August 7, 2018

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification for Sprint DO Macro: 806387 Sprint Site ID: CT33XC547 <br> 14 Route 80, Killingworth, CT 06419 <br> Latitude: $41^{\circ}$ 21' 26.43"/ Longitude: $-72^{\circ} 31$ ' $11.83^{\prime \prime}$

Dear Ms. Bachman:

Sprint currently maintains six (6) antennas at the 144 -foot level of the existing 160 -foot selfsupport tower located at 14 Route 80, Killingworth, CT. The tower is owned by Crown Castle. The property is owned by 14 Route 80 LLC. Sprint now intends to replace six (6) antennas with six (6) new antennas. These antennas would be installed at the 144 -foot level of the tower. Sprint also intends to install twelve (12) RRH's, add four (4) Hybrid cables and remove six (6) existing coaxial cables

On August $7^{\text {th }}$, an email was sent to the Land Use Department inquiring on the original zoning or planning approval of the tower in the town of Killingworth, CT.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j73 , for construction that constitutes an exempt modification pursuant to R.C.S.A. § $16-50 \mathrm{j}-72(\mathrm{~b})(2)$. In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to the First Selectwomen, Ms. Catherine Lino, Zoning Enforcement Officer, Ms. Cathie Jefferson, the land owner, 14 Route 80 LLC. Crown Castle is the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § $16-$ $50 \mathrm{j}-72(\mathrm{~b})(2)$.please send approval/rejection letter to Attn: Jeffrey Barbadora.


Jeffrey Barbadora
Real Estate Specialist
12 Gill Street, Suite 5800, Woburn, MA 01801
781-729-0053
Jeff.Barbadora@crowncastle.com
Attachments:
Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes
Tab 2: Exhibit-2: Structural Modification Report
Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)
cc: Ms. Catherine Lino
Town of Killingworth-First Selectwomen
323 Route 81
Killingworth, CT 06419
(860) 663-1765

Ms. Cathie Jefferson
Zoning Enforcement Officer
323 Route 81
Killingworth, CT 06419
(860) 663-1765 ext. 505

14 Route 80 LLC
93A Glenwood Road
Clinton, CT 06413

## Barbadora, Jeff

| From: | Barbadora, Jeff |
| :--- | :--- |
| Sent: | Tuesday, August 7, 2018 3:09 PM |
| To: | 'cjefferson@townofkillingworth.com' |
| Subject: | 14 Route 80 - Cell Tower |

Good Afternoon Ms. Jefferson,

I have an inquiry regarding original zoning documents for a tower and I am hoping you can provide more information.
We are applying for CSC Zoning Approval for tower modifications and new requirements ask that we procure original zoning documents from the jurisdiction, if possible. However, if these documents are not available, please let me know.

The tower is located at 14 Route 80 and according to lease documents this may have been approved around 1999-The property is owned by 14 Route 80 LLC, Map/Block 34-36A.

If you have any questions, please don't hesitate to call or e-mail me.
Thank you for your time,

Thanks,

## Jeffrey Barbadora

781-970-0053
12 Gill Street, Suite 5800, Woburn, MA 01801
CrownCastle.com

The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at $70 \%$ of the estimated market value of real property at the time of the last revaluation which was 2016.


Information on the Property Records for the Municipality of Killingworth was last updated on 8/4/2018.

## Parcel Information

| Location: | 14 ROUTE 80 | Property Use: | Industrial | Primary Use: | Light Industrial |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Unique ID: | 00218500 | Map Block | 34-36A | Acres: | 2.00 |
|  |  | Lot: |  |  |  |
| 490 Acres: | 0.00 | Zone: | ID | Volume / | 0225/0110 |
|  |  |  |  | Page: |  |
| Developers | DEV MP 312 | Census: | 6401 |  |  |
| Map / Lot: |  |  |  |  |  |

## Value Information

|  | Appraised Value | Assessed Value |
| :--- | :---: | :---: |
| Land | 200,000 |  |
| Buildings | 252,719 | 140,000 |
| $\ldots$ | $\ldots$ | 176,900 |
| Detached Outbuildings | 251,459 | 176,020 |
| Total | 704,178 |  |

## Owner's Information

## Owner's Data

14 ROUTE 80 LLC<br>93A GLENWOOD RD<br>CLINTON CT 06413

## Building 1



| Category: | Industrial | Use: | Light Industrial | GLA: | 7,508 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Stories: | 1.00 | Construction: | Average | Year Built: | 1969 |
| Heating: | Susp. Space | Fuel: | Oil | Cooling | 0\% |
|  |  |  |  | Percent: |  |
| Siding: | Metal | Roof Material: | Arch Shingles | Beds/Units: | 0 |

## Special Features

## Attached Components

## Detached Outbuildings

| Type: | Year Built: | Length: | Width: | Area: |
| :---: | :---: | :---: | :---: | :---: |
| Fencing | 1999 | 9 | 234 | 2,106 |
| Concrete/Masonry Patio | 1999 |  |  | 432 |
| Concrete/Masonry Patio | 1999 | 8 | 20 | 160 |
| Cell Tower | 2000 |  |  | 1 |

## Owner History - Sales

| Owner Name | Volume | Page | Sale Date | Deed Type | Valid Sale | Sale Price |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 14 ROUTE 80 LLC | 0225 | 0110 | $06 / 14 / 2007$ | Quit Claim | No | $\$ 0$ |

## Building Permits

$\left.\begin{array}{|l|l|l|l|l|l|l|}\begin{array}{l}\text { Permit } \\ \text { Number }\end{array} & \text { Permit Type } & \begin{array}{l}\text { Date } \\ \text { Opened }\end{array} & \begin{array}{l}\text { Date } \\ \text { Closed }\end{array} & \begin{array}{l}\text { Permit } \\ \text { Status }\end{array} & \text { Reason } \\ \hline 12-410 & \text { Commercial } & 04 / 12 / 2013 & & \text { Closed } & \text { CELL TOWER MAINTENANCE }\end{array}\right]$.

| Permit <br> Number | Permit Type | Date <br> Opened | Date <br> Closed | Permit <br> Status | Reason |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $08-$ E018 |  | $04 / 13 / 2008$ |  | Closed | ELECTRICAL SERVICE PANEL INSTALLATION; ELECTRICAL <br> SERVICE PANEL INSTALLATION; |
| $99-099$ |  |  |  |  |  |

Information Published With Permission From The Assessor


## 14 Route 80

## 8/7/2018 2:59:35 PM

Scale: 1"=100'
Scale is approximate


The information depicted on this map is for planning purposes only. It is not adequate for legal boundary definition, regulatory interpretation, or parcel-level analyses.











 \& COMPANY

Date: June 15, 2018

Rebecca Klein<br>Crown Castle<br>3530 Toringdon Way, Suite 300<br>Charlotte, NC 28277<br>1-704-405-6525

Paul J. Ford and Company<br>250 East Broad st., Suite 600<br>Columbus, OH 43215<br>(614) 221-6679<br>jjacobs@pjfweb.com

## Subject: Structural Analysis Report

## Carrier Designation:

## Crown Castle Designation:

## Engineering Firm Designation:

Site Data:

Sprint PCS Co-Locate
Carrier Site Number: CT33XC547
Carrier Site Name:
Crown Castle BU Number: 806387
Crown Castle Site Name: HRT 088943629
Crown Castle JDE Job Number:
Crown Castle Work Order Number:
Crown Castle Order Number:
CT33XC547

505982
1589524
441482 Rev. 0

Paul J. Ford and Company Project Number: 37518-2158-002-8700
\#14 Route 80, KILLINGWORTH, Middlesex County, CT
Latitude $41^{\circ}$ 21' $26.43^{\prime \prime}$, Longitude -72 $^{\circ} 31^{\prime} 11.83^{\prime \prime}$
160 Foot - Self Support Tower

Dear Ms. Klein,
Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1204283, in accordance with order 441482, revision 0.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4.7: Modified Structure: Existing + Reserved + Proposed Equipment Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

Sufficient Capacity

This analysis has been performed In accordance with the 2016 Connecticut State Building Code based upon an ultimate 3 -second gust wind speed of 130 mph converted to a nominal 3 -second gust wind speed of 101 mph per section 1609.3 and Appendix N as required for use in the TIA-222-G Standard per Exception \#5 of Section 1609.1.1. Exposure Category B with a topographic category 1 and crest height of 0 feet, and Risk Category II were used in this analysis.

All modifications and equipment proposed in this report shall be installed in accordance with the drawings stated in Table 3, for the determined available structural capacity to be effective.

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have ansyufugtions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared

Project Manager
tnxTower Report - version 7.0.5.1

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## 1) INTRODUCTION

This tower is a 160 ft Self Support tower designed by ROHN The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

## 2). ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA-222-G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a 3 -second gust wind speed of 100.7 mph with no ice, 50 mph with 0.75 inch ice thickness and 60 mph under service loads, exposure category $B$ with topographic category 1 and crest height of 0 feet.

Table 1 - Proposed Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 144.0 | 144.0 | 3 | alcatel lucent | $\begin{gathered} \text { PCS 1900MHZ 4X45W- } \\ 65 \mathrm{MHZ} \end{gathered}$ | 13 | $\begin{gathered} 7 / 8 \\ 11 / 4 \end{gathered}$ |
|  |  | 6 | alcatel lucent | RRH2X50-800 |  |  |
|  |  | 3 | alcatel lucent | TD-RRH8X20-25 |  |  |
|  |  | 3 | commscope | NNVV-65B-R4 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVTM14-ALU-I20 w/ Mount Pipe |  |  |

Table 2 - Existing and Reserved Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | $\begin{array}{\|c\|} \text { Feed } \\ \text { Line } \\ \text { Size (in) } \end{array}$ | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 157.0 | 157.0 | 3 |  | B13 RRH 4X30 | 2 | $15 / 8$ | 2 |
|  |  | 3 |  | B5 4T4R RRH4X40 AIRSCALE |  |  |  |
|  |  | 3 |  | B66A RRH4X45 |  |  |  |
|  |  | 6 | antel | LPA-80080/6CF w/ Mount Pipe | 10 | $15 / 8$ | 1 |
|  |  | 6 | commscope | JAHH-65B-R3B w/ Mount Pipe |  |  | 2 |
|  |  | 2 | raycap | RC3DC-3315-PF-48 |  |  |  |
|  |  | 1 | tower mounts | Sector Mount [SM 508-3] |  |  | 1 |
| 144.0 | 144.0 | 6 | decibel | DB978H90T2E-M w/ Mount Pipe | 6 | $15 / 8$ | 3 |
|  |  | 1 | tower mounts | Sector Mount [SM 506-3] |  |  | 1 |
| 118.0 | 118.0 | 12 | decibel | $\underset{\text { DB844H90E-XY w/ Mount }}{\text { Pipe }}$ | - | - | 1 |
|  |  | 1 | tower mounts | Sector Mount [SM 404-3] |  |  |  |
| 109.0 | 115.0 | 1 | celwave | PD1110 |  |  | 1 |
|  | 109.0 | 1 | tower mounts | Side Arm Mount [SO 308- | 1 | $11 / 4$ | 1 |

tnxTower Report - version 7.0.5.1

| Mounting Level ( ft ) | Center Line Elevation <br> (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1] |  |  |  |
| 90.0 | 90.0 | 6 | ericsson | RRUS-11 | $\begin{gathered} 12 \\ 1 \\ 2 \end{gathered}$ | $\begin{gathered} 7 / 8 \\ 3 / 8 \\ 7 / 16 \end{gathered}$ | 1 |
|  |  | 2 | kmw communications | $\begin{gathered} \text { AM-X-CD-16-65-00T-RET } \\ \text { w/ Mount Pipe } \end{gathered}$ |  |  |  |
|  |  | 6 | powerwave technologies | 7770.00 w/ Mount Pipe |  |  |  |
|  |  | 6 | powerwave technologies | LGP21401 |  |  |  |
|  |  | 6 | powerwave technologies | LGP21901 |  |  |  |
|  |  | 1 | powerwave technologies | $\underset{\text { Pipe }}{\text { P45-16-XLH-RR w/ Mount }}$ |  |  |  |
|  |  | 1 | raycap | DC6-48-60-18-8F |  |  |  |
|  |  | 1 | tower mounts | Pipe Mount [PM 601-3] |  |  |  |
|  |  | 1 | tower mounts | Sector Mount [SM 802-3] |  |  |  |
| 50.0 | 50.0 | 1 | lucent | KS24019-L112A | 1 | 1/2 | 1 |
|  |  | 1 | tower mounts | Side Arm Mount [SO 306- |  |  |  |

