

**JULIE D. KOHLER**

PLEASE REPLY TO: Bridgeport  
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April 8, 2015

Attorney Melanie Bachman  
Acting Executive Director  
Connecticut Siting Council  
Ten Franklin Square  
New Britain, CT 06051

**Re: Notice of Exempt Modification  
UCONN/T-Mobile equipment upgrade  
Site ID CT11303B  
82 North Eagleville Road, Mansfield (Storrs) CT**

Dear Attorney Bachman:

This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, UCONN owns the existing telecommunications tower and related facility at 82 North Eagleville Road, Mansfield (Storrs) Connecticut (latitude 41.814537, longitude - 72.259742). T-Mobile intends to add three (3) antennas and related equipment at this existing facility at UCONN ("UCONN Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Mayor of Mansfield, Elizabeth C. Paterson and the property owner, the University of Connecticut.

The existing UCONN Facility consists of a 245 foot lattice tower.<sup>1</sup> T-Mobile plans to add three (3) antennas and three (3) RRU (remote radio units) mounted on the tower at a centerline of 235 feet. (See the plans dated February 18, 2015 attached hereto as Exhibit A). The existing tower is structurally capable of supporting T-Mobile's proposed use assuming the modifications detailed in the structural analysis and modification report are implemented. See the structural analysis and modification report dated April 1, 2015 and attached hereto as Exhibit B.<sup>2</sup>

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<sup>1</sup> The Connecticut Siting Council database does not contain any Dockets or Petitions relative to this Facility however there is notices of intent captioned EM-SPRINT-078-150213, EM-T-MOBILE-078-120614 and EM-VER-078-100114.

<sup>2</sup> T-Mobile will implement the modifications shown on SK-1 through SK-3 of the report prior to installation of the proposed equipment.



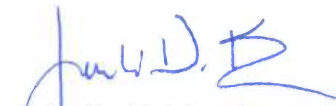
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The planned modifications to the UCONN Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

- 1 . The proposed modification will not increase the height of the tower. T-Mobile's additional antennas and equipment will be installed at the 235 foot level. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.
- 2 . T-Mobile does not propose any changes to the existing compound area, so no extension of the site boundaries is required.
- 3 . The proposed modification to the Facility will not increase the noise levels at the existing facility by six decibels or more.
- 4 . The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a RF Exposure Analysis prepared by EBI dated March 25, 2105 T-Mobile' operations would add 2.30% of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be 10.19% of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, T-Mobile respectfully submits that the proposed additional antennas and equipment at the UCONN Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,



Julie D. Kohler, Esq.

cc: Mayor Elizabeth C. Paterson, Town of Mansfield  
University of Connecticut  
Mark Richard, T-Mobile  
Sheldon Freinkle, NSS





T-MOBILE USA, INC.  
12920 SE 38TH STREET  
BELLEVUE, WA 98006  
(425) 378-4000

3050106  
2/23/2015  
2000011160

Invoice Number	Inv. Date	Description	Deductions	Voucher	Amount Paid
CT11303B-1	2/19/2015	Exempt Mod Filing Fees	0.00	1100314072	625.00

DO NOT ACCEPT THIS CHECK UNLESS THE FACE FADES FROM BLACK TO RED WITH LOGO IN BACKGROUND. THE BACK OF THIS DOCUMENT HAS HEAT-SENSITIVE INK THAT CHANGES FROM ORANGE TO YELLOW.



T-MOBILE USA, INC.  
12920 SE 38th Street  
Bellevue, WA 98006  
(425) 378-4000

The Bank of New York Mellon  
Pittsburgh, PA  
60160/433

3050106  
2/23/2015  
VID 2000011160

PAY **\$625.00**  
SIX TWO FIVE CTS CTS

**\*\$625.00**

\*\*\*Six Hundred Twenty Five Dollars Only\*\*\*

To  
The  
Order  
Of

CONNECTICUT SITING COUNCIL  
10 FRANKLIN SQ  
NEW BRITAIN, CT 06051

VOID AFTER 180 DAYS  
THIS CHECK CLEARS THROUGH POSITIVE PAY

0003050106 043301601 0138430



# EXHIBIT A







ELECTRICAL NOTES:

1. INCLUDE ALL LABOR, MATERIALS, EQUIPMENT, PLANT SERVICES AND ADMINISTRATIVE TASKS REQUIRED TO COMPLETE AND MAKE OPERABLE THE ELECTRICAL WORK SHOWN ON THE DRAWINGS AND SPECIFIED HEREIN, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:  
A. PREPARE AND SUBMIT SHOP DRAWINGS, DIAGRAMS AND ILLUSTRATIONS.  
B. PROCURE ALL NECESSARY PERMITS AND APPROVALS AND PAY ALL REQUIRED FEES AND CHARGES IN CONNECTION WITH THE WORK OF THIS CONTRACT.  
C. SUBMIT AS-BUILT DRAWINGS, OPERATING AND MAINTENANCE INSTRUCTIONS AND MANUALS.  
D. EXECUTE ALL CUTTING, DRILLING, ROUGH AND FINISH PATCHING OF EXISTING OR NEWLY INSTALLED CONSTRUCTION REQUIRED FOR THE WORK OF THIS CONTRACT. FOR SLAB PENETRATIONS THROUGH POST TENSION SLABS, X-RAY EXACT AREA OF PENETRATION PRIOR TO PERFORMING WORK.  
E. COORDINATE ALL X-RAY WORK WITH BUILDING ENGINEER, PROVIDE HANGERS, SUPPORTS, FOUNDATIONS, STRUCTURAL FRAMING SUPPORTS, AND BASES FOR CONDUIT AND EQUIPMENT PROVIDED OR INSTALLED UNDER THE WORK OF HIS CONTRACT. PROVIDE COUNTER FLASHING, SLEEVES AND SEALS FOR FLOOR AND WALL PENETRATIONS.  
F. MAINTAIN ALL EXISTING ELECTRICAL SERVICES IN THE BUILDING AREAS NOT AFFECTED BY THE ALTERATION DURING THE PROGRESS OF THE WORK INCLUDING PROVIDING ALL TEMPORARY JUMPERS, CONDUITS, CAPS, PROTECTIVE DEVICES, CONNECTIONS AND EQUIPMENT REQUIRED. PROVIDE TEMPORARY LIGHT AND POWER FOR CONSTRUCTION PURPOSES.  
2. IT IS THE INTENT OF THESE DRAWINGS AND SPECIFICATIONS TO CALL FOR AN INSTALLATION THAT IS COMPLETE IN EVERY RESPECT. IT IS NOT THE INTENT TO GIVE EVERY DETAIL ON THE DRAWINGS AND THE SPECIFICATIONS. IF AN ITEM OF WORK IS INDICATED IN THE DRAWINGS, IT IS CONSIDERED SUFFICIENT FOR INCLUSION IN THE CONTRACT. FURNISH AND INSTALL ALL MATERIAL AND EQUIPMENT USUALLY FURNISHED OR NEEDED TO MAKE A COMPLETE INSTALLATION WHETHER OR NOT SPECIFICALLY MENTIONED IN THE CONTRACT DOCUMENTS.
- GENERAL REQUIREMENTS  
1. PROVIDE ALL WORK IN ACCORDANCE WITH THE NATIONAL ELECTRICAL CODE (NEC) AND LOCAL AND STATE ELECTRICAL CODES.  
2. THE ELECTRICAL PLANS ARE DIAGRAMATIC ONLY. REFER TO THE ARCHITECTURAL PLANS FOR THE EXACT DIMENSIONS OF THE BUILDING.  
3. LOAD CALCULATIONS ARE BASED ON EXISTING BUILDING INFORMATION/DRAWINGS PROVIDED TO ENGINEERING. CONTRACTOR IS TO VERIFY ALL EXISTING RATINGS AND LOADS PRIOR TO PURCHASING OF SPECIED EQUIPMENT FOR COMPLIANCE TO NEC. CONTRACTOR TO NOTIFY ENGINEER OF ANY DISCREPANCIES AND REQUEST FURTHER DIRECTION BY ENGINEER.  
4. EXISTING BUILDING EQUIPMENT IS NOTED ON THE DRAWINGS. NEW OR RELOCATED EQUIPMENT IS SHOWN WITH SOLID LINES. FUTURE EQUIPMENT (NOT IN THIS CONTRACT) IS DEPICTED WITH SHADOWED LINES. REQUEST CLARIFICATION OF DRAWINGS OR SPECIFICATIONS PRIOR TO PRICING OR INSTALLATION.  
5. GENERAL  
A. AFTER CAREFULLY STUDYING THE DRAWINGS AND SPECIFICATIONS, AND BEFORE SUBMITTING THE PROPOSAL, MAKE A MANDATORY SITE VISIT TO ASCERTAIN CONDITIONS OF THE SITE, AND THE NATURE AND EXACT QUANTITY OF WORK TO BE PERFORMED. NO EXTRA COMPENSATION WILL BE ALLOWED FOR FAILURE TO NOTIFY THE OWNER, IN WRITING, OF ANY DISCREPANCIES THAT MAY HAVE BEEN NOTED BETWEEN THE EXISTING CONDITIONS AND THE DRAWINGS AND SPECIFICATIONS.  
B. VERIFY ALL MEASUREMENTS AT THE SITE AND BE RESPONSIBLE FOR CORRECTNESS OF SAME.  
6. QUALITY, WORKMANSHIP, MATERIALS AND SAFETY  
A. PROVIDE NEW MATERIALS AND EQUIPMENT OF A DOMESTIC MANUFACTURER BY THOSE REGULARLY ENGAGED IN THE PRODUCTION AND MANUFACTURE OF SPECIFIED MATERIALS AND EQUIPMENT. WHERE UL, OR OTHER AGENCY, HAS ESTABLISHED STANDARDS FOR MATERIALS, PROVIDE MATERIALS WHICH ARE LISTED AND LABELED ACCORDINGLY. THE COMMERCIALLY STANDARD ITEMS OF EQUIPMENT AND THE SPECIFIC NAMES MENTIONED HEREIN ARE INTENDED FOR THE PROPER FUNCTIONING OF THE WORK.  
B. WORK SHALL BE PERFORMED BY WORKMEN SKILLED IN THE TRADE REQUIRED FOR THE WORK. INSTALL MATERIALS AND EQUIPMENT TO PRESENT A NEAT APPEARANCE WHEN COMPLETED AND IN ACCORDANCE WITH THE APPROVED RECOMMENDATIONS OF THE MANUFACTURER AND IN ACCORDANCE WITH CONTRACT DOCUMENTS.  
C. PROVIDE LABOR, MATERIALS, APPARATUS AND APPLIANCES ESSENTIAL TO THE FUNCTIONING OF THE SYSTEMS DESCRIBED OR INDICATED HEREIN, OR WHICH MAY BE REASONABLY IMPLIED AS ESSENTIAL, WHENEVER MENTIONED IN THE CONTRACT DOCUMENT OR NOT.  
D. MAKE WRITTEN REQUESTS FOR SUPPLEMENTARY INSTRUCTIONS TO ARCHITECT/ENGINEER IN CASE OF DOUBT AS TO WORK INTENDED OR IN EVENT OF NEED FOR EXPLANATION THEREOF.  
E. PERFORMANCE AND MATERIAL REQUIREMENTS SCHEDULED OR SPECIFIED ARE MINIMUM STANDARD ACCEPTABLE. THE RIGHT TO JUDGE THE QUALITY OF EQUIPMENT THAT DEVIATES FROM THE CONTRACT DOCUMENT REMAINS SOLELY WITH ARCHITECT/ENGINEER. CONTRACT DOCUMENT OR NOT.
- GUARANTEE  
1. GUARANTEE MATERIALS, PARTS AND LABOR FOR WORK FOR ONE YEAR FROM THE DATE OF ISSUANCE OF OCCUPANCY PERMIT. DURING THAT PERIOD, MAKE GOOD FAILURES OR IMPERFECTIONS THAT MAY ARISE DUE TO DEFECTS OR OMISSIONS IN MATERIALS OR WORKMANSHIP WITH NO ADDITIONAL COMPENSATION AND AS DIRECTED BY ARCHITECT.

CLEANING

1. REMOVE ALL CONSTRUCTION DEBRIS RESULTING FROM THE WORK.  
2. CLEAN EQUIPMENT AND SYSTEMS FOLLOWING THE COMPLETION OF THE PROJECT TO THE SATISFACTION OF THE ENGINEER.
- COORDINATION AND SUPERVISION  
1. CAREFULLY LAY OUT ALL WORK IN ADVANCE TO AVOID UNNECESSARY CUTTING, CHAMFERING, CHASING OR DRILLING OF FLOORS, WALLS, PARTITIONS, CEILINGS OR OTHER SURFACES. BEFORE SUCH WORK IS NECESSARY, HOWEVER, PATCH AND REPAIR THE WORK IN AN APPROPRIED MANNER BY SKILLED MECHANICS AT NO ADDITIONAL COST TO THE OWNER. RENDER FULL COOPERATION TO OTHER TRADES WHERE WORK WILL BE INSTALLED IN CLOSE PROXIMITY TO WORK OF OTHER TRADES. ASSIST IN WORKING OUT SPACE CONDITIONS. IF WORK IS CAUSED INTERFERENCE, MAKE CHANGES NECESSARY TO CORRECT CONDITIONS WITHOUT EXTRA CHARGE.

SUBMITTALS

1. AS-BUILT DRAWINGS:  
A. UPON COMPLETION OF THE WORK, FURNISH TO THE OWNER TWO-SET BUILD DRAWINGS.  
2. SERVICE MANUALS.  
A. UPON COMPLETION OF THE WORK, FULLY INSTRUCT T-MOBILE AS TO THE OPERATION AND MAINTENANCE OF ALL MATERIAL, EQUIPMENT AND SYSTEMS.  
B. PROVIDE 3 COMPLETE BOUND SETS OF INSTRUCTIONS FOR OPERATING AND MAINTAINING ALL SYSTEMS AND EQUIPMENT.
- CUTTING AND PATCHING  
1. PROVIDE ALL CUTTING, DRILLING, ROUGH AND FINISH PATCHING REQUIRED TO COMPLETE THE WORK.  
2. OBTAIN OWNER APPROVAL PRIOR TO CUTTING THROUGH FLOORS OR WALLS FOR PIPING OR CONDUIT.

TESTS, INSPECTION AND APPROVAL

1. BEFORE ENERGIZING ANY ELECTRICAL INSTALLATION, INSPECT EACH UNIT IN DETAIL. TIGHTEN ALL BOLTS AND CONNECTIONS (TORQUE-TIGHTEN WHERE REQUIRED) AND DETERMINE THAT ALL COMPONENTS ARE ALIGNED, AND THE EQUIPMENT IS IN SAFE, OPERATIONAL CONDITION.  
2. PROVIDE THE COMPLETE ELECTRICAL SYSTEM FREE OF GROUND FAULTS AND SHORT CIRCUITS SUCH THAT THE SYSTEM WILL OPERATE SATISFACTORILY UNDER FULL LOAD CONDITIONS, WITHOUT EXCESSIVE HEATING AT ANY POINT IN THE SYSTEM.
- SPECIAL REQUIREMENTS  
1. DO NOT LEAVE ANY WORK INCOMPLETE NOR ANY HAZARDOUS SITUATIONS CREATED WHICH WILL AFFECT THE LIFE OR SAFETY OF THE PUBLIC AND/OR BUILDING OCCUPANTS. DO NOT INTERFERE WITH OR CUTOFF ANY OF THE EXISTING SERVICES WITHOUT THE OWNER'S WRITTEN PERMISSION.  
2. WHEN NECESSARY TO TEMPORARILY DISCONNECT ANY EXISTING BUILDING UTILITIES AND SERVICE SYSTEMS, INCLUDING FEEDER OR BRANCH CIRCUITING SUPPLYING EXISTING FACILITIES, CONFER WITH THE OWNER AND ARRANGE THE PERIOD OF INTERRUPTION FOR A TIME MUTUALLY AGREED UPON. SHUTDOWN NOTE: SCHEDULE AND NOTIFY OWNER 48 HOURS PRIOR TO SHUTDOWN. ALL SHUTDOWN WORK TO BE SCHEDULED AT A TIME CONVENIENT TO OWNER.

GROUNDING

1. ROUTE ALL GROUNDING CONDUCTORS AS SHOWN ON CONDUIT/GROUNDING RISER.  
2. ROUTE 500 KCMIL CU. THIN CONDUCTOR FROM THE MGB TO LOCATION TO BUILDING STEEL. VERIFY BUILDING STEEL IS EFFECTIVELY GROUNDDED PER NEC TO THE MAIN SERVICE GROUNDING ELECTRODE CONDUCTOR (GEC).  
3. MAKE ALL GROUND CONNECTIONS FROM MGB TO ELECTRICAL EQUIPMENT WITH 2 HOLE, CRIMP TYPE, BURNDY COMPRESSION TERMINATIONS, SIZED AS REQUIRED.  
4. USE 1 HOLE, CRIMP TYPE, BURNDY COMPRESSIONS TERMINATIONS, SIZED AS REQUIRED, AT EQUIPMENT GROUND CONNECTIONS.  
5. HIRE AN INDEPENDENT LAB TO PERFORM THE SPECIFIED OHMS TESTING. PROVIDE 4 SETS OF THE CERTIFIED DOCUMENTS TO THE OWNER FOR VERIFICATION PRIOR TO THE PROJECT COMPLETION.

RACEWAYS

1. ALL WIRING TO BE INSTALLED IN CONDUIT SYSTEMS IN ACCORDANCE WITH THE FOLLOWING:  
A. EXTERIOR FEEDERS AND CONTROL, WHERE UNDERGROUND, TO BE IN SCH 40 PVC.  
B. EXTERIOR, ABOVE GROUND POWER CONDUITS TO BE GALVANIZED RIGID STEEL (RGS).  
C. ALL TELECOMMUNICATION CONDUITS, INTERIOR/EXTERIOR, TO BE BUI.  
D. INSTALL PULL ROPES IN ALL NEW EMPTY CONDUITS INSTALLED ON THIS PROJECT.  
E. ALL TELECOM CONDUITS AND PULL BOXES INSTALLED ON THIS PROJECT TO BE LABELED "T-MOBILE". OWNER WILL PROVIDE LABELS FOR CONTRACTOR TO INSTALL.  
F. INTERIOR FEEDERS TO BE INSTALLED IN EMT, WITH STEEL COMPRESSION FITTINGS.  
G. MINIMUM SIZE CONDUIT TO BE ¾" TRADE SIZE.  
H. UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FINAL CONNECTIONS TO MOTORS AND WIRING EQUIPMENT TO BE INSTALLED IN LIQUID-TIGHT FLEXIBLE METAL CONDUIT.  
I. CONDUIT TO BE RUN CONCEALED IN CEILINGS, FINISHED AREAS OR DRYPALL PARTITIONS, UNLESS OTHERWISE NOTED.  
J. THE ROUTING OF CONDUITS INDICATED ON THE DRAWINGS IS DIAGRAMATIC. BEFORE INSTALLING ANY WORK, EXAMINE THE WORKING LAYOUTS AND SHOP DRAWINGS OF THE OTHER TRADES TO DETERMINE THE EXACT LOCATIONS AND CLEARANCES.  
K. ALL EXTERIOR MOUNTING HARDWARE TO BE GALVANIZED STEEL. COORDINATE WITH BUILDING ENGINEER PRIOR TO ATTACHING TO BUILDING STRUCTURE.

RACEWAYS CONT'D

- L. PENETRATIONS OF WALLS, FLOORS AND ROOFS, FOR THE PASSAGE OF ELECTRICAL RACEWAYS, TO BE PROPERLY SEALED AFTER INSTALLATION OF RACEWAYS SO AS TO MAINTAIN THE STRUCTURAL OR WATERPROOF INTEGRITY OF THE WALL, FLOOR OR ROOF. SYSTEM TO BE PENETRATED, SEAL ALL CONDUIT PENETRATIONS THROUGH FIRE OR SMOKE PARTITIONS TO MAINTAIN PROPER RATING OF WALL OR CEILING.  
M. PROVIDE ALL CONDUIT ENDS WITH INSULATED METALLIC GROUNDING BUSINES.  
N. CONDUIT TO BE SUPPORTED AT MAXIMUM DISTANCE OF 8'-0" OR AS REQUIRED BY NEC, IN HORIZONTAL AND VERTICAL DIRECTIONS.  
O. PROVIDE STAINLESS STEEL BLANK COVER PLATES FOR ALL JUNCTION BOXES AND/OR OUTLET BOXES NOT USED IN EXPOSED AREAS. PROVIDE ALL OTHER UNUSED BOXES WITH STAINLESS STEEL COVER PLATES.  
P. WHERE APPLICABLE, PROVIDE ROOFTOP CONDUIT SUPPORT SYSTEM CONFORMING TO ROOFTOP WARRANTY REQUIREMENTS, PER BUILDING.

WIRES AND CABLES

1. CONTRACTOR TO COORDINATE WITH EQUIPMENT SUPPLIER AND VENDOR FOR EXACT EQUIPMENT OVER-CURRENT PROTECTION VOLTAGE, WIRE SIZE AND PULG CONFIGURATION, IF APPLICABLE, PRIOR TO BID.  
2. ALL EQUIPMENT/DEVICES TO BE PROVIDED WITH INSULATED GROUND CONDUCTOR.  
3. ALL WIRE AND CABLE TO BE 80/20LT, COPPER, WITH THIN/T HIN INSULATION, EXCEPT AS NOTED.  
4. WIRE FOR POWER AND LIGHTING WILL NOT BE LESS THAN NO. 12AWG.  
5. CONTROL WIRING IS NOT TO BE LESS THAN NO. 14AWG. FLEXIBLE IN SINGLE CONDUCTORS OR MULTI-CONDUCTOR CABLES. CONTROL WIRING WILL CONSIST OF MULTI-CONDUCTOR CABLES WHEREVER POSSIBLE. CABLES TO BE PROVIDED WITH AN OVERALL FLAME-RETARDANT, EXTRUDED JACKET AND RATED FOR PLENUM USE. ALL CONTROL WIRE TO BE 80/20LT RATED.  
6. WIRE PREVIOUSLY PULLED INTO CONDUIT IS CONSIDERED USED AND IS NOT TO BE RE-PULLED.  
7. HOME RUNS AND BRANCH CIRCUIT WIRING FOR 20A, 120V CIRCUITS:  
LENGTH (FT.) HOME RUN WIRE SIZE  
0 TO 50 NO. 12  
51 TO 100 NO. 10  
101 TO 150 NO. 8  
8. VOLTAGE DROP IS NOT TO EXCEED 3%.

9. MAKE ALL CONNECTIONS WITH UL APPROVED, SOLDERLESS, PRESSURE-TYPE INSULATED CONNECTORS: SCOTCHLOK OR AND APPROVED EQUAL.

WIRING DEVICES

1. ALL RECEPTACLES INSTALLED IN THIS PROJECT TO BE GROUNDING TYPE, WITH GROUNDING PIN SLOT CONNECTED TO DEVICE GROUND SCREW FOR GROUND WIRE CONNECTION.  
2. DISCONNECT SWITCHES AND FUSES  
1. DISCONNECT SWITCHES TO BE VOLTAGE-RATED TO SUIT THE CHARACTERISTICS OF THE SYSTEM FROM WHICH THEY ARE SUPPLIED.  
2. PROVIDE HEAVY-DUTY, METAL-ENCLOSED, EXTERNALLY-OPERATED DISCONNECT SWITCHES, FUSED OR UNFUSED, OF SUCH TYPE AND SIZE AS REQUIRED TO PROPERLY PROTECT OR DISCONNECT THE LOAD FOR WHICH THEY ARE INTENDED.  
3. PROVIDE NEMA 1 DISCONNECT SWITCHES FOR INTERIOR INSTALLATION. NEMA 3R FOR EXTERIOR INSTALLATION.  
4. DISCONNECT SWITCHES TO BE MANUFACTURED BY:  
A. GENERAL ELECTRIC COMPANY  
B. SQUARE-D  
5. PROVIDE RMC-1 TYPE FUSES, UNLESS NOTED OTHERWISE.  
INSTALLATION  
1. INSTAL DISCONNECT SWITCHES WHERE INDICATED ON DRAWINGS.  
2. INSTAL FUSES IN FUSIBLE DISCONNECT SWITCHES. FUSES MUST MATCH IN TYPE AND RATING.  
3. FUSES TO BE MOUNTED SO THAT THE LABELS SHOWING THEIR RATINGS CAN BE READ WITHOUT REQUIRING FUSE REMOVAL.  
4. FURNISH AND DEPOSIT SPARE FUSES AT THE JOB SITE AS FOLLOWS:  
A. THREE SPARES FOR EACH TYPE AND SIZE, IN EXCESS OF 60A, USED FOR INITIAL FUSING.  
B. TEN PERCENT SPARES FOR EACH TYPE AND SIZE, UP TO WILL LESS THAN THREE FUSES OF ONE PARTICULAR TYPE AND SIZE BE FURNISHED.

GENERAL NOTES:

- INTENT  
1. THESE SPECIFICATIONS AND CONSTRUCTION DRAWINGS ACCOMPANYING THEM DESCRIBE THE WORK TO BE DONE AND THE MATERIALS TO BE FURNISHED FOR CONSTRUCTION.  
2. THE DRAWINGS AND SPECIFICATIONS ARE INTENDED TO BE FULLY EXPLANATORY AND SUPPLEMENTARY. HOWEVER, SHOULD ANYTHING BE SHOWN, INDICATED, OR SPECIFIED ON ONE AND NOT THE OTHER, IT SHALL BE DONE THE SAME AS IF SHOWN, INDICATED OR SPECIFIED IN BOTH.  
3. THE INTENTION OF THE DOCUMENTS IS TO INCLUDE ALL LABOR AND MATERIALS REASONABLY NECESSARY FOR THE PROPER EXECUTION AND COMPLETION OF THE WORK AS STIPULATED IN THE CONTRACT.  
4. THE PURPOSE OF THE SPECIFICATIONS IS TO INTERPRET THE INTENT OF THE DRAWINGS AND TO DESIGNATE THE METHOD OF THE PROCEDURE, TYPE AND QUALITY OF MATERIALS REQUIRED TO COMPLETE THE WORK. THE DESIGN LAYOUT ARE ANTICIPATED MINOR DEVIATIONS FROM THE DESIGN LAYOUT ARE ANTICIPATED AND SHALL BE CONSIDERED AS PART OF THE WORK. NO CHANGES THAT ALTER THE CHARACTER OF THE WORK WILL BE MADE, OR PERMITTED BY THE OWNER WITHOUT ISSUING A CHANGE ORDER.

CONFLICTS

1. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFICATIONS OF ALL MEASUREMENTS AT THE SITE BEFORE ORDERING ANY MATERIALS OR DOING ANY WORK. NO EXTRA CHARGE OR COMPENSATION SHALL BE ALLOWED DUE TO DIFFERENCE BETWEEN ACTUAL DIMENSIONS AND DIMENSIONS INDICATED ON THE CONSTRUCTION DRAWINGS. ANY SUCH DISCREPANCY IN DIMENSION WHICH MAY BE FOUND SHALL BE SUBMITTED TO THE OWNER FOR CONSIDERATION BEFORE THE CONTRACTOR PROCEEDS WITH THE WORK IN THE AFFECTED AREAS.  
2. THE BIDDER, IF AWARDED THE CONTRACT, WILL NOT BE ALLOWED ANY EXTRA COMPENSATION BY REASON OF ANY MATERIAL OR THING CONCERNING SUCH BIDDER MIGHT HAVE FULLY INFORMED THEMSELVES PRIOR TO THE BIDDING.  
3. NO PLEA OF IGNORANCE OF CONDITIONS THAT EXIST, OR OF DIFFICULTIES OR CONDITIONS THAT MAY BE ENCOUNTERED, OR OF ANY OTHER RELEVANT MATTER CONCERNING THE WORK TO BE PERFORMED IN THE EXECUTION OF THE WORK WILL BE ACCEPTED AS AN EXCUSE FOR ANY FAILURE OR OMISSION ON THE PART OF THE CONTRACTOR TO FULFILL EVERY DETAIL OF ALL THE REQUIREMENTS OF THE CONTRACT DOCUMENTS GOVERNING THE WORK.

CONTRACTS AND WARRANTIES

1. CONTRACTOR IS RESPONSIBLE FOR APPLICATION AND PAYMENT OF CONTRACTOR LICENSES AND BONDS.  
2. SEE MASTER CONTRACTION SERVICES AGREEMENT FOR ADDITIONAL DETAILS.

STORAGE

1. ALL MATERIALS MUST BE STORED IN A LEVEL AND DRY FASHION AND IN A MANNER THAT DOES NOT NECESSARILY OBSTRUCT THE FLOW OF OTHER WORK. ANY STORAGE METHOD MUST MEET ALL RECOMMENDATIONS OF THE ASSOCIATED MANUFACTURER.

CLEANUP

1. THE CONTRACTORS SHALL, AT ALL TIMES, KEEP THE SITE FREE FROM ACCUMULATION OF WASTE MATERIALS OR RUBBISH CAUSED BY THEIR EMPLOYEES AT WORK AND AT THE COMPLETION OF THE WORK, THEY SHALL REMOVE ALL RUBBISH FROM AND ABOUT THE BUILDING AREA, INCLUDING ALL THEIR TOOLS, SCRAPFOLDING AND SUPPLUS MATERIALS AND SHALL LEAVE THEIR WORK CLEAN AND READY TO USE.  
2. EXTERIOR  
A. VISUALLY INSPECT EXTERIOR SURFACES AND REMOVE ALL TRACES OF SOIL, WASTE MATERIALS, SMUDGES AND OTHER FOREIGN MATTER.  
B. REMOVE ALL TRACES OF SPLASHED MATERIALS FROM ADJACENT SURFACES.  
C. IF NECESSARY, TO ACHIEVE A UNIFORM DEGREE OF CLEANLINESS, HOSE DOWN THE EXTERIOR OF THE STRUCTURE.

3. INTERIOR  
A. VISUALLY INSPECT INTERIOR SURFACE AND REMOVE ALL TRACES OF SOIL, WASTE MATERIALS, SMUDGES AND OTHER FOREIGN MATTER FROM WALLS, FLOOR, AND CEILING.  
B. REMOVE ALL TRACES OF SPLASHED MATERIALS FROM ADJACENT SURFACES.  
C. REMOVE PAINT DROPPINGS, SPOTS, STAINS, AND DIRT FROM FINISHED SURFACES.

CHANGE ORDER PROCEDURE:

1. REFER TO SECTION 17 OF SIGNED MCSA: SEE PROFESSIONAL SERVICE AGREEMENT FOR MCSA.  
RELATED DOCUMENTS AND COORDINATION  
1. GENERAL CARPENTRY, ELECTRICAL AND ANTENNA DRAWINGS ARE INTERRELATED. IN PERFORMANCE OF THE WORK, THE CONTRACTOR MUST REFER TO ALL DRAWINGS. ALL COORDINATION TO BE THE RESPONSIBILITY OF THE CONTRACTOR.  
SHOP DRAWINGS  
1. CONTRACTOR SHALL SUBMIT SHOP DRAWINGS AS REQUIRED AND LISTED IN THESE SPECIFICATIONS TO THE OWNER FOR APPROVAL.  
2. ALL SHOP DRAWINGS SHALL BE REVIEWED, CHECKED AND CORRECTED BY CONTRACTOR PRIOR TO SUBMITTAL TO THE OWNER.

PRODUCTS AND SUBSTITUTIONS

1. SUBMIT 3 COPIES OF EACH REQUEST FOR SUBSTITUTION. IN EACH REQUEST, IDENTIFY THE PRODUCT OR FABRICATION OR INSTALLATION METHOD TO BE REPLACED BY THE SUBSTITUTION. INCLUDE RELATED SPECIFICATION SECTION AND DRAWING NUMBERS AND COMPLETE DOCUMENTATION SHOWING COMPLIANCE WITH THE REQUIREMENTS FOR SUBSTITUTIONS.  
2. SUBMIT ALL NECESSARY PRODUCT DATA AND CUT SHEETS WHICH PROPERLY IDENTIFY AND DESCRIBE THE ITEMS. PRODUCTS AND MATERIALS BEING INSTALLED. THE CONTRACTOR SHALL, IF DEEMED NECESSARY BY THE OWNER, SUBMIT ACTUAL SAMPLES TO THE OWNER FOR APPROVAL IN LIEU OF CUT SHEETS.

