

**From:** Kri Pelletier [mailto:KPelletier@sbsite.com]  
**Sent:** Friday, March 30, 2018 12:22 PM  
**To:** Galligan, Coleen  
**Cc:** CSC-DL Siting Council; Rick Woods  
**Subject:** RE: Incomplete - EM-SPRINT-073-180321 - Mell Rd

Good Afternoon Coleen,

The provided Structural Report does list the New Mount Augmentation items provided on sheet S3 of GeoStructural's Mount Augmentation plans. (Sheet A-3 of Infinigy's plans listed preliminary mount augmentation which was then refined with GeoStructural's plans. Both were submitted to Council.)

As to site plan sheet T-1's note, it is addressed with the attached passing Structural Assessment.

Please let me know if you need anything further.

Thank you,

**Kri Pelletier**  
*Prop Spec - Svcs*

508.251.0720 x3804 + **T**  
508.366.2610 + **F**  
203.446.7700 + **C**

**From:** Galligan, Coleen [mailto:Coleen.Galligan@ct.gov]  
**Sent:** Thursday, March 29, 2018 3:46 PM  
**To:** Kri Pelletier <KPelletier@sbsite.com>  
**Cc:** CSC-DL Siting Council <Siting.Council@ct.gov>  
**Subject:** Incomplete - EM-SPRINT-073-180321 - Mell Rd

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Please see the attached correspondence.

Coleen Galligan  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051  
(860) 827-2935  
[Coleen.Galligan@ct.gov](mailto:Coleen.Galligan@ct.gov)

## Antenna Mount Structural Analysis



Source: SBA Date: 11.13.2017

SBA Site: CT00167-S Lisbon  
Sprint Site Number: CT23XC404  
Project: Sprint DO Macro Upgrade

Prepared For: Sprint

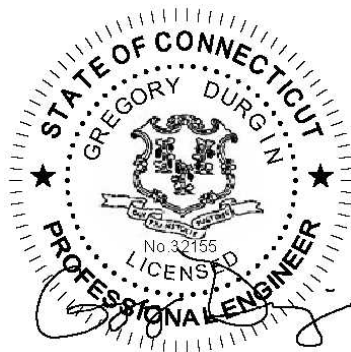
Mount Description: (3) Sector Frames

Site Location: Lisbon, CT  
New London County  
41.591033°, -72.01696°

Design Codes: ANSI/TIA-222-G  
IBC 2012 w/ 2016 CT Building Code

Analysis Load Case: Sprint Final Configuration

Analysis Result: Adequate @ 74% - Once Augmented  
See Conclusion



Revision 0  
March 7, 2018

## **1.0 Introduction**

An antenna mount structural analysis has been performed on Sprint's existing mount assembly located at the CT00167-S Lisbon communications site in New London County, CT considering the final equipment loading configuration listed in Section 3.0.

## **2.0 Analysis Criteria**

An elastic three-dimensional model of the mount structure has been analyzed pursuant to the following criteria:

- IBC 2012 - International Building Code.
- ANSI/TIA-222-G - Structural Standard for Antenna Supporting Structures and Antennas.
- AISC - Steel Construction Manual.
- ANSI/AWS D1.1 - Structural Welding Code.

Wind w/o ice = 135 mph (3-sec gust Ultimate Wind Speed)	
Wind w/o ice = 105 mph (3-sec gust Equivalent per TIA-222-G Tower Code)	
Wind with ice = 50 mph (3-sec gust, 3/4" Ice)	Topographic Category 1
Exposure Category C	Structure Class II

The following documents were provided:

<ul style="list-style-type: none"> <li>• <u>Prelim Construction Drawings</u> Infinigy, 2/20/18.</li> <li>• <u>Mount and Tower Record Documents</u> SBA</li> <li>• <u>Mount Assessment</u> Westchester, 12/21/17.</li> <li>• <u>RF Design</u> Sprint DOMU Project</li> </ul>
---

The results of the analysis are illustrated in Section 4.0. If any of the existing or proposed conditions reported in this analysis are not properly represented, please contact our office immediately to request an amended report.

### **3.0 Appurtenance Information**

**Table 3.1 – Sprint Final Configuration<sup>1</sup>**

<b>COR</b>	<b>(Quantity) Appurtenance Make/Model</b>	<b>Mount Description</b>
173.0'±	(3) RFS APXVSP18-C-A20	(3) Sector Frames
	(3) ANDREW DT465B-2XR	
	(6) ALU 800MHz RRH	
	(3) ALU 1900MHz RRH	
	(3) ALU 2500MHz RRH	

1. Refer to antenna installation Construction Drawings (by others, when applicable) for additional information regarding final antenna and equipment orientations.
2. Panel antennas to be installed in Positions 1 and 2 with a horizontal separation not to exceed 4.5'. Existing 800 and 1900 RRH units to remain in their currently installed locations on the sector frame standoffs. New 800 and 2500 RRH units to be installed behind each panel antenna on dual RRH swivel brackets (one RRH per panel mount pipe).

### **4.0 Analysis Results**

**Table 4.1 – Existing Mount Capacity**

<b>Load Case</b>	<b>Governing Mount Component<sup>1</sup></b>	<b>% Capacity<sup>2</sup></b>	<b>Result</b>
Final Sprint Configuration	Angle Top Rail	>200%	<b>Inadequate<sup>3</sup></b>

1. Refer to the Calculations & Software Output portion of this report for mount component and structural information.
2. Listed results are expressed as a percentage of available mount member capacity based upon the assumed material strengths listed in Table 4.3. 105% is an acceptable allowable stress percentage for mount components.
3. Structural augments to the existing mount structure are required to obtain a mount structure capable of supporting the currently proposed final loading configuration in Table 3.1.

**Table 4.2 – Augmented Mount Capacity**

Load Case	Governing Mount Component <sup>1</sup>	% Capacity <sup>2</sup>	Result
Final Sprint Configuration	Standoff Connection Plates	70%	<b>Adequate Once Augmented<sup>3</sup></b>

1. Refer to the Calculations & Software Output portion of this report for mount component and structural information.
2. Listed results are expressed as a percentage of available mount member capacity based upon the assumed material strengths listed in Table 4.3. 105% is an acceptable allowable stress percentage for mount components.
3. Refer to [GeoStructural Mount Augmentation Drawings](#) and Section 5.0 for information regarding required mount augments.

**Table 4.3 – Structural Component Material Strengths**

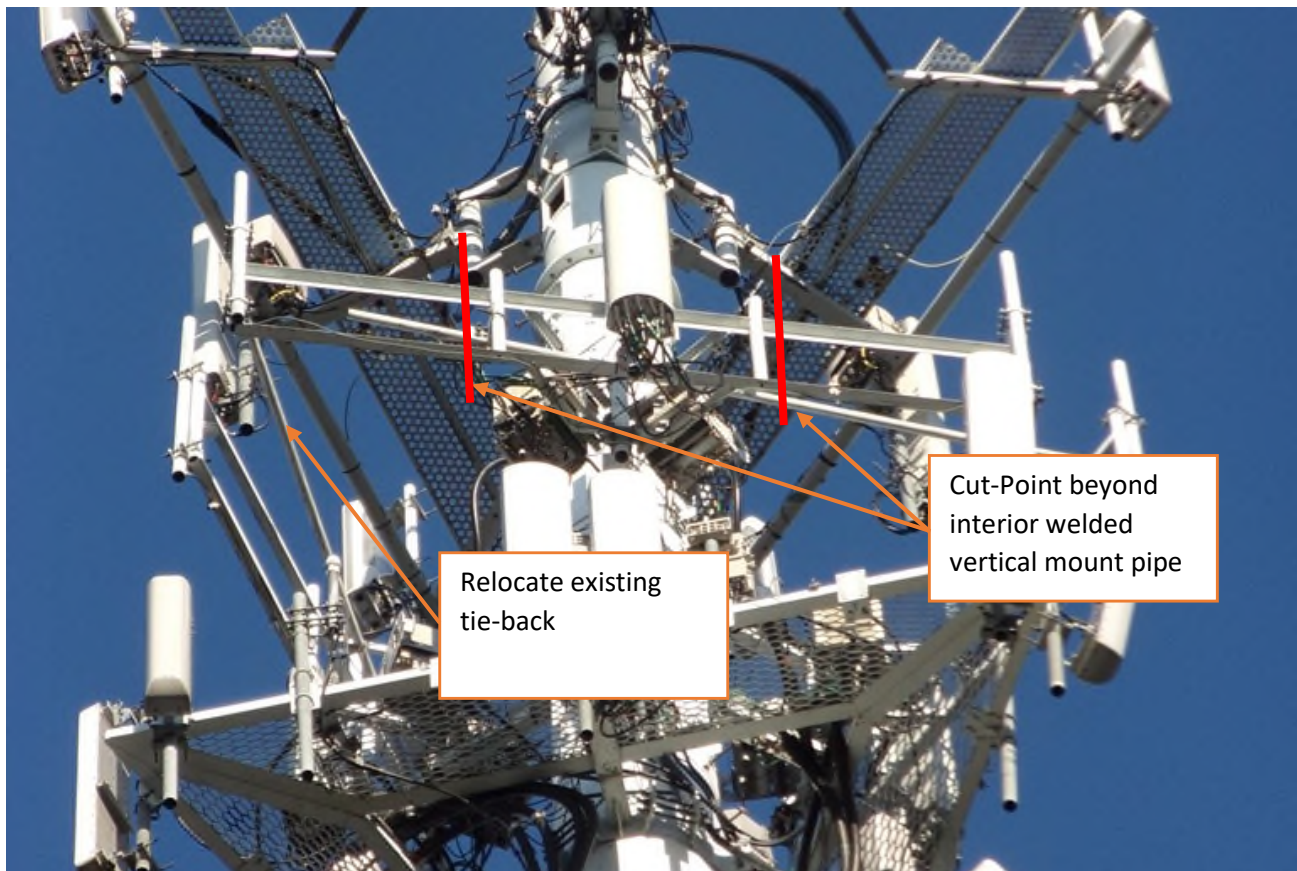
Structural Component	Nominal Strength/Material <sup>4</sup>
Pipe	F <sub>y</sub> = 35 ksi (A53, Gr. B)
Tube	F <sub>y</sub> = 46 ksi (A500, Gr. B)
Structural Shapes (L, C, W, etc.), Plate / Bar	F <sub>y</sub> = 36 ksi (A36)
Uni-Strut	F <sub>y</sub> = 33 ksi (A570, Gr. 33)
Connection Bolts	A325
Stainless Steel Bolts	18-8 Stainless, Grade 316/304 F <sub>y</sub> = 74 ksi (Yield) & F <sub>u</sub> = 29 ksi (Tension)
U-Bolts / Threaded Rod	SAE J429 Grade 2 (Substitution: ASTM A449) F <sub>y</sub> = 57 ksi (Yield) & F <sub>u</sub> = 74 ksi (Tension)
Welds	E70XX Electrodes

1. Strengths listed were assumed for this analysis and are based upon ASTM, AISC, RCSC, AWS and ACI preferred specification values. Values and materials are consistent with industry standards. Material strengths were taken from original design documents when available.

## 5.0 Conclusion & Recommendations

Based on Sprint's final equipment loading configuration, the existing mount assembly does not have sufficient capacity to support the loading considered in this analysis pursuant to the listed standards. Structural augments (reinforcements) will be required and are briefly summarized below:

- Modify (Cut) the front face of the mount to a 4.5' face width;
  - Existing tie-back to be relocated. Top and bottom angle rails to be cut just beyond the welded interior mount pipes.
- Install V-Brace Kit; located 1.0' above the existing mount top face rail.
  - Sitepro1 PRK-SFR-K-L, (3) total. Attach SFR-K-L to existing tower legs.
  - Pipe2.0STD x 7.0' Horizontal Rail, (3) total. Attach new rail to SFR-K.
  - Sitepro1 SCX1-K, (6) total. Attach new mount pipes to new rail.
- Panel antennas to be installed in Positions 1 and 2 with a horizontal separation not to exceed 4.5'. Existing 800 and 1900 RRH units to remain in their currently installed locations on the sector frame standoffs. New 800 and 2500 RRH units to be installed behind each panel antenna on dual RRH swivel brackets (one RRH per panel mount pipe).



Once the recommended augments are successfully implemented, the **augmented** mount assembly has sufficient capacity to support the loading considered in this analysis pursuant to the listed standards.

