



Crown Castle  
3530 Toringdon Way, Suite 300  
Charlotte, NC 28277

October 14, 2015

Melanie A. Bachman  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**RE: T-Mobile - Exempt Modification - Crown Site BU: 806359**  
**T-Mobile Site ID: CTNH009B**  
**Located at: 423 Oronoque Road, Milford, CT 06460**

Dear Ms. Bachman:

This letter and exhibits are submitted on behalf of T-Mobile. T-Mobile is making modifications to certain existing sites in its Connecticut system in order to implement their 700MHz technology. Please accept this letter and exhibits as notification, pursuant to § 16-50j-73 of the Regulations of Connecticut State Agencies (“R.C.S.A.”), of construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In compliance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to The Honorable Benjamin G. Blake, Mayor, City of Milford and Mr. Paul Guernsey and Mr. David Guernsey, Property Owner’s.

T-Mobile plans to modify the existing wireless communications facility owned by Crown Castle and located at **423 Oronoque Road, Milford, CT**. Attached are a compound plan and elevation depicting the planned changes (Exhibit-1), and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration (Exhibit-2). Also included is a power density table report reflecting the modification to T-Mobile’s operations at the site (Exhibit-3).

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes (“C.G.S.”) § 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in the R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing tower. T-Mobile’s additional antennas will be located at the same elevation on the existing tower.
2. There will be no proposed modifications to the ground and no extension of boundaries.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more.

Melanie A. Bachman

August 27, 2015

Page 2

4. A Structural Modification Report confirming that the tower and foundation can support T-Mobile's proposed modifications is included as Exhibit-2.
5. The operation of the additional antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table report for T-Mobile's modified facility is included as Exhibit-3.

For the foregoing reasons, T-Mobile respectfully submits the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Kimberly Myl.

Sincerely,

Kimberly Myl  
Real Estate Specialist

Enclosures

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc: Mr. Benjamin G. Blake, Mayor of City of Milford  
City of Milford  
70 West River Street  
Milford, CT 06460

Mr. David Guernsey  
423 Oronoque Road  
Milford, CT 06460

Mr. Paul Guernsey  
1247 Middle Road  
Warren, ME 04864

Winthrop S. Smith, Jr., Esq.  
Dey Smith, LLC  
9 Depot Street, 2<sup>nd</sup> Floor  
Milford, CT 06460



T-MOBILE NORTHEAST LLC

T-MOBILE SITE #: CTNH009B
CROWN CASTLE BU #: 806359
SITE NAME: NHV 104 943122
423 ORONOQUE ROAD
MILFORD, CT 06460
NEW HAVEN COUNTY



T-MOBILE NORTHEAST LLC
4 SYLVAN WAY
PARSIPPANY, NJ 07054



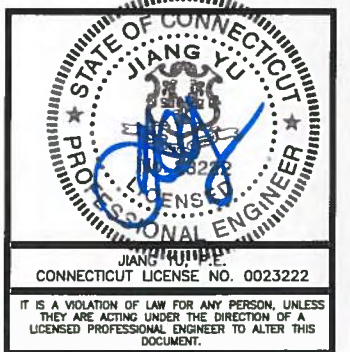
CROWN CASTLE
3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

CTNH009B
NHV 104 943122

Table with 2 columns: Revision, Description. Row 1: 10/16/15 ISSUED AS FINAL. Row 2: 10/07/15 ISSUED FOR REVIEW.



Dewberry Engineers Inc.
600 PARSSIPANY ROAD
SUITE 301
PARSSIPANY, NJ 07054
PHONE: 973.739.9400
FAX: 973.739.9710



DRAWN BY: RA
REVIEWED BY: BSH
CHECKED BY: GHN
PROJECT NUMBER: 50066258
JOB NUMBER: 50074607
SITE ADDRESS:

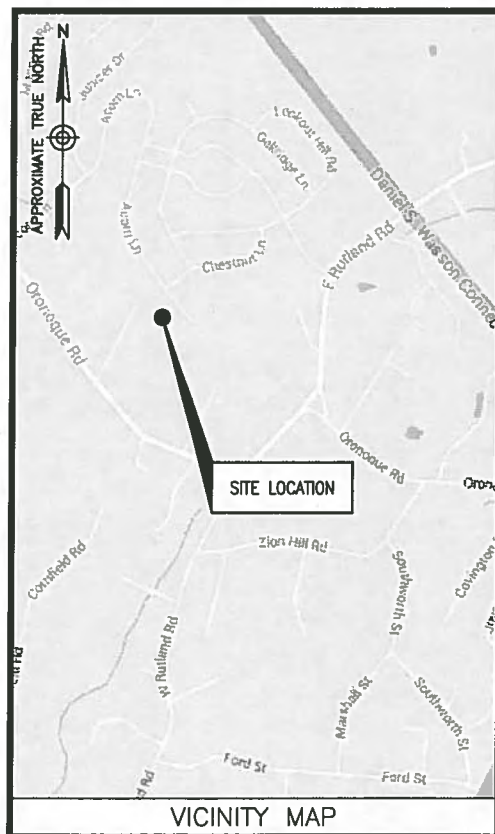
423 ORONOQUE ROAD
MILFORD, CT 06460
NEW HAVEN COUNTY

SHEET TITLE

TITLE SHEET

SHEET NUMBER

T-1



VICINITY MAP

FROM PARSSIPANY, NJ:

DEPART SYLVAN WAY AND TAKE I-80 E TO I-95 N. TAKE EXIT 1C-D FOR ALBANY N TOWARD ALBANY. USE THE RIGHT LANE TO MERGE ONTO I-87 N. TAKE EXIT 4 TOWARD CROSS COUNTRY PKWY E. MERGE ONTO CENTRAL PARK AVENUE. USE THE RIGHT LANE TO TAKE THE CROSS COUNTRY PKWY E RAMP. KEEP LEFT AND MERGE ONTO ROUTE 907K. CONTINUE ONTO HUTCHINSON RIVER PKWY N. CONTINUE ONTO CT-15 N. TAKE EXIT 55A FOR WHEELERS FARMS RD. TURN RIGHT ONTO WHEELER FARMS RD. TURN RIGHT ONTO E RUTLAND RD. TURN RIGHT ONTO LEXINGTON WAY. TURN RIGHT ONTO LOOKOUT HILL RD. TURN LEFT ONTO CHESTNUT LN. TURN LEFT ONTO ACORN LN. SITE WILL BE ON THE RIGHT.

ENGINEER
DEWBERRY ENGINEERS INC.
600 PARSSIPANY ROAD
SUITE 301
PARSSIPANY, NJ 07054
CONTACT: BRYAN HUFF
PHONE #: (973) 576-0147
CONSTRUCTION
CROWN CASTLE
3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065
CONTACT: PATRICIA PELON
PHONE #: (518) 373-3507
CONSULTANT TEAM

SITE NAME:
NHV 104 943122
SITE NUMBER:
CTNH009B
TOWER OWNER:
CROWN CASTLE
3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065
APPLICANT/DEVELOPER:
T-MOBILE NORTHEAST LLC
4 SYLVAN WAY
PARSSIPANY, NJ 07054
COORDINATES:
LATITUDE: 41°-14'-16.23" N (NAD83)
LONGITUDE: 73°-05'-10.0" W (NAD83)
(PER CROWN CASTLE)
CONFIGURATION
704Bu
PROJECT SUMMARY

SITE ADDRESS:
423 ORONOQUE ROAD
MILFORD, CT 06460
NEW HAVEN COUNTY
PROJECT DIRECTORY

- INSTALL (3) NEW ANTENNAS.
INSTALL (3) NEW BIAS TEES.
INSTALL (6) NEW LINES OF COAX ALONG MONOPOLE EXTERIOR.
INSTALL (3) NEW RRU'S ON A UNISTRUT RACK INSIDE EXISTING EQUIPMENT SHELTER AT GRADE.
INSTALL (1) NEW BBU CABINET INSIDE EXISTING EQUIPMENT SHELTER AT GRADE.
SCOPE OF WORK

THIS DOCUMENT WAS DEVELOPED TO REFLECT A SPECIFIC SITE AND ITS SITE CONDITIONS AND IS NOT TO BE USED FOR ANOTHER SITE OR WHEN OTHER CONDITIONS PERTAIN. REUSE OF THIS DOCUMENT IS AT THE SOLE RISK OF THE USER.
A.D.A. COMPLIANCE:
FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION.

Table with 2 columns: SHT. NO., DESCRIPTION. Rows include T-1 TITLE SHEET, G-1 GENERAL NOTES, C-1 COMPOUND PLAN & EQUIPMENT PLANS, C-2 ANTENNA LAYOUTS & ELEVATIONS, C-3 CONSTRUCTION DETAILS, E-1 GROUNDING NOTES & DETAILS.

SHEET INDEX







**CTNH009B**  
**NHV 104 943122**

**CONSTRUCTION DRAWINGS**

0 10/16/15 ISSUED AS FINAL  
A 10/07/15 ISSUED FOR REVIEW

Dewberry Engineers Inc.  
600 PARSIPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973.739.9400  
FAX: 973.739.9710



CONNECTICUT LICENSE NO. 0023222  
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER TO ALTER THIS DOCUMENT.

DRAWN BY:	RA
REVIEWED BY:	BSH
CHECKED BY:	GHN
PROJECT NUMBER:	50066258
JOB NUMBER:	50074607
SITE ADDRESS:	

