{array}$ | 0.6000 | 0.5888 |
| T27 | 20 | 0.3 " dia. RET | $181.25-$ 206.25 | 0.6000 | 0.5888 |
| T27 | 22 | $6 \times 24$ HYBRID | $181.25-$ 206.25 | 0.6000 | 0.5888 |
| T28 | 7 | 7/8 | $175.00-$ 180.00 | 0.6000 | 0.5314 |
| T28 | 8 | 7/8 | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 9 | $15 / 8$ | $175.00-$ 181.25 175.00 | 0.6000 | 0.5314 |
| T28 | 10 | 7/8 | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 11 | 7/8 | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 12 | 7/8 | 175.00 181.25 | 0.6000 | 0.5314 |
| T28 | 13 | $15 / 8$ | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 14 | HYBRIFLEX $15 / 8$ | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 15 | $15 / 8$ | 175.00 181.25 | 0.6000 | 0.5314 |
| T28 | 16 | Fiber Trunk | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 17 | DC Trunk | 175.00 181.25 | 0.6000 | 0.5314 |
| T28 | 18 | Fiber Trunk | $175.00-$ 181.25 | 0.6000 | 0.5314 |


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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & \mathrm{Ice} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T28 | 19 | DC Trunk | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 20 | 0.3" dia. RET | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T28 | 22 | $6 \times 24$ HYBRID | $175.00-$ 181.25 | 0.6000 | 0.5314 |
| T29 | 7 | 7/8 | $\begin{array}{r} 168.75- \\ 175.00 \end{array}$ | 0.6000 | 0.5732 |
| T29 | 8 | 7/8 | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 9 | $15 / 8$ | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 10 | 7/8 | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 11 | 7/8 | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 12 | 7/8 | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 13 | $15 / 8$ | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 14 | HYBRIFLEX $15 / 8$ | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 15 | $15 / 8$ | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 16 | Fiber Trunk | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 17 | DC Trunk | $\begin{array}{r} 168.75- \\ 175.00 \end{array}$ | 0.6000 | 0.5732 |
| T29 | 18 | Fiber Trunk | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 19 | DC Trunk | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 20 | 0.3" dia. RET | $168.75-$ 175.00 | 0.6000 | 0.5732 |
| T29 | 22 | 6x24 HYBRID | $168.75-$ 175.00 162.50 | 0.6000 | 0.5732 |
| T30 | 7 | 7/8 | 162.50 168.75 | 0.6000 | 0.5742 |
| T30 | 8 | 7/8 | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 9 | $15 / 8$ | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 10 | 7/8 | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 11 | 7/8 | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 12 | 7/8 | 162.50 168.75 | 0.6000 | 0.5742 |
| T30 | 13 | $15 / 8$ | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 14 | HYBRIFLEX $15 / 8$ | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 15 | $15 / 8$ | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 16 | Fiber Trunk | $\begin{array}{r} 162.50- \\ 168.75 \end{array}$ | 0.6000 | 0.5742 |
| T30 | 17 | DC Trunk | $\begin{array}{r} 162.50- \\ 168.75 \end{array}$ | 0.6000 | 0.5742 |
| T30 | 18 | Fiber Trunk | $\begin{array}{r} 162.50- \\ 168.75 \end{array}$ | 0.6000 | 0.5742 |
| T30 | 19 | DC Trunk | $\begin{array}{r} 162.50- \\ 168.75 \end{array}$ | 0.6000 | 0.5742 |


| tnxTower | Job CTNL024A |  | $\begin{aligned} & \text { Page } 34 \text { of } 69 \end{aligned}$ |
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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Section | Feed Line <br> Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \\ \hline \end{gathered}$ | $\begin{gathered} K_{a} \\ \text { Ice } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T30 | 20 | 0.3" dia. RET | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T30 | 22 | 6x24 HYBRID | $162.50-$ 168.75 | 0.6000 | 0.5742 |
| T31 | 7 | 7/8 | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 8 | 7/8 | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 9 | $15 / 8$ | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 10 | 7/8 | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 11 | 7/8 | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 12 | 7/8 | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 13 | $15 / 8$ | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 14 | HYBRIFLEX $15 / 8$ | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 15 | $15 / 8$ | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 16 | Fiber Trunk | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 17 | DC Trunk | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 18 | Fiber Trunk | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 19 | DC Trunk | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 20 | 0.3 " dia. RET | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T31 | 22 | $6 \times 24$ HYBRID | $156.25-$ 162.50 | 0.6000 | 0.5778 |
| T32 | 7 | 7/8 | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 8 | 7/8 | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 9 | $15 / 8$ | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 10 | 7/8 | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 11 | 7/8 | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 12 | 7/8 | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 13 | $15 / 8$ | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 14 | HYBRIFLEX $15 / 8$ | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 15 | $15 / 8$ | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 16 | Fiber Trunk | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 17 | DC Trunk | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 18 | Fiber Trunk | $\begin{array}{r} 150.00- \\ 156.25 \end{array}$ | 0.6000 | 0.5897 |
| T32 | 19 | DC Trunk | $150.00-$ 156.25 | 0.6000 | 0.5897 |
| T32 | 20 | 0.3" dia. RET | $150.00-$ 156.25 | 0.6000 | 0.5897 |


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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T32 | 22 | 6x24 HYBRID | $\begin{array}{r} 150.00- \\ 156.25 \end{array}$ | 0.6000 | 0.5897 |
| T33 | 5 | 7/8 | $125.00-$ 140.00 | 0.6000 | 0.5924 |
| T33 | 6 | 1/2 | $125.00-$ 148.00 | 0.6000 | 0.5924 |
| T33 | 7 | 7/8 | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 8 | 7/8 | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 9 | $15 / 8$ | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 10 | 7/8 | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 11 | 7/8 | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 12 | 7/8 | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 13 | $15 / 8$ | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 14 | HYBRIFLEX $15 / 8$ | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 15 | $15 / 8$ | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 16 | Fiber Trunk | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 17 | DC Trunk | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 18 | Fiber Trunk | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 19 | DC Trunk | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 20 | 0.3 " dia. RET | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T33 | 22 | $6 \times 24$ HYBRID | $125.00-$ 150.00 | 0.6000 | 0.5924 |
| T34 | 4 | 1/2 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 5 | 7/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 6 | 1/2 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 7 | 7/8 | 100.00- 125.00 | 0.6000 | 0.5246 |
| T34 | 8 | 7/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 9 | $15 / 8$ | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 10 | 7/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 11 | 7/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 12 | 7/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 13 | $15 / 8$ | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 14 | HYBRIFLEX $15 / 8$ | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 15 | 15/8 | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 16 | Fiber Trunk | $100.00-$ 125.00 | 0.6000 | 0.5246 |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } 36 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T34 | 17 | DC Trunk | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 18 | Fiber Trunk | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 19 | DC Trunk | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T34 | 20 | 0.3 " dia. RET | 100.00 125.00 | 0.6000 | 0.5246 |
| T34 | 22 | $6 \times 24$ HYBRID | $100.00-$ 125.00 | 0.6000 | 0.5246 |
| T35 | 4 | 1/2 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 5 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 6 | 1/2 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 7 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 8 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 9 | $15 / 8$ | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 10 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 11 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 12 | 7/8 | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 13 | $15 / 8$ | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 14 | HYBRIFLEX $15 / 8$ | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 15 | $15 / 8$ | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 16 | Fiber Trunk | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 17 | DC Trunk | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 18 | Fiber Trunk | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 19 | DC Trunk | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 20 | 0.3 " dia. RET | 93.75-100.00 | 0.6000 | 0.5172 |
| T35 | 22 | $6 \times 24$ HYBRID | 93.75-100.00 | 0.6000 | 0.5172 |
| T36 | 3 | 1/2 | 87.50-88.00 | 0.6000 | 0.5870 |
| T36 | 4 | 1/2 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 5 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 6 | 1/2 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 7 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 8 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 9 | $15 / 8$ | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 10 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 11 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 12 | 7/8 | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 13 | $15 / 8$ | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 14 | HYBRIFLEX $15 / 8$ | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 15 | $15 / 8$ | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 16 | Fiber Trunk | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 17 | DC Trunk | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 18 | Fiber Trunk | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 19 | DC Trunk | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 20 | 0.3 " dia. RET | 87.50-93.75 | 0.6000 | 0.5870 |
| T36 | 22 | 6x24 HYBRID | 87.50-93.75 | 0.6000 | 0.5870 |
| T37 | 3 | 1/2 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 4 | 1/2 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 5 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 6 | 1/2 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 7 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 8 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 9 | $15 / 8$ | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 10 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 11 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 12 | 7/8 | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 13 | $15 / 8$ | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 14 | HYBRIFLEX $15 / 8$ | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 15 | $15 / 8$ | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 16 | Fiber Trunk | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 17 | DC Trunk | 81.25-87.50 | 0.6000 | 0.6000 |


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| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T37 | 18 | Fiber Trunk | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 19 | DC Trunk | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 20 | 0.3 " dia. RET | 81.25-87.50 | 0.6000 | 0.6000 |
| T37 | 22 | $6 \times 24$ HYBRID | 81.25-87.50 | 0.6000 | 0.6000 |
| T38 | 3 | 1/2 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 4 | 1/2 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 5 | 7/8 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 6 | 1/2 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 7 | 7/8 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 8 | $7 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 9 | $15 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 10 | 7/8 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 11 | $7 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 12 | 7/8 | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 13 | $15 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 14 | HYBRIFLEX $15 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 15 | $15 / 8$ | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 16 | Fiber Trunk | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 17 | DC Trunk | 75.00-81.25 | 0.6000 | 0.6000 |
| T38 | 18 | Fiber Trunk | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 19 | DC Trunk | $75.00-81.25$ | 0.6000 | 0.6000 |
| T38 | 20 | 0.3 " dia. RET | 75.00-81.25 | 0.6000 | 0.6000 |
| T38 | 22 | 6x24 HYBRID | $75.00-81.25$ | 0.6000 | 0.6000 |
| T39 | 2 | 7/8 | 50.00-62.00 | 0.6000 | 0.6000 |
| T39 | 3 | 1/2 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 4 | 1/2 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 5 | 7/8 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 6 | 1/2 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 7 | 7/8 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 8 | $7 / 8$ | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 9 | $15 / 8$ | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 10 | 7/8 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 11 | 7/8 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 12 | 7/8 | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 13 | $15 / 8$ | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 14 | HYBRIFLEX $15 / 8$ | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 15 | $15 / 8$ | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 16 | Fiber Trunk | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 17 | DC Trunk | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 18 | Fiber Trunk | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 19 | DC Trunk | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 20 | 0.3 " dia. RET | 50.00-75.00 | 0.6000 | 0.6000 |
| T39 | 22 | $6 \times 24$ HYBRID | 50.00-75.00 | 0.6000 | 0.6000 |
| T40 | 1 | 7/8 | 25.00-40.00 | 0.6000 | 0.6000 |
| T40 | 2 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 3 | 1/2 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 4 | 1/2 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 5 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 6 | 1/2 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 7 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 8 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 9 | $15 / 8$ | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 10 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 11 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 12 | 7/8 | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 13 | $15 / 8$ | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 14 | HYBRIFLEX $15 / 8$ | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 15 | $15 / 8$ | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 16 | Fiber Trunk | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 17 | DC Trunk | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 18 | Fiber Trunk | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 19 | DC Trunk | 25.00-50.00 | 0.6000 | 0.6000 |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 38 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Tower <br> Section | Feed Line <br> Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T40 | 20 | 0.3" dia. RET | 25.00-50.00 | 0.6000 | 0.6000 |
| T40 | 22 | 6x24 HYBRID | 25.00-50.00 | 0.6000 | 0.6000 |
| T41 | 1 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 2 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 3 | 1/2 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 4 | 1/2 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 5 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 6 | 1/2 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 7 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 8 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 9 | $15 / 8$ | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 10 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 11 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 12 | 7/8 | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 13 | $15 / 8$ | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 14 | HYBRIFLEX $15 / 8$ | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 15 | $15 / 8$ | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 16 | Fiber Trunk | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 17 | DC Trunk | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 18 | Fiber Trunk | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 19 | DC Trunk | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 20 | 0.3" dia. RET | 3.00-25.00 | 0.6000 | 0.6000 |
| T41 | 22 | 6x24 HYBRID | 3.00-25.00 | 0.6000 | 0.6000 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert \(f t\) \(f t\) ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front \\
\(f t^{2}\)
\end{tabular} \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight

$l b$ <br>

\hline Search Antenna \& C \& From Leg \& \[
$$
\begin{aligned}
& 1.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 370.00 \& | No Ice $1 / 2^{\prime \prime}$ Ice |
| :--- |
| 1" Ice | \& \[

$$
\begin{aligned}
& 1.28 \\
& 3.73 \\
& 6.18
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 3.73 \\
& 4.39 \\
& 5.05
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 300.00 \\
& 450.00 \\
& 600.00
\end{aligned}
$$
\] <br>

\hline \multicolumn{10}{|l|}{***} <br>
\hline \multirow[t]{2}{*}{10'6"x4' Pipe Mount} \& A \& From Leg \& 0.50 \& 0.0000 \& 355.00 \& No Ice \& 2.99 \& 2.99 \& 110.00 <br>
\hline \& \& \& 0.00
0.00 \& \& \& 1/2" Ice \& 5.62
6.25 \& 5.62
6.25 \& 150.00
190.00 <br>
\hline \multirow[t]{3}{*}{Rohn 6' Side-Arm} \& B \& From Leg \& 3.00 \& 0.0000 \& 355.00 \& No Ice \& 6.00 \& 6.00 \& 140.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 8.50 \& 8.50 \& 210.00 <br>
\hline \& \& \& 0.00 \& \& \& 1 I' Ice \& 11.00 \& 11.00 \& 280.00 <br>
\hline \multicolumn{10}{|l|}{***} <br>
\hline \multirow[t]{3}{*}{$20^{\prime} \times 3$ " Dia Ommi} \& C \& From Leg \& 1.00 \& 0.0000 \& 350.00 \& No Ice \& 5.70 \& 5.70 \& 50.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.03 \& 8.03 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 10.08 \& 10.08 \& 150.00 <br>
\hline \multirow[t]{3}{*}{6'x4' Pipe Mount} \& C \& From Leg \& 0.50 \& 0.0000 \& 350.00 \& No Ice \& 1.59 \& 1.59 \& 50.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.46 \& 2.46 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.83 \& 2.83 \& 90.00 <br>
\hline \multicolumn{10}{|l|}{***} <br>
\hline \multirow[t]{3}{*}{$10^{\prime} \times 3$ " Dia Ommi} \& B \& From Leg \& 3.00 \& 0.0000 \& 325.00 \& No Ice \& 2.87 \& 2.87 \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 4.03 \& 4.03 \& 50.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 5.03 \& 5.03 \& 80.00 <br>
\hline ROHN 3-ft Side Arm \& B \& From Leg \& 2.00 \& 0.0000 \& 325.00 \& No Ice \& 3.10 \& 3.10 \& 70.00 <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.00 | 5.00 | 100.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 6.90 | 6.90 | 130.00 |
| *** ${ }^{\text {c* }}$ |  |  |  |  |  |  |  |  |  |
| $20^{\prime} \times 3$ " Dia Omni | C | From Leg | 1.00 | 0.0000 | 250.00 | No Ice | 5.90 | 5.90 | 50.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 8.03 | 8.03 | 90.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 10.08 | 10.08 | 150.00 |
| 6'x4" Pipe Mount | C | From Leg | 0.50 | 0.0000 | 250.00 | No Ice | 1.63 | 1.63 | 50.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.46 | 2.46 | 70.00 |
|  |  |  | 0.00 |  |  | I" Ice | 2.83 | 2.83 | 90.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | A | From Leg | 1.00 | 0.0000 | 200.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| (4) Yagi | C | From Leg | 1.00 | 0.0000 | 180.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 8.00 | 8.00 | 80.00 |
| (2) $5^{\prime} 3$ "x4" Pipe Mount | C | From Leg | 1.00 | 0.0000 | 180.00 | No Ice | 1.44 | 2.44 | 60.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.21 | 2.21 | 70.00 |
|  |  |  | 0.00 |  |  | 1 " Ice | 2.54 | 2.54 | 90.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | B | From Leg | 1.00 | 0.0000 | 148.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | I" Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | C | From Leg | 1.00 | 0.0000 | 140.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | A | From Leg | 1.00 | 0.0000 | 125.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | 1 I' Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| X-Style | A | From Leg | 1.00 | 0.0000 | 88.00 |  |  |  |  |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.00 | 2.50 | 30.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 2.50 | 3.00 | 40.00 |
| *** |  |  |  |  |  |  |  |  |  |
| (2) X-Style | B | From Leg | 1.00 | 0.0000 | 88.00 | No Ice | 1.50 | 2.00 | 20.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.00 | 2.50 | 30.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 2.50 | 3.00 | 40.00 |
| *** |  |  |  |  |  |  |  |  |  |
| X-Style | A | From Leg | 1.00 | 0.0000 | 88.00 | No Ice | 1.50 | 2.00 | 20.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.00 | 2.50 | 30.00 |
|  |  |  | 0.00 |  |  | 1 " Ice | 2.50 | 3.00 | 40.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | C | From Leg | 1.00 | 0.0000 | 62.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | I" Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| Yagi | A | From Leg | 1.00 | 0.0000 | 40.00 | No Ice | 5.00 | 5.00 | 40.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 6.50 | 6.50 | 60.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 8.00 | 8.00 | 80.00 |
| *** |  |  |  |  |  |  |  |  |  |
| HPA-65R-BUU-H6 | A | From Leg | 3.00 | 0.0000 | 242.50 | No Ice | 9.66 | 6.45 | 50.00 |
|  |  |  | -6.00 |  |  | 1/2" Ice | 10.13 | 6.91 | 110.00 |
|  |  |  | 0.00 |  |  | 1 " Ice | 10.61 | 7.38 | 180.00 |
| HPA-65R-BUU-H8 | B | From Leg | 3.00 | 0.0000 | 242.50 | No Ice | 12.98 | 7.52 | 70.00 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 40 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or Leg
\end{tabular} \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front
\[
f t^{2}
\]
\end{tabular} \& \(C_{A} A_{A}\) Side
\[
f t^{2}
\] \& Weight

$l b$ <br>
\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& -6.00 \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{242.50} \& 1/2" Ice \& 13.56 \& 8.09 \& 140.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.15 \& 8.67 \& 220.00 <br>
\hline HPA-65R-BUU-H8 \& \& \& 3.00 \& \& \& No Ice \& 12.98 \& 7.52 \& 70.00 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 13.56 \& 8.09 \& 140.00 <br>
\hline \multirow{4}{*}{80010965} \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 14.15 \& 8.67 \& 220.00 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 13.81 \& 5.83 \& 110.00 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 14.35 \& 6.32 \& 190.00 <br>
\hline \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& 1" Ice \& 14.89 \& 6.82 \& 270.00 <br>
\hline \multirow[t]{3}{*}{80010966} \& \& \& 3.00 \& \& \& No Ice \& 17.36 \& 7.50 \& 130.00 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 17.99 \& 8.09 \& 220.00 <br>
\hline \& \multirow{3}{*}{C} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{1 \prime}$ Ice \& 18.63 \& 8.69 \& 320.00 <br>
\hline \multirow[t]{3}{*}{80010966} \& \& \& 3.00 \& \& \& No Ice \& 17.36 \& 7.50 \& 130.00 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 17.99 \& 8.09 \& 220.00 <br>
\hline \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& 1 Ice \& 18.63 \& 8.69 \& 320.00 <br>
\hline \multirow[t]{3}{*}{80010965} \& \& \& 3.00 \& \& \& No Ice \& 13.81 \& 5.83 \& 110.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 14.35 \& 6.32 \& 190.00 <br>
\hline \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 14.89 \& 6.82 \& 270.00 <br>
\hline \multirow[t]{3}{*}{80010966} \& \& \& 3.00 \& \& \& No Ice \& 17.36 \& 7.50 \& 130.00 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 17.99 \& 8.09 \& 220.00 <br>
\hline \& \multirow{3}{*}{C} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& 1" Icc \& 18.63 \& 8.69 \& 320.00 <br>
\hline \multirow[t]{3}{*}{80010966} \& \& \& 3.00 \& \& \& No Ice \& 17.36 \& 7.50 \& 130.00 <br>
\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 17.99 \& 8.09 \& 220.00 <br>
\hline \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& 1" Ice \& 18.63 \& 8.69 \& 320.00 <br>
\hline \multirow[t]{3}{*}{7770.00} \& \& \& 3.00 \& \& \& No Ice \& 5.51 \& 2.93 \& 40.00 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" Ice \& 5.87 \& 3.27 \& 70.00 <br>
\hline \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 6.23 \& 3.63 \& 110.00 <br>
\hline \multirow[t]{3}{*}{7770.00} \& \& \& 3.00 \& \& \& No Ice \& 5.51 \& 2.93 \& 40.00 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" Ice \& 5.87 \& 3.27 \& 70.00 <br>
\hline \& \multirow{3}{*}{C} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 6.23 \& 3.63 \& 110.00 <br>
\hline \multirow[t]{3}{*}{7770.00} \& \& \& 3.00 \& \& \& No Ice \& 5.51 \& 2.93 \& 40.00 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" Ice \& 5.87 \& 3.27 \& 70.00 <br>
\hline \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 6.23 \& 3.63 \& 110.00 <br>
\hline \multirow[t]{3}{*}{(2) LPG21401 TMA} \& \& \& 3.00 \& \& \& No Ice \& 0.82 \& 0.35 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.94 \& 0.44 \& 25.00 <br>
\hline \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 1.06 \& 0.54 \& 30.00 <br>
\hline \multirow[t]{3}{*}{(2) LPG21401 TMA} \& \& \& 3.00 \& \& \& No Ice \& 0.82 \& 0.35 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.94 \& 0.44 \& 25.00 <br>
\hline \& \multirow{3}{*}{C} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& 1 " Ice \& 1.06 \& 0.54 \& 30.00 <br>
\hline \multirow[t]{3}{*}{(2) LPG21401 TMA} \& \& \& 3.00 \& \& \& No Ice \& 0.82 \& 0.35 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.94 \& 0.44 \& 25.00 <br>
\hline \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 1.06 \& 0.54 \& 30.00 <br>
\hline \multirow[t]{2}{*}{8843 B2/B66A} \& \& \& 3.00 \& \& \& No Ice \& 1.64 \& 1.35 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.80 \& 1.50 \& 90.00 <br>
\hline \multirow{3}{*}{8843 B2/B66A} \& \multirow{3}{*}{B} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 1.97 \& 1.65 \& 110.00 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.64 \& 1.35 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.80 \& 1.50 \& 90.00 <br>
\hline \multirow{3}{*}{8843 B2/B66A} \& \multirow{3}{*}{C} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 1.97 \& 1.65 \& 110.00 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.64 \& 1.35 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' Ice \& 1.80 \& 1.50 \& 90.00 <br>
\hline \multirow{3}{*}{4449 B5/B12} \& \multirow{3}{*}{A} \& \multirow{3}{*}{From Leg} \& 0.00 \& \multirow{3}{*}{0.0000} \& \multirow{3}{*}{242.50} \& $1{ }^{\prime \prime}$ Ice \& 1.97 \& 1.65 \& 110.00 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.97 \& 1.41 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.14 \& 1.56 \& 90.00 <br>
\hline \multirow{4}{*}{4449 B5/B12} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Leg} \& 0.00 \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{242.50} \& $1^{\prime \prime}$ Ice \& 2.33 \& 1.73 \& 110.00 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 1.97 \& 1.41 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2' Ice \& 2.14 \& 1.56 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.33 \& 1.73 \& 110.00 <br>
\hline 4449 B5/B12 \& C \& From Leg \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.97 \& 1.41 \& 70.00 <br>
\hline
\end{tabular}

| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | Page <br> 41 of 69 |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side \& Weight