**Augmentation Requirements:**

- **In order to obtain a mount structure capable of supporting the currently proposed final loading configuration, upgrade augments must be installed in accordance with GeoStructural's Mount Augmentation Drawings.**
- **Antennas and equipment shall be installed centered vertically on the mount front face rails. If this assumption is incorrect, the results of this analysis will be affected.**

This analysis only encompasses the antenna mount assembly. The tower, overall mount support structure, foundation, etc. are beyond the scope of this analysis. If any of the existing or proposed conditions (appurtenance loading, member sizes, etc.) reported in this analysis are not properly represented, please contact our office immediately to request an amended report.

Prepared by:



**Jesse Drennen, PE, MLE**  
208.761.7986  
[jesse.drennen@geostructural.com](mailto:jesse.drennen@geostructural.com)

Reviewed and Approved by:



**Don George, PE, SE, MLSE**  
208.602.6569  
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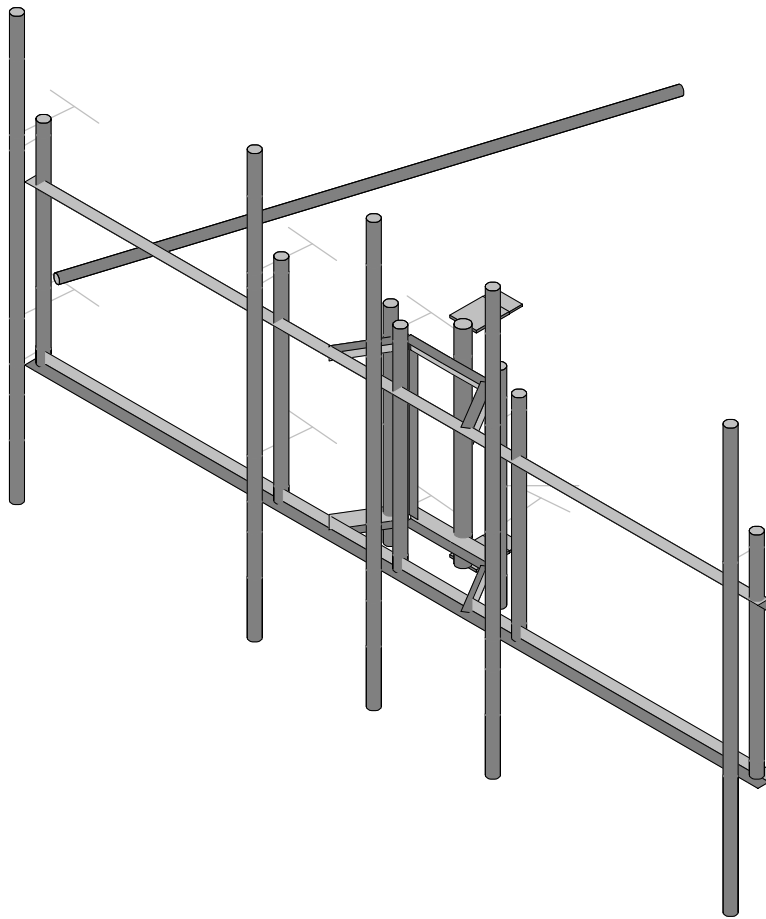
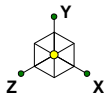
## **6.0 Standard Conditions**

- All data required to complete our structural analysis was furnished by our client and provided record data. GeoStructural has not conducted a site visit or independent study to verify existing conditions and the results of this analysis are based solely on the information provided. It has been assumed that the tower, antenna support structure and foundation have been constructed according to the provided existing drawings, previous structural analysis reports, mapping documents, etc.
- The default Structure Classification is Class II in accordance with ANSI/TIA-222-G §A.2.2 & §A.15.3 and has been assumed for this analysis. The owner shall verify this classification conforms with original or desired reliability criteria.
- This analysis assumes that the structure has been properly installed and maintained in accordance with ANSI/TIA-222-G §15.5 and that no physical deterioration has occurred in any of the components of the structure. Damaged, missing, or rusted members were not considered.
- This analysis verifies the adequacy of the main components of the structure. Not all connections, welds, bolts, plates, etc. were individually detailed and analyzed. Where not specifically analyzed, the existing connection plates, welds, bolts, etc. were assumed adequate to develop the full capacity of the main structural members.
- No consideration has been made for unusual or extreme wind events, rime/in-cloud ice loadings, harmonic or nodal vibration, vortex shedding or other similar conditions.
- It is the owner's responsibility to determine the appropriate design wind speed and amount of ice accumulation beyond code minimum values that should be considered in the analysis.
- This analysis report does not constitute a maintenance and condition assessment. No certifications regarding maintenance and condition are expressed or implied. If desired, GeoStructural can provide these services under a subsequent contract.
- This analysis only encompasses the antenna mount assembly. The tower, overall mount support structure, foundation, etc. are beyond the scope of this analysis. If desired, GeoStructural can provide these services under a subsequent contract.



## **7.0 Calculations & Software Output**

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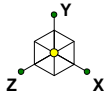
Jesse Drennen, PE

CT23XC404

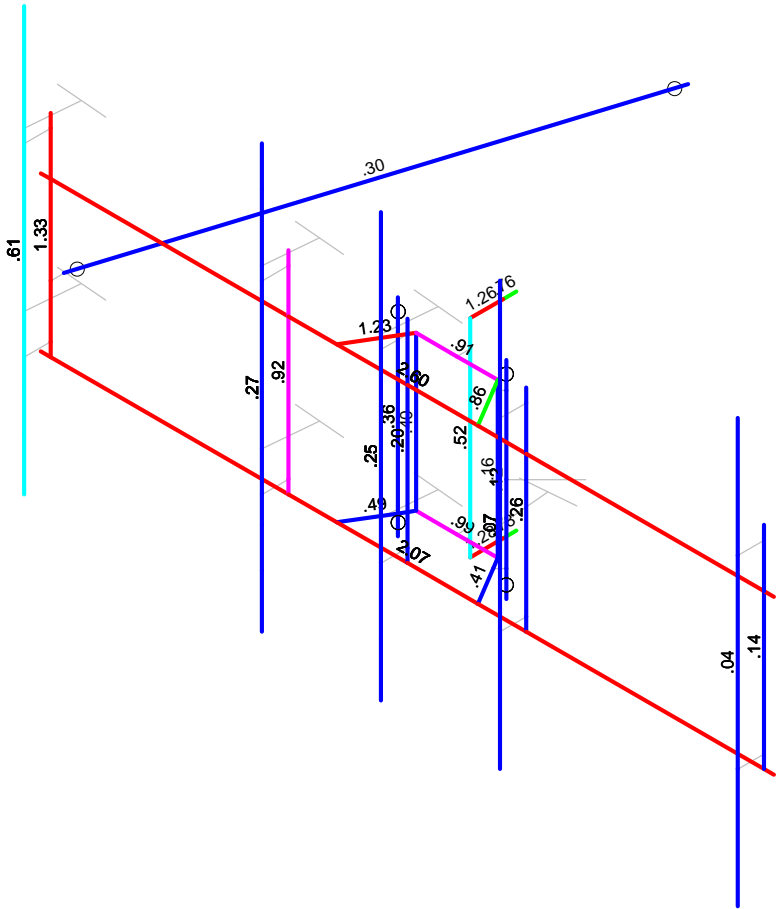
SK - 1

Mar 7, 2018 at 3:03 PM

CT23XC404\_Mount Analysis\_R0 1...



Code Check ( Env )	
Black	No Calc
Red	> 1.0
Magenta	.90-1.0
Green	.75-.90
Cyan	.50-.75
Blue	0-.50



Member Code Checks Displayed (Enveloped)  
Envelope Only Solution

GeoStructural, LLC

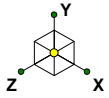
Jesse Drennen, PE

CT23XC404

SK - 2

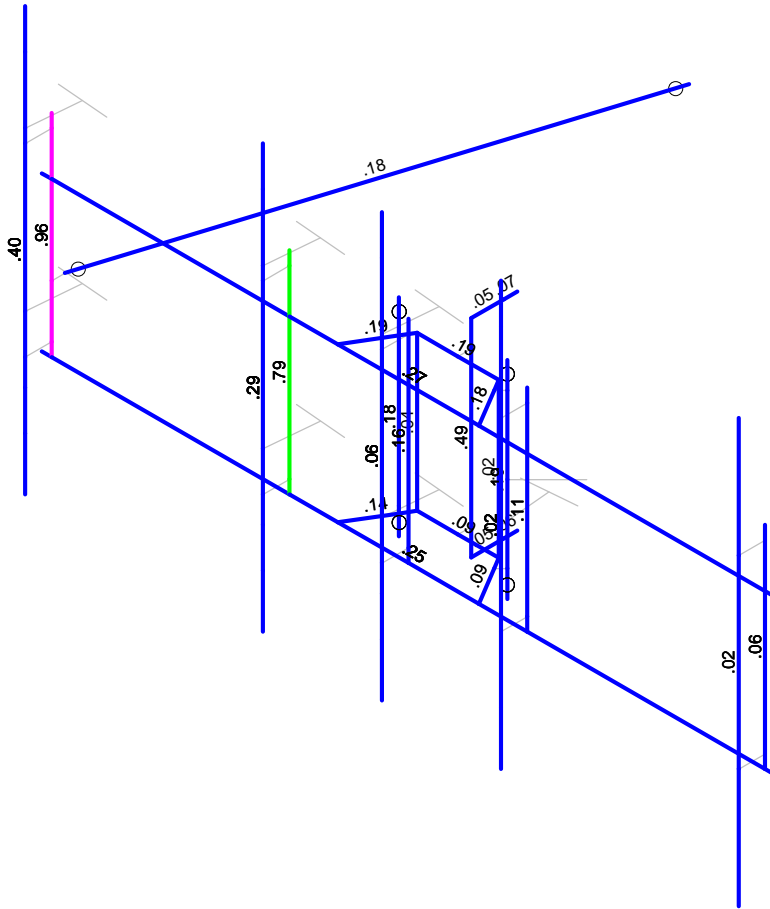
Mar 7, 2018 at 3:03 PM

CT23XC404\_Mount Analysis\_R0 1...



Shear Check  
( Env )

- No Calc
- > 1.0
- .90-1.0
- .75-.90
- .50-.75
- 0-.50



Member Shear Checks Displayed (Enveloped)  
Envelope Only Solution

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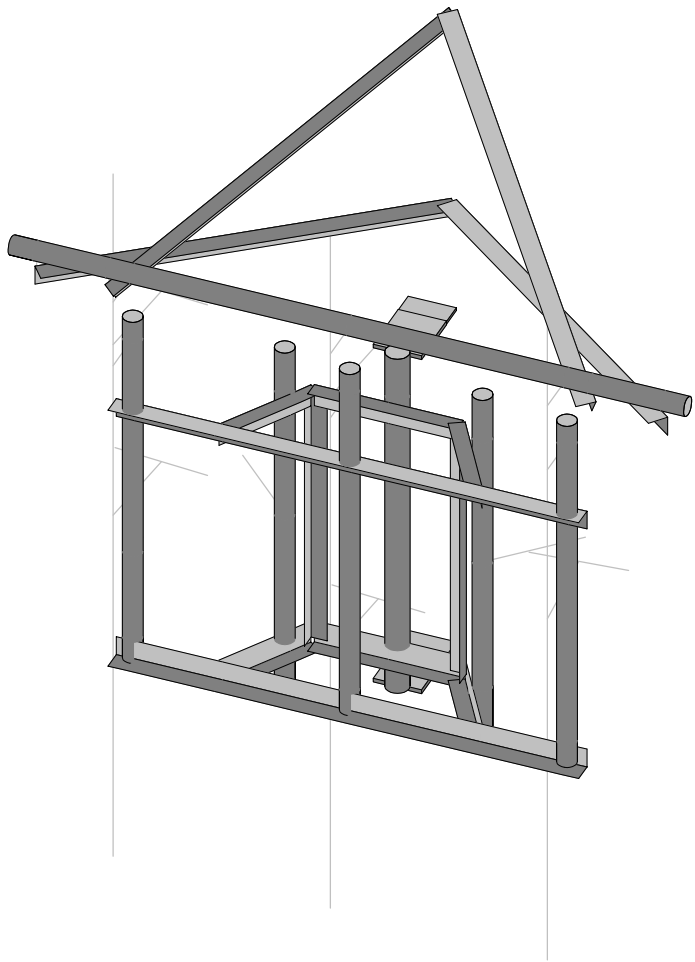
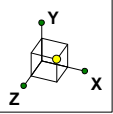
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CT23XC404

