56 Prospect Street,
P.O. Box 270

Hartford, CT 06103

Kathleen M. Shanley Manager - Transmission Siting Tel: (860) 728-4527

July 22, 2020

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification <br> Eversource Site Meriden Cooper St. <br> 56 Cooper Street, Meriden, CT 06451 <br> Latitude: 41-31-57.1 N / Longitude: 72-48-21.4 W

Dear Ms. Bachman:

The Connecticut Light and Power Company doing business as Eversource Energy ("Eversource") currently maintains multiple antennas at various mounting heights on an existing building located at 56 Cooper Street in Meriden, CT. See Attachment A, Parcel Map and Property Card. The building and property are owned by Eversource. Eversource plans to install one 24-foot 3-inch tall omni-directional antenna on the existing penthouse wall; the top of the antenna will extend to approximately 67 feet above ground level ("AGL"). Two 7/8-inch diameter coaxial cables will be routed from the antenna into the existing building where it will terminate in an existing communications room. There will be no ground disturbance and no changes to the building or the existing antennas and equipment. The existing and proposed antennas on the building are depicted on Attachment B, Construction Drawings, dated March 30, 2020.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies ("R.C.S.A.") §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this notice is being delivered to Kevin Scarpati, Mayor of the City of Meriden and Renata Bertotti, Director of Planning, Development \& Enforcement for the City of Meriden via the United States Postal Service or private carrier. Proof of delivery is attached. See Attachment C, Proof of Delivery of Notice.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2):

1. There will be no change to the height of the existing building; an existing omni-directional antenna extends to 60'-11" AGL; the proposed omni-directional antenna will extend to 67'-0" AGL.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antenna will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard as shown in the attached Radio Frequency Emissions Report, dated March 6, 2020 (Attachment D - Power Density Report) ${ }^{1}$.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading as shown in the attached Structural Analysis, dated March 26, 2020 (Attachment E - Structural Analysis).

For the foregoing reasons, Eversource respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Two copies of this notice and a check in the amount of $\$ 625$ are enclosed.

Communications regarding this Notice of Exempt Modification should be directed to Kathleen Shanley at (860) 728-4527.

## By:



Kathleen M. Shanley
Manager - Transmission Siting
cc: Honorable Kevin Scarpati, Mayor, City of Meriden
Renata Bertotti, Director of Planning, Development \& Enforcement, City of Meriden

Attachments
A. Parcel Map and Property Card
B. Construction Drawings
C. Proof of Delivery of Notice
D. Power Density Report
E. Structural Analysis

[^0]ATTACHMENT A - PARCEL MAP AND PROPERTY CARD


| OWNER <br> INFORMATION | Owner(s): <br> YANKEE GAS SERVICES CO | Owner Address: |  |
| :--- | :--- | :--- | :--- |
|  | P O BOX 270 |  |  |
|  | C/O PROPERTY TAX DEPT | HARTFORD, CT 06141 |  |



Sub Area

## Summary

> No Sub Area data found

Special Features

No Special Features found.
$\left.\begin{array}{|c|c|c|c|c|c|c|c|c|}\hline \begin{array}{c}\text { Land } \\ \text { Appraised }\end{array} & \begin{array}{c}\text { Building } \\ \text { Appraised }\end{array} & \begin{array}{c}\text { Yard } \\ \text { Appraised }\end{array} & \begin{array}{c}\text { Total } \\ \text { Appraised } \\ \text { Value }\end{array} & \begin{array}{c}\text { Land } \\ \text { Assessed }\end{array} & \begin{array}{c}\text { Building } \\ \text { Assessed }\end{array} & \begin{array}{c}\text { Yard } \\ \text { Assessed }\end{array} & \begin{array}{c}\text { Special } \\ \begin{array}{c}\text { Total } \\ \text { Vand } \\ \text { Value }\end{array} \\ \hline \$ 1,751,200\end{array} \$ 2,059,300 & \$ 625,300 \\ \hline \text { Assessed } \\ \text { Value }\end{array}\right]$

Previous Year: 2018

| Land <br> Value | Building <br> Value | Yard <br> Items | Appraised <br> Value | Land <br> Value | Building <br> Value | Yard <br> Items | Assessed <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\$ 1,749,800$ | $\$ 2,057,800$ | $\$ 625,300$ | $\$ 4,432,900$ | $\$ 1,224,860$ | $\$ 1,440,460$ | $\$ 437,710$ | $\$ 3,103,030$ |


| LAND |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| INFORMATION | Land Use | Zoning | Land Area | Neighborhood Description |  |  |
|  | Comm Bldg | M-3 | 10.46919 | INNER CITY AREA |  |  |

*Confirm zoning with Planning Office.
Zoning_map_is the official document to determine zone.

| SALES <br> INFORMATION | Sale Date | Sale Price | Book | Page | Grantor | Grantee | Deed Type |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $6 / 30 / 1989$ | $\$ 0$ | 1646 | 11 |  |  |  |

ASSESSOR'S PERMIT HISTORY
No data found.

PROPERTY IMAGES



909
0113-0059-0001-0010
1

ATTACHMENT B - CONSTRUCTION DRAWINGS

## EVERS=URCE <br> ENERGY




| CONTACT INFORMATION |  |
| :---: | :---: |
|  107 SELDEN SIREET BERLN, CT O6037 | POWER PROVIER: EVERSOURCE ENERGY (800) 286-2000 |
|  | TELCO PROVIDER: (800) 921-8102 |
| EVERSOURCE ENERGY NIKOLL PRECI <br> 60) 655-3079 |  |

## MERIDEN 56 COOPER STREET MERIDEN, CT 06451

| Project no: | 403093 |
| :---: | :---: |
| DRamm Br: | ${ }^{\text {cta }}$ |

CHECKED BY:

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DO NOT SCALE DRAWINGS
MERIDEN
56 COOPER STREE
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TITLE SHEET

| SHEET NUMBER |
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DETAIL A

107 SELDEN STRET
BERLNET 0 O63T
PHONE: ( 800 ) $286-2000$
a
BLACK \& VEATCH

OVERLAND PARK, KS 66211
PHONE: (913) 458-3595


MERIDEN
56 COOPER STREE
MERIDEN, CT 0645

SHEET TTILE
STRUCTURAL DETAILS


## DESIGN BASIS

Governing cooe: 2018 Connecticut state bullong cooe (2015 IBC basis)

## GENERAL CONDITIONS





detals ncluoed in this plan set are trical and apply to smiar conotions.


8. THE CONTRACTOR SHALL SAFEGURD AGANST: CREATMG A FRE HAZARO, AFFECTMG TENANT EGRESS
9. THE CONTRACTOR SHALL REMOVE ALL DEERRS AND CONSTRUCTON WASTE FROM THE STE EACH DAY.
10. THE Contractor's hours of work shall ge in accordance wit local codes and


THERMAL \& MOISTURE PROTECTION


 HDERWERIRSS LABORACORES (LL) STSIEM NUMBER
3. Firesioppng shall be appled as soon as practicable after pentiratons are made and



6. ALL PENETRATONS

contractor to remuve and re-INSTALL AlL fire proofing as reaured during
construction.

## SUBMITTALS

contractor to subut shop drawngs to enginer for revew prior to fabricaton.
2. Contractor to notif engineer for inspection prior to closng penetrations.

4. ALL STEEL MATERAL EXPOSED To WEATER SHALL BE GALVANZED ATER FAARRCATON IN


2. DAMAGED GALVANIZD SURFACES SHALL BE CleANED WTH A WRE BRUSH AND PANTED WTH TWO

3. DESIIN, FABRICATON AND ERECTON OF

5. All steel elements shall be installed plumb and level
6. Tower manufactuerr's desions shall preval for tower.

CONNECTIONS

Design connectons at beam ons ior io
3. all bulloing connection ponins are to be centered over bearng walls

5. nut locking devices are regured for all bolt assembles.


 L BE REPARED. SEE NOTE ABOVE.

10. ALI ARC AND GAS WELING SHALL BE DONE BY LICENSED ANO CEETIFED WELOER IN ACCORDANCE
 12. USE Precautions and proceoures per aws 01.1 when welong galvanized metals.

## ANCHOR

XPPNSION ACCHORS SHALL BE UEED WHERE ATACHING TO CONCRETE. MASONRY MOUNTS SHAL
2. Exadnsion bolts shall be hiti kwi bolt 3 or approved equal. minmum embedment shal

BRICK wITH Holess:
SPACE ANCHORS

minom



ANCHORS SHALL RE ENSTALLED PER MANUFACTURER'S RECOMMENDATONS AND SHALL NOT BE
NSTTLLLE N MORTAR JONTS.


## SITE GENERAL









6. Coniracion is responsile for repainng or replaing structures or utlites damage




$F$

## BLACK \& VEATCH


OVERLAND PARK, KS 6621
PHONE: (913) 488-3595

|  | Ject No: |  | 403093 |
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|  | CkED BY: |  | JR |
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MERIDEN 56 COOPER STREET
shet mer
\& SPECIFICATIONS

## ELECTRICAL





4. ALL ELECTRCCAL CONOUCTors shall be $100 \%$ COPPER AND SHALL HAVE TPPE THHN INSULATION




9. Condut ANo caale witin corriors shall ee concealeo and exposed elsewtere, unless







15. ALL conouctor ends shall be tagged and electrical equipment labeled wth engraved
16. CONTtactor is responsible for all control wring and allarm tie-ns.

## GROUNDING

\#G THWN Shal be strandoe \#g copper with green thwn insulaton sutable for wet
NStalations.
2. \#2 THWN SHALL BE STRANDED \#2 COPPER WTH THWN INSULATION SUTABELE FOR WET
3. \#2 bare tined shall ee solid copper tineed. all buried wie shall meet this crtera.






9. ALL Connectons to the ground ring shall be exothermi welo.
10. BoND HEE FENCE TO THE GRound RNG AT EACH CORNER, AND AT EACH GATE POST WTH \# \#

12. FERRROUS METAL CLIPS WHICH COMPLETELY SURROUND THE GRounong conouctor SHALL bE

14. Mge ground connecton shall be exothermi weloed to the ground srstem.
15. ALL CABEE TRAY AND/OR PLATFORM STEEL SHALL BE BONDED TOGETHER WTH UUMPERS (\#6 IN

## CABLE TRAY

CaBEE TRAY SHALL
RESSITAT F FIISH.
2. Cable tray shall be of ladoer tray ippe wit flat cover clamped to side ralls.
3. CABLE LADOER SHALLL BE SIZED to FIT ALL CABLES IN ACCORD WTH NEC ANO NEMA 11-15-84.
. Cable ladoer trays shall be nema class 12 A ey pw inoustres, inc or equal.
5. CABLE LAODER TRAY Shall be supporied in accordance wit manufacturer's specifcations.
6. ALL WORKMANSHP SHALL CONFORM TO THEEE REOUREMENTS AND ALL LOCAL CODES AND

## ANTENNA \& CABLE NOTES


 AND Yerir All of the M.
2. ATER NSTAALLTONN THE TRANMMSSON INE SYSTEM SHALL BE PMM SMEEP TESTED FOR PROPER
3. ANEENA CABEES SHALL BE COLOR COOED AT THE FOLLOWNG LOCATONS:

- AT THE WNEGUSE ENRY PLATE ON BoTH SIES OF THE EQUPMENT SHELITR WALL
JUMPER CABELES AT THE EQUIPMENT ENTER.

4. SYTEM NSTALATOTON.


- ALL CONECCTORS. ASSOCATEE CABEE MOUNTNG, AND GROUNONG HAROWARE
- WAAL L NOUHTS, STANOOFFS. AND ASSOCATEE HARODNARE.