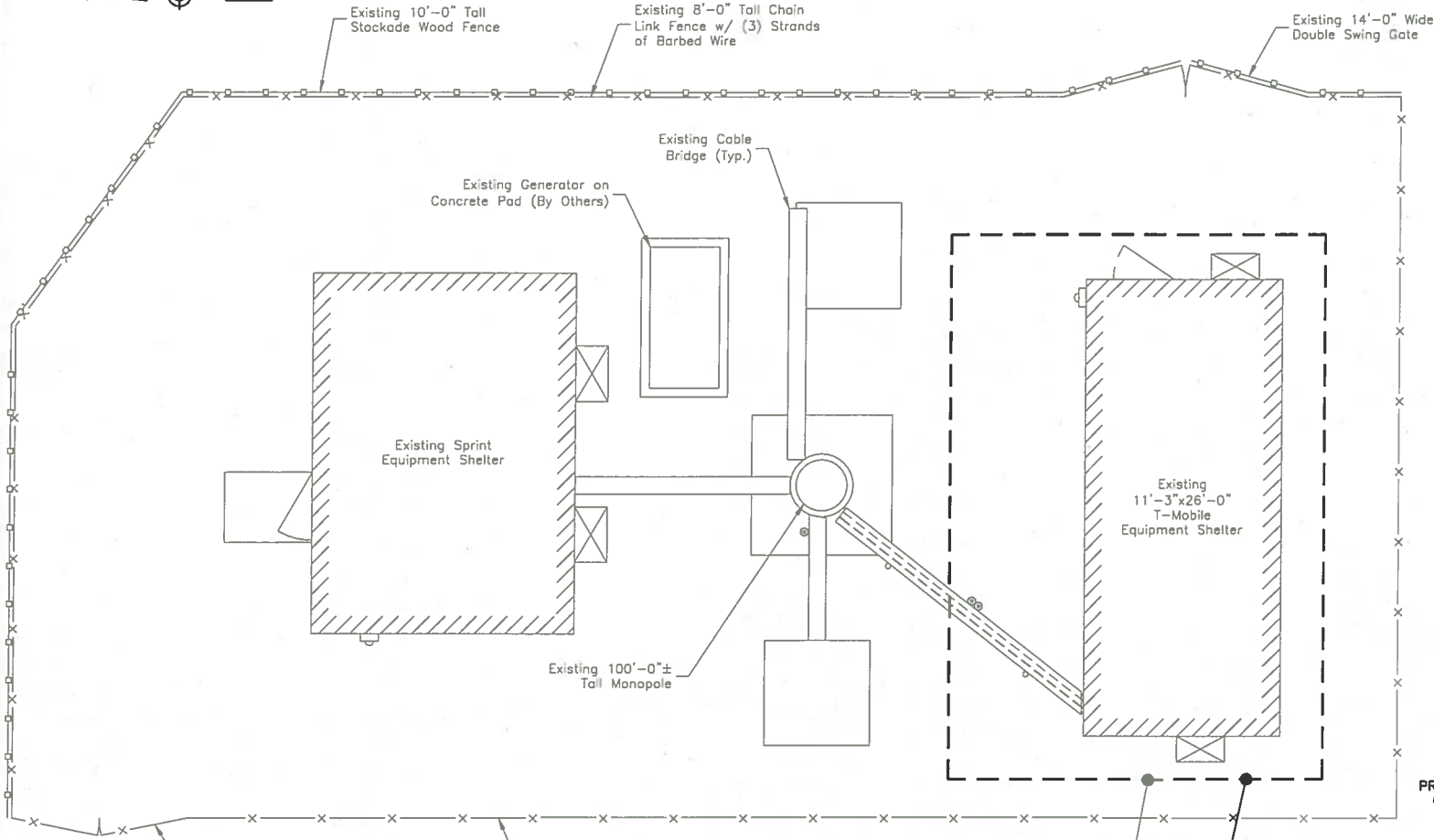
423 ORONOQUE ROAD  
MILFORD, CT 06460  
NEW HAVEN COUNTY

SHEET TITLE

COMPOUND PLAN &  
EQUIPMENT PLANS

SHEET NUMBER

APPROXIMATE TRUE NORTH



**COMPOUND PLAN**  
SCALE: 1"=10' FOR 11"x17"  
1"=5' FOR 22"x34"

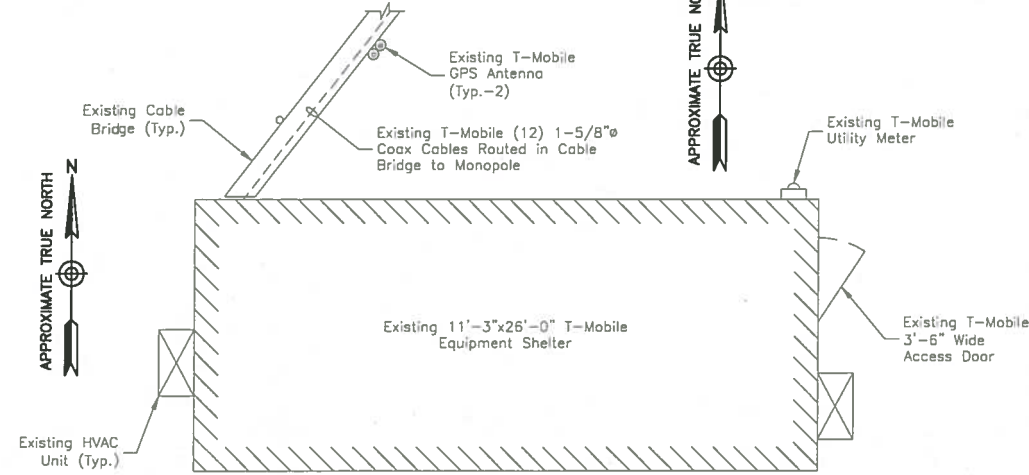


- NOTES:**
- NORTH ARROW SHOWN AS APPROXIMATE.
  - NOT ALL INFORMATION IS SHOWN FOR CLARITY.
  - ALL PROPOSED EQUIPMENT, INCLUDING ANTENNAS, BIAS TEES, COAX, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS BY AW SOLUTIONS DATED SEPTEMBER 18, 2015.

2 Existing T-Mobile Equipment in Equipment Shelter

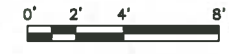
3 PROPOSED T-MOBILE EQUIPMENT IN EQUIPMENT SHELTER

APPROXIMATE TRUE NORTH



**EXISTING EQUIPMENT PLAN**

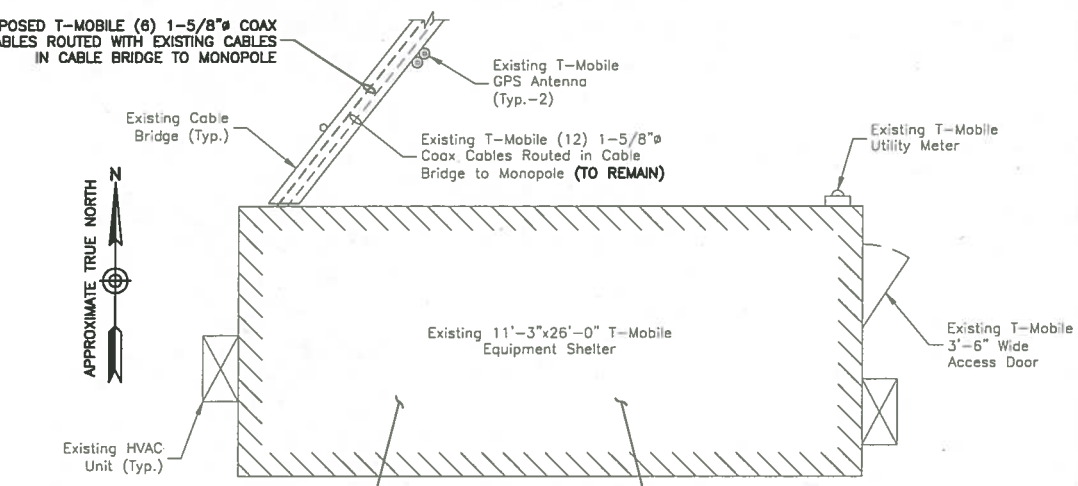
SCALE: 1/8"=1' FOR 11"x17"  
1/4"=1' FOR 22"x34"



- NOTE:**
- NO ACCESS WAS AVAILABLE TO EXISTING T-MOBILE SHELTER AT TIME OF SITE VISIT.

PROPOSED T-MOBILE (6) 1-5/8" COAX CABLES Routed WITH EXISTING CABLES IN CABLE BRIDGE TO MONOPOLE

APPROXIMATE TRUE NORTH



**PROPOSED EQUIPMENT PLAN**

SCALE: 1/8"=1' FOR 11"x17"  
1/4"=1' FOR 22"x34"



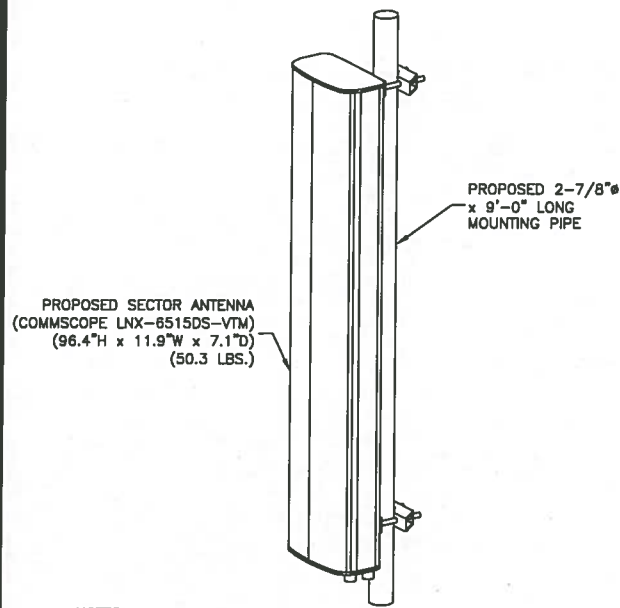
- NOTES:**
- NO ACCESS WAS AVAILABLE TO EXISTING T-MOBILE SHELTER AT TIME OF SITE VISIT.
  - PROPOSED EQUIPMENT TO BE FIELD LOCATED BY T-MOBILE CONSTRUCTION MANAGER.

5 PROPOSED T-MOBILE BBU CABINET INSIDE EXISTING EQUIPMENT SHELTER (LOCATION TO BE FIELD VERIFIED)

PROPOSED T-MOBILE (3) RRU'S ON PROPOSED EQUIPMENT RACK INSIDE EXISTING EQUIPMENT SHELTER (LOCATION TO BE FIELD VERIFIED)

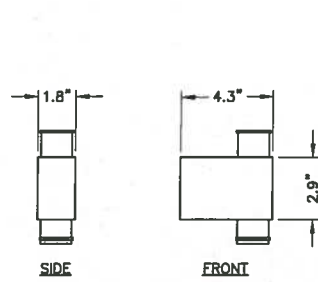






- NOTES:**
1. MOUNT ANTENNAS PER MANUFACTURER'S RECOMMENDATIONS.
  2. GROUND ANTENNAS AND MOUNTS PER MANUFACTURER'S RECOMMENDATIONS AND T-MOBILE STANDARDS.
  3. CONFIRM REQUIRED ANTENNAS WITH THE LATEST RFDS.

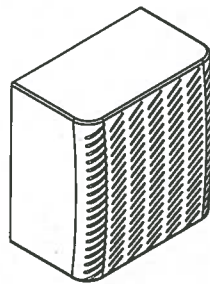
**ISOMETRIC ANTENNA DETAIL**  
SCALE: N.T.S.



ANDREW ATBT-BOTTOM-24V

- NOTES:**
1. MOUNT EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.
  2. GROUND EQUIPMENT AND MOUNTS PER MANUFACTURER'S RECOMMENDATIONS AND T-MOBILE STANDARDS.
  3. CONFIRM REQUIRED EQUIPMENT WITH THE LATEST RFDS.

**BIAS TEE DETAIL**  
SCALE: N.T.S.

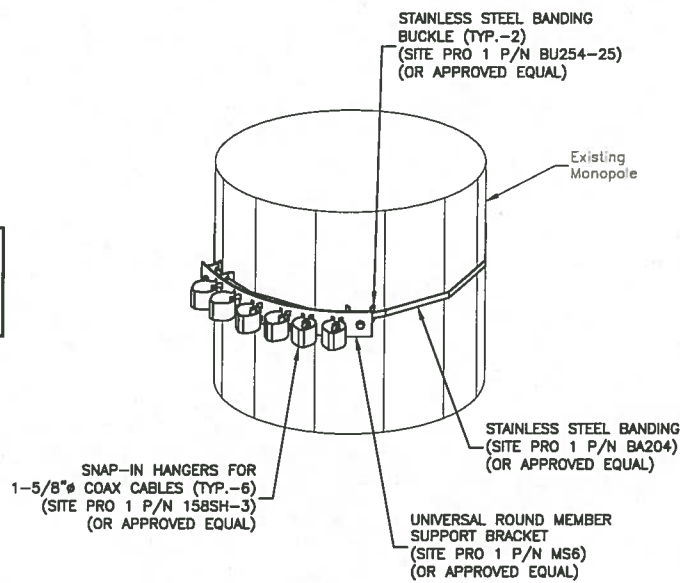


**SPECIFICATIONS:**  
HEIGHT: 20.0"  
WIDTH: 17.0"  
DEPTH: 7.0"  
WEIGHT: 50.7 LBS

ERICSSON RRUS-11 B12

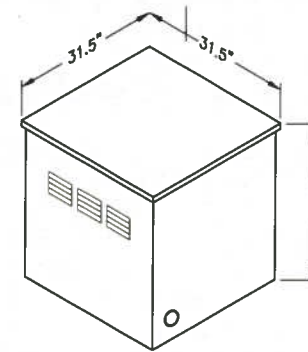
- RRU NOTES:**
1. MOUNT EQUIPMENT WITH MANUFACTURER PROVIDED MOUNTING BRACKETS.
  2. GROUND EQUIPMENT AND MOUNTS PER MANUFACTURER'S RECOMMENDATIONS AND T-MOBILE STANDARDS.
  3. CONFIRM REQUIRED EQUIPMENT WITH THE LATEST RFDS.

**RRUS-11 - REMOTE RADIO UNIT**  
SCALE: N.T.S.



- NOTES:**
1. SUPPORT BRACKETS SHALL BE SPACED AT 4'-0" C-C MAX.
  2. COAX CABLES SHALL BE INSTALLED NEXT TO VERIZON WIRELESS CABLES ON MONOPOLE EXTERIOR.