QUALITY ASSURANCE

1. ALL WORK SHALL BE IN ACCORDANCE WITH APPLICABLE LOCAL, STATE AND FEDERAL REGULATIONS. THESE SHALL INCLUDE, BUT NOT BE LIMITED TO THE APPLICABLE CODES SET FORTH BY THE LOCAL GOVERNING BODY. SEE "CODE COMPLIANCE" 1-1.
- ADMINISTRATION  
1. BEFORE THE COMPLETMENT OF ANY WORK, THE CONTRACTOR WILL ASSIGN A PROJECT MANAGER WHO WILL ACT AS A SINGLE POINT OF CONTACT FOR ALL PERSONNEL INVOLVED IN THIS PROJECT. THIS PROJECT MANAGER WILL DEVELOP A MASTER SCHEDULE FOR THE PROJECT WHICH WILL BE SUBMITTED TO THE OWNER PRIOR TO THE COMENCEMENT OF ANY WORK.  
2. SUBMIT A BAR TYPE PROGRESS CHART, NOT MORE THAN 3 DAYS AFTER THE DATE ESTABLISHED FOR COMENCEMENT OF THE WORK ON THE SCHEDULE, INDICATING A TIME BAR FOR EACH MAJOR CATEGORY OR UNIT OF WORK TO BE PERFORMED AT THE SITE. PROPERLY SEQUENCED AND COORDINATED WITH OTHER ELEMENTS OF WORK AND SHOWING COMPLETION OF THE WORK SUFFICIENTLY IN ADVANCE OF THE DATE ESTABLISHED FOR SUBSTANTIAL COMPLETION OF THE WORK.  
3. PRIOR TO COMMENCING CONSTRUCTION, THE OWNER SHALL SCHEDULE AN ON-SITE MEETING WITH ALL MAJOR PARTIES. THIS WOULD INCLUDE, BUT NOT LIMITED TO, THE OWNER, PROJECT MANAGER, CONTRACTOR, LAND OWNER REPRESENTATIVE, LOCAL TELEPHONE CONTRACTOR, TOWER ERECTION FOREMAN (IF SUBCONTRACTED).  
4. CONTRACTOR SHALL BE EQUIPPED WITH SOME MEANS OF CONSTANT COMMUNICATIONS, SUCH AS A MOBILE PHONE OR A BEEPER. THIS EQUIPMENT WILL NOT BE SUPPLIED BY THE OWNER, NOR WILL WIRELESS SERVICE BE ARRANGED.  
5. DURING CONSTRUCTION, CONTRACTOR MUST ENSURE THAT EMPLOYEES AND SUBCONTRACTORS WEAR HARD HATS AT ALL TIMES. CONTRACTOR SHALL COMPLY WITH ALL WHOS SAFETY REQUIREMENTS IN THEIR AGREEMENT.  
6. PROVIDE WRITTEN DAILY UPDATES ON SITE PROGRESS TO THE OWNER.  
7. COMPLETE INVENTORY OF CONSTRUCTION MATERIALS AND EQUIPMENT IS REQUIRED PRIOR TO START OF CONSTRUCTION.  
8. NOTIFY THE OWNER/PROJECT MANAGER IN WRITING NO LESS THAN 48 HOURS IN ADVANCE OF CONCRETE POURS, TOWER ERECTIONS, AND EQUIPMENT CABINET PLACEMENTS.

INSURANCE AND BONDS

1. CONTRACTOR, AT THEIR OWN EXPENSE, SHALL CARRY AND MAINTAIN, FOR THE DURATION OF THE PROJECT, ALL INSURANCE, AS REQUIRED AND LISTED, AND SHALL NOT COMMENCE WITH THEIR WORK UNTIL THEY HAVE PRESENTED AN ORIGINAL CERTIFICATE OF INSURANCE STATING ALL COVERAGE TO THE OWNER. REFER TO THE MASTER AGREEMENT FOR REQUIRED INSURANCE NAMES.  
2. THE OWNER SHALL BE NAMED AS AN ADDITIONAL INSURED ON ALL POLICES.  
3. CONTRACTOR MUST PROVIDE PROOF OF INSURANCE.

ABBREVIATIONS

ADJ	ADJUSTABLE
AGL	ABOVE GROUND LINE
&	AND
APPROX	APPROXIMATE
BTS	BASE TRANSMISSION STATION
CAB	CABINET
CCE	CEILING
CONC	CONCRETE
CONUT	CONINUOUS
DIA OR Ø	DIAETER
DWG	DRAWING
EAC	EACH
ELEC	ELECTRICAL
ELEV	ELEVATION
EQ	EQUAL
EQUIP	EQUIPMENT
ESB	EQUIPMENT GROUND BAR
EXT	EXISTING
(E)	EXTERIOR
FF	FINISHED FLOOR
GA	GALVE
GALV	GALVANIZED
GC	GENERAL CONTRACTOR
GRND	GROUND
LG	LONG
MAX	MAXIMUM
MECH	MECHANICAL
MW	MICROWAVE DISH MANUFACTURER
MFR	MANUFACTURER
MGB	MASTER GROUND BAR
MN	MINIMUM
MTL	METAL
(N)	NEW
(N)	NOT IN CONTRACT
NIC	NOT TO SCALE
NIS	ON CENTER
OC	OPPOSITE
OPP	PROPOSED
(P)	PROPOSED
PCC	PERSONAL COMMUNICATION SYSTEM
PCS	POWER PROTECTION CABINET
SF	SQUARE FOOT
SHT	SHEET
SIM	SIMILAR
SSL	STAINLESS STEEL
STL	STEEL
TOM	TOP OF CONCRETE
TYP	TYPICAL
VF	VERTICAL IN FIELD
W	WELDED WIRE FABRIC
W/	WITH



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DATE	DESCRIPTION	REVISION
02/04/15	ISSUED FOR REVIEW	A

DETL	DATE	APPRO	REVISIONS
REV			
BY NAME			
DESIGNED			
DATE			
CHKD			
CONTR			
SITE AC			

DRAWN BY: FG  
CHECKED BY: SM

PROFESSIONAL SEAL

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SITE NAME  
CT11303B

SITE NAME  
UCONN

SITE ADDRESS  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 06268

SHEET TITLE  
GENERAL  
AND ELECTRICAL  
NOTES

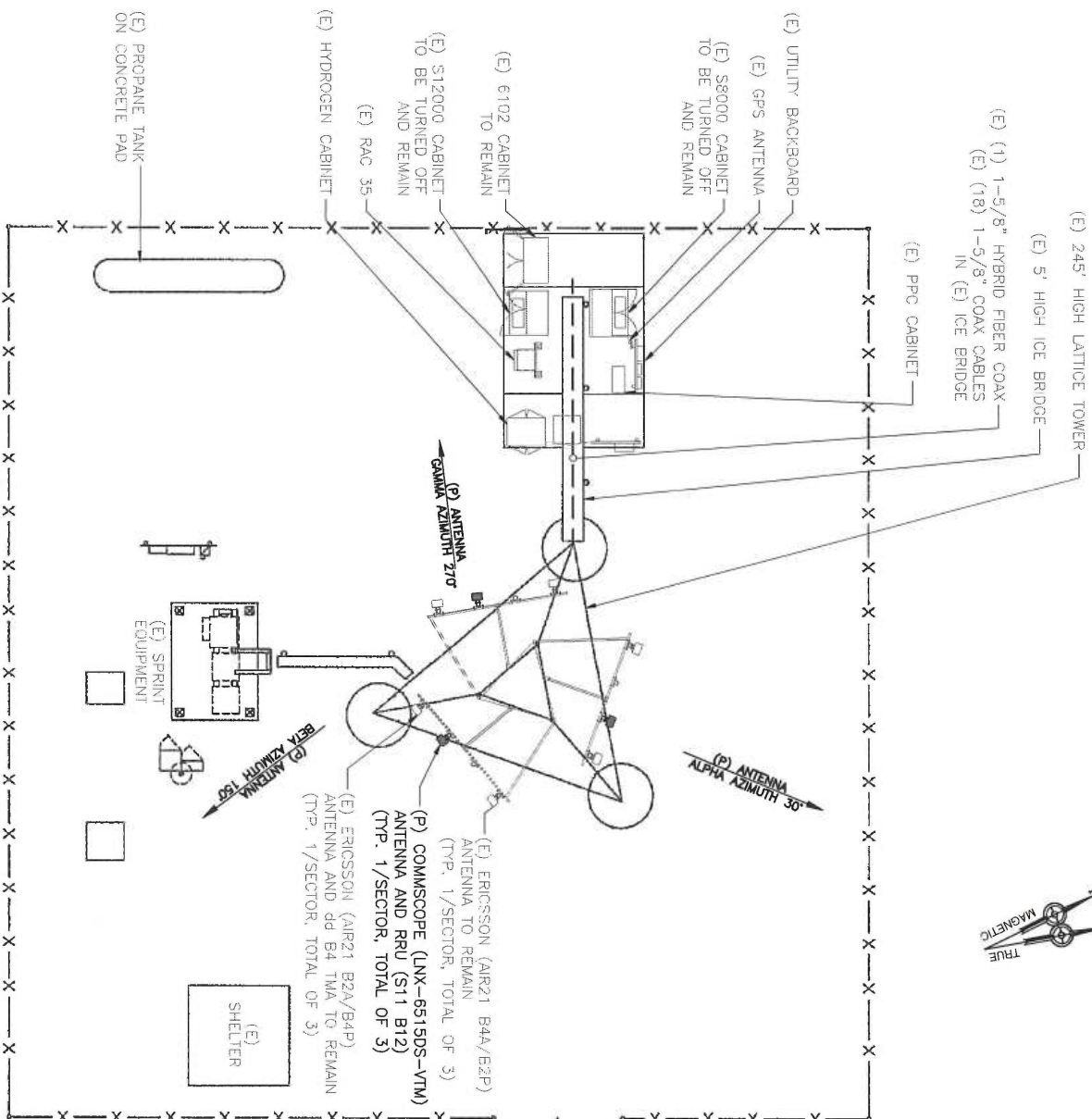
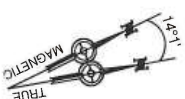
SHEET NUMBER  
N-1





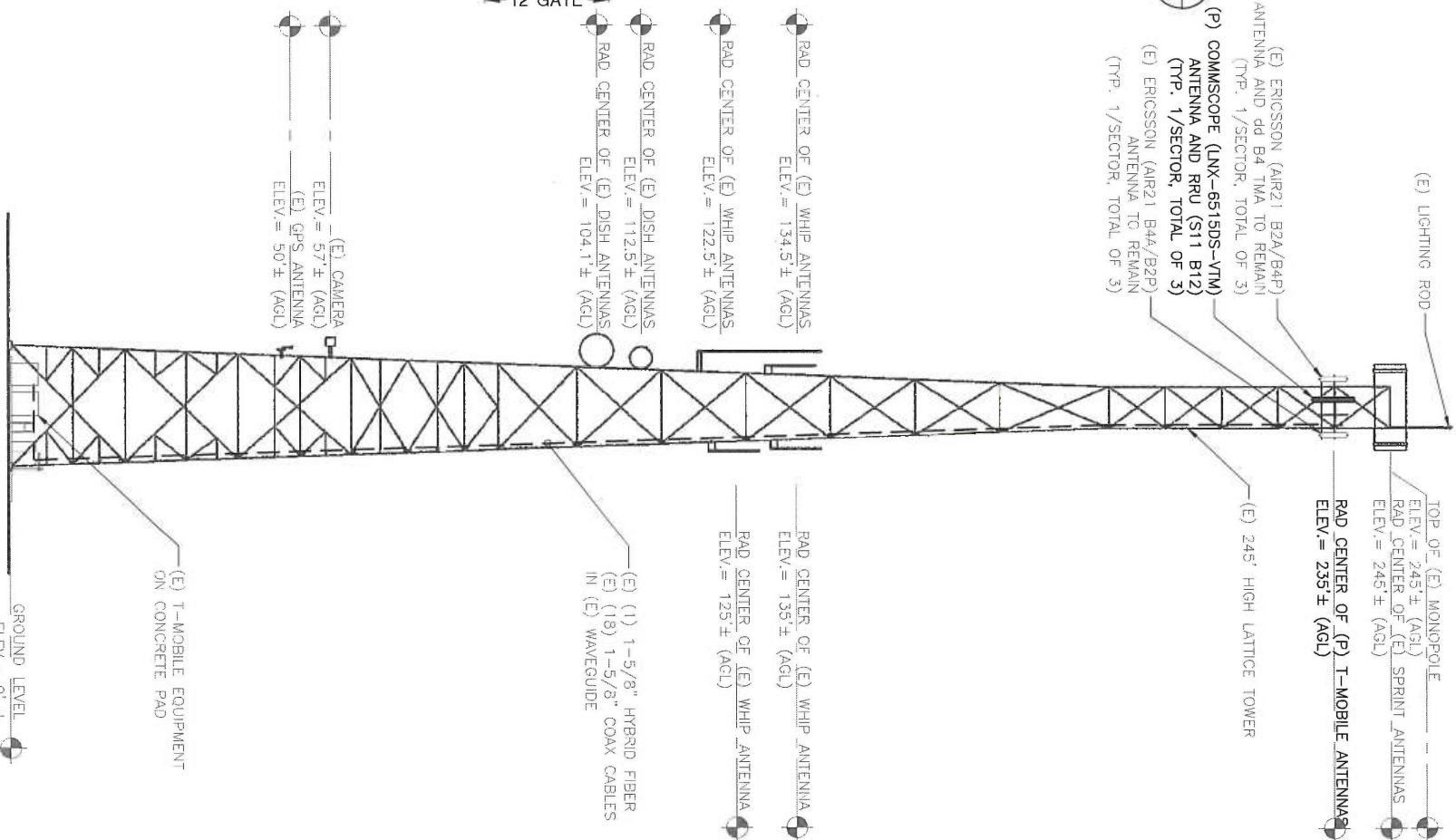
(E) SITE LOCATION  
(E) DRIVEWAY  
SCALE: N.T.S.

KEY PLAN  
SCALE: N.T.S.



COMPOUND PLAN

SCALE: 1/8" = 1'-0" (11x17)  
1/8" = 1'-0" (24x36)



ELEVATION VIEW

SCALE: 1" = 30'-0" (11x17)  
1" = 15'-0" (24x36)



GENERAL SITE NOTES:

1. SITE INFORMATION WAS OBTAINED FROM A FIELD INVESTIGATION PERFORMED BY ATLANTIS GROUP, INC. CONTRACTOR TO FIELD VERIFY DIMENSIONS AS NECESSARY BEFORE CONSTRUCTION.
2. THE PROPOSED DEVELOPMENT DOES NOT INCLUDE SIGNS OF ADVERTISING.
3. THE PROPOSED DEVELOPMENT IS UNMANNED AND THEREFORE DOES NOT REQUIRE A MEANS OF WATER SUPPLY OR SEWAGE DISPOSAL.
4. NO LANDSCAPING WORK IS PROPOSED IN CONJUNCTION WITH THIS DEVELOPMENT OTHER THAN THAT WHICH IS SHOWN.
5. THE PROPOSED DEVELOPMENT DOES NOT INCLUDE OUTDOOR STORAGE OR ANY SOLID WASTE RECEPTACLES.
6. UTILITIES SHOWN ON PLAN ARE TAKEN FROM OWNERS RECORDS AND FIELD LOCATION OF VISIBLE SURFACE FEATURES. THE EXISTENCE, EXTENT AND EXACT HORIZONTAL AND VERTICAL LOCATIONS OF UTILITIES HAS NOT BEEN VERIFIED. ANY CONTRACTOR PERFORMING WORK ON THIS SITE MUST CONTACT CALL BEFORE YOU DIG THREE WORKING DAYS PRIOR TO COMMENCING WORK.
7. ALL OBSOLETE OR UNUSED FACILITIES SHALL BE REMOVED WITHIN 12 MONTHS OF CESSATION OF OPERATIONS.

SITE LEGEND

- SITE PROPERTY LINE
- STREET OR ROAD
- CHAIN LINK FENCE
- OPAQUE WOODEN FENCE
- BOARD ON BOARD FENCE
- DECIDUOUS TREES/SHRUBS
- EVERGREEN TREES/SHRUBS
- TREE LINE
- UTILITY POLE
- (E) EXISTING
- (N) NEW
- (P) PROPOSED
- (F) FUTURE
- PROP. LTE ANTENNA
- PROP. UMTS/GSM ANTENNA
- EX. GSM ANTENNA
- EX. UMTS ANTENNA



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SUBMITTALS	
DATE	REVISION
02/14/15	ISSUED FOR REVIEW A

DEPT.	DATE	REVISIONS
RF		
RF		
DESIGN		
OPS		
CONSTR.		
SITE AD.		

DRAWN BY: FG  
CHECKED BY: SM

PROFESSIONAL SEAL

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SITE NAME  
**CT11303B**

SITE NAME  
**UCONN**

SITE ADDRESS  
**82 NORTH EAGLEVILLE ROAD  
STORRS, CT 06268**

SHEET TITLE  
**COMPOUND PLAN  
AND  
ELEVATION**

SHEET NUMBER

**A-1**



SUBMITTALS	
DATE	REVISION
04/16/15	ISSUED FOR REVIEW A

DEPT.	DATE	REVISIONS
RF MGR.		
DESIGN		
ENGINEER		
CHECKER		
DRAWN BY:		
CHECKED BY:		

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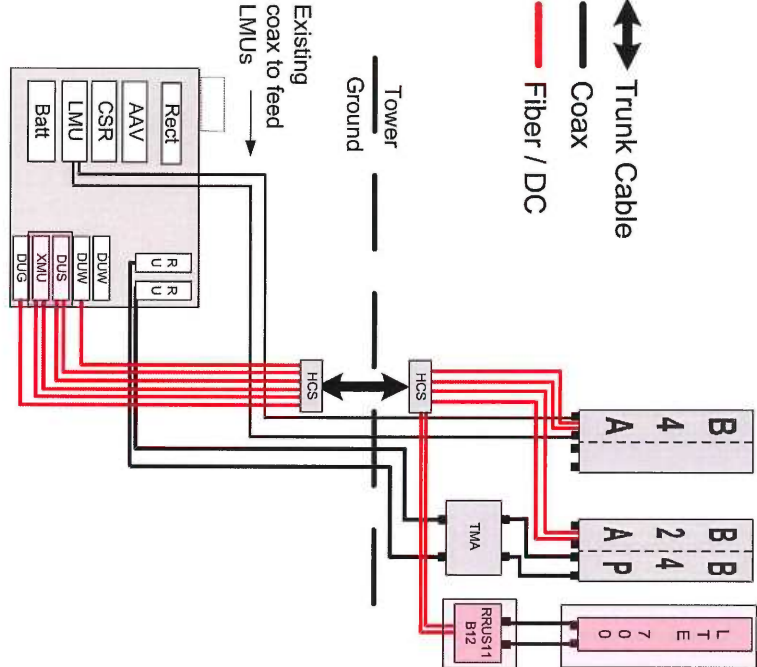
SITE NAME  
CT11303B

SITE NAME  
UCONN

SITE ADDRESS  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 06268

SHEET TITLE  
GROUNDING AND  
POWER ONE LINE  
DIAGRAM

SHEET NUMBER  
E-1



- TRUNK FIBER NOTES:
1. IN GENERAL, THIS CABLE WILL HANDLE SIMILARLY TO 3/4" COAXIAL CABLE, AND SIMILAR INSTALLATION TECHNIQUES APPLY. ALL CABLES ARE INDIVIDUALLY SERIALIZED. BE SURE TO WRITE DOWN THE CABLE SERIAL NUMBER FOR FUTURE REFERENCE.
  2. THE TERMINATED FIBER ENDS (THE BROKEN OUT FIBERS PLUS CONNECTORS) HOWEVER ARE FRAGILE, AND THESE MUST BE PROTECTED DURING THE INSTALLATION PROCESS.
  3. LEAVE THE PROTECTIVE TUBE AND SOCK AROUND THE FIBER TAILS AND CONNECTORS IN PLACE DURING HOISTING AND SECURING THE CABLE. REMOVE THIS ONLY JUST PRIOR TO MAKING THE FINAL CONNECTIONS TO THE OVP BOX.
  4. DO NOT BEND THE FIBER ENDS (IN THE ORANGE FIBRATION TUBES) TIGHTER THAN 3/4" (19MM) BEND RADIUS, ELSE THERE IS A RISK OF BREAKING THE GLASS FIBERS.
  5. BE SURE THAT THE LACE UP ENDS AND FIBER CONNECTORS ARE NOT DAMAGED BY ATTACHMENT OF A HOISTING GRIP OR DURING THE HOISTING PROCESS. ATTACH A HOISTING GRIP ON THE JACKETED CABLE NO LESS THAN 6 INCHES BELOW THE FIBER BREAK-OUT POINT. IF A HOISTING GRIP IS NOT EASILY ATTACHED, USE A SIMPLE LINE ATTACHED BELOW THE FIBER BREAK-OUT POINT (I.E. AT THE CABLE OUTER JACKET). PREVENT THE FIBER TAILS (IN PROTECTIVE TUBE) AT THE CABLE END FROM UNDE. MOVEMENT DURING HOISTING BY SECURING THE PROTECTIVE TUBE (WITH OUTER SOCK) TO THE HOISTING LINE.
  6. DURING HOISTING ENSURE THAT THERE IS A FREE PATH AND THAT THE CABLE, AND ESPECIALLY THE FIBER ENDS, WILL NOT BE SWAGGED ON TOWER MEMBERS OR OTHER OBSTACLES.
  7. INSTALLATION TEMPERATURE RANGE IS -22F TO 158F (-30C TO +70C).
  8. MINIMUM CABLE BEND RADI ARE 22.2" (565MM) LOADED (WITH TENSION ON THE CABLE) AND 11.1" (280MM) UNLOADED.
  9. MAXIMUM CABLE TENSILE LOAD IS 3560 N (800 LB) SHORT TERM (DURING INSTALLATION) AND 1070 N (240 LB) LONG TERM.
  10. COMPOSITE NON LACE UP GRIP RECOMMENDED FOR MONOPOLE INSTALLATIONS.
  11. MAXIMUM HANGER SPACING 3FT (0.9 M).

- HYBRID FIBER/POWER JUMPER NOTES:
1. IN GENERAL, THIS CABLE WILL HANDLE SIMILARLY TO A 3/4" COAXIAL CABLE.
  2. THE TERMINATED FIBER ENDS HOWEVER ARE FRAGILE AND MUST BE PROTECTED DURING INSTALLATION. LEAVE THE PACKAGING AROUND THE FIBER ENDS IN PLACE UNTIL READY TO CONNECT THE JUMPER BETWEEN OVP AND RRU OR BRU.
  3. DO NOT BEND THE FIBER BREAKOUT CABLE (BETWEEN THE MAIN CABLE AND THE FIBER CONNECTOR) TIGHTER THAN 3/4" (19MM) RADIUS, ELSE THERE IS A RISK OF BREAKING THE GLASS.
  4. ATTACH THE MAIN CABLE SECURELY TO THE STRUCTURE OR EQUIPMENT USING HANGERS AND/OR CABLE TIES TO PREVENT STRAIN ON CONNECTIONS FROM MOVEMENT IN WIND OR SNOW/ICE CONDITIONS.
  5. ENSURE THE LC FIBER CONNECTORS ARE SEATED FIRMLY IN PANEL IN OVP OR IN EQUIPMENT.
  6. INSTALLATION TEMPERATURE RANGE IS -22F TO 158F (-30C TO 70C).
  7. MINIMUM CABLE BEND RADI ARE 10.3 INCH (265MM) LOADED (WITH TENSION ON THE CABLE) AND 5.2 INCH (130MM) UNLOADED.
  8. MAXIMUM CABLE TENSILE LOAD IS 350 LB (1560N) SHORT TERM (DURING INSTALLATION) AND 105 LB (470N) LONG TERM.
  9. STANDARD LENGTHS AVAILABLE ARE 6 FEET, 15 FEET AND 20 FEET

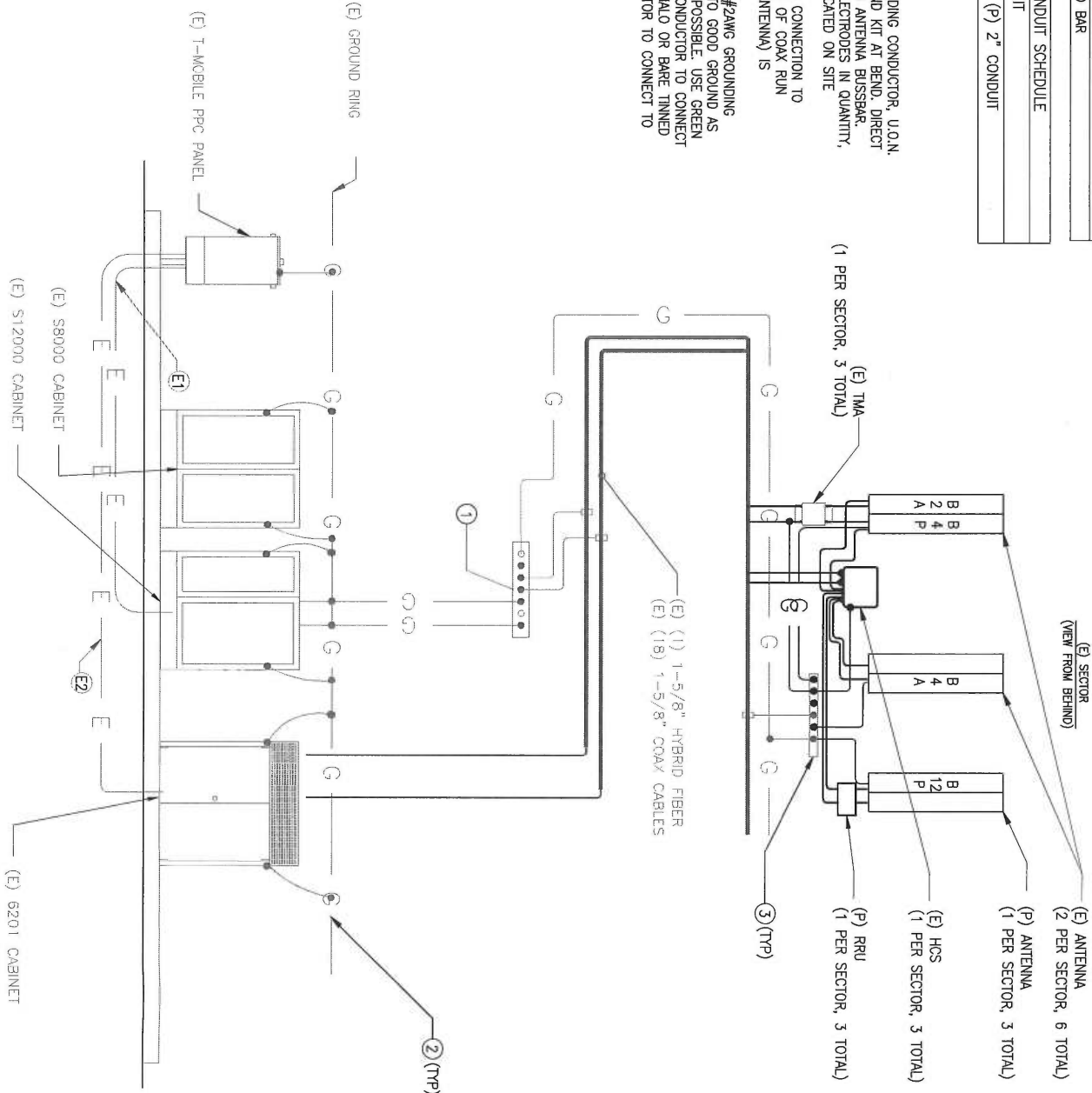
## 702Cu CONFIGURATION COAX/FIBER PLUMBING DIAGRAM

SCALE: N.T.S

2  
E-1

GROUNDING SCHEDULE	
①	(E) MGB (BUSSBAR #1)
②	(E) #2AWG BARE TINNED SOLID COPPER CONDUCTOR BONDED TO GROUND RING (GROUND CABINETS PER MANU. SPECS)
③	(E) SECTOR GROUND BAR
CONDUIT SCHEDULE	
(E1)	(E) POWER CONDUIT
(E2)	(E) 3#6+1#9G IN (P) 2" CONDUIT

- NOTES:
- A. PROVIDE #2AWG GROUNDING CONDUCTOR, U.O.N.
  - B. DO NOT INSTAL. GROUND KIT AT BEND. DIRECT GROUND WIRE DOWN TO ANTENNA BUSSBAR.
  - C. PROVIDE GROUNDING ELECTRODES IN QUANTITY, TYPE AND SIZE AS INDICATED ON SITE GROUNDING PLAN.
  - D. ADD COAX GROUND KIT CONNECTION TO BUSSBAR WHEN LENGTH OF COAX RUN (FROM EQUIPMENT TO ANTENNA) IS GREATER THAN 20'-0".
  - E. GROUND HCS BOX W/ #2AWG GROUNDING CONDUCTOR ATTACHED TO GOOD GROUND AS DIRECT AND SHORT AS POSSIBLE. USE GREEN STRANDED INSULATED CONDUCTOR TO CONNECT TO BUSSBAR/GROUND HALO OR BARE TINNED SOLID COPPER CONDUCTOR TO CONNECT TO GROUND RING.



## GROUNDING DIAGRAM

SCALE: N.T.S

1  
E-1







# **EXHIBIT B**





Submitted to  
Northeast Site Solutions  
199 Brickyard Road  
Farmington, CT 06032

Submitted by  
AECOM  
500 Enterprise Drive,  
Suite 3B  
Rocky Hill, CT 06067  
April 1, 2015

# DETAILED STRUCTURAL ANALYSIS AND MODIFICATION OF AN EXISTING 245' SELF SUPPORTING LATTICE TOWER AND FOUNDATION FOR PROPOSED ANTENNA ARRANGEMENT



Site ID : CT11303B  
Site Name: UCONN  
Site Address: 82 North Eagleville Road  
Storrs, Connecticut

36931420  
NSS-021 Rev. 1



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- 2. INTRODUCTION**
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  - TNX TOWER FEEDLINE DISTRIBUTION
  - TNX TOWER FEEDLINE PLAN
  - TNX TOWER DETAILED OUTPUT
  - ANCHOR BOLT ANALYSIS
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## 1. EXECUTIVE SUMMARY

This report summarizes the structural analysis of the reinforced 245' self-supporting tower located at the campus of the University of Connecticut, on North Eagleville Road in Storrs, Connecticut. The analysis was conducted in accordance with the 2005 Connecticut State Building Code which requires a three second gust wind speed of 100 mph which converts to an 80 mph fastest mile per 2003 IBC (Table 1609.3.1) and the TIA/EIA-222-F standard for a wind velocity of 85 mph (fastest mile). The wind speed from the TIA/EIA-222-F standard governs the design at 85 mph (fastest mile) and 74 mph (fastest mile) concurrence 1/2" ice.

The antenna loading considered in the analysis consists of all existing and proposed antennas, transmission lines, and ancillary items as outlined in the Introduction Section of this report. The proposed T-Mobile modification is as follows:

Proposed Antenna and Mount	Carrier	Antenna Center Elevation
<b><u>Remove:</u></b> <b>(1) ADFD 1820-80B-R2DM Panel Antenna (Beta Sector)</b>	<b>T-Mobile (Proposed)</b>	<b>@ 235'</b>
<b><u>Install:</u></b> <b>(3) Commscope LNX-6515DS-VTM Panel Antennas</b> <b>(3) Ericsson RRUS-11 RRH Units</b>	<b>T-Mobile (Proposed)</b>	<b>@ 235'</b>

The results of an initial analysis indicated that the existing tower structure did not have enough capacity for the proposed loading conditions stated above. The tower structure requires modifications shown on SK-1 through SK-3. **Once the modifications indicated on SK-1 through SK-3 are performed, the modified structure is considered to be structurally adequate with the wind load classification specified above with the existing and propose antenna loading.**

The results of an initial analysis indicated that the existing tower anchor bolts and the foundation have the capacity for the proposed loading conditions stated above. **The tower anchor bolts and foundation are considered structurally adequate with the wind load classification specified above for the existing and proposed loading and do NOT require modification.**



1. **EXECUTIVE SUMMARY** *(continued)*

This analysis is based on:

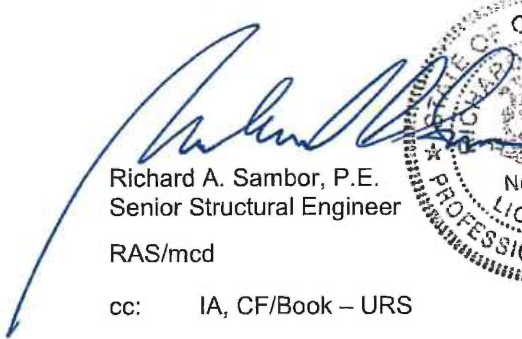
- 1) The tower structure's theoretical capacity, not including any assessment of the condition of the tower.
- 2) Tower foundation, geometry and structural member sizes taken from the manufacturers original design documents prepared by Pirod Inc., drawing number 202932-B, dated September 23, 1997.
- 3) Structural analysis performed by URS Corporation, on behalf of Sprint, project TWS-019 / 36932110, signed and sealed December 30, 2014.
- 4) Proposed antennas via T-Mobile RFDS form, dated February 5, 2015.
- 5) Previous structural analysis performed by URS Corporation, on behalf of T-Mobile, project number 36931419 / NSS-021, signed and sealed February 24, 2015.
- 6) Antenna and mount configuration as specified on the following page of this report.