Notes:

1) Existing Equipment
2) Reserved Equipment
3) Equipment To Be Removed

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | JGI Eastern 05204G March 25, <br> 2005 | 1237256 | CCISITES |
| 4-TOWER FOUNDATION <br> DRAWINGS/DESIGN/SPECS | Rohn/ HEB Civil Engineers | 821498 | CCISITES |
| Tower manufacturer drawing | PJF 41706-0238 Dec 18, 2006 <br> As built Drawing Phase 1 | 2281721 | CCISITES |
| Partial PMI | PJF 41706-0238 Dec 18, 2006 <br> As built Drawing Phase 1 | 1296500 | CCISITES |
| PMI | PJF 37518-0397 <br> Dated June 22, 2009 | 2340021 | CCISITES |
| Reinforcement Drawing | PJF <br> 37517-3262-003-8800 <br> $12-4-2017$ | 7235023 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.
Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically, and must be replaced if damaged or cracked. Refer to crown document PRC-10012, Base Plate Grout Inspection \& Classification.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)


| Section No. | Elevation (ft) | Component Type | Size | Critical Element | P (K) | $\underset{(\mathrm{K})}{\mathrm{SF}^{*} \mathrm{P} \text { allow }}$ | $\left\lvert\, \begin{gathered} \text { \% } \\ \text { Capacity } \end{gathered}\right.$ | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 47.8 (b) |  |
| T9 | 80-60 | Leg | ROHN 4 EH (GR) | 122 | -134.95 | 192.91 | 70.0 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 3 / 16$ (1/4) | 124 | -6.14 | 38.73 | $\begin{gathered} 15.9 \\ 49.3(\mathrm{~b}) \end{gathered}$ | Pass |
| T10 | 60-40 | Leg | Rohn $5.563^{\prime \prime} \times 0.375^{\prime \prime}(5$ $E H)(G R)$ | 143 | -161.06 | 246.97 | 65.2 | Pass |
|  |  | Diagonal | 2L $3 \times 3 \times 3 / 16$ (1/4) | 145 | -7.25 | 28.70 | $\begin{array}{c\|} 25.3 \\ 47.7 \text { (b) } \\ \hline \end{array}$ | Pass |
| T11 | 40-20 | Leg | $\begin{gathered} \text { Rohn } 5.563^{\prime \prime} \times 0.375^{\prime \prime}(5 \\ E H)(G R) \\ \hline \end{gathered}$ | 158 | -188.02 | 246.94 | 76.1 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} \times 3 \times 1 / 4$ (1/4) | 160 | -7.31 | 35.24 | $\begin{gathered} 20.7 \\ 48.3(\mathrm{~b}) \end{gathered}$ | Pass |
| T12 | 20-0 | Leg | $\begin{gathered} \text { Rohn } 6.6255^{\prime \prime} \times 0.432^{\prime \prime}(6 \\ E H)(G R) \end{gathered}$ | 173 | -214.46 | 381.11 | $\begin{gathered} 56.3 \\ 56.5(\mathrm{~b}) \end{gathered}$ | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3.5 \times 3.5 \times 1 / 4(1 / 4)$ | 175 | -8.11 | 50.21 | $\begin{array}{\|c\|} \hline 16.2 \\ 52.7(\mathrm{~b}) \\ \hline \end{array}$ | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T11) | 76.1 | Pass |
|  |  |  |  |  |  | Diagonal (T4) | 76.5 | Pass |
|  |  |  |  |  |  | Top Girt (T1) | 12.7 | Pass |
|  |  |  |  |  |  | Bolt Checks | 76.5 | Pass |
|  |  |  |  |  |  | Rating = | 76.5 | Pass |

Table 5 - Tower Component Stresses vs. Capacity - LC7

| Notes | Component | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 66.9 | Pass |
| 1 | Base Foundation | 31.3 | Pass |
| 1 | Base Foundation <br> Soil Interaction | 68.1 | Pass |


| Structure Rating (max from all components) $=$ | $76.5 \%$ |
| :---: | :--- |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

Please see cci doc 7235023

## APPENDIX A

## TNXTOWER OUTPUT

## Tower Input Data

The main tower is a $3 x$ free standing tower with an overall height of 160.00 ft above the ground line. The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 6.52 ft at the top and 20.86 ft at the base.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:

1) Tower is located in Middlesex County, Connecticut.
2) ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
3) Basic wind speed of 101 mph .
4) Structure Class II.
5) Exposure Category B.
6) Topographic Category 1.
7) Crest Height 0.00 ft .
8) Nominal ice thickness of 0.7500 in.
9) Ice thickness is considered to increase with height.
10) Ice density of 56 pcf.
11) A wind speed of 50 mph is used in combination with ice.
12) Deflections calculated using a wind speed of 60 mph .
13) $\quad$ Grouted pipe $f_{c}$ is 7 ksi .
14) Pressures are calculated at each section.
15) Stress ratio used in tower member design is 1.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
$\sqrt{ }$ Use Code Stress Ratios
$\sqrt{\text { Use Code Safety Factors - Guys }}$
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
$\sqrt{ }$ Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section
$\sqrt{\text { Secondary Horizontal Braces Leg }}$ Use Diamond Inner Bracing (4 Sided)
SR Members Have Cut Ends
SR Members Are Concentric

SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area
$\sqrt{ } \sqrt{ }$ Use Clear Spans For KL/r
$\checkmark$ Retension Guys To Initial Tension Bypass Mast Stability Checks
$\checkmark$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
Autocalc Torque Arm Areas
Add IBC .6D+W Combination Sort Capacity Reports By Component
$\sqrt{ }$ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder

Use ASCE 10 X -Brace Ly Rules
$\checkmark$ Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\sqrt{ }$ Consider Feed Line Torque
$\sqrt{ }$ Include Angle Block Shear Check
Use TIA-222-G Bracing Resist.
Exemption
Use TIA-222-G Tension Splice
Exemption
Poles
Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets


Triangular Tower

Tower Section Geometry

| Tower <br> Section | Tower <br> Elevation | Assembly <br> Database | Description | Section <br> Width | Number <br> of <br> Sections |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 |  |  | Section <br> Length |  |  |
| T2 | $160.00-156.00$ | $66.00-152.00$ | 6.52 | 1 | 4. |
| T3 | $152.00-148.00$ | 6.53 | 4.00 |  |  |
| T4 | $148.00-144.00$ | 6.54 | 1 | 4.00 |  |
| T5 | $144.00-140.00$ | 6.55 | 4.00 |  |  |
| T6 | $140.00-120.00$ | 6.55 | 1 | 4.00 |  |
| T7 | $120.00-100.00$ | 6.56 | 1 | 4.00 |  |
| T8 | $100.00-80.00$ | 8.60 | 1 | 20.00 |  |
| T9 | $80.00-60.00$ | 10.64 | 1 | 20.00 |  |
| T10 | $60.00-40.00$ | 12.68 | 1 | 20.00 |  |
| T11 | $40.00-20.00$ | 14.77 | 1 | 20.00 |  |
| T12 | $20.00-0.00$ | 16.77 | 1 | 20.00 |  |

## Tower Section Geometry (cont'd)

| Tower Section | Tower Elevation <br> ft | Diagonal Spacing ft | Bracing Type | Has KBrace End Panels | Has Horizontals | Top Girt Offset in | Bottom Girt Offset in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 160.00-156.00 | 4.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T2 | 156.00-152.00 | 4.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T3 | 152.00-148.00 | 4.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T4 | 148.00-144.00 | 4.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T5 | 144.00-140.00 | 4.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T6 | 140.00-120.00 | 5.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T7 | 120.00-100.00 | 6.67 | X Brace | No | No | 0.0000 | 0.0000 |
| T8 | .100.00-80.00 | 6.67 | X Brace | No | No | 0.0000 | 0.0000 |
| T9 | 80.00-60.00 | 6.67 | X Brace | No | No | 0.0000 | 0.0000 |
| T10 | 60.00-40.00 | 10.00 | X Brace | No | No | 0.0000 | 0.0000 |
| T11 | 40.00-20.00 | 10.00 | X Brace | No | No | 0.0000 | 0.0000 |

tnxTower Report - version 7.0.5.1

| Tower Section | Tower Elevation <br> ft | Diagonal Spacing <br> ft | Bracing Type | Has KBrace End Panels | Has Horizontals | Top Girt Offset in | Bottom Girt Offset in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T12 | 20.00-0.00 | 10.00 | X Brace | No | No | 0.0000 | 0.0000 |

## Tower Section Geometry (cont'd)

| Tower Elevation ft | $\begin{aligned} & \text { Leg } \\ & \text { Type } \end{aligned}$ | Leg <br> Size | Leg Grade | Diagonal Type | $\begin{gathered} \text { Diagonal } \\ \text { Size } \end{gathered}$ | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T1 160.00- } \\ 156.00 \end{gathered}$ | Pipe | Rohn 2.375" $\times 0.218^{\prime \prime}(2$ EH) | $\begin{aligned} & \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ | Single Angle | L $1.5 \times 1.5 \times 1 / 8$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T2 } 156.00- \\ 152.00 \end{gathered}$ | Pipe | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ EH) | $\begin{aligned} & \text { A572-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Single Angle | L $1.5 \times 1.5 \times 1 / 8$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T3 } 152.00- \\ 148.00 \end{gathered}$ | Pipe | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ EH) | $\begin{aligned} & \text { A572-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Single Angle | L $1.5 \times 1.5 \times 1 / 8$ | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T4 } 148.00- \\ 144.00 \end{gathered}$ | Pipe | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ EH) | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Single Angle | L $1.5 \times 1.5 \times 1 / 8$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T5 } 144.00- \\ 140.00 \end{gathered}$ | Pipe | $\begin{gathered} \text { Rohn } 2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \\ \text { EH) } \end{gathered}$ | $\begin{aligned} & \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ | Single Angle | L $2 \times 2 \times 1 / 4$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T6 140.00- } \\ 120.00 \end{gathered}$ | Pipe | $\begin{gathered} \text { Rohn } 2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5 \\ E H) \end{gathered}$ | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 1.5 \times 1.5 \times 1 / 8(3 / 16)$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T7 } 120.00- \\ 100.00 \end{gathered}$ | Pipe | Rohn 4" $\times 0.318$ " (3.5 EH) | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 2 \times 2 \times 3 / 16$ (3/16) | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T8 } 100.00- \\ 80.00 \end{gathered}$ | Grouted Pipe | Rohn 4" $\times 0.318^{\prime \prime}$ ( 3.5 EH ) | $\begin{aligned} & \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ | Double Angle | $2 L 2.5 \times 2.5 \times 3 / 16(3 / 16)$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T9 80.00-60.00 | Grouted Pipe | ROHN 4 EH | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4)$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T10 } 60.00- \\ 40.00 \end{gathered}$ | Grouted Pipe | Rohn 5.563" x 0.375" (5 EH) | $\begin{aligned} & \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ | Double Angle | $2 \mathrm{~L} 3 \times 3 \times 3 / 16$ (1/4) | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T11 40.00- } \\ 20.00 \end{gathered}$ | Grouted Pipe | Rohn 5.563" x 0.375" (5 EH) | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3 \times 3 \times 1 / 4(1 / 4)$ | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ |
| T12 20.00-0.00 | Grouted Pipe | Rohn 6.625" $\times 0.432^{\prime \prime}(6$ $E H)$ | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \\ \hline \end{gathered}$ | Double Angle | $2 \mathrm{~L} 3.5 \times 3.5 \times 1 / 4(1 / 4)$ | $\begin{gathered} A 36 \\ (36 \mathrm{ksi}) \end{gathered}$ |