**COAX SUPPORT DETAIL**  
SCALE: N.T.S.

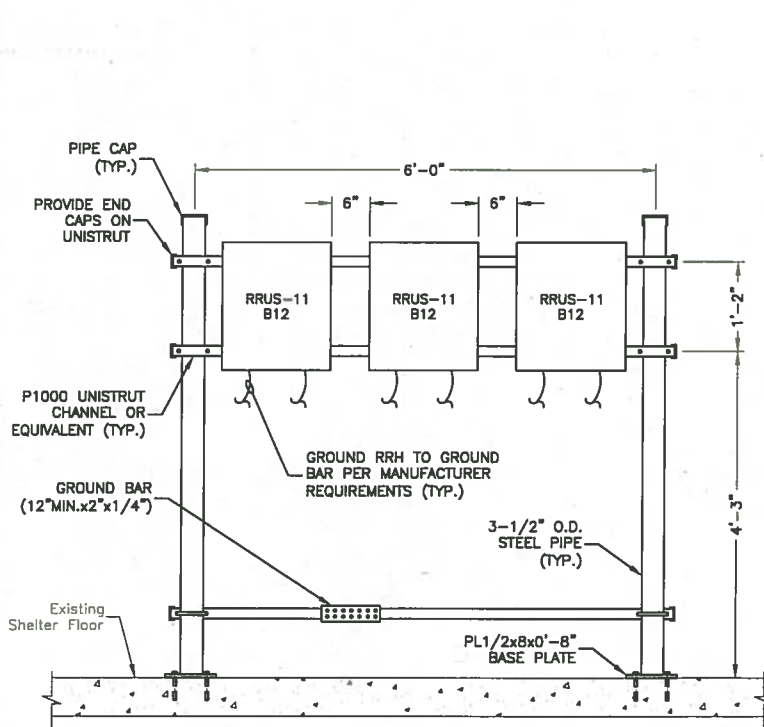


ALCATEL-LUCENT EZBFC BATTERY BACKUP SYSTEM

MATERIAL:	ANCHOR:
CONCRETE	3/8" HILTI KWIK BOLT 3 W/2-1/2" MIN. EMBED.
STRUCTURAL STEEL	1/2" STRUCTURAL BOLTS

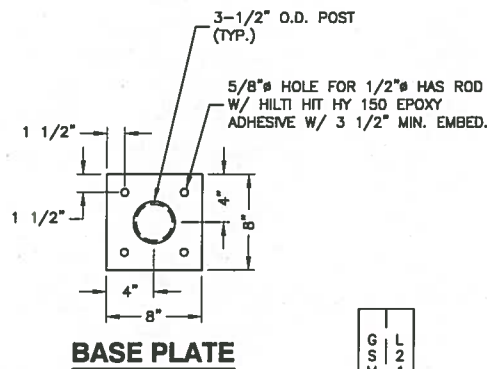
- NOTE:**
1. CONTRACTOR SHALL ANCHOR CABINET IN ACCORDANCE WITH MANUFACTURER RECOMMENDATIONS.

**BBU CABINET DETAIL**  
SCALE: N.T.S.

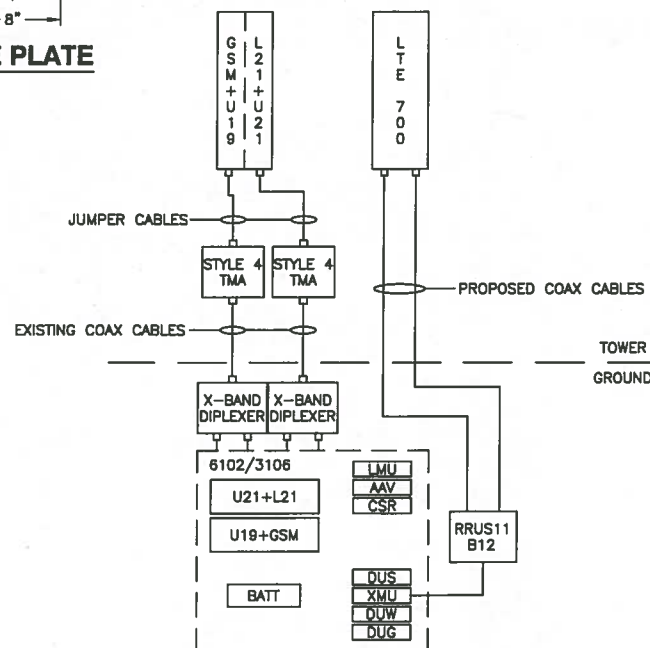


- NOTES:**
1. CONTRACTOR SHALL SUPPLY AND INSTALL UNISTRUT (OR EQUIVALENT) MOUNTING CHANNELS.
  2. CONTRACTOR SHALL SUPPLY (BUT NOT INSTALL) 3/8" UNISTRUT BOLTING HARDWARE AND SPRING NUTS. TYPICAL FOUR PER RRU. CONTRACTOR SHALL BAG THE BOLTING HARDWARE AND HANG FROM INSTALLED UNISTRUT FRAME.
  3. SPACING MAY VARY BASED ON SELECTED EQUIPMENT. ADJUSTMENTS TO SPACING WILL BE MADE BY RRU INSTALLER.
  4. NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

**RRU RACK DETAIL**  
SCALE: N.T.S.



**BASE PLATE**



**SITE CONFIGURATION 704Bu**  
SCALE: N.T.S.

DESIGN CONFIGURATION					
	ANTENNAS		COAX		COAX LENGTH
	EXISTING	PROPOSED	EXISTING	PROPOSED	
ALPHA	APX16DWV-16DWVS-E-A20	EXISTING TO REMAIN	(4) 1-5/8"	(2) 1-5/8"	133'-0"
BETA	APX16DWV-16DWVS-E-A20	EXISTING TO REMAIN	(4) 1-5/8"	(2) 1-5/8"	133'-0"
GAMMA	APX16DWV-16DWVS-E-A20	EXISTING TO REMAIN	(4) 1-5/8"	(2) 1-5/8"	133'-0"

**T-Mobile**

T-MOBILE NORTHEAST LLC  
4 SYLVAN WAY  
PARSIPPANY, NJ 07054

**CROWN CASTLE**

CROWN CASTLE  
3 CORPORATE PARK DRIVE, SUITE 101  
CLIFTON PARK, NY 12065

**CTNH009B**  
**NHV 104 943122**

CONSTRUCTION DRAWINGS

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A 10/07/15 ISSUED FOR REVIEW

**Dewberry**

Dewberry Engineers Inc.  
600 PARSIPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973.739.9400  
FAX: 973.739.9710



DRAWN BY: RA

REVIEWED BY: BSH

CHECKED BY: GHN

PROJECT NUMBER: 50066258

JOB NUMBER: 50074607

SITE ADDRESS:

423 ORONOQUE ROAD  
MILFORD, CT 06460  
NEW HAVEN COUNTY

SHEET TITLE

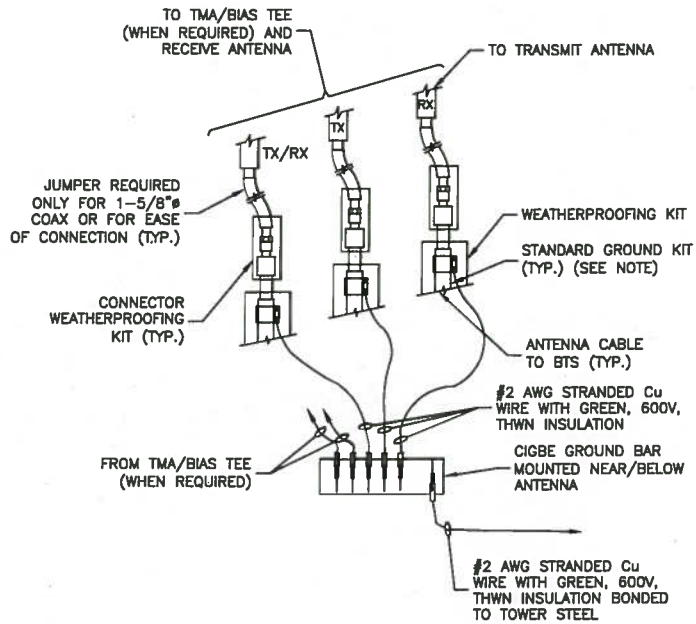
CONSTRUCTION  
DETAILS

SHEET NUMBER

C-3

**GROUNDING NOTES:**

- THE CONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE CONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE ENGINEER FOR RESOLUTION.
- ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS. ALL AVAILABLE GROUNDING ELECTRODES SHALL BE CONNECTED TOGETHER IN ACCORDANCE WITH THE NEC.
- THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS. USE OF OTHER METHODS MUST BE PRE-APPROVED BY THE ENGINEER IN WRITING.
- THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS ON TOWER SITES AND 10 OHMS OR LESS ON ROOFTOP SITES. WHEN ADDING ELECTRODES, CONTRACTOR SHALL MAINTAIN A MINIMUM DISTANCE BETWEEN THE ADDED ELECTRODE AND ANY OTHER EXISTING ELECTRODE EQUAL TO THE BURIED LENGTH OF THE ROD. IDEALLY, CONTRACTOR SHALL STRIVE TO KEEP THE SEPARATION DISTANCE EQUAL TO TWICE THE BURIED LENGTH OF THE RODS.
- THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT.
- METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWG COPPER WIRE AND UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO TRANSMISSION EQUIPMENT.
- CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED. BACK-TO-BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
- ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED. IN ALL CASES, BENDS SHALL BE MADE WITH A MINIMUM BEND RADIUS OF 8 INCHES.
- EACH INTERIOR TRANSMISSION CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH 6 AWG STRANDED, GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRE UNLESS NOTED OTHERWISE IN THE DETAILS. EACH OUTDOOR CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER WIRE UNLESS NOTED OTHERWISE IN THE DETAILS.
- ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING, SHALL BE 2 AWG SOLID TIN-PLATED COPPER UNLESS OTHERWISE INDICATED.
- EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE. CONNECTIONS TO ABOVE GRADE UNITS SHALL BE MADE WITH EXOTHERMIC WELDS WHERE PRACTICAL OR WITH 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS. HIGH PRESSURE CRIMP CONNECTORS MAY ONLY BE USED WITH WRITTEN PERMISSION FROM T-MOBILE MARKET REPRESENTATIVE.
- EXOTHERMIC WELDS SHALL BE PERMITTED ON TOWERS ONLY WITH THE EXPRESS APPROVAL OF THE TOWER MANUFACTURER OR THE CONTRACTOR'S STRUCTURAL ENGINEER.
- ALL WIRE TO WIRE GROUND CONNECTIONS TO THE INTERIOR GROUND RING SHALL BE FORMED USING HIGH PRESS CRIMPS OR SPLIT BOLT CONNECTORS WHERE INDICATED IN THE DETAILS.
- ON ROOFTOP SITES WHERE EXOTHERMIC WELDS ARE A FIRE HAZARD COPPER COMPRESSION CAP CONNECTORS MAY BE USED FOR WIRE TO WIRE CONNECTORS. 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS SHALL BE USED FOR CONNECTION TO ALL ROOFTOP TRANSMISSION EQUIPMENT AND STRUCTURAL STEEL.
- COAX BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR USING TWO-HOLE MECHANICAL TYPE BRASS CONNECTORS AND STAINLESS STEEL HARDWARE.
- APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
- MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- BOND ALL METALLIC OBJECTS WITHIN 6 FT OF THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER GROUND CONDUCTOR. DURING EXCAVATION FOR NEW GROUND CONDUCTORS, IF EXISTING GROUND CONDUCTORS ARE ENCOUNTERED, BOND EXISTING GROUND CONDUCTORS TO NEW CONDUCTORS.
- GROUND CONDUCTORS USED IN THE FACILITY GROUND AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC PLASTIC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (E.G., NON-METALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT WITH LISTED BONDING FITTINGS.



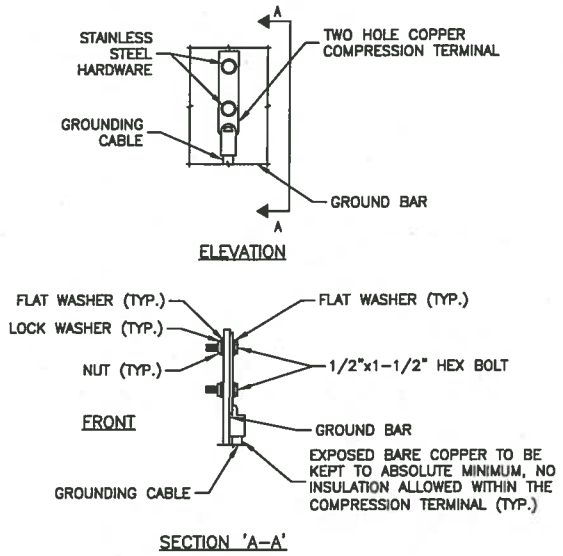
**NOTE:**

- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

**CONNECTION OF GROUND WIRES TO GROUNDING BAR (CIGBE)**

SCALE: N.T.S.