SK - 3

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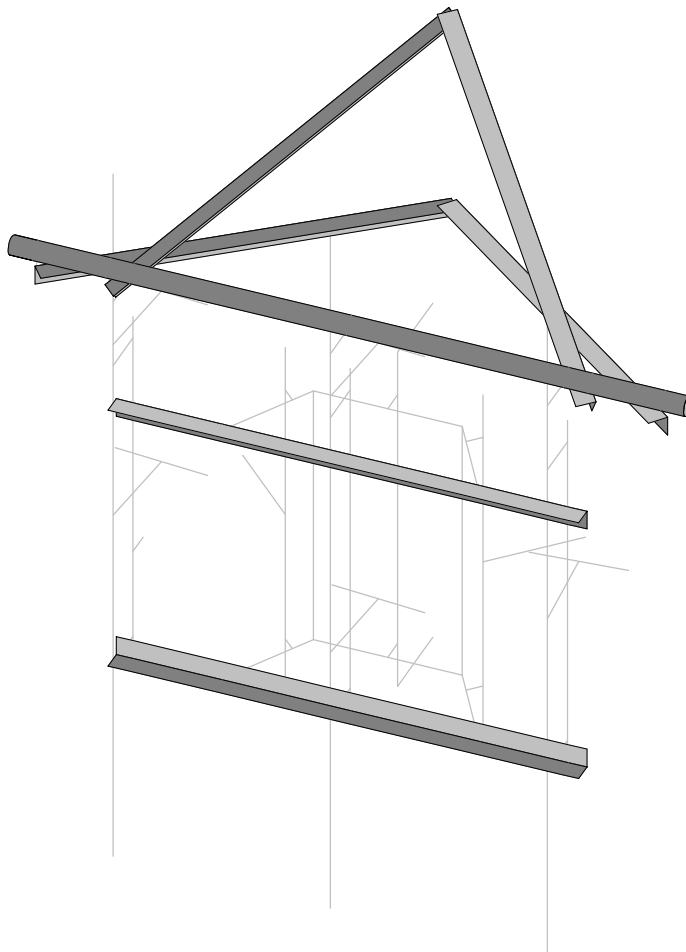
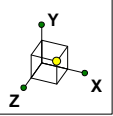
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CT23XC404

SK - 1

Mar 7, 2018 at 3:31 PM

CT23XC404\_Mount Analysis\_R0 1...



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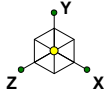
Jesse Drennen, PE

CT23XC404

SK - 7

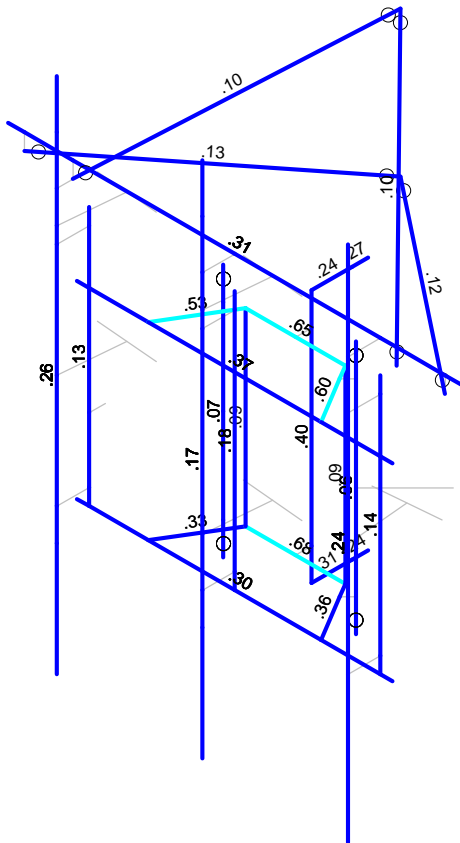
Mar 7, 2018 at 3:32 PM

CT23XC404\_Mount Analysis\_R0 1...



Code Check  
( Env )

- No Calc
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- .90-1.0
- .75-.90
- .50-.75
- 0-.50



Member Code Checks Displayed (Enveloped)  
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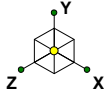
Jesse Drennen, PE

CT23XC404

SK - 5

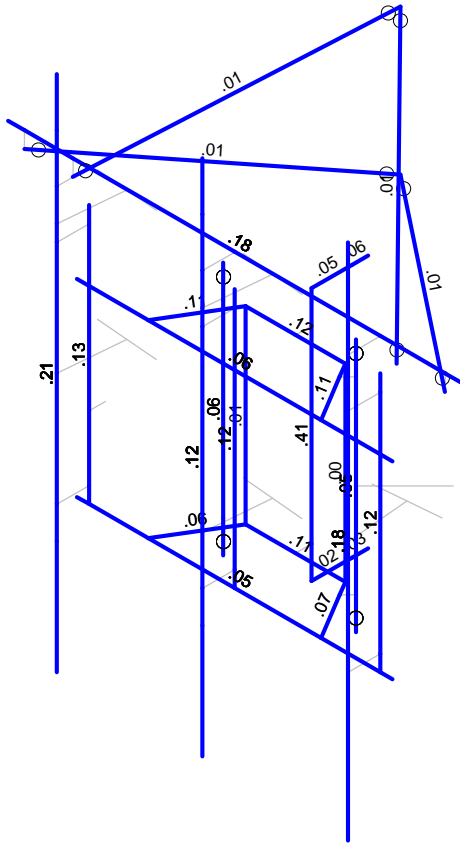
Mar 7, 2018 at 3:31 PM

CT23XC404\_Mount Analysis\_R0 1...



Shear Check (Env)

- No Calc
- > 1.0
- .90-1.0
- .75-.90
- .50-.75
- 0-.50



Member Shear Checks Displayed (Enveloped)  
Envelope Only Solution

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Jesse Drennen, PE

CT23XC404

SK - 6

Mar 7, 2018 at 3:31 PM

CT23XC404\_Mount Analysis\_R0 1...



**Basic Load Cases**

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed Area(Me...	Surface(P...
1	D	DL		-1		9			
2	Di	SL				9		27	
3	Lm [500]	LL				1			
4	Lv [250]	LL				2			
5	Woz	WL				9		25	
6	Wox	WL				9		25	
7	Wiz	WL				9		25	
8	Wix	WL				9		25	
9	Ez	EL				9			
10	Ex	EL				9			

**Load Combination Design**

	Description	ASIF	CD	ABIF	Service	Hot Rolled	Cold For...	Wood	Concrete	Masonry	Footings	Aluminum	Connecti...
1	1) 1.4D					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
2	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
3	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
4	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
5	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
6	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
7	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
8	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
9	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
10	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
11	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
12	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
13	2) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
14	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
15	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
16	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
17	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
18	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
19	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
20	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
21	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
22	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
23	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
24	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
25	3) 0.9D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
26	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
27	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
28	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
29	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
30	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
31	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
32	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
33	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
34	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
35	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
36	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
37	4) 1.2D+1.0...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
38	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
39	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
40	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
41	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes

**Load Combination Design (Continued)**

	Description	ASIF	CD	ABIF	Service	Hot Rolled	Cold For...	Wood	Concrete	Masonry	Footings	Aluminum	Connecti...
42	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
43	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
44	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
45	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
46	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
47	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
48	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
49	5) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
50	6) 1.2D+1.5...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
51	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
52	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
53	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
54	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
55	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
56	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
57	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
58	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
59	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
60	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
61	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
62	7) (1.2+0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
63	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
64	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
65	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
66	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
67	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
68	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
69	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
70	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
71	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
72	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
73	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
74	8) (0.9-0.2S...					Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes

**Envelope Joint Reactions**

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N28	max	1.757	5	.257	32	1.346	2	0	1	2.462	5	0	1
2		min	-1.749	23	.044	14	-.845	20	0	1	-2.447	23	0	1
3	N27	max	.714	17	.36	26	1.112	14	0	1	1.571	17	0	1
4		min	-.732	11	-.094	20	-1.166	8	0	1	-1.583	11	0	1
5	N21	max	0	1	0	1	0	1	0	1	0	1	0	1
6		min	0	1	0	1	0	1	0	1	0	1	0	1
7	N33	max	0	1	0	1	0	1	0	1	0	1	0	1
8		min	0	1	0	1	0	1	0	1	0	1	0	1
9	N68	max	.624	23	.063	32	1.325	26	0	1	0	1	0	1
10		min	-.657	5	.01	14	-.426	20	0	1	0	1	0	1
11	N73	max	.47	5	1.846	32	-.204	14	0	1	0	6	0	1
12		min	-.427	23	.297	14	-2.035	32	0	1	0	11	0	1
13	Totals:	max	2.281	5	2.469	27	3.227	2						
14		min	-2.281	23	.569	70	-3.227	20						

**Envelope Member Section Deflections**

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	0	20	.064	10	.015	11	7.76e-03	10	NC	1	NC	1
2			min	-.101	26	-.062	16	-.015	17	-7.725e-03	16	2799.574	9	1746.662	33
3		2	max	0	20	.066	22	.02	22	7.645e-03	22	NC	1	NC	1
4			min	-.101	26	-.069	4	-.021	4	-7.824e-03	4	4030.604	9	2384.586	33
5		3	max	0	20	.067	22	.024	22	7.544e-03	22	NC	2	NC	1
6			min	-.101	26	-.074	4	-.026	4	-7.939e-03	4	3572.918	34	2648.712	4
7		4	max	0	20	.063	22	.025	22	7.443e-03	22	NC	3	NC	1
8			min	-.101	26	-.075	4	-.026	4	-8.053e-03	4	2281.567	34	3174.41	4
9		5	max	0	20	.052	22	.023	11	7.342e-03	22	NC	3	NC	1
10			min	-.101	26	-.068	4	-.023	17	-8.168e-03	4	1594.345	35	4168.531	56
11	M2	1	max	0	20	.015	17	.054	6	7.351e-03	23	NC	1	NC	1
12			min	-.1	26	-.015	11	-.05	24	-7.55e-03	5	4422.39	7	1810.891	29
13		2	max	0	20	.02	17	.055	18	7.415e-03	11	NC	1	NC	1
14			min	-.1	26	-.021	11	-.057	12	-7.409e-03	17	7150.865	30	2512.684	30
15		3	max	0	20	.023	17	.056	18	7.507e-03	11	NC	4	NC	1
16			min	-.1	26	-.025	11	-.063	12	-7.296e-03	17	3649.702	29	3124.636	12
17		4	max	0	20	.025	17	.053	18	7.599e-03	11	NC	4	NC	1
18			min	-.1	26	-.026	11	-.064	12	-7.183e-03	17	2330.622	28	3760.452	12
19		5	max	0	20	.023	5	.044	18	7.691e-03	11	NC	4	NC	1
20			min	-.1	26	-.023	23	-.059	12	-7.07e-03	17	1596.083	28	4395.369	57
21	M5	1	max	.01	18	.167	5	.232	5	7.738e-03	23	NC	1	NC	1
22			min	-.077	36	-.166	23	-.205	23	-8.044e-03	5	NC	1	957.819	5
23		2	max	.01	18	.161	5	.203	5	7.738e-03	23	NC	1	NC	1
24			min	-.077	36	-.158	23	-.194	23	-8.044e-03	5	NC	1	1340.379	5
25		3	max	.01	18	.168	5	.179	17	6.141e-03	23	NC	1	NC	1
26			min	-.076	36	-.165	23	-.19	11	-6.535e-03	5	8289.254	50	2120.112	5
27		4	max	.01	18	.193	5	.153	17	5.975e-03	22	NC	1	NC	13
28			min	-.076	36	-.187	23	-.185	11	-6.743e-03	4	3109.213	4	1692.74	9
29		5	max	.01	18	.248	5	.154	18	5.316e-03	22	NC	13	NC	1
30			min	-.076	36	-.228	23	-.179	12	-6.528e-03	4	1105.324	4	995.945	2
31	M6	1	max	.2	5	.007	19	.113	5	2.749e-04	50	NC	1	NC	1
32			min	-.193	23	-.084	37	-.112	23	-1.476e-04	24	NC	1	NC	1
33		2	max	.2	5	.008	19	.125	5	2.749e-04	50	NC	1	NC	1
34			min	-.193	23	-.082	37	-.124	23	-1.476e-04	24	NC	1	NC	1
35		3	max	.2	5	.009	19	.137	5	2.749e-04	50	NC	1	NC	1
36			min	-.193	23	-.08	37	-.135	23	-1.476e-04	24	NC	1	NC	1
37		4	max	.2	5	.009	19	.149	5	2.749e-04	50	NC	1	NC	1
38			min	-.193	23	-.078	37	-.147	23	-1.476e-04	24	NC	1	NC	1
39		5	max	.2	5	.01	18	.161	5	2.749e-04	50	NC	1	NC	1
40			min	-.193	23	-.077	36	-.158	23	-1.476e-04	24	NC	1	NC	1
41	M7	1	max	.157	17	.008	19	.145	5	2.047e-03	4	NC	1	NC	1
42			min	-.186	11	-.084	37	-.144	23	-1.846e-03	22	NC	1	NC	1
43		2	max	.157	17	.008	19	.156	5	2.047e-03	4	NC	1	NC	1
44			min	-.186	11	-.082	37	-.153	23	-1.846e-03	22	NC	1	NC	1
45		3	max	.157	17	.009	19	.166	5	2.047e-03	4	NC	1	NC	1
46			min	-.186	11	-.08	37	-.163	23	-1.846e-03	22	NC	1	NC	1
47		4	max	.157	17	.009	19	.176	5	2.047e-03	4	NC	1	NC	1
48			min	-.186	11	-.078	37	-.172	23	-1.846e-03	22	NC	1	NC	1
49		5	max	.157	17	.01	18	.187	5	2.047e-03	4	NC	1	NC	1
50			min	-.186	11	-.076	36	-.182	23	-1.846e-03	22	NC	1	NC	1
51	M8	1	max	0	20	.005	17	0	8	8.479e-04	11	NC	1	NC	1
52			min	-.099	26	-.005	11	0	14	-8.452e-04	17	NC	1	NC	1
53		2	max	0	20	.005	17	.026	20	2.997e-03	23	NC	1	NC	1
54			min	-.099	26	-.005	11	-.026	2	-3.007e-03	5	NC	1	1810.299	2
55		3	max	0	20	.008	17	.033	20	3.076e-03	23	NC	1	NC	5
56			min	-.099	26	-.008	11	-.04	2	-3.093e-03	5	NC	1	1173.406	2

