May 15, 2014
Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## Re: $\quad$ Notice of Exempt Modification - Antenna Swap <br> Property Address: 244 Gates Road, Lebanon, CT <br> (the "Property") <br> Applicant: New Cingular Wireless PCS, LLC ("AT\&T")

Dear Ms. Bachman:
AT\&T currently maintains a wireless telecommunications facility on an existing 121 -foot tower location on the Property, consisting of nine (9) wireless telecommunication antennas at an antenna center line height of 123 -feet. The tower is owned by Southern New England Telephone ("AT\&T"). The Council approved AT\&T's use of the tower in the following prior decisions; EM-CING-071-081124 and EM-CING-071-130124. AT\&T now intends to replace three (3) CSS DUO1417-8686-4-0 panel antennas and three (3) Andrew SBNH 1D6565C panel antennas with nine (9) CCI HPA - 65R-BUU H-8 panel antennas, while retaining three (3) Powerwave 7770 panel antennas (for a total of twelve (12) panel antennas) at the 123-foot level. Please refer to Tab 1 for further specifications of the replacement antennas.

Please accept this application as notification pursuant to R.C.S.A. §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16-50j-72(b)(2). In accordance with R.C.S.A. §16-50j-73, a copy of this letter is being sent to Joyce Okonuk, First Selectman of the Town of Lebanon, 570 Exeter Road, Lebanon, CT 06249. A copy of this letter is also being sent to Southern New England Telephone ("AT\&T Towers"), the owner of the property where the tower is located.

The planned modifications to AT\&T's facility fall squarely within those activities explicitly provided for in R.C.S.A. §16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing tower. AT\&T's replacement antennas will be installed at the 123 -foot level of the 121 -foot tower.
2. The proposed modifications will not involve any changes to ground-mounted equipment and, therefore, will not require and extension of the site boundary.
3. The proposed modifications will not increase the noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the modified facility will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative worst-case RF emissions calculation for AT\&T's modified facility is provided in the RF Emissions Compliance Report, included in Tab 2.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The tower and its foundation can support AT\&T's proposed modifications. (See Structural Analysis Report included in Tab 3).

For the foregoing reasons, AT\&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitutes an exempt modification under R.C.S.A. §16-50j-72(b)(2).

Sincerely,

Kristen Smith

## Enclosures

CC: Joyce Okonuk, First Selectman Town of Lebanon
Southern New England Telephone ("AT\&T")


GENERAL NOTES:





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Dewberry Engineers inc.




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244 GATES RD, LEBANON, CT 06249 NEW LONDON COUNTY SHEET TIIE

GENERAL NOTES
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ROCKY HILL., CT 06067

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CT1065 LEBANON

CONSTRUCTION DRAWINGS


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244 GATES RD, LEBANON, CT 06249 NEW LONDON COUNTY
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500 ENTERPRISE DRIVE SUITE 3A
ROCKY HILL, CT 06067
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smartlink ANNAPOLS EXCHANGE PARKWA SUITE 200
ANNAPOLIS, MD 21401

CT1065
LEBANON


Dewlberry Dewberty Engineers Inc.



244 GATES RD, LEBANON, CT 06249 NEW LONDON COUNTY SHIET TIIE

GROUNDING NOTES \& DETAILS
SHEET NUMER
$E-1$

Todd Oliver
Smartlink, LLC
Market Manager, NE
33 Boston Post Road, Suite 210
Marlborough, MA 01752
Reference: Smartlink LLC Site, Lebanon: 244 Gates Road Lebanon CT 06249
Date: 05 May 2014

1. This letter will address the additional RF impact that adding AT\&T LTE antennas to the referenced site. Attached are two documents which cover the modeled RF emissions from the site.
2. The first report, "RF Emissions Compliance Report," for the site complied by Sitesafe, uses the antenna patterns for the antennas at the site to calculate the General Public Maximum Permissible Exposure (MPE) on the ground. The total MPE of all the carriers is 1.392\% (based on the General Public MPE) based on this modeling, with AT\&T antennas emitting a maximum of $1.213 \%$ of the General Public MPE on the ground.
3. The second attachment has the calculations, used by the Connecticut Siting Council, which assumes the maximum antenna gain transmits in a spherical pattern where the worst case results would be at the base of the tower. That calculation, based on the existing antennas, gives a result of $23.72 \%$ of the General Public MPE, with the AT\&T antennas emitting 22.35\% of the General Public MPE on the ground, using the modeling predictions used by Connecticut Siting Council.
4. In either case, the site is compliant with FCC guidelines. If you have any questions regarding this site, the compliance report, please contact me at 719-434-0700 or dcotton@sitesafe.com.

Director, RF Compliance

# RF EMISSIONS COMPLIANCE REPORT 

# Smartlink on behalf of AT\&T Mobility, LLC 

Site FA: 10035007
Site ID: CT1065
Site Name: Lebanon
Address: 244 Gates Road
Lebanon, CT 06249
5/5/2014

Report Status:

## AT\&T Mobility LLC Is Compliant.

Prepared By:
Sitesafe, Inc.

Engineering Statement in Re:<br>Electromagnetic Energy Analysis<br>AT\&T Mobility LLC<br>Lebanon, CT 06249

My signature on the cover of this document indicates:
That I am registered as a Professional Engineer in the jurisdiction indicated; and
That I have extensive professional experience in the wireless communications engineering industry; and

That I am an employee of Sitesafe, Inc. in Arlington, Virginia; and
That I am thoroughly familiar with the Rules and Regulations of the Federal Communications Commission ("the FCC" and "the FCC Rules") both in general and specifically as they apply to the FCC's Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields; and

That the technical information serving as the basis for this report was supplied by Smartlink (See attached Site Summary and Carrier documents), and that AT\&T Mobility LLC's installations involve communications equipment, antennas and associated technical equipment at a location referred to as the "Lebanon" ("the site"); and

That AT\&T Mobility LLC proposes to operate at the site with transmit antennas listed in the carrier summary and with a maximum effective radiated power as specified by AT\&T Mobility LLC and shown on the worksheet, and that worst-case $100 \%$ duty cycle have been assumed; and

That this analysis has been performed with the assumption that the ground immediately surrounding the tower is primarily flat or falling; and

That at this time, the FCC requires that certain licensees address specific levels of radiofrequency energy to which workers or members of the public might possibly be exposed (at §1.1307(b) of the FCC Rules); and

