



STATE OF CONNECTICUT  
CONNECTICUT SITING COUNCIL

Ten Franklin Square  
New Britain, Connecticut 06051  
Phone: (860) 827-2935  
Fax: (860) 827-2950

December 19, 2000

Kenneth C. Baldwin  
Robinson & Cole  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **EM-XM-077-001129** - XM Satellite Radio notice of intent to modify an existing telecommunications facility located at 266 Center Street, Manchester, Connecticut. (Docket No. 129)

Dear Attorney Baldwin:


At a public meeting held on December 14, 2000, the Connecticut Siting Council (Council) acknowledged your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modifications are to be implemented as specified here and in your notices dated November 28, 2000, and December 11, 2000. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,

  
Mortimer A. Gelston  
Chairman

MAG/FOC/laf

c: Honorable Stephen T. Cassano, Mayor, Town of Manchester  
Richard J. Sartor, General Manager, Town of Manchester  
Christine Belvin, LCC International, Inc.  
Christopher Ciolfi, Crown Atlantic Company  
Sandy M. Carter, Verizon Wireless

# ROBINSON & COLE LLP

HARTFORD • STAMFORD • GREENWICH • NEW YORK • BOSTON

LAW OFFICES

280 Trumbull Street  
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860-275-8200  
Fax 860-275-8299

Kenneth C. Baldwin  
860-275-8345  
Internet: kbaldwin@rc.com

December 11, 2000

## *Fax and Regular Mail*

Fred O. Cunliff  
Siting Analyst  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**RECEIVED**

DEC 12 2000

CONNECTICUT  
SITING COUNCIL

**Re: Corrections to Exempt Modification Filings**

Dear Mr. Cunliff:

As a follow-up to our telephone conversation, I am writing to make the Council aware of certain corrections which need to be made to the Crown Atlantic Company LLC exempt modification notices for Manchester, East Hartford and Fairfield. Those corrections are as follows:

### XM Radio/Manchester

Replace paragraph number 4 of Crown's November 28, 2000 filing with the following:

The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst case" RF power density calculation for the closest point at the site boundary for the existing Cellco antennas on the tower, as described in the Council's Decision and Order dated March 12, 1990, would be 0.0737 mW/cm<sup>2</sup> or 2.92% of the FCC standard for uncontrolled environments. XM's operation at the Manchester site would add 0.144607 mW/cm<sup>2</sup> or 14.4607% of the FCC standard. (See attached RF power density calculations.) The calculated worst case power density for the combined operation at the site would therefore be 17.3807% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

### XM Radio/Fairfield

Replace paragraph number 4 of Crown's November 28, 2000 filing with the following:

Fred O. Cunliff  
December 11, 2000  
Page 2

The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst case" RF power density calculation for the closest point at the site boundary for the existing providers on the tower, would be 14.66% of the FCC standard for uncontrolled environments. XM's operation at the Fairfield site would add 0.184215 mW/cm<sup>2</sup> or 18.4251% of the FCC standard. (See attached RF power density calculations.) The proposed Metricom installation would add 0.0002 mW/cm<sup>2</sup> (0.028% of the FCC standard). The calculated worst case power density for the combined operation at the site would therefore be 33.1131% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

### XM Radio/East Hartford

The third paragraph on the first page of the November 29, 2000 filing incorrectly references an antenna height for the XM Radio of 126 feet above ground level. As stated in paragraph number 1 of the filing the antenna height will not exceed 123 feet.

### Metricom/XM Radio/Fairfield

Lastly, I have enclosed complete copies of the June 5, 2000 and September 13, 2000 structural analyses for the Fairfield tower. First and forward, these analyses conclude that the tower is structurally capable of supporting the addition of both Metricom and XM Radio antennas. The best way to explain the reduction in tower stresses referred to on page three of the June 5 and September 13 analyses is by referring you back to the antennae load listing on page one of each report.

In the June 5 analysis, the antenna load listing included 3-RR90-17 antennas for AT&T; 12-ALP 9212 antennas for Verizon Wireless; 12-ALP 11011A antennas for SNET; 6-ALP199015 antennas for Voicestream; 12-ALP 9212 antennas for a potential "future carrier"; 3 whip antennas for PageNet; 1-TA-2350-LCC whip antenna for XM Radio; and 1 TA2324-LHCP dish antenna.


The September 13 analysis includes the same antenna loading requirements for the AT&T, Verizon Wireless, SNET, Voicestream, PageNet and XM Radio antennas, adds 16 Larson panel antennas on side-arms for Metricom and removes the 12-ALP 9212 panel antennas listed for the "future carrier", and its associated antenna platform. The removal of the "future carriers" antennas and antenna platform from the 128 foot level, together with the addition of the Metricom antennas at the 100 foot level explains the reduction in tower stresses documented in the September 13 analysis.

# ROBINSON & COLE LLP

Fred O. Cunliff  
December 11, 2000  
Page 3

If you have any additional questions or concerns regarding these filings please do not hesitate to contact me.

Sincerely,

A handwritten signature in black ink, appearing to read "Kenneth C. Baldwin". The signature is fluid and cursive, with a long horizontal stroke at the end.

Kenneth C. Baldwin

KCB/kmd  
Enclosure  
cc: Hal Giglio

# ROBINSON & COLE LLP

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LAW OFFICES

280 Trumbull Street  
Hartford, CT 06103-3597  
860-275-8200  
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Kenneth C. Baldwin  
860-275-8345  
Internet: kbaldwin@rc.com

November 29, 2000

Mr. Joel M. Rinebold  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**RECEIVED**

NOV 30 2000

**CONNECTICUT  
SITING COUNCIL**


**Re: Exempt Modification Filings for XM Radio in Manchester and Fairfield,  
Connecticut**

Dear Mr. Rinebold:

Enclosed please find two letters from H. E. Bergeron Engineers relating to the structural analysis completed for the Crown towers in Fairfield and Manchester, Connecticut. This information is intended to supplement Crown's recent filings on behalf of XM Radio.

Please contact me if you have any questions.

Sincerely,



Kenneth C. Baldwin

KCB/kmd  
Enclosures

cc: John G. Metsopoulos, Fairfield First Selectman  
Stephen T. Cassano, Manchester Mayor  
Christine Belvin, LCC International, Inc.

HEB

November 28, 2000

Crown Castle International  
156 Old Chester Road  
Haddam, Connecticut 06438

Attn: Hal Giglio  
Re: Fairfield, Connecticut  
XM Radio Antenna Change

Dear Hal,


H. E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of Crown Castle's 171-foot Valmont monopole tower located in Fairfield, Connecticut.

HEB performed this analysis with XM Radio using a TA-2350-LCC omnidirectional antenna mounted and a TA-2324-LHCP parabolic antenna mounted at 128-feet. You indicated that XM Radio is proposing to install the TA2324-LHCP parabolic antenna at 75-feet.

Because the parabolic antenna will be located at a lower elevation, stresses on the tower are reduced. Therefore the tower is capable of supporting the proposed antenna change.

Please feel free to contact me if you have any questions.

Sincerely,  
H. E. Bergeron Engineers, P.A.



Robert E. Adair, P.E.  
Senior Project Engineer



P:\jobs\2000-085\Fairfield, CT ltr 11-28-00.doc

P.O. Box 440  
2605 White Mountain Highway  
North Conway, NH 03860  
(603) 356-6936  
(603) 356-7715 (fax)

65 W. Commercial Street  
Portland, ME 04101  
(207) 780-1100  
(207) 780-1101 (fax)  
www.hebcivil.com



November 28, 2000

Crown Castle International  
156 Old Chester Road  
Haddam, Connecticut 06438

Attn: Hal Giglio  
Re: Manchester, Connecticut  
XM Radio Antenna Change

Dear Hal,

H. E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of Crown Castle's 115-foot Valmont monopole tower located in Manchester, Connecticut.

HEB performed this analysis with XM Radio using a TA-2350-LCC omnidirectional antenna mounted at a centerline elevation of 124-feet on a pipe extension, and a TA-2324-LHCP parabolic antenna mounted at 80-feet. You indicated that XM Radio is proposing to install the TA2324-LHCP parabolic antenna at 30-feet.

Because the parabolic antenna will be located at a lower elevation, stresses on the tower are reduced. Therefore the tower is capable of supporting the proposed antenna change.

Please feel free to contact me if you have any questions.

Sincerely,  
H. E. Bergeron Engineers, P.A.

Robert E. Adair, P.E.  
Senior Project Engineer



P:\jobs\2000-084\Manchester, CT ltr 11-28-00.doc

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860-275-8200  
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EM-XM-077-001129

Kenneth C. Baldwin  
860-275-8345  
Internet: kbaldwin@rc.com

November 28, 2000

*Via Federal Express*

Mr. Joel M. Rinebold  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**RECEIVED**

NOV 29 2000

CONNECTICUT  
SITING COUNCIL

**Re: Notice of Exempt Modification  
Siting Council Docket No. 129  
266 Center Street, Manchester, Connecticut**

Dear Mr. Rinebold:

Crown Atlantic Company LLC ("Crown") holds the Siting Council certificate for the existing telecommunications tower and related facility in Manchester, Connecticut (Docket No. 129). Crown intends to allow XM Satellite Radio ("XM") to install antennas and related equipment at the existing facility in Manchester. Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Manchester Mayor, Stephen T. Cassano.

The existing facility consists of a self-supporting monopole tower and a single-story equipment building within a fenced compound, located off Center Street in Manchester. This facility was approved by the Connecticut Siting Council on March 12, 1990. The tower currently supports antennas of Cellco Partnership d/b/a Verizon Wireless ("Cellco").

XM proposes to install a single Til-Tek omnidirectional antenna on the top of the tower and a 25.25 inch diameter, received only, dish antenna at the 30-foot level on the tower. XM equipment will be located in a new 10-foot by 12-foot building located near the base of the tower within the existing site compound. (See attached plans.)

The planned modifications to the Manchester facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the overall height of the structure above that which was approved by the Council at this site. In its Docket No. 129 Decision and Order, the Council stated that "[t]he monopole tower including antennas and associated equipment shall not exceed a height of 128 feet above ground level, 324 feet AMSL". The XM



# ROBINSON & COLE LLP

Joel M. Rinebold  
November 28, 2000  
Page 2

omnidirectional antenna will be mounted on the tower, with its center line at approximately the 125-foot level and its top at the 128-foot level, within the Council's height restriction. The XM dish antenna would be mounted at the 30-foot level on the tower. The enclosed tower drawings confirm that the planned modifications will not extend above the 128-foot height limitation for the tower including antennas approved by the Council in Docket No. 129.

2. The installation of the XM equipment shelter, as shown on the attached project plans, will not require an extension of the site boundaries.

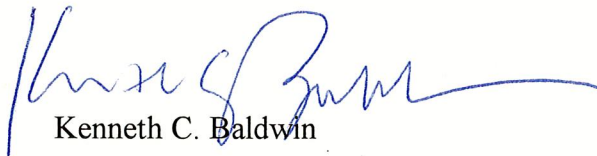
3. The proposed modifications to the facility will not increase the noise levels at the existing facility by six decibels or more.

4. The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst-case" RF power density calculation for the closest point at the site boundary for the existing Cellco antennas on the tower, as described in the Council's Decision and Order dated March 12, 1990, would be  $0.0737 \text{ mW/cm}^2$  or 2.92% of the FCC standard for uncontrolled environments. XM's operations at the Manchester site would add  $0.184520 \text{ mW/cm}^2$  or 18.452% of the FCC standard. (See attached RF Power Density Calculations.) The calculated "worst-case" power density for the combined operations at the site would therefore be 21.372% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

Also attached is a copy of a structural analysis verifying that the tower can accommodate the XM antennas. Please note that the structural analysis contemplated the XM dish antenna being located at the 80-foot level on the tower rather than the 30-foot level as proposed. The structural analysis is therefore more conservative than necessary for the proposed antenna installation.