$l b$ <br>
\hline \multirow{5}{*}{B14 4478} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& 0.00 \& \& \& 1/2" Ice \& 2.14 \& 1.56 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 2.33 \& 1.73 \& 110.00 <br>
\hline \& \& \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.84 \& 1.06 \& 60.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.01 \& 1.20 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 2.19 \& 1.34 \& 90.00 <br>
\hline \multirow[t]{3}{*}{B14 4478} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.84 \& 1.06 \& 60.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.01 \& 1.20 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.19 \& 1.34 \& 90.00 <br>
\hline \multirow[t]{3}{*}{B14 4478} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.84 \& 1.06 \& 60.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.01 \& 1.20 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.19 \& 1.34 \& 90.00 <br>
\hline \multirow[t]{3}{*}{DC6-48-60-18-8F Surge Arrestor} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.91 \& 1.91 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.10 \& 2.10 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.29 \& 2.29 \& 60.00 <br>
\hline \multirow[t]{3}{*}{DC6-48-60-18-8F Surge Arrestor} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.91 \& 1.91 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.10 \& 2.10 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.29 \& 2.29 \& 60.00 <br>
\hline \multirow[t]{3}{*}{DC6-48-60-18-8F Surge Arrestor} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 242.50 \& No Ice \& 1.91 \& 1.91 \& 20.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.10 \& 2.10 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.29 \& 2.29 \& 60.00 <br>
\hline \multirow[t]{3}{*}{Pirod 12' T-Frame Sector Mount} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 13.60 \& 13.60 \& 470.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 18.40 \& 18.40 \& 600.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 23.20 \& 23.20 \& 730.00 <br>
\hline \multirow[t]{3}{*}{Pirod 12' T-Frame Sector Mount} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 13.60 \& 13.60 \& 470.00 <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 18.40 \& 18.40 \& 600.00 <br>

\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 23.20 \& 23.20 \& 730.00 <br>
\hline \multirow[t]{3}{*}{Pirod 12' T-Frame Sector Mount} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 13.60 \& 13.60 \& 470.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 18.40 \& 18.40 \& 600.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 23.20 \& 23.20 \& 730.00 <br>
\hline \multirow[t]{3}{*}{Site Pro Horizontal Stabilizer SFS-H} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 2.00 \& 2.00 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.50 \& 3.50 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 5.00 \& 5.00 \& 130.00 <br>
\hline \multirow[t]{3}{*}{Site Pro Horizontal Stabilizer SFS-H} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 2.00 \& 2.00 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.50 \& 3.50 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 5.00 \& 5.00 \& 130.00 <br>
\hline \multirow[t]{3}{*}{Site Pro Horizontal Stabilizer SFS-H} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 1.00 \& 0.0000 \& 242.50 \& No Ice \& 2.00 \& 2.00 \& 70.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.50 \& 3.50 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& 1 Ice \& 5.00 \& 5.00 \& 130.00 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{QUAD656C0000} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& \& 13.24 \& 5.62 \& 60.00 <br>

\hline \& \& \& -6.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 13.75 \& 6.09 \& 130.00 <br>

\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.27 \& 6.56 \& 210.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 9.48 \& 6.18 \& 160.00 <br>
\hline \multirow[t]{3}{*}{LNX-6514DS-T4M} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.17 \& 5.41 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.63 \& 5.86 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 9.10 \& 6.33 \& 150.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.48 \& 6.18 \& 160.00 <br>
\hline \multirow[t]{3}{*}{QUAD656C0000} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 13.24 \& 5.62 \& 60.00 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 13.75 \& 6.09 \& 130.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 14.27 \& 6.56 \& 210.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 9.48 \& 6.18 \& 160.00 <br>
\hline
\end{tabular}

| tnxTower | Job | CTNL024A | $\begin{aligned} & \text { Page } 42 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side \& Weight

$l b$ <br>
\hline \multirow[t]{3}{*}{LNX-6514DS-T4M} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.17 \& 5.41 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.63 \& 5.86 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 9.10 \& 6.33 \& 150.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 9.48 \& 6.18 \& 160.00 <br>
\hline \multirow[t]{3}{*}{QUAD656C0000} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 13.24 \& 5.62 \& 60.00 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 13.75 \& 6.09 \& 130.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.27 \& 6.56 \& 210.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>

\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& $$
100.00
$$ <br>

\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Icc \& 9.48 \& 6.18 \& 160.00 <br>
\hline \multirow[t]{3}{*}{LNX-6514DS-T4M} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.17 \& 5.41 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.63 \& 5.86 \& 90.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.10 \& 6.33 \& 150.00 <br>
\hline \multirow[t]{3}{*}{HBXX-6517DS} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 8.53 \& 5.24 \& 50.00 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 9.00 \& 5.71 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.48 \& 6.18 \& 160.00 <br>
\hline \multirow[t]{3}{*}{RRH4x45/2x90-AWS} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.58 \& 1.69 \& 80.00 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 2.79 \& 1.87 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 3.01 \& 2.06 \& 120.00 <br>
\hline \multirow[t]{3}{*}{RRH4x45/2x90-AWS} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.58 \& 1.69 \& 80.00 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 2.79 \& 1.87 \& 100.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.01 \& 2.06 \& 120.00 <br>

\hline \multirow[t]{3}{*}{RRH4x45/2x90-AWS} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.58 \& 1.69 \& $$
80.00
$$ <br>

\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 2.79 \& 1.87 \& $$
100.00
$$ <br>

\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 3.01 \& 2.06 \& 120.00 <br>
\hline \multirow[t]{3}{*}{RRH4×30-B13} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.16 \& 1.62 \& 60.00 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 2.35 \& 1.79 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 2.55 \& 1.97 \& 100.00 <br>
\hline \multirow[t]{3}{*}{RRH4×30-B13} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.16 \& 1.62 \& 60.00 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 2.35 \& 1.79 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.55 \& 1.97 \& 100.00 <br>
\hline \multirow[t]{3}{*}{RRH4×30-B13} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 2.16 \& 1.62 \& 60.00 <br>
\hline \& \& \& -4.00 \& \& \& 1/2" Ice \& 2.35 \& 1.79 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.55 \& 1.97 \& 100.00 <br>
\hline \multirow[t]{3}{*}{DB-T1-6Z-8AB-0Z} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 4.80 \& 2.00 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.07 \& 2.19 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.35 \& 2.39 \& 120.00 <br>
\hline \multirow[t]{3}{*}{DB-T1-6Z-8AB-0Z} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 305.00 \& No Ice \& 4.80 \& 2.00 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Icc \& 5.07 \& 2.19 \& 80.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.35 \& 2.39 \& 120.00 <br>
\hline \multirow[t]{3}{*}{Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 305.00 \& No Ice \& 16.60 \& 16.60 \& 560.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.80 \& 19.80 \& 700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 23.00 \& 23.00 \& 840.00 <br>
\hline \multirow[t]{3}{*}{Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& 0.0000 \& 305.00 \& No Ice \& 16.60 \& 16.60 \& 560.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.80 \& 19.80 \& 700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 23.00 \& 23.00 \& 840.00 <br>
\hline \multirow[t]{3}{*}{Rohn $6^{\prime} \times 12^{\prime}$ Boom Gate} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 1.00 \& 0.0000 \& 305.00 \& No Ice \& 16.60 \& 16.60 \& 560.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.80 \& 19.80 \& 700.00 <br>
\hline \& \& \& 0.00 \& \& \& I" Ice \& 23.00 \& 23.00 \& 840.00 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{$$
\begin{gathered}
\text { APX16DWV-16DWV-S-E-A } \\
20 \\
\text { (T-MOBILE) }
\end{gathered}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& 0.0000 \& 230.00 \& No Ice \& 6.46 \& 2.15 \& 40.70 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.83 \& 2.49 \& 73.65 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.21 \& 2.84 \& 111.47 <br>

\hline \multirow[t]{2}{*}{$$
\begin{gathered}
\text { APX16DWV-16DWV-S-E-A } \\
20
\end{gathered}
$$} \& \multirow[t]{2}{*}{B} \& \multirow[t]{2}{*}{From Leg} \& 3.00 \& 0.0000 \& 230.00 \& No Ice \& 6.46 \& 2.15 \& 40.70 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.83 \& 2.49 \& 73.65 <br>
\hline
\end{tabular}

| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 43 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front
\[
f t^{2}
\]
\end{tabular} \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Side \\
\(f t^{2}\)
\end{tabular} \& Weight

$l b$ <br>
\hline (T-MOBILE) \& \multirow{4}{*}{C} \& \& 0.00 \& \& \& 1" Ice \& 7.21 \& 2.84 \& 111.47 <br>
\hline APX16DWV-16DWV-S-E-A \& \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 6.46 \& 2.15 \& 40.70 <br>
\hline 20 \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.83 \& 2.49 \& 73.65 <br>
\hline (T-MOBILE) \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 7.21 \& 2.84 \& 111.47 <br>

\hline \multirow[t]{3}{*}{| APXVAALL24 43-U-NA20 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 20.24 \& 8.89 \& 153.30 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 20.89 \& 9.49 \& 265.89 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 21.54 \& 10.09 \& 387.02 <br>

\hline \multirow[t]{3}{*}{| APXVAALL24 43-U-NA20 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 20.24 \& 8.89 \& 153.30 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 20.89 \& 9.49 \& 265.89 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 21.54 \& 10.09 \& 387.02 <br>

\hline \multirow[t]{3}{*}{| APXVAALL24_43-U-NA20 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 20.24 \& 8.89 \& 153.30 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 20.89 \& 9.49 \& 265.89 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 21.54 \& 10.09 \& 387.02 <br>

\hline \multirow[t]{3}{*}{| AIR 6449 B41 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 5.68 \& 2.49 \& 104.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.98 \& 2.72 \& 143.12 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 6.29 \& 2.95 \& 186.46 <br>

\hline \multirow[t]{3}{*}{| AIR 6449 B4I |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 5.68 \& 2.49 \& 104.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.98 \& 2.72 \& 143.12 <br>
\hline \& \& \& 0.00 \& \& \& I" Ice \& 6.29 \& 2.95 \& 186.46 <br>

\hline \multirow[t]{3}{*}{| AIR 6449 B4I |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 5.68 \& 2.49 \& 104.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.98 \& 2.72 \& 143.12 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 6.29 \& 2.95 \& 186.46 <br>
\hline \multirow[t]{3}{*}{RADIO 4460 B25_B66 (T-MOBILE)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 2.14 \& 1.50 \& 108.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.32 \& 1.65 \& 130.16 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\text {" Ice }}$ \& 2.51 \& 1.81 \& 155.36 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { RADIO } 4460 \text { B25_B66 } \\
& \text { (T-MOBILE) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 2.14 \& 1.50 \& 108.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.32 \& 1.65 \& 130.16 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 2.51 \& 1.81 \& 155.36 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { RADIO } 4460 \text { B25_B66 } \\
& \text { (T-MOBILE) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 2.14 \& 1.50 \& 108.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.32 \& 1.65 \& 130.16 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 2.51 \& 1.81 \& 155.36 <br>

\hline \multirow[t]{3}{*}{| RADIO 4480 B71 + B85 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 1.63 \& 1.00 \& 74.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.13 \& 89.91 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.95 \& 1.27 \& 108.43 <br>
\hline \multirow[t]{3}{*}{RADIO 4480 B7I + B85 (T-MOBILE)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 1.63 \& 1.00 \& 74.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.13 \& 89.91 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.95 \& 1.27 \& 108.43 <br>

\hline \multirow[t]{3}{*}{| RADIO 4480 B71+B85 |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 1.63 \& 1.00 \& 74.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.13 \& 89.91 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\text {" Ice }}$ \& 1.95 \& 1.27 \& 108.43 <br>
\hline \multirow[t]{3}{*}{Site Pro 1 VFA12-HD (T-MOBILE)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 13.20 \& 9.20 \& 658.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.50 \& 14.60 \& 804.00 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 25.80 \& 19.50 \& 1015.00 <br>
\hline \multirow[t]{3}{*}{Site Pro 1 VFA12-HD (T-MOBILE)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 13.20 \& 9.20 \& 658.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.50 \& 14.60 \& 804.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 25.80 \& 19.50 \& 1015.00 <br>
\hline \multirow[t]{3}{*}{Site Pro 1 VFA12-HD (T-MOBILE)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 13.20 \& 9.20 \& 658.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 19.50 \& 14.60 \& 804.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 25.80 \& 19.50 \& 1015.00 <br>
\hline \multirow[t]{3}{*}{(4) 7'x2" Antenna Mount Pipe (T-MOBILE)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 1.66 \& 1.66 \& 26.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.39 \& 2.39 \& 38.58 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 2.83 \& 2.83 \& 55.84 <br>
\hline \multirow[t]{3}{*}{(4) $7^{\prime} \times 2^{\prime \prime}$ Antenna Mount Pipe (T-MOBILE)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{230.00} \& No Ice \& 1.66 \& 1.66 \& 26.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.39 \& 2.39 \& 38.58 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 2.83 \& 2.83 \& 55.84 <br>

\hline \multirow[t]{2}{*}{| (4) 7'x2" Antenna Mount Pipe |
| :--- |
| (T-MOBILE) |} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{From Leg} \& 1.50 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{230.00} \& No Ice \& 1.66 \& 1.66 \& 26.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.39 \& 2.39 \& 38.58 <br>
\hline
\end{tabular}

| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 44 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& Offset Type \& Offsets:
Horz
Lateral
Vert
\(f t\)
\(f t\)
\(f t\) \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\) Side
\[
f t^{2}
\] \& Weight

$l b$ <br>
\hline *** \& \& \& 0.00 \& \& \& 1" Ice \& 2.83 \& 2.83 \& 55.84 <br>
\hline
\end{tabular}

## Dishes

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Dish <br> Type | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ | Azimuth Adjustment <br> - | $3 d B$ <br> Beam <br> Width <br> 0 | Elevation | Outside Diameter. <br> ft |  | Aperture Area <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $8^{\prime}$ Dish | A | Paraboloid w/o | From | 1.00 | 0.0000 |  | 355.00 | 8.00 | No Ice | 50.27 | 100.00 |
|  |  | Radome | Leg | 0.00 |  |  |  |  | 1/2" Ice | 51.32 | 260.00 |
|  |  |  |  | 0.00 |  |  |  |  | 1" Ice | 52.37 | 490.00 |

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy |
| 3 | 1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy |
| 4 | 1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy |
| 5 | 1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy |
| 6 | 1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy |
| 7 | 1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy |
| 8 | 1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy |
| 9 | 1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy |
| 10 | 1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy |
| 11 | 1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy |
| 12 | 1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy |
| 13 | 1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy |
| 14 | 1.2 Dead+1.0 Ice+1.0 Temp+Guy |
| 15 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 16 | 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 17 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 18 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 19 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0 \mathrm{Ice}+1.0 \mathrm{Temp}+1.0 \mathrm{Guy}$ |
| 20 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp+1.0 Guy |
| 21 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 22 | 1.2 Dead+1.0 Wind $210 \mathrm{deg}+1.0$ Ice+1.0 Temp+1.0 Guy |
| 23 | 1.2 Dead+1.0 Wind $240 \mathrm{deg}+1.0$ Ice+1.0 Temp+1.0 Guy |
| 24 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy |
| 25 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0 \mathrm{Ice}+1.0 \mathrm{Temp}+1.0 \mathrm{Guy}$ |
| 26 | 1.2 Dead+1.0 Wind $330 \mathrm{deg}+1.0$ Ice+1.0 Temp+1.0 Guy |
| 27 | Dead+Wind 0 deg - Service+Guy |
| 28 | Dead+Wind 30 deg - Service+Guy |
| 29 | Dead+Wind 60 deg - Service+Guy |
| 30 | Dead+Wind 90 deg - Service+Guy |


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| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Comb. <br> No. | Description |  |
| :---: | :--- | :--- |
| 31 | Dead+Wind 120 deg - Service+Guy |  |
| 32 | Dead+Wind 150 deg - Service+Guy |  |
| 33 | Dead+Wind 180 deg - Service+Guy |  |
| 34 | Dead+Wind 210 deg - Service+Guy |  |
| 35 | Dead+Wind 240 deg - Service+Guy |  |
| 36 | Dead+Wind 270 deg - Service+Guy |  |
| 37 | Dead+Wind 300 deg - Service+Guy |  |
| 38 | Dead+Wind 330 deg - Service+Guy |  |


|  |  | Maximum Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Condition | Gov. <br> Load <br> Comb | Vertical $l b$ | $\begin{gathered} \text { Horizontal, } X \\ l b \end{gathered}$ | $\begin{gathered} \text { Horizontal, Z } \\ l b \end{gathered}$ |
| $\text { Guy C@ }{ }_{\mathrm{ft}} 251.45$ | Max. Vert | 10 | -6511.44 | -3245.33 | 1873.15 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 10 | -6511.44 | -3245.33 | 1873.15 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 3 | -28865.84 | -18188.58 | 11280.46 |
|  | Min. Vert | 4 | -29638.84 | -19075.21 | 11018.02 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 4 | -29638.84 | -19075.21 | 11018.02 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 10 | -6511.44 | -3245.33 | 1873.15 |
| $\text { Guy B } \underset{\mathrm{ft}}{\text { @ }} 247.51$ | Max. Vert | 6 | -6055.01 | 3084.86 | 1780.43 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 12 | -29380.62 | 19302.74 | 11151.59 |
|  | Max. $\mathrm{H}_{2}$ | 13 | -28391.21 | 18282.38 | 11324.37 |
|  | Min. Vert | 12 | -29380.62 | 19302.74 | 11151.59 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 6 | -6055.01 | 3084.86 | 1780.43 |
|  | Min. $\mathrm{H}_{2}$ | 6 | -6055.01 | 3084.86 | 1780.43 |
| Guy A@247.15 | Max. Vert | 2 | -6189.51 | 0.46 | -3534.51 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -19239.20 | 1469.52 | -13643.90 |
|  | Max. $\mathrm{H}_{2}$ | 2 | -6189.51 | 0.46 | -3534.51 |
|  | Min. Vert | 8 | -31977.07 | -3.95 | -23634.57 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -19104.73 | -1470.40 | -13550.96 |
|  | Min. $\mathrm{H}_{\text {z }}$ | 8 | -31977.07 | -3.95 | -23634.57 |
| $\begin{gathered} \text { Guy C@ } 227.42 \\ \mathrm{ft} \end{gathered}$ | Max. Vert | 10 | -4664.75 | -2452.89 | 1417.84 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 10 | -4664.75 | -2452.89 | 1417.84 |
|  | Max. $\mathrm{H}_{2}$ | 3 | -60652.69 | -45064.16 | 27170.29 |
|  | Min. Vert | 4 | -62310.43 | -46859.86 | 27018.06 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 4 | -62310.43 | -46859.86 | 27018.06 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 10 | -4664.75 | -2452.89 | 1417.84 |
| Guy B @ 219.43 | Max. Vert | 6 | -4403.74 | 2298.82 | 1328.83 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 12 | -62497.93 | 47278.97 | 27251.05 |
|  | Max. $\mathrm{H}_{2}$ | 13 | -60497.52 | 45229.00 | 27281.79 |
|  | Min. Vert | 12 | -62497.93 | 47278.97 | 27251.05 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 6 | -4403.74 | 2298.82 | 1328.83 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 6 | -4403.74 | 2298.82 | 1328.83 |