1



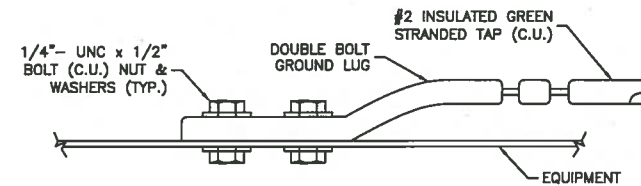
**NOTES:**

- DOUBLING UP OR STACKING OF CONNECTIONS IS NOT PERMITTED.
- OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

**TYPICAL GROUND BAR MECHANICAL CONNECTION DETAIL**

SCALE: N.T.S.

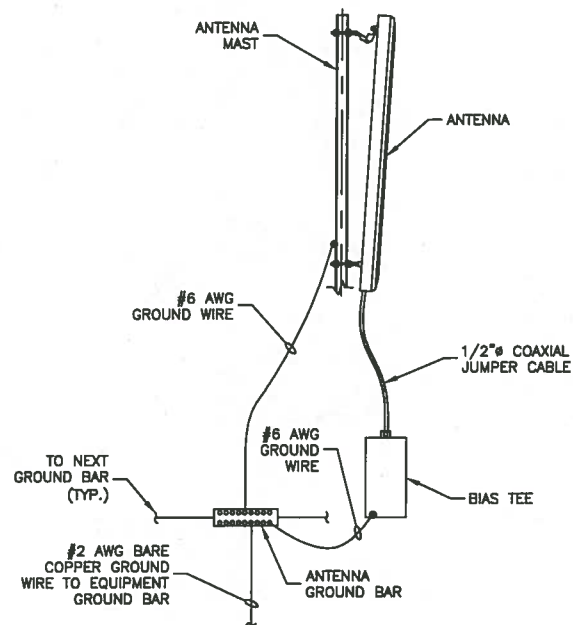
2



**CONNECTION TO EQUIPMENT DETAIL**

SCALE: N.T.S.

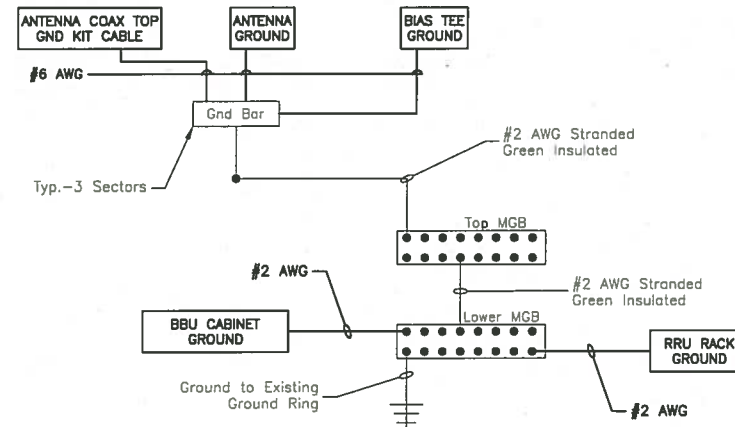
3



**TYPICAL ANTENNA GROUNDING DETAIL**

SCALE: N.T.S.

4



**NOTES:**

- BOND ANTENNA GROUNDING KIT CABLE TO TOP CIGBE
- BOND ANTENNA GROUNDING KIT CABLE TO BOTTOM CIGBE.
- SCHEMATIC GROUNDING DIAGRAM IS TYPICAL FOR EACH SECTOR.
- VERIFY EXISTING GROUND SYSTEM IS INSTALLED PER T-MOBILE STANDARDS.

**SCHEMATIC GROUNDING DIAGRAM**

SCALE: N.T.S.

5

**T-Mobile**

T-MOBILE NORTHEAST LLC  
4 SYLVAN WAY  
PARSIPPANY, NJ 07054

**CROWN CASTLE**

CROWN CASTLE  
3 CORPORATE PARK DRIVE, SUITE 101  
CLIFTON PARK, NY 12065

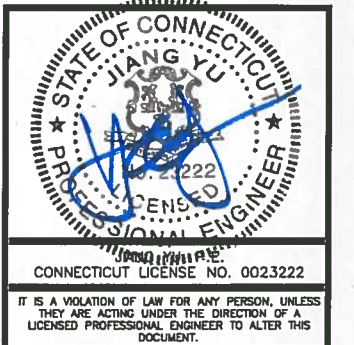
**CTNH009B  
NHV 104 943122**

**CONSTRUCTION DRAWINGS**

NO.	DATE	ISSUED FOR
0	10/16/15	ISSUED AS FINAL
A	10/07/15	ISSUED FOR REVIEW

**Dewberry**

Dewberry Engineers Inc.  
800 PARSIPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973.739.8400  
FAX: 973.739.8710



DRAWN BY: RA

REVIEWED BY: BSH

CHECKED BY: GHN

PROJECT NUMBER: 50066258

JOB NUMBER: 50074807

SITE ADDRESS:

423 ORONOQUE ROAD  
MILFORD, CT 06460  
NEW HAVEN COUNTY

SHEET TITLE

GROUNDING NOTES & DETAILS

SHEET NUMBER





Date: **September 18, 2015**

Cheryl Schultz  
Crown Castle  
3530 Toringdon Way Suite 300  
Charlotte, NC 28277

AW Solutions  
300 Crown Oak Centre Dr  
Longwood, FL 32750  
(407) 260-0231

**Subject: Structural Analysis Report**

**Carrier Designation:** **T-Mobile Co-Locate**  
**Carrier Site Number:** CTNH009B  
**Carrier Site Name:** NH009/CrownOronoque\_ET

**Crown Castle Designation:** **Crown Castle BU Number:** 806359  
**Crown Castle Site Name:** NHV 104 943122  
**Crown Castle JDE Job Number:** 346200  
**Crown Castle Work Order Number:** 1122514  
**Crown Castle Application Number:** 310127 Rev. 4

**Engineering Firm Designation:** **AW Solutions Project Number:** 806359

**Site Data:** **423 ORONOQUE ROAD, MILFORD, New Haven County, CT**  
**Latitude 41° 14' 16.23", Longitude -73° 5' 10"**  
**100 Foot - Monopole Tower**

Dear Cheryl Schultz,

AW Solutions is pleased to submit this “**Structural Analysis Report**” to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural ‘Statement of Work’ and the terms of Crown Castle Purchase Order Number 827331, in accordance with application 310127, revision 4.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC5: Installed + Proposed Equipment **Sufficient Capacity**  
Note: See Table I and Table II for the proposed and existing loading, respectively.

The analysis has been performed in accordance with the TIA/EIA-222-F standard and 2005 CT State Building Code with 2009 amendment based upon a wind speed of 90 mph fastest mile.

We at AW Solutions appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared by: Joseph Jimenez, EI / JFB

Respectfully submitted by:



Alan Lockrem, PE  
Director of Engineering

09/18/15

## TABLE OF CONTENTS

### 1) INTRODUCTION

### 2) ANALYSIS CRITERIA

Table 1 - Proposed Antenna and Cable Information

Table 2 - Existing and Reserved Antenna and Cable Information

Table 3 - Design Antenna and Cable Information

### 3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

3.1) Analysis Method

3.2) Assumptions

### 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Table 6 – Tower Components vs. Capacity

4.1) Recommendations

### 5) APPENDIX A

tnxTower Output

### 6) APPENDIX B

Base Level Drawing

### 7) APPENDIX C

Additional Calculations



## 1) INTRODUCTION

This tower is a 100 ft Monopole tower designed by VALMONT in August of 1986. The tower was originally designed for an unknown wind speed per EIA-222-C. The tower was modified per reinforcement drawings by Paul J Ford and Company, dated April 2009.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 90 mph with no ice, 37.6 mph with 0.75 inch ice thickness and 50 mph under service loads.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
83.0	83.0	3	commscope	ATBT-BOTTOM-24V	6	1-5/8	-
		3	commscope	LNx-6515DS-VTM w/ Mount Pipe			
		3	ericsson	KRY 112 144/1			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
100.0	105.0	3	alcatel lucent	RRH2x40-AWS	14 1 1	7/8 1/2 1-5/8	1
		3	antel	BXA-171063-8BF-EDIN-0 w/ Mount Pipe			
		5	decibel	DB846F65ZAXY w/ Mount Pipe			
		1	rfs	DB-T1-6Z-8AB-0Z			
		5	rfs celwave	FD9R6004/2C-3L			
	102.0	3	antel	BXA-171063-8BF-EDIN-2 w/ Mount Pipe			
		1	decibel	DB846F65ZAXY w/ Mount Pipe			
		1	gps	GPS_A			
		1	rfs celwave	FD9R6004/2C-3L			
	100.0	3	swedcom	SWCP 2x5514 w/ Mount Pipe			
100.0	1	tower mounts	Platform Mount [LP 602-1]				
95.0	95.0	1	til-tek	TA-2335-DAB-L-095	1	7/8	1
		1	tower mounts	Pipe Mount [PM 602-1]			
83.0	83.0	3	ericsson	KRY 112 144/1	12	1-5/8	1
		3	rfs celwave	APX16DWV-16DWVS-E-A20 w/ Mount Pipe			
		1	tower mounts	Platform Mount [LP 602-1]			
73.0	73.0	3	rfs celwave	APXV18-206517S-C	6	1-5/8	1
		1	tower mounts	Pipe Mount [PM 602-3]			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
50.0	50.0	1	til-tek	TA-2324-LHCP	1	1/2	1
		1	tower mounts	Side Arm Mount [SO 102-3]			
45.0	45.0	1	prodelin	1111	2	19/64	1
		1	tower mounts	Side Arm Mount [SO 102-3]			
		1	trimble	57860-30			

Notes:  
 1) Existing Equipment

**Table 3 - Design Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
-						

### 3) ANALYSIS PROCEDURE

**Table 4 - Documents Provided**

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH	1256016	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	FPL Construction	1256012	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Valmont	1245431	CCISITES
4-POST-MODIFICATION INSPECTION	Paul J Ford and Company	2419763	CCISITES

#### 3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) When applicable, transmission cables are considered as structural components for calculating wind loads as allowed by TIA/EIA-222-F.

This analysis may be affected if any assumptions are not valid or have been made in error. AW Solutions should be notified to determine the effect on the structural integrity of the tower.



#### 4) ANALYSIS RESULTS

**Table 5 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	100 - 46.8333	Pole	TP33.26x23.43x0.313	1	-9.238	1673.581	57.7	Pass
L2	46.8333 - 0	Pole	TP41.3x31.68x0.375	2	-19.595	2569.037	81.0	Pass
							Summary	
						Pole (L2)	81.0	Pass
						<b>RATING =</b>	<b>81.0</b>	<b>Pass</b>

**Table 6 - Tower Component Stresses vs. Capacity - LC5**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	77.1	Pass
1	Base Plate	0	46.5	Pass
1	Base Foundation Structural	0	38.6	Pass
1	Base Foundation Soil Interaction	0	41.1	Pass

<b>Structure Rating (max from all components) =</b>	<b>81.0%</b>
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Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

#### 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the existing and proposed loads. No modifications are required at this time.

