



4545 East River Road, Suite 320
West Henrietta, NY 14586

April 1, 2020

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

**RE: Notice of Exempt Modification for Verizon:
Crown Castle Site ID#: 806372
266R Center Street, Manchester, CT 06040
Latitude: 41 ° -46' 19.0" / Longitude: -72° -31' 48.8"**

Dear Ms. Bachman:

Verizon currently maintains twelve (12) total antennas at the 115-foot mount on the existing 115-foot monopole tower, located at 266R Center Street in Manchester. Both the tower and property are owned by Crown Castle. Verizon now intends to replace six (6) antennas and add (3) remote radio units.

Tower modifications:

- Replace three (3) existing antennas with three (3) new CBRS antennas
- Replace three (3) existing antennas with three (3) new LNX-6512DS-A1M antennas
- Add three (3) new CBRS remote radio units

Ground modifications:

- None

Melanie A. Bachman

This facility was approved by the Connecticut Siting Council on August 24, 1990 in Docket No. 129. There were no conditions listed in the approval.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to Town General Manager Mr. Scott Shanley and the town of Manchester Planning Department. Crown Castle is the tower and property owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Verizon respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to my attention at the address listed below.

Sincerely,



Richard Zajac
Network Real Estate Specialist
4545 East River Road, Suite 320
West Henrietta, NY 14586
585-445-5896
richard.zajac@crowncastle.com

Melanie A. Bachman

cc:

Mr. Scott Shanley
General Manager
Town of Manchester
41 Center Street
Manchester, CT 06045
860-647-3123

Mr. Gary Anderson
Planning and Zoning
Town of Manchester
494 Main Street
Lincoln Center, 2nd FL
Manchester, CT 06045
860-647-3044

From: [Zajac, Richard](#)
To: ganderson@manchesterct.gov
Subject: Connecticut Siting Council exempt modification application notification
Date: Wednesday, April 1, 2020 10:27:00 AM
Attachments: [CSC Exempt Modification application - 266R Center Street.pdf](#)

Good morning Mr. Anderson,
Please see the attached application to the Connecticut Siting Council regarding antenna work on the existing cell tower located at 266R Center Street in Manchester.

Should you have any questions/comments/concerns regarding this application, please do not hesitate to contact me.

Thank you,
RICH ZAJAC
Network Real Estate Specialist
T: (585) 445-5896 M: (607) 346-7212
F: (724) 416-4461
CROWN CASTLE
[4545 East River Road, Suite 320](#)
[West Henrietta, NY 14586](#)

From: [Zajac, Richard](#)
To: "sshanley@manchesterct.gov"
Subject: Connecticut Siting Council exempt modification application notification
Date: Wednesday, April 1, 2020 10:25:00 AM
Attachments: [CSC Exempt Modification application - 266R Center Street.pdf](#)

Good morning Mr. Shanley,

Please see the attached application to the Connecticut Siting Council regarding antenna work on the existing cell tower located at 266R Center Street in Manchester.

Should you have any questions/comments/concerns regarding this application, please do not hesitate to contact me.

Thank you,

RICH ZAJAC

Network Real Estate Specialist

T: (585) 445-5896 M: (607) 346-7212

F: (724) 416-4461

CROWN CASTLE

4545 East River Road, Suite 320

West Henrietta, NY 14586

Exhibit A

Original Facility Approval

BH
B1

STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401
New Britain, Connecticut 06051
Phone: 827-7682



August 24, 1990

Gloria Dibble Pond
Chairperson

COMMISSIONERS

Energy/Telecommunications

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Leslie Carothers

Hazardous Waste/Low-level
Radioactive Waste

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Bernard R. Sullivan

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Mortimer A. Gelston
Daniel P. Lynch, Jr.
Paulann H. Sheets
William H. Smith
Colin C. Tait

Joel M. Rinebold
Executive Director

Stanley J. Modzelesky
Executive Assistant

Mr. David S. Malko
Manager, Engineering and Regulatory Services
Metro Mobile
50 Rockland Road
South Norwalk, CT 06854

RE: DOCKET NO. 129 - Metro Mobile CTS of Hartford, Inc.,
Certificate of Environmental Compatibility and Public
Need for the construction, maintenance, and operation
of a cellular telephone tower and associated equipment
in the Town of Manchester, Connecticut.

Dear Mr. Malko:

On August 22, 1990, the Siting Council considered and approved all remaining sections of the Development and Management Plan (D&M) for this cellular telephone tower and associated equipment in the Town of Manchester, Connecticut. This decision confirms use of barbed wire on the security fence surrounding the cellular site that was approved by the Council by its Decision and Order on March 12, 1990.

This approval applies only to the D&M plan submitted for the Manchester site. Modifications to this D&M Plan require advance Council notification and approval. Please notify the Council when construction is completed.

Enclosed for your use is a copy of the Staff Report regarding the D&M Plan.

Very truly yours,

Gloria Dibble Pond
Chairperson

SMH/smh

enclosure

4706-2

METRO MOBILE

July 20, 1990

Connecticut Siting Council
136 Main Street
Suite 401
New Britain, CT 06051

Attention: Joel M. Rinebold, Executive Director

Re: Docket No. 129 - Metro Mobile CTS of Hartford, Inc.
Manchester Cell Site

Dear Mr. Rinebold:

Metro Mobile CTS of Hartford, Inc. ("Metro Mobile") has submitted a proposed D&M Plan in the above-referenced proceeding and has received comments on it from the Town of Manchester and the Council.

Metro Mobile intends to construct an eight foot security fence around the facility with three strands of barbed wire on top. One of the comments received addresses the potential restriction on the use of barbed wire in constructing a fence at the proposed facility under Section 47-47 of the Connecticut General Statutes. This communication sets forth Metro Mobile's position that Metro Mobile is unaffected by said provision, as well as the Company's arguments in support of its position that the fencing plans already submitted are within State laws.

The provision of interest is Section 47-47 of the Connecticut General Statutes, which reads, in relevant part, as follows:

Barbed wire between adjoining premises or enclosing grounds of public buildings. No person shall use barbed wire in the construction of fences or have barbed wire upon existing fences between his own premises and those of an adjoining proprietor, within twenty-five rods of any house or barn belonging to such proprietor, unless either premises are used in connection with raising livestock, without first obtaining his written consent

.....

A. THE SITING COUNCIL'S JURISDICTION SUPERSEDES THE RESTRICTIONS IMPOSED BY C.G.S. SECTION 16-50x.

The Connecticut Siting Council was created with the express purpose of considering applications for the construction, operation, and maintenance of certain types of facilities within the state, including the proposed Manchester facility. The Council's jurisdiction overrides select state and local laws which would otherwise place restrictions on such activities. Section 16-50x of the C.G.S. contains the override language, as follows:

(a) Notwithstanding any other provision of the general statutes to the contrary, except as provided in Section 16-243, the council shall have exclusive jurisdiction over the location and type of facilities and over the location and type of modifications of facilities subject to the provisions of subsection (d) of this section. (emphasis added)

It should be noted that neither Section 16-243 nor subsection (d) of Section 16-50x modifies the applicability of the section quoted above with respect to the proposed Metro Mobile facility.

Whether the proposed facility uses barbed wire is an issue as to the type of facility to be constructed. Thus, it falls within the exclusive jurisdiction of the Council and cannot be affected by other statutes or local regulations.

B. EVEN IF THE COUNCIL'S JURISDICTION DOES NOT SUPERSEDE SECTION 47-47, METRO MOBILE'S PROPOSED FACILITY WILL NOT COME WITHIN THE AMBIT OF THAT PROVISION.

As set forth above, Metro Mobile's position is that the Council's jurisdiction supersedes the provisions of Section 47-47, and that the statute is therefore inapplicable to Metro Mobile at the Manchester facility certificated by the Council. If, however, the Council concludes that its jurisdiction does not supersede the statute, Metro Mobile contends that the provisions of the statute are inapplicable to Metro Mobile for the following reasons.

1. Proposed Fence Not Between Proprietors

The statute prohibits the use of barbed wire ". . . between his own premises and those of an adjoining proprietor . . ." In Manchester, Metro Mobile's proposed facility will not border two separate land parcels except on the east and southwest sides (see page 5 of Tab 1 in the Metro Mobile Application for the Manchester Site, Siting Council Docket No. 129).

Connecticut Siting Council
Mr. Joel M. Rinebold - Docket No. 129
July 20, 1990
Page 3

On the north side of Metro Mobile's facility, the proposed barbed wire will not be between two adjoining proprietors, since Metro Mobile facility is located on a portion of a parcel owned by S. Mark Stephens.

2. No Houses or Barns Located on Adjacent Property

The statute prohibits the use of barbed wire ". . . within twenty-five rods of any house or barn belonging to such proprietor" On the east side of the Metro Mobile facility, there is a strip of land owned by Kenneth C. Burkamp over which the Consolidated Rail Corporation at one time had an easement to operate a railway. There are no houses or barns located on this parcel, and therefore the prohibition cannot apply to Metro Mobile with respect to this parcel.

Similarly, the southwest side of the Metro Mobile facility is bordered by a parcel owned by Kenneth C. Burkamp. There are no houses or barns located on this parcel. The prohibition stated in the barbed wire statute therefore cannot apply to Metro Mobile with respect to this parcel.

Thus, even if the Council finds that its jurisdiction does not supersede the provisions of Section 47-47 of the C.G.S., those provisions do not apply to Metro Mobile in this case.

Respectfully yours,

David S. Malko
DSS

David S. Malko, P.E.
Manager, Engineering and Regulatory Services

DSM:mb

cc: Service List Docket 129



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401
New Britain, Connecticut 06051
Phone: 827-7682

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Paulann H. Sheets
William H. Smith
Colin C. Tait

Joel M. Rinebold
Executive Director

Stanley J. Modzelesky
Executive Assistant

June 22, 1990

Metro Mobile CTS of Hartford, Inc.
100 Corporate Drive
Windsor, CT. 06095
Attn: Gary N. Shulman
Vice Pres. & Gen. Mgr.

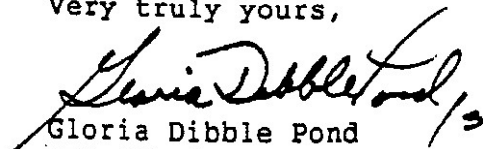
DOCKET NO. 129 - Metro Mobile CTS of Hartford, Inc.,
Certificate of Environmental Compatibility and Public Need
for the construction, maintenance, and operation of a
cellular telephone tower and associated equipment in the
Town of Manchester, Connecticut.

Dear Mr. Shulman:

At a meeting of the Connecticut Siting Council (Council)
on June 18, 1990, the Council considered and approved the
Development and Management (D&M) Plan for the Manchester
facility except for the subject of fencing to be reserved
for final approval by the Council at a later date.
Pursuant to Connecticut General Statutes Section 47-47, it
states that no barbed wire is permitted on an existing or
newly constructed fence. Enclosed for your reference is a
copy of the staff report for this D&M Plan.

This approval applies only to the Manchester facility.
Modifications to this D&M Plan require advance Council
notification and approval. The Council awaits your
submission of fencing plans, within State laws, that would
meet Metro Mobile's needs and the Town of Manchester's
requirements.

Very truly yours,


Gloria Dibble Pond
GDP:SJM:fc

Enclosures (3)

cc: Parties of Record
Council Members

4442E-5



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401
New Britain, Connecticut 06051
Phone: 827-7682

DOCKET NO. 129

METRO MOBILE CTS OF HARTFORD, INC.
D&M PLAN MANCHESTER CELL SITE - MAY 21, 1990

On May 15, 1990, Metro Mobile CTS of Hartford, Inc. submitted to the Connecticut Siting Council a D&M Plan for its Manchester cell site. The plan includes construction of a 128 foot tower including antennas, at a total height of 324 feet above mean sea level, and a 14-foot by 40-foot equipment building surrounded by an eight foot security fence. In addition, Metro Mobile would remove an existing one story wood building from the site. In accordance with Regulations of State Agencies Section 16-50j-77, Metro Mobile has notified the Council of its intention to begin access work and clearing, to be followed immediately by the construction of the tower and associated equipment upon approval of the D&M Plan by the Council.

The existing site is flat, paved, and surrounded by buildings and railroad tracks. All areas disturbed by construction will be repaved. The right-of-way from Pine Street over the existing parking lot will be maintained, and all new pavement will meet the minimum specifications required by the Town.

Metro Mobile proposes to construct the tower foundation and the building foundation as per manufacturer specifications, soil test boring logs, and detailed engineering. Underground grounding will be installed as per Metro Mobile's specifications. The tower has been moved within the site as far east as possible to separate the fall zone of the tower from a residence located southwest of the tower site.

In preparation of the D&M Plan, Metro Mobile consulted with the Town of Manchester pursuant to the Council's Decision and Order. The Manchester Zoning Enforcement Officer recommended installation of erosion controls prior to the disturbance of the site. Metro Mobile will abide by this recommendation through the installation and maintenance of approximately 85 linear feet of hay bales located along the west perimeter of the site. The Town of Manchester has also provided comments requesting provisions for landscaping, delineation of areas to be paved, details regarding modifications to the drainage

pattern, removal of barbed wire from the security fence, maintenance of the right-of-way, and installation of a driveway apron on Pine Street. Metro Mobile has responded indicating that it does not believe landscaping is appropriate or necessary, that all disturbed areas will be repaved, that drainage patterns will not be affected, that barbed wire on the security fence is necessary to provide security for its equipment, that the right-of-way will be maintained, and that the apron onto Pine Street will not be modified, but if it is, it will be restored as per Town requirements.

Staff recommends the approval of Town recommendations regarding erosion control, paving, and right-of-way maintenance. In addition, if dewatering is to be performed during site construction, the certificate holder must be prepared for proper disposal of water from dewatering operations.

No staff recommendations regarding site landscaping and the use of barbed wire in the security fence are made.

All other orders and provisions regarding the D&M Plan have been complied with.

JMR:bw

4442E



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401
New Britain, Connecticut 06051
Phone: 827-7682

DOCKET NO. 129
METRO MOBILE CTS OF HARTFORD, INC.
D&M PLAN MANCHESTER CELL SITE
June 18, 1990
Addendum

On Thursday, June 14, 1990, Brian Emerick of the Connecticut Siting Council (Council) and Fred Cunliffe of the Council staff met with David Malko of Metro Mobile and Stuart Popper of the Town of Manchester at the site of a telecommunications tower and building on Pine Street in Manchester, Connecticut.

The Town of Manchester recommends landscaping along the north and east sides of the leased parcel. White Pine or hemlock were preferred by the town. The town requests that the plantings be a minimum of four feet in height and four feet on center as required by town regulations. Metro Mobile would be willing to move the building and north-side of the fence several feet to the south and move the gate closer to the building to accommodate these plantings.

The town has requested that barbed wire not be used on the fence and have stated that the use of barbed wire on the fence is potentially inconsistent with Connecticut General Statutes section 47-47. No recommendations were made by the town or applicant for alternate fencing but Metro Mobile contends that security must be maintained.

Fred Cunliffe
Siting Analyst
4442E-4

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Sec. 47-46a. Payment for fence between agricultural property and property in control of environmental protection department. Where there is no fence between property used for agricultural purposes and adjoining property of the state under control of the department of environmental protection sufficient for the purposes of section 47-43, or when any fence so located is in need of replacement, and the boundary has been mutually agreed upon, the adjoining proprietor may, with the written agreement of the commissioner of environmental protection, executed within sixty days of a written request by such proprietor, cause such a fence to be constructed or replaced within six months of the date of the agreement; and the commissioner shall, within sixty days after the construction or replacement is completed, reimburse the proprietor for one-half the cost thereof, the state's share not to exceed four dollars a rod, payments to be made in the order of receipt of applications and completion of projects. Total payments under this section shall not exceed five thousand dollars in any fiscal year.

(1961, P.A. 558; 1967, P.A. 72; 1971, P.A. 872, S. 205, P.A. 79-530, S. 1, 3.)

History. 1967 act increased state's maximum share in reimbursement from one to two dollars per rod; 1971 act replaced state's maximum for total payments to reflect change from biennial to annual budget; P.A. 79-530 raised state's maximum share for reimbursement to four dollars per rod and raised maximum amount for total payments from twenty-five hundred to five thousand dollars per fiscal year.

Sec. 47-47. Barbed wire between adjoining premises or enclosing grounds of public buildings. No person shall use barbed wire in the construction of fences, or have barbed wire upon existing fences, between his own premises and those of an adjoining proprietor, within twenty-five rods of any house or barn belonging to such proprietor, unless either premises are used in connection with raising livestock, without first obtaining his written consent. No barbed wire shall be used in the construction of fences, or retained upon existing fences, connected with or enclosing the grounds of any public school or public building, except a department of transportation storage facility or a vessel operations area of a state-owned waterfront facility or aircraft operations area of a state-owned airport. Any person who violates any provision of this section shall be fined not more than one hundred dollars.

(1949 Rev. S. 7157; P.A. 80-105; P.A. 84-322.)

History. P.A. 80-105 added exception re premises used in raising livestock to provision requiring written consent for barbed wire fence within twenty-five rods of house or barn; P.A. 84-322 allowed use of barbed wire at department of transportation storage facilities, vessel operations areas of state-owned waterfront facilities and aircraft operations areas of state-owned airports.

See note to Sec. 47-48.

Sec. 47-48. Barbed wire along sidewalks. No barbed wire shall be installed along any sidewalk unless it is at least six and one-half feet above the ground. Any barbed wire in use in conformity with section 7156 of the general statutes, revision of 1949, on October 1, 1957, may be continued in use.

(1949 Rev. S. 7156; 1957, P.A. 157, S. 1.)

When violation of a statute concerning barbed wire is not set up in complaint in action for damages for personal injuries, it is to be read statute to the jury to show that legislature thought barbed wire a dangerous thing. 101 C. 549

Sec. 47-49. Purchase of division fence. If one proprietor or his predecessor in title makes the whole fence and the adjoining proprietor afterwards encloses his land, such adjoining proprietor shall purchase and maintain half of the divisional fence. If the parties do not agree in dividing and appraising it, either may call on the selectmen of the town in which such fence is situated, who may set out, to each, his proportion of such fence and determine how much shall be paid to the party erecting or owning the same by the other; a certificate of which determination, under the hands of the selectmen, shall be sufficient evidence for the recovery of the amount so determined. No action therefor shall be maintained unless the proprietor, who, or whose predecessor in title, first occupied his land and made the whole of

Date: December 13, 1989

Docket No. 129

LIST OF PARTIES AND INTERVENORS - SERVICE LIST

Status Granted	Status Holder (name, address & phone number)	Representative (name, address & phone number)
Party <input checked="" type="checkbox"/>	Metro Mobile CTS of Hartford, Inc. 100 Corporate Drive Windsor, CT 06095 Attn: Gary N. Schulman Vice President and Gen. Mgr.	Robinson & Cole One Commercial Plaza Hartford, CT 06103-3597 Attn: Earl W. Phillips, Jr. (203) 275-8200
Intervenor <input type="checkbox"/>		
Party <input type="checkbox"/>	SNET Cellular, Inc. 227 Church Street New Haven, CT 06506	Peter J. Tyrrell Senior Attorney SNET Cellular, Inc. 227 Church Street Room 1021 New Haven, CT 06506
Intervenor <input checked="" type="checkbox"/>		
Party <input checked="" type="checkbox"/>	Town of Manchester Planning & Zoning Comm. Town Hall 41 Center Street Manchester, CT 06040	Mark Pellegrini Director of Planning and Economic Development Town Hall 41 Center Street Manchester, CT 06040
Intervenor <input type="checkbox"/>		

Date: December 13, 1989

Docket No. 129

LIST OF PARTIES AND INTERVENORS - SERVICE LIST

Status Granted	Status Holder (name, address & phone number)	Representative (name, address & phone number)
Party <input checked="" type="checkbox"/>	Cheney Brothers National Historic Landmark District and Cheney National Historic Commission	Bruce J. Comollo Garrity, Diana, Conti & Houck 1091 Main Street Manchester, CT 06040 (203) 643-2181
Intervenor <input type="checkbox"/>		
Party <input type="checkbox"/>		
Intervenor <input type="checkbox"/>		
Party <input type="checkbox"/>		
Intervenor <input type="checkbox"/>		

DOCKET NO. 129 - AN APPLICATION OF : Connecticut Siting
METRO MOBILE CTS OF HARTFORD, INC., : Council
FOR A CERTIFICATE OF ENVIRONMENTAL :
COMPATIBILITY AND PUBLIC NEED FOR : March 12, 1990
THE CONSTRUCTION, OPERATION, AND :
MAINTENANCE OF A CELLULAR TELEPHONE
TOWER AND ASSOCIATED EQUIPMENT IN
THE TOWN OF MANCHESTER, CONNECTICUT.

FINDINGS OF FACT

1. Metro Mobile CTS of Hartford, Inc., in accordance with provisions of sections 16-50g to 16-50z of the Connecticut General Statutes (CGS), applied to the Connecticut Siting Council (Council) on September 29, 1989, for a Certificate of Environmental Compatibility and Public Need (Certificate) for the construction, maintenance, and operation of a telecommunications tower, associated equipment, and building to provide Domestic Public Cellular Radio Telecommunications Service (cellular service) in the Town of Manchester, part of the Hartford, Connecticut, New England County Metropolitan Area ("Hartford NECMA"). (Record)
2. The application was accompanied by proof of service as required by section 16-50l of the CGS. (Record)
3. Affidavit of newspaper notice as required by section 16-50l of the CGS was supplied by the applicant. Newspaper notice of this application was published twice by the applicant in The Hartford Courant. (Metro Mobile 1, pp.4-5, Exhibit 5)
4. The Council and its staff inspected the proposed and alternate sites in the Town of Manchester, Connecticut, on December 28, 1989. (Record)
5. Pursuant to section 16-50m of the CGS, the Council, after giving due notice thereof, held a public hearing on this application on December 28, 1989, at 3:30 P.M., and 7:00 P.M., at the Lincoln Center Hearing Room, 494 Main Street, Manchester, Connecticut. (Record)
6. The parties to the proceeding are the applicant and those persons and organizations whose names are listed in the Decision and Order which accompanies these Findings. (Record)
7. The Department of Environmental Protection (DEP) filed written comments with the Council pursuant to section 16-50j of the CGS. (Record)

8. In 1981, the Federal Communications Commission (FCC) recognized a national need for technical improvement, wide-area coverage, high quality service, and competitive pricing in mobile telephone service. (Metro Mobile 1, p.5; Docket 107, Finding of Fact 10)
9. The FCC has pre-empted State regulation in determining that a public need currently exists for cellular service, setting technical standards for that service, and establishing a competitive market. (Metro Mobile 1, p.6; Docket 107, Finding of Fact 12)
10. The FCC has determined that the public interest requires two licenses for cellular service be made available in each market area or NECMA to provide competition. One license is awarded to a wireline company, the other to a non-wireline company. (Metro Mobile 1, pp.6, 10; Docket 107, Finding of Fact 11)
11. Conventional mobile telephone service has been limited by insufficient frequency availability, inefficient frequency use, and poor quality of service. These limitations have resulted in congestion, blocking of transmission, interference, lack of coverage, and high costs. (Metro Mobile 1, p.5; Docket 107 Finding of Fact 9)
12. Cellular service consists of small, overlapping broadcast regions. These regions or cells are limited in coverage by the FCC's technical standards governing transmitting power. The system design provides frequency reuse and hand-off and would be capable of an orderly and compatible expansion. (Metro Mobile 1, pp.13-14, Exhibit 11, p.6)
13. Cell site locations are limited by a basic need for a 10 percent to 20 percent overlap of coverage between cell sites. Location of cell sites is essential to provide for uninterrupted hand-off of calls in progress. (Metro Mobile 1, Exhibit 11, pp.6-7)
14. Presently, the proposed cellular system represents state-of-the-art technology and Metro Mobile is aware of no viable alternatives. A mobile satellite service has been under consideration by the FCC and may become available in the distant future. (Metro Mobile 1, p.18)
15. Metro Mobile expects digital cellular technology to be commercially available in the late 1990's. The technology would increase the capability of handling calls over present cellular technology without having to add additional sites. (Tr. 12/28/89, pp.33-34)

16. In selecting a site for the cell, Metro Mobile found no available structures of adequate height or structural strength in or near a 0.6 mile theoretical search area within Manchester. (Metro Mobile 1, Exhibit 11, pp.8-9 and Attachment "A"; Metro Mobile 7)
17. Before selecting the proposed and alternate sites Metro Mobile considered and rejected four sites within the search area. One site in an industrial zone to the west of the alternate cell site location was rejected because of inadequate space for a cell site. A second area in a B1 and B2 business zone located along Hartford Road to the west of Prospect Street was rejected by Metro Mobile because land uses were mostly small businesses on shallow lots adjacent to high density residential development. A third area in a B2 business zone located along Center Street east and west of Pine Street was rejected because of adjacent high-density residential development. A fourth site in a B3 business zone located near the intersection of High Street and Pine Street was rejected because it was a small site surrounded by high-density multi-family dwellings. (Metro Mobile 1, Exhibit 11, pp.8-9 and Attachment "A"; Metro Mobile 3, Q.5, Attachment 2)
18. At the hearing, attention was brought to a site at the Town-owned Lincoln Center as a possible location for Metro Mobile's tower and equipment building. The site is one-tenth of a mile outside the search area at a ground elevation of 260 feet AMSL, and is in a residential zone. The site had no acceptable space to construct a tower or building. (Metro Mobile 7; Tr. 12/28/89)
19. The applicant had no communication with the Town of Manchester to share antennas or tower space on Metro Mobile's proposed tower at the time of the hearing. The Town had not shown interest in sharing tower space from the time of the hearing to the close of the record on February 15, 1990. (Tr. 12/28/89, pp.40, 111, 112; Record)
20. The proposed monopole could be designed to handle the Town of Manchester's police and fire antennas if the Town were interested. (Tr. 12/28/89, pp.105, 109)

21. The Town of Manchester's Planning and Zoning Commission, a party to the proceeding, stated that Metro Mobile's tower at the proposed site would be very obtrusive and potentially incompatible with surrounding zoning districts and land uses, while the tower at the alternate site would be very obtrusive and totally incompatible with the surrounding Historic and residential neighborhood. The Town was also disappointed that Metro Mobile focused on two locations in the center of the urbanized portion of Manchester. (Town of Manchester 1; Tr. 12/28/89, p.91)
22. Both the proposed and alternate sites would primarily provide additional cellular traffic handling capacity, as opposed to providing coverage to an area otherwise unserved. (Metro Mobile 1, p.10)
23. The proposed tower would primarily provide "off-loading" of calls from existing sites in Hartford, Vernon, and Glastonbury. (Metro Mobile 1, pp.10, 15-16, Exhibit 8, Exhibit 11, p.10; Metro Mobile 3, Q.12; Tr. 12/28/89, p.31)
24. The existing Hartford, Glastonbury, and Vernon sites have been in service for a little over two years. (Tr. 12/28/89, p.25)
25. The interrelationship of the traffic load between all of the sites in the area, not just one site, is causing the need for the proposed Manchester site. (Tr. 12/28/89, p.28)
26. The proposed site would also increase the quality of coverage in the Manchester area. (Tr. 12/28/89, pp.22, 23)
27. At the time of installation of the proposed Manchester facility, all existing sites in the area, including the Manchester site, would be fully sectorized. Such sectorization provides for increased call handling capacity within a cell by dividing the geographic service area into six directional sectors which allows for additional frequency reuse. Even with sectorization, the projected cellular traffic demands and frequency reuse requirements necessitate location of a site within the Manchester area. Operation of the proposed facility would off load the existing sites and improve coverage to the Manchester area. (Metro Mobile 3, Q.7, Q.11, Q.12, Q.13; Tr. 12/28/89, p.26)
28. The proposed site would increase the total cellular capacity in the Manchester area by up to 3,600 calls per hour. (Metro Mobile 4, Q.26)

29. With the addition of the proposed Manchester site, potential frequency interference problems from the Vernon, Glastonbury, and Hartford sites would be limited by a reassignment of frequencies recognizing their coverage areas and overlap. (Metro Mobile 3, Q.8)
30. The Vernon and Glastonbury sites are currently omnidirectional sites which normally could accommodate approximately 45 channels and handle approximately 1,200 calls during the peak hour, however, because of a potential frequency separation problem due to the addition of new sites and the sectorization of surrounding sites, the Vernon and Glastonbury sites could only accommodate approximately 30 channels or 800 calls during the peak hour. Hartford is a sectorized site that can accommodate 12 to 15 channels in each of its six sectors which can handle approximately 3,600 calls or 600 calls per sector during the peak hour. (Metro Mobile 3, Q.10; Tr. 12/28/89, pp.20, 27-29)
31. The Vernon site currently handles approximately 250 calls during the peak hours and approximately 175 calls per hour averaged over a 12-hour business day from 7:00 a.m. to 7:00 p.m. The peak hour occurs during the afternoon on weekdays. (Metro Mobile 3, Q.14; Tr. 12/28/89, pp.26-27)
32. The Glastonbury site currently handles approximately 300 calls during the peak hours and approximately 250 calls per hour averaged over a 12-hour business day from 7:00 a.m. to 7:00 p.m. The peak hour occurs during the afternoon on weekdays. (Metro Mobile 3, Q.14; Tr. 12/28/89, pp.26-27)
33. The Hartford site currently handles approximately 2,225 calls from all six sectors during the peak hours and approximately 1,610 calls per hour averaged over a 12-hour business day from 7:00 a.m. to 7:00 p.m. The peak hour occurs during the afternoon on weekdays. (Metro Mobile 3, Q.14)