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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Location | Condition | Gov. <br> Load <br> Comb. | Vertical $l b$ | $\begin{gathered} \text { Horizontal, } X \\ l b \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ l b \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Guy A@ } 224.79 \\ \mathrm{ft} \\ \text { Elev - } 5.41 \mathrm{ft} \\ \text { Azimuth } 0 \mathrm{deg} \end{gathered}$ | Max. Vert | 2 | -4421.84 | 0.88 | -2672.62 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -32601.96 | 2120.19 | -27678.73 |
|  | Max. $\mathrm{H}_{2}$ | 2 | -4421.84 | 0.88 | -2672.62 |
|  | Min. Vert | 8 | -64150.35 | -21.92 | -55759.94 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -32301.61 | -2122.79 | -27425.50 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 8 | -64150.35 | -21.92 | -55759.94 |
| $\begin{gathered} \text { Guy C@ } 206.73 \\ \mathrm{ft} \\ \text { Elev-8.98 ft } \\ \text { Azimuth } 240 \mathrm{deg} \end{gathered}$ | Max. Vert | 10 | -196.36 | -415.16 | 240.21 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 10 | -196.36 | -415.16 | 240.21 |
|  | Max. $\mathrm{H}_{7}$ | 4 | -22116.63 | -29104.43 | 16768.14 |
|  | Min. Vert | 4 | -22116.63 | -29104.43 | 16768.14 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 4 | -22116.63 | -29104.43 | 16768.14 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 10 | -196.36 | -415.16 | 240.21 |
| $\begin{gathered} \text { Guy B@193.65 } \\ \mathrm{ft} \\ \text { Elev } 0.72 \mathrm{ft} \\ \text { Azimuth } 120 \mathrm{deg} \end{gathered}$ | Max. Vert | 6 | -174.01 | 373.76 | 216.71 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 12 | -22430.99 | 29714.46 | 17084.51 |
|  | Max. $\mathrm{H}_{7}$ | 13 | -22039.77 | 29112.67 | 17120.24 |
|  | Min. Vert | 12 | -22430.99 | 29714.46 | 17084.51 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 6 | -174.01 | 373.76 | 216.71 |
|  | Min. $\mathrm{H}_{\text {z }}$ | 6 | -174.01 | 373.76 | 216.71 |
| $\begin{gathered} \text { Guy A@ } 201.41 \\ \mathrm{ft} \\ \text { Elev }-4.96 \mathrm{ft} \\ \text { Azimuth } 0 \mathrm{deg} \end{gathered}$ | Max. Vert | 2 | -195.67 | 0.12 | -476.97 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -11557.49 | 652.61 | -17878.45 |
|  | Max. $\mathrm{H}_{\mathbf{z}}$ | 2 | -195.67 | 0.12 | -476.97 |
|  | Min. Vert | 7 | -21915.62 | -275.71 | -33481.13 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -11441.75 | -653.65 | -17704.82 |
|  | Min. $\mathrm{H}_{2}$ | 7 | -21915.62 | -275.71 | -33481.13 |
| $\begin{gathered} \text { Guy C @ } 114.41 \\ \mathrm{ft} \\ \text { Elev }-5.4 \mathrm{ft} \\ \text { Azimuth } 240 \mathrm{deg} \end{gathered}$ | Max. Vert | 10 | -70.90 | -164.04 | 94.73 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 10 | -70.90 | -164.04 | 94.73 |
|  | Max. $\mathrm{H}_{2}$ | 5 | -4220.85 | -7504.92 | 4285.72 |
|  | Min. Vert | 5 | -4220.85 | -7504.92 | 4285.72 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -4220.85 | -7504.92 | 4285.72 |
|  | Min. $\mathrm{H}_{7}$ | 10 | -70.90 | -164.04 | 94.73 |
| $\begin{gathered} \text { Guy B@ } 115.63 \\ \mathrm{ft} \\ \text { Elev } 0.5 \mathrm{ft} \\ \text { Azimuth } 120 \mathrm{deg} \end{gathered}$ | Max. Vert | 6 | -67.04 | 184.46 | 106.57 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -3692.37 | 7434.54 | 4247.45 |
|  | Max. $\mathrm{H}_{\mathbf{z}}$ | 13 | -3671.76 | 7355.97 | 4289.23 |
|  | Min. Vert | 12 | -3697.35 | 7417.33 | 4279.70 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 6 | -67.04 | 184.46 | 106.57 |
|  | Min. $\mathrm{H}_{7}$ | 6 | -67.04 | 184.46 | 106.57 |
| $\begin{gathered} \text { Guy A@ } 114.04 \\ \mathrm{ft} \\ \text { Elev }-3.6 \mathrm{ft} \\ \text { Azimuth } 0 \mathrm{deg} \end{gathered}$ | Max. Vert | 2 | -74.13 | -0.00 | -203.39 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 11 | -2238.59 | 89.04 | -4732.17 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ Min. Vert | 2 | $\begin{gathered} -74.13 \\ -4046.86 \end{gathered}$ | -0.00 -37.95 | -203.39 -8538.00 |


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|  | Client | T-MOBILE | Designed by Arielle Novak |


| Location | Condition | Gov. Load Comb. | Vertical $l b$ | $\begin{gathered} \text { Horizontal, } X \\ l b \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ l b \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mast | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | -2218.75 | -89.67 | -4690.95 |
|  | Min. $\mathrm{H}_{\text {z }}$ | 7 | -4046.86 | -37.95 | -8538.00 |
|  | Max. Vert | 23 | 467830.32 | -296.33 | 356.34 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 7 | 288721.57 | 506.47 | -135.45 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 11 | 284759.89 | 55.87 | 521.54 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 1 | 0.00 | -36.93 | 40.83 |
|  | Max. M ${ }_{\text {z }}$ | 1 | 0.00 | -36.93 | 40.83 |
|  | Max. Torsion | 12 | 7356.37 | 382.79 | 365.05 |
|  | Min. Vert | 1 | 202316.83 | -36.93 | 40.83 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 9 | 288645.84 | -591.06 | -132.26 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 2 | 293873.16 | 2.23 | -413.28 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 1 | 0.00 | -36.93 | 40.83 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 1 | 0.00 | -36.93 | 40.83 |
|  | Min. Torsion | 6 | -6912.99 | 227.24 | 109.08 |

Tower Mast Reaction Summary

| Load Combination | Vertical <br> lb | Shear $x_{x}$ <br> lb | Shear: <br> lb | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 202316.83 | 36.93 | -40.83 | 0.00 | 0.00 | -0.14 |
| 1.2 Dead+ 1.6 Wind 0 deg - No | 293873.16 | -2.23 | 413.28 | 0.00 | 0.00 | 1770.71 |
| 1.2 Dead+1.6 Wind 30 deg - No Ice +1.0 Guy | 287562.35 | 391.52 | 341.62 | 0.00 | 0.00 | 4167.09 |
| $\begin{aligned} & \text { 1.2 Dead+1.6 Wind } 60 \text { deg - No } \\ & \text { Ice }+1.0 \text { Guy } \end{aligned}$ | 276712.17 | 421.34 | -273.03 | 0.00 | 0.00 | 4702.90 |
| 1.2 Dead+1.6 Wind 90 deg - No Ice +1.0 Guy | 283895.00 | 62.46 | -494.30 | 0.00 | 0.00 | 6074.80 |
| 1.2 Dead+1.6 Wind 120 deg No Ice+1.0 Guy | 294018.45 | -227.24 | -109.08 | 0.00 | 0.00 | 6912.99 |
| 1.2 Dead+1.6 Wind 150 deg No Ice+1.0 Guy | 288721.57 | -506.47 | 135.45 | 0.00 | 0.00 | 3102.63 |
| 1.2 Dead+1.6 Wind 180 deg No Ice+1.0 Guy | 279362.19 | 93.42 | 298.34 | 0.00 | 0.00 | -1913.27 |
| 1.2 Dead+1.6 Wind 210 deg No Ice+1.0 Guy | 288645.84 | 591.06 | 132.26 | 0.00 | 0.00 | -4150.25 |
| 1.2 Dead+1.6 Wind 240 deg No Ice+1.0 Guy | 293398.80 | 233.86 | -113.90 | 0.00 | 0.00 | -4255.41 |
| 1.2 Dead+1.6 Wind 270 deg No Ice+1.0 Guy | 284759.89 | -55.87 | -521.54 | 0.00 | 0.00 | -6000.22 |
| 1.2 Dead+1.6 Wind 300 deg No Ice+1.0 Guy | 278658.52 | -382.79 | -365.05 | 0.00 | 0.00 | -7356.37 |
| 1.2 Dead+1.6 Wind 330 deg No Ice+1.0 Guy | 288460.32 | -376.96 | 277.19 | 0.00 | 0.00 | -3058.22 |
| $\text { 1.2 Dead+1.0 Ice }+1.0$ Temp+Guy | 460840.98 | 210.93 | -328.55 | 0.00 | 0.00 | 42.74 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 Ice +1.0 Temp+1.0 Guy | 467665.40 | 188.14 | -207.22 | 0.00 | 0.00 | 49.34 |
| 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0$ Ice +1.0 Temp +1.0 Guy | 466275.89 | 91.96 | -235.57 | 0.00 | 0.00 | 677.19 |
| 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0$ Ice+1.0 Temp+1.0 Guy | 465196.52 | 84.73 | -233.01 | 0.00 | 0.00 | 942.18 |
| 1.2 Dead +1.0 Wind 90 deg +1.0 Ice +1.0 Temp+1.0 Guy | 466339.22 | 117.11 | -239.30 | 0.00 | 0.00 | 1103.74 |
| $\begin{aligned} & \text { 1.2 Dead }+1.0 \text { Wind } 120 \\ & \text { deg+1.0 Ice+1.0 Temp+1.0 Guy } \end{aligned}$ | 467680.53 | 137.29 | -324.80 | 0.00 | 0.00 | 1159.01 |


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|  | Project | ANCHOR | Date $14: 28: 20 \text { 08/12/21 }$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Load Combination | Vertical <br> lb | Shear: <br> lb | Shear: <br> lb | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy | 466540.43 | 210.94 | -417.65 | 0.00 | 0.00 | 783.66 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy | 465475.66 | 239.68 | -457.30 | 0.00 | 0.00 | 7.20 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy | 466514.68 | 251.64 | -427.49 | 0.00 | 0.00 | -589.90 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy | 467830.32 | 296.33 | -356.34 | 0.00 | 0.00 | -822.15 |
| $\begin{aligned} & \text { 1.2 Dead }+1.0 \text { Wind } 270 \\ & \text { deg+1.0 Ice }+1.0 \text { Temp+1.0 Guy } \end{aligned}$ | 466726.41 | 291.28 | -291.23 | 0.00 | 0.00 | -1076.36 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy | 465715.91 | 307.39 | -279.58 | 0.00 | 0.00 | -1234.58 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy | 466684.17 | 290.61 | -261.27 | 0.00 | 0.00 | -802.42 |
| Dead+Wind 0 deg Service+Guy | 204308.77 | 32.18 | -282.19 | 0.00 | 0.00 | 366.12 |
| Dead+Wind 30 deg Service+Guy | 203974.99 | 142.82 | -254.69 | 0.00 | 0.00 | 845.66 |
| Dead+Wind 60 deg Service+Guy | 203756.25 | 257.07 | -167.76 | 0.00 | 0.00 | 888.97 |
| Dead+Wind 90 deg Service+Guy | 203904.16 | 297.12 | -24.13 | 0.00 | 0.00 | 1225.09 |
| Dead+Wind 120 deg Service+Guy | 204122.08 | 271.05 | 108.67 | 0.00 | 0.00 | 1468.68 |
| Dead+Wind 150 deg Service+Guy | 204025.42 | 167.97 | 172.31 | 0.00 | 0.00 | 621.08 |
| Dead+Wind 180 deg Service+Guy | 203947.53 | 40.19 | 192.60 | 0.00 | 0.00 | -365.83 |
| Dead+Wind 210 deg Service+Guy | 204182.84 | -88.30 | 168.17 | 0.00 | 0.00 | -847.23 |
| Dead+Wind 240 deg Service+Guy | 204478.63 | -194.89 | 101.97 | 0.00 | 0.00 | -891.92 |
| Dead+Wind 270 deg Service+Guy | 204369.62 | -226.74 | -32.16 | 0.00 | 0.00 | -1222.18 |
| Dead+Wind 300 deg Service+Guy | 204248.26 | -191.04 | -176.26 | 0.00 | 0.00 | -1458.69 |
| Dead+Wind 330 deg Service+Guy | 204309.05 | -78.52 | -260.71 | 0.00 | 0.00 | -618.46 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | PX | PY | PZ | PX | PY | PZ |  |
| Comb. | $l b$ | $l b$ | $l b$ | $l b$ | $l b$ | $l b$ |  |
| 1 | -0.00 | -76000.61 | 0.00 | 5.57 | 76000.45 | 0.40 | 0.007\% |
| 2 | -134.05 | -89554.32 | -96522.37 | 134.10 | 89554.13 | 96516.20 | 0.005\% |
| 3 | 47394.08 | -88855.19 | -82389.06 | -47394.68 | 88855.09 | 82385.17 | 0.003\% |
| 4 | 81661.65 | -88146.62 | -47486.10 | -81662.89 | 88146.61 | 47483.53 | 0.002\% |
| 5 | 92538.13 | -88898.12 | 106.59 | -92534.88 | 88898.02 | -103.92 | 0.003\% |
| 6 | 82653.39 | -89628.91 | 51275.60 | -82647.05 | 89628.70 | -51272.15 | 0.005\% |
| 7 | 46990.11 | -88862.95 | 84941.21 | -46985.60 | 88862.83 | -84939.61 | 0.004\% |
| 8 | 134.05 | -88085.71 | 96498.81 | -134.67 | 88085.72 | -96499.16 | 0.001\% |
| 9 | -46412.02 | -88784.84 | 84207.68 | 46408.71 | 88784.76 | -84206.46 | 0.003\% |
| 10 | -82182.04 | -89493.41 | 50848.69 | 82177.24 | 89493.25 | -50846.01 | 0.004\% |
| 11 | -92538.13 | -88741.91 | -161.15 | 92535.67 | 88741.84 | 163.18 | 0.002\% |
| 12 | -82133.00 | -88011.12 | -47913.02 | 82133.42 | 88011.12 | 47912.96 | 0.000\% |
| 13 | -47972.16 | -88777.08 | -83122.59 | 47972.86 | 88776.99 | 83118.59 | 0.003\% |
| 14 | -0.00 | -271800.95 | 0.00 | -0.31 | 271800.95 | 0.91 | 0.000\% |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 49 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | PX | PY | $P Z$ | PX | PY | PZ |  |
| Comb. | $l b$ | $l b$ | $l b$ | $l b$ | $1 b$ | $l b$ |  |
| 15 | 7.28 | -272368.37 | -34685.79 | -7.16 | 272368.36 | 34684.25 | 0.001\% |
| 16 | 17292.57 | -271824.11 | -29936.99 | -17292.21 | 271824.10 | 29935.92 | 0.000\% |
| 17 | 30051.73 | -271273.72 | -17399.32 | -30049.07 | 271273.69 | 17397.74 | 0.001\% |
| 18 | 34830.15 | -271852.74 | -10.62 | -34829.12 | 271852.73 | 10.94 | 0.000\% |
| 19 | 30197.09 | -272418.27 | 17943.30 | -30195.79 | 272418.26 | -17942.43 | 0.001\% |
| 20 | 17198.91 | -271829.59 | 30326.11 | -17198.29 | 271829.58 | -30325.33 | 0.000\% |
| 21 | -7.28 | -271233.53 | 34736.08 | 6.64 | 271233.50 | -34732.82 | 0.001\% |
| 22 | -17142.33 | -271777.80 | 30215.21 | 17141.39 | 271777.78 | -30214.29 | 0.000\% |
| 23 | -30084.67 | -272328.18 | 17886.80 | 30083.16 | 272328.16 | -17885.69 | 0.001\% |
| 24 | -34830.15 | -271749.16 | 2.28 | 34829.01 | 271749.15 | -1.68 | 0.000\% |
| 25 | -30164.15 | -271183.63 | -17455.82 | 30161.72 | 271183.60 | 17455.15 | 0.001\% |
| 26 | -17349.15 | -271772.32 | -30047.89 | 17348.97 | 271772.31 | 30046.91 | 0.000\% |
| 27 | -27.36 | -76150.47 | -19702.38 | 27.61 | 76150.46 | 19698.91 | 0.004\% |
| 28 | 9674.23 | -76007.79 | -16817.51 | -9673.23 | 76007.78 | 16814.90 | 0.004\% |
| 29 | 16669.06 | -75863.19 | -9693.01 | -16667.16 | 75863.18 | 9691.88 | 0.003\% |
| 30 | 18889.27 | -76016.55 | 21.75 | -18886.86 | 76016.54 | -21.32 | 0.003\% |
| 31 | 16871.45 | -76165.69 | 10466.38 | -16868.68 | 76165.68 | -10464.48 | 0.004\% |
| 32 | 9591.79 | -76009.37 | 17338.35 | -9590.17 | 76009.36 | -17336.30 | 0.003\% |
| 33 | 27.36 | -75850.76 | 19697.58 | -27.41 | 75850.74 | -19695.28 | 0.003\% |
| 34 | -9473.81 | -75993.44 | 17188.65 | 9472.13 | 75993.42 | -17186.37 | 0.004\% |
| 35 | -16775.26 | -76138.04 | 10379.25 | 16772.43 | 76138.02 | -10377.06 | 0.005\% |
| 36 | -18889.27 | -75984.67 | -32.89 | 18886.91 | 75984.66 | 33.61 | 0.003\% |
| 37 | -16765.25 | -75835.53 | -9780.14 | 16763.61 | 75835.52 | 9779.21 | 0.002\% |
| 38 | -9792.21 | -75991.85 | -16967.21 | 9791.66 | 75991.84 | 16964.67 | 0.003\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 7 | 0.00000001 | 0.00004973 |
| 2 | Yes | 13 | 0.00009881 | 0.00011007 |
| 3 | Yes | 13 | 0.00006322 | 0.00007177 |
| 4 | Yes | 9 | 0.00008062 | 0.00013945 |
| 5 | Yes | 13 | 0.00006166 | 0.00008127 |
| 6 | Yes | 13 | 0.00010445 | 0.00012003 |
| 7 | Yes | 13 | 0.00007393 | 0.00008319 |
| 8 | Yes | 10 | 0.00000001 | 0.00006820 |
| 9 | Yes | 13 | 0.00005840 | 0.00006407 |
| 10 | Yes | 13 | 0.00008404 | 0.00009830 |
| 11 | Yes | 13 | 0.00000001 | 0.00006364 |
| 12 | Yes | 10 | 0.00000001 | 0.00005427 |
| 13 | Yes | 13 | 0.00006536 | 0.00007382 |
| 14 | Yes | 9 | 0.00000001 | 0.00003571 |
| 15 | Yes | 11 | 0.00000001 | 0.00005388 |
| 16 | Yes | 11 | 0.00000001 | 0.00004015 |
| 17 | Yes | 10 | 0.0000001 | 0.00004348 |
| 18 | Yes | 11 | 0.00000001 | 0.00003662 |
| 19 | Yes | 11 | 0.00000001 | 0.00005229 |
| 20 | Yes | 11 | 0.00000001 | 0.00003479 |
| 21 | Yes | 10 | 0.00000001 | 0.00004283 |
| 22 | Yes | 11 | 0.00000001 | 0.00004674 |
| 23 | Yes | 11 | 0.00000001 | 0.0006187 |
| 24 | Yes | 11 | 0.0000001 | 0.00004638 |
| 25 | Yes | 10 | 0.00004135 |  |
| 26 | Yes | 11 | 0 | 0.00003815 |
| 27 | Yes | 80000001 | 0.00011620 |  |
|  |  |  | 0.0000001 |  |


| tnxTower | Job | CTNL024A | Page 50 of 69 |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| Centerline Communications <br> 750 West Center Street, Suite 301 | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
| West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Client | T-MOBILE | Designed by Arielle Novak |


| 28 | Yes | 8 | 0.00000001 | 0.00008698 |
| :--- | :--- | :--- | :--- | :--- |
| 29 | Yes | 8 | 0.00000001 | 0.00004195 |
| 30 | Yes | 8 | 0.00000001 | 0.00007823 |
| 31 | Yes | 8 | 0.00000001 | 0.00011224 |
| 32 | Yes | 8 | 0.00000001 | 0.00008247 |
| 33 | Yes | 8 | 0.00000001 | 0.00003652 |
| 34 | Yes | 8 | 0.00000001 | 0.00009372 |
| 35 | Yes | 8 | 0.00000001 | 0.00012243 |
| 36 | Yes | 8 | 0.00000001 | 0.00008739 |
| 37 | Yes | 8 | 0.00000001 | 0.00004395 |
| 38 | Yes | 8 | 0.00000001 | 0.00008388 |