For the foregoing reasons, Crown respectfully submits that the proposed addition of antennas and equipment at the Manchester facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

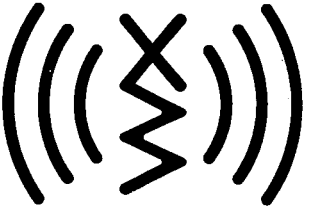
Sincerely,



Kenneth C. Baldwin

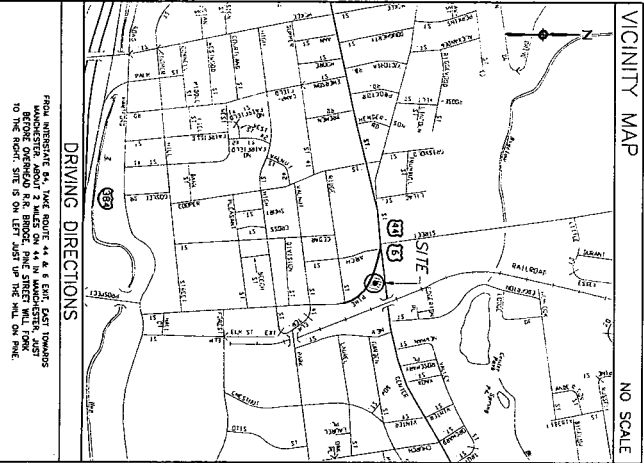
KCB/kmd  
Attachments

cc: Stephen T. Cassano, Manchester Mayor  
Tara K. Rand, Crown Atlantic Company, LLC  
Christine Belvin, LCC International, Inc.



SATELLITE  
RADIO

**CROWN-MANCHESTER HRT093  
REAR 266 CENTER STREET  
MANCHESTER, CONNECTICUT 06040  
SITE ID: HAR011.A**



PROJECT DESCRIPTION						
1. THE PROPOSED SITE IS AN EXISTING ONE-FAMILY RESIDENTIAL HOME.						
2. THE PROPOSED REGULATORY CONSIDERS THE FOLLOWING:						
(1) - One Antenna						
(2) - Satellite Dish						
(3) - One to Two Jumper						
(4) - One to Two 4' x 12'-0" Equipment Shelter						
ANTENNA DATA						
TYPE: X-M	MODEL NO.: T					
OWNER: X-M	NUMBER: 1					
DIAMETER: 16'-0"	HEIGHT: 14'					
MANUFACTURER: T-1524-100	TYPE: DISH					
APPROVALS: BY DATE	23,217					
SITE ACQUISITION						
OWNER: _____	DATE: _____					
SITE INFORMATION						
CONTACT: 789 840 (781)-728-4001						
LONGITUDE: -72.5528						
SITE NUMBER: 100						
SITE ADDRESS: 266 CENTER STREET MANCHESTER, CONNECTICUT 06040						
SITE NUMBER: 06011A						
CURRENT ZONING: RR - (RURAL RESIDENTIAL)						
JURISDICTION: TOWN OF MANCHESTER, CONNECTICUT						
PROPERTY OWNER: CROWN CASTLE COMMUNICATIONS, INC. 500 WEST CHAMBERS PARK MANHATTAN, NY 10101						
APPLICANT: X-M SATELLITE RADIO CROWN CORPORATION, A.S. 500 WEST CHAMBERS PARK MANHATTAN, NY 10101						
DRAWING LIST						
1-1 TITLE SHEET						
A-1 COMPOUND PLAN, DETAILS AND ANTENNA SPECIFICATIONS						
A-2 WINDSHIELD EXTENSION AND DETAILS						
A-3 TYPICAL EQUIPMENT RISER DIAGRAM						
E-1 EQUIPMENT FOUNDATION PLAN, DETAILS AND SYMBOL LIST						
E-2 ELECTRICAL RISER DIAGRAM AND DETAILS						
GH-1 GENERAL NOTES						
MATERIAL LIST						
ITEM NO.	DESCRIPTION	SIZE	QTY.	LENGTH	SUPPLIER/MODEL #	MANUFACTURER
1	DISH ANTENNA	32.37' DIAMETER	1	14'-3.33'-10.00"-H	1A-2320-100-1	T-1524-100
2	ONE ANTENNA	64" H x 4" W DIA.	1	N/A	1A-2320-100-1	T-1524-100
3	EQUIPMENT SHELTER	10'-0" x 12'-0"	1	N/A	10'-0" x 12'-0"	AMERICAN CORP.
4	ONE CABLE FOR DISH	7/8"	1	36'	1001-50A	AMERICAN CORP.
5	ONE CABLE FOR DISH	1 5/8"	1	160'	1001-50A	AMERICAN CORP.
6	JUMPER FOR DISH CABLE TOP/BOTTOM	1/2"	2	6'	155001 20611	AMERICAN CORP.
7	JUMPER FOR DISH CABLE TOP	1/2"	1	3'	155001 8233A	AMERICAN CORP.
8	JUMPER FOR DISH CABLE BOTTOM	1/2"	1	3'	155001 8233Z	AMERICAN CORP.
9	CONNECTION FOR DISH BOTTOM JUMPER	1/2" 4-WALE	2	N/A	1430A	AMERICAN CORP.
10	CONNECTION FOR DISH CABLE	7/16" DIN-FEMALE	2	N/A	155001 55568	AMERICAN CORP.
11	CONNECTION FOR DISH, TOP AND BOTTOM JUMPER	7/16" DIN-FEMALE	2	N/A	155001 55568	AMERICAN CORP.
12	CONNECTION FOR DISH, TOP JUMPER	7/16" DIN-FEMALE	2	N/A	155001 55568	AMERICAN CORP.
13	CONNECTION FOR DISH, BOTTOM JUMPER	7/16" DIN-FEMALE	2	N/A	155001 55568	AMERICAN CORP.
14	CONNECTION FOR DISH, BOTTOM JUMPER	7/16" DIN-FEMALE	2	N/A	155001 55568	AMERICAN CORP.

**URSA**  
URS CORPORATION  
500 ENTERPRISE DRIVE  
ROCKVILLE, CT 06067  
TEL: (860) 231-0227  
FAX: (860) 231-0227

**STATE OF CONNECTICUT**  
REGISTERED PROFESSIONAL ENGINEER  
No. 11330  
PROJECT# 11111330009

DRAWN BY: DFC  
CHECKED BY: ICA  
ISSUED FOR: 10-13-09 REVIEW  
11-13-09 PRINTING

THE INFORMATION CONTAINED IN THIS SET OF DOCUMENTS IS FOR USE ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED THEREIN. IT IS STRICTLY PROHIBITED TO REPRODUCE, TRANSMIT, OR DISSEMINATE THIS INFORMATION IN ANY MANNER WITHOUT THE WRITTEN PERMISSION OF THE ENGINEER OF RECORD.

**CROWN-MANCHESTER  
SITE ID: HAR011.A**  
REAR 266 CENTER STREET  
MANCHESTER, CONNECTICUT  
06040

SCALE: AS NOTED  
DATE: 11-07-09

TITLE SHEET  
**T-1**

**HEAD POWER DIRECTIONAL ANTENNA**

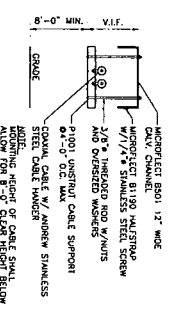
IL-TEK IA-230-1-0C-H ELECTRICAL SPECIFICATIONS  
 FREQUENCY RANGE: 2300-2345 MHz  
 GAIN: 10 dBi  
 VSWR: 1.3:1 MAXIMUM  
 POLARIZATION: LEFT HANDED CIRCULAR  
 POWER RATING: 2000 WATT AVERAGE  
 8000 WATT PEAK  
 H-PLANE BEAMWIDTH (-3 dB): 360 DEGREES  
 E-PLANE BEAMWIDTH (-3 dB): 13.5 DEGREES  
 CROSS-POLARIZATION DISCRIMINATION: 15 dB  
 FRONT TO BACK RATIO: N/A  
 NULL FILL: DOWN-HILL  
 TERMINATION: 7/8" CW RFLX  
 IMPEDANCE: 50 OHMS NOMINAL

**DSL SPECIFICATIONS**

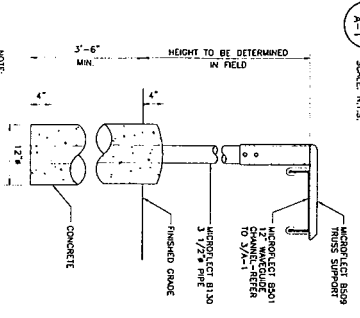
IL-TEK IA-232-1-0C-E ELECTRICAL SPECIFICATIONS  
 FREQUENCY RANGE: 2300-2345 MHz  
 GAIN: 21 dBi  
 VSWR: 1.3:1 MAXIMUM  
 POLARIZATION: LEFT HANDED CIRCULAR  
 POWER RATING: 2000 WATT AVERAGE  
 8000 WATT PEAK  
 H-PLANE BEAMWIDTH (-3 dB): 360 DEGREES  
 E-PLANE BEAMWIDTH (-3 dB): 13.5 DEGREES  
 CROSS-POLARIZATION DISCRIMINATION: 15 dB  
 FRONT TO BACK RATIO: N/A  
 NULL FILL: NONE  
 TERMINATION: 7/8" CW RFLX  
 IMPEDANCE: 50 OHMS NOMINAL

IL-TEK IA-230-1-0C-H MECHANICAL SPECIFICATIONS  
 LENGTH: 64in (1625 mm)  
 DIAMETER: 9 1/4" (235 mm)  
 WEIGHT INCLUDING CLAMPS: 148 lb (67 kg)  
 MOUNTS TO A 1.75-4 DIA. (44.5-102mm) O.D. PIPE