5. MNIMUM BENOING RADUS FOR COAXALL CABLES:
$7 / 8$ INCHMHNMN RMI 15 INCHES
$15 / 8$ NCH, RMIN $=25$ NCHES
6. CABEE SHAL BE MSTALLD WTH AMNMUM NUMBER OF BENOS WHER POSSBLEE CABLE SHAL all cable connectons outside shall be covered wit waterproof splicing ki.
7. CONTRACTOR SHALL VERIT EXACT LENGTH AND DRECTON OF TRAVEL IN FIELD PRIOR TO

Cable shall be furnshed without splices ano wit connectors at fach en


## Fr <br> BLACK \& VEATCH



| PRouect no: |  |  | 403093 |
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| CHECKED BY: |  |  | JR |
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MERIDEN 6 COOPER STREE MERIDEN, CT 0645


## REFERENCE CUTSHEETS

## VHF Omni Antennas (160-222 MHz)

| Model Number |  | 160-174 MHz |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
|  | Input Connector | N(F) | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | N(F) | $\begin{array}{r} 7 / 16 \\ \text { DIN } \end{array}$ | $N(F)$ | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ |
|  | Type | Single |  | Single |  | Dual |  |
| $\begin{aligned} & \frac{1}{d} \\ & \frac{0}{d x} \\ & \frac{1}{6} \\ & \text { 피 } \end{aligned}$ | Bandwidth, MHz | 14 |  | 14 |  | 14 |  |
|  | Power, Watts | 500 |  | 500 |  | 350 |  |
|  | Gain, dBd | 3 |  | 6 |  | 3 |  |
|  | Horizontal Beamwidth, degrees | 360 |  | 360 |  | 360 |  |
|  | Vertical Beamwidth, degrees | 30 |  | 16 |  | 30 |  |
|  | Beam Tilt, degrees | 0 |  | 0 |  | 0 |  |
|  | Isolation (minimum), dB | N/A |  | N/A |  | 30 |  |
|  | Number of Connectors | 1 |  | 1 |  | 2 |  |
|  | Flat Plate Area, $\mathrm{ft}^{2}\left(\mathrm{~m}^{2}\right)$ | 2.53 (0.24) |  | 4.38 (0.41) |  | 4.5 (0.42) |  |
|  | Lateral Windload Thrust, Ibf(N) | 95 (423) |  | 164 (730) |  | 169 (752) |  |
|  | Survival Wind Speed without ice, $\mathrm{mph}(\mathrm{kph})$ with $0.5^{\prime \prime}$ radial ice, $\mathrm{mph}(\mathrm{kph})$ | $\begin{aligned} & 110(177) \\ & 93(150) \\ & \hline \end{aligned}$ |  | $\begin{gathered} 75(121) \\ 60(97) \end{gathered}$ |  | $\begin{aligned} & 75(121) \\ & 65(105) \end{aligned}$ |  |
|  | Mounting Hardware included | DSH3V3R |  | DSH3V3N |  | DSH3V3N |  |
|  | Length, ft(m) | 12.7 (3.9) |  | 21.9 (6.7) |  | 22.3 (6.8) |  |
|  | Radome O.D., in(cm) | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  |
|  | Mast O.D., in(cm) | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  |
|  | Net Weight w/o bracket, lb(kg) | 37 (16.8) |  | $60 \text { (27.2) }$ |  | $63 \text { (28.6) }$ |  |
|  | Shipping Weight, lb(kg) | $67 \text { (30.4) }$ |  | $90 \text { (40.8) }$ |  | 93 (42.2) |  |


| 217-222 MHz |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { z } \\ & \text { ì } \\ & \text { N} \\ & \text { M } \\ & \text { U } \\ & \text { Nin } \end{aligned}$ |  |
| $\begin{array}{l\|l} \hline \text { N(F) } & \begin{array}{c} 7 / 16 \\ \text { DIN } \end{array} \end{array}$ | $\begin{array}{l\|l} \hline \text { N(F) } & \begin{array}{c} 7 / 16 \\ \text { DIN } \end{array} \end{array}$ | $\begin{array}{l\|l} \hline \text { N(F) } & \begin{array}{c} 7 / 16 \\ \text { DIN } \end{array} \end{array}$ | $\begin{array}{l\|l} \hline \text { N(F) } & \begin{array}{c} 7 / 16 \\ \text { DIN } \end{array} \end{array}$ | $N(F)$ | $\begin{aligned} & \hline 7 / 16 \\ & \text { DIN } \end{aligned}$ |
| Single | Single | Single | Dual | Dual |  |
| 5 | 5 | 5 | 5 | 5 |  |
| 500 | 500 | 500 | 350 | 350 |  |
| 0 | 3 | 6 | 0 | 3 |  |
| 360 | 360 | 360 | 360 | 360 |  |
| 60 | 30 | 16 | 60 | 30 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| N/A | N/A | N/A | 30 | 30 |  |
| 1 | 1 | 1 | 2 | 2 |  |
| 1.9 (0.18) | 1.9 (0.18) | 2.58 (0.24) | 2.4 (0.22) | 4.1 (0.38) |  |
| 53 (236) | 69 (307) | 108 (480) | 90 (400) | 169 (752) |  |
| $\begin{aligned} & 222(357) \\ & 193 \text { (311) } \end{aligned}$ | $\begin{aligned} & 172(277) \\ & 150(241) \end{aligned}$ | 110 (177) | 130 (209) | 75 (121) |  |
|  |  | 96 (154) | 115 (185) | 65 |  |
| DSH2V3R | DSH2V3R | DSH3V3N | DSH3V3R | DSH3V3N |  |
| 7.7 (2.3) | 9.9 (3) | 18.1 (5.5) | 13.6 (4.1) | 24.3 (7.4) |  |
| 3 (7.6) | 3 (7.6) | 3 (7.6) | 3 (7.6) | 3 (7.6) |  |
| 2.5 (6.4) | 2.5 (6.4) | 2.5 (6.4) | 2.5 (6.4) | 2.5 (6.4) |  |
| 19 (8.6) | 26 (11.8) | 47 (21.3) | 40 (18.1) | 70 (31.8) |  |
| 39 (17.7) | 56 (25.4) | 77 (34.9) | 70 (31.8) | 100 (45.4) |  |






## Product Classification

## Dimensions

| Height | $203.2 \mathrm{~mm} \mid 8.0 \mathrm{in}$ |
| :--- | :--- |
| Length | $152.4 \mathrm{~mm} \mid 6.0 \mathrm{in}$ |
| Pipe Outer Diameter | $23 / 8 \mathrm{in} \mathrm{\mid} \mathrm{2} \mathrm{7/8} \mathrm{in} \mathrm{\mid} 31 / 2 \mathrm{in} \mathrm{\mid} 41 / 2 \mathrm{in}$ |
| Weight | $20.6 \mathrm{~kg} \mathrm{\mid} 45.5 \mathrm{lb}$ |
| Width | $203.2 \mathrm{~mm} \mid 8.0 \mathrm{in}$ |

## Environmental Specifications

Wind Rating
For Specifications, please contact steelproducts@commscope.com or call 800-255-1479

## General Specifications

Mounting
Includes
Material Type
Package Quantity
Stand-off Distance

Solid walls
Backing plates or anchors | Wall brackets (2)
Hot dip galvanized steel
2
152.4 mm | 6.0 in

## Outline Drawing

Regulatory Compliance/Certifications

Agency
ISO 9001:2015

## Classification

Designed, manufactured and/or distributed under this quality management system

| PARTS LIST |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITEM | QTY | PART NO. | PART DESCRIPTION | LENGTH | UNIT WT. | NET WT. |  |  |
| 1 | 1 | SP1586 | WALL MOUNT BRACKET FOR 4 RUNS OF COAX | $111 / 4$ in | 2.81 | 2.81 |  |  |





A valmont $\boldsymbol{F}$ COMPANY

## MonoBloc Stackable Snap-In Hangers (SIC1, SIC2, SIC3, SIC4)



## Features:

- Allows cable attachment without the need for hardware
- One-hand mounting
-Stack up to four $1 / 2$ ", $7 / 8$ " or $1-1 / 4$ " cables or three $1-5 / 8$ " cables


## Construction:

- 301 stainless steel


## Design Criteria:

- Can be used outdoors or indoors

| Part \# | AT\&T | Cable Size | U of $\mathbf{M}$ | A | B | H |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| SIC1 | CEQ.11469 | $1 / 2^{\prime \prime}$ | 10 pack | $1-1 / 4^{\prime \prime}$ | $1-9 / 16^{\prime \prime}$ | $1-1 / 2^{\prime \prime}$ |
| SIC2 | ANT.13860 | $7 / 8^{\prime \prime}$ | 10 pack | $1-1 / 4^{\prime \prime}$ | $1-9 / 16^{\prime \prime}$ | $1-1 / 2^{\prime \prime}$ |
| SIC3 | ANT.13859 | $1-1 / 4^{\prime \prime}$ | 10 pack | $2-1 / 4^{\prime \prime}$ | $1-3 / 4^{\prime \prime}$ | $2-5 / 8^{\prime \prime}$ |
| SIC4 | ANT.12719 | $1-5 / 8^{\prime \prime}$ | 10 pack | $2-1 / 4^{\prime \prime}$ | $1-3 / 4^{\prime \prime}$ | $2-5 / 8^{\prime \prime}$ |



ATTACHMENT C - STRUCTURAL ANALYSIS REPORT

# STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL 

MERIDEN COOPER ST.<br>46 COOPER ST.<br>MERIDEN, CT 06451

B\&V PROJECT NO. 403093.2000.2200
PROJECT NAME: LMR EPC PHASE 1.5

PREPARED FOR

# EVERS $=$ URCE ENERGY 

## 107 SELDEN STREET

 BERLIN, CT 06037BLACK \& VEATCH CORPORATION
6800 WEST 115TH ST, SUITE 2292
OVERLAND PARK, KANSAS 66211

March 26, 2020


| Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :--- | :--- | ---: | ---: |
| Site Name: | MERIDEN COOPER ST. | Date: | $2 / 21 / 2020$ |
| Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
|  | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT | Date: | $2 / 21 / 2020$ |
|  | AND PENTHOUSE WALL |  |  |

## TABLE OF CONTENTS

1. PURPOSE
2. REFERENCES
3. ASSUMPTIONS
4. CONCLUSION
5. ANALYSIS \& DESIGN
5.1 Structural Analysis of Proposed Antenna Mount
5.2 Structural Analysis of Existing Penthouse Wall
6. ATTACHMENTS

Owner: EVERSOURCE Computed By: Nattakit S.
Site Name: MERIDEN COOPER ST. $\quad$ Date: $2 / 21 / 2020$
$\begin{array}{llrl}\text { Project No. } & \text { 403093.2000.2200 } & \text { Verified By: } & \text { K. Hyun } \\ & \text { STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT } & \text { Date: } & 2 / 21 / 2020\end{array}$ AND PENTHOUSE WALL

## 1. PURPOSE

The purpose of this calculation is to evaluate the proposed antenna mount and the existing penthouse wall under proposed loading.

## 2. REFERENCES

A. 2018 Connecticut State Building Code
B. International Building Code, IBC 2015
C. Structural Standard for Antenna Supporting Structures and Antennas, TIA-222-H
D. American Society of Civil Engineers, ASCE 7-10
E. American Institute of Steel Construction, 14th Edition
F. Site Survey Report Completed by Black \& Veatch Corp., dated 1/10/2019
G. Site Photos

## 3. ASSUMPTIONS

- The existing penthouse walls are assumed to be Masonry wall.

