



Together with Nextel

10 Industrial Ave, Suite 3  
Mahwah, NJ 07430  
Phone: 201-704-8157  
Jennifer Ardis  
Real Estate Consultant

2/11/15

**Hand Delivered**

Ms. Melanie A. Bachman  
Acting Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

CC to Property Owner  
U-CONN  
82 North Eagleville Rd.  
Storrs, CT 06269

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 82 North Eagleville Rd. Storrs, CT 06269 Known to Sprint Spectrum L.P. as site CT03XC214

Dear Ms. Bachman:

In order to accommodate technological changes, implement Code Division Multiple Access (“CDMA”) and/or Long Term Evolution (“LTE”) capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs Spread-Spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel.

LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in Sprint's operations at the site. Also included is documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

The changes to the facility do not constitute modification as defined Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for the R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will not be affected.
2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound.
3. The proposed changes will not increase the noise level at the existing facility by 6 decibels or more.
4. Radio Frequency power density may increase due to the use of one or more CDMA transmissions. Moreover, LTE will utilize additional radio frequencies newly licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons Sprint Spectrum L.P. respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at 201-704-8157 or email [JArdis@Transcendwireless.com](mailto:JArdis@Transcendwireless.com) with questions concerning this matter.

Thank you for your consideration.

Sincerely,

Jennifer Ardis  
Real Estate Consultant

RADIO FREQUENCY FCC REGULATORY COMPLIANCE  
MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

Sprint Existing Facility

Site ID: CT03XC214

U-Conn

82 North Eaglesville Road  
Storrs, CT 06269

**January 21, 2015**

**EBI Project Number: 62143748**

January 21, 2015

Sprint  
Attn: RF Engineering Manager  
1 International Boulevard, Suite 800  
Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:  
**CT03XC214 - U-Conn**

**Site Total: 6.10% - MPE% in full compliance**

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 82 North Eaglesville Road, Storrs, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the cellular band (850 MHz Band) is approximately  $567 \mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the 1900 MHz and 2500 MHz bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 82 North Eaglesville Road, Storrs, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 7 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20, RFS APXV9ERR18-C-A20 and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXV9ERR18-C-A20 has a 14.9 dBd gain value at its main lobe at 1900 MHz and 11.9 dBd at its main lobe for 850 MHz. The RFS APXV9TM14-ALU-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antenna mounting height centerline for the proposed antennas is **247 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

Site ID	CT03XC214 - U-Conn
Site Address	82 North Eaglesville Road, Storrs, CT, 06269
Site Type	Self Support Tower

Sector 1															
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	Antenna analysis height	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
1a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	7	140	5.9	247	241	1/2 "	0	485.43	0.30%
1a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	247	241	1/2 "	0	39.00	0.04%
1B	RFS	APXV9TM14-ALU-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	247	241	1/2 "	0	138.69	0.15%
Sector total Power Density Value:													0.49%		

Sector 2															
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	Antenna analysis height	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
2a	RFS	APXV9ERR18-C-A20	RRH	1900 MHz	CDMA / LTE	20	7	140	4.9	247	241	1/2 "	0	385.59	0.24%
2a	RFS	APXV9ERR18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	1.9	247	241	1/2 "	0	27.61	0.03%
2B	RFS	APXV9TM14-ALU-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	247	241	1/2 "	0	138.69	0.15%
Sector total Power Density Value:													0.42%		

Sector 3															
Antenna Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain (10 db reduction)	Antenna Height (ft)	Antenna analysis height	Cable Loss (dB)	Additional Loss (dB)	ERP	Power Density Percentage
3a	RFS	APXVSP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	7	140	5.9	247	241	1/2 "	0	485.43	0.30%
3a	RFS	APXVSP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	247	241	1/2 "	0	39.00	0.04%
3B	RFS	APXV9TM14-ALU-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	247	241	1/2 "	0	138.69	0.15%
Sector total Power Density Value:													0.49%		

Site Composite MPE %	
Carrier	MPE %
Sprint	1.41%
CT Broadcasting	1.66%
Uconn	2.14%
Uconn Fire	0.83%
T-Mobile	0.06%
<b>Total Site MPE %</b>	<b>6.10%</b>

## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are **1.41% (0.49% from sector 1, 0.42% from sector 2 and 0.49% from sector 3)** of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **6.10%** of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



Scott Heffernan  
RF Engineering Director

### **EBI Consulting**

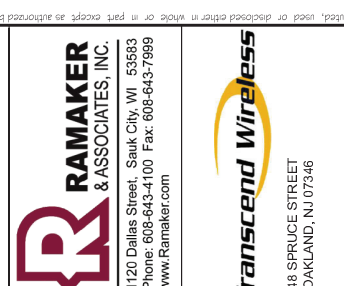
21 B Street  
Burlington, MA 01803





**SECTION 01 100 - SCOPE OF WORK**

**THE WORK:**  
 THE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE CONSTRUCTION DRAWINGS AND THE CONDITIONS OF CONTRACT SHALL BE THE BASIS FOR THE WORK. ALL WORK SHALL BE PERFORMED BY THIS CONSTRUCTION CONTRACTOR (SITTER).  
**RELATED DOCUMENTS:**  
 A. ALL CITY ORDINANCES, ORDINANCES, LOCAL ORDINANCES, ORDINANCES, ORDINANCES, ORDINANCES AND ALL APPLICABLE CODES AND STANDARDS.  
 B. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.  
 C. ALL CITY ORDINANCES, ORDINANCES, LOCAL ORDINANCES, ORDINANCES, ORDINANCES, ORDINANCES AND ALL APPLICABLE CODES AND STANDARDS.  
 D. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.  
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 T. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.  
 U. ALL CITY ORDINANCES, ORDINANCES, LOCAL ORDINANCES, ORDINANCES, ORDINANCES, ORDINANCES AND ALL APPLICABLE CODES AND STANDARDS.  
 V. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.  
 W. ALL CITY ORDINANCES, ORDINANCES, LOCAL ORDINANCES, ORDINANCES, ORDINANCES, ORDINANCES AND ALL APPLICABLE CODES AND STANDARDS.  
 X. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.  
 Y. ALL CITY ORDINANCES, ORDINANCES, LOCAL ORDINANCES, ORDINANCES, ORDINANCES, ORDINANCES AND ALL APPLICABLE CODES AND STANDARDS.  
 Z. ALL DRAWINGS, SPECIFICATIONS, CONTRACTS AND ADDENDUMS.



SECTION 01 200 - COMPANY FURNISHED MATERIAL AND EQUIPMENT  
 COMPANY FURNISHED MATERIALS AND EQUIPMENT TO BE INSTALLED BY THE CONTRACTOR (IF APPLICABLE) SHALL BE IDENTIFIED ON THE "B" DATA SHEET IN THE CONSTRUCTION DOCUMENTS.  
 RECEIPT OF MATERIAL AND EQUIPMENT:  
 A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING MATERIAL AND EQUIPMENT AND UPON RECEIPT OF THE MATERIAL AND EQUIPMENT, THE CONTRACTOR SHALL:  
 1. VERIFY QUANTITIES AND CONDITION OF ALL DELIVERIES.  
 2. VERIFY DIMENSIONS FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN THE CONTRACT DOCUMENTS.  
 3. RECORD ANY DEFECTS OR DAMAGES WITHIN TWENTY-FOUR HOURS AFTER RECEIPT, REPORT TO THE CONTRACTOR AND PROVIDE PROTECTED WAREHOUSING.  
 4. PROVIDE SECURE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND UNLOADING FROM CONTRACTORS WAREHOUSE TO SITE.  
 5. DELIVERABLES:  
 A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.  
 B. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.  
 C. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.  
 D. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.  
 E. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.  
 F. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.



**SECTION 01 400 - TESTS, INSPECTIONS, SUBMITTALS, AND PROJECT CLOSEOUT**  
**TESTS AND INSPECTIONS:**  
 A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.  
 B. CONTRACTOR SHALL ACCOMPANY TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:  
 1. CONW SWEAP AND FIBER TESTS PER ITS-0200 (CURRENT VERSION) ANTENNA LINE ACCEPTANCE.  
 2. POST CONSTRUCTION HEIGHT VERIFICATION, AZIMUTH AND DOWN TILT USING ELECTRONIC LEVELING TOOLS.  
 3. COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.  
 4. SITE RESISTANCE TO EARTH TEST.  
 5. STRUCTURAL BACKFILL COMPACTION TESTS  
 6. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS DEFECTIVE OR UNACCEPTABLE.  
 7. ADDITIONAL TESTING AS REQUIRED ELSEWHERE IN THIS SPECIFICATION.  
**EXEMPTIONS:**  
 A. THE CONTRACTOR SHALL COPY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.  
 B. UPDATES TO THE FOLLOWING SITEMAP AS APPLICABLE INCLUDING BUT NOT LIMITED TO THE FOLLOWING:  
 1. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.  
 2. CHEMICAL GROUNDING SYSTEM.  
 3. STRUCTURAL BACKFILL TEST RESULTS  
 4. SWEAP AND FIBER TEST RESULTS  
 5. ANTENNA AZIMUTH AND DOWN-TILT VERIFICATION  
 6. ADDITIONAL SUBMITTALS MAY BE REQUIRED FOR SPECIAL CONSTRUCTION OR MINOR MATERIALS ALTERNATES, AT THE COMPANY'S REQUEST, ANY ALTERNATE TO THE MATERIALS OR METHODS IDENTIFIED IN THE CONSTRUCTION DOCUMENTS SHALL BE SUBMITTED TO THE COMPANY AND BEING SHIPPED TO SITE. SITEMAP WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.  
**TESTING BY THIRD PARTY AGENCY:**  
 A. EMPLOYMENT OF REGISTERED ENGINEERS AND SCIENTISTS WHO IS REGULARLY ENGAGED IN FIELD AND LABORATORY TESTING AND ANALYSIS WORK SHALL HAVE BEEN IN BUSINESS A MINIMUM OF FIVE YEARS AND SHALL BE SUBJECT TO APPROVAL BY COMPANY.  
 B. AGENCY MUST HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING MATERIALS TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.  
 C. DIFFERENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM METHODS SHALL BE USED.  
 D. REQUIRED THIRD PARTY TESTS:  
 1. SITE RESISTANCE TO EARTH TEST PER NF-760-500  
 2. STANDARDS  
 3. STRUCTURAL SOILS COMPACTION TESTS PER TOWER-PILE AND ANCHORS PER NATIONALLY RECOGNIZED STANDARDS  
 4. REBAR PLACEMENT VERIFICATION WITH REPORT  
 5. MICROVAVE LINK TESTS PER NF-760-500  
 6. ALL THIRD PARTY TESTS AS REQUIRED BY LOCAL JURISDICTION  
 C. REQUIRED TESTS BY CONTRACTOR:  
 1. SWEAP AND FIBER TESTS PER STANDARD BLOS-649  
 2. FIBER TESTS PER SPRINT STANDARD BLOS-649  
 3. MICROVAVE LINK TESTS PER NF-760-500  
 4. ANTENNA AZIMUTH AND DOWN TILT USING ELECTRONIC ALIGNMENT TOOL PER ANTENNA INSULATION SPECIFICATION PER TOWER-PILE AND ANCHORS PER NATIONALLY RECOGNIZED STANDARDS



**SECTION 01 300 - CELL SITE CONSTRUCTION**  
 NOTICE TO PROCEED:  
 A. WORK SHALL BE PROCEEDED PRIOR TO COMPANY'S ISSUANCE OF THE WORK ORDER.  
 B. UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.  
**GENERAL REQUIREMENTS FOR CONSTRUCTION:**  
 A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH, AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING WASTE MATERIAL, DEBRIS, AND TRASH, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:  
 B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF HAZARDOUS DEBRIS.  
 C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.  
 1. IF ANY CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN IDENTIFIED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESTARTED UNTIL THE CONTRACTOR HAS OBTAINED APPROVAL FROM THE COMPANY.  
 2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD. SHOULD AREAS OUTSIDE THE CONTRACTOR'S CONTROL BE AFFECTED BY HAZARDOUS CONDITIONS, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION.  
**FUNCTIONAL REQUIREMENTS:**  
 A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCEDURES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. CONTRACTOR SHALL TAKE ALL ACTIONS AS NECESSARY TO COMPLETE THE WORK AND TO MAINTAIN THE WIRELESS FACILITY.  
 B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED THEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS IN PROGRESS.  
 C. CHANGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES.  
 D. PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:  
 1. MATERIALS STORAGE AND HANDLING, MATERIALS STORAGE AND HANDLING.  
 2. SURFACE GRADING, SITE, PROVIDE GRUBBING, AND ROUGH AND FINAL GRADING, AND COMPOUND PREPARE TREATMENTS.  
 3. MAINTAIN RECORDS FOR ALL UTILITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELEPHONE, TELEPHONE, CABLE, AND MICROVAVE.  
 4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.  
 5. PROVIDE EARTHWORK, DRAINAGE, AND BARRIERS, CURBS, AND BENCHES.  
 6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.  
 7. INSTALL "H-FRAMES", CABINETS AND PAIS AND PLATFORMS AS INDICATED.  
 8. INSTALL ROADS, ACCESS WAYS, CURBS AND BENCHES AS INDICATED.  
 9. CALCULATION REQUIRED VERIFICATION OF EXISTING FACILITIES.

PRODUCT TITLE: U-CONN CTO3XC2 14-P

PROJECT INFORMATION:  
 82 NORTH EAGLEVILLE ROAD STORRS, CT 062269 TOLLAND COUNTY

DATE ISSUED: 02/09/2015

PHASE	FINAL	DATE	DESCRIPTION
3	ISSUED		ISSUED

SCALE: NONE

23003

SIP-1





**SUPPORTING DEVICES:**

- INSTALL SUPPORTING DEVICES TO FASTEN ELECTRICAL COMPONENTS SECURELY AND PERMANENTLY IN ACCORDANCE WITH NEC.
- COORDINATE WITH THE BUILDING STRUCTURAL SYSTEM AND WITH OTHER TRADES.
- UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FASTEN ELECTRICAL ITEMS AND THEIR SUPPORTING HARDWARE SECURELY TO THE STRUCTURE IN ACCORDANCE WITH THE FOLLOWING:
  - ENSURE THAT THE LOAD APPLIED BY ANY FASTENER DOES NOT EXCEED 25 PERCENT OF THE PROOF TEST LOAD.
  - USE VIBRATION AND SHOCK-RESISTANT FASTENERS FOR ATTACHMENTS TO CONCRETE SLABS.

**ELECTRICAL IDENTIFICATION:**

- UPDATE AND PROVIDE TYPED CIRCUIT BREAKER SCHEDULES IN THE MOUNTING BRACKET, INSIDE DOORS OF AC PANEL BOARDS WITH ANY CHANGES MADE TO THE AC SYSTEM.
- BRANCH CIRCUITS FEEDING AVIATION OBSTRUCTION LIGHTING EQUIPMENT SHALL BE CLEARLY IDENTIFIED AS SUCH AT THE BRANCH CIRCUIT PANEBOARD.

**SECTION 26 200 - ELECTRICAL MATERIALS AND EQUIPMENT**

- RIGID GALVANIZED STEEL (RGS) CONDUIT SHALL BE USED FOR EXTERIOR LOCATIONS ABOVE GROUND AND IN UNFINISHED INTERIOR LOCATIONS AND FOR UNDERGROUND RUNS. RIGID CONDUIT AND FITTINGS SHALL BE STEEL COATED WITH ZINC EXTERIOR AND INTERIOR BY THE HOT DIP GALVANIZING PROCESS. CONDUIT SHALL BE PRODUCED TO ANSI SPECIFICATIONS GOVT. FEDERAL SPECIFICATION THREADED - SET SCREW OR COMPRESSION FITTINGS WILL NOT BE ACCEPTABLE. RGS CONDUITS SHALL BE MANUFACTURED BY ALLED, REPUBLIC OR WHEATLAND.
- UNDERGROUND CONDUIT IN CONCRETE SHALL BE POLYVINYLCHLORIDE (PVC) SUITABLE FOR DIRECT BURIAL AS APPLICABLE. JOINTS SHALL BE BELLED, AND FLUSH SOLVENT WELDED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. CONDUIT SHALL BE CARBON ELECTRICAL PRODUCTS OR APPROVED EQUAL.
- TRANSITIONS BETWEEN PVC AND RIGID (RGS) SHALL BE MADE WITH PVC COATED METALLIC LONG SWEET 90-DIGREE ELBOWS.
- EMT OR RIGID GALVANIZED STEEL CONDUIT MAY BE USED IN FINISHED SPACES CONCEALED IN WALLS AND CEILINGS. EMT SHALL BE MILD STEEL, ELECTRICALLY WELDED, ELECTRO-GALVANIZED OR HOT-DIPPED IN ZINC. EMT SHALL BE MANUFACTURED BY ALLED, REPUBLIC OR WHEATLAND, OR APPROVED EQUAL. FITTINGS SHALL BE METALLIC COMPRESSION. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE.
- LIQUID TIGHT FLEXIBLE METALLIC CONDUIT SHALL BE USED FOR FINAL CONNECTION TO EQUIPMENT. FITTINGS SHALL BE METALLIC GRANTYPE COMPRESSION FITTINGS, MAINTAINING THE INTEGRITY OF THE CONDUIT. FLEXIBLE CONDUIT SHALL NOT EXCEED 6 FEET. IPMC SHALL BE PROTECTED AND SUPPORTED AS REQUIRED BY NEC. MANUFACTURERS OF FLEXIBLE CONDUITS SHALL BE CAROL, ANACONDA METAL HOSE OR UNIVERSAL METAL HOSE, OR APPROVED EQUAL.
- MINIMUM SIZE CONDUIT SHALL BE 3/4 INCH (2 INMM).

**HUBS AND BOXES:**

- AT ENTRANCES TO CABINETS OR OTHER EQUIPMENT NOT HAVING INTEGRAL THREADED HUBS PROVIDE CONDUIT TERMINATIONS TO THE EQUIPMENT USING THE MANUFACTURER'S RECOMMENDED CONDUIT AND NEOPRENE OR RINGS SHALL PROVIDE IMPACT RESISTANT 105 DEGREE C PLASTIC BUSHINGS TO PROTECT CABLE INSULATION.
- CABLE TERMINATION FITTINGS FOR CONDUIT
  - CABLE TERMINATORS FOR RGS CONDUITS SHALL BE TYPE CRC BY O-Z/GEDNEY OR EQUAL BY ROKITEC.
  - CABLE TERMINATORS FOR IPMC SHALL BE ETCO - G12075, OR MADE FOR THE PURPOSE PRODUCTS BY ROKITEC.
- EXTERIOR PULL BOXES AND PULL BOXES IN INTERIOR INDUSTRIAL AREAS SHALL BE PLATED CAST ALLOY, HEAVY DUTY, WEATHERPROOF, DUST PROOF, WITH GASKET, PLATED IRON ALLOY COVER AND STAINLESS STEEL COVER SOCKETS, CROUSE-HINDS WAB SERIES OR EQUAL.
- CONDUIT OUTLET BODIES SHALL BE PLATED CAST ALLOY WITH SIMILAR GASKET COVERS. OUTLET BODIES SHALL BE OF THE CONFIGURATION AND SIZE SUITABLE FOR THE APPLICATION, PROVIDE CROUSE-HINDS FORM 8 OR EQUAL.
- MANUFACTURER FOR BOXES AND COVERS SHALL BE HOFFMAN, SQUARE D, CROUSE-HINDS, COOPER, ADALET, APTEKON, O-Z GEDNEY, RACO, OR APPROVED EQUAL.

**SUPPLEMENTAL GROUNDING SYSTEM:**

- FURNISH AND INSTALL A SUPPLEMENTAL GROUNDING SYSTEM TO THE POTENTIAL INDICATED ON THE DRAWINGS. SUPPORT SYSTEM WITH NON-MAGNETIC STAINLESS STEEL CLIPS WITH RUBBER GROMMETS. GROUNDING CONNECTORS SHALL BE TINNED COPPER WIRE, SIZES AS INDICATED ON THE DRAWINGS. PROVIDE STRANDED OR SOLID BARE OR INSULATED CONDUCTORS EXCEPT AS OTHERWISE NOTED.
- SUPPLEMENTAL GROUNDING SYSTEM: ALL CONNECTIONS TO BE MADE WITH CAD WELDS, EXCEPT AT EQUIPMENT USE LUGS OR OTHER AVAILABLE GROUNDING MEANS AS REQUIRED BY MANUFACTURER, AT GROUND BARS USE TWO HOLE SPACERS WITH INCOG.
- STOLEN GROUND BARS: IN THE EVENT OF STOLEN GROUND BARS, CONTACT SPRINT CM FOR REPLACEMENT INSTRUCTION USING THREADED ROD KITS.

**EXISTING STRUCTURE:**

- EXISTING PIPING AND ALL EXPOSED OUTLETS, RECEPTACLES, SWITCHES, DEVICES, BOXES, AND OTHER EQUIPMENT THAT ARE NOT TO BE UTILIZED IN THE COMPLETED PROJECT SHALL BE REMOVED OR DE-ENERGIZED AND CAPPED IN THE WALL, CEILING, OR FLOOR SO THAT THEY ARE CONCEALED AND SAFE. WALL, CEILING, OR FLOOR SHALL BE PATCHED TO MATCH THE ADJACENT CONSTRUCTION.

**CONDUIT AND CONDUCTOR INSTALLATION:**

- CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED, NON-PERFORATED STRAPS AND HANGERS. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND MAINTAIN PROXIMITY TO THE STRUCTURE. CONDUITS SHALL BE INSTALLED IN A MANNER THAT WILL NOT BE DAMAGED BY THE STRUCTURE. CONDUITS SHALL BE INSTALLED IN A MANNER, PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES. ALL CONDUIT SHALL BE FINISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED TO PREVENT GALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCATIONS OUTSIDE AND INSIDE.
- CONDUCTORS SHALL BE RULLED IN ACCORDANCE WITH ACCEPTED GOOD PRACTICE.

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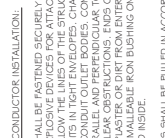


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Phone: 608-643-4100 Fax: 608-643-7999  
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OAKLAND, NJ 07346

Certification # State  
I hereby certify that I am a duly Licensed Professional Engineer under the laws of the State of Connecticut.



James P. Skowronski  
Professional Engineer  
2009/2015

MARKS	DATE	DESCRIPTION
3	2/20/14	FINAL CD'S ISSUED
PHASE	FINAL	DATE ISSUED: 02/09/2015

PROJECT TITLE:  
U-CONN  
CTO3XC2 I 4-P

PROJECT INFORMATION:  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 06269  
TOLLAND COUNTY

SHEET TITLE:  
SPRINT SPECIFICATIONS

SCALE: NONE

PROJECT NUMBER: 23003  
SHEET NUMBER: SP-3





**Sprint**  
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OAKLAND, NJ 07346

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**STATE OF CONNECTICUT PROFESSIONAL ENGINEER**  
JAMES P. SKOWRUP  
26266  
DATE ISSUED: 02/09/2015  
SYMBOL: [Signature]

NO.	DATE	DESCRIPTION
3	02/09/14	FINAL CD'S ISSUED

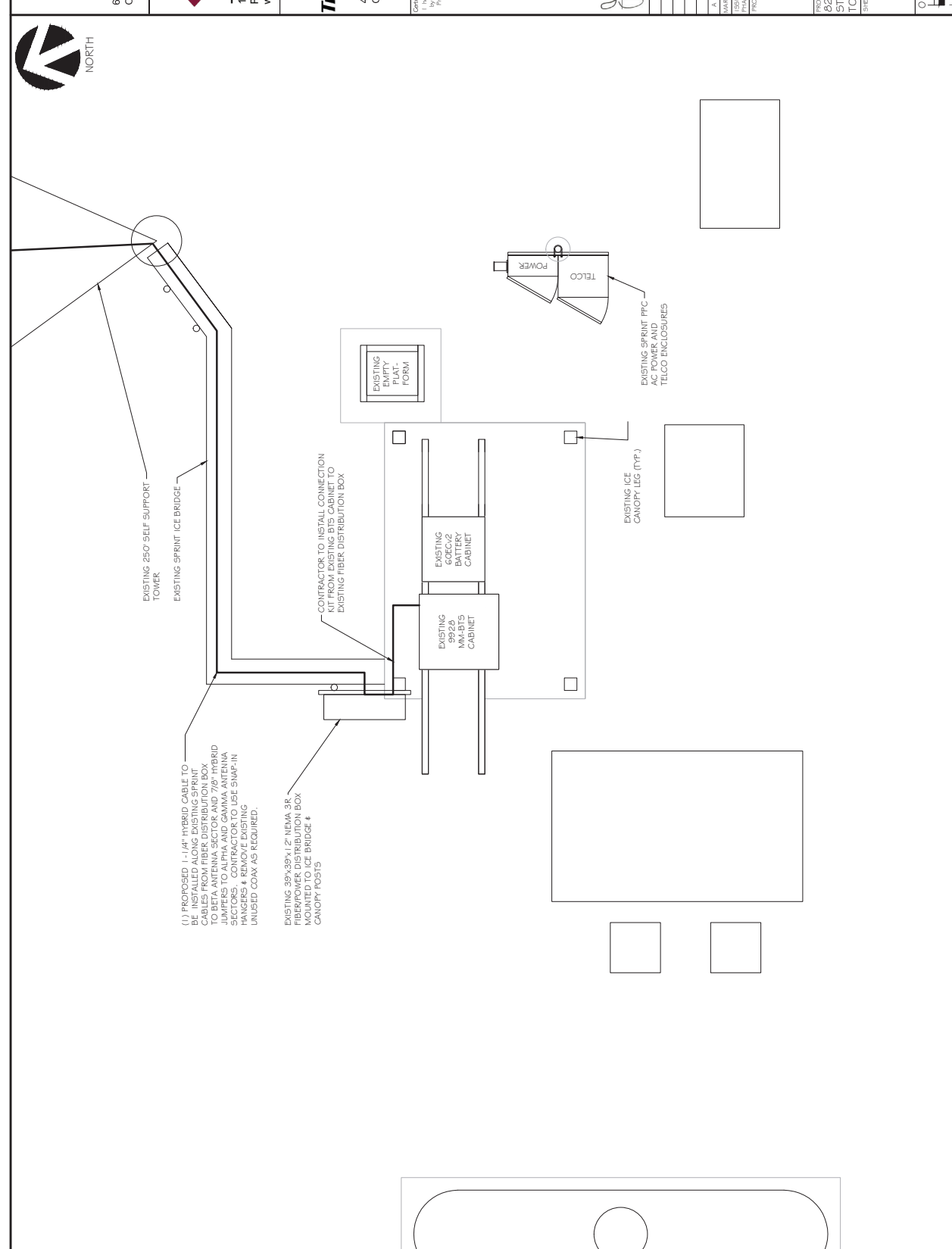
PHASE: FINAL      DATE ISSUED: 02/09/2015  
PROJECT TITLE:  
**U-CONN**  
**CT03XC2 I4-P**

PROJECT INFORMATION:  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 062269  
TOLLAND COUNTY

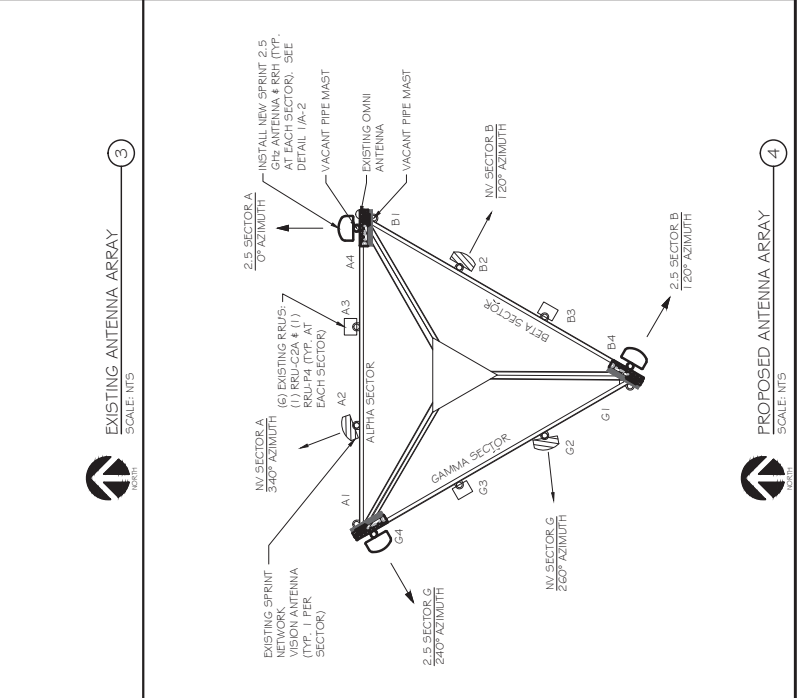
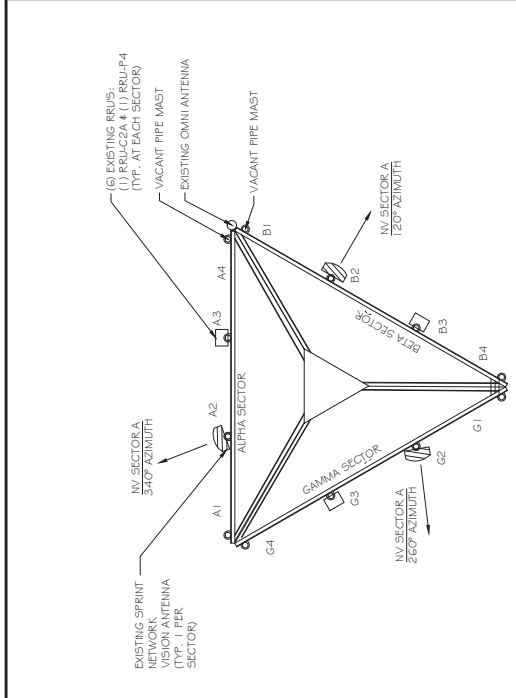
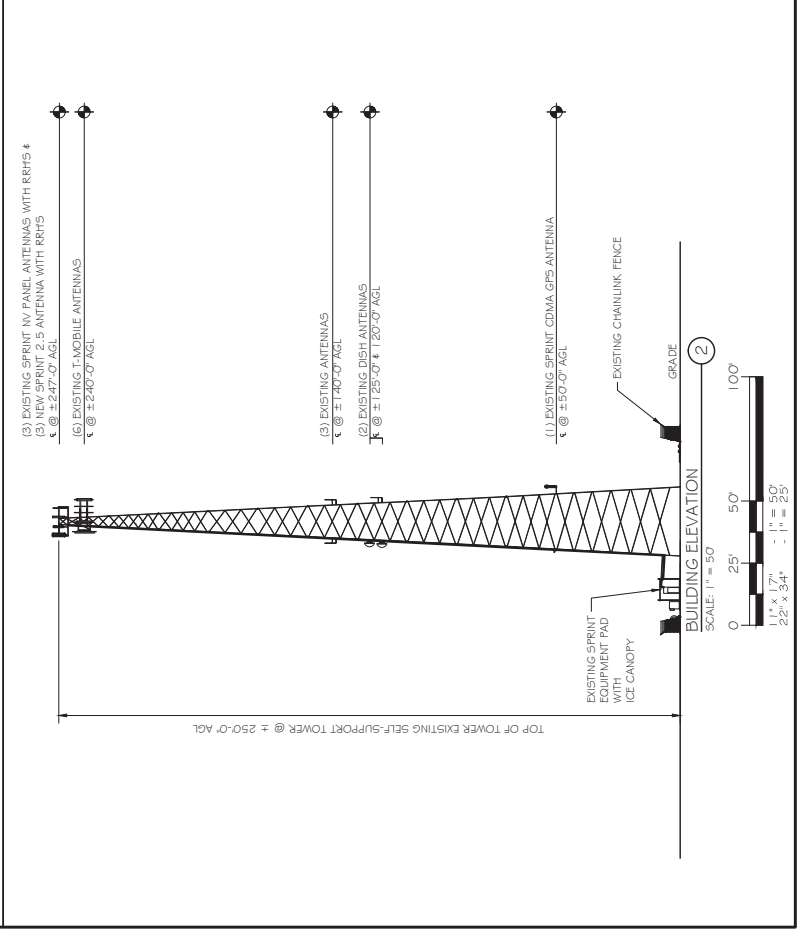
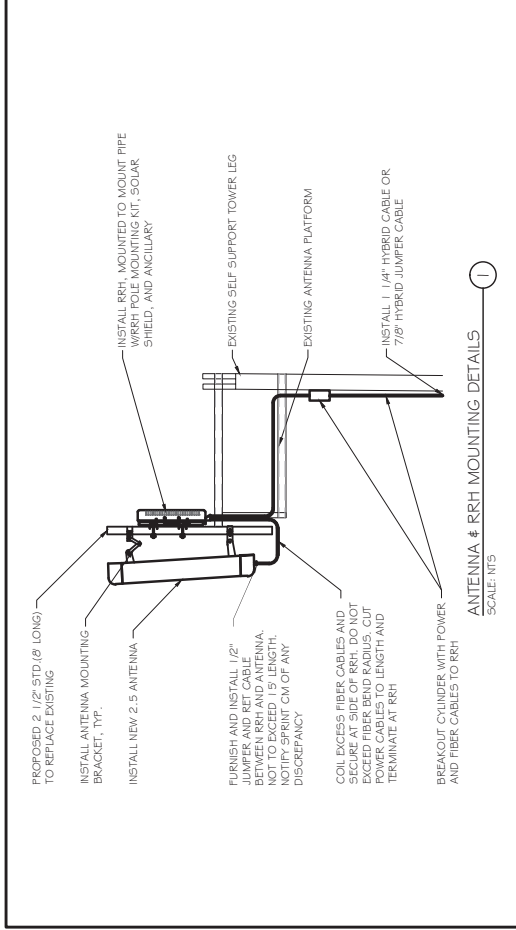
SHEET TITLE:  
**EQUIPMENT PLAN**

0 1.875' 3.75' 7.5'  
1" = 17'      1" = 3.75'  
22" x 34"      1" = 1.675'

SHEET NUMBER: **23003**  
A-2



**EQUIPMENT PLAN**  
SCALE: 1" = 3.75'



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 OAKLAND, NJ 07346

Continuation of State of Wisconsin Professional Engineer License No. 262686  
 James P. Skowronski  
 State of Wisconsin Professional Engineer License No. 262686  
 State of Connecticut Professional Engineer License No. 262686  
 State of Kansas Professional Engineer License No. 262686

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 State of Kansas Professional Engineer License No. 262686

NO.	DATE	DESCRIPTION
3	02/09/2015	FINAL
2	02/09/2015	ISSUED FOR PERMIT
1	02/09/2015	ISSUED FOR PERMIT

PROJECT INFORMATION:  
 U-CONN  
 CTO3XC2 14-P  
 82 NORTH EAGLEVILLE ROAD  
 STORRS, CT 062269  
 TOLLAND COUNTY

SHEET TITLE:  
 BUILDING ELEVATIONS & ANTENNA DETAILS

SCALE:  
 AS NOTED

PROJECT NUMBER: 23003  
 SHEET NUMBER: A-3

**RFDS Sheet**

**General Site Information**

Site ID	CT03XC214
Market	Northern Connecticut
Region	Northeast
M/A	N/A
Structure Type	Guyed tower
BTS Type	

Equipment Vendor	Alcatel-Lucent
Latitude	41.81436
Longitude	-72.26033
LL SITE ID	N/A

Solution ID	
Siterra SR Equipment type	Alcatel-Lucent
Equipment Vendor	Alcatel-Lucent
Incremental Power Draw needed by added Equipment	N/A

**Base Equipment**

BBU Kit	ALU BBU Kit	Top Hat	None
BBU Kit Qty	1	Top Hat Qty	N/A
Growth Cabinet		Top Hat Dimensions	N/A
Growth Cabinet Qty	None	Top Hat Weight (lbs)	N/A
Growth Cabinet Dimensions			
Growth Cabinet Weight			

**RF Path Information**

RRH	TD-RRH820-25
RRH Qty	3
RRH Dimensions	26.1"x18.6"x6.7"
RRH Weight, lbs.	70
RRH Mount Weight, lbs.	10
Power and Fiber Cable	ALU Hybrid Cable
Cable Qty	1
Weight per foot, lbs.	0.992
Diameter, inches.	1.25
Length Ft.	324
Coax Jumper	5/8"
Coax Jumper Qty	27
Coax Jumper Length, Feet.	8
Coax Jumper Weight	1.7
Coax Jumper Diameter, Inches	0.5
AISG Cable	COMMSCOPE ATCB-B01-006
AISG Cable Qty	3
AISG Diameter, Inches.	0.315
AISG Cable length, Feet.	8
Weight of entire AISG cable, lbs.	1.3

**Antenna Sector Information**

Antenna make/model	Sector 1	Sector 2	Sector 3
Antenna qty	1	1	1
Antenna Dimensions, inches	56.3"x12.6"x6.3"	56.3"x12.6"x6.3"	56.3"x12.6"x6.3"
Antenna Weight, lbs	55.12	55.12	55.12
Antenna Mounting Kit Weight, lbs.	11.5	11.5	11.5
CL Height	247	247	247
Antenna Azimuth	0	120	240
Antenna Mechanical Downtilt	0	0	0
Antenna etilt	-2	-2	-2

**NOTES:**

- GENERAL CONTRACTOR TO FIELD VERIFY AZIMUTH AND CL HEIGHT AND MECHANICAL DOWNTILT. IF DIFFERENT THAN CALLED OUT BELOW, CONTRACTOR SHALL WORK FOR CORRECTION. CONTRACTOR SHALL BE RESPONSIBLE FOR A MESSAGE TO RF ENGINEER USING CONTACT INFORMATION PROVIDED IN THESE DRAWINGS. IF SPRINT DOES NOT RESPOND WITHIN ONE HOUR, PLACE 2.5GHZ ANTENNA AT SAME CL HEIGHT AS 1.9GHZ ANTENNA AND SWAL CORRECT CL HEIGHT AS-BUILT DRAWING WITH CORRECT CL HEIGHT. ALSO EMAIL CORRECT 1.9GHZ AND 2.5GHZ ANTENNA CL, AZIMUTH AND MECHANICAL DOWNTILT TO RF ENGINEER.
- ALSO TESTS TO VERIFY OPERATION IS TO BE ANTENNAS AND AISG CABLES HAVE BEEN CONNECTED. VERIFY OPERATION OF ALL EXISTING SPRINT AISG EQUIPMENT AND TEST TO VERIFY OPERATION OF ALL NEW TEST TO INCLUDE COMPLETE DOWNTILT, AZIMUTH (IF APPLICABLE) AND BEAMWIDTH SWINGS (IF APPLICABLE). DOCUMENT AISG TEST RESULTS IN COAX SHEET TEST SPREADSHEET.
- GENERAL CONTRACTOR MUST INSURE THAT NO COAX CABLES ARE PLACED IN FRONT OF, AND RIGHT OF FRONT OF ANTENNA OR 7 DEGREES UP AND DOWN FROM CENTER OF ANTENNA. IF THIS IS NOT POSSIBLE, CONTACT RF ENGINEER FOR FURTHER INSTRUCTIONS. ALL ANTENNAS MUST BE PLACED IN FRONT OF ANY OTHER ANTENNA USING THE SAME 45 DEGREE RULE. THIS INCLUDES SPRINT AND NON-SPRINT ANTENNS.
- 2.5GHZ ANTENNA MUST BE AT LEAST 6' FROM 1.9GHZ ANTENNA, 30' FROM 800MHZ ANTENNA AND 30' FROM DUAL BAND 1.9GHZ AND 800MHZ ANTENNA.
- GENERAL CONTRACTOR IS REQUIRED TO USE A DIGITAL DOWNTILT ANTENNA WITH A DIGITAL DOWNTILT ACCURACY (S) TO BE WITHIN 1 DEGREE. DOWNTILT AND ROLL (LEFT TO RIGHT TILT) IS TO BE WITHIN 0.1 DEGREES. IF FOR SOME REASON ANTENNA DOES NOT MEET THESE REQUIREMENTS, CONTACT RF ENGINEER FOR FURTHER INSTRUCTIONS. CONTRACTOR SHALL VERIFY AND OBTAIN FINAL RFDS FROM SPRINT CONSTRUCTION MANAGER PRIOR TO CONSTRUCTION.