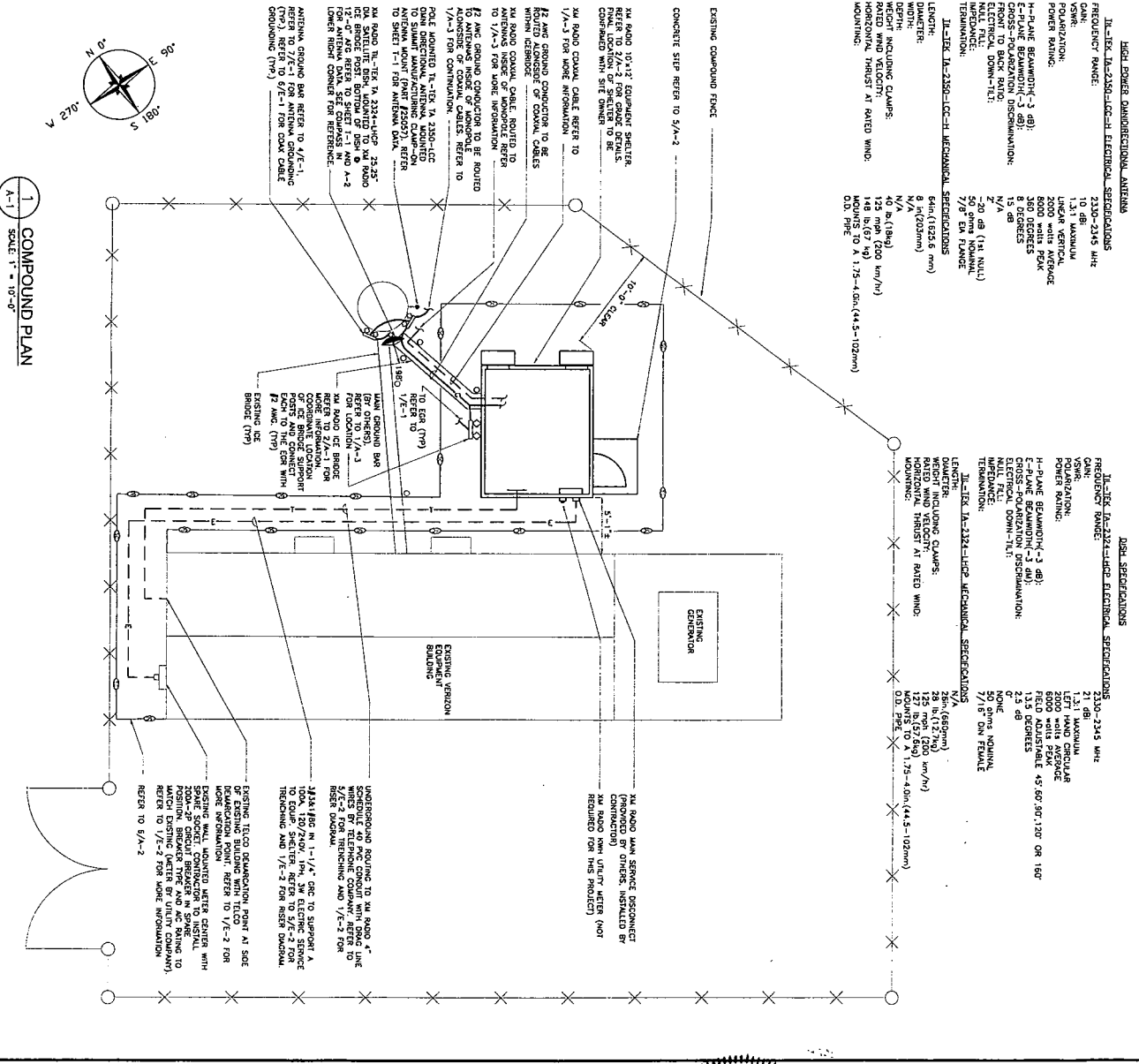
IL-TEK IA-232-1-0C-E MECHANICAL SPECIFICATIONS  
 LENGTH: 26in (660 mm)  
 DIAMETER: 12 1/2" (318 mm)  
 WEIGHT INCLUDING CLAMPS: 127 lb (57 kg)  
 MOUNTS TO A 1.75-4 DIA. (44.5-102mm) O.D. PIPE



**3 CABLE SUPPORT DETAIL**  
 SCALE: N.T.S.



**2 ICE BRIDGE DETAIL**  
 SCALE: N.T.S.



**1 COMPOUND PLAN**  
 SCALE: 1" = 10'-0"

**ULCC**  
 1792 MAIN STREET  
 EAST HARTFORD, CT 06108  
 1-(860)-291-0627

**URS**  
 URS CORPORATION  
 500 ENTERPRISE DRIVE  
 ROCKY HILL, CT 06067  
 (860) 270-1100

**STATE OF CONNECTICUT**  
 REGISTERED PROFESSIONAL ENGINEER  
 No. 8704  
 PROJECT No. A-1588-09

**ISSUED FOR**  
 10-15-09 REVIEW  
 11-13-09 PERMITTING

**CHOWN-MANCHESTER**  
 SITE ID: HARBOTLA  
 266 CENTER STREET  
 MANCHESTER, CONNECTICUT  
 06040

**SCALE: AS NOTED**  
**DATE: 11-07-00**  
**COMPOUND PLAN, DETAILS AND ANTENNA SPECS.**  
**A-1**

**CONCRETE AND REINFORCING STEEL NOTES**

1. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH THE ACI 301, ACI 318 AND THE SPECIFICATION CAST-IN-PLACE CONCRETE.
2. ALL CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 3000 PSF AT 28 DAYS. STEELS WIELD OTHERWISE.
3. UNLESS NOTED OTHERWISE, WELDED WIRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC.
4. THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON DRAWINGS:  
CONCRETE CAST AGAINST EARTH.....3 IN.  
CONCRETE EXPOSED TO EARTH OR WEATHER.....1 1/2 IN.  
CONCRETE NOT EXPOSED TO EARTH OR WEATHER OR NOT CAST AGAINST THE GROUND.....1 1/2 IN.  
SLAB AND WALL.....1 1/2 IN.

**DESIGN LIVE LOADS**

SHOW LIVE LOAD (PL)  
UNIFORM LOAD (PL)  
CONCENTRATED LOAD (P)  
IMPOSED FACTOR (IF)  
EXPLOSION FACTOR (EF)

30 PSF	80 LBS/FT
1.75	18.4 PSF
	1.17

**FOUNDATION NOTES**

1. A PRESUMED SOIL BEARING CAPACITY OF 3000 PSF WAS USED FOR THE DESIGN OF FOUNDATIONS UNLESS OTHERWISE SPECIFIED.
2. ALL FOUNDATIONS SHALL BE ON EXISTING UNDISTURBED ORGANIC FREE SOIL. ALL UNDESIRABLE SOIL SHALL BE REMOVED AS DIRECTED BY THE CONTRACTOR AND REPLACED WITH APPROVED GRANULAR FILL. ALL FOUNDATIONS SHALL BE CONSTRUCTED TO A MINIMUM DEPTH OF 36" BELOW FINISHED GRADE UNLESS OTHERWISE SPECIFIED.

**STRUCTURAL STEEL NOTES**

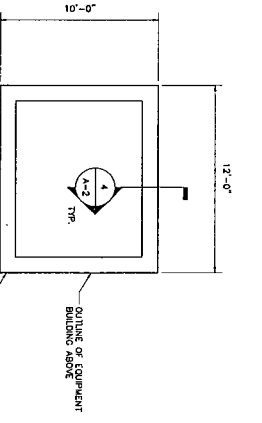
1. ALL WORK SHALL COMPLY WITH THE 1989 CONNECTICUT STATE BUILDING CODE.
2. ALL STEEL WORK SHALL BE GALVANIZED AND IN ACCORDANCE WITH THE SPECIFICATION ASTM A572 GRADE 50 UNLESS OTHERWISE NOTED OTHERWISE.
3. ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AWS D1.1 WELDED FIELD JOINTS. ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AWS D1.1 WELDED FIELD JOINTS.
4. BOLTED CONNECTIONS SHALL USE BOLTING THE GALVANIZED ASTM A325 BOLTS (3/4" DIA) AND SHALL HAVE MINIMUM OF TWO BOLTS UNLESS NOTED OTHERWISE.
5. CONNECTIONS TO METAL SHALL BE WELDED TO MEETING FRAME WITH (4) 1/2" DIA. BOLTS TO BE PROVIDED BY OTHER.



**6 BITUMINOUS REPAIR DETAIL**  
SCALE: 1/8" = 1'-0"

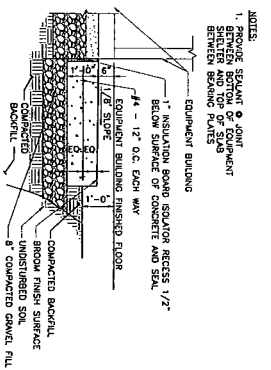


**4 SECTION - ALTERNATE #1**  
SCALE: 1/8" = 1'-0"

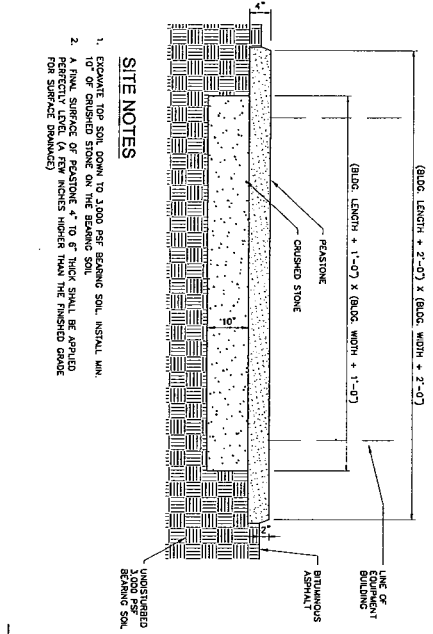


**3 CONC. GRADE BEAM DETAIL - ALTERNATE #1**  
SCALE: 1/8" = 1'-0"

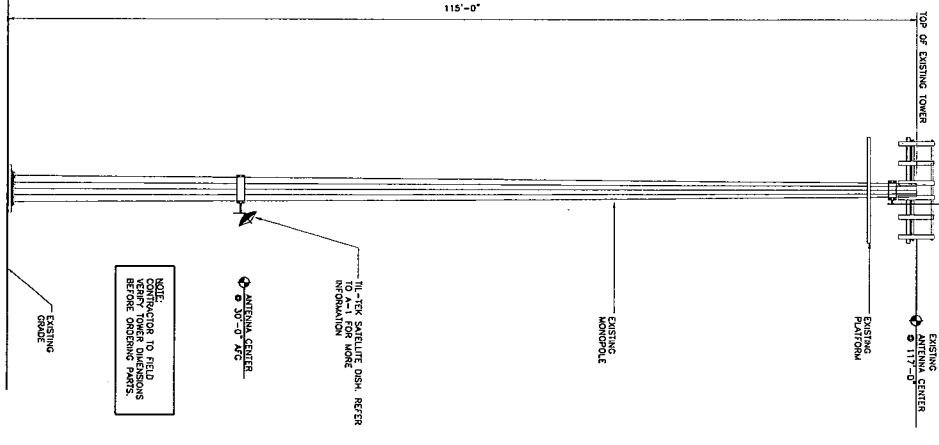
**5 CONCRETE STEP DETAIL**  
SCALE: 1/8" = 1'-0"



**2 GRADE DETAIL**  
SCALE: 1/8" = 1'-0"



**1 MONOPOLE ELEVATION**  
SCALE: 1/16" = 1'-0"



<p><b>URS</b> URS CORPORATION 405 NORTH WASHINGTON ST. ANN ARBOR, MI 48106-1500 TEL: 734.769.7000</p>	<p>7921 MAIN STREET SUITE D EAST HARTFORD CT 06108 1-860-281-0627</p>
	<p>THE INFORMATION CONTAINED IS PROPRIETARY BY NATURE ANY USE OR DISCLOSURE OTHER THAN THAT WHICH SPECIFICALLY PROHIBITED.</p>
	<p><b>CROWN-MANCHESTER</b> SITE ID: HARTF1A REAR 266 CENTER STREET MANCHESTER CT 06040</p>
	<p>SCALE: AS NOTED DATE: 11-07-00</p>
	<p><b>MONOPOLE ELEVATION AND DETAILS</b> <b>A-2</b></p>



520 2341 RT. 1N. GATE 12  
 WASHINGTON, DC 20008  
 PHONE (202) 396-7200  
 FAX (202) 396-7100

**URS**

URS CORPORATION, A/E/S  
 500 ENTERPRISE DRIVE  
 ROCKY HILL, CT 06067



PROJECT: 10211190188003

DRAWN BY: DFG

CHECKED BY:

ISSUED FOR:

10-12-00 REVIEW

11-13-00 FINALING

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**CROWN-MANCHESTER  
 SITE ID: HAR011A**

