# JULIE D. KOHLER 

PLEASE REPLY TO: Bridgeport WRITER'S DIRECT DIAL: (203) 337-4157 E-Mail Address: jkohler@cohenandwolf.com

November 18, 2014

Attorney Melanie Bachman<br>Acting Executive Director Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051

## Re: Notice of Exempt Modification <br> AT\&T Towers/T-Mobile co-location <br> Site ID CT11056J <br> 290 Preston Avenue, Middletown CT

Dear Attorney Bachman:
This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, AT\&T Towers owns the existing monopole telecommunications tower and related facility at 290 Preston Avenue, Middletown Connecticut (longitude -72.7429/ latitude 41.5573). T-Mobile intends to add three (3) antennas and related equipment at this existing telecommunications facility in Middletown ("Middletown Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Mayor, Daniel T. Drew, and the property owners Ernest and Brenda Trumpold.

The existing Middletown Facility consists of a 148 foot tall monopole structure. TMobile plans to add three (3) antennas and three (3) RRUs (remote radio units) on pipe mounts at a centerline of 140 feet. T-Mobile will also use implement a spare fiber run along the length of the tower. See the plans revised to November 7, 2014 attached hereto as Exhibit A. The existing Facility is structurally capable of supporting T-Mobile's proposed modifications, as indicated in the structural analysis dated October 13, 2014 and stamped November 6, 2014 attached hereto as Exhibit B.

The planned modifications to the Middletown Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

November 18, 2014
Site ID CT11056J
Page 2

1. The proposed modification will not increase the height of the tower. T-Mobile's proposed antennas will be installed at the 140 foot level of the 148 foot monopole tower. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.
2. T-Mobile does not proposed to alter the existing compound, and therefore will not require an extension of the site boundaries.
3. The proposed modification to the Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the proposed antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated November 14, 2014 T-Mobile's operations would add $6.72 \%$ of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be $64.40 \%$ of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, T-Mobile respectfully submits that the proposed antennas and equipment at the Middletown Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,
hi


Juke D. Kohler, Esq.
cc: City of Middletown, Mayor Daniel T. Drew
AT\&T Towers
Ernest and Brenda Trumpold
Sheldon Freincle, NSS







Ping Jiang

AT\&T Towers
2300 Northlake Center Drive Suite 405
Tucker, GA 30084
770-708-6100
Monday, October 13, 2014

## AT\&T DESIGNATION:

ANALYSIS CRITERIA:

| AT\&T DESIGNATION: | Site ID: |
| :--- | :--- |
|  | Site FA: |
|  | Site Name: |
|  | AT\&T Project: |
|  | BV Project: |
|  | Codes: |

Black \& Veatch Corp.
10950 Grandview Drive
Overland Park, KS 66210
(913) 458-7245

JiangP@bv.com

## STRUCTURAL ANALYSIS

148' Monopole
14635
10035088
MIDDLETOWN SW
T-Mobile Modification 9/5/2014
176850 (14635TMOCT-S)
TIAEIA-222-F $\quad 85 \mathrm{mph}$ Fastest-Mile
IBC 2003
Connecticut State Building Code 2005
SITE DATA: 290 Preston Avenue, Middletown, CT ,06457, Middlesex County
Latitude 41.557353, Longitude -72.743277
Market: MA/RI/NT/NH/ME/CT
148' Monopole

Black \& Veatch Corp. is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

## Analysis Results

| Tower Stress Level with Proposed Equipment: | $94.50 \%$ | Pass |
| :--- | :--- | :--- |
| Connection Stress Level with Proposed Equipment: | $90.50 \%$ | Pass |
| Foundation Ratio with Proposed Equipment: | $98.10 \%$ | Pass |

We at Black \& Veatch Corp. appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully Submitted by: Black \& Veatch Corp.
Analysis Prepared by:
Analysis Reviewed by:
Brennan J. Sedlacek, E.I.T.
Chris A. Krafft, P.E.


Black \& Veatch Corp.<br>10950 Grandview Drive<br>Overland Park, KS 66210<br>B\&V: 176850 (14635TMOCT-S)

## Assumptions, Disclaimers, and Notes

1. This analysis was performed under the assumption that all information provided to Black \& Veatch is current and correct. This is to include site data, existing/proposed appurtenance loading, tower/foundation details, and geotechnical data. If this information is not current and correct, this report should be considered obsolete and further analysis will be required.
2. This analysis assumes that the tower structural components and mounts, including all steel sections and attachment hardware, are in good working order and in their original state, free of rust or other forms of corrosion. Furthermore, it is assumed that the tower and the tower foundation have been properly maintained and monitored since the time of construction. This report should be considered obsolete and further analysis will be required if the tower and/or foundation does not meet all of the above specifications.
3. This analysis assumes that all existing and/or proposed equipment mounts on the tower will have adequate capacity to support the existing and proposed equipment loading.
4. Capacity of the structural members is based on theoretical values as shown in the attached TAS form.
5. When applicable, this structural analysis is only valid if the proposed coax cables are stacked as shown in the attached feedline sketch.
6. Although there is grout present between the tower's foundation and base plate, the effect of grout has not been considered in this analysis. This is due to the difficult installation circumstances associated with relatively large base plates with narrow flanges used for the pole structures. This also matches industry standards/practice and TIA recommendations.







 5.250 4.750 $\quad 4.000$ 69.8 \# DESIGNED APPURTENANCE LOADING

| thxTOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
|  | Project | Client | 17635 Middleton SW |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Allow Shield \& Component Type \& Placement
ft \& Total Number \& \& $C_{A} A_{A}$

$f t^{2} / f t$ \& Weight
plf <br>
\hline \multirow[t]{5}{*}{LDF7-50A(1-5/8") (T-Mobile - Existing)} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{140.000-5.000} \& \multirow[t]{5}{*}{18} \& No Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 0.000 \& 0.820 <br>
\hline \multirow[t]{5}{*}{3/8" RET cable (T-Mobile - Existing)} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{140.000-5.000} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.000 \& 0.067 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.000 \& 0.067 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.000 \& 0.067 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.000 \& 0.067 <br>
\hline \& \& \& \& \& \& $4^{\prime \prime}$ Ice \& 0.000 \& 0.067 <br>
\hline \multicolumn{9}{|l|}{*****} <br>

\hline \multirow[t]{5}{*}{| LDF6-50A(1-1/4") |
| :--- |
| (Sprint - Existing) |} \& \multirow[t]{5}{*}{A} \& \multirow[t]{6}{*}{No} \& \multirow[t]{6}{*}{Inside Pole} \& \multirow[t]{6}{*}{124.000-5.000} \& \multirow[t]{5}{*}{3} \& No Ice \& 0.000 \& 0.660 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 0.000 \& 0.660 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.000 \& 0.660 <br>
\hline \& \& \& \& \& \& 2"Ice \& 0.000 \& 0.660 <br>
\hline \& \& \& \& \& \& 4"Ice \& 0.000 \& 0.660 <br>
\hline ***** \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{5}{*}{| LDF7-50A(1-5/8") |
| :--- |
| (Verizon-Existing) |} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{110.000-5.000} \& \multirow[t]{5}{*}{13} \& No Ice \& 0.000 \& 0.820 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.000 \& 0.820 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 0.000 \& 0.820 <br>
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\hline \multirow[t]{5}{*}{$$
\begin{gathered}
\text { LDF7-50A(1-5/8") } \\
\text { (Metro PCS - Existing) }
\end{gathered}
$$} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{\[

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\begin{aligned}
& \text { CaAa (Out Of } \\
& \text { Face) }
\end{aligned}
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\]} \& \multirow[t]{5}{*}{$90.000-5.000$} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.198 \& 0.820 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 0.298 \& 2.335 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 0.398 \& 4.461 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.598 \& 10.545 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 0.998 \& 30.044 <br>