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 OAKLAND, NJ 07346

Contractor's Seal  
 James P. Skowronski, PE  
 Professional Engineer under the laws of the State of Connecticut



James P. Skowronski  
 02/09/2015

NO. 3	REVISION	REVISION	DATE	02/09/2015
NO. 2	ISSUED FOR PERMIT	ISSUED FOR PERMIT	DATE	02/09/2015
NO. 1	ISSUED FOR PERMIT	ISSUED FOR PERMIT	DATE	02/09/2015

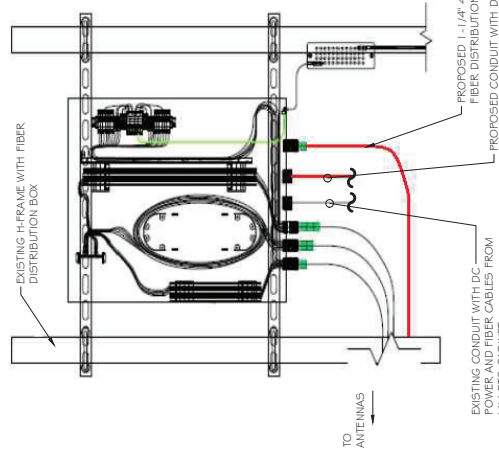
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PROJECT INFORMATION:  
 82 NORTH EAGLEVILLE ROAD  
 STORRS, CT 062269  
 TOLLAND COUNTY

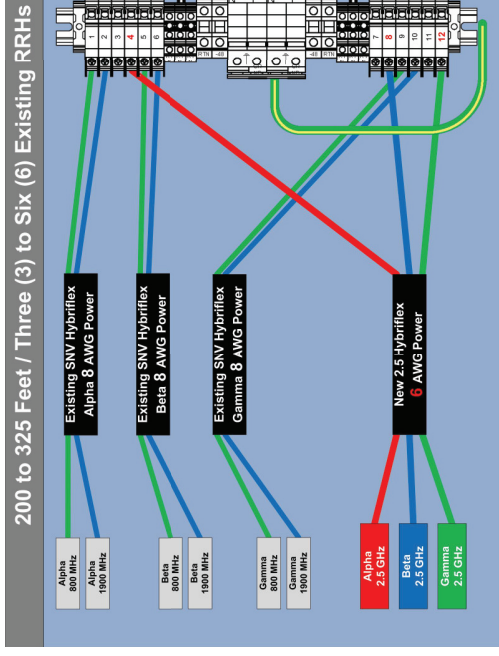
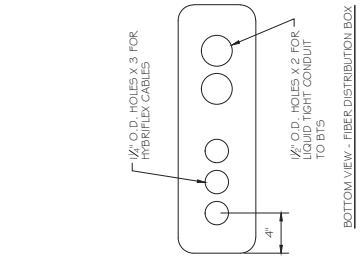
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 RF DATA SHEET

SCALE:  
 AS NOTED

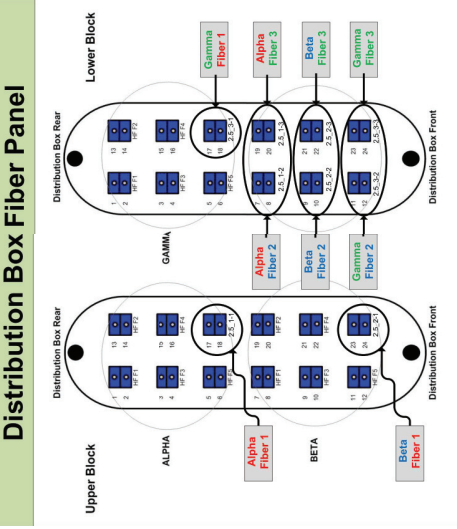
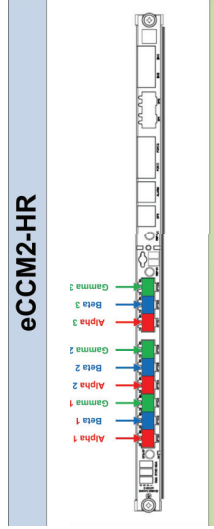
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 SHEET NUMBER  
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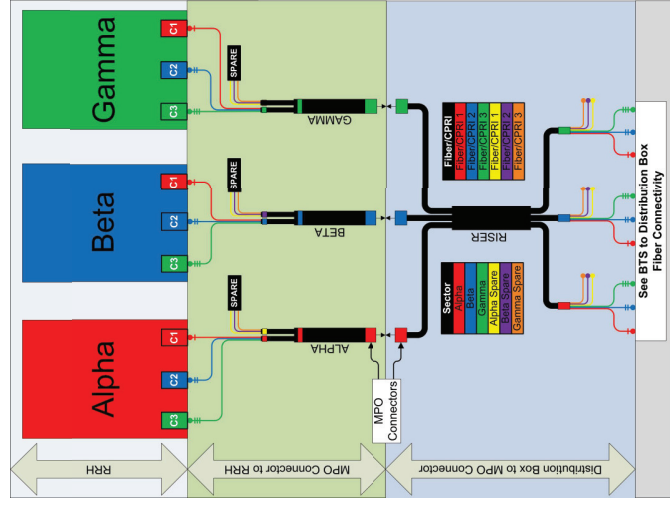
TYPICAL FIBER DISTRIBUTION BOX DETAIL  
 SCALE: NT5



RRH TO DISTRIBUTION BOX POWER CONNECTIVITY DETAIL  
 SCALE: NT5



BT5 TO DISTRIBUTION BOX FIBER CONNECTIVITY DETAIL  
 SCALE: NT5



RRH TO DISTRIBUTION BOX FIBER CONNECTIVITY DETAIL  
 SCALE: NT5

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 48 SPRUCE STREET  
 OAKLAND, NJ 07346

Confirmation State: WI  
 License No: 100000000  
 Professional Engineer under the laws of the State of Connecticut



James P. Skowronski  
 02/09/2015

NO.	REVISED	DATE	DESCRIPTION
3	ISSUED FOR FINAL CD'S ISSUED		
2	ISSUED FOR FINAL CD'S ISSUED		
1	ISSUED FOR FINAL CD'S ISSUED		

PROJECT TITLE:  
**U-CONN**  
**CT03XC2 I 4-P**

PROJECT INFORMATION:  
 82 NORTH EAGLEVILLE ROAD  
 STORRS, CT 06269  
 TOLLAND COUNTY

SHEET TITLE:  
**FIBER PLUMBING DIAGRAM**

SCALE:  
 AS NOTED

PROJECT NUMBER:  
 23003

DRAWING NUMBER:  
 A-5




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OAKLAND, NJ 07346



Professional Engineer under the laws of the State of Connecticut  
 26266  
 JAMES P. SKOWRODZKI  
 02/09/2015

PROJECT TITLE:  
 U-CONN  
 CT03XC2 I 4-P

PROJECT INFORMATION:  
 82 NORTH EAGLEVILLE ROAD  
 STORRS, CT 062269  
 TOLLAND COUNTY

SHEET TITLE:  
 CABLE COLOR CODING

SCALE:  
 AS NOTED

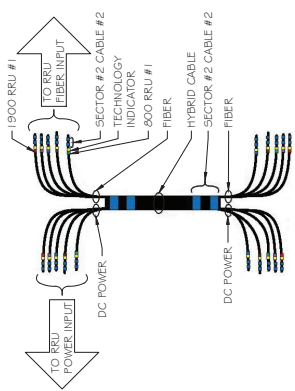
PROJECT NUMBER:  
 23003


SHEET NUMBER:  
 A-6

Sector	Cable	First Ring	Second Ring	Third Ring
1 Alpha	1	Green	No Tape	No Tape
	2	Blue	No Tape	No Tape
	3	Brown	No Tape	No Tape
	4	White	No Tape	No Tape
	5	Red	No Tape	No Tape
	6	Grey	No Tape	No Tape
	7	Purple	No Tape	No Tape
	8	Orange	No Tape	No Tape
2 Beta	1	Green	Green	No Tape
	2	Blue	Blue	No Tape
	3	Brown	Brown	No Tape
	4	White	White	No Tape
	5	Red	Red	No Tape
	6	Grey	Grey	No Tape
	7	Purple	Purple	No Tape
	8	Orange	Orange	No Tape
3 Gamma	1	Green	Green	Green
	2	Blue	Blue	Blue
	3	Brown	Brown	Brown
	4	White	White	White
	5	Red	Red	Red
	6	Grey	Grey	Grey
	7	Purple	Purple	Purple
	8	Orange	Orange	Orange


**CABLE MARKING NOTES**

- ALL CABLES SHALL BE MARKED WITH 2" WIDE, UV STABILIZED, UL APPROVED TAPE.
- THE FIRST RING SHALL BE CLOSEST TO THE END OF THE CABLE. THE SECOND RING SHALL BE AT THE END CONNECTOR, WEATHERPROOFING, OR BREAKOUT UNIT. THERE SHALL BE 1" SPACE BETWEEN EACH RING.
- A 2" GAP SHALL SEPARATE THE CABLE COLOR CODE FROM THE FREQUENCY COLOR CODE. THE 2" GAP SHALL BE MARKED WITH TAPE. THE TAPE SHALL BE PLACED NEXT TO EACH OTHER WITH NO SPACES.
- THE 2" COLORED TUBES SHALL BE MARKED A MINIMUM OF 3" TIMES AROUND THE INDIVIDUAL CABLES AND THE TAPE SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE.
- SITES WITH MORE THAN FOUR (4) SECTORS WILL REQUIRE ADDITIONAL RINGS FOR EACH SECTOR. ADDITIONAL RINGS SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE. THE TAPE WILL USE THE SECOND CABLE IDENTIFIED BY BLUE BANDS OF TAPE.
- HYBRID FIBER CABLE SHALL BE SECTOR IDENTIFIED INSIDE THE CABINET ON FREQUENCY BUNDLES ON THE SEALANTE, ON THE MAIN LINE UPON EXIT OF THE CABINET AND ON THE MAIN LINE UPON EXIT OF THE UNIT (INDOOR) AS WELL AS BEFORE AND AFTER ANY ENTRANCE OR EXIT.
- HYC MAIN TRUNKS WILL NOT BE MARKED WITH THE FREQUENCY CODES, AS IT CONTAINS ALL FREQUENCIES.
- INDIVIDUAL POWER PABS AND FIBER BUNDLES SHALL BE LABELED WITH BOTH THE CABLE AND FREQUENCY.






Example - Sector 2, Cable 2, 800mhz Radio #1



Example - Sector 3, Cable 1, 1900mhz Radio #1



Example - Sector 4, Cable 4, 800mhz Radio #1 and 1900mhz Radio #1

COLOR CODING CHARTS  
 SCALE: 1:1

2.5 FREQUENCY	INDICATOR	ID
2500 -1	YEL	GRN
2500 -2	YEL	RED
2500 -3	YEL	BRN
2500 -4	YEL	BLU
2500 -5	YEL	SLT
2500 -6	YEL	ORG
2500 -7	YEL	WHT
2500 -8	YEL	PPL

NW FREQUENCY	INDICATOR	ID
800-1	YEL	GRN
1900-1	YEL	RED
1900-2	YEL	BRN
1900-3	YEL	BLU
1900-4	YEL	SLT
800-1	YEL	ORG
RESERVED	YEL	WHT
RESERVED	YEL	PPL





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**Transcend Wireless**  
48 SPRUCE STREET  
OAKLAND, NJ 07346

Certification # State: WI  
Professional Engineer License # 26286  
Professional Engineer under the laws of the State of Connecticut.  
James P. Skowronski  
Professional Engineer  
02/09/2015



NO.	DATE	DESCRIPTION
3	02/09/15	FINAL CD'S ISSUED
2	02/09/15	ISSUED
1	02/09/15	ISSUED

**U-CONN**  
CTO3XC2 I 4-P

PROJECT INFORMATION:  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 062269  
TOLLAND COUNTY

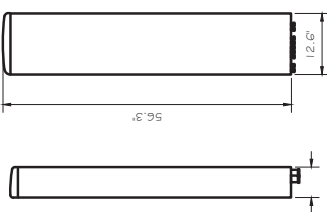
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ANTENNA & HYBRID CABLE  
DETAILS

SCALE:  
AS NOTED

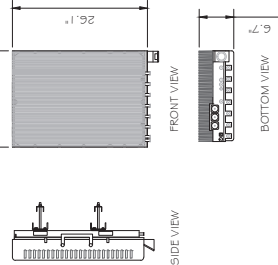
3003  
A-7

**RFS: APXV9TM I 4-ALU- I 20**

DIMENSIONS, HWAD: 56.3" x 1.2" x 6.3"  
WEIGHT, WITHOUT PRE-MOUNTED BRACKETS: 55.12 lbs.  
CONNECTOR: (9) XX" MINI-DIN FEMALE/BOTTOM



2.5 ANTENNA DETAIL  
SCALE: NTS



ALCATEL-LUCENT: TD-RRH5X20  
HWAD = (26.1" x 1.86" x 6.7")  
WEIGHT = 70 lbs.

2.5 RRH DETAIL  
SCALE: NTS

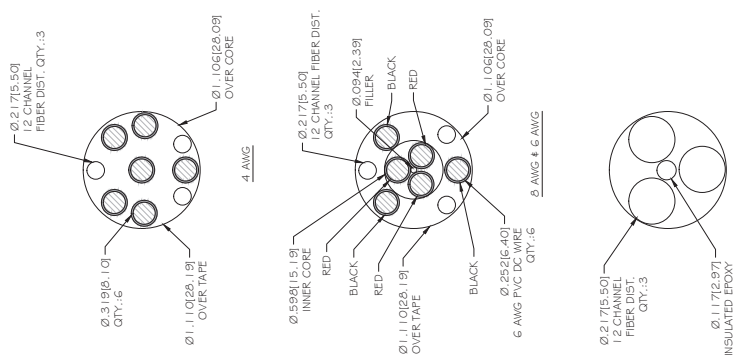
CABLE	LENGTH	DC CONDUCTOR	CABLE DIAMETER
Fiber Only	Varies	Size N/A	0.8"
Hybrid	<500'	6 AWG	1.14"
Hybrid	500-2000'	4 AWG	1.31"

Part Code	Description	Length	Notes
MNH1808R412Z00P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 200 ft.	200 ft.	
MNH1808R412Z05P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 500 ft.	500 ft.	
MNH1808R412Z10P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 1000 ft.	1000 ft.	
MNH1808R412Z15P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 1500 ft.	1500 ft.	
MNH1808R412Z20P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 2000 ft.	2000 ft.	

Part Code	Description	Length	Notes
MNH1814130M12Z00P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 200 ft.	200 ft.	
MNH1814130M12Z05P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 500 ft.	500 ft.	
MNH1814130M12Z10P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 1000 ft.	1000 ft.	
MNH1814130M12Z15P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 1500 ft.	1500 ft.	
MNH1814130M12Z20P	3x4 AWG power pairs, 12 mini-modes four pairs, Outdoor rated connectors & LC connectors, 1.14 inch cable, 2000 ft.	2000 ft.	

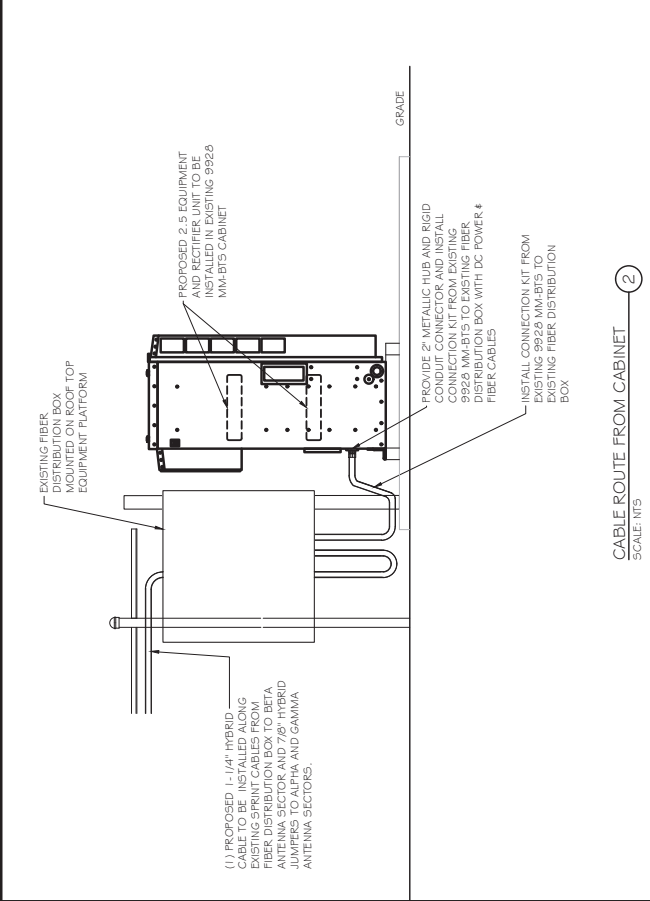
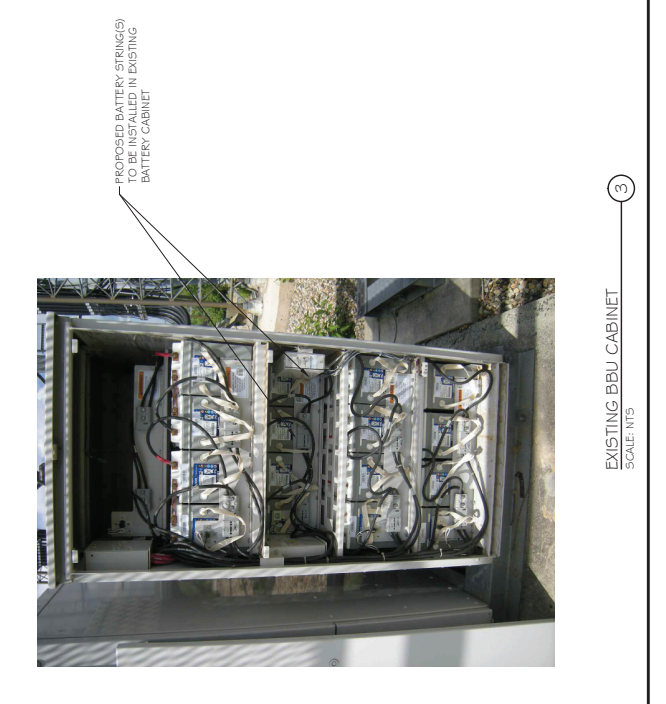
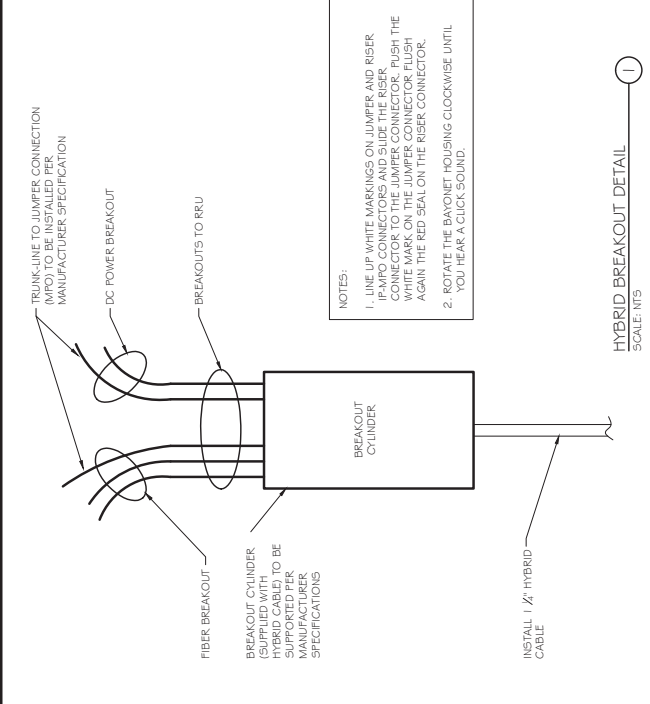


Ø 3.19(Ø 1.0) QTY: 6  
Ø 2.17(5.50) 12 CHANNEL FIBER DIST. QTY: 3  
Ø 1.10(Ø 28.19) OVER TAPE  
Ø 1.10(Ø 28.19) OVER CORE  
Ø 5.98(15.19) INNER CORE QTY: 3  
Ø 2.17(5.50) 12 CHANNEL FIBER DIST. QTY: 3  
Ø 0.94(2.39) FILLER  
BLACK OVER TAPE  
RED  
BLACK  
RED  
BLACK  
Ø 252(6.40) 6 AWG PVC DC WIRE QTY: 6  
Ø 1.10(Ø 28.19) OVER TAPE  
Ø 1.10(Ø 28.19) OVER CORE  
Ø 2.17(5.50) 12 CHANNEL FIBER DIST. QTY: 3  
Ø 1.17(2.97) INSULATED GLASS ROD

4 AWG POWER  
FIBER ONLY  
FIBER ONLY  
FIBER ONLY

NOTE: SPRINT CM TO CONFIRM HYBRID/FIBER RISER CABLE # & HYBRID/FIBER JUMPER CABLE MODEL NUMBERS BEFORE PREPARING BOM.

RISER CABLE CROSS-SECTION # DATA  
SCALE: NTS



EXISTING MMBs CABINET  
SCALE: NTS

DC Power Distribution Panel  
User Space  
Rectifiers  
AC PDA

19" User Space  
Power Injector Tray 2  
Power Injector Tray 1  
7210 SAS-M 2  
7210 SAS-M 1  
7705 SAR-F/SAR-8  
LTE BBU 2.5GHz  
PDP-1  
PDP-2  
3CC-B

Fan Tray  
Digital Shelf  
EIOU

INSTALL NEW 2.5 EQUIPMENT, INCLUDING BASE BAND UNIT, CELL SITE ROUTER, RECTIFIERS, AND AC PDA IN EXISTING MMB-BTS CABINET

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James P. Skowronski  
Professional Engineer  
02/09/2015

NO.	REVISION	DATE	DESCRIPTION
1	ISSUE	02/09/2015	FINAL
2	REVISED	02/09/2015	FINAL

**U-CONN**  
CT03XC2 I 4-P

PROJECT INFORMATION:  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 06269  
TOLLAND COUNTY

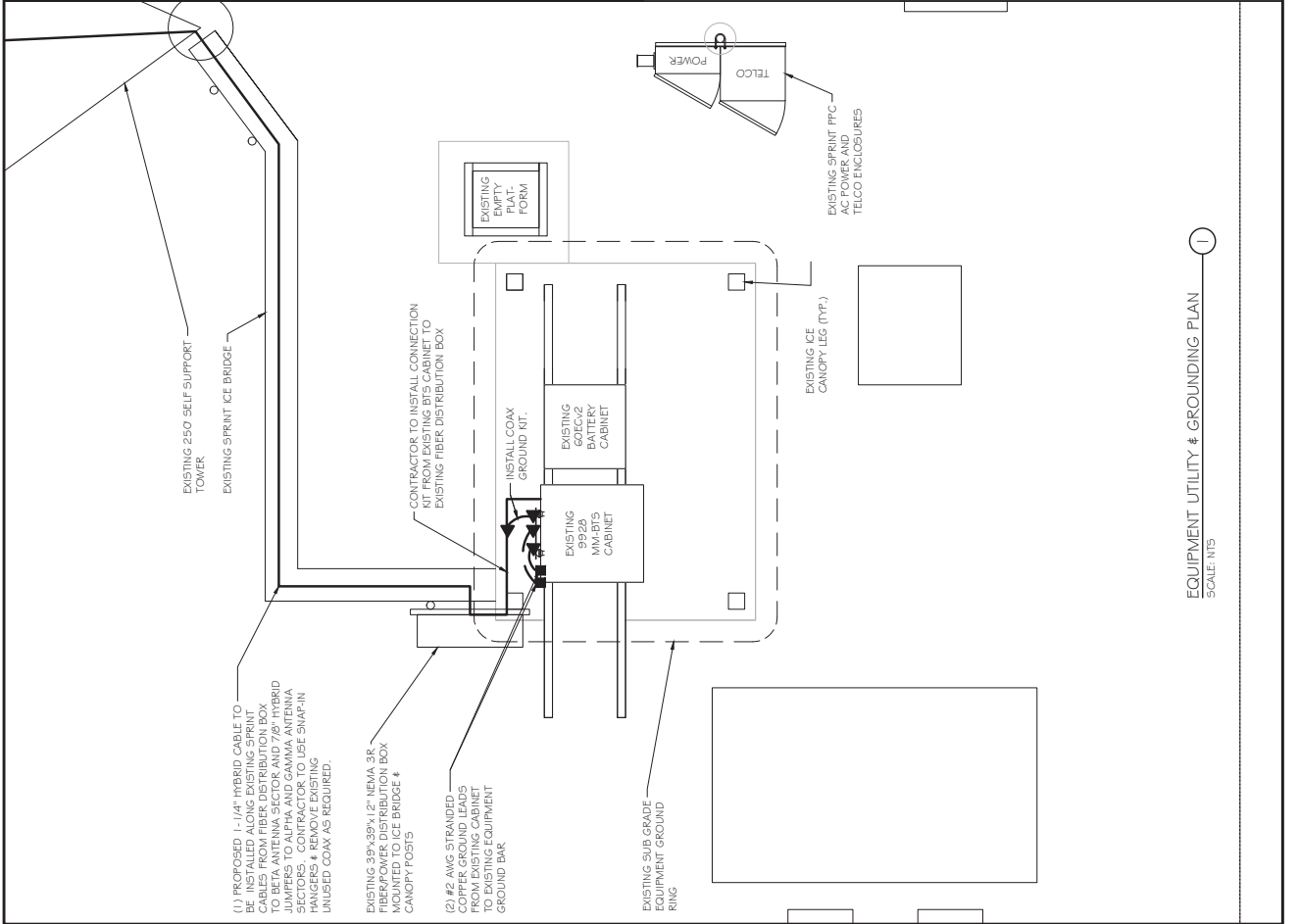
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EQUIPMENT DETAILS

SCALE:  
AS NOTED

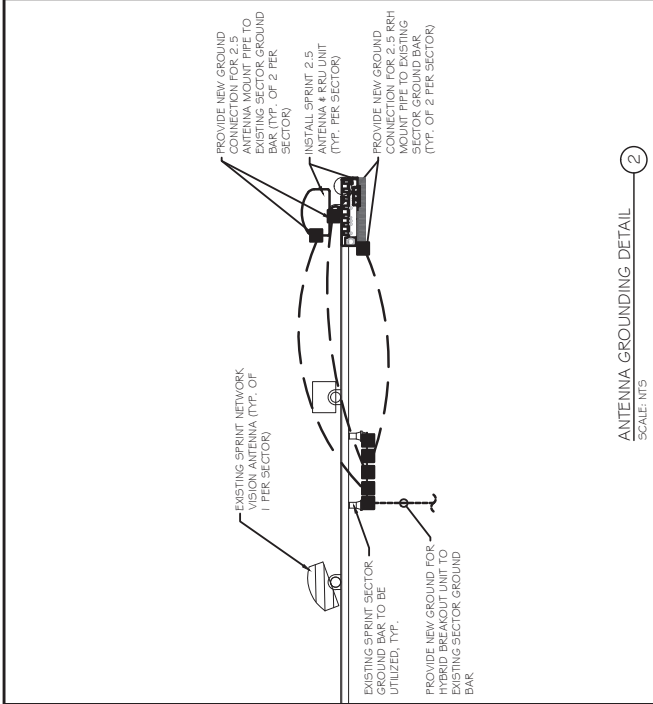
PROJECT NUMBER  
23003

SHEET NUMBER  
A-8





EQUIPMENT UTILITY & GROUNDING PLAN  
 SCALE: NTS




ANTENNA GROUNDING DETAIL  
 SCALE: NTS


- GROUNDING NOTES:**
- CONTRACTOR TO ENSURE PROPER SEQUENCING OF GROUNDING AND UNDERGROUND CONDUIT INSTALLATION TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM AND/OR DAMAGE TO THE CONDUIT.
  - ALL EXTERIOR GROUND CONDUCTORS SHALL BE #2 AWG SOLID TINNED COPPER.
  - ALL GROUNDING CONNECTIONS SHALL BE PROTECTED BY AN ANTI-OXIDATION BRAGIT FINISH AND COATED WITH AN ANTI-OXIDATION MATERIAL BEFORE CONNECTIONS ARE MADE.
  - ALL GROUND CONNECTIONS BELOW GRADE SHALL BE PROTECTIVE GALVANIZED TYPE, TWO-HOLE LUGS OR DOUBLE-CRIMP "C" TAPS.
  - ALL GROUND CONNECTIONS ABOVE GRADE AND/OR INTERIOR SHALL BE COMPRESSION TYPE. TWO-HOLE LUGS OR DOUBLE-CRIMP "C" TAPS.
  - ALL GROUND CONNECTIONS SHALL BE PREPARED TO A BASE BRAGIT FINISH AND COATED WITH AN ANTI-OXIDATION MATERIAL BEFORE CONNECTIONS ARE MADE.
  - MINIMUM RESISTANCE OF THE COMPLETED GROUND SYSTEM SHALL NOT EXCEED 5 OHMS.
  - WHERE GROUNDING CONNECTIONS ARE MADE TO PAINTED METAL SURFACES, PAINT SHALL BE REMOVED TO BARE METAL TO ENSURE PROPER CONTACT AND RESTORED TO ORIGINAL FINISH.
  - GROUND DEPTH SHALL BE 30" MINIMUM BELOW FINISHED GRADE, OR 6" BELOW FROST LINE, WHICHEVER IS GREATER.

