

JULIE D. KOHLER

PLEASE REPLY TO: Bridgeport
WRITER'S DIRECT DIAL: (203) 337-4157
E-Mail Address: jkohler@cohenandwolf.com

April 1, 2015

Attorney Melanie Bachman
Acting Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

**Re: Notice of Exempt Modification
Town of Quinebaug Valley Emergency/T-Mobile equipment upgrade
Site ID CT11156A
818 Providence Pike, Killingly Connecticut**

Dear Attorney Bachman:

This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, the Quinebaug Valley Emergency owns the existing guyed tower and related facility located at 818 Providence Pike, Killingly, Connecticut (Latitude: 41.791417; Longitude: -71.822361). T-Mobile intends to replace (3) antennas and add related equipment at this existing telecommunications facility in Killingly ("Killingly Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Town Manager, Sean Hendricks. Quinebaug Valley Emergency is also the property owner.

The existing Killingly Facility consists of a 187 foot tall guyed tower.¹ T-Mobile plans to replace three (3) antennas and add three (3) smart bias Ts at a centerline of 145 feet. T-Mobile will install a BBU cabinet on an existing concrete pad and mount three (3) RRU's (remote radio units) on a proposed H-frame, all within the existing compound area. T-Mobile will also add coax cable. (See the plans revised to March 11, 2015 attached hereto as Exhibit A). The existing Killingly Facility is structurally capable of supporting T-Mobile's proposed modifications, as indicated in the structural analysis dated March 31, 2015 and attached hereto as Exhibit B.

The planned modifications to the Killingly Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the height of the tower. T-Mobile's

¹ The Connecticut Siting Council database does not contain any Dockets or Petitions relative to this Facility however there is a notice of intent captioned TS-VER-069-140117.

April 1, 2015
Site ID CT11156A
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proposed modifications will be installed at a centerline of 145 feet, merely modifying existing antennas located at the same 145 foot elevation. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.

2 . The proposed modifications will not require an extension of the site boundaries. T-Mobile's modifications are all within the existing compound area as shown on Sheets LE-1.

3 . The proposed modification to the Killingly Facility will not increase the noise levels at the existing facility by six decibels or more.

4 . The operation of the replacement antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated March 16, 2015, T-Mobile's operations would add 4.72% of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be 18.71% of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

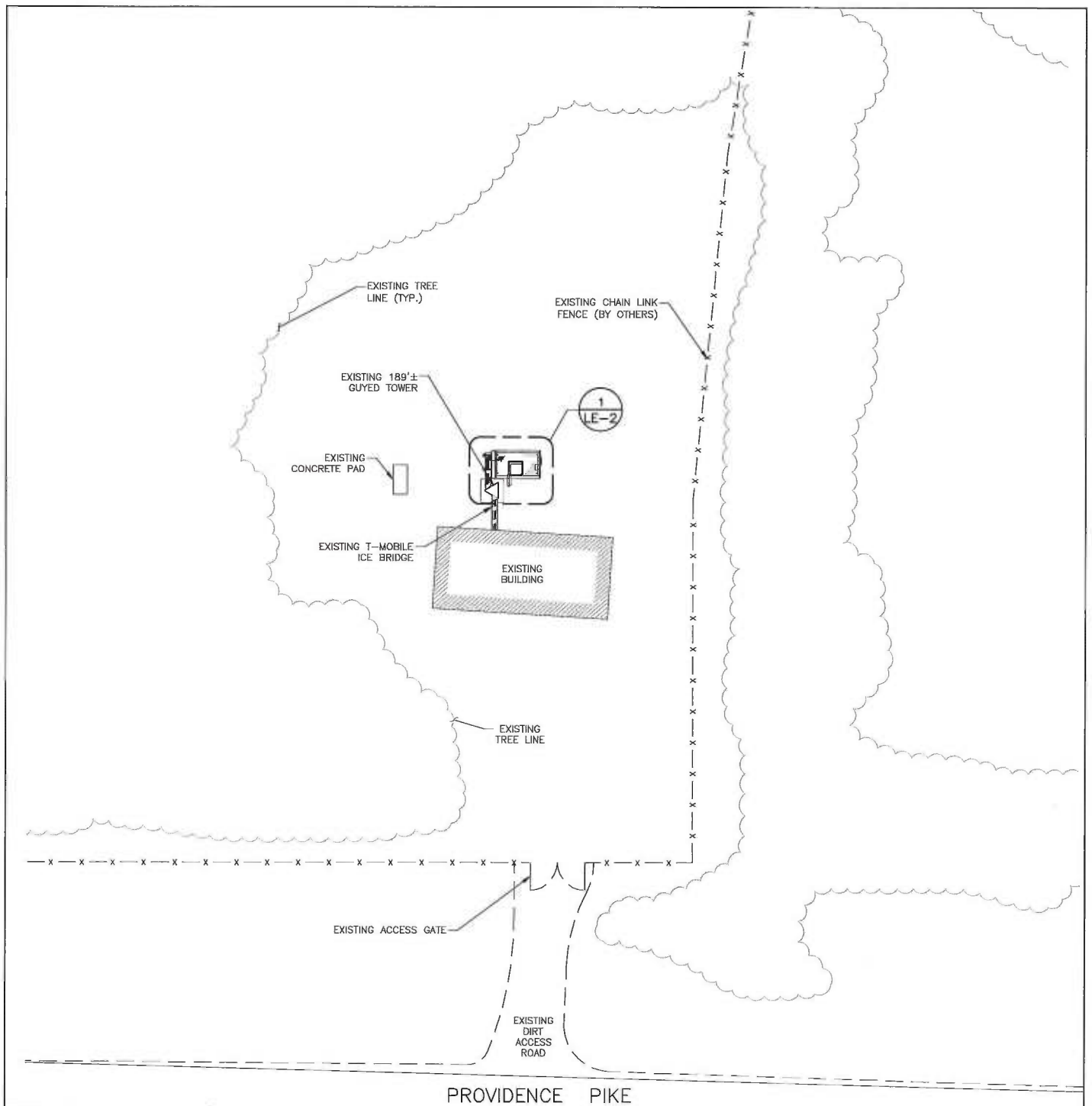
For the foregoing reasons, T-Mobile respectfully submits that the proposed replacement antennas and additional equipment at the Killingly Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,


Julie D. Kohler, Esq.

cc: Town of Killingly, Town Manager Sean Hendricks
Quinebaug Valley Emergency
Jamie Ford, EBI Consulting

EXHIBIT A



CONFIGURATION
704G



NOTE:
 ALL EQUIPMENT LOCATIONS ARE APPROXIMATE AND ARE SUBJECT TO APPROVAL BY LESSEE/LICENSEE STRUCTURAL AND RF ENGINEERS.

EXISTING SITE PLAN

SCALE: 1:30

PREPARED BY:

 21 B Street | Burlington, MA 01803
 Tel: (781) 273-2500 | Fax: (781) 273-3311
 www.ebiconsulting.com

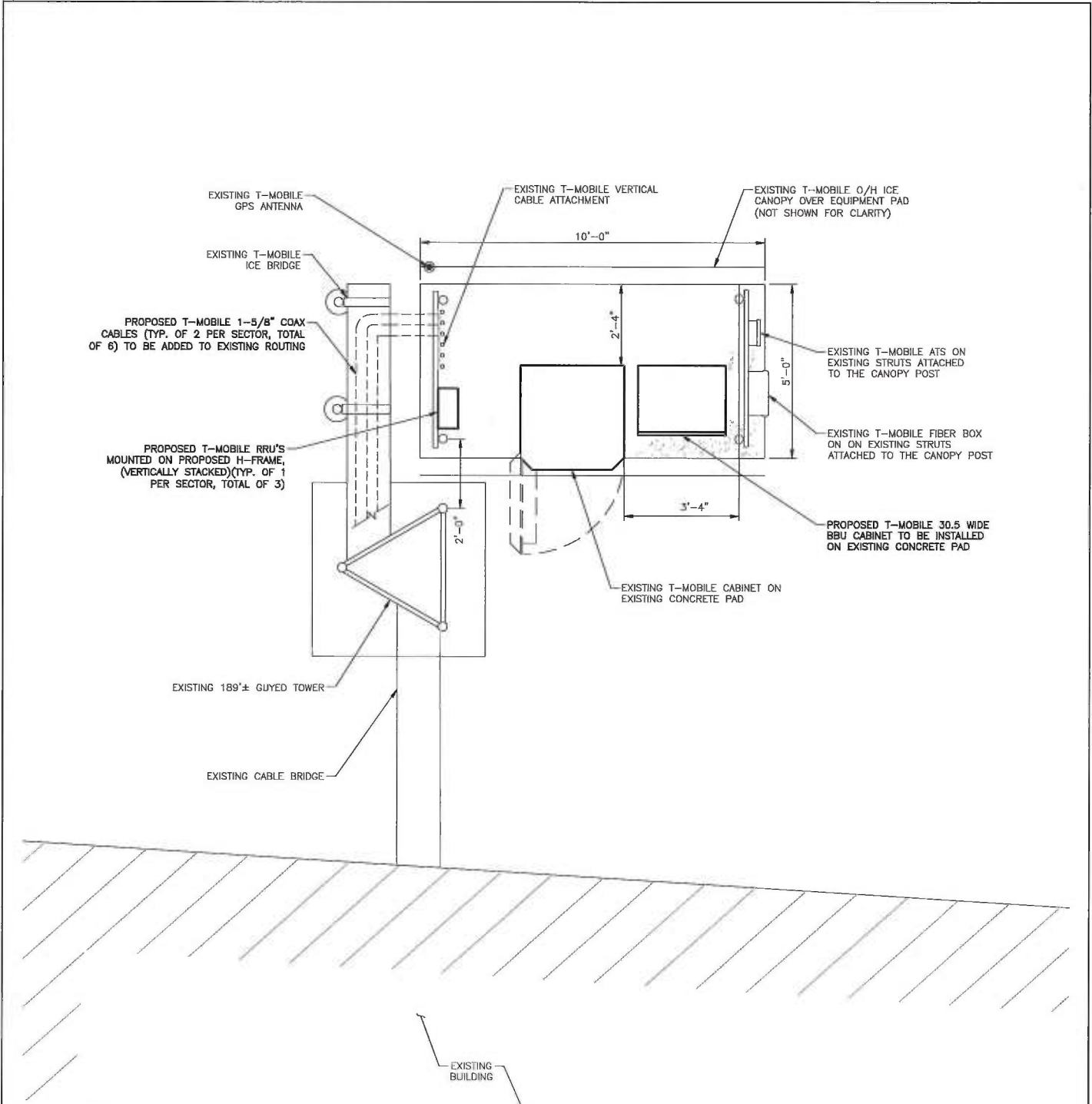
CLIENT:
 T-Mobile Northeast, LLC
 35 GRIFFIN ROAD SOUTH
 BLOOMFIELD, CT 06002
 860.892.7100

SITE INFO:
 KILLINGLY/MARGARET
 HENR1
 CT11156A
 818 PROVIDENCE PIKE
 KILLINGLY, CT 06239

| SUBMITTALS | | | |
|------------|----------|-------------|----|
| NO. | DATE | DESCRIPTION | BY |
| A | 03/11/15 | FOR REVIEW | MK |
| | | | |
| | | | |
| | | | |

DRAWN BY: MK
 CHECKED BY: BB
 DATE: 03/04/15

SHEET NO:
LE-1



CONFIGURATION
704G

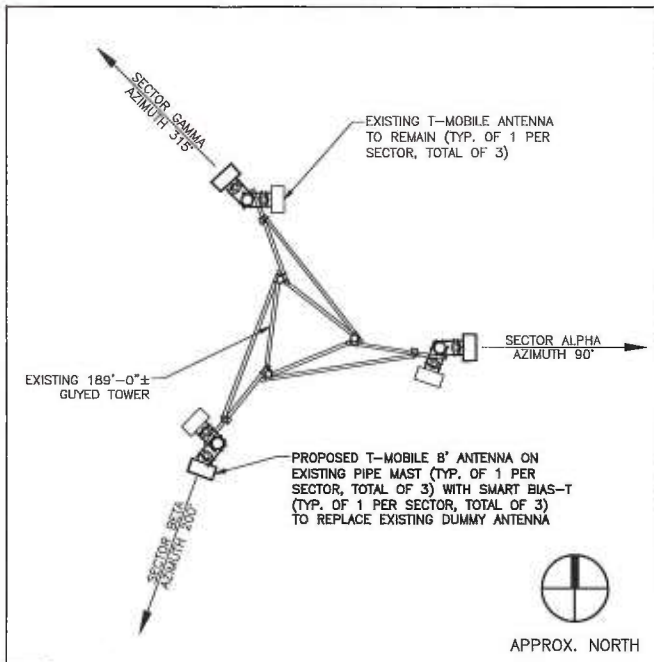


NOTE:
 ALL EQUIPMENT LOCATIONS ARE APPROXIMATE AND ARE SUBJECT TO APPROVAL BY LESSEE/LICENSEE STRUCTURAL AND RF ENGINEERS.

EQUIPMENT PLAN

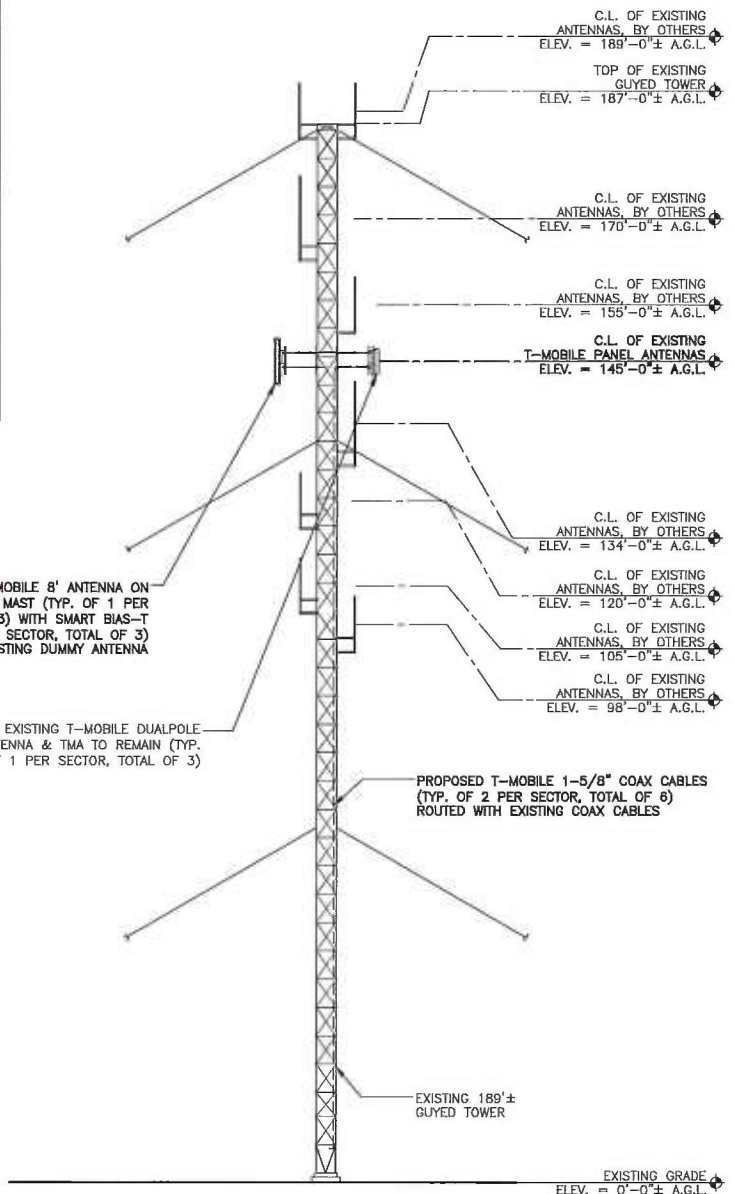
SCALE: 1/4" = 1'-0"

| | | | | | | | | |
|--|---|---|------------|------|-------------|----------|-------------|-----------|
| PREPARED BY: 21 B Street Burlington, MA 01803 Tel: (781) 273-2500 Fax: (781) 273-3311 www.ebiconsulting.com EBI JOB NO.: B115000099 | CLIENT: T-Mobile Northeast, LLC 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 860.892.7100 | SITE INFO: KILLINGLY/MARGARET HENR1 CT11156A 818 PROVIDENCE PIKE KILLINGLY, CT 06239 | SUBMITTALS | | | | DRAWN BY: | SHEET NO: |
| | | | NO. | DATE | DESCRIPTION | BY | MK | |
| | A | 03/11/15 | FOR REVIEW | MK | | BB | LE-1 | |
| | | | | | DATE: | 03/04/15 | | |



ANTENNA CONFIGURATION

NTS



TOWER ELEVATION

SCALE: 1/32" = 1'-0"

CONFIGURATION
704G

NOTE:
ALL EQUIPMENT LOCATIONS ARE APPROXIMATE AND ARE SUBJECT TO APPROVAL BY LESSEE/LICENSEE STRUCTURAL AND RF ENGINEERS.

PREPARED BY:
EBC Consulting
environmental engineering | due diligence
21 B Street | Burlington, MA 01803
Tel: (781) 273-2500 | Fax: (781) 273-3311
www.ebiconsulting.com
EBC JOB NO.:
8115000099

CLIENT:
T-Mobile Northeast, LLC
35 GRIFFIN ROAD SOUTH
BLOOMFIELD, CT 06002
860.692.7100

SITE INFO:
KILLINGLY/MARGARET
HENR1
CT11156A
818 PROVIDENCE PIKE
KILLINGLY, CT 06239

| SUBMITTALS | | | |
|------------|----------|-------------|----|
| NO. | DATE | DESCRIPTION | BY |
| A | 03/11/15 | FOR REVIEW | MK |
| | | | |
| | | | |
| | | | |

DRAWN BY: MK
CHECKED BY: BB
DATE: 03/04/15

SHEET NO:
LE-2

EXHIBIT B

STRUCTURAL ANALYSIS REPORT

March 31, 2015

T-Mobile, USA
35 Griffin Rd
South Bloomfield, CT 06002

Subject: Site #: CT 11156 A
 EBI Reference #: 8115000099
 Site Name: Killingly / Margaret Henr1
 Address: 818 Providence Pike, Killingly, CT 06239

Dear Client:

In accordance with your request, EBI Consulting's structural engineers have prepared this structural analysis report for the 190' guyed tower for supporting the additional loads imposed by the proposed T-Mobile antenna, remote radio units, smart bias-t's, and related equipment cables, to be installed at the locations specified in the Construction Drawings accompanying this analysis. This analysis is in accordance with the following design codes governing this project:

- International Building Code, 2003 with CT 2005, 2009, 2011, and 2013 amendments
- ASCE 7-05
- AISC Steel Construction Manual, 13th Edition
- ANSI/TIA-222-F

The following sources of information were considered in preparing this analysis:

- Photographs taken by EBI personnel on a site visit on February 18, 2015
- Verizon Structural Analysis Report prepared by Centek Engineering, dated December 6, 2013
- Construction drawings prepared by ArcNet Architects, Inc., dated October 14, 1997

The tower was analyzed using ANSI/TIA-222-F for a wind speed of 85 mph without ice and with 1/2" radial ice at a reduced wind speed of 74 mph.

The analysis provided by EBI Engineering includes the following existing and proposed appurtenances, distributed among three sectors where applicable. For this analysis to be valid, a substantial amount of existing equipment must be removed, prior to installation of proposed equipment. The landlord has confirmed that the referenced equipment can and will be removed. Additionally, the tower modifications specified in the Verizon Wireless structural analysis report must be in place prior to T-Mobile's proposed equipment adjustments.

Table 1 - Proposed Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
|---------------------|----------------------------|--------------------|----------------------|-----------------------------|----------------------|---------------------|
| 145.0 | 145.0 | 3 | Commscope | LNX-6515DS-VTM W/ Mast Pipe | 6** | 1-5/8 |
| | 145 | 3 | - | Smart Bias-T | | |
| 0 | 0 | 3 | - | RRUS11-B12 | | |

**Note= (6) Proposed 1-5/8" coax to be stacked on (6) existing 1-1/4" coax for a total of (2) rows of (6) coax each

Table 2 - Existing and Reserved Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
|---------------------|----------------------------|--------------------|----------------------|------------------------------|----------------------|---------------------|
| 189.0 | 194.0 | 2* | - | 10' Omni Antenna* | 3* | 7/8* |
| | | 1* | - | 10' Dipole Antenna* | | |
| | 189.0 | 3* | - | 2' Side Mount Standoff* | | |
| 187.0 | 187.0 | 6 | - | BXA-171063-12CF W/ Mast Pipe | 2 | 1-5/8 |
| | | 6 | - | BXA-70063-6CF W/ Mast Pipe | | |
| | | 1 | - | DB-T1-6Z-8AB-0Z | | |
| | | 3 | - | RRH2x40-07-U | | |
| | | 3 | - | RRH2x40-AWS | | |
| | | 3 | - | PiRod 12' PCS T-Frame | | |
| 185.0 | 185.0 | 1* | - | 6' Dipole Antenna* | 1* | 7/8* |
| 161.0 | 168.5 | 1* | - | 15' Dipole Antenna* | 1* | 1-1/4* |
| | 161.0 | 1* | - | 2' Side Mount Standoff* | | |

| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
|---------------------|----------------------------|--------------------|----------------------|----------------------------|----------------------|---------------------|
| | 156.0 | 1* | - | 10' Omni Antenna* | 1* | 1/2* |
| 160.0 | 160.0 | 1* | - | 10' Dipole Antenna* | 1* | 7/8* |
| 156.5 | 156.5 | 1* | - | 6' Dipole Antenna* | 1* | 7/8* |
| 149.0 | 149.0 | 2* | - | 2' Side Mount Standoff* | 2* | 1/2* |
| | | 2* | - | 10' Dipole Antenna* | | |
| 145.0 | 145.0 | 3 | - | ROHN 4-ft Side Arm | 6 | 1-1/4 |
| | | 3 | - | RR90-17-02DP W/ Mast Pipe | | |
| | | 3* | - | RR90-17-02DP W/ Mast Pipe* | | |
| | | 3 | - | D B2 TMA | | |
| | | 3* | - | D B2 TMA* | | |
| 142.0 | 147.0 | 1* | - | 10' Omni Antenna* | 1* | 7/8* |
| 136.0 | 136.0 | 1* | - | 2' Side Mount Standoff* | 1* | 7/8* |
| | 123.5 | 1* | - | 25' Dipole Antenna* | | |
| 120.0 | 120.0 | 2 | - | US Army MARS | 2 | 1/2 |
| 117.0 | 129.5 | 1* | - | 25' Omni Antenna* | 1* | 7/8* |
| | 117.0 | 1* | - | 2' Side Mount Standoff* | | |
| 110.0 | 110.0 | 1* | - | 10' Sector Frame* | 1* | 7/8* |
| | 97.5 | 1* | - | 25' Dipole Antenna* | | |
| 106.0 | 106.0 | 1* | - | 10' Dipole Antenna* | 1* | 1/2* |
| 90.0 | 102.5 | 1* | - | 25' Omni Antenna* | 1* | 1/2* |

| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
|---------------------|----------------------------|--------------------|----------------------|-------------------------|----------------------|---------------------|
| | 90.0 | 1* | - | 3' Side Mount Standoff* | | |
| 85.0 | 85.0 | 2 | - | US Army MARS | 2 | 1/2 |
| 80.0 | 80.0 | 1* | - | 3' Yagi* | 1* | 1/2* |
| 68.0 | 68.0 | 1* | - | 3' Side Mount Standoff* | 1* | 1/2* |
| | | 1* | - | 10' Dipole Antenna* | | |

NOTES:

* = Existing antennas / mounts/ equipment to be removed prior to installation of proposed equipment

Bold = Existing Antennas/ mounts/ equipment to remain

Summary of Results: (Refer to attached TNX Tower Analysis for detailed analysis results)

Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|----------------|----------------|----------------|------------------|-----------|--------------------------|------------|-----------|
| T1 | 190.6 - 175.35 | Leg | ROHN 2.5 X-STR | 1 | -14927.60 | 66498.57 | 22.4 | Pass |
| T2 | 175.35 - 160.1 | Leg | ROHN 2.5 X-STR | 29 | -13270.70 | 66498.57 | 20.0 | Pass |
| T3 | 160.1 - 140.1 | Leg | ROHN 2 STD | 56 | -34169.80 | 37604.33 | 90.9 | Pass |
| T4 | 140.1 - 120.1 | Leg | ROHN 2 STD | 113 | -36462.60 | 37555.67 | 97.1 | Pass |
| T5 | 120.1 - 100.1 | Leg | ROHN 2 STD | 170 | -28353.30 | 37537.54 | 75.5 | Pass |
| T6 | 100.1 - 80.1 | Leg | ROHN 2 STD | 228 | -33345.10 | 37531.28 | 88.8 | Pass |
| T7 | 80.1 - 60.1 | Leg | ROHN 2 X-STR | 285 | -31342.50 | 51431.54 | 60.9 | Pass |
| T8 | 60.1 - 40.1 | Leg | ROHN 2.5 STD | 342 | -34332.30 | 51062.96 | 67.2 | Pass |
| T9 | 40.1 - 20.1 | Leg | ROHN 2.5 STD | 375 | -32375.20 | 51062.96 | 63.4 | Pass |
| T10 | 20.1 - 4.85 | Leg | ROHN 2.5 STD | 406 | -29043.90 | 50903.13 | 57.1 | Pass |
| T11 | 4.85 - 0 | Leg | ROHN 2.5 X-STR | 433 | -30985.10 | 82667.32 | 37.5 | Pass |
| T1 | 190.6 - 175.35 | Diagonal | P1.5x.058 | 25 | -2360.27 | 5298.14 | 44.5 | Pass |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|----------------|----------------|-----------|------------------|----------|--------------------------|------------|-----------|
| | | | | | | | 64.3 (b) | |
| T2 | 175.35 - 160.1 | Diagonal | P1.5x.058 | 38 | -1934.84 | 5298.14 | 36.5 | Pass |
| | | | | | | | 51.9 (b) | |
| T3 | 160.1 - 140.1 | Diagonal | P1.5x.058 | 65 | -2121.40 | 5242.38 | 40.5 | Pass |
| | | | | | | | 54.6 (b) | |
| T4 | 140.1 - 120.1 | Diagonal | P1.5x.058 | 167 | -1506.92 | 5242.38 | 28.7 | Pass |
| | | | | | | | 33.0 (b) | |
| T5 | 120.1 - 100.1 | Diagonal | P1.5x.058 | 225 | -751.60 | 5242.38 | 14.3 | Pass |
| T6 | 100.1 - 80.1 | Diagonal | P1.5x.058 | 252 | -1210.82 | 5242.38 | 23.1 | Pass |
| | | | | | | | 29.6 (b) | |
| T7 | 80.1 - 60.1 | Diagonal | P1.5x.058 | 335 | -767.56 | 5242.38 | 14.6 | Pass |
| T8 | 60.1 - 40.1 | Diagonal | P1.5x.058 | 350 | -1721.11 | 5309.43 | 32.4 | Pass |
| | | | | | | | 38.8 (b) | |
| T9 | 40.1 - 20.1 | Diagonal | P1.5x.058 | 404 | -1533.48 | 5309.43 | 28.9 | Pass |
| | | | | | | | 36.2 (b) | |
| T10 | 20.1 - 4.85 | Diagonal | P1.5x.058 | 417 | 1089.13 | 8826.21 | 12.3 | Pass |
| | | | | | | | 29.8 (b) | |
| T2 | 175.35 - 160.1 | Top Girt | P1.5x.058 | 32 | -349.77 | 6191.77 | 5.6 | Pass |
| | | | | | | | 9.4 (b) | |
| T3 | 160.1 - 140.1 | Top Girt | P1.5x.058 | 60 | 305.48 | 8826.21 | 3.5 | Pass |
| | | | | | | | 8.4 (b) | |
| T4 | 140.1 - 120.1 | Top Girt | P1.5x.058 | 116 | -2484.63 | 6142.88 | 40.4 | Pass |
| | | | | | | | 65.4 (b) | |
| T5 | 120.1 - 100.1 | Top Girt | P1.5x.058 | 172 | 346.80 | 8826.21 | 3.9 | Pass |
| | | | | | | | 9.5 (b) | |
| T6 | 100.1 - 80.1 | Top Girt | P1.5x.058 | 229 | 296.10 | 8826.21 | 3.4 | Pass |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|----------------|----------------|-----------|------------------|---------|--------------------------|------------|-----------|
| | | | | | | | 8.1 (b) | |
| T7 | 80.1 - 60.1 | Top Girt | P1.5x.058 | 287 | 393.71 | 8826.21 | 4.5 | Pass |
| | | | | | | | 10.8 (b) | |
| T8 | 60.1 - 40.1 | Top Girt | P1.5x.058 | 345 | 242.68 | 8826.21 | 2.7 | Pass |
| | | | | | | | 6.6 (b) | |
| T9 | 40.1 - 20.1 | Top Girt | P1.5x.058 | 377 | -370.90 | 6191.77 | 6.0 | Pass |
| | | | | | | | 13.6 (b) | |
| T10 | 20.1 - 4.85 | Top Girt | P1.5x.058 | 410 | 240.53 | 8826.21 | 2.7 | Pass |
| | | | | | | | 6.6 (b) | |
| T11 | 4.85 - 0 | Top Girt | 14x3/16 | 436 | 2777.82 | 75581.10 | 3.7 | Pass |
| T1 | 190.6 - 175.35 | Bottom Girt | P1.5x.058 | 9 | -275.32 | 6191.77 | 4.4 | Pass |
| | | | | | | | 8.8 (b) | |
| T2 | 175.35 - 160.1 | Bottom Girt | P1.5x.058 | 34 | -676.24 | 6191.77 | 10.9 | Pass |
| | | | | | | | 20.7 (b) | |
| T3 | 160.1 - 140.1 | Bottom Girt | P1.5x.058 | 61 | 2465.94 | 8826.21 | 27.9 | Pass |
| | | | | | | | 67.5 (b) | |
| T4 | 140.1 - 120.1 | Bottom Girt | P1.5x.058 | 119 | 272.75 | 8826.21 | 3.1 | Pass |
| | | | | | | | 7.5 (b) | |
| T5 | 120.1 - 100.1 | Bottom Girt | P1.5x.058 | 176 | 366.25 | 8826.21 | 4.1 | Pass |
| | | | | | | | 10.0 (b) | |
| T6 | 100.1 - 80.1 | Bottom Girt | P1.5x.058 | 233 | 449.27 | 8826.21 | 5.1 | Pass |
| | | | | | | | 12.3 (b) | |
| T7 | 80.1 - 60.1 | Bottom Girt | P1.5x.058 | 289 | 324.51 | 8826.21 | 3.7 | Pass |
| | | | | | | | 8.9 (b) | |
| T8 | 60.1 - 40.1 | Bottom Girt | P1.5x.058 | 347 | 628.51 | 8826.21 | 7.1 | Pass |
| | | | | | | | 17.2 (b) | |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail | |
|-------------|----------------|--------------------------|-----------|------------------|----------|--------------------------|------------|-----------|------|
| T9 | 40.1 - 20.1 | Bottom Girt | P1.5x.058 | 380 | 256.94 | 8826.21 | 2.9 | Pass | |
| | | | | | | | 7.0 (b) | | |
| T10 | 20.1 - 4.85 | Bottom Girt | P1.5x.058 | 412 | 3939.21 | 8826.21 | 44.6 | Pass | |
| | | | | | | | 71.7 (b) | | |
| T11 | 4.85 - 0 | Bottom Girt | 14x3/16 | 439 | -869.28 | 63486.65 | 7.7 | Pass | |
| T11 | 4.85 - 0 | Mid Girt | 14x3/16 | 443 | -154.89 | 9245.91 | 1.7 | Pass | |
| T1 | 190.6 - 175.35 | Guy A@189.985 | 1/2 | 450 | 12266.50 | 13450.00 | 91.2 | Pass | |
| T4 | 140.1 - 120.1 | Guy A@139.485 | 1/2 | 460 | 10750.80 | 13450.00 | 79.9 | Pass | |
| T6 | 100.1 - 80.1 | Guy A@87.3695 | 7/16 | 468 | 7193.11 | 10400.00 | 69.2 | Pass | |
| T8 | 60.1 - 40.1 | Guy A@44.9464 | 3/8 | 474 | 4915.99 | 7700.00 | 63.8 | Pass | |
| T1 | 190.6 - 175.35 | Guy B@189.985 | 1/2 | 449 | 12399.20 | 13450.00 | 92.2 | Pass | |
| T4 | 140.1 - 120.1 | Guy B@139.485 | 1/2 | 455 | 10798.80 | 13450.00 | 80.3 | Pass | |
| T6 | 100.1 - 80.1 | Guy B@87.3695 | 7/16 | 467 | 7350.41 | 10400.00 | 70.7 | Pass | |
| T8 | 60.1 - 40.1 | Guy B@44.9464 | 3/8 | 473 | 4980.93 | 7700.00 | 64.7 | Pass | |
| T1 | 190.6 - 175.35 | Guy C@189.985 | 1/2 | 448 | 12356.70 | 13450.00 | 91.9 | Pass | |
| T4 | 140.1 - 120.1 | Guy C@139.485 | 1/2 | 451 | 10627.90 | 13450.00 | 79.0 | Pass | |
| T6 | 100.1 - 80.1 | Guy C@87.3695 | 7/16 | 463 | 7293.25 | 10400.00 | 70.1 | Pass | |
| T8 | 60.1 - 40.1 | Guy C@44.9464 | 3/8 | 469 | 4884.91 | 7700.00 | 63.4 | Pass | |
| T1 | 190.6 - 175.35 | Top Guy Pull-Off@189.985 | 4 1/2x3/8 | 4 | 3362.80 | 48587.85 | 7.2 | Pass | |
| T6 | 100.1 - 80.1 | Top Guy Pull-Off@87.3695 | C4x5.4 | 464 | 2738.20 | 45780.55 | 6.3 | Pass | |
| T8 | 60.1 - 40.1 | Top Guy Pull-Off@44.9464 | C4x5.4 | 470 | 2492.47 | 45780.55 | 5.7 | Pass | |
| T4 | 140.1 - 120.1 | Torque Arm Top@139.485 | C10x15.3 | 457 | -2605.30 | 76183.08 | 97.8 | Pass | |
| | | | | | | | Summary | | |
| | | | | | | | Leg (T4) | 97.1 | Pass |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|--------------|----------------|------|------------------|------|--------------------------|-------------|-------------|
| | | | | | | Diagonal (T1) | 64.3 | Pass |
| | | | | | | Top Girt (T4) | 65.4 | Pass |
| | | | | | | Bottom Girt (T10) | 71.7 | Pass |
| | | | | | | Mid Girt (T11) | 1.7 | Pass |
| | | | | | | Guy A (T1) | 91.2 | Pass |
| | | | | | | Guy B (T1) | 92.2 | Pass |
| | | | | | | Guy C (T1) | 91.9 | Pass |
| | | | | | | Top Guy Pull-Off (T1) | 7.2 | Pass |
| | | | | | | Torque Arm Top (T4) | 97.8 | Pass |
| | | | | | | Bolt Checks | 71.7 | Pass |
| | | | | | | RATING = | 97.8 | Pass |

The maximum stress under the proposed conditions and configurations is **97.8%** of the tower capacity, governed by the Torque Arm Top (T4), and is considered adequate.