## Maximum Tower Deflections - Service Wind

| Section No. | Elevation ft | Horz. Deflection in | Gov. <br> Load <br> Comb. | Tilt 。 | Twist 。 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 368.75-362.5 | 1.358 | 33 | 0.0614 | 0.0414 |
| T2 | 362.5-356.25 | 1.406 | 33 | 0.0616 | 0.0415 |
| T3 | 356.25-350 | 1.454 | 33 | 0.0619 | 0.0416 |
| T4 | 350-343.75 | 1.502 | 33 | 0.0626 | 0.0413 |
| T5 | 343.75-337.5 | 1.555 | 33 | 0.0631 | 0.0414 |
| T6 | 337.5-331.25 | 1.608 | 33 | 0.0620 | 0.0462 |
| T7 | 331.25-325 | 1.658 | 33 | 0.0606 | 0.0508 |
| T8 | 325-318.75 | 1.705 | 33 | 0.0589 | 0.0550 |
| T9 | 318.75-312.5 | 1.750 | 33 | 0.0573 | 0.0558 |
| T10 | 312.5-306.25 | 1.792 | 33 | 0.0557 | 0.0563 |
| T11 | 306.25-300 | 1.833 | 33 | 0.0541 | 0.0568 |
| T12 | 300-293.75 | 1.866 | 33 | 0.0529 | 0.0568 |
| T13 | 293.75-287.5 | 1.911 | 33 | 0.0516 | 0.0572 |
| T14 | 287.5-281.25 | 1.956 | 33 | 0.0479 | 0.0656 |
| T15 | 281.25-275 | 1.997 | 33 | 0.0436 | 0.0757 |
| T16 | 275-268.75 | 2.031 | 33 | 0.0388 | 0.0835 |
| T17 | 268.75-262.5 | 2.057 | 33 | 0.0335 | 0.0890 |
| T18 | 262.5-256.25 | 2.073 | 33 | 0.0280 | 0.0923 |
| T19 | 256.25-250 | 2.081 | 33 | 0.0223 | 0.0933 |
| T20 | 250-243.75 | 2.080 | 33 | 0.0166 | 0.0923 |
| T21 | 243.75-237.5 | 2.070 | 33 | 0.0114 | 0.0911 |
| T22 | 237.5-231.25 | 2.045 | 33 | 0.0145 | 0.0843 |
| T23 | 231.25-225 | 2.012 | 33 | 0.0181 | 0.0796 |
| T24 | 225-218.75 | 1.976 | 33 | 0.0199 | 0.0795 |
| T25 | 218.75-212.5 | 1.961 | 29 | 0.0211 | 0.0800 |
| T26 | 212.5-206.25 | 1.945 | 29 | 0.0250 | 0.1020 |
| T27 | 206.25-181.25 | 1.920 | 29 | 0.0291 | 0.1221 |
| T28 | 181.25-175 | 1.738 | 29 | 0.0442 | 0.1798 |
| T29 | 175-168.75 | 1.673 | 29 | 0.0465 | 0.1821 |
| T30 | 168.75-162.5 | 1.611 | 29 | 0.0474 | 0.1812 |
| T31 | 162.5-156.25 | 1.547 | 29 | 0.0473 | 0.1796 |
| T32 | 156.25-150 | 1.493 | 29 | 0.0476 | 0.1741 |
| T33 | 150-125 | 1.437 | 29 | 0.0482 | 0.1660 |
| T34 | 125-100 | 1.172 | 29 | 0.0517 | 0.1064 |
| T35 | 100-93.75 | 0.891 | 29 | 0.0483 | 0.0747 |
| T36 | 93.75-87.5 | 0.830 | 29 | 0.0460 | 0.0747 |
| T37 | 87.5-81.25 | 0.775 | 29 | 0.0451 | 0.0800 |
| T38 | 81.25-75 | 0.720 | 29 | 0.0445 | 0.0864 |
| T39 | 75-50 | 0.664 | 29 | 0.0442 | 0.0907 |
| T40 | 50-25 | 0.430 | 29 | 0.0420 | 0.0858 |
| T41 | 25-0 | 0.229 | 29 | 0.0416 | 0.0537 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } 51 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. <br> Load <br> Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 370.00 | Search Antenna | 33 | 1.358 | 0.0614 | 0.0414 | 86797 |
| 355.00 | $8{ }^{\prime}$ Dish | 33 | 1.464 | 0.0620 | 0.0416 | 114124 |
| 350.00 | Guy | 33 | 1.502 | 0.0626 | 0.0413 | 50669 |
| 325.00 | $10^{\prime} \times 3$ " Dia Ommi | 33 | 1.705 | 0.0589 | 0.0550 | 125385 |
| 305.00 | QUAD656C0000 | 33 | 1.840 | 0.0538 | 0.0568 | 57971 |
| 300.00 | Guy | 33 | 1.866 | 0.0529 | 0.0568 | 31059 |
| 250.00 | $20^{\prime} \times 3$ " Dia Omni | 33 | 2.080 | 0.0166 | 0.0923 | 58194 |
| 242.50 | HPA-65R-BUU-H6 | 33 | 2.066 | 0.0112 | 0.0902 | 28433 |
| 230.00 | APX16DWV-16DWV-S-E-A20 | 33 | 2.004 | 0.0186 | 0.0799 | 297626 |
| 225.00 | Guy | 33 | 1.976 | 0.0199 | 0.0795 | 36833 |
| 200.00 | Yagi | 29 | 1.888 | 0.0333 | 0.1405 | 52906 |
| 180.00 | (4) Yagi | 29 | 1.725 | 0.0448 | 0.1807 | 84529 |
| 162.50 | Guy | 29 | 1.547 | 0.0473 | 0.1796 | 35900 |
| 148.00 | Yagi | 29 | 1.418 | 0.0484 | 0.1626 | 101293 |
| 140.00 | Yagi | 29 | 1.337 | 0.0496 | 0.1447 | 120734 |
| 125.00 | Yagi | 29 | 1.172 | 0.0517 | 0.1064 | 191350 |
| 100.00 | Guy | 29 | 0.891 | 0.0483 | 0.0747 | 75465 |
| 88.00 | X-Style | 29 | 0.779 | 0.0451 | 0.0794 | 308853 |
| 62.00 | Yagi | 29 | 0.541 | 0.0430 | 0.0921 | 388600 |
| 50.00 | Guy | 29 | 0.430 | 0.0420 | 0.0858 | 95330 |
| 40.00 | Yagi | 29 | 0.348 | 0.0416 | 0.0760 | 260791 |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: |


| thxTOWer | Job | PTNLO24A | Page |
| :---: | :--- | :--- | :--- |
|  | Project | Client | ANCHOR |


| Section | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | $\circ$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T25 | $218.75-212.5$ | 17.537 | 6 | 0.1845 | Twist |
| T26 | $212.5-206.25$ | 17.425 | 6 | 0.2044 | 0 |
| T27 | $206.25-181.25$ | 17.246 | 6 | 0.2253 | 0.5350 |
| T28 | $181.25-175$ | 15.847 | 6 | 0.3449 | 0.6724 |
| T29 | $175-168.75$ | 15.321 | 6 | 0.3682 | 1.22045 |
| T30 | $168.75-162.5$ | 14.826 | 6 | 0.3828 | 1.2269 |
| T31 | $162.5-156.25$ | 14.311 | 6 | 0.3912 | 1.2107 |
| T32 | $156.25-150$ | 13.834 | 6 | 0.4008 | 1.1907 |
| T33 | $150-125$ | 13.331 | 6 | 0.4112 | 1.1671 |
| T34 | $125-100$ | 10.969 | 6 | 0.4485 | 1.1314 |
| T35 | $100-93.75$ | 8.459 | 6 | 0.4415 | 0.7510 |
| T36 | $93.75-87.5$ | 7.896 | 6 | 0.4300 | 0.5300 |
| T37 | $87.5-81.25$ | 7.356 | 6 | 0.4246 | 0.5299 |
| T38 | $81.25-75$ | 6.822 | 6 | 0.4208 | 0.5543 |
| T39 | $75-50$ | 6.280 | 6 | 0.4179 | 0.5884 |
| T40 | $50-25$ | 4.065 | 6 | 0.4017 | 0.6070 |
| T41 | $25-0$ | 2.122 | 6 | 0.3957 | 0.5660 |
|  |  |  |  | 0.3252 |  |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. <br> Load <br> Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 370.00 | Search Antenna | 8 | 11.903 | 0.3871 | 0.3885 | 11642 |
| 355.00 | $8{ }^{\prime}$ Dish | 8 | 12.217 | 0.3884 | 0.3898 | 8058 |
| 350.00 | Guy | 2 | 12.356 | 0.3915 | 0.3884 | 7347 |
| 325.00 | $10^{\prime} \times 3$ " Dia Ommi | 2 | 14.254 | 0.3644 | 0.4530 | 12792 |
| 305.00 | QUAD656C0000 | 2 | 15.561 | 0.3285 | 0.4597 | 10221 |
| 300.00 | Guy | 2 | 15.834 | 0.3207 | 0.4589 | 6256 |
| 250.00 | $20^{\prime} \times 3$ " Dia Ommi | 2 | 17.878 | 0.1009 | 0.6435 | 8704 |
| 242.50 | HPA-65R-BUU-H6 | 2 | 17.866 | 0.1294 | 0.6280 | 4552 |
| 230.00 | APX16DWV-16DWV-S-E-A20 | 6 | 17.720 | 0.1709 | 0.5296 | 23536 |
| 225.00 | Guy | 6 | 17.627 | 0.1781 | 0.5325 | 5788 |
| 200.00 | Yagi | 6 | 17.004 | 0.2480 | 0.9370 | 7082 |
| 180.00 | (4) Yagi | 6 | 15.743 | 0.3501 | 1.2252 | 10349 |
| 162.50 | Guy | 6 | 14.311 | 0.3912 | 1.1907 | 6931 |
| 148.00 | Yagi | 6 | 13.161 | 0.4147 | 1.1127 | 11881 |
| 140.00 | Yagi | 6 | 12.441 | 0.4280 | 1.0018 | 15335 |
| 125.00 | Yagi | 6 | 10.969 | 0.4485 | 0.7510 | 35787 |
| 100.00 | Guy | 6 | 8.459 | 0.4415 | 0.5300 | 12243 |
| 88.00 | X-Style | 6 | 7.399 | 0.4249 | 0.5516 | 36297 |
| 62.00 | Yagi | 6 | 5.112 | 0.4036 | 0.6099 | 38553 |
| 50.00 | Guy | 6 | 4.065 | 0.4017 | 0.5660 | 13990 |
| 40.00 | Yagi | 6 | 3.273 | 0.4196 | 0.4892 | 34717 |

## Bolt Design Data



| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | CTNL024A |  | Page 53 of 69 |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| West Bridgewater, MA 02379 Phone: $781-713-4725$ FAX: | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation <br> ft | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Maximum Load per Bolt lb | Allowable Load per Bolt lb | Ratio Load Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T2 | 362.5 | Diagonal | A325N | 0.5000 | 2 | 194.40 | 7952.16 | 0.024 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 47.04 | 19167.20 | 0.002 | 1 | Member Block Shear |
|  |  | Diagonal | A325N | 0.5000 | 2 | 585.70 | 15904.30 | 0.037 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 140.80 | 15904.30 | 0.009 | 1 | Bolt Shear |
| T3 | 356.25 | Diagonal | A325N | 0.5000 | 2 | 1553.83 | 15904.30 | 0.098 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 484.98 | 15904.30 | 0.030 | 1 | Bolt Shear |
| T4 | 350 | Leg | A325N | 0.7500 | 6 | 714.45 | 29820.60 | 0.024 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.6250 | 2 | 1511.90 | 10263.30 | 0.147 | 1 | Member Block Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 4218.61 | 19167.20 | 0.220 | 1 | Member Block Shear |
| T5 | 343.75 | Diagonal | A325N | 0.5000 | 2 | 2158.49 | 7952.16 | 0.271 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 1925.23 | 24850.50 | 0.077 | 1 | Bolt Shear |
| T6 | 337.5 | Diagonal | A325N | 0.5000 | 2 | 2054.34 | 7952.16 | 0.258 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1574.63 | 7952.16 | 0.198 | 1 | Bolt Shear |
| T7 | 331.25 | Diagonal | A325N | 0.5000 | 2 | 1949.42 | 7952.16 | 0.245 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1530.17 | 7952.16 | 0.192 | 1 | Bolt Shear |
| T8 | 325 | Leg | A325N | 0.7500 | 6 | 2461.70 | 29820.60 | 0.083 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 2213.58 | 7952.16 | 0.278 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1837.22 | 7952.16 | 0.231 | 1 | Bolt Shear |
| T9 | 318.75 | Diagonal | A325N | 0.5000 | 2 | 2078.67 | 7952.16 | 0.261 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2103.56 | 7952.16 | 0.265 | 1 | Bolt Shear |
| T10 | 312.5 | Diagonal | A325N | 0.5000 | 2 | 2211.63 | 7952.16 | 0.278 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2156.60 | 7952.16 | 0.271 | 1 | Bolt Shear |
| T11 | 306.25 | Diagonal | A325N | 0.5000 | 2 | 3532.74 | 7952.16 | 0.444 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 2912.43 | 24850.50 | 0.117 | 1 | Bolt Shear |
| T12 | 300 | Leg | A325N | 0.7500 | 6 | 2320.66 | 29820.60 | 0.078 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.6250 | 2 | 3738.84 | 12425.20 | 0.301 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 5075.57 | 19167.20 | 0.265 | 1 | Member Block Shear |
| T13 | 293.75 | Diagonal | A325N | 0.5000 | 2 | 3718.15 | 7952.16 | 0.468 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 1361.47 | 24850.50 | 0.055 | 1 | Bolt Shear |
| T14 | 287.5 | Diagonal | A325N | 0.5000 | 2 | 3284.56 | 7952.16 | 0.413 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2175.69 | 7952.16 | 0.274 | 1 | Bolt Shear |
| T15 | 281.25 | Diagonal | A325N | 0.5000 | 2 | 2907.91 | 7952.16 | 0.366 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 1950.36 | 12425.20 | 0.157 | 1 | Bolt Shear |
| T16 | 275 | Leg | A325N | 0.7500 | 6 | 5715.63 | 29820.60 | 0.192 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 2454.20 | 7952.16 | 0.309 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1692.80 | 7952.16 | 0.213 | 1 | Bolt Shear |
| T17 | 268.75 | Diagonal | A325N | 0.5000 | 2 | 2028.60 | 7952.16 | 0.255 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1568.08 | 7952.16 | 0.197 | 1 | Bolt Shear |
| T18 | 262.5 | Diagonal | A325N | 0.5000 | 2 | 1790.10 | 7952.16 | 0.225 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1562.59 | 7952.16 | 0.196 | 1 | Bolt Shear |
| T19 | 256.25 | Diagonal | A325N | 0.5000 | 2 | 2129.41 | 7952.16 | 0.268 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1926.12 | 7952.16 | 0.242 | 1 | Bolt Shear |
| T20 | 250 | Leg | A325N | 0.7500 | 6 | 6148.35 | 29820.60 | 0.206 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 2137.31 | 7952.16 | 0.269 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2354.23 | 15904.30 | 0.148 | 1 | Bolt Shear |
| T2 1 | 243.75 | Diagonal | A325N | 0.5000 | 2 | 4295.25 | 7952.16 | 0.540 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 2921.07 | 24850.50 | 0.118 | 1 | Bolt Shear |
| T22 | 237.5 | Diagonal | A325N | 0.5000 | 2 | 5385.14 | 7952.16 | 0.677 | 1 | Bolt Shear |
|  |  | Top Girt | A 325 N | 0.6250 | 2 | 3045.54 | 24850.50 | 0.123 | 1 | Bolt Shear |
| T23 | 231.25 | Diagonal | A325N | 0.5000 | 2 | 7710.78 | 7952.16 | 0.970 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 4081.67 | 24850.50 | 0.164 | 1 | Bolt Shear |
| T24 | 225 | Leg | A325N | 0.7500 | 6 | 4138.82 | 29820.60 | 0.139 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.6250 | 2 | 6974.14 | 24850.50 | 0.281 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 6665.83 | 19167.20 | 0.348 | 1 | Member Block Shear |
| T25 | 218.75 | Diagonal | A325N | 0.5000 | 2 | 2831.85 | 7952.16 | 0.356 | 1 | Bolt Shear |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 | Job |  | $\text { Page } 54 \text { of } 69$ |
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|  | CTNL024A |  |  |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \\ \hline \end{array}$ |
| $\begin{aligned} & \text { West Bridgevater; MA } 02379 \\ & \text { Phone: } 71-1113-4725 \\ & \text { FAX: } \end{aligned}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation $f t$ | Component Type | Bolt Grade | Bolt Size <br> in | Number Of Bolts | Maximum Load per Bolt lb | Allowable Load per Bolt lb | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T26 | 212.5 | Top Girt | A325N | 0.6250 | 2 | 3097.18 | 19167.20 | 0.162 | 1 | Member Block Shear |
|  |  | Diagonal | A325N | 0.5000 | 2 | 2138.81 | 7952.16 | 0.269 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1497.41 | 7952.16 | 0.188 | 1 | Bolt Shear |
| T27 | 206.25 | Diagonal | A325N | 0.5000 | 2 | 3110.98 | 7952.16 | 0.391 | 1 | Bolt Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 1781.74 | 12425.20 | 0.143 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1196.72 | 7952.16 | 0.150 | 1 | Bolt Shear |
| T28 | 181.25 | Leg | A325N | 0.7500 | 6 | 6759.03 | 29820.60 | 0.227 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 3519.24 | 7952.16 | 0.443 | 1 | Bolt Shear |
|  |  | Sccondary | A307 | 0.6250 | 1 | 2111.45 | 6212.62 | 0.340 | 1 | Bolt Shear |
|  |  | Horizontal |  |  |  |  |  |  |  |  |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2001.11 | 7952.16 | 0.252 | 1 | Bolt Shear |
| T29 | 175 | Leg | A325N | 0.7500 | 6 | 6713.55 | 29820.60 | 0.225 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 4311.70 | 7952.16 | 0.542 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2397.97 | 7952.16 | 0.302 | 1 | Bolt Shear |
| T30 | 168.75 | Diagonal | A325N | 0.5000 | 2 | 4805.29 | 7952.16 | 0.604 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2838.97 | 7952.16 | 0.357 | 1 | Bolt Shear |
| T31 | 162.5 | Diagonal | A325N | 0.5000 | 2 | 1700.26 | 7952.16 | 0.214 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 2472.09 | 15904.30 | 0.155 | 1 | Bolt Shear |
| T32 | 156.25 | Diagonal | A325N | 0.5000 | 2 | 1502.24 | 7952.16 | 0.189 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1111.25 | 7952.16 | 0.140 | 1 | Bolt Shear |
| T33 | 150 | Leg | A325N | 0.7500 | 6 | 7203.16 | 29820.60 | 0.242 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 3450.28 | 7952.16 | 0.434 | 1 | Bolt Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 2028.45 | 12425.20 | 0.163 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1130.10 | 7952.16 | 0.142 | 1 | Bolt Shear |
| T34 | 125 | Leg | A325N | 0.7500 | 6 | 7244.46 | 29820.60 | 0.243 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.6250 | 2 | 6328.89 | 7187.70 | 0.881 | 1 | Member Block Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 3807.50 | 12425.20 | 0.306 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 2480.93 | 12425.20 | 0.200 | 1 | Bolt Shear |
| T35 | 100 | Leg | A325N | 0.7500 | 6 | 6088.51 | 29820.60 | 0.204 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.6250 | 2 | 7759.17 | 24850.50 | 0.312 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 6457.24 | 19167.20 | 0.337 | 1 | Member Block Shear |
| T36 | 93.75 | Diagonal | A325N | 0.5000 | 2 | 2166.99 | 7952.16 | 0.273 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 4243.63 | 15904.30 | 0.267 | 1 | Bolt Shear |
| T37 | 87.5 | Diagonal | A325N | 0.5000 | 2 | 1493.19 | 7952.16 | 0.188 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1231.35 | 7952.16 | 0.155 | 1 | Bolt Shear |
| T38 | 81.25 | Diagonal | A325N | 0.5000 | 2 | 1071.58 | 7952.16 | 0.135 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1241.43 | 7952.16 | 0.156 | 1 | Bolt Shear |
| T39 | 75 | Leg | A325N | 0.7500 | 6 | 8019.77 | 29820.60 | 0.269 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 1755.26 | 7952.16 | 0.221 | 1 | Bolt Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 1287.52 | 12425.20 | 0.104 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1287.52 | 7952.16 | 0.162 | 1 | Bolt Shear |
| T40 | 50 | Leg | A325N | 0.7500 | 6 | 8447.21 | 29820.60 | 0.283 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 2326.84 | 7952.16 | 0.293 | 1 | Bolt Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 1369.83 | 12425.20 | 0.110 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1576.13 | 7952.16 | 0.198 | 1 | Bolt Shear |
| T41 | 25 | Leg | A325N | 0.7500 | 6 | 8622.27 | 29820.60 | 0.289 | 1 | Bolt Tension |
|  |  | Diagonal | A325N | 0.5000 | 2 | 1871.40 | 7952.16 | 0.235 | 1 | Bolt Shear |
|  |  | Horizontal | A325N | 0.6250 | 2 | 1356.80 | 12425.20 | 0.109 | 1 | Bolt Shear |
|  |  | Top Girt | A325N | 0.5000 | 2 | 1356.80 | 7952.16 | 0.171 | 1 | Bolt Shear |


| tnxTower | Job | CTNL024A | Page 55 of 69 |
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|  |  |  |  |
| Centerline Communications <br> 750 West Center Street, Suite 301 | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
| $\begin{gathered} \text { West Bridgewater, MA } 02379 \\ \text { Phone: } 781-713-4725 \\ \text { FAX: } \\ \hline \end{gathered}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation $f t$ | Size | Initial Tension $l b$ | Breaking Load lb | Actual $T_{u}$ $l b$ | Allowable <br> $\phi T_{n}$ <br> $l b$ | Required S.F. | Actual S.F. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | $\begin{gathered} 350.00(\mathrm{~A}) \\ (670) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 20577.20 | 47820.00 | 1.000 | 2.324 |
|  | $\begin{gathered} 350.00(\mathrm{~A}) \\ (671) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 20308.00 | 47820.00 | 1.000 | 2.355 |
|  | $\begin{gathered} 350.00(\mathrm{~B}) \\ (664) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 18874.40 | 47820.00 | 1.000 | 2.534 |
|  | $\begin{gathered} 350.00(\mathrm{~B}) \\ (665) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 19104.50 | 47820.00 | 1.000 | 2.503 |
|  | $\begin{gathered} 350.00(\mathrm{C}) \\ (658) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 19079.60 | 47820.00 | 1.000 | 2.506 |
|  | $\begin{gathered} 350.00(\mathrm{C}) \\ (659) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 18991.20 | 47820.00 | 1.000 | 2.518 |
| T12 | $\begin{gathered} 300.00(\mathrm{~A}) \\ (688) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 23402.00 | 47820.00 | 1.000 | 2.043 |
|  | $\begin{gathered} 300.00(\mathrm{~A}) \\ (689) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 22767.60 | 47820.00 | 1.000 | 2.100 |
|  | $\begin{gathered} 300.00(\mathrm{~B}) \\ (682) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 22134.80 | 47820.00 | 1.000 | 2.160 |
|  | $\begin{gathered} 300.00(\mathrm{~B}) \\ (683) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 21908.20 | 47820.00 | 1.000 | 2.183 |
|  | $\begin{gathered} 300.00(\mathrm{C}) \\ (676) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 21780.80 | 47820.00 | 1.000 | 2.196 |
|  | $\begin{gathered} 300.00(\mathrm{C}) \\ (677) \end{gathered}$ | 7/8 EHS | 7970.00 | 79699.84 | 22288.50 | 47820.00 | 1.000 | 2.145 |
| T24 | $\begin{gathered} 225.00(\mathrm{~A}) \\ (706) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 20607.30 | 34980.00 | 1.000 | 1.697 |
|  | $\begin{gathered} 225.00(\mathrm{~A}) \\ (707) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 19898.70 | 34980.00 | 1.000 | 1.758 |
|  | $\begin{gathered} 225.00(\mathrm{~B}) \\ (700) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 21076.90 | 34980.00 | 1.000 | 1.660 |
|  | $\begin{gathered} 225.00(\mathrm{~B}) \\ (701) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 19674.40 | 34980.00 | 1.000 | 1.778 |
|  | $\begin{gathered} 225.00(\mathrm{C}) \\ (694) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 19443.00 | 34980.00 | 1.000 | 1.799 |
|  | $\begin{gathered} 225.00(\mathrm{C}) \\ (695) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 20690.70 | 34980.00 | 1.000 | 1.691 |
| T31 | $\begin{gathered} 162.50(\mathrm{~A}) \\ (714) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 19985.30 | 34980.00 | 1.000 | 1.750 |
|  | $\begin{gathered} 162.50(\mathrm{~B}) \\ (713) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 20629.00 | 34980.00 | 1.000 | 1.696 |
|  | $\begin{gathered} 162.50(\mathrm{C}) \\ (712) \end{gathered}$ | 3/4 EHS | 5830.00 | 58299.91 | 20258.50 | 34980.00 | 1.000 | 1.727 |
| T35 | $\begin{gathered} 100.00(\mathrm{~A}) \\ (727) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 10617.00 | 21000.00 | 1.000 | 1.978 |
|  | $\begin{gathered} 100.00(\mathrm{~A}) \\ (728) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 10756.00 | 21000.00 | 1.000 | 1.952 |
|  | $\begin{gathered} 100.00(\mathrm{~B}) \\ (721) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 11388.80 | 21000.00 | 1.000 | 1.844 |
|  | $\begin{gathered} 100.00(\mathrm{~B}) \\ (722) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 9906.98 | 21000.00 | 1.000 | 2.120 |
|  | $\begin{gathered} 100.00(\mathrm{C}) \\ (715) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 9724.67 | 21000.00 | 1.000 | 2.159 |
|  | $\begin{gathered} 100.00(\mathrm{C}) \\ (716) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 10822.80 | 21000.00 | 1.000 | 1.940 |
| T40 | $\begin{gathered} 50.00(\mathrm{~A}) \\ (735) \end{gathered}$ | 9/16 EHS | 3500.00 | 35000.04 | 9484.38 | 21000.00 | 1.000 | 2.214 |
|  | 50.00 (B) (734) | 9/16 EHS | 3500.00 | 35000.04 | 9360.65 | 21000.00 | 1.000 | 2.243 |
|  | 50.00 (C) (733) | 9/16 EHS | 3500.00 | 35000.04 | 9655.01 | 21000.00 | 1.000 | 2.175 |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 56 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