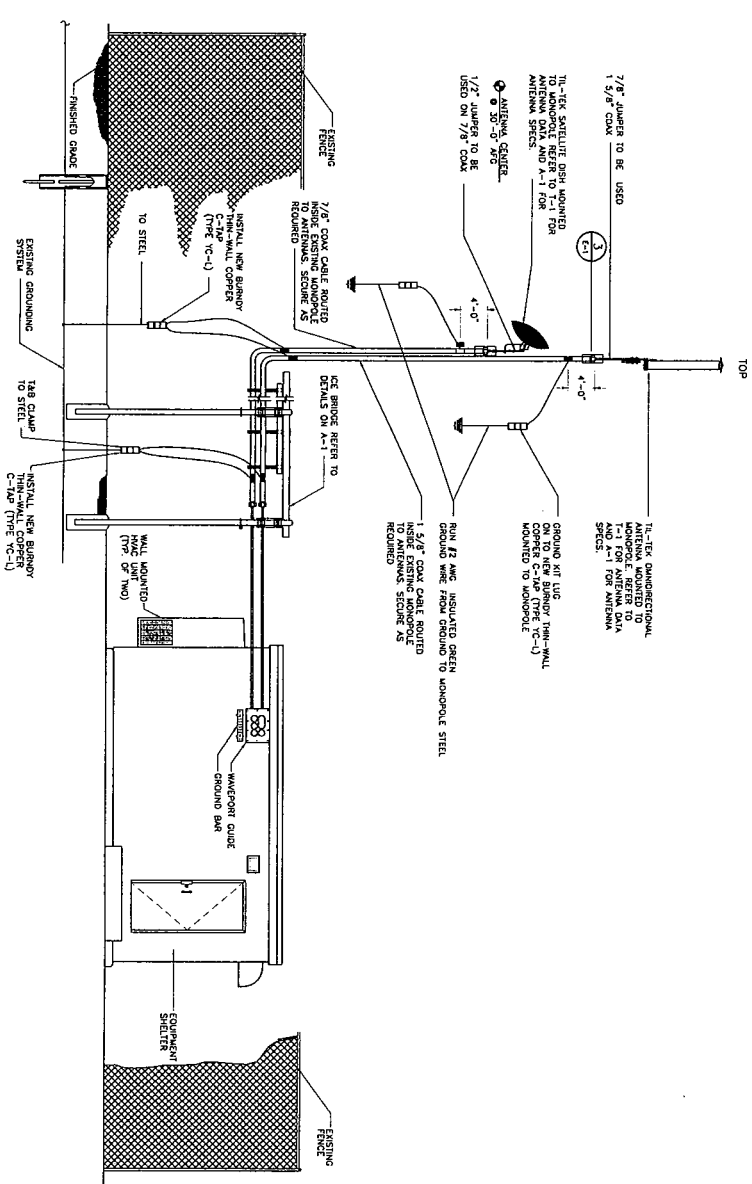
REAR 266 CENTER STREET  
 MANCHESTER, CONNECTICUT  
 06040

SCALE: AS NOTED

DATE: 11-07-00

TYPICAL  
 EQUIPMENT  
 RISER  
 DIAGRAM

A-3



1 TYPICAL EQUIPMENT RISER DIAGRAM  
 SCALE: N.T.S.

2 SEDIMENTATION CONTROL BARRIER-SILT FENCE  
 SCALE: N.T.S.

**URS**  
 URS CORPORATION  
 500 ENTERPRISE DRIVE  
 ROCKY HILL, CT 06067  
 (860) 261-1111

**PROFESSIONAL ENGINEER**  
 No. 1498  
 LICENSED IN THE STATE OF CONNECTICUT  
 PROJECT NO. 1301960.08

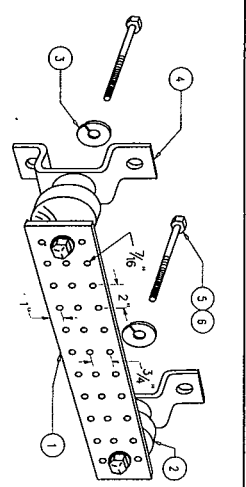
ISSUED FOR	10-12-01 REVISION
CHECKED BY:	11-11-01 FRANKLIN
DRAWN BY:	DFG

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**CROWN-MANCHESTER**  
 SITE ID: HARTFORD  
 REAR 268 CENTER STREET  
 MANCHESTER, CONNECTICUT  
 06040

SCALE: AS NOTED  
 DATE: 11-07-00

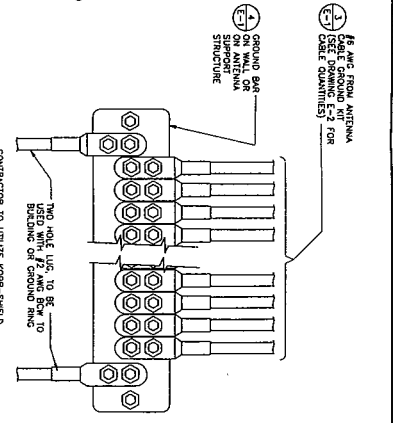
**EQUIPMENT**  
**GROUNDING PLAN**  
**DETAILS AND**  
**SYMBOL LIST**



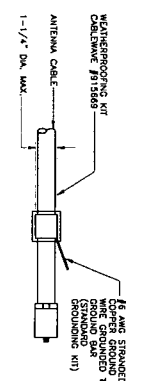
- LEGEND**
- 1 - COPPER GROUND BAR 1/4" x 4" x 30" NEWTON INSTRUMENT CO. CAT. NO. B-6142. HOLE CENTERS TO MATCH NEAR DOUBLE LUG CONNECTION.
  - 2 - INSULATORS, NEWTON INSTRUMENT CO. NO. 2041-4. USE 2015-8.
  - 3 - 1/2" DIA. LOCK WASHER, NEWTON INSTRUMENT CO. CAT. NO. 1012-8.
  - 4 - 1/2" DIA. LOCK NUT, NEWTON INSTRUMENT CO. CAT. NO. 1012-1.
  - 5 - 1/2" DIA. LOCK WASHER, NEWTON INSTRUMENT CO. CAT. NO. 1012-1.
  - 6 - 1/2" DIA. LOCK NUT, NEWTON INSTRUMENT CO. CAT. NO. 1012-1.

**4 GROUNDING - GROUND BAR DETAIL**  
 SCALE: 1" = 5'-0"

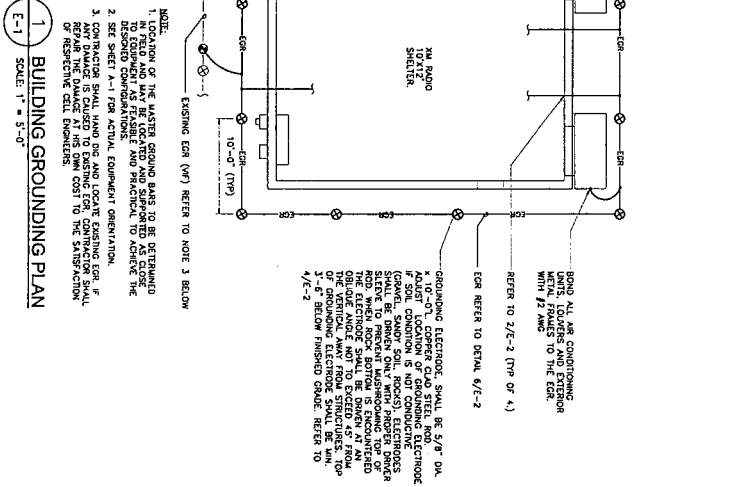
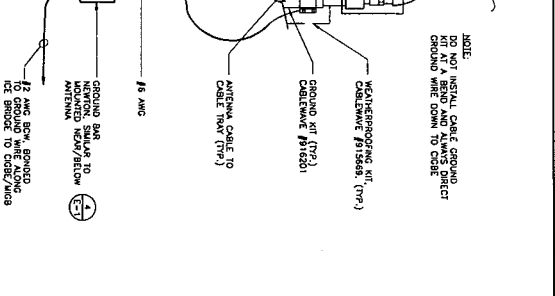
**5 GROUNDING - INSTALLATION OF GROUND WIRE TO GROUND BAR**  
 SCALE: NIS



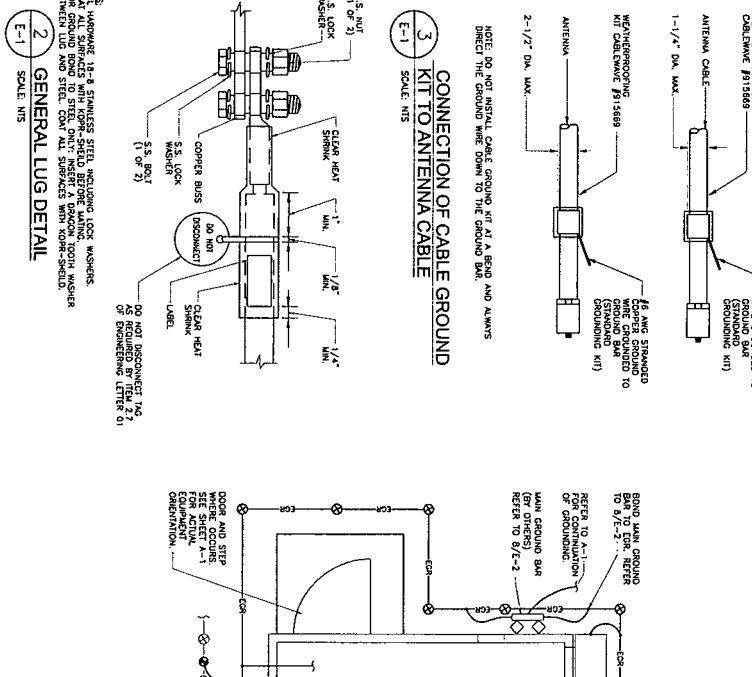
**6 TYPICAL COAX CABLE GROUNDING DETAIL**  
 SCALE: NIS



**7 GROUNDING - CONNECTION OF GROUND WIRES TO GROUNDING BAR**  
 SCALE: NIS



**1 BUILDING GROUNDING PLAN**  
 SCALE: 1" = 5'-0"



**3 CONNECTION OF CABLE GROUND KIT TO ANTENNA CABLE**  
 SCALE: NIS

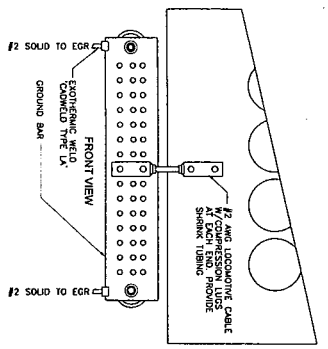
**SYMBOL LIST**

SYMBOL	DESCRIPTION
□	DISCONNECT SWITCH, NON-FUSED, ROOMS DISCONNECT SWITCH, NON-FUSED, ROOMS DISCONNECT SWITCH (MATERIAL AND FOLDS NOTED ON PLANS)
—E—	ELECTRICAL CONDUIT AND CABLES
—G—	GROUND SYSTEM CONDUIT AND CABLE
—GR—	EXTERIOR GROUND RING
[R]	MANUAL TRANSFER SWITCH
[P]	PHILLIPS, 12" x 12" x 6", LING
[T]	TRANSFORMER
⊗	PERMANENT LETTER AND BASE, COORDINATE WITH PERMANENT LETTER
•	EXOTHERMIC WELD CONNECTION
⊙	GROUND BAR
⊕	GROUNDING ELECTRODE
—T—	EXOTHERMIC WELD, T OF THREE CONDUCTOR AND TWO CONDUCTOR, COVERED TYPE TX
AMC	AMERICAN WIRE GAUGE
BOW	BARE COPPER WIRE
C	CONDUIT
C/B	CIRCUIT BREAKER
ORC	QUANTITY OF ROD CONDUIT
KWH	KILO-WATT-HOUR
NR	NON-FUSED
SA	SURGE ARRESTOR
TBR	TO BE REPEATED
UNO	UNLESS NOTED OTHERWISE
WP	WEATHERPROOF
⊕	CONNECTION POINT TO EXISTING SYSTEM

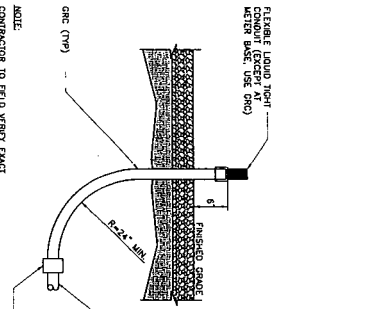
**2 GENERAL LUG DETAIL**  
 SCALE: NIS



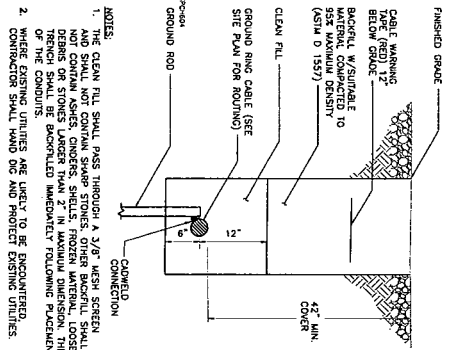
**NOTE:**  
 1. ALL SURFACES WITH UPPER-SHIELD BEFORE LAMINATING.  
 2. PER GROUNDING ROD TO STEEL DIRT INSERT A WORKING TIGHT WASHER.  
 3. CONTRACTOR SHALL HANG 6G AND LOCATE EXISTING EGR. IF ANY EXISTING EGR IS FOUND, CONTRACTOR SHALL REMOVE AND REINSTALL TO THE SPECIFICATION.