This report is only valid as per the assumptions and data utilized in this report for antenna inventory, mounts and associated cables. The user of this report shall field verify the assumption of the antenna and mount configuration as well as the physical condition of the tower and connections. Notify the engineer in writing immediately if any of the information in this report is found to be other than specified.

If you should have any questions, please call.

Sincerely,

**URS Corporation AES,**  
*a subsidiary of AECOM*

  
Richard A. Sambor, P.E.  
Senior Structural Engineer

RAS/mcd

cc: IA, CF/Book – URS





## 2. INTRODUCTION

The subject tower is located at 82 North Eagleville Road in Storrs, Connecticut. The structure is a 245' self-supporting tower designed and manufactured by Pirod, Inc.

The tower geometry and structural member sizes taken from original construction drawings (Pirod Drawing #: 202932-B) prepared by Pirod, dated September 23, 1997.

The inventory is summarized in the table below:

<i>Antenna Type</i>	<i>Carrier</i>	<i>Mount</i>	<i>Antenna Centerline Elevation</i>	<i>Cable</i>
Lightning Rod	Tower (existing)	15' Rotatable Platform	247'	---
Flash Beacon	Tower (existing)	See Above Mount	247'	(1) 1/2" DC cable
(3) APXV9TM14-ALU-I20 Panel Antennas (3) Alcatel-Lucent TD-RRH 8x20 RRH Units (2) Sector Jumper Cables (27) RRH Jumper Cables (2) APXVSP18-C-A20 (Alpha & Gamma) (1) RFS APX9ERR18-C-A20 (Beta) (6) 1900 MHz RRH Units (3) 800 MHz RRH Units (3) IBC1900BB-1 (3) IBC1900HG-2A	Sprint (existing)	See Above Mount	247'	(1) Alcatel-Lucent ALU Hybrid Cable (3) 1-1/4" Hybrid Cables
<b>(3) LNX-6515DS-VTM</b> <b>(3) RRUS-11 RRH Units</b>	<b>T-Mobile (Proposed)</b>	See Below Mount	<b>232'</b>	See Below Cables
(3) AIR21 B2A/B4P (3) AIR21 B4A/B2P (3) TMA Units	T-Mobile (existing)	(3) Sector Mounts	232'	(1) Fiber Optic Cable (12) 1-5/8" coax cables
(2) 10' Omni Antennas	Unknown (existing)	(2) 4' Standoff	135'	(2) 7/8" coax cables
(1) 20' Omni Antenna	Unknown (existing)	6' Standoff	125'	(1) 7/8" coax cable
(3) L-810 Obstruction Lights	Tower (existing)	Leg mounted	125'	(1) 1/2" DC cable
(1) 10' Omni Antenna	Unknown (existing)	4' Standoff	110'	(1) 7/8" coax cable
4' Grid Dish	Unknown (existing)	Leg mounted	110'	(1) 7/8" coax cable
(1) 6' Dish w/ Radome	Unknown (existing)	Leg mounted	105'	(1) EW63 cable
(1) Camera	Unknown (existing)	Leg mounted	60'	(1) 7/8" coax cable
(1) 4' Omni	Unknown (existing)	4' Standoff	50'	(1) 7/8" coax cable

This structural analysis of the communications tower was performed by URS Corporation AES, a subsidiary of AECOM, for T-Mobile. The purpose of this analysis was to investigate the structural integrity of the modified tower with its existing and proposed antenna loads. This analysis was conducted to evaluate stress on the tower and the effect of forces to the foundation of the tower resulting from existing and proposed antenna arrangements.



### 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS

The structural analysis was done in accordance with the 2005 Connecticut State Building Code, TIA/EIA-222-F—Structural Standard for Steel Antenna Towers and Antenna Supporting Structures and the American Institute of Steel Construction (AISC) Manual of Steel Construction—Allowable Stress Design (ASD).

The analysis was conducted using TNX Tower 6.1.3.1. Two load conditions were evaluated as shown below which were compared to allowable stresses according to AISC and TIA/EIA.

The Connecticut State Building Code required a three second wind speed of 100 mph which converts to a 80 mph fastest mile per IBC (Table 1609.3.1). The TIA/EIA-222-F requires a basic wind speed of 85 mph (fastest mile). In this case the wind speed from the TIA/EIA-222-F governs the design.

Load Condition 1 = 85 mph (fastest mile) Wind Load (without ice) + Tower Dead Load

Load Condition 2 = 74 mph (fastest mile) Wind Load (with ice) + Ice Load + Tower Dead Load

Please note that wind pressure is a function of velocity squared. Under Load Condition 2, a 25% reduction in wind pressure is allowed by code to account for the unlikelihood of the full wind pressure and ice load occurring at the same time. The same results may be achieved by utilizing a lower wind pressure without taking the 25 percent reduction, as shown above.

The TIA/EIA standard permits a one-third increase in allowable stresses for towers and monopoles less than 700 feet tall. For the purposes of this analysis, in computing the load capacity the allowable stresses of the tower members were increased by one-third.



#### 4. FINDINGS AND EVALUATION

Stresses on the tower structure were evaluated to compare with allowable stresses in accordance with AISC. The results of an initial analysis indicated that the existing tower structure did not have enough capacity to support the proposed loading conditions. The tower structure requires modifications shown on SK-1 through SK-3. **Once the modifications indicated on SK-1 through SK-3 are performed, the modified structure is considered structurally adequate with the wind load classification specified with the existing and proposed antenna loading noted herein.** See below for tower and foundation capacity summary.

##### Tower Reactions

Component	Value (kips)
Base Shear	51
Base Compression	345
Anchor Uplift	296
Anchor Shear	33

##### Tower Component Stress vs. Capacity Summary:

Component/ (Section No.)	Existing Component Size	Controlling Component/Elevation	Stress (% capacity)	Pass/Fail
Tower Leg (T2)	2" SR	Compression / 230' – 210'	83.6 %	Pass
Diagonal (T1)	3/4" SR	Compression / 245' – 230'	98.3 %	Pass
Secondary Horizontal (T9)	L3x3x5/16	Compression / 110' – 100'	67.3 %	Pass
Top Girt (T2)	1" SR	Compression / 230' - 210'	47.9 %	Pass
Bottom Girt (T1)	7/8" SR	Compression / 245' – 230'	64.4 %	Pass
<b>Bolt Checks</b>				
Anchor Bolts	(6) 2" Dia. Bolts	Tension	64 %	Pass

##### Foundation Summary:

Foundation	Component	Stress (% capacity/Factor of Safety)	Pass/Fail	Comments:
Drilled Concrete Caisson	Uplift	93.5 % / 2.14	Pass	Min. FOS of 2.0 req'd per IBC 2003 Section 3108.4.2



## 5. CONCLUSIONS

The results of an initial analysis indicated that the existing tower structure did not have enough capacity for the proposed loading conditions stated above. The tower structure requires modifications shown on SK-1 through SK-3. **Once the modifications indicated on SK-1 through SK-3 are performed, the modified structure is considered to be structurally adequate with the wind load classification specified above with the existing and propose antenna loading.**

The results of an initial analysis indicated that the existing tower anchor bolts and the foundation have the capacity for the proposed loading conditions stated above. **The tower anchor bolts and foundation are considered structurally adequate with the wind load classification specified above for the existing and proposed loading and do NOT require modification.**

### Limitations/Assumptions:

This report is based on the following:

1. Tower inventory as listed in this report.
2. Tower is properly installed and maintained.
3. All members are as specified in the original design documents and are in good condition.
4. All required members are in place.
5. All bolts are in place and are properly tightened.
6. Tower is in plumb condition.
7. All member protective coatings are in good condition.
8. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
9. Foundations were properly constructed to support original design loads as specified in the original design documents.
10. All coaxial cable is installed as specified in Section 6 of this report.

URS is not responsible for any modifications completed prior to or hereafter in which URS is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing/replacing antennas
- C. Adding coaxial cables

URS hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact URS. URS disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

### Ongoing and Periodic Inspection and Maintenance:

After the Contractor has successfully completed the installation and the work has been accepted, the owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA/EIA-222-F for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. According to TIA/EIA-222-F section 14.1, Note 1: It is recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.



## 6. DRAWINGS AND DATA



## REINFORCEMENT DRAWINGS SK-1 THROUGH SK-3



## GENERAL CONSTRUCTION NOTES

1. ALL WORK SHALL COMPLY WITH THE CONNECTICUT STATE BUILDING, SUPPLEMENTS AND AMENDMENTS AND LIFE SAFETY CODES.
2. CONTRACTOR IS TO REVIEW ALL DRAWINGS AND NOTES IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUB-CONTRACTORS AND ALL RELATED PARTIES. THE SUB-CONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND NOTES FOR THE INFORMATION THAT AFFECTS THEIR WORK.
3. CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON DRAWINGS.
4. CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
5. CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION AND ELECTRICAL SUB-CONTRACTORS SHALL PAY FOR THEIR PERMITS.
6. CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS ON SITE AT ALL TIMES AND ENSURE THE DISTRIBUTION OF NEW DRAWINGS TO SUB-CONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. CONTRACTOR SHALL FURNISH 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
7. INSTALLATION OF THIS WIRELESS COMMUNICATIONS EQUIPMENT SITE REQUIRES WORK IN THE IMMEDIATE VICINITY OF EXISTING OPERATING TELECOMMUNICATION SYSTEMS. THE CONTRACTOR SHALL PROVIDE AND COORDINATE THE METHODS OF PROTECTION WITH THE VARIOUS TELECOMMUNICATION CARRIERS AND THE TOWER OWNER. THERE SHALL BE NO INTERRUPTION OF OPERATION WITHOUT TIMELY COORDINATION WITH AND APPROVAL BY THE VARIOUS COMMUNICATIONS OPERATORS.
8. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS FOR ANY CONDITION PER MFR'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR ARCHITECT.
9. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
10. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ARCHITECT FOR REVIEW. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTAL TO THE ARCHITECT FOR REVIEW.
11. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA. SUBMIT ANY DISCREPANCIES FROM THE DRAWINGS TO THE ARCHITECT.
12. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURE AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
13. CONTRACTOR TO CONTACT "CALL BEFORE YOU DIG" AT 1-800-922-4455 TO VERIFY AND IDENTIFY THE EXACT LOCATIONS OF ALL UNDERGROUND UTILITIES AND OBSTRUCTIONS IDENTIFIED PRIOR TO COMMENCING WORK IN THE CONTRACT AREA.
14. EXISTING DIMENSIONS OF STRUCTURE SHOWN ON THESE DOCUMENTS ARE BASED ON ORIGINAL TOWER CONSTRUCTION DRAWINGS PERFORMED BY PIROD, DATED SEPTEMBER 1997, ARE NOT GUARANTEED. CONTRACTOR SHALL TAKE FIELD DIMENSIONS AS NECESSARY TO ASSURE PROPER FIT OF ALL FINISHED WORK AND SHALL ASSUME FULL RESPONSIBILITY FOR THEIR ACCURACY. WHEN SHOP DRAWINGS BASED ON FIELD MEASUREMENT ARE SUBMITTED FOR REVIEW, DIMENSIONS ARE PROVIDED FOR THE ENGINEER'S REFERENCE ONLY.
15. TOWER INVENTORY IS BASED ON INFORMATION OBTAINED FROM T-MOBILE DATED FEBRUARY 2015.

## STRUCTURAL NOTES

### STRUCTURAL STEEL MATERIAL:

STRUCTURAL STEEL BEAMS, CHANNELS, PLATES.....	A36
STRUCTURAL ANGLES.....	A36
EXISTING TOWER LEG .....	A 572-Gr. 50
EXISTING TOWER LEG PIROD TRUSS .....	A 572-Gr. 50

STRUCTURAL STEEL SHALL CONFORM TO ALL THE REQUIREMENTS OF THE ASTM SPECIFICATION, AS REFERENCED IN THE CODE.

UNLESS OTHERWISE NOTED, ALL STEEL WILL BE GALVANIZED IN ACCORDANCE WITH ASTM 123 AFTER FABRICATION. TOUCH UP ALL DAMAGED GALVANIZED STEEL WITH APPROVED COLD ZINC, "GALVANOX", "DRY GALV", "ZINC-IT", OR APPROVED EQUIVALENT, IN ACCORDANCE WITH MANUFACTURERS GUIDELINES. TOUCH-UP DAMAGED NON GALVANIZED STEEL WITH SAME PAINT APPLIED IN SHOP OR FIELD.

SHOP AND ERECTION DRAWINGS SHALL BE SUBMITTED FOR ALL STRUCTURAL STEEL WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. SUBMIT 2 SETS OF PRINTS FOR THE ENGINEER REVIEW.

MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.

THE OMISSION OF ANY MATERIAL THAT WAS SHOWN ON THE CONTRACT DRAWINGS SHALL NOT RELIEVE THE CONTRACTOR OF PROVIDING THE SAME.

### CONNECTIONS / FIELD ASSEMBLY:

BOLTED CONNECTIONS: UNLESS OTHERWISE NOTED, ALL JOINTS ARE SLIP CRITICAL TYPE, REQUIRING 3/4" DIA. A325-N BOLTS, A563 NUTS AND F436 WASHERS, ALL GALVANIZED. BEVELED WASHERS SHALL BE USED ON BEAM FLANGES HAVING A SLOPE GREATER THAN 1:20.

STRUCTURE IS DESIGNED TO BE LEVEL AND PLUMB, SELF-SUPPORTING AND STABLE AFTER WORK IS COMPLETED.

COMMENCEMENT OF WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.

THE CONTRACTOR IS RESPONSIBLE FOR THE STABILITY OF THE STRUCTURE DURING CONSTRUCTION. NO MEMBER OF THE TOWER SHALL BE LEFT DISCONNECTED FOR THE NEXT WORKING DAY. THE CONTRACTOR SHALL BE AWARE OF WEATHER AND WIND CONDITIONS AND NOT PERFORM MEMBER REPLACEMENT IN A WIND.

### INSPECTIONS:

SPECIAL INSPECTIONS ARE REQUIRED PER THE CODE FOR STRUCTURAL STEEL WORK.

OWNER WILL SUPPLY THE SERVICES OF A SPECIAL INSPECTOR AND TESTING AGENTS AS REQUIRED. CONTRACTOR SHALL COORDINATE INSPECTIONS OF FABRICATOR'S AND ERECTOR'S WORK AND MATERIALS TO MEET THE REQUIREMENTS OF THE STATEMENT OF SPECIAL INSPECTIONS FOR THIS PROJECT.

COPIES OF TESTING AND INSPECTION REPORTS WILL BE PROVIDED TO THE OWNER, BUILDING OFFICIAL, ENGINEER OF RECORD AND CONTRACTOR.

PROJECT NO.  
36931420

Designed by:  
MCD

Drawn by:  
KAP

Checked by:  
KAB

Approved by:  
RAS

**AECOM**

500 ENTERPRISE DRIVE  
ROCKY HILL, CONNECTICUT  
(860)-529-8882

• T • Mobile •

SITE ADDRESS: 82 NORTH EAGLEVILLE ROAD  
STORRS, CONNECTICUT 06268

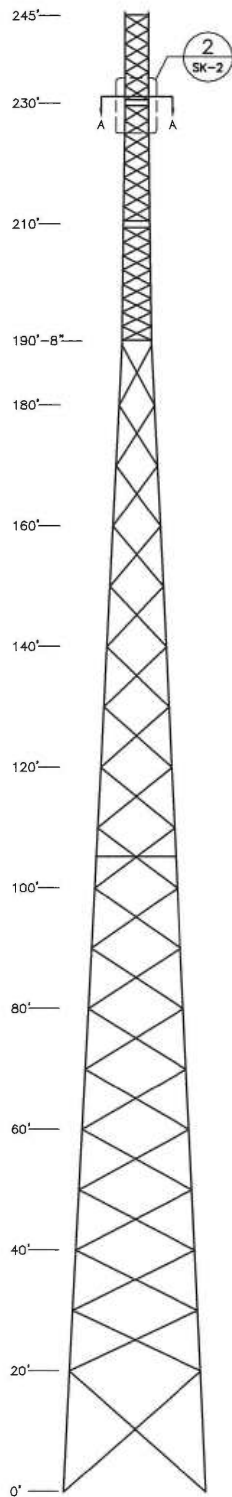
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Scale:	AS NOTED	Date: 04/01/15
Job No.	NSS-022	File No.

Dwg. No.

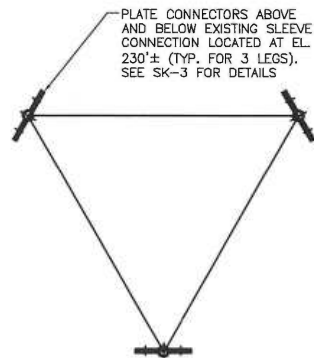
SK-1

Dwg. 1 of 3



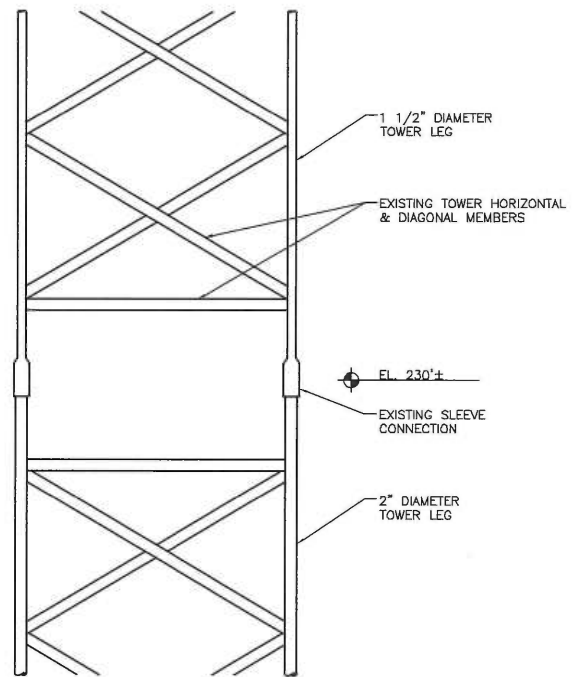


**1**  
SK-2  
**TOWER ELEVATION**  
SCALE: 1" = 30'-0"



**PLAN SECTION A-A**

**NOTE:**  
CONTRACTOR SHALL INSTALL CONNECTOR PLATES AS CLOSE TO EXISTING SLEEVE CONNECTION AS POSSIBLE WITHOUT CONFLICTING WITH EXISTING TOWER HORIZONTAL & DIAGONAL MEMBERS.



**2**  
SK-2  
**EXISTING TOWER ELEVATION DETAIL**  
SCALE: 1" = 30'-0"

PROJECT NO.  
36931420  
Designed by:  
MCD  
Drawn by:  
KAP  
Checked by:  
KAB  
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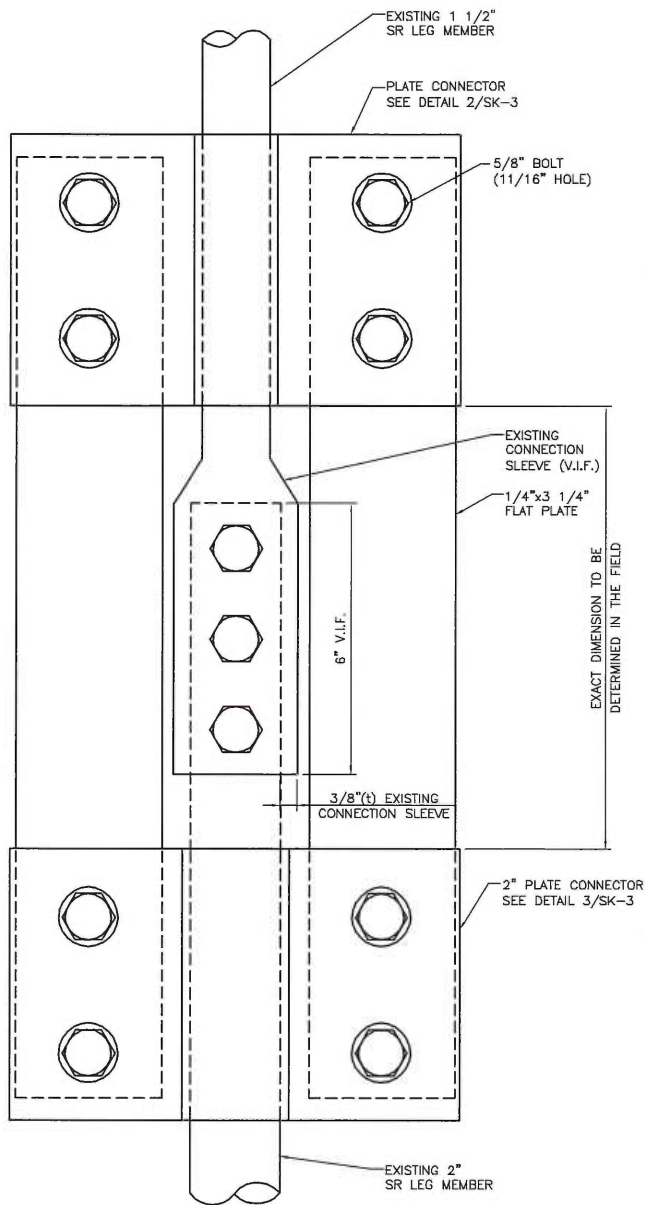
SITE ADDRESS: 82 NORTH EAGLEVILLE ROAD  
STORRS, CONNECTICUT 06268

REV.	DATE:	DESCRIPTION

Scale: AS NOTED Date: 04/01/15  
Job No. NSS-022 File No. Dwg. 2 of 3

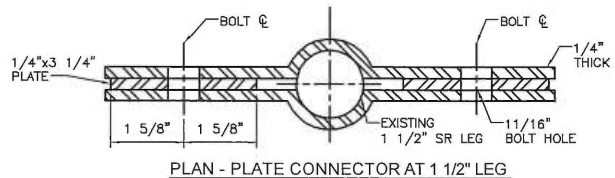
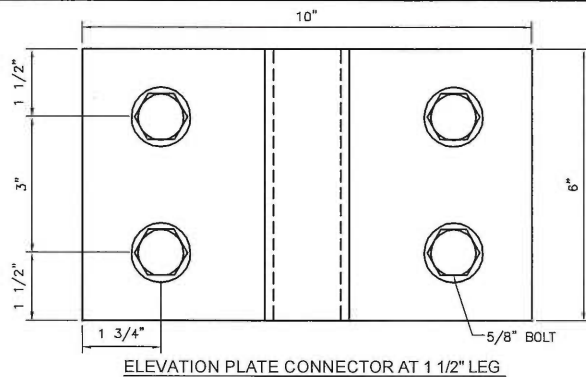
Dwg. No.  
**SK-2**



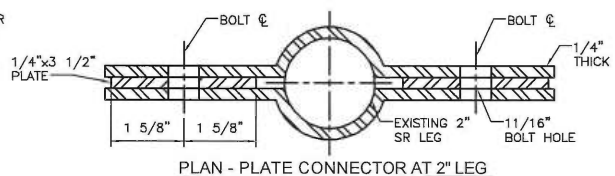
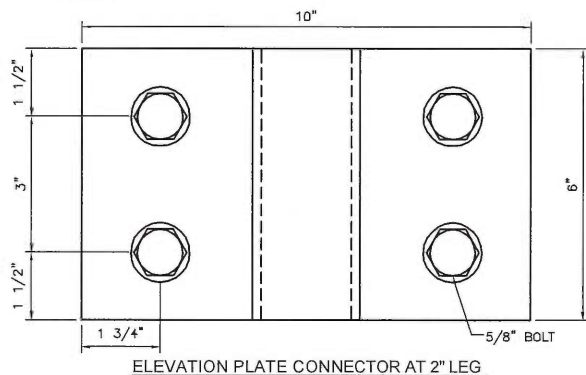


**1** PLATE CONNECTORS  
SK-3 SCALE: 3"=1'-0"

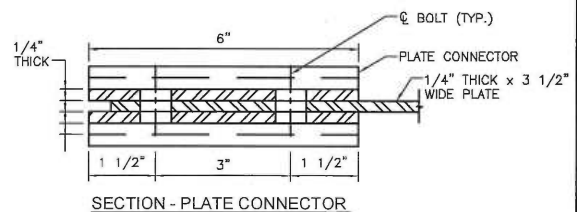
SR = SOLID ROD



**2** PLATE CONNECTOR AT 1 1/2" LEG  
SK-3 SCALE: 3"=1'-0"



**3** PLATE CONNECTOR AT 2" LEG  
SK-3 SCALE: 3"=1'-0"



**4** TYPICAL SECTION  
SK-3 SCALE: 3"=1'-0"

PROJECT NO.  
36931420  
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REV.	DATE:	DESCRIPTION

Scale: AS NOTED Date: 04/01/15  
Job No. NSS-022 File No. Dwg. 3 of 3

Dwg. No.  
**SK-3**



## **TNX TOWER INPUT/OUTPUT SUMMARY**



Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14	T15	T16	T17	T18	T19	T20	T21	T22	T23	T24	T25	T26	T27	T28	T29	T30	T31	T32	T33	T34	T35	T36	T37	T38	T39	T40	T41	T42	T43	T44	T45	T46	T47	T48	T49	T50	T51	T52	T53	T54	T55	T56	T57	T58	T59	T60	T61	T62	T63	T64	T65	T66	T67	T68	T69	T70	T71	T72	T73	T74	T75	T76	T77	T78	T79	T80	T81	T82	T83	T84	T85	T86	T87	T88	T89	T90	T91	T92	T93	T94	T95	T96	T97	T98	T99	T100	T101	T102	T103	T104	T105	T106	T107	T108	T109	T110	T111	T112	T113	T114	T115	T116	T117	T118	T119	T120	T121	T122	T123	T124	T125	T126	T127	T128	T129	T130	T131	T132	T133	T134	T135	T136	T137	T138	T139	T140	T141	T142	T143	T144	T145	T146	T147	T148	T149	T150	T151	T152	T153	T154	T155	T156	T157	T158	T159	T160	T161	T162	T163	T164	T165	T166	T167	T168	T169	T170	T171	T172	T173	T174	T175	T176	T177	T178	T179	T180	T181	T182	T183	T184	T185	T186	T187	T188	T189	T190	T191	T192	T193	T194	T195	T196	T197	T198	T199	T200	T201	T202	T203	T204	T205	T206	T207	T208	T209	T210	T211	T212	T213	T214	T215	T216	T217	T218	T219	T220	T221	T222	T223	T224	T225	T226	T227	T228	T229	T230	T231	T232	T233	T234	T235	T236	T237	T238	T239	T240	T241	T242	T243	T244	T245	T246	T247	T248	T249	T250	T251	T252	T253	T254	T255	T256	T257	T258	T259	T260	T261	T262	T263	T264	T265	T266	T267	T268	T269	T270	T271	T272	T273	T274	T275	T276	T277	T278	T279	T280	T281	T282	T283	T284	T285	T286	T287	T288	T289	T290	T291	T292	T293	T294	T295	T296	T297	T298	T299	T300	T301	T302	T303	T304	T305	T306	T307	T308	T309	T310	T311	T312	T313	T314	T315	T316	T317	T318	T319	T320	T321	T322	T323	T324	T325	T326	T327	T328	T329	T330	T331	T332	T333	T334	T335	T336	T337	T338	T339	T340	T341	T342	T343	T344	T345	T346	T347	T348	T349	T350	T351	T352	T353	T354	T355	T356	T357	T358	T359	T360	T361	T362	T363	T364	T365	T366	T367	T368	T369	T370	T371	T372	T373	T374	T375	T376	T377	T378	T379	T380	T381	T382	T383	T384	T385	T386	T387	T388	T389	T390	T391	T392	T393	T394	T395	T396	T397	T398	T399	T400	T401	T402	T403	T404	T405	T406	T407	T408	T409	T410	T411	T412	T413	T414	T415	T416	T417	T418	T419	T420	T421	T422	T423	T424	T425	T426	T427	T428	T429	T430	T431	T432	T433	T434	T435	T436	T437	T438	T439	T440	T441	T442	T443	T444	T445	T446	T447	T448	T449	T450	T451	T452	T453	T454	T455	T456	T457	T458	T459	T460	T461	T462	T463	T464	T465	T466	T467	T468	T469	T470	T471	T472	T473	T474	T475	T476	T477	T478	T479	T480	T481	T482	T483	T484	T485	T486	T487	T488	T489	T490	T491	T492	T493	T494	T495	T496	T497	T498	T499	T500	T501	T502	T503	T504	T505	T506	T507	T508	T509	T510	T511	T512	T513	T514	T515	T516	T517	T518	T519	T520	T521	T522	T523	T524	T525	T526	T527	T528	T529	T530	T531	T532	T533	T534	T535	T536	T537	T538	T539	T540	T541	T542	T543	T544	T545	T546	T547	T548	T549	T550	T551	T552	T553	T554	T555	T556	T557	T558	T559	T560	T561	T562	T563	T564	T565	T566	T567	T568	T569	T570	T571	T572	T573	T574	T575	T576	T577	T578	T579	T580	T581	T582	T583	T584	T585	T586	T587	T588	T589	T590	T591	T592	T593	T594	T595	T596	T597	T598	T599	T600	T601	T602	T603	T604	T605	T606	T607	T608	T609	T610	T611	T612	T613	T614	T615	T616	T617	T618	T619	T620	T621	T622	T623	T624	T625	T626	T627	T628	T629	T630	T631	T632	T633	T634	T635	T636	T637	T638	T639	T640	T641	T642	T643	T644	T645	T646	T647	T648	T649	T650	T651	T652	T653	T654	T655	T656	T657	T658	T659	T660	T661	T662	T663	T664	T665	T666	T667	T668	T669	T670	T671	T672	T673	T674	T675	T676	T677	T678	T679	T680	T681	T682	T683	T684	T685	T686	T687	T688	T689	T690	T691	T692	T693	T694	T695	T696	T697	T698	T699	T700	T701	T702	T703	T704	T705	T706	T707	T708	T709	T710	T711	T712	T713	T714	T715	T716	T717	T718	T719	T720	T721	T722	T723	T724	T725	T726	T727	T728	T729	T730	T731	T732	T733	T734	T735	T736	T737	T738	T739	T740	T741	T742	T743	T744	T745	T746	T747	T748	T749	T750	T751	T752	T753	T754	T755	T756	T757	T758	T759	T760	T761	T762	T763	T764	T765	T766	T767	T768	T769	T770	T771	T772	T773	T774	T775	T776	T777	T778	T779	T780	T781	T782	T783	T784	T785	T786	T787	T788	T789	T790	T791	T792	T793	T794	T795	T796	T797	T798	T799	T800	T801	T802	T803	T804	T805	T806	T807	T808	T809	T810	T811	T812	T813	T814	T815	T816	T817	T818	T819	T820	T821	T822	T823	T824	T825	T826	T827	T828	T829	T830	T831	T832	T833	T834	T835	T836	T837	T838	T839	T840	T841	T842	T843	T844	T845	T846	T847	T848	T849	T850	T851	T852	T853	T854	T855	T856	T857	T858	T859	T860	T861	T862	T863	T864	T865	T866	T867	T868	T869	T870	T871	T872	T873	T874	T875	T876	T877	T878	T879	T880	T881	T882	T883	T884	T885	T886	T887	T888	T889	T890	T891	T892	T893	T894	T895	T896	T897	T898	T899	T900	T901	T902	T903	T904	T905	T906	T907	T908	T909	T910	T911	T912	T913	T914	T915	T916	T917	T918	T919	T920	T921	T922	T923	T924	T925	T926	T927	T928	T929	T930	T931	T932	T933	T934	T935	T936	T937	T938	T939	T940	T941	T942	T943	T944	T945	T946	T947	T948	T949	T950	T951	T952	T953	T954	T955	T956	T957	T958	T959	T960	T961	T962	T963	T964	T965	T966	T967	T968	T969	T970	T971	T972	T973	T974	T975	T976	T977	T978	T979	T980	T981	T982	T983	T984	T985	T986	T987	T988	T989	T990	T991	T992	T993	T994	T995	T996	T997	T998	T999	T1000	T1001	T1002	T1003	T1004	T1005	T1006	T1007	T1008	T1009	T1010	T1011	T1012	T1013	T1014	T1015	T1016	T1017	T1018	T1019	T1020	T1021	T1022	T1023	T1024	T1025	T1026	T1027	T1028	T1029	T1030	T1031	T1032	T1033	T1034	T1035	T1036	T1037	T1038	T1039	T1040	T1041	T1042	T1043	T1044	T1045	T1046	T1047	T1048	T1049	T1050	T1051	T1052	T1053	T1054	T1055	T1056	T1057	T1058	T1059	T1060	T1061	T1062	T1063	T1064	T1065	T1066	T1067	T1068	T1069	T1070	T1071	T1072	T1073	T1074	T1075	T1076	T1077	T1078	T1079	T1080	T1081	T1082	T1083	T1084	T1085	T1086	T1087	T1088	T1089	T1090	T1091	T1092	T1093	T1094	T1095	T1096	T1097	T1098	T1099	T1100	T1101	T1102	T1103	T1104	T1105	T1106	T1107	T1108	T1109	T1110	T1111	T1112	T1113	T1114	T1115	T1116	T1117	T1118	T1119	T1120	T1121	T1122	T1123	T1124	T1125	T1126	T1127	T1128	T1129	T1130	T1131	T1132	T1133	T1134	T1135	T1136	T1137	T1138	T1139	T1140	T1141	T1142	T1143	T1144	T1145	T1146	T1147	T1148	T1149	T1150	T1151	T1152	T1153	T1154	T1155	T1156	T1157	T1158	T1159	T1160	T1161	T1162	T1163	T1164	T1165	T1166	T1167	T1168	T1169	T1170	T1171	T1172	T1173	T1174	T1175	T1176	T1177	T1178	T1179	T1180	T1181	T1182	T1183	T1184	T1185	T1186	T1187	T1188	T1189	T1190	T1191	T1192	T1193	T1194	T1195	T1196	T1197	T1198	T1199	T1200	T1201	T1202	T1203	T1204	T1205	T1206	T1207	T1208	T1209	T1210	T1211	T1212	T1213	T1214	T1215	T1216	T1217	T1218	T1219	T1220	T1221	T1222	T1223	T1224	T1225	T1226	T1227	T1228	T1229	T1230	T1231	T1232	T1233	T1234	T1235	T1236	T1237	T1238	T1239	T1240	T1241	T1242	T1243	T1244	T1245	T1246	T1247	T1248	T1249	T1250	T1251	T1252	T1253	T1254	T1255	T1256	T1257	T1258	T1259	T1260	T1261	T1262	T1263	T1264	T1265	T1266	T1267	T1268	T1269	T1270	T1271	T1272	T1273	T1274	T1275	T1276	T1277	T1278	T1279	T1280	T1281	T1282	T1283	T1284	T1285	T1286	T1287	T1288	T1289	T1290	T1291	T1292	T1293	T1294	T1295	T1296	T1297	T1298	T1299	T1300	T1301	T1302	T1303	T1304	T1305	T1306	T1307	T1308	T1309	T1310	T1311	T1312	T1313	T1314	T1315	T1316	T1317	T1318	T1319	T1320	T1321	T1322	T1323	T1324	T1325	T1326	T1327	T1328	T1329	T1330	T1331	T1332	T1333	T1334	T1335	T1336	T1337	T1338	T1339	T1340	T1341	T1342	T1343	T1344	T1345	T1346	T1347	T1348	T1349	T1350	T1351	T1352	T1353	T1354	T1355	T1356	T1357	T1358	T1359	T1360	T1361	T1362	T1363	T1364	T1365	T1366	T1367	T1368	T1369	T1370	T1371	T1372	T1373	T1374	T1375	T1376	T1377	T1378	T1379	T1380	T1381	T1382	T1383	T1384	T1385	T1386	T1387	T1388	T1389	T1390	T1391	T1392	T1393	T1394	T1395	T1396	T1397	T1398	T1399	T1400	T1401	T1402	T1403	T1404	T1405	T1406	T1407	T1408	T1409	T1410	T1411	T1412	T1413	T1414	T1415	T1416	T1417	T1418	T1419	T1420	T1421	T1422	T1423	T1424	T1425	T1426	T1427	T1428	T1429	T1430	T1431	T1432	T1433	T1434	T1435	T1436	T1437	T1438	T1439	T1440	T1441	T1442	T1443	T1444	T1445	T1446	T1447	T1448	T1449	T1450	T1451	T1452	T1453	T1454	T1455	T1456	T1457	T1458	T1459	T1460	T1461	T1462	T1463	T1464	T1465	T1466	T1467	T1468	T1469	T1470	T1471	T1472	T1473	T1474	T1475	T1476	T1477	T1478	T1479	T1480	T1481	T1482	T1483	T1484	T1485	T1486	T1487	T1488	T1489	T1490	T1491	T1492	T1493	T1494	T1495
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## **TNX TOWER FEEDLINE DISTRIBUTION**