## Compression Checks

## Leg Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | Mast Stability | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | Index | $1 b$ | $l b$ | $\phi P_{n}$ |
| TI | 368.75-362.5 | $23 / 4$ | 6.25 | 6.25 | $\begin{gathered} 109.1 \\ K=1.00 \end{gathered}$ | 5.9396 | 1.00 | -1648.36 | 102851.00 | $0.016^{1}$ |
| T2 | 362.5-356.25 | $23 / 4$ | 6.25 | 6.25 | $\begin{gathered} 109.1 \\ \mathrm{~K}=1.00 \end{gathered}$ | 5.9396 | 1.00 | -2308.03 | 102851.00 | $0.022^{1}$ |
| T3 | 356.25-350 | $23 / 4$ | 6.25 | 6.25 | $\begin{gathered} 109.1 \\ K=1.00 \end{gathered}$ | 5.9396 | 1.00 | -7365.11 | 102851.00 | $0.072{ }^{1}$ |
| T4 | 350-343.75 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 7.0686 | 1.00 | -5643.73 | 135284.00 | $0.042^{1}$ |
| T5 | 343.75-337.5 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 7.0686 | 1.00 | -40354.80 | 135284.00 | $0.298{ }^{1}$ |
| T6 | 337.5-331.25 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ K=1.00 \end{gathered}$ | 7.0686 | 1.00 | -41272.70 | 135284.00 | $0.305^{1}$ |
| T7 | 331.25-325 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 7.0686 | 1.00 | -42144.90 | 135284.00 | $0.312^{1}$ |
| T8 | 325-318.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -44310.60 | 171629.00 | $0.258{ }^{1}$ |
| T9 | 318.75-312.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -46132.80 | 171629.00 | $0.269^{1}$ |
| T10 | 312.5-306.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -48317.50 | 171629.00 | $0.282^{1}$ |
| T11 | 306.25-300 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -50010.20 | 171629.00 | $0.291^{1}$ |
| T12 | 300-293.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -41771.80 | 171629.00 | $0.243^{\text { }}$ |
| T13 | 293.75-287.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -87458.20 | 171629.00 | $0.510^{1}$ |
| T14 | 287.5-281.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -93174.90 | 171629.00 | $0.543{ }^{1}$ |
| T15 | 281.25-275 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -98618.00 | 171629.00 | $0.575{ }^{1}$ |
| T16 | 275-268.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -102881.00 | 171629.00 | $0.599^{1}$ |
| T17 | 268.75-262.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -106219.00 | 171629.00 | $0.619^{1}$ |
| T18 | 262.5-256.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -108310.00 | 171629.00 | $0.631{ }^{1}$ |
| T19 | 256.25-250 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -110446.00 | 171629.00 | $0.644^{1}$ |
| T20 | 250-243.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -110670.00 | 171629.00 | $0.645^{1}$ |
| T21 | 243.75-237.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -107859.00 | 171629.00 | $0.628^{1}$ |
| T22 | 237.5-231.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -98956.40 | 171629.00 | $0.577{ }^{1}$ |
| T23 | 231.25-225 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -98309.20 | 171629.00 | $0.573{ }^{1}$ |
| T24 | 225-218.75 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ K=1.00 \end{gathered}$ | 7.0686 | 1.00 | -74498.70 | 135284.00 | $0.551^{1}$ |
| T25 | 218.75-212.5 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ K=1.00 \end{gathered}$ | 7.0686 | 1.00 | -119480.00 | 135284.00 | $0.883{ }^{1}$ |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 FAX: | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 57 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | Mast Stability | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | Index | $l b$ | $l b$ | $\phi P_{n}$ |
| T26 | 212.5-206.25 | 3 | 6.25 | 6.25 | $\begin{gathered} 100.0 \\ K=1.00 \end{gathered}$ | 7.0686 | 1.00 | -121146.00 | 135284.00 | $0.895{ }^{1}$ |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | 3 | 25.00 | 6.25 | $\begin{gathered} 100.0 \\ K=1.00 \end{gathered}$ | 7.0686 | 1.00 | -123424.00 | 135284.00 | $0.912^{1}$ |
| T28 | 181.25-175 | 3 | 6.25 | 3.13 | $\begin{gathered} 50.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 7.0686 | 1.00 | -121904.00 | 200780.00 | $0.607{ }^{\text {I }}$ |
| T29 | 175-168.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -120844.00 | 171629.00 | $0.704^{1}$ |
| T30 | 168.75-162.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -119558.00 | 171629.00 | $0.697{ }^{\text {I }}$ |
| T31 | 162.5-156.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -126905.00 | 171629.00 | $0.739^{1}$ |
| T32 | 156.25-150 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -128316.00 | 171629.00 | $0.748^{\text {1 }}$ |
| T33 | 150-125 | $31 / 4$ | 25.00 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -130492.00 | 171629.00 | $0.760^{1}$ |
| T34 | 125-100 | $31 / 4$ | 25.00 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -132847.00 | 171629.00 | $0.774^{1}$ |
| T35 | 100-93.75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -109593.00 | 171629.00 | $0.639^{\text {1 }}$ |
| T36 | 93.75-87.5 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -141823.00 | 171629.00 | $0.826^{1}$ |
| T37 | 87.5-81.25 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -142184.00 | 171629.00 | $0.828^{1}$ |
| T38 | 81.25-75 | $31 / 4$ | 6.25 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -143347.00 | 171629.00 | $0.835^{\text {1 }}$ |
| T39 | 75-50 | $31 / 4$ | 25.00 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -148670.00 | 171629.00 | $0.866{ }^{1}$ |
| T40 | 50-25 | $31 / 4$ | 25.00 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -154278.00 | 171629.00 | $0.899^{\text {1 }}$ |
| T41 | 25-0 | $31 / 4$ | 25.00 | 6.25 | $\begin{gathered} 92.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.2958 | 1.00 | -156670.00 | 171629.00 | $0.913^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Diagonal Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $1 b$ | $1 b$ | $\phi P_{n}$ |
| TI | 368.75-362.5 | L2 $1 / 2 \times 2 \mathrm{~L} / 2 \times 1 / 4$ | 8.00 | 3.65 | $\begin{gathered} 96.9 \\ \mathrm{~K}=1.09 \end{gathered}$ | 1.1900 | -388.79 | 23509.60 | $0.017^{\text {1 }}$ |
| T2 | 362.5-356.25 | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 8.00 | 3.65 | $\begin{gathered} 47.5 \\ \mathrm{~K}=1.00 \end{gathered}$ | 3.5500 | -1171.40 | 102123.00 | $0.011^{1}$ |
| T3 | 356.25-350 | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 8.00 | 3.65 | $\begin{gathered} 47.5 \\ \mathrm{~K}=1.00 \end{gathered}$ | 3.5500 | -2991.88 | 102123.00 | $0.029^{1}$ |
| T4 | 350-343.75 | L3 $21 / 2 \times 1 / 4$ | 8.00 | 3.60 | $\begin{gathered} 91.4 \\ \mathrm{~K}=1.12 \end{gathered}$ | 1.3100 | -3340.61 | 27333.10 | $0.122^{1}$ |
| T12 | 300-293.75 | L3x2 1/2x1/4 | 8.00 | 3.59 | $\begin{gathered} 91.1 \\ \mathrm{~K}=1.12 \end{gathered}$ | 1.3100 | -7477.68 | 27407.90 | $0.273{ }^{\text {1 }}$ |
| T24 | 225-218.75 | 2L2 1/2x2 1/2x1/4 | 8.00 | 3.60 | $\begin{gathered} 56.2 \\ K=1.00 \end{gathered}$ | 2.3800 | -13948.30 | 65284.70 | $0.214^{1}$ |
| T35 | 100-93.75 | 2L2 1/2x2 1/2x1/4 | 8.00 | 3.59 | $\begin{gathered} 56.0 \\ K=1.00 \end{gathered}$ | 2.3800 | -15518.30 | 65385.10 | $0.237^{\prime}$ |


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| :---: | :---: | :---: | :---: |
|  |  | CTNL024A |  |
| Centerline Communications 750 West Center Street, Suite 301 | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| West Bridgevater, MA 02379 Phone: $781-713-4725$ FAX: | Client | T-MOBILE | Designed by Arielle Novak |

[^2]

Secondary Horizontal Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | ft | $f t$ |  | $i \mathrm{n}^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| T28 | 181.25-175 | P1.25x. 14 | 5.00 | 4.75 | $\begin{gathered} 105.6 \\ K=1.00 \end{gathered}$ | 0.6685 | -2111.45 | 12039.80 | $0.175^{\text {1 }}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } 59 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Section No. \& \begin{tabular}{l}
Elevation \\
\(f t\)
\end{tabular} \& Size \& \begin{tabular}{l}
\(L\) \\
ft
\end{tabular} \& \(L_{u}\)

$f t$ \& $\mathrm{Kl} / \mathrm{r}$ \& A

\[
i n^{2}

\] \& | $P_{u}$ |
| :--- |
| $l b$ | \& | $\phi P_{n}$ |
| :--- |
| $l b$ | \& Ratio $P_{u}$ <br>

\hline \& \& \& \& \& $\mathrm{K}=1.00$ \& \& \& \& <br>

\hline T8 \& 325-318.75 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -3674.43 \& 12101.80 \& $0.304^{1}$ <br>

\hline T9 \& 318.75-312.5 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -4207.12 \& 12101.80 \& $0.348^{\text {I }}$ <br>

\hline T10 \& 312.5-306.25 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -4313.19 \& 12101.80 \& $0.356^{\text {1 }}$ <br>

\hline T11 \& 306.25-300 \& 2L2 $1 / 2 \times 2 \times 1 / 4$ \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
K=1.00
\end{gathered}
$$ \& 2.1300 \& -5824.86 \& 54745.00 \& $0.106^{\text {1 }}$ <br>

\hline T12 \& 300-293.75 \& 2L2 1/2x2x1/4 \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -7469.15 \& 54745.00 \& $0.136^{\text {1 }}$ <br>

\hline T13 \& 293.75-287.5 \& 2L2 $1 / 2 \times 2 \times 1 / 4$ \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
K=1.00
\end{gathered}
$$ \& 2.1300 \& -2722.94 \& 54745.00 \& $0.050^{\text {1 }}$ <br>

\hline T14 \& 287.5-281.25 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -4351.37 \& 12101.80 \& $0.360{ }^{\text {I }}$ <br>

\hline T15 \& 281.25-275 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -3900.72 \& 12101.80 \& $0.322^{1}$ <br>

\hline T16 \& 275-268.75 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -3385.59 \& 12101.80 \& $0.280^{\text {1 }}$ <br>

\hline T17 \& 268.75-262.5 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -3136.15 \& 12101.80 \& $0.259^{\text {1 }}$ <br>

\hline T18 \& 262.5-256.25 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -3125.18 \& 12101.80 \& $0.258^{\text {1 }}$ <br>

\hline T19 \& 256.25-250 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -3852.24 \& 12101.80 \& $0.318^{1}$ <br>

\hline T20 \& 250-243.75 \& 2L2 1/2x2x1/4 \& 5.00 \& 4.40 \& $$
\begin{gathered}
67.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -4708.46 \& 54377.90 \& $0.087{ }^{\text {1 }}$ <br>

\hline T21 \& 243.75-237.5 \& 2L2 $1 / 2 \times 2 \times 1 / 4$ \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -5842.14 \& 54745.00 \& $0.107^{1}$ <br>

\hline T22 \& 237.5-231.25 \& 2L2 1/2x2x1/4 \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -6091.08 \& 54745.00 \& $0.111^{1}$ <br>

\hline T23 \& 231.25-225 \& 2L2 $1 / 2 \times 2 \times 1 / 4$ \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -8163.35 \& 54745.00 \& $0.149^{1}$ <br>

\hline T24 \& 225-218.75 \& 2L2 1/2×2x1/4 \& 5.00 \& 4.35 \& $$
\begin{gathered}
66.6 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -5116.14 \& 54623.00 \& $0.094^{1}$ <br>

\hline T25 \& 218.75-212.5 \& 2L2 1/2×2x1/4 \& 5.00 \& 4.35 \& $$
\begin{gathered}
66.6 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -2069.45 \& 54623.00 \& $0.038^{1}$ <br>

\hline T26 \& 212.5-206.25 \& P1.25x. 14 \& 5.00 \& 4.75 \& $$
\begin{gathered}
105.6 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -2994.82 \& 12039.80 \& $0.249^{1}$ <br>

\hline T27 \& $$
\begin{gathered}
206.25 \\
181.25
\end{gathered}
$$ \& P1.25x. 14 \& 5.00 \& 4.75 \& \[

$$
\begin{gathered}
105.6 \\
K=1.00
\end{gathered}
$$
\] \& 0.6685 \& -2393.45 \& 12039.80 \& $0.199^{1}$ <br>

\hline T28 \& 181.25-175 \& P1.25x. 14 \& 5.00 \& 4.75 \& $$
\begin{gathered}
105.6 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -4002.23 \& 12039.80 \& $0.332^{1}$ <br>

\hline T29 \& 175-168.75 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -4795.94 \& 12101.80 \& $0.396{ }^{1}$ <br>

\hline T30 \& 168.75-162.5 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
K=1.00
\end{gathered}
$$ \& 0.6685 \& -5677.95 \& 12101.80 \& $0.469{ }^{\text {1 }}$ <br>

\hline T31 \& 162.5-156.25 \& 2L2 1/2x2x1/4 \& 5.00 \& 4.40 \& $$
\begin{gathered}
67.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -2198.05 \& 54377.90 \& $0.040^{\text {1 }}$ <br>

\hline T32 \& 156.25-150 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -2222.50 \& 12101.80 \& $0.184^{1}$ <br>

\hline T33 \& 150-125 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -2260.19 \& 12101.80 \& $0.187^{1}$ <br>

\hline T34 \& 125-100 \& P1.25x. 14 \& 5.00 \& 4.73 \& $$
\begin{gathered}
105.2 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 0.6685 \& -4961.87 \& 12101.80 \& $0.410^{1}$ <br>

\hline T35 \& 100-93.75 \& 2L2 1/2×2x1/4 \& 5.00 \& 4.33 \& $$
\begin{gathered}
66.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -4529.80 \& 54745.00 \& $0.083{ }^{\text {' }}$ <br>

\hline T36 \& 93.75-87.5 \& 2L2 1/2x2x1/4 \& 5.00 \& 4.40 \& $$
\begin{gathered}
67.3 \\
\mathrm{~K}=1.00
\end{gathered}
$$ \& 2.1300 \& -2456.45 \& 54377.90 \& $0.045^{\text {' }}$ <br>

\hline T37 \& 87.5-81.25 \& P1.25x.14 \& 5.00 \& 4.73 \& 105.2 \& 0.6685 \& -2462.69 \& 12101.80 \& $0.203{ }^{1}$ <br>
\hline
\end{tabular}

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|  | Project | ANCHOR | Date 14:28:20 08/12/21 |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T38 | 81.25-75 | P1.25x. 14 | 5.00 | 4.73 | $\mathrm{K}=1.00$ | 0.6685 | -2482.85 | 12101.80 | $0.205^{1}$ |
|  |  |  |  |  | 105.2 |  |  |  |  |
|  |  |  |  |  | $\mathrm{K}=1.00$ |  |  |  |  |
| T39 | 75-50 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | -2575.05 | 12101.80 | $0.213^{1}$ |
|  |  |  |  |  | $\mathrm{K}=1.00$ |  |  |  |  |
| T40 | 50-25 | L2 1/2x2x1/4 | 5.00 | 4.40 | 122.7 | 1.0600 | -2672.18 | 15544.20 | $0.172^{\text {1 }}$ |
|  |  |  |  |  | $\mathrm{K}=0.99$ |  |  |  |  |
| T41 | 25-0 | P1.25x.14 | 5.00 | 4.73 | 105.2 | 0.6685 | -2713.61 | 12101.80 | $0.224^{1}$ |
|  |  |  |  |  | $\mathrm{K}=1.00$ |  |  |  |  |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Torque-Arm Top Design Data

| Section No. | Elevation | Size | $L$ | $\overline{L_{u}}$ | $\mathrm{Kl} / \mathrm{r}$ | $A$ | $\overline{P_{u}}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (717) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{I} / 2 \mathrm{xI} / 4$ | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ K=1.00 \end{gathered}$ | 2.6300 | -1011.85 | 63460.30 | $0.016^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (718) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -933.93 | 63460.30 | $0.015^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (723) \end{gathered}$ | 2L3x2 1/2xI/4 | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -1216.62 | 63460.30 | $0.019^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (724) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{l} / 2 \mathrm{xI} / 4$ | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -1305.66 | 63460.30 | $0.021^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (729) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{l} / 2 \times 1 / 4$ | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -1132.44 | 63460.30 | $0.018^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (730) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | $\begin{gathered} 74.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -964.27 | 63460.30 | $0.015^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Torque-Arm Bottom Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r. | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | in ${ }^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (662) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -20711.70 | 46126.40 | $0.449^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (663) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -21466.00 | 46126.40 | $0.465^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (668) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -20852.90 | 46126.40 | $0.452^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (669) \end{gathered}$ | 2L3x2 1/2×1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -20719.40 | 46126.40 | $0.449^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (674) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -20408.00 | 46126.40 | $0.442^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (675) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -21837.80 | 46126.40 | $0.473^{\text {1 }}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (680) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ K=1.00 \end{gathered}$ | 2.6300 | -23504.50 | 46226.30 | $0.508{ }^{\text {1 }}$ |


| tnxTower <br> Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX. | Job | CTNL024A | $\begin{aligned} & \text { Page } \\ & 61 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | lb | $l b$ | $\phi P_{n}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (681) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -24755.50 | 46226.30 | $0.536{ }^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (686) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ K=1.00 \end{gathered}$ | 2.6300 | -24757.50 | 46226.30 | $0.536{ }^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (687) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -24610.10 | 46226.30 | $0.532^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (692) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -23860.90 | 46226.30 | $0.516^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (693) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -25674.50 | 46226.30 | $0.555^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (698) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -19737.40 | 46126.40 | $0.428^{\text {1 }}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (699) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -20082.50 | 46126.40 | $0.435^{\text {1 }}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (704) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -20833.50 | 46126.40 | $0.452^{\text {1 }}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (705) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -21487.20 | 46126.40 | $0.466^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (710) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -19796.80 | 46126.40 | $0.429^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (711) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | $\begin{gathered} 108.0 \\ K=1.00 \end{gathered}$ | 2.6300 | -20183.20 | 46126.40 | $0.438{ }^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (719) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -7346.70 | 46226.30 | $0.159^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (720) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -7589.24 | 46226.30 | $0.164^{\text {1 }}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (725) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -8317.80 | 46226.30 | $0.180^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (726) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -8250.43 | 46226.30 | $0.178^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (731) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -7464.19 | 46226.30 | $0.161^{\text {1 }}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (732) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | $\begin{gathered} 107.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.6300 | -7522.77 | 46226.30 | $0.163^{\text {1 }}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Tension Checks

