## Transcend Wireless

July 15, 2019

Members of the Siting Council
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

RE: Notice of Exempt Modification
101 Talmadge Road, Hamden, CT 06518
Latitude: 41.422862400
Longitude: -72.9511365000
T-Mobile Site\#: CT11474A - L600

Dear Ms. Bachman:

T-Mobile currently maintains six (6) antennas at the 315-foot level of the existing 765 -foot lattice tower at 101 Talmadge Road, Hamden, CT. The 765 -foot lattice tower and property are owned by LIN Television Corp. TMobile now intends to replace the six (6) existing antennas with six (6) new 600/700/1900/2100 MHz antennas. The new antennas will be installed at the same 315-foot level of the tower.

## Planned Modifications:

## Tower:

Remove
(12) 7/8" Coax
(3) TMA

Remove and Replace:
(3) LNX-6515DS (Remove) - APXVAARR24_43-U-NA20 Antenna (Replace) 600/700/1900 MHz
(3) APXV18-206517S-C-A20 (Remove) - APXV16DWV-16DWV-S-E-A20 (Replace) 2100 MHz

Install New:
(3) 1-3/8" Hybrid Cables
(3) Radio 4449 B71+B12
(3) Radio 4415 B25
(3) Radio 4415 B66
(1) 1.25 STD Mount Brace

Existing to Remain:
N/A

## Ground:

Remove: (2) 6201 ODE Cabinets

## Install: (1) 6102 Cabinet

There is no record of an original approval of this facility by the Siting Council. T-Mobile and other carriers have been approved previously for exempt modifications. T-Mobile was unable to obtain any documentation from the jurisdiction pertaining to an original approval. The proposed modification will not be violating any previous approvals.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies§ 16-SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.SA. § 16-SOj-73, a copy of this letter is being sent to Mayor -Curt B. Leng, Elected Official, and Daniel Kops, Town Planner for the Town of Hamden, as well as the owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

## Kyle Richers

Transcend Wireless
Cell: 908-447-4716
Email: krichers@transcendwireless.com

## Attachments

cc: Curt Leng - Town of Hamden Mayor
Daniel Kops- Town of Hamden Town Planner
LIN Television Corp - owner

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Monday, July 15, 2019 12:24 PM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CT11474A CSC ZO

## x

## You have a package coming.

Scheduled Delivery Date: Tuesday, 07/16/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424295937829 |
| Ship To: | Daniel Kops Town of Hamden 2750 DIXWELL AVENUE HAMDEN, CT 065183320 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 07/16/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CT11474A CSC zo |
|  | x |
| x Download the UPS mobile app |  |

From:
Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Monday, July 15, 2019 12:26 PM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CT11474A CSC EO

## x

## You have a package coming.

Scheduled Delivery Date: Tuesday, 07/16/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424296607835 |
| Ship To: | Curt Leng <br> Town of Hamden 2750 Dixwell Avenue HAMDEN, CT 065183320 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 07/16/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CT11474A CSC EO |
|  |  |
| Download the UPS mobile app |  |

## From:

Sent:
To:
Subject:

UPS Quantum View [pkginfo@ups.com](mailto:pkginfo@ups.com)
Monday, July 15, 2019 12:27 PM
krichers@transcendwireless.com
UPS Ship Notification, Reference Number 1: CT11474A CSC Owner

## x

## You have a package coming.

Scheduled Delivery Date: Wednesday, 07/17/2019

This message was sent to you at the request of TRANSCEND WIRELESS to notify you that the shipment information below has been transmitted to UPS. The physical package may or may not have actually been tendered to UPS for shipment. To verify the actual transit status of your shipment, click on the tracking link below.

## Shipment Details

| From: | TRANSCEND WIRELESS |
| :---: | :---: |
| Tracking Number: | 1ZV257424297297848 |
| Ship To: | LIN Television Corp 333 East Franklin Street RICHMOND, VA 232192213 US |
| UPS Service: | UPS GROUND |
| Number of Packages: | 1 |
| Scheduled Delivery: | 07/17/2019 |
| Signature Required: | A signature is required for package delivery |
| Weight: | 1.0 LBS |
| Reference Number 1: | CT11474A CSC Owner |
|  | $\square$ |
| $x$ Download the UPS mobile app |  |

Location 0 TALMADGE RD Mblu 3123/008///

| Acct\# | Owner | L I N TELEVISION CORP |  |
| ---: | ---: | ---: | :--- |
| Assessment | $\$ 373,940$ | Appraisal | $\$ 534,200$ |
| PID 100690 | Building Count | 1 |  |

## Current Value

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$34,500 | \$499,700 | \$534,200 |
| Assessment |  |  |  |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$24,150 | \$349,790 | \$373,940 |

## Owner of Record

Owner L I N TELEVISION CORP Sale Price \$0

## Co-Owner

Address 333 EAST FRANKLIN ST
RICHMOND, VA 23219

Certificate
Book \& Page 1905/ 206
Sale Date $\quad 11 / 29 / 1999$

## Ownership History

| Ownership History |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Owner | Sale Price | Certificate | Book \& Page | Sale Date |
| L I N TELEVISION CORP | \$0 |  | 1905/206 | 11/29/1999 |
| L W W I BROADCASTING INC | \$605,000 |  | 1470/ 283 | 12/29/1994 |
| COOK INLET COMMUNICATIONS CORP | \$0 |  | 740/459 | 01/03/1986 |

## Building Information

## Building 1 : Section 1

| Year Built: | 1965 |  |  |  |
| :--- | :--- | :---: | :---: | :---: |
| Living Area: | 812 |  |  |  |
| Building Percent | 65 |  |  |  |
| Good: | Building Attributes |  |  |  |
| Field |  |  |  | Description |
|  |  |  |  |  |
| STYLE | Warehouse |  |  |  |


| MODEL | Ind/Comm |
| :---: | :---: |
| Grade | C |
| Stories: | 1 |
| Occupancy | 1 |
| Exterior Wall 1 | Pre-finsh Metl |
| Exterior Wall 2 |  |
| Roof Structure | Flat |
| Roof Cover | T\&G/Rubber |
| Interior Wall 1 | Minim/Masonry |
| Interior Wall 2 |  |
| Interior Floor 1 | Concr-Finished |
| Interior Floor 2 |  |
| Heating Fuel | Gas |
| Heating Type | Hot Air-no Duc |
| AC Type | None |
| Bldg Use | RAD/TV TR M96 |
| Total Rooms |  |
| Total Bedrms | 00 |
| Total Baths | 0 |
| 1st Floor Use: | 4330 |
| Heat/AC | NONE |
| Frame Type | StEEL |
| Baths/Plumbing | NONE |
| Ceiling/Wall | NONE |
| Rooms/Prtns | AVERAGE |
| Wall Height | 10 |
| \% Comn Wall | 0 |

Building Photo

(http://images.vgsi.com/photos/HamdenCTPhotos//\00\02\80/12
Building Layout

(http://images.vgsi.com/photos/HamdenCTPhotos//Sketches/10C

| Building Sub-Areas (sq ft) |  |  | Legend |
| :--- | :--- | ---: | ---: |
| Code | Description | Gross <br> Area | Living <br> Area |
| BAS | First Floor | 812 | 812 |
| CAN | Canopy | 324 | 0 |
| SLB | Slab | 0 | 0 |
|  |  | 1,136 | 812 |

## Extra Features

| Extra Features | Legend |  |
| :--- | :--- | :--- |
|  | No Data for Extra Features |  |

## Land

## Land Use

| Description | RAD/TV TR M96 | Frontage | 0 |
| :--- | :--- | :--- | :--- |
| Zone | R2 | Depth | 0 |
| Neighborhood | 140 | Assessed Value | $\$ 349,790$ |
| Alt Land Appr | No | Appraised Value | $\$ 499,700$ |
| Category |  |  |  |

## Outbuildings

| Outbuildings |  |  |  |  |  | Legend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code | Description | Sub Code | Sub Description | Size | Value | Bldg \# |
| FN3 | FENCE-6' CHAIN |  |  | 770 L.F. | \$3,500 | 1 |

Valuation History

| Appraisal |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :---: |
|  | Valuation Year | Improvements | Land |  |  |
| 2017 |  | $\$ 34,500$ | Total |  |  |
| 2016 |  | $\$ 34,500$ | $\$ 499,700$ | $\$ 534,200$ |  |
| 2015 | $\$ 477,600$ | $\$ 499,700$ | $\$ 534,200$ |  |  |


| Assessment |  |  |  |  |  |
| :--- | :--- | ---: | ---: | ---: | :---: |
|  | Valuation Year | Improvements |  |  |  |
| 2017 |  | $\$ 24,150$ | Land | Total |  |
| 2016 |  | $\$ 24,150$ | $\$ 349,790$ |  |  |
| 2015 | $\$ 334,320$ | $\$ 349,790$ | $\$ 373,940$ |  |  |

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Town of Hamden, Connecticut - Assessment Parcel Map
Parcel: 3123-008-00-0000


## ESICN BASIS



- Desig critera:

RISK CAIEOORY: | ( (Based on IBC TABE 1804.5)




## GENERAL NOTES

ALL Constructon Shall 日e in compance wit the governicg buloung





- dmensions and detalls shall be checked aganst exxting felo conotions.

5. THE Contractor shal verf and coronane the siz Ano locanon of all

















## STRUCTURAL STEE

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C.





6. NsTALL FARERCOTONS PLUMM ANO LNELL ACCURATEY FITED, AND RREE FROM




11. CoNNECTON ANGLES SHAL HANE A MNMUM THCCNEESS OF $1 / 4$ NCHES.

13. Lock washer are not pexumteo for azz5 Stel assemules.













DATE: 5/31/2019
SUFFICIENT CAPACITY - 97\%

RIGOROUS STRUCTURAL ANALYSIS
FOR A 907' G-12 GUYED TOWER
NEW HAVEN (HAMDEN), CONNECTICUT

| PREPARED BY: | CD |
| :--- | :--- |
| CHECKED BY: | AP |

APPROVED: KP


| Date | Pages | Remarks |
| :---: | :---: | :---: |

STAINLESS
A Business of FDH Infrastructure Services, LLC

| Rev. | Date | Description |
| :--- | :--- | :--- |

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LINEAR APPURTENANCES ..... A-2

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| :--- | :--- | :--- |

## A. AUTHORIZATION/PURPOSE

As authorized by Kyle Richers of Transcend Wireless, a structural analysis was performed to investigate the adequacy of a 907' overall height Stainless G-12 guyed tower located at 101 Talmadge Road in Hamden, Connecticut to support specified equipment.

## B. TOWER HISTORY

The tower was originally designed and furnished in 1995 by Stainless. It was designed in accordance with TIA/EIA-222-E for a wind speed of 85 mph and 73.6 mph with $1 / 2$ " ice while supporting the following equipment:

1. One (1) top mounted Dielectric TCL-12A8 (S) antenna, fed by two (2) 6-1/8" rigid lines.
2. One (1) top mounted HDTV antenna, fed by one (1) WR1150 waveguide (future).
3. One (1) Dielectric TFU-28JSM Ch. 59 antenna, at the 730 ' level, fed by one (1) WR1150 waveguide.
4. One (1) Dielectric TFU-28JSM HDTV Ch. 14 antenna, at the 670 ' level, fed by one (1) WR1150 waveguide (future).
5. Two (2) ENG Super Quad antennas at the 760 ' level, fed by one (1) $1-5 / 8$ " line and one (1) $1 / 2$ " control cable (one future).
6. One (1) ERI 6-bay panel type FM antenna at the $610^{\prime}$ level, fed by one (1) $6-1 / 8$ " rigid line (future).
7. Two (2) Andrew MMDS wireless cable antennas at the $565^{\prime}$ level, fed by one (1) EW20 waveguide (future).
8. One (1) ERI SHPX-3AE FM antenna at the 545 ' level, fed by one (1) 3 " line.
9. One (1) ERI SHPX-3AE FM antenna at the 520 ' level, fed by one (1) 3 " line.
10. Three (3) whip antennas at the 750 ' level, fed by one (1) $1-5 / 8$ " line to each.
11. Three (3) whip antennas at the $500^{\prime}$ level, fed by one (1) $1-5 / 8^{\prime \prime}$ line to each.
12. Three (3) whip antennas at the $400^{\prime}$ level, fed by one (1) $1-5 / 8^{\prime \prime}$ line to each.
13. Three (3) whip antennas at the 350 ' level, fed by one (1) $1-5 / 8^{\prime \prime}$ line to each (future).
14. Three (3) whip antennas at the $325^{\prime}$ level, fed by one (1) $1-5 / 8$ " line to each (future).
15. Three (3) whip antennas at the 300 ' level, fed by one (1) $1-5 / 8$ " line to each (future).
16. One (1) Scala PR-450U antenna at the $339^{\prime}$ level, fed by one (1) $7 / 8^{\prime \prime}$ line.
17. One (1) Scala PR-450U antenna at the 247 ' level, fed by one (1) $7 / 8$ " line.
18. One (1) $6^{\prime}$ grid dish at the 400 ' level, fed by one (1) $1-5 / 8$ ' line.
19. Two (2) $6^{\prime}$ grid dishes at the $325^{\prime}$ level, fed by one (1) $1-5 / 8^{\prime \prime}$ line to each (future).
20. Two (2) $6^{\prime}$ grid dishes at the $225^{\prime}$ level, fed by one (1) $1-5 / 8 "$ line to each (future).
21. Two (2) $8^{\prime}$ dishes with radomes at the $325^{\prime}$ level, fed by one (1) EW63 waveguide to each (one future).

| Rev. | Date | Description |
| :--- | :--- | :--- |

22. One (1) $8^{\prime}$ dish with radome at the 166 ' level, fed by one (1) EW63 waveguide (future).
23. One (1) $8^{\prime}$ dish with radome at the 150 ' level, fed by one (1) EW63 waveguide (future).
24. One (1) inside climbing ladder with cable type safety device for the full height of the tower.
25. One (1) single car elevator with guide rails, cables, motor and elevator equipment.
26. Ice shields for all side mounted antennas, except the whip antennas.
27. One (1) red lighting system with circuits in rigid conduit for the full height of the tower.

* In 1998, the bottom stack Dielectric THP-O-2-1 antenna of the top mounted stack system was installed per Stainless Report 362006. The guy wires of all the four levels were also retensioned.
* The tower was modified in 2015 by Stainless per Report 362017. The modifications were as follows:
- Installed additional horizontal sub-bracing at the midpoints of the following bay:

| Location | No of bays |
| :---: | :---: |
| $591.3^{\prime}-583.8{ }^{\prime}$ | 1 |

- Replaced existing diagonal braces with new, higher capacity members at the following bay:

| Location | No of bays |
| :---: | :---: |
| $621.3^{\prime}-613.8^{\prime}$ | 1 |

* In 2018, the tower was modified per Stainless Report 362023. The modifications consisted the following:
- Installed additional horizontal sub-bracing at the midpoints of the following bay:

| Location | No of bays |
| :---: | :---: |
| $553.8^{\prime}-546.3^{\prime}$ | 1 |

Stainless has no record of any other modifications to the tower structure or its foundations.