## Tower Section Geometry (cont'd)

| Tower <br> Elevation <br> $f t$ | Top Girt <br> Type | Top Girt <br> Size |  | Top Girt <br> Grade | Bottom Girt <br> Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 $160.00-$ | Equal Angle | $\mathrm{L} 2 \times 2 \times 1 / 8$ |  | Bottom Girt <br> Size | Bottom Girt <br> Grade |
| 156.00 |  |  |  |  |  |
| T6 $140.00-$ | Equal Angle | $\mathrm{L} 2 \times 2 \times 1 / 8$ | $(36 \mathrm{ksi})$ | Single Angle |  |
| 120.00 |  |  | A36 | Single Angle | A36 |

Tower Section Geometry (cont'd)

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| Tower Elevation <br> ft | Gusset Area (perface) $\qquad$ | Gusset Thickness in | Gusset GradeAdjust. Factor $A_{f}$ |  | Adjust. Factor $A_{\text {r }}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Boit Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 144.00 |  |  | (36 ksi) |  |  |  |  |  |  |
| $\begin{gathered} \text { T5 } 144.00- \\ 140.00 \end{gathered}$ | 0.00 | 0.1875 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 30.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T6 } 140.00- \\ 120.00 \end{gathered}$ | 0.00 | 0.1875 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 30.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T7 } 120.00- \\ 100.00 \end{gathered}$ | 0.00 | 0.1875 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 36.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T8 } 100.00- \\ 80.00 \end{gathered}$ | 0.00 | 0.4375 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 48.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T9 } 80.00- \\ 60.00 \end{gathered}$ | 0.00 | 0.4375 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 48.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T10 } 60.00- \\ 40.00 \end{gathered}$ | 0.00 | 0.2500 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 60.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T11 40.00 } \\ 20.00 \end{gathered}$ | 0.00 | 0.2500 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 60.0000 | 30.0000 | 36.0000 |
| $\begin{gathered} \text { T12 } 20.00- \\ 0.00 \\ \hline \end{gathered}$ | 0.00 | 0.2500 | $\begin{gathered} \mathrm{A} 36 \\ (36 \mathrm{ksi}) \end{gathered}$ | 1.03 | 1 | 1.05 | 60.0000 | 30.0000 | 36.0000 |

Tower Section Geometry (cont'd)

|  |  |  | $K$ Factors ${ }^{1}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tower Elevation | Calc K | Calc K | Legs | Brace | $\begin{gathered} \text { K } \\ \text { Brace } \end{gathered}$ | Single Diags | Girts | Horiz. | Sec. Horiz. | Inner Brace |
|  | Single | Solid |  | Diags | Diags |  |  |  |  |  |
|  | Angles | Rounds |  | $X$ | $\chi$ | $X$ | $X$ | $X$ | $X$ | $X$ |
| ft |  |  |  | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ | $Y$ |
| T1 160.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 156.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T2 156.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 152.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T3 152.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 148.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T4 148.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 144.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T5 144.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 140.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T6 140.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 120.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T7 120.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 100.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T8 100.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 80.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T9 80.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 60.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T10 60.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 40.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T11 40.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 20.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T12 20.00- | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 0.00 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

${ }^{1}$ Note: $K$ factors are applied to member segment lengths. K-braces without inner supporting members will have the $K$ factor in the out-ofplane direction applied to the overall length.

## Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width <br> Deduct <br> in | $U$ | Net <br> Width <br> Deduct in | $U$ | $\begin{gathered} \text { Net Width } \\ \text { Deduct } \\ \text { in } \end{gathered}$ |  | Net <br> Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net <br> Width Deduct in | $U$ |
| $\begin{gathered} \text { T1 160.00- } \\ 156.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T2 156.00- } \\ 152.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T3 } 152.00- \\ 148.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T4 148.00- } \\ 144.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T5 144.00- } \\ 140.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T6 } 140.00- \\ 120.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T7 } 120.00- \\ 100.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T8 100.00- } \\ 80.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T9 80.00 } \\ 60.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T10 } 60.00- \\ 40.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T11 40.00- } \\ 20.00 \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| $\begin{gathered} \text { T12 } 20.00- \\ 0.00 \\ \hline \end{gathered}$ | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |

## Tower Section Geometry (cont'd)

| Tower Elevation | Connection Offsets |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Diagonal |  |  |  | K-Bracing |  |  |  |
|  | Vert. <br> Top <br> in | Horiz. Top in | Vert. <br> Bot. <br> in | Horiz. Bot. in | Vert. <br> Top <br> in | Horiz. Top in | Vert. Bot. in | Horiz. Bot. in |
| $\begin{gathered} \text { T1 } 160.00- \\ 156.00 \end{gathered}$ | 2.5000 | 3.5000 | 2.5000 | 3.5000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T2 } 156.00- \\ 152.00 \end{gathered}$ | 2.5000 | 3.5000 | 2.5000 | 3.5000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T3 } 152.00- \\ 148.00 \end{gathered}$ | 2.5000 | 3.5000 | 2.5000 | 3.5000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T4 148.00- } \\ 144.00 \end{gathered}$ | 2.5000 | 3.5000 | 2.5000 | 3.5000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T5 } 144.00- \\ 140.00 \end{gathered}$ | 2.5000 | 3.5000 | 2.5000 | 3.5000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T6 } 140.00- \\ 120.00 \end{gathered}$ | 2.5000 | 4.4000 | 2.5000 | 4.4000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T7 } 120.00- \\ 100.00 \end{gathered}$ | 2.5000 | 4.9000 | 2.5000 | 4.9000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T8 } 100.00 \\ 80.00 \end{gathered}$ | 2.5000 | 4.9000 | 2.5000 | 4.9000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T9 } 80.00 \\ 60.00 \end{gathered}$ | 2.5000 | 4.8000 | 2.5000 | 4.8000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T10 } 60.00- \\ 40.00 \end{gathered}$ | 2.5000 | 5.3000 | 2.5000 | 5.3000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T11 } 40.00- \\ 20.00 \end{gathered}$ | 2.5000 | 5.4000 | 2.5000 | 5.4000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| $\begin{gathered} \text { T12 } 20.00- \\ 0.00 \\ \hline \end{gathered}$ | 2.5000 | 5.4000 | 2.5000 | 5.4000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

## Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg Connection Type | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bolt Size in | No. | $\begin{gathered} \text { Bolt Size } \\ \text { in } \end{gathered}$ |  | $\begin{gathered} \text { Bolt Size } \\ \text { in } \end{gathered}$ | No. | $\begin{gathered} \text { Bolt Size } \\ \text { in } \\ \hline \end{gathered}$ |  | $\begin{array}{\|c} \hline \begin{array}{c} \text { Bolt Size } \\ \text { in } \end{array} \\ \hline \end{array}$ |  | $\begin{gathered} \text { Bolt Size } \\ \text { in } \end{gathered}$ |  | $\begin{array}{\|c} \text { Bolt Size } \\ \text { in } \end{array}$ |  |
| T1 160.00- | Flange | 0.6250 | 4 | 0.5000 | 1 | 0.5000 | 1 | 0.0000 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 156.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T2 156.00- | Flange | 0.6250 | 0 | 0.5000 | 1 | 0.6250 | 0 | 0.0000 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 152.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T3 152.00- | Flange | 0.6250 | 0 | 0.5000 | 1 | 0.6250 | 0 | 0.0000 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 148.00 |  | A325N |  | A 325 N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T4 148.00- | Flange | 0.6250 | 0 | 0.5000 | 1 | 0.6250 | 0 | 0.0000 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 144.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T5 144.00- | Flange | 0.6250 | 0 | 0.5000 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 140.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T6 140.00- | Flange | 0.6250 | 4 | 0.5000 | 1 | 0.5000 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 120.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T7 120.00- | Flange | 0.7500 | 4 | 0.5000 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 100.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T8 100.00- | Flange | 0.8750 | 4 | 0.5000 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.5000 | 1 |
| 80.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T9 80.00- | Flange | 1.0000 | 6 | 0.5000 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.5000 | 1 |
| 60.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A 325 N |  | A325N |  | A325N |  |
| T10 60.00- | Flange | 1.0000 | 6 | 0.6250 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 40.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T11 40.00- | Flange | 1.0000 | 6 | 0.6250 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.5000 | 1 |
| 20.00 |  | A325N |  | A325N |  | A325N |  | A325N |  | A 325 N |  | A 325 N |  | A325N |  |
| T12 20.00- | Flange | 1.0000 | 6 | 0.6250 | 1 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 | 0.6250 | 0 |
| 0.00 |  | A449 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A 325 N |  |

## Grouted Pipe Properties

| Size | $\begin{aligned} & F_{y} \\ & k s i \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{s} \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & A_{c} \\ & i n^{2} \\ & \hline \end{aligned}$ | $\begin{aligned} & W / t \\ & p l f \end{aligned}$ | $\begin{aligned} & E_{c} \\ & \mathrm{ksi} \end{aligned}$ | $\begin{aligned} & E_{m} \\ & k s i \end{aligned}$ | $\begin{aligned} & F_{y m} \\ & k s i \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Rohn } 4^{\prime \prime} \times 0.318^{\prime \prime} \\ (3.5 \mathrm{EH})(\mathrm{GR}) \end{gathered}$ | 50 | 3.6784 | 8.8880 | 31.033 | 4769 | 38218 | 64 |
| ROHN 4 EH (GR) | 50 | 4.4074 | 11.4969 | 38.949 | 4769 | 38952 | 66 |
| $\begin{aligned} & \text { Rohn } 5.563^{\prime \prime} \mathrm{x} \\ & 0.375^{\prime \prime}(5 \mathrm{EH}) \\ & (\mathrm{GR}) \end{aligned}$ | 50 | 6.1120 | 18.1937 | 58.701 | 4769 | 40357 | 68 |
| $\begin{gathered} \text { Rohn } 6.625^{\prime \prime} \mathrm{x} \\ 0.432^{\prime \prime}(6 \mathrm{EH})(\mathrm{GR}) \end{gathered}$ | 50 | 8.4049 | 26.0667 | 82.906 | 4769 | 40832 | 68 |

Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Face or Leg | Allow Shield | Component Type | Placement <br> ft | Face Offset in | Lateral Offset (Frac FW) | \# | $\begin{gathered} \# \\ \text { Per } \\ \text { Row } \end{gathered}$ | Clear Spacing in | Width or Diameter in | Perimete <br> $r$ <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| **FACE C** LDF4- 50A(1/2") | A | No | $\mathrm{Ar}(\mathrm{CaAa})$ | 50.00-0.00 | 0.0000 | 0.42 | 1 | 1 | 0.6300 | 0.6300 |  | 0.15 |
| 1.5" flat Cable Ladder Rail **FACE B** | A | No | $\mathrm{Af}(\mathrm{CaAa})$ | 150.00-0.00 | 0.0000 | 0.42 | 2 | 2 | $\begin{gathered} 12.0000 \\ 1.5000 \end{gathered}$ | 1.5000 |  | 1.80 |
| $\begin{aligned} & \text { LDF7-50A(1- } \\ & \left.5 / 8^{\prime \prime}\right) \\ & \text { (INCLUDING } \end{aligned}$ | B | No | $\mathrm{Ar}(\mathrm{CaAa})$ | 157.00-0.00 | 0.0000 | 0.4 | 12 | 12 | $\begin{aligned} & 1.0000 \\ & 0.5200 \end{aligned}$ | 1.9800 |  | 0.82 |