\hline \multirow[t]{5}{*}{$$
\begin{gathered}
\text { LDF7-50A(1-5/8") } \\
\text { (Metro PCS - Existing) }
\end{gathered}
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\begin{aligned}
& \mathrm{CaAa} \text { (Out Of } \\
& \text { Face) }
\end{aligned}
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\]} \& \multirow[t]{5}{*}{90.000-5.000} \& \multirow[t]{5}{*}{5} \& No Ice \& 0.000 \& 0.820 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 0.000 \& 2.335 <br>
\hline \& \& \& \& \& \& 1"Ice \& 0.000 \& 4.461 <br>
\hline \& \& \& \& \& \& 2"Ice \& 0.000 \& 10.545 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.000 \& 30.044 <br>
\hline ***** \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{5}{*}{FLC38-50J (3/8 FOAM) (Metro PCS - Existing)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{55.000-5.000} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.000 \& 0.080 <br>

\hline \& \& \& \& \& \& $$
1 / 2^{1} \text { Ice }
$$ \& 0.000 \& 0.654 <br>

\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.000 \& 1.839 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.000 \& 6.042 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.000 \& 21.778 <br>
\hline ***** \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{5}{*}{| LDF4-50A(1/2") |
| :--- |
| (Unknown-Existing) |} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{50.000-5.000} \& \multirow[t]{5}{*}{1} \& \& 0.000 \& 0.150 <br>

\hline \& \& \& \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 0.000 \& 0.840 <br>

\hline \& \& \& \& \& \& 1" Ice \& 0.000 \& 2.141 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.000 \& 6.576 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.000 \& 22.776 <br>
\hline ***** \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{5}{*}{Aero Channel MP308 (reinforcement)} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{30.500-0.000} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.467 \& 0.000 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 0.578 \& 0.000 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.689 \& 0.000 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.911 \& 0.000 <br>
\hline \& \& \& \& \& \& 4" Ice \& 1.356 \& 0.000 <br>

\hline \multirow[t]{5}{*}{Aero Channel MP308 (reinforcement)} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{$$
\begin{gathered}
\mathrm{CaAa} \text { (Out Of } \\
\text { Face) }
\end{gathered}
$$} \& \multirow[t]{5}{*}{30.500-0.000} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.467 \& 0.000 <br>

\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 0.578 \& 0.000 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.689 \& 0.000 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.911 \& 0.000 <br>
\hline \& \& \& \& \& \& 4"Ice \& 1.356 \& 0.000 <br>
\hline \multirow[t]{5}{*}{Aero Channel MP308 (reinforcement)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{30.500-0.000} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.467 \& 0.000 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 0.578 \& 0.000 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.689 \& 0.000 <br>
\hline \& \& \& \& \& \& 2"Ice \& 0.911 \& 0.000 <br>
\hline \& \& \& \& \& \& 4" Ice \& 1.356 \& 0.000 <br>
\hline
\end{tabular}

| tnxTower <br> Black \& Veatch Corp. <br> 10950 Grandview Drive | Job | 14635 Middleton SW | $\text { Page } 4 \text { of } 12$ |
| :---: | :---: | :---: | :---: |
|  | Project | 176850 (14635TMOCT-S) | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:09:07 10/13/14 } \end{array}$ |
| Overland Park, KS 66210 <br> Phone: (913) 458-7245 <br> FAX: (913) 458-8136 | Client | AT\&T | Designed by Brennan J. Sedlacek, E.IT |



| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | 14635 Middleton SW | 6 of 12 |
| Black \& Veatch Corp. 10950 Grandview Drive | Project | 176850 (14635TMOCT-S) | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:09:07 10/13/14 } \\ \hline \end{array}$ |
| Overland Park, KS 66210 <br> Phone: (913) 458-7245 <br> FAX: (913) 458-8136 | Client | AT\&T | Designed by Brennan J. Sedlacek, E.I.T |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral Vert $f t$ $f t$ $f t$ | Azimuth Adjustment | Placement $f t$ |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ Side $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (AT\&T - Existing) |  |  |  |  |  | $\begin{gathered} 1 / 2^{\prime \prime} \text { Ice } \\ 1^{\prime \prime} \text { Ice } \\ 2^{\text {" Ice }} \\ 4^{\prime \prime} \text { Ice } \end{gathered}$ | $\begin{aligned} & 26.800 \\ & 30.500 \\ & 37.900 \\ & 52.700 \end{aligned}$ | $\begin{aligned} & 26.800 \\ & 30.500 \\ & 37.900 \\ & 52.700 \end{aligned}$ | $\begin{aligned} & 2.50 \\ & 2.90 \\ & 3.70 \\ & 5.30 \end{aligned}$ |
| ERICSSON AIR 21 B2A <br> B4P w/ Mount Pipe <br> (T-Mobile - Existing) | A | From Leg | $\begin{aligned} & 4.000 \\ & 6.000 \\ & 0.000 \end{aligned}$ | 0.000 | 140.000 | No Ice $1 / 2^{\text {" }}$ Ice 1" Ice 2" Ice 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{gathered} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| ERICSSON AIR 21 B2A <br> B4P w/ Mount Pipe (T-Mobile - Existing) | A | From Leg | $\begin{gathered} 4.000 \\ -6.000 \\ 0.000 \end{gathered}$ | 0.000 | 140.000 | No Ice $1 / 2^{\prime \prime}$ Ice 1" Ice 2" Ice 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{gathered} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe (T-Mobile - Existing) | B | From Leg | $\begin{aligned} & 4.000 \\ & 6.000 \\ & 0.000 \end{aligned}$ | 0.000 | 140.000 | No Ice $1 / 2^{11}$ Ice 1" Ice 2" Ice 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{array}{r} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{array}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| $\begin{aligned} & \text { ERICSSON AIR } 21 \text { B2A } \\ & \text { B4P w/ Mount Pipe } \\ & \text { (T-Mobile - Existing) } \end{aligned}$ | B | From Leg | $\begin{gathered} 4.000 \\ -6.000 \\ 0.000 \end{gathered}$ | 0.000 | 140.000 | No Ice $1 / 2^{\text {" }}$ Ice 1" Ice 2" Ice 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{gathered} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe (T-Mobile - Existing) | C | From Leg | $\begin{aligned} & 4.000 \\ & 6.000 \\ & 0.000 \end{aligned}$ | 0.000 | 140.000 | No Ice 1/2" Ice 1" Ice $2^{11}$ Ice 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{gathered} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe (T-Mobile - Existing) | C | From Leg | $\begin{gathered} 4.000 \\ -6.000 \\ 0.000 \end{gathered}$ | 0.000 | 140.000 | No Ice <br> $1 / 2^{\text {" }}$ Ice <br> 1" Ice <br> $2^{\prime \prime}$ Ice <br> 4" Ice | $\begin{gathered} 6.825 \\ 7.347 \\ 7.863 \\ 8.926 \\ 11.175 \end{gathered}$ | $\begin{gathered} 5.642 \\ 6.480 \\ 7.257 \\ 8.864 \\ 12.293 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.17 \\ & 0.23 \\ & 0.38 \\ & 0.81 \end{aligned}$ |
| SBNHH-1D65C w/ Mount Pipe <br> (T-Mobile - Proposed) | A | From Leg | $\begin{gathered} 4.000 \\ -1.500 \\ 0.000 \end{gathered}$ | 40.000 | 140.000 | No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice | $\begin{aligned} & 11.626 \\ & 12.346 \\ & 13.074 \\ & 14.543 \\ & 17.807 \end{aligned}$ | $\begin{gathered} 9.793 \\ 11.311 \\ 12.854 \\ 15.192 \\ 20.047 \end{gathered}$ | $\begin{aligned} & 0.08 \\ & 0.17 \\ & 0.27 \\ & 0.50 \\ & 1.15 \end{aligned}$ |
| SBNHH-1D65C w/ Mount Pipe <br> (T-Mobile - Proposed) | B | From Leg | $\begin{gathered} 4.000 \\ -1.500 \\ 0.000 \end{gathered}$ | 85.000 | 140.000 | No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice | $\begin{aligned} & 11.626 \\ & 12.346 \\ & 13.074 \\ & 14.543 \\ & 17.807 \end{aligned}$ | $\begin{gathered} 9.793 \\ 11.311 \\ 12.854 \\ 15.192 \\ 20.047 \end{gathered}$ | $\begin{aligned} & 0.08 \\ & 0.17 \\ & 0.27 \\ & 0.50 \\ & 1.15 \end{aligned}$ |
| SBNHH-1D65C w/ Mount Pipe (T-Mobile - Proposed) | C | From Leg | $\begin{gathered} 4.000 \\ -1.500 \\ 0.000 \end{gathered}$ | 40.000 | 140.000 | No Ice $1 / 2^{\text {" }}$ Ice 1" Ice 2" Ice 4" Ice | $\begin{aligned} & 11.626 \\ & 12.346 \\ & 13.074 \\ & 14.543 \\ & 17.807 \end{aligned}$ | $\begin{gathered} 9.793 \\ 11.311 \\ 12.854 \\ 15.192 \\ 20.047 \end{gathered}$ | $\begin{aligned} & 0.08 \\ & 0.17 \\ & 0.27 \\ & 0.50 \\ & 1.15 \end{aligned}$ |
| T-19-A-V : TMA (T-Mobile - Existing) | A | From Leg | $\begin{gathered} 4.000 \\ -1.500 \\ 0.000 \end{gathered}$ | 0.000 | 140.000 | No Ice 1/2" Ice <br> 1" Ice <br> 2" Ice <br> 4" Ice | $\begin{aligned} & 0.664 \\ & 0.778 \\ & 0.901 \\ & 1.172 \\ & 1.817 \end{aligned}$ | $\begin{aligned} & 0.367 \\ & 0.461 \\ & 0.564 \\ & 0.796 \\ & 1.364 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \\ & 0.03 \\ & 0.04 \\ & 0.11 \end{aligned}$ |
| T-19-A-V : TMA (T-Mobile - Existing) | B | From Leg | $\begin{gathered} 4.000 \\ -1.500 \end{gathered}$ | 0.000 | 140.000 | No Ice $1 / 2^{\text {" }}$ Ice | $\begin{aligned} & 0.664 \\ & 0.778 \end{aligned}$ | $\begin{aligned} & 0.367 \\ & 0.461 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ |


| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | 14635 Middleton SW | 8 of 12 |
| Black \& Veatch Corp. 10950 Grandview Drive | Project | 176850 (14635TMOCT-S) | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:09:07 10/13/14 } \end{array}$ |
| $\begin{gathered} \text { Overland Park, KS } 66210 \\ \text { Phone: (913) 458-7245 } \\ \text { FAX: (913) 458-8136 } \end{gathered}$ | Client | AT\&T | Designed by Brennan J. Sediacek, E.I.T. |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment <br> - | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1900 MHz RRH <br> (Sprint - Existing) | A | From Leg |  | 0.000 | 124.000 | $2^{\text {" I Ice }}$ | 11.031 | 10.844 | 0.41 |
|  |  |  |  |  |  | 4" Ice | 13.679 | 14.851 | 0.91 |
|  |  |  | 4.000 |  |  | No Ice | 2.907 | 3.801 | 0.04 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 3.145 | 4.065 | 0.07 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 3.383 | 4.329 | 0.11 |
|  |  |  |  | 0.000 | 124.000 | 2" Ice | 3.859 | 4.857 | 0.17 |
|  | B | From Leg |  |  |  | 4" Ice | 4.811 | 5.913 | 0.29 |
| 1900 MHz RRH <br> (Sprint - Existing) |  |  | 4.000 |  |  | No Ice | 2.907 | 3.801 | 0.04 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 3.145 | 4.065 | 0.07 |
|  |  |  | 1.000 |  |  | $1{ }^{\prime \prime}$ Ice | 3.383 | 4.329 | 0.11 |
|  | C | From Leg |  | 0.000 | 124.000 | $2^{\prime \prime}$ Ice | 3.859 | 4.857 | 0.17 |
|  |  |  |  |  |  | 4" Ice | 4.811 | 5.913 | 0.29 |
| 1900 MHz RRH <br> (Sprint - Existing) |  |  | 4.000 |  |  | No Ice | 2.907 | 3.801 | 0.04 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.145 | 4.065 | 0.07 |
|  |  |  | 1.000 |  |  | 1 Ice | 3.383 | 4.329 | 0.11 |
|  | A | From Leg |  | 0.000 | 124.000 | $2^{\prime \prime}$ Ice | 3.859 | 4.857 | 0.17 |
| 800 MHz RRH <br> (Sprint - Existing) |  |  |  |  |  | 4" Ice | 4.811 | 5.913 | 0.29 |
|  |  |  | 4.000 |  |  | No Ice | 2.490 | 2.068 | 0.05 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 2.706 | 2.271 | 0.07 |
|  |  |  | 1.000 |  |  | $1^{\prime \prime}$ Ice | 2.922 | 2.474 | 0.10 |
|  | B | From Leg |  | 0.000 | 124.000 | $2^{\prime \prime}$ Ice | 3.354 | 2.880 | 0.14 |
| 800 MHz RRH (Sprint - Existing) |  |  |  |  |  | $4^{\prime \prime}$ Ice | 4.218 | 3.692 | 0.22 |
|  |  |  | 4.000 |  |  | No Ice | 2.490 | 2.068 | 0.05 |
|  |  |  | 0.000 |  |  | $1 / 2$ I' Ice | 2.706 | 2.271 | 0.07 |
|  |  |  | 1.000 |  |  | $1^{\prime \prime}$ Ice | 2.922 | 2.474 | 0.10 |
|  | C | From Leg |  | 0.000 | 124.000 | $2^{\prime \prime}$ Ice | 3.354 | 2.880 | 0.14 |
| 800 MHz RRH (Sprint - Existing) |  |  |  |  |  | 4 " Ice | 4.218 | 3.692 | 0.22 |
|  |  |  | 4.000 |  |  | No Ice | 2.490 | 2.068 | 0.05 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 2.706 | 2.271 | 0.07 |
|  |  |  | 1.000 |  |  | $1^{\prime \prime}$ Ice | 2.922 | 2.474 | 0.10 |
|  | A | From Leg |  | 0.000 | 124.000 | $2^{\prime \prime}$ Ice | 3.354 | 2.880 | 0.14 |
| 6' x 2" Mount Pipe (Sprint-Existing) |  |  |  |  |  | $4^{\prime \prime}$ Ice | 4.218 | 3.692 | 0.22 |
|  |  |  | 4.000 |  |  | No Ice | 1.425 | 1.425 | 0.02 |
|  |  |  | 6.500 |  |  | $1 / 2^{\prime \prime}$ Ice | 1.925 | 1.925 | 0.03 |
|  |  |  | 0.000 |  |  | 1 I' Ice | 2.294 | 2.294 | 0.05 |
|  | A | From Leg |  | 0.000 | 124.000 | 2 " Ice | 3.060 | 3.060 | 0.09 |
| $6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (Sprint - Existing) |  |  |  |  |  | 4 " Ice | 4.702 | 4.702 | 0.23 |
|  |  |  | 4.000 |  |  | No Ice | 1.425 | 1.425 | 0.02 |
|  |  |  | -6.500 |  |  | 1/2" Ice | 1.925 | 1.925 | 0.03 |
|  |  |  | 0.000 |  |  | 1 I' Ice | 2.294 | 2.294 | 0.05 |
|  | B | From Leg |  | 0.000 | 124.000 | 2" Ice | 3.060 | 3.060 | 0.09 |
| $6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (Sprint - Existing) |  |  |  |  |  | 4 " Ice | 4.702 | 4.702 | 0.23 |
|  |  |  | 4.000 |  |  | No Ice | 1.425 | 1.425 | 0.02 |
|  |  |  | 6.500 |  |  | 1/2" Ice | 1.925 | 1.925 | 0.03 |
|  |  |  | 0.000 |  |  | 1 I' Ice | 2.294 | 2.294 | 0.05 |
|  | B | From Leg |  | 0.000 | 124.000 | 2 " Ice | 3.060 | 3.060 | 0.09 |
| $6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (Sprint - Existing) |  |  |  |  |  | 4 Ice | 4.702 | 4.702 | 0.23 |
|  |  |  | 4.000 |  |  | No Ice | 1.425 | 1.425 | 0.02 |
|  |  |  | -6.500 |  |  | 1/2" Ice | 1.925 | 1.925 | 0.03 |
|  |  |  | 0.000 |  |  | 1 " Ice | 2.294 | 2.294 | 0.05 |
|  | C | From Leg |  | 0.000 | 124.000 | 2" Ice | 3.060 | 3.060 | 0.09 |
| $6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (Sprint - Existing) |  |  |  |  |  | 4" Ice | 4.702 | 4.702 | 0.23 |
|  |  |  | 4.000 |  |  | No Ice | 1.425 | 1.425 | 0.02 |
|  |  |  | 6.500 |  |  | 1/2" Ice | 1.925 | 1.925 | 0.03 |
|  |  |  | 0.000 |  |  | $1 "$ Ice | 2.294 | 2.294 | 0.05 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 3.060 | 3.060 | 0.09 |
|  |  |  |  |  |  | 4 " Ice | 4.702 | 4.702 | 0.23 |