## C. CONDITIONS INVESTIGATED

The analysis was performed for the tower supporting the equipment listed below based on the following sources:

- Stainless Proposal P19_3620_001 dated 4/18/2019.
- Stainless Report 362022 dated 8/22/2018.
- Emails from Kyle Richers of Transcend Wireless dated 4/12/2019, 5/2/2019, 5/23/2019 and $5 / 24 / 2019$ with details of proposed and existing equipment.

| Rev. | Date | Description |
| :--- | :--- | :--- |

- Mount analysis by Centek Engineering per Project No. 19027.14 Rev 1 dated 4/29/2019.
- CT11474A_Mount Analysis_Rev 1_19.04.29_L600.pdf

| APPURTENANCE | ELEVATION, <br> ft. | FEED LINES |
| :---: | :---: | :---: |
| $\begin{aligned} & \text { Stacked TCL-12A8(S) Ch. } 8 \text { / THP-O- } \\ & 2-1 \mathrm{Ch} .10 \end{aligned}$ | Tower top | 6-1/8"/3-1/8" rigid |
| 10' omni | 758 | 1-5/8"* |
| 5' omni | 750 | 7/8" |
| Super Quad ENG | 744 | 1-5/8"* \& 1/2" control cable |
| DB408 | 742 | 1-5/8"* |
| Ice shield | 681 | - |
| PL8 8' diameter dish/radome | 678 | EW63 \& 1/2" cable |
| PL6-65 6' diameter dish/radome | 630 | EW63 \& 1/2" cable |
| (2) Dualight 12004-rot-1r07-001 | 605 | -- |
| 6015-2/3R FM | 591 | 4-1/16" rigid |
| (2) DB408 | 529 | 7/8" to each |
| DB408 | 510 | 7/8" |
| 6810-2R 2-bay FM | 458 | 6-1/8" ${ }^{\text {rigid** }}$ |
| 15 " omni (unused) | 420 | 1/2" |
| 10' omni (unused) | 420 | 1-5/8" |
| 5" omni | 348 | 7/8" |
| Ice shield | 346 | - |
| 6' diameter grid dish | 339 | 7/8" |
| (3) RFS APX16DWV-16DWV-S-EA20 (Proposed) <br> (3) RFS APXVAARR24 43-U-NA20 <br> (Proposed) <br> (3) Radio 4449 B71+B12 (Proposed) <br> (3) Radio 4415 B25 (Proposed) <br> (3) Radio 4415 B66 (Proposed) <br> (3) Sector mounts | 315 | (3) 1-3/8" hybrid cables (Proposed) |
| (2) Dualight 12004-rot-1r07-001 | 302 | -- |
| (3) APXVSPP18-C-A20 <br> (3) APXVTM14-C-120 <br> (3) TD-RRH8×20 <br> (6) RRUs <br> (3) sector mounts | 200 | (3) 1-1/4" Hybriflex <br> (1) 1-1/4" Hybriflex cable |
| Ice shield | 166 | - |
| 8' diameter dish/radome | 160 | (2) EW63 |
| $15^{\prime \prime}$ omni (unused) | 102 | 1/2" |


| Rev. | Date | Description |
| :--- | :--- | :--- |


| ASPG952 (unused) | 100 | $2-1 / 4 "$ |
| :---: | :---: | :---: |
| GPS unit | 75 | $1 / 2^{\prime \prime}$ |
| (2) support conduits | To 200 \& 45 | $1 "$ conduit |
| Support conduit | To 315 | $1-1 / 4 "$ conduit |
| (7) support conduits | To 200', 348', <br> $2 \times 420^{\prime}, 529^{\prime}$, <br> $758^{\prime}$, top of <br> tower | $1-1 / 2^{\prime \prime}$ conduit |
| Ladder with cable safety device | To top of tower | $3 / 8^{\prime \prime}$ cable |
| Elevator system | To top of tower | - |
| FAA red lighting system | To top of tower | $1 "$ ' to 45 <br> $1-1 / 2 "$ from 45 ' to tower top |


| REMOVING EQUIPMENT |  |  |
| :---: | :---: | :---: |
| (3) APXV18-206517S-C-A20 <br> (3) LNX-6515DS-VTM | 315 | (12) $7 / 8 \%$ |

* Shared line
** This coax was cut at the $440^{\prime}-480^{\prime}$ level and a $20^{\prime}$ length of 3 " heliax was used to connect the $6-1 / 8^{\prime \prime}$ rigid coax to the antenna. The remaining length of the $6-1 / 8^{\prime \prime}$ rigid coax from $480^{\prime}$ to the top of tower was left in place

The locations of the transmission lines have been based upon the cross section from Stainless Report 362022 dated 08/22/2018 and shown on Page A-2 of this Report. Proposed transmission lines have been located to minimize the wind load on the tower. Deviating from the line arrangement as shown may invalidate the results of this analysis.

## D. LOADS AND STRESSES

The analysis was performed using the following design parameters in accordance with the 2018 Connecticut Building Code, based on the 2015 IBC, and ANSI/TIA 222-G-2005, Structural Standard for Antenna Supporting Structures and Antennas, including Addenda 1 \& 2, dated 2007 and 2009 respectively.

- Risk Category II
- 125 mph ultimate design wind speed with no ice.
- 50 mph nominal design wind speed with $3 / 4$ " design ice thickness
- Exposure Category B
- Topographic Category 5 (Mad Mare Ridge, SEE wind direction, ridge, crest $=650$ ', base $=400^{\prime}, \mathrm{L} / 2=980^{\prime}, \mathrm{x}=390^{\prime}$ windward, Kzt $\max =1.546$ )
- 0.187 earthquake spectral response acceleration at short periods (Ss)
- Earthquake Site Class D

| Rev. | Date | Description |
| :--- | :--- | :--- |

The ultimate design wind speed is converted to a nominal design wind speed for use in ANSI/TIA 222-G based upon the following formula:

$$
\begin{aligned}
\mathrm{V}_{\mathrm{asd}} & =\mathrm{V}_{\mathrm{ult}} *(0.6)^{1 / 2} \\
& =125 *(0.6)^{1 / 2} \\
& =97 \mathrm{mph}
\end{aligned}
$$

Seismic effects need not be considered as the value of Ss is less than 1.0 per Section 2.7.3 of ANSI/TIA 222-G. Load and resistance factors used to evaluate the adequacy of the structure were in accordance with ANSI/TIA 222-G.

## E. METHOD OF ANALYSIS

The analysis was performed using tnxTower, a computerized program which idealizes the tower as a structure consisting of finite elements, and subjected to simultaneous transverse and axial loads.

## F. RESULTS

The results of the analysis show the following ratings:

| COMPONENT | SPAN | \% RATING |
| :---: | :---: | :---: |
| Tower top | -- | 92 |
| Leg compression | 4 | 97 |
|  | 3 | 97 |
|  | 2 | 79 |
|  | 1 | 84 |
| Leg tension | 4 | 80 |
|  | 3 | -- |
|  | 2 | -- |
|  | 1 | -- |
| Diagonals | 4 | 60 |
|  | 3 | 67 |
|  | 2 | 72 |
|  | 1 | 76 |
| Horizontals | 4 | 50 |
|  | 3 | 68 |
|  | 2 | 51 |
|  | 1 | 47 |
| Guys | 4 | 69 |
|  | 3 | 64 |
|  | 2 | 69 |
|  | 1 | 79 |


| Rev. | Date | Description |
| :--- | :--- | :--- |


| COMPONENT | SPAN | \% RATING |
| :---: | :---: | :---: |
| Foundations | Base | 79 |
|  | Inner anchors | 72 |
|  | Outer anchors | 62 |

The rating is defined as the percentage of the component design capacity that is used up in supporting itself and the loading from the antennas and transmission lines under the design wind and ice loading conditions. Ratings of up to $105 \%$ for tower members, and up to $110 \%$ for foundations are considered acceptable due to tolerances in calculating the applied loads on the tower as well as member design capacities.

However the state of Connecticut mandates a maximum rating of $100 \%$, and the tower has been reviewed based on $100 \%$ maximum rating.

The twist and sway of the dishes under a service wind load of 60 mph are as follows:

| Dish | Elevation, ft. | Twist, degrees | Sway, degrees |
| :---: | :---: | :---: | :---: |
| PL8 8' diameter dish/ radome | 678 | 0.92 | 0.08 |
| PL6-65 6' diameter dish/radome | 630 | 0.91 | 0.08 |
| 6' diameter grid dish | 339 | 0.84 | 0.03 |
| 8' diameter dish/radome | 160 | 0.71 | 0.07 |

## G. CONCLUSIONS AND RECOMMENDATIONS

Based on the preceding results, the following conclusions may be drawn:

1. The tower supporting equipment as specified in Section C above is adequate to achieve an ultimate design wind speed of 125 mph with no ice, and a nominal design wind speed of 50 mph with $3 / 4$ " design ice thickness in accordance with the 2018 Connecticut Building Code, based on the 2015 IBC, and ANSI/TIA 222-G with the analysis parameters of Section D.
2. The existing mounts at 315 ' have been analyzed by Centek Engineering per Project No. 19027.14 Rev 1 dated 4/29/2019. Based on the recommendations of this report, the mounts are adequate after installing pipe bracing to the existing mounts.

## H. PROVISIONS OF ANALYSIS

The analysis performed and the conclusions contained herein are based on the assumption that the tower has been properly installed and maintained, including, but not limited to the following:

1. Proper alignment and plumbness.
2. Correct bolt tightness.
3. Correct guy tensions.

| Rev. | Date | Description |
| :--- | :--- | :--- |

4. No significant deterioration or damage to any component.

Furthermore, the information and conclusions contained in this Report were determined by application of the current "state-of-the-arts" engineering and analysis procedures and formulae, and Stainless assumes no obligations to revise any of the information or conclusions contained in this Report in the event that such engineering and analysis procedures and formulae are hereafter modified or revised. In addition, under no circumstances will Stainless have any obligation or responsibility whatsoever for or on account of consequential or incidental damages sustained by any person, firm or organization as a result of any information or conclusions contained in the Report, and the maximum liability of Stainless, if any, pursuant to this Report shall be limited to the total funds actually received by Stainless for preparation of this Report. Customer has requested Stainless to prepare and submit to Customer an engineering analysis with respect to the Subject Tower and has further requested Stainless to make appropriate recommendations regarding suggested structural modifications and changes to the Subject Tower. In making such request of Stainless, Customer has informed Stainless that Customer will make a determination as to whether or not to implement any of the changes or modifications which may be suggested by Stainless and that Customer will have any such changes or modifications made by riggers, erectors and other subcontractors of Customer's choice.

Customer hereby agrees and acknowledges that Stainless shall have no liability whatsoever to Customer or to others for any work or services performed by any persons other than Stainless in connection with the implementation of any structural changes or modifications recommended by Stainless including but not limited to any services rendered for Customer or for others by riggers, erectors or other subcontractors. Customer acknowledges and agrees that any riggers, erectors or subcontractors retained or employed by Customer shall be solely responsible to Customer and to others for the quality of work performed by them and that Stainless shall have no liability or responsibility whatsoever as a result of any negligence or breach of contract by any such rigger, erector or subcontractor.
R=643.00 ft (-131)

DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :--- | :--- | :--- | :--- |
| Dielectric THP-O2-1 wraparound | 802.58 | Radio 4415 B25 (Proposed) | 315 |
| ELEVATOR BEAMS _WEIGHT | 767 | Radio 4415 B25 (Proposed) | 315 |
| 10' WHIP | 758 | Radio 4415 B25 (Proposed) | 315 |
| 5' OMNI ANTENNA | 750 | Radio 4415 B66 (Proposed) | 315 |
| NURAD SUPERQUAD II ENG | 744 | Radio 4415 B66 (Proposed) | 315 |
| DB408 | 742 | Radio 4415 B66 (Proposed) | 315 |
| ICE SHIELD | Sector mount | 315 |  |
| PL8 | Sector mount | 315 |  |
| Andrew PL6-65 | 678 | Sector mount | 315 |
| (2) Dualight 12004-RTO-1R07-001 | 630 | (2) Dualight 12004-RTO-1R07-001 | 302 |
| SHIVELY 6015-2/3R wraparound FM | 591 | APXSPP18-C-A20 w/ Mount Pipe | 200 |
| (2) DB408 | 529 | APXSPP18-C-A20 w/ Mount Pipe | 200 |
| DB408 | 510 | APXSPP18-C-A20 w/ Mount Pipe | 200 |
| SHVLY 6810 FW RAD _MT | 458 | APXVTM14-C-I20 w/ Mount Pipe | 200 |
| 15' WHIP (UNUSED) | 420 | APXVTM14-C-I20 w/ Mount Pipe | 200 |
| 10' WHIP (UNUSED) | 420 | APXVTM14-C-I20 w/ Mount Pipe | 200 |
| 5' OMNI ANTENNA | 348 | TD-RRH8x20 | 200 |
| ICE SHIELD | 346 | TD-RRH8x20 | 200 |
| 6' Grid Dish | 339 | TD-RRH8x20 | 200 |
| APX16DWV-16DWVS-E-A20 w/ Mount <br> Pipe (Proposed) | 315 | (2) 800 MHz RRH | 200 |
| APX16DWV-16DWVS-E-A20 w/ Mount | 315 | (2) 800 MHz RRH | 200 |
| Pipe (Proposed) | (2) 800 MHz RRH | 200 |  |
| APX16DWV-16DWVS-E-A20 w/ Mount <br> Pipe (Proposed) | 315 | Sector mount | 200 |
| APXVAARR24_43-U-NA20 (Proposed) | 315 | Sector mount | 200 |
| APXVAARR24_43-U-NA20 (Proposed) | 315 | Sector mount | 200 |
| APXVAARR24_43-U-NA20 (Proposed) | 315 | ICE SHIELD | 166 |
| Radio 4449 B71+B12 (Proposed) | 315 | 8160 |  |
| Radio 4449 B71+B12 (Proposed) | 315 | DSiF03F36D-D on sidearm | 110 |
| Radio 4449 B71+B12 (Proposed) | 315 | 15' WHIP (UNUSED) | 102 |
|  |  | ASGP952 ANTENNA (UNUSED) | 100 |
|  | GPS ANTENNA | 75 |  |

$\underline{906.1 \mathrm{ft}}$

## TOWER DESIGN NOTES

1. Tower designed for Exposure B to the TIA-222-G Standard.
2. Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
3. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 60 mph wind.
5. Tower Structure Class II.
6. Topographic Category 5 with Crest Height of 250.00 ft
7. 129.00 ft TCL-12A8 (S) is included for load transfer only.
73.8 ft
3.8 ft
$\frac{43.8 \mathrm{tt}}{28.8 \mathrm{ft}}$
2109716
1294141 lb (Axial)
44 kip-ft (Torque)


## Structural Analysis Report

Antenna Mount Analysis

$$
T-M o b i l e ~ S i t e ~ \#: ~ C T 11474 A
$$

101 Talmadge Road $H$ a mden, CT

Centek Project No. 19027.14

Dato: April 24, 2019 Rev 1: April 29, 2019

Max Stress Ratio=92.1\%


Prepared for:
T-Mobile USA
35 Griffin Road Bloomfield, CT 06002

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- CONCLUSION


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- T-MOBILE, RF DATA SHEET


## Centered on Solutions"

April 29, 2019

Mr. Dan Reid
Transcend Wireless
10 Industrial Ave
Mahwah, NJ 07430

Re: Structural Letter ~ Antenna Mount
T-Mobile - Site Ref: CT11474A
101 Talmadge Road
Hamden, CT 06518

Centek Project No. 19027.14

Dear Mr. Reid,

Centek Engineering, Inc. has reviewed the T-Mobile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the existing mount, consisting of three (3) custom-made T-Frames attached to the existing structure, to support the equipment configuration. The review considered the effects of wind load, dead load and ice load. The review considered the effects of wind load, dead load and ice load in accordance with the 2015 International Building Code as modified by the 2018 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G Structural Standards for Steel Antenna Towers and Supporting Structures.