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000 .2200 | Verified By: | K. Hyun |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL | Date: | 2/21/2020 |
| BLACK \& VEATCH |  |  |  |  |

## 4. CONCLUSION



### 4.1 Structural Analysis of Proposed Antenna Mount

| Governing Load Combination: | $1.2 \mathrm{DL}+\mathrm{WL}(0 \mathrm{DEG},+\mathrm{X})+0.5 R \mathrm{LL}$ |
| :--- | ---: |
| Max Stress Ratio on Proposed Pipe Mast: Pipe $3.0 \mathrm{STD}:$ | $81.3 \% *$ |
| Governing Load Combination: | $1.2 \mathrm{DL}+\mathrm{WL}(0 \mathrm{DEG},+\mathrm{X})+0.5 R \mathrm{LL}$ |
| Max Stress Ratio on Proposed Wall Mount Anchorage: | $54.8 \% *$ |
| The Proposed Antenna Mount Result: | $\underline{\text { SUFFICIENT }}$ |
| Use Pipe 3 STD (O.D. 3.5") pipe x 9'-0" long min., with Commscope MT-222 wall mount bracket. |  |
| Anchor (4) 1/2" Dia. Thru - Bolts (ASTM A325) drill to the existing penthouse wall or engineer approve |  |
| equal. |  |

[^1]

## 4. CONCLUSION (CONTINUED)

### 4.2 Structural Analysis of Existing Penthouse Wall

By engineering judgment/inspection, the existing penthouse wall is SUFFICIENT to support the proposed loads.

### 4.3 Disclaimers

This calculation is based on the loading and equipment position provided by client. If the installed loading and/or equipment position are different from the calculation, the calculation is considered invalid.

This certification assumes that all structural members are in good condition. Contractor shall inspect the condition of all relevant members and connectors and report any perceived deficiencies to the engineer prior to installation of any new equipment.

The contractor shall be responsible for the means and methods of construction. It is contractor's responsibility to provide necessary intermediate or temporary support during construction.


## Summary of Final Loading

## Eversource's Loading

| Final Antenna/Equipment |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment <br> Owner | Equipment <br> Elevation (ft) | Mount Location | Position | Type | Quantity | Manufacturer | Model |
| Eversource | 55 | Pipe Mount | - | Omni | 1 | dbSpectra | (P) dbSpectra DS2C03F36D |
|  |  |  |  |  |  |  |  |

## Note:

(P) = Proposed Equipment

| Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: |
| Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
| Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
| Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL | Date: | 2/21/2020 |

## 5. ANALYSIS \& DESIGN

### 5.1 Structural Analysis of Proposed Antenna Mount

Equipment Dead Load $\quad$ EVERSOURCE'S LOADING
(P) dbSpectra DS2C03F36D
100.0 lbs

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL | Date: | 2/21/2020 |

## Wind Pressure per ASCE 7-10 / IBC 2012 / IBC 2015 / TIA-222-H

a. Ultimate Velocity Pressure, $\mathrm{q}_{\mathrm{z} \text { or }} \mathrm{q}_{\mathrm{h}}$

$$
\begin{aligned}
\mathrm{qz} & =0.00256 \mathrm{Kz} \text { Kzt Kd Ke Ks V}{ }^{2} \\
& =0.00256 \times 1.19 \times 1.00 \times 0.95 \times 1.00 \times 1.00 \times 135.00^{\wedge} 2 \\
\mathrm{qz} & =\quad 52.80 \mathrm{psf}
\end{aligned}
$$

b. Velocity pressure coefficient, Kz

$$
\begin{aligned}
\mathrm{Kz} & =2.01\left(\mathrm{z} / \mathrm{z}_{\mathrm{g}}\right)^{2 / \alpha} \\
& =2.01(75 / 900 \\
\mathrm{Kz} & =1.19 \\
\alpha & =9.50
\end{aligned}
$$

Basic Wind Speed, Vult $=\quad 135 \mathrm{mph}$

| qz | $=0.00256 \mathrm{Kz} \mathrm{Kzt} \mathrm{Kd} \mathrm{Ke} \mathrm{Ks} \mathrm{V}{ }^{2}$ |
| ---: | :--- |
|  | $=0.00256 \times 1.19 \times 1.00 \times 0.95 \times 1.00 \times 1.00 \times 135.00^{\wedge} 2$ |
| qz | $=\quad 52.80 \mathrm{psf}$ |

$$
\begin{aligned}
& \text { Exposure Category }=\begin{array}{r}
\text { C } \\
\text { Height above Ground Level, } \\
z
\end{array} \\
&=\square 75 \mathrm{ft}
\end{aligned}
$$

$$
z_{\mathrm{g}}=\quad 900.00 \mathrm{ft}
$$

c. Topographic Factor, Kzt

$$
\begin{aligned}
\mu & =0.00 \\
\gamma & =0.00 \\
\mathrm{~K}_{1} & =0.00 \\
\mathrm{~K}_{2} & =(1-\mathrm{x} / \mu \mathrm{Lh}) \\
& =[1-15 /(0.0 \times 15)] \\
\mathrm{K}_{2} & =0.00 \\
\mathrm{~K}_{3} & =\mathrm{e}^{(\gamma z / \mathrm{Lh})} \\
& =\mathrm{e}^{\wedge}-(0.0 \times 75 / 15) \\
\mathrm{K}_{3} & =0.00
\end{aligned}
$$

$$
\begin{array}{r}
\text { Her } \mathrm{ft} \\
\text { Hill Shape } \begin{array}{r}
\text { Flat Terrain } \\
\text { Crest Type } \square \text { Upwind }
\end{array}
\end{array}
$$

Distance Upwind of crest, Lh =
$\square$
d. Wind Directionality Factor, Kd

| (7) Chimney, Tank \& Similar Structures - Round Shape | $\mathrm{Kd}=$ |  |  |
| :--- | :--- | ---: | :--- |
| e. Ground Elevation Factor, Ke |  | $\mathrm{Ke}=$1.00 <br> f. Rooftop Wind Speed-up Factor, Ks <br> g. Structure Risk Category <br> h. Gust Effect Factor, G | $\mathrm{Ks}=$1.00 |

Fig. 26.8-1

Eq. 26.8-1
ASCE 7-10 Section \# 29.3.2

Fig. $26.5-1 \mathrm{~A}$
TIA-222-H
Sec. 2.6.11.6

Table 26.6-1

TIA-222-H
Table 2-6

TIA-222-H
Sec. 2.6.7

Table 1.5-1
26.9

|  | Owner: <br> Site Name: | EVERSOURCE | Computed By: | Nattakit S. |
| :--- | :--- | :--- | ---: | :--- |
|  | Project No. | MERIDEN COOPER ST. | Date: | $2 / 21 / 2020$ |
| Title: |  |  |  |  |

## Wind Load

Wind Velocity Pressure @ z = 75 ft
Gust factor:

Wind Load on Members:
Proposed Pipe Mast: Pipe 3.0 STD

Depth:
Force Coefficient:
Wind Load:

| $\mathrm{Q}_{\mathrm{z}}$ | $=$ |
| :---: | :---: |
| $\mathrm{G}=$ | 52.80 psf |
|  | 0.85 |


| $\mathrm{Dp}=$ | 3.5 in. |
| :--- | ---: |
| $\mathrm{Ca}=$ | 0.93 |
| $\mathrm{Pp}=$ | $\mathrm{Qz}^{*} \mathrm{G}^{*} \mathrm{Ca}{ }^{*} \mathrm{Dp}$ |

$P p=\quad Q z^{*} G^{*} C a * D p$
$=$
12.2 plf


## Wind Load (Continued)

Wind Load on Equipment:
(P) dbSpectra DS2C03F36D

| Dimensions: | $\mathrm{B}=$ | 0.25 ft. |  |  |
| :--- | ---: | ---: | :--- | :--- |
|  | $\mathrm{H}=$ | 24.30 ft. |  |  |
| Force Coefficient: | $\mathrm{Ca}=$ | 1.20 |  |  |
| Wind Load: | $\mathrm{Pa}=$ | $\mathrm{Qz}^{*} \mathrm{G}^{*} \mathrm{Ca}^{*} \mathrm{~B}^{*} \mathrm{H}$ | $=$ | $\mathbf{3 2 7 . 2} \mathbf{~ l b s .}$ |
|  |  |  | $=$ | $\mathbf{1 3 . 5} \mathbf{~ p l f}$ |

Note:


| Ice Dead Load |  |  | ASCE 7-10 <br> Section \# |
| :---: | :---: | :---: | :---: |
| Design Ice Thickness @ z=33 ft $\quad \mathrm{T}_{\mathrm{i}}=$ | 0.75 in. (Per TIA | nex B) | Fig. 10.2 |
| Note: The design ice thickness shall be escalated with height when calculating the ice weight and wind force on the ice. |  |  |  |
| Platform and antennas height elevation, Z: 75 ft |  |  |  |
| Factored Ice Thickness, Tiz at Z for Ice Weight Calculations: |  |  | 10.4 .6 |
| $\mathrm{T}_{\mathrm{iz}}=\left.2.0 * \mathrm{~T}_{\mathrm{i}}{ }^{*}\right\|_{i}{ }^{*} \mathrm{f}_{\mathrm{z}}{ }^{*}\left(\mathrm{~K}_{z t}\right)^{0.35}$ | $\mathrm{T}_{\mathrm{iz}}=2$. |  | Eq. 10.4-5 |
| where, |  |  |  |
| Importance Factor for Ice Thickness, $\mathrm{I}_{\mathrm{i}}$ |  |  | 10.4.4 |
| Structure Risk Category: |  |  | Table 1.5-1 |
| $I_{i}=1.25$ <br> (multiplier on ice thickness) |  |  | Table 1.5-2 |
| Height Factor, $\mathrm{f}_{\mathrm{z}}$ |  |  | 10.4.3 |
| $\mathrm{f}_{\mathrm{z}}=(\mathrm{Z} / 33)^{0.10}=(75 / 33)^{\wedge} 0.10$ | 1.09 |  | Eq. 10.4-4 |
| Topographic Factor, $\mathrm{K}_{\mathrm{zt}}$ |  |  | 10.4 .5 |
| $\mathrm{K}_{\mathrm{zt}}=\left[1+\mathrm{K}_{1} \mathrm{~K}_{2} \mathrm{~K}_{3}\right]^{2}=\quad[1+0.00 \times 0.00 \times 0.00]^{\wedge} 2=1.000$ |  |  | Eq. 26.8-1 |
| $\mathrm{K}_{1}=0.00 \quad \mu=0.00 \quad \gamma=0.00$ |  |  | Fig. 26.8-1 |
| Exposure Category = C |  |  | (Use same values |
|  | Hill Shape $=$ Flat Terr |  | from wind calcs) |
|  | Hill Height, H = 15 |  |  |
| Distance | wind of crest, Lh = 15 | ft |  |
| Distance Up | d to Bldg Site, $\mathrm{x}=15$ | ft |  |
| $\mathrm{K}_{2}=\left(1-\mathrm{x} / \mu \mathrm{L}_{\mathrm{h}}\right)=[$ | $15 /(0.0 \times 15)]=0.00$ |  | Fig. 26.8-1 |
| $K_{3}=\mathrm{e}^{-(\gamma z / L h)}=$ | (0.0 $\times 75 / 15)=0.00$ |  | Fig. 26.8-1 |
| Ice Topographic Factor, $\left(\mathrm{K}_{\mathrm{zt}}\right)^{0.35}=$ | ( $000{ }^{\wedge} 0.35=1.000$ |  | 10.4.5 |
| The weight of ice shall be based on a unit weight of 56 pcf . Therefore | (Per TIA | 2-G 2.6.8) | 10.4.1 |
| $\mathrm{W}_{\text {ice }}=56 \mathrm{pcf}$ * Tiz /12= | 9.50 psf |  |  |


|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000 .2200 | Verified By: | K. Hyun |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND | Date: | 2/21/2020 |
| BLACK \& VEATCH |  | PENTHOUSE WALL |  |  |



|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
| = | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
| - | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND | Date: | 2/21/2020 |
| BLACK \& VEATCH |  | PENTHOUSE WALL |  |  |