34. Sector three of the existing Hartford cell site is currently exceeding its 600 call per hour maximum call handling capacity during its peak hour. This sector covers parts of Hartford, East Hartford, and Glastonbury. The proposed Manchester site would provide relief to this sector. Sector five, the next busiest sector of the Hartford cell site, covers West Hartford and is also approaching its 600 call per hour capacity. A sector is the area within a 60 degree arc with sector one being between a vector starting at zero degrees and ending at 60 degrees, sector two between 60 degrees and 120 degrees, sector three between 120 degrees and 180 degrees, sector four between 180 degrees and 240 degrees, sector five between 240 degrees and 300 degrees, and sector six between 300 degrees and 360 degrees. (Metro Mobile 3, Q.15; Metro Mobile 4, Q.24; Tr. 12/28/89, p.21)
35. Without the proposed Manchester site, additional Hartford site sectors and the existing Vernon and Glastonbury cell sites would begin to exceed their maximum call handling capacity during 1990. No call projection data was provided, but Metro Mobile contends that the Vernon and Glastonbury sites could handle approximately twice the current demand. (Metro Mobile 3, Q.15; Metro Mobile 4, Q.24, Q.25, Q.27; Tr. 12/28/89, pp.30-31, 32; Record)
36. The proposed cellular site would be a triangular 7,600 square foot parcel of land located in the rear of a larger, 1.35 acre lot at 266 Center Street, Manchester, Connecticut. The remainder of the lot is used for storage and manufacturing. The proposed tower would be located approximately 12 feet west of an abutting property owned by Kenneth C. Burkamp, which has a metal storage shed on-site, and approximately 25 feet south of a manufacturing building owned by S. Mark Stephens, lessor of the site. The proposed tower would be located approximately 260 feet south of Center Street and approximately 140 feet east of the nearest residential building. (Metro Mobile 1, Exhibit 1, p.1; Metro Mobile 3, Q.6, Attachment 3; Tr. 12/28/89, pp.15-16, 17, 18)
37. Access to the proposed site would be over an existing driveway on land of an adjacent property owner (Kenneth C. Burkamp) and land of the lessor (S. Mark Stephens). Vehicular access over the adjacent property is permitted by a non-exclusive right of passage granted to the lessor. (Metro Mobile 1, p.9, Exhibit 1, p.1; Metro Mobile 3, Q.3)

38. Metro Mobile proposes to construct a 115-foot self-supporting monopole tower to which two platforms would be attached. Two 15-foot omnidirectional call-processing, whip transmit antennas would be mounted at 113 feet on the corners of the platform with six 11 1/2-foot transmit/receive antennas side mounted with center of radiation at 106 feet. The total height of the tower with antennas would be 128 feet above ground level. (Metro Mobile 1, Exhibit 1, p.8; Tr. 12/28/89, pp.18, 19, 77, 78)
39. The horizontal off-set of the antennas placed on the corners of the platform would be a maximum of 6 1/2 feet from the tower structure. (Tr. 12/28/89, p.78)
40. Ground elevation at the proposed site is 196 feet AMSL. Residential properties in the immediate area on Pine Street, Park Street, and New Street from where the tower would be visible are at an elevation ranging from 198 feet to 220 feet. (Tr. 12/28/89, pp.15-16, 17; Town of Manchester 1, pp.2-3)
41. Metro Mobile would raze an abandoned wood-frame building and construct a 20-foot by 40-foot single-story, prefabricated concrete building on the proposed site. The building would house receiving, transmitting, switching, processing, performance monitoring, and climate control equipment. The abandoned building could not be utilized for equipment because it is in poor condition, and the owner wanted it razed as part of the lease arrangement. (Metro Mobile 1, p.9; Metro Mobile 3, Q.2)
42. The alternate site would be on a 50-foot by 85-foot parcel of land located in the northern portion of a larger 1.1 acre lot at 218 Hartford Road, Manchester, Connecticut. The remainder of the lot is used for manufacturing. The proposed tower would be approximately 141 feet west of Prospect Street, approximately 44 feet west of an on-site two story brick manufacturing building, 46 feet south of Hartford Road, 120 feet east of abutting property also owned by S. Mark Stephens, and 120 feet north of land owned by Millbridge Hollow Condominiums. (Metro Mobile 1, Exhibit 2, p.1; Metro Mobile 3, Q.6, Attachment 3; Tr. 12/28/89, p.18; Town of Manchester 1, pp.3-4)
43. The southern boundary of the alternate site lot is 60 feet from the northern edge of Hop Brook. (Town of Manchester 1, p.4)
44. Access to the alternate site would be over an existing driveway and parking lot on land of the lessor (S. Mark Stephens). (Metro Mobile 1, Exhibit 1, p.9, Exhibit 2, pp.1, 7; Metro Mobile 3, Q.6, Attachment 3)

45. The alternate site tower would consist of a 140-foot self-supporting tower to which two platforms would be attached. Two 15-foot omnidirectional call-processing, whip transmit antennas would be mounted at 138-feet on the corners of the platform with six 11 1/2-foot transmit/receive antennas side mounted with center of radiation at 131 feet. The total height of the alternate site tower with antennas would be 153 feet above ground level. (Metro Mobile 1, p.8; Exhibit 2, p.8; Tr. 12/28/89, p. 78)
46. Ground elevation at the alternate site would be at 170 feet AMSL. (Tr. 12/28/89, p.18)
47. A 20-foot by 40-foot single story building would be constructed on the alternate site. The building would house the same equipment as the proposed site. (Metro Mobile 1, p.9)
48. Minimal site leveling or backfilling would be required at the proposed site. Removal of an on-site dirt pile would be required at the alternate site. (Metro Mobile 1, Exhibit 1, p.7, Exhibit 2, p.7; Tr. 12/28/89, p.18)
49. Utility lines for the proposed site would be routed from Center Street to the proposed cell site over land of the lessor. Utility lines for the alternate site would be routed from existing utility poles along Hartford Road to the alternate site. (Metro Mobile 1, p.9, Exhibit 1, p.1, Exhibit 2, p.1, Exhibit 9, pp. 1, 11; Tr. 12/28/89, p.88)
50. The metal storage shed east of the site on adjacent property owned by Kenneth C. Burkamp, a one-story brick manufacturing building on the lessor's property, and property west of the site owned by Kenneth C. Burkamp would be within the fall zone of the proposed site tower. Hartford Road, land owned by the Millbridge Hollow Condominiums, and a two-story brick manufacturing building on property of the lessor would be within the fall zone of the alternate site tower. The fall zones would not be totally within the lessor's properties. (Town of Manchester 1, p.2; Metro Mobile 3, Q.6, Attachment 3)

51. The zoning of the proposed cellular site is I, Industrial. This zone is approximately three acres in size and is surrounded to the north by a Business zone, to the east and west by Residential zones, and to the south by the Cheney Brothers National Historic Landmark District. The proposed tower would be a use requiring a special exception under Manchester zoning regulations. The zoning of the alternate cellular site is H, Historical, and is within the Cheney Brothers National Historic Landmark District. The alternate tower would be a use requiring a special exception under Manchester zoning regulations. (Town of Manchester 1, p.2; Metro Mobile 1, Exhibit 11, Attachment "A"; Metro Mobile 3, Q.5, Attachment 2)
52. The Cheney Brothers National Historic Landmark District was established in 1978 through a designation by the United States Department of the Interior, and is listed in the National Register of Historic Places. (Town of Manchester 1, pp.3-4; Tr. 12/28/89, p.59)
53. Metro Mobile does not have any existing towers within a national landmark district. (Tr. 12/28/89, p.59)
54. Within the Cheney Brothers District north of the alternate site are rehabilitated mill buildings used for multi-family dwellings and some neighborhood commercial purposes. Within the Cheney Brothers District east of the alternate site are buildings used for commercial purposes. To the west of the alternate site lot is property in an industrial zone used for commercial purposes. (Town of Manchester 1, pp.3-4)
55. The proposed site would be less than 200 feet north of the Cheney Brothers Historic District. (Town of Manchester 1, p.5; Metro Mobile 3, Q.5, Attachment 2)
56. There are approximately 159 residences within a 1,000-foot radius of the proposed tower. The nearest residence is 140 feet southwest of the proposed property. There are approximately 24 residences, six condominium buildings, and two apartment buildings within a 1,000-foot radius of the alternate cell site. The nearest residence is 180 feet from the alternate tower. (Metro Mobile 1, Exhibit 1, p.7, Exhibit 2, p.7, Exhibit 9, p.12; Tr. 12/28/89, pp.17-18, 103)

57. The electromagnetic radio frequency power density at the proposed and alternate sites, assuming all channels operating simultaneously at maximum allowable power and broadcasting from the lowest set of antennas would be 0.1124 milliwatts per square centimeter (mW/cm²) at the proposed site and 0.0737 mW/cm² at the alternate site, and would be well below the American National Standards Institute standard of 2.92mW/cm², as adopted by the State in CGS 22a-162. (Metro Mobile 1, p.12, Exhibit 9, pp.2, 12; DEP comments of 12/14/89; Tr. 12/28/89, p.19)
58. Both the proposed and alternate towers would be designed to withstand pressure equivalent to a 90 mph wind with a 1/2-inch solid ice accumulation in accordance with Electronic Industries Association standard RS-222-D. The overturn moment for the foundation would be 1.5. The antenna mounting arrangement, the support brackets, and the antenna structure would be designed to withstand 125 mph winds. (Metro Mobile 1, Exhibit 1, p.9, Exhibit 2, p.9; Tr. 12/28/89, pp.82-83, 87)
59. According to the Connecticut Historical Commission, "the prime site,..., does not appear to meet the eligibility criteria for the National Register of Historic Places, while the alternate site,...does appear to be of local historic and architectural significance. Therefore, we recommend that the proposed telecommunications tower and associated equipment shelter be constructed at the 266 Center Street [prime] site." (Metro Mobile 3, Q.1, Attachment 1)
60. There are no known extant populations of Connecticut "Species of Special Concern" or Federal Endangered and Threatened Species that occur at the site in question. (Metro Mobile 3, Q.1, Attachment 1; DEP Comments of 12/14/89)
61. The total estimated cost of construction for the proposed site is as follows:
- | | |
|-------------------------------------|------------|
| Radio equipment | \$676,500 |
| Tower and antennas | 38,800 |
| Power system | 18,000 |
| Building | 76,600 |
| Miscellaneous | 140,200 |
| (Site preparation and installation) | |
| TOTAL | \$950,100. |
- (Metro Mobile 1, pp.16-17, Exhibit 1, p.9)

62. The total estimated cost of construction for the alternate site is as follows:

Radio equipment	\$676,500
Tower and antennas	41,760
Power system	18,000
Building	76,600
Miscellaneous	135,200
(Site preparation and installation	

TOTAL \$948,060.

(Metro Mobile 1, p.17, Exhibit 2, p.9)

JAW

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DOCKET NO. 129 - AN APPLICATION OF : Connecticut Siting
METRO MOBILE CTS OF HARTFORD, INC., : Council
FOR A CERTIFICATE OF ENVIRONMENTAL :
COMPATIBILITY AND PUBLIC NEED FOR : March 12, 1990
THE CONSTRUCTION, OPERATION, AND :
MAINTENANCE OF A CELLULAR TELEPHONE :
TOWER AND ASSOCIATED EQUIPMENT IN :
THE TOWN OF MANCHESTER, CONNECTICUT.

O P I N I O N

On September 29, 1989, Metro Mobile CTS of Hartford, Inc., (Metro Mobile) applied to the Connecticut Siting Council (Council) for a Certificate of Environmental Compatibility and Public Need (Certificate) to construct, maintain, and operate a cellular telecommunications tower, associated equipment, and building in the Town of Manchester, Connecticut.

A determination of public need for cellular telephone service has been pre-empted by the Federal Communications Commission (FCC). Under Connecticut State law, the Council must balance the need to develop the proposed site as a cellular telephone facility with the need to protect the environment, including public health and safety.

In finding a proposed tower site, an applicant must locate a site or existing tower to share, offering the necessary coverage that would not have a substantial effect on the environment and be adequately distant from wetlands, public recreation areas, and adjacent homes. Because Metro Mobile does not have the authority to take land through eminent domain, acquisition of a site requires consent of the property owners to lease or sell the property. These requirements restrict the number of potential tower sites within defined search areas.

The proposed or alternate site would function as a secondary cellular facility, located near the intersection of three existing, primary cellular facilities in Hartford, Glastonbury, and Vernon, Connecticut. Cellular service demand is exceeding the call-handling capacity of Sector three in Hartford and is soon expected to exceed the call-handling capacity of the facilities in Glastonbury and Vernon. The proposed Manchester site would provide additional overlapping coverage between these three cells for the continuous transfer of calls in the Hartford-Glastonbury-Vernon region, in which there are presently weak signals and interference. The proposed and alternate sites would provide similar coverage and call-handling capability throughout the area.

The proposed site would be leased and developed in the rear of a privately owned 1.35 acre lot located at 266 Center Street. The proposed 128-foot, self-supporting monopole tower and antenna structure would be located approximately 12 feet west of Kenneth C. Burkamp's property and 140 feet east of the nearest residential building. The fall zone of the tower could encompass a metal storage shed on Kenneth C. Burkamp's property east of the site; a one-story brick manufacturing building on the lessor's property; and a portion of the adjacent property that the nearest residential building is located on, west of the site. Metro Mobile would raze an abandoned wood-frame building and construct a single story equipment building, measuring 20 feet by 40 feet, on the site. Vehicle access to the proposed site would be over an existing driveway on land of Kenneth C. Burkamp and land of the lessor permitted by a non-exclusive right of passage granted by Kenneth C. Burkamp to the lessor. Utilities from Center Street would be available to the facility. Minimal site leveling or backfilling would be required at the site.

The alternate site would be leased and located on the northern boundary of a 1.1 acre lot at 218 Hartford Road. The 153-foot, self-supporting monopole tower and antenna structure would be located 46 feet south of Hartford Road and 120 feet north of land owned by Millbridge Hollow Condominiums. The fall zone of the alternate tower could encompass Hartford Road, land owned by the Millbridge Hollow Condominiums, and a two-story brick manufacturing building on the lessor's lot. A single story equipment building, measuring 20 feet by 40 feet, would be constructed on the site. Vehicle access to the cell site would be over an existing driveway and parking lot on land of the lessor. Utilities from existing utility poles along Hartford Road would be routed to the facility. Removal of an on-site dirt pile would be required:

Electromagnetic radio frequency power density is a health and safety concern of the Council. However, the power density level measured at the base of the proposed tower would be 0.1124 milliwatts per square centimeter (mW/cm^2), and at the base of the alternate tower it would be $0.0737 \text{ mW}/\text{cm}^2$. These power densities are well below the American National Standards Institute (ANSI) safety standard of $2.92 \text{ mW}/\text{cm}^2$, as adopted by the State in Connecticut General Statutes Section 22a-162. The power density would rapidly decrease as distance from the tower increases.

No wetlands or watercourses exist at either site. No water flow and/or quality changes would be expected to result from the construction and operation of either the proposed or the alternate facilities.

There are no existing records of federally endangered or threatened species or Connecticut species of special concern occurring in the area of the proposed or alternate sites, according to the latest available information from the Connecticut Department of Environmental Protection Natural Resources Center.

The proposed facility is located near a historical zone. However, this historical zone is also a highly urbanized area that consists of industrial and commercial uses. There is no reason to believe that the proposed tower would have any significant effect on the zone. Furthermore, the State Historical Commission has stated that there would be no significant effect on the State's historic and architectural resources at the proposed site.

Moreover the Council believes that the industrial and urban nature of the proposed site lends itself to a commercial use such as the proposed cellular telecommunications tower. Visually, the tower will be acceptable with the site and surrounding land uses. Furthermore, the height of the tower is not so great that it will be visually obtrusive in the immediate area to adjacent residential units, or for any significant distance to the community in general.

The intrusion of the fall zone on adjacent structures and property should be avoided whenever possible to maintain a reasonable setback from other land uses. Nonetheless, the close proximity of tall urban structures on small urban sites make this goal impractical if not impossible. Although the Council will require the tower to be shifted the greatest distance possible from adjacent properties and structures to enhance the site, there is insufficient reason to deny the proposed site due to the location of the tower in relation to the adjacent land uses, properties, and structures.

In comparison, the alternate site tower would be 25 feet taller and located within the historic zone. Consequently it is the opinion of the Council that the proposed site is superior, and the alternate site should be denied.

Based on its record in this proceeding, the Council is of the opinion that the effects associated with the construction, operation, and maintenance of a cellular tower and associated equipment building at the proposed site, including the effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildlife are not significant either alone or cumulatively with other effects, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application for the proposed site.

The Council will require Metro Mobile to submit a Development and Management (D&M) plan for approval prior to the commencement of any construction at the proposed site. This D&M plan shall include detailed plans of the site preparation with the final tower height in relation to the site elevation, and placement of the tower as great a distance as possible from abutting properties.

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DOCKET NO. 129 - AN APPLICATION OF : Connecticut Siting
METRO MOBILE CTS OF HARTFORD, INC., : Council
FOR A CERTIFICATE OF ENVIRONMENTAL :
COMPATIBILITY AND PUBLIC NEED FOR : March 12, 1990
THE CONSTRUCTION, OPERATION, AND :
MAINTENANCE OF A CELLULAR TELEPHONE
TOWER AND ASSOCIATED EQUIPMENT IN
THE TOWN OF MANCHESTER, CONNECTICUT.

DECISION AND ORDER

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council finds that the effects associated with the construction, operation, and maintenance of a cellular telephone facility at the proposed Manchester site, including effects on the natural environment; ecological integrity and balance; forests and parks; air and water purity; and fish and wildlife are not significant either alone or cumulatively with other effects, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application, and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by Section 16-50k of the General Statutes of Connecticut (CGS), be issued to Metro Mobile CTS of Hartford, Inc., for the construction, operation, and maintenance of a cellular telecommunications tower, associated equipment, and building at the proposed site in Manchester, Connecticut.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The monopole tower including antennas and associated equipment shall not exceed a height of 128 feet above ground level, 324 feet AMSL.
2. The facility shall be constructed in accordance with the State of Connecticut Basic Building Code.
3. The Certificate Holder shall prepare a Development and Management (D&M) plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of State Agencies. The D&M plan shall include detailed plans of the site preparation with a soil boring report; plans, design details, and specifications for the tower foundation; and a site plan with placement of the tower as far removed from abutting properties and structures as possible.
4. The Certificate Holder shall prepare the D&M plan in consultation with the Town of Manchester which may provide its comments to the Council within 20 days of submission to the Town.

5. The Certificate Holder shall comply with any future radio frequency (RF) standard promulgated by State or federal regulatory agencies. Upon the establishment of any new governmental RF standards, the facility granted in this Decision and Order shall be brought into compliance with such standards.
6. The Certificate Holder shall provide the Council a recalculated report of power density if and when additional channels over the proposed 90 channels, higher wattage over the proposed 100 watts per channel, or if other circumstances in operation cause a change in power density above the levels originally calculated in the application.
7. The Certificate Holder shall permit public or private entities to share space on the tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
8. If this facility does not initially provide, or permanently ceases to provide cellular service following the completion of construction, this Decision and Order shall be void, and the tower and all associated equipment in this application shall be dismantled and removed or reapplication of any new use shall be made to the Council before any such new use is made.
9. Unless otherwise approved by the Council, this Decision and Order shall be void if construction authorized herein is not completed within three years of the effective date of this Decision and Order.


Pursuant to Section 16-50p of the CGS, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below. A notice of issuance shall be published in the Hartford Courant and Journal Inquirer.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of State Agencies.

CERTIFICATE
OF
ENVIRONMENTAL COMPATIBILITY AND PUBLIC NEED
DOCKET NO. 129

Pursuant to section 16-50k of the General Statutes of Connecticut, as amended, the Connecticut Siting Council hereby issues a Certificate of Environmental Compatibility and Public Need to Metro Mobile CTS of Hartford, Inc., for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telephone tower and associated equipment at the proposed primary site in the Town of Manchester, Connecticut. This Certificate is issued in accordance with and subject to the terms and conditions set forth in the Decision and Order of the Council on March 12, 1990.

By order of the Council,


Gloria Dibble Pond, Chairperson

March 12, 1990

Exhibit B

Property Card

266R CENTER STREET

Location 266R CENTER STREET

Mblu 62/ 1020/ 266/ /

Acct# 102000266R

Owner CROWN ATLANTIC CO LLC

Assessment \$115,000

Appraisal \$164,200

PID 2635

Building Count 1

DISTRICT T

CONCRETE

Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2016	\$82,000	\$82,200	\$164,200

Assessment			
Valuation Year	Improvements	Land	Total
2016	\$57,500	\$57,500	\$115,000

Owner of Record

Owner CROWN ATLANTIC CO LLC
PMB 353-806372
Address 4017 WASHINGTON ROAD
MCMURRAY, PA 15317

Sale Price \$0
Certificate C
Book & Page 2071/ 309
Sale Date 04/19/1999
Instrument 25

Ownership History

Ownership History					
Owner	Sale Price	Certificate	Book & Page	Instrument	Sale Date
CROWN ATLANTIC CO LLC	\$0	C	2071/ 309	25	04/19/1999
CELCO PARTNERSHIP	\$0		1923/ 202	25	10/16/1997
METRO MOBILE	\$0		1382_142		04/01/1990

Building Information

Building 1 : Section 1

Year Built:
Living Area: 0
Replacement Cost: \$0
Replacement Cost
Less Depreciation: \$0

Building Attributes


Field	Description
Style	Outbuildings
Model	
Grade:	
Stories:	
Occupancy	
Exterior Wall 1	
Exterior Wall 2	
Roof Structure:	
Roof Cover	
Interior Wall 1	
Interior Wall 2	
Interior Flr 1	
Interior Flr 2	
Heat Fuel	
Heat Type:	
AC Type:	
Total Bedrooms:	
Total Bthrms:	
Total Half Baths:	
Total Xtra Fixtrs:	
Total Rooms:	
Bath Style:	
Kitchen Style:	
Extra Kitchens	
Whirlpool	
Fireplace	
Fin Basement	
Fin Bsmnt Qual	
Fin Bsmnt 2	
Fin Bsmnt2 Qual	
Bsmnt Garage	
SFA Code	

Building Photo



(<http://images.vgsi.com/photos2/ManchesterCTPhotos//\00\02\4>)

Building Layout

 Building Layout

(<http://images.vgsi.com/photos2/ManchesterCTPhotos//Sketches>)

Building Sub-Areas (sq ft)	Legend
No Data for Building Sub-Areas	

Extra Features

Extra Features	Legend
No Data for Extra Features	

Land**Land Use**

Use Code 302
Description Ind Vac
Zone IND
Neighborhood 4500
Alt Land Appr Category No

Land Line Valuation

Size (Acres) 0.17
Frontage 0
Depth 0
Assessed Value \$57,500
Appraised Value \$82,200

Outbuildings

Outbuildings						Legend
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
FN4	Fence 8' Chain			264 L.F.	\$4,000	1
PAV1	Paving Asphalt			14000 S.F.	\$17,500	1
SHDT	Telephone Shed			720 S.F.	\$59,400	1
LT1	Lights 1Fix			2 UNITS	\$800	1
PAV2	Paving Concrete			12 S.F.	\$300	1

Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2015	\$85,100	\$82,200	\$167,300
2010	\$81,400	\$86,500	\$167,900
2005	\$71,100	\$61,800	\$132,900

Assessment			
Valuation Year	Improvements	Land	Total
2015	\$59,600	\$57,500	\$117,100
2010	\$57,000	\$60,600	\$117,600
2005	\$49,900	\$43,300	\$93,200

Exhibit C

Construction Drawings



VERIZON SITE NUMBER: 1904
VERIZON SITE NAME: MANCHESTER CT
SITE TYPE: MONOPOLE
TOWER HEIGHT: 115'-0"

BUSINESS UNIT #: 806372
SITE ADDRESS: 266R CENTER STREET
COUNTY: HARTFORD
JURISDICTION: TOWN OF MANCHESTER

VERIZON LTE



VERIZON SITE NUMBER: 1904
BU #: 806372
HRT 093 943228
266R CENTER STREET
MANCHESTER, CT 06040
EXISTING 115'-0" MONOPOLE



DRAWING INDEX

SHEET #	TITLE DESCRIPTION
T-1	TITLE SHEET
T-2	GENERAL NOTES
G-1	SITE PLAN
G-2	TOWER ELEVATION & ANTENNA PLANS
G-3	EQUIPMENT SCHEDULES
G-4	EQUIPMENT DETAILS
G-5	EQUIPMENT DETAILS
G-6	GROUNDING DETAILS
G-7	GROUNDING DETAILS

ALL DRAWINGS CONTAINED HEREIN ARE FORAMTTED FOR THE CONSTRUCTION OF THE WORK. THE CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

APPROVALS

APPROVAL	SIGNATURE	DATE
STATE ACQUISITION		
CONSTRUCTION		
RADIO		
MOBILWAVE		
TELCO		
EQUIPMENT		
PROJECT ADMINISTRATOR		
PROJECT ENGINEER		
PROJECT MANAGER		
CROWN CASTLE USA INC SIGNATURE BLOCK		
APPROVAL	SIGNATURE	DATE
STATE ACQUISITION		
CONSTRUCTION		
PLANNER		
PROJECT MANAGER		
CROWN CASTLE USA INC SIGNATURE BLOCK		
LANDFORD		

SITE INFORMATION

GROWN CASTLE USA INC.
 SITE NAME: HRT 093 943228
 SITE ADDRESS: 266R CENTER STREET, MANCHESTER, CT 06040
 COUNTY: HARTFORD
 MAP/Parcel #: MANCHESTER 060400026
 AREA OF CONSTRUCTION: EXISTING
 LANG CODE: 4300
 LAYING TYPE: 72 41 48 50
 NAD83
 GROUND ELEVATION: 197 FT
 CLIMATE ZONING: IND
 JURISDICTION: TOWN OF MANCHESTER
 OCCUPANCY CLASSIFICATION: U
 TYPE OF CONSTRUCTION: U
 A.D.A COMPLIANCE: FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION
PROPERTY OWNER: M STEPHENS CO LLC, 218 HARTFORD ROAD, MANCHESTER, CT 06040
TOWER OWNER: GROWN ATLANTIC COMPANY LLC, 2000 CORPORATE DRIVE, GAINESBURG, VA 15117
CARRIER/APPLICANT: VERIZON WIRELESS NETWORK REAL ESTATE, 20 ALEXANDER DRIVE, 2ND FLOOR, WALLINGFORD, CT 06492
ELECTRIC PROVIDER: CONNECTICUT LIGHT & POWER CO (800) 266-2000
TELCO PROVIDER: AT&T (866) 626-6900

PROJECT TEAM

AREA FIRM: GROWN CASTLE USA INC, 2000 CORPORATE DRIVE, GAINESBURG, VA 15117, CONTACT: JASON D'AMICO - CONSTRUCTION MANAGER (813) 265-5044
GROWN CASTLE USA INC DISTRICT CONTACTS: WILLIAM GATES - PROJECT MANAGER (313) 265-5044, JASON D'AMICO - CONSTRUCTION MANAGER (813) 265-5044
VERIZON CONTACT: ANDREW LEONE, ALEONE@STRUCTURECONNECTING.NET

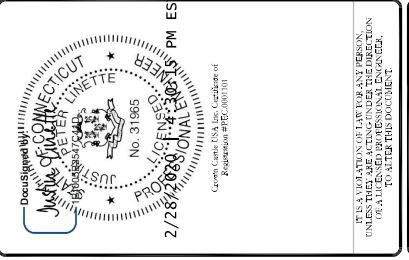
APPLICABLE CODES/REFERENCE DOCUMENTS

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL LEGAL AUTHORITY UNLESS OTHERWISE NOTED. THESE PLANS IS TO BE CONSTRUCTED TO MEET THE FOLLOWING APPLICABLE CODES, NOT LIMITED TO THESE CODES:
 BUILDING 2018 CT STATE BUILDING CODE 2015 IBC W/ CT AMENDMENTS
 MECHANICAL 2018 CT STATE BUILDING CODE 2015 IBC W/ CT AMENDMENTS
 ELECTRICAL 2018 CT STATE BUILDING CODE 2017 NEC W/ CT AMENDMENTS
REFERENCE DOCUMENTS:
 STRUCTURE ANALYSIS: PAUL J. FORD AND COMPANY, DATED: JANUARY 22, 2020
 MOUNT ANALYSIS: PAUL J. FORD AND COMPANY, DATED: JANUARY 21, 2020
 REDS REVISED: 9/11/2019, ORDER ID: 511445, REVISION: 0
 CALL CROWN CASTLE USA INC (800) 922-4455 (313) 265-5044
 CALL WORKING DATES RETURN FOR DEL:

PROJECT DESCRIPTION

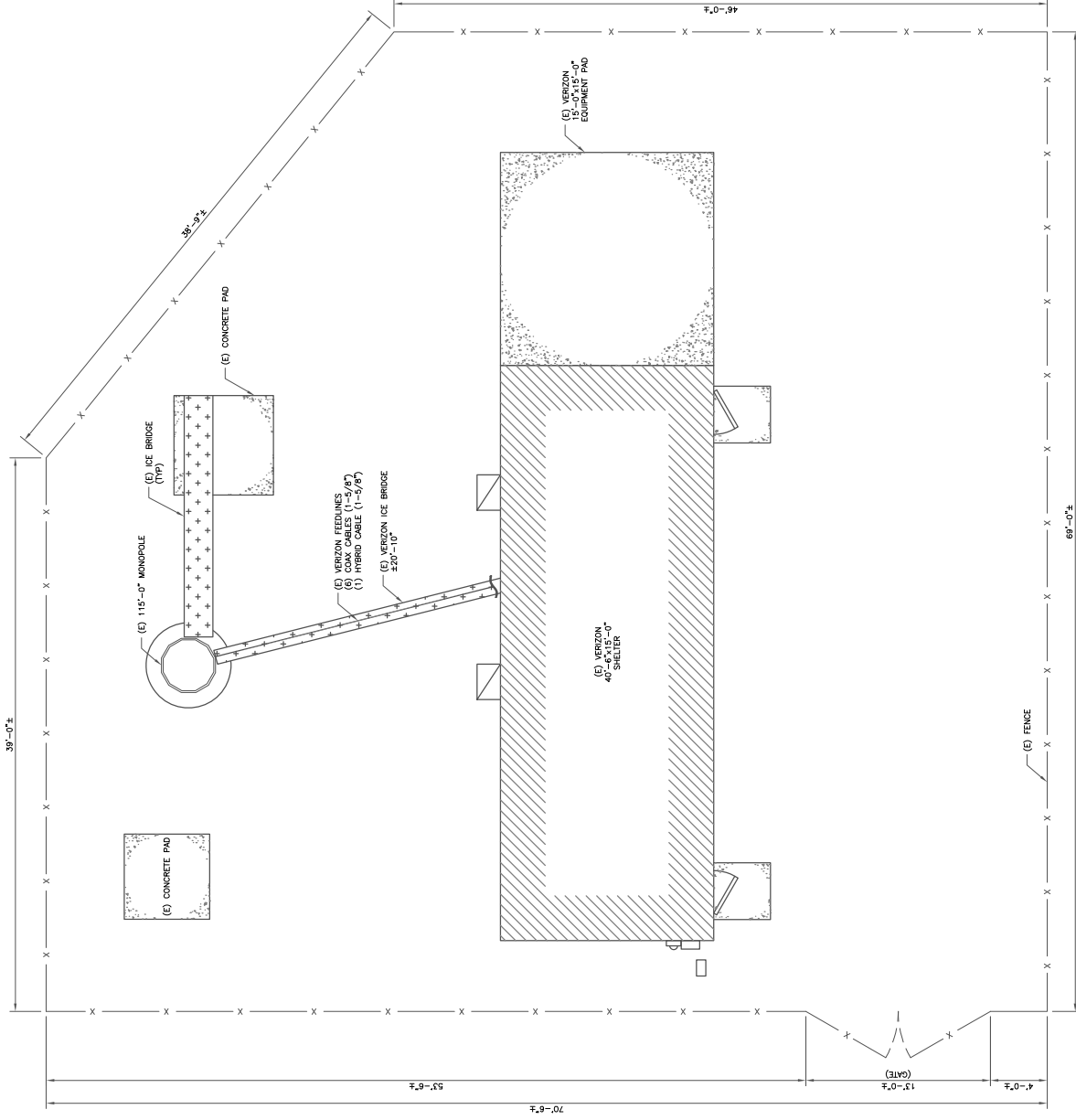
THE PURPOSE OF THIS PROJECT IS TO ENHANCE BROADBAND CONNECTIVITY AND CAPACITY TO THE EXISTING ELIGIBLE WIRELESS FACILITY.
TOWER SCOPE OF WORKS:
 • REPAIR OF EXISTING ANTENNAS
 • INSTALL (6) ANTENNAS
 • INSTALL MOUNT MODIFICATION PER MOUNT ANALYSIS BY PAUL J. FORD AND COMPANY, DATED JANUARY 21, 2020
 • NONE
GROUND SCOPE OF WORKS:
 • NONE
INSTALLER NOTE:
 ALL WORK SHALL BE ADDED TO THE MOUNT MODIFICATION PER MOUNT ANALYSIS BY PAUL J. FORD AND COMPANY DATED JANUARY 21, 2020.
NOTE:
 PRIOR TO ACCESSING/ENTERING THE SITE YOU MUST CONTACT THE CROWN NOC AT (800) 788-7011 & CROWN CONSTRUCTION MANAGER

REV#	DATE	ISSUED FOR:	DESCRIPTION	DESIGN
1	02/24/20	EA	CONSTRUCTION	EA
1	02/24/20	EA	CONSTRUCTION	EA



SHEET NUMBER:	REVISION:
T-1	1

ALL PLANS SHALL BE IN ACCORDANCE WITH THE LATEST EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL LEGAL AUTHORITY UNLESS OTHERWISE NOTED. THESE PLANS IS TO BE CONSTRUCTED TO MEET THE FOLLOWING APPLICABLE CODES, NOT LIMITED TO THESE CODES:



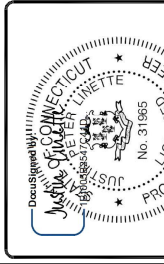
20 ALEXANDER DRIVE, 2ND FLOOR
WALLINGFORD, CT 06492



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

VERIZON SITE NUMBER: 1904
BU #: 806372
HRT 093 943228
260R CENTER STREET
MANCHESTER, CT 06040
EXISTING 115'-0" MONOPOLE

REV.	DATE	BY	DESCRIPTION	CHKD.
1	02/28/20	EA	CONSTRUCTION	CJL
1	02/28/20	EA	CONSTRUCTION	FE



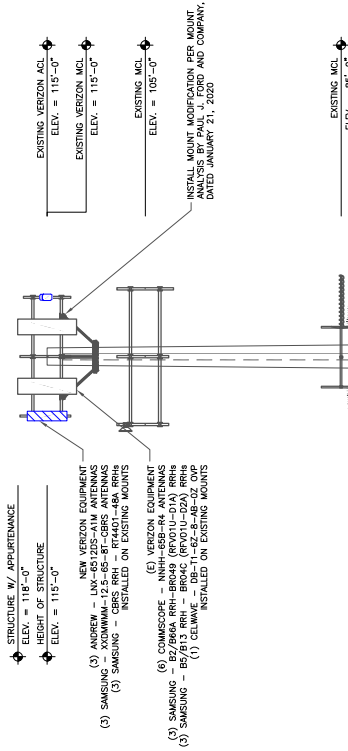
2/28/2020 1:00 PM EST
James Peter Gimette
Professional Engineer
Registration #PEJ0001018

THESE PLANS OR ANY PART THEREOF ARE NOT VALID UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER. NO PART BE LOANED OR REPRODUCED.

SHEET NUMBER: **C-1** REVISION: **1**



1 SITE PLAN
SCALE: 1/8" = 1'-0" (PLANS)
1/4" = 1'-0" (DETAILS)



- STRUCTURE W/ APRURTEANCE
ELEV. = 118'-0"
- HEIGHT OF STRUCTURE
ELEV. = 115'-0"
- (3) ANDREW - LNK-65-205-ATM ANTENNAS
- (3) SAMSUNG - B2/BB6A RRR-BR049 (RPV01U-D1A) RRRs
(3) SAMSUNG - B2/BB6A RRR-BR049 (RPV01U-D1A) RRRs
(1) CEILING - INSTALLED ON EXISTING MOUNTS
- (6) COMSCOPE - (E) VERIZON EQUIPMENT
- (3) SAMSUNG - B2/BB6A RRR-BR049 (RPV01U-D1A) RRRs
- (3) SAMSUNG - B2/BB6A RRR-BR049 (RPV01U-D1A) RRRs
(1) CEILING - INSTALLED ON EXISTING MOUNTS

VERIZON EQUIPMENT
ANTENNA CL: 115'-0"
MOUNT CL: 115'-0"

EXISTING MCL
ELEV. = 85'-0"

EXISTING VERIZON MCL
ELEV. = 115'-0"

EXISTING VERIZON MCL
ELEV. = 115'-0"

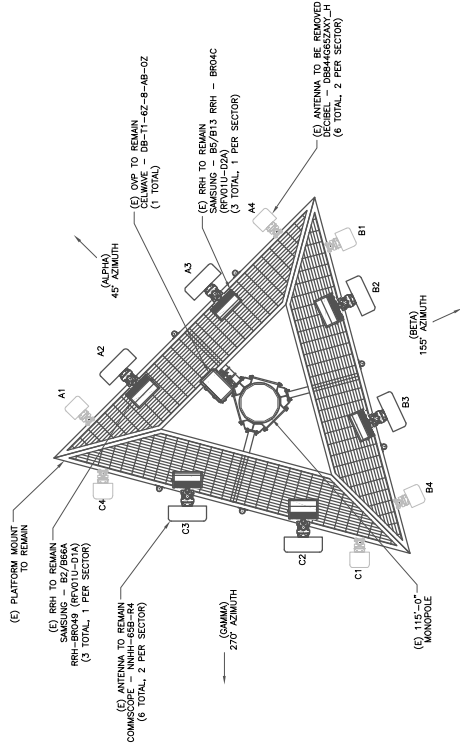
EXISTING MCL
ELEV. = 105'-0"

INSTALL MOUNT MODIFICATION PER MOUNT
ANALYSIS BY PAUL J. FORD AND COMPANY,
DATED JANUARY 21, 2020

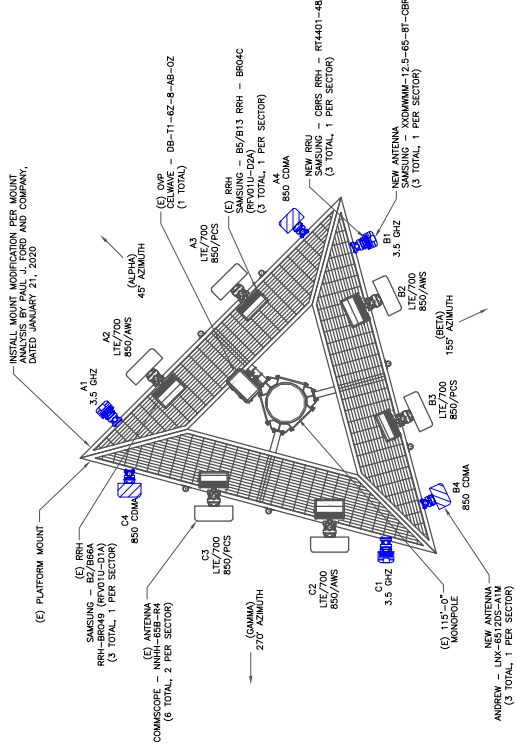
- (3) VERIZON PERMANENT
- (6) COAX CABLES (1-5/8")
- (1) HYBRID CABLE (1-5/8")

(E) 115'-0" MONOPOLE

1 TOWER ELEVATION
SCALE: NOT TO SCALE



2 EXISTING ANTENNA PLAN
SCALE: NOT TO SCALE



3 NEW ANTENNA PLAN
SCALE: NOT TO SCALE



201 ALEXANDER DRIVE, 2ND FLOOR
WALLINGFORD, CT 06492



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

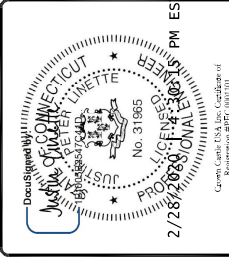
VERIZON SITE NUMBER: 1904

BU #: 806372
HRT 093 943228

260R CENTER STREET
MANCHESTER, CT 06040

EXISTING 115'-0" MONOPOLE

REV	DATE	DRWN	DESCRIPTION	CHKD/QC
1	02/24/20	EA	CONSTRUCTION	CJL
2	02/24/20	EA	CONSTRUCTION	JL



2/28/2020 12:43:05 PM EST
James J. Peter, P.E.
Professional Engineer
State of Connecticut
License No. 31865

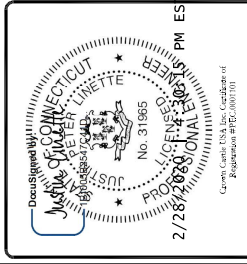
PER THE TERMS OF THE PROFESSIONAL ENGINEERING AGREEMENT, THESE PLANS ARE VALID ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED HEREIN. ANY OTHER USE OF THESE PLANS IS PROHIBITED.

SHEET NUMBER: C-2
REVISION: 1



VERIZON SITE NUMBER: 1904
 BU #: 806372
 HRT 093 943228
 260R CENTER STREET
 MANCHESTER, CT 06040
 EXISTING 115'-0" MONOPOLE

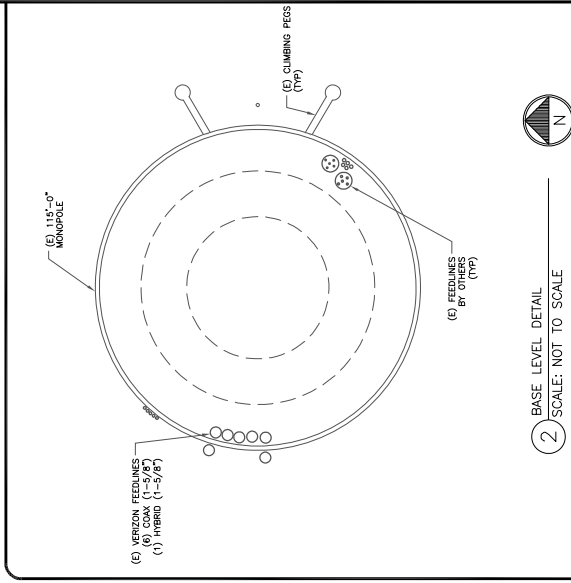
REV	DATE	DESCRPTION	PREPARED BY
1	02/28/20	EA CONSTRUCTION	CJL
2	02/28/20	EA CONSTRUCTION	JL



2/28/20 2:00 PM EST
 State of Connecticut
 PROFESSIONAL ENGINEER
 No. 31965
 James J. Conecticut
 1000 Main Street, Suite 100
 Wallingford, CT 06492

SHEET NUMBER: **C-3**
 REVISION: **1**

STATUS	CABLE TYPE	SIZE	LENGTH	QTY
EXISTING	COAX	1-5/8"	185'-0" \pm	6
EXISTING	HYBRID	1-5/8"	185'-0" \pm	1
TOTAL CABLE QTY:				7



② BASE LEVEL DETAIL
 SCALE: NOT TO SCALE

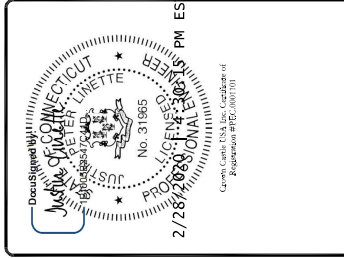
SECTOR	STATUS	ANTENNA MANUFACTURER	ANTENNA MODEL	ANTENNA CENTERLINE	AZIMUTH	MCHANICAL DOWN TILT	ELECTRICAL DOWN TILT	TOWER EQUIPMENT MANUFACTURER	TOWER EQUIPMENT QTY/MODEL
A1	NEW	ANDREW	LWK-651205-A1M	115'-0"	45°	0'	2'	CELWAVE	(1) DB-T1-6Z-SAB-0Z
A2	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	45°	0'	5/5/2'	NOKIA	(1) B2/B6EA RRH-BR049 (RFV01U-D1A)
A3	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	45°	0'	5/5/2'	NOKIA	(1) B5/B13 RRH-BR04C (RFV01U-D2A)
A4	NEW	SAMSUNG	XDDMM-12.5-65-8T-CBR5	115'-0"	45°	0'	8'	SAMSUNG	(1) CBR5 RRH-RT4401-48A
B1	NEW	ANDREW	LWK-651205-A1M	115'-0"	155°	0'	1'	-	-
B2	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	155°	0'	7/7/4'	NOKIA	(1) B2/B6EA RRH-BR049 (RFV01U-D1A)
B3	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	155°	0'	7/7/4'	NOKIA	(1) B5/B13 RRH-BR04C (RFV01U-D2A)
B4	NEW	SAMSUNG	XDDMM-12.5-65-8T-CBR5	115'-0"	155°	0'	8'	SAMSUNG	(1) CBR5 RRH-RT4401-48A
C1	NEW	ANDREW	LWK-651205-A1M	115'-0"	270°	0'	4'	-	-
C2	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	270°	0'	6/6/4'	NOKIA	(1) B2/B6EA RRH-BR049 (RFV01U-D1A)
C3	EXISTING	COMSCOPE	NNH-65B-R4	115'-0"	270°	0'	6/6/4'	NOKIA	(1) B5/B13 RRH-BR04C (RFV01U-D2A)
C4	NEW	SAMSUNG	XDDMM-12.5-65-8T-CBR5	115'-0"	270°	0'	8'	SAMSUNG	(1) CBR5 RRH-RT4401-48A

① VERIZON TOWER EQUIPMENT SCHEDULE
 SCALE: NOT TO SCALE



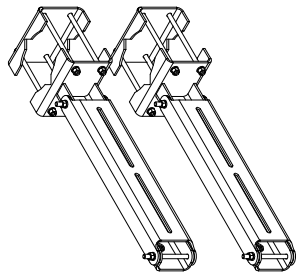
VERIZON SITE NUMBER: 1904
 BU #: 806372
 HRT 093 943228
 266R CENTER STREET
 MANCHESTER, CT 06040
 EXISTING 115'-0" MONOPOLE

REV.	DATE	BY	DESCRIPTION	CHK'D BY
1	02/28/20	EA	CONSTRUCTION	JL
2	02/28/20	EA	CONSTRUCTION	JL



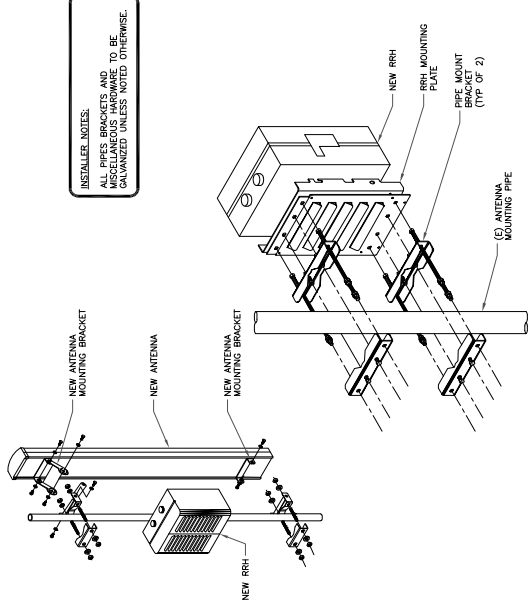
FOR ALL WORKS IN THE STATE OF CONNECTICUT, THESE DRAWINGS AND SPECIFICATIONS SHALL BE UNDER THE DIRECTION AND SUPERVISION OF A LICENSED PROFESSIONAL ENGINEER OR ARCHITECT.

SHEET NUMBER: C-4
 REVISION: 1



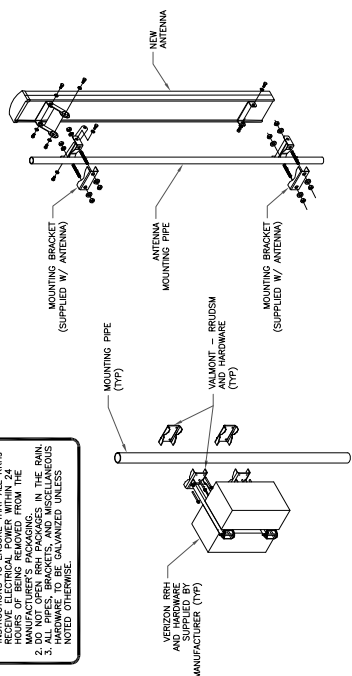
1 VALMONT - RRUDSM
 DUAL SWIVEL MOUNT KITS FOR RRUs
 (2 SWIVEL MOUNTS PER KIT)

2 VALMONT - RRUDSM
 SCALE: NOT TO SCALE



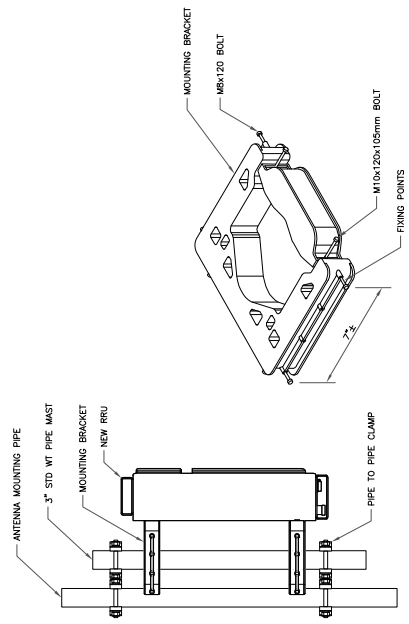
INSTALLER NOTES:
 ALL PIPES BRACKETS AND MISCELLANEOUS HARDWARE TO BE GALVANIZED UNLESS NOTED OTHERWISE.

3 ANTENNA & RRU MOUNTING DETAIL
 SCALE: NOT TO SCALE

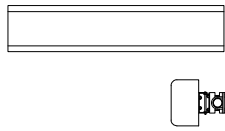


INSTALLER NOTES:
 1. FOLLOW MANUFACTURER'S INSTRUCTIONS TO ENSURE THAT ALL RRUs RECEIVE ELECTRICAL POWER WITHIN 24 HOURS OF INSTALLATION FROM THE MANUFACTURER'S PACKAGING.
 2. DO NOT OPEN RRU PACKAGES IN THE RAIN.
 3. ALL HARDWARE TO BE GALVANIZED UNLESS NOTED OTHERWISE.

4 ANTENNA WITH RRUs MOUNTING DETAIL
 SCALE: NOT TO SCALE

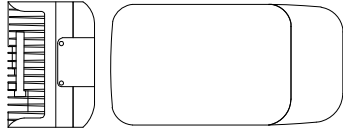


5 NOKIA - FPKA BRACKET MOUNTING DETAIL
 SCALE: NOT TO SCALE



ANDREW - LNX-6512DS-A1M
 WEIGHT (WITHOUT MOUNTING HARDWARE): 28.7 LBS
 MOUNTING HARDWARE P/N: DR380-3 & DR50830
 RATED WIND VELOCITY: 149.8 MPH

1 NOT USED
 SCALE: NOT TO SCALE



SAMSUNG - CBR5
 WEIGHT (FULLY EQUIPPED): 23.14 LBS
 SIZE (HxWxD): 16.6x11.3x9.45 IN.

2 SAMSUNG - CBR5
 SCALE: NOT TO SCALE

3 NOT USED
 SCALE: NOT TO SCALE



VERIZON SITE NUMBER: 1904

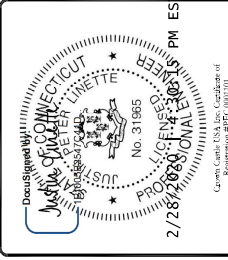
BU #: 806372
 HRT 093 943228

266R CENTER STREET
 MANCHESTER, CT 06040

EXISTING 115'-0" MONOPOLE

ISSUED FOR:

REV	DATE	BY	DESCRIPTION	CHK'D BY
1	01/29/20	EA	CONSTRUCTION	FE
1	02/24/20	EA	CONSTRUCTION	FE



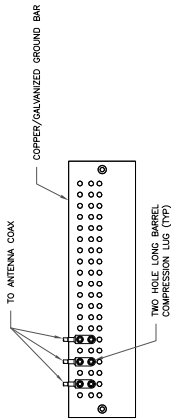
THESE DRAWINGS OR INFORMATION CONTAINED HEREIN ARE THE PROPERTY OF CROWN CASTLE AND ARE TO BE USED ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED HEREON.

SHEET NUMBER: C-5
 REVISION: 1

6 NOT USED
 SCALE: NOT TO SCALE

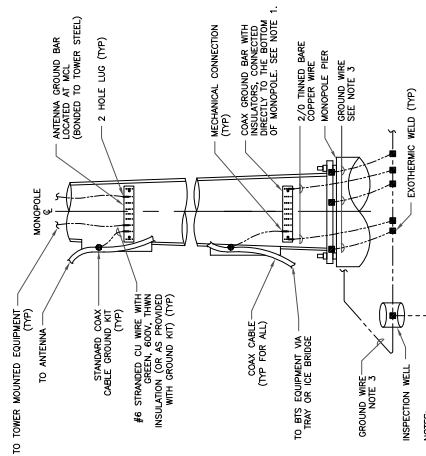
5 NOT USED
 SCALE: NOT TO SCALE

4 NOT USED
 SCALE: NOT TO SCALE



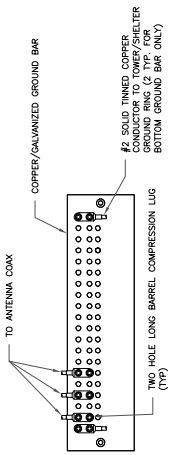
- NOTES:
1. DOUBLING UP "OR STACKING" OF CONNECTIONS IS NOT PERMITTED.
 2. EXTERIOR ANTIOXIDANT JOINT COMPOUND TO BE USED ON ALL EXTERIOR CONNECTIONS.
 3. GROUND BAR SHALL NOT BE ISOLATED FROM TOWER, MOUNT DIRECTLY TO ANTENNA MOUNT STEEL.

① ANTENNA SECTOR GROUND BAR DETAIL
SCALE: NOT TO SCALE



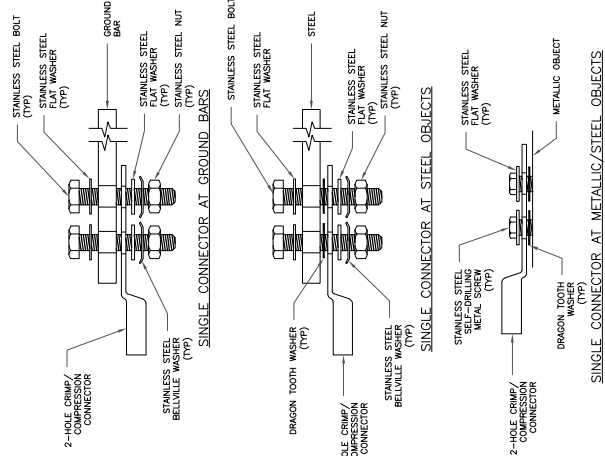
- NOTES:
1. NUMBER OF MONOPOLES VARY PER DESIGN ON THE FACE OF TOWER. ANTENNA DOWNLEADS AND CONNECTION OBSERVATION COAX CABLES EXCEEDING 200 FEET ON THE TOWER SHALL HAVE GROUND RITS AT THE MIDPOINT. PROVIDE AS REQUIRED.
 2. ONLY MECHANICAL CONNECTIONS ARE ALLOWED TO GROWN CASTLE USA INC. TOWERS. ALL MECHANICAL CONNECTIONS SHALL BE TREATED WITH AN ANTI-OXIDANT COATING.
 3. ALL TOWER GROUNDING SYSTEMS SHALL COMPLY WITH THE REQUIREMENTS OF THE RECOGNIZED EDITION OF ANSI/TIA 222 AND NFPA 78B.

④ TYPICAL ANTENNA CABLE GROUNDING
SCALE: NOT TO SCALE

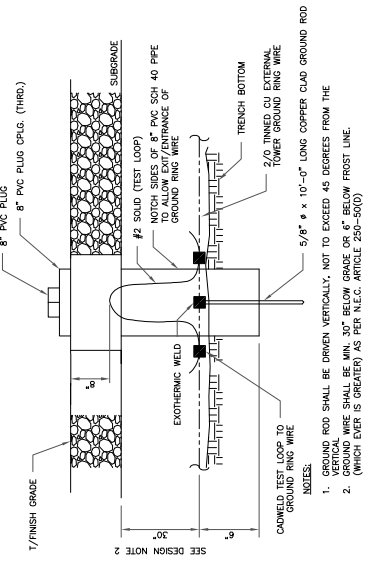


- NOTES:
1. EXTERIOR ANTIOXIDANT JOINT COMPOUND TO BE USED ON ALL EXTERIOR CONNECTIONS.
 2. GROUND BAR SHALL NOT BE ISOLATED FROM TOWER, MOUNT DIRECTLY TO TOWER STEEL (TOWER ONLY).
 3. GROUND BAR SHALL BE ISOLATED FROM BUILDING OR SHELTER.

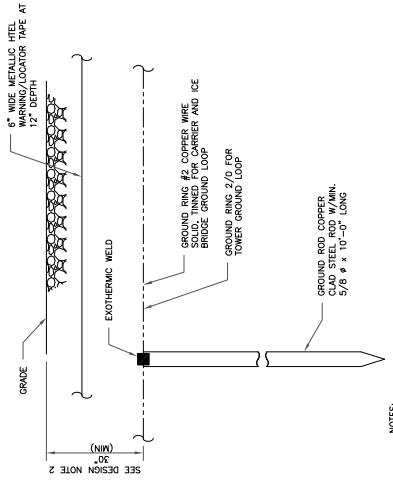
② TOWER/SHELTER GROUND BAR DETAIL
SCALE: NOT TO SCALE



⑤ HARDWARE DETAIL FOR EXTERIOR CONNECTIONS
SCALE: NOT TO SCALE



③ INSPECTION WELL DETAIL
SCALE: NOT TO SCALE



⑥ GROUND ROD DETAIL
SCALE: NOT TO SCALE



VERIZON SITE NUMBER: 1904

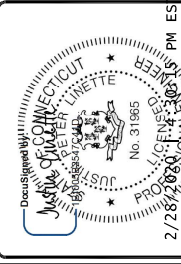
BU #: 806372
HRT 093 943228

260R CENTER STREET
MANCHESTER, CT 06040

EXISTING 115'-0" MONOPOLE

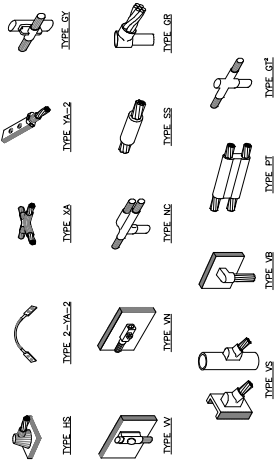
ISSUED FOR:

REV.	DATE	DESCRIPTION	REVISED BY
1	01/29/20	EA	CONSTRUCTION
2	02/24/20	EA	CONSTRUCTION
3			



THIS DRAWING IS THE PROPERTY OF CROWN CASTLE. IT IS TO BE USED ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED HEREON. IT IS NOT TO BE REPRODUCED OR COPIED IN ANY MANNER WITHOUT THE WRITTEN PERMISSION OF CROWN CASTLE.

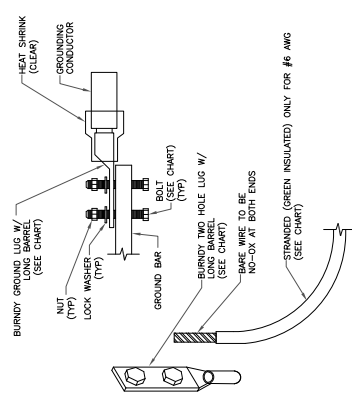
SHEET NUMBER: G-1
REVISION: 1



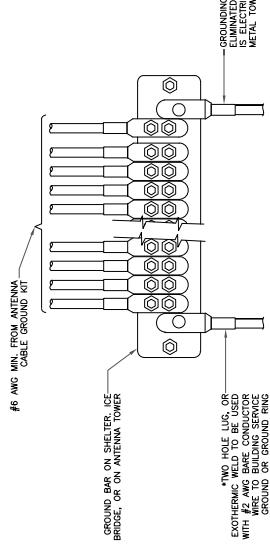
NOTE:
 1. BEND SYSTEMS "WILD FIRE" SHOWN HERE ARE EXAMPLES. CONSULT WITH CONSTRUCTION MANAGER FOR SPECIFIC WELDS TO BE USED FOR THIS PROJECT.
 2. WELD TYPE ONLY TO BE USED BELOW GRADE WHEN CONNECTING GROUND RING TO GROUND ROD.