160 Ft Self Support Tower Structural Analysis


## Discrete Tower Loads


tnxTower Report - version 7.0.5.1

160 Ft Self Support Tower Structural Analysis
CCI BU No 806387
Project Number 37518-2158-002-8700, Order 441482, Revision 0

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Offset Type \& Offsets: Horz Lateral Vert $f t$ ft ft \& $$
\begin{aligned}
& \text { Azimuth } \\
& \text { Adjustmen } \\
& t
\end{aligned}
$$ \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
f t^{2}
$$ \& $C_{A} A_{A}$ Side

$$
f^{2}
$$ \& Weight

K <br>

\hline \multirow{4}{*}{(3) 4' x 2" Pipe Mount} \& \multirow{3}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{144.00} \& $$
\begin{gathered}
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$ \& 65.73 \& 65.73 \& 2.95 <br>

\hline \& \& \& 4.00 \& \& \& No Ice \& 0.79 \& 0.79 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.03 \& 1.03 \& 0.04 <br>

\hline \& \multirow{4}{*}{B} \& \& 0.00 \& \& \& $$
\begin{aligned}
& \text { Ice } \\
& 1 \text { " lce }
\end{aligned}
$$ \& 1.28 \& 1.28 \& 0.04 <br>

\hline \multirow[t]{3}{*}{(3) 4' x 2" Pipe Mount} \& \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{144.00} \& No lce \& 0.79 \& 0.79 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.03 \& 1.03 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.28 \& 1.28 \& 0.04 <br>
\hline \multirow{4}{*}{(3) $4^{\prime} \times 2$ " Pipe Mount} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{144.00} \& 1" Ice \& \& \& <br>
\hline \& \& \& 4.00 \& \& \& No Ice \& 0.79 \& 0.79 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.03 \& 1.03 \& 0.04 <br>

\hline \& \& \& 0.00 \& \& \& $$
\begin{gathered}
\text { Ice } \\
\text { 1" Jce }
\end{gathered}
$$ \& 1.28 \& 1.28 \& 0.04 <br>

\hline * \& \& \& \& \& \& \& \& \& <br>
\hline * \& \& \& \& \& \& \& \& \& <br>
\hline * \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(4) DB844H90E-XY w/ Mount Pipe (ABANDONED)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{118.00} \& No lce \& 3.30 \& 4.80 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.67 \& 5.42 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice

$$
1^{11} \text { Ice }
$$ \& 4.03 \& 6.04 \& 0.12 <br>

\hline \multirow[t]{4}{*}{(4) DB844H90E-XY w/ Mount Pipe (ABANDONED)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{3}{*}{118.00} \& No Ice \& 3.30 \& 4.80 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.67 \& 5.42 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 4.03 \& 6.04 \& 0.12 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(4) DB844H90E-XY w/ Mount Pipe (ABANDONED)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{118.00} \& No lce \& 3.30 \& 4.80 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.67 \& 5.42 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 4.03 \& 6.04 \& 0.12 <br>

\hline \& \& \& \& \& \& $$
1^{\prime \prime} \text { Ice }
$$ \& \& \& <br>

\hline \multirow[t]{6}{*}{| Sector Mount [SM 404-3] |
| :--- |
| (ABANDONED) |} \& \multirow[t]{6}{*}{C} \& \multirow[t]{6}{*}{None} \& \& \multirow[t]{6}{*}{0.0000} \& \multirow[t]{6}{*}{118.00} \& No Ice \& 20.47 \& 20.47 \& 0.92 <br>

\hline \& \& \& \& \& \& 1/2" \& 28.97 \& 28.97 \& 1.34 <br>

\hline \& \& \& \& \& \& Ice \& $$
37.47
$$ \& 37.47 \& 1.75 <br>

\hline \& \& \& \& \& \& 1 I' Ice \& \& \& <br>
\hline \& \& \& \& \& \& \& \& \& <br>
\hline \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) $7770.00 \mathrm{w} /$ Mount Pipe (x)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& \& \& 4.25 \& <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime}
$$ \& 6.18 \& 5.01 \& 0.10 <br>

\hline \& \& \& 0.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) LGP21401} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) LGP21901} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 0.23 \& 0.16 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.29 \& 0.21 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.36 \& 0.28 \& 0.01 <br>
\hline \& \& \& \& \& \& 1 Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) $7770.00 \mathrm{w} /$ Mount Pipe (x)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 5.75 \& 4.25 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.18 \& 5.01 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \& \& \& \& \& $1{ }^{1 /}$ Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) LGP21401} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.38 \& 0.54 \& 0.03 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) LGP21901} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 0.23 \& 0.16 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.29 \& 0.21 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.36 \& 0.28 \& 0.01 <br>
\hline \& \& \& \& \& \& 1 1' Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) $7770.00 \mathrm{w} /$ Mount Pipe (x)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 5.75 \& 4.25 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.18 \& 5.01 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 6.61 \& 5.71 \& 0.16 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline (2) LGP21401 \& C \& From Leg \& 4.00 \& 0.0000 \& 90.00 \& No lce \& 1.10 \& 0.35 \& 0.01 <br>
\hline
\end{tabular}

tnxTower Report - version 7.0.5.1

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Offset Type \& Offsets: Horz Lateral Vert ft $f t$ ft \& Azimuth Adjustmen $t$ \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
{f t^{2}}^{2}
$$ \& $C_{A} A_{A}$ Side $t t^{2}$ \& Weight

K <br>
\hline \multirow{6}{*}{(2) LGP21901} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& 0.00 \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{90.00} \& $1 / 2^{\prime \prime}$ \& 1.24 \& 0.44 \& 0.02 <br>

\hline \& \& \& 0.00 \& \& \& $$
\begin{aligned}
& \text { Ice } \\
& \text { 1" Ice }
\end{aligned}
$$ \& 1.38 \& 0.54 \& 0.03 <br>

\hline \& \& \& 4.00 \& \& \& No Ice \& 0.23 \& 0.16 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.29 \& 0.21 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.36 \& 0.28 \& 0.01 <br>
\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{None} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{90.00} \& $1{ }^{1 \prime}$ Ice \& \& \& <br>
\hline \multirow[t]{3}{*}{Sector Mount [SM 802-3]
*} \& \& \& \& \& \& No lce \& 24.41 \& 24.41 \& 0.93 <br>
\hline \& \& \& \& \& \& 1/2" \& 31.39 \& 31.39 \& 1.36 <br>

\hline \& \& \& \& \& \& $$
\begin{gathered}
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$ \& 38.37 \& 38.37 \& 1.79 <br>

\hline * \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{4}{*}{| KS24019-L112A |
| :--- |
| (x) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{3}{*}{50.00} \& No Ice \& 0.14 \& 0.14 \& 0.01 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ \& 0.20 \& 0.20 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& ice \& 0.26 \& 0.26 \& 0.01 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& \text { Side Arm Mount [SO } 306- \\
& \text { 1] } \\
& (x)
\end{aligned}
$$} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 2.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{50.00} \& No Ice \& 0.98 \& 2.18 \& 0.04 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.70 \& 3.80 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.42 \& 5.42 \& 0.08 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) RRUS-11 (Proposed)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 2.79 \& 1.19 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.00 \& 1.34 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.21 \& 1.50 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{P45-16-XLH-RR w/ Mount Pipe (Proposed)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 8.24 \& 4.83 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 8.70 \& 5.57 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 9.16 \& 6.27 \& 0.17 <br>
\hline \& \& \& \& \& \& 1"Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) RRUS-11 (Proposed)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No lce \& 2.79 \& 1.19 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2"' \& 3.00 \& 1.34 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.21 \& 1.50 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{| AM-X-CD-16-65-00T-RET |
| :--- |
| w/ Mount Pipe (Proposed) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No lce \& 8.26 \& 6.30 \& 0.07 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 8.82 \& 7.48 \& 0.14 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 9.35 \& 8.37 \& 0.21 <br>
\hline \& \& \& \& \& \& 1"Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& \text { DC6-48-60-18-8F } \\
& \text { (Proposed) }
\end{aligned}
$$} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 0.92 \& 0.92 \& 0.02 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ \& 1.46 \& 1.46 \& 0.04 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 1.64 \& 1.64 \& 0.06 <br>
\hline \& \& \& \& \& \& 1 ' Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{Pipe Mount [PM 601-3]

$$
(\mathrm{x})
$$} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No Ice \& 4.39 \& 4.39 \& 0.20 <br>

\hline \& \& \& \& \& \& 1/2" \& 5.48 \& 5.48 \& 0.24 <br>
\hline \& \& \& \& \& \& Ice \& 6.57 \& 6.57 \& 0.28 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{| (2) RRUS-11 |
| :--- |
| (Proposed) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{90.00} \& No lce \& 2.79 \& 1.19 \& 0.05 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.00 \& 1.34 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 3.21 \& 1.50 \& 0.09 <br>
\hline \& \& \& \& \& \& 1 ' lce \& \& \& <br>
\hline \multirow[t]{4}{*}{AM-X-CD-16-65-00T-RET w/ Mount Pipe (Proposed)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{5}{*}{90.00} \& Nolce \& 8.26 \& 6.30 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 8.82 \& 7.48 \& 0.14 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 9.35 \& 8.37 \& 0.21 <br>
\hline \& \& \& \& \& \& 1 Ice \& \& \& <br>
\hline ** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{4}{*}{B13 RRH $4 \times 30$
(Proposed/ shielded)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{157.00} \& No Ice \& 0.00 \& 1.32 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.00 \& 1.48 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.00 \& 1.64 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{B66A RRH4X45 (Proposed/ shielded)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{157.00} \& Nolce \& 0.00 \& 1.63 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 0.00 \& 1.81 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 0.00 \& 2.00 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{3}{*}{(2) JAHH-65B-R3B wl Mount Pipe (Proposed)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{157.00} \& No Ice \& 12.57 \& 11.82 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 13.19 \& 13.09 \& 0.20 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 13.79 \& 14.14 \& 0.32 <br>
\hline
\end{tabular}

tnxTower Report - version 7.0.5.1

160 Ft Self Support Tower Structural Analysis
Project Number 37518-2158-002-8700, Order 441482, Revision 0

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Offset Type \& Offsets: Horz Lateral Vert ft ft ft \& $$
\begin{gathered}
\text { Azimuth } \\
\text { Adjustmen } \\
t
\end{gathered}
$$ \& Placement \& \& $C_{A} A_{A}$ Front
$$
f^{2}
$$ \& $C_{A} A_{A}$ Side
$$
\tilde{\pi}^{2}
$$ \& Weight

K <br>

\hline | B5 4T4R RRH4X40 AIRSCALE |
| :--- |
| (Proposed/shielded) | \& A \& From Leg \& \[

$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { 1" Ice } \\
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.75 \\
& 0.86 \\
& 0.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.05 \\
& 0.06 \\
& 0.07
\end{aligned}
$$
\] <br>

\hline B13 RRH 4X30 (Proposed/ shielded) \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.32 \\
& 1.48 \\
& 1.64
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.07 \\
& 0.09
\end{aligned}
$$
\] <br>

\hline B66A RRH4X45 (Proposed/ shielded) \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.63 \\
& 1.81 \\
& 2.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.09 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline (2) JAHH-65B-R3B wl Mount Pipe (Proposed) \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \\
& \text { Ice } \\
& 1^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 12.57 \\
& 13.19 \\
& 13.79
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 11.82 \\
& 13.09 \\
& 14.14
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.09 \\
& 0.20 \\
& 0.32
\end{aligned}
$$
\] <br>

\hline | B5 4T4R RRH4X40 AIRSCALE |
| :--- |
| (Proposed/ shielded) | \& B \& From Leg \& \[

$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1 " \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.75 \\
& 0.86 \\
& 0.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.05 \\
& 0.06 \\
& 0.07
\end{aligned}
$$
\] <br>

\hline B13 RRH 4X30 (Proposed/ shielded) \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.32 \\
& 1.48 \\
& 1.64
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.07 \\
& 0.09
\end{aligned}
$$
\] <br>

\hline B66A RRH4X45 (Proposed/ shielded) \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No lce } \\
1 / 2^{" \prime} \\
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.63 \\
& 1.81 \\
& 2.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.09 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline (2) JAHH-65B-R3B w/ Mount Pipe (Proposed) \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No lce } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1 \text { " Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 12.57 \\
& 13.19 \\
& 13.79
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 11.82 \\
& 13.09 \\
& 14.14
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.09 \\
& 0.20 \\
& 0.32
\end{aligned}
$$
\] <br>

\hline B5 4T4R RRH4X40 AIRSCALE (Proposed/shielded) \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.75 \\
& 0.86 \\
& 0.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.05 \\
& 0.06 \\
& 0.07
\end{aligned}
$$
\] <br>

\hline RC3DC-3315-PF-48 (Proposed/ not shielded) \& B \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No lce } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 3.79 \\
& 4.04 \\
& 4.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.51 \\
& 2.72 \\
& 2.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.03 \\
& 0.06 \\
& 0.10
\end{aligned}
$$
\] <br>

\hline RC3DC-3315-PF-48 (Proposed/ not shielded) \& C \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 157.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 3.79 \\
& 4.04 \\
& 4.30
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.51 \\
& 2.72 \\
& 2.94
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.03 \\
& 0.06 \\
& 0.10
\end{aligned}
$$
\] <br>

\hline $$
\begin{gathered}
\text { PCS } 1900 \mathrm{MHZ} 4 \mathrm{X} 45 \mathrm{~W}- \\
65 \mathrm{MHZ} \\
\text { (Proposed) }
\end{gathered}
$$ \& A \& From Leg \& \[

$$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 144.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1 " \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 2.32 \\
& 2.53 \\
& 2.74
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.24 \\
& 2.44 \\
& 2.65
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.08 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline (2) RRH2X50-800 (Proposed) \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 144.00 \& \[

$$
\begin{gathered}
\text { No Ice } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 1.70 \\
& 1.86 \\
& 2.03
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.28 \\
& 1.43 \\
& 1.58
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.05 \\
& 0.07 \\
& 0.09
\end{aligned}
$$
\] <br>

\hline TD-RRH8X20-25 (Proposed) \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 144.00 \& \[

$$
\begin{gathered}
\text { No lce } \\
1 / 2^{\prime \prime} \\
\text { Ice } \\
1^{\prime \prime} \text { lce }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 4.05 \\
& 4.30 \\
& 4.56
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.53 \\
& 1.71 \\
& 1.90
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.10 \\
& 0.13
\end{aligned}
$$
\] <br>

\hline NNVV-65B-R4 w/ Mount Pipe (Proposed) \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 144.00 \& \[

$$
\begin{aligned}
& \text { No lce } \\
& 1 / 2^{\prime \prime} \\
& \text { Ice } \\
& 1^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 12.51 \\
& 13.11 \\
& 13.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 7.41 \\
& 8.60 \\
& 9.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.10 \\
& 0.19 \\
& 0.29
\end{aligned}
$$
\] <br>

\hline APXVTM14-ALU-I20 w/ Mount Pipe (Proposed) \& A \& From Leg \& $$
\begin{aligned}
& 4.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 144.00 \& No lce 1/2" Ice \& \[

$$
\begin{aligned}
& 6.58 \\
& 7.03 \\
& 7.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.96 \\
& 5.75 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.13 \\
& 0.19
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

tnxTower Report - version 7.0.5.1

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) Front \\
\(\pi^{2}\)
\end{tabular} \& \(C_{A} A_{A}\) Side
\[
f^{2}
\] \& Weight

$K$ <br>

\hline \multirow{5}{*}{$$
\begin{gathered}
\text { PCS } 1900 \mathrm{MHZ} 4 \mathrm{XX} 45 \mathrm{~W}- \\
65 \mathrm{MHZ} \\
\text { (Proposed) }
\end{gathered}
$$} \& \multirow{5}{*}{B} \& \multirow{4}{*}{From Leg} \& \& \& \& 1" Ice \& \& \& <br>

\hline \& \& \& 4.00 \& 0.0000 \& 144.00 \& No lce \& 2.32 \& 2.24 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.53 \& 2.44 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.74 \& 2.65 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) RRH2X50-800 (Proposed)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 1.70 \& 1.28 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.86 \& 1.43 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.03 \& 1.58 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{| TD-RRH8X20-25 |
| :--- |
| (Proposed) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 4.05 \& 1.53 \& 0.07 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.30 \& 1.71 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 4.56 \& 1.90 \& 0.13 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{NNV -65B-R4 w/ Mount Pipe (Proposed)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 12.51 \& 7.41 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 13.11 \& 8.60 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 13.67 \& 9.50 \& 0.29 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{APXVTM14-ALU-I20 w/ Mount Pipe (Proposed)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 6.58 \& 4.96 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 7.03 \& 5.75 \& 0.13 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 7.47 \& 6.47 \& 0.19 <br>
\hline \& \& \& \& \& \& 1"Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{$$
\begin{gathered}
\text { PCS 1900MHZ } 4 \mathrm{X} 45 \mathrm{~W}- \\
65 \mathrm{MHZ} \\
\text { (Proposed) }
\end{gathered}
$$} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& Nolce \& 2.32 \& 2.24 \& 0.06 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" \& 2.53 \& 2.44 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1ce \& 2.74 \& 2.65 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) $\mathrm{RRH} 2 \times 50-800$ (Proposed)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No lce \& 1.70 \& 1.28 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.86 \& 1.43 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.03 \& 1.58 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{TD-RRH8X20-25 (Proposed)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No lce \& 4.05 \& 1.53 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 4.30 \& 1.71 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 4.56 \& 1.90 \& 0.13 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{NNV-65B-R4 w/ Mount Pipe (Proposed)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 12.51 \& 7.41 \& 0.10 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 13.11 \& 8.60 \& 0.19 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 13.67 \& 9.50 \& 0.29 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{3}{*}{APXVTM14-ALU-I20 w/ Mount Pipe (Proposed)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& 0.0000 \& 144.00 \& No Ice \& 6.58 \& 4.96 \& <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 7.03 \& 5.75 \& 0.13 <br>

\hline \& \& \& 0.00 \& \& \& $$
\begin{gathered}
\text { Ice } \\
\text { 1" Ice }
\end{gathered}
$$ \& 7.47 \& 6.47 \& 0.19 <br>

\hline ** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{4}{*}{PD1110} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 0.00 \& 0.0000 \& 109.00 \& No Ice \& 2.50 \& 2.50 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.84 \& 3.84 \& 0.04 <br>
\hline \& \& \& 6.00 \& \& \& Ice \& 5.20 \& 5.20 \& 0.07 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{Side Arm Mount [SO 3081]} \& \multirow[t]{4}{*}{c} \& \multirow[t]{4}{*}{From Leg} \& 0.00 \& 0.0000 \& 109.00 \& No lce \& 0.98 \& 3.03 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.70 \& 5.22 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& Ice \& 2.42 \& 7.41 \& 0.10 <br>
\hline \& \& \& \& \& \& 1" Ice \& \& \& <br>
\hline
\end{tabular}

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load | Tilt | Comb. |
| :---: | :---: | :---: | :---: | :---: | :---: |


| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load | Tilt | Comb. |
| :---: | :---: | :---: | :---: | :---: | :---: |


| Critical Deflections and Radius of Curvature - Service Wind |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation ft | Appurtenance | $\begin{aligned} & \text { Gov. } \\ & \text { Load } \\ & \text { comb. } \end{aligned}$ | Deflection in | Tilt | Twist | Radius of Curvature ft |
| 157.00 | (2) LPA-80080/6CF w/ Mount Pipe | 43 | 2.784 | 0.1733 | 0.0073 | 52758 |
| 144.00 | Sector Mount [SM 506-3] | 43 | 2.301 | 0.1664 | 0.0059 | 32201 |
| 118.00 | (4) DB844H90E-XY w/ Mount | 43 | 1.470 | 0.1279 | 0.0036 | 34335 |
| 109.00 | PD1110 | 43 | 1.233 | 0.1159 | 0.0032 | 38969 |
| 90.00 50.00 | (2) 7770.00 w/ Mount Pipe | 43 43 | 0.811 0.236 | 0.0910 0.0430 | 0.0025 0.0011 | 43844 56813 |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 157.00 | (2) LPA-80080/6CF w/ Mount Pipe | 10 | 12.513 | 0.7763 | 0.0333 | 11745 |
| 144.00 | Sector Mount [SM 506-3] | 10 | 10.348 | 0.7459 | 0.0269 | 7259 |
| 118.00 | (4) DB844H90E-XY w/ Mount Pipe | 10 | 6.618 | 0.5744 | 0.0165 | 7668 |
| 109.00 | PD1110 | 10 | 5.551 | 0.5210 | 0.0144 | 8698 |
| 90.00 | (2) $7770.00 \mathrm{w} / \mathrm{Mount}$ Pipe | 10 | 3.651 | 0.4094 | 0.0113 | 9775 |
| 50.00 | KS24019-L112A | 10 | 1.063 | 0.1938 | 0.0050 | 12626 |



## Compression Checks

## Leg Design Data (Compression)

| Section <br> No. | Elevation | Size | L | $L_{u}$ | Kl/r |  | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | ft | ft |  | $i n^{2}$ | K | $K$ | $\phi P_{n}$ |
| T1 | 160-156 | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ EH) | 4.00 | 4.00 | $\begin{gathered} 62.6 \\ K=1.00 \end{gathered}$ | 1.4773 | -4.14 | 49.90 | $\begin{gathered} 0.083^{1} \\ \% \end{gathered}$ |
| T2 | 156-152 | Rohn 2.375" x 0.218" (2 <br> EH) | 4.00 | 4.00 | $\begin{gathered} 62.6 \\ K=1.00 \end{gathered}$ | 1.4773 | -5.46 | 49.90 | $0.109^{1}$ |
| T3 | 152-148 | Rohn 2.375" x 0.218" (2 <br> EH) | 4.00 | 4.00 | $\begin{gathered} 62.6 \\ K=1.00 \end{gathered}$ | 1.4773 | -8.64 | 49.90 | $0.173^{1}$ |
| T4 | 148-144 | Rohn 2.375" $\times 0.218^{\prime \prime}$ (2 EH) | 4.00 | 4.00 | $\begin{gathered} 62.6 \\ K=1.00 \end{gathered}$ | 1.4773 | -12.89 | 49.90 | $\begin{gathered} 0.258^{1} \\ 4 \end{gathered}$ |
| T5 | 144-140 | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ | 4.00 | 4.00 | 62.6 | 1.4773 | -19.93 | 49.90 | $0.399^{1}$ |

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| Section No. | Elevation | Size | $L$ | $L_{u}$ | KI/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  |  |  |  |  |  |  | $\phi P_{n}$ |
|  |  | EH) |  | $K=1.00$ |  |  |  |  | 4 |
| T6 | 140-120 | Rohn 2.875" $\times 0.276^{\prime \prime}(2.5$ <br> EH) | 20.03 | 5.01 | $\begin{gathered} 65.0 \\ K=1.00 \end{gathered}$ | 2.2535 | -48.88 | 74.43 | $\begin{gathered} 0.657^{1} \\ 7 \end{gathered}$ |
| T7 | 120-100 | Rohn 4" $\times 0.318^{\prime \prime}$ (3.5 EH) | 20.03 | 6.68 | $\begin{gathered} 61.3 \\ K=1.00 \end{gathered}$ | 3.6784 | -76.39 | 125.73 | ${ }_{0}^{0.608^{1}}$ |
| T8 | 100-80 | $\begin{gathered} \text { Rohn } 4 " \times 0.318^{\prime \prime}(3.5 \mathrm{EH}) \\ (\mathrm{GR}) \end{gathered}$ | 20.03 | 6.68 | $\begin{gathered} 61.3 \\ K=1.00 \end{gathered}$ | 3.6784 | -105.52 | 148.29 | $0.712^{1}$ |
| T9 | 80-60 | ROHN 4 EH (GR) | 20.04 | 6.68 | $\begin{gathered} 54.3 \\ K=1.00 \end{gathered}$ | 4.4074 | -134.95 | 192.91 | $0.700^{1}$ |
| T10 | 60-40 | Rohn 5.563" x 0.375" (5 EH ) (GR) | 20.03 | 10.02 | $\begin{gathered} 65.4 \\ K=1.00 \end{gathered}$ | 6.1120 | -161.06 | 246.97 | $0.652^{1}$ |
| T11 | 40-20 | $\begin{gathered} \text { Rohn } 5.563^{\prime \prime} \times 0.375^{\prime \prime}(5 \\ E H)(G R) \end{gathered}$ | 20.04 | 10.02 | $\begin{gathered} 65.4 \\ K=1.00 \end{gathered}$ | 6.1120 | -188.02 | 246.94 | $0.761^{1}$ |
| T12 | 20-0 | Rohn 6.625" $\times 0.432^{\prime \prime}$ ( 6 EH ) (GR) | 20.03 | 10.02 | $\begin{gathered} 54.8 \\ K=1.00 \end{gathered}$ | 8.4049 | -214.46 | 381.11 | $0.563^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls
Diagonal Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K / / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft |  | $f t$ | $f$ |  | $i n^{2}$ | $K$ | $K$ | $\phi P_{n}$ |
| T1 | 160-156 | L $1.5 \times 1.5 \times 1 / 8$ | 6.94 | 3.37 | $\begin{gathered} 136.4 \\ K=1.00 \end{gathered}$ | 0.3594 | - -0.87 | 4.36 | $\begin{gathered} 0.200^{1} \\ 4 \end{gathered}$ |
| T2 | 156-152 | L $1.5 \times 1.5 \times 1 / 8$ | 6.95 | 3.37 | $\begin{gathered} 136.6 \\ K=1.00 \end{gathered}$ | 0.3594 | -2.38 | 4.35 | $0.547^{1}$ |
| T3 | 152-148 | L $1.5 \times 1.5 \times 1 / 8$ | 6.95 | 3.37 | $\begin{gathered} 136.7 \\ K=1.00 \end{gathered}$ | 0.3594 | -2.40 | 4.34 | $0.552^{1}$ |
| T4 | 148-144 | L $1.5 \times 1.5 \times 1 / 8$ | 6.96 | 3.38 | $\begin{gathered} 136.9 \\ K=1.00 \end{gathered}$ | 0.3594 | -2.59 | 4.33 | $0.598^{1}$ |
| T5 | 144-140 | L $2 \times 2 \times 1 / 4$ | 6.97 | 3.38 | $\begin{gathered} 107.8 \\ K=1.04 \end{gathered}$ | 0.9380 | -4.14 | 16.48 | $0.251^{1}$ |
| T6 | 140-120 | $2 \mathrm{~L} 1.5 \times 1.5 \times 1 / 8(3 / 16)$ | 8.46 | 4.26 | $\begin{gathered} 125.3 \\ K=1.00 \end{gathered}$ | 0.7188 | -3.62 | 10.20 | $0.355^{1}$ |
| T7 | 120-100 | $\begin{aligned} & 2 \mathrm{~L} \text { 'a'> } 24.4215 \text { in }-61 \\ & 2 \mathrm{~L} 2 \times 2 \times 3 / 16(3 / 16) \end{aligned}$ | 11.36 | 5.76 | $\begin{gathered} 119.1 \\ K=1.00 \end{gathered}$ | 1.4297 | -4.72 | 21.96 | $0.215^{1}$ |
| T8 | 100-80 | $\begin{gathered} 2 \mathrm{~L} ' \mathrm{a}^{\prime}>33.0734 \mathrm{in}-82 \\ 2 \mathrm{~L} 2.5 \times 2.5 \times 3 / 16(3 / 16) \end{gathered}$ | 13.11 | 6.63 | $\begin{gathered} 120.7 \\ K=1.00 \end{gathered}$ | 1.8047 | -5.98 | 27.16 | $0^{0.220^{1}}$ |
| T9 | 80-60 | $\begin{gathered} 2 \mathrm{~L} \text { 'a' }>37.9460 \mathrm{in}-103 \\ 2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4) \end{gathered}$ | 14.99 | 7.57 | $\begin{gathered} 105.5 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.1797 | -6.14 | 38.73 | $0.159^{1}$ |
| T10 | 60-40 | $\begin{gathered} 2 \mathrm{~L} \text { 'a' }>43.2580 \text { in }-124 \\ 2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4) \end{gathered}$ | 18.13 | 9.22 | $\begin{gathered} 130.5 \\ K=1.00 \end{gathered}$ | 2.1797 | -7.25 | 28.70 | $0.253^{1}$ |
| T11 | 40-20 | $\begin{gathered} 2 L^{\prime} \mathrm{a} \text { ' }>52.6982 \mathrm{in}-145 \\ 2 \mathrm{~L} 3 \times 3 \times 1 / 4(1 / 4) \end{gathered}$ | 19.90 | 10.11 | $\begin{gathered} 135.8 \\ K=1.00 \end{gathered}$ | 2.8750 | -7.31 | 35.24 | $0.207^{1}$ |
| T12 | 20-0 | $\begin{aligned} & \text { 2L 'a' }>57.9396 \text { in }-160 \\ & 2 \mathrm{~L} 3.5 \times 3.5 \times 1 / 4(1 / 4) \end{aligned}$ | 21.70 | 11.00 | $\begin{gathered} 121.6 \\ K=1.00 \end{gathered}$ | 3.3750 | -8.11 | 50.21 | $0.162^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls
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## Top Girt Design Data (Compression)

| Section No. | Elevation | Size | $L$ | $L_{u}$ | K//r |  | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | ft | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 160-156 | L2 $2 \times 1 / 8$ | 6.52 | 6.11 | $\begin{gathered} 184.6 \\ K=1.00 \end{gathered}$ | 0.4844 | -0.41 | 3.21 | $2^{0.127^{1}}$ |
| T6 | 140-120 | L $2 \times 2 \times 1 / 8$ | 6.56 | 6.16 | $\begin{gathered} 185.8 \\ K=1.00 \end{gathered}$ | 0.4844 | -0.27 | 3.17 | $0.087^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

Tension Checks

| Leg Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. |  | Size |  | $L_{u}$ | KI/r |  | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
|  | t |  | ft | $f t$ |  | $i n^{2}$ | K | $K$ | $\phi P_{n}$ |
| T1 | 160-156 | $\begin{gathered} \text { Rohn } 2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \\ E H) \end{gathered}$ | 4.00 | 4.00 | 62.6 | 1.4773 | 0.01 | 66.48 | $0.000^{1}$ |
| T2 | 156-152 | Rohn 2.375" $\times 0.218^{\prime \prime}(2$ EH) | 4.00 | 4.00 | 62.6 | 1.4773 | 1.61 | 66.48 | $0.024^{1}$ |
| T3 | 152-148 | Rohn 2.375" x 0.218" (2 EH) | 4.00 | 4.00 | 62.6 | 1.4773 | 5.93 | 66.48 | $0.089^{1}$ |
| T4 | 148-144 | Rohn 2.375" $\times 0.218^{\prime \prime}$ ( 2 EH) | 4.00 | 4.00 | 62.6 | 1.4773 | 9.84 | 66.48 | $0.148^{1}$ |
| T5 | 144-140 | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2$ <br> EH) | 4.00 | 4.00 | 62.6 | 1.4773 | 14.48 | 66.48 | $\gamma^{0.218^{1}}$ |
| T6 | 140-120 | Rohn $2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5$ EH) | 20.03 | 5.01 | 65.0 | 2.2535 | 41.65 | 101.41 | $0.411^{1}$ |
| T7 | 120-100 | Rohn 4" $\times 0.318{ }^{\prime \prime}(3.5 \mathrm{EH}$ ) | 20.03 | 6.68 | 61.3 | 3.6784 | 66.03 | 165.53 | $0.399^{1}$ |
| T8 | 100-80 | Rohn 4" x 0.318" (3.5 EH) <br> (GR) | 20.03 | 6.68 | 61.3 | 3.6784 | 90.34 | 165.53 | ${ }^{0.546^{1}}$ |
| T9 | 80-60 | ROHN 4 EH (GR) | 20.04 | 6.68 | 54.3 | 4.4074 | 115.54 | 198.34 | ${ }^{0.583^{1}}$ |
| T10 | 60-40 | Rohn 5.563" $\times 0.375^{\prime \prime}$ ( 5 <br> EH ) (GR) | 20.03 | 10.02 | 65.4 | 6.1120 | 137.44 | 275.04 | $0.500^{1}$ |
| T11 | 40-20 | Rohn 5.563" $\times 0.375^{\prime \prime}$ ( 5 <br> EH) (GR) | 20.04 | 10.02 | 65.4 | 6.1120 | 159.31 | 275.04 | $0^{0.579^{1}}$ |
| T12 | 20-0 | Rohn 6.625" $\times 0.432^{\prime \prime}(6$ <br> EH ) (GR) | 20.03 | 10.02 | 54.8 | 8.4049 | 179.65 | 378.22 | $0.475^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Diagonal Design Data (Tension)

| Section No. | Elevation | Size | L | $L_{u}$ | K/I/ | A | Pu $K$ | ${ }_{\phi}^{\phi} P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| fo. ft |  |  | $f$ | $f t$ |  | $i n^{2}$ | K | K | ${ }_{\phi} P_{n}$ |
| T1 | 160-156 | L $1.5 \times 1.5 \times 1 / 8$ | 6.94 | 3.37 | 89.6 | 0.2109 | 0.83 | 9.18 | $\begin{gathered} 0.091^{1} \end{gathered}$ |
| T2 | 156-152 | L $1.5 \times 1.5 \times 1 / 8$ | 6.95 | 3.37 | 89.6 | 0.2109 | 2.42 | 9.18 | $0.264{ }^{1}$ |
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| Section No. | Elevation <br> ft | Size | ft | $L_{u}$ <br> ft | KI/r | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | Ratio $P_{u}$ $\phi P_{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | $K$ | $\phi P_{n}$ |
| T3 | 152-148 | L $1.5 \times 1.5 \times 1 / 8$ | 6.95 | 3.37 | 89.7 | 0.2109 | 2.35 | 9.18 | $0.256^{\dagger}$ |
| T4 | 148-144 | L $1.5 \times 1.5 \times 1 / 8$ | 6.96 | 3.38 | 89.8 | 0.2109 | 2.65 | 9.18 | $89^{1}$ |
| T5 | 144-140 | L $2 \times 2 \times 1 / 4$ | 6.97 | 3.38 | 68.7 | 0.5863 | 4.04 | 25.50 | $0.158^{1}$ |
| T6 | 140-120 | $2 \mathrm{~L} 1.5 \times 1.5 \times 1 / 8(3 / 16)$ | 8.03 | 4.05 | 107.2 | 0.4219 | 3.61 | 18.35 | . $197{ }^{1}$ |
| T7 | 120-100 | $\begin{gathered} \text { 2L 'a' > } 23.2191 \mathrm{in}-68 \\ 2 \mathrm{~L} .2 \times 2 \times 3 / 16(3 / 16) \end{gathered}$ | 10.80 | 5.48 | 108.6 | 0.8965 | 4.70 | 39.00 | $0.121{ }^{1}$ |
|  |  | 2 L 'a' > 31.4884 in - 89 |  |  |  |  |  |  |  |
| T8 | 100-80 | $2 \mathrm{~L} 2.5 \times 2.5 \times 3 / 16$ (3/16) | 13.11 | 6.63 | 103.8 | 1.1777 | 5.93 | 51.23 | $116^{1}$ |
| T9 | 80-60 | $\begin{gathered} \text { 2L 'a' > } 37.9460 \text { in }-104 \\ 2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4) \end{gathered}$ | 14.99 | 7.57 | 98.1 | 1.4590 | 6.11 | 63.47 | $0.09{ }^{1}$ |
| T10 | 60-40 | $\begin{gathered} 2 \mathrm{~L} \text { 'a' }>43.2580 \mathrm{in}-125 \\ 2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4) \end{gathered}$ | 18.13 | 9.22 | 119.4 | 1.4238 | 7.06 | 61.94 | $0.114^{1}$ |
|  |  | $2 L^{\prime} \mathrm{a}$ ' $>52.6982$ in - 146 |  |  |  |  |  |  |  |
| T11 | 40-20 | $2 \mathrm{~L} 3 \times 3 \times 1 / 4$ (1/4) | 19.90 | 10.11 | 132.0 | 1.8750 | 7.15 | 81.56 | $3.088^{1}$ |
| T12 | 20-0 | $\begin{gathered} \text { 2L 'a' > } 57.9396 \text { in }-161 \\ 2 \mathrm{~L} 3.5 \times 3.5 \times 1 / 4(1 / 4) \end{gathered}$ | 21.70 | 11.00 | 122.2 | 2.2500 | 7.79 | 97.88 | $0.080^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Top Girt Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{u}$ | $K 1 / r$ | $\bar{A}$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
|  | ft |  | ft | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 160-156 | $L 2 \times 2 \times 1 / 8$ | 6.52 | 6.11 | 121.2 | 0.3047 | 0.43 | 13.25 | $0.032^{1}$ |
| T6 | 140-120 | L. $2 \times 2 \times 1 / 8$ | 6.56 | 6.16 | 122.0 | 0.3047 | 0.27 | 13.25 | $\begin{gathered} 0.021^{1} \\ 4 \end{gathered}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \emptyset P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 160-156 | Leg | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}$ (2 EH) | 2 | -4.14 | 49.90 | 8.3 | Pass |
|  |  | Diagonal | L $1.5 \times 1.5 \times 1 / 8$ | 10 | -0.87 | 4.36 | 20.0 | Pass |
|  |  |  |  |  |  |  | 24.1 (b) |  |
|  |  | Top Girt | L. $2 \times 2 \times 1 / 8$ | 6 | -0.41 | 3.21 | 12.7 | Pass |
| T2 | 156-152 | Leg | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{EH})$ | 14 | -5.46 | 49.90 | 10.9 | Pass |
|  |  | Diagonal | L $1.5 \times 1.5 \times 1 / 8$ | 16 | -2.38 | 4.35 | 54.7 | Pass |
|  |  |  |  |  |  |  | 69.8 (b) |  |
| T3 | 152-148 | Leg | Rohn $2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{EH})$ | 23 | -8.64 | 49.90 | 17.3 | Pass |
|  |  | Diagonal | L $1.5 \times 1.5 \times 1 / 8$ | 25 | -2.40 | 4.34 | 55.2 | Pass |
|  |  |  |  |  |  |  | 67.8 (b) |  |

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| Section No. | $\begin{aligned} & \text { Elevation } \\ & \quad f t \\ & \hline \end{aligned}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{aligned} & \emptyset P_{\text {antow }} \\ & K \end{aligned}$ | \% Capacity | $\begin{gathered} \text { Pass } \\ \text { Fail } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | 148-144 | $\begin{gathered} \text { Leg } \\ \text { Diagonal } \end{gathered}$ | $\begin{gathered} \text { Rohn } 2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{EH}) \\ \mathrm{L} 1.5 \times 1.5 \times 1 / 8 \end{gathered}$ | 32 | -12.89 | 49.90 | 25.8 | Pass |
|  |  |  |  | 34 | -2.59 | 4.33 | 59.8 | Pass |
|  |  |  |  |  |  |  | 76.5 (b) |  |
| T5 | 144-140 | Leg Diagonal | $\begin{gathered} \text { Rohn } 2.375^{\prime \prime} \times 0.218^{\prime \prime}(2 \mathrm{EH}) \\ \mathrm{L} 2 \times 2 \times 1 / 4 \end{gathered}$ | 41 | -19.93 | 49.90 | 39.9 | Pass |
|  |  |  |  | 44 | -4.14 | 16.48 | 25.1 | Pass |
|  |  |  |  |  |  |  | 53.8 (b) |  |
| T6 | 140-120 | Leg | Rohn $2.875^{\prime \prime} \times 0.276^{\prime \prime}(2.5$ E.H) | 50 | -48.88 | 74.43 | 65.7 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 1.5 \times 1.5 \times 1 / 8(3 / 16)$ | 61 | -3.62 | 10.20 | 35.5 | Pass |
|  |  |  |  |  |  |  | 57.7 (b) |  |
|  |  | Top Girt | L $2 \times 2 \times 1 / 8$ | 54 | -0.27 | 3.17 | 8.7 | Pass |
| T7 | 120-100 | Leg | Rohn 4" $\times 0.318^{\prime \prime}$ (3.5 EH) | 80 | -76.39 | 125.73 | 60.8 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 2 \times 2 \times 3 / 16(3 / 16)$ | 82 | -4.72 | 21.96 | 21.5 | Pass |
|  |  |  |  |  |  |  | 62.6 (b) |  |
| T8 | 100-80 | Leg | Rohn 4" x 0.318" (3.5 EH) <br> (GR) | 101 | -105.52 | 148.29 | 71.2 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 2.5 \times 2.5 \times 3 / 16$ (3/16) | 103 | -5.98 | 27.16 | 22.0 | Pass |
|  |  |  |  |  |  |  | 47.8 (b) |  |
| T9 | 80-60 | Leg | ROHN 4 EH (GR) | $122$ | $-134.95$ | $192.91$ | 70.0 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4)$ | $124$ | $-6.14$ | $38.73$ | 15.9 | Pass |
|  |  |  |  |  |  |  | 49.3 (b) |  |
| T10 | 60-40 | Leg | Rohn $5.563^{\prime \prime} \times 0.375^{\prime \prime}$ ( 5 EH ) <br> (GR) | 143 | -161.06 | 246.97 | 65.2 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 3 / 16(1 / 4)$ | 145 | -7.25 | 28.70 | 25.3 | Pass |
|  |  |  |  |  |  |  | 47.7 (b) |  |
| T11 | 40-20 | Leg | Rohn 5.563" $\times 0.375$ " ( 5 EH ) (GR) | 158 | -188.02 | 246.94 | 76.1 | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3 \times 3 \times 1 / 4(1 / 4)$ | 160 | -7.31 | 35.24 | 20.7 | Pass |
|  |  |  |  |  |  |  | 48.3 (b) |  |
| T12 | 20-0 | Leg | Rohn 6.625 " $\times 0.432 "(6 \mathrm{EH})$ (GR) | 173 | -214.46 | 381.11 | $\begin{gathered} 56.3 \\ 56.5(\mathrm{~b}) \end{gathered}$ | Pass |
|  |  | Diagonal | $2 \mathrm{~L} 3.5 \times 3.5 \times 1 / 4(1 / 4)$ | 175 | -8.11 | 50.21 | 16.2 | Pass |
|  |  |  |  |  |  |  | 52.7 (b) |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | $76.1$ | Pass |
|  |  |  |  |  |  | Diagonal (T4) | 76.5 | Pass |
|  |  |  |  |  |  | Top Girt (T1) | 12.7 | Pass |
|  |  |  |  |  |  | Bolt | 76.5 | Pass |
|  |  |  |  |  |  | Checks RATING = | 76.5 | Pass |

## APPENDIX B

## BASE LEVEL DRAWING



## APPENDIX C

## ADDITIONAL CALCULATIONS

Pier and Pad Foundation


| TIA-222 Revision: | G |
| ---: | :--- |
| Tower Type: | Self Support |
|  |  |


| Block Foundation?: | $\square$ |
| :--- | :--- |


| Superstructure Analysis Reactions |  |  |
| ---: | :---: | :--- |
| Compression, $\mathbf{P}_{\text {comp: }}$ | 220 | kips |
| Compression Shear, Vu_comp: | 30 | kips |
| Uplift, $\mathrm{P}_{\text {uplifi: }}$ | 185 | kips |
| Uplift Shear, $\mathrm{V}_{\text {u_uplif: }}$ | 25 | kips |
|  |  |  |
| Tower Height, $\mathrm{H}:$ | 162 | ft |
| Base Face Width, $\mathbf{B W}:$ | 21 | ft |
| BP Dist. Above Fdn, $\mathrm{bp}_{\text {dist: }}$ | 0 | in |
|  |  |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating | Check |
| Uplift (kips) | 276.24 | 185.00 | $67.0 \%$ | Pass |
| Lateral (Sliding) (kips) | 91.37 | 30.00 | $32.8 \%$ | Pass |
| Bearing Pressure (ksf) | 13.04 | 4.30 | $33.0 \%$ | Pass |
|  |  |  |  |  |
| Pier Flexure (Comp.) (kip*ft) | 1095.93 | 315.00 | $\mathbf{2 8 . 7} \%$ | Pass |
| Pier Flexure (Tension) (kip*ft) | 708.69 | 262.50 | $37.0 \%$ | Pass |
| Pier Compression (kip) | 2214.70 | 238.18 | $10.8 \%$ | Pass |
| Pad Flexure (kip*ft) | 564.21 | 103.38 | $18.3 \%$ | Pass |
| Pad Shear - 1-way (kips) | 181.87 | 31.07 | $\mathbf{1 7 . 1} \%$ | Pass |
| Pad Shear - 2-way (ksi) | 0.16 | 0.05 | $\mathbf{3 0 . 1 \%}$ | Pass |


| Pier Properties |  |  |
| ---: | :---: | :--- |
| Pier Shape: | Circular |  |
| Pier Diameter, dpier: | 3.5 | ft |
| Ext. Above Grade, E: | 0.5 | ft |
| Pier Rebar Size, Sc: | 8 |  |
| Pier Rebar Quantity, mc: | 16 |  |
| Pier Tie/Spiral Size, St: | 3 |  |
| Pier Tie/Spiral Quantity, mt: | 7 |  |
| Pier Reinforcement Type: | Tie |  |
| Pier Clear Cover, cc $\mathbf{p i e r}^{2}$ | 3 | in |


| Soil Rating: | $67.0 \%$ |
| ---: | ---: |
| Structural Rating: | $37.0 \%$ |


| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 12.0 | ft |
| Pad Width, W: | 9.4 | ft |
| Pad Thickness, T: | 2.0 | ft |
| Pad Rebar Size, Sp: | 7 |  |
| Pad Rebar Quantity, mp: | 11 |  |
| Pad Clear Cover, $\mathrm{cc}_{\text {pad }}:$ | 3 | in |


| Material Properties |  |  |
| ---: | :---: | :---: |
| Rebar Grade, Fy: | 60000 | psi |
| Concrete Compressive Strength, F'c: | 3000 | psi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |


| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 115 | pcf |
| Ultimate Net Bearing, Qnet: | 16.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 30 | degrees |
| SPT Blow Count, N | blows: | 0 |
|  |  |  |
| Base Friction, $\mu:$ | 0 |  |
| Neglected Depth, $\mathbf{N}:$ | 4.0 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | None | ft |

<--Toggle between Gross and Net

## Anchor Rod Check for Self Supporting Towers

TIA-222-G, Section 4.9.9

| Site Data |  |
| ---: | :---: |
| BU\#: |  |
| Site Name: |  |
| App\#: |  |


| Reactions |  |  |
| ---: | :---: | :--- |
| Eta Factor, $\eta$ | $\mathbf{0 . 5 5}$ | Detail Type |
| Uplift, Pu: | $\mathbf{1 8 5}$ | kips |
| Shear, Vu: | $\mathbf{2 5}$ | kips |


| Anchor Rod Data |  |  |
| ---: | :---: | :--- |
| Qty: | 6 |  |
| Diam: | 1 | in |
| Rod Material: | A449 (1/4 to 1 Incl.) |  |
| Strength (Fu): | 120 | ksi |
| Yield (Fy): | 92 | ksi |


| *Rod Circle: |  |  |  |
| ---: | :--- | :---: | :---: |
| * $\mathrm{e}:$ | in |  |  |
| *\# of Rods |  |  |  |
| in |  |  |  |
| Mu= Puxe: |  |  | 1 or 2 |

* Enter rod circle, offset (e) and number of anchor rods at the extreme fiber to consider if eccentric load due to leg reinforcement exists.


Figure 4-4 of TIA-222-G


Columbus, OH 43215
Phone: (614) 221-6679
FAX:

| Project: PJF JOB \#37518-2158-002-8700 |  |  |
| :---: | :---: | :---: |
| Client: Crown Castle | Drawn by ${ }_{\text {jjacobs }}$ | App'd: |
| Code: TIA-222-G | Date: 06/15/18 | Scale: NTS |
| Path: |  |  |

MODIFIED 160' SELF SUPPORT TOWER




[^0]| TOWER MANUFACTURER: ROHN TOMER MANUFACTURER \#. 2281721 |
| :---: |
| QUALIFIED ENGINEERING SERVICES ARE AVAILABLE FR AND COMPANY TO ASSIST CONTRACTORS IN CLASS IV REVIEWS. FOR REQUESTED QUALIFIED ENGINEERING CONTACT US AT RIGGING@PJFWEB.COM. |













## EBI Consulting

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# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

SPRINT Existing Facility
Site ID: CT33XC547
W. Deep River

14 Route 80
Killingworth, CT 06419
August 1, 2018
EBI Project Number: 6218005231

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population <br> allowable limit: | $\mathbf{7 . 5 2 \%}$ |

environmental | engineering | due diligence

August 1, 2018
SPRINT
Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495

Emissions Analysis for Site: CT33XC547 - W. Deep River

EBI Consulting was directed to analyze the proposed SPRINT facility located at $\mathbf{1 4}$ Route $\mathbf{8 0}$, Killingworth, CT, for the purpose of determining whether the emissions from the Proposed SPRINT Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

General population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limits for the 850 MHz Band is approximately $567 \mu \mathrm{~W} / \mathrm{cm}^{2}$. The general population exposure limit for the 1900 MHz (PCS) and 2500 MHz (BRS) bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.
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Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

1
Calculations were done for the proposed SPRINT Wireless antenna facility located at $\mathbf{1 4}$ Route 80, Killingworth, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65 . Since SPRINT is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6 -foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 1 CDMA channels ( 850 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.
2) 2 LTE channels ( 850 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 50 Watts per Channel.
3) 5 CDMA channels ( $1900 \mathrm{MHz}(\mathrm{PCS})$ ) were considered for each sector of the proposed installation. These Channels have a transmit power of 16 Watts per Channel.
4) 2 LTE channels ( $1900 \mathrm{MHz}(\mathrm{PCS})$ ) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
5) 8 LTE channels ( 2500 MHz (BRS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.

## EBI Consulting

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6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
7) For the following calculations, the sample point was the top of a 6 -foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antennas used in this modeling are the Commscope NNVV-65B-R4 and the RFS APXVTM14-ALU-I20 for transmission in the $850 \mathrm{MHz}, 1900 \mathrm{MHz}$ (PCS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
9) The antenna mounting height centerlines of the proposed panel antennas are 144 feet above ground level (AGL) for Sector A, $\mathbf{1 4 4}$ feet above ground level (AGL) for Sector B and $\mathbf{1 4 4}$ feet above ground level (AGL) for Sector C.
10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general population threshold limits.

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## SPRINT Site Inventory and Power Data by Antenna

| Sector: | A |  |  | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna:\#: | 1 |  | 1 | Antenna \#\#: | 1 |
| Mâke $/$ Módel | Commscope NNVV-65B-R4 | Make Módel | Commscope NNVV-65B-R4 | Make Model | Commscope NNVV-65B-R4 |
|  | $12.75 / 15.05 \mathrm{dBd}$ |  | $12.75 / 15.05 \mathrm{dBd}$ |  | $12.75 / 15.05 \mathrm{dBd}$ |
|  | 144 feet |  | 144 feet |  | 144 feet |
| Trequency Bands | $\begin{gathered} 850 \mathrm{MHz} / \\ 1900 \mathrm{MHz}(\mathrm{PCS}) \end{gathered}$ | Ftequency Bands | $\begin{gathered} 850 \mathrm{MHz} / \\ 1900 \mathrm{MHz} \text { (PCS) } \end{gathered}$ | Frequency Bands | $\begin{gathered} 850 \mathrm{MHz} / \\ 1900 \mathrm{MHz}(\mathrm{PCS}) \end{gathered}$ |
|  | 10 | KWa Channe Count | 10 | S- ${ }^{\text {a }}$ Chamel Count | 10 |
|  | 280 Watts |  | 280 Watts |  | 280 Watts |
|  | 7,378.61 |  | 7,378.61 |  | 7,378.61 |
| WvivkintennaA | 1.71 \% |  | 1.71 \% |  | 1.71 \% |
| , Antennai\#: | 2 |  | 2 | Antena \#: | 2 |
| Make $/$ Model | RFS APXVTM14-ALU- I20 | Make Model | RFS APXVTM14-ALU- I20 | Make: Model | RFS APXVTM14-ALU- I20 |
|  | 15.9 dBd |  | 15.9 dBd |  | 15.9 dBd |
|  | 144 feet |  | 144 feet | 3xameligh (AGL) | 144 feet |
| - Erequency Bands | 2500 MHz (BRS) | WrFrequency Bands | 2500 MHz (BRS) | Warequency Bands | 2500 MHz (BRS) |
| \% \% \% Chamme Countu | 8 | W ${ }^{\text {a }}$ O- Chamel Count | 8 | 第紬 Chanhe Count | 8 |
|  | 160 Watts |  | 160 Watts |  | 160 Watts |
|  | 6,224.72 |  | 6,224.72 |  | 6,224.72 |
|  | 1.18 \% |  | 1.18 \% |  | 1.18 \% |


| Site Composite MPEO\%, |  |
| :---: | :---: |
| Carrier | MPE $\%$ |
| SPRINT - Max per sector | $\mathbf{2 . 8 9} \%$ |
| AT\&T | $1.05 \%$ |
| Nextel | $0.65 \%$ |
| Verizon Wireless | $2.93 \%$ |
| Site Total MPE \%: | $\mathbf{7 . 5 2} \%$ |


| SPRINT Sector A Total: | $2.89 \%$ |
| ---: | :---: |
| SPRINT Sector B Total: | $2.89 \%$ |
| SPRINT Sector C Total: | $2.89 \%$ |
| Site Total: | $7.52 \%$ |


| SPRINT Frequency Band/ Tecbnology (All Sectors) | $\#$ Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density $\left(\mu W / \mathrm{cm}^{2}\right)$ | Frequency (MHz) | Allowable MPE <br> $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$ | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sprint 850 MHz CDMA | 1 | 376.73 | 144 | 0.71 | 850 MHz | 567 | 0.12\% |
| Sprint 850 MHz LTE | 2 | 941.82 | 144 | 3.56 | 850 MHz | 567 | 0.63\% |
| Sprint 1900 MHz (PCS) CDMA | 5 | 511.82 | 144 | 4.83 | 1900 MHz (PCS) | 1000 | 0.48\% |
| Sprint 1900 MHz (PCS) LTE | 2 | 1,279.56 | 144 | 4.83 | 1900 MHz (PCS) | 1000 | 0.48\% |
| Sprint 2500 MHz (BRS) LTE | 8 | 778.09 | 144 | 11.75 | 2500 MHz (BRS) | 1000 | 1.18\% |
| YN |  |  |  |  |  | Total: | 2.89\% |

## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the SPRINT facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| SPRINT Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector A: | $2.89 \%$ |
| Sector B: | $2.89 \%$ |
| Sector C: | $2.89 \%$ |
| SPRINT Maximum | $2.89 \%$ |
| MPE \% (per sector): |  |
| Site Total: | $7.52 \%$ |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{7 . 5 2} \%$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


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From:
Sent:
To:
Subject:

TrackingUpdates@fedex.com
Wednesday, August 8, 2018 10:39 AM
Barbadora, Jeff
FedEx Shipment 772918662444 Delivered

## Your package has been delivered

## Tracking \# 772918662444

Ship date:


Delivery date:
Wed, 8/8/2018 10:36
am
14 Route 80 LLC
14 Route 80 LLC
93A Glenwood Road
CLINTON, CT 06413
US

## Shipment Facts

Our records indicate that the following package has been delivered.
\(\left.\begin{array}{ll}Tracking number: \& 772918662444 <br>
Status: \& Delivered: 08/08/2018 10:36 <br>

\& AM Signed for By: L.GRUM\end{array}\right\}\)| Reference: | 1766.6680 |
| :--- | :--- |
| Signed for by: | L.GRUM |
| Delivery location: | CLINTON, CT |
| Delivered to: | Receptionist/Front Desk |
| Service type: | FedEx Priority Overnight $® 8$ |
| Packaging type: | 1 |
| Number of pieces: | 1.00 lb. |
| Weight: | Deliver Weekday |
| Special handling/Services: | Residential Delivery |
| Standard transit: | $8 / 8 / 2018$ by 10:30 am |



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From:
Sent:
To:
Subject:

TrackingUpdates@fedex.com
Wednesday, August 8, 2018 12:29 PM
Barbadora, Jeff
FedEx Shipment 772918561489 Delivered


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From:
Sent:
To:
Subject:

TrackingUpdates@fedex.com
Wednesday, August 8, 2018 12:28 PM
Barbadora, Jeff
FedEx Shipment 772918585648 Delivered

## Your package has been delivered

## Tracking \# 772918585648

Ship date:
Tue, 8/7/2018
Jeff Barbadora
Crown Castle
WOBURN, MA 01801
us


Delivered

Delivery date:
Wed, 8/8/2018 12:27
pm
Ms. Cathie Jefferon-Zoning
Officer
Town of Killingworth
323 Route 81
KILLINGWORTH, CT 06419
US

## Shipment Facts

Our records indicate that the following package has been delivered.

| Tracking number: | 772918585648 |
| :--- | :--- |
| Status: | Delivered: 08/08/2018 12:27 <br> PM Signed for By: <br> M.OTOOLE |
| Reference: | 1766.6680 |
| Signed for by: | M.OTOOLE |
| Delivery location: | KILLINGWORTH, CT |
| Delivered to: | Receptionist/Front Desk |
| Service type: | FedEx Priority Overnight® |
| Packaging type: | FedEx® Envelope |
| Number of pieces: | 1 |
| Weight: | 1.00 lb. |
| Special handling/Services: | Deliver Weekday |
| Standard transit: | $8 / 8 / 2018$ by $12: 00$ pm |

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