## Ice Dead Load (Continued)

Ice Dead Load on Equipment:
(P) dbSpectra DS2C03F36D

Dimensions w/out ice:

Ice cross sectional area:
Ice Dead Load:

| $B=$ | 3 in. | W= | 3 in . |
| :---: | :---: | :---: | :---: |
| $\mathrm{H}=$ | 291.6 in. | Dc= | 4.24 in. |
| Aiz= | iz (Dc + Tiz) $=$ | 40.15 |  |
| DLice $=[A i z(H+2 T i z)+2 \mathrm{Tiz} \mathrm{B} \mathrm{D}]^{*} 56 \mathrm{pcf} / 1728 \mathrm{in}^{\wedge} 3=$ |  |  |  |

385.9 lbs 15.9 plf

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT | Date: | 2/21/2020 |
| BLACK \& VEATCH |  |  |  |  |

## Ice Wind Pressure per ASCE 7-10 / IBC 2012 / IBC 2015 / TIA-222-H

a. Ultimate Velocity Pressure, $\mathrm{q}_{\mathrm{z} \text { or }} \mathrm{q}_{\mathrm{h}}$

Basic Wind Speed, Vult $=\quad 50 \mathrm{mph}$

$$
\begin{aligned}
q z & =0.00256 \mathrm{Kz} \text { Kzt Kd Ke Ks V} \\
& \\
& =0.00256 \times 1.19 \times 1.00 \times 0.95 \times 1.00 \times 1.00 \times 50.00^{\wedge} 2 \\
q z & =\quad 7.24 \mathrm{psf}
\end{aligned}
$$

b. Velocity pressure coefficient, Kz

$$
\begin{aligned}
\mathrm{Kz} & =2.01\left(\mathrm{z} / \mathrm{z}_{\mathrm{g}}\right)^{2 / \alpha} \\
& =2.01\left(75 / 900^{\wedge}(2 / 9.5)\right. \\
\mathrm{Kz} & =1.19 \\
\alpha & =9.50
\end{aligned}
$$

| Exposure Category | $=\square$ C |
| ---: | :--- |
| Height above Ground Level, z | $=\square \mathrm{ft}$ |

c. Topographic Factor, Kzt

$$
\begin{aligned}
\mu & =0.00 \\
\gamma & =0.00 \\
\mathrm{~K}_{1} & =0.00 \\
\mathrm{~K}_{2} & =(1-\mathrm{x} / \mu \mathrm{Lh}) \\
& =[1-15 /(0.0 \times 15)] \\
\mathrm{K}_{2} & =0.00 \\
\mathrm{~K}_{3} & =\mathrm{e}^{(\gamma z / \mathrm{Lh})} \\
& =\mathrm{e}^{\wedge}-(0.0 \times 75 / 15) \\
\mathrm{K}_{3} & =0.00
\end{aligned}
$$

$$
\begin{aligned}
\mathrm{Kzt} & =\left[1+\mathrm{K}_{1} \mathrm{~K}_{2} \mathrm{~K}_{3}\right]^{2} \\
& =[1+0.00 \times 0.00 \times 0.00]^{\wedge} 2 \\
\mathrm{Kzt} & =1.00
\end{aligned}
$$

d. Wind Directionality Factor, Kd

| (7) Chimney, Tank \& Similar Structures - Round Shape | $\mathrm{Kd}=0.95$ |  |
| :---: | :---: | :---: |
| e. Ground Elevation Factor, Ke | $\mathrm{Ke}=1.00$ |  |
| f. Rooftop Wind Speed-up Factor, Ks | $K s=1.00$ |  |
| g. Structure Risk Category $\quad$ III |  |  |
| h. Gust Effect Factor, G | $\mathrm{G}=$ | 0.85 |

Table 26.6-1

TIA-222-H
Table 2-6

TIA-222-H
Sec. 2.6.7

Table 1.5-1
26.9

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Site Name: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND | Date: | 2/21/2020 |
| BLACK \& VEATCH |  | PENTHOUSE WALL |  |  |

## Ice Wind Load

Wind Velocity Pressure @ z = 75 ft
Gust factor:

Ice Wind Load on Members:
Proposed Pipe Mast: Pipe 3.0 STD

| Member Depth: | $\mathrm{Dp}=$ | $3.5 \mathrm{in} .+2 \mathrm{Tiz}=$ |
| :--- | :--- | :---: |
| Force Coefficient: | $\mathrm{Ca}=$ | 0.93 |
| Ice wind load: | $\mathrm{Pp}=\mathrm{Qz}$ ice* $\mathrm{G}^{*} \mathrm{Ca}{ }^{*} \mathrm{Dp}=$ | 8 in. |
|  | $\mathbf{3 . 6}$ plf |  |


| $Q_{\text {zice }}$ | $=$ | 7.24 psf | (based on $\mathbf{5 0} \mathbf{~ m p h}$ wind $)$ |
| ---: | :--- | ---: | :--- |
| $G$ | $=$ | 0.85 |  | $P p=Q z$ ice* ${ }^{*}{ }^{*} \mathrm{Ca}$ *Dp = 3.6 plf



## Ice Wind Load (Continued)

Ice Wind Load on Equipment:
(P) dbSpectra DS2C03F36D

Dimensions:

Force Coefficient:
Wind Load:

| $\mathrm{B}=$ | $0.25 \mathrm{ft}+(2 \mathrm{Tiz}) / 12$ | $=$ | 0.59 ft. |
| :---: | :---: | :---: | :---: |
| $\mathrm{H}=$ | $24.30 \mathrm{ft}+(2 \mathrm{Tiz}) / 12=$ | 24.64 ft. |  |
| $\mathrm{Ca}=$ | 1.20 |  |  |
| $\mathrm{~Pa}=$ | Qz ice* ${ }^{*} \mathrm{G}^{*} \mathrm{Ca}^{*} \mathrm{~B}^{*} \mathrm{H}=$ |  | 107.3 lbs. |
|  |  |  | 4.4 plf |

Note:
$30^{\circ}$ and $60^{\circ}$ application of wind load will be considered directly in the load combinations by applying load factors of 0.866 (from $\cos 30$ or $\sin 60$ ) and 0.5 (from $\sin 30$ or $\cos 60$ )

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Plant: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
| $\checkmark$ | Project No. | 403093.2000 .2200 | Verified By: | K. Hyun |
| - | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND | Date: | 2/21/2020 |
| BLACK \& VEATCH |  | PENTHOUSE WALL |  |  |

## Seismic Load

The Equipment is considered a Non-Structural Component per section 13.3 of ASCE 7-10.
Location Information: Latitude: N 41.532722 Longitude: W 72.805667
$F p=0.4 a_{p} S_{D S} W p(1+2 z / h) /(R p / l p)=\quad 0.4 \times 1.00 \times 0.195 \mathrm{Wp}(1+2 \times 1.00) /(2.50 / 1.25)$
$F p=0.117 \quad W p$
$\mathrm{Fp}=1.6 \mathrm{~S}_{\mathrm{DS}} \mathrm{Ip} \mathrm{Wp}=$
$F p=0.390 \quad W p$
$1.6 \times 0.195 \times 1.25 \mathrm{Wp}$
$\mathrm{Fp}=0.30 \mathrm{~S}_{\mathrm{DS}} \mathrm{lp} \mathrm{Wp}=$
$\mathrm{Fp}=0.073 \quad \mathrm{Wp}$
$0.30 \times 0.195 \times 1.25 \mathrm{Wp}$

Use $F_{p}=0.117 W_{p}$

$$
\begin{aligned}
S_{D S} & =2 / 3 S_{M S} \\
& =2 / 3(0.293)
\end{aligned}
$$

$S_{D S}=0.195 \mathrm{~g}$
$\begin{array}{rc}\mathrm{SDC} & = \\ \mathrm{S}_{\mathrm{S}} & = \\ & 0.183 \mathrm{~g}\end{array}$
$\mathrm{Fa}=\quad 1.600$
$\mathrm{Ip}=\quad 1.25$
component importance factor
$R p=2.50$ component response modification factor
ap $=1.00 \quad$ component amplification factor
$z / h=\quad 1.00$

| Equipment | DL on each <br> $\mathbf{p o i n t}(\mathbf{l b} / \mathbf{p t})$ | Vertical Seismic Load <br> $\mathbf{W}_{\mathbf{p}} \mathbf{S}_{\mathbf{D S}}(\mathbf{l b})$ | Horiz Seismic Load <br> $\mathbf{W}_{\mathbf{p}} \mathbf{F}_{\mathbf{p}}(\mathbf{l b})$ |
| :---: | :---: | :---: | :---: |
| $(\mathrm{P})$ dbSpectra DS2C03F36D | 100.0 | 19.50 | 11.70 |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

ASCE 7-10
Section \#
eq. 13.3-1
eq. 13.3-2
eq. 13.3-3

IBC-2015
eq. 16-37
eq. 16-39

Tbl.1613.3.3(1)
ASCE 7-10
sec. 13.1.3
Table 13.6-1
Table 13.6-1
sec. 13.1.3


| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Jan 9, 2020 at 1:12 PM |
| :--- | :--- | :--- |
| T. Eakkalak |  | Members in 3D |
| 403093.2000 .2200 |  | MeridenCooperSt_Phase 1.5-Pro... |



Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Joint Numbers |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:12 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Member Numbers |
| :--- | :---: | :--- |
| T. Eakkalak |  | Jan 9,2020 at $1: 13$ PM |
| 403093.2000 .2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Member Shape |
| :--- | :---: | :--- |
| T. Eakkalak |  | Jan 9,2020 at $1: 14$ PM |
| 403093.2000 .2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



Member Length (ft) Displayed
Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Member Length |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:03 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5-Pro... |




| Black \& Veatch Corp. |  | Appurtenance Loads |
| :--- | :--- | :--- |
| T. Eakkalak |  | Jan 9, 2020 at $1: 05$ PM |
|  |  | MeridenCooperSt_Phase 1.5 - Pro... |
| 403093.2000 .2200 |  |  |



| Black \& Veatch Corp. |  | Wind Loads - X Direction |
| :--- | :--- | :--- |
| T. Eakkalak |  | Jan 9, 2020 at 1:06 PM |
|  |  | MeridenCooperSt_Phase 1.5 - Pro... |



| Black \& Veatch Corp. |  | Wind Loads - Z Direction |
| :--- | :--- | :--- |
| T. Eakkalak |  | Jan 9, 2020 at 1:06 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5-Pro... |



| Black \& Veatch Corp. |  | Ice Loads |
| :--- | :--- | :--- |
| T. Eakkalak |  | Jan 9, 2020 at 1:07 PM |
| 403093.2000 .2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



Loads: BLC 6, Ice Wind - 0 Deg (+X)
Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Ice Wind Loads - X Direction |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:08 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



Loads: BLC 7, Ice Wind - 90 Deg (+Z)
Envelope Only Solution

| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Ice Wind Loads - Z Direction |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:08 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Horizontal Seismic Load (X) |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:59 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |



| Black \& Veatch Corp. | Meriden Cooper St. Proposed Antenna Mount Analysis | Horizontal Seismic Load (Z) |
| :---: | :---: | :---: |
| T. Eakkalak |  | Jan 9, 2020 at 1:59 PM |
| 403093.2000.2200 |  | MeridenCooperSt_Phase 1.5 - Pro... |




| Black \& Veatch Corp. |  | Vertical Seismic Load |
| :--- | :--- | :--- |
| T. Eakkalak |  | Jan 9, 2020 at $1: 10$ PM |
|  |  | MeridenCooperSt_Phase 1.5 - Pro... |
| 403093.2000 .2200 |  |  |