Component	Material Type
Round	Red
Flat	Black
App In Face	Blue
App Out Face	Green
Truss Leg	Yellow



<b>Job: <i>Modification Structural Analysis - Tower</i></b>			
<b>Project: <i>Storrs (UCONN), CT (Site: CT11303B) / NSS-022</i></b>			
<b>Client: <i>Northeast Site Solutions / T-Mobile</i></b>		<b>Drawn by: <i>MCD</i></b>	<b>App'd:</b>
<b>Code: <i>TIA/EIA-222-F</i></b>		<b>Date: <i>04/01/15</i></b>	<b>Scale: <i>NTS</i></b>
<b>Path:</b>			<b>Dwg No. <i>E-7</i></b>
<small>Workstream: By: Location\Correspondent\Method\EST User\NAME\$NOID: 36811436-04-0222-008\Barnfield on 4/1/2015 10:55:06 AM</small>			



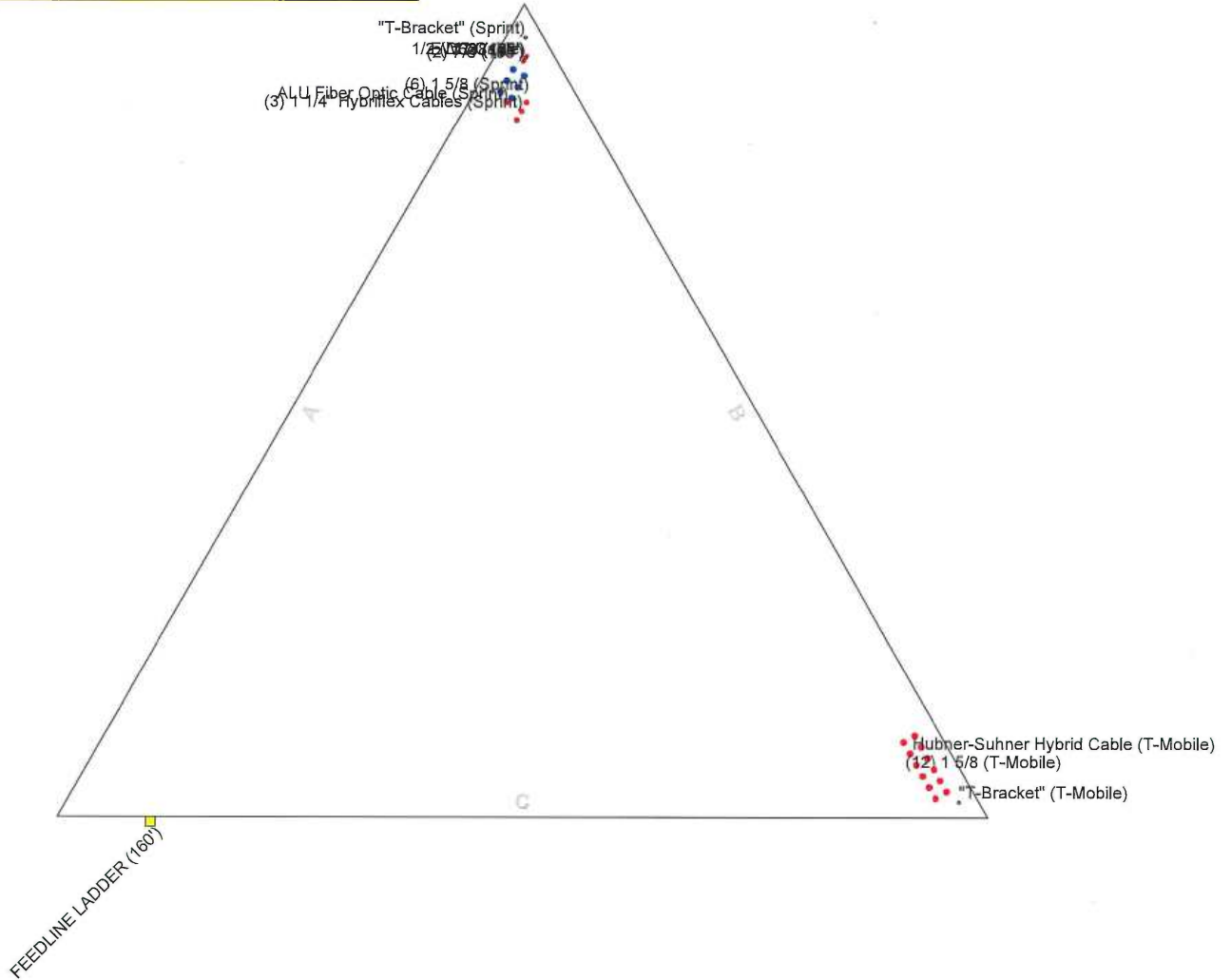
## TNX TOWER FEEDLINE PLAN



# Feed Line Plan

Round Flat App In Face App Out Face Truss-Leg

- (6) 1-5/8" coax cables - Sprint
- (3) 1-1/4" Hybrid cables - Sprint
- (1) "T-Bracket"
- (2) 1/2" DC cables
- (7) 7/8" coax cables
- (1) EW63 Elliptical cable
- (1) Fiber Optic Cable - Sprint



<b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991		<b>Job: MODification Structural Analysis - Tower</b> <b>Project: Storrs (UConn), CT (Site: CT11303B) / NSS-022</b> <b>Client: Northeast Site Solutions / T-Mobile</b> <b>Code: TIA/EIA-222-F</b> <b>Path:</b>		<b>Drawn by: MCD</b> <b>Date: 04/01/15</b> <b>Scale: NTS</b> <b>Dwg No. E-7</b>
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## TNX TOWER DETAILED OUTPUT



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	MODification Structural Analysis - Tower	<b>Page</b>	1 of 46
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	<b>Client</b>	Northeast Site Solutions / T-Mobile	<b>Designed by</b>	MCD

## Tower Input Data

The main tower is a 3x free standing tower with an overall height of 245.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 4.00 ft at the top and 24.00 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Tolland County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 74 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.333.

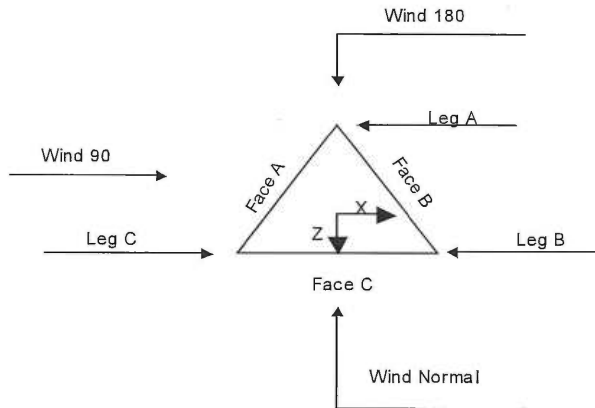
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs	Distribute Leg Loads As Uniform	Treat Feedline Bundles As Cylinder
Consider Moments - Horizontals	Assume Legs Pinned	Use ASCE 10 X-Brace Ly Rules
Consider Moments - Diagonals	✓ Assume Rigid Index Plate	✓ Calculate Redundant Bracing Forces
Use Moment Magnification	✓ Use Clear Spans For Wind Area	Ignore Redundant Members in FEA
✓ Use Code Stress Ratios	✓ Use Clear Spans For KL/r	SR Leg Bolts Resist Compression
✓ Use Code Safety Factors - Guys	Retension Guys To Initial Tension	All Leg Panels Have Same Allowable
Escalate Ice	Bypass Mast Stability Checks	Offset Girt At Foundation
Always Use Max Kz	✓ Use Azimuth Dish Coefficients	✓ Consider Feedline Torque
Use Special Wind Profile	✓ Project Wind Area of Appurt.	Include Angle Block Shear Check
✓ Include Bolts In Member Capacity	✓ Autocalc Torque Arm Areas	Poles
✓ Leg Bolts Are At Top Of Section	✓ SR Members Have Cut Ends	Include Shear-Torsion Interaction
✓ Secondary Horizontal Braces Leg	✓ Sort Capacity Reports By Component	Always Use Sub-Critical Flow
Use Diamond Inner Bracing (4 Sided)	✓ Triangulate Diamond Inner Bracing	Use Top Mounted Sockets
Add IBC .6D+W Combination	Use TIA-222-G Tension Splice Capacity Exemption	



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**Triangular Tower**

### Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	245.00-230.00			4.00	1	15.00
T2	230.00-210.00			4.00	1	20.00
T3	210.00-190.00			4.50	1	20.00
T4	190.00-180.00		U6.0 105245	5.00	1	10.00
T5	180.00-160.00		U8.0 105217	6.00	1	20.00
T6	160.00-140.00		U10.0 105216	8.00	1	20.00
T7	140.00-120.00		U12.0 105218	10.00	1	20.00
T8	120.00-110.00		U14.0 105218	12.00	1	10.00
T9	110.00-100.00		U14.0 105218	13.00	1	10.00
T10	100.00-80.00		U16.0 105219	14.00	1	20.00
T11	80.00-60.00		U18.0 105219	16.00	1	20.00
T12	60.00-40.00		U20.0 105219 L3.5x5/16	18.00	1	20.00
T13	40.00-20.00		U22.0 105220 L4x1/4	20.00	1	20.00
T14	20.00-0.00		U24.0 105220	22.00	1	20.00

### Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	245.00-230.00	2.33	X Brace	No	Steps	6.0000	6.0000



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Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T2	230.00-210.00	2.38	X Brace	No	Steps	6.0000	6.0000
T3	210.00-190.00	2.33	X Brace	No	No	8.0160	8.0160
T4	190.00-180.00	10.00	X Brace	No	No	0.0000	0.0000
T5	180.00-160.00	10.00	X Brace	No	No	0.0000	0.0000
T6	160.00-140.00	10.00	X Brace	No	No	0.0000	0.0000
T7	140.00-120.00	10.00	X Brace	No	No	0.0000	0.0000
T8	120.00-110.00	10.00	X Brace	No	No	0.0000	0.0000
T9	110.00-100.00	10.00	X Brace	No	Yes	0.0000	0.0000
T10	100.00-80.00	10.00	X Brace	No	No	0.0000	0.0000
T11	80.00-60.00	10.00	X Brace	No	No	0.0000	0.0000
T12	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T13	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T14	20.00-0.00	20.00	X Brace	No	No	0.0000	0.0000

### Tower Section Geometry (cont'd)

Tower Elevation	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
ft						
T1 245.00-230.00	Solid Round	1 1/2	A572-50 (50 ksi)	Solid Round	3/4	A572-50 (50 ksi)
T2 230.00-210.00	Solid Round	2	A572-50 (50 ksi)	Solid Round	7/8	A572-50 (50 ksi)
T3 210.00-190.00	Solid Round	2 1/2	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T4 190.00-180.00	Truss Leg	Pirol 105245	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T5 180.00-160.00	Truss Leg	Pirol 105217	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 160.00-140.00	Truss Leg	Pirol 105218	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T7 140.00-120.00	Truss Leg	Pirol 105218	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T8 120.00-110.00	Truss Leg	Pirol 105219	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T9 110.00-100.00	Truss Leg	Pirol 105219	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T10 100.00-80.00	Truss Leg	Pirol 105219	A572-50 (50 ksi)	Single Angle	L3x3x5/16	A36 (36 ksi)
T11 80.00-60.00	Truss Leg	Pirol 105220	A572-50 (50 ksi)	Single Angle	L3x3x5/16	A36 (36 ksi)
T12 60.00-40.00	Truss Leg	Pirol 105220	A572-50 (50 ksi)	Single Angle	L3 1/2x3 1/2x5/16	A36 (36 ksi)
T13 40.00-20.00	Truss Leg	Pirol 105220	A572-50 (50 ksi)	Single Angle	L4x4x1/4	A36 (36 ksi)
T14 20.00-0.00	Truss Leg	Pirol 112738	A572-50 (50 ksi)	Double Equal Angle	2L3 1/2x3 1/2x5/16x3/4	A36 (36 ksi)

### Tower Section Geometry (cont'd)



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<i>Tower Elevation</i> <i>ft</i>	<i>Top Girt Type</i>	<i>Top Girt Size</i>	<i>Top Girt Grade</i>	<i>Bottom Girt Type</i>	<i>Bottom Girt Size</i>	<i>Bottom Girt Grade</i>
T1 245.00-230.00	Solid Round	7/8	A572-50 (50 ksi)	Solid Round	7/8	A572-50 (50 ksi)
T2 230.00-210.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T3 210.00-190.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)

### Tower Section Geometry (cont'd)

<i>Tower Elevation</i> <i>ft</i>	<i>Secondary Horizontal Type</i>	<i>Secondary Horizontal Size</i>	<i>Secondary Horizontal Grade</i>	<i>Inner Bracing Type</i>	<i>Inner Bracing Size</i>	<i>Inner Bracing Grade</i>
T9 110.00-100.00	Equal Angle	L3x3x5/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)

### Tower Section Geometry (cont'd)

<i>Tower Elevation</i> <i>ft</i>	<i>Gusset Area</i> <i>(per face)</i> <i>ft<sup>2</sup></i>	<i>Gusset Thickness</i> <i>in</i>	<i>Gusset Grade</i>	<i>Adjust. Factor</i> <i>A<sub>f</sub></i>	<i>Adjust. Factor</i> <i>A<sub>r</sub></i>	<i>Weight Mult.</i>	<i>Double Angle</i> <i>Stitch Bolt</i> <i>Spacing</i> <i>Diagonals</i> <i>in</i>	<i>Double Angle</i> <i>Stitch Bolt</i> <i>Spacing</i> <i>Horizontals</i> <i>in</i>
T1 245.00-230.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T2 230.00-210.00	0.00	0.0000	A36 (36 ksi)	1	1	1.1	36.0000	36.0000
T3 210.00-190.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T4 190.00-180.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T5 180.00-160.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T6 160.00-140.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T7 140.00-120.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T8 120.00-110.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T9 110.00-100.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T10 100.00-80.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T11 80.00-60.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T12 60.00-40.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T13 40.00-20.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T14 20.00-0.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000



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### Tower Section Geometry (cont'd)

Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	K Factors <sup>1</sup>							
			Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y
ft										
T1	No	No	1	1	1	1	1	1	1	1
245.00-230.00				1	1	1	1	1	1	1
T2	No	No	1	1	1	1	1	1	1	1
230.00-210.00				1	1	1	1	1	1	1
T3	No	No	1	1	1	1	1	1	1	1
210.00-190.00				1	1	1	1	1	1	1
T4	No	No	1	1	1	1	1	1	1	1
190.00-180.00				1	1	1	1	1	1	1
T5	No	No	1	1	1	1	1	1	1	1
180.00-160.00				1	1	1	1	1	1	1
T6	No	No	1	1	1	1	1	1	1	1
160.00-140.00				1	1	1	1	1	1	1
T7	No	No	1	1	1	1	1	1	1	1
140.00-120.00				1	1	1	1	1	1	1
T8	No	No	1	1	1	1	1	1	1	1
120.00-110.00				1	1	1	1	1	1	1
T9	No	No	1	1	1	1	1	1	1	1
110.00-100.00				1	1	1	1	1	1	1
T10	No	No	1	1	1	1	1	1	1	1
100.00-80.00				1	1	1	1	1	1	1
T11	No	No	1	1	1	1	1	1	1	1
80.00-60.00				1	1	1	1	1	1	1
T12	No	No	1	1	1	1	1	1	1	1
60.00-40.00				1	1	1	1	1	1	1
T13	No	No	1	1	1	1	1	1	1	1
40.00-20.00				1	1	1	1	1	1	1
T14	No	No	1	1	1	1	1	1	1	1
20.00-0.00				1	1	1	1	1	1	1

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### Tower Section Geometry (cont'd)

Tower Elevation	Truss-Leg K Factors					
	Truss-Legs Used As Leg Members			Truss-Legs Used As Inner Members		
	Leg Panels	X Brace Diagonals	Z Brace Diagonals	Leg Panels	X Brace Diagonals	Z Brace Diagonals
ft						
T4	1	0.5	0.85	1	0.5	0.85
190.00-180.00						
T5	1	0.5	0.85	1	0.5	0.85
180.00-160.00						
T6	1	0.5	0.85	1	0.5	0.85
160.00-140.00						
T7	1	0.5	0.85	1	0.5	0.85
140.00-120.00						
T8	1	0.5	0.85	1	0.5	0.85
120.00-110.00						



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T9	1	0.5	0.85	1	0.5	0.85
110.00-100.00						
T10	1	0.5	0.85	1	0.5	0.85
100.00-80.00						
T11	1	0.5	0.85	1	0.5	0.85
80.00-60.00						
T12	1	0.5	0.85	1	0.5	0.85
60.00-40.00						
T13	1	0.5	0.85	1	0.5	0.85
40.00-20.00						
T14	1	0.5	0.85	1	0.5	0.85
20.00-0.00						

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
245.00-230.00														
T2	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
230.00-210.00														
T3	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
210.00-190.00														
T4	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
190.00-180.00														
T5	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
180.00-160.00														
T6	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
160.00-140.00														
T7	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
140.00-120.00														
T8	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
120.00-110.00														
T9	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
110.00-100.00														
T10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
100.00-80.00														
T11	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
80.00-60.00														
T12	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
60.00-40.00														
T13	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
40.00-20.00														
T14	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
20.00-0.00														

### Tower Section Geometry (cont'd)



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Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1	Sleeve DS	0.6250	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
245.00-230.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2	Flange	0.7500	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
230.00-210.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3	Flange	1.0000	6	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
210.00-190.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
190.00-180.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
180.00-160.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
160.00-140.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
140.00-120.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8	Flange	1.0000	0	1.2500	1	0.6250	0	0.0000	0	0.6250	0	0.6250	0	0.6250	0
120.00-110.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T9	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
110.00-100.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T10	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
100.00-80.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T11	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
80.00-60.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T12	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
60.00-40.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T13	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
40.00-20.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T14 20.00-0.00	Flange	1.2500	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 5/8 (Sprint)	A	Yes	Ar (CaAa)	245.00 - 0.00	-10.0000	0.42	6	3	1.9800	1.9800		1.04
1 1/4" Hybriflex Cables (Sprint)	A	Yes	Ar (CfAe)	245.00 - 0.00	-15.0000	0.4	3	3	1.5400	1.5400		1.08
"T-Bracket" (Sprint)	A	Yes	Af (CfAe)	245.00 - 0.00	-5.0000	0.47	1	1	0.7500	0.7500	3.0000	1.50
ALU Fiber Optic Cable (Sprint)	A	Yes	Ar (CfAe)	245.00 - 0.00	-10.0000	0.4	1	1	1.2500	1.2500		0.99
FEEDLINE LADDER (160')	C	Yes	Af (CfAe)	160.00 - 0.00	0.0000	0.4	1	1	3.0000	3.0000	12.0000	8.40
1/2 (DC Cable)	A	Yes	Ar (CfAe)	245.00 - 0.00	-8.0000	0.45	1	1	0.5800	0.5800		0.25
7/8 (135')	A	Yes	Ar (CfAe)	135.00 - 0.00	-8.0000	0.45	2	2	1.1100	1.1100		0.54
7/8 (125')	A	Yes	Ar (CfAe)	125.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54



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Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1/2 (125')	A	Yes	Ar (CfAe)	125.00 - 0.00	-8.0000	0.45	1	1	0.5800	0.5800		0.25
7/8 (110')	A	Yes	Ar (CfAe)	110.00 - 0.00	-8.0000	0.45	2	2	1.1100	1.1100		0.54
EW63 (105')	A	Yes	Af (CfAe)	105.00 - 0.00	-8.0000	0.45	1	1	1.5742	1.5742	5.0668	0.51
7/8 (60')	A	Yes	Ar (CfAe)	60.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54
7/8 (50')	A	Yes	Ar (CfAe)	50.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54
1 5/8 (T-Mobile)	B	Yes	Ar (CfAe)	235.00 - 0.00	-10.0000	0.42	12	6	1.9800	1.9800		1.04
"T-Bracket" (T-Mobile)	B	Yes	Af (CfAe)	235.00 - 0.00	-5.0000	0.47	1	1	0.7500	0.7500	3.0000	1.50
Hubner-Suhne r Hybrid Cable (T-Mobile)	B	Yes	Ar (CfAe)	235.00 - 0.00	-10.0000	0.4	1	1	0.7087	0.7087		0.48

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
T1	245.00-230.00	A	8.063	0.938	16.252	0.000	0.18
		B	5.245	0.313	0.000	0.000	0.07
		C	0.000	0.000	0.000	0.000	0.00
T2	230.00-210.00	A	10.750	1.250	21.670	0.000	0.24
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	0.000	0.000	0.000	0.00
T3	210.00-190.00	A	10.750	1.250	21.670	0.000	0.24
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	0.000	0.000	0.000	0.00
T4	190.00-180.00	A	5.375	0.625	10.835	0.000	0.12
		B	10.491	0.625	0.000	0.000	0.14
		C	0.000	0.000	0.000	0.000	0.00
T5	180.00-160.00	A	10.750	1.250	21.670	0.000	0.24
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	0.000	0.000	0.000	0.00
T6	160.00-140.00	A	10.750	1.250	21.670	0.000	0.24
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17
T7	140.00-120.00	A	14.229	1.250	21.670	0.000	0.26
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17
T8	120.00-110.00	A	8.633	0.625	10.835	0.000	0.14
		B	10.491	0.625	0.000	0.000	0.14
		C	0.000	2.500	0.000	0.000	0.08
T9	110.00-100.00	A	10.483	1.281	10.835	0.000	0.15
		B	10.491	0.625	0.000	0.000	0.14
		C	0.000	2.500	0.000	0.000	0.08
T10	100.00-80.00	A	20.967	3.874	21.670	0.000	0.31
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17
T11	80.00-60.00	A	20.967	3.874	21.670	0.000	0.31
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17
T12	60.00-40.00	A	23.742	3.874	21.670	0.000	0.33



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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T13	40.00-20.00	B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17
		A	24.667	3.874	21.670	0.000	0.34
		B	20.981	1.250	0.000	0.000	0.29
T14	20.00-0.00	C	0.000	5.000	0.000	0.000	0.17
		A	24.667	3.874	21.670	0.000	0.34
		B	20.981	1.250	0.000	0.000	0.29
		C	0.000	5.000	0.000	0.000	0.17

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T1	245.00-230.00	A	0.500	14.313	1.771	17.752	0.000	0.42
		B		8.162	0.590	0.000	0.000	0.17
		C		0.000	0.000	0.000	0.000	0.00
T2	230.00-210.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	0.000	0.000	0.000	0.00
T3	210.00-190.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	0.000	0.000	0.000	0.00
T4	190.00-180.00	A	0.500	9.542	1.181	11.835	0.000	0.28
		B		16.324	1.181	0.000	0.000	0.34
		C		0.000	0.000	0.000	0.000	0.00
T5	180.00-160.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	0.000	0.000	0.000	0.00
T6	160.00-140.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T7	140.00-120.00	A	0.500	25.896	2.361	23.670	0.000	0.61
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T8	120.00-110.00	A	0.500	16.133	1.181	11.835	0.000	0.33
		B		16.324	1.181	0.000	0.000	0.34
		C		0.000	3.056	0.000	0.000	0.11
T9	110.00-100.00	A	0.500	19.650	2.114	11.835	0.000	0.37
		B		16.324	1.181	0.000	0.000	0.34
		C		0.000	3.056	0.000	0.000	0.11
T10	100.00-80.00	A	0.500	39.300	6.096	23.670	0.000	0.76
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T11	80.00-60.00	A	0.500	39.300	6.096	23.670	0.000	0.76
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T12	60.00-40.00	A	0.500	44.575	6.096	23.670	0.000	0.81
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T13	40.00-20.00	A	0.500	46.333	6.096	23.670	0.000	0.82
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22
T14	20.00-0.00	A	0.500	46.333	6.096	23.670	0.000	0.82
		B		32.648	2.361	0.000	0.000	0.69
		C		0.000	6.111	0.000	0.000	0.22



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### Feed Line Shielding

Section	Elevation	Face	$A_R$	$A_{R_{Ice}}$	$A_F$	$A_{F_{Ice}}$
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>
T1	245.00-230.00	A	1.110	4.314	0.000	0.000
		B	0.376	1.386	0.000	0.000
		C	0.000	0.000	0.000	0.000
T2	230.00-210.00	A	1.646	5.901	0.000	0.000
		B	1.671	5.687	0.000	0.000
		C	0.000	0.000	0.000	0.000
T3	210.00-190.00	A	1.809	6.098	0.000	0.000
		B	1.837	5.877	0.000	0.000
		C	0.000	0.000	0.000	0.000
T4	190.00-180.00	A	0.000	0.637	0.946	1.594
		B	0.000	0.614	0.960	1.536
		C	0.000	0.000	0.000	0.000
T5	180.00-160.00	A	0.000	1.076	1.597	2.690
		B	0.000	1.037	1.621	2.593
		C	0.000	0.000	0.000	0.000
T6	160.00-140.00	A	0.000	0.921	1.367	2.302
		B	0.000	0.888	1.387	2.219
		C	0.000	0.166	0.312	0.416
T7	140.00-120.00	A	0.000	0.986	1.717	2.957
		B	0.000	0.802	1.504	2.406
		C	0.000	0.150	0.338	0.451
T8	120.00-110.00	A	0.000	0.534	0.910	1.603
		B	0.000	0.380	0.712	1.139
		C	0.000	0.071	0.160	0.213
T9	110.00-100.00	A	0.000	0.861	1.458	2.584
		B	0.000	0.517	0.969	1.551
		C	0.000	0.097	0.218	0.291
T10	100.00-80.00	A	0.000	1.231	2.088	3.692
		B	0.000	0.713	1.336	2.138
		C	0.000	0.134	0.301	0.401
T11	80.00-60.00	A	0.000	1.188	2.016	3.563
		B	0.000	0.688	1.290	2.064
		C	0.000	0.129	0.290	0.387
T12	60.00-40.00	A	0.000	1.256	2.473	4.396
		B	0.000	0.670	1.466	2.345
		C	0.000	0.126	0.330	0.440
T13	40.00-20.00	A	0.000	1.264	2.839	5.054
		B	0.000	0.657	1.642	2.626
		C	0.000	0.123	0.369	0.492
T14	20.00-0.00	A	0.000	0.756	1.486	2.645
		B	0.000	0.393	0.859	1.374
		C	0.000	0.074	0.193	0.258

### Feed Line Center of Pressure

Section	Elevation	$CP_X$	$CP_Z$	$CP_{X_{Ice}}$	$CP_{Z_{Ice}}$
	ft	in	in	in	in
T1	245.00-230.00	2.4274	-3.7725	2.3713	-3.2824
T2	230.00-210.00	3.5092	-2.1483	3.5744	-1.6269
T3	210.00-190.00	3.5931	-2.4523	3.7063	-1.9085



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Section	Elevation	CP <sub>X</sub>	CP <sub>Z</sub>	CP <sub>X</sub> Ice	CP <sub>Z</sub> Ice
	ft	in	in	in	in
T4	190.00-180.00	3.0332	-2.3256	3.1758	-1.8195
T5	180.00-160.00	3.7537	-3.3037	4.0139	-2.6798
T6	160.00-140.00	3.5542	-3.6778	4.0783	-3.0506
T7	140.00-120.00	4.0133	-5.3865	4.6799	-5.0227
T8	120.00-110.00	4.3079	-6.7785	5.0377	-6.7517
T9	110.00-100.00	4.1500	-8.0208	4.8313	-8.2418
T10	100.00-80.00	4.8833	-10.0135	5.7279	-10.3607
T11	80.00-60.00	5.2414	-11.1077	6.1752	-11.5158
T12	60.00-40.00	5.3930	-12.7766	6.4235	-13.6460
T13	40.00-20.00	5.5013	-13.7065	6.6369	-14.8720
T14	20.00-0.00	6.2812	-15.7421	7.6827	-17.3842