**LEGEND:**


---	EXISTING GROUND CABLE
---	PROPOSED GROUND CABLE
▲	MECHANICAL CONNECTION
■	DIATHERMIC CONNECTION
---	PROPOSED ELECTRIC




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OAKLAND, NJ 07346



James P. Skowronski  
Professional Engineer  
2/09/2015

DATE: 02/09/2015  
 TIME: 10:00 AM  
 DRAWN BY: JLG  
 CHECKED BY: KMB  
 PROJECT TITLE: U-CONN CTO3XC2 I 4-P


PROJECT INFORMATION:  
 82 NORTH EAGLEVILLE ROAD  
 STORRS, CT 06226-9  
 TOLLAND COUNTY

SHEET TITLE:  
 EQUIPMENT UTILITY &  
 GROUNDING PLAN

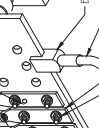
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PROJECT NUMBER:  
 23003


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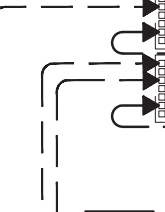


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James P. Skowronski  
Professional Engineer  
No. 26266  
State of Connecticut  
Date: 02/09/2015

MARK	DATE	DESCRIPTION
3	02/09/14	FINAL CD'S ISSUED
1	02/09/14	ISSUE
0	02/09/15	FINAL

PROJECT TITLE:  
**U-CONN  
CT03XC2 I 4-P**

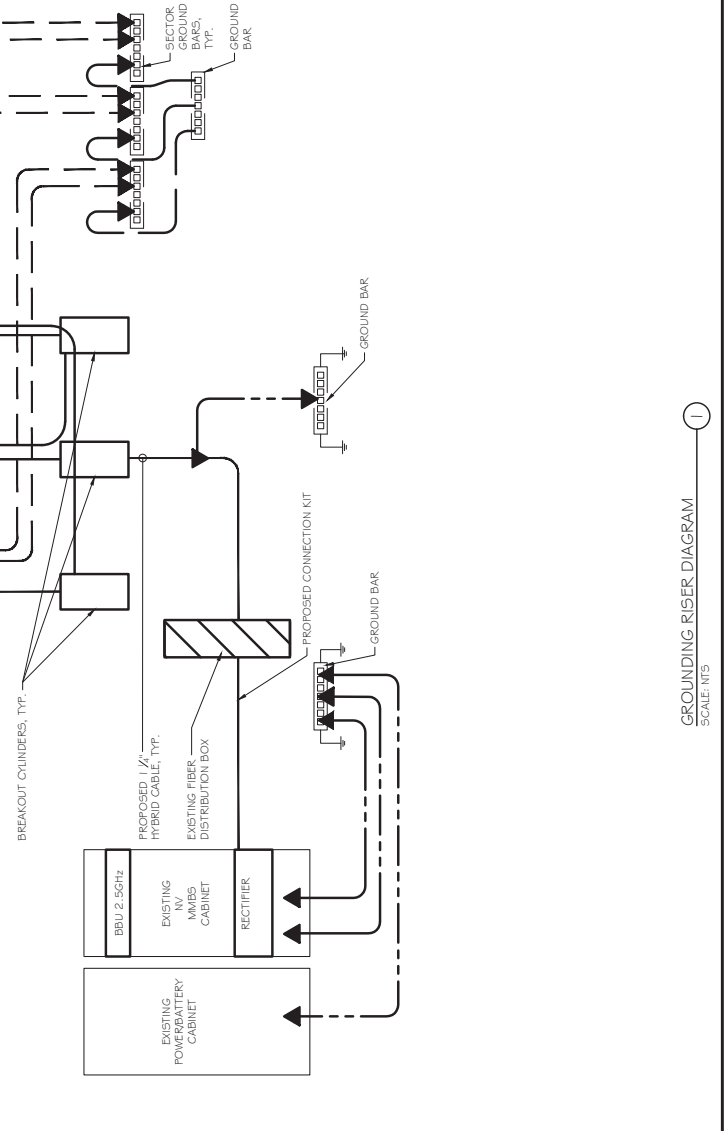
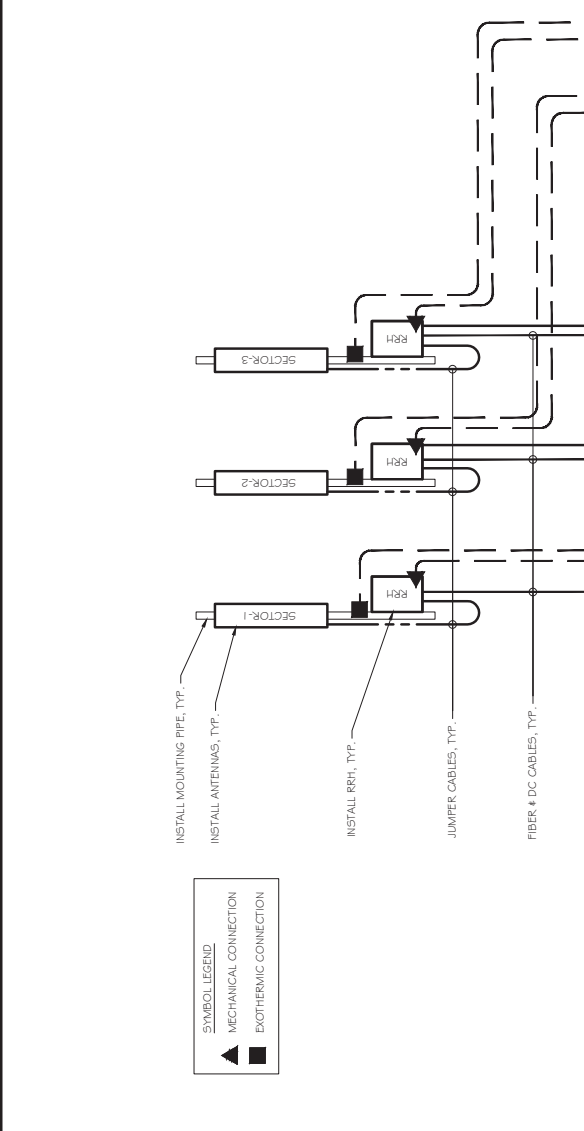
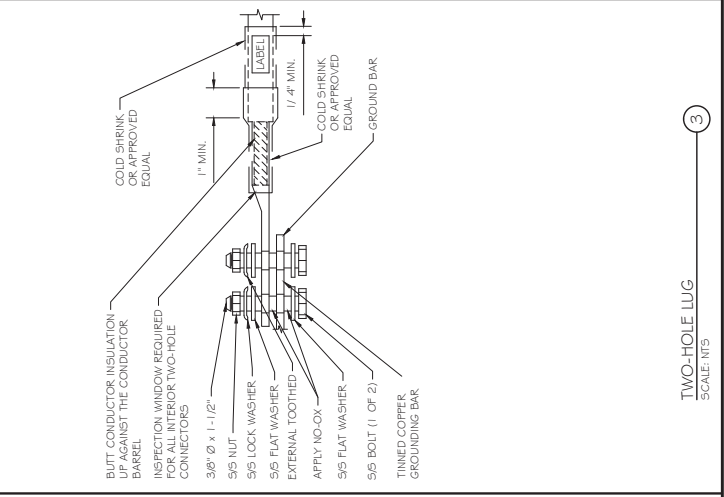
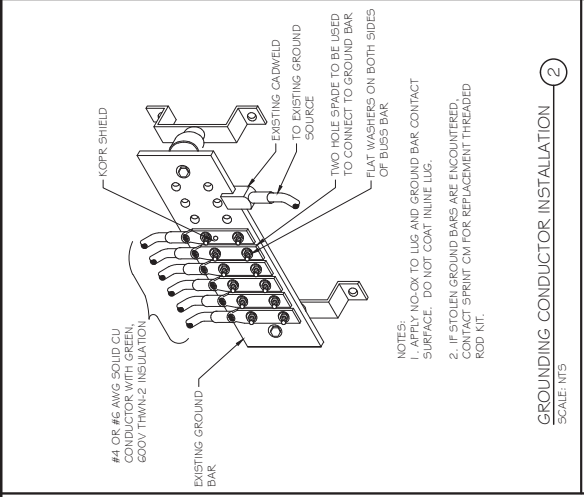
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82 NORTH EAGLEVILLE ROAD  
STORRS, CT 062269  
TOLLAND COUNTY

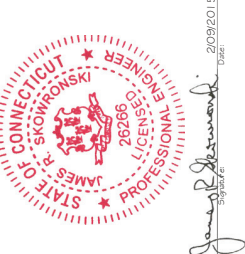
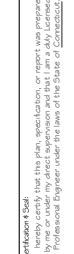
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**GROUNDING DETAILS**

SCALE:  
AS NOTED

PROJECT NUMBER:  
23003

SHEET NUMBER:  
E-2





NO.	DATE	DESCRIPTION	DATE ISSUED
3	02/09/2015	FINAL	02/09/2015

U-CONN  
CTO3XC2 I 4-P

PROJECT INFORMATION:  
82 NORTH EAGLEVILLE ROAD  
STORRS, CT 062269  
TOLLAND COUNTY

SHEET TITLE:  
DC POWER DETAILS  
& PANEL SCHEDULES

SCALE:  
AS NOTED

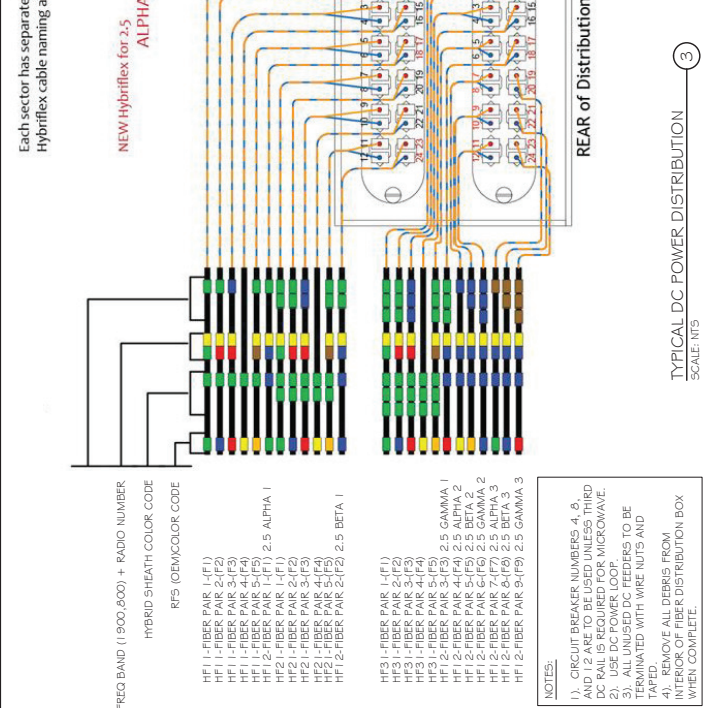
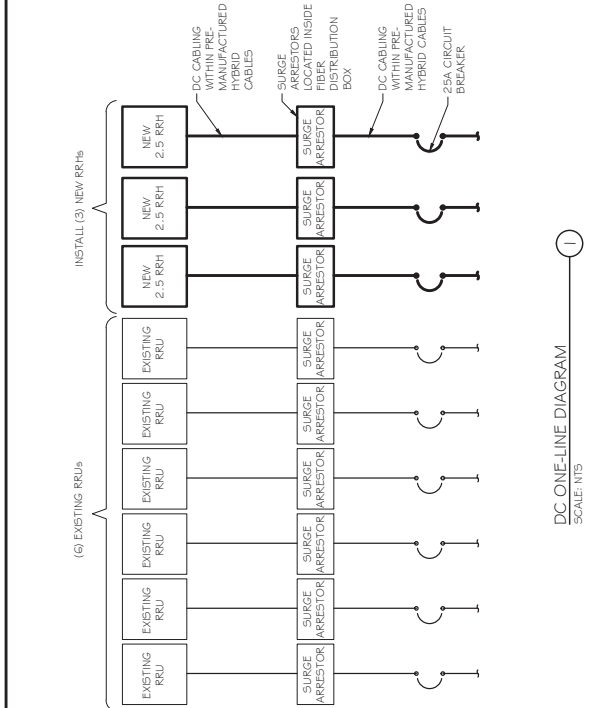
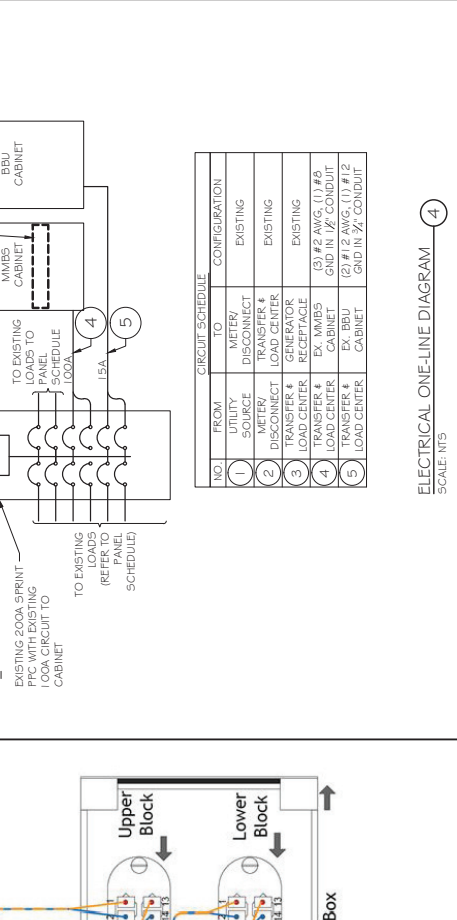
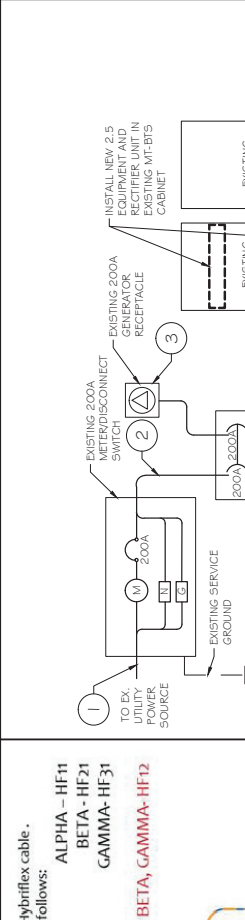
DATE: 02/09/2015

PROJECT TITLE:

**A/C PANEL SCHEDULE**

VOLTAGE:	240V/120	PANEL STATUS:	EXISTING	N TO GROUND BOND:	YES
MAIN BREAKER:	200 AMP	MODEL NUMBER:	TBD	INTERNAL TYS:	YES
MOUNT:	OUTDOOR	PHASE:	1	WIRE:	3
ENCLOSURE TYPE:	NEMA 3R	BUS RATING:	200 AMP	GROUND BAR:	YES
NEUTRAL BAR:	YES				

Ckt	DESCRIPTION	BREAKER TYPE	BREAKER AMP	PHASE	PHASE	PHASE	BREAKER	BREAKER	DESCRIPTION	Ckt
				STATUS	STATUS	STATUS	AMPS	AMPS		
1	CIRCUIT #1	80	2	OFF	ON	2	60	60	SURGE PROTECTOR	7
2										
3	CIRCUIT #2	80	2	OFF	ON	2	20	20	OVER LIGHT	8
4									GEN OUTLET	9
5	MMBTS	100	2	ON	ON	1	20	20	TELCO OUTLET	10
6									TELCO FAX	11
										12



---

# DETAILED STRUCTURAL ANALYSIS AND EVALUATION OF AN EXISTING 245' SELF SUPPORTING LATTICE TOWER AND FOUNDATION FOR PROPOSED ANTENNA ARRANGEMENTS

Site ID: CT03XC214  
Site Name: UCONN  
Site Address: 82 North Eagleville Road  
Storrs, CT

---

*prepared for*



**Transcend Wireless**  
**10 Industrial Ave.**  
**Suite 3**  
**Mahwah, NJ. 07430**

*prepared by*



URS CORPORATION  
500 ENTERPRISE DRIVE, SUITE 3B  
ROCKY HILL, CT 06067  
TEL. 860-529-8882

36932110.00000  
TWS-019

December 30, 2014

## **TABLE OF CONTENTS**

- 1. EXECUTIVE SUMMARY**
- 2. INTRODUCTION**
- 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS**
- 4. FINDINGS AND EVALUATION**
- 5. CONCLUSIONS**
- 6. DRAWINGS AND DATA**
  - **ORIGINAL TOWER MANUFACTURER DRAWINGS**
  - **TNX TOWER INPUT / OUTPUT SUMMARY**
  - **TNX TOWER FEEDLINE DISTRIBUTION**
  - **TNX TOWER FEEDLINE PLAN**
  - **TNX TOWER DETAILED OUTPUT**
  - **ANCHOR BOLT ANALYSIS**
  - **FOUNDATION ANALYSIS**

1. EXECUTIVE SUMMARY

This report summarizes the structural analysis of the existing 245' self-supporting tower located at the campus of the University of Connecticut, on North Eagleville Road in Storrs, Connecticut. The analysis was conducted in accordance with the 2005 Connecticut State Building Code which requires a three second gust wind speed of 100 mph which converts to an 80 mph fastest mile per 2003 IBC (Table 1609.3.1) and the TIA/EIA-222-F standard for a wind velocity of 85 mph (fastest mile). The wind speed from the TIA/EIA-222-F standard governs the design at 85 mph (fastest mile) and 74 mph (fastest mile) concurrence 1/2" ice.

The antenna loading considered in the analysis consists of all existing and proposed antennas, transmission lines, and ancillary items as outlined in the Introduction Section of this report. The proposed Sprint modification is as follows:

Proposed Antenna and Mount	Carrier	Antenna Center Elevation
<b>Install:</b> (3) APXV9TM14-ALU-I20 Panel Antennas (3) Alcatel-Lucent TD-RRH 8x20 RRH Units (1) Alcatel-Lucent ALU Hybrid Cable (2) Sector Jumper Cables (27) RRH Jumper Cables	Sprint (Proposed)	@ 247'

The results of the analysis indicate that the tower and foundation components has the capacity to support the proposed loading conditions. **The tower and its foundation components are considered structurally adequate with the wind load classification specified above with the existing and proposed antenna loading.**

1. **EXECUTIVE SUMMARY** *(continued)*

This analysis is based on:

- 1) The tower structure's theoretical capacity, not including any assessment of the condition of the tower.
- 2) Tower foundation, geometry and structural member sizes taken from the manufacturers original design documents prepared by Pirod Inc., drawing number 202932-B, dated September 23, 1997.
- 3) Existing antenna, mount and coaxial cable quantities taken from structural report performed by Atlantis Group, on behalf of T-Mobile, dated May 23, 2012.
- 4) Existing antenna, mount and coaxial cable quantities and locations taken from structural analysis performed by Ramaker & Associates, Inc, on behalf of Sprint, project number 23003, signed and sealed October 26, 2012.
- 5) Preliminary construction drawings for proposed Sprint antenna upgrades provided from Ramaker & Associates, dated June 17, 2014.
- 6) Antenna and mount configuration as specified on the following page of this report.

This report is only valid as per the assumptions and data utilized in this report for antenna inventory, mounts and associated cables. The user of this report shall field verify the assumption of the antenna and mount configuration as well as the physical condition of the tower and connections. Notify the engineer in writing immediately if any of the information in this report is found to be other than specified.

If you should have any questions, please call.

Sincerely,

**URS Corporation**

  
Richard A. Sambor, P.E.  
Senior Structural Engineer

RAS/mcd

cc: IA, CF/Book – URS





## 2. INTRODUCTION

The subject tower is located on 82 North Eagleville Road in Storrs, Connecticut. The structure is a 245' self-supporting tower designed and manufactured by Pirod, Inc.

The tower geometry and structural member sizes taken from original construction drawings (Pirod Drawing #: 202932-B) prepared by Pirod, dated September 23, 1997.

The inventory is summarized in the table below:

<i>Antenna Type</i>	<i>Carrier</i>	<i>Mount</i>	<i>Antenna Centerline Elevation</i>	<i>Cable</i>
Lightning Rod	Tower (existing)	15' Rotatable Platform	247'	---
Flash Beacon	Tower (existing)	See Above Mount	247'	(1) 1/2" DC cable
<b>(3) APXV9TM14-ALU-I20 Panel Antennas (3) Alcatel-Lucent TD-RRH 8x20 RRH Units (2) Sector Jumper Cables (27) RRH Jumper Cables</b>	<b>Sprint (Proposed)</b>	<b>See Above Mount</b>	<b>247'</b>	<b>(1) Alcatel-Lucent ALU Hybrid Cable</b>
(2) APXVSP18-C-A20 (Alpha & Gamma) (1) RFS APX9ERR18-C-A20 (Beta) (6) 1900 MHz RRH Units (3) 800 MHz RRH Units (3) IBC1900BB-1 (3) IBC1900HG-2A	Sprint (existing)	See Above Mount	247'	(3) 1-1/4" Hybrid Cables
(3) AIR21 B2A/B4P (3) AIR21 B4A/B2P (1) ADFD1820-80B-R2DM (3) TMA Units	T-Mobile (existing)	(3) Sector Mounts	232'	(21) 1-5/8" coax cables
(2) 10' Omni Antennas	Unknown (existing)	(2) 4' Standoff	135'	(2) 7/8" coax cables
(1) 20' Omni Antenna	Unknown (existing)	6' Standoff	125'	(1) 7/8" coax cable
(3) L-810 Obstruction Lights	Tower (existing)	Leg mounted	125'	(1) 1/2" DC cable
(1) 10' Omni Antenna	Unknown (existing)	4' Standoff	110'	(1) 7/8" coax cable
4' Grid Dish	Unknown (existing)	Leg mounted	110'	(1) 7/8" coax cable
(1) 6' Dish w/ Radome	Unknown (existing)	Leg mounted	105'	(1) EW63 cable
(1) Camera	Unknown (existing)	Leg mounted	60'	(1) 7/8" coax cable
(1) 4' Omni	Unknown (existing)	4' Standoff	50'	(1) 7/8" coax cable

This structural analysis of the communications tower was performed by URS Corporation (URS) for Sprint. The purpose of this analysis was to investigate the structural integrity of the existing tower with its existing, proposed and future antenna loads. This analysis was conducted to evaluate stress on the tower and the effect of forces to the foundation of the tower resulting from existing and proposed antenna arrangements.



### 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS

The structural analysis was done in accordance with the 2005 Connecticut State Building Code, TIA/EIA-222-F—Structural Standard for Steel Antenna Towers and Antenna Supporting Structures and the American Institute of Steel Construction (AISC) Manual of Steel Construction—Allowable Stress Design (ASD).

The analysis was conducted using TNX Tower 6.1.3.1. Two load conditions were evaluated as shown below which were compared to allowable stresses according to AISC and TIA/EIA.

The Connecticut State Building Code required a three second wind speed of 100 mph which converts to a 80 mph fastest mile per IBC (Table 1609.3.1). The TIA/EIA-222-F requires a basic wind speed of 85 mph (fastest mile). In this case the wind speed from the TIA/EIA-222-F governs the design.

Load Condition 1 = 85 mph (fastest mile) Wind Load (without ice) + Tower Dead Load

Load Condition 2 = 74 mph (fastest mile) Wind Load (with ice) + Ice Load + Tower Dead Load

Please note that wind pressure is a function of velocity squared. Under Load Condition 2, a 25% reduction in wind pressure is allowed by code to account for the unlikelihood of the full wind pressure and ice load occurring at the same time. The same results may be achieved by utilizing a lower wind pressure without taking the 25 percent reduction, as shown above.

The TIA/EIA standard permits a one-third increase in allowable stresses for towers and monopoles less than 700 feet tall. For the purposes of this analysis, in computing the load capacity the allowable stresses of the tower members were increased by one-third.

#### 4. FINDINGS AND EVALUATION

Stresses on the tower structure were evaluated to compare with allowable stresses in accordance with AISC. The calculated stresses under the proposed loading were BELOW the allowable stresses. Detailed analysis and calculations for the proposed load condition are provided in Section 6 of this report. The foundation caisson and tower anchor bolts were found to be structurally adequate.

##### Tower Reactions

Component	Value (kips)
Base Shear	36
Base Compression	377
Anchor Uplift	310
Anchor Shear	34

##### Tower Component Stress vs. Capacity Summary:

Component/ (Section No.)	Existing Component Size	Controlling Component/Elevation	Stress (% capacity)	Pass/Fail
Tower Leg (T2)	2" SR	Compression / 230' – 210'	99.1 %	<b>Pass</b>
Diagonal (T11)	L3x3x5/16	Compression / 80' – 60'	90.1 %	<b>Pass</b>
Secondary Horizontal (T9)	L3x3x5/16	Compression / 110' – 100'	72.5 %	<b>Pass</b>
Top Girt (T3)	1" SR	Compression / 210' – 190'	46.1 %	<b>Pass</b>
Bottom Girt (T1)	7/8" SR	Compression / 245' – 230'	64.4 %	<b>Pass</b>
<b>Bolt Checks</b>				
Anchor Bolts	(6) 2" Dia. Bolts	Tension	68%	<b>Pass</b>

##### Foundation Summary:

Foundation	Component	Stress (% capacity/Factor of Safety)	Pass/Fail	Comments:
Drilled Concrete Caisson	Uplift	98.0% / 2.04	<b>Pass</b>	Min. FOS of 2.0 req'd per IBC 2003 Section 3108.4.2

## 5. CONCLUSIONS

The results of the analysis indicate that the tower and foundation components have the capacity to support the proposed loading conditions. **The tower and its foundation components are considered structurally adequate with the wind load classification specified with the existing and proposed antenna loading.**

### Limitations/Assumptions:

This report is based on the following:

1. Tower inventory as listed in this report.
2. Tower is properly installed and maintained.
3. All members are as specified in the original design documents and are in good condition.
4. All required members are in place.
5. All bolts are in place and are properly tightened.
6. Tower is in plumb condition.
7. All member protective coatings are in good condition.
8. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
9. Foundations were properly constructed to support original design loads as specified in the original design documents.
10. All coaxial cable is installed as specified in Section 6 of this report.

URS is not responsible for any modifications completed prior to or hereafter in which URS is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing/replacing antennas
- C. Adding coaxial cables

URS hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact URS. URS disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

### Ongoing and Periodic Inspection and Maintenance:

After the Contractor has successfully completed the installation and the work has been accepted, the owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA/EIA-222-F for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. According to TIA/EIA-222-F section 14.1, Note 1: It is recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.

## 6. DRAWINGS AND DATA

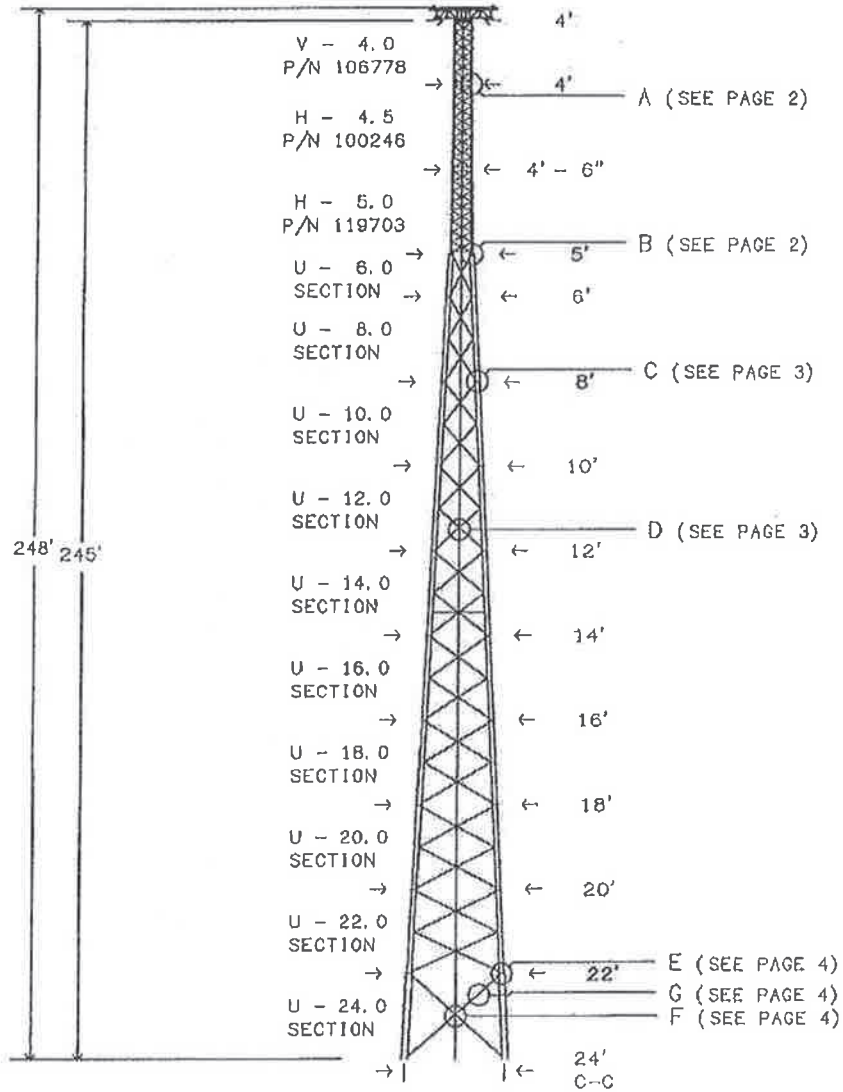
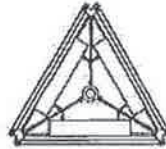
# ORIGINAL TOWER MANUFACTURER DRAWINGS


TOP VIEW  
(ENLARGED)

ROTATABLE TOP  
(REF ASSEMBLY  
DWG # 122379)

SIDE VIEW  
(ENLARGED)

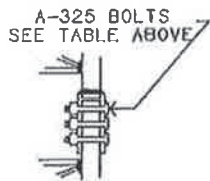
SHOP WELD TOP PLATE P/N  
121018 AT TOP OF TOP SECTION.



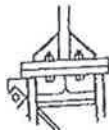
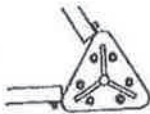
				BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' SELF-SUPPORTING TOWER	
APPROVED/ENG.		MLH 09/23/1997		 1545 Pidco Dr. Plymouth, IN 46563-0128 219-936-4221	
APPROVED/FOUND.		N/A			
REV	DESCRIPTION OF REVISIONS	INI	DATE	DRAWN BY	RCH
A	ADDED FOUNDATIONS PER SOIL REPORT	MLH	09/23/1997		
From 69370.DFT - 09/23/07 10:26				ENG. FILE NO.	A-113846-
Printed from 202932.D10A.DWG - 09/23/1997 15:00 @ 12/19/2014 14:21				ARCHIVE	Q-69379
				DRAWING NO.	202932-B
				PAGE	1 OF 9

FABRICATED SECTION DATA 190' - 245' ELEVATION							
SECT LEN	SEC #	SECTION PART#	LEG SIZE	BRACE SIZE	SECT WT. #	BOLTS AT BOTTOM	
						DIAM	LENGTH #
15'	V- 4.0	106778+	1- 1/2 "	3/4 "	602#	5/8"	4-1/2" 15
20'	H- 4.5	100246	2 "	7/8 "	1190#	3/4"	5" 15
20'	H- 5.0	119703	2- 1/2 "	1 "	1802#	1 "	3-1/2" 18

\*THE WEIGHTS LISTED ARE THEORETICAL. THE ACTUAL WEIGHTS WILL VARY.  
 ALL WEIGHTS SHOULD BE CONFIRMED IN THE FIELD PRIOR TO ERECTION.  
 +WELD TOP PLATE P/N 121018 AT TOP OF TOP SECTION.

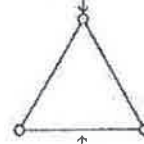


VIEW A  
 TYPICAL LEG CONNECTION  
 FOR FABRICATED SECTIONS




TOP VIEW @ B      VIEW B  
 LEG CONNECTION AT 190 FT.  
 USE 1 FLATWASHER UNDER EACH LOCKNUT,  
 FOR LEG CONNECTION ONLY.

TOP VIEW  
 MARKED LEG



LADDER FACE

THE MARKED LEG OF EACH SECTION IS STAMPED WITH THE LAST 3 DIGITS OF THE TOWER SERIAL #. ASSEMBLE THE TOWER WITH MARKED LEGS TOGETHER. THE MARKED LEG MAY ALSO CONTAIN JOINT NUMBERS. IF SO, ASSEMBLE SECTIONS WITH JOINTS IN THE PROPER SEQUENCE.

		BECHTEL NATIONAL, INC.		 <b>PARCO INC.</b> 1545 Pldco Dr. Plymouth, IN 46583-0128 219-936-4221
		STORRS #C214, CT		
		U - 24.0 X 248' SELF-SUPPORTING TOWER		
		APPROVED/ENG.	WLF 9/23/1997	
APPROVED/FOUND.	N/A			
COPYRIGHT	2014			
DRAWN BY	RCH			
ENG. FILE NO.	A-113846-	DRAWING NO.	202932-B	
ARCHIVE	Q-69379	PAGE	2 OF 9	



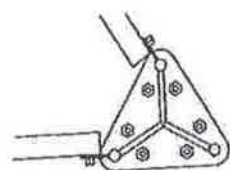
BREAKDOWN SECTION DATA (12" LEG) 20' - 190' ELEVATION

SEC #	SECTION LENGTH	LEG SIZE	LEG PART#	TOP DIAG PART#	BOT DIAG PART#	DIAGONAL FACE	ANGLE THICK	TOTY HOR	SECTION WEIGHT	LEG CONNECT+ DIAM	LENGTH	DIAG CONNECT DIAM	LENGTH
U- 6.0	10'	1- 1/2"	105245		105556	2-1/2"	3/16"		1047#	1 "	3-1/2"	1 "	2-1/4"
U- 8.0	20'	1- 1/2"	105217	105558	105561	2-1/2"	3/16"		2118#	1 "	3-1/2"	1 "	2-1/4"
U-10.0	20'	1- 3/4"	105218	105564	105567	2-1/2"	3/16"		2548#	1 "	3-1/2"	1 "	2-1/4"
U-12.0	20'	1- 3/4"	105218	105571	105574	3"	3/16"		2698#	1 "	4-1/2"	1 "	2-1/4"
U-14.0	20'	2 "	105219	113409	113410	3"	5/16"	1	4065#	1-1/4"	4-1/2"	1-1/4"	2-3/4"
U-16.0	20'	2 "	105219	113411	113412	3"	5/16"		3913#	1-1/4"	4-1/2"	1-1/4"	2-3/4"
U-18.0	20'	2- 1/4"	105220	127370	127371	3-1/2"	5/16"		4770#	1-1/4"	4-1/2"	1-1/4"	2-3/4"
U-20.0	20'	2- 1/4"	105220	105598	105801	3-1/2"	5/16"		4920#	1-1/4"	4-1/2"	1-1/4"	2-3/4"
U-22.0	20'	2- 1/4"	105220	105604	105607	4"	1/4"		4922#	1-1/4"	5"	1-1/4"	2-3/4"

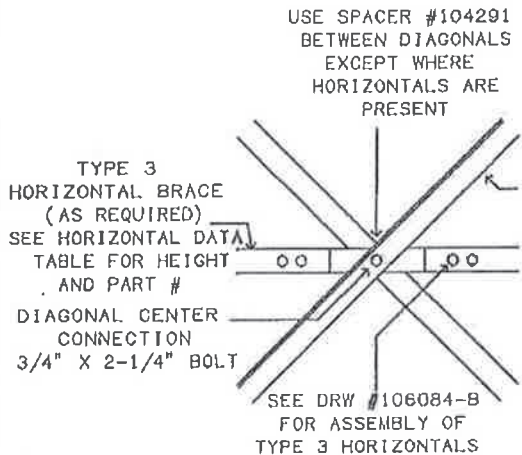
\* THE WEIGHTS LISTED ARE THEORETICAL. THE ACTUAL WEIGHTS WILL VARY. ALL WEIGHTS SHOULD BE CONFIRMED IN THE FIELD PRIOR TO ERECTION.  
 + USE 1 FLATWASHER UNDER EACH LOCKNUT, FOR LEG CONNECTION ONLY. ALSO USE 1 FLATWASHER UNDER EACH BOLT HEAD WHERE BUSHINGS ARE REQUIRED.

ANGLE HORIZONTAL DATA (12" LEG)

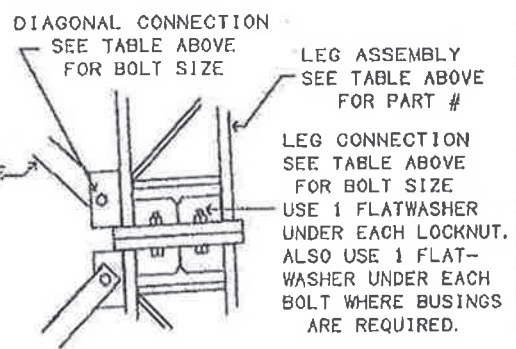
HORIZ HT	IN SEC#	HORIZ PART#	HORIZ TYPE	BOLTS	
				DIAM	LENGTH
105	U-14.0	106207	3	SEE #	106084-B



TOP VIEW @ C



VIEW D (SEE PAGE 1 FOR VIEW DEFINITION)  
 TYPICAL BRACE CONNECTION  
 #12 SECTIONS

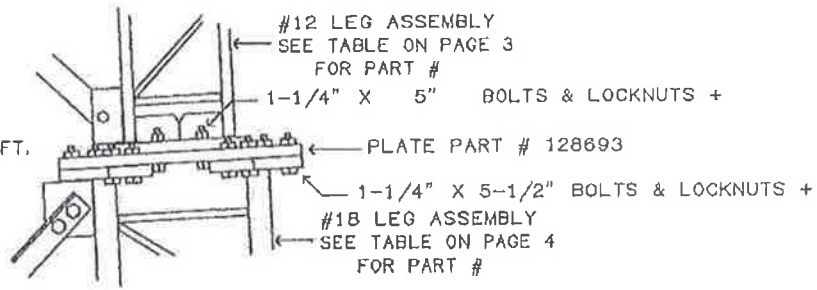


VIEW C  
 TYPICAL LEG CONNECTION  
 #12 SECTIONS

BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' SELF-SUPPORTING TOWER		1545 Pldco Dr. Plymouth, IN 46563-0128 219-936-4221	
APPROVED/ENG.	WJH 9/23/1997		
APPROVED/FOUND.	N/A		
COPYRIGHT	2014		
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ENG. FILE NO.	A-113846-	DRAWING NO.	202932-B
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VIEW E  
LEG CONNECTION AT 20 FT.