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC	
57	4	max	0	20	.012	17	.024	20	3.156e-03	23	NC	1	NC	17	
58		min	-.099	26	-.012	11	-.034	2	-3.178e-03	5	NC	1	1381.015	2	
59	5	max	0	20	.008	5	0	20	1.143e-03	23	NC	1	NC	1	
60		min	-.099	26	-.008	23	0	2	-1.151e-03	5	NC	1	NC	1	
61	M9	1	max	0	14	.005	11	.099	26	2.284e-04	13	NC	1	NC	1
62		min	0	8	-.005	17	0	20	-2.226e-04	19	1568.98	11	714.812	9	
63	2	max	0	14	.004	11	.095	26	2.284e-04	13	NC	1	NC	6	
64		min	0	8	-.004	17	-.003	20	-2.226e-04	19	2313.713	11	782.137	26	
65	3	max	0	14	.003	11	.083	26	2.284e-04	13	NC	1	NC	6	
66		min	0	8	-.003	17	-.005	20	-2.226e-04	19	3913.13	11	639.875	26	
67	4	max	0	14	.001	11	.065	26	2.284e-04	13	NC	1	NC	6	
68		min	0	8	-.001	17	-.005	20	-2.226e-04	19	9053.263	11	938.871	26	
69	5	max	0	14	0	11	.043	26	2.284e-04	13	NC	1	NC	1	
70		min	0	8	0	17	-.004	20	-2.226e-04	19	NC	1	NC	1	
71	M10	1	max	0	2	.008	23	.099	26	9.003e-04	17	NC	1	NC	1
72		min	0	20	-.008	5	0	20	-9.15e-04	11	1070.209	5	NC	1	
73	2	max	0	2	.006	23	.091	26	9.003e-04	17	NC	1	5910.356	14	
74		min	0	20	-.006	5	.004	20	-9.15e-04	11	1550.611	5	1084.137	32	
75	3	max	0	2	.004	23	.077	26	9.003e-04	17	NC	1	4815.533	14	
76		min	0	20	-.004	5	.005	20	-9.15e-04	11	2578.949	5	886.144	32	
77	4	max	0	2	.002	23	.06	26	9.003e-04	17	NC	1	7038.294	14	
78		min	0	20	-.002	5	.005	20	-9.15e-04	11	5871.179	5	1299.066	32	
79	5	max	0	2	.001	23	.039	26	9.003e-04	17	NC	1	NC	1	
80		min	0	20	-.001	5	.004	20	-9.15e-04	11	NC	1	NC	1	
81	M11	1	max	.036	21	.101	26	.044	22	1.58e-03	10	NC	1	NC	2
82		min	-.05	3	0	20	-.053	4	-1.472e-03	16	1902.554	70	581.105	29	
83	2	max	.036	21	.099	26	.071	22	4.512e-04	9	NC	1	NC	1	
84		min	-.05	3	-.001	20	-.081	4	-2.515e-04	15	958.665	10	520.914	5	
85	3	max	.036	21	.098	26	.101	22	5.861e-04	10	NC	1	NC	1	
86		min	-.05	3	-.004	20	-.112	4	-4.857e-04	16	472.114	10	244.688	5	
87	4	max	.036	21	.097	26	.131	22	7.226e-04	10	NC	1	NC	1	
88		min	-.05	3	-.006	20	-.141	4	-7.222e-04	16	311.568	10	159.373	5	
89	5	max	.036	21	.096	26	.157	23	8.719e-04	22	NC	1	NC	1	
90		min	-.05	3	-.009	20	-.168	4	-9.716e-04	4	233.142	10	121.653	5	
91	M12	1	max	.023	5	.1	26	.044	18	1.722e-03	5	NC	1	NC	1
92		min	-.023	23	0	20	-.059	12	-1.157e-03	23	494.926	23	292.527	6	
93	2	max	.022	5	.103	26	.021	19	1.334e-03	19	NC	1	NC	8	
94		min	-.022	23	-.003	20	-.032	13	-1.507e-03	13	701.103	23	440.356	6	
95	3	max	.022	5	.105	26	.014	20	1.961e-03	20	NC	1	NC	68	
96		min	-.022	23	-.005	20	-.022	2	-2.868e-03	2	999.273	17	509.651	10	
97	4	max	.022	17	.103	26	.026	21	1.583e-03	21	NC	1	NC	2	
98		min	-.022	23	-.003	20	-.038	3	-1.787e-03	3	689.442	17	352.336	10	
99	5	max	.023	17	.101	26	.052	22	1.855e-03	10	NC	1	NC	1	
100		min	-.023	11	0	20	-.068	4	-1.358e-03	16	486.071	5	235.715	22	
101	M13	1	max	.041	12	.093	26	.158	17	7.354e-04	18	NC	1	NC	1
102		min	-.028	18	-.006	20	-.166	11	-9.089e-04	12	230.561	5	122.393	11	
103	2	max	.041	12	.095	26	.13	17	5.901e-04	18	NC	1	NC	1	
104		min	-.028	18	-.004	20	-.137	11	-6.42e-04	12	309.032	5	160.14	11	
105	3	max	.041	12	.096	26	.098	17	4.55e-04	6	NC	1	NC	1	
106		min	-.028	18	-.002	20	-.106	11	-3.855e-04	24	470.746	5	245.454	11	
107	4	max	.041	12	.098	26	.066	17	3.655e-04	30	NC	1	NC	1	
108		min	-.028	18	0	20	-.075	11	-1.356e-04	24	963.222	5	521.896	11	
109	5	max	.041	12	.1	26	.039	17	1.33e-03	6	NC	1	NC	1	
110		min	-.028	18	0	20	-.047	11	-1.217e-03	24	3190.144	68	623.396	35	
111	M14	1	max	.046	16	.001	20	.153	10	1.044e-03	23	NC	1	NC	1
112		min	-.048	10	-.091	27	-.153	16	-1.124e-03	5	398.034	6	123.421	11	
113	2	max	.046	16	0	20	.125	10	8.259e-04	23	NC	1	NC	1	

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC	
114		min	-.048	10	-.094	26	-.125	16	-9.617e-04	5	531.681	6	165.276	11	
115	3	max	.046	16	0	20	.098	10	6.144e-04	22	NC	1	NC	1	
116		min	-.048	10	-.096	26	-.097	16	-8.122e-04	4	608.031	4	254.739	11	
117	4	max	.046	16	0	20	.071	10	4.936e-04	22	NC	1	NC	1	
118		min	-.048	10	-.098	26	-.069	16	-7.449e-04	4	403.207	4	534.625	11	
119	5	max	.046	16	0	20	.044	10	1.023e-03	21	NC	1	NC	1	
120		min	-.048	10	-.101	26	-.043	16	-1.478e-03	3	300.939	4	1359.783	58	
121	M15	1	max	.015	11	0	.064	10	3.205e-04	22	NC	1	NC	1	
122		min	-.015	17	-.101	26	-.062	16	-1.07e-03	28	487.355	11	202.411	4	
123	2	max	.015	11	-.005	20	.032	9	1.129e-03	20	NC	1	NC	1	
124		min	-.015	17	-.099	26	-.031	15	-1.465e-03	2	684.072	23	309.649	4	
125	3	max	.015	11	-.007	20	.016	8	2.142e-03	20	NC	1	NC	1	
126		min	-.015	17	-.098	26	-.015	14	-2.167e-03	2	1002.293	22	466.036	4	
127	4	max	.015	11	-.004	20	.026	6	1.07e-03	20	NC	1	NC	1	
128		min	-.015	17	-.099	26	-.024	24	-1.416e-03	2	685.179	17	411.333	12	
129	5	max	.015	11	0	20	.054	6	2.502e-04	18	NC	1	NC	1	
130		min	-.015	17	-.1	26	-.05	24	-1.08e-03	36	488.058	17	263.137	6	
131	M16	1	max	.04	6	0	.039	5	8.459e-04	18	NC	1	NC	1	
132		min	-.037	24	-.1	26	-.038	23	-1.267e-03	12	366.868	12	3719.747	56	
133	2	max	.04	6	0	20	.066	5	3.967e-04	18	NC	1	NC	1	
134		min	-.037	24	-.098	26	-.064	23	-6.248e-04	12	491.04	12	527.869	5	
135	3	max	.04	6	0	20	.095	5	5.936e-04	17	NC	1	NC	1	
136		min	-.037	24	-.095	26	-.093	23	-7.412e-04	11	597.976	11	251.943	5	
137	4	max	.04	6	-.001	20	.124	5	8.641e-04	16	NC	1	NC	1	
138		min	-.037	24	-.092	26	-.122	23	-9.253e-04	10	397.471	11	163.785	5	
139	5	max	.04	6	0	19	.152	5	1.212e-03	4	NC	1	NC	1	
140		min	-.037	24	-.089	37	-.15	23	-1.193e-03	22	298.583	11	122.467	5	
141	M17	1	max	.124	23	.194	.088	27	4.685e-04	16	NC	1	NC	1	
142		min	-.125	5	-.219	4	-.014	21	-1.966e-03	34	249.325	6	NC	1	
143	2	max	.124	23	.1	.096	.26	1.226e-03	16	NC	1	NC	1		
144		min	-.125	5	-.118	4	-.009	20	-1.55e-03	10	335.733	6	3957.176	26	
145	3	max	.124	23	.032	20	.095	26	4.701e-04	20	NC	1	NC	1	
146		min	-.125	5	-.053	2	-.004	20	-1.758e-03	26	498.835	6	6560.457	32	
147	4	max	.124	23	.089	17	.094	37	9.906e-04	23	NC	1	NC	1	
148		min	-.125	5	-.104	11	-.006	19	-1.374e-03	5	957.493	6	3994.155	26	
149	5	max	.125	23	.186	17	.083	37	4.514e-04	22	NC	1	NC	1	
150		min	-.125	5	-.205	11	-.009	19	-1.862e-03	28	NC	1	NC	1	
151	M18	1	max	.111	23	.013	.238	10	4.397e-04	17	NC	1	NC	1	
152		min	-.112	5	-.088	27	-.233	16	-1.302e-03	35	207.897	23	180.346	4	
153	2	max	.111	23	.001	.20	.109	10	2.477e-04	50	NC	1	NC	1	
154		min	-.111	5	-.092	26	-.107	16	-7.911e-04	30	285.072	23	256.867	4	
155	3	max	.111	23	.004	.20	.027	8	4.392e-04	20	NC	1	NC	1	
156		min	-.111	5	-.095	26	-.024	14	-1.374e-03	26	415.962	11	370.424	4	
157	4	max	.111	23	0	.20	.099	5	9.228e-05	16	NC	1	NC	1	
158		min	-.111	5	-.09	26	-.096	23	-8.301e-04	34	393.292	18	334.596	12	
159	5	max	.111	23	.008	.19	.221	5	5.206e-04	22	NC	1	NC	1	
160		min	-.112	5	-.083	37	-.212	23	-1.318e-03	28	274.938	18	231.978	6	
161	M21	1	max	.007	19	.112	.5	.203	5	7.766e-03	23	NC	1	NC	1
162		min	-.084	37	-.111	23	-.194	23	-8.107e-03	5	NC	1	1652.252	19	
163	2	max	.007	19	.113	.5	.191	17	7.359e-03	23	NC	1	NC	3	
164		min	-.084	37	-.113	23	-.191	23	-7.571e-03	5	NC	1	2058.07	19	
165	3	max	.008	19	.115	.17	.183	17	6.854e-03	23	NC	1	NC	6	
166		min	-.084	37	-.115	11	-.192	11	-6.941e-03	5	NC	1	1718.524	31	
167	4	max	.008	19	.127	.5	.17	17	6.39e-03	23	NC	1	NC	6	
168		min	-.084	37	-.126	23	-.19	11	-6.413e-03	5	3157.998	5	1040.22	31	
169	5	max	.008	19	.151	.5	.153	17	6.379e-03	23	NC	1	NC	3	
170		min	-.084	37	-.149	23	-.185	11	-6.863e-03	5	1205.505	5	720.702	27	