Foundation:

The foundation reactions are summarized below:

| Reaction | 2013 Analysis Centek 12/6/13 (TIA-222 Rev F) | Current analysis loads (TIA 222 Rev F) | % of existing |
|------------------------------|--|---|---------------|
| Axial | 75 K | 84.5 K | +113% |
| Base Shear | 1K | 0.8 K | +80% |
| Guy Anchor Horizontal, Inner | 8 K | 8.9 K | +111% |
| Guy Anchor Horizontal, Outer | 17 K | 17.7 K | +104% |
| Guy Anchor Uplift, Inner | 7 K | 8.2 K | +117% |
| Guy Anchor Uplift, Outer | 26 K | 27.5 K | +106% |

From Centek's Structural Analysis, dated 12/16/13, it was noted that the existing tower foundation is 2'-0" diameter x 3'-9" long concrete pier (1'-0" of pier above grade) with a 4'-0" x 4'-0" x 1'-3" thick reinforced concrete pad bearing directly on the existing sub grade. The bottom of footing is 4'-0" below grade. The tower reaction from the current analysis exceeded the tower reactions from the prior analysis, **but when reanalyzed, the tower foundation is at 84.9% of the allowable soil bearing capacity and is adequate for new equipment loads listed in this analysis.**

Additionally, guy wire loading is transferred to six existing 7'-0" x 4'-0" x 2'-0" thick concrete anchor support blocks, where the top of concrete block is 8'-0" below the grade. From our analysis, **the outer foundation anchor is at 65.3% of its capacity and the inner foundation anchor is at 32.8% of its capacity. Both inner foundation anchors and outer foundation anchors are adequate for new equipment loads listed in this analysis.**

Limitations and Assumptions:

The report is based on the following:

1. Tower is properly installed and maintained.
2. All members are as specified in the original design documents and are in good condition.
3. All required members are in place.
4. All bolts are in place and are tightly fastened.
5. Tower is in plumb condition.
6. All member protective coatings are in good condition.
7. All tower members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
8. Modifications listed in the previous report have been installed.

EBI is not responsible for any modifications completed prior to or hereafter in which EBI is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing / replacing antennas
- C. Adding coaxial cables

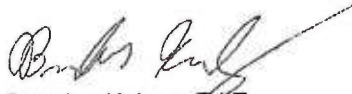
EBI hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and


conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from the original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact EBI. EBI disclaims all liability for representation, recommendation, or conclusion not expressly stated herein.

THE CONCLUSION OF THE TOWER STRUCTURAL ANALYSIS IS THAT THE TOWER IS AT 97.8% CAPACITY FOR THE PROPOSED AND EXISTING LOADING AND IS CONSIDERED ADEQUATE.

Please feel free to contact our office should you have any questions.

Sincerely yours,
EBI Consulting
March 31, 2015


Brandon Kelsey, E.I.T.

 3/31/15
Richard L. Peterman, P.E.
Professional Engineer



Attachment: Photograph Log, Calculations

PHOTOGRAPH LOG

Photo 1:
Existing guy tower.



Photo 2:
T-Mobile existing antennas.



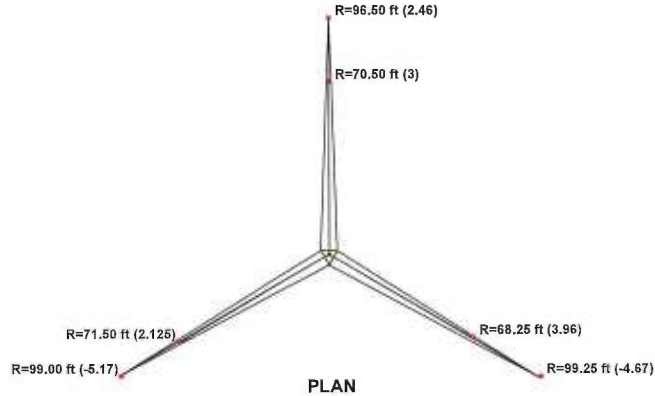
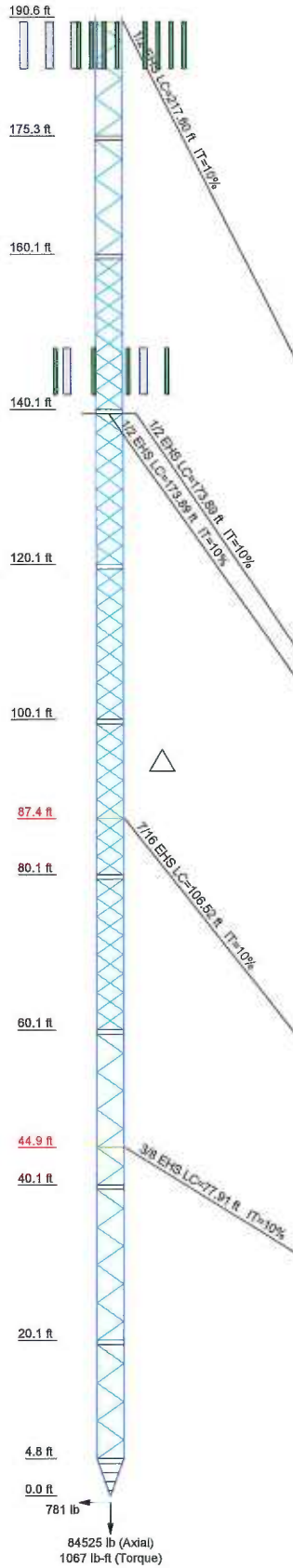
Photo 3:
Existing guy tower base.



STRUCTURAL DESIGN PARAMETERS

| | |
|-------------------------------------|---|
| BUILDING CODE: | 2003 IBC WITH CT 2005, 2009, 2011, and 2013 AMENDMENTS ASCE7-05 TIA- 222-F |
| OCCUPANCY CATEGORY: | II |
| WIND LOADS: | |
| BASIC WIND SPEED (fastest mile), V: | 85 MPH (TIA 222 Rev F) |
| IMPORTANCE FACTOR, I: | 1.0 |
| ICE LOADS: | |
| ICE THICKNESS | 0.5 INCH |
| BASIC WIND SPEED WITH ICE, Vi | 74 MPH |

| | | | | | | | | | | | |
|-------------------|--------|-------------|--------------|-------|--------------|-------|------------|-------|----------------|-------|--------------|
| Section | T11 | T10 | T9 | T8 | T7 | T6 | T5 | T4 | T3 | T2 | T1 |
| Legs | A | | ROHN 2.5 STD | | ROHN 2 X-STR | | ROHN 2 STD | | ROHN 2.5 X-STR | | |
| Leg Grade | | | | | A572-50 | | | | | | |
| Diagonals | N.A. | | | | P1.5x0.058 | | | | | | |
| Diagonal Grade | N.A. | | | | A53-B-42 | | | | | | |
| Top Girts | B | | | | P1.5x0.058 | | | | | | N.A. |
| Mid Girts | B | | | | N.A. | | | | | | |
| Bottom Girts | B | | | | P1.5x0.058 | | | | | | |
| Top Guy Pull-Offs | | | | | N.A. | | | | | | 4 1/2x3/8 |
| Face Width (ft) | | | | | | | | | | | 12 @ 2.43924 |
| # Panels @ (ft) | C | 6 @ 2.43924 | | | | | | | | | 487.8 |
| Weight (lb) | 5117.1 | 396.1 | 467.1 | 513.3 | 591.5 | 476.4 | 419.2 | 747.9 | 418.2 | 437.5 | 487.8 |



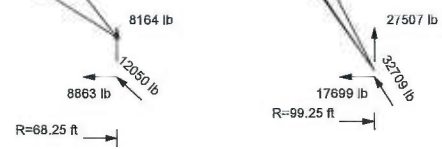
SYMBOL LIST

| MARK | SIZE | MARK | SIZE |
|------|----------------|------|-------------|
| A | ROHN 2.5 X-STR | C | 4 @ 1.17222 |
| B | 14x3/16 | | |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
|---------|--------|--------|----------|--------|--------|
| A572-50 | 50 ksi | 65 ksi | A53-B-42 | 42 ksi | 63 ksi |

- TOWER DESIGN NOTES**
1. Tower is located in Windham County, Connecticut.
 2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 3. Tower is also designed for a 74 mph basic wind with 0.50 in ice.
 4. Deflections are based upon a 60 mph wind.
 5. Weld together tower sections have flange connections.
 6. Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications.
 7. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
 8. Welds are fabricated with ER-70S-6 electrodes.
 9. TOWER RATING: 97.8%



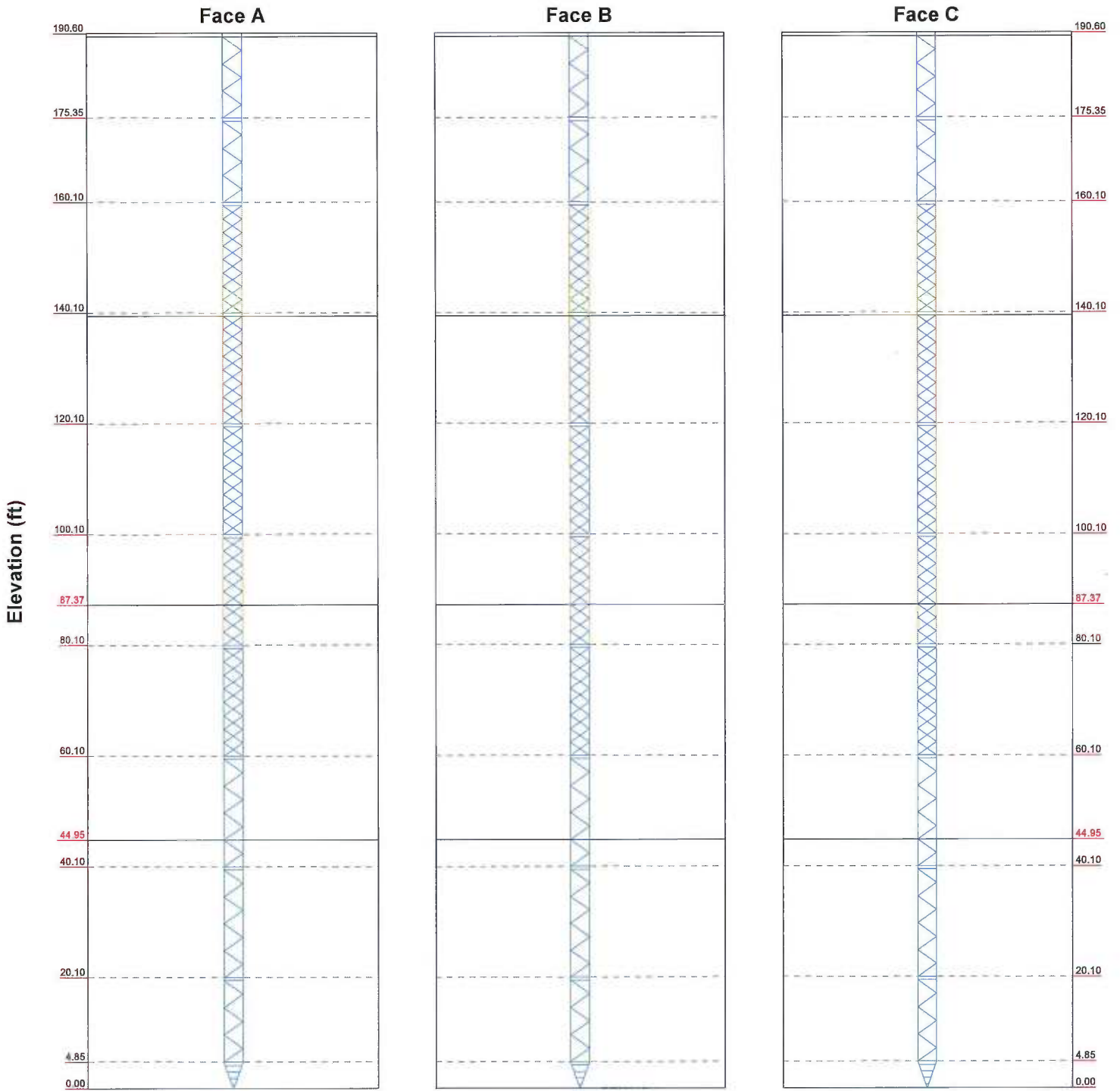
| | | | |
|---|----------------------------|--------------------------|-------------|
| <p>EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141</p> | Job: CT11156A | | |
| | Project: 8115000099 | | |
| | Client: T-Mobile | Drawn by: Kelly Shanahan | App'd: |
| | Code: TIA/EIA-222-F | Date: 03/18/15 | Scale: NTS |
| | Path: | | Dwg No. E-1 |


© Active Projects/T-Mobile CTIA&F/Phase (RGT11156A)/Structure/CT11156A Guy Tower.dwg

Stress Distribution Chart

0' - 190'7-3/16"

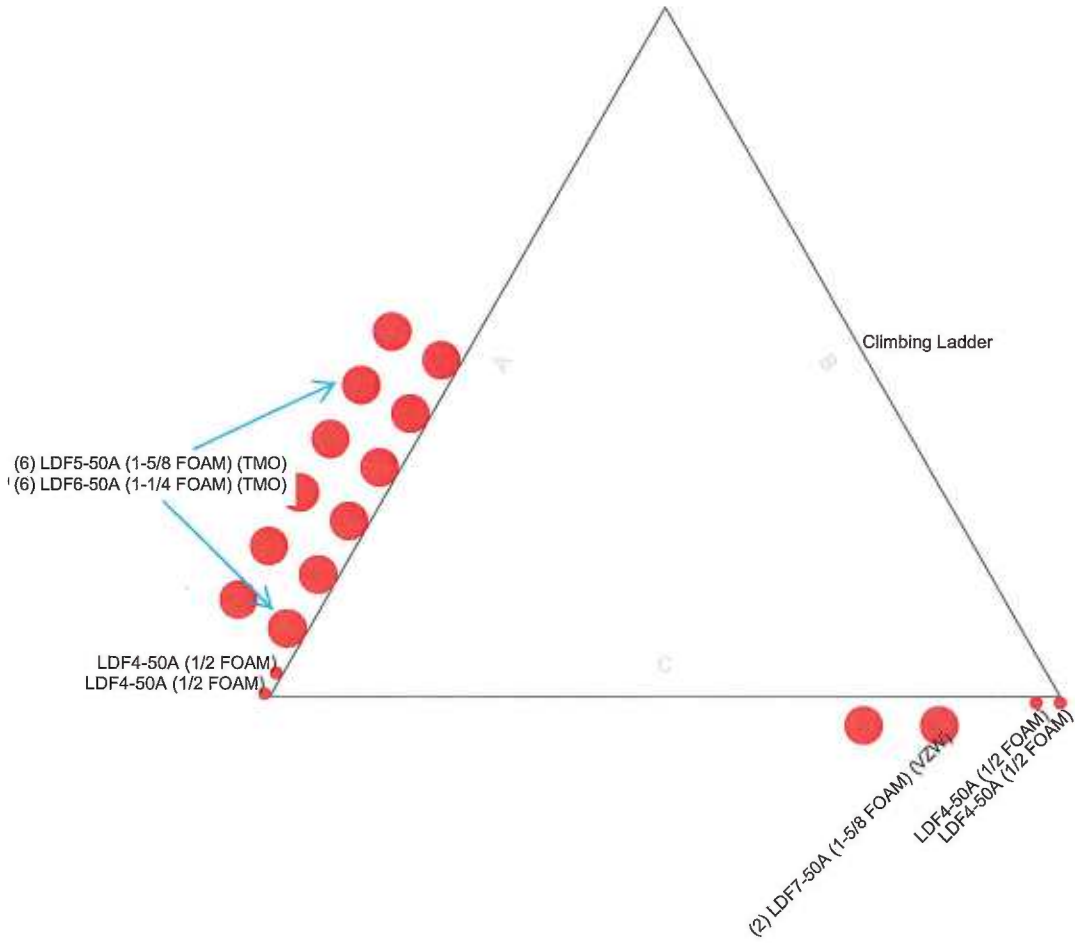
■ > 100%
 ■ 90%-100%
 ■ 75%-90%
 ■ 50%-75%
 ■ < 50% Overstress




| | | | |
|---|---------------------------|--------------------------|------------|
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| | Project: 811500099 | | |
| | Client: T-Mobile | Drawn by: Kelly Shanahan | App'd: |
| | Code: TIA/EIA-222-F | Date: 03/18/15 | Scale: NTS |
| Path: S:\Active Projects\Turnkey T-Mobile CTIA&P\Phase II\CT11156A\Struct\90\CT11156A Guy Tower.dwg | | Dwg No. E-8 | |

Feed Line Plan

_____ Round _____ Flat _____ App In Face _____ App Out Face



| | | | | |
|---|-----------------------|---------------------------|--------------------------|------------|
|  | EBI Consulting | Job: CT11156A | | |
| | 21 B Street | Project: 811500099 | | |
| | Burlington, MA 01803 | Client: T-Mobile | Drawn by: Kelly Shanahan | App'd: |
| | Phone: (781) 425-5100 | Code: TIA/EIA-222-F | Date: 03/18/15 | Scale: NTS |
| | FAX: (781) 425-5141 | Path: | Dwg No. E-7 | |

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| | | | | |
|---|---------|------------|-------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

Tower Input Data

The main tower is a 3x guyed tower with an overall height of 190.60 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 3.46 ft at the top and tapered at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Windham County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 74 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Weld together tower sections have flange connections..

Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications..

Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..

Welds are fabricated with ER-70S-6 electrodes..

Pressures are calculated at each section.

Safety factor used in guy design is 2.

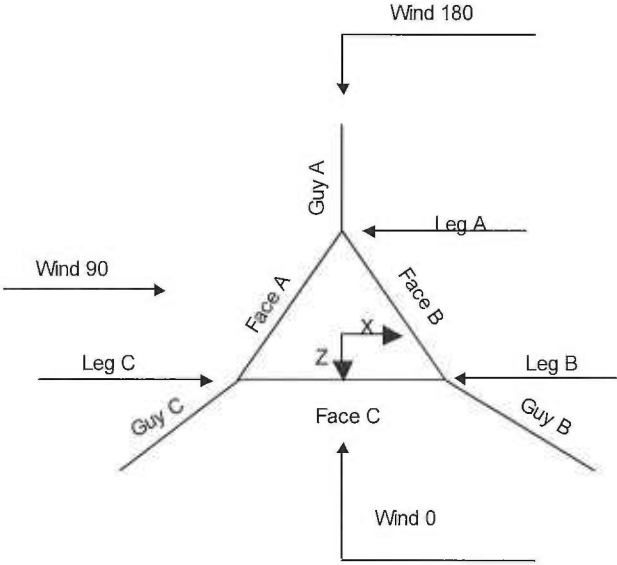
Stress ratio used in tower member design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

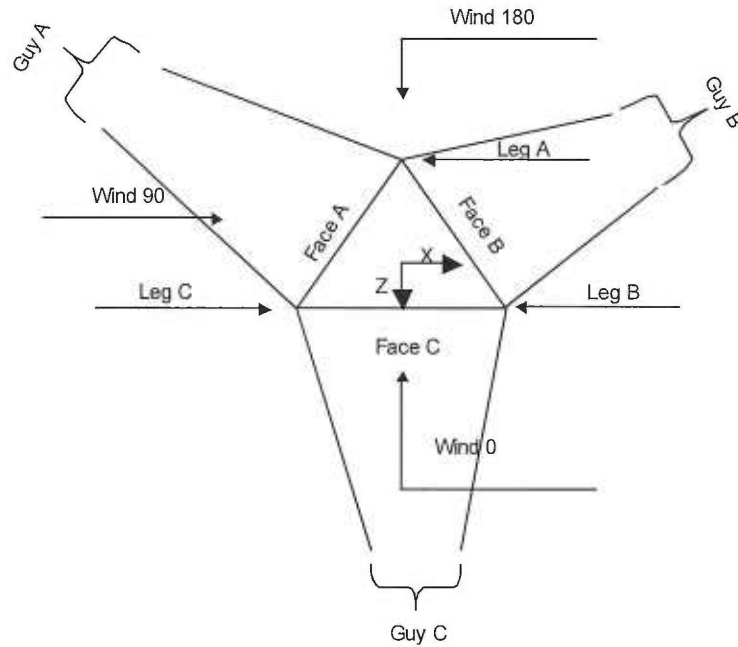
| | | |
|--|---|---|
| <ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination | <ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r √ Retension Guys To Initial Tension Bypass Mast Stability Checks √ Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. √ Autocalc Torque Arm Areas √ SR Members Have Cut Ends √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption | <ul style="list-style-type: none"> Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA √ SR Leg Bolts Resist Compression √ All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feedline Torque √ Include Angle Block Shear Check <li style="padding-left: 40px;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets |
|--|---|---|

| | | |
|---|------------------------------|--------------------------------------|
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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |



Corner & Starmount Guyed Tower

| | | |
|---|------------------------------|--------------------------------------|
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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |



Face Guyed

Tower Section Geometry

| Tower Section | Tower Elevation | Assembly Database | Description | Section Width | Number of Sections | Section Length |
|---------------|-----------------|-------------------|-------------|---------------|--------------------|----------------|
| | <i>ft</i> | | | <i>ft</i> | | <i>ft</i> |
| T1 | 190.60-175.35 | | | 3.46 | 1 | 15.25 |
| T2 | 175.35-160.10 | | | 3.46 | 1 | 15.25 |
| T3 | 160.10-140.10 | | | 3.46 | 1 | 20.00 |
| T4 | 140.10-120.10 | | | 3.46 | 1 | 20.00 |
| T5 | 120.10-100.10 | | | 3.46 | 1 | 20.00 |
| T6 | 100.10-80.10 | | | 3.46 | 1 | 20.00 |
| T7 | 80.10-60.10 | | | 3.46 | 1 | 20.00 |
| T8 | 60.10-40.10 | | | 3.46 | 1 | 20.00 |
| T9 | 40.10-20.10 | | | 3.46 | 1 | 20.00 |
| T10 | 20.10-4.85 | | | 3.46 | 1 | 15.25 |
| T11 | 4.85-0.00 | | | 3.46 | 1 | 4.85 |

Tower Section Geometry (cont'd)

| | | | | |
|---|---------|------------|-------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 4 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Tower Section | Tower Elevation | Diagonal Spacing | Bracing Type | Has K Brace End Panels | Has Horizontals | Top Girt Offset | Bottom Girt Offset |
|---------------|-----------------|------------------|--------------|------------------------|-----------------|-----------------|--------------------|
| | ft | ft | | | | in | in |
| T1 | 190.60-175.35 | 2.44 | K Brace Left | No | Yes | 7.3750 | 0.0000 |
| T2 | 175.35-160.10 | 2.44 | K Brace Left | No | Yes | 7.3750 | 0.0000 |
| T3 | 160.10-140.10 | 2.42 | CX Brace | No | Yes | 7.3750 | 0.0000 |
| T4 | 140.10-120.10 | 2.42 | CX Brace | No | Yes | 7.3750 | 0.0000 |
| T5 | 120.10-100.10 | 2.42 | CX Brace | No | Yes | 7.3750 | 0.0000 |
| T6 | 100.10-80.10 | 2.42 | CX Brace | No | Yes | 7.3750 | 0.0000 |
| T7 | 80.10-60.10 | 2.42 | CX Brace | No | Yes | 7.3750 | 0.0000 |
| T8 | 60.10-40.10 | 2.42 | K Brace Left | No | Yes | 7.3750 | 0.0000 |
| T9 | 40.10-20.10 | 2.42 | K Brace Left | No | Yes | 7.3750 | 0.0000 |
| T10 | 20.10-4.85 | 2.44 | K Brace Left | No | Yes | 7.3750 | 0.0000 |
| T11 | 4.85-0.00 | 1.17 | X Brace | No | Yes | 8.0000 | 8.0000 |

Tower Section Geometry (cont'd)

| Tower Elevation | Leg Type | Leg Size | Leg Grade | Diagonal Type | Diagonal Size | Diagonal Grade |
|------------------|----------|----------------|------------------|---------------|---------------|-------------------|
| ft | | | | | | |
| T1 190.60-175.35 | Pipe | ROHN 2.5 X-STR | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T2 175.35-160.10 | Pipe | ROHN 2.5 X-STR | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T3 160.10-140.10 | Pipe | ROHN 2 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T4 140.10-120.10 | Pipe | ROHN 2 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T5 120.10-100.10 | Pipe | ROHN 2 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T6 100.10-80.10 | Pipe | ROHN 2 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T7 80.10-60.10 | Pipe | ROHN 2 X-STR | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T8 60.10-40.10 | Pipe | ROHN 2.5 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T9 40.10-20.10 | Pipe | ROHN 2.5 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T10 20.10-4.85 | Pipe | ROHN 2.5 STD | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T11 4.85-0.00 | Pipe | ROHN 2.5 X-STR | A572-50 (50 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |

Tower Section Geometry (cont'd)

| Tower Elevation | Top Girt Type | Top Girt Size | Top Girt Grade | Bottom Girt Type | Bottom Girt Size | Bottom Girt Grade |
|------------------|---------------|---------------|-------------------|------------------|------------------|-------------------|
| ft | | | | | | |
| T1 190.60-175.35 | Pipe | P1.5x.058 | A53-B-42 (42 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T2 175.35-160.10 | Pipe | P1.5x.058 | A53-B-42 (42 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T3 160.10-140.10 | Pipe | P1.5x.058 | A53-B-42 (42 ksi) | Pipe | P1.5x.058 | A53-B-42 (42 ksi) |
| T4 140.10-120.10 | Pipe | P1.5x.058 | A53-B-42 | Pipe | P1.5x.058 | A53-B-42 |

| | | | | |
|---|----------------|------------|--------------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Tower Elevation ft | Top Girt Type | Top Girt Size | Top Girt Grade | Bottom Girt Type | Bottom Girt Size | Bottom Girt Grade |
|-----------------------|---------------|---------------|----------------------|------------------|------------------|---|
| T5 120.10-100.10 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T6 100.10-80.10 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T7 80.10-60.10 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T8 60.10-40.10 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T9 40.10-20.10 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T10 20.10-4.85 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 | Pipe | P1.5x.058 | (42 ksi) A53-B-42 |
| T11 4.85-0.00 | Flat Bar | 14x3/16 | A36 (36 ksi) | Flat Bar | 14x3/16 | 42 ksi modified for bearing on pipes A36 (36 ksi) |

Tower Section Geometry (cont'd)

| Tower Elevation ft | No. of Mid Girts | Mid Girt Type | Mid Girt Size | Mid Girt Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
|-----------------------|------------------|---------------|---------------|-----------------|-----------------|-----------------|---------------------|
| T11 4.85-0.00 | 2 | Flat Bar | 14x3/16 | A36 (36 ksi) | Solid Round | | A572-50 (50 ksi) |

Tower Section Geometry (cont'd)

| Tower Elevation ft | Gusset Area (per face) ft ² | Gusset Thickness in | Gusset Grade | Adjust. Factor A _f | Adjust. Factor A _r | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in |
|-----------------------|--|------------------------|-----------------|----------------------------------|----------------------------------|--------------|---|---|
| T1 190.60-175.35 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T2 175.35-160.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T3 160.10-140.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T4 140.10-120.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T5 120.10-100.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T6 100.10-80.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T7 80.10-60.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T8 60.10-40.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |
| T9 40.10-20.10 | 0.00 | 0.0000 | A36 (36 ksi) | 1 | 1 | 1 | 36.0000 | 36.0000 |

| | | |
|---|------------------------------|--------------------------------------|
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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Tower Elevation ft | Leg | | Diagonal | | Top Girt | | Bottom Girt | | Mid Girt | | Long Horizontal | | Short Horizontal | |
|-----------------------|---------------------------|---|---------------------------|------|---------------------------|------|------------------------------|------|------------------------------|------|------------------------------|------|------------------------------|------|
| | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U |
| T3 160.10-140.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T4 140.10-120.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T5 120.10-100.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T6 100.10-80.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T7 80.10-60.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T8 60.10-40.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T9 40.10-20.10 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T10 20.10-4.85 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |
| T11 4.85-0.00 | 0.0000 | 1 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 | 0.0000 | 0.75 |

Tower Section Geometry (cont'd)

| Tower Elevation ft | Connection Offsets | | | | | | | |
|-----------------------|--------------------|---------------|---------------|----------------|--------------|---------------|---------------|----------------|
| | Diagonal | | | | K-Bracing | | | |
| | Vert. Top | Horiz. Top | Vert. Bot. | Horiz. Bot. | Vert. Top | Horiz. Top | Vert. Bot. | Horiz. Bot. |
| in | in | in | in | in | in | in | in | |
| T1 190.60-175.35 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T2 175.35-160.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T3 160.10-140.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T4 140.10-120.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T5 120.10-100.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T6 100.10-80.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T7 80.10-60.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T8 60.10-40.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T9 40.10-20.10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T10 20.10-4.85 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |
| T11 4.85-0.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.2500 | 0.0000 | 3.2500 | 0.0000 |

Tower Section Geometry (cont'd)

| | | |
|---|------------------------------|--------------------------------------|
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| Tower Elevation ft | Leg Connection Type | Leg Bolt Size in | Leg No. | Diagonal | | Top Girt | | Bottom Girt | | Mid Girt | | Long Horizontal | | Short Horizontal | |
|-----------------------|---------------------|------------------|---------|-----------------|-----|-----------------|-----|-----------------|-----|-----------------|-----|-----------------|-----|------------------|-----|
| | | | | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in | No. |
| T1 190.60-175.35 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T2 175.35-160.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T3 160.10-140.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T4 140.10-120.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T5 120.10-100.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T6 100.10-80.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T7 80.10-60.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T8 60.10-40.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T9 40.10-20.10 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T10 20.10-4.85 | Flange | 0.7500 A325N | 4 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.5000 A325N | 1 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |
| T11 4.85-0.00 | Flange | 0.7500 A325N | 0 | 0.0000 A325N | 0 | 0.0000 A325N | 0 | 0.0000 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 | 0.6250 A325N | 0 |