The loads considered in this analysis consist of the following:

- T-Mobile:
- T-Frames: Three (3) Ericsson RFS APX16DWV-16DWV-S-E-A20 panel antennas, three (3) RFS APXVAARR24-43-NA20 panel antennas, three (3) Ericsson 4415 B66 remote radio units, three (3) Ericsson 4415 B25 remote radio units, three (3) Ericsson 4449 B71_B12 remote radio units mounted on three (3) T-Frames with a RAD center elevation of 315-ft +/- AGL. (NOTE: APXVAARR24-43 antenna must be mounted at a maximum of 3-ft away from outrigger arm.
- The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering a nominal design wind speed of 97 mph for Hamden as required in Appendix N of the 2018 Connecticut State Building Code.

A structural analysis of tower and foundation needs to be completed prior to any work.
Based on our review of the installation, it is our opinion that the existing T-frames with the installation of one (1) Pipe 1.25 STD mount brace are structurally adequate to support the proposed antenna configuration. If there are any questions regarding this matter, please feel free to call.


Prepared by:

Fernando J. Palacios
Engineer

Structural Analysis - Mount Analysis
T-Mobile Site Ref. ~ CT11474A
Hamden, CT
Rev 1~ April 29, 2019

## Section2-Calculations

Hamden, CT
Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Design Heights, Exposure Coefficients,

## and Velocity Pressures Per TIA-222-G

## Wind Speeds

Basic Wind

| Basic Wind Speed | $\mathrm{V}:=97$ | mp |
| ---: | :--- | :--- |
| Basic Wind Speed with Ice | $\mathrm{V}_{\mathrm{i}}:=50$ | mph |

Input
Structure Type =
Structure Category =
Structure_Type:= Lattice
(User Input)

Exposure Category $=$
Structure Height
Height to Center of Antennas =
$\mathrm{h}:=765$
ft

Radial Ice Thickness =
Radial Ice Density =
z:= 315
ft
in
pcf
(User Input)
Topograpic Factor $=$

Gust Response Factor =
$\mathrm{t}_{\mathrm{i}}:=0.75$
(User Input - 2018 CSBC Appendix N)
(User Input per Annex B of TIA-222-G)

| Structure Type = | Structure_Type:= Lattice |  | (User Input |
| :---: | :---: | :---: | :---: |
| Structure Category = | SC: $=11$ |  | (User Input) |
| Exposure Category = | Exp : = C |  | (User Input |
| Structure Height = | $\mathrm{h}:=765$ | ft | (User Input) |
| Height to Center of Antennas = | $\mathrm{z}:=315$ | $f t$ | (User Input) |
| Radial Ice Thickness = | $\mathrm{t}_{\mathrm{i}}=0.75$ | in | (User Input |
| Radial Ice Density = | Id := 56.00 | pcf | (User Input |
| Topograpic Factor $=$ | $\mathrm{K}_{\text {zt }}:=1.0$ |  | (User Input) |
|  | $\mathrm{K}_{\mathrm{a}}:=1.0$ |  | (User Input |
| Gust Response Factor = | $\mathrm{G}_{\mathrm{H}}=1.165$ |  | (User Input) |

## Output

Wind Direction Probability Factor $=$

Importance Factors =

$$
\mathrm{K}_{\mathrm{iz}}:=\left(\frac{\mathrm{z}}{33}\right)^{0.1}=1.253
$$

Velocity Pressure Coefficient Antennas =

Velocity Pressure w/o Ice Antennas =
Velocity Pressure with Ice Antennas =
$\mathrm{t}_{\mathrm{iz}}:=2.0 \cdot \mathrm{t}_{\mathrm{i}} \cdot \mathrm{I}_{\text {ice }} \cdot \mathrm{K}_{\text {iz }} \cdot \mathrm{K}_{\mathrm{zt}}{ }^{0.35}=1.88$
$\mathrm{Kz}:=2.01 \cdot\left(\left(\frac{\mathrm{z}}{\mathrm{zg}}\right)\right)^{\bar{\alpha}}=1.611$

$K_{d}:=\|$| if Structure_Type $=$ Pole |
| :--- |
| $\left.\\|$$\\| .95$ <br> if Structure_Type $=$ Lattice <br> $\\|$$\\| .85$ \right\rvert\,$=0.85$ |
| (Per Table 2-2 of |
| TIA-222-G) |

$\mathrm{I}_{\text {Wind }}:=\left|\begin{array}{c}\text { if } \mathrm{SC}=1 \\ \left.\| \begin{array}{l}\| \\ 0.87 \\ \text { if } \mathrm{SC}=2 \\ \| \\ \| .00 \\ \text { if } \mathrm{SC}=3 \\ \| 1.15\end{array} \right\rvert\,\end{array}\right|=1$

$\mathrm{I}_{\text {ice }}:=\left|\begin{array}{c}\text { if } \mathrm{SC}=1 \\ \| \mathrm{O} \\ \text { if } \mathrm{SC}=2 \\ \| 1.00 \\ \text { if } \mathrm{SC}=3 \\ \| 1.25\end{array}\right|=1$

$$
\mathrm{qz}:=0.00256 \cdot \mathrm{~K}_{\mathrm{d}} \cdot \mathrm{Kz} \cdot \mathrm{~V}^{2} \cdot \mathrm{I}_{\text {wind }}=32.992 \mathrm{psf}
$$

$q Z_{\text {ice }}:=0.00256 \cdot \mathrm{~K}_{\mathrm{d}} \cdot \mathrm{Kz} \cdot \mathrm{V}_{\mathrm{i}}{ }^{2} \cdot \mathrm{I}_{\text {Wind }}=8.766 \mathrm{psf}$

## Subject:

Location:
Rev. 1: 04/29/19

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on Antennas

Antenna Data:

| Antenna Model $=$ | RFS APXVAARR24_43 |  |  |
| ---: | :--- | ---: | :--- |
| Antenna Shape $=$ | Flat | in | (User Input) |
| Antenna Height $=$ | $\mathrm{L}_{\mathrm{ant}}:=95.9$ | (User Input) |  |
| Antenna Width $=$ | $\mathrm{W}_{\mathrm{ant}}:=19.7$ | in | (User Input) |
| Antenna Thickness $=$ | $\mathrm{T}_{\mathrm{ant}}:=8.7$ | in | (User Input) |
| Antenna Weight | $=$ | $\mathrm{WT}_{\mathrm{ant}}:=133.4$ | (User Input) |
| Number of Antennas | $=$ | $\mathrm{N}_{\mathrm{ant}}:=1$ |  |
| Antenna Aspect Ratio | $=$ | $\mathrm{Ar}_{\mathrm{ant}}:=\frac{\mathrm{L}_{\mathrm{ant}}}{\mathrm{W}_{\mathrm{ant}}}=4.9$ |  |
| (User Input) |  |  |  |

## Wind Load (without ice)

| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{antF}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{W}_{\mathrm{ant}}}{144}=13.1$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force Front $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{antF}}=658$ | lbs |
| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{ants}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{T}_{\mathrm{ant}}}{144}=5.8$ | sf |
| Total Antenna Wind Force Side $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{ants}}=291$ | lbs |

## Wind Load (with ice)

| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{\text {ICEantF }}:=\frac{\left(\mathrm{L}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=16.2$ | sf |
| :---: | :---: | :---: |
| Total Antenna Wind Force w/ Ice Front = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qz} \mathrm{i}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca} \mathrm{a}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEantF }}=216$ | lbs |
| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{\text {ICEants }}:=\frac{\left(\mathrm{L}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=8.6$ | sf |
| Total Antenna Wind Force w/ Ice Side = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qz}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {ant }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICEantS }}=115$ | lbs |

## Gravity Load (without ice)



## Subject:

Location: Hamden, CT
Centered on Solutions ${ }^{53}$ www.centekeng.com
63-2 North Branford Road P: (203) 488-0580
Branford, CT 06405

Loads on Equipment

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on Antennas

| Antenna Data: |  |  |  |
| :---: | :---: | :---: | :---: |
| Antenna Model $=$Antenna Shape $=$ | RFS APX16DWV-16DWVS-E-A20 |  |  |
|  | Flat |  | (User Input) |
| Antenna Height = | $\mathrm{L}_{\text {ant }}:=55.9$ | in | (User Input) |
| Antenna Width = | $\mathrm{W}_{\text {ant }}:=13$ | in | (User Input) |
| Antenna Thickness = | $\mathrm{T}_{\text {ant }}:=3.15$ | in | (User Input) |
| Antenna Weight = | $W T_{\text {ant }}:=40.7$ | Ibs | (User Input) |
| Number of Antennas = | $\mathrm{Nant}_{\text {a }}:=1$ |  | (User Input) |
| Antenna Aspect Ratio = | $\mathrm{Ar}_{\text {ant }}:=\frac{\mathrm{L}_{\text {ant }}}{\mathrm{W}_{\text {ant }}}$ |  |  |
| Antenna Force Coefficient = | $\mathrm{Ca}_{\text {ant }}=1.28$ |  |  |

## Wind Load (without ice)

| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{antF}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{W}_{\mathrm{ant}}}{144}=5$ | sf |
| :--- | :--- | :--- |
| Total Antenna Wind Force Front $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{antF}}=248$ | lbs |
| Surface Area for One Antenna $=$ | $\mathrm{SA}_{\mathrm{ants}}:=\frac{\mathrm{L}_{\mathrm{ant}} \cdot \mathrm{T}_{\mathrm{ant}}}{144}=1.2$ | sf |
| Total Antenna Wind Force Side $=$ | $\mathrm{F}_{\mathrm{ant}}:=\mathrm{qZ} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\mathrm{ant}} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\mathrm{ants}}=60$ | lbs |

## Wind Load (with ice)

| Surface Area for One Antenna w/ Ice = | $\mathrm{SA}_{\text {ICEantF }}:=\frac{\left(\mathrm{L}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\mathrm{ant}}+2 \cdot \mathrm{t}_{\mathrm{i} \mathrm{z}}\right)}{144}=6.9$ | sf |
| :---: | :---: | :---: |
| Total Antenna Wind Force w/ Ice Front = | $\mathrm{Fi}_{\text {ant }}:=\mathrm{qZ} \mathrm{i}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca} \mathrm{antr} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA} \mathrm{IICEantF}=91$ | lbs |
| Surface Area for One Antenna w/ Ice = | $\text { SAICEants }:=\frac{\left(\mathrm{L}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {ant }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=2.9$ | sf |
| Total Antenna Wind Force w/ Ice Side = |  | lbs |

## Gravity Load (without ice)



Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on RRUS's

RRUS Data:

RRUS Model = RRUS Shape = RRUS Height = RRUS Width = RRUS Thickness = RRUS Weight = Number of RRUS's =

RRUS Aspect Ratio $=\quad \operatorname{Ar}_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.1$
RRUS Force Coefficient =

## Wind Load (without ice)

Surface Area for One RRUS
Total RRUS Wind Force =

Surface Area for One RRUS =
Total RRUS Wind Force =
Ericsson 4449 B71B12

| Flat |  |
| :--- | :--- |
| $L_{\text {RRUS }}:=14.9$ | in |
| $W_{\text {RRUS }}:=13.2$ | in |
| $T_{\text {RRUS }}:=10.4$ | in |
| $W_{\text {RRUS }}:=74$ | lbs |
| $N_{\text {RRUS }}:=1$ |  |
| Ar $_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.1$ |  |

$C a_{\text {RRUS }}=1.2$
$\mathrm{SA}_{\text {RRUSF }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{W}_{\text {RRUS }}}{144}=1.4 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSF }}=63 \mathrm{lbs}$
$\mathrm{SA}_{\text {RRUSS }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{T}_{\text {RRUS }}}{144}=1.1 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSS }}=50 \quad \mathrm{lbs}$

## Wind Load (with ice)

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =
$\mathrm{SA}_{\text {ICERRUSF }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=2.2 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA} \mathrm{I}_{\text {ICERRUSF }}=27 \quad \mathrm{lbs}$
$\mathrm{SA}_{\text {ICERRUSS }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=1.8 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ice}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICERRUSS }}=22 \quad \mathrm{lbs}$

## Gravity Load (without ice)

Weight of All RRUSs $=\quad W T_{\text {RRUS }} \cdot N_{\text {RRUS }}=74 \quad \mathrm{lbs}$
Gravity Loads (ice only)
Volume of Each RRUS $=\quad V_{\text {RRUS }}:=L_{\text {RRUS }} \cdot W_{\text {RRUS }} \cdot T_{\text {RRUS }}=2045 \quad c u$ in

Volume of Ice on Each RRUS
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)-\mathrm{V}_{\text {RRUS }}=2435$
cu in
Weight of Ice on Each RRUS $=\quad W_{\text {ICERrus }}:=\frac{V_{\text {ice }}}{1728} \cdot 1 d=79 \quad$ Ibs

Weight of Ice on All RRUSs =
$W_{\text {ICERRUS }} \cdot \mathrm{N}_{\text {RRUS }}=79$
lbs

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on RRUS's

RRUS Data:

RRUS Model = RRUS Shape RRUS Height = RRUS Width = RRUS Thickness = RRUS Weight = Number of RRUS's =

RRUS Aspect Ratio $=\quad \operatorname{Ar}_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.2$
RRUS Force Coefficient =