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y Ratio	LC (n)	L/z Ratio	LC	
171	M26	1	max	.022	2	.005	20	.022	23	8.974e-05	20	NC	1	NC	1
172			min	-.014	20	-.105	26	-.022	5	-2.036e-04	39	NC	1	NC	1
173		2	max	.022	2	.003	20	.02	23	8.974e-05	20	NC	1	NC	1
174			min	-.014	20	-.104	26	-.02	17	-2.036e-04	39	NC	1	NC	1
175		3	max	.022	2	.002	20	.017	23	8.974e-05	20	NC	1	NC	1
176			min	-.014	20	-.102	26	-.017	17	-2.036e-04	39	NC	1	NC	1
177		4	max	.022	2	0	20	.015	11	8.974e-05	20	NC	1	NC	1
178			min	-.014	20	-.101	26	-.015	17	-2.036e-04	39	NC	1	NC	1
179		5	max	.022	2	0	20	.013	11	8.974e-05	20	NC	1	NC	1
180			min	-.014	20	-.099	26	-.013	17	-2.036e-04	39	NC	1	NC	1
181	M27	1	max	.015	14	-.007	20	.015	11	3.143e-04	16	NC	1	NC	1
182			min	-.016	8	-.098	26	-.015	17	-3.078e-04	22	NC	1	NC	1
183		2	max	.015	14	-.006	20	.013	11	3.143e-04	16	NC	1	NC	1
184			min	-.016	8	-.098	26	-.012	17	-3.078e-04	22	NC	1	NC	1
185		3	max	.015	14	-.004	20	.01	11	3.143e-04	16	NC	1	NC	1
186			min	-.016	8	-.099	26	-.01	17	-3.078e-04	22	NC	1	NC	1
187		4	max	.015	14	-.002	20	.008	11	3.143e-04	16	NC	1	NC	1
188			min	-.016	8	-.099	26	-.008	17	-3.078e-04	22	NC	1	NC	1
189		5	max	.015	14	0	20	.006	11	3.143e-04	16	NC	1	NC	1
190			min	-.016	8	-.099	26	-.006	17	-3.078e-04	22	NC	1	NC	1
191	M28	1	max	0	2	.001	23	.039	26	9.003e-04	17	NC	1	NC	1
192			min	0	20	-.001	5	.004	20	-9.15e-04	11	2869.1	5	NC	1
193		2	max	0	2	0	23	.03	26	9.003e-04	17	NC	1	NC	1
194			min	0	20	0	5	.003	20	-9.15e-04	11	4675.848	5	4713.363	32
195		3	max	0	2	0	23	.02	26	9.003e-04	17	NC	1	NC	1
196			min	0	20	0	5	.002	20	-9.15e-04	11	9104.884	5	4122.803	32
197		4	max	0	2	0	23	.01	26	9.003e-04	17	NC	1	NC	1
198			min	0	20	0	5	.001	20	-9.15e-04	11	NC	1	6594.81	32
199		5	max	0	1	0	1	0	1	9.003e-04	17	NC	1	NC	1
200			min	0	1	0	1	0	1	-9.15e-04	11	NC	1	NC	1
201	M29	1	max	0	14	0	11	.043	26	2.284e-04	13	NC	1	NC	1
202			min	0	8	0	17	-.004	20	-2.226e-04	19	4779.858	11	855.274	22
203		2	max	0	14	0	11	.033	26	2.284e-04	13	NC	1	NC	5
204			min	0	8	0	17	-.003	20	-2.226e-04	19	7993.687	11	1143.977	22
205		3	max	0	14	0	11	.023	26	2.284e-04	13	NC	1	NC	6
206			min	0	8	0	17	-.002	20	-2.226e-04	19	NC	1	1719.675	22
207		4	max	0	14	0	11	.011	26	2.284e-04	13	NC	1	NC	1
208			min	0	8	0	17	-.001	20	-2.226e-04	19	NC	1	3443.601	22
209		5	max	0	1	0	1	0	1	2.284e-04	13	NC	1	NC	1
210			min	0	1	0	1	0	1	-2.226e-04	19	NC	1	NC	1
211	M36A	1	max	.21	4	.012	21	.113	23	7.078e-05	22	NC	1	NC	1
212			min	-.203	22	-.088	27	-.114	5	-1.568e-04	50	NC	1	NC	1
213		2	max	.21	4	.011	21	.107	23	7.078e-05	22	NC	1	NC	1
214			min	-.203	22	-.089	27	-.108	5	-1.568e-04	50	NC	1	NC	1
215		3	max	.21	4	.01	21	.102	23	7.078e-05	22	NC	1	NC	1
216			min	-.203	22	-.09	27	-.103	5	-1.568e-04	50	NC	1	NC	1
217		4	max	.21	4	.01	21	.096	23	7.078e-05	22	NC	1	NC	1
218			min	-.203	22	-.09	27	-.097	5	-1.568e-04	50	NC	1	NC	1
219		5	max	.21	4	.009	21	.091	23	7.078e-05	22	NC	1	NC	1
220			min	-.203	22	-.091	27	-.092	5	-1.568e-04	50	NC	1	NC	1
221	M45	1	max	.017	21	.167	17	.255	10	8.335e-03	10	NC	1	NC	1
222			min	-.081	27	-.168	11	-.233	16	-8.204e-03	16	NC	1	958.197	11
223		2	max	.017	21	.16	17	.22	10	8.335e-03	10	NC	1	NC	1
224			min	-.081	27	-.161	11	-.215	16	-8.204e-03	16	9518.791	8	1341.614	11
225		3	max	.017	21	.166	17	.195	22	6.593e-03	11	NC	1	NC	1
226			min	-.081	27	-.167	11	-.211	4	-6.291e-03	17	7534.213	49	2150.878	11
227		4	max	.017	21	.189	17	.163	22	6.548e-03	11	NC	1	NC	2

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
228		min	-.081	27	-.192	11	-.2	4	-5.919e-03	17	3437.231	12	1455.057	8
229	5	max	.017	21	.23	17	.179	22	5.946e-03	11	NC	2	NC	1
230		min	-.081	27	-.247	11	-.206	4	-4.845e-03	17	1205.739	12	1151.162	13
231	M46	1	max	.216	10	.012	.112	5	1.913e-04	41	NC	1	NC	1
232		min	-.213	16	-.088	27	-.112	23	-1.707e-04	11	NC	1	NC	1
233	2	max	.216	10	.013	.124	.17	17	1.913e-04	41	NC	1	NC	1
234		min	-.213	16	-.086	27	-.124	23	-1.707e-04	11	NC	1	NC	1
235	3	max	.216	10	.015	.136	.17	17	1.913e-04	41	NC	1	NC	1
236		min	-.213	16	-.085	27	-.136	11	-1.707e-04	11	NC	1	NC	1
237	4	max	.216	10	.016	.148	.17	17	1.913e-04	41	NC	1	NC	1
238		min	-.213	16	-.083	27	-.148	11	-1.707e-04	11	NC	1	NC	1
239	5	max	.216	10	.017	.159	.17	17	1.913e-04	41	NC	1	NC	1
240		min	-.213	16	-.081	27	-.161	11	-1.707e-04	11	NC	1	NC	1
241	M47	1	max	.166	22	.012	.144	17	1.793e-03	17	NC	1	NC	1
242		min	-.201	4	-.088	27	-.144	11	-1.961e-03	11	NC	1	NC	1
243	2	max	.166	22	.013	.154	.17	17	1.793e-03	17	NC	1	NC	1
244		min	-.201	4	-.086	27	-.155	11	-1.961e-03	11	NC	1	NC	1
245	3	max	.166	22	.015	.164	.17	17	1.793e-03	17	NC	1	NC	1
246		min	-.201	4	-.084	27	-.165	11	-1.961e-03	11	NC	1	NC	1
247	4	max	.166	22	.016	.173	.17	17	1.793e-03	17	NC	1	NC	1
248		min	-.201	4	-.083	27	-.175	11	-1.961e-03	11	NC	1	NC	1
249	5	max	.166	22	.017	.183	.17	17	1.793e-03	17	NC	1	NC	1
250		min	-.201	4	-.081	27	-.185	11	-1.961e-03	11	NC	1	NC	1
251	M48	1	max	.012	21	.112	.219	10	8.556e-03	10	NC	1	NC	1
252		min	-.088	27	-.111	23	-.215	16	-8.387e-03	16	NC	1	1096.266	8
253	2	max	.012	21	.113	.206	.22	22	7.731e-03	10	NC	1	NC	2
254		min	-.088	27	-.113	23	-.21	4	-7.704e-03	16	NC	1	1362.927	8
255	3	max	.012	21	.116	.194	.22	22	6.936e-03	22	NC	1	NC	2
256		min	-.088	27	-.115	23	-.207	4	-7.047e-03	4	NC	1	1598.69	32
257	4	max	.012	21	.127	.179	.22	22	6.387e-03	23	NC	1	NC	2
258		min	-.088	27	-.126	23	-.204	4	-6.506e-03	5	3113.641	5	963.241	32
259	5	max	.012	21	.15	.163	.22	22	6.85e-03	11	NC	1	NC	2
260		min	-.088	27	-.15	11	-.2	4	-6.457e-03	17	1226.755	11	685.819	32
261	M50A	1	max	.107	11	0	.124	17	5.507e-05	23	NC	1	NC	1
262		min	-.105	17	-.095	37	-.138	11	-1.779e-03	29	NC	1	NC	1
263	2	max	.107	11	0	.144	.17	17	5.507e-05	23	NC	1	NC	1
264		min	-.105	17	-.096	37	-.156	11	-1.779e-03	29	NC	1	NC	1
265	3	max	.107	11	0	.163	.17	17	5.507e-05	23	NC	1	NC	1
266		min	-.105	17	-.096	37	-.175	11	-1.779e-03	29	NC	1	NC	1
267	4	max	.107	11	-.002	.183	.17	17	5.507e-05	23	NC	1	NC	1
268		min	-.105	17	-.096	37	-.193	11	-1.779e-03	29	NC	1	NC	1
269	5	max	.107	11	-.002	.202	.17	17	5.507e-05	23	NC	1	NC	1
270		min	-.105	17	-.096	36	-.211	11	-1.779e-03	29	NC	1	NC	1
271	M51A	1	max	.175	11	.01	.181	23	5.576e-04	9	NC	1	NC	1
272		min	-.163	17	-.076	36	-.183	5	-4.988e-04	15	NC	1	NC	1
273	2	max	.175	11	.007	.162	.23	23	5.576e-04	9	NC	1	NC	1
274		min	-.163	17	-.081	36	-.163	5	-4.988e-04	15	NC	1	NC	1
275	3	max	.175	11	.004	.144	.11	11	5.576e-04	9	NC	1	NC	1
276		min	-.163	17	-.086	37	-.144	17	-4.988e-04	15	NC	1	NC	1
277	4	max	.175	11	.002	.126	.11	11	5.576e-04	9	NC	1	NC	1
278		min	-.163	17	-.091	37	-.124	17	-4.988e-04	15	NC	1	NC	1
279	5	max	.175	11	0	.107	.11	11	5.576e-04	9	NC	1	NC	1
280		min	-.163	17	-.096	37	-.105	17	-4.988e-04	15	NC	1	NC	1
281	M50B	1	max	.107	5	.003	.159	4	2.005e-03	33	NC	1	NC	1
282		min	-.103	23	-.101	27	-.142	22	-2.601e-04	15	NC	1	NC	1
283	2	max	.107	5	.002	.178	.4	4	2.005e-03	33	NC	1	NC	1
284		min	-.103	23	-.102	27	-.161	22	-2.601e-04	15	NC	1	NC	1