Company
Designer
T. Eakkalak

2:00 PM
Job Number : 403093.2000.2200
Checked By: K. Hyun
Model Name : Meriden Cooper St. Proposed Antenna Mount Analysis
(Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :--- | :--- |
| Max Internal Sections for Member Calcs | 97 |
| Include Shear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include Warping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | .12 |
| P-Delta Analysis Tolerance | $0.50 \%$ |
| Include P-Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | Yes |
| Max Iterations for Wall Stiffness | 3 |
| Gravity Acceleration (ft/sec^2) | 32.2 |
| Wall Mesh Size (in) | 12 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Y |
| Global Member Orientation Plane | XZ |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |


| Hot Rolled Steel Code | AISC 14th(360-10): LRFD |
| :--- | :--- |
| Adjust Stiffness? | Yes(Iterative) |
| RISAConnection Code | None |
| Cold Formed Steel Code | None |
| Wood Code | None |
| Wood Temperature | < 100F |
| Concrete Code | None |
| Masonry Code | None |
| Aluminum Code | None - Building |
| Stainless Steel Code | None |


| Number of Shear Regions | 4 |
| :--- | :--- |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | .65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections Slab? | No |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| Concrete Rebar Set | REBAR_SET_ASTMA615 |
| Min \% Steel for Column | 1 |
| Max \% Steel for Column | 8 |

(Global) Model Settings, Continued

| Seismic Code | None |
| :--- | :--- |
| Seismic Base Elevation (ft) | Not Entered |
| Add Base Weight? | Yes |
| Ct X | .02 |
| Ct Z | .02 |
| T X (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
|  |  |

## Hot Rolled Steel Properties

| Label |  | E [ksi] | G [ksi] | Nu | Therm (/1E5 F) | Density[k/f. | Yield[ksi] | Ry | Fu[ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | . 49 | 36 | 1.5 | 58 | 1.2 |
| 2 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 3 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | . 3 | . 65 | 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | . 3 | . 65 | . 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 3 | . 65 | . 49 | 50 | 1.4 | 65 | 1.3 |

General Material Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (/1E5 F) | Density[k/ft^3] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | gen Conc3NW | 3155 | 1372 | . 15 | . 6 | . 145 |
| 2 | gen_Conc4NW | 3644 | 1584 | . 15 | 6 | 145 |
| 3 | gen Conc3LW | 2085 | 906 | . 15 | 6 | . 11 |
| 4 | gen Conc4LW | 2408 | 1047 | . 15 | 6 | 11 |
| 5 | gen Alum | 10600 | 4077 | . 3 | 1.29 | 173 |
| 6 | gen Steel | 29000 | 11154 | . 3 | . 65 | . 49 |
| 7 | RIGID | $1 \mathrm{e}+6$ |  | . 3 | 0 | 0 |

## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design Ru... A [in2] |  | Iyy [in4] | Izz [in4] | $J$ [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Pipe 3.0 STD | PIPE_3.0 | Column | Pipe | A53 Gr.B | Typical | 2.07 | 2.85 | 2.85 | 5.69 |

General Section Sets

|  | Label | Shape | Material | A [in2] | lyy [in4] | Izz [in4] | J [in4] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | GEN1A | RE4X4 | Beam | gen_Conc3NW | 16 | 21.333 | 21.333 | 31.573 |
| 2 | RIGID |  | None | RIGID | $1 \mathrm{e}+6$ | $1 \mathrm{e}+6$ | $1 \mathrm{e}+6$ | $1 \mathrm{e}+6$ |

Joint Coordinates and Temperatures

|  | Label | $\mathrm{X}[\mathrm{ft}]$ | $\mathrm{Y}[\mathrm{ft}]$ | Z [ft] | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | 0 | -1 | 0 | 0 |  |
| 2 | N2 | 0 | -. 5 | 0 | 0 |  |
| 3 | N3 | 0 | 2.5 | 0 | 0 |  |
| 4 | N4 | -. 5 | -. 5 | 0 | 0 |  |
| 5 | N5 | -. 5 | 2.5 | 0 | 0 |  |
| 6 | N6 | . 5 | 7.5 | 0 | 0 |  |
| 7 | N7 | . 5 | 28.8 | 0 | 0 |  |
| 8 | N8 | 0 | 7.5 | 0 | 0 |  |
| 9 | N9 | . 5 | 4.5 | 0 | 0 |  |

Joint Coordinates and Temperatures (Continued)

|  | Label | $\mathrm{X}[\mathrm{ft}]$ | $\mathrm{Y}[\mathrm{ft}]$ | $\mathrm{Z}[\mathrm{ft}]$ | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | N 10 | 0 | 4.5 | 0 | 0 |  |
| 11 | N 11 | 0 | 8 | 0 | 0 |  |
| 12 | N 12 | .5 | 6.5 | 0 | 0 |  |
| 13 | N 13 | 0 | 6.5 | 0 | 0 |  |

## Joint Boundary Conditions

| Joint Labe |  | X [k/in] | Y [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N4 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 2 | N5 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |

## Member Primary Data

| Label |  | 1 Joint | $J$ Joint | K Joint Rotate(.. |  | Section/Shape | Type Design List |  | Material | Design R. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N11 | N1 |  |  | Pipe 3.0 STD | Column | Pipe | A53 Gr.B | Typical |
| 2 | M2 | N4 | N2 |  |  | RIGID | None | None | RIGID | Typical |
| 3 | M3 | N5 | N3 |  |  | RIGID | None | None | RIGID | Typical |
| 4 | M4 | N9 | N7 |  |  | RIGID | None | None | RIGID | Typical |
| 5 | M5 | N10 | N9 |  |  | RIGID | None | None | RIGID | Typical |
| 6 | M6 | N8 | N6 |  |  | RIGID | None | None | RIGID | Typical |
| 7 | M7 | N13 | N12 |  |  | RIGID | None | None | RIGID | Typical |

## Hot Rolled Steel Design Parameters

| Label |  | Shape | Length... Lbyy[ft] |  | Lbzz[ft] | Lcomp to.. | Lcomp bo... | .L-tor... | Kyy | Kzz | Cb Funct.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Pipe 3.0 STD |  |  |  |  |  |  |  |  | Lateral |

## Member Point Loads (BLC 1 : DL)

| Member Label | Direction |  | Magnitude[ $[\mathrm{b}, \mathrm{lb}-\mathrm{ft}]$ | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 4 | Y | -100 | $\%$ |
| 2 | M 1 | Y | -20 | $\% 25$ |

Member Point Loads (BLC 10 : Lateral Seismic - Eh (X))

| Member Label |  |  | Direction | Magnitude[lb,lb-ft] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | X | 11.7 | Location $[\mathrm{ft}, \%]$ |

Member Point Loads (BLC 11 : Lateral Seismic - Eh (Z))

| Member Label | Direction |  | Magnitude[lb,lb-ft] | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 4 | Z | 11.7 | $\% 50$ |

Member Point Loads (BLC 12 : Vertical Seismic - Ev (Y))

| Member Label |  |  |  |  |  |  |  |  | Mirection | Magnitude $[\mathrm{lb}, \mathrm{lb}-\mathrm{ft}]$ | Location $[\mathrm{ft}, \%]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M4 | Y | -19.5 | $\% 50$ |  |  |  |  |  |  |  |

## Member Distributed Loads (BLC 3 : Wind - 0 Deg (+X))

| Member Label |  |  | Direction | Start Magnitude[lb/ft,F,psf] |  | End Magnitude[lb/...Start Location[ft,\%] End Location[ft,\%] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | PX | 12.2 | 12.2 | 0 | 0 |  |
| 2 | M4 | PX | 13.5 | 13.5 | 0 | 0 |  |

[^2]RISA-3D Version 17.0.4 [C:\.........................\...\MeridenCooperSt_Phase 1.5-Proposed Antenna Mourfiagedßl.r3d]

|  | Member Label | Direction | Start Magnitude[lb/ft,F,psf] | End Magnitude[lb/.. | Start Location[ft, \%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | PZ | 12.2 | 12.2 | 0 | 0 |
| 2 | M4 | PZ | 13.5 | 13.5 | 0 | 0 |

## Member Distributed Loads (BLC 5 : Ice DL)

|  | Member Label | Direction | Start Magnitude[lb/ft,F,psf] | End Magnitude[lb/.. | Start Location[ft, \%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -13.8 | -13.8 | 0 | 0 |
| 2 | M4 | Y | -15.9 | -15.9 | 0 | 0 |

## Member Distributed Loads (BLC 6 : Ice Wind - 0 Deg (+X))

|  | Member Label | Direction | Start Magnitude[lb/ft,F,psf] | End Magnitude[lb/.. | Start Location[ft,\%] | End Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | PX | 3.6 | 3.6 | 0 | 0 |
| 2 | M4 | PX | 4.4 | 4.4 | 0 | 0 |

## Member Distributed Loads (BLC 7 : Ice Wind - 90 Deg (+Z))

Member Label Direction Start Magnitude[lb/ft,F,psf] End Magnitude[lb/...Start Location[ft,\%] End Location[ft,\%]

| 1 | M 1 | PZ | 3.6 | 3.6 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | M 4 | PZ | 4.4 | 4.4 | 0 | 0 |

## Basic Load Cases

| BLC Description |  | Category | X Grav...Y Grav.. Z Grav... Joint |  |  |  | Point | Distributed | Area(Mem... | Surfac... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | DL | DL |  | -1 |  |  | 2 |  |  |  |
| 3 | Wind - 0 Deg (+X) | WL |  |  |  |  |  | 2 |  |  |
| 4 | Wind -90 Deg (+Z) | WL |  |  |  |  |  | 2 |  |  |
| 5 | Ice DL | DL |  |  |  |  |  | 2 |  |  |
| 6 | Ice Wind - 0 Deg (+X) | WL |  |  |  |  |  | 2 |  |  |
| 7 | Ice Wind - 90 Deg ( $+Z$ ) | WL |  |  |  |  |  | 2 |  |  |
| 10 | Lateral Seismic - Eh (X) | ELX | . 094 |  |  |  | 1 |  |  |  |
| 11 | Lateral Seismic - Eh (Z) | ELZ |  |  | . 094 |  | 1 |  |  |  |
| 12 | Vertical Seismic - Ev (Y) | ELY |  | -. 195 |  |  | 1 |  |  |  |