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
Lightning Rod 2"x10' (Tower)	C	From Leg	5.00 0.00 5.00	0.0000	247.00	No Ice 1/2" Ice 3.02	2.00 3.02	0.04 0.06
Flash Beacon Lighting (Tower)	A	From Leg	0.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice 2.76	2.50 2.76	0.03 0.06
2.5" Dia. 12' OMNI	A	From Leg	4.00 0.00 5.00	0.0000	135.00	No Ice 1/2" Ice 3.53	2.50 3.53	0.03 0.05
4' Standoff Mount	A	From Leg	2.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice 4.91	2.72 4.91	0.05 0.09
2.5" Dia. 12' OMNI	C	From Leg	4.00 0.00 5.00	0.0000	135.00	No Ice 1/2" Ice 3.53	2.50 3.53	0.03 0.05
4' Standoff Mount	C	From Leg	2.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice 4.91	2.72 4.91	0.05 0.09
20' Omni	A	From Leg	6.00 0.00 10.00	0.0000	125.00	No Ice 1/2" Ice 8.03	6.00 8.03	0.06 0.10
6' Standoff Mount	A	From Leg	3.00 0.00 0.00	0.0000	125.00	No Ice 1/2" Ice 6.12	4.97 7.27	0.07 0.13
(3) L-810 Obstruction Lights w/ Mount Kit (Tower)	C	None		0.0000	125.00	No Ice 1/2" Ice 0.97	0.85 0.53	0.05 0.05
2.5" Dia. 12' OMNI	C	From Leg	4.00 0.00 5.00	0.0000	110.00	No Ice 1/2" Ice 3.53	2.50 3.53	0.03 0.05
4' Standoff Mount	C	From Leg	2.00 0.00 0.00	0.0000	110.00	No Ice 1/2" Ice 4.91	2.72 4.91	0.05 0.09
Camera with Mount	A	From Leg	0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 5.92	5.60 5.92	0.15 0.21



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
1.5" Dia 4' Omni w/Pipe Mount	A	From Leg	0.00 4.00 0.00 5.00	0.0000	50.00	No Ice 1/2" Ice	0.94 1.39	0.94 1.39	0.02 0.03
4' Standoff Mount	A	From Leg	2.00 0.00 0.00	0.0000	50.00	No Ice 1/2" Ice	2.72 4.91	2.72 4.91	0.05 0.09
APXVSPP18-C-A20 w/ Mounting Pipe (Sprint)	A	From Face	4.00 -2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	8.56 9.21	6.95 8.13	0.08 0.15
APXV9ERR18-C-A20 w/ 6' Mount Pipe (Sprint)	B	From Face	4.00 -2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	10.35 10.97	6.37 7.37	0.06 0.13
APXVSPP18-C-A20 w/ Mounting Pipe (Sprint)	C	From Face	4.00 -2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	8.56 9.21	6.95 8.13	0.08 0.15
(2) Panasonic RRH 1900MHZ (Sprint)	A	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.71 2.95	2.61 2.84	0.06 0.08
(2) Panasonic RRH 1900MHZ (Sprint)	B	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.71 2.95	2.61 2.84	0.06 0.08
(2) Panasonic RRH 1900MHZ (Sprint)	C	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.71 2.95	2.61 2.84	0.06 0.08
Andrew 800MHz RRH (Sprint)	A	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.49 2.57	1.97 2.17	0.06 0.08
Andrew 800MHz RRH (Sprint)	B	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.49 2.57	1.97 2.17	0.06 0.08
Andrew 800MHz RRH (Sprint)	C	From Face	4.00 2.00 0.00	0.0000	247.00	No Ice 1/2" Ice	2.49 2.57	1.97 2.17	0.06 0.08
IBC1900BB-1 Combiner (Sprint)	A	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
IBC1900BB-1 Combiner (Sprint)	B	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
IBC1900BB-1 Combiner (Sprint)	C	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
IBC1900HG-2A Combiner (Sprint)	A	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
IBC1900HG-2A Combiner (Sprint)	B	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
IBC1900HG-2A Combiner (Sprint)	C	From Face	4.00 0.00 0.00	0.0000	247.00	No Ice 1/2" Ice	1.13 1.27	0.54 0.65	0.02 0.03
PiROD Rotatable Platform #122379 (Sprint)	C	None		0.0000	247.00	No Ice 1/2" Ice	24.90 30.70	24.90 30.70	1.81 2.44
APXV9TM14-120 (Sprint)	A	From Face	4.00 6.00	0.0000	247.00	No Ice 1/2" Ice	7.27 7.80	5.33 6.05	0.10 0.16



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
APXV9TM14-120 (Sprint)	B	From Face	0.00 4.00 6.00 0.00	0.0000	247.00	No Ice 1/2" Ice	7.27 7.80	5.33 6.05	0.10 0.16
APXV9TM14-120 (Sprint)	C	From Face	4.00 6.00 0.00	0.0000	247.00	No Ice 1/2" Ice	7.27 7.80	5.33 6.05	0.10 0.16
TD-RRH 8x20 (Sprint)	A	From Face	4.00 6.00 0.00	0.0000	247.00	No Ice 1/2" Ice	4.72 5.01	1.70 1.92	0.07 0.10
TD-RRH 8x20 (Sprint)	B	From Face	4.00 6.00 0.00	0.0000	247.00	No Ice 1/2" Ice	4.72 5.01	1.70 1.92	0.07 0.10
TD-RRH 8x20 (Sprint)	C	From Face	4.00 6.00 0.00	0.0000	247.00	No Ice 1/2" Ice	4.72 5.01	1.70 1.92	0.07 0.10
TMA (T-Mobile)	A	From Face	4.00 0.00 0.00	0.0000	235.00	No Ice 1/2" Ice	1.40 1.56	0.70 0.82	0.01 0.02
TMA (T-Mobile)	B	From Face	4.00 0.00 0.00	0.0000	235.00	No Ice 1/2" Ice	1.40 1.56	0.70 0.82	0.01 0.02
TMA (T-Mobile)	C	From Face	4.00 0.00 0.00	0.0000	235.00	No Ice 1/2" Ice	1.40 1.56	0.70 0.82	0.01 0.02
PiROD 12' Universal T-Frame (3) (T-Mobile)	C	None		0.0000	235.00	No Ice 1/2" Ice	21.88 30.68	21.88 30.68	1.07 1.49
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	A	From Face	4.00 -6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
AIR B4A/B2P w/ 6' Sch 40 Pipe Mount (T-Mobile)	A	From Face	4.00 6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	B	From Face	4.00 -6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
AIR B4A/B2P w/ 6' Sch 40 Pipe Mount (T-Mobile)	B	From Face	4.00 6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	C	From Face	4.00 -6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
AIR B4A/B2P w/ 6' Sch 40 Pipe Mount (T-Mobile)	C	From Face	4.00 6.00 0.00	0.0000	235.00	No Ice 1/2" Ice	6.75 7.31	5.65 6.56	0.10 0.16
LNx-6515DS-VTM (T-Mobile)	A	From Face	4.00 2.00 0.00	0.0000	235.00	No Ice 1/2" Ice	11.39 12.01	9.96 11.38	0.09 0.18
LNx-6515DS-VTM (T-Mobile)	B	From Face	4.00 2.00 0.00	0.0000	235.00	No Ice 1/2" Ice	11.39 12.01	9.96 11.38	0.09 0.18
LNx-6515DS-VTM (T-Mobile)	C	From Face	4.00 2.00 0.00	0.0000	235.00	No Ice 1/2" Ice	11.39 12.01	9.96 11.38	0.09 0.18
RRUS-11 (T-Mobile)	A	From Face	4.00 2.00	0.0000	235.00	No Ice 1/2" Ice	3.00 3.23	1.53 1.82	0.06 0.08



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	<b>Project</b>	<b>Date</b>
	Storrs (UCONN), CT (Site: CT11303B) / NSS-022	15:37:53 04/01/15
	<b>Client</b>	<b>Designed by</b>
	Northeast Site Solutions / T-Mobile	MCD

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
RRUS-11 (T-Mobile)	B	From Face	0.00 4.00 2.00 0.00	0.0000	235.00	No Ice 1/2" Ice 3.00 3.23	1.53 1.82	0.06 0.08
RRUS-11 (T-Mobile)	C	From Face	4.00 2.00 0.00	0.0000	235.00	No Ice 1/2" Ice 3.00 3.23	1.53 1.82	0.06 0.08

### Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert ft	Azimuth Adjustment °	3 dB Beam Width °	Elevation ft	Outside Diameter ft	Aperture Area ft <sup>2</sup>	Weight K
KP4F-23	B	Grid	From Face	1.00 -6.00 0.00	0.0000		110.00	4.00	No Ice 1/2" Ice 10.05 13.09	0.05 0.12
Andrew 6' w/Radome	B	Paraboloid w/Radome	From Face	1.00 -6.00 0.00	0.0000		105.00	6.00	No Ice 1/2" Ice 28.27 29.07	0.38 0.45

### Truss-Leg Properties

Section Designation	Area in <sup>2</sup>	Area Ice in <sup>2</sup>	Self Weight K	Ice Weight K	Equiv. Diameter in	Equiv. Diameter Ice in	Leg Area in <sup>2</sup>
Pirol 105245	1090.3344	1814.3549	0.68	0.22	7.5718	12.5997	5.3014
Pirol 105217	2130.7479	3520.4599	0.62	0.44	7.3984	12.2238	5.3014
Pirol 105218	2263.4687	3690.8612	0.75	0.46	7.8593	12.8155	7.2158
Pirol 105218	2263.4687	3690.8612	0.75	0.46	7.8593	12.8155	7.2158
Pirol 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirol 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirol 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirol 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirol 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirol 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirol 112738	3466.5160	5074.9521	1.69	0.68	12.0365	17.6214	14.7262

### Tower Pressures - No Ice

$$G_H = 1.101$$



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 245.00-230.00	237.50	1.758	33	61.875	A	0.938	14.632	3.750	24.09	16.252	0.000
					B	0.313	12.549		29.16	0.000	0.000
					C	0.000	7.680		48.83	0.000	0.000
T2 230.00-210.00	220.00	1.72	32	88.334	A	1.250	21.909	6.667	28.79	21.670	0.000
					B	1.250	32.116		19.98	0.000	0.000
					C	0.000	12.806		52.07	0.000	0.000
T3 210.00-190.00	200.00	1.673	31	99.167	A	1.250	24.779	8.334	32.02	21.670	0.000
					B	1.250	34.982		23.00	0.000	0.000
					C	0.000	15.838		52.62	0.000	0.000
T4 190.00-180.00	185.00	1.636	30	66.264	A	3.914	18.016	12.641	57.64	10.835	0.000
					B	3.900	23.131		46.76	0.000	0.000
					C	4.235	12.641		74.90	0.000	0.000
T5 180.00-160.00	170.00	1.597	30	162.528	A	8.376	35.453	24.703	56.36	21.670	0.000
					B	8.352	45.684		45.72	0.000	0.000
					C	8.723	24.703		73.90	0.000	0.000
T6 160.00-140.00	150.00	1.541	29	202.945	A	9.854	36.991	26.241	56.02	21.670	0.000
					B	9.833	47.222		45.99	0.000	0.000
					C	14.658	26.241		64.16	0.000	0.000
T7 140.00-120.00	130.00	1.48	27	242.945	A	13.053	40.470	26.241	49.03	21.670	0.000
					B	13.266	47.222		43.38	0.000	0.000
					C	18.182	26.241		59.07	0.000	0.000
T8 120.00-110.00	115.00	1.429	26	136.681	A	7.080	22.788	14.155	47.39	10.835	0.000
					B	7.278	24.645		44.34	0.000	0.000
					C	9.705	14.155		59.32	0.000	0.000
T9 110.00-100.00	105.00	1.392	26	146.681	A	10.723	24.638	14.155	40.03	10.835	0.000
					B	10.555	24.645		40.21	0.000	0.000
					C	13.182	14.155		51.78	0.000	0.000
T10 100.00-80.00	90.00	1.332	25	323.362	A	18.615	49.276	28.309	41.70	21.670	0.000
					B	16.743	49.291		42.87	0.000	0.000
					C	21.529	28.309		56.80	0.000	0.000
T11 80.00-60.00	70.00	1.24	23	363.780	A	20.424	50.864	29.897	41.94	21.670	0.000
					B	18.526	50.878		43.08	0.000	0.000
					C	23.276	29.897		56.23	0.000	0.000
T12 60.00-40.00	50.00	1.126	21	403.780	A	25.135	53.639	29.897	37.95	21.670	0.000
					B	23.519	50.878		40.19	0.000	0.000
					C	28.405	29.897		51.28	0.000	0.000
T13 40.00-20.00	30.00	1	18	443.780	A	30.574	54.564	29.897	35.12	21.670	0.000
					B	29.148	50.878		37.36	0.000	0.000
					C	34.170	29.897		46.67	0.000	0.000
T14 20.00-0.00	10.00	1	18	494.209	A	19.205	64.855	40.189	47.81	21.670	0.000
					B	17.208	61.170		51.28	0.000	0.000
					C	21.624	40.189		65.02	0.000	0.000

### Tower Pressure - With Ice

$$G_H = 1.101$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 245.00-230.00	237.50	1.758	24	0.5000	63.125	A	1.771	25.310	6.250	23.08	17.752	0.000
						B	0.590	22.087		27.56	0.000	0.000
						C	0.000	15.312		40.82	0.000	0.000
T2 230.00-210.00	220.00	1.72	24	0.5000	90.000	A	2.361	36.240	10.001	25.91	23.670	0.000
						B	2.361	50.018		19.09	0.000	0.000



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	I <sub>Z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T3 210.00-190.00	200.00	1.673	23	0.5000	100.834	C	0.000	23.057		43.37	0.000	0.000
						A	2.361	39.661	11.668	27.77	23.670	0.000
						B	2.361	53.447		20.91	0.000	0.000
						C	0.000	26.676		43.74	0.000	0.000
T4 190.00-180.00	185.00	1.636	23	0.5000	67.098	A	3.822	31.633	21.034	59.33	11.835	0.000
						B	3.880	38.438		49.71	0.000	0.000
						C	4.235	22.728		78.01	0.000	0.000
T5 180.00-160.00	170.00	1.597	22	0.5000	164.197	A	8.393	62.310	40.814	57.73	23.670	0.000
						B	8.491	75.914		48.36	0.000	0.000
						C	8.723	44.303		76.97	0.000	0.000
T6 160.00-140.00	150.00	1.541	21	0.5000	204.614	A	10.029	64.940	42.789	57.08	23.670	0.000
						B	10.112	78.538		48.27	0.000	0.000
						C	15.665	46.611		68.71	0.000	0.000
T7 140.00-120.00	130.00	1.48	21	0.5000	244.614	A	12.924	72.206	42.789	50.26	23.670	0.000
						B	13.475	79.142		46.20	0.000	0.000
						C	19.180	47.146		64.51	0.000	0.000
T8 120.00-110.00	115.00	1.429	20	0.5000	137.516	A	6.942	40.906	22.852	47.76	11.835	0.000
						B	7.407	41.252		46.96	0.000	0.000
						C	10.207	25.236		64.48	0.000	0.000
T9 110.00-100.00	105.00	1.392	19	0.5000	147.516	A	10.429	45.274	22.852	41.02	11.835	0.000
						B	10.529	42.292		43.26	0.000	0.000
						C	13.664	26.388		57.06	0.000	0.000
T10 100.00-80.00	90.00	1.332	18	0.5000	325.031	A	19.234	89.384	45.704	42.08	23.670	0.000
						B	17.053	83.249		45.57	0.000	0.000
						C	22.540	51.181		62.00	0.000	0.000
T11 80.00-60.00	70.00	1.24	17	0.5000	365.448	A	21.099	92.211	47.910	42.28	23.670	0.000
						B	18.864	86.059		45.66	0.000	0.000
						C	24.291	53.970		61.22	0.000	0.000
T12 60.00-40.00	50.00	1.126	16	0.5000	405.448	A	25.434	98.010	47.910	38.81	23.670	0.000
						B	23.751	86.669		43.39	0.000	0.000
						C	29.406	54.566		57.05	0.000	0.000
T13 40.00-20.00	30.00	1	14	0.5000	445.448	A	30.581	100.365	47.910	36.59	23.670	0.000
						B	29.274	87.286		41.10	0.000	0.000
						C	35.158	55.172		53.04	0.000	0.000
T14 20.00-0.00	10.00	1	14	0.5000	495.878	A	20.268	109.218	58.836	45.44	23.670	0.000
						B	17.803	95.896		51.75	0.000	0.000
						C	22.670	63.567		68.23	0.000	0.000

## Tower Pressure - Service

$$G_H = 1.101$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 245.00-230.00	237.50	1.758	11	61.875	A	0.938	14.632	3.750	24.09	16.252	0.000
					B	0.313	12.549		29.16	0.000	0.000
					C	0.000	7.680		48.83	0.000	0.000
T2 230.00-210.00	220.00	1.72	11	88.334	A	1.250	21.909	6.667	28.79	21.670	0.000
					B	1.250	32.116		19.98	0.000	0.000
					C	0.000	12.806		52.07	0.000	0.000
T3 210.00-190.00	200.00	1.673	11	99.167	A	1.250	24.779	8.334	32.02	21.670	0.000
					B	1.250	34.982		23.00	0.000	0.000
					C	0.000	15.838		52.62	0.000	0.000



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T4 190.00-180.00	185.00	1.636	10	66.264	A	3.914	18.016	12.641	57.64	10.835	0.000
					B	3.900	23.131		46.76	0.000	0.000
					C	4.235	12.641		74.90	0.000	0.000
T5 180.00-160.00	170.00	1.597	10	162.528	A	8.376	35.453	24.703	56.36	21.670	0.000
					B	8.352	45.684		45.72	0.000	0.000
					C	8.723	24.703		73.90	0.000	0.000
T6 160.00-140.00	150.00	1.541	10	202.945	A	9.854	36.991	26.241	56.02	21.670	0.000
					B	9.833	47.222		45.99	0.000	0.000
					C	14.658	26.241		64.16	0.000	0.000
T7 140.00-120.00	130.00	1.48	9	242.945	A	13.053	40.470	26.241	49.03	21.670	0.000
					B	13.266	47.222		43.38	0.000	0.000
					C	18.182	26.241		59.07	0.000	0.000
T8 120.00-110.00	115.00	1.429	9	136.681	A	7.080	22.788	14.155	47.39	10.835	0.000
					B	7.278	24.645		44.34	0.000	0.000
					C	9.705	14.155		59.32	0.000	0.000
T9 110.00-100.00	105.00	1.392	9	146.681	A	10.723	24.638	14.155	40.03	10.835	0.000
					B	10.555	24.645		40.21	0.000	0.000
					C	13.182	14.155		51.78	0.000	0.000
T10 100.00-80.00	90.00	1.332	9	323.362	A	18.615	49.276	28.309	41.70	21.670	0.000
					B	16.743	49.291		42.87	0.000	0.000
					C	21.529	28.309		56.80	0.000	0.000
T11 80.00-60.00	70.00	1.24	8	363.780	A	20.424	50.864	29.897	41.94	21.670	0.000
					B	18.526	50.878		43.08	0.000	0.000
					C	23.276	29.897		56.23	0.000	0.000
T12 60.00-40.00	50.00	1.126	7	403.780	A	25.135	53.639	29.897	37.95	21.670	0.000
					B	23.519	50.878		40.19	0.000	0.000
					C	28.405	29.897		51.28	0.000	0.000
T13 40.00-20.00	30.00	1	6	443.780	A	30.574	54.564	29.897	35.12	21.670	0.000
					B	29.148	50.878		37.36	0.000	0.000
					C	34.170	29.897		46.67	0.000	0.000
T14 20.00-0.00	10.00	1	6	494.209	A	19.205	64.855	40.189	47.81	21.670	0.000
					B	17.208	61.170		51.28	0.000	0.000
					C	21.624	40.189		65.02	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>R</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.26	0.60	A	0.252	2.433	0.602	1	1	9.750	1.43	95.33	A
			B	0.208	2.57	0.592	1	1	7.742			
			C	0.124	2.869	0.578	1	1	4.438			
T2 230.00-210.00	0.53	1.31	A	0.262	2.401	0.605	1	1	14.506	2.38	118.76	B
			B	0.378	2.11	0.643	1	1	21.893			
			C	0.145	2.79	0.581	1	1	7.436			
T3 210.00-190.00	0.53	1.85	A	0.262	2.401	0.605	1	1	16.244	2.45	122.68	B
			B	0.365	2.137	0.638	1	1	23.572			
			C	0.16	2.736	0.583	1	1	9.234			
T4 190.00-180.00	0.27	1.24	A	0.331	2.217	0.626	1	1	15.189	1.66	166.08	B
			B	0.408	2.049	0.655	1	1	19.048			
			C	0.255	2.424	0.603	1	1	11.858			
T5 180.00-160.00	0.53	2.33	A	0.27	2.38	0.607	1	1	29.899	3.37	168.25	B
			B	0.332	2.213	0.626	1	1	36.967			
			C	0.206	2.577	0.592	1	1	23.336			
T6 160.00-140.00	0.70	2.79	A	0.231	2.496	0.597	1	1	31.944	3.53	176.33	B
			B	0.281	2.347	0.61	1	1	38.653			



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T7	0.72	2.96	C	0.202	2.591	0.591	1	1	30.159			
140.00-120.00			A	0.22	2.53	0.595	1	1	37.123	3.72	185.80	B
			B	0.249	2.441	0.602	1	1	41.676			
T8	0.37	1.79	C	0.183	2.654	0.587	1	1	33.587			
120.00-110.00			A	0.219	2.535	0.594	1	1	20.624	1.91	190.75	B
			B	0.234	2.488	0.598	1	1	22.012			
T9	0.38	2.07	C	0.175	2.683	0.586	1	1	17.993			
110.00-100.00			A	0.241	2.465	0.6	1	1	25.497	2.09	208.75	A
			B	0.24	2.468	0.599	1	1	25.327			
T10	0.77	4.21	C	0.186	2.642	0.588	1	1	21.500			
100.00-80.00			A	0.21	2.563	0.592	1	1	47.810	3.91	195.51	A
			B	0.204	2.582	0.591	1	1	45.887			
T11	0.77	4.87	C	0.154	2.756	0.582	1	1	38.009			
80.00-60.00			A	0.196	2.61	0.59	1	1	50.413	3.87	193.33	A
			B	0.191	2.627	0.589	1	1	48.471			
T12	0.79	5.29	C	0.146	2.786	0.581	1	1	40.643			
60.00-40.00			A	0.195	2.612	0.589	1	1	56.750	3.90	194.76	A
			B	0.184	2.649	0.587	1	1	53.400			
T13	0.79	5.30	C	0.144	2.792	0.581	1	1	45.764			
40.00-20.00			A	0.192	2.623	0.589	1	1	62.700	3.79	189.48	A
			B	0.18	2.663	0.587	1	1	58.992			
T14	0.79	7.81	C	0.144	2.792	0.581	1	1	51.529			
20.00-0.00			A	0.17	2.699	0.585	1	1	57.129	3.58	178.99	A
			B	0.159	2.74	0.583	1	1	52.859			
			C	0.125	2.865	0.578	1	1	44.852			
Sum Weight:	8.21	44.43						OTM	4649.66 kip-ft	41.56		

### Tower Forces - No Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.26	0.60	A	0.252	2.433	0.602	0.825	1	9.586	1.42	94.38	A
245.00-230.00			B	0.208	2.57	0.592	0.825	1	7.687			
			C	0.124	2.869	0.578	0.825	1	4.438			
T2	0.53	1.31	A	0.262	2.401	0.605	0.825	1	14.288	2.36	117.95	B
230.00-210.00			B	0.378	2.11	0.643	0.825	1	21.674			
			C	0.145	2.79	0.581	0.825	1	7.436			
T3	0.53	1.85	A	0.262	2.401	0.605	0.825	1	16.026	2.44	121.89	B
210.00-190.00			B	0.365	2.137	0.638	0.825	1	23.353			
			C	0.16	2.736	0.583	0.825	1	9.234			
T4	0.27	1.24	A	0.331	2.217	0.626	0.825	1	14.505	1.61	161.42	B
190.00-180.00			B	0.408	2.049	0.655	0.825	1	18.365			
			C	0.255	2.424	0.603	0.825	1	11.117			
T5	0.53	2.33	A	0.27	2.38	0.607	0.825	1	28.433	3.26	162.99	B
180.00-160.00			B	0.332	2.213	0.626	0.825	1	35.505			
			C	0.206	2.577	0.592	0.825	1	21.809			
T6	0.70	2.79	A	0.231	2.496	0.597	0.825	1	30.219	3.40	169.99	B
160.00-140.00			B	0.281	2.347	0.61	0.825	1	36.933			
			C	0.202	2.591	0.591	0.825	1	27.594			
T7	0.72	2.96	A	0.22	2.53	0.595	0.825	1	34.839	3.55	177.27	B
140.00-120.00			B	0.249	2.441	0.602	0.825	1	39.354			
			C	0.183	2.654	0.587	0.825	1	30.405			
T8	0.37	1.79	A	0.219	2.535	0.594	0.825	1	19.385	1.82	181.54	B



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
120.00-110.00			B	0.234	2.488	0.598	0.825	1	20.738			
			C	0.175	2.683	0.586	0.825	1	16.295			
T9	0.38	2.07	A	0.241	2.465	0.6	0.825	1	23.620	1.96	195.65	A
110.00-100.00			B	0.24	2.468	0.599	0.825	1	23.480			
			C	0.186	2.642	0.588	0.825	1	19.194			
T10	0.77	4.21	A	0.21	2.563	0.592	0.825	1	44.553	3.68	184.19	A
100.00-80.00			B	0.204	2.582	0.591	0.825	1	42.957			
			C	0.154	2.756	0.582	0.825	1	34.241			
T11	0.77	4.87	A	0.196	2.61	0.59	0.825	1	46.838	3.63	181.56	A
80.00-60.00			B	0.191	2.627	0.589	0.825	1	45.229			
			C	0.146	2.786	0.581	0.825	1	36.570			
T12	0.79	5.29	A	0.195	2.612	0.589	0.825	1	52.351	3.63	181.59	A
60.00-40.00			B	0.184	2.649	0.587	0.825	1	49.284			
			C	0.144	2.792	0.581	0.825	1	40.793			
T13	0.79	5.30	A	0.192	2.623	0.589	0.825	1	57.349	3.50	175.19	A
40.00-20.00			B	0.18	2.663	0.587	0.825	1	53.891			
			C	0.144	2.792	0.581	0.825	1	45.549			
T14	0.79	7.81	A	0.17	2.699	0.585	0.825	1	53.768	3.40	169.76	A
20.00-0.00			B	0.159	2.74	0.583	0.825	1	49.848			
			C	0.125	2.865	0.578	0.825	1	41.067			
Sum Weight:	8.21	44.43						OTM	4487.04 kip-ft	39.65		

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.26	0.60	A	0.252	2.433	0.602	0.8	1	9.563	1.41	94.25	A
245.00-230.00			B	0.208	2.57	0.592	0.8	1	7.680			
			C	0.124	2.869	0.578	0.8	1	4.438			
T2	0.53	1.31	A	0.262	2.401	0.605	0.8	1	14.256	2.36	117.84	B
230.00-210.00			B	0.378	2.11	0.643	0.8	1	21.643			
			C	0.145	2.79	0.581	0.8	1	7.436			
T3	0.53	1.85	A	0.262	2.401	0.605	0.8	1	15.994	2.44	121.77	B
210.00-190.00			B	0.365	2.137	0.638	0.8	1	23.322			
			C	0.16	2.736	0.583	0.8	1	9.234			
T4	0.27	1.24	A	0.331	2.217	0.626	0.8	1	14.407	1.61	160.75	B
190.00-180.00			B	0.408	2.049	0.655	0.8	1	18.268			
			C	0.255	2.424	0.603	0.8	1	11.011			
T5	0.53	2.33	A	0.27	2.38	0.607	0.8	1	28.224	3.24	162.24	B
180.00-160.00			B	0.332	2.213	0.626	0.8	1	35.296			
			C	0.206	2.577	0.592	0.8	1	21.591			
T6	0.70	2.79	A	0.231	2.496	0.597	0.8	1	29.973	3.38	169.09	B
160.00-140.00			B	0.281	2.347	0.61	0.8	1	36.687			
			C	0.202	2.591	0.591	0.8	1	27.228			
T7	0.72	2.96	A	0.22	2.53	0.595	0.8	1	34.512	3.52	176.05	B
140.00-120.00			B	0.249	2.441	0.602	0.8	1	39.023			
			C	0.183	2.654	0.587	0.8	1	29.950			
T8	0.37	1.79	A	0.219	2.535	0.594	0.8	1	19.208	1.80	180.22	B
120.00-110.00			B	0.234	2.488	0.598	0.8	1	20.556			
			C	0.175	2.683	0.586	0.8	1	16.052			
T9	0.38	2.07	A	0.241	2.465	0.6	0.8	1	23.352	1.94	193.77	A
110.00-100.00			B	0.24	2.468	0.599	0.8	1	23.216			
			C	0.186	2.642	0.588	0.8	1	18.864			



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T10 100.00-80.00	0.77	4.21	A	0.21	2.563	0.592	0.8	1	44.087	3.65	182.57	A
			B	0.204	2.582	0.591	0.8	1	42.539			
			C	0.154	2.756	0.582	0.8	1	33.703			
T11 80.00-60.00	0.77	4.87	A	0.196	2.61	0.59	0.8	1	46.328	3.60	179.88	A
			B	0.191	2.627	0.589	0.8	1	44.766			
			C	0.146	2.786	0.581	0.8	1	35.988			
T12 60.00-40.00	0.79	5.29	A	0.195	2.612	0.589	0.8	1	51.723	3.59	179.71	A
			B	0.184	2.649	0.587	0.8	1	48.696			
			C	0.144	2.792	0.581	0.8	1	40.083			
T13 40.00-20.00	0.79	5.30	A	0.192	2.623	0.589	0.8	1	56.585	3.46	173.15	A
			B	0.18	2.663	0.587	0.8	1	53.162			
			C	0.144	2.792	0.581	0.8	1	44.695			
T14 20.00-0.00	0.79	7.81	A	0.17	2.699	0.585	0.8	1	53.288	3.37	168.44	A
			B	0.159	2.74	0.583	0.8	1	49.417			
			C	0.125	2.865	0.578	0.8	1	40.527			
Sum Weight:	8.21	44.43						OTM	4463.81 kip-ft	39.38		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.26	0.60	A	0.252	2.433	0.602	0.85	1	9.609	1.42	94.52	A
			B	0.208	2.57	0.592	0.85	1	7.695			
			C	0.124	2.869	0.578	0.85	1	4.438			
T2 230.00-210.00	0.53	1.31	A	0.262	2.401	0.605	0.85	1	14.319	2.36	118.07	B
			B	0.378	2.11	0.643	0.85	1	21.705			
			C	0.145	2.79	0.581	0.85	1	7.436			
T3 210.00-190.00	0.53	1.85	A	0.262	2.401	0.605	0.85	1	16.057	2.44	122.00	B
			B	0.365	2.137	0.638	0.85	1	23.384			
			C	0.16	2.736	0.583	0.85	1	9.234			
T4 190.00-180.00	0.27	1.24	A	0.331	2.217	0.626	0.85	1	14.602	1.62	162.08	B
			B	0.408	2.049	0.655	0.85	1	18.463			
			C	0.255	2.424	0.603	0.85	1	11.223			
T5 180.00-160.00	0.53	2.33	A	0.27	2.38	0.607	0.85	1	28.642	3.27	163.74	B
			B	0.332	2.213	0.626	0.85	1	35.714			
			C	0.206	2.577	0.592	0.85	1	22.027			
T6 160.00-140.00	0.70	2.79	A	0.231	2.496	0.597	0.85	1	30.466	3.42	170.90	B
			B	0.281	2.347	0.61	0.85	1	37.178			
			C	0.202	2.591	0.591	0.85	1	27.961			
T7 140.00-120.00	0.72	2.96	A	0.22	2.53	0.595	0.85	1	35.165	3.57	178.49	B
			B	0.249	2.441	0.602	0.85	1	39.686			
			C	0.183	2.654	0.587	0.85	1	30.859			
T8 120.00-110.00	0.37	1.79	A	0.219	2.535	0.594	0.85	1	19.562	1.83	182.86	B
			B	0.234	2.488	0.598	0.85	1	20.920			
			C	0.175	2.683	0.586	0.85	1	16.537			
T9 110.00-100.00	0.38	2.07	A	0.241	2.465	0.6	0.85	1	23.888	1.98	197.52	A
			B	0.24	2.468	0.599	0.85	1	23.744			
			C	0.186	2.642	0.588	0.85	1	19.523			
T10 100.00-80.00	0.77	4.21	A	0.21	2.563	0.592	0.85	1	45.018	3.72	185.81	A
			B	0.204	2.582	0.591	0.85	1	43.376			
			C	0.154	2.756	0.582	0.85	1	34.779			
T11 80.00-60.00	0.77	4.87	A	0.196	2.61	0.59	0.85	1	47.349	3.66	183.24	A
			B	0.191	2.627	0.589	0.85	1	45.692			