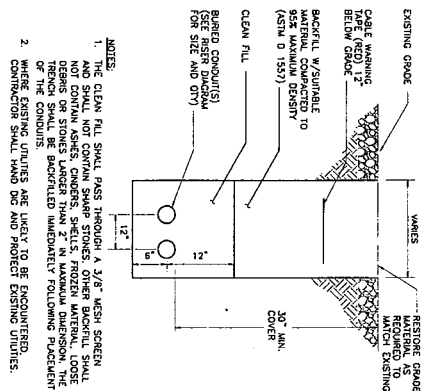
8 EXTERNAL GROUND BAR  
SCALE: N.T.S.



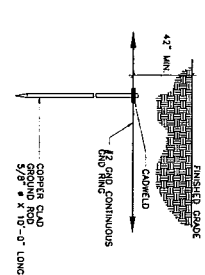
7 UTILITY STUB UP DETAIL  
SCALE: N.T.S.



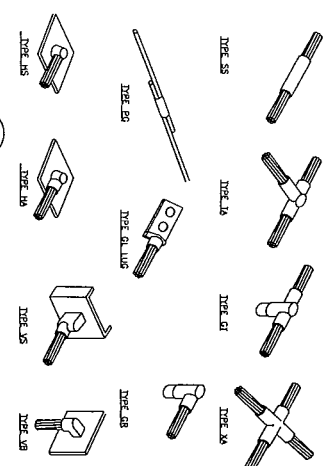
6 EGR DETAIL  
SCALE: N.T.S.



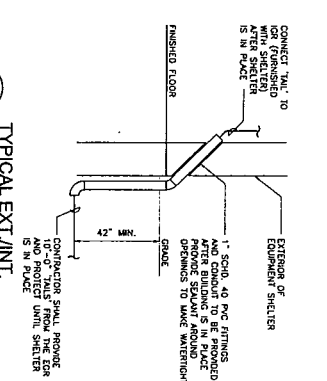
5 ELECTRICAL/TELCO TRENCH DETAIL  
SCALE: N.T.S.



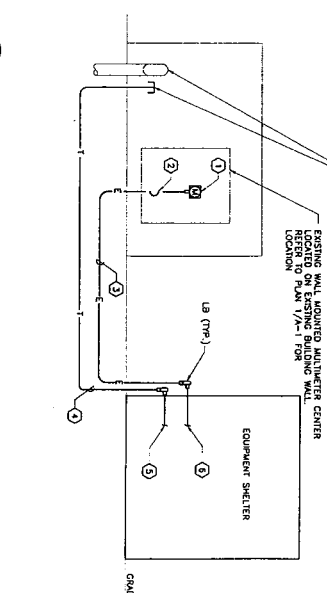
4 GROUND ROD DETAIL  
SCALE: N.T.S.



3 STANDARD CADWELD DETAILS  
SCALE: N.T.S.



2 TYPICAL EXT./INT. GROUNDING CONNECTION  
SCALE: N.T.S.



1 RISER DIAGRAM  
SCALE: N.T.S.

- RISER NOTES:**
1. RISING SPARE METE SERVICE WIRE SHALL BE INSTALLED BY UTILTY COMPANY. COORDINATE LOCATION OF METE WITH UTILITY COMPANY AND LOCAL ELECTRICAL ENGINEER.
  2. PROVIDE 100A/100A 2 POLE BRANCH CIRCUIT BREAKER, MATCH EXISTING THE BREAKER AND THE RATING.
  3. PROVIDE #12 & #18 G IN 1-1/4\"/>

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**ULCC**  
1792 MAIN STREET  
SHELTON CT 06488  
1-860-291-0927

**URS**  
URS CORPORATION  
500 ENTERPRISE DRIVE  
ROCKHILL, CT 06067  
1-860-231-7777

STATE OF CONNECTICUT  
REGISTERED PROFESSIONAL ENGINEER  
NO. 11418  
PROJECT NO. 11-03-09-08

ISSUED FOR  
10-13-09 REVIEW  
11-13-09 PERMITTING

**CROWN-MANCHESTER**  
SITE ID: HAR011A  
REAR 268 CENTER STREET  
MANCHESTER, CONNECTICUT  
06040

SCALE: AS NOTED  
DATE: 11-07-00  
**ELECTRICAL RISER DIAGRAM AND DETAILS**

**E-2**







**Power Density Calculation for XM Radio's proposed installation at 266 Center Street, Manchester, CT 06040**

XM Radio Internal Site ID: HAR-011A

Power Density Calculation - Worst Case	
Base Station TX Output	1000 watts
Number of Tx Channels	2
Antenna Model	TA-2350-DAB-H Omni
Antenna Gain	10 dBi
Cable Type/Size	LDF7-50A 1-5/8"
Cable Length	160 ft
Jumper and Connector Loss	0.69 dB
Cable Loss (per foot)	0.0137 dB/ft
Total Cable Loss	2.19 dB
Total Attenuation	2.88 dB
EIRP Per Channel	67.12 dBm
Total EIRP	70.12 dBm
Ground Reflection	1.60
Frequency	2337.49 MHZ 2340.02 MHZ
Antenna Height	125 ft
msg	10.00
Power Density (S)	0.144607 mw/cm <sup>2</sup>
% MPE From XM Radio	14.4607%
% MPE From Other Sources	0.00%
Total % MPE From All Sources	14.4607%

Equation Used:

$$\text{Power Density (S)} = (2.56 * 1000 * \text{EIRP}) / 4 * (p)^2 * (R)^2$$

Office of Engineering and Technology (OET) Bulletin 65, Edition 97-01, August 1997

**H. E. Bergeron Engineers**

• Civil • Structural • Land Surveying

P.O. Box 440  
2605 White Mountain Highway  
North Conway, NH 03860  
(603) 356-6936  
(603) 356-7715 (fax)

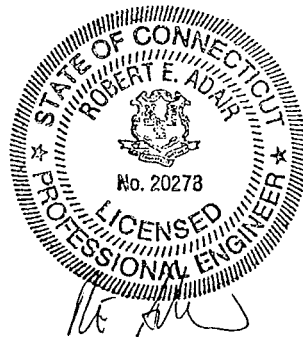
65 W. Commercial Street  
Portland, ME 04101  
(207) 780-1100  
(207) 780-1101 (fax)  
www.hebcivil.com

HEB

STRUCTURAL ANALYSIS REPORT  
OF  
115' VALMONT MONOPOLE  
MANCHESTER, CONNECTICUT

Prepared for Crown Castle Atlantic, LLC

July 25, 2000



Prepared by:

H. E. Bergeron Engineers, P.A.  
P.O. Box 440, 2605 White Mountain Highway  
North Conway, NH 03860  
HEB Project No. 2000-084-002



P.O. Box 440  
2605 White Mountain Highway  
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(207) 780-1101 (fax)  
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**STRUCTURAL ANALYSIS REPORT**  
of  
**115' VALMONT MONOPOLE**  
**MANCHESTER, CONNECTICUT**  
prepared for  
**CROWN CASTLE ATLANTIC, LLC**

**EXECUTIVE SUMMARY:**

H.E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of this 115-foot Valmont monopole tower. The analysis was performed with the addition of a TA-2335-LCC panel antenna mounted at a centerline elevation of 124-feet on a pipe extension, and a TA-2324-LHCP parabolic antenna mounted at 80-feet.

Our analysis indicates the tower and its foundation are capable of supporting the proposed antennas. The pipe extension supporting the proposed panel antenna should consist of 3" X-Strong steel pipe, ASTM A-500 grade B. Should the extended height exceed 9', the pipe size should be increased to accommodate the additional length.

**INTRODUCTION:**

A structural analysis of this communications tower was performed by H.E. Bergeron Engineers, P.A. (HEB) for Crown Castle Atlantic, LLC. HEB did not visit the tower site. This analysis was based on information provided by Crown Castle, which included a Valmont design drawing, and TIL-TEK antenna catalog sheets.

The structure is a 115-foot, galvanized steel monopole manufactured by Valmont. This analysis was conducted with the following antenna loads:

- (12) ALP9212 panel antennas on 15' platform at 112'; 1-5/8" waveguide
- A vacant platform at 99'
- (1) TA-2335-LCC panel antenna at 124' on a 9' pipe extension; 1-5/8" waveguide
- (1) TA2324-LHCP solid parabolic antenna at 80'; 7/8" waveguide

For the purpose of the analysis, all cables were assumed to be installed on the inside of the pole.

## STRUCTURAL ANALYSIS:

### Methodology:

The structural analysis was done in accordance with TIA/EIA-222-F (EIA), Structural Standards for Steel Antenna Towers and Antenna Supporting Structures; and the American Institute of Steel Construction (AISC), Manual of Steel Construction, Allowable Stress Design, Ninth Edition.

The analysis was conducted using a wind speed of 85 miles per hour and one-half inch of radial ice over the entire structure and all appurtenances. The TIA/EIA Standard requires a minimum of 80-mph wind load for Hartford County, Connecticut.

Two analytical methods were used to evaluate the structure: a two-dimensional linear model using spreadsheet programs developed by HEB, and a P-delta analysis using CSTRAAD finite element software distributed by ECOM Associates. The HEB 2-D model was used to generate dead loads of the tower and all of its appurtenances, radial ice loads and the resultant wind loading. The maximum bending moments and axial loads were used to calculate combined axial and bending stresses at intervals on the monopole, which were compared to allowable stresses according to AISC and TIA/EIA.

Loads generated in the 2-D model were input into the CSTRAAD program to evaluate secondary bending moments induced during deflection of the structure under load and to independently evaluate stresses. Evaluation of secondary bending moments is required by EIA paragraph 3.1.15. Our analysis indicates that the secondary moments exceed those of the linear analysis, and therefore govern in determining the capacity of the structure.

Two loading conditions were evaluated in accordance with EIA to determine the tower's capacity. The higher stresses resulting from the two cases is used to calculate the tower capacity:

- Case 1 = Wind Load (without ice) + Tower Dead Load (controls)
- Case 2 = 0.75 Wind Load (with ice) + Ice Load + Tower Dead Load



EIA permits a one-third increase in allowable stresses for towers less than 700-feet tall. Allowable stresses of tower members were increased by one-third in computing the load capacity values indicated herein.

#### ANALYSIS RESULTS:

Our analysis determined the tower will support the proposed antennae in addition to its current loading. Supporting calculations are provided in Appendix A.

The following table summarizes the capacity of the tower based on combined axial and bending stresses:

Elevation	Capacity
0'-10'	43%
10'-20'	40%
20'-29'	37%
29'-40'	44%
40'-51'	39%
51'-62'	34%
62'-72'	29%
72'-83'	40%
83'-94'	29%
94'-104'	19%
104'-115'	8%

The capability of the existing foundation to support the proposed loading was evaluated by comparing calculated values of shear, compression and overturning moment to design reactions provided on the Valmont record drawings. We found that the reactions were less than the design values. Based on these figures, the tower's foundation is adequate to support the proposed loading, provided the foundations were designed and built to the requirements of the original design drawing.

HEB

## CONCLUSIONS AND SUGGESTIONS:

As detailed above, our analysis indicates that the existing 115' Valmont monopole tower and foundation are capable of supporting the additional antenna loading proposed.

The pipe extension supporting the proposed omnidirectional antenna should consist of 3" X-Strong ASTM A-500 grade B steel pipe. Should the extended height exceed 9', the pipe size should be increased to accommodate the additional length.

## LIMITATIONS:

This report is based on the following:

1. Tower is properly installed and maintained.
2. All members are in new condition.
3. All required members are in place.
4. All bolts are in place and are properly tightened.
5. Tower is in plumb condition.
6. All members are galvanized.
7. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
8. Record drawings accurately reflect tower dimensions and height.

H.E. Bergeron Engineers, P.A. (HEB) is not responsible for any modifications completed prior to or hereafter which HEB is not or was not directly involved. Modifications include but are not limited to:

1. Adding or relocating antennas.
2. Installing antenna mounting gates or side arms.
3. Extending tower.

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# *Appendix A*

*Calculations*

**H. E. BERGERON ENGINEERS, P.A.**  
 2605 White Mountain Highway, PO Box 440  
 North Conway, NH 03860  
 (603) 356-6936

Client: **Crown Castle Atlantic**  
 Job: **Manchester, CT**

Job No.: 2000-084

Calculated By: **J. Klementovich**  
 Checked By: *[Signature]*

Date: 17-Jul-00  
 Date: *7/24*

**General Information**

Tower Manufacturer Valmont  
 Tower Type Monopole  
 Total Height of Tower 115 ft.  
 Wind Speed 85 mph.  
 Radial Ice 0.5 in.  
 75% Reduction for ice yes (yes or no)  
 1/3 increase for allowable loads yes (yes or no)  
 Number of faces 12 faces  
 Calculations based on EIA/TIA-222-F, using the following formulas:  
 Force on discrete appurtenance:  $F=Qz \cdot Gh \cdot Ca \cdot A$   
 Force on microwave antennae:  $F=Cr \cdot A \cdot Gh \cdot Kz \cdot V^2$ , where  $Cr=((Ca^2)+(Cs^2))^{1/2}$   
 Gh=1.69 for monopoles Gh= 1.69  
 V as specified EIA-222-F  
 E (Modulus of Elasticity) 29000 ksi  
 Fb 0.6  
 K 1  
 Min. Width = 21.91 in  
 Max. Width = 48.85 in  
 Slope of Tower = 0.0195 in/in

**Tower Information**

Section	Length (ft.)	Midpt Elev.	Base Width (in.)	Top Width (in.)	Area (sf) w/o Ice	Area (sf) w/ Ice	Wall Thknss	Wt. (lbs) Tower	Wt. (lbs) Ice
20		0.00	0.00	0.00	0.00	0.00		0.00	0.00
19		0.00	0.00	0.00	0.00	0.00		0.00	0.00
18		0.00	0.00	0.00	0.00	0.00		0.00	0.00
17		0.00	0.00	0.00	0.00	0.00		0.00	0.00
16		0.00	0.00	0.00	0.00	0.00		0.00	0.00
15		0.00	0.00	0.00	0.00	0.00		0.00	0.00
14		0.00	0.00	0.00	0.00	0.00		0.00	0.00
13		0.00	0.00	0.00	0.00	0.00		0.00	0.00
12		0.00	0.00	0.00	0.00	0.00		0.00	0.00
11	10.70	109.65	24.42	21.91	20.65	21.55	0.219	747.19	154.67
10	10.70	98.95	26.92	24.42	22.89	23.78	0.219	828.82	171.05
9	10.70	88.25	29.43	26.92	25.12	26.02	0.219	910.45	187.44
8	10.70	77.55	31.94	29.43	27.36	28.25	0.219	877.60	203.82
7	10.70	66.85	34.44	31.94	29.59	30.49	0.313	1351.48	220.20
6	10.70	56.15	36.95	34.44	31.83	32.72	0.313	1454.52	236.59
5	10.70	45.45	39.46	36.95	34.06	34.96	0.313	1557.56	252.97
4	10.70	34.75	41.96	39.46	36.30	37.19	0.313	1660.60	269.36
3	9.80	24.50	44.26	41.96	35.21	36.02	0.375	1930.77	261.07
2	9.80	14.70	46.55	44.26	37.08	37.90	0.375	2034.49	274.82
1	9.80	4.90	48.85	46.55	38.96	39.77	0.375	2138.21	288.56
	115.00						Total	15492	2521



H. E. BERGERON ENGINEERS, P.A.  
 2605 White Mountain Highway, PO Box 440  
 North Conway, NH 03860  
 (603) 356-6936

Client: Crown Castle Atlantic  
 Job: Manchester, CT

Job No.: 2000-084

Calculated By: J. Klementovich  
 Checked By: *[Signature]*

Date: 17-Jul-00  
 Date: 7/24

**Section Properties**

Section	I in <sup>4</sup>	I mid	Area mid	Area in <sup>2</sup>	L / side in	r in	S in <sup>3</sup>
Top	919.91			15.27			
20	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
19	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
18	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
17	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
16	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
15	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
14	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
13	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
12	0.00	0.0	0.0	0.00	0.00	#DIV/0!	#DIV/0!
11	1277.06	1098.5	16.2	17.04	6.54	8.66	104.61
10	1716.43	1496.7	17.9	18.80	7.21	9.55	127.51
9	2246.54	1981.5	19.7	20.57	7.89	10.45	152.67
8	2875.89	2561.2	21.5	22.33	8.56	11.35	180.10
7	5113.62	3994.8	28.3	34.29	9.23	12.21	296.93
6	6324.98	5719.3	35.6	36.81	9.90	13.11	342.36
5	7713.96	7019.5	38.1	39.33	10.57	14.00	391.01
4	9292.72	8503.3	40.6	41.85	11.24	14.90	442.90
3	13043.15	11167.9	47.4	52.91	11.86	15.70	589.41
2	15199.05	14121.1	54.3	55.68	12.47	16.52	652.96
1	17580.32	16389.7	57.1	58.45	13.09	17.34	719.77

**Tower Dead Load Summary**

Elev.	Dead load Tower (lbs)	Dead load Ice (lbs)
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
115.0	0	0
104.3	747	155
93.6	1576	326
82.9	2486	513
72.2	3364	717
61.5	4716	937
50.8	6170	1174
40.1	7728	1427
29.4	9388	1696
19.6	11319	1957
9.8	13353	2232
0.0	15492	2521

H. E. BERGERON ENGINEERS, P.A.  
 2605 White Mountain Highway, PO Box 440  
 North Conway, NH 03860  
 (603) 356-6936

Client: Crown Castle Atlantic  
 Job: Manchester, CT Job No.: 2000-084  
 Calculated By: J. Klementovich Date: 17-Jul-00  
 Checked By: *[Signature]* Date: *7/20*

**Antennae Summary**

Input:  
 Wind Velocity= 85 mph  
 Tower Hgt= 115 ft.

ANTENNAS

Type	Elev. (z)	Coeff. (C)	Kz	Qz	Area (no ice)	Area (ice)	Force (no ice)	Force (ice)	Weight
			1.00	18.50			0	0	
			1.00	18.50			0	0	
(12) ALP9212 & platform	112	1.4	1.42	26.22	56.2	63.2	3484	3920	1624
			1.00	18.50			0	0	
TIL-TEK TA-2335-LCC-H	124	1.2	1.46	27.00	8.0	8.4	436	559	96
			1.00	18.50			0	0	
Empty LP platform	99	1.2	1.37	25.32	9.4	11.6	480	678	1100
			1.00	18.50			0	0	
			1.00	18.50			0	0	
			1.00	18.50			0	0	

DISHES

Type	Elev. (z)	Coeff. (C)	Kz	Qz	Area (no ice)	Area (ice)	Force (no ice)	Force (ice)	Weight	Orient
TIL-TEK TA-2324-LHCP	80	0.00426	1.29	23.82	3.5	3.8	233	252	125	50 0.0043
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		

2945

**CABLES & LINEAR APPURT.**

Section	Area w/o Ice	Area w/ Ice	Weight w/o Ice	Weight w/ Ice
20	0.00	0.00	0	0
19	0.00	0.00	0	0
18	0.00	0.00	0	0
17	0.00	0.00	0	0
16	0.00	0.00	0	0
15	0.00	0.00	0	0
14	0.00	0.00	0	0
13	0.00	0.00	0	0
12	0.00	0.00	0	0
11	0.33	1.23	161	171
10	0.33	1.23	161	171
9	0.33	1.23	161	171
8	0.33	1.23	161	171
7	0.33	1.23	161	171
6	0.33	1.23	161	171
5	0.33	1.23	161	171
4	0.33	1.23	161	171
3	0.31	1.12	147	157
2	0.31	1.12	147	157
1	0.31	1.12	147	157

# H. E. BERGERON ENGINEERS, P.A.

2605 White Mountain Highway, PO Box 440  
 North Conway, NH 03860  
 (603) 356-6936

Client: **Crown Castle Atlantic**  
 Job: **Manchester, CT**

Job No.: 2000-084

Calculated By: **J. Klementovich**

Date: 17-Jul-00

Checked By: *[Signature]*

Date: 7/24

$K_z = \text{Exposure coefficient} = (z/33)^{2.7}; 1.00 \leq K_z \leq 2.58$

$Q_z = \text{Velocity pressure} = .00256 * K_z * V^2$

Gh = Gust response factor = 1.69

Cf = Structure force coefficient from Table 1 of TIA/EIA

Aa and Ai = Areas of linear apputenances, w/o & with ice

Ae = Effective area = Avg. width\*section length

Force =  $Q_z * G_h * (C_f * A_e + C_a * A_a)$

## Wind Load Summary

Wind Velocity = 85 mph  
 Height of Tower = 115 feet

## Wind Load Without Ice

Section	Midpoint Height	Areas		Kz	Qz	Gh	Cf	Wind Load	Wind Load
		Ae	Aa						
20	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
19	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
18	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
17	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
16	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
15	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
14	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
13	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
12	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
11	109.65	20.7	0.33	1.41	26.07	1.69	1.03	955 lbs.	89 plf.
10	98.95	22.9	0.33	1.37	25.31	1.69	1.03	1026 lbs.	96 plf.
9	88.25	25.1	0.33	1.32	24.50	1.69	1.03	1088 lbs.	102 plf.
8	77.55	27.4	0.33	1.28	23.61	1.69	1.03	1140 lbs.	107 plf.
7	66.85	29.6	0.33	1.22	22.63	1.69	1.03	1181 lbs.	110 plf.
6	56.15	31.8	0.33	1.16	21.53	1.69	1.03	1207 lbs.	113 plf.
5	45.45	34.1	0.33	1.10	20.27	1.69	1.03	1216 lbs.	114 plf.
4	34.75	36.3	0.33	1.01	18.77	1.69	1.03	1199 lbs.	112 plf.
3	24.50	35.2	0.31	1.00	18.50	1.69	1.03	1145 lbs.	117 plf.
2	14.70	37.1	0.31	1.00	18.50	1.69	1.03	1205 lbs.	123 plf.
1	4.90	39.0	0.31	1.00	18.50	1.69	1.03	1266 lbs.	129 plf.