**APPENDIX A**  
**TNXTOWER OUTPUT**





## Tower Input Data

There is a pole section.  
 This tower is designed using the TIA/EIA-222-F standard.  
 The following design criteria apply:

- 1) Tower is located in New Haven County, Connecticut.
- 2) Basic wind speed of 90 mph.
- 3) Nominal ice thickness of 0.750 in.
- 4) Ice density of 56.000 pcf.
- 5) A wind speed of 38 mph is used in combination with ice.
- 6) Temperature drop of 50.000 °F.
- 7) Deflections calculated using a wind speed of 50 mph.
- 8) A non-linear (P-delta) analysis was used.
- 9) Pressures are calculated at each section.
- 10) Stress ratio used in pole design is 1.333.
- 11) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification ✓ Use Code Stress Ratios ✓ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination	Distribute Leg Loads As Uniform Assume Legs Pinned ✓ Assume Rigid Index Plate ✓ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension ✓ Bypass Mast Stability Checks ✓ Use Azimuth Dish Coefficients ✓ Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption	Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation ✓ Consider Feedline Torque Include Angle Block Shear Check <div style="text-align: center; background-color: #e0e0e0; padding: 2px;">Poles</div> ✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets
--	--	--

## Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	100.000- 46.833	53.167	5.167	12	23.430	33.260	0.313	1.250	A572-65 (65 ksi)
L2	46.833-0.000	52.000		12	31.680	41.300	0.375	1.500	A572-65 (65 ksi)

## Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	It/Q in <sup>2</sup>	w in	w/t
L1	24.257	23.262	1586.772	8.276	12.137	130.741	3215.230	11.449	5.442	17.414
	34.433	33.153	4593.664	11.795	17.229	266.629	9308.009	16.317	8.076	25.844
L2	33.787	37.800	4728.280	11.207	16.410	288.132	9580.776	18.604	7.485	19.96
	42.757	49.417	10564.262	14.651	21.393	493.809	21406.058	24.322	10.063	26.836

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_r$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
ft	ft <sup>2</sup>	in						
L1 100.000-46.833				1	1	1		
L2 46.833-0.000				1	1	1		

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		$C_{AA}$ ft <sup>2</sup> /ft	Weight plf
LDF4-50A(1/2")	B	No	Inside Pole	100.000 - 8.000	1	No Ice	0.000	0.150
						1/2" Ice	0.000	0.150
						1" Ice	0.000	0.150
LDF5-50A(7/8)	B	No	Inside Pole	100.000 - 8.000	14	No Ice	0.000	0.330
						1/2" Ice	0.000	0.330
						1" Ice	0.000	0.330
HB158-1-08U8-S8J18(1-5/8)	B	No	Inside Pole	100.000 - 8.000	1	No Ice	0.000	1.300
						1/2" Ice	0.000	1.300
						1" Ice	0.000	1.300
AVA5-50( 7/8")	B	No	Inside Pole	95.000 - 8.000	1	No Ice	0.000	0.300
						1/2" Ice	0.000	0.300
						1" Ice	0.000	0.300
LDF7-50A(1-5/8")	C	No	Inside Pole	83.000 - 8.000	12	No Ice	0.000	0.820
						1/2" Ice	0.000	0.820
						1" Ice	0.000	0.820
CR 50 1873(1-5/8")	A	No	CaAa (Out Of Face)	83.000 - 73.000	5	No Ice	0.000	0.830
						1/2" Ice	0.000	2.345
						1" Ice	0.000	4.471
CR 50 1873(1-5/8")	A	No	CaAa (Out Of Face)	73.000 - 8.000	11	No Ice	0.000	0.830
						1/2" Ice	0.000	2.345
						1" Ice	0.000	4.471
CR 50 1873(1-5/8")	A	No	CaAa (Out Of Face)	83.000 - 8.000	1	No Ice	0.198	0.830
						1/2" Ice	0.298	2.345
						1" Ice	0.398	4.471
LDF4-50A(1/2")	B	No	Inside Pole	50.000 - 0.000	1	No Ice	0.000	0.150
						1/2" Ice	0.000	0.150
						1" Ice	0.000	0.150
7916A(19/64)	B	No	Inside Pole	45.000 - 0.000	2	No Ice	0.000	0.033
						1/2" Ice	0.000	0.033
						1" Ice	0.000	0.033
***								
Safety Line 3/8	C	No	CaAa (Out Of Face)	100.000 - 10.000	1	No Ice	0.037	0.220
						1/2" Ice	0.137	0.750
						1" Ice	0.238	1.280

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
L1	100.000-46.833	A	0.000	0.000	0.000	7.161	0.310
		B	0.000	0.000	0.000	0.000	0.338
		C	0.000	0.000	0.000	1.994	0.368
L2	46.833-0.000	A	0.000	0.000	0.000	7.689	0.387
		B	0.000	0.000	0.000	0.000	0.257
		C	0.000	0.000	0.000	1.381	0.390

### Feed Line/Linear Appurtenances Section Areas - With Ice



Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	100.000-46.833	A	0.750	0.000	0.000	0.000	12.586	1.275
		B		0.000	0.000	0.000	0.000	0.338
		C		0.000	0.000	0.000	9.969	0.410
L2	46.833-0.000	A	0.750	0.000	0.000	0.000	13.514	1.588
		B		0.000	0.000	0.000	0.000	0.257
		C		0.000	0.000	0.000	6.906	0.420

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
L1	100.000-46.833	-0.045	-0.173	-0.198	-0.190
L2	46.833-0.000	-0.035	-0.207	-0.158	-0.268

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K	
SWCP 2x5514 w/ Mount Pipe	A	From Leg	4.000	0.000	100.000	No Ice	7.251	6.966	0.039
			0.000			1/2"	7.751	7.746	0.104
			2.000			Ice	8.252	8.499	0.174
SWCP 2x5514 w/ Mount Pipe	B	From Leg	4.000	0.000	100.000	No Ice	7.251	6.966	0.039
			0.000			1/2"	7.751	7.746	0.104
			2.000			Ice	8.252	8.499	0.174
SWCP 2x5514 w/ Mount Pipe	C	From Leg	4.000	0.000	100.000	No Ice	7.251	6.966	0.039
			0.000			1/2"	7.751	7.746	0.104
			2.000			Ice	8.252	8.499	0.174
(2) DB846F65ZAXY w/ Mount Pipe	A	From Leg	4.000	0.000	100.000	No Ice	7.271	7.821	0.047
			0.000			1/2"	7.877	9.010	0.114
			5.000			Ice	8.484	9.912	0.189
(2) DB846F65ZAXY w/ Mount Pipe	B	From Leg	4.000	0.000	100.000	No Ice	7.271	7.821	0.047
			0.000			1/2"	7.877	9.010	0.114
			5.000			Ice	8.484	9.912	0.189
DB846F65ZAXY w/ Mount Pipe	C	From Leg	4.000	0.000	100.000	No Ice	7.271	7.821	0.047
			0.000			1/2"	7.877	9.010	0.114
			5.000			Ice	8.484	9.912	0.189
DB846F65ZAXY w/ Mount Pipe	C	From Leg	4.000	0.000	100.000	No Ice	7.271	7.821	0.047
			0.000			1/2"	7.877	9.010	0.114
			2.000			Ice	8.484	9.912	0.189
BXA-171063-8BF-EDIN-0 w/ Mount Pipe	A	From Leg	4.000	0.000	100.000	No Ice	3.179	3.353	0.029
			0.000			1/2"	3.555	3.971	0.061
			5.000			Ice	3.964	4.595	0.099
BXA-171063-8BF-EDIN-0 w/ Mount Pipe	B	From Leg	4.000	0.000	100.000	No Ice	3.179	3.353	0.029
			0.000			1/2"	3.555	3.971	0.061
			5.000			Ice	3.964	4.595	0.099
						1" Ice			

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
BXA-171063-8BF-EDIN-0 w/ Mount Pipe	C	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	3.179	3.353	0.029
						1/2"	3.555	3.971	0.061
						Ice	3.964	4.595	0.099
						1" Ice			
BXA-171063-8BF-EDIN-2 w/ Mount Pipe	A	From Leg	4.000 0.000 2.000	0.000	100.000	No Ice	3.179	3.353	0.029
						1/2"	3.555	3.971	0.061
						Ice	3.964	4.595	0.099
						1" Ice			
BXA-171063-8BF-EDIN-2 w/ Mount Pipe	B	From Leg	4.000 0.000 2.000	0.000	100.000	No Ice	3.179	3.353	0.029
						1/2"	3.555	3.971	0.061
						Ice	3.964	4.595	0.099
						1" Ice			
BXA-171063-8BF-EDIN-2 w/ Mount Pipe	C	From Leg	4.000 0.000 2.000	0.000	100.000	No Ice	3.179	3.353	0.029
						1/2"	3.555	3.971	0.061
						Ice	3.964	4.595	0.099
						1" Ice			
(2) FD9R6004/2C-3L	A	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	0.367	0.085	0.003
						1/2"	0.451	0.136	0.005
						Ice	0.543	0.196	0.009
						1" Ice			
(2) FD9R6004/2C-3L	B	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	0.367	0.085	0.003
						1/2"	0.451	0.136	0.005
						Ice	0.543	0.196	0.009
						1" Ice			
FD9R6004/2C-3L	C	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	0.367	0.085	0.003
						1/2"	0.451	0.136	0.005
						Ice	0.543	0.196	0.009
						1" Ice			
FD9R6004/2C-3L	C	From Leg	4.000 0.000 2.000	0.000	100.000	No Ice	0.367	0.085	0.003
						1/2"	0.451	0.136	0.005
						Ice	0.543	0.196	0.009
						1" Ice			
RRH2x40-AWS	A	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	2.522	1.589	0.044
						1/2"	2.753	1.795	0.061
						Ice	2.993	2.010	0.082
						1" Ice			
RRH2x40-AWS	B	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	2.522	1.589	0.044
						1/2"	2.753	1.795	0.061
						Ice	2.993	2.010	0.082
						1" Ice			
RRH2x40-AWS	C	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	2.522	1.589	0.044
						1/2"	2.753	1.795	0.061
						Ice	2.993	2.010	0.082
						1" Ice			
GPS_A	C	From Leg	4.000 0.000 2.000	0.000	100.000	No Ice	0.297	0.297	0.001
						1/2"	0.374	0.374	0.005
						Ice	0.459	0.459	0.010
						1" Ice			
DB-T1-6Z-8AB-0Z	A	From Leg	4.000 0.000 5.000	0.000	100.000	No Ice	5.600	2.333	0.044
						1/2"	5.915	2.558	0.080
						Ice	6.240	2.791	0.120
						1" Ice			
Platform Mount [LP 602-1]	C	None		0.000	100.000	No Ice	32.030	32.030	1.343
						1/2"	38.710	38.710	1.800
						Ice	45.390	45.390	2.257
						1" Ice			
*95* TA-2335-DAB-L-095	B	From Leg	1.000 0.000 0.000	0.000	95.000	No Ice	7.758	2.956	0.033
						1/2"	8.145	3.258	0.076
						Ice	8.540	3.569	0.124
						1" Ice			
Pipe Mount [PM 602-1]	B	From Leg	1.000 0.000 0.000	0.000	95.000	No Ice	5.250	1.580	0.093
						1/2"	6.500	1.950	0.118
						Ice	7.750	2.320	0.142
						1" Ice			

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
*83*									
APX16DWV-16DWVS-E-A20 w/ Mount Pipe	A	From Leg	4.000	0.000	83.000	No Ice	7.808	3.782	0.064
			0.000			1/2"	8.368	4.643	0.115
			0.000			Ice	8.915	5.382	0.173
APX16DWV-16DWVS-E-A20 w/ Mount Pipe	B	From Leg	4.000	0.000	83.000	No Ice	7.808	3.782	0.064
			0.000			1/2"	8.368	4.643	0.115
			0.000			Ice	8.915	5.382	0.173
APX16DWV-16DWVS-E-A20 w/ Mount Pipe	C	From Leg	4.000	0.000	83.000	No Ice	7.808	3.782	0.064
			0.000			1/2"	8.368	4.643	0.115
			0.000			Ice	8.915	5.382	0.173
KRY 112 144/1	A	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
KRY 112 144/1	B	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
KRY 112 144/1	C	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
KRY 112 144/1	A	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
KRY 112 144/1	B	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
KRY 112 144/1	C	From Leg	4.000	0.000	83.000	No Ice	0.408	0.204	0.011
			0.000			1/2"	0.497	0.273	0.014
			0.000			Ice	0.594	0.351	0.019
LNx-6515DS-VTM w/ Mount Pipe	A	From Leg	4.000	0.000	83.000	No Ice	11.683	9.842	0.083
			0.000			1/2"	12.404	11.366	0.173
			0.000			Ice	13.135	12.914	0.273
LNx-6515DS-VTM w/ Mount Pipe	B	From Leg	4.000	0.000	83.000	No Ice	11.683	9.842	0.083
			0.000			1/2"	12.404	11.366	0.173
			0.000			Ice	13.135	12.914	0.273
LNx-6515DS-VTM w/ Mount Pipe	C	From Leg	4.000	0.000	83.000	No Ice	11.683	9.842	0.083
			0.000			1/2"	12.404	11.366	0.173
			0.000			Ice	13.135	12.914	0.273
ATBT-BOTTOM-24V	A	From Leg	4.000	0.000	83.000	No Ice	0.121	0.075	0.003
			0.000			1/2"	0.172	0.119	0.004
			0.000			Ice	0.232	0.172	0.006
ATBT-BOTTOM-24V	B	From Leg	4.000	0.000	83.000	No Ice	0.121	0.075	0.003
			0.000			1/2"	0.172	0.119	0.004
			0.000			Ice	0.232	0.172	0.006
ATBT-BOTTOM-24V	C	From Leg	4.000	0.000	83.000	No Ice	0.121	0.075	0.003
			0.000			1/2"	0.172	0.119	0.004
			0.000			Ice	0.232	0.172	0.006
Platform Mount [LP 602-1]	C	None		0.000	83.000	No Ice	32.030	32.030	1.343
						1/2"	38.710	38.710	1.800
						Ice	45.390	45.390	2.257
						1" Ice			



Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
<b>*73*</b>									
APXV18-206517S-C	A	From Leg	1.000 0.000 0.000	0.000	73.000	No Ice 1/2" Ice 1" Ice	5.167 5.618 6.077	3.038 3.469 3.909	0.026 0.053 0.085
APXV18-206517S-C	B	From Leg	1.000 0.000 0.000	0.000	73.000	No Ice 1/2" Ice 1" Ice	5.167 5.618 6.077	3.038 3.469 3.909	0.026 0.053 0.085
APXV18-206517S-C	C	From Leg	1.000 0.000 0.000	0.000	73.000	No Ice 1/2" Ice 1" Ice	5.167 5.618 6.077	3.038 3.469 3.909	0.026 0.053 0.085
Pipe Mount [PM 602-3]	C	None		0.000	73.000	No Ice 1/2" Ice 1" Ice	7.680 9.500 11.320	7.680 9.500 11.320	0.279 0.353 0.427
<b>*50*</b>									
Side Arm Mount [SO 102-3]	C	None		0.000	50.000	No Ice 1/2" Ice 1" Ice	3.000 3.480 3.960	3.000 3.480 3.960	0.081 0.111 0.141
6' x 2" Mount Pipe	C	From Leg	1.000 0.000 0.000	0.000	50.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
<b>*45*</b>									
57860-30	A	From Leg	4.000 0.000 0.000	0.000	45.000	No Ice 1/2" Ice 1" Ice	0.077 0.118 0.168	0.077 0.118 0.168	0.000 0.002 0.003
Side Arm Mount [SO 102-3]	C	None		0.000	45.000	No Ice 1/2" Ice 1" Ice	3.000 3.480 3.960	3.000 3.480 3.960	0.081 0.111 0.141
6' x 2" Mount Pipe	A	From Leg	1.000 0.000 0.000	0.000	45.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe	C	From Leg	1.000 0.000 0.000	0.000	45.000	No Ice 1/2" Ice 1" Ice	1.425 1.925 2.294	1.425 1.925 2.294	0.022 0.033 0.048

### Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	3 dB Beam Width °	Elevation ft	Outside Diameter ft	Aperture Area ft <sup>2</sup>	Weight K	
TA-2324-LHCP	C	Paraboloid w/Radome	From Leg	1.000 0.000 0.000	0.000		50.000	2.167	No Ice 1/2" Ice 1" Ice	3.690 3.980 4.270	0.028 0.048 0.069
*** 1111	C	Paraboloid w/o Radome	From Leg	1.000 0.000 0.000	0.000		45.000	3.330	No Ice 1/2" Ice 1" Ice	8.709 9.151 9.592	0.040 0.087 0.134

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	100 - 46.8333	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-15.912	-0.324	1.729
			Max. Mx	5	-9.244	-615.461	-7.121
			Max. My	2	-9.248	7.339	615.457
			Max. Vy	5	17.216	-615.461	-7.121
			Max. Vx	2	-17.173	7.339	615.457
			Max. Torque	5			0.563
L2	46.8333 - 0	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-29.030	0.242	4.065
			Max. Mx	5	-19.596	-1707.674	-3.423
			Max. My	2	-19.596	-3.800	1700.167
			Max. Vy	5	24.043	-1707.674	-3.423
			Max. Vx	2	-23.870	-3.800	1700.167
			Max. Torque	9			-0.726

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	15	29.030	-0.050	4.891
	Max. H <sub>x</sub>	11	19.619	23.828	0.154
	Max. H <sub>z</sub>	2	19.619	-0.278	23.851
	Max. M <sub>x</sub>	2	1700.167	-0.278	23.851
	Max. M <sub>z</sub>	5	1707.674	-24.024	0.098
	Max. Torsion	5	0.500	-24.024	0.098
	Min. Vert	1	19.619	0.000	0.000
	Min. H <sub>x</sub>	5	19.619	-24.024	0.098
	Min. H <sub>z</sub>	8	19.619	-0.123	-23.677
	Min. M <sub>x</sub>	8	-1690.074	-0.123	-23.677
	Min. M <sub>z</sub>	11	-1698.641	23.828	0.154
	Min. Torsion	9	-0.726	11.780	-20.503

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	19.619	0.000	0.000	-0.974	0.036	0.000
Dead+Wind 0 deg - No Ice	19.619	0.278	-23.851	-1700.167	-3.800	-0.183
Dead+Wind 30 deg - No Ice	19.619	12.097	-20.546	-1463.259	-850.007	-0.248
Dead+Wind 60 deg - No Ice	19.619	20.782	-11.877	-840.769	-1473.380	-0.442
Dead+Wind 90 deg - No Ice	19.619	24.024	-0.098	3.423	-1707.674	-0.500
Dead+Wind 120 deg - No Ice	19.619	21.004	11.685	845.266	-1492.270	-0.209
Dead+Wind 150 deg - No Ice	19.619	11.978	20.506	1467.962	-859.888	0.306
Dead+Wind 180 deg - No Ice	19.619	0.123	23.677	1690.074	-14.462	0.629
Dead+Wind 210 deg - No Ice	19.619	-11.780	20.503	1459.137	835.582	0.726
Dead+Wind 240 deg - No Ice	19.619	-20.617	11.782	834.397	1465.844	0.392
Dead+Wind 270 deg - No Ice	19.619	-23.828	-0.154	-16.887	1698.641	-0.028
Dead+Wind 300 deg - No Ice	19.619	-20.653	-11.945	-859.067	1476.148	-0.186
Dead+Wind 330 deg - No Ice	19.619	-11.951	-20.521	-1470.743	858.570	-0.254
Dead+Ice+Temp	29.030	0.000	-0.000	-4.065	0.242	0.000
Dead+Wind 0 deg+Ice+Temp	29.030	0.050	-4.891	-361.003	-0.195	-0.071
Dead+Wind 30 deg+Ice+Temp	29.030	2.477	-4.214	-311.300	-178.252	-0.081
Dead+Wind 60 deg+Ice+Temp	29.030	4.262	-2.434	-180.461	-309.419	-0.107
Dead+Wind 90 deg+Ice+Temp	29.030	4.928	-0.016	-3.002	-358.699	-0.104
Dead+Wind 120 deg+Ice+Temp	29.030	4.306	2.402	173.930	-313.282	-0.034
Dead+Wind 150 deg+Ice+Temp	29.030	2.460	4.208	304.582	-180.620	0.078
Dead+Wind 180 deg+Ice+Temp	29.030	0.026	4.857	351.200	-2.789	0.152
Dead+Wind 210 deg+Ice+Temp	29.030	-2.418	4.205	302.628	175.994	0.175
Dead+Wind 240 deg+Ice+Temp	29.030	-4.230	2.416	171.373	308.464	0.105
Dead+Wind 270 deg+Ice+Temp	29.030	-4.890	-0.032	-7.424	357.452	0.008
Dead+Wind 300 deg+Ice+Temp	29.030	-4.240	-2.451	-184.418	310.694	-0.044
Dead+Wind 330 deg+Ice+Temp	29.030	-2.454	-4.211	-312.994	180.838	-0.076
Dead+Wind 0 deg - Service	19.619	0.086	-7.361	-525.706	-1.147	-0.059
Dead+Wind 30 deg - Service	19.619	3.734	-6.341	-452.544	-262.459	-0.074
Dead+Wind 60 deg - Service	19.619	6.414	-3.666	-260.317	-454.959	-0.131
Dead+Wind 90 deg - Service	19.619	7.415	-0.030	0.373	-527.315	-0.152
Dead+Wind 120 deg - Service	19.619	6.483	3.606	260.342	-460.801	-0.068



Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 150 deg - Service	19.619	3.697	6.329	452.633	-265.516	0.089
Dead+Wind 180 deg - Service	19.619	0.038	7.308	521.217	-4.443	0.192
Dead+Wind 210 deg - Service	19.619	-3.636	6.328	449.898	258.053	0.227
Dead+Wind 240 deg - Service	19.619	-6.363	3.636	256.977	452.680	0.127
Dead+Wind 270 deg - Service	19.619	-7.354	-0.048	-5.901	524.573	-0.006
Dead+Wind 300 deg - Service	19.619	-6.374	-3.687	-265.974	455.871	-0.060
Dead+Wind 330 deg - Service	19.619	-3.689	-6.334	-454.863	265.158	-0.084

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-19.619	0.000	0.000	19.619	0.000	0.000%
2	0.278	-19.619	-23.851	-0.278	19.619	23.851	0.000%
3	12.097	-19.619	-20.546	-12.097	19.619	20.546	0.000%
4	20.782	-19.619	-11.877	-20.782	19.619	11.877	0.000%
5	24.024	-19.619	-0.098	-24.024	19.619	0.098	0.000%
6	21.004	-19.619	11.685	-21.004	19.619	-11.685	0.000%
7	11.978	-19.619	20.506	-11.978	19.619	-20.506	0.000%
8	0.123	-19.619	23.677	-0.123	19.619	-23.677	0.000%
9	-11.780	-19.619	20.503	11.780	19.619	-20.503	0.000%
10	-20.617	-19.619	11.782	20.617	19.619	-11.782	0.000%
11	-23.828	-19.619	-0.154	23.828	19.619	0.154	0.000%
12	-20.653	-19.619	-11.945	20.653	19.619	11.945	0.000%
13	-11.951	-19.619	-20.521	11.951	19.619	20.521	0.000%
14	0.000	-29.030	0.000	0.000	29.030	0.000	0.000%
15	0.050	-29.030	-4.891	-0.050	29.030	4.891	0.000%
16	2.477	-29.030	-4.214	-2.477	29.030	4.214	0.000%
17	4.262	-29.030	-2.434	-4.262	29.030	2.434	0.000%
18	4.928	-29.030	-0.016	-4.928	29.030	0.016	0.000%
19	4.306	-29.030	2.402	-4.306	29.030	-2.402	0.000%
20	2.460	-29.030	4.208	-2.460	29.030	-4.208	0.000%
21	0.026	-29.030	4.857	-0.026	29.030	-4.857	0.000%
22	-2.418	-29.030	4.205	2.418	29.030	-4.205	0.000%
23	-4.230	-29.030	2.416	4.230	29.030	-2.416	0.000%
24	-4.890	-29.030	-0.032	4.890	29.030	0.032	0.000%
25	-4.240	-29.030	-2.451	4.240	29.030	2.451	0.000%
26	-2.454	-29.030	-4.211	2.454	29.030	4.211	0.000%
27	0.086	-19.619	-7.361	-0.086	19.619	7.361	0.000%
28	3.734	-19.619	-6.341	-3.734	19.619	6.341	0.000%
29	6.414	-19.619	-3.666	-6.414	19.619	3.666	0.000%
30	7.415	-19.619	-0.030	-7.415	19.619	0.030	0.000%
31	6.483	-19.619	3.606	-6.483	19.619	-3.606	0.000%
32	3.697	-19.619	6.329	-3.697	19.619	-6.329	0.000%
33	0.038	-19.619	7.308	-0.038	19.619	-7.308	0.000%
34	-3.636	-19.619	6.328	3.636	19.619	-6.328	0.000%
35	-6.363	-19.619	3.636	6.363	19.619	-3.636	0.000%
36	-7.354	-19.619	-0.048	7.354	19.619	0.048	0.000%
37	-6.374	-19.619	-3.687	6.374	19.619	3.687	0.000%
38	-3.689	-19.619	-6.334	3.689	19.619	6.334	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000841
3	Yes	4	0.00000001	0.00068622
4	Yes	4	0.00000001	0.00069462
5	Yes	4	0.00000001	0.00001747
6	Yes	4	0.00000001	0.00070024
7	Yes	4	0.00000001	0.00071719
8	Yes	4	0.00000001	0.00001616
9	Yes	4	0.00000001	0.00069028
10	Yes	4	0.00000001	0.00067282
11	Yes	4	0.00000001	0.00002975
12	Yes	4	0.00000001	0.00072049
13	Yes	4	0.00000001	0.00071203
14	Yes	4	0.00000001	0.00000001
15	Yes	4	0.00000001	0.00020816
16	Yes	4	0.00000001	0.00022350
17	Yes	4	0.00000001	0.00022346
18	Yes	4	0.00000001	0.00020643
19	Yes	4	0.00000001	0.00022342
20	Yes	4	0.00000001	0.00022223
21	Yes	4	0.00000001	0.00020263
22	Yes	4	0.00000001	0.00021783
23	Yes	4	0.00000001	0.00021855
24	Yes	4	0.00000001	0.00020596
25	Yes	4	0.00000001	0.00022724
26	Yes	4	0.00000001	0.00022721
27	Yes	4	0.00000001	0.00000001
28	Yes	4	0.00000001	0.00003817
29	Yes	4	0.00000001	0.00003982
30	Yes	4	0.00000001	0.00000001
31	Yes	4	0.00000001	0.00003838
32	Yes	4	0.00000001	0.00004048
33	Yes	4	0.00000001	0.00000001
34	Yes	4	0.00000001	0.00003917
35	Yes	4	0.00000001	0.00003641
36	Yes	4	0.00000001	0.00000001
37	Yes	4	0.00000001	0.00004111
38	Yes	4	0.00000001	0.00003977