1 CADWELD GROUNDING CONNECTIONS
 SCALE: NOT TO SCALE

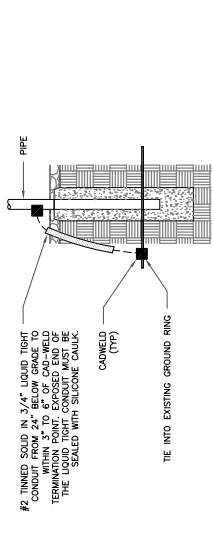
WIRE SIZE	BURNED LUG	BOLT SIZE
#6 AWG GREEN INSULATED	YA6C-2TC3B	3/8" - 16 NC S 2 BOLT
#2 AWG SOLID TINNED	YA3C-2TC3B	3/8" - 16 NC S 2 BOLT
#2 AWG STRANDED	YA2C-2TC3B	3/8" - 16 NC S 2 BOLT
#2/0 AWG STRANDED	YA28-2N	1/2" - 16 NC S 2 BOLT



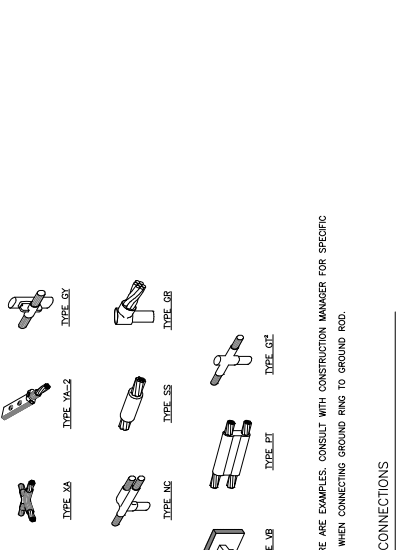
NOTES:
 1. ALL GROUNDING LUGS ARE TO BE INSTALLED PER MANUFACTURER'S SPECIFICATIONS. ALL HARDWARE BOLTS, NUTS, LOCK WASHERS SHALL BE STAINLESS STEEL. ALL FLAT WASHERS, BOLTS, FLAT WASHERS AND NUTS.
 2. MECHANICAL LUG CONNECTION
 SCALE: NOT TO SCALE



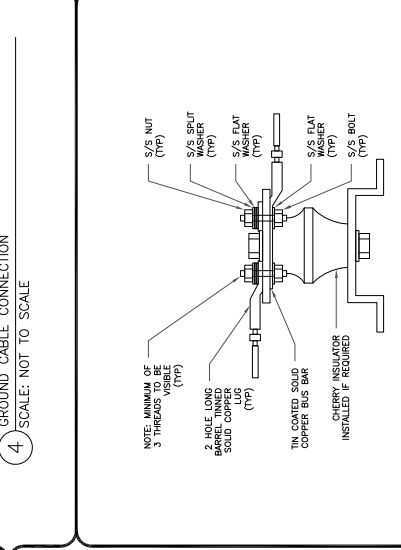
NOTES:
 1. TWO-HOLE LUG, OR EXOTHERMIC WELD TO BE USED WITH #2 AWG BARE CONDUCTOR GROUND OR GROUND RING.
 2. TINNED SOLID IN 3/4" UNID. THICK CONDUCTOR SHALL BE USED TO TERMINATION POINT. EXPOSED END OF THE WIRE SHALL BE SEaled WITH SILICONE CAULK.
 3. GROUNDWIRE INSTALLATION
 SCALE: NOT TO SCALE



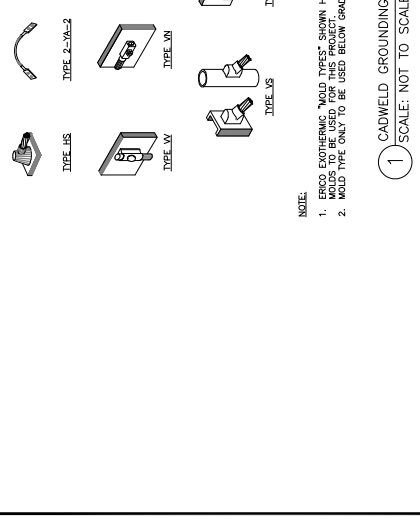
NOTES:
 1. DOWN LEAD (HOME RUN) CONDUCTORS ARE NOT TO BE INSTALLED ON CROWN CASTLE USA INC. TOWERS. PER THE GROUNDING DOWN CONDUCTOR POLICY (GAS-57P-10091, NO CAD-WELDING ON THE TOWER AND/OR IN THE AIR ARE NOT PERMITTED.
 2. OMT INSULATOR WHEN MOUNTING TO TOWER STEEL OR PLATFORM STEEL. USE INSULATORS WHEN ATTACHING TO BUILDING OR SHELTERS.
 3. GROUND BAR DETAIL
 SCALE: NOT TO SCALE



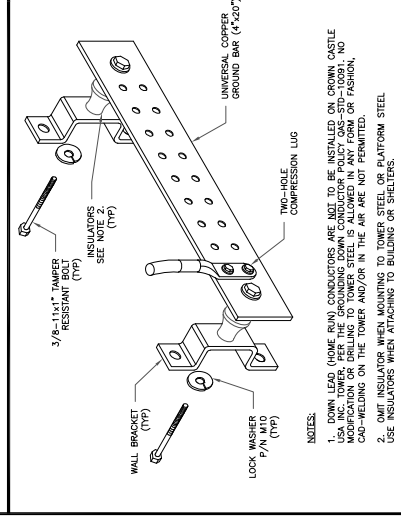
NOTES:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO ANTENNA GROUND BAR.
 2. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT. COLD SHRINK SHALL NOT BE USED.
 3. CABLE GROUND KIT CONNECTION
 SCALE: NOT TO SCALE



NOTES:
 1. DOWN LEAD (HOME RUN) CONDUCTORS ARE NOT TO BE INSTALLED ON CROWN CASTLE USA INC. TOWERS. PER THE GROUNDING DOWN CONDUCTOR POLICY (GAS-57P-10091, NO CAD-WELDING ON THE TOWER AND/OR IN THE AIR ARE NOT PERMITTED.
 2. OMT INSULATOR WHEN MOUNTING TO TOWER STEEL OR PLATFORM STEEL. USE INSULATORS WHEN ATTACHING TO BUILDING OR SHELTERS.
 3. GROUND BAR DETAIL
 SCALE: NOT TO SCALE



NOTES:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.
 2. GROUNDING KIT SHALL BE TYPE AND PART NUMBER AS SUPPLIED OR RECOMMENDED BY CABLE MANUFACTURER.
 3. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT. COLD SHRINK SHALL NOT BE USED.
 4. CABLE GROUND KIT CONNECTION
 SCALE: NOT TO SCALE

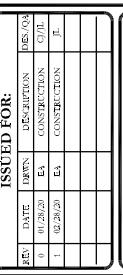


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 3. GROUND BAR DETAIL
 SCALE: NOT TO SCALE



VERIZON SITE NUMBER: 1904
 BU #: 806372
 HRT 093 943228
 260R CENTER STREET
 MANCHESTER, CT 06040
 EXISTING 115'-0\"/>

REV.	DATE	ISSUED FOR:	DESCRIPTION	REV. Q3
1	02/28/20	EA	CONSTRUCTION	01
2	02/28/20	EA	CONSTRUCTION	02



PROJECT: VERIZON 1904
 SHEET NUMBER: G-2
 REVISION: 1

Exhibit D

Structural Analysis Report

Date: **January 21, 2020**

Amanda D Brown
Crown Castle
6325 Ardrey Kell Rd. Suite 600
Charlotte, NC 28277

Paul J. Ford and Company
250 East Broad St., Suite 600
Columbus, OH 43215
614-221-6679

Subject: **Structural Analysis Report**

Carrier Designation: **Verizon Wireless Co-Locate**
Carrier Site Number: 1904
Carrier Site Name: Manchester CT

Crown Castle Designation: **Crown Castle BU Number:** 806372
Crown Castle Site Name: HRT 093 943228
Crown Castle JDE Job Number: 598729
Crown Castle Work Order Number: 1823106
Crown Castle Order Number: 511445 Rev. 0

Engineering Firm Designation: **Paul J. Ford and Company Project Number:** 37520-0127.002.7805

Site Data: **266R Center Street, MANCHESTER, Hartford County, CT**
Latitude 41° 46' 19", Longitude -72° 31' 48.8"
115 Foot - Monopole Tower

Dear Amanda D Brown,

Paul J. Ford and Company is pleased to submit this "**Structural Analysis Report**" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC5: Proposed Equipment Configuration

Sufficient Capacity (53.7%)

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Respectfully submitted by:


Aaron E. Pike, E.I.
Structural Designer
apike@pauljford.com



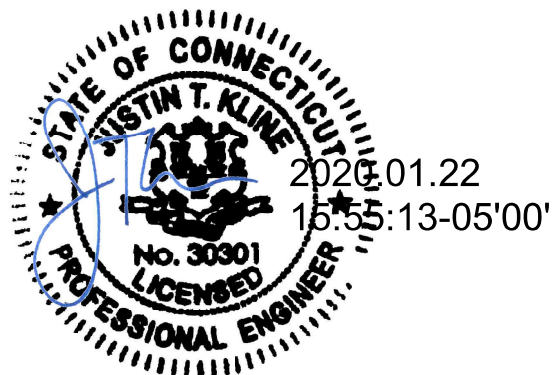


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1) INTRODUCTION

This tower is a 115 ft Monopole tower designed by VALMONT in May of 1990.

2) ANALYSIS CRITERIA

TIA-222 Revision:	TIA-222-H
Risk Category:	II
Wind Speed:	125 mph
Exposure Category:	B
Topographic Factor:	1
Ice Thickness:	2 in
Wind Speed with Ice:	50 mph
Service Wind Speed:	60 mph

Table 1 - Proposed Equipment Configuration

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
115.0	115.0	3	andrew	LNx-6512DS-A1M w/ Mount Pipe	7	1-5/8
		6	commscope	NNHH-65B-R4 w/ Mount Pipe		
		1	rfs celwave	DB-T1-6Z-8AB-0Z		
		3	samsung telecommunications	20W CBRS		
		3	samsung telecommunications	CBRS w/ Mount Pipe		
		3	samsung telecommunications	RFV01U-D1A		
		3	samsung telecommunications	RFV01U-D2A		
		1	tower mounts	Miscellaneous [NA 507-1]		
		1	tower mounts	Platform Mount [LP 712-1_KCKR]		

Table 2 - Other Considered Equipment

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
105.0	107.0	2	andrew	VHLP1-23	5	1/2
		1	andrew	VHLP2-23	5	5/16
	105.0	1	tower mounts	Platform Mount [LP 602-1]	5	1/4
85.0	85.0	2	tower mounts	Side Arm Mount [SO 701-1]	5	13/32
		1	wade antenna	WH14-69/S		
	84.0	3	wade antenna	WL 14-69/S		
	78.0	2	tower mounts	Side Arm Mount [SO 701-1]		
		1	wade antenna	J105-HI		

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	Testwell Craig Laboratories of CT, Inc, 04/12/1990	262174	CCISites
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	FDH Engineering, 10-06100E N1, 06/21/2010 (Mapping)	2668863	CCISites
4-TOWER MANUFACTURER DRAWINGS	Valmont, DC03902, 05/01/1990	262172	CCISites

3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) The foundation drawings were not available at the time of this analysis. Therefore, we have assumed the material yield strengths (F'_c and F_y) as per the following:
 - a) Concrete: 3000 PSI
 - b) Foundation Reinforcing: ASTM A615 Gr 60
- 5) At the time of analysis, the referenced geotechnical report did not provide definitive values for the soil properties. The soil properties were estimated off the boring logs.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	115 - 72.3334	Pole	TP30.45x21.91x0.219	1	-9.40	1269.02	38.8	Pass
L2	72.3334 - 29.3334	Pole	TP38.61x29.0779x0.313	2	-16.32	2300.73	43.6	Pass
L3	29.3334 - 0	Pole	TP43.85x36.8508x0.375	3	-24.88	3224.57	44.0	Pass
							Summary	
						Pole (L3)	44.0	Pass
						Rating =	44.0	Pass

Table 5 - Tower Component Stresses vs. Capacity – LC5

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	38.1	Pass
1	Base Plate	0	24.0	Pass
1	Base Foundation Steel	0	38.8	Pass
1	Base Foundation Soil Interaction	0	53.7	Pass
Structure Rating (max from all components) =				53.7%

Notes:

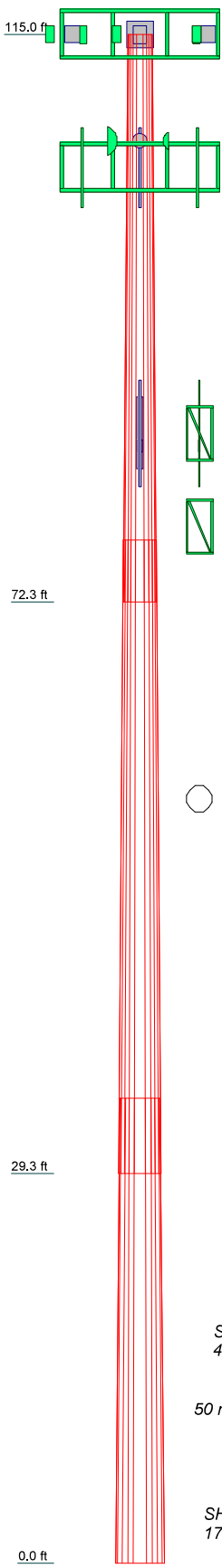
- All structural ratings are per TIA-222-H Section 15.5
- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

APPENDIX A
TNXTOWER OUTPUT

Section	1	2	3
Length (ft)	42.6666	47.6666	35.0000
Number of Sides	12	12	12
Thickness (in)	0.2190	0.3130	0.3750
Socket Length (ft)	4.6666	5.6666	56.8508
Top Dia (in)	21.9100	29.0779	36.8508
Bot Dia (in)	30.4500	38.6100	43.8500
Grade		A572-65	
Weight (K)	2.7	5.5	5.7



MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

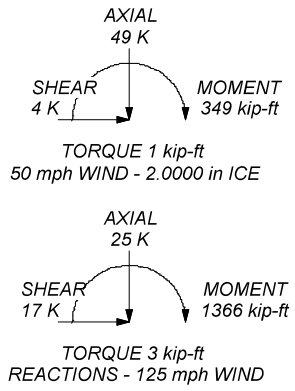
1. Tower is located in Hartford County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 125 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 2.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.
7. Topographic Category 1 with Crest Height of 0.0000 ft
8. TIA-222-H Annex S
9. TOWER RATING: 44%


72.3 ft

29.3 ft

0.0 ft

ALL REACTIONS ARE FACTORED



 Paul J. Ford and Company 250 East Broad St., Suite 600 Columbus, OH 43215 Phone: 614-221-6679 FAX:	Job: 115' Monopole HRT 093 943228	
	Project: PJF # 37520-0127.002.7805 BU# 806372	
Client: CCI	Drawn by: apike	App'd:
Code: TIA-222-H	Date: 01/22/20	Scale: NTS
Path:	Dwg No. E-1	

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

- 1) Tower is located in Hartford County, Connecticut.
- 2) Tower base elevation above sea level: 195.0000 ft.
- 3) Basic wind speed of 125 mph.
- 4) Risk Category II.
- 5) Exposure Category B.
- 6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- 7) Topographic Category: 1.
- 8) Crest Height: 0.0000 ft.
- 9) Nominal ice thickness of 2.0000 in.
- 10) Ice thickness is considered to increase with height.
- 11) Ice density of 56.00 pcf.
- 12) A wind speed of 50 mph is used in combination with ice.
- 13) Temperature drop of 50 °F.
- 14) Deflections calculated using a wind speed of 60 mph.
- 15) TIA-222-H Annex S.
- 16) A non-linear (P-delta) analysis was used.
- 17) Pressures are calculated at each section.
- 18) Stress ratio used in pole design is 1.05.
- 19) Tower analysis based on target reliabilities in accordance with Annex S.
- 20) Load Modification Factors used: $K_{es}(F_w) = 0.95$, $K_{es}(t_i) = 0.85$.
- 21) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification Use Code Stress Ratios Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric	Distribute Leg Loads As Uniform Assume Legs Pinned ✓ Assume Rigid Index Plate ✓ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension ✓ Bypass Mast Stability Checks ✓ Use Azimuth Dish Coefficients ✓ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs	Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation ✓ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption <div style="text-align: center; background-color: #e0e0e0; padding: 2px;">Poles</div> ✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	115.0000- 72.3334	42.6666	4.67	12	21.9100	30.4500	0.2190	0.8760	A572-65 (65 ksi)
L2	72.3334- 29.3334	47.6666	5.67	12	29.0779	38.6100	0.3130	1.2520	A572-65 (65 ksi)
L3	29.3334- 0.0000	35.0000		12	36.8508	43.8500	0.3750	1.5000	A572-65 (65 ksi)

Tapered Pole Properties

Section	Tip Dia. in	Area in ²	I in ⁴	r in	C in	I/C in ³	J in ⁴	I/Q in ²	w in	w/t
L1	22.6056	15.2961	918.5962	7.7654	11.3494	80.9380	1861.3250	7.5283	5.2850	24.132
	31.4469	21.3183	2486.8150	10.8227	15.7731	157.6618	5038.9614	10.4922	7.5737	34.583
L2	30.9594	28.9910	3061.8012	10.2979	15.0624	203.2748	6204.0393	14.2685	6.9541	22.217
	39.8616	38.5980	7225.7083	13.7103	20.0000	361.2858	14641.244	18.9968	9.5086	30.379
L3	39.1917	44.0446	7479.7774	13.0583	19.0887	391.8426	15156.056	21.6774	8.8710	23.656
	45.2646	52.4961	12664.611	15.5641	22.7143	557.5611	25661.935	25.8370	10.7468	28.658

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor Ar	Adjust. Factor Ar	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L1 115.0000- 72.3334				1	1	1			
L2 72.3334- 29.3334				1	1	1			
L3 29.3334- 0.0000				1	1	1			

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Exclude From Torque Calculation	Component Type	Placement ft	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight plf
HB158-1-08U8-S8J18(1-5/8) ***	A	No	Surface Ar (CaAa)	115.0000 - 0.0000	2	2	-0.283 -0.233	1.9800		1.30
1110(13/32)	A	No	Surface Ar (CaAa)	85.0000 - 0.0000	5	5	0.058 0.117	0.4050		0.05

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Total Number	Ice	CAAA ft ² /ft	Weight plf
HB158-1-08U8-S8J18(1-5/8) ***	A	No	No	Inside Pole	115.0000 - 0.0000	5	No Ice	0.0000	1.30
							1/2" Ice	0.0000	1.30
							1" Ice	0.0000	1.30
							2" Ice	0.0000	1.30
FSJ1-50A(1/4)	C	No	No	Inside Pole	105.0000 - 0.0000	5	No Ice	0.0000	0.04
							1/2" Ice	0.0000	0.04
							1" Ice	0.0000	0.04
							2" Ice	0.0000	0.04
FSJ4-50B(1/2)	C	No	No	Inside Pole	105.0000 - 0.0000	5	No Ice	0.0000	0.14
							1/2" Ice	0.0000	0.14
							1" Ice	0.0000	0.14
							2" Ice	0.0000	0.14
9207(5/16)	C	No	No	Inside Pole	105.0000 - 0.0000	5	No Ice	0.0000	0.06
							1/2" Ice	0.0000	0.06
							1" Ice	0.0000	0.06
							2" Ice	0.0000	0.06
2-1/2" (Nominal) Conduit	C	No	No	Inside Pole	105.0000 - 0.0000	2	No Ice	0.0000	1.14
							1/2" Ice	0.0000	1.14
							1" Ice	0.0000	1.14
							2" Ice	0.0000	1.14

Feed Line/Linear Appurtenances Section Areas

Tower Sectio n	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
L1	115.0000- 72.3334	A	0.000	0.000	19.461	0.000	0.39
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.11
L2	72.3334-29.3334	A	0.000	0.000	25.735	0.000	0.40
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.15
L3	29.3334-0.0000	A	0.000	0.000	17.556	0.000	0.27
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.10

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Sectio n	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
L1	115.0000- 72.3334	A	1.885	0.000	0.000	50.406	0.000	1.01
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.11
L2	72.3334-29.3334	A	1.774	0.000	0.000	72.703	0.000	1.26
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.15
L3	29.3334-0.0000	A	1.564	0.000	0.000	47.967	0.000	0.81
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.10

Feed Line Center of Pressure

Section	Elevation ft	CP _x in	CP _z in	CP _x Ice in	CP _z Ice in
L1	115.0000-72.3334	-2.4083	-0.1852	-3.1205	-0.3564
L2	72.3334-29.3334	-2.8976	-0.6343	-3.9555	-1.1478
L3	29.3334-0.0000	-2.9617	-0.6519	-4.2001	-1.2163

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
L1	3	HB158-1-08U8-S8J18(1-5/8)	72.33 - 115.00	1.0000	1.0000
L1	11	1110(13/32)	72.33 - 85.00	1.0000	1.0000
L2	3	HB158-1-08U8-S8J18(1-5/8)	29.33 - 72.33	1.0000	1.0000
L2	11	1110(13/32)	29.33 - 72.33	1.0000	1.0000

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustmen t °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K
DB-T1-6Z-8AB-0Z	A	From Leg	4.0000 0.00	0.0000	115.0000	No Ice 4.8000 5.0704	2.0000 2.1926	0.04 0.08

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAAA Front ft²	CAAA Side ft²	Weight K
			0.00			1/2" Ice 5.3481 2.3926 0.12		
						2" Ice 5.9259 2.8148 0.21		
CBRS w/ Mount Pipe	A	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.7135 1.1683 0.03		
						1/2" Ice 1.9342 1.4373 0.05		
						2" Ice 2.1662 1.7226 0.07		
						1" Ice 2.6643 2.3506 0.13		
CBRS w/ Mount Pipe	B	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.7135 1.1683 0.03		
						1/2" Ice 1.9342 1.4373 0.05		
						2" Ice 2.1662 1.7226 0.07		
						1" Ice 2.6643 2.3506 0.13		
CBRS w/ Mount Pipe	C	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.7135 1.1683 0.03		
						1/2" Ice 1.9342 1.4373 0.05		
						2" Ice 2.1662 1.7226 0.07		
						1" Ice 2.6643 2.3506 0.13		
(2) NNHH-65B-R4 w/ Mount Pipe	A	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 7.5500 4.2300 0.11		
						1/2" Ice 8.0400 4.6700 0.20		
						2" Ice 8.5300 5.1200 0.30		
						1" Ice 9.5600 6.0500 0.53		
(2) NNHH-65B-R4 w/ Mount Pipe	B	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 7.5500 4.2300 0.11		
						1/2" Ice 8.0400 4.6700 0.20		
						2" Ice 8.5300 5.1200 0.30		
						1" Ice 9.5600 6.0500 0.53		
(2) NNHH-65B-R4 w/ Mount Pipe	C	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 7.5500 4.2300 0.11		
						1/2" Ice 8.0400 4.6700 0.20		
						2" Ice 8.5300 5.1200 0.30		
						1" Ice 9.5600 6.0500 0.53		
LNX-6512DS-A1M w/ Mount Pipe	A	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 2.6700 2.1500 0.05		
						1/2" Ice 2.9400 2.4200 0.09		
						2" Ice 3.2200 2.6900 0.14		
						1" Ice 3.8100 3.2500 0.27		
LNX-6512DS-A1M w/ Mount Pipe	B	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 2.6700 2.1500 0.05		
						1/2" Ice 2.9400 2.4200 0.09		
						2" Ice 3.2200 2.6900 0.14		
						1" Ice 3.8100 3.2500 0.27		
LNX-6512DS-A1M w/ Mount Pipe	C	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 2.6700 2.1500 0.05		
						1/2" Ice 2.9400 2.4200 0.09		
						2" Ice 3.2200 2.6900 0.14		
						1" Ice 3.8100 3.2500 0.27		
(2) RFV01U-D1A	A	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.8750 1.2500 0.08		
						1/2" Ice 2.0454 1.3926 0.10		
						2" Ice 2.2231 1.5426 0.12		
						1" Ice 2.6009 1.8648 0.18		
RFV01U-D1A	B	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.8750 1.2500 0.08		
						1/2" Ice 2.0454 1.3926 0.10		
						2" Ice 2.2231 1.5426 0.12		
						1" Ice 2.6009 1.8648 0.18		
RFV01U-D2A	B	From Leg	4.0000 0.00 0.00	0.0000	115.0000	No Ice 1.8750 1.0125 0.07		
						1/2" Ice 2.0454 1.1445 0.09		
						2" Ice 2.2231 1.2840 0.11		
						1" Ice 2.6009 1.5851 0.15		
(2) RFV01U-D2A	C	From Leg	4.0000	0.0000	115.0000	No Ice 1.8750 1.0125 0.07		

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K	
			0.00			1/2"	2.0454	1.1445	0.09
			0.00			Ice	2.2231	1.2840	0.11
						1" Ice	2.6009	1.5851	0.15
						2" Ice			
20W CBRS	A	From Leg	4.0000	0.0000	115.0000	No Ice	0.8571	0.4203	0.02
			0.00			1/2"	0.9752	0.5105	0.03
			0.00			Ice	1.1008	0.6082	0.03
						1" Ice	1.3741	0.8327	0.06
						2" Ice			
20W CBRS	B	From Leg	4.0000	0.0000	115.0000	No Ice	0.8571	0.4203	0.02
			0.00			1/2"	0.9752	0.5105	0.03
			0.00			Ice	1.1008	0.6082	0.03
						1" Ice	1.3741	0.8327	0.06
						2" Ice			
20W CBRS	C	From Leg	4.0000	0.0000	115.0000	No Ice	0.8571	0.4203	0.02
			0.00			1/2"	0.9752	0.5105	0.03
			0.00			Ice	1.1008	0.6082	0.03
						1" Ice	1.3741	0.8327	0.06
						2" Ice			
Platform Mount [LP 712-1_KCKR]	C	None		0.0000	115.0000	No Ice	35.7800	35.7800	1.61
						1/2"	42.1400	42.1400	2.33
						Ice	48.6600	48.6600	3.15
						1" Ice	62.2300	62.2300	5.06
						2" Ice			
Miscellaneous [NA 507-1]	C	None		0.0000	115.0000	No Ice	4.5600	4.5600	0.25
						1/2"	6.3900	6.3900	0.31
						Ice	8.1800	8.1800	0.40
						1" Ice	11.6600	11.6600	0.66
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	A	From Leg	4.0000	0.0000	115.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	B	From Leg	4.0000	0.0000	115.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	C	From Leg	4.0000	0.0000	115.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			

Platform Mount [LP 602-1]	C	None		0.0000	105.0000	No Ice	31.0700	31.0700	1.34
						1/2"	34.8200	34.8200	1.97
						Ice	38.4800	38.4800	2.67
						1" Ice	45.6000	45.6000	4.31
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	A	From Leg	4.0000	0.0000	105.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	B	From Leg	4.0000	0.0000	105.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			
(2) 2.375" OD x 6' Mount Pipe	C	From Leg	4.0000	0.0000	105.0000	No Ice	1.4250	1.4250	0.03
			0.00			1/2"	1.9250	1.9250	0.04
			0.00			Ice	2.2939	2.2939	0.05
						1" Ice	3.0596	3.0596	0.09
						2" Ice			

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft		C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K

WH14-69/S	A	From Leg	4.0000 0.00 0.00	0.0000	85.0000	No Ice	1.8544	1.8544	0.01
						1/2" Ice	2.7029	2.7029	0.03
						Ice	3.0540	3.0540	0.06
						1" Ice	3.7841	3.7841	0.13
						2" Ice			
WL 14-69/S	A	From Leg	4.0000 0.00 -1.00	0.0000	85.0000	No Ice	0.2869	4.1479	0.01
						1/2" Ice	0.3655	4.4641	0.03
						Ice	0.4511	4.7877	0.06
						1" Ice	0.6454	5.4572	0.12
						2" Ice			
WL 14-69/S	B	From Leg	4.0000 0.00 -1.00	0.0000	85.0000	No Ice	0.2869	4.1479	0.01
						1/2" Ice	0.3655	4.4641	0.03
						Ice	0.4511	4.7877	0.06
						1" Ice	0.6454	5.4572	0.12
						2" Ice			
WL 14-69/S	B	From Leg	4.0000 0.00 -1.00	0.0000	85.0000	No Ice	0.2869	4.1479	0.01
						1/2" Ice	0.3655	4.4641	0.03
						Ice	0.4511	4.7877	0.06
						1" Ice	0.6454	5.4572	0.12
						2" Ice			
J105-HI	A	From Leg	4.0000 0.00 -7.00	0.0000	85.0000	No Ice	3.2500	3.2500	0.02
						1/2" Ice	0.0000	0.0000	0.03
						Ice	8.4790	8.4790	0.03
						1" Ice	0.0000	0.0000	0.04
						2" Ice			
Side Arm Mount [SO 701-1]	A	From Leg	4.0000 0.00 0.00	0.0000	85.0000	No Ice	0.8500	1.6700	0.07
						1/2" Ice	1.1400	2.3400	0.08
						Ice	1.4300	3.0100	0.09
						1" Ice	2.0100	4.3500	0.12
						2" Ice			
Side Arm Mount [SO 701-1]	A	From Leg	4.0000 0.00 -7.00	0.0000	85.0000	No Ice	0.8500	1.6700	0.07
						1/2" Ice	1.1400	2.3400	0.08
						Ice	1.4300	3.0100	0.09
						1" Ice	2.0100	4.3500	0.12
						2" Ice			
Side Arm Mount [SO 701-1]	B	From Leg	4.0000 0.00 0.00	0.0000	85.0000	No Ice	0.8500	1.6700	0.07
						1/2" Ice	1.1400	2.3400	0.08
						Ice	1.4300	3.0100	0.09
						1" Ice	2.0100	4.3500	0.12
						2" Ice			
Side Arm Mount [SO 701-1]	B	From Leg	4.0000 0.00 -7.00	0.0000	85.0000	No Ice	0.8500	1.6700	0.07
						1/2" Ice	1.1400	2.3400	0.08
						Ice	1.4300	3.0100	0.09
						1" Ice	2.0100	4.3500	0.12
						2" Ice			
2.375" OD x 8' Mount Pipe	A	From Leg	4.0000 0.00 0.00	0.0000	85.0000	No Ice	1.9000	1.9000	0.03
						1/2" Ice	2.7281	2.7281	0.04
						Ice	3.4009	3.4009	0.06
						1" Ice	4.3962	4.3962	0.12
						2" Ice			
2.375" OD x 8' Mount Pipe	B	From Leg	4.0000 0.00 0.00	0.0000	85.0000	No Ice	1.9000	1.9000	0.03
						1/2" Ice	2.7281	2.7281	0.04
						Ice	3.4009	3.4009	0.06
						1" Ice	4.3962	4.3962	0.12
						2" Ice			