That such consideration of possible exposure of humans to radio-frequency radiation must utilize the standards set by the FCC, which is the Federal Agency having jurisdiction over communications facilities; and

That the FCC rules define two tiers of permissible exposure guidelines: 1) "uncontrolled environments," defined as situations in which persons may not be aware of (the "general public"), or may not be able to control their exposure to a transmission facility; and (2) "controlled environments," which defines situations in which persons are aware of their potential for exposure (industry personnel); and

That this statement specifically addresses the uncontrolled environment (which is more conservative than the controlled environment) and the limit set forth in the FCC rules for licensees of AT\&T Mobility LLC's operating frequency as shown on the attached antenna worksheet; and

That when applying the uncontrolled environment standards, the predicted Maximum Power Density at two meters above ground level from the proposed AT\&T Mobility LLC operation is no more than $1.213 \%$ of the maximum in any accessible area on the ground and

That it is understood per FCC Guidelines and OET65 Appendix A, that regardless of the existent radio-frequency environment, only those licenses whose contributions exceed five percent of the exposure limit pertinent to their operation(s) bear any responsibility for bringing any noncompliant area(s) into compliance; and

That when applying the uncontrolled environment standards, the cumulative predicted energy density from the proposed operation is no more than $1.392 \%$ of the maximum in any accessible area up to two meters above the ground per OET-65; and

That the calculations provided in this report are based on data provided by the client and antenna pattern data supplied by the antenna manufacturer, in accordance with FCC guidelines listed in OET-65. Horizontal and vertical antenna patterns are combined for modeling purposes to accurately reflect the energy two meters above ground level where on-axis energy refers to maximum energy two meters above the ground along the azimuth of the antenna and where area energy refers to the maximum energy anywhere two meters above the ground regardless of the antenna azimuth, accounting for cumulative energy from multiple antennas for the carrier and frequency range indicated; and

That the Occupational Safety and Health Administration has policies in place which address worker safety in and around communications sites, thus individual companies will be responsible for their employees’ training regarding Radio Frequency Safety.

In summary, it is stated here that the proposed operation at the site would not result in exposure of the Public to excessive levels of radio-frequency energy as defined in the FCC Rules and Regulations, specifically 47 CFR 1.1307 and that AT\&T Mobility LLC's proposed operation is completely compliant.

Finally, it is stated that access to the tower should be restricted to communication industry professionals, and approved contractor personnel trained in radio-frequency safety; and that the instant analysis addresses exposure levels at two meters above ground level and does not address exposure levels on the tower, or in the immediate proximity of the antennas.

Note: Sitesafe has used data obtained from the "Connecticut Siting Council" to create this report. The manufacturer antenna patterns for AT\&T Mobility, LLC were used to determine the RF emissions from the AT\&T Mobility, LLC antennas. Generic antennas were used for the other carriers on the tower, as this information was not available, or provided at the time the study was conducted. Sitesafe has conducted FCC research on this site, and was updated in this report with the appropriate FCC call signs and Maximum ERP values. Sitesafe has also referenced the AT\&T Mobility, LLC construction diagram for this site.

The following documents below were the primary sources of data used to create this report. The primary document was the "Connecticut Siting Council" document. The AT\&T Mobility, LLC construction diagram was referenced when appropriate.

Connecticut Siting Council: AlphaExMPowDens 4-16-14
AT\&T Mobility, LLC Construction Diagram: 10035007.AE201.140307 (CT1065)
Dewberry.RevA KES2 MD2 DC Comments 4-8-14.pdf

# AT\&T Mobility LLC <br> Lebanon <br> Site Summary 

| Carrier | Area Maximum Percentage MPE |
| :---: | :---: |
| AT\&T Mobility LLC | $0.477 \%$ |
| AT\&T Mobility LLC | $0.32 \%$ |
| AT\&T Mobility LLC | $0.416 \%$ |
| T-Mobile (VoiceStream) | $0.179 \%$ |
|  |  |
| Composite Site MPE: | $1.392 \%$ |

Attachment 2

| Control Number | Site | Carrier | \#Channels | ERP/Ch | Ant Ht | Power Der | MHz | S | \%MPE | Site Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EM-CING-071-130124 | Lebanon-244 Gates Road | AT\&T UMTS | 2 | 565 | 124 | 0.026425 | 880 | 0.5867 | 4.50\% |  |
| EM-CING-071-130124 | Lebanon-244 Gates Road | AT\&T UMTS | 2 | 875 | 124 | 0.040924 | 1900 | 1.0000 | 4.09\% |  |
| EM-CING-071-130124 | Lebanon-244 Gates Road | AT\&T GSM | 1 | 283 | 124 | 0.006618 | 880 | 0.5867 | 1.13\% |  |
| EM-CING-071-130124 | Lebanon-244 Gates Road | AT\&T GSM | 4 | 525 | 124 | 0.049108 | 1900 | 1.0000 | 4.91\% |  |
| EM-CING-071-130124 | Lebanon-244 Gates Road | AT\&T LTE | 1 | 1615 | 124 | 0.037767 | 734 | 0.4893 | 7.72\% |  |
| Omnipt Ex Mod 12/10/ | Lebanon-244 Gates Road | VoiceStream | 2 | 197 | 102 | 0.013617 | 1930 | 1.0000 | 1.36\% | 23.72\% |

# STRUCTURAL ANALYSIS REPORT 

AT\&T DESIGNATION:

## SITE DATA:

ANALYSIS CRITERIA:
Codes:

Kevin Clements
520 S. Main Street, Suite 2531
Akron, OH 44311
(330) 572-3546
kclements@gpdgroup.com

GPD\# 2014723.21.65054.01
February 26, 2014


65054
10035007
CT1065
LEBANON
MOD LTE 01.11.14

TIA/EIA-222-F, 2003 IBC, ASCE7-05 \& 2005 CBC
$100-\mathrm{mph}$ (fastest-mile) with $0 "$ ice
$120-\mathrm{mph}$ ( 3 -second gust) with $0^{\prime \prime}$ ice
$38-\mathrm{mph}$ (fastest-mile) with $0.75^{\prime \prime}$ ice
244 Gates Road, Lebanon, CT 06249, New London County Latitude $41^{\circ} 40^{\prime} 58.57{ }^{\prime \prime} \mathrm{N}$, Longitude $72^{\circ}{ }^{12}$ 58.295" W Market: NEW ENGLAND
121' Self Support Tower
Mr. Jerry Bruno,
GPD is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

## Analysis Results

| Tower Stress Level with Proposed Equipment: | $95.9 \%$ | Pass |
| :--- | :--- | :--- |
| Foundation Ratio with Proposed Equipment: | $95.6 \%$ | Pass |

We at GPD appreciate the opportunity of providing our continuing professional services to you and Smartlink, LLC. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.