| tnxTower <br> Black \& Veatch Corp. <br> 10950 Grandview Drive <br> Overland Park, KS 66210 <br> Phone: (913) 458-7245 <br> FAX: (913) 458-8136 | Job | 14635 Middleton SW | $\begin{aligned} & \text { Page } \\ & 10 \text { of } 12 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 176850 (14635TMOCT-S) | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:09:07 10/13/14 } \end{array}$ |
|  | Client | AT\&T | Designed by Brennan J. Sedlacek, E.I.T. |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment | Placement |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount Pipe (Verizon - Existing) |  |  | 6.500 |  |  | 1/2" Ice | 7.051 | 5.926 | 0.11 |
|  |  |  | 0.000 |  |  | 1" Ice | 7.557 | 6.670 | 0.17 |
|  |  |  |  |  |  | 2" Ice | 8.601 | 8.239 | 0.31 |
|  |  |  |  |  |  | 4" Ice | 10.811 | 11.590 | 0.71 |
| LNX-6513DS-VTM w/ Mount Pipe (Verizon - Existing) | B | From Leg | 4.000 | 30.000 | 110.000 | No Ice | 6.542 | 5.161 | 0.05 |
|  |  |  | 6.500 |  |  | $1 / 2^{\prime \prime}$ Ice | 7.051 | 5.926 | 0.11 |
|  |  |  | 0.000 |  |  | 1" Ice | 7.557 | 6.670 | 0.17 |
|  |  |  |  |  |  | 2" Ice | 8.601 | 8.239 | 0.31 |
|  |  |  |  |  |  | 4" Ice | 10.811 | 11.590 | 0.71 |
| LNX-6513DS-VTM w/ Mount Pipe (Verizon - Existing) | C | From Leg | 4.000 | 30.000 | 110.000 | No Ice | 6.542 | 5.161 | 0.05 |
|  |  |  | 6.500 |  |  | 1/2" Ice | 7.051 | 5.926 | 0.11 |
|  |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 7.557 | 6.670 | 0.17 |
|  |  |  |  |  |  | 2" Ice | 8.601 | 8.239 | 0.31 |
|  |  |  |  |  |  | 4" Ice | 10.811 | 11.590 | 0.71 |
| HBX-6516DS-VTM w/ Mount Pipe (Verizon - Existing) | A | From Leg | 4.000 | 30.000 | 110.000 | No Ice | 3.598 | 3.241 | 0.03 |
|  |  |  | -6.500 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.998 | 3.914 | 0.06 |
|  |  |  | 0.000 |  |  | 1 I' Ice | 4.435 | 4.564 | 0.10 |
|  |  |  |  |  |  | 2"Ice | 5.368 | 5.914 | 0.20 |
|  |  |  |  |  |  | 4" Ice | 7.361 | 8.877 | 0.50 |
| HBX-6516DS-VTM w/ Mount Pipe (Verizon - Existing) | B | From Leg | 4.000 | 30.000 | 110.000 | No Ice | 3.598 | 3.241 | 0.03 |
|  |  |  | -6.500 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.998 | 3.914 | 0.06 |
|  |  |  | 0.000 |  |  | 1" Ice | 4.435 | 4.564 | 0.10 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 5.368 | 5.914 | 0.20 |
|  |  |  |  |  |  | 4" Ice | 7.361 | 8.877 | 0.50 |
| $\begin{gathered} \text { HBX-6516DS-VTM w/ } \\ \text { Mount Pipe } \\ \text { (Verizon - Existing) } \end{gathered}$ | C | From Leg | 4.000 | 30.000 | 110.000 | No Ice | 3.598 | 3.241 | 0.03 |
|  |  |  | -6.500 |  |  | $1 / 2^{\prime \prime}$ Ice | 3.998 | 3.914 | 0.06 |
|  |  |  | 0.000 |  |  | 1 " Ice | 4.435 | 4.564 | 0.10 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 5.368 | 5.914 | 0.20 |
|  |  |  |  |  |  | 4" Ice | 7.361 | 8.877 | 0.50 |
| RRH2X40-AWS (Verizon - Existing) | A | From Leg | 4.000 | 0.000 | 110.000 | No Ice | 2.522 | 1.589 | 0.04 |
|  |  |  | 0.000 |  |  | $1 / 2^{\text {" }}$ Ice | 2.753 | 1.795 | 0.06 |
|  |  |  | 0.000 |  |  | 1 " Ice | 2.993 | 2.010 | 0.08 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 3.499 | 2.465 | 0.13 |
|  |  |  |  |  |  | 4 " Ice | 4.615 | 3.479 | 0.28 |
| RRH2X40-AWS (Verizon - Existing) | B | From Leg | 4.000 | 0.000 | 110.000 | No Ice | 2.522 | 1.589 | 0.04 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 2.753 | 1.795 | 0.06 |
|  |  |  | 0.000 |  |  | 1 " Ice | 2.993 | 2.010 | 0.08 |
|  |  |  |  |  |  | 2" Ice | 3.499 | 2.465 | 0.13 |
|  |  |  |  |  |  | 4" Ice | 4.615 | 3.479 | 0.28 |
| RRH2X40-AWS (Verizon - Existing) | C | From Leg | 4.000 | 0.000 | 110.000 | No Ice | 2.522 | 1.589 | 0.04 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 2.753 | 1.795 | 0.06 |
|  |  |  | 0.000 |  |  | 1" Ice | 2.993 | 2.010 | 0.08 |
|  |  |  |  |  |  | 2" Ice | 3.499 | 2.465 | 0.13 |
|  |  |  |  |  |  | $4^{\prime \prime}$ Ice | 4.615 | 3.479 | 0.28 |
| $\begin{aligned} & \text { DB-T1-6Z-8AB-0Z : } \\ & \text { Distribution Box } \\ & \text { (Verizon - Existing) } \end{aligned}$ | C | From Leg | 1.000 | 0.000 | 110.000 | No Ice | 5.600 | 2.333 | 0.04 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 5.915 | 2.558 | 0.08 |
|  |  |  | 0.000 |  |  | 1 " Ice | 6.240 | 2.791 | 0.12 |
|  |  |  |  |  |  | 2" Ice | 6.914 | 3.284 | 0.21 |
|  |  |  |  |  |  | 4" Ice | 8.365 | 4.373 | 0.45 |
| Side Arm Mount [SO 104-1] (Verizon - Existing) | A | None |  | 0.000 | 110.000 | No Ice | 1.510 | 0.670 | 0.10 |
|  |  |  |  |  |  | 1/2" Ice | 1.820 | 0.930 | 0.14 |
|  |  |  |  |  |  | 1 Ice | 2.130 | 1.190 | 0.18 |
|  |  |  |  |  |  | 2" Ice | 2.750 | 1.710 | 0.26 |
|  |  |  |  |  |  | 4 " Ice | 3.990 | 2.750 | 0.42 |
| Platform Mount [LP 1201-1] (Verizon - Existing) | A | None |  | 0.000 | 110.000 | No Ice | 23.100 | 23.100 | 2.10 |
|  |  |  |  |  |  | 1/2" Ice | 26.800 | 26.800 | 2.50 |
|  |  |  |  |  |  | 1 " Ice | 30.500 | 30.500 | 2.90 |


| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | 14635 Middleton SW | 12 of 12 |
| Black \& Veatch Corp. 10950 Grandview Drive | Project | 176850 (14635TMOCT-S) | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:09:07 10/13/14 } \end{array}$ |
| Overland Park, KS 66210 <br> Phone: (913) 458-7245 <br> FAX: (913) 458-8136 | Client | AT\&T | Designed by Brennan J. Sedlacek, E.I.T |


| Section <br> No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ K \end{gathered}$ | $\%$ Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L4 | 133-128 | Pole | TP27.601×26.7×0.25 | 4 | -7.33 | 129.12 | 39.9 | Pass |
| L5 | 128-123 | Pole | TP28.501×27.601x0.25 | 5 | -10.28 | 142.29 | 50.4 | Pass |
| L6 | 123-118 | Pole | TP29.401x28.501×0.25 | 6 | -10.85 | 156.33 | 59.8 | Pass |
| L7 | 118-111 | Pole | TP30.661×29.401×0.25 | 7 | -11.20 | 165.18 | 65.0 | Pass |
| L8 | 111-110 | Pole | TP30.341x29.441x0.25 | 8 | -12.10 | 171.96 | 75.8 | Pass |
| L9 | 110-105 | Pole | TP31.241x30.341x0.25 | 9 | -15.33 | 187.86 | 87.7 | Pass |
| L10 | 105-100 | Pole | TP32.142x31.241x0.25 | 10 | -16.06 | 204.71 | 97.0 | Pass |
| L11 | 100-99.3333 | Pole | TP32.262×32.142×0.25 | 11 | -16.16 | 207.03 | 98.1 | Pass |
| L12 | $\begin{gathered} 99.3333- \\ 99.0833 \end{gathered}$ | Pole | TP32.307x32.262×0.344 | 12 | -16.21 | 283.36 | 72.3 | Pass |
| L13 | $\begin{gathered} 99.0833- \\ 94.0833 \end{gathered}$ | Pole | TP33.207x32.307x0.344 | 13 | -17.07 | 307.99 | 78.4 | Pass |
| L14 | 94.0833-90.5 | Pole | TP33.852x33.207x0.344 | 14 | -17.70 | 326.49 | 82.4 | Pass |
| L15 | 90.5-90.25 | Pole | TP33.897x33.852x0.431 | 15 | -17.77 | 408.04 | 66.4 | Pass |
| L16 | 90.25-85.25 | Pole | TP34.797x33.897x0.425 | 16 | -19.03 | 435.69 | 71.9 | Pass |
| L17 | 85.25-80.25 | Pole | TP35.698x34.797x0.425 | 17 | -20.09 | 470.83 | 76.0 | Pass |
| L18 | 80.25-75 | Pole | TP36.643x35.698x0.425 | 18 | -20.21 | 474.45 | 76.4 | Pass |
| L19 | 75-74.75 | Pole | TP36.188×35.288x0.488 | 19 | -22.09 | 559.95 | 72.5 | Pass |
| L20 | 74.75-69.75 | Pole | TP37.088x36.188x0.475 | 20 | -23.30 | 588.52 | 77.5 | Pass |
| L21 | 69.75-64.75 | Pole | TP37.988×37.088×0.475 | 21 | -24.54 | 633.00 | 80.5 | Pass |
| L22 | 64.75-60.5 | Pole | TP38.753x37.988x0.469 | 22 | -25.61 | 664.01 | 83.9 | Pass |
| L23 | 60.5-60.25 | Pole | TP38.798x38.753x0.55 | 23 | -25.70 | 776.89 | 72.0 | Pass |
| L24 | 60.25-55.25 | Pole | TP39.699x38.798x0.55 | 24 | -27.10 | 833.04 | 74.3 | Pass |
| L25 | 55.25-50.25 | Pole | TP40.599x39.699x0.538 | 25 | -28.56 | 872.39 | 78.0 | Pass |
| L26 | 50.25-45.25 | Pole | TP41.499x40.599x0.538 | 26 | -30.05 | 932.52 | 80.0 | Pass |
| L27 | 45.25-39.75 | Pole | TP42.489x41.499x0.538 | 27 | -30.14 | 935.60 | 80.1 | Pass |
| L28 | 39.75-38.75 | Pole | TP42.044x40.919x0.6 | 28 | -33.26 | 1078.19 | 76.6 | Pass |
| L29 | 38.75-33.75 | Pole | TP42.944x $42.044 \times 0.588$ | 29 | -34.90 | 1127.02 | 79.7 | Pass |
| L30 | 33.75-30.5 | Pole | TP43.529x42.944x0.588 | 30 | -35.97 | 1174.37 | 80.6 | Pass |
| L31 | 30.5-30.25 | Pole | TP43.574x43.529x0.638 | 31 | -36.07 | 1273.87 | 74.6 | Pass |
| L32 | 30.25-25.25 | Pole | TP44.474x $43.574 \times 0.625$ | 32 | -37.81 | 1330.24 | 77.3 | Pass |
| L33 | 25.25-20.25 | Pole | TP45.374x $44.474 \times 0.625$ | 33 | -39.59 | 1413.85 | 78.4 | Pass |
| L34 | 20.25-15.25 | Pole | TP46.275x45.374x0.613 | 34 | -41.39 | 1472.09 | 81.1 | Pass |
| L35 | 15.25-10.25 | Pole | TP47.175x46.275x0.613 | 35 | -43.22 | 1560.86 | 82.1 | Pass |
| L36 | 10.25-5.25 | Pole | TP48.075x47.175x0.613 | 36 | -45.07 | 1653.16 | 83.0 | Pass |
| L37 | 5.25-0.25 | Pole | TP48.975x48.075×0.6 | 37 | -46.71 | 1714.64 | 85.6 | Pass |
| L38 | 0.25-0 | Pole | TP49.02x48.975 0.6 | 38 | -46.81 | 1719.44 | 85.6 | Pass |
|  |  |  |  |  |  | Pole (L11) RATING $=$ | $\begin{gathered} \text { Summary } \\ 98.1 \\ \mathbf{9 8 . 1} \end{gathered}$ | Pass Pass |

**Reinforced Tower Stresses are as follows:

| Pole <br> Section | Pole <br> Stress | Plate <br> Stress | Governing <br> Stress |
| :---: | :---: | :---: | :---: |
| L 1 | $59.1 \%$ | - | $59.1 \%$ |
| L 2 | $91.4 \%$ | $94.5 \%$ | $94.5 \%$ |
| L 3 | $80.3 \%$ | $93.8 \%$ | $93.8 \%$ |
| L 4 | $82.4 \%$ | $94.2 \%$ | $94.2 \%$ |

Program Version 6.1.4.1-3/21/2014 File:C:/Users/SED77779/Desktop/Projects/14635TMOCT-S.176850/structural/14635TMOCT-S Structural Analysis.eri