## Leg Design Data (Tension)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r. | A | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | $f t$ | $f t$ |  | $i n^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| TI | 368.75-362.5 | $23 / 4$ | 6.25 | 6.25 | 109.1 | 5.9396 | 283.32 | 192442.00 | $0.001^{1}$ |
| T2 | 362.5-356.25 | $23 / 4$ | 6.25 | 6.25 | 109.1 | 5.9396 | 920.29 | 192442.00 | $0.005^{1}$ |
| T3 | 356.25-350 | $23 / 4$ | 6.25 | 6.25 | 109.1 | 5.9396 | 5143.46 | 192442.00 | $0.027{ }^{1}$ |
| T4 | 350-343.75 | 3 | 6.25 | 6.25 | 100.0 | 7.0686 | 4286.67 | 229022.00 | $0.019^{1}$ |
| T12 | 300-293.75 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 681.07 | 268783.00 | $0.003{ }^{\text {1 }}$ |
| T14 | 287.5-281.25 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 8109.27 | 268783.00 | $0.030^{1}$ |
| T15 | 281.25-275 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 15339.90 | 268783.00 | $0.057{ }^{\text {1 }}$ |
| T16 | 275-268.75 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 21020.60 | 268783.00 | $0.078{ }^{1}$ |
| T17 | 268.75-262.5 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 25052.60 | 268783.00 | $0.093{ }^{1}$ |
| T18 | 262.5-256.25 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 27801.80 | 268783.00 | $0.103{ }^{\text {1 }}$ |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | Job |  | $\begin{aligned} & \text { Page } 62 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | CTNL024A |  |  |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| $\begin{gathered} \text { West Bridgewater; MA } 02379 \\ \text { Phone: 78I-713-4725 } \\ \text { FAX: } \end{gathered}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| T19 | 256.25-250 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 27251.70 | 268783.00 | $0.101^{1}$ |
| T20 | 250-243.75 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 26683.20 | 268783.00 | $0.099^{1}$ |
| T21 | 243.75-237.5 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 20938.60 | 268783.00 | $0.078^{1}$ |
| T22 | 237.5-231.25 | $31 / 4$ | 6.25 | 6.25 | 92.3 | 8.2958 | 8012.42 | 268783.00 | $0.030^{\text {1 }}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Diagonal Design Data (Tension)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $\mathrm{Kl} / \mathrm{r}$ | A | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| T1 | 368.75-362.5 | L2 1/2x2 1/2x1/4 | 8.00 | 3.65 | 59.6 | 0.7753 | 314.99 | 33726.10 | $0.009^{1}$ |
| T2 | 362.5-356.25 | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 8.00 | 3.65 | 49.7 | 2.3695 | 775.15 | 103075.00 | $0.00{ }^{1}$ |
| T3 | 356.25-350 | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 8.00 | 3.65 | 49.7 | 2.3695 | 3107.66 | 103075.00 | $0.030{ }^{1}$ |
| T4 | 350-343.75 | L3x2 1/2xI/4 | 8.00 | 3.60 | 60.7 | 0.8419 | 3023.79 | 36621.60 | $0.083{ }^{\text {1 }}$ |
| T5 | 343.75-337.5 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 4316.98 | 9940.20 | $0.434^{1}$ |
| T6 | 337.5-331.25 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 4108.69 | 9940.20 | $0.413^{1}$ |
| T7 | 331.25-325 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 3898.84 | 9940.20 | $0.392{ }^{1}$ |
| T8 | 325-318.75 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4427.16 | 14313.90 | $0.309{ }^{1}$ |
| T9 | 318.75-312.5 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4157.34 | 14313.90 | $0.290^{1}$ |
| T10 | 312.5-306.25 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4423.26 | 14313.90 | $0.309{ }^{1}$ |
| T11 | 306.25-300 | $3 / 4$ | 8.00 | 7.57 | 484.5 | 0.4418 | 7065.48 | 14313.90 | $0.494{ }^{\text {1 }}$ |
| T12 | 300-293.75 | L3x2 1/2xI/4 | 8.00 | 3.59 | 60.4 | 0.8419 | 3217.30 | 36621.60 | $0.08{ }^{\text {1 }}$ |
| T13 | 293.75-287.5 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 7436.29 | 14313.90 | $0.520^{1}$ |
| T14 | 287.5-281.25 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 6569.13 | 9940.20 | $0.661^{1}$ |
| T15 | 281.25-275 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 5815.81 | 9940.20 | $0.585{ }^{\text {1 }}$ |
| T16 | 275-268.75 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 4908.40 | 9940.20 | $0.494{ }^{1}$ |
| T17 | 268.75-262.5 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 4057.20 | 9940.20 | $0.40{ }^{1}$ |
| T18 | 262.5-256.25 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 3580.21 | 9940.20 | $0.36{ }^{\text {1 }}$ |
| T19 | 256.25-250 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4258.81 | 14313.90 | $0.298{ }^{1}$ |
| T20 | 250-243.75 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4274.63 | 14313.90 | $0.299{ }^{1}$ |
| T21 | 243.75-237.5 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 8590.50 | 14313.90 | $0.600^{\text {1 }}$ |
| T22 | 237.5-231.25 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 10770.30 | 14313.90 | $0.752^{1}$ |
| T23 | 231.25-225 | 1 | 8.00 | 7.57 | 363.4 | 0.7854 | 15421.60 | 25446.90 | $0.606^{1}$ |
| T25 | 218.75-212.5 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 5663.70 | 9940.20 | $0.570^{1}$ |
| T26 | 212.5-206.25 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 4277.62 | 9940.20 | $0.430^{1}$ |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 6221.96 | 9940.20 | $0.626^{\text {1 }}$ |
| T28 | 181.25-175 | 5/8 | 8.00 | 7.60 | 584.0 | 0.3068 | 7038.48 | 9940.20 | $0.708^{1}$ |
| T29 | 175-168.75 | 1 | 8.00 | 7.57 | 363.4 | 0.7854 | 8623.41 | 25446.90 | $0.339^{1}$ |
| T30 | 168.75-162.5 | 1 | 8.00 | 7.57 | 363.4 | 0.7854 | 9610.58 | 25446.90 | $0.378^{1}$ |
| T31 | 162.5-156.25 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 3400.53 | 9940.20 | $0.342{ }^{1}$ |
| T32 | 156.25-150 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 3004.49 | 9940.20 | $0.302{ }^{\text {I }}$ |
| T33 | 150-125 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 6900.56 | 9940.20 | 0.694 |
| T34 | 125-100 | L2 $1 / 2 \times 21 / 2 \times 3 / 16$ | 8.00 | 7.17 | 116.8 | 0.5710 | 12657.80 | 24839.90 | $0.510^{1}$ |
| T36 | 93.75-87.5 | 3/4 | 8.00 | 7.57 | 484.5 | 0.4418 | 4333.98 | 14313.90 | $0.303{ }^{\text {1 }}$ |
| T37 | 87.5-81.25 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 2986.39 | 9940.20 | $0.30{ }^{\text {' }}$ |
| T38 | 81.25-75 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 2143.16 | 9940.20 | $0.216^{1}$ |
| T39 | 75-50 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 3510.52 | 9940.20 | $0.353^{1}$ |
| T40 | 50-25 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 4653.67 | 9940.20 | $0.468{ }^{1}$ |
| T41 | 25-0 | 5/8 | 8.00 | 7.57 | 581.4 | 0.3068 | 3742.79 | 9940.20 | $0.377^{1}$ |

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| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ 14: 28: 20 ~ 08 / 12 / 21 \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Horizontal Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 2137.76 | 21660.40 | $0.099^{1}$ |
| T33 | 150-125 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2260.19 | 21660.40 | $0.104^{1}$ |
| T34 | 125-100 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2300.98 | 21660.40 | $0.106^{1}$ |
| T39 | 75-50 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2575.05 | 21660.40 | $0.119^{1}$ |
| T40 | 50-25 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2672.18 | 21660.40 | $0.123^{1}$ |
| T41 | 25-0 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2713.61 | 21660.40 | $0.125^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

|  |  | Secondary Horizontal Design Data (Tension) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{n}$ | $\mathrm{Kl} / \mathrm{r}$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| T28 | 181.25-175 | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 2111.45 | 21660.40 | $0.097{ }^{\text {l }}$ |

Top Girt Design Data (Tension)

| Section <br> No. | Elevation | Size | $L$ | $L_{u}$ | $K 1 / r$ | A | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | $f t$ | $f t$ |  | $i n^{2}$ | $1 b$ | $l b$ | $\phi P_{n}$ |
| TI | 368.75-362.5 | 2L2 1/2x2x1/4 | 5.00 | 4.38 | 73.0 | 1.3162 | 94.07 | 57256.90 | $0.002{ }^{1}$ |
| T2 | 362.5-356.25 | 2L2 1/2x3x1/4 | 5.00 | 4.44 | 76.0 | 1.7381 | 281.61 | 75608.40 | $0.004^{1}$ |
| T3 | 356.25-350 | 2L2 1/2x3x1/4 | 5.00 | 4.44 | 76.0 | 1.7381 | 925.04 | 75608.40 | $0.012^{1}$ |
| T4 | 350-343.75 | 2L2 1/2x2x1/4 | 5.00 | 4.35 | 72.7 | 1.3162 | 8437.21 | 57256.90 | $0.147^{1}$ |
| T5 | 343.75-337.5 | 2L2 1/2x2x1/4 | 5.00 | 4.35 | 72.7 | 1.3162 | 698.97 | 57256.90 | $0.012^{1}$ |
| T6 | 337.5-331.25 | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 714.86 | 21660.40 | $0.033^{1}$ |
| T7 | 331.25-325 | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 729.97 | 21660.40 | $0.034^{1}$ |
| T8 | 325-318.75 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 767.48 | 21660.40 | $0.035^{1}$ |
| T9 | 318.75-312.5 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 799.04 | 21660.40 | $0.037{ }^{1}$ |
| T10 | 312.5-306.25 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 836.88 | 21660.40 | $0.039^{1}$ |
| T11 | 306.25-300 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 866.20 | 57256.90 | $0.015^{1}$ |
| T12 | 300-293.75 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 10151.10 | 57256.90 | $0.177^{1}$ |
| T13 | 293.75-287.5 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 1514.82 | 57256.90 | $0.026^{1}$ |
| T14 | 287.5-281.25 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1613.84 | 21660.40 | $0.075^{\text {1 }}$ |
| T15 | 281.25-275 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1708.11 | 21660.40 | $0.079{ }^{1}$ |
| T16 | 275-268.75 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1781.96 | 21660.40 | $0.082^{\text {1 }}$ |
| T17 | 268.75-262.5 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1839.76 | 21660.40 | $0.085^{1}$ |
| T18 | 262.5-256.25 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1875.99 | 21660.40 | $0.087^{\text {' }}$ |
| T19 | 256.25-250 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 1912.99 | 21660.40 | $0.088^{1}$ |
| T20 | 250-243.75 | 2L2 1/2x2x1/4 | 5.00 | 4.40 | 72.4 | 1.3631 | 1916.86 | 59295.90 | $0.032^{1}$ |
| T21 | 243.75-237.5 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 1868.16 | 57256.90 | $0.033^{1}$ |
| T22 | 237.5-231.25 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 1713.98 | 57256.90 | $0.030^{\text {1 }}$ |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 64 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater, MA 02379 <br> Phone: 781-713-4725 <br> FAX: | Project | ANCHOR | $\begin{aligned} & \text { Date } \\ & \text { 14:28:20 08/12/21 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | $\mathrm{Kl} / \mathrm{r}$ | A | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i \mathrm{n}^{2}$ | $l b$ | $1 b$ | $\phi P_{n}$ |
| T23 | 231.25-225 | 2L2 1/2x2x1/4 | 5.00 | 4.33 | 72.4 | 1.3162 | 1702.77 | 57256.90 | $0.03{ }^{1}$ |
| T24 | 225-218.75 | 2L2 I/ $2 \times 2 \times 1 / 4$ | 5.00 | 4.35 | 72.7 | 1.3162 | 13331.70 | 57256.90 | $0.233{ }^{1}$ |
| T25 | 218.75-212.5 | 2L2 1/2x2x1/4 | 5.00 | 4.35 | 72.7 | 1.3162 | 6194.35 | 57256.90 | $0.10{ }^{1}$ |
| T26 | 212.5-206.25 | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 2098.31 | 21660.40 | $0.097{ }^{1}$ |
| T27 | $\begin{gathered} 206.25- \\ 181.25 \end{gathered}$ | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 2137.76 | 21660.40 | $0.099^{1}$ |
| T28 | 181.25-175 | P1.25x. 14 | 5.00 | 4.75 | 105.6 | 0.6685 | 2111.45 | 21660.40 | $0.097{ }^{1}$ |
| T29 | 175-168.75 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2093.08 | 21660.40 | $0.097{ }^{1}$ |
| T30 | 168.75-162.5 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2070.80 | 21660.40 | $0.096{ }^{1}$ |
| T31 | 162.5-156.25 | 2L2 1/2x2x1/4 | 5.00 | 4.40 | 72.4 | 1.3631 | 4944.19 | 59295.90 | $0.083{ }^{1}$ |
| T32 | 156.25-150 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2222.50 | 21660.40 | $0.103{ }^{\text {' }}$ |
| T33 | 150-125 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2260.19 | 21660.40 | $0.104{ }^{1}$ |
| T34 | 125-100 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2300.98 | 21660.40 | $0.106^{1}$ |
| T35 | 100-93.75 | 2L2 $1 / 2 \times 2 \times 1 / 4$ | 5.00 | 4.33 | 72.4 | 1.3162 | 12914.50 | 57256.90 | $0.226^{1}$ |
| T36 | 93.75-87.5 | 2L2 1/2x2x1/4 | 5.00 | 4.40 | 72.4 | 1.3631 | 8487.25 | 59295.90 | $0.143^{1}$ |
| T37 | 87.5-81.25 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2462.69 | 21660.40 | $0.114^{1}$ |
| T38 | 81.25-75 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2482.85 | 21660.40 | $0.115^{1}$ |
| T39 | 75-50 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2575.05 | 21660.40 | $0.119^{1}$ |
| T40 | 50-25 | L2 $1 / 2 \times 2 \times 1 / 4$ | 5.00 | 4.40 | 95.8 | 0.6778 | 3152.26 | 29484.80 | $0.107{ }^{1}$ |
| T41 | 25-0 | P1.25x. 14 | 5.00 | 4.73 | 105.2 | 0.6685 | 2713.61 | 21660.40 | $0.125^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Torque-Arm Top Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $\mathrm{Kl} / \mathrm{r}$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (660) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 18529.80 | 85212.00 | $0.217^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (661) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{l} / 2 \times 1 / 4$ | 6.03 | 5.90 | 75.0 | 2.6300 | 18165.10 | 85212.00 | $0.213^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (666) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 18153.60 | 85212.00 | $0.213^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (667) \end{gathered}$ | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ | 6.03 | 5.90 | 75.0 | 2.6300 | 17993.10 | 85212.00 | $0.211^{1}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (672) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 18509.60 | 85212.00 | $0.217^{\text {1 }}$ |
| T4 | $\begin{gathered} 350-343.75 \\ (673) \end{gathered}$ | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ | 6.03 | 5.90 | 75.0 | 2.6300 | 18097.30 | 85212.00 | $0.212^{\text {1 }}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (678) \end{gathered}$ | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ | 6.03 | 5.89 | 74.8 | 2.6300 | 20160.20 | 85212.00 | $0.237^{\prime}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (679) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 19140.80 | 85212.00 | $0.225^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (684) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{~L} / 2 \mathrm{xl} / 4$ | 6.03 | 5.89 | 74.8 | 2.6300 | 19393.80 | 85212.00 | $0.228^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (685) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 19752.00 | 85212.00 | $0.232^{\prime}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (690) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{~L} / 2 \times 1 / 4$ | 6.03 | 5.89 | 74.8 | 2.6300 | 20533.60 | 85212.00 | $0.241^{1}$ |
| T12 | $\begin{gathered} 300-293.75 \\ (691) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{I} / 2 \mathrm{xI} / 4$ | 6.03 | 5.89 | 74.8 | 2.6300 | 19296.20 | 85212.00 | $0.226^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (696) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 19350.30 | 85212.00 | $0.227^{\text { }}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (697) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 17996.70 | 85212.00 | $0.211^{1}$ |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 65 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{\text {u }}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (702) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 19429.50 | 85212.00 | $0.228^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (703) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 19718.50 | 85212.00 | $0.231^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (708) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 19990.60 | 85212.00 | $0.235^{1}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (709) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.90 | 75.0 | 2.6300 | 18452.70 | 85212.00 | $0.217^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (717) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 10891.60 | 85212.00 | $0.128^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (718) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 10591.10 | 85212.00 | $0.124^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (723) \end{gathered}$ | 2L3x2 1/2xI/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 12338.80 | 85212.00 | $0.145^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (724) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 11812.00 | 85212.00 | $0.139^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (729) \end{gathered}$ | 2L3x2 1/2x1/4 | 6.03 | 5.89 | 74.8 | 2.6300 | 10800.50 | 85212.00 | $0.127^{\text {I }}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (730) \end{gathered}$ | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ | 6.03 | 5.89 | 74.8 | 2.6300 | 10862.60 | 85212.00 | $0.127^{1}$ |

${ }^{1} P_{n} / \phi P_{n}$ controls

Torque-Arm Bottom Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $l b$ | $1 b$ | $\phi P_{n}$ |
| T24 | $\begin{gathered} 225-218.75 \\ (705) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.50 | 108.0 | 2.6300 | 139.03 | 85212.00 | $0.002^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (719) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | 107.8 | 2.6300 | 341.10 | 85212.00 | $0.004^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (720) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | 107.8 | 2.6300 | 226.98 | 85212.00 | $0.003{ }^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (725) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{~L} / 2 \times 1 / 4$ | 8.68 | 8.49 | 107.8 | 2.6300 | 602.04 | 85212.00 | $0.007{ }^{\text {1 }}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (726) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | 107.8 | 2.6300 | 648.61 | 85212.00 | $0.008^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (731) \end{gathered}$ | 2L3x2 1/2x1/4 | 8.68 | 8.49 | 107.8 | 2.6300 | 359.90 | 85212.00 | $0.004^{1}$ |
| T35 | $\begin{gathered} 100-93.75 \\ (732) \end{gathered}$ | $2 \mathrm{~L} 3 \times 2 \mathrm{~L} / 2 \times 1 / 4$ | 8.68 | 8.49 | 107.8 | 2.6300 | 432.54 | 85212.00 | $0.005^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Section Capacity Table

| Section <br> No. | Elevation <br> $f t$ | Component <br> Type | Size | Critical <br> Element | $P$ <br> $l b$ | aPallow <br> lb | $\%$ <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | $368.75-362.5$ | Leg | $23 / 4$ | 1 | -1648.36 | 102851.00 | 1.6 | Pass |
| T2 | $362.5-356.25$ | Leg | $23 / 4$ | 13 | -2308.03 | 102851.00 | 2.2 | Pass |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | Job |  | $\begin{aligned} & \text { Page } 66 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | CTNL024A |  |  |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| West Bridgevater, MA 02379 Phone: 781-713-4725 FAX: | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical <br> Element | $\begin{aligned} & P \\ & l b \\ & l \end{aligned}$ | $\begin{gathered} \ominus P_{\text {allow }} \\ l b \end{gathered}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \text { Pass } \\ \text { Fail } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T3 | 356.25-350 | Leg | $23 / 4$ | 27 | -7365.11 | 102851.00 | 7.2 | Pass |
| T4 | 350-343.75 | Leg | 3 | 38 | -5643.73 | 135284.00 | 4.2 | Pass |
| T5 | 343.75-337.5 | Leg | 3 | 49 | -40354.80 | 135284.00 | 29.8 | Pass |
| T6 | 337.5-331.25 | Leg | 3 | 61 | -41272.70 | 135284.00 | 30.5 | Pass |
| T7 | 331.25-325 | Leg | 3 | 73 | -42144.90 | 135284.00 | 31.2 | Pass |
| T8 | 325-318.75 | Leg | $31 / 4$ | 86 | -44310.60 | 171629.00 | 25.8 | Pass |
| T9 | 318.75-312.5 | Leg | $31 / 4$ | 98 | -46132.80 | 171629.00 | 26.9 | Pass |
| T10 | 312.5-306.25 | Leg | $31 / 4$ | 110 | -48317.50 | 171629.00 | 28.2 | Pass |
| T11 | 306.25-300 | Leg | $31 / 4$ | 122 | -50010.20 | 171629.00 | 29.1 | Pass |
| T12 | 300-293.75 | Leg | $31 / 4$ | 134 | -41771.80 | 171629.00 | 24.3 | Pass |
| T13 | 293.75-287.5 | Leg | $31 / 4$ | 145 | -87458.20 | 171629.00 | 51.0 | Pass |
| T14 | 287.5-281.25 | Leg | $31 / 4$ | 157 | -93174.90 | 171629.00 | 54.3 | Pass |
| T15 | 281.25-275 | Leg | $31 / 4$ | 169 | -98618.00 | 171629.00 | 57.5 | Pass |
| T16 | 275-268.75 | Leg | $31 / 4$ | 181 | -102881.00 | 171629.00 | 59.9 | Pass |
| T17 | 268.75-262.5 | Leg | $31 / 4$ | 193 | -106219.00 | 171629.00 | 61.9 | Pass |
| T18 | 262.5-256.25 | Leg | $31 / 4$ | 205 | -108310.00 | 171629.00 | 63.1 | Pass |
| T19 | 256.25-250 | Leg | $31 / 4$ | 217 | -110446.00 | 171629.00 | 64.4 | Pass |
| T20 | 250-243.75 | Leg | $31 / 4$ | 229 | -110670.00 | 171629.00 | 64.5 | Pass |
| T21 | 243.75-237.5 | Leg | $31 / 4$ | 241 | -107859.00 | 171629.00 | 62.8 | Pass |
| T22 | 237.5-231.25 | Leg | $31 / 4$ | 253 | -98956.40 | 171629.00 | 57.7 | Pass |
| T23 | 231.25-225 | Leg | $31 / 4$ | 266 | -98309.20 | 171629.00 | 57.3 | Pass |
| T24 | 225-218.75 | Leg | 3 | 278 | -74498.70 | 135284.00 | 55.1 | Pass |
| T25 | 218.75-212.5 | Leg | 3 | 290 | -119480.00 | 135284.00 | 88.3 | Pass |
| T26 | 212.5-206.25 | Leg | 3 | 302 | -121146.00 | 135284.00 | 89.5 | Pass |
| T27 | 206.25-181.25 | Leg | 3 | 314 | -123424.00 | 135284.00 | 91.2 | Pass |
| T28 | 181.25-175 | Leg | 3 | 353 | -121904.00 | 200780.00 | 60.7 | Pass |
| T29 | 175-168.75 | Leg | $31 / 4$ | 368 | -120844.00 | 171629.00 | 70.4 | Pass |
| T30 | 168.75-162.5 | Leg | $31 / 4$ | 380 | -119558.00 | 171629.00 | 69.7 | Pass |
| T31 | 162.5-156.25 | Leg | $31 / 4$ | 392 | -126905.00 | 171629.00 | 73.9 | Pass |
| T32 | 156.25-150 | Leg | $31 / 4$ | 404 | -128316.00 | 171629.00 | 74.8 | Pass |
| T33 | 150-125 | Leg | $31 / 4$ | 416 | -130492.00 | 171629.00 | 76.0 | Pass |
| T34 | 125-100 | Leg | $31 / 4$ | 454 | -132847.00 | 171629.00 | 77.4 | Pass |
| T35 | 100-93.75 | Leg | $31 / 4$ | 493 | -109593.00 | 171629.00 | 63.9 | Pass |
| T36 | 93.75-87.5 | Leg | $31 / 4$ | 505 | -141823.00 | 171629.00 | 82.6 | Pass |
| T37 | 87.5-81.25 | Leg | $31 / 4$ | 517 | -142184.00 | 171629.00 | 82.8 | Pass |
| T38 | 81.25-75 | Leg | $31 / 4$ | 529 | -143347.00 | 171629.00 | 83.5 | Pass |
| T39 | 75-50 | Leg | $31 / 4$ | 541 | -148670.00 | 171629.00 | 86.6 | Pass |
| T40 | 50-25 | Leg | $31 / 4$ | 580 | -154278.00 | 171629.00 | 89.9 | Pass |
| T41 | 25-0 | Leg | $31 / 4$ | 619 | -156670.00 | 171629.00 | 91.3 | Pass |
| T1 | 368.75-362.5 | Diagonal | L2 1/2x2 1/2x1/4 | 11 | -388.79 | 23509.60 | $\begin{gathered} 1.7 \\ 2.4 \text { (b) } \end{gathered}$ | Pass |
| T2 | 362.5-356.25 | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 20 | -1171.40 | 102123.00 | $\begin{gathered} 1.1 \\ 3.7 \text { (b) } \end{gathered}$ | Pass |
| T3 | 356.25-350 | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 5 / 16$ | 34 | 3107.66 | 103075.00 | $3.0$ | Pass |
|  |  |  |  |  |  |  | $9.8 \text { (b) }$ |  |
| T4 | 350-343.75 | Diagonal | L3x2 1/2x1/4 | 46 | -3340.61 | 27333.10 | $\begin{gathered} 12.2 \\ 14.7 \text { (b) } \end{gathered}$ | Pass |
| T5 | 343.75-337.5 | Diagonal | 5/8 | 55 | 4316.98 | 9940.20 | 43.4 | Pass |
| T6 | 337.5-331.25 | Diagonal | 5/8 | 70 | 4108.69 | 9940.20 | 41.3 | Pass |
| T7 | 331.25-325 | Diagonal | 5/8 | 82 | 3898.84 | 9940.20 | 39.2 | Pass |
| T8 | 325-318.75 | Diagonal | 3/4 | 94 | 4427.16 | 14313.90 | 30.9 | Pass |
| T9 | 318.75-312.5 | Diagonal | 3/4 | 106 | 4157.34 | 14313.90 | 29.0 | Pass |
| T10 | 312.5-306.25 | Diagonal | 3/4 | 118 | 4423.26 | 14313.90 | 30.9 | Pass |
| T11 | 306.25-300 | Diagonal | 3/4 | 132 | 7065.48 | 14313.90 | 49.4 | Pass |
| T12 | 300-293.75 | Diagonal | L3x2 1/2x1/4 | 142 | -7477.68 | 27407.90 | 27.3 | Pass |
|  |  |  |  |  |  |  | 30.1 (b) 52.0 |  |
| T14 | -287.5-281.25 | Diagonal | 5/8 | 154 | 7436.29 6569.13 | 14313.90 9940.20 | 52.0 66.1 | Pass Pass |
| T15 | 281.25-275 | Diagonal | 5/8 | 176 | 5815.81 | 9940.20 | 58.5 | Pass |
| T16 | 275-268.75 | Diagonal | 5/8 | 188 | 4908.40 | 9940.20 | 49.4 | Pass |
| T17 | 268.75-262.5 | Diagonal | 5/8 | 200 | 4057.20 | 9940.20 | 40.8 | Pass |


| thxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  | CTNL024A |  | 67 of 69 |
| Centerline Communications 750 West Center Street, Suite 301 | Project | ANCHOR | Date <br> 14:28:20 08/12/21 |
| $\begin{gathered} \text { West Bridgevater MA } 02379 \\ \text { Phone: } 71-113-4725 \\ \text { FAX: } \end{gathered}$ | T-MOBILE |  | Designed by Arielle Novak |


| Section No. | Elevation $f t$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} \curvearrowleft P_{\text {allow }} \\ l b \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T18 | 262.5-256.25 | Diagonal | 5/8 | 212 | 3580.21 | 9940.20 | 36.0 | Pass |
| T19 | 256.25-250 | Diagonal | 3/4 | 227 | 4258.81 | 14313.90 | 29.8 | Pass |
| T20 | 250-243.75 | Diagonal | 3/4 | 239 | 4274.63 | 14313.90 | 29.9 | Pass |
| T21 | 243.75-237.5 | Diagonal | 3/4 | 249 | 8590.50 | 14313.90 | 60.0 | Pass |
| T22 | 237.5-231.25 | Diagonal | 3/4 | 261 | 10770.30 | 14313.90 | 75.2 | Pass |
| T23 | 231.25-225 | Diagonal | 1 | 273 | 15421.60 | 25446.90 | 60.6 | Pass |
| T24 | 225-218.75 | Diagonal | 2L2 1/2x2 1/2x1/4 | 287 | -13948.30 | 65284.70 | 97.0 (b) |  |
|  |  |  |  |  |  |  | 21.4 | Pass |
|  |  |  |  |  |  |  | 28.1 (b) |  |
| T25 | 218.75-212.5 | Diagonal | 5/8 | 295 | 5663.70 | 9940.20 | 57.0 | Pass |
| T26 | 212.5-206.25 | Diagonal | 5/8 | 307 | 4277.62 | 9940.20 | 43.0 | Pass |
| T27 | 206.25-181.25 | Diagonal | 5/8 | 321 | 6221.96 | 9940.20 | 62.6 | Pass |
| T28 | 181.25-175 | Diagonal | 5/8 | 363 | 7038.48 | 9940.20 | 70.8 | Pass |
| T29 | 175-168.75 | Diagonal | 1 | 378 | 8623.41 | 25446.90 | 33.9 | Pass |
|  |  |  |  |  |  |  | 54.2 (b) |  |
| T30 | 168.75-162.5 | Diagonal | 1 | 385 | 9610.58 | 25446.90 | 37.8 | Pass |
|  |  |  |  |  |  |  | 60.4 (b) |  |
| T31 | 162.5-156.25 | Diagonal | 5/8 | 400 | 3400.53 | 9940.20 | 34.2 | Pass |
| T32 | 156.25-150 | Diagonal | 5/8 | 412 | 3004.49 | 9940.20 | 30.2 | Pass |
| T33 | 150-125 | Diagonal | 5/8 | 421 | 6900.56 | 9940.20 | 69.4 | Pass |
| T34 | 125-100 | Diagonal | L2 $1 / 2 \times 21 / 2 \times 3 / 16$ | 460 | 12657.80 | 24839.90 | 51.0 | Pass |
|  |  |  |  |  |  |  | 88.1 (b) |  |
| T35 | 100-93.75 | Diagonal | 2L2 1/2x2 1/2x1/4 | 502 | -15518.30 | 65385.10 | 23.7 | Pass |
|  |  |  |  |  |  |  | 31.2 (b) |  |
| T36 | 93.75-87.5 | Diagonal | 3/4 | 511 | 4333.98 | 14313.90 | 30.3 | Pass |
| T37 | 87.5-81.25 | Diagonal | 5/8 | 523 | 2986.39 | 9940.20 | 30.0 | Pass |
| T38 | 81.25-75 | Diagonal | 5/8 | 535 | 2143.16 | 9940.20 | 21.6 | Pass |
| T39 | 75-50 | Diagonal | 5/8 | 547 | 3510.52 | 9940.20 | 35.3 | Pass |
| T40 | 50-25 | Diagonal | 5/8 | 615 | 4653.67 | 9940.20 | 46.8 | Pass |
| T41 | 25-0 | Diagonal | 5/8 | 625 | 3742.79 | 9940.20 | 37.7 | Pass |
| T27 | 206.25-181.25 | Horizontal | P1.25x. 14 | 326 | -3563.47 | 12039.80 | 29.6 | Pass |
| T33 | 150-125 | Horizontal | P1.25x. 14 | 427 | -4056.89 | 12101.80 | 33.5 | Pass |
| T34 | 125-100 | Horizontal | P1.25x. 14 | 466 | -7614.99 | 12101.80 | 62.9 | Pass |
| T39 | 75-50 | Horizontal | P1.25x. 14 | 564 | -2575.05 | 12101.80 | 21.3 | Pass |
| T40 | 50-25 | Horizontal | P1.25x. 14 | 612 | -2739.65 | 12101.80 | 22.6 | Pass |
| T41 | 25-0 | Horizontal | P1.25x. 14 | 633 | -2713.61 | 12101.80 | 22.4 | Pass |
| T28 | 181.25-175 | Sccondary Horizontal | P1.25x. 14 | 364 | -2111.45 | 12039.80 | 17.5 | Pass |
|  |  |  |  |  |  |  | 34.0 (b) |  |
| T1 | 368.75-362.5 | Top Girt | 2L2 1/2x2x1/4 | 4 | 93.76 | 57256.90 | 0.3 | Pass |
| T2 | 362.5-356.25 | Top Girt | 2L2 $1 / 2 \times 3 \times 1 / 4$ | 16 | 281.61 | 75608.40 | 0.4 | Pass |
|  |  |  |  |  |  |  | 0.9 (b) |  |
| T3 | 356.25-350 | Top Girt | 2L2 1/2x3x1/4 | 28 | -969.96 | 65488.30 | 1.5 | Pass |
|  |  |  |  |  |  |  | 3.0 (b) |  |
| T4 | 350-343.75 | Top Girt | 2L2 $1 / 2 \times 2 \times 1 / 4$ | 40 | 8437.21 | 57256.90 | 14.7 | Pass |
|  |  |  |  |  |  |  | 22.0 (b) |  |
| T5 | 343.75-337.5 | Top Girt | 2L2 1/2x2x1/4 | 52 | -3850.46 | 54623.00 | 7.0 | Pass |
|  |  |  |  |  |  |  | 7.7 (b) |  |
| T6 | 337.5-331.25 | Top Girt | P1.25x. 14 | 65 | -3149.26 | 12039.80 | 26.2 | Pass |
| T7 | 331.25-325 | Top Girt | P1.25x. 14 | 77 | -3060.34 | 12039.80 | 25.4 | Pass |
| T8 | 325-318.75 | Top Girt | P1.25x. 14 | 89 | -3674.43 | 12101.80 | 30.4 | Pass |
| T9 | 318.75-312.5 | Top Girt | P1.25x. 14 | 101 | -4207.12 | 12101.80 | 34.8 | Pass |
| T10 | 312.5-306.25 | Top Girt | P1.25x. 14 | 113 | -4313.19 | 12101.80 | 35.6 | Pass |
| T11 | 306.25-300 | Top Girt | 2L2 $1 / 2 \times 2 \times 1 / 4$ | 126 | -5824.86 | 54745.00 | 10.6 | Pass |
|  |  |  |  |  |  |  | 11.7 (b) |  |
| T12 | 300-293.75 | Top Girt | 2L2 1/2×2×1/4 | 136 | 10151.10 | 57256.90 | 17.7 | Pass |
|  |  |  |  |  |  |  | 26.5 (b) |  |
| T13 | 293.75-287.5 | Top Girt | 2L2 1/2×2x1/4 | 148 | -2722.94 | 54745.00 | 5.0 | Pass |
|  |  |  |  |  |  |  | 5.5 (b) |  |
| T14 | 287.5-281.25 | Top Girt | P1.25x. 14 | 160 | -4351.37 | 12101.80 | 36.0 | Pass |
| T15 | 281.25-275 | Top Girt | P1.25x.14 | 172 | -3900.72 | 12101.80 | 32.2 | Pass |
| T16 | 275-268.75 | Top Girt | P1.25x. 14 | 184 | -3385.59 | 12101.80 | 28.0 | Pass |


| tnxTower | CTNL024A |  | $\begin{aligned} & \text { Page } \\ & 68 \text { of } 69 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Centerline Communications <br> 750 West Center Street, Suite 301 <br> West Bridgewater; MA 02379 <br> Phone: 781-713-4725 FAX: | Project | ANCHOR | Date $14: 28: 20 \quad 08 / 12 / 21$ |
|  | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} o P_{\text {allow }} \\ l b \end{gathered}$ | $\%$ <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T17 | 268.75-262.5 | Top Girt | P1.25x. 14 | 197 | -3136.15 | 12101.80 | 25.9 | Pass |
| T18 | 262.5-256.25 | Top Girt | P1.25x. 14 | 209 | -3125.18 | 12101.80 | 25.8 | Pass |
| T19 | 256.25-250 | Top Girt | P1.25x.14 | 221 | -3852.24 | 12101.80 | 31.8 | Pass |
| T20 | 250-243.75 | Top Girt | 2L2 1/2x2x1/4 | 233 | -4708.46 | 54377.90 | 8.7 | Pass |
|  |  |  |  |  |  |  | 14.8 (b) |  |
| T21 | 243.75-237.5 | Top Girt | 2L2 1/2×2x1/4 | 245 | -5842.14 | 54745.00 | 10.7 | Pass |
|  |  |  |  |  |  |  | 11.8 (b) |  |
| T22 | 237.5-231.25 | Top Girt | 2L2 1/2x2x1/4 | 257 | -6091.08 | 54745.00 | 11.1 | Pass |
|  |  |  |  |  |  |  | 12.3 (b) |  |
| T23 | 231.25-225 | Top Girt | 2L2 1/2x2x1/4 | 269 | -8163.35 | 54745.00 | 14.9 | Pass |
|  |  |  |  |  |  |  | 16.4 (b) |  |
| T24 | 225-218.75 | Top Girt | 2L2 1/2x2x1/4 | 280 | 13331.70 | 57256.90 | 23.3 | Pass |
|  |  |  |  |  |  |  | 34.8 (b) |  |
| T25 | 218.75-212.5 | Top Girt | 2L2 1/2x2x1/4 | 292 | 6194.35 | 57256.90 | 10.8 | Pass |
|  |  |  |  |  |  |  | 16.2 (b) |  |
| T26 | 212.5-206.25 | Top Girt | P1.25x. 14 | 304 | -2994.82 | 12039.80 | 24.9 | Pass |
| T27 | 206.25-181.25 | Top Girt | P1.25x. 14 | 317 | -2393.45 | 12039.80 | 19.9 | Pass |
| T28 | 181.25-175 | Top Girt | P1.25x. 14 | 356 | -4002.23 | 12039.80 | 33.2 | Pass |
| T29 | 175-168.75 | Top Girt | P1.25x. 14 | 372 | -4795.94 | 12101.80 | 39.6 | Pass |
| T30 | 168.75-162.5 | Top Girt | P1.25x. 14 | 382 | -5677.95 | 12101.80 | 46.9 | Pass |
| T31 | 162.5-156.25 | Top Girt | 2L2 1/2x2x1/4 | 396 | 4944.19 | 59295.90 | 8.3 | Pass |
|  |  |  |  |  |  |  | 15.5 (b) |  |
| T32 | 156.25-150 | Top Girt | P1.25x. 14 | 406 | -2222.50 | 12101.80 | 18.4 | Pass |
| T33 | 150-125 | Top Girt | P1.25x. 14 | 418 | -2260.19 | 12101.80 | 18.7 | Pass |
| T34 | 125-100 | Top Girt | P1.25x. 14 | 457 | -4961.87 | 12101.80 | 41.0 | Pass |
| T35 | 100-93.75 | Top Girt | 2L2 1/2x2x1/4 | 498 | 12914.50 | 57256.90 | 22.6 | Pass |
|  |  |  |  |  |  |  | 33.7 (b) |  |
| T36 | 93.75-87.5 | Top Girt | 2L2 1/2x2x1/4 | 508 | 8487.25 | 59295.90 | 14.3 | Pass |
|  |  |  |  |  |  |  | 26.7 (b) |  |
| T37 | 87.5-81.25 | Top Girt | P1.25x. 14 | 522 | -2462.69 | 12101.80 | 20.3 | Pass |
| T38 | 81.25-75 | Top Girt | P1.25x. 14 | 534 | -2482.85 | 12101.80 | 20.5 | Pass |
| T39 | 75-50 | Top Girt | P1.25x. 14 | 546 | -2575.05 | 12101.80 | 21.3 | Pass |
| T40 | 50-25 | Top Girt | L2 1/2x2x1/4 | 585 | -2672.18 | 15544.20 | 17.2 | Pass |
|  |  |  |  |  |  |  | 19.8 (b) |  |
| T41 | 25-0 | Top Girt | P1.25x. 14 | 624 | -2713.61 | 12101.80 | 22.4 | Pass |
| T4 | 350-343.75 | Guy A@350 | 7/8 | 670 | 20577.20 | 47820.00 | 43.0 | Pass |
| T12 | 300-293.75 | Guy A@300 | 7/8 | 688 | 23402.00 | 47820.00 | 48.9 | Pass |
| T24 | 225-218.75 | Guy A@225 | 3/4 | 706 | 20607.30 | 34980.00 | 58.9 | Pass |
| T31 | 162.5-156.25 | Guy A@162.5 | 3/4 | 714 | 19985.30 | 34980.00 | 57.1 | Pass |
| T35 | 100-93.75 | Guy A@100 | 9/16 | 728 | 10756.00 | 21000.00 | 51.2 | Pass |
| T40 | 50-25 | Guy A@50 | 9/16 | 735 | 9484.38 | 21000.00 | 45.2 | Pass |
| T4 | 350-343.75 | Guy B@350 | 7/8 | 665 | 19104.50 | 47820.00 | 40.0 | Pass |
| T12 | 300-293.75 | Guy B@300 | 7/8 | 682 | 22134.80 | 47820.00 | 46.3 | Pass |
| T24 | 225-218.75 | Guy B@225 | 3/4 | 700 | 21076.90 | 34980.00 | 60.3 | Pass |
| T31 | 162.5-156.25 | Guy B@162.5 | 3/4 | 713 | 20629.00 | 34980.00 | 59.0 | Pass |
| T35 | 100-93.75 | Guy B@100 | 9/16 | 721 | 11388.80 | 21000.00 | 54.2 | Pass |
| T40 | 50-25 | Guy B@50 | 9/16 | 734 | 9360.65 | 21000.00 | 44.6 | Pass |
| T4 | 350-343.75 | Guy C@350 | 7/8 | 658 | 19079.60 | 47820.00 | 39.9 | Pass |
| T12 | 300-293.75 | Guy C@300 | 7/8 | 677 | 22288.50 | 47820.00 | 46.6 | Pass |
| T24 | 225-218.75 | Guy C@225 | 3/4 | 695 | 20690.70 | 34980.00 | 59.1 | Pass |
| T31 | 162.5-156.25 | Guy C@162.5 | 3/4 | 712 | 20258.50 | 34980.00 | 57.9 | Pass |
| T35 | 100-93.75 | Guy C@100 | 9/16 | 716 | 10822.80 | 21000.00 | 51.5 | Pass |
| T40 | 50-25 | Guy C@50 | 9/16 | 733 | 9655.01 | 21000.00 | 46.0 | Pass |
| T4 | 350-343.75 | Torque Arm Top@350 | 2L3x2 1/2x1/4 | 660 | 18529.80 | 85212.00 | 21.7 | Pass |
| T12 | 300-293.75 | Torque Arm <br> Top@300 | 2L3x2 1/2x1/4 | 690 | 20533.60 | 85212.00 | 24.1 | Pass |
| T24 | 225-218.75 | Torque Arm Top@225 | $2 \mathrm{~L} 3 \times 21 / 2 \times 1 / 4$ | 708 | 19990.60 | 85212.00 | 23.5 | Pass |
| T35 | 100-93.75 | Torque Arm <br> Top@100 | 2L3x2 1/2x1/4 | 723 | 12338.80 | 85212.00 | 14.5 | Pass |


| tnxTower <br> Centerline Communications 750 West Center Street, Suite 301 | Job | CTNL024A | Page 69 of 69 |
| :---: | :---: | :---: | :---: |
|  | Project | ANCHOR | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:28:20 08/12/21 } \end{array}$ |
| $\begin{aligned} & \text { West Bridgevater, MA } 02379 \\ & \text { Phone: } 78-1173-4725 \\ & \text { FAX: } \end{aligned}$ | Client | T-MOBILE | Designed by Arielle Novak |


| Section No. | $\begin{gathered} \text { Elevation } \\ f t \\ \hline \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} \curvearrowleft P_{\text {allow }} \\ l b \end{gathered}$ | $\%$ <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | 350-343.75 | Torque Arm Bottom@350 | 2L3x2 1/2x1/4 | 675 | -21837.80 | 46126.40 | 47.3 | Pass |
| T12 | 300-293.75 | Torque Arm Bottom@300 | 2L3x2 1/2x1/4 | 693 | -25674.50 | 46226.30 | 55.5 | Pass |
| T24 | 225-218.75 | Torque Arm Bottom@225 | 2L3x2 1/2x1/4 | 705 | -21487.20 | 46126.40 | 46.6 | Pass |
| T35 | 100-93.75 | Torque Arm Bottom@100 | 2L3x2 1/2x1/4 | 725 | -8317.80 | 46226.30 | 18.0 | Pass |
|  |  |  |  |  |  | Leg (T41) <br> Diagonal <br> (T23) | $\begin{gathered} \text { Summary } \\ 91.3 \\ 97.0 \end{gathered}$ | Pass Pass |
|  |  |  |  |  |  | Horizontal <br> (T34) | 62.9 | Pass |
|  |  |  |  |  |  | Secondary Horizontal (T28) | 34.0 | Pass |
|  |  |  |  |  |  | Top Girt (T30) | 46.9 | Pass |
|  |  |  |  |  |  | Guy A (T24) | 58.9 | Pass |
|  |  |  |  |  |  | Guy B (T24) | $60.3$ | Pass |
|  |  |  |  |  |  | Guy C (T24) | 59.1 | Pass |
|  |  |  |  |  |  | Torque Arm Top (T12) | 24.1 | Pass |
|  |  |  |  |  |  | Torque Arm Bottom (T12) | 55.5 | Pass |
|  |  |  |  |  |  | Bolt Checks | 97.0 | Pass |
|  |  |  |  |  |  | RATING = | 97.0 | Pass |