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC	
285	3	max	.107	5	0	21	.196	4	2.005e-03	33	NC	1	NC	1	
286		min	-.103	23	-.102	27	-.18	22	-2.601e-04	15	NC	1	NC	1	
287	4	max	.107	5	0	21	.215	4	2.005e-03	33	NC	1	NC	1	
288		min	-.103	23	-.102	27	-.2	22	-2.601e-04	15	NC	1	NC	1	
289	5	max	.107	5	0	21	.233	4	2.005e-03	33	NC	1	NC	1	
290		min	-.103	23	-.102	27	-.219	22	-2.601e-04	15	NC	1	NC	1	
291	M51B	1	max	.196	4	.017	21	.182	23	5.6e-04	25	NC	1	NC	1
292		min	-.18	22	-.081	27	-.182	5	-6.369e-04	7	NC	1	NC	1	
293	2	max	.196	4	.013	21	.162	23	5.6e-04	25	NC	1	NC	1	
294		min	-.18	22	-.086	27	-.163	5	-6.369e-04	7	NC	1	NC	1	
295	3	max	.196	4	.009	21	.142	23	5.6e-04	25	NC	1	NC	1	
296		min	-.18	22	-.091	27	-.144	5	-6.369e-04	7	NC	1	NC	1	
297	4	max	.196	4	.005	21	.123	23	5.6e-04	25	NC	1	NC	1	
298		min	-.18	22	-.097	27	-.126	5	-6.369e-04	7	NC	1	NC	1	
299	5	max	.196	4	0	21	.103	23	5.6e-04	25	NC	1	NC	1	
300		min	-.18	22	-.102	27	-.107	5	-6.369e-04	7	NC	1	NC	1	
301	M54	1	max	.134	5	.016	20	.154	4	1.591e-03	12	NC	1	NC	1
302		min	-.126	23	-.093	26	-.113	22	-1.114e-03	18	NC	1	NC	1	
303	2	max	.134	5	.016	20	.169	4	1.591e-03	12	NC	1	NC	1	
304		min	-.126	23	-.091	26	-.13	22	-1.114e-03	18	NC	1	NC	1	
305	3	max	.134	5	.016	20	.184	4	1.591e-03	12	NC	1	NC	1	
306		min	-.126	23	-.09	26	-.147	22	-1.114e-03	18	NC	1	NC	1	
307	4	max	.134	5	.017	21	.199	4	1.591e-03	12	NC	1	NC	1	
308		min	-.126	23	-.089	27	-.164	22	-1.114e-03	18	NC	1	NC	1	
309	5	max	.134	5	.02	21	.214	4	1.591e-03	12	NC	1	NC	1	
310		min	-.126	23	-.088	27	-.181	22	-1.114e-03	18	NC	1	NC	1	
311	M55	1	max	.184	4	.017	21	.204	23	1.974e-03	11	NC	1	NC	1
312		min	-.147	22	-.081	27	-.204	5	-1.727e-03	17	NC	1	NC	1	
313	2	max	.184	4	.017	21	.184	23	1.974e-03	11	NC	1	NC	1	
314		min	-.147	22	-.083	27	-.186	5	-1.727e-03	17	NC	1	NC	1	
315	3	max	.184	4	.016	21	.165	23	1.974e-03	11	NC	1	NC	1	
316		min	-.147	22	-.085	27	-.169	5	-1.727e-03	17	NC	1	NC	1	
317	4	max	.184	4	.015	21	.146	23	1.974e-03	11	NC	1	NC	1	
318		min	-.147	22	-.087	27	-.151	5	-1.727e-03	17	NC	1	NC	1	
319	5	max	.184	4	.016	20	.126	23	1.974e-03	11	NC	1	NC	1	
320		min	-.147	22	-.09	26	-.134	5	-1.727e-03	17	NC	1	NC	1	
321	M56	1	max	.004	20	.111	5	.027	8	6.174e-03	23	NC	1	NC	1
322		min	-.095	26	-.111	23	-.024	14	-6.207e-03	5	NC	1	7993.319	10	
323	2	max	.004	20	.113	5	.03	20	6.196e-03	23	NC	1	NC	5	
324		min	-.095	26	-.112	23	-.035	2	-6.239e-03	5	NC	1	3402.775	26	
325	3	max	.004	20	.116	5	.03	20	6.12e-03	23	NC	1	NC	6	
326		min	-.095	26	-.115	23	-.042	2	-6.171e-03	5	NC	1	1958.639	26	
327	4	max	.004	20	.127	5	.033	20	6.14e-03	23	NC	1	NC	6	
328		min	-.095	26	-.126	23	-.054	2	-6.198e-03	5	3147.662	5	1181.606	26	
329	5	max	.004	20	.153	5	.041	20	6.952e-03	23	NC	1	NC	6	
330		min	-.095	26	-.152	23	-.075	2	-7.007e-03	5	1158.083	5	761.72	26	
331	M35	1	max	.147	17	.021	19	.17	5	1.964e-03	4	NC	1	NC	1
332		min	-.179	11	-.073	37	-.168	23	-1.309e-03	22	NC	1	NC	1	
333	2	max	.147	17	.018	19	.179	5	1.964e-03	4	NC	1	NC	1	
334		min	-.179	11	-.073	37	-.176	23	-1.309e-03	22	NC	1	NC	1	
335	3	max	.147	17	.015	19	.188	5	1.964e-03	4	NC	1	NC	1	
336		min	-.179	11	-.074	37	-.183	23	-1.309e-03	22	NC	1	NC	1	
337	4	max	.147	17	.013	19	.196	5	1.964e-03	4	NC	1	NC	1	
338		min	-.179	11	-.075	37	-.19	23	-1.309e-03	22	NC	1	NC	1	
339	5	max	.147	17	.01	18	.205	5	1.964e-03	4	NC	1	NC	1	
340		min	-.179	11	-.076	36	-.197	23	-1.309e-03	22	NC	1	NC	1	
341	M36	1	max	.162	22	.027	21	.17	5	1.247e-03	17	NC	1	NC	1



**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
342		min	-.199	4	-.076	27	-.169	23	-1.873e-03	11	NC	1	NC	1
343	2	max	.162	22	.025	21	.177	17	1.247e-03	17	NC	1	NC	1
344		min	-.199	4	-.077	27	-.177	11	-1.873e-03	11	NC	1	NC	1
345	3	max	.162	22	.022	21	.184	17	1.247e-03	17	NC	1	NC	1
346		min	-.199	4	-.078	27	-.186	11	-1.873e-03	11	NC	1	NC	1
347	4	max	.162	22	.02	21	.191	17	1.247e-03	17	NC	1	NC	1
348		min	-.199	4	-.079	27	-.195	11	-1.873e-03	11	NC	1	NC	1
349	5	max	.162	22	.017	21	.198	17	1.247e-03	17	NC	1	NC	1
350		min	-.199	4	-.08	27	-.204	11	-1.873e-03	11	NC	1	NC	1
351	M37	1	max	.169	23	.03	.225	23	3.034e-03	8	NC	1	NC	1
352		min	-.17	5	-.055	4	-.226	5	-3.033e-03	14	2180.82	21	NC	1
353	2	max	.169	23	.024	20	.133	22	2.373e-03	7	NC	5	NC	6
354		min	-.169	5	-.082	26	-.174	4	-2.066e-03	25	2344.274	37	1091.135	2
355	3	max	.168	23	.013	20	.051	20	1.952e-03	20	NC	7	NC	6
356		min	-.169	5	-.093	26	-.09	2	-2.517e-03	2	1759.064	26	1028.067	2
357	4	max	.168	23	.018	19	.112	18	2.516e-03	8	NC	6	NC	5
358		min	-.17	5	-.079	26	-.15	12	-2.317e-03	15	2426.932	27	1195.429	37
359	5	max	.169	23	.025	18	.226	5	3.014e-03	20	NC	1	NC	1
360		min	-.17	5	-.049	12	-.225	23	-3.117e-03	2	3735.106	7	NC	1
361	M38	1	max	.054	36	.17	.217	11	6.798e-03	4	NC	1	NC	1
362		min	-.024	18	-.169	23	-.211	17	-4.075e-03	22	NC	1	NC	1
363	2	max	.054	36	.169	5	.217	11	6.798e-03	4	NC	1	NC	1
364		min	-.024	18	-.169	23	-.211	17	-4.075e-03	22	NC	1	NC	1
365	3	max	.054	36	.168	17	.217	11	6.798e-03	4	NC	1	NC	1
366		min	-.024	18	-.169	11	-.211	17	-4.075e-03	22	NC	1	NC	1
367	4	max	.054	36	.167	17	.217	11	6.798e-03	4	NC	1	NC	1
368		min	-.024	18	-.169	11	-.211	17	-4.075e-03	22	NC	1	NC	1
369	5	max	.054	36	.166	17	.218	11	6.798e-03	4	NC	1	NC	1
370		min	-.024	18	-.169	11	-.211	17	-4.075e-03	22	NC	1	NC	1
371	M39	1	max	0	1	0	0	1	1.975e-03	8	NC	1	NC	1
372		min	0	1	0	0	0	1	-1.156e-03	14	NC	1	NC	1
373	2	max	0	18	.077	5	.022	34	1.975e-03	8	NC	1	NC	1
374		min	0	36	-.076	23	.001	15	-1.156e-03	14	1118.015	16	1267.125	22
375	3	max	0	18	.148	5	.038	35	1.975e-03	8	NC	1	NC	1
376		min	-.001	36	-.148	11	.001	17	-1.156e-03	14	557.834	16	627.412	22
377	4	max	0	18	.211	17	.048	36	1.975e-03	8	NC	1	NC	1
378		min	-.002	36	-.214	11	-.008	18	-1.156e-03	14	370.927	16	413.319	22
379	5	max	0	18	.269	17	.054	36	1.975e-03	8	NC	1	NC	1
380		min	-.003	36	-.276	11	-.024	18	-1.156e-03	14	277.546	16	306.701	22
381	M40	1	max	.06	3	.17	.219	5	3.547e-03	18	NC	1	NC	1
382		min	-.03	21	-.169	23	-.209	23	-6.314e-03	12	NC	1	NC	1
383	2	max	.06	3	.17	5	.219	5	3.547e-03	18	NC	1	NC	1
384		min	-.03	21	-.168	23	-.21	23	-6.314e-03	12	NC	1	NC	1
385	3	max	.06	3	.17	5	.219	5	3.547e-03	18	NC	1	NC	1
386		min	-.03	21	-.167	23	-.21	23	-6.314e-03	12	NC	1	NC	1
387	4	max	.06	3	.17	5	.219	5	3.547e-03	18	NC	1	NC	1
388		min	-.03	21	-.166	23	-.21	23	-6.314e-03	12	NC	1	NC	1
389	5	max	.06	3	.171	5	.219	5	3.547e-03	18	NC	1	NC	1
390		min	-.03	21	-.165	23	-.21	23	-6.314e-03	12	NC	1	NC	1
391	M41	1	max	0	1	0	0	1	1.084e-03	14	NC	1	NC	1
392		min	0	1	0	0	0	1	-2.012e-03	8	NC	1	NC	1
393	2	max	0	21	.023	28	.08	22	1.084e-03	14	NC	1	NC	1
394		min	0	27	.003	23	-.081	4	-2.012e-03	8	1417.852	24	1534.813	18
395	3	max	0	21	.04	28	.15	22	1.084e-03	14	NC	1	NC	1
396		min	-.001	27	0	22	-.153	4	-2.012e-03	8	707.04	24	758.402	18
397	4	max	0	21	.051	28	.21	23	1.084e-03	14	NC	1	NC	1
398		min	-.002	27	-.011	22	-.216	4	-2.012e-03	8	469.816	24	498.377	18