Respectfully submitted,


## SUMMARY \& RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT\&T Mobility to Smartlink, LLC. This report was commissioned by Mr. Jerry Bruno of Smartlink, LLC.

## TOWER SUMMARY AND RESULTS

| Member | Capacity | Results |
| :--- | :---: | :---: |
| Leg | $58.0 \%$ | Pass |
| Diagonal | $90.7 \%$ | Pass |
| Secondary Horizontal | $37.2 \%$ | Pass |
| Top Girt | $95.9 \%$ | Pass |
| Bolt Checks | $68.3 \%$ | Pass |
| Anchor Rods | $91.0 \%$ | Pass |
|  |  |  |
| Foundation | $95.6 \%$ | Pass |

## ANALYSIS METHOD

tnxTower (Version 6.1.4.1), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a recent site visit.

DOCUMENTS PROVIDED

| Document | Remarks | Source |
| :--- | :--- | :---: |
| Equipment Modification Form | Equipment Modification Form, dated 1/14/2014 | Siterra |
| RF Data Sheet | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Tower Design | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Geotechnical Report | GPD Job \#: 2012832.03, dated 12/10/2012 | Siterra |
| Tower Mapping | GPD Job \#: 2012832.03, dated 12/19/2012 | Siterra |
| Foundation Mapping | GPD Job \#: 2012832.03, dated 12/10/2012 | Siterra |

## ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. All prior structural modifications are assumed to be as per data supplied/available and to have been properly installed.
10. Loading interpreted from photos is accurate to $\pm 5^{\prime} \mathrm{AGL}$, antenna size accurate to $\pm 3.3 \mathrm{sf}$, and coax equal to the number of existing antennas without reserve.
11. All existing loading was obtained from the Provided Equipment Modification Form, the Tower Mapping by GPD (Job \#: 2012832.03, dated 12/19/2012) and site photos and is assumed to be accurate.
12. Tower Leg A is assumed to face 0 degrees from true north based on satellite imagery.
13. Foundation steel was not able to be determined through testing. Therefore it was assumed that the foundation steel in place is equal to or in excess of the soil failure criteria in the foundation analysis.
14. The existing AT\&T loading has been modeled based on the most recent site photos.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

## DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a recent site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the specified code recommended amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

## APPENDIX A

Tower Analysis Summary Form

## Tower Analysis Summary Form

General Info

| Site Name | LEBANON |
| :--- | :---: |
| Site Number | 65054 |
| FA Number | 10035007 |
| Date of Analysis | February 26, 2014 |
| Company Performing Analysis | GPD |$\quad$|  |
| :--- |

## The information contained in this summary report is not to be used independently from the PE stamped tower analysis.

| Tower Info | Description | Date |
| :--- | :--- | :--- |
| Tower Type (G, SST, MP) SST <br> Tower Height (top of steel AGL) 121' <br> Tower Manufacturer N/A <br> Tower Model N/A |  |  |
| Tower Design | N/A |  |
| Foundation Design | N/A |  |
| Geotech Report | GPD Job \#: 2012832.03 | $12 / 10 / 2012$ |
| Tower Mapping | GPD Job \#: 2012832.03 | $12 / 19 / 2012$ |
| Previous Structural Analysis | N/A |  |
| Foundation Mapping | GPD Job \#: 2012832.03 | 12/10/2012 |

Design Parameters

| Design Code Used | TIA/EIA-222-F |
| :--- | :---: |
|  | 2003 IBC, ASCE7-05 \& 2005 CBC |
| Location of Tower (County, State) | New London, CT |
| Basic Wind Speed (mph) | 100 (fastest-mile) |
| IIe Thickness ( (m) | 0.75 |
| Structure Classification (I, II, III) |  |
| Exposure Category (B, C, D) |  |
| Topographic Category (1 to 5) |  |

Analysis Results (\% Maximum Usage)

| Existing/Reserved + Future + Proposed Condition |  |
| :--- | :---: |
| Tower (\%) | $95.9 \%$ |
| Anchor Rods (\%) | $91.0 \%$ |
| Foundation $(\%)$ | $95.6 \%$ |
| Foundation Adequate? | Yes |


| Legs | 50 |
| :--- | :--- |
| Diagonals | 36 |
| Bolts | A325N |
| Anchor Rods | 36 |

Existing / Reserved Loading

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | Antenna $\mathrm{CL}(\mathrm{ft})$ | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Face/Leg |
| AT\&T Mobility | 121 | 129 | 1 | Dipole | Unknown | 16' Dipole |  | 4 | Unknown | Star Mount | 1 | Unknown | 1/2" | Face "B" |
| AT\&T Mobility | 121 | 124 | 6 | Panel | Powerwave | RA21.7770.00 | 30/150/270 |  |  | on the same mounts | 9 | Unknown | 1-5/8" | Face "A" |
| AT\&T Mobility | 121 | 124 | 6 | TMA | Powerwave | LGP21401 |  |  |  | on the same mounts | 3 | Unknown | 1-5/8" | Face "B" |
| AT\&T Mobility | 121 | 124 | 6 | TMA | Powerwave | LGP21901 |  |  |  | on the same mounts | 1 | Unknown | 1/2" | Face "A" |
| AT\&T Mobility | 121 | 124 | 2 | Panel | Powerwave | P65-17-XLH-RR | 30/270 |  |  | on the same mounts | 2 | DC Power | 3/4" | Face "B" |
| AT\&T Mobility | 121 | 124 | 1 | Panel | Andrew | SBNH-1D6565C | 150 |  |  | on the same mounts | 1 | Fiber | 1/2" | Face "B" |
| AT\&T Mobility | 121 | 124 | 6 | RRU | Ericsson | RRUS-11 |  |  |  | on the same mounts |  |  |  |  |
| AT\&T Mobility | 121 | 121 | 1 | Squid | Raycap | DC6-48-60-18-8F |  |  |  | on the same mounts |  |  |  |  |

Note: All existing atnennas and TMAs shall be removed prior to the installation of the proposed equipment and have not been considered for this analysis. All other equipment shall be removed

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | Antenna CL (ft) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Face/Leg |
| AT\&T Mobility | 121 | 124 | - | Panel | CCI | HPA-65R-BUU-H8-K | 30/150/270 |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 | 6 | TMA | CCI | Twin TMACCI-BP |  |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 |  | RRU | Ericsson | RRUS 12 |  |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 | 2 | RRU | Ericsson | RRUS-11 |  |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 | 2 | RRU | Ericsson | RRUS A2 MODULE |  |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 | 1 | RRU | Ericsson | RRUS-32 |  |  |  | on the existing mounts |  |  |  |  |
| AT\&T Mobility | 121 | 124 | 1 | RRU | Ericsson | RRUS E2 |  |  |  | on the existing mounts |  |  |  |  |

Note: The proposed equipment shall be installed in addition to the remaining equipment at the same elevation.