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert ft	Azimuth Adjustment °	3 dB Beam Width °	Elevation ft	Outside Diameter ft	Aperture Area ft²	Weight K
VHLP1-23	A	Paraboloid w/o Radome	From Leg	1.0000	57.0000		105.0000	1.2750	No Ice	0.01
				0.00					1/2" Ice	0.02
				2.00					1" Ice	0.03
									2" Ice	0.04
VHLP2-23	C	Paraboloid w/o Radome	From Leg	1.0000	40.0000		105.0000	2.1750	No Ice	0.03
				0.00					1/2" Ice	0.05
				2.00					1" Ice	0.07
									2" Ice	0.11
VHLP1-23	B	Paraboloid w/o Radome	From Leg	1.0000	67.0000		105.0000	1.2750	No Ice	0.01
				0.00					1/2" Ice	0.02
				2.00					1" Ice	0.03
									2" Ice	0.04

Tower Pressures - No Ice

$G_H = 1.100$

Section Elevation ft	z ft	K_z	q_z psf	A_G ft²	F a c e	A_F ft²	A_R ft²	A_{leg} ft²	Leg %	$C_A A_A$ In Face ft²	$C_A A_A$ Out Face ft²
L1 115.0000-72.3334	92.8501	0.968	34.598	96.093	A	0.000	96.093	96.093	100.00	19.461	0.000
					B	0.000	96.093		100.00	0.000	0.000
					C	0.000	96.093		100.00	0.000	0.000
L2 72.3334-29.3334	50.5924	0.813	28.912	126.888	A	0.000	126.888	126.888	100.00	25.735	0.000
					B	0.000	126.888		100.00	0.000	0.000
					C	0.000	126.888		100.00	0.000	0.000
L3 29.3334-0.0000	14.3163	0.7	25.092	103.225	A	0.000	103.225	103.225	100.00	17.556	0.000
					B	0.000	103.225		100.00	0.000	0.000
					C	0.000	103.225		100.00	0.000	0.000

Tower Pressure - With Ice

$G_H = 1.100$

Section Elevation ft	z ft	K_z	q_z psf	t_z in	A_G ft²	F a c e	A_F ft²	A_R ft²	A_{leg} ft²	Leg %	$C_A A_A$ In Face ft²	$C_A A_A$ Out Face ft²
L1 115.0000-72.3334	92.8501	0.968	5.536	1.8853	109.500	A	0.000	109.500	109.500	100.00	50.406	0.000
						B	0.000	109.500		100.00	0.000	0.000
						C	0.000	109.500		100.00	0.000	0.000
L2 72.3334-29.3334	50.5924	0.813	4.626	1.7742	140.399	A	0.000	140.399	140.399	100.00	72.703	0.000
						B	0.000	140.399		100.00	0.000	0.000
						C	0.000	140.399		100.00	0.000	0.000
L3 29.3334-0.0000	14.3163	0.7	4.015	1.5638	111.898	A	0.000	111.898	111.898	100.00	47.967	0.000
						B	0.000	111.898		100.00	0.000	0.000
						C	0.000	111.898		100.00	0.000	0.000

Tower Pressure - Service

$G_H = 1.100$

Section Elevation ft	z ft	K_z	q_z psf	A_G ft²	F a c e	A_F ft²	A_R ft²	A_{leg} ft²	Leg %	$C_A A_A$ In Face ft²	$C_A A_A$ Out Face ft²
L1 115.0000-72.3334	92.8501	0.968	7.508	96.093	A	0.000	96.093	96.093	100.00	19.461	0.000
					B	0.000	96.093		100.00	0.000	0.000
					C	0.000	96.093		100.00	0.000	0.000

Section Elevation ft	z ft	K _z	q _z psf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L2 72.3334- 29.3334	50.5924	0.813	6.274	126.88 8	A	0.000	126.888	126.888	100.00	25.735	0.000
					B	0.000	126.888		100.00	0.000	0.000
					C	0.000	126.888		100.00	0.000	0.000
L3 29.3334- 0.0000	14.3163	0.7	5.445	103.22 5	A	0.000	103.225	103.225	100.00	17.556	0.000
					B	0.000	103.225		100.00	0.000	0.000
					C	0.000	103.225		100.00	0.000	0.000

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 60 deg - No Ice
7	0.9 Dead+1.0 Wind 60 deg - No Ice
8	1.2 Dead+1.0 Wind 90 deg - No Ice
9	0.9 Dead+1.0 Wind 90 deg - No Ice
10	1.2 Dead+1.0 Wind 120 deg - No Ice
11	0.9 Dead+1.0 Wind 120 deg - No Ice
12	1.2 Dead+1.0 Wind 150 deg - No Ice
13	0.9 Dead+1.0 Wind 150 deg - No Ice
14	1.2 Dead+1.0 Wind 180 deg - No Ice
15	0.9 Dead+1.0 Wind 180 deg - No Ice
16	1.2 Dead+1.0 Wind 210 deg - No Ice
17	0.9 Dead+1.0 Wind 210 deg - No Ice
18	1.2 Dead+1.0 Wind 240 deg - No Ice
19	0.9 Dead+1.0 Wind 240 deg - No Ice
20	1.2 Dead+1.0 Wind 270 deg - No Ice
21	0.9 Dead+1.0 Wind 270 deg - No Ice
22	1.2 Dead+1.0 Wind 300 deg - No Ice
23	0.9 Dead+1.0 Wind 300 deg - No Ice
24	1.2 Dead+1.0 Wind 330 deg - No Ice
25	0.9 Dead+1.0 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	115 - 72.3334	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-25.22	-2.10	3.63
			Max. Mx	8	-9.42	-292.55	1.68
			Max. My	2	-9.42	-1.07	293.12
			Max. Vy	8	10.42	-292.55	1.68
			Max. Vx	14	10.38	-0.63	-291.06
			Max. Torque	24		-2.92	
L2	72.3334 - 29.3334	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-36.45	-0.92	4.45
			Max. Mx	8	-16.32	-807.21	7.62
			Max. My	2	-16.32	-6.23	806.31
			Max. Vy	8	14.06	-807.21	7.62
			Max. Vx	14	14.02	4.61	-804.11
			Max. Torque	24		-2.92	
L3	29.3334 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-48.78	0.24	5.05
			Max. Mx	8	-24.88	-1350.57	12.50
			Max. My	2	-24.88	-10.43	1348.50
			Max. Vy	8	17.00	-1350.57	12.50
			Max. Vx	14	16.96	9.00	-1346.18
			Max. Torque	24		-2.92	

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	26	48.78	0.00	-0.00
	Max. H _x	20	24.89	16.93	-0.21
	Max. H _z	3	18.67	-0.12	16.95
	Max. M _x	2	1348.50	-0.12	16.95
	Max. M _z	8	1350.57	-16.99	0.13
	Max. Torsion	12	2.73	-8.48	-14.56
	Min. Vert	21	18.67	16.93	-0.21
	Min. H _x	9	18.67	-16.99	0.13
	Min. H _z	15	18.67	0.12	-16.95
	Min. M _x	14	-1346.18	0.12	-16.95
	Min. M _z	20	-1343.20	16.93	-0.21
	Min. Torsion	24	-2.92	8.27	14.63

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Dead Only	20.74	-0.00	0.00	-1.05	-0.37	0.00
1.2 Dead+1.0 Wind 0 deg - No Ice	24.89	0.12	-16.95	-1348.50	-10.43	2.24
0.9 Dead+1.0 Wind 0 deg - No Ice	18.67	0.12	-16.95	-1339.08	-10.25	2.23
1.2 Dead+1.0 Wind 30 deg - No Ice	24.89	8.73	-14.75	-1174.14	-697.98	1.27
0.9 Dead+1.0 Wind 30 deg - No Ice	18.67	8.73	-14.75	-1165.89	-693.16	1.26
1.2 Dead+1.0 Wind 60 deg - No Ice	24.89	14.84	-8.59	-684.43	-1181.44	-0.17
0.9 Dead+1.0 Wind 60 deg - No Ice	18.67	14.84	-8.59	-679.49	-1173.36	-0.17

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
1.2 Dead+1.0 Wind 90 deg - No Ice	24.89	16.99	-0.13	-12.50	-1350.57	-1.68
0.9 Dead+1.0 Wind 90 deg - No Ice	18.67	16.99	-0.13	-12.10	-1341.35	-1.67
1.2 Dead+1.0 Wind 120 deg - No Ice	24.89	14.67	8.32	658.15	-1166.24	-2.68
0.9 Dead+1.0 Wind 120 deg - No Ice	18.67	14.67	8.32	654.03	-1158.25	-2.67
1.2 Dead+1.0 Wind 150 deg - No Ice	24.89	8.48	14.56	1154.25	-676.64	-2.73
0.9 Dead+1.0 Wind 150 deg - No Ice	18.67	8.48	14.56	1146.79	-671.94	-2.71
1.2 Dead+1.0 Wind 180 deg - No Ice	24.89	-0.12	16.95	1346.18	9.00	-2.02
0.9 Dead+1.0 Wind 180 deg - No Ice	18.67	-0.12	16.95	1337.43	9.07	-2.01
1.2 Dead+1.0 Wind 210 deg - No Ice	24.89	-8.65	14.73	1169.61	688.69	-0.94
0.9 Dead+1.0 Wind 210 deg - No Ice	18.67	-8.65	14.73	1162.06	684.18	-0.93
1.2 Dead+1.0 Wind 240 deg - No Ice	24.89	-14.73	8.63	686.72	1168.70	0.65
0.9 Dead+1.0 Wind 240 deg - No Ice	18.67	-14.73	8.63	682.42	1160.96	0.64
1.2 Dead+1.0 Wind 270 deg - No Ice	24.89	-16.93	0.21	17.88	1343.20	1.93
0.9 Dead+1.0 Wind 270 deg - No Ice	18.67	-16.93	0.21	18.09	1334.21	1.92
1.2 Dead+1.0 Wind 300 deg - No Ice	24.89	-14.59	-8.36	-665.83	1157.34	2.88
0.9 Dead+1.0 Wind 300 deg - No Ice	18.67	-14.59	-8.36	-661.00	1149.66	2.87
1.2 Dead+1.0 Wind 330 deg - No Ice	24.89	-8.27	-14.63	-1164.27	652.84	2.92
0.9 Dead+1.0 Wind 330 deg - No Ice	18.67	-8.27	-14.63	-1156.06	648.55	2.90
1.2 Dead+1.0 Ice+1.0 Temp	48.78	-0.00	0.00	-5.05	0.24	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	48.78	0.03	-4.01	-345.93	-2.40	0.65
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	48.78	2.07	-3.49	-301.89	-176.04	0.38
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	48.78	3.52	-2.03	-178.20	-298.82	-0.01
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	48.78	4.03	-0.03	-8.17	-341.89	-0.42
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	48.78	3.48	1.97	161.58	-295.10	-0.71
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	48.78	2.01	3.44	286.98	-170.72	-0.76
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	48.78	-0.03	4.01	335.43	2.88	-0.59
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	48.78	-2.05	3.49	290.78	174.84	-0.31
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	48.78	-3.49	2.04	168.54	296.76	0.11
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	48.78	-4.02	0.05	-0.52	340.97	0.48
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	48.78	-3.46	-1.98	-173.28	293.91	0.76
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	48.78	-1.96	-3.46	-299.31	166.05	0.80
Dead+Wind 0 deg - Service	20.74	0.03	-3.68	-292.15	-2.54	0.49
Dead+Wind 30 deg - Service	20.74	1.89	-3.20	-254.48	-151.09	0.28
Dead+Wind 60 deg - Service	20.74	3.22	-1.86	-148.68	-255.54	-0.04
Dead+Wind 90 deg - Service	20.74	3.69	-0.03	-3.51	-292.08	-0.36
Dead+Wind 120 deg - Service	20.74	3.18	1.80	141.39	-252.25	-0.58
Dead+Wind 150 deg - Service	20.74	1.84	3.16	248.57	-146.47	-0.59

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Dead+Wind 180 deg - Service	20.74	-0.03	3.68	290.04	1.66	-0.44
Dead+Wind 210 deg - Service	20.74	-1.88	3.20	251.89	148.51	-0.20
Dead+Wind 240 deg - Service	20.74	-3.20	1.87	147.56	252.21	0.14
Dead+Wind 270 deg - Service	20.74	-3.67	0.04	3.06	289.92	0.42
Dead+Wind 300 deg - Service	20.74	-3.17	-1.81	-144.65	249.75	0.62
Dead+Wind 330 deg - Service	20.74	-1.79	-3.17	-252.34	140.76	0.63

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-20.74	0.00	0.00	20.74	-0.00	0.000%
2	0.12	-24.89	-16.95	-0.12	24.89	16.95	0.001%
3	0.12	-18.67	-16.95	-0.12	18.67	16.95	0.001%
4	8.73	-24.89	-14.75	-8.73	24.89	14.75	0.000%
5	8.73	-18.67	-14.75	-8.73	18.67	14.75	0.000%
6	14.84	-24.89	-8.59	-14.84	24.89	8.59	0.000%
7	14.84	-18.67	-8.59	-14.84	18.67	8.59	0.000%
8	16.99	-24.89	-0.13	-16.99	24.89	0.13	0.001%
9	16.99	-18.67	-0.13	-16.99	18.67	0.13	0.001%
10	14.67	-24.89	8.32	-14.67	24.89	-8.32	0.000%
11	14.67	-18.67	8.32	-14.67	18.67	-8.32	0.000%
12	8.48	-24.89	14.56	-8.48	24.89	-14.56	0.000%
13	8.48	-18.67	14.56	-8.48	18.67	-14.56	0.000%
14	-0.12	-24.89	16.95	0.12	24.89	-16.95	0.001%
15	-0.12	-18.67	16.95	0.12	18.67	-16.95	0.001%
16	-8.65	-24.89	14.73	8.65	24.89	-14.73	0.000%
17	-8.65	-18.67	14.73	8.65	18.67	-14.73	0.000%
18	-14.73	-24.89	8.63	14.73	24.89	-8.63	0.000%
19	-14.73	-18.67	8.63	14.73	18.67	-8.63	0.000%
20	-16.93	-24.89	0.21	16.93	24.89	-0.21	0.001%
21	-16.93	-18.67	0.21	16.93	18.67	-0.21	0.004%
22	-14.59	-24.89	-8.36	14.59	24.89	8.36	0.000%
23	-14.59	-18.67	-8.36	14.59	18.67	8.36	0.000%
24	-8.27	-24.89	-14.63	8.27	24.89	14.63	0.000%
25	-8.27	-18.67	-14.63	8.27	18.67	14.63	0.001%
26	0.00	-48.78	0.00	0.00	48.78	-0.00	0.003%
27	0.03	-48.78	-4.01	-0.03	48.78	4.01	0.001%
28	2.07	-48.78	-3.49	-2.07	48.78	3.49	0.001%
29	3.52	-48.78	-2.03	-3.52	48.78	2.03	0.001%
30	4.03	-48.78	-0.03	-4.03	48.78	0.03	0.001%
31	3.48	-48.78	1.97	-3.48	48.78	-1.97	0.001%
32	2.01	-48.78	3.44	-2.01	48.78	-3.44	0.001%
33	-0.03	-48.78	4.01	0.03	48.78	-4.01	0.001%
34	-2.05	-48.78	3.49	2.05	48.78	-3.49	0.001%
35	-3.49	-48.78	2.04	3.49	48.78	-2.04	0.001%
36	-4.02	-48.78	0.05	4.02	48.78	-0.05	0.001%
37	-3.46	-48.78	-1.98	3.46	48.78	1.98	0.001%
38	-1.96	-48.78	-3.46	1.96	48.78	3.46	0.001%
39	0.03	-20.74	-3.68	-0.03	20.74	3.68	0.004%
40	1.89	-20.74	-3.20	-1.89	20.74	3.20	0.004%
41	3.22	-20.74	-1.86	-3.22	20.74	1.86	0.004%
42	3.69	-20.74	-0.03	-3.69	20.74	0.03	0.004%
43	3.18	-20.74	1.80	-3.18	20.74	-1.80	0.004%
44	1.84	-20.74	3.16	-1.84	20.74	-3.16	0.004%
45	-0.03	-20.74	3.68	0.03	20.74	-3.68	0.004%
46	-1.88	-20.74	3.20	1.88	20.74	-3.20	0.004%
47	-3.20	-20.74	1.87	3.20	20.74	-1.87	0.004%
48	-3.67	-20.74	0.04	3.67	20.74	-0.04	0.004%
49	-3.17	-20.74	-1.81	3.17	20.74	1.81	0.004%

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
50	-1.79	-20.74	-3.17	1.79	20.74	3.17	0.004%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	12	0.00000001	0.00007371
3	Yes	12	0.00000001	0.00006105
4	Yes	13	0.00000001	0.00008497
5	Yes	13	0.00000001	0.00006706
6	Yes	13	0.00000001	0.00007835
7	Yes	13	0.00000001	0.00006170
8	Yes	12	0.00000001	0.00006355
9	Yes	12	0.00000001	0.00005263
10	Yes	13	0.00000001	0.00006322
11	Yes	13	0.00000001	0.00004995
12	Yes	13	0.00000001	0.00008875
13	Yes	13	0.00000001	0.00007055
14	Yes	12	0.00000001	0.00006179
15	Yes	12	0.00000001	0.00005144
16	Yes	13	0.00000001	0.00007280
17	Yes	13	0.00000001	0.00005748
18	Yes	13	0.00000001	0.00007260
19	Yes	13	0.00000001	0.00005736
20	Yes	12	0.00000001	0.00005977
21	Yes	11	0.00000001	0.00014925
22	Yes	13	0.00000001	0.00008936
23	Yes	13	0.00000001	0.00007105
24	Yes	13	0.00000001	0.00006179
25	Yes	12	0.00000001	0.00014959
26	Yes	7	0.00000001	0.00002613
27	Yes	12	0.00000001	0.00008015
28	Yes	12	0.00000001	0.00008697
29	Yes	12	0.00000001	0.00008609
30	Yes	12	0.00000001	0.00007870
31	Yes	12	0.00000001	0.00008160
32	Yes	12	0.00000001	0.00008206
33	Yes	12	0.00000001	0.00007602
34	Yes	12	0.00000001	0.00008138
35	Yes	12	0.00000001	0.00008166
36	Yes	12	0.00000001	0.00007736
37	Yes	12	0.00000001	0.00008448
38	Yes	12	0.00000001	0.00008375
39	Yes	10	0.00000001	0.00010500
40	Yes	10	0.00000001	0.00009618
41	Yes	10	0.00000001	0.00009427
42	Yes	10	0.00000001	0.00010386
43	Yes	10	0.00000001	0.00009369
44	Yes	10	0.00000001	0.00009793
45	Yes	10	0.00000001	0.00010295
46	Yes	10	0.00000001	0.00009208
47	Yes	10	0.00000001	0.00009205
48	Yes	10	0.00000001	0.00010288
49	Yes	10	0.00000001	0.00009904
50	Yes	10	0.00000001	0.00009418

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	115 - 72.3334	9.0275	40	0.6798	0.0044
L2	77 - 29.3334	4.1174	40	0.5029	0.0028
L3	35 - 0	0.8515	40	0.2178	0.0008

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
115.0000	DB-T1-6Z-8AB-0Z	40	9.0275	0.6798	0.0044	61229
107.0000	VHLP1-23	40	7.9216	0.6470	0.0041	38268
105.0000	Platform Mount [LP 602-1]	40	7.6475	0.6387	0.0040	30614
85.0000	WH14-69/S	40	5.0444	0.5467	0.0031	10204

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	115 - 72.3334	41.5807	4	3.1287	0.0200
L2	77 - 29.3334	18.9850	4	2.3173	0.0127
L3	35 - 0	3.9293	4	1.0050	0.0035

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
115.0000	DB-T1-6Z-8AB-0Z	4	41.5807	3.1287	0.0200	13416
107.0000	VHLP1-23	4	36.4932	2.9786	0.0185	8385
105.0000	Platform Mount [LP 602-1]	4	35.2321	2.9404	0.0182	6707
85.0000	WH14-69/S	4	23.2534	2.5187	0.0143	2234

Compression Checks Pole Design Data

Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in ²	P _u K	φP _n K	Ratio P _u φP _n
L1	115 - 72.3334 (1)	TP30.45x21.91x0.219	42.666 6	0.0000	0.0	20.659 6	-9.40	1208.59	0.008
L2	72.3334 - 29.3334 (2)	TP38.61x29.0779x0.313	47.666 6	0.0000	0.0	37.455 9	-16.32	2191.17	0.007
L3	29.3334 - 0 (3)	TP43.85x36.8508x0.375	35.000 0	0.0000	0.0	52.496 1	-24.88	3071.02	0.008

Pole Bending Design Data

Section No.	Elevation ft	Size	M _{ux} kip-ft	φM _{nx} kip-ft	Ratio M _{ux} φM _{nx}	M _{uy} kip-ft	φM _{ny} kip-ft	Ratio M _{uy} φM _{ny}
L1	115 - 72.3334 (1)	TP30.45x21.91x0.219	295.82	741.46	0.399	0.00	741.46	0.000
L2	72.3334 - 29.3334 (2)	TP38.61x29.0779x0.313	817.11	1815.79	0.450	0.00	1815.79	0.000
L3	29.3334 - 0 (3)	TP43.85x36.8508x0.375	1365.94	3010.72	0.454	0.00	3010.72	0.000

Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V_u K	ϕV_n K	Ratio $\frac{V_u}{\phi V_n}$	Actual T_u kip-ft	ϕT_n kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	115 - 72.3334 (1)	TP30.45x21.91x0.219	10.58	362.58	0.029	1.27	934.38	0.001
L2	72.3334 - 29.3334 (2)	TP38.61x29.0779x0.313	14.21	657.35	0.022	1.27	2148.91	0.001
L3	29.3334 - 0 (3)	TP43.85x36.8508x0.375	17.15	921.31	0.019	1.27	3523.25	0.000

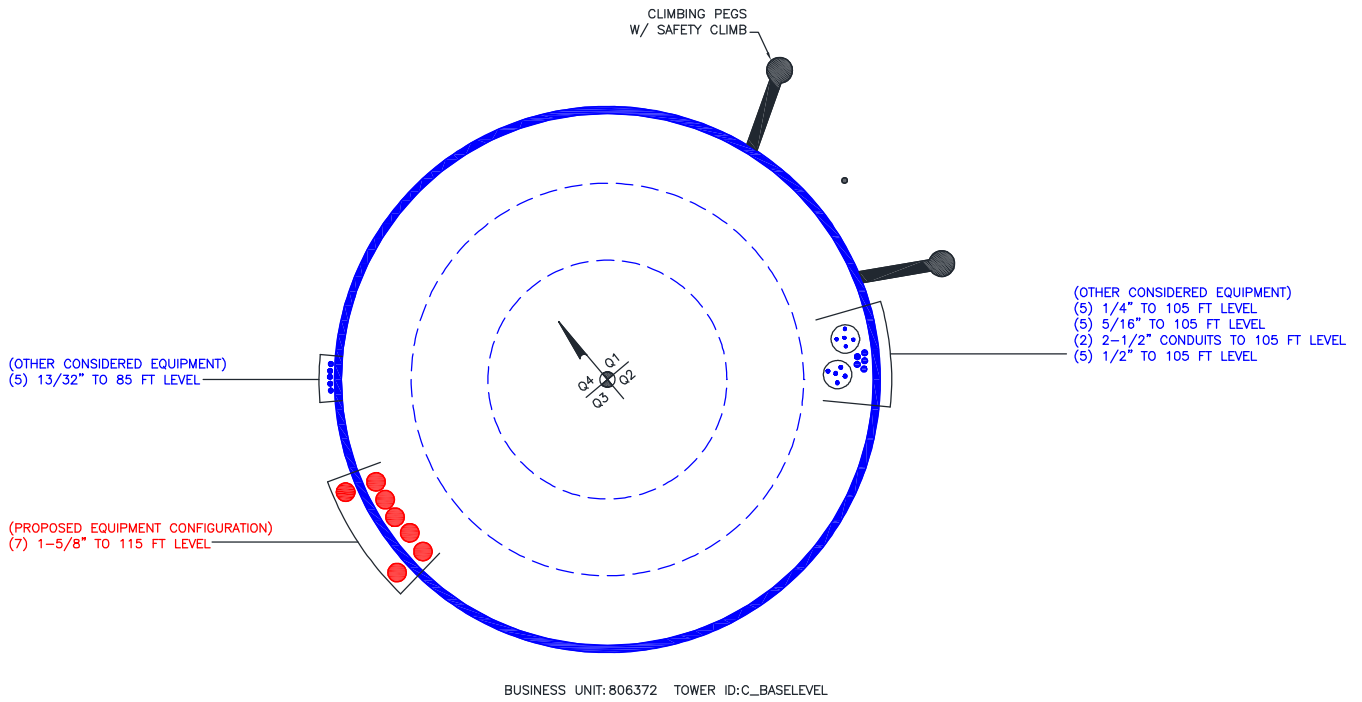
Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	Ratio $\frac{M_{uy}}{\phi M_{ny}}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	115 - 72.3334 (1)	0.008	0.399	0.000	0.029	0.001	0.408	1.050	4.8.2
L2	72.3334 - 29.3334 (2)	0.007	0.450	0.000	0.022	0.001	0.458	1.050	4.8.2
L3	29.3334 - 0 (3)	0.008	0.454	0.000	0.019	0.000	0.462	1.050	4.8.2

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
L1	115 - 72.3334	Pole	TP30.45x21.91x0.219	1	-9.40	1269.02	38.8	Pass	
L2	72.3334 - 29.3334	Pole	TP38.61x29.0779x0.313	2	-16.32	2300.73	43.6	Pass	
L3	29.3334 - 0	Pole	TP43.85x36.8508x0.375	3	-24.88	3224.57	44.0	Pass	
							Summary		
							Pole (L3)	44.0	Pass
							RATING =	44.0	Pass

APPENDIX B
BASE LEVEL DRAWING



APPENDIX C
ADDITIONAL CALCULATIONS

Monopole Base Plate Connection

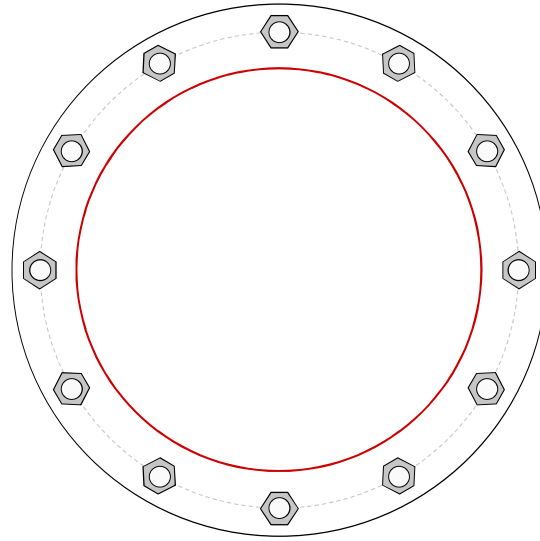


Site Info	
BU #	806372
Site Name	HRT 093 943228
Order #	511445 Rev. 0

Analysis Considerations	
TIA-222 Revision	H
Grout Considered:	No
I_{ar} (in)	2

Applied Loads	
Moment (kip-ft)	1365.94
Axial Force (kips)	24.88
Shear Force (kips)	17.15

*TIA-222-H Section 15.5 Applied



Connection Properties	Analysis Results
-----------------------	------------------

Anchor Rod Data
(12) 2-1/4" ϕ bolts (A615-75 N; $F_y=75$ ksi, $F_u=100$ ksi) on 51.9" BC
Base Plate Data
57.9" OD x 2.625" Plate (A572-60; $F_y=60$ ksi, $F_u=75$ ksi)
Stiffener Data
N/A
Pole Data
43.85" x 0.375" 12-sided pole (A572-65; $F_y=65$ ksi, $F_u=80$ ksi)

Anchor Rod Summary	(units of kips, kip-in)	
$Pu_c = 107.27$	$\phi Pn_c = 268.39$	Stress Rating
$Vu = 1.43$	$\phi Vn = 120.77$	38.1%
$Mu = n/a$	$\phi Mn = n/a$	Pass
Base Plate Summary		
Max Stress (ksi):	13.62	(Flexural)
Allowable Stress (ksi):	54	
Stress Rating:	24.0%	Pass