## Wind Load (without ice)

Surface Area for One RRUS
Total RRUS Wind Force =

Surface Area for One RRUS =
Total RRUS Wind Force =
Ericsson 4415 B66A

| Flat |  |
| :--- | :--- |
| $L_{\text {RRUS }}:=16.5$ | in |
| $W_{\text {RRUS }}:=13.4$ | in |
| $T_{\text {RRUS }}:=5.9$ | in |
| $W_{\text {RRUS }}:=47.40$ | lbs |
| $N_{\text {RRUS }}:=1$ |  |
| Ar RRUS $:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.2$ |  |

$C a_{\text {RRUS }}=1.2$
$\mathrm{SA}_{\text {RRUSF }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{W}_{\text {RRUS }}}{144}=1.5 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSF }}=71 \quad \mathrm{lbs}$
$\mathrm{SA}_{\text {RRUSS }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{T}_{\text {RRUS }}}{144}=0.7 \quad \mathrm{sf}$
$\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSS }}=31 \quad \mathrm{lbs}$

## Wind Load (with ice)

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =
$\mathrm{SA}_{\text {ICERRUSF }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{i} 2}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{i} 2}\right)}{144}=2.4 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{i}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot S \mathrm{I}_{\text {ICERRUSF }}=30 \quad \mathrm{lbs}$
$\mathrm{SA}_{\text {ICERRUSS }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=1.4 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICERRUSS }}=17 \quad \mathrm{lbs}$

## Gravity Load (without ice)

Weight of All RRUSs $=\quad W_{\text {RRUS }} \cdot N_{\text {RRUS }}=47 \quad$ lbs
Gravity Loads (ice only)
Volume of Each RRUS $=\quad V_{\text {RRUS }}:=L_{\text {RRUS }} \cdot W_{\text {RRUS }} \cdot T_{\text {RRUS }}=1304 \quad$ cu in

Volume of Ice on Each RRUS
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)-\mathrm{V}_{\text {RRUS }}=2053$
cu in
Weight of Ice on Each RRUS $=\quad W_{\text {ICERRUS }}:=\frac{V_{\text {ice }}}{1728} \cdot I d=67 \quad$ Ibs

Weight of Ice on All RRUSs =
$W_{\text {ICERRUS }} \cdot N_{\text {Rrus }}=67$
lbs

Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on RRUS's

RRUS Data:

RRUS Model = RRUS Shape RRUS Height RRUS Width RRUS Thickness = RRUS Weight = Number of RRUS's =

RRUS Aspect Ratio $=\quad A r_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.2$
RRUS Force Coefficient =

## Wind Load (without ice)

| Surface Area for One RRUS $=$ | $\mathrm{SA}_{\text {RRUSF }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{W}_{\text {RRUS }}}{144}=1.5$ | sf |
| ---: | :--- | ---: |
| Total RRUS Wind Force $=$ | $\mathrm{F}_{\text {RRUS }}:=\mathrm{qz} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSF }}=71$ | lbs |
| Surface Area for One RRUS $=$ | $\mathrm{SA}_{\text {RRUSS }}:=\frac{\mathrm{L}_{\text {RRUS }} \cdot \mathrm{T}_{\text {RRUS }}}{144}=0.7$ | sf |
| Total RRUS Wind Force $=$ | $\mathrm{F}_{\text {RRUS }}:=\mathrm{qZ} \cdot \mathrm{G}_{H} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {RRUSS }}=31$ | lbs |

## Wind Load (with ice)

Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice = Surface Area for One RRUS w/ Ice =

Total RRUS Wind Force w/ Ice =

Ericsson 4415 B25

| Flat |  |
| :--- | :--- |
| $L_{\text {RRUS }}:=16.5$ | in |
| $W_{\text {RRUS }}:=13.4$ | in |
| $T_{\text {RRUS }}:=5.9$ | in |
| $W_{\text {RRUS }}:=46$ | lb |
| $N_{\text {RRUS }}:=1$ |  |
| Ar $_{\text {RRUS }}:=\frac{L_{\text {RRUS }}}{W_{\text {RRUS }}}=1.2$ |  |

$C a_{\text {RRUS }}=1.2$
lbs
sf lbs
$\mathrm{SA}_{\text {ICERRUSF }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=2.4 \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ} \mathrm{Z}_{\mathrm{ie}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICERRUSF }}=30 \quad \mathrm{lbs}$
$\mathrm{SA}_{\text {ICERRUSS }}:=\frac{\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=1.4 \quad \mathrm{sf}$
$\mathrm{Fi}_{\text {RRUS }}:=\mathrm{qZ}_{\mathrm{i}_{\mathrm{ce}}} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca}_{\text {RRUS }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {ICERRUSS }}=17 \mathrm{lbs}$

## Gravity Load (without ice)

Weight of All RRUSs $=\quad W_{\text {RRUS }} \cdot N_{\text {RRUS }}=46 \quad$ lbs
Gravity Loads (ice only)
Volume of Each RRUS $=\quad V_{\text {RRUS }}:=L_{\text {RRUS }} \cdot W_{\text {RRUS }} \cdot T_{\text {RRUS }}=1304 \quad$ cu in

Volume of Ice on Each RRUS
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {RRUS }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)-\mathrm{V}_{\text {RRUS }}=2053$
cu in
Weight of Ice on Each RRUS $=\quad W_{\text {ICERRUS }}:=\frac{V_{\text {ice }}}{1728} \cdot I d=67 \quad$ Ibs

Weight of Ice on All RRUSs =
$W_{\text {ICERRUS }} \cdot N_{\text {RRUS }}=67$
lbs

Hamden, CT
Prepared by: F.J.P Checked by: C.A.G. Job No. 19027.14

## Development of Wind \& Ice Load on TMA's

## TMA Data:

TMA Model =
Ericsson KRY112 TMA
TMA Shape $=\quad$ Flat $\quad$ in $\quad$ (User Input)
TMA Height $=\quad L_{\text {TMA }}:=6.9 \quad$ in $\quad$ (User Input)
TMA Width $=\quad W_{\text {TMA }}:=6.1 \quad$ in $\quad$ (User Input)
TMA Thickness $=\quad \mathrm{T}_{\text {TMA }}:=2.8 \quad$ lbs (User Input)
TMA Weight $=\quad \mathrm{WT}_{\text {тмА }}:=11 \quad$ (User Input)
Number of TMA's $=\quad \mathrm{N}_{\text {TMA }}:=1 \quad$ (User Input)
TMA Aspect Ratio $=\quad \operatorname{Ar}_{\text {TMA }}:=\frac{\mathrm{L}_{\text {TMA }}}{\mathrm{W}_{\text {TMA }}}=1.1$
TMA Force Coefficient $=\quad$ Са тм $=1.2$

## Wind Load (without ice)

| Surface Area for One TMA $=$ | $\mathrm{SA}_{\text {TMAF }}:=\frac{\mathrm{L}_{\text {TMA }} \cdot \mathrm{W}_{\text {TMA }}}{144}=0.3$ | sf |
| ---: | :--- | :--- |
| Total TMA Wind Force $=$ | $\mathrm{F}_{\text {TMA }}:=\mathrm{qZ} \cdot \mathrm{G}_{H} \cdot \mathrm{Ca} \mathrm{a}_{\text {TMA }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {TMAF }}=13$ | lbs |
| Surface Area for One TMA $=$ | $\mathrm{SA}_{\text {TMAS }}:=\frac{\mathrm{L}_{\text {TMA }} \cdot \mathrm{T}_{\text {TMA }}}{144}=0.1$ | sf |
| Total TMA Wind Force $=$ | $\mathrm{F}_{\text {TMA }}:=\mathrm{qZ} \cdot \mathrm{G}_{H} \cdot \mathrm{Ca}_{\text {TMA }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA}_{\text {TMAS }}=6$ | lbs |

## Wind Load (with ice)

| Surface Area for One TMA w/ Ice = | $\mathrm{SA}_{\text {ICETMAF }}:=\frac{\left(\mathrm{L}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=0.7$ | sf |
| :---: | :---: | :---: |
| Total TMA Wind Force w/ Ice = | $\mathrm{Fi}_{\text {TMA }}:=\mathrm{qZ} \mathrm{i}_{\text {ce }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{C} \mathrm{a}_{\text {TMA }} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA} \mathrm{I}_{\text {ICETMAF }}=9$ | lbs |
| Surface Area for One TMA w/ Ice = | $\mathrm{SA}_{\text {ICETMAS }}:=\frac{\left(\mathrm{L}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right)}{144}=0.5$ | sf |
| Total TMA Wind Force w/ Ice = | $F \mathrm{i}_{\text {TMA }}:=\mathrm{qZ} \mathrm{i}_{\text {ice }} \cdot \mathrm{G}_{\mathrm{H}} \cdot \mathrm{Ca} \mathrm{TMA} \cdot \mathrm{K}_{\mathrm{a}} \cdot \mathrm{SA} \mathrm{ICETMAS}=6$ | bs |

## Gravity Load (without ice)

$$
\text { Weight of All TMAs }=\quad W T_{T M A} \cdot N_{T M A}=11
$$

## Gravity Loads (ice only)

Volume of Each TMA $=\quad \mathrm{V}_{\text {TMA }}:=\mathrm{L}_{\text {TMA }} \cdot \mathrm{W}_{\text {TMA }} \cdot \mathrm{T}_{\text {TMA }}=118 \quad$ cu in

Volume of Ice on Each TMA
$\mathrm{V}_{\text {ice }}:=\left(\mathrm{L}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{W}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iz}}\right) \cdot\left(\mathrm{T}_{\text {TMA }}+2 \cdot \mathrm{t}_{\mathrm{iZ}}\right)-\mathrm{V}_{\text {TMA }}=\underset{\mathrm{cu}}{571}$

Weight of Ice on Each TMA $=\quad W_{\text {ICETMA }}:=\frac{V_{\text {ice }}}{1728} \cdot I d=19 \quad$ lb

Weight of Ice on All TMAs $=\quad W_{\text {ICETMA }} \cdot N_{\text {TMA }}=19 \quad$ lbs


| Envelope only Solution |  |  |  |  |
| :--- | :--- | :--- | :---: | :---: |
| Centek |  |  |  |  |
| FJP | CT11474A_AMA | Member Framing |  |  |

Eqo rcp\｛＜Egpıgm
Crt＂46．＂423；
Fguk pgt＜HLR
Lqd＂Pwo dgt＜3；249036
Oqf gitPcog＜EV33696CaCOC

447＂RO
Ej gengf＂ $\mathrm{D}\{2 \mathrm{E} \mathrm{ECl}$

## （Global）Model Settings

| F kur re\｛＂Ugevqpu＂tat＂Ogo dgt＂Ecreu | 7＂ |
| :---: | :---: |
| Ocz＂｜bugtpcr゙Ugevqpu＂kqt＂Ogo dgt＂Ecreu | ；9＂ |
| Werwf g＂Uj gct＂F ghqto cvapA | ［ gu |
| Wetgcug＂Pckppi＂Ecr cek\｛＂hat＂Y kpf A | ［ gu |
| Kerwi g＂Y ctr lpi A | ［ gu |
|  | ［ gu |
| Ctgc＂Nqcf＂Oguj＂＊kp 4＋ | 366 |
| Ogti g＂Vqrgtcpeg＂＊p＋ | C34 |
| R／F gruc＂Cpcr\｛ uku＂Vargtcpeg | 202＇ |
| 1perwf g＂R／Fgnc＂lqt＂Y cmuA | ［ gu |
| Cmqo ckec nif＂Kgtcig＂UVłtpguu＂17qt＂Y cmuA | ［ gu |
| Ocz＂Kgtc＊qpu＂1pt＂Y cm＂U＊łtpguu | 5 |
| 1 tcxk\｛＂Ceegrgtcvap＂＊hNuge ${ }^{\text {4＋}}$ | 5404 |
| Y cm＇Oguj＂UK g＂＊p＋ | 34 |
| Gk gpuqrw＊qp＂Eqpxgti gpeg＂Vqı0＊30G／＋ | 6 |
| Xgtvecri＇Czku | ［ |
| I radcri＇Ogo dgt＂Qtlgpvevap＂Rrepg | Z |
| Uvcve＂Uqugt | Ur ctug＂Ceegrgtcugf |
| F \｛ pco le＂Uqixgt | Ceegrgtcugf＂Uqrxgt |
| J qV＇T qungf＂Uvggn＂Eqf g | CKE＂36i＊582／32＋セNT HF |
| Cf Inuv＂UvkipguuA | ［ gu＊Kgtckxg＋ |
| TKCEqppgevap＂Eqf g | CKE＂36i＊582／32＋ゼCUF |
| Eqri＂Hat o gf＂Urggr＇Eqf g | CKUKU322／32＜CUF |
| Y qqf＂Eqf g | CY E＂PF U／34＜゙CUF |
| Y qqf＂Vgo r gtcutg | ＞＂322H |
| Eqpetgıg＂Eqf g | CEK53：／33 |
| Ocuqpt\｛＂Eqf g | CEK752／332CUF |
| Crwo kowo＂Eqf g | CC＂CFO3／32＜＇CUF＂／＂Dwkf lpi |
| Uvclprguu＂Uvggn＇Eqf g | CKE＂36i＊＊582／32＋ゼCUF |
| Cf Imuv＂UlkhpguuA | ［ gu＊Kgtckkx ${ }^{\text {＋}}$ |
| Pwo dgt＂qh＇Uj gct＂T gi qqpu | 6 |
| T gi kqp＂Ur celpi＂1petgo gpv＊｜p＋ | 6 |
| DlczlcriEqrwo p＂Ogy qf | Gzcev＇lpogi tckqp |
| Rcto g＂Dgıc＂Hcevat＂＊REC＋ | 87 |
| Eqpetgug＂Uvguu＂Drqem | T gevcpi wret |
| Wug＂Etcengf＂UgevqpuA | ［ gu |
| Wug＂Etcengf＂Ugevapu＂Ura dA | ［ gu |
| Dcf＂Htco hpi＂Y ctplpi uA | Pq |
| Wpwugf＂Hqteg＂Y ctplpi uA | ［ gu |
| Olp＂3＂Dct＂F lco O＇Ur celpi A | Pq |
| Eqpetgrg＇Tgdct＂Ugv | T GDCT aUGVaCUVOC837 |
| Opo＂＂Uvggrntqt＂Eqıo p | 3 |
| Ocz＂’＂Ulgghhtht＂Eqrwo p |  |


| C=NT $=1$ | engineering | Eqo rcp\{ Fguk pgt | $\begin{aligned} & \text { < Egpvgm } \\ & \text { < HLR } \end{aligned}$ | $\begin{aligned} & \text { Crt"46."423; } \\ & 447 \mathrm{RO} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Centered on Solutions ${ }^{\text {m" }}$ | www.centekeng.com | Lqd"Pwo dgt | < 3; 249036 | Ej gengf "D $\lll \mathrm{ECl}$ |
| 63-2 North Branford Road Branford CT 06405 | P: (203) 488-0580 <br> F:(203) 488-8587 | Oqf gr'Pco g | < EV33696CaCOC |  |