BREAKDOWN SECTION DATA (18" LEG - DOUBLE ANGLE DIAGONALS) 0' - 20' ELEVATION

SEC #	SECTION LENGTH	LEG SIZE	LEG PART#	DIAGONAL PART #			DIAG ANGLE		SECTION WEIGHT	LEG CONNECT+		DIAG CONNECT	
				UPPER	LOWER	LONG	FACE	THICK		DIAM	LENGTH	DIAM	LENGTH
U-24.0	20'	2- 1/2"	112738	112889	112885	112807	3-1/2"	5/16"	7275#		1"	3-1/2"	

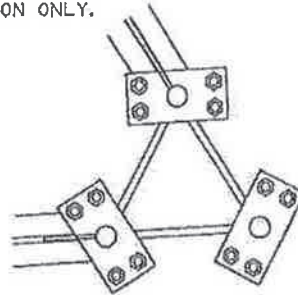
\* THE WEIGHTS LISTED ARE THEORETICAL. THE ACTUAL WEIGHTS WILL VARY. ALL WEIGHTS SHOULD BE CONFIRMED IN THE FIELD PRIOR TO ERECTION.  
+ USE 1 FLATWASHER UNDER EACH LOCKNUT, FOR LEG CONNECTION ONLY.

SPACER # 104293  
2 REQUIRED PER BOLT



VIEW G

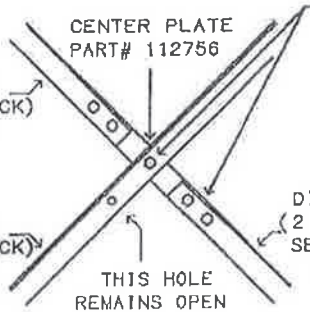
TYPICAL SPACER INSTALLATION  
#18 SECTIONS - DOUBLE ANGLE BRACES  
(4 PLACES EACH SECTION PER FACE)



TOP VIEW @

"UPPER"  
DIAGONAL BRACE  
(2 - BACK TO BACK)  
SEE TABLE ABOVE  
FOR PART #

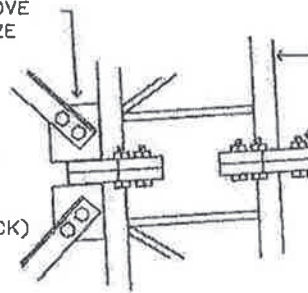
"LONG"  
DIAGONAL BRACE  
(2 - BACK TO BACK)  
SEE TABLE ABOVE  
FOR PART #



VIEW F (SEE PAGE 1 FOR VIEW DEFINITION) VIEW  
TYPICAL BRACE CONNECTION  
#18 SECTIONS - DOUBLE ANGLE BRACES

DIAGONAL BOLTS  
SEE TABLE ABOVE  
FOR BOLT SIZE

"LOWER"  
DIAGONAL BRACE  
(2 - BACK TO BACK)  
SEE TABLE ABOVE  
FOR PART #



TYPICAL LEG CONNECTION  
#18 SECTIONS - DOUBLE ANGLE BRACES


<p>BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' SELF-SUPPORTING TOWER</p>		<p>1545 Pidco Dr. Plymouth, IN 46563-0128 219-936-4221</p>
<p>From 09379.DFT - 09/23/97 10:29</p> <p>Printed from 202932_0400.DWG - 09/23/1997 10:29 @ 12/19/2014 14:21</p>	<p>ENG. FILE NO. A-113846-</p> <p>ARCHIVE Q-69379</p>	<p>DRAWING NO. 202932-B</p> <p>PAGE 4 OF 9</p>

### GENERAL NOTES

1. TOWER DESIGN CONFORMS TO STANDARD EIA/TIA-222-F FOR 90 MPH BASIC WIND SPEED WITH NO ICE.  
TOWER DESIGN CONFORMS TO STANDARD EIA/TIA-222-F FOR 90 MPH BASIC WIND SPEED WITH .50" RADIAL ICE WITH LOAD DUE TO WIND REDUCED BY 25% WHEN CONSIDERED SIMULTANEOUSLY WITH ICE.
2. MATERIAL: (A) SOLID RODS CONFORM TO ASTM A-572 GRADE 50 REQUIREMENTS.  
(B) ANGLES CONFORM TO ASTM A-36 REQUIREMENTS.  
(C) PIPE CONFORMS TO ASTM A-53 TYPE E, GRADE B REQUIREMENTS. (MIN YIELD STRENGTH=42 KSI)  
(D) ALL STEEL PLATES CONFORM TO ASTM A-36 REQUIREMENTS.
3. BASE REACTIONS PER EIA/TIA-222-F FOR 90 MPH BASIC WIND SPEED WITH NO ICE.  


TOTAL WEIGHT =	52.0 KIPS.	MAXIMUM COMPRESSION =	454.9 KIPS PER LEG.
MOMENT =	9094.3 KIP-FT.	MAXIMUM UPLIFT =	420.2 KIPS PER LEG.
MAXIMUM SHEAR =	71.3 KIPS TOTAL.		
4. BASE REACTIONS PER EIA/TIA-222-F FOR 90 MPH BASIC WIND SPEED WITH .50" RADIAL ICE:  

TOTAL WEIGHT =	73.7 KIPS.	MAXIMUM COMPRESSION =	472.0 KIPS PER LEG.
MOMENT =	9299.9 KIP-FT.	MAXIMUM UPLIFT =	422.9 KIPS PER LEG.
MAXIMUM SHEAR =	72.4 KIPS TOTAL.		
5. FINISH: HOT DIPPED GALVANIZED AFTER FABRICATION.
6. ANTENNAS: 247' (12) DB980 WITH 1 5/8" LINES MOUNTED ON A ROTATABLE PLATFORM.  
225' (12) ALP0212 WITH 1 5/8" LINES MOUNTED ON UNIVERSAL T-FRAMES.  
120' (1) DB201 WITH 7/8" LINE MOUNTED ON A 3' STANDOFF.  
115' (2) DB201 WITH 7/8" LINES MOUNTED ON 3' STANDOFFS.  
115' (1) 4' GRID DISH WITH 7/8" LINE.  
103' (1) 6' SOLID DISH WITH RADOME AND 7/8" LINE.  
65' (1) CAMERA. (CoAa= 4 SQ. FT.)  
50' (1) GPS ANTENNA & MOUNT. (TOTAL CoAa= 14 SQ. FT.)
7. REMOVE FOUNDATION TEMPLATE PRIOR TO ERECTING TOWER. INSTALL BASE SECTION WITH MINIMUM OF 2" CLEARANCE ABOVE CONCRETE. GROUT NUTS BELOW BASE SECTION WITH NON-SHRINK GROUT AFTER LEVELING TOWER.
8. MIN. WELDS 5/16" UNLESS OTHERWISE SPECIFIED. ALL WELDING TO CONFORM TO AWS SPECIFICATIONS.
9. ALL BOLTS AND NUTS MUST BE IN PLACE BEFORE THE ADJOINING SECTION(S) ARE INSTALLED.
10. ALL A-325 BOLTS SHALL BE PRE-TENSIONED PER AISC SPECIFICATIONS. REFER TO DRAWING # 123107-A ("BOLT PRE-TENSIONING GUIDELINES".)
11. EIA GROUNDING FOR TOWER.
12. DUAL LIGHT KIT (151' - 350')

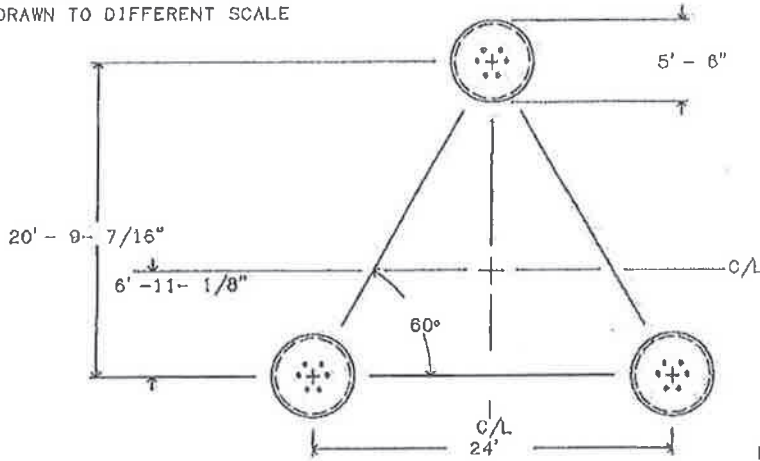
BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' SELF-SUPPORTING TOWER		 1545 Pidgea Dr. Plymouth, IN 46563-0128 219-936-4221
APPROVED/ENG.	MLH 9/23/1997	
APPROVED/FOUND.	N/A	
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### FOUNDATION NOTES

1. SOIL AS PER REPORT BY CLOUGH, HARBOUR, AND ASSOCIATES, LLC, DATED 8/08/97 (FILE #5835.07.64).
2. CONCRETE TO BE 3000 PSI @ 28 DAYS. REINFORCING BAR TO CONFORM TO ASTM A615 GRADE 60 SPECIFICATIONS. CONCRETE INSTALLATION TO CONFORM TO ACI-318 BUILDING REQUIREMENTS FOR REINFORCED CONCRETE. ALL CONCRETE TO BE PLACED AGAINST UNDISTURBED EARTH FREE OF WATER AND ALL FOREIGN OBJECTS AND MATERIALS. A MINIMUM OF THREE INCHES OF CONCRETE SHALL COVER ALL REINFORCEMENT. WELDING OF REBAR NOT PERMITTED.
3. A COLD JOINT IS PERMISSIBLE UPON CONSULTATION WITH PIROD. ALL COLD JOINTS SHALL BE COATED WITH BONDING AGENTS PRIOR TO SECOND POUR.
4. ALL REINFORCING STEEL TO BE FORMED INTO A CAGE PRIOR TO SETTING INTO POSITION IN THE EXCAVATED PIER.
5. PERMANENT STEEL CASING SHALL NOT BE USED WITHOUT CONSENT FROM FOUNDATION DESIGNERS.
6. CROWN TOP OF FOUNDATION FOR PROPER DRAINAGE.
7. A TEMPORARY STEEL CASING IS REQUIRED FOR INSTALLATION.
8. CONCRETE MUST BE PLACED BY TREMIE METHODS.

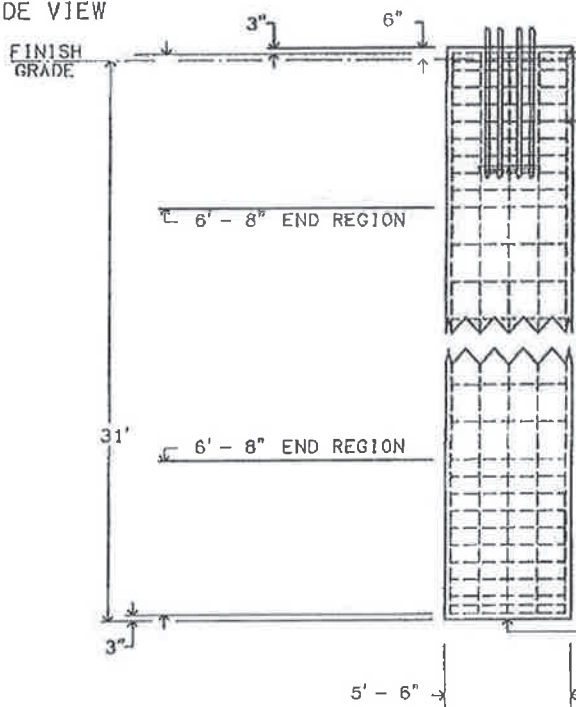
BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' SELF-SUPPORTING TOWER					
		APPROVED/ENG.	MLH	09/23/1997	1545 Pideo Dr. Plymouth, IN 46583-0128 219-936-4221
		APPROVED/FOUND.	MLH	09/23/1997	
A	ADDED FOUNDATIONS PER SOIL REPORT	MLH	09/23/1997	COPYRIGHT 2014	
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TOP VIEW  
 TOP AND SIDE VIEWS ARE  
 DRAWN TO DIFFERENT SCALE



NOTE: ALL REBAR REQUIRES MINIMUM  
 3" CONCRETE COVERAGE  
 FOR ANCHOR STEEL IDENTIFICATION  
 AND PLACEMENT INFORMATION, SEE  
 PAGE 9.

SIDE VIEW



FOR DETAIL VIEW OF REBAR CAGE  
 END AREA, SEE (E) ON PAGE 8.


# 5 HORIZONTAL TIES -- SEE (B) ON PAGE 8.  
 33 PIECES REQUIRED PER PIER.  
 PLACE TIES AT 9" NOMINAL  
 SPACING WITHIN END REGIONS,  
 AND 1'-6" NOMINAL SPACING IN  
 REMAINDER OF PIER.


# 9 VERTICAL REBAR -- SEE (A) ON PAGE 8.  
 18 PIECES REQUIRED PER PIER,  
 EQUALLY SPACED, TO BE PLACED  
 INSIDE TIES.

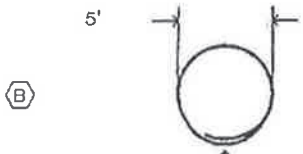
TOWER FOUNDATION

THREE PIERS REQUIRED  
 27.7 CUBIC YARDS CONCRETE REQUIRED EACH PIER

FOR INSTALLATION SPECIFICATIONS AND  
 ADDITIONAL INFORMATION, SEE PAGE 6  
 OF THIS DRAWING.

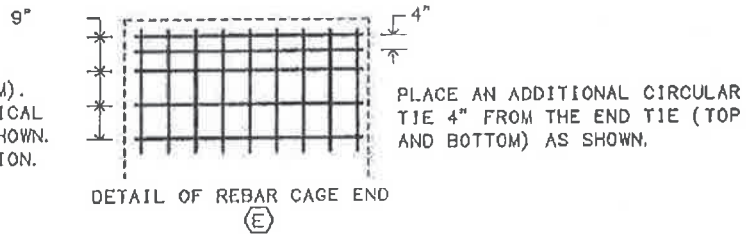
				BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' BASE FOUNDATION	
		APPROVED/ENG.	MLH	09/23/1997	 1545 Pideo Dr. Plymouth, IN 46563-0128 219-836-4221
		APPROVED/FOUND.	MLH	09/23/1997	
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A	ADDED FOUNDATIONS PER SOIL REPORT	MLH	09/23/1997		
REV	DESCRIPTION OF REVISIONS	INI	DATE	DRAWN BY	RCH
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Printed from 202932_070A.DWG - 09/23/1997 15:10 @ 12/19/2014 14:21				ARCHIVE Q-69379	PAGE 7 OF 9

(A)  # 9 REBAR - 54 PIECES REQ. TOTAL  
 APPROX WT = 105.4# EACH, 5692# TOTAL

(B)  # 5 REBAR - 89 PIECES REQUIRED TOTAL  
 APPROX UNBENT LENGTH = 17'-11- 1/4"  
 APPROX WT = 18.7# EACH, 1851# TOTAL

LAP DIMENSION: 2'- 2- 3/4"  
 PLACE CIRCULAR TIES SO THAT LAPS ON  
 ADJACENT TIES ARE 180 DEGREES APART.

PLACE 10 CIRCULAR TIES WITHIN  
 EACH END REGION (TOP AND BOTTOM).  
 PLACE FIRST TIE AT END OF VERTICAL  
 BARS AND CONTINUE SPACING AS SHOWN.  
 SEE PAGE 7 FOR REGION DEFINITION.



REBAR DETAIL

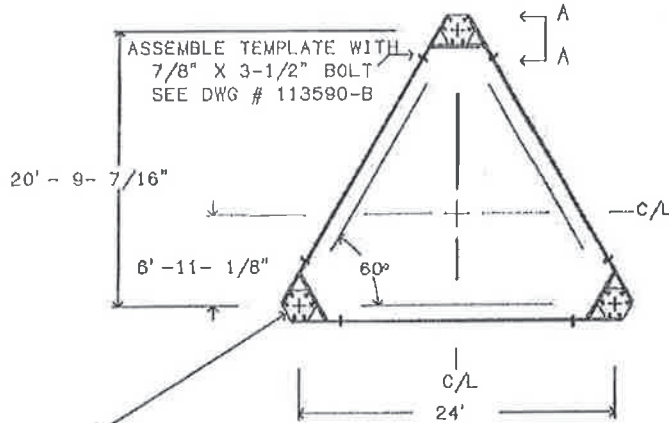
TOTAL APPROX REBAR WEIGHT = 7543#  
 REINFORCING BAR TO CONFORM TO  
 ASTM A615 GRADE 60 SPECIFICATIONS.

				BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' REBAR DETAIL	
				APPROVED/ENG.	MLH 8/23/1997
				APPROVED/FOUND.	MLH 8/23/1997
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A	ADDED FOUNDATIONS PER SOIL REPORT	MLH	09/23/1997	DRAWN BY	RCH
REV	DESCRIPTION OF REVISIONS	INI	DATE	ARCHIVE	Q-69379
From: 89378.DFT - 09/23/07 14:49 Printed from 202932_D88A.DWG - 09/23/1997 15:10 @ 12/19/2014 14:21				ENG. FILE NO. A-113846~	DRAWING NO. 202932-B
				PAGE	8 OF 9

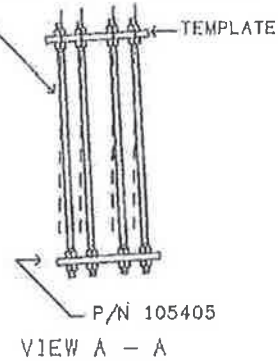




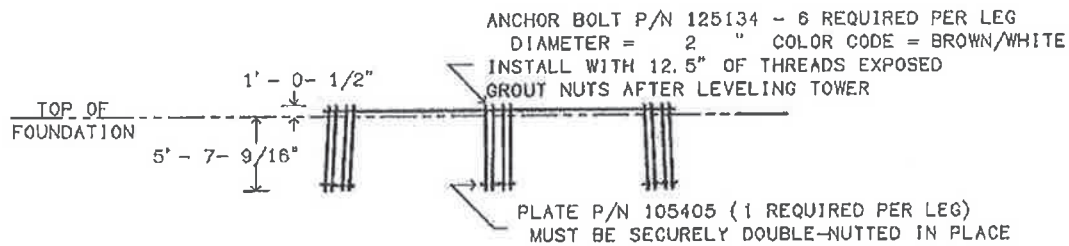
EACH LEG MUST BE CENTERED IN PIER  
WITHIN +/- 10% OF PIER DIAMETER



REFERENCE ANGLE = 3.30 DEGREES  
TEMPLATE MUST BE UTILIZED TO  
INSURE CORRECT PLACEMENT



TEMPLATE P/N 103620 IS REQUIRED FOR INSTALLATION. COLOR CODE OF TEMPLATE MUST MATCH COLOR CODE OF ANCHOR BOLTS. TEMPLATE MUST BE SECURELY DOUBLE-NUTTED TO ANCHOR BOLTS DURING CONCRETE INSTALLATION AND MUST BE LEVEL +/- 1/2". INSTALL TEMPLATE WITH WELDED LIFTING ANGLES FACING UPWARD. INSTALL TEMPLATE WITH SUFFICIENT SPACE BENEATH TO PERMIT FINISHING OF CONCRETE. AND TO FACILITATE TEMPLATE REMOVAL PRIOR TO TOWER ERECTION.



**ATTENTION INSTALLER**

**2" DIAMETER ANCHOR STEEL**

THE ANCHOR BOLTS PROVIDED FOR THIS PROJECT ARE 2" DIA. AND COLOR CODED BROWN & WHITE. THE CORNER TEMPLATE IS PART NUMBER 103620 FOR A TAPERED TOWER AND SHOULD HAVE THREE SETS OF 2-1/16" DIA. HOLES ON 10" CENTERS. EMBEDMENT PLATES ARE PART NUMBER 105405.

IF THERE ARE ANY DISCREPANCIES, PLEASE NOTIFY PIROD, INC., PRIOR TO INSTALLATION.

**TOWER ANCHOR STEEL PLACEMENT**

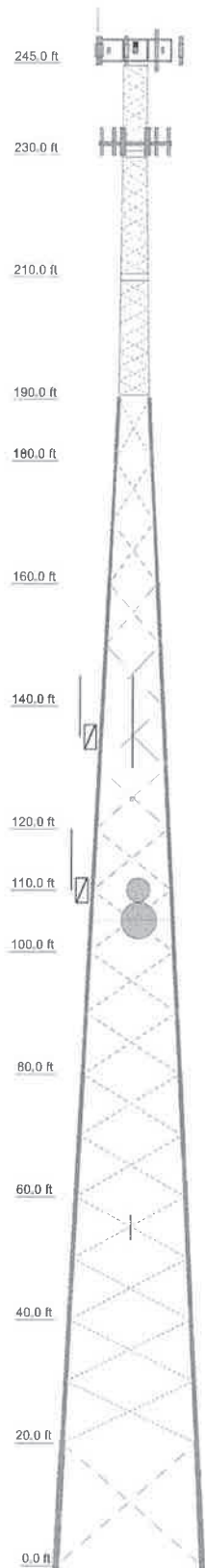
				BECHTEL NATIONAL, INC. STORRS #C214, CT U - 24.0 X 248' ANCHOR INSTALLATION	
				APPROVED/ENG.	MLH 9/23/1997
				APPROVED/FOUND.	MLH 9/23/1997
				COPYRIGHT 2014	
				DRAWN BY	RCH
				ENG. FILE NO.	A-113846-
				DRAWING NO.	202932-B
				ARCHIVE	Q-69379
				PAGE	9 OF 9
À	ADDED FOUNDATIONS PER SOIL REPORT	MLH	09/23/1997		
REV	DESCRIPTION OF REVISIONS	JNI	DATE		
From: 69379.DFT - 09/23/97 14:49					
Printed from 202932_090A.DWG - 09/23/1997 15:10 0 12/19/2014 14:21					



## TNX TOWER INPUT/OUTPUT SUMMARY



Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	T12	T13	T14
Legs	SR 1 1/2	SR 2	SR 2 1/2	A	Pirolod 105217	Pirolod 105218	Pirolod 105219	Pirolod 105220	Pirolod 105221	Pirolod 105222	Pirolod 105223	Pirolod 105224	Pirolod 105225	Pirolod 105226
Diagonals	SR 3/4	SR 7/8	SR 1	SR 1	L2 1/2x2 1/2x3/16	L2 1/2x2 1/2x3/16	L3x3x3/16	L3x3x5/16	A36	L3x3x5/16	L4x4x1/4	L3 1/2x3 1/2x5/16	L4x4x1/4	B
Diagonal Grade		A572-50		N.A.										
Top Girts	SR 7/8	SR 1	SR 1											
Bottom Girts	SR 7/8	SR 1												
Sec. Horizontals														
Face Width (ft)	4	4.5	5	5	6	6	8	8	10	10	12	12	14	14
# Panels @ (ft)	6 @ 2.33333	8 @ 2.375	9 @ 2.333	12	12	12	12	12	17 @ 10	17 @ 10	17 @ 10	17 @ 10	17 @ 10	17 @ 10
Weight (K)	0.6	1.2	1.8	2.3	2.3	2.3	2.6	2.6	3.0	3.0	3.0	3.0	3.0	3.0



### DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Lightning Rod 2"x10" (Tower)	247	TMA (T-Mobile)	232
Flash Beacon Lighting (Tower)	247	PIROD 12" Universal T-Frame (3) (T-Mobile)	232
APXVSP18-C-A20 w/ Mounting Pipe (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
APXV9ERR18-C-A20 w/ 6" Mount Pipe (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
APXVSP18-C-A20 w/ Mounting Pipe (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
(2) Panasonic RRH 1900MHZ (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
(2) Panasonic RRH 1900MHZ (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
(2) Panasonic RRH 1900MHZ (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
Andrew 800MHz RRH (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
Andrew 800MHz RRH (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
Andrew 800MHz RRH (Sprint)	247	AIR B2A/B4P w/ 6" Sch 40 Pipe Mount (T-Mobile)	232
IBC1900BB-1 Combiner (Sprint)	247	2.5" Dia, 12' OMNI	135
IBC1900BB-1 Combiner (Sprint)	247	4' Standoff Mount	135
IBC1900BB-1 Combiner (Sprint)	247	2.5" Dia, 12' OMNI	135
IBC1900HG-2A Combiner (Sprint)	247	4' Standoff Mount	135
IBC1900HG-2A Combiner (Sprint)	247	20' Omni	125
IBC1900HG-2A Combiner (Sprint)	247	6' Standoff Mount	125
PIROD Rotatable Platform #122379 (Sprint)	247	(3) L-810 Obstruction Lights w/ Mount Kit (Tower)	125
APXV9TM14-120 (Sprint)	247	4' Standoff Mount	110
APXV9TM14-120 (Sprint)	247	2.5" Dia, 12' OMNI	110
APXV9TM14-120 (Sprint)	247	KP4F-23	110
TD-RRH 8x20 (Sprint)	247	Andrew 6" w/Radome	105
TD-RRH 8x20 (Sprint)	247	Camera with Mount	60
TD-RRH 8x20 (Sprint)	247	4' Standoff Mount	50
TMA (T-Mobile)	232	1.5" Dia 4' Omni w/Pipe Mount	50
TMA (T-Mobile)	232		

### SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	Pirolod 105245	C	L3x3x5/16
B	2L3 1/2x3 1/2x5/16x3/4		

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

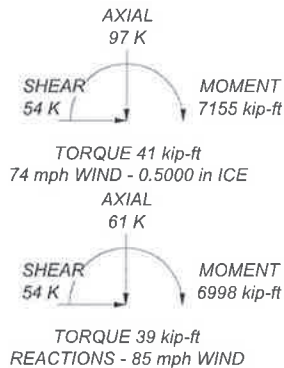
### TOWER DESIGN NOTES

1. Tower is located in Tolland County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 74 mph basic wind with 0.50 in ice.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 99.1%

#### MAX. CORNER REACTIONS AT BASE:

DOWN: 377 K  
SHEAR: 36 K

UPLIFT: -310 K  
SHEAR: 34 K



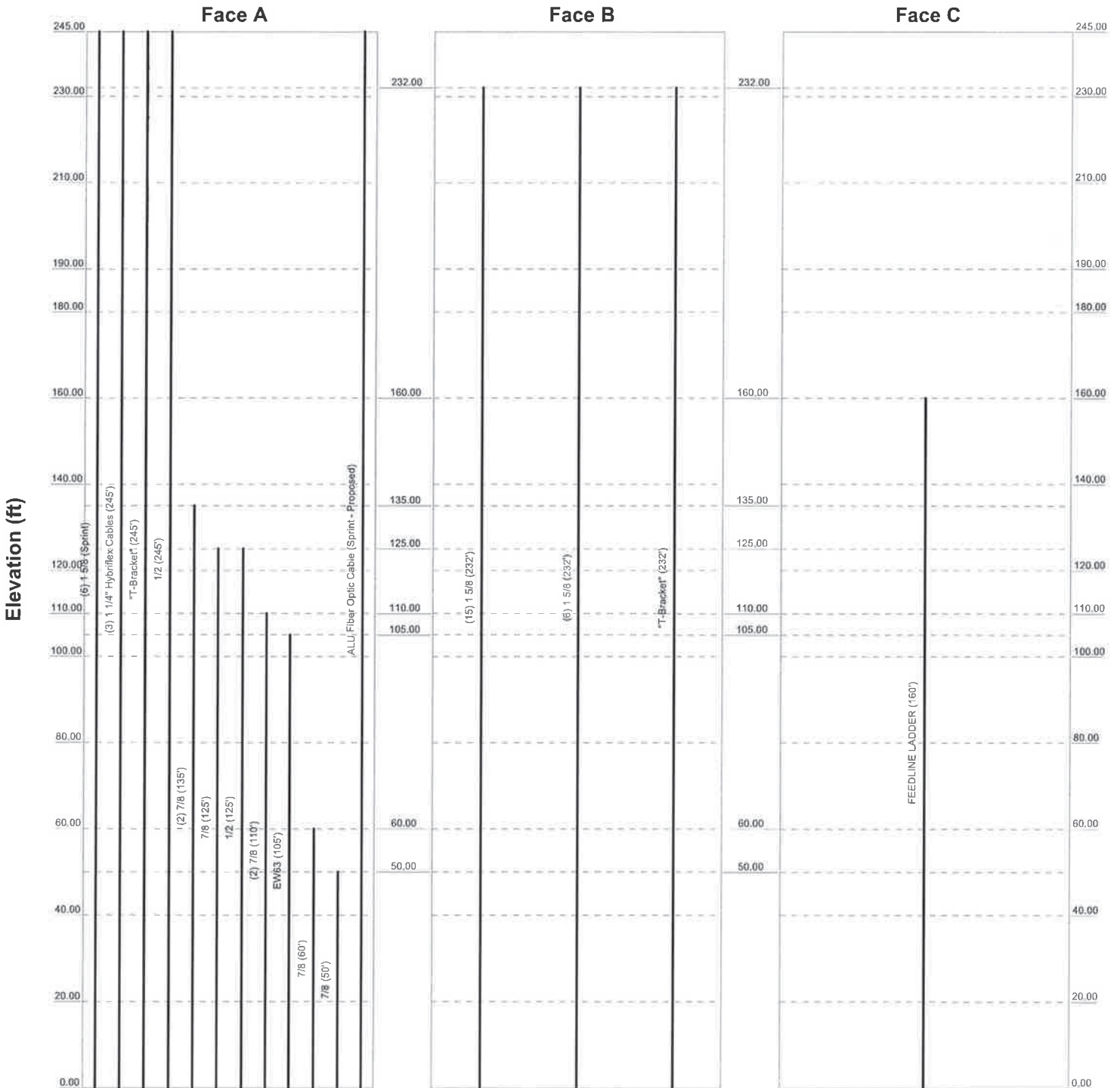
<b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job: Structural Analysis - Tower</b>
	Project: <b>Mansfield (UCONN), CT (Site #: CT03XC214)</b>
	Client: <b>Sprint - TWS-019</b> Drawn by: <b>MCD</b> App'd:
	Code: <b>TIA/EIA-222-F</b> Date: <b>12/30/14</b> Scale: <b>NTS</b>
	Path: _____      Dwg No. <b>E-1</b>

## TNX TOWER FEEDLINE DISTRIBUTION

# Feed Line Distribution Chart

## 0' - 245'

\_\_\_\_\_ Round \_\_\_\_\_ Flat \_\_\_\_\_ App In Face \_\_\_\_\_ App Out Face \_\_\_\_\_ Truss Leg



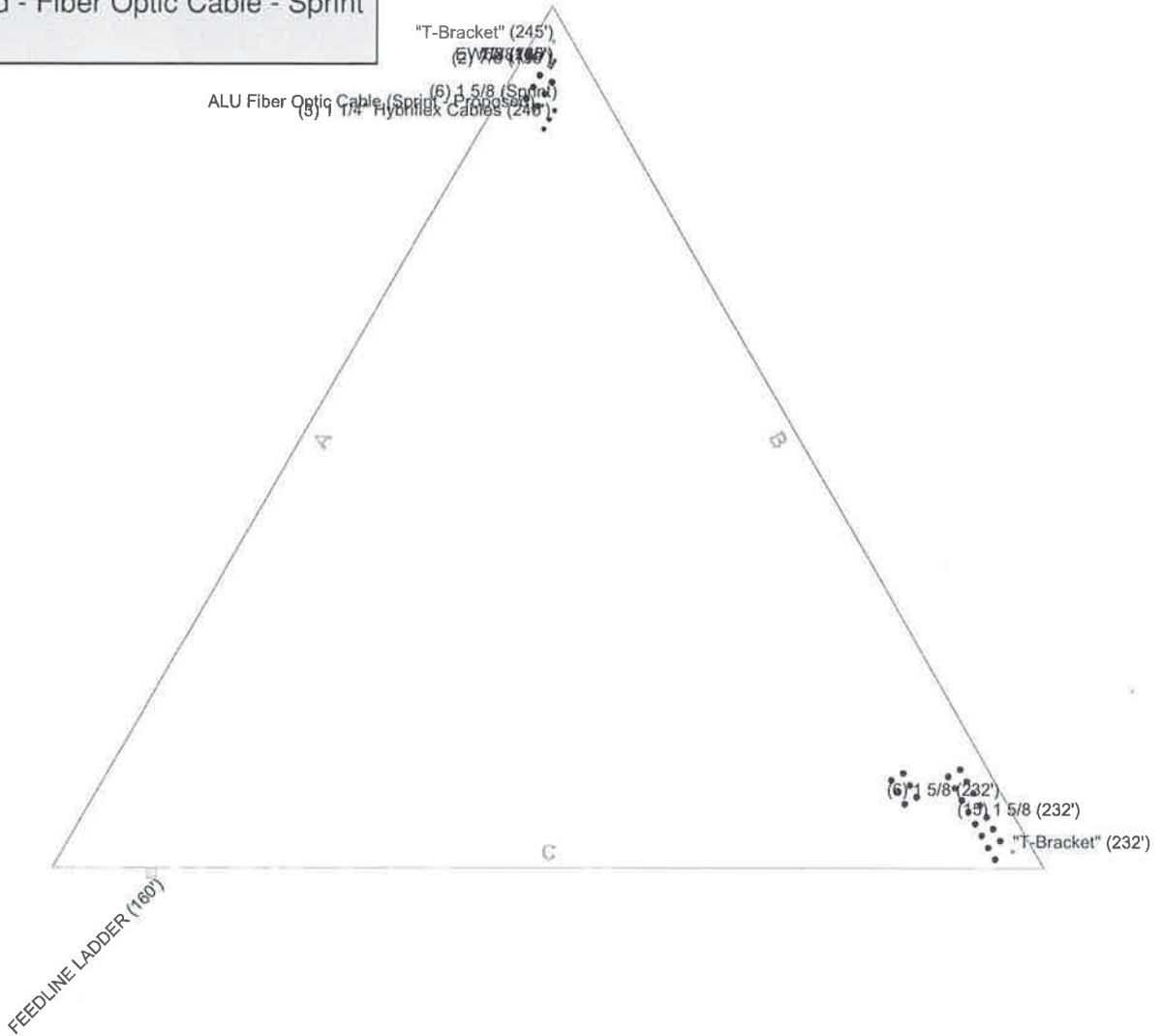
<b>URS Corporation</b>		<b>Job: Structural Analysis - Tower</b>	
500 Enterprise Drive, Suite 3B		Project: <b>Mansfield (UCONN), CT (Site #: CT03XC214)</b>	
Rocky Hill, CT 06067		Client: Sprint - TWS-019	Drawn by: MCD
Phone: 860-529-8882		Code: TIA/EIA-222-F	Date: 12/30/14
FAX: 860-529-3991			Scale: NTS
		Path:	Dwg No. E-7

# TNX TOWER FEEDLINE PLAN

# Feed Line Plan

Round
Flat
App In Face
App Out Face
Truss-Leg

- (6) 1-5/8" coax cables - Sprint
- (3) 1-1/4" Hybrid cables - Sprint
- (1) "T-Bracket"
- (2) 1/2" DC cables
- (7) 7/8" coax cables
- (1) EW63 Elliptical cable
- (1) Proposed - Fiber Optic Cable - Sprint



<b>URS Corporation</b>		<b>Job: Structural Analysis - Tower</b>	
500 Enterprise Drive, Suite 3B		Project: <b>Mansfield (UCONN), CT (Site #: CT03XC214)</b>	
Rocky Hill, CT 06067		Client: Sprint - TWS-019	Drawn by: MCD
Phone: 860-529-8882		Code: TIA/EIA-222-F	Date: 12/30/14
FAX: 860-529-3991		Scale: NTS	Dwg No. E-7

## TNX TOWER DETAILED OUTPUT

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 1 of 45
	<b>Project</b> Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b> 16:11:49 12/30/14
	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD

## Tower Input Data

The main tower is a 3x free standing tower with an overall height of 245.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 4.00 ft at the top and 24.00 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Tolland County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 74 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.333.