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | Antenna CL (ft) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Face/Leg |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## APPENDIX B

tnxTower Output File

| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 | Job | 65054 - LEBANON | $\begin{aligned} & \text { Page } \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:08:07 02/26/14 } \end{array}$ |
| Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Client | Smartlink, LLC | Designed by jboegel |

## Tower Input Data

The main tower is a 4 x free standing tower with an overall height of 121.00 ft above the ground line.
The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 6.25 ft at the top and 11.25 ft at the base.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in New London County, Connecticut.
Basic wind speed of 100 mph .
Nominal ice thickness of 0.7500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 38 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in tower member design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Face or Leg | Allow Shield | Component Type | Placement <br> ft | Face Offset in | Lateral Offset (Frac FW) | \# | \# Per Row | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Climbing | A | Yes | Af (CfAe) | 121.00-8.00 | 1.0000 | 0 | 1 | 1 | 3.8400 | 3.8400 | 15.3600 | 4.81 |
| Ladder (Af) LDF4-50A (1/2 FOAM) | A | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.05 | 1 | 1 | 0.6300 | 0.6300 |  | 0.15 |
| $\begin{aligned} & \text { LDF7-50A } \\ & (1-5 / 8 \text { FOAM }) \end{aligned}$ | A | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.08 | 3 | 2 | 0.7500 | 1.9800 |  | 0.82 |
| $\begin{gathered} \text { LDF7-50A } \\ (1-5 / 8 \text { FOAM }) \end{gathered}$ | A | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.45 | 6 | 3 | 0.7500 | 1.9800 |  | 0.82 |
| $\begin{gathered} \text { LDF7-50A } \\ (1-5 / 8 \text { FOAM }) \end{gathered}$ | B | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0 | 3 | 2 | 0.7500 | 1.9800 |  | 0.82 |
| $\begin{aligned} & \text { LDF4-50A } \\ & (1 / 2 \text { FOAM }) \end{aligned}$ | B | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.05 | 1 | 1 | 0.6300 | 0.6300 |  | 0.15 |
| 1/2" Fiber Cable | B | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.03 | 1 | 1 | 0.6300 | 0.6300 |  | 0.15 |
| 3/4" DC | B | Yes | Ar (CfAe) | 121.00-8.00 | 0.5000 | 0.05 | 2 | 2 | 0.7500 | 0.7500 |  | 0.33 |
| Power Line Safety Line 3/8 | A | Yes | Af (CfAe) | 121.00-8.00 | 1.0000 | 0 | 1 | 1 | 0.3750 | 0.3750 | 1.1800 | 0.22 |



| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | $\begin{aligned} & \text { Page } 2 \text { of } 8 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:08:07 02/26/14 } \end{array}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |



| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | $\begin{aligned} & \text { Page } \\ & \\ & \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{array}{\|l\|l\|} \hline \text { Date } \\ \text { 15:08:07 02/26/14 } \end{array}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment <br> 0 | Placement <br> ft |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight <br> $l b$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HPA-65R-BUU-H8-K w/ Mount Pipe | B | From Face |  | -15.0000 | 121.00 | 2" Ice | 16.14 | 9.85 | 411.60 |
|  |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | B | From Face |  | 90.0000 | 121.00 | $2^{\prime \prime}$ Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | C | From Face |  | 15.0000 | 121.00 | 2 " Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | D | From Face |  | 45.0000 | 121.00 | $2{ }^{\prime \prime}$ Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | B | From Face |  | -15.0000 | 121.00 | 2 " Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | C | From Leg |  | -30.0000 | 121.00 | 2 " Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | D | From Face |  | 45.0000 | 121.00 | $2^{\prime \prime}$ Ice | 16.14 | 9.85 | 411.60 |
| HPA-65R-BUU-H8-K w/ Mount Pipe |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 13.30 | 7.52 | 70.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 13.99 | 8.09 | 143.77 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 14.70 | 8.67 | 225.17 |
|  | A | From Face |  | 75.0000 | 121.00 | $2^{\prime \prime}$ Ice | 16.14 | 9.85 | 411.60 |
| Twin TMACCI-BP |  |  |  |  |  | 4" Ice | 19.13 | 12.29 | 884.49 |
|  |  |  | 3.46 |  |  | No Ice | 0.64 | 0.35 | 14.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 0.76 | 0.45 | 18.54 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.89 | 0.56 | 24.60 |
| Twin TMACCI-BP | A | From Face |  | -45.0000 | 121.00 | $2^{\prime \prime}$ Ice | 1.16 | 0.81 | 42.06 |
|  |  |  |  |  |  | 4" Ice | 1.83 | 1.40 | 103.83 |
|  |  |  | 3.46 |  |  | No Ice | 0.64 | 0.35 | 14.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 0.76 | 0.45 | 18.54 |
|  |  |  | 3.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.89 | 0.56 | 24.60 |
| Twin TMACCI-BP | B | From Face |  | -15.0000 | 121.00 | 2 " Ice | 1.16 | 0.81 | 42.06 |
|  |  |  |  |  |  | 4" Ice | 1.83 | 1.40 | 103.83 |
|  |  |  | 3.46 |  |  | No Ice | 0.64 | 0.35 | 14.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 0.76 | 0.45 | 18.54 |
|  |  |  | 3.00 |  |  | $1^{\prime \prime}$ Ice | 0.89 | 0.56 | 24.60 |
| Twin TMACCI-BP | B | From Face |  | 90.0000 | 121.00 | 2 " Ice | 1.16 | 0.81 | 42.06 |
|  |  |  |  |  |  | 4" Ice | 1.83 | 1.40 | 103.83 |
|  |  |  | 3.46 |  |  | No Ice | 0.64 | 0.35 | 14.00 |
|  |  |  | 2.00 |  |  | 1/2" Ice | 0.76 | 0.45 | 18.54 |
|  |  |  | 3.00 |  |  | 1" Ice | 0.89 | 0.56 | 24.60 |
|  |  |  |  |  |  | 2" Ice | 1.16 | 0.81 | 42.06 |
|  |  |  |  |  |  | 4" Ice | 1.83 | 1.40 | 103.83 |


| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | $\text { Page } 4 \text { of } 8$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{aligned} & \text { Date } \\ & \text { 15:08:07 02/26/14 } \end{aligned}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight <br>
\hline \multirow[t]{5}{*}{Twin TMACCI-BP} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{15.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 0.64 \& 0.35 \& 14.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 0.76 \& 0.45 \& 18.54 <br>
\hline \& \& \& \multirow[t]{3}{*}{3.00} \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.89 \& 0.56 \& 24.60 <br>
\hline \& \& \& \& \& \& 2" Ice \& 1.16 \& 0.81 \& 42.06 <br>
\hline \& \& \& \& \& \& 4" Ice \& 1.83 \& 1.40 \& 103.83 <br>
\hline \multirow[t]{5}{*}{Twin TMACCI-BP} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{45.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 0.64 \& 0.35 \& 14.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 0.76 \& 0.45 \& 18.54 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.89 \& 0.56 \& 24.60 <br>
\hline \& \& \& \& \& \& 2" Ice \& 1.16 \& 0.81 \& 42.06 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 1.83 \& 1.40 \& 103.83 <br>
\hline \multirow[t]{5}{*}{RRUS 12} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{75.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 2.89 \& 1.00 \& 58.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 3.11 \& 1.15 \& 75.97 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.35 \& 1.31 \& 96.77 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 3.85 \& 1.66 \& 147.66 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 4.95 \& 2.46 \& 292.03 <br>
\hline \multirow[t]{5}{*}{RRUS 12} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{-45.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 2.89 \& 1.00 \& 58.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 3.11 \& 1.15 \& 75.97 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.35 \& 1.31 \& 96.77 <br>
\hline \& \& \& \& \& \& 2" Ice \& 3.85 \& 1.66 \& 147.66 <br>
\hline \& \& \& \& \& \& 4" Ice \& 4.95 \& 2.46 \& 292.03 <br>
\hline \multirow[t]{5}{*}{RRUS-11} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{75.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 3.25 \& 1.37 \& 47.62 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 3.49 \& 1.55 \& 68.42 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.74 \& 1.74 \& 92.25 <br>
\hline \& \& \& \& \& \& 2" Ice \& 4.27 \& 2.14 \& 149.81 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 5.43 \& 3.04 \& 309.89 <br>
\hline \multirow[t]{5}{*}{RRUS-11} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{-45.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 3.25 \& 1.37 \& 47.62 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 3.49 \& 1.55 \& 68.42 <br>
\hline \& \& \& 3.00 \& \& \& 1" Ice \& 3.74 \& 1.74 \& 92.25 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 4.27 \& 2.14 \& 149.81 <br>
\hline \& \& \& \& \& \& 4" Ice \& 5.43 \& 3.04 \& 309.89 <br>
\hline \multirow[t]{5}{*}{RRUS A2 MODULE} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{75.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 1.87 \& 0.42 \& 21.16 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 0.53 \& 31.49 <br>
\hline \& \& \& 3.00 \& \& \& 1 " Ice \& 2.24 \& 0.65 \& 44.03 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 2.66 \& 0.91 \& 76.55 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 3.58 \& 1.54 \& 176.75 <br>
\hline \multirow[t]{5}{*}{RRUS A2 MODULE} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{-45.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 1.87 \& 0.42 \& 21.16 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 0.53 \& 31.49 <br>
\hline \& \& \& 3.00 \& \& \& 1 " Ice \& 2.24 \& 0.65 \& 44.03 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 2.66 \& 0.91 \& 76.55 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.58 \& 1.54 \& 176.75 <br>
\hline \multirow[t]{5}{*}{RRUS-32} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{-75.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 3.87 \& 2.76 \& 77.00 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 4.15 \& 3.02 \& 104.93 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 4.44 \& 3.29 \& 136.47 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 5.06 \& 3.85 \& 211.15 <br>
\hline \& \& \& \& \& \& 4" Ice \& 6.38 \& 5.08 \& 412.40 <br>
\hline \multirow[t]{5}{*}{RRUS E2} \& \multirow[t]{5}{*}{D} \& \multirow[t]{5}{*}{From Face} \& 3.46 \& \multirow[t]{5}{*}{-75.0000} \& \multirow[t]{5}{*}{121.00} \& No Ice \& 1.87 \& 0.42 \& 21.16 <br>
\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 0.53 \& 31.49 <br>
\hline \& \& \& 3.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.24 \& 0.65 \& 44.03 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.66 \& 0.91 \& 76.55 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.58 \& 1.54 \& 176.75 <br>
\hline
\end{tabular}

| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | Page 5 of 8 |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:08:07 02/26/14 } \end{array}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |

## Critical Deflections and Radius of Curvature - Service Wind



| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | $\begin{aligned} & \text { Page } \quad 6 \text { of } 8 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{aligned} & \text { Date } \\ & \text { 15:08:07 02/26/14 } \end{aligned}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |


| Section No. | Elevation <br> $f t$ | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Махітит <br> Load per Bolt $l b$ | Allowable Load lb | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T8 | 50.4167 | Leg | A325N | 0.7500 | 28 | 7750.45 | 18555.00 | 0.418 | 1.333 | Shear Bolt DS |
|  |  | Diagonal | A325N | 0.6250 | 2 | 4582.07 | 6442.72 | 0.711 | 1.333 | Bolt Shear |
|  |  | Secondary <br> Horizontal | A325N | 0.6250 | 1 | 1628.23 | 5103.52 | 0.319 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 2667.78 | 6442.72 | 0.414 | 1.333 | Bolt Shear |
| T9 | 40.4167 | Leg | A325N | 0.7500 | 32 | 7742.16 | 18555.00 | 0.417 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.6250 | 2 | 4771.97 | 6442.72 |  | 1.333 | Bolt Shear |
|  | 30.4167 | Secondary Horizontal | A325N | 0.6250 | 1 | 1858.82 | 5103.52 | 0.364 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 2879.26 | 6442.72 | 0.447 | 1.333 | Bolt Shear |
| T10 |  | Leg | A325N | 0.7500 | 36 | 7742.99 | 18555.00 |  | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.6250 | 2 | 4884.09 | 6442.72 | 0.758 | 1.333 | Bolt Shear |
|  | 20.4167 | Secondary Horizontal | A325N | 0.6250 | 1 | 2091.43 | 5103.52 | $\begin{aligned} & 0.410 \\ & 0.469 \end{aligned}$ | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 3023.27 | 6442.72 |  | 1.333 | Bolt Shear |
| T11 |  | Leg | A325N | 0.7500 | 40 | 7754.80 | 18555.00 | 0.418 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.6250 | 2 | 5045.55 | 6442.72 | 0.783 | 1.333 | Bolt Shear |
|  | 10.2083 | Secondary <br> Horizontal | A325N | 0.6250 | 1 | 2327.28 | 5103.52 | 0.456 | 1.333 | Member Block Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 3218.53 | 8224.22 | 0.391 | 1.333 | Member Block Shear |
| T12 |  | Leg | A325N | 0.7500 | 40 | 8458.52 | 18555.00 | 0.456 | 1.333 | Bolt DS |
|  |  | Diagonal | A325N | 0.6250 | 2 | 5869.67 | 6442.72 | 0.911 | 1.333 | Bolt Shear |
|  |  | Secondary Horizontal | A325N | 0.6250 | 1 | 2538.51 | 6442.72 | 0.394 | 1.333 | Bolt Shear |
|  |  | Top Girt | A325N | 0.6250 | 2 | 3877.73 | 8224.22 | 0.472 | 1.333 | Member Block Shear |
| T12 | 0.0000 | Anchor Rods | A36 | 1.5000 | 4 | 41007.10 | 33823.20 | 1.212 | 1.333 | Bolt Tension |

## Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ l b \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 121-110 | Leg | L5x5x1/2 | 1 | -7970.86 | 135887.35 | 5.9 | Pass |
| T2 | 110-100.417 | Leg | L5x5x1/2 | 21 | -19565.30 | 145458.29 | 13.5 | Pass |
| T3 | $\begin{gathered} 100.417- \\ 90.4167 \end{gathered}$ | Leg | L5x5x1/2 | 41 | -33470.70 | 142714.97 | 23.5 | Pass |
| T4 | $\begin{gathered} 90.4167- \\ 80.4167 \end{gathered}$ | Leg | L5x5x1/2 | 61 | -46719.80 | 139774.38 | 33.4 | Pass |
| T5 | $\begin{gathered} 80.4167- \\ 70.4167 \end{gathered}$ | Leg | L5x5x1/2 | 81 | -60459.60 | 140052.97 | 43.2 | Pass |
| T6 | $\begin{gathered} 70.4167- \\ 60.4167 \end{gathered}$ | Leg | L6x6x3/4 | 101 | -78424.40 | 268254.24 | 29.2 | Pass |
| T7 | $\begin{gathered} 60.4167- \\ 50.4167 \end{gathered}$ | Leg | L6x6x3/4 | 121 | -93071.20 | 268543.50 | 34.7 | Pass |
| T8 | $\begin{gathered} 50.4167- \\ 40.4167 \end{gathered}$ | Leg | L6x6x3/4 | 141 | -108506.00 | 268684.80 | 40.4 | Pass |
| T9 | $\begin{gathered} 40.4167- \\ 30.4167 \end{gathered}$ | Leg | L6x6x3/4 | 161 | -123875.00 | 268914.08 | 46.1 | Pass |
| T10 | 30.4167 - | Leg | L6x6x3/4 | 181 | -139374.00 | 269018.05 | 51.8 | Pass |


| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job 65054 - LEBANON |  | $\begin{aligned} & \text { Page } \\ & \\ & \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | Date 15:08:07 02/26/14 |
|  | Client | Smartlink, LLC | Designed by jboegel |


| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ l b \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T11 | $\begin{gathered} 20.4167 \\ 20.4167- \\ 10.2083 \end{gathered}$ | Leg | L6x6x3/4 | 201 | -155096.00 | 267223.83 | 58.0 | Pass |
| T12 | 10.2083-0 | Leg | L6x6x3/4 | 221 | -169170.00 | 297119.02 | 56.9 | Pass |
| T1 | 121-110 | Diagonal | L2 1/2x2 1/2x3/16 | 16 | -5092.75 | 8764.61 | 58.1 | Pass |
| T2 | 110-100.417 | Diagonal | L2x3x1/4 | 36 | -5862.19 | 10918.98 | 53.7 | Pass |
| T3 | $\begin{gathered} 100.417- \\ 90.4167 \end{gathered}$ | Diagonal | L3x3x3/16 | 56 | -7778.68 | 16590.12 | 46.9 | Pass |
| T4 | $\begin{gathered} 90.4167- \\ 80.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 76 | -8809.69 | 20133.76 | 43.8 | Pass |
| T5 | $\begin{gathered} 80.4167- \\ 70.4167 \end{gathered}$ | Diagonal | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 96 | -9777.98 | 20457.82 | 47.8 | Pass |
| T6 | $\begin{gathered} 70.4167- \\ 60.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 116 | -8210.35 | 18648.67 | 44.0 | Pass |
| T7 | $\begin{gathered} 60.4167- \\ 50.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 133 | -8929.51 | 17640.52 | 50.6 | Pass |
| T8 | $\begin{gathered} 50.4167- \\ 40.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 153 | -9164.14 | 16622.11 | 55.1 | Pass |
| T9 | $\begin{gathered} 40.4167- \\ 30.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 173 | -9543.95 | 15699.14 | 60.8 | Pass |
| T10 | $\begin{gathered} 30.4167- \\ 20.4167 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 193 | -9768.18 | 14796.03 | 66.0 | Pass |
| T11 | $\begin{gathered} 20.4167- \\ 10.2083 \end{gathered}$ | Diagonal | L3x $3 \times 1 / 4$ | 213 | -10091.10 | 13701.11 | 73.7 | Pass |
| T12 | 10.2083-0 | Diagonal | L3x $3 \times 1 / 4$ | 233 | -11739.30 | 12936.03 | 90.7 | Pass |
| T1 | 121-110 | Secondary Horizontal | L2x $2 \times 3 / 16$ | 17 | -119.56 | 16381.77 | 0.7 | Pass |
| T2 | 110-100.417 | Secondary Horizontal | L2x $2 \times 3 / 16$ | 37 | -293.48 | 16381.77 | 1.8 | Pass |
| T3 | $\begin{gathered} 100.417- \\ 90.4167 \end{gathered}$ | Secondary Horizontal | L2x $2 \times 3 / 16$ | 57 | -502.06 | 16381.77 | 3.1 | Pass |
| T4 | $\begin{gathered} 90.4167- \\ 80.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 77 | -701.07 | 15539.58 | 4.5 | Pass |
| T5 | $\begin{gathered} 80.4167- \\ 70.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 97 | -907.24 | 13708.97 | 6.6 | Pass |
| T6 | $\begin{gathered} 70.4167- \\ 60.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 117 | -1176.83 | 12073.41 | 9.7 | Pass |
| T7 | $\begin{gathered} 60.4167- \\ 50.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 137 | -1396.59 | 10389.68 | 13.4 | Pass |
| T8 | $\begin{gathered} 50.4167- \\ 40.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 157 | -1628.23 | 9036.77 | 18.0 | Pass |
| T9 | $\begin{gathered} 40.4167- \\ 30.4167 \end{gathered}$ | Secondary Horizontal | L2x2x3/16 | 177 | -1858.82 | 7930.87 | 23.4 | Pass |
| T10 | $\begin{gathered} 30.4167- \\ 20.4167 \end{gathered}$ | Secondary Horizontal | L2x $2 \times 3 / 16$ | 197 | -2091.43 | 7017.19 | 29.8 | Pass |
| T11 | $\begin{gathered} 20.4167- \\ 10.2083 \end{gathered}$ | Secondary Horizontal | L2x $2 \times 3 / 16$ | 217 | -2327.28 | 6252.13 | 37.2 | Pass |
| T12 | 10.2083-0 | Secondary Horizontal | L2x $2 \times 1 / 4$ | 237 | -2538.51 | 7243.27 | 35.0 | Pass |
| T1 | 121-110 | Top Girt | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 6 | -238.04 | 21353.06 | 1.1 | Pass |
| T2 | 110-100.417 | Top Girt | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 26 | -1042.81 | 21353.06 | 4.9 | Pass |
| T3 | $\begin{gathered} 100.417- \\ 90.4167 \end{gathered}$ | Top Girt | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 45 | -2258.27 | 21353.06 | 10.6 | Pass |
| T4 | $\begin{gathered} 90.4167- \\ 80.4167 \end{gathered}$ | Top Girt | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 65 | -3294.71 | 21353.06 | 15.4 | Pass |
| T5 | $\begin{gathered} 80.4167- \\ 70.4167 \end{gathered}$ | Top Girt | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ | 85 | -5650.34 | 18397.27 | 30.7 | Pass |
| T6 | $\begin{gathered} 70.4167- \\ 60.4167 \end{gathered}$ | Top Girt | 2L2x $2 \times 3 / 16$ | 105 | -5048.09 | 15609.56 | 32.3 | Pass |
| T7 | $\begin{gathered} 60.4167- \\ 50.4167 \end{gathered}$ | Top Girt | 2L2 1/2x2 1/2x3/16 | 125 | -4402.77 | 26548.43 | 16.6 | Pass |
| T8 | $\begin{gathered} 50.4167- \\ 40.4167 \end{gathered}$ | Top Girt | L3x $3 \times 1 / 4$ | 145 | -4829.58 | 10982.68 | 44.0 | Pass |
| T9 | 40.4167 - | Top Girt | L3x $3 \times 1 / 4$ | 165 | -5200.69 | 9587.98 | 54.2 | Pass |


| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572.2100 <br> FAX: 330.572.2101 | Job | 65054 - LEBANON | $\begin{array}{ll} \text { Page } \\ & 8 \text { of } 8 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2014723.21.65054.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:08:07 02/26/14 } \end{array}$ |
|  | Client | Smartlink, LLC | Designed by jboegel |


| Section No. | Elevation ft | Component Type | Size | Critical <br> Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ \quad l b \end{gathered}$ | \% Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T10 | $\begin{gathered} 30.4167 \\ 30.4167 \\ 20.4167 \end{gathered}$ | Top Girt | L3x3x1/4 | 185 | -5449.30 | 8461.60 | 64.4 | Pass |
| T11 | $\begin{gathered} 20.4167- \\ 10.2083 \end{gathered}$ | Top Girt | 2L2 $2 \times 3 / 16$ | 205 | -5793.08 | 8097.88 | 71.5 | Pass |
| T12 | 10.2083-0 | Top Girt | 2L2 $2 \times 3 / 16$ | 225 | -6950.76 | 7247.31 | 95.9 | Pass |
|  |  |  |  |  |  | Summary | ELC: | Existing + Proposed |
|  |  |  |  |  |  | Leg (T11) | 58.0 | Pass |
|  |  |  |  |  |  | Diagonal (T12) | 90.7 | Pass |
|  |  |  |  |  |  | Secondary Horizontal (T11) | 37.2 | Pass |
|  |  |  |  |  |  | Top Girt (T12) | 95.9 | Pass |
|  |  |  |  |  |  | Bolt Checks | 91.0 | Pass |
|  |  |  |  |  |  | Rating = | 95.9 | Pass |

## APPENDIX C

Tower Elevation Drawing


121.0 ft咢
$\begin{array}{r} \\ \\ \\ \hline 6.25 \\ \hline\end{array}$

DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :--- | :--- | :--- | :--- |
| (2) Sabre 6' Sidearm C10-151-006 | 121 | HPA-65R-BUU-H8-K w/ Mount Pipe | 121 |
| (2) Sabre 6' Sidearm C10-151-006 | 121 | HPA-65R-BUU-H8-K w/ Mount Pipe | 121 |
| (2) Sabre 6' Sidearm C10-151-006 | 121 | HPA-65R-BUU-H8-K w/ Mount Pipe | 121 |
| (2) Sabre 6' Sidearm C10-151-006 | 121 | HPA-65R-BUU-H8-K w/ Mount Pipe | 121 |
| RRUS-11 | 121 | Twin TMACCI-BP | 121 |
| RRUS-11 | 121 | Twin TMACCI-BP | 121 |
| RRUS-11 | Twin TMACCI-BP | 121 |  |
| DC6-48-60-18-8F Surge Suppression <br> Unit | 121 | Twin TMACCI-BP | 121 |
| Andrew Double Pipe Mount <br> MC-DA14-B | 121 | Twin TMACCI-BP | 121 |
| Andrew Double Pipe Mount <br> MC-DA14-B | Twin TMACCI-BP | 121 |  |
| MTS 60" Standoff | 121 | RRUS 12 | 121 |
| HPA-65R-BUU-H8-K w/ Mount Pipe | 121 | RRUS 12 | 121 |
| HPA-65R-BUU-H8-K w/ Mount Pipe | 121 | RRUS-11 | 121 |
| HPA-65R-BUU-H8-K w/ Mount Pipe | 121 | RRUS-11 | 121 |
| HPA-65R-BUU-H8-K w/ Mount Pipe | 121 | RRUS A2 MODULE | 121 |
| HPA-65R-BUU-H8-K w/ Mount Pipe | 121 | RRUS A2 MODULE | 121 |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :---: | :--- | :--- | :--- | :--- | :--- |
| A572-50 | 50 ksi | 65 ksi | A36 | 36 ksi | 58 ksi |

## TOWER DESIGN NOTES

1. Tower is located in New London County, Connecticut.
2. Tower designed for a 100 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: $95.9 \%$

MAX. CORNER REACTIONS AT BASE:

## DOWN: 184130 lb

SHEAR: 18290 lb
UPLIFT: -178553 lb
SHEAR: 18183 lb


TORQUE 2286 lb -ft 38 mph WIND - 0.7500 in ICE


TORQUE 21275 lb -ft REACTIONS - 100 mph WIND


520 South Main Street, Suite 2531
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Phone: 330.572.2100
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65054 - LEBANON
Project: 2014723.21.65054.01

| Client: Smartlink, LLC | Drawn by: jboegel | App'd: |
| :---: | :---: | :---: |
| Code: TIA/EIA-222-F | Date: 02/26/14 | Scale: NTS |
| Path: ${ }_{\text {C:IUsersijboegelidesktopiUpdated Since on Desktopl\|65054.011TNXAAnchor Rods.eri\| }}$ |  | Dwg No. E |

Feed Line Distribution Chart
0' - 121'
$\qquad$ _ound Flat $\qquad$ App In Face $\qquad$ App Out Face $\qquad$ Truss Leg


| GPD GROUP <br> Consulting Engineer | GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, Ohio 44311 <br> Phone: 330.572 .2100 <br> FAX: 330.572.2101 | $\text { Pob: } 65054 \text { - LEBANON }$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  |  | Drawn by j jboegel | App |
|  |  | Code: TIA/EIA-222-F | Date: 02/26/14 | NTS |
|  |  |  |  | No. E |

$\qquad$ Flat $\qquad$ App In Face


## APPENDIX D

## Foundation Analysis

Mat Foundation Analysis
65054 - LEBANON
2014723.21.65054.01

| Bearing Summary |  | Load Case |  |
| :---: | :---: | :--- | :---: |
| Qxmax | 2.97 | ksf | $1 \mathrm{D}+1 \mathrm{~W}$ |
| Qymax | 2.97 | ksf | $1 \mathrm{D}+1 \mathrm{~W}$ |
| Qmax @ 45 $^{\circ}$ | 4.01 | ksf | $1 \mathrm{D}+1 \mathrm{~W}$ |
| $\mathrm{Q}_{\text {(all) Gross }}$ | 25.33 | ksf |  |
|  |  |  |  |
| Controlling Capacity | $\mathbf{1 5 . 8 \%}$ | Pass |  |


| General Info |  |
| :---: | :---: |
| Code | TIA/EIA-222-F (ASD) |
| Bearing On | Rock |
| Foundation Type | SS Pad |
| Pier Type | Square |
| Reinforcing Known | No |
| Max Capacity | 1.05 |


| Tower Reactions |  |
| :---: | :---: |
| Moment, M | $2885.129 \mathrm{k}-\mathrm{ft}$ |
| Axial, P | 24.399 k |
| Shear, V | 38.375 k |


| Overturning Summary (Required FS=1.5) |  | Load Case |  |
| :---: | :---: | :---: | :---: |
| FS(ot)x | 1.57 | $<1.5$ | $1 \mathrm{D}+1 \mathrm{~W}$ |
| FS(ot)y | 1.57 | $\geq 1.5$ | $1 \mathrm{D}+1 \mathrm{~W}$ |
| Controlling Capacity | $\mathbf{9 5 . 6 \%}$ | Pass |  |


| Pad \& Pier Geometry |  |  |
| :---: | :---: | :---: |
| Pier Width, $\varnothing$ | 3 | ft |
| Pad Length, L | 23 | ft |
| Pad Width, W | 23 | ft |
| Pad Thickness, t | 3 | ft |
| Depth, D | 5.5 | ft |
| Height Above Grade, HG | 1 | ft |



| Pad \& Pier Reinforcing |  |  |
| :---: | :---: | :--- |
| Rebar Fy | 60 | ksi |
| Concrete Fc' | 3 | ksi |
| Clear Cover | 3 | in |
| Reinforced Top \& Bottom? | Yes |  |
| Pad Reinforcing Size | $\# 8$ |  |
| Pad Quantity Per Layer | 33 |  |
| Pier Rebar Size | $\# 8$ |  |
| Pier Quantity of Rebar | 16 |  |


| Soil Properties |  |
| :---: | :---: |
| Soil Type | Cohesive |
| Soil Unit Weight | 120 pcf |
| Cohesion, Cu | 15 ksf |
| Bearing Type | Net |
| Ultimate Bearing | 50 ksf |
| Water Table Depth | 99 ft |
| Frost Depth | 5 ft |



GPD Mat Foundation Analysis - V1.02



NOTE: EOR OF RECORD MUST PROVIDE MEMO w/ LOE WHEN CURRENT ANALYSIS DEVIATES FROM PRIOR ANALYSIS OF RECORD FOR THIS SITE !!! (TO EXPLAIN CHANGES IN ENGINEERING IN CURRENT REPORT -. EXAMPLES: TOPO/EXPOSURE/K-VALUECLLASSIFICATION)