(Global) Model Settings, Continued

| Ugko le"Eqf g | CUEG'9/32 |
| :---: | :---: |
| Ugko le"Dcug"Grgxc*app"*h* | Pqv'Gpıgtgf |
| Cf f "Dcug'Y gk j vA | [ gu |
| Ev゙Z | (2) |
| Evil | C24 |
| V'Z"*uge+ | Pqv'Gpugtgf |
| V"\ "*uge+ | Pqv'Gpugtgf |
| T"Z | 5 |
| T" | 5 |
| Ev゙Gzr OZ | Q7 |
| EviGzr O\ | (97 |
| UF3 | 3 |
| UFU | 3 |
| U3 | 3 |
| VN'*uge+ | 7 |
| Tkun'Ecv | Kqt"KK |
| Fthv'Ecv | Qẏ gt |
| Qo " | 3 |
| Qo "Z | 3 |
| Ef " | 3 |
| Ef "Z | 3 |
| Tj q" | 3 |
| Tj q'Z | 3 |

## Hot Rolled Steel Properties

|  | N ${ }^{\text {dgn }}$ | G"]muk | \| "]muk | Pw | Vj gto "*3G7"H+ | Fgpuk [ ]mill 5 | [ lgif ]mak | T\{ | Hw]muk | Tv |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | C58"I t058 | 4;222 | 33376 | (5) | ©87 | Cb; | 58 | 30 | 7: | 304 |
| 4 | C794"1 t072 | 4;222 | 33376 | 5 | C87 | C\%; | 72 | 3CB | 7: | 304 |
| 5 | C; ; 4 | 4;222 | 33376 | (5) | C87 | C\%; | 72 | 3CB | 7: | 304 |
| 6 | C722"I t064 | 4;222 | 33376 | (5) | 87 | Cb; | 64 | 35 | 7: | 3CB |
| 7 | C722'l t068 | 4;222 | 33376 | (5) | C87 | C6; | 68 | 304 | 7: | 3CB |
| 8 | C75"I tcf g"D | 4;222 | 33376 | Б5 | ©87 | Cb; | 57 | 30 | 7: | 304 |

Hot Rolled Steel Design Parameters

|  | N 6 dgn | Ujcrg N | Ngpi y ]h |  | $\mathrm{Nd} \mid \mathrm{l}$ ] h | Neqo r "var ]00 | Oneqo r "dqu 00 V vat smom | M \{ | M \| | Ed | Hapevem |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O3 | *G+'UVkt'Cto | 80: 5 |  |  | Nd\{ \{ |  |  |  |  | Nugtcn |
| 4 | O4 | *G+UN*H'Cto | 8®2:5 |  |  | Nd\{ \{ |  |  |  |  | Nevgten |
| 5 | O5 | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugio 0 |  |  |  | Nevgten |
| 6 | O6 | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugi o 0 |  |  |  | Nevgten |
| 7 | O7 | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugio 0 |  |  |  | Nevgtcn |
| 8 | O8 | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugi o m |  |  |  | Nevgten |
| 9 | O9 | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugio © |  |  |  | Nevgtcn |
| : | O: | *G+'J qt\| | 38 | Ugi o gpv | Ugi o gpv | Ugi o gpv | Ugi o gpv Ugi o © |  |  |  | Nevgten |
| ; | O; | *G+Cprgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgtcn |
| 32 | 032 | *G+Cprgppom | - 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgten |
| 33 | 033 | *G+Cprgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgtcn |
| 34 | O34 | *G+Cprgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgtcn |
| 35 | 035 | *G+Cprgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgtcn |
| 36 | O36 | *G+Cprgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgten |
| 37 | O37 | *G+Cpıgppom | 8 |  |  | Nd\{ \{ |  |  |  |  | Nevgtcn |



Hot Rolled Steel Design Parameters（Continued）


## Hot Rolled Steel Section Sets

| N ${ }^{\text {dgn }}$ |  | Uj cr g | V 2 rg | Fguki p＂Nuı | Ocigtlen |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | ＊G＋＇J qt｜ | RIRGa4\％ | Dgco | Rkg | C75＂l tcf g＂D | V\｛rlecn3683 367 366740； |
| 4 | ＊G＋＂Ukłh＇Cto | RIRGa4®2 | Dgco | Rkg | C75＂l tcf g＂D | V r recn3C24 8849 C849 3047 |
| 5 | ＊G＋Cpvgppc＂O cuv | RKRGa4®2 | Equmom | Rkg | C75＂l tcf g＂D | V rlecn3C24 C849 ©849 3047 |
| 6 | ＊R＋＂Ukth＇Cto | RKRGa3017 | Dgco | Rkg | C75＂I tcf g＂D | V rlecn（847 CB： 6 CB： 6 ¢็8： |

Member Primary Data

|  | N Cdgn | K－qhov | L＂Lqhov | M＇Lqıpv | Tqucıg＊gi＋ | Ugevap 1Uj crg | V 2 rg | Fguki p＂Nav | Ocruticn | Fguk p＂Twgu |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O3 | P7 | P8 |  |  | ＊G＋＂U＊łth＇Cto | Dgco | Rkg g | C75＂I tcf 00 | V r leen |
| 4 | O4 | P5； | P62 |  |  | ＊G＋＂U＊＊t＇Cto | Dgco | Rkg | C75＂I tcf 00 | V r reen |
| 5 | O5 | P3 | P4 |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V r lecn |
| 6 | O6 | P5 | P6 |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V \｛rlecn |
| 7 | O7 | P3； | P42 |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V 亿rlecn |
| 8 | O8 | P43 | P44 |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V r reen |
| 9 | O9 | P57 | P58 |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V r lecn |
| ： | O： | P59 | P5： |  |  | ＊G＋＇J qt｜ | Dgco | Rkg | C75＂I tcf 00 | V r reen |
| ； | O； | P： | P9 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rk g | C75＂I tcf 00 | V \｛rlecn |
| 32 | O32 | P34 | P33 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V $\{$ rlecn |
| 33 | 033 | P38 | P37 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V ［rlecn |
| 34 | O34 | P3： | P39 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V $\{$ rlecn |
| 35 | O35 | P46 | P45 |  | 82 | ＊G＋Cpıgppc＂Ocuv | Eqrwo p | Rk g | C75＂I tcf 00 | V $\{$ rlecn |
| 36 | O36 | P4： | P49 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V r reen |
| 37 | 037 | P54 | P53 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V \｛rlecn |
| 38 | 038 | P56 | P55 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V r reen |
| 39 | O39 | P64 | P63 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rk g | C75＂I tcf $0^{0}$ | V r reen |
| 3： | O3： | P68 | P67 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V $\{$ rlecn |
| 3； | O3； | P72 | P6； |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf 00 | V $\{$ r lecn |
| 42 | 042 | P74 | P73 |  | 82 | ＊G＋Cprgppc＂Ocuv | Eqrwo p | Rkg | C75＂I tcf $0^{0}$ | V $\{$ rlecn |
| 43 | O43 | P82 | P83 |  |  | ＊R＋＂U＊łt＇＇Cto | Dgco | Rk g | C75＂I tcf $\infty$ | V r reen |

Joint Coordinates and Temperatures

|  | Ncdgn | Z＂］h／ | ［＂］h／ | $\ \mathrm{l} \mathrm{l} \mathrm{h}$ | Vgo r＂］${ }_{\text {H }}$ | Fgucej＂Htqo＂Fkrj tci o |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | P3 | ：©236378 | 3 | 17ら429： | 2 |  |
| 4 | P4 | 190：7：66 | 3 | 17ら429： | 2 |  |
| 5 | P5 | ：©236378 | ／3 | ／7¢5429： | 2 |  |
| 6 | P6 | 190：7：66 | ／3 | ／7ら5429： | 2 |  |
| 7 | P7 | 70736378 | 3 | ／7らூ429： | 2 |  |
| 8 | P8 | 4074377 | 3 | 2®36；3； 8 | 2 |  |
| 9 | P9 | ：©36378 | 5 | ／7Б429： | 2 |  |

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Eqo rcp\｛
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Lqd＂Pwo dgt
Oqf gilPcog＜EV33696CaCOC

Crt＂46．＂423；
447＂RO
Ej gengf＂D\｛2ECI

Joint Coordinates and Temperatures（Continued）

|  | N 6 dgn | Z＂］h／ | ［＂］h／ | \＂ $\mathrm{h} / \mathrm{L}$ | Vgo r＂］H | Fgucej＂Htqo＂Ficrj tci o |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ： | $P$ ： | ：©36378 | 15 | 17ら429： | 2 |  |
| ； | P； | 5036378 | 3 | 17ら429： | 2 |  |
| 32 | P32 | 5036378 | ／3 | 17ら429： | 2 |  |
| 33 | P33 | 50736378 | 5 | ／7ら429： | 2 |  |
| 34 | P34 | 50736378 | 15 | 17ら429： | 2 |  |
| 35 | P35 | ／50 3； 399 | 3 | ／7ら429： | 2 |  |
| 36 | P36 | 150 3； 399 | ／3 | 17ら429： | 2 |  |
| 37 | P37 | ／50 3； 399 | 5 | ／7ら429： | 2 |  |
| 38 | P38 | ／50 3； 399 | ／5 | 17ら429： | 2 |  |
| 39 | P39 | ／90：7：66 | 5 | ／7ら429： | 2 |  |
| 3： | P3： | 190：7：66 | 15 | 17ら429： | 2 |  |
| 3； | P3； | ／：© 62328 | 3 | 1609；8855 | 2 |  |
| 42 | P42 | ／2622328 | 3 | ；C27； 995 | 2 |  |
| 43 | P43 | ／： 622328 | ／3 | 16ツ；8855 | 2 |  |
| 44 | P44 | ／2622328 | ／3 | ；©7； 995 | 2 |  |
| 45 | P45 | ／：©22328 | 5 | 16ツ；8855 | 2 |  |
| 46 | P46 | 1： 622328 | ／5 | 16ツ；8855 | 2 |  |
| 47 | P47 | ／7997328 | 3 | ／2047 | 2 |  |
| 48 | P48 | ／7097328 | ／3 | ／2047 | 2 |  |
| 49 | P49 | ／7997328 | 5 | ／2947 | 2 |  |
| 4： | P4： | ／7997328 | 15 | 1297 | 2 |  |
| 4； | P4； | ／50247328 | 3 | $6 \% 3536$ | 2 |  |
| 52 | P52 | 150477328 | 13 | $6 \square 3536$ | 2 |  |
| 53 | P53 | ／51247328 | 5 | 603536 | 2 |  |
| 54 | P54 | 150477328 | 15 | 603536 | 2 |  |
| 55 | P55 | ／2622328 | 5 | ；©27； 995 | 2 |  |
| 56 | P56 | ／2622328 | 15 | ；©27； 995 | 2 |  |
| 57 | P57 | 20399838 | 3 | ；C234345 | 2 |  |
| 58 | P58 | ：C399838 | 3 | ／60 664：5 | 2 |  |
| 59 | P59 | 2C399838 | ／3 | ；©334345 | 2 |  |
| 5： | P5： | ： C999838 | ／3 | ／60 664：5 | 2 |  |
| 5； | P5； | 2899838 | 3 | ：CB682；： | 2 |  |
| 62 | P62 | 14094： 743 | 3 | 5®2797 | 2 |  |
| 63 | P63 | 2®399838 | 5 | ；©234345 | 2 |  |
| 64 | P64 | 20399838 | 15 | ；C234345 | 2 |  |
| 65 | P65 | 4049838 | 3 | 696：；： 6 | 2 |  |
| 66 | P66 | 4049838 | 13 | 6916：；： 6 | 2 |  |
| 67 | P67 | 4049838 | 5 | 6016：；： 6 | 2 |  |
| 68 | P68 | 4049838 | ／5 | 6016：；： 6 | 2 |  |
| 69 | P69 | 7649838 | 3 | ／2C2： 3365 | 2 |  |
| 6： | P6： | 7649838 | 13 | ／2®2： 3365 | 2 |  |
| 6； | P6； | 7649838 | 5 | ／2C2： 3365 | 2 |  |
| 72 | P72 | 7649838 | 15 | 1202： 3365 | 2 |  |
| 73 | P73 | ：CB99838 | 5 | ／60 664：5 | 2 |  |
| 74 | P74 | ：©399838 | 15 | ／60 664：5 | 2 |  |
| 75 | P75 | ／2C347 | 2 | ／2ら8： 65 | 2 |  |
| 76 | P76 | ／2C374733 | 3 | 17ら429： | 2 |  |
| 77 | P77 | ／2CB74733 | ／3 | ／7ら429： | 2 |  |
| 78 | P78 | ／6622328 | 3 | 4®3579 | 2 |  |
| 79 | P79 | ／6622328 | ／3 | 4C35379 | 2 |  |
| 7： | P7： | 60399838 | 3 | 4®：5； 4 | 2 |  |
| 7； | P7； | 6®399838 | ／3 | 4C2：5； 4 | 2 |  |


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Joint Coordinates and Temperatures (Continued)

|  | Ncdgn | Z"]h/ | [ "]h_ | $\ \mathrm{l} \mathrm{l} \mathrm{h}$ | Vgo r"]H | Fgucej "Htqo "Flcrj tci o |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 82 | P82 | /9045565; | 3 | 14097; 29 | 2 |  |
| 83 | P83 | /3C387523 | 3 | /50427757 | 2 |  |

Joint Boundary Conditions

|  | Lqlov"Nedgn | Z"]milp | [ "]mill | \ "]nulp | Z"Tqugndhatcf_ | [ "Tqugmindtcf_ | \ "Tqugnhatt cf _ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | P8 | Tgcekqp | T gcekpp | Tgcekqp |  |  |  |
| 4 | P62 | Tgcekqp | T gcekpp | T gcekqp |  |  |  |
| 5 | P76 | Tgcekqp | Tgcekpp | Tgcekqp | Tgcekap | Tgcekap | Tgcevap |
| 6 | P77 | Tgcekqp | T gcekpp | T gcekqp | Tgcevqp | Tgcekqp | Tgcevap |
| 7 | P78 | Tgcekqp | Tgcekqp | Tgcekqp | Tgcekqp | Tgcekqp | Tgcevap |
| 8 | P79 | Tgcekqp | T gcekap | Tgcekap | Tgcevap | T gcekqp | T gcevap |
| 9 | P7: | Tgcekqp | T gcekpp | Tgcekqp | Tgcekqp | T gcekqp | Tgcevap |
| : | P7; | Tgcekqp | T gcekpp | T gcekqp | Tgcekqp | Tgcekqp | Tgcevap |
| , | P83 | T gcekqp | Tgcekpp | Tgcekqp |  |  |  |