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T12	0.79	5.29	C	0.146	2.786	0.581	0.85	1	37.152			
60.00-40.00			A	0.195	2.612	0.589	0.85	1	52.980	3.67	183.47	A
			B	0.184	2.649	0.587	0.85	1	49.872			
			C	0.144	2.792	0.581	0.85	1	41.503			
T13	0.79	5.30	A	0.192	2.623	0.589	0.85	1	58.114	3.54	177.23	A
40.00-20.00			B	0.18	2.663	0.587	0.85	1	54.620			
			C	0.144	2.792	0.581	0.85	1	46.404			
T14	0.79	7.81	A	0.17	2.699	0.585	0.85	1	54.248	3.42	171.08	A
20.00-0.00			B	0.159	2.74	0.583	0.85	1	50.278			
			C	0.125	2.865	0.578	0.85	1	41.608			
Sum Weight:	8.21	44.43						OTM	4510.27 kip-ft	39.92		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.59	0.80	A	0.429	2.009	0.664	1	1	18.573	1.48	98.52	A
245.00-230.00			B	0.359	2.15	0.636	1	1	14.634			
			C	0.243	2.46	0.6	1	1	9.187			
T2	1.24	1.62	A	0.429	2.01	0.664	1	1	26.418	2.51	125.27	B
230.00-210.00			B	0.582	1.816	0.743	1	1	39.512			
			C	0.256	2.419	0.603	1	1	13.914			
T3	1.24	2.21	A	0.417	2.032	0.659	1	1	28.481	2.54	127.02	B
210.00-190.00			B	0.553	1.84	0.726	1	1	41.175			
			C	0.265	2.395	0.606	1	1	16.157			
T4	0.62	1.73	A	0.528	1.866	0.712	1	1	26.357	1.80	179.62	B
190.00-180.00			B	0.631	1.788	0.773	1	1	33.587			
			C	0.402	2.06	0.652	1	1	19.062			
T5	1.24	4.01	A	0.431	2.007	0.665	1	1	49.803	3.42	171.16	B
180.00-160.00			B	0.514	1.882	0.705	1	1	61.992			
			C	0.323	2.237	0.623	1	1	36.332			
T6	1.46	4.54	A	0.366	2.134	0.638	1	1	51.491	3.50	174.82	B
160.00-140.00			B	0.433	2.002	0.666	1	1	62.397			
			C	0.304	2.284	0.617	1	1	44.436			
T7	1.52	4.82	A	0.348	2.176	0.632	1	1	58.542	3.60	179.98	B
140.00-120.00			B	0.379	2.108	0.643	1	1	64.372			
			C	0.271	2.376	0.607	1	1	47.821			
T8	0.79	2.78	A	0.348	2.176	0.632	1	1	32.784	1.84	184.09	B
120.00-110.00			B	0.354	2.163	0.634	1	1	33.554			
			C	0.258	2.414	0.604	1	1	25.447			
T9	0.83	3.18	A	0.378	2.11	0.643	1	1	39.528	2.02	202.40	A
110.00-100.00			B	0.358	2.153	0.635	1	1	37.401			
			C	0.272	2.375	0.608	1	1	29.698			
T10	1.67	6.26	A	0.334	2.209	0.627	1	1	75.274	3.86	193.14	A
100.00-80.00			B	0.309	2.273	0.619	1	1	68.548			
			C	0.227	2.509	0.596	1	1	53.056			
T11	1.67	7.02	A	0.31	2.27	0.619	1	1	78.181	3.81	190.31	A
80.00-60.00			B	0.287	2.331	0.612	1	1	71.535			
			C	0.214	2.549	0.593	1	1	56.316			
T12	1.72	7.60	A	0.304	2.284	0.617	1	1	85.933	3.78	189.07	A
60.00-40.00			B	0.272	2.372	0.608	1	1	76.431			
			C	0.207	2.572	0.592	1	1	61.702			
T13	1.73	7.78	A	0.294	2.312	0.614	1	1	92.212	3.62	180.83	A



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
40.00-20.00			B	0.262	2.403	0.605	1	1	82.075			
			C	0.203	2.587	0.591	1	1	67.763			
T14	1.73	10.87	A	0.261	2.405	0.605	1	1	86.320	3.53	176.51	A
20.00-0.00			B	0.229	2.501	0.597	1	1	75.035			
			C	0.174	2.685	0.585	1	1	59.884			
Sum Weight:	18.05	65.24						OTM	4688.04 kip-ft	41.30		

### Tower Forces - With Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.59	0.80	A	0.429	2.009	0.664	0.825	1	18.263	1.46	97.40	A
245.00-230.00			B	0.359	2.15	0.636	0.825	1	14.531			
			C	0.243	2.46	0.6	0.825	1	9.187			
T2	1.24	1.62	A	0.429	2.01	0.664	0.825	1	26.005	2.49	124.28	B
230.00-210.00			B	0.582	1.816	0.743	0.825	1	39.099			
			C	0.256	2.419	0.603	0.825	1	13.914			
T3	1.24	2.21	A	0.417	2.032	0.659	0.825	1	28.068	2.52	126.05	B
210.00-190.00			B	0.553	1.84	0.726	0.825	1	40.762			
			C	0.265	2.395	0.606	0.825	1	16.157			
T4	0.62	1.73	A	0.528	1.866	0.712	0.825	1	25.688	1.77	176.59	B
190.00-180.00			B	0.631	1.788	0.773	0.825	1	32.908			
			C	0.402	2.06	0.652	0.825	1	18.321			
T5	1.24	4.01	A	0.431	2.007	0.665	0.825	1	48.334	3.35	167.75	B
180.00-160.00			B	0.514	1.882	0.705	0.825	1	60.506			
			C	0.323	2.237	0.623	0.825	1	34.805			
T6	1.46	4.54	A	0.366	2.134	0.638	0.825	1	49.736	3.41	170.65	B
160.00-140.00			B	0.433	2.002	0.666	0.825	1	60.628			
			C	0.304	2.284	0.617	0.825	1	41.694			
T7	1.52	4.82	A	0.348	2.176	0.632	0.825	1	56.280	3.49	174.37	B
140.00-120.00			B	0.379	2.108	0.643	0.825	1	62.014			
			C	0.271	2.376	0.607	0.825	1	44.464			
T8	0.79	2.78	A	0.348	2.176	0.632	0.825	1	31.570	1.78	177.97	B
120.00-110.00			B	0.354	2.163	0.634	0.825	1	32.258			
			C	0.258	2.414	0.604	0.825	1	23.660			
T9	0.83	3.18	A	0.378	2.11	0.643	0.825	1	37.703	1.94	194.21	A
110.00-100.00			B	0.358	2.153	0.635	0.825	1	35.559			
			C	0.272	2.375	0.608	0.825	1	27.307			
T10	1.67	6.26	A	0.334	2.209	0.627	0.825	1	71.908	3.71	185.58	A
100.00-80.00			B	0.309	2.273	0.619	0.825	1	65.564			
			C	0.227	2.509	0.596	0.825	1	49.111			
T11	1.67	7.02	A	0.31	2.27	0.619	0.825	1	74.488	3.65	182.38	A
80.00-60.00			B	0.287	2.331	0.612	0.825	1	68.234			
			C	0.214	2.549	0.593	0.825	1	52.065			
T12	1.72	7.60	A	0.304	2.284	0.617	0.825	1	81.482	3.61	180.33	A
60.00-40.00			B	0.272	2.372	0.608	0.825	1	72.274			
			C	0.207	2.572	0.592	0.825	1	56.556			
T13	1.73	7.78	A	0.294	2.312	0.614	0.825	1	86.860	3.43	171.38	A
40.00-20.00			B	0.262	2.403	0.605	0.825	1	76.952			
			C	0.203	2.587	0.591	0.825	1	61.610			
T14	1.73	10.87	A	0.261	2.405	0.605	0.825	1	82.773	3.40	170.00	A
20.00-0.00			B	0.229	2.501	0.597	0.825	1	71.919			
			C	0.174	2.685	0.585	0.825	1	55.917			



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Modification Structural Analysis - Tower	<b>Page</b>	23 of 46
	<b>Project</b>	Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b>	15:37:53 04/01/15
	<b>Client</b>	Northeast Site Solutions / T-Mobile	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
Sum Weight:	18.05	65.24						OTM	4575.50 kip-ft	40.00		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.59	0.80	A	0.429	2.009	0.664	0.8	1	18.219	1.46	97.24	A
			B	0.359	2.15	0.636	0.8	1	14.516			
			C	0.243	2.46	0.6	0.8	1	9.187			
T2 230.00-210.00	1.24	1.62	A	0.429	2.01	0.664	0.8	1	25.946	2.48	124.14	B
			B	0.582	1.816	0.743	0.8	1	39.039			
			C	0.256	2.419	0.603	0.8	1	13.914			
T3 210.00-190.00	1.24	2.21	A	0.417	2.032	0.659	0.8	1	28.009	2.52	125.91	B
			B	0.553	1.84	0.726	0.8	1	40.703			
			C	0.265	2.395	0.606	0.8	1	16.157			
T4 190.00-180.00	0.62	1.73	A	0.528	1.866	0.712	0.8	1	25.593	1.76	176.15	B
			B	0.631	1.788	0.773	0.8	1	32.811			
			C	0.402	2.06	0.652	0.8	1	18.215			
T5 180.00-160.00	1.24	4.01	A	0.431	2.007	0.665	0.8	1	48.124	3.35	167.26	B
			B	0.514	1.882	0.705	0.8	1	60.294			
			C	0.323	2.237	0.623	0.8	1	34.587			
T6 160.00-140.00	1.46	4.54	A	0.366	2.134	0.638	0.8	1	49.485	3.40	170.05	B
			B	0.433	2.002	0.666	0.8	1	60.375			
			C	0.304	2.284	0.617	0.8	1	41.303			
T7 140.00-120.00	1.52	4.82	A	0.348	2.176	0.632	0.8	1	55.957	3.47	173.57	B
			B	0.379	2.108	0.643	0.8	1	61.677			
			C	0.271	2.376	0.607	0.8	1	43.985			
T8 120.00-110.00	0.79	2.78	A	0.348	2.176	0.632	0.8	1	31.396	1.77	177.10	B
			B	0.354	2.163	0.634	0.8	1	32.073			
			C	0.258	2.414	0.604	0.8	1	23.405			
T9 110.00-100.00	0.83	3.18	A	0.378	2.11	0.643	0.8	1	37.442	1.93	193.04	A
			B	0.358	2.153	0.635	0.8	1	35.295			
			C	0.272	2.375	0.608	0.8	1	26.965			
T10 100.00-80.00	1.67	6.26	A	0.334	2.209	0.627	0.8	1	71.427	3.69	184.50	A
			B	0.309	2.273	0.619	0.8	1	65.138			
			C	0.227	2.509	0.596	0.8	1	48.548			
T11 80.00-60.00	1.67	7.02	A	0.31	2.27	0.619	0.8	1	73.961	3.63	181.25	A
			B	0.287	2.331	0.612	0.8	1	67.762			
			C	0.214	2.549	0.593	0.8	1	51.458			
T12 60.00-40.00	1.72	7.60	A	0.304	2.284	0.617	0.8	1	80.847	3.58	179.09	A
			B	0.272	2.372	0.608	0.8	1	71.680			
			C	0.207	2.572	0.592	0.8	1	55.821			
T13 40.00-20.00	1.73	7.78	A	0.294	2.312	0.614	0.8	1	86.096	3.40	170.03	A
			B	0.262	2.403	0.605	0.8	1	76.220			
			C	0.203	2.587	0.591	0.8	1	60.731			
T14 20.00-0.00	1.73	10.87	A	0.261	2.405	0.605	0.8	1	82.266	3.38	169.07	A
			B	0.229	2.501	0.597	0.8	1	71.474			
			C	0.174	2.685	0.585	0.8	1	55.350			
Sum Weight:	18.05	65.24						OTM	4559.42 kip-ft	39.82		



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.59	0.80	A	0.429	2.009	0.664	0.85	1	18.307	1.46	97.56	A
245.00-230.00			B	0.359	2.15	0.636	0.85	1	14.545			
			C	0.243	2.46	0.6	0.85	1	9.187			
T2	1.24	1.62	A	0.429	2.01	0.664	0.85	1	26.064	2.49	124.42	B
230.00-210.00			B	0.582	1.816	0.743	0.85	1	39.158			
			C	0.256	2.419	0.603	0.85	1	13.914			
T3	1.24	2.21	A	0.417	2.032	0.659	0.85	1	28.127	2.52	126.19	B
210.00-190.00			B	0.553	1.84	0.726	0.85	1	40.821			
			C	0.265	2.395	0.606	0.85	1	16.157			
T4	0.62	1.73	A	0.528	1.866	0.712	0.85	1	25.784	1.77	177.02	B
190.00-180.00			B	0.631	1.788	0.773	0.85	1	33.005			
			C	0.402	2.06	0.652	0.85	1	18.427			
T5	1.24	4.01	A	0.431	2.007	0.665	0.85	1	48.543	3.36	168.23	B
180.00-160.00			B	0.514	1.882	0.705	0.85	1	60.718			
			C	0.323	2.237	0.623	0.85	1	35.023			
T6	1.46	4.54	A	0.366	2.134	0.638	0.85	1	49.986	3.42	171.24	B
160.00-140.00			B	0.433	2.002	0.666	0.85	1	60.880			
			C	0.304	2.284	0.617	0.85	1	42.086			
T7	1.52	4.82	A	0.348	2.176	0.632	0.85	1	56.603	3.50	175.17	B
140.00-120.00			B	0.379	2.108	0.643	0.85	1	62.351			
			C	0.271	2.376	0.607	0.85	1	44.944			
T8	0.79	2.78	A	0.348	2.176	0.632	0.85	1	31.743	1.79	178.84	B
120.00-110.00			B	0.354	2.163	0.634	0.85	1	32.443			
			C	0.258	2.414	0.604	0.85	1	23.916			
T9	0.83	3.18	A	0.378	2.11	0.643	0.85	1	37.964	1.95	195.38	A
110.00-100.00			B	0.358	2.153	0.635	0.85	1	35.822			
			C	0.272	2.375	0.608	0.85	1	27.648			
T10	1.67	6.26	A	0.334	2.209	0.627	0.85	1	72.389	3.73	186.66	A
100.00-80.00			B	0.309	2.273	0.619	0.85	1	65.990			
			C	0.227	2.509	0.596	0.85	1	49.675			
T11	1.67	7.02	A	0.31	2.27	0.619	0.85	1	75.016	3.67	183.52	A
80.00-60.00			B	0.287	2.331	0.612	0.85	1	68.706			
			C	0.214	2.549	0.593	0.85	1	52.672			
T12	1.72	7.60	A	0.304	2.284	0.617	0.85	1	82.118	3.63	181.58	A
60.00-40.00			B	0.272	2.372	0.608	0.85	1	72.868			
			C	0.207	2.572	0.592	0.85	1	57.291			
T13	1.73	7.78	A	0.294	2.312	0.614	0.85	1	87.625	3.45	172.73	A
40.00-20.00			B	0.262	2.403	0.605	0.85	1	77.684			
			C	0.203	2.587	0.591	0.85	1	62.489			
T14	1.73	10.87	A	0.261	2.405	0.605	0.85	1	83.280	3.42	170.93	A
20.00-0.00			B	0.229	2.501	0.597	0.85	1	72.365			
			C	0.174	2.685	0.585	0.85	1	56.483			
Sum Weight:	18.05	65.24						OTM	4591.57 kip-ft	40.19		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	<b>Page</b>
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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.26	0.60	A	0.252	2.433	0.602	1	1	9.750	0.49	32.99	A
			B	0.208	2.57	0.592	1	1	7.742			
			C	0.124	2.869	0.578	1	1	4.438			
T2 230.00-210.00	0.53	1.31	A	0.262	2.401	0.605	1	1	14.506	0.82	41.09	B
			B	0.378	2.11	0.643	1	1	21.893			
			C	0.145	2.79	0.581	1	1	7.436			
T3 210.00-190.00	0.53	1.85	A	0.262	2.401	0.605	1	1	16.244	0.85	42.45	B
			B	0.365	2.137	0.638	1	1	23.572			
			C	0.16	2.736	0.583	1	1	9.234			
T4 190.00-180.00	0.27	1.24	A	0.331	2.217	0.626	1	1	15.189	0.57	57.47	B
			B	0.408	2.049	0.655	1	1	19.048			
			C	0.255	2.424	0.603	1	1	11.858			
T5 180.00-160.00	0.53	2.33	A	0.27	2.38	0.607	1	1	29.899	1.16	58.22	B
			B	0.332	2.213	0.626	1	1	36.967			
			C	0.206	2.577	0.592	1	1	23.336			
T6 160.00-140.00	0.70	2.79	A	0.231	2.496	0.597	1	1	31.944	1.22	61.01	B
			B	0.281	2.347	0.61	1	1	38.653			
			C	0.202	2.591	0.591	1	1	30.159			
T7 140.00-120.00	0.72	2.96	A	0.22	2.53	0.595	1	1	37.123	1.29	64.29	B
			B	0.249	2.441	0.602	1	1	41.676			
			C	0.183	2.654	0.587	1	1	33.587			
T8 120.00-110.00	0.37	1.79	A	0.219	2.535	0.594	1	1	20.624	0.66	66.01	B
			B	0.234	2.488	0.598	1	1	22.012			
			C	0.175	2.683	0.586	1	1	17.993			
T9 110.00-100.00	0.38	2.07	A	0.241	2.465	0.6	1	1	25.497	0.72	72.23	A
			B	0.24	2.468	0.599	1	1	25.327			
			C	0.186	2.642	0.588	1	1	21.500			
T10 100.00-80.00	0.77	4.21	A	0.21	2.563	0.592	1	1	47.810	1.35	67.65	A
			B	0.204	2.582	0.591	1	1	45.887			
			C	0.154	2.756	0.582	1	1	38.009			
T11 80.00-60.00	0.77	4.87	A	0.196	2.61	0.59	1	1	50.413	1.34	66.90	A
			B	0.191	2.627	0.589	1	1	48.471			
			C	0.146	2.786	0.581	1	1	40.643			
T12 60.00-40.00	0.79	5.29	A	0.195	2.612	0.589	1	1	56.750	1.35	67.39	A
			B	0.184	2.649	0.587	1	1	53.400			
			C	0.144	2.792	0.581	1	1	45.764			
T13 40.00-20.00	0.79	5.30	A	0.192	2.623	0.589	1	1	62.700	1.31	65.56	A
			B	0.18	2.663	0.587	1	1	58.992			
			C	0.144	2.792	0.581	1	1	51.529			
T14 20.00-0.00	0.79	7.81	A	0.17	2.699	0.585	1	1	57.129	1.24	61.93	A
			B	0.159	2.74	0.583	1	1	52.859			
			C	0.125	2.865	0.578	1	1	44.852			
Sum Weight:	8.21	44.43						OTM	1608.88 kip-ft	14.38		

### Tower Forces - Service - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.26	0.60	A	0.252	2.433	0.602	0.825	1	9.586	0.49	32.66	A
			B	0.208	2.57	0.592	0.825	1	7.687			
			C	0.124	2.869	0.578	0.825	1	4.438			
T2 230.00-210.00	0.53	1.31	A	0.262	2.401	0.605	0.825	1	14.288	0.82	40.81	B
			B	0.378	2.11	0.643	0.825	1	21.674			



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>		<b>Page</b>
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	<b>Project</b>	Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b>	Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T3	0.53	1.85	A	0.145	2.79	0.581	0.825	1	7.436			
210.00-190.00			A	0.262	2.401	0.605	0.825	1	16.026	0.84	42.18	B
			B	0.365	2.137	0.638	0.825	1	23.353			
			C	0.16	2.736	0.583	0.825	1	9.234			
T4	0.27	1.24	A	0.331	2.217	0.626	0.825	1	14.505	0.56	55.85	B
190.00-180.00			B	0.408	2.049	0.655	0.825	1	18.365			
			C	0.255	2.424	0.603	0.825	1	11.117			
T5	0.53	2.33	A	0.27	2.38	0.607	0.825	1	28.433	1.13	56.40	B
180.00-160.00			B	0.332	2.213	0.626	0.825	1	35.505			
			C	0.206	2.577	0.592	0.825	1	21.809			
T6	0.70	2.79	A	0.231	2.496	0.597	0.825	1	30.219	1.18	58.82	B
160.00-140.00			B	0.281	2.347	0.61	0.825	1	36.933			
			C	0.202	2.591	0.591	0.825	1	27.594			
T7	0.72	2.96	A	0.22	2.53	0.595	0.825	1	34.839	1.23	61.34	B
140.00-120.00			B	0.249	2.441	0.602	0.825	1	39.354			
			C	0.183	2.654	0.587	0.825	1	30.405			
T8	0.37	1.79	A	0.219	2.535	0.594	0.825	1	19.385	0.63	62.82	B
120.00-110.00			B	0.234	2.488	0.598	0.825	1	20.738			
			C	0.175	2.683	0.586	0.825	1	16.295			
T9	0.38	2.07	A	0.241	2.465	0.6	0.825	1	23.620	0.68	67.70	A
110.00-100.00			B	0.24	2.468	0.599	0.825	1	23.480			
			C	0.186	2.642	0.588	0.825	1	19.194			
T10	0.77	4.21	A	0.21	2.563	0.592	0.825	1	44.553	1.27	63.73	A
100.00-80.00			B	0.204	2.582	0.591	0.825	1	42.957			
			C	0.154	2.756	0.582	0.825	1	34.241			
T11	0.77	4.87	A	0.196	2.61	0.59	0.825	1	46.838	1.26	62.82	A
80.00-60.00			B	0.191	2.627	0.589	0.825	1	45.229			
			C	0.146	2.786	0.581	0.825	1	36.570			
T12	0.79	5.29	A	0.195	2.612	0.589	0.825	1	52.351	1.26	62.83	A
60.00-40.00			B	0.184	2.649	0.587	0.825	1	49.284			
			C	0.144	2.792	0.581	0.825	1	40.793			
T13	0.79	5.30	A	0.192	2.623	0.589	0.825	1	57.349	1.21	60.62	A
40.00-20.00			B	0.18	2.663	0.587	0.825	1	53.891			
			C	0.144	2.792	0.581	0.825	1	45.549			
T14	0.79	7.81	A	0.17	2.699	0.585	0.825	1	53.768	1.17	58.74	A
20.00-0.00			B	0.159	2.74	0.583	0.825	1	49.848			
			C	0.125	2.865	0.578	0.825	1	41.067			
Sum Weight:	8.21	44.43						OTM	1552.61 kip-ft	13.72		

### Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.26	0.60	A	0.252	2.433	0.602	0.8	1	9.563	0.49	32.61	A
245.00-230.00			B	0.208	2.57	0.592	0.8	1	7.680			
			C	0.124	2.869	0.578	0.8	1	4.438			
T2	0.53	1.31	A	0.262	2.401	0.605	0.8	1	14.256	0.82	40.77	B
230.00-210.00			B	0.378	2.11	0.643	0.8	1	21.643			
			C	0.145	2.79	0.581	0.8	1	7.436			
T3	0.53	1.85	A	0.262	2.401	0.605	0.8	1	15.994	0.84	42.14	B
210.00-190.00			B	0.365	2.137	0.638	0.8	1	23.322			
			C	0.16	2.736	0.583	0.8	1	9.234			
T4	0.27	1.24	A	0.331	2.217	0.626	0.8	1	14.407	0.56	55.62	B



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	<b>Project</b> Storrs (UCONN), CT (Site: CT11303B) / NSS-022	<b>Date</b> 15:37:53 04/01/15
	<b>Client</b> Northeast Site Solutions / T-Mobile	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
190.00-180.00			B	0.408	2.049	0.655	0.8	1	18.268			
			C	0.255	2.424	0.603	0.8	1	11.011			
T5	0.53	2.33	A	0.27	2.38	0.607	0.8	1	28.224	1.12	56.14	B
180.00-160.00			B	0.332	2.213	0.626	0.8	1	35.296			
			C	0.206	2.577	0.592	0.8	1	21.591			
T6	0.70	2.79	A	0.231	2.496	0.597	0.8	1	29.973	1.17	58.51	B
160.00-140.00			B	0.281	2.347	0.61	0.8	1	36.687			
			C	0.202	2.591	0.591	0.8	1	27.228			
T7	0.72	2.96	A	0.22	2.53	0.595	0.8	1	34.512	1.22	60.92	B
140.00-120.00			B	0.249	2.441	0.602	0.8	1	39.023			
			C	0.183	2.654	0.587	0.8	1	29.950			
T8	0.37	1.79	A	0.219	2.535	0.594	0.8	1	19.208	0.62	62.36	B
120.00-110.00			B	0.234	2.488	0.598	0.8	1	20.556			
			C	0.175	2.683	0.586	0.8	1	16.052			
T9	0.38	2.07	A	0.241	2.465	0.6	0.8	1	23.352	0.67	67.05	A
110.00-100.00			B	0.24	2.468	0.599	0.8	1	23.216			
			C	0.186	2.642	0.588	0.8	1	18.864			
T10	0.77	4.21	A	0.21	2.563	0.592	0.8	1	44.087	1.26	63.17	A
100.00-80.00			B	0.204	2.582	0.591	0.8	1	42.539			
			C	0.154	2.756	0.582	0.8	1	33.703			
T11	0.77	4.87	A	0.196	2.61	0.59	0.8	1	46.328	1.24	62.24	A
80.00-60.00			B	0.191	2.627	0.589	0.8	1	44.766			
			C	0.146	2.786	0.581	0.8	1	35.988			
T12	0.79	5.29	A	0.195	2.612	0.589	0.8	1	51.723	1.24	62.18	A
60.00-40.00			B	0.184	2.649	0.587	0.8	1	48.696			
			C	0.144	2.792	0.581	0.8	1	40.083			
T13	0.79	5.30	A	0.192	2.623	0.589	0.8	1	56.585	1.20	59.91	A
40.00-20.00			B	0.18	2.663	0.587	0.8	1	53.162			
			C	0.144	2.792	0.581	0.8	1	44.695			
T14	0.79	7.81	A	0.17	2.699	0.585	0.8	1	53.288	1.17	58.28	A
20.00-0.00			B	0.159	2.74	0.583	0.8	1	49.417			
			C	0.125	2.865	0.578	0.8	1	40.527			
Sum Weight:	8.21	44.43						OTM	1544.57 kip-ft	13.62		

### Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.26	0.60	A	0.252	2.433	0.602	0.85	1	9.609	0.49	32.71	A
245.00-230.00			B	0.208	2.57	0.592	0.85	1	7.695			
			C	0.124	2.869	0.578	0.85	1	4.438			
T2	0.53	1.31	A	0.262	2.401	0.605	0.85	1	14.319	0.82	40.85	B
230.00-210.00			B	0.378	2.11	0.643	0.85	1	21.705			
			C	0.145	2.79	0.581	0.85	1	7.436			
T3	0.53	1.85	A	0.262	2.401	0.605	0.85	1	16.057	0.84	42.21	B
210.00-190.00			B	0.365	2.137	0.638	0.85	1	23.384			
			C	0.16	2.736	0.583	0.85	1	9.234			
T4	0.27	1.24	A	0.331	2.217	0.626	0.85	1	14.602	0.56	56.08	B
190.00-180.00			B	0.408	2.049	0.655	0.85	1	18.463			
			C	0.255	2.424	0.603	0.85	1	11.223			
T5	0.53	2.33	A	0.27	2.38	0.607	0.85	1	28.642	1.13	56.66	B
180.00-160.00			B	0.332	2.213	0.626	0.85	1	35.714			
			C	0.206	2.577	0.592	0.85	1	22.027			



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	<b>Project</b>	<b>Date</b>
	Storrs (UCONN), CT (Site: CT11303B) / NSS-022	15:37:53 04/01/15
	<b>Client</b>	<b>Designed by</b>
	Northeast Site Solutions / T-Mobile	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T6	0.70	2.79	A	0.231	2.496	0.597	0.85	1	30.466	1.18	59.14	B
160.00-140.00			B	0.281	2.347	0.61	0.85	1	37.178			
			C	0.202	2.591	0.591	0.85	1	27.961			
T7	0.72	2.96	A	0.22	2.53	0.595	0.85	1	35.165	1.24	61.76	B
140.00-120.00			B	0.249	2.441	0.602	0.85	1	39.686			
			C	0.183	2.654	0.587	0.85	1	30.859			
T8	0.37	1.79	A	0.219	2.535	0.594	0.85	1	19.562	0.63	63.27	B
120.00-110.00			B	0.234	2.488	0.598	0.85	1	20.920			
			C	0.175	2.683	0.586	0.85	1	16.537			
T9	0.38	2.07	A	0.241	2.465	0.6	0.85	1	23.888	0.68	68.35	A
110.00-100.00			B	0.24	2.468	0.599	0.85	1	23.744			
			C	0.186	2.642	0.588	0.85	1	19.523			
T10	0.77	4.21	A	0.21	2.563	0.592	0.85	1	45.018	1.29	64.29	A
100.00-80.00			B	0.204	2.582	0.591	0.85	1	43.376			
			C	0.154	2.756	0.582	0.85	1	34.779			
T11	0.77	4.87	A	0.196	2.61	0.59	0.85	1	47.349	1.27	63.41	A
80.00-60.00			B	0.191	2.627	0.589	0.85	1	45.692			
			C	0.146	2.786	0.581	0.85	1	37.152			
T12	0.79	5.29	A	0.195	2.612	0.589	0.85	1	52.980	1.27	63.48	A
60.00-40.00			B	0.184	2.649	0.587	0.85	1	49.872			
			C	0.144	2.792	0.581	0.85	1	41.503			
T13	0.79	5.30	A	0.192	2.623	0.589	0.85	1	58.114	1.23	61.33	A
40.00-20.00			B	0.18	2.663	0.587	0.85	1	54.620			
			C	0.144	2.792	0.581	0.85	1	46.404			
T14	0.79	7.81	A	0.17	2.699	0.585	0.85	1	54.248	1.18	59.20	A
20.00-0.00			B	0.159	2.74	0.583	0.85	1	50.278			
			C	0.125	2.865	0.578	0.85	1	41.608			
Sum Weight:	8.21	44.43						OTM	1560.65 kip-ft	13.81		

## Force Totals

Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Z	Sum of Overturning Moments, M <sub>x</sub>	Sum of Overturning Moments, M <sub>z</sub>	Sum of Torques
	K	K	K	kip-ft	kip-ft	kip-ft
Leg Weight	30.31					
Bracing Weight	14.11					
Total Member Self-Weight	44.43			-11.56	-8.77	
Total Weight	59.10			-11.56	-8.77	
Wind 0 deg - No Ice		0.04	-50.57	-6645.30	-18.15	13.61
Wind 30 deg - No Ice		24.67	-42.55	-5657.16	-3285.49	-8.14
Wind 45 deg - No Ice		34.68	-34.63	-4615.07	-4621.94	-18.08
Wind 60 deg - No Ice		42.25	-24.38	-3259.90	-5638.77	-26.90
Wind 90 deg - No Ice		49.21	-0.07	-24.62	-6539.58	-38.03
Wind 120 deg - No Ice		43.84	25.25	3297.19	-5762.16	-39.75
Wind 135 deg - No Ice		34.38	34.39	4558.85	-4583.34	-34.46
Wind 150 deg - No Ice		24.38	42.38	5611.01	-3246.06	-28.77
Wind 180 deg - No Ice		-0.14	48.58	6457.72	11.78	-11.40
Wind 210 deg - No Ice		-24.77	42.75	5654.70	3278.98	9.47
Wind 225 deg - No Ice		-34.79	34.74	4603.12	4616.58	19.37
Wind 240 deg - No Ice		-44.25	25.53	3336.01	5793.09	28.73
Wind 270 deg - No Ice		-49.43	0.07	0.74	6545.44	38.98
Wind 300 deg - No Ice		-42.18	-24.17	-3228.40	5607.78	38.78
Wind 315 deg - No Ice		-34.56	-34.34	-4576.95	4584.87	35.37
Wind 330 deg - No Ice		-24.54	-42.29	-5624.57	3245.08	29.87



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	Northeast Site Solutions / T-Mobile	MCD