## Load Combinations

|  | Description | Solve | PDelta | SRSS |  | Factor |  |  |  | F. |  | F. | F | F...... | F.. | F. | F. | F. | F. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LOAD COMBINATION USING ... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | WIND LOAD COMBINATIONS (.. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | 1.4DL | Yes | Y |  | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | 1.2DL + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 1.2DL + 1.6RLL + 0.5WL (0 DE... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 |  | . 5 |  |  |  |  |  |  |  |  |  |
| 6 | 1.2DL + 1.6RLL - 0.5WL (0 DE... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 3 | -. 5 |  |  |  |  |  |  |  |  |  |
| 7 | 1.2DL + 1.6RLL + 0.5WL (30 D... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 3 | 4.. | 4 | 25 |  |  |  |  |  |  |  |
| 8 | 1.2DL + 1.6RLL - 0.5WL (30 DE. | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 3 | -.... | 4 | -.... |  |  |  |  |  |  |  |
| 9 | 1.2DL + 1.6RLL + 0.5WL (60 D... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 4 | 4.. | 3 | 25 |  |  |  |  |  |  |  |
| 10 | 1.2DL + 1.6RLL - 0.5WL (60 DE... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 4 | -.... | 3 | -... |  |  |  |  |  |  |  |
| 11 | 1.2DL + 1.6RLL + 0.5WL (90 D... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 | 4 | . 5 |  |  |  |  |  |  |  |  |  |
| 12 | 1.2DL + 1.6RLL - 0.5WL (90 DE... | Yes | Y |  | 1 | 1.2 | 2 | 1.6 |  | -. 5 |  |  |  |  |  |  |  |  |  |
| 13 | 1.2DL+ WL (0 DEG, +X) + 0.5R... | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 3 | 1 |  |  |  |  |  |  |  |  |  |
| 14 | 1.2DL - WL (0 DEG, -X) + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 3 | -1 |  |  |  |  |  |  |  |  |  |
| 15 | 1.2DL + WL (30 DEG) + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 3 | .8.. | 4 | . 5 |  |  |  |  |  |  |  |
| 16 | 1.2DL - WL (30 DEG) + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 3 |  | 4 | -. 5 |  |  |  |  |  |  |  |
| 17 | 1.2DL + WL (60 DEG) + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 4 | 8.. | 3 | . 5 |  |  |  |  |  |  |  |
| 18 | 1.2DL - WL (60 DEG) + 0.5RLL | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 4 | ... | 3 | -. 5 |  |  |  |  |  |  |  |
| 19 | 1.2DL + WL (90 DEG, +Z) + 0.5... | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 4 | 1 |  |  |  |  |  |  |  |  |  |
| 20 | 1.2DL - WL (90 DEG, -Z) + 0.5R.. | Yes | Y |  | 1 | 1.2 | 2 | . 5 | 4 | -1 |  |  |  |  |  |  |  |  |  |

Company Designer Job Number

## Load Combinations (Continued)

|  | Description | Solve | Delt | SRSS | BLC | Factor |  |  |  |  |  |  |  |  |  |  | F. | F. | F. | F. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 0.9DL + WL (0 DEG, +X) | Yes | Y |  | 1 | . 9 | 3 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | 0.9DL - WL (0 DEG, -X) | Yes | Y |  | 1 | . 9 | 3 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 | 0.9DL + WL (30 DEG) | Yes | Y |  | 1 | . 9 | 3 | .8... | 4 | . 5 |  |  |  |  |  |  |  |  |  |  |
| 24 | 0.9DL - WL (30 DEG) | Yes | Y |  | 1 | . 9 | 3 | -.... | 4 | -. 5 |  |  |  |  |  |  |  |  |  |  |
| 25 | 0.9DL + WL (60 DEG) | Yes | Y |  | 1 | . 9 | 4 | 8... | 3 | . 5 |  |  |  |  |  |  |  |  |  |  |
| 26 | 0.9DL - WL (60 DEG) | Yes | Y |  | 1 | . 9 | 4 | . | 3 | -. 5 |  |  |  |  |  |  |  |  |  |  |
| 27 | 0.9DL + WL (90 DEG, +Z) | Yes | Y |  | 1 | . 9 | 4 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | 0.9DL - WL (90 DEG, -Z) | Yes | Y |  | 1 | . 9 | 4 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 29 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | LOAD COMBINATIONS WITH I... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | 1.2DL + 0.2Ice DL + 0.5SL1 | Yes | Y |  | 1 | 1.2 | 5 | . 2 | 8 | . 5 |  |  |  |  |  |  |  |  |  |  |
| 32 | 1.2DL + Ice DL + Ice WL (0 DE... | Yes | Y |  | 1 | 1.2 | 5 | 1 | 6 | 1 | 8 | . 5 |  |  |  |  |  |  |  |  |
| 33 | 1.2DL + Ice DL - Ice WL (0 DEG.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 6 | -1 | 8 | . 5 |  |  |  |  |  |  |  |  |
| 34 | 1.2DL + Ice DL + Ice WL (30 DE.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 6 | .8.. | 7 | . 5 | 8 | . 5 |  |  |  |  |  |  |
| 35 | 1.2DL + Ice DL - Ice WL (30 DE.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 6 | -.... | 7 | -. 5 | 8 | . 5 |  |  |  |  |  |  |
| 36 | 1.2DL + Ice DL + Ice WL (60 DE.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 7 | 8.. | 6 | . 5 | 8 | . 5 |  |  |  |  |  |  |
| 37 | 1.2DL + Ice DL - Ice WL (60 DE.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 7 | - | 6 | -. 5 | 8 | . 5 |  |  |  |  |  |  |
| 38 | 1.2DL + Ice DL + Ice WL (90 DE.. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 7 | 1 | 8 | . 5 |  |  |  |  |  |  |  |  |
| 39 | 1.2DL + Ice DL - Ice WL (90 DE. | Yes | Y |  | 1 | 1.2 | 5 | 1 | 7 | -1 | 8 | . 5 |  |  |  |  |  |  |  |  |
| 40 | 0.9DL + Ice DL + Ice WL (0 DE... | Yes | Y |  | 1 | . 9 | 5 | 1 | 6 | 1 |  |  |  |  |  |  |  |  |  |  |
| 41 | 0.9DL + Ice DL - Ice WL (0 DEG... | Yes | Y |  | 1 | . 9 | 5 | 1 | 6 | -1 |  |  |  |  |  |  |  |  |  |  |
| 42 | 0.9DL + Ice DL + Ice WL (30 DE.. | Yes | Y |  | 1 | . 9 | 5 | 1 | 6 | 8. | 7 | . 5 |  |  |  |  |  |  |  |  |
| 43 | 0.9DL + Ice DL - Ice WL (30 DE... | Yes | Y |  | 1 | . 9 | 5 | 1 | 6 | - | 7 | -. 5 |  |  |  |  |  |  |  |  |
| 44 | 0.9DL + Ice DL + Ice WL (60 DE.. | Yes | Y |  | 1 | . 9 | 5 | 1 | 7 | 8. | 6 | . 5 |  |  |  |  |  |  |  |  |
| 45 | 0.9DL + Ice DL - Ice WL (60 DE... | Yes | Y |  | 1 | . 9 | 5 | 1 | 7 | -.... | 6 | -. 5 |  |  |  |  |  |  |  |  |
| 46 | 0.9DL + Ice DL + Ice WL (90 DE.. | Yes | Y |  | 1 | . 9 | 5 | 1 | 7 | 1 |  |  |  |  |  |  |  |  |  |  |
| 47 | 0.9DL + Ice DL - Ice WL (90 DE. | Yes | Y |  | 1 | . 9 | 5 | 1 | 7 | -1 |  |  |  |  |  |  |  |  |  |  |
| 48 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 49 | SEISMIC LOAD COMBINATIO... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | 1.2DL + 0.2Ev $(Y)+E h(X)+0 . .$. | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | 2.2 | 10 | 1 |  |  |  |  |  |  |  |  |
| 51 | 1.2DL - 0.2Ev $(Y)+\mathrm{Eh}(\mathrm{X})+0.2 \ldots$ | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | -. 2 | 10 | 1 |  |  |  |  |  |  |  |  |
| 52 | 1.2DL + 0.2Ev $(Y)-E h(X)+0.2 \ldots$ | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | 2.2 | 10 | -1 |  |  |  |  |  |  |  |  |
| 53 | 1.2DL -0.2Ev (Y) - Eh (X) + 0.2... | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | --. 2 | 10 | -1 |  |  |  |  |  |  |  |  |
| 54 | 1.2DL + 0.2Ev $(Y)+E h(Z)+0 . \ldots$ | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | 2.2 | 11 | 1 |  |  |  |  |  |  |  |  |
| 55 | 1.2DL-0.2Ev $(Y)+E h(Z)+0.2$. | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | --. 2 | 11 | 1 |  |  |  |  |  |  |  |  |
| 56 | 1.2DL + 0.2Ev $(Y)-\operatorname{Eh}(Z)+0.2 \ldots$ | Yes | Y |  | 1 | 1.2 | 8 | 2 | 12 | 2.2 | 11 | -1 |  |  |  |  |  |  |  |  |
| 57 | 1.2DL-0.2Ev (Y)-Eh $(Z)+0.2$.. | Yes | Y |  | 1 | 1.2 | 8 | . 2 | 12 | --. 2 | 11 | -1 |  |  |  |  |  |  |  |  |
| 58 | 0.9DL - 0.2Ev (Y) + Eh (X) | Yes | Y |  | 1 | . 9 |  | -. 2 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |
| 59 | 0.9DL + 0.2Ev (Y) + Eh (X) | Yes | Y |  | 1 | . 9 | 12 | . 2 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |
| 60 | 0.9DL - 0.2Ev (Y) - Eh (X) | Yes | Y |  | 1 | . 9 | 12 | -. 2 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |
| 61 | 0.9DL + 0.2Ev (Y) - Eh (X) | Yes | Y |  | 1 | . 9 |  | . 2 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |
| 62 | 0.9DL-0.2Ev $(Y)+E h(Z)$ | Yes | Y |  | 1 | . 9 | 12 | -. 2 | 11 | 11 |  |  |  |  |  |  |  |  |  |  |
| 63 | 0.9DL + 0.2Ev (Y) + Eh (Z) | Yes | Y |  | 1 | . 9 |  | . 2 | 11 | 11 |  |  |  |  |  |  |  |  |  |  |
| 64 | 0.9DL - 0.2Ev (Y) - Eh (Z) | Yes | Y |  | 1 | 9 | 12 | -. 2 | 11 | 1-1 |  |  |  |  |  |  |  |  |  |  |
| 65 | 0.9DL + 0.2Ev (Y) - Eh (Z) | Yes | Y |  | 1 | . 9 | 12 | . 2 | 11 | 1-1 |  |  |  |  |  |  |  |  |  |  |
| 66 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Envelope Joint Reactions

| Joint |  |  | X [Ib] | LC | Y [lb] | LC | Z [lb] | LC | MX [lb-ft] | LC MY [lb-..LC MZ [lb- |  |  |  | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N4 | max | 24.4 | 14 | 44.506 | 32 | 24.4 | 28 | 7.625 | 28 | 12.2 | 27 | 24.503 | 32 |
| 2 |  | min | -24.4 | 21 | 12.129 | 60 | -24.4 | 27 | -7.625 | 27 | -12.2 | 28 | -1.286 | 22 |
| 3 | N5 | max | 413.399 | 14 | 686.138 | 33 | 413.438 | 28 | 4854.291 | 20 | 370.738 | 27 | 5012.9.. | 13 |
| 4 |  | min | -413.398 | 21 | 146.553 | 58 | -413.438 | 27 | -4854.291 | 19 | -370.7... | 28 | -4726.... | 22 |
| 5 | Totals: | max | 437.799 | 14 | 730.643 | 33 | 437.838 | 28 |  |  |  |  |  |  |
| 6 |  | min | -437.798 | 21 | 158.682 | 58 | -437.838 | 27 |  |  |  |  |  |  |



Envelope AISC 14th(360-10): LRFD Steel Code Checks

| Memb. |  | Shape | Code Check | Loc[ft] | LC | Sh... Lo |  | phi*Pnc [lb] phi* ...phi*M...phi*Mn z-. |  |  | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | PIPE 3.0 | . 854 | 5.438 | 13 | . 0525 | 5.... | ... 42263.948 | 652... 5748.... | 5748.75 | . $\mathrm{H} 1-.$. |


| LC |  | Joint Label | X [16] | Y [lb] | Z [lb] | MX [lb-ft] | MY [lb-ft $] \quad \mathrm{MZ}[\mathrm{lb-ft}]$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13 | N4 | -24.4 | 16.906 | 0 | 0 | 0 | 16.078 |
| 2 | 13 | N5 | -413.398 | 203.164 | 0 | 0 | 0 | 5012.955 |
| 3 | 13 | Totals: | -437.798 | 220.07 | 0 |  |  |  |
| 4 | 13 | COG (ft): | X: . 273 | Y: 10.916 | Z: 0 |  |  |  |

Maximum Joint Reactions (L.C. 13)

|  | Owner: <br> Plant: | EVERSOURCE | Prepared By: | T. Eakkalak |
| :--- | :--- | :--- | ---: | :--- |
|  | Project No. | MERIDEN COOPER ST. | Date: | $1 / 9 / 2020$ |
|  | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND | Verified By: | K. Hyun |

Wall Anchor Check (LRFD) - Bolted Thru Wall
AISC 14th Ed.