Program Version 8.1.1.0-6/3/2021 File:C:/Box/Box/Projects/New England Projects/T-Mobile/SITES/CT/CTNL024A - 689 OLD COLCHESTER RD GT/ANCHOR/Structural/Working Files/Analysis/tnx/CTNL024A.eri

## Pier and Pad Foundation

## BU \# : <br> Site Name: CTNL024A <br> App. Number: <br> CTNLO24A

| TIA-222 Revision: | G |
| ---: | :---: |
| Tower Type: | Guyed |


| Top \& Bot. Pad Rein. Different?: | $\Gamma$ |
| ---: | :--- |
| Block Foundation?: | $\Gamma$ |


| Superstructure Analysis Reactions |  |  |  |
| ---: | :---: | :---: | :---: |
| Compression, $\mathbf{P}_{\text {comp: }}:$ | 467.83 | kips |  |
| Base Shear, V_comp: | 0.606 | kips |  |
|  |  |  |  |
|  |  |  |  |
| Moment, $\mathbf{M}_{\mathbf{u}}:$ | 0 | ft-kips |  |
| Tower Height, H: | 368.75 | ft |  |
|  |  |  |  |
| Bolt Circle / Bearing Plate Width, BC: |  | in |  |
| BP Dist. Above Fdn, |  |  |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating $^{*}$ | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 136.50 | 0.61 | $\mathbf{0 . 4 \%}$ | Pass |
| Bearing Pressure (ksf) | 9.60 | 10.19 | $\mathbf{9 6 . 5 \%}$ | Pass |
| Overturning (kipft) | 160.59 | 3.03 | $\mathbf{1 . 9 \%}$ | Pass |
|  |  |  |  |  |
|  |  |  |  |  |


| Pier Properties |  |  |
| ---: | :---: | :---: |
| Pier Shape: | Circular |  |
| Pier Diameter, dpier: | 3 | ft |
| Ext. Above Grade, E: | 1.5 | ft |


| Pad Properties |  |  |
| ---: | :---: | :---: |
| Depth, D: | 3.5 | ft |
| Pad Width, W: | 7 | ft |
| Pad Thickness, T: | 2 | ft |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 3 | ksi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |


| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ |  | 120 |
| Ucf |  |  |
| Ultimate Gross Bearing, Qult: | 16.000 | ksf |
| Cohesion, $\mathbf{C u}:$ | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 30 | degrees |
| SPT Blow Count, $\mathrm{N}_{\text {blows: }}$ | 10 |  |
| Base Friction, $\mu:$ | 0.45 |  |
| Neglected Depth, N: | 0.00 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | $\mathrm{N} / \mathrm{A}$ | ft |



| Neglect Depth, Neg: | 0 | ft |
| ---: | :---: | :--- |
| Groundwater Level, gw: | N/A | ft |



Guyed Anchor Block Foundation
Checks capacity of anchor blocks for a guyed tower. $\begin{aligned} & \text { BU\#: } \\ & \text { Site Name: } \text { CTNLO24A } \\ & \text { Order Number: } \\ & \text { Location: } \\ & \text { TIA-222 Revision: } \\ &\end{aligned}$




| Wt. Avg.Concrete Density, $\delta \mathbf{x x}$ | 0.150 | kcf |
| :--- | :--- | :--- |

Guyed Anchor Block Foundation



Guyed Anchor Block Foundation



| Neglect Depth, Neg: | 0 | ft |
| ---: | :---: | :--- |
| Groundwater Level, gw: | $\mathrm{N} / \mathrm{A}$ | ft |



Guyed Anchor Block Foundation



| Wt. Avg.Concrete Density, $\mathbf{x}$ | 0.150 | kcf |
| :--- | :--- | :--- |

## Exhibit F

## Power Density/RF Emissions Report

# Radio Frequency Emissions Analysis Report 

T-Mobile Wireless Tower Facility
August 23, 2021
Analysis Format: Theoretical Calculations


## Statement of Compliance

T-Mobile will be compliant with FCC Regulations once the mitigation measures recommended in this report are implemented.

Centerline PN: 950003-009
CTNL024A
MONTVILLE-OLD COLCHESTER RD
689 Old Colchester Rd, Uncasville, CT 06382

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## Overview

Centerline Communications, LLC ("Centerline") has been contracted to provide a Radio Frequency (RF) Analysis for the following T-Mobile wireless tower facility to determine whether the facility is in compliance with federal standards and regulations regarding RF emissions. This analysis includes theoretical emissions calculations for all existing equipment for T -Mobile .

The facility is located on a 370' Tower in Uncasville, Connecticut. Access to the facility is restricted to authorized personnel and facility management.

Analysis Site Data

| Site ID: | CTNLO24A |
| ---: | :--- |
| Site Name: | MONTVILLE-OLD COLCHESTER RD |
| Site Address: | 689 Old Colchester Rd, Uncasville, CT 06382 |
| Site Latitude: | 41.453110 |
| Site Longitude: | -72.15403 |
| Facility Type: | Tower |

## Compliance Summary

| Status: | T-Mobile will be compliant with FCC Regulations upon <br> installation of signage. |
| ---: | :--- |
| Site Modeled Composite MPE\% (General Public Limit): | $0.16 \%$ |
| T-Mobile Max Modeled MPE\% (General Public Limit): | $0.16 \%$ |
| Lock or Control Measures if Present: | Not Restricted |

In addition to the T-Mobile antennas and radio equipment there are antennas and radio equipment for AT\&T which have been included in this analysis as part of the overall site compliance determination.
*To be conservative, all sites are considered uncontrolled for modeling purposes unless confirmed otherwise by a site visit.

## FCC Guidelines

All power density values used in this report were analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General Population/Uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limit for the 600,700 , and 800 MHz Bands is approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}, 467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and $567 \mu \mathrm{~W} / \mathrm{cm}^{2}$ respectively, and the general population exposure limit for the 1900 MHz PCS, 2100 MHz AWS, $2500 \mathrm{MHz}, 3500 \mathrm{MHz}$ CBRS, 5000 MHz LAA, 28 GHz , and 39 GHz bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density. Reference the Site Antenna Data Table for list of frequencies in operation at this site.

Occupational/Controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure, have been properly trained in RF safety and can exercise control over their exposure. Occupational/Controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure, have been trained in RF safety and can exercise control over his or her exposure by leaving the area or by some other appropriate means. The Occupational/Controlled exposure limits all utilized frequency bands is five (5) times the FCC's General Public / Uncontrolled exposure limit.

Additional details can be found in FCC OET 65.

## Calculation Methodology \& Data

Centerline has performed theoretical calculations on all transmission equipment located on this facility. All calculations have been performed using the RoofMaster ${ }^{\oplus}$ software from Waterford Consultants LLC. This software performs calculations using a cylindrical model for very conservative power density predictions within the near-field of the antenna where the antenna pattern has not truly formed yet. Within this area power density values tend to decrease based upon an inverse distance function. At the point where it is appropriate for modeling to change from near-field calculations to far-field calculations the power decreases inversely with the square of the distance. This modeling technique is accurate with low antenna centerlines, such as rooftops, where persons can get close to the antennas and pass through fields in close proximity.

The below calculation in Figure 1 shows the theoretical distribution of power over an imaginary cylinder with equal power distribution in all directions.


$$
S=\frac{P}{2 \pi R h}
$$

Figure 1: Distribution of power over an imaginary cylinder in all directions
This model can be modified for directional antennas to show directionality of power distribution. This formula will tend to be conservative as it assumes that all power is focused between the 3 dB power roll off points as shown in Figure 2.


Figure 2: Distribution of power over an imaginary cylinder in all directions inside the half power roll off points (HBW)

The proposed antenna configuration for T-Mobile and any other known wireless carriers at this facility are shown below in Table 1 - Site Antenna Data Table.

All calculations for this facility were performed assuming that all radios were running at full power and were uncombined in their RF paths with the configuration shown in table 1. FCC OET Bulletin 65 Edition 97-01 recommends that modeling of this nature should be done as described prior to yield a worst-case scenario. Due to the dynamic nature of many deployed systems the "real world" values will most likely be less than those shown in this report due to worst-case values being shown in all instances.

For all "Other" systems on this facility, exact equipment was used if available. In instances where "Other" system equipment was not available, standard radio configurations for these systems were utilized based upon prior experience with these systems on facilities in this area.

## Site Antenna Data Table



Centerline Communications, LLC 750 W Center St West Bridgewater MA 02379 Page|6

| Sector | Operator | Frequency Band | TX <br> Power <br> Per <br> Channel | $\begin{gathered} \text { Tx } \\ \# \end{gathered}$ | ERP | Antenna Make | Antenna Model | Gain <br> (dBd) | $A z\left({ }^{\circ}\right)$ | Antenna <br> Centerline <br> Height (ft) | Z Value <br> (ft)** |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16 | Unknown | 700 | 40 | 4 | 2736.02 | GENERIC | PANEL 6FT | 12.33 | 30 | 304.9 | 301.90 |
| 17 | Unknown | 3700 | 50 | 4 | 43154.89 | GENERIC | PANEL 6FT | 23.34 | 150 | 304.9 | 303.44 |
| 18 | Unknown | 1900 | 40 | 4 | 6139.32 | GENERIC | PANEL 6FT | 15.84 | 150 | 304.9 | 301.90 |
| 19 | Unknown | 2100 | 40 | 4 | 6968.19 | GENERIC | PANEL 6FT | 16.39 | 150 | 304.9 | 301.90 |
| 19 | Unknown | 700 | 40 | 4 | 2736.02 | GENERIC | PANEL 6FT | 12.33 | 150 | 304.9 | 301.90 |
| 20 | Unknown | 3700 | 50 | 4 | 43154.89 | GENERIC | PANEL 6FT | 23.34 | 270 | 304.9 | 303.44 |
| 21 | Unknown | 1900 | 40 | 4 | 6139.32 | GENERIC | PANEL 6FT | 15.84 | 270 | 304.9 | 301.90 |
| 22 | Unknown | 2100 | 40 | 4 | 6968.19 | GENERIC | PANEL 6FT | 16.39 | 270 | 304.9 | 301.90 |
| 22 | Unknown | 700 | 40 | 4 | 2736.02 | GENERIC | PANEL 6FT | 12.33 | 270 | 304.9 | 301.90 |
| 23 | Unknown | 850 | 13 | 1 | 102.32 | GENERIC | OMNI 12FT | 8.96 | 30 | 249.8 | 243.80 |
| 24 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 30 | 242.1 | 240.87 |
| 25 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 30 | 242.1 | 240.87 |
| 26 | Unknown | 850 | 40 | 4 | 2924.96 | GENERIC | PANEL 6FT | 12.62 | 30 | 242.1 | 239.10 |
| 27 | Unknown | 1900 | 30 | 4 | 4604.49 | GENERIC | PANEL 6FT | 15.84 | 30 | 242.1 | 239.10 |
| 28 | Unknown | 2100 | 40 | 4 | 6968.19 | GENERIC | PANEL 6FT | 16.39 | 30 | 242.1 | 239.10 |
| 29 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 150 | 242.1 | 240.87 |
| 30 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 150 | 242.1 | 240.87 |
| 31 | Unknown | 850 | 40 | 4 | 2924.96 | GENERIC | PANEL 6FT | 12.62 | 150 | 242.1 | 239.10 |
| 32 | Unknown | 1900 | 30 | 4 | 4604.49 | GENERIC | PANEL 6FT | 15.84 | 150 | 242.1 | 239.10 |
| 33 | Unknown | 2100 | 40 | 4 | 6968.19 | GENERIC | PANEL 6FT | 16.39 | 150 | 242.1 | 239.10 |
| 34 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 270 | 242.1 | 240.87 |
| 35 | Unknown | 3840 | 75 | 1 | 13805.79 | GENERIC | PANEL 6FT | 22.65 | 270 | 242.1 | 240.87 |
| 36 | Unknown | 850 | 40 | 4 | 2924.96 | GENERIC | PANEL 6FT | 12.62 | 270 | 242.1 | 239.10 |
| 37 | Unknown | 1900 | 30 | 4 | 4604.49 | GENERIC | PANEL 6FT | 15.84 | 270 | 242.1 | 239.10 |
| 38 | Unknown | 2100 | 40 | 4 | 6968.19 | GENERIC | PANEL 6FT | 16.39 | 270 | 242.1 | 239.10 |
| 39 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 200.1 | 199.56 |
| 40 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 180 | 179.46 |
| 41 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 147.8 | 147.26 |
| 42 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 140.2 | 139.66 |
| 43 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 124.9 | 124.36 |
| 44 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 62.2 | 61.66 |
| 45 | Unknown | 850 | 20 | 1 | 129.13 | GENERIC | YAGI 1FT | 8.1 | 30 | 39.8 | 39.26 |

Table 1: Total Site Antenna data table ${ }^{* *}(Z$ Value is distance from bottom of antenna to walking surface)

## Results

All calculations performed based upon the data listed for this facility have produced results that are within allowable limits for General Population for exposure to RF emissions as specified by federal standards.

T-Mobile's RF Exposure: Responsibilities, Procedures \& Guidelines document states that microwave dishes are compliant if they are mounted 20 feet or greater above any accessible walking or working surface.

| Maximum Predicted MPE Level on Site: | \% of MPE Limit: | Location: |
| ---: | :---: | :---: |
| Accessible General Population MPE Limits: | $0.16 \%$ |  |
| Accessible Occupational MPE Limits: | $0.03 \%$ |  |


| Ground Level Assessment: | \% of MPE Limit: |
| ---: | :---: |
| Ground Level General Population MPE Limits: | $0.16 \%$ |
| Ground Level Occupational MPE Limits: | $0.03 \%$ |


| Sector A: Transmitting over Ground | \% of MPE Limit: | *Distance from Antenna: |
| ---: | :---: | :---: |
| Accessible General Population MPE Limits: | $\mathbf{0 . 1 6 \%}$ | N/A |
| Accessible Occupational MPE Limits: | $\mathbf{0 . 0 3 \%}$ | N/A |


| Sector B: Transmitting over Ground | \% of MPE Limit: | *Distance from Antenna: |
| ---: | :---: | :---: |
| Accessible General Population MPE Limits: | $\mathbf{0 . 0 2 \%}$ | N/A |
| Accessible Occupational MPE Limits: | $\mathbf{0 . 0 0 \%}$ | N/A |


| Sector C: Transmitting over Ground | \% of MPE Limit: | *Distance from Antenna: |
| ---: | :---: | :---: |
| Accessible General Population MPE Limits: | $\mathbf{0 . 0 2 \%}$ | N/A |
| Accessible Occupational MPE Limits: | $\mathbf{0 . 0 0 \%}$ | N/A |

*Distance from Antenna is the distance in feet that the MPE limits are exceeded from the front face of the antenna, outward across an accessible area.

## APPENDIX A: Emissions Thresholds for Walking Surfaces and Signage




## Compliance Actions

| Access | - Ensure all access points are locked. |
| ---: | :--- |
|  | - <br>  <br>  <br>  <br> - Install (1) Guideline sign on the inside of the access point. (1) Caution sign on the inside of the access point. <br> - Install (1) Emergency sign on the inside of the access point. |
| Alpha Sector | - No Action Needed. |
| Beta Sector | - No Action Needed. |
| Gamma Sector | - No Action Needed. |
| Notes: | - If there is a fixed climbing point located on this site, a Guideline and |
|  | Caution sign should be installed at that location. |

## APPENDIX B: RF Signage Description Table

COMMUNICATIONS

| Sign | Description |
| :---: | :---: |
|  | RF Guideline Sign <br> Gives guidelines on how to proceed in areas that may exceed either the FCC's General Population or Occupational emissions limits. |
| IN CASE OF EMERGENC CALL 911 Site No: Address: | Emergency Sign <br> Used to inform individuals to call 911 in case of emergency. |
|  | Blue Notice Sign <br> Used to inform individuals that they are entering an area that may exceed the FCC's General Population limits. Must be placed anywhere the public can get within 30 feet vertically or horizontally of an antenna. |
|  | Yellow Caution Sign <br> Used to inform individuals that they are entering an area that may exceed the either the FCC's General Population or Occupational Emissions limits. It must be placed so it is visible from all approachable sides. It must also be just outside of the area predicted to exceed the MPE limits so it can be read without standing within the affected area. |
|  | Orange Warning Sign (Previously Red) <br> Used to inform individuals that they are entering an area that may exceed $5 x$ the FCC's Occupational emissions limit. It must be placed so it is visible from all approachable sides. It must also be just outside of the area predicted to exceed the MPE limits so it can be read without standing within the affected area. |

## APPENDIX C: FCC Emissions Threshold Limits

| Table 1: Limits for Maximum Permissible Exposure (MPE) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| (A) Limits for Occupational/Controlled Exposure |  |  |  |  |
| Frequency Range (MHz) | Electric Field Strength <br> (E) <br> (V/m) | Magnetic Field Strength <br> (H) <br> (A/m) | Power Density (S) $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time $[\mathrm{E}]^{2}$, $[\mathrm{H}]^{2}$, or S <br> (minutes) |
| 0.3-3.0 | 614 | 1.63 | (100)* | 6 |
| 3.0-30 | 1842/f | 4.89/f | $\left(900 / \mathrm{f}^{2}\right)^{*}$ | 6 |
| 30-300 | 61.4 | 0.163 | 1.0 | 6 |
| 300-1,500 | -- | -- | f/300 | 6 |
| 1,500-100,000 | -- | -- | 5 | 6 |
| (B) Limits for General Public/Uncontrolled Exposure |  |  |  |  |
| Frequency Range ( MHz ) | Electric Field Strength <br> (E) $(\mathrm{V} / \mathrm{m})$ | Magnetic Field Strength <br> ( H ) $(\mathrm{A} / \mathrm{m})$ | Power Density (S) $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time $[E]^{2}$, $[H]^{2}$, or $S$ (minutes) |
| 0.3-1.34 | 614 | 1.63 | (100)* | 30 |
| 1.34-30 | 824/f | 2.19/f | $\left(180 / \mathrm{f}^{2}\right)^{*}$ | 30 |
| 30-300 | 27.5 | 0.073 | 0.2 | 30 |
| 300-1,500 | -- | -- | f/1,500 | 30 |
| 1,500-100,000 | -- | -- | 1.0 | 30 |
| $\mathrm{f}=$ Frequency in (MHz) |  |  |  |  |

Figure 1. FCC Limits for Maximum Permissible Exposure (MPE)
Plane-wave Equivalent Power Density


## APPENDIX D: Certifications

I, Devon Wangeline, preparer of this report certify that I am fully trained and aware of the Rules and Regulations of both the Federal Communications Commissions (FCC) and the Occupational Safety and Health Administration (OSHA) with regard to Human Exposure to Radio Frequency Radiation. I have been trained in the procedures and requirements outlined in T-Mobile's FCC Regulatory Compliance Manual.

Devon Wangeline
8/23/2021

I, Brandon Green, reviewer and approver of this report certify that I am fully trained and aware of the Rules and Regulations of both the Federal Communications Commissions (FCC) and the Occupational Safety and Health Administration (OSHA) with regard to Human Exposure to Radio Frequency Radiation. I have been trained in the procedures and requirements outlined in T-Mobile's FCC Regulatory Compliance Manual.

Brandon Green
8/23/2021

## Exhibit G

## Mailing Receipts/Proof of Notice

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Customer Center, Staples ${ }^{\circledR}$ or Authorized Shipping Outlet near you. Items sent via UPS Return Services(SM) (including via Ground) are also accepted at Drop Boxes. To find the location nearest you, please visit the Resources area of CampusShip and select UPS Locations.
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## 〈 1 of 3 〉

Tropical Storm Ida's Effects Continue to Impact Service in Louisiana ...More (/us/en/service-ale


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## 〈 1 of 3 〉

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Your shinnenteturnto=https\%3A\%2F\%2Fwww.ups.com\%2Ftrack\%3Floc\%3Den_US\%26Requester\%3Dlasso)
1Z9Y45030318473961
$\overline{\bar{E}}$ stimated delivery
Friday, September 17 by 7:00 P.M.

| $\checkmark$ | Label Created |
| :--- | :--- |
| $\checkmark$ | Shipped |
|  | Out for Delivery |
|  | Delivery |

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QUINCY, MA US

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Tropical Storm Ida's Effects Continue to Impact Service in Louisiana ...More (/us/en/service-ale

Your shinment arnt =https\%3A\%2F\%2Fwww.ups.com\%2Ftrack\%3Floc\%3Den_US\%26Requester\%3Dlasso)
129Y45030307065986
Delivered On
Friday, September 17 at 9:54 A.M. at Front Desk

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[^0]:    Description
    Generac Automatic Transfer Switches are designed for use with single phase generators that utilize an Evolution ${ }^{\text {to }}$ or Nexus'm Controller. The 100.200 . and 400 amp open transition switches are available in single phase in both service equipment rated and
    non-service equipment rated configurations. The 150 and 300 amp open transition switches are only available in a service rated non-service equipment

    Standard Features
    Service rated (RXSW) Generac Automatic Transfer Switches are housed in an aluminum NEMA/UL Type 3R enclosuren. with electrostatically applied and baked powder paint. The Heavy Duty Generac Contactor is a ULrecognized device. designed for
    years of service. The controller the the generator handles all the timing. sensing. exercising functions, and transfer commands. All years of service. The controller at the generator $h$
    switches are covered by a 5 year limited warranty.
    (DPM), these switches have the capability to manage up to 4 individual HVAC (24VAC
    DPM Technology Through the use of digital power technology (DPM), these switches have the capability to manage up to 4 individual HVAC ( 24 VAC
    controlled) loads with noaddditional hardware. When used in tandem with Smart Management Modules, up to 8 more loads can be controlled) loads with no additiona h hardware. When used in tandem with smar ManagementMo
    managed as well. providing the most installationefficientpowermanagement options available.

[^1]:    ${ }^{\prime}$ Note: $K$ factors are applied to member segment lengths. $K$-braces without inner supporting members will have the $K$ factor in the out-of-plane direction applied to the overall length.

[^2]:    ${ }^{1} P_{u} / \phi P_{n}$ controls

[^3]:    ${ }^{1} P_{u} / \phi P_{n}$ controls