Drilled Pier Foundation

BU #: 806372
 Site Name: HRT 093 943228
 Order Number: 511445 Rev. 0

TIA-222 Revision: H
 Tower Type: Monopole



Check Limitation	
Apply TIA-222-H Section 15.5:	N/A

Analysis Results			
Soil Lateral Capacity	Compression	Uplift	
D _{cr0} (ft from TOC)	6.85	-	
Soil Safety Factor	2.36	-	
Max Moment (kip-ft)	1481.62	-	
Rating*	53.7%	-	
Soil Vertical Capacity	Compression	Uplift	
Skin Friction (kips)	179.25	-	
End Bearing (kips)	127.23	-	
Weight of Concrete (kips)	109.42	-	
Total Capacity (kips)	306.49	-	
Axial (kips)	134.30	-	
Rating*	41.7%	-	
Reinforced Concrete Capacity	Compression	Uplift	
Critical Depth (ft from TOC)	6.73	-	
Critical Moment (kip-ft)	1481.52	-	
Critical Moment Capacity	3637.63	-	
Rating*	38.8%	-	
Soil Interaction Rating*	53.7%		
Structural Foundation Rating*	38.8%		

*Rating per TIA-222-H Section 15.5

Soil Profile

# of Layers	4
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Layer	Top (ft)	Bottom (ft)	Thickness (ft)	Y _{soil} (pcf)	Y _{concrete} (pcf)	Cohesion (ksf)	Angle of Friction (degrees)	Calculated Ultimate Skin Friction Comp (ksf)	Calculated Ultimate Skin Friction Uplift (ksf)	Ultimate Skin Friction Comp Override (ksf)	Ultimate Skin Friction Uplift Override (ksf)	Ult. Gross Bearing Capacity (ksf)	SPT Blow Count	Soil Type
1	0	5	5	90	150	0	0	0.000	0.000	0.00	0.00			Cohesionless
2	5	14	9	90	150		30	0.247	0.247				4	Cohesionless
3	14	18	4	90	150		39	1.382	1.382				43	Cohesionless
4	18	21.1	3.1	90	150		30	1.589	1.589			6	16	Cohesionless

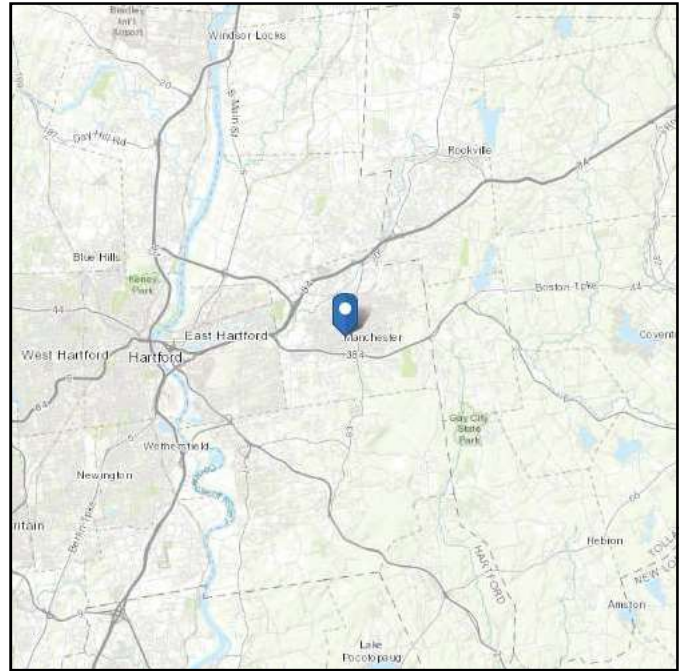
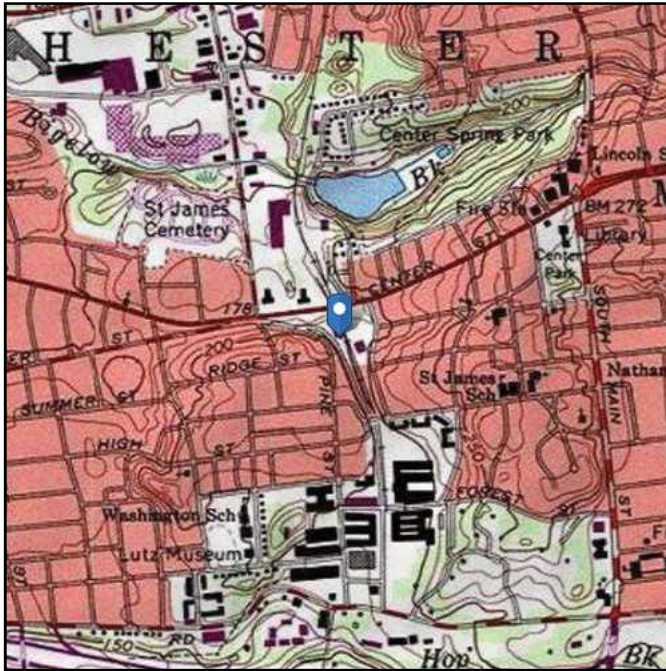
Groundwater Depth	n/a	ft
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ASCE 7 Hazards Report

Address:
No Address at This
Location

Standard: ASCE/SEI 7-10
Risk Category: II
Soil Class: D - Stiff Soil

Elevation: 195.7 ft (NAVD 88)
Latitude: 41.771944
Longitude: -72.530222



Wind

Results:

Wind Speed:	124 Vmph
10-year MRI	77 Vmph
25-year MRI	87 Vmph
50-year MRI	94 Vmph
100-year MRI	101 Vmph

Data Source: ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of March 12, 2014

Date Accessed: Tue Apr 02 2019

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

Ice

Results:

Ice Thickness: 1.00 in.

Concurrent Temperature: 5 F

Gust Speed: 50 mph

Data Source: Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8

Date Accessed: Tue Apr 02 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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Exhibit E

Mount Analysis

Date: January 21, 2020

Kevin Morrow
Crown Castle
6325 Ardrey Kell Road
Charlotte, NC 28277

Paul J Ford and Company
250 E. Broad Street, Suite 600
Columbus, OH 43215
614.221.6679

Subject: Mount Analysis Report

Carrier Designation: **Verizon Wireless Equipment Change-out**
Carrier Site Number: 1904
Carrier Site Name: Manchester CT

Crown Castle Designation: **Crown Castle BU Number:** 806372
Crown Castle Site Name: HRT 093 943228
Crown Castle JDE Job Number: 598729
Crown Castle Purchase Order Number: 1490876
Crown Castle Order Number: 511445 Rev. 0

Engineering Firm Designation: **Paul J Ford and Company Project Number:** A37520-0127.001.7190

Site Data: **266R Center Street, Manchester, Hartford County, CT 06040**
Latitude 41.771944°, Longitude -72.530222°

Structure Information: **Tower Height & Type:** 115 Foot Monopole
Mount Elevation: 115 Foot
Mount Type: (1) 14 Foot Platform

Dear Kevin Morrow,

Paul J Ford and Company is pleased to submit this "Mount Analysis Report" to determine the structural integrity of the Verizon Wireless antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

14' Platform **79.2%** **SUFFICIENT***
 *The mount has sufficient capacity once the modifications, as described in Section 4.1 Recommendations of this report, are completed.

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Respectfully submitted by:

Angela Sage, E.I.
Structural Designer
asage@pauljford.com

JGF

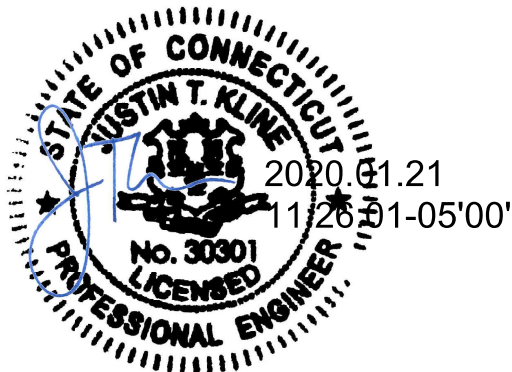


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POST MODIFICATION INSPECTION (PMI) REQUIREMENTS FOR DESKTOP
REVIEW

1) INTRODUCTION

The existing mount under consideration is (1) 14' Platform mount mapped by B+T on 04/17/2019.

2) ANALYSIS CRITERIA

TIA-222 Revision:	TIA-222-H
Risk Category:	II
Ultimate Wind Speed:	125 mph
Exposure Category:	B
Topographic Factor at Base:	1.00
Topographic Factor at Mount:	1.00
Ice Thickness:	2 in
Wind Speed with Ice:	50 mph
Live Loading Wind Speed:	30 mph
Maintenance Load at Mid/End-Points:	250 lb
Maintenance Load at Mount Pipes:	500 lb

Table 1 - Proposed Equipment Configuration

Mount Centerline (ft)	Antenna Centerline (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Mount / Modification Details
115	115	3	Andrew	LNx-6512DS-A1M	(1) 14' Platform
		6	Commscope	NNHH-65B-R4	
		3	Samsung Tele	CBRS	
		1	RFS Celwave	DB-T1-6Z-8AB-0Z	
		3	Samsung Tele	20W CBRS	
		3	Samsung Tele	RFV01U-D1A	
		3	Samsung Tele	RFV01U-D2A	

3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

Document	Remarks	Reference	Source
Mount Mapping	File #: B+T, 134993.002.01 Dated: 04/25/2019	8364339	CCISites
Mount Modification Drawings	File #: B+T, 134993.003.01 Dated: 05/03/2019	8390235	CCISites
Order	ID: 511445 Rev. 0 Dated: 01/16/2020	-	CCISites
Radio Frequency Data Sheet	1559441 Dated: 09/11/2019	-	Crown Castle

3.1) Analysis Method

RISA-3D (version 17.0.3), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 *Tower Mount Analysis* (Revision C). In addition, this analysis is in accordance with Verizon's NSTD-446 *Antenna Mount Analysis and Modification Process* (dated 03/29/19).

3.2) Assumptions

- 1) *The analysis of the existing tower or the effect of the mount attachment to the tower is not within the current scope of work.*
- 2) *The antenna mounting system was properly fabricated, installed and maintained in good condition, twist free and plumb in accordance with its original design and manufacturer's specifications and all bolts are tightened as specified by the manufacturer and AISC requirements.*
- 3) *The configuration of antennas, mounts, and other appurtenances are as specified in Table 1.*
- 4) *All member connections have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report. All U-Bolt connections have been properly tightened. This analysis will be required to be revised if the existing conditions in the field differ from those shown in the above referenced documents or assumed in this analysis. No allowance was made for any damaged, missing, or rusted members.*
- 5) *Steel grades are as follows, unless noted otherwise:*

a) Channel, Solid Round, Angle, Plate, Unistrut	ASTM A36 (GR 36)
b) Pipe	ASTM A53 (GR 35)
c) HSS (Rectangular)	ASTM 500 (GR B-46)
d) HSS (Round)	ASTM 500 (GR B-42)
e) Threaded Rods	ASTM F1554 (GR 36)
f) Connection Bolts	ASTM A325
g) U-Bolts	SAE J429 (GR 2)
- 6) *Proposed equipment is to be installed in the locations specified in Appendix A. Any changes to the proposed equipment locations will render this report invalid.*

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the mount.

4) ANALYSIS RESULTS

Table 3- Mount Component Capacity

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Face Horizontals	115	79.2	Pass
1	Support Rails		26.9	Pass
1	Grating Support Members		26.0	Pass
1	Standoff Members		38.9	Pass
1	Kick-Brace		14.5	Pass
1	Mount Pipes		37.6	Pass
1	Mount to Tower Connection		70.8	Pass

Mount Rating (max from all components) =	79.2%
-------------------------------------------------	--------------

Notes:

- 1) See additional documentation in "Appendix C – Software Analysis Output" for calculations supporting the % capacity consumed.

4.1) Recommendations

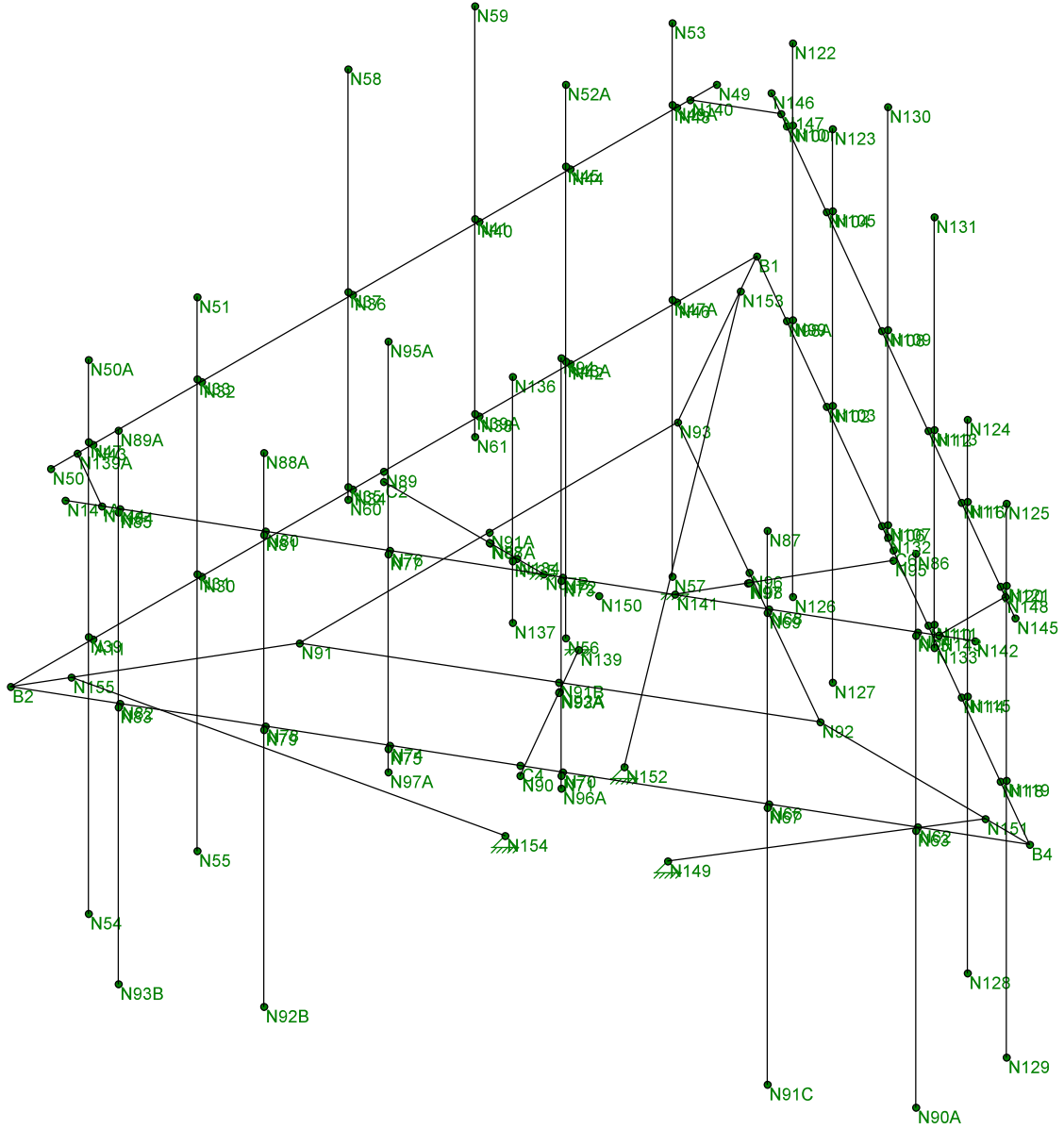
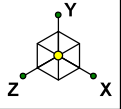
- All referenced proposed modifications designed by B+T (Project #:134993.003.01, dated 05/03/2019) must be installed prior to installation of the proposed loading.

**STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING
SERVICES ON EXISTING MOUNTS BY PAUL J. FORD AND COMPANY**

- 1) It is the responsibility of the client to ensure that the information provided to Paul J. Ford and Company is accurate and complete. Paul J. Ford and Company will rely on the accuracy and completeness of such information in performing or furnishing services under this project.
- 2) If the existing conditions are not as represented on the referenced drawings and/or documents, Paul J. Ford and Company should be contacted immediately to evaluate the significance of the deviation.
- 3) The mount has been analyzed according to the minimum design loads recommended by the Reference Standard. If additional design loads are required, Paul J. Ford and Company should be made aware of this prior to the start of the project.
- 4) The standard of care for all Professional Engineering Services performed or furnished by Paul J. Ford and Company under this project will be the skill and care used by members of the Consultant's profession practicing under similar circumstances at the same time and in the same locality.
- 5) All Services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Paul J. Ford and Company is not responsible for the conclusions, opinions and/or recommendations made by others based on the information supplied herein.

APPENDIX A

WIRE FRAME AND RENDERED MODELS



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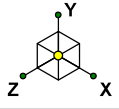
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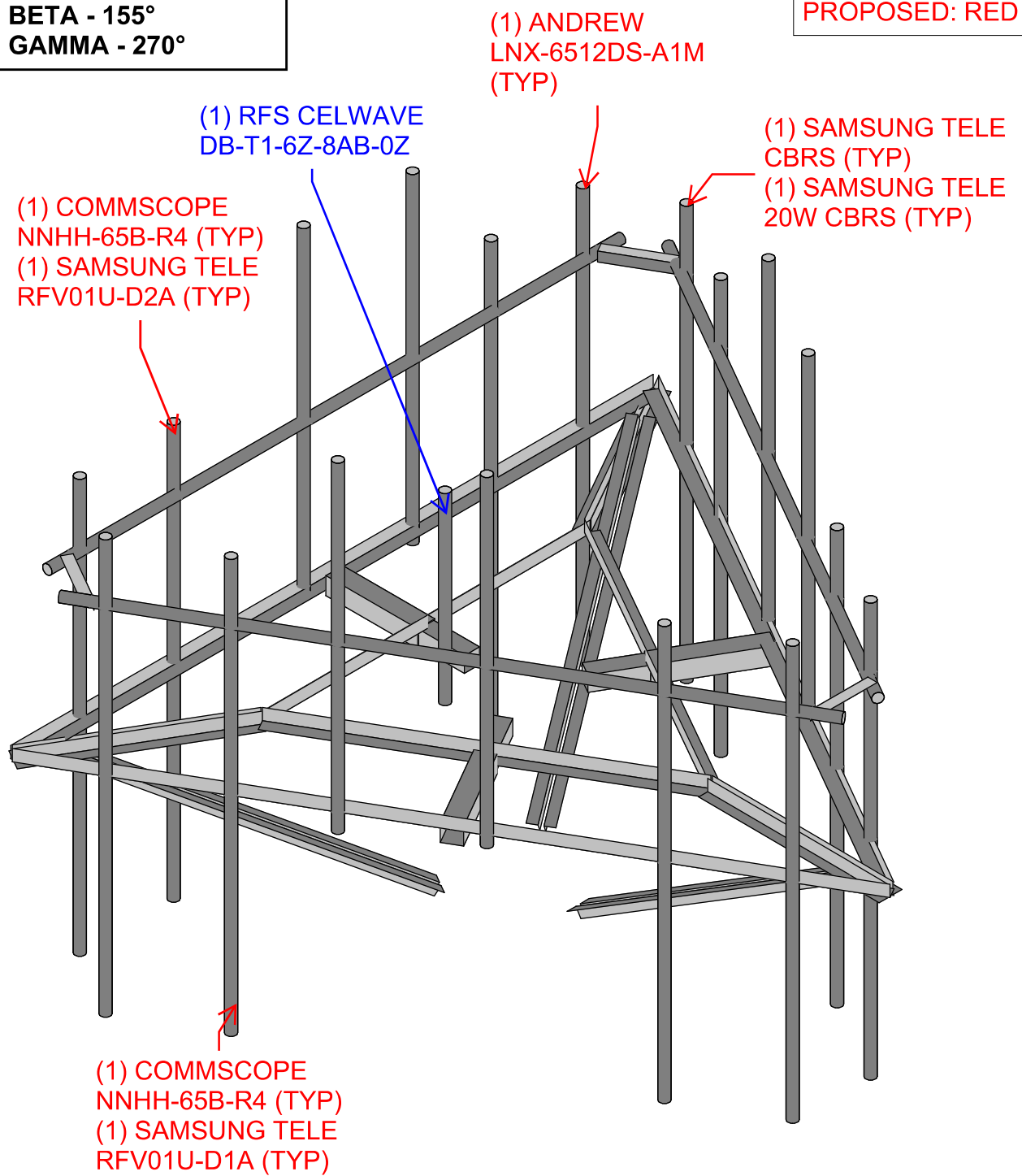
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ANTENNA AZIMUTHS
ALPHA - 45°
BETA - 155°
GAMMA - 270°

LEGEND
EXISTING: BLUE
PROPOSED: RED



NOTES:

- 1) A 6" VERTICAL TOLERANCE FOR PROPOSED EQUIPMENT IS ACCEPTABLE.
- 2) CONTRACTOR TO VERIFY LOCATION OF EXISTING EQUIPMENT PRIOR TO INSTALLATION OF PROPOSED EQUIPMENT. NOTIFY EOR FOR ANY DEVIATIONS.
- 3) INSTALL SHALL NOT CAUSE HARM TO THE STRUCTURE, CLIMBING FACILITY, SAFETY CLIMB OR ANY SYSTEM INSTALLED ON THE STRUCTURE.

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APPENDIX B

SOFTWARE INPUT CALCULATION

Mount Loading per TIA-222-H

Structure & Wind Speed

Analysis Scope = Client
 Structure Type = Mount
 Mount Type = 3 Sectors
 Mount Centrline (Z) = 115 ft
 CIL Y Coordinate = 0 in
 Ultimate Wind Speed = 125 mph
 Service Wind Speed = 30 mph
 Ice Thickness = 30 mph
 Const. Duration = 2 in
 Non-Op Wind Speed = #N/A mph
 Op Wind Speed = 30 mph

Topography

Risk Category = II
 Exposure Category = B
 Topographic Category = 1
 Structure Base Height (Z₀) = 195.7 ft
 Crest Height (H) = ft

Maintenance Point Loads

Load	Label	Node #	Load	Label	Node #
L _{m1} = 500 lbs	N62	61	L ₁ = 250 lbs	B4	4
L _{m2} = 500 lbs	N66	65	L ₂ = 250 lbs	B4	4
L _{m3} = 500 lbs	N78	77	L ₃ = 250 lbs	B2	3
L _{m4} = 500 lbs	N82	81	L ₄ = 250 lbs	B2	3

Velocity Pressure Coefficients

(Table 2-4)
 (Table 2-4)
 (Section 2.6.5.2)

(Section 2.6.6.2.1)
 (Section 16.6)
 (Section 2.6.6)
 (Section 2.6.6)
 (Section 16.6)
 (Annex S - Wind Force)
 (Section 2.6.11.6)

Ice Loading

(Table 2-3)
 (Annex S - Ice)
 (Section 2.6.11.6)
 (Section 2.6.10)
 (Section 2.6.10)
 (Bar Grating Height)
 (Grating Ice Weight)

Wind Pressure

(on all Appurt. / Member Forces)
 (q_z) (G₁) (K_{wp}) =
 (q_z) (G₁) (K_{wp}) =

Antennas

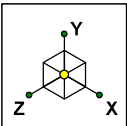
Item	Status	Manufacturer	Antenna	Height (ft)	Width (ft)	Depth (in)	Flat or Round	Weight (lbs)	Sector / Face	Position	Quantity	Orientation	Use In Tower C _A (CFD)	Top/Bottom Mounting Point Spacing (in)	Override Spacing (in)	Max Antenna C/L (ft)	Min Antenna C/L (ft)	Antenna C/L (ft)	Antenna Top Mount Location from Mount Pipe Bottom (in)	Antenna Bottom Mount Location from Mount Pipe Bottom (in)	Override Bottom Antenna Mounting Location (in)	Normal Wind Force per Antenna (lbs)	Transverse Wind Force per Antenna (lbs)
1	P	ANDREW	LNX-651ZDS-A1M_CCI CFD	48.5	11.9	7.1	Flat	28.7	A	6	1	Normal	Yes	42.50	117.229	117.229	112.271	118	75.25	32.75	93.951	56.590	
2	P	ANDREW	LNX-651ZDS-A1M_CCI CFD	48.5	11.9	7.1	Flat	28.7	A	6	1	Normal	Yes	42.50	117.229	117.229	112.271	118	75.25	32.75	93.951	56.590	
3	P	ANDREW	LNX-651ZDS-A1M_CCI CFD	48.5	11.9	7.1	Flat	28.7	A	6	1	Normal	Yes	42.50	117.229	117.229	112.271	118	75.25	32.75	93.951	56.590	
4	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	A	2	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
5	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	A	5	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
6	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	B	2	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
7	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	B	5	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
8	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	C	2	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
9	P	COMMSCOPE	NNHH-658-R4_CCI CFD	72	19.6	7.8	Flat	77.4	C	5	1	Normal	Yes	66.00	116.750	116.750	113.250	118	87.00	21.00	266.137	105.128	
10	P	ANTENNA TELECOMMUNICATIONS	CBRS	16.16	11.39	5.45	Flat	23.14	A	1	1	Normal	No	10.16	119.077	119.077	110.923	118	59.08	48.92	53.672	26.075	
11	P	ANTENNA TELECOMMUNICATIONS	CBRS	16.16	11.39	5.45	Flat	23.14	C	1	1	Normal	No	10.16	119.077	119.077	110.923	118	59.08	48.92	53.672	26.075	
12	P	ANTENNA TELECOMMUNICATIONS	CBRS	24	24	10	Flat	44	A	7	1	Normal	No	18.00	117.083	117.083	114.563	117	47.00	28.00	167.645	69.852	
13	P	ANTENNA TELECOMMUNICATIONS	20W CBRS	12.1	8.5	4.1	Flat	18.64	A	1	1	Normal	No	6.10	119.246	119.246	110.754	116	69.05	62.95	23.935	14.680	
14	P	ANTENNA TELECOMMUNICATIONS	20W CBRS	12.1	8.5	4.1	Flat	18.64	B	1	1	Normal	No	6.10	119.246	119.246	110.754	116	69.05	62.95	23.935	14.680	
15	P	ANTENNA TELECOMMUNICATIONS	20W CBRS	12.1	8.5	4.1	Flat	18.64	C	1	1	Normal	No	6.10	119.246	119.246	110.754	116	69.05	62.95	23.935	14.680	
16	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D1A	15	15	10	Flat	84.4	A	5	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	43.658	
17	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D1A	15	15	10	Flat	84.4	A	5	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	43.658	
18	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D1A	15	15	10	Flat	84.4	B	5	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	43.658	
19	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D1A	15	15	10	Flat	84.4	C	5	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	43.658	
20	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D2A	15	15	8.1	Flat	70.3	A	2	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	35.363	
21	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D2A	15	15	8.1	Flat	70.3	B	2	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	35.363	
22	P	ANTENNA TELECOMMUNICATIONS	RFV01U-D2A	15	15	8.1	Flat	70.3	C	2	1	Normal	No	9.00	118.125	118.125	110.875	116	70.50	61.50	65.468	35.363	

Dishes

Item	Status	Manufacturer	Microwave Dish	Dia (in)	Dish Type	Weight (lbs)	Sector / Face	Position	Top/Bottom Mounting Point Spacing	Override Spacing (in)	Max Dish C/L (ft)	Min Dish C/L (ft)	Dish Top Mount Location from Mount Pipe Bottom	Dish Bottom Mount Location from Mount Pipe Bottom	Override Top Dish Mounting Location (in)	Override Bottom Dish Mounting Location (in)
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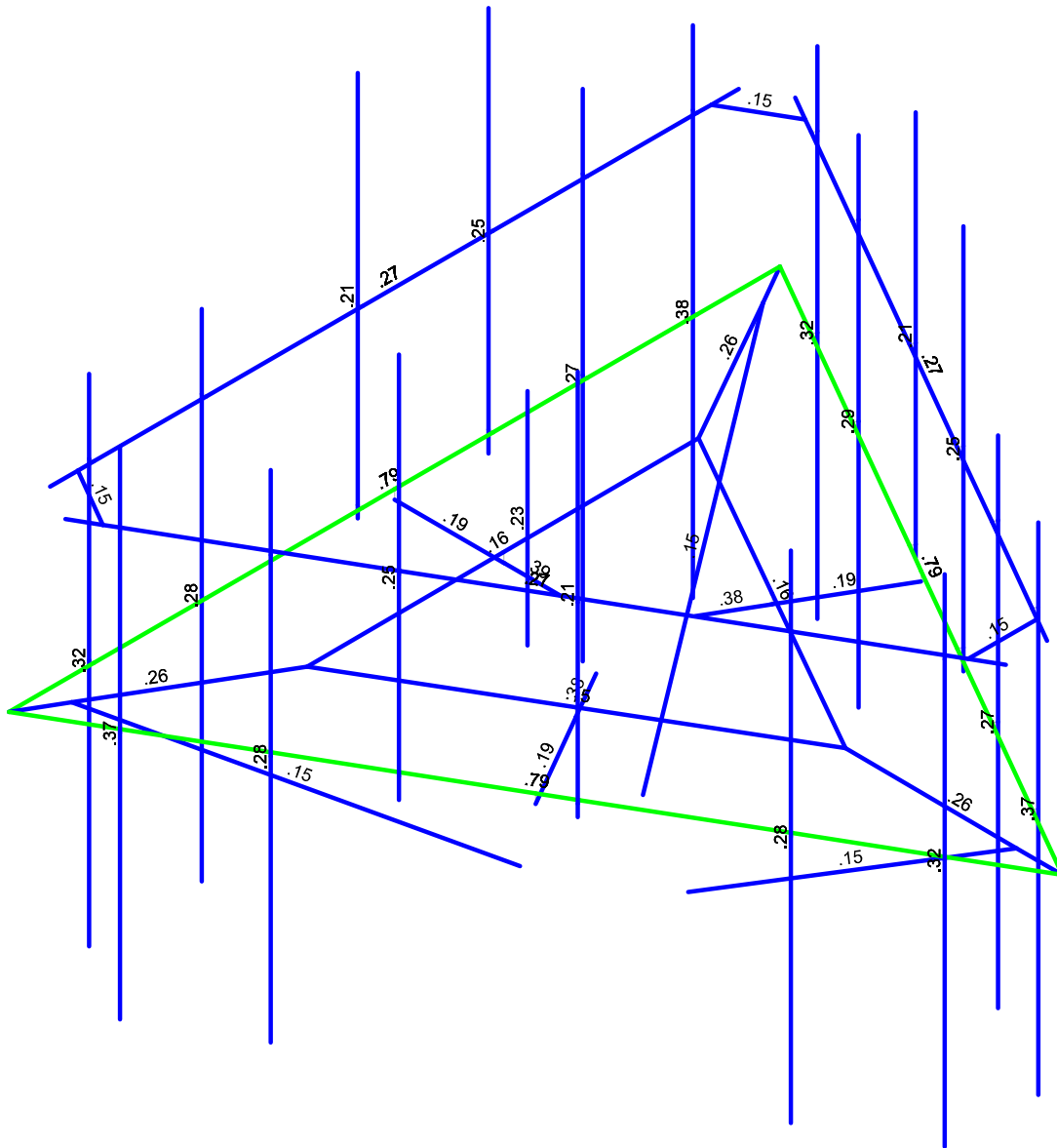
APPENDIX C