Load Inputs:

Vertical Force
Horizontal Force (Tension)
Horizontal Force
Moment about Y-Axis
Moment about X-Axis
Moment about Z-Axis

Force Couple Y-Axis
Force Couple Z-Axis
Number of Anchors

Shear from Fy
Tension from Fx
Shear from Fz
Tension from My
Shear from Mx
Tension from Mz

Total Shear
Total Tension

LC13 : 1.2DL+ WL (0 DEG, +X) + 0.5RLL


$$
\begin{aligned}
& S y=F y / N \\
& T x=F x / N \\
& S z=F z / N \\
& T m y=M y / D z /(N / 2) \\
& S m x=M x / D z /(N / 2) \\
& T m z=M z / D y /(N / 2)
\end{aligned}
$$



$$
\begin{aligned}
& S=\operatorname{SQRT}\left(S x^{2}+S z^{2}+S m y^{2}\right) \\
& T=T y+T m x+T m z
\end{aligned}
$$

|  | Owner: <br> Plant: <br> Project No. <br> Title: | EVERSOURCE |  | Prepared By: | T. Eakkalak |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MERIDEN COOPE |  | Date: | 1/9/2020 |
|  |  | 403093.2000 .2200 | File No. | Verified By: | K. Hyun |
|  |  | STRUCTURAL AN | OF PROPOSED ANTENNA MOUNT AND | Date: | 1/9/2020 |
| BLACK \& VEATCH |  | PENTHOUSE WALL |  |  |  |

## Wall Anchor Check (LRFD) - Bolted Thru Wall (Continued)

## Thru Bolt Steel Analysis

Loads
Applied Shear Load
Applied Tensile Load

## Parameters

Bolt Diameter
Bolt Gross Area
Specified Yield Strength of Bolt
Specified Tensile Strength of Bolt

## Results

Strength Resistance Factor
Nominal Shear Strength
Nominal Tensile Strength
Design Shear Strength of Bolt
Design Tensile Strength of Bolt
Required Shear Stress for Bolt
Required Tensile Stress for Bolt
Combined Shear and Tension
$F_{n t}^{\prime}=1.3^{*} F_{n t}-F_{n t}^{*} f_{v} / F_{n v} / \phi \leq F_{n t}$
Available Tensile Strength of Bolt Stress Ratio (Less than 1.0)

Available Shear Strength of Bolt
Stress Ratio (Less than 1.0)

| $V_{\text {ua }}$ | $=51$ | lbs |
| :--- | :--- | :--- |
| $N_{\text {ua }}$ | $=7,623$ | per bolt |
| lbs | per bolt |  |


| $\mathrm{d}_{\mathrm{b}}=1 / 2$ | in |
| :--- | :--- |
| $\mathrm{A}_{\mathrm{b}}=0.196 \mathrm{in}^{2}$ | $\pi \mathrm{~d}_{\mathrm{b}}^{2} / 4$ |


| $\mathrm{f}_{\mathrm{y}}=$ | 92 | ksi |  |
| :---: | :---: | :---: | :---: |
| $f_{\text {uta }}=$ | 120 | ksi | A325 |


| $\varphi$ | $=0.75$ |  |  |
| ---: | :--- | ---: | :--- |
| $\mathrm{~F}_{\mathrm{nv}}$ | $=54.0$ | ksi | $0.45 \times \mathrm{f}_{\mathrm{uta}}$ |
| $\mathrm{F}_{\mathrm{nt}}$ | $=90.0$ | (ductile) |  |
|  |  | ksi | $0.75 \times \mathrm{F}_{\mathrm{ut}}$ | (ductile)


| $\varphi \mathrm{R}_{\mathrm{nv}}=$ |  |  |
| :--- | :--- | :--- |
| $\varphi \mathrm{R}_{\mathrm{nt}}=$ | $=7,952$ | lbs |
| $13,254 \mathrm{lbs}$ | $\varphi \times \mathrm{F}_{\mathrm{nv}} \times \mathrm{A}_{\mathrm{b}}$ |  |
| $\varphi \times \mathrm{F}_{\mathrm{nt}} \times \mathrm{A}_{\mathrm{b}}$ |  |  |


| $\mathrm{f}_{\mathrm{v}}=$ |  |  |
| :--- | :--- | :--- |
| $\mathrm{f}_{\mathrm{t}}=$ | $=0.3$ | ksi |
| ksi | $\mathrm{V}_{\text {ua }} / \mathrm{A}_{\mathrm{b}}$ |  |
| ksi | $\mathrm{N}_{\text {ua }} / \mathrm{A}_{\mathrm{b}}$ |  |


| $\mathrm{F}_{\text {nt }}=$ | 116.4 | $] \mathrm{ksi}>\mathrm{Fnt}$ <br> lbs | Use Fnt for Eq. J3-2 |  |
| :---: | :---: | :---: | :---: | :---: |
| $\varphi \mathrm{R}_{\mathrm{nt}}=$ | 13,254 |  | $\varphi \times$ Fnt $\times$ Ab |  |
| SR = | 0.575 |  | $\mathrm{N}_{\mathrm{ua}} / \varphi \mathrm{R}_{\mathrm{nt}}$ | OK |

AISC 14th Ed.
Section \#

J3.2
C-J3-4
C-J3-2

Eq. J3-1
Eq. J3-1

Eq. J3-3a
Eq. J3-2

## J3.7

Use 1/2" dia A325 bolts thru existing penthouse wall

|  | Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: | :---: |
|  | Project: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
|  | Project No. | 403093.2000.2200 | Verified By: | K. Hyun |
| BLACK \& VEAT | Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL | Date: | 2/21/2020 |

### 5.2 Structural Analysis of Existing Penthouse Wall

By inspection and engineering judgment, the final configuration of the equipment loading will not have significant adverse effect on the existing penthouse wall.

| Owner: | EVERSOURCE | Computed By: | Nattakit S. |
| :---: | :---: | :---: | :---: |
| Project: | MERIDEN COOPER ST. | Date: | 2/21/2020 |
| Project No. | 403093.2000 .2200 | Verified By: | K. Hyun |
| Title: | STRUCTURAL ANALYSIS OF PROPOSED ANTENNA MOUNT AND PENTHOUSE WALL | Date: | 2/21/2020 |

BLACK \& VEATCH

## 6. ATTACHMENTS



MT-222
Adjustable Wall Mount for solid walls, 6 in stand-off

## Dimensions

| Height | 203.2 mm \| 8.0 in |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Length | 152.4 mm \| 6.0 in |  |  |
| Pipe Outer Diameter | $23 / 8 \mathrm{in} \mathrm{\mid} 27 / 8 \mathrm{in} \mathrm{\mid} 31 / 2 \mathrm{in} \mathrm{\mid} 41 / 2 \mathrm{in}$ |  |  |
| Width | $203.2 \mathrm{~mm} \mid 8.0 \mathrm{in}$ |  |  |
| Weight | $20.6 \mathrm{~kg} \mathrm{\mid} 45.5 \mathrm{lb}$ |  |  |

## Environmental Specifications

Wind Rating For specifications—contact 828-324-2200 or 1-800-982-1708 (toll free), or your local CommScope representative

## General Specifications

Product Type
Mounting
Stand-off Distance
Includes
Material Type
Package Quantity

Wall mount
Solid walls
152.4 mm | 6.0 in

Backing plates or anchors | Wall brackets (2)
Hot dip galvanized steel
2



| 140-222 MHz |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Model Number | DS1E03F36D-D | DS1F03F36D-D | DS1G03F36D-D | DS2C00F36D-D | DS2C03F36D-D |
|  | Input Connector | 7/16 DIN | 7/16 DIN | 7/16 DIN | 7/16 DIN | 7/16 DIN |
|  | Type | Dual | Dual | Dual | Dual | Dual |
|  | Frequency | 140-150 MHz | 150-164 MHz | 160-174 MHz | 217-222 MHz | 217-222 MHz |
|  | Bandwidth | 11 MHz | 15 MHz | 15 MHz | 6 MHz | 6 MHz |
|  | Power | 500 Watts | 500 Watts | 500 Watts | 500 Watts | 500 Watts |
|  | Gain | 3 dBd | 3 dBd | 3 dBd | 0 dBd | 3 dBd |
|  | Horizontal Beamwidth | $360{ }^{\circ}$ | $360^{\circ}$ | $360^{\circ}$ | $360^{\circ}$ | $360^{\circ}$ |
|  | Vertical Beamwidth | $30^{\circ}$ | $30^{\circ}$ | $30^{\circ}$ | $60^{\circ}$ | $30^{\circ}$ |
|  | Beam Tilt | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ |
|  | Isolation (minimum) | 30 | 30 | 30 dB | 30 dB | 30 dB |
| MECHANICAL | Number of Connectors | 2 | 2 | 2 | 2 | 2 |
|  | Flat Plate Area | $4.1 \mathrm{ft}^{2}\left(0.38 \mathrm{~m}^{2}\right)$ | $4.5 \mathrm{ft}^{2}\left(0.42 \mathrm{~m}^{2}\right)$ | $4.5 \mathrm{ft}^{2}\left(0.42 \mathrm{~m}^{2}\right)$ | $2.4 \mathrm{ft}^{2}\left(0.22 \mathrm{~m}^{2}\right)$ | $4.1 \mathrm{ft}^{2}\left(0.38 \mathrm{~m}^{2}\right)$ |
|  | Lateral Windload Thrust | $169 \operatorname{lbf}($ ( 752 N ) | 169 lbf (752 N) | 169 lbf (752 N) | $90 \mathrm{lbf}(400 \mathrm{~N})$ | 169 lbf (752 N) |
|  | Survival Wind Speed |  |  |  |  |  |
|  | without ice with 0.5 " radial ice | 75 mph (121 kph) <br> $65 \mathrm{mph}(105 \mathrm{kph})$ | 75 mph (121 kph) <br> $65 \mathrm{mph}(105 \mathrm{kph})$ | 75 mph (121 kph) 65 mph (105 kph) | 130 mph (209 kph) <br> 115 mph ( 185 kph ) | $75 \mathrm{mph}(121 \mathrm{kph})$ <br> $65 \mathrm{mph}(105 \mathrm{kph})$ |
|  | Mounting Hardware included | DSH3V3N | DSH3V3N | DSH3V3N | DSH3V3R | DSH3V3N |
| 0$\frac{0}{2}$$\frac{0}{2}$$\frac{11}{2}$$\frac{1}{2}$ | Length | 24.3 ft (7.4 m) | 22.3 ft (6.8 m) | 22.3 ft (6.8 m) | 13.6 ft (4.1 m) | 24.3 ft (7.4 m) |
|  | Radome O.D. | $3 \mathrm{in}(7.6 \mathrm{~cm})$ | $3 \mathrm{in}(7.6 \mathrm{~cm})$ | $3 \mathrm{in}(7.6 \mathrm{~cm})$ | $3 \mathrm{in}(7.6 \mathrm{~cm})$ | $3 \mathrm{in}(7.6 \mathrm{~cm})$ |
|  | Mast O.D. | $2.5 \mathrm{in}(6.4 \mathrm{~cm})$ | 2.5 in (6.4 cm ) | 2.5 in (6.4 cm ) | 2.5 in (6.4 cm ) | $2.5 \mathrm{in}(6.4 \mathrm{~cm})$ |
|  | Net Weight w/o bracket | $70 \mathrm{lb}(31.8 \mathrm{~kg})$ | $63 \mathrm{lb}(28.6 \mathrm{~kg})$ | $63 \mathrm{lb}(28.6 \mathrm{~kg})$ | $40 \mathrm{lb}(18.1 \mathrm{~kg})$ | $70 \mathrm{lb}(31.8 \mathrm{~kg})$ |
|  | Shipping Weight | $100 \mathrm{lb}(45.4 \mathrm{~kg})$ | $93 \mathrm{lb}(42.2 \mathrm{~kg})$ | $93 \mathrm{lb}(42.2 \mathrm{~kg})$ | $70 \mathrm{lb}(31.8 \mathrm{~kg})$ | $100 \mathrm{lb}(45.4 \mathrm{~kg})$ |

Antenna Patterns on the next page.

