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April 24, 2023

VIA EMAIL AND FEDERAL EXPRESS

Members of the Connecticut Siting Council
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

Re: Tower Sharing Request by New Cingular Wireless PCS, LLC
TS-ATT-069-230331
Premises: 812 Providence Pike, Danielson (Killingly, Connecticut)

Dear Members of the Siting Council:

This letter is respectfully submitted on behalf of our client, New Cingular Wireless PCS, LLC (“AT&T”), in connection with the request dated March 30, 2023 for an order from the Connecticut Siting Council (the “Council”) to approve the shared use of a communications tower and compound at the parcel identified as 812 Providence Pike, in the Town of Danielson (Killingly).

The Council issued a Notice of Incompletion dated April 19, 2023 requesting an updated mount analysis that comports with the current 2022 CSBC. The Mount Analysis prepared by TEP Northeast dated August 2, 2022, enclosed as **Attachment 1**, and the Structural Analysis Report & Reinforcement Design prepared by CENTEK Engineering, Inc., dated February 20, 2023, enclosed as **Attachment 2**, are hereby submitted which finds that the proposed mounts comports with the current 2022 CSBC, supporting AT&T’s proposed installation. These materials together demonstrate that the proposed antenna mounts can support the proposed loading.

Thank you for your consideration of this request. Should the Council members or Staff have any questions regarding the foregoing, please do not hesitate to contact me.

Very truly yours,

A handwritten signature in blue ink, appearing to read 'DP', is written over a light blue horizontal line.

Daniel Patrick

Attachments

cc: AT&T
Lucia Chiochio, Esq.
Riddar Nget

Attachment 1

December 7, 2021
August 2, 2022 (Rev. 1)
November 28, 2022 (Rev. 2)



SAI Communications
12 Industrial Way
Salem NH, 03079

RE: AT&T Site Number: CT1166 (NSB)
 FA Number: 10141308
 PACE Number: MRCTB061417
 PT Number: 2051A13RPW
 TEP Project Number: 350560
 AT&T Site Name: DANIELSON
 Site Address: 812 Providence Pike
 Danielson, CT 06239

To Whom It May Concern:

TEP Northeast (TEP NE) has been authorized by SAI Communications to perform a mount analysis on the proposed AT&T antenna/RRH mounts to determine their capability of supporting the following additional loading:

- **(3) TPA65R-BU8DA-K Antennas (96.0"x20.7"x7.7" – Wt. = 87 lbs. /each) (Pos. 1)**
- **(3) DMP65R-BU8DA-K Antennas (96.0"x20.7"x7.7" – Wt. = 119 lbs. /each) (Pos. 2)**
- **(3) 4478 B14 RRH's (18.1"x13.4"x8.3" – Wt. = 60 lbs. /each) (Tower Leg)**
- **(3) 4415 B25 RRH's (14.9"x13.2"x5.4" – Wt. = 44 lbs. /each) (Tower Leg)**
- **(3) 4449 B5/B12 RRH's (17.9"x13.2"x9.4" – Wt. = 73 lbs. /each) (Tower Leg)**
- **(3) 4426 B66 RRH's (14.9"x13.2"x5.8" – Wt. = 49 lbs. /each) (Tower Leg)**
- **(2) Surge Arrestor (31.4"x10.2"Ø – Wt. = 29 lbs. /each) (Tower Leg)**

**Proposed equipment shown in bold.*

Mount fabrication drawings prepared by SitePro1, P/N TAP-472, dated March 29, 2011, P/N R5, dated November 12, 2015, and P/N MM02, dated May 10, 2010 were used to perform this analysis.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-H, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2021 with 2022 Connecticut State Building Code, and AT&T Mount Technical Directive – R22.
- TEP NE considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all around the mount. Per TIA-222-H and Appendix P of the Connecticut State Building Code, the max basic wind speed for this site is equal to 125 mph with a max basic wind speed with ice of 50 mph and a max ice thickness of 1.0 in. An escalated ice thickness of 1.18 in was used for this analysis.
- TEP NE considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.
- TEP NE considers this site to be topographic category 1; tower is located on flat terrain or the bottom of a hill or ridge.
- TEP NE considers this site to have a spectral response acceleration parameter at short periods, S_s , of 0.186 and a spectral response acceleration parameter at a period of 1 second, S_1 , of 0.054.
- The mount has been analyzed with load combinations consisting of 500 lbs live load using a service wind speed of 30 mph wind on the worst case antenna. Analysis performed on each antenna pipe to determine worst case location; worst case location was antenna position 2.
- The mount has been analyzed with load combinations consisting of a 250 lbs live load in a worst case location on the mount.
- The proposed mounts will be secured to the existing guyed tower with threaded rods and steel plates tightened around the tower leg. TEP NE considers the threaded rods as the governing connection members.

Based on our evaluation, we have determined that the (6) Proposed SitePro1 TAP-472 mounts, (8) Proposed SitePro1 MM02 standoffs, and (2) Proposed SitePro1 R5 mount **ARE CAPABLE** of supporting the proposed installation.

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Proposed Mount Rating	269	LC7	62%	PASS

Reference Documents:

- Fabrication drawings prepared by SitePro1, P/N TAP-472 dated March 29, 2011.
- Fabrication drawings prepared by SitePro1, P/N R5 dated November 12, 2015.
- Fabrication drawings prepared by SitePro1, P/N MM02 dated May 10, 2010.

This determination was based on the following limitations and assumptions:

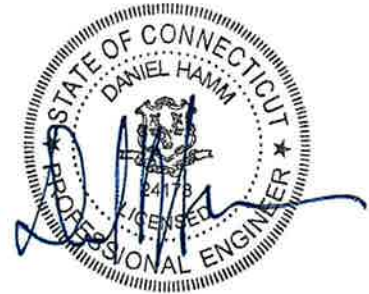
1. TEP NE is not responsible for any modifications completed prior to and hereafter which TEP NE was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The proposed mounts will be adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. TEP NE performed a localized analysis on the mounts itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,
TEP Northeast



Michael Cabral
Director



Daniel P. Hamm, PE
Vice President



Wind & Ice Calculations

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$z = 175$ (ft)
 $z_g = 1200$ (ft)
 $\alpha = 7.0$

$K_z = 1.160$

$K_{zmin} \leq K_z \leq 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_c
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.2 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_c K_t / K_h)]^2$$

$$K_h = e^{(-z/H)}$$

$K_{zt} = 1$

(If Category 1 then $K_{zt} = 1.0$)

Category = 1

$K_h = 1$
 $K_c = 0.9$ (from Table 2-4)
 $K_t = 0$ (from Table 2-5)
 $f = 0$ (from Table 2-5)
 $z = 175$
 $z_s = 665$ (Mean elevation of base of structure above sea level)
 $H = 0$ (Ht. of the crest above surrounding terrain)
 $K_{zt} = 1.00$ (from 2.6.6.2.1)
 $K_e = 0.98$ (from 2.6.8)

2.6.10 Design Ice Thickness

Max Ice Thickness =
 Importance Factor =

$t_i = 1.00$ in
 $I = 1.00$ (from Table 2-3)
 $K_{iz} = 1.18$ (from Sec. 2.6.10)

$$t_{iz} = t_i * I * K_{iz} * (K_{zt})^{0.35}$$

$t_{iz} = 1.18$ in

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



2.6.9 Gust Effect Factor

2.6.9.1 Self Supporting Lattice Structures

$G_h = 1.0$ Latticed Structures > 600 ft

$G_h = 0.85$ Latticed Structures 450 ft or less

$G_h = 0.85 + 0.15 [h/150 - 3.0]$

$h =$ ht. of structure

$h =$ 190

$G_h =$ 0.85

2.6.9.2 Guyed Masts

$G_h =$ 0.85

2.6.9.3 Pole Structures

$G_h =$ 1.1

2.6.9 Appurtenances

$G_h =$ 1.0

2.6.9.4 Structures Supported on Other Structures

(Cantilevered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5))

$G_h =$ 1.35

$G_h =$ 1.00

2.6.11.2 Design Wind Force on Appurtenances

$F = q_z * G_h * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_s * K_e * K_d * V_{max}^2$

$q_z =$ 38.49
 $q_{z(ice)} =$ 6.16
 $q_{z(30)} =$ 2.22

$K_z =$ 1.160 (from 2.6.5.2)
 $K_{zt} =$ 1.0 (from 2.6.6.2.1)
 $K_s =$ 1.0 (from 2.6.7)
 $K_e =$ 0.98 (from 2.6.8)
 $K_d =$ 0.85 (from Table 2-2)
 $V_{max} =$ 125 mph (Ultimate Wind Speed)
 $V_{max(ice)} =$ 50 mph
 $V_{30} =$ 30 mph

Table 2-2

Structure Type	Wind Direction Probability Factor, K_d
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95
Tubular pole structures supporting antennas enclosed within a cylindrical shroud	1.00

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



Determine Ca:

Table 2-9

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Square/Rectangular HSS		$1.2 - 2.8(r_s) ≥ 0.85$	$1.4 - 4.0(r_s) ≥ 0.90$	$2.0 - 6.0(r_s) ≥ 1.25$
Round	C < 39 (Subcritical)	0.7	0.8	1.2
	39 ≤ C ≤ 78 (Transitional)	$4.14/(C^{0.485})$	$3.66/(C^{0.415})$	$46.8/(C^{1.0})$
	C > 78 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
 (Aspect ratio is independent of the spacing between support points of a linear appurtenance.)

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = **1.18 in** **Angle = 0 (deg)** **Equivalent Angle = 180 (deg)**

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	4.64	1.30	688	126	40
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	4.64	1.30	688	126	40
4478 B14 RRH	18.1	13.4	8.3	1.68	1.35	1.20	78	17	4
4415 B25 RRH	16.5	13.5	6.3	1.55	1.22	1.20	71	15	4
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.36	1.20	76	16	4
4426 B66 RRH	14.9	13.2	5.8	1.37	1.13	1.20	63	14	4
Surge Arrestor	31.4	10.2	10.2	2.22	3.08	0.70	60	13	3
2" Pipe	2.4	12.0		0.20	0.20	1.20	9		
4" Pipe	4.5	12.0		0.38	0.38	1.20	17		
HSS 2-1/2x2-1/2	2.5	12.0		0.21	0.21	1.25	10		
HSS 4x4	4.0	12.0		0.33	0.33	1.25	16		

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 30 (deg)

Ice Thickness = 1.18 in.

Equivalent Angle = 210 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	594
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	594
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	78	48	70
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	71	33	62
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	76	54	70
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	63	28	54

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	109
DMP65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	109
4478 B14 RRH	20.5	15.8	10.7	2.24	1.52	1.30	1.92	1.20	1.20	17	11	15
4415 B25 RRH	18.9	15.9	8.7	2.08	1.13	1.19	2.18	1.20	1.20	15	8	14
4449 B5/B12 RRH	20.3	15.6	11.8	2.19	1.66	1.30	1.72	1.20	1.20	16	12	15
4426 B66 RRH	17.3	15.6	8.2	1.87	0.98	1.11	2.11	1.20	1.20	14	7	12

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	34
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	34
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	4	3	4
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	4	2	4
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	4	3	4
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	4	2	3

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 60 (deg)

Ice Thickness = 1.18 in.

Equivalent Angle = 240 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	406
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	406
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	78	48	56
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	71	33	43
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	76	54	59
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	63	28	37

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	78
DMP65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	78
4478 B14 RRH	20.5	15.8	10.7	2.24	1.52	1.30	1.92	1.20	1.20	17	11	13
4415 B25 RRH	18.9	15.9	8.7	2.08	1.13	1.19	2.18	1.20	1.20	15	8	10
4449 B5/B12 RRH	20.3	15.6	11.8	2.19	1.66	1.30	1.72	1.20	1.20	16	12	13
4426 B66 RRH	17.3	15.6	8.2	1.87	0.98	1.11	2.11	1.20	1.20	14	7	9

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	23
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	23
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	4	3	3
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	4	2	2
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	4	3	3
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	4	2	2

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 90 (deg) Ice Thickness = 1.18 in. Equivalent Angle = 270 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	313
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	313
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	78	48	48
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	71	33	33
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	76	54	54
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	63	28	28

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	63
DMP65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	63
4478 B14 RRH	20.5	15.8	10.7	2.24	1.52	1.30	1.92	1.20	1.20	17	11	11
4415 B25 RRH	18.9	15.9	8.7	2.08	1.13	1.19	2.18	1.20	1.20	15	8	8
4449 B5/B12 RRH	20.3	15.6	11.8	2.19	1.66	1.30	1.72	1.20	1.20	16	12	12
4426 B66 RRH	17.3	15.6	8.2	1.87	0.98	1.11	2.11	1.20	1.20	14	7	7

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	18
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	18
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	4	3	3
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	4	2	2
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	4	3	3
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	4	2	2

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 120 (deg) Ice Thickness = 1.18 in. Equivalent Angle = 300 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	406
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	406
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	78	48	56
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	71	33	43
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	76	54	59
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	63	28	37

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	78
DMP65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	78
4478 B14 RRH	20.5	15.8	10.7	2.24	1.52	1.30	1.92	1.20	1.20	17	11	13
4415 B25 RRH	18.9	15.9	8.7	2.08	1.13	1.19	2.18	1.20	1.20	15	8	10
4449 B5/B12 RRH	20.3	15.6	11.8	2.19	1.66	1.30	1.72	1.20	1.20	16	12	13
4426 B66 RRH	17.3	15.6	8.2	1.87	0.98	1.11	2.11	1.20	1.20	14	7	9

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	23
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	23
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	4	3	3
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	4	2	2
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	4	3	3
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	4	2	2

Date: 11/28/2022
 Project Name: DANIELSON
 Project No.: CT1166
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 150 (deg) Ice Thickness = 1.18 in. Equivalent Angle = 330 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	594
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	688	313	594
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	78	48	70
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	71	33	62
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	76	54	70
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	63	28	54

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	109
DMP65R-BU8DA-K Antenna	98.4	23.1	10.1	15.75	6.87	4.26	9.77	1.28	1.49	124	63	109
4478 B14 RRH	20.5	15.8	10.7	2.24	1.52	1.30	1.92	1.20	1.20	17	11	15
4415 B25 RRH	18.9	15.9	8.7	2.08	1.13	1.19	2.18	1.20	1.20	15	8	14
4449 B5/B12 RRH	20.3	15.6	11.8	2.19	1.66	1.30	1.72	1.20	1.20	16	12	15
4426 B66 RRH	17.3	15.6	8.2	1.87	0.98	1.11	2.11	1.20	1.20	14	7	12

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	34
DMP65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	40	18	34
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	4	3	4
4415 B25 RRH	16.5	13.5	6.3	1.55	0.72	1.22	2.62	1.20	1.21	4	2	4
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	4	3	4
4426 B66 RRH	14.9	13.2	5.8	1.37	0.60	1.13	2.57	1.20	1.20	4	2	3

Date: 11/28/2022

Project Name: DANIELSON

Project No.: CT1166

Designed By: JC Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice: 1.18 in.
Density of ice: 56 pcf

TPA65R-BU8DA-K Antenna

Weight of ice based on total radial SF area:
Height (in): 96.0
Width (in): 20.7
Depth (in): 7.7
Total weight of ice on object: 268 lbs
Weight of object: 87.0 lbs
Combined weight of ice and object: 355 lbs

DMP65R-BU8DA-K Antenna

Weight of ice based on total radial SF area:
Height (in): 96.0
Width (in): 20.7
Depth (in): 7.7
Total weight of ice on object: 268 lbs
Weight of object: 119.0 lbs
Combined weight of ice and object: 387 lbs

4478 B14 RRH

Weight of ice based on total radial SF area:
Height (in): 18.1
Width (in): 13.4
Depth (in): 8.3
Total weight of ice on object: 37 lbs
Weight of object: 60.0 lbs
Combined weight of ice and object: 97 lbs

4415 B25 RRH

Weight of ice based on total radial SF area:
Height (in): 16.5
Width (in): 13.5
Depth (in): 6.3
Total weight of ice on object: 32 lbs
Weight of object: 50.0 lbs
Combined weight of ice and object: 82 lbs

4449 B5/B12 RRH

Weight of ice based on total radial SF area:
Height (in): 17.9
Width (in): 13.2
Depth (in): 9.4
Total weight of ice on object: 37 lbs
Weight of object: 73.0 lbs
Combined weight of ice and object: 110 lbs

4426 B66 RRH

Weight of ice based on total radial SF area:
Height (in): 14.9
Width (in): 13.2
Depth (in): 5.8
Total weight of ice on object: 28 lbs
Weight of object: 49.0 lbs
Combined weight of ice and object: 77 lbs

Squid Surge Arrestor

Weight of ice based on total radial SF area:
Depth (in): 31.4
Diameter(in): 10.2
Total weight of ice on object: 43 lbs
Weight of object: 29 lbs
Combined weight of ice and object: 72 lbs

2" pipe

Per foot weight of ice:
diameter (in): 2.38
Per foot weight of ice on object: 5 plf

HSS 2-1/2x2-1/2

Weight of ice based on total radial SF area:
Height (in): 2.5
Width (in): 2.5
Per foot weight of ice on object: 7 plf

4" Pipe

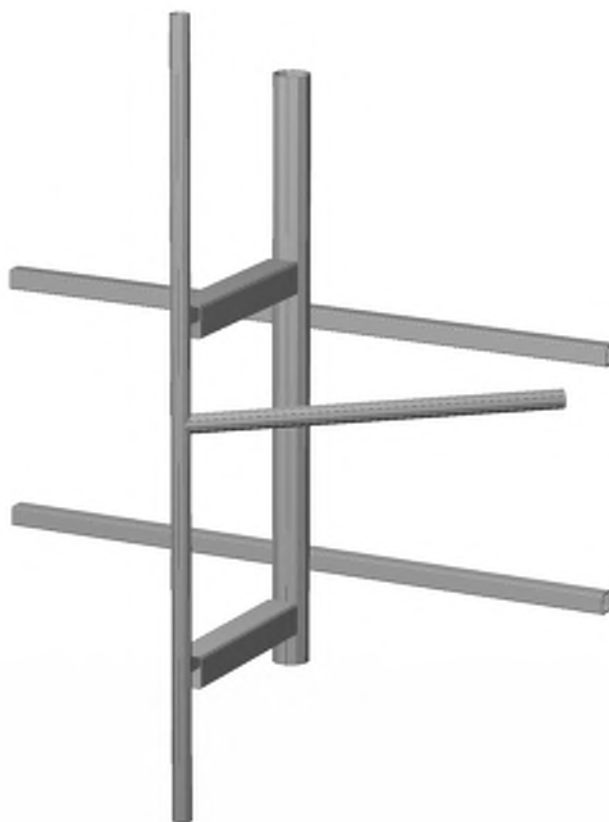
Per foot weight of ice:
diameter (in): 4.5
Per foot weight of ice on object: 8 plf

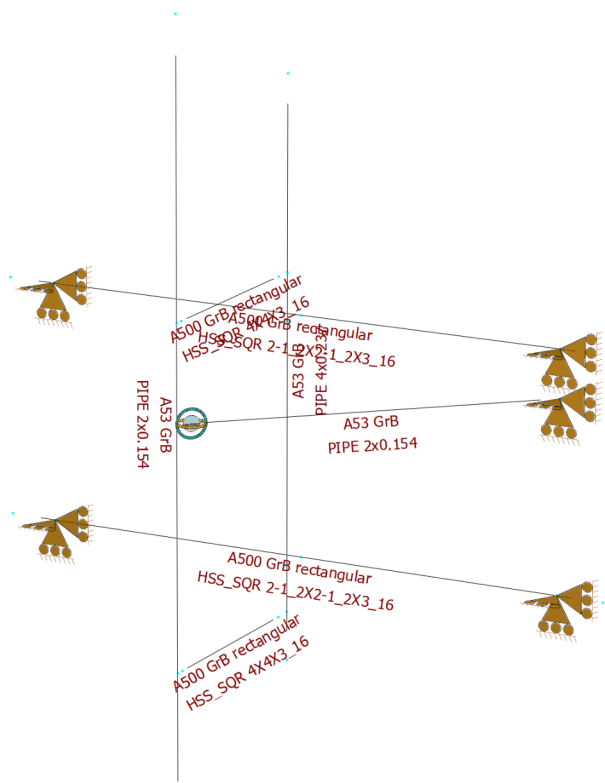
HSS 4x4

Weight of ice based on total radial SF area:
Height (in): 4
Width (in): 4
Per foot weight of ice on object: 10 plf



**Mount Calculations
(Proposed Conditions)**

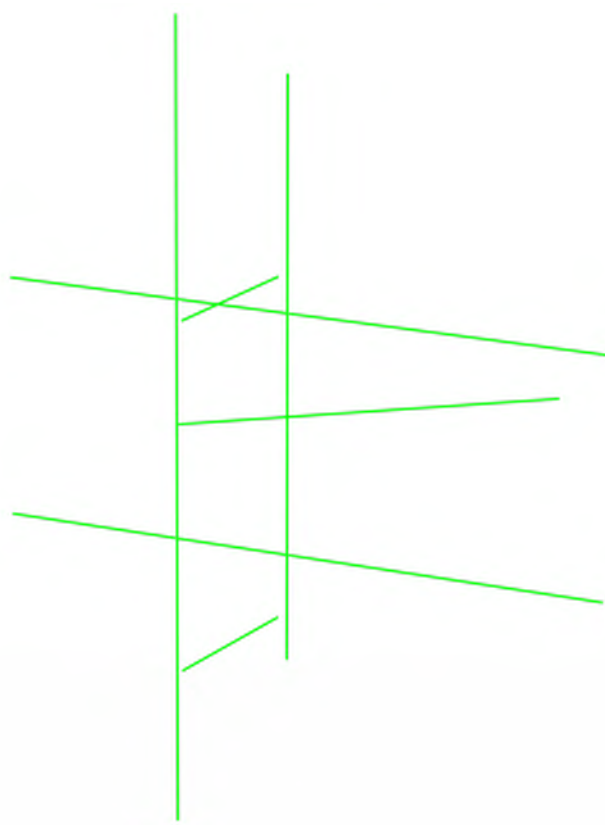


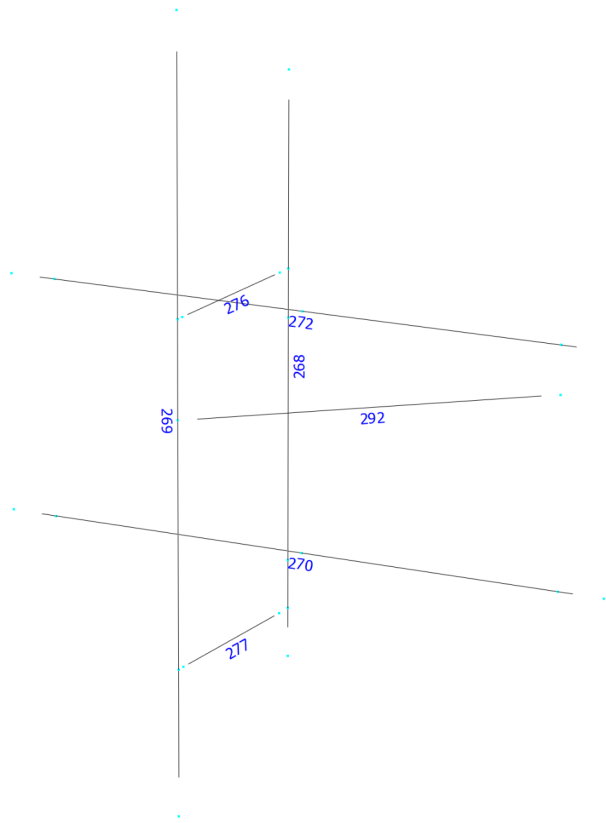




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Load data

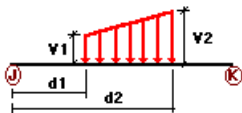
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND
LL1	250 lb Live Load Center of Mount	No	LL
LL2	250 lb Live Load Right End of Mount	No	LL
LL3	250 lb Live Load Left End of Mount	No	LL
LLa1	500 lb Live Load Antenna 1	No	LL

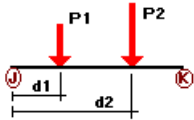
Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	268	z	-0.017	0.00	0.00	No	0.00	No
	270	z	-0.01	0.00	0.00	No	0.00	No
	272	z	-0.01	0.00	0.00	No	0.00	No
	292	z	-0.009	0.00	0.00	No	0.00	No
W30	268	z	-0.017	0.00	0.00	No	0.00	No
	270	z	-0.01	0.00	0.00	No	0.00	No
	272	z	-0.01	0.00	0.00	No	0.00	No
	276	z	-0.016	0.00	0.00	No	0.00	No
	277	z	-0.016	0.00	0.00	No	0.00	No
	292	z	-0.009	0.00	0.00	No	0.00	No
W60	268	x	-0.017	0.00	0.00	No	0.00	No
	269	3	-0.009	0.00	0.00	No	0.00	No
	270	x	-0.01	0.00	0.00	No	0.00	No

	272	x	-0.01	0.00	0.00	No	0.00	No
	276	x	-0.016	0.00	0.00	No	0.00	No
	277	x	-0.016	0.00	0.00	No	0.00	No
	292	x	-0.009	0.00	0.00	No	0.00	No
W90	268	x	-0.017	0.00	0.00	No	0.00	No
	269	x	-0.009	0.00	0.00	No	0.00	No
	276	x	-0.016	0.00	0.00	No	0.00	No
	277	x	-0.016	0.00	0.00	No	0.00	No
	292	x	-0.009	0.00	0.00	No	0.00	No
W120	268	x	-0.017	0.00	0.00	No	0.00	No
	269	2	-0.009	0.00	0.00	No	0.00	No
	270	x	-0.01	0.00	0.00	No	0.00	No
	272	x	-0.01	0.00	0.00	No	0.00	No
	276	x	-0.016	0.00	0.00	No	0.00	No
	277	x	-0.016	0.00	0.00	No	0.00	No
	292	x	-0.009	0.00	0.00	No	0.00	No
W150	268	z	0.017	0.00	0.00	No	0.00	No
	269	2	-0.009	0.00	0.00	No	0.00	No
	270	z	0.01	0.00	0.00	No	0.00	No
	272	z	0.01	0.00	0.00	No	0.00	No
	276	z	0.016	0.00	0.00	No	0.00	No
	277	z	0.016	0.00	0.00	No	0.00	No
	292	z	0.009	0.00	0.00	No	0.00	No
Di	268	y	-0.008	0.00	0.00	No	0.00	No
	269	y	-0.005	0.00	0.00	No	0.00	No
	270	y	-0.007	0.00	0.00	No	0.00	No
	272	y	-0.007	0.00	0.00	No	0.00	No
	276	y	-0.01	0.00	0.00	No	0.00	No
	277	y	-0.01	0.00	0.00	No	0.00	No
	292	y	-0.005	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	269	y	-0.044	0.50	No
		y	-0.044	7.50	No
Wo	269	z	-0.344	0.50	No
		z	-0.344	7.50	No
W30	269	3	-0.298	0.50	No
		3	-0.298	7.50	No
W60	269	3	-0.204	0.50	No
		3	-0.204	7.50	No
W90	269	x	-0.157	0.50	No
		x	-0.157	7.50	No
W120	269	2	-0.204	0.50	No
		2	-0.204	7.50	No
W150	269	2	-0.298	0.50	No
		2	-0.298	7.50	No
Di	269	y	-0.134	0.50	No
		y	-0.134	7.50	No
WI0	269	z	-0.063	0.50	No
		z	-0.063	7.50	No
WI30	269	3	-0.055	0.50	No
		3	-0.055	7.50	No
WI60	269	3	-0.04	0.50	No
		3	-0.04	7.50	No

WI90	269	x	-0.032	0.50	No
		x	-0.032	7.50	No
WI120	269	2	-0.04	0.50	No
		2	-0.04	7.50	No
WI150	269	2	-0.055	0.50	No
		2	-0.055	7.50	No
WL0	269	z	-0.02	0.50	No
		z	-0.02	7.50	No
WL30	269	3	-0.018	0.50	No
		3	-0.018	7.50	No
WL60	269	3	-0.012	0.50	No
		3	-0.012	7.50	No
WL90	269	x	-0.01	0.50	No
		x	-0.01	7.50	No
WL120	269	2	-0.012	0.50	No
		2	-0.012	7.50	No
WL150	269	2	-0.018	0.50	No
		2	-0.018	7.50	No
LLa1	269	y	-0.50	4.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00
LL1	250 lb Live Load Center of Mount	No	0.00	0.00	0.00
LL2	250 lb Live Load Right End of Mount	No	0.00	0.00	0.00
LL3	250 lb Live Load Left End of Mount	No	0.00	0.00	0.00
LLa1	500 lb Live Load Antenna 1	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00
LL1	0.00	0.00	0.00
LL2	0.00	0.00	0.00
LL3	0.00	0.00	0.00
LLa1	0.00	0.00	0.00

Steel Code Check

Report: Summary - Group by member**Load conditions to be included in design :**

LC1=1.2D+Wo
LC2=1.2D+W30
LC3=1.2D+W60
LC4=1.2D+W90
LC5=1.2D+W120
LC6=1.2D+W150
LC7=1.2D-Wo
LC8=1.2D-W30
LC9=1.2D-W60
LC10=1.2D-W90
LC11=1.2D-W120
LC12=1.2D-W150
LC13=0.9D+Wo
LC14=0.9D+W30
LC15=0.9D+W60
LC16=0.9D+W90
LC17=0.9D+W120
LC18=0.9D+W150
LC19=0.9D-Wo
LC20=0.9D-W30
LC21=0.9D-W60
LC22=0.9D-W90
LC23=0.9D-W120
LC24=0.9D-W150
LC25=1.2D+Di+Wi0
LC26=1.2D+Di+Wi30
LC27=1.2D+Di+Wi60
LC28=1.2D+Di+Wi90
LC29=1.2D+Di+Wi120
LC30=1.2D+Di+Wi150
LC31=1.2D+Di-Wi0
LC32=1.2D+Di-Wi30
LC33=1.2D+Di-Wi60
LC34=1.2D+Di-Wi90
LC35=1.2D+Di-Wi120
LC36=1.2D+Di-Wi150
LC37=1.2D+1.6LL1
LC38=1.2D+1.6LL2
LC39=1.2D+1.6LL3
LC40=1.2D+WLo+1.6LLa1
LC41=1.2D+WLo30+1.6LLa1
LC42=1.2D+WLo60+1.6LLa1
LC43=1.2D+WLo90+1.6LLa1
LC44=1.2D+WLo120+1.6LLa1
LC45=1.2D+WLo150+1.6LLa1
LC46=1.2D-WLo+1.6LLa1
LC47=1.2D-WLo30+1.6LLa1
LC48=1.2D-WLo60+1.6LLa1
LC49=1.2D-WLo90+1.6LLa1
LC50=1.2D-WLo120+1.6LLa1
LC51=1.2D-WLo150+1.6LLa1
LC52=1.2D+WLo
LC53=1.2D+WLo30
LC54=1.2D+WLo60
LC55=1.2D+WLo90
LC56=1.2D+WLo120
LC57=1.2D+WLo150
LC58=1.2D-WLo
LC59=1.2D-WLo30
LC60=1.2D-WLo60

LC61=1.2D-WL90
 LC62=1.2D-WL120
 LC63=1.2D-WL150
 LC64=1.2D+WL0
 LC65=1.2D+WL30
 LC66=1.2D+WL60
 LC67=1.2D+WL90
 LC68=1.2D+WL120
 LC69=1.2D+WL150
 LC70=1.2D-WL0
 LC71=1.2D-WL30
 LC72=1.2D-WL60
 LC73=1.2D-WL90
 LC74=1.2D-WL120
 LC75=1.2D-WL150
 LC76=1.2D+WL0
 LC77=1.2D+WL30
 LC78=1.2D+WL60
 LC79=1.2D+WL90
 LC80=1.2D+WL120
 LC81=1.2D+WL150
 LC82=1.2D-WL0
 LC83=1.2D-WL30
 LC84=1.2D-WL60
 LC85=1.2D-WL90
 LC86=1.2D-WL120
 LC87=1.2D-WL150

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	<i>HSS_SQR 2-1_2X2-1_2X3_16</i>	270	LC40 at 50.00%	0.52	OK	
		272	LC47 at 48.44%	0.48	OK	
	<i>HSS_SQR 4X4X3_16</i>	276	LC47 at 100.00%	0.06	OK	
		277	LC47 at 100.00%	0.06	OK	
	<i>PIPE 2x0.154</i>	269	LC7 at 35.94%	0.62	OK	
		292	LC24 at 100.00%	0.02	OK	
	<i>PIPE 4x0.237</i>	268	LC45 at 82.50%	0.09	OK	

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
469	0.00	0.00	2.0833	0
471	3.3333	0.00	2.0833	0
473	-3.3333	0.00	2.0833	0
475	0.00	0.00	2.375	0
477	-3.3333	2.50	2.0833	0
479	3.3333	2.50	2.0833	0
481	0.00	2.50	2.375	0
483	0.00	2.50	2.0833	0
485	0.00	-1.00	2.375	0
487	0.00	5.00	2.375	0
489	0.00	-0.50	2.375	0
491	0.00	3.00	2.375	0
493	0.00	-0.50	2.5625	0
495	0.00	3.00	2.5625	0
497	0.00	-0.50	4.5625	0
499	0.00	3.00	4.5625	0
501	0.00	-0.50	4.6617	0
503	0.00	3.00	4.6617	0
505	0.00	-2.00	4.6617	0
507	0.00	6.00	4.6617	0
509	2.8333	0.00	2.0833	0
513	-2.8333	0.00	2.0833	0
517	2.8333	2.00	2.0833	0
518	0.00	2.00	4.6617	0
519	-2.8333	2.50	2.0833	0
520	2.8333	2.50	2.0833	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
509	1	1	1	0	0	0
513	1	1	1	0	0	0
517	1	1	1	0	0	0
519	1	1	1	0	0	0
520	1	1	1	0	0	0

Members

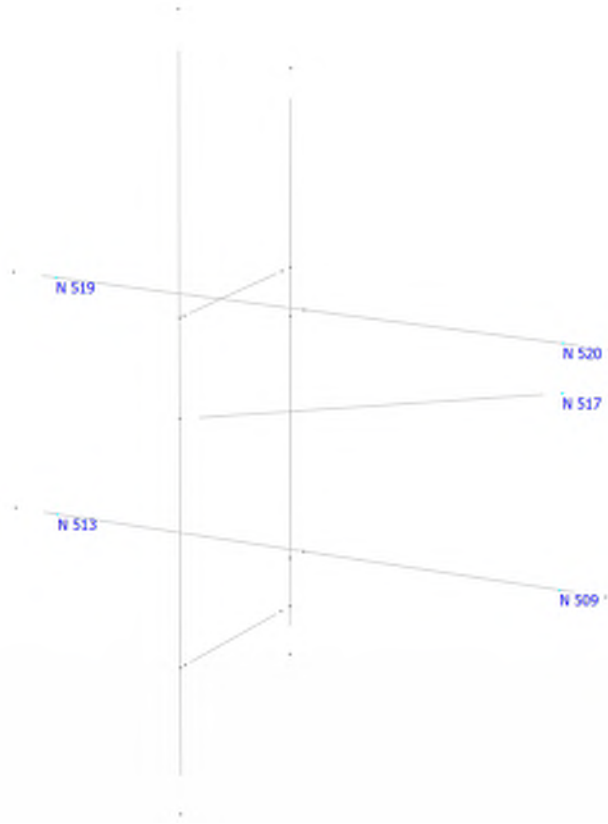
Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
268	487	485		PIPE 4x0.237	A53 GrB	0.00	0.00	0.00
269	507	505		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
270	473	471		HSS_SQR 2-1_2X2-1_2X...	A500 GrB rectangular	0.00	0.00	0.00
272	477	479		HSS_SQR 2-1_2X2-1_2X...	A500 GrB rectangular	0.00	0.00	0.00
276	499	495		HSS_SQR 4X4X3_16	A500 GrB rectangular	0.00	0.00	0.00
277	497	493		HSS_SQR 4X4X3_16	A500 GrB rectangular	0.00	0.00	0.00
292	518	517		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

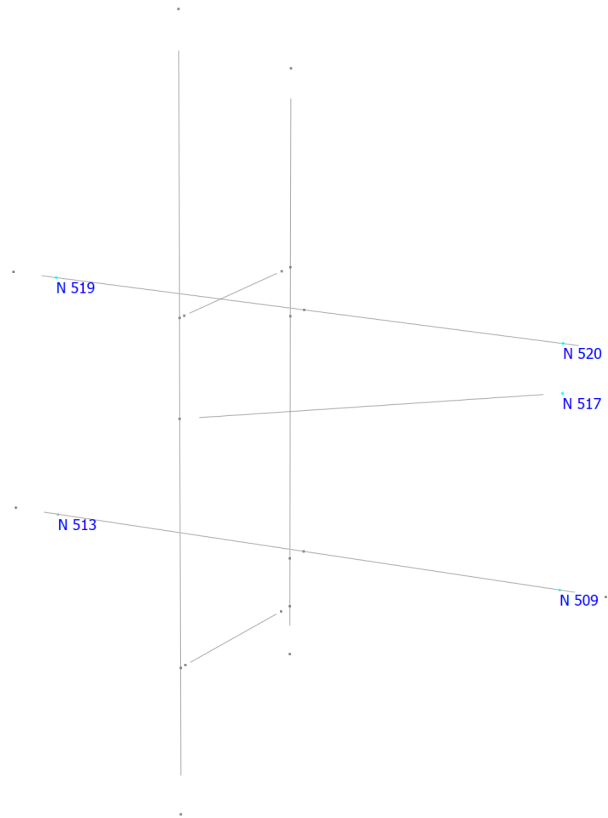
Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
269	315.00	0	0.00	0.00	0.00

Hinges

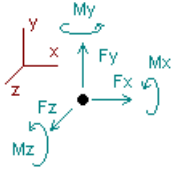
Member	Node-J				Node-K				TOR	AXL	Axial rigidity
	M33	M22	V3	V2	M33	M22	V3	V2			
292	1	1	0	0	0	0	0	0	0	0	Full





Analysis result

Reactions



Direction of positive forces and moments

Node	Forces [Kip]			Moments [Kip*ft]		
	FX	FY	FZ	MX	MY	MZ
Condition LC1=1.2D+Wo						
519	0.04014	0.08927	0.24964	0.00000	0.00000	0.00000
513	0.01085	0.08711	0.21884	0.00000	0.00000	0.00000
520	0.04014	0.08866	0.20018	0.00000	0.00000	0.00000
517	-0.10198	0.00773	0.10526	0.00000	0.00000	0.00000
509	0.01085	0.08671	0.17492	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	0.94883	0.00000	0.00000	0.00000
Condition LC2=1.2D+W30						
519	0.08186	0.09468	0.28193	0.00000	0.00000	0.00000
513	0.02200	0.08232	0.24481	0.00000	0.00000	0.00000
520	0.08186	0.08355	0.18348	0.00000	0.00000	0.00000
517	0.21372	0.00791	-0.18097	0.00000	0.00000	0.00000
509	0.02200	0.09102	0.15302	0.00000	0.00000	0.00000
SUM	0.42144	0.35947	0.68227	0.00000	0.00000	0.00000
Condition LC3=1.2D+W60						
519	0.10000	0.09361	0.16789	0.00000	0.00000	0.00000
513	0.03843	0.08317	0.18353	0.00000	0.00000	0.00000
520	0.10000	0.08405	0.09250	0.00000	0.00000	0.00000
517	0.25177	0.00806	-0.21798	0.00000	0.00000	0.00000
509	0.03843	0.09058	0.11348	0.00000	0.00000	0.00000
SUM	0.52862	0.35947	0.33941	0.00000	0.00000	0.00000
Condition LC4=1.2D+W90						
519	0.08604	0.09345	0.05331	0.00000	0.00000	0.00000
513	0.03467	0.08296	0.14951	0.00000	0.00000	0.00000
520	0.08604	0.08327	-0.00466	0.00000	0.00000	0.00000
517	0.33377	0.00848	-0.29278	0.00000	0.00000	0.00000
509	0.03467	0.09131	0.09463	0.00000	0.00000	0.00000
SUM	0.57520	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC5=1.2D+W120						
519	0.06054	0.09225	-0.09083	0.00000	0.00000	0.00000
513	0.02783	0.08361	0.10289	0.00000	0.00000	0.00000
520	0.06054	0.08329	-0.11774	0.00000	0.00000	0.00000
517	0.35188	0.00891	-0.30979	0.00000	0.00000	0.00000
509	0.02783	0.09141	0.07605	0.00000	0.00000	0.00000
SUM	0.52862	0.35947	-0.33941	0.00000	0.00000	0.00000

Condition LC6=1.2D+W150						
519	0.01343	0.09276	-0.19350	0.00000	0.00000	0.00000
513	0.00362	0.08260	0.04852	0.00000	0.00000	0.00000
520	0.01343	0.08209	-0.20748	0.00000	0.00000	0.00000
517	0.43823	0.00949	-0.41216	0.00000	0.00000	0.00000
509	0.00362	0.09252	0.03144	0.00000	0.00000	0.00000

SUM	0.47235	0.35947	-0.73318	0.00000	0.00000	0.00000
Condition LC7=1.2D-W0						
519	-0.06162	0.08635	-0.42629	0.00000	0.00000	0.00000
513	-0.01650	0.08831	-0.04108	0.00000	0.00000	0.00000
520	-0.06162	0.08728	-0.35098	0.00000	0.00000	0.00000
517	0.15625	0.00862	-0.15561	0.00000	0.00000	0.00000
509	-0.01650	0.08891	0.02512	0.00000	0.00000	0.00000

SUM	0.00000	0.35947	-0.94883	0.00000	0.00000	0.00000
Condition LC8=1.2D-W30						
519	-0.10419	0.08130	-0.45995	0.00000	0.00000	0.00000
513	-0.02796	0.09347	-0.06640	0.00000	0.00000	0.00000
520	-0.10419	0.09277	-0.33490	0.00000	0.00000	0.00000
517	-0.15714	0.00694	0.13105	0.00000	0.00000	0.00000
509	-0.02796	0.08498	0.04792	0.00000	0.00000	0.00000

SUM	-0.42144	0.35947	-0.68227	0.00000	0.00000	0.00000
Condition LC9=1.2D-W60						
519	-0.12192	0.08234	-0.34665	0.00000	0.00000	0.00000
513	-0.04431	0.09260	-0.00477	0.00000	0.00000	0.00000
520	-0.12192	0.09222	-0.24465	0.00000	0.00000	0.00000
517	-0.19616	0.00691	0.16867	0.00000	0.00000	0.00000
509	-0.04431	0.08539	0.08799	0.00000	0.00000	0.00000

SUM	-0.52862	0.35947	-0.33941	0.00000	0.00000	0.00000
Condition LC10=1.2D-W90						
519	-0.10753	0.08243	-0.23290	0.00000	0.00000	0.00000
513	-0.04045	0.09274	0.02976	0.00000	0.00000	0.00000
520	-0.10753	0.09292	-0.14865	0.00000	0.00000	0.00000
517	-0.27925	0.00678	0.24428	0.00000	0.00000	0.00000
509	-0.04045	0.08460	0.10751	0.00000	0.00000	0.00000

SUM	-0.57520	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC11=1.2D-W120						
519	-0.08158	0.08346	-0.08842	0.00000	0.00000	0.00000
513	-0.03345	0.09192	0.07623	0.00000	0.00000	0.00000
520	-0.08158	0.09273	-0.03573	0.00000	0.00000	0.00000
517	-0.29855	0.00704	0.26143	0.00000	0.00000	0.00000
509	-0.03345	0.08433	0.12590	0.00000	0.00000	0.00000

SUM	-0.52862	0.35947	0.33941	0.00000	0.00000	0.00000
Condition LC12=1.2D-W150						
519	-0.03435	0.08281	0.01489	0.00000	0.00000	0.00000
513	-0.00917	0.09278	0.13033	0.00000	0.00000	0.00000
520	-0.03435	0.09378	0.05446	0.00000	0.00000	0.00000
517	-0.38532	0.00701	0.36342	0.00000	0.00000	0.00000
509	-0.00917	0.08308	0.17009	0.00000	0.00000	0.00000

SUM	-0.47235	0.35947	0.73318	0.00000	0.00000	0.00000

Condition LC13=0.9D+Wo						
519	0.04278	0.06728	0.27223	0.00000	0.00000	0.00000
513	0.01157	0.06514	0.19628	0.00000	0.00000	0.00000
520	0.04278	0.06661	0.21953	0.00000	0.00000	0.00000
517	-0.10869	0.00586	0.11133	0.00000	0.00000	0.00000
509	0.01157	0.06471	0.14947	0.00000	0.00000	0.00000
SUM	0.00000	0.26960	0.94883	0.00000	0.00000	0.00000
Condition LC14=0.9D+W30						
519	0.08442	0.07276	0.30439	0.00000	0.00000	0.00000
513	0.02277	0.06041	0.22233	0.00000	0.00000	0.00000
520	0.08442	0.06156	0.20276	0.00000	0.00000	0.00000
517	0.20705	0.00580	-0.17488	0.00000	0.00000	0.00000
509	0.02277	0.06907	0.12766	0.00000	0.00000	0.00000
SUM	0.42144	0.26960	0.68227	0.00000	0.00000	0.00000
Condition LC15=0.9D+W60						
519	0.10257	0.07170	0.19033	0.00000	0.00000	0.00000
513	0.03918	0.06127	0.16108	0.00000	0.00000	0.00000
520	0.10257	0.06207	0.11175	0.00000	0.00000	0.00000
517	0.24511	0.00594	-0.21188	0.00000	0.00000	0.00000
509	0.03918	0.06863	0.08814	0.00000	0.00000	0.00000
SUM	0.52862	0.26960	0.33941	0.00000	0.00000	0.00000
Condition LC16=0.9D+W90						
519	0.08861	0.07155	0.07566	0.00000	0.00000	0.00000
513	0.03543	0.06107	0.12712	0.00000	0.00000	0.00000
520	0.08861	0.06130	0.01452	0.00000	0.00000	0.00000
517	0.32712	0.00629	-0.28668	0.00000	0.00000	0.00000
509	0.03543	0.06938	0.06938	0.00000	0.00000	0.00000
SUM	0.57521	0.26960	0.00000	0.00000	0.00000	0.00000
Condition LC17=0.9D+W120						
519	0.06311	0.07035	-0.06855	0.00000	0.00000	0.00000
513	0.02858	0.06173	0.08057	0.00000	0.00000	0.00000
520	0.06311	0.06133	-0.09863	0.00000	0.00000	0.00000
517	0.34523	0.00670	-0.30367	0.00000	0.00000	0.00000
509	0.02858	0.06950	0.05087	0.00000	0.00000	0.00000
SUM	0.52862	0.26960	-0.33941	0.00000	0.00000	0.00000
Condition LC18=0.9D+W150						
519	0.01598	0.07087	-0.17126	0.00000	0.00000	0.00000
513	0.00439	0.06074	0.02623	0.00000	0.00000	0.00000
520	0.01598	0.06016	-0.18842	0.00000	0.00000	0.00000
517	0.43160	0.00720	-0.40604	0.00000	0.00000	0.00000
509	0.00439	0.07062	0.00631	0.00000	0.00000	0.00000
SUM	0.47235	0.26960	-0.73318	0.00000	0.00000	0.00000
Condition LC19=0.9D-Wo						
519	-0.05899	0.06440	-0.40403	0.00000	0.00000	0.00000
513	-0.01580	0.06639	-0.06337	0.00000	0.00000	0.00000
520	-0.05899	0.06531	-0.33195	0.00000	0.00000	0.00000
517	0.14958	0.00653	-0.14948	0.00000	0.00000	0.00000
509	-0.01580	0.06697	0.00000	0.00000	0.00000	0.00000
SUM	0.00000	0.26960	-0.94883	0.00000	0.00000	0.00000

Condition LC20=0.9D-W30						
519	-0.10148	0.05929	-0.43757	0.00000	0.00000	0.00000
513	-0.02731	0.07149	-0.08877	0.00000	0.00000	0.00000
520	-0.10148	0.07075	-0.31580	0.00000	0.00000	0.00000
517	-0.16385	0.00509	0.13716	0.00000	0.00000	0.00000
509	-0.02731	0.06299	0.02271	0.00000	0.00000	0.00000
SUM	-0.42144	0.26960	-0.68227	0.00000	0.00000	0.00000
Condition LC21=0.9D-W60						
519	-0.11923	0.06032	-0.32425	0.00000	0.00000	0.00000
513	-0.04364	0.07062	-0.02716	0.00000	0.00000	0.00000
520	-0.11923	0.07020	-0.22554	0.00000	0.00000	0.00000
517	-0.20288	0.00507	0.17477	0.00000	0.00000	0.00000
509	-0.04364	0.06340	0.06277	0.00000	0.00000	0.00000
SUM	-0.52862	0.26960	-0.33941	0.00000	0.00000	0.00000
Condition LC22=0.9D-W90						
519	-0.10483	0.06039	-0.21041	0.00000	0.00000	0.00000
513	-0.03978	0.07074	0.00729	0.00000	0.00000	0.00000
520	-0.10483	0.07088	-0.12945	0.00000	0.00000	0.00000
517	-0.28598	0.00501	0.25037	0.00000	0.00000	0.00000
509	-0.03978	0.06258	0.08220	0.00000	0.00000	0.00000
SUM	-0.57520	0.26960	0.00000	0.00000	0.00000	0.00000
Condition LC23=0.9D-W120						
519	-0.07889	0.06142	-0.06585	0.00000	0.00000	0.00000
513	-0.03278	0.06991	0.05370	0.00000	0.00000	0.00000
520	-0.07889	0.07068	-0.01646	0.00000	0.00000	0.00000
517	-0.30528	0.00530	0.26751	0.00000	0.00000	0.00000
509	-0.03278	0.06230	0.10051	0.00000	0.00000	0.00000
SUM	-0.52862	0.26960	0.33941	0.00000	0.00000	0.00000
Condition LC24=0.9D-W150						
519	-0.03163	0.06076	0.03750	0.00000	0.00000	0.00000
513	-0.00852	0.07075	0.10777	0.00000	0.00000	0.00000
520	-0.03163	0.07170	0.07378	0.00000	0.00000	0.00000
517	-0.39206	0.00534	0.36948	0.00000	0.00000	0.00000
509	-0.00852	0.06104	0.14465	0.00000	0.00000	0.00000
SUM	-0.47235	0.26960	0.73318	0.00000	0.00000	0.00000
Condition LC25=1.2D+Di+W10						
519	-0.02084	0.19073	-0.19160	0.00000	0.00000	0.00000
513	-0.00562	0.19015	0.25457	0.00000	0.00000	0.00000
520	-0.02084	0.19100	-0.16593	0.00000	0.00000	0.00000
517	0.05292	0.01773	-0.04824	0.00000	0.00000	0.00000
509	-0.00562	0.19034	0.27720	0.00000	0.00000	0.00000
SUM	0.00000	0.77996	0.12600	0.00000	0.00000	0.00000
Condition LC26=1.2D+Di+W130						
519	-0.01290	0.19163	-0.18503	0.00000	0.00000	0.00000
513	-0.00362	0.18917	0.25934	0.00000	0.00000	0.00000
520	-0.01290	0.18997	-0.16859	0.00000	0.00000	0.00000
517	0.11083	0.01815	-0.10100	0.00000	0.00000	0.00000
509	-0.00362	0.19104	0.27306	0.00000	0.00000	0.00000
SUM	0.07778	0.77996	0.07778	0.00000	0.00000	0.00000

Condition LC27=1.2D+Di+W160						
519	-0.01703	0.19132	-0.19989	0.00000	0.00000	0.00000
513	-0.00469	0.18946	0.25394	0.00000	0.00000	0.00000
520	-0.01703	0.19021	-0.17853	0.00000	0.00000	0.00000
517	0.10001	0.01808	-0.09116	0.00000	0.00000	0.00000
509	-0.00469	0.19089	0.27221	0.00000	0.00000	0.00000
SUM	0.05657	0.77996	0.05657	0.00000	0.00000	0.00000
Condition LC28=1.2D+Di+W190						
519	-0.01923	0.19130	-0.21902	0.00000	0.00000	0.00000
513	-0.00530	0.18939	0.24819	0.00000	0.00000	0.00000
520	-0.01923	0.19005	-0.19491	0.00000	0.00000	0.00000
517	0.11306	0.01819	-0.10308	0.00000	0.00000	0.00000
509	-0.00530	0.19101	0.26881	0.00000	0.00000	0.00000
SUM	0.06400	0.77996	0.00000	0.00000	0.00000	0.00000
Condition LC29=1.2D+Di+W1120						
519	-0.02349	0.19110	-0.24289	0.00000	0.00000	0.00000
513	-0.00643	0.18952	0.24042	0.00000	0.00000	0.00000
520	-0.02349	0.19008	-0.21361	0.00000	0.00000	0.00000
517	0.11639	0.01824	-0.10614	0.00000	0.00000	0.00000
509	-0.00643	0.19101	0.26566	0.00000	0.00000	0.00000
SUM	0.05657	0.77996	-0.05657	0.00000	0.00000	0.00000
Condition LC30=1.2D+Di+W1150						
519	-0.02178	0.19133	-0.24416	0.00000	0.00000	0.00000
513	-0.00600	0.18926	0.24076	0.00000	0.00000	0.00000
520	-0.02178	0.18978	-0.21683	0.00000	0.00000	0.00000
517	0.13334	0.01838	-0.12160	0.00000	0.00000	0.00000
509	-0.00600	0.19121	0.26406	0.00000	0.00000	0.00000
SUM	0.07778	0.77996	-0.07778	0.00000	0.00000	0.00000
Condition LC31=1.2D+Di-W10						
519	-0.03525	0.19025	-0.28736	0.00000	0.00000	0.00000
513	-0.00949	0.19030	0.22444	0.00000	0.00000	0.00000
520	-0.03525	0.19071	-0.24403	0.00000	0.00000	0.00000
517	0.08948	0.01806	-0.08165	0.00000	0.00000	0.00000
509	-0.00949	0.19063	0.26260	0.00000	0.00000	0.00000
SUM	0.00000	0.77996	-0.12600	0.00000	0.00000	0.00000
Condition LC32=1.2D+Di-W130						
519	-0.04322	0.18936	-0.29396	0.00000	0.00000	0.00000
513	-0.01150	0.19130	0.21968	0.00000	0.00000	0.00000
520	-0.04322	0.19176	-0.24138	0.00000	0.00000	0.00000
517	0.03165	0.01760	-0.02888	0.00000	0.00000	0.00000
509	-0.01150	0.18994	0.26676	0.00000	0.00000	0.00000
SUM	-0.07778	0.77996	-0.07778	0.00000	0.00000	0.00000
Condition LC33=1.2D+Di-W160						
519	-0.03908	0.18966	-0.27911	0.00000	0.00000	0.00000
513	-0.01042	0.19100	0.22510	0.00000	0.00000	0.00000
520	-0.03908	0.19151	-0.23147	0.00000	0.00000	0.00000
517	0.04242	0.01768	-0.03871	0.00000	0.00000	0.00000
509	-0.01042	0.19009	0.26763	0.00000	0.00000	0.00000
SUM	-0.05657	0.77996	-0.05657	0.00000	0.00000	0.00000

Condition LC34=1.2D+Di-WI90						
519	-0.03686	0.18968	-0.26001	0.00000	0.00000	0.00000
513	-0.00981	0.19107	0.23086	0.00000	0.00000	0.00000
520	-0.03686	0.19167	-0.21513	0.00000	0.00000	0.00000
517	0.02934	0.01758	-0.02677	0.00000	0.00000	0.00000
509	-0.00981	0.18996	0.27105	0.00000	0.00000	0.00000

SUM	-0.06400	0.77996	0.00000	0.00000	0.00000	0.00000

Condition LC35=1.2D+Di-WI120						
519	-0.03260	0.18988	-0.23613	0.00000	0.00000	0.00000
513	-0.00868	0.19093	0.23862	0.00000	0.00000	0.00000
520	-0.03260	0.19164	-0.19642	0.00000	0.00000	0.00000
517	0.02598	0.01754	-0.02370	0.00000	0.00000	0.00000
509	-0.00868	0.18996	0.27419	0.00000	0.00000	0.00000

SUM	-0.05657	0.77996	0.05657	0.00000	0.00000	0.00000

Condition LC36=1.2D+Di-WI150						
519	-0.03430	0.18965	-0.23486	0.00000	0.00000	0.00000
513	-0.00910	0.19120	0.23829	0.00000	0.00000	0.00000
520	-0.03430	0.19193	-0.19320	0.00000	0.00000	0.00000
517	0.00903	0.01742	-0.00823	0.00000	0.00000	0.00000
509	-0.00910	0.18976	0.27579	0.00000	0.00000	0.00000

SUM	-0.07778	0.77996	0.07778	0.00000	0.00000	0.00000

Condition LC37=1.2D+1.6LL1						
519	-0.01054	0.08788	-0.08965	0.00000	0.00000	0.00000
513	-0.00284	0.08779	0.08965	0.00000	0.00000	0.00000
520	-0.01054	0.08804	-0.07671	0.00000	0.00000	0.00000
517	0.02675	0.00785	-0.02436	0.00000	0.00000	0.00000
509	-0.00284	0.08790	0.10108	0.00000	0.00000	0.00000

SUM	0.00000	0.35947	0.00000	0.00000	0.00000	0.00000

Condition LC38=1.2D+1.6LL2						
519	-0.01054	0.08788	-0.08965	0.00000	0.00000	0.00000
513	-0.00284	0.08779	0.08965	0.00000	0.00000	0.00000
520	-0.01054	0.08804	-0.07671	0.00000	0.00000	0.00000
517	0.02675	0.00785	-0.02436	0.00000	0.00000	0.00000
509	-0.00284	0.08790	0.10108	0.00000	0.00000	0.00000

SUM	0.00000	0.35947	0.00000	0.00000	0.00000	0.00000

Condition LC39=1.2D+1.6LL3						
519	-0.01054	0.08788	-0.08965	0.00000	0.00000	0.00000
513	-0.00284	0.08779	0.08965	0.00000	0.00000	0.00000
520	-0.01054	0.08804	-0.07671	0.00000	0.00000	0.00000
517	0.02675	0.00785	-0.02436	0.00000	0.00000	0.00000
509	-0.00284	0.08790	0.10108	0.00000	0.00000	0.00000

SUM	0.00000	0.35947	0.00000	0.00000	0.00000	0.00000

Condition LC40=1.2D+WLO+1.6LLa1						
519	-0.05508	0.28750	-0.47395	0.00000	0.00000	0.00000
513	-0.01468	0.28678	0.49396	0.00000	0.00000	0.00000
520	-0.05508	0.28811	-0.40604	0.00000	0.00000	0.00000
517	0.13953	0.00983	-0.12752	0.00000	0.00000	0.00000
509	-0.01468	0.28725	0.55354	0.00000	0.00000	0.00000

SUM	0.00000	1.15947	0.04000	0.00000	0.00000	0.00000

Condition LC41=1.2D+WL30+1.6LLa1						
519	-0.05245	0.28776	-0.47123	0.00000	0.00000	0.00000
513	-0.01395	0.28642	0.49560	0.00000	0.00000	0.00000
520	-0.05245	0.28774	-0.40645	0.00000	0.00000	0.00000
517	0.15826	0.01011	-0.14463	0.00000	0.00000	0.00000
509	-0.01395	0.28745	0.55216	0.00000	0.00000	0.00000
SUM	0.02546	1.15947	0.02546	0.00000	0.00000	0.00000
Condition LC42=1.2D+WL60+1.6LLa1						
519	-0.05409	0.28764	-0.47714	0.00000	0.00000	0.00000
513	-0.01440	0.28654	0.49340	0.00000	0.00000	0.00000
520	-0.05409	0.28784	-0.41039	0.00000	0.00000	0.00000
517	0.15394	0.01005	-0.14069	0.00000	0.00000	0.00000
509	-0.01440	0.28739	0.55179	0.00000	0.00000	0.00000
SUM	0.01697	1.15947	0.01697	0.00000	0.00000	0.00000
Condition LC43=1.2D+WL90+1.6LLa1						
519	-0.05465	0.28764	-0.48254	0.00000	0.00000	0.00000
513	-0.01454	0.28650	0.49171	0.00000	0.00000	0.00000
520	-0.05465	0.28778	-0.41509	0.00000	0.00000	0.00000
517	0.15837	0.01012	-0.14475	0.00000	0.00000	0.00000
509	-0.01454	0.28743	0.55066	0.00000	0.00000	0.00000
SUM	0.02000	1.15947	0.00000	0.00000	0.00000	0.00000
Condition LC44=1.2D+WL120+1.6LLa1						
519	-0.05603	0.28757	-0.48988	0.00000	0.00000	0.00000
513	-0.01491	0.28655	0.48920	0.00000	0.00000	0.00000
520	-0.05603	0.28779	-0.42076	0.00000	0.00000	0.00000
517	0.15884	0.01014	-0.14519	0.00000	0.00000	0.00000
509	-0.01491	0.28742	0.54965	0.00000	0.00000	0.00000
SUM	0.01697	1.15947	-0.01697	0.00000	0.00000	0.00000
Condition LC45=1.2D+WL150+1.6LLa1						
519	-0.05536	0.28765	-0.49034	0.00000	0.00000	0.00000
513	-0.01472	0.28643	0.48930	0.00000	0.00000	0.00000
520	-0.05536	0.28766	-0.42200	0.00000	0.00000	0.00000
517	0.16561	0.01024	-0.15137	0.00000	0.00000	0.00000
509	-0.01472	0.28748	0.54896	0.00000	0.00000	0.00000
SUM	0.02546	1.15947	-0.02546	0.00000	0.00000	0.00000
Condition LC46=1.2D-WL0+1.6LLa1						
519	-0.05965	0.28733	-0.50397	0.00000	0.00000	0.00000
513	-0.01589	0.28680	0.48406	0.00000	0.00000	0.00000
520	-0.05965	0.28799	-0.43048	0.00000	0.00000	0.00000
517	0.15109	0.01004	-0.13812	0.00000	0.00000	0.00000
509	-0.01589	0.28731	0.54851	0.00000	0.00000	0.00000
SUM	0.00000	1.15947	-0.04000	0.00000	0.00000	0.00000
Condition LC47=1.2D-WL30+1.6LLa1						
519	-0.06228	0.28707	-0.50669	0.00000	0.00000	0.00000
513	-0.01663	0.28716	0.48242	0.00000	0.00000	0.00000
520	-0.06228	0.28836	-0.43007	0.00000	0.00000	0.00000
517	0.13236	0.00976	-0.12102	0.00000	0.00000	0.00000
509	-0.01663	0.28712	0.54990	0.00000	0.00000	0.00000
SUM	-0.02546	1.15947	-0.02546	0.00000	0.00000	0.00000

Condition LC48=1.2D-WL60+1.6LLa1						
519	-0.06064	0.28719	-0.50078	0.00000	0.00000	0.00000
513	-0.01618	0.28703	0.48462	0.00000	0.00000	0.00000
520	-0.06064	0.28825	-0.42613	0.00000	0.00000	0.00000
517	0.13668	0.00982	-0.12495	0.00000	0.00000	0.00000
509	-0.01618	0.28718	0.55028	0.00000	0.00000	0.00000

SUM	-0.01697	1.15947	-0.01697	0.00000	0.00000	0.00000

Condition LC49=1.2D-WL90+1.6LLa1						
519	-0.06008	0.28719	-0.49539	0.00000	0.00000	0.00000
513	-0.01604	0.28707	0.48631	0.00000	0.00000	0.00000
520	-0.06008	0.28832	-0.42143	0.00000	0.00000	0.00000
517	0.13225	0.00974	-0.12089	0.00000	0.00000	0.00000
509	-0.01604	0.28714	0.55140	0.00000	0.00000	0.00000

SUM	-0.02000	1.15947	0.00000	0.00000	0.00000	0.00000

Condition LC50=1.2D-WL120+1.6LLa1						
519	-0.05870	0.28726	-0.48805	0.00000	0.00000	0.00000
513	-0.01567	0.28703	0.48882	0.00000	0.00000	0.00000
520	-0.05870	0.28831	-0.41577	0.00000	0.00000	0.00000
517	0.13177	0.00973	-0.12045	0.00000	0.00000	0.00000
509	-0.01567	0.28715	0.55241	0.00000	0.00000	0.00000

SUM	-0.01697	1.15947	0.01697	0.00000	0.00000	0.00000

Condition LC51=1.2D-WL150+1.6LLa1						
519	-0.05937	0.28718	-0.48759	0.00000	0.00000	0.00000
513	-0.01586	0.28714	0.48873	0.00000	0.00000	0.00000
520	-0.05937	0.28843	-0.41452	0.00000	0.00000	0.00000
517	0.12501	0.00963	-0.11426	0.00000	0.00000	0.00000
509	-0.01586	0.28708	0.55310	0.00000	0.00000	0.00000

SUM	-0.02546	1.15947	0.02546	0.00000	0.00000	0.00000

Condition LC52=1.2D+WL0						
519	-0.00825	0.08795	-0.07439	0.00000	0.00000	0.00000
513	-0.00222	0.08776	0.09439	0.00000	0.00000	0.00000
520	-0.00825	0.08808	-0.06426	0.00000	0.00000	0.00000
517	0.02095	0.00783	-0.01907	0.00000	0.00000	0.00000
509	-0.00222	0.08784	0.10334	0.00000	0.00000	0.00000

SUM	0.00000	0.35947	0.04000	0.00000	0.00000	0.00000

Condition LC53=1.2D+WL30						
519	-0.00562	0.08827	-0.07181	0.00000	0.00000	0.00000
513	-0.00152	0.08746	0.09612	0.00000	0.00000	0.00000
520	-0.00562	0.08776	-0.06477	0.00000	0.00000	0.00000
517	0.03972	0.00789	-0.03617	0.00000	0.00000	0.00000
509	-0.00152	0.08809	0.10208	0.00000	0.00000	0.00000

SUM	0.02546	0.35947	0.02546	0.00000	0.00000	0.00000

Condition LC54=1.2D+WL60						
519	-0.00726	0.08814	-0.07776	0.00000	0.00000	0.00000
513	-0.00196	0.08757	0.09397	0.00000	0.00000	0.00000
520	-0.00726	0.08785	-0.06875	0.00000	0.00000	0.00000
517	0.03540	0.00787	-0.03223	0.00000	0.00000	0.00000
509	-0.00196	0.08803	0.10175	0.00000	0.00000	0.00000

SUM	0.01697	0.35947	0.01697	0.00000	0.00000	0.00000

Condition LC55=1.2D+WL90						
519	-0.00782	0.08815	-0.08326	0.00000	0.00000	0.00000
513	-0.00211	0.08755	0.09237	0.00000	0.00000	0.00000
520	-0.00782	0.08780	-0.07355	0.00000	0.00000	0.00000
517	0.03984	0.00789	-0.03628	0.00000	0.00000	0.00000
509	-0.00211	0.08808	0.10073	0.00000	0.00000	0.00000
SUM	0.02000	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC56=1.2D+WL120						
519	-0.00920	0.08808	-0.09070	0.00000	0.00000	0.00000
513	-0.00248	0.08760	0.08994	0.00000	0.00000	0.00000
520	-0.00920	0.08782	-0.07931	0.00000	0.00000	0.00000
517	0.04032	0.00789	-0.03672	0.00000	0.00000	0.00000
509	-0.00248	0.08807	0.09982	0.00000	0.00000	0.00000
SUM	0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000
Condition LC57=1.2D+WL150						
519	-0.00853	0.08818	-0.09122	0.00000	0.00000	0.00000
513	-0.00230	0.08750	0.09009	0.00000	0.00000	0.00000
520	-0.00853	0.08771	-0.08061	0.00000	0.00000	0.00000
517	0.04711	0.00791	-0.04290	0.00000	0.00000	0.00000
509	-0.00230	0.08816	0.09920	0.00000	0.00000	0.00000
SUM	0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000
Condition LC58=1.2D-WL0						
519	-0.01283	0.08781	-0.10490	0.00000	0.00000	0.00000
513	-0.00345	0.08783	0.08491	0.00000	0.00000	0.00000
520	-0.01283	0.08801	-0.08916	0.00000	0.00000	0.00000
517	0.03256	0.00787	-0.02966	0.00000	0.00000	0.00000
509	-0.00345	0.08795	0.09881	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	-0.04000	0.00000	0.00000	0.00000
Condition LC59=1.2D-WL30						
519	-0.01546	0.08749	-0.10748	0.00000	0.00000	0.00000
513	-0.00416	0.08813	0.08317	0.00000	0.00000	0.00000
520	-0.01546	0.08832	-0.08865	0.00000	0.00000	0.00000
517	0.01379	0.00781	-0.01256	0.00000	0.00000	0.00000
509	-0.00416	0.08771	0.10007	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000
Condition LC60=1.2D-WL60						
519	-0.01382	0.08762	-0.10154	0.00000	0.00000	0.00000
513	-0.00372	0.08802	0.08533	0.00000	0.00000	0.00000
520	-0.01382	0.08823	-0.08467	0.00000	0.00000	0.00000
517	0.01811	0.00783	-0.01650	0.00000	0.00000	0.00000
509	-0.00372	0.08777	0.10041	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000
Condition LC61=1.2D-WL90						
519	-0.01326	0.08761	-0.09604	0.00000	0.00000	0.00000
513	-0.00357	0.08804	0.08693	0.00000	0.00000	0.00000
520	-0.01326	0.08828	-0.07987	0.00000	0.00000	0.00000
517	0.01366	0.00781	-0.01244	0.00000	0.00000	0.00000
509	-0.00357	0.08772	0.10142	0.00000	0.00000	0.00000
SUM	-0.02000	0.35947	0.00000	0.00000	0.00000	0.00000

Condition LC62=1.2D-WL120						
519	-0.01188	0.08768	-0.08860	0.00000	0.00000	0.00000
513	-0.00320	0.08799	0.08936	0.00000	0.00000	0.00000
520	-0.01188	0.08826	-0.07411	0.00000	0.00000	0.00000
517	0.01318	0.00781	-0.01200	0.00000	0.00000	0.00000
509	-0.00320	0.08772	0.10233	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	0.01697	0.00000	0.00000	0.00000
Condition LC63=1.2D-WL150						
519	-0.01255	0.08758	-0.08807	0.00000	0.00000	0.00000
513	-0.00337	0.08809	0.08921	0.00000	0.00000	0.00000
520	-0.01255	0.08837	-0.07281	0.00000	0.00000	0.00000
517	0.00639	0.00779	-0.00582	0.00000	0.00000	0.00000
509	-0.00337	0.08764	0.10296	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	0.02546	0.00000	0.00000	0.00000
Condition LC64=1.2D+WL0						
519	-0.00825	0.08795	-0.07439	0.00000	0.00000	0.00000
513	-0.00222	0.08776	0.09439	0.00000	0.00000	0.00000
520	-0.00825	0.08808	-0.06426	0.00000	0.00000	0.00000
517	0.02095	0.00783	-0.01907	0.00000	0.00000	0.00000
509	-0.00222	0.08784	0.10334	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	0.04000	0.00000	0.00000	0.00000
Condition LC65=1.2D+WL30						
519	-0.00562	0.08827	-0.07181	0.00000	0.00000	0.00000
513	-0.00152	0.08746	0.09612	0.00000	0.00000	0.00000
520	-0.00562	0.08776	-0.06477	0.00000	0.00000	0.00000
517	0.03972	0.00789	-0.03617	0.00000	0.00000	0.00000
509	-0.00152	0.08809	0.10208	0.00000	0.00000	0.00000
SUM	0.02546	0.35947	0.02546	0.00000	0.00000	0.00000
Condition LC66=1.2D+WL60						
519	-0.00726	0.08814	-0.07776	0.00000	0.00000	0.00000
513	-0.00196	0.08757	0.09397	0.00000	0.00000	0.00000
520	-0.00726	0.08785	-0.06875	0.00000	0.00000	0.00000
517	0.03540	0.00787	-0.03223	0.00000	0.00000	0.00000
509	-0.00196	0.08803	0.10175	0.00000	0.00000	0.00000
SUM	0.01697	0.35947	0.01697	0.00000	0.00000	0.00000
Condition LC67=1.2D+WL90						
519	-0.00782	0.08815	-0.08326	0.00000	0.00000	0.00000
513	-0.00211	0.08755	0.09237	0.00000	0.00000	0.00000
520	-0.00782	0.08780	-0.07355	0.00000	0.00000	0.00000
517	0.03984	0.00789	-0.03628	0.00000	0.00000	0.00000
509	-0.00211	0.08808	0.10073	0.00000	0.00000	0.00000
SUM	0.02000	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC68=1.2D+WL120						
519	-0.00920	0.08808	-0.09070	0.00000	0.00000	0.00000
513	-0.00248	0.08760	0.08994	0.00000	0.00000	0.00000
520	-0.00920	0.08782	-0.07931	0.00000	0.00000	0.00000
517	0.04032	0.00789	-0.03672	0.00000	0.00000	0.00000
509	-0.00248	0.08807	0.09982	0.00000	0.00000	0.00000
SUM	0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000

Condition LC69=1.2D-WL150

519	-0.00853	0.08818	-0.09122	0.00000	0.00000	0.00000
513	-0.00230	0.08750	0.09009	0.00000	0.00000	0.00000
520	-0.00853	0.08771	-0.08061	0.00000	0.00000	0.00000
517	0.04711	0.00791	-0.04290	0.00000	0.00000	0.00000
509	-0.00230	0.08816	0.09920	0.00000	0.00000	0.00000
SUM	0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000

Condition LC70=1.2D-WL0

519	-0.01283	0.08781	-0.10490	0.00000	0.00000	0.00000
513	-0.00345	0.08783	0.08491	0.00000	0.00000	0.00000
520	-0.01283	0.08801	-0.08916	0.00000	0.00000	0.00000
517	0.03256	0.00787	-0.02966	0.00000	0.00000	0.00000
509	-0.00345	0.08795	0.09881	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	-0.04000	0.00000	0.00000	0.00000

Condition LC71=1.2D-WL30

519	-0.01546	0.08749	-0.10748	0.00000	0.00000	0.00000
513	-0.00416	0.08813	0.08317	0.00000	0.00000	0.00000
520	-0.01546	0.08832	-0.08865	0.00000	0.00000	0.00000
517	0.01379	0.00781	-0.01256	0.00000	0.00000	0.00000
509	-0.00416	0.08771	0.10007	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000

Condition LC72=1.2D-WL60

519	-0.01382	0.08762	-0.10154	0.00000	0.00000	0.00000
513	-0.00372	0.08802	0.08533	0.00000	0.00000	0.00000
520	-0.01382	0.08823	-0.08467	0.00000	0.00000	0.00000
517	0.01811	0.00783	-0.01650	0.00000	0.00000	0.00000
509	-0.00372	0.08777	0.10041	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000

Condition LC73=1.2D-WL90

519	-0.01326	0.08761	-0.09604	0.00000	0.00000	0.00000
513	-0.00357	0.08804	0.08693	0.00000	0.00000	0.00000
520	-0.01326	0.08828	-0.07987	0.00000	0.00000	0.00000
517	0.01366	0.00781	-0.01244	0.00000	0.00000	0.00000
509	-0.00357	0.08772	0.10142	0.00000	0.00000	0.00000
SUM	-0.02000	0.35947	0.00000	0.00000	0.00000	0.00000

Condition LC74=1.2D-WL120

519	-0.01188	0.08768	-0.08860	0.00000	0.00000	0.00000
513	-0.00320	0.08799	0.08936	0.00000	0.00000	0.00000
520	-0.01188	0.08826	-0.07411	0.00000	0.00000	0.00000
517	0.01318	0.00781	-0.01200	0.00000	0.00000	0.00000
509	-0.00320	0.08772	0.10233	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	0.01697	0.00000	0.00000	0.00000

Condition LC75=1.2D-WL150

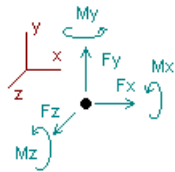
519	-0.01255	0.08758	-0.08807	0.00000	0.00000	0.00000
513	-0.00337	0.08809	0.08921	0.00000	0.00000	0.00000
520	-0.01255	0.08837	-0.07281	0.00000	0.00000	0.00000
517	0.00639	0.00779	-0.00582	0.00000	0.00000	0.00000
509	-0.00337	0.08764	0.10296	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	0.02546	0.00000	0.00000	0.00000

Condition LC76=1.2D+WL0						
519	-0.00825	0.08795	-0.07439	0.00000	0.00000	0.00000
513	-0.00222	0.08776	0.09439	0.00000	0.00000	0.00000
520	-0.00825	0.08808	-0.06426	0.00000	0.00000	0.00000
517	0.02095	0.00783	-0.01907	0.00000	0.00000	0.00000
509	-0.00222	0.08784	0.10334	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	0.04000	0.00000	0.00000	0.00000
Condition LC77=1.2D+WL30						
519	-0.00562	0.08827	-0.07181	0.00000	0.00000	0.00000
513	-0.00152	0.08746	0.09612	0.00000	0.00000	0.00000
520	-0.00562	0.08776	-0.06477	0.00000	0.00000	0.00000
517	0.03972	0.00789	-0.03617	0.00000	0.00000	0.00000
509	-0.00152	0.08809	0.10208	0.00000	0.00000	0.00000
SUM	0.02546	0.35947	0.02546	0.00000	0.00000	0.00000
Condition LC78=1.2D+WL60						
519	-0.00726	0.08814	-0.07776	0.00000	0.00000	0.00000
513	-0.00196	0.08757	0.09397	0.00000	0.00000	0.00000
520	-0.00726	0.08785	-0.06875	0.00000	0.00000	0.00000
517	0.03540	0.00787	-0.03223	0.00000	0.00000	0.00000
509	-0.00196	0.08803	0.10175	0.00000	0.00000	0.00000
SUM	0.01697	0.35947	0.01697	0.00000	0.00000	0.00000
Condition LC79=1.2D+WL90						
519	-0.00782	0.08815	-0.08326	0.00000	0.00000	0.00000
513	-0.00211	0.08755	0.09237	0.00000	0.00000	0.00000
520	-0.00782	0.08780	-0.07355	0.00000	0.00000	0.00000
517	0.03984	0.00789	-0.03628	0.00000	0.00000	0.00000
509	-0.00211	0.08808	0.10073	0.00000	0.00000	0.00000
SUM	0.02000	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC80=1.2D+WL120						
519	-0.00920	0.08808	-0.09070	0.00000	0.00000	0.00000
513	-0.00248	0.08760	0.08994	0.00000	0.00000	0.00000
520	-0.00920	0.08782	-0.07931	0.00000	0.00000	0.00000
517	0.04032	0.00789	-0.03672	0.00000	0.00000	0.00000
509	-0.00248	0.08807	0.09982	0.00000	0.00000	0.00000
SUM	0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000
Condition LC81=1.2D+WL150						
519	-0.00853	0.08818	-0.09122	0.00000	0.00000	0.00000
513	-0.00230	0.08750	0.09009	0.00000	0.00000	0.00000
520	-0.00853	0.08771	-0.08061	0.00000	0.00000	0.00000
517	0.04711	0.00791	-0.04290	0.00000	0.00000	0.00000
509	-0.00230	0.08816	0.09920	0.00000	0.00000	0.00000
SUM	0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000
Condition LC82=1.2D-WL0						
519	-0.01283	0.08781	-0.10490	0.00000	0.00000	0.00000
513	-0.00345	0.08783	0.08491	0.00000	0.00000	0.00000
520	-0.01283	0.08801	-0.08916	0.00000	0.00000	0.00000
517	0.03256	0.00787	-0.02966	0.00000	0.00000	0.00000
509	-0.00345	0.08795	0.09881	0.00000	0.00000	0.00000
SUM	0.00000	0.35947	-0.04000	0.00000	0.00000	0.00000

Condition LC83=1.2D-WL30						
519	-0.01546	0.08749	-0.10748	0.00000	0.00000	0.00000
513	-0.00416	0.08813	0.08317	0.00000	0.00000	0.00000
520	-0.01546	0.08832	-0.08865	0.00000	0.00000	0.00000
517	0.01379	0.00781	-0.01256	0.00000	0.00000	0.00000
509	-0.00416	0.08771	0.10007	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	-0.02546	0.00000	0.00000	0.00000
Condition LC84=1.2D-WL60						
519	-0.01382	0.08762	-0.10154	0.00000	0.00000	0.00000
513	-0.00372	0.08802	0.08533	0.00000	0.00000	0.00000
520	-0.01382	0.08823	-0.08467	0.00000	0.00000	0.00000
517	0.01811	0.00783	-0.01650	0.00000	0.00000	0.00000
509	-0.00372	0.08777	0.10041	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	-0.01697	0.00000	0.00000	0.00000
Condition LC85=1.2D-WL90						
519	-0.01326	0.08761	-0.09604	0.00000	0.00000	0.00000
513	-0.00357	0.08804	0.08693	0.00000	0.00000	0.00000
520	-0.01326	0.08828	-0.07987	0.00000	0.00000	0.00000
517	0.01366	0.00781	-0.01244	0.00000	0.00000	0.00000
509	-0.00357	0.08772	0.10142	0.00000	0.00000	0.00000
SUM	-0.02000	0.35947	0.00000	0.00000	0.00000	0.00000
Condition LC86=1.2D-WL120						
519	-0.01188	0.08768	-0.08860	0.00000	0.00000	0.00000
513	-0.00320	0.08799	0.08936	0.00000	0.00000	0.00000
520	-0.01188	0.08826	-0.07411	0.00000	0.00000	0.00000
517	0.01318	0.00781	-0.01200	0.00000	0.00000	0.00000
509	-0.00320	0.08772	0.10233	0.00000	0.00000	0.00000
SUM	-0.01697	0.35947	0.01697	0.00000	0.00000	0.00000
Condition LC87=1.2D-WL150						
519	-0.01255	0.08758	-0.08807	0.00000	0.00000	0.00000
513	-0.00337	0.08809	0.08921	0.00000	0.00000	0.00000
520	-0.01255	0.08837	-0.07281	0.00000	0.00000	0.00000
517	0.00639	0.00779	-0.00582	0.00000	0.00000	0.00000
509	-0.00337	0.08764	0.10296	0.00000	0.00000	0.00000
SUM	-0.02546	0.35947	0.02546	0.00000	0.00000	0.00000

Envelope for nodal reactions

Note.- I_c is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

LC1=1.2D+W0
LC2=1.2D+W30
LC3=1.2D+W60
LC4=1.2D+W90
LC5=1.2D+W120
LC6=1.2D+W150
LC7=1.2D-W0
LC8=1.2D-W30
LC9=1.2D-W60
LC10=1.2D-W90
LC11=1.2D-W120
LC12=1.2D-W150
LC13=0.9D+W0
LC14=0.9D+W30
LC15=0.9D+W60
LC16=0.9D+W90
LC17=0.9D+W120
LC18=0.9D+W150
LC19=0.9D-W0
LC20=0.9D-W30
LC21=0.9D-W60
LC22=0.9D-W90
LC23=0.9D-W120
LC24=0.9D-W150
LC25=1.2D+Di+W0
LC26=1.2D+Di+W30
LC27=1.2D+Di+W60
LC28=1.2D+Di+W90
LC29=1.2D+Di+W120
LC30=1.2D+Di+W150
LC31=1.2D+Di-W0
LC32=1.2D+Di-W30
LC33=1.2D+Di-W60
LC34=1.2D+Di-W90
LC35=1.2D+Di-W120
LC36=1.2D+Di-W150
LC37=1.2D+1.6LL1
LC38=1.2D+1.6LL2
LC39=1.2D+1.6LL3
LC40=1.2D+W0+1.6LLa1
LC41=1.2D+W30+1.6LLa1
LC42=1.2D+W60+1.6LLa1
LC43=1.2D+W90+1.6LLa1
LC44=1.2D+W120+1.6LLa1
LC45=1.2D+W150+1.6LLa1
LC46=1.2D-W0+1.6LLa1
LC47=1.2D-W30+1.6LLa1
LC48=1.2D-W60+1.6LLa1
LC49=1.2D-W90+1.6LLa1
LC50=1.2D-W120+1.6LLa1
LC51=1.2D-W150+1.6LLa1
LC52=1.2D+W0
LC53=1.2D+W30
LC54=1.2D+W60
LC55=1.2D+W90
LC56=1.2D+W120
LC57=1.2D+W150
LC58=1.2D-W0
LC59=1.2D-W30
LC60=1.2D-W60
LC61=1.2D-W90
LC62=1.2D-W120
LC63=1.2D-W150
LC64=1.2D+W0
LC65=1.2D+W30
LC66=1.2D+W60
LC67=1.2D+W90
LC68=1.2D+W120
LC69=1.2D+W150

LC70=1.2D-WL0
 LC71=1.2D-WL30
 LC72=1.2D-WL60
 LC73=1.2D-WL90
 LC74=1.2D-WL120
 LC75=1.2D-WL150
 LC76=1.2D+WL0
 LC77=1.2D+WL30
 LC78=1.2D+WL60
 LC79=1.2D+WL90
 LC80=1.2D+WL120
 LC81=1.2D+WL150
 LC82=1.2D-WL0
 LC83=1.2D-WL30
 LC84=1.2D-WL60
 LC85=1.2D-WL90
 LC86=1.2D-WL120
 LC87=1.2D-WL150

Node	Forces						Moments						
	Fx [Kip]	lc	Fy [Kip]	lc	Fz [Kip]	lc	Mx [Kip*ft]	lc	My [Kip*ft]	lc	Mz [Kip*ft]	lc	
519	Max	0.103	LC15	0.288	LC41	0.304	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.122	LC9	0.059	LC20	-0.507	LC47	0.00000	LC1	0.00000	LC1	0.00000	LC1
513	Max	0.039	LC15	0.287	LC47	0.496	LC41	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.044	LC9	0.060	LC14	-0.089	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
520	Max	0.103	LC15	0.288	LC51	0.220	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.122	LC9	0.060	LC18	-0.430	LC46	0.00000	LC1	0.00000	LC1	0.00000	LC1
517	Max	0.438	LC6	0.018	LC30	0.369	LC24	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.392	LC24	0.005	LC22	-0.412	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
509	Max	0.039	LC15	0.287	LC45	0.554	LC40	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.044	LC9	0.061	LC24	0.000	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1



Connection Check

Date: 11/28/2022
Project Name: DANIELSON
Project No.: CT1166
Designed By: JC Checked By: MSC



CHECK CONNECTION CAPACITY (Worst Case)

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A36 1/2" Threaded Rod

Allowable Tensile Load =

$F_{Tall} =$ 4271 lbs.

Allowable Shear Load =

$F_{Vall} =$ 2562 lbs.

TENSILE FORCES

Reaction $F =$ 412 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 438 lbs. (See Bentley Output)

Reactions in Y direction: 18 lbs. (See Bentley Output)

Resultant: 438 lbs.

No. of Supports = 1

No. of Bolts / Support = 2

Tension Design Load /Bolts =

$f_t =$ 206.00 lbs. < 4271 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

$f_v =$ 219.18 lbs. < 2562 lbs. **Therefore, OK !**

CHECK COMBINED TENSION AND SHEAR

f_t / F_T + f_v / F_V \leq 1.0
0.048 + 0.086 = 0.134 < 1.0 **Therefore, OK !**

Attachment 2

Structural Analysis Report
& Reinforcement Design

190-ft Existing ROHN Guyed Lattice Tower

*Proposed AT&T
Antenna Installation*

AT&T Site Ref: CT1166

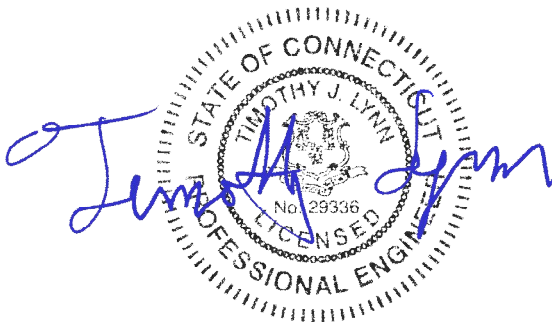
*812 Providence Pike
Danielson, CT*

Centek Project No. 21140.00

~~*Date: December 20, 2021*~~

Rev 8: February 20, 2023

Max Stress Ratio = 71.6%



Prepared for:
AT&T Mobility
500 Enterprise Drive, Suite 3A
Rocky Hill, CT 06067

Table of Contents

SECTION 1 - REPORT

- INTRODUCTION
- ANTENNA AND APPURTENANCE SUMMARY
- PRIMARY ASSUMPTIONS USED IN THE ANALYSIS
- ANALYSIS
- TOWER LOADING
- TOWER CAPACITY
- FOUNDATION AND ANCHORS
- CONCLUSION

SECTION 2 – CONDITIONS & SOFTWARE

- STANDARD ENGINEERING CONDITIONS
- GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

SECTION 3 – CALCULATIONS

- tnxTower INPUT/OUTPUT SUMMARY
- tnxTower DETAILED OUTPUT
- FOUNDATION ANALYSIS

SECTION 4 – TOWER REINFORCEMENT DRAWINGS

- TOWER REINFORCEMENT DRAWINGS

SECTION 5 – REFERENCE MATERIAL

- RFDS

Introduction

The purpose of this report is to summarize the results of the non-linear, P- Δ structural analysis of the antenna installation proposed by AT&T on the existing guyed lattice tower located in Danielson, CT.

The host tower is a 190-ft tall, eleven-section, Rohn model 80 guyed lattice tower. The manufacturer's drawings and calculations were unavailable for use in this report. The tower geometry, structure member sizes and foundation system information were obtained from a previous structural analysis report prepared by Centek; job no; 20074.28 dated May 27, 2020.

Antenna and appurtenance information were obtained from a previous structural analysis report prepared by All-Points Technology; job no; CT141_12710 dated December 1, 2021 and an RF data sheet.

The tower consists of eleven (11) vertical sections constructed of steel pipe legs conforming to ASTM A572-50. Diagonal and horizontal lateral support bracing consists of steel pipe construction conforming to ASTM A53-B-42. The vertical tower sections are connected by bolted flange plates with the diagonal and horizontal bracing to pipe legs consisting of bolted connections. The width of the tower face is 3.42-ft throughout its length with the exception of a 5'-0" high tapered base section.

Antenna and Appurtenance Summary

- VERIZON (Existing):
Antennas: Three (3) Samsung MT6407-77A panel antennas, six (6) Commscope JAHH-65B-R3B panel antennas, three (3) Samsung RF4439d-25A remote radio heads, three (3) Samsung RF4440d-13A remote radio heads, three (3) Commscope CBC78T-Ds-43 diplexers and one (1) main distribution box mounted on three (3) Valmont 13-ft lightweight T-Frames with a RAD center elevation of 187-ft above the existing tower base.
Cables: One (1) 1-5/8" dia. Hybriflex Fiber feeder cables running on the exterior of the existing tower.
- T-MOBILE (Existing):
Antennas: Three (3) RFS APX16DWV-16DWVS panel antennas, three (3) RFS APXVAARR24_43 panel antennas, three (3) Ericsson AIR6449 panel antennas, three (3) Ericsson 4415 remote radio units, three (3) Ericsson 4424 remote radio units and three (3) Ericsson 4449 B71 B12 remote radio units mounted three (3) V-Frames with a RAD center elevation of 140-ft above the existing tower base.
Coax Cables: Four (4) 6x12 fiber cable running on the exterior of the existing tower.
- **AT&T (Proposed):**
Antenna: Three (3) CCI TPA65R-BU8DA antennas face mounted on 2-ft standoffs (SitePro p/n MM02) with a RAD center elevation of \pm 175-ft AGL. Three (3) Ericsson 4478 B14 RRHs and three (3) Ericsson 4415 B25 RRHs mounted 2-ft below antennas on Commscope RR-B2B-AR brackets. Three (3) CCI DMP65R-BU8DA antennas face mounted on 2-ft standoffs (SitePro p/n MM02) with a RAD center elevation of \pm 161-ft AGL. Three (3) Ericsson 4449 B5/B12 RRHs and three (3) Ericsson 4426 B66 RRHs mounted 2-ft below antennas on Commscope RR-B2B-AR brackets. One (1) Raycap DC6-48-60-0-8C-EV surge arrester mounted to the face of the tower on unistrut at 168' and one (1) Raycap DC9-48-60-24-8C-EV surge arrester mounted to the face of the tower on unistrut at 154'

Coax Cable: One (1) fiber cable and four (4) DC cables running on a leg/face of the existing tower as specified in Section 3 of this report.

Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents or reinforcement drawings.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- All coax cables to be installed as indicated in this report.

A n a l y s i s

The existing tower was analyzed using a comprehensive computer program entitled tnxTower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower, and the model assumes that the tower members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for the controlling basic wind speed (3-second gust) with no ice and the applicable wind and ice combination to determine stresses in members as per guidelines of TIA-222-H entitled “Structural Standard for Antenna Support Structures and Antennas”, the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Load and Resistance Factor Design (LRFD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix P of the CSBC¹ and the wind speed data available in the TIA-222-H Standard.

T o w e r L o a d i n g

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA-222-H, gravity loads of the tower structure and its components, and the application of 1.00” radial ice on the tower structure and its components.

Load Cases:	<u>Load Case 1</u> ; 125 mph (Ultimate) wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation.	<i>[Appendix P of the 2022 CT Building Code]</i>
	<u>Load Case 2</u> ; 50 mph wind speed w/ 1.00” radial ice plus gravity load – used in calculation of tower stresses.	<i>[Annex B of TIA-222-H]</i>

¹ The 2021 International Building Code as amended by the 2022 Connecticut State Building Code (CSBC).

Tower Capacity

- Calculated stresses **with the reinforcements detailed in section 4 of this report were found** to be within allowable limits. This tower was found to be at **76.5%** of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Leg (T6)	80.1' - 100.1'	68.9%	PASS
Diagonal (T1)	175.35' - 190.6'	56.2%	PASS
Bottom Girt (T10)	4.58' - 20.1'	63.1%	PASS
Guy B (T4)	139.49'	66.4%	PASS
Torque Arm (T4)	139.49'	71.6%	PASS

Foundations and Anchorage

The existing tower base foundation consists of a 2.0-ft square x 3.75-ft long reinforced concrete pedestal with a 4.0-ft square x 1.75-ft thick reinforced concrete pad bearing directly on the existing sub grade. Additionally, guy wire loading is transferred to six (6) existing 7-ft x 4-ft x 2-ft reinforced concrete anchor support blocks. The foundation information was obtained from the original design documents prepared by ROHN dated September 27, 1979.

- The worst case tower base and guy anchor reactions developed from the governing Load Case were used in the verification of the anchorage foundations:

Tower Guy Reactions		
Vector	Inner	Outer
Horizontal (In Plane of GW)	7 kips	18 kips
Horizontal (Out of Plane of GW)	0 kips	1 kips
Vertical	7 kips	29 kips
Resultant Force at end of Guy Wire	10 kips	34 kips
Tower Base Reactions		
Vector	Proposed Reaction	
Horizontal Shear	1.0 kips	
Axial Compression	83 kips	

Foundation	Design Limit	TIA-222-G Section 9.4 FS ⁽¹⁾	Proposed Loading (FS) ⁽¹⁾	Result
Reinf. Conc. Anchor Block (C) at 99-ft radius.	Uplift	1.0	1.9	PASS
	Sliding	1.0	1.3	PASS
		Ultimate Bearing	Proposed	
Base Foundation	Bearing	12.0 ksf	5.4 ksf	PASS

Note 1: FS denotes 'Factor of Safety'.

Conclusion

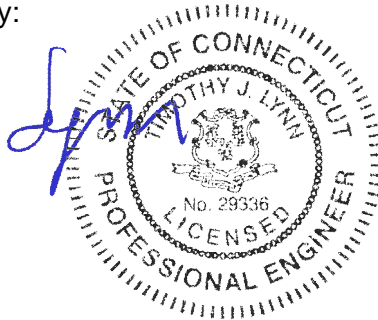
This analysis shows that the subject tower **with the reinforcements detailed in section 4 of this report is structurally adequate** to support the proposed modified antenna configuration.

The analysis is based, in part, on the information provided to this office by AT&T. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:

Timothy J. Lynn, PE
 Structural Engineer



*Standard Conditions for Furnishing of
Professional Engineering Services on
Existing Structures*

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

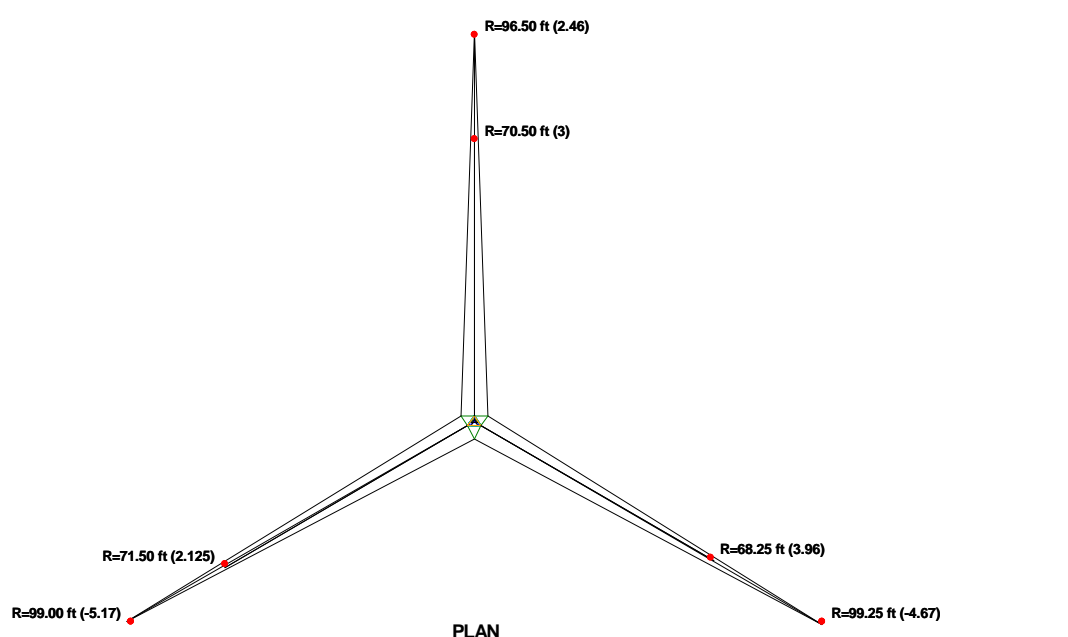
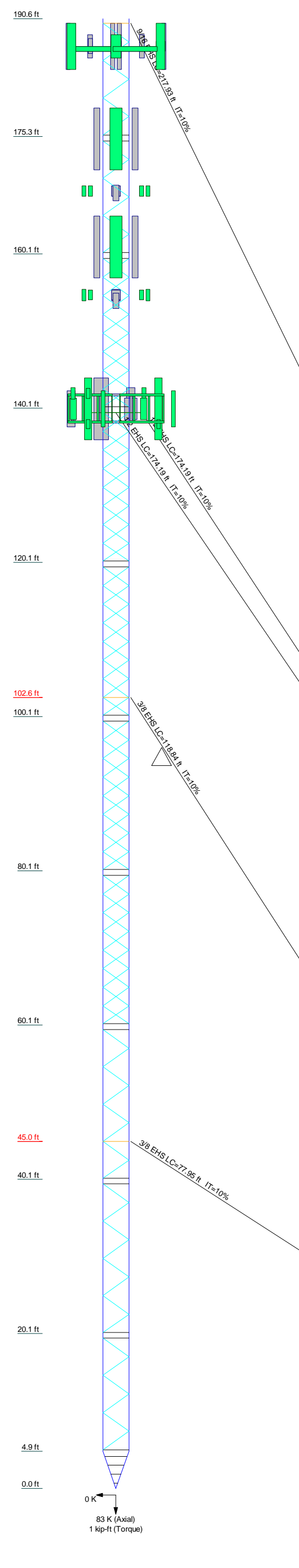
GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

TnxTower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, TnxTower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

TnxTower Features:

- TnxTower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-H standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- TnxTower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11
Legs	ROHN 2.5 X-STR		ROHN 2 STD		ROHN 2.5 X-STR		ROHN 2 EH		ROHN 2.5 STD		A
Leg Grade	A572-50		A572-50		ROHN TS1.5x16 ga		A572-50		ROHN TS1.5x16 ga		N.A.
Diagonals	ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		N.A.
Diagonal Grade	A53-B-42		A53-B-42		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		N.A.
Top Girts	N.A.		N.A.		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		14x3/16
Mid Girts	N.A.		N.A.		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		14x3/16
Bottom Girts	N.A.		N.A.		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		ROHN TS1.5x16 ga		14x3/16
Top Guy Pull-Offs	4 1/2x3/8		N.A.		C4x5.4		N.A.		C4x5.4		N.A.
Face Width (ft)	12 @ 2.420/14		12 @ 2.420/14		56 @ 2.408/85		6 @ 2.419/47		6 @ 2.419/47		B
# Panels @ (ft)	0.5		0.4		0.5		0.4		0.5		0.3
Weight (K)	3.458		0.5		0.5		0.5		0.5		5.1



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
JAHH-65B-R3B (Verizon - Existing)	187	4415 B25 (ATI - Proposed)	168.25
MT6407-77A (Verizon - Existing)	187	DC6-48-60-0-8C-EV (ATI - Proposed)	168
JAHH-65B-R3B (Verizon - Existing)	187	DMP65R-BU8DA (ATI - Proposed)	161
JAHH-65B-R3B (Verizon - Existing)	187	DMP65R-BU8DA (ATI - Proposed)	161
MT6407-77A (Verizon - Existing)	187	DMP65R-BU8DA (ATI - Proposed)	161
JAHH-65B-R3B (Verizon - Existing)	187	SitePro TAP-472 (ATI - Proposed)	161
JAHH-65B-R3B (Verizon - Existing)	187	SitePro TAP-472 (ATI - Proposed)	161
MT6407-77A (Verizon - Existing)	187	SitePro TAP-472 (ATI - Proposed)	161
JAHH-65B-R3B (Verizon - Existing)	187	SitePro MM02 (ATI - Proposed)	161
RF4439d-25A (B2/B66A RRH) (Verizon - Existing)	187	SitePro MM02 (ATI - Proposed)	161
RF4439d-25A (B2/B66A RRH) (Verizon - Existing)	187	SitePro MM02 (ATI - Proposed)	161
RF4439d-25A (B2/B66A RRH) (Verizon - Existing)	187	SitePro MM02 (ATI - Proposed)	161
RF4440d-13A (B5/B13 RRH) (Verizon - Existing)	187	4449 B5/B12 (ATI - Proposed)	154.75
RF4440d-13A (B5/B13 RRH) (Verizon - Existing)	187	4426 B66 (ATI - Existing)	154.75
RF4440d-13A (B5/B13 RRH) (Verizon - Existing)	187	4449 B5/B12 (ATI - Proposed)	154.75
CBC78T-DS-43 (Verizon - Existing)	187	4426 B66 (ATI - Proposed)	154.75
CBC78T-DS-43 (Verizon - Existing)	187	4449 B5/B12 (ATI - Proposed)	154.75
CBC78T-DS-43 (Verizon - Existing)	187	4426 B66 (ATI - Proposed)	154.75
RC2DC-3315-PF-48 (Verizon - Existing)	187	DC9-48-60-24-8C-EV (ATI - Proposed)	154
Pirod 12' T-Frame Sector Mount (1) (Verizon - Existing)	187	Radio 4449 B71 B12 (T-Mobile - Existing)	140
Pirod 12' T-Frame Sector Mount (1) (Verizon - Existing)	187	4415 B25 (T-Mobile - Existing)	140
Pirod 12' T-Frame Sector Mount (1) (Verizon - Existing)	187	4424 B25 (T-Mobile - Existing)	140
Pirod 12' T-Frame Sector Mount (1) (Verizon - Existing)	187	4415 B25 (T-Mobile - Existing)	140
Pirod 12' T-Frame Sector Mount (1) (Verizon - Existing)	187	4415 B25 (T-Mobile - Existing)	140
TPA65R-BU8DA (ATI - Proposed)	175	4424 B25 (T-Mobile - Existing)	140
TPA65R-BU8DA (ATI - Proposed)	175	Radio 4449 B71 B12 (T-Mobile - Existing)	140
TPA65R-BU8DA (ATI - Proposed)	175	APX16DWV-16DWVS-E-A20 (T-Mobile - Existing)	140
SitePro TAP-472 (ATI - Proposed)	175	APXVAARR24-43 (T-Mobile - Existing)	140
SitePro TAP-472 (ATI - Proposed)	175	AIR6449 (T-Mobile - Existing)	140
SitePro TAP-472 (ATI - Proposed)	175	APX16DWV-16DWVS-E-A20 (T-Mobile - Existing)	140
SitePro MM02 (ATI - Proposed)	175	APXVAARR24-43 (T-Mobile - Existing)	140
SitePro MM02 (ATI - Proposed)	175	AIR6449 (T-Mobile - Existing)	140
SitePro MM02 (ATI - Proposed)	175	Radio 4449 B71 B12 (T-Mobile - Existing)	140
SitePro MM02 (ATI - Proposed)	175	12' V-Frame (T-Mobile - Existing)	140
SitePro MM02 (ATI - Proposed)	175	APX16DWV-16DWVS-E-A20 (T-Mobile - Existing)	140
4478 B14 (ATI - Proposed)	168.25	4424 B25 (T-Mobile - Existing)	140
4415 B25 (ATI - Proposed)	168.25	APXVAARR24-43 (T-Mobile - Existing)	140
4478 B14 (ATI - Proposed)	168.25	12' V-Frame (T-Mobile - Existing)	140
4415 B25 (ATI - Proposed)	168.25	AIR6449 (T-Mobile - Existing)	140
4478 B14 (ATI - Proposed)	168.25	12' V-Frame (T-Mobile - Existing)	140

SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	ROHN 2.5 X-STR	B	4 @ 1.17356

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A53-B-42	42 ksi	63 ksi

TOWER DESIGN NOTES

1. Tower designed for Exposure B to the TIA-222-H Standard.
2. Tower designed for a 125 mph basic wind in accordance with the TIA-222-H Standard.
3. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 60 mph wind.
5. Tower Risk Category II.
6. Topographic Category 1 with Crest Height of 0.00 ft
7. TOWER RATING: 71.6%

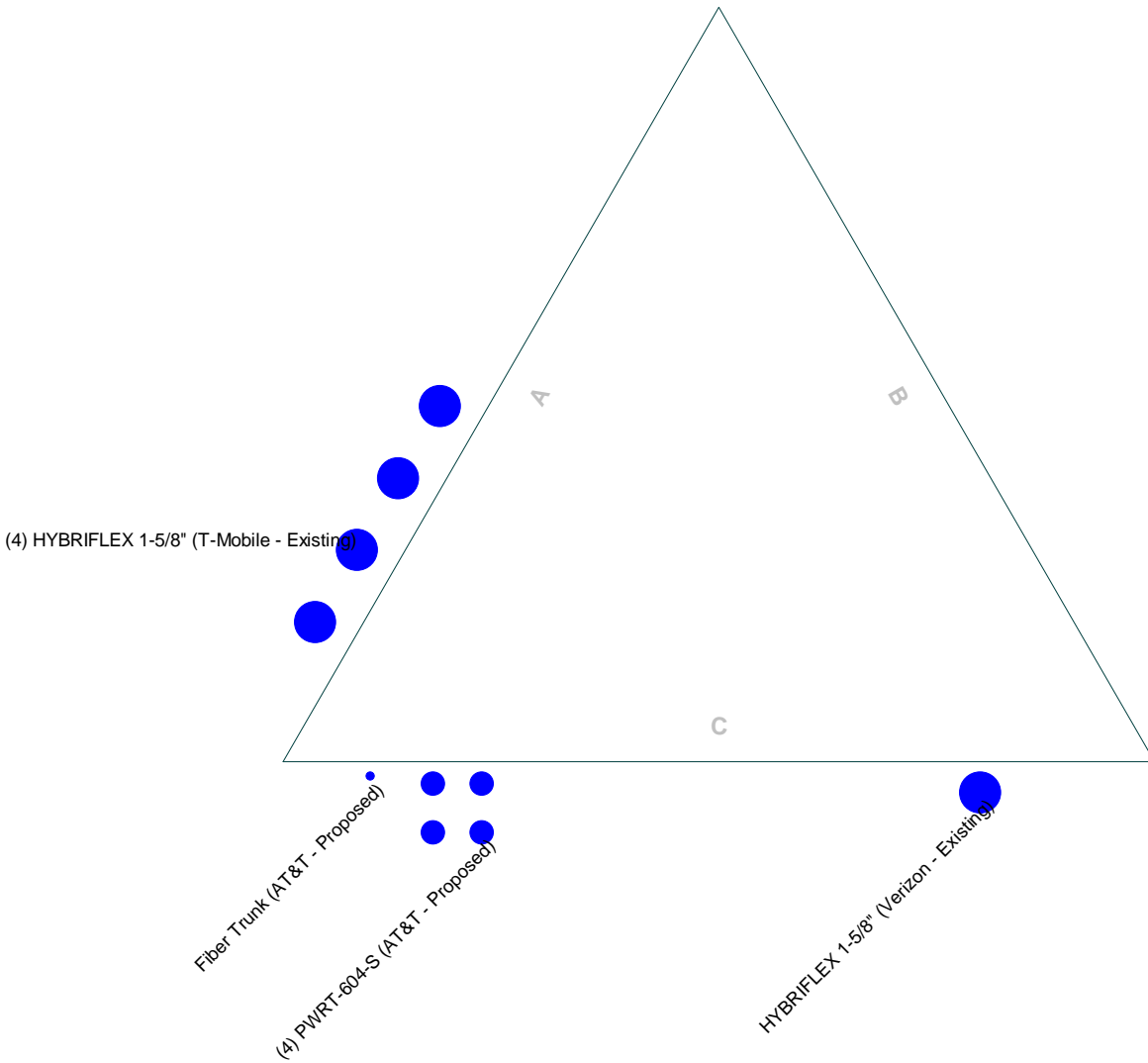


ALL REACTIONS ARE FACTORED

<p>Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587</p>	Job: 21140.00 - CT1166
	Project: 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT
	Client: AT&T
	Code: TIA-222-H
	Drawn by: TJL
	Date: 02/20/23
	App'd:
	Scale: NTS
	Dwg No. E-1

Feed Line Plan

— Round
 — Flat
 — App In Face
 — App Out Face

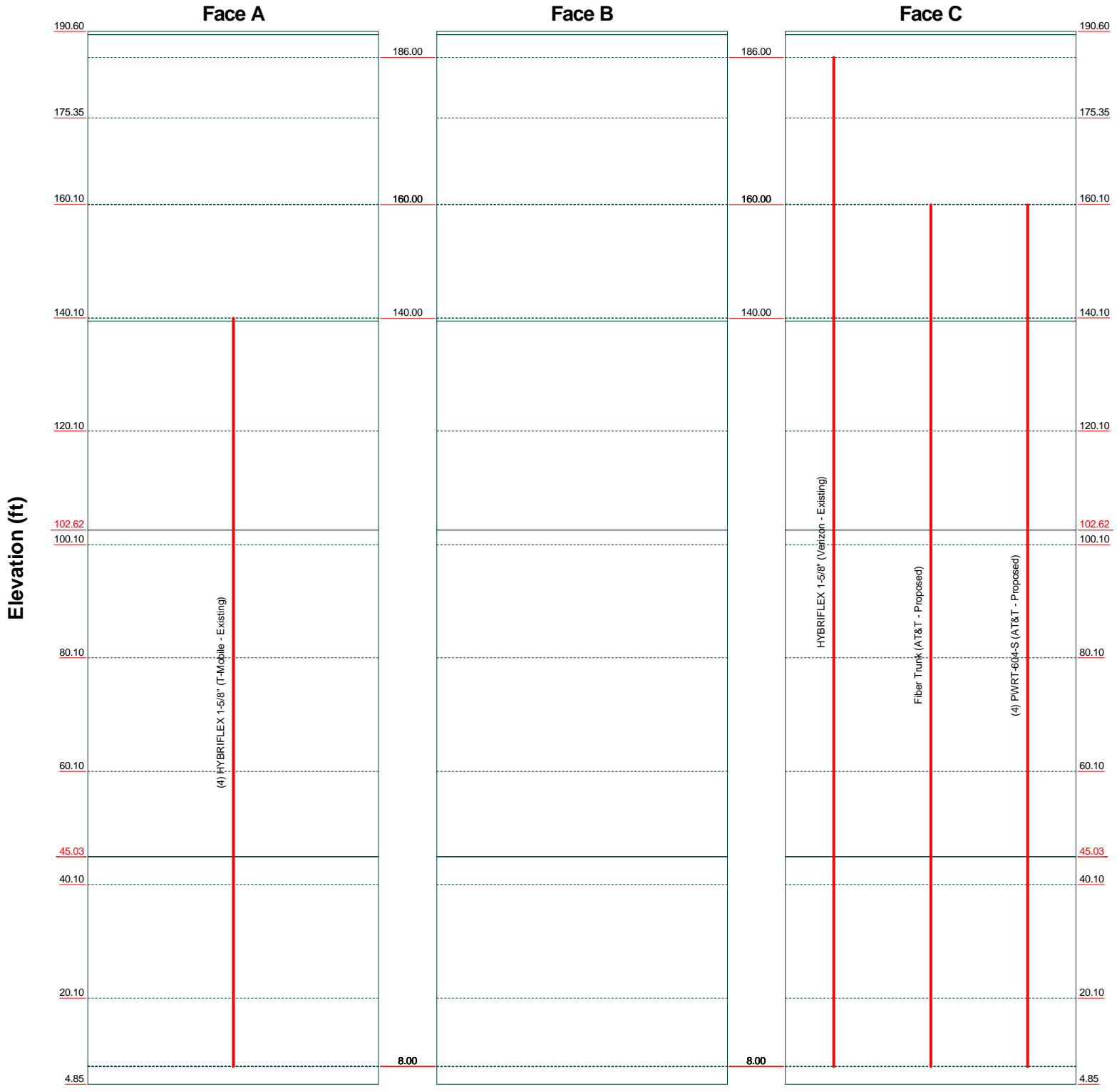


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Client: AT&T	Drawn by: T.JL	App'd:	
Code: TIA-222-H	Date: 02/20/23	Scale: NTS	
Path:		Dwg No: E-7	

Feed Line Distribution Chart

4'10-3/16" - 190'7-3/16"

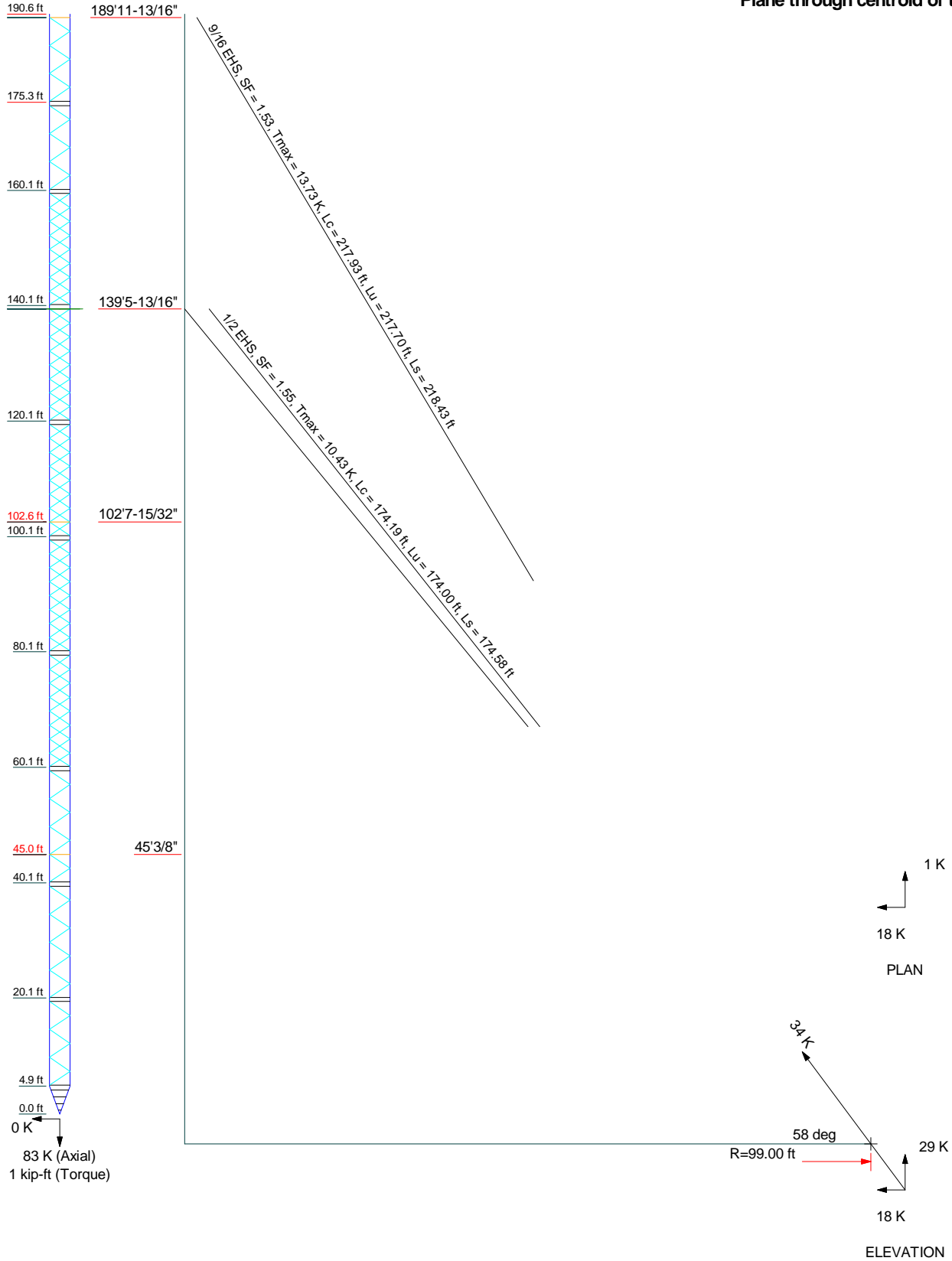
— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



Centek Engineering Inc.			Job: 21140.00 - CT1166		
63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587			Project: 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		
Client: AT&T	Drawn by: T.JL	App'd:	Code: TIA-222-H	Date: 02/20/23	Scale: NTS
Path:				Dwg No: E-7	

Guy Tensions and Tower Reactions
TIA-222-H - 125 mph/50 mph 1.0000 in Ice Exposure B

Maximum Values
Anchor 'C' @99 ft Azimuth 240 deg Elev -5.17 ft
Plane through centroid of tower



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	Client: AT&T	Drawn by: T.JL	App'd:
	Code: TIA-222-H	Date: 02/20/23	Scale: NTS
	Path:		Dwg No: E-6

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 1 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Input Data

The main tower is a 3x guyed tower with an overall height of 190.60 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 3.46 ft at the top and tapered at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower base elevation above sea level: 0.00 ft.

Basic wind speed of 125 mph.

Risk Category II.

Exposure Category B.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

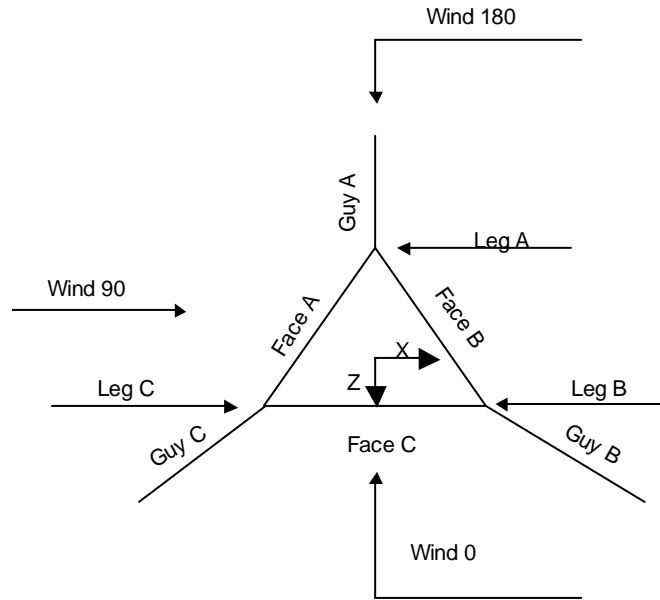
Safety factor used in guy design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

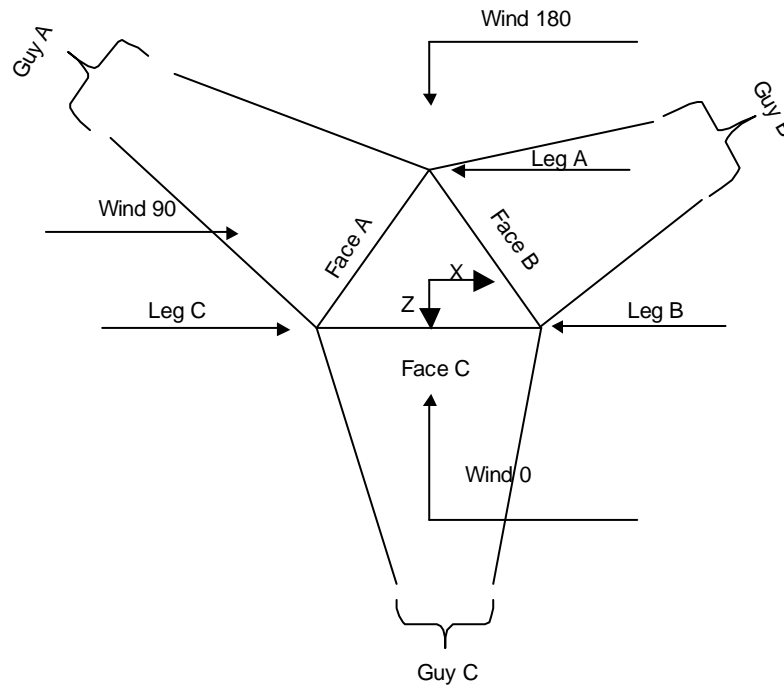
<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) √ SR Members Have Cut Ends SR Members Are Concentric 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r √ Retension Guys To Initial Tension Bypass Mast Stability Checks Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. √ Autocalc Torque Arm Areas Add IBC .6D+W Combination √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs 	<ul style="list-style-type: none"> Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression √ All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
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Job	21140.00 - CT1166	Page	2 of 55
Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date	14:02:32 02/20/23
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Corner & Starmount Guyed Tower

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	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ



Face Guyed

Tower Section Geometry

<i>Tower Section</i>	<i>Tower Elevation</i>	<i>Assembly Database</i>	<i>Description</i>	<i>Section Width</i>	<i>Number of Sections</i>	<i>Section Length</i>
	<i>ft</i>			<i>ft</i>		<i>ft</i>
T1	190.60-175.35			3.46	1	15.25
T2	175.35-160.10			3.46	1	15.25
T3	160.10-140.10			3.46	1	20.00
T4	140.10-120.10			3.46	1	20.00
T5	120.10-100.10			3.46	1	20.00
T6	100.10-80.10			3.46	1	20.00
T7	80.10-60.10			3.46	1	20.00
T8	60.10-40.10			3.46	1	20.00
T9	40.10-20.10			3.46	1	20.00
T10	20.10-4.85			3.46	1	15.25
T11	4.85-0.00			3.46	1	4.85

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 4 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Section Geometry (cont'd)

Tower Section	Tower Elevation ft	Diagonal Spacing ft	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset in	Bottom Girt Offset in
T1	190.60-175.35	2.42	K Brace Left	No	Yes	7.3750	1.3750
T2	175.35-160.10	2.42	K Brace Left	No	Yes	7.3750	1.3750
T3	160.10-140.10	2.41	CX Brace	No	Yes	7.3750	1.3750
T4	140.10-120.10	2.41	CX Brace	No	Yes	7.3750	1.3750
T5	120.10-100.10	2.41	CX Brace	No	Yes	7.3750	1.3750
T6	100.10-80.10	2.41	CX Brace	No	Yes	7.3750	1.3750
T7	80.10-60.10	2.41	CX Brace	No	Yes	7.3750	1.3750
T8	60.10-40.10	2.41	K Brace Left	No	Yes	7.3750	1.3750
T9	40.10-20.10	2.41	K Brace Left	No	Yes	7.3750	1.3750
T10	20.10-4.85	2.42	K Brace Left	No	Yes	7.3750	1.3750
T11	4.85-0.00	1.17	X Brace	No	Yes	8.0000	8.0000

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 190.60-175.35	Pipe	ROHN 2.5 X-STR	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T2 175.35-160.10	Pipe	ROHN 2.5 X-STR	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T3 160.10-140.10	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T4 140.10-120.10	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T5 120.10-100.10	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T6 100.10-80.10	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T7 80.10-60.10	Pipe	ROHN 2 EH	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T8 60.10-40.10	Pipe	ROHN 2.5 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T9 40.10-20.10	Pipe	ROHN 2.5 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T10 20.10-4.85	Pipe	ROHN 2.5 STD	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T11 4.85-0.00	Pipe	ROHN 2.5 X-STR	A572-50 (50 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 190.60-175.35	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T2 175.35-160.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	5 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T3 160.10-140.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T4 140.10-120.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T5 120.10-100.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T6 100.10-80.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T7 80.10-60.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T8 60.10-40.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T9 40.10-20.10	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T10 20.10-4.85	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)	Pipe	ROHN TS1.5x16 ga	A53-B-42 (42 ksi)
T11 4.85-0.00	Flat Bar	14x3/16	A36 (36 ksi)	Flat Bar	14x3/16	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T11 4.85-0.00	2	Flat Bar	14x3/16	A36 (36 ksi)	Flat Bar		A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
T1 190.60-175.35	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T2 175.35-160.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T3 160.10-140.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T4 140.10-120.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T5 120.10-100.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T6 100.10-80.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T7 80.10-60.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000
T8 60.10-40.10	0.00	0.3750	A36 (36 ksi)	1	1	1	36.0000	36.0000	36.0000

<p style="text-align: center;">tnxTower</p> <p style="text-align: center;">Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587</p>	Job		21140.00 - CT1166		Page		7 of 55	
	Project		190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date		14:02:32 02/20/23	
	Client		AT&T		Designed by		TJL	

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T2 175.35-160.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T3 160.10-140.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T4 140.10-120.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T5 120.10-100.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T6 100.10-80.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T7 80.10-60.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T8 60.10-40.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T9 40.10-20.10	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T10 20.10-4.85	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T11 4.85-0.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1

Tower Elevation ft	Redundant Horizontal		Redundant Diagonal		Redundant Sub-Diagonal		Redundant Sub-Horizontal		Redundant Vertical		Redundant Hip		Redundant Hip Diagonal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 190.60-175.35	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 175.35-160.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 160.10-140.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 140.10-120.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 120.10-100.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 100.10-80.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 80.10-60.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 60.10-40.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 40.10-20.10	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10 20.10-4.85	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T11 4.85-0.00	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 190.60-175.35	Flange	0.7500 A325N	4	0.5000 A325X	1	0.5000 A325X	1	0.5000 A325X	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 8 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T2 175.35-160.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T3 160.10-140.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T4 140.10-120.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T5 120.10-100.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T6 100.10-80.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T7 80.10-60.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T8 60.10-40.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T9 40.10-20.10	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T10 20.10-4.85	Flange	0.7500	4	0.5000	1	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	
T11 4.85-0.00	Flange	0.7500	0	0.0000	0	0.0000	0	0.0000	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325X		A325X		A325X		A325N		A325N		A325N	

Guy Data

Guy Elevation ft	Guy Grade	Guy Size	Initial Tension K	%	Guy Modulus ksi	Guy Weight plf	L _u ft	Anchor Radius ft	Anchor Azimuth Adj. °	Anchor Elevation ft	End Fitting Efficiency %
189.985	EHS	A 9/16	3.50	10%	21000	0.671	209.81	96.50	0.0000	2.46	100%
		B 9/16	3.50	10%	21000	0.671	217.41	99.25	0.0000	-4.67	100%
		C 9/16	3.50	10%	21000	0.671	217.75	99.00	0.0000	-5.17	100%
139.485	EHS	A 1/2	2.69	10%	21000	0.517	166.33	96.50	0.0000	2.46	100%
		B 1/2	2.69	10%	21000	0.517	173.77	99.25	0.0000	-4.67	100%
		C 1/2	2.69	10%	21000	0.517	174.04	99.00	0.0000	-5.17	100%
102.623	EHS	A 3/8	1.54	10%	21000	0.273	120.79	70.50	0.0000	3.00	100%
		B 3/8	1.54	10%	21000	0.273	118.73	68.25	0.0000	3.96	100%
		C 3/8	1.54	10%	21000	0.273	122.08	71.50	0.0000	2.13	100%
45.0323	EHS	A 3/8	1.54	10%	21000	0.273	80.30	70.50	0.0000	3.00	100%
		B 3/8	1.54	10%	21000	0.273	77.88	68.25	0.0000	3.96	100%
		C 3/8	1.54	10%	21000	0.273	81.61	71.50	0.0000	2.13	100%

Guy Data(cont'd)

Guy Elevation ft	Mount Type	Torque-Arm Spread ft	Torque-Arm Leg Angle °	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
189.985	Corner						
139.485	Torque Arm	7.00	0.0000	Channel	A36 (36 ksi)	Channel	C10x15.3
102.623	Corner						

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 9 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Guy Elevation ft	Mount Type	Torque-Arm Spread ft	Torque-Arm Leg Angle °	Torque-Arm Style	Torque-Arm Grade	Torque-Arm Type	Torque-Arm Size
45.0323	Corner						

Guy Data (cont'd)

Guy Elevation ft	Diagonal Grade	Diagonal Type	Upper Diagonal Size	Lower Diagonal Size	Is Strap.	Pull-Off Grade	Pull-Off Type	Pull-Off Size
189.99	A53-B-42 (42 ksi)	Pipe			No	A36 (36 ksi)	Flat Bar	4 1/2x3/8
139.49	A53-B-42 (42 ksi)	Pipe				A36 (36 ksi)	Flat Bar	
102.62	A53-B-42 (42 ksi)	Pipe			No	A36 (36 ksi)	Channel	C4x5.4
45.03	A53-B-42 (42 ksi)	Pipe			Yes	A36 (36 ksi)	Channel	C4x5.4

Guy Data (cont'd)

Guy Elevation ft	Cable Weight A K	Cable Weight B K	Cable Weight C K	Cable Weight D K	Tower Intercept A ft	Tower Intercept B ft	Tower Intercept C ft	Tower Intercept D ft
189.985	0.14	0.15	0.15		4.15	4.45	4.47	
					3.5 sec/pulse	3.6 sec/pulse	3.6 sec/pulse	
139.485	0.09	0.09	0.09		2.63	2.86	2.87	
					2.8 sec/pulse	2.9 sec/pulse	2.9 sec/pulse	
102.623	0.03	0.03	0.03		1.28	1.24	1.31	
					2.0 sec/pulse	1.9 sec/pulse	2.0 sec/pulse	
45.0323	0.02	0.02	0.02		0.57	0.54	0.59	
					1.3 sec/pulse	1.3 sec/pulse	1.3 sec/pulse	

Guy Data (cont'd)

Guy Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Torque Arm		Pull Off		Diagonal	
			K _x	K _y	K _x	K _y	K _x	K _y
189.985	Yes	No			1	1	1	1
139.485	Yes	No	1	1	1	1	1	1
102.623	Yes	No			1	1	1	1
45.0323	No	No			1	1	1	1

Guy Data (cont'd)

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 10 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Guy Elevation ft	Torque-Arm				Pull Off				Diagonal			
	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U
189.985	0.6250 A325N	2	0.0000	1	0.0000 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
139.485	0.6250 A325N	0	0.0000	1	0.0000 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
102.623	0.6250 A325N	2	0.0000	1	0.0000 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75
45.0323	0.0000 A325N	0	0.0000	1	0.0000 A325N	0	0.0000	0.75	0.6250 A325N	0	0.0000	0.75

Guy Pressures

Guy Elevation ft	Guy Location	z ft	q _z psf	q _z Ice psf	Ice Thickness in
189.985	A	96.22	33	5	1.1130
	B	92.66	33	5	1.1088
	C	92.41	33	5	1.1085
139.485	A	70.97	30	5	1.0796
	B	67.41	30	5	1.0740
	C	67.16	30	5	1.0736
102.623	A	52.81	28	4	1.0481
	B	53.29	28	4	1.0491
	C	52.37	28	4	1.0473
45.0323	A	24.02	24	4	0.9687
	B	24.50	24	4	0.9706
	C	23.58	24	4	0.9669

Guy-Mast Forces (Excluding Wind) - No Ice

Guy Elevation ft	Guy Location	Chord Angle °	Guy Tension Top Bottom K	F _x K	F _y K	F _z K	M _x kip-ft	M _y kip-ft	M _z kip-ft
189.985	A	63.2542	3.63 3.50	0.00	3.25	-1.60	-6.49	0.00	0.00
	B	63.4524	3.63 3.50	1.38	3.26	0.80	3.26	0.00	-5.64
	C	63.5700	3.63 3.50	-1.37	3.27	0.79	3.26	0.00	5.65
139.485			Sum:	0.01	9.78	-0.01	0.02	0.00	0.01
	A	55.3953	2.76 2.69	-0.06	2.29	-1.55	-4.62	5.53	-8.00
	A	55.3953	2.76 2.69	0.06	2.29	-1.55	-4.62	-5.53	8.00
	B	55.9841	2.76 2.69	1.35	2.31	0.71	9.32	5.45	0.00
	B	55.9841	2.76 2.69	1.29	2.31	0.81	-4.66	-5.45	-8.07
	C	56.1442	2.76 2.69	-1.29	2.31	0.81	-4.67	5.42	8.08
	C	56.1442	2.76	-1.34	2.31	0.71	9.34	-5.42	0.00

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 11 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
			2.69						
			Sum:	0.01	13.80	-0.05	0.09	0.00	0.02
102.623	A	55.4866	1.57	0.00	1.30	-0.88	-2.59	0.00	0.00
			1.54						
	B	56.1182	1.57	0.75	1.31	0.43	1.30	0.00	-2.26
			1.54						
	C	55.3327	1.57	-0.77	1.29	0.44	1.29	0.00	2.24
			1.54						
			Sum:	-0.02	3.90	-0.01	0.01	0.00	-0.02
45.0323	A	31.5324	1.55	0.00	0.82	-1.32	-1.64	0.00	0.00
			1.54						
	B	31.7959	1.55	1.14	0.82	0.66	0.82	0.00	-1.43
			1.54						
	C	31.6887	1.55	-1.14	0.82	0.66	0.82	0.00	1.42
			1.54						
			Sum:	-0.00	2.47	-0.00	0.01	0.00	-0.00

Guy-Mast Forces (Excluding Wind) - Ice

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
189.985	A	63.2542	5.58	0.00	5.05	-2.39	-10.08	0.00	0.00
			5.03						
	B	63.4524	5.61	2.06	5.08	1.19	5.07	0.00	-8.79
			5.04						
	C	63.5700	5.61	-2.05	5.09	1.18	5.08	0.00	8.79
			5.04						
			Sum:	0.01	15.22	-0.01	0.07	0.00	0.01
139.485	A	55.3953	4.34	-0.09	3.64	-2.36	-7.36	8.44	-12.75
			3.98						
	A	55.3953	4.34	0.09	3.64	-2.36	-7.36	-8.44	12.75
			3.98						
	B	55.9841	4.36	2.06	3.69	1.09	14.90	8.34	0.00
			3.99						
	B	55.9841	4.36	1.98	3.69	1.24	-7.45	-8.34	-12.91
			3.99						
	C	56.1442	4.36	-1.97	3.69	1.23	-7.46	8.30	12.92
			3.99						
	C	56.1442	4.36	-2.05	3.69	1.09	14.92	-8.30	0.00
			3.99						
			Sum:	0.02	22.04	-0.06	0.20	0.00	0.02
102.623	A	55.4866	2.45	0.00	2.06	-1.33	-4.11	0.00	0.00
			2.24						
	B	56.1182	2.44	1.12	2.06	0.65	2.06	0.00	-3.56
			2.23						
	C	55.3327	2.46	-1.16	2.06	0.67	2.06	0.00	3.56
			2.25						
			Sum:	-0.03	6.18	-0.01	0.00	0.00	0.00
45.0323	A	31.5324	2.33	0.00	1.27	-1.95	-2.54	0.00	0.00
			2.25						
	B	31.7959	2.32	1.68	1.27	0.97	1.27	0.00	-2.20

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 12 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
	C	31.6887	2.24 2.34 2.26	-1.69	1.28	0.98	1.28	0.00	2.22
			Sum:	-0.01	3.83	-0.01	0.01	0.00	0.01

Guy-Mast Forces (Excluding Wind) - Service

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F _x	F _y	F _z	M _x	M _y	M _z
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
189.985	A	63.2542	3.63 3.50	0.00	3.25	-1.60	-6.49	0.00	0.00
	B	63.4524	3.63 3.50	1.38	3.26	0.80	3.26	0.00	-5.64
	C	63.5700	3.63 3.50	-1.37	3.27	0.79	3.26	0.00	5.65
			Sum:	0.01	9.78	-0.01	0.02	0.00	0.01
139.485	A	55.3953	2.76 2.69	-0.06	2.29	-1.55	-4.62	5.53	-8.00
	A	55.3953	2.76 2.69	0.06	2.29	-1.55	-4.62	-5.53	8.00
	B	55.9841	2.76 2.69	1.35	2.31	0.71	9.32	5.45	0.00
	B	55.9841	2.76 2.69	1.29	2.31	0.81	-4.66	-5.45	-8.07
	C	56.1442	2.76 2.69	-1.29	2.31	0.81	-4.67	5.42	8.08
	C	56.1442	2.76 2.69	-1.34	2.31	0.71	9.34	-5.42	0.00
			Sum:	0.01	13.80	-0.05	0.09	0.00	0.02
102.623	A	55.4866	1.57 1.54	0.00	1.30	-0.88	-2.59	0.00	0.00
	B	56.1182	1.57 1.54	0.75	1.31	0.43	1.30	0.00	-2.26
	C	55.3327	1.57 1.54	-0.77	1.29	0.44	1.29	0.00	2.24
			Sum:	-0.02	3.90	-0.01	0.01	0.00	-0.02
45.0323	A	31.5324	1.55 1.54	0.00	0.82	-1.32	-1.64	0.00	0.00
	B	31.7959	1.55 1.54	1.14	0.82	0.66	0.82	0.00	-1.43
	C	31.6887	1.55 1.54	-1.14	0.82	0.66	0.82	0.00	1.42
			Sum:	-0.00	2.47	-0.00	0.01	0.00	-0.00

Guy-Tensioning Information

Temperature At Time Of Tensioning

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 13 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Guy Elevation ft	H ft	V ft	0 F		20 F		40 F		60 F		80 F		100 F		120 F	
			Initial Tension K	Intercept ft	Initial Tension K	Intercept ft	Initial Tension K	Intercept ft	Initial Tension K	Intercept ft	Initial Tension K	Intercept ft	Initial Tension K	Intercept ft	Initial Tension K	Intercept ft
189.985	A 94.50	187.53	3.814	3.81	3.709	3.92	3.605	4.03	3.500	4.15	3.396	4.27	3.292	4.41	3.188	4.55
	B 97.25	194.66	3.810	4.09	3.706	4.21	3.603	4.33	3.500	4.45	3.397	4.58	3.295	4.72	3.193	4.87
	C 97.00	195.16	3.807	4.11	3.704	4.22	3.602	4.34	3.500	4.47	3.398	4.60	3.297	4.74	3.196	4.88
139.485	A 94.54	137.03	3.076	2.30	2.947	2.40	2.818	2.51	2.690	2.63	2.562	2.76	2.435	2.90	2.309	3.05
	B 97.29	144.16	3.064	2.52	2.939	2.62	2.814	2.74	2.690	2.86	2.566	3.00	2.443	3.15	2.321	3.31
	C 97.04	144.66	3.061	2.53	2.937	2.63	2.813	2.75	2.690	2.87	2.567	3.01	2.445	3.16	2.324	3.32
102.623	A 68.50	99.62	1.746	1.13	1.677	1.18	1.608	1.23	1.540	1.28	1.471	1.34	1.403	1.41	1.335	1.48
	B 66.25	98.66	1.740	1.10	1.673	1.14	1.607	1.19	1.540	1.24	1.474	1.30	1.408	1.36	1.341	1.42
	C 69.50	100.50	1.748	1.16	1.678	1.20	1.609	1.25	1.540	1.31	1.471	1.37	1.402	1.44	1.333	1.51
45.0323	A 68.50	42.03	2.008	0.44	1.851	0.47	1.695	0.52	1.540	0.57	1.385	0.63	1.231	0.71	1.079	0.81
	B 66.25	41.07	2.005	0.41	1.850	0.45	1.695	0.49	1.540	0.54	1.386	0.60	1.233	0.67	1.081	0.76
	C 69.50	42.91	2.006	0.45	1.850	0.49	1.695	0.53	1.540	0.59	1.386	0.65	1.232	0.73	1.081	0.84

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
HYBRIFLEX 1-5/8" (Verizon - Existing)	C	No	No	Ar (CaAa)	186.00 - 8.00	0.5000	-0.3	1	1	1.9800	1.9800		1.90
HYBRIFLEX 1-5/8" (T-Mobile - Existing)	A	No	No	Ar (CaAa)	140.00 - 8.00	1.0000	-0.2	4	4	1.9800	1.9800		1.90
Fiber Trunk (AT&T - Proposed)	C	No	No	Ar (CaAa)	160.00 - 8.00	0.5000	0.4	1	1	0.4000	0.4000		1.00
PWRT-604-S (AT&T - Proposed)	C	No	No	Ar (CaAa)	160.00 - 8.00	0.5000	0.3	4	2	1.1600	1.1600		1.25

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
T1	190.60-175.35	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	2.109	0.000	0.02
T2	175.35-160.10	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	3.019	0.000	0.03
T3	160.10-140.10	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	13.990	0.000	0.16
T4	140.10-120.10	A	0.000	0.000	15.761	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16
T5	120.10-100.10	A	0.000	0.000	15.840	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	14 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T6	100.10-80.10	A	0.000	0.000	15.840	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16
T7	80.10-60.10	A	0.000	0.000	15.840	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16
T8	60.10-40.10	A	0.000	0.000	15.840	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16
T9	40.10-20.10	A	0.000	0.000	15.840	0.000	0.15
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	14.040	0.000	0.16
T10	20.10-4.85	A	0.000	0.000	9.583	0.000	0.09
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	8.494	0.000	0.10
T11	4.85-0.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.00

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T1	190.60-175.35	A	1.187	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	4.637	0.000	0.07
T2	175.35-160.10	A	1.177	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	6.608	0.000	0.10
T3	160.10-140.10	A	1.164	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	34.470	0.000	0.50
T4	140.10-120.10	A	1.147	0.000	0.000	41.566	0.000	0.56
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	34.351	0.000	0.50
T5	120.10-100.10	A	1.128	0.000	0.000	41.659	0.000	0.56
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	34.065	0.000	0.49
T6	100.10-80.10	A	1.106	0.000	0.000	41.522	0.000	0.55
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	33.727	0.000	0.48
T7	80.10-60.10	A	1.078	0.000	0.000	41.355	0.000	0.54
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	33.314	0.000	0.47
T8	60.10-40.10	A	1.043	0.000	0.000	41.138	0.000	0.53
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	32.777	0.000	0.46
T9	40.10-20.10	A	0.991	0.000	0.000	40.824	0.000	0.52
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	31.997	0.000	0.45
T10	20.10-4.85	A	0.907	0.000	0.000	18.366	0.000	0.25
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	18.596	0.000	0.25
T11	4.85-0.00	A	0.770	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.00

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 15 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Feed Line Center of Pressure

Section	Elevation	CP _X	CP _Z	CP _X Ice	CP _Z Ice
	ft	in	in	in	in
T1	190.60-175.35	0.7840	0.8683	0.9885	1.0811
T2	175.35-160.10	1.2279	1.3286	1.4434	1.5616
T3	160.10-140.10	-1.4505	3.5814	-1.7939	3.5953
T4	140.10-120.10	-4.7815	2.8302	-5.3001	2.8006
T5	120.10-100.10	-4.5399	2.7015	-5.0513	2.6583
T6	100.10-80.10	-4.7944	2.8273	-5.4052	2.8214
T7	80.10-60.10	-4.7923	2.8260	-5.4643	2.8356
T8	60.10-40.10	-4.8282	2.8756	-6.3810	3.2990
T9	40.10-20.10	-5.1288	3.0245	-6.6305	3.3747
T10	20.10-4.85	-4.4631	2.6319	-5.1953	3.1727
T11	4.85-0.00	0.0000	0.0000	0.0000	0.0000

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
T1	2	HYBRIFLEX 1-5/8"	175.35 - 186.00	0.6000	0.5988
T2	2	HYBRIFLEX 1-5/8"	160.10 - 175.35	0.6000	0.6000
T3	2	HYBRIFLEX 1-5/8"	140.10 - 160.10	0.6000	0.5061
T3	4	Fiber Trunk	140.10 - 160.00	0.6000	0.5061
T3	5	PWRT-604-S	140.10 - 160.00	0.6000	0.5061
T4	2	HYBRIFLEX 1-5/8"	120.10 - 140.10	0.6000	0.5097
T4	3	HYBRIFLEX 1-5/8"	120.10 - 140.00	0.6000	0.5097
T4	4	Fiber Trunk	120.10 - 140.10	0.6000	0.5097
T4	5	PWRT-604-S	120.10 - 140.10	0.6000	0.5097
T5	2	HYBRIFLEX 1-5/8"	100.10 - 120.10	0.6000	0.4917
T5	3	HYBRIFLEX 1-5/8"	100.10 - 120.10	0.6000	0.4917
T5	4	Fiber Trunk	100.10 - 120.10	0.6000	0.4917
T5	5	PWRT-604-S	100.10 - 120.10	0.6000	0.4917
T6	2	HYBRIFLEX 1-5/8"	80.10 - 100.10	0.6000	0.5187
T6	3	HYBRIFLEX 1-5/8"	80.10 - 100.10	0.6000	0.5187
T6	4	Fiber Trunk	80.10 - 100.10	0.6000	0.5187
T6	5	PWRT-604-S	80.10 - 100.10	0.6000	0.5187
T7	2	HYBRIFLEX 1-5/8"	60.10 - 80.10	0.6000	0.5246
T7	3	HYBRIFLEX 1-5/8"	60.10 - 80.10	0.6000	0.5246

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 16 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
T7	4	Fiber Trunk	60.10 - 80.10	0.6000	0.5246
T7	5	PWRT-604-S	60.10 - 80.10	0.6000	0.5246
T8	2	HYBRIFLEX 1-5/8"	40.10 - 60.10	0.6000	0.6000
T8	3	HYBRIFLEX 1-5/8"	40.10 - 60.10	0.6000	0.6000
T8	4	Fiber Trunk	40.10 - 60.10	0.6000	0.6000
T8	5	PWRT-604-S	40.10 - 60.10	0.6000	0.6000
T9	2	HYBRIFLEX 1-5/8"	20.10 - 40.10	0.6000	0.6000
T9	3	HYBRIFLEX 1-5/8"	20.10 - 40.10	0.6000	0.6000
T9	4	Fiber Trunk	20.10 - 40.10	0.6000	0.6000
T9	5	PWRT-604-S	20.10 - 40.10	0.6000	0.6000
T10	2	HYBRIFLEX 1-5/8"	8.00 - 20.10	0.6000	0.6000
T10	3	HYBRIFLEX 1-5/8"	8.00 - 20.10	0.6000	0.6000
T10	4	Fiber Trunk	8.00 - 20.10	0.6000	0.6000
T10	5	PWRT-604-S	8.00 - 20.10	0.6000	0.6000

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	$C_A A_A$ Front ft ²	$C_A A_A$ Side ft ²	Weight K	
JAHH-65B-R3B (Verizon - Existing)	A	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			-6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
MT6407-77A (Verizon - Existing)	A	From Face	3.00	0.0000	187.00	No Ice	4.71	1.84	0.09
			0.00			1/2" Ice	5.00	2.06	0.12
			0.00			1" Ice	5.29	2.29	0.15
JAHH-65B-R3B (Verizon - Existing)	A	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
JAHH-65B-R3B (Verizon - Existing)	B	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			-6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
MT6407-77A (Verizon - Existing)	B	From Face	3.00	0.0000	187.00	No Ice	4.71	1.84	0.09
			0.00			1/2" Ice	5.00	2.06	0.12
			0.00			1" Ice	5.29	2.29	0.15
JAHH-65B-R3B (Verizon - Existing)	B	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
JAHH-65B-R3B (Verizon - Existing)	C	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			-6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
MT6407-77A (Verizon - Existing)	C	From Face	3.00	0.0000	187.00	No Ice	4.71	1.84	0.09
			0.00			1/2" Ice	5.00	2.06	0.12
			0.00			1" Ice	5.29	2.29	0.15
JAHH-65B-R3B (Verizon - Existing)	C	From Face	3.00	0.0000	187.00	No Ice	9.11	5.98	0.06
			6.00			1/2" Ice	9.58	6.44	0.12
			0.00			1" Ice	10.05	6.91	0.19
RF4439d-25A (B2/B66A RRH) (Verizon - Existing)	A	From Face	3.00	0.0000	187.00	No Ice	1.88	1.25	0.08
			-6.00			1/2" Ice	2.05	1.39	0.09
			0.00			1" Ice	2.22	1.54	0.11
RF4439d-25A (B2/B66A)	B	From Face	3.00	0.0000	187.00	No Ice	1.88	1.25	0.08

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	17 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K
			Horz Lateral ft	Vert ft					
RRH)			-6.00			1/2" Ice	2.05	1.39	0.09
(Verizon - Existing)			0.00			1" Ice	2.22	1.54	0.11
RF4439d-25A (B2/B66A	C	From Face	3.00	0.0000	187.00	No Ice	1.88	1.25	0.08
RRH)			-6.00			1/2" Ice	2.05	1.39	0.09
(Verizon - Existing)			0.00			1" Ice	2.22	1.54	0.11
RF4440d-13A (B5/B13 RRH)	A	From Face	3.00	0.0000	187.00	No Ice	1.88	1.13	0.08
(Verizon - Existing)			0.00			1/2" Ice	2.05	1.26	0.09
			0.00			1" Ice	2.22	1.41	0.11
RF4440d-13A (B5/B13 RRH)	B	From Face	3.00	0.0000	187.00	No Ice	1.88	1.13	0.08
(Verizon - Existing)			0.00			1/2" Ice	2.05	1.26	0.09
			0.00			1" Ice	2.22	1.41	0.11
RF4440d-13A (B5/B13 RRH)	C	From Face	3.00	0.0000	187.00	No Ice	1.88	1.13	0.08
(Verizon - Existing)			0.00			1/2" Ice	2.05	1.26	0.09
			0.00			1" Ice	2.22	1.41	0.11
CBC78T-DS-43	A	From Face	3.00	0.0000	187.00	No Ice	0.37	0.26	0.01
(Verizon - Existing)			-6.00			1/2" Ice	0.45	0.32	0.02
			0.00			1" Ice	0.53	0.40	0.02
CBC78T-DS-43	B	From Face	3.00	0.0000	187.00	No Ice	0.37	0.26	0.01
(Verizon - Existing)			-6.00			1/2" Ice	0.45	0.32	0.02
			0.00			1" Ice	0.53	0.40	0.02
CBC78T-DS-43	C	From Face	3.00	0.0000	187.00	No Ice	0.37	0.26	0.01
(Verizon - Existing)			-6.00			1/2" Ice	0.45	0.32	0.02
			0.00			1" Ice	0.53	0.40	0.02
RC2DC-3315-PF-48	A	From Face	3.00	0.0000	187.00	No Ice	3.01	1.96	0.03
(Verizon - Existing)			0.00			1/2" Ice	3.23	2.15	0.05
			0.00			1" Ice	3.46	2.35	0.08
Pirot 12' T-Frame Sector	A	From Leg	1.00	0.0000	187.00	No Ice	13.60	13.60	0.47
Mount (1)			0.00			1/2" Ice	18.40	18.40	0.60
(Verizon - Existing)			0.00			1" Ice	23.20	23.20	0.73
Pirot 12' T-Frame Sector	B	From Leg	1.00	0.0000	187.00	No Ice	13.60	13.60	0.47
Mount (1)			0.00			1/2" Ice	18.40	18.40	0.60
(Verizon - Existing)			0.00			1" Ice	23.20	23.20	0.73
Pirot 12' T-Frame Sector	C	From Leg	1.00	0.0000	187.00	No Ice	13.60	13.60	0.47
Mount (1)			0.00			1/2" Ice	18.40	18.40	0.60
(Verizon - Existing)			0.00			1" Ice	23.20	23.20	0.73
APX16DWV-16DWVS-E-A	A	From Leg	3.50	0.0000	140.00	No Ice	6.46	2.15	0.04
20			-6.00			1/2" Ice	6.83	2.49	0.07
(T-Mobile - Existing)			0.00			1" Ice	7.21	2.84	0.11
APXVAARR24-43	A	From Leg	3.50	0.0000	140.00	No Ice	20.24	8.89	0.15
(T-Mobile - Existing)			-2.00			1/2" Ice	20.89	9.49	0.27
			0.00			1" Ice	21.54	10.09	0.39
AIR6449	A	From Leg	3.50	0.0000	140.00	No Ice	5.65	2.42	0.10
(T-Mobile - Existing)			2.00			1/2" Ice	5.96	2.64	0.14
			0.00			1" Ice	6.26	2.87	0.18
APX16DWV-16DWVS-E-A	B	From Leg	3.50	0.0000	140.00	No Ice	6.46	2.15	0.04
20			-6.00			1/2" Ice	6.83	2.49	0.07
(T-Mobile - Existing)			0.00			1" Ice	7.21	2.84	0.11
APXVAARR24-43	B	From Leg	3.50	0.0000	140.00	No Ice	20.24	8.89	0.15
(T-Mobile - Existing)			-2.00			1/2" Ice	20.89	9.49	0.27
			0.00			1" Ice	21.54	10.09	0.39
AIR6449	B	From Leg	3.50	0.0000	140.00	No Ice	5.65	2.42	0.10
(T-Mobile - Existing)			2.00			1/2" Ice	5.96	2.64	0.14
			0.00			1" Ice	6.26	2.87	0.18
APX16DWV-16DWVS-E-A	C	From Leg	3.50	0.0000	140.00	No Ice	6.46	2.15	0.04
20			-6.00			1/2" Ice	6.83	2.49	0.07
(T-Mobile - Existing)			0.00			1" Ice	7.21	2.84	0.11
APXVAARR24-43	C	From Leg	3.50	0.0000	140.00	No Ice	20.24	8.89	0.15

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job		21140.00 - CT1166		Page		18 of 55	
	Project		190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date		14:02:32 02/20/23	
	Client		AT&T		Designed by		TJL	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment °	Placement ft	C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K
			Horz Lateral ft	Vert ft					
(T-Mobile - Existing)			-2.00			1/2" Ice	20.89		0.27
			0.00			1" Ice	21.54	10.09	0.39
AIR6449	C	From Leg	3.50	0.0000	140.00	No Ice	5.65	2.42	0.10
(T-Mobile - Existing)			2.00			1/2" Ice	5.96	2.64	0.14
			0.00			1" Ice	6.26	2.87	0.18
Radio 4449 B71 B12	A	From Leg	3.50	0.0000	140.00	No Ice	1.64	1.29	0.07
(T-Mobile - Existing)			-2.00			1/2" Ice	1.80	1.44	0.09
			-2.00			1" Ice	1.97	1.59	0.11
Radio 4449 B71 B12	B	From Leg	3.50	0.0000	140.00	No Ice	1.64	1.29	0.07
(T-Mobile - Existing)			-2.00			1/2" Ice	1.80	1.44	0.09
			-2.00			1" Ice	1.97	1.59	0.11
Radio 4449 B71 B12	C	From Leg	3.50	0.0000	140.00	No Ice	1.64	1.29	0.07
(T-Mobile - Existing)			-2.00			1/2" Ice	1.80	1.44	0.09
			-2.00			1" Ice	1.97	1.59	0.11
4415 B25	A	From Leg	3.50	0.0000	140.00	No Ice	1.84	0.82	0.05
(T-Mobile - Existing)			-2.00			1/2" Ice	2.01	0.94	0.06
			2.00			1" Ice	2.19	1.07	0.08
4415 B25	B	From Leg	3.50	0.0000	140.00	No Ice	1.84	0.82	0.05
(T-Mobile - Existing)			-2.00			1/2" Ice	2.01	0.94	0.06
			2.00			1" Ice	2.19	1.07	0.08
4415 B25	C	From Leg	3.50	0.0000	140.00	No Ice	1.84	0.82	0.05
(T-Mobile - Existing)			-2.00			1/2" Ice	2.01	0.94	0.06
			2.00			1" Ice	2.19	1.07	0.08
4424 B25	A	From Leg	3.50	0.0000	140.00	No Ice	2.05	1.61	0.09
(T-Mobile - Existing)			2.00			1/2" Ice	2.23	1.77	0.11
			2.00			1" Ice	2.42	1.94	0.13
4424 B25	B	From Leg	3.50	0.0000	140.00	No Ice	2.05	1.61	0.09
(T-Mobile - Existing)			2.00			1/2" Ice	2.23	1.77	0.11
			2.00			1" Ice	2.42	1.94	0.13
4424 B25	C	From Leg	3.50	0.0000	140.00	No Ice	2.05	1.61	0.09
(T-Mobile - Existing)			2.00			1/2" Ice	2.23	1.77	0.11
			2.00			1" Ice	2.42	1.94	0.13
12' V-Frame	A	From Leg	2.00	0.0000	140.00	No Ice	9.22	12.97	0.30
(T-Mobile - Existing)			0.00			1/2" Ice	9.22	12.97	0.40
			0.00			1" Ice	9.22	12.97	0.50
12' V-Frame	B	From Leg	2.00	0.0000	140.00	No Ice	9.22	12.97	0.30
(T-Mobile - Existing)			0.00			1/2" Ice	9.22	12.97	0.40
			0.00			1" Ice	9.22	12.97	0.50
12' V-Frame	C	From Leg	2.00	0.0000	140.00	No Ice	9.22	12.97	0.30
(T-Mobile - Existing)			0.00			1/2" Ice	9.22	12.97	0.40
			0.00			1" Ice	9.22	12.97	0.50
TPA65R-BU8DA	A	From Face	2.00	0.0000	175.00	No Ice	17.87	8.12	0.09
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.19
			0.00			1" Ice	19.14	9.32	0.29
DMP65R-BU8DA	A	From Face	2.00	0.0000	161.00	No Ice	17.87	8.12	0.12
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.22
			0.00			1" Ice	19.14	9.32	0.32
TPA65R-BU8DA	B	From Face	2.00	0.0000	175.00	No Ice	17.87	8.12	0.09
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.19
			0.00			1" Ice	19.14	9.32	0.29
DMP65R-BU8DA	B	From Face	2.00	0.0000	161.00	No Ice	17.87	8.12	0.12
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.22
			0.00			1" Ice	19.14	9.32	0.32
TPA65R-BU8DA	C	From Face	2.00	0.0000	175.00	No Ice	17.87	8.12	0.09
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.19
			0.00			1" Ice	19.14	9.32	0.29
DMP65R-BU8DA	C	From Face	2.00	0.0000	161.00	No Ice	17.87	8.12	0.12

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job		21140.00 - CT1166		Page		19 of 55	
	Project		190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date		14:02:32 02/20/23	
	Client		AT&T		Designed by		TJL	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz Lateral	Vert					
(AT&T - Proposed)			0.00			1/2" Ice	18.50	8.72	0.22
			0.00			1" Ice	19.14	9.32	0.32
4478 B14	A	From Leg	3.00		0.0000	No Ice	1.84	1.06	0.06
(AT&T - Proposed)			0.00			1/2" Ice	2.01	1.20	0.08
			0.00			1" Ice	2.19	1.34	0.09
4415 B25	A	From Leg	2.00		0.0000	No Ice	1.84	0.82	0.05
(AT&T - Proposed)			0.00			1/2" Ice	2.01	0.94	0.06
			0.00			1" Ice	2.19	1.07	0.08
4449 B5/B12	A	From Leg	3.00		0.0000	No Ice	1.97	1.41	0.07
(AT&T - Proposed)			0.00			1/2" Ice	2.14	1.56	0.09
			0.00			1" Ice	2.33	1.73	0.11
4426 B66	A	From Leg	2.00		0.0000	No Ice	1.65	0.73	0.05
(AT&T - Proposed)			0.00			1/2" Ice	1.81	0.84	0.06
			0.00			1" Ice	1.98	0.97	0.08
4478 B14	B	From Leg	3.00		0.0000	No Ice	1.84	1.06	0.06
(AT&T - Proposed)			0.00			1/2" Ice	2.01	1.20	0.08
			0.00			1" Ice	2.19	1.34	0.09
4415 B25	B	From Leg	2.00		0.0000	No Ice	1.84	0.82	0.05
(AT&T - Proposed)			0.00			1/2" Ice	2.01	0.94	0.06
			0.00			1" Ice	2.19	1.07	0.08
4449 B5/B12	B	From Leg	3.00		0.0000	No Ice	1.97	1.41	0.07
(AT&T - Proposed)			0.00			1/2" Ice	2.14	1.56	0.09
			0.00			1" Ice	2.33	1.73	0.11
4426 B66	B	From Leg	2.00		0.0000	No Ice	1.65	0.73	0.05
(AT&T - Proposed)			0.00			1/2" Ice	1.81	0.84	0.06
			0.00			1" Ice	1.98	0.97	0.08
4478 B14	C	From Leg	3.00		0.0000	No Ice	1.84	1.06	0.06
(AT&T - Proposed)			0.00			1/2" Ice	2.01	1.20	0.08
			0.00			1" Ice	2.19	1.34	0.09
4415 B25	C	From Leg	2.00		0.0000	No Ice	1.84	0.82	0.05
(AT&T - Proposed)			0.00			1/2" Ice	2.01	0.94	0.06
			0.00			1" Ice	2.19	1.07	0.08
4449 B5/B12	C	From Leg	3.00		0.0000	No Ice	1.97	1.41	0.07
(AT&T - Proposed)			0.00			1/2" Ice	2.14	1.56	0.09
			0.00			1" Ice	2.33	1.73	0.11
4426 B66	C	From Leg	2.00		0.0000	No Ice	1.65	0.73	0.05
(AT&T - Proposed)			0.00			1/2" Ice	1.81	0.84	0.06
			0.00			1" Ice	1.98	0.97	0.08
DC6-48-60-0-8C-EV	A	From Leg	1.00		0.0000	No Ice	1.91	1.91	0.02
(AT&T - Proposed)			0.00			1/2" Ice	2.10	2.10	0.04
			0.00			1" Ice	2.29	2.29	0.06
DC9-48-60-24-8C-EV	A	From Leg	1.00		0.0000	No Ice	1.91	1.91	0.02
(AT&T - Proposed)			0.00			1/2" Ice	2.10	2.10	0.04
			0.00			1" Ice	2.29	2.29	0.06
SitePro TAP-472	A	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro TAP-472	B	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro TAP-472	C	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro MM02	A	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	A	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	20 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft ²	ft ²	K
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			-1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	B	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	B	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			-1.50			1" Ice	1.50	2.40	0.08
SitePro TAP-472	A	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro TAP-472	B	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro TAP-472	C	From Face	0.50		0.0000	No Ice	0.00	2.70	0.24
(AT&T - Proposed)			0.00			1/2" Ice	0.00	3.80	0.30
			0.00			1" Ice	0.00	4.90	0.36
SitePro MM02	A	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	A	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			-1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	B	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			1.50			1" Ice	1.50	2.40	0.08
SitePro MM02	B	From Face	0.50		0.0000	No Ice	0.50	0.80	0.04
(AT&T - Proposed)			0.00			1/2" Ice	1.00	1.60	0.06
			-1.50			1" Ice	1.50	2.40	0.08

Tower Pressures - No Ice

$$G_H = 0.850$$

Section Elevation	z	K _Z	q _z	A _G	F _a	A _F	A _R	A _{leg}	Leg %	C _{AA} In Face	C _{AA} Out Face
ft	ft		psf	ft ²	c	ft ²	ft ²	ft ²	%	ft ²	ft ²
T1 190.60-175.35	182.98	1.174	40	56.388	A	1.207	10.656	7.307	61.60	0.000	0.000
					B	1.207	10.656			0.000	0.000
					C	1.207	10.656			2.109	0.000
T2 175.35-160.10	167.73	1.146	39	56.388	A	0.000	11.058	7.307	66.08	0.000	0.000
					B	0.000	11.058			0.000	0.000
					C	0.000	11.058			3.019	0.000
T3 160.10-140.10	150.10	1.11	38	73.118	A	0.000	16.678	7.917	47.47	0.000	0.000
					B	0.000	16.678			0.000	0.000
					C	0.000	16.678			13.990	0.000
T4 140.10-120.10	130.10	1.065	36	73.118	A	0.000	16.678	7.917	47.47	15.761	0.000
					B	0.000	16.678			47.47	0.000
					C	0.000	16.678			47.47	14.040

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	21 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _{AA} In Face ft ²	C _{AA} Out Face ft ²
T5 120.10-100.10	110.10	1.016	35	73.118	A B C	1.087 1.087 1.087	16.678 16.678 16.678	7.917	44.56 44.56 44.56	15.840 0.000 14.040	0.000 0.000 0.000
T6 100.10-80.10	90.10	0.959	33	73.118	A B C	0.000 0.000 0.000	16.678 16.678 16.678	7.917	47.47 47.47 47.47	15.840 0.000 14.040	0.000 0.000 0.000
T7 80.10-60.10	70.10	0.893	30	73.127	A B C	0.000 0.000 0.000	16.693 16.693 16.693	7.933	47.52 47.52 47.52	15.840 0.000 14.040	0.000 0.000 0.000
T8 60.10-40.10	50.10	0.811	28	73.952	A B C	1.073 1.073 1.073	14.310 14.310 14.310	9.583	62.30 62.30 62.30	15.840 0.000 14.040	0.000 0.000 0.000
T9 40.10-20.10	30.10	0.701	24	73.952	A B C	0.000 0.000 0.000	14.310 14.310 14.310	9.583	66.97 66.97 66.97	15.840 0.000 14.040	0.000 0.000 0.000
T10 20.10-4.85	12.48	0.7	24	56.373	A B C	0.000 0.000 0.000	11.056 11.056 11.056	7.305	66.08 66.08 66.08	9.583 0.000 8.494	0.000 0.000 0.000
T11 4.85-0.00	2.43	0.7	24	9.627	A B C	6.951 6.951 6.951	2.515 2.515 2.515	2.515	26.57 26.57 26.57	0.000 0.000 0.000	0.000 0.000 0.000

Tower Pressure - With Ice

$G_H = 0.850$

Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _{AA} In Face ft ²	C _{AA} Out Face ft ²
T1 190.60-175.35	182.98	1.174	6	1.1868	59.405	A B C	1.207 1.207 1.207	22.624 22.624 22.624	13.340	55.98 55.98 55.98	0.000 0.000 4.637	0.000 0.000 0.000
T2 175.35-160.10	167.73	1.146	6	1.1765	59.379	A B C	0.000 0.000 0.000	22.923 22.923 22.923	13.288	57.97 57.97 57.97	0.000 0.000 6.608	0.000 0.000 0.000
T3 160.10-140.10	150.10	1.11	6	1.1636	76.997	A B C	0.000 0.000 0.000	38.027 38.027 38.027	15.674	41.22 41.22 41.22	0.000 0.000 34.470	0.000 0.000 0.000
T4 140.10-120.10	130.10	1.065	6	1.1470	76.942	A B C	0.000 0.000 0.000	37.724 37.724 37.724	15.564	41.26 41.26 41.26	41.566 0.000 34.351	0.000 0.000 0.000
T5 120.10-100.10	110.10	1.016	6	1.1280	76.878	A B C	1.087 1.087 1.087	37.989 37.989 37.989	15.437	39.51 39.51 39.51	41.659 0.000 34.065	0.000 0.000 0.000
T6 100.10-80.10	90.10	0.959	5	1.1057	76.804	A B C	0.000 0.000 0.000	36.965 36.965 36.965	15.288	41.36 41.36 41.36	41.522 0.000 33.727	0.000 0.000 0.000
T7 80.10-60.10	70.10	0.893	5	1.0783	76.721	A B C	0.000 0.000 0.000	36.476 36.476 36.476	15.122	41.46 41.46 41.46	41.355 0.000 33.314	0.000 0.000 0.000
T8 60.10-40.10	50.10	0.811	4	1.0426	77.427	A B C	1.073 1.073 1.073	28.392 28.392 28.392	16.534	56.12 56.12 56.12	41.138 0.000 32.777	0.000 0.000 0.000
T9 40.10-20.10	30.10	0.701	4	0.9908	77.254	A B C	0.000 0.000 0.000	27.161 27.161 27.161	16.189	59.60 59.60 59.60	40.824 0.000 0.000	0.000 0.000 0.000

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	22 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
T10 20.10-4.85	12.48	0.7	4	0.9073	58.679	C	0.000	27.161	11.916	59.60	31.997	0.000
						A	0.000	20.204		58.98	18.366	0.000
						B	0.000	20.204		58.98	0.000	0.000
T11 4.85-0.00	2.43	0.7	4	0.7703	10.289	C	0.000	20.204	3.863	58.98	18.596	0.000
						A	6.951	4.627		33.36	0.000	0.000
						B	6.951	4.627		33.36	0.000	0.000
						C	6.951	4.627		33.36	0.000	0.000

Tower Pressure - Service

$G_H = 0.850$

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e ft ²	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
T1 190.60-175.35	182.98	1.174	9	56.388	A	1.207	10.656	7.307	61.60	0.000	0.000
					B	1.207	10.656		61.60	0.000	0.000
					C	1.207	10.656		61.60	2.109	0.000
T2 175.35-160.10	167.73	1.146	9	56.388	A	0.000	11.058	7.307	66.08	0.000	0.000
					B	0.000	11.058		66.08	0.000	0.000
					C	0.000	11.058		66.08	3.019	0.000
T3 160.10-140.10	150.10	1.11	9	73.118	A	0.000	16.678	7.917	47.47	0.000	0.000
					B	0.000	16.678		47.47	0.000	0.000
					C	0.000	16.678		47.47	13.990	0.000
T4 140.10-120.10	130.10	1.065	8	73.118	A	0.000	16.678	7.917	47.47	15.761	0.000
					B	0.000	16.678		47.47	0.000	0.000
					C	0.000	16.678		47.47	14.040	0.000
T5 120.10-100.10	110.10	1.016	8	73.118	A	1.087	16.678	7.917	44.56	15.840	0.000
					B	1.087	16.678		44.56	0.000	0.000
					C	1.087	16.678		44.56	14.040	0.000
T6 100.10-80.10	90.10	0.959	8	73.118	A	0.000	16.678	7.917	47.47	15.840	0.000
					B	0.000	16.678		47.47	0.000	0.000
					C	0.000	16.678		47.47	14.040	0.000
T7 80.10-60.10	70.10	0.893	7	73.127	A	0.000	16.693	7.933	47.52	15.840	0.000
					B	0.000	16.693		47.52	0.000	0.000
					C	0.000	16.693		47.52	14.040	0.000
T8 60.10-40.10	50.10	0.811	6	73.952	A	1.073	14.310	9.583	62.30	15.840	0.000
					B	1.073	14.310		62.30	0.000	0.000
					C	1.073	14.310		62.30	14.040	0.000
T9 40.10-20.10	30.10	0.701	5	73.952	A	0.000	14.310	9.583	66.97	15.840	0.000
					B	0.000	14.310		66.97	0.000	0.000
					C	0.000	14.310		66.97	14.040	0.000
T10 20.10-4.85	12.48	0.7	5	56.373	A	0.000	11.056	7.305	66.08	9.583	0.000
					B	0.000	11.056		66.08	0.000	0.000
					C	0.000	11.056		66.08	8.494	0.000
T11 4.85-0.00	2.43	0.7	5	9.627	A	6.951	2.515	2.515	26.57	0.000	0.000
					B	6.951	2.515		26.57	0.000	0.000
					C	6.951	2.515		26.57	0.000	0.000

Tower Forces - No Ice - Wind Normal To Face

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 23 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.02	0.49	A	0.21	2.562	40	1	1	7.349	0.68	44.71	C
			B	0.21	2.562		1	1	7.349			
			C	0.21	2.562		1	1	7.349			
T2 175.35-160.10	0.03	0.44	A	0.196	2.609	39	1	1	6.345	0.61	39.87	C
			B	0.196	2.609		1	1	6.345			
			C	0.196	2.609		1	1	6.345			
T3 160.10-140.10	0.16	0.42	A	0.228	2.505	38	1	1	9.673	1.05	52.32	C
			B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T4 140.10-120.10	0.31	0.42	A	0.228	2.505	36	1	1	9.673	1.30	64.83	C
		TA 0.32	B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T5 120.10-100.10	0.31	0.47	A	0.243	2.459	35	1	1	10.815	1.31	65.35	C
			B	0.243	2.459		1	1	10.815			
			C	0.243	2.459		1	1	10.815			
T6 100.10-80.10	0.31	0.42	A	0.228	2.505	33	1	1	9.673	1.17	58.43	C
			B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T7 80.10-60.10	0.31	0.50	A	0.228	2.504	30	1	1	9.682	1.09	54.41	C
			B	0.228	2.504		1	1	9.682			
			C	0.228	2.504		1	1	9.682			
T8 60.10-40.10	0.31	0.51	A	0.208	2.569	28	1	1	9.315	0.98	49.07	C
			B	0.208	2.569		1	1	9.315			
			C	0.208	2.569		1	1	9.315			
T9 40.10-20.10	0.31	0.46	A	0.194	2.618	24	1	1	8.205	0.80	39.93	C
			B	0.194	2.618		1	1	8.205			
			C	0.194	2.618		1	1	8.205			
T10 20.10-4.85	0.19	0.35	A	0.196	2.609	24	1	1	6.344	0.55	36.35	C
			B	0.196	2.609		1	1	6.344			
			C	0.196	2.609		1	1	6.344			
T11 4.85-0.00	0.00	0.31	A	0.983	2.066	24	1	1	9.466	0.40	81.49	C
			B	0.983	2.066		1	1	9.466			
			C	0.983	2.066		1	1	9.466			
Sum Weight:	2.25	5.11								9.93		

Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.02	0.49	A	0.21	2.562	40	0.8	1	7.107	0.66	43.34	C
			B	0.21	2.562		0.8	1	7.107			
			C	0.21	2.562		0.8	1	7.107			
T2 175.35-160.10	0.03	0.44	A	0.196	2.609	39	0.8	1	6.345	0.61	39.87	C
			B	0.196	2.609		0.8	1	6.345			
			C	0.196	2.609		0.8	1	6.345			
T3 160.10-140.10	0.16	0.42	A	0.228	2.505	38	0.8	1	9.673	1.05	52.32	C
			B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T4 140.10-120.10	0.31	0.42	A	0.228	2.505	36	0.8	1	9.673	1.30	64.83	C
		TA 0.32	B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T5	0.31	0.47	A	0.243	2.459	35	0.8	1	10.598	1.29	64.56	C

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 24 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
120.10-100.10			B	0.243	2.459		0.8	1	10.598			
			C	0.243	2.459		0.8	1	10.598			
T6	0.31	0.42	A	0.228	2.505	33	0.8	1	9.673	1.17	58.43	C
100.10-80.10			B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T7	0.31	0.50	A	0.228	2.504	30	0.8	1	9.682	1.09	54.41	C
80.10-60.10			B	0.228	2.504		0.8	1	9.682			
			C	0.228	2.504		0.8	1	9.682			
T8	0.31	0.51	A	0.208	2.569	28	0.8	1	9.100	0.97	48.42	C
60.10-40.10			B	0.208	2.569		0.8	1	9.100			
			C	0.208	2.569		0.8	1	9.100			
T9	0.31	0.46	A	0.194	2.618	24	0.8	1	8.205	0.80	39.93	C
40.10-20.10			B	0.194	2.618		0.8	1	8.205			
			C	0.194	2.618		0.8	1	8.205			
T10	0.19	0.35	A	0.196	2.609	24	0.8	1	6.344	0.55	36.35	C
20.10-4.85			B	0.196	2.609		0.8	1	6.344			
			C	0.196	2.609		0.8	1	6.344			
T11 4.85-0.00	0.00	0.31	A	0.983	2.066	24	0.8	1	8.075	0.34	69.52	C
			B	0.983	2.066		0.8	1	8.075			
			C	0.983	2.066		0.8	1	8.075			
Sum Weight:	2.25	5.11								9.82		

Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1	0.02	0.49	A	0.21	2.562	40	0.85	1	7.168	0.67	43.68	C
190.60-175.35			B	0.21	2.562		0.85	1	7.168			
			C	0.21	2.562		0.85	1	7.168			
T2	0.03	0.44	A	0.196	2.609	39	0.85	1	6.345	0.61	39.87	C
175.35-160.10			B	0.196	2.609		0.85	1	6.345			
			C	0.196	2.609		0.85	1	6.345			
T3	0.16	0.42	A	0.228	2.505	38	0.85	1	9.673	1.05	52.32	C
160.10-140.10			B	0.228	2.505		0.85	1	9.673			
			C	0.228	2.505		0.85	1	9.673			
T4	0.31	0.42	A	0.228	2.505	36	0.85	1	9.673	1.30	64.83	C
140.10-120.10		TA 0.32	B	0.228	2.505		0.85	1	9.673			
			C	0.228	2.505		0.85	1	9.673			
T5	0.31	0.47	A	0.243	2.459	35	0.85	1	10.652	1.30	64.76	C
120.10-100.10			B	0.243	2.459		0.85	1	10.652			
			C	0.243	2.459		0.85	1	10.652			
T6	0.31	0.42	A	0.228	2.505	33	0.85	1	9.673	1.17	58.43	C
100.10-80.10			B	0.228	2.505		0.85	1	9.673			
			C	0.228	2.505		0.85	1	9.673			
T7	0.31	0.50	A	0.228	2.504	30	0.85	1	9.682	1.09	54.41	C
80.10-60.10			B	0.228	2.504		0.85	1	9.682			
			C	0.228	2.504		0.85	1	9.682			
T8	0.31	0.51	A	0.208	2.569	28	0.85	1	9.154	0.97	48.58	C
60.10-40.10			B	0.208	2.569		0.85	1	9.154			
			C	0.208	2.569		0.85	1	9.154			
T9	0.31	0.46	A	0.194	2.618	24	0.85	1	8.205	0.80	39.93	C
40.10-20.10			B	0.194	2.618		0.85	1	8.205			

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	25 of 55
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date	14:02:32 02/20/23
	Client	AT&T	Designed by	TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T10 20.10-4.85	0.19	0.35	C	0.194	2.618		0.85	1	8.205			
			A	0.196	2.609	24	0.85	1	6.344	0.55	36.35	C
			B	0.196	2.609		0.85	1	6.344			
T11 4.85-0.00	0.00	0.31	C	0.196	2.609		0.85	1	6.344			
			A	0.983	2.066	24	0.85	1	8.423	0.35	72.52	C
			B	0.983	2.066		0.85	1	8.423			
			C	0.983	2.066		0.85	1	8.423			
Sum Weight:	2.25	5.11								9.85		

Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.07	1.18	A	0.401	2.062	6	1	1	15.613	0.19	12.45	C
			B	0.401	2.062		1	1	15.613			
			C	0.401	2.062		1	1	15.613			
T2 175.35-160.10	0.10	1.08	A	0.386	2.092	6	1	1	14.449	0.18	11.88	C
			B	0.386	2.092		1	1	14.449			
			C	0.386	2.092		1	1	14.449			
T3 160.10-140.10	0.50	1.57	A	0.494	1.908	6	1	1	25.924	0.34	17.17	C
			B	0.494	1.908		1	1	25.924			
			C	0.494	1.908		1	1	25.924			
T4 140.10-120.10	1.06	1.54	A	0.49	1.913	6	1	1	25.645	0.43	21.62	C
		TA 0.66	B	0.49	1.913		1	1	25.645			
			C	0.49	1.913		1	1	25.645			
T5 120.10-100.10	1.05	1.65	A	0.508	1.889	6	1	1	27.280	0.42	20.85	C
			B	0.508	1.889		1	1	27.280			
			C	0.508	1.889		1	1	27.280			
T6 100.10-80.10	1.03	1.49	A	0.481	1.926	5	1	1	24.954	0.39	19.31	C
			B	0.481	1.926		1	1	24.954			
			C	0.481	1.926		1	1	24.954			
T7 80.10-60.10	1.02	1.53	A	0.475	1.934	5	1	1	24.513	0.36	17.87	C
			B	0.475	1.934		1	1	24.513			
			C	0.475	1.934		1	1	24.513			
T8 60.10-40.10	0.99	1.28	A	0.381	2.104	4	1	1	18.904	0.32	15.78	C
			B	0.381	2.104		1	1	18.904			
			C	0.381	2.104		1	1	18.904			
T9 40.10-20.10	0.96	1.11	A	0.352	2.168	4	1	1	16.749	0.26	12.97	C
			B	0.352	2.168		1	1	16.749			
			C	0.352	2.168		1	1	16.749			
T10 20.10-4.85	0.50	0.80	A	0.344	2.185	4	1	1	12.405	0.16	10.46	C
			B	0.344	2.185		1	1	12.405			
			C	0.344	2.185		1	1	12.405			
T11 4.85-0.00	0.00	0.65	A	1	2.1	4	1	1	11.578	0.07*	14.41	C
			B	1	2.1		1	1	11.578			
			C	1	2.1		1	1	11.578			
Sum Weight:	7.28	14.52								3.11		

*2.1A_g limit

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 26 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K				psf			ft ²	K	plf	
T1 190.60-175.35	0.07	1.18	A	0.401	2.062	6	0.8	1	15.372	0.19	12.27	C
			B	0.401	2.062		0.8	1	15.372			
			C	0.401	2.062		0.8	1	15.372			
T2 175.35-160.10	0.10	1.08	A	0.386	2.092	6	0.8	1	14.449	0.18	11.88	C
			B	0.386	2.092		0.8	1	14.449			
			C	0.386	2.092		0.8	1	14.449			
T3 160.10-140.10	0.50	1.57	A	0.494	1.908	6	0.8	1	25.924	0.34	17.17	C
			B	0.494	1.908		0.8	1	25.924			
			C	0.494	1.908		0.8	1	25.924			
T4 140.10-120.10	1.06	1.54	A	0.49	1.913	6	0.8	1	25.645	0.43	21.62	C
		TA 0.66	B	0.49	1.913		0.8	1	25.645			
			C	0.49	1.913		0.8	1	25.645			
T5 120.10-100.10	1.05	1.65	A	0.508	1.889	6	0.8	1	27.063	0.42	20.75	C
			B	0.508	1.889		0.8	1	27.063			
			C	0.508	1.889		0.8	1	27.063			
T6 100.10-80.10	1.03	1.49	A	0.481	1.926	5	0.8	1	24.954	0.39	19.31	C
			B	0.481	1.926		0.8	1	24.954			
			C	0.481	1.926		0.8	1	24.954			
T7 80.10-60.10	1.02	1.53	A	0.475	1.934	5	0.8	1	24.513	0.36	17.87	C
			B	0.475	1.934		0.8	1	24.513			
			C	0.475	1.934		0.8	1	24.513			
T8 60.10-40.10	0.99	1.28	A	0.381	2.104	4	0.8	1	18.689	0.31	15.69	C
			B	0.381	2.104		0.8	1	18.689			
			C	0.381	2.104		0.8	1	18.689			
T9 40.10-20.10	0.96	1.11	A	0.352	2.168	4	0.8	1	16.749	0.26	12.97	C
			B	0.352	2.168		0.8	1	16.749			
			C	0.352	2.168		0.8	1	16.749			
T10 20.10-4.85	0.50	0.80	A	0.344	2.185	4	0.8	1	12.405	0.16	10.46	C
			B	0.344	2.185		0.8	1	12.405			
			C	0.344	2.185		0.8	1	12.405			
T11 4.85-0.00	0.00	0.65	A	1	2.1	4	0.8	1	10.188	0.07	14.27	C
			B	1	2.1		0.8	1	10.188			
			C	1	2.1		0.8	1	10.188			
Sum Weight:	7.28	14.52								3.10		

Tower Forces - With Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	q _z	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K				psf			ft ²	K	plf	
T1 190.60-175.35	0.07	1.18	A	0.401	2.062	6	0.85	1	15.432	0.19	12.32	C
			B	0.401	2.062		0.85	1	15.432			
			C	0.401	2.062		0.85	1	15.432			
T2 175.35-160.10	0.10	1.08	A	0.386	2.092	6	0.85	1	14.449	0.18	11.88	C
			B	0.386	2.092		0.85	1	14.449			
			C	0.386	2.092		0.85	1	14.449			
T3 160.10-140.10	0.50	1.57	A	0.494	1.908	6	0.85	1	25.924	0.34	17.17	C
			B	0.494	1.908		0.85	1	25.924			
			C	0.494	1.908		0.85	1	25.924			

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 27 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T4 140.10-120.10	1.06	1.54 TA 0.66	A	0.49	1.913	6	0.85	1	25.645	0.43	21.62	C
			B	0.49	1.913		0.85	1	25.645			
			C	0.49	1.913		0.85	1	25.645			
T5 120.10-100.10	1.05	1.65	A	0.508	1.889	6	0.85	1	27.117	0.42	20.78	C
			B	0.508	1.889		0.85	1	27.117			
			C	0.508	1.889		0.85	1	27.117			
T6 100.10-80.10	1.03	1.49	A	0.481	1.926	5	0.85	1	24.954	0.39	19.31	C
			B	0.481	1.926		0.85	1	24.954			
			C	0.481	1.926		0.85	1	24.954			
T7 80.10-60.10	1.02	1.53	A	0.475	1.934	5	0.85	1	24.513	0.36	17.87	C
			B	0.475	1.934		0.85	1	24.513			
			C	0.475	1.934		0.85	1	24.513			
T8 60.10-40.10	0.99	1.28	A	0.381	2.104	4	0.85	1	18.743	0.31	15.71	C
			B	0.381	2.104		0.85	1	18.743			
			C	0.381	2.104		0.85	1	18.743			
T9 40.10-20.10	0.96	1.11	A	0.352	2.168	4	0.85	1	16.749	0.26	12.97	C
			B	0.352	2.168		0.85	1	16.749			
			C	0.352	2.168		0.85	1	16.749			
T10 20.10-4.85	0.50	0.80	A	0.344	2.185	4	0.85	1	12.405	0.16	10.46	C
			B	0.344	2.185		0.85	1	12.405			
			C	0.344	2.185		0.85	1	12.405			
T11 4.85-0.00	0.00	0.65	A	1	2.1	4	0.85	1	10.535	0.07*	14.41	C
			B	1	2.1		0.85	1	10.535			
			C	1	2.1		0.85	1	10.535			
Sum Weight:	7.28	14.52			*2.1A _g limit					3.11		

Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.02	0.49	A	0.21	2.562	9	1	1	7.349	0.16	10.30	C
			B	0.21	2.562		1	1	7.349			
			C	0.21	2.562		1	1	7.349			
T2 175.35-160.10	0.03	0.44	A	0.196	2.609	9	1	1	6.345	0.14	9.19	C
			B	0.196	2.609		1	1	6.345			
			C	0.196	2.609		1	1	6.345			
T3 160.10-140.10	0.16	0.42	A	0.228	2.505	9	1	1	9.673	0.24	12.05	C
			B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T4 140.10-120.10	0.31	0.42 TA 0.32	A	0.228	2.505	8	1	1	9.673	0.30	14.94	C
			B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T5 120.10-100.10	0.31	0.47	A	0.243	2.459	8	1	1	10.815	0.30	15.06	C
			B	0.243	2.459		1	1	10.815			
			C	0.243	2.459		1	1	10.815			
T6 100.10-80.10	0.31	0.42	A	0.228	2.505	8	1	1	9.673	0.27	13.46	C
			B	0.228	2.505		1	1	9.673			
			C	0.228	2.505		1	1	9.673			
T7 80.10-60.10	0.31	0.50	A	0.228	2.504	7	1	1	9.682	0.25	12.54	C
			B	0.228	2.504		1	1	9.682			
			C	0.228	2.504		1	1	9.682			

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 28 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T8 60.10-40.10	0.31	0.51	A	0.208	2.569	6	1	1	9.315	0.23	11.30	C
			B	0.208	2.569		1	1	9.315			
			C	0.208	2.569		1	1	9.315			
T9 40.10-20.10	0.31	0.46	A	0.194	2.618	5	1	1	8.205	0.18	9.20	C
			B	0.194	2.618		1	1	8.205			
			C	0.194	2.618		1	1	8.205			
T10 20.10-4.85	0.19	0.35	A	0.196	2.609	5	1	1	6.344	0.13	8.38	C
			B	0.196	2.609		1	1	6.344			
			C	0.196	2.609		1	1	6.344			
T11 4.85-0.00	0.00	0.31	A	0.983	2.066	5	1	1	9.466	0.09	18.78	C
			B	0.983	2.066		1	1	9.466			
			C	0.983	2.066		1	1	9.466			
Sum Weight:	2.25	5.11								2.29		

Tower Forces - Service - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.02	0.49	A	0.21	2.562	9	0.8	1	7.107	0.15	9.99	C
			B	0.21	2.562		0.8	1	7.107			
			C	0.21	2.562		0.8	1	7.107			
T2 175.35-160.10	0.03	0.44	A	0.196	2.609	9	0.8	1	6.345	0.14	9.19	C
			B	0.196	2.609		0.8	1	6.345			
			C	0.196	2.609		0.8	1	6.345			
T3 160.10-140.10	0.16	0.42	A	0.228	2.505	9	0.8	1	9.673	0.24	12.05	C
			B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T4 140.10-120.10	0.31	0.42	A	0.228	2.505	8	0.8	1	9.673	0.30	14.94	C
		TA 0.32	B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T5 120.10-100.10	0.31	0.47	A	0.243	2.459	8	0.8	1	10.598	0.30	14.88	C
			B	0.243	2.459		0.8	1	10.598			
			C	0.243	2.459		0.8	1	10.598			
T6 100.10-80.10	0.31	0.42	A	0.228	2.505	8	0.8	1	9.673	0.27	13.46	C
			B	0.228	2.505		0.8	1	9.673			
			C	0.228	2.505		0.8	1	9.673			
T7 80.10-60.10	0.31	0.50	A	0.228	2.504	7	0.8	1	9.682	0.25	12.54	C
			B	0.228	2.504		0.8	1	9.682			
			C	0.228	2.504		0.8	1	9.682			
T8 60.10-40.10	0.31	0.51	A	0.208	2.569	6	0.8	1	9.100	0.22	11.16	C
			B	0.208	2.569		0.8	1	9.100			
			C	0.208	2.569		0.8	1	9.100			
T9 40.10-20.10	0.31	0.46	A	0.194	2.618	5	0.8	1	8.205	0.18	9.20	C
			B	0.194	2.618		0.8	1	8.205			
			C	0.194	2.618		0.8	1	8.205			
T10 20.10-4.85	0.19	0.35	A	0.196	2.609	5	0.8	1	6.344	0.13	8.38	C
			B	0.196	2.609		0.8	1	6.344			
			C	0.196	2.609		0.8	1	6.344			
T11 4.85-0.00	0.00	0.31	A	0.983	2.066	5	0.8	1	8.075	0.08	16.02	C
			B	0.983	2.066		0.8	1	8.075			
			C	0.983	2.066		0.8	1	8.075			
Sum Weight:	2.25	5.11								2.26		

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 29 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C _F	q _z psf	D _F	D _R	A _E ft ²	F K	w plf	Ctrl. Face
T1 190.60-175.35	0.02	0.49	A	0.21	2.562	9	0.85	1	7.168	0.15	10.06	C
			B	0.21	2.562		0.85	1	7.168			
			C	0.21	2.562		0.85	1	7.168			
T2 175.35-160.10	0.03	0.44	A	0.196	2.609	9	0.85	1	6.345	0.14	9.19	C
			B	0.196	2.609		0.85	1	6.345			
			C	0.196	2.609		0.85	1	6.345			
T3 160.10-140.10	0.16	0.42	A	0.228	2.505	9	0.85	1	9.673	0.24	12.05	C
			B	0.228	2.505		0.85	1	9.673			
			C	0.228	2.505		0.85	1	9.673			
T4 140.10-120.10	0.31	0.42	A	0.228	2.505	8	0.85	1	9.673	0.30	14.94	C
		TA	B	0.228	2.505		0.85	1	9.673			
		C	0.228	2.505	0.85		1	9.673				
T5 120.10-100.10	0.31	0.47	A	0.243	2.459	8	0.85	1	10.652	0.30	14.92	C
			B	0.243	2.459		0.85	1	10.652			
			C	0.243	2.459		0.85	1	10.652			
T6 100.10-80.10	0.31	0.42	A	0.228	2.505	8	0.85	1	9.673	0.27	13.46	C
			B	0.228	2.505		0.85	1	9.673			
			C	0.228	2.505		0.85	1	9.673			
T7 80.10-60.10	0.31	0.50	A	0.228	2.504	7	0.85	1	9.682	0.25	12.54	C
			B	0.228	2.504		0.85	1	9.682			
			C	0.228	2.504		0.85	1	9.682			
T8 60.10-40.10	0.31	0.51	A	0.208	2.569	6	0.85	1	9.154	0.22	11.19	C
			B	0.208	2.569		0.85	1	9.154			
			C	0.208	2.569		0.85	1	9.154			
T9 40.10-20.10	0.31	0.46	A	0.194	2.618	5	0.85	1	8.205	0.18	9.20	C
			B	0.194	2.618		0.85	1	8.205			
			C	0.194	2.618		0.85	1	8.205			
T10 20.10-4.85	0.19	0.35	A	0.196	2.609	5	0.85	1	6.344	0.13	8.38	C
			B	0.196	2.609		0.85	1	6.344			
			C	0.196	2.609		0.85	1	6.344			
T11 4.85-0.00	0.00	0.31	A	0.983	2.066	5	0.85	1	8.423	0.08	16.71	C
			B	0.983	2.066		0.85	1	8.423			
			C	0.983	2.066		0.85	1	8.423			
Sum Weight:	2.25	5.11								2.27		

Force Totals (Does not include forces on guys)

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Torques kip-ft
Leg Weight	2.96			
Bracing Weight	2.14			
Total Member Self-Weight	5.11			
Guy Weight	1.13			
Total Weight	16.57			

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 30 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Torques kip-ft
Wind 0 deg - No Ice		-0.01	-19.64	-3.06
Wind 30 deg - No Ice		9.76	-16.93	-1.89
Wind 60 deg - No Ice		16.89	-9.75	-0.22
Wind 90 deg - No Ice		19.54	0.01	1.51
Wind 120 deg - No Ice		17.00	9.83	2.84
Wind 150 deg - No Ice		9.78	16.94	3.41
Wind 180 deg - No Ice		0.01	19.53	3.06
Wind 210 deg - No Ice		-9.76	16.93	1.89
Wind 240 deg - No Ice		-16.99	9.81	0.22
Wind 270 deg - No Ice		-19.54	-0.01	-1.51
Wind 300 deg - No Ice		-16.91	-9.78	-2.84
Wind 330 deg - No Ice		-9.78	-16.94	-3.41
Member Ice	9.42			
Guy Ice	4.63			
Total Weight Ice	43.87			
Wind 0 deg - Ice		-0.00	-5.07	-1.13
Wind 30 deg - Ice		2.52	-4.39	-0.71
Wind 60 deg - Ice		4.37	-2.53	-0.09
Wind 90 deg - Ice		5.05	0.00	0.55
Wind 120 deg - Ice		4.38	2.54	1.05
Wind 150 deg - Ice		2.53	4.39	1.26
Wind 180 deg - Ice		0.00	5.06	1.13
Wind 210 deg - Ice		-2.52	4.39	0.71
Wind 240 deg - Ice		-4.38	2.53	0.09
Wind 270 deg - Ice		-5.05	-0.00	-0.55
Wind 300 deg - Ice		-4.38	-2.53	-1.05
Wind 330 deg - Ice		-2.53	-4.39	-1.26
Total Weight	16.57			
Wind 0 deg - Service		-0.00	-4.52	-0.71
Wind 30 deg - Service		2.25	-3.90	-0.44
Wind 60 deg - Service		3.89	-2.25	-0.05
Wind 90 deg - Service		4.50	0.00	0.35
Wind 120 deg - Service		3.92	2.26	0.65
Wind 150 deg - Service		2.25	3.90	0.78
Wind 180 deg - Service		0.00	4.50	0.71
Wind 210 deg - Service		-2.25	3.90	0.44
Wind 240 deg - Service		-3.91	2.26	0.05
Wind 270 deg - Service		-4.50	-0.00	-0.35
Wind 300 deg - Service		-3.90	-2.25	-0.65
Wind 330 deg - Service		-2.25	-3.90	-0.78

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.0 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.0 Wind 60 deg - No Ice+1.0 Guy
5	1.2 Dead+1.0 Wind 90 deg - No Ice+1.0 Guy
6	1.2 Dead+1.0 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.0 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.0 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.0 Wind 210 deg - No Ice+1.0 Guy

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 31 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Comb. No.	Description
10	1.2 Dead+1.0 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.0 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.0 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.0 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	190.6 - 175.35	Leg	Max Tension	2	6.75	-0.02	-0.04
			Max. Compression	4	-21.73	0.06	-0.12
			Max. Mx	6	-12.40	0.91	0.19
			Max. My	2	-12.47	-0.24	-0.95
			Max. Vy	10	0.91	0.26	0.41
		Diagonal	Max. Vx	2	0.89	-0.54	0.01
			Max Tension	5	3.29	0.00	0.00
			Max. Compression	11	-3.30	0.00	0.00
			Max. Mx	17	-0.12	0.01	0.00
			Max. My	2	0.27	0.00	0.00
		Bottom Girt	Max. Vy	17	-0.01	0.00	0.00
			Max. Vx	2	-0.00	0.00	0.00
			Max Tension	4	0.35	0.00	0.00
			Max. Compression	10	-0.31	0.00	0.00
			Max. Mx	25	-0.02	0.01	0.00
		Guy A	Max. My	13	0.28	0.00	-0.00
			Max. Vy	25	0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
			Bottom Tension	7	13.45		
			Top Tension	7	13.57		
Top Cable Vert	7		12.15				
Top Cable Norm	7		6.03				
Top Cable Tan	7	0.00					
Bot Cable Vert	7	-11.91					

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 32 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T2	175.35 - 160.1	Guy B	Bot Cable Norm	7	6.25			
			Bot Cable Tan	7	0.15			
			Bottom Tension	11	13.58			
			Top Tension	11	13.71			
			Top Cable Vert	11	12.30			
			Top Cable Norm	11	6.05			
			Top Cable Tan	11	0.00			
			Bot Cable Vert	11	-12.05			
			Bot Cable Norm	11	6.27			
			Bot Cable Tan	11	0.16			
			Guy C	Bottom Tension	5	13.61		
				Top Tension	5	13.73		
				Top Cable Vert	5	12.34		
				Top Cable Norm	5	6.04		
		Top Cable Tan		5	0.00			
		Bot Cable Vert		5	-12.08			
		Bot Cable Norm		5	6.26			
		Bot Cable Tan		5	0.16			
		Top Guy Pull-Off		Max Tension	13	3.69	0.00	0.00
				Max. Compression	1	0.00	0.00	0.00
			Max. Mx	14	1.04	0.02	0.00	
			Max. My	2	2.84	0.00	0.00	
			Max. Vy	14	0.03	0.00	0.00	
			Max. Vx	2	0.00	0.00	0.00	
			Leg	Max Tension	2	6.75	-0.02	-0.08
				Max. Compression	4	-22.17	0.13	-0.13
				Max. Mx	5	-17.93	0.65	-0.18
				Max. My	8	-17.66	0.06	0.67
		Max. Vy		5	1.17	0.36	0.08	
		Max. Vx		2	-1.33	-0.04	-0.39	
		Diagonal		Max Tension	13	2.01	0.00	0.00
				Max. Compression	7	-2.07	0.00	0.00
				Max. Mx	17	0.39	0.01	0.00
				Max. My	26	-0.23	0.00	0.00
			Max. Vy	17	-0.01	0.00	0.00	
			Max. Vx	26	-0.00	0.00	0.00	
		Top Girt	Max Tension	11	0.29	0.00	0.00	
			Max. Compression	6	-0.26	0.00	0.00	
			Max. Mx	25	-0.02	0.01	0.00	
			Max. My	13	0.21	0.00	-0.00	
			Max. Vy	25	-0.01	0.00	0.00	
			Max. Vx	13	0.00	0.00	0.00	
Bottom Girt	Max Tension	7	0.96	0.00	0.00			
	Max. Compression	13	-0.96	0.00	0.00			
	Max. Mx	23	-0.01	0.01	0.00			
	Max. My	13	-0.96	0.00	-0.00			
	Max. Vy	23	-0.01	0.00	0.00			
	Max. Vx	13	0.00	0.00	0.00			
T3	160.1 - 140.1	Leg	Max Tension	8	7.96	-0.01	0.20	
			Max. Compression	6	-27.21	0.11	0.07	
			Max. Mx	11	-2.63	0.41	-0.07	
			Max. My	2	-1.12	-0.03	0.44	
			Max. Vy	5	2.83	-0.06	0.02	
			Max. Vx	13	-2.51	0.04	0.04	
		Diagonal	Max Tension	9	1.86	0.00	0.00	
			Max. Compression	9	-2.07	0.00	0.00	
			Max. Mx	17	0.28	0.01	0.00	
			Max. My	2	0.03	0.00	0.00	
			Max. Vy	17	0.01	0.00	0.00	
			Max. Vx	2	-0.00	0.00	0.00	
		Top Girt	Max Tension	6	0.57	0.00	0.00	

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 33 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
			Max. Compression	12	-0.36	0.00	0.00
			Max. Mx	23	0.21	0.01	0.00
			Max. My	13	0.10	0.00	-0.00
			Max. Vy	23	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
		Bottom Girt	Max Tension	8	2.53	0.00	0.00
			Max. Compression	6	-2.14	0.00	0.00
			Max. Mx	23	-0.38	0.01	0.00
			Max. My	13	0.24	0.00	-0.00
			Max. Vy	23	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
T4	140.1 - 120.1	Leg	Max Tension	8	7.96	-0.01	0.17
			Max. Compression	6	-29.08	0.11	0.06
			Max. Mx	5	-9.60	-2.29	-0.10
			Max. My	13	-9.74	1.03	2.01
			Max. Vy	5	3.78	-2.29	-0.10
			Max. Vx	13	-3.34	1.03	2.01
		Diagonal	Max Tension	7	1.01	0.00	0.00
			Max. Compression	8	-1.01	0.00	0.00
			Max. Mx	17	-0.38	0.01	0.00
			Max. My	26	-0.08	0.00	0.00
			Max. Vy	17	-0.01	0.00	0.00
			Max. Vx	26	-0.00	0.00	0.00
		Top Girt	Max Tension	8	2.50	0.00	0.00
			Max. Compression	10	-2.11	0.00	0.00
			Max. Mx	26	0.71	0.01	0.00
			Max. My	13	0.05	0.00	-0.00
			Max. Vy	26	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
		Bottom Girt	Max Tension	6	0.29	0.00	0.00
			Max. Compression	1	0.00	0.00	0.00
			Max. Mx	19	0.23	0.01	0.00
			Max. My	13	0.26	0.00	-0.00
			Max. Vy	19	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
		Guy A	Bottom Tension	7	10.60		
			Top Tension	7	10.67		
			Top Cable Vert	7	8.81		
			Top Cable Norm	7	6.02		
			Top Cable Tan	7	0.00		
			Bot Cable Vert	7	-8.65		
			Bot Cable Norm	7	6.13		
			Bot Cable Tan	7	0.10		
		Guy B	Bottom Tension	13	10.64		
			Top Tension	13	10.72		
			Top Cable Vert	13	8.91		
			Top Cable Norm	13	5.95		
			Top Cable Tan	13	0.00		
			Bot Cable Vert	13	-8.75		
			Bot Cable Norm	13	6.07		
			Bot Cable Tan	13	0.10		
		Guy C	Bottom Tension	5	10.36		
			Top Tension	5	10.43		
			Top Cable Vert	5	8.69		
			Top Cable Norm	5	5.77		
			Top Cable Tan	5	0.00		
			Bot Cable Vert	5	-8.53		
			Bot Cable Norm	5	5.88		
			Bot Cable Tan	5	0.10		
		Torque Arm Top	Max Tension	9	6.55	0.00	0.00
			Max. Compression	9	-3.21	0.00	0.00

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 34 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft	
T5	120.1 - 100.1	Leg	Max. Mx	3	0.06	-29.90	0.00	
			Max. My	2	-2.55	-23.90	-0.00	
			Max. Vy	3	8.57	-29.90	0.00	
			Max. Vx	2	-0.00	-23.90	-0.00	
			Max Tension	1	0.00	0.00	0.00	
			Max. Compression	2	-29.76	-0.04	0.06	
			Max. Mx	11	-17.84	0.23	0.02	
			Max. My	8	-16.29	0.04	-0.23	
			Max. Vy	11	0.68	0.23	0.02	
			Max. Vx	8	-0.68	0.04	-0.23	
		Diagonal	Max Tension	13	0.75	0.00	0.00	
			Max. Compression	2	-2.15	0.00	0.00	
			Max. Mx	25	0.16	0.01	0.00	
			Max. My	26	-0.25	0.00	0.00	
			Max. Vy	25	-0.01	0.00	0.00	
			Max. Vx	26	-0.00	0.00	0.00	
			Top Girt	Max Tension	6	0.29	0.00	0.00
				Max. Compression	1	0.00	0.00	0.00
				Max. Mx	19	0.23	0.01	0.00
				Max. My	13	0.23	0.00	-0.00
		Max. Vy		19	-0.01	0.00	0.00	
		Max. Vx		13	0.00	0.00	0.00	
		Bottom Girt	Max Tension	10	0.96	0.00	0.00	
			Max. Compression	1	0.00	0.00	0.00	
			Max. Mx	23	0.90	0.01	0.00	
			Max. My	13	0.90	0.00	-0.00	
			Max. Vy	23	-0.01	0.00	0.00	
			Max. Vx	13	0.00	0.00	0.00	
		Guy A	Bottom Tension	9	5.24			
			Top Tension	9	5.26			
			Top Cable Vert	9	4.35			
			Top Cable Norm	9	2.96			
			Top Cable Tan	9	0.00			
			Bot Cable Vert	9	-4.28			
			Bot Cable Norm	9	3.02			
			Bot Cable Tan	9	0.04			
			Guy B	Bottom Tension	11	5.42		
				Top Tension	11	5.45		
		Top Cable Vert		11	4.54			
		Top Cable Norm		11	3.02			
		Top Cable Tan		11	0.00			
		Bot Cable Vert		11	-4.47			
		Guy C	Bot Cable Norm	11	3.07			
Bot Cable Tan	11		0.05					
Bottom Tension	5		5.41					
Top Tension	5		5.43					
Top Cable Vert	5		4.48					
Top Cable Norm	5		3.07					
Top Guy Pull-Off	Top Cable Tan	5	0.00					
	Bot Cable Vert	5	-4.41					
	Bot Cable Norm	5	3.13					
	Bot Cable Tan	5	0.05					
	Max Tension	2	2.67	0.00	0.00			
	Max. Compression	1	0.00	0.00	0.00			
	Max. Mx	26	1.74	0.02	0.00			
	Max. My	13	2.24	0.00	-0.00			
	Max. Vy	26	-0.02	0.00	0.00			
	Max. Vx	13	0.00	0.00	0.00			
T6	100.1 - 80.1	Leg	Max Tension	1	0.00	0.00	0.00	
			Max. Compression	2	-29.76	0.05	-0.01	
			Max. Mx	11	-19.87	-0.27	-0.06	

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 35 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft		
T7	80.1 - 60.1	Diagonal	Max. My	8	-16.29	-0.04	0.27		
			Max. Vy	11	0.68	0.15	0.01		
			Max. Vx	8	-0.68	0.03	-0.15		
			Max Tension	11	0.60	0.00	0.00		
			Max. Compression	2	-0.92	0.00	0.00		
			Max. Mx	25	-0.32	0.01	0.00		
			Max. My	26	-0.24	0.00	0.00		
			Max. Vy	25	-0.01	0.00	0.00		
			Max. Vx	26	0.00	0.00	0.00		
			Max Tension	5	0.60	0.00	0.00		
			Max. Compression	1	0.00	0.00	0.00		
			Max. Mx	23	0.34	0.01	0.00		
		Top Girt			Max. My	13	0.42	0.00	-0.00
					Max. Vy	23	-0.01	0.00	0.00
					Max. Vx	13	0.00	0.00	0.00
					Max Tension	6	0.31	0.00	0.00
					Max. Compression	1	0.00	0.00	0.00
					Max. Mx	17	0.27	0.01	0.00
					Max. My	13	0.29	0.00	-0.00
					Max. Vy	17	-0.01	0.00	0.00
					Max. Vx	13	0.00	0.00	0.00
					Max Tension	1	0.00	0.00	0.00
					Max. Compression	2	-31.01	0.07	-0.02
					Bottom Girt			Max. Mx	5
		Max. My	8	-17.09				-0.02	0.23
		Max. Vy	11	-0.50				-0.06	-0.07
		Max. Vx	2	-0.51				0.07	-0.02
		Max Tension	3	0.52				0.00	0.00
		Max. Compression	3	-0.80				0.00	0.00
		Max. Mx	24	0.27				0.01	0.00
		Max. My	26	-0.38				0.00	0.00
		Max. Vy	24	0.01				0.00	0.00
		Max. Vx	26	-0.00				0.00	0.00
		Max Tension	15	0.24				0.00	0.00
		Max. Compression	1	0.00				0.00	0.00
		Top Girt			Max. Mx	17	0.19	0.01	0.00
					Max. My	13	0.22	0.00	-0.00
					Max. Vy	17	-0.01	0.00	0.00
					Max. Vx	13	0.00	0.00	0.00
					Max Tension	7	0.39	0.00	0.00
					Max. Compression	1	0.00	0.00	0.00
					Max. Mx	19	0.17	0.01	0.00
Max. My	13				0.30	0.00	-0.00		
Max. Vy	19				-0.01	0.00	0.00		
Max. Vx	13				0.00	0.00	0.00		
Max Tension	1				0.00	0.00	0.00		
Max. Compression	2				-37.74	-0.18	-0.18		
Diagonal			Max. Mx	6	-36.86	-0.37	0.01		
			Max. My	2	-36.31	0.07	0.39		
			Max. Vy	10	0.65	0.33	-0.23		
			Max. Vx	2	0.65	0.07	0.39		
			Max Tension	7	1.41	0.00	0.00		
			Max. Compression	13	-1.70	0.00	0.00		
			Max. Mx	24	0.32	0.01	0.00		
			Max. My	26	0.16	0.00	0.00		
			Max. Vy	24	-0.01	0.00	0.00		
			Max. Vx	26	-0.00	0.00	0.00		
			Max Tension	8	0.49	0.00	0.00		
			Max. Compression	2	-0.37	0.00	0.00		
Top Girt			Max. Mx	19	0.11	0.01	0.00		
			Max. My	13	0.41	0.00	-0.00		

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 36 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T9	40.1 - 20.1	Bottom Girt	Max. Vy	19	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
			Max Tension	13	0.67	0.00	0.00
			Max. Compression	7	-0.41	0.00	0.00
			Max. Mx	19	0.14	0.01	0.00
			Max. My	13	0.67	0.00	-0.00
		Guy A	Max. Vy	19	-0.01	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
			Bottom Tension	9	4.60		
			Top Tension	9	4.62		
			Top Cable Vert	9	2.42		
			Top Cable Norm	9	3.93		
		Guy B	Top Cable Tan	9	0.00		
			Bot Cable Vert	9	-2.39		
			Bot Cable Norm	9	3.94		
			Bot Cable Tan	9	0.02		
			Bottom Tension	11	4.68		
			Top Tension	11	4.69		
		Guy C	Top Cable Vert	11	2.48		
			Top Cable Norm	11	3.98		
			Top Cable Tan	11	0.00		
			Bot Cable Vert	11	-2.45		
			Bot Cable Norm	11	3.99		
			Bot Cable Tan	11	0.02		
		Top Guy Pull-Off	Bottom Tension	3	4.62		
			Top Tension	3	4.63		
			Top Cable Vert	3	2.44		
			Top Cable Norm	3	3.93		
			Top Cable Tan	3	0.00		
			Bot Cable Vert	3	-2.41		
		Leg	Bot Cable Norm	3	3.94		
			Bot Cable Tan	3	0.02		
			Max Tension	13	2.39	0.00	0.00
			Max. Compression	1	0.00	0.00	0.00
			Max. Mx	19	1.51	0.02	0.00
			Max. My	13	0.47	0.00	-0.00
			Max. Vy	19	-0.02	0.00	0.00
			Max. Vx	13	0.00	0.00	0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	2	-35.88	0.09	-0.08
			Max. Mx	6	-35.28	-0.30	-0.13
			Max. My	2	-35.87	0.08	0.32
Max. Vy	10		0.66	0.26	-0.21		
Max. Vx	2		0.66	0.08	0.32		
Max Tension	13		1.38	0.00	0.00		
Max. Compression	7		-1.57	0.00	0.00		
Diagonal	Max. Mx		24	-0.42	0.01	0.00	
	Max. My		26	-0.19	0.00	0.00	
	Max. Vy	24	0.01	0.00	0.00		
	Max. Vx	26	-0.00	0.00	0.00		
	Max Tension	7	0.57	0.00	0.00		
	Max. Compression	13	-0.44	0.00	0.00		
Top Girt	Max. Mx	19	0.05	0.01	0.00		
	Max. My	13	-0.44	0.00	-0.00		
	Max. Vy	19	-0.01	0.00	0.00		
	Max. Vx	13	0.00	0.00	0.00		
	Max Tension	13	0.40	0.00	0.00		
	Max. Compression	7	-0.29	0.00	0.00		
Bottom Girt	Max. Mx	14	0.07	0.01	0.00		
	Max. My	13	0.40	0.00	-0.00		
	Max. Vy	14	-0.01	0.00	0.00		

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 37 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T10	20.1 - 4.854	Leg	Max. Vx	13	0.00	0.00	0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	2	-29.12	0.04	0.00
			Max. Mx	6	-27.15	1.08	0.39
			Max. My	10	-27.47	-0.09	-1.13
			Max. Vy	6	5.59	-0.89	0.74
		Diagonal	Max. Vx	6	6.41	-0.18	-1.12
			Max Tension	13	0.88	0.00	0.00
			Max. Compression	7	-1.05	0.00	0.00
			Max. Mx	16	0.23	0.01	0.00
			Max. My	26	0.00	0.00	0.00
			Max. Vy	16	-0.01	0.00	0.00
		Top Girt	Max. Vx	26	-0.00	0.00	0.00
			Max Tension	7	0.41	0.00	0.00
			Max. Compression	13	-0.27	0.00	0.00
			Max. Mx	14	0.06	0.01	0.00
			Max. My	13	-0.27	0.00	-0.00
			Max. Vy	14	-0.01	0.00	0.00
		Bottom Girt	Max. Vx	13	0.00	0.00	0.00
			Max Tension	2	3.73	0.00	0.00
			Max. Compression	1	0.00	0.00	0.00
Max. Mx	23		3.39	0.01	0.00		
Max. My	13		3.47	0.00	-0.00		
Max. Vy	23		-0.01	0.00	0.00		
T11	4.854 - 0	Leg	Max. Vx	13	0.00	0.00	0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	2	-29.94	0.05	-0.30
			Max. Mx	2	-27.81	-2.27	-0.11
			Max. My	13	-27.10	-0.51	-0.84
			Max. Vy	2	4.69	-2.27	-0.11
		Top Girt	Max. Vx	13	1.73	0.48	0.40
			Max Tension	2	2.91	-1.77	-0.01
			Max. Compression	1	0.00	0.00	0.00
			Max. Mx	2	2.89	-1.81	-0.01
			Max. My	13	2.60	-1.67	-0.01
			Max. Vy	13	0.36	-1.77	-0.01
		Bottom Girt	Max. Vx	26	0.01	-1.52	-0.01
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	2	-0.84	0.46	0.01
			Max. Mx	13	-0.79	-1.45	-0.01
			Max. My	13	-0.74	-1.43	-0.01
			Max. Vy	13	4.48	-1.45	-0.01
		Mid Girt	Max. Vx	13	0.06	-1.43	-0.01
			Max Tension	20	0.08	0.00	0.00
			Max. Compression	6	-0.16	0.00	0.00
Max. Mx	19		0.08	0.01	0.00		
Max. My	15		0.08	0.00	0.00		
Max. Vy	21		-0.03	0.00	0.00		
		Max. Vx	15	-0.01	0.00	0.00	

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Mast	Max. Vert	2	82.72	-0.02	-0.22
	Max. H _x	7	75.79	0.18	-0.09

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	38 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Guy C @ 99 ft Elev -5.17 ft Azimuth 240 deg	Max. H _z	5	76.01	0.03	0.21
	Max. M _x	1	0.00	-0.01	0.01
	Max. M _z	1	0.00	-0.01	0.01
	Max. Torsion	13	1.16	0.13	-0.16
	Min. Vert	1	45.38	-0.01	0.01
	Min. H _x	9	75.81	-0.21	-0.09
	Min. H _z	8	63.18	-0.01	-0.25
	Min. M _x	1	0.00	-0.01	0.01
	Min. M _z	1	0.00	-0.01	0.01
	Min. Torsion	7	-1.27	0.18	-0.09
Guy B @ 99.25 ft Elev -4.67 ft Azimuth 120 deg	Max. Vert	10	-1.19	-0.39	0.22
	Max. H _x	10	-1.19	-0.39	0.22
	Max. H _z	3	-29.00	-15.36	9.27
	Min. Vert	5	-29.08	-15.74	8.69
	Min. H _x	5	-29.08	-15.74	8.69
Guy A @ 96.5 ft Elev 2.46 ft Azimuth 0 deg	Min. H _z	9	-1.61	-0.72	0.21
	Max. Vert	6	-1.18	0.38	0.22
	Max. H _x	11	-29.01	15.80	8.72
	Max. H _z	13	-28.96	15.43	9.29
	Min. Vert	11	-29.01	15.80	8.72
Guy C @ 71.5 ft Elev 2.125 ft Azimuth 240 deg	Min. H _x	6	-1.18	0.38	0.22
	Min. H _z	7	-1.60	0.72	0.21
	Max. Vert	2	-1.08	-0.00	-0.41
	Max. H _x	10	-24.68	0.53	-15.52
	Max. H _z	2	-1.08	-0.00	-0.41
	Min. Vert	7	-28.67	-0.33	-18.12
Guy B @ 68.25 ft Elev 3.96 ft Azimuth 120 deg	Min. H _x	6	-24.71	-0.52	-15.54
	Min. H _z	7	-28.67	-0.33	-18.12
	Max. Vert	10	-0.16	-0.07	0.04
	Max. H _x	10	-0.16	-0.07	0.04
	Max. H _z	3	-6.81	-6.09	3.59
	Min. Vert	3	-6.81	-6.09	3.59
Guy A @ 70.5 ft Elev 3 ft Azimuth 0 deg	Min. H _x	5	-6.81	-6.14	3.47
	Min. H _z	10	-0.16	-0.07	0.04
	Max. Vert	6	-0.17	0.07	0.04
	Max. H _x	11	-6.91	6.15	3.48
	Max. H _z	13	-6.89	6.07	3.58
	Min. Vert	11	-6.91	6.15	3.48
Guy C @ 99 ft Elev -5.17 ft Azimuth 240 deg	Min. H _x	6	-0.17	0.07	0.04
	Min. H _z	6	-0.17	0.07	0.04
	Max. Vert	2	-0.16	-0.00	-0.08
	Max. H _x	10	-5.72	0.11	-5.96
	Max. H _z	2	-0.16	-0.00	-0.08
	Min. Vert	9	-6.67	0.07	-6.96
Guy B @ 99.25 ft Elev -4.67 ft Azimuth 120 deg	Min. H _x	5	-3.52	-0.11	-3.65
	Min. H _z	9	-6.67	0.07	-6.96

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 39 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ

Tower Mast Reaction Summary

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	45.38	0.01	-0.01	0.00	0.00	0.03
1.2 Dead+1.0 Wind 0 deg - No Ice+1.0 Guy	82.72	0.02	0.22	0.00	0.00	-0.98
1.2 Dead+1.0 Wind 30 deg - No Ice+1.0 Guy	76.07	0.17	0.15	0.00	0.00	-0.56
1.2 Dead+1.0 Wind 60 deg - No Ice+1.0 Guy	62.98	0.21	-0.13	0.00	0.00	0.02
1.2 Dead+1.0 Wind 90 deg - No Ice+1.0 Guy	76.01	-0.03	-0.21	0.00	0.00	0.64
1.2 Dead+1.0 Wind 120 deg - No Ice+1.0 Guy	82.40	-0.15	-0.08	0.00	0.00	1.09
1.2 Dead+1.0 Wind 150 deg - No Ice+1.0 Guy	75.79	-0.18	0.09	0.00	0.00	1.27
1.2 Dead+1.0 Wind 180 deg - No Ice+1.0 Guy	63.18	0.01	0.25	0.00	0.00	1.19
1.2 Dead+1.0 Wind 210 deg - No Ice+1.0 Guy	75.81	0.21	0.09	0.00	0.00	0.66
1.2 Dead+1.0 Wind 240 deg - No Ice+1.0 Guy	82.41	0.20	-0.08	0.00	0.00	0.08
1.2 Dead+1.0 Wind 270 deg - No Ice+1.0 Guy	76.07	0.08	-0.20	0.00	0.00	-0.52
1.2 Dead+1.0 Wind 300 deg - No Ice+1.0 Guy	63.15	-0.16	-0.12	0.00	0.00	-1.10
1.2 Dead+1.0 Wind 330 deg - No Ice+1.0 Guy	76.11	-0.13	0.16	0.00	0.00	-1.16
1.2 Dead+1.0 Ice+1.0 Temp+Guy	79.11	0.05	-0.02	0.00	0.00	0.06
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.04	0.05	-0.10	0.00	0.00	-0.35
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.44	0.05	-0.08	0.00	0.00	-0.16
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.79	0.07	-0.04	0.00	0.00	0.04
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.42	0.10	-0.00	0.00	0.00	0.25
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.04	0.11	0.02	0.00	0.00	0.45
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.56	0.09	0.02	0.00	0.00	0.55
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.98	0.05	0.01	0.00	0.00	0.47
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.59	0.00	0.02	0.00	0.00	0.28
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.10	-0.02	0.02	0.00	0.00	0.08
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.52	-0.00	0.00	0.00	0.00	-0.12
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.89	0.03	-0.04	0.00	0.00	-0.33
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy	80.50	0.04	-0.08	0.00	0.00	-0.43
Dead+Wind 0 deg - Service+Guy	45.38	0.02	-0.12	0.00	0.00	-0.20
Dead+Wind 30 deg - Service+Guy	45.45	0.06	-0.10	0.00	0.00	-0.09
Dead+Wind 60 deg -	45.55	0.09	-0.06	0.00	0.00	0.03

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 40 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
Service+Guy						
Dead+Wind 90 deg -	45.55	0.11	-0.01	0.00	0.00	0.16
Service+Guy						
Dead+Wind 120 deg -	45.55	0.11	0.05	0.00	0.00	0.26
Service+Guy						
Dead+Wind 150 deg -	45.68	0.06	0.08	0.00	0.00	0.31
Service+Guy						
Dead+Wind 180 deg -	45.78	0.01	0.09	0.00	0.00	0.27
Service+Guy						
Dead+Wind 210 deg -	45.71	-0.04	0.08	0.00	0.00	0.16
Service+Guy						
Dead+Wind 240 deg -	45.60	-0.08	0.05	0.00	0.00	0.04
Service+Guy						
Dead+Wind 270 deg -	45.60	-0.08	-0.00	0.00	0.00	-0.09
Service+Guy						
Dead+Wind 300 deg -	45.60	-0.06	-0.05	0.00	0.00	-0.19
Service+Guy						
Dead+Wind 330 deg -	45.48	-0.03	-0.09	0.00	0.00	-0.24
Service+Guy						

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-16.57	0.00	0.00	16.57	-0.00	0.016%
2	-0.01	-19.72	-21.88	0.01	19.72	21.88	0.009%
3	10.88	-19.67	-18.87	-10.88	19.67	18.87	0.007%
4	18.84	-19.61	-10.87	-18.84	19.61	10.87	0.004%
5	21.79	-19.66	0.01	-21.78	19.66	-0.01	0.010%
6	18.94	-19.71	10.95	-18.94	19.71	-10.95	0.007%
7	10.90	-19.66	18.89	-10.90	19.66	-18.88	0.010%
8	0.01	-19.60	21.77	-0.01	19.60	-21.77	0.006%
9	-10.88	-19.66	18.87	10.88	19.66	-18.87	0.009%
10	-18.93	-19.71	10.93	18.93	19.71	-10.93	0.007%
11	-21.79	-19.66	-0.01	21.78	19.66	0.01	0.010%
12	-18.85	-19.61	-10.90	18.85	19.61	10.90	0.004%
13	-10.90	-19.67	-18.89	10.90	19.67	18.88	0.007%
14	0.00	-46.96	0.00	-0.00	46.96	-0.00	0.004%
15	-0.00	-47.01	-6.99	0.00	47.01	6.99	0.003%
16	3.48	-46.97	-6.05	-3.48	46.97	6.05	0.003%
17	6.04	-46.92	-3.49	-6.04	46.92	3.49	0.002%
18	6.97	-46.96	0.00	-6.97	46.96	-0.00	0.003%
19	6.05	-47.01	3.50	-6.04	47.01	-3.50	0.003%
20	3.49	-46.96	6.05	-3.49	46.96	-6.05	0.002%
21	0.00	-46.91	6.98	-0.00	46.91	-6.98	0.005%
22	-3.48	-46.96	6.05	3.48	46.96	-6.05	0.003%
23	-6.04	-47.01	3.49	6.04	47.01	-3.49	0.003%
24	-6.97	-46.96	-0.00	6.97	46.96	0.00	0.003%
25	-6.04	-46.91	-3.49	6.04	46.91	3.49	0.002%
26	-3.49	-46.96	-6.05	3.49	46.96	6.05	0.003%
27	-0.00	-16.59	-5.04	0.00	16.59	5.04	0.012%
28	2.51	-16.57	-4.35	-2.51	16.57	4.35	0.006%
29	4.34	-16.56	-2.51	-4.34	16.56	2.50	0.008%
30	5.02	-16.57	0.00	-5.02	16.57	-0.00	0.006%
31	4.36	-16.59	2.52	-4.36	16.59	-2.52	0.012%
32	2.51	-16.57	4.35	-2.51	16.57	-4.35	0.006%
33	0.00	-16.56	5.02	-0.00	16.56	-5.02	0.007%

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 41 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
34	-2.51	-16.57	4.35	2.51	16.57	-4.35	0.006%
35	-4.36	-16.58	2.52	4.36	16.58	-2.52	0.012%
36	-5.02	-16.57	-0.00	5.02	16.57	0.00	0.007%
37	-4.34	-16.56	-2.51	4.34	16.56	2.51	0.008%
38	-2.51	-16.57	-4.35	2.51	16.57	4.35	0.006%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	9	0.0000001	0.00009662
2	Yes	22	0.00007849	0.00007715
3	Yes	22	0.00006699	0.00006007
4	Yes	15	0.00000001	0.00005020
5	Yes	21	0.00009935	0.00009041
6	Yes	22	0.00006470	0.00006378
7	Yes	21	0.00009949	0.00008695
8	Yes	14	0.00000001	0.00008303
9	Yes	21	0.00009544	0.00008455
10	Yes	22	0.00006209	0.00006129
11	Yes	21	0.00009528	0.00008668
12	Yes	15	0.00000001	0.00007484
13	Yes	22	0.00006696	0.00005966
14	Yes	9	0.00000001	0.00004634
15	Yes	14	0.00000001	0.00006626
16	Yes	14	0.00000001	0.00005124
17	Yes	14	0.00000001	0.00003022
18	Yes	14	0.00000001	0.00004522
19	Yes	14	0.00000001	0.00005815
20	Yes	14	0.00000001	0.00004355
21	Yes	13	0.00000001	0.00006198
22	Yes	14	0.00000001	0.00005166
23	Yes	14	0.00000001	0.00006796
24	Yes	14	0.00000001	0.00005214
25	Yes	14	0.00000001	0.00003058
26	Yes	14	0.00000001	0.00005038
27	Yes	9	0.00000001	0.00007995
28	Yes	10	0.00000001	0.00005306
29	Yes	10	0.00000001	0.00006842
30	Yes	10	0.00000001	0.00005655
31	Yes	9	0.00000001	0.00008530
32	Yes	10	0.00000001	0.00004992
33	Yes	10	0.00000001	0.00005794
34	Yes	10	0.00000001	0.00004913
35	Yes	9	0.00000001	0.00007498
36	Yes	10	0.00000001	0.00005428
37	Yes	10	0.00000001	0.00006595
38	Yes	10	0.00000001	0.00005187

Maximum Tower Deflections - Service Wind

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 42 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	190.6 - 175.35	2.403	29	0.0504	0.0682
T2	175.35 - 160.1	2.237	29	0.0690	0.0692
T3	160.1 - 140.1	1.969	29	0.0894	0.0705
T4	140.1 - 120.1	1.549	37	0.0815	0.0719
T5	120.1 - 100.1	1.265	37	0.0633	0.1004
T6	100.1 - 80.1	1.030	37	0.0494	0.1241
T7	80.1 - 60.1	0.823	37	0.0550	0.1384
T8	60.1 - 40.1	0.576	37	0.0593	0.1426
T9	40.1 - 20.1	0.341	28	0.0464	0.1322
T10	20.1 - 4.854	0.177	28	0.0411	0.1111
T11	4.854 - 0	0.044	27	0.0426	0.0623

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
189.99	Guy	29	2.398	0.0511	0.0682	64368
187.00	JAHH-65B-R3B	29	2.369	0.0544	0.0683	64368
175.00	TPA65R-BU8DA	29	2.232	0.0695	0.0693	22673
168.25	4478 B14	29	2.126	0.0800	0.0702	25520
168.00	DC6-48-60-0-8C-EV	29	2.121	0.0803	0.0702	25708
161.00	DMP65R-BU8DA	29	1.988	0.0887	0.0706	33483
154.75	4449 B5/B12	29	1.854	0.0909	0.0698	108927
154.00	DC9-48-60-24-8C-EV	29	1.838	0.0908	0.0696	160369
140.00	APX16DWV-16DWVS-E-A20	37	1.547	0.0814	0.0720	22307
139.49	Guy	37	1.538	0.0809	0.0724	22221
102.62	Guy	37	1.057	0.0502	0.1217	75652
45.03	Guy	28	0.392	0.0498	0.1368	54225

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	190.6 - 175.35	25.020	2	0.7392	0.3989
T2	175.35 - 160.1	22.636	2	0.8192	0.3955
T3	160.1 - 140.1	19.812	2	0.9051	0.3940
T4	140.1 - 120.1	15.846	2	0.8473	0.4033
T5	120.1 - 100.1	12.575	2	0.7327	0.4932
T6	100.1 - 80.1	9.723	2	0.6181	0.5762
T7	80.1 - 60.1	7.291	2	0.5645	0.6247
T8	60.1 - 40.1	4.981	2	0.5219	0.6307
T9	40.1 - 20.1	2.959	2	0.4134	0.5671
T10	20.1 - 4.854	1.450	2	0.3544	0.4526
T11	4.854 - 0	0.355	2	0.3485	0.2794

Critical Deflections and Radius of Curvature - Design Wind

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 43 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
189.99	Guy	2	24.928	0.7421	0.3987	14676
187.00	JAHH-65B-R3B	2	24.479	0.7561	0.3977	14676
175.00	TPA65R-BU8DA	2	22.577	0.8214	0.3955	5196
168.25	4478 B14	2	21.377	0.8667	0.3959	5976
168.00	DC6-48-60-0-8C-EV	2	21.331	0.8683	0.3960	6024
161.00	DMP65R-BU8DA	2	19.990	0.9027	0.3945	8103
154.75	4449 B5/B12	2	18.736	0.9072	0.3895	30836
154.00	DC9-48-60-24-8C-EV	2	18.583	0.9061	0.3888	50971
140.00	APX16DWV-16DWVS-E-A20	2	15.828	0.8468	0.4036	4595
139.49	Guy	2	15.734	0.8439	0.4051	4573
102.62	Guy	2	10.059	0.6298	0.5678	8992
45.03	Guy	2	3.409	0.4516	0.5948	7902

Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	190.6	Leg	A325N	0.7500	4	1.81	30.10	0.060 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	3.29	5.92	0.555 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.38	5.92	0.064 ✓	1	Member Bearing
T2	175.35	Leg	A325N	0.7500	4	1.42	30.10	0.047 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	2.01	5.92	0.340 ✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	0.38	4.17	0.092 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.96	5.92	0.162 ✓	1	Member Bearing
T3	160.1	Leg	A325N	0.7500	4	2.27	30.10	0.075 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	1.86	5.92	0.314 ✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	0.57	4.17	0.138 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	2.53	5.92	0.427 ✓	1	Member Bearing
T4	140.1	Leg	A325N	0.7500	4	2.22	30.10	0.074 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	1.01	5.92	0.170 ✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	2.50	4.17	0.599 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.50	5.92	0.085 ✓	1	Member Bearing
T5	120.1	Leg	A325N	0.7500	4	2.48	30.10	0.082 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	2.15	7.02	0.306 ✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	0.52	4.17	0.124 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.96	5.92	0.163 ✓	1	Member Bearing
T6	100.1	Leg	A325N	0.7500	4	2.23	30.10	0.074 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	0.92	7.02	0.131 ✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	0.60	4.17	0.144 ✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.52	5.92	0.087 ✓	1	Member Bearing
T7	80.1	Leg	A325N	0.7500	4	2.58	30.10	0.086 ✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	0.80	7.02	0.114 ✓	1	Member Bearing

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	21140.00 - CT1166	Page	44 of 55	
	Project	190-ft Guyed Tower - 812 Providence Pike, Danielson, CT		Date	14:02:32 02/20/23
	Client	AT&T		Designed by	TJL

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria	
T8	60.1	Top Girt	A325X	0.5000	1	0.54	4.17	0.129	✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.54	5.92	0.091	✓	1	Member Bearing
		Leg	A325N	0.7500	4	2.99	30.10	0.099	✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	1.70	7.02	0.242	✓	1	Member Bearing
T9	40.1	Top Girt	A325X	0.5000	1	0.65	4.17	0.157	✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.67	5.92	0.114	✓	1	Member Bearing
		Leg	A325N	0.7500	4	2.43	30.10	0.081	✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	1.38	5.92	0.233	✓	1	Member Bearing
T10	20.1	Top Girt	A325X	0.5000	1	0.62	4.17	0.149	✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	0.62	5.92	0.105	✓	1	Member Bearing
		Leg	A325N	0.7500	4	2.30	30.10	0.076	✓	1	Bolt Tension
		Diagonal	A325X	0.5000	1	1.05	7.02	0.149	✓	1	Member Bearing
		Top Girt	A325X	0.5000	1	0.50	4.17	0.121	✓	1	Member Bearing
		Bottom Girt	A325X	0.5000	1	3.73	5.92	0.631	✓	1	Member Bearing

Guy Design Data

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual T_u K	Allowable ϕT_n K	Required S.F.	Actual S.F.
T1	189.99 (A) (450)	9/16 EHS	3.50	35.00	13.57	21.00	1.000	1.548 ✓
	189.99 (B) (449)	9/16 EHS	3.50	35.00	13.71	21.00	1.000	1.532 ✓
	189.99 (C) (448)	9/16 EHS	3.50	35.00	13.73	21.00	1.000	1.529 ✓
T4	139.49 (A) (459)	1/2 EHS	2.69	26.90	10.34	16.14	1.000	1.561 ✓
	139.49 (A) (460)	1/2 EHS	2.69	26.90	10.67	16.14	1.000	1.512 ✓
	139.49 (B) (455)	1/2 EHS	2.69	26.90	10.72	16.14	1.000	1.506 ✓
	139.49 (B) (456)	1/2 EHS	2.69	26.90	10.42	16.14	1.000	1.549 ✓
	139.49 (C) (451)	1/2 EHS	2.69	26.90	10.43	16.14	1.000	1.547 ✓
	139.49 (C) (452)	1/2 EHS	2.69	26.90	10.37	16.14	1.000	1.557 ✓
T5	102.62 (A) (468)	3/8 EHS	1.54	15.40	5.26	9.24	1.000	1.755 ✓
	102.62 (B) (467)	3/8 EHS	1.54	15.40	5.45	9.24	1.000	1.696 ✓
	102.62 (C) (463)	3/8 EHS	1.54	15.40	5.43	9.24	1.000	1.701 ✓
T8	45.03 (A) (474)	3/8 EHS	1.54	15.40	4.62	9.24	1.000	2.002 ✓
	45.03 (B) (473)	3/8 EHS	1.54	15.40	4.69	9.24	1.000	1.969 ✓

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 45 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual T_u K	Allowable ϕT_n K	Required S.F.	Actual S.F.
	45.03 (C) (469)	3/8 EHS	1.54	15.40	4.63	9.24	1.000	1.995 ✓

Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	Mast Stability Index	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN 2.5 X-STR	15.25	2.42	62.9 K=2.00	2.2535	1.00	-21.73	75.97	0.286 ¹ ✓
T2	175.35 - 160.1	ROHN 2.5 X-STR	15.25	2.42	62.9 K=2.00	2.2535	1.00	-22.17	75.97	0.292 ¹ ✓
T3	160.1 - 140.1	ROHN 2 STD	20.00	2.41	36.7 K=1.00	1.0745	1.00	-27.21	43.81	0.621 ¹ ✓
T4	140.1 - 120.1	ROHN 2 STD	20.00	2.41	36.7 K=1.00	1.0745	1.00	-29.08	43.81	0.664 ¹ ✓
T5	120.1 - 100.1	ROHN 2 STD	20.00	2.41	36.7 K=1.00	1.0745	1.00	-29.76	43.81	0.679 ¹ ✓
T6	100.1 - 80.1	ROHN 2 STD	20.00	2.41	36.7 K=1.00	1.0745	0.98	-29.76	43.14	0.690 ¹ ✓
T7	80.1 - 60.1	ROHN 2 EH	20.00	2.41	37.6 K=1.00	1.4807	0.99	-31.01	59.31	0.523 ¹ ✓
T8	60.1 - 40.1	ROHN 2.5 STD	20.00	2.41	61.0 K=2.00	1.7040	1.00	-37.74	58.41	0.646 ¹ ✓
T9	40.1 - 20.1	ROHN 2.5 STD	20.00	2.41	61.0 K=2.00	1.7040	1.00	-35.88	58.41	0.614 ¹ ✓
T10	20.1 - 4.854	ROHN 2.5 STD	15.25	2.42	61.3 K=2.00	1.7040	1.00	-29.12	58.27	0.500 ¹ ✓
T11	4.854 - 0	ROHN 2.5 X-STR	5.25	1.27	16.5 K=1.00	2.2535	0.96	-29.94	95.65	0.313 ¹ ✓

¹ $P_u / \phi P_n$ controls

Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN TS1.5x16 ga	4.22	3.93	92.4 K=1.00	0.2627	-3.30	5.88	0.562 ¹ ✓
T2	175.35 - 160.1	ROHN TS1.5x16 ga	4.22	3.93	92.4 K=1.00	0.2627	-2.07	5.88	0.353 ¹ ✓
T3	160.1 - 140.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	-2.07	5.81	0.356 ¹ ✓

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 46 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T4	140.1 - 120.1	ROHN TS1.5x16 ga	4.21	3.97	K=1.00 93.4	0.2627	-1.01	5.81	0.174 ¹ ✓
T5	120.1 - 100.1	ROHN TS1.5x16 ga	4.21	3.97	K=1.00 93.4	0.2627	-2.15	5.81	0.370 ¹ ✓
T6	100.1 - 80.1	ROHN TS1.5x16 ga	4.21	3.97	K=1.00 93.4	0.2627	-0.92	5.81	0.158 ¹ ✓
T7	80.1 - 60.1	ROHN TS1.5x16 ga	4.21	3.97	K=1.00 93.4	0.2627	-0.80	5.81	0.138 ¹ ✓
T8	60.1 - 40.1	ROHN TS1.5x16 ga	4.21	3.92	K=1.00 92.2	0.2627	-1.70	5.89	0.288 ¹ ✓
T9	40.1 - 20.1	ROHN TS1.5x16 ga	4.21	3.92	K=1.00 92.2	0.2627	-1.57	5.89	0.266 ¹ ✓
T10	20.1 - 4.854	ROHN TS1.5x16 ga	4.22	3.93	K=1.00 92.4	0.2627	-1.05	5.88	0.178 ¹ ✓

¹ P_u / φP_n controls

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	175.35 - 160.1	ROHN TS1.5x16 ga	3.46	3.22	K=1.00 75.7	0.2627	-0.38	6.99	0.055 ¹ ✓
T3	160.1 - 140.1	ROHN TS1.5x16 ga	3.46	3.26	K=1.00 76.7	0.2627	-0.47	6.92	0.068 ¹ ✓
T4	140.1 - 120.1	ROHN TS1.5x16 ga	3.46	3.26	K=1.00 76.7	0.2627	-2.11	6.92	0.305 ¹ ✓
T5	120.1 - 100.1	ROHN TS1.5x16 ga	3.46	3.26	K=1.00 76.7	0.2627	-0.52	6.92	0.074 ¹ ✓
T6	100.1 - 80.1	ROHN TS1.5x16 ga	3.46	3.26	K=1.00 76.7	0.2627	-0.52	6.92	0.074 ¹ ✓
T7	80.1 - 60.1	ROHN TS1.5x16 ga	3.46	3.26	K=1.00 76.7	0.2627	-0.54	6.92	0.078 ¹ ✓
T8	60.1 - 40.1	ROHN TS1.5x16 ga	3.46	3.22	K=1.00 75.7	0.2627	-0.65	6.99	0.094 ¹ ✓
T9	40.1 - 20.1	ROHN TS1.5x16 ga	3.46	3.22	K=1.00 75.7	0.2627	-0.62	6.99	0.089 ¹ ✓
T10	20.1 - 4.854	ROHN TS1.5x16 ga	3.46	3.22	K=1.00 75.7	0.2627	-0.50	6.99	0.072 ¹ ✓
T11	4.854 - 0	14x3/16	2.98	2.74	K=1.00 608.2	2.6250	-0.55	1.60	0.343 ¹ ✓

¹ P_u / φP_n controls

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 47 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	KL/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN TS1.5x16 ga	3.46	3.22	75.7 K=1.00	0.2627	-0.38	6.99	0.054 ¹ ✓
T2	175.35 - 160.1	ROHN TS1.5x16 ga	3.46	3.22	75.7 K=1.00	0.2627	-0.96	6.99	0.137 ¹ ✓
T3	160.1 - 140.1	ROHN TS1.5x16 ga	3.46	3.26	76.7 K=1.00	0.2627	-2.14	6.92	0.310 ¹ ✓
T4	140.1 - 120.1	ROHN TS1.5x16 ga	3.46	3.26	76.7 K=1.00	0.2627	-0.50	6.92	0.073 ¹ ✓
T5	120.1 - 100.1	ROHN TS1.5x16 ga	3.46	3.26	76.7 K=1.00	0.2627	-0.52	6.92	0.074 ¹ ✓
T6	100.1 - 80.1	ROHN TS1.5x16 ga	3.46	3.26	76.7 K=1.00	0.2627	-0.52	6.92	0.074 ¹ ✓
T7	80.1 - 60.1	ROHN TS1.5x16 ga	3.46	3.26	76.7 K=1.00	0.2627	-0.54	6.92	0.078 ¹ ✓
T8	60.1 - 40.1	ROHN TS1.5x16 ga	3.46	3.22	75.7 K=1.00	0.2627	-0.65	6.99	0.094 ¹ ✓
T9	40.1 - 20.1	ROHN TS1.5x16 ga	3.46	3.22	75.7 K=1.00	0.2627	-0.62	6.99	0.089 ¹ ✓
T10	20.1 - 4.854	ROHN TS1.5x16 ga	3.46	3.22	75.7 K=1.00	0.2627	-0.50	6.99	0.072 ¹ ✓
T11	4.854 - 0	14x3/16	0.47	0.24	52.2 K=1.00	2.6250	-0.84	73.69	0.011 ¹ ✓

¹ P_u / φP_n controls

Mid Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	KL/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T11	4.854 - 0	14x3/16	1.31	1.07	237.5 K=1.00	2.6250	-0.16	10.51	0.015 ¹ ✓
KL/R > 200 (C) - 443									

¹ P_u / φP_n controls

Torque-Arm Top Design Data

Section No.	Elevation ft	Size	L ft	L _u ft	KL/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T4	140.1 - 120.1 (453)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.17	122.43	0.026
T4	140.1 - 120.1 (454)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.21	122.43	0.026

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 48 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T4	140.1 - 120.1 (457)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.14	122.43	0.026
T4	140.1 - 120.1 (458)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.16	122.43	0.026
T4	140.1 - 120.1 (461)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.00	122.43	0.025
T4	140.1 - 120.1 (462)	C10x15.3	3.50	3.40	57.2 K=1.00	4.4900	-3.04	122.43	0.025

Torque-Arm Top Bending Design Data

Section No.	Elevation ft	Size	M _{ux} kip-ft	φM _{ux} kip-ft	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	M _{uy} kip-ft	φM _{uy} kip-ft	Ratio $\frac{M_{uy}}{\phi M_{uy}}$
T4	140.1 - 120.1 (453)	C10x15.3	-28.65	41.76	0.686	-0.00	4.70	0.000
T4	140.1 - 120.1 (454)	C10x15.3	-28.23	41.76	0.676	0.00	4.70	0.000
T4	140.1 - 120.1 (457)	C10x15.3	-28.62	41.76	0.685	0.00	4.70	0.000
T4	140.1 - 120.1 (458)	C10x15.3	-28.59	41.76	0.685	-0.00	4.70	0.000
T4	140.1 - 120.1 (461)	C10x15.3	-27.67	41.76	0.663	-0.00	4.70	0.000
T4	140.1 - 120.1 (462)	C10x15.3	-27.39	41.76	0.656	0.00	4.70	0.000

Torque-Arm Top Interaction Design Data

Section No.	Elevation ft	Size	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	Ratio $\frac{M_{uy}}{\phi M_{uy}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
T4	140.1 - 120.1 (453)	C10x15.3	0.026	0.686	0.000	0.699	1.000	4.8.1 ✓
T4	140.1 - 120.1 (454)	C10x15.3	0.026	0.676	0.000	0.689	1.000	4.8.1 ✓
T4	140.1 - 120.1 (457)	C10x15.3	0.026	0.685	0.000	0.698	1.000	4.8.1 ✓
T4	140.1 - 120.1 (458)	C10x15.3	0.026	0.685	0.000	0.698	1.000	4.8.1 ✓
T4	140.1 - 120.1 (461)	C10x15.3	0.025	0.663	0.000	0.675	1.000	4.8.1 ✓
T4	140.1 - 120.1 (462)	C10x15.3	0.025	0.656	0.000	0.668	1.000	4.8.1 ✓

Tension Checks

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 49 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN 2.5 X-STR	15.25	2.42	31.4	2.2535	6.75	101.41	0.067 ¹
T2	175.35 - 160.1	ROHN 2.5 X-STR	15.25	2.42	31.4	2.2535	6.75	101.41	0.067 ¹
T3	160.1 - 140.1	ROHN 2 STD	20.00	2.41	36.7	1.0745	7.96	48.35	0.165 ¹
T4	140.1 - 120.1	ROHN 2 STD	20.00	2.41	36.7	1.0745	7.96	48.35	0.165 ¹

¹ P_u / φP_n controls

Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN TS1.5x16 ga	4.22	3.93	92.4	0.2627	3.29	9.93	0.331 ¹
T2	175.35 - 160.1	ROHN TS1.5x16 ga	4.22	3.93	92.4	0.2627	2.01	9.93	0.202 ¹
T3	160.1 - 140.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	1.86	9.93	0.187 ¹
T4	140.1 - 120.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	1.01	9.93	0.101 ¹
T5	120.1 - 100.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	0.75	9.93	0.075 ¹
T6	100.1 - 80.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	0.60	9.93	0.060 ¹
T7	80.1 - 60.1	ROHN TS1.5x16 ga	4.21	3.97	93.4	0.2627	0.52	9.93	0.053 ¹
T8	60.1 - 40.1	ROHN TS1.5x16 ga	4.21	3.92	92.2	0.2627	1.41	9.93	0.142 ¹
T9	40.1 - 20.1	ROHN TS1.5x16 ga	4.21	3.92	92.2	0.2627	1.38	9.93	0.139 ¹
T10	20.1 - 4.854	ROHN TS1.5x16 ga	4.22	3.93	92.4	0.2627	0.88	9.93	0.089 ¹

¹ P_u / φP_n controls

Top Girt Design Data (Tension)

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 50 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	175.35 - 160.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.38	9.93	0.039 ¹
T3	160.1 - 140.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.57	9.93	0.058 ¹
T4	140.1 - 120.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	2.50	9.93	0.251 ¹
T5	120.1 - 100.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.52	9.93	0.052 ¹
T6	100.1 - 80.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.60	9.93	0.060 ¹
T7	80.1 - 60.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.54	9.93	0.054 ¹
T8	60.1 - 40.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.65	9.93	0.066 ¹
T9	40.1 - 20.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.62	9.93	0.063 ¹
T10	20.1 - 4.854	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.50	9.93	0.051 ¹
T11	4.854 - 0	14x3/16	2.98	2.74	608.2	2.6250	2.91	85.05	0.034 ¹

L/R > 500 (T) - 436

¹ P_u / φP_n controls

Bottom Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.38	9.93	0.038 ¹
T2	175.35 - 160.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.96	9.93	0.097 ¹
T3	160.1 - 140.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	2.53	9.93	0.254 ¹
T4	140.1 - 120.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.50	9.93	0.051 ¹
T5	120.1 - 100.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.96	9.93	0.097 ¹
T6	100.1 - 80.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.52	9.93	0.052 ¹
T7	80.1 - 60.1	ROHN TS1.5x16 ga	3.46	3.26	76.7	0.2627	0.54	9.93	0.054 ¹
T8	60.1 - 40.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.67	9.93	0.068 ¹
T9	40.1 - 20.1	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	0.62	9.93	0.063 ¹
T10	20.1 - 4.854	ROHN TS1.5x16 ga	3.46	3.22	75.7	0.2627	3.73	9.93	0.376 ¹

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 51 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

¹ $P_u / \phi P_n$ controls

Mid Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T11	4.854 - 0	14x3/16	2.15	1.91	422.9	2.6250	0.08	85.05	0.001 ¹ ✓

¹ $P_u / \phi P_n$ controls

Top Guy Pull-Off Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	190.6 - 175.35	4 1/2x3/8	3.46	3.22	356.8	1.6875	3.69	54.67	0.067 ¹
T5	120.1 - 100.1	C4x5.4	3.46	3.26	87.1	1.5900	2.67	51.52	0.052 ¹
T8	60.1 - 40.1	C4x5.4	3.46	3.22	86.0	1.5900	2.39	51.52	0.046 ¹

¹ $P_u / \phi P_n$ controls

Top Guy Pull-Off Bending Design Data

Section No.	Elevation ft	Size	M _{ux} kip-ft	φM _{ux} kip-ft	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	M _{uy} kip-ft	φM _{uy} kip-ft	Ratio $\frac{M_{uy}}{\phi M_{uy}}$
T1	190.6 - 175.35	4 1/2x3/8	0.00	5.13	0.000	0.00	0.43	0.000
T5	120.1 - 100.1	C4x5.4	0.00	5.74	0.000	0.00	1.15	0.000
T8	60.1 - 40.1	C4x5.4	0.00	5.75	0.000	0.00	1.15	0.000

Top Guy Pull-Off Interaction Design Data

Section No.	Elevation ft	Size	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	Ratio $\frac{M_{uy}}{\phi M_{uy}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
T1	190.6 - 175.35	4 1/2x3/8	0.067	0.000	0.000	0.067 ¹ ✓	1.000	4.8.1 ✓
T5	120.1 - 100.1	C4x5.4	0.052	0.000	0.000	0.052 ¹ ✓	1.000	4.8.1 ✓
T8	60.1 - 40.1	C4x5.4	0.046	0.000	0.000	0.046 ¹ ✓	1.000	4.8.1 ✓

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 52 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJJ

¹ $P_u / \phi P_n$ controls

Torque-Arm Top Design Data

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in ²	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T4	140.1 - 120.1 (453)	C10x15.3	3.50	3.40	57.2	4.4900	0.04	145.48	0.000
T4	140.1 - 120.1 (454)	C10x15.3	3.50	3.40	57.2	4.4900	2.39	145.48	0.016
T4	140.1 - 120.1 (457)	C10x15.3	3.50	3.40	57.2	4.4900	0.06	145.48	0.000
T4	140.1 - 120.1 (458)	C10x15.3	3.50	3.40	57.2	4.4900	2.38	145.48	0.016
T4	140.1 - 120.1 (461)	C10x15.3	3.50	3.40	57.2	4.4900	0.04	145.48	0.000
T4	140.1 - 120.1 (462)	C10x15.3	3.50	3.40	57.2	4.4900	0.00	145.48	0.000

Torque-Arm Top Bending Design Data

Section No.	Elevation ft	Size	M_{ux} kip-ft	ϕM_{nx} kip-ft	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	M_{uy} kip-ft	ϕM_{ny} kip-ft	Ratio $\frac{M_{uy}}{\phi M_{ny}}$
T4	140.1 - 120.1 (453)	C10x15.3	-29.83	41.76	0.714	-0.00	4.70	0.000
T4	140.1 - 120.1 (454)	C10x15.3	-25.87	41.76	0.619	-0.00	4.70	0.000
T4	140.1 - 120.1 (457)	C10x15.3	-29.90	41.76	0.716	0.00	4.70	0.000
T4	140.1 - 120.1 (458)	C10x15.3	-26.08	41.76	0.625	0.00	4.70	0.000
T4	140.1 - 120.1 (461)	C10x15.3	-29.79	41.76	0.713	0.00	4.70	0.000
T4	140.1 - 120.1 (462)	C10x15.3	-29.47	41.76	0.706	-0.00	4.70	0.000

Torque-Arm Top Interaction Design Data

Section No.	Elevation ft	Size	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	Ratio $\frac{M_{uy}}{\phi M_{ny}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
T4	140.1 - 120.1 (453)	C10x15.3	0.000	0.714	0.000	0.715	1.000	4.8.1 ✓
T4	140.1 - 120.1 (454)	C10x15.3	0.016	0.619	0.000	0.628	1.000	4.8.1 ✓
T4	140.1 - 120.1 (457)	C10x15.3	0.000	0.716	0.000	0.716	1.000	4.8.1 ✓
T4	140.1 - 120.1	C10x15.3	0.016	0.625	0.000	0.633	1.000	4.8.1 ✓

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 53 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Size	Ratio	Ratio	Ratio	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
			P_u	M_{ux}	M_{uy}			
			ϕP_n	ϕM_{nx}	ϕM_{ny}			
T4	140.1 - 120.1 (461)	C10x15.3	0.000	0.713	0.000	0.714	1.000	4.8.1 ✓
T4	140.1 - 120.1 (462)	C10x15.3	0.000	0.706	0.000	0.706	1.000	4.8.1 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail
T1	190.6 - 175.35	Leg	ROHN 2.5 X-STR	1	-21.73	75.97	28.6	Pass
T2	175.35 - 160.1	Leg	ROHN 2.5 X-STR	28	-22.17	75.97	29.2	Pass
T3	160.1 - 140.1	Leg	ROHN 2 STD	56	-27.21	43.81	62.1	Pass
T4	140.1 - 120.1	Leg	ROHN 2 STD	113	-29.08	43.81	66.4	Pass
T5	120.1 - 100.1	Leg	ROHN 2 STD	171	-29.76	43.81	67.9	Pass
T6	100.1 - 80.1	Leg	ROHN 2 STD	228	-29.76	43.14	69.0	Pass
T7	80.1 - 60.1	Leg	ROHN 2 EH	285	-31.01	59.31	52.3	Pass
T8	60.1 - 40.1	Leg	ROHN 2.5 STD	342	-37.74	58.41	64.6	Pass
T9	40.1 - 20.1	Leg	ROHN 2.5 STD	375	-35.88	58.41	61.4	Pass
T10	20.1 - 4.854	Leg	ROHN 2.5 STD	408	-29.12	58.27	50.0	Pass
T11	4.854 - 0	Leg	ROHN 2.5 X-STR	433	-29.94	95.65	31.3	Pass
T1	190.6 - 175.35	Diagonal	ROHN TS1.5x16 ga	25	-3.30	5.88	56.2	Pass
T2	175.35 - 160.1	Diagonal	ROHN TS1.5x16 ga	38	-2.07	5.88	35.3	Pass
T3	160.1 - 140.1	Diagonal	ROHN TS1.5x16 ga	69	-2.07	5.81	35.6	Pass
T4	140.1 - 120.1	Diagonal	ROHN TS1.5x16 ga	167	-1.01	5.81	17.4	Pass
T5	120.1 - 100.1	Diagonal	ROHN TS1.5x16 ga	183	-2.15	5.81	37.0	Pass
T6	100.1 - 80.1	Diagonal	ROHN TS1.5x16 ga	282	-0.92	5.81	15.8	Pass
T7	80.1 - 60.1	Diagonal	ROHN TS1.5x16 ga	296	-0.80	5.81	13.8	Pass
T8	60.1 - 40.1	Diagonal	ROHN TS1.5x16 ga	350	-1.70	5.89	28.8	Pass
T9	40.1 - 20.1	Diagonal	ROHN TS1.5x16 ga	404	-1.57	5.89	26.6	Pass
T10	20.1 - 4.854	Diagonal	ROHN TS1.5x16 ga	431	-1.05	5.88	17.8	Pass
T2	175.35 - 160.1	Top Girt	ROHN TS1.5x16 ga	33	-0.38	6.99	5.5	Pass
T3	160.1 - 140.1	Top Girt	ROHN TS1.5x16 ga	58	-0.47	6.92	9.2 (b) 6.8	Pass
T4	140.1 - 120.1	Top Girt	ROHN TS1.5x16 ga	116	-2.11	6.92	13.8 (b) 30.5	Pass
T5	120.1 - 100.1	Top Girt	ROHN TS1.5x16 ga	173	-0.52	6.92	59.9 (b) 7.4	Pass
T6	100.1 - 80.1	Top Girt	ROHN TS1.5x16 ga	230	-0.52	6.92	12.4 (b) 7.4	Pass
T7	80.1 - 60.1	Top Girt	ROHN TS1.5x16 ga	287	-0.54	6.92	14.4 (b) 7.8	Pass
T8	60.1 - 40.1	Top Girt	ROHN TS1.5x16 ga	344	-0.65	6.99	12.9 (b) 9.4	Pass
T9	40.1 - 20.1	Top Girt	ROHN TS1.5x16 ga	377	-0.62	6.99	15.7 (b) 8.9	Pass
T10	20.1 - 4.854	Top Girt	ROHN TS1.5x16 ga	410	-0.50	6.99	14.9 (b) 7.2	Pass
T11	4.854 - 0	Top Girt	14x3/16	438	-0.55	1.60	12.1 (b) 34.3	Pass
T1	190.6 - 175.35	Bottom Girt	ROHN TS1.5x16 ga	9	-0.38	6.99	5.4	Pass
T2	175.35 - 160.1	Bottom Girt	ROHN TS1.5x16 ga	35	-0.96	6.99	6.4 (b) 13.7	Pass
T3	160.1 - 140.1	Bottom Girt	ROHN TS1.5x16 ga	63	-2.14	6.92	16.2 (b) 31.0	Pass

tnxTower Centek Engineering Inc. 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 21140.00 - CT1166	Page 54 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
T4	140.1 - 120.1	Bottom Girt	ROHN TS1.5x16 ga	118	-0.50	6.92	42.7 (b) 7.3	Pass	
T5	120.1 - 100.1	Bottom Girt	ROHN TS1.5x16 ga	176	0.96	9.93	8.5 (b) 9.7	Pass	
T6	100.1 - 80.1	Bottom Girt	ROHN TS1.5x16 ga	233	-0.52	6.92	16.3 (b) 7.4	Pass	
T7	80.1 - 60.1	Bottom Girt	ROHN TS1.5x16 ga	290	-0.54	6.92	8.7 (b) 7.8	Pass	
T8	60.1 - 40.1	Bottom Girt	ROHN TS1.5x16 ga	347	-0.65	6.99	9.1 (b) 9.4	Pass	
T9	40.1 - 20.1	Bottom Girt	ROHN TS1.5x16 ga	380	-0.62	6.99	11.4 (b) 8.9	Pass	
T10	20.1 - 4.854	Bottom Girt	ROHN TS1.5x16 ga	412	3.73	9.93	10.5 (b) 37.6	Pass	
T11	4.854 - 0	Bottom Girt	14x3/16	439	-0.83	73.69	63.1 (b) 8.8	Pass	
T11	4.854 - 0	Mid Girt	14x3/16	443	-0.16	10.51	1.5	Pass	
T1	190.6 - 175.35	Guy A@189.985	9/16	450	13.57	21.00	64.6	Pass	
T4	140.1 - 120.1	Guy A@139.485	1/2	460	10.67	16.14	66.1	Pass	
T5	120.1 - 100.1	Guy A@102.623	3/8	468	5.26	9.24	57.0	Pass	
T8	60.1 - 40.1	Guy A@45.0323	3/8	474	4.62	9.24	50.0	Pass	
T1	190.6 - 175.35	Guy B@189.985	9/16	449	13.71	21.00	65.3	Pass	
T4	140.1 - 120.1	Guy B@139.485	1/2	455	10.72	16.14	66.4	Pass	
T5	120.1 - 100.1	Guy B@102.623	3/8	467	5.45	9.24	59.0	Pass	
T8	60.1 - 40.1	Guy B@45.0323	3/8	473	4.69	9.24	50.8	Pass	
T1	190.6 - 175.35	Guy C@189.985	9/16	448	13.73	21.00	65.4	Pass	
T4	140.1 - 120.1	Guy C@139.485	1/2	451	10.43	16.14	64.6	Pass	
T5	120.1 - 100.1	Guy C@102.623	3/8	463	5.43	9.24	58.8	Pass	
T8	60.1 - 40.1	Guy C@45.0323	3/8	469	4.63	9.24	50.1	Pass	
T1	190.6 - 175.35	Top Guy	4 1/2x3/8	4	3.69	54.67	6.7	Pass	
T5	120.1 - 100.1	Pull-Off@189.985							
		Top Guy	C4x5.4	464	2.67	51.52	5.2	Pass	
T8	60.1 - 40.1	Pull-Off@102.623							
		Top Guy	C4x5.4	470	2.39	51.52	4.6	Pass	
T4	140.1 - 120.1	Pull-Off@45.0323							
		Torque Arm	C10x15.3	457	-3.14	122.43	71.6	Pass	
		Top@139.485							
							Summary		
							Leg (T6)	69.0	Pass
							Diagonal (T1)	56.2	Pass
							Top Girt (T4)	59.9	Pass
							Bottom Girt (T10)	63.1	Pass
							Mid Girt (T11)	1.5	Pass
							Guy A (T4)	66.1	Pass
							Guy B (T4)	66.4	Pass
							Guy C (T1)	65.4	Pass
							Top Guy Pull-Off (T1)	6.7	Pass
							Torque Arm Top (T4)	71.6	Pass
							Bolt Checks	63.1	Pass
							RATING =	71.6	Pass

<i>tnxTower</i> <i>Centek Engineering Inc.</i> <i>63-2 North Branford Rd.</i> <i>Branford, CT 06405</i> <i>Phone: (203) 488-0580</i> <i>FAX: (203) 488-8587</i>	Job 21140.00 - CT1166	Page 55 of 55
	Project 190-ft Guyed Tower - 812 Providence Pike, Danielson, CT	Date 14:02:32 02/20/23
	Client AT&T	Designed by TJL

Program Version 8.1.1.0 - 6/3/2021 File:J:/Jobs/2114000.WI/05_Structural/04_Structural/Backup Documentation/Rev (8)/Calcs/ERI/190-ft Guyed Tower - Danielson, CT - reinforced.eri

Job : AT&T ~ CT1166: 190-ft Guyed Lattice Tower
 Address: 812 Providence Pike, Danileson, CT
 Description: Guy Anchor Evaluation

Project No. 21140.00
 Computed by TJL
 Checked by CFC

Sheet 1 of 2
 Date 11/7/22
 Date

CHECK UPLIFT RESISTANCE

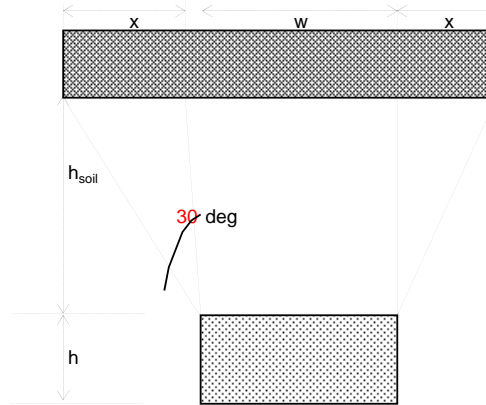
ANCHOR (C) AT 99ft RADIUS

RESULTS FROM COMPUTER ANALYSIS:

Uplift = 29 kips
 Sliding = 18 kips
 Wdepth = 1 ft

CONCRETE PARAMETERS:

$\gamma_{conc} = 150$ pcf
 $\gamma_{conc.sub} = 87.6$ pcf
 $w = 4$ ft
 $h = 2$ ft
 $d = 7$ ft
 Vol. = 0.00 ft³
 Vol.sub = 56.00 ft³
 $Wc = 4.91$ kips
 $\emptyset = 0.90$
 4.42



Foundation Section

SOIL PARAMETERS:

$\gamma_{soil} = 105$ pcf
 $\gamma_{soil.sub} = 42.6$ pcf
 $h_{soil} = 8$ ft
 $x = 4.62$ ft

Soil Weight (Wr):

B1 = 28.00
 B2 = 182.25
 B3 = 214.95

W.soil = 20.83 kips
 W.soil.sub = 28.00 kips
 Total = 48.83 kips
 $\emptyset = 0.75$
 36.62

SF AGAINST SLIDING

1.85 > 1 OK

GUY ANCHORS AGAINST UPLIFT ARE ADEQUATE

Job : AT&T ~ CT1166: 190-ft Guyed Lattice Tower
 Address: 812 Providence Pike, Danileson, CT
 Description: Guy Anchor Evaluation

Project No. 21140.00
 Computed by TJL
 Checked by CFC

Sheet 2 of 2
 Date 11/7/22
 Date

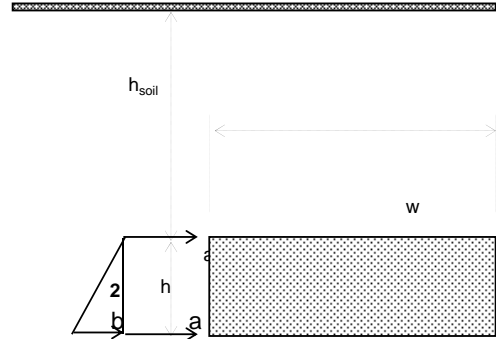
CHECK SLIDING RESISTANCE

SOIL PARAMETERS

$\gamma_{soil} = 105$ pcf
 $\gamma_{soil} = 42.6$ pcf
 $h_{soil} = 8$ ft
 $h = 2$ ft
 $\phi = 30$ degrees

ANCHOR PARAMETERS

$w = 4.0$ ft
 $h = 2.0$ ft
 $d = 7.0$ ft



Foundation Elevation View

$K_p = 3.00$

HORIZONTAL FORCES

RESIST TO SLIDING =

1.21 ksf
 1.47 ksf
 18.72 k

SOIL & CONCRETE WEIGHT =
 UPLIFT REACTIONS =
 SUM =

$W_r + W_c = 41.04$ k
 -29 k
 12.04 k

COEF. OF FRICTION, (0.45) =
 RESIST TO SLIDING =
 SUM =

5.42 k
 18.72 k
 24.14 k

SF AGAINST SLIDING

$SF = 1.3 > 1$ OK

Guyed Tower Base Foundation:

Input Data:

Tower Data

Shear Force = Shear := 1-kip (User Input from tnxTower)
 Axial Force = Axial := 83-kip (User Input from tnxTower)
 Tower Height = $H_t := 190\text{-ft}$ (User Input)

Footing Data:

Overall Depth of Footing = $D_f := 4.0\text{-ft}$ (User Input)
 Length of Pier = $L_p := 3.75\text{-ft}$ (User Input)
 Extension of Pier Above Grade = $L_{pag} := 1.0\text{-ft}$ (User Input)
 Width of Pier = $W_p := 2.0\text{-ft}$ (User Input)
 Thickness of Footing = $T_f := 1.25\text{-ft}$ (User Input)
 Width of Footing = $W_{f1} := 4\text{-ft}$ (User Input)
 Length of Footing = $W_{f2} := 4\text{-ft}$ (User Input)

Material Properties:

Concrete Compressive Strength = $f_c := 3000\text{-psi}$ (User Input)
 Steel Reinforcement Yield Strength = $f_y := 60000\text{-psi}$ (User Input)
 Internal Friction Angle of Soil = $\Phi_s := 30\text{-deg}$ (User Input)
 Ultimate Soil Bearing Capacity = $q_s := 12000\text{-psf}$ (User Input)
 Unit Weight of Soil = $\gamma_{soil} := 120\text{-pcf}$ (User Input)
 Unit Weight of Concrete = $\gamma_{conc} := 150\text{-pcf}$ (User Input)
 Foundation Bouyancy = Bouyancy := 1 (User Input) (Yes=1 / No=0)
 Depth to Neglect = $n := 0\text{-ft}$ (User Input)
 Cohesion of Clay Type Soil = $c := 0\text{-ksf}$ (User Input) (Use 0 for Sandy Soil)
 Seismic Zone Factor = $Z := 2$ (User Input)
 Coefficient of Friction Between Concrete = $\mu := 0.45$ (User Input)

Calculated Factors:

Coefficient of Lateral Soil Pressure = $K_p := \frac{1 + \sin(\Phi_s)}{1 - \sin(\Phi_s)} = 3$

Load Factor = $LF := \begin{cases} 1.333 & \text{if } H_t \leq 700\text{-ft} \\ 1.7 & \text{if } H_t \geq 1200\text{-ft} \\ 1.333 + \left(\frac{H_t - 700\text{ft}}{1200\text{ft} - 700\text{ft}} \right) \cdot 0.4 & \text{otherwise} \end{cases} = 1.333$

Stability of Footing:

Adjusted Concrete Unit Weight = $\gamma_c := \text{if}(\text{Bouyancy} = 1, \gamma_{\text{conc}} - 62.4\text{pcf}, \gamma_{\text{conc}}) = 87.6\text{pcf}$

Adjusted Soil Unit Weight = $\gamma_s := \text{if}(\text{Bouyancy} = 1, \gamma_{\text{soil}} - 62.4\text{pcf}, \gamma_{\text{soil}}) = 57.6\text{pcf}$

Passive Pressure = $P_{pn} := K_p \cdot \gamma_s \cdot n + c \cdot 2 \cdot \sqrt{K_p} = 0\text{ksf}$

$P_{pt} := K_p \cdot \gamma_s \cdot (D_f - T_f) + c \cdot 2 \cdot \sqrt{K_p} = 0.475\text{ksf}$

$P_{top} := \text{if}[n < (D_f - T_f), P_{pt}, P_{pn}] = 0.475\text{ksf}$

$P_{bot} := K_p \cdot \gamma_s \cdot D_f + c \cdot 2 \cdot \sqrt{K_p} = 0.691\text{ksf}$

$P_{ave} := \frac{P_{top} + P_{bot}}{2} = 0.583\text{ksf}$

$T_p := \text{if}[n < (D_f - T_f), T_f \cdot (D_f - n)] = 1.25$

$A_p := W_{f1} \cdot T_p = 5$

Soil Shear Resistance = $Sl_1 := P_{ave} \cdot A_p = 2.92\text{kip}$

Weight of Concrete = $WT_c := [(W_{f1} \cdot W_{f2} \cdot T_f) + W_p^2 \cdot L_p] \cdot \gamma_c = 3.07\text{kip}$

Total Weight = $WT_{tot} := WT_c + \text{Axial} = 86.07\text{kip}$

Soil/Concrete Friction Resistance = $Sl_2 := \mu \cdot WT_{tot} = 38.73\text{kips}$

Total Sliding Resistance = $Sl_{tot} := Sl_1 + Sl_2 = 41.65\text{kips}$

Sliding Resistance Ratio = $\text{Sliding_Resistance_ratio} := \frac{0.75Sl_{tot}}{\text{Shear}} = 31.23$

$\text{Sliding_Resistance_Check} := \text{if}\left[\left(\frac{\text{Shear}}{0.75Sl_{tot}} < 1.0\right), \text{"Okay"}, \text{"No Good"}\right]$

Sliding_Resistance_Check = "Okay"

Bearing Pressure Caused by Footing:

Area of the Mat = $A_{mat} := W_{f1} \cdot W_{f2} = 16$

Maximum Pressure in Mat = $P_{max} := \frac{WT_{tot}}{A_{mat}} = 5.38\text{ksf}$

$\text{Max_Pressure_Check} := \text{if}(P_{max} < 0.6q_s, \text{"Okay"}, \text{"No Good"})$

Max_Pressure_Check = "Okay"

TOWER REINFORCEMENT DESIGN

CT1166

812 PROVIDENCE PIKE

DANIELSON, CT 06239



VICINITY MAP



PROJECT SUMMARY

SITE ADDRESS: 812 PROVIDENCE PIKE
DANIELSON, CT 06239

PROJECT COORDINATES: LAT: 41°-47'-29.44N
LON: 71°-49'-20.66W
ELEV:±680' AMSL

AT&T SITE REF.: CT1166

AT&T CONTACT: DAN BILEZIKIAN
401.368.0006

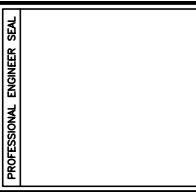
ENGINEER OF RECORD: CENTEK ENGINEERING, INC.
63-2 NORTH BRANFORD ROAD
BRANFORD, CT 06405

CEN TEK CONTACT: TIMOTHY J. LYNN, PE
203.433.7507

SHEET INDEX

SHT. NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	7
N-1	DESIGN BASIS & GENERAL NOTES	7
N-2	STRUCTURAL STEEL NOTES	7
MI-1	MODIFICATION INSPECTION REQUIREMENTS	7
S-1	TOWER REINFORCEMENT ELEVATION & PLAN	7
S-2	TOWER REINFORCEMENT DETAILS	7

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812 PROVIDENCE PIKE
DANIELSON, CT 06239

DATE: 1/3/2022
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JOB NO. 21140.00

TITLE SHEET

SHEET NO.
T-1
Sheet No. 1 of 6

DESIGN BASIS

GOVERNING CODE: 2021 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2022 CT STATE BUILDING CODE.

1. TIA-222-H, "STRUCTURAL STANDARD FOR ANTENNA SUPPORTING STRUCTURES, ANTENNAS AND SMALL WIND TURBINE SUPPORT STRUCTURES"
2. DESIGN CRITERIA

WIND LOAD:

ULTIMATE DESIGN WIND SPEED (Vult) = 125 MPH (2022 CSBC: APPENDIX 'P')

GENERAL NOTES

1. REFER TO STRUCTURAL ANALYSIS AND REINFORCEMENT DESIGN PREPARED BY CENTEK ENGINEERING, INC., MARKED REV 8 DATED 2/20/23.
2. TOWER GEOMETRY AND STRUCTURE MEMBER SIZES WERE OBTAINED FROM A TOWER MAPPING REPORT PREPARED BY CSB COMMUNICATIONS, DATED OCTOBER 26, 2013.
3. PROVIDE TEMPORARY ANCHORS, GUYING AND/OR BRACING AS REQUIRED TO SAFELY CONDUCT THE WORK.
4. ALL WORK SHALL BE IN ACCORDANCE WITH TIA-222-F "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES".
5. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY TO DETERMINE ERECTION PROCEDURE AND SEQUENCE AND TO INSURE THE SAFETY OF THE TOWER STRUCTURE AND ITS COMPONENT PARTS DURING ERECTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, TEMPORARY BRACING, GUYS OR TIE-DOWNS, WHICH MIGHT BE NECESSARY.
6. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS SCOPE OF WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
7. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
8. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
9. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
11. TOWER REINFORCING SHALL BE CONDUCTED BY FIELD CREWS EXPERIENCED IN THE ASSEMBLY AND ERECTION OF RADIO ANTENNAS AND SUPPORT STRUCTURES. ALL SAFETY PROCEDURES, RIGGING AND ERECTION METHODS SHALL BE STANDARD TO THE INDUSTRY AND IN COMPLIANCE WITH OSHA.
12. EXISTING COAXIAL CABLES AND ALL ACCESSORIES SHALL BE RELOCATED AS NECESSARY AND REINSTALLED BY THE CONTRACTOR WITHOUT INTERRUPTION IN SERVICE WHERE THEY ARE IN CONFLICT WITH TOWER REINFORCEMENT.
13. IF ANY FIELD CONDITIONS EXIST WHICH PRECLUDE COMPLIANCE WITH THE DRAWINGS, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ENGINEER AND SHALL PROCEED WITH AFFECTED WORK AFTER CONFLICT IS SATISFACTORILY RESOLVED.

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 DANIELSON, CT 06239

DATE: 1/3/2022
 SCALE: AS SHOWN
 JOB NO. 21140.00

DESIGN BASIS &
 GENERAL NOTES

SHEET NO.
N-1
 Sheet No. 2 of 6

STRUCTURAL STEEL

1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD).
2. MATERIAL SPECIFICATIONS
 - A. STRUCTURAL STEEL (W SHAPES)---ASTM A992 (FY = 50 KSI)
 - B. STRUCTURAL STEEL (OTHER SHAPES)---ASTM A36 (FY = 36 KSI).
 - C. STRUCTURAL STEEL (TOWER REINF. PLATES)---ASTM A572 GR50 (FY = 50 KSI)
 - D. STRUCTURAL HSS (RECTANGULAR SHAPES)---ASTM A500 GRADE B, (FY = 46 KSI)
 - E. STRUCTURAL HSS (ROUND SHAPES)---ASTM A500 GRADE B, (FY = 42 KSI)
 - F. PIPE ---ASTM A53 GRADE B (FY = 35 KSI)
3. FASTENER SPECIFICATIONS
 - A. CONNECTION BOLTS---ASTM A325-N, UNLESS OTHERWISE SCHEDULED.
 - B. U-BOLTS---ASTM A307
 - C. ANCHOR RODS---ASTM F1554
 - D. WELDING ELECTRODES---ASTM E70XX FOR A36 & A572_GR50 STEELS, ASTM E80XX FOR A572_GR65 STEEL.
 - E. BLIND BOLTS---AS1252 PROPERTY CLASS 8.8 (FU=120 KSI).
4. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLUDE THE FOLLOWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE, SIZE AND TYPE OF FASTENERS AND ACCESSORIES. INCLUDE ERECTION DRAWINGS, ELEVATIONS AND DETAILS.
5. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL CONSTRUCTION.
6. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS, MISCELLANEOUS PIECES AND HOLES REQUIRED TO COMPLETE THE STRUCTURE.
7. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR DELIVERY TO SITE.
8. INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM DISTORTIONS OR DEFECTS.
9. AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN ACCORDANCE WITH ASTM 780.
10. ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED) COATINGS" ON IRONS AND STEEL PRODUCTS.
11. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL HARDWARE".
12. CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES APPEARANCE AND QUALITY OF WELDS, AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES". ALL WELDING SHALL BE DONE USING THE SCHEDULED ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D1.1 WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION" 14TH EDITION. AT THE COMPLETION OF WELDING, ALL DAMAGE TO GALVANIZED COATING SHALL BE REPAIRED.
13. THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER REVIEW.
14. CONNECTION ANGLES SHALL HAVE A MINIMUM THICKNESS OF 1/4 INCHES.
15. STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DIAMETER MINIMUM AND SHALL HAVE A MINIMUM OF TWO BOLTS, UNLESS OTHERWISE ON THE DRAWINGS.
16. LOCK WASHER ARE NOT PERMITTED FOR A325 BOLTED STEEL ASSEMBLIES.
17. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
18. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.
19. FABRICATE BEAMS WITH MILL CAMBER UP.
20. LEVEL AND PLUMB INDIVIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.
21. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.

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STRUCTURAL STEEL NOTES

SHEET NO. **N-2**
 Sheet No. 3 of 6

MODIFICATION INSPECTION REPORT REQUIREMENTS

PRE-CONSTRUCTION		DURING CONSTRUCTION		POST-CONSTRUCTION	
SCHEDULED ITEM	REPORT ITEM	SCHEDULED ITEM	REPORT ITEM	SCHEDULED ITEM	REPORT ITEM
X	EOR MODIFICATION INSPECTION DRAWING	-	FOUNDATIONS	X	MODIFICATION INSPECTOR RECORD REDLINE DRAWING
X	EOR APPROVED SHOP DRAWINGS	-	EARTHWORK: BACKFILL MATERIAL & COMPACTION	-	POST-INSTALLED ANCHOR ROD PULL-OUT TEST
-	EOR APPROVED POST-INSTALLED ANCHOR MPII	-	CONCRETE TESTING	X	PHOTOGRAPHS
-	FABRICATION INSPECTION	X	STEEL INSPECTION		
-	FABRICATOR CERTIFIED WELDER INSPECTION	-	POST INSTALLED ANCHOR ROD VERIFICATION		
X	MATERIAL CERTIFICATIONS	-	BASE PLATE GROUT VERIFICATION		
		-	CONTRACTOR'S CERTIFIED WELD INSPECTION		
		X	ON-SITE COLD GALVANIZING VERIFICATION		
		X	GUY WIRE TENSION REPORT		
		X	CONTRACTOR AS-BUILT REDLINE DRAWINGS		

NOTES:

1. REFER TO MODIFICATION INSPECTION NOTES FOR ADDITIONAL REQUIREMENTS
2. "X" DENOTES DOCUMENT REQUIRED FOR INCLUSION IN MODIFICATION INSPECTION FINAL REPORT.
3. "-" DENOTES DOCUMENT NOT REQUIRED FOR INCLUSION IN MODIFICATION INSPECTION FINAL REPORT.
4. EOR - ENGINEER OF RECORD
4. MPII - "MANUFACTURER'S PRINTED INSTALLATION GUIDELINES"

GENERAL

1. THE MODIFICATION INSPECTION IS A VISUAL INSPECTION OF STRUCTURAL MODIFICATIONS, TO INCLUDE A REVIEW AND COMPILATION OF SPECIFIED SUBMITTALS AND CONSTRUCTION INSPECTIONS, AS AN ASSURANCE OF COMPLIANCE WITH THE CONSTRUCTION DOCUMENTS PREPARED UNDER THE DIRECTION OF THE ENGINEER OF RECORD (EOR).
2. THE MODIFICATION INSPECTION IS TO CONFIRM INSTALLATION CONFIGURATION AND GENERAL WORKMANSHIP AND IS NOT A REVIEW OF THE MODIFICATION DESIGN. OWNERSHIP OF THE MODIFICATION DESIGN EFFECTIVENESS AND INTENT RESIDES WITH THE ENGINEER OF RECORD.
3. TO ENSURE COMPLIANCE WITH THE MODIFICATION INSPECTION REQUIREMENTS THE GENERAL CONTRACTOR (GC) AND THE MODIFICATION INSPECTOR (MI) COMMENCE COMMUNICATION UPON AUTHORIZATION TO PROCEED BY THE CLIENT. EACH PARTY SHALL BE PROACTIVE IN CONTACTING THE OTHER. THE EOR SHALL BE CONTACTED IF SPECIFIC GC/MI CONTACT INFORMATION IS NOT MADE AVAILABLE.
4. THE GC SHALL PROVIDE THE MI WITH A MINIMUM OF 5 BUSINESS DAYS NOTICE OF IMPENDING INSPECTIONS.
5. WHEN POSSIBLE, THE GC AND MI SHALL BE ON SITE DURING THE MODIFICATION INSPECTION TO HAVE ANY NOTED DEFICIENCIES ADDRESSED DURING THE INITIAL MODIFICATION INSPECTION.

MODIFICATION INSPECTOR (MI)

1. THE MI SHALL CONTACT THE GC UPON AUTHORIZATION BY THE CLIENT TO:
 - REVIEW THE MODIFICATION INSPECTION REPORT REQUIREMENTS.
 - WORK WITH THE GC IN DEVELOPMENT OF A SCHEDULE FOR ON-SITE INSPECTIONS.
 - DISCUSS CRITICAL INSPECTIONS AND PROJECT CONCERNS.
2. THE MI IS RESPONSIBLE FOR COLLECTION OF ALL INSPECTION AND TEST REPORTS, REVIEWING REPORTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING ON-SITE INSPECTIONS AND COMPILATION & SUBMISSION OF THE MODIFICATION INSPECTION REPORT TO THE CLIENT AND THE EOR.

GENERAL CONTRACTOR (GC)

1. THE GC IS REQUIRED TO CONTACT THE GC UPON AUTHORIZATION TO PROCEED WITH CONSTRUCTION BY THE CLIENT TO:
 - REVIEW THE MODIFICATION INSPECTION REPORT REQUIREMENTS.
 - WORK WITH THE MI IN DEVELOPMENT OF A SCHEDULE FOR ON-SITE INSPECTIONS.
 - DISCUSS CRITICAL INSPECTIONS AND PROJECT CONCERNS.
2. THE GC IS RESPONSIBLE FOR COORDINATING AND SCHEDULING IN ADVANCE ALL REQUIRED INSPECTIONS AND TESTS WITH THE MI.

CORRECTION OF FAILING MODIFICATION INSPECTION

1. SHOULD THE STRUCTURAL MODIFICATION NOT COMPLY WITH THE REQUIREMENTS OF THE CONSTRUCTION DOCUMENTS, THE GC SHALL WORK WITH THE MODIFICATION INSPECTOR IN A VIABLE REMEDIATION PLAN AS FOLLOWS:
 - CORRECT ALL DEFICIENCIES TO COMPLY WITH THE CONTRACT DOCUMENTS AND COORDINATE WITH THE MI FOR A FOLLOW UP INSPECTION.
 - WITH CLIENT AUTHORIZATION, THE GC MAY WORK WITH THE EOR TO REANALYZE THE MODIFICATION USING THE AS-BUILT CONDITION.

REQUIRED PHOTOGRAPHS

1. THE GC AND MI SHALL AT MINIMUM PHOTO DOCUMENT THE FOLLOWING FOR INCLUSION IN THE MODIFICATION INSPECTION REPORT:
 - PRE-CONSTRUCTION: GENERAL CONDITION OF THE SITE.
 - DURING CONSTRUCTION: RAW MATERIALS, CRITICAL DETAILS, WELD PREPARATION, BOLT INSTALLATION & TORQUE, FINAL INSTALLED CONDITION & SURFACE COATING REPAIRS.
 - POST-CONSTRUCTION: FINAL CONDITION OF THE SITE

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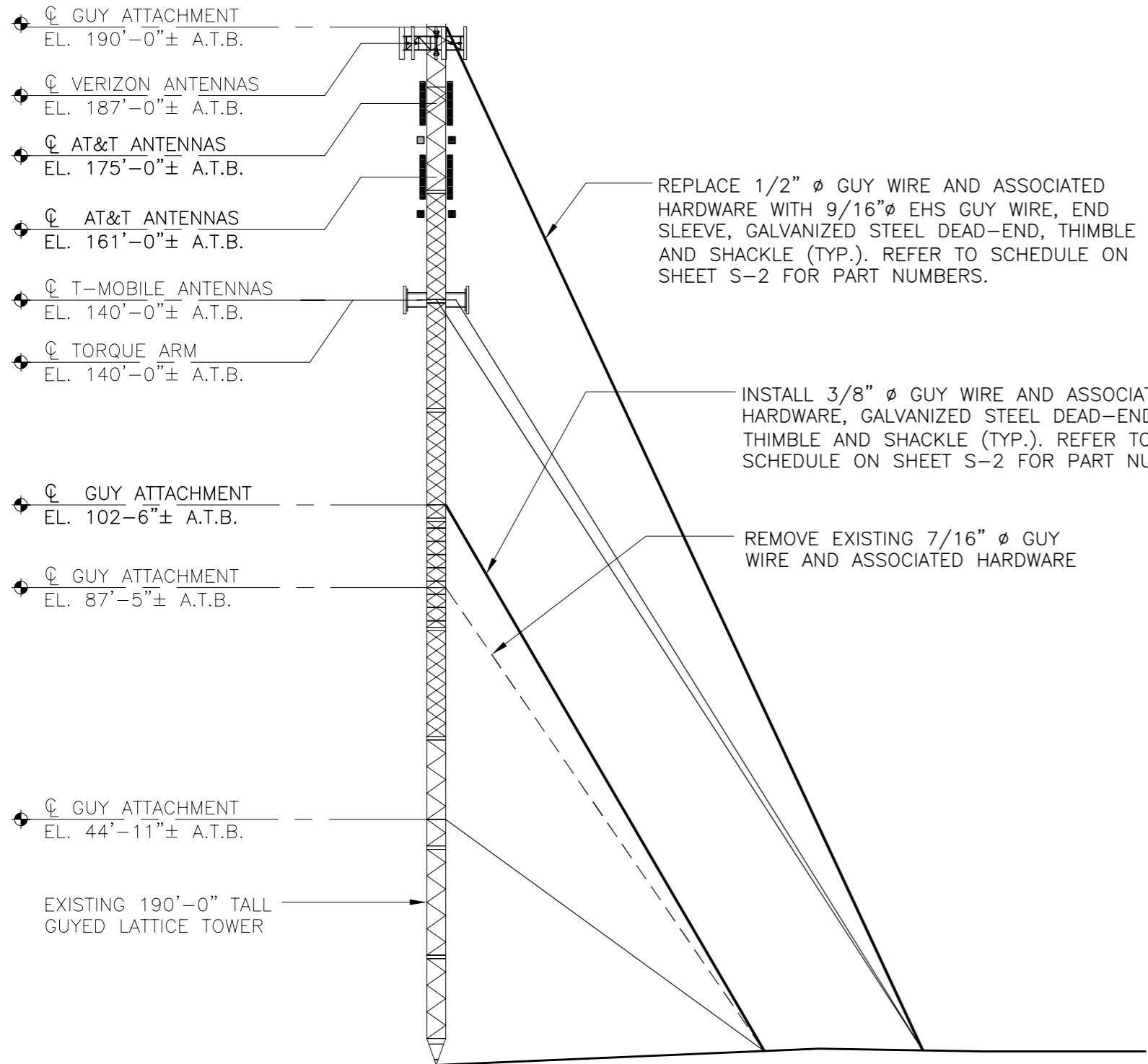
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MODIFICATION INSPECTION REQUIREMENTS

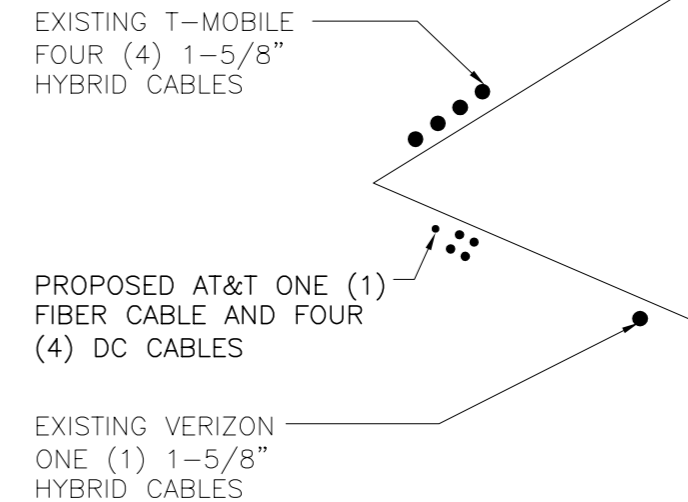
SHEET NO.
MI-1
 Sheet No. 4 of 6

AGL DENOTES ABOVE GRADE LEVEL
 ATB DENOTES ABOVE TOWER BASE



NOTES

- WHERE REINFORCEMENT INSTALLATION COINCIDES WITH EXIST. EXTERIOR COAX CABLE PLACEMENT. GC. TO TEMPORARILY DETACH COAX TO PERMIT THE INSTALLATION OF THE REINFORCEMENT THEN REINSTATE COAX PRE-EXISTING CONDITION



1 TOWER ELEVATION - PROPOSED
 S-1 SCALE: 1" = 25'-0"

2 FEEDLINE PLAN - PROPOSED
 S-1 NOT TO SCALE

APPROX
 TRUE
 NORTH



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TOWER REINFORCEMENT ELEVATION & PLAN

SHEET NO. S-1
 Sheet No. 5 of 6

TOWER GUY WIRE COMPONENT SCHEDULE

ELEVATION	GUY WIRE SIZE	GUY WIRE ATTACHMENT/ TORQUE ARM P/N	BOLT TYPE SHACKLE P/N	END SLEEVE (ICE CLIP) P/N	GALV. DEAD END (BIG GRIP) P/N	THIMBLE P/N	TURNBUCKLE P/N	ANCHOR ROD P/N
190' (A.T.B)	9/16" (320107)	EXIST.	5/8" (320752-I)	9/16" (320556)	9/16" (320506)	5/8" (320782-I)	7/8" JAW EYE (162930-I)	EXIST.
140' (A.T.B)	EXIST. 1/2"	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.
102.5' (A.T.B)	3/8" (320103)	RGA-0002-42*	1/2" (320751-I)	3/8" (320553)	3/8" (320503)	3/8" (320778-I)	1/2" JAW EYE (320596-I)	EXIST.
44.9' (A.T.B)	EXIST. 3/8"	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.	EXIST.

NOTE: ALL PART NUMBERS SHOWN ABOVE ARE BASED ON SITEPRO MATERIALS UNLESS OTHERWISE SPECIFIED.
 * STRUCTURAL COMPONENTS ADJUSTABLE GUY ATTACHEMENT RGA-002-42 WITH RGA-1000-23 PIPE SLEEVE

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REGISTERED PROFESSIONAL ENGINEER
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 JOB NO. 21140.00

TOWER REINFORCEMENT DETAILS

SHEET NO.
S-2
 Sheet No. 2 of 6

Section 1 - RFDS GENERAL INFORMATION

RFDS NAME:	CT1166	DATE:	10/14/2022	RF DESIGN ENG:	Radu Alecsandru	RF PERF ENG:		RFDS PROGRAM TYPE:	2023 New Site		
ISSUE:	Bronze Standard	Approved? (Y/N):	Yes	RF DESIGN PHONE:		RF PERF PHONE:		RFDS TECHNOLOGY:	New		
REVISION:	FINAL	RF MANAGER:	John Benedetto	RF DESIGN EMAIL:	RA9161@ATT.COM	RF PERF EMAIL:		STATE/STATUS:	Preliminary/In Progress		
INITIATIVE /PROJECT:	11/16/2021 initial release of the RFDS					ADDITIONAL WORKFLOW NOTIFICATIONS:	4863735				
	6/3/2022 stacked the two antennas of each sector due to structural issues					RFDS VERSION:	4.00	Created By:	ra9161		
	9/6/2022 6630 BBU updated to 6651 BBU per HQ.					UMTS FREQUENCY:		Date Created:	11/16/2021 12:01:51 PM		
	10/14/2022 section 16/17 corrections to match the plumbing					LTE FREQUENCY:	700, 1900, AWS	Estimated SQIN:	15.356		
						5G FREQUENCY:	850, 1900, AWS	RER Initiative:			
						I-PLAN JOB # 1:	NER-RCTB-15-01636	IPLAN PRD GRP SUB GRP #1:	New Site LTE Only 1C		
						I-PLAN JOB # 2:	ER_RCTB-21-10298	IPLAN PRD GRP SUB GRP #2:	LTE Next Carrier LTE 4C		
						I-PLAN JOB # 3:	ER_RCTB-21-10251	IPLAN PRD GRP SUB GRP #3:	LTE Software Carrier LTE 3C		
						I-PLAN JOB # 4:	ER_RCTB-21-10387	IPLAN PRD GRP SUB GRP #4:	5G NR Radio 5G NR 10R-1		
						I-PLAN JOB # 5:	ER_RCTB-21-10441	IPLAN PRD GRP SUB GRP #5:	5G NR Software Radio 5G NR Activation		
						I-PLAN JOB # 6:	ER_RCTB-21-10194	IPLAN PRD GRP SUB GRP #6:	LTE Next Carrier LTE 2C		
						I-PLAN JOB # 7:	ER_RCTB-21-10440	IPLAN PRD GRP SUB GRP #7:	5G NR Software Radio 5G NR Activation		
						I-PLAN JOB # 8:		IPLAN PRD GRP SUB GRP #8:			
						I-PLAN JOB # 9:		IPLAN PRD GRP SUB GRP #9:			
						I-PLAN JOB # 10:		IPLAN PRD GRP SUB GRP #10:			
						I-PLAN JOB # 11:		IPLAN PRD GRP SUB GRP #11:			
					I-PLAN JOB # 12:		IPLAN PRD GRP SUB GRP #12:				
					I-PLAN JOB # 13:		IPLAN PRD GRP SUB GRP #13:				
					I-PLAN JOB # 14:		IPLAN PRD GRP SUB GRP #14:				
					I-PLAN JOB # 15:		IPLAN PRD GRP SUB GRP #15:				
					I-PLAN JOB # 16:		IPLAN PRD GRP SUB GRP #16:				

Section 2 - LOCATION INFORMATION

USID:	314085	FA LOCATION CODE:	10141308	LOCATION NAME:	DANIELSON	ORACLE PTN # 1:	2051A12J0J	PACE JOB # 1:	MRCTB057569
REGION:	NORTHEAST	MARKET CLUSTER:	NEW ENGLAND	MARKET:	CONNECTICUT	ORACLE PTN # 2:	2051A13RSB	PACE JOB # 2:	MRCTB061480
ADDRESS:	812 PROVIDENCE PIKE	CITY:	DANIELSON	STATE:	CT	ORACLE PTN # 3:	2051A13RPV	PACE JOB # 3:	MRCTB061417
ZIP CODE:	06239	COUNTY:	WINDHAM	LONG (DEC. DEG.):	-71.8223556	ORACLE PTN # 4:	2051A13RQW	PACE JOB # 4:	MRCTB061493
LATITUDE (D-M-S):	41d 47m29.14008s	LONGITUDE (D-M-S):	-71d -49m-20.48016s	LAT (DEC. DEG.):	41.7914278	ORACLE PTN # 5:		PACE JOB # 5:	MRCTB061261
DIRECTIONS, ACCESS AND EQUIPMENT LOCATION:	QUINEBAUG VALLEY EMERGENCY COMMUNICATIONS GUYED TOWER, 812 PROVIDENCE PIKE, DANIELSON (KILLINGLY), CT 06239.COORDINATES CORRECTED FOR FRONT GUYED TOWER. BACK SELF SUPPORT IS LOADED WITH PUBLIC SAFETY WHIPS.					ORACLE PTN # 6:	2051A13RKP	PACE JOB # 6:	MRCTB061305
						ORACLE PTN # 7:		PACE JOB # 7:	MRCTB061250
						ORACLE PTN # 8:		PACE JOB # 8:	
						ORACLE PTN # 9:		PACE JOB # 9:	
						ORACLE PTN # 10:		PACE JOB # 10:	
						ORACLE PTN # 11:		PACE JOB # 11:	
						ORACLE PTN # 12:		PACE JOB # 12:	
						ORACLE PTN # 13:		PACE JOB # 13:	
						ORACLE PTN # 14:		PACE JOB # 14:	
						ORACLE PTN # 15:		PACE JOB # 15:	
						ORACLE PTN # 16:		PACE JOB # 16:	
						BORDER CELL WITH CONTOUR COORD:		SEARCH RING NAME:	
						AM STUDY REQ'D (Y/N):	No	SEARCH RING ID:	
						FREQ COORD:		BTA:	
								MSA / RSA:	
						RF DISTRICT:		LAC(UMTS):	
RF ZONE:		RNC(UMTS):							
		MME POOL ID(LTE):	FF01						
PARENT NAME(UMTS):									

Section 3 - LICENSE COVERAGE/FILING INFORMATION

CGSA - NO FILING TRIGGERED (Yes/No):	No	CGSA LOSS:		PCS REDUCED - UPS ZIP:		CGSA CALL SIGNS:
CGSA - MINOR FILING NEEDED (Yes/No):	No	CGSA EXT AGMT NEEDED:		PCS POPS REDUCED:		
CGSA - MAJOR FILING NEEDED (Yes/No):	Yes	CGSA SCORECARD UPDATED:				

Section 4 - TOWER/REGULATORY INFORMATION

STRUCTURE AT&T OWNED?:	No	GROUND ELEVATION (ft):		STRUCTURE TYPE:	GUYED	MARKET LOCATION 700 MHz Band:			
ADDITIONAL REGULATORY?:	Yes	HEIGHT OVERALL (ft):		FCC ASR NUMBER:	NR	MARKET LOCATION 850 MHz Band:			
SUB-LEASE RIGHTS?:	No	STRUCTURE HEIGHT (ft):	190.00			MARKET LOCATION 1900 MHz Band:			
LIGHTING TYPE:	NOT REQUIRED								
						MARKET LOCATION AWS Band:			
						MARKET LOCATION WCS Band:			
						MARKET LOCATION Future Band:			

	PORT 6			CTCN001166_N002A_1	CTCN001166_N002A_1	TxRx/ TxRx	5G 1900	TPA65R- BU8D_1930MHz_02D T	17.8	0	2	Top	FIBER	0	0	0							
	PORT 7			CTL01166_9A_1.CTL 01166_9A_2	CTL01166_9A_1.CTL 01166_9A_2	TxRx/ TxRx	LTE 1900	TPA65R- BU8D_1930MHz_02D T	17.8	0	2	Top	FIBER	0	0	0							
ANTENNA POSITION 2	PORT 1			CTL01166_7A_1	CTL01166_7A_1	TxRx/ TxRx	LTE 700	DMP65R- BU8D_725MHz_02DT	14.3	0	2	Top	FIBER	0	0	0							
	PORT 3			CTCN001166_N005A_1	CTCN001166_N005A_1	TxRx/ TxRx	5G 850	DMP65R- BU8D_850MHz_02DT	14.7	0	2	Top	FIBER	0	0	0							
	PORT 5			CTL01166_2A_2	CTL01166_2A_2	TxRx/ TxRx	LTE AWS	DMP65R- BU8D_2170MHz_02D T	16.7	0	2	Top	FIBER	0	0	0							
	PORT 6			CTCN001166_N066A_1	CTCN001166_N066A_1	TxRx/ TxRx	5G AWS	DMP65R- BU8D_2170MHz_02D T	16.7	0	2	Top	FIBER	0	0	0							

	PORT 6			CTCN001166_N002B _1	CTCN001166_N002B _1	TxRx/ TxRx	5G 1900	TPA65R- BU8D_1930MHz_02D T	17.8	150	2	Top	FIBER	0	0	0							
	PORT 7			CTL01166_9B_1.CTL 01166_9B_2	CTL01166_9B_1.CTL 01166_9B_2	TxRx/ TxRx	LTE 1900	TPA65R- BU8D_1930MHz_02D T	17.8	150	2	Top	FIBER	0	0	0							
ANTENNA POSITION 2	PORT 1			CTL01166_7B_1	CTL01166_7B_1	TxRx/ TxRx	LTE 700	DMP65R- BU8D_725MHz_02DT	14.3	150	2	Top	FIBER	0	0	0							
	PORT 3			CTCN001166_N005B _1	CTCN001166_N005B _1	TxRx/ TxRx	5G 850	DMP65R- BU8D_850MHz_02DT	14.7	150	2	Top	FIBER	0	0	0							
	PORT 5			CTL01166_2B_2	CTL01166_2B_2	TxRx/ TxRx	LTE AWS	DMP65R- BU8D_2170MHz_02D T	16.7	150	2	Top	FIBER	0	0	0							
	PORT 6			CTCN001166_N066B _1	CTCN001166_N066B _1	TxRx/ TxRx	5G AWS	DMP65R- BU8D_2170MHz_02D T	16.7	150	2	Top	FIBER	0	0	0							

Section 17A - FINAL TOWER CONFIGURATION - SECTOR A (OR OMNI)

ANTENNA POSITION is LEFT to RIGHT from BACK OF ANTENNA (unless otherwise specified)	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
ANTENNA MAKE - MODEL	TPA65R-BU8DA-K	DMP65R-BU8DA-K					
ANTENNA VENDOR	CCI Antennas	CCI Antennas					
ANTENNA SIZE (H x W x D)	96X21X7.8	96X20.7X7.7					
ANTENNA WEIGHT	83	96					
AZIMUTH	0	0					
MAGNETIC DECLINATION							
RADIATION CENTER (feet)	175	161					
ANTENNA TIP HEIGHT	179	165					
MECHANICAL DOWNTILT	0	0					
FEEDER AMOUNT							
VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)	36	36					
VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)	36	36					
HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)							
Antenna RET Motor (QTY/MODEL)	Built-in	Built-in					
SURGE ARRESTOR (QTY/MODEL)							
DIPLEXER (QTY/MODEL)							
DUPLEXER (QTY/MODEL)							
Antenna RET CONTROL UNIT (QTY/MODEL)							
DC BLOCK (QTY/MODEL)							
TMA/LNA (QTY/MODEL)							
CURRENT INJECTORS FOR TMA (QTY/MODEL)							
PDU FOR TMA (QTY/MODEL)							
FILTER (QTY/MODEL)							
SQUID (QTY/MODEL)	1	DC6-48-60-0-8C-EV	1	DC9-48-60-24-8C-EV			
FIBER TRUNK (QTY/MODEL)							
DC TRUNK (QTY/MODEL)							
REPEATER (QTY/MODEL)							
RRH - 700 band (QTY/MODEL)	1	4478 B14	1	4449 B5/B12			
RRH - 850 band (QTY/MODEL)				RRH is shared with another band			
RRH - 1900 band (QTY/MODEL)	1	4415 B25					
RRH - AWS band (QTY/MODEL)			1	4426 B66			
RRH - WCS band (QTY/MODEL)							
Additional RRH #1 - any band (QTY/MODEL)							
Additional RRH #2 - any band (QTY/MODEL)							
RRH 7B 1 (QTY/MODEL)							
RRH 7B 2 (QTY/MODEL)							
RRH 7B 3 (QTY/MODEL)							
Additional Component 1 (QTY/MODEL)							
Additional Component 2 (QTY/MODEL)							
Additional Component 3 (QTY/MODEL)							
Local Market Note 1	4 DC and 1 Fiber lines with the DC power split cable per site						
Local Market Note 2							
Local Market Note 3							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	Tx/Rx ?	TECHNOLOGY/FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None)	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID (CSSNG)
ANTENNA POSITION 1	PORT 1	314085.A.700.4G.tmp6		CTL01166_7A_3_F	CTL01166_7A_3_F	TxRx/ TxRx	LTE 700	TPA65R-BU8D_770MHz_02DT	14.9	0	2	Top	FIBER	0	0	0							
	PORT 5	314085.A.1900.4G.tmp1. 314085.A.1900.4G.tmp4		CTL01166_9A_1.CTL 01166_9A_2	CTL01166_9A_1.CTL 01166_9A_2	TxRx/ TxRx	LTE 1900	TPA65R-BU8D_1930MHz_02DT	17.8	0	2	Top	FIBER	0	0	0							
	PORT 6	314085.A.1900.5G.tmp1		CTCN001166_N002A	CTCN001166_N002A	TxRx/	5G 1900	TPA65R-	17.8	0	2	Top	FIBER	0	0	0							

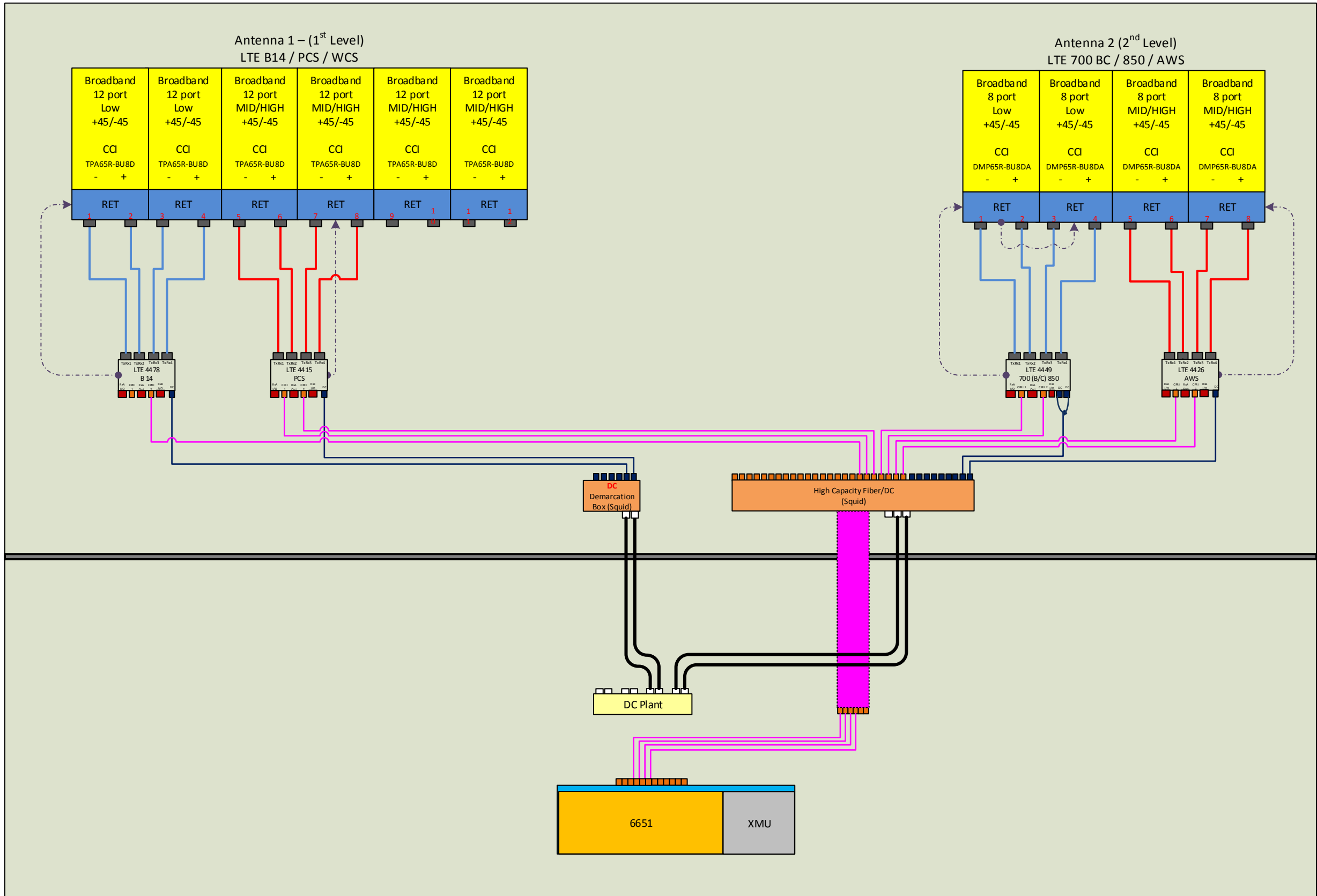
				_1	_1	TxRx		BU8D_1930MHz_02DT																
	PORT 7	314085.A.1900.4G.tmp1. 314085.A.1900.4G.tmp4		CTL01166_9A_1.CTL 01166_9A_2	CTL01166_9A_1.CTL 01166_9A_2	TxRx/ TxRx	LTE 1900	TPA65R- BU8D_1930MHz_02DT	17.8	0	2	Top	FIBER	0	0	0								
ANTENNA POSITION 2	PORT 1	314085.A.700.4G.tmp1		CTL01166_7A_1	CTL01166_7A_1	TxRx/ TxRx	LTE 700	DMP65R- BU8D_725MHz_02DT	14.3	0	2	Top	FIBER	0	0	0								
	PORT 3	314085.A.850.5G.tmp1		CTCN001166_N005A _1	CTCN001166_N005A _1	TxRx/ TxRx	5G 850	DMP65R- BU8D_850MHz_02DT	14.7	0	2	Top	FIBER	0	0	0								
	PORT 5	314085.A.AWS.4G.tmp4		CTL01166_2A_2	CTL01166_2A_2	TxRx/ TxRx	LTE AWS	DMP65R- BU8D_2170MHz_02DT	16.7	0	2	Top	FIBER	0	0	0								
	PORT 6	314085.A.AWS.5G.tmp1		CTCN001166_N066A _1	CTCN001166_N066A _1	TxRx/ TxRx	5G AWS	DMP65R- BU8D_2170MHz_02DT	16.7	0	2	Top	FIBER	0	0	0								

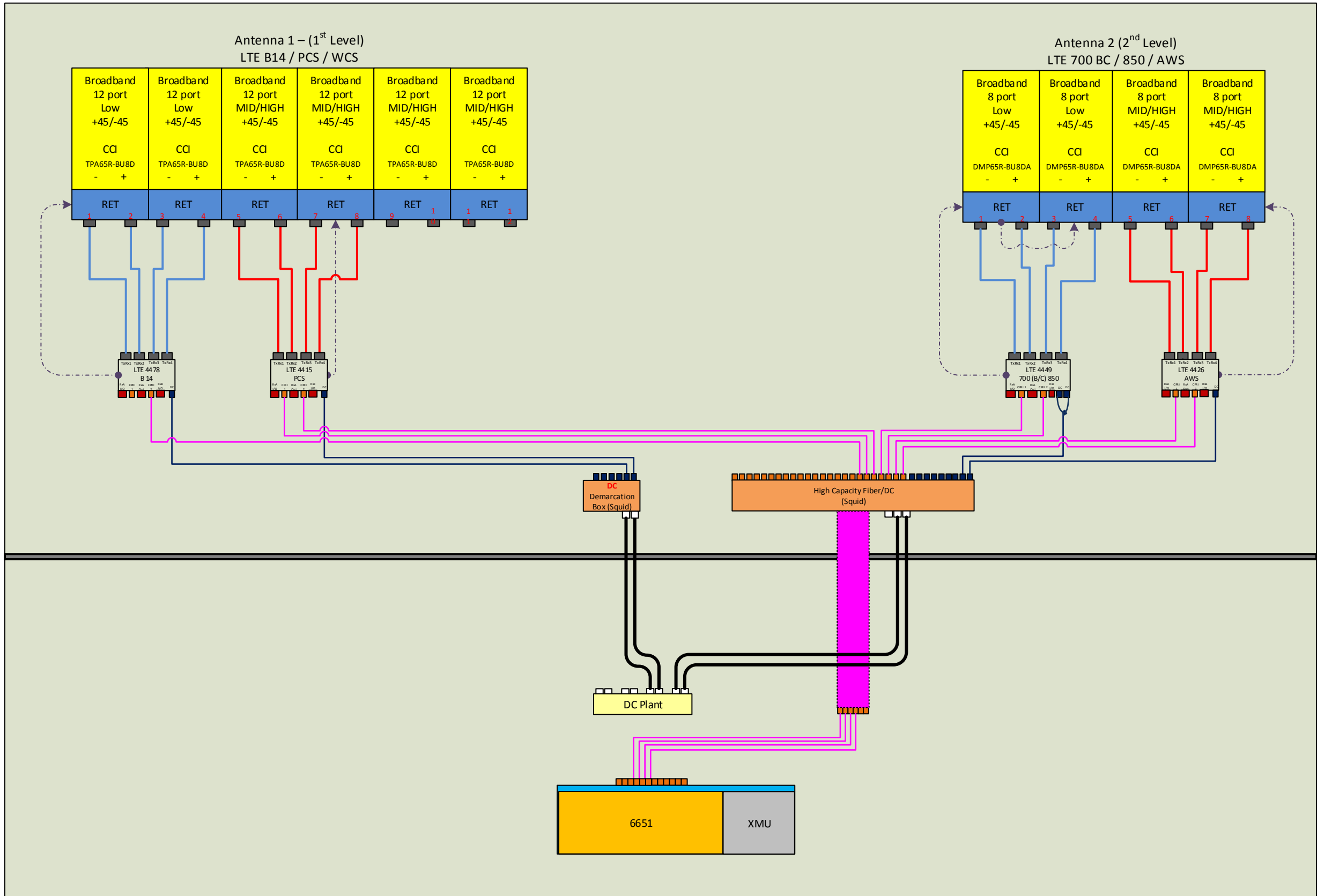
Section 17B - FINAL TOWER CONFIGURATION - SECTOR B

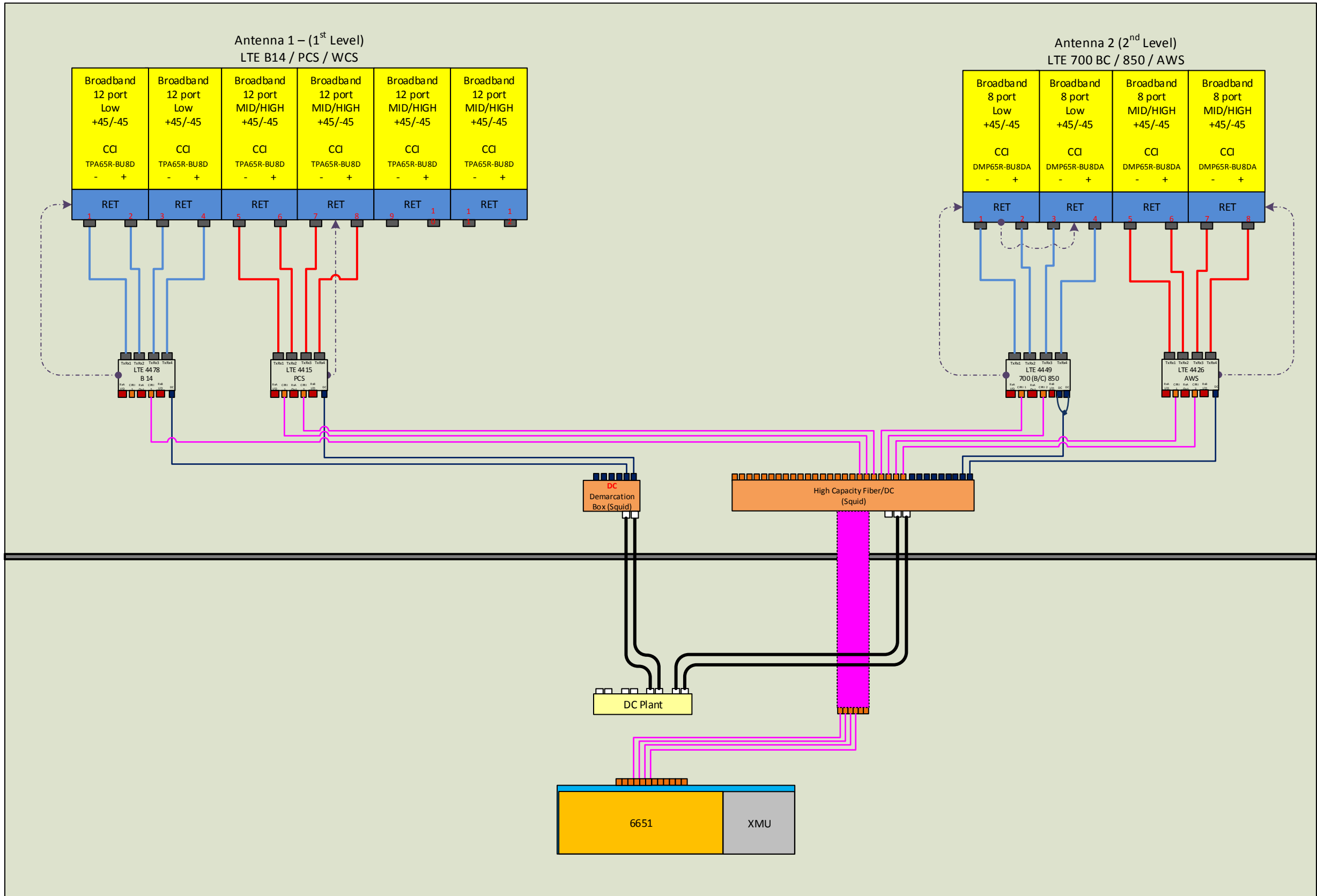
ANTENNA POSITION is LEFT to RIGHT from BACK OF ANTENNA (unless otherwise specified)	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
ANTENNA MAKE - MODEL	TPA65R-BU8DA-K	DMP65R-BU8DA-K					
ANTENNA VENDOR	CCI Antennas	CCI Antennas					
ANTENNA SIZE (H x W x D)	96X21X7.8	96X20.7X7.7					
ANTENNA WEIGHT	83	96					
AZIMUTH	150	150					
MAGNETIC DECLINATION							
RADIATION CENTER (feet)	175	161					
ANTENNA TIP HEIGHT	179	165					
MECHANICAL DOWNTILT	0	0					
FEEDER AMOUNT							
VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)	36	36					
VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)	36	36					
HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)							
Antenna RET Motor (QTY/MODEL)	Built-in	Built-in					
SURGE ARRESTOR (QTY/MODEL)							
DIPLEXER (QTY/MODEL)							
DUPLEXER (QTY/MODEL)							
Antenna RET CONTROL UNIT (QTY/MODEL)							
DC BLOCK (QTY/MODEL)							
TMA/LNA (QTY/MODEL)							
CURRENT INJECTORS FOR TMA (QTY/MODEL)							
PDU FOR TMA (QTY/MODEL)							
FILTER (QTY/MODEL)							
SQUID (QTY/MODEL)							
FIBER TRUNK (QTY/MODEL)							
DC TRUNK (QTY/MODEL)							
REPEATER (QTY/MODEL)							
RRH - 700 band (QTY/MODEL)	1	4478 B14	1	4449 B5/B12			
RRH - 850 band (QTY/MODEL)				RRH is shared with another band			
RRH - 1900 band (QTY/MODEL)	1	4415 B25					
RRH - AWS band (QTY/MODEL)			1	4426 B66			
RRH - WCS band (QTY/MODEL)							
Additional RRH #1 - any band (QTY/MODEL)							
Additional RRH #2 - any band (QTY/MODEL)							
RRH 7B 1 (QTY/MODEL)							
RRH 7B 2 (QTY/MODEL)							
RRH 7B 3 (QTY/MODEL)							
Additional Component 1 (QTY/MODEL)							
Additional Component 2 (QTY/MODEL)							
Additional Component 3 (QTY/MODEL)							
Local Market Note 1	4 DC and 1 Fiber lines with the DC power split cable per site						
Local Market Note 2							
Local Market Note 3							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	Tx/Rx ?	TECHNOLOGY/FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None)	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID (CSSNG)
ANTENNA POSITION 1	PORT 1	314085.B.700.4G.tmp6		CTL01166_7B_3_F	CTL01166_7B_3_F	TxRx/ TxRx	LTE 700	TPA65R-BU8D_770MHz_02DT	14.9	150	2	Top	FIBER	0	0	0							
	PORT 5	314085.B.1900.4G.tmp1, 314085.B.1900.4G.tmp4		CTL01166_9B_1.CTL01166_9B_2	CTL01166_9B_1.CTL01166_9B_2	TxRx/ TxRx	LTE 1900	TPA65R-BU8D_1930MHz_02DT	17.8	150	2	Top	FIBER	0	0	0							
	PORT 6	314085.B.1900.5G.tmp1		CTCN001166_N002B	CTCN001166_N002B	TxRx/	5G 1900	TPA65R-	17.8	150	2	Top	FIBER	0	0	0							

				..1	..1	TxRx		BU8D_1930MHz_02DT														
	PORT 7	314085.B.1900.4G.tmp1, 314085.B.1900.4G.tmp4		CTL01166_9B_1.CTL 01166_9B_2	CTL01166_9B_1.CTL 01166_9B_2	TxRx/ TxRx	LTE 1900	TPA65R- BU8D_1930MHz_02DT	17.8	150	2	Top	FIBER	0	0	0						
ANTENNA POSITION 2	PORT 1	314085.B.700.4G.tmp1		CTL01166_7B_1	CTL01166_7B_1	TxRx/ TxRx	LTE 700	DMP65R- BU8D_725MHz_02DT	14.3	150	2	Top	FIBER	0	0	0						
	PORT 3	314085.B.850.5G.tmp1		CTCN001166_N005B ..1	CTCN001166_N005B ..1	TxRx/ TxRx	5G 850	DMP65R- BU8D_850MHz_02DT	14.7	150	2	Top	FIBER	0	0	0						
	PORT 5	314085.B.AWS.4G.tmp4		CTL01166_2B_2	CTL01166_2B_2	TxRx/ TxRx	LTE AWS	DMP65R- BU8D_2170MHz_02DT	16.7	150	2	Top	FIBER	0	0	0						
	PORT 6	314085.B.AWS.5G.tmp1		CTCN001166_N066B ..1	CTCN001166_N066B ..1	TxRx/ TxRx	5G AWS	DMP65R- BU8D_2170MHz_02DT	16.7	150	2	Top	FIBER	0	0	0						







NOTES

Date Time (Eastern)	Version	ATTUID	Note
6/3/2022 1:25:28 PM	2.00	ra9161	RFDS VERSION incremented.
8/26/2022 5:14:23 PM	3.00	mh705r	RFDS VERSION incremented.
10/14/2022 10:42:41 AM	4.00	ra9161	RFDS VERSION incremented.