Member Point Loads (BLC 2 : Equipment Weight)

|  | Ogo dgt"Nbdgn | Fig gevap | Oci plont g]mmhn | Naecvap]lv. |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | [ | /@43 | (97 |
| 4 | O38 | [ | /0243 | 7 |
| 5 | O34 | [ | /@43 | (97) |
| 6 | O34 | [ | /0243 | 7 |
| 7 | O42 | [ | /@23 | Q7 |
| 8 | O42 | [ | 10243 | 7 |
| 9 | O35 | [ | /089 | Q7 |
| : | O35 | [ | /089 | 7 |
| ; | O; | - | /0889 | 07 |
| 32 | O; | - | /0889 | 7 |
| 33 | O39 | [ | /089 | Q7 |
| 34 | O39 | [ | /089 | 7 |
| 35 | O38 | [ | /@69 | 40 |
| 36 | O34 | [ | /0269 | 40 |
| 37 | O42 | [ | /@69 | 40 |
| 38 | O35 |  | /0269 | 40 |
| 39 | O; |  | /@69 | 40 |
| 3: | O39 | [ | /0269 | 4\% |
| 3; | O38 | [ | /0296 | 607: 5 |
| 42 | O34 | [ | /0296 | 607:5 |
| 43 | O42 | [ | /0296 | 607:5 |

Member Point Loads (BLC 3 : Ice Weight)

|  | Ogo dgt"Ncdgn | Fitgevap | Oci plenf g]mmin_ | Naecvap]lv.' |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | [ | /®297 | (97) |
| 4 | O38 | [ | 10297 | 7 |
| 5 | O34 | [ | /@97 | 07 |
| 6 | O34 | [ | /0297 | 7 |
| 7 | O42 | [ | /0297 | 07 |
| 8 | O42 | [ | /0297 | 7 |
| 9 | O35 | [ | /0427 | 07 |


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## Member Point Loads（BLC 3 ：Ice Weight）（Continued）

|  | Ogo dgt＂Ncdgn | Flagevap | Oci plenf g］mmin＿ | Nqeckap］lv． |
| :---: | :---: | :---: | :---: | :---: |
| ： | O35 | ［ | 10427 | 7 |
| ； | O； | ［ | ／0427 | （97） |
| 32 | O； | ［ | 10427 | 7 |
| 33 | 039 | ［ | ／0427 | Q7 |
| 34 | O39 | ［ | 10427 | 7 |
| 35 | O38 | ［ | ／089 | 40 |
| 36 | O34 | ［ | ／0899 | 40 |
| 37 | O42 | ［ | ／0889 | 40 |
| 38 | O35 | ［ | ／0889 | 4\％ |
| 39 | O； | ［ | ／0889 | 40 |
| 3： | 039 |  | ／0889 | 4\％ |
| 3； | O38 |  | ／029； | 60： 5 |
| 42 | O34 |  | ／029； | 6\％：5 |
| 43 | O42 | ［ | ／029； | 607：5 |

## Member Point Loads（BLC 4 ：Wind w／Ice X）

|  | Ogo dgt＂Nedgn | Fitgevap | Oci plowi g］mmb | Naecvap］lv． |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | Z | ／C； 3 | 07 |
| 4 | O38 | Z | ／O； 3 | 7 |
| 5 | O34 | Z | ／®2： | Q7 |
| 6 | O34 | Z | ／Q23： | 7 |
| 7 | O42 | Z | ／＠； 3 | Q7 |
| 8 | O42 | Z | ／0； 3 | 7 |
| 9 | O35 | Z | ／＠2： | Q7 |
| ： | O35 | Z | ／032： | 7 |
| ； | O； | Z | ／＠7： | Q7 |
| 32 | O； | Z | ／＠27： | 7 |
| 33 | O39 | Z | ／＠2： | 07 |
| 34 | O39 | Z | ／032： | 7 |
| 35 | O38 | Z | ／025 | 48 |
| 36 | O34 | Z | ／0239 | 40 |
| 37 | O42 | Z | ／025 | 40 |
| 38 | 035 | Z | 1025 | 48 |
| 39 | O； | Z | ／0339 | 40 |
| 3： | 039 | Z | ／025 | 407 |
| 3； | O38 | Z | ／0249 | 607： 5 |
| 42 | O34 | Z | ／0244 | 6『7：5 |
| 43 | O42 | Z | ／＠49 | 6『7： 5 |

## Member Point Loads（BLC 5 ：Wind X）

|  | Ogo dgt＂Ncdgn | Fitgevap | Oci pkenf g］mmin＿ | Nqecklap］lv．＇ |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | Z | ／＠46 | Q7 |
| 4 | O38 | Z | ／0346 | 7 |
| 5 | O34 | Z | ／025 | Q7 |
| 6 | O34 | Z | ／025 | 7 |
| 7 | O42 | Z | ／0346 | 07 |
| 8 | O42 | Z | ／0346 | 7 |
| 9 | O35 | Z | ／054； | 07 |
| ： | O35 | Z | ／054； | 7 |
| ； | O； | Z | ／0367 | Q7 |
| 32 | O； | Z | ／0367 | 7 |


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## Member Point Loads (BLC 5 : Wind X) (Continued)

|  | Ogo dgt" lc dgn | Figevap | Oci pkan g]mmiv | Naeckap] $\mathbf{l}$. |
| :---: | :---: | :---: | :---: | :---: |
| 33 | O39 | Z | /054; | (97 |
| 34 | O39 | Z | /064; | 7 |
| 35 | O38 | Z | /®R93 | $4{ }^{7}$ |
| 36 | O34 | Z | /®53 | $4{ }^{4}$ |
| 37 | 042 | Z | /®293 | $4{ }^{4}$ |
| 38 | O35 | Z | /®293 | $4{ }^{4}$ |
| 39 | O; | Z | /®253 | $4{ }^{4}$ |
| 3: | O39 | Z | /0293 | $4{ }^{4}$ |
| 3 ; | O38 | Z | /@885 | 67: 5 |
| 42 | O34 | Z | 1087 | 60: 5 |
| 43 | 042 | Z | /@85 | 607:5 |

Member Point Loads (BLC 6 : Wind w/ Ice Z)

|  | Ogo dgt"NLdgn | Fitgevap | Oci phent g]mmin_ | Ngecklaplv.' |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | 1 | /@3: | © 7 |
| 4 | O38 | 1 | /®3: | 7 |
| 5 | O34 | 1 | /@; 3 | © 7 |
| 6 | O34 | 1 | /®; 3 | 7 |
| 7 | 042 | 1 | /@3: | (97 |
| 8 | 042 | 1 | /®3: | 7 |
| 9 | O35 | 1 | /@7: | (97 |
| : | O35 | 1 | /127: | 7 |
|  | O; | 1 | /032: | © 7 |
| 32 | O; | 1 | 1032 : | 7 |
| 33 | O39 | 1 | /@7: | © 7 |
| 34 | O39 | 1 | /@27: | 7 |
| 35 | O38 | 1 | /®39 | $4{ }^{1 / 8}$ |
| 36 | O34 | 1 | /R5 | $4{ }^{4}$ |
| 37 | 042 | 1 | /®39 | $4{ }^{4}$ |
| 38 | O35 | 1 | /Q239 | $4{ }^{4}$ |
| 39 | O; | 1 | /R5 | $4{ }^{4}$ |
| 3: | O39 | 1 | /®239 | $4{ }^{1}$ |
| 3; | O38 | 1 | /®44 | 607:5 |
| 42 | O34 | 1 | /®49 | 607:5 |
| 43 | 042 | 1 | /®44 | 6\%:5 |

## Member Point Loads (BLC 7: Wind Z)

|  | Ogo dgt"Ncdgn | Fitgevap | Oci pkenf g]mmin_ | Ngeckipp]lv.' |
| :---: | :---: | :---: | :---: | :---: |
| 3 | O38 | 1 | /025 | ©7 |
| 4 | O38 | 1 | /025 | 7 |
| 5 | O34 | 1 | /0346 | (97) |
| 6 | O34 | 1 | /0346 | 7 |
| 7 | O42 | 1 | /025 | (97) |
| 8 | O42 | 1 | /025 | 7 |
| 9 | O35 | 1 | /0367 | Q7 |
| : | 035 | 1 | /0367 | 7 |
| ; | O; | 1 | /054; | Q7 |
| 32 | O; | 1 | /054; | 7 |
| 33 | O39 | 1 | /0367 | (97) |
| 34 | O39 | 1 | /0367 | 7 |
| 35 | O38 | 1 | /0253 | 40 |


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Member Point Loads (BLC 7 : Wind Z) (Continued)

|  | Ogo dgt"Nとdgn | Fitgevap | Oci plenf g]mmin_ | Nqeckap]lv |
| :---: | :---: | :---: | :---: | :---: |
| 36 | O34 | 1 | /0293 | 40 |
| 37 | O42 | 1 | /@53 | 40 |
| 38 | O35 | 1 | /0253 | 40 |
| 39 | O; | 1 | /0293 | 40 |
| 3: | O39 | 1 | /0253 | 4\% |
| 3; | O38 | 1 | /@7 | 6\%:5 |
| 42 | O34 | 1 | /0285 | 6\%:5 |
| 43 | O42 | 1 | /@7 | 6\%:5 |

Joint Loads and Enforced Displacements
Lqłpv"Ncdgn
NF .O
Pq"Fcvc"vq"Rtpv"m

Fligevap Oci pkevi g]*mmht."* $\ddagger$

Member Distributed Loads (BLC 4 : Wind w/ Ice X)

|  | Ogo dgt"Nedgn | Flagevap | Uvctv"Oci pkewf g]mulv.H.muh | Gpf "Oci pkwf g]mlk.H.muh | Uuctv'Naecvap][v.' | Gpf 'Naec kqp]h.' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O7 | Z | /0224 | /0224 | 2 | 2 |
| 4 | O8 | Z | 10224 | /0224 | 2 | 2 |
| 5 | O9 | Z | /0224 | /0224 | 2 | 2 |
| 6 | O: | Z | /0224 | /0224 | 2 | 2 |
| 7 | O36 | Z | /024 | /024 | 2 | 2 |
| 8 | O37 | Z | /0224 | /024 | 2 | 2 |
| 9 | O3: | Z | /0224 | /024 | 2 | 2 |
| : | O3; | Z | /0224 | /0224 | 2 | 2 |
| , | O32 | Z | /0224 | /0224 | 2 | 2 |
| 32 | O33 | Z | 1024 | /0224 | 2 | 2 |
| 33 | O; | Z | /0224 | /024 | 2 | 2 |
| 34 | O34 | Z | /0224 | /0224 | 2 | 2 |
| 35 | O3 | Z | /0224 | /@24 | 2 | 2 |
| 36 | O4 | Z | /0224 | /0224 | 2 | 2 |

Member Distributed Loads (BLC 5 : Wind X)

|  | Ogo dgt"NEdgn | Fitgevap | Unctv'Oci pkexf g]ndlv.H.mun | Gpf "Oci pkwf g]milk.H.muh | Usctv'Nqecvapp]lv.' | Gpf "Nqee kap]h.' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O7 | Z | /@2: | /@2: | 2 | 2 |
| 4 | O8 | Z | /®22: | /®22: | 2 | 2 |
| 5 | O9 | Z | /®2: | /®2: | 2 | 2 |
| 6 | O: | Z | /®2: | /®22: | 2 | 2 |
| 7 | O36 | Z | /®2: | /®2: | 2 | 2 |
| 8 | O37 | Z | /022: | /®2: | 2 | 2 |
| 9 | O3: | Z | /®2: | /®2: | 2 | 2 |
| : | O3; | Z | /QR2: | /®2: | 2 | 2 |
| ; | O32 | Z | /®2: | /®2: | 2 | 2 |
| 32 | O33 | Z | /®22: | /®22: | 2 | 2 |
| 33 | O; | Z | /®2: | /®2: | 2 | 2 |
| 34 | O34 | Z | /®2: | /®2: | 2 | 2 |
| 35 | O3 | Z | /@28 | /028 | 2 | 2 |
| 36 | O4 | Z | /0228 | /0228 | 2 | 2 |


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## Member Distributed Loads（BLC 6 ：Wind w／Ice Z）

| Ogo dgt＂NLdgn | Fhgevap | Uketv＇Oci prexf g］niv．H．mun | Gpf＂Oci pkwf g］ndw．H．mu＿ |  | Gpf＇Nqec＊qp］ l ．＇ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| O5 | 1 | ／®224 | ／＠24 | 2 | 2 |
| 06 | 1 | ／®24 | ／®24 | 2 | 2 |
| O32 | 1 | ／＠24 | ／®24 | 2 | 2 |
| O33 | 1 | ／R24 | ／®24 | 2 | 2 |
| O36 | 1 | ／＠24 | ／＠24 | 2 | 2 |
| O37 | 1 | ／＠24 | ／®24 | 2 | 2 |
| O3： | 1 | ／®24 | ／®24 | 2 | 2 |
| O3； | 1 | ／R24 | ／®24 | 2 | 2 |
| O3 | 1 | ／®24 | ／®24 | 2 | 2 |
| O4 | 1 | ／®24 | ／®24 | 2 | 2 |
| 043 | 1 | ／®23 | ／＠23 | 2 | 2 |

Member Distributed Loads（BLC 7 ：Wind Z）

|  | Ogo dgt＂NLdgn | Figevap | Uctv＇Oci phent g］nlv．H．muh | Gpf＂Oci plewt g］nlw．H．muh | Unctv＇Naeckap］｜r．＇ | Gpf＇Ngec vapl．${ }^{\text {c }}$ ． |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O5 | 1 | ／®2： | ／＠2： | 2 | 2 |
| 4 | 06 | 1 | ／®22： | ／®2： | 2 | 2 |
| 5 | O32 | 1 | ／＠2： | ／＠2： | 2 | 2 |
| 6 | O33 | 1 | ／®2： | ／®2： | 2 | 2 |
| 7 | O36 | 1 | ／®2： | ／＠2： | 2 | 2 |
| 8 | O37 | 1 | ／®2： | 1®2： | 2 | 2 |
| 9 | O3： | 1 | ／®2： | ／＠2： | 2 | 2 |
| ： | O3； | 1 | 1®2： | $1 ® 22$ | 2 | 2 |
|  | O3 | 1 | ／®28 | ／®28 | 2 | 2 |
| 32 | 04 | 1 | 1 ／R28 | ／0228 | 2 | 2 |
| 33 | O43 | 1 | ／®27 | ／®27 | 2 | 2 |