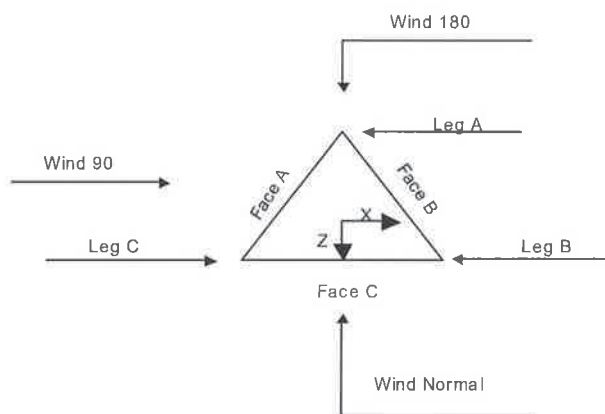
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

<ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>√ Include Bolts In Member Capacity</li> <li>√ Leg Bolts Are At Top Of Section</li> <li>√ Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>Add IBC .6D+W Combination</li> </ul>	<ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>√ Autocalc Torque Arm Areas</li> <li>√ SR Members Have Cut Ends</li> <li>√ Sort Capacity Reports By Component</li> <li>√ Triangulate Diamond Inner Bracing</li> <li>Use TIA-222-G Tension Splice Capacity Exemption</li> </ul>	<ul style="list-style-type: none"> <li>Treat Feedline Bundles As Cylinder</li> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feedline Torque</li> <li>Include Angle Block Shear Check</li> </ul> <p style="text-align: center;"><b>Poles</b></p> <ul style="list-style-type: none"> <li>Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul>
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<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 2 of 45
	<b>Project</b> Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b> 16:11:49 12/30/14
	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD



**Triangular Tower**

### Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	245.00-230.00			4.00	1	15.00
T2	230.00-210.00			4.00	1	20.00
T3	210.00-190.00			4.50	1	20.00
T4	190.00-180.00		U6.0 105245	5.00	1	10.00
T5	180.00-160.00		U8.0 105217	6.00	1	20.00
T6	160.00-140.00		U10.0 105216	8.00	1	20.00
T7	140.00-120.00		U12.0 105218	10.00	1	20.00
T8	120.00-110.00		U14.0 105218	12.00	1	10.00
T9	110.00-100.00		U14.0 105218	13.00	1	10.00
T10	100.00-80.00		U16.0 105219	14.00	1	20.00
T11	80.00-60.00		U18.0 105219	16.00	1	20.00
T12	60.00-40.00		U20.0 105219 L3.5x5/16	18.00	1	20.00
T13	40.00-20.00		U22.0 105220 L4x1/4	20.00	1	20.00
T14	20.00-0.00		U24.0 105220	22.00	1	20.00

### Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	245.00-230.00	2.33	X Brace	No	Steps	6.0000	6.0000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	3 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T2	230.00-210.00	2.38	X Brace	No	Steps	6.0000	6.0000
T3	210.00-190.00	2.33	X Brace	No	Steps	8.0160	8.0160
T4	190.00-180.00	10.00	X Brace	No	No	0.0000	0.0000
T5	180.00-160.00	10.00	X Brace	No	No	0.0000	0.0000
T6	160.00-140.00	10.00	X Brace	No	No	0.0000	0.0000
T7	140.00-120.00	10.00	X Brace	No	No	0.0000	0.0000
T8	120.00-110.00	10.00	X Brace	No	No	0.0000	0.0000
T9	110.00-100.00	10.00	X Brace	No	Yes	0.0000	0.0000
T10	100.00-80.00	10.00	X Brace	No	No	0.0000	0.0000
T11	80.00-60.00	10.00	X Brace	No	No	0.0000	0.0000
T12	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T13	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T14	20.00-0.00	20.00	X Brace	No	No	0.0000	0.0000

### Tower Section Geometry (cont'd)

Tower Elevation	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
ft						
T1 245.00-230.00	Solid Round	1 1/2	A572-50 (50 ksi)	Solid Round	3/4	A572-50 (50 ksi)
T2 230.00-210.00	Solid Round	2	A572-50 (50 ksi)	Solid Round	7/8	A572-50 (50 ksi)
T3 210.00-190.00	Solid Round	2 1/2	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T4 190.00-180.00	Truss Leg	Pirod 105245	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T5 180.00-160.00	Truss Leg	Pirod 105217	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 160.00-140.00	Truss Leg	Pirod 105218	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T7 140.00-120.00	Truss Leg	Pirod 105218	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T8 120.00-110.00	Truss Leg	Pirod 105219	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T9 110.00-100.00	Truss Leg	Pirod 105219	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T10 100.00-80.00	Truss Leg	Pirod 105219	A572-50 (50 ksi)	Single Angle	L3x3x5/16	A36 (36 ksi)
T11 80.00-60.00	Truss Leg	Pirod 105220	A572-50 (50 ksi)	Single Angle	L3x3x5/16	A36 (36 ksi)
T12 60.00-40.00	Truss Leg	Pirod 105220	A572-50 (50 ksi)	Single Angle	L3 1/2x3 1/2x5/16	A36 (36 ksi)
T13 40.00-20.00	Truss Leg	Pirod 105220	A572-50 (50 ksi)	Single Angle	L4x4x1/4	A36 (36 ksi)
T14 20.00-0.00	Truss Leg	Pirod 112738	A572-50 (50 ksi)	Double Equal Angle	2L3 1/2x3 1/2x5/16x3/4	A36 (36 ksi)

### Tower Section Geometry (cont'd)

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 4 of 45
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Tower Elevation <i>ft</i>	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 245.00-230.00	Solid Round	7/8	A572-50 (50 ksi)	Solid Round	7/8	A572-50 (50 ksi)
T2 230.00-210.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T3 210.00-190.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
T9 110.00-100.00	Equal Angle	L3x3x5/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation <i>ft</i>	Gusset Area (per face) <i>ft<sup>2</sup></i>	Gusset Thickness <i>in</i>	Gusset Grade	Adjust. Factor <i>A<sub>f</sub></i>	Adjust. Factor <i>A<sub>r</sub></i>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals <i>in</i>	Double Angle Stitch Bolt Spacing Horizontals <i>in</i>
T1 245.00-230.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T2 230.00-210.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T3 210.00-190.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T4 190.00-180.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T5 180.00-160.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T6 160.00-140.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T7 140.00-120.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T8 120.00-110.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T9 110.00-100.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T10 100.00-80.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T11 80.00-60.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T12 60.00-40.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T13 40.00-20.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000
T14 20.00-0.00	0.00	0.0000	A36 (36 ksi)	1	1	1.05	36.0000	36.0000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 5 of 45
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### Tower Section Geometry (cont'd)

Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	K Factors <sup>1</sup>							
			Legs	X Brace Diags	K Brace Diags	Single Diags	Girls	Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y
T1	No	No	1	1	1	1	1	1	1	1
245.00-230.00										
T2	No	No	1	1	1	1	1	1	1	1
230.00-210.00										
T3	No	No	1	1	1	1	1	1	1	1
210.00-190.00										
T4	No	No	1	1	1	1	1	1	1	1
190.00-180.00										
T5	No	No	1	1	1	1	1	1	1	1
180.00-160.00										
T6	No	No	1	1	1	1	1	1	1	1
160.00-140.00										
T7	No	No	1	1	1	1	1	1	1	1
140.00-120.00										
T8	No	No	1	1	1	1	1	1	1	1
120.00-110.00										
T9	No	No	1	1	1	1	1	1	1	1
110.00-100.00										
T10	No	No	1	1	1	1	1	1	1	1
100.00-80.00										
T11	No	No	1	1	1	1	1	1	1	1
80.00-60.00										
T12	No	No	1	1	1	1	1	1	1	1
60.00-40.00										
T13	No	No	1	1	1	1	1	1	1	1
40.00-20.00										
T14	No	No	1	1	1	1	1	1	1	1
20.00-0.00										

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### Tower Section Geometry (cont'd)

Tower Elevation ft	Truss-Leg K Factors					
	Truss-Legs Used As Leg Members			Truss-Legs Used As Inner Members		
	Leg Panels	X Brace Diagonals	Z Brace Diagonals	Leg Panels	X Brace Diagonals	Z Brace Diagonals
T4	1	0.5	0.85	1	0.5	0.85
190.00-180.00						
T5	1	0.5	0.85	1	0.5	0.85
180.00-160.00						
T6	1	0.5	0.85	1	0.5	0.85
160.00-140.00						
T7	1	0.5	0.85	1	0.5	0.85
140.00-120.00						
T8	1	0.5	0.85	1	0.5	0.85
120.00-110.00						

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T9	1	0.5	0.85	1	0.5	0.85
110.00-100.00						
T10	1	0.5	0.85	1	0.5	0.85
100.00-80.00						
T11	1	0.5	0.85	1	0.5	0.85
80.00-60.00						
T12	1	0.5	0.85	1	0.5	0.85
60.00-40.00						
T13	1	0.5	0.85	1	0.5	0.85
40.00-20.00						
T14	1	0.5	0.85	1	0.5	0.85
20.00-0.00						

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 245.00-230.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 230.00-210.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 210.00-190.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 190.00-180.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T5 180.00-160.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T6 160.00-140.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T7 140.00-120.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T8 120.00-110.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T9 110.00-100.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T10 100.00-80.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T11 80.00-60.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T12 60.00-40.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T13 40.00-20.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T14 20.00-0.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1

### Tower Section Geometry (cont'd)

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Tower Elevation ft	Leg Connection Type	Leg Bolt Size in	Leg No.	Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
				Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 245.00-230.00	Sleeve DS	0.6250	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 230.00-210.00	Sleeve DS	0.7500	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3 210.00-190.00	Flange	1.0000	6	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 190.00-180.00	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5 180.00-160.00	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 160.00-140.00	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 140.00-120.00	Flange	1.0000	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8 120.00-110.00	Flange	1.0000	0	1.2500	1	0.6250	0	0.0000	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T9 110.00-100.00	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T10 100.00-80.00	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T11 80.00-60.00	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T12 60.00-40.00	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T13 40.00-20.00	Flange	1.2500	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T14 20.00-0.00	Flange	1.2500	6	1.0000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 5/8 (Sprint)	A	Yes	Ar (CaAa)	245.00 - 0.00	-10.0000	0.42	6	3	1.9800	1.9800		1.04
1 1/4" Hybriflex Cables (245')	A	Yes	Ar (CfAe)	245.00 - 0.00	-15.0000	0.4	3	3	1.5400	1.5400		1.08
"T-Bracket" (245')	A	Yes	Af (CfAe)	245.00 - 0.00	-5.0000	0.47	1	1	0.7500	0.7500	3.0000	1.50
1 5/8 (232')	B	Yes	Ar (CfAe)	232.00 - 0.00	-10.0000	0.42	15	8	1.9800	1.9800		1.04
1 5/8 (232')	B	Yes	Ar (CfAe)	232.00 - 0.00	-25.0000	0.36	6	3	1.9800	1.9800		1.04
"T-Bracket" (232')	B	Yes	Af (CfAe)	232.00 - 0.00	-5.0000	0.47	1	1	0.7500	0.7500	3.0000	1.50
FEEDLINE LADDER (160')	C	Yes	Af (CfAe)	160.00 - 0.00	0.0000	0.4	1	1	3.0000	3.0000	12.0000	8.40
1/2 (245')	A	Yes	Ar (CfAe)	245.00 - 0.00	-8.0000	0.45	1	1	0.5800	0.5800		0.25
7/8	A	Yes	Ar (CfAe)	135.00 - 0.00	-8.0000	0.45	2	2	1.1100	1.1100		0.54

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Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
(135') 7/8	A	Yes	Ar (CfAe)	125.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54
(125') 1/2	A	Yes	Ar (CfAe)	125.00 - 0.00	-8.0000	0.45	1	1	0.5800	0.5800		0.25
(125') 7/8	A	Yes	Ar (CfAe)	110.00 - 0.00	-8.0000	0.45	2	2	1.1100	1.1100		0.54
(110') EW63	A	Yes	Af (CfAe)	105.00 - 0.00	-8.0000	0.45	1	1	1.5742	1.5742	5.0668	0.51
(105') 7/8	A	Yes	Ar (CfAe)	60.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54
(60') 7/8	A	Yes	Ar (CfAe)	50.00 - 0.00	-8.0000	0.45	1	1	1.1100	1.1100		0.54
(50') ALU Fiber Optic Cable (Sprint - Proposed)	A	Yes	Ar (CfAe)	245.00 - 0.00	-10.0000	0.4	1	1	1.2500	1.2500		0.99

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
T1	245.00-230.00	A	8.063	0.938	16.252	0.000	0.18
		B	3.630	0.125	0.000	0.000	0.05
		C	0.000	0.000	0.000	0.000	0.00
T2	230.00-210.00	A	10.750	1.250	21.670	0.000	0.24
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	0.000	0.000	0.000	0.00
T3	210.00-190.00	A	10.750	1.250	21.670	0.000	0.24
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	0.000	0.000	0.000	0.00
T4	190.00-180.00	A	5.375	0.625	10.835	0.000	0.12
		B	18.150	0.625	0.000	0.000	0.23
		C	0.000	0.000	0.000	0.000	0.00
T5	180.00-160.00	A	10.750	1.250	21.670	0.000	0.24
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	0.000	0.000	0.000	0.00
T6	160.00-140.00	A	10.750	1.250	21.670	0.000	0.24
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
T7	140.00-120.00	A	14.229	1.250	21.670	0.000	0.26
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
T8	120.00-110.00	A	8.633	0.625	10.835	0.000	0.14
		B	18.150	0.625	0.000	0.000	0.23
		C	0.000	2.500	0.000	0.000	0.08
T9	110.00-100.00	A	10.483	1.281	10.835	0.000	0.15
		B	18.150	0.625	0.000	0.000	0.23
		C	0.000	2.500	0.000	0.000	0.08
T10	100.00-80.00	A	20.967	3.874	21.670	0.000	0.31
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
T11	80.00-60.00	A	20.967	3.874	21.670	0.000	0.31
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
T12	60.00-40.00	A	23.742	3.874	21.670	0.000	0.33



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	9 of 45
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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T13	40.00-20.00	B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
		A	24.667	3.874	21.670	0.000	0.34
T14	20.00-0.00	B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17
		A	24.667	3.874	21.670	0.000	0.34
		B	36.300	1.250	0.000	0.000	0.47
		C	0.000	5.000	0.000	0.000	0.17

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T1	245.00-230.00	A	0.500	14.313	1.771	17.752	0.000	0.42
		B		5.463	0.236	0.000	0.000	0.11
		C		0.000	0.000	0.000	0.000	0.00
T2	230.00-210.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	0.000	0.000	0.000	0.00
T3	210.00-190.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	0.000	0.000	0.000	0.00
T4	190.00-180.00	A	0.500	9.542	1.181	11.835	0.000	0.28
		B		27.317	1.181	0.000	0.000	0.56
		C		0.000	0.000	0.000	0.000	0.00
T5	180.00-160.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	0.000	0.000	0.000	0.00
T6	160.00-140.00	A	0.500	19.083	2.361	23.670	0.000	0.55
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T7	140.00-120.00	A	0.500	25.896	2.361	23.670	0.000	0.61
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T8	120.00-110.00	A	0.500	16.133	1.181	11.835	0.000	0.33
		B		27.317	1.181	0.000	0.000	0.56
		C		0.000	3.056	0.000	0.000	0.11
T9	110.00-100.00	A	0.500	19.650	2.114	11.835	0.000	0.37
		B		27.317	1.181	0.000	0.000	0.56
		C		0.000	3.056	0.000	0.000	0.11
T10	100.00-80.00	A	0.500	39.300	6.096	23.670	0.000	0.76
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T11	80.00-60.00	A	0.500	39.300	6.096	23.670	0.000	0.76
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T12	60.00-40.00	A	0.500	44.575	6.096	23.670	0.000	0.81
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T13	40.00-20.00	A	0.500	46.333	6.096	23.670	0.000	0.82
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22
T14	20.00-0.00	A	0.500	46.333	6.096	23.670	0.000	0.82
		B		54.633	2.361	0.000	0.000	1.12
		C		0.000	6.111	0.000	0.000	0.22

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	10 of 45
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### Feed Line Shielding

Section	Elevation ft	Face	$A_R$	$A_{R\ Ice}$	$A_F$	$A_{F\ Ice}$
			ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>
T1	245.00-230.00	A	1.110	4.314	0.000	0.000
		B	0.254	0.897	0.000	0.000
		C	0.000	0.000	0.000	0.000
T2	230.00-210.00	A	1.646	5.901	0.000	0.000
		B	2.823	9.203	0.000	0.000
		C	0.000	0.000	0.000	0.000
T3	210.00-190.00	A	1.809	6.098	0.000	0.000
		B	3.102	9.510	0.000	0.000
		C	0.000	0.000	0.000	0.000
T4	190.00-180.00	A	0.000	0.637	0.946	1.594
		B	0.000	0.994	1.622	2.485
		C	0.000	0.000	0.000	0.000
T5	180.00-160.00	A	0.000	1.076	1.597	2.690
		B	0.000	1.678	2.738	4.196
		C	0.000	0.000	0.000	0.000
T6	160.00-140.00	A	0.000	0.921	1.367	2.302
		B	0.000	1.436	2.343	3.591
		C	0.000	0.166	0.312	0.416
T7	140.00-120.00	A	0.000	0.986	1.717	2.957
		B	0.000	1.298	2.540	3.893
		C	0.000	0.150	0.338	0.451
T8	120.00-110.00	A	0.000	0.534	0.910	1.603
		B	0.000	0.614	1.202	1.842
		C	0.000	0.071	0.160	0.213
T9	110.00-100.00	A	0.000	0.861	1.458	2.584
		B	0.000	0.837	1.638	2.510
		C	0.000	0.097	0.218	0.291
T10	100.00-80.00	A	0.000	1.231	2.088	3.692
		B	0.000	1.153	2.257	3.460
		C	0.000	0.134	0.301	0.401
T11	80.00-60.00	A	0.000	1.188	2.016	3.563
		B	0.000	1.113	2.179	3.339
		C	0.000	0.129	0.290	0.387
T12	60.00-40.00	A	0.000	1.256	2.473	4.396
		B	0.000	1.084	2.476	3.794
		C	0.000	0.126	0.330	0.440
T13	40.00-20.00	A	0.000	1.264	2.839	5.054
		B	0.000	1.063	2.773	4.250
		C	0.000	0.123	0.369	0.492
T14	20.00-0.00	A	0.000	0.756	1.486	2.645
		B	0.000	0.635	1.451	2.224
		C	0.000	0.074	0.193	0.258

### Feed Line Center of Pressure

Section	Elevation ft	$CP_x$	$CP_z$	$CP_x$	$CP_z$
		in	in	Ice in	Ice in
T1	245.00-230.00	2.0901	-4.0440	2.0049	-3.5868
T2	230.00-210.00	3.7501	-0.4007	3.7743	0.0508
T3	210.00-190.00	4.0220	-0.6905	4.0905	-0.2060

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 11 of 45
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Section	Elevation	CP <sub>X</sub>	CP <sub>Z</sub>	CP <sub>X</sub>	CP <sub>Z</sub>
		Ice	Ice	Ice	Ice
	ft	in	in	in	in
T4	190.00-180.00	3.6349	-0.8813	3.7417	-0.4080
T5	180.00-160.00	4.8067	-1.5711	5.0281	-0.9759
T6	160.00-140.00	5.1904	-1.7387	5.6740	-1.1254
T7	140.00-120.00	6.1134	-3.2176	6.7468	-2.8409
T8	120.00-110.00	6.7189	-4.4539	7.4087	-4.4038
T9	110.00-100.00	6.5671	-5.7738	7.2004	-5.9769
T10	100.00-80.00	7.8382	-7.3344	8.6371	-7.6433
T11	80.00-60.00	8.6018	-8.2417	9.4943	-8.6048
T12	60.00-40.00	9.0169	-9.8116	10.0355	-10.5926
T13	40.00-20.00	9.3532	-10.6906	10.5194	-11.7251
T14	20.00-0.00	10.7777	-12.2738	12.2636	-13.7062

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Horz Lateral	Vert					
Lightning Rod 2"x10' (Tower)	C	From Leg	5.00	0.0000	247.00	No Ice	2.00	2.00	0.04
			0.00		1/2" Ice	3.02	3.02	0.06	
Flash Beacon Lighting (Tower)	A	From Leg	0.00	0.0000	247.00	No Ice	2.50	2.50	0.03
			0.00		1/2" Ice	2.76	2.76	0.06	
APXVSPP18-C-A20 w/ Mounting Pipe (Sprint)	A	From Face	4.00	0.0000	247.00	No Ice	8.56	6.95	0.08
			-2.00		1/2" Ice	9.21	8.13	0.15	
APXV9ERR18-C-A20 w/ 6' Mount Pipe (Sprint)	B	From Face	4.00	0.0000	247.00	No Ice	10.35	6.37	0.06
			-2.00		1/2" Ice	10.97	7.37	0.13	
APXVSPP18-C-A20 w/ Mounting Pipe (Sprint)	C	From Face	4.00	0.0000	247.00	No Ice	8.56	6.95	0.08
			-2.00		1/2" Ice	9.21	8.13	0.15	
(2) Panasonic RRH 1900MHZ (Sprint)	A	From Face	4.00	0.0000	247.00	No Ice	2.71	2.61	0.06
			2.00		1/2" Ice	2.95	2.84	0.08	
(2) Panasonic RRH 1900MHZ (Sprint)	B	From Face	4.00	0.0000	247.00	No Ice	2.71	2.61	0.06
			2.00		1/2" Ice	2.95	2.84	0.08	
(2) Panasonic RRH 1900MHZ (Sprint)	C	From Face	4.00	0.0000	247.00	No Ice	2.71	2.61	0.06
			2.00		1/2" Ice	2.95	2.84	0.08	
Andrew 800MHz RRH (Sprint)	A	From Face	4.00	0.0000	247.00	No Ice	2.49	1.97	0.06
			2.00		1/2" Ice	2.57	2.17	0.08	
Andrew 800MHz RRH (Sprint)	B	From Face	4.00	0.0000	247.00	No Ice	2.49	1.97	0.06
			2.00		1/2" Ice	2.57	2.17	0.08	
Andrew 800MHz RRH (Sprint)	C	From Face	4.00	0.0000	247.00	No Ice	2.49	1.97	0.06
			2.00		1/2" Ice	2.57	2.17	0.08	
IBC1900BB-1 Combiner (Sprint)	A	From Face	4.00	0.0000	247.00	No Ice	1.13	0.54	0.02
			0.00		1/2" Ice	1.27	0.65	0.03	

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Lateral						°
IBC1900BB-1 Combiner (Sprint)	B	From Face	0.00		0.0000	247.00	No Ice	1.13	0.54	0.02
			4.00				1/2" Ice	1.27	0.65	0.03
			0.00							
IBC1900BB-1 Combiner (Sprint)	C	From Face	4.00		0.0000	247.00	No Ice	1.13	0.54	0.02
			0.00				1/2" Ice	1.27	0.65	0.03
			0.00							
IBC1900HG-2A Combiner (Sprint)	A	From Face	4.00		0.0000	247.00	No Ice	1.13	0.54	0.02
			0.00				1/2" Ice	1.27	0.65	0.03
			0.00							
IBC1900HG-2A Combiner (Sprint)	B	From Face	4.00		0.0000	247.00	No Ice	1.13	0.54	0.02
			0.00				1/2" Ice	1.27	0.65	0.03
			0.00							
IBC1900HG-2A Combiner (Sprint)	C	From Face	4.00		0.0000	247.00	No Ice	1.13	0.54	0.02
			0.00				1/2" Ice	1.27	0.65	0.03
			0.00							
PiROD Rotatable Platform #122379 (Sprint)	C	None			0.0000	247.00	No Ice	24.90	24.90	1.81
							1/2" Ice	30.70	30.70	2.44
2.5" Dia. 12' OMNI	A	From Leg	4.00		0.0000	135.00	No Ice	2.50	2.50	0.03
			0.00				1/2" Ice	3.53	3.53	0.05
			5.00							
4' Standoff Mount	A	From Leg	2.00		0.0000	135.00	No Ice	2.72	2.72	0.05
			0.00				1/2" Ice	4.91	4.91	0.09
			0.00							
2.5" Dia. 12' OMNI	C	From Leg	4.00		0.0000	135.00	No Ice	2.50	2.50	0.03
			0.00				1/2" Ice	3.53	3.53	0.05
			5.00							
4' Standoff Mount	C	From Leg	2.00		0.0000	135.00	No Ice	2.72	2.72	0.05
			0.00				1/2" Ice	4.91	4.91	0.09
			0.00							
20' Omni	A	From Leg	6.00		0.0000	125.00	No Ice	6.00	6.00	0.06
			0.00				1/2" Ice	8.03	8.03	0.10
			10.00							
6' Standoff Mount	A	From Leg	3.00		0.0000	125.00	No Ice	4.97	6.12	0.07
			0.00				1/2" Ice	6.12	7.27	0.13
			0.00							
(3) L-810 Obstruction Lights w/ Mount Kit (Tower)	C	None			0.0000	125.00	No Ice	0.85	0.43	0.05
							1/2" Ice	0.97	0.53	0.05
2.5" Dia. 12' OMNI	C	From Leg	4.00		0.0000	110.00	No Ice	2.50	2.50	0.03
			0.00				1/2" Ice	3.53	3.53	0.05
			5.00							
4' Standoff Mount	C	From Leg	2.00		0.0000	110.00	No Ice	2.72	2.72	0.05
			0.00				1/2" Ice	4.91	4.91	0.09
			0.00							
Camera with Mount	A	From Leg	0.00		0.0000	60.00	No Ice	5.60	5.60	0.15
			0.00				1/2" Ice	5.92	5.92	0.21
			0.00							
1.5" Dia 4' Omni w/Pipe Mount	A	From Leg	4.00		0.0000	50.00	No Ice	0.94	0.94	0.02
			0.00				1/2" Ice	1.39	1.39	0.03
			5.00							
4' Standoff Mount	A	From Leg	2.00		0.0000	50.00	No Ice	2.72	2.72	0.05
			0.00				1/2" Ice	4.91	4.91	0.09
			0.00							
APXV9TM14-120 (Sprint)	A	From Face	4.00		0.0000	247.00	No Ice	7.27	5.33	0.10
			6.00				1/2" Ice	7.80	6.05	0.16

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Lateral						°
				0.00						
APXV9TM14-120 (Sprint)	B	From Face	4.00	4.00	0.0000	247.00	No Ice	7.27	5.33	0.10
			6.00	6.00			1/2" Ice	7.80	6.05	0.16
			0.00	0.00						
APXV9TM14-120 (Sprint)	C	From Face	4.00	4.00	0.0000	247.00	No Ice	7.27	5.33	0.10
			6.00	6.00			1/2" Ice	7.80	6.05	0.16
			0.00	0.00						
TD-RRH 8x20 (Sprint)	A	From Face	4.00	4.00	0.0000	247.00	No Ice	4.72	1.70	0.07
			6.00	6.00			1/2" Ice	5.01	1.92	0.10
			0.00	0.00						
TD-RRH 8x20 (Sprint)	B	From Face	4.00	4.00	0.0000	247.00	No Ice	4.72	1.70	0.07
			6.00	6.00			1/2" Ice	5.01	1.92	0.10
			0.00	0.00						
TD-RRH 8x20 (Sprint)	C	From Face	4.00	4.00	0.0000	247.00	No Ice	4.72	1.70	0.07
			6.00	6.00			1/2" Ice	5.01	1.92	0.10
			0.00	0.00						
TMA (T-Mobile)	A	From Face	4.00	4.00	0.0000	232.00	No Ice	1.40	0.70	0.01
			0.00	0.00			1/2" Ice	1.56	0.82	0.02
			0.00	0.00						
TMA (T-Mobile)	B	From Face	4.00	4.00	0.0000	232.00	No Ice	1.40	0.70	0.01
			0.00	0.00			1/2" Ice	1.56	0.82	0.02
			0.00	0.00						
TMA (T-Mobile)	C	From Face	4.00	4.00	0.0000	232.00	No Ice	1.40	0.70	0.01
			0.00	0.00			1/2" Ice	1.56	0.82	0.02
			0.00	0.00						
PiROD 12' Universal T-Frame (3) (T-Mobile)	C	None			0.0000	232.00	No Ice	21.88	21.88	1.07
							1/2" Ice	30.68	30.68	1.49
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	A	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			-2.00	-2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	A	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			2.00	2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	B	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			-2.00	-2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	B	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			2.00	2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	C	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			-2.00	-2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						
AIR B2A/B4P w/ 6' Sch 40 Pipe Mount (T-Mobile)	C	From Face	4.00	4.00	0.0000	232.00	No Ice	6.75	5.65	0.10
			2.00	2.00			1/2" Ice	7.31	6.56	0.16
			0.00	0.00						

**Dishes**

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	14 of 45
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Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight	
				ft	°	°	ft	ft	ft <sup>2</sup>	K	
KP4F-23	B	Grid	From Face	1.00 -6.00 0.00	0.0000		110.00	4.00	No Ice 1/2" Ice	10.05 13.09	0.05 0.12
Andrew 6' w/Radome	B	Paraboloid w/Radome	From Face	1.00 -6.00 0.00	0.0000		105.00	6.00	No Ice 1/2" Ice	28.27 29.07	0.38 0.45

### Truss-Leg Properties

Section Designation	Area	Area Ice	Self Weight	Ice Weight	Equiv. Diameter	Equiv. Diameter Ice	Leg Area
	in <sup>2</sup>	in <sup>2</sup>	K	K	in	in	in <sup>2</sup>
Pirod 105245	1090.3344	1814.3549	0.68	0.22	7.5718	12.5997	5.3014
Pirod 105217	2130.7479	3520.4599	0.62	0.44	7.3984	12.2238	5.3014
Pirod 105218	2263.4687	3690.8612	0.75	0.46	7.8593	12.8155	7.2158
Pirod 105218	2263.4687	3690.8612	0.75	0.46	7.8593	12.8155	7.2158
Pirod 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirod 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirod 105219	2441.8688	3942.2854	0.94	0.49	8.4787	13.6885	9.4248
Pirod 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirod 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirod 105220	2578.8005	4132.5504	1.12	0.50	8.9542	14.3491	11.9282
Pirod 112738	3466.5160	5074.9521	1.69	0.68	12.0365	17.6214	14.7262

### Tower Pressures - No Ice

$$G_H = 1.101$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>AA</sub> In Face	C <sub>AA</sub> Out Face
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	%	ft <sup>2</sup>	ft <sup>2</sup>
T1	237.50	1.758	33	61.875	A	0.938	14.632	3.750	24.09	16.252	0.000
245.00-230.00					B	0.125	11.056		33.54	0.000	0.000
					C	0.000	7.680		48.83	0.000	0.000
T2	220.00	1.72	32	88.334	A	1.250	21.909	6.667	28.79	21.670	0.000
230.00-210.00					B	1.250	46.283		14.03	0.000	0.000
					C	0.000	12.806		52.07	0.000	0.000
T3	200.00	1.673	31	99.167	A	1.250	24.779	8.334	32.02	21.670	0.000
210.00-190.00					B	1.250	49.036		16.57	0.000	0.000
					C	0.000	15.838		52.62	0.000	0.000
T4	185.00	1.636	30	66.264	A	3.914	18.016	12.641	57.64	10.835	0.000
190.00-180.00					B	3.238	30.791		37.15	0.000	0.000
					C	4.235	12.641		74.90	0.000	0.000
T5	170.00	1.597	30	162.528	A	8.376	35.453	24.703	56.36	21.670	0.000
180.00-160.00					B	7.235	61.003		36.20	0.000	0.000
					C	8.723	24.703		73.90	0.000	0.000
T6	150.00	1.541	29	202.945	A	9.854	36.991	26.241	56.02	21.670	0.000
160.00-140.00					B	8.877	62.541		36.74	0.000	0.000
					C	14.658	26.241		64.16	0.000	0.000
T7	130.00	1.48	27	242.945	A	13.053	40.470	26.241	49.03	21.670	0.000

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	15 of 45
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	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
140.00-120.00					B	12.230	62.541		35.10	0.000	0.000
					C	18.182	26.241		59.07	0.000	0.000
T8	115.00	1.429	26	136.681	A	7.080	22.788	14.155	47.39	10.835	0.000
120.00-110.00					B	6.788	32.305		36.21	0.000	0.000
					C	9.705	14.155		59.32	0.000	0.000
T9	105.00	1.392	26	146.681	A	10.723	24.638	14.155	40.03	10.835	0.000
110.00-100.00					B	9.887	32.305		33.55	0.000	0.000
					C	13.182	14.155		51.78	0.000	0.000
T10	90.00	1.332	25	323.362	A	18.615	49.276	28.309	41.70	21.670	0.000
100.00-80.00					B	15.822	64.609		35.20	0.000	0.000
					C	21.529	28.309		56.80	0.000	0.000
T11	70.00	1.24	23	363.780	A	20.424	50.864	29.897	41.94	21.670	0.000
80.00-60.00					B	17.638	66.197		35.66	0.000	0.000
					C	23.276	29.897		56.23	0.000	0.000
T12	50.00	1.126	21	403.780	A	25.135	53.639	29.897	37.95	21.670	0.000
60.00-40.00					B	22.509	66.197		33.70	0.000	0.000
					C	28.405	29.897		51.28	0.000	0.000
T13	30.00	1	18	443.780	A	30.574	54.564	29.897	35.12	21.670	0.000
40.00-20.00					B	28.016	66.197		31.73	0.000	0.000
					C	34.170	29.897		46.67	0.000	0.000
T14	20.00-0.00	1	18	494.209	A	19.205	64.855	40.189	47.81	21.670	0.000
	10.00				B	16.616	76.489		43.17	0.000	0.000
					C	21.624	40.189		65.02	0.000	0.000

**Tower Pressure - With Ice**

$G_H = 1.101$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	l <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1	237.50	1.758	24	0.5000	63.125	A	1.771	25.310	6.250	23.08	17.752	0.000
245.00-230.00						B	0.236	19.878		31.07	0.000	0.000
						C	0.000	15.312		40.82	0.000	0.000
T2	220.00	1.72	24	0.5000	90.000	A	2.361	36.240	10.001	25.91	23.670	0.000
230.00-210.00						B	2.361	68.488		14.12	0.000	0.000
						C	0.000	23.057		43.37	0.000	0.000
T3	200.00	1.673	23	0.5000	100.834	A	2.361	39.661	11.668	27.77	23.670	0.000
210.00-190.00						B	2.361	71.799		15.73	0.000	0.000
						C	0.000	26.676		43.74	0.000	0.000
T4	185.00	1.636	23	0.5000	67.098	A	3.822	31.633	21.034	59.33	11.835	0.000
190.00-180.00						B	2.930	49.051		40.47	0.000	0.000
						C	4.235	22.728		78.01	0.000	0.000
T5	170.00	1.597	22	0.5000	164.197	A	8.393	62.310	40.814	57.73	23.670	0.000
180.00-160.00						B	6.888	97.258		39.19	0.000	0.000
						C	8.723	44.303		76.97	0.000	0.000
T6	150.00	1.541	21	0.5000	204.614	A	10.029	64.940	42.789	57.08	23.670	0.000
160.00-140.00						B	8.740	99.974		39.36	0.000	0.000
						C	15.665	46.611		68.71	0.000	0.000
T7	130.00	1.48	21	0.5000	244.614	A	12.924	72.206	42.789	50.26	23.670	0.000
140.00-120.00						B	11.988	100.632		37.99	0.000	0.000
						C	19.180	47.146		64.51	0.000	0.000
T8	115.00	1.429	20	0.5000	137.516	A	6.942	40.906	22.852	47.76	11.835	0.000
120.00-110.00						B	6.703	52.010		38.92	0.000	0.000
						C	10.207	25.236		64.48	0.000	0.000