Guy Data

| Guy Elevation ft | Guy Grade | Guy Size | Initial Tension lb | % | Guy Modulus ksi | Guy Weight plf | L_u ft | Anchor Radius ft | Anchor Azimuth Adj. ° | Anchor Elevation ft | End Fitting Efficiency % |
|---------------------|-----------|----------|-----------------------|-----|--------------------|-------------------|-------------|---------------------|--------------------------|------------------------|-----------------------------|
| 189.985 | EHS | A 1/2 | 2690.00 | 10% | 21000 | 0.517 | 209.81 | 96.50 | 0.0000 | 2.46 | 100% |
| | | B 1/2 | 2690.00 | 10% | 21000 | 0.517 | 217.41 | 99.25 | 0.0000 | -4.67 | 100% |
| | | C 1/2 | 2690.00 | 10% | 21000 | 0.517 | 217.75 | 99.00 | 0.0000 | -5.17 | 100% |
| 139.485 | EHS | A 1/2 | 2690.00 | 10% | 21000 | 0.517 | 166.31 | 96.50 | 0.0000 | 2.46 | 100% |
| | | B 1/2 | 2690.00 | 10% | 21000 | 0.517 | 173.74 | 99.25 | 0.0000 | -4.67 | 100% |
| | | C 1/2 | 2690.00 | 10% | 21000 | 0.517 | 174.02 | 99.00 | 0.0000 | -5.17 | 100% |
| 87.3695 | EHS | A 7/16 | 2080.00 | 10% | 21000 | 0.399 | 108.58 | 70.50 | 0.0000 | 3.00 | 100% |
| | | B 7/16 | 2080.00 | 10% | 21000 | 0.399 | 106.43 | 68.25 | 0.0000 | 3.96 | 100% |
| | | C 7/16 | 2080.00 | 10% | 21000 | 0.399 | 109.89 | 71.50 | 0.0000 | 2.13 | 100% |
| 44.9464 | EHS | A 3/8 | 1540.00 | 10% | 21000 | 0.273 | 80.25 | 70.50 | 0.0000 | 3.00 | 100% |
| | | B 3/8 | 1540.00 | 10% | 21000 | 0.273 | 77.83 | 68.25 | 0.0000 | 3.96 | 100% |
| | | C 3/8 | 1540.00 | 10% | 21000 | 0.273 | 81.56 | 71.50 | 0.0000 | 2.13 | 100% |

Guy Data(cont'd)

| Guy Elevation ft | Mount Type | Torque-Arm Spread ft | Torque-Arm Leg Angle | Torque-Arm Style | Torque-Arm Grade | Torque-Arm Type | Torque-Arm Size |
|---------------------|----------------------|-------------------------|----------------------|------------------|------------------|-----------------|-----------------|
| 189.985 139.485 | Corner Torque Arm | 7.17 | 0.0000 | Channel | A36 (36 ksi) | Channel | C10x15.3 |

| | | |
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| Guy Elevation ft | Mount Type | Torque-Arm Spread ft | Torque-Arm Leg Angle ° | Torque-Arm Style | Torque-Arm Grade | Torque-Arm Type | Torque-Arm Size |
|---------------------|------------|-------------------------|---------------------------|------------------|------------------|-----------------|-----------------|
| 87.3695 | Corner | | | | | | |
| 44.9464 | Corner | | | | | | |

Guy Data (cont'd)

| Guy Elevation ft | Diagonal Grade | Diagonal Type | Upper Diagonal Size | Lower Diagonal Size | Is Strap. | Pull-Off Grade | Pull-Off Type | Pull-Off Size |
|---------------------|----------------------|---------------|---------------------|---------------------|-----------|-----------------|---------------|---------------|
| 189.99 | A53-B-42 (42 ksi) | Pipe | | | No | A36 (36 ksi) | Flat Bar | 4 1/2x3/8 |
| 139.49 | A53-B-42 (42 ksi) | Pipe | | | | A36 (36 ksi) | Flat Bar | |
| 87.37 | A242-42 (42 ksi) | Pipe | | | No | A36 (36 ksi) | Channel | C4x5.4 |
| 44.95 | A53-B-42 (42 ksi) | Pipe | | | Yes | A36 (36 ksi) | Channel | C4x5.4 |

Guy Data (cont'd)

| Guy Elevation ft | Cable Weight A lb | Cable Weight B lb | Cable Weight C lb | Cable Weight D lb | Tower Intercept A ft | Tower Intercept B ft | Tower Intercept C ft | Tower Intercept D ft |
|---------------------|-------------------------|-------------------------|-------------------------|-------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| 189.985 | 108.47 | 112.40 | 112.58 | | 4.16 | 4.46 | 4.48 | |
| 139.485 | 85.98 | 89.82 | 89.97 | | 3.5 sec/pulse 2.63 | 3.6 sec/pulse 2.86 | 3.7 sec/pulse 2.87 | |
| 87.3695 | 43.33 | 42.47 | 43.85 | | 2.8 sec/pulse 1.12 | 2.9 sec/pulse 1.08 | 2.9 sec/pulse 1.15 | |
| 44.9464 | 21.91 | 21.25 | 22.27 | | 1.8 sec/pulse 0.57 | 1.8 sec/pulse 0.54 | 1.9 sec/pulse 0.59 | |
| | | | | | 1.3 sec/pulse | 1.3 sec/pulse | 1.3 sec/pulse | |

Guy Data (cont'd)

| Guy Elevation ft | Calc K Single Angles | Calc K Solid Rounds | Torque Arm | | Pull Off | | Diagonal | |
|---------------------|----------------------------|---------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | | | K _x | K _y | K _x | K _y | K _x | K _y |
| 189.985 | No | No | | | 1 | 1 | 1 | 1 |
| 139.485 | Yes | No | 1 | 1 | 1 | 1 | 1 | 1 |
| 87.3695 | No | No | | | 1 | 1 | 1 | 1 |
| 44.9464 | No | No | | | 1 | 1 | 1 | 1 |

Guy Data (cont'd)

| | | |
|---|------------------------------|--------------------------------------|
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| Guy Elevation ft | Torque-Arm | | | | Pull Off | | | | Diagonal | | | |
|------------------------|-----------------|--------|---------------------------|---|-----------------|--------|---------------------------|------|-----------------|--------|---------------------------|------|
| | Bolt Size in | Number | Net Width Deduct in | U | Bolt Size in | Number | Net Width Deduct in | U | Bolt Size in | Number | Net Width Deduct in | U |
| 189.985 | 0.7500 A325N | 8 | 0.0000 | 1 | 0.5000 A325N | 0 | 0.0000 | 0.75 | 0.6250 A325N | 0 | 0.0000 | 0.75 |
| 139.485 | 0.6250 A325N | 0 | 0.0000 | 1 | 0.6250 A325N | 0 | 0.0000 | 0.75 | 0.6250 A325N | 0 | 0.0000 | 0.75 |
| 87.3695 | 0.0000 A325N | 0 | 0.0000 | 1 | 0.6250 A325N | 0 | 0.0000 | 0.75 | 0.6250 A325N | 0 | 0.0000 | 0.75 |
| 44.9464 | 0.0000 A325N | 0 | 0.0000 | 1 | 0.6250 A325N | 0 | 0.0000 | 0.75 | 0.6250 A325N | 0 | 0.0000 | 0.75 |

Guy Pressures

| Guy Elevation ft | Guy Location | z ft | q _z psf | q _z Ice psf | Ice Thickness in |
|------------------------|-----------------|---------|-----------------------|------------------------------|------------------------|
| 189.985 | A | 96.22 | 25 | 19 | 0.5000 |
| | B | 92.66 | 25 | 19 | 0.5000 |
| | C | 92.41 | 25 | 19 | 0.5000 |
| 139.485 | A | 70.97 | 23 | 17 | 0.5000 |
| | B | 67.41 | 23 | 17 | 0.5000 |
| | C | 67.16 | 23 | 17 | 0.5000 |
| 87.3695 | A | 45.18 | 20 | 15 | 0.5000 |
| | B | 45.66 | 20 | 15 | 0.5000 |
| | C | 44.75 | 20 | 15 | 0.5000 |
| 44.9464 | A | 23.97 | 18 | 14 | 0.5000 |
| | B | 24.45 | 18 | 14 | 0.5000 |
| | C | 23.54 | 18 | 14 | 0.5000 |

Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Face or Leg | Allow Shield | Component Type | Placement ft | Face Offset in | Lateral Offset (Frac FW) | # | # Per Row | Clear Spacing in | Width or Diameter in | Perimeter in | Weight plf |
|---|-------------------|-----------------|-------------------|-----------------|----------------------|--------------------------------|----|-----------------|------------------------|----------------------------|-----------------|---------------|
| LDF7-50A (1-5/8 FOAM) (VZW) | C | Yes | Ar (CfAe) | 8.00 - 187.00 | 0.5000 | -0.3 | 2 | 2 | 1.9800 | 1.9800 | | 0.82 |
| LDF7-50A (1-5/8 FOAM) (TMO)** Climbing Ladder | A | Yes | Ar (CfAe) | 8.00 - 145.00 | 0.0000 | -0.22 | 12 | 6 | 1.2500 1.0000 | 1.9800 | | 0.82 |
| LDF4-50A (1/2 FOAM) | B | Yes | Af (CfAe) | 8.00 - 190.00 | 0.0000 | 0 | 1 | 1 | 0.2500 | 0.0000 | 0.0000 | 7.90 |
| LDF4-50A (1/2 FOAM) | A | Yes | Ar (CfAe) | 8.00 - 85.00 | 0.0000 | -0.47 | 1 | 1 | 0.6300 | 0.6300 | | 0.15 |
| LDF4-50A (1/2 FOAM) | C | Yes | Ar (CfAe) | 8.00 - 85.00 | 0.0000 | -0.47 | 1 | 1 | 0.6300 | 0.6300 | | 0.15 |
| LDF4-50A (1/2 FOAM) | A | Yes | Ar (CfAe) | 8.00 - 120.00 | 0.0000 | -0.5 | 1 | 1 | 0.6300 | 0.6300 | | 0.15 |
| LDF4-50A (1/2 FOAM) | C | Yes | Ar (CfAe) | 8.00 - 120.00 | 0.0000 | -0.5 | 1 | 1 | 0.6300 | 0.6300 | | 0.15 |

**Note: due to software modeling limitations, the proposed (6) 1-5/8" coax to be stacked on top of the (6) existing 1-1/4" coax was input as (12) 1-5/8" coax stacked in (2) rows of (6) coax each.

| | | |
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Feed Line/Linear Appurtenances Section Areas

| Tower Section | Tower Elevation ft | Face | A_R ft ² | A_F ft ² | $C_A A_A$ In Face ft ² | $C_A A_A$ Out Face ft ² | Weight lb |
|---------------|-----------------------|------|--------------------------|--------------------------|---|--|--------------|
| T1 | 190.60-175.35 | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 115.74 |
| | | C | 3.845 | 0.000 | 0.000 | 0.000 | 19.11 |
| T2 | 175.35-160.10 | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 120.47 |
| | | C | 5.032 | 0.000 | 0.000 | 0.000 | 25.01 |
| T3 | 160.10-140.10 | A | 4.851 | 0.000 | 0.000 | 0.000 | 48.22 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 6.600 | 0.000 | 0.000 | 0.000 | 32.80 |
| T4 | 140.10-120.10 | A | 19.800 | 0.000 | 0.000 | 0.000 | 196.80 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 6.600 | 0.000 | 0.000 | 0.000 | 32.80 |
| T5 | 120.10-100.10 | A | 20.845 | 0.000 | 0.000 | 0.000 | 199.79 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 7.645 | 0.000 | 0.000 | 0.000 | 35.78 |
| T6 | 100.10-80.10 | A | 21.107 | 0.000 | 0.000 | 0.000 | 200.54 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 7.907 | 0.000 | 0.000 | 0.000 | 36.53 |
| T7 | 80.10-60.10 | A | 21.900 | 0.000 | 0.000 | 0.000 | 202.80 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 8.700 | 0.000 | 0.000 | 0.000 | 38.80 |
| T8 | 60.10-40.10 | A | 21.900 | 0.000 | 0.000 | 0.000 | 202.80 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 8.700 | 0.000 | 0.000 | 0.000 | 38.80 |
| T9 | 40.10-20.10 | A | 21.900 | 0.000 | 0.000 | 0.000 | 202.80 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 158.00 |
| | | C | 8.700 | 0.000 | 0.000 | 0.000 | 38.80 |
| T10 | 20.10-4.85 | A | 13.249 | 0.000 | 0.000 | 0.000 | 122.69 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 95.59 |
| | | C | 5.263 | 0.000 | 0.000 | 0.000 | 23.47 |
| T11 | 4.85-0.00 | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Section | Tower Elevation ft | Face or Leg | Ice Thickness in | A_R ft ² | A_F ft ² | $C_A A_A$ In Face ft ² | $C_A A_A$ Out Face ft ² | Weight lb |
|---------------|-----------------------|-------------|---------------------|--------------------------|--------------------------|---|--|--------------|
| T1 | 190.60-175.35 | A | 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | | 0.000 | 0.814 | 0.000 | 0.000 | 121.13 |
| | | C | | 5.786 | 0.000 | 0.000 | 0.000 | 54.40 |
| T2 | 175.35-160.10 | A | 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | | 0.000 | 0.847 | 0.000 | 0.000 | 126.09 |
| | | C | | 7.574 | 0.000 | 0.000 | 0.000 | 71.22 |
| T3 | 160.10-140.10 | A | 0.500 | 7.301 | 0.000 | 0.000 | 0.000 | 137.29 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| | | C | | 9.933 | 0.000 | 0.000 | 0.000 | 93.40 |
| T4 | 140.10-120.10 | A | 0.500 | 29.800 | 0.000 | 0.000 | 0.000 | 560.39 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| | | C | | 9.933 | 0.000 | 0.000 | 0.000 | 93.40 |
| T5 | 120.10-100.10 | A | 0.500 | 32.503 | 0.000 | 0.000 | 0.000 | 577.11 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| | | C | | 12.636 | 0.000 | 0.000 | 0.000 | 110.12 |
| T6 | 100.10-80.10 | A | 0.500 | 33.182 | 0.000 | 0.000 | 0.000 | 581.31 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |

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| Tower Section | Tower Elevation ft | Face or Leg | Ice Thickness in | A_R ft^2 | A_F ft^2 | $C_A A_A$ In Face ft^2 | $C_A A_A$ Out Face ft^2 | Weight lb |
|---------------|-----------------------|-------------|---------------------|-----------------|-----------------|--------------------------------|---------------------------------|--------------|
| T7 | 80.10-60.10 | C | | 13.316 | 0.000 | 0.000 | 0.000 | 114.32 |
| | | A | 0.500 | 35.233 | 0.000 | 0.000 | 0.000 | 594.00 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| T8 | 60.10-40.10 | C | | 15.367 | 0.000 | 0.000 | 0.000 | 127.01 |
| | | A | 0.500 | 35.233 | 0.000 | 0.000 | 0.000 | 594.00 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| T9 | 40.10-20.10 | C | | 15.367 | 0.000 | 0.000 | 0.000 | 127.01 |
| | | A | 0.500 | 35.233 | 0.000 | 0.000 | 0.000 | 594.00 |
| | | B | | 0.000 | 1.111 | 0.000 | 0.000 | 165.36 |
| T10 | 20.10-4.85 | C | | 15.367 | 0.000 | 0.000 | 0.000 | 127.01 |
| | | A | 0.500 | 21.316 | 0.000 | 0.000 | 0.000 | 359.37 |
| | | B | | 0.000 | 0.672 | 0.000 | 0.000 | 100.04 |
| T11 | 4.85-0.00 | C | | 9.297 | 0.000 | 0.000 | 0.000 | 76.84 |
| | | A | 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | B | | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| | | C | | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |

Feed Line Shielding

| Section | Elevation ft | Face | A_R ft^2 | A_R Ice ft^2 | A_F ft^2 | A_F Ice ft^2 |
|---------|-----------------|------|-----------------|------------------------|-----------------|------------------------|
| T1 | 190.60-175.35 | A | 0.000 | 0.000 | 0.000 | 0.000 |
| | | B | 0.000 | 0.146 | 0.000 | 0.030 |
| | | C | 0.263 | 0.691 | 0.095 | 0.142 |
| T2 | 175.35-160.10 | A | 0.000 | 0.000 | 0.000 | 0.000 |
| | | B | 0.000 | 0.162 | 0.000 | 0.000 |
| | | C | 0.385 | 0.967 | 0.000 | 0.000 |
| T3 | 160.10-140.10 | A | 0.653 | 1.638 | 0.000 | 0.000 |
| | | B | 0.000 | 0.374 | 0.000 | 0.000 |
| | | C | 0.888 | 2.228 | 0.000 | 0.000 |
| T4 | 140.10-120.10 | A | 2.665 | 6.684 | 0.000 | 0.000 |
| | | B | 0.000 | 0.374 | 0.000 | 0.000 |
| | | C | 0.888 | 2.228 | 0.000 | 0.000 |
| T5 | 120.10-100.10 | A | 2.805 | 7.291 | 0.000 | 0.000 |
| | | B | 0.000 | 0.374 | 0.000 | 0.000 |
| | | C | 1.029 | 2.834 | 0.000 | 0.000 |
| T6 | 100.10-80.10 | A | 2.841 | 7.581 | 0.352 | 0.553 |
| | | B | 0.000 | 0.381 | 0.000 | 0.028 |
| | | C | 1.064 | 3.042 | 0.132 | 0.222 |
| T7 | 80.10-60.10 | A | 2.947 | 7.903 | 0.000 | 0.000 |
| | | B | 0.000 | 0.374 | 0.000 | 0.000 |
| | | C | 1.171 | 3.447 | 0.000 | 0.000 |
| T8 | 60.10-40.10 | A | 1.611 | 4.465 | 0.365 | 0.587 |
| | | B | 0.000 | 0.211 | 0.000 | 0.028 |
| | | C | 0.640 | 1.948 | 0.145 | 0.256 |
| T9 | 40.10-20.10 | A | 1.611 | 4.319 | 0.000 | 0.000 |
| | | B | 0.000 | 0.204 | 0.000 | 0.000 |
| | | C | 0.640 | 1.884 | 0.000 | 0.000 |
| T10 | 20.10-4.85 | A | 1.014 | 2.720 | 0.000 | 0.000 |
| | | B | 0.000 | 0.129 | 0.000 | 0.000 |
| | | C | 0.403 | 1.186 | 0.000 | 0.000 |
| T11 | 4.85-0.00 | A | 0.000 | 0.000 | 0.000 | 0.000 |
| | | B | 0.000 | 0.000 | 0.000 | 0.000 |
| | | C | 0.000 | 0.000 | 0.000 | 0.000 |

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| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 13 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

Feed Line Center of Pressure

| Section | Elevation | CP _X | CP _Z | CP _X | CP _Z |
|---------|---------------|-----------------|-----------------|-----------------|-----------------|
| | ft | in | in | Ice in | Ice in |
| T1 | 190.60-175.35 | 1.1107 | 1.2017 | 1.2123 | 1.1165 |
| T2 | 175.35-160.10 | 1.5293 | 1.6545 | 1.6070 | 1.5265 |
| T3 | 160.10-140.10 | -0.0104 | 1.3302 | 0.0743 | 1.1253 |
| T4 | 140.10-120.10 | -3.0406 | 1.2145 | -2.6694 | 1.0538 |
| T5 | 120.10-100.10 | -2.9704 | 1.4770 | -2.5758 | 1.4609 |
| T6 | 100.10-80.10 | -2.7949 | 1.4544 | -2.4237 | 1.4731 |
| T7 | 80.10-60.10 | -2.9102 | 1.7167 | -2.4991 | 1.8234 |
| T8 | 60.10-40.10 | -3.1649 | 1.8670 | -2.9280 | 2.1371 |
| T9 | 40.10-20.10 | -3.3454 | 1.9735 | -3.0796 | 2.2480 |
| T10 | 20.10-4.85 | -2.8601 | 1.6872 | -2.6403 | 1.9273 |
| T11 | 4.85-0.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Discrete Tower Loads

| Description | Face or Leg | Offset Type | Offsets: Horz Lateral Vert | Azimuth Adjustment | Placement | C _{AA} Front | C _{AA} Side | Weight | |
|------------------------------------|-------------|-------------|----------------------------|--------------------|-----------|-----------------------|----------------------|--------------|-----------------|
| | | | ft ft ft | ° | ft | ft ² | ft ² | lb | |
| BXA-70063-6CF W/ Mast Pipe (VZW) | A | From Leg | 3.00 -6.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-70063-6CF W/ Mast Pipe (VZW) | B | From Leg | 3.00 -6.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-70063-6CF W/ Mast Pipe (VZW) | C | From Leg | 3.00 -6.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-171063-12CF W/ Mast Pipe (VZW) | A | From Leg | 3.00 -4.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 4.80 5.25 | 5.35 6.15 | 72.74 118.96 |
| BXA-171063-12CF W/ Mast Pipe (VZW) | B | From Leg | 3.00 -4.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 4.80 5.25 | 5.35 6.15 | 72.74 118.96 |
| BXA-171063-12CF W/ Mast Pipe (VZW) | C | From Leg | 3.00 -4.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 4.80 5.25 | 5.35 6.15 | 72.74 118.96 |
| BXA-70063-6CF W/ Mast Pipe (VZW) | A | From Leg | 3.00 0.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-70063-6CF W/ Mast Pipe (VZW) | B | From Leg | 3.00 0.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-70063-6CF W/ Mast Pipe (VZW) | C | From Leg | 3.00 0.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 7.76 8.30 | 5.88 6.68 | 52.00 113.00 |
| BXA-171063-12CF W/ Mast Pipe (VZW) | A | From Leg | 3.00 4.00 0.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 4.80 5.25 | 5.35 6.15 | 72.74 118.96 |
| BXA-171063-12CF W/ Mast Pipe | B | From Leg | 3.00 4.00 | 0.0000 | 187.00 | No Ice 1/2" Ice | 4.80 5.25 | 5.35 6.15 | 72.74 118.96 |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Description | Face or Leg | Offset Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustment ° | Placement ft | | C _{AA} _{Front} ft ² | C _{AA} _{Side} ft ² | Weight lb |
|------------------------------|-------------|-------------|--|-------------------------|-----------------|----------|---|--|--------------|
| (VZW) | | | 0.00 | | | | | | |
| BXA-171063-12CF W/ Mast Pipe | C | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 4.80 | 5.35 | 72.74 |
| (VZW) | | | 4.00 | | | 1/2" Ice | 5.25 | 6.15 | 118.96 |
| RRH2x40-AWS | A | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.52 | 1.59 | 40.00 |
| (VZW) | | | -6.00 | | | 1/2" Ice | 2.75 | 1.80 | 60.00 |
| RRH2x40-AWS | B | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.52 | 1.59 | 40.00 |
| (VZW) | | | -6.00 | | | 1/2" Ice | 2.75 | 1.80 | 60.00 |
| RRH2x40-AWS | C | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.52 | 1.59 | 40.00 |
| (VZW) | | | -6.00 | | | 1/2" Ice | 2.75 | 1.80 | 60.00 |
| RRH2x40-07-U | A | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.25 | 1.23 | 50.00 |
| (VZW) | | | 0.00 | | | 1/2" Ice | 2.45 | 1.39 | 70.00 |
| RRH2x40-07-U | B | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.25 | 1.23 | 50.00 |
| (VZW) | | | 0.00 | | | 1/2" Ice | 2.45 | 1.39 | 70.00 |
| RRH2x40-07-U | C | From Leg | 3.00 | 0.0000 | 187.00 | No Ice | 2.25 | 1.23 | 50.00 |
| (VZW) | | | 0.00 | | | 1/2" Ice | 2.45 | 1.39 | 70.00 |
| DB-T1-6Z-8AB-0Z | A | From Face | 3.00 | 0.0000 | 187.00 | No Ice | 5.60 | 2.33 | 40.00 |
| (VZW) | | | 0.00 | | | 1/2" Ice | 5.92 | 2.56 | 80.00 |
| Pirod 12' PCS T-Frame (1) | A | From Leg | 1.00 | 0.0000 | 187.00 | No Ice | 9.80 | 9.80 | 260.00 |
| 104569 | | | 0.00 | | | 1/2" Ice | 14.80 | 14.80 | 360.00 |
| (VZW) | | | 0.00 | | | | | | |
| Pirod 12' PCS T-Frame (1) | B | From Leg | 1.00 | 0.0000 | 187.00 | No Ice | 9.80 | 9.80 | 260.00 |
| 104569 | | | 0.00 | | | 1/2" Ice | 14.80 | 14.80 | 360.00 |
| (VZW) | | | 0.00 | | | | | | |
| Pirod 12' PCS T-Frame (1) | C | From Leg | 1.00 | 0.0000 | 187.00 | No Ice | 9.80 | 9.80 | 260.00 |
| 104569 | | | 0.00 | | | 1/2" Ice | 14.80 | 14.80 | 360.00 |
| (VZW) | | | 0.00 | | | | | | |
| Commscope | A | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 11.39 | 9.96 | 111.32 |
| LNx-6515DS-VTM w/ pipe mast | | | -0.50 | | | 1/2" Ice | 12.01 | 11.38 | 201.80 |
| (TMO) | | | 0.00 | | | | | | |
| Commscope | B | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 11.39 | 9.96 | 111.32 |
| LNx-6515DS-VTM w/ pipe mast | | | -0.50 | | | 1/2" Ice | 12.01 | 11.38 | 201.80 |
| (TMO) | | | 0.00 | | | | | | |
| Commscope | C | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 11.39 | 9.96 | 111.32 |
| LNx-6515DS-VTM w/ pipe mast | | | -0.50 | | | 1/2" Ice | 12.01 | 11.38 | 201.80 |
| (TMO) | | | 0.00 | | | | | | |
| RR90-17-02DP W/ Mast Pipe | A | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 4.74 | 3.72 | 73.74 |
| (TMO) | | | 0.50 | | | 1/2" Ice | 5.24 | 4.42 | 114.99 |
| | | | 0.00 | | | | | | |
| RR90-17-02DP W/ Mast Pipe | B | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 4.74 | 3.72 | 73.74 |
| (TMO) | | | 0.50 | | | 1/2" Ice | 5.24 | 4.42 | 114.99 |
| | | | 0.00 | | | | | | |
| RR90-17-02DP W/ Mast Pipe | C | From Leg | 3.50 | 0.0000 | 145.00 | No Ice | 4.74 | 3.72 | 73.74 |
| (TMO) | | | 0.50 | | | 1/2" Ice | 5.24 | 4.42 | 114.99 |
| | | | 0.00 | | | | | | |
| d B2 TMA | A | From Leg | 2.00 | 0.0000 | 145.00 | No Ice | 0.82 | 0.39 | 10.00 |
| (TMO) | | | 0.50 | | | 1/2" Ice | 0.95 | 0.49 | 20.00 |
| | | | 0.00 | | | | | | |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Description | Face or Leg | Offset Type | Offsets: | | Azimuth Adjustment | Placement | C _A A _A Front | C _A A _A Side | Weight | |
|--------------------------|-------------|-------------|----------|---------|--------------------|-----------|-------------------------------------|------------------------------------|--------------|----------------|
| | | | Horz | Lateral | | | | | | Vert |
| | | | ft | ft | ° | ft | ft ² | ft ² | lb | |
| d B2 TMA (TMO) | B | From Leg | 2.00 | 0.00 | 0.0000 | 145.00 | No Ice 1/2" Ice | 0.82 0.95 | 0.39 0.49 | 10.00 20.00 |
| d B2 TMA (TMO) | C | From Leg | 2.00 | 5.00 | 0.0000 | 145.00 | No Ice 1/2" Ice | 0.82 0.95 | 0.39 0.49 | 10.00 20.00 |
| ROHN 4-ft Side Arm (TMO) | A | From Leg | 2.00 | 0.00 | 0.0000 | 145.00 | No Ice 1/2" Ice | 5.28 7.88 | 5.28 7.88 | 70.00 80.00 |
| ROHN 4-ft Side Arm (TMO) | B | From Leg | 2.00 | 0.00 | 0.0000 | 145.00 | No Ice 1/2" Ice | 5.28 7.88 | 5.28 7.88 | 70.00 80.00 |
| ROHN 4-ft Side Arm (TMO) | C | From Leg | 2.00 | 0.00 | 0.0000 | 145.00 | No Ice 1/2" Ice | 5.28 7.88 | 5.28 7.88 | 70.00 80.00 |
| US Army Mars | A | From Leg | 1.00 | 0.00 | 0.0000 | 85.00 | No Ice 1/2" Ice | 0.25 0.66 | 0.25 0.66 | 31.00 33.82 |
| US Army Mars | C | From Leg | 1.00 | 0.00 | 0.0000 | 85.00 | No Ice 1/2" Ice | 0.25 0.66 | 0.25 0.66 | 31.00 33.82 |
| US Army Mars | A | From Leg | 1.00 | 0.00 | 0.0000 | 120.00 | No Ice 1/2" Ice | 0.25 0.66 | 0.25 0.66 | 31.00 33.82 |
| US Army Mars | C | From Leg | 1.00 | 0.00 | 0.0000 | 120.00 | No Ice 1/2" Ice | 0.25 0.66 | 0.25 0.66 | 31.00 33.82 |

Tower Pressures - No Ice

$$G_H = 1.117$$

| Section Elevation | z | K _Z | q _z | A _G | F _a | A _F | A _R | A _{leg} | Leg % | C _A A _A In Face | C _A A _A Out Face |
|---------------------|--------|----------------|----------------|-----------------|----------------|-----------------|-----------------|------------------|-------|---------------------------------------|--|
| ft | ft | | psf | ft ² | c | ft ² | ft ² | ft ² | % | ft ² | ft ² |
| T1 190.60-175.35 | 182.98 | 1.631 | 30 | 56.419 | A | 1.208 | 10.665 | 7.307 | 61.55 | 0.000 | 0.000 |
| | | | | | B | 1.208 | 10.665 | | 61.55 | 0.000 | 0.000 |
| | | | | | C | 1.113 | 14.247 | | 47.57 | 0.000 | 0.000 |
| T2 175.35-160.10 | 167.73 | 1.591 | 29 | 56.419 | A | 0.000 | 11.068 | 7.307 | 66.02 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 11.068 | | 66.02 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 15.715 | | 46.50 | 0.000 | 0.000 |
| T3 160.10-140.10 | 150.10 | 1.542 | 29 | 73.158 | A | 0.000 | 20.895 | 7.917 | 37.89 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.409 | | 35.33 | 0.000 | 0.000 |
| T4 140.10-120.10 | 130.10 | 1.48 | 27 | 73.158 | A | 0.000 | 33.832 | 7.917 | 23.40 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.409 | | 35.33 | 0.000 | 0.000 |
| T5 120.10-100.10 | 110.10 | 1.411 | 26 | 73.158 | A | 0.000 | 34.737 | 7.917 | 22.79 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 23.313 | | 33.96 | 0.000 | 0.000 |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | z | K _Z | q _z | A _G | F a c e | A _F | A _R | A _{leg} | Leg % | C _A A _A In Face | C _A A _A Out Face |
|--------------------|-------|----------------|----------------|-----------------|---------|-----------------|-----------------|------------------|-------|---------------------------------------|--|
| ft | ft | | psf | ft ² | | ft ² | ft ² | ft ² | | ft ² | ft ² |
| T6 100.10-80.10 | 90.10 | 1.332 | 25 | 73.158 | A | 0.736 | 34.964 | 7.917 | 22.18 | 0.000 | 0.000 |
| | | | | | B | 1.087 | 16.697 | | 44.51 | 0.000 | 0.000 |
| | | | | | C | 0.956 | 23.540 | | 32.32 | 0.000 | 0.000 |
| T7 80.10-60.10 | 70.10 | 1.24 | 23 | 73.158 | A | 0.000 | 35.650 | 7.917 | 22.21 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 24.226 | | 32.68 | 0.000 | 0.000 |
| T8 60.10-40.10 | 50.10 | 1.127 | 21 | 73.992 | A | 0.708 | 34.610 | 9.583 | 27.13 | 0.000 | 0.000 |
| | | | | | B | 1.073 | 14.320 | | 62.26 | 0.000 | 0.000 |
| | | | | | C | 0.928 | 22.380 | | 41.11 | 0.000 | 0.000 |
| T9 40.10-20.10 | 30.10 | 1 | 18 | 73.992 | A | 0.000 | 34.610 | 9.583 | 27.69 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 14.320 | | 66.92 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.380 | | 42.82 | 0.000 | 0.000 |
| T10 20.10-4.85 | 12.48 | 1 | 18 | 56.419 | A | 0.000 | 23.303 | 7.307 | 31.36 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 11.068 | | 66.02 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 15.928 | | 45.88 | 0.000 | 0.000 |
| T11 4.85-0.00 | 2.43 | 1 | 18 | 9.624 | A | 6.955 | 2.513 | 2.513 | 26.54 | 0.000 | 0.000 |
| | | | | | B | 6.955 | 2.513 | | 26.54 | 0.000 | 0.000 |
| | | | | | C | 6.955 | 2.513 | | 26.54 | 0.000 | 0.000 |

Tower Pressure - With Ice

$$G_H = 1.117$$

| Section Elevation | z | K _Z | q _z | t _z | A _G | F a c e | A _F | A _R | A _{leg} | Leg % | C _A A _A In Face | C _A A _A Out Face |
|---------------------|--------|----------------|----------------|----------------|-----------------|---------|-----------------|-----------------|------------------|-------|---------------------------------------|--|
| ft | ft | | psf | in | ft ² | | ft ² | ft ² | ft ² | | ft ² | ft ² |
| T1 190.60-175.35 | 182.98 | 1.631 | 23 | 0.5000 | 57.689 | A | 1.208 | 15.714 | 9.849 | 58.20 | 0.000 | 0.000 |
| | | | | | | B | 1.992 | 15.568 | | 56.09 | 0.000 | 0.000 |
| | | | | | | C | 1.065 | 20.809 | | 45.03 | 0.000 | 0.000 |
| T2 175.35-160.10 | 167.73 | 1.591 | 22 | 0.5000 | 57.689 | A | 0.000 | 16.116 | 9.849 | 61.11 | 0.000 | 0.000 |
| | | | | | | B | 0.847 | 15.954 | | 58.62 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 22.724 | | 43.34 | 0.000 | 0.000 |
| T3 160.10-140.10 | 150.10 | 1.542 | 21 | 0.5000 | 74.825 | A | 0.000 | 31.548 | 11.250 | 35.66 | 0.000 | 0.000 |
| | | | | | | B | 1.111 | 25.510 | | 42.26 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 33.589 | | 33.49 | 0.000 | 0.000 |
| T4 140.10-120.10 | 130.10 | 1.48 | 21 | 0.5000 | 74.825 | A | 0.000 | 49.000 | 11.250 | 22.96 | 0.000 | 0.000 |
| | | | | | | B | 1.111 | 25.510 | | 42.26 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 33.589 | | 33.49 | 0.000 | 0.000 |
| T5 120.10-100.10 | 110.10 | 1.411 | 20 | 0.5000 | 74.825 | A | 0.000 | 51.097 | 11.250 | 22.02 | 0.000 | 0.000 |
| | | | | | | B | 1.111 | 25.510 | | 42.26 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 35.686 | | 31.52 | 0.000 | 0.000 |
| T6 100.10-80.10 | 90.10 | 1.332 | 18 | 0.5000 | 74.825 | A | 0.534 | 51.757 | 11.250 | 21.51 | 0.000 | 0.000 |
| | | | | | | B | 2.171 | 25.775 | | 40.26 | 0.000 | 0.000 |
| | | | | | | C | 0.865 | 36.429 | | 30.17 | 0.000 | 0.000 |
| T7 80.10-60.10 | 70.10 | 1.24 | 17 | 0.5000 | 74.825 | A | 0.000 | 53.214 | 11.250 | 21.14 | 0.000 | 0.000 |
| | | | | | | B | 1.111 | 25.510 | | 42.26 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 37.804 | | 29.76 | 0.000 | 0.000 |
| T8 60.10-40.10 | 50.10 | 1.127 | 16 | 0.5000 | 75.658 | A | 0.486 | 51.848 | 12.917 | 24.68 | 0.000 | 0.000 |
| | | | | | | B | 2.157 | 20.868 | | 56.10 | 0.000 | 0.000 |
| | | | | | | C | 0.817 | 34.499 | | 36.57 | 0.000 | 0.000 |
| T9 40.10-20.10 | 30.10 | 1 | 14 | 0.5000 | 75.658 | A | 0.000 | 51.726 | 12.917 | 24.97 | 0.000 | 0.000 |
| | | | | | | B | 1.111 | 20.607 | | 59.47 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 34.294 | | 37.66 | 0.000 | 0.000 |
| T10 20.10-4.85 | 12.48 | 1 | 14 | 0.5000 | 57.689 | A | 0.000 | 34.712 | 9.849 | 28.37 | 0.000 | 0.000 |
| | | | | | | B | 0.672 | 15.987 | | 59.12 | 0.000 | 0.000 |
| | | | | | | C | 0.000 | 24.227 | | 40.65 | 0.000 | 0.000 |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | z | K _Z | q _z | t _z | A _G | F a c e | A _F | A _R | A _{leg} | Leg % | C _A A _A In Face | C _A A _A Out Face |
|-------------------|------|----------------|----------------|----------------|-----------------|---------|-----------------|-----------------|------------------|-------|---------------------------------------|--|
| ft | ft | | psf | in | ft ² | e | ft ² | ft ² | ft ² | | ft ² | ft ² |
| T11 4.85-0.00 | 2.43 | 1 | 14 | 0.5000 | 10.053 | A | 6.955 | 3.884 | 3.388 | 31.25 | 0.000 | 0.000 |
| | | | | | | B | 6.955 | 3.884 | | 31.25 | 0.000 | 0.000 |
| | | | | | | C | 6.955 | 3.884 | | 31.25 | 0.000 | 0.000 |

Tower Pressure - Service

$$G_H = 1.117$$

| Section Elevation | z | K _Z | q _z | A _G | F a c e | A _F | A _R | A _{leg} | Leg % | C _A A _A In Face | C _A A _A Out Face |
|-------------------|--------|----------------|----------------|-----------------|---------|-----------------|-----------------|------------------|-------|---------------------------------------|--|
| ft | ft | | psf | ft ² | e | ft ² | ft ² | ft ² | | ft ² | ft ² |
| T1 190.60-175.35 | 182.98 | 1.631 | 15 | 56.419 | A | 1.208 | 10.665 | 7.307 | 61.55 | 0.000 | 0.000 |
| | | | | | B | 1.208 | 10.665 | | 61.55 | 0.000 | 0.000 |
| | | | | | C | 1.113 | 14.247 | | 47.57 | 0.000 | 0.000 |
| T2 175.35-160.10 | 167.73 | 1.591 | 15 | 56.419 | A | 0.000 | 11.068 | 7.307 | 66.02 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 11.068 | | 66.02 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 15.715 | | 46.50 | 0.000 | 0.000 |
| T3 160.10-140.10 | 150.10 | 1.542 | 14 | 73.158 | A | 0.000 | 20.895 | 7.917 | 37.89 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.409 | | 35.33 | 0.000 | 0.000 |
| T4 140.10-120.10 | 130.10 | 1.48 | 14 | 73.158 | A | 0.000 | 33.832 | 7.917 | 23.40 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.409 | | 35.33 | 0.000 | 0.000 |
| T5 120.10-100.10 | 110.10 | 1.411 | 13 | 73.158 | A | 0.000 | 34.737 | 7.917 | 22.79 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 23.313 | | 33.96 | 0.000 | 0.000 |
| T6 100.10-80.10 | 90.10 | 1.332 | 12 | 73.158 | A | 0.736 | 34.964 | 7.917 | 22.18 | 0.000 | 0.000 |
| | | | | | B | 1.087 | 16.697 | | 44.51 | 0.000 | 0.000 |
| | | | | | C | 0.956 | 23.540 | | 32.32 | 0.000 | 0.000 |
| T7 80.10-60.10 | 70.10 | 1.24 | 11 | 73.158 | A | 0.000 | 35.650 | 7.917 | 22.21 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 16.697 | | 47.41 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 24.226 | | 32.68 | 0.000 | 0.000 |
| T8 60.10-40.10 | 50.10 | 1.127 | 10 | 73.992 | A | 0.708 | 34.610 | 9.583 | 27.13 | 0.000 | 0.000 |
| | | | | | B | 1.073 | 14.320 | | 62.26 | 0.000 | 0.000 |
| | | | | | C | 0.928 | 22.380 | | 41.11 | 0.000 | 0.000 |
| T9 40.10-20.10 | 30.10 | 1 | 9 | 73.992 | A | 0.000 | 34.610 | 9.583 | 27.69 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 14.320 | | 66.92 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 22.380 | | 42.82 | 0.000 | 0.000 |
| T10 20.10-4.85 | 12.48 | 1 | 9 | 56.419 | A | 0.000 | 23.303 | 7.307 | 31.36 | 0.000 | 0.000 |
| | | | | | B | 0.000 | 11.068 | | 66.02 | 0.000 | 0.000 |
| | | | | | C | 0.000 | 15.928 | | 45.88 | 0.000 | 0.000 |
| T11 4.85-0.00 | 2.43 | 1 | 9 | 9.624 | A | 6.955 | 2.513 | 2.513 | 26.54 | 0.000 | 0.000 |
| | | | | | B | 6.955 | 2.513 | | 26.54 | 0.000 | 0.000 |
| | | | | | C | 6.955 | 2.513 | | 26.54 | 0.000 | 0.000 |

Tower Forces - No Ice - Wind Normal To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|------|----------------|----------------|----------------|----------------|-----------------|--------|-------|------------|
| ft | lb | lb | e | | | | | | ft ² | lb | plf | |
| T1 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 1 | 1 | 7.528 | 781.40 | 51.24 | C |

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|---|----------------------------------|--|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 18 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|---------------------------|----------------|----------------|----------------|-----------------|----------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| 190.60-175.35 | | | B | 0.21 | 2.562 | 0.593 | 1 | 1 | 7.528 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 1 | 1 | 9.772 | | | |
| T2 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | 741.55 | 48.63 | C |
| 175.35-160.10 | | | B | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 1 | 1 | 9.579 | | | |
| T3 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 1 | 1 | 12.780 | 1005.13 | 50.26 | C |
| 160.10-140.10 | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 1 | 1 | 13.845 | | | |
| T4 | 387.60 | 419.23 | A | 0.462 | 1.954 | 0.679 | 1 | 1 | 22.975 | 1372.29 | 68.61 | A |
| 140.10-120.10 | | TA 328.71 | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 1 | 1 | 13.845 | | | |
| T5 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 1 | 1 | 23.794 | 1342.07 | 67.10 | A |
| 120.10-100.10 | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 1 | 1 | 14.496 | | | |
| T6 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 1 | 1 | 24.911 | 1313.98 | 65.70 | A |
| 100.10-80.10 | | | B | 0.243 | 2.458 | 0.6 | 1 | 1 | 11.108 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 1 | 1 | 15.720 | | | |
| T7 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 1 | 1 | 24.638 | 1210.23 | 60.51 | A |
| 80.10-60.10 | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 1 | 1 | 15.164 | | | |
| T8 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 1 | 1 | 24.457 | 1099.50 | 54.98 | A |
| 60.10-40.10 | | | B | 0.208 | 2.569 | 0.592 | 1 | 1 | 9.552 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 1 | 1 | 14.818 | | | |
| T9 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 1 | 1 | 23.589 | 948.16 | 47.41 | A |
| 40.10-20.10 | | | B | 0.194 | 2.618 | 0.589 | 1 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 1 | 1 | 13.801 | | | |
| T10 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 1 | 1 | 15.310 | 644.89 | 42.29 | A |
| 20.10-4.85 | | | B | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 1 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 1 | 1 | 9.469 | 397.68* | 82.00 | C |
| | | | B | 0.984 | 2.067 | 1 | 1 | 1 | 9.469 | | | |
| | | | C | 0.984 | 2.067 | 1 | 1 | 1 | 9.469 | | | |
| Sum Weight: | 3136.14 | 5117.06 | | | *2A _g limit | | | | | 10856.89 | | |

Tower Forces - No Ice - Wind 60 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 0.8 | 1 | 7.286 | 763.60 | 50.07 | C |
| 190.60-175.35 | | | B | 0.21 | 2.562 | 0.593 | 0.8 | 1 | 7.286 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 0.8 | 1 | 9.550 | | | |
| T2 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | 741.55 | 48.63 | C |
| 175.35-160.10 | | | B | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 0.8 | 1 | 9.579 | | | |
| T3 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 0.8 | 1 | 12.780 | 1005.13 | 50.26 | C |
| 160.10-140.10 | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.8 | 1 | 13.845 | | | |
| T4 | 387.60 | 419.23 | A | 0.462 | 1.954 | 0.679 | 0.8 | 1 | 22.975 | 1372.29 | 68.61 | A |
| 140.10-120.10 | | TA 328.71 | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.8 | 1 | 13.845 | | | |
| T5 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 0.8 | 1 | 23.794 | 1342.07 | 67.10 | A |
| 120.10-100.10 | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 0.8 | 1 | 14.496 | | | |
| T6 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 0.8 | 1 | 24.764 | 1306.22 | 65.31 | A |

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| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 19 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|----------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| 100.10-80.10 | | | B | 0.243 | 2.458 | 0.6 | 0.8 | 1 | 10.891 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 0.8 | 1 | 15.528 | | | |
| T7 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 0.8 | 1 | 24.638 | 1210.23 | 60.51 | A |
| 80.10-60.10 | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 0.8 | 1 | 15.164 | | | |
| T8 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 0.8 | 1 | 24.316 | 1093.13 | 54.66 | A |
| 60.10-40.10 | | | B | 0.208 | 2.569 | 0.592 | 0.8 | 1 | 9.337 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 0.8 | 1 | 14.632 | | | |
| T9 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 0.8 | 1 | 23.589 | 948.16 | 47.41 | A |
| 40.10-20.10 | | | B | 0.194 | 2.618 | 0.589 | 0.8 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 0.8 | 1 | 13.801 | | | |
| T10 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 0.8 | 1 | 15.310 | 644.89 | 42.29 | A |
| 20.10-4.85 | | | B | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 0.8 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | 344.95 | 71.12 | C |
| | | | B | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | | | |
| | | | C | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | | | |
| Sum Weight: | 3136.14 | 5117.06 | | | | | | | | 10772.23 | | |

Tower Forces - No Ice - Wind 90 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 0.85 | 1 | 7.346 | 768.05 | 50.36 | C |
| 190.60-175.35 | | | B | 0.21 | 2.562 | 0.593 | 0.85 | 1 | 7.346 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 0.85 | 1 | 9.605 | | | |
| T2 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | 741.55 | 48.63 | C |
| 175.35-160.10 | | | B | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 0.85 | 1 | 9.579 | | | |
| T3 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 0.85 | 1 | 12.780 | 1005.13 | 50.26 | C |
| 160.10-140.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.85 | 1 | 13.845 | | | |
| T4 | 387.60 | 419.23 | A | 0.462 | 1.954 | 0.679 | 0.85 | 1 | 22.975 | 1372.29 | 68.61 | A |
| 140.10-120.10 | | TA 328.71 | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.85 | 1 | 13.845 | | | |
| T5 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 0.85 | 1 | 23.794 | 1342.07 | 67.10 | A |
| 120.10-100.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 0.85 | 1 | 14.496 | | | |
| T6 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 0.85 | 1 | 24.801 | 1308.16 | 65.41 | A |
| 100.10-80.10 | | | B | 0.243 | 2.458 | 0.6 | 0.85 | 1 | 10.945 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 0.85 | 1 | 15.576 | | | |
| T7 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 0.85 | 1 | 24.638 | 1210.23 | 60.51 | A |
| 80.10-60.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 0.85 | 1 | 15.164 | | | |
| T8 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 0.85 | 1 | 24.351 | 1094.72 | 54.74 | A |
| 60.10-40.10 | | | B | 0.208 | 2.569 | 0.592 | 0.85 | 1 | 9.391 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 0.85 | 1 | 14.679 | | | |
| T9 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 0.85 | 1 | 23.589 | 948.16 | 47.41 | A |
| 40.10-20.10 | | | B | 0.194 | 2.618 | 0.589 | 0.85 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 0.85 | 1 | 13.801 | | | |
| T10 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 0.85 | 1 | 15.310 | 644.89 | 42.29 | A |
| 20.10-4.85 | | | B | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 0.85 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | 359.80 | 74.19 | C |
| | | | B | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | | | |

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| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 20 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|----------|-----|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| Sum Weight: | 3136.14 | 5117.06 | C | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | 10795.06 | | |

Tower Forces - With Ice - Wind Normal To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|---------------------|------------|-------------|---------|-------|---------------------------|----------------|----------------|----------------|-----------------|---------------------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 190.60-175.35 | 175.53 | 710.79 | A | 0.293 | 2.314 | 0.614 | 1 | 1 | 10.854 | 769.63 | 50.47 | C |
| | | | B | 0.304 | 2.284 | 0.617 | 1 | 1 | 11.601 | | | |
| | | | C | 0.379 | 2.107 | 0.643 | 1 | 1 | 14.452 | | | |
| T2 175.35-160.10 | 197.30 | 650.30 | A | 0.279 | 2.352 | 0.61 | 1 | 1 | 9.828 | 755.14 | 49.52 | C |
| | | | B | 0.291 | 2.32 | 0.613 | 1 | 1 | 10.631 | | | |
| | | | C | 0.394 | 2.076 | 0.649 | 1 | 1 | 14.751 | | | |
| T3 160.10-140.10 | 396.05 | 797.68 | A | 0.422 | 2.023 | 0.661 | 1 | 1 | 20.842 | 1066.28 | 53.31 | C |
| | | | B | 0.356 | 2.158 | 0.635 | 1 | 1 | 17.299 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 1 | 1 | 22.598 | | | |
| T4 140.10-120.10 | 819.15 | 797.68 | A | 0.655 | 1.78 | 0.789 | 1 | 1 | 38.647 | 1577.65 | 78.88 | A |
| | | TA 465.74 | B | 0.356 | 2.158 | 0.635 | 1 | 1 | 17.299 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 1 | 1 | 22.598 | | | |
| T5 120.10-100.10 | 852.59 | 797.68 | A | 0.683 | 1.776 | 0.808 | 1 | 1 | 41.277 | 1602.73 | 80.14 | A |
| | | | B | 0.356 | 2.158 | 0.635 | 1 | 1 | 17.299 | | | |
| | | | C | 0.477 | 1.932 | 0.686 | 1 | 1 | 24.481 | | | |
| T6 100.10-80.10 | 860.99 | 887.53 | A | 0.699 | 1.776 | 0.819 | 1 | 1 | 42.927 | 1573.98 | 78.70 | A |
| | | | B | 0.373 | 2.119 | 0.641 | 1 | 1 | 18.696 | | | |
| | | | C | 0.498 | 1.902 | 0.697 | 1 | 1 | 26.246 | | | |
| T7 80.10-60.10 | 886.37 | 879.91 | A | 0.711 | 1.777 | 0.828 | 1 | 1 | 44.059 | 1504.66 | 75.23 | A |
| | | | B | 0.356 | 2.158 | 0.635 | 1 | 1 | 17.299 | | | |
| | | | C | 0.505 | 1.893 | 0.7 | 1 | 1 | 26.470 | | | |
| T8 60.10-40.10 | 886.37 | 819.89 | A | 0.692 | 1.776 | 0.814 | 1 | 1 | 42.691 | 1323.52 | 66.18 | A |
| | | | B | 0.304 | 2.285 | 0.617 | 1 | 1 | 15.038 | | | |
| | | | C | 0.467 | 1.947 | 0.681 | 1 | 1 | 24.315 | | | |
| T9 40.10-20.10 | 886.37 | 730.04 | A | 0.684 | 1.776 | 0.808 | 1 | 1 | 41.814 | 1150.69 | 57.53 | A |
| | | | B | 0.287 | 2.331 | 0.612 | 1 | 1 | 13.723 | | | |
| | | | C | 0.453 | 1.968 | 0.675 | 1 | 1 | 23.141 | | | |
| T10 20.10-4.85 | 536.25 | 564.75 | A | 0.602 | 1.803 | 0.755 | 1 | 1 | 26.195 | 731.84 | 47.99 | A |
| | | | B | 0.289 | 2.326 | 0.613 | 1 | 1 | 10.465 | | | |
| | | | C | 0.42 | 2.026 | 0.66 | 1 | 1 | 15.988 | | | |
| T11 4.85-0.00 | 0.00 | 459.43 | A | 1 | 2.1 | 1 | 1 | 1 | 10.840 | 311.56 [†] | 64.24 | C |
| | | | B | 1 | 2.1 | 1 | 1 | 1 | 10.840 | | | |
| | | | C | 1 | 2.1 | 1 | 1 | 1 | 10.840 | | | |
| Sum Weight: | 6496.97 | 8561.42 | | | *2A _s limit | | | | | 12367.67 | | |

Tower Forces - With Ice - Wind 60 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|--------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 | 175.53 | 710.79 | A | 0.293 | 2.314 | 0.614 | 0.8 | 1 | 10.612 | 758.28 | 49.72 | C |

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| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 21 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|----------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| 190.60-175.35 | | | B | 0.304 | 2.284 | 0.617 | 0.8 | 1 | 11.202 | | | |
| | | | C | 0.379 | 2.107 | 0.643 | 0.8 | 1 | 14.239 | | | |
| T2 | 197.30 | 650.30 | A | 0.279 | 2.352 | 0.61 | 0.8 | 1 | 9.828 | 755.14 | 49.52 | C |
| 175.35-160.10 | | | B | 0.291 | 2.32 | 0.613 | 0.8 | 1 | 10.462 | | | |
| | | | C | 0.394 | 2.076 | 0.649 | 0.8 | 1 | 14.751 | | | |
| T3 | 396.05 | 797.68 | A | 0.422 | 2.023 | 0.661 | 0.8 | 1 | 20.842 | 1066.28 | 53.31 | C |
| 160.10-140.10 | | | B | 0.356 | 2.158 | 0.635 | 0.8 | 1 | 17.077 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 0.8 | 1 | 22.598 | | | |
| T4 | 819.15 | 797.68 | A | 0.655 | 1.78 | 0.789 | 0.8 | 1 | 38.647 | 1577.65 | 78.88 | A |
| 140.10-120.10 | | TA 465.74 | B | 0.356 | 2.158 | 0.635 | 0.8 | 1 | 17.077 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 0.8 | 1 | 22.598 | | | |
| T5 | 852.59 | 797.68 | A | 0.683 | 1.776 | 0.808 | 0.8 | 1 | 41.277 | 1602.73 | 80.14 | A |
| 120.10-100.10 | | | B | 0.356 | 2.158 | 0.635 | 0.8 | 1 | 17.077 | | | |
| | | | C | 0.477 | 1.932 | 0.686 | 0.8 | 1 | 24.481 | | | |
| T6 | 860.99 | 887.53 | A | 0.699 | 1.776 | 0.819 | 0.8 | 1 | 42.821 | 1570.06 | 78.50 | A |
| 100.10-80.10 | | | B | 0.373 | 2.119 | 0.641 | 0.8 | 1 | 18.262 | | | |
| | | | C | 0.498 | 1.902 | 0.697 | 0.8 | 1 | 26.073 | | | |
| T7 | 886.37 | 879.91 | A | 0.711 | 1.777 | 0.828 | 0.8 | 1 | 44.059 | 1504.66 | 75.23 | A |
| 80.10-60.10 | | | B | 0.356 | 2.158 | 0.635 | 0.8 | 1 | 17.077 | | | |
| | | | C | 0.505 | 1.893 | 0.7 | 0.8 | 1 | 26.470 | | | |
| T8 | 886.37 | 819.89 | A | 0.692 | 1.776 | 0.814 | 0.8 | 1 | 42.594 | 1320.50 | 66.03 | A |
| 60.10-40.10 | | | B | 0.304 | 2.285 | 0.617 | 0.8 | 1 | 14.606 | | | |
| | | | C | 0.467 | 1.947 | 0.681 | 0.8 | 1 | 24.152 | | | |
| T9 | 886.37 | 730.04 | A | 0.684 | 1.776 | 0.808 | 0.8 | 1 | 41.814 | 1150.69 | 57.53 | A |
| 40.10-20.10 | | | B | 0.287 | 2.331 | 0.612 | 0.8 | 1 | 13.501 | | | |
| | | | C | 0.453 | 1.968 | 0.675 | 0.8 | 1 | 23.141 | | | |
| T10 | 536.25 | 564.75 | A | 0.602 | 1.803 | 0.755 | 0.8 | 1 | 26.195 | 731.84 | 47.99 | A |
| 20.10-4.85 | | | B | 0.289 | 2.326 | 0.613 | 0.8 | 1 | 10.331 | | | |
| | | | C | 0.42 | 2.026 | 0.66 | 0.8 | 1 | 15.988 | | | |
| T11 | 4.85-0.00 | 0.00 | A | 1 | 2.1 | 1 | 0.8 | 1 | 9.449 | 307.46 | 63.39 | C |
| | | | B | 1 | 2.1 | 1 | 0.8 | 1 | 9.449 | | | |
| | | | C | 1 | 2.1 | 1 | 0.8 | 1 | 9.449 | | | |
| Sum Weight: | 6496.97 | 8561.42 | | | | | | | | 12345.29 | | |

Tower Forces - With Ice - Wind 90 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 | 175.53 | 710.79 | A | 0.293 | 2.314 | 0.614 | 0.85 | 1 | 10.673 | 761.12 | 49.91 | C |
| 190.60-175.35 | | | B | 0.304 | 2.284 | 0.617 | 0.85 | 1 | 11.302 | | | |
| | | | C | 0.379 | 2.107 | 0.643 | 0.85 | 1 | 14.292 | | | |
| T2 | 197.30 | 650.30 | A | 0.279 | 2.352 | 0.61 | 0.85 | 1 | 9.828 | 755.14 | 49.52 | C |
| 175.35-160.10 | | | B | 0.291 | 2.32 | 0.613 | 0.85 | 1 | 10.504 | | | |
| | | | C | 0.394 | 2.076 | 0.649 | 0.85 | 1 | 14.751 | | | |
| T3 | 396.05 | 797.68 | A | 0.422 | 2.023 | 0.661 | 0.85 | 1 | 20.842 | 1066.28 | 53.31 | C |
| 160.10-140.10 | | | B | 0.356 | 2.158 | 0.635 | 0.85 | 1 | 17.132 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 0.85 | 1 | 22.598 | | | |
| T4 | 819.15 | 797.68 | A | 0.655 | 1.78 | 0.789 | 0.85 | 1 | 38.647 | 1577.65 | 78.88 | A |
| 140.10-120.10 | | TA 465.74 | B | 0.356 | 2.158 | 0.635 | 0.85 | 1 | 17.132 | | | |
| | | | C | 0.449 | 1.975 | 0.673 | 0.85 | 1 | 22.598 | | | |
| T5 | 852.59 | 797.68 | A | 0.683 | 1.776 | 0.808 | 0.85 | 1 | 41.277 | 1602.73 | 80.14 | A |
| 120.10-100.10 | | | B | 0.356 | 2.158 | 0.635 | 0.85 | 1 | 17.132 | | | |
| | | | C | 0.477 | 1.932 | 0.686 | 0.85 | 1 | 24.481 | | | |
| T6 | 860.99 | 887.53 | A | 0.699 | 1.776 | 0.819 | 0.85 | 1 | 42.847 | 1571.04 | 78.55 | A |
| 100.10-80.10 | | | B | 0.373 | 2.119 | 0.641 | 0.85 | 1 | 18.371 | | | |

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|---|------------------------------|--------------------------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job CT11156A | Page 22 of 49 |
| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|----------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T7 80.10-60.10 | 886.37 | 879.91 | C | 0.498 | 1.902 | 0.697 | 0.85 | 1 | 26.116 | 1504.66 | 75.23 | A |
| | | | A | 0.711 | 1.777 | 0.828 | 0.85 | 1 | 44.059 | | | |
| | | | B | 0.356 | 2.158 | 0.635 | 0.85 | 1 | 17.132 | | | |
| T8 60.10-40.10 | 886.37 | 819.89 | C | 0.505 | 1.893 | 0.7 | 0.85 | 1 | 26.470 | 1321.25 | 66.06 | A |
| | | | A | 0.692 | 1.776 | 0.814 | 0.85 | 1 | 42.618 | | | |
| | | | B | 0.304 | 2.285 | 0.617 | 0.85 | 1 | 14.714 | | | |
| T9 40.10-20.10 | 886.37 | 730.04 | C | 0.467 | 1.947 | 0.681 | 0.85 | 1 | 24.193 | 1150.69 | 57.53 | A |
| | | | A | 0.684 | 1.776 | 0.808 | 0.85 | 1 | 41.814 | | | |
| | | | B | 0.287 | 2.331 | 0.612 | 0.85 | 1 | 13.556 | | | |
| T10 20.10-4.85 | 536.25 | 564.75 | C | 0.453 | 1.968 | 0.675 | 0.85 | 1 | 23.141 | 731.84 | 47.99 | A |
| | | | A | 0.602 | 1.803 | 0.755 | 0.85 | 1 | 26.195 | | | |
| | | | B | 0.289 | 2.326 | 0.613 | 0.85 | 1 | 10.364 | | | |
| T11 4.85-0.00 | 0.00 | 459.43 | C | 0.42 | 2.026 | 0.66 | 0.85 | 1 | 15.988 | 311.56* | 64.24 | C |
| | | | A | 1 | 2.1 | 1 | 0.85 | 1 | 9.796 | | | |
| | | | B | 1 | 2.1 | 1 | 0.85 | 1 | 9.796 | | | |
| Sum Weight: | 6496.97 | 8561.42 | C | 1 | 2.1 | 1 | 0.85 | 1 | 9.796 | 12353.96 | | |

Tower Forces - Service - Wind Normal To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|---------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 190.60-175.35 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 1 | 1 | 7.528 | 389.35 | 25.53 | C |
| | | | B | 0.21 | 2.562 | 0.593 | 1 | 1 | 7.528 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 1 | 1 | 9.772 | | | |
| T2 175.35-160.10 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | 369.49 | 24.23 | C |
| | | | B | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 1 | 1 | 9.579 | | | |
| T3 160.10-140.10 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 1 | 1 | 12.780 | 500.83 | 25.04 | C |
| | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 1 | 1 | 13.845 | | | |
| T4 140.10-120.10 | 387.60 | 419.23 | A | 0.462 | 1.954 | 0.679 | 1 | 1 | 22.975 | 683.77 | 34.19 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 1 | 1 | 13.845 | | | |
| T5 120.10-100.10 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 1 | 1 | 23.794 | 668.71 | 33.44 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 1 | 1 | 14.496 | | | |
| T6 100.10-80.10 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 1 | 1 | 24.911 | 654.72 | 32.74 | A |
| | | | B | 0.243 | 2.458 | 0.6 | 1 | 1 | 11.108 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 1 | 1 | 15.720 | | | |
| T7 80.10-60.10 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 1 | 1 | 24.638 | 603.02 | 30.15 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 1 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 1 | 1 | 15.164 | | | |
| T8 60.10-40.10 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 1 | 1 | 24.457 | 547.85 | 27.39 | A |
| | | | B | 0.208 | 2.569 | 0.592 | 1 | 1 | 9.552 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 1 | 1 | 14.818 | | | |
| T9 40.10-20.10 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 1 | 1 | 23.589 | 472.44 | 23.62 | A |
| | | | B | 0.194 | 2.618 | 0.589 | 1 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 1 | 1 | 13.801 | | | |
| T10 20.10-4.85 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 1 | 1 | 15.310 | 321.33 | 21.07 | A |
| | | | B | 0.196 | 2.609 | 0.59 | 1 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 1 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 1 | 1 | 9.469 | 198.15* | 40.86 | C |
| | | | B | 0.984 | 2.067 | 1 | 1 | 1 | 9.469 | | | |

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|---|---------|------------|-------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 23 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|------------------------------------|----------------|----------------|----------------|-----------------|---------|-----|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| Sum Weight: | 3136.14 | 5117.06 | C | 0.984 | 2.067 *2A _B limit | 1 | 1 | 1 | 9.469 | 5409.66 | | |

Tower Forces - Service - Wind 60 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|---------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 190.60-175.35 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 0.8 | 1 | 7.286 | 380.48 | 24.95 | C |
| | | | B | 0.21 | 2.562 | 0.593 | 0.8 | 1 | 7.286 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 0.8 | 1 | 9.550 | | | |
| T2 175.35-160.10 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | 369.49 | 24.23 | C |
| | | | B | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 0.8 | 1 | 9.579 | | | |
| T3 160.10-140.10 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 0.8 | 1 | 12.780 | 500.83 | 25.04 | C |
| | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.8 | 1 | 13.845 | | | |
| T4 140.10-120.10 | 387.60 | TA 328.71 | A | 0.462 | 1.954 | 0.679 | 0.8 | 1 | 22.975 | 683.77 | 34.19 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.8 | 1 | 13.845 | | | |
| T5 120.10-100.10 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 0.8 | 1 | 23.794 | 668.71 | 33.44 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 0.8 | 1 | 14.496 | | | |
| T6 100.10-80.10 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 0.8 | 1 | 24.764 | 650.85 | 32.54 | A |
| | | | B | 0.243 | 2.458 | 0.6 | 0.8 | 1 | 10.891 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 0.8 | 1 | 15.528 | | | |
| T7 80.10-60.10 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 0.8 | 1 | 24.638 | 603.02 | 30.15 | A |
| | | | B | 0.228 | 2.504 | 0.597 | 0.8 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 0.8 | 1 | 15.164 | | | |
| T8 60.10-40.10 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 0.8 | 1 | 24.316 | 544.67 | 27.23 | A |
| | | | B | 0.208 | 2.569 | 0.592 | 0.8 | 1 | 9.337 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 0.8 | 1 | 14.632 | | | |
| T9 40.10-20.10 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 0.8 | 1 | 23.589 | 472.44 | 23.62 | A |
| | | | B | 0.194 | 2.618 | 0.589 | 0.8 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 0.8 | 1 | 13.801 | | | |
| T10 20.10-4.85 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 0.8 | 1 | 15.310 | 321.33 | 21.07 | A |
| | | | B | 0.196 | 2.609 | 0.59 | 0.8 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 0.8 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | 171.88 | 35.44 | C |
| | | | B | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | | | |
| | | | C | 0.984 | 2.067 | 1 | 0.8 | 1 | 8.078 | | | |
| Sum Weight: | 3136.14 | 5117.06 | | | | | | | | 5367.48 | | |

Tower Forces - Service - Wind 90 To Face

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|------|----------------|----------------|----------------|----------------|-----------------|--------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| T1 | 134.84 | 487.84 | A | 0.21 | 2.562 | 0.593 | 0.85 | 1 | 7.346 | 382.69 | 25.09 | C |

| | | | | |
|---|----------------|------------|--------------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 24 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section Elevation | Add Weight | Self Weight | F a c e | e | C _F | R _R | D _F | D _R | A _E | F | w | Ctrl. Face |
|-------------------|------------|-------------|---------|-------|----------------|----------------|----------------|----------------|-----------------|---------|-------|------------|
| ft | lb | lb | | | | | | | ft ² | lb | plf | |
| 190.60-175.35 | | | B | 0.21 | 2.562 | 0.593 | 0.85 | 1 | 7.346 | | | |
| | | | C | 0.272 | 2.372 | 0.608 | 0.85 | 1 | 9.605 | | | |
| T2 | 145.48 | 437.52 | A | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | 369.49 | 24.23 | C |
| 175.35-160.10 | | | B | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | | | |
| | | | C | 0.279 | 2.355 | 0.61 | 0.85 | 1 | 9.579 | | | |
| T3 | 239.02 | 419.23 | A | 0.286 | 2.335 | 0.612 | 0.85 | 1 | 12.780 | 500.83 | 25.04 | C |
| 160.10-140.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.85 | 1 | 13.845 | | | |
| T4 | 387.60 | 419.23 | A | 0.462 | 1.954 | 0.679 | 0.85 | 1 | 22.975 | 683.77 | 34.19 | A |
| 140.10-120.10 | | TA 328.71 | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.306 | 2.279 | 0.618 | 0.85 | 1 | 13.845 | | | |
| T5 | 393.57 | 419.23 | A | 0.475 | 1.935 | 0.685 | 0.85 | 1 | 23.794 | 668.71 | 33.44 | A |
| 120.10-100.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.319 | 2.248 | 0.622 | 0.85 | 1 | 14.496 | | | |
| T6 | 395.07 | 475.39 | A | 0.488 | 1.916 | 0.691 | 0.85 | 1 | 24.801 | 651.82 | 32.59 | A |
| 100.10-80.10 | | | B | 0.243 | 2.458 | 0.6 | 0.85 | 1 | 10.945 | | | |
| | | | C | 0.335 | 2.207 | 0.627 | 0.85 | 1 | 15.576 | | | |
| T7 | 399.60 | 501.45 | A | 0.487 | 1.917 | 0.691 | 0.85 | 1 | 24.638 | 603.02 | 30.15 | A |
| 80.10-60.10 | | | B | 0.228 | 2.504 | 0.597 | 0.85 | 1 | 9.961 | | | |
| | | | C | 0.331 | 2.216 | 0.626 | 0.85 | 1 | 15.164 | | | |
| T8 | 399.60 | 513.27 | A | 0.477 | 1.931 | 0.686 | 0.85 | 1 | 24.351 | 545.47 | 27.27 | A |
| 60.10-40.10 | | | B | 0.208 | 2.569 | 0.592 | 0.85 | 1 | 9.391 | | | |
| | | | C | 0.315 | 2.257 | 0.621 | 0.85 | 1 | 14.679 | | | |
| T9 | 399.60 | 457.11 | A | 0.468 | 1.945 | 0.682 | 0.85 | 1 | 23.589 | 472.44 | 23.62 | A |
| 40.10-20.10 | | | B | 0.194 | 2.618 | 0.589 | 0.85 | 1 | 8.436 | | | |
| | | | C | 0.302 | 2.289 | 0.617 | 0.85 | 1 | 13.801 | | | |
| T10 | 241.76 | 351.97 | A | 0.413 | 2.039 | 0.657 | 0.85 | 1 | 15.310 | 321.33 | 21.07 | A |
| 20.10-4.85 | | | B | 0.196 | 2.609 | 0.59 | 0.85 | 1 | 6.526 | | | |
| | | | C | 0.282 | 2.344 | 0.611 | 0.85 | 1 | 9.726 | | | |
| T11 4.85-0.00 | 0.00 | 306.10 | A | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | 179.28 | 36.96 | C |
| | | | B | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | | | |
| | | | C | 0.984 | 2.067 | 1 | 0.85 | 1 | 8.425 | | | |
| Sum Weight: | 3136.14 | 5117.06 | | | | | | | | 5378.85 | | |

Force Totals (Does not include forces on guys)

| Load Case | Vertical Forces | Sum of Forces X | Sum of Forces Z | Sum of Torques |
|--------------------------|-----------------|-----------------|-----------------|----------------|
| | lb | lb | lb | lb-ft |
| Leg Weight | 2962.57 | | | |
| Bracing Weight | 2154.49 | | | |
| Total Member Self-Weight | 5117.06 | | | |
| Guy Weight | 1060.06 | | | |
| Total Weight | 12070.87 | | | |
| Wind 0 deg - No Ice | | -48.02 | -17294.15 | -2190.32 |
| Wind 30 deg - No Ice | | 8602.30 | -14899.62 | -1364.11 |
| Wind 60 deg - No Ice | | 14927.86 | -8563.16 | -174.34 |
| Wind 90 deg - No Ice | | 17287.77 | 48.02 | 1063.14 |
| Wind 120 deg - No Ice | | 15049.21 | 8688.66 | 2018.28 |
| Wind 150 deg - No Ice | | 8685.47 | 14947.64 | 2427.25 |
| Wind 180 deg - No Ice | | 48.02 | 17209.49 | 2188.48 |
| Wind 210 deg - No Ice | | -8602.30 | 14899.62 | 1364.11 |
| Wind 240 deg - No Ice | | -15001.19 | 8605.49 | 172.04 |
| Wind 270 deg - No Ice | | -17287.77 | -48.02 | -1063.14 |
| Wind 300 deg - No Ice | | -14975.88 | -8646.33 | -2014.14 |
| Wind 330 deg - No Ice | | -8685.47 | -14947.64 | -2427.25 |

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|---|---------|------------|-------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 25 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Load Case | Vertical Forces lb | Sum of Forces X lb | Sum of Forces Z lb | Sum of Torques lb-ft |
|------------------------|-----------------------|--------------------------|--------------------------|-------------------------|
| Member Ice | 3444.36 | | | |
| Guy Ice | 1336.20 | | | |
| Total Weight Ice | 21782.03 | | | |
| Wind 0 deg - Ice | | -37.01 | -18181.20 | -2269.67 |
| Wind 30 deg - Ice | | 9073.06 | -15715.01 | -1300.24 |
| Wind 60 deg - Ice | | 15744.50 | -9047.36 | 16.89 |
| Wind 90 deg - Ice | | 18210.22 | 37.01 | 1330.19 |
| Wind 120 deg - Ice | | 15800.89 | 9122.65 | 2288.16 |
| Wind 150 deg - Ice | | 9137.16 | 15752.01 | 2630.44 |
| Wind 180 deg - Ice | | 37.01 | 18158.82 | 2269.28 |
| Wind 210 deg - Ice | | -9073.06 | 15715.01 | 1300.24 |
| Wind 240 deg - Ice | | -15763.89 | 9058.55 | -18.50 |
| Wind 270 deg - Ice | | -18210.22 | -37.01 | -1330.19 |
| Wind 300 deg - Ice | | -15781.51 | -9111.46 | -2286.18 |
| Wind 330 deg - Ice | | -9137.16 | -15752.01 | -2630.44 |
| Total Weight | 12070.87 | | | |
| Wind 0 deg - Service | | -23.93 | -8617.16 | -1091.37 |
| Wind 30 deg - Service | | 4286.27 | -7424.03 | -679.69 |
| Wind 60 deg - Service | | 7438.10 | -4266.76 | -86.87 |
| Wind 90 deg - Service | | 8613.98 | 23.93 | 529.73 |
| Wind 120 deg - Service | | 7498.57 | 4329.30 | 1005.65 |
| Wind 150 deg - Service | | 4327.71 | 7447.96 | 1209.42 |
| Wind 180 deg - Service | | 23.93 | 8574.97 | 1090.45 |
| Wind 210 deg - Service | | -4286.27 | 7424.03 | 679.69 |
| Wind 240 deg - Service | | -7474.64 | 4287.86 | 85.72 |
| Wind 270 deg - Service | | -8613.98 | -23.93 | -529.73 |
| Wind 300 deg - Service | | -7462.03 | -4308.21 | -1003.58 |
| Wind 330 deg - Service | | -4327.71 | -7447.96 | -1209.42 |

Load Combinations

| Comb. No. | Description |
|-----------|--------------------------------|
| 1 | Dead Only |
| 2 | Dead+Wind 0 deg - No Ice+Guy |
| 3 | Dead+Wind 30 deg - No Ice+Guy |
| 4 | Dead+Wind 60 deg - No Ice+Guy |
| 5 | Dead+Wind 90 deg - No Ice+Guy |
| 6 | Dead+Wind 120 deg - No Ice+Guy |
| 7 | Dead+Wind 150 deg - No Ice+Guy |
| 8 | Dead+Wind 180 deg - No Ice+Guy |
| 9 | Dead+Wind 210 deg - No Ice+Guy |
| 10 | Dead+Wind 240 deg - No Ice+Guy |
| 11 | Dead+Wind 270 deg - No Ice+Guy |
| 12 | Dead+Wind 300 deg - No Ice+Guy |
| 13 | Dead+Wind 330 deg - No Ice+Guy |
| 14 | Dead+Ice+Temp+Guy |
| 15 | Dead+Wind 0 deg+Ice+Temp+Guy |
| 16 | Dead+Wind 30 deg+Ice+Temp+Guy |
| 17 | Dead+Wind 60 deg+Ice+Temp+Guy |
| 18 | Dead+Wind 90 deg+Ice+Temp+Guy |
| 19 | Dead+Wind 120 deg+Ice+Temp+Guy |
| 20 | Dead+Wind 150 deg+Ice+Temp+Guy |
| 21 | Dead+Wind 180 deg+Ice+Temp+Guy |
| 22 | Dead+Wind 210 deg+Ice+Temp+Guy |

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|---|---------|------------|-------------|-------------------|
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| Comb. No. | Description |
|-----------|---------------------------------|
| 23 | Dead+Wind 240 deg+Ice+Temp+Guy |
| 24 | Dead+Wind 270 deg+Ice+Temp+Guy |
| 25 | Dead+Wind 300 deg+Ice+Temp+Guy |
| 26 | Dead+Wind 330 deg+Ice+Temp+Guy |
| 27 | Dead+Wind 0 deg - Service+Guy |
| 28 | Dead+Wind 30 deg - Service+Guy |
| 29 | Dead+Wind 60 deg - Service+Guy |
| 30 | Dead+Wind 90 deg - Service+Guy |
| 31 | Dead+Wind 120 deg - Service+Guy |
| 32 | Dead+Wind 150 deg - Service+Guy |
| 33 | Dead+Wind 180 deg - Service+Guy |
| 34 | Dead+Wind 210 deg - Service+Guy |
| 35 | Dead+Wind 240 deg - Service+Guy |
| 36 | Dead+Wind 270 deg - Service+Guy |
| 37 | Dead+Wind 300 deg - Service+Guy |
| 38 | Dead+Wind 330 deg - Service+Guy |

Maximum Member Forces

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft |
|-------------|----------------|----------------|------------------|-----------------|-----------|-------------------------|-------------------------|
| T1 | 190.6 - 175.35 | Leg | Max Tension | 2 | 2107.15 | 480.54 | -208.71 |
| | | | Max. Compression | 17 | -14927.60 | -63.47 | -79.71 |
| | | | Max. Mx | 6 | -9881.69 | 1224.04 | 289.34 |
| | | | Max. My | 2 | -9815.11 | -293.61 | -1272.61 |
| | | | Max. Vy | 11 | 1231.70 | 255.41 | -2.30 |
| | | | Max. Vx | 2 | 1200.69 | -738.83 | 29.32 |
| | | Diagonal | Max Tension | 5 | 2348.17 | 0.00 | 0.00 |
| | | | Max. Compression | 11 | -2360.27 | 0.00 | 0.00 |
| | | | Max. Mx | 19 | 1075.72 | 3.93 | 0.00 |
| | | | Max. My | 15 | 386.56 | 0.00 | 0.05 |
| | | | Max. Vy | 19 | -3.71 | 0.00 | 0.00 |
| | | | Max. Vx | 15 | -0.04 | 0.00 | 0.00 |
| | | Bottom Girt | Max Tension | 16 | 322.20 | 0.00 | 0.00 |
| | | | Max. Compression | 9 | -275.32 | 0.00 | 0.00 |
| | | | Max. Mx | 14 | 11.37 | 3.17 | 0.00 |
| | | | Max. My | 26 | -260.39 | 0.00 | -0.00 |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 |
| | | Guy A | Bottom Tension | 21 | 12059.01 | | |
| | | | Top Tension | 21 | 12266.46 | | |
| | | | Top Cable Vert | 21 | 11062.29 | | |
| | | | Top Cable Norm | 21 | 5300.17 | | |
| | | | Top Cable Tan | 21 | 0.29 | | |
| | | | Bot Cable Vert | 21 | -10588.12 | | |
| | | | Bot Cable Norm | 21 | 5771.59 | | |
| | | | Bot Cable Tan | 21 | 0.29 | | |
| | | Guy B | Bottom Tension | 25 | 12183.90 | | |
| | | | Top Tension | 25 | 12399.22 | | |
| | | | Top Cable Vert | 25 | 11202.52 | | |
| | | | Top Cable Norm | 25 | 5314.52 | | |
| | | | Top Cable Tan | 25 | 2.82 | | |
| | | | Bot Cable Vert | 25 | -10714.65 | | |
| | | | Bot Cable Norm | 25 | 5800.31 | | |
| | | | Bot Cable Tan | 25 | 2.82 | | |
| | | Guy C | Bottom Tension | 18 | 12142.45 | | |
| | | | Top Tension | 18 | 12356.68 | | |
| | | | Top Cable Vert | 18 | 11162.37 | | |
| | | | Top Cable Norm | 18 | 5299.29 | | |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft | |
|-------------|------------------|------------------|------------------|------------------|-----------|-------------------------|-------------------------|-------|
| T2 | 175.35 - 160.1 | Top Guy Pull-Off | Top Cable Tan | 18 | 81.25 | | | |
| | | | Bot Cable Vert | 18 | -10700.52 | | | |
| | | | Bot Cable Norm | 18 | 5734.46 | | | |
| | | | Bot Cable Tan | 18 | 232.07 | | | |
| | | | Max Tension | 26 | 3362.87 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 761.10 | 11.89 | 0.00 | |
| | | | Max. My | 26 | 634.96 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | -13.74 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | 0.00 | 0.00 | 0.00 | |
| | | | Max Tension | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Compression | 19 | -13270.75 | 238.52 | 171.85 | |
| | | Max. Mx | 18 | -5477.61 | 297.47 | -54.21 | | |
| | | Max. My | 21 | -4486.70 | -9.31 | 303.28 | | |
| | | Max. Vy | 18 | 673.60 | -202.31 | -60.14 | | |
| | | Max. Vx | 15 | -651.74 | -62.44 | 208.60 | | |
| | | Diagonal | Max Tension | 18 | 1896.86 | 0.00 | 0.00 | |
| | | | Max. Compression | 20 | -1934.84 | 0.00 | 0.00 | |
| | | | Max. Mx | 19 | 1330.23 | 3.93 | 0.00 | |
| | | | Max. My | 19 | -3.17 | 0.00 | -0.04 | |
| | | | Max. Vy | 19 | -3.71 | 0.00 | 0.00 | |
| | | | Max. Vx | 19 | -0.04 | 0.00 | 0.00 | |
| | | | Top Girt | Max Tension | 25 | 342.39 | 0.00 | 0.00 |
| | | | | Max. Compression | 19 | -349.78 | 0.00 | 0.00 |
| | | | | Max. Mx | 14 | 11.43 | 3.17 | 0.00 |
| | | | | Max. My | 26 | 329.03 | 0.00 | -0.00 |
| | | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 |
| | | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 |
| | | Bottom Girt | Max Tension | 19 | 757.34 | 0.00 | 0.00 | |
| | | | Max. Compression | 18 | -676.24 | 0.00 | 0.00 | |
| Max. Mx | 14 | | 7.47 | 3.17 | 0.00 | | | |
| Max. My | 26 | | -675.23 | 0.00 | -0.00 | | | |
| Max. Vy | 14 | | 3.66 | 0.00 | 0.00 | | | |
| Max. Vx | 26 | | -0.00 | 0.00 | 0.00 | | | |
| Leg | Max Tension | | 12 | 14165.60 | 44.82 | 24.14 | | |
| | Max. Compression | | 19 | -34169.81 | -148.34 | -74.68 | | |
| | Max. Mx | | 18 | -4401.88 | 297.45 | -54.18 | | |
| | Max. My | | 15 | -13918.30 | -25.92 | 310.48 | | |
| | Max. Vy | | 24 | -916.16 | 294.25 | -60.02 | | |
| | Max. Vx | | 15 | -974.40 | -25.92 | 310.48 | | |
| | Diagonal | Max Tension | 3 | 1996.06 | 0.00 | 0.00 | | |
| | | Max. Compression | 5 | -2121.40 | 0.00 | 0.00 | | |
| | | Max. Mx | 19 | 816.38 | 3.92 | 0.00 | | |
| | | Max. My | 15 | -44.84 | 0.00 | 0.04 | | |
| | | Max. Vy | 19 | -3.71 | 0.00 | 0.00 | | |
| | | Max. Vx | 15 | -0.04 | 0.00 | 0.00 | | |
| Top Girt | Max Tension | 18 | 305.48 | 0.00 | 0.00 | | | |
| | Max. Compression | 7 | -141.42 | 0.00 | 0.00 | | | |
| | Max. Mx | 14 | 53.54 | 3.17 | 0.00 | | | |
| | Max. My | 26 | -28.01 | 0.00 | -0.00 | | | |
| | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | | | |
| | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| Bottom Girt | Max Tension | 21 | 2465.94 | 0.00 | 0.00 | | | |
| | Max. Compression | 6 | -1636.80 | 0.00 | 0.00 | | | |
| | Max. Mx | 14 | 280.30 | 3.17 | 0.00 | | | |
| | Max. My | 26 | 541.88 | 0.00 | -0.00 | | | |
| | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | | | |
| | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| Leg | Max Tension | 12 | 15973.54 | 36.53 | 28.57 | | | |
| | Max. Compression | 19 | -36464.83 | -135.52 | -70.80 | | | |
| | Max. Mx | 18 | -5985.96 | -1619.63 | -445.89 | | | |
| | Max. My | 26 | -6422.60 | 413.09 | 1631.03 | | | |
| | | | | | | | | |
| | | | | | | | | |

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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft |
|-------------|---------------|----------------|------------------|-----------------|-----------|-------------------------|-------------------------|
| | | | Max. Vy | 24 | -2664.86 | 1619.07 | -441.31 |
| | | | Max. Vx | 26 | -2693.61 | 413.09 | 1631.03 |
| | | Diagonal | Max Tension | 21 | 1203.93 | 0.00 | 0.00 |
| | | | Max. Compression | 22 | -1506.92 | 0.00 | 0.00 |
| | | | Max. Mx | 19 | -1370.09 | 3.91 | 0.00 |
| | | | Max. My | 15 | -690.58 | 0.00 | 0.03 |
| | | | Max. Vy | 19 | -3.70 | 0.00 | 0.00 |
| | | | Max. Vx | 15 | -0.03 | 0.00 | 0.00 |
| | | Top Girt | Max Tension | 21 | 2389.99 | 0.00 | 0.00 |
| | | | Max. Compression | 23 | -2484.63 | 0.00 | 0.00 |
| | | | Max. Mx | 14 | -4.23 | 3.17 | 0.00 |
| | | | Max. My | 26 | -120.18 | 0.00 | -0.00 |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 |
| | | Bottom Girt | Max Tension | 23 | 272.75 | 0.00 | 0.00 |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 |
| | | | Max. Mx | 14 | 128.38 | 3.17 | 0.00 |
| | | | Max. My | 26 | 245.24 | 0.00 | -0.00 |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 |
| | | Guy A | Bottom Tension | 20 | 10598.85 | | |
| | | | Top Tension | 20 | 10750.80 | | |
| | | | Top Cable Vert | 20 | 8940.65 | | |
| | | | Top Cable Norm | 20 | 5969.92 | | |
| | | | Top Cable Tan | 20 | 67.52 | | |
| | | | Bot Cable Vert | 20 | -8586.24 | | |
| | | | Bot Cable Norm | 20 | 6211.89 | | |
| | | | Bot Cable Tan | 20 | 157.10 | | |
| | | Guy B | Bottom Tension | 26 | 10638.88 | | |
| | | | Top Tension | 26 | 10798.78 | | |
| | | | Top Cable Vert | 26 | 9045.04 | | |
| | | | Top Cable Norm | 26 | 5898.78 | | |
| | | | Top Cable Tan | 26 | 72.52 | | |
| | | | Bot Cable Vert | 26 | -8677.88 | | |
| | | | Bot Cable Norm | 26 | 6152.63 | | |
| | | | Bot Cable Tan | 26 | 159.29 | | |
| | | Guy C | Bottom Tension | 18 | 10467.42 | | |
| | | | Top Tension | 18 | 10627.89 | | |
| | | | Top Cable Vert | 18 | 8920.57 | | |
| | | | Top Cable Norm | 18 | 5776.71 | | |
| | | | Top Cable Tan | 18 | 72.57 | | |
| | | | Bot Cable Vert | 18 | -8553.20 | | |
| | | | Bot Cable Norm | 18 | 6031.94 | | |
| | | | Bot Cable Tan | 18 | 159.68 | | |
| | | Torque Arm Top | Max Tension | 22 | 6115.92 | 0.00 | 0.00 |
| | | | Max. Compression | 9 | -2667.70 | 0.00 | 0.00 |
| | | | Max. Mx | 18 | 208.35 | -31577.12 | -0.00 |
| | | | Max. My | 26 | -962.18 | -17950.01 | -0.00 |
| | | | Max. Vy | 18 | 8845.14 | -31577.12 | -0.00 |
| | | | Max. Vx | 26 | -0.00 | -17950.01 | -0.00 |
| T5 | 120.1 - 100.1 | Leg | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
| | | | Max. Compression | 19 | -28353.30 | -193.74 | -66.75 |
| | | | Max. Mx | 19 | -28353.30 | -193.74 | -66.75 |
| | | | Max. My | 15 | -27826.35 | -45.63 | 196.64 |
| | | | Max. Vy | 25 | 393.60 | 72.69 | -13.63 |
| | | | Max. Vx | 21 | -397.86 | 66.77 | -154.81 |
| | | Diagonal | Max Tension | 26 | 486.14 | 0.00 | 0.00 |
| | | | Max. Compression | 15 | -751.60 | 0.00 | 0.00 |
| | | | Max. Mx | 15 | -353.26 | 3.90 | 0.00 |
| | | | Max. My | 15 | -396.59 | 0.00 | 0.03 |
| | | | Max. Vy | 15 | -3.69 | 0.00 | 0.00 |
| | | | Max. Vx | 15 | -0.03 | 0.00 | 0.00 |

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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft | |
|------------------|----------------|------------------|------------------|------------------|-----------|-------------------------|-------------------------|------|
| T6 | 100.1 - 80.1 | Top Girt | Max Tension | 20 | 346.80 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 135.46 | 3.17 | 0.00 | |
| | | | Max. My | 26 | 230.93 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | Bottom Girt | Max Tension | 18 | 366.25 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 142.23 | 3.17 | 0.00 | |
| | | | Max. My | 26 | 264.32 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | Leg | Max Tension | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Compression | 15 | -33345.07 | 2.10 | -42.29 | |
| | | | Max. Mx | 24 | -28576.45 | 171.94 | -35.86 | |
| | | | Max. My | 15 | -28594.26 | 23.52 | 193.83 | |
| | | | Max. Vy | 17 | 319.95 | -53.97 | 28.01 | |
| | | | Max. Vx | 26 | -342.38 | -6.62 | 76.13 | |
| | | | Diagonal | Max Tension | 24 | 1082.68 | 0.00 | 0.00 |
| | | | | Max. Compression | 15 | -1210.82 | 0.00 | 0.00 |
| | | | | Max. Mx | 15 | 107.18 | 3.89 | 0.00 |
| | | | | Max. My | 26 | -181.83 | 0.00 | 0.03 |
| | | Max. Vy | | 15 | -3.69 | 0.00 | 0.00 | |
| | | Top Girt | Max. Vx | 26 | -0.03 | 0.00 | 0.00 | |
| | | | Max Tension | 15 | 296.10 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 154.72 | 3.17 | 0.00 | |
| | | | Max. My | 26 | 262.84 | 0.00 | -0.00 | |
| | | Bottom Girt | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | | Max Tension | 23 | 449.27 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 227.27 | 3.17 | 0.00 | |
| | | Guy A | Max. My | 26 | 397.65 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | | Bottom Tension | 21 | 7111.85 | | | |
| | | | Top Tension | 21 | 7193.11 | | | |
| | | | Top Cable Vert | 21 | 5642.35 | | | |
| | | | Top Cable Norm | 21 | 4461.46 | | | |
| | | | Top Cable Tan | 21 | 1.30 | | | |
| | | | Bot Cable Vert | 21 | -5436.36 | | | |
| Bot Cable Norm | 21 | | 4585.24 | | | | | |
| Guy B | Bot Cable Tan | 21 | 1.30 | | | | | |
| | Bottom Tension | 25 | 7270.12 | | | | | |
| | Top Tension | 25 | 7350.41 | | | | | |
| | Top Cable Vert | 25 | 5811.46 | | | | | |
| | Top Cable Norm | 25 | 4500.61 | | | | | |
| | Top Cable Tan | 25 | 1.34 | | | | | |
| | Bot Cable Vert | 25 | -5608.88 | | | | | |
| | Bot Cable Norm | 25 | 4625.47 | | | | | |
| | Bot Cable Tan | 25 | 1.34 | | | | | |
| | Guy C | Bottom Tension | 17 | 7211.16 | | | | |
| Top Tension | | 17 | 7293.25 | | | | | |
| Top Cable Vert | | 17 | 5711.17 | | | | | |
| Top Cable Norm | | 17 | 4535.86 | | | | | |
| Top Cable Tan | | 17 | 0.17 | | | | | |
| Bot Cable Vert | | 17 | -5503.06 | | | | | |
| Bot Cable Norm | | 17 | 4660.16 | | | | | |
| Bot Cable Tan | | 17 | 0.17 | | | | | |
| Top Guy Pull-Off | | Max Tension | 15 | 2738.20 | 0.00 | 0.00 | | |
| | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | | |

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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft | |
|----------------|------------------|----------------|------------------|------------------|-----------|-------------------------|-------------------------|---------|
| T7 | 80.1 - 60.1 | Leg | Max. Mx | 14 | 1286.37 | 12.95 | 0.00 | |
| | | | Max. My | 26 | 2131.13 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | 14.98 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | | Max Tension | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Compression | 15 | -31342.51 | 15.37 | -25.78 | |
| | | | Max. Mx | 24 | -19732.59 | -210.54 | -52.23 | |
| | | | Max. My | 21 | -19071.05 | -8.29 | 223.06 | |
| | | | Max. Vy | 24 | 483.85 | 85.65 | -15.94 | |
| | | | Max. Vx | 21 | -500.22 | 8.32 | -83.37 | |
| | | | Max Tension | 24 | 485.08 | 0.00 | 0.00 | |
| | | | Max. Compression | 24 | -767.56 | 0.00 | 0.00 | |
| | | Diagonal | Max. Mx | 15 | -587.82 | 3.88 | 0.00 | |
| | | | Max. My | 26 | -494.84 | 0.00 | 0.03 | |
| | | | Max. Vy | 15 | -3.68 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.03 | 0.00 | 0.00 | |
| | | | Top Girt | Max Tension | 18 | 393.71 | 0.00 | 0.00 |
| | | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 |
| | | | | Max. Mx | 14 | 165.68 | 3.17 | 0.00 |
| | | | | Max. My | 26 | 280.16 | 0.00 | -0.00 |
| | | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 |
| | | | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 |
| | | | Bottom Girt | Max Tension | 19 | 324.51 | 0.00 | 0.00 |
| | | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 |
| | | Max. Mx | | 17 | 256.49 | 3.17 | 0.00 | |
| | | Max. My | | 26 | 287.47 | 0.00 | -0.00 | |
| | | Max. Vy | | 17 | 3.66 | 0.00 | 0.00 | |
| | | Max. Vx | | 26 | -0.00 | 0.00 | 0.00 | |
| T8 | 60.1 - 40.1 | Leg | | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
| | | | | Max. Compression | 15 | -34332.30 | -171.07 | -187.55 |
| | | | | Max. Mx | 19 | -33891.14 | -347.60 | 9.78 |
| | | | | Max. My | 15 | -32884.75 | 49.18 | 366.57 |
| | | | Max. Vy | 19 | -252.83 | -347.60 | 9.78 | |
| | | | Max. Vx | 15 | -235.31 | 49.18 | 366.57 | |
| | | Diagonal | Max Tension | 20 | 1417.38 | 0.00 | 0.00 | |
| | | | Max. Compression | 26 | -1721.11 | 0.00 | 0.00 | |
| | | | Max. Mx | 23 | 283.96 | 3.88 | 0.00 | |
| | | | Max. My | 26 | 252.95 | 0.00 | 0.03 | |
| | | | Max. Vy | 23 | -3.68 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | -0.03 | 0.00 | 0.00 | |
| Top Girt | Max Tension | 21 | 242.68 | 0.00 | 0.00 | | | |
| | Max. Compression | 15 | -79.82 | 0.00 | 0.00 | | | |
| | Max. Mx | 17 | 5.25 | 3.17 | 0.00 | | | |
| | Max. My | 26 | 192.48 | 0.00 | -0.00 | | | |
| | Max. Vy | 17 | 3.66 | 0.00 | 0.00 | | | |
| | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| Bottom Girt | Max Tension | 26 | 628.50 | 0.00 | 0.00 | | | |
| | Max. Compression | 20 | -337.38 | 0.00 | 0.00 | | | |
| | Max. Mx | 17 | 53.87 | 3.17 | 0.00 | | | |
| | Max. My | 26 | 628.47 | 0.00 | -0.00 | | | |
| | Max. Vy | 17 | 3.66 | 0.00 | 0.00 | | | |
| | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| | Guy A | Bottom Tension | 21 | 4882.29 | | | | |
| | | Top Tension | 21 | 4915.99 | | | | |
| | | Top Cable Vert | 21 | 2604.68 | | | | |
| | | Top Cable Norm | 21 | 4169.24 | | | | |
| Top Cable Tan | | 21 | 1.03 | | | | | |
| Bot Cable Vert | | 21 | -2500.12 | | | | | |
| Bot Cable Norm | | 21 | 4193.58 | | | | | |
| Bot Cable Tan | | 21 | 1.03 | | | | | |
| Guy B | | Bottom Tension | 25 | 4948.01 | | | | |
| | | Top Tension | 25 | 4980.93 | | | | |

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|---|----------------|------------|--------------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 31 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft |
|------------------|--------------|------------------|----------------|-----------------|----------|-------------------------|-------------------------|
| T9 | 40.1 - 20.1 | Guy C | Top Cable Vert | 25 | 2656.55 | | |
| | | | Top Cable Norm | 25 | 4213.36 | | |
| | | | Top Cable Tan | 25 | 0.98 | | |
| | | | Bot Cable Vert | 25 | -2554.67 | | |
| | | | Bot Cable Norm | 25 | 4237.51 | | |
| | | | Bot Cable Tan | 25 | 0.98 | | |
| | | | Bottom Tension | 17 | 4850.51 | | |
| | | | Top Tension | 17 | 4884.91 | | |
| | | | Top Cable Vert | 17 | 2600.76 | | |
| | | | Top Cable Norm | 17 | 4135.02 | | |
| | | | Top Cable Tan | 17 | 0.26 | | |
| | | | Bot Cable Vert | 17 | -2494.20 | | |
| | | Bot Cable Norm | 17 | 4160.10 | | | |
| | | Bot Cable Tan | 17 | 0.26 | | | |
| | | Top Guy Pull-Off | 26 | 2492.50 | 0.00 | 0.00 | |
| | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | Max. Mx | 17 | 728.64 | 12.95 | 0.00 | |
| | | Max. My | 26 | 627.98 | 0.00 | -0.00 | |
| | | Max. Vy | 17 | 14.98 | 0.00 | 0.00 | |
| | | Max. Vx | 26 | -0.00 | 0.00 | 0.00 | |
| | | Leg | 1 | 0.00 | 0.00 | 0.00 | |
| | | Max. Compression | 15 | -32375.15 | 104.69 | -72.64 | |
| | | Max. Mx | 19 | -32125.80 | -331.54 | -174.38 | |
| | | Max. My | 15 | -32371.56 | 49.18 | 366.57 | |
| | | Max. Vy | 23 | 743.29 | 314.51 | -211.26 | |
| | | Max. Vx | 15 | 716.14 | 49.18 | 366.57 | |
| | | Diagonal | 26 | 1321.97 | 0.00 | 0.00 | |
| | | Max. Compression | 20 | -1533.48 | 0.00 | 0.00 | |
| | | Max. Mx | 22 | -216.13 | 3.88 | 0.00 | |
| | | Max. My | 26 | -433.22 | 0.00 | 0.02 | |
| | | Max. Vy | 22 | -3.67 | 0.00 | 0.00 | |
| | | Max. Vx | 26 | -0.02 | 0.00 | 0.00 | |
| | | Top Girt | 20 | 495.19 | 0.00 | 0.00 | |
| Max. Compression | 26 | -370.90 | 0.00 | 0.00 | | | |
| Max. Mx | 19 | 16.67 | 3.17 | 0.00 | | | |
| Max. My | 26 | -370.90 | 0.00 | -0.00 | | | |
| Max. Vy | 19 | 3.66 | 0.00 | 0.00 | | | |
| Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| Bottom Girt | 26 | 256.94 | 0.00 | 0.00 | | | |
| Max. Compression | 19 | -132.71 | 0.00 | 0.00 | | | |
| Max. Mx | 14 | 45.78 | 3.17 | 0.00 | | | |
| Max. My | 26 | 256.91 | 0.00 | -0.00 | | | |
| Max. Vy | 14 | 3.66 | 0.00 | 0.00 | | | |
| Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |
| Leg | 1 | 0.00 | 0.00 | 0.00 | | | |
| Max. Compression | 19 | -29043.85 | -511.50 | 546.85 | | | |
| Max. Mx | 19 | -27275.20 | 684.29 | 134.19 | | | |
| Max. My | 23 | -28758.49 | -106.65 | -708.15 | | | |
| Max. Vy | 19 | -338.75 | -127.30 | 100.17 | | | |
| Max. Vx | 22 | 322.03 | -165.52 | -698.37 | | | |
| Diagonal | 21 | 1089.13 | 0.00 | 0.00 | | | |
| Max. Compression | 19 | -644.39 | 0.00 | 0.00 | | | |
| Max. Mx | 22 | 817.25 | 3.89 | 0.00 | | | |
| Max. My | 26 | 296.64 | 0.00 | 0.02 | | | |
| Max. Vy | 22 | -3.67 | 0.00 | 0.00 | | | |
| Max. Vx | 26 | -0.02 | 0.00 | 0.00 | | | |
| Top Girt | 20 | 240.53 | 0.00 | 0.00 | | | |
| Max. Compression | 26 | -104.25 | 0.00 | 0.00 | | | |
| Max. Mx | 14 | 43.83 | 3.17 | 0.00 | | | |
| Max. My | 26 | -104.25 | 0.00 | -0.00 | | | |
| Max. Vy | 14 | 3.66 | 0.00 | 0.00 | | | |
| Max. Vx | 26 | -0.00 | 0.00 | 0.00 | | | |

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|---|---------|------------|-------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 32 of 49 |
| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Condition | Gov. Load Comb. | Force lb | Major Axis Moment lb-ft | Minor Axis Moment lb-ft | |
|-------------|--------------|----------------|------------------|------------------|-----------|-------------------------|-------------------------|--------|
| T11 | 4.85 - 0 | Bottom Girt | Max Tension | 15 | 3939.21 | 0.00 | 0.00 | |
| | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Mx | 14 | 2289.95 | 3.17 | 0.00 | |
| | | | Max. My | 26 | 3651.50 | 0.00 | -0.00 | |
| | | | Max. Vy | 14 | 3.66 | 0.00 | 0.00 | |
| | | | Max. Vx | 26 | 0.00 | 0.00 | 0.00 | |
| | | Leg | Max Tension | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Compression | 19 | -30987.80 | 45.10 | 238.38 | |
| | | | Max. Mx | 15 | -29008.58 | -2507.63 | -144.25 | |
| | | | Max. My | 26 | -28217.69 | -531.86 | -711.69 | |
| | | | Max. Vy | 15 | 4413.25 | -2507.63 | -144.25 | |
| | | | Max. Vx | 26 | 1521.41 | -531.86 | -711.69 | |
| | | | Top Girt | Max Tension | 15 | 2777.82 | -1869.62 | -10.69 |
| | | | | Max. Compression | 1 | 0.00 | 0.00 | 0.00 |
| | | | | Max. Mx | 26 | 2706.23 | -1902.66 | -12.20 |
| | | | | Max. My | 26 | 2706.23 | -1902.66 | -12.20 |
| | | Max. Vy | | 26 | 337.16 | -1902.66 | -12.20 | |
| | | Bottom Girt | Max. Vx | 26 | 11.17 | -1774.39 | -12.19 | |
| | | | Max Tension | 1 | 0.00 | 0.00 | 0.00 | |
| | | | Max. Compression | 19 | -873.15 | -1131.12 | -6.87 | |
| | | | Max. Mx | 26 | -832.25 | -1352.50 | -13.10 | |
| | | | Max. My | 26 | -832.25 | -1352.50 | -13.10 | |
| | | | Max. Vy | 26 | 3865.33 | -1352.50 | -13.10 | |
| | | Mid Girt | Max. Vx | 26 | 55.21 | -1352.50 | -13.10 | |
| | | | Max Tension | 19 | 64.54 | 0.00 | 0.00 | |
| | | | Max. Compression | 19 | -154.89 | 0.00 | 0.00 | |
| | | | Max. Mx | 21 | 54.94 | 8.34 | 0.00 | |
| Max. My | 25 | | 37.55 | 0.00 | 1.72 | | | |
| Max. Vy | 21 | | 15.52 | 0.00 | 0.00 | | | |
| Max. Vx | 25 | | 3.20 | 0.00 | 0.00 | | | |

Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical lb | Horizontal, X lb | Horizontal, Z lb | |
|-----------------------------------|---|---------------------|-------------|------------------|------------------|---------|
| Mast | Max. Vert | 19 | 84524.91 | -276.92 | -159.14 | |
| | Max. H _x | 12 | 51827.05 | 642.64 | 378.45 | |
| | Max. H _z | 2 | 65711.52 | -7.91 | 468.34 | |
| | Max. M _x | 1 | 0.00 | -6.09 | -2.92 | |
| | Max. M _z | 1 | 0.00 | -6.09 | -2.92 | |
| | Max. Torsion | 26 | 940.17 | 343.26 | 294.10 | |
| | Min. Vert | 1 | 39747.68 | -6.09 | -2.92 | |
| | Min. H _x | 4 | 51586.01 | -657.02 | 387.35 | |
| | Min. H _z | 8 | 51808.68 | 0.79 | -780.71 | |
| | Min. M _x | 1 | 0.00 | -6.09 | -2.92 | |
| | Min. M _z | 1 | 0.00 | -6.09 | -2.92 | |
| | Min. Torsion | 20 | -1066.67 | -101.68 | -496.52 | |
| | Guy C @ 99 ft Elev -5.17 ft Azimuth 240 deg | Max. Vert | 35 | -1175.00 | -546.53 | 315.52 |
| | | Max. H _x | 10 | -1221.68 | -421.96 | 243.83 |
| | | Max. H _z | 16 | -27273.24 | -14860.29 | 9183.54 |
| Min. Vert | | 18 | -27537.84 | -15522.74 | 8355.88 | |
| Min. H _x | | 18 | -27537.84 | -15522.74 | 8355.88 | |
| Min. H _z | | 10 | -1221.68 | -421.96 | 243.83 | |
| Guy B @ 99.25 ft Elev -4.67 ft | Max. Vert | 31 | -1126.79 | 524.95 | 304.03 | |

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|---|---------|------------|-------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Location | Condition | Gov. Load Comb. | Vertical lb | Horizontal, X lb | Horizontal, Z lb |
|---|---------------------|-----------------|-------------|------------------|------------------|
| Azimuth 120 deg | Max. H _x | 24 | -27507.27 | 15589.69 | 8395.63 |
| | Max. H _z | 26 | -27337.34 | 14978.87 | 9237.14 |
| | Min. Vert | 24 | -27507.27 | 15589.69 | 8395.63 |
| | Min. H _x | 6 | -1196.90 | 413.68 | 239.26 |
| | Min. H _z | 6 | -1196.90 | 413.68 | 239.26 |
| | Max. Vert | 27 | -1007.47 | -0.91 | -543.46 |
| Guy A @ 96.5 ft Elev 2.46 ft Azimuth 0 deg | Max. H _x | 24 | -15163.05 | 926.04 | -9600.88 |
| | Max. H _z | 2 | -1106.21 | -0.20 | -441.01 |
| | Min. Vert | 21 | -27137.09 | 7.92 | -17794.95 |
| | Min. H _x | 18 | -15251.41 | -927.89 | -9649.74 |
| | Min. H _z | 21 | -27137.09 | 7.92 | -17794.95 |
| | Max. Vert | 10 | -144.85 | -84.48 | 48.78 |
| Guy C @ 71.5 ft Elev 2.125 ft Azimuth 240 deg | Max. H _x | 10 | -144.85 | -84.48 | 48.78 |
| | Max. H _z | 17 | -7997.26 | -7638.36 | 4410.50 |
| | Min. Vert | 17 | -7997.26 | -7638.36 | 4410.50 |
| | Min. H _x | 17 | -7997.26 | -7638.36 | 4410.50 |
| | Min. H _z | 10 | -144.85 | -84.48 | 48.78 |
| | Max. Vert | 6 | -147.71 | 82.89 | 47.89 |
| Guy B @ 68.25 ft Elev 3.96 ft Azimuth 120 deg | Max. H _x | 25 | -8163.55 | 7676.73 | 4429.49 |
| | Max. H _z | 25 | -8163.55 | 7676.73 | 4429.49 |
| | Min. Vert | 25 | -8163.55 | 7676.73 | 4429.49 |
| | Min. H _x | 6 | -147.71 | 82.89 | 47.89 |
| | Min. H _z | 6 | -147.71 | 82.89 | 47.89 |
| | Max. Vert | 2 | -142.44 | -0.03 | -95.59 |
| Guy A @ 70.5 ft Elev 3 ft Azimuth 0 deg | Max. H _x | 24 | -4201.34 | 238.75 | -4614.19 |
| | Max. H _z | 2 | -142.44 | -0.03 | -95.59 |
| | Min. Vert | 21 | -7936.48 | 2.33 | -8778.83 |
| | Min. H _x | 18 | -4160.06 | -238.55 | -4564.58 |
| | Min. H _z | 21 | -7936.48 | 2.33 | -8778.83 |

Tower Mast Reaction Summary

| Load Combination | Vertical lb | Shear _x lb | Shear _z lb | Overturing Moment, M _x lb-ft | Overturing Moment, M _z lb-ft | Torque lb-ft |
|--------------------------------|-------------|-----------------------|-----------------------|---|---|--------------|
| Dead Only | 39747.68 | 6.09 | 2.92 | 0.00 | 0.00 | 34.32 |
| Dead+Wind 0 deg - No Ice+Guy | 65711.52 | 7.91 | -468.34 | 0.00 | 0.00 | -703.68 |
| Dead+Wind 30 deg - No Ice+Guy | 60574.51 | 413.52 | -422.72 | 0.00 | 0.00 | -386.49 |
| Dead+Wind 60 deg - No Ice+Guy | 51586.01 | 657.02 | -387.35 | 0.00 | 0.00 | 23.38 |
| Dead+Wind 90 deg - No Ice+Guy | 60861.47 | 576.20 | -131.15 | 0.00 | 0.00 | 440.69 |
| Dead+Wind 120 deg - No Ice+Guy | 65764.30 | 425.33 | 261.05 | 0.00 | 0.00 | 779.64 |
| Dead+Wind 150 deg - No Ice+Guy | 60685.22 | 179.11 | 593.08 | 0.00 | 0.00 | 930.25 |
| Dead+Wind 180 deg - No Ice+Guy | 51808.68 | -0.79 | 780.71 | 0.00 | 0.00 | 842.63 |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

| Load Combination | Vertical lb | Shear _x lb | Shear _z lb | Overturning Moment, M _x lb-ft | Overturning Moment, M _z lb-ft | Torque lb-ft |
|---------------------------------|----------------|--------------------------|--------------------------|---|---|-----------------|
| Ice+Guy | | | | | | |
| Dead+Wind 210 deg - No Ice+Guy | 60437.12 | -173.96 | 592.76 | 0.00 | 0.00 | 490.17 |
| Dead+Wind 240 deg - No Ice+Guy | 65510.14 | -413.22 | 261.77 | 0.00 | 0.00 | 90.60 |
| Dead+Wind 270 deg - No Ice+Guy | 60782.94 | -560.76 | -127.52 | 0.00 | 0.00 | -328.78 |
| Dead+Wind 300 deg - No Ice+Guy | 51827.05 | -642.64 | -378.45 | 0.00 | 0.00 | -750.57 |
| Dead+Wind 330 deg - No Ice+Guy | 60745.84 | -398.43 | -416.69 | 0.00 | 0.00 | -841.35 |
| Dead+Ice+Temp+Guy | 52083.34 | 26.24 | -4.06 | 0.00 | 0.00 | 46.00 |
| Dead+Wind 0 deg+Ice+Temp+Guy | 84409.75 | 30.07 | -281.60 | 0.00 | 0.00 | -732.25 |
| Dead+Wind 30 deg+Ice+Temp+Guy | 80156.44 | 402.86 | -301.63 | 0.00 | 0.00 | -336.13 |
| Dead+Wind 60 deg+Ice+Temp+Guy | 73512.17 | 590.44 | -347.47 | 0.00 | 0.00 | 129.75 |
| Dead+Wind 90 deg+Ice+Temp+Guy | 80482.38 | 466.32 | -175.72 | 0.00 | 0.00 | 566.36 |
| Dead+Wind 120 deg+Ice+Temp+Guy | 84524.91 | 276.92 | 159.14 | 0.00 | 0.00 | 922.52 |
| Dead+Wind 150 deg+Ice+Temp+Guy | 80356.33 | 101.68 | 496.52 | 0.00 | 0.00 | 1066.67 |
| Dead+Wind 180 deg+Ice+Temp+Guy | 73838.94 | 21.07 | 679.36 | 0.00 | 0.00 | 900.05 |
| Dead+Wind 210 deg+Ice+Temp+Guy | 80334.61 | -52.82 | 494.75 | 0.00 | 0.00 | 471.10 |
| Dead+Wind 240 deg+Ice+Temp+Guy | 84486.60 | -218.77 | 158.64 | 0.00 | 0.00 | 30.60 |
| Dead+Wind 270 deg+Ice+Temp+Guy | 80612.60 | -404.27 | -171.72 | 0.00 | 0.00 | -413.63 |
| Dead+Wind 300 deg+Ice+Temp+Guy | 73817.50 | -530.13 | -337.71 | 0.00 | 0.00 | -850.62 |
| Dead+Wind 330 deg+Ice+Temp+Guy | 80308.63 | -343.26 | -294.10 | 0.00 | 0.00 | -940.17 |
| Dead+Wind 0 deg - Service+Guy | 42193.18 | 6.80 | -455.70 | 0.00 | 0.00 | -348.44 |
| Dead+Wind 30 deg - Service+Guy | 42053.42 | 218.16 | -370.86 | 0.00 | 0.00 | -162.48 |
| Dead+Wind 60 deg - Service+Guy | 41771.61 | 365.56 | -209.04 | 0.00 | 0.00 | 24.71 |
| Dead+Wind 90 deg - Service+Guy | 42267.25 | 429.55 | 2.86 | 0.00 | 0.00 | 212.88 |
| Dead+Wind 120 deg - Service+Guy | 42425.39 | 397.33 | 232.90 | 0.00 | 0.00 | 400.59 |
| Dead+Wind 150 deg - Service+Guy | 42411.14 | 217.40 | 376.41 | 0.00 | 0.00 | 484.11 |
| Dead+Wind 180 deg - Service+Guy | 42115.91 | 4.30 | 425.10 | 0.00 | 0.00 | 405.73 |
| Dead+Wind 210 deg - Service+Guy | 42386.80 | -208.37 | 376.72 | 0.00 | 0.00 | 236.30 |
| Dead+Wind 240 deg - Service+Guy | 42423.03 | -387.04 | 234.32 | 0.00 | 0.00 | 51.42 |
| Dead+Wind 270 deg - Service+Guy | 42334.98 | -416.83 | 5.14 | 0.00 | 0.00 | -138.57 |
| Dead+Wind 300 deg - Service+Guy | 41892.74 | -351.54 | -206.56 | 0.00 | 0.00 | -323.28 |
| Dead+Wind 330 deg - Service+Guy | 42152.14 | -204.22 | -369.16 | 0.00 | 0.00 | -420.29 |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
| | Client T-Mobile | Designed by Kelly Shanahan |

Solution Summary

| Load Comb. | Sum of Applied Forces | | | Sum of Reactions | | | % Error |
|------------|-----------------------|-----------|-----------|------------------|----------|-----------|---------|
| | PX lb | PY lb | PZ lb | PX lb | PY lb | PZ lb | |
| 1 | 0.00 | -12070.67 | 0.00 | 0.39 | 12070.65 | -1.94 | 0.016% |
| 2 | -49.24 | -12132.92 | -19414.63 | 49.24 | 12132.86 | 19413.42 | 0.005% |
| 3 | 9660.98 | -12077.02 | -16734.08 | -9660.99 | 12076.98 | 16733.24 | 0.004% |
| 4 | 16764.01 | -12019.46 | -9622.06 | -16763.64 | 12019.45 | 9622.59 | 0.003% |
| 5 | 19408.16 | -12072.09 | 48.93 | -19407.08 | 12072.03 | -48.32 | 0.005% |
| 6 | 16886.96 | -12124.27 | 9749.90 | -16886.13 | 12124.22 | -9749.45 | 0.004% |
| 7 | 9746.42 | -12065.72 | 16784.22 | -9745.37 | 12065.67 | -16783.66 | 0.005% |
| 8 | 49.24 | -12008.39 | 19329.96 | -48.57 | 12008.39 | -19329.90 | 0.003% |
| 9 | -9660.98 | -12064.29 | 16734.08 | 9659.99 | 12064.24 | -16733.56 | 0.005% |
| 10 | -16837.33 | -12121.86 | 9664.39 | 16836.56 | 12121.81 | -9663.97 | 0.004% |
| 11 | -19408.16 | -12069.22 | -48.93 | 19407.14 | 12069.17 | 49.51 | 0.005% |
| 12 | -16813.63 | -12017.05 | -9707.57 | 16812.67 | 12017.01 | 9707.50 | 0.004% |
| 13 | -9746.42 | -12075.59 | -16784.22 | 9746.44 | 12075.55 | 16783.37 | 0.004% |
| 14 | 0.00 | -21781.58 | 0.00 | -0.91 | 21781.55 | -1.31 | 0.007% |
| 15 | -40.39 | -21928.82 | -23052.47 | 40.39 | 21928.74 | 23050.85 | 0.005% |
| 16 | 11504.56 | -21796.14 | -19928.51 | -11504.66 | 21796.08 | 19927.17 | 0.004% |
| 17 | 19962.50 | -21659.63 | -11479.40 | -19961.83 | 21659.62 | 11480.06 | 0.003% |
| 18 | 23081.41 | -21785.35 | 39.53 | -23080.54 | 21785.30 | -38.98 | 0.003% |
| 19 | 20023.35 | -21909.86 | 11561.16 | -20022.25 | 21909.79 | -11560.57 | 0.004% |
| 20 | 11574.96 | -21770.78 | 19971.38 | -11574.03 | 21770.74 | -19970.96 | 0.003% |
| 21 | 40.39 | -21634.32 | 23030.09 | -39.64 | 21634.28 | -23029.07 | 0.004% |
| 22 | -11504.56 | -21767.00 | 19928.51 | 11503.68 | 21766.96 | -19928.11 | 0.003% |
| 23 | -19981.88 | -21903.51 | 11490.59 | 19980.84 | 21903.45 | -11490.02 | 0.004% |
| 24 | -23081.41 | -21777.79 | -39.53 | 23080.58 | 21777.75 | 40.06 | 0.003% |
| 25 | -20003.97 | -21653.28 | -11549.97 | 20003.00 | 21653.26 | 11550.42 | 0.003% |
| 26 | -11574.96 | -21792.36 | -19971.38 | 11575.06 | 21792.30 | 19970.02 | 0.004% |
| 27 | -24.53 | -12101.69 | -9673.72 | 24.54 | 12101.67 | 9673.07 | 0.004% |
| 28 | 4813.77 | -12073.84 | -8338.09 | -4813.81 | 12073.82 | 8337.53 | 0.004% |
| 29 | 8353.00 | -12045.15 | -4794.38 | -8352.08 | 12045.14 | 4794.12 | 0.006% |
| 30 | 9670.50 | -12071.38 | 24.38 | -9670.03 | 12071.36 | -24.10 | 0.004% |
| 31 | 8414.26 | -12097.38 | 4858.08 | -8413.82 | 12097.36 | -4857.85 | 0.003% |
| 32 | 4856.35 | -12068.21 | 8363.07 | -4855.92 | 12068.19 | -8362.88 | 0.003% |
| 33 | 24.53 | -12039.64 | 9631.54 | -24.38 | 12039.63 | -9630.90 | 0.004% |
| 34 | -4813.78 | -12067.49 | 8338.09 | 4813.41 | 12067.48 | -8337.92 | 0.003% |
| 35 | -8389.54 | -12096.18 | 4815.48 | 8389.15 | 12096.16 | -4815.27 | 0.003% |
| 36 | -9670.50 | -12069.95 | -24.38 | 9670.08 | 12069.94 | 24.63 | 0.003% |
| 37 | -8377.73 | -12043.95 | -4836.99 | 8376.92 | 12043.94 | 4836.59 | 0.006% |
| 38 | -4856.35 | -12073.12 | -8363.07 | 4856.39 | 12073.11 | 8362.49 | 0.004% |

Non-Linear Convergence Results

| Load Combination | Converged? | Number of Cycles | Displacement Tolerance | Force Tolerance |
|------------------|------------|------------------|------------------------|-----------------|
| 1 | Yes | 9 | 0.00000001 | 0.00009197 |
| 2 | Yes | 22 | 0.00006573 | 0.00007677 |
| 3 | Yes | 22 | 0.00000001 | 0.00005527 |
| 4 | Yes | 17 | 0.00000001 | 0.00003852 |
| 5 | Yes | 21 | 0.00007548 | 0.00008212 |
| 6 | Yes | 22 | 0.00000001 | 0.00006157 |
| 7 | Yes | 21 | 0.00007520 | 0.00007890 |
| 8 | Yes | 16 | 0.00000001 | 0.00003961 |
| 9 | Yes | 21 | 0.00007090 | 0.00007379 |
| 10 | Yes | 22 | 0.00000001 | 0.00005764 |

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|---|------------------------------|--------------------------------------|
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| | | | | |
|----|-----|----|------------|------------|
| 11 | Yes | 21 | 0.00007210 | 0.00007793 |
| 12 | Yes | 14 | 0.00000001 | 0.00007101 |
| 13 | Yes | 22 | 0.00000001 | 0.00005609 |
| 14 | Yes | 6 | 0.00000001 | 0.00005115 |
| 15 | Yes | 22 | 0.00008665 | 0.00009040 |
| 16 | Yes | 22 | 0.00008147 | 0.00007331 |
| 17 | Yes | 16 | 0.00008199 | 0.00004801 |
| 18 | Yes | 22 | 0.00006114 | 0.00005777 |
| 19 | Yes | 22 | 0.00006729 | 0.00007168 |
| 20 | Yes | 22 | 0.00006351 | 0.00005734 |
| 21 | Yes | 14 | 0.00009191 | 0.00007392 |
| 22 | Yes | 22 | 0.00006013 | 0.00005404 |
| 23 | Yes | 22 | 0.00006401 | 0.00006787 |
| 24 | Yes | 22 | 0.00005915 | 0.00005557 |
| 25 | Yes | 15 | 0.00008119 | 0.00005391 |
| 26 | Yes | 22 | 0.00008341 | 0.00007494 |
| 27 | Yes | 17 | 0.00000001 | 0.00007052 |
| 28 | Yes | 16 | 0.00000001 | 0.00006211 |
| 29 | Yes | 12 | 0.00000001 | 0.00008717 |
| 30 | Yes | 16 | 0.00000001 | 0.00006091 |
| 31 | Yes | 17 | 0.00000001 | 0.00005643 |
| 32 | Yes | 16 | 0.00000001 | 0.00005264 |
| 33 | Yes | 12 | 0.00000001 | 0.00006273 |
| 34 | Yes | 16 | 0.00000001 | 0.00004568 |
| 35 | Yes | 17 | 0.00000001 | 0.00004900 |
| 36 | Yes | 16 | 0.00000001 | 0.00005485 |
| 37 | Yes | 12 | 0.00000001 | 0.00008159 |
| 38 | Yes | 16 | 0.00000001 | 0.00006430 |

Maximum Tower Deflections - Service Wind

| Section No. | Elevation ft | Horz. Deflection in | Gov. Load Comb. | Tilt ° | Twist ° |
|-------------|-----------------|------------------------|-----------------|-----------|------------|
| T1 | 190.6 - 175.35 | 7.352 | 31 | 0.3935 | 0.1513 |
| T2 | 175.35 - 160.1 | 6.064 | 31 | 0.4150 | 0.1494 |
| T3 | 160.1 - 140.1 | 4.688 | 31 | 0.4155 | 0.1449 |
| T4 | 140.1 - 120.1 | 3.120 | 30 | 0.2941 | 0.1420 |
| T5 | 120.1 - 100.1 | 2.245 | 36 | 0.1842 | 0.1786 |
| T6 | 100.1 - 80.1 | 1.627 | 37 | 0.1347 | 0.2076 |
| T7 | 80.1 - 60.1 | 1.195 | 37 | 0.0812 | 0.2238 |
| T8 | 60.1 - 40.1 | 0.883 | 29 | 0.0745 | 0.2278 |
| T9 | 40.1 - 20.1 | 0.588 | 29 | 0.0632 | 0.2089 |
| T10 | 20.1 - 4.85 | 0.334 | 33 | 0.0708 | 0.1706 |
| T11 | 4.85 - 0 | 0.084 | 33 | 0.0809 | 0.1049 |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt ° | Twist ° | Radius of Curvature ft |
|-----------------|--|-----------------|------------------|-----------|------------|---------------------------|
| 189.99 | Guy | 31 | 7.301 | 0.3943 | 0.1512 | 52343 |
| 187.00 | BXA-70063-6CF W/ Mast Pipe | 31 | 7.053 | 0.3985 | 0.1509 | 52343 |
| 145.00 | Commscope LNX-6515DS-VTM w/ pipe mast | 30 | 3.430 | 0.3296 | 0.1395 | 6640 |
| 139.49 | Guy | 30 | 3.085 | 0.2898 | 0.1426 | 5706 |
| 120.00 | US Army Mars | 36 | 2.242 | 0.1838 | 0.1788 | 26722 |

| | | | | |
|---|---------|------------|-------------|-------------------|
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| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Elevation | Appurtenance | Gov. Load Comb. | Deflection | Tilt | Twist | Radius of Curvature |
|-----------|--------------|-----------------|------------|--------|--------|---------------------|
| ft | | | in | ° | ° | ft |
| 87.37 | Guy | 37 | 1.334 | 0.0976 | 0.2190 | 23616 |
| 85.00 | US Army Mars | 37 | 1.286 | 0.0914 | 0.2207 | 24826 |
| 44.95 | Guy | 29 | 0.655 | 0.0654 | 0.2147 | 62132 |

Maximum Tower Deflections - Design Wind

| Section No. | Elevation | Horz. Deflection | Gov. Load Comb. | Tilt | Twist |
|-------------|----------------|------------------|-----------------|--------|--------|
| | ft | in | | ° | ° |
| T1 | 190.6 - 175.35 | 27.028 | 15 | 1.2147 | 0.3048 |
| T2 | 175.35 - 160.1 | 23.119 | 15 | 1.2564 | 0.3079 |
| T3 | 160.1 - 140.1 | 19.046 | 15 | 1.2520 | 0.3092 |
| T4 | 140.1 - 120.1 | 14.175 | 15 | 0.9803 | 0.3111 |
| T5 | 120.1 - 100.1 | 10.675 | 15 | 0.7522 | 0.3938 |
| T6 | 100.1 - 80.1 | 7.799 | 15 | 0.6237 | 0.4588 |
| T7 | 80.1 - 60.1 | 5.545 | 15 | 0.4504 | 0.4968 |
| T8 | 60.1 - 40.1 | 3.825 | 15 | 0.3818 | 0.5085 |
| T9 | 40.1 - 20.1 | 2.368 | 15 | 0.3029 | 0.4692 |
| T10 | 20.1 - 4.85 | 1.227 | 15 | 0.2843 | 0.3820 |
| T11 | 4.85 - 0 | 0.303 | 15 | 0.2956 | 0.2373 |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. Load Comb. | Deflection | Tilt | Twist | Radius of Curvature |
|-----------|---------------------------------------|-----------------|------------|--------|--------|---------------------|
| ft | | | in | ° | ° | ft |
| 189.99 | Guy | 15 | 26.873 | 1.2163 | 0.3049 | 26192 |
| 187.00 | BXA-70063-6CF W/ Mast Pipe | 15 | 26.117 | 1.2244 | 0.3054 | 26192 |
| 145.00 | Commscope LNX-6515DS-VTM w/ pipe mast | 15 | 15.252 | 1.0574 | 0.3043 | 3071 |
| 139.49 | Guy | 15 | 14.048 | 0.9713 | 0.3125 | 2664 |
| 120.00 | US Army Mars | 15 | 10.660 | 0.7514 | 0.3942 | 8725 |
| 87.37 | Guy | 15 | 6.290 | 0.5078 | 0.4852 | 6530 |
| 85.00 | US Army Mars | 15 | 6.038 | 0.4870 | 0.4893 | 6703 |
| 44.95 | Guy | 15 | 2.689 | 0.3199 | 0.4817 | 11570 |

Bolt Design Data

| Section No. | Elevation | Component Type | Bolt Grade | Bolt Size | Number Of Bolts | Maximum Load per Bolt | Allowable Load | Ratio Load Allowable | Allowable Ratio | Criteria | |
|-------------|-----------|----------------|------------|-----------|-----------------|-----------------------|----------------|----------------------|-----------------|----------|----------------|
| | ft | | | in | | lb | lb | | | | |
| T1 | 190.6 | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.60 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 2348.17 | 2740.50 | 0.857 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 322.20 | 2740.50 | 0.118 | ✓ | 1.333 | Member Bearing |
| T2 | 175.35 | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.60 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1896.86 | 2740.50 | 0.692 | ✓ | 1.333 | Member Bearing |

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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Maximum Load per Bolt lb | Allowable Load lb | Ratio Load Allowable | Allowable Ratio | Criteria | |
|-------------|--------------|----------------|------------|--------------|-----------------|--------------------------|-------------------|----------------------|-----------------|----------|----------------|
| T3 | 160.1 | Top Girt | A325N | 0.5000 | 1 | 342.39 | 2740.50 | 0.125 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 757.34 | 2740.50 | 0.276 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 3541.40 | 19438.60 | 0.182 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1996.06 | 2740.50 | 0.728 | ✓ | 1.333 | Member Bearing |
| T4 | 140.1 | Top Girt | A325N | 0.5000 | 1 | 305.48 | 2740.50 | 0.111 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 2465.94 | 2740.50 | 0.900 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.50 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1203.93 | 2740.50 | 0.439 | ✓ | 1.333 | Member Bearing |
| T5 | 120.1 | Top Girt | A325N | 0.5000 | 1 | 2389.99 | 2740.50 | 0.872 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 272.75 | 2740.50 | 0.100 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.60 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 751.60 | 4123.34 | 0.182 | ✓ | 1.333 | Bolt Shear |
| T6 | 100.1 | Top Girt | A325N | 0.5000 | 1 | 346.80 | 2740.50 | 0.127 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 366.25 | 2740.50 | 0.134 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.60 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1082.68 | 2740.50 | 0.395 | ✓ | 1.333 | Member Bearing |
| T7 | 80.1 | Top Girt | A325N | 0.5000 | 1 | 296.10 | 2740.50 | 0.108 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 449.27 | 2740.50 | 0.164 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.50 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 767.56 | 4123.34 | 0.186 | ✓ | 1.333 | Bolt Shear |
| T8 | 60.1 | Top Girt | A325N | 0.5000 | 1 | 393.71 | 2740.50 | 0.144 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 324.51 | 2740.50 | 0.118 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.40 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1417.38 | 2740.50 | 0.517 | ✓ | 1.333 | Member Bearing |
| T9 | 40.1 | Top Girt | A325N | 0.5000 | 1 | 242.68 | 2740.50 | 0.089 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 628.51 | 2740.50 | 0.229 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.50 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1321.97 | 2740.50 | 0.482 | ✓ | 1.333 | Member Bearing |
| T10 | 20.1 | Top Girt | A325N | 0.5000 | 1 | 495.19 | 2740.50 | 0.181 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 256.94 | 2740.50 | 0.094 | ✓ | 1.333 | Member Bearing |
| | | Leg | A325N | 0.7500 | 4 | 0.00 | 19438.10 | 0.000 | ✓ | 1.333 | Bolt Tension |
| | | Diagonal | A325N | 0.5000 | 1 | 1089.13 | 2740.50 | 0.397 | ✓ | 1.333 | Member Bearing |
| | | Top Girt | A325N | 0.5000 | 1 | 240.53 | 2740.50 | 0.088 | ✓ | 1.333 | Member Bearing |
| | | Bottom Girt | A325N | 0.5000 | 1 | 3939.21 | 4123.34 | 0.955 | ✓ | 1.333 | Bolt Shear |

Guy Design Data

| | | | | |
|---|----------------|------------|--------------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Size | Initial Tension lb | Breaking Load lb | Actual T lb | Allowable T _a lb | Required S.F. | Actual S.F. |
|-------------|---------------------|----------|-----------------------|---------------------|----------------|--------------------------------|---------------|-------------|
| T1 | 189.99 (A) (450) | 1/2 EHS | 2690.00 | 26900.04 | 12266.50 | 13450.00 | 2.000 | 2.193 ✓ |
| | 189.99 (B) (449) | 1/2 EHS | 2690.00 | 26900.04 | 12399.20 | 13450.00 | 2.000 | 2.169 ✓ |
| | 189.99 (C) (448) | 1/2 EHS | 2690.00 | 26900.04 | 12356.70 | 13450.00 | 2.000 | 2.177 ✓ |
| T4 | 139.49 (A) (459) | 1/2 EHS | 2690.00 | 26900.04 | 10488.70 | 13450.00 | 2.000 | 2.565 ✓ |
| | 139.49 (A) (460) | 1/2 EHS | 2690.00 | 26900.04 | 10750.80 | 13450.00 | 2.000 | 2.502 ✓ |
| | 139.49 (B) (455) | 1/2 EHS | 2690.00 | 26900.04 | 10798.80 | 13450.00 | 2.000 | 2.491 ✓ |
| | 139.49 (B) (456) | 1/2 EHS | 2690.00 | 26900.04 | 10618.00 | 13450.00 | 2.000 | 2.533 ✓ |
| | 139.49 (C) (451) | 1/2 EHS | 2690.00 | 26900.04 | 10627.90 | 13450.00 | 2.000 | 2.531 ✓ |
| | 139.49 (C) (452) | 1/2 EHS | 2690.00 | 26900.04 | 10511.40 | 13450.00 | 2.000 | 2.559 ✓ |
| | 87.37 (A) (468) | 7/16 EHS | 2080.00 | 20800.02 | 7193.11 | 10400.00 | 2.000 | 2.892 ✓ |
| T6 | 87.37 (B) (467) | 7/16 EHS | 2080.00 | 20800.02 | 7350.41 | 10400.00 | 2.000 | 2.830 ✓ |
| | 87.37 (C) (463) | 7/16 EHS | 2080.00 | 20800.02 | 7293.25 | 10400.00 | 2.000 | 2.852 ✓ |
| T8 | 44.95 (A) (474) | 3/8 EHS | 1540.00 | 15399.96 | 4915.99 | 7700.00 | 2.000 | 3.133 ✓ |
| | 44.95 (B) (473) | 3/8 EHS | 1540.00 | 15399.96 | 4980.93 | 7700.00 | 2.000 | 3.092 ✓ |
| | 44.95 (C) (469) | 3/8 EHS | 1540.00 | 15399.96 | 4884.91 | 7700.00 | 2.000 | 3.153 ✓ |

Compression Checks

Leg Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | KI/r | Mast Stability Index | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio P/P _a |
|-------------|-----------------|----------------|---------|----------------------|----------------|----------------------|-----------------------|----------------------|----------------|-----------------------------|------------------------|
| T1 | 190.6 - 175.35 | ROHN 2.5 X-STR | 15.25 | 2.44 | 63.4 K=2.00 | 1.00 | 22.137 | 2.2535 | -14927.60 | 49886.40 | 0.299 ✓ |
| T2 | 175.35 - 160.1 | ROHN 2.5 X-STR | 15.25 | 2.44 | 63.4 K=2.00 | 1.00 | 22.137 | 2.2535 | -13270.70 | 49886.40 | 0.266 ✓ |
| T3 | 160.1 - 140.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 K=1.00 | 1.00 | 26.254 | 1.0745 | -34169.80 | 28210.30 | 1.211 ✓ |
| T4 | 140.1 - 120.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 K=1.00 | 1.00 | 26.220 | 1.0745 | -36462.60 | 28173.80 | 1.294 ✓ |
| T5 | 120.1 - 100.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 K=1.00 | 1.00 | 26.207 | 1.0745 | -28353.30 | 28160.20 | 1.007 ✓ |
| T6 | 100.1 - 80.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 K=1.00 | 1.00 | 26.203 | 1.0745 | -33345.10 | 28155.50 | 1.184 ✓ |
| T7 | 80.1 - 60.1 | ROHN 2 X-STR | 20.00 | 2.42 | 37.9 K=1.00 | 1.00 | 26.118 | 1.4773 | -31342.50 | 38583.30 | 0.812 ✓ |
| T8 | 60.1 - 40.1 | ROHN 2.5 STD | 20.00 | 2.42 | 61.4 K=2.00 | 1.00 | 22.480 | 1.7040 | -34332.30 | 38306.80 | 0.896 ✓ |

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| | Project 8115000099 | Date 11:30:25 03/18/15 |
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| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | Mast Stability Index | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|----------------|---------|----------------------|--------|----------------------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T9 | 40.1 - 20.1 | ROHN 2.5 STD | 20.00 | 2.42 | 61.4 | 1.00 | 22.480 | 1.7040 | -32375.20 | 38306.80 | 0.845 |
| | | | | | K=2.00 | | | | | | ✓ |
| T10 | 20.1 - 4.85 | ROHN 2.5 STD | 15.25 | 2.44 | 61.8 | 1.00 | 22.410 | 1.7040 | -29043.90 | 38186.90 | 0.761 |
| | | | | | K=2.00 | | | | | | ✓ |
| T11 | 4.85 - 0 | ROHN 2.5 X-STR | 5.25 | 1.27 | 16.5 | 0.96 | 27.519 | 2.2535 | -30985.10 | 62016.00 | 0.500 |
| | | | | | K=1.00 | | | | | | ✓ |

Diagonal Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|--------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 15.127 | 0.2627 | -2360.27 | 3974.60 | 0.594 |
| | | | | | K=1.00 | | | | | ✓ |
| T2 | 175.35 - 160.1 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 15.127 | 0.2627 | -1934.84 | 3974.60 | 0.487 |
| | | | | | K=1.00 | | | | | ✓ |
| T3 | 160.1 - 140.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 14.968 | 0.2627 | -2121.40 | 3932.77 | 0.539 |
| | | | | | K=1.00 | | | | | ✓ |
| T4 | 140.1 - 120.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 14.968 | 0.2627 | -1506.92 | 3932.77 | 0.383 |
| | | | | | K=1.00 | | | | | ✓ |
| T5 | 120.1 - 100.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 14.968 | 0.2627 | -751.60 | 3932.77 | 0.191 |
| | | | | | K=1.00 | | | | | ✓ |
| T6 | 100.1 - 80.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 14.968 | 0.2627 | -1210.82 | 3932.77 | 0.308 |
| | | | | | K=1.00 | | | | | ✓ |
| T7 | 80.1 - 60.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 14.968 | 0.2627 | -767.56 | 3932.77 | 0.195 |
| | | | | | K=1.00 | | | | | ✓ |
| T8 | 60.1 - 40.1 | P1.5x.058 | 4.22 | 3.93 | 92.5 | 15.159 | 0.2627 | -1721.11 | 3983.07 | 0.432 |
| | | | | | K=1.00 | | | | | ✓ |
| T9 | 40.1 - 20.1 | P1.5x.058 | 4.22 | 3.93 | 92.5 | 15.159 | 0.2627 | -1533.48 | 3983.07 | 0.385 |
| | | | | | K=1.00 | | | | | ✓ |
| T10 | 20.1 - 4.85 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 15.127 | 0.2627 | -644.39 | 3974.60 | 0.162 |
| | | | | | K=1.00 | | | | | ✓ |

Top Girt Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|--------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T2 | 175.35 - 160.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 17.678 | 0.2627 | -349.77 | 4644.99 | 0.075 |
| | | | | | K=1.00 | | | | | ✓ |
| T3 | 160.1 - 140.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 17.539 | 0.2627 | -141.42 | 4608.31 | 0.031 |
| | | | | | K=1.00 | | | | | ✓ |
| T4 | 140.1 - 120.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 17.539 | 0.2627 | -2484.63 | 4608.31 | 0.539 |
| | | | | | K=1.00 | | | | | ✓ |
| T8 | 60.1 - 40.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 17.678 | 0.2627 | -79.82 | 4644.99 | 0.017 |
| | | | | | K=1.00 | | | | | ✓ |

| | | | | |
|---|----------------|------------|--------------------|-------------------|
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| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|----------------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T9 | 40.1 - 20.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -370.90 | 4644.99 | 0.080 ✓ |
| T10 | 20.1 - 4.85 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -104.25 | 4644.99 | 0.022 ✓ |

Bottom Girt Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|----------------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -275.32 | 4644.99 | 0.059 ✓ |
| T2 | 175.35 - 160.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -676.24 | 4644.99 | 0.146 ✓ |
| T3 | 160.1 - 140.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 K=1.00 | 17.539 | 0.2627 | -1636.80 | 4608.31 | 0.355 ✓ |
| T8 | 60.1 - 40.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -337.38 | 4644.99 | 0.073 ✓ |
| T9 | 40.1 - 20.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 K=1.00 | 17.678 | 0.2627 | -132.71 | 4644.99 | 0.029 ✓ |
| T11 | 4.85 - 0 | 14x3/16 | 0.48 | 0.24 | 52.3 K=1.00 | 18.144 | 2.6250 | -873.15 | 47626.90 | 0.018 ✓ |

Mid Girt Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|---------|---------|----------------------|-----------------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T11 | 4.85 - 0 | 14x3/16 | 1.31 | 1.07 | 237.7 K=1.00 | 2.642 | 2.6250 | -154.89 | 6936.17 | 0.022 ✓ |

KL/R > 200 (C) - 443

Top Guy Pull-Off Design Data (Compression)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|-----------------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 3.46 | 3.22 | 357.0 K=1.00 | 21.600 | 1.6875 | 0.00 | 1977.38 | 0.000* |
| T6 | 100.1 - 80.1 | C4x5.4 | 3.46 | 3.26 | 87.2 K=1.00 | 21.600 | 1.5900 | 0.00 | 23113.10 | 0.000* |
| T8 | 60.1 - 40.1 | C4x5.4 | 3.46 | 3.22 | 86.1 K=1.00 | 21.600 | 1.5900 | 0.00 | 23319.00 | 0.000* |

* DL controls

| | | | | |
|---|---------|------------|-------------|-------------------|
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Top Guy Pull-Off Bending Design Data

| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|----------------|-----------|--------------------|---------------------|---------------------|-------------------------------|--------------------|---------------------|---------------------|-------------------------------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 11.89 | -0.113 | 27.000 | 0.004 | 0.00 | 0.000 | 27.000 | 0.000 |
| T6 | 100.1 - 80.1 | C4x5.4 | 12.95 | -0.081 | 21.600 | 0.004 | 0.00 | 0.000 | 21.600 | 0.000 |
| T8 | 60.1 - 40.1 | C4x5.4 | 12.95 | -0.081 | 21.600 | 0.004 | 0.00 | 0.000 | 21.600 | 0.000 |

Top Guy Pull-Off Interaction Design Data

| Section No. | Elevation ft | Size | Ratio $\frac{P}{P_a}$ | Ratio $\frac{f_{bx}}{F_{bx}}$ | Ratio $\frac{f_{by}}{F_{by}}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
|-------------|----------------|-----------|-----------------------|-------------------------------|-------------------------------|--------------------|---------------------|----------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 0.000 | 0.004 | 0.000 | 0.004* ✓ | 1.000 | H1-3 ✓ |
| T6 | 100.1 - 80.1 | C4x5.4 | 0.000 | 0.004 | 0.000 | 0.004* ✓ | 1.000 | H1-3 ✓ |
| T8 | 60.1 - 40.1 | C4x5.4 | 0.000 | 0.004 | 0.000 | 0.004* ✓ | 1.000 | H1-3 ✓ |

* DL controls

Torque-Arm Top Design Data

| Section No. | Elevation ft | Size | L ft | L_u ft | KI/r | F_a ksi | A in ² | Actual P lb | Allow. P_a lb | Ratio $\frac{P}{P_a}$ |
|-------------|---------------------|----------|------|----------|-----------------|-----------|-------------------|-------------|-----------------|-----------------------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | 3.59 | 3.49 | 58.7 K=1.00 | 21.600 | 4.4900 | 0.00 | 57151.60 | 0.000 |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | 3.59 | 3.49 | 102.0 K=1.00 | 12.729 | 4.4900 | -2650.51 | 57151.60 | 0.046 |
| T4 | 140.1 - 120.1 (457) | C10x15.3 | 3.59 | 3.49 | 102.0 K=1.00 | 12.729 | 4.4900 | -2605.30 | 57151.60 | 0.046 |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | 3.59 | 3.49 | 102.0 K=1.00 | 12.729 | 4.4900 | -2633.07 | 57151.60 | 0.046 |
| T4 | 140.1 - 120.1 (461) | C10x15.3 | 3.59 | 3.49 | 58.7 K=1.00 | 21.600 | 4.4900 | 0.00 | 57151.60 | 0.000 |
| T4 | 140.1 - 120.1 (462) | C10x15.3 | 3.59 | 3.49 | 58.7 K=1.00 | 21.600 | 4.4900 | 0.00 | 57151.60 | 0.000 |

Torque-Arm Top Bending Design Data

| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|---------------------|----------|--------------------|---------------------|---------------------|-------------------------------|--------------------|---------------------|---------------------|-------------------------------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | -31577.0 8 | -28.069 | 21.600 | 1.299 | -0.00 | -0.000 | 21.600 | 0.000 |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | -29913.8 3 | -26.590 | 21.600 | 1.231 | 0.00 | -0.000 | 21.600 | 0.000 |

| | | | | |
|---|---------|------------|-------------|-------------------|
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| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|------------------------|----------|--------------------------|---------------------------|---------------------------|----------------------------------|--------------------------|---------------------------|---------------------------|----------------------------------|
| T4 | 140.1 - 120.1 (457) | C10x15.3 | -30576.1 7 | -27.179 | 21.600 | 1.258 | 0.00 | -0.000 | 21.600 | 0.000 |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | -30563.5 8 | -27.168 | 21.600 | 1.258 | -0.00 | -0.000 | 21.600 | 0.000 |
| T4 | 140.1 - 120.1 (461) | C10x15.3 | -31544.8 3 | -28.040 | 21.600 | 1.298 | 0.00 | -0.000 | 21.600 | 0.000 |
| T4 | 140.1 - 120.1 (462) | C10x15.3 | -30896.3 3 | -27.463 | 21.600 | 1.271 | -0.00 | -0.000 | 21.600 | 0.000 |

Torque-Arm Top Interaction Design Data

| Section No. | Elevation ft | Size | Ratio $\frac{P}{P_a}$ | Ratio $\frac{f_{bx}}{F_{bx}}$ | Ratio $\frac{f_{by}}{F_{by}}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
|-------------|------------------------|----------|--------------------------|----------------------------------|----------------------------------|--------------------------|---------------------------|----------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | 0.000 | 1.299 | 0.000 | 1.299 | 1.333 | H1-3 ✓ |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | 0.046 | 1.231 | 0.000 | 1.277 | 1.333 | H1-3 ✓ |
| T4 | 140.1 - 120.1 (457) | C10x15.3 | 0.046 | 1.258 | 0.000 | 1.304 | 1.333 | H1-3 ✓ |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | 0.046 | 1.258 | 0.000 | 1.304 | 1.333 | H1-3 ✓ |
| T4 | 140.1 - 120.1 (461) | C10x15.3 | 0.000 | 1.298 | 0.000 | 1.298 | 1.333 | H1-3 ✓ |
| T4 | 140.1 - 120.1 (462) | C10x15.3 | 0.000 | 1.271 | 0.000 | 1.271 | 1.333 | H1-3 ✓ |

Tension Checks

Leg Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | L_u ft | KI/r | F_a ksi | A in ² | Actual P lb | Allow. P_a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|----------------|---------|-------------|------|--------------|----------------------|-------------------|-----------------------|--------------------------|
| T1 | 190.6 - 175.35 | ROHN 2.5 X-STR | 15.25 | 2.44 | 31.7 | 30.000 | 2.2535 | 2107.15 | 67606.20 | 0.031 |
| T3 | 160.1 - 140.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 | 30.000 | 1.0745 | 14165.60 | 32235.90 | 0.439 |
| T4 | 140.1 - 120.1 | ROHN 2 STD | 20.00 | 2.42 | 36.9 | 30.000 | 1.0745 | 15973.50 | 32235.90 | 0.496 |

Diagonal Design Data (Tension)

| | | | | |
|---|----------------|------------|--------------------|-------------------|
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| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 25.200 | 0.2627 | 2348.17 | 6621.31 | 0.355 |
| T2 | 175.35 - 160.1 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 25.200 | 0.2627 | 1896.86 | 6621.31 | 0.286 |
| T3 | 160.1 - 140.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 25.200 | 0.2627 | 1996.06 | 6621.31 | 0.301 |
| T4 | 140.1 - 120.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 25.200 | 0.2627 | 1203.93 | 6621.31 | 0.182 |
| T5 | 120.1 - 100.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 25.200 | 0.2627 | 486.14 | 6621.31 | 0.073 |
| T6 | 100.1 - 80.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 25.200 | 0.2627 | 1082.68 | 6621.31 | 0.164 |
| T7 | 80.1 - 60.1 | P1.5x.058 | 4.22 | 3.98 | 93.7 | 25.200 | 0.2627 | 485.08 | 6621.31 | 0.073 |
| T8 | 60.1 - 40.1 | P1.5x.058 | 4.22 | 3.93 | 92.5 | 25.200 | 0.2627 | 1417.38 | 6621.31 | 0.214 |
| T9 | 40.1 - 20.1 | P1.5x.058 | 4.22 | 3.93 | 92.5 | 25.200 | 0.2627 | 1321.97 | 6621.31 | 0.200 |
| T10 | 20.1 - 4.85 | P1.5x.058 | 4.23 | 3.94 | 92.7 | 25.200 | 0.2627 | 1089.13 | 6621.31 | 0.164 |

Top Girt Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|-------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T2 | 175.35 - 160.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 342.39 | 6621.31 | 0.052 |
| T3 | 160.1 - 140.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 305.48 | 6621.31 | 0.046 |
| T4 | 140.1 - 120.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 2389.99 | 6621.31 | 0.361 |
| T5 | 120.1 - 100.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 346.80 | 6621.31 | 0.052 |
| T6 | 100.1 - 80.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 296.10 | 6621.31 | 0.045 |
| T7 | 80.1 - 60.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 393.71 | 6621.31 | 0.059 |
| T8 | 60.1 - 40.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 242.68 | 6621.31 | 0.037 |
| T9 | 40.1 - 20.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 495.19 | 6621.31 | 0.075 |
| T10 | 20.1 - 4.85 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 240.53 | 6621.31 | 0.036 |
| T11 | 4.85 - 0 | 14x3/16 | 2.98 | 2.74 | 608.5 | 21.600 | 2.6250 | 2777.82 | 56700.00 | 0.049 |

L/R > 500 (T) - 436

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Bottom Girt Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 322.20 | 6621.31 | 0.049 |
| T2 | 175.35 - 160.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 757.34 | 6621.31 | 0.114 |
| T3 | 160.1 - 140.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 2465.94 | 6621.31 | 0.372 |
| T4 | 140.1 - 120.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 272.75 | 6621.31 | 0.041 |
| T5 | 120.1 - 100.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 366.25 | 6621.31 | 0.055 |
| T6 | 100.1 - 80.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 449.27 | 6621.31 | 0.068 |
| T7 | 80.1 - 60.1 | P1.5x.058 | 3.46 | 3.26 | 76.7 | 25.200 | 0.2627 | 324.51 | 6621.31 | 0.049 |
| T8 | 60.1 - 40.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 628.51 | 6621.31 | 0.095 |
| T9 | 40.1 - 20.1 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 256.94 | 6621.31 | 0.039 |
| T10 | 20.1 - 4.85 | P1.5x.058 | 3.46 | 3.22 | 75.7 | 25.200 | 0.2627 | 3939.21 | 6621.31 | 0.595 |

Mid Girt Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|---------|---------|----------------------|-------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T11 | 4.85 - 0 | 14x3/16 | 2.15 | 1.91 | 423.1 | 21.600 | 2.6250 | 64.54 | 56700.00 | 0.001 |

Top Guy Pull-Off Design Data (Tension)

| Section No. | Elevation ft | Size | L ft | L _u ft | Kl/r | F _a ksi | A in ² | Actual P lb | Allow. P _a lb | Ratio $\frac{P}{P_a}$ |
|-------------|-----------------|-----------|---------|----------------------|-------|-----------------------|----------------------|----------------|-----------------------------|--------------------------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 3.46 | 3.22 | 357.0 | 21.600 | 1.6875 | 3362.80 | 36450.00 | 0.092 |
| T6 | 100.1 - 80.1 | C4x5.4 | 3.46 | 3.26 | 87.2 | 21.600 | 1.5900 | 2738.20 | 34344.00 | 0.080 |
| T8 | 60.1 - 40.1 | C4x5.4 | 3.46 | 3.22 | 86.1 | 21.600 | 1.5900 | 2492.47 | 34344.00 | 0.073 |

Top Guy Pull-Off Bending Design Data

| Section No. | Elevation ft | Size | Actual M _x lb-ft | Actual f _{bx} ksi | Allow. F _{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M _y lb-ft | Actual f _{by} ksi | Allow. F _{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|-----------------|------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|
|-------------|-----------------|------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|

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|---|---------|------------|-------------|-------------------|
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| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|----------------|-----------|--------------------|---------------------|---------------------|-------------------------------|--------------------|---------------------|---------------------|-------------------------------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 11.89 | 0.113 | 27.000 | 0.004 | 0.00 | 0.000 | 27.000 | 0.000 |
| T6 | 100.1 - 80.1 | C4x5.4 | 12.95 | 0.081 | 21.600 | 0.004 | 0.00 | 0.000 | 27.000 | 0.000 |
| T8 | 60.1 - 40.1 | C4x5.4 | 12.95 | 0.081 | 21.600 | 0.004 | 0.00 | 0.000 | 27.000 | 0.000 |

Top Guy Pull-Off Interaction Design Data

| Section No. | Elevation ft | Size | Ratio $\frac{P}{P_a}$ | Ratio $\frac{f_{bx}}{F_{bx}}$ | Ratio $\frac{f_{by}}{F_{by}}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
|-------------|----------------|-----------|-----------------------|-------------------------------|-------------------------------|--------------------|---------------------|----------|
| T1 | 190.6 - 175.35 | 4 1/2x3/8 | 0.092 | 0.004 | 0.000 | 0.096 | 1.333 | H2-1 ✓ |
| T6 | 100.1 - 80.1 | C4x5.4 | 0.080 | 0.004 | 0.000 | 0.083 | 1.333 | H2-1 ✓ |
| T8 | 60.1 - 40.1 | C4x5.4 | 0.073 | 0.004 | 0.000 | 0.076 | 1.333 | H2-1 ✓ |

Torque-Arm Top Design Data

| Section No. | Elevation ft | Size | L ft | L_u ft | Kl/r | F_a ksi | A in ² | Actual P lb | Allow. P_a lb | Ratio $\frac{P}{P_a}$ |
|-------------|---------------------|----------|------|----------|------|-----------|-------------------|-------------|-----------------|-----------------------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 208.60 | 96984.00 | 0.002 |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 2302.44 | 96984.00 | 0.024 |
| T4 | 140.1 - 120.1 (457) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 191.00 | 96984.00 | 0.002 |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 2262.04 | 96984.00 | 0.023 |
| T4 | 140.1 - 120.1 (461) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 193.55 | 96984.00 | 0.002 |
| T4 | 140.1 - 120.1 (462) | C10x15.3 | 3.59 | 3.49 | 58.7 | 21.600 | 4.4900 | 169.07 | 96984.00 | 0.002 |

Torque-Arm Top Bending Design Data

| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|---------------------|----------|--------------------|---------------------|---------------------|-------------------------------|--------------------|---------------------|---------------------|-------------------------------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | -31577.0 | 28.069 | 21.600 | 1.299 | -0.00 | 0.000 | 27.000 | 0.000 |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | -27251.4 | 24.223 | 21.600 | 1.121 | -0.00 | 0.000 | 27.000 | 0.000 |
| T4 | 140.1 - 120.1 (457) | C10x15.3 | -31304.5 | 27.826 | 21.600 | 1.288 | 0.00 | 0.000 | 27.000 | 0.000 |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | -27463.5 | 24.412 | 21.600 | 1.130 | 0.00 | 0.000 | 27.000 | 0.000 |
| T4 | 140.1 - 120.1 | C10x15.3 | -31544.8 | 28.040 | 21.600 | 1.298 | 0.00 | 0.000 | 27.000 | 0.000 |

| | | | | |
|---|---------|------------|-------------|-------------------|
| tnxTower EBI Consulting 21 B Street Burlington, MA 01803 Phone: (781) 425-5100 FAX: (781) 425-5141 | Job | CT11156A | Page | 47 of 49 |
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| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Size | Actual M_x lb-ft | Actual f_{bx} ksi | Allow. F_{bx} ksi | Ratio $\frac{f_{bx}}{F_{bx}}$ | Actual M_y lb-ft | Actual f_{by} ksi | Allow. F_{by} ksi | Ratio $\frac{f_{by}}{F_{by}}$ |
|-------------|---------------------------------|----------|-----------------------|------------------------|------------------------|-------------------------------|-----------------------|------------------------|------------------------|-------------------------------|
| T4 | 140.1 - 120.1 (461) (462) | C10x15.3 | -30896.3 3 | 27.463 3 | 21.600 | 1.271 | -0.00 | 0.000 | 27.000 | 0.000 |

Torque-Arm Top Interaction Design Data

| Section No. | Elevation ft | Size | Ratio P P_a | Ratio f_{bx} F_{bx} | Ratio f_{by} F_{by} | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
|-------------|------------------------|----------|--------------------|----------------------------|----------------------------|--------------------|---------------------|----------|
| T4 | 140.1 - 120.1 (453) | C10x15.3 | 0.002 | 1.299 | 0.000 | 1.302 | 1.333 | H2-1 ✓ |
| T4 | 140.1 - 120.1 (454) | C10x15.3 | 0.024 | 1.121 | 0.000 | 1.145 | 1.333 | H2-1 ✓ |
| T4 | 140.1 - 120.1 (457) | C10x15.3 | 0.002 | 1.288 | 0.000 | 1.290 | 1.333 | H2-1 ✓ |
| T4 | 140.1 - 120.1 (458) | C10x15.3 | 0.023 | 1.130 | 0.000 | 1.154 | 1.333 | H2-1 ✓ |
| T4 | 140.1 - 120.1 (461) | C10x15.3 | 0.002 | 1.298 | 0.000 | 1.300 | 1.333 | H2-1 ✓ |
| T4 | 140.1 - 120.1 (462) | C10x15.3 | 0.002 | 1.271 | 0.000 | 1.273 | 1.333 | H2-1 ✓ |

Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF* P_{allow} lb | % Capacity | Pass Fail |
|-------------|----------------|----------------|----------------|------------------|-----------|-----------------------|------------|-----------|
| T1 | 190.6 - 175.35 | Leg | ROHN 2.5 X-STR | 1 | -14927.60 | 66498.57 | 22.4 | Pass |
| T2 | 175.35 - 160.1 | Leg | ROHN 2.5 X-STR | 29 | -13270.70 | 66498.57 | 20.0 | Pass |
| T3 | 160.1 - 140.1 | Leg | ROHN 2 STD | 56 | -34169.80 | 37604.33 | 90.9 | Pass |
| T4 | 140.1 - 120.1 | Leg | ROHN 2 STD | 113 | -36462.60 | 37555.67 | 97.1 | Pass |
| T5 | 120.1 - 100.1 | Leg | ROHN 2 STD | 170 | -28353.30 | 37537.54 | 75.5 | Pass |
| T6 | 100.1 - 80.1 | Leg | ROHN 2 STD | 228 | -33345.10 | 37531.28 | 88.8 | Pass |
| T7 | 80.1 - 60.1 | Leg | ROHN 2 X-STR | 285 | -31342.50 | 51431.54 | 60.9 | Pass |
| T8 | 60.1 - 40.1 | Leg | ROHN 2.5 STD | 342 | -34332.30 | 51062.96 | 67.2 | Pass |
| T9 | 40.1 - 20.1 | Leg | ROHN 2.5 STD | 375 | -32375.20 | 51062.96 | 63.4 | Pass |
| T10 | 20.1 - 4.85 | Leg | ROHN 2.5 STD | 406 | -29043.90 | 50903.13 | 57.1 | Pass |
| T11 | 4.85 - 0 | Leg | ROHN 2.5 X-STR | 433 | -30985.10 | 82667.32 | 37.5 | Pass |
| T1 | 190.6 - 175.35 | Diagonal | P1.5x.058 | 25 | -2360.27 | 5298.14 | 44.5 | Pass |
| T2 | 175.35 - 160.1 | Diagonal | P1.5x.058 | 38 | -1934.84 | 5298.14 | 36.5 | Pass |
| T3 | 160.1 - 140.1 | Diagonal | P1.5x.058 | 65 | -2121.40 | 5242.38 | 40.5 | Pass |
| T4 | 140.1 - 120.1 | Diagonal | P1.5x.058 | 167 | -1506.92 | 5242.38 | 28.7 | Pass |
| T5 | 120.1 - 100.1 | Diagonal | P1.5x.058 | 225 | -751.60 | 5242.38 | 14.3 | Pass |
| T6 | 100.1 - 80.1 | Diagonal | P1.5x.058 | 252 | -1210.82 | 5242.38 | 23.1 | Pass |
| T7 | 80.1 - 60.1 | Diagonal | P1.5x.058 | 335 | -767.56 | 5242.38 | 14.6 | Pass |
| T8 | 60.1 - 40.1 | Diagonal | P1.5x.058 | 350 | -1721.11 | 5309.43 | 32.4 | Pass |
| | | | | | | | 38.8 (b) | |

| | | | | |
|---|----------------|------------|--------------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|----------------|------------------|-----------|------------------|----------|--------------------------|------------------|-----------|
| T9 | 40.1 - 20.1 | Diagonal | P1.5x.058 | 404 | -1533.48 | 5309.43 | 28.9 | Pass |
| T10 | 20.1 - 4.85 | Diagonal | P1.5x.058 | 417 | 1089.13 | 8826.21 | 36.2 (b) 12.3 | Pass |
| T2 | 175.35 - 160.1 | Top Girt | P1.5x.058 | 32 | -349.77 | 6191.77 | 29.8 (b) 5.6 | Pass |
| T3 | 160.1 - 140.1 | Top Girt | P1.5x.058 | 60 | 305.48 | 8826.21 | 9.4 (b) 3.5 | Pass |
| T4 | 140.1 - 120.1 | Top Girt | P1.5x.058 | 116 | -2484.63 | 6142.88 | 8.4 (b) 40.4 | Pass |
| T5 | 120.1 - 100.1 | Top Girt | P1.5x.058 | 172 | 346.80 | 8826.21 | 65.4 (b) 3.9 | Pass |
| T6 | 100.1 - 80.1 | Top Girt | P1.5x.058 | 229 | 296.10 | 8826.21 | 9.5 (b) 3.4 | Pass |
| T7 | 80.1 - 60.1 | Top Girt | P1.5x.058 | 287 | 393.71 | 8826.21 | 8.1 (b) 4.5 | Pass |
| T8 | 60.1 - 40.1 | Top Girt | P1.5x.058 | 345 | 242.68 | 8826.21 | 10.8 (b) 2.7 | Pass |
| T9 | 40.1 - 20.1 | Top Girt | P1.5x.058 | 377 | -370.90 | 6191.77 | 6.6 (b) 6.0 | Pass |
| T10 | 20.1 - 4.85 | Top Girt | P1.5x.058 | 410 | 240.53 | 8826.21 | 13.6 (b) 2.7 | Pass |
| T11 | 4.85 - 0 | Top Girt | 14x3/16 | 436 | 2777.82 | 75581.10 | 6.6 (b) 3.7 | Pass |
| T1 | 190.6 - 175.35 | Bottom Girt | P1.5x.058 | 9 | -275.32 | 6191.77 | 4.4 8.8 (b) | Pass |
| T2 | 175.35 - 160.1 | Bottom Girt | P1.5x.058 | 34 | -676.24 | 6191.77 | 10.9 20.7 (b) | Pass |
| T3 | 160.1 - 140.1 | Bottom Girt | P1.5x.058 | 61 | 2465.94 | 8826.21 | 27.9 67.5 (b) | Pass |
| T4 | 140.1 - 120.1 | Bottom Girt | P1.5x.058 | 119 | 272.75 | 8826.21 | 3.1 7.5 (b) | Pass |
| T5 | 120.1 - 100.1 | Bottom Girt | P1.5x.058 | 176 | 366.25 | 8826.21 | 4.1 10.0 (b) | Pass |
| T6 | 100.1 - 80.1 | Bottom Girt | P1.5x.058 | 233 | 449.27 | 8826.21 | 5.1 12.3 (b) | Pass |
| T7 | 80.1 - 60.1 | Bottom Girt | P1.5x.058 | 289 | 324.51 | 8826.21 | 3.7 8.9 (b) | Pass |
| T8 | 60.1 - 40.1 | Bottom Girt | P1.5x.058 | 347 | 628.51 | 8826.21 | 7.1 17.2 (b) | Pass |
| T9 | 40.1 - 20.1 | Bottom Girt | P1.5x.058 | 380 | 256.94 | 8826.21 | 2.9 7.0 (b) | Pass |
| T10 | 20.1 - 4.85 | Bottom Girt | P1.5x.058 | 412 | 3939.21 | 8826.21 | 44.6 71.7 (b) | Pass |
| T11 | 4.85 - 0 | Bottom Girt | 14x3/16 | 439 | -869.28 | 63486.65 | 7.7 | Pass |
| T11 | 4.85 - 0 | Mid Girt | 14x3/16 | 443 | -154.89 | 9245.91 | 1.7 | Pass |
| T1 | 190.6 - 175.35 | Guy A@189.985 | 1/2 | 450 | 12266.50 | 13450.00 | 91.2 | Pass |
| T4 | 140.1 - 120.1 | Guy A@139.485 | 1/2 | 460 | 10750.80 | 13450.00 | 79.9 | Pass |
| T6 | 100.1 - 80.1 | Guy A@87.3695 | 7/16 | 468 | 7193.11 | 10400.00 | 69.2 | Pass |
| T8 | 60.1 - 40.1 | Guy A@44.9464 | 3/8 | 474 | 4915.99 | 7700.00 | 63.8 | Pass |
| T1 | 190.6 - 175.35 | Guy B@189.985 | 1/2 | 449 | 12399.20 | 13450.00 | 92.2 | Pass |
| T4 | 140.1 - 120.1 | Guy B@139.485 | 1/2 | 455 | 10798.80 | 13450.00 | 80.3 | Pass |
| T6 | 100.1 - 80.1 | Guy B@87.3695 | 7/16 | 467 | 7350.41 | 10400.00 | 70.7 | Pass |
| T8 | 60.1 - 40.1 | Guy B@44.9464 | 3/8 | 473 | 4980.93 | 7700.00 | 64.7 | Pass |
| T1 | 190.6 - 175.35 | Guy C@189.985 | 1/2 | 448 | 12356.70 | 13450.00 | 91.9 | Pass |
| T4 | 140.1 - 120.1 | Guy C@139.485 | 1/2 | 451 | 10627.90 | 13450.00 | 79.0 | Pass |
| T6 | 100.1 - 80.1 | Guy C@87.3695 | 7/16 | 463 | 7293.25 | 10400.00 | 70.1 | Pass |
| T8 | 60.1 - 40.1 | Guy C@44.9464 | 3/8 | 469 | 4884.91 | 7700.00 | 63.4 | Pass |
| T1 | 190.6 - 175.35 | Top Guy | 4 1/2x3/8 | 4 | 3362.80 | 48587.85 | 7.2 | Pass |
| T6 | 100.1 - 80.1 | Pull-Off@189.985 | | | | | | |
| T6 | 100.1 - 80.1 | Top Guy | C4x5.4 | 464 | 2738.20 | 45780.55 | 6.3 | Pass |
| T8 | 60.1 - 40.1 | Pull-Off@87.3695 | | | | | | |
| T8 | 60.1 - 40.1 | Top Guy | C4x5.4 | 470 | 2492.47 | 45780.55 | 5.7 | Pass |

| | | | | |
|---|---------|------------|-------------|-------------------|
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| | Project | 8115000099 | Date | 11:30:25 03/18/15 |
| | Client | T-Mobile | Designed by | Kelly Shanahan |

| Section No. | Elevation ft | Component Type | Size | Critical Element | P lb | SF*P _{allow} lb | % Capacity | Pass Fail |
|-------------|---------------|---|----------|------------------|----------|--------------------------|-------------|-------------|
| T4 | 140.1 - 120.1 | Pull-Off@44.9464 Torque Arm Top@139.485 | C10x15.3 | 457 | -2605.30 | 76183.08 | 97.8 | Pass |
| | | | | | | Summary | | |
| | | | | | | Leg (T4) | 97.1 | Pass |
| | | | | | | Diagonal (T1) | 64.3 | Pass |
| | | | | | | Top Girt (T4) | 65.4 | Pass |
| | | | | | | Bottom Girt (T10) | 71.7 | Pass |
| | | | | | | Mid Girt (T11) | 1.7 | Pass |
| | | | | | | Guy A (T1) | 91.2 | Pass |
| | | | | | | Guy B (T1) | 92.2 | Pass |
| | | | | | | Guy C (T1) | 91.9 | Pass |
| | | | | | | Top Guy | 7.2 | Pass |
| | | | | | | Pull-Off (T1) | | |
| | | | | | | Torque Arm Top (T4) | 97.8 | Pass |
| | | | | | | Bolt Checks | 71.7 | Pass |
| | | | | | | RATING = | 97.8 | Pass |

General Footing

File = C:\Users\rapted\Desktop\1_Jobs\818353~1\1_MOVE~1\TOWERF~1.EC6
 ENERCALC, INC. 1983-2014, Build:6.14.9.18, Ver:6.14.9.18
 Licensee : ENVIROBUSINESS, INC.

Lic. # : KW-06008663
 Description : Tower Foundation

Code References

Calculations per ACI 318-05, IBC 2006, CBC 2007, ASCE 7-05
 Load Combinations Used : ASCE 7-05

General Information

Material Properties

| | | | |
|----------------------------------|---|---------|-----|
| f_c : Concrete 28 day strength | = | 3.0 | ksi |
| f_y : Rebar Yield | = | 60.0 | ksi |
| E_c : Concrete Elastic Modulus | = | 3,122.0 | ksi |
| Concrete Density | = | 145.0 | pcf |
| ϕ Values Flexure | = | 0.90 | |
| Shear | = | 0.750 | |

Analysis Settings

| | | |
|--|---|----------|
| Min Steel % Bending Reinf. | = | |
| Min Allow % Temp Reinf. | = | |
| Min. Overturning Safety Factor | = | 2.0 : 1 |
| Min. Sliding Safety Factor | = | 1.50 : 1 |
| Add Ftg Wt for Soil Pressure | : | Yes |
| Use ftg wt for stability, moments & shears | : | Yes |
| Add Pedestal Wt for Soil Pressure | : | Yes |
| Use Pedestal wt for stability, mom & shear | : | Yes |

Soil Design Values

| | | | |
|---------------------------------------|---|-------|-----|
| Allowable Soil Bearing | = | 6.0 | ksf |
| Increase Bearing By Footing Weight | = | No | |
| Soil Passive Resistance (for Sliding) | = | 250.0 | pcf |
| Soil/Concrete Friction Coeff. | = | 0.450 | |

Increases based on footing Depth

| | | | |
|---|---|-----|-----|
| Footing base depth below soil surface | = | 4.0 | ft |
| Allowable pressure increase per foot of dept= | = | | ksf |
| when footing base is below | = | | ft |

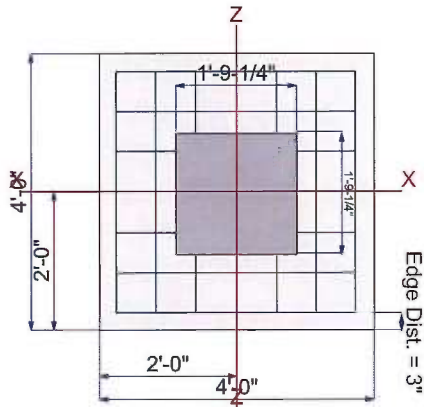
Increases based on footing plan dimension

| | | | |
|--|---|--|-----|
| Allowable pressure increase per foot of dep= | = | | ksf |
| when maximum length or width is greater= | = | | ft |

Dimensions

| | | | |
|-----------------------------|---|------|----|
| Width parallel to X-X Axis | = | 4.0 | ft |
| Length parallel to Z-Z Axis | = | 4.0 | ft |
| Footing Thicknes | = | 15.0 | in |

| | | | |
|---------------------------------------|---|--------|----|
| Pedestal dimensions... | | | |
| px : parallel to X-X Axis | = | 21.270 | in |
| pz : parallel to Z-Z Axis | = | 21.270 | in |
| Height | = | 45.0 | in |
| Rebar Centerline to Edge of Concrete. | | | |
| at Bottom of footing | = | | in |



From TNX
 DL=39.7K
 DL+ice=84.5K
 ice=44.8
 DL+0.7ice=39.7+.7x44.8=71.0K

Applied Loads

| | D | Lr | L | S | W | E | H |
|-----------------|---|------|---|---|------|---|------|
| P : Column Load | = | 71.0 | | | | | k |
| OB : Overburden | = | | | | | | ksf |
| M-xx | = | | | | | | k-ft |
| M-zz | = | | | | | | k-ft |
| V-x | = | | | | 0.80 | | k |
| V-z | = | | | | 0.80 | | k |

EBI Consulting
 21 B Street
 Burlington, MA 01803
 Tel:1-800-786-2346

Project Title:
 Engineer:
 Project Descr:

Project ID:

Printed: 18 MAR 2015, 11:13AM

General Footing

File = C:\Users\traped\Desktop\1_Jobs\818353-1\1_MOVE-1\TOWERF-1.EC6
 ENERCALC, INC. 1983-2014, Build:6.14.9.18, Ver:6.14.9.18
 Licensee : ENVIROBUSINESS, INC.

Lic. # : KW-06008663
 Description : Tower Foundation

DESIGN SUMMARY

Design OK

| | Min. Ratio | Item | Applied | Capacity | Governing Load Combination |
|------|------------|------------------|------------|-------------|----------------------------|
| PASS | 0.8490 | Soil Bearing | 5.094 ksf | 6.0 ksf | +D+W+H about Z-Z axis |
| PASS | 22.683 | Overturing - X-X | 4.0 k-ft | 90.730 k-ft | +0.60D+W+H |
| PASS | 22.683 | Overturing - Z-Z | 4.0 k-ft | 90.730 k-ft | +0.60D+W+H |
| PASS | 30.791 | Sliding - X-X | 0.80 k | 24.633 k | +0.60D+W+H |
| PASS | 30.791 | Sliding - Z-Z | 0.80 k | 24.633 k | +0.60D+W+H |
| PASS | n/a | Uplift | 0.0 k | 0.0 k | No Uplift |
| | | | | | |
| PASS | n/a | 1-way Shear (+X) | 0.0 psi | 82.158 psi | n/a |
| PASS | 0.0 | 1-way Shear (-X) | 0.0 psi | 0.0 psi | n/a |
| PASS | n/a | 1-way Shear (+Z) | 0.0 psi | 82.158 psi | n/a |
| PASS | n/a | 1-way Shear (-Z) | 0.0 psi | 82.158 psi | n/a |
| PASS | n/a | 2-way Punching | 19.282 psi | 82.158 psi | +1.40D |

Detailed Results

Soil Bearing

| Rotation Axis & Load Combination... | Gross Allowable | Xecc | Zecc | Bottom, -Z | Actual Soil Bearing Stress | | | Actual / Allowable Ratio | |
|-------------------------------------|-----------------|--------|--------|------------|----------------------------|----------|-----------|--------------------------|--|
| | | | | | Top, +Z | Left, -X | Right, +X | | |
| X-X, D Only | 6.0 | n/a | 0.0 | 4.726 | 4.726 | n/a | n/a | 0.788 | |
| X-X, +D+W+H | 6.0 | n/a | 0.6349 | 4.357 | 5.094 | n/a | n/a | 0.849 | |
| X-X, +D+0.750Lr+0.750L+0.750W+H | 6.0 | n/a | 0.4761 | 4.449 | 5.002 | n/a | n/a | 0.834 | |
| X-X, +0.60D+W+H | 6.0 | n/a | 1.058 | 2.467 | 3.204 | n/a | n/a | 0.534 | |
| Z-Z, D Only | 6.0 | 0.0 | n/a | n/a | n/a | 4.726 | 4.726 | 0.788 | |
| Z-Z, +D+W+H | 6.0 | 0.6349 | n/a | n/a | n/a | 4.357 | 5.094 | 0.849 | |
| Z-Z, +D+0.750Lr+0.750L+0.750W+H | 6.0 | 0.4761 | n/a | n/a | n/a | 4.449 | 5.002 | 0.834 | |
| Z-Z, +0.60D+W+H | 6.0 | 1.058 | n/a | n/a | n/a | 2.467 | 3.204 | 0.534 | |

Overturing Stability

| Rotation Axis & Load Combination... | Overturing Moment | Resisting Moment | Stability Ratio | Status |
|-------------------------------------|-------------------|------------------|-----------------|--------|
| X-X, D Only | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+L+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+Lr+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+S+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+0.750Lr+0.750L+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+0.750L+0.750S+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+W+H | 4.0 k-ft | 151.217 k-ft | 37.804 | OK |
| X-X, +D+0.70E+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+0.750Lr+0.750L+0.750W+H | 3.0 k-ft | 151.217 k-ft | 50.406 | OK |
| X-X, +D+0.750L+0.750S+0.750W+H | 3.0 k-ft | 151.217 k-ft | 50.406 | OK |
| X-X, +D+0.750Lr+0.750L+0.5250E+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +D+0.750L+0.750S+0.5250E+H | None | 0.0 k-ft | Infinity | OK |
| X-X, +0.60D+W+H | 4.0 k-ft | 90.730 k-ft | 22.683 | OK |
| X-X, +0.60D+0.70E+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, D Only | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+L+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+Lr+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+S+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+0.750Lr+0.750L+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+0.750L+0.750S+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+W+H | 4.0 k-ft | 151.217 k-ft | 37.804 | OK |
| Z-Z, +D+0.70E+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+0.750Lr+0.750L+0.750W+H | 3.0 k-ft | 151.217 k-ft | 50.406 | OK |
| Z-Z, +D+0.750L+0.750S+0.750W+H | 3.0 k-ft | 151.217 k-ft | 50.406 | OK |
| Z-Z, +D+0.750Lr+0.750L+0.5250E+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +D+0.750L+0.750S+0.5250E+H | None | 0.0 k-ft | Infinity | OK |
| Z-Z, +0.60D+W+H | 4.0 k-ft | 90.730 k-ft | 22.683 | OK |
| Z-Z, +0.60D+0.70E+H | None | 0.0 k-ft | Infinity | OK |

EBI Consulting
 21 B Street
 Burlington, MA 01803
 Tel:1-800-786-2346

Project Title:
 Engineer:
 Project Descr:

Project ID:

Printed: 18 MAR 2015, 11:13AM

General Footing

File = C:\Users\rapted\Desktop\1_Jobs\818353~1\1_MOVE~1\TOWERF~1.EC6
 ENERCALC, INC. 1983-2014, Build:6.14.9.18, Ver:6.14.9.18
 Licensee : ENVIROBUSINESS, INC.

Lic. # : KW-06008663
 Description : Tower Foundation

Sliding Stability

All units k

**Force Application Axis
 Load Combination...**

| Force Application Axis Load Combination... | Sliding Force | Resisting Force | Sliding SafetyRatio | Status |
|---|---------------|-----------------|---------------------|--------|
| X-X, D Only | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+L+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+Lr+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+S+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+0.750Lr+0.750L+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+0.750L+0.750S+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+W+H | 0.80 k | 38.243 k | 47.803 | OK |
| X-X, +D+0.70E+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+0.750Lr+0.750L+0.750W+H | 0.60 k | 38.243 k | 63.738 | OK |
| X-X, +D+0.750L+0.750S+0.750W+H | 0.60 k | 38.243 k | 63.738 | OK |
| X-X, +D+0.750Lr+0.750L+0.5250E+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +D+0.750L+0.750S+0.5250E+H | 0.0 k | 38.243 k | No Sliding | OK |
| X-X, +0.60D+W+H | 0.80 k | 24.633 k | 30.791 | OK |
| X-X, +0.60D+0.70E+H | 0.0 k | 24.633 k | No Sliding | OK |
| Z-Z, D Only | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+L+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+Lr+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+S+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+0.750Lr+0.750L+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+0.750L+0.750S+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+0.750Lr+0.750L+0.5250E+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+0.750L+0.750S+0.5250E+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +0.60D+W+H | 0.80 k | 24.633 k | 30.791 | OK |
| Z-Z, +0.60D+0.70E+H | 0.0 k | 24.633 k | No Sliding | OK |
| Z-Z, +D+W+H | 0.80 k | 38.243 k | 47.803 | OK |
| Z-Z, +D+0.70E+H | 0.0 k | 38.243 k | No Sliding | OK |
| Z-Z, +D+0.750Lr+0.750L+0.750W+H | 0.60 k | 38.243 k | 63.738 | OK |

One Way Shear

| Load Combination... | Vu @ -X | Vu @ +X | Vu @ -Z | Vu @ +Z | Vu:Max | Phi Vn | Vu / Phi*Vn | Status |
|---------------------------|---------|---------|---------|---------|--------|------------|-------------|--------|
| +1.40D | 0 psi | 0 psi | 0 psi | 0 psi | 0 psi | 82.158 psi | 0 | OK |
| +1.20D+1.60Lr+0.80W | 0 psi | 0 psi | 0 psi | 0 psi | 0 psi | 82.158 psi | 0 | OK |
| +1.20D+0.50Lr+0.50L+1.60W | 0 psi | 0 psi | 0 psi | 0 psi | 0 psi | 82.158 psi | 0 | OK |
| +0.90D+1.60W+1.60H | 0 psi | 0 psi | 0 psi | 0 psi | 0 psi | 82.158 psi | 0 | OK |

All units k

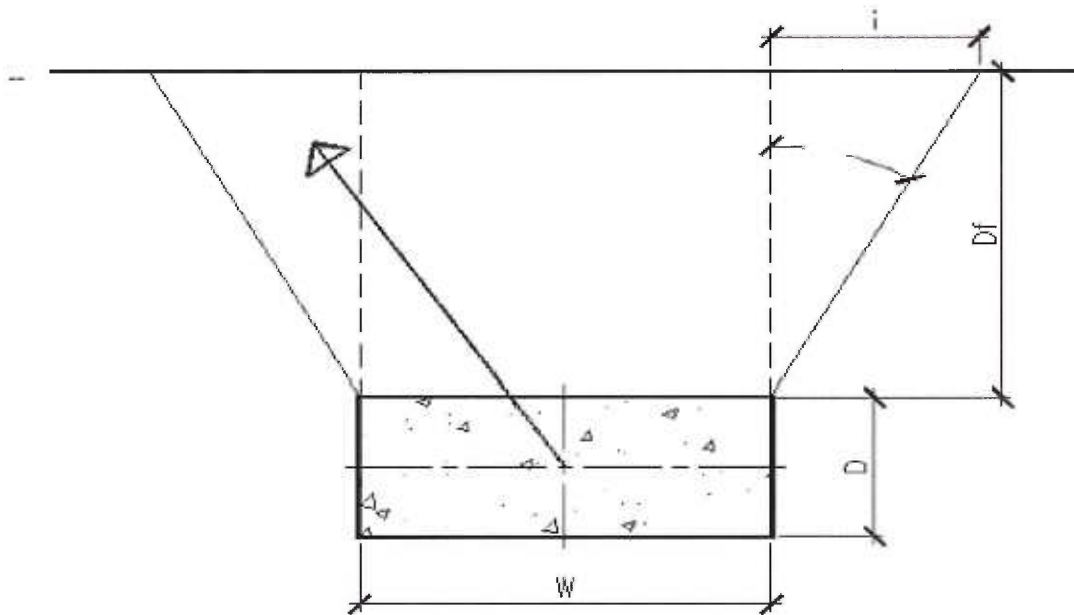
Punching Shear

| Load Combination... | Vu | Phi*Vn | Vu / Phi*Vn | Status |
|---------------------------|------------|------------|-------------|--------|
| +1.40D | 19.282 psi | 164.317psi | 0.1173 | OK |
| +1.20D+1.60Lr+0.80W | 16.527 psi | 164.317psi | 0.1006 | OK |
| +1.20D+0.50Lr+0.50L+1.60W | 16.527 psi | 164.317psi | 0.1006 | OK |
| +0.90D+1.60W+1.60H | 12.395 psi | 164.317psi | 0.07544 | OK |

Uplift and Sliding Capacity for Deadman Anchors, Inner Anchor

Spreadsheet Notes

User Note: Input all values in yellow highlighted regions, actual qualification output in green
 This spreadsheet calculates the uplift and sliding capacity of deadman anchors
 All units are noted
 Anchor Reactions from TNX Tower Output
 Foundation Dimensions per Centek's Structural Analysis, dated 12/6/13



Design Parameters

| | |
|---|--------------------------------|
| Anchor Radius | 68.25 feet |
| Axial Load On Anchor | 8.20 kips |
| Shear Load On Anchor | 8.90 kips |
| Depth to Top of Footing, Df | 8.00 feet |
| Anchor Width, W | 4.00 feet |
| Anchor Length, L | 7.00 feet |
| Anchor Thickness, D | 2.00 feet |
| Unit Weight of Soil | 68.00 pcf (Centek SA 12/06/13) |
| Unit Weight of Concrete | 150.00 pcf |
| Unit Weight of Water | 62.40 pcf |
| Depth to Ground Water | 20.00 ft (not encountered) |
| Coefficient of Passive Earth Pressure, Kp | 3.00 (estimated) |
| Angle of Friction, ϕ , degrees | 30.00 deg (estimated) |

| | |
|--|---------------|
| Angle of Friction, ϕ , radians | 0.52 radians |
| Guy anchor resultant load angle, degrees | 42.66 deg |
| Guy anchor resultant load angle, radians | 0.744 radians |

Soil Volume

| | |
|--------------------------------------|-----------|
| Inverted Pyramid Dimension, i | 4.62 ft |
| Effective Pyramid Width at Grade, a | 13.24 ft |
| Effective Pyramid Length at Grade, b | 16.24 ft |
| Inverted Pyramid Soil Volume, V | 858.01 cf |

Water Volume

| | |
|--------------------------------------|---------|
| Inverted Pyramid Dimension, i | 0.00 ft |
| Effective Pyramid Width at Water, a | 0.00 ft |
| Effective Pyramid Length at Water, b | 0.00 ft |
| Inverted Pyramid Water Volume, V | 0.00 cf |

Concrete Volume

| | |
|--|----------|
| Volume of Concrete, V | 56.00 cf |
| Buoyancy Effects, Effective Depth Water (concrete) | 0.00 ft |
| Buoyancy Effects, Volume of Water | 0.00 cf |

Material Weights

| | |
|------------------------------|------------|
| Weight of Soil | 58.34 kips |
| Weight of Water | 0.00 kips |
| Effective Weight of Soil | 58.34 kips |
| Weight of Concrete | 8.40 kips |
| Effective Weight of Concrete | 8.40 kips |

Skin Friction

| | |
|---|------------|
| Type of Soil, (S)and, (C)lay | S |
| Top of Block (Horizontal Component) | 5.57 kips |
| Ends of Block, total (Hor. & Vert. Component) | 0.00 kips |
| Ends of Block (Horizontal Component) | 0.00 kips |
| Ends of Block (Vertical Component) | 0.00 kips |
| Front of Block (Vertical Component) | 10.39 kips |

Uplift Check

| | |
|-------------------------------------|------------|
| Strength Reduction Factor, ϕ_s | 0.75 |
| Uplift Resistance, Rs | 57.85 kips |
| Anchor Adequate, Yes or No | YES |
| Anchor Usage | 14.2% |

Sliding Check

| | |
|-------------------------------------|-------------|
| Strength Reduction Factor, ϕ s | 0.75 |
| Passive Earth Pressure | 408.00 plf |
| Passive Earth Pressure | 2.86 kips |
| Surcharge Pressure | 3264.00 plf |
| Surcharge Pressure | 22.85 kips |
| Sliding Resistance | 4.85 kips |
| Total Lateral Earth Pressure | 36.13 kips |
| Sliding Resistance, R_s | 27.10 kips |
| Anchor Adequate, Yes or No | YES |
| Anchor Usage | 32.8% |

Uplift and Sliding Capacity for Deadman Anchors, Outer Anchor

Spreadsheet Notes

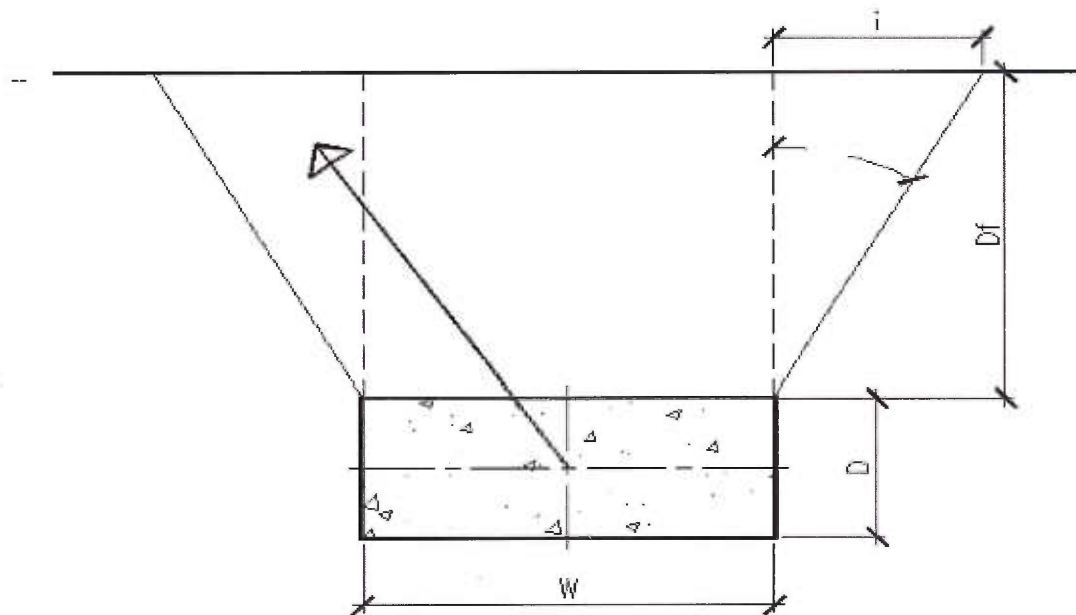
User Note: Input all values in yellow highlighted regions, actual qualification output in green

This spreadsheet calculates the uplift and sliding capacity of deadman anchors

All units are noted

Anchor Reactions from TNX Tower Output

Foundation Dimensions per Centek's Structural Analysis, dated 12/6/13



Design Parameters

| | |
|--|--------------------------------|
| Anchor Radius | 99.00 feet |
| Axial Load On Anchor | 27.50 kips |
| Shear Load On Anchor | 17.70 kips |
| Depth to Top of Footing, D_f | 8.00 feet |
| Anchor Width, W | 4.00 feet |
| Anchor Length, L | 7.00 feet |
| Anchor Thickness, D | 2.00 feet |
| Unit Weight of Soil | 68.00 pcf (Centek SA 12/06/13) |
| Unit Weight of Concrete | 150.00 pcf |
| Unit Weight of Water | 62.40 pcf |
| Depth to Ground Water | 20.00 ft (not encountered) |
| Coefficient of Passive Earth Pressure, K_p | 3.00 (estimated) |
| Angle of Friction, ϕ , degrees | 30.00 deg (estimated) |

| | |
|--|---------------|
| Angle of Friction, ϕ , radians | 0.52 radians |
| Guy anchor resultant load angle, degrees | 57.23 deg |
| Guy anchor resultant load angle, radians | 0.999 radians |

Soil Volume

| | |
|--------------------------------------|-----------|
| Inverted Pyramid Dimension, i | 4.62 ft |
| Effective Pyramid Width at Grade, a | 13.24 ft |
| Effective Pyramid Length at Grade, b | 16.24 ft |
| Inverted Pyramid Soil Volume, V | 858.01 cf |

Water Volume

| | |
|--------------------------------------|---------|
| Inverted Pyramid Dimension, i | 0.00 ft |
| Effective Pyramid Width at Water, a | 0.00 ft |
| Effective Pyramid Length at Water, b | 0.00 ft |
| Inverted Pyramid Water Volume, V | 0.00 cf |

Concrete Volume

| | |
|--|----------|
| Volume of Concrete, V | 56.00 cf |
| Buoyancy Effects, Effective Depth Water (concrete) | 0.00 ft |
| Buoyancy Effects, Volume of Water | 0.00 cf |

Material Weights

| | |
|------------------------------|------------|
| Weight of Soil | 58.34 kips |
| Weight of Water | 0.00 kips |
| Effective Weight of Soil | 58.34 kips |
| Weight of Concrete | 8.40 kips |
| Effective Weight of Concrete | 8.40 kips |

Skin Friction

| | |
|---|------------|
| Type of Soil, (S)and, (C)lay | S |
| Top of Block (Horizontal Component) | 5.57 kips |
| Ends of Block, total (Hor. & Vert. Component) | 0.00 kips |
| Ends of Block (Horizontal Component) | 0.00 kips |
| Ends of Block (Vertical Component) | 0.00 kips |
| Front of Block (Vertical Component) | 10.39 kips |

Uplift Check

| | |
|-------------------------------------|------------|
| Strength Reduction Factor, ϕ_s | 0.75 |
| Uplift Resistance, R_s | 57.85 kips |
| Anchor Adequate, Yes or No | YES |
| Anchor Usage | 47.5% |

Sliding Check

| | |
|-------------------------------------|-------------|
| Strength Reduction Factor, ϕ s | 0.75 |
| Passive Earth Pressure | 408.00 plf |
| Passive Earth Pressure | 2.86 kips |
| Surcharge Pressure | 3264.00 plf |
| Surcharge Pressure | 22.85 kips |
| Sliding Resistance | 4.85 kips |
| Total Lateral Earth Pressure | 36.13 kips |
| Sliding Resistance, R_s | 27.10 kips |
| Anchor Adequate, Yes or No | YES |
| Anchor Usage | 65.3% |

EXHIBIT C

RADIO FREQUENCY EMISSIONS ANALYSIS REPORT
EVALUATION OF HUMAN EXPOSURE POTENTIAL
TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11156A

Killingly/ Margaret Henr1
818 Providence Pike
Killingly, CT 06239

March 16, 2015

EBI Project Number: 6215001659

| Site Compliance Summary | |
|--|------------------|
| Compliance Status: | COMPLIANT |
| Site total MPE% of FCC general public allowable limit: | 18.71 % |

March 16, 2015

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

Emissions Analysis for Site: **CT11156A – Killingly/ Margaret Henri**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **818 Providence Pike, Killingly, CT**, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limit for the 700 MHz Band is $467 \mu\text{W}/\text{cm}^2$, and the general population exposure limit for the PCS band is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **818 Providence Pike, Killingly, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
- 2) 2 UMTS channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 LTE channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 1 LTE channel (700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
- 5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.

- 6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antennas used in this modeling are the **EMS RR90_17_02DP** for 1900 MHz (PCS) channels and the **Commscope LNX-6515DS-VTM** for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The **EMS RR90_17_02DP** has a maximum gain of **14.4 dBd** at its main lobe. The **Commscope LNX-6515DS-VTM** has a maximum gain of **14.6 dBd** at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antenna mounting height centerline of the proposed antennas is **145 feet** above ground level (AGL).
- 9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
|-----------------|------------------------------|-----------------|------------------------------|-----------------|------------------------------|
| Antenna #: | 1 | Antenna #: | 1 | Antenna #: | 1 |
| Make / Model: | EMS RR90 17 02DP | Make / Model: | EMS RR90 17 02DP | Make / Model: | EMS RR90 17 02DP |
| Gain: | 14.4 dBd | Gain: | 14.4 dBd | Gain: | 14.4 dBd |
| Height (AGL): | 145 | Height (AGL): | 145 | Height (AGL): | 145 |
| Frequency Bands | 1900 MHz(PCS) | Frequency Bands | 1900 MHz(PCS) | Frequency Bands | 1900 MHz(PCS) |
| Channel Count | 6 | Channel Count | 6 | # PCS Channels: | 6 |
| Total TX Power: | 240 | Total TX Power: | 240 | # AWS Channels: | 240 |
| ERP (W): | 6,610.15 | ERP (W): | 6,610.15 | ERP (W): | 6,610.15 |
| Antenna A1 MPE% | 1.23 | Antenna B1 MPE% | 1.23 | Antenna C1 MPE% | 1.23 |
| Antenna #: | 2 | Antenna #: | 2 | Antenna #: | 2 |
| Make / Model: | Commscope LNX- 6515DS-VTM | Make / Model: | Commscope LNX- 6515DS-VTM | Make / Model: | Commscope LNX- 6515DS-VTM |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 145 | Height (AGL): | 145 | Height (AGL): | 145 |
| Frequency Bands | 700 MHz | Frequency Bands | 700 MHz | Frequency Bands | 700 MHz |
| Channel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power: | 30 | Total TX Power: | 30 |
| ERP (W): | 865.21 | ERP (W): | 865.21 | ERP (W): | 865.21 |
| Antenna A2 MPE% | 0.34 | Antenna B2 MPE% | 0.34 | Antenna C2 MPE% | 0.34 |

| Site Composite MPE% | |
|--------------------------|----------------|
| Carrier | MPE% |
| T-Mobile | 4.72 |
| Verizon Wireless | 13.99 % |
| Site Total MPE %: | 18.71 % |

| | |
|--------------------------|----------------|
| T-Mobile Sector 1 Total: | 1.57 % |
| T-Mobile Sector 2 Total: | 1.57 % |
| T-Mobile Sector 3 Total: | 1.57 % |
| Site Total: | 18.71 % |

Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (%) |
|-------------------------|-------------------------|
| Sector 1: | 1.57 % |
| Sector 2: | 1.57 % |
| Sector 3 : | 1.57 % |
| T-Mobile Total: | 4.72 % |
| | |
| Site Total: | 18.71 % |
| | |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is **18.71%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



Scott Heffernan
RF Engineering Director

EBI Consulting
21 B Street
Burlington, MA 01803