SOFTWARE ANALYSIS OUTPUT



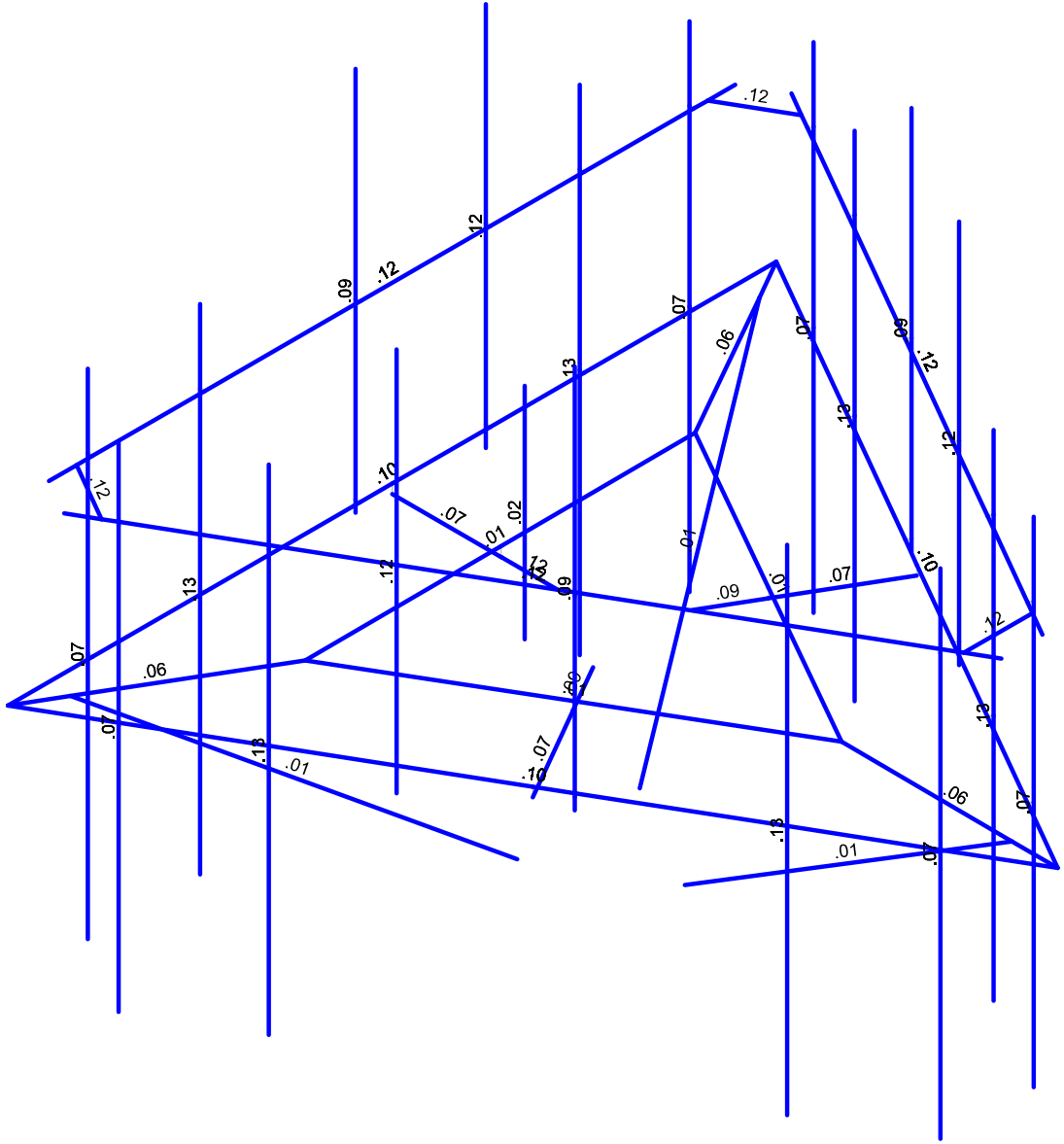
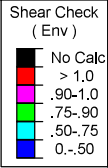
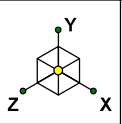
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- .75-.90
- .50-.75
- 0.-.50



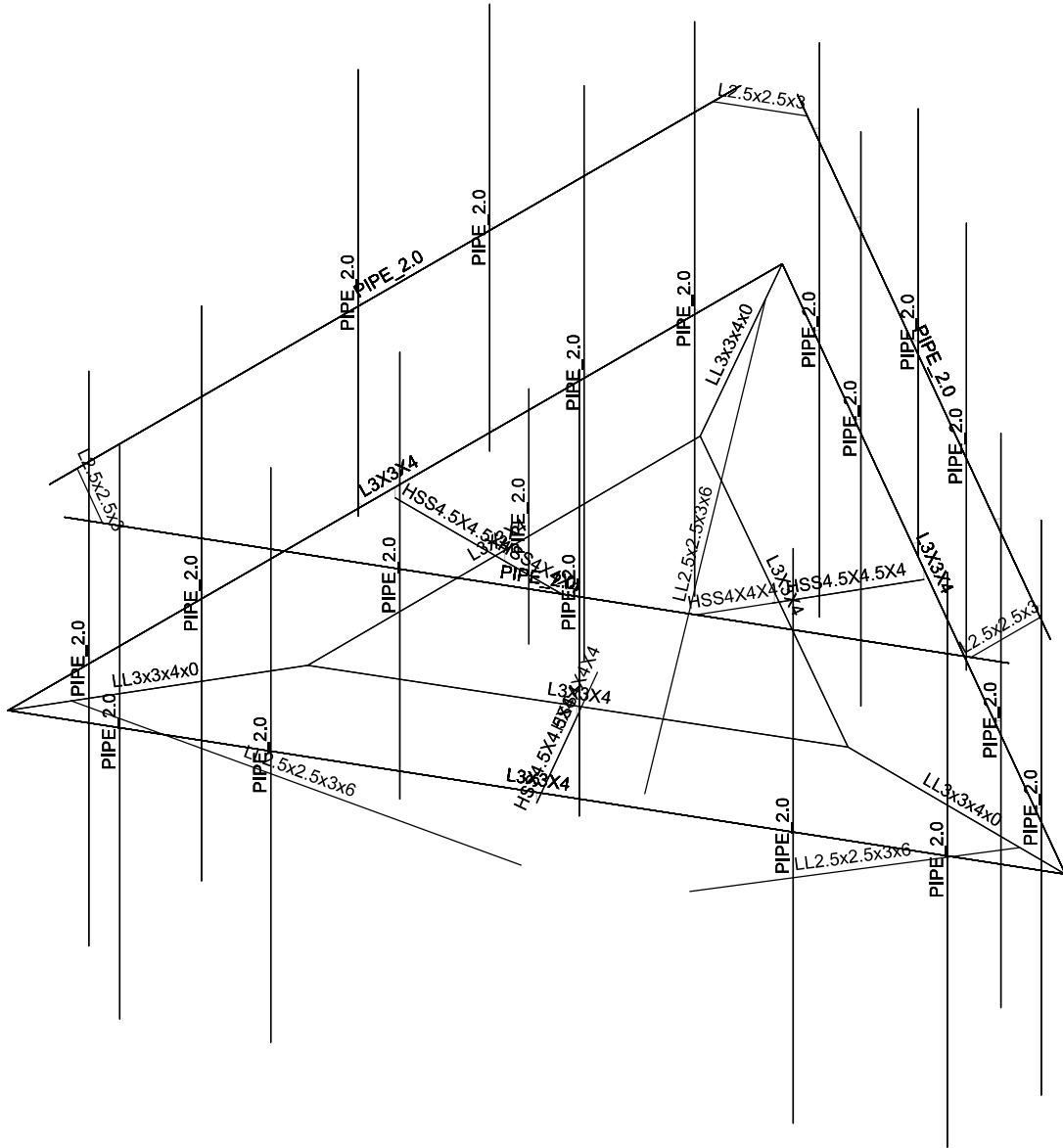
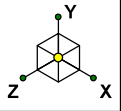
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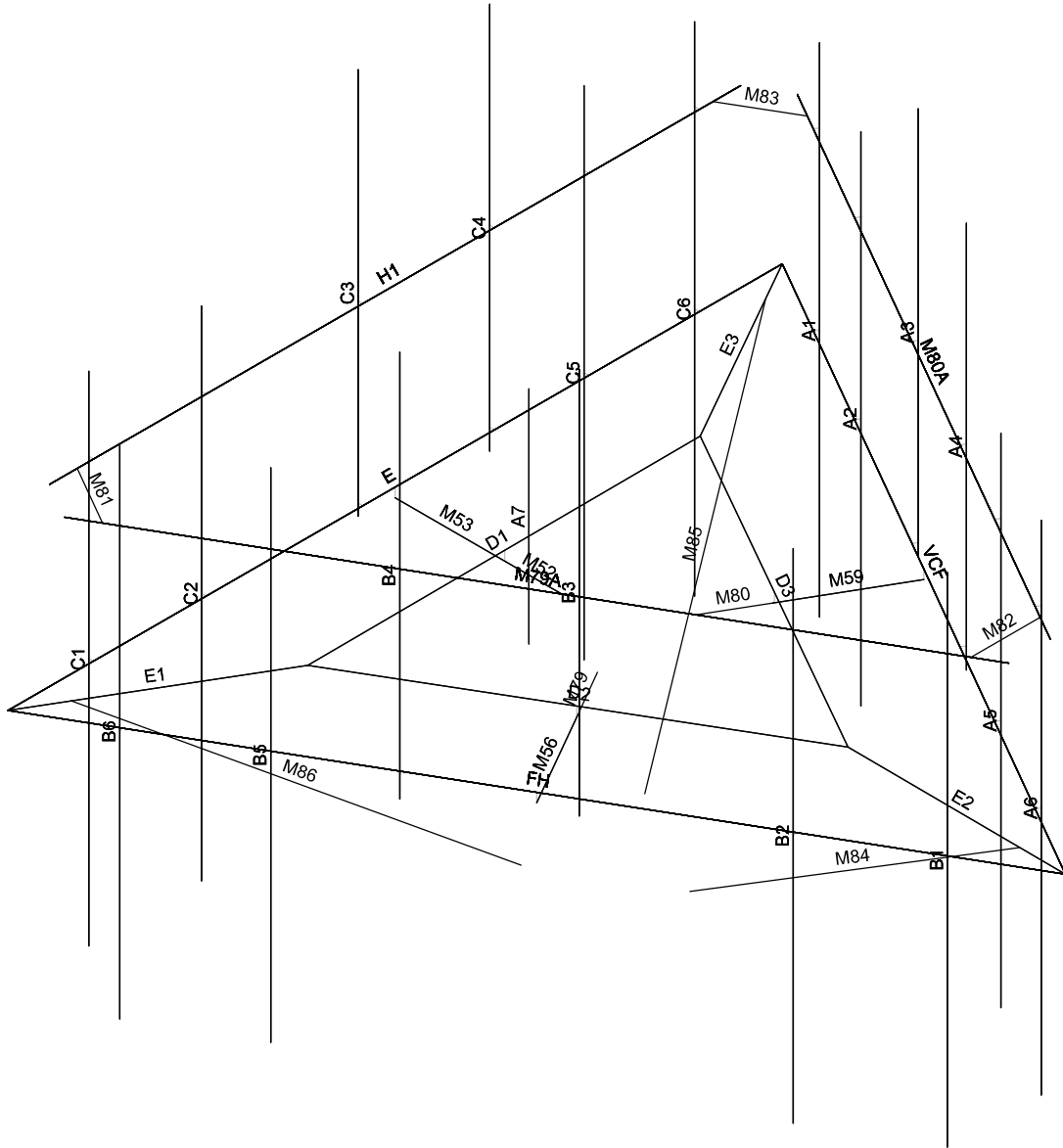
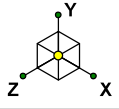
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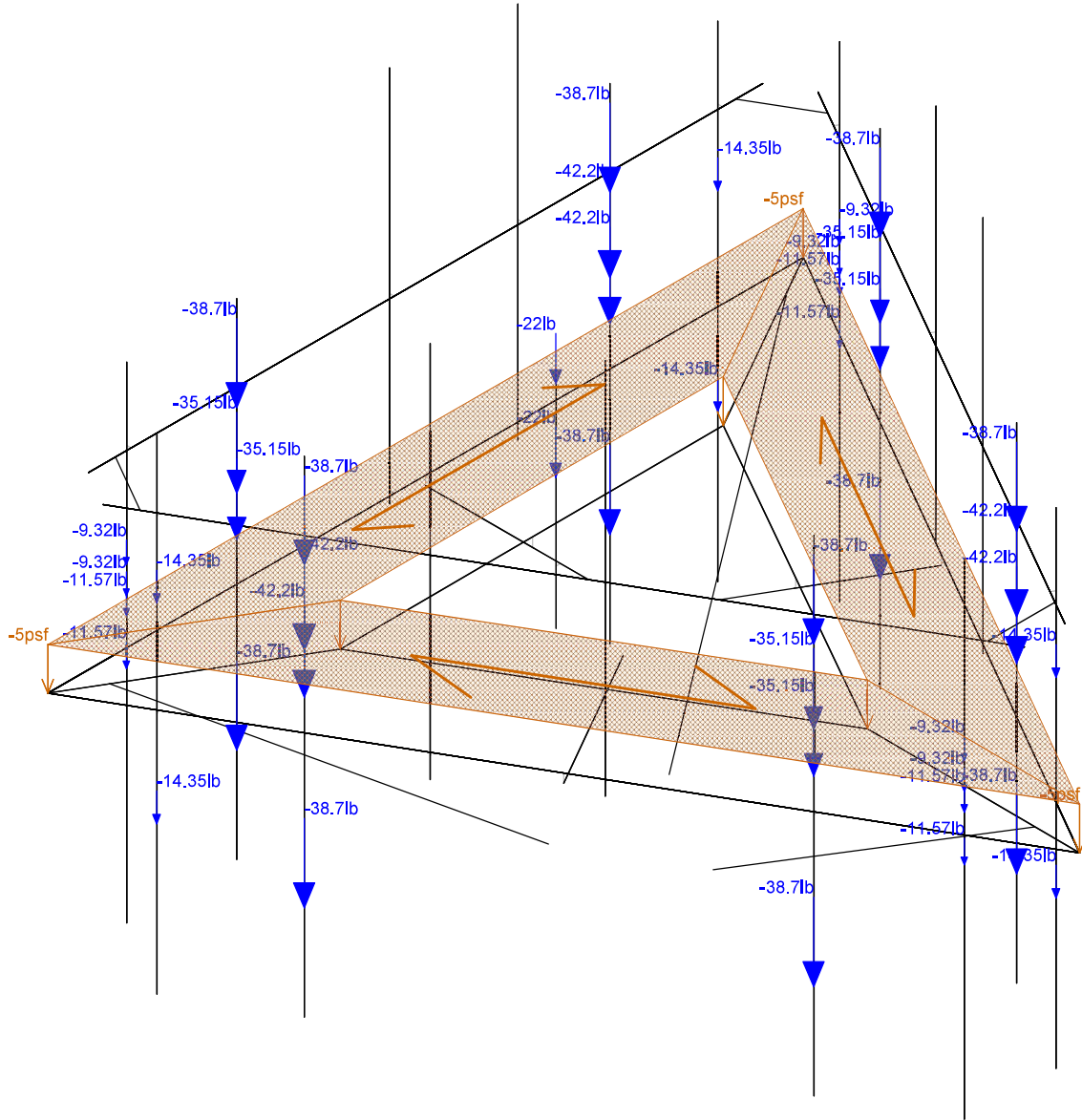
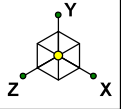
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Loads: BLC 1, Dead
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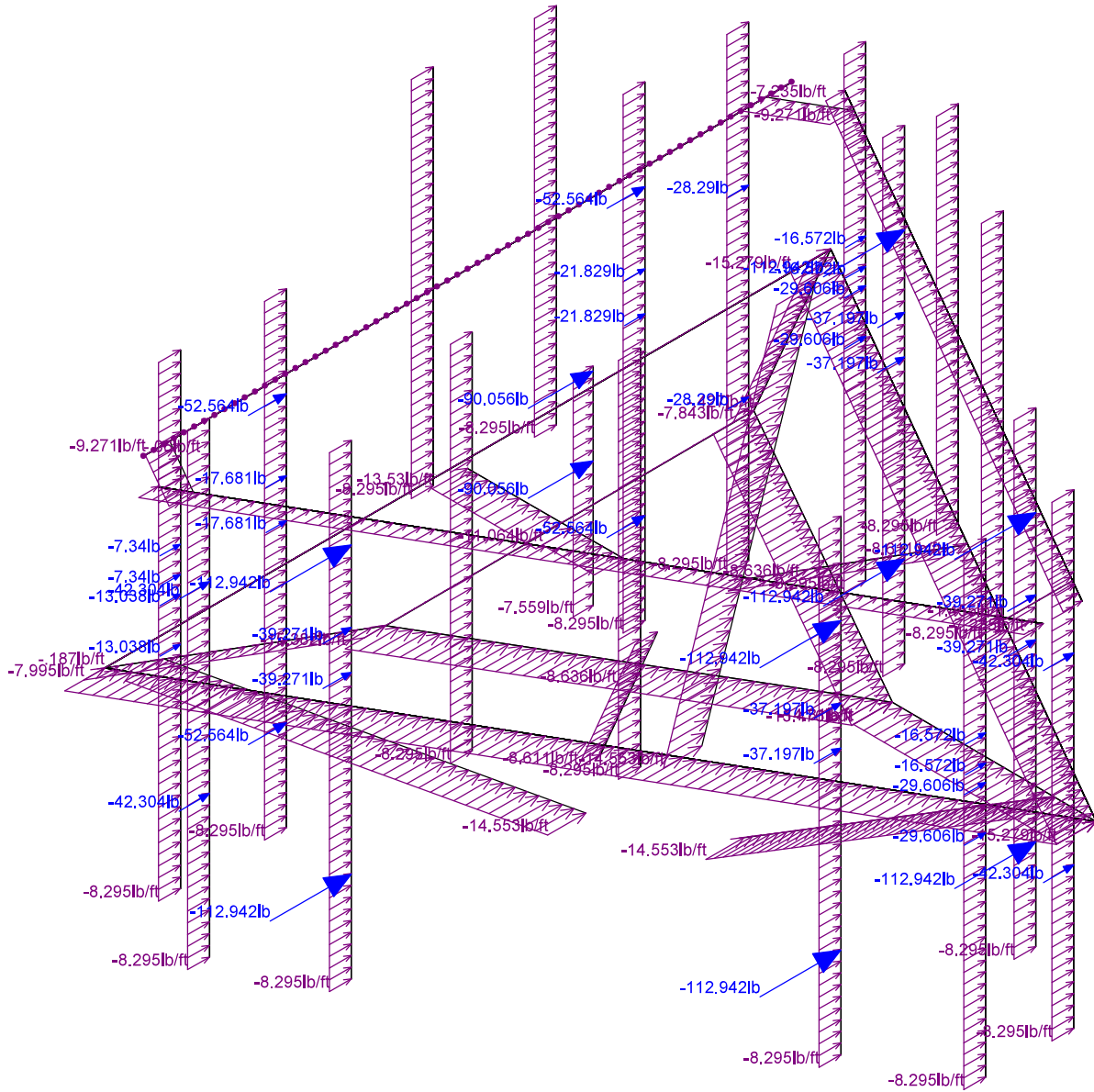
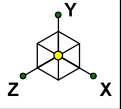
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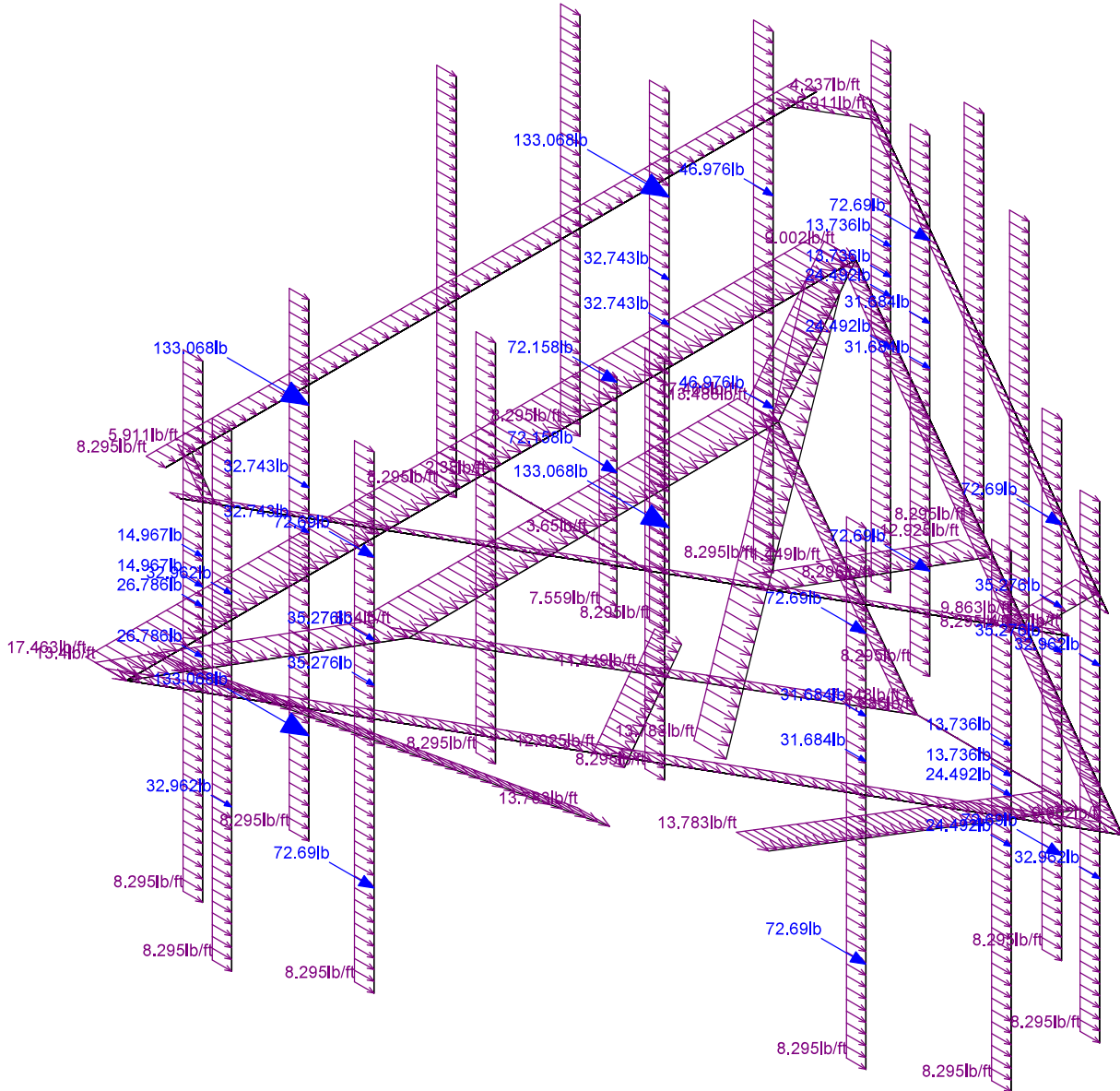
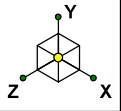


Loads: BLC 2, Wind 0
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Loads: BLC 5, Wind 90
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(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	No
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISACONNECTION CODE	None
Cold Formed Steel Code	None
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parame Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8



(Global) Model Settings, Continued

Seismic Code	ASCE 7-05
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
R X	3
R Z	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Occupancy Cat	I or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (/1E...Density[k/ft...	Yield[ksi]	Ry	Fu[ksi]	Rt	
1	A53 Gr. B (35 ksi)	29000	11154	.3	.65	.49	35	1.5	60	1.2
2	A500 Gr. B (46ksi)	29000	11154	.3	.65	.49	46	1.5	58	1.2
3	A36	29000	11154	.3	.65	.49	36	1.5	58	1.2

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	E	B2	B1			L3X3X4	None	None	A36	Typical
2	FH	B4	B2			L3X3X4	None	None	A36	Typical
3	VCF	B1	B4			L3X3X4	None	None	A36	Typical
4	D1	N93	N91			L3X3X4	None	None	A36	Typical
5	D2	N91	N92			L3X3X4	None	None	A36	Typical
6	D3	N92	N93			L3X3X4	None	None	A36	Typical
7	E1	B2	N91		180	LL3x3x4x0	None	None	A36	Typical
8	E2	N92	B4		180	LL3x3x4x0	None	None	A36	Typical
9	E3	N93	B1		180	LL3x3x4x0	None	None	A36	Typical
10	H1	N50	N49			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
11	Z4	A11	N39			RIGID	None	None	RIGID	Typical
12	Z8	N43	N47			RIGID	None	None	RIGID	Typical
13	M52	N87A	N87B			HSS4X4X4	None	None	A500 Gr. B (46...	Typical
14	M53	C2	N87A			HSS4.5X4.5X4	None	None	A500 Gr. B (46...	Typical
15	M54	C2	N89			RIGID	None	None	RIGID	Typical
16	M55	N88	N91A			RIGID	None	None	RIGID	Typical
17	M56	N90	N92A			HSS4.5X4.5X4	None	None	A500 Gr. B (46...	Typical
18	M57	N90	C4			RIGID	None	None	RIGID	Typical
19	M58	N93A	N91B			RIGID	None	None	RIGID	Typical
20	M59	N95	N97			HSS4.5X4.5X4	None	None	A500 Gr. B (46...	Typical
21	M60	N95	C6			RIGID	None	None	RIGID	Typical
22	M61	N98	N96			RIGID	None	None	RIGID	Typical
23	M25	N30	N31			RIGID	None	None	RIGID	Typical



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 Designer : AMS
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Member Primary Data (Continued)

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
24	M26	N32	N33			RIGID	None	None	RIGID	Typical
25	M27	N34	N35			RIGID	None	None	RIGID	Typical
26	M28	N36	N37			RIGID	None	None	RIGID	Typical
27	M29	N38	N39A			RIGID	None	None	RIGID	Typical
28	M30	N40	N41			RIGID	None	None	RIGID	Typical
29	M31	N42	N43A			RIGID	None	None	RIGID	Typical
30	M32	N44	N45			RIGID	None	None	RIGID	Typical
31	M33	N46	N47A			RIGID	None	None	RIGID	Typical
32	M34	N48	N49A			RIGID	None	None	RIGID	Typical
33	C1	N54	N50A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
34	C2	N55	N51			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
35	C5	N56	N52A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
36	C6	N57	N53			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
37	C3	N60	N58			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
38	C4	N61	N59			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
39	M41	N62	N63			RIGID	None	None	RIGID	Typical
40	M42	N64	N65			RIGID	None	None	RIGID	Typical
41	M43	N66	N67			RIGID	None	None	RIGID	Typical
42	M44	N68	N69			RIGID	None	None	RIGID	Typical
43	M45	N70	N71			RIGID	None	None	RIGID	Typical
44	M46	N72	N73			RIGID	None	None	RIGID	Typical
45	M47	N74	N75			RIGID	None	None	RIGID	Typical
46	M48	N76	N77			RIGID	None	None	RIGID	Typical
47	M49	N78	N79			RIGID	None	None	RIGID	Typical
48	M50	N80	N81			RIGID	None	None	RIGID	Typical
49	M51	N82	N83			RIGID	None	None	RIGID	Typical
50	M52A	N84	N85			RIGID	None	None	RIGID	Typical
51	B1	N90A	N86			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
52	B2	N91C	N87			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
53	B5	N92B	N88A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
54	B6	N93B	N89A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
55	B3	N96A	N94			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
56	B4	N97A	N95A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
57	M59A	N98A	N99			RIGID	None	None	RIGID	Typical
58	M60A	N100	N101			RIGID	None	None	RIGID	Typical
59	M61A	N102	N103			RIGID	None	None	RIGID	Typical
60	M62	N104	N105			RIGID	None	None	RIGID	Typical
61	M63	N106	N107			RIGID	None	None	RIGID	Typical
62	M64	N108	N109			RIGID	None	None	RIGID	Typical
63	M65	N110	N111			RIGID	None	None	RIGID	Typical
64	M66	N112	N113			RIGID	None	None	RIGID	Typical
65	M67	N114	N115			RIGID	None	None	RIGID	Typical
66	M68	N116	N117			RIGID	None	None	RIGID	Typical
67	M69	N118	N119			RIGID	None	None	RIGID	Typical
68	M70	N120	N121			RIGID	None	None	RIGID	Typical
69	A1	N126	N122			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
70	A2	N127	N123			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
71	A5	N128	N124			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
72	A6	N129	N125			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
73	A3	N132	N130			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
74	A4	N133	N131			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
75	M77	N135	N134			RIGID	None	None	RIGID	Typical
76	A7	N137	N136			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
77	M79	N92A	N139			HSS4X4X4	None	None	A500 Gr. B (46...	Typical
78	M80	N97	N141			HSS4X4X4	None	None	A500 Gr. B (46...	Typical
79	M79A	N142	N141A			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical
80	M80A	N146	N145			PIPE 2.0	None	None	A53 Gr. B (35 ...	Typical