TNX Geometry Input

|  | Section Height ( ft ) |  |  | Section Length ( ft ) | Lap Splice Length (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Tapered Pole Grade | Weight <br> Multiplier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 148 | - | 143 | 5 |  | 18 | 24.000 | 24.900 | 0.25 | A607-65 | 1.000 |
| 2 | 143 | - | 138 | 5 |  | 18 | 24.900 | 25.800 | 0.25 | A607-65 | 1.000 |
| 3 | 138 | - | 133 | 5 |  | 18 | 25.800 | 26.700 | 0.25 | A607-65 | 1.000 |
| 4 | 133 | - | 128 | 5 |  | 18 | 26.700 | 27.601 | 0.25 | A607-65 | 1.000 |
| 5 | 128 | - | 123 | 5 |  | 18 | 27.601 | 28.501 | 0.25 | A607-65 | 1.000 |
| 6 | 123 | - | 118 | 5 |  | 18 | 28.501 | 29.401 | 0.25 | A607-65 | 1.000 |
| 7 | 118 | - | 115 | 7 | 4 | 18 | 29.401 | 30.661 | 0.25 | A607-65 | 1.000 |
| 8 | 115 | - | 110 | 5 |  | 18 | 29.441 | 30.341 | 0.25 | A607-65 | 1.000 |
| 9 | 110 | - | 105 | 5 |  | 18 | 30.341 | 31.241 | 0.25 | A607-65 | 1.000 |
| 10 | 105 | - | 100 | 5 |  | 18 | 31.241 | 32.142 | 0.25 | A607-65 | 1.000 |
| 11 | 100 | - | 99.3333 | 0.6667 |  | 18 | 32.142 | 32.262 | 0.25 | A607-65 | 1.000 |
| 12 | 99,3333 | - | 99.0833 | 0.25 |  | 18 | 32.262 | 32.307 | 0.34375 | A607-65 | 0.981 |
| 13 | 99.0833 | - | 94.0833 | 5 |  | 18 | 32.307 | 33.207 | 0.34375 | A607-65 | 0.974 |
| 14 | 94.0833 | - | 90.5 | 3.5833 |  | 18 | 33.207 | 33.852 | 0.34375 | A607-65 | 0.969 |
| 15 | 90.5 | - | 90.25 | 0.25 |  | 18 | 33.852 | 33.897 | 0.43125 | A607-65 | 0.953 |
| 16 | 90.25 | - | 85.25 | 5 |  | 18 | 33.897 | 34.797 | 0.425 | A607-65 | 0.957 |
| 17 | 85.25 | - | 80.25 | 5 |  | 18 | 34.797 | 35.698 | 0.425 | A607-65 | 0.947 |
| 18 | 80.25 | - | 79.75 | 5.25 | 4.75 | 18 | 35.698 | 36.643 | 0.425 | A607-65 | 0.946 |
| 19 | 79.75 | - | 74.75 | 5 |  | 18 | 35.288 | 36.188 | 0.4875 | A607-65 | 0.951 |
| 20 | 74.75 | - | 69.75 | 5 |  | 18 | 36.188 | 37.088 | 0.475 | A607-65 | 0.968 |
| 21 | 69.75 | - | 64.75 | 5 |  | 18 | 37.088 | 37.988 | 0.475 | A607-65 | 0.960 |
| 22 | 64.75 | - | 60.5 | 4.25 |  | 18 | 37.988 | 38.753 | 0.46875 | A607-65 | 0.967 |
| 23 | 60.5 | - | 60.25 | 0.25 |  | 18 | 38.753 | 38.798 | 0.55 | A607-65 | 0.952 |
| 24 | 60.25 | - | 55.25 | 5 |  | 18 | 38.798 | 39.699 | 0.55 | A607-65 | 0.943 |
| 25 | 55.25 | - | 50.25 | 5 |  | 18 | 39.699 | 40.599 | 0.5375 | A607-65 | 0.956 |
| 26 | 50.25 | - | 45.25 | 5 |  | 18 + | 40.599 | 41.499 | 0.5375 | A607-65 | 0.948 |
| 27 | 45.25 | - |  | 5.5 | 5.25 | 18 | 41.499 | 42.489 | 0.5375 | A607-65 | 0.948 |
| 28 | 45 | - | 38.75 | 6.25 |  | 18 | 40.919 | 42.044 | 0.6 | A607-65 | 0.950 |
| 29 | 38.75 | - | 33.75 | 5 |  | 18 | 42.044 | 42.944 | 0.5875 | A607-65 | 0.963 |
| 30 | 33.75 | - | 30.5 | 3.25 |  | 18 | 42.944 | 43.529 | 0.5875 | A607-65 | 0.959 |
| 31 | 30.5 | - | 30.25 | 0.25 |  | 18 | 43.529 | 43.574 | 0.6375 | A607-65 | 0.948 |
| 32 | 30.25 | - | 25.25 | 5 |  | 18 | 43.574 | 44.474 | 0.625 | A607-65 | 0.959 |
| 33 | 25.25 | - | 20.25 | 5 |  | 18 | 44.474 | 45.374 | 0.625 | A607-65 | 0.952 |
| 34 | 20.25 | - | 15.25 | 5 |  | 18 | 45.374 | 46.275 | 0.6125 | A607-65 | 0.964 |
| 35 | 15.25 | - | 10.25 | 5 |  | 18 | 46.275 | 47.175 | 0.6125 | A607-65 | 0.957 |
| 36 | 10.25 | - | 5.25 | 5 |  | 18 | 47.175 | 48.075 | 0.6125 | A607-65 | 0.951 |
| 37 | 5.25 | - | 0.25 | 5 |  | 18 | 48.075 | 48.975 | 0.6 | A607-65 | 0.964 |
| 38 | 0.25 | - | 0 | 0.25 |  | 18 | 48.975 | 49.020 | 0.6 | A607-65 | 0.964 |

## Analysis Results

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 148-143 | Pole | TP24.9x24x0.25 | Pole | 8.0\% | Pass |
| 143-138 | Pole | TP25.8×24.9x0.25 | Pole | 16.1\% | Pass |
| 138-133 | Pole | TP26.7×25.8×0.25 | Pole | 26.0\% | Pass |
| 133-128 | Pole | TP27.601×26.7×0.25 | Pole | 34.8\% | Pass |
| 128-123 | Pole | TP28.501×27.601×0.25 | Pole | 43.9\% | Pass |
| 123-118 | Pole | TP29.401×28.501×0.25 | Pole | 53.7\% | Pass |
| 118-115 | Pole | TP30.661×29.401x0.25 | Pole | 59.1\% | Pass |
| 115-110 | Pole | TP30.341x29.441×0.25 | Pole | 69.7\% | Pass |
| 110-105 | Pole | TP31.241×30.341x0.25 | Pole | 80.6\% | Pass |
| 105-100 | Pole | TP32.142×31.241×0.25 | Pole | 90.2\% | Pass |
| 100-99.33 | Pole | TP32.262×32.142x0.25 | Pole | 91.4\% | Pass |
| 99.33-99.08 | Pole + Reinf. | TP32.307x32.262x0.3438 | Reinf. 4 Tension Rupture | 80.8\% | Pass |
| 99.08-94.08 | Pole + Reinf | TP33.207×32.307×0.3438 | Reinf. 4 Tension Rupture | 89.0\% | Pass |
| 94.08-90.5 | Pole + Reinf | TP33.852×33.207×0.3438 | Reinf. 4 Tension Rupture | 94.5\% | Pass |
| 90.5-90.25 | Pole + Reinf. | TP33.897x33.852x0.4313 | Reinf. 3 Tension Rupture | 73.3\% | Pass |
| 90.25-85.25 | Pole + Reinf | TP34.797×33.897×0.425 | Reinf. 3 Tension Rupture | 79.4\% | Pass |
| 85.25-80.25 | Pole + Reinf. | TP35.698×34.797×0.425 | Reinf. 3 Tension Rupture | 85.0\% | Pass |
| 80.25-79.75 | Pole + Reinf. | TP36.643×35.698×0.425 | Reinf. 3 Tension Rupture | 85.9\% | Pass |
| 79.75-74.75 | Pole + Reinf. | TP36.188×35.288×0.4875 | Reinf. 3 Tension Rupture | 81.2\% | Pass |
| 74.75-69.75 | Pole + Reinf. | .TP37.088×36.188×0.475 | Reinf. 3 Tension Rupture | 85.7\% | Pass |
| 69.75-64.75 | Pole + Reinf. | TP37.988×37.088×0.475 | Reinf. 3 Tension Rupture | 90.3\% | Pass |
| 64.75-60.5 | Pole + Reinf | TP38.753×37.988×0.4688 | Reinf. 3 Tension Rupture | 93.4\% | Pass |
| 60.5-60.25 | Pole + Reinf. | TP38.798×38.753×0.55 | Reinf. 2 Tension Rupture | 77.7\% | Pass |
| 60.25-55.25 | Pole + Reinf. | TP39.699x38.798×0.55 | Reinf. 2 Tension Rupture | 82.0\% | Pass |
| 55.25-50.25 | Pole + Reinf. | TP40.599×39.699x0.5375 | Reinf. 2 Tension Rupture | 85.6\% | Pass |
| 50.25-45.25 | Pole + Reinf. | TP41.499×40.599×0.5375 | Reinf. 2 Tension Rupture | 88.8\% | Pass |
| 45.25-45 | Pole + Reinf. | TP42.489x41.499x0.5375 | Reinf. 2 Tension Rupture | 89.0\% | Pass |
| 45-38.75 | Pole + Reinf. | TP42.044×40.919x0.6 | Reinf. 2 Tension Rupture | 85.1\% | Pass |
| 38.75-33.75 | Pole + Reinf. | TP42.944×42.044×0.5875 | Reinf. 2 Tension Rupture | 87.6\% | Pass |
| $33.75-30.5$ | Pole + Reinf. | TP43.529×42.944×0.5875 | Reinf. 2 Tension Rupture | 89.1\% | Pass |
| 30.5-30.25 | Pole + Reinf. | TP43.574×43.529×0.6375 | Reinf. 1 Tension Rupture | 82.4\% | Pass |
| 30.25-25.25 | Pole + Reinf. | TP44.474×43.574×0.625 | Reinf. 1 Tension Rupture | 84.6\% | Pass |
| 25.25-20.25 | Pole + Reinf. | TP45.374×44.474×0.625 | Reinf. 1 Tension Rupture | 86.7\% | Pass |
| 20.25-15.25 | Pole + Reinf. | TP46.275×45.374×0.6125 | Reinf. 1 Tension Rupture | 88.7\% | Pass |
| 15.25-10.25 | Pole + Reinf | TP47.175×46.275×0.6125 | Reinf. 1 Tension Rupture | 90.6\% | Pass |
| 10.25-5.25 | Pole + Reinf. | TP48.075×47.175x0.6125 | Reinf. 1 Tension Rupture | 91.0\% | Pass |
| 5.25-0.25 | Pole + Reinf. | TP48.975 $48.075 \times 0.6$ | Reinf. 1 Tension Rupture | 94.2\% | Pass |
| 0.25-0 | Pole + Reinf. | TP49.02×48.975×0.6 | Reinf. 1 Tension Rupture | 94.2\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 91.4\% | Pass |
|  |  |  | Reinforcement | 94.5\% | Pass |
|  |  |  | Overall | 94.5\% | Pass |