## ANTENNA PATTERNS




## Address:

No Address at This Location

## ASCE 7 Hazards Report



## Data Source:

## Date Accessed:

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 3\% probability of exceedance in 50 years (annual exceedance probability $=$ $0.000588, \mathrm{MRI}=1,700$ years )

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

## Seismic

Site Soil Class: D - Stiff Soil

Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.183 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.063 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.293 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.151 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.195 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.101 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.094 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.15 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1.25 |

## Seismic Design Category <br> B




## Data Accessed:

Date Source:

Wed Dec 042019
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

## Ice

## Results

Ice Thickness: $\quad 0.75 \mathrm{in}$.

Concurrent Temperature: 15 F
Gust Speed: $\quad 50 \mathrm{mph}$
Data Source:
Date Accessed:
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed Dec 042019
Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

## Snow

## Results:

Ground Snow Load, $\mathrm{p}_{\mathrm{g}}$ : $\quad 30 \mathrm{lb} / \mathrm{ft}^{2}$
Elevation:
Data Source:
Date Accessed:
127.1 ft

ASCE/SEI 7-10, Fig. 7-1.
Wed Dec 042019
Values provided are ground snow loads. In areas designated "case study required," extreme local variations in ground snow loads preclude mapping at this scale. Site-specific case studies are required to establish ground snow loads at elevations not covered.

## ATTACHMENT D - PROOF OF DELIVERY OF NOTICE





ATTACHMENT E - POWER DENSITY REPORT

# Calculated Radio Frequency Emissions Report EVERS=URCE ENERGY 

ES-281

## 46 Cooper Street

Meriden, CT 06451

## Table of Contents

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## 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed Eversource installation to be located on the rooftop of 46 Cooper Street in Meriden, CT.

Eversource is proposing to install an omnidirectional antenna as part of its 220 MHz communications system.
This report considers the planned antenna configuration as provided by Eversource along with power density information of the existing antennas to calculate the cumulative \% MPE (Maximum Permissible Exposure) of the proposed facility at ground level.

## 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz . The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter ( $\mathrm{mW} / \mathrm{cm}^{2}$ ). The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

## 3. Power Density Calculation Methods

The power density calculation results were generated using the following formula as outlined in FCC bulletin OET 65, and Connecticut Siting Council recommendations:

Power Density $=\left(\frac{1.6^{2} \times 1.64 \times \text { ERP }}{4 \pi \times R^{2}}\right) X$ Off Beam Loss

Where:
EIRP $=$ Effective Isotropic Radiated Power $=1.64 \times$ ERP
$\mathrm{R}=$ Radial Distance $=\sqrt{\left(H^{2}+V^{2}\right)}$
$\mathrm{H}=$ Horizontal Distance from antenna
$\mathrm{V}=$ Vertical Distance from radiation center of antenna
Ground reflection factor of 1.6
Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and full power, and that all antenna channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not consider actual terrain elevations which could attenuate the signal. Furthermore, all antennas on the rooftop are assumed to in the same location. As a result, the calculated power density and corresponding \% MPE levels reported below are much higher than the actual levels will be from the final installation.

## 4. Calculated \% MPE Results

Table 1 below outlines the power density information for the site. The proposed Eversource omnidirectional antenna has a relatively narrow vertical beamwidth of $30^{\circ}$; therefore, the majority of the RF power is focused out towards the horizon. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the facility. The vertical patterns of the other existing antennas also exhibit varying degrees of directionality. Please refer to Attachment C for the vertical pattern of the existing and proposed Eversource antenna. The calculated results in Table 1 for the Eversource antennas include a nominal of 10 dB off-beam pattern loss for the antennas to account for the lower relative gain below the antennas.

| Carrier | Antenna <br> Height <br> (Feet) | Operating <br> Frequency <br> (MHz) | Number of <br> Trans. | ERP Per <br> Transmitter <br> (Watts) | Power Density <br> $\left(\mathbf{m w} / \mathbf{c m}^{2}\right)$ | Limit | \%MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Eversource | 33 | 37.62 | 1 | 120 | 0.0059 | 0.2000 | $2.96 \%$ |
| Eversource | 35 | 37.84 | 1 | 120 | 0.0051 | 0.2000 | $2.57 \%$ |
| Eversource | 51.4 | 173.25 | 1 | 380 | 0.0066 | 0.2000 | $3.32 \%$ |
| Eversource | 45.3 | 938 | 1 | 240 | 0.0056 | 0.6256 | $0.89 \%$ |
| Eversource | 48 | 217 | 4 | 124 | 0.0101 | 0.2000 | $5.06 \%$ |

Table 1: Proposed Tower \% MPE 123

[^3]
## 5. Conclusion

The above analysis concludes that RF exposure at ground level with the proposed antenna installation will be below the maximum power density limits as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Using the conservative calculation methods discussed herein, the highest expected percent of Maximum Permissible Exposure at ground level with the proposed installation is $\mathbf{1 4 . 8 0 \%}$ of the FCC General Population/Uncontrolled limit.

As noted previously, the calculated \% MPE levels are more conservative (higher) than the actual levels will be from the finished installation.

## 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in FCC OET Bulletin 65 Edition 97-01, IEEE Std. C95.1, and IEEE Std. C95.3.


Report Prepared By: Sokol Andoni
RF Engineer
C Squared Systems, LLC

## Keith Vellante

Reviewed/Approved By: Keith Vellante
Director of RF Services
C Squared Systems, LLC
© squared Systems, LLC

March 4, 2020
Date

March 6, 2020
Date

## Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering \& Technology
IEEE C95.1-2005, IEEE Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz IEEE-SA Standards Board

IEEE C95.3-2002 (R2008), IEEE Recommended Practice for Measurements and Computations of Radio Frequency Electromagnetic Fields With Respect to Human Exposure to Such Fields, $100 \mathrm{kHz}-300 \mathrm{GHz}$ IEEE-SA Standards Board

## Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)

(A) Limits for Occupational/Controlled Exposure ${ }^{4}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength (E) <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength (E) <br> $(\mathrm{A} / \mathrm{m})$ | Power Density $(\mathrm{S})$ <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-3.0$ | 614 | 1.63 | $(100)^{*}$ | 6 |
| $3.0-30$ | $1842 / \mathrm{f}$ | $4.89 / \mathrm{f}$ | $\left(900 / \mathrm{f}^{2}\right)^{*}$ | 6 |
| $30-300$ | 61.4 | 0.163 | 1.0 | 6 |
| $300-1500$ | - | - | $\mathrm{f} / 300$ | 6 |
| $1500-100,000$ | - | - | 5 | 6 |

(B) Limits for General Population/Uncontrolled Exposure ${ }^{5}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength (E) <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength $(\mathrm{E})$ <br> $(\mathrm{A} / \mathrm{m})$ | Power Density (S) <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-1.34$ | 614 | 1.63 | $(100)^{*}$ | 30 |
| $1.34-30$ | $824 / \mathrm{f}$ | $2.19 / \mathrm{f}$ | $\left(180 / \mathrm{f}^{2}\right)^{*}$ | 30 |
| $30-300$ | 27.5 | 0.073 | 0.2 | 30 |
| $300-1500$ | - | - | f 1500 | 30 |
| $1500-100,000$ | - | - | 1.0 | 30 |
| $\mathrm{f}=$ frequency in MHz * Plane-wave equivalent power density |  |  |  |  |

Table 2: FCC Limits for Maximum Permissible Exposure (MPE)

[^4]

Figure 1: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

## Attachment C: Eversource Antenna Data Sheets and Electrical Patterns

| 38 MHz |  |  |
| :---: | :---: | :---: |
| Manufacturer: <br> Model \#: <br> Frequency Band: <br> Gain: <br> Vertical <br> Beamwidth: <br> Horizontal <br> Beamwidth: <br> Polarization: <br> Length: | Amphenol <br> MA431E40 <br> $34.3-40.8 \mathrm{MHz}$ <br> 0.0 dBd <br> $84^{\circ}$ <br> $360^{\circ}$ <br> Vertical- <br> Polarization <br> 16.2' | Vertical |
| 173 MHz |  |  |
| Manufacturer: <br> Model \#: <br> Frequency Band: <br> Gain: <br> Vertical <br> Beamwidth: <br> Horizontal <br> Beamwidth: <br> Polarization: <br> Length: | Commander $220-7 \mathrm{~N}$ $165-174 \mathrm{MHz}$ 5.25 dBd $18^{\circ}$ $360^{\circ}$ Vertical- $^{\text {Polarization }}$ $19^{\prime}$ | Vertical Pattern |
| $217 \mathrm{MHz}$ |  | DS2C03F36D-N DS2C03F36D-D |
| Manufacturer: <br> Model \#: <br> Frequency Band: <br> Gain: <br> Vertical <br> Beamwidth: <br> Horizontal <br> Beamwidth: <br> Polarization: <br> Length: | dbSpectra <br> DS2C03F36D <br> $217-222 \mathrm{MHz}$ <br> 3.0 dBd <br> $30^{\circ}$ <br> $360^{\circ}$ <br> Vertical- <br> Polarization <br> 24.3' |  <br> Top  <br> Bottom |


| 938 MHz |  |
| ---: | :--- |
| Manufacturer: | CommScope |
| Model \#: | DB589-Y |
| Frequency Band: | $890-960 \mathrm{MHz}$ |
| Gain: | 9.0 dBd |
| Vertical Beamwidth: | $30^{\circ}$ |
| Length: | 9.2 |


[^0]:    ${ }^{1}$ It should be noted that the number of transmitting antennas accounted for in the Power Density Report accounts for two channels on the $88^{\prime}$ centerline antenna. Also, the "Antenna Height" column on Table 1 in the Power Density Report only accounts for the centerline of the Transmit or "TX" antenna centerline.

[^1]:    * Note: The \% ratio rating per TIA-222-H Section 15.5.

[^2]:    Member Distributed Loads (BLC 4 : Wind - 90 Deq (+Z))
    Member Label Direction Start Magnitude[lb/ft,F,psf] End Magnitude[lb/...Start Location[ft,\%] End Location[ft,\%]

[^3]:    ${ }^{1}$ The operating parameters for the existing Eversource antennas were taken from a survey report conducted by C Squared Systems on October 11, 2013 and recently confirmed through Eversource's agent. Please note that \% MPE values listed are rounded to two decimal points and the total \% MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not identically match the total value reflected in the table.
    ${ }^{2}$ The heights listed for the proposed (highlighted in blue) and existing Eversource antennas are in reference to Black \& Veatch construction drawing dated 01/07/2020 (Rev. A).
    ${ }^{3}$ In cases where Eversource antennas were unable to be identified during the 2013 field survey ( 37.76 MHz and 37.84 MHz ), an antenna model with like characteristics was considered in this analysis.

[^4]:    ${ }^{4}$ Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure
    ${ }^{5}$ General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure

