

STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square New Britain, Connecticut 06051 Phone: (860) 827-2935 Fax: (860) 827-2950

December 19, 2000

Kenneth C. Baldwin Robinson & Cole 280 Trumbull Street Hartford, CT 06103-3597

RE:

EM-XM-077-001129 - XM Satellite Radio notice of intent to modify an existing telecommunications facility located at 266 Center Street, Manchester, Connecticut. (Docket No. 129)

Dear Attorney Baldwin:

At a public meeting held on December 14, 2000, the Connecticut Siting Council (Council) acknowledged your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modifications are to be implemented as specified here and in your notices dated November 28, 2000, and December 11, 2000. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,

Mortimer A. Gelston

Chairman

MAG/FOC/laf

c: Honorable Stephen T. Cassano, Mayor, Town of Manchester Richard J. Sartor, General Manager, Town of Manchester Christine Belvin, LCC International, Inc. Christopher Ciolfi, Crown Atlantic Company Sandy M. Carter, Verizon Wireless

ROBINSON & COLE LLP

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LAW OFFICES

280 Trumbull Street Hartford, CT 06103-3597 860-275-8200 Fax 860-275-8299

Kenneth C. Baldwin 860-275-8345 Internet: kbaldwin@rc.com

December 11, 2000

Fax and Regular Mail

Fred O. Cunliff Siting Analyst Connecticut Siting Council 10 Franklin Square New Britain, CT 06051



DEC 12 2000

CONNECTICUT SITING COUNCIL

Re: Corrections to Exempt Modification Filings

Dear Mr. Cunliff:

As a follow-up to our telephone conversation, I am writing to make the Council aware of certain corrections which need to be made to the Crown Atlantic Company LLC exempt modification notices for Manchester, East Hartford and Fairfield. Those corrections are as follows:

XM Radio/Manchester

Replace paragraph number 4 of Crown's November 28, 2000 filing with the following:

The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst case" RF power density calculation for the closest point at the site boundary for the existing Cellco antennas on the tower, as described in the Council's Decision and Order dated March 12, 1990, would be 0.0737 mW/cm² or 2.92% of the FCC standard for uncontrolled environments. XM's operation at the Manchester site would add 0.144607 mW/cm² or 14.4607% of the FCC standard. (See attached RF power density calculations.) The calculated worst case power density for the combined operation at the site would therefore be 17.3807% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

XM Radio/Fairfield

Replace paragraph number 4 of Crown's November 28, 2000 filing with the following:

ROBINSON & COLE IIP

Fred O. Cunliff December 11, 2000 Page 2

The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst case" RF power density calculation for the closest point at the site boundary for the existing providers on the tower, would be 14.66% of the FCC standard for uncontrolled environments. XM's operation at the Fairfield site would add 0.184215 mW/cm² or 18.4251% of the FCC standard. (See attached RF power density calculations.) The proposed Metricom installation would add 0.0002 mW/cm² (0.028% of the FCC standard). The calculated worst case power density for the combined operation at the site would therefore be 33.1131% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

XM Radio/East Hartford

The third paragraph on the first page of the November 29, 2000 filing incorrectly references an antenna height for the XM Radio of 126 feet above ground level. As stated in paragraph number 1 of the filing the antenna height will not exceed 123 feet.

Metricom/XM Radio/Fairfield

Lastly, I have enclosed complete copies of the June 5, 2000 and September 13, 2000 structural analyses for the Fairfield tower. First and forward, these analyses conclude that the tower is structurally capable of supporting the addition of both Metricom and XM Radio antennas. The best way to explain the reduction in tower stresses referred to on page three of the June 5 and September 13 analyses is by referring you back to the antennae load listing on page one of each report.

In the June 5 analysis, the antenna load listing included 3-RR90-17 antennas for AT&T; 12-ALP 9212 antennas for Verizon Wireless; 12-ALP 11011A antennas for SNET; 6-ALP199015 antennas for Voicestream; 12-ALP 9212 antennas for a potential "future carrier"; 3 whip antennas for PageNet; 1-TA-2350-LCC whip antenna for XM Radio; and 1 TA2324-LHCP dish antenna.

The September 13 analysis includes the same antenna loading requirements for the AT&T, Verizon Wireless, SNET, Voicestream, PageNet and XM Radio antennas, adds 16 Larson panel antennas on side-arms for Metricom and removes the 12-ALP 9212 panel antennas listed for the "future carrier", and its associated antenna platform. The removal of the "future carriers" antennas and antenna platform from the 128 foot level, together with the addition of the Metricom antennas at the 100 foot level explains the reduction in tower stresses documented in the September 13 analysis.

ROBINSON & COLE LLP

Fred O. Cunliff December 11, 2000 Page 3

If you have any additional questions or concerns regarding these filings please do not hesitate to contact me.

Sincerely,

Kenneth C. Baldwin

KCB/kmd Enclosure

cc: Hal Giglio

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LAW OFFICES

280 Trumbull Street Hartford, CT 06103-3597 860-275-8200 Fax 860-275-8299

Kenneth C. Baldwin 860-275-8345 Internet: kbaldwin@rc.com

November 29, 2000

Mr. Joel M. Rinebold
Executive Director
Connecticut Siting Christ
10 Franklin Square
New Britain, CT 06051

CONNECTICUT

New Britain, CT 06051 CONNECTICUT SITING COUNCIL

Exempt Modification Filings for XM Radio in Manchester and Fairfield,

Connecticut

Dear Mr. Rinebold:

Re:

Enclosed please find two letters from H. E. Bergeron Engineers relating to the structural analysis completed for the Crown towers in Fairfield and Manchester, Connecticut. This information is intended to supplement Crown's recent filings on behalf of XM Radio.

Please contact me if you have any questions.

Sincerely,

Kenneth C. Baldwin

KCB/kmd Enclosures

cc: John G. Metsopoulos, Fairfield First Selectman

Stephen T. Cassano, Manchester Mayor Christine Belvin, LCC International, Inc.

H...E. Bergeron Engineers

- Civil - Structural - Land Surveying

P.O. Box 440 2605 White Mountain Highway North Conway, NH 03860 (603) 356-6936 (603) 356-7715 (fax)

65 W. Commercial Street
Portland, ME 04101
(207) 780-1100
(207) 780-1101 (fax)
www.hebcivil.com



November 28, 2000

Crown Castle International 156 Old Chester Road Haddam, Connecticut 06438

Attn: Hal Giglio

Fairfield, Connecticut

XM Radio Antenna Change

Dear Hal,

Re:

H. E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of Crown Castle's 171-foot Valmont monopole tower located in Fairfield, Connecticut.

HEB performed this analysis with XM Radio using a TA-2350-LCC omnidirectional antenna mounted and a TA-2324-LHCP parabolic antenna mounted at 128-feet. You indicated that XM Radio is proposing to install the TA2324-LHCP parabolic antenna at 75-feet.

Because the parabolic antenna will be located at a lower elevation, stresses on the tower are reduced. Therefore the tower is capable of supporting the proposed antenna change.

Please feel free to contact me if you have any questions.

Sincerely,

H. E. Bergeron Engineers, P.A.

Robert E. Adair, P.E. Senior Project Engineer

P: jobs\2000-085\Fairfield, CT ltr 11-28-00.doc



P.O. Box 440 2605 White Mountain Highway North Conway, NH 03860 (603) 356-6936 (603) 356-7715 (fax)

65 W. Commercial Street
Portland, ME 04101
(207) 780-1100
(207) 780-1101 (fax)
www.hebcivil.com



November 28, 2000

Crown Castle International 156 Old Chester Road Haddam, Connecticut 06438

Attn: Hal Giglio

Manchester, Connecticut

XM Radio Antenna Change

Dear Hal.

Re:

H. E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of Crown Castle's 115-foot Valmont monopole tower located in Manchester, Connecticut.

HEB performed this analysis with XM Radio using a TA-2350-LCC omnidirectional antenna mounted at a centerline elevation of 124-feet on a pipe extension, and a TA-2324-LHCP parabolic antenna mounted at 80-feet. You indicated that XM Radio is proposing to install the TA2324-LHCP parabolic antenna at 30-feet.

Because the parabolic antenna will be located at a lower elevation, stresses on the tower are reduced. Therefore the tower is capable of supporting the proposed antenna change.

Please feel free to contact me if you have any questions.

Sincerely,

H. E. Bergeron Engineers, P.A.

Robert E. Adair, P.E. Senior Project Engineer

NO. 20278

P: jobs\2000-084\Manchester, CT ltr 11-28-00.doc

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LAW OFFICES

280 Trumbull Street Hartford, CT 06103-3597 860-275-8200 Fax 860-275-8299

Kenneth C. Baldwin 860-275-8345 Internet: kbaldwin@rc.com

130vember 28, 2000

EM-XM-077-001129

Via Federal Express

Mr. Joel M. Rinebold Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051 RECEIVED

NOV 2 9 2000

CONNECTICUT SITING COUNCIL

Re: Notice of Exempt Modification

Siting Council Docket No. 129

266 Center Street, Manchester, Connecticut

Dear Mr. Rinebold:

Crown Atlantic Company LLC ("Crown") holds the Siting Council certificate for the existing telecommunications tower and related facility in Manchester, Connecticut (Docket No. 129). Crown intends to allow XM Satellite Radio ("XM") to install antennas and related equipment at the existing facility in Manchester. Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Manchester Mayor, Stephen T. Cassano.

The existing facility consists of a self-supporting monopole tower and a single-story equipment building within a fenced compound, located off Center Street in Manchester. This facility was approved by the Connecticut Siting Council on March 12, 1990. The tower currently supports antennas of Cellco Partnership d/b/a Verizon Wireless ("Cellco").

XM proposes to install a single Til-Tek omnidirectional antenna on the top of the tower and a 25.25 inch diameter, received only, dish antenna at the 30-foot level on the tower. XM equipment will be located in a new 10-foot by 12-foot building located near the base of the tower within the existing site compound. (See attached plans.)

The planned modifications to the Manchester facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the overall height of the structure above that which was approved by the Council at this site. In its Docket No. 129 Decision and Order, the Council stated that "[t]he monopole tower including antennas and associated equipment shall not exceed a height of 128 feet above ground level, 324 feet AMSL". The XM

ROBINSON & COLE LLP

Joel M. Rinebold November 28, 2000 Page 2

omnidirectional antenna will be mounted on the tower, with its center line at approximately the 125-foot level and its top at the 128-foot level, within the Council's height restriction. The XM dish antenna would be mounted at the 30-foot level on the tower. The enclosed tower drawings confirm that the planned modifications will not extend above the 128-foot height limitation for the tower including antennas approved by the Council in Docket No. 129.

- 2. The installation of the XM equipment shelter, as shown on the attached project plans, will not require an extension of the site boundaries.
- 3. The proposed modifications to the facility will not increase the noise levels at the existing facility by six decibels or more.
- 4. The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the applicable standard. The "worst-case" RF power density calculation for the closest point at the site boundary for the existing Cellco antennas on the tower, as described in the Council's Decision and Order dated March 12, 1990, would be 0.0737 mW/cm² or 2.92% of the FCC standard for uncontrolled environments. XM's operations at the Manchester site would add 0.184520 mW/cm² or 18.452% of the FCC standard. (See attached RF Power Density Calculations.) The calculated "worst-case" power density for the combined operations at the site would therefore be 21.372% of the FCC standard for uncontrolled environments as calculated for a mixed frequency site.

Also attached is a copy of a structural analysis verifying that the tower can accommodate the XM antennas. Please note that the structural analysis contemplated the XM dish antenna being located at the 80-foot level on the tower rather than the 30-foot level as proposed. The structural analysis is therefore more conservative than necessary for the proposed antenna installation.

For the foregoing reasons, Crown respectfully submits that the proposed addition of antennas and equipment at the Manchester facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

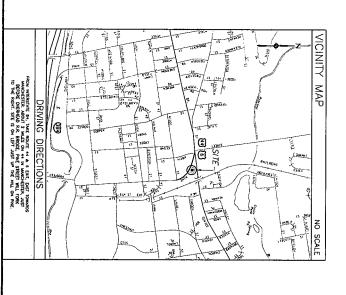
Kenneth C. Baldwin

KCB/kmd Attachments

cc: Stephen T. Cassano, Manchester Mayor Tara K. Rand, Crown Atlantic Company, LLC Christine Belvin, LCC International, Inc.



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CONTACT

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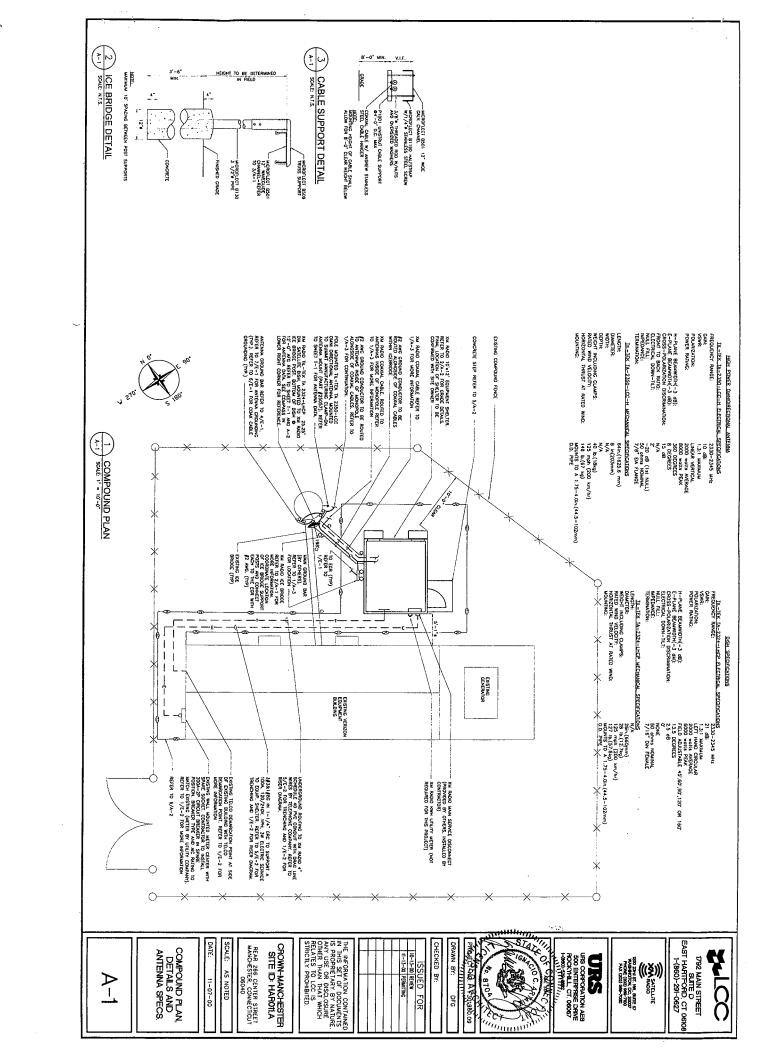
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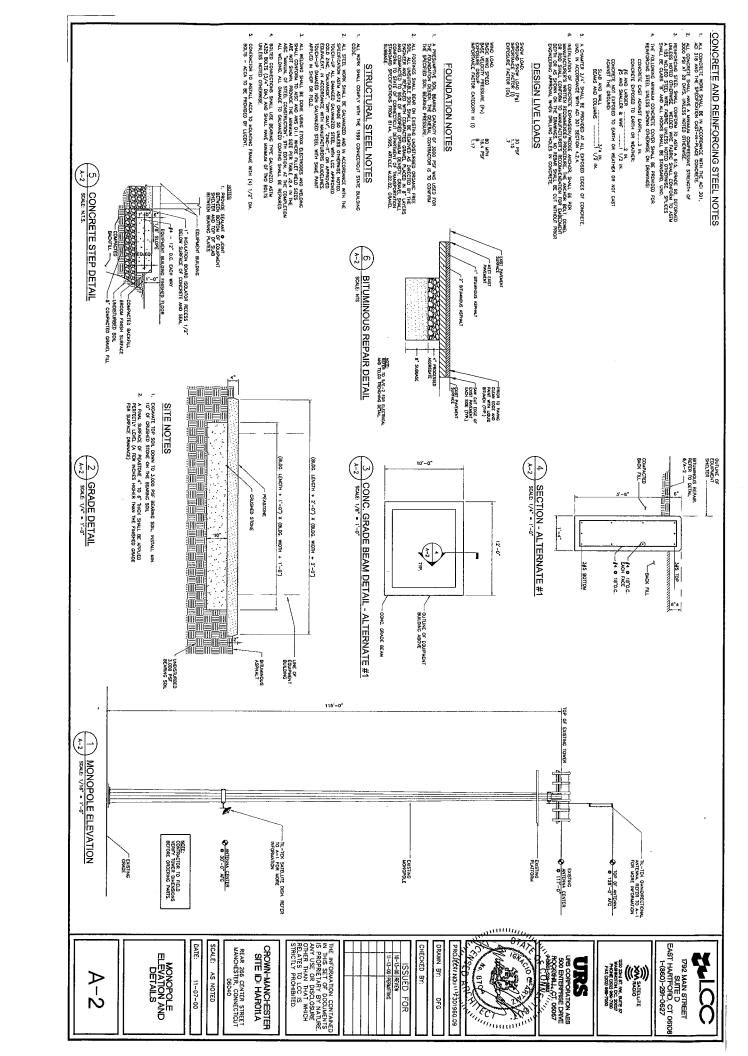
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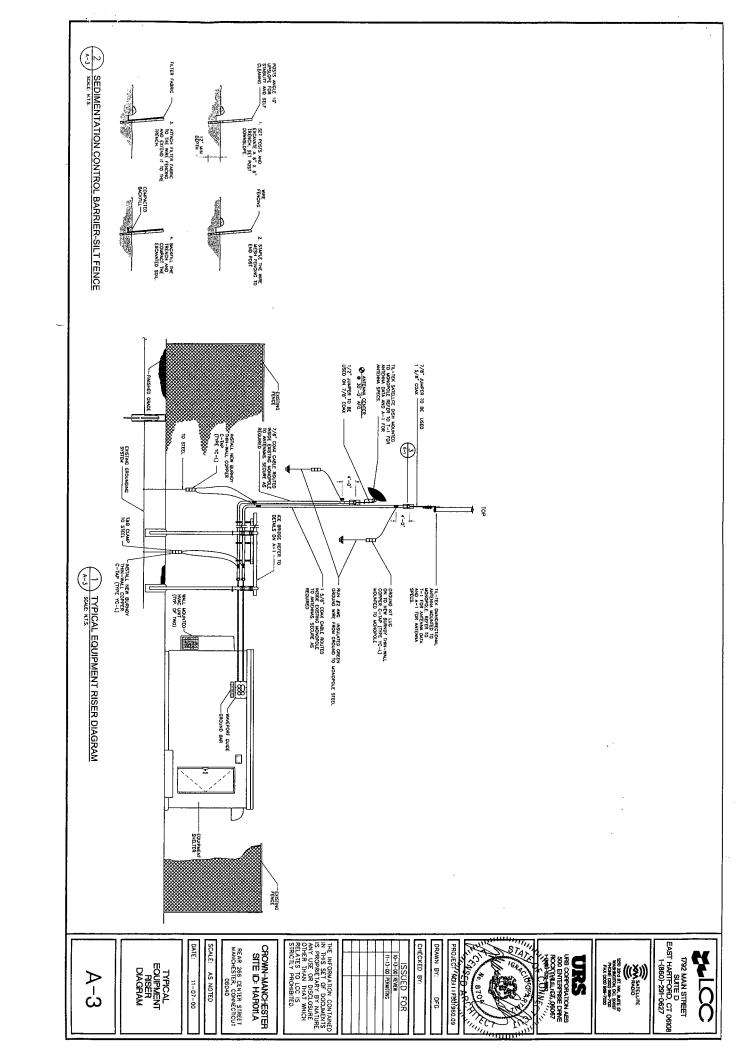
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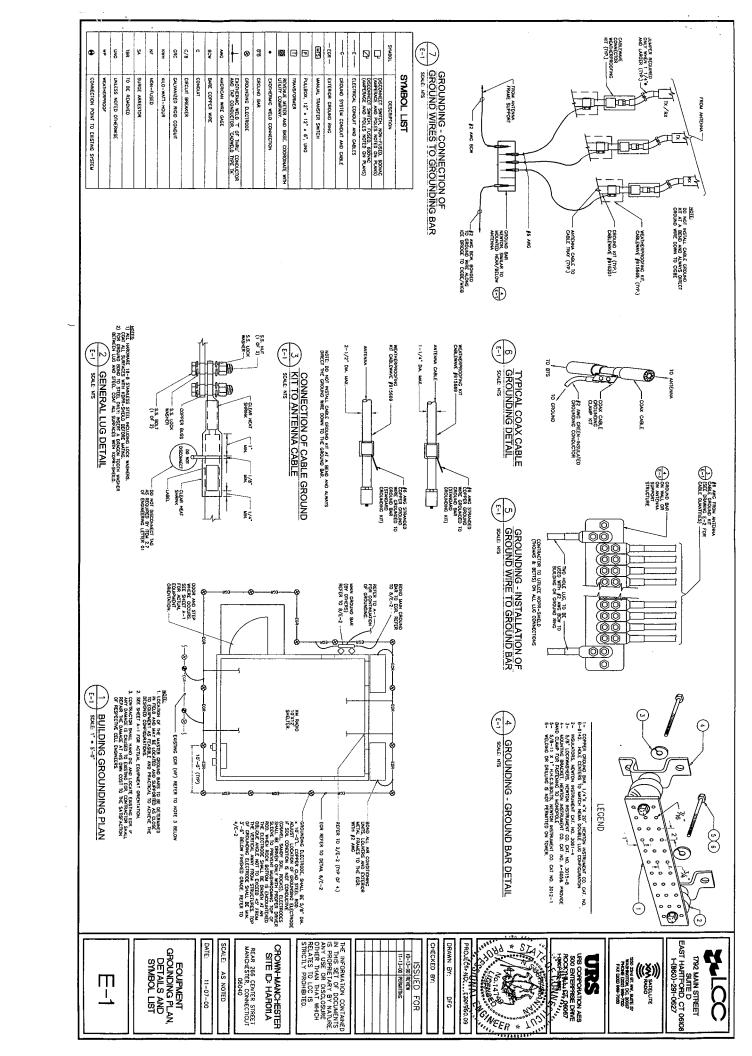
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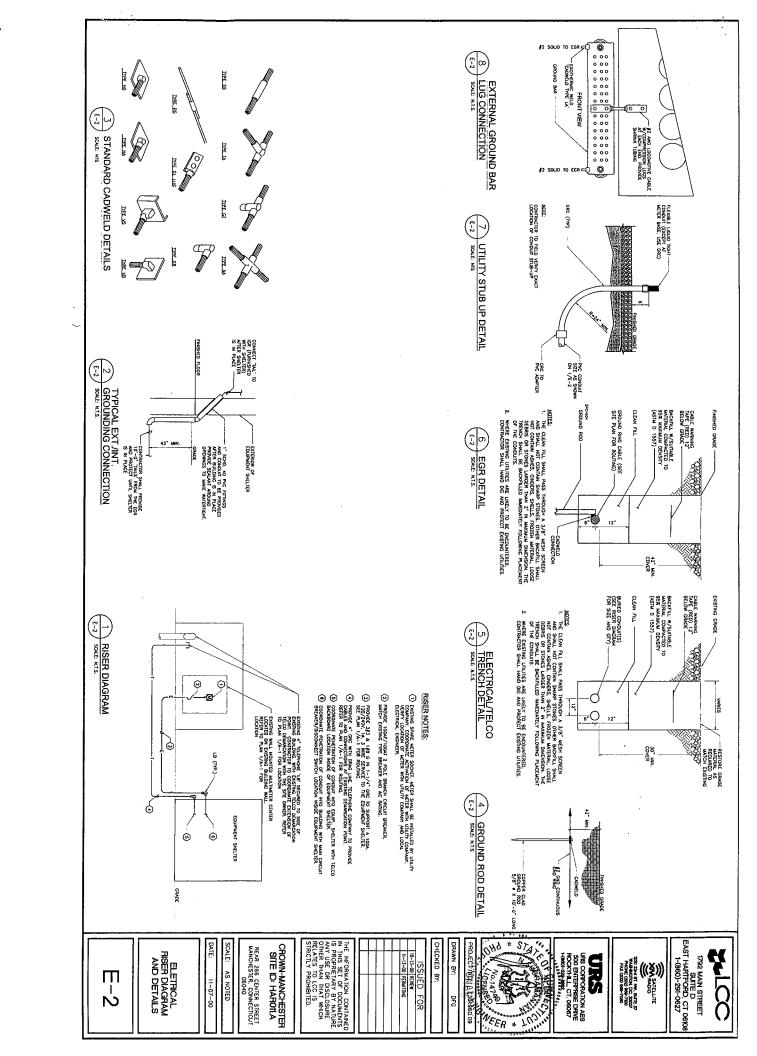
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- CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING HIS WORK WITH THE WORK OF OTHERS AS IT MAY RELATE TO RADIO EQUIPMENT, ANTENIAS AND ANY OTHER PORTIONS OF THE WORK.
- CONTRACTOR SHALL PROVIDE ACCESS TO THE SITE AND ASSIST THE RADIO EQUIPMENT VENDOR AND THE ANTENNA INSTALLATION CONTRACTOR AS THEY MAY REQUIRE.
- CONTRACTOR SHALL MAINTAIN LIMBILITY INSURANCE TO PROTECT THE OWNER, AGENT & LCCI PROVIDE 48 HOURS WRITTEN NOTICE TO THE ENGINEER, LCCI & OWNER PRIOR TO COMMENCEMENT OF WORK.
- PROVIDE A PORTABLE FIRE EXTINGUISHER WITH A RATING OF NOT LESS THAN 2-A OR 2-A/10-BC WITHIN 75 FEET TRAVEL DISTANCE TO ALL PORTIONS OF THE WORK AREA DURING CONSTRUCTION.
- INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURERS RECOMMENDATIONS UNLESS SPECIFICALLY DIHERWISE INDICATED OR WHERE LOCAL CODES OR RECOULATIONS TAKE PRECEDENCE.
- MAKE RECESSARY PROVISIONS TO PROTECT EXISTING SURFACES, EQUIPMENT, IMPROVEMENTS, PRINCE ETC. AND IMMEDIATELY REPAIR ANY DAMAGE THAT OCCURS DURING CONSTRUCTION. VERIFY FINAL EQUIPMENT LOCATIONS WITH THE PAGIO EQUIPMENT VENDOR.
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- MINIMUM BEND RADIUS OF ANTENNA CABLES SHALL BE IN ACCORDANCE WITH CABLE MANUFACTURERS RECOMMENDATIONS.

GENERAL CONCRETE NOTES

- DESIGN AND CONSTRUCTION SAUL CONFORM TO THE AMERICAN CONCRETE INSTITUTE "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE" ACI 318. ULTIMATE COMPRESSIVE STRENGTH OF CONCRETE AT 28 DAYS SHALL BE 3500 PSI.
- CONCRETE WORK AND MATERIALS SHALL CONFORM TO THE AMERICAN CONCRETE MISTITUTE "SPECIFICATIONS FOR STRUCTURAL CONCRETE FOR BUILDINGS", ACI 301.
- CEMENT SHALL BE PORTLAND CEMENT CONFORMING TO ASTM C150 TYPE 1
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- READY MIX CONCRETE SHALL COMPLY WITH AGI-304 AND ASTAL G-94 WITH A MAXIMUM WATER CEMENT PAID OF 0.50. THAE BETWEEN INTRODUCTION OF WATER AND THE PLACEMENT OF CONCRETE SHALL NOT EXCEED 1-1/2 HOURS.
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 EXERCISE CHRE NOT TO DAMAGE SURFACE.
- SUBBIT SHOP DETAL DRAWNOS OF ALL STRUCTURAL AND MISCELLANEOUS STEEL TO THE ENGINEER FOR APPROVAL, AND INCORPORATE ALL COMMENTS PRIOR TO FABRICATION.
- CANING SHALL BE CALVANIZED SERBATED MELDED STEEL BAR GRAING WITH 1-3/16" BEARING BARS AT 1-3/16" DC. FASTEN TO SUPPORTING MEMBERS WITH SADDLE-TYPE CLIPS AND BAND ALL EXPOSED EDGES. SILERY ANCHORS SMALL COMPORM TO FEDERAL SPECE/CAMON FF.-5-328, GROUP M. THE F. ST. MANSS. J. AS MANHACHINED BY MITH FASTINAN SOSTILMS OR APPROVED EQUAL INSTALLATION SMALL BE IN ACCORDANCE WITH THE MANHACHINERY'S RECONMENDATIONS. MAINIAUM EMBEDMENT SMALL BE THREE (3) INCHES.
- MASION BOLTS SHALL CONFORM TO REDERAL SPECIFICATION FF.-S.-325, UP 7. THE 4. CLASS 1, HILT KHIK BOLT II OR APPROVED EQUAL. TALLATION SHALL BE IM ACCORDANCE WITH THE MAURIFACTIBET'S COMMENDATIONS, MINIMUM EMBEDMENT SHALL BE FOUR (4) INCHES.
- DRILL THE HOLE USING MANUFACTURER RECOMMENDED DRILL BIT UP TO SPECIFIED DEPTH. HAMMERING IS NOT PERMITTED.
- CLEAN THE HOLE USING WILON BRUSH AND/OR COMPRESSED AIR. THE HOLE SHOULD BE CLEAR OF ANY LOOSE MATERIAL. IF WET, THE MASONRY SHOULD BE ALLOWED TO DRY FULLY BEFORE ANCHOR INSTALLATION.
- C. INSERT SPECIFIED SCREEN TUBE INTO THE HOLE.
- INSERT ANCHOR ROD OR INTERNALLY THREADED INSERT INTO THE ADHESINE-FILLED SCREEN TUBE, TWISTING SLIGHTLY.

FILL THE SCREEN TUBE COMPLETELY WITH ADHESIVE, BEGINNING AT THE BOTTOM END.

- LOAD FASTENER ONLY AFTER MANUFACTURER SPECIFIED CURE TIME HAS ELAPSED.
- NCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITING OR NONCOMPORAME MATERILS OR CONDITIONS SIMIL BE REPORTED TO THE ENGINEER PERIOR TO RELEDIAL OR CORRECTIVE ACTION, MAY SUCH ACTION SHALL REQUIRE ENGINEER APPROVAL.

ANTENNA MOUNTING NOTES

- DESIGN AND CONSTRUCTION OF ARTEMA SUPPORES SALL COMODA TO ANS/PA/TIM- 2023 "STRUCTURA SUPACADROS FOR SEEL MITEMA (OMERS AND ANTEMA SUPPORTING STRUCTURES" OR APPLICABLE LOCAL CODES, DESIGN WIND SPEED. 85 MPH.

 (85 MPH IN CONJUNCTION WITH 0.5 INCHES RODAL ICE)
- ALL STEEL MATERIALS SHALL BE CALVANZED AFTER FABRICATION IN ACCORDANCE WITH ASTIM ATCLL TIME (NOT-DIP CALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS. LINLESS OTHERMISE MOTED.
- AL BOLTS, ANCHORS AND MISCELLACTOUS HARDWARE SHALL BE CALVANIZED IN ACCORDANGE WITH ASTIM ALSO, "TIME-COATING (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS OTHERWISE NOTED.
- DAWAGED GALVANIZED SURFACES SHALL BE REPAIRED BY COLD GALVANIZING IN ACCORDANCE WITH ASTM A780.

ALL ANTENNA MOUNTS SHALL BE INSTALLED WITH DOUBLE NUTS AND SHALL BE INSTALLED SHUG TIGHT.

- CONTRACTOR SHALL PROVIDE ALL LABOR, MATERIALS, INSURANCE, EQUIPALENT, INSTALLATION, CONSTRUCTION TOOLS, TRANSPORTATION, ETC., FOR A COMPLETE AND PROPERTY OFFERANCE SYSTEM, REFERCIZED THROUGHOUT MAD AS INDICATED ON DRAWNINGS, AS SPECIFIED HEREIN AND/OR AS OTHERWISE REQUIRED.
- ALL MATERIAL MO EQUIPMENT SMIL ER REW MO IN PERFECT CONDITION WISH.

 WISHLALDS MOS SMIL RE OF THE REST PACED MAD OF THE VEHICLE OF THE REST PACED MAD OF THE VEHICLE OF THE

- ALL CROUIT BREAKERS, FISSES AND EXECTRICAL EQUIPMENT SMALL HIME AN INTERNETING NATIONS THAN THE MANUALM SHORT DROUIT COMPRENT TO WHICH THEY MAY BE SUBJECTED, AS INDICATED BY UTILITY COMPANY AND A MINIMAM OF 22,000
- WIRE AND CABLE CONDUCTORS SHALL BE COPPER \$12 AND MINIMUM WITH TYPE THWN INSULATION UNLESS SPECIFICALLY HOTED OTHERWISE.

13. MASTER GROUND BAR IS TO BE 4" x 1'-8". ALL OTHER GROUND BARS ARE TO BE 4" x 1'-4". 12. ALL EXPOSED #2 WIRE MUST BE TINN NOT BCW.

- RIDD COMDUT SMALL BE U.L. LABEL CALMANZED ZIAC COATED WITH ZINC MICRORA AND SMALL BE USED WHEN INSTALLED IN OR UNDER CONCRETE SLABS, IN CONTICT WITH THE CAPIT, LINDER PUBLIC ROLDWAYS, IN ANSONRY WALLS OR EXPERIOR.
- FLEXIBLE WETALLIC CONDUIT SWALL HAVE UIT. LUBEL AND MAY BE USED WHERE REMAITED BY CODE. FITHINGS SWALL BE "LWE" OR "SQUEEZE" TYPE, SEAL TIGHT FLEXIBLE CONDUIT. ALL COMDUIT IN EXCESS OF SIX FEET IN LENGTH SWALL HAVE FULL SIZE GROUND WIRE. ELECTRICAL METALLIC TUBNO (EMT) SHALL HAVE UIL. LABEL, FITTINGS SHALL BE EGLAND RING COMPRESSION TYPE. EMT SHALL BE USED ONLY FOR INTERIOR RUNS NO SET SCREW OR CRIMP TYPE FITTINGS SHALL BE USED.
- CONDUIT SHALL BE SIZED PER NEC OR ANY GOVERNING LOCAL CODE, AND AS SHOWN. PVC CONDUIT AND FITTINGS SHALL HAVE U.L. LABEL AND SHALL BE PVC SCHEDULE 40.
- CONDUIT RUNS MAY BE SURFACE MOUNTED IN CEILINGS OR WALLS UNLESS MOLOCIED D'HERWISE. CONDUIT MOLOCIED SMALL RUIN PARALLE, OR AT RIGHT ANGLES TO CEILING, FLOOR OR BEMAS, NEBRY EXACT ROUTING OF ALL EXPOSED COMDUIT WITH DWINER PRIOR TO INSTINLING.
- 11. REFER TO MANUFACTURERS MANUAL FOR RECOMMENDED FUSE AND WIRE SIZES. G. ALL CONDUIT ONLY (C.O.) RUNS SHALL HAVE A PULL WIRE OR ROPE.
- ALL FINAL CONNECTIONS TO THE EQUIPMENT ARE TO BE OF FLEXIBLE WEATHERPROOF CONDUIT TO MEET APPLICABLE CODES.
- PROVIDE LCCI WITH ONE SET OF COMPLETE ELECTRICAL "AS INSTALLED" DRAWINGS AT THE COMPLETION OF THE JOB, SHOWING ACTUAL DIMENSIONS, ROUTINGS, AND CRICUITS
- CONTRACTOR SHALL BE RESPONSIBLE FOR CODRDINATING WITH, GAINING APPROVALS AND PAYING ALL FEES ASSESSED BY UTILITY COMPANY FOR ELECTRICAL SERVICE.
- 15. SEAL PENETRATIONS THROUGH FIRE RATED AREAS WITH UL LISTED AND CODE APPROVED MATERIALS.
- TELCO CONDUIT RUN HA/ON BURDINGS SHALL BE 2" DIA, AND HAVE MINIMUM IS ARANGE BENDS A LEBOMS, CONDUIT RUNS BUALL HARE ONE 18" 18" APILL BOX AT DEMARC LOCATION. TWO (2) PULL ROPES SHALL BE INSTALLED IN TELCO CONDUIT.
- 17. CONTRACTOR TO INSTALL BRASS TAGS ON THE COAX CABLE AT THE ANTENNA END & AT THE EQUIPMENT END. THE TAGS MUST INCLUDE SECTOR NO. AND CABLE LENGTH.

GENERAL ELECTRICAL NOTES

- ONIFICATION SWALL PERFORM ALL VERFICATION DESERVATION TESTS, AND EXAMINATION WORK PRIOR TO THE CHECKNOL TO THE ELECTRICAL COMPARTY AND THE ACTUAL CONSTRUCTION CONTRACTION SHALL RESULT A WINDIFF NOTICE OF ALL FRINGHOS TO THE ENUNCITION SHALL RESULT AND THE ENUNCIATION SHALL PROVIDE THE PROVIDE

- CONTRACTOR TO COORDINATE WITH BUILDING OWNER FOR CONNECTION OF TEMPORARY AND REMANSET POWER TO THE SITE. THE TEMPORARY POWER AND ALL HOOKUP COSTS TO BE FAILD BY CONTRACTOR.
- ALL ELECTRICAL EQUIPMENT SHALL BE LABELED WITH PERMANENT ENGRAVED PLASTIC LABELS.
- WETER SOCKET JAMPERES, YOLTAGE, AND MUMBER OF PHASES SHALL BE AS NOTED AND SHALL BE MANUFACTURED BY SOQUARE TO COMPANY, SANCHAMO, OR APPROVED EQUAL METER SOCKET SHALL BE APPROVED BY UTILITY COMPANY PRIOR TO INSTILLATION.
- BUCH COMPUTION OF POERY SYSTEM SHALL BE PERMANENTLY TAGGED IN EACH PAINCEDARD, PULLDOX, J-BOX, SMITCH BOX, ETC., IN COMPLANCE WITH THE OCCUPATIONAL SAFETY AND HEALTH ACT (O.S.H.A.)

GENERAL NOTES

- 1. THIS FACILITY IS UNMANED AND NOT FOR HUMAN OCCUPANCY.
- ALL WORK SHALL CONFORM TO THE LOCAL BUILDING CODE.

 RECHANG CHEPATIONS SHALL BE DONE IN ACCREAWING WITH LOCAL

 AND FEDERAL SWETE REGULATIONS (SOUTH) ETERNAL

 AND FEDERAL SWETE REGULATIONS (SOUTH) ETERNAL

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 CHARACTER DOES NOT FOLLOW SUCH SWETE REGULATIONS:

TENANT PROTECTION NOTES

- PRECAL PRECALTION SHALL BE TAKEN BY THE CONTRACTOR SO THAT THE EDULPHEN ON THIS APPLICATION AND IT'S INSTALLATION WILL NO VFECT THE FOLLOWING:
- TENANT ECRESS TO AND FROM THE BUILDING/SITE.
- FIRE SAFETY OR CREATE A FIRE HAZARO.
- STRUCTURAL SAFETY OF THE ADJACENT STRUCTURES.
- ACCUMULATION OF DUST: THE CONTRACTOR SMALL EARS THE WORKSTE BROOM CLAUM CACH DAY. HE RE PORT HAIN ASSESSOS IS FOUND ON THE JUSTICE, MOTENT THE LICE CONSTRUCTION LIMANER MACEDIATE, VAN PERLOWAL SMALL THE PROFESSION SMALL STATE AND FOUNDATE RECOUNTINGS OF CORN SECTION 1910.1 INCLUMENT STATE AND FOUNDATE DUMENTS CONCESSION STATEMENTS.
- THERE SHALL BE NO CREATION OF NOISE OUTSIDE THE NORMAL HOURS OF BUILDING OPERATION.
- BUILDING SECURITY SHALL BE MANIANED IN ORDER TO PREVENT UNAUTHORIZED PERSONS FROM ENTERING THE PREMISES.
- ELECTRICITY, GAS, WATER AND ANY OTHER UTILITIES WILL NOT BE INTERRUPTED DURING CONSTRUCTION.

GENERAL GROUNDING NOTES

- THE ENTIRE ELECTRICAL INSTALLATION SHALL BE CROUNDED AS REQUIRED BY ALL APPLICABLE CODES.
- ALL BUS CONNECTORS SHALL BE TWO-HOLE, LONG-BARRE, TYPE COMPRESSION LIUGS, TAB OR EQUAL, UNLESS OTHERWISE NOTED ON DRAWNINGS. ALL LUGS SHALL BE ATTACHED TO BUSSES USING BOLTS, MUTS, AND LOCK WASHERS. NO WISHERS ARE ALLOWED BETWEEN THE ITEMS BEING GROUNDED.

1792 MAIN STREET SUITE D EAST HARTIFOND, CT 06108 1-(860)-291-0627

ALL CONNECTORS SHALL BE CRIMPED USING HYDRAULIC CRIMPING TOOLS, TAB #TBM B OR EQUIVALENT. I. CONNECTIONS SHALL BE MADE TO BARE METAL. ALL PAINTED SUBFACES
VALL BE TILED TO ENSURE PROPER CONTACT. NO WASHERS ARE ALLOWED
THEELN THE TEAS BEING GROUNDED. ALL CONNECTIONS ARE TO HAVE A
DN-OXIDIZING AGENT APPLIED PRIOR TO INSTALLATION.

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PLONE (2000) 969-7000

FAX (2002) 969-7000

- ALL COPPER BUSSES SHALL BE CLEANED, POLISHED, AND A NON-OXIDIZING ACENT APPLIED. NO PINCEPPRINTS OR DISCOLORED COPPER WILL BE PERMITTED.
- all bends shall be as shallow as possible, with no turn shorter than an $\theta-\mbox{inch}$ hominal radius.
- GROUNDING COMDUCTORS SHALL BE SOLD THINED COPPER AND AMPLEDD 72.
 ALL GROUNDING COMPUCTORS SHALL BLAW THROUGH PCT, SLEEKS HEREVER
 COMPUCTORS RAW THROUGH WALLS, FLOORS, OR CELIMOS. IF COMPUCTORS
 MUST RAW THROUGH WALLS, FLOORS OF COMDUIT SHALL BE GROUNDED. SEA
 BOTH ENDS OF COMDUIT WITH SILKCOME CHUIK.

URS CORPORATION AES SOC ENTERPRISE DANE ROCKTHILL ST. 06067

URS

- CROUNDING SYSTEM RESISTANCE SHALL NOT EXCEED 10 CHMS. IF THE RESISTANCE VALUE IS EXCEEDED, NOTIFY THE PROJECT INAMAGER FOR FURTHER INSTRUCTION ON METHODS FOR REDUCING THE RESISTANCE VALUE.
- ALL ROOF TOP ANTENNA MOUNTS SWALL BE GROUNDED WITH A #2 GROUND WIRE CONNECTED TO THE NEAREST GROUND BUS. ALL CONNECTIONS ARE TO BE CAD-WELDED IF POSSIBLE.
- 11. GROUNDING CONNECTION TO TRAVEL IN A DOWNWARD DIRECTION. UPON COMPETION OF WORK, CONDUCT CONTINUITY, SHORT CHCUIT, AND FALL OF POTENTIAL GROUNDING TESTS FOR APPROVAL. SUBMIT TEST REPORTS TO THE PROJECT MANAGER.
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- ISSUED FO
- THE INFORMATION CONTAINED
 IN THIS SET OF DOCUMENTS
 IS PROPRIETARY BY NATURE
 ANY USE OR DISCLOSURE
 OTHER THAN THAT WHICH
 RELATES TO LCC IS
 STRICTLY PROHIBITED.
- CROWN-MANCHESTER SITE ID: HAROII.A
- REAR 266 CENTER STREET
- AS NOTED

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GN-1

Power Density Calculation for XM Radio's proposed installation at 266 Center Street, Manchester, CT 06040

XM Radio Internal Site ID: HAR-011A

Power Density Calculation - Worst Case	t Case	
Base Station TX Output	1000 watts	60 dBm
Number of Tx Channels	2	
Antenna Model	TA-2350-DAB-H Omni	
Antenna Gain	10 <i>dBi</i>	
Cable Type/Size	LDF7-50A 1-5/8"	
Cable Length	160 ft	
Jumper and Connector Loss	0.69 <i>dB</i>	
Cable Loss (per foot)	0.0137 <i>dB/ft</i>	
Total Cable Loss	2.19 <i>dB</i>	
Total Attenuation	2.88 <i>dB</i>	
EIRP Per Channel	67.12 dBm	5,152.05 Watts
Total EIRP	70.12 dBm	10,304.10 Watts
Ground Reflection	1.60	
Frequency	2337.49 MHZ 2340.02 MHZ	
Antenna Height	125 ft	3,810.00 cm
nsg	10.00	
Power Density (S)	0.144607 mw/cm ²	
% MPE From XM Radio	14.4607%	
% MPE From Other Sources	0.00%	
Total % MPE From All Sources	14.4607%	

Equation Used:

Power Density (S) = $(2.56*1000*EIRP)/4*(pi)*(R)^2$

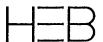
Office of Engineering and Technology (OET) Bulletin 65, Edition 97-01, August 1997

🛂 H. E. Bergeron Engineers

• Civil • Structural • Land Surveying

P.O. Box 440 2605 White Mountain Highway North Conway, NH 03860 (603) 356-6936 (603) 356-7715 (fax)

65 W. Commercial Street Portland, ME 04101 (207) 780-1100 (207) 780-1101 (fax) www.hebcivil.com



STRUCTURAL ANALYSIS REPORT **OF** 115' VALMONT MONOPOLE MANCHESTER, CONNECTICUT

Prepared for Crown Castle Atlantic, LLC

July 25, 2000



Prepared by:

H. E. Bergeron Engineers, P.A. P.O. Box 440, 2605 White Mountain Highway North Conway, NH 03860 HEB Project No. 2000-084-002

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• Civil	• Structural	Land Sur	veying
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P.O. Box 440
2605 White Mountain Highway
North Conway, NH 03860
(603) 356-6936
(603) 356-7715 (fax)

65 W. Commercial Street
Portland, ME 04101
(207) 780-1100
(207) 780-1101 (fax)
www.hebcivil.com

of
115' VALMONT MONOPOLE
MANCHESTER, CONNECTICUT
prepared for
CROWN CASTLE ATLANTIC, LLC

EXECUTIVE SUMMARY:

H.E. Bergeron Engineers, P.A. (HEB) performed a structural analysis of this 115-foot Valmont monopole tower. The analysis was performed with the addition of a TA-2335-LCC panel antenna mounted at a centerline elevation of 124-feet on a pipe extension, and a TA-2324-LHCP parabolic antenna mounted at 80-feet.

Our analysis indicates the tower and its foundation are capable of supporting the proposed antennas. The pipe extension supporting the proposed panel antenna should consist of 3" X-Strong steel pipe, ASTM A-500 grade B. Should the extended height exceed 9', the pipe size should be increased to accommodate the additional length.

INTRODUCTION:

A structural analysis of this communications tower was performed by H.E. Bergeron Engineers, P.A. (HEB) for Crown Castle Atlantic, LLC. HEB did not visit the tower site. This analysis was based on information provided by Crown Castle, which included a Valmont design drawing, and TIL-TEK antenna catalog sheets.

The structure is a 115-foot, galvanized steel monopole manufactured by Valmont. This analysis was conducted with the following antenna loads:

- (12) ALP9212 panel antennas on 15' platform at 112'; 1-5/8" waveguide
- A vacant platform at 99'
- (1) TA-2335-LCC panel antenna at 124' on a 9' pipe extension; 1-5/8" waveguide
- (1) TA2324-LHCP solid parabolic antenna at 80'; 7/8" waveguide



For the purpose of the analysis, all cables were assumed to be installed on the inside of the pole.

STRUCTURAL ANALYSIS:

Methodology:

The structural analysis was done in accordance with TIA/EIA-222-F (EIA), Structural Standards for Steel Antenna Towers and Antenna Supporting Structures; and the American Institute of Steel Construction (AISC), Manual of Steel Construction, Allowable Stress Design, Ninth Edition.

The analysis was conducted using a wind speed of 85 miles per hour and one-half inch of radial ice over the entire structure and all appurtenances. The TIA/EIA Standard requires a minimum of 80-mph wind load for Hartford County, Connecticut.

Two analytical methods were used to evaluate the structure: a two-dimensional linear model using spreadsheet programs developed by HEB, and a P-delta analysis using CSTRAAD finite element software distributed by ECOM Associates. The HEB 2-D model was used to generate dead loads of the tower and all of its appurtenances, radial ice loads and the resultant wind loading. The maximum bending moments and axial loads were used to calculate combined axial and bending stresses at intervals on the monopole, which were compared to allowable stresses according to AISC and TIA/EIA.

Loads generated in the 2-D model were input into the CSTRAAD program to evaluate secondary bending moments induced during deflection of the structure under load and to independently evaluate stresses. Evaluation of secondary bending moments is required by EIA paragraph 3.1.15. Our analysis indicates that the secondary moments exceed those of the linear analysis, and therefore govern in determining the capacity of the structure.

Two loading conditions were evaluated in accordance with EIA to determine the tower's capacity. The higher stresses resulting from the two cases is used to calculate the tower capacity:

- Case 1 = Wind Load (without ice) + Tower Dead Load (controls)
- Case 2 = 0.75 Wind Load (with ice) + Ice Load + Tower Dead Load



EIA permits a one-third increase in allowable stresses for towers less than 700-feet tall. Allowable stresses of tower members were increased by one-third in computing the load capacity values indicated herein.

ANALYSIS RESULTS:

Our analysis determined the tower will support the proposed antennae in addition to its current loading. Supporting calculations are provided in Appendix A.

The following table summarizes the capacity of the tower based on combined axial and bending stresses:

Elevation	Capacity
0'-10'	43%
10'-20'	40%
20'-29'	37%
29'-40'	44%
40'-51'	39%
51'-62'	34%
62'-72'	29%
72'-83'	40%
83'-94'	29%
94'-104'	19%
104'-115'	8%

The capability of the existing foundation to support the proposed loading was evaluated by comparing calculated values of shear, compression and overturning moment to design reactions provided on the Valmont record drawings. We found that the reactions were less than the design values. Based on these figures, the tower's foundation is adequate to support the proposed loading, provided the foundations were designed and built to the requirements of the original design drawing.



CONCLUSIONS AND SUGGESTIONS:

As detailed above, our analysis indicates that the existing 115' Valmont monopole tower and foundation are capable of supporting the additional antenna loading proposed.

The pipe extension supporting the proposed omnidirectional antenna should consist of 3" X-Strong ASTM A-500 grade B steel pipe. Should the extended height exceed 9', the pipe size should be increased to accommodate the additional length.

LIMITATIONS:

This report is based on the following:

- 1. Tower is properly installed and maintained.
- 2. All members are in new condition.
- 3. All required members are in place.
- 4. All bolts are in place and are properly tightened.
- 5. Tower is in plumb condition.
- 6. All members are galvanized.
- 7. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
- 8. Record drawings accurately reflect tower dimensions and height.

H.E. Bergeron Engineers, P.A. (HEB) is not responsible for any modifications completed prior to or hereafter which HEB is not or was not directly involved. Modifications include but are not limited to:

- 1. Adding or relocating antennas.
- 2. Installing antenna mounting gates or side arms.
- 3. Extending tower.

HEB hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon the information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact HEB. HEB disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

Appendix A

Calculations

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.: 2000-084

Calculated By: Checked By:

J. Klementovich

Mf

Date: 17-Jul-00 Date: 7/24

General Information

Tower Manufacturer Tower Type Total Height of Tower Wind Speed Radial Ice

Valmont Monopole 115 ft. 85 mph. 0.5 in.

75% Reduction for ice 1/3 increase for allowable loads yes (yes or no) yes (yes or no)

Number of faces 12 faces Calculations based on EIA/TIA-222-F, using the following formulas:

Force on discrete appurtenance: F=Qz*Gh*Ca*A Force on microwave antennae: F=Cr*A*Gh*Kz*V^2, where Cr=((Ca^2)+(Cs^2))^(1/2)

Gh=1,69 for monopoles V as specified EIA-222-F Gh= 1.69

E (Modulus of Elasticity)

29000 ksi 0.6

K

21.91 in

Min. Width = Max. Width =

48.85 in Slope of Tower = 0.0195 in/in

Tower Information

Section	Length	Midpt	Base	Тор	Area (sf)	Area (sf)	Wall	Wt. (lbs)	Wt. (lbs)
	(ft.)	Elev.	Width (in.)	Width (in.)	wlo Ice	w/ Ice	Thknss	Tower	lce
20		0.00	0.00	0.00	0.00	0.00		0.00	0.00
19	ļ .	0.00	0.00	0.00	0.00	0.00		0.00	0.00
18	1	0.00	0.00	0.00	0.00	0.00	1	0.00	0.00
17	[0.00	0.00	0.00	0.00	0.00]	0.00	0.00
16	[0.00	0.00	0.00	0.00	0.00		0.00	0.00
15	l	0.00	0.00	0.00	0.00	0.00		0.00	0.00
14		0.00	0.00	0.00	0.00	0.00		0.00	0.00
13		0.00	0.00	0.00	0.00	0.00		0.00	0.00
.12	1 1	0.00	0.00	0.00	0.00	0.00		0.00	0.00
11	10.70	109.65	24.42	21.91	20.65	21.55	0.219	747.19	154.67
10	10.70	98.95	26.92	24.42	22.89	23.78	0.219	828.82	171.05
9	10.70	88.25	29.43	26.92	25.12	26.02	0.219	910.45	187.44
8	10.70	77.55	31.94	29.43	27.36	28.25	0.219	877.60	203.82
7	10.70	66,85	34,44	31.94	29.59	30.49	0.313	1351.48	220.20
6	10.70	56.15	36.95	34.44	31.83	32.72	0.313	1454.52	236.59
5	10.70	45.45	39.46	36.95	34.06	34.96	0.313	1557.56	252.97
] 4	10.70	34.75	41.96	39.46	36.30	37.19	0.313	1660.60	269.36
3	9.80	24.50	44.26	41.96	35.21	36.02	0.375	1930.77	261.07
2	9.80	14.70	46.55	44.26	37.08	37.90	0.375	2034.49	274.82
1	9.80	4.90	48.85	46.55	38.96	39.77	0.375	2138.21	288.56
	115.00						Total	15492	2521

Monopole Summary

Page 1

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.: 2000-084

Calculated By: Checked By: J. Klementovich

Date: 17-Jul-00

Date: 7/24

Section Properties

Section	1 1	1	Area	Area	L/side	r	S
	in ⁴	mid	mid	in²	in	in	in ³
Top	919.91			15,27			
20	0.00	0.0	0.0	0,00	0.00	#DIV/0I	#DIV/0!
19	0.00	0.0	0.0	0.00	0.00	#DIV/0I	#DIV/0I
18	0.00	0.0	0.0	0.00	0.00	#DIV/01	#DIV/0I
17	0.00	0.0	0.0	0.00	0.00	#DIV/01	#DIV/0I
16	0.00	0.0	0.0	0.00	0.00	#DIV/0I	#DIV/0I
15	0.00	0.0	0,0	0.00	0.00	#DIV/01	#DIV/0!
14	0.00	0.0	0.0	0.00	0.00	#DIV/0i	#DIV/01
13	0.00	0.0	0.0	0.00	0.00	#DIV/01	#DIV/01
12	0.00	0.0	0.0	0.00	0.00	#DIV/01	#DIV/0!
11	1277.06	1098.5	16.2	17.04	6.54	8.66	104.61
10	1716.43	1496.7	17.9	18.80	7.21	9.55	127.51
9	2246.54	1981.5	19.7	20.57	7.89	10.45	152.67
8	2875,89	2561.2	21.5	22.33	8.56	11.35	180.10
7	5113.62	3994.8	28.3	34.29	9.23	12.21	296.93
6	6324.98	5719.3	35.6	36.81	9.90	13.11	342.36
5	7713.96	7019.5	38.1	39.33	10.57	14.00	391.01
4	9292.72	8503.3	40.6	41.85	11.24	14.90	442.90
3	13043.15	11167.9	47.4	52.91	11.86	15.70	589.41
2	15199.05	14121.1	54.3	55.68	12.47	16.52	652.96
1	17580.32	16389.7	57.1	58.45	13.09	17.34	719.77

Tower Dead Load Summary

Elev.		Dead load	Dead load
		Tower (lbs)	ice (lbs)
1	15.0	0	0
1	15.0	0	0
1	15.0	0	0
1	15.0	0	0
1	15.0	0	0
1	15.0	0	0
1	15.0	0	0
1	15.0	. 0	0]
1	15.0	0	0
1	15.0	0	0
1	04.3	747	155
	93.6	1576	326
	82.9	2486	513
	72.2	3364	717
	61.5	4716	937
	50.8	6170	1174
	40.1	7728	1427
	29.4	9388	1696
	19.6	11319	1957
	9.8	13353	2232
	0.0	15492	2521

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.:

2000-084

Calculated By:

J. Klementovich

Date:

17-Jul-00

1/24

Checked By:

Date:

Antennae Summary

Input:

Wind Velocity=

85 mph

	Tower Hat=	115	ft,							
<u>ANTENNAS</u>	J				Area	Area	Force	Force		
<u>Type</u>	Elev. (z)	Coeff. (C)	<u>Kz</u>	<u>Qz</u>	(no ice)	(ice)	(no ice)	(ice)	Weight	
			1.00	18.50			0	0		
			1.00	18.50			0	0		
(12) ALP9212 & platform	112	1.4	1.42	26.22	56.2	63.2	3484	3920	1624	
			1.00	18.50			0	0		
TIL-TEK TA-2335-LCC-H	124	1.2	1.46	27.00	8.0	8.4	436	559	96	
			1.00	18.50			0	0		
Empty LP platform	99	1.2	1.37	25.32	9.4	11.6	480	678	1100	
			1.00	18.50			0	0		
			1.00	18.50			0	0		
			1.00	18.50			0	0		
DISHES									9	<u>Orient</u>
TIL-TEK TA-2324-LHCP	80	0.00426	1.29	23.82	3.5	3.8	233	252	125	50 0.0043
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		
		0.00000	1.00	18.50			0	0		
									2945	

CABLES & LINEAR APPURT.

	Area	Area	Weight	Weight
Section	w/o lce	w/ Ice	w/o lce	w/lce
20	0.00	0.00	0	0
19	0.00	0.00	0	0
18	0.00	0.00	0	0
17	0.00	0.00	0	0
16	0.00	0.00	0	0
15	0.00	0.00	0	0
14	0.00	0.00	0	0
13	0.00	0.00	0	0
12	0.00	0.00	0	0
11	0.33	1.23	161	171
10	0.33	1.23	161	171
9	0,33	1.23	161	171
8	0.33	1.23	161	171
7	0.33	1.23	161	171
6	0.33	1.23	161	171
5	0.33	1.23	161	171
4	0.33	1.23	161	171
3	0.31	1.12	147	157
2	0.31	1.12	147	157
11	0.31	1.12	147	157

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Checked By:

2/24 Date:

 $Kz = Exposure coefficient = (z/33)^{2/7}; 1.00 <= Kz <= 2.58$

 $Qz = Velocity pressure = .00256*Kz*V^2$

Gh = Gust response factor = 1.69

Wind Load Summary

Wind Velocity =

85 mph

Height of Tower =

115 feet

Cf = Structure force coefficient from Table 1 of TIA/EIA Aa and Ai = Areas of linear apputenances, w/o & with ice

Ae = Effective area = Avg. width*section length

Force = Qz*Gh*(Cf*Ae+Ca*Aa)

Wind Load Without Ice

	Midpoint	Area	as						
Section	Height	Ae	Aa	Kz	Qz	Gh	Cf	Wind Load	Wind Load
20	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
19	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
18	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
17	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
16	0.00	0.0	0.00	1.00	1 8.50	1.69	1.03	0 lbs.	##### plf.
15	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
14	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
13	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
12	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
11	109.65	20.7	0.33	1.41	26.07	1.69	1.03	955 lbs.	89 plf.
10	98.95	22.9	0.33	1.37	25.31	1.69	1.03	1026 lbs.	96 plf.
9	88.25	25.1	0.33	1.32	24.50	1.69	1.03	1088 lbs.	102 plf.
8	77.55	27.4	0.33	1.28	23.61	1.69	1.03	1140 lbs.	107 plf.
7	66.85	29.6	0.33	1.22	22.63	1.69	1.03	1181 lbs.	110 plf.
6	56.15	31.8	0.33	1.16	21.53	1.69	1.03	1207 lbs.	113 plf.
5	45.45	34.1	0.33	1.10	20.27	1.69	1.03	1216 lbs.	114 plf.
4	34.75	36.3	0.33	1.01	18.77	1.69	1.03	1199 lbs.	112 plf.
3	24.50	35.2	0.31	1.00	18.50	1.69	1.03	1145 lbs.	117 plf.
2	14.70	37.1	0.31	1.00	18.50	1.69	1.03	1205 lbs.	123 plf.
1	4.90	39.0	0.31	1.00	18.50	1.69	1.03	1266 lbs.	129 plf.

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.: 000-084

Calculated By:

J. Klementovich

Date: 17-Jul-00

Checked By:

By: M

Date: 1/14

Wind Load With Ice

	Midpoint	Area	ıs						
									75% Wind
Section	Height	Ae	Ai	Kz	Qz	Gh	Cf	Wind Load	Load
20	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
19	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
18	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
17	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
16	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
15	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
14	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
13	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
12	0.00	0.0	0.00	1.00	18.50	1.69	1.03	0 lbs.	##### plf.
11	109.65	21.5	1.23	1.41	26.07	1.69	1.03	1042 lbs.	73 plf.
10	98.95	23.8	1.23	1.37	25.31	1.69	1.03	1111 lbs.	78 plf.
9	88.25	26.0	1.23	1.32	24.50	1.69	1.03	1170 lbs.	82 plf.
8	77.55	28.3	1.23	1.28	23.61	1.69	1.03	1220 lbs.	85 plf.
7	66.85	30.5	1.23	1.22	22.63	1.69	1.03	1257 lbs.	88 plf.
6	56.15	32.7	1.23	1.16	21.53	1.69	1.03	1280 lbs.	90 plf.
5	45.45	35.0	1.23	1.10	20.27	1.69	1.03	1284 lbs.	90 plf.
4	34.75	37.2	1.23	1.01	18.77	1.69	1.03	1262 lbs.	88 plf.
3	24.50	36.0	1.12	1.00	18.50	1.69	1.03	1202 lbs.	92 plf.
2	14.70	37.9	1.12	1.00	18.50	1.69	1.03	1262 lbs.	97 plf.
1	4.90	39.8	1.12	1.00	18.50	1.69	1.03	1323 lbs.	101 plf.

ELEMENT LIST : 1-11

0.000

-1.300

0.000

July 25, 2000 Page 1 HEB Project #2000-084-002

NODE	REBAND		иори	r cc	ORD	INATE	S						٠,	r-r1x,3-3	UP,M=M DDDC		
ИО	ИО		x	Y		z		ODE TEM			BETA		GAMMA	DIR	XYZX	KYZ	STIFFNESS
Jnits			rt Ft	Ft		Ft		F	Deg		Deg	====	Deg				K /In /Deg
1	1		0.00		0.00	0.0	00	0	.00 0	00	0.00		0.00		FFF	FFF	
2	2		0.00		9.80	0.0				00	0.00		0.00				
3	3		0.00	_	9.60	0.0				00	0.00		0.00				
4 5	4 5		0.00		9.40 0.10	0.0				00	0.00		0.00				
6	6		0.00		0.80	0.0				00	0.00		0.00				
7	7		0.00		1.50	0.0				00	0.00		0.00				
8	8		0.00	7	2.20	0.0	00	0	.00 0	00	0.00		0.00				
9	9		0.00		2.90	0.0				00	0.00		0.00				
10	10		0.00		3.60	0.0				00	0.00		0.00				
11 12	11 12		0.00		4.30 5.00	0.0				00 00	0.00 0.00		0.00				
			TIVE NOD UATIONS		12 66												
====	**==**			=======					TIC B						SPEECS:		
LEM	NE	PE	ALPHA	BETA		LENGTH		PROP	RELEASE		REF	E P	ENI	OFFSET			STIFFNESS
NO	NO	NO	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2211	0,,,,,,,	22.011		TYPE	NE PE		TEMP	DIR	NI		PE	NI	
====		=====	=======	=======	=======			======	========					=======		======	
nits	:		Deg	Deg	Deg	Ft					F		Ft	:	Ft	K /In	/Deg K /In /
1	1	2		-90.00	0.00		1	1									
2	2	3	90.00	-90.00	0.00		1	2									
3	3	4 5	90.00 90.00	-90.00 -90.00	0.00		1	3									
4 5	4 5	6	90.00	-90.00	0.00		1	4 5									
6	6	7		-90.00	0.00		1										
7	7	8	90.00	-90.00	0.00	10.70	1	7									
8	8	9	90.00	-90.00	0.00	10.70	1	8									•
9	9	10	90.00	-90.00	0.00		1	9									
10 11	10 11	11 12		-90.00 -90.00	0.00		1	10 11									
TAL	NUMBER	OF AC	TIVE PRI	SMATIC B	BEAM ELE	MENTS =	11										
		=====	=======	=======					ROPER			===:			=====		
iatl No			NATION	OM	DULUS DUNG'S	RA'	SON'S	THE CC	CRMAL DEFF	MAS: DENS:	S ITY		WEIGHT DENSI	ľY			
nits		22255	=======		/In ^2					=====: /Ft^3		:===:	Lb/F				xxxxxx#=====
m_1 \downarrow S					.9e+004		.250	6.5	-006	1	5.2		4:	90			
	Pole			2) = + 0 0 4												
1			======														
1 PROP	DESIGN	ATION	r	2 NO	DE P	R I S M I	ATI	C B E	AM EL J	E M 1	E N T	PI	R O P I	ERTIE SFX	s C	W	
1 PROP	DESIGN	ATION	r	2 NO	DE P	R I S M I	ATI	C B E	AM EL J	E M 1	E N T	PI	R O P I	ERTIE SFX	S	W	D t = 2 U H A S = 7 T = 7 T
1 PROP	DESIGN	ATION	r	2 NO	DE P	RISMI IXX In^4	A T I	C B F	EAM EL J In^4	E M 1	E N T	P 1	ROPI SFY	ERTIE SFX	S	w ====== n^6	************
1 PROP Jnits	DESIGN	ATION	r	2 NO	DE P	R I S M I IXX In^4	A T I	C B F IYY In^4 54e+004	IAM EL J In^4 3.28e+00	E M 1	E N T	P 1	R O P 1 SFY =====:	E R T I E SFX ========	S	w ====== n^6	
1 PROP Jnits	DESIGN	ATION	r	2 N O A	D E P	RISMI IXX In^4	1.4 1.4	C B F	EAM EL J In^4 3.28e+00 2.82e+00	E M 1	E N T	P 1	ROPI SFY	ERTIE SFX ======= 1.000 1.000	S	w ====== n^6	
PROP Inits	DESIGN	ATION	r	2 NO A	DE P	IXX IXX In^4 1.64e+004 1.41e+004	1.6 1.6	C B F IYY ======= In^4 54e+004 41e+004 12e+004 .5e+003	In^4 3.28e+00 2.82e+00 2.23e+00 1.7e+00	E M 1 ====: 4 4 4	E N T	P 1	SFY ======: 1.000 1.000 1.000 1.000	1.000 1.000 1.000	S	W ====== n^6 0 0 0	***********
1 PROP ==== Units 1 2 3 4 5	DESIGN ====================================	ATION	r	2 NO A	DE P 57.1 54.3 47.4 40.6 38.1	R I S M IXX In^4 1.64e+004 1.41e+004 1.12e+004 8.5e+003 7.02e+003	1.4 1.4 1.5 8	C B F IYY ======= In^4	In^4 3.28e+00 2.82e+00 2.82e+00 1.7e+00 1.4e+00	E M 1 ====: 4 4 4 4 4	E N T	P 1	SFY ======: 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000	S	0 0 0 0 0	
1 ==== ROP ==== nits 1 2 3 4 5 6	DESIGN ======= : Section 2 3 4 5 6	ATION	r	2 NO A	DE P 57.1 54.3 47.4 40.6 38.1 35.6	R I S M IXX ======== In^4 1.64e+004 1.12e+004 8.5e+003 7.02e+003 5.72e+003	1.: 1.: 8.7.:	C B F IYY ======= In^4	I A M E L J In^4 3.28e+00 2.82e+00 2.23e+00 1.7e+00 1.4e+00 1.14e+00	E M 1 =====	E N T	P 1	SFY SFY 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000	S	0 0 0 0 0 0	***************************************
1 PROP Jnits 1 2 3 4 5 6 7	DESIGN :: Sectio 2 3 4 5 6 7	ATION	r	2 NO A	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3	R I S M IXX ======= In^4 1.64e+004 1.41e+004 1.12e+004 8.5e+003 5.72e+003 4e+003	1.4 1.4 1.6 8 7.6	C B F IYY ======== In^4 64e+004 11e+004 12e+003 02e+003 72e+003 4e+003	3.28e+00 2.82e+00 2.82e+00 2.23e+00 1.7e+00 1.4e+00 7.99e+00	E M 1 4 4 4 4 4 4 4 4 4 4	E N T	P 1	SFY SFY 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000	S	w ====== n^6 0 0 0 0 0	
1 PROP ==== Jnits 1 2 3 4 5 6 7 8	DESIGN ====================================	ATION	r	2 N O A I	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3 21.5	R I S M IXX In^4 1.64e+004 1.41e+004 1.12e+004 8.5e+003 7.02e+003 4e+003 2.56e+003	1.4 1.4 1.7 2.1	C B F IYY ======== In^4 64e+004 11e+004 12e+003 5e+003 72e+003 4e+003 56e+003	In^4 3.28e+00 2.82e+00 2.23e+00 1.7e+00 1.4e+00 7.99e+00 5.12e+00	E M 1 4 4 4 4 4 4 4 3 3	E N T	P 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	S	0 0 0 0 0 0	
1 PROP ==== Jnits 1 2 3 4 5 6 7	DESIGN Section 3 4 5 6 7 8	ATION	r	2 NO A	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3 21.5	R I S M IXX ======= In^4 1.64e+004 1.41e+004 1.12e+004 8.5e+003 5.72e+003 4e+003	1.6 1.6 1.6 8 7.0 5.1	C B F IYY ======== In^4 64e+004 11e+004 12e+003 02e+003 72e+003 4e+003	In M E L J In M S L I	E M 1 4 4 4 4 4 4 4 3 3 3 3	E N T	P 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000	S	0 0 0 0 0 0 0	
1 PROP ==== Jnits 1 2 3 4 5 6 7 8	DESIGN Section 3 4 5 6 7 8 9 10	ATION	r	2 NO A	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3 21.5 19.7	R I S M 1XX ======== In^4 1.64e+004 1.12e+004 1.12e+003 7.02e+003 5.72e+003 4e+003 2.56e+003	1.6 1.6 1.7 2.1 1.1	C B F IYY ======= In^4 54e+004 12e+004 .5e+003 02e+003 72e+003 4e+003 56e+003 98e+003	In^4 3.28e+00 2.82e+00 2.23e+00 1.7e+00 1.4e+00 7.99e+00 3.96e+00	E M 1 ====== 4 4 4 4 4 4 3 3 3 3 3	E N T	P 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	S	0 0 0 0 0 0 0	
1 PROP 1 2 3 4 5 6 7 8 9 10 11	DESIGN Section 3 4 5 6 7 8 9 10	ation	(= === ====	2 NOA	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3 21.5 19.7 17.9 16.2	R I S M 1XX ======== In^4 1.64e+004 1.41e+004 1.12e+003 7.02e+003 4.02e+003 2.56e+003 1.5e+003 1.1e+003	1.4 1 1 8 7 2 1 1	C B F IYY	I A M E L J III 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E M 1 4444444433333333333333333333333333333	ENT IXY ====== In^4	P 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	S C	0 0 0 0 0 0 0 0	
1 PROP ===== Units 1 2 3 4 5 6 7 8 9 10 11	DESIGN Section 3 4 5 6 7 8 9 10	ation		2 NOA	DE P 57.1 54.3 47.4 40.6 38.1 35.6 28.3 21.5 19.7 17.9 16.2	R I S M 1XX ======== In^4 1.64e+004 1.41e+004 1.12e+003 7.02e+003 4.02e+003 2.56e+003 1.5e+003 1.1e+003	1.4 1 1 8 7 2 1 1	C B F IYY	I A M E L J In^4 3.28e+00 2.82e+00 1.7e+00 1.4e+00 7.99e+00 3.96e+00 2.29e+00 2.2e+00	E M 1 4444444433333333333333333333333333333	ENT IXY ====== In^4	P 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	S C	0 0 0 0 0 0 0 0	

	2 N	O D E	PRISM					MATION	**************	====
REC LOAD LOAD NO TYPE SYS	SPEC		DIST	PX	PΥ	PZ	мх	MY	MZ	
Units:			Ft	K.	К	К	Ft-K	Ft-K	Ft-K	-
DESCRIPTION : W LOAD CASES : 1 ELEMENT LIST : 1	ind on s	ection	n 1							
1 UNIF GLO	FRAC	B E	0.000 1.000	0.129 0.129	0.000	0.000	0.000 0.000	0.000	0.000	
DESCRIPTION : 2 LOAD CASES : 1 ELEMENT LIST : 2										
2 UNIF GLO	FRAC	B E	0.000 1.000	0.123 0.123	0.000	0.000	0.000 0.000	0.000	0.000	
DESCRIPTION : 3 LOAD CASES : 1 ELEMENT LIST : 3										
3 UNIF GLO	FRAC	B E	0.000 1.000	0.117 0.117	0.000 0.000	0.000	0.000 0.000	0.000	0.000	•
DESCRIPTION : 4 LOAD CASES : 1 ELEMENT LIST : 4										
4 UNIF GLO	FRAC	B E	0.000 1.000	0.112 0.112	0.000	0.000	0.000 0.000	0.000	0.000 0.000	
DESCRIPTION : 5 LOAD CASES : 1 ELEMENT LIST : 5										
5 UNIF GLO	FRAC	B E	0.000 1.000	0.114 0.114	0.000	0.000	0.000	0.000 0.000	0.000 0.000	
DESCRIPTION : 6 LOAD CASES : 1 ELEMENT LIST : 6										
	FRAC	B E	0.000	0.113	0.000 0.000	0.000	0.000	0.000	0.000	
DESCRIPTION : 7 LOAD CASES : 1 ELEMENT LIST : 7										
7 UNIF GLO		B E	0.000 1.000	0.110 0.110	0.000	0.000	0.000	0.000	0.000 0.000	
DESCRIPTION : 8 LOAD CASES : 1 ELEMENT LIST : 8										
8 UNIF GLO	FRAC	B E	0.000 1.000	0.107 0.107	0.000	0.000	0.000	0.000	0.000 0.000	
DESCRIPTION : 9 LOAD CASES : 1 ELEMENT LIST : 9										
9 UNIF GLO	FRAC	B E	0.000 1.000	0.102 0.102	0.000	0.000	0.000	0.000	0.000 0.000	
DESCRIPTION : 1 LOAD CASES : 1 ELEMENT LIST : 1	-									
10 UNIF GLO	FRAC	B E	0.000 1.000	0.096 0.096	0.000	0.000	0.000	0.000 0.000	0.000 0.000	
DESCRIPTION : I LOAD CASES : I ELEMENT LIST : I	L									
11 UNIF GLO	FRAC	B E	0.000	0.089 0.089	0.000	0.000	0.000 0.000	0.000 0.000	0.000 0.000	

DESCRIPTION : (12) ALP92 LOAD CASES : 1 ELEMENT LIST : 11 DISTANCES : 7.7	12 & platform @ :	112'					
101 CONC GLO DIST		3.484	-1.624	0.000	0.000	0.000	0.000
DESCRIPTION : TIL-TEK TA LOAD CASES : 1 ELEMENT LIST : 11 DISTANCES : 10.7	.2335 @ 124' on p	ipe mount					
102 CONC GLO DIST		0.436	-0.096	0.000	0.000	0.000	3.924
DESCRIPTION : TIL-TEK TALOAD CASES : 1 ELEMENT LIST : 8 DISTANCES : 7.8	.2324 dish @ 80'						
103 CONC GLO DIST		0.233	-0.125	0.000	0.000	0.000	0.000
DESCRIPTION : Empty plat LOAD CASES : 1 ELEMENT LIST : 10 DISTANCES : 5.4	form at 99'						
104 CONC GLO DIST		0.480	-1.100	0.000	0.000	0.000	0.000
REC NO ALPHA BETA	GAMMA PX			OADS PZ	MX	мү	MZ
Units: Deg Deg			K	K	Ft-K	Ft-K	Ft-K
DESCRIPTION : Waveguide LOAD CASES : 1 NODE LIST : 2-4	dead loads						
1 0.00 0.00	0.00	0.000	-0.147	0.000	0.000	0.000	0.000
DESCRIPTION : WG d.1. LOAD CASES : 1 NODE LIST : 5-12							
2 0.00 0.00	0.00	0.000	-0.161	0.000	0.000	0.000	0.000
COMB LIST OF FACTORS *	S T R	UCTURE	LOAD CO	MBINATIO	N S		

DESCRIPTION : Wind + dead loads 1 1*1

IODE	LOAD		/* T-4:		ISPLACEM				
NO	COMB		DX	cates Displacement DY	DZ	ox	OY	oz	
nits:			In	In	In	Deg	Deg	Deg	
2	1		0.2009	-0.0015	0.0000	0.0000	0.0000	-0.1883	
3	1		0.7878	-0.0028	0.0000	0.0000	0.0000	-0.3758	
4	1		1.7745	-0.0042	0.0000	0.0000	0.0000	-0.5768	
5	1		3.3467	-0.0056	0.0000	0.0000	0.0000	-0.8149	
6	1		5.4450	-0.0070	0.0000	0.0000	0.0000	-1.0455	
7	1		8.0481	-0.0082	0.0000	0.0000	0.0000	-1.2646	
8	1	*	11.1600	-0.0094	0.0000	0.0000	0.0000	-1.4965	
9	1		14.8167	-0.0108	0.0000	0.0000	0.0000	-1.7457	
10	1		18.9760	-0.0120	0.0000	0.0000	0.0000	-1.9438	
11	1		23.4979	-0.0129	0.0000	0.0000	0.0000	-2.0683	
12	1		28.1862	-0.0134	0.0000	0.0000	0.0000	-2.0953	
ELEM NO	2 LOAD COMB	N O D E NODE NO		C BEAM EL IGN CONVENTION: BE SHEAR X		FORCES MOMENT X	AND MOME MOMENT Y	N T S TORSION	
				X				=======================================	
	-					K -Ft		K -Ft	
1	1	1 2	-21.8720 -19.3966	0.0000 0.0000	17.2693 16.0051	-1189.4116 -1026.3670	0.0000	0.0000 0.0000	
2	1	2	-19.2496	0.0000	16.0051	-1026.3670	0.0000	0.0000	
		3	-16.8956	0.0000	14.7997	-875.4235	0.0000	0.0000	
3	1	3 4	-16.7486 -14.6938	0.0000 0.0000	14.7997 13.6531	-875.4235 -736.0048	0.0000 0.0000	0.0000 0.0000	
4	1	4	-14.5468	0.0000	13.6531	-736.0048	0.0000	0.0000	
		5	-12.6251	0.0000	12.4547	-596.3280	0.0000	0.0000	
5	1	5 6	-12.4641 -10.6607	0.0000 0.0000	12.4547 11.2349	~596.3280 -469.5887	0.0000 0.0000	0.0000 0.0000	
6	1	6	-10.4997	0.0000	11.2349	-469.5887	0.0000	0.0000	
_		7	-8.8147	0.0000	10.0258	-355.8439	0.0000	0.0000	
7	1	7	-8.6537	0.0000	10.0258	-355.8439	0.0000	0.0000	
_	_	8	-7.3141	0.0000	8.8488	-254.8648	0.0000	0.0000	
8	1	8 9	-7.1531 -6.0105	0.0000 0.0000	8.8488 7.4709	-254.8648 -166.9836	0.0000 0.0000	0.0000 0.0000	
9	1	9	-5.8495	0.0000	7.4709	-166.9836	0.0000	0.0000	
		10	-4.9170	0.0000	6.3795	-92.8839	0.0000	0.0000	
10	1	10 11	-4.7560 -2.8088	0.0000 0.0000	6.3795 4.8723	-92.8839 -32.6628	0.0000 0.0000	0.0000 0.0000	
11	1	11	-2.6478	0.0000	4.8723	-32.6628	0.0000	0.0000	
		12	-0.2570	0.0000	0.4360	3.9240	0.0000	0.0000	
				R E A C	T I O N S	=======================================			
NODE NO	LOAD COMB		(* . PX	Indicates Reactions PY		Local System) MX	му	MZ	
		.======:		K K			 K -Ft	K -Ft	
							- •		

******			P-D E L		LYSIS			
NODE NO	LOAD COMB		(* Indi	NODAL D; cates Displacement DY	ISPLACEM s Occur in Noda: DZ	ENTS Local System) OX	ОУ	OZ
nits:	========		In	In	In	Deg	Deg	Deg
2	1		0.2038	-0.0016	0.0000	0.0000	0.0000	-0.1911
3	1		0.7997	-0.0045	0.0000	0.0000	0.0000	-0.3817
4	1		1.8022	-0.0101	0.0000	0.0000	0.0000	-0.5863
5	1		3.4012	-0.0215	0.0000	0.0000	0.0000	-0.8291
6	1		5.5370	-0.0406	0.0000	0.0000	0.0000	-1.0646
7	1		8.1884	-0.0692	0.0000	0.0000	0.0000	-1.2886
8	1		11.3600	-0.1095	0.0000	0.0000	0.0000	-1.5258
9	1		15.0889	-0.1650	0.0000	0.0000	0.0000	-1.7809
10	1		19.3320	-0.2363	0.0000	0.0000	0.0000	-1.9836
11	1		23.9457	-0.3201	0.0000	0.0000	0.0000	-2.1108
12	1		28.7293	-0.4097	0.0000	0.0000	0.0000	-2.1385
		*********		P=====================================			******	.======================================
ELEM	2 LOAD	N O D E NODE	PRISMATI SI	C BEAM EL: GN CONVENTION: BE	E M E N T AM DESIGNERS	FORCES	AND MOME	ENTS
NO	COMB	NO	AXIAL	SHEAR X	SHEAR Y	MOMENT X	MOMENT Y	TORSION
nits:			·ĸ	к	к	K -Ft	K -Ft	K -Ft
1	1	1 2	-21.8420 -19.3689	0.0000 0.0000	17.3072 16.0387	-1205.9820 -1042.5874	0.0000 0.0000	0.0000 0.0000
2	1	2 3	-19.1683 -16.8204	0.0000	16.1025 14.8852	-1042.5878 -890.7483	0.0000	0.0000
3	1	3 4	-16.6219 -14.5769	0.0000	14.9420 13.7779	-890.7490 -750.0214	0.0000 0.0000	0.0000
4	1	4 5	-14.3757 -12.4691	0.0000 0.0000	13.8330 12.6108	-750.0213 -608.5467	0.0000 0.0000	0.0000 0.0000
5	1	5 6	-12.2552 -10.4724	0.0000 0.0000	12.6603 11.4107	-608.5465 -479.7670	0.0000	0.0000
6	1	6 7	-10.2654 -8.6057	0.0000 0.0000	11.4494 10.2058	-479.7681 -363.9125	0.0000	0.0000
7	1	7 8	-8.4035 -7.0935	0.0000 0.0000	10.2361 9.0264	-363.9119 -260.8574	0.0000	0.0000
8	1	8 9	-6.8932 -5.7910	0.0000 0.0000	9.0527 7.6422	-260.8555 -170.9585	0.0000	0.0000 0.0000
9	1	9 10	-5.5994 -4.7035	0.0000 0.0000	7.6604 6.5388	-170.9599 -94.9945	0.0000	0.0000
10	1	10 11	-4.5239 -2.6321	0.0000	6.5461 4.9699	-94.9957 -33.3590	0.0000 0.0000	0.0000 0.0000
11	1	11 12	-2.4644 -0.2569	0.0000	4.9675 0.4419	-33.3581 3.9238	0.0000 0.0000	0.0000 0.0000
======= NODE	LOAD	##=======			TIONS			
NO	COMB	=======================================	PX	P Y ===##########	PZ ====================================	MX =========		MZ
Jnits:			к	к	K	K -Ft	K -Ft	K -Ft
1	1		-17.2693	21.8720	0.0000	0.0000	0.0000	1205.9820

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.:

2000-084

Calculated By:

J. Klementovich

Date:

17,-Jul-00

Checked By:

ROA

Date:

7/24

Total Moment (Tower & Antennas)

Axial Loads (kips)

Shear

							· , ,				
	Mom,	75% Mom	100% Mom		D+A	D+A+I		Tower	Antenna	Total	
Elevation	w/o lce	w/ lce	w/ lce	Secondary	Force	Force	Secondary	(lbs.)	(lbs)	(kips)	Secondary
0	1196.8	997.7	1330.3	1206	18.5	21.0	21.8	13413	4634	18.05	17.3
10	1033.8	864.3	1152.4	1043	16.3	18.6	19.2	12090	4634	16.72	16.1
20	883.0	740.3	987.0	891	14.3	16.3	16.6	10828	4634	15.46	14.9
29	743.6	625.4	833.8	750	12.4	14.1	14.4]	9626	4634	14.26	13.8
40	604.0	509.8	679.7	609	10.7	12.2	12.3	8364	4634	13.00	12.7
51	477.4	404.4	539.2	480	9.2	10.4	10.3	7080	4634	11.71	11.4
62	363.6	309.3	412.4	364	7.7	8.7	8.4	5800	4634	10.43	10.2
72	262.7	224.4	299.2	261	6.4	7.1	6.9	4543	4634	9.18	9.1
83	174.9	150.0	199.9	171	5.4	5.9	5.6	3323	4401	7.72	7.7
94	100.8	86.6	115.5	95	4.5	4.8	4.5	2153	4401	6.55	6.5
104	40.5	35.1	46.8	33	2.6	2.8	2.5	1042	3920	4.96	5.0
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115	3.9	3,8	5.0		0.1	0.1		О	436	0.00	
115	3.9	3.8	5.0		0.1	0.1		0	436	0.00	
115		1	ł	ł	0.1	0.1	}	0	436	0.00	1 1
115		4	1	ł	0.1	0.1	1	0	436	0.00	1 1

2605 White Mountain Highway, PO Box 440 North Conway, NH 03860 (603) 356-6936

Client:

Crown Castle Atlantic

Job:

Manchester, CT

Job No.: 20

2000-084

Calculated By:

J. Klementovich

Date:

17-Jul-00

Checked By:

MH

Date: 1/24

Axial Force

				Stress Ratio
Elev.	w/o ice	Area	Fy	w/o ice
0	21.8	58.45	65	0.37
10	19.2	55.68	65	0.34
20	16.6	52.91	65	0.31
29	14.4	41.85	65	0.34
40	12.3	39.33	65	0.31
51	10.3	36.81	65	0.28
62	8.4	34.29	. 65	0.24
72	6.9	22.33	65	0.31
83	5.6	20.57	65	- 0.27
94	4.5	18.80	65	0.24
104	2.5	17.04	65	0.15
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!
115	0.0	0.00		#DIV/0!

Bending Force

fb=	Moment/Section Mo		Bending Stress				
		Allowa	Allowable				
Elev.	w/o ice	S	(FY)^.5 w/t	Fb	1.33 Fb	w/o ice	
0	1206.0	719.77	281.4	36.02	47.91	20.11	
10	1043.0	652.96	268.2	36.99	49.19	19.17	
20	891.0	589.41	255.0	37.95	50.47	18.14	
29	750.0	442.90	290.1	35.39	47.07	20.32	
40	609.0	391.01	272.8	36.65	48.75	18.69	
51	480.0	342.36	255.4	37.92	50.43	16.82	
62	364.0	296.93	240.0	39.04	51.93	14.71	
72 .	261.0	180.10	315.0	33.57	44.65	17.39	
83	171.0	152.67	290.3	35.37	47.05	13.44	
94	95.0	127.51	265.6	37.18	49.44	8.94	
104	33.0	104.61	240.9	38.98	51.84	3.79	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
115	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	

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Job:

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Calculated By:

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Checked By:

2000-084

Date: Date:

Job No.:

17-Jul-00 7/24

Combined Axial and Bending

Elev.	Comb. Loads	Capacity
0	0.427	43%
10	0.397	40%
20	0.366	37%
29	0.439	44%
40	0.390	39%
· 51	0.339	34%
62	0.288	29%
72	0.396	40%
83	0.291	29%
94	0.186	19%
104	0.076	8%
115	#DIV/0!	#DIV/0!