**Maximum Tower Deflections - Service Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	100 - 46.8333	12.955	31	1.034	0.001
L2	52 - 0	3.901	31	0.668	0.000

**Critical Deflections and Radius of Curvature - Service Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
100.000	SWCP 2x5514 w/ Mount Pipe	31	12.955	1.034	0.001	33810
95.000	TA-2335-DAB-L-095	31	11.877	1.002	0.001	33810
83.000	APX16DWV-16DWVS-E-A20 w/ Mount Pipe	31	9.343	0.923	0.001	9944
73.000	APXV18-206517S-C	31	7.359	0.851	0.001	6260
50.000	TA-2324-LHCP	31	3.640	0.647	0.000	3689
45.000	1111	31	3.043	0.593	0.000	4068

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	100 - 46.8333	41.939	6	3.348	0.003
L2	52 - 0	12.638	6	2.164	0.002

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
100.000	SWCP 2x5514 w/ Mount Pipe	6	41.939	3.348	0.004	10504
95.000	TA-2335-DAB-L-095	6	38.451	3.245	0.004	10504
83.000	APX16DWV-16DWVS-E-A20 w/ Mount Pipe	6	30.251	2.989	0.003	3088
73.000	APXV18-206517S-C	6	23.830	2.757	0.002	1943
50.000	TA-2324-LHCP	6	11.792	2.097	0.002	1143
45.000	1111	6	9.857	1.922	0.001	1260

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KI/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
L1	100 - 46.8333 (1)	TP33.26x23.43x0.313	53.167	0.000	0.0	39.00	32.192	-9.238	1255.500	0.007
L2	46.8333 - 0 (2)	TP41.3x31.68x0.375	52.000	0.000	0.0	39.00	49.417	-19.595	1927.260	0.010

### Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M <sub>x</sub> kip-ft	Actual f <sub>bx</sub> ksi	Allow. F <sub>bx</sub> ksi	Ratio $\frac{f_{bx}}{F_{bx}}$	Actual M <sub>y</sub> kip-ft	Actual f <sub>by</sub> ksi	Allow. F <sub>by</sub> ksi	Ratio $\frac{f_{by}}{F_{by}}$
L1	100 - 46.8333 (1)	TP33.26x23.43x0.313	621.89 3	29.69	39.00	0.761	0.000	0.00	39.00	0.000
L2	46.8333 - 0 (2)	TP41.3x31.68x0.375	1715.0 33	41.68	39.00	1.069	0.000	0.00	39.00	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f <sub>v</sub> ksi	Allow. F <sub>v</sub> ksi	Ratio $\frac{f_v}{F_v}$	Actual T kip-ft	Actual f <sub>vt</sub> ksi	Allow. F <sub>vt</sub> ksi	Ratio $\frac{f_{vt}}{F_{vt}}$
L1	100 - 46.8333 (1)	TP33.26x23.43x0.313	17.337	0.54	26.00	0.042	0.501	0.01	26.00	0.000
L2	46.8333 - 0 (2)	TP41.3x31.68x0.375	24.055	0.49	26.00	0.038	0.209	0.00	26.00	0.000

Section No.	Elevation ft	Size	Actual V K	Actual $f_v$ ksi	Allow. $F_v$ ksi	Ratio $\frac{f_v}{F_v}$	Actual T kip-ft	Actual $f_{vt}$ ksi	Allow. $F_{vt}$ ksi	Ratio $\frac{f_{vt}}{F_{vt}}$
-------------	-----------------	------	---------------	---------------------	---------------------	-------------------------	--------------------	------------------------	------------------------	-------------------------------

### Pole Interaction Design Data

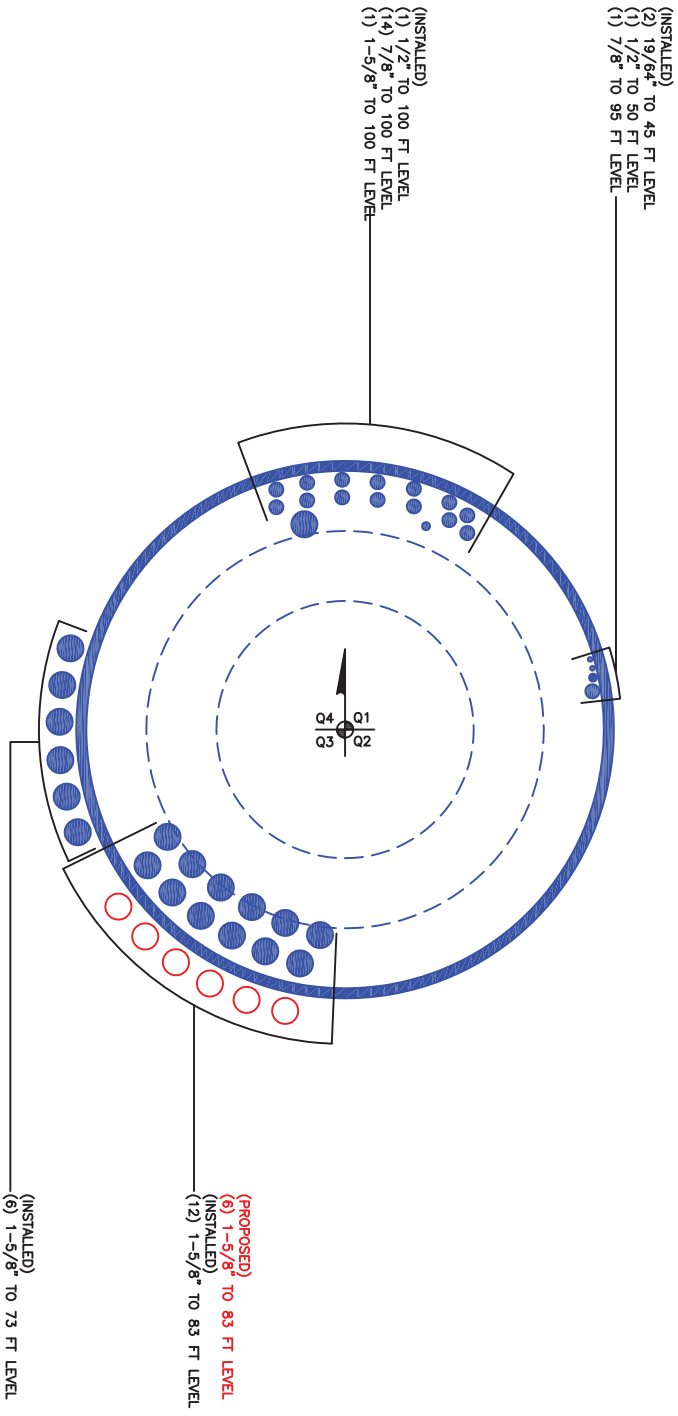
Section No.	Elevation ft	Ratio P $P_a$	Ratio $f_{bx}$ $F_{bx}$	Ratio $f_{by}$ $F_{by}$	Ratio $f_v$ $F_v$	Ratio $f_{vt}$ $F_{vt}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	100 - 46.8333 (1)	0.007	0.761	0.000	0.042	0.000	0.769	1.333	H1-3+VT ✓
L2	46.8333 - 0 (2)	0.010	1.069	0.000	0.038	0.000	1.079	1.333	H1-3+VT ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF* $P_{allow}$ K	% Capacity	Pass Fail	
L1	100 - 46.8333	Pole	TP33.26x23.43x0.313	1	-9.238	1673.581	57.7	Pass	
L2	46.8333 - 0	Pole	TP41.3x31.68x0.375	2	-19.595	2569.037	81.0	Pass	
							Summary		
							Pole (L2)	81.0	Pass
							<b>RATING =</b>	<b>81.0</b>	<b>Pass</b>



**APPENDIX B**  
**BASE LEVEL DRAWING**



BUSINESS UNIT: 806359 TOWER ID: C\_BASELEVEL

**APPENDIX C**  
**ADDITIONAL CALCULATIONS**

## Asymmetric Anchor Rod

	Reactions
Moment (k-ft)	<b>1,715.0</b>
Axial (k)	<b>20.0</b>
Shear (k)	<b>24.0</b>
Code	<b>F</b>
Total Anchor Rods	<b>12</b>

	Original	Additional
Anchor Rods	<b>8</b>	<b>4</b>
Anchor Rod Grade	<b>A615-J</b>	<b>Dywidag</b>
Fy (ksi)	<b>75</b>	<b>127.7</b>
Fu (ksi)	<b>100</b>	<b>150</b>
Anchor Rod Diameter (in)	<b>2.25</b>	<b>1.75</b>
Anchor Rod Circle (in)	<b>47.58</b>	<b>52.8</b>
Base Plate	<b>Round</b>	
ETA Factor, $\eta$	<b>0.5</b>	

### Additional Anchor Rods

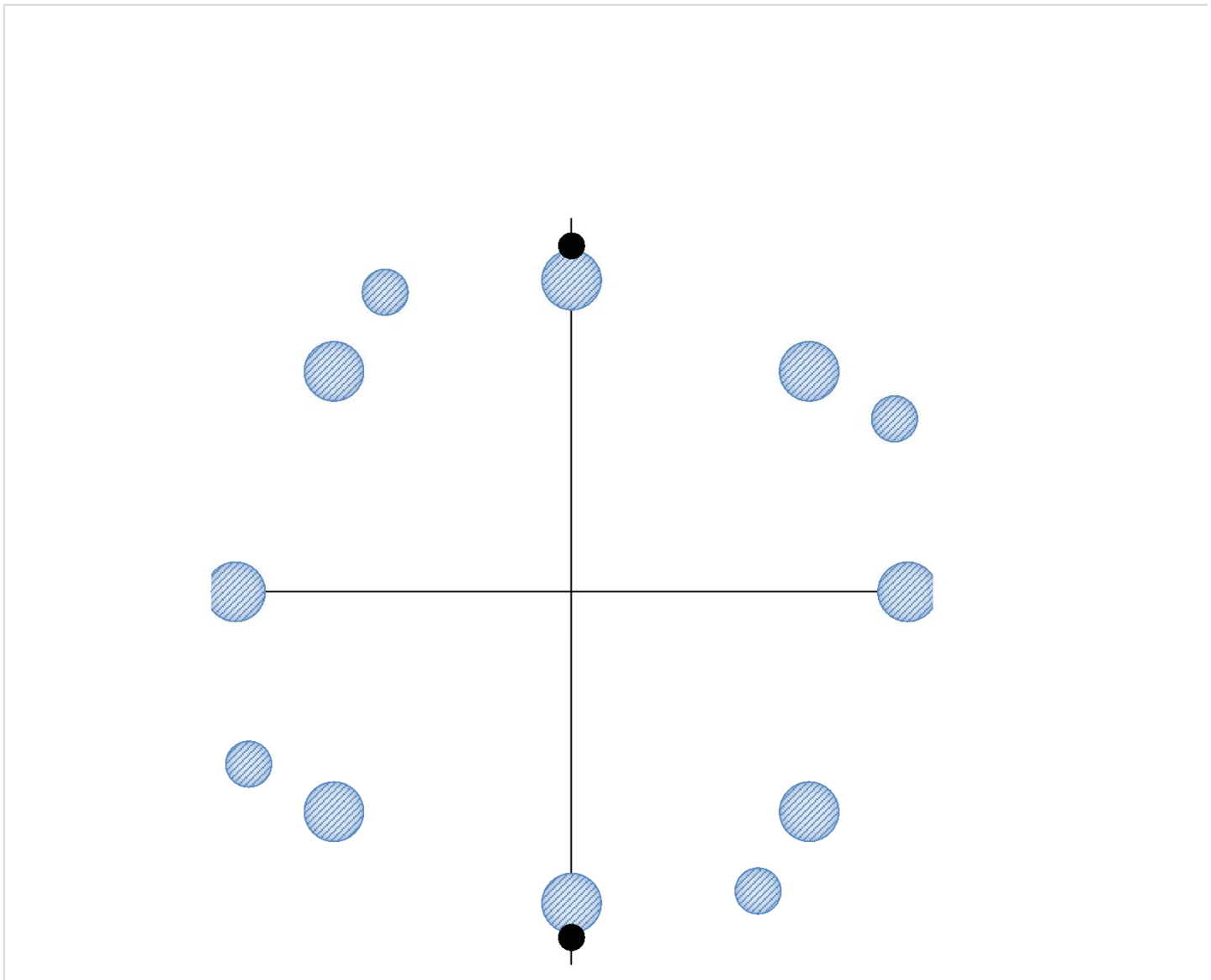
Anchor Rod	Anchor Rod Diameter, in	Anchor Rod Circle, in	Location, degrees	Anchor Rod Gross Area, in <sup>2</sup>	Force, kips	Anchor Rod Stress Ratio	
1	A615-J	2.25	47.58	0.0	3.98	150.4	<b>77.1%</b>
2	A615-J	2.25	47.58	45.0	3.98	105.8	54.3%
3	A615-J	2.25	47.58	90.0	3.98	-1.9	1.0%
4	A615-J	2.25	47.58	135.0	3.98	-105.8	54.3%
5	A615-J	2.25	47.58	180.0	3.98	-150.4	<b>77.1%</b>
6	A615-J	2.25	47.58	225.0	3.98	-105.8	54.3%
7	A615-J	2.25	47.58	270.0	3.98	1.9	1.0%
8	A615-J	2.25	47.58	315.0	3.98	105.8	54.3%
9	Dywidag	1.75	52.8	30.0	2.71	98.6	<b>55.1%</b>
10	Dywidag	1.75	52.8	120.0	2.71	-56.4	31.5%
11	Dywidag	1.75	52.8	210.0	2.71	-98.6	<b>55.1%</b>
12	Dywidag	1.75	52.8	300.0	2.71	56.4	31.5%