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC	
399		5	max	.001	21	.06	3	.267	23	1.084e-03	14	NC	1	NC	1
400			min	-.003	27	-.03	21	-.278	5	-2.012e-03	8	351.321	24	369.012	18
401	M42	1	max	.069	37	.17	5	.192	11	6.616e-03	4	NC	1	NC	1
402			min	-.022	19	-.168	23	-.164	17	-4.841e-03	22	NC	1	NC	1
403		2	max	.069	37	.169	5	.193	11	6.616e-03	4	NC	1	NC	1
404			min	-.022	19	-.168	23	-.164	17	-4.841e-03	22	NC	1	NC	1
405		3	max	.069	37	.167	5	.193	11	6.616e-03	4	NC	1	NC	1
406			min	-.022	19	-.167	23	-.164	17	-4.841e-03	22	NC	1	NC	1
407		4	max	.069	37	.166	17	.194	11	6.616e-03	4	NC	1	NC	1
408			min	-.022	19	-.166	11	-.165	17	-4.841e-03	22	NC	1	NC	1
409		5	max	.069	37	.165	17	.195	11	6.616e-03	4	NC	1	NC	1
410			min	-.022	19	-.166	11	-.165	17	-4.841e-03	22	NC	1	NC	1
411	M43	1	max	0	1	0	1	0	1	3.804e-03	5	NC	1	NC	1
412			min	0	1	0	1	0	1	-2.136e-03	23	NC	1	NC	1
413		2	max	.001	34	.076	17	.028	27	3.804e-03	5	NC	1	NC	1
414			min	0	16	-.079	11	-.006	21	-2.136e-03	23	1145.762	10	2108.493	6
415		3	max	.002	34	.141	17	.051	26	3.804e-03	5	NC	1	NC	1
416			min	0	16	-.149	11	-.009	21	-2.136e-03	23	570.821	10	1502.301	6
417		4	max	.003	34	.192	17	.067	26	3.804e-03	5	NC	1	NC	1
418			min	0	16	-.206	11	-.013	20	-2.136e-03	23	378.864	10	1636.908	2
419		5	max	.004	34	.233	17	.079	37	3.804e-03	5	NC	1	NC	1
420			min	0	16	-.255	11	-.027	19	-2.136e-03	23	283.015	10	1093.115	2
421	M44	1	max	.073	27	.17	5	.208	4	4.197e-03	18	NC	1	NC	1
422			min	-.029	21	-.169	23	-.175	22	-5.945e-03	12	NC	1	NC	1
423		2	max	.073	27	.169	5	.208	4	4.197e-03	18	NC	1	NC	1
424			min	-.029	21	-.167	23	-.174	22	-5.945e-03	12	NC	1	NC	1
425		3	max	.073	27	.168	5	.208	4	4.197e-03	18	NC	1	NC	1
426			min	-.029	21	-.166	23	-.173	22	-5.945e-03	12	NC	1	NC	1
427		4	max	.073	27	.167	5	.207	4	4.197e-03	18	NC	1	NC	1
428			min	-.029	21	-.165	23	-.173	22	-5.945e-03	12	NC	1	NC	1
429		5	max	.073	27	.167	5	.207	4	4.197e-03	18	NC	1	NC	1
430			min	-.029	21	-.164	23	-.172	22	-5.945e-03	12	NC	1	NC	1
431	M45A	1	max	0	1	0	1	0	1	2.119e-03	17	NC	1	NC	1
432			min	0	1	0	1	0	1	-3.853e-03	11	NC	1	NC	1
433		2	max	.001	30	.029	37	.077	22	2.119e-03	17	NC	1	NC	1
434			min	0	24	-.008	19	-.082	4	-3.853e-03	11	1382.163	6	2108.495	10
435		3	max	.002	30	.053	26	.143	22	2.119e-03	17	NC	1	NC	1
436			min	0	24	-.013	19	-.154	4	-3.853e-03	11	688.085	6	1502.303	10
437		4	max	.003	30	.071	26	.193	22	2.119e-03	17	NC	1	NC	1
438			min	0	24	-.02	20	-.212	4	-3.853e-03	11	456.28	6	2108.495	10
439		5	max	.004	30	.083	27	.232	22	2.119e-03	17	NC	1	NC	1
440			min	0	24	-.035	21	-.26	4	-3.853e-03	11	340.569	6	4840.104	66
441	M54A	1	max	.001	20	.152	5	.036	32	6.254e-03	23	NC	1	NC	1
442			min	-.086	26	-.152	23	-.002	14	-6.29e-03	5	NC	1	4373.295	70
443		2	max	.001	20	.149	5	.027	8	6.254e-03	23	NC	1	NC	1
444			min	-.086	26	-.149	23	-.024	14	-6.29e-03	5	NC	1	2911.757	26
445		3	max	0	20	.159	5	.033	20	6.603e-03	23	NC	1	NC	1
446			min	-.086	26	-.158	23	-.048	2	-6.649e-03	5	NC	1	1519.206	26
447		4	max	0	20	.195	5	.042	20	6.632e-03	23	NC	1	NC	1
448			min	-.086	26	-.194	23	-.076	2	-6.693e-03	5	2253.637	5	995.954	26
449		5	max	0	20	.227	5	.087	20	5.993e-03	23	NC	1	NC	1
450			min	-.086	26	-.225	23	-.137	2	-6.064e-03	5	1285.883	5	698.37	2
451	M55A	1	max	.028	8	.004	20	.112	5	3.162e-04	50	NC	1	NC	1
452			min	-.027	14	-.095	26	-.111	23	-9.487e-05	24	NC	1	NC	1
453		2	max	.028	8	.003	20	.121	5	3.162e-04	50	NC	1	NC	1
454			min	-.027	14	-.093	26	-.121	23	-9.487e-05	24	NC	1	NC	1
455		3	max	.028	8	.002	20	.131	5	3.162e-04	50	NC	1	NC	1

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
456		min	-.027	14	-.091	26	-.13	23	-9.487e-05	24	NC	1	NC	1
457	4	max	.028	8	.002	20	.14	5	3.162e-04	50	NC	1	NC	1
458		min	-.027	14	-.088	26	-.139	23	-9.487e-05	24	NC	1	NC	1
459	5	max	.028	8	.001	20	.15	5	3.162e-04	50	NC	1	NC	1
460		min	-.027	14	-.086	26	-.149	23	-9.487e-05	24	NC	1	NC	1
461	M56A	1	max	.039	20	.004	.146	5	2.202e-03	5	NC	1	NC	1
462		min	-.07	2	-.095	26	-.145	23	-2.184e-03	23	NC	1	NC	1
463		2	max	.039	20	.003	.157	5	2.202e-03	5	NC	1	NC	1
464		min	-.07	2	-.093	26	-.156	23	-2.184e-03	23	NC	1	NC	1
465	3	max	.039	20	.003	.167	5	2.202e-03	5	NC	1	NC	1	
466		min	-.07	2	-.09	26	-.166	23	-2.184e-03	23	NC	1	NC	1
467	4	max	.039	20	.002	.178	5	2.202e-03	5	NC	1	NC	1	
468		min	-.07	2	-.088	26	-.177	23	-2.184e-03	23	NC	1	NC	1
469	5	max	.039	20	0	.188	5	2.202e-03	5	NC	1	NC	1	
470		min	-.07	2	-.086	26	-.187	23	-2.184e-03	23	NC	1	NC	1
471	M57	1	max	.074	5	.004	.06	12	1.228e-03	26	NC	1	NC	1
472		min	-.073	23	-.1	26	-.054	18	-2.746e-04	20	NC	1	NC	1
473	2	max	.074	5	.004	.046	12	1.228e-03	26	NC	1	NC	1	
474		min	-.073	23	-.1	26	-.039	18	-2.746e-04	20	NC	1	NC	1
475	3	max	.074	5	.004	.037	13	1.228e-03	26	NC	1	NC	1	
476		min	-.073	23	-.101	26	-.031	19	-2.746e-04	20	NC	1	NC	1
477	4	max	.074	5	.004	.038	2	1.228e-03	26	NC	1	NC	1	
478		min	-.073	23	-.101	26	-.032	20	-2.746e-04	20	NC	1	NC	1
479	5	max	.074	5	.004	.05	3	1.228e-03	26	NC	1	NC	1	
480		min	-.073	23	-.102	26	-.043	21	-2.746e-04	20	NC	1	NC	1
481	M58	1	max	.037	13	.001	.15	23	3.342e-04	23	NC	1	NC	1
482		min	-.031	19	-.086	26	-.151	5	-4.123e-04	5	NC	1	NC	1
483	2	max	.037	13	.002	.131	23	3.342e-04	23	NC	1	NC	1	
484		min	-.031	19	-.09	26	-.132	5	-4.123e-04	5	NC	1	NC	1
485	3	max	.037	13	.003	.112	23	3.342e-04	23	NC	1	NC	1	
486		min	-.031	19	-.094	26	-.113	5	-4.123e-04	5	NC	1	NC	1
487	4	max	.037	13	.004	.092	23	3.342e-04	23	NC	1	NC	1	
488		min	-.031	19	-.097	26	-.093	5	-4.123e-04	5	NC	1	NC	1
489	5	max	.037	13	.004	.073	23	3.342e-04	23	NC	1	NC	1	
490		min	-.031	19	-.101	26	-.074	5	-4.123e-04	5	NC	1	NC	1
491	M59	1	max	.116	5	.014	.092	12	1.977e-03	2	NC	1	NC	1
492		min	-.112	23	-.105	37	-.058	18	-1.075e-03	20	NC	1	NC	1
493	2	max	.116	5	.012	.081	13	1.977e-03	2	NC	1	NC	1	
494		min	-.112	23	-.105	26	-.047	19	-1.075e-03	20	NC	1	NC	1
495	3	max	.116	5	.014	.074	13	1.977e-03	2	NC	1	NC	1	
496		min	-.112	23	-.106	26	-.04	19	-1.075e-03	20	NC	1	NC	1
497	4	max	.116	5	.015	.076	2	1.977e-03	2	NC	1	NC	1	
498		min	-.112	23	-.106	26	-.042	20	-1.075e-03	20	NC	1	NC	1
499	5	max	.116	5	.016	.084	3	1.977e-03	2	NC	1	NC	1	
500		min	-.112	23	-.107	26	-.049	21	-1.075e-03	20	NC	1	NC	1
501	M60	1	max	.074	13	0	.192	23	2.049e-03	23	NC	1	NC	1
502		min	-.04	19	-.086	26	-.196	5	-2.15e-03	5	NC	1	NC	1
503	2	max	.074	13	.004	.172	23	2.049e-03	23	NC	1	NC	1	
504		min	-.04	19	-.091	26	-.176	5	-2.15e-03	5	NC	1	NC	1
505	3	max	.074	13	.007	.152	23	2.049e-03	23	NC	1	NC	1	
506		min	-.04	19	-.096	26	-.156	5	-2.15e-03	5	NC	1	NC	1
507	4	max	.074	13	.01	.132	23	2.049e-03	23	NC	1	NC	1	
508		min	-.04	19	-.101	26	-.136	5	-2.15e-03	5	NC	1	NC	1
509	5	max	.074	13	.014	.112	23	2.049e-03	23	NC	1	NC	1	
510		min	-.04	19	-.106	26	-.116	5	-2.15e-03	5	NC	1	NC	1
511	M61	1	max	.09	2	0	.204	23	1.085e-03	23	NC	1	NC	1
512		min	-.051	20	-.086	26	-.206	5	-1.123e-03	5	NC	1	NC	1

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC	
513	2	max	.09	2	.004	20	.195	23	1.085e-03	23	NC	1	NC	1	
514		min	-.051	20	-.088	26	-.197	5	-1.123e-03	5	NC	1	NC	1	
515	3	max	.09	2	.007	20	.186	23	1.085e-03	23	NC	1	NC	1	
516		min	-.051	20	-.089	26	-.188	5	-1.123e-03	5	NC	1	NC	1	
517	4	max	.09	2	.01	20	.177	23	1.085e-03	23	NC	1	NC	1	
518		min	-.051	20	-.091	26	-.178	5	-1.123e-03	5	NC	1	NC	1	
519	5	max	.09	2	.013	20	.168	23	1.085e-03	23	NC	1	NC	1	
520		min	-.051	20	-.093	26	-.169	5	-1.123e-03	5	NC	1	NC	1	
521	M70	1	max	.075	22	0	.034	21	3.688e-04	16	NC	1	NC	1	
522		min	-.088	4	-.1	26	-.046	3	-6.89e-04	10	NC	1	NC	1	
523	2	max	.075	22	0	20	.031	21	3.688e-04	16	NC	1	NC	1	
524		min	-.088	4	-.1	26	-.043	3	-6.89e-04	10	NC	1	NC	1	
525	3	max	.075	22	0	20	.028	21	3.688e-04	16	NC	1	NC	1	
526		min	-.088	4	-.1	26	-.039	3	-6.89e-04	10	NC	1	NC	1	
527	4	max	.075	22	.001	20	.025	21	3.688e-04	16	NC	1	NC	1	
528		min	-.088	4	-.099	26	-.036	3	-6.89e-04	10	NC	1	NC	1	
529	5	max	.075	22	.001	20	.021	21	3.688e-04	16	NC	1	NC	1	
530		min	-.088	4	-.099	26	-.033	3	-6.89e-04	10	NC	1	NC	1	
531	M71	1	max	.078	10	0	.047	10	2.256e-04	17	NC	1	NC	1	
532		min	-.076	16	-.1	26	-.046	16	-6.05e-04	35	NC	1	NC	1	
533	2	max	.078	10	0	20	.043	10	2.256e-04	17	NC	1	NC	1	
534		min	-.076	16	-.1	26	-.042	16	-6.05e-04	35	NC	1	NC	1	
535	3	max	.078	10	0	20	.039	10	2.256e-04	17	NC	1	NC	1	
536		min	-.076	16	-.099	26	-.037	16	-6.05e-04	35	NC	1	NC	1	
537	4	max	.078	10	0	20	.036	9	2.256e-04	17	NC	1	NC	1	
538		min	-.076	16	-.099	26	-.034	15	-6.05e-04	35	NC	1	NC	1	
539	5	max	.078	10	0	20	.032	9	2.256e-04	17	NC	1	NC	1	
540		min	-.076	16	-.099	26	-.031	15	-6.05e-04	35	NC	1	NC	1	
541	M72	1	max	.1	26	.031	5	.092	4	8.929e-03	4	NC	1	NC	1
542		min	0	20	-.031	23	-.072	22	-8.635e-03	23	8199.14	50	1194.61	32	
543	2	max	.1	26	.032	5	.097	4	8.722e-03	4	NC	1	NC	1	
544		min	0	20	-.031	23	-.082	22	-8.394e-03	22	NC	1	1536.067	32	
545	3	max	.1	26	.032	5	.095	4	8.297e-03	4	NC	1	NC	1	
546		min	0	20	-.031	23	-.087	22	-8.064e-03	22	7454.666	4	2347.507	35	
547	4	max	.1	26	.026	17	.089	4	8.255e-03	4	NC	1	NC	1	
548		min	0	20	-.026	11	-.088	22	-8.094e-03	22	NC	1	1499.153	35	
549	5	max	.1	26	.02	17	.084	16	8.279e-03	5	NC	1	NC	1	
550		min	0	20	-.02	11	-.09	10	-8.239e-03	23	NC	1	1157.515	35	
551	M73	1	max	.083	22	-.003	20	.143	22	-3.894e-06	18	NC	1	NC	1
552		min	-.089	4	-.113	26	-.152	4	-6.682e-04	36	NC	1	NC	1	
553	2	max	.083	22	-.002	20	.118	22	-3.894e-06	18	NC	1	NC	1	
554		min	-.089	4	-.11	26	-.125	4	-6.682e-04	36	NC	1	NC	1	
555	3	max	.083	22	-.001	20	.092	22	-3.894e-06	18	NC	1	NC	1	
556		min	-.089	4	-.107	26	-.099	4	-6.682e-04	36	NC	1	NC	1	
557	4	max	.083	22	0	20	.066	22	-3.894e-06	18	NC	1	NC	1	
558		min	-.089	4	-.103	26	-.073	4	-6.682e-04	36	NC	1	NC	1	
559	5	max	.083	22	0	20	.041	21	-3.894e-06	18	NC	1	NC	1	
560		min	-.089	4	-.1	26	-.047	3	-6.682e-04	36	NC	1	NC	1	
561	M74	1	max	.067	17	0	.039	12	6.353e-04	5	NC	1	NC	1	
562		min	-.079	11	-.099	26	-.028	18	-2.479e-04	23	NC	1	NC	1	
563	2	max	.067	17	0	20	.035	12	6.353e-04	5	NC	1	NC	1	
564		min	-.079	11	-.099	26	-.024	18	-2.479e-04	23	NC	1	NC	1	
565	3	max	.067	17	0	20	.031	12	6.353e-04	5	NC	1	NC	1	
566		min	-.079	11	-.099	26	-.021	18	-2.479e-04	23	NC	1	NC	1	
567	4	max	.067	17	0	20	.029	13	6.353e-04	5	NC	1	NC	1	
568		min	-.079	11	-.098	26	-.018	19	-2.479e-04	23	NC	1	NC	1	
569	5	max	.067	17	0	20	.027	13	6.353e-04	5	NC	1	NC	1	

**Envelope Member Section Deflections (Continued)**

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y Ratio	LC (n)	L/z Ratio	LC	
570		min	-.079	11	-.098	26	-.016	19	-2.479e-04	23	NC	1	NC	1	
571	M75	1	max	.071	5	0	20	.036	24	6.753e-04	28	NC	1	NC	1
572		min	-.068	23	-.099	26	-.039	6	-2.237e-04	22	NC	1	NC	1	
573		2	max	.071	5	0	20	.033	24	6.753e-04	28	NC	1	NC	1
574		min	-.068	23	-.099	26	-.035	6	-2.237e-04	22	NC	1	NC	1	
575		3	max	.071	5	0	20	.029	24	6.753e-04	28	NC	1	NC	1
576		min	-.068	23	-.098	26	-.032	6	-2.237e-04	22	NC	1	NC	1	
577		4	max	.071	5	0	20	.026	24	6.753e-04	28	NC	1	NC	1
578		min	-.068	23	-.098	26	-.028	6	-2.237e-04	22	NC	1	NC	1	
579		5	max	.071	5	0	20	.022	24	6.753e-04	28	NC	1	NC	1
580		min	-.068	23	-.098	26	-.025	6	-2.237e-04	22	NC	1	NC	1	
581	M76	1	max	.099	26	.031	17	.079	12	8.746e-03	17	NC	1	NC	1
582		min	0	20	-.031	11	-.06	17	-8.891e-03	11	NC	1	1221.501	31	
583		2	max	.099	26	.03	17	.082	12	8.489e-03	17	NC	1	NC	1
584		min	0	20	-.031	11	-.068	18	-8.601e-03	11	NC	1	1599.275	31	
585		3	max	.099	26	.03	17	.079	12	7.964e-03	17	NC	1	NC	1
586		min	0	20	-.03	11	-.072	17	-8.007e-03	11	9916.891	5	2374.087	29	
587		4	max	.099	26	.026	5	.075	23	8.208e-03	5	NC	1	NC	1
588		min	0	20	-.026	23	-.075	5	-8.195e-03	23	NC	1	1540.264	29	
589		5	max	.099	26	.02	17	.072	23	8.331e-03	5	NC	1	NC	1
590		min	0	20	-.02	11	-.079	5	-8.29e-03	23	NC	1	1171.814	29	
591	M77	1	max	.073	17	-.002	20	.136	11	6.337e-04	27	NC	1	NC	1
592		min	-.077	11	-.111	26	-.131	17	-9.17e-05	21	NC	1	NC	1	
593		2	max	.073	17	-.002	20	.111	11	6.337e-04	27	NC	1	NC	1
594		min	-.077	11	-.108	26	-.106	17	-9.17e-05	21	NC	1	NC	1	
595		3	max	.073	17	-.001	20	.085	11	6.337e-04	27	NC	1	NC	1
596		min	-.077	11	-.105	26	-.081	17	-9.17e-05	21	NC	1	NC	1	
597		4	max	.073	17	0	20	.06	11	6.337e-04	27	NC	1	NC	1
598		min	-.077	11	-.102	26	-.055	17	-9.17e-05	21	NC	1	NC	1	
599		5	max	.073	17	0	20	.038	12	6.337e-04	27	NC	1	NC	1
600		min	-.077	11	-.099	26	-.033	18	-9.17e-05	21	NC	1	NC	1	

**Envelope AISC 14th(360-10): LRFD Steel Code Checks**

Member	Shape	Code Check	Loc[ft]	LC	Shear ..Loc[ft]	Dir	LC	phi*Pnc...	phi*Pnt...	phi*Mn...	phi*Mn...Cb	Eqn			
1	M15	L3x2x4	.680	.771	10	.106	.771	z	9	35.286	38.88	.826	2.489	1..	H2-1
2	M12	L3x2x4	.654	.771	3	.121	.771	z	3	35.286	38.88	.826	2.453	1..	H2-1
3	M13	L3x2x4	.600	1.093	4	.115	1.093	z	5	37.029	38.88	.826	2.489	1..	H2-1
4	M11	L3x2x4	.527	0	12	.115	0	z	11	37.029	38.88	.826	2.489	1..	H2-1
5	M8	PIPE 2.5	.400	3.427	4	.408	3.917		5	44.732	50.715	3.596	3.596	3..	H3-6
6	M17	L2.5x2.5x3	.369	3.809	4	.061	3.809	y	3	17.176	29.192	.873	1.784	1..	H2-1
7	M16	L3x2x4	.362	0	9	.065	.251	z	9	37.029	38.88	.826	2.489	1..	H2-1
8	M14	L3x2x4	.326	1.093	6	.065	1.093	z	13	37.029	38.88	.826	2.489	1..	H2-1
9	M9	1/2"x6"	.313	0	27	.019	.625	y	11	84.321	97.2	1.012	12.15	1..	H1-1b
10	M37	PIPE 2.0	.312	1.24	3	.175	.292	z	27	26.521	32.13	1.872	1.872	1..	H1-1b
11	M18	L2.5x2.5x3	.303	1.066	8	.053	1.066	z	9	17.176	29.192	.873	1.97	2..	H2-1
12	M28	3/8x6	.272	.25	5	.060	.25	y	5	69.866	72.9	.57	9.113	1..	H1-1b
13	M45	PIPE 2.0	.263	6.5	32	.213	6.5		3	14.916	32.13	1.872	1.872	2.5	H1-1b
14	M5	PIPE 2.0	.245	6.5	32	.179	5.75		12	14.916	32.13	1.872	1.872	2..	H1-1b
15	M29	3/8x6	.237	0	4	.025	.25	y	11	69.866	72.9	.57	9.113	1..	H1-1b
16	M10	1/2"x6"	.236	0	29	.045	.625	y	5	84.321	97.2	1.012	12.15	1..	H1-1b
17	M56	PIPE 2.0	.177	2.917	11	.117	2.917		11	26.521	32.13	1.872	1.872	2..	H1-1b
18	M54A	PIPE 2.0	.171	6.5	11	.122	5.75		11	14.916	32.13	1.872	1.872	2..	H1-1b
19	M21	PIPE 2.0	.142	2.917	4	.120	2.917		3	26.521	32.13	1.872	1.872	1..	H1-1b
20	M48	PIPE 2.0	.135	2.917	11	.128	0		8	26.521	32.13	1.872	1.872	1..	H1-1b
21	M41	L2.5x2.5x3	.134	2.069	3	.006	4.139	z	3	16.566	29.192	.873	1.738	1..	H2-1

**Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)**

Member	Shape	Code Check	Loc[ft]	LC	Shear ..	Loc[ft]	Dir	LC	phi*Pnc...	phi*Pnt ...	phi*Mn ...	phi*Mn ...	Cb	Eqn
22	M39	L2.5x2.5x3	.123	2.069	13	.006	4.139	y	25	16.566	29.192	.873	1.738	1... H2-1
23	M45A	L2.5x2.5x3	.098	2.114	35	.006	4.228	z	16	16.172	29.192	.873	1.729	1... H2-1
24	M43	L2.5x2.5x3	.095	2.114	29	.006	4.228	y	12	16.172	29.192	.873	1.729	1... H2-1
25	M2	L2x2x3	.094	2.917	5	.004	0	z	29	15.276	23.393	.558	1.239	2... H2-1
26	M1	L2x2x3	.088	2.917	11	.006	0	y	50	15.276	23.393	.558	1.239	2... H2-1
27	M72	PIPE 2.0	.070	1.958	3	.062	.53		6	26.732	32.13	1.872	1.872	1... H1-1b
28	M76	PIPE 2.0	.057	1.958	12	.047	.53		10	26.732	32.13	1.872	1.872	1... H1-1b