## Basic Load Cases

|  | DNE＂F guetk vap | Ecrgi qt \｛ | Z＂I tom＂1 too | ＂I tomLqłp | Rqıpv | Fkuthom |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | Ugrti＇Y gkj v | Pqpg | ／3 |  |  |  |  |
| 4 | Gswk o gpvi＇gli jv | Pqpg |  |  | 43 |  |  |
| 5 | Keg＂Y gk j v | Pqpg |  |  | 43 |  |  |
| 6 | Y hpf＂y t＂leg＂Z | Pqpg |  |  | 43 | 36 |  |
| 7 | Y lpf＂Z | Pqpg |  |  | 43 | 36 |  |
| 8 | Y lpf＂y t＂｜eg＂｜ | Pqpg |  |  | 43 | 33 |  |
| 9 | Y lpf＂ | Pqpg |  |  | 43 | 33 |  |

## Load Combinations

|  | Fguetk vap | Uqıxg | ROD | UTO | DNE | HOODNE | Hcmob | ODO | OHCO | DC |  |  | com | OOH | cmom | $\mathrm{OH}_{\mathrm{Hc}} \mathrm{O}$ | ODOOH | HcOm | WHCOOL | IDOOHcOm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 304F＂－＂388Y＂XZ／f Hgevap＋ | ［ gu | ［ |  | 3 | 3004 | 304 | 7 | 308 |  |  |  |  |  |  |  |  |  |  |  |
| 4 | 20，F＂－＂308Y＂XZ／f Hgevap＋ | ［ gu |  |  | 3 | 04 | 0 | 7 | ЗС8 |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 304F＂－＂302FK－＂3＠Y к゙ZめD | ［ gu | ［ |  | 3 | 3004 | 304 | 5 | 3 | 6 | 3 |  |  |  |  |  |  |  |  |  |
| 6 | 304F＂－＂3CBY＂XZ／f Hgevap＋ | ［ gu | ［ |  | 3 | 3004 | 304 | 9 | 38 |  |  |  |  |  |  |  |  |  |  |  |
| 7 | 20，F＂－＂388Y＂X／f Hgevap＋ | ［ gu | ［ |  | 3 | Q 4 | 0 | 9 | 308 |  |  |  |  |  |  |  |  |  |  |  |
|  | 304F＂－＂3＠FK－＂3＠Y K゙Z＠ | ［ gu | ［ |  | 3 | 3004 | 304 | 5 | 3 | 8 | 3 |  |  |  |  |  |  |  |  |  |

## Envelope Joint Reactions

| Lqłpv |  |  | Z"]m | NE | [ "]m | NE | \"]m | NE | OZ"]man |  | O[ "]mbu | NE | O\ "]mbu | NE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | P8 | O cz | Q25 | 4 | C239 | 6 | 30; 6 | 6 | 2 | 8 | 2 | 8 | 2 | 8 |
| 4 |  | 0 lp | 10,77 | 6 | ¢3 | 4 | 2 | 4 | 2 | 3 | 2 | 3 | 2 | 3 |
| 5 | P62 | O cz | 03 ; | 3 | C234 | 8 | 3C387 | 3 | 2 | 8 | 2 | 8 | 2 | 8 |
| 6 |  | 0 lp | (26; | 8 | C229 | 4 | (29: | 8 | 2 | 3 | 2 | 3 | 2 | 3 |
| 7 | P76 | O cz | 08 | 7 | 0987 | 8 | C264 | 8 | 2 | 4 | 5099 | 7 | O: ; | 8 |
| 8 |  | 0 p | 10769 | 5 | 0486 | 4 | /@267 | 7 | /08: : | 6 | 2 | 4 | C244 | 4 |
| 9 | P77 | O cz | 034 | 5 | 065 | 5 | C677 | 7 | 2 | 4 | 4045 | 6 | Б5 | 5 |
| : |  | 0 lp | (2; 6 | 7 | 0495 | 7 | 2 | 5 | /0: 3 | 6 | 2 | 4 | (257 | 7 |
| ; | P78 | O Cz | ¢597 | 8 | Q87 | 8 | 863 | 8 | 523 | 3 | 5¢5: : | 4 | ¢637 | 4 |
| 32 |  | 0 lp | /034 | 4 | 6: : | 4 | /034; | 4 | /@43 | 7 | /0935 | 7 | /036: | 8 |
| 33 | P79 | O Cz | (8; 4 | 4 | Q5; | 5 | ธ553 | 7 | ¢568 | 3 | 30; 9 | 3 | 826 | 4 |
| 34 |  | 0 lp | 10487 | 8 | 0478 | 4 | /0665 | 5 | /029 | 7 | /0546 | 7 | 10377 | 8 |
| 35 | P7: | O cz | (9) 4 | 3 | 088 | 5 | C89: | 7 | /@73 | 7 | /@; | 8 | 9: 8 | 4 |
| 36 |  | 0 lp | 10894 | 7 | 677; | 7 | /3C23 | 3 | 10479 | 5 | 15033; | 4 | /0324 | 8 |
| 37 | P7; | O cz | 027 | 4 | 069 | 8 | ©6 | 8 | /0325 | 7 | /0335 | 8 | ©: 3 | 4 |
| 38 |  | 0 lp | 10555 | 8 | 6479 | 4 | /0394 | 4 | 104; | 3 | 1309 | 3 | /CR; 8 | 8 |
| 39 | P83 | O cz | 398: | 3 | C233 | 3 | Q76 | 6 | 2 | 8 | 2 | 8 | 2 | 8 |
| 3: |  | 0 lp | /066 | 6 | C227 | 7 | /0347 | 3 | 2 | 3 | 2 | 3 | 2 | 3 |
| 3; | Vqucru< | O cz | 7075 | 4 | 687 | 8 | 655 | 7 |  |  |  |  |  |  |
| 42 |  | 0 lp | 2 | 6 | 3893 | 4 | 2 | 3 |  |  |  |  |  |  |

## Envelope Joint Displacements

| Lqłp |  |  | $\begin{aligned} & \text { Z"l\|p } \\ & \text { C226 } \end{aligned}$ | NE5 | $\begin{aligned} & \text { [ "]lp- } \\ & \text { /@37: } \end{aligned}$ | $\begin{gathered} \mathrm{NE} \\ 7 \end{gathered}$ | $\begin{aligned} & \backslash \mathrm{llp} \\ & \text { C224 } \end{aligned}$ | NE5 | Z"Tquckap"000NE |  | [ "Tqucuapp"]cone |  | \ "Tqucvap"]OONE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | P3 | ocz |  |  |  |  |  |  | $3068 \mathrm{~g} / 24$ | 6 | 4644g/24 | 7 |  |  |
| 4 |  | 0 p | 2 | 7 | /077; | 5 | 10847 | 7 | : 0 83g/29 | 4 | /40, 26g/27 | 5 | /565; ; g/25 | 8 |
| 5 | P4 | O cz | 2 | 7 | /035 | 7 | 2 | 5 | 2 | 5 | 2 | 5 | 4¢43g/25 | 5 |
| 6 |  | 0 p | /0R25 | 5 | /0583 | 5 | 14043 | 7 | /4@: 5g/25 | 7 | /60789g/24 | 7 | $9035 \mathrm{~g} / 26$ | 7 |
| 7 | P5 | O cz | /@23 | 7 | /@37: | 7 | C224 | 5 | 48894g/24 | 6 | 40135g/24 | 6 | /: 0988g/26 | 7 |
| 8 |  | O po | /®26 | 5 | /077; | 5 | /30123 | 6 | : $074 \mathrm{~g} / 29$ | 4 | /50263g/27 | 5 | /508: g/25 | 5 |
| 9 | P6 | O cz | [225 | 8 | /035 | 7 | 2 | 5 | 30174g/25 | 6 | 2 | 5 |  | 8 |
| : |  | 0 p | 2 | 4 | /0583 | 5 | 1403 | 6 | 2 | 3 | /60779g/24 | 6 | 7Ф9:; g/26 | 4 |
| ; | P7 | O cz | (225 | 5 | /0327 | 7 | C223 | 5 | 36: $7 \mathrm{~g} / 24$ | 6 | 30455g/24 | 7 | /40453g/25 | 7 |
| 32 |  | 0 p | 2 | 7 | /0584 | 5 | /022: | 7 | 91229g/29 | 4 | /50888g/27 | 5 | I: $0427 \mathrm{~g} / 25$ | 5 |
| 33 | P8 | O cz | 2 | 8 | 2 | 8 | 2 | 8 | 4CB84g/25 | 7 | : $8868 \mathrm{~g} / 26$ | 4 | /4Q 37g/25 | 4 |
| 34 |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | /30795g/25 | 5 | $56858 \mathrm{~g} / 27$ | 8 | /3@34g/24 | 8 |
| 35 | P9 | O cz | © 217 | 8 | /037: | 7 | C225 | 5 | 307:9g/24 | 6 | 46644g/24 | 7 | 3016; g/25 | 4 |
| 36 |  | 0 p | 10247 | 4 | /078 | 5 | 10457 | 7 | : 0 89g/29 | 4 | /4Q, 26g/27 | 5 | /5062; g/25 | 8 |
| 37 | P: | O cz | /@44 | 7 | /@7: | 7 | Q24 | 5 | 5098g/24 | 6 | 40135g/24 | 6 | /: ©8g/26 | 7 |
| 38 |  | 0 p | /0323 | 5 | /078 | 5 | 13043 | 6 | : 0 68g/29 | 4 | /5@263g/27 | 5 | /60475g/25 | 3 |
| 39 | P; | O Cz | (224 | 5 | /027: | 7 | CB2; | 6 | 3CB; 7g/24 | 6 | 4CB7: g/26 | 7 | /36548g/25 | 7 |
| 3: |  | 0 p | 2 | 7 | /03; 4 | 5 | 2 | 4 | 7666g/29 | 4 | /409; 6g/27 | 5 | /60885g/25 | 5 |
| 3; | P32 | O cz | 2 | 7 | /@7: | 7 | 2 | 5 | 362; g/24 | 6 | 3¢26g/24 | 6 | /3046: g/25 | 4 |
| 42 |  | 0 p | /0R25 | 5 | /03; 4 | 5 | 1045 | 6 | 7664g/29 | 4 | /4W5; ; g/27 | 5 | /607; 3g/25 | 8 |
| 43 | P33 | O cz | C336 | 5 | /@7: | 7 | (5) 5 | 6 | 3CB9: g/24 | 6 | 4C37: g/26 | 7 | /36548g/25 | 7 |
| 44 |  | 0 p | ¢253 | 7 | /03; 4 | 5 | 2 | 4 | 7666g/29 | 4 | /409; 6g/27 | 5 | /60858g/25 | 5 |
| 45 | P34 | O cz | /@25 | 7 | /@7: | 7 | 2 | 5 | 3648g/24 | 6 | 3¢26g/24 | 6 | /3636g/25 | 7 |
| 46 |  | 0 p | /0335 | 5 | /03; 4 | 5 | 10793 | 6 | 7663g/29 | 4 | 146; ; g/27 | 5 | /68827g/25 | 5 |
| 47 | P35 | O cz | 2 | 7 | /0274 | 7 | 2 | 5 | 2 | 5 | 2 | 5 | 501g/25 | 8 |
| 48 |  | - p | /0R24 | 5 | /0359 | 8 | 10.54 | 7 | /90974g/26 | 7 | /5689g/24 | 7 | 3CB7; g/25 | 4 |