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Member Primary Data (Continued)

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
81	M81	N139A	N144		90	L2.5x2.5x3	None	None	A36	Typical
82	M82	N143	N148		90	L2.5x2.5x3	None	None	A36	Typical
83	M83	N147	N140		90	L2.5x2.5x3	None	None	A36	Typical
84	M84	N149	N151			LL2.5x2.5x3x6	None	None	A36	Typical
85	M85	N152	N153			LL2.5x2.5x3x6	None	None	A36	Typical
86	M86	N154	N155			LL2.5x2.5x3x6	None	None	A36	Typical

Member Advanced Data

	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Defl Rat..	Analysis ...	Inactive	Seismic..
1	E						Yes	** NA **			None
2	FH						Yes	** NA **			None
3	VCF						Yes	** NA **			None
4	D1						Yes	** NA **			None
5	D2						Yes	** NA **			None
6	D3						Yes	** NA **			None
7	E1	BenPIN	BenPIN				Yes	** NA **			None
8	E2	BenPIN	BenPIN				Yes	** NA **			None
9	E3	BenPIN	BenPIN				Yes	** NA **			None
10	H1						Yes	** NA **			None
11	Z4						Yes	** NA **		Exclude	None
12	Z8	OOOXOX					Yes	** NA **		Exclude	None
13	M52						Yes	** NA **			None
14	M53						Yes	** NA **			None
15	M54		BenPIN				Yes	** NA **			None
16	M55		BenPIN				Yes	** NA **			None
17	M56						Yes	** NA **			None
18	M57		BenPIN				Yes	** NA **			None
19	M58		BenPIN				Yes	** NA **			None
20	M59						Yes	** NA **			None
21	M60		BenPIN				Yes	** NA **			None
22	M61		BenPIN				Yes	** NA **			None
23	M25						Yes	** NA **		Exclude	None
24	M26	OOOXOX					Yes	** NA **		Exclude	None
25	M27						Yes	** NA **		Exclude	None
26	M28	OOOXOX					Yes	** NA **		Exclude	None
27	M29						Yes	** NA **		Exclude	None
28	M30	OOOXOX					Yes	** NA **		Exclude	None
29	M31						Yes	** NA **		Exclude	None
30	M32	OOOXOX					Yes	** NA **		Exclude	None
31	M33						Yes	** NA **		Exclude	None
32	M34	OOOXOX					Yes	** NA **		Exclude	None
33	C1						Yes	** NA **			None
34	C2						Yes	** NA **			None
35	C5						Yes	** NA **			None
36	C6						Yes	** NA **			None
37	C3						Yes	** NA **			None
38	C4						Yes	** NA **			None
39	M41						Yes	** NA **		Exclude	None
40	M42	OOOXOX					Yes	** NA **		Exclude	None
41	M43						Yes	** NA **		Exclude	None
42	M44	OOOXOX					Yes	** NA **		Exclude	None
43	M45						Yes	** NA **		Exclude	None
44	M46	OOOXOX					Yes	** NA **		Exclude	None
45	M47						Yes	** NA **		Exclude	None
46	M48	OOOXOX					Yes	** NA **		Exclude	None



Member Advanced Data (Continued)

	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Defl Rat...	Analysis ...	Inactive	Seismic...
47	M49						Yes	** NA **		Exclude	None
48	M50	OOOXOX					Yes	** NA **		Exclude	None
49	M51						Yes	** NA **		Exclude	None
50	M52A	OOOXOX					Yes	** NA **		Exclude	None
51	B1						Yes	** NA **			None
52	B2						Yes	** NA **			None
53	B5						Yes	** NA **			None
54	B6						Yes	** NA **			None
55	B3						Yes	** NA **			None
56	B4						Yes	** NA **			None
57	M59A						Yes	** NA **		Exclude	None
58	M60A	OOOXOX					Yes	** NA **		Exclude	None
59	M61A						Yes	** NA **		Exclude	None
60	M62	OOOXOX					Yes	** NA **		Exclude	None
61	M63						Yes	** NA **		Exclude	None
62	M64	OOOXOX					Yes	** NA **		Exclude	None
63	M65						Yes	** NA **		Exclude	None
64	M66	OOOXOX					Yes	** NA **		Exclude	None
65	M67						Yes	** NA **		Exclude	None
66	M68	OOOXOX					Yes	** NA **		Exclude	None
67	M69						Yes	** NA **		Exclude	None
68	M70	OOOXOX					Yes	** NA **		Exclude	None
69	A1						Yes	** NA **			None
70	A2						Yes	** NA **			None
71	A5						Yes	** NA **			None
72	A6						Yes	** NA **			None
73	A3						Yes	** NA **			None
74	A4						Yes	** NA **			None
75	M77						Yes	** NA **			None
76	A7						Yes	** NA **			None
77	M79						Yes	** NA **			None
78	M80						Yes	** NA **			None
79	M79A						Yes	** NA **			None
80	M80A						Yes	** NA **			None
81	M81	OOOOXO	OOOOXO				Yes	** NA **			None
82	M82	OOOOXO	OOOOXO				Yes	** NA **			None
83	M83	OOOOXO	OOOOXO				Yes	** NA **			None
84	M84		BenPIN				Yes	** NA **			None
85	M85		BenPIN				Yes	** NA **			None
86	M86		BenPIN				Yes	** NA **			None

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torqu...	Kyy	Kzz	Cb	Function
1	E	L3X3X4	168	84		Lbyy						Lateral
2	FH	L3X3X4	168	84		Lbyy						Lateral
3	VCF	L3X3X4	168	84		Lbyy						Lateral
4	D1	L3X3X4	85.717			Lbyy						Lateral
5	D2	L3X3X4	85.717			Lbyy						Lateral
6	D3	L3X3X4	85.717			Lbyy						Lateral
7	E1	LL3x3x4x0	47.508			Lbyy						Lateral
8	E2	LL3x3x4x0	47.508			Lbyy						Lateral
9	E3	LL3x3x4x0	47.508			Lbyy						Lateral
10	H1	PIPE 2.0	150			Lbyy						Lateral
11	M52	HSS4X4X4	12									Lateral
12	M53	HSS4.5X4.5...	24									Lateral



Hot Rolled Steel Design Parameters (Continued)

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torqu...	Kyy	Kzz	Cb	Function
13	M56	HSS4.5X4.5...	24									Lateral
14	M59	HSS4.5X4.5...	24									Lateral
15	C1	PIPE 2.0	108									Lateral
16	C2	PIPE 2.0	108									Lateral
17	C5	PIPE 2.0	108									Lateral
18	C6	PIPE 2.0	108									Lateral
19	C3	PIPE 2.0	84									Lateral
20	C4	PIPE 2.0	84									Lateral
21	B1	PIPE 2.0	108									Lateral
22	B2	PIPE 2.0	108									Lateral
23	B5	PIPE 2.0	108									Lateral
24	B6	PIPE 2.0	108									Lateral
25	B3	PIPE 2.0	84									Lateral
26	B4	PIPE 2.0	84									Lateral
27	A1	PIPE 2.0	108									Lateral
28	A2	PIPE 2.0	108									Lateral
29	A5	PIPE 2.0	108									Lateral
30	A6	PIPE 2.0	108									Lateral
31	A3	PIPE 2.0	84									Lateral
32	A4	PIPE 2.0	84									Lateral
33	A7	PIPE 2.0	48									Lateral
34	M79	HSS4X4X4	12									Lateral
35	M80	HSS4X4X4	12									Lateral
36	M79A	PIPE 2.0	150			Lbyy						Lateral
37	M80A	PIPE 2.0	150			Lbyy						Lateral
38	M81	L2.5x2.5x3	15									Lateral
39	M82	L2.5x2.5x3	15									Lateral
40	M83	L2.5x2.5x3	15									Lateral
41	M84	LL2.5x2.5x3...	83.952									Lateral
42	M85	LL2.5x2.5x3...	83.952									Lateral
43	M86	LL2.5x2.5x3...	83.952									Lateral

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead	None		-1.1			44		3	
2	Wind 0	None					88	86		
3	Wind 30	None					88	86		
4	Wind 60	None					88	86		
5	Wind 90	None					88	86		
6	Wind 120	None					88	86		
7	Wind 150	None					88	86		
8	Ice Load	None					44	43	3	
9	Ice 0	None					88	86		
10	Ice 30	None					88	86		
11	Ice 60	None					88	86		
12	Ice 90	None					88	86		
13	Ice 120	None					88	86		
14	Ice 150	None					88	86		
15	Lm1	None				1				
16	Lm2	None				1				
17	Lm3	None				1				
18	Lm4	None				1				
19	Lv1	None				1				
20	Lv2	None				1				
21	Lv3	None				1				



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Basic Load Cases (Continued)

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
22	Lv4	None				1				
23	BLC 1 Transient Area Loads	None						30		
24	BLC 8 Transient Area Loads	None						30		

Load Combinations

Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	
1	1.4 D	Yes	Y		1	1.4																
2	1.2 D + 1.0 Wo @ 0	Yes	Y		1	1.2	2	1														
3	1.2 D + 1.0 Wo @ 30	Yes	Y		1	1.2	3	1														
4	1.2 D + 1.0 Wo @ 60	Yes	Y		1	1.2	4	1														
5	1.2 D + 1.0 Wo @ 90	Yes	Y		1	1.2	5	1														
6	1.2 D + 1.0 Wo @ 120	Yes	Y		1	1.2	6	1														
7	1.2 D + 1.0 Wo @ 150	Yes	Y		1	1.2	7	1														
8	1.2 D + 1.0 Wo @ 180	Yes	Y		1	1.2	2	-1														
9	1.2 D + 1.0 Wo @ 210	Yes	Y		1	1.2	3	-1														
10	1.2 D + 1.0 Wo @ 240	Yes	Y		1	1.2	4	-1														
11	1.2 D + 1.0 Wo @ 270	Yes	Y		1	1.2	5	-1														
12	1.2 D + 1.0 Wo @ 300	Yes	Y		1	1.2	6	-1														
13	1.2 D + 1.0 Wo @ 330	Yes	Y		1	1.2	7	-1														
14	1.2 D + 1.0 Di + 1.0 Wi @ 0	Yes	Y		1	1.2	8	1	9	1												
15	1.2 D + 1.0 Di + 1.0 Wi @ 30	Yes	Y		1	1.2	8	1	10	1												
16	1.2 D + 1.0 Di + 1.0 Wi @ 60	Yes	Y		1	1.2	8	1	11	1												
17	1.2 D + 1.0 Di + 1.0 Wi @ 90	Yes	Y		1	1.2	8	1	12	1												
18	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	13	1												
19	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	14	1												
20	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	9	-1												
21	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	10	-1												
22	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	11	-1												
23	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	12	-1												
24	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	13	-1												
25	1.2 D + 1.0 Di + 1.0 Wi @ ...	Yes	Y		1	1.2	8	1	14	-1												
26	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	2	.058												
27	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	3	.058												
28	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	4	.058												
29	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	5	.058												
30	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	6	.058												
31	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	7	.058												
32	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	2	.058												
33	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	3	.058												
34	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	4	.058												
35	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	5	.058												
36	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	6	.058												
37	1.2 D + 1.5 Lm1 + 1.0 Wm ...	Yes	Y		1	1.2	15	1.5	7	.058												
38	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	2	.058												
39	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	3	.058												
40	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	4	.058												
41	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	5	.058												
42	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	6	.058												
43	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	7	.058												
44	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	2	.058												
45	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	3	.058												
46	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	4	.058												
47	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	5	.058												
48	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	6	.058												
49	1.2 D + 1.5 Lm2 + 1.0 Wm ...	Yes	Y		1	1.2	16	1.5	7	.058												



Company : Paul J. Ford and Company
 Designer : AMS
 Job Number : 37520-0127.001.7190
 Model Name : 806372 | HRT 093 943228

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Load Combinations (Continued)

Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	
50	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	2	.058													
51	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	3	.058													
52	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	4	.058													
53	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	5	.058													
54	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	6	.058													
55	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	7	.058													
56	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	2	.058													
57	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	3	.058													
58	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	4	.058													
59	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	5	.058													
60	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	6	.058													
61	1.2 D + 1.5 Lm3 + 1.0 Wm ...	Yes	Y	1	1.2	17	1.5	7	.058													
62	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	2	.058													
63	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	3	.058													
64	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	4	.058													
65	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	5	.058													
66	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	6	.058													
67	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	7	.058													
68	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	2	-.058													
69	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	3	-.058													
70	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	4	-.058													
71	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	5	-.058													
72	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	6	-.058													
73	1.2 D + 1.5 Lm4 + 1.0 Wm ...	Yes	Y	1	1.2	18	1.5	7	-.058													
74	1.2 D + 1.5 Lv1	Yes	Y	1	1.2	19	1.5															
75	1.2 D + 1.5 Lv2	Yes	Y	1	1.2	20	1.5															
76	1.2 D + 1.5 Lv3	Yes	Y	1	1.2	21	1.5															
77	1.2 D + 1.5 Lv4	Yes	Y	1	1.2	22	1.5															
78	1.0 D	Yes	Y	1	1																	

Envelope Joint Reactions

Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-in]	LC	MY [k-in]	LC	MZ [k-in]	LC	
1	N87B	max	993.272	11	2193.364	21	2395.795	3	9.064	2	20.866	13	-11.475	4
2		min	-1140.959	5	511.161	78	-2384.65	7	-9.177	8	-21.125	7	-69.204	23
3	N139	max	2097.314	11	1917.005	17	1479.785	3	-11.929	2	19.968	9	34.251	17
4		min	-2003.979	5	452.249	78	-1367.429	9	-57.988	20	-20.224	3	4.464	11
5	N141	max	2117.425	11	1917.216	25	1327.218	2	58.066	14	19.717	5	34.231	17
6		min	-2048.346	5	447.578	27	-1466.566	8	11.622	8	-19.974	11	4.747	11
7	N149	max	3661.051	17	2371.302	17	58.827	13	0	78	0	78	0	78
8		min	686.024	11	420.983	11	-58.809	9	0	1	0	1	0	1
9	N152	max	-345.328	8	2372.515	25	-609.404	7	0	78	0	78	0	78
10		min	-1830.458	14	419.623	7	-3164.829	25	0	1	0	1	0	1
11	N154	max	-350.049	2	2372.552	21	3164.973	21	0	78	0	78	0	78
12		min	-1828.536	20	419.42	3	609.131	3	0	1	0	1	0	1
13	Totals:	max	4846.451	11	12894.646	23	4782.146	2						
14		min	-4846.423	5	2977.05	78	-4782.174	8						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

Member	Shape	Code C...	Loc[in]	LC	Shear ...	Loc[in]	Dir	LC	phi*Pnc [lb]	phi*Pnt [lb]	phi*Mn y...	phi*Mn z...	Cb	Eqn	
1	E	L3X3X4	.792	150.5	24	.100	0	y	24	15745.952	46656	20.258	25.927	1	H2-1
2	FH	L3X3X4	.791	150.5	20	.100	0	y	20	15745.952	46656	20.258	25.927	1	H2-1
3	VCF	L3X3X4	.791	150.5	16	.100	0	y	16	15745.952	46656	20.258	25.927	1	H2-1
4	M52	HSS4X4X4	.389	12	22	.115	12	z	8	138935.3...	139518	194.166	194.166	1...	H1-1b
5	M80	HSS4X4X4	.376	12	25	.085	12	z	7	138935.3...	139518	194.166	194.166	1...	H1-1b



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 Designer : AMS
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Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)

Member	Shape	Code C...	Loc[in]	LC	Shear ...	Loc[in]	Dir	LC	phi*Pnc [lb]	phi*Pnt [lb]	phi*Mn y...	phi*Mn z...	Cb	Eqn	
6	C6	PIPE 2.0	.376	54	25	.072	54	12	12143.947	32130	22.459	22.459	1...	H1-1b	
7	M79	HSS4X4X4	.375	12	17	.085	12	z	138935.3...	139518	194.166	194.166	1...	H1-1b	
8	A6	PIPE 2.0	.375	54	17	.072	54	4	12143.947	32130	22.459	22.459	1...	H1-1b	
9	B6	PIPE 2.0	.374	54	21	.072	54	8	12143.947	32130	22.459	22.459	1...	H1-1b	
10	C1	PIPE 2.0	.324	54	21	.069	54	10	12143.947	32130	22.459	22.459	1...	H1-1b	
11	A1	PIPE 2.0	.323	54	25	.069	54	2	12143.947	32130	22.459	22.459	1...	H1-1b	
12	B1	PIPE 2.0	.323	54	17	.069	54	6	12143.947	32130	22.459	22.459	1...	H1-1b	
13	A2	PIPE 2.0	.291	54	4	.133	54	2	12143.947	32130	22.459	22.459	1...	H1-1b	
14	B2	PIPE 2.0	.279	54	9	.133	54	6	12143.947	32130	22.459	22.459	1...	H1-1b	
15	C2	PIPE 2.0	.277	54	13	.133	54	10	12143.947	32130	22.459	22.459	1...	H1-1b	
16	B5	PIPE 2.0	.276	54	12	.128	54	8	12143.947	32130	22.459	22.459	1...	H1-1b	
17	H1	PIPE 2.0	.269	117.1...	23	.116	10.938	2	6295.422	32130	22.459	22.459	1...	H1-1b	
18	M79A	PIPE 2.0	.268	117.1...	19	.116	10.937	10	6295.422	32130	22.459	22.459	1...	H1-1b	
19	M80A	PIPE 2.0	.268	117.1...	15	.116	10.937	6	6295.422	32130	22.459	22.459	1...	H1-1b	
20	A5	PIPE 2.0	.267	54	8	.129	54	4	12143.947	32130	22.459	22.459	1...	H1-1b	
21	C5	PIPE 2.0	.265	54	4	.128	54	12	12143.947	32130	22.459	22.459	1...	H1-1b	
22	E1	LL3x3x4x0	.260	10.392	21	.058	9.897	y	19	76330.895	93312	77.76	58.931	1...	H1-1b
23	E3	LL3x3x4x0	.260	37.116	25	.059	37.61	y	23	76330.895	93312	77.76	58.931	1...	H1-1b
24	E2	LL3x3x4x0	.260	37.116	17	.058	37.61	y	15	76330.895	93312	77.76	58.931	1...	H1-1b
25	A4	PIPE 2.0	.250	5.25	25	.121	42	4	17855.085	32130	22.459	22.459	2...	H1-1b	
26	B4	PIPE 2.0	.250	5.25	17	.121	42	8	17855.085	32130	22.459	22.459	2...	H1-1b	
27	C4	PIPE 2.0	.250	5.25	21	.121	42	12	17855.085	32130	22.459	22.459	2...	H1-1b	
28	A7	PIPE 2.0	.228	12	10	.021	12	10	26521.424	32130	22.459	22.459	1...	H1-1b	
29	B3	PIPE 2.0	.209	2.625	9	.092	2.625	5	17855.085	32130	22.459	22.459	2...	H1-1b	
30	A3	PIPE 2.0	.209	2.625	5	.092	2.625	13	17855.085	32130	22.459	22.459	2...	H1-1b	
31	C3	PIPE 2.0	.209	2.625	13	.092	2.625	9	17855.085	32130	22.459	22.459	1...	H1-1b	
32	M56	HSS4.5X4.5X4	.188	24	22	.072	24	z	3	156914.6...	158976	250.884	250.884	1...	H1-1b
33	M59	HSS4.5X4.5X4	.188	24	18	.071	24	z	7	156914.6...	158976	250.884	250.884	1...	H1-1b
34	M53	HSS4.5X4.5X4	.188	24	14	.071	24	z	7	156914.6...	158976	250.884	250.884	1...	H1-1b
35	D1	L3X3X4	.158	42.858	71	.012	85.717	y	69	15152.423	46656	20.258	38.243	1...	H2-1
36	D3	L3X3X4	.158	41.966	33	.012	0	y	35	15152.423	46656	20.258	37.909	1...	H2-1
37	D2	L3X3X4	.147	41.966	3	.012	85.717	y	69	15152.423	46656	20.258	38.937	1...	H2-1
38	M81	L2.5x2.5x3	.146	0	8	.116	15	z	6	27407.4	29192.4	10.471	23.662	1...	H2-1
39	M83	L2.5x2.5x3	.146	0	12	.116	15	z	10	27407.4	29192.4	10.471	23.662	1...	H2-1
40	M82	L2.5x2.5x3	.146	0	4	.115	15	z	2	27407.4	29192.4	10.471	23.662	1...	H2-1
41	M85	LL2.5x2.5x3x6	.145	41.976	15	.006	83.952	y	25	31242.507	58320	55.717	30.294	1...	H1-1b
42	M84	LL2.5x2.5x3x6	.145	41.976	19	.006	83.952	y	18	31242.507	58320	55.717	30.294	1...	H1-1b
43	M86	LL2.5x2.5x3x6	.145	41.976	19	.006	0	y	21	31242.507	58320	55.717	30.294	1...	H1-1b

PF PAUL J. FORD & COMPANY Y

250 E Broad St, Ste 600 • Columbus, OH 43215
Phone 614.221.6679 www.pauljford.com

Project # **37520-0127.001.7190**

By **AMS**

Date: 01/21/20

v0.1, Effective 07/10/18

MOUNT TO TOWER CONNECTION CHECKS

REACTIONS

Px= **2.396** Kip
Py= **2.193** Kip
(Axial)Pz= **1.141** Kip
Mx= **69.204** Kip-in
My= **21.125** Kip-in
(Torque)Mz= **9.177** Kip-in

WELD CHECKS

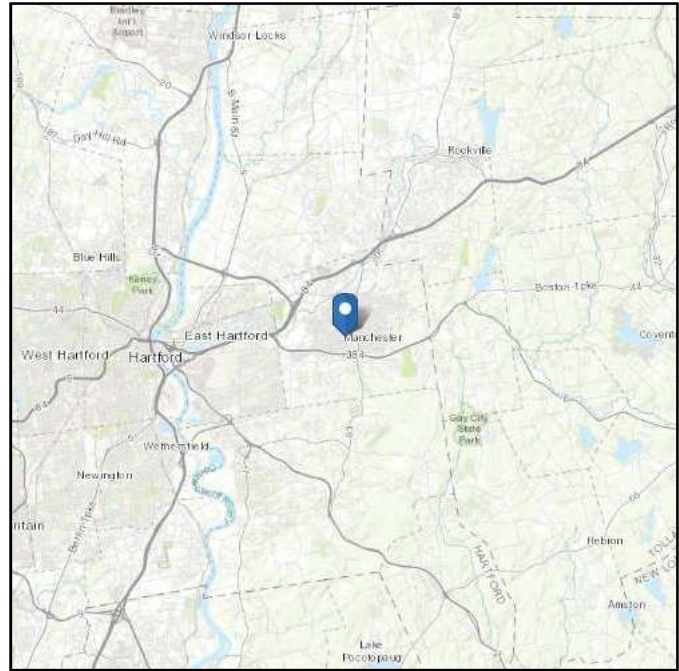
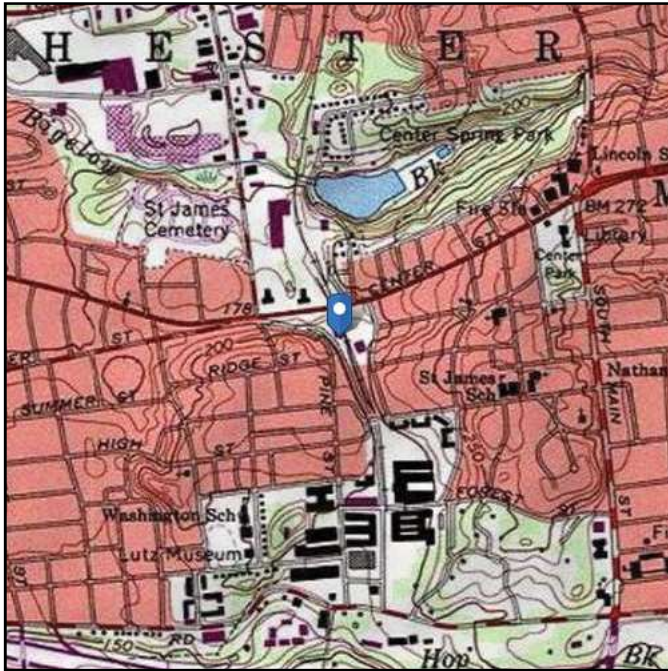
Standoff Member Type	=	Square
Width	=	4 in
Depth (only for square members)	=	4 in
Assumed Weld Size	=	0.1875
Total Forces in X direction	=	0.515 kips
Total Forces in Y direction	=	0.489 kips
Total Forces in Z direction	=	2.87 kips
Resultant	=	2.96 kips
$\Phi * F_w$ (Kip/in)/16" weld	=	1.392
Capacity used		70.81%

ASCE 7 Hazards Report

Address:
No Address at This
Location

Standard: ASCE/SEI 7-10
Risk Category: II
Soil Class: D - Stiff Soil

Elevation: 195.7 ft (NAVD 88)
Latitude: 41.771944
Longitude: -72.530222



Wind

Results:

Wind Speed:	124 Vmph
10-year MRI	77 Vmph
25-year MRI	87 Vmph
50-year MRI	94 Vmph
100-year MRI	101 Vmph

Data Source: ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of March 12, 2014

Date Accessed: Tue Apr 02 2019

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

Ice

Results:

Ice Thickness: 1.00 in.

Concurrent Temperature: 5 F

Gust Speed: 50 mph

Data Source: Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8

Date Accessed: Tue Apr 02 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided “as is” and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

APPENDIX D

POST MODIFICATION INSPECTION (PMI) REQUIREMENTS FOR DESKTOP REVIEW

Post Modification Inspection (PMI) Report Requirements Documents & Photos Required from Contractor

Purpose – to provide PJF the proper documentation in order to complete the required Mount Desktop review of the Post Modification Inspection Report.

- Contractor is responsible for making certain the photos provided as noted below provide confirmation that the modification was completed in accordance with the modification drawings.
- Contractor shall relay any data that can impact the performance of the mount or the mount modification, this includes safety issues.

Base Requirements:

- Provide “as built drawings” showing contractor’s name, preparer’s signature, and date. Any deviations from the drawing (proposed modification) must be shown.
- Notation that all hardware was properly installed, and the existing hardware was inspected for any issues.
- Verification that loading is as communicated in the modification drawings. NOTE if loading is different than what is conveyed in the modification drawing contact PJF immediately.
- Each photo should be time and date stamped.
- Photos should be high resolution and submitted in a Zip File and should be organized in the file structure as depicted in Schedule A attached.
- Any special photos outside of the standard requirements will be indicated on the drawings.
- Contractor shall ensure that the safety climb wire rope is supported and not adversely impacted by the install of the modification components. This may involve the install of wire rope guides, or other items to protect the wire rope.
- The photos in the file structure should be uploaded to pjfmount@pauljford.com as depicted on the drawings.

Photo Requirements:

- Base and “During Installation Photos”
 - Base pictures include
 - Photo of Gate Signs showing the tower owner, site name, and number.
 - Photo of carrier shelter showing the carrier site name and number if available.
 - Photos of the galvanizing compound and/or paint used (if applicable), clearly showing the label and name.
 - “During Installation” Photos if provided – must be placed only in this folder
- Photos taken at ground level
 - Overall tower structure before and after installation of the modifications
 - Photos of the appropriate mount before and after installation of the modifications; if the mounts are at different rad elevations, pictures must be provided for all elevations that the modifications were installed.
- Photos taken at Mount Elevation
 - Photos showing each individual sector before and after installation of modifications. Each entire sector must be in one photo to show in the inter-connection of members.
 - Close-up photos of each installed modification per the modification drawings; pictures should also include connection hardware (U-bolts, bolts, nuts, all-threaded rods, etc.)
 - Photos showing the measurements of the installed modification member sizes (i.e. lengths, widths, depths, diameters, thicknesses).
 - Photos showing the elevation or distances of the installed modifications from the appropriate reference locations shown in the modification drawings.

Schedule A – Photo & Document File Structure

- VzW Site Number / Name
 - Base & “During Installation” Photos
 - Pre-Installation Photos
 - Alpha
 - Beta
 - Gamma
 - Ground Level
 - Tape Drop
 - Post-Installation Photos
 - Alpha
 - Beta
 - Gamma
 - Ground Level
 - Tape Drop
 - Material Certification – Submission of this document including executed certification on Page 2
 - Specific Required Additional Photos
 - Required Additional Photos

Special Instructions / Validation as required from the MA or any other information the contractor deems necessary to share that was identified:

Issue:

Response:

Exhibit F

Power Density/RF Emissions Report

General Power Density

Site Name: Manchester, CT
 Cumulative Power Density

Operator	Operating Frequency (MHz)	Number of Trans.	ERP Per Trans. (watts)	Total ERP (watts)	Distance to Target (feet)	Calculated Power Density (mW/cm ²)	Maximum Permissible Exposure* (mW/cm ²)	Fraction of MPE (%)
CBRS	3500	1	50	50	115	0.0014	1.0	0.14%
VZW PCS	1970	1	4690	4690	115	0.1275	1.0	12.75%
VZW Cellular LTE	869	1	1470	1470	115	0.0400	0.5793333333	6.90%
VZW Cellular	869	2	389	778	115	0.0212	0.5793333333	3.65%
VZW AWS	2145	1	4860	4860	115	0.1322	1.0	13.22%
VZW 700	746	1	2470	2470	115	0.0672	0.4973333333	13.51%

Total Percentage of Maximum Permissible Exposure

50.16%

*Guidelines adopted by the FCC on August 1, 1996, 47 CFR Section 1.13101 based on NCRP Report 86, 1986 and generally on ANSI/IEEE C95.1-1992

MHz = Megahertz

mW/cm² = milliwatts per square centimeter

ERP = Effective Radiated Power

Absolute worst case maximum values used, including the following assumptions:

1. closest accessible point is distance from antenna to base of pole;
2. continuous transmission from all available channels at full power for indefinite time period; and,
3. all RF energy is assumed to be directed solely to the base of the pole.