(Bearing and Stability Checks) Tool for TIA Rev F or G - Application (MP, SST with unitbase)

Site Data
BU\#:
Site Name: Middletown SW
App \#:

| Enter Load Factors Below: |  |  |
| :---: | :---: | :---: |
| For P (DL) | 1.2 | <--- Enter Factor |
| For P,V, and M <br> $(\mathrm{WL})$ | 1.35 | <---- Enter Factor |


| Pad \& Pier Data |  |  |
| :---: | :---: | :---: |
| Base PL Dist. Above Pier: | 3 | in |
| Pier Dist. Above Grade: | 6 | in |
| Pad Bearing Depth, D: | 8 | ft |
| Pad Thickness, T: | 3 | ft |
| Pad Width=Length, L: | 22 | ft |
| Pier Cross Section Shape: | Round | <--Pull Down |
| Enter Pier Diameter: | 7 | ft |
| Concrete Density: | 150.0 | pcf |
| Pier Cross Section Area: | 38.48 | $\mathrm{ft}^{\wedge} 2$ |
| Pier Height: | 5.50 | ft |
| Soil (above pad) Height: | 5.00 | ft |


| Soil Parameters |  |  |
| ---: | :---: | :--- |
| Unit Weight, $\mathrm{y}:$ | 125.0 | pcf |
|  | 12.00 | ksf |
| Ultimate Bearing Capacity, qn: | 10.75 |  |
| Strength Reduct. factor, $\phi:$ | 0.75 |  |
| Angle of Friction, $\Phi:$ | 34.0 | degrees |
| Undrained Shear Strength, $\mathrm{Cu}:$ | 0.00 | ksf |
| Allowable Bearing: $\phi^{*} \mathrm{qn}:$ | 9.00 | ksf |
| Passive Pres. Coeff., Kp | 3.54 |  |


| Forces/Moments due to Wind and Lateral Soil |  |  |
| :---: | :---: | :---: |
| Minimum of ( $\varphi^{*}$ Ultimate Pad Passive Force, Vu): | 51.2 | kips <br> ft <br> ft-kips <br> ft-kips <br> ft-kips |
| Pad Force Location Above D: | 1.38 |  |
| $\phi$ (Passive Pressure Moment): | 70.85 |  |
| Factored O.T. M(WL), "1.6W": | 5764.7 |  |
| Factored OT (MW-Msoil), M1 | 5693.84 |  |


| Resistance due to Foundation Gravity |  |  |
| ---: | :---: | :--- |
| Soil Wedge Projection grade, a: | 3.37 | ft |
| Sum of Soil Wedges Wt: | 51.81 | kips |
| Soil Wedges ecc, K1: | 9.01 | ft |
| Ftg+Soil above Pad wt: | 528.0 | kips |
| Unfactored (Total ftg-soil Wt): | 579.80 | kips |
| 1.2D. No Soil Wedges. | 689.76 | kips |
| 0.9D. With Soil Wedges | 563.95 | kips |


| Resistance due to Cohesion (Vertical) |  |  |
| ---: | :---: | :--- |
| $\phi^{*}\left(1 / 2^{*} \mathrm{Cu}\right)($ Total Vert. Planes) | 0.00 | kips |
| Cohesion Force Eccentricity, K2 | 0.00 | ft |


| Monopole Base Reaction Forces |  |  |
| ---: | :---: | :---: |
| TIA Revision: | F | <--Pull Down |
| Unfactored DL Axial, PD: | 46.806 | kips |
| Unfactored WL Axial, PW: | 0 | kips |
| Unfactored WL Shear, V: | 37.905 | kips |
| Unfactored WL Moment, M: | 3938.478 | ft -kips |


| Load Factor | Shaft Factored Loads |  |  |
| :---: | ---: | :---: | :---: |
| 1.20 | $1.2 \mathrm{D}+1.6 \mathrm{~W}$, Pu: | 56.1672 |  |
| 0.90 | kips |  |  |
| 1.35 | Vu: | 51.17175 |  |
|  | Mu: | 5316.945 |  |

1.2D+1.6W Load Combination, Bearing Results:

| (No Soil Wedges) <br> [Reaction+Conc+Soil] | 689.76 | P1="1.2D $+1.6 \mathrm{~W} "$ <br> (Kips) |
| :---: | :---: | :---: |
| Factored "1.6W" Overturning <br> Moment (MW-Msoil), M1 | 5693.84 | ft-kips |

## Orthogonal Direction:

| ecc1 $=\mathrm{M} 1 / \mathrm{P} 1=$ | 8.25 | ft |
| ---: | :---: | :--- |
| Orthogonal qu | $=5.71$ | ksf |
| qu $/ \phi^{*}$ qn Ratio $=$ | $63.45 \%$ | Pass |

## Diagonal Direction:

$$
\begin{array}{rccl}
\text { ecc2 }=(0.707 \mathrm{M} 1) / \mathrm{P} 1 & = & 5.84 & \mathrm{ft} \\
\text { Diagonal qu } & =6.47 & \mathrm{ksf} \\
\text { qu } / \phi^{*} \text { qn Ratio } & = & 71.85 \% & \text { Pass }
\end{array}
$$

Run <-- Press Upon Completing All Input

0.9D+1.6W Load Combination, Bearing Results:

| (w/ Soil Wedges) <br> [Reaction+Conc+Soil] | 563.95 | $\mathrm{P} 2=" 0.9 \mathrm{D}+1.6 \mathrm{W"}$ |
| :---: | :---: | :---: |
| (Kips) |  |  |$|$| Factored "1.6W" Overturning |
| :---: |
| Moment (MW-Msoil)-0.9(M of <br> Wedge + M of Cohesion), M2 |
| 5273.86 |
| ft-kips |


| Orthogonal ecc3 $=\mathrm{M} 2 / \mathrm{P} 2$ | $=$ | 9.35 |
| :---: | :---: | :---: |
| ft |  |  |
| Ortho Non Bearing Length, NBL $=$ | 18.70 | ft |