**H. E. BERGERON ENGINEERS, P.A.**

2605 White Mountain Highway, PO Box 440

North Conway, NH 03860

(603) 356-6936

Client: **Crown Castle Atlantic**

Job: **Manchester, CT**

Job No.: **000-084**

Calculated By: **J. Klementovich**

Date: **17-Jul-00**

Checked By: *WJ*

Date: *7/14*

**Wind Load With Ice**

Section	Midpoint	Areas		Kz	Qz	Gh	Cf	Wind Load	75% Wind Load
	Height	Ae	Ai						
20	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
19	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
18	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
17	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
16	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
15	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
14	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
13	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
12	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
11	109.65	21.5	1.23	1.41	26.07	1.69	1.03	1042 lbs.	73 plf.
10	98.95	23.8	1.23	1.37	25.31	1.69	1.03	1111 lbs.	78 plf.
9	88.25	26.0	1.23	1.32	24.50	1.69	1.03	1170 lbs.	82 plf.
8	77.55	28.3	1.23	1.28	23.61	1.69	1.03	1220 lbs.	85 plf.
7	66.85	30.5	1.23	1.22	22.63	1.69	1.03	1257 lbs.	88 plf.
6	56.15	32.7	1.23	1.16	21.53	1.69	1.03	1280 lbs.	90 plf.
5	45.45	35.0	1.23	1.10	20.27	1.69	1.03	1284 lbs.	90 plf.
4	34.75	37.2	1.23	1.01	18.77	1.69	1.03	1262 lbs.	88 plf.
3	24.50	36.0	1.12	1.00	18.50	1.69	1.03	1202 lbs.	92 plf.
2	14.70	37.9	1.12	1.00	18.50	1.69	1.03	1262 lbs.	97 plf.
1	4.90	39.8	1.12	1.00	18.50	1.69	1.03	1323 lbs.	101 plf.

*MA 7/24*

NODAL COORDINATES					BOUNDARY CONDITIONS (F=FIX, S=SUP, M=MASTER/SLAVE)						
NODE NO	REBAND NO	X	Y	Z	NODE TEMP	ALPHA	BETA	GAMMA	DIR	DDDDOO XYZXYZ	STIFFNESS
Units:		Ft	Ft	Ft	F	Deg	Deg	Deg			K /In /Deg
1	1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	FFFFFF	
2	2	0.00	9.80	0.00	0.00	0.00	0.00	0.00	0.00		
3	3	0.00	19.60	0.00	0.00	0.00	0.00	0.00	0.00		
4	4	0.00	29.40	0.00	0.00	0.00	0.00	0.00	0.00		
5	5	0.00	40.10	0.00	0.00	0.00	0.00	0.00	0.00		
6	6	0.00	50.80	0.00	0.00	0.00	0.00	0.00	0.00		
7	7	0.00	61.50	0.00	0.00	0.00	0.00	0.00	0.00		
8	8	0.00	72.20	0.00	0.00	0.00	0.00	0.00	0.00		
9	9	0.00	82.90	0.00	0.00	0.00	0.00	0.00	0.00		
10	10	0.00	93.60	0.00	0.00	0.00	0.00	0.00	0.00		
11	11	0.00	104.30	0.00	0.00	0.00	0.00	0.00	0.00		
12	12	0.00	115.00	0.00	0.00	0.00	0.00	0.00	0.00		

TOTAL NUMBER OF ACTIVE NODES = 12  
 TOTAL NUMBER OF EQUATIONS = 66

2 NODE PRISMATIC BEAM ELEMENT														
ELEM NO	NE NO	PE NO	ALPHA	BETA	GAMMA	LENGTH	MAT TYPE	PROP TYPE	RELEASE NE	RELEASE PE	REF TEMP	DIR	OFFSET PE	STIFFNESS NE PE
Units:			Deg	Deg	Deg	Ft			F		F		Ft	K /In /Deg K /In /Deg
1	1	2	90.00	-90.00	0.00	9.80	1	1						
2	2	3	90.00	-90.00	0.00	9.80	1	2						
3	3	4	90.00	-90.00	0.00	9.80	1	3						
4	4	5	90.00	-90.00	0.00	10.70	1	4						
5	5	6	90.00	-90.00	0.00	10.70	1	5						
6	6	7	90.00	-90.00	0.00	10.70	1	6						
7	7	8	90.00	-90.00	0.00	10.70	1	7						
8	8	9	90.00	-90.00	0.00	10.70	1	8						
9	9	10	90.00	-90.00	0.00	10.70	1	9						
10	10	11	90.00	-90.00	0.00	10.70	1	10						
11	11	12	90.00	-90.00	0.00	10.70	1	11						

TOTAL NUMBER OF ACTIVE PRISMATIC BEAM ELEMENTS = 11

MATERIAL PROPERTIES						
MATL NO	DESIGNATION	YOUNG'S MODULUS	POISSON'S RATIO	THERMAL COEFF	MASS DENSITY	WEIGHT DENSITY
Units:		K /In ^2		F	Slug/Ft^3	Lb/Ft ^3
1	Pole	2.9e+004	0.250	6.5e-006	15.2	490

2 NODE PRISMATIC BEAM ELEMENT PROPERTIES									
PROP DESIGNATION	A	IXX	IYY	J	IXY	SFY	SFX	CW	
Units:	In^2	In^4	In^4	In^4	In^4			In^6	
1	Section 1	57.1	1.64e+004	1.64e+004	3.28e+004	0	1.000	1.000	0
2		54.3	1.41e+004	1.41e+004	2.82e+004	0	1.000	1.000	0
3		47.4	1.12e+004	1.12e+004	2.23e+004	0	1.000	1.000	0
4		40.6	8.5e+003	8.5e+003	1.7e+004	0	1.000	1.000	0
5		38.1	7.02e+003	7.02e+003	1.4e+004	0	1.000	1.000	0
6		35.6	5.72e+003	5.72e+003	1.14e+004	0	1.000	1.000	0
7		28.3	4e+003	4e+003	7.99e+003	0	1.000	1.000	0
8		21.5	2.56e+003	2.56e+003	5.12e+003	0	1.000	1.000	0
9		19.7	1.98e+003	1.98e+003	3.96e+003	0	1.000	1.000	0
10		17.9	1.5e+003	1.5e+003	2.99e+003	0	1.000	1.000	0
11		16.2	1.1e+003	1.1e+003	2.2e+003	0	1.000	1.000	0

GRAVITY LOAD MULTIPLIERS			
REC NO	PX	PY	PZ
1	0.000	-1.300	0.000

DESCRIPTION : Dead load of pole  
 LOAD CASES : 1  
 ELEMENT LIST : 1-11

=====											
2 NODE PRISMATIC BEAM ELEMENT LOAD INFORMATION											
REC	LOAD	LOAD	DIST								
NO	TYPE	SYS	SPEC		DIST	PX	PY	PZ	MX	MY	MZ
=====											
Units:					Ft	K	K	K	Ft-K	Ft-K	Ft-K
DESCRIPTION : Wind on section 1											
LOAD CASES : 1											
ELEMENT LIST : 1											
1	UNIF	GLO	FRAC	B	0.000	0.129	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.129	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 2											
LOAD CASES : 1											
ELEMENT LIST : 2											
2	UNIF	GLO	FRAC	B	0.000	0.123	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.123	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 3											
LOAD CASES : 1											
ELEMENT LIST : 3											
3	UNIF	GLO	FRAC	B	0.000	0.117	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.117	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 4											
LOAD CASES : 1											
ELEMENT LIST : 4											
4	UNIF	GLO	FRAC	B	0.000	0.112	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.112	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 5											
LOAD CASES : 1											
ELEMENT LIST : 5											
5	UNIF	GLO	FRAC	B	0.000	0.114	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.114	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 6											
LOAD CASES : 1											
ELEMENT LIST : 6											
6	UNIF	GLO	FRAC	B	0.000	0.113	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.113	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 7											
LOAD CASES : 1											
ELEMENT LIST : 7											
7	UNIF	GLO	FRAC	B	0.000	0.110	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.110	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 8											
LOAD CASES : 1											
ELEMENT LIST : 8											
8	UNIF	GLO	FRAC	B	0.000	0.107	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.107	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 9											
LOAD CASES : 1											
ELEMENT LIST : 9											
9	UNIF	GLO	FRAC	B	0.000	0.102	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.102	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 10											
LOAD CASES : 1											
ELEMENT LIST : 10											
10	UNIF	GLO	FRAC	B	0.000	0.096	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.096	0.000	0.000	0.000	0.000	0.000
DESCRIPTION : 11											
LOAD CASES : 1											
ELEMENT LIST : 11											
11	UNIF	GLO	FRAC	B	0.000	0.089	0.000	0.000	0.000	0.000	0.000
				E	1.000	0.089	0.000	0.000	0.000	0.000	0.000

DESCRIPTION : (12) ALP9212 & platform @ 112'  
 LOAD CASES : 1  
 ELEMENT LIST : 11  
 DISTANCES : 7.7

101	CONC	GLO	DIST	3.484	-1.624	0.000	0.000	0.000	0.000
-----	------	-----	------	-------	--------	-------	-------	-------	-------

DESCRIPTION : TIL-TEK TA2335 @ 124' on pipe mount  
 LOAD CASES : 1  
 ELEMENT LIST : 11  
 DISTANCES : 10.7

102	CONC	GLO	DIST	0.436	-0.096	0.000	0.000	0.000	3.924
-----	------	-----	------	-------	--------	-------	-------	-------	-------

DESCRIPTION : TIL-TEK TA2324 dish @ 80'  
 LOAD CASES : 1  
 ELEMENT LIST : 8  
 DISTANCES : 7.8

103	CONC	GLO	DIST	0.233	-0.125	0.000	0.000	0.000	0.000
-----	------	-----	------	-------	--------	-------	-------	-------	-------

DESCRIPTION : Empty platform at 99'  
 LOAD CASES : 1  
 ELEMENT LIST : 10  
 DISTANCES : 5.4

104	CONC	GLO	DIST	0.480	-1.100	0.000	0.000	0.000	0.000
-----	------	-----	------	-------	--------	-------	-------	-------	-------