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 16 of 45
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	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T9 110.00-100.00	105.00	1.392	19	0.5000	147.516	A	10.429	45.274	22.852	41.02	11.835	0.000
						B	9.570	52.965		36.54	0.000	0.000
						C	13.664	26.388		57.06	0.000	0.000
T10 100.00-80.00	90.00	1.332	18	0.5000	325.031	A	19.234	89.384	45.704	42.08	23.670	0.000
						B	15.731	104.794		37.92	0.000	0.000
						C	22.540	51.181		62.00	0.000	0.000
T11 80.00-60.00	70.00	1.24	17	0.5000	365.448	A	21.099	92.211	47.910	42.28	23.670	0.000
						B	17.588	107.619		38.26	0.000	0.000
						C	24.291	53.970		61.22	0.000	0.000
T12 60.00-40.00	50.00	1.126	16	0.5000	405.448	A	25.434	98.010	47.910	38.81	23.670	0.000
						B	22.301	108.241		36.70	0.000	0.000
						C	29.406	54.566		57.05	0.000	0.000
T13 40.00-20.00	30.00	1	14	0.5000	445.448	A	30.581	100.365	47.910	36.59	23.670	0.000
						B	27.650	108.866		35.09	0.000	0.000
						C	35.158	55.172		53.04	0.000	0.000
T14 20.00-0.00	10.00	1	14	0.5000	495.878	A	20.268	109.218	58.836	45.44	23.670	0.000
						B	16.954	117.638		43.71	0.000	0.000
						C	22.670	63.567		68.23	0.000	0.000

### Tower Pressure - Service

$$G_H = 1.101$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 245.00-230.00	237.50	1.758	11	61.875	A	0.938	14.632	3.750	24.09	16.252	0.000
					B	0.125	11.056		33.54	0.000	0.000
					C	0.000	7.680		48.83	0.000	0.000
T2 230.00-210.00	220.00	1.72	11	88.334	A	1.250	21.909	6.667	28.79	21.670	0.000
					B	1.250	46.283		14.03	0.000	0.000
					C	0.000	12.806		52.07	0.000	0.000
T3 210.00-190.00	200.00	1.673	11	99.167	A	1.250	24.779	8.334	32.02	21.670	0.000
					B	1.250	49.036		16.57	0.000	0.000
					C	0.000	15.838		52.62	0.000	0.000
T4 190.00-180.00	185.00	1.636	10	66.264	A	3.914	18.016	12.641	57.64	10.835	0.000
					B	3.238	30.791		37.15	0.000	0.000
					C	4.235	12.641		74.90	0.000	0.000
T5 180.00-160.00	170.00	1.597	10	162.528	A	8.376	35.453	24.703	56.36	21.670	0.000
					B	7.235	61.003		36.20	0.000	0.000
					C	8.723	24.703		73.90	0.000	0.000
T6 160.00-140.00	150.00	1.541	10	202.945	A	9.854	36.991	26.241	56.02	21.670	0.000
					B	8.877	62.541		36.74	0.000	0.000
					C	14.658	26.241		64.16	0.000	0.000
T7 140.00-120.00	130.00	1.48	9	242.945	A	13.053	40.470	26.241	49.03	21.670	0.000
					B	12.230	62.541		35.10	0.000	0.000
					C	18.182	26.241		59.07	0.000	0.000
T8 120.00-110.00	115.00	1.429	9	136.681	A	7.080	22.788	14.155	47.39	10.835	0.000
					B	6.788	32.305		36.21	0.000	0.000
					C	9.705	14.155		59.32	0.000	0.000
T9 110.00-100.00	105.00	1.392	9	146.681	A	10.723	24.638	14.155	40.03	10.835	0.000
					B	9.887	32.305		33.55	0.000	0.000
					C	13.182	14.155		51.78	0.000	0.000
T10 90.00	90.00	1.332	9	323.362	A	18.615	49.276	28.309	41.70	21.670	0.000

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	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
100.00-80.00					B	15.822	64.609		35.20	0.000	0.000
					C	21.529	28.309		56.80	0.000	0.000
T11	70.00	1.24	8	363.780	A	20.424	50.864	29.897	41.94	21.670	0.000
80.00-60.00					B	17.638	66.197		35.66	0.000	0.000
					C	23.276	29.897		56.23	0.000	0.000
T12	50.00	1.126	7	403.780	A	25.135	53.639	29.897	37.95	21.670	0.000
60.00-40.00					B	22.509	66.197		33.70	0.000	0.000
					C	28.405	29.897		51.28	0.000	0.000
T13	30.00	1	6	443.780	A	30.574	54.564	29.897	35.12	21.670	0.000
40.00-20.00					B	28.016	66.197		31.73	0.000	0.000
					C	34.170	29.897		46.67	0.000	0.000
T14	20.00-0.00	1	6	494.209	A	19.205	64.855	40.189	47.81	21.670	0.000
	10.00				B	16.616	76.489		43.17	0.000	0.000
					C	21.624	40.189		65.02	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F <sub>a</sub>	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K	e						ft <sup>2</sup>	K	plf	
T1	0.23	0.60	A	0.252	2.433	0.602	1	1	9.750	1.43	95.33	A
245.00-230.00			B	0.181	2.662	0.587	1	1	6.611			
			C	0.124	2.869	0.578	1	1	4.438			
T2	0.71	1.25	A	0.262	2.401	0.605	1	1	14.506	3.00	149.84	B
230.00-210.00			B	0.538	1.855	0.718	1	1	34.466			
			C	0.145	2.79	0.581	1	1	7.436			
T3	0.71	1.85	A	0.262	2.401	0.605	1	1	16.244	3.03	151.66	B
210.00-190.00			B	0.507	1.891	0.701	1	1	35.631			
			C	0.16	2.736	0.583	1	1	9.234			
T4	0.36	1.24	A	0.331	2.217	0.626	1	1	15.189	1.92	192.47	B
190.00-180.00			B	0.514	1.883	0.704	1	1	24.930			
			C	0.255	2.424	0.603	1	1	11.858			
T5	0.71	2.33	A	0.27	2.38	0.607	1	1	29.899	3.83	191.67	B
180.00-160.00			B	0.42	2.026	0.66	1	1	47.490			
			C	0.206	2.577	0.592	1	1	23.336			
T6	0.88	2.79	A	0.231	2.496	0.597	1	1	31.944	3.98	198.79	B
160.00-140.00			B	0.352	2.167	0.633	1	1	48.476			
			C	0.202	2.591	0.591	1	1	30.159			
T7	0.90	2.96	A	0.22	2.53	0.595	1	1	37.123	4.14	207.05	B
140.00-120.00			B	0.308	2.276	0.618	1	1	50.900			
			C	0.183	2.654	0.587	1	1	33.587			
T8	0.46	1.79	A	0.219	2.535	0.594	1	1	20.624	2.12	211.70	B
120.00-110.00			B	0.286	2.334	0.612	1	1	26.549			
			C	0.175	2.683	0.586	1	1	17.993			
T9	0.47	2.07	A	0.241	2.465	0.6	1	1	25.497	2.26	226.49	B
110.00-100.00			B	0.288	2.329	0.612	1	1	29.664			
			C	0.186	2.642	0.588	1	1	21.500			
T10	0.95	4.21	A	0.21	2.563	0.592	1	1	47.810	4.21	210.38	B
100.00-80.00			B	0.249	2.441	0.602	1	1	54.689			
			C	0.154	2.756	0.582	1	1	38.009			
T11	0.95	4.87	A	0.196	2.61	0.59	1	1	50.413	4.15	207.47	B
80.00-60.00			B	0.23	2.497	0.597	1	1	57.163			
			C	0.146	2.786	0.581	1	1	40.643			
T12	0.96	5.29	A	0.195	2.612	0.589	1	1	56.750	4.09	204.35	B
60.00-40.00			B	0.22	2.532	0.595	1	1	61.870			
			C	0.144	2.792	0.581	1	1	45.764			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 18 of 45
	<b>Project</b> Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b> 16:11:49 12/30/14
	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T13 40.00-20.00	0.97	5.30	A	0.192	2.623	0.589	1	1	62.700	3.94	197.02	B
			B	0.212	2.555	0.593	1	1	67.270			
			C	0.144	2.792	0.581	1	1	51.529			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	1	1	57.129	3.75	187.27	B
			B	0.188	2.635	0.588	1	1	61.598			
			C	0.125	2.865	0.578	1	1	44.852			
Sum Weight:	10.23	44.37						OTM	5258.44 kip-ft	45.85		

### Tower Forces - No Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	0.825	1	9.586	1.42	94.38	A
			B	0.181	2.662	0.587	0.825	1	6.589			
			C	0.124	2.869	0.578	0.825	1	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	0.825	1	14.288	2.98	149.13	B
			B	0.538	1.855	0.718	0.825	1	34.247			
			C	0.145	2.79	0.581	0.825	1	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	0.825	1	16.026	3.02	150.95	B
			B	0.507	1.891	0.701	0.825	1	35.412			
			C	0.16	2.736	0.583	0.825	1	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	0.825	1	14.505	1.89	188.92	B
			B	0.514	1.883	0.704	0.825	1	24.364			
			C	0.255	2.424	0.603	0.825	1	11.117			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	0.825	1	28.433	3.75	187.50	B
			B	0.42	2.026	0.66	0.825	1	46.224			
			C	0.206	2.577	0.592	0.825	1	21.809			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	0.825	1	30.219	3.87	193.51	B
			B	0.352	2.167	0.633	0.825	1	46.922			
			C	0.202	2.591	0.591	0.825	1	27.594			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	0.825	1	34.839	3.99	199.72	B
			B	0.308	2.276	0.618	0.825	1	48.759			
			C	0.183	2.654	0.587	0.825	1	30.405			
T8 120.00-110.00	0.46	1.79	A	0.219	2.535	0.594	0.825	1	19.385	2.04	203.64	B
			B	0.286	2.334	0.612	0.825	1	25.361			
			C	0.175	2.683	0.586	0.825	1	16.295			
T9 110.00-100.00	0.47	2.07	A	0.241	2.465	0.6	0.825	1	23.620	2.15	215.07	B
			B	0.288	2.329	0.612	0.825	1	27.934			
			C	0.186	2.642	0.588	0.825	1	19.194			
T10 100.00-80.00	0.95	4.21	A	0.21	2.563	0.592	0.825	1	44.553	4.02	201.21	B
			B	0.249	2.441	0.602	0.825	1	51.920			
			C	0.154	2.756	0.582	0.825	1	34.241			
T11 80.00-60.00	0.95	4.87	A	0.196	2.61	0.59	0.825	1	46.838	3.95	197.75	B
			B	0.23	2.497	0.597	0.825	1	54.076			
			C	0.146	2.786	0.581	0.825	1	36.570			
T12 60.00-40.00	0.96	5.29	A	0.195	2.612	0.589	0.825	1	52.351	3.86	192.92	B
			B	0.22	2.532	0.595	0.825	1	57.931			
			C	0.144	2.792	0.581	0.825	1	40.793			
T13 40.00-20.00	0.97	5.30	A	0.192	2.623	0.589	0.825	1	57.349	3.69	184.27	B
			B	0.212	2.555	0.593	0.825	1	62.367			
			C	0.144	2.792	0.581	0.825	1	45.549			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	0.825	1	53.768	3.59	179.48	B
			B	0.188	2.635	0.588	0.825	1	58.691			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 19 of 45
	<b>Project</b> Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b> 16:11:49 12/30/14
	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
Sum Weight:	10.23	44.37	C	0.125	2.865	0.578	0.825	1 OTM	41.067 5121.42 kip-ft	44.22		

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	0.8	1	9.563	1.41	94.25	A
			B	0.181	2.662	0.587	0.8	1	6.586			
			C	0.124	2.869	0.578	0.8	1	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	0.8	1	14.256	2.98	149.03	B
			B	0.538	1.855	0.718	0.8	1	34.216			
			C	0.145	2.79	0.581	0.8	1	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	0.8	1	15.994	3.02	150.85	B
			B	0.507	1.891	0.701	0.8	1	35.381			
			C	0.16	2.736	0.583	0.8	1	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	0.8	1	14.407	1.88	188.41	B
			B	0.514	1.883	0.704	0.8	1	24.283			
			C	0.255	2.424	0.603	0.8	1	11.011			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	0.8	1	28.224	3.74	186.90	B
			B	0.42	2.026	0.66	0.8	1	46.043			
			C	0.206	2.577	0.592	0.8	1	21.591			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	0.8	1	29.973	3.86	192.75	B
			B	0.352	2.167	0.633	0.8	1	46.700			
			C	0.202	2.591	0.591	0.8	1	27.228			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	0.8	1	34.512	3.97	198.67	B
			B	0.308	2.276	0.618	0.8	1	48.454			
			C	0.183	2.654	0.587	0.8	1	29.950			
T8 120.00-110.00	0.46	1.79	A	0.219	2.535	0.594	0.8	1	19.208	2.02	202.49	B
			B	0.286	2.334	0.612	0.8	1	25.192			
			C	0.175	2.683	0.586	0.8	1	16.052			
T9 110.00-100.00	0.47	2.07	A	0.241	2.465	0.6	0.8	1	23.352	2.13	213.44	B
			B	0.288	2.329	0.612	0.8	1	27.686			
			C	0.186	2.642	0.588	0.8	1	18.864			
T10 100.00-80.00	0.95	4.21	A	0.21	2.563	0.592	0.8	1	44.087	4.00	199.90	B
			B	0.249	2.441	0.602	0.8	1	51.524			
			C	0.154	2.756	0.582	0.8	1	33.703			
T11 80.00-60.00	0.95	4.87	A	0.196	2.61	0.59	0.8	1	46.328	3.93	196.36	B
			B	0.23	2.497	0.597	0.8	1	53.635			
			C	0.146	2.786	0.581	0.8	1	35.988			
T12 60.00-40.00	0.96	5.29	A	0.195	2.612	0.589	0.8	1	51.723	3.83	191.29	B
			B	0.22	2.532	0.595	0.8	1	57.369			
			C	0.144	2.792	0.581	0.8	1	40.083			
T13 40.00-20.00	0.97	5.30	A	0.192	2.623	0.589	0.8	1	56.585	3.65	182.45	B
			B	0.212	2.555	0.593	0.8	1	61.667			
			C	0.144	2.792	0.581	0.8	1	44.695			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	0.8	1	53.288	3.57	178.36	B
			B	0.188	2.635	0.588	0.8	1	58.275			
			C	0.125	2.865	0.578	0.8	1	40.527			
Sum Weight:	10.23	44.37						OTM	5101.85 kip-ft	43.99		

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	20 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	0.85	1	9.609	1.42	94.52	A
			B	0.181	2.662	0.587	0.85	1	6.592			
			C	0.124	2.869	0.578	0.85	1	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	0.85	1	14.319	2.98	149.23	B
			B	0.538	1.855	0.718	0.85	1	34.278			
			C	0.145	2.79	0.581	0.85	1	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	0.85	1	16.057	3.02	151.05	B
			B	0.507	1.891	0.701	0.85	1	35.443			
			C	0.16	2.736	0.583	0.85	1	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	0.85	1	14.602	1.89	189.43	B
			B	0.514	1.883	0.704	0.85	1	24.445			
			C	0.255	2.424	0.603	0.85	1	11.223			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	0.85	1	28.642	3.76	188.09	B
			B	0.42	2.026	0.66	0.85	1	46.405			
			C	0.206	2.577	0.592	0.85	1	22.027			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	0.85	1	30.466	3.89	194.26	B
			B	0.352	2.167	0.633	0.85	1	47.144			
			C	0.202	2.591	0.591	0.85	1	27.961			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	0.85	1	35.165	4.02	200.76	B
			B	0.308	2.276	0.618	0.85	1	49.065			
			C	0.183	2.654	0.587	0.85	1	30.859			
T8 120.00-110.00	0.46	1.79	A	0.219	2.535	0.594	0.85	1	19.562	2.05	204.79	B
			B	0.286	2.334	0.612	0.85	1	25.531			
			C	0.175	2.683	0.586	0.85	1	16.537			
T9 110.00-100.00	0.47	2.07	A	0.241	2.465	0.6	0.85	1	23.888	2.17	216.70	B
			B	0.288	2.329	0.612	0.85	1	28.181			
			C	0.186	2.642	0.588	0.85	1	19.523			
T10 100.00-80.00	0.95	4.21	A	0.21	2.563	0.592	0.85	1	45.018	4.05	202.52	B
			B	0.249	2.441	0.602	0.85	1	52.315			
			C	0.154	2.756	0.582	0.85	1	34.779			
T11 80.00-60.00	0.95	4.87	A	0.196	2.61	0.59	0.85	1	47.349	3.98	199.14	B
			B	0.23	2.497	0.597	0.85	1	54.517			
			C	0.146	2.786	0.581	0.85	1	37.152			
T12 60.00-40.00	0.96	5.29	A	0.195	2.612	0.589	0.85	1	52.980	3.89	194.55	B
			B	0.22	2.532	0.595	0.85	1	58.494			
			C	0.144	2.792	0.581	0.85	1	41.503			
T13 40.00-20.00	0.97	5.30	A	0.192	2.623	0.589	0.85	1	58.114	3.72	186.09	B
			B	0.212	2.555	0.593	0.85	1	63.068			
			C	0.144	2.792	0.581	0.85	1	46.404			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	0.85	1	54.248	3.61	180.59	B
			B	0.188	2.635	0.588	0.85	1	59.106			
			C	0.125	2.865	0.578	0.85	1	41.608			
Sum Weight:	10.23	44.37						OTM	5141.00 kip-ft	44.45		

### Tower Forces - With Ice - Wind Normal To Face



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 21 of 45
	<b>Project</b> Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b> 16:11:49 12/30/14
	<b>Client</b> Sprint - TWS-019	<b>Designed by</b> MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.53	0.80	A	0.429	2.009	0.664	1	1	18.573	1.48	98.52	A
			B	0.319	2.248	0.622	1	1	12.596			
			C	0.243	2.46	0.6	1	1	9.187			
T2 230.00-210.00	1.68	1.56	A	0.429	2.01	0.664	1	1	26.418	3.61	180.61	B
			B	0.787	1.807	0.886	1	1	63.045			
			C	0.256	2.419	0.603	1	1	13.914			
T3 210.00-190.00	1.68	2.21	A	0.417	2.032	0.659	1	1	28.481	3.48	173.88	B
			B	0.735	1.782	0.846	1	1	63.094			
			C	0.265	2.395	0.606	1	1	16.157			
T4 190.00-180.00	0.84	1.73	A	0.528	1.866	0.712	1	1	26.357	2.36	235.94	B
			B	0.775	1.799	0.876	1	1	45.903			
			C	0.402	2.06	0.652	1	1	19.062			
T5 180.00-160.00	1.68	4.01	A	0.431	2.007	0.665	1	1	49.803	4.16	208.13	B
			B	0.634	1.787	0.775	1	1	82.280			
			C	0.323	2.237	0.623	1	1	36.332			
T6 160.00-140.00	1.90	4.54	A	0.366	2.134	0.638	1	1	51.491	4.07	203.43	B
			B	0.531	1.863	0.714	1	1	80.119			
			C	0.304	2.284	0.617	1	1	44.436			
T7 140.00-120.00	1.96	4.82	A	0.348	2.176	0.632	1	1	58.542	4.08	204.04	B
			B	0.46	1.957	0.678	1	1	80.227			
			C	0.271	2.376	0.607	1	1	47.821			
T8 120.00-110.00	1.00	2.78	A	0.348	2.176	0.632	1	1	32.784	2.07	206.64	B
			B	0.427	2.013	0.663	1	1	41.184			
			C	0.258	2.414	0.604	1	1	25.447			
T9 110.00-100.00	1.04	3.18	A	0.378	2.11	0.643	1	1	39.528	2.17	216.54	B
			B	0.424	2.019	0.662	1	1	44.615			
			C	0.272	2.375	0.608	1	1	29.698			
T10 100.00-80.00	2.11	6.26	A	0.334	2.209	0.627	1	1	75.274	4.06	202.97	B
			B	0.371	2.125	0.64	1	1	82.813			
			C	0.227	2.509	0.596	1	1	53.056			
T11 80.00-60.00	2.11	7.02	A	0.31	2.27	0.619	1	1	78.181	3.98	199.24	B
			B	0.343	2.189	0.63	1	1	85.374			
			C	0.214	2.549	0.593	1	1	56.316			
T12 60.00-40.00	2.15	7.60	A	0.304	2.284	0.617	1	1	85.933	3.86	193.04	B
			B	0.322	2.239	0.623	1	1	89.721			
			C	0.207	2.572	0.592	1	1	61.702			
T13 40.00-20.00	2.17	7.78	A	0.294	2.312	0.614	1	1	92.212	3.66	183.19	B
			B	0.306	2.279	0.618	1	1	94.919			
			C	0.203	2.587	0.591	1	1	67.763			
T14 20.00-0.00	2.17	10.87	A	0.261	2.405	0.605	1	1	86.320	3.57	178.37	B
			B	0.271	2.375	0.608	1	1	88.427			
			C	0.174	2.685	0.585	1	1	59.884			
Sum Weight:	23.00	65.18						OTM	5574.00 kip-ft	46.61		

### Tower Forces - With Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.53	0.80	A	0.429	2.009	0.664	0.825	1	18,263	1.46	97.40	A
			B	0.319	2.248	0.622	0.825	1	12,554			
			C	0.243	2.46	0.6	0.825	1	9,187			
T2 230.00-210.00	1.68	1.56	A	0.429	2.01	0.664	0.825	1	26,005	3.59	179.63	B
			B	0.787	1.807	0.886	0.825	1	62,631			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	22 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T3 210.00-190.00	1.68	2.21	C	0.256	2.419	0.603	0.825	1	13.914	3.46	172.94	B
			A	0.417	2.032	0.659	0.825	1	28.068			
			B	0.735	1.782	0.846	0.825	1	62.680			
T4 190.00-180.00	0.84	1.73	C	0.265	2.395	0.606	0.825	1	16.157	2.34	233.63	B
			A	0.528	1.866	0.712	0.825	1	25.688			
			B	0.775	1.799	0.876	0.825	1	45.390			
T5 180.00-160.00	1.68	4.01	C	0.402	2.06	0.652	0.825	1	18.321	4.11	205.50	B
			A	0.431	2.007	0.665	0.825	1	48.334			
			B	0.634	1.787	0.775	0.825	1	81.074			
T6 160.00-140.00	1.90	4.54	C	0.323	2.237	0.623	0.825	1	34.805	4.00	200.08	B
			A	0.366	2.134	0.638	0.825	1	49.736			
			B	0.531	1.863	0.714	0.825	1	78.590			
T7 140.00-120.00	1.96	4.82	C	0.304	2.284	0.617	0.825	1	41.694	3.99	199.40	B
			A	0.348	2.176	0.632	0.825	1	56.280			
			B	0.46	1.957	0.678	0.825	1	78.129			
T8 120.00-110.00	1.00	2.78	C	0.271	2.376	0.607	0.825	1	44.464	2.01	201.49	B
			A	0.348	2.176	0.632	0.825	1	31.570			
			B	0.427	2.013	0.663	0.825	1	40.011			
T9 110.00-100.00	1.04	3.18	C	0.258	2.414	0.604	0.825	1	23.660	2.09	209.35	B
			A	0.378	2.11	0.643	0.825	1	37.703			
			B	0.424	2.019	0.662	0.825	1	42.940			
T10 100.00-80.00	2.11	6.26	C	0.272	2.375	0.608	0.825	1	27.307	3.94	197.02	B
			A	0.334	2.209	0.627	0.825	1	71.908			
			B	0.371	2.125	0.64	0.825	1	80.060			
T11 80.00-60.00	2.11	7.02	C	0.227	2.509	0.596	0.825	1	49.111	3.86	192.86	B
			A	0.31	2.27	0.619	0.825	1	74.488			
			B	0.343	2.189	0.63	0.825	1	82.296			
T12 60.00-40.00	2.15	7.60	C	0.214	2.549	0.593	0.825	1	52.065	3.71	185.53	B
			A	0.304	2.284	0.617	0.825	1	81.482			
			B	0.322	2.239	0.623	0.825	1	85.818			
T13 40.00-20.00	2.17	7.78	C	0.207	2.572	0.592	0.825	1	56.556	3.50	174.78	B
			A	0.294	2.312	0.614	0.825	1	86.860			
			B	0.306	2.279	0.618	0.825	1	90.080			
T14 20.00-0.00	2.17	10.87	C	0.203	2.587	0.591	0.825	1	61.610	3.46	172.99	B
			A	0.261	2.405	0.605	0.825	1	82.773			
			B	0.271	2.375	0.608	0.825	1	85.461			
Sum Weight:	23.00	65.18						OTM	5479.91 kip-ft	45.52		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 245.00-230.00	0.53	0.80	A	0.429	2.009	0.664	0.8	1	18.219	1.46	97.24	A
			B	0.319	2.248	0.622	0.8	1	12.548			
			C	0.243	2.46	0.6	0.8	1	9.187			
T2 230.00-210.00	1.68	1.56	A	0.429	2.01	0.664	0.8	1	25.946	3.59	179.49	B
			B	0.787	1.807	0.886	0.8	1	62.572			
			C	0.256	2.419	0.603	0.8	1	13.914			
T3 210.00-190.00	1.68	2.21	A	0.417	2.032	0.659	0.8	1	28.009	3.46	172.81	B
			B	0.735	1.782	0.846	0.8	1	62.621			
			C	0.265	2.395	0.606	0.8	1	16.157			
T4	0.84	1.73	A	0.528	1.866	0.712	0.8	1	25.593	2.33	233.30	B



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	23 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
190.00-180.00			B	0.775	1.799	0.876	0.8		45.317			
			C	0.402	2.06	0.652	0.8		18.215			
T5	1.68	4.01	A	0.431	2.007	0.665	0.8		48.124	4.10	205.13	B
180.00-160.00			B	0.634	1.787	0.775	0.8		80.902			
			C	0.323	2.237	0.623	0.8		34.587			
T6	1.90	4.54	A	0.366	2.134	0.638	0.8		49.485	3.99	199.60	B
160.00-140.00			B	0.531	1.863	0.714	0.8		78.371			
			C	0.304	2.284	0.617	0.8		41.303			
T7	1.96	4.82	A	0.348	2.176	0.632	0.8		55.957	3.97	198.74	B
140.00-120.00			B	0.46	1.957	0.678	0.8		77.829			
			C	0.271	2.376	0.607	0.8		43.985			
T8	1.00	2.78	A	0.348	2.176	0.632	0.8		31.396	2.01	200.75	B
120.00-110.00			B	0.427	2.013	0.663	0.8		39.843			
			C	0.258	2.414	0.604	0.8		23.405			
T9	1.04	3.18	A	0.378	2.11	0.643	0.8		37.442	2.08	208.33	B
110.00-100.00			B	0.424	2.019	0.662	0.8		42.701			
			C	0.272	2.375	0.608	0.8		26.965			
T10	2.11	6.26	A	0.334	2.209	0.627	0.8		71.427	3.92	196.17	B
100.00-80.00			B	0.371	2.125	0.64	0.8		79.667			
			C	0.227	2.509	0.596	0.8		48.548			
T11	2.11	7.02	A	0.31	2.27	0.619	0.8		73.961	3.84	191.95	B
80.00-60.00			B	0.343	2.189	0.63	0.8		81.856			
			C	0.214	2.549	0.593	0.8		51.458			
T12	2.15	7.60	A	0.304	2.284	0.617	0.8		80.847	3.69	184.46	B
60.00-40.00			B	0.322	2.239	0.623	0.8		85.261			
			C	0.207	2.572	0.592	0.8		55.821			
T13	2.17	7.78	A	0.294	2.312	0.614	0.8		86.096	3.47	173.57	B
40.00-20.00			B	0.306	2.279	0.618	0.8		89.389			
			C	0.203	2.587	0.591	0.8		60.731			
T14	2.17	10.87	A	0.261	2.405	0.605	0.8		82.266	3.44	172.23	B
20.00-0.00			B	0.271	2.375	0.608	0.8		85.037			
			C	0.174	2.685	0.585	0.8		55.350			
Sum Weight:	23.00	65.18						OTM	5466.47 kip-ft	45.37		

**Tower Forces - With Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.53	0.80	A	0.429	2.009	0.664	0.85		18.307	1.46	97.56	A
245.00-230.00			B	0.319	2.248	0.622	0.85		12.560			
			C	0.243	2.46	0.6	0.85		9.187			
T2	1.68	1.56	A	0.429	2.01	0.664	0.85		26.064	3.60	179.77	B
230.00-210.00			B	0.787	1.807	0.886	0.85		62.690			
			C	0.256	2.419	0.603	0.85		13.914			
T3	1.68	2.21	A	0.417	2.032	0.659	0.85		28.127	3.46	173.08	B
210.00-190.00			B	0.735	1.782	0.846	0.85		62.739			
			C	0.265	2.395	0.606	0.85		16.157			
T4	0.84	1.73	A	0.528	1.866	0.712	0.85		25.784	2.34	233.96	B
190.00-180.00			B	0.775	1.799	0.876	0.85		45.464			
			C	0.402	2.06	0.652	0.85		18.427			
T5	1.68	4.01	A	0.431	2.007	0.665	0.85		48.543	4.12	205.88	B
180.00-160.00			B	0.634	1.787	0.775	0.85		81.247			
			C	0.323	2.237	0.623	0.85		35.023			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	24 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
	<b>Client</b>	Sprint - TWS-019	<b>Designed by</b>	MCD

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T6 160.00-140.00	1.90	4.54	A	0.366	2.134	0.638	0.85	1	49.986	4.01	200.55	B
			B	0.531	1.863	0.714	0.85	1	78.808			
			C	0.304	2.284	0.617	0.85	1	42.086			
T7 140.00-120.00	1.96	4.82	A	0.348	2.176	0.632	0.85	1	56.603	4.00	200.06	B
			B	0.46	1.957	0.678	0.85	1	78.429			
			C	0.271	2.376	0.607	0.85	1	44.944			
T8 120.00-110.00	1.00	2.78	A	0.348	2.176	0.632	0.85	1	31.743	2.02	202.23	B
			B	0.427	2.013	0.663	0.85	1	40.178			
			C	0.258	2.414	0.604	0.85	1	23.916			
T9 110.00-100.00	1.04	3.18	A	0.378	2.11	0.643	0.85	1	37.964	2.10	210.38	B
			B	0.424	2.019	0.662	0.85	1	43.180			
			C	0.272	2.375	0.608	0.85	1	27.648			
T10 100.00-80.00	2.11	6.26	A	0.334	2.209	0.627	0.85	1	72.389	3.96	197.87	B
			B	0.371	2.125	0.64	0.85	1	80.453			
			C	0.227	2.509	0.596	0.85	1	49.675			
T11 80.00-60.00	2.11	7.02	A	0.31	2.27	0.619	0.85	1	75.016	3.88	193.77	B
			B	0.343	2.189	0.63	0.85	1	82.735			
			C	0.214	2.549	0.593	0.85	1	52.672			
T12 60.00-40.00	2.15	7.60	A	0.304	2.284	0.617	0.85	1	82.118	3.73	186.60	B
			B	0.322	2.239	0.623	0.85	1	86.376			
			C	0.207	2.572	0.592	0.85	1	57.291			
T13 40.00-20.00	2.17	7.78	A	0.294	2.312	0.614	0.85	1	87.625	3.52	175.98	B
			B	0.306	2.279	0.618	0.85	1	90.771			
			C	0.203	2.587	0.591	0.85	1	62.489			
T14 20.00-0.00	2.17	10.87	A	0.261	2.405	0.605	0.85	1	83.280	3.48	173.76	B
			B	0.271	2.375	0.608	0.85	1	85.884			
			C	0.174	2.685	0.585	0.85	1	56.483			
Sum Weight:	23.00	65.18						OTM	5493.35 kip-ft	45.68		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	1	1	9.750	0.49	32.99	A
			B	0.181	2.662	0.587	1	1	6.611			
			C	0.124	2.869	0.578	1	1	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	1	1	14.506	1.04	51.85	B
			B	0.538	1.855	0.718	1	1	34.466			
			C	0.145	2.79	0.581	1	1	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	1	1	16.244	1.05	52.48	B
			B	0.507	1.891	0.701	1	1	35.631			
			C	0.16	2.736	0.583	1	1	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	1	1	15.189	0.67	66.60	B
			B	0.514	1.883	0.704	1	1	24.930			
			C	0.255	2.424	0.603	1	1	11.858			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	1	1	29.899	1.33	66.32	B
			B	0.42	2.026	0.66	1	1	47.490			
			C	0.206	2.577	0.592	1	1	23.336			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	1	1	31.944	1.38	68.79	B
			B	0.352	2.167	0.633	1	1	48.476			
			C	0.202	2.591	0.591	1	1	30.159			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	1	1	37.123	1.43	71.64	B
			B	0.308	2.276	0.618	1	1	50.900			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	25 of 45
	<b>Project</b>	Storrs (UCONN), CT (Site #: CT03XC214)	<b>Date</b>	16:11:49 12/30/14
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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T8 120.00-110.00	0.46	1.79	C	0.183	2.654	0.587	1	1	33.587	0.73	73.25	B
			A	0.219	2.535	0.594	1	1	20.624			
			B	0.286	2.334	0.612	1	1	26.549			
T9 110.00-100.00	0.47	2.07	C	0.175	2.683	0.586	1	1	17.993	0.78	78.37	B
			A	0.241	2.465	0.6	1	1	25.497			
			B	0.288	2.329	0.612	1	1	29.664			
T10 100.00-80.00	0.95	4.21	C	0.186	2.642	0.588	1	1	21.500	1.46	72.80	B
			A	0.21	2.563	0.592	1	1	47.810			
			B	0.249	2.441	0.602	1	1	54.689			
T11 80.00-60.00	0.95	4.87	C	0.154	2.756	0.582	1	1	38.009	1.44	71.79	B
			A	0.196	2.61	0.59	1	1	50.413			
			B	0.23	2.497	0.597	1	1	57.163			
T12 60.00-40.00	0.96	5.29	C	0.146	2.786	0.581	1	1	40.643	1.41	70.71	B
			A	0.195	2.612	0.589	1	1	56.750			
			B	0.22	2.532	0.595	1	1	61.870			
T13 40.00-20.00	0.97	5.30	C	0.144	2.792	0.581	1	1	45.764	1.36	68.17	B
			A	0.192	2.623	0.589	1	1	62.700			
			B	0.212	2.555	0.593	1	1	67.270			
T14 20.00-0.00	0.97	7.81	C	0.144	2.792	0.581	1	1	51.529	1.30	64.80	B
			A	0.17	2.699	0.585	1	1	57.129			
			B	0.188	2.635	0.588	1	1	61.598			
Sum Weight:	10.23	44.37	C	0.125	2.865	0.578	1	1	1819.53 kip-ft	15.86		

**Tower Forces - Service - Wind 45 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	0.825	1	9.586	0.49	32.66	A
			B	0.181	2.662	0.587	0.825	1	6.589			
			C	0.124	2.869	0.578	0.825	1	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	0.825	1	14.288	1.03	51.60	B
			B	0.538	1.855	0.718	0.825	1	34.247			
			C	0.145	2.79	0.581	0.825	1	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	0.825	1	16.026	1.04	52.23	B
			B	0.507	1.891	0.701	0.825	1	35.412			
			C	0.16	2.736	0.583	0.825	1	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	0.825	1	14.505	0.65	65.37	B
			B	0.514	1.883	0.704	0.825	1	24.364			
			C	0.255	2.424	0.603	0.825	1	11.117			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	0.825	1	28.433	1.30	64.88	B
			B	0.42	2.026	0.66	0.825	1	46.224			
			C	0.206	2.577	0.592	0.825	1	21.809			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	0.825	1	30.219	1.34	66.96	B
			B	0.352	2.167	0.633	0.825	1	46.922			
			C	0.202	2.591	0.591	0.825	1	27.594			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	0.825	1	34.839	1.38	69.11	B
			B	0.308	2.276	0.618	0.825	1	48.759			
			C	0.183	2.654	0.587	0.825	1	30.405			
T8 120.00-110.00	0.46	1.79	A	0.219	2.535	0.594	0.825	1	19.385	0.70	70.46	B
			B	0.286	2.334	0.612	0.825	1	25.361			
			C	0.175	2.683	0.586	0.825	1	16.295			
T9	0.47	2.07	A	0.241	2.465	0.6	0.825	1	23.620	0.74	74.42	B