## Adjusted Loads for Base Plate Check

Welded Anchor Brackets?	<b>No</b>	
Adjusted Moment	<b>1715.0</b>	k-ft
Adjusted Axial	<b>20.0</b>	kips
Shear	<b>24.0</b>	kips

$I_x, \text{in}^4$	$I_y, \text{in}^4$	$I_{xy}, \text{in}^4$	x bar, in	y bar, in	$\Phi$	c, in
12781.58	12781.58	0.00	0.000	0.000	90.00	23.79



## Stiffened or Unstiffened, UngROUTed, Circular Base Plate - Any Rod Material

### TIA Rev F

#### Site Data

BU#: 806359  
 Site Name: NHV 104 943122  
 App #: 310127 Rev. 4

Pole Manufacturer: Other

#### Anchor Rod Data

Qty:	8	
Diam:	2.25	in
Rod Material:	A615-J	
Strength (Fu):	100	ksi
Yield (Fy):	75	ksi
Bolt Circle:	47.58	in

#### Plate Data

Diam:	53.58	in
Thick:	2.5	in
Grade:	60	ksi
Single-Rod B-eff:	14.81	in

#### Stiffener Data (Welding at both sides)

Config:	0	*
Weld Type:		
Groove Depth:		<-- Disregard
Groove Angle:		<-- Disregard
Fillet H. Weld:		in
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

#### Pole Data

Diam:	41.3	in
Thick:	0.375	in
Grade:	65	ksi
# of Sides:	12	"0" IF Round
Fu	80	ksi
Reinf. Fillet Weld	0	"0" if None

#### Stress Increase Factor

ASIF:	1.333
-------	-------

#### Reactions

Moment:	1715	ft-kips
Axial:	20	kips
Shear:	24	kips

If No stiffeners, Criteria: AISC ASD <-Only Applicable to Unstiffened Cases

#### Base Plate Results

Base Plate Stress:	27.9 ksi
Allowable Plate Stress:	60.0 ksi
Base Plate Stress Ratio:	46.5% <span style="color: green;">Pass</span>

#### Flexural Check

Rigid
Service ASD
0.75*Fy*ASIF
Y.L. Length:
23.63

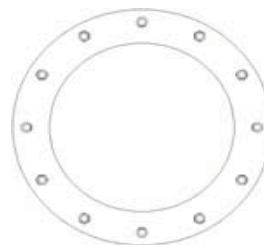
n/a

#### Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, fb/Fb+(fv/Fv)^2:	n/a
Plate Tension+Shear, ft/Ft+(fv/Fv)^2:	n/a
Plate Comp. (AISC Bracket):	n/a

#### Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

BU:	806359
Site Name:	NHV 104 943122
App Number:	310127 R.4
Work Order:	1122514

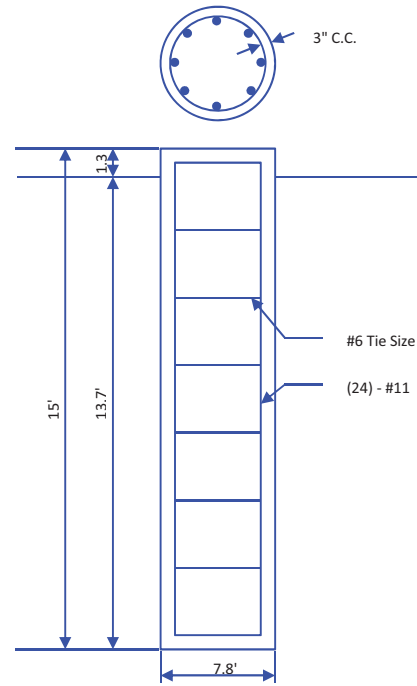


Monopole Drilled Pier

Input

<b>Criteria</b>	
TIA Revision:	F
ACI 318 Revision:	2002
Seismic Category:	B
<b>Forces</b>	
Compression	20 kips
Shear	24 kips
Moment	1715 k-ft
Swelling Force	0 kips
<b>Foundation Dimensions</b>	
Pier Diameter:	7.8 ft
Ext. above grade:	1.3 ft
Depth below grade:	13.7 ft
<b>Material Properties</b>	
Number of Rebar:	24
Rebar Size:	11
Tie Size	6
Rebar tensile strength:	60 ksi
Concrete Strength:	3000 psi
Ultimate Concrete Strain	0.003 in/in
Clear Cover to Ties:	3 in

Soil Profile: 123



Layer	Thickness (ft)	From (ft)	To (ft)	Unit Weight (pcf)	Cohesion (psf)	Friction Angle (deg)	Ultimate Uplift Friction (ksf)	Ultimate Comp. Friction (ksf)	Ultimate Bearing Capacity (ksf)	SPT 'N' Counts
1	4	0	4	105	0				0	
2	2	4	6	105		29			0	
3	2.3	6	8.3	135		40			0	
4	5.4	8.3	13.7	150	20000				0	

Analysis Results

<b>Soil Lateral Capacity</b>	
Depth to Zero Shear:	6.64 ft
Max Moment, Mu:	1972.97 k-ft
Soil Safety Factor:	4.87
Safety Factor Req'd:	2
<b>RATING:</b>	<b>41.1%</b>

<b>Soil Axial Capacity</b>	
Skin Friction (k):	450.69 kips
End Bearing (k):	0.00 kips
Comp. Capacity (k), φCn:	450.69 kips
Comp. (k), Cu:	26.00 kips
<b>RATING:</b>	<b>5.8%</b>

<b>Concrete/Steel Check</b>	
Mu (from soil analysis)	2564.86 k-ft
φMn	6651.55 k-ft
<b>RATING:</b>	<b>38.6%</b>

rho provided	0.54
rho required	0.33 OK

Rebar Spacing	9.68
Spacing required	22.56 OK

Dev. Length required	6.81
Dev. Length provided	61.78 OK

**Overall Foundation Rating: 41.1%**

**RADIO FREQUENCY EMISSIONS ANALYSIS REPORT  
EVALUATION OF HUMAN EXPOSURE POTENTIAL  
TO NON-IONIZING EMISSIONS**

**T-Mobile Existing Facility**

**Site ID: CTNH009B**

**NH009/CrownOronoque\_ET  
423 Oronoque Road  
Milford, CT 06460**

**September 16, 2015**

**EBI Project Number: 6215004761**

<b>Site Compliance Summary</b>	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general public allowable limit:	<b>14.20 %</b>



September 16, 2015

T-Mobile USA  
Attn: Jason Overbey, RF Manager  
35 Griffin Road South  
Bloomfield, CT 06002

Emissions Analysis for Site: **CTNH009B – NH009/CrownOronoque\_ET**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **423 Oronoque Road, Milford, CT**, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the 700 MHz Band is approximately 467  $\mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the PCS and AWS bands is 1000  $\mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **423 Oronoque Road, Milford, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM / UMTS channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
- 2) 2 UMTS channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 LTE channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 1 LTE channel (700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
- 5) Since the radios are ground mounted there are additional cabling losses accounted for. For each RF path the following losses were calculated. 1.24 dB of additional cable loss for all 1900 MHz and 2100 MHz channels and 0.673 dB of additional cable loss at 700 MHz. This is based on manufacturers Specifications for 120 feet of 1-5/8” coax cable on each path.

- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the **RFS APX16DWV-16DWVS-E-A20** for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the **Commscope LNX-6515DS-VTM** for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The **RFS APX16DWV-16DWVS-E-A20** has a maximum gain of **16.3 dBd** at its main lobe. The **Commscope LNX-6515DS-VTM** has a maximum gain of **14.6 dBd** at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerline of the proposed antennas is **83 feet** above ground level (AGL).
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

### T-Mobile Site Inventory and Power Data

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	RFS APX16DWV-16DWVS-E-A20	Make / Model:	RFS APX16DWV-16DWVS-E-A20	Make / Model:	RFS APX16DWV-16DWVS-E-A20
Gain:	16.3 dBd	Gain:	16.3 dBd	Gain:	16.3 dBd
Height (AGL):	83	Height (AGL):	83	Height (AGL):	83
Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)
Channel Count	6	Channel Count	6	# PCS Channels:	6
Total TX Power:	240	Total TX Power:	240	# AWS Channels:	240
ERP (W):	7,695.05	ERP (W):	7,695.05	ERP (W):	7,695.05
Antenna A1 MPE%	4.67	Antenna B1 MPE%	4.67	Antenna C1 MPE%	4.67
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM
Gain:	14.6 dBd	Gain:	14.6 dBd	Gain:	14.6 dBd
Height (AGL):	83	Height (AGL):	83	Height (AGL):	83
Frequency Bands	700 MHz	Frequency Bands	700 MHz	Frequency Bands	700 MHz
Channel Count	1	Channel Count	1	Channel Count	1
Total TX Power:	30	Total TX Power:	30	Total TX Power:	30
ERP (W):	741.01	ERP (W):	741.01	ERP (W):	741.01
Antenna A2 MPE%	0.96	Antenna B2 MPE%	0.96	Antenna C2 MPE%	0.96

Site Composite MPE%	
Carrier	MPE%
T-Mobile (Per Sector Max)	5.63 %
MetroPCS	1.28 %
Verizon Wireless	4.03 %
Sirius XM Radio	3.26 %
<b>Site Total MPE %:</b>	<b>14.20 %</b>

T-Mobile Sector 1 Total:	5.63 %
T-Mobile Sector 2 Total:	5.63 %
T-Mobile Sector 3 Total:	5.63 %
<b>Site Total:</b>	<b>14.20 %</b>

T-Mobile _per sector	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
T-Mobile 2100 MHz (AWS) LTE	2	1923.76	83	23.33	2100	1000	2.33 %
T-Mobile 700 MHz LTE	1	741.01	83	4.49	700	467	0.96 %
T-Mobile 1900 MHz (PCS) GSM/UMTS	2	961.88	83	11.66	1900	1000	1.17 %
T-Mobile 2100 MHz (AWS) UMTS	2	961.88	83	11.66	2100	1000	1.17 %
						<b>Total:</b>	<b>4.31 %</b>

## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector 1:	5.63 %
Sector 2:	5.63 %
Sector 3 :	5.63 %
T-Mobile Per Sector Maximum:	5.63 %
Site Total:	14.20 %
Site Compliance Status:	<b>COMPLIANT</b>

The anticipated composite MPE value for this site assuming all carriers present is **14.20%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



Scott Heffernan  
RF Engineering Director

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