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, $M_x$ kip-ft	Sum of Overturning Moments, $M_z$ kip-ft	Sum of Torques kip-ft
Member Ice	20.81					
Total Weight Ice	92.83			-29.01	-30.34	
Wind 0 deg - Ice		0.06	-49.37	-6466.75	-40.77	14.95
Wind 30 deg - Ice		24.31	-41.96	-5540.78	-3226.05	-6.59
Wind 45 deg - Ice		34.23	-34.20	-4526.36	-4535.26	-16.84
Wind 60 deg - Ice		41.81	-24.13	-3206.57	-5536.81	-26.25
Wind 90 deg - Ice		48.51	-0.06	-39.30	-6403.93	-38.13
Wind 120 deg - Ice		42.81	24.64	3180.83	-5613.58	-40.34
Wind 135 deg - Ice		34.01	33.92	4431.99	-4505.84	-36.05
Wind 150 deg - Ice		24.03	41.76	5456.94	-3189.73	-30.14
Wind 180 deg - Ice		-0.47	48.17	6309.61	24.74	-10.62
Wind 210 deg - Ice		-24.64	42.12	5499.07	3202.07	9.72
Wind 225 deg - Ice		-34.53	34.31	4479.84	4506.54	19.48
Wind 240 deg - Ice		-43.31	24.99	3226.12	5610.50	28.45
Wind 270 deg - Ice		-48.82	0.27	4.90	6375.73	39.43
Wind 300 deg - Ice		-41.97	-23.68	-3150.62	5489.39	41.19
Wind 315 deg - Ice		-34.33	-33.79	-4476.39	4478.84	37.85
Wind 330 deg - Ice		-24.17	-41.68	-5506.71	3143.35	31.09
Total Weight	59.10			-11.56	-8.77	
Wind 0 deg - Service		0.01	-17.50	-2302.34	-2.12	4.71
Wind 30 deg - Service		8.54	-14.72	-1960.42	-1132.69	-2.82
Wind 45 deg - Service		12.00	-11.98	-1599.84	-1595.13	-6.25
Wind 60 deg - Service		14.62	-8.44	-1130.92	-1946.97	-9.31
Wind 90 deg - Service		17.03	-0.03	-11.44	-2258.67	-13.16
Wind 120 deg - Service		15.17	8.74	1137.97	-1989.67	-13.76
Wind 135 deg - Service		11.90	11.90	1574.53	-1581.77	-11.92
Wind 150 deg - Service		8.44	14.67	1938.60	-1119.05	-9.95
Wind 180 deg - Service		-0.05	16.81	2231.58	8.24	-3.94
Wind 210 deg - Service		-8.57	14.79	1953.72	1138.75	3.28
Wind 225 deg - Service		-12.04	12.02	1589.85	1601.59	6.70
Wind 240 deg - Service		-15.31	8.83	1151.40	2008.69	9.94
Wind 270 deg - Service		-17.10	0.02	-2.67	2269.02	13.49
Wind 300 deg - Service		-14.59	-8.36	-1120.02	1944.57	13.42
Wind 315 deg - Service		-11.96	-11.88	-1586.65	1590.62	12.24
Wind 330 deg - Service		-8.49	-14.63	-1949.14	1127.03	10.33

## Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 45 deg - No Ice
5	Dead+Wind 60 deg - No Ice
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice
8	Dead+Wind 135 deg - No Ice
9	Dead+Wind 150 deg - No Ice
10	Dead+Wind 180 deg - No Ice
11	Dead+Wind 210 deg - No Ice
12	Dead+Wind 225 deg - No Ice
13	Dead+Wind 240 deg - No Ice
14	Dead+Wind 270 deg - No Ice
15	Dead+Wind 300 deg - No Ice
16	Dead+Wind 315 deg - No Ice



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Comb. No.	Description
17	Dead+Wind 330 deg - No Ice
18	Dead+Ice+Temp
19	Dead+Wind 0 deg+Ice+Temp
20	Dead+Wind 30 deg+Ice+Temp
21	Dead+Wind 45 deg+Ice+Temp
22	Dead+Wind 60 deg+Ice+Temp
23	Dead+Wind 90 deg+Ice+Temp
24	Dead+Wind 120 deg+Ice+Temp
25	Dead+Wind 135 deg+Ice+Temp
26	Dead+Wind 150 deg+Ice+Temp
27	Dead+Wind 180 deg+Ice+Temp
28	Dead+Wind 210 deg+Ice+Temp
29	Dead+Wind 225 deg+Ice+Temp
30	Dead+Wind 240 deg+Ice+Temp
31	Dead+Wind 270 deg+Ice+Temp
32	Dead+Wind 300 deg+Ice+Temp
33	Dead+Wind 315 deg+Ice+Temp
34	Dead+Wind 330 deg+Ice+Temp
35	Dead+Wind 0 deg - Service
36	Dead+Wind 30 deg - Service
37	Dead+Wind 45 deg - Service
38	Dead+Wind 60 deg - Service
39	Dead+Wind 90 deg - Service
40	Dead+Wind 120 deg - Service
41	Dead+Wind 135 deg - Service
42	Dead+Wind 150 deg - Service
43	Dead+Wind 180 deg - Service
44	Dead+Wind 210 deg - Service
45	Dead+Wind 225 deg - Service
46	Dead+Wind 240 deg - Service
47	Dead+Wind 270 deg - Service
48	Dead+Wind 300 deg - Service
49	Dead+Wind 315 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	245 - 230	Leg	Max Tension	5	26.12	0.80	-0.48
			Max. Compression	13	-30.08	0.66	-0.40
			Max. Mx	14	-26.27	-0.92	0.06
			Max. My	2	-29.74	0.02	-0.95
			Max. Vy	14	-3.27	0.71	-0.11
		Diagonal	Max. Vx	2	-3.44	-0.01	0.77
			Max Tension	3	4.20	0.00	0.00
			Max. Compression	11	-4.20	0.00	0.00
			Max. Mx	30	0.08	-0.00	-0.00
			Max. My	4	-1.85	-0.00	-0.00
		Top Girt	Max. Vy	29	-0.00	-0.00	0.00
			Max. Vx	4	-0.00	0.00	0.00
			Max Tension	13	1.18	0.00	0.00
			Max. Compression	5	-1.27	0.00	0.00
			Max. Mx	18	-0.00	0.01	0.00
		Bottom Girt	Max. My	24	-0.47	0.00	0.00
			Max. Vy	18	0.01	0.00	0.00
			Max. Vx	24	0.00	0.00	0.00
			Max Tension	5	1.53	0.00	0.00



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T2	230 - 210	Leg	Max. Compression	13	-1.71	0.00	0.00
			Max. Mx	18	0.00	0.01	0.00
			Max. My	32	-0.57	0.00	-0.00
			Max. Vy	18	0.01	0.00	0.00
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	76.18	1.33	-0.03
			Max. Compression	13	-81.26	0.52	-0.01
			Max. Mx	13	-30.14	2.25	-0.06
			Max. My	6	-2.30	0.00	2.00
			Max. Vy	13	-3.82	0.52	-0.01
		Diagonal	Max. Vx	6	-3.05	0.00	0.34
			Max Tension	11	4.65	0.00	0.00
			Max. Compression	3	-4.78	0.00	0.00
			Max. Mx	12	0.89	-0.01	0.00
			Max. My	11	-4.77	0.00	0.00
		Top Girt	Max. Vy	29	-0.01	-0.01	0.00
			Max. Vx	11	-0.00	0.00	0.00
			Max Tension	13	2.31	0.00	0.00
			Max. Compression	5	-2.20	0.00	0.00
			Max. Mx	18	-0.00	0.01	0.00
		Bottom Girt	Max. My	25	-0.72	0.00	0.00
			Max. Vy	18	-0.01	0.00	0.00
			Max. Vx	25	-0.00	0.00	0.00
			Max Tension	5	2.06	0.00	0.00
			Max. Compression	13	-2.21	0.00	0.00
T3	210 - 190	Leg	Max. Mx	18	0.03	0.01	0.00
			Max. My	32	-0.78	0.00	-0.00
			Max. Vy	18	-0.01	0.00	0.00
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	125.59	0.25	-0.00
			Max. Compression	13	-132.26	2.99	-0.05
			Max. Mx	13	-81.27	3.02	-0.06
			Max. My	6	-3.11	-0.01	2.37
			Max. Vy	13	-4.91	2.99	-0.05
			Max. Vx	6	-3.05	-0.01	2.37
		Diagonal	Max Tension	17	5.24	0.00	0.00
			Max. Compression	17	-5.49	0.00	0.00
			Max. Mx	12	1.47	-0.01	0.00
			Max. My	9	-5.46	0.00	-0.00
			Max. Vy	29	-0.01	-0.01	0.00
		Top Girt	Max. Vx	9	0.00	0.00	-0.00
			Max Tension	13	1.87	0.00	0.00
			Max. Compression	5	-1.73	0.00	0.00
			Max. Mx	18	0.02	0.01	0.00
			Max. My	25	-0.68	0.00	0.00
		Bottom Girt	Max. Vy	18	-0.01	0.00	0.00
			Max. Vx	25	-0.00	0.00	0.00
			Max Tension	5	1.43	0.00	0.00
			Max. Compression	13	-1.36	0.00	0.00
			Max. Mx	18	0.04	0.01	0.00
T4	190 - 180	Leg	Max. My	32	-0.68	0.00	-0.00
			Max. Vy	18	0.01	0.00	0.00
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	124.40	-2.81	0.04
			Max. Compression	13	-130.50	5.89	-0.01
			Max. Mx	5	124.15	-6.22	0.01
			Max. My	6	-4.31	-0.14	10.24
			Max. Vy	32	0.49	-5.87	-0.03
			Max. Vx	6	-1.00	-0.14	10.24
		Diagonal	Max Tension	7	4.43	0.00	0.00
			Max. Compression	6	-4.65	0.00	0.00



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T5	180 - 160	Leg	Max. Mx	5	2.70	0.09	-0.01
			Max. My	34	-2.37	-0.06	-0.03
			Max. Vy	22	0.02	0.09	-0.01
			Max. Vx	26	-0.01	0.00	0.00
			Max Tension	5	142.02	-6.06	0.00
			Max. Compression	13	-150.58	5.55	-0.01
		Diagonal	Max. Mx	5	134.45	-6.22	0.01
			Max. My	6	-4.95	-0.14	10.24
			Max. Vy	32	-0.19	-5.65	-0.03
			Max. Vx	6	0.60	-0.14	10.24
			Max Tension	25	3.62	0.00	0.00
			Max. Compression	33	-4.03	0.00	0.00
			Max. Mx	24	2.71	0.09	0.01
			Max. My	33	2.15	0.07	-0.01
T6	160 - 140	Leg	Max. Vy	24	-0.03	0.09	0.01
			Max. Vx	26	-0.00	0.00	0.00
			Max Tension	5	158.34	-5.28	-0.00
			Max. Compression	13	-169.98	5.25	-0.04
			Max. Mx	5	150.44	-5.61	0.00
			Max. My	6	-6.63	-0.01	5.30
		Diagonal	Max. Vy	32	-0.19	-5.30	-0.03
			Max. Vx	31	0.20	-0.04	-5.07
			Max Tension	34	3.92	0.00	0.00
			Max. Compression	34	-4.26	0.00	0.00
			Max. Mx	24	2.51	0.06	0.00
			Max. My	25	0.57	0.05	0.01
			Max. Vy	22	0.02	0.06	0.00
			Max. Vx	25	0.00	0.00	0.00
T7	140 - 120	Leg	Max Tension	5	175.74	-4.88	0.09
			Max. Compression	13	-190.90	4.54	-0.07
			Max. Mx	5	166.88	-5.27	0.03
			Max. My	6	-8.13	-0.03	5.41
			Max. Vy	27	-0.26	-5.09	0.04
			Max. Vx	14	0.36	-0.05	-5.40
		Diagonal	Max Tension	34	4.72	0.00	0.00
			Max. Compression	34	-5.03	0.00	0.00
			Max. Mx	24	3.12	0.09	0.01
			Max. My	24	-0.25	0.06	0.01
			Max. Vy	22	0.03	0.09	0.01
			Max. Vx	24	0.00	0.00	0.00
T8	120 - 110	Leg	Max Tension	5	185.13	-4.56	0.08
			Max. Compression	13	-201.93	3.08	0.02
			Max. Mx	5	185.13	-4.56	0.08
			Max. My	6	-8.33	-0.03	5.41
			Max. Vy	7	0.28	4.55	0.06
			Max. Vx	31	-0.26	-0.08	-5.23
		Diagonal	Max Tension	33	5.30	0.00	0.00
			Max. Compression	26	-5.50	0.00	0.00
			Max. Mx	24	3.37	0.08	0.01
			Max. My	25	0.97	0.06	0.01
			Max. Vy	21	0.03	0.08	-0.01
			Max. Vx	25	-0.00	0.00	0.00
T9	110 - 100	Leg	Max Tension	5	194.05	-3.37	-0.03
			Max. Compression	13	-212.67	4.14	-0.28
			Max. Mx	19	-210.61	8.65	0.08
			Max. My	14	-8.97	-0.14	-6.56
			Max. Vy	19	-1.27	8.65	0.08
			Max. Vx	14	1.52	-0.14	-6.56
		Diagonal	Max Tension	33	5.70	0.00	0.00
			Max. Compression	30	-6.17	0.00	0.00
			Max. Mx	22	4.36	0.08	0.01



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T10	100 - 80	Secondary Horizontal	Max. My	32	-4.52	0.03	-0.01
			Max. Vy	22	0.03	0.08	0.01
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	13	3.69	0.00	0.00
			Max. Compression	13	-3.69	0.00	0.00
			Max. Mx	30	-1.96	-0.21	0.00
		Leg	Max. My	31	3.16	0.00	0.01
			Max. Vy	30	0.06	0.00	0.00
			Max. Vx	31	-0.00	0.00	0.00
			Max Tension	5	214.61	-3.99	-0.02
			Max. Compression	13	-237.95	4.59	-0.01
			Max. Mx	13	-237.95	4.59	-0.01
		Diagonal	Max. My	14	-9.34	-0.14	-6.56
			Max. Vy	13	-0.20	4.59	-0.01
			Max. Vx	6	0.35	-0.08	5.38
			Max Tension	34	6.39	0.00	0.00
			Max. Compression	34	-6.61	0.00	0.00
			Max. Mx	19	4.80	0.13	-0.01
T11	80 - 60	Leg	Max. My	32	-5.59	0.05	-0.02
			Max. Vy	22	0.05	0.13	0.01
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	234.10	-4.11	-0.00
			Max. Compression	13	-262.35	4.61	-0.05
			Max. Mx	13	-262.35	4.61	-0.05
		Diagonal	Max. My	14	-12.44	-0.04	-4.27
			Max. Vy	27	0.20	-4.37	0.01
			Max. Vx	31	0.22	-0.03	-3.98
			Max Tension	33	6.88	0.00	0.00
			Max. Compression	34	-7.06	0.00	0.00
			Max. Mx	22	4.81	0.14	0.01
		Leg	Max. My	32	-6.20	0.08	-0.02
			Max. Vy	22	0.05	0.14	0.01
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	253.52	-3.83	-0.01
			Max. Compression	19	-287.50	5.30	0.05
			Max. Mx	30	-287.29	5.31	0.03
T12	60 - 40	Leg	Max. My	3	-15.30	-0.51	-5.47
			Max. Vy	27	-0.52	-4.48	-0.01
			Max. Vx	6	-0.27	-0.51	5.43
			Max Tension	17	7.56	0.00	0.00
			Max. Compression	34	-8.04	0.00	0.00
			Max. Mx	22	4.86	0.19	0.02
		Diagonal	Max. My	32	-6.75	0.10	-0.03
			Max. Vy	22	0.07	0.19	0.02
			Max. Vx	32	0.00	0.00	0.00
			Max Tension	5	273.96	-4.62	-0.05
			Max. Compression	13	-313.54	5.62	-0.42
			Max. Mx	30	-312.73	13.29	-0.41
		Leg	Max. My	14	-16.98	-1.21	-19.78
			Max. Vy	30	-1.36	13.29	-0.41
			Max. Vx	14	2.50	-1.21	-19.78
			Max Tension	33	9.28	0.00	0.00
			Max. Compression	32	-10.27	0.00	0.00
			Max. Mx	20	-2.51	0.29	0.04
T13	40 - 20	Leg	Max. My	32	-10.22	0.19	-0.07
			Max. Vy	20	0.08	0.29	0.04
			Max. Vx	32	0.01	0.00	0.00
			Max Tension	5	282.60	-7.62	0.40
			Max. Compression	19	-331.38	0.00	0.00
			Max. Mx	30	-329.22	13.29	-0.41
		Diagonal	Max. My	32	-10.22	0.19	-0.07
			Max. Vy	20	0.08	0.29	0.04
			Max. Vx	32	0.01	0.00	0.00
			Max Tension	5	282.60	-7.62	0.40
T14	20 - 0	Leg	Max. Compression	19	-331.38	0.00	0.00
			Max. Mx	30	-329.22	13.29	-0.41



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
		Diagonal	Max. My	14	-16.47	-1.21	-19.78
			Max. Vy	30	0.87	13.29	-0.41
			Max. Vx	14	-1.32	-1.21	-19.78
			Max Tension	32	17.32	0.00	0.00
			Max. Compression	7	-15.95	0.00	0.00
			Max. Mx	21	15.07	-0.52	0.09
			Max. My	24	6.35	-0.50	-0.11
			Max. Vy	21	-0.16	-0.52	0.09
			Max. Vx	24	0.01	0.00	0.00

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	30	345.29	28.15	-17.06
	Max. H <sub>x</sub>	13	343.35	32.75	-19.71
	Max. H <sub>z</sub>	22	-279.85	-31.16	18.71
	Min. Vert	5	-295.66	-27.56	16.65
	Min. H <sub>x</sub>	22	-279.85	-31.16	18.71
Leg B	Min. H <sub>z</sub>	13	343.35	32.75	-19.71
	Max. Vert	24	344.33	-27.69	-17.19
	Max. H <sub>x</sub>	32	-276.50	30.87	18.92
	Max. H <sub>z</sub>	32	-276.50	30.87	18.92
	Min. Vert	15	-293.60	27.28	16.82
Leg A	Min. H <sub>x</sub>	7	341.12	-32.33	-19.80
	Min. H <sub>z</sub>	7	341.12	-32.33	-19.80
	Max. Vert	19	345.04	0.42	32.59
	Max. H <sub>x</sub>	5	177.54	1.06	19.54
	Max. H <sub>z</sub>	2	341.43	0.35	37.90
	Min. Vert	10	-292.97	-0.27	-32.01
	Min. H <sub>x</sub>	14	19.67	-0.98	2.25
	Min. H <sub>z</sub>	27	-275.55	-0.22	-36.15

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	59.10	-0.00	0.00	-11.56	-8.77	-0.00
Dead+Wind 0 deg - No Ice	59.10	0.04	-50.56	-6687.11	-18.34	13.68
Dead+Wind 30 deg - No Ice	59.10	24.67	-42.55	-5693.04	-3306.32	-8.07
Dead+Wind 45 deg - No Ice	59.10	34.67	-34.63	-4644.37	-4651.25	-18.04
Dead+Wind 60 deg - No Ice	59.10	42.25	-24.38	-3280.65	-5674.58	-26.92
Dead+Wind 90 deg - No Ice	59.10	49.20	-0.07	-24.84	-6581.05	-38.13
Dead+Wind 120 deg - No Ice	59.10	43.84	25.25	3317.85	-5798.49	-39.85
Dead+Wind 135 deg - No Ice	59.10	34.38	34.39	4587.75	-4612.58	-34.54
Dead+Wind 150 deg - No Ice	59.10	24.38	42.38	5646.59	-3266.78	-28.82
Dead+Wind 180 deg - No Ice	59.10	-0.14	48.58	6498.78	11.81	-11.47
Dead+Wind 210 deg - No Ice	59.10	-24.77	42.74	5690.50	3299.79	9.40
Dead+Wind 225 deg - No Ice	59.10	-34.79	34.73	4632.27	4645.92	19.36
Dead+Wind 240 deg - No Ice	59.10	-44.25	25.53	3356.91	5829.50	28.74
Dead+Wind 270 deg - No Ice	59.10	-49.43	0.07	0.70	6586.87	39.07



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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead+Wind 300 deg - No Ice	59.10	-42.17	-24.16	-3248.99	5643.35	38.87
Dead+Wind 315 deg - No Ice	59.10	-34.56	-34.34	-4606.10	4613.89	35.44
Dead+Wind 330 deg - No Ice	59.10	-24.54	-42.29	-5660.32	3265.56	29.92
Dead+Ice+Temp	92.83	-0.00	0.00	-28.97	-30.25	0.00
Dead+Wind 0 deg+Ice+Temp	92.83	0.06	-49.37	-6528.45	-41.21	15.16
Dead+Wind 30 deg+Ice+Temp	92.83	24.30	-41.96	-5593.87	-3257.03	-6.43
Dead+Wind 45 deg+Ice+Temp	92.83	34.23	-34.20	-4569.76	-4578.82	-16.76
Dead+Wind 60 deg+Ice+Temp	92.83	41.81	-24.12	-3237.36	-5590.00	-26.25
Dead+Wind 90 deg+Ice+Temp	92.83	48.51	-0.06	-39.71	-6465.40	-38.30
Dead+Wind 120 deg+Ice+Temp	92.83	42.81	24.63	3211.21	-5667.26	-40.57
Dead+Wind 135 deg+Ice+Temp	92.83	34.01	33.91	4474.67	-4549.23	-36.27
Dead+Wind 150 deg+Ice+Temp	92.83	24.03	41.76	5509.45	-3220.47	-30.36
Dead+Wind 180 deg+Ice+Temp	92.83	-0.47	48.16	6370.34	24.77	-10.83
Dead+Wind 210 deg+Ice+Temp	92.83	-24.64	42.12	5551.87	3232.67	9.56
Dead+Wind 225 deg+Ice+Temp	92.83	-34.53	34.31	4522.86	4549.73	19.40
Dead+Wind 240 deg+Ice+Temp	92.83	-43.30	24.99	3256.85	5663.95	28.46
Dead+Wind 270 deg+Ice+Temp	92.83	-48.81	0.27	4.81	6436.81	39.60
Dead+Wind 300 deg+Ice+Temp	92.83	-41.97	-23.68	-3181.09	5542.01	41.41
Dead+Wind 315 deg+Ice+Temp	92.83	-34.32	-33.79	-4519.53	4521.74	38.07
Dead+Wind 330 deg+Ice+Temp	92.83	-24.17	-41.68	-5559.62	3173.49	31.31
Dead+Wind 0 deg - Service	59.10	0.01	-17.50	-2321.60	-12.11	4.73
Dead+Wind 30 deg - Service	59.10	8.53	-14.72	-1977.61	-1149.90	-2.80
Dead+Wind 45 deg - Service	59.10	12.00	-11.98	-1614.73	-1615.30	-6.25
Dead+Wind 60 deg - Service	59.10	14.62	-8.43	-1142.82	-1969.41	-9.31
Dead+Wind 90 deg - Service	59.10	17.03	-0.03	-16.17	-2283.08	-13.19
Dead+Wind 120 deg - Service	59.10	15.17	8.74	1140.54	-2012.27	-13.79
Dead+Wind 135 deg - Service	59.10	11.90	11.90	1579.98	-1601.89	-11.96
Dead+Wind 150 deg - Service	59.10	8.44	14.66	1946.36	-1136.19	-9.98
Dead+Wind 180 deg - Service	59.10	-0.05	16.81	2241.25	-1.68	-3.97
Dead+Wind 210 deg - Service	59.10	-8.57	14.79	1961.55	1136.08	3.26
Dead+Wind 225 deg - Service	59.10	-12.04	12.02	1595.37	1601.89	6.71
Dead+Wind 240 deg - Service	59.10	-15.31	8.83	1154.05	2011.46	9.95
Dead+Wind 270 deg - Service	59.10	-17.10	0.02	-7.33	2273.55	13.51
Dead+Wind 300 deg - Service	59.10	-14.59	-8.36	-1131.86	1947.07	13.45
Dead+Wind 315 deg - Service	59.10	-11.96	-11.88	-1601.47	1590.83	12.27
Dead+Wind 330 deg - Service	59.10	-8.49	-14.63	-1966.28	1124.26	10.36

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-59.10	0.00	0.00	59.10	-0.00	0.000%
2	0.04	-59.10	-50.57	-0.04	59.10	50.56	0.005%
3	24.67	-59.10	-42.55	-24.67	59.10	42.55	0.005%
4	34.68	-59.10	-34.63	-34.67	59.10	34.63	0.005%
5	42.25	-59.10	-24.38	-42.25	59.10	24.38	0.005%
6	49.21	-59.10	-0.07	-49.20	59.10	0.07	0.005%
7	43.84	-59.10	25.25	-43.84	59.10	-25.25	0.005%
8	34.38	-59.10	34.39	-34.38	59.10	-34.39	0.005%
9	24.38	-59.10	42.38	-24.38	59.10	-42.38	0.005%
10	-0.14	-59.10	48.58	0.14	59.10	-48.58	0.005%
11	-24.77	-59.10	42.75	24.77	59.10	-42.74	0.005%
12	-34.79	-59.10	34.74	34.79	59.10	-34.73	0.005%
13	-44.25	-59.10	25.53	44.25	59.10	-25.53	0.005%
14	-49.43	-59.10	0.07	49.43	59.10	-0.07	0.005%
15	-42.18	-59.10	-24.17	42.17	59.10	24.16	0.005%
16	-34.56	-59.10	-34.34	34.56	59.10	34.34	0.005%



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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
17	-24.54	-59.10	-42.29	24.54	59.10	42.29	0.005%
18	0.00	-92.83	0.00	0.00	92.83	-0.00	0.001%
19	0.06	-92.83	-49.37	-0.06	92.83	49.37	0.003%
20	24.31	-92.83	-41.96	-24.30	92.83	41.96	0.003%
21	34.23	-92.83	-34.20	-34.23	92.83	34.20	0.003%
22	41.81	-92.83	-24.13	-41.81	92.83	24.12	0.003%
23	48.51	-92.83	-0.06	-48.51	92.83	0.06	0.003%
24	42.81	-92.83	24.64	-42.81	92.83	-24.63	0.003%
25	34.01	-92.83	33.92	-34.01	92.83	-33.91	0.003%
26	24.03	-92.83	41.76	-24.03	92.83	-41.76	0.003%
27	-0.47	-92.83	48.17	0.47	92.83	-48.16	0.003%
28	-24.64	-92.83	42.12	24.64	92.83	-42.12	0.003%
29	-34.53	-92.83	34.31	34.53	92.83	-34.31	0.003%
30	-43.31	-92.83	24.99	43.30	92.83	-24.99	0.003%
31	-48.82	-92.83	0.27	48.81	92.83	-0.27	0.003%
32	-41.97	-92.83	-23.68	41.97	92.83	23.68	0.003%
33	-34.33	-92.83	-33.79	34.32	92.83	33.79	0.003%
34	-24.17	-92.83	-41.68	24.17	92.83	41.68	0.003%
35	0.01	-59.10	-17.50	-0.01	59.10	17.50	0.002%
36	8.54	-59.10	-14.72	-8.53	59.10	14.72	0.002%
37	12.00	-59.10	-11.98	-12.00	59.10	11.98	0.002%
38	14.62	-59.10	-8.44	-14.62	59.10	8.43	0.002%
39	17.03	-59.10	-0.03	-17.03	59.10	0.03	0.002%
40	15.17	-59.10	8.74	-15.17	59.10	-8.74	0.002%
41	11.90	-59.10	11.90	-11.90	59.10	-11.90	0.002%
42	8.44	-59.10	14.67	-8.44	59.10	-14.66	0.002%
43	-0.05	-59.10	16.81	0.05	59.10	-16.81	0.002%
44	-8.57	-59.10	14.79	8.57	59.10	-14.79	0.002%
45	-12.04	-59.10	12.02	12.04	59.10	-12.02	0.002%
46	-15.31	-59.10	8.83	15.31	59.10	-8.83	0.002%
47	-17.10	-59.10	0.02	17.10	59.10	-0.02	0.002%
48	-14.59	-59.10	-8.36	14.59	59.10	8.36	0.002%
49	-11.96	-59.10	-11.88	11.96	59.10	11.88	0.002%
50	-8.49	-59.10	-14.63	8.49	59.10	14.63	0.002%

## Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	15	0.00007196	0.00012233
3	Yes	15	0.00007818	0.00013269
4	Yes	15	0.00008215	0.00013928
5	Yes	15	0.00008375	0.00014195
6	Yes	15	0.00007821	0.00013274
7	Yes	15	0.00007197	0.00012237
8	Yes	15	0.00007394	0.00012573
9	Yes	15	0.00007812	0.00013263
10	Yes	15	0.00008373	0.00014195
11	Yes	15	0.00007807	0.00013250
12	Yes	15	0.00007390	0.00012561
13	Yes	15	0.00007191	0.00012220
14	Yes	15	0.00007808	0.00013248
15	Yes	15	0.00008371	0.00014187
16	Yes	15	0.00008210	0.00013921
17	Yes	15	0.00007810	0.00013256



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18	Yes	6	0.00000001	0.00007867
19	Yes	16	0.00006509	0.00011179
20	Yes	16	0.00006870	0.00011779
21	Yes	16	0.00007104	0.00012168
22	Yes	16	0.00007199	0.00012327
23	Yes	16	0.00006872	0.00011786
24	Yes	16	0.00006512	0.00011188
25	Yes	16	0.00006623	0.00011379
26	Yes	16	0.00006866	0.00011780
27	Yes	16	0.00007199	0.00012330
28	Yes	16	0.00006863	0.00011768
29	Yes	16	0.00006619	0.00011366
30	Yes	16	0.00006504	0.00011169
31	Yes	16	0.00006862	0.00011764
32	Yes	16	0.00007196	0.00012319
33	Yes	16	0.00007100	0.00012160
34	Yes	16	0.00006910	0.00011770
35	Yes	15	0.00000001	0.00012739
36	Yes	15	0.00000001	0.00013104
37	Yes	15	0.00000001	0.00013336
38	Yes	15	0.00000001	0.00013434
39	Yes	15	0.00000001	0.00013113
40	Yes	15	0.00000001	0.00012753
41	Yes	15	0.00000001	0.00012882
42	Yes	15	0.00000001	0.00013108
43	Yes	15	0.00000001	0.00013436
44	Yes	15	0.00000001	0.00013099
45	Yes	15	0.00000001	0.00012870
46	Yes	15	0.00000001	0.00012736
47	Yes	15	0.00000001	0.00013089
48	Yes	15	0.00000001	0.00013418
49	Yes	15	0.00000001	0.00013321
50	Yes	15	0.00000001	0.00013090

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	245 - 230	13.089	35	0.6586	0.0498
T2	230 - 210	10.978	35	0.6259	0.0515
T3	210 - 190	8.443	35	0.5339	0.0458
T4	190 - 180	6.354	35	0.4297	0.0384
T5	180 - 160	5.500	35	0.3772	0.0333
T6	160 - 140	4.098	35	0.2877	0.0266
T7	140 - 120	2.995	35	0.2303	0.0217
T8	120 - 110	2.121	35	0.1778	0.0183
T9	110 - 100	1.759	35	0.1587	0.0160
T10	100 - 80	1.432	35	0.1401	0.0136
T11	80 - 60	0.903	46	0.1034	0.0101
T12	60 - 40	0.507	46	0.0754	0.0069
T13	40 - 20	0.227	46	0.0480	0.0041
T14	20 - 0	0.050	46	0.0210	0.0013

### Critical Deflections and Radius of Curvature - Service Wind



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<i>Elevation</i>	<i>Appurtenance</i>	<i>Gov. Load Comb.</i>	<i>Deflection in</i>	<i>Tilt °</i>	<i>Twist °</i>	<i>Radius of Curvature ft</i>
<i>ft</i>						
247.00	Lightning Rod 2"x10'	35	13.089	0.6586	0.0498	39977
235.00	TMA	35	11.669	0.6398	0.0514	19988
135.00	2.5" Dia. 12' OMNI	35	2.757	0.2166	0.0208	22236
125.00	20' Omni	35	2.320	0.1895	0.0192	23100
110.00	KP4F-23	35	1.759	0.1587	0.0160	36173
105.00	Andrew 6' w/Radome	35	1.591	0.1496	0.0147	31286
60.00	Camera with Mount	46	0.507	0.0754	0.0069	39657
50.00	1.5" Dia 4' Omni w/Pipe Mount	46	0.354	0.0620	0.0055	46758

### Maximum Tower Deflections - Design Wind

<i>Section No.</i>	<i>Elevation ft</i>	<i>Horz. Deflection in</i>	<i>Gov. Load Comb.</i>	<i>Tilt °</i>	<i>Twist °</i>
T1	245 - 230	37.872	13	1.9054	0.1442
T2	230 - 210	31.754	13	1.8088	0.1489
T3	210 - 190	24.416	13	1.5429	0.1325
T4	190 - 180	18.375	13	1.2419	0.1111
T5	180 - 160	15.906	13	1.0903	0.0962
T6	160 - 140	11.853	13	0.8313	0.0768
T7	140 - 120	8.668	13	0.6655	0.0640
T8	120 - 110	6.143	13	0.5134	0.0538
T9	110 - 100	5.095	13	0.4585	0.0472
T10	100 - 80	4.150	13	0.4049	0.0400
T11	80 - 60	2.618	13	0.2991	0.0300
T12	60 - 40	1.469	13	0.2182	0.0208
T13	40 - 20	0.656	13	0.1390	0.0125
T14	20 - 0	0.144	13	0.0608	0.0038