Orthogonal qu= 7.78 ksf
Diagonal qu= 7.32 ksf
Max Reaction Moment (ft-kips) so that qu $=\varphi^{*} \mathrm{qn}=100 \%$ Capacity Rating

| Actual M: | 3938.48 |  |  |
| ---: | :---: | :---: | :---: |
| M Orthogonal: | 4041.09 | $\mathbf{9 7 . 4 6 \%}$ | Pass |
| M Diagonal: | 4041.09 | $\mathbf{9 7 . 4 6 \%}$ | Pass |


| Dimensional Solutions Mat3D |  | Version | $\mathbf{6 . 0 . 0}$ |  |
| :--- | :--- | :--- | :--- | :--- |
| Foundation Name | Middletown SW |  | Date | 10/13/2014 |
| Designed By: | Black \& Veatch Corp. | Engineer |  | B. Sedlacek |
|  |  |  |  |  |
| Cilename: |  |  |  |  |

## DETAIL REPORT <br> UNFACTORED (ALLOWABLE) LOAD COMBINATIONS

| pier |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Load Comb | Axial (kips) | Shear X (kips) | Mom Z <br> (kip ft) | Shear Z <br> (kips) | Mom X (kip ft) |
| 1 - Dead | 46.81 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2-Dead + Wind | 46.81 | 37.91 | 3938.48 | 0.00 | 0.00 |
| FACTORED (ULTIMATE) LOAD COMBINATIONS |  |  |  |  |  |
| pier |  |  |  |  |  |
| Load <br> Comb | Axial <br> (kips) | Shear X (kips) | Mom Z <br> (kip ft) | Shear $Z$ <br> (kips) | Mom X (kip ft) |
| 1-1.4Dead | 65.53 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2-1.2Dead + 1.6Wind | 56.17 | 60.65 | 6301.57 | 0.00 | 0.00 |
| 3-0.9Dead + 1.6Wind | 42.13 | 60.65 | 6301.57 | 0.00 | 0.00 |

## FOOTING DESIGN INFORMATION

| $X \operatorname{Dim}(\mathrm{ft})$ | 22.00 |
| :--- | ---: |
| $Z \operatorname{Dim}(\mathrm{ft})$ | 22.00 |
| Thickness (ft) | 3.00 |

Top Steel

| Governing Combination | No of Bars | $\begin{gathered} \text { Bar } \\ \text { Size } \end{gathered}$ | Bar <br> Spac <br> (in) | Area Prov $(\mathrm{sq} \mathrm{in} / \mathrm{tt})$ | $\begin{array}{r} \text { Area } \\ \text { Req } \\ (\mathrm{sq} \mathrm{in} / \mathrm{ft}) \end{array}$ | Moment <br> (kip ft/ft) | Direction |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2. 1.2Dead + 1.6Wind | 22 | 11 | 12 | 1.56 | 0.35 | -38.38 | X |
| 3. $0.9 \mathrm{Dead}+1.6 \mathrm{Wind}$ | 22 | 11 | 12 | 1.56 | 0 | 0 | Z |
|  |  |  |  | $\mathrm{SR}=$ | 22.4 |  |  |
|  |  |  |  | $\mathrm{SR}=$ | 0 |  |  |
|  | Bottom Steel |  |  |  |  |  |  |
| Governing | No of | Bar | Bar | Area | Area | Moment | Direction |
| Combination | Bars | Size | Spac | Prov | Req |  |  |
|  |  |  | (in) | (sq in/ft) | (sq in/ft) | (kip ft/ft) |  |
| 3. 0.9Dead + 1.6Wind | 22 | 11 | 12 | 1.56 | 1.5 | 208.15 | X |
| 1. 1.4Dead | 22 | 11 | 12 | 1.56 | 0.39 | 7.09 | Z |
|  |  |  |  | SR= | 96.2 |  |  |
|  |  |  |  | SR= | 25 |  |  |


| Dimensional Solutions Mat3D | Viddletown SW | Version | 6.0 .0 | Date |
| :--- | :--- | :--- | :--- | :--- |
| Foundation Name | Black \& Veatch Corp. | Engineer |  | Time |
| Designed By: |  |  | B. Sedlacek | Checker |
|  |  |  |  |  |
| Filename: |  |  |  |  |

## DETAIL REPORT

## PIER ULTIMATE LOAD CAPACITIES




# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility

Site ID: CT11056J
ATT Middletown
290 Preston Avenue
Middletown, CT 06457
November 14, 2014
EBI Project Number: 62146124

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general public <br> allowable limit: | $64.40 \%$ |

November 14, 2014

T-Mobile USA<br>Attn: Jason Overbey, RF Manager<br>35 Griffin Road South<br>Bloomfield, CT 06002

## Emissions Analysis for Site: CT11056J - ATT Middletown

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 290 Preston Avenue, Middletown, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limit for the 700 MHz Band is $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the PCS and AWS bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 290 Preston Avenue, Middletown, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
2) 2 UMTS channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 1 LTE channel ( 700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 W atts.
5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antennas used in this modeling are the Ericsson AIR21 B4A/B2P for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the Commscope LNX-6515DS-VTM for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The Ericsson AIR21 B4A/B2P has a maximum gain of $\mathbf{1 5 . 9} \mathbf{~ d B d}$ at its main lobe. The Commscope LNX-6515DS-VTM has a maximum gain of $\mathbf{1 4 . 6} \mathbf{d B d}$ at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antenna mounting height centerline of the proposed antennas is $\mathbf{1 4 0}$ feet above ground level (AGL).
9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

## EBI Consulting

environmental | engineering | due diligence

T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | 1 | Antenna \#: | 1 | Antenna \#: | 1 |
| Make / Model: | $\begin{gathered} \text { Ericsson ALR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson ATR21 } \\ \text { B4A/B2P } \end{gathered}$ | Make / Model: | Ericsson AIR21 B4A/B2P |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 140 | Height (AGL) : | 140 | Height (AGL): | 140 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz}(\mathrm{AWS}) \\ & \hline \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\text { PCS }) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 2 | Channel Count | 2 | \# PCS Channels: | 2 |
| Total TX Power: | 120 | Total TX Power: | 120 | \# AWS Channels: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna A1 MPE\% | 0.93 | Antenna B1 MPE\% | 0.93 | Antenna Cl MPE\% | 0.93 |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson A/R21 } \\ \text { B4A/B2P } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AlR21 } \\ \text { B4A/B2P } \\ \hline \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 140 | Height (AGL): | 140 | Height (AGL): | 140 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 4 | Channel Count | 4 | Channel Count | 4 |
| Total TX Power: | 120 | Total TX Power: | 120 | Total TX Power: | 120 |
| ERP (W): | 1,906.06 | ERP (W): | 1,906.06 | ERP (W): | 1,906.06 |
| Antenna A2 MPE\% | 0.93 | Antenna B2 MPE\% | 0.93 | Antenna C2 MPE\% | 0.93 |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna \#: | 3 |
| Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX- 6515DS-VTM |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 140 | Height (AGL) | 140 | Height (AGL): | 140 |
| Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz | Frequency Bands | 700 Mhz |
| Channel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power. | 30 | Total TX Power: | 30 |
| ERP (W): | 445.37 | ERP (W): | 445.37 | ERP (W): | 445.37 |
| Antenna A3 MPE\% | 0.37 | Antenna B3 MPE\% | 0.37 | Antenna C3 MPE\% | 0.37 |
|  | Site Composite MPE\% |  |  | T-Mobile Sector 1 Total: | : $\quad 2.24 \%$ |
|  | Carrier | MPE\% |  | T-Mobile Sector 2 T | : $\quad 2.24 \%$ |
|  | T-Mobile | 6.72 |  | T-Mobile Sector 3 T | : $2.24 \%$ |
|  | Sprint | 4.77 \% |  | Site Total: | : $64.40 \%$ |

environmental | engineering | due diligence

## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector 1: | $2.24 \%$ |
| Sector 2: | $2.24 \%$ |
| Sector 3: | $2.24 \%$ |
| T-Mobile Total: | $6.72 \%$ |
|  |  |
| Site Total: | $64.40 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{6 4 . 4 0 \%}$ of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


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