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=====
REC          N O D A L   L O A D S
NO          ALPHA  BETA  GAMMA  PX          PY          PZ          MX          MY          MZ
-----
Units:      Deg    Deg    Deg    K          K          K          Ft-K       Ft-K       Ft-K
=====
```

DESCRIPTION : Waveguide dead loads  
 LOAD CASES : 1  
 NODE LIST : 2-4

1	0.00	0.00	0.00	0.000	-0.147	0.000	0.000	0.000	0.000
---	------	------	------	-------	--------	-------	-------	-------	-------

DESCRIPTION : WG d.l.  
 LOAD CASES : 1  
 NODE LIST : 5-12

2	0.00	0.00	0.00	0.000	-0.161	0.000	0.000	0.000	0.000
---	------	------	------	-------	--------	-------	-------	-------	-------

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=====
COMB LIST OF FACTORS * CASES
=====
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DESCRIPTION : Wind + dead loads  
 1 1\*1

=====

L I N E A R   A N A L Y S I S   R E S U L T S

=====

N O D A L   D I S P L A C E M E N T S  
 (\* Indicates Displacements Occur in Nodal Local System)

NODE NO	LOAD COMB	DX	DY	DZ	OX	OY	OZ
Units:		In	In	In	Deg	Deg	Deg
2	1	0.2009	-0.0015	0.0000	0.0000	0.0000	-0.1883
3	1	0.7878	-0.0028	0.0000	0.0000	0.0000	-0.3758
4	1	1.7745	-0.0042	0.0000	0.0000	0.0000	-0.5768
5	1	3.3467	-0.0056	0.0000	0.0000	0.0000	-0.8149
6	1	5.4450	-0.0070	0.0000	0.0000	0.0000	-1.0455
7	1	8.0481	-0.0082	0.0000	0.0000	0.0000	-1.2646
8	1	11.1600	-0.0094	0.0000	0.0000	0.0000	-1.4965
9	1	14.8167	-0.0108	0.0000	0.0000	0.0000	-1.7457
10	1	18.9760	-0.0120	0.0000	0.0000	0.0000	-1.9438
11	1	23.4979	-0.0129	0.0000	0.0000	0.0000	-2.0683
12	1	28.1862	-0.0134	0.0000	0.0000	0.0000	-2.0953

2 N O D E   P R I S M A T I C   B E A M   E L E M E N T   --   F O R C E S   A N D   M O M E N T S  
 SIGN CONVENTION : BEAM DESIGNERS

ELEM NO	LOAD COMB	NODE NO	AXIAL	SHEAR X	SHEAR Y	MOMENT X	MOMENT Y	TORSION
Units:			K	K	K	K -Ft	K -Ft	K -Ft
1	1	1	-21.8720	0.0000	17.2693	-1189.4116	0.0000	0.0000
		2	-19.3966	0.0000	16.0051	-1026.3670	0.0000	0.0000
2	1	2	-19.2496	0.0000	16.0051	-1026.3670	0.0000	0.0000
		3	-16.8956	0.0000	14.7997	-875.4235	0.0000	0.0000
3	1	3	-16.7486	0.0000	14.7997	-875.4235	0.0000	0.0000
		4	-14.6938	0.0000	13.6531	-736.0048	0.0000	0.0000
4	1	4	-14.5468	0.0000	13.6531	-736.0048	0.0000	0.0000
		5	-12.6251	0.0000	12.4547	-596.3280	0.0000	0.0000
5	1	5	-12.4641	0.0000	12.4547	-596.3280	0.0000	0.0000
		6	-10.6607	0.0000	11.2349	-469.5887	0.0000	0.0000
6	1	6	-10.4997	0.0000	11.2349	-469.5887	0.0000	0.0000
		7	-8.8147	0.0000	10.0258	-355.8439	0.0000	0.0000
7	1	7	-8.6537	0.0000	10.0258	-355.8439	0.0000	0.0000
		8	-7.3141	0.0000	8.8488	-254.8648	0.0000	0.0000
8	1	8	-7.1531	0.0000	8.8488	-254.8648	0.0000	0.0000
		9	-6.0105	0.0000	7.4709	-166.9836	0.0000	0.0000
9	1	9	-5.8495	0.0000	7.4709	-166.9836	0.0000	0.0000
		10	-4.9170	0.0000	6.3795	-92.8839	0.0000	0.0000
10	1	10	-4.7560	0.0000	6.3795	-92.8839	0.0000	0.0000
		11	-2.8088	0.0000	4.8723	-32.6628	0.0000	0.0000
11	1	11	-2.6478	0.0000	4.8723	-32.6628	0.0000	0.0000
		12	-0.2570	0.0000	0.4360	3.9240	0.0000	0.0000

R E A C T I O N S  
 (\* Indicates Reactions Occur in Nodal Local System)

NODE NO	LOAD COMB	PX	PY	PZ	MX	MY	MZ
Units:		K	K	K	K -Ft	K -Ft	K -Ft
1	1	-17.2693	21.8720	0.0000	0.0000	0.0000	1189.4116



P-D E L T A A N A L Y S I S R E S U L T S

N O D A L D I S P L A C E M E N T S

(\* Indicates Displacements Occur in Nodal Local System)

NODE NO	LOAD COMB	DX	DY	DZ	OX	OY	OZ
Units:		In	In	In	Deg	Deg	Deg
2	1	0.2038	-0.0016	0.0000	0.0000	0.0000	-0.1911
3	1	0.7997	-0.0045	0.0000	0.0000	0.0000	-0.3817
4	1	1.8022	-0.0101	0.0000	0.0000	0.0000	-0.5863
5	1	3.4012	-0.0215	0.0000	0.0000	0.0000	-0.8291
6	1	5.5370	-0.0406	0.0000	0.0000	0.0000	-1.0646
7	1	8.1884	-0.0692	0.0000	0.0000	0.0000	-1.2886
8	1	11.3600	-0.1095	0.0000	0.0000	0.0000	-1.5258
9	1	15.0889	-0.1650	0.0000	0.0000	0.0000	-1.7809
10	1	19.3320	-0.2363	0.0000	0.0000	0.0000	-1.9836
11	1	23.9457	-0.3201	0.0000	0.0000	0.0000	-2.1108
12	1	28.7293	-0.4097	0.0000	0.0000	0.0000	-2.1385

F O R C E S A N D M O M E N T S

SIGN CONVENTION : BEAM DESIGNERS

ELEM NO	LOAD COMB	NODE NO	AXIAL	SHEAR X	SHEAR Y	MOMENT X	MOMENT Y	TORSION
Units:			K	K	K	K -Ft	K -Ft	K -Ft
1	1	1	-21.8420	0.0000	17.3072	-1205.9820	0.0000	0.0000
		2	-19.3689	0.0000	16.0387	-1042.5874	0.0000	0.0000
2	1	2	-19.1683	0.0000	16.1025	-1042.5878	0.0000	0.0000
		3	-16.8204	0.0000	14.8852	-890.7483	0.0000	0.0000
3	1	3	-16.6219	0.0000	14.9420	-890.7490	0.0000	0.0000
		4	-14.5769	0.0000	13.7779	-750.0214	0.0000	0.0000
4	1	4	-14.3757	0.0000	13.8330	-750.0213	0.0000	0.0000
		5	-12.4691	0.0000	12.6108	-608.5467	0.0000	0.0000
5	1	5	-12.2552	0.0000	12.6603	-608.5465	0.0000	0.0000
		6	-10.4724	0.0000	11.4107	-479.7670	0.0000	0.0000
6	1	6	-10.2654	0.0000	11.4494	-479.7681	0.0000	0.0000
		7	-8.6057	0.0000	10.2058	-363.9125	0.0000	0.0000
7	1	7	-8.4035	0.0000	10.2361	-363.9119	0.0000	0.0000
		8	-7.0935	0.0000	9.0264	-260.8574	0.0000	0.0000
8	1	8	-6.8932	0.0000	9.0527	-260.8555	0.0000	0.0000
		9	-5.7910	0.0000	7.6422	-170.9585	0.0000	0.0000
9	1	9	-5.5994	0.0000	7.6604	-170.9599	0.0000	0.0000
		10	-4.7035	0.0000	6.5388	-94.9945	0.0000	0.0000
10	1	10	-4.5239	0.0000	6.5461	-94.9957	0.0000	0.0000
		11	-2.6321	0.0000	4.9699	-33.3590	0.0000	0.0000
11	1	11	-2.4644	0.0000	4.9675	-33.3581	0.0000	0.0000
		12	-0.2569	0.0000	0.4419	3.9238	0.0000	0.0000

R E A C T I O N S

(\* Indicates Reactions Occur in Nodal Local System)

NODE NO	LOAD COMB	PX	PY	PZ	MX	MY	MZ
Units:		K	K	K	K -Ft	K -Ft	K -Ft
1	1	-17.2693	21.8720	0.0000	0.0000	0.0000	1205.9820

**H. E. BERGERON ENGINEERS, P.A.**  
 2605 White Mountain Highway, PO Box 440  
 North Conway, NH 03860  
 (603) 356-6936

Client: **Crown Castle Atlantic**  
 Job: **Manchester, CT**

Job No.: **2000-084**

Calculated By: **J. Klementovich**  
 Checked By: *[Signature]*

Date: **17-Jul-00**  
 Date: *7/24*

**Total Moment (Tower & Antennas)      Axial Loads (kips)      Shear**

Elevation	Total Moment (Tower & Antennas)			Axial Loads (kips)			Shear				
	Mom. w/o Ice	75% Mom w/ Ice	100% Mom w/ Ice	Secondary	D+A Force	D+A+I Force	Tower (lbs.)	Antenna (lbs)	Total (kips)	Secondary	
0	1196.8	997.7	1330.3	1206	18.5	21.0	21.8	13413	4634	18.05	17.3
10	1033.8	864.3	1152.4	1043	16.3	18.6	19.2	12090	4634	16.72	16.1
20	883.0	740.3	987.0	891	14.3	16.3	16.6	10828	4634	15.46	14.9
29	743.6	625.4	833.8	750	12.4	14.1	14.4	9626	4634	14.26	13.8
40	604.0	509.8	679.7	609	10.7	12.2	12.3	8364	4634	13.00	12.7
51	477.4	404.4	539.2	480	9.2	10.4	10.3	7080	4634	11.71	11.4
62	363.6	309.3	412.4	364	7.7	8.7	8.4	5800	4634	10.43	10.2
72	262.7	224.4	299.2	261	6.4	7.1	6.9	4543	4634	9.18	9.1
83	174.9	150.0	199.9	171	5.4	5.9	5.6	3323	4401	7.72	7.7
94	100.8	86.6	115.5	95	4.5	4.8	4.5	2153	4401	6.55	6.5
104	40.5	35.1	46.8	33	2.6	2.8	2.5	1042	3920	4.96	5.0
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	

**H. E. BERGERON ENGINEERS, P.A.**

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Job No.: **2000-084**

Calculated By: **J. Klementovich**  
 Checked By: *[Signature]*

Date: **17-Jul-00**  
 Date: *7/24*

***Axial Force***

Elev.	Stress Ratio			
	w/o ice	Area	Fy	w/o ice
0	21.8	58.45	65	0.37
10	19.2	55.68	65	0.34
20	16.6	52.91	65	0.31
29	14.4	41.85	65	0.34
40	12.3	39.33	65	0.31
51	10.3	36.81	65	0.28
62	8.4	34.29	65	0.24
72	6.9	22.33	65	0.31
83	5.6	20.57	65	0.27
94	4.5	18.80	65	0.24
104	2.5	17.04	65	0.15
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!

***Bending Force***

Elev.	fb= Moment/Section Modulus			Bending Stress		
	w/o ice	S	(FY)^.5 w/t	Allowable		Actual
				Fb	1.33 Fb	w/o ice
0	1206.0	719.77	281.4	36.02	47.91	20.11
10	1043.0	652.96	268.2	36.99	49.19	19.17
20	891.0	589.41	255.0	37.95	50.47	18.14
29	750.0	442.90	290.1	35.39	47.07	20.32
40	609.0	391.01	272.8	36.65	48.75	18.69
51	480.0	342.36	255.4	37.92	50.43	16.82
62	364.0	296.93	240.0	39.04	51.93	14.71
72	261.0	180.10	315.0	33.57	44.65	17.39
83	171.0	152.67	290.3	35.37	47.05	13.44
94	95.0	127.51	265.6	37.18	49.44	8.94
104	33.0	104.61	240.9	38.98	51.84	3.79
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

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Job No.: 2000-084

Calculated By: J. Klementovich  
Checked By: *[Signature]*

Date: 17-Jul-00  
Date: *7/24*

***Combined Axial and Bending***

Elev.	Comb. Loads	Capacity
0	0.427	43%
10	0.397	40%
20	0.366	37%
29	0.439	44%
40	0.390	39%
51	0.339	34%
62	0.288	29%
72	0.396	40%
83	0.291	29%
94	0.186	19%
104	0.076	8%
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!
115	#DIV/0!	#DIV/0!