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	26 of 45
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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
110.00-100.00			B	0.288	2.329	0.612	0.825	1	27.934			
			C	0.186	2.642	0.588	0.825	1	19.194			
T10	0.95	4.21	A	0.21	2.563	0.592	0.825	1	44.553	1.39	69.62	B
100.00-80.00			B	0.249	2.441	0.602	0.825	1	51.920			
			C	0.154	2.756	0.582	0.825	1	34.241			
T11	0.95	4.87	A	0.196	2.61	0.59	0.825	1	46.838	1.37	68.42	B
80.00-60.00			B	0.23	2.497	0.597	0.825	1	54.076			
			C	0.146	2.786	0.581	0.825	1	36.570			
T12	0.96	5.29	A	0.195	2.612	0.589	0.825	1	52.351	1.34	66.75	B
60.00-40.00			B	0.22	2.532	0.595	0.825	1	57.931			
			C	0.144	2.792	0.581	0.825	1	40.793			
T13	0.97	5.30	A	0.192	2.623	0.589	0.825	1	57.349	1.28	63.76	B
40.00-20.00			B	0.212	2.555	0.593	0.825	1	62.367			
			C	0.144	2.792	0.581	0.825	1	45.549			
T14	0.97	7.81	A	0.17	2.699	0.585	0.825	1	53.768	1.24	62.10	B
20.00-0.00			B	0.188	2.635	0.588	0.825	1	58.691			
			C	0.125	2.865	0.578	0.825	1	41.067			
Sum Weight:	10.23	44.37						OTM	1772.12	15.30		
									kip-ft			

### Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1	0.23	0.60	A	0.252	2.433	0.602	0.8	1	9.563	0.49	32.61	A
245.00-230.00			B	0.181	2.662	0.587	0.8	1	6.586			
			C	0.124	2.869	0.578	0.8	1	4.438			
T2	0.71	1.25	A	0.262	2.401	0.605	0.8	1	14.256	1.03	51.57	B
230.00-210.00			B	0.538	1.855	0.718	0.8	1	34.216			
			C	0.145	2.79	0.581	0.8	1	7.436			
T3	0.71	1.85	A	0.262	2.401	0.605	0.8	1	15.994	1.04	52.20	B
210.00-190.00			B	0.507	1.891	0.701	0.8	1	35.381			
			C	0.16	2.736	0.583	0.8	1	9.234			
T4	0.36	1.24	A	0.331	2.217	0.626	0.8	1	14.407	0.65	65.19	B
190.00-180.00			B	0.514	1.883	0.704	0.8	1	24.283			
			C	0.255	2.424	0.603	0.8	1	11.011			
T5	0.71	2.33	A	0.27	2.38	0.607	0.8	1	28.224	1.29	64.67	B
180.00-160.00			B	0.42	2.026	0.66	0.8	1	46.043			
			C	0.206	2.577	0.592	0.8	1	21.591			
T6	0.88	2.79	A	0.231	2.496	0.597	0.8	1	29.973	1.33	66.70	B
160.00-140.00			B	0.352	2.167	0.633	0.8	1	46.700			
			C	0.202	2.591	0.591	0.8	1	27.228			
T7	0.90	2.96	A	0.22	2.53	0.595	0.8	1	34.512	1.37	68.74	B
140.00-120.00			B	0.308	2.276	0.618	0.8	1	48.454			
			C	0.183	2.654	0.587	0.8	1	29.950			
T8	0.46	1.79	A	0.219	2.535	0.594	0.8	1	19.208	0.70	70.07	B
120.00-110.00			B	0.286	2.334	0.612	0.8	1	25.192			
			C	0.175	2.683	0.586	0.8	1	16.052			
T9	0.47	2.07	A	0.241	2.465	0.6	0.8	1	23.352	0.74	73.85	B
110.00-100.00			B	0.288	2.329	0.612	0.8	1	27.686			
			C	0.186	2.642	0.588	0.8	1	18.864			
T10	0.95	4.21	A	0.21	2.563	0.592	0.8	1	44.087	1.38	69.17	B
100.00-80.00			B	0.249	2.441	0.602	0.8	1	51.524			
			C	0.154	2.756	0.582	0.8	1	33.703			

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	27 of 45
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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T11 80.00-60.00	0.95	4.87	A	0.196	2.61	0.59	0.8	I	46.328	1.36	67.94	B
			B	0.23	2.497	0.597	0.8	I	53.635			
			C	0.146	2.786	0.581	0.8	I	35.988			
T12 60.00-40.00	0.96	5.29	A	0.195	2.612	0.589	0.8	I	51.723	1.32	66.19	B
			B	0.22	2.532	0.595	0.8	I	57.369			
			C	0.144	2.792	0.581	0.8	I	40.083			
T13 40.00-20.00	0.97	5.30	A	0.192	2.623	0.589	0.8	I	56.585	1.26	63.13	B
			B	0.212	2.555	0.593	0.8	I	61.667			
			C	0.144	2.792	0.581	0.8	I	44.695			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	0.8	I	53.288	1.23	61.72	B
			B	0.188	2.635	0.588	0.8	I	58.275			
			C	0.125	2.865	0.578	0.8	I	40.527			
Sum Weight:	10.23	44.37						OTM	1765.35 kip-ft	15.22		

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 245.00-230.00	0.23	0.60	A	0.252	2.433	0.602	0.85	I	9.609	0.49	32.71	A
			B	0.181	2.662	0.587	0.85	I	6.592			
			C	0.124	2.869	0.578	0.85	I	4.438			
T2 230.00-210.00	0.71	1.25	A	0.262	2.401	0.605	0.85	I	14.319	1.03	51.64	B
			B	0.538	1.855	0.718	0.85	I	34.278			
			C	0.145	2.79	0.581	0.85	I	7.436			
T3 210.00-190.00	0.71	1.85	A	0.262	2.401	0.605	0.85	I	16.057	1.05	52.27	B
			B	0.507	1.891	0.701	0.85	I	35.443			
			C	0.16	2.736	0.583	0.85	I	9.234			
T4 190.00-180.00	0.36	1.24	A	0.331	2.217	0.626	0.85	I	14.602	0.66	65.55	B
			B	0.514	1.883	0.704	0.85	I	24.445			
			C	0.255	2.424	0.603	0.85	I	11.223			
T5 180.00-160.00	0.71	2.33	A	0.27	2.38	0.607	0.85	I	28.642	1.30	65.08	B
			B	0.42	2.026	0.66	0.85	I	46.405			
			C	0.206	2.577	0.592	0.85	I	22.027			
T6 160.00-140.00	0.88	2.79	A	0.231	2.496	0.597	0.85	I	30.466	1.34	67.22	B
			B	0.352	2.167	0.633	0.85	I	47.144			
			C	0.202	2.591	0.591	0.85	I	27.961			
T7 140.00-120.00	0.90	2.96	A	0.22	2.53	0.595	0.85	I	35.165	1.39	69.47	B
			B	0.308	2.276	0.618	0.85	I	49.065			
			C	0.183	2.654	0.587	0.85	I	30.859			
T8 120.00-110.00	0.46	1.79	A	0.219	2.535	0.594	0.85	I	19.562	0.71	70.86	B
			B	0.286	2.334	0.612	0.85	I	25.531			
			C	0.175	2.683	0.586	0.85	I	16.537			
T9 110.00-100.00	0.47	2.07	A	0.241	2.465	0.6	0.85	I	23.888	0.75	74.98	B
			B	0.288	2.329	0.612	0.85	I	28.181			
			C	0.186	2.642	0.588	0.85	I	19.523			
T10 100.00-80.00	0.95	4.21	A	0.21	2.563	0.592	0.85	I	45.018	1.40	70.08	B
			B	0.249	2.441	0.602	0.85	I	52.315			
			C	0.154	2.756	0.582	0.85	I	34.779			
T11 80.00-60.00	0.95	4.87	A	0.196	2.61	0.59	0.85	I	47.349	1.38	68.91	B
			B	0.23	2.497	0.597	0.85	I	54.517			
			C	0.146	2.786	0.581	0.85	I	37.152			
T12 60.00-40.00	0.96	5.29	A	0.195	2.612	0.589	0.85	I	52.980	1.35	67.32	B
			B	0.22	2.532	0.595	0.85	I	58.494			



<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b> Structural Analysis - Tower	<b>Page</b> 28 of 45
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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T13 40.00-20.00	0.97	5.30	C	0.144	2.792	0.581	0.85	I	41.503	1.29	64.39	B
			A	0.192	2.623	0.589	0.85	I	58.114			
			B	0.212	2.555	0.593	0.85	I	63.068			
			C	0.144	2.792	0.581	0.85	I	46.404			
T14 20.00-0.00	0.97	7.81	A	0.17	2.699	0.585	0.85	I	54.248	1.25	62.49	B
			B	0.188	2.635	0.588	0.85	I	59.106			
			C	0.125	2.865	0.578	0.85	I	41.608			
								OTM	1778.89			
Sum Weight:	10.23	44.37							15.38			

### Force Totals

Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Z	Sum of Overturning Moments, M <sub>x</sub>	Sum of Overturning Moments, M <sub>z</sub>	Sum of Torques
	K	K	K	kip-ft	kip-ft	kip-ft
Lcg Weight	30.28					
Bracing Weight	14.09					
Total Member Self-Weight	44.37					
Total Weight	60.61			-5.14	-17.30	
Wind 0 deg - No Ice		0.04	-53.46	-6913.78	-26.69	23.88
Wind 30 deg - No Ice		26.24	-45.27	-5907.82	-3442.45	3.70
Wind 45 deg - No Ice		36.92	-36.88	-4821.14	-4842.96	-6.62
Wind 60 deg - No Ice		45.04	-25.99	-3405.56	-5910.72	-16.61
Wind 90 deg - No Ice		52.35	-0.07	-18.20	-6844.96	-31.74
Wind 120 deg - No Ice		46.35	26.70	3441.06	-6008.77	-39.01
Wind 135 deg - No Ice		36.63	36.64	4777.76	-4804.36	-37.13
Wind 150 deg - No Ice		25.95	45.10	5874.51	-3403.02	-34.31
Wind 180 deg - No Ice		-0.14	51.80	6768.31	3.25	-21.36
Wind 210 deg - No Ice		-26.34	45.46	5918.20	3418.87	-2.37
Wind 225 deg - No Ice		-37.04	36.98	4822.03	4820.53	7.91
Wind 240 deg - No Ice		-46.76	26.98	3479.88	6022.63	17.70
Wind 270 deg - No Ice		-52.57	0.07	7.16	6833.75	32.68
Wind 300 deg - No Ice		-44.97	-25.78	-3374.06	5862.65	38.45
Wind 315 deg - No Ice		-36.81	-36.59	-4783.02	4788.82	38.04
Wind 330 deg - No Ice		-26.11	-45.01	-5875.22	3384.97	35.41
Member Ice	20.81					
Total Weight Ice	96.92			-13.26	-51.26	
Wind 0 deg - Ice		0.06	-53.53	-7061.01	-61.69	25.24
Wind 30 deg - Ice		26.48	-45.72	-6067.01	-3559.89	5.68
Wind 45 deg - Ice		37.32	-37.29	-4955.00	-5000.58	-4.81
Wind 60 deg - Ice		45.62	-26.33	-3506.37	-6104.29	-15.28
Wind 90 deg - Ice		52.85	-0.06	-23.55	-7050.68	-31.19
Wind 120 deg - Ice		46.41	26.72	3501.58	-6162.79	-39.17
Wind 135 deg - Ice		37.10	37.00	4892.13	-4971.16	-38.34
Wind 150 deg - Ice		26.20	45.52	6014.67	-3523.57	-35.47
Wind 180 deg - Ice		-0.47	52.56	6956.46	3.81	-20.73
Wind 210 deg - Ice		-26.81	45.87	6056.81	3494.05	-2.55
Wind 225 deg - Ice		-37.62	37.40	4939.98	4930.00	7.45
Wind 240 deg - Ice		-46.91	27.07	3546.88	6117.85	16.99
Wind 270 deg - Ice		-53.15	0.27	20.65	6980.63	32.49
Wind 300 deg - Ice		-45.78	-25.88	-3450.42	6015.01	40.34
Wind 315 deg - Ice		-37.41	-36.88	-4905.03	4902.30	40.15
Wind 330 deg - Ice		-26.34	-45.44	-6032.94	3435.33	36.41
Total Weight	60.61			-5.14	-17.30	
Wind 0 deg - Service		0.01	-18.50	-2397.46	-2.12	8.26

<b>tnxTower</b>  <b>URS Corporation</b> 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Phone: 860-529-8882 FAX: 860-529-3991	<b>Job</b>	Structural Analysis - Tower	<b>Page</b>	29 of 45
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Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, $M_x$ kip-ft	Sum of Overturning Moments, $M_z$ kip-ft	Sum of Torques kip-ft
Wind 30 deg - Service		9.08	-15.66	-2049.38	-1184.05	1.28
Wind 45 deg - Service		12.78	-12.76	-1673.36	-1668.65	-2.29
Wind 60 deg - Service		15.59	-8.99	-1183.54	-2038.12	-5.75
Wind 90 deg - Service		18.11	-0.03	-11.44	-2361.39	-10.98
Wind 120 deg - Service		16.04	9.24	1185.53	-2072.05	-13.50
Wind 135 deg - Service		12.67	12.68	1648.06	-1655.30	-12.85
Wind 150 deg - Service		8.98	15.61	2027.56	-1170.40	-11.87
Wind 180 deg - Service		-0.05	17.93	2336.83	8.24	-7.39
Wind 210 deg - Service		-9.11	15.73	2042.67	1190.11	-0.82
Wind 225 deg - Service		-12.82	12.80	1663.38	1675.12	2.74
Wind 240 deg - Service		-16.18	9.33	1198.97	2091.07	6.13
Wind 270 deg - Service		-18.19	0.02	-2.67	2371.73	11.31
Wind 300 deg - Service		-15.56	-8.92	-1172.64	2035.71	13.30
Wind 315 deg - Service		-12.74	-12.66	-1660.17	1664.14	13.16
Wind 330 deg - Service		-9.03	-15.57	-2038.10	1178.38	12.25

## Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 45 deg - No Ice
5	Dead+Wind 60 deg - No Ice
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice
8	Dead+Wind 135 deg - No Ice
9	Dead+Wind 150 deg - No Ice
10	Dead+Wind 180 deg - No Ice
11	Dead+Wind 210 deg - No Ice
12	Dead+Wind 225 deg - No Ice
13	Dead+Wind 240 deg - No Ice
14	Dead+Wind 270 deg - No Ice
15	Dead+Wind 300 deg - No Ice
16	Dead+Wind 315 deg - No Ice
17	Dead+Wind 330 deg - No Ice
18	Dead+Ice+Temp
19	Dead+Wind 0 deg+Ice+Temp
20	Dead+Wind 30 deg+Ice+Temp
21	Dead+Wind 45 deg+Ice+Temp
22	Dead+Wind 60 deg+Ice+Temp
23	Dead+Wind 90 deg+Ice+Temp
24	Dead+Wind 120 deg+Ice+Temp
25	Dead+Wind 135 deg+Ice+Temp
26	Dead+Wind 150 deg+Ice+Temp
27	Dead+Wind 180 deg+Ice+Temp
28	Dead+Wind 210 deg+Ice+Temp
29	Dead+Wind 225 deg+Ice+Temp
30	Dead+Wind 240 deg+Ice+Temp
31	Dead+Wind 270 deg+Ice+Temp
32	Dead+Wind 300 deg+Ice+Temp
33	Dead+Wind 315 deg+Ice+Temp
34	Dead+Wind 330 deg+Ice+Temp
35	Dead+Wind 0 deg - Service
36	Dead+Wind 30 deg - Service



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Comb. No.	Description
37	Dead+Wind 45 deg - Service
38	Dead+Wind 60 deg - Service
39	Dead+Wind 90 deg - Service
40	Dead+Wind 120 deg - Service
41	Dead+Wind 135 deg - Service
42	Dead+Wind 150 deg - Service
43	Dead+Wind 180 deg - Service
44	Dead+Wind 210 deg - Service
45	Dead+Wind 225 deg - Service
46	Dead+Wind 240 deg - Service
47	Dead+Wind 270 deg - Service
48	Dead+Wind 300 deg - Service
49	Dead+Wind 315 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov.	Force	Major Axis	Minor Axis
				Load Comb.	K	Moment kip-ft	Moment kip-ft
T1	245 - 230	Leg	Max Tension	5	22.22	0.60	-0.37
			Max. Compression	13	-25.94	0.65	-0.40
			Max. Mx	14	-3.23	0.74	-0.01
			Max. My	2	-25.60	-0.01	0.75
			Max. Vy	14	-2.78	0.70	-0.09
			Max. Vx	2	-2.95	-0.01	0.75
		Diagonal	Max Tension	4	3.30	0.00	0.00
			Max. Compression	12	-3.29	0.00	0.00
			Max. Mx	29	1.06	-0.00	0.00
			Max. My	12	-3.29	0.00	0.00
			Max. Vy	29	-0.00	-0.00	0.00
			Max. Vx	12	0.00	0.00	0.00
		Top Girt	Max Tension	13	1.02	0.00	0.00
			Max. Compression	5	-1.10	0.00	0.00
			Max. Mx	18	-0.00	0.01	0.00
			Max. My	25	-0.16	0.00	0.00
			Max. Vy	18	0.01	0.00	0.00
			Max. Vx	25	0.00	0.00	0.00
		Bottom Girt	Max Tension	5	1.60	0.00	0.00
			Max. Compression	13	-1.71	0.00	0.00
			Max. Mx	18	0.01	0.01	0.00
Max. My	34		0.18	0.00	0.00		
Max. Vy	18		0.01	0.00	0.00		
Max. Vx	34		0.00	0.00	0.00		
T2	230 - 210	Leg	Max Tension	5	67.05	1.26	-0.01
			Max. Compression	13	-71.96	0.48	-0.00
			Max. Mx	13	-25.99	2.02	-0.07
			Max. My	6	-2.14	0.00	1.79
			Max. Vy	30	-3.62	0.48	0.00
		Diagonal	Max. Vx	20	2.85	0.00	-0.32
			Max Tension	34	4.35	0.00	0.00
			Max. Compression	34	-4.33	0.00	0.00
			Max. Mx	29	0.69	-0.01	0.00
			Max. My	11	-4.14	-0.00	0.00
		Top Girt	Max. Vy	23	-0.01	-0.01	0.00
			Max. Vx	11	-0.00	0.00	0.00
			Max Tension	13	1.96	0.00	0.00
			Max. Compression	5	-1.86	0.00	0.00
			Max. Mx	18	-0.00	0.01	0.00

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T3	210 - 190	Bottom Girt	Max. My	34	-0.17	0.00	0.00	
			Max. Vy	18	-0.01	0.00	0.00	
			Max. Vx	34	-0.00	0.00	0.00	
			Max Tension	22	1.94	0.00	0.00	
			Max. Compression	13	-2.05	0.00	0.00	
			Max. Mx	18	0.03	0.01	0.00	
			Max. My	34	0.30	0.00	0.00	
			Max. Vy	18	-0.01	0.00	0.00	
			Max. Vx	34	-0.00	0.00	0.00	
			Leg	Max Tension	5	115.07	0.33	0.01
				Max. Compression	13	-121.67	2.97	0.00
				Max. Mx	30	-120.43	3.11	0.03
		Max. My		20	-4.55	-0.01	-2.22	
		Max. Vy		30	-5.28	3.11	0.03	
		Max. Vx		20	2.94	0.04	-1.64	
		Diagonal		Max Tension	34	5.04	0.00	0.00
				Max. Compression	34	-5.26	0.00	0.00
				Max. Mx	29	1.50	-0.01	0.00
				Max. My	26	-5.23	-0.00	-0.00
				Max. Vy	29	-0.01	-0.01	0.00
				Max. Vx	26	0.00	-0.00	-0.00
		Top Girt	Max Tension	30	1.81	0.00	0.00	
			Max. Compression	22	-1.69	0.00	0.00	
			Max. Mx	18	0.01	0.01	0.00	
Max. My	34		-0.24	0.00	0.00			
Max. Vy	18		-0.01	0.00	0.00			
Max. Vx	34		-0.00	0.00	0.00			
Bottom Girt	Max Tension	5	1.31	0.00	0.00			
	Max. Compression	13	-1.25	0.00	0.00			
	Max. Mx	18	0.04	0.01	0.00			
	Max. My	34	-0.04	0.00	0.00			
	Max. Vy	18	0.01	0.00	0.00			
	Max. Vx	34	0.00	0.00	0.00			
	Leg	Max Tension	5	115.04	-2.80	-0.01		
		Max. Compression	24	-121.67	5.34	-0.03		
		Max. Mx	22	111.50	-5.86	-0.06		
		Max. My	6	-4.04	-0.14	9.46		
		Max. Vy	32	0.47	-5.78	-0.01		
		Max. Vx	20	0.97	-0.20	-9.35		
Diagonal		Max Tension	28	4.69	0.00	0.00		
		Max. Compression	20	-5.26	0.00	0.00		
		Max. Mx	22	3.56	0.09	0.01		
		Max. My	26	-3.42	-0.06	0.03		
		Max. Vy	22	0.02	0.09	0.01		
		Max. Vx	26	-0.01	0.00	0.00		
Leg	Max Tension	5	135.55	-5.72	-0.02			
	Max. Compression	24	-149.18	5.41	-0.00			
	Max. Mx	22	124.35	-5.86	-0.06			
	Max. My	6	-4.72	-0.14	9.46			
	Max. Vy	32	-0.19	-5.70	-0.02			
	Max. Vx	20	-0.55	-0.20	-9.35			
	Diagonal	Max Tension	34	4.63	0.00	0.00		
		Max. Compression	34	-5.09	0.00	0.00		
		Max. Mx	24	3.51	0.09	0.00		
		Max. My	26	2.06	0.07	0.01		
		Max. Vy	24	-0.03	0.09	0.00		
		Max. Vx	19	-0.00	0.00	0.00		
Leg	Max Tension	22	156.15	-5.24	-0.03			
	Max. Compression	24	-175.33	5.38	0.03			
	Max. Mx	22	145.86	-5.51	-0.03			
	Max. My	23	-9.95	-0.03	5.40			

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T7	140 - 120	Diagonal	Max. Vy	32	-0.19	-5.44	-0.02
			Max. Vx	20	0.21	-0.00	-5.39
			Max Tension	34	4.95	0.00	0.00
			Max. Compression	34	-5.33	0.00	0.00
			Max. Mx	24	3.34	0.06	0.00
			Max. My	27	-4.37	0.00	0.01
			Max. Vy	22	0.02	0.06	-0.01
		Leg	Max. Vx	19	-0.00	0.00	0.00
			Max Tension	22	177.67	-5.00	0.07
			Max. Compression	24	-202.10	4.68	0.05
			Max. Mx	22	166.86	-5.45	-0.03
			Max. My	23	-12.70	-0.08	5.61
			Max. Vy	32	-0.26	-5.39	-0.05
			Max. Vx	31	0.35	-0.09	-5.56
T8	120 - 110	Diagonal	Max Tension	34	5.75	0.00	0.00
			Max. Compression	34	-6.09	0.00	0.00
			Max. Mx	24	3.89	0.10	0.01
			Max. My	27	-4.79	-0.00	0.01
			Max. Vy	22	0.03	0.09	0.01
			Max. Vx	27	-0.00	0.00	0.00
			Max Tension	22	188.90	-4.76	0.05
		Leg	Max. Compression	24	-215.88	2.97	-0.01
			Max. Mx	22	188.90	-4.76	0.05
			Max. My	23	-13.23	-0.08	5.61
			Max. Vy	19	0.29	4.64	0.04
			Max. Vx	31	-0.24	-0.09	-5.56
			Max Tension	34	6.33	0.00	0.00
			Max. Compression	34	-6.58	0.00	0.00
T9	110 - 100	Diagonal	Max. Mx	24	4.15	0.09	0.01
			Max. My	25	1.19	0.07	0.01
			Max. Vy	21	0.03	0.08	-0.01
			Max. Vx	25	-0.00	0.00	0.00
			Max Tension	22	199.51	-3.52	-0.08
			Max. Compression	24	-229.03	4.16	0.25
			Max. Mx	24	-228.52	9.41	-0.20
		Leg	Max. My	31	-14.83	-0.29	-6.88
			Max. Vy	19	-1.39	9.39	0.07
			Max. Vx	31	1.53	-0.29	-6.88
			Max Tension	33	6.64	0.00	0.00
			Max. Compression	25	-7.01	0.00	0.00
			Max. Mx	22	5.38	0.09	0.01
			Max. My	33	-6.24	0.02	-0.01
T10	100 - 80	Secondary Horizontal	Max. Vy	22	0.03	0.09	0.01
			Max. Vx	33	0.00	0.00	0.00
			Max Tension	24	3.97	0.00	0.00
			Max. Compression	24	-3.97	0.00	0.00
			Max. Mx	32	2.60	-0.21	0.00
			Max. My	32	2.07	0.00	0.01
			Max. Vy	32	0.06	0.00	0.00
		Leg	Max. Vx	32	-0.00	0.00	0.00
			Max Tension	22	222.77	-4.22	-0.03
			Max. Compression	24	-258.51	4.81	0.00
			Max. Mx	30	-257.21	4.82	-0.02
			Max. My	31	-15.44	-0.29	-6.88
			Max. Vy	32	-0.21	-4.73	-0.26
			Max. Vx	23	0.35	-0.12	5.71
Diagonal	Max Tension	34	7.36	0.00	0.00		
	Max. Compression	34	-7.63	0.00	0.00		
	Max. Mx	24	5.01	0.14	0.01		
	Max. My	33	-7.16	0.03	-0.02		

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft			
T11	80 - 60	Leg	Max. Vy	22	0.05	0.14	0.01			
			Max. Vx	33	0.00	0.00	0.00			
			Max Tension	22	244.50	-4.36	-0.01			
			Max. Compression	24	-286.50	5.01	0.06			
			Max. Mx	30	-285.44	5.03	-0.03			
			Max. My	23	-21.70	0.08	4.58			
		Diagonal	Max. Vy	32	0.20	-4.81	-0.07			
			Max. Vx	23	-0.21	-0.02	4.39			
			Max Tension	34	7.77	0.00	0.00			
			Max. Compression	34	-8.02	0.00	0.00			
			Max. Mx	22	5.73	0.14	0.01			
			Max. My	32	-6.91	0.08	-0.02			
			Max. Vy	22	0.05	0.14	0.01			
			Max. Vx	32	0.00	0.00	0.00			
T12	60 - 40	Leg	Max Tension	22	265.91	-4.89	-0.03			
			Max. Compression	24	-314.30	5.56	-0.07			
			Max. Mx	30	-313.36	5.56	0.00			
			Max. My	20	-26.08	1.99	-5.85			
			Max. Vy	27	-0.52	-4.85	0.01			
			Max. Vx	23	-0.27	1.98	5.85			
		Diagonal	Max Tension	17	8.40	0.00	0.00			
			Max. Compression	34	-8.95	0.00	0.00			
			Max. Mx	22	5.74	0.20	0.02			
			Max. My	32	-7.46	0.10	-0.03			
			Max. Vy	22	0.07	0.20	0.02			
			Max. Vx	32	0.00	0.00	0.00			
			T13	40 - 20	Leg	Max Tension	22	289.30	-10.77	-0.02
						Max. Compression	24	-341.99	13.65	0.49
Max. Mx	30	-341.07				13.76	-0.29			
Max. My	23	-27.16				6.48	21.12			
Max. Vy	30	-1.34				13.76	-0.29			
Max. Vx	23	-2.65				6.48	21.12			
Diagonal	Max Tension	33			10.10	0.00	0.00			
	Max. Compression	32			-10.98	0.00	0.00			
	Max. Mx	23			-1.67	0.29	-0.04			
	Max. My	32			-10.92	0.19	-0.07			
	Max. Vy	23			0.08	0.29	-0.04			
	Max. Vx	32			0.01	0.00	0.00			
	T14	20 - 0			Leg	Max Tension	5	295.74	-7.97	0.23
						Max. Compression	24	-361.37	0.00	-0.00
Max. Mx			30	-358.26		13.76	-0.29			
Max. My			23	-34.12		6.48	21.12			
Max. Vy			30	0.89		13.76	-0.29			
Max. Vx			23	1.36		6.48	21.12			
Diagonal			Max Tension	32	18.39	0.00	0.00			
			Max. Compression	7	-16.82	0.00	0.00			
			Max. Mx	21	15.67	-0.53	0.09			
			Max. My	25	2.92	-0.49	-0.12			
			Max. Vy	23	-0.16	-0.53	-0.11			
			Max. Vx	25	0.01	0.00	0.00			

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	30	375.77	31.05	-18.36

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Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg B	Max. H <sub>x</sub>	13	356.89	34.54	-20.42
	Max. H <sub>z</sub>	22	-309.61	-33.94	20.04
	Min. Vert	5	-310.01	-29.44	17.47
	Min. H <sub>x</sub>	22	-309.61	-33.94	20.04
	Min. H <sub>z</sub>	13	356.89	34.54	-20.42
	Max. Vert	24	376.57	-30.49	-18.76
	Max. H <sub>x</sub>	32	-304.50	33.49	20.41
	Max. H <sub>z</sub>	32	-304.50	33.49	20.41
	Min. Vert	15	-307.23	29.03	17.82
	Min. H <sub>x</sub>	7	355.37	-34.01	-20.75
Leg A	Min. H <sub>z</sub>	7	355.37	-34.01	-20.75
	Max. Vert	19	375.26	0.70	35.74
	Max. H <sub>x</sub>	22	202.61	1.57	16.55
	Max. H <sub>z</sub>	2	354.86	0.61	39.80
	Min. Vert	10	-307.43	-0.50	-34.04
	Min. H <sub>x</sub>	30	-139.96	-1.36	-21.18
	Min. H <sub>z</sub>	27	-305.58	-0.44	-39.24

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	60.61	0.00	0.00	-5.13	-17.30	-0.00
Dead+Wind 0 deg - No Ice	60.61	0.04	-53.45	-6955.81	-26.94	24.00
Dead+Wind 30 deg - No Ice	60.61	26.23	-45.26	-5943.93	-3463.51	3.83
Dead+Wind 45 deg - No Ice	60.61	36.92	-36.88	-4850.63	-4872.58	-6.51
Dead+Wind 60 deg - No Ice	60.61	45.04	-25.99	-3426.43	-5946.89	-16.57
Dead+Wind 90 deg - No Ice	60.61	52.34	-0.07	-18.36	-6886.80	-31.78
Dead+Wind 120 deg - No Ice	60.61	46.34	26.69	3461.90	-6045.36	-39.08
Dead+Wind 135 deg - No Ice	60.61	36.63	36.63	4806.96	-4833.89	-37.20
Dead+Wind 150 deg - No Ice	60.61	25.95	45.10	5910.42	-3423.96	-34.38
Dead+Wind 180 deg - No Ice	60.61	-0.14	51.80	6809.77	3.21	-21.47
Dead+Wind 210 deg - No Ice	60.61	-26.34	45.46	5954.35	3439.78	-2.50
Dead+Wind 225 deg - No Ice	60.61	-37.04	36.98	4851.50	4850.05	7.81
Dead+Wind 240 deg - No Ice	60.61	-46.75	26.98	3500.98	6059.21	17.66
Dead+Wind 270 deg - No Ice	60.61	-52.56	0.07	7.17	6875.48	32.72
Dead+Wind 300 deg - No Ice	60.61	-44.96	-25.77	-3394.80	5898.50	38.52
Dead+Wind 315 deg - No Ice	60.61	-36.81	-36.59	-4812.39	4818.05	38.11
Dead+Wind 330 deg - No Ice	60.61	-26.11	-45.01	-5911.24	3405.57	35.48
Dead+Ice+Temp	96.92	-0.00	-0.00	-13.27	-51.14	0.00
Dead+Wind 0 deg+Ice+Temp	96.92	0.06	-53.53	-7128.02	-62.32	25.59
Dead+Wind 30 deg+Ice+Temp	96.92	26.47	-45.72	-6124.72	-3593.82	6.01
Dead+Wind 45 deg+Ice+Temp	96.92	37.32	-37.29	-5002.15	-5048.23	-4.56
Dead+Wind 60 deg+Ice+Temp	96.92	45.62	-26.32	-3539.76	-6162.45	-15.13
Dead+Wind 90 deg+Ice+Temp	96.92	52.85	-0.06	-23.79	-7117.82	-31.25
Dead+Wind 120 deg+Ice+Temp	96.92	46.41	26.71	3534.85	-6221.33	-39.36
Dead+Wind 135 deg+Ice+Temp	96.92	37.10	37.00	4938.88	-5018.62	-38.57
Dead+Wind 150 deg+Ice+Temp	96.92	26.20	45.52	6072.12	-3557.23	-35.73
Dead+Wind 180 deg+Ice+Temp	96.92	-0.47	52.56	7022.91	3.67	-21.07
Dead+Wind 210 deg+Ice+Temp	96.92	-26.81	45.87	6114.57	3527.24	-2.87
Dead+Wind 225 deg+Ice+Temp	96.92	-37.62	37.39	4987.10	4976.94	7.19
Dead+Wind 240 deg+Ice+Temp	96.92	-46.90	27.07	3580.51	6175.86	16.83
Dead+Wind 270 deg+Ice+Temp	96.92	-53.15	0.27	20.72	7047.09	32.55
Dead+Wind 300 deg+Ice+Temp	96.92	-45.77	-25.88	-3483.53	6072.30	40.52
Dead+Wind 315 deg+Ice+Temp	96.92	-37.41	-36.88	-4951.96	4948.97	40.38
Dead+Wind 330 deg+Ice+Temp	96.92	-26.34	-45.44	-6090.51	3468.07	36.68

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Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 0 deg - Service	60.61	0.01	-18.50	-2410.35	-20.68	8.31
Dead+Wind 30 deg - Service	60.61	9.08	-15.66	-2060.20	-1209.88	1.32
Dead+Wind 45 deg - Service	60.61	12.78	-12.76	-1681.87	-1697.48	-2.26
Dead+Wind 60 deg - Service	60.61	15.58	-8.99	-1189.04	-2069.24	-5.73
Dead+Wind 90 deg - Service	60.61	18.11	-0.03	-9.71	-2394.48	-10.99
Dead+Wind 120 deg - Service	60.61	16.04	9.24	1194.61	-2103.30	-13.52
Dead+Wind 135 deg - Service	60.61	12.67	12.68	1660.04	-1684.07	-12.89
Dead+Wind 150 deg - Service	60.61	8.98	15.60	2041.87	-1196.18	-11.91
Dead+Wind 180 deg - Service	60.61	-0.05	17.92	2353.07	-10.25	-7.43
Dead+Wind 210 deg - Service	60.61	-9.11	15.73	2057.06	1178.91	-0.85
Dead+Wind 225 deg - Service	60.61	-12.82	12.80	1675.44	1666.92	2.72
Dead+Wind 240 deg - Service	60.61	-16.18	9.33	1208.12	2085.34	6.11
Dead+Wind 270 deg - Service	60.61	-18.19	0.02	-0.87	2367.80	11.32
Dead+Wind 300 deg - Service	60.61	-15.56	-8.92	-1178.08	2029.74	13.33
Dead+Wind 315 deg - Service	60.61	-12.74	-12.66	-1668.62	1655.87	13.20
Dead+Wind 330 deg - Service	60.61	-9.03	-15.57	-2048.87	1167.10	12.29