＜Egpvgm
＜HLR
＜3；249036
＜EV33696CaCOC

Crt＂46．＂423；
4\＆47＂RO
Ej gengf＂D $\{2 \mathrm{ECl}$

Envelope Joint Displacements（Continued）

|  | Lqłpv |  | $\begin{aligned} & \mathrm{z}^{\prime \prime\|l\|}-1 \\ & \text { CR24 } \end{aligned}$ | $\begin{gathered} \mathrm{NE} \\ 8 \end{gathered}$ |  | NE7 | $\underset{2}{\mid 11 p}$ | NE5 | z＂Tqu＊ap＂］00Ne |  | ［＂Tacuap＂］mone |  | \＂Tquckqp＂］ 100 <br> 5434g／25 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 49 | P36 | o cz |  |  |  |  |  |  | 5675g／26 | 6 | 2 | 5 |  |  |
| 4： |  | 0 p | 2 | 4 | 10359 | 8 | 104： | 6 | 2 | 3 | ／5676g／24 | 6 | 31387g／25 | 7 |
| 4； | P37 | 0 cz | ／＠4； | 7 | ／®74 | 7 | 2 | 5 | 2 | 5 | 2 | 5 | 543；g／25 |  |
| 52 |  | 0 ¢ | 1029； | 5 | 10359 | 8 | 10.75 | 7 | 1：0 5：g／26 | 7 | 156589g／24 | 7 | 31387g／25 |  |
| 53 | P38 | o cz | C29； | 8 | ／＠274 | 7 | 2 | 5 | 7CB5：g／26 | 6 | 2 | 5 | 504g／25 | 8 |
| 54 |  | 0 ¢p | （248 | 4 | 10359 | 8 | 10．5； | 6 |  | 3 | 156576g／24 | 6 | 3c246g／25 |  |
| 55 | P39 | 0 cz | ／®4 | 7 | 1035 | 7 | 2 | 5 | 2 | 5 | 2 | 5 | 4『：7g／25 |  |
| 56 |  | 0 p | 1086 | 5 | 10583 | 5 | 140；9 | 7 | 15c559g／25 | 7 | 160789g／24 | 7 | $904 \mathrm{~g} / 26$ |  |
| 57 | P3： | 0 cz | Q27： | 8 | 1035 | 7 | 2 | 5 | 4ツ：8g／25 | 6 | 2 | 5 | 4Б2：g／25 |  |
| 58 |  | 0 p | C226 | 4 | 10583 | 5 | 1408 ； | 6 | － | 3 | 160779g／24 | 6 | 50 33g／27 |  |
| 59 | P3； | 0 cz | C27 | 7 | ／0386 | 4 | 967 | 4 | 4C688g／26 | 7 | 30 ；g／24 | 4 | 6C378g／25 |  |
| 5： |  | 0 p | 10646 | 4 | 108 | 8 | ／＠85 | 6 | ／； $0644 \mathrm{~g} / 25$ | 3 | 160 65g／25 | 6 | 1303；3g／24 |  |
| 5； | P42 | o cz | C685 | 7 | ／0376 | 7 | 3679 | 7 | 46665g／25 | 5 | ：CB：7g／25 | 7 | 36665g／25 |  |
| 62 |  | 0 ¢ | 1467 | 4 | 1065 ； | 5 | 10489 | 7 | 34；： $\mathrm{g} / 26$ | 7 | 160387g／24 | 4 | 130723g／25 |  |
| 63 | P43 | 0 cz | O2： | 6 | 10386 | 4 | ¢6： 7 | 3 | 40：；g／25 | 7 | 3093g／24 | 3 | 60：8g／25 |  |
| 64 |  | 0 p | 106 | 3 | 108 | 8 | 1033； | 7 | 136346g／24 | 3 | ／6 $6569 \mathrm{~g} / 25$ | 6 | 130，54g／24 |  |
| 65 | P44 | 0 cz | C66； | 7 | ／0376 | 7 | 3¢573 | 3 | 4629g／25 | 8 | ：C279g／25 | 6 | l：©；7g／26 |  |
| 66 |  | 0 ¢ | 14655 | 3 | 1065； | 5 | 10483 | 6 | 8（564g／26 | 4 | 16037： $\mathrm{g} / 24$ | 3 | 140444g／25 |  |
| 67 | P45 | 0 cz | CR2； | 7 | ／0386 | 4 | （248 | 4 | ／；®84g／26 | 7 | $30 ; \mathrm{g} / 24$ | 4 | 6CB8g／25 |  |
| 68 |  | 0 p | 103； 7 | 3 | 10823 | 8 | MR； 9 | 8 | ／；C65g／25 | 3 | 160 65g／25 | 6 | ／；©28g／25 |  |
| 69 | P46 | ocz | ¢549 | 6 | 10386 | 4 | （977 | 3 | 6ந5：9g／25 | 7 | $3093 \mathrm{~g} / 24$ | 3 | 60：3g／25 |  |
| 6： |  | 0 p | ／3¢5： 4 | 4 | 10823 | 8 | 10438 | 7 | ／36345g／24 | 3 | 16¢569g／25 | 6 | 14C559g／24 |  |
| 6； | P47 | 0 cz | C285 | 4 | ／®55 | 4 | C22： | 7 | 14046；g／26 | 7 | 6С6：；g／26 | 7 | 4 $7 \mathrm{~g} / 25$ |  |
| 72 |  | 0 p | 10238 | 6 | 1033 | 8 | ／R59 | 3 | 166889g／25 | 3 | 130 84g／25 | 3 | 170197g／25 |  |
| 73 | P48 | 0 cz | C247 | 6 | ／＠55 | 4 | （28 | 3 | $136655 \mathrm{~g} / 26$ | 7 | 8ツ5：g／25 | 3 | 4C879g／25 | 6 |
| 74 |  | Op | 10325 | 4 | 1033 | 8 | ／＠26 | 7 | 170894g／25 | 3 | 130864g／25 | 6 | 1806：7g／25 |  |
| 75 | P49 | o cz | CB： 8 | 4 | ／＠255 | 4 | 2 | 7 | ／50 57g／26 | 7 | 6С6：；g／26 | 7 | 4 $7 \mathrm{~g} / 25$ | 8 |
| 76 |  | 0 p | ／®8： | 6 | 1033 | 8 | 1036； | 3 | 166889g／25 | 3 | 130 84g／25 | 3 | 170329g／25 |  |
| 77 | P4： | 0 cz | C2： | 6 | ／®255 | 4 | CB； 8 | 3 | 4ه743g／27 | 7 | 8095： $\mathrm{g} / 25$ | 3 | 4C879g／25 |  |
| 78 |  | 0 ¢ | 10484 | 4 | 1033 | 8 | ／®36 | 7 | 170894g／25 | 3 | ／30864g／25 | 6 | 188875g／25 |  |
| 79 | P4； | o cz | C298 | 6 | ／025 | 7 | 044 | 3 | $4027 \mathrm{~g} / 25$ | 5 | $6055 \mathrm{~g} / 25$ | 7 | ／30833g／26 |  |
| 7： |  | 0 ¢p | 105： 3 | 4 | ／＠： 3 | 5 | ／R65 | 7 | ： $0969 \mathrm{~g} / 26$ | 7 | ／40677g／24 | 4 | ／30854g／25 |  |
| 7； | P52 | ocz | C294 | 7 |  | 7 | 643： | 4 | 4 （946g／25 | 8 | 66899g／25 | 6 | 18063；g／26 |  |
| 82 |  | 0 p | ／069； | 3 | ／＠： 3 | 5 | ／®64 | 6 | ：©63；g／26 | 4 | $146667 \mathrm{~g} / 24$ | 3 | 130955g／25 |  |
| 83 | P53 | ocz | CB | 6 | ／Q25 | 7 | 047； | 3 | $4027 \mathrm{~g} / 25$ | 5 | $6055 \mathrm{~g} / 25$ | 7 | 140763g／28 |  |
| 84 |  | 0 p | 105： | 4 | ／＠： 3 | 5 | $1 \ll 48$ | 7 | 80：；g／26 | 7 | 146677g／24 | 4 | ／38854g／25 |  |
| 85 | P54 | 0 cz | C279 | 7 | ／＠5 | 7 | CB； | 4 | 4ツ74g／25 | 8 | 68899g／25 | 6 | 18063；g／26 |  |
| 86 |  | 0 p | 10628 | 3 | I®： 3 | 5 | I®： 3 | 8 | ：©63：g／26 | 4 | $140667 \mathrm{~g} / 24$ | 3 | ／3088／25 |  |
| 87 | P55 | 0 cz | ¢； 5 | 6 | 10376 | 7 | 35； 8 | 3 | 4C66；g／25 | 5 | ：CB： $7 \mathrm{~g} / 25$ | 7 | 4ه；9g／25 |  |
| 88 |  | 0 ¢p | 1462； | 4 | 1065 ； | 5 | 10494 | 7 | ／40649g／26 | 7 | 160387g／24 | 4 | 130727g／25 |  |
| 89 | P56 | 0 cz | C64； | 7 | 10376 | 7 | 3¢57 | 4 | 4076：g／25 | 8 | ：© P79g／25 | 6 | I：© 6 ； $5 \mathrm{~g} / 26$ |  |
| 8： |  | 0 p | 14638 | 3 | 1065； | 5 | 104； 5 | 6 | 856g／26 | 4 | 16087：g／24 | 3 | 15676g／25 | 3 |
| 8； | P57 | ocz | ／＠2； | 8 | ／＠： 6 | 4 | ／®23 | 8 | ； $\mathbb{F} 54 \mathrm{~g} / 25$ | 3 | 170，39g／26 | 8 | 3C28：g／25 | 8 |
| 92 |  | 0 ¢p | I®®； 3 | 3 | 10863 | 8 | ／®26： | 4 | 4C283g／25 | 7 | 1： $8369 / 25$ | 3 | 13C38；$/ 24$ |  |
| 93 | P58 | 0 cz | 10369 | 8 | ／0386 | 4 | ／＠：： | 8 | ／36837g／25 | 4 | 6C377g／24 | 4 | 3665；g／25 |  |
| 94 |  | 0 p | 14ら66 | 4 | 10885 | 5 | 13¢576 | 4 | ／4C859g／25 | 8 | $41867 \mathrm{~g} / 25$ | 8 | 1304： $6 \mathrm{~g} / 25$ | 8 |
| 95 | P59 | ocz | ／C254 | 8 | ／03： 6 | 4 | ／＠245 | 8 | 3CB57g／24 | 3 | 180865g／26 | 8 | ： 0 83g／26 | 8 |
| 96 |  | 0 p | 10729 | 3 | 10863 | 8 | 104； 5 | 3 | 6历528g／25 | 8 | 1：095g／25 | 3 | 13Q 38g／24 |  |
| 97 | P5： | 0 cz | 10369 | 8 | 10386 | 4 | ／＠： 4 | 8 | 188895／26 | 4 | 6C36：g／24 | 3 | ／36336g／26 |  |
| 98 |  | 0 p | 14ら58 | 3 | 10885 | 5 | ／3¢569 | 3 | $146626 \mathrm{~g} / 25$ | 8 | $46845 \mathrm{~g} / 25$ | 8 | 14099； $\mathrm{g} / 25$ |  |
| 99 | P5； | 0 cz | ／＠24 | 7 | 10377 | 4 | （224 | 8 | ；9077g／25 | 3 | 160796g／26 | 8 | 5¢P： $8 \mathrm{~g} / 25$ |  |
| 9： |  | 0 p | ／0229 | 3 | 10793 | 8 | 2 | 4 | 5（B9g／25 | 7 | 18073g／25 | 3 | 1；09； $9 / 25$ |  |


| Lqłov |  |  | $\begin{gathered} Z^{\prime \prime}\| \| p_{-} \\ 2 \end{gathered}$ | NE8 | [ "llo | NE8 | $\backslash$ | NE8 | z"Tquikap" 100 NE$30264 \mathrm{~g} / 248$ |  | [ "Tquakap"Imone |  | \ "Tquckqp"]CONE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9; | P62 | 0 cz |  |  |  |  |  |  |  |  | 70446g/26 | 7 | 90777g/26 | 8 |
| :2 |  | 0 p | 2 | 3 | 2 |  | 2 | 3 | 301:3g/26 |  | 1: $026 \mathrm{~g} / 26$ | 3 | 160353g/25 | 4 |
| : 3 | P63 | 0 cz | C359 | 4 | /OB: 6 | 4 | CB: 3 | 3 | (\%63g/25 |  | 170 39g/26 | 8 | 3C293g/25 | 8 |
| : 4 |  | 0 lp | /®57 | 8 | /0863 | 8 | (236 | 7 | (2) $5 \mathrm{~g} / 26$ | 7 | 1: $8369 / 25$ | 3 | 1; @: : $\mathrm{g} / 25$ | 4 |
| : 5 | P64 | 0 cz | /®33 | 8 | /03: 6 | 4 | /0356 | 8 | $3 C B 56 \mathrm{~g} / 24$ | 3 | 180365g/26 | 8 | : 0 58g/26 | 8 |
| : 6 |  | 0 lp | /3C267 | 4 | 10863 | 8 | 10787 | 3 | 60159g/25 | 8 | 1: 095g/25 | 3 | 146544g/24 | 4 |
| : 7 | P65 | 0 cz | C253 | 4 | /®4; | 4 | C24 | 3 | 6C36: $\mathrm{g} / 25$ | 5 | 35588g/25 | 4 | $3023 \mathrm{~g} / 25$ | 8 |
| : 8 |  | 0 lp | C223 | 8 | /®R; 6 | 8 | (225 | 8 | $30949 \mathrm{~g} / 25$ | 7 | : CB73g/27 | 8 | /5C563g/25 | 4 |
| : 9 | P66 | 0 cz | /@26 | 8 | /®4; | 4 | /®26 | 8 | 6079: g/25 | 3 | /4099g/26 | 8 | 3Ф; 5g/25 | 8 |
| : |  | 0 ¢p | /®295 | 4 | /®2; 6 | 8 | 10264 | 3 | 3ツ; $4 \mathrm{~g} / 25$ | 7 | 16076;9/25 | 3 | 160699g/25 | 4 |
|  | P67 | 0 cz | C32: | 4 | /@4; | 4 | C329 | 3 | 6C36: g/25 | 5 | 3658g/25 | 4 | $3023 \mathrm{~g} / 25$ | 8 |
| ; 2 |  | 0 ¢ | /®66 | 8 | /®2; 6 | 8 | C265 | 7 | 367: g/25 | 7 | : CB73g/27 | 8 | 150395g/25 | 4 |
| ; 3 | P68 | 0 cz | Q25; | 8 | /®4; | 4 | /®279 | 7 | 60799g/25 | 3 | 14099g/26 | 8 | $3 \oplus ; 5 \mathrm{~g} / 25$ | 8 |
| ; 4 |  | 0 p | 103: 5 | 4 | /®; 6 | 8 | 10374 | 3 | $3083 \mathrm{~g} / 25$ | 7 | 16076; $\mathrm{g} / 25$ | 3 | /68868g/25 | 4 |
| 5 | P69 | ocz | /®3; | 8 | /®48 | 4 | /®235 | 8 | /30334g/25 | 7 | 40195g/24 | 4 | /30; ; $9 / 26$ | 4 |
| ; 6 |  | 0 ¢ | 1033: | 4 | /®8; | 5 | 103: 6 | 3 | 140976g/25 | 5 | $36646 \mathrm{~g} / 25$ | 8 | 130723g/25 | 8 |
| ; 7 | P6: | 0 cz | /®4 | 8 | /@48 | 4 | $1 ® 3$ | 8 | 1: ©529g/26 | 4 | $40485 \mathrm{~g} / 24$ | 3 | 17®3: 6g/26 | 7 |
| ; 8 |  | 0 p | 10539 | 3 | /®8; | 5 | 103: 4 | 4 | 1408; 5g/25 | 8 | 36; $7 \mathrm{~g} / 25$ | 8 | /308; 3g/25 | 5 |
| 9 | P6; | 0 cz | C239 | 8 | /@48 | 4 | $1 ® 88$ | 7 | /3017g/25 | 4 | 40495g/24 | 4 | /40356g/27 | 4 |
| ; : |  | 0 p | 10639 | 4 | /®8; | 5 | 10444 | 3 | $140076 \mathrm{~g} / 25$ | 5 | 36646g/25 | 8 | 130723g/25 | 8 |
|  | P72 | 0 cz | /@79 | 8 | /@48 | 4 | (276 | 8 | 1: ©528g/26 | 4 | $40485 \mathrm{~g} / 24$ | 3 | 17®3: 5g/26 | 7 |
| 322 |  | 0 p | 10665 | 3 | /®8; | 5 | 10384 | 4 | 140887g/25 | 8 | 3¢丅; 7g/25 | 8 | 13003; $\mathrm{g} / 25$ | 5 |
| 323 | P73 | 0 cz | 10338 | 8 | 10386 | 4 | 10376 | 8 | /30639g/25 | 4 | 6C377g/24 | 4 | 4 $/ 75 \mathrm{~g} / 25$ | 4 |
| 324 |  | - p | 14624 | 4 | 10685 | 5 | /3¢5; 5 | 3 | 140995g/25 | 8 | $46867 \mathrm{~g} / 25$ |  | 1304: :9/25 | 8 |
| 325 | P74 | 0 cz | $103:$ | 8 | /0386 | 4 | /®249 | 8 | 17@779/26 | 7 | 6C36: g/24 | 3 | /30336g/26 | 7 |
| 326 |  | 0 p | 14633 | 3 | 10685 | 5 | /3¢553 | 4 | 14047; g/25 | 8 | $48845 \mathrm{~g} / 25$ | 8 | 15¢\%; 5g/25 | 3 |
| 327 | P75 | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 328 |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 |
| 329 | P76 | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 32: |  | 0 ¢p | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 |  |
| 32; | P77 | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 332 |  | Op | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 |  |
| 333 | P78 | o cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 334 |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 |
| 335 | P79 | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 336 |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 |  |
| 337 | P7: | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 338 |  | 0 ¢ | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 |
| 339 | P7; | o cz | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 |
| 33: |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 | 2 | 3 |
| 33; | P82 | 0 cