December 10, 2018

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification for Verizon Wireless: 876363 <br> Verizon Site ID: 79283 <br> 219 New Park Ave. Hartford, CT 06141-0270 <br> Latitude: $41^{\circ}-45^{\prime}-2.79^{\prime \prime} /$ Longitude: $\mathbf{7 2}^{\circ}-42^{\prime} 43.23^{\prime \prime}$

Dear Ms. Bachman:

Verizon currently maintains twelve (12) antennas at the 105 -foot level of the existing 108 -foot monopole tower at 219 New park Ave. Hartford, CT 06141-0270. The tower is owned by Crown Castle. The Connecticut Light and Power Company own the property. Verizon now intends to remove three (3) RRH's, replace six (6) RRH's. Verizon also intends to replace one (1) OVP and one (1) hybrid cable and remove six (6) coaxial cables.

This facility was approved by the City of Hartford in the mid-2000 and an email was sent to the town on 12/06/2018 in an effort to ascertain the original zoning documents.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j73 , for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to Mayor Luke Bronin, City of Hartford, John Collins, Building Official, City of Hartford, the property owner, and Crown Castle is the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Verizon respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § $16-$ $50 \mathrm{j}-72(\mathrm{~b})(2)$. Please send approval/rejection letter to Attn: Jeffrey Barbadora.


Real Estate Specialist
12 Gill Street, Suite 5800, Woburn, MA 01801
781-729-0053
Jeff.Barbadora@crowncastle.com
Attachments:
Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes
Tab 2: Exhibit-2: Structural Modification Report
Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)
cc: City Mayor Luke Bronin
550 Main St \#1, Hartford, CT 06103

Building Official John Collins
550 Main St \#1,
Hartford, CT 06103
Connecticut Light and Power 107 Selden St.
C/O corporate Property
Management Department
Berlin, CT 06037

# Unofficial Property Record Card - City of Hartford, CT <br> General Property Data 

Parcel ID 138-472-001<br>Prior Parcel ID<br>Property Owner CONN LIGHT \& POWER CO<br>Mailing Address PO BOX 270<br>Account Number<br>Property Location 219 NEW PARK AVE HARTFORD Property Use OTHER UTILTY<br>Most Recent Sale Date 7/2/1982<br>Legal Reference 019770129<br>City HARTFORD<br>Mailing State CT Zip 06141-0270<br>Grantor<br>Sale Price 0<br>Land Area 311,018.000 square feet

## Current Property Assessment

Card 1 Value Building Value 12,460 | Xtra Features |
| :---: |
| Value | 10,570 Land Value 1,094,870 Total Value 1,117,900

## Building Description

Building Style WAREHSE
\# of Living Units 0
Year Built 1978
Building Grade Economy
Building Condition N/A
Finished Area (SF) 1632
Number Rooms 0
\# of 3/4 Baths 0

Foundation Type Concrete Frame Type Steel Light
Roof Structure GABLE/HIP Roof Cover Metal Siding Metal Interior Walls DRYWALL
\# of Bedrooms 0
\# of $1 / 2$ Baths 0

Flooring Type COMBINATION
Basement Floor N/A
Heating Type Electric
Heating Fuel Electric
Air Conditioning 0\%
\# of Bsmt Garages 0
\# of Full Baths 0
\# of Other Fixtures 0

## Legal Description

## Narrative Description of Property

This property contains $311,018.000$ square feet of land mainly classified as OTHER UTILTY with a(n) WAREHSE style building, built about 1978 , having Metal exterior and Metal roof cover, with 0 commercial unit(s) and 0 residential unit(s), 0 room( $s$ ), 0 bedroom(s), 0 bath(s), 0 half bath(s).

## Property Images



Disclaimer: This information is believed to be correct but is subject to change and is not warranteed. The Property Use designation depicted on this website is for assessment purposes only, it does not guarantee or imply rights to such
use or approval of the premises for such use. Any questions regarding the approved or allowed use of a property should be confirmed with the Planning \& Economic Development Division of the City of Hartford.


## McKay, Kristian <br> Thursday, December 6, 2018 4:52 PM 'vanessa.walton@hartford.gov' Original zoning docs

$\Sigma_{\text {Paremom }}$
B+T Group
1717 S. Boulder, Suite 300
Tulsa, OK 74119
(918) 587-4630

Structural Analysis Report
Verizon Wireless Co-Locate Carrier Site Number: 79283
Carrier Site Name:
Crown Castle BU Number: Crown Castle Site Name:
Crown Castle JDE Job Number:
Crown Castle Work Order Number:
Crown Castle Order Number:
B+T Group Project Number:
West Hartford 4 CT
876363
Hartford - NU (SSUSA)
528518
1626542
457785 Rev. 0
85565.009 .01

219 New Park Rd., HARTFORD, Hartford County, CT Latitude $41^{\circ} 45^{\prime} 2.79^{\prime \prime}$, Longitude $-72^{\circ} 42^{\prime} 49.23^{\prime \prime}$
108 Foot - Monopole Tower

Dear Amanda D Brown,
$B+T$ Group is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration
Sufficient Capacity
The analysis has been performed in accordance with the TIA-222-H Standard. This analysis utilizes an ultimate 3 -second gust wind speed of 125 mph as required by the 2012 International Building Code. Exposure Category $C$ and Risk Category II were used in this analysis.

Structural analysis prepared by: Xavier Jones
Respectfully submitted by: B+T Engineering, Inc.
COA: PEC. 0001564 Expires: 02/10/2019


Scott S. Vance, P.E.

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## 1) INTRODUCTION

This tower is a 108 ft . Monopole designed by Summit in October of 2000. The tower was originally designed for a wind speed of 90 mph per TIA/EIA-222-F. This tower has been modified multiple times and those modifications were incorporated in this analysis.
2) ANALYSIS CRITERIA

| Building Code: | 2012 IBC |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| Wind Speed: | 125 mph |
| Exposure Category: | C |
| Topographic Factor: | 1 |
| Ice Thickness: | 1.7 in |
| Wind Speed with Ice: | 50 mph |
| Service Wind Speed: | 60 mph |

Table 1 - Proposed Equipment Configuration

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | $\begin{gathered} \text { Feed } \\ \text { Line Size } \\ \text { (in) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.0 | 105.0 | 3 | Alcatel Lucent | B13 RRH 4X30 | $\begin{aligned} & 1 \\ & 7 \end{aligned}$ | $\begin{aligned} & 1-5 / 8 \\ & 1-1 / 4 \end{aligned}$ |
|  |  | 3 | Alcatel Lucent | B25 RRH4X30 |  |  |
|  |  | 3 | Alcatel Lucent | RRH4X45-AWS4 B66 |  |  |
|  |  | 6 | Antel | BXA-70063/6CF |  |  |
|  |  | 6 | Commscope | SBNHH-1D65B |  |  |
|  |  | 1 | Raycap | RVZDC-6627-PF-48 |  |  |
|  |  | 1 | Rfs Celwave | DB-T1-6Z-8AB-0Z |  |  |
|  |  | 3 | Samsung Tele. | RFV01U-D1A |  |  |
|  |  | 3 | Samsung Tele. | RFV01U-D2A |  |  |
|  |  | 1 | Rfs Celwave | DB-T1-6Z-8AB-0Z |  |  |
|  |  | 1 | -- | Sector Mount [SM 402-3] |  |  |

Table 2 - Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{aligned} & \text { Number } \\ & \text { of } \\ & \text { Antennas } \end{aligned}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 98.0 | 99.0 | 3 | Nokia | AAHC | $\begin{aligned} & 4 \\ & 2 \\ & 3 \end{aligned}$ | 1-1/4 |
|  |  | 1 | Rfs Celwave | APXV9ERR18-C-A20 |  |  |
|  |  | 2 | Rfs Celwave | APXVSPP18-C-A20 |  |  |
|  | 98.0 | 3 | Rfs Celwave | IBC1900BB-1 |  |  |
|  |  | 3 | Rfs Celwave | IBC1900HG-2A |  |  |
|  |  | 1 | -- | Platform Mount [LP 1201-1] |  |  |
| 96.0 | 96.0 | 3 | Alcatel Lucent | $800 \mathrm{MHz} 2 \times 50 \mathrm{~W}$ RRH W/FILTER | -- | -- |
|  |  | 3 | Alcatel Lucent | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ |  |  |
|  |  | 1 | -- | Side Arm Mount [SO 102-3] |  |  |
|  | 95.0 | 3 | Alcatel Lucent | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ |  |  |


| Mounting <br> Level (ft) | Center <br> Line <br> Elivation <br> (ft) | Number <br> of <br> Antennas | Antenna <br> Manufacturer | Antenna Model | Number <br> of Feed <br> Lines | Feed <br> Line Size <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81.0 | 81.0 | 1 | -- | T-Arm Mount [TA 602-3] | 6 | $7 / 8$ |
|  | 80.0 | 3 | Andrew | HBX-6516DS-VTM | 1 | $5 / 16$ |
|  | 76.0 | 1 | Lucent | KS24019-L112A | 1 | $1 / 2$ |

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Online Order Information | Verizon Wireless Co-Locate, Rev. 0 | 457785 | CCI Sites |
| Tower Manufacturer Drawing | Summit, Job No. 11049 | 1947570 | CCI Sites |
| Tower Modification Drawings | Vertical Solutions, Date: 01/28/2009 | 2445633 | CCI Sites |
| Post Modification Inspection | PJF, Date: $10 / 25 / 2010$ | 2445631 | CCI Sites |
| Tower Modification Drawings | B+T Group, Date: $10 / 15 / 2012$ | 3348853 | CCI Sites |
| Post Modification Inspection | TEP, Date: $12 / 20 / 2013$ | 4424435 | CCI Sites |
| Tower Modification Drawings | B+T Group, Date: $05 / 16 / 2017$ | 6859034 | CCI Sites |
| Post Modification Inspection | ETS, Date: $12 / 07 / 2017$ | 7243678 | CCI Sites |
| Foundation Drawings | Summit, Job No. 11049 | 1613616 | CCI Sites |
| Geotech Report | FDH, Project No. 08-10012E G1 | 2337384 | CCI Sites |
| Antenna Configuration | Crown CAD Package | Date: $08 / 30 / 2018$ | CCI Sites |

## 3.1) Analysis Method

tnxTower (version 8.0.4.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) Mount areas and weights are assumed based on photographs provided.
5) The existing base plate grout was not considered in this analysis.
6) The existing base plate grout was considered in this analysis. Grout must be maintained and

This analysis may be affected if any assumptions are not valid or have been made in error. $\mathrm{B}+\mathrm{T}$ Group should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

| Section <br> No. | Elevation (ft) | Component <br> Type | Size | Critical <br> Element | $\mathbf{P ( K )}$ | SF*P_allow <br> (K) | \% <br> Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $108-103$ | Pole | TP8.625x8.625x0.313 | 1 | -2.346 | 269.918 | $24.4 \%$ | Pass |


| $\begin{gathered} \text { Section } \\ \text { No. } \\ \hline \end{gathered}$ | Elevation (ft) | Component Type | Size | Critical Element | P (K) | SF*P_allow (K) |  | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | 103-98.5 | Pole | TP8.625×8.625 $\times 0.313$ | 2 | -2.563 | 269.918 | 74.3\% | Pass |
| L3 | 98.5-98 | Pole | TP16.5 $\times 16.5 \times 0.313$ | 3 | -2.609 | 525.629 | 21.3\% | Pass |
| L4 | 98-93 | Pole | TP17.3×16.5 $\times 0.188$ | 4 | -6.988 | 794.471 | 36.9\% | Pass |
| L5 | 93-88 | Pole | TP18.101×17.3×0.188 | 5 | -7.367 | 830.635 | 52.2\% | Pass |
| L6 | 88-83 | Pole | TP18.901×18.101×0.188 | 6 | -7.789 | 858.446 | 65.7\% | Pass |
| L7 | 83-82.33 | Pole | TP19.008×18.901×0.188 | 7 | -7.851 | 862.113 | 67.4\% | Pass |
| L8 | 82.33-82.08 | Pole | TP19.048×19.008×0.325 | 8 | -7.886 | 1506.666 | 57.4\% | Pass |
| L9 | 82.08-77.08 | Pole | TP19.848×19.048×0.319 | 9 | -9.465 | 1541.347 | 69.0\% | Pass |
| L10 | 77.08-76.25 | Pole | TP19.981×19.84880.319 | 10 | -9.566 | 1551.837 | 70.8\% | Pass |
| L11 | 76.25-76 | Pole | TP20.021×19.981×0.456 | 11 | -9.614 | 2210.239 | 55.8\% | Pass |
| L12 | 76-74.5 | Pole | TP20.261×20.021×0.45 | 12 | -9.847 | 2207.415 | 58.5\% | Pass |
| L13 | 74.5-74.25 | Pole | TP20.301 $\times 20.261 \times 0.588$ | 13 | -9.902 | 2867.718 | 51.3\% | Pass |
| L14 | 74.25-69.25 | Pole | TP21.102×20.301×0.575 | 14 | -10.84 | 2922.423 | 59.1\% | Pass |
| L15 | 69.25-64.25 | Pole | TP21.902x21.102×0.55 | 15 | -11.729 | 2907.744 | 66.6\% | Pass |
| L16 | 64.25-59.25 | Pole | TP22.702x21.902×0.544 | 16 | -12.64 | 2983.291 | 73.7\% | Pass |
| L17 | 59.25-58.08 | Pole | TP22.89×22.702×0.538 | 17 | -12.856 | 2974.755 | 75.3\% | Pass |
| L18 | 58.08-57.73 | Pole | TP22.946x22.89×0.713 | 18 | -12.942 | 3922.296 | 56.3\% | Pass |
| L19 | 57.73-57.5 | Pole | TP22.982x22.946x0.713 | 19 | -12.994 | 3928.785 | 56.6\% | Pass |
| L20 | 57.5-52.5 | Pole | TP23.783×22.982x0.688 | 20 | -14.096 | 3931.42 | 61.8\% | Pass |
| L21 | 52.5-47 | Pole | TP24.663×23.783×0.688 | 21 | -14.603 | 3992.73 | 64.0\% | Pass |
| 122 | 47-45.25 | Pole | TP24.568×23.768×0.75 | 22 | -16.43 | 4423.062 | 64.3\% | Pass |
| L23 | 45.25-40.5 | Pole | TP25.328×24.568×0.725 | 23 | -17.617 | 4416.583 | 68.4\% | Pass |
| L24 | 40.5-40.25 | Pole | TP25.368×25.328x0.725 | 24 | -17.69 | 4423.765 | 68.6\% | Pass |
| L25 | 40.25-35.25 | Pole | TP26.168×25.368×0.7 | 25 | -18.951 | 4414.242 | 72.7\% | Pass |
| L26 | 35.25-30.25 | Pole | TP26.969 $26.168 \times 0.688$ | 26 | -20.241 | 4473.766 | 76.6\% | Pass |
| L27 | 30.25-27.75 | Pole | TP27.369×26.969x0.675 | 27 | -20.893 | 4461.387 | 78.4\% | Pass |
| L28 | 27.75-27.5 | Pole | TP27.409×27.369×0.725 | 28 | -20.974 | 4790.068 | 69.5\% | Pass |
| L29 | 27.5-22.5 | Pole | TP28.209x27.409x0.7 | 29 | -22.35 | 4767.924 | 72.7\% | Pass |
| L30 | 22.5-19.5 | Pole | TP28.689×28.209x0.688 | 30 | -23.192 | 4766.643 | 74.6\% | Pass |
| L31 | 19.5-19.25 | Pole | TP28.729×28.689×0.8 | 31 | -23.276 | 5532.271 | 69.6\% | Pass |
| L32 | 19.25-14.25 | Pole | TP29.529x28.729x0.775 | 32 | -24.763 | 5517.739 | 72.5\% | Pass |
| L33 | 14.25-14 | Pole | TP29.569×29.529x0.775 | 33 | -24.847 | 5525.425 | 72.7\% | Pass |
| L34 | 14-13.75 | Pole | TP29.609×29.569x0.775 | 34 | -24.927 | 5533.101 | 73.2\% | Pass |
| L35 | 13.75-12.98 | Pole | TP29.733×29.609x0.8 | 35 | -25.176 | 5731.047 | 69.2\% | Pass |
| L36 | 12.98-12.73 | Pole | TP29.773x29.733x0.8 | 36 | -25.263 | 5738.974 | 69.3\% | Pass |
| L37 | 12.73-7.73 | Pole | TP30.573×29.773×0.788 | 37 | -26.904 | 5807.77 | 72.0\% | Pass |
| L38 | 7.73-2.73 | Pole | TP31.373 $30.573 \times 0.775$ | 38 | -28.571 | 5871.537 | 74.6\% | Pass |
| L39 | 2.73-0 | Pole | TP31.81×31.373×0.763 | 39 | -29.489 | 5861.688 | 75.9\% | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L2) | 74.3\% | Pass |
|  |  |  |  |  |  | Reinforcement | 78.4\% | Pass |
|  |  |  |  |  |  | Rating = | 78.4\% | Pass |

Table 5 - Tower Component Stresses vs. Capacity - LC7

| Notes | Component | Elevation (ft) | $\%$ Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Flange Connection | Base | 86.6 | Pass |
| 1 | Anchor Rods | Base | 68.8 | Pass |
| 1 | Base Plate | Base | 56.9 | Pass |
| 1 | Base Foundation (Structure) | Base | 82.3 | Pass |
| 1 | Base Foundation (Soil Interaction) | Base | 46.8 | Pass |


| Structure Rating (max from all components) $=$ | $86.6 \%$ |
| :---: | :---: |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity
consumed.
2) Rating per TIA-222-H Section 15.5

## 4.1) Recommendations

The tower and its foundations have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

TNXTOWER OUTPUT

| Section | 39 | 38 | 37 | 防碞 $32=$ | 30 | 29 | 限27 | 26 | 252 | 43 | 22 | 21 | 20 隹7 | 16 | 15 | 14 | 18120 | $9 \quad 7$ | 7 | 6 | 5 | 43 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length（tt） | 2.730 | 5.000 | 5.000000 | Whatim 5.0000 .2 | 46.000 | 5.0000 .2 | 450500 | 5.000 | 5.0000 .2 | 504.750 |  | ， 500 |  | 5.000 | 5.000 | 5.0000. | Heareco | 5.000 cop | po | 5.000 | 5.000 | 5.0000 .50 | 04.500 | 5.000 |
| Number of Sides | 18 | 18 | 18 | 暆 18 | 限 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 ， 1818 | 18 | 18 | 18 | 8188 | 18 | 8 | 18 | 18 | 18 | 0 | 0 |
| Thickness（in） | 0.762 | 0.775 | 0.787008 |  | \＄00．688 | 0.7000 .7 | 126675 | 0.688 | 0.7000 .7 | 250.725 |  | 0.688 | 0.688 的敉如 | 0.544 | 0．550 | 0.5750 .4 | 4808189 | 0，319 oufe |  | 0.188 | 0.188 | 0.1880 .3 | 30.313 | 0.313 |
| Socket Length（ft） |  |  |  |  |  |  |  |  |  |  |  | 3.250 |  |  |  |  |  |  |  |  |  |  |  |  |
| Top Dia（in） | 31.373 | 30.573 | 29.773288 | ［ 1 （1） | 289． 209 | 27．40¢87． | ．paper | 23.168 | 25，36®5． | 2204.568 |  | 23.783 |  | 21.902 | 21.102 | 20.301200 | prsaig | 19．048198p |  | 18.101 | 17.300 | 16．50016 | 008.625 | 8.625 |
| Bot Dla（in） | 31.810 | 31.373 | 30.573298 |  | 29.689 | 28.20977 | 48936 | 26.969 | 26.16855 | 6®25．328 | 24.568 | 24.663 |  | 22.702 | 21.902 | 21.10200 | ramelig | 119.848188 |  | 18.901 | 18.101 | 17．30016 | 08．625 | 8.625 |
| Grade |  |  |  |  |  |  |  |  |  |  |  | 07－65 |  |  |  |  |  |  |  |  |  |  | A53－B－35 |  |
| Weight（K） 15.5 | 0.7 | 1.2 | 1.20 | \％atin 1.1 | ｜h 0.6 | 1.0 | 100.5 | 0.9 | 0.9 O｜｜ | 0.8 | 0.9 | 0.9 |  | 0.6 | 0.6 | 0.6 | de．201 | 0.3 op | \％ | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 |


| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| BXA－70063／6CF w／Mount Pipe（E） | 105 | APXVSPP18－C－A20 w／Mount Pipe（E） | 98 |
| BXA－70063／6CF w／Mount Pipe（E） | 105 | JBC1900BE－1（E） | 98 |
| BXA－70063／6CF w／Mount Pipe（E） | 105 | IBC1900日B－1（E） | 98 |
| DE－T1－6Z－8AB－02（E） | 105 | IEC1900日B－1（E） | 98 |
| （2）SBNHH－1D65B（P） | 105 | IBC1900HG－2A（E） | 98 |
| （2）S8NHH－1065B（P） | 105 | IBC1900HG－2A（E） | 98 |
| （2）SBNHH－1D65B（P） | 105 | IBC1900HG－2A（E） | 98 |
| BXA－70063／6CF w／Mount Pipe（P） | 105 | AAHC w／Mount Pipe（R） | 98 |
| BXA－70063／6CF w／Mount Pipe（P） | 105 | AAHC w／Mount Pipe（R） | 98 |
| EXA．70063／BCF w／Mount Pipe（P） | 105 | AAHC wl Mount Pipe（R） | 98 |
| （2）RFV01U－D1A（P） | 105 | Flatform Mount［LP 1201－1］（E） | 98 |
| RFV01U－D1A（P） | 105 | PCS 1900MHz 4x45W－65MHz（E） | 96 |
| RFV01U－D2A（P） | 105 |  | 96 |
| （2）RFV01U－D2A（P） | 105 | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$（E） | 96 |
| RVZDC－6627－PF－48（P） | 105 | PCS 1900MHz 4x45W－65MHz（E） | 96 |
| B13 RRH 4X30（P－previous App） | 105 | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$（E） | 96 |
| B13 RRH 4X30（P－previous App） | 105 | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$（E） | 96 |
| B13 RRH 4X30（P－previous App） | 105 | $800 \mathrm{MHz} 2 \times 50 \mathrm{~W}$ RRH W／FILTER（E） | 96 |
| RRH4X45－AWS4 B66（P－previous App） | 105 | 800MHz 2X50W RRH WIFILTER（E） | 96 |
|  |  | 800MHz 2X50W RRH W／FILTER（E） | 96 |
| RRH4X45－AWS4 B66（P－previousApp）RR | 105 | $4^{4} \times 2^{\prime \prime}$ Pipe Mount（E） | 96 |
|  |  | 4：$\times 2$ 2＂Pipe Mount（E） | 96 |
| RRH4X45－AWS4 B66（P－previous <br> App） | 105 | $4^{4} \times 2^{\prime \prime}$ Pipe Mount（E） | 96 |
|  |  | Side Arm Mount［SO 102－3］（E） | 90 |
| B25 RRH4X30（P－previous App） | 105 | HBX－6516DS－VTM w／Mount Pipe（E） | 81 |
| B25 RRH4X30（P－previous App） | 105 | HBX－6516DS－VTM w／Mount Pipe（E） | 81 |
| B25 RRH4X30（P－previous App） | 105 | HBX－6516DS－VTM w／Mount Pipe（E） | 81 |
| DB－T1－6Z－8AB－0Z（P－previous App） | 105 | $6^{\prime} \times 2^{\prime \prime}$ Mount Pipe（E） | 81 |
| Sector Mount［SM 402－3］ （E－2M．P／sector） | 105 | $6^{6} \times 2^{\prime \prime}$ Mount Pipe（E） | 81 |
| APXVGERR18－C－A20 w／Mouni Pipe （E） | 98 | 6＇x ${ }^{\prime \prime}$ Mount Pipe（E） | 81 |
|  |  | T－Arm Mount［TA 602－3］（E） | 81 |
| APXVSPP18－C－A20 w／Mount Pipe（E） | 98 | KS24019－L112A（E） | 74 |
|  |  | Side Arm Mount［SO 701－1］（E） | 74 |


| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A53－B－35 | 35 ksi | 63 ksi | A607－65 | 65 ksi | 80 ksi |

## TOWER DESIGN NOTES

1．Tower is located in Hartford County，Connecticut．
2．Tower designed for Exposure $C$ to the TIA－222－H Standard．
3．Tower designed for a 125 mph basic wind in accordance with the TlA－222－H Standard．
4．Tower is also designed for a 50 mph basic wind with 1.70 in ice．Ice is considered to increase in thickness with height．
5．Deflections are based upon a 60 mph wind．
6．Tower Risk Category II．
7．Topographic Category 1 with Crest Height of 0.000 ft
8．TIA－222－H Annex S
9．TOWER RATING： $83.6 \%$


TORQUE 0 kip－ft
50 mph WIND－ 1.700 in ICE


TORQUE $0 \mathrm{kip-ft}$
REACTIONS－ 125 mph WIND

|  | Pob：85565．009．01－HARTFORD－NU（SSUSA），CT（BU\＃ 87636 |  |  |
| :---: | :---: | :---: | :---: |
|  | Project：－－ |  |  |
|  | Client：Crown Castle | Drawn by xjones | App＇d： |
| $37-4630$ | Code：TIA－222－H | Date：09／21／18 | Scale：NTS |
| FAX：（918）295－0265 | Path： |  | Dwg No．E－1 |




| B+T Group  <br> B+T GRN 1717 S. Boulder, Suite 300 <br>  Tulsa, OK 7419 74 <br> Phone: (918) 587-4630  <br> FAX: $\{918) 295-0265$  |  | ${ }^{\text {Pob: } 85565.009 .01-H A R T F O R D ~-~ N U ~(S S U S A), ~ C T ~(B U \# ~} 87636$. |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  | Project:    <br> Client: Crown Castle Drawn by xjones |  |  |
|  |  | Code: Tl A-222-H | Date: 09/21/18 | Scale: NTS |
|  |  | Path: |  | Dwg No. E-4 |





| B+T Group  <br> B+T GF:F 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119  <br> Phone: (918) 587-4630  <br> FAX: (918) 295-0265  |  | Frob: 85565.009 .01 - HARTFORD - NU (SSUSA), CT (BU\# 87636 |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  | Project:   <br> Client: Crown Castle Drawn by $x$ xjones App'd: |  |  |
|  |  | Code: TIA-222-H | Date: 09/21/18 | Scale: NTS |
|  |  | Path: |  | Dwg No. E-5 |

Feed Line Distribution Chart 0' - 108'
$\qquad$
$\qquad$ App In Face $\qquad$ App Out Faca $\qquad$ Truss Leg


| B+T Group  <br> B+T GN: 1717 S. Boulder, Suite 300 <br> Tuls, OK 74119  <br> Phone: (918) 587-4630  <br> FAX: (918) 295-0265  |  | Pob: 85565.009.01 - HARTFORD - NU (SSUSA),CT (BU\# 87636 |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{\text {Client }}$ Crown Castle | Drawn by xjones | App |
|  |  | Code: $\mathrm{T} \mid \mathrm{A}-222-\mathrm{H}$ | Date: 09/21/18 | Scale: NTS |
|  |  |  |  | Wg No. E-7 |

## tnxTower

B+TGroup
1717 S. Boulder, Suite 300
Tulsa, OK 74119
Phone: (918) 587-4630
FAX: (918) 295-0265

| $\text { Job } 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# } 876363 \text { ) }$ | $\begin{array}{ll} \text { Page } \\ & \\ & \\ \end{array}$ |
| :---: | :---: |
| Project | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Client Crown Castle | Designed by xjones |

## Tower Input Data

The tower is a monopole.
This tower is designed using the TLA-222-H standard.
The following design criteria apply:
Tower is located in Hartford County, Connecticut.
Tower base elevation above sea level: 71.000 ft .
Basic wind speed of 125 mph .
Risk Category II.
Exposure Category C.
Simplified Topographic Factor Procedure for wind speed-up calculations is used.
Topographic Category: 1.
Crest Height 0.000 ft .
Nominal ice thickness of 1.700 in .
Ice thickness is considered to increase with height.
Ice density of 56.000 pcf .
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50.000^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
TLA-222-H Annex S.
TOWER RATING: 83.6\%.
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1.05 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section
Secondary Horizontal Braces Leg
Use Diamond Inner Bracing (4 Sided)
SR Members Have Cut Ends
SR Members Are Concentric

Distribute Leg Loads As Uniform
Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area
Use Clear Spans For KL/r
Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\checkmark$ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\checkmark$ Consider Feed Line Torque
Include Angle Block Shear Check
Use TIA-222-H Bracing Resist. Exemption
Use TIA-222-H Tension Splice Exemption Poles
$\checkmark$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No Appurtenances
Outside and Inside Corner Radii Are
Known

| thxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 . \end{array}$ | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 2 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Section | Elevation <br> $f t$ | Section Length $f t$ | Splice <br> Length <br> $f t$ | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $\begin{gathered} 108.000-103.00 \\ 0 \end{gathered}$ | 5.000 | 0.000 | Round | 8.625 | 8.625 | 0.313 |  | $\begin{gathered} \text { A53-B-35 } \\ (35 \mathrm{ksi}) \end{gathered}$ |
| L2 | 103.000-98.500 | 4.500 | 0.000 | Round | 8.625 | 8.625 | 0.313 |  | $\begin{gathered} \text { A53-B-35 } \\ (35 \mathrm{ksi}) \end{gathered}$ |
| L3 | 98.500-98.000 | 0.500 | 0.000 | Round | 16.500 | 16.500 | 0.313 |  | $\begin{gathered} \text { A53-B- } 35 \\ (35 \mathrm{ksi}) \end{gathered}$ |
| L4 | 98.000-93.000 | 5.000 | 0.000 | 18 | 16.500 | 17.300 | 0.188 | 0.750 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L5 | 93.000-88.000 | 5.000 | 0.000 | 18 | 17.300 | 18.101 | 0.188 | 0.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L6 | 88.000-83.000 | 5.000 | 0.000 | 18 | 18.101 | 18.901 | 0.188 | 0.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L7 | 83.000-82.330 | 0.670 | 0.000 | 18 | 18.901 | 19.008 | 0.188 | 0.750 | $\begin{gathered} \mathrm{A} 607-65 \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L8 | 82.330-82.080 | 0.250 | 0.000 | 18 | 19.008 | 19.048 | 0.325 | 1.300 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L9 | 82.080-77.080 | 5.000 | 0.000 | 18 | 19.048 | 19.848 | 0.319 | 1.275 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L10 | $77.080-76.250$ | 0.830 | 0.000 | 18 | 19.848 | 19.981 | 0.319 | 1.275 | A607-65 <br> ( 65 ksi ) |
| L11 | 76.250-76.000 | 0.250 | 0.000 | 18 | 19.981 | 20.021 | 0.456 | 1.825 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L12 | $76.000-74.500$ | 1.500 | 0.000 | 18 | 20.021 | 20.261 | 0.450 | 1.800 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L13 | $74.500-74.250$ | 0.250 | 0.000 | 18 | 20.261 | 20.301 | 0.588 | 2.350 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L14 | 74.250-69.250 | 5.000 | 0.000 | 18 | 20.301 | 21.102 | 0.575 | 2.300 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L15 | 69.250-64.250 | 5.000 | 0.000 | 18 | 21.102 | 21.902 | 0.550 | 2.200 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L16 | 64.250-59.250 | 5.000 | 0.000 | 18 | 21.902 | 22.702 | 0.544 | 2.175 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L17 | 59.250-58.080 | 1.170 | 0.000 | 18 | 22.702 | 22.890 | 0.537 | 2.150 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L18 | 58.080-57.730 | 0.350 | 0.000 | 18 | 22.890 | 22.946 | 0.713 | 2.850 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L19 | $57.730-57.500$ | 0.230 | 0.000 | 18 | 22.946 | 22.982 | 0.713 | 2.850 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L20 | 57.500-52.500 | 5.000 | 0.000 | 18 | 22.982 | 23.783 | 0.688 | 2.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L21 | $52.500-47.000$ | 5.500 | 3.250 | 18 | 23.783 | 24.663 | 0.688 | 2.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L22 | 47.000-45.250 | 5.000 | 0.000 | 18 | 23.768 | 24.568 | 0.750 | 3.000 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L23 | 45.250-40.500 | 4.750 | 0.000 | 18 | 24.568 | 25.328 | 0.725 | 2.900 | $\begin{aligned} & \mathrm{A} 607-65 \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L24 | 40.500-40.250 | 0.250 | 0.000 | 18 | 25.328 | 25.368 | 0.725 | 2.900 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L25 | 40.250-35.250 | 5.000 | 0.000 | 18 | 25.368 | 26.168 | 0.700 | 2.800 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L26 | $35.250-30.250$ | 5.000 | 0.000 | 18 | 26.168 | 26.969 | 0.688 | 2.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L27 | 30.250-27.750 | 2.500 | 0.000 | 18 | 26.969 | 27.369 | 0.675 | 2.700 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L28 | 27.750-27.500 | 0.250 | 0.000 | 18 | 27.369 | 27.409 | 0.725 | 2.900 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L29 | 27.500-22.500 | 5.000 | 0.000 | 18 | 27.409 | 28.209 | 0.700 | 2.800 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L30 | 22.500-19.500 | 3.000 | 0.000 | 18 | 28.209 | 28.689 | 0.688 | 2.750 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |



| Section | Elevation <br> $f t$ | Section Length $f t$ | Splice Length $f t$ | Number of Sides | Top Diameter in | Bottom <br> Diameter <br> in | Wall Thiclness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L31 | 19.500-19.250 | 0.250 | 0.000 | 18 | 28.689 | 28.729 | 0.800 | 3.200 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L32 | 19.250-14.250 | 5.000 | 0.000 | 18 | 28.729 | 29.529 | 0.775 | 3.100 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L33 | 14.250-14.000 | 0.250 | 0.000 | 18 | 29.529 | 29.569 | 0.775 | 3.100 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L34 | 14.000-13.750 | 0.250 | 0.000 | 18 | 29.569 | 29.609 | 0.775 | 3.100 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L35 | 13.750-12.980 | 0.770 | 0.000 | 18 | 29.609 | 29.733 | 0.800 | 3.200 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L36 | 12.980-12.730 | 0.250 | 0.000 | 18 | 29.733 | 29.773 | 0.800 | 3.200 | $\begin{gathered} \mathrm{A} 607-65 \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L37 | 12.730-7.730 | 5.000 | 0.000 | 18 | 29.773 | 30.573 | 0.787 | 3.150 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L38 | 7.730-2.730 | 5.000 | 0.000 | 18 | 30.573 | 31.373 | 0.775 | 3.100 | $\begin{aligned} & \text { A607-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L39 | $2.730-0.000$ | 2.730 |  | 18 | 31.373 | 31.810 | 0.762 | 3.050 | $\begin{aligned} & \text { A } 607-65 \\ & (65 \mathrm{ksi}) \end{aligned}$ |

Tapered Pole Properties

| Section | Tip Dia. in | Area $\mathrm{in}^{2}$ | $\begin{gathered} I \\ i n^{4} \end{gathered}$ | $\begin{aligned} & r \\ & \text { in } \end{aligned}$ | $\begin{aligned} & C \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{I} / \mathrm{C} \\ & \mathrm{in}^{3} \\ & \hline \end{aligned}$ | $\begin{gathered} J \\ i n^{4} \end{gathered}$ | $\begin{gathered} I t / Q \\ i n^{2} \\ \hline \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \\ & \hline \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 8.625 | 8.161 | 70.586 | 2.941 | 4.313 | 16.368 | 141.172 | 4.078 | 0.000 | 0 |
|  | 8.625 | 8.161 | 70.586 | 2.941 | 4.313 | 16.368 | 141.172 | 4.078 | 0.000 | 0 |
| L2 | 8.625 | 8.161 | 70.586 | 2.941 | 4.313 | 16.368 | 141.172 | 4.078 | 0.000 | 0 |
|  | 8.625 | 8.161 | 70.586 | 2.941 | 4.313 | 16.368 | 141.172 | 4.078 | 0.000 | 0 |
| L3 | 16.500 | 15.892 | 520.728 | 5.724 | 8.250 | 63.119 | 1041.456 | 7.941 | 0.000 | 0 |
|  | 16.500 | 15.892 | 520.728 | 5.724 | 8.250 | 63.119 | 1041.456 | 7.941 | 0.000 | 0 |
| L4 | 16.726 | 9.708 | 326.368 | 5.791 | 8.382 | 38.937 | 653.165 | 4.855 | 2.574 | 13.728 |
|  | 17.538 | 10.184 | 376.798 | 6.075 | 8.789 | 42.874 | 754.091 | 5.093 | 2.715 | 14.479 |
| L5 | 17.538 | 10.184 | 376.798 | 6.075 | 8.789 | 42.874 | 754.091 | 5.093 | 2.715 | 14.479 |
|  | 18.351 | 10.661 | 432.172 | 6.359 | 9.195 | 47.000 | 864.913 | 5.331 | 2.856 | 15.23 |
| L6 | 18.351 | 10.661 | 432.172 | 6.359 | 9.195 | 47.000 | 864.913 | 5.331 | 2.856 | 15.23 |
|  | 19.164 | 11.137 | 492.723 | 6.643 | 9.602 | 51.316 | 986.094 | 5.569 | 2.997 | 15.982 |
| L7 | 19.164 | 11.137 | 492.723 | 6.643 | 9.602 | 51.316 | 986.094 | 5.569 | 2.997 | 15.982 |
|  | 19.272 | 11.201 | 501.242 | 6.681 | 9.656 | 51.909 | 1003.144 | 5.601 | 3.015 | 16.082 |
| L8 | 19.251 | 19.273 | 849.916 | 6.633 | 9.656 | 88.018 | 1700.951 | 9.638 | 2.773 | 8.534 |
|  | 19.292 | 19.314 | 855.389 | 6.647 | 9.676 | 88.399 | 1711.903 | 9.659 | 2.780 | 8.555 |
| L9 | 19.293 | 18.949 | 839.779 | 6.649 | 9.676 | 86.786 | 1680.664 | 9.476 | 2.791 | 8.758 |
|  | 20.105 | 19.758 | 952.094 | 6.933 | 10.083 | 94.426 | 1905.442 | 9.881 | 2.932 | 9.199 |
| L10 | 20.105 | 19.758 | 952.094 | 6.933 | 10.083 | 94.426 | 1905.442 | 9.881 | 2.932 | 9.199 |
|  | 20.240 | 19.893 | 971.656 | 6.980 | 10.150 | 95.725 | 1944.591 | 9.948 | 2.956 | 9.273 |
| L11 | 20.219 | 28.275 | 1361.828 | 6.931 | 10.150 | 134.164 | 2725.448 | 14.140 | 2.714 | 5.948 |
|  | 20.260 | 28.333 | 1370.218 | 6.946 | 10.171 | 134.721 | 2742.239 | 14.169 | 2.721 | 5.963 |
| L12 | 20.261 | 27.954 | 1352.744 | 6.948 | 10.171 | 133.002 | 2707.267 | 13.979 | 2.732 | 6.071 |
|  | 20.505 | 28.297 | 1403.141 | 7.033 | 10.293 | 136.323 | 2808.128 | 14.151 | 2.774 | 6.164 |
| L13 | 20.483 | 36.686 | 1794.000 | 6.984 | 10.293 | 174.297 | 3590.361 | 18.347 | 2.532 | 4.31 |
|  | 20.524 | 36.761 | 1804.969 | 6.998 | 10.313 | 175.017 | 3612.313 | 18.384 | 2.539 | 4.322 |
| L14 | 20.526 | 36.002 | 1769.928 | 7.003 | 10.313 | 171.619 | 3542.184 | 18.004 | 2.561 | 4.454 |
|  | 21.339 | 37.462 | 1994.202 | 7.287 | 10.720 | 186.032 | 3991.027 | 18.735 | 2.702 | 4.699 |
| L15 | 21.342 | 35.877 | 1914.475 | 7.296 | 10.720 | 178.595 | 3831.470 | 17.942 | 2.746 | 4.993 |
|  | 22.155 | 37.274 | 2146.949 | 7.580 | 11.126 | 192.963 | 4296.724 | 18.641 | 2.887 | 5.249 |
| L16 | 22.156 | 36.861 | 2124.417 | 7.582 | 11.126 | 190.938 | 4251.629 | 18.434 | 2.898 | 5.329 |
|  | 22.969 | 38.243 | 2372.283 | 7.866 | 11.533 | 205.700 | 4747.687 | 19.125 | 3.039 | 5.588 |
| L17 | 22.970 | 37.814 | 2347.000 | 7.868 | 11.533 | 203.507 | 4697.088 | 18.910 | 3.050 | 5.674 |



| Section | Tip Dia. <br> in | Area in $^{2}$ | $\begin{aligned} & \bar{I} \\ & i n^{4} \end{aligned}$ | in | $\begin{aligned} & \bar{C} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\begin{aligned} & J \\ & i n^{4} \end{aligned}$ | $\begin{gathered} \text { It/Q } \\ i i^{2} \\ \hline \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \\ & \hline \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L18 | 23.160 | 38.133 | 2406.993 | 7.935 | 11.628 | 207.002 | 4817.153 | 19.070 | 3.083 | 5.735 |
|  | 23.133 | 50.153 | 3116.309 | 7.873 | 11.628 | 268.003 | 6236.718 | 25.081 | 2.775 | 3.894 |
|  | 23.190 | 50.280 | 3139.984 | 7.893 | 11.656 | 269.380 | 6284.100 | 25.145 | 2.784 | 3.908 |
| L19 | 23.190 | 50.280 | 3139.984 | 7.893 | 11.656 | 269.380 | 6284.100 | 25.145 | 2.784 | 3.908 |
|  | 23.227 | 50.363 | 3155.608 | 7.906 | 11.675 | 270.286 | 6315.367 | 25.186 | 2.791 | 3.917 |
| L20 | 23.231 | 48.650 | 3055.151 | 7.915 | 11.675 | 261.682 | 6114.321 | 24.330 | 2.835 | 4.123 |
|  | 24.044 | 50.397 | 3396.104 | 8.199 | 12.082 | 281.097 | 6796.676 | 25.203 | 2.976 | 4.328 |
| L21 | 24.044 | 50.397 | 3396.104 | 8.199 | 12.082 | 281.097 | 6796.676 | 25.203 | 2.976 | 4.328 |
|  | 24.937 | 52.318 | 3799.444 | 8.511 | 12.529 | 303.257 | 7603.888 | 26.164 | 3.131 | 4.554 |
| L22 | 24.547 | 54.794 | 3667.732 | 8.171 | 12.074 | 303.770 | 7340.290 | 27.402 | 2.863 | 3.818 |
|  | 24.831 | 56.699 | 4063.713 | 8.455 | 12.481 | 325.603 | 8132.772 | 28.355 | 3.004 | 4.005 |
| L23 | 24.835 | 54.866 | 3940.638 | 8.464 | 12.481 | 315.742 | 7886.461 | 27.438 | 3.048 | 4.204 |
|  | 25.607 | 56.616 | 4329.712 | 8.734 | 12.867 | 336.504 | 8665.120 | 28.313 | 3.182 | 4.389 |
| L24 | 25.607 | 56.616 | 4329.712 | 8.734 | 12.867 | 336.504 | 8665.120 | 28.313 | 3.182 | 4.389 |
|  | 25.648 | 56.708 | 4350.870 | 8.748 | 12.887 | 337.615 | 8707.464 | 28.359 | 3.189 | 4.398 |
| L25 | 25.652 | 54.808 | 4213.638 | 8.757 | 12.887 | 326.966 | 8432.819 | 27.409 | 3.233 | 4.618 |
|  | 26.464 | 56.586 | 4637.144 | 9.041 | 13.294 | 348.826 | 9280.391 | 28.298 | 3.374 | 4.819 |
| L26 | 26.466 | 55.603 | 4561.047 | 9.046 | 13.294 | 343.102 | 9128.096 | 27.807 | 3.396 | 4.939 |
|  | 27.279 | 57.349 | 5004.396 | 9.330 | 13.700 | 365.282 | 10015.378 | 28.680 | 3.536 | 5.144 |
| L27 | 27.281 | 56.333 | 4920.422 | 9.334 | 13.700 | 359.153 | 9847.318 | 28.172 | 3.558 | 5.272 |
|  | 27.687 | 57.190 | 5148.478 | 9.476 | 13.903 | 370.305 | 10303.731 | 28.600 | 3.629 | 5.376 |
| L28 | 27.679 | 61.311 | 5498.831 | 9.459 | 13.903 | 395.504 | 11004.898 | 30.662 | 3.541 | 4.884 |
|  | 27.720 | 61.403 | 5523.641 | 9.473 | 13.924 | 396.709 | 11054.551 | 30.708 | 3.548 | 4.894 |
| L29 | 27.724 | 59.342 | 5348.175 | 9.482 | 13.924 | 384.107 | 10703.387 | 29.676 | 3.592 | 5.131 |
|  | 28.536 | 61.120 | 5843.428 | 9.766 | 14.330 | 407.771 | 11694.546 | 30.566 | 3.733 | 5.333 |
| L30 | 28.538 | 60.055 | 5746.908 | 9.770 | 14.330 | 401.035 | 11501.379 | 30.033 | 3.755 | 5.462 |
|  | 29.026 | 61.103 | 6052.962 | 9.941 | 14.574 | 415.324 | 12113.889 | 30.557 | 3.839 | 5.584 |
| L31 | 29.008 | 70.816 | 6958.894 | 9.901 | 14.574 | 477.484 | 13926.944 | 35.415 | 3.641 | 4.552 |
|  | 29.049 | 70.918 | 6988.887 | 9.915 | 14.594 | 478.874 | 13986.970 | 35.466 | 3.648 | 4.56 |
| L32 | 29.053 | 68.763 | 6788.682 | 9.924 | 14.594 | 465.156 | 13586.297 | 34.388 | 3.692 | 4.764 |
|  | 29.865 | 70.731 | 7388.530 | 10.208 | 15.001 | 492.538 | 14786.782 | 35.372 | 3.833 | 4.946 |
| L33 | 29.865 | 70.731 | 7388.530 | 10.208 | 15.001 | 492.538 | 14786.782 | 35.372 | 3.833 | 4.946 |
|  | 29.906 | 70.830 | 749.416 | 10.222 | 15.021 | 493.928 | 14848.595 | 35.422 | 3.840 | 4.955 |
| L34 | 29.906 | 70.830 | 7419.416 | 10.222 | 15.021 | 493.928 | 14848.595 | 35.422 | 3.840 | 4.955 |
|  | 29.947 | 70.928 | 7450.387 | 10.236 | 15.042 | 495.320 | 14910.577 | 35.471 | 3.847 | 4.964 |
| L35 | 29.943 | 73.153 | 7670.735 | 10.227 | 15.042 | 509.969 | 15351.564 | 36.583 | 3.803 | 4.754 |
|  | 30.068 | 73.466 | 7769.593 | 10.271 | 15.104 | 514.400 | 15549.410 | 36.740 | 3.825 | 4.781 |
| L36 | 30.068 | 73.466 | 7769.593 | 10.271 | 15.104 | 514.400 | 15549.410 | 36.740 | 3.825 | 4.781 |
|  | 30.109 | 73.567 | 7801.872 | 10.285 | 15.125 | 515.843 | 15614.009 | 36.791 | 3.832 | 4.79 |
| L37 | 30.110 | 72.449 | 7689.912 | 10.290 | 15.125 | 508.441 | 15389.942 | 36.231 | 3.854 | 4.894 |
|  | 30.923 | 74.449 | 8344.564 | 10.574 | 15.531 | 537.284 | 16700.107 | 37.232 | 3.995 | 5.073 |
| L38 | 30.925 | 73.298 | 8222.454 | 10.578 | 15.531 | 529.422 | 16455.727 | 36.656 | 4.017 | 5.183 |
|  | 31.738 | 75.267 | 8902.842 | 10.862 | 15.938 | 558.609 | 17817.398 | 37.640 | 4.158 | 5.365 |
| L39 | 31.739 | 74.083 | 8769.987 | 10.867 | 15.938 | 550.273 | 17551.513 | 37.049 | 4.180 | 5.482 |
|  | 32.183 | 75.140 | 9150.907 | 11.022 | 16.159 | 566.287 | 18313.854 | 37.577 | 4.257 | 5.582 |


| Tower <br> Elevation <br> ft | Gusset Area (perface) | Gusset Thickness <br> in | Gusset Grade | $\begin{gathered} \text { Adjust. Factor } \\ A_{f} \end{gathered}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle <br> Stitch Bolt <br> Spacing <br> Horizontals <br> in | Double Angle <br> Stitch Bolt <br> Spacing <br> Redundants <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 |  |  |  | 1 | 1 | 1 |  |  |  |
| 108.000-103.0 |  |  |  |  |  |  |  |  |  |
| L2 |  |  |  | 1 | 1 | 1 |  |  |  |
| 103.000-98.50 |  |  |  |  |  |  |  |  |  |
| 0 |  |  |  |  |  |  |  |  |  |
| L3$98.500-98.000$ |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| L4 |  |  |  | 1 | 1 | 1 |  |  |  |
| 98.000-93.000 |  |  |  |  |  |  |  |  |  |



| Tower Elevation <br> $f t$ | $\begin{gathered} \text { Gusset } \\ \text { Area } \\ \text { (per face) } \\ f^{2} \end{gathered}$ | Gusset Thickness <br> in | Gusset Grade Adjust. Factor | $\begin{gathered} \text { Adjust. } \\ \text { Factor } \\ A_{r} \end{gathered}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle <br> Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L5 |  |  | I | 1 | 1 |  |  |  |
| 93.000-88.000 |  |  |  |  |  |  |  |  |
| L6 |  |  | 1 | 1 | 1 |  |  |  |
| 88.000-83.000 |  |  |  |  |  |  |  |  |
| L7 |  |  | 1 | 1 | 1 |  |  |  |
| 83.000-82.330 |  |  |  |  |  |  |  |  |
| L8 |  |  | 1 | 1 | 1.03474 |  |  |  |
| 82.330-82.080 |  |  |  |  |  |  |  |  |
| L9 |  |  | 1 | 1 | 1.03556 |  |  |  |
| 82.080-77.080 |  |  |  |  |  |  |  |  |
| L10 |  |  | 1 | 1 | 1.03254 |  |  |  |
| 77.080-76.250 |  |  |  |  |  |  |  |  |
| Ll1 |  |  | 1 | 1 | 1.15217 |  |  |  |
| 76.250-76.000 |  |  |  |  |  |  |  |  |
| L12 |  |  | 1 | 1 | 1.1587 |  |  |  |
| 76.000-74.500 |  |  |  |  |  |  |  |  |
| L13 |  |  | 1 | 1 | 0.971985 |  |  |  |
| 74.500-74.250 |  |  |  |  |  |  |  |  |
| L14 |  |  | 1 | 1 | 0.966504 |  |  |  |
| 74.250-69.250 |  |  |  |  |  |  |  |  |
| L15 |  |  | 1 | 1 | 0.984159 |  |  |  |
| 69.250-64.250 |  |  |  |  |  |  |  |  |
| L16 |  |  | 1 | 1 | 0.971691 |  |  |  |
| 64.250-59.250 |  |  |  |  |  |  |  |  |
| L17 |  |  | 1 | 1 | 0.977402 |  |  |  |
| 59.250-58.080 |  |  |  |  |  |  |  |  |
| L18 |  |  | 1 | 1 | 0.932812 |  |  |  |
| 58.080-57.730 |  |  |  |  |  |  |  |  |
| L19 |  |  | 1 | 1 | 0.931705 |  |  |  |
| 57.730-57.500 |  |  |  |  |  |  |  |  |
| L20 |  |  | 1 | 1 | 0.940531 |  |  |  |
| 57.500-52.500 |  |  |  |  |  |  |  |  |
| L21 |  |  | 1 | 1 | 0.930278 |  |  |  |
| 52.500-47.000 |  |  |  |  |  |  |  |  |
| L22 |  |  | 1 | 1 | 0.928658 |  |  |  |
| 47.000-45.250 |  |  |  |  |  |  |  |  |
| L23 |  |  | 1 | 1 | 0.940675 |  |  |  |
| 45.250-40.500 |  |  |  |  |  |  |  |  |
| L24 |  |  | 1 | 1 | 0.939708 |  |  |  |
| 40.500-40.250 |  |  |  |  |  |  |  |  |
| L25 |  |  | 1 | 1 | 0.952955 |  |  |  |
| 40.250-35.250 |  |  |  |  |  |  |  |  |
| L26 |  |  | 1 | 1 | 0.951349 |  |  |  |
| 35.250-30.250 |  |  |  |  |  |  |  |  |
| L27 |  |  | 1 | 1 | 0.95954 |  |  |  |
| 30.250-27.750 |  |  |  |  |  |  |  |  |
| L28 |  |  | 1 | 1 | 0.947656 |  |  |  |
| 27.750-27.500 |  |  |  |  |  |  |  |  |
| L29 |  |  | 1 | 1 | 0.962447 |  |  |  |
| 27.500-22.500 |  |  |  |  |  |  |  |  |
| L30 |  |  | 1 | 1 | 0.968941 |  |  |  |
| 22.500-19.500 |  |  |  |  |  |  |  |  |
| L31 |  |  | 1 | 1 | 0.898748 |  |  |  |
| 19.500-19.250 |  |  |  |  |  |  |  |  |
| L32 |  |  | 1 | 1 | 0.910092 |  |  |  |
| 19.250-14.250 |  |  |  |  |  |  |  |  |
| L33 |  |  | 1 | 1 | 0.909276 |  |  |  |
| $\underset{\text { 14.250-14.000 }}{ }$ |  |  |  |  |  |  |  |  |
| L34 |  |  |  |  | 0.971909 |  |  |  |



| Tower Elevation <br> ft | Gusset Area (per face) $f t^{2}$ | Gusset Thickness <br> in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle <br> Stitch Bolt <br> Spacing <br> Horizontals <br> in | Double Angle <br> Stitch Bolt <br> Spacing <br> Redundants <br> in <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14.000-13.750 |  |  |  |  |  |  |  |  |  |
| L35 |  |  |  | 1 | 1 | 0.967746 |  |  |  |
| 13.750-12.980 |  |  |  |  |  |  |  |  |  |
| L36 |  |  |  | 1 | 1 | 0.966841 |  |  |  |
| 12.980-12.730 |  |  |  |  |  |  |  |  |  |
| L37 |  |  |  | 1 | 1 | 0.963917 |  |  |  |
| 12.730-7.730 |  |  |  |  |  |  |  |  |  |
| L38 |  |  |  | 1 | 1 | 0.961885 |  |  |  |
| 7.730-2.730 |  |  |  |  |  |  |  |  |  |
| L39 |  |  |  | 1 | 1 | 0.968116 |  |  |  |
| 2.730-0.000 |  |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> $f t$ | Total Number | Number Per Row | Start/End Position | Width or Diameter in | Perimeter <br> in | Weight $k l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { LDF6-50A(1-1/4) } \\ (6 \mathrm{E}+1 \mathrm{P}) \end{gathered}$ | A | No | $\begin{aligned} & \text { Surface } \mathrm{Ar} \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 105.000- \\ 0.000 \end{gathered}$ | 7 | 6 | $\begin{aligned} & -0.500 \\ & -0.200 \end{aligned}$ | 1.550 |  | 0.001 |
| HB158-1-08U8-\$8J18(1- $5 / 8)$ $(\mathrm{E})$ $* \$ \$^{*}$ $* \$ \$^{*}$ | A | No | $\begin{aligned} & \text { Surface Ar } \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 105.000- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{gathered} -0.300 \\ -0.200 \end{gathered}$ | 1.980 |  | 0.001 |
| ATCB-B01(5/16) <br> (E) | C | No | $\begin{aligned} & \text { Surface Ar } \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 81.000- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{gathered} -0.360 \\ -0.350 \end{gathered}$ | 0.315 |  | 0.000 |
| FXL $780 \mathrm{PE}(7 / 8)$ <br> (E) | C | No | $\begin{gathered} \text { Surface Ar } \\ \text { (CaAa) } \end{gathered}$ | $\begin{gathered} 81.000- \\ 0.000 \end{gathered}$ | 6 | 3 | $\begin{aligned} & -0.500 \\ & -0.350 \end{aligned}$ | 1.090 |  | 0.000 |
| *\$* <br> Safety Line 3/8 <br> (E) | B | No | $\begin{aligned} & \text { Surface Ar } \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 108.000- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 0.375 |  | 0.000 |
| $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate (E-VSI Mod) | A | No | Surface Af <br> (CaAa) | $\begin{gathered} 29.750- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 5.250 | 13.000 | 0.000 |
| $5.25^{\prime \prime} \times 1.25^{\prime \prime} \text { Plate }$ <br> (E-VSI Mod) | B | No | $\begin{gathered} \text { Surface Af } \\ \text { (CaAa) } \end{gathered}$ | $\begin{gathered} 15.500- \\ 0.000 \end{gathered}$ | 2 | 2 | $\begin{aligned} & 0.200 \\ & 0.300 \end{aligned}$ | 5.250 | 13.000 | 0.000 |
| $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate (E-VSI Mod) | B | No | $\begin{gathered} \text { Surface Af } \\ \text { (CaAa) } \end{gathered}$ | $\begin{gathered} 29.750- \\ 10.250 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 5.250 | 13.000 | 0.000 |
| $5.25^{\prime \prime}$ x $1.25^{\prime \prime}$ Plate <br> (E-VSI Mod) *\$* | C | No | $\begin{gathered} \text { Surface Af } \\ \text { (CaAa) } \end{gathered}$ | $\begin{gathered} 29.750- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 5.250 | 13.000 | 0.000 |
| $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate (E-VSI Mod) | A | No | $\begin{gathered} \text { Surface Af } \\ (\mathrm{CaAa}) \end{gathered}$ | $\begin{gathered} 59.500- \\ 29.750 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.375 | 11.250 | 0.000 |
| $\begin{aligned} & 4.375^{\circ 1} \times 1.25^{\prime \prime} \text { Plate } \\ & \text { (E-VSI Mod) } \end{aligned}$ | B | No | $\begin{gathered} \text { Surface Af } \\ (\mathrm{CaAa}) \end{gathered}$ | $\begin{gathered} 59.500- \\ 29.750 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.375 | 11.250 | 0.000 |
| $\begin{aligned} & 4.375^{\prime \prime} \times 1.25^{\prime \prime} \text { Plate } \\ & \text { (E-VSI Mod) } \\ & * \$ \$^{*} \end{aligned}$ | C | No | $\begin{gathered} \text { Surface Af } \\ \text { (CaAa) } \end{gathered}$ | $\begin{gathered} 59.500- \\ 29.750 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.375 | 11.250 | 0.000 |
| $4.0^{\prime \prime} \times 1.25^{\prime \prime} \text { Plate }$ <br> (E-VSI Mod) | A | No | $\begin{aligned} & \text { Surface Af } \\ & (\mathrm{CaAa}) \end{aligned}$ | $\begin{gathered} 78.000- \\ 59.500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.000 | 10.500 | 0.000 |
| $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate <br> (E-VSI Mod) | B | No | Surface Af (CaAa) | $\begin{gathered} 78.000- \\ 59.500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.000 | 10.500 | 0.000 |
| $4.0^{\prime \prime}$ x I. $25^{\prime \prime}$ Plate <br> (E-VSI Mod) | C | No | Surface Af (CaAa) | $\begin{gathered} 78.000- \\ 59.500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.000 | 10.500 | 0.000 |


| thxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 | $\begin{array}{\|l} \text { Job } \\ 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{array}$ |  | $\begin{gathered} \text { Page } \\ 7 \text { of } 42 \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Description | Sector | Exclude From Torque Calculation | Component Type | Placement <br> ft | $\begin{gathered} \text { Total } \\ \text { Number } \end{gathered}$ | Number Per Row | Start/End Position | Width or Diameter in | Perimeter in | Weight klf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *\$ ${ }^{*}$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { MP3-05 } \\ \text { (E-B+T Mod) } \end{gathered}$ | A | No | Surface Af (CaAa) | $\begin{gathered} 40.500- \\ 0.000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.400 \\ & 0.400 \end{aligned}$ | 5.330 | 14.840 | 0.000 |
| MP3-05 | B | No | Surface Af | $15.500-$ | 1 | 1 | 0.200 | 5.330 | 14.840 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 0.000 |  |  | 0.200 |  |  |  |
| MP3-05 | B | No | Surface Af | $40.500-$ | 1 | 1 | 0.400 | 5.330 | 14.840 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 10.500 |  |  | 0.400 |  |  |  |
| MP3-05 | C | No | Surface Af | $40.500-$ | 1 | 1 | 0.400 | 5.330 | 14.840 | 0.000 |
| *\$* |  |  |  |  |  |  |  |  |  |  |
| MP3-05 | A | No | Surface Af | $60.500-$ | 1 | 1 | 0.400 | 5.330 | 14.840 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 40.500 |  |  | 0.400 |  |  |  |
| MP3-05 | B | No | Surface Af | $60.500-$ | 1 | 1 | 0.400 | 5.330 | 14.840 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 40.500 |  |  | 0.400 |  |  |  |
| MP3-05 | C | No | Surface Af | $60.500-$ | 1 | 1 | 0.400 | 5.330 | 14.840 | 0.000 |
| (E-B+T Mod) |  |  | (СаАа) | 40.500 |  |  | 0.400 |  |  |  |
| *\$8* |  |  |  |  |  |  |  |  |  |  |
| MP3-03 | A | No | Sufface Af | $84.050-$ | 1 | 1 | 0.400 | 4.060 | 11.260 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 60.500 |  |  | 0.400 |  |  |  |
| MP3-03 | B | No | Surface Af | $84.050-$ | 1 | 1 | 0.400 | 4.060 | 11.260 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 60.500 |  |  | 0.400 |  |  |  |
| MP3-03 | C | No | Surface Af | $84.050-$ | 1 | 1 | 0.400 | 4.060 | 11.260 | 0.000 |
| (E-B+T Mod) |  |  | (CaAa) | 60.500 |  |  | 0.400 |  |  |  |
| *\$\$* |  |  |  |  |  |  |  |  |  |  |
| CCI 4.5"x $1^{\prime \prime}$ Plate | A | No | Surface Af | 15.500- | 1 | 1 | 0.000 | 4.500 | 11.000 | 0.000 |
| ( $\mathrm{E}-\mathrm{B}+\mathrm{TMod}$ ) |  |  | (CaAa) | 0.000 |  |  | 0.020 |  |  |  |
| CCI 4.5"x 1" Plate | B | No | Surface Af | 21.000- | 1 | 1 | 0.300 | 4.500 | 11.000 | 0.000 |
| $(\mathrm{E}-\mathrm{B}+\mathrm{TMOM} \mathrm{Mod})$ |  |  | (CaAa) | 11.000 |  |  | 0.320 |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> $f t$ | Total <br> Number |  | $C_{A} A_{A}$ <br> $f t^{2} / f t$ | Weight <br> $k l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *\$8* Calculation |  |  |  |  |  |  |  |  |  |
| HB114-1-08U4-M5J | B | No | No | Inside Pole | 98.000-0.000 | 3 | No Ice | 0.000 | 0.001 |
| (1-1/4) |  |  |  |  |  |  | $1 / 2^{\prime \prime}$ Ice | 0.000 | 0.001 |
| (E-Sprint) |  |  |  |  |  |  | 1" Ice | 0.000 | 0.001 |
|  |  |  |  |  |  |  | 2 Ice | 0.000 | 0.001 |
| 3X4AWG(1-1/4) | B | No | No | Inside Pole | 98.000-0.000 | 1 | No Ice | 0.000 | 0.001 |
| (R) |  |  |  |  |  |  | $1 / 2^{1 /}$ Ice | 0.000 | 0.001 |
|  |  |  |  |  |  |  | 1" Ice | 0.000 | 0.001 |
|  |  |  |  |  |  |  | 2" Ice | 0.000 | 0.001 |
| *\$* |  |  |  |  |  |  |  |  |  |
| LDF4-50A(1/2) | B | No | No | Inside Pole | 74.000-0.000 | 1 | No Ice | 0.000 | 0.000 |
| (E) |  |  |  |  |  |  | 1/2" Ice | 0.000 | 0.000 |
|  |  |  |  |  |  |  | 1" Ice | 0.000 | 0.000 |
|  |  |  |  |  |  |  | 2 " Ice | 0.000 | 0.000 |
| *\$8* |  |  |  |  |  |  |  |  |  |



Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower \\
Section
\end{tabular} \& Tower Elevation \(f t\) \& Face \& \(A_{R}\)

$f l^{2}$ \& $A_{F}$

$f^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
f^{2} \\
\hline
\end{gathered}
$$

\] \& | Weight |
| :---: |
| $K$ | <br>

\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{108.000-103.000} \& A \& 0.000 \& 0.000 \& 2.256 \& 0.000 \& 0.011 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{103.000-98.500} \& A \& 0.000 \& 0.000 \& 5.076 \& 0.000 \& 0.025 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.169 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{98.500-98.000} \& A \& 0.000 \& 0.000 \& 0.564 \& 0.000 \& 0.003 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.019 \& 0.000 \& 0.000 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{98.000-93.000} \& A \& 0.000 \& 0.000 \& 5.640 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{93.000-88.000} \& A \& 0.000 \& 0.000 \& 5.640 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L6} \& \multirow[t]{3}{*}{88.000-83.000} \& A \& 0.000 \& 0.000 \& 6.351 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.898 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.711 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L7} \& \multirow[t]{3}{*}{83.000-82.330} \& A \& 0.000 \& 0.000 \& 1.209 \& 0.000 \& 0.004 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.478 \& 0.000 \& 0.003 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.453 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L8} \& \multirow[t]{3}{*}{82.330-82.080} \& A \& 0.000 \& 0.000 \& 0.451 \& 0.000 \& 0.001 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.179 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.169 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L9} \& \multirow[t]{3}{*}{82.080-77.080} \& A \& 0.000 \& 0.000 \& 9.637 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.184 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.402 \& 0.000 \& 0.006 <br>
\hline \multirow[t]{3}{*}{L10} \& \multirow[t]{3}{*}{77.080-76.250} \& A \& 0.000 \& 0.000 \& 2.051 \& 0.000 \& 0.005 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.146 \& 0.000 \& 0.004 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.413 \& 0.000 \& 0.001 <br>
\hline \multirow[t]{3}{*}{L11} \& \multirow[t]{3}{*}{76.250-76.000} \& A \& 0.000 \& 0.000 \& 0.618 \& 0.000 \& 0.001 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.345 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.425 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L12} \& \multirow[t]{3}{*}{$76.000-74.500$} \& A \& 0.000 \& 0.000 \& 3.707 \& 0.000 \& 0.008 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.071 \& 0.000 \& 0.007 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.553 \& 0.000 \& 0.002 <br>
\hline \multirow[t]{3}{*}{L13} \& \multirow[t]{3}{*}{$74.500-74.250$} \& A \& 0.000 \& 0.000 \& 0.618 \& 0.000 \& 0.001 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.345 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.425 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L14} \& \multirow[t]{3}{*}{$74.250-69.250$} \& A \& 0.000 \& 0.000 \& 12.357 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 6.904 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.509 \& 0.000 \& 0.008 <br>
\hline \multirow[t]{3}{*}{L15} \& \multirow[t]{3}{*}{69.250-64.250} \& A \& 0.000 \& 0.000 \& 12.357 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 6.904 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.509 \& 0.000 \& 0.008 <br>
\hline \multirow[t]{3}{*}{L16} \& \multirow[t]{3}{*}{$64.250-59.250$} \& A \& 0.000 \& 0.000 \& 12.637 \& 0.000 \& 0.028 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 7.184 \& 0.000 \& 0.022 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.789 \& 0.000 \& 0.008 <br>
\hline \multirow[t]{3}{*}{L17} \& \multirow[t]{3}{*}{59.250-58.080} \& A \& 0.000 \& 0.000 \& 3.212 \& 0.000 \& 0.006 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.936 \& 0.000 \& 0.005 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.312 \& 0.000 \& 0.002 <br>
\hline \multirow[t]{3}{*}{Li 8} \& \multirow[t]{3}{*}{58.080-57.730} \& A \& 0.000 \& 0.000 \& 0.961 \& 0.000 \& 0.002 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.579 \& 0.000 \& 0.002 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.692 \& 0.000 \& 0.001 <br>
\hline \multirow[t]{3}{*}{L19} \& \multirow[t]{3}{*}{$57.730-57.500$} \& A \& 0.000 \& 0.000 \& 0.631 \& 0.000 \& 0.001 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.381 \& 0.000 \& 0.001 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.454 \& 0.000 \& 0.000 <br>
\hline L20 \& 57.500-52.500 \& A \& 0.000 \& 0.000 \& 13.728 \& 0.000 \& 0.028 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 | Job <br> 85565.009.01 - HARTFORD - NU (SSUSA), CT (BU\# 876363) <br> Prict |  | $\text { Page } 9 \text { of } 42$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |  |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 FAX: (918) 295-0265 | Client | Crown Castle | Design | ned by xjones |


| Tower Section | Tower Elevation $f t$ | Face | $\overline{A_{R}}$ $f t^{2}$ | $\begin{gathered} A_{F} \\ {f t^{2}}^{2} \end{gathered}$ | $\begin{gathered} C_{A A} A_{A} \\ \text { In Face } \\ {f t^{2}}^{2} \\ \hline \end{gathered}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ f_{1}^{2} \end{gathered}$ | Weight . $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L21 | 52.500-47.000 | B | 0.000 | 0.000 | 8.275 | 0.000 | 0.022 |
|  |  | C | 0.000 | 0.000 | 9.880 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 15.100 | 0.000 | 0.030 |
|  |  | B | 0.000 | 0.000 | 9.102 | 0.000 | 0.025 |
| L22 | 47.000-45.250 | C | 0.000 | 0.000 | 10.868 | 0.000 | 0.009 |
|  |  | A | 0.000 | 0.000 | 4.805 | 0.000 | 0.010 |
|  |  | B | 0.000 | 0.000 | 2.896 | 0.000 | 0.008 |
| L23 | 45.250-40.500 | C | 0.000 | 0.000 | 3.458 | 0.000 | 0.003 |
|  |  | A | 0.000 | 0.000 | 13.041 | 0.000 | 0.026 |
|  |  | B | 0.000 | 0.000 | 7.861 | 0.000 | 0.021 |
| L24 | 40.500-40.250 | C | 0.000 | 0.000 | 9.386 | 0.000 | 0.007 |
|  |  | A | 0.000 | 0.000 | 0.686 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 0.414 | 0.000 | 0.001 |
| L25 | 40.250-35.250 | C | 0.000 | 0.000 | 0.494 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 13.728 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 8.275 | 0.000 | 0.022 |
| L26 | 35.250-30.250 | C | 0.000 | 0.000 | 9.880 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 13.728 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 8.275 | 0.000 | 0.022 |
| L27 | 30.250-27.750 | C | 0.000 | 0.000 | 9.880 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 7.155 | 0.000 | 0.014 |
|  |  | B | 0.000 | 0.000 | 4.429 | 0.000 | 0.011 |
| L28 | 27.750-27.500 | C | 0.000 | 0.000 | 5.232 | 0.000 | 0.004 |
|  |  | A | 0.000 | 0.000 | 0.723 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 0.450 | 0.000 | 0.001 |
| L29 | 27.500-22.500 | C | 0.000 | 0.000 | 0.530 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 14.457 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 9.004 | 0.000 | 0.022 |
| L30 | 22.500-19.500 | C | 0.000 | 0.000 | 10.609 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 8.674 | 0.000 | 0.017 |
|  |  | B | 0.000 | 0.000 | 6.527 | 0.000 | 0.013 |
| L31 | 19.500-19.250 | C | 0.000 | 0.000 | 6.365 | 0.000 | 0.005 |
|  |  | A | 0.000 | 0.000 | 0.723 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 0.638 | 0.000 | 0.001 |
| L32 | 19.250-14.250 | C | 0.000 | 0.000 | 0.530 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 15.394 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 16.052 | 0.000 | 0.022 |
| L33 | 14.250-14.000 | C | 0.000 | 0.000 | 10.609 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 0.910 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 1.297 | 0.000 | 0.001 |
| L34 | 14.000-13.750 | C | 0.000 | 0.000 | 0.530 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 0.910 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 1.297 | 0.000 | 0.001 |
| L35 | 13.750-12.980 | C | 0.000 | 0.000 | 0.530 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 2.804 | 0.000 | 0.004 |
|  |  | B | 0.000 | 0.000 | 3.996 | 0.000 | 0.003 |
| L36 | 12.980-12.730 | C | 0.000 | 0.000 | 1.634 | 0.000 | 0.001 |
|  |  | A | 0.000 | 0.000 | 0.910 | 0.000 | 0.001 |
|  |  | B | 0.000 | 0.000 | 1.297 | 0.000 | 0.001 |
| L37 | 12.730-7.730 | C | 0.000 | 0.000 | 0.530 | 0.000 | 0.000 |
|  |  | A | 0.000 | 0.000 | 18.207 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 18.828 | 0.000 | 0.022 |
| L38 | 7.730-2.730 | C | 0.000 | 0.000 | 10.609 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 18.207 | 0.000 | 0.028 |
|  |  | B | 0.000 | 0.000 | 13.379 | 0.000 | 0.022 |
| L39 | 2.730-0.000 | C | 0.000 | 0.000 | 10.609 | 0.000 | 0.008 |
|  |  | A | 0.000 | 0.000 | 9.941 | 0.000 | 0.015 |
|  |  | B | 0.000 | 0.000 | 7.305 | 0.000 | 0.012 |
|  |  | C | 0.000 | 0.000 | 5.793 | 0.000 | 0.004 |



Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation ft \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Ice
Thickness
in \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
\text { ft }^{2}
\end{gathered}
$$
\] \& Weight

$K$ <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{108.000-103.000} \& A \& \multirow[t]{3}{*}{1.910} \& 0.000 \& 0.000 \& 4.440 \& 0.000 \& 0.077 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.097 \& 0.000 \& 0.028 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{103.000-98.500} \& A \& \multirow[t]{3}{*}{1.901} \& 0.000 \& 0.000 \& 9.971 \& 0.000 \& 0.173 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.879 \& 0.000 \& 0.025 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{98.500-98.000} \& A \& \multirow[t]{3}{*}{1.896} \& 0.000 \& 0.000 \& 1.107 \& 0.000 \& 0.019 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.208 \& 0.000 \& 0.003 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{98.000-93.000} \& A \& \multirow[t]{3}{*}{1.891} \& 0.000 \& 0.000 \& 11.056 \& 0.000 \& 0.191 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.078 \& 0.000 \& 0.048 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{93.000-88.000} \& A \& \multirow[t]{3}{*}{1.880} \& 0.000 \& 0.000 \& 11.033 \& 0.000 \& 0.190 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.068 \& 0.000 \& 0.048 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow[t]{3}{*}{L6} \& \multirow[t]{3}{*}{88.000-83.000} \& A \& \multirow[t]{3}{*}{1.870} \& 0.000 \& 0.000 \& 12.113 \& 0.000 \& 0.203 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 3.160 \& 0.000 \& 0.061 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.103 \& 0.000 \& 0.014 <br>
\hline \multirow[t]{3}{*}{L7} \& \multirow[t]{3}{*}{83.000-82.330} \& A \& \multirow[t]{3}{*}{1.864} \& 0.000 \& 0.000 \& 2.176 \& 0.000 \& 0.034 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.978 \& 0.000 \& 0.015 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.703 \& 0.000 \& 0.009 <br>
\hline \multirow[t]{3}{*}{L.8} \& \multirow[t]{3}{*}{82.330-82.080} \& A \& \multirow[t]{3}{*}{1.862} \& 0.000 \& 0.000 \& 0.812 \& 0.000 \& 0.013 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.365 \& 0.000 \& 0.006 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.262 \& 0.000 \& 0.003 <br>
\hline \multirow[t]{3}{*}{L9} \& \multirow[t]{3}{*}{82.080-77.080} \& A \& \multirow[t]{3}{*}{1.856} \& 0.000 \& 0.000 \& 17.174 \& 0.000 \& 0.265 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 8.239 \& 0.000 \& 0.125 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 11.195 \& 0.000 \& 0.158 <br>
\hline \multirow[t]{3}{*}{L10} \& \multirow[t]{3}{*}{77.080-76.250} \& A \& \multirow[t]{3}{*}{1.850} \& 0.000 \& 0.000 \& 3.549 \& 0.000 \& 0.052 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.067 \& 0.000 \& 0.029 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 2.785 \& 0.000 \& 0.038 <br>
\hline \multirow[t]{3}{*}{L11} \& \multirow[t]{3}{*}{76.250-76.000} \& A \& \multirow[t]{3}{*}{1.848} \& 0.000 \& 0.000 \& 1.069 \& 0.000 \& 0.016 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.622 \& 0.000 \& 0.009 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.839 \& 0.000 \& 0.012 <br>
\hline \multirow[t]{3}{*}{L12} \& \multirow[t]{3}{*}{76.000-74.500} \& A \& \multirow[t]{3}{*}{1.846} \& 0.000 \& 0.000 \& 6.409 \& 0.000 \& 0.094 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 3.733 \& 0.000 \& 0.053 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 5.029 \& 0.000 \& 0.069 <br>
\hline \multirow[t]{3}{*}{L13} \& \multirow[t]{3}{*}{$74.500-74.250$} \& A \& \multirow[t]{3}{*}{1.844} \& 0.000 \& 0.000 \& 1.068 \& 0.000 \& 0.016 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.622 \& 0.000 \& 0.009 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.838 \& 0.000 \& 0.011 <br>
\hline \multirow[t]{3}{*}{L14} \& \multirow[t]{3}{*}{74.250-69.250} \& A \& \multirow[t]{3}{*}{1.837} \& 0.000 \& 0.000 \& 21.328 \& 0.000 \& 0.313 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 12.416 \& 0.000 \& 0.175 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 16.726 \& 0.000 \& 0.228 <br>
\hline \multirow[t]{3}{*}{L15} \& \multirow[t]{3}{*}{69.250-64.250} \& A \& \multirow[t]{3}{*}{1.824} \& 0.000 \& 0.000 \& 21.271 \& 0.000 \& 0.310 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 12.376 \& 0.000 \& 0.173 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 16.670 \& 0.000 \& 0.226 <br>
\hline \multirow[t]{3}{*}{L16} \& \multirow[t]{3}{*}{64.250-59.250} \& A \& \multirow[t]{3}{*}{1.810} \& 0.000 \& 0.000 \& 21.491 \& 0.000 \& 0.311 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 12.614 \& 0.000 \& 0.175 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 16.890 \& 0.000 \& 0.227 <br>
\hline \multirow[t]{3}{*}{L17} \& \multirow[t]{3}{*}{59.250-58.080} \& A \& 1.801 \& 0.000 \& 0.000 \& 5.275 \& 0.000 \& 0.075 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 3.200 \& 0.000 \& 0.043 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 4.198 \& 0.000 \& 0.056 <br>
\hline \multirow[t]{3}{*}{L18} \& \multirow[t]{3}{*}{58.080-57.730} \& A \& 1.798 \& 0.000 \& 0.000 \& 1.577 \& 0.000 \& 0.022 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.957 \& 0.000 \& 0.013 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.255 \& 0.000 \& 0.017 <br>
\hline \multirow[t]{2}{*}{L19} \& \multirow[t]{2}{*}{57.730-57.500} \& A \& 1.797 \& 0.000 \& 0.000 \& 1.036 \& 0.000 \& 0.015 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.629 \& 0.000 \& 0.009 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\left\lvert\, \begin{array}{l\|l} \text { Job } \\ 85565 \end{array}\right.$ | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 11 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Tower | Tower | Face | Ice | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ | $C_{A} A_{A}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | or | Thickness |  | fl $^{2}$ | $f l^{2}$ | InFace | Out Face |


| tnxTower <br> B+TGroup <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 | $\begin{array}{\|l} \text { Job } \\ 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# } 876363 \text { ) } \end{array}$ |  | $\text { Page } 12 \text { of } 42$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

Feed Line Center of Pressure

| Section | Elevation $f t$ | $C P_{X}$ in | $C P_{2}$ <br> in | $\begin{gathered} C P_{X} \\ \text { Ice } \\ \text { in } \\ \hline \end{gathered}$ | $\begin{gathered} C P_{Z} \\ \text { Ice } \\ \text { in } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 108.000-103.000 | -2.765 | 0.433 | -1.276 | -0.033 |
| L2 | 103.000-98.500 | -4.120 | 0.702 | -2.515 | 0.261 |
| L3 | 98.500-98.000 | -5.432 | 0.909 | -3.487 | 0.320 |
| L4 | 98.000-93.000 | -4.995 | 0.835 | -3.514 | 0.322 |
| L5 | 93.000-88.000 | -5.076 | 0.848 | -3.597 | 0.328 |
| L6 | 88.000-83.000 | -4.350 | 0.726 | -3.283 | 0.298 |
| L7 | 83.000-82.330 | -2.310 | 0.385 | -2.376 | 0.216 |
| L8 | 82.330-82.080 | -2.316 | 0.386 | -2.383 | 0.216 |
| L9 | 82.080-77.080 | -1.674 | 0.680 | -1.207 | 0.839 |
| L10 | 77.080-76.250 | -1.218 | 0.600 | -0.802 | 0.814 |
| L11 | 76.250-76.000 | -1.221 | 0.602 | -0.805 | 0.816 |
| L12 | 76.000-74.500 | -1.226 | 0.604 | -0.809 | 0.820 |
| L13 | 74.500-74.250 | -1.232 | 0.607 | -0.813 | 0.824 |
| L14 | 74.250-69.250 | -1.247 | 0.614 | -0.825 | 0.836 |
| L15 | 69.250-64.250 | -1.275 | 0.629 | -0.847 | 0.859 |
| L16 | 64.250-59.250 | -1.273 | 0.628 | -0.859 | 0.871 |
| L17 | 59.250-58.080 | -1.186 | 0.585 | -0.834 | 0.845 |
| L18 | 58.080-57.730 | -1.190 | 0.588 | -0.838 | 0.848 |
| L19 | 57.730-57.500 | -1.191 | 0.588 | -0.839 | 0.850 |
| L20 | 57.500-52.500 | -1.204 | 0.595 | -0.851 | 0.860 |
| L21 | 52.500-47.000 | -1.231 | 0.608 | -0.874 | 0.882 |
| L22 | 47.000-45.250 | -1.237 | 0.612 | -0.878 | 0.887 |
| L23 | 45.250-40.500 | -1.253 | 0.620 | -0.896 | 0.899 |
| L24 | 40.500-40.250 | -1.265 | 0.626 | -0.907 | 0.909 |
| L25 | 40.250-35.250 | -1.278 | 0.632 | -0.919 | 0.919 |
| L26 | 35.250-30.250 | -1.302 | 0.644 | -0.943 | 0.938 |
| L27 | 30.250-27.750 | -1.269 | 0.629 | -0.939 | 0.930 |
| L28 | 27.750-27.500 | -1.263 | 0.626 | -0.940 | 0.929 |
| L29 | 27.500-22.500 | -1.275 | 0.632 | -0.953 | 0.938 |
| L30 | 22.500-19.500 | -0.752 | 0.995 | -0.542 | 1.240 |
| L31 | 19.500-19.250 | -0.259 | 1.326 | -0.140 | 1.519 |
| L32 | 19.250-14.250 | 0.427 | 1.461 | -0.056 | 1.392 |
| L33 | 14.250-14.000 | 1.986 | 1.748 | 0.152 | 1.060 |
| L34 | 14.000-13.750 | 1.988 | 1.750 | 0.152 | 1.061 |
| L35 | 13.750-12.980 | 1.993 | 1.754 | 0.152 | 1.063 |
| L36 | 12.980-12.730 | 1.997 | 1.758 | 0.152 | 1.065 |
| L37 | 12.730-7.730 | 0.822 | 1.213 | -1.189 | 0.464 |
| L38 | 7.730-2.730 | -0.294 | 0.846 | -2.470 | 0.034 |
| L39 | $2.730-0.000$ | -0.296 | 0.858 | -2.539 | 0.018 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Shielding Factor Ka

| Tower <br> Section | Feed Line <br> Record No. | Description | Feed Line <br> Segment Elev. | $K_{a}$ <br> No Ice | $K_{a}$ <br> Ice |
| ---: | ---: | ---: | ---: | :---: | :---: |
| L1 | 2 | LDF6-50A(1-1/4) | $103.00-1.000$ | 1.0000 |  |


| thxTower | 85565.009.01-HARTFORD - NU (SSUSA), CT (BU\# 876363) |  | $\begin{aligned} & \text { Page } \\ & 13 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| B + T Group <br> 1717 S. Boulder, Suite 300 | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265 |  |  | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | $\begin{gathered} \text { Feed Line } \\ \text { Segment Elev. } \end{gathered}$ | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & \hline K_{a} \\ & \text { Ice } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 105.00 |  |  |
| L1 | 3 | HB158-1-08U8-S8J18(1-5/8) | $\begin{array}{r}103.00 \\ 105.00 \\ \hline\end{array}$ | 1.0000 | 1.0000 |
| LI | 18 | Safety Line 3/8 | 103.00- | 1.0000 | 1.0000 |
| L2 | 2 | LDF6-50A(1-1/4) | 98.50-103.00 | 1.0000 | 1.0000 |
| L2 | 3 | HB158-1-08U8-S8J18(1-5/8) | 98.50-103.00 | 1.0000 | 1.0000 |
| L2 | 18 | Safety Line 3/8 | 98.50-103.00 | 1.0000 | 1.0000 |
| L3 | 2 | LDF6-50A(1-1/4) | 98.00-98.50 | 1.0000 | 1.0000 |
| L3 | 3 | HB158-1-08U8-S8J18(1-5/8) | 98.00-98.50 | 1.0000 | 1.0000 |
| L3 | 18 | Safety Line 3/8 | 98.00-98.50 | 1.0000 | 1.0000 |
| L4 | 2 | LDF6-50A(1-1/4) | 93.00-98.00 | 1.0000 | 1.0000 |
| L4 | 3 | HB158-1-08U8-S8J18(1-5/8) | 93.00-98.00 | 1.0000 | 1.0000 |
| L4 | 18 | Safety Line 3/8 | 93.00-98.00 | 1.0000 | 1.0000 |
| L5 | 2 | LDF6-50A(1-1/4) | 88.00-93.00 | 1.0000 | 1.0000 |
| L5 | 3 | HB158-1-08U8-S8118(1-5/8) | $88.00-93.00$ | 1.0000 | 1.0000 |
| L5 | 18 | Safety Line 3/8 | $88.00-93.00$ | 1.0000 | 1.0000 |
| ${ }^{\text {L } 6}$ | 2 | LDF6-50A(1-1/4) | $83.00-88.00$ | 1.0000 | 1.0000 |
| ${ }^{\text {L } 6}$ | ${ }_{3}$ | HB158-1-08U8-S8J18(1-5/8) | $83.00-88.00$ | 1.0000 | 1.0000 |
| L6 | 18 | Safety Line 3/8 | $83.00-88.00$ | 1.0000 | 1.0000 |
| ${ }^{2} 6$ | 42 | MP3-03 | 83.00-84.05 | 1.0000 | 1.0000 |
| L6 | 43 | MP3-03 | 83.00-84.05 | 1.0000 | 1.0000 |
| L6 | 44 | MP3-03 | 83.00-84.05 | 1.0000 | 1.0000 |
| L7 | 2 | LDF6-50A(1-1/4) | 82.33-83.00 | 1.0000 | 1.0000 |
| L7 | 3 | HB158-1-08U8-S8J18(1-5/8) | 82.33-83.00 | 1.0000 | 1.0000 |
| L7 | 18 | Safety Line 3/8 | 82.33-83.00 | 1.0000 | 1.0000 |
| L7 | 42 | MP3-03 | 82.33-83.00 | 1.0000 | 1.0000 |
| L7 | 43 | MP3-03 | 82.33-83.00 | 1.0000 | 1.0000 |
| L7 | 44 | MP3-03 | 82.33-83.00 | 1.0000 | 1.0000 |
| L8 | 2 | LDF6-50A(1-1/4) | 82.08-82.33 | 1.0000 | 1.0000 |
| L8 | 3 | HB158-1-08U8-S8J18(1-5/8) | 82.08-82.33 | 1.0000 | 1.0000 |
| L8 | 18 | Safety Line 3/8 | 82.08-82.33 | 1.0000 | 1.0000 |
| L8 | 42 | MP3-03 | 82.08-82.33 | 1.0000 | 1.0000 |
| L8 | 43 | MP3-03 | 82.08-82.33 | 1.0000 | 1.0000 |
| L8 | 44 | MP3-03 | 82.08-82.33 | 1.0000 | 1.0000 |
| L9 | 2 | LDF6-50A(1-1/4) | 77.08-82.08 | 1.0000 | 1.0000 |
| L9 | 3 | HB158-1-08U8-S8J18(1-5/8) | 77.08-82.08 | 1.0000 | 1.0000 |
| L9 | 13 | ATCB-B01(5/16) | $77.08-81.00$ | 1.0000 | 1.0000 |
| L9 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 77.08-81.00 | 1.0000 | 1.0000 |
| L9 | 18 | Safety Line 3/8 | 77.08-82.08 | 1.0000 | 1.0000 |
| L9 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 77.08-78.00 | 1.0000 | 1.0000 |
| L9 | 30 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 77.08-78.00 | 1.0000 | 1.0000 |
| L9 | 31 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 77.08-78.00 | 1.0000 | 1.0000 |
| L9 | 42 | MP3-03 | 77.08-82.08 | 1.0000 | 1.0000 |
| L9 | 43 | MP3-03 | 77.08-82.08 | 1.0000 | 1.0000 |
| L9 | 44 | MP3-03 | 77.08-82.08 | 1.0000 | 1.0000 |
| L10 | 2 | LDF6-50A(1-1/4) | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 3 | HB158-1-08U8-S8518(1-5/8) | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 13 | ATCB-B01(5/16) | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 18 | Safety Line 3/8 | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 30 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 31 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 42 | MP3-03 | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 43 | MP3-03 | 76.25-77.08 | 1.0000 | 1.0000 |
| L10 | 44 | MP3-03 | 76.25-77.08 | 1.0000 | 1.0000 |
| L11 | 2 | LDF6-50A(1-1/4) | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 3 | HB158-1-08U8-S8J18(1-5/8) | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 13 | ATCB-B01(5/16) | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 18 | Safety Line 3/8 | 76.00-76.25 | 1.0000 | 1.0000 |


| tnxTower <br> B+T Group | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA), CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 14 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date 15:01:04 09/21/18 |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L11 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 30 | $4.00^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 31 | 4.0 " $\times 1.25$ " Plate | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 42 | MP3-03 | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 43 | MP3-03 | 76.00-76.25 | 1.0000 | 1.0000 |
| L11 | 44 | MP3-03 | 76.00-76.25 | 1.0000 | 1.0000 |
| L12 | , | LDF6-50A(1-1/4) | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 3 | HB158-1-08U8-S8J18(1-5/8) | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 13 | ATCB-B01(5/16) | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 18 | Safety Line 3/8 | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 30 | $4.0{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 31 | $4.0^{\prime \prime} \times 1.25$ " Plate | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 42 | MP3-03 | 74.50-76.00 | 1.0000 | 1.0000 |
| L.12 | 43 | MP3-03 | 74.50-76.00 | 1.0000 | 1.0000 |
| L12 | 44 | MP3-03 | 74.50-76.00 | 1.0000 | 1.0000 |
| L13 | 2 | LDF6-50A(1-1/4) | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 3 | HB158-1-08U8-S8J18(1-5/8) | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 13 | ATCB-B01(5/16) | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 18 | Safety Line 3/8 | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 29 | 4.01 x 1.25" Plate | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 30 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 31 | $4.0^{\prime \prime} \times 1.25$ " Plate | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 42 | MP3-03 | 74.25-74.50 | 1.0000 | 1.0000 |
| L13 | 43 | MP3-03 | $74.25-74.50$ | 1.0000 | 1.0000 |
| L13 | 44 | MP3-03 | $74.25-74.50$ | 1.0000 | 1.0000 |
| L14 | 2 | LDF6-50A(1-1/4) | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 3 | HB158-1-08U8-S8J18(1-5/8) | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 13 | ATCB-B01(5/16) | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 14 | FXL 780 PE(7/8) | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 18 | Safety Line 3/8 | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 30 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 31 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 42 | MP3-03 | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 43 | MP3-03 | 69.25-74.25 | 1.0000 | 1.0000 |
| L14 | 44 | MP3-03 | 69.25-74.25 | 1.0000 | 1.0000 |
| L15 | 2 | LDF6-50A(1-1/4) | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 3 | HB158-1-08U8-S8J18(1-5/8) | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 13 | ATCB-B01(5/16) | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 18 | Safety Line 3/8 | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 29 | 4.01 x $1.25^{\prime \prime}$ Plate | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 30 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 31 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 42 | MP3-03 | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 43 | MP3-03 | 64.25-69.25 | 1.0000 | 1.0000 |
| L15 | 44 | MP3-03 | 64.25-69.25 | 1.0000 | 1.0000 |
| L16 | 2 | LDF6-50A(1-1/4) | 59.25-64.25 | 1.0000 | 1.0000 |
| L16 | 3 | HB158-1-08U8-S8J18(1-5/8) | 59.25-64.25 | 1.0000 | 1.0000 |
| L16 | 13 | ATCB-B01(5/16) | 59.25-64.25 | 1.0000 | 1.0000 |
| L16 | 14 | FXL 780 PE (7/8) | 59.25-64.25 | 1.0000 | 1.0000 |
| L16 | 18 | Safety Line 3/8 | 59.25-64.25 | 1.0000 | 1.0000 |
| L16 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.25-59.50 | 1.0000 | 1.0000 |
| L16 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.25-59.50 | 1.0000 | 1.0000 |
| L16 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.25-59.50 | 1.0000 | 1.0000 |
| L16 | 29 | $4.0^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.50-64.25 | 1.0000 | 1.0000 |
| L16 | 30 | $4.00^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.50-64.25 | 1.0000 | 1.0000 |
| L16 | 31 | $4.00^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 59.50-64.25 | 1.0000 | 1.0000 |
| L16 | 38 | MP3-05 | -59.25-60.50 | 1.0000 | 1.0000 |


| tnxTower <br> B + T Group | $\begin{array}{\|l} \text { Job } \\ 85565.009 .01 \text { - HARTFORD - NU (SSUSA), CT (BU\# 876363) } \end{array}$ |  | $\begin{aligned} & \text { Page } \\ & 15 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \\ \hline \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L16 | 39 | MP3-05 | 59.25-60.50 | 1.0000 | 1.0000 |
| L16 | 40 | MP3-05 | 59.25-60.50 | 1.0000 | 1.0000 |
| L16 | 42 | MP3-03 | 60.50-64.25 | 1.0000 | 1.0000 |
| L16 | 43 | MP3-03 | 60.50-64.25 | 1.0000 | 1.0000 |
| L16 | 44 | MP3-03 | 60.50-64.25 | 1.0000 | 1.0000 |
| L17 | 2 | LDF6-50A(1-1/4) | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 3 | HB158-1-08U8-S8J18(1-5/8) | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 13 | ATCB-B01(5/16) | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 18 | Safety Line 3/8 | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 38 | MP3-05 | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 39 | MP3-05 | 58.08-59.25 | 1.0000 | 1.0000 |
| L17 | 40 | MP3-05 | 58.08-59.25 | 1.0000 | 1.0000 |
| L18 | 2 | LDF6-50A(1-1/4) | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 3 | HB158-1-08U8-S8J18(1-5/8) | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 13 | ATCB-B01(5/16) | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 14 | FXL 780 PE(7/8) | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 18 | Safety Line 3/8 | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 38 | MP3-05 | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 39 | MP3-05 | 57.73-58.08 | 1.0000 | 1.0000 |
| L18 | 40 | MP3-05 | 57.73-58.08 | 1.0000 | 1.0000 |
| L19 | 2 | LDF6-50A(1-1/4) | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 3 | HB158-1-08U8-S8J18(1-5/8) | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 13 | ATCB-B01(5/16) | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 18 | Safety Line 3/8 | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 38 | MP3-05 | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 39 | MP3-05 | 57.50-57.73 | 1.0000 | 1.0000 |
| L19 | 40 | MP3-05 | 57.50-57.73 | 1.0000 | 1.0000 |
| L20 | 2 | LDF6-50A(1-1/4) | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 3 | HB158-1-08U8-S8J18(1-5/8) | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 13 | ATCB-B01(5/16) | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 18 | Safety Line 3/8 | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 38 | MP3-05 | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 39 | MP3-05 | 52.50-57.50 | 1.0000 | 1.0000 |
| L20 | 40 | MP3-05 | 52.50-57.50 | 1.0000 | 1.0000 |
| L21 | 2 | LDF6-50A(1-1/4) | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 3 | HB158-1-08U8-S8J18(1-5/8) | 47,00-52.50 | 1.0000 | 1.0000 |
| L21 | 13 | ATCB-B01(5/16) | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 18 | Safety Line 3/8 | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 27 | $4.375^{\prime \prime} \times 1.25$ " Plate | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 38 | MP3-05 | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 39 | MP3-05 | 47.00-52.50 | 1.0000 | 1.0000 |
| L21 | 40 | MP3-05 | 47.00-52.50 | 1.0000 | 1.0000 |
| L23 | 2 | LDF6-50A(1-1/4) | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 3 | HB158-1-08U8-S8J18(1-5/8) | 40.50-45.25 | 1.0000 | 1.0000 |


| tnxTower <br> B + T Group | Job85565.009 .01 - HARTFORD - NU (SSUSA),CT (BU\# 876363) |  | Page 16 of 42 |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line RecordNo. | Description | Feed Line Segment Eley. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{gathered} K_{a} \\ \mathrm{Ice} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L23 | 13 | ATCB-B01(5/16) | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 18 | Safety Line 3/8 | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 38 | MP3-05 | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 39 | MP3-05 | 40.50-45.25 | 1.0000 | 1.0000 |
| L23 | 40 | MP3-05 | 40.50-45.25 | 1.0000 | 1.0000 |
| L24 | 2 | LDF6-50A(1-1/4) | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 3 | HB158-1-08U8-S8J18(1-5/8) | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 13 | ATCB-B01(5/16) | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 18 | Safety Line 3/8 | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 33 | MP3-05 | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 35 | MP3-05 | 40.25-40.50 | 1.0000 | 1.0000 |
| L24 | 36 | MP3-05 | 40.25-40.50 | 1.0000 | 1.0000 |
| L25 | 2 | LDF6-50A(1-1/4) | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 3 | HB158-1-08U8-S8J18(1-5/8) | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 13 | ATCB-B01(5/16) | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 18 | Safety Line 3/8 | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 33 | MP3-05 | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 35 | MP3-05 | 35.25-40.25 | 1.0000 | 1.0000 |
| L25 | 36 | MP3-05 | 35.25-40.25 | 1.0000 | 1.0000 |
| L26 | 2 | LDF6-50A(1-1/4) | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 3 | HB158-1-08U8-S8J18(1-5/8) | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 13 | ATCB-B01(5/56) | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 18 | Safety Line 3/8 | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 33 | MP3-05 | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 35 | MP3-05 | 30.25-35.25 | 1.0000 | 1.0000 |
| L26 | 36 | MP3-05 | 30.25-35.25 | 1.0000 | 1.0000 |
| L27 | 2 | LDF6-50A(1-1/4) | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 3 | HB158-1-08U8-S8J18(1-5/8) | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 13 | ATCB-B01(5/16) | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 18 | Safety Line 3/8 | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 27.75-29.75 | 1.0000 | 1.0000 |
| L27 | 22 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 27.75-29.75 | 1.0000 | 1.0000 |
| L27 | 23 | 5.25 " $\times 1.25^{\prime \prime}$ Plate | 27.75-29.75 | 1.0000 | 1.0000 |
| L27 | 25 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 29.75-30.25 | 1.0000 | 1.0000 |
| L27 | 26 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 29.75-30.25 | 1.0000 | 1.0000 |
| L27 | 27 | $4.375^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 29.75-30.25 | 1.0000 | 1.0000 |
| L27 | 33 | MP3-05 | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 35 | MP3-05 | 27.75-30.25 | 1.0000 | 1.0000 |
| L27 | 36 | MP3-05 | 27.75-30.25 | 1.0000 | 1.0000 |
| L28 | 2 | LDF6-50A(1-1/4) | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 3 | HB158-1-08U8-S8J18(1-5/8) | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 13 | ATCB-B01(5/16) | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 18 | Safety Line 3/8 | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | \| 27.50-27.75| | 1.0000 | 1.0000 |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA), CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 17 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{gathered} K_{a} \\ \text { Ice } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L28 | 22 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 23 | 5.25 ' x 1.25 " Plate | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 33 | MP3-05 | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 35 | MP3-05 | 27.50-27.75 | 1.0000 | 1.0000 |
| L28 | 36 | MP3-05 | 27.50-27.75 | 1.0000 | 1.0000 |
| L29 | 2 | LDF6-50A(1-1/4) | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 3 | HB158-1-08U8-S8J18(1-5/8) | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 13 | ATCB-B01(5/16) | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 18 | Safety Line 3/8 | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 22 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 23 | 5.25 ' x $1.25^{\prime \prime}$ Plate | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 33 | MP3-05 | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 35 | MP3-05 | 22.50-27.50 | 1.0000 | 1.0000 |
| L29 | 36 | MP3-05 | 22.50-27.50 | 1.0000 | 1.0000 |
| L30 | 2 | LDF6-50A(1-1/4) | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 3 | HB158-1-08U8-S8J18(1-5/8) | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 13 | ATCB-B01(5/16) | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 18 | Safety Line 3/8 | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 20 | 5.25 ' x 1.25" Plate | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 22 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 23 | 5.25 " $\times 1.25^{\prime \prime}$ Plate | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 33 | MP3-05 | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 35 | MP3-05 | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 36 | MP3-05 | 19.50-22.50 | 1.0000 | 1.0000 |
| L30 | 47 | $\mathrm{CCl} 4.5^{\prime \prime} \times 1$ " Plate | 19.50-21.00 | 1.0000 | 1.0000 |
| L31 | 2 | LDF6-50A(1-1/4) | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 3 | HB158-1-08U8-S8J18(1-5/8) | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 13 | ATCB-B01(5/16) | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 18 | Safety Line 3/8 | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 20 | 5.25 ' x $1.25^{\prime \prime}$ Plate | 19.25-19.50 | 1.0000 | 1.0000 |
| L. 31 | 22 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 23 | 5.25 " x 1.25" Plate | 19.25-19.50 | 1.0000 | 1.0000 |
| L3] | 33 | MP3-05 | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 35 | MP3-05 | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 36 | MP3-05 | 19.25-19.50 | 1.0000 | 1.0000 |
| L31 | 47 | CCI 4.5" x 1" Plate | 19.25-19.50 | 1.0000 | 1.0000 |
| L32 | 2 | LDF6-50A(1-1/4) | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 3 | HB158-1-08U8-S8J18(1-5/8) | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 13 | ATCB-B01(5/16) | $14.25-19.25$ | 1.0000 | 1.0000 |
| L32 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 18 | Safety Line 3/8 | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 20 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 21 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 14.25-15.50 | 1.0000 | 1.0000 |
| L32 | 22 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 23 | 5.25 " x I. $25^{\prime \prime}$ Plate | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 33 | MP3-05 | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 34 | MP3-05 | 14.25-15.50 | 1.0000 | 1.0000 |
| L32 | 35 | MP3-05 | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 36 | MP3-05 | 14.25-19.25 | 1.0000 | 1.0000 |
| L32 | 46 | CCl $4.5{ }^{\prime \prime} \times 1^{\prime \prime}$ Plate | 14.25-15.50 | 1.0000 | 1.0000 |
| L32 | 47 | CCI $4.5{ }^{\prime \prime} \mathrm{x} 1^{\prime \prime}$ Plate | 14.25-19.25 | 1.0000 | 1.0000 |
| L33 | 2 | LDF6-50A(1-1/4) | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 3 | HB158-1-08U8-S8J18(1-5/8) | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 13 | ATCB-B01(5/16) | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 18 | Safety Line 3/8 | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 21 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |


| tnxTower <br> B + T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\text { Page } 18 \text { of } 42$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \\ \hline \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L33 | 22 | 5.25 " x $1.25{ }^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 23 | 5.25 " $\times 1.25^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 33 | MP3-05 | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 34 | MP3-05 | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 35 | MP3-05 | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 36 | MP3-05 | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 46 | CCI $4.5^{\prime \prime} \times 1^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |
| L33 | 47 | CCI $4.5^{\prime \prime} \times 1^{\prime \prime}$ Plate | 14.00-14.25 | 1.0000 | 1.0000 |
| L34 | 2 | LDF6-50A(1-1/4) | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 3 | HB158-1-08U8-S8118(1-5/8) | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 13 | ATCB-B01(5/16) | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 18 | Safety Line 3/8 | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 20 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 21 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 22 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 23 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 33 | MP3-05 | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 34 | MP3-05 | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 35 | MP3-05 | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 36 | MP3-05 | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 46 | CCI $4.5^{\prime \prime} \times 1$ " Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L34 | 47 | CCI $4.5^{\prime \prime} \times 1$ " Plate | 13.75-14.00 | 1.0000 | 1.0000 |
| L35 | 2 | LDF6-50A(1-1/4) | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 3 | HB158-1-08U8-S8J18(1-5/8) | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 13 | ATCB-B01(5/16) | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 18 | Safety Line 3/8 | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 20 | 5.25 ' x $1.25^{\prime \prime}$ Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 21 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 22 | 5.25 " $\times 1.25^{\prime \prime}$ Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 23 | $5.25{ }^{\prime \prime}$ x 1.25" Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 33 | MP3-05 | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 34 | MP3-05 | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 35 | MP3-05 | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 36 | MP3-05 | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 46 | $\mathrm{CCl} 4.5{ }^{\prime \prime} \times 1^{\prime \prime}$ Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L35 | 47 | CCI $4.5{ }^{\prime \prime} \times 1$ " Plate | 12.98-13.75 | 1.0000 | 1.0000 |
| L36 | 2 | LDF6-50A(1-1/4) | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 3 | HB158-1-08U8-S8J18(1-5/8) | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 13 | ATCB-B01(5/16) | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 18 | Safety Line 3/8 | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 20 | 5.25 " x 1.25" Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 21 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 22 | 5.25 " x $1.255^{\prime \prime}$ Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 23 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 33 | MP3-05 | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 34 | MP3-05 | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 35 | MP3-05 | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 36 | MP3-05 | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 46 | $\mathrm{CCl} 4.5{ }^{\prime \prime} \mathrm{x} 1^{\prime \prime}$ Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L36 | 47 | CCI $4.55^{\prime \prime} \times 1$ " Plate | 12.73-12.98 | 1.0000 | 1.0000 |
| L37 | 2 | LDF6-50A(1-1/4) | $7.73-12.73$ | 1.0000 | 1.0000 |
| L37 | 3 | HB158-1-08U8-S8J18(1-5/8) | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 13 | ATCB-B01(5/16) | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | $7.73-12.73$ | 1.0000 | 1.0000 |
| L37 | 18 | Safety Line 3/8 | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 20 | 5.25 " x $1.25^{\prime \prime}$ Plate | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 21 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 22 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 10.25-12.73 | 1.0000 | 1.0000 |
| L37 | 23 | 5.25 ' x 1.25" Plate | 7.73-12.73 | 1.0000 | 1.0000 |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\text { Page } 19 \text { of } 42$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { NoIce } \\ \hline \end{gathered}$ | $\begin{aligned} & \tilde{K}_{a} \\ & \text { Ice } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L37 | 33 | MP3-05 | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 34 | MP3-05 | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 35 | MP3-05 | 10.50-12.73 | 1.0000 | 1.0000 |
| L37 | 36 | MP3-05 | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 46 | CCI 4.5" $\times 1$ 1" Plate | 7.73-12.73 | 1.0000 | 1.0000 |
| L37 | 47 | CCI 4.5" x 1" Plate | 11.00-12.73 | 1.0000 | 1.0000 |
| L38 | 2 | LDF6-50A(1-1/4) | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 3 | HB158-1-08U8-S8J18(1-5/8) | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 13 | ATCB-B01(5/16) | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 18 | Safety Line 3/8 | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 21 | $5.25{ }^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 23 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 33 | MP3-05 | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 34 | MP3-05 | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 36 | MP3-05 | 2.73-7.73 | 1.0000 | 1.0000 |
| L38 | 46 | CCI 4.5 " x $1^{\prime \prime}$ Plate | 2.73-7.73 | 1.0000 | 1.0000 |
| L39 | 2 | LDF6-50A(1-1/4) | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 3 | HB158-1-08U8-S8J18(1-5/8) | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 13 | ATCB-B01(5/16) | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 14 | FXL $780 \mathrm{PE}(7 / 8)$ | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 18 | Safety Line 3/8 | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 20 | $5.25^{\prime \prime} \times 1.25^{\prime \prime}$ Plate | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 21 | 5.25 " x 1.25" Plate | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 23 | 5.25 " $\times 1.25^{\prime \prime}$ Plate | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 33 | MP3-05 | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 34 | MP3-05 | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 36 | MP3-05 | 0.00-2.73 | 1.0000 | 1.0000 |
| L39 | 46 | CCI $4.5{ }^{\prime \prime} \times 1^{\prime \prime}$ Plate | 0.00-2.73 | 1.0000 | 1.0000 |

## Discrete Tower Loads

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: <br> Horz <br> Lateral <br> Vert <br> ft <br> $f t$ <br> $f t$ | Azimuth Adjustment <br> 0 | Placement |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A} A_{A}$ Side $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BXA-70063/6CF w/ Mount Pipe (E) | A | From Leg | 4.000 | 0.000 | 105.000 | No Ice | 7.819 | 5.407 | 0.042 |
|  |  |  | 0.000 |  |  | $1 / 2^{11}$ Ice | 8.370 | 6.558 | 0.101 |
|  |  |  | 0.000 |  |  | 1" Ice | 8.886 | 7.422 | 0.168 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 9.942 | 9.198 | 0.328 |
| BXA-70063/6CF w/ Mount Pipe (E) | B | From Leg | 4.000 | 0.000 | 105.000 | No Ice | 7.819 | 5.407 | 0.042 |
|  |  |  | 0.000 |  |  | $1 / 2^{\text {I }}$ Ice | 8.370 | 6.558 | 0.101 |
|  |  |  | 0.000 |  |  | $1^{11}$ Ice | 8.886 | 7.422 | 0.168 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 9.942 | 9.198 | 0.328 |
| BXA-70063/6CF w/ Mount Pipe (E) | C | From Leg | 4.000 | 0.000 | 105.000 | No Ice | 7.819 | 5.407 | 0.042 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 8.370 | 6.558 | 0.101 |
|  |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 8.886 | 7.422 | 0.168 |
|  |  |  |  |  |  | $2^{\prime \prime}$ Ice | 9.942 | 9.198 | 0.328 |
| DB-T1-6Z-8AB-0Z <br> (E) | A | From Leg | 4.000 | 0.000 | 105.000 | No Ice | 4.800 | 2.000 | 0.044 |
|  |  |  | 0.000 |  |  | $1 / 2^{\prime \prime}$ Ice | 5.070 | 2.193 | 0.080 |
|  |  |  | 0.000 |  |  | $1^{1 \prime}$ Ice | 5.348 | 2.393 | 0.120 |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA), CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 20 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date $15: 01: 04 \text { 09/21/18 }$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face or \\
Leg
\end{tabular} \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front $f l^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight <br>

\hline \multirow[b]{4}{*}{| (2) SBNHH-1D65B |
| :--- |
| (P) |} \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{105.000} \& 2"Ice \& 5.926 \& 2.815 \& 0.213 <br>

\hline \& \& \& 4.000 \& \& \& No Ice \& 8.160 \& 5.396 \& 0.041 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 8.619 \& 5.853 \& 0.091 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 9.085 \& 6.317 \& 0.148 <br>
\hline \multirow[b]{4}{*}{(2) SBNHHY-1D65B (P)} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{105.000} \& $2^{\prime \prime}$ Ice \& 10.039 \& 7.267 \& 0.280 <br>
\hline \& \& \& 4.000 \& \& \& No Ice \& 8.160 \& 5.396 \& 0.041 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 8.619 \& 5.853 \& 0.091 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 9.085 \& 6.317 \& 0.148 <br>
\hline \multirow{4}{*}{(2) SBNHH-1D65B (P)} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.000} \& \multirow{4}{*}{105.000} \& $2^{\prime \prime}$ Ice \& 10.039 \& 7.267 \& 0.280 <br>
\hline \& \& \& 4.000 \& \& \& No Ice \& 8.160 \& 5.396 \& 0.041 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {" }}$ Ice \& 8.619 \& 5.853 \& 0.091 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\text {" }}$ Ice \& 9.085 \& 6.317 \& 0.148 <br>
\hline \multirow[b]{5}{*}{BXA-70063/6CF w/ Mount Pipe (P)} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.000} \& \multirow{5}{*}{105.000} \& $2^{\prime \prime}$ Ice \& 10.039 \& 7.267 \& 0.280 <br>
\hline \& \& \& 4.000 \& \& \& No Ice \& 7.819 \& 5.407 \& 0.042 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.370 \& 6.558 \& 0.101 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 8.886 \& 7.422 \& 0.168 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.942 \& 9.198 \& 0.328 <br>

\hline \multirow[t]{4}{*}{| BXA-70063/6CF w/ Mount Pipe |
| :--- |
| (P) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 7.819 \& 5.407 \& 0.042 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.370 \& 6.558 \& 0.101 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 8.886 \& 7.422 \& 0.168 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.942 \& 9.198 \& 0.328 <br>
\hline \multirow[t]{4}{*}{BXA-70063/6CF w/ Mount Pipe (P)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 7.819 \& 5.407 \& 0.042 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.370 \& 6.558 \& 0.101 <br>
\hline \& \& \& 0.000 \& \& \& 1 " Ice \& 8.886 \& 7.422 \& 0.168 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 9.942 \& 9.198 \& 0.328 <br>

\hline \multirow[t]{4}{*}{| (2) RFV01U-D1A |
| :--- |
| (P) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 1.875 \& 1.250 \& 0.084 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.045 \& 1.393 \& 0.103 <br>
\hline \& \& \& 0.000 \& \& \& ! Ice \& 2.223 \& 1.543 \& 0.124 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.601 \& 1.865 \& 0.175 <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& \text { RFV01U-DIA } \\
& (\mathrm{P})
\end{aligned}
$$} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 1.875 \& 1.250 \& 0.084 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {" }}$ Ice \& 2.045 \& 1.393 \& 0.103 <br>
\hline \& \& \& 0.000 \& \& \& $1^{1 \prime}$ Ice \& 2.223 \& 1.543 \& 0.124 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.601 \& 1.865 \& 0.175 <br>

\hline \multirow[t]{4}{*}{| RFV01U-D2A |
| :--- |
| (P) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 1.875 \& 1.013 \& 0.070 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.045 \& 1.145 \& 0.087 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.223 \& 1.284 \& 0.106 <br>
\hline \& \& \& \& \& \& $2^{11}$ Ice \& 2.601 \& 1.585 \& 0.153 <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& \text { (2) RFV01U-D2A } \\
& \text { (P) }
\end{aligned}
$$} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 1.875 \& 1.013 \& 0.070 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.045 \& 1.145 \& 0.087 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.223 \& 1.284 \& 0.106 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.601 \& 1.585 \& 0.153 <br>

\hline \multirow[t]{4}{*}{| RVZDC-6627-PF-48 |
| :--- |
| (P) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 3.792 \& 2.514 \& 0.032 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 4.044 \& 2.727 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 4.303 \& 2.947 \& 0.099 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 4.844 \& 3.417 \& 0.181 <br>
\hline \multirow[t]{4}{*}{B13 RRH 4X30 (P-previous App)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.055 \& 1.320 \& 0.056 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {n }}$ Ice \& 2.241 \& 1.475 \& 0.073 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.433 \& 1.638 \& 0.093 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.841 \& 1.997 \& 0.142 <br>

\hline \multirow[t]{4}{*}{| B13 RRH 4X30 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.055 \& 1.320 \& 0.056 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.241 \& 1.475 \& 0.073 <br>
\hline \& \& \& 0.000 \& \& \& $1^{1 \prime}$ Ice \& 2.433 \& 1.638 \& 0.093 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.841 \& 1.997 \& 0.142 <br>
\hline \multirow[t]{4}{*}{B13 RRH 4X30
(P-previous App)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.055 \& 1.320 \& 0.056 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.241 \& 1.475 \& 0.073 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.433 \& 1.638 \& 0.093 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.841 \& 1.997 \& 0.142 <br>
\hline
\end{tabular}



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& Offsets:
Horz
Lateral
Vert
\(f t\)
\(f t\)
\(f t\)
\(f t\) \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ Front |
| :--- |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side \& Weight

$K$ <br>

\hline \multirow[t]{4}{*}{| RRH4X45-AWS4 B66 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.660 \& 1.586 \& 0.064 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{11}$ Ice \& 2.878 \& 1.769 \& 0.084 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.104 \& 1.959 \& 0.108 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.577 \& 2.359 \& 0.165 <br>

\hline \multirow[t]{4}{*}{| RRH4X45-AWS4 B66 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.660 \& 1.586 \& 0.064 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.878 \& 1.769 \& 0.084 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.104 \& 1.959 \& 0.108 <br>
\hline \& \& \& \& \& \& 2 I' Ice \& 3.577 \& 2.359 \& 0.165 <br>

\hline \multirow[t]{4}{*}{| RRH4X45-AWS4 B66 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.660 \& 1.586 \& 0.064 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.878 \& 1.769 \& 0.084 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\text {I }}$ Ice \& 3.104 \& 1.959 \& 0.108 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.577 \& 2.359 \& 0.165 <br>

\hline \multirow[t]{4}{*}{| B25 RRH4X30 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.200 \& 1.742 \& 0.055 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {" }}$ Ice \& 2.393 \& 1.920 \& 0.075 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.593 \& 2.106 \& 0.099 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.015 \& 2.501 \& 0.156 <br>

\hline \multirow[t]{4}{*}{| B25 RRH4X30 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.200 \& 1.742 \& 0.055 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.393 \& 1.920 \& 0.075 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.593 \& 2.106 \& 0.099 <br>
\hline \& \& \& \& \& \& 2"Ice \& 3.015 \& 2.501 \& 0.156 <br>

\hline \multirow[t]{4}{*}{| B25 RRH4X30 |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 2.200 \& 1.742 \& 0.055 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.393 \& 1.920 \& 0.075 <br>
\hline \& \& \& 0.000 \& \& \& $1^{1 \prime}$ Ice \& 2.593 \& 2.106 \& 0.099 <br>
\hline \& \& \& \& \& \& $2^{11}$ Ice \& 3.015 \& 2.501 \& 0.156 <br>

\hline \multirow[t]{4}{*}{| DB-T1-6Z-8AB-0Z |
| :--- |
| (P-previous App) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 4.800 \& 2.000 \& 0.044 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {¹ }}$ Ice \& 5.070 \& 2.193 \& 0.080 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.348 \& 2.393 \& 0.120 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 5.926 \& 2.815 \& 0.213 <br>
\hline \multirow[t]{4}{*}{Sector Mount [SM 402-3] (E-2M.P/sector)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{105.000} \& No Ice \& 18.910 \& 18.910 \& 0.851 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 26.780 \& 26.780 \& 1.233 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 34.650 \& 34.650 \& 1.616 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 50.390 \& 50.390 \& 2.381 <br>
\hline *\$* \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{4}{*}{| APXV9ERR18-C-A20 w/ Mount Pipe |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 8.262 \& 7.471 \& 0.088 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.822 \& 8.656 \& 0.158 <br>
\hline \& \& \& 1.000 \& \& \& $1^{11}$ Ice \& 9.346 \& 9.556 \& 0.237 <br>
\hline \& \& \& \& \& \& 2"Ice \& 10.418 \& 11.388 \& 0.421 <br>

\hline \multirow[t]{4}{*}{APXVSPP18-C-A20 w/ Mount Pipe (E)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& $$
4.000
$$ \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 8.262 \& 6.946 \& 0.083 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 8.822 \& 8.127 \& 0.151 <br>
\hline \& \& \& 1.000 \& \& \& 1" Ice \& 9.346 \& 9.021 \& 0.227 <br>
\hline \& \& \& \& \& \& 2" Ice \& 10.418 \& 10.844 \& 0.406 <br>
\hline \multirow[t]{4}{*}{APXVSPP18-C-A20 w/ Mount Pipe (E)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 8.262 \& 6.946 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 8.822 \& 8.127 \& 0.151 <br>
\hline \& \& \& 1.000 \& \& \& 1 I' Ice \& 9.346 \& 9.021 \& 0.227 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 10.418 \& 10.844 \& 0.406 <br>

\hline \multirow[t]{4}{*}{| IBC1900BB-1 |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& 2"Ice \& 1.510 \& 0.893 \& 0.065 <br>

\hline \multirow[t]{4}{*}{| IBC1900BB-1 |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& \[

4.000
\] \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& $1^{11}$ Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.510 \& 0.893 \& 0.065 <br>

\hline \multirow[t]{4}{*}{| IBC1900BB-1 |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 1.510 \& 0.893 \& 0.065 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 \end{array}$ | ORD - NU (SS | $\begin{aligned} & \text { Page } 22 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{c} 
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft \\
\hline
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
-
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front \\
\(f t^{2}\)
\end{tabular} \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Side \\
\(f t^{2}\)
\end{tabular} \& Weight

$K$ <br>

\hline \multirow[t]{4}{*}{| IBC1900HG-2A |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& 2"Ice \& 1.510 \& 0.893 \& 0.065 <br>

\hline \multirow[t]{4}{*}{| IBC1900HG-2A |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& $1 "$ Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.510 \& 0.893 \& 0.065 <br>

\hline \multirow[t]{4}{*}{| IBCl900HG-2A |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 0.966 \& 0.463 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.091 \& 0.558 \& 0.030 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.223 \& 0.660 \& 0.039 <br>
\hline \& \& \& \& \& \& 2 'Ice \& 1.510 \& 0.893 \& 0.065 <br>

\hline \multirow[t]{4}{*}{| AAHC w/ Mount Pipe |
| :--- |
| (R) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 4.409 \& 2.691 \& 0.115 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {It }}$ Ice \& 4.727 \& 3.079 \& 0.156 <br>
\hline \& \& \& 1.000 \& \& \& 1" Ice \& 5.055 \& 3.486 \& 0.202 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 5.743 \& 4.359 \& 0.310 <br>

\hline \multirow[t]{4}{*}{| AAHC w/ Mount Pipe |
| :--- |
| (R) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 4.409 \& 2.691 \& 0.115 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 4.727 \& 3.079 \& 0.156 <br>
\hline \& \& \& 1.000 \& \& \& $1^{\prime \prime}$ Ice \& 5.055 \& 3.486 \& 0.202 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 5.743 \& 4.359 \& 0.310 <br>

\hline \multirow[t]{4}{*}{| AAHC w/ Mount Pipe |
| :--- |
| (R) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 4.409 \& 2.691 \& 0.115 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 4.727 \& 3.079 \& 0.156 <br>
\hline \& \& \& 1.000 \& \& \& 1 ' Ice \& 5.055 \& 3.486 \& 0.202 <br>
\hline \& \& \& \& \& \& $2^{11}$ Ice \& 5.743 \& 4.359 \& 0.310 <br>

\hline \multirow[t]{4}{*}{| Platform Mount [LP 1201-1] |
| :--- |
| (E) |} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{98.000} \& No Ice \& 23.100 \& 23.100 \& 2.100 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 26.800 \& 26.800 \& 2.500 <br>
\hline \& \& \& \& \& \& 1" Ice \& 30.500 \& 30.500 \& 2.900 <br>
\hline \& \& \& \& \& \& 2" Ice \& 37.900 \& 37.900 \& 3.700 <br>
\hline \multicolumn{8}{|l|}{*\$\$* ${ }^{\text {* }}$} \& \& <br>
\hline PCS 1900MHz \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>
\hline $4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ \& \& \& 0.000 \& \& \& 1/2 $2^{\text {I' }}$ Ice \& 2.527 \& 2.441 \& 0.083 <br>
\hline \multirow[t]{2}{*}{(E)} \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>

\hline $$
4 \times 45 \mathrm{~W}-65 \mathrm{MHz}
$$ \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.527 \& 2.441 \& 0.083 <br>

\hline \multirow[t]{2}{*}{(E)} \& \& \& 0.000 \& \& \& $1^{11}$ Ice \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline PCS 1900 MHz \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>
\hline $4 \mathrm{x} 45 \mathrm{~W}-65 \mathrm{MHz}$ \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.527 \& 2.441 \& 0.083 <br>
\hline \multirow[t]{2}{*}{} \& \& \& 0.000 \& \& \& 1 " Ice \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline PCS 1900 MHz \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>
\hline $4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.527 \& 2.441 \& 0.083 <br>
\hline \multirow[t]{2}{*}{(E)} \& \& \& -1.000 \& \& \& 1" Ice \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline PCS 1900 MHz \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>
\hline $4 \mathrm{x} 45 \mathrm{~W}-65 \mathrm{MHz}$ \& \& \& 0.000 \& \& \& $1 / 2^{1}$ Ice \& 2.527 \& 2.441 \& 0.083 <br>
\hline \multirow[t]{2}{*}{(E)} \& \& \& $-1.000$ \& \& \& $1^{\prime \prime}$ Ice \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline PCS 1900 MHz \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.322 \& 2.238 \& 0.060 <br>
\hline $4 \mathrm{x} 45 \mathrm{~W}-65 \mathrm{MHz}$ \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.527 \& 2.441 \& 0.083 <br>
\hline \multirow[t]{2}{*}{} \& \& \& -1.000 \& \& \& 1 1ce \& 2.739 \& 2.651 \& 0.110 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.185 \& 3.093 \& 0.173 <br>
\hline 800 MHz 2 X 50 W RRH \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.058 \& 1.932 \& 0.064 <br>
\hline W/FILTER \& \& \& 0.000 \& \& \& $1 / 2^{\text {1 }}$ Ice \& 2.240 \& 2.109 \& 0.086 <br>
\hline (E) \& \& \& 0.000 \& \& \& 1" Ice \& 2.429 \& 2.293 \& 0.111 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 2.829 \& 2.684 \& 0.172 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 | Job <br> 85565.009 .01 - HARTFORD - NU (SSUSA),CT (BU\# 876363) |  | $\begin{aligned} & \text { Page } \\ & 23 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
-
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f l^{2}
\] \& \begin{tabular}{l}
\(C_{A} A_{A}\) Side \\
\(f t^{2}\)
\end{tabular} \& Weight

$K$ <br>
\hline \multirow[t]{4}{*}{800MHz 2X50W RRH W/FILTER (E)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.058 \& 1.932 \& 0.064 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.240 \& 2.109 \& 0.086 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& $1^{\prime \prime}$ Ice \& 2.429 \& 2.293 \& 0.111 <br>
\hline \& \& \& \& \& \& $2^{11}$ Ice \& 2.829 \& 2.684 \& 0.172 <br>
\hline \multirow[t]{4}{*}{800 MHz 2 X 50 W RRH W/FILTER (E)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 2.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 2.058 \& 1.932 \& 0.064 <br>
\hline \& \& \& 0.000 \& \& \& 1/2 ${ }^{\text {11 }}$ Ice \& 2.240 \& 2.109 \& 0.086 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 2.429 \& 2.293 \& 0.111 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.829 \& 2.684 \& 0.172 <br>
\hline \multirow[t]{4}{*}{$4^{\prime} \times 2$ 2" Pipe Mount (E)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 1.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 0.785 \& 0.785 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.028 \& 1.028 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\text {H }}$ Ice \& 1.281 \& 1.281 \& 0.044 <br>
\hline \& \& \& \& \& \& $2^{11}$ Ice \& 1.814 \& 1.814 \& 0.072 <br>

\hline \multirow[t]{4}{*}{| $4^{\prime} \times 2^{\prime \prime}$ Pipe Mount |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 1.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 0.785 \& 0.785 \& 0.029 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {" }}$ Ice \& 1.028 \& 1.028 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.281 \& 1.281 \& 0.044 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.814 \& 1.814 \& 0.072 <br>

\hline \multirow[t]{4}{*}{| 4' x 2" Pipe Mount |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 1.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 0.785 \& 0.785 \& 0.029 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.028 \& 1.028 \& 0.035 <br>
\hline \& \& \& 0.000 \& \& \& 1 Ice \& 1.281 \& 1.281 \& 0.044 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.814 \& 1.814 \& 0.072 <br>

\hline \multirow[t]{4}{*}{| Side Arm Mount [SO 102-3] |
| :--- |
| (E) |} \& \multirow[t]{6}{*}{C} \& \multirow[t]{6}{*}{None} \& \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{96.000} \& No Ice \& 3.000 \& 3.000 \& 0.081 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 3.480 \& 3.480 \& 0.111 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 3.960 \& 3.960 \& 0.141 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 4.920 \& 4.920 \& 0.201 <br>
\hline \& \& \& \& \& \& \& \& \& <br>
\hline \multicolumn{8}{|l|}{*\$\$} \& \& <br>

\hline \multirow[t]{4}{*}{| HBX-6516DS-VTM w/ Mount Pipe |
| :--- |
| (E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 3.598 \& 3.241 \& 0.029 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.998 \& 3.914 \& 0.062 <br>
\hline \& \& \& -1.000 \& \& \& $1^{\prime \prime}$ Ice \& 4.389 \& 4.564 \& 0.101 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 5.187 \& 5.914 \& 0.199 <br>
\hline \multirow[t]{4}{*}{HBX-6516DS-VTM w/ Mount Pipe (E)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 3.598 \& 3.241 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\text {H }}$ Ice \& 3.998 \& 3.914 \& 0.062 <br>
\hline \& \& \& -1.000 \& \& \& $1^{\prime \prime}$ Ice \& 4.389 \& 4.564 \& 0.101 <br>
\hline \& \& \& \& \& \& 2" Ice \& 5.187 \& 5.914 \& 0.199 <br>
\hline \multirow[t]{4}{*}{HBX-6516DS-VTM w/ Mount Pipe (E)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 3.598 \& 3.241 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.998 \& 3.914 \& 0.062 <br>
\hline \& \& \& -1.000 \& \& \& $1{ }^{1 \prime}$ Ice \& 4.389 \& 4.564 \& 0.101 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 5.187 \& 5.914 \& 0.199 <br>

\hline \multirow[t]{4}{*}{$6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (E)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& $$
4.000
$$ \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 1.425 \& 1.425 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.925 \& 1.925 \& 0.033 <br>
\hline \& \& \& -1.000 \& \& \& 1 I' Ice \& 2.294 \& 2.294 \& 0.048 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.060 \& 3.060 \& 0.090 <br>
\hline \multirow[t]{4}{*}{$6^{\prime} \times 2^{\prime \prime}$ Mount Pipe (E)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 1.425 \& 1.425 \& 0.022 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.925 \& 1.925 \& 0.033 <br>
\hline \& \& \& -1.000 \& \& \& 1" Ice \& 2.294 \& 2.294 \& 0.048 <br>
\hline \& \& \& \& \& \& 2"Ice \& 3.060 \& 3.060 \& 0.090 <br>
\hline \multirow[t]{4}{*}{$6 \times 2^{11}$ Mount Pipe (E)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 1.425 \& 1.425 \& 0.022 <br>

\hline \& \& \& $$
0.000
$$ \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.925 \& 1.925 \& 0.033 <br>

\hline \& \& \& -1.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.294 \& 2.294 \& 0.048 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.060 \& 3.060 \& 0.090 <br>

\hline \multirow[t]{4}{*}{| T-Arm Mount [TA 602-3] |
| :--- |
| (E) |} \& \multirow[t]{5}{*}{C} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{81.000} \& No Ice \& 11.590 \& 11.590 \& 0.774 <br>

\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 15.440 \& 15.440 \& 0.990 <br>
\hline \& \& \& \& \& \& 1 1' Ice \& 19.290 \& 19.290 \& 1.206 <br>
\hline \& \& \& \& \& \& 2"Ice \& 26.990 \& 26.990 \& 1.639 <br>
\hline *\$* \& \& \& \& \& \& \& \& \& <br>
\hline KS24019-L112A \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{From Leg} \& 3.000 \& \multirow[t]{2}{*}{0.000} \& \multirow[t]{2}{*}{74.000} \& No Ice \& 0.141 \& 0.141 \& 0.005 <br>
\hline (E) \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 0.198 \& 0.198 \& 0.007 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 24 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
-
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight

$K$ <br>

\hline \multirow{6}{*}{| Side Arm Mount [SO 701-1] |
| :--- |
| (E) |} \& \multirow{6}{*}{A} \& \multirow{7}{*}{From Leg} \& 2.000 \& \multirow{7}{*}{0.000} \& \multirow{7}{*}{74.000} \& 1" Ice \& 0.262 \& 0.262 \& 0.009 <br>

\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 0.415 \& 0.415 \& 0.018 <br>
\hline \& \& \& 1.500 \& \& \& No Ice \& 0.850 \& 1.670 \& 0.065 <br>
\hline \& \& \& 0.000 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 1.140 \& 2.340 \& 0.079 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.430 \& 3.010 \& 0.093 <br>
\hline \& \& \& \& \& \& 2 İce \& 2.010 \& 4.350 \& 0.121 <br>
\hline *\$ * \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Dishes

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Dish Type \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& \begin{tabular}{l}
\(3 d B\) \\
Beam \\
Width \\
-
\end{tabular} \& Elevation \& \begin{tabular}{l}
Outside Diameter \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Aperture Area \\
\(f t^{2}\)
\end{tabular} \& Weight

K <br>
\hline *\$\$* \& \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | $0.9 \mathrm{Dead}+1.0 \mathrm{~W}$ ind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead +1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | I.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead +1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | $1.2 \mathrm{Dead}+1.0 \mathrm{Ice}+1.0 \mathrm{Temp}$ |
| 27 | 1.2 Dead+1.0 Wind $0 \mathrm{deg}+1.0 \mathrm{Ice+1.0}$ Temp |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 \end{array}$ | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 25 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Comb. No. | Description |
| :---: | :---: |
| 28 | 1.2 Dead+I.0 Wind $30 \mathrm{deg}+1.0$ Ice+ 1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice +1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind $210 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead +1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0$ Ice +1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind $330 \mathrm{deg}+1.0 \mathrm{Ice}+1.0 \mathrm{Temp}$ |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |


|  | Maximum Member Forces |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | $\begin{gathered} \text { Elevation } \\ \mathrm{ft} \end{gathered}$ | Component Type | Condition | Gov. <br> Load <br> Comb. | Axial $K$ | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| L1 | 108-103 | Pole | Max Tension | 48 | 0.000 | -0.000 | -0.000 |
|  |  |  | Max. Compression | 26 | -9.569 | 1.499 | 0.268 |
|  |  |  | Max. Mx | 20 | -2.394 | 13.847 | 0.035 |
|  |  |  | Max. My | 2 | -2.395 | 0.620 | 13.264 |
|  |  |  | Max. Vy | 20 | -6.512 | 13.847 | 0.035 |
|  |  |  | Max. Vx | 2 | -6.527 | 0.620 | 13.264 |
|  |  |  | Max. Torque | 2 |  |  | 0.352 |
| L2 | 103-98.5 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -10.032 | 1.614 | 0.331 |
|  |  |  | Max. Mx | 20 | -2.614 | 43.379 | -0.198 |
|  |  |  | Max. My | 2 | -2.615 | 0.398 | 42.860 |
|  |  |  | Max. Vy | 20 | -6.609 | 43.379 | -0.198 |
|  |  |  | Max. Vx | 2 | -6.624 | 0.398 | 42.860 |
|  |  |  | Max. Torque | 2 |  |  | 0.352 |
| L3 | 98.5-98 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max Compression | 26 | -10.108 | 1.631 | 0.342 |
|  |  |  | Max. Mx | 20 | -2.659 | 46.690 | -0.223 |
|  |  |  | Max. My | 2 | -2.659 | 0.374 | 46.178 |
|  |  |  | Max. Vy | 20 | -6.629 | 46.690 | -0.223 |
|  |  |  | Max. Vx | 2 | -6.644 | 0.374 | 46.178 |
|  |  |  | Max. Torque | 2 |  |  | 0.352 |
| L4 | 98-93 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -19.444 | 1.823 | 0.531 |
|  |  |  | Max. Mx | 20 | -6.789 | 100.043 | -0.465 |
|  |  |  | Max. My | 2 | -6.792 | 0.132 | 99.498 |
|  |  |  | Max. Vy | 20 | -11.020 | 100.043 | -0.465 |
|  |  |  | Max. Vx | 2 | -11.014 | 0.132 | 99.498 |
|  |  |  | Max. Torque | 16 |  |  | -0.373 |
| L5 | 93-88 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 26 | -20.131 | 2.015 | 0.649 |


| tnxTower <br> B + T Group | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 26 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Section No. \& Elevation $f t$ \& Component Type \& Condition \& Gov. Load Comb. \& Axial

$K$ \& \[
$$
\begin{gathered}
\text { Major Axis } \\
\text { Moment } \\
\text { kip-ft } \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
\text { Minor Axis } \\
\text { Moment } \\
\text { kip-ft }
\end{gathered}
$$
\] <br>

\hline \multirow{9}{*}{L6} \& \multirow{9}{*}{88-83} \& \multirow{8}{*}{Pole} \& Max Mx \& 20 \& -7.118 \& 155.747 \& -0.725 <br>
\hline \& \& \& Max. My \& 2 \& -7.121 \& -0.112 \& 155.161 <br>
\hline \& \& \& Max. Vy \& 20 \& -11.261 \& 155.747 \& -0.725 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-11.255} \& \multirow[t]{2}{*}{-0.112} \& 155.161 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.372 <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -20.877 \& 2.200 \& 0.767 <br>
\hline \& \& \& Max. Mx \& 20 \& -7.484 \& 212.618 \& -0.984 <br>
\hline \& \& \multirow{8}{*}{Pole} \& Max. My \& 2 \& -7.487 \& -0.357 \& 211.991 <br>
\hline \multirow{7}{*}{L7} \& \multirow{7}{*}{83-82.33} \& \& Max. Vy \& 20 \& -11.491 \& 212.618 \& -0.984 <br>

\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-11.485} \& \multirow[t]{2}{*}{-0.357} \& \multirow[t]{2}{*}{$$
\begin{gathered}
211.991 \\
-0.372
\end{gathered}
$$} <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -20.999 \& 2.225 \& 0.782 <br>
\hline \& \& \& Max. Mx \& 20 \& -7.537 \& 220.334 \& -1.018 <br>
\hline \& \& \& Max. My \& 2 \& -7.540 \& -0.390 \& 219.703 <br>
\hline \multirow{7}{*}{L8} \& \multirow{6}{*}{82.33-82.08} \& \multirow{6}{*}{Pole} \& Max. Vy \& 20 \& -11.547 \& 220.334 \& -1.018 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-11.541} \& \multirow[t]{2}{*}{-0.390} \& 219.703 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.372 <br>

\hline \& \& \& Max Tension \& 1 \& $$
0.000
$$ \& 0.000 \& 0.000 <br>

\hline \& \& \& Max. Compression \& 26 \& -21.054 \& 2.235 \& 0.789 <br>
\hline \& \& \& Max. Mx \& 20 \& -7.569 \& 223.224 \& -1.031 <br>
\hline \& \multirow{8}{*}{82.08-77.08} \& \multirow{8}{*}{Pole} \& Max. My \& 2 \& -7.571 \& -0.402 \& 222.590 <br>
\hline \multirow{7}{*}{L9} \& \& \& Max. Vy \& 20 \& -11.567 \& 223.224 \& -1.031 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-11.561} \& \multirow[t]{2}{*}{-0.402} \& \multirow[t]{2}{*}{222.590
-0.372} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -24.838 \& 2.419 \& 0.834 <br>
\hline \& \& \& Max. Mx \& 20 \& -9.106 \& 286.418 \& -1.296 <br>
\hline \& \& \& Max. My \& 2 \& $-9.109$ \& -0.647 \& 285.736 <br>
\hline \multirow{6}{*}{L10} \& \multirow{6}{*}{77.08-76.25} \& \multirow{6}{*}{Pole} \& Max. Vy \& 20 \& -13.251 \& 286.418 \& -1.296 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-13.245} \& \multirow[t]{2}{*}{-0.647} \& \multirow[t]{2}{*}{285.736
-0.372} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -25.070 \& 2.450 \& 0.839 <br>
\hline \& \& \& Max. Mx \& 20 \& -9.198 \& 297.449 \& -1.341 <br>
\hline \multirow{9}{*}{L11} \& \multirow{9}{*}{76.25-76} \& \multirow{9}{*}{Pole} \& Max. My \& 2 \& -9.201 \& -0.687 \& 296.759 <br>
\hline \& \& \& Max. Vy \& 20 \& -13.333 \& 297.449 \& -1.341 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-13.327} \& \multirow[t]{2}{*}{-0.687} \& \multirow[t]{2}{*}{296.759
-0.372} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -25.152 \& 2.461 \& 0.840 <br>
\hline \& \& \& Max. Mx \& 20 \& -9.243 \& 300.786 \& -1.354 <br>
\hline \& \& \& Max. My \& 2 \& -9.245 \& -0.700 \& 300.093 <br>
\hline \& \& \& Max. Vy \& 20 \& -13.356 \& 300.786 \& -1.354 <br>
\hline \multirow{5}{*}{L12} \& \multirow{5}{*}{76-74.5} \& \multirow{4}{*}{Pole} \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-13.350} \& \multirow[t]{2}{*}{-0.700} \& \multirow[b]{2}{*}{-0.371} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -25.647 \& 2.515 \& 0.847 <br>
\hline \& \& \multirow{12}{*}{Pole} \& Max. Mx \& 20 \& -9.463 \& 320.947 \& -1.434 <br>
\hline \multirow{11}{*}{L13} \& \multirow{11}{*}{74.5-74.25} \& \& Max. My \& 2 \& -9.466 \& -0.773 \& 320.240 <br>
\hline \& \& \& Max. Vy \& 20 \& -13.525 \& 320.947 \& -1.434 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-13.518} \& \multirow[t]{2}{*}{-0.773} \& 320.240 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& \multirow[t]{2}{*}{-0.371
0.000} <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& <br>
\hline \& \& \& Max. Compression \& 26 \& -25.732 \& 2.527 \& 0.849 <br>
\hline \& \& \& Max. Mx \& 20 \& -9.514 \& 324.332 \& -1.447 <br>
\hline \& \& \& Max. My \& 2 \& -9.517 \& -0.785 \& 323.621 <br>
\hline \& \& \& Max. Vy \& 20 \& -13.546 \& 324.332 \& -1.447 <br>
\hline \& \& \& Max. Vx \& 2 \& -13.540 \& -0.785 \& 323.621 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.371 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 . \end{array}$ | ORD - NU (SSl | $\begin{aligned} & \text { Page } \\ & 27 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Section No. \& $$
\begin{aligned}
& \text { Elevation } \\
& f t
\end{aligned}
$$ \& Component Type \& Condition \& Gov. Load Comb. \& Axial
$K$ \& Major Axis Moment kip-ft \& Minor Axis Moment kip-ft <br>
\hline \multirow[t]{8}{*}{L14

15} \& \multirow[t]{7}{*}{74.25-69.25} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -27.587 \& 2.712 \& 1.245 <br>
\hline \& \& \& Max. Mx \& 20 \& -10.407 \& 393.904 \& -1.522 <br>
\hline \& \& \& Max. My \& 2 \& -10.412 \& -1.029 \& 393.166 <br>
\hline \& \& \& Max. Vy \& 20 \& -14.193 \& 393.904 \& -1.522 <br>
\hline \& \& \& Max. Vx \& 2 \& -14.149 \& -1.029 \& 393.166 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.475 <br>
\hline \& \multirow[t]{7}{*}{69.25-64.25} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \multirow{6}{*}{L15} \& \& \& Max. Compression \& 26 \& -29.306 \& 2.901 \& 1.269 <br>
\hline \& \& \& Max. Mx \& 20 \& -11.250 \& 466.243 \& -1.789 <br>
\hline \& \& \& Max. My \& 2 \& -11.254 \& -1.273 \& 465.260 <br>
\hline \& \& \& Max. Vy \& 20 \& -14.744 \& 466.243 \& -1.789 <br>
\hline \& \& \& Max. Vx \& 2 \& -14.699 \& -1.273 \& 465.260 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.475 <br>
\hline \multirow[t]{7}{*}{L16} \& \multirow[t]{7}{*}{64.25-59.25} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -31.044 \& 3.092 \& 1.292 <br>
\hline \& \& \& Max. Mx \& 20 \& -12.112 \& 541.333 \& -2.055 <br>
\hline \& \& \& Max. My \& 2 \& -12.117 \& -1.515 \& 540.105 <br>
\hline \& \& \& Max. Vy \& 20 \& -15.295 \& 541.333 \& -2.055 <br>
\hline \& \& \& Max. Vx \& 2 \& -15.250 \& -1.515 \& 540.105 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.475 <br>
\hline \multirow[t]{7}{*}{L17} \& \multirow[t]{7}{*}{59.25-58.08} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -31.462 \& 3.136 \& 1.297 <br>
\hline \& \& \& Max. Mx \& 20 \& -12.317 \& 559.304 \& -2.118 <br>
\hline \& \& \& Max. My \& 2 \& -12.321 \& $-1.572$ \& 558.019 <br>
\hline \& \& \& Max. Vy \& 20 \& -15.429 \& 559.304 \& -2.118 <br>
\hline \& \& \& Max. Vx \& 2 \& -15.384 \& -1.572 \& 558.019 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.474 <br>
\hline \multirow[t]{7}{*}{L18} \& \multirow[t]{7}{*}{58.08-57.73} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -31.601 \& 3.151 \& 1.299 <br>
\hline \& \& \& Max. Mx \& 20 \& -12.399 \& 564.711 \& -2.136 <br>
\hline \& \& \& Max. My \& 2 \& -12.403 \& -1.589 \& 563.409 <br>
\hline \& \& \& Max. Vy \& 20 \& -15.464 \& 564.711 \& -2.136 <br>
\hline \& \& \& Max. Vx \& 2 \& -15.419 \& -1.589 \& 563.409 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.474 <br>
\hline \multirow[t]{7}{*}{L19} \& \multirow[t]{7}{*}{57.73-57.5} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -31.693 \& 3.161 \& 1.300 <br>
\hline \& \& \& Max. Mx \& 20 \& -12.449 \& 568.271 \& -2.149 <br>
\hline \& \& \& Max. My \& 2 \& -12.453 \& -1.600 \& 566.958 <br>
\hline \& \& \& Max. Vy \& 20 \& -15.490 \& 568.271 \& -2.149 <br>
\hline \& \& \& Max. Vx \& 2 \& -15.445 \& -1.600 \& 566.958 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.474 <br>
\hline \multirow[t]{7}{*}{L20} \& \multirow[t]{7}{*}{57.5-52.5} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -33.671 \& 3.350 \& 1.321 <br>
\hline \& \& \& Max. Mx \& 20 \& -13.505 \& 647.201 \& -2.414 <br>
\hline \& \& \& Max. My \& 2 \& -13.509 \& -1.842 \& 645.642 <br>
\hline \& \& \& Max. Vy \& 20 \& -16.079 \& 647.201 \& -2.414 <br>
\hline \& \& \& Max. Vx \& 2 \& -16.034 \& -1.842 \& 645.642 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.474 <br>
\hline \multirow[t]{7}{*}{L21} \& \multirow[t]{7}{*}{52.5-47} \& \multirow[t]{7}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -34.566 \& 3.437 \& 1.330 <br>
\hline \& \& \& Max. Mx \& 20 \& -13.991 \& 683.670 \& -2.534 <br>
\hline \& \& \& Max. My \& 2 \& -13.995 \& -1.950 \& 681.999 <br>
\hline \& \& \& Max. Vy \& 20 \& -16.339 \& 683.670 \& -2.534 <br>
\hline \& \& \& Max. Vx \& 2 \& -16.294 \& -1.950 \& 681.999 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.474 <br>
\hline \multirow[t]{5}{*}{L22} \& \multirow[t]{5}{*}{47-45.25} \& \multirow[t]{5}{*}{Pole} \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -37.471 \& 3.630 \& 1.351 <br>
\hline \& \& \& Max. Mx \& 20 \& -15.775 \& 766.989 \& -2.799 <br>
\hline \& \& \& Max. My \& 2 \& -15.779 \& -2.190 \& 765.072 <br>
\hline \& \& \& Max. Vy \& 20 \& -16.975 \& 766.989 \& -2.799 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Job 85565 | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 28 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date 15:01:04 09/21/18 |
|  | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Section No. \& $$
\begin{aligned}
& \text { Elevation } \\
& f l
\end{aligned}
$$ \& Component Type \& Condition \& Gov. Load Comb. \& Axial

$K$ \& Major Axis Moment kip-ft \& $$
\begin{gathered}
\text { Minor Axis } \\
\text { Moment } \\
\text { kip-ft } \\
\hline
\end{gathered}
$$ <br>

\hline \multirow{6}{*}{L23} \& \multirow{6}{*}{45.25-40.5} \& \multirow{5}{*}{Pole} \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-16.931} \& \multirow[t]{2}{*}{-2.190} \& \multirow[t]{2}{*}{765.072
-0.474} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -39.453 \& 3.814 \& 1.370 <br>
\hline \& \& \& Max. Mx \& 20 \& -16.917 \& 848.855 \& -3.052 <br>
\hline \& \& \multirow{8}{*}{Pole} \& Max. My \& 2 \& -16.921 \& -2.418 \& 846.703 <br>
\hline \multirow{7}{*}{L24} \& \multirow{7}{*}{40.5-40.25} \& \& Max. Vy \& 20 \& -17.505 \& 848.855 \& -3.052 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-17.461} \& \multirow[t]{2}{*}{-2.418} \& \multirow[t]{2}{*}{846.703
-0.474} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -39.557 \& 3.826 \& 1.372 <br>
\hline \& \& \& Max. Mx \& 20 \& -16.986 \& 853.235 \& -3.065 <br>
\hline \& \& \& Max. My \& 2 \& -16.989 \& -2.430 \& 851.070 <br>
\hline \multirow{7}{*}{L25} \& \multirow{7}{*}{40.25-35.25} \& \multirow{6}{*}{Pole} \& Max. Vy \& 20 \& -17.526 \& 853.235 \& -3.065 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-17.481} \& \multirow[t]{2}{*}{-2.430} \& 851.070 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& \multirow[t]{2}{*}{-0.474
0.000} <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& <br>
\hline \& \& \& Max. Compression \& 26 \& -41.650 \& 4.017 \& 1.391 <br>
\hline \& \& \& Max. Mx \& 20 \& -18.200 \& 942.250 \& -3.330 <br>
\hline \& \& \multirow{8}{*}{Pole} \& Max. My \& 2 \& -18.203 \& -2.669 \& 939.838 <br>
\hline \multirow{8}{*}{L26} \& \multirow{8}{*}{35.25-30.25} \& \& Max. Vy \& 20 \& -18.080 \& 942.250 \& -3.330 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-18.035} \& \multirow[t]{2}{*}{-2.669} \& \multirow[t]{2}{*}{939.838
-0.474} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -43.748 \& 4.209 \& 1.410 <br>
\hline \& \& \& Max. Mx \& 20 \& -19.441 \& 1033.963 \& -3.593 <br>
\hline \& \& \& Max. My \& 2 \& -19.443 \& -2.906 \& 1031.303 <br>
\hline \& \& \multirow{6}{*}{Pole} \& Max. Vy \& 20 \& -18.612 \& 1033.963 \& -3.593 <br>
\hline \multirow{6}{*}{L27} \& \multirow{6}{*}{30.25-27.75} \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-18.567} \& -2.906 \& 1031.303 <br>

\hline \& \& \& Max. Torque \& 16 \& \& \multirow[t]{2}{*}{$$
0.000
$$} \& \multirow[t]{2}{*}{\[

$$
\begin{gathered}
-0.474 \\
0.000
\end{gathered}
$$
\]} <br>

\hline \& \& \& Max Tension \& 1 \& $$
0.000
$$ \& \& <br>

\hline \& \& \& Max. Compression \& 26 \& -44.807 \& 4.299 \& 1.417 <br>
\hline \& \& \& Max. Mx \& 20 \& -20.069 \& 1080.812 \& -3.724 <br>
\hline \& \& \multirow{8}{*}{Pole} \& Max. My \& 2 \& -20.072 \& -3.024 \& 1078.028 <br>
\hline \multirow{8}{*}{L28} \& \multirow{8}{*}{27.75-27.5} \& \& Max. Vy \& 20 \& -18.876 \& 1080.812 \& -3.724 <br>

\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-18.831} \& -3.024 \& \multirow[t]{2}{*}{$$
\begin{gathered}
1078.028 \\
-0.473
\end{gathered}
$$} <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -44.917 \& 4.310 \& 1.418 <br>
\hline \& \& \& Max. Mx \& 20 \& -20.146 \& 1085.532 \& -3.738 <br>
\hline \& \& \& Max. My \& 2 \& -20.148 \& -3.036 \& 1082.736 <br>
\hline \& \& \multirow{6}{*}{Pole} \& Max. Vy \& 20 \& -18.892 \& 1085.532 \& -3.738 <br>
\hline \multirow{5}{*}{L29} \& \multirow{5}{*}{27.5-22.5} \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-18.847} \& \multirow[t]{2}{*}{-3.036} \& \multirow[t]{2}{*}{1082.736
-0.473} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max Compression \& 26 \& -47.100 \& 4.480 \& 1.429 <br>
\hline \& \& \& Max. Mx \& 20 \& -21.474 \& 1181.287 \& -3.999 <br>
\hline \multirow{9}{*}{L30} \& \multirow{9}{*}{22.5-19.5} \& \multirow{9}{*}{Pole} \& Max. My \& 2 \& -21.476 \& -3.270 \& 1178.244 <br>
\hline \& \& \& Max. Vy \& 20 \& -19.410 \& 1181.287 \& -3.999 <br>

\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-19.366} \& -3.270 \& \multirow[t]{2}{*}{$$
\begin{gathered}
1178.244 \\
-0.473
\end{gathered}
$$} <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -48.428 \& 4.560 \& 1.436 <br>
\hline \& \& \& Max. Mx \& 20 \& -22.287 \& 1239.947 \& -4.155 <br>
\hline \& \& \& Max. My \& 2 \& -22.289 \& -3.410 \& 1236.767 <br>
\hline \& \& \& Max. Vy \& 20 \& -19.704 \& 1239.947 \& -4.155 <br>

\hline \multirow{5}{*}{L31} \& \multirow{5}{*}{19.5-19.25} \& \multirow{5}{*}{Pole} \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-19.668} \& \multirow[t]{2}{*}{-3.410} \& $$
1236.767
$$ <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& -0.473 <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -48.544 \& 4.567 \& 1.437 <br>
\hline \& \& \& Max. Mx \& 20 \& -22.368 \& 1244.876 \& -4.168 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa OK 74119 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 29 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Section No. \& \[
\begin{aligned}
\& \text { Elevation } \\
\& f t
\end{aligned}
\] \& Component Type \& Condition \& \begin{tabular}{l}
Gov. Load \\
Comb.
\end{tabular} \& Axial

$K$ \& \[
$$
\begin{gathered}
\text { Major Axis } \\
\text { Moment } \\
\text { kip-ft } \\
\hline
\end{gathered}
$$

\] \& | Minor Axis |
| :--- |
| Moment |
| kip-ft | <br>

\hline \multirow{8}{*}{L32} \& \multirow{8}{*}{19.25-14.25} \& \multirow{7}{*}{Pole} \& Max. My \& 2 \& -22.369 \& -3.422 \& 1241.685 <br>
\hline \& \& \& Max. Vy \& 20 \& -19.720 \& 1244.876 \& -4.168 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-19.685} \& \multirow[t]{2}{*}{-3.422} \& \multirow[t]{2}{*}{1241.685
-0.473} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -50.914 \& 4.621 \& 1.462 <br>
\hline \& \& \& Max. Mx \& 20 \& -23.808 \& 1344.705 \& -4.427 <br>
\hline \& \& \multirow{9}{*}{Pole} \& Max. My \& 2 \& -23.809 \& -3.653 \& 1341.375 <br>
\hline \multirow{8}{*}{L33} \& \multirow{8}{*}{14.25-14} \& \& Max. Vy \& 20 \& -20.211 \& 1344.705 \& -4.427 <br>

\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.201} \& \multirow[t]{2}{*}{-3.653} \& \multirow[t]{2}{*}{$$
\begin{gathered}
1341.375 \\
-0.473
\end{gathered}
$$} <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -51.040 \& 4.619 \& 1.466 <br>
\hline \& \& \& Max. Mx \& 20 \& -23.888 \& 1349.760 \& -4.440 <br>
\hline \& \& \& Max. My \& 2 \& -23.889 \& -3.665 \& 1346.426 <br>
\hline \& \& \& Max. Vy \& 20 \& -20.227 \& 1349.760 \& -4.440 <br>
\hline \multirow{7}{*}{L34} \& \multirow{7}{*}{14-13.75} \& \multirow{5}{*}{Pole} \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.219} \& \multirow[t]{2}{*}{-3.665} \& \multirow[t]{2}{*}{1346.426
-0.473} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -51.170 \& 4.616 \& 1.470 <br>
\hline \& \& \& Max. Mx \& 20 \& -23.966 \& 1354.821 \& -4.453 <br>
\hline \& \& \multirow{9}{*}{Pole} \& Max. My \& 2 \& -23.967 \& -3.676 \& 1351.484 <br>
\hline \& \& \& Max. Vy \& 20 \& -20.252 \& 1354.821 \& -4.453 <br>

\hline \multirow{7}{*}{L35} \& \multirow{7}{*}{13.75-12.98} \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.245} \& \multirow[t]{2}{*}{-3.676} \& \multirow[t]{2}{*}{$$
\begin{gathered}
1351.484 \\
-0.473
\end{gathered}
$$} <br>

\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -51.579 \& 4.605 \& 1.480 <br>
\hline \& \& \& Max. Mx \& 20 \& -24.208 \& 1370.448 \& -4.493 <br>
\hline \& \& \& Max. My \& 2 \& -24.208 \& -3.711 \& 1367.103 <br>
\hline \& \& \& Max. Vy \& 20 \& -20.333 \& 1370.448 \& -4.493 <br>
\hline \multirow{5}{*}{L36} \& \multirow{5}{*}{12.98-12.73} \& \multirow{5}{*}{Pole} \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.330} \& \multirow[t]{2}{*}{-3.711} \& \multirow[t]{2}{*}{1367.103
-0.473} <br>
\hline \& \& \& \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -51.711 \& 4.603 \& 1.484 <br>
\hline \& \& \& Max. Mx \& 20 \& -24.293 \& 1375.534 \& -4.506 <br>
\hline \multirow{9}{*}{L37} \& \multirow{9}{*}{12.73-7.73} \& \multirow{10}{*}{Pole} \& Max. My \& 2 \& -24.293 \& -3.723 \& 1372.187 <br>
\hline \& \& \& Max. Vy \& 20 \& -20.352 \& 1375.534 \& -4.506 <br>
\hline \& \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.351} \& \multirow[t]{2}{*}{-3.723} \& \multirow[t]{2}{*}{1372.187
-0.473} <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -54.235 \& 4.681 \& 1.541 <br>
\hline \& \& \& Max. Mx \& 20 \& -25.886 \& 1478.549 \& -4.762 <br>
\hline \& \& \& Max. My \& 2 \& -25.887 \& -3.952 \& 1475.160 <br>
\hline \& \& \& Max. Vy \& 20 \& -20.853 \& 1478.549 \& -4.762 <br>

\hline \multirow{5}{*}{L38} \& \multirow{5}{*}{7.73-2.73} \& \& Max. Vx \& 2 \& \multirow[t]{2}{*}{-20.848} \& -3.952 \& \multirow[t]{2}{*}{$$
\begin{gathered}
1475.160 \\
-0.473
\end{gathered}
$$} <br>

\hline \& \& \multirow{3}{*}{Pole} \& Max. Torque \& 16 \& \& \& <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -56.635 \& 4.853 \& 1.585 <br>
\hline \& \& \multirow{12}{*}{Pole} \& Max. Mx \& 20 \& -27.505 \& 1584.021 \& -5.017 <br>
\hline \multirow{11}{*}{L39} \& \multirow{11}{*}{2.73-0} \& \& Max. My \& 2 \& -27.505 \& -4.178 \& 1580.521 <br>
\hline \& \& \& Max. Vy \& 20 \& -21.344 \& 1584.021 \& -5.017 <br>
\hline \& \& \& Max. Vx \& 14 \& \multirow[t]{2}{*}{21.326} \& \multirow[t]{2}{*}{7.098} \& -1575.225 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.473 <br>
\hline \& \& \& Max Tension \& 1 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& \& Max. Compression \& 26 \& -57.887 \& 4.939 \& 1.606 <br>
\hline \& \& \& Max. Mx \& 20 \& -28.396 \& 1642.642 \& -5.156 <br>
\hline \& \& \& Max. My \& 2 \& -28.396 \& -4.301 \& 1639.032 <br>

\hline \& \& \& Max. Vy \& 20 \& $$
-21.616
$$ \& 1642.642 \& -5.156 <br>

\hline \& \& \& Max. Vx \& 14 \& 21.614 \& 7.264 \& -1633.791 <br>
\hline \& \& \& Max. Torque \& 16 \& \& \& -0.473 <br>
\hline
\end{tabular}

| tnxTower <br> B+TGroup <br> 1717 S. Boulder, Suite 300 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 30 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

## Maximum Reactions

| Location | Condition | Gov. Load <br> Comb. | Vertical K | $\begin{gathered} \text { Horizontal, } X \\ K \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 36 | 57.887 | 4.686 | -0.010 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 20 | 28.409 | 21.599 | -0.053 |
|  | Max. $\mathrm{H}_{z}$ | 2 | 28.409 | -0.053 | 21.557 |
|  | Max. $\mathrm{M}_{\mathbf{x}}$ | 2 | 1639.032 | -0.053 | 21.557 |
|  | Max. $\mathrm{M}_{\mathbf{z}}$ | 8 | 1639.691 | -21.599 | 0.053 |
|  | Max. Torsion | 4 | 0.472 | -10.899 | 18.787 |
|  | Min. Vert | 7 | 21.307 | -18.667 | 10.786 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 28.409 | -21.599 | 0.053 |
|  | Min. $\mathrm{H}_{z}$ | 14 | 28.409 | 0.053 | -21.596 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -1633.791 | 0.053 | -21.596 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 20 | -1642.642 | 21.599 | -0.053 |
|  | Min Torsion | 16 | -0.473 | 10.899 | -18.787 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $x_{x}$ K | Shear ${ }_{z}$ K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-fi | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 23.675 | 0.000 | 0.000 | -0.505 | 1.191 | -0.000 |
| 1.2 Dead+1.0 Wind 0 deg - No | 28.409 | 0.053 | -21.557 | -1639.032 | -4.301 | -0.349 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 0 deg - No | 21.307 | 0.053 | -21.557 | -1623.326 | -4.625 | -0.327 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead +1.0 Wind 30 deg - No | 28.409 | 10.899 | -18.787 | -1423.209 | -824.841 | -0.472 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 30 deg - No | 21.307 | 10.899 | -18.787 | -1409.552 | -817.390 | -0.450 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 60 deg - No | 28.409 | 18.667 | -10.786 | -822.311 | -1418.804 | -0.468 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 60 deg - No | 21.307 | 18.667 | -10.786 | -814.337 | -1405.706 | -0.453 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind $90 \mathrm{deg}-$ No | 28.409 | 21.599 | -0.053 | $-6.409$ | -1639.691 | -0.340 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 90 deg - No | 21.307 | 21.599 | -0.053 | -6.180 | -1624.511 | -0.336 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 deg - | 28.409 | 18.678 | 10.732 | 813.305 | -1416.941 | -0.121 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 120 deg - | 21.307 | 18.678 | 10.732 | 805.754 | -1403.879 | -0.128 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 150 deg - | 28.409 | 10.836 | 18.784 | 1416.473 | -814.999 | 0.131 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 150 deg - | 21.307 | 10.836 | 18.784 | 1403.206 | -807.657 | 0.114 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 deg - | 28.409 | -0.053 | 21.596 | 1633.791 | 7.264 | 0.349 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 180 deg - | 21.307 | -0.053 | 21.596 | 1618.445 | 6.811 | 0.326 |
| No Ice |  |  |  |  |  |  |
| I.2 Dead+1.0 Wind 210 deg - | 28.409 | -10.899 | 18.787 | 1421.952 | 827.802 | 0.473 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 210 deg - | 21.307 | -10.899 | 18.787 | 1408.624 | 819.574 | 0.452 |
| No Ice |  |  |  |  |  |  |


| tnxTower <br> B+T Group <br> I717 S. Boulder, Suite 300 | Job85565.009 .01 - HARTFORD - NU (SSUSA),CT (BU\# 876363) |  | $\begin{aligned} & \text { Page } \\ & 31 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Load Combination | Vertical <br> K | Shear $_{x}$ <br> K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 Dead+1.0 Wind 240 deg - | 28.409 | -18.825 | 10.877 | 824.035 | 1426.924 | 0.470 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 240 deg - | 21.307 | -18.825 | 10.877 | 816.373 | 1413.022 | 0.455 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 270 deg - | 28.409 | -21.599 | 0.053 | 5.156 | 1642.642 | 0.341 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 270 deg - | 21.307 | -21.599 | 0.053 | 5.255 | 1626.689 | 0.336 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 300 deg - | 28.409 | -18.708 | -10.749 | -813.047 | 1417.287 | 0.120 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead +1.0 Wind 300 deg - | 21.307 | -18.708 | -10.749 | -805.184 | 1403.475 | 0.127 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead +1.0 Wind 330 deg - | 28.409 | -10.836 | -18.784 | -1417.720 | 817.959 | -0.133 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 330 deg - | 21.307 | -10.836 | -18.784 | -1404.127 | 809.841 | -0.116 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Yce+1.0 Temp | 57.887 | -0.000 | -0.000 | -1.606 | 4.939 | -0.000 |
| 1.2 Dead +1.0 Wind 0 deg+1.0 | 57.887 | 0.010 | -4.669 | -411.565 | 3.877 | -0.114 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0$ | 57.887 | 2.357 | -4.058 | -357.277 | -201.681 | -0.155 |
| Ice +1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 60 deg+1.0 | 57.887 | 4.063 | -2.343 | -207.570 | -351.788 | -0.155 |
| Ice +1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg +1.0 | 57.887 | 4.686 | -0.010 | -2.751 | -406.335 | -0.113 |
| Ice +1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 | 57.887 | 4.054 | 2.326 | 202.369 | -350.664 | -0.041 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 150 | 57.887 | 2.341 | 4.048 | 352.900 | -199.734 | 0.042 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 | 57.887 | -0.010 | 4.669 | 408.312 | 6.127 | 0.114 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 210 | 57.887 | $-2.357$ | 4.058 | 354.024 | 211.685 | 0.155 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 240 | 57.887 | -4.073 | 2.348 | 204.357 | 361.862 | 0.155 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead +1.0 Wind 270 | 57.887 | -4.686 | 0.010 | -0.502 | 416.336 | 0.113 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead +1.0 Wind 300 | 57.887 | -4.063 | -2.332 | -205.662 | 360.737 | 0.041 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead +1.0 Wind 330 | 57.887 | -2.341 | -4.048 | -356.152 | 209.737 | -0.042 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| Dead+Wind 0 deg - Service | 23.675 | 0.011 | -4.470 | -339.338 | 0.040 | -0.070 |
| Dead+Wind 30 deg - Service | 23.675 | 2.260 | -3.895 | -294.704 | -169.646 | -0.096 |
| Dead+Wind 60 deg - Service | 23.675 | 3.871 | -2.236 | -170.438 | -292.485 | -0.096 |
| Dead+Wind 90 deg - Service | 23.675 | 4.478 | -0.011 | -1.705 | -338.161 | -0.070 |
| Dead+Wind 120 deg - Service | 23.675 | 3.873 | 2.225 | 167.807 | -292.100 | -0.026 |
| Dead+Wind 150 deg - Service | 23.675 | 2.247 | 3.895 | 292.534 | -167.625 | 0.025 |
| Dead + Wind 180 deg - Service | 23.675 | -0.011 | 4.478 | 337.478 | 2.410 | 0.070 |
| Dead+Wind 210 deg - Service | 23.675 | -2.260 | 3.895 | 293.664 | 172.096 | 0.096 |
| Dead+Wind 240 deg - Service | 23.675 | -3.903 | 2.255 | 170.012 | 295.998 | 0.096 |
| Dead+Wind 270 deg - Service | 23.675 | -4.478 | 0.011 | 0.666 | 340.610 | 0.070 |
| Dead+Wind 300 deg - Service | 23.675 | -3.879 | -2.229 | -168.537 | 294.013 | 0.026 |
| Dead+Wind 330 deg - Service | 23.675 | -2.247 | -3.895 | -293.574 | 170.075 | -0.026 |


| tnxTower <br> B+T Group 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265 | Job $85565 .$ | ORD - NU (SSL | $\begin{aligned} & \text { Page } \\ & 32 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date $15: 01: 0409 / 21 / 18$ |
|  | Client | Crown Castle | Designed by xjones |


|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | $P Z$ | PX | PY | $P Z$ |  |
| Comb. | $K$ | K | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.000 | -23.675 | 0.000 | 0.000 | 23.675 | 0.000 | 0.000\% |
| 2 | 0.053 | -28.409 | -21.557 | -0.053 | 28.409 | 21.557 | 0.000\% |
| 3 | 0.053 | -21.307 | -21.557 | -0.053 | 21.307 | 21.557 | 0.000\% |
| 4 | 10.899 | -28.409 | -18.787 | -10.899 | 28.409 | 18.787 | 0.000\% |
| 5 | 10.899 | -21.307 | -18.787 | -10.899 | 21.307 | 18.787 | 0.000\% |
| 6 | 18.667 | -28.409 | -10.786 | -18.667 | 28.409 | 10.786 | 0.000\% |
| 7 | 18.667 | -21.307 | -10.786 | -18.667 | 21.307 | 10.786 | 0.000\% |
| 8 | 21.599 | -28.409 | -0.053 | -21.599 | 28.409 | 0.053 | 0.000\% |
| 9 | 21.599 | -21.307 | -0.053 | -21.599 | 21.307 | 0.053 | 0.000\% |
| 10 | 18.678 | -28.409 | 10.732 | -18.678 | 28.409 | -10.732 | 0.000\% |
| 11 | 18.678 | -21.307 | 10.732 | -18.678 | 21.307 | -10.732 | 0.000\% |
| 12 | 10.836 | -28.409 | 18.784 | -10.836 | 28.409 | -18.784 | 0.000\% |
| 13 | 10.836 | -21.307 | 18.784 | -10.836 | 21.307 | -18.784 | 0.000\% |
| 14 | -0.053 | -28.409 | 21.596 | 0.053 | 28.409 | -21.596 | 0.000\% |
| 15 | -0.053 | -21.307 | 21.596 | 0.053 | 21.307 | -21.596 | 0.000\% |
| 16 | -10.899 | -28.409 | 18.787 | 10.899 | 28.409 | -18.787 | 0.000\% |
| 17 | -10.899 | -21.307 | 18.787 | 10.899 | 21.307 | -18.787 | 0.000\% |
| 18 | -18.825 | -28.409 | 10.877 | 18.825 | 28.409 | -10.877 | 0.000\% |
| 19 | -18.825 | -21.307 | 10.877 | 18.825 | 21.307 | -10.877 | 0.000\% |
| 20 | -21.599 | -28.409 | 0.053 | 21.599 | 28.409 | -0.053 | 0.000\% |
| 21 | -21.599 | -21.307 | 0.053 | 21.599 | 21.307 | -0.053 | 0.000\% |
| 22 | -18.708 | -28.409 | -10.749 | 18.708 | 28.409 | 10.749 | 0.000\% |
| 23 | -18.708 | -21.307 | -10.749 | 18.708 | 21.307 | 10.749 | 0.000\% |
| 24 | -10.836 | -28.409 | -18.784 | 10.836 | 28.409 | 18.784 | 0.000\% |
| 25 | -10.836 | -21.307 | -18.784 | 10.836 | 21.307 | 18.784 | 0.000\% |
| 26 | 0.000 | -57.887 | 0.000 | 0.000 | 57.887 | 0.000 | 0.000\% |
| 27 | 0.010 | -57.887 | -4.669 | -0.010 | 57.887 | 4.669 | 0.000\% |
| 28 | 2.357 | -57.887 | -4.058 | -2.357 | 57.887 | 4.058 | 0.000\% |
| 29 | 4.063 | -57.887 | -2.343 | -4.063 | 57.887 | 2.343 | 0.000\% |
| 30 | 4.686 | -57.887 | -0.010 | -4.686 | 57.887 | 0.010 | 0.000\% |
| 31 | 4.054 | -57.887 | 2.326 | -4.054 | 57.887 | -2.326 | 0.000\% |
| 32 | 2.341 | -57.887 | 4.048 | -2.341 | 57.887 | -4.048 | 0.000\% |
| 33 | -0.010 | -57.887 | 4.669 | 0.010 | 57.887 | -4.669 | 0.000\% |
| 34 | -2.357 | -57.887 | 4.058 | 2.357 | 57.887 | -4.058 | 0.000\% |
| 35 | -4.073 | -57.887 | 2.348 | 4.073 | 57.887 | -2.348 | 0.000\% |
| 36 | -4.686 | -57.887 | 0.010 | 4.686 | 57.887 | -0.010 | 0.000\% |
| 37 | -4.063 | -57.887 | -2.332 | 4.063 | 57.887 | 2.332 | 0.000\% |
| 38 | -2.341 | -57.887 | -4.048 | 2.341 | 57.887 | 4.048 | 0.000\% |
| 39 | 0.011 | -23.675 | -4.470 | -0.011 | 23.675 | 4.470 | 0.000\% |
| 40 | 2.260 | -23.675 | -3.895 | -2.260 | 23.675 | 3.895 | 0.000\% |
| 41 | 3.871 | -23.675 | -2.236 | -3.871 | 23.675 | 2.236 | 0.000\% |
| 42 | 4.478 | -23.675 | -0.011 | -4.478 | 23.675 | 0.011 | 0.000\% |
| 43 | 3.873 | -23.675 | 2.225 | -3.873 | 23.675 | -2.225 | 0.000\% |
| 44 | 2.247 | -23.675 | 3.895 | -2.247 | 23.675 | -3.895 | 0.000\% |
| 45 | -0.011 | -23.675 | 4.478 | 0.011 | 23.675 | -4.478 | 0.000\% |
| 46 | -2.260 | -23.675 | 3.895 | 2.260 | 23.675 | -3.895 | 0.000\% |
| 47 | -3.903 | -23.675 | 2.255 | 3.903 | 23.675 | -2.255 | 0.000\% |
| 48 | -4.478 | -23.675 | 0.011 | 4.478 | 23.675 | -0.011 | 0.000\% |
| 49 | -3.879 | -23.675 | -2.229 | 3.879 | 23.675 | 2.229 | 0.000\% |
| 50 | -2.247 | -23.675 | -3.895 | 2.247 | 23.675 | 3.895 | 0.000\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |


| thxTower | Job 85565 | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 33 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| B+TGroup <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| 2 |  |  | 0.00000001 | 0.00012702 |
| :--- | :--- | :--- | :--- | :--- |
| 3 | Yes | 5 | 0.00000001 | 0.00004883 |
| 4 | Yes | 5 | 0.00000001 | 0.00031467 |
| 5 | Yes | 6 | 0.0000001 | 0.0009576 |
| 6 | Yes | 6 | 0.00000001 | 0.00032480 |
| 7 | Yes | 6 | 0.00000001 | 0.00009926 |
| 8 | Yes | 6 | 0.00000001 | 0.00023716 |
| 9 | Yes | 5 | 0.00000001 | 0.00010321 |
| 10 | Yes | 5 | 0.00000001 | 0.0031371 |
| 11 | Yes | 6 | 0.0000001 | 0.0009602 |
| 12 | Yes | 6 | 0.0000001 | 0.00031323 |
| 13 | Yes | 6 | 0.00000001 | 0.00009594 |
| 14 | Yes | 6 | 0.00000001 | 0.00026238 |
| 15 | Yes | 5 | 0.00000001 | 0.00010962 |
| 16 | Yes | 5 | 0.00000001 | 0.00032673 |
| 17 | Yes | 6 | 0.00000001 | 0.00009964 |
| 18 | Yes | 6 | 0.00000001 | 0.00031562 |
| 19 | Yes | 6 | 0.00000001 | 0.00009591 |
| 20 | Yes | 6 | 0.00000001 | 0.00010467 |
| 21 | Yes | Yes | 5 | 0.00000001 |
| 22 | 5 | 0.00004298 |  |  |
| 23 | Yes | Yes | 5 | 0.0000001 |

Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{aligned} & \hline \text { Job } \\ & 85565 \end{aligned}$ | ORD - NU (SSL | $\begin{aligned} & \text { Page } \\ & \\ & 34 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation <br> $f t$ | Horz. Deflection in | Gov. Load Comb. | Till | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L6 | 88-83 | 9.217 | 47 | 1.108 | 0.001 |
| L7 | 83-82.33 | 8.118 | 47 | 0.989 | 0.001 |
| L8 | 82.33-82.08 | 7.980 | 47 | 0.972 | 0.001 |
| L9 | 82.08-77.08 | 7.929 | 47 | 0.968 | 0.001 |
| L10 | 77.08-76.25 | 6.959 | 47 | 0.884 | 0.001 |
| L11 | 76.25-76 | 6.806 | 47 | 0.869 | 0.001 |
| L12 | 76-74.5 | 6.761 | 47 | 0.865 | 0.001 |
| L13 | 74.5-74.25 | 6.492 | 47 | 0.846 | 0.001 |
| L14 | 74.25-69.25 | 6.448 | 47 | 0.843 | 0.001 |
| L15 | 69.25-64.25 | 5.595 | 47 | 0.786 | 0.001 |
| L16 | 64.25-59.25 | 4.804 | 47 | 0.724 | 0.000 |
| L17 | 59.25-58.08 | 4.081 | 47 | 0.657 | 0.000 |
| L18 | 58.08-57.73 | 3.922 | 47 | 0.641 | 0.000 |
| L19 | 57.73-57.5 | 3.875 | 47 | 0.638 | 0.000 |
| L20 | 57.5-52.5 | 3.844 | 47 | 0.635 | 0.000 |
| L2I | 52.5-47 | 3.208 | 47 | 0.579 | 0.000 |
| L22 | 50.25-45.25 | 2.941 | 47 | 0.554 | 0.000 |
| L23 | 45.25-40.5 | 2.378 | 47 | 0.516 | 0.000 |
| L24 | 40.5-40.25 | 1.891 | 47 | 0.461 | 0.000 |
| L25 | 40.25-35.25 | 1.867 | 47 | 0.458 | 0.000 |
| L26 | 35.25-30.25 | 1.419 | 47 | 0.398 | 0.000 |
| L27 | 30.25-27.75 | 1.034 | 47 | 0.337 | 0.000 |
| L28 | 27.75-27.5 | 0.865 | 47 | 0.306 | 0.000 |
| L29 | 27.5-22.5 | 0.849 | 47 | 0.303 | 0.000 |
| L30 | 22.5-19.5 | 0.563 | 47 | 0.243 | 0.000 |
| L31 | 19.5-19.25 | 0.422 | 47 | 0.207 | 0.000 |
| L32 | 19.25-14.25 | 0.411 | 47 | 0.204 | 0.000 |
| L33 | 14.25-14 | 0.225 | 47 | 0.150 | 0.000 |
| L.34 | 14-13.75 | 0.217 | 47 | 0.148 | 0.000 |
| L35 | 13.75-12.98 | 0.210 | 47 | 0.145 | 0.000 |
| L36 | 12.98-12.73 | 0.187 | 47 | 0.137 | 0.000 |
| L37 | 12.73-7.73 | 0.180 | 47 | 0.135 | 0.000 |
| L38 | 7.73-2.73 | 0.066 | 47 | 0.082 | 0.000 |
| L39 | 2.73-0 | 0.008 | 47 | 0.029 | 0.000 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist <br>  | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.000 | BXA-70063/6CF w/ Mount Pipe | 47 | 13.698 | 1.409 | 0.004 | 4118 |
| 98.000 | APXV9ERR18-C-A20 w/ Mount Pipe | 47 | 11.726 | 1.266 | 0.002 | 3111 |
| 96.000 | PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ | 47 | 11.200 | 1.249 | 0.002 | 3801 |
| 81.000 | HBX-6516DS-VTM w/ Mount Pipe | 47 | 7.712 | 0.952 | 0.001 | 3021 |
| 74.000 | KS24019-L112A | 47 | 6.404 | 0.840 | 0.001 | 4519 |

## Maximum Tower Deflections - Design Wind

| Section | Elevation | Horz. | Gov. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Deflection | Load |  | 0 |  |
|  | in |  | Comb. | $\circ$ | 0 |


| tnxTower <br> B+TGroup <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 . \end{array}$ | ORD - NU (SSL | $\begin{aligned} & \text { Page } \\ & 35 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \\ \hline \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation $\qquad$ | Horz. Deflection in | Gov. Load Comb. | Till | Twist <br>  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 108-103 | 70.019 | 18 | 6.669 | 0.018 |
| L2 | 103-98.5 | 63.072 | 18 | 6.610 | 0.015 |
| L3 | 98.5-98 | 57.066 | 18 | 6.091 | 0.009 |
| LA | 98-93 | 56.431 | 18 | 6.079 | 0.009 |
| L5 | 93-88 | 50.225 | 18 | 5.783 | 0.007 |
| L6 | 88-83 | 44.409 | 18 | 5.333 | 0.006 |
| L7 | 83-82.33 | 39.125 | 18 | 4.765 | 0.004 |
| L8 | 82.33-82.08 | 38.464 | 18 | 4.682 | 0.004 |
| L9 | 82.08-77.08 | 38.220 | 18 | 4.664 | 0.004 |
| L10 | 77.08-76.25 | 33.552 | 18 | 4.259 | 0.004 |
| L11 | 76.25-76 | 32.819 | 18 | 4.188 | 0.003 |
| L12 | 76-74.5 | 32.600 | 18 | 4.172 | 0.003 |
| L13 | 74.5-74.25 | 31.306 | 18 | 4.077 | 0.003 |
| L14 | 74.25-69.25 | 31.093 | 18 | 4.065 | 0.003 |
| L15 | 69.25-64.25 | 26.983 | 18 | 3.792 | 0.003 |
| L16 | 64.25-59.25 | 23.173 | 18 | 3.490 | 0.002 |
| L17 | 59.25-58.08 | 19.688 | 18 | 3.171 | 0.002 |
| L18 | 58.08-57.73 | 18.921 | 18 | 3.094 | 0.002 |
| L19 | 57.73-57.5 | 18.695 | 18 | 3.076 | 0.002 |
| L20 | 57.5-52.5 | 18.547 | 18 | 3.065 | 0.002 |
| L21 | 52.5-47 | 15.480 | 18 | 2.796 | 0.002 |
| L22 | 50.25-45.25 | 14.192 | 18 | 2.673 | 0.001 |
| L23 | 45.25-40.5 | 11.474 | 18 | 2.491 | 0.001 |
| L24 | 40.5-40.25 | 9.129 | 18 | 2.226 | 0.001 |
| L25 | 40.25-35.25 | 9.013 | 18 | 2.212 | 0.001 |
| L26 | 35.25-30.25 | 6.849 | 18 | 1.923 | 0.001 |
| L27 | 30.25-27.75 | 4.990 | 18 | 1.628 | 0.001 |
| L28 | 27.75-27.5 | 4.177 | 18 | 1.478 | 0.001 |
| L29 | 27.5-22.5 | 4.100 | 18 | 1.464 | 0.001 |
| L30 | 22.5-19.5 | 2.718 | 18 | 1.175 | 0.001 |
| L31 | 19.5-19.25 | 2.035 | 18 | 1.000 | 0.000 |
| L32 | 19.25-14.25 | 1.983 | 18 | 0.987 | 0.000 |
| L33 | 14.25-14 | 1.086 | 18 | 0.726 | 0.000 |
| L34 | 14-13.75 | 1.049 | 18 | 0.713 | 0.000 |
| L35 | 13.75-12.98 | 1.012 | 18 | 0.700 | 0.000 |
| L36 | 12.98-12.73 | 0.902 | 18 | 0.662 | 0.000 |
| L37 | 12.73-7.73 | 0.867 | 18 | 0.649 | 0.000 |
| L38 | 7.73-2.73 | 0.320 | 18 | 0.395 | 0.000 |
| L39 | 2.73-0 | 0.040 | 18 | 0.140 | 0.000 |

## Critical Deflections and Radius of Curvature - Design Wind

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Elevation \& Appurtenance \& Gov. Load Comb. \& Deflection in \& Tilt

$\circ$ \& | Twist |
| :---: | \& Radius of Curvature $f t$ <br>

\hline 105.000 \& BXA-70063/6CF w/ Mount Pipe \& 18 \& 65.836 \& 6.715 \& 0.017 \& 991 <br>
\hline 98.000 \& APXV9ERR18-C-A20 w/ Mount Pipe \& 18 \& 56.431 \& 6.079 \& 0.009 \& 701 <br>
\hline 96.000 \& PCS $1900 \mathrm{MHz} 4 \times 45 \mathrm{~W}-65 \mathrm{MHz}$ \& 18 \& 53.915 \& 5.998 \& 0.008 \& 840 <br>
\hline 81.000 \& HBX-6516DS-VTM w/ Mount Pipe \& 18 \& 37.176 \& 4.587 \& 0.004 \& 641 <br>
\hline 74.000 \& KS24019-L112A \& 18 \& 30.881 \& 4.052 \& 0.003 \& 953 <br>
\hline
\end{tabular}

| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | Page <br>  <br> 36 of 42 |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |

Pole Design Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Section No. \& Elevation \& Size \& \(L\) \& \(L_{u}\) \& Kl/r \& A \& \(P_{u}\) \& \(\phi P_{n}\) \& Ratio \(P_{u}\) \\
\hline \& \(f t\) \& \& \(f t\) \& \(f t\) \& \& \(i n^{2}\) \& \(K\) \& K \& \(\phi P_{n}\) \\
\hline LI \& 108-103 (1) \& TP8.625x8.625x0.313 \& 5.000 \& 0.000 \& 0.0 \& 8.161 \& -2.394 \& 257.065 \& 0.009 \\
\hline L2 \& 103-98.5 (2) \& TP8.625x8.625x0.313 \& 4.500 \& 0.000 \& 0.0 \& 8.161 \& -2.607 \& 257.065 \& 0.010 \\
\hline L3 \& 98.5-98 (3) \& TP16.5×16.5x0.313 \& 0.500 \& 0.000 \& 0.0 \& 15.892 \& -2.652 \& 500.599 \& 0.005 \\
\hline L4 \& 98-93 (4) \& TP17.3x16.5×0.188 \& 5.000 \& 0.000 \& 0.0 \& 10.184 \& -6.781 \& 756.639 \& 0.009 \\
\hline L5 \& 93-88 (5) \& TP18.101x17.3x0.188 \& 5.000 \& 0.000 \& 0.0 \& 10.660 \& -7.110 \& 791.081 \& 0.009 \\
\hline L6 \& 88-83 (6) \& TP18.901x18.101×0.188 \& 5.000 \& 0.000 \& 0.0 \& 11.137 \& -7.477 \& 817.568 \& 0.009 \\
\hline L7 \& 83-82.33 (7) \& TP19.008×18.901×0.188 \& 0.670 \& 0.000 \& 0.0 \& 11.201 \& -7.531 \& 821.060 \& 0.009 \\
\hline L8 \& \begin{tabular}{l}
\[
82.33-82.08
\] \\
(8)
\end{tabular} \& TP19.048×19.008x0.325 \& 0.250 \& 0.000 \& 0.0 \& 19.314 \& -7.562 \& 1434.920 \& 0.005 \\
\hline L9 \& \begin{tabular}{l}
\[
82.08-77.08
\] \\
(9)
\end{tabular} \& TP19.848×19.048x0.319 \& 5.000 \& 0.000 \& 0.0 \& 19.758 \& -9.100 \& 1467.950 \& 0.006 \\
\hline L10 \& \begin{tabular}{l}
\[
77.08-76.25
\] \\
(10)
\end{tabular} \& TP19.981×19.848x0.319 \& 0.830 \& 0.000
0.000 \& 0.0 \& 19.893
28.333 \& -9.192
-9.237 \& 1477.940
2104.990 \& 0.006
0.004 \\
\hline L11 \& \(76.25-76(11)\) \& TP20.021×19.981×0.456 \& 0.250 \& 0.000 \& 0.0 \& 28.333 \& -9.237 \& 2104.990 \& 0.004 \\
\hline L12 \& 76-74.5 (12) \& TP20.261x20.021x0.45 \& 1.500 \& 0.000 \& 0.0 \& 28.297 \& -9.457 \& 2102.300 \& 0.004 \\
\hline L13 \& \[
\begin{gathered}
74.5-74.25 \\
(13)
\end{gathered}
\] \& TP20.301×20.261×0.588 \& 0.250 \& 0.000 \& 0.0 \& 36.761 \& -9.508 \& 2731.160 \& 0.003 \\
\hline L14 \& \[
\begin{gathered}
74.25-69.25 \\
(14)
\end{gathered}
\] \& TP21.102x20.301x0.575 \& 5.000 \& 0.000 \& 0.0 \& 37.462 \& -10.402 \& 2783.260 \& 0.004 \\
\hline L15 \& \[
\begin{gathered}
69.25-64.25 \\
(15)
\end{gathered}
\] \& TP21.902×21.102x0.55 \& 5.000 \& 0.000 \& 0.0 \& 37.274 \& -11.245 \& 2769.280 \& 0.004 \\
\hline L16 \& \begin{tabular}{l}
\[
64.25-59.25
\] \\
(16)
\end{tabular} \& TP22.702×21.902x0.544 \& 5.000 \& 0.000 \& 0.0 \& 38.243 \& -12.108 \& 2841.230 \& 0.004 \\
\hline L17 \& \begin{tabular}{l}
59.25-58.08 \\
(17)
\end{tabular} \& TP22.89x22.702x0.538 \& 1.170 \& 0.000 \& 0.0 \& 38.133
50.279 \& -12.313
-12395 \& 2833.100
3735.520 \& 0.004
0.003 \\
\hline L18 \& \begin{tabular}{l}
\[
58.08-57.73
\] \\
(18)
\end{tabular} \& TP22.946x22.89x0.713 \& 0.350 \& 0.000 \& 0.0 \& 50.279 \& -12.395 \& 3735.520
3741.700 \& 0.003
0.003 \\
\hline L19 \& \begin{tabular}{l}
\[
57.73-57.5
\] \\
(19)
\end{tabular} \& TP22.982×22.946x0.713 \& 0.230 \& 0.000 \& 0.0 \& 50.363 \& -12.445 \& 3741.700 \& 0.003 \\
\hline L20 \& 57.5-52.5 (20) \& TP23.783x22.982x0.688 \& 5.000 \& 0.000 \& 0.0 \& 50.397 \& -13.502 \& 3744.210 \& 0.004 \\
\hline L21 \& 52.5-47 (21) \& TP24.663×23.783x0.688 \& 5.500 \& 0.000 \& 0.0 \& 51.182 \& -13.987 \& 3802.600 \& 0.004 \\
\hline L22 \& 47-45.25 (22) \& TP24.568x23.768x0.75 \& 5.000 \& 0.000 \& 0.0 \& 56.699 \& -15.772 \& 4212.440 \& 0.004 \\
\hline L23 \& \[
\begin{gathered}
45.25-40.5 \\
(23)
\end{gathered}
\] \& TP25.328x24.568x0.725 \& 4.750 \& 0.000 \& 0.0 \& 56.616 \& -16.914 \& 4206.270 \& 0.004 \\
\hline L24 \& \begin{tabular}{l}
\[
40.5-40.25
\] \\
(24)
\end{tabular} \& TP25.368x25.328x0.725 \& 0.250 \& 0.000 \& 0.0 \& 56.708
56.586 \& -16.983

18.197 \& 4213.110 \& 0.004 <br>

\hline L25 \& $$
\begin{gathered}
40.25-35.25 \\
(25)
\end{gathered}
$$ \& TP26.168x25.368x0.7 \& 5.000 \& 0.000 \& 0.0 \& 56.586 \& -18.197 \& 4204.040 \& 0.004 <br>

\hline L26 \& $$
\begin{gathered}
35.25-30.25 \\
(26)
\end{gathered}
$$ \& TP26.969x26.168x0.688 \& 5.000 \& 0.000 \& 0.0 \& 57.349 \& -19.438 \& 4260.730 \& 0.005 <br>

\hline L27 \& $$
\begin{gathered}
30.25-27.75 \\
(27)
\end{gathered}
$$ \& TP27.369x26.969x0.675 \& 2.500 \& 0.000

0.000 \& 0.0 \& 57.190
61.403 \& $\begin{array}{r}-20.067 \\ \\ \hline\end{array}$ \& 4248.940
4561.970 \& 0.005
0.004 <br>

\hline L28 \& $$
\begin{gathered}
27.75-27.5 \\
(28)
\end{gathered}
$$ \& TP27.409x27.369x0.725 \& 0.250 \& 0.000 \& 0.0 \& 61.403 \& -20.144 \& 4561.970 \& 0.004 <br>

\hline L29 \& 27.5-22.5 (29) \& TP28.209x27.409x0.7 \& 5.000 \& 0.000 \& 0.0 \& 61.119 \& -21.472 \& 4540.880 \& 0.005 <br>
\hline L30 \& 22.5-19.5 (30) \& TP28.689x28.209×0.688 \& 3.000 \& 0.000 \& 0.0 \& 61.103 \& -22.286 \& 4539.660 \& 0.005 <br>

\hline L31 \& $$
\begin{gathered}
19.5-19.25 \\
(31)
\end{gathered}
$$ \& TP28.729x28.689x0.8 \& 0.250

5 \& 0.000
0.000 \& 0.0 \& 70.918
70.731 \& -22.366
-23.806 \& 5268.830
5254.990 \& 0.004
0.005 <br>

\hline L32 \& $$
\begin{gathered}
19.25-14.25 \\
(32)
\end{gathered}
$$ \& TP29.529x28.729x0.775 \& 5.000 \& 0.000 \& 0.0 \& 70.731 \& -23.806 \& 5254.990 \& 0.005 <br>

\hline L33 \& 14.25-14 (33) \& TP29.569 $29.529 \times 0.775$ \& 0.250 \& 0.000 \& 0.0 \& 70.830 \& -23.886 \& 5262.310 \& 0.005 <br>
\hline L34 \& 14-13.75 (34) \& TP29.609x29.569x0.775 \& 0.250 \& 0.000 \& 0.0 \& 70.928 \& -23.964 \& 5269.620 \& 0.005 <br>

\hline L35 \& $$
\begin{gathered}
13.75-12.98 \\
(35)
\end{gathered}
$$ \& TP29.733×29.609×0.8 \& 0.770 \& 0.000 \& 0.0 \& 73.466 \& -24.206 \& 5458.140 \& 0.004 <br>

\hline L36 \& 12.98-12.73 \& TP29.773x29.733x0.8 \& 0.250 \& 0.000 \& 0.0 \& 73.567 \& -24.291 \& 5465.690 \& 0.004 <br>
\hline
\end{tabular}



| Section No. | Elevation <br> ft | Size | $\bar{L}$ | $\begin{aligned} & \overline{L_{u}} \\ & f t \end{aligned}$ | Kl/r | A $i n^{2}$ | $\begin{gathered} \hline P_{u} \\ K \end{gathered}$ | $\begin{gathered} \phi P_{n} \\ K \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L37 | $\begin{gathered} (36) \\ 12.73-7.73 \\ (37)) \end{gathered}$ | TP30.573x29.773x0.788 | 5.000 | 0.000 | 0.0 | 74.449 | -25.885 | 5531.210 | 0.005 |
| L38 | 7.73-2.73 (38) | TP31.373x30.573x0.775 | 5.000 | 0.000 | 0.0 | 75.267 | -27.504 | 5591.940 | 0.005 |
| L39 | 2.73-0(39) | TP31.81×31.373x0.763 | 2.730 | 0.000 | 0.0 | 75.140 | -28.396 | 5582.560 | 0.005 |

## Pole Bending Design Data

| Section No. | Elevation <br> $f t$ | Size | $\begin{gathered} M_{u x} \\ k i p \cdot f t \end{gathered}$ | $\phi M_{n x}$ kip-ft | $\begin{gathered} \hline \text { Ratio } \\ M_{\mu x} \\ \hline \phi M \end{gathered}$ | $M_{x y}$ $k i p-f t$ | $\phi M_{n y}$ kip-ft | $\begin{gathered} \text { Ratio } \\ M_{x y} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | fir |  | $k i p \sim f t$ | kip fft | $\phi M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| L1 | 108-103 (1) | TP8.625x8.625x0.313 | 13.847 | 56.708 | 0.244 | 0.000 | 56.708 | 0.000 |
| L2 | 103-98.5 (2) | TP8.625x8.625x0.313 | 43.528 | 56.708 | 0.768 | 0.000 | 56.708 | 0.000 |
| L3 | 98.5-98 (3) | TP16.5x16.5x0.313 | 46.863 | 214.977 | 0.218 | 0.000 | 214.977 | 0.000 |
| L4 | 98-93 (4) | TP17.3x16.5x0.188 | 100.418 | 265.442 | 0.378 | 0.000 | 265.442 | 0.000 |
| $L 5$ | 93-88 (5) | TP18.101x17.3x0.188 | 156.343 | 290.644 | 0.538 | 0.000 | 290.644 | 0.000 |
| L6 | 88-83 (6) | TP18.901x18.101x0.188 | 213.434 | 313.934 | 0.680 | 0.000 | 313.934 | 0.000 |
| L7 | 83-82.33 (7) | TP19.008×18.901×0.188 | 221.180 | 317.100 | 0.698 | 0.000 | 317.100 | 0.000 |
| L8 | $82.33-82.08$ <br> (8) | TP19.048x19.008x0.325 | 224.081 | 547.300 | 0.409 | 0.000 | 547.300 | 0.000 |
| L9 | $\begin{gathered} 82.08-77.08 \\ (9) \end{gathered}$ | TP19.848x19.048×0.319 | 287.498 | 584.613 | 0.492 | 0.000 | 584.613 | 0.000 |
| L10 | $\begin{gathered} 77.08-76.25 \\ (10) \end{gathered}$ | TP19.981x19.848x0.319 | 298.567 | 592.658 | 0.504 | 0.000 | 592.658 | 0.000 |
| L11 | 76.25-76(11) | TP20.021×19.981x0.456 | 301.915 | 834.092 | 0.362 | 0.000 | 834.092 | 0.000 |
| L12 | 76-74.5 (12) | TP20.261×20.021x0.45 | 322.143 | 844.008 | 0.382 | 0.000 | 844.008 | 0.000 |
| L13 | $\begin{gathered} 74.5-74.25 \\ (13) \end{gathered}$ | TP20.301x20.261x0.588 | 325.539 | 1083.575 | 0.300 | 0.000 | 1083.575 | 0.000 |
| L14 | $\begin{gathered} 74.25-69.25 \\ (14) \end{gathered}$ | TP21.102x20.301×0.575 | 395.187 | 1151.775 | 0.343 | 0.000 | 1151.775 | 0.000 |
| L15 | $\begin{gathered} 69.25-64.25 \\ (15) \end{gathered}$ | TP21.902x21.102x0.55 | 467.702 | 1194.683 | 0.391 | 0.000 | 1194.683 | 0.000 |
| L16 | $\begin{gathered} 64.25-59.25 \\ (16) \end{gathered}$ | TP22.702x21.902x0.544 | 542.967 | 1273.533 | 0.426 | 0.000 | 1273.533 | 0.000 |
| L17 | $\begin{gathered} 59.25-58.08 \\ (17) \end{gathered}$ | TP22.89x22.702x0.538 | 560.979 | 1281.600 | 0.438 | 0.000 | 1281.600 | 0.000 |
| L18 | $58.08-57.73$ <br> (18) | TP22.946x22.89x0.713 | 566.398 | 1667.800 | 0.340 | 0.000 | 1667.800 | 0.000 |
| L19 | $57.73-57.5$ <br> (19) | TP22.982x22.946x0.713 | 569.967 | 1673.408 | 0.341 | 0.000 | 1673.408 | 0.000 |
| L20 | 57.5-52.5 (20) | TP23.783x22.982x0.688 | 649.071 | 1740.342 | 0.373 | 0.000 | 1740.342 | 0.000 |
| L21 | 52.5-47 (21) | TP24.663x23.783x0.688 | 685.618 | 1795.842 | 0.382 | 0.000 | 1795.842 | 0.000 |
| L22 | 47-45.25 (22) | TP24.568×23.768×0.75 | 769.112 | 2015.892 | 0.382 | 0.000 | 2015.892 | 0.000 |
| L23 | $\begin{gathered} 45.25-40.5 \\ (23) \end{gathered}$ | TP25.328x24.568x0.725 | 851.142 | 2083.383 | 0.409 | 0.000 | 2083.383 | 0.000 |
| L24 | $40.5-40.25$ <br> (24) | TP25.368x25.328×0.725 | 855.533 | 2090.258 | 0.409 | 0.000 | 2090.258 | 0.000 |
| L25 | $\begin{gathered} 40.25-35.25 \\ (25) \end{gathered}$ | TP26.168×25.368x0.7 | 944.725 | 2159.667 | 0.437 | 0.000 | 2159.667 | 0.000 |
| L26 | $\begin{gathered} 35.25-30.25 \\ (26) \end{gathered}$ | TP26.969x26.168x0.688 | 1036.608 | 2261.550 | 0.458 | 0.000 | 2261.550 | 0.000 |
| L27 | $\begin{gathered} 30.25-27.75 \\ (27) \end{gathered}$ | TP27.369x26.969x0.675 | 1083.542 | 2292.650 | 0.473 | 0.000 | 2292.650 | 0.000 |
| L28 | $\begin{gathered} 27.75-27.5 \\ (28) \end{gathered}$ | TP27.409x27.369x0.725 | 1088.267 | 2456.125 | 0.443 | 0.000 | 2456.125 | 0.000 |
| L29 | 27.5-22.5 (29) | TP28.209x27.409x0.7 | 1184.200 | 2524.608 | 0.469 | 0.000 | 2524.608 | 0.000 |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{aligned} & \text { Job } \\ & \text { 85565.009.01 - HARTFORD - NU (SSUSA), CT (BU\# } 876363 \text { ) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 38 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
|  | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{\pi x}$ | $\begin{gathered} \text { Ratio } \\ M_{n x} \\ \hline \end{gathered}$ | $M_{u y}$ | $\phi M_{n y}$ | $\begin{gathered} \text { Ratio } \\ M_{x y y} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | $k i p-f t$ | kip-ft | $\phi M_{n x}$ | $k i p-f t$ | $k i p-f t$ | $\phi M_{n j}$ |
| L30 | 22.5-19.5 (30) | TP28.689×28.209×0.688 | 1242.967 | 2571.375 | 0.483 | 0.000 | 2571.375 | 0.000 |
| L31 | $\begin{gathered} 19.5-19.25 \\ \text { (31) } \end{gathered}$ | TP28.729×28.689x0.8 | 1247.908 | 2964.833 | 0.421 | 0.000 | 2964.833 | 0.000 |
| L32 | $\begin{gathered} 19.25-14.25 \\ (32) \end{gathered}$ | TP29.529x28.729x0.775 | 1348.050 | 3049.425 | 0.442 | 0.000 | 3049.425 | 0.000 |
| L33 | 14.25-14 (33) | TP29.569×29.529x0.775 | 1353.125 | 3058.033 | 0.442 | 0.000 | 3058.033 | 0.000 |
| L34 | 14-13.75 (34) | TP29.609x29.569x0.775 | 1358.208 | 3066.650 | 0.443 | 0.000 | 3066.650 | 0.000 |
| L35 | $\begin{gathered} 13.75-12.98 \\ (35) \end{gathered}$ | TP29.733x29.609x0.8 | 1373.908 | 3184.783 | 0.431 | 0.000 | 3184.783 | 0.000 |
| L36 | $\begin{gathered} 12.98-12.73 \\ (36) \end{gathered}$ | TP29.773x29.733x0.8 | 1379.017 | 3193.717 | 0.432 | 0.000 | 3193.717 | 0.000 |
| L37 | $\begin{gathered} 12.73-7.73 \\ (37) \end{gathered}$ | TP30.573x29.773x0.788 | 1482.608 | 3326.458 | 0.446 | 0.000 | 3326.458 | 0.000 |
| L38 | 7.73-2.73 (38) | TP31.373x30.573x0.775 | 1588.767 | 3458.483 | 0.459 | 0.000 | 3458.483 | 0.000 |
| L39 | 2.73-0(39) | TP31.81×31.373x0.763 | 1647.767 | 3506.025 | 0.470 | 0.000 | 3506.025 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Actual } \\ T_{u} \end{gathered}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $K$ | $K$ | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | 108-103 (1) | TP8.625x8.625x0.313 | 6.512 | 77.119 | 0.084 | 0.034 | 56.361 | 0.001 |
| L2 | 103-98.5 (2) | TP8.625x8.625x0.313 | 6.659 | 77.119 | 0.086 | 0.206 | 56.361 | 0.004 |
| L3 | 98.5-98 (3) | TP16.5x16.5x0.313 | 6.680 | 150.180 | 0.044 | 0.206 | 213.732 | 0.001 |
| L4 | 98-93(4) | TP17.3x16.5x0.188 | 11.067 | 178.734 | 0.062 | 0.294 | 262.022 | 0.001 |
| L5 | 93-88 (5) | TP18.101x17.3x0.188 | 11.307 | 187.092 | 0.060 | 0.293 | 287.387 | 0.001 |
| L6 | 88-83 (6) | TP18.901x18.101×0.188 | 11.537 | 195.451 | 0.059 | 0.293 | 313.923 | 0.001 |
| L7 | 83-82.33 (7) | TP19.008×18.901×0.188 | 11.593 | 196.571 | 0.059 | 0.293 | 317.568 | 0.001 |
| L8 | $82.33-82.08$ <br> (8) | TP19.048×19.008×0.325 | 11.614 | 338.958 | 0.034 | 0.293 | 536.655 | 0.001 |
| L9 | $82.08-77.08$ <br> (9) | TP19.848x19.048x0.319 | 13.297 | 346.760 | 0.038 | 0.293 | 573.867 | 0.001 |
| L10 | $77.08-76.25$ <br> (10) | TP19.981x19.848x0.319 | 13.380 | 349.119 | 0.038 | 0.293 | 581.831 812706 | 0.001 0.000 |
| L11 | 76.25-76(11) | TP20.021x19.981x0.456 | 13.404 | 497.242 | 0.027 | 0.293 | 812.706 | 0.000 |
| L12 | 76-74.5 (12) | TP20.261×20.021x0.45 | 13.571 | 496.605 | 0.027 | 0.293 | 822.904 | 0.000 |
| L13 | $74.5-74.25$ <br> (13) | TP20.301×20.261x0.588 | 13.593 | 645.156 | 0.021 | 0.293 | 1048.425 | 0.000 |
| L14 | $\begin{gathered} 74.25-69.25 \\ (14) \end{gathered}$ | TP21.102×20.301x0.575 | 14.230 | 657.462 | 0.022 | 0.472 | 1116.583 | 0.000 0.000 |
| L15 | $\begin{gathered} 69.25-64.25 \\ (15) \end{gathered}$ | TP21.902×21.102×0.55 | 14.781 | 654.162 | 0.023 0.023 | 0.472 0.472 | 1161.008 1239267 | 0.000 0.000 |
| L16 | $\begin{gathered} 64.25-59.25 \\ (16) \end{gathered}$ | TP22.702x21.902×0.544 | 15.332 | 671.157 | 0.023 | 0.472 | 1239.267 1247.775 | 0.000 0.000 |
| L17 | $59.25-58.08$ <br> (17) | TP22.89 $22.702 \times 0.538$ | 15.465 15.501 | 669.237 | 0.023 0.018 | 0.472 0.472 | 1247.775 1609.742 | 0.000 0.000 |
| L18 | $58.08-57.73$ <br> (18) | TP22.946x22.89x0.713 | 15.501 | 882.406 | 0.018 | 0.472 | 1609.742 | 0.000 0.000 |
| L19 | 57.73-57.5 <br> (19) | TP22.982×22.946x0.713 | 15.528 | 883.867 | 0.018 0.018 | 0.472 0.471 | 1615.258 1683.958 | 0.000 0.000 |
| L20 | 57.5-52.5 (20) | TP23.783×22.982×0.688 | 16.116 | 884.460 | 0.018 | 0.471 | 1683.958 | 0.000 |
| L21 | 52.5-47(21) | TP24.663×23.783×0.688 | 16.376 | 898.251 | 0.018 | 0.471 | 1738.517 | 0.000 |
| L22 | 47-45.25 (22) | TP24.568x23.768x0.75 | 17.012 | 995.064 | 0.017 | 0.471 | 1946.908 | 0.000 |
| L23 | $\begin{gathered} 45.25-40.5 \\ (23) \end{gathered}$ | TP25.328x24.568x0.725 | 17.542 | 993.606 | 0.018 | 0.471 | 2016.542 | 0.000 |
| L24 | 40.5-40.25 | TP25.368x25.328x0.725 | 17.563 | 995.222 | 0.018 | 0.471 | 2023.300 | 0.000 |


| tnxTower <br> B+T Group <br> 1717 S. Boulder, Suite 300 <br> Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | $\begin{aligned} & \text { Job } \\ & 85565 . \end{aligned}$ | ORD - NU (SSL | $\begin{aligned} & \text { Page } \\ & 39 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | Date 15:01:04 09/21/18 |
|  | Client | Crown Castle | Designed by xjones |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Section No. \& Elevation

$f t$ \& Size \& Actual $V_{u}$ K \& $\phi V_{n}$

$K$ \& \[
$$
\begin{gathered}
\text { Ratio } \\
V_{k} \\
\hline
\end{gathered}
$$

\] \& | Actual |
| :--- |
| $T_{u}$ | \& $\phi T_{n}$ \& \[

$$
\begin{gathered}
\text { Ratio } \\
T_{u} \\
\hline
\end{gathered}
$$
\] <br>

\hline \& $f t$ \& \& K \& $K$ \& $\phi V_{n}$ \& $k i p-f t$ \& $k i p-f t$ \& $\phi T_{n}$ <br>
\hline \& (24) \& \& \& \& \& \& \& <br>

\hline L25 \& $$
\begin{gathered}
40.25-35.25 \\
(25)
\end{gathered}
$$ \& TP26.168x25.368x0.7 \& 18.116 \& 993.081 \& 0.018 \& 0.471 \& 2094.883 \& 0.000 <br>

\hline L26 \& $$
\begin{gathered}
35.25-30.25 \\
(26)
\end{gathered}
$$ \& TP26.969x26.168×0.688 \& 18.648 \& 1006.470 \& 0.019 \& 0.471 \& 2196.858 \& 0.000 <br>

\hline L27 \& $$
\begin{gathered}
30.25-27.75 \\
(27)
\end{gathered}
$$ \& TP27.369x26.969x0.675 \& 18.912 \& 1003.690 \& 0.019 \& 0.471 \& 2229.167 \& 0.000 <br>

\hline L28 \& $$
\begin{gathered}
27.75-27.5 \\
(28)
\end{gathered}
$$ \& TP27.409x27.369x0.725 \& 18.928 \& 1077.630 \& 0.018 \& 0.470 \& 2383.258 \& 0.000 <br>

\hline L29 \& 27.5-22.5 (29) \& TP28.209x27.409x0.7 \& 19.446 \& 1072.650 \& 0.018 \& 0.470 \& 2454.275 \& 0.000 <br>
\hline L30 \& 22.5-19.5 (30) \& TP28.689x28.209x0.688 \& 19.748 \& 1072.360 \& 0.018 \& 0.470 \& 2502.142 \& 0.000 <br>

\hline L31 \& $$
\begin{gathered}
19.5-19.25 \\
(31)
\end{gathered}
$$ \& TP28.729x28.689x0.8 \& 19.765 \& 1244.610 \& 0.016 \& 0.470 \& 2872.283 \& 0.000 <br>

\hline L32 \& $$
\begin{gathered}
19.25-14.25 \\
(32)
\end{gathered}
$$ \& TP29.529x28.729x0.775 \& 20.295 \& 1241.340 \& 0.016 \& 0.470 \& 2959.658 \& 0.000 <br>

\hline L33 \& 14.25-14 (33) \& TP29.569x29.529x0.775 \& 20.314 \& 1243.060 \& 0.016 \& 0.470 \& 2968.133 \& 0.000 <br>
\hline L34 \& 14-13.75 (34) \& TP29.609x29.569x0.775 \& 20.341 \& 1244.790 \& 0.016 \& 0.470 \& 2976.617 \& 0.000 <br>

\hline L35 \& $$
\begin{gathered}
13.75-12.98 \\
(35)
\end{gathered}
$$ \& TP29.733×29.609x0.8 \& 20.430 \& 1289.320 \& 0.016 \& 0.470 \& 3088.692 \& 0.000 <br>

\hline L36 \& $$
\begin{gathered}
12.98-12.73 \\
(36)
\end{gathered}
$$ \& TP29.773x29.733x0.8 \& 20.452 \& 1291.110 \& 0.016 \& 0.470 \& 3097.483 \& 0.000 <br>

\hline L37 \& $$
\begin{gathered}
12.73-7.73 \\
(37)
\end{gathered}
$$ \& TP30.573x29.773x0.788 \& 20.990 \& 1306.580 \& 0.016 \& 0.470 \& 3230.325 \& 0.000 <br>

\hline L38 \& 7.73-2.73 (38) \& TP31.373×30.573×0.775 \& 21.485 \& 1320.930 \& 0.016 \& 0.470 \& 3362.567 \& 0.000 <br>
\hline L39 \& 2.73-0 (39) \& TP31.81×31.373×0.763 \& 21.759 \& 1318.710 \& 0.017 \& 0.470 \& 3411.608 \& 0.000 <br>
\hline
\end{tabular}

Pole Interaction Design Data

| Section No. | Elevation | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ | Ratio $M_{u t}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ | Comb. Stress | Allow. <br> Stress <br> Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n v}$ | $\phi V_{n}$ | $\phi T_{n}$ |  |  |  |
| L1 | 108-103 (1) | 0.009 | 0.244 | 0.000 | 0.084 | 0.001 | $\begin{gathered} 0.261 \\ \end{gathered}$ | 1.050 | 4.8 .2 |
| L2 | 103-98.5 (2) | 0.010 | 0.768 | 0.000 | 0.086 | 0.004 | $\begin{gathered} 0.786 \\ 4 \end{gathered}$ | 1.050 | 4.8 .2 |
| L3 | 98.5-98(3) | 0.005 | 0.218 | 0.000 | 0.044 | 0.001 | $0.225$ | 1.050 | 4.8.2 |
| L.4 | 98-93(4) | 0.009 | 0.378 | 0.000 | 0.062 | 0.001 | $0.391$ | 1.050 | 4.8 .2 ¢ |
| L5 | 93-88(5) | 0.009 | 0.538 | 0.000 | 0.060 | 0.001 | $\begin{gathered} 0.551 \\ \end{gathered}$ | 1.050 | 4.8 .2 |
| L6 | 88-83 (6) | 0.009 | 0.680 | 0.000 | 0.059 | 0.001 | $0.693$ | 1.050 | 4.8.2 |
| L7 | 83-82.33(7) | 0.009 | 0.698 | 0.000 | 0.059 | 0.001 | $\begin{gathered} 0.710 \\ \% \end{gathered}$ | 1.050 | 4.8.2 |
| L8 | $82.33-82.08$ <br> (8) | 0.005 | 0.409 | 0.000 | 0.034 | 0.001 | $\begin{gathered} 0.416 \\ \% \end{gathered}$ | 1.050 | 4.8.2 |
| L9 | $82.08-77.08$ <br> (9) | 0.006 | 0.492 | 0.000 | 0.038 | 0.001 | $\begin{gathered} 0.499 \\ 8 \end{gathered}$ | 1.050 | 4.8 .2 |
| L10 | $77.08-76.25$ <br> (10) | 0.006 | 0.504 | 0.000 | 0.038 | 0.001 | $\begin{gathered} 0.512 \\ \% \end{gathered}$ | 1.050 | 4.8 .2 |


| InxTower | $\begin{array}{\|l\|} \hline \text { Job } \\ 85565 \end{array}$ | ORD - NU (SS | $\begin{aligned} & \text { Page } \\ & 40 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| B+T Group <br> 1717 S. Boulder, Suite 300 | Project |  | $\begin{array}{\|l} \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation | $\begin{gathered} \mathrm{Ratiog}_{P_{u}} \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ M_{u x} \end{gathered}$ | $\begin{aligned} & \overline{\text { Ratio }} \\ & M_{x y} \end{aligned}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ | Comb. Stress <br> Ratio | Allow. <br> Stress <br> Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi_{\text {P }}{ }_{n}$ | $\phi M_{7 x}$ | $\phi M_{n v}$ | $\phi V_{n}$ | $\phi T_{n}$ |  | Ratio |  |
| L11 | 76.25-76 (11) | 0.004 | 0.362 | 0.000 | 0.027 | 0.000 | $\overline{0.367}$ | 1.050 | 4.8.2 |
| L12 | 76-74.5(12) | 0.004 | 0.382 | 0.000 | 0.027 | 0.000 | $0.387$ | 1.050 | 4.8.2 |
| L13 | $74.5-74.25$ <br> (13) | 0.003 | 0.300 | 0.000 | 0.021 | 0.000 | $0.304$ | 1.050 | 4.8 .2 |
| L14 | $\underset{\text { (14) }}{74.25-69.25}$ | 0.004 | 0.343 | 0.000 | 0.022 | 0.000 | $0.347$ | 1.050 | 4.8.2 |
| L15 | 69.25-64.25 <br> (15) | 0.004 | 0.391 | 0.000 | 0.023 | 0.000 | $0.396$ | 1.050 | 4.8.2 / |
| L16 | $64.25-59.25$ <br> (16) | 0.004 | 0.426 | 0.000 | 0.023 | 0.000 | $0.431$ | 1.050 | 4.8.2 |
| L17 | $59.25-58.08$ <br> (17) | 0.004 | 0.438 | 0.000 | 0.023 | 0.000 | $0.443$ | 1.050 | 4.8.2 |
| L18 | $58.08-57.73$ <br> (18) | 0.003 | 0.340 | 0.000 | 0.018 | 0.000 | $0.343$ | 1.050 | 4.8.2 |
| L19 | 57.73-57.5 <br> (19) | 0.003 | 0.341 | 0.000 | 0.018 | 0.000 |  | 1.050 | 4.8.2 |
| L20 | 57.5-52.5 (20) | 0.004 | 0.373 | 0.000 | 0.018 | 0.000 | $0.377$ | 1.050 | 4.8.2 |
| L21 | 52.5-47 (21) | 0.004 | 0.382 | 0.000 | 0.018 | 0.000 | $0.386$ | 1.050 | 4.8.2 |
| L22 | 47-45.25 (22) | 0.004 | 0.382 | 0.000 | 0.017 | 0.000 | $0.386$ | 1.050 | 4.8.2 |
| L23 | $45.25-40.5$ <br> (23) | 0.004 | 0.409 | 0.000 | 0.018 | 0.000 | ${ }_{0}^{7}$ | 1.050 | 4.8.2 |
| L24 | $40.5-40.25$ <br> (24) | 0.004 | 0.409 | 0.000 | 0.018 | 0.000 | $0.414$ | 1.050 | 4.8.2 |
| L25 | $\begin{gathered} 40.25-35.25 \\ (25) \end{gathered}$ | 0.004 | 0.437 | 0.000 | 0.018 | 0.000 | $0.442$ | 1.050 | 4.8.2 |
| L26 | $\begin{gathered} 35.25-30.25 \\ (26) \end{gathered}$ | 0.005 | 0.458 | 0.000 | 0.019 | 0.000 | $0.463$ | 1.050 | 4.8.2 |
| L27 | $\begin{gathered} 30.25-27.75 \\ (27) \end{gathered}$ | 0.005 | 0.473 | 0.000 | 0.019 | 0.000 | $0.478$ | 1.050 | 4.8.2 |
| L28 | $\begin{gathered} 27.75-27.5 \\ (28) \end{gathered}$ | 0.004 | 0.443 | 0.000 | 0.018 | 0.000 | $0.448$ | 1.050 | 4.8.2 |
| L29 | 27.5-22.5 (29) | 0.005 | 0.469 | 0.000 | 0.018 | 0.000 | $0.474$ | 1.050 | 4.8.2 |
| L30 | 22.5-19.5 (30) | 0.005 | 0.483 | 0.000 | 0.018 | 0.000 | $0.489$ | 1.050 | 4.8 .2 ل |
| L31 | $\begin{gathered} 19.5-19.25 \\ (31) \end{gathered}$ | 0.004 | 0.421 | 0.000 | 0.016 | 0.000 | $0.425$ | 1.050 | 4.8.2 |
| L32 | $\begin{gathered} 19.25-14.25 \\ (32) \end{gathered}$ | 0.005 | 0.442 | 0.000 | 0.016 | 0.000 | $0.447$ | 1.050 | 4.8.2 |
| L33 | 14.25-14 (33) | 0.005 | 0.442 | 0.000 | 0.016 | 0.000 | $0.447$ | 1.050 | 4.8.2 |
| L34 | 14-13.75 (34) | 0.005 | 0.443 | 0.000 | 0.016 | 0.000 | 0.448 <br> $\downarrow$ | 1.050 | 4.8 .2 V |
| L35 | $\begin{gathered} 13.75-12.98 \\ (35) \end{gathered}$ | 0.004 | 0.431 | 0.000 | 0.016 | 0.000 | $0.436$ | 1.050 | 4.8.2 |
| L36 | $\underset{(36)}{12.98-12.73}$ | 0.004 | 0.432 | 0.000 | 0.016 | 0.000 | $0.436$ | 1.050 | 4.8.2 |


| tnxTower <br> B+T Group | $\begin{aligned} & \text { Job } \\ & 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{aligned}$ |  | $\begin{aligned} & \text { Page } \\ & 41 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation | Ratio $P_{u}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \end{gathered}$ | $\begin{aligned} & \text { Ratio } \\ & M_{t y y} \end{aligned}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ | Comb. Stress | Allow. Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L37 | $12.73-7.73$ <br> (37) | 0.005 | 0.446 | 0.000 | 0.016 | 0.000 | $\begin{gathered} 0.451 \\ \end{gathered}$ | 1.050 | 4.8 .2 |
| L38 | 7.73-2.73(38) | 0.005 | 0.459 | 0.000 | 0.016 | 0.000 | $\begin{gathered} 0.465 \\ \end{gathered}$ | 1.050 | 4.8 .2 |
| L39 | 2.73-0 (39) | 0.005 | 0.470 | 0.000 | 0.017 | 0.000 | $\begin{gathered} 0.475 \\ \end{gathered}$ | 1.050 | 4.8.2 |

## Section Capacity Table

| Section No. | Elevation $f t$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \curvearrowleft P_{\text {allow }} \\ K \end{gathered}$ | $\%$ <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 108-103 | Pole | TP8.625x8.625x0.313 | 1 | -2.394 | 269.918 | ** | ** |
| L2 | 103-98.5 | Pole | TP8.625x8.625x0.313 | 2 | -2.607 | 269.918 | ** | ** |
| L3 | 98.5-98 | Pole | TP16.5x16.5x0.313 | 3 | -2.652 | 525.629 | ** | ** |
| L4 | 98-93 | Pole | TP17.3×16.5x0.188 | 4 | -6.781 | 794.471 | ** | ** |
| L5 | 93-88 | Pole | TP18.101×17.3x0.188 | 5 | -7.110 | 830.635 | ** | ** |
| L6 | 88-83 | Pole | TP18.901x18.101x0.188 | 6 | -7.477 | 858.446 | ** | ** |
| L7 | 83-82.33 | Pole | TP19.008x18.901×0.188 | 7 | -7.531 | 862.113 | ** | ** |
| L8 | 82.33-82.08 | Pole | TP19.048×19.008×0.325 | 8 | -7.562 | 1506.666 | ** | ** |
| L9 | 82.08-77.08 | Pole | TP19.848x19.048x0.319 | 9 | -9.100 | 1541.347 | ** | ** |
| L10 | 77.08-76.25 | Pole | TP19.981×19.848×0.319 | 10 | -9.192 | 1551.837 | ** | ** |
| L11 | 76.25-76 | Pole | TP20.021x19.981x0.456 | 11 | -9.237 | 2210.239 | ** | ** |
| L12 | 76-74.5 | Pole | TP20.261×20.021×0.45 | 12 | -9.457 | 2207.415 | ** | ** |
| L13 | 74.5-74.25 | Pole | TP20.301x20.261×0.588 | 13 | -9.508 | 2867.718 | ** | ** |
| L14 | 74.25-69.25 | Pole | TP21.102x20.301x0.575 | 14 | -10.402 | 2922.423 | ** | ** |
| L15 | 69.25-64.25 | Pole | TP21.902x21.102×0.55 | 15 | -11.245 | 2907.744 | ** | ** |
| Li6 | 64.25-59.25 | Pole | TP22.702x21.902x0.544 | 16 | -12.108 | 2983.291 | ** | ** |
| L17 | 59.25-58.08 | Pole | TP22.89x22.702x0.538 | 17 | -12.313 | 2974.755 | ** | ** |
| L18 | 58.08-57.73 | Pole | TP22.946x22.89x0.713 | 18 | -12.395 | 3922.296 | ** | ** |
| L19 | 57.73-57.5 | Pole | TP22.982x22.946x0.713 | 19 | -12.445 | 3928.785 | ** | ** |
| L20 | 57.5-52.5 | Pole | TP23.783x22.982x0.688 | 20 | -13.502 | 3931.420 | ** | ** |
| L21 | 52.5-47 | Pole | TP24.663x23.783x0.688 | 21 | -13.987 | 3992.730 | ** | ** |
| L22 | 47-45.25 | Pole | TP24.568×23.768×0.75 | 22 | -15.772 | 4423.062 | ** | ** |
| L23 | 45.25-40.5 | Pole | TP25.328×24.568x0.725 | 23 | -16.914 | 4416.583 | ** | ** |
| L24 | 40.5-40.25 | Pole | TP25.368x25.328x0.725 | 24 | -16.983 | 4423.765 | ** | ** |
| L25 | 40.25-35.25 | Pole | TP26.168x25.368x0.7 | 25 | -18.197 | 4414.242 | ** | ** |
| L26 | 35.25-30.25 | Pole | TP26.969x26.168x0.688 | 26 | -19.438 | 4473.766 | ** | ** |
| L27 | 30.25-27.75 | Pole | TP27.369x26.969x0.675 | 27 | -20.067 | 4461.387 | ** | ** |
| L28 | 27.75-27.5 | Pole | TP27.409x27.369x0.725 | 28 | -20.144 | 4790.068 | ** | ** |
| L29 | 27.5-22.5 | Pole | TP28.209x27.409x0.7 | 29 | -21.472 | 4767.924 | ** | ** |
| L30 | 22.5-19.5 | Pole | TP28.689x28.209x0.688 | 30 | -22.286 | 4766.643 | ** | ** |
| L31 | 19.5-19.25 | Pole | TP28.729x28.689x0.8 | 31 | -22.366 | 5532.271 | ** | ** |
| L32 | 19.25-14.25 | Pole | TP29.529x28.729x0.775 | 32 | -23.806 | 5517.739 | ** | ** |
| L33 | 14.25-14 | Pole | TP29.569x29.529x0.775 | 33 | -23.886 | 5525.425 | ** | ** |
| L34 | 14-13.75 | Pole | TP29.609×29.569x0.775 | 34 | -23.964 | 5533.101 | ** | ** |
| L35 | 13.75-12.98 | Pole | TP29.733x29.609x0.8 | 35 | -24.206 | 5731.047 | ** | ** |
| L36 | 12.98-12.73 | Pole | TP29.773x29.733×0.8 | 36 | -24.291 | 5738.974 | ** | ** |
| L37 | 12.73-7.73 | Pole | TP30.573x29.773x0.788 | 37 | -25.885 | 5807.770 | ** | ** |
| L38 | 7.73-2.73 | Pole | TP31.373x30.573x0.775 | 38 | -27.504 | 5871.537 | ** | ** |
| L39 | 2.73-0 | Pole | TP31.81x31.373x0.763 | 39 | -28.396 | 5861.688 | ** | ** |
|  |  |  |  |  |  | $\text { Pole (L2) } \begin{array}{cc} \text { Summary } \\ * * \end{array}$ |  | ** |


| tnxTower <br> B+T Group | $\begin{array}{\|l} \text { Job } \\ 85565.009 .01 \text { - HARTFORD - NU (SSUSA),CT (BU\# 876363) } \end{array}$ |  | $\begin{aligned} & \text { Page } \\ & 42 \text { of } 42 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 15:01:04 09/21/18 } \end{array}$ |
| Tulsa, OK 74119 <br> Phone: (918) 587-4630 <br> FAX: (918) 295-0265 | Client | Crown Castle | Designed by xjones |


| Section No. | Elevation ft | Component Type | Size | Critical Element | $P$ $K$ | $\begin{gathered} o P_{\text {allow }} \\ K \end{gathered}$ | $\%$ Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |

** Additional Calculations in Appendix C
Program Version 8.0.4.0

APPENDIX B
BASE LEVEL DRAWING


BUSINESS UNIT: 876363

APPENDIX C
ADDITIONAL CALCULATIONS
CClpole - version 4.1.1
$\underset{\text { per } \operatorname{TA-222-H}}{\text { C(ClPO }}$


## TNX Geometry Input

Increment (ft): 5

|  | Section Height ( ft ) |  | Section Length ( ft ) | Lap Splice Length (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Tapered Pole Grade | Weight Multiplier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 108 | - 103 | 5 |  | 0 | 8.625 | 8.625 | 0.3125 | A53-B-35 | 1.000 |
| 2 | 103 | - 98.5 | 4.5 | 0 | 0 | 8.625 | 8.625 | 0.3125 | A53-8-35 | 1.000 |
| 3 | 98.5 | - 98 | 0.5 | 0 | 0 | 16.500 | 16.500 | 0.3125 | A53-B-35 | 1.000 |
| 4 | 98 | - 93 | 5 |  | 18 | 16.500 | 17.300 | 0.1875 | A607-65 | 1.000 |
| 5 | 93 | - 88 | 5 |  | 18 | 17.300 | 18.101 | 0.1875 | A607-65 | 1.000 |
| 6 | 88 | - 83 | 5 |  | 18 | 18.101 | 18.901 | 0.1875 | A607-65 | 1.000 |
| 7 | 83 | - 82.33 | 0.67 | $\therefore$ | 18 | 18.901 | 19.008 | 0.1875 | A607-65 | 1.000 |
| 8 | 82.33 | - 82.08 | 0.25 |  | 18 | 19.008 | 19.048 | 0.325 | A607-65 | 1.035 |
| 9 | 82.08 | - 77.08 | 5 |  | 18 | 19.048 | 19.848 | 0.31875 | A607-65 | 1.036 |
| 10 | 77.08 | - 76.25 | 0.83 | . | 18 | 19.848 | 19.981 | 0.31875 | A607-65 | 1.033 |
| 11 | 76.25 | - 76 | 0.25 |  | 18 | 19.981 | 20.021 | 0.45625 | A607-65 | 1.152 |
| 12 | 76 | - 74.5 | 1.5 |  | 18 | 20.021 | 20.261 | 0.45 | A607-65 | 1.159 |
| 13 | 74.5 | - 74.25 | 0.25 |  | 18 | 20.261 | 20.301 | 0.5875 | A607-65 | 0.972 |
| 14 | 74.25 | - 69.25 | 5 |  | 18 | 20.301 | 21.102 | 0.575 | A607-65 | 0.967 |
| 15 | 69.25 | - 64.25 | 5 | . | 18 | 21.102 | 21.902 | 0.55 | A607-65 | 0.984 |
| 16 | 64.25 | - 59.25 | 5 |  | 18 | 21.902 | 22.702 | 0.54375 | A607-65 | 0.972 |
| 17 | 59.25 | - 58.08 | 1.17 |  | 18 | 22.702 | 22.890 | 0.5375 | A607-65 | 0.977 |
| 18 | 58.08 | - 57.73 | 0.35 |  | 18 | 22.890 | 22.946 | 0.7125 | A607-65 | 0.933 |
| 19 | 57.73 | - 57.5 | 0.23 |  | 18 | 22.946 | 22.982 | 0.7125 | A607-65 | 0.932 |
| 20 | 57.5 | - 52.5 | 5 |  | 18 | 22.982 | 23.783 | 0.6875 | A607-65 | 0.941 |
| 21 | 52.5 | - 50.25 | 5.5 | 3.25 | 18 | 23.783 | 24.663 | 0.6875 | A607-65 | 0.930 |
| 22 | 50.25 | - 45.25 | 5 |  | 18 | 23.768 | 24.568 | 0.75 | A607-65 | 0.929 |
| 23 | 45.25 | - 40.5 | 4.75 |  | 18 | 24.568 | 25.328 | 0.725 | A607-65 | 0.941 |
| 24 | 40.5 | - 40.25 | 0.25 |  | 18 | 25.328 | 25.368 | 0.725 | A607-65 | 0.940 |
| 25 | 40.25 | - 35.25 | 5 |  | 18 | 25.368 | 26.168 | 0.7 | A607-65 | 0.953 |
| 26 | 35.25 | - 30.25 | 5 |  | 18 | 26.168 | 26.969 | 0.6875 | A607-65 | 0.951 |
| 27 | 30.25 | - 27.75 | 2.5 | . | 18 | 26.969 | 27.369 | 0.675 | A607-65 | 0.960 |
| 28 | 27.75 | - 27.5 | 0.25 |  | 18 | 27.369 | 27.409 | 0.725 | A607-65 | 0.948 |
| 29 | 27.5 | - 22.5 | 5 |  | 18 | 27.409 | 28.209 | 0.7 | A607-65 | 0.962 |
| 30 | 22.5 | - 19.5 | 3 |  | 18 | 28.209 | 28.689 | 0.6875 | A607-65 | 0.969 |
| 31 | 19.5 | - 19.25 | 0.25 |  | 18 | 28.689 | 28.729 | 0.8 | A607-65 | 0.899 |
| 32 | 19.25 | - 14.25 | 5 |  | 18 | 28.729 | 29.529 | 0.775 | A607-65 | 0.910 |
| 33 | 14.25 | - 14 | 0.25 |  | 18 | 29.529 | 29.569 | 0.775 | A607-65 | 0.909 |
| 34 | 14 | - 13.75 | 0.25 |  | 18 | 29.569 | 29.609 | 0.775 | A607-65 | 0.972 |
| 35. | 13.75 | - 12.98 | 0.77 |  | 18 | 29.609 | 29.733 | 0.8 | A607-65 | 0.968 |
| 36 | 12.98 | - 12.73 | 0.25 |  | 18 | 29.733 | 29.773 | 0.8 | A607-65 | 0.967 |
| 37 | 12.73 | - 7.73 | 5 |  | 18 | 29.773 | 30.573 | 0.7875 | A607-65 | 0.964 |
| 38 | 7.73 | - 2.73 | 5 |  | 18 | 30.573 | 31.373 | 0.775 | A607-65 | 0.962 |
| 39 | 2.73 | - 0 | 2.73 |  | 18 | 31.373 | 31.810 | 0.7625 | A607-65 | 0.968 |

## TNX Section Forces

| Increment (ft): |  |  | 5 | TNX Output |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Section |  | ght (ft) | $\mathbf{P}_{\mathbf{u}} \quad$ (K) | $\mathrm{M}_{\mathrm{ux}} \text { (kip- }$ <br> ft) | $\mathrm{V}_{\mathrm{u}} \quad(\mathrm{K})$ |
| 1 | 108 | - | 103 | 2.39 | 13.85 | 6.51 |
| 2 | 103 | - | 98.5 | 2.61 | 43.53 | 6.66 |
| 3 | 98.5 | - | 98 | 2.65 | 46.86 | 6.68 |
| 4 | 98 | - | 93 | 6.78 | 100.42 | 11.07 |
| 5 | 93 | - | 88 | 7.11 | 156.34 | 11.31 |
| 6 | 88 | - | 83 | 7.48 | 213.43 | 11.54 |
| 7 | 83 | - | 82.33 | 7.53 | 221.18 | 11.59 |
| 8 | 82.33 | - | 82.08 | 7.56 | 224.08 | 11.61 |
| 9 | 82.08 | - | 77.08 | 9.10 | 287.50 | 13.30 |
| 10 | 77.08 | - | 76.25 | 9.19 | 298.57 | 13.38 |
| 11 | 76.25 | - | 76 | 9.24 | 301.91 | 13.40 |
| 12 | 76 | - | 74.5 | 9.46 | 322.14 | 13.57 |
| 13 | 74.5 | - | 74.25 | 9.51 | 325.54 | 13.59 |
| 14 | 74.25 | - | 69.25 | 10.40 | 395.19 | 14.23 |
| 15 | 69.25 | - | 64.25 | 11.24 | 467.70 | 14.78 |
| 16 | 64.25 | - | 59.25 | 12.11 | 542.97 | 15.33 |
| 17 | 59.25 | - | 58.08 | 12.31 | 560.98 | 15.47 |
| 18 | 58.08 | - | 57.73 | 12.39 | 566.40 | 15.50 |
| 19 | 57.73 | - | 57.5 | 12.44 | 569.97 | 15.53 |
| 20 | 57.5 | - | 52.5 | 13.50 | 649.07 | 16.12 |
| 21 | 52.5 | - | 50.25 | 13.99 | 685.62 | 16.38 |
| 22 | 50.25 | - | 45.25 | 15.77 | 769.11 | 17.01 |
| 23 | 45.25 | - | 40.5 | 16.91 | 851.14 | 17.54 |
| 24 | 40.5 | - | 40.25 | 16.98 | 855.53 | 17.56 |
| 25 | 40.25 | - | 35.25 | 18.20 | 944.72 | 18.12 |
| 26 | 35.25 | - | 30.25 | 19.44 | 1036.61 | 18.65 |
| 27 | 30.25 | - | 27.75 | 20.07 | 1083.54 | 18.91 |
| 28 | 27.75 | - | 27.5 | 20.14 | 1088.27 | 18.93 |
| 29 | 27.5 | - | 22.5 | 21.47 | 1184.20 | 19.45 |
| 30 | 22.5 | - | 19.5 | 22.29 | 1242.97 | 19.75 |
| 31 | 19.5 | - | 19.25 | 22.37 | 1247.91 | 19.77 |
| 32 | 19.25 | - | 14.25 | 23.81 | 1348.05 | 20.29 |
| 33 | 14.25 | - | 14 | 23.89 | 1353.13 | 20.31 |
| 34 | 14 | - | 13.75 | 23.96 | 1358.21 | 20.34 |
| 35 | 13.75 | - | 12.98 | 24.21 | 1373.90 | 20.43 |
| 36 | 12.98 | - | 12.73 | 24.29 | 1379.01 | 20.45 |
| 37 | 12.73 | - | 7.73 | 25.88 | 1482.61 | 20.99 |
| 38 | 7.73 | - | 2.73 | 27.50 | 1588.77 | 21.48 |
| 39 | 2.73 | - | 0 | 28.40 | 1647.77 | 21.76 |

## Analysis Results

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 108-103 | Pole | TP8.625x8.625x0.3125 | Pole | 24.4\% | Pass |
| 103-98.5 | Pole | TP8.625x8.625×0.3125 | Pole | 74.3\% | Pass |
| 98.5-98 | Pole | TP16.5×16.5×0.3125 | Pole | 21.3\% | Pass |
| 98-93 | Pole | TP17.3×16.5×0.1875 | Pole | 36.9\% | Pass |
| 93-88 | Pole | TP18.101×17.3x0.1875 | Pole | 52.2\% | Pass |
| 88-83 | Pole | TP18.901×18.101×0.1875 | Pole | 65.7\% | Pass |
| 83-82.33 | Pole | TP19.008×18.901×0.1875 | Pole | 67.4\% | Pass |
| 82.33-82.08 | Pole + Reinf. | TP19.048×19.008×0.325 | Reinf. 10 Tension Rupture | 57.4\% | Pass |
| 82.08-77.08 | Pole + Reinf. | TP19.848×19.048×0.3188 | Reinf. 10 Tension Rupture | 69.0\% | Pass |
| 77.08-76.25 | Pole + Reinf. | TP19.981×19.848×0.3188 | Reinf. 10 Tension Rupture | 70.8\% | Pass |
| 76.25-76 | Pole + Reinf. | TP20.021×19.981×0.4563 | Reinf. 4 Tension Rupture | 55.8\% | Pass |
| 76-74.5 | Pole + Reinf. | TP20.261×20.021×0.45 | Reinf. 4 Tension Rupture | 58.5\% | Pass |
| 74.5-74.25 | Pole + Reinf. | TP20.301×20.261×0.5875 | Reinf. 4 Tension Rupture | 51.3\% | Pass |
| 74.25-69.25 | Pole + Reinf. | TP21.102x20.301×0.575 | Reinf. 4 Tension Rupture | 59.1\% | Pass |
| 69.25-64.25 | Pole + Reinf. | TP21.902×21.102x0.55 | Reinf. 4 Tension Rupture | 66.6\% | Pass |
| 64.25-59.25 | Pole + Reinf. | TP22.702x21.902x0.5438 | Reinf. 4 Tension Rupture | 73.7\% | Pass |
| 59.25-58.08 | Pole + Reinf. | TP22.89x22.702x0.5375 | Reinf. 4 Tension Rupture | 75.3\% | Pass |
| 58.08-57.73 | Pole + Reinf. | TP22.946x22.89x0.7125 | Reinf. 3 Tension Rupture | 56.3\% | Pass |
| 57.73-57.5 | Pole + Reinf. | TP22.982x22.946×0.7125 | Reinf. 3 Tension Rupture | 56.6\% | Pass |
| 57.5-52.5 | Pole + Reinf. | TP23.783x22.982x0.6875 | Reinf, 3 Tension Rupture | 61.8\% | Pass |
| 52.5-50.25 | Pole + Reinf. | TP24.663x23.783×0.6875 | Reinf. 3 Tension Rupture | 64.0\% | Pass |
| 50.25-45.25 | Pole + Reinf. | TP24.568×23.768×0.75 | Reinf. 3 Tension Rupture | 64.3\% | Pass |
| 45.25-40.5 | Pole + Reinf. | TP25.328x24.568×0.725 | Reinf. 3 Tension Rupture | 68.4\% | Pass |
| 40.5-40.25 | Pole + Reinf. | TP25.368×25.328×0.725 | Reinf. 3 Tension Rupture | 68.6\% | Pass |
| 40.25-35.25 | Pole + Reinf. | TP26.168×25.368×0.7 | Reinf. 3 Tension Rupture | 72.7\% | Pass |
| $35.25-30.25$ | Pole + Reinf. | TP26.969x26.168×0.6875 | Reinf. 3 Tension Rupture | 76.6\% | Pass |
| 30.25-27.75 | Pole + Reinf. | TP27.369×26.969x0.675 | Reinf. 3 Tension Rupture | $78.4 \%$ | Pass |
| 27.75-27.5 | Pole + Reinf. | TP27.409×27.369x0.725 | Reinf, 2 Tension Rupture | 69.5\% | Pass |
| 27.5-22.5 | Pole + Reinf. | TP28.209x27.409×0.7 | Reinf. 2 Tension Rupture | 72.7\% | Pass |
| 22.5-19.5 | Pole + Reinf. | TP28.689×28.209x0.6875 | Reinf. 2 Tension Rupture | 74.6\% | Pass |
| 19.5-19.25 | Pole + Reinf. | TP28.729x28.689x0.8 | Reinf. 2 Tension Rupture | 69.6\% | Pass |
| 19.25-14.25 | Pole + Reinf. | TP29.529x28.729x0.775 | Reinf. 2 Tension Rupture | 72.5\% | Pass |
| 14.25-14 | Pole + Reinf. | TP29.569×29.529x0.775 | Reinf. 2 Tension Rupture | 72.7\% | Pass |
| 14-13.75 | Pole + Reinf. | TP29.609×29.569x0.775 | Reinf. 2 Tension Rupture | 73.2\% | Pass |
| 13.75-12.98 | Pole + Reinf. | TP29.733 $29.609 \times 0.8$ | Reinf. 1 Tension Rupture | $69.2 \%$ | Pass |
| 12.98-12.73 | Pole + Reinf. | TP29.773x29.733×0.8 | Reinf. 1 Tension Rupture | 69.3\% | Pass |
| 12.73-7.73 | Pole + Reinf. | TP30.573×29.773×0.7875 | Reinf. 1 Tension Rupture | 72.0\% | Pass |
| $7.73-2.73$ | Pole + Reinf. | TP31.373×30.573×0.775 | Reinf. 1 Tension Rupture | $74.6 \%$ | Pass |
| 2.73-0 | Pole + Reinf. | TP31.81×31.373×0.7625 | Reinf. 1 Tension Rupture | 75.9\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 74.3\% | Pass |
|  |  |  | Reinforcement | 78.4\% | Pass |
|  |  |  | Overall | 78.4\% | Pass |

Additional Calculations


| Site Info |  |
| ---: | :---: |
| BU \# | 876363 |
| Site Name | artford -NU (SSUSA), C |
| Order \# | 85565.009 .01 |


| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{I}_{\mathrm{ar} \text { ( } \mathrm{in}\rangle}$ | 0 |


| Applied Loads |  |
| ---: | :---: |
| Moment (kip-ft) | 1648.00 |
| Axial Force (kips) | 28.00 |
| Shear Force (kips) | 22.00 |



## Connection Properties

Anchor Rod Data
GROUP 1: (8) 2-1/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 38" BC GROUP 2: (3) $2-1 / 4^{\prime \prime} \varnothing$ bolts (A615-75 $\mathrm{N} ; \mathrm{Fy}=75 \mathrm{ksi}, \mathrm{Fu}=100 \mathrm{ksi}$ ) on $43.8^{\prime \prime} \mathrm{BC}$ pos. (deg): 35, 135, 235

GROUP 3: (3) 2-1/4" $\varnothing$ bolts $\left\langle\mathrm{A} 193 \mathrm{Gr}\right.$. $\mathrm{B} 7 \mathrm{~N} ; \mathrm{Fy}=105 \mathrm{ksi}, \mathrm{Fu}=125 \mathrm{ksi}$ ) on $43.5^{\prime \prime} \mathrm{BC}$ pos. (deg): 55, 215, 315

Base Plate Data
$36^{\prime \prime}$ OD x $2.5^{\prime \prime}$ Plate (F1554-55; Fy=55 ksi, Fu=75 ksi)
Stiffener Data
N/A
Pole Data
$31.81^{\prime \prime} \times 0.25^{\prime \prime} 18$-sided pole (A607-65; Fy=65 ksi, Fu=80 ksi)

## Analysis Results

Anchor Rod Summary GROUP 1:

| $\mathrm{Pu}=155.66$ | $\phi \mathrm{Pn}=243.75$ | Stress Rating |
| :--- | :--- | :---: |
| $\mathrm{Vu}=2.75$ | $\phi V n=73.13$ | $61.0 \%$ |
| $M u=n / a$ | $\phi M n=n / a$ | Pass |

GROUP 2:

| $\mathrm{Pu}=176.16$ | $\phi \mathrm{Pn}=243.75$ | Stress Rating |
| :--- | :--- | :---: |
| $\mathrm{Vu}=0$ | $\phi \mathrm{Vn}=73.13$ | $68.8 \%$ |
| $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |

GROUP 3:

| $P u=175.07$ | $\phi P n=341.25$ | Stress Rating |
| :--- | :--- | :---: |
| $V u=0$ | $\phi V n=102.38$ | $48.9 \%$ |
| $M u=n / a$ | $\phi M n=n / a$ | Pass |


| Base Plate Summary |  |  |
| :--- | :--- | :--- |
| Max Stress (ksi): | 29.58 | (Flexural) |
| Allowable Stress $\{\mathrm{ksi}):$ | 49.5 |  |
| Stress Rating: | $\mathbf{5 6 . 9 \%}$ | Pass |


| BU \# | 876363 |
| ---: | :---: |
| Site Name | artford - NU (SSUSA), |
| Order \# | 85565.009 .01 |


| TIA-222 Revision | $H$ |
| :---: | :---: |


| Applied Loads |  |
| ---: | :---: |
| Moment (kip-ft) | 47.00 |
| Axial Force (kips) | 2.70 |
| Shear Force (kips) | 6.70 |

Top Plate - External
Bottom Plate - External


| Top Plate Capacity |  |  |
| :--- | :--- | :--- |
| Max Stress (ksi): | 40.92 | (Flexural) |
| Allowable Stress (ksi): | 45.00 |  |
| Stress Rating: | $\mathbf{8 6 . 6 \%}$ | Pass |
| Tension Side Stress Rating: | $\mathbf{7 9 . 3 \%}$ | Pass |


| Bottom Plate Capacity |  |  |
| :--- | :---: | :--- |
| Max Stress (ksi): | 12.90 | (Flexural) |
| Allowable Stress (ksi): | 45.00 |  |
| Stress Rating: | $\mathbf{2 7 . 3 \%}$ | Pass |
| Tension Side Stress Rating: | $\mathbf{8 . 6 \%}$ | Pass |

Pier and Pad Foundation

BU \# : 876363
Site Name: Hartford - NU (SSU
App. Number: 457785 Rev. 0

|  | Block Foundation?: |
| ---: | ---: |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating* | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 203.71 | 22.00 | $10.3 \%$ | Pass |
| Bearing Pressure (ksf) | 5.18 | 1.91 | $35.2 \%$ | Pass |
| Overturning (kip*ft) | 3888.50 | 1818.50 | $46.8 \%$ | Pass |
| Pier Flexure (Comp.) (kip*ft) | 2022.59 | 1747.00 | $82.3 \%$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 11934.00 | 48.25 | $0.4 \%$ | Pass |
| Pad Flexure (kip $* f)$ | 2323.42 | 655.88 | $26.9 \%$ | Pass |
| Pad Shear - 1-way (kips) | 646.50 | 108.64 | $16.0 \%$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.164 | 0.028 | $16.3 \%$ | Pass |
| Flexural 2-way (Comp) (kip*ft) | 1496.79 | 1048.20 | $66.7 \%$ | Pass |

*Rating per TIA-222-H Section
15.5

| Soil Rating*: | $\mathbf{4 6 . 8} \%$ |
| :---: | :---: |
|  | $\mathbf{8 2 . 3} \%$ |


| Pad Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Depth, $\mathrm{D}:$ | 7 | ft |  |
| Pad Width, $\mathrm{W}:$ | 21.5 | ft |  |
| Pad Thickness, $\mathrm{T}:$ | 3 | ft |  |
| Pad Rebar Size, $\mathrm{Sp}:$ | 8 |  |  |
| Pad Rebar Quantity, mp: | 22 |  |  |
| Pad Clear Cover, $\mathrm{cc}_{\mathrm{pad}}:$ | 4 | in |  |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60000 | psi |
| Concrete Compressive Strength, F'c: | 3000 | psi |
| Dry Concrete Density, oc: | 150 | pcf |


| Soll Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\mathrm{Y}:$ | 111 | pcf |
| Utimate Gross Bearing, Qult: | 6.900 | ksf |
| Cohesion, $\mathrm{Cu}:$ | 0.000 | ksf |
| Friction Angle, $\phi:$ | 32 | degrees |
| SPT Blow Count, $\mathbf{N}_{\text {blows: }}:$ |  |  |
| Base Friction, $\boldsymbol{\mu}:$ | 0.35 |  |
| Neglected Depth, $\mathrm{N}:$ | 3.30 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | 10 | ft |

## Address:

No Address at This Location

## ASCE 7 Hazards Report

| Standard: | ASCE/SEI 7-10 | Elevation: 71.06 ft (NAVD 88) |
| :--- | :--- | :--- |
| Risk Category: | II | Latitude: 41.750775 |
| Soil Class: | D - Stiff Soil | Longitude: -72.713675 |



## Wind

Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

122 Vmph
76 Vmph
86 Vmph
92 Vmph
100 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Wed Sep 192018

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

## Seismic

## Site Soil Class: <br> D - Stiff Soil

Results:

| $\mathrm{S}_{\mathrm{s}}:$ | 0.181 | $\mathrm{~S}_{\mathrm{DS}}:$ | 0.193 |
| :--- | :--- | :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.064 | $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.102 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.600 | $\mathrm{~T}_{\mathrm{L}}:$ | 6.000 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.400 | $\mathrm{PGA}:$ | 0.091 |
| $\mathrm{~S}_{\mathrm{MS}}:$ | 0.290 | $\mathrm{PGA}_{\mathrm{M}}:$ | 0.146 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.153 | $\mathrm{~F}_{\text {PGA }}:$ | 1.600 |
|  |  | $\mathrm{I}_{\mathrm{e}}:$ |  |

## Seismic Design Category <br> B




## Data Accessed:

Date Source:

Wed Sep 192018
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2
Additional data for site-specific ground motion procedures in accordance with
ASCE/SEI 7-10 Ch. 21 are available from USGS.

## Results:

Ice Thickness: $\quad 1.00 \mathrm{in}$.
Concurrent Temperature: 5 F
Gust Speed: $\quad 50 \mathrm{mph}$
Data Source:
Date Accessed: Wed Sep 192018
Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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Date: October 08, 2018
Charles McGuirt
Crown Castle
3530 Toringdon Way, Suite 300
Charlotte, NC 28277
Charles.McGuirt@crowncastle.com
Subject:
Contractor Designation:

## Engineering Firm Designation:

Site Data:

Structure Information:


BOLLTIロNG, PLLC
Engineered Tower Solutions, PLLC
8120 Sheridan Blvd, Suite A-311
Westminster, CO 80003
(919) 782-2710
brandon.little@ets-pllc.com

| Mount Structural Analysis |  |
| :--- | :--- |
| Verizon Wireless Co-Locate |  |
| Carrier Site Number: | 79283 |
| Carrier Site Name: | West Hartford 4 CT |
|  |  |
| Crown Castle BU Number: | 876363 |
| Crown Castle Site Name: | HARTFORD - NU (SSUSA) |
| Crown Castle JDE Number: | 528518 |
| Crown Castle PO Number: | 1263856 |
| Crown Castle Application Number: | 457785 Rev. 0 |
|  |  |
| ETS Project No.: | 184431.14 |

219 New Park Road, Hartford, Hartford County, CT 06106-2949

Tower Height \& Type: 108.0-ft Monopole

Mount Elevation:
105.0-ft
10.0-ft Sector Mount

Dear Charles McGuirt,

Engineered Tower Solutions, PLLC is pleased to submit this "Mount Structural Analysis Report" to determine the structural integrity of Verizon Wireless antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

Based upon our analysis, we have determined the adequacy of the antenna mounting system that will support the existing and proposed loading to be for the following Load Case:

Sector Mount (Multiple) Sufficient Capacity
The analysis has been performed in accordance with the TIA-222-H Standard. This analysis utilizes an ultimate 3 -second gust wind speed of 125 mph as required by the 2016 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

We at Engineered Tower Solutions, PLLC appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects, please give us a call.

Mount structural analysis prepared by:

Helen Tesfaye, El
Structural Engineer

Respectfully Submitted by:

Frederic G. Bost, PE
Owner/President


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ASCE 7 Hazards Report

## 1) INTRODUCTION

This mount is a 10.0 ft Sector mount installed at the 105.0 ft elevation of the 108.0 ft Monopole. Engineered Tower Solutions, PLLC, did not visit the site. A mapping and/or mount manufacturer drawings were not provided. Therefore, per direction of Crown Castle, photos of the tower were compared with other mounts within our database and a similar and comparable mount was used to perform this mount analysis
2) ANALYSIS CRITERIA

| Building Code: | 2012 IBC |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| Wind Speed: | 125 mph |
| Exposure Category: | C |
| Topographic Factor: | 1 |
| Ice Thickness: | 2.00 in |
| Wind Speed with Ice: | 50 mph |
| Seismic Ss: | 0.181 |
| Seismic S1: | 0.064 |
| Service Wind Speed: | 30 mph |

Table 1 - Proposed Equipment Configuration

| Mount Centerline (f) | Antenna Centerline (ft) |  | Antenna Manufacturer | Antenna Model | Mount/ Modification Details |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 105.0 | 105.0 | 6 | ANTEL | BXA-70063/6CF | (3) 10.0 ft Sector Mount |
|  |  | 6 | COMMSCOPE | SBNHH-1D65B |  |
|  |  | 1 | RAYCAP | RVZDC-6627-PF-48 |  |
|  |  | 1 | RFS/CELWAVE | DB-T1-6Z-8AB-0Z |  |
|  |  | 3 | SAMSUNG <br> TELECOMMUNICATIONS | RFV01U-D1A |  |
|  |  | 3 | SAMSUNG TELECOMMUNICATIONS | RFV01U-D2A |  |

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Structural Level Drawings (Installed) | Crown Castle | Rocument | $08 / 30 / 2018$ |
| :---: | :---: | :---: | :---: |
| Structural Level Drawing (Proposed) | Crown Castle | $08 / 30 / 2018$ | CCI Sites |
| Carrier Application | App\# 457785 Rev. 0 | $08 / 22 / 2018$ | CCI Sites |
| 4-Structural Analysis Report | B+T Group | 7861410 | CCI Sites |
| CCI Sites |  |  |  |

## 3.1) Analysis Method

RISA-3D (version 16.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix C.

## 3.2) Assumptions

1) Engineered Tower Solutions, PLLC, did not visit the site. A mapping and/or mount manufacturer drawings were not provided. Therefore, per direction of Crown Castle, photos of the tower were compared with other mounts within our database and a similar and comparable mount was used to perform this mount analysis
2) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specification.
3) The configuration of antennas, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
5) This Structural Analysis is not a condition assessment of the mount and is an evaluation of the theoretical structural capacity.
6) This analysis is based from the information supplied, and therefore, this report's results are as accurate as the supplied data.
7) Engineered Tower Solutions, PLLC makes no warranties, expressed and/or implied, in connection with this report, and disclaims any liability associated with material, fabrication, or erection of the mount. Engineered Tower Solutions, PLLC will not be held responsible from any consequential or incidental damages sustained by any person, firm, or organization as a result of the contents of this report. The maximum liability of Engineered Tower Solutions, PLLC pursuant to this report will be limited to the total fee received for compilation of this report.
8) It is the tower owner's responsibility to verify that the mount modeled and analyzed is the correct structure modeled.
9) The use of this report shall be limited to the purpose for which it was commissioned and may not be used for any other purposes without the written consent of Engineered Tower Solutions, PLLC.
10) Member connections are assumed to have been designed to meet or exceed the theoretical capacity of the connected member.
11) Steel grades have been assumed as follows:

| a) Channel, Solid Round, Angle, Plate | ASTM A36 (Gr 36) |
| :--- | :--- |
| b) HSS (Rectangular) | ASTM 500 (Gr B-46) |
| c) HSS (Round) | ASTM 500 (Gr B-42) |
| d) Pipe | ASTM A53 (Gr 35) |
| e) Connection Bolts | ASTM A325 |
| f) U-Bolts | SAE 429 Gr.2 |

This analysis may be affected if any assumptions are not valid or have been made in error. Engineered Tower Solutions, PLLC should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 3a- Mount Component Stresses vs. Capacity, Alpha

| Mount Centerline <br> (ft) | Component | \% Capacity | Pass/Fail | Notes |
| :---: | :---: | :---: | :---: | :---: |
| 105.0 | Face Mount - Horizontal | 83.5 | PASS | 1 |
|  | Mount Pipe - Vertical | 47.9 | PASS | 1 |
|  | Sidearm - Horizontal | 20.4 | PASS | 1 |

Table 3b-Mount Component Stresses vs. Capacity, Beta

| Mount <br> Centerline <br> (ft) | Component | \% Capacity | Pass/Fail | Notes |
| :---: | :---: | :---: | :---: | :---: |
| 105.0 | Face Mount-Horizontal | 90.3 | PASS | 1 |
|  | Mount Pipe - Vertical | 44.8 | PASS | 1 |
|  | Sidearm-Horizontal | 19.0 | PASS | 1 |

Table 3c-Mount Component Stresses vs. Capacity, Gamma

| Mount <br> Centerline <br> (ft) | Component | \% Capacity | Pass/Fail | Notes |
| :---: | :---: | :---: | :---: | :---: |
| 105.0 | Face Mount - Horizontal | 82.8 | PASS | 1 |
|  | Mount Pipe - Vertical | 47.1 | PASS | 1 |
|  | Sidearm - Horizontal | 20.2 | PASS | 1 |

Notes:

1) See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the \% capacity consumed.

| Tower Mount Rating (max from all components) $=$ | $90.3 \%$ |
| :---: | :---: |

## 4.1) Recommendations

The tower mount has sufficient capacity to carry the existing and proposed load configuration. No modifications are required at this time.

WIRE FRAME AND RENDERED MODELS

Site Name: $\quad$ West Hartford 4, CT Cumulative Power Density

| Operator | Operating Frequency | Number of Trans. | ERP Per Trans: | Total ERP | Distance to Target | Calculated <br> Power Density | Maximum Permissablë Exposure | Fraction of MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (MHz) |  | (watts) | (watts) | (feet) | (mW/cm^2) | ( $\mathrm{mW} / \mathrm{cm}^{\wedge} \mathbf{2}$ ) | (\%) |
| VZW PCS | 1970 | 1 | 5000 | 5000 | 105 | 0.1631 | 1.0 | 16.31\% |
| VZW Cellular LTE | 869 | 1 | 3050 | 3050 | 105 | 0.0995 | 0.579333333 | 17.17\% |
| VZW Cellular | 869 | 3 | 410 | 1230 | 105 | 0.0401 | 0.579333333 | 6.93\% |
| VZW AWS | 2145 | 1 | 7400 | 7400 | 105 | 0.2414 | 1.0 | 24.14\% |
| VZW 700 | 746 | 1 | 2200 | 2200 | 105 | 0.0718 | 0.497333333 | 14.43\% |
| Total Percentage of Maximum Permissible Exposure |  |  |  |  |  |  |  |  |

Total Percentage of Maximum Permissible Exposure

$\mathrm{MHz}=$ Megahertz
$\mathrm{mW} / \mathrm{cm}^{\wedge} 2=$ milliwatts per square centimeter ERP = Effective Radiated Power

Absolute worst case maximum values used, including the following assumptions: 1. closest accessible point is distance from antenna to base of pole;
2. continuous transmission from all available channels at full power for indefinite time period; and, 3. all RF energy is assumed to be directed solely to the base of the pole.

General Power Density
Page 2
$\stackrel{\text { N }}{\text { \% }}$

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