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-60.61	0.00	-0.00	60.61	-0.00	0.000%
2	0.04	-60.61	-53.46	-0.04	60.61	53.45	0.004%
3	26.24	-60.61	-45.27	-26.23	60.61	45.26	0.005%
4	36.92	-60.61	-36.88	-36.92	60.61	36.88	0.005%
5	45.04	-60.61	-25.99	-45.04	60.61	25.99	0.005%
6	52.35	-60.61	-0.07	-52.34	60.61	0.07	0.005%
7	46.35	-60.61	26.70	-46.34	60.61	-26.69	0.004%
8	36.63	-60.61	36.64	-36.63	60.61	-36.63	0.004%
9	25.95	-60.61	45.10	-25.95	60.61	-45.10	0.005%
10	-0.14	-60.61	51.80	0.14	60.61	-51.80	0.005%
11	-26.34	-60.61	45.46	26.34	60.61	-45.46	0.005%
12	-37.04	-60.61	36.98	37.04	60.61	-36.98	0.004%
13	-46.76	-60.61	26.98	46.75	60.61	-26.98	0.004%
14	-52.57	-60.61	0.07	52.56	60.61	-0.07	0.005%
15	-44.97	-60.61	-25.78	44.96	60.61	25.77	0.005%
16	-36.81	-60.61	-36.59	36.81	60.61	36.59	0.005%
17	-26.11	-60.61	-45.01	26.11	60.61	45.01	0.005%
18	0.00	-96.92	0.00	0.00	96.92	0.00	0.001%
19	0.06	-96.92	-53.53	-0.06	96.92	53.53	0.003%
20	26.48	-96.92	-45.72	-26.47	96.92	45.72	0.003%
21	37.32	-96.92	-37.29	-37.32	96.92	37.29	0.003%
22	45.62	-96.92	-26.33	-45.62	96.92	26.32	0.003%
23	52.85	-96.92	-0.06	-52.85	96.92	0.06	0.003%
24	46.41	-96.92	26.72	-46.41	96.92	-26.71	0.003%
25	37.10	-96.92	37.00	-37.10	96.92	-37.00	0.003%
26	26.20	-96.92	45.52	-26.20	96.92	-45.52	0.003%
27	-0.47	-96.92	52.56	0.47	96.92	-52.56	0.003%
28	-26.81	-96.92	45.87	26.81	96.92	-45.87	0.003%
29	-37.62	-96.92	37.40	37.62	96.92	-37.39	0.003%
30	-46.91	-96.92	27.07	46.90	96.92	-27.07	0.003%
31	-53.15	-96.92	0.27	53.15	96.92	-0.27	0.003%
32	-45.78	-96.92	-25.88	45.77	96.92	25.88	0.003%
33	-37.41	-96.92	-36.88	37.41	96.92	36.88	0.003%
34	-26.34	-96.92	-45.44	26.34	96.92	45.44	0.003%
35	0.01	-60.61	-18.50	-0.01	60.61	18.50	0.002%
36	9.08	-60.61	-15.66	-9.08	60.61	15.66	0.002%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
37	12.78	-60.61	-12.76	-12.78	60.61	12.76	0.002%
38	15.59	-60.61	-8.99	-15.58	60.61	8.99	0.002%
39	18.11	-60.61	-0.03	-18.11	60.61	0.03	0.002%
40	16.04	-60.61	9.24	-16.04	60.61	-9.24	0.002%
41	12.67	-60.61	12.68	-12.67	60.61	-12.68	0.002%
42	8.98	-60.61	15.61	-8.98	60.61	-15.60	0.002%
43	-0.05	-60.61	17.93	0.05	60.61	-17.92	0.002%
44	-9.11	-60.61	15.73	9.11	60.61	-15.73	0.002%
45	-12.82	-60.61	12.80	12.82	60.61	-12.80	0.002%
46	-16.18	-60.61	9.33	16.18	60.61	-9.33	0.002%
47	-18.19	-60.61	0.02	18.19	60.61	-0.02	0.002%
48	-15.56	-60.61	-8.92	15.56	60.61	8.92	0.002%
49	-12.74	-60.61	-12.66	12.74	60.61	12.66	0.002%
50	-9.03	-60.61	-15.57	9.03	60.61	15.57	0.002%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	15	0.00006904	0.00011706
3	Yes	15	0.00007497	0.00012692
4	Yes	15	0.00007875	0.00013319
5	Yes	15	0.00008026	0.00013571
6	Yes	15	0.00007494	0.00012689
7	Yes	15	0.00006903	0.00011706
8	Yes	15	0.00007087	0.00012021
9	Yes	15	0.00007487	0.00012681
10	Yes	15	0.00008025	0.00013572
11	Yes	15	0.00007486	0.00012674
12	Yes	15	0.00007086	0.00012015
13	Yes	15	0.00006898	0.00011693
14	Yes	15	0.00007483	0.00012666
15	Yes	15	0.00008021	0.00013562
16	Yes	15	0.00007869	0.00013309
17	Yes	15	0.00007486	0.00012675
18	Yes	6	0.00000001	0.00010438
19	Yes	16	0.00006296	0.00010801
20	Yes	16	0.00006666	0.00011415
21	Yes	16	0.00006905	0.00011811
22	Yes	16	0.00006999	0.00011969
23	Yes	16	0.00006661	0.00011409
24	Yes	16	0.00006295	0.00010804
25	Yes	16	0.00006407	0.00010994
26	Yes	16	0.00006657	0.00011409
27	Yes	16	0.00007001	0.00011976
28	Yes	16	0.00006660	0.00011407
29	Yes	16	0.00006407	0.00010991
30	Yes	16	0.00006290	0.00010791
31	Yes	16	0.00006653	0.00011393
32	Yes	16	0.00006997	0.00011963
33	Yes	16	0.00006899	0.00011801
34	Yes	16	0.00006655	0.00011398
35	Yes	15	0.00000001	0.00012167
36	Yes	15	0.00000001	0.00012513
37	Yes	15	0.00000001	0.00012732



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38	Yes	15	0.00000001	0.00012824
39	Yes	15	0.00000001	0.00012516
40	Yes	15	0.00000001	0.00012180
41	Yes	15	0.00000001	0.00012298
42	Yes	15	0.00000001	0.00012516
43	Yes	15	0.00000001	0.00012830
44	Yes	15	0.00000001	0.00012513
45	Yes	15	0.00000001	0.00012293
46	Yes	15	0.00000001	0.00012168
47	Yes	15	0.00000001	0.00012496
48	Yes	15	0.00000001	0.00012809
49	Yes	15	0.00000001	0.00012717
50	Yes	15	0.00000001	0.00012497

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	245 - 230	12.952	40	0.6275	0.0444
T2	230 - 210	10.940	40	0.5971	0.0478
T3	210 - 190	8.506	40	0.5177	0.0440
T4	190 - 180	6.464	40	0.4238	0.0372
T5	180 - 160	5.615	40	0.3752	0.0322
T6	160 - 140	4.208	40	0.2900	0.0256
T7	140 - 120	3.089	40	0.2341	0.0208
T8	120 - 110	2.196	40	0.1818	0.0174
T9	110 - 100	1.823	40	0.1627	0.0152
T10	100 - 80	1.486	40	0.1440	0.0129
T11	80 - 60	0.940	40	0.1067	0.0097
T12	60 - 40	0.528	40	0.0780	0.0067
T13	40 - 20	0.237	46	0.0498	0.0041
T14	20 - 0	0.052	46	0.0218	0.0013

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
247.00	Lightning Rod 2"x10'	40	12.952	0.6275	0.0444	44214
232.00	TMA	40	11.202	0.6024	0.0476	17212
135.00	2.5" Dia. 12' OMNI	40	2.846	0.2205	0.0200	22434
125.00	20' Omni	40	2.400	0.1936	0.0183	23240
110.00	KP4F-23	40	1.823	0.1627	0.0152	36092
105.00	Andrew 6' w/Radome	40	1.650	0.1535	0.0140	30857
60.00	Camera with Mount	40	0.528	0.0780	0.0067	38394
50.00	1.5" Dia 4' Omni w/Pipe Mount	46	0.370	0.0642	0.0054	45414

### Maximum Tower Deflections - Design Wind

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	245 - 230	38.023	24	1.8133	0.1285
T2	230 - 210	32.268	24	1.7227	0.1416
T3	210 - 190	25.229	24	1.5095	0.1347
T4	190 - 180	19.248	24	1.2480	0.1140
T5	180 - 160	16.740	24	1.1104	0.0974
T6	160 - 140	12.551	24	0.8640	0.0777
T7	140 - 120	9.208	24	0.6991	0.0631
T8	120 - 110	6.536	24	0.5433	0.0526
T9	110 - 100	5.422	24	0.4862	0.0463
T10	100 - 80	4.417	24	0.4300	0.0392
T11	80 - 60	2.787	30	0.3182	0.0295
T12	60 - 40	1.564	30	0.2324	0.0204
T13	40 - 20	0.698	30	0.1481	0.0122
T14	20 - 0	0.152	30	0.0648	0.0038

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
247.00	Lightning Rod 2"x10'	24	38.023	1.8133	0.1285	15393
232.00	TMA	24	33.019	1.7385	0.1400	5991
135.00	2.5" Dia. 12' OMNI	24	8.481	0.6586	0.0602	7511
125.00	20' Omni	24	7.146	0.5784	0.0552	7739
110.00	KP4F-23	24	5.422	0.4862	0.0463	11977
105.00	Andrew 6' w/Radome	24	4.904	0.4585	0.0427	10243
60.00	Camera with Mount	30	1.564	0.2324	0.0204	12829
50.00	1.5" Dia 4' Omni w/Pipe Mount	30	1.092	0.1910	0.0163	15108

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	245	Leg	A325N	0.6250	5	0.28	12.89	0.022 ✓	1.333	Bolt DS
T2	230	Leg	A325N	0.7500	5	4.45	18.56	0.240 ✓	1.333	Bolt DS
T3	210	Leg	A325N	1.0000	6	11.17	34.54	0.324 ✓	1.333	Bolt Tension
T4	190	Leg	A325N	1.0000	6	19.17	34.56	0.555 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	4.69	8.16	0.575 ✓	1.333	Member Bearing
T5	180	Leg	A325N	1.0000	6	21.07	34.56	0.610 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	4.63	8.16	0.567 ✓	1.333	Member Bearing
T6	160	Leg	A325N	1.0000	6	24.31	34.56	0.703 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	4.95	8.16	0.607 ✓	1.333	Member Bearing
T7	140	Leg	A325N	1.0000	6	27.81	34.56	0.805 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	5.75	8.16	0.705 ✓	1.333	Member Bearing
T8	120	Diagonal	A325N	1.2500	1	6.33	10.20	0.621 ✓	1.333	Member Bearing

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T9	110	Leg	A325N	1.2500	6	33.25	54.00	0.616 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6.64	10.20	0.651 ✓	1.333	Member Bearing
T10	100	Leg	A325N	1.2500	6	35.17	54.00	0.651 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	7.36	16.99	0.433 ✓	1.333	Member Bearing
T11	80	Leg	A325N	1.2500	6	38.98	54.00	0.722 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	7.77	16.99	0.457 ✓	1.333	Member Bearing
T12	60	Leg	A325N	1.2500	6	42.55	54.00	0.788 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	8.40	16.99	0.494 ✓	1.333	Member Bearing
T13	40	Leg	A325N	1.2500	6	45.87	53.99	0.850 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	10.10	13.59	0.743 ✓	1.333	Member Bearing
T14	20	Leg	A325N	1.2500	6	49.29	54.00	0.913 ✓	1.333	Bolt Tension
		Diagonal	A325N	1.0000	1	18.39	27.19	0.676 ✓	1.333	Member Bearing

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	1 1/2	15.00	2.33	74.7 K=1.00	20.058	1.7672	-25.94	35.44	0.732 ✓
T2	230 - 210	2	20.00	2.38	57.0 K=1.00	23.222	3.1416	-71.96	72.95	0.986 ✓
T3	210 - 190	2 1/2	20.00	2.33	44.8 K=1.00	25.141	4.9087	-118.16	123.41	0.957 ✓
T4	190 - 180	Pirod 105245	10.02	10.02	37.8 K=1.00	26.132	5.3014	-121.67	138.54	0.878 ✓
T5	180 - 160	Pirod 105217	20.03	10.02	37.8 K=1.00	26.132	5.3014	-149.18	138.54	1.077 ✓
T6	160 - 140	Pirod 105218	20.03	10.02	32.4 K=1.00	26.848	7.2158	-175.33	193.73	0.905 ✓
T7	140 - 120	Pirod 105218	20.03	10.02	32.4 K=1.00	26.848	7.2158	-202.10	193.73	1.043 ✓
T8	120 - 110	Pirod 105219	10.02	10.02	28.4 K=1.00	27.351	9.4248	-215.88	257.78	0.837 ✓
T9	110 - 100	Pirod 105219	10.02	5.19	28.4 K=1.00	27.351	9.4248	-229.03	257.78	0.888 ✓
T10	100 - 80	Pirod 105219	20.03	10.02	28.4 K=1.00	27.351	9.4248	-258.51	257.78	1.003 ✓
T11	80 - 60	Pirod 105220	20.03	10.02	25.2 K=1.00	27.723	11.9282	-286.50	330.69	0.866 ✓
T12	60 - 40	Pirod 105220	20.03	10.02	25.2	27.723	11.9282	-314.30	330.69	0.950 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>o</sub> K	Ratio $\frac{P}{P_o}$
T13	40 - 20	Pirod 105220	20.03	10.02	K=1.00 25.2	27.723	11.9282	-341.99	330.69	1.034 ✓
T14	20 - 0	Pirod 112738	20.03	20.03	K=1.00 32.6	26.826	14.7262	-361.37	395.05	0.915 ✓

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L <sub>d</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual V K	Allow. V <sub>o</sub> K	Stress Ratio
T4	190 - 180	0.5	1.47	120.0	10.366	0.1963	0.97	2.28	0.424 ✓
T5	180 - 160	0.5	1.47	120.0	10.279	0.1963	0.55	2.26	0.243 ✓
T6	160 - 140	0.5	1.46	119.0	10.423	0.1963	0.22	2.29	0.097 ✓
T7	140 - 120	0.5	1.46	119.0	10.423	0.1963	0.35	2.29	0.155 ✓
T8	120 - 110	0.625	1.45	94.4	13.671	0.3068	0.29	4.69	0.061 ✓
T9	110 - 100	0.625	1.45	94.4	13.671	0.3068	1.54	4.69	0.329 ✓
T10	100 - 80	0.625	1.45	94.4	13.671	0.3068	0.35	4.69	0.074 ✓
T11	80 - 60	0.625	1.43	93.6	13.766	0.3068	0.22	4.73	0.047 ✓
T12	60 - 40	0.625	1.43	93.6	13.766	0.3068	0.48	4.73	0.101 ✓
T13	40 - 20	0.625	1.43	93.6	13.766	0.3068	2.89	4.73	0.611 ✓
T14	20 - 0	0.75	1.73	93.9	16.080	0.4418	1.41	9.78	0.145 ✓

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>o</sub> K	Ratio $\frac{P}{P_o}$
T1	245 - 230	3/4	4.63	2.24	143.6 K=1.00	7.246	0.4418	-3.29	3.20	1.027 ✓
T2	230 - 210	7/8	5.05	2.45	134.3 K=1.00	8.281	0.6013	-4.33	4.98	0.870 ✓
T3	210 - 190	1	5.48	2.64	126.7 K=1.00	9.307	0.7854	-4.87	7.31	0.666 ✓
T4	190 - 180	L2 1/2x2 1/2x3/16	11.42	5.19	125.8 K=1.00	9.431	0.9020	-5.26	8.51	0.618 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T5	180 - 160	L2 1/2x2 1/2x3/16	12.50	5.84	141.5 K=1.00	7.462	0.9020	-5.09	6.73	0.756
T6	160 - 140	L2 1/2x2 1/2x3/16	13.80	6.54	158.4 K=1.00	5.949	0.9020	-5.33	5.37	0.992
T7	140 - 120	L3x3x3/16	15.24	7.29	146.8 K=1.00	6.931	1.0900	-6.09	7.56	0.806
T8	120 - 110	L3x3x3/16	16.01	7.69	154.7 K=1.00	6.237	1.0900	-6.58	6.80	0.968
T9	110 - 100	L3x3x3/16	16.80	8.09	162.9 K=1.00	5.628	1.0900	-7.01	6.13	1.142
T10	100 - 80	L3x3x5/16	18.45	8.93	181.9 K=1.00	4.515	1.7800	-7.63	8.04	0.949
T11	80 - 60	L3x3x5/16	20.16	9.79	199.5 K=1.00	3.753	1.7800	-8.02	6.68	1.201
T12	60 - 40	L3 1/2x3 1/2x5/16	21.92	10.68	185.7 K=1.00	4.331	2.0900	-8.95	9.05	0.989
T13	40 - 20	L4x4x1/4	23.71	11.58	174.8 K=1.00	4.887	1.9400	-10.98	9.48	1.158
T14	20 - 0	2L3 1/2x3 1/2x5/16x3/4	30.49	14.91	165.7 K=1.00	5.440	4.1800	-16.82	22.74	0.740

### Secondary Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T9	110 - 100	L3x3x5/16	13.48	12.48	254.3 K=1.00	2.309	1.7800	-3.97	4.11	0.966
KL/R > 250 (C) - 232										

### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
T1	245 - 230	7/8	4.00	3.88	212.6 K=1.00	3.305	0.6013	-1.10	1.99	0.555
T2	230 - 210	KL/R > 200 (C) - 5 1	4.01	3.85	184.6 K=1.00	4.382	0.7854	-1.86	3.44	0.542
T3	210 - 190	1	4.52	4.31	206.8 K=1.00	3.492	0.7854	-1.69	2.74	0.615
KL/R > 200 (C) - 107										

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### Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	245 - 230	7/8	4.00	3.88	212.6 K=1.00	3.305	0.6013	-1.71	1.99	0.859 ✓
T2	230 - 210	KL/R > 200 (C) - 8 1	4.49	4.32	207.4 K=1.00	3.472	0.7854	-2.05	2.73	0.751 ✓
T3	210 - 190	KL/R > 200 (C) - 53 1	4.98	4.77	229.2 K=1.00	2.843	0.7854	-1.25	2.23	0.561 ✓
		KL/R > 200 (C) - 110								

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	245 - 230	1 1/2	15.00	0.50	16.0	32.500	0.7732	22.22	25.13	0.884 ✓
T2	230 - 210	2	20.00	0.50	12.0	32.500	1.5625	67.05	50.78	1.320 ✓
T3	210 - 190	2 1/2	20.00	0.67	12.8	30.000	4.9087	115.07	147.26	0.781 ✓
T4	190 - 180	Pirod 105245	10.02	10.02	37.8	30.000	5.3014	115.04	159.04	0.723 ✓
T5	180 - 160	Pirod 105217	20.03	10.02	37.8	30.000	5.3014	135.55	159.04	0.852 ✓
T6	160 - 140	Pirod 105218	20.03	10.02	32.4	30.000	7.2158	156.15	216.47	0.721 ✓
T7	140 - 120	Pirod 105218	20.03	10.02	32.4	30.000	7.2158	177.67	216.47	0.821 ✓
T8	120 - 110	Pirod 105219	10.02	10.02	28.4	30.000	9.4248	188.90	282.74	0.668 ✓
T9	110 - 100	Pirod 105219	10.02	4.82	28.4	30.000	9.4248	199.51	282.74	0.706 ✓
T10	100 - 80	Pirod 105219	20.03	10.02	28.4	30.000	9.4248	222.77	282.74	0.788 ✓
T11	80 - 60	Pirod 105220	20.03	10.02	25.2	30.000	11.9282	244.50	357.85	0.683 ✓
T12	60 - 40	Pirod 105220	20.03	10.02	25.2	30.000	11.9282	265.93	357.85	0.743 ✓
T13	40 - 20	Pirod 105220	20.03	10.02	25.2	30.000	11.9282	289.30	357.85	0.808 ✓
T14	20 - 0	Pirod 112738	20.03	20.03	32.6	30.000	14.7262	295.74	441.79	0.669 ✓

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### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	$L_d$ ft	$Kl/r$	$F_a$ ksi	$A$ in <sup>2</sup>	Actual $V$ K	Allow. $V_a$ K	Stress Ratio
T4	190 - 180	0.5	1.47	120.0	10.366	0.1963	0.97	2.28	0.424 ✓
T5	180 - 160	0.5	1.47	120.0	10.279	0.1963	0.55	2.26	0.243 ✓
T6	160 - 140	0.5	1.46	119.0	10.423	0.1963	0.22	2.29	0.097 ✓
T7	140 - 120	0.5	1.46	119.0	10.423	0.1963	0.35	2.29	0.155 ✓
T8	120 - 110	0.625	1.45	94.4	13.671	0.3068	0.29	4.69	0.061 ✓
T9	110 - 100	0.625	1.45	94.4	13.671	0.3068	1.54	4.69	0.329 ✓
T10	100 - 80	0.625	1.45	94.4	13.671	0.3068	0.35	4.69	0.074 ✓
T11	80 - 60	0.625	1.43	93.6	13.766	0.3068	0.22	4.73	0.047 ✓
T12	60 - 40	0.625	1.43	93.6	13.766	0.3068	0.48	4.73	0.101 ✓
T13	40 - 20	0.625	1.43	93.6	13.766	0.3068	2.89	4.73	0.611 ✓
T14	20 - 0	0.75	1.73	93.9	16.080	0.4418	1.41	9.78	0.145 ✓

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	$L$ ft	$L_u$ ft	$Kl/r$	$F_a$ ksi	$A$ in <sup>2</sup>	Actual $P$ K	Allow. $P_a$ K	Ratio $P/P_a$
T1	245 - 230	3/4	4.63	2.24	143.6	30.000	0.4418	3.30	13.25	0.249 ✓
T2	230 - 210	7/8	5.05	2.45	134.3	30.000	0.6013	4.35	18.04	0.241 ✓
T3	210 - 190	1	5.11	2.46	117.9	30.000	0.7854	5.04	23.56	0.214 ✓
T4	190 - 180	L2 1/2x2 1/2x3/16	11.42	5.19	80.1	21.600	0.9020	4.69	19.48	0.241 ✓
T5	180 - 160	L2 1/2x2 1/2x3/16	11.93	5.59	86.2	21.600	0.9020	4.63	19.48	0.237 ✓
T6	160 - 140	L2 1/2x2 1/2x3/16	13.80	6.54	100.8	21.600	0.9020	4.95	19.48	0.254 ✓
T7	140 - 120	L3x3x3/16	15.24	7.29	93.2	21.600	1.0900	5.75	23.54	0.244 ✓
T8	120 - 110	L3x3x3/16	16.01	7.69	98.2	21.600	1.0900	6.33	23.54	0.269 ✓
T9	110 - 100	L3x3x3/16	16.80	8.09	103.4	21.600	1.0900	6.64	23.54	0.282 ✓



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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T10	100 - 80	L3x3x5/16	18.45	8.93	116.2	21.600	1.7800	7.36	38.45	0.191 ✓
T11	80 - 60	L3x3x5/16	20.16	9.79	127.4	21.600	1.7800	7.77	38.45	0.202 ✓
T12	60 - 40	L3 1/2x3 1/2x5/16	21.92	10.68	118.6	21.600	2.0900	8.40	45.14	0.186 ✓
T13	40 - 20	L4x4x1/4	22.81	11.13	106.9	21.600	1.9400	10.10	41.90	0.241 ✓
T14	20 - 0	2L3 1/2x3 1/2x5/16x3/4	30.49	14.91	165.7	21.600	4.1800	18.39	90.29	0.204 ✓

### Secondary Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T9	110 - 100	L3x3x5/16	13.48	12.48	162.4	21.600	1.7800	3.97	38.45	0.103 ✓

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	7/8	4.00	3.88	212.6	30.000	0.6013	1.02	18.04	0.057 ✓
T2	230 - 210	1	4.01	3.85	184.6	30.000	0.7854	1.96	23.56	0.083 ✓
T3	210 - 190	1	4.52	4.31	206.8	30.000	0.7854	1.81	23.56	0.077 ✓

### Bottom Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	245 - 230	7/8	4.00	3.88	212.6	30.000	0.6013	1.60	18.04	0.088 ✓
T2	230 - 210	1	4.49	4.32	207.4	30.000	0.7854	1.94	23.56	0.082 ✓
T3	210 - 190	1	4.98	4.77	229.2	30.000	0.7854	1.31	23.56	0.056 ✓

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### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	245 - 230	Leg	1 1/2	1	22.22	33.50	66.3	Pass
T2	230 - 210	Leg	2	46	67.05	67.69	99.1	Pass
T3	210 - 190	Leg	2 1/2	103	-118.16	164.50	71.8	Pass
T4	190 - 180	Leg	Pirod 105245	161	-121.67	184.67	65.9	Pass
T5	180 - 160	Leg	Pirod 105217	170	-149.18	184.67	80.8	Pass
T6	160 - 140	Leg	Pirod 105218	185	-175.33	258.24	67.9	Pass
T7	140 - 120	Leg	Pirod 105218	200	-202.10	258.24	78.3	Pass
T8	120 - 110	Leg	Pirod 105219	215	-215.88	343.62	62.8	Pass
T9	110 - 100	Leg	Pirod 105219	224	-229.03	343.62	66.7	Pass
T10	100 - 80	Leg	Pirod 105219	236	-258.51	343.62	75.2	Pass
T11	80 - 60	Leg	Pirod 105220	251	-286.50	440.81	65.0	Pass
T12	60 - 40	Leg	Pirod 105220	266	-314.30	440.81	71.3	Pass
T13	40 - 20	Leg	Pirod 105220	281	-341.99	440.81	77.6	Pass
T14	20 - 0	Leg	Pirod 112738	296	-361.37	526.59	68.6	Pass
T1	245 - 230	Diagonal	3/4	15	-3.29	4.27	77.1	Pass
T2	230 - 210	Diagonal	7/8	58	-4.33	6.64	65.2	Pass
T3	210 - 190	Diagonal	1	115	-4.87	9.74	49.9	Pass
T4	190 - 180	Diagonal	L2 1/2x2 1/2x3/16	166	-5.26	11.34	46.4	Pass
T5	180 - 160	Diagonal	L2 1/2x2 1/2x3/16	175	-5.09	8.97	56.7	Pass
T6	160 - 140	Diagonal	L2 1/2x2 1/2x3/16	190	-5.33	7.15	74.4	Pass
T7	140 - 120	Diagonal	L3x3x3/16	205	-6.09	10.07	60.5	Pass
T8	120 - 110	Diagonal	L3x3x3/16	220	-6.58	9.06	72.6	Pass
T9	110 - 100	Diagonal	L3x3x3/16	228	-7.01	8.18	85.7	Pass
T10	100 - 80	Diagonal	L3x3x5/16	241	-7.63	10.71	71.2	Pass
T11	80 - 60	Diagonal	L3x3x5/16	256	-8.02	8.90	90.1	Pass
T12	60 - 40	Diagonal	L3 1/2x3 1/2x5/16	271	-8.95	12.07	74.2	Pass
T13	40 - 20	Diagonal	L4x4x1/4	286	-10.98	12.64	86.9	Pass
T14	20 - 0	Diagonal	2L3 1/2x3 1/2x5/16x3/4	300	-16.82	30.31	55.5	Pass
T9	110 - 100	Secondary Horizontal	L3x3x5/16	233	-3.97	5.48	72.5	Pass
T1	245 - 230	Top Girt	7/8	5	-1.10	2.65	41.7	Pass
T2	230 - 210	Top Girt	1	50	-1.86	4.59	40.6	Pass
T3	210 - 190	Top Girt	1	107	-1.69	3.66	46.1	Pass
T1	245 - 230	Bottom Girt	7/8	8	-1.71	2.65	64.4	Pass
T2	230 - 210	Bottom Girt	1	53	-2.05	3.63	56.3	Pass
T3	210 - 190	Bottom Girt	1	110	-1.25	2.98	42.1	Pass
							<b>Summary</b>	
							Leg (T2)	99.1 Pass
							Diagonal (T11)	90.1 Pass
							Secondary Horizontal (T9)	72.5 Pass
							Top Girt (T3)	46.1 Pass
							Bottom Girt (T1)	64.4 Pass
							Bolt Checks	68.5 Pass
							<b>RATING =</b>	<b>99.1 Pass</b>

# ANCHOR BOLT ANALYSIS

## ANCHOR BOLT ANALYSIS

### Input Data

#### Max Pier Reactions:

Uplift:	Uplift := 310 kips	user input
Shear:	Shear := 54 kips	user input
Compression:	Compression := 377 kips	user input

#### Anchor Bolt Data:

Bolt Material -> A572 - Gr. 42 (for bolts up to 6" Dia.)

Number of Anchor Bolts = N	$N_b := 6$	user input
Bolt Ultimate Strength:	$F_u := 60 \text{ ksi}$	user input
Bolt Yield Strength:	$F_y := 42 \text{ ksi}$	user input
Bolt Modulus:	$E := 29000 \text{ ksi}$	user input
Thickness of Anchor Bolts	$D := 2.0 \text{ in}$	user input From PiROD DWG No. 202932-B
Threads per Inch:	$n := 4.5$	user input
Coefficient of Friction:	$\mu := 0.55$	user input (for baseplate with grout ASCE 10-97)

## Anchor Bolt Area:

Gross Area of Bolt:

$$A_g := \frac{\pi}{4} \cdot D^2 \qquad A_g = 3.142 \cdot \text{in}^2$$

Net Area of Bolt:

$$A_n := \frac{\pi}{4} \cdot \left( D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 \qquad A_n = 2.498 \cdot \text{in}^2$$

## Check Tensile Forces:

Maximum Tensile Force (Gross Area):

$$\text{AllowableTension} := 1.333 \cdot (0.33 \cdot A_g \cdot F_u) \qquad \text{AllowableTension} = 82.9 \cdot \text{kips}$$

Note: 1.333 increase allowed per TIA/EIA

Maximum Tensile Force (Net Area):

$$F_{\text{net.area}} := 1.333 \cdot (0.60 \cdot A_n \cdot F_y) \qquad F_{\text{net.area}} = 83.9 \cdot \text{kips}$$

Note: 1.333 increase allowed per TIA/EIA

Applied Tension:

$$\text{MaxTension} := \frac{\text{Uplift}}{N} \qquad \text{MaxTension} = 51.7 \cdot \text{kips}$$

Check Stresses:

$$\frac{\text{MaxTension}}{F_{\text{net.area}}} = 0.62$$

$$\text{Condition1} := \text{if} \left( \frac{\text{MaxTension}}{F_{\text{net.area}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

**Condition1 = "OK"**

## Check Anchor Bolt Area:

Based on the ASCE 10-97 Design of Latticed Steel Transmission Structures

Required Area:

$$A_{s1} := \frac{\text{Uplift}}{F_y} + \frac{\text{Shear}}{\mu \cdot 0.85 \cdot F_y} \quad A_{s1} = 10.1 \cdot \text{in}^2$$

$$A_{s2} := \left\lceil \frac{\text{Shear} - (0.3 \cdot \text{Compression})}{\mu \cdot 0.85 \cdot F_y} \right\rceil \quad A_{s2} = 3.0 \cdot \text{in}^2$$

Provided Area:

$$A_{s\text{provided}} := A_n \cdot N \quad A_{s\text{provided}} = 15.0 \cdot \text{in}^2$$

$$\text{Condition2} := \text{if} \left( \frac{A_{s1}}{A_{s\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

$$\frac{A_{s1}}{A_{s\text{provided}}} = 0.68$$

Condition2 = "OK"

$$\text{Condition3} := \text{if} \left( \frac{A_{s2}}{A_{s\text{provided}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

$$\frac{A_{s2}}{A_{s\text{provided}}} = 0.20$$

Condition3 = "OK"

# FOUNDATION ANALYSIS



## FOUNDATION ANALYSIS

### Input Data

#### Maximum Pier Reactions:

Compression:  $C_t := 377 \text{ kips}$  *user input*  
 Uplift:  $U_t := 310 \text{ kips}$  *user input*

#### Material Properties:

Unit Weight of Concrete:  $\gamma_c := 150 \text{ pcf}$  *user input*  
 Unit Weight of Water:  $\gamma_w := 62.4 \text{ pcf}$  *user input*  
 Unit Weight of Soil:  $\gamma_s := 125 \text{ pcf}$  *user input*

#### Foundation Dimensions:

Drilled Caisson Length:  $C_{Length} := 31 \text{ ft}$  *user input*  
 Diameter of Pier:  $d_p := 5.5 \text{ ft}$  *user input*  
 Extension of Pier Above Grade:  $L_{pag} := 0.5 \text{ ft}$  *user input*

Allowable Soil Bearing Capacity:  $q_s := 5000 \text{ psf}$  *user input*  
 Water Table Below Grade:  $Wd := 32 \text{ ft}$  *user input*  
 Average Allowable Shear:  $fl := 1020 \text{ psf}$  *user input*  
 Depth Neglected for Skin Friction at Top:  $Depthunbond := 1.0 \text{ ft}$  *user input*

#### Loading:

$$TotalDownLoad := C_t + \pi \cdot \frac{d_p^2}{4} \cdot [L_{pag} \cdot \gamma_c + [\gamma_c \cdot (C_{Length} - L_{pag})]]$$

TotalDownLoad = 487.5 kips

$$PierWeight := \pi \cdot \frac{d_p^2}{4} \cdot [(Wd + L_{pag}) \cdot \gamma_c + (C_{Length} - Wd - L_{pag}) \cdot (\gamma_c - \gamma_w)]$$

PierWeight = 112.7 kips

$$SoilShear := \pi \cdot d_p \cdot [fl \cdot (Wd - Depthunbond) + fl \cdot (C_{Length} - Wd - L_{pag})]$$

SoilShear = 519.9 kips

Job	<u>250' (SST) Self-Supporting Tower - Mansfield, CT</u>	Project No.	<u>TWS-019</u>	Sheet	<u>2</u> of <u>2</u>
Description	<u>Drilled Pier Caisson Evaluation</u>	Computed by	<u>MCD</u>	Date	<u>12/30/14</u>
		Checked by	<u>    </u>	Date	<u>    </u>

## Compression Capacity:

$$\text{TotalDownLoadCapacity} := \text{SoilShear} + q_s \left( \pi \cdot \frac{d_p^2}{4} \right)$$

$$\text{TotalDownLoadCapacity} = 638.7 \text{ kips}$$

$$\text{CheckDownLoadCapacity} := \text{if}(\text{TotalDownLoad} < \text{TotalDownLoadCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckDownLoadCapacity} = \text{"Okay"}$$

## Tension Capacity:

$$\text{TotalUpLiftCapacity} := \text{SoilShear} + \text{PierWeight}$$

$$\text{TotalUpLiftCapacity} = 632.6 \text{ kips}$$

$$\text{CheckUpLiftCapacity} := \text{if}(U_t < \text{TotalUpLiftCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckUpLiftCapacity} = \text{"Okay"}$$

$$\text{SafetyFactor}_{\text{provided}} := \frac{\text{TotalUpLiftCapacity}}{U_t}$$

$$\text{SafetyFactor}_{\text{provided}} = 2.04$$

## Check Cone Failure:

$$\text{ConeFailureCapacity} := \frac{\left[ (C_{\text{Length}} - L_{\text{pag}}) \tan(30\text{deg}) \cdot 2 + d_p \right]^2 \cdot \pi \cdot C_{\text{Length}} - L_{\text{pag}}}{4} \cdot \gamma_s$$

$$\text{ConeFailureCapacity} = 1654.85 \text{ kips}$$

$$\text{CheckConeFailureCapacity} := \text{if}(U_t < \text{ConeFailureCapacity}, \text{"Okay"}, \text{"No Good"})$$

$$\text{CheckConeFailureCapacity} = \text{"Okay"}$$

$$\text{ConeSafetyFactor}_{\text{provided}} := \frac{\text{ConeFailureCapacity}}{U_t}$$

$$\text{ConeSafetyFactor}_{\text{provided}} = 5.34$$