### Critical Deflections and Radius of Curvature - Design Wind

<i>Elevation</i>	<i>Appurtenance</i>	<i>Gov. Load Comb.</i>	<i>Deflection in</i>	<i>Tilt °</i>	<i>Twist °</i>	<i>Radius of Curvature ft</i>
<i>ft</i>						
247.00	Lightning Rod 2"x10'	13	37.872	1.9054	0.1442	13909
235.00	TMA	13	33.757	1.8493	0.1487	6954
135.00	2.5" Dia. 12' OMNI	13	7.979	0.6257	0.0614	7708
125.00	20' Omni	13	6.717	0.5475	0.0566	8005
110.00	KP4F-23	13	5.095	0.4585	0.0472	12536
105.00	Andrew 6' w/Radome	13	4.609	0.4321	0.0435	10855
60.00	Camera with Mount	13	1.469	0.2182	0.0208	13704
50.00	1.5" Dia 4' Omni w/Pipe Mount	13	1.026	0.1793	0.0166	16163

### Bolt Design Data



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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	245	Leg	A325N	0.6250	5	0.28	12.89	0.022 ✓	1.333	Bolt DS
T2	230	Leg	A325N	0.7500	5	5.23	19.40	0.270 ✓	1.333	Bolt Tension
T3	210	Leg	A325N	1.0000	6	12.70	34.53	0.368 ✓	1.333	Bolt Tension
T4	190	Leg	A325N	1.0000	6	20.73	34.56	0.600 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	4.43	8.16	0.543 ✓	1.333	Member Bearing
T5	180	Leg	A325N	1.0000	6	22.41	34.56	0.648 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	3.62	8.16	0.444 ✓	1.333	Member Bearing
T6	160	Leg	A325N	1.0000	6	25.07	34.56	0.726 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	3.92	8.16	0.481 ✓	1.333	Member Bearing
T7	140	Leg	A325N	1.0000	6	27.81	34.56	0.805 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	4.72	8.16	0.579 ✓	1.333	Member Bearing
T8	120	Diagonal	A325N	1.2500	1	5.30	10.20	0.520 ✓	1.333	Member Bearing
T9	110	Leg	A325N	1.2500	6	32.34	54.00	0.599 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	5.70	10.20	0.559 ✓	1.333	Member Bearing
T10	100	Leg	A325N	1.2500	6	34.04	54.00	0.630 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6.39	16.99	0.376 ✓	1.333	Member Bearing
T11	80	Leg	A325N	1.2500	6	37.42	54.00	0.693 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6.88	16.99	0.405 ✓	1.333	Member Bearing
T12	60	Leg	A325N	1.2500	6	40.66	54.00	0.753 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	7.56	16.99	0.445 ✓	1.333	Member Bearing
T13	40	Leg	A325N	1.2500	6	43.88	54.00	0.813 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	9.28	13.59	0.683 ✓	1.333	Member Bearing
T14	20	Leg	A325N	1.2500	6	47.10	54.00	0.872 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	17.32	27.19	0.637 ✓	1.333	Member Bearing

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	1 1/2	15.00	2.33	74.7 K=1.00	20.058	1.7672	-30.08	35.44	0.849 ✓
T2	230 - 210	2	20.00	2.38	57.0 K=1.00	23.222	3.1416	-81.26	72.95	1.114 ✓
T3	210 - 190	2 1/2	20.00	2.33	44.8 K=1.00	25.141	4.9087	-128.75	123.41	1.043 ✓
T4	190 - 180	Pirol 105245	10.02	10.02	37.8	26.132	5.3014	-130.50	138.54	0.942 ✓



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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
					K=1.00					
T5	180 - 160	Pirol 105217	20.03	10.02	37.8	26.132	5.3014	-150.58	138.54	1.087
					K=1.00					
T6	160 - 140	Pirol 105218	20.03	10.02	32.4	26.848	7.2158	-169.98	193.73	0.877
					K=1.00					
T7	140 - 120	Pirol 105218	20.03	10.02	32.4	26.848	7.2158	-190.90	193.73	0.985
					K=1.00					
T8	120 - 110	Pirol 105219	10.02	10.02	28.4	27.351	9.4248	-201.93	257.78	0.783
					K=1.00					
T9	110 - 100	Pirol 105219	10.02	5.19	28.4	27.351	9.4248	-212.67	257.78	0.825
					K=1.00					
T10	100 - 80	Pirol 105219	20.03	10.02	28.4	27.351	9.4248	-237.95	257.78	0.923
					K=1.00					
T11	80 - 60	Pirol 105220	20.03	10.02	25.2	27.723	11.9282	-262.35	330.69	0.793
					K=1.00					
T12	60 - 40	Pirol 105220	20.03	10.02	25.2	27.723	11.9282	-287.50	330.69	0.869
					K=1.00					
T13	40 - 20	Pirol 105220	20.03	10.02	25.2	27.723	11.9282	-313.54	330.69	0.948
					K=1.00					
T14	20 - 0	Pirol 112738	20.03	20.03	32.6	26.826	14.7262	-331.38	395.05	0.839
					K=1.00					

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L <sub>d</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual V K	Allow. V <sub>a</sub> K	Stress Ratio
T4	190 - 180	0.5	1.47	120.0	10.366	0.1963	1.00	2.28	0.440
T5	180 - 160	0.5	1.47	120.0	10.279	0.1963	0.60	2.26	0.265
T6	160 - 140	0.5	1.46	119.0	10.423	0.1963	0.21	2.29	0.091
T7	140 - 120	0.5	1.46	119.0	10.423	0.1963	0.36	2.29	0.159
T8	120 - 110	0.625	1.45	94.4	13.671	0.3068	0.29	4.69	0.061
T9	110 - 100	0.625	1.45	94.4	13.671	0.3068	1.52	4.69	0.324
T10	100 - 80	0.625	1.45	94.4	13.671	0.3068	0.35	4.69	0.074
T11	80 - 60	0.625	1.43	93.6	13.766	0.3068	0.23	4.73	0.048
T12	60 - 40	0.625	1.43	93.6	13.766	0.3068	0.48	4.73	0.101
T13	40 - 20	0.625	1.43	93.6	13.766	0.3068	2.71	4.73	0.573
T14	20 - 0	0.75	1.73	93.9	16.080	0.4418	1.35	9.78	0.138



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### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	3/4	4.63	2.24	143.6 K=1.00	7.246	0.4418	-4.20	3.20	1.311
T2	230 - 210	7/8	5.05	2.45	134.3 K=1.00	8.281	0.6013	-4.57	4.98	0.917
T3	210 - 190	1	5.11	2.46	117.9 K=1.00	10.745	0.7854	-5.49	8.44	0.650
T4	190 - 180	L2 1/2x2 1/2x3/16	11.42	5.19	125.8 K=1.00	9.431	0.9020	-4.65	8.51	0.547
T5	180 - 160	L2 1/2x2 1/2x3/16	12.50	5.84	141.5 K=1.00	7.462	0.9020	-4.00	6.73	0.594
T6	160 - 140	L2 1/2x2 1/2x3/16	13.80	6.54	158.4 K=1.00	5.949	0.9020	-4.26	5.37	0.795
T7	140 - 120	L3x3x3/16	15.24	7.29	146.8 K=1.00	6.931	1.0900	-5.03	7.56	0.665
T8	120 - 110	L3x3x3/16	16.01	7.69	154.7 K=1.00	6.237	1.0900	-5.50	6.80	0.810
T9	110 - 100	L3x3x3/16	16.80	8.09	162.9 K=1.00	5.628	1.0900	-6.17	6.13	1.006
T10	100 - 80	L3x3x5/16	18.45	8.93	181.9 K=1.00	4.515	1.7800	-6.61	8.04	0.823
T11	80 - 60	L3x3x5/16	20.16	9.79	199.5 K=1.00	3.753	1.7800	-7.06	6.68	1.057
T12	60 - 40	L3 1/2x3 1/2x5/16	21.92	10.68	185.7 K=1.00	4.331	2.0900	-8.04	9.05	0.888
T13	40 - 20	L4x4x1/4	23.71	11.58	174.8 K=1.00	4.887	1.9400	-10.27	9.48	1.084
T14	20 - 0	2L3 1/2x3 1/2x5/16x3/4	30.49	14.91	165.7 K=1.00	5.440	4.1800	-15.95	22.74	0.702

### Secondary Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	110 - 100	L3x3x5/16	13.48	12.48	254.3 K=1.00	2.309	1.7800	-3.69	4.11	0.897
KL/R > 250 (C) - 232										

### Top Girt Design Data (Compression)



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Section No.	Elevation	Size	L	L <sub>a</sub>	KL/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	245 - 230	7/8	4.00	3.88	212.6 K=1.00	3.305	0.6013	-1.27	1.99	0.638 ✓
		KL/R > 200 (C) - 5								
T2	230 - 210	1	4.01	3.85	184.6 K=1.00	4.382	0.7854	-2.20	3.44	0.639 ✓
T3	210 - 190	1	4.52	4.31	206.8 K=1.00	3.492	0.7854	-1.73	2.74	0.632 ✓
		KL/R > 200 (C) - 107								

### Bottom Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>a</sub>	KL/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	245 - 230	7/8	4.00	3.88	212.6 K=1.00	3.305	0.6013	-1.71	1.99	0.859 ✓
		KL/R > 200 (C) - 8								
T2	230 - 210	1	4.49	4.32	207.4 K=1.00	3.472	0.7854	-2.21	2.73	0.810 ✓
		KL/R > 200 (C) - 53								
T3	210 - 190	1	4.98	4.77	229.2 K=1.00	2.843	0.7854	-1.36	2.23	0.609 ✓
		KL/R > 200 (C) - 110								

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>a</sub>	KL/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	245 - 230	1 1/2	15.00	0.50	16.0	32.500	0.7732	26.12	25.13	1.039 ✓
T2	230 - 210	2	20.00	0.50	12.0	30.000	3.1416	76.18	94.25	0.808 ✓
T3	210 - 190	2 1/2	20.00	0.67	12.8	30.000	4.9087	125.59	147.26	0.853 ✓
T4	190 - 180	Pirod 105245	10.02	10.02	37.8	30.000	5.3014	124.40	159.04	0.782 ✓
T5	180 - 160	Pirod 105217	20.03	10.02	37.8	30.000	5.3014	142.02	159.04	0.893 ✓
T6	160 - 140	Pirod 105218	20.03	10.02	32.4	30.000	7.2158	158.34	216.47	0.731 ✓
T7	140 - 120	Pirod 105218	20.03	10.02	32.4	30.000	7.2158	175.74	216.47	0.812 ✓
T8	120 - 110	Pirod 105219	10.02	10.02	28.4	30.000	9.4248	185.13	282.74	0.655 ✓



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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	110 - 100	Pirol 105219	10.02	4.82	28.4	30.000	9.4248	194.05	282.74	0.686 ✓
T10	100 - 80	Pirol 105219	20.03	10.02	28.4	30.000	9.4248	214.61	282.74	0.759 ✓
T11	80 - 60	Pirol 105220	20.03	10.02	25.2	30.000	11.9282	234.10	357.85	0.654 ✓
T12	60 - 40	Pirol 105220	20.03	10.02	25.2	30.000	11.9282	253.54	357.85	0.709 ✓
T13	40 - 20	Pirol 105220	20.03	10.02	25.2	30.000	11.9282	273.96	357.85	0.766 ✓
T14	20 - 0	Pirol 112738	20.03	20.03	32.6	30.000	14.7262	282.60	441.79	0.640 ✓

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L <sub>d</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual V K	Allow. V <sub>a</sub> K	Stress Ratio
T4	190 - 180	0.5	1.47	120.0	10.366	0.1963	1.00	2.28	0.440 ✓
T5	180 - 160	0.5	1.47	120.0	10.279	0.1963	0.60	2.26	0.265 ✓
T6	160 - 140	0.5	1.46	119.0	10.423	0.1963	0.21	2.29	0.091 ✓
T7	140 - 120	0.5	1.46	119.0	10.423	0.1963	0.36	2.29	0.159 ✓
T8	120 - 110	0.625	1.45	94.4	13.671	0.3068	0.29	4.69	0.061 ✓
T9	110 - 100	0.625	1.45	94.4	13.671	0.3068	1.52	4.69	0.324 ✓
T10	100 - 80	0.625	1.45	94.4	13.671	0.3068	0.35	4.69	0.074 ✓
T11	80 - 60	0.625	1.43	93.6	13.766	0.3068	0.23	4.73	0.048 ✓
T12	60 - 40	0.625	1.43	93.6	13.766	0.3068	0.48	4.73	0.101 ✓
T13	40 - 20	0.625	1.43	93.6	13.766	0.3068	2.71	4.73	0.573 ✓
T14	20 - 0	0.75	1.73	93.9	16.080	0.4418	1.35	9.78	0.138 ✓

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KI/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	3/4	4.63	2.24	143.6	30.000	0.4418	4.20	13.25	0.317
T2	230 - 210	7/8	4.69	2.27	124.4	30.000	0.6013	4.65	18.04	0.258
T3	210 - 190	1	5.11	2.46	117.9	30.000	0.7854	5.24	23.56	0.222
T4	190 - 180	L2 1/2x2 1/2x3/16	11.42	5.19	80.1	21.600	0.9020	4.43	19.48	0.227
T5	180 - 160	L2 1/2x2 1/2x3/16	11.93	5.59	86.2	21.600	0.9020	3.62	19.48	0.186
T6	160 - 140	L2 1/2x2 1/2x3/16	13.80	6.54	100.8	21.600	0.9020	3.92	19.48	0.201
T7	140 - 120	L3x3x3/16	15.24	7.29	93.2	21.600	1.0900	4.72	23.54	0.201
T8	120 - 110	L3x3x3/16	16.01	7.69	98.2	21.600	1.0900	5.30	23.54	0.225
T9	110 - 100	L3x3x3/16	16.80	8.09	103.4	21.600	1.0900	5.70	23.54	0.242
T10	100 - 80	L3x3x5/16	18.45	8.93	116.2	21.600	1.7800	6.39	38.45	0.166
T11	80 - 60	L3x3x5/16	20.16	9.79	127.4	21.600	1.7800	6.88	38.45	0.179
T12	60 - 40	L3 1/2x3 1/2x5/16	21.92	10.68	118.6	21.600	2.0900	7.56	45.14	0.168
T13	40 - 20	L4x4x1/4	22.81	11.13	106.9	21.600	1.9400	9.28	41.90	0.221
T14	20 - 0	2L3 1/2x3 1/2x5/16x3/4	30.49	14.91	165.7	21.600	4.1800	17.32	90.29	0.192

### Secondary Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KI/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	110 - 100	L3x3x5/16	13.48	12.48	162.4	21.600	1.7800	3.69	38.45	0.096

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	KI/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	7/8	4.00	3.88	212.6	30.000	0.6013	1.18	18.04	0.065
T2	230 - 210	1	4.01	3.85	184.6	30.000	0.7854	2.31	23.56	0.098
T3	210 - 190	1	4.52	4.31	206.8	30.000	0.7854	1.87	23.56	0.079



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	Storrs (UCONN), CT (Site: CT11303B) / NSS-022	15:37:53 04/01/15
	<b>Client</b>	<b>Designed by</b>
	Northeast Site Solutions / T-Mobile	MCD

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	



### Bottom Girt Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T1	245 - 230	7/8	4.00	3.88	212.6	30.000	0.6013	1.53	18.04	0.085
T2	230 - 210	1	4.49	4.32	207.4	30.000	0.7854	2.06	23.56	0.087
T3	210 - 190	1	4.98	4.77	229.2	30.000	0.7854	1.43	23.56	0.060



### Section Capacity Table

Section No.	Elevation	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	245 - 230	Leg	1 1/2	1	26.12	33.50	78.0	Pass
T2	230 - 210	Leg	2	46	-81.26	97.25	83.6	Pass
T3	210 - 190	Leg	2 1/2	103	-128.75	164.50	78.3	Pass
T4	190 - 180	Leg	Pirol 105245	160	-130.50	184.67	70.7	Pass
T5	180 - 160	Leg	Pirol 105217	169	-150.58	184.67	81.5	Pass
T6	160 - 140	Leg	Pirol 105218	184	-169.98	258.24	65.8	Pass
T7	140 - 120	Leg	Pirol 105218	199	-190.90	258.24	73.9	Pass
T8	120 - 110	Leg	Pirol 105219	214	-201.93	343.62	58.8	Pass
T9	110 - 100	Leg	Pirol 105219	223	-212.67	343.62	61.9	Pass
T10	100 - 80	Leg	Pirol 105219	235	-237.95	343.62	69.2	Pass
T11	80 - 60	Leg	Pirol 105220	250	-262.35	440.81	59.5	Pass
T12	60 - 40	Leg	Pirol 105220	267	-287.50	440.81	65.2	Pass
T13	40 - 20	Leg	Pirol 105220	280	-313.54	440.81	71.1	Pass
T14	20 - 0	Leg	Pirol 112738	297	-331.38	526.59	62.9	Pass
65.4 (b)								
T1	245 - 230	Diagonal	3/4	15	-4.20	4.27	98.3	Pass
T2	230 - 210	Diagonal	7/8	58	-4.57	6.64	68.8	Pass
T3	210 - 190	Diagonal	1	157	-5.49	11.25	48.8	Pass
T4	190 - 180	Diagonal	L2 1/2x2 1/2x3/16	165	-4.65	11.34	41.0	Pass
T5	180 - 160	Diagonal	L2 1/2x2 1/2x3/16	175	-4.00	8.97	44.6	Pass
T6	160 - 140	Diagonal	L2 1/2x2 1/2x3/16	190	-4.26	7.15	59.6	Pass
T7	140 - 120	Diagonal	L3x3x3/16	205	-5.03	10.07	49.9	Pass
T8	120 - 110	Diagonal	L3x3x3/16	219	-5.50	9.06	60.7	Pass
T9	110 - 100	Diagonal	L3x3x3/16	231	-6.17	8.18	75.4	Pass
T10	100 - 80	Diagonal	L3x3x5/16	241	-6.61	10.71	61.7	Pass
T11	80 - 60	Diagonal	L3x3x5/16	256	-7.06	8.90	79.3	Pass
T12	60 - 40	Diagonal	L3 1/2x3 1/2x5/16	271	-8.04	12.07	66.6	Pass
T13	40 - 20	Diagonal	L4x4x1/4	286	-10.27	12.64	81.3	Pass
T14	20 - 0	Diagonal	2L3 1/2x3 1/2x5/16x3/4	300	-15.95	30.31	52.6	Pass
T9	110 - 100	Secondary Horizontal	L3x3x5/16	232	-3.69	5.48	67.3	Pass
T1	245 - 230	Top Girt	7/8	5	-1.27	2.65	47.9	Pass
T2	230 - 210	Top Girt	1	50	-2.20	4.59	47.9	Pass
T3	210 - 190	Top Girt	1	107	-1.73	3.66	47.4	Pass



<b>tnxTower</b>  <b>AECOM</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	MODification Structural Analysis - Tower	<b>Page</b>	46 of 46
	<b>Project</b>	Storrs (UConn), CT (Site: CT11303B) / NSS-022	<b>Date</b>	15:37:53 04/01/15
	<b>Client</b>	Northeast Site Solutions / T-Mobile	<b>Designed by</b>	MCD

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	245 - 230	Bottom Girt	7/8	8	-1.71	2.65	64.4	Pass
T2	230 - 210	Bottom Girt	1	53	-2.21	3.63	60.8	Pass
T3	210 - 190	Bottom Girt	1	110	-1.36	2.98	45.7	Pass
Summary								
Leg (T2)							83.6	Pass
Diagonal (T1)							98.3	Pass
Secondary Horizontal (T9)							67.3	Pass
Top Girt (T2)							47.9	Pass
Bottom Girt (T1)							64.4	Pass
Bolt Checks							65.4	Pass
<b>RATING =</b>							<b>98.3</b>	<b>Pass</b>



## ANCHOR BOLT ANALYSIS



## ANCHOR BOLT ANALYSIS

### Input Data

#### Max Pier Reactions:

Uplift:	Uplift := 296 kips	user input
Shear:	Shear := 51 kips	user input
Compression:	Compression := 345 kips	user input

#### Anchor Bolt Data:

Bolt Material → A572 - Gr. 42 (for bolts up to 6" Dia.)

Number of Anchor Bolts = N	N := 6	user input
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Bolt Ultimate Strength:	F <sub>u</sub> := 60 ksi	user input
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Bolt Yield Strength:	F <sub>y</sub> := 42 ksi	user input
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Bolt Modulus:	E := 29000 ksi	user input
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Thickness of Anchor Bolts	D := 2.0 in	user input	From PiROD DWG No. 202932-B
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Threads per Inch:	n := 4.5	user input
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Coefficient of Friction:	μ := 0.55	user input	(for baseplate with grout ASCE 10-97)
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Description	Anchor Bolt Analysis	Computed by	MCD	Sheet	2 of 3
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### Anchor Bolt Area:

Gross Area of Bolt:

$$A_g := \frac{\pi}{4} \cdot D^2 \quad A_g = 3.142 \cdot \text{in}^2$$

Net Area of Bolt:

$$A_n := \frac{\pi}{4} \cdot \left( D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 \quad A_n = 2.498 \cdot \text{in}^2$$

### Check Tensile Forces:

Maximum Tensile Force (Gross Area):

$$\text{AllowableTension} := 1.333 \cdot (0.33 \cdot A_g \cdot F_u) \quad \text{AllowableTension} = 82.9 \cdot \text{kips}$$

Note: 1.333 increase allowed per TIA/EIA

Maximum Tensile Force (Net Area):

$$F_{\text{net.area}} := 1.333 \cdot (0.60 \cdot A_n \cdot F_y) \quad F_{\text{net.area}} = 83.9 \cdot \text{kips}$$

Note: 1.333 increase allowed per TIA/EIA

Applied Tension:

$$\text{MaxTension} := \frac{\text{Uplift}}{N} \quad \text{MaxTension} = 49.3 \cdot \text{kips}$$

Check Stresses:

$$\frac{\text{MaxTension}}{F_{\text{net.area}}} = 0.59$$

$$\text{Condition1} := \text{if} \left( \frac{\text{MaxTension}}{F_{\text{net.area}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition1 = "OK"



**Check Anchor Bolt Area:**

Based on the ASCE 10-97 Design of Latticed Steel Transmission Structures

Required Area:

$$A_{s1} := \frac{\text{Uplift}}{F_y} + \frac{\text{Shear}}{\mu \cdot 0.85 \cdot F_y} \quad A_{s1} = 9.6 \cdot \text{in}^2$$

$$A_{s2} := \left| \frac{\text{Shear} - (0.3 \cdot \text{Compression})}{\mu \cdot 0.85 \cdot F_y} \right| \quad A_{s2} = 2.7 \cdot \text{in}^2$$

Provided Area:

$$A_{\text{provided}} := A_n \cdot N \quad A_{\text{provided}} = 15.0 \cdot \text{in}^2$$

$$\text{Condition2} := \text{if} \left( \frac{A_{s1}}{A_{\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition2 = "OK"

$$\frac{A_{s1}}{A_{\text{provided}}} = 0.64$$

$$\text{Condition3} := \text{if} \left( \frac{A_{s2}}{A_{\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition3 = "OK"

$$\frac{A_{s2}}{A_{\text{provided}}} = 0.18$$



## FOUNDATION ANALYSIS



## FOUNDATION ANALYSIS

### Input Data

#### Maximum Pier Reactions:

Compression:  $C_t := 345 \text{ kips}$  *user input*  
 Uplift:  $U_t := 296 \text{ kips}$  *user input*

#### Material Properties:

Unit Weight of Concrete:  $\gamma_c := 150 \text{ pcf}$  *user input*  
 Unit Weight of Water:  $\gamma_w := 62.4 \text{ pcf}$  *user input*  
 Unit Weight of Soil:  $\gamma_s := 125 \text{ pcf}$  *user input*

#### Foundation Dimensions:

Drilled Caisson Length:  $C_{\text{Length}} := 31 \text{ ft}$  *user input*  
 Diameter of Pier:  $d_p := 5.5 \text{ ft}$  *user input*  
 Extension of Pier Above Grade:  $L_{\text{pag}} := 0.5 \text{ ft}$  *user input*

Allowable Soil Bearing Capacity:  $q_s := 5000 \text{ psf}$  *user input*  
 Water Table Below Grade:  $W_d := 32 \text{ ft}$  *user input*  
 Average Allowable Shear:  $f_l := 1020 \text{ psf}$  *user input*  
 Depth Neglected for Skin Friction at Top:  $\text{Depthunbond} := 1.0 \text{ ft}$  *user input*

### Loading:

$$\text{TotalDownLoad} := C_t + \pi \cdot \frac{d_p^2}{4} \cdot [L_{\text{pag}} \cdot \gamma_c + [\gamma_c \cdot (C_{\text{Length}} - L_{\text{pag}})]]$$

$$\text{TotalDownLoad} = 455.5 \text{ kips}$$

$$\text{PierWeight} := \pi \cdot \frac{d_p^2}{4} \cdot [(W_d + L_{\text{pag}}) \cdot \gamma_c + (C_{\text{Length}} - W_d - L_{\text{pag}}) \cdot (\gamma_c - \gamma_w)]$$

$$\text{PierWeight} = 112.7 \text{ kips}$$

$$\text{SoilShear} := \pi \cdot d_p \cdot [f_l \cdot (W_d - \text{Depthunbond}) + f_l \cdot (C_{\text{Length}} - W_d - L_{\text{pag}})]$$

$$\text{SoilShear} = 519.9 \text{ kips}$$





Job	<u>245' SST Self-Supporting Tower, Mansfield, CT</u>	Project No.	<u>NSS-021 Rev. 1</u>	Page	of
Description	<u>Drilled Pier Cassion Evaluation</u>	Computed by	<u>MCD</u>	Sheet	<u>2</u> of <u>2</u>
		Checked by		Date	<u>04/01/15</u>
				Date	

### Compression Capacity:

$$\text{TotalDownLoadCapacity} := \text{SoilShear} + q_s \cdot \left( \pi \cdot \frac{d_p^2}{4} \right)$$

$$\text{TotalDownLoadCapacity} = 638.7 \cdot \text{kips}$$

$$\text{CheckDownLoadCapacity} := \text{if}(\text{TotalDownLoad} < \text{TotalDownLoadCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckDownLoadCapacity} = \text{"Okay"}$$

### Tension Capacity:

$$\text{TotalUpLiftCapacity} := \text{SoilShear} + \text{PierWeight}$$

$$\text{TotalUpLiftCapacity} = 632.6 \cdot \text{kips}$$

$$\text{CheckUpLiftCapacity} := \text{if}(U_t < \text{TotalUpLiftCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckUpLiftCapacity} = \text{"Okay"}$$

$$\text{SafetyFactor}_{\text{provided}} := \frac{\text{TotalUpLiftCapacity}}{U_t}$$

$$\text{SafetyFactor}_{\text{provided}} = 2.14$$

### Check Cone Failure:

$$\text{ConeFailureCapacity} := \frac{[(C_{\text{Length}} - L_{\text{pag}}) \cdot \tan(30\text{deg}) \cdot 2 + d_p]^2 \cdot \pi \cdot C_{\text{Length}} - L_{\text{pag}}}{4 \cdot 3} \cdot \gamma_s$$

$$\text{ConeFailureCapacity} = 1654.85 \cdot \text{kips}$$

$$\text{CheckConeFailureCapacity} := \text{if}(U_t < \text{ConeFailureCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckConeFailureCapacity} = \text{"Okay"}$$

$$\text{ConeSafetyFactor}_{\text{provided}} := \frac{\text{ConeFailureCapacity}}{U_t}$$

$$\text{ConeSafetyFactor}_{\text{provided}} = 5.59$$



#### About AECOM

AECOM (NYSE: ACM) is a global provider of professional technical and management support services to a broad range of markets, including transportation, facilities, environmental, energy, water and government. With approximately 45,000 employees around the world, AECOM is a leader in all of the key markets that it serves. AECOM provides a blend of global reach, local knowledge, innovation, and collaborative technical excellence in delivering solutions that enhance and sustain the world's built, natural, and social environments. A Fortune 500 company, AECOM serves clients in more than 100 countries and has annual revenue in excess of \$6 billion.

More information on AECOM and its services can be found at [www.aecom.com](http://www.aecom.com).

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# EXHIBIT C



**RADIO FREQUENCY EMISSIONS ANALYSIS REPORT  
EVALUATION OF HUMAN EXPOSURE POTENTIAL  
TO NON-IONIZING EMISSIONS**

**T-Mobile Existing Facility**

**Site ID: CT11303B**

**UConn  
82 North Eagleville Road  
Storrs, CT 06268**

**March 25, 2015**

**EBI Project Number: 6215001747**

Site Compliance Summary	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general public allowable limit:	<b>10.19 %</b>



March 25, 2015

T-Mobile USA  
Attn: Jason Overbey, RF Manager  
35 Griffin Road South  
Bloomfield, CT 06002

Emissions Analysis for Site: **CT11303B – UCONN**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **82 North Eagleville Road, Storrs, CT**, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the 700 MHz Band is  $467 \mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the PCS and AWS bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **82 North Eagleville Road, Storrs, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
- 2) 2 UMTS channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 LTE channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 1 LTE channel (700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
- 5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.



- 6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antennas used in this modeling are the **Ericsson AIR21 (B4A/B2P & B4A/B2P)** for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the **Commscope LNX-6515DS-VTM** for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The **Ericsson AIR21 (B4A/B2P & B4A/B2P)** have a maximum gain of **15.9 dBd** at their main lobe. The **Commscope LNX-6515DS-VTM** has a maximum gain of **14.6 dBd** at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antenna mounting height centerline of the proposed antennas is **235 feet** above ground level (AGL).
- 9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.



### T-Mobile Site Inventory and Power Data

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Ericsson AIR21 B4A/B2P	Make / Model:	Ericsson AIR21 B4A/B2P	Make / Model:	Ericsson AIR21 B4A/B2P
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	235	Height (AGL):	235	Height (AGL):	235
Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)
Channel Count	2	Channel Count	2	# PCS Channels:	2
Total TX Power:	120	Total TX Power:	120	# AWS Channels:	120
ERP (W):	4,668.54	ERP (W):	4,668.54	ERP (W):	4,668.54
Antenna A1 MPE%	0.32	Antenna B1 MPE%	0.32	Antenna C1 MPE%	0.32
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Ericsson AIR21 B2A/B4P	Make / Model:	Ericsson AIR21 B2A/B4P	Make / Model:	Ericsson AIR21 B2A/B4P
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	235	Height (AGL):	235	Height (AGL):	235
Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz(PCS) / 2100 MHz (AWS)
Channel Count	4	Channel Count	4	Channel Count	4
Total TX Power:	120	Total TX Power:	120	Total TX Power:	120
ERP (W):	4,668.54	ERP (W):	4,668.54	ERP (W):	4,668.54
Antenna A2 MPE%	0.32	Antenna B2 MPE%	0.32	Antenna C2 MPE%	0.32
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM
Gain:	14.6 dBd	Gain:	14.6 dBd	Gain:	14.6 dBd
Height (AGL):	235	Height (AGL):	235	Height (AGL):	235
Frequency Bands	700 MHz	Frequency Bands	700 MHz	Frequency Bands	700 MHz
Channel Count	1	Channel Count	1	Channel Count	1
Total TX Power:	30	Total TX Power:	30	Total TX Power:	30
ERP (W):	865.21	ERP (W):	865.21	ERP (W):	865.21
Antenna A3 MPE%	0.13	Antenna B3 MPE%	0.13	Antenna C3 MPE%	0.13

Site Composite MPE%	
Carrier	MPE%
T-Mobile	2.30
CT Public Broadcasting	1.66 %
UCONN	2.14 %
UCONN Fire	0.83 %
Sprint	3.26 %
Site Total MPE %:	10.19 %

T-Mobile Sector 1 Total:	0.77 %
T-Mobile Sector 2 Total:	0.77 %
T-Mobile Sector 3 Total:	0.77 %
Site Total:	10.19 %



## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector 1:	0.77 %
Sector 2:	0.77 %
Sector 3 :	0.77 %
T-Mobile Total:	2.30 %
Site Total:	10.19 %
Site Compliance Status:	<b>COMPLIANT</b>

The anticipated composite MPE value for this site assuming all carriers present is **10.19%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



Scott Heffernan  
RF Engineering Director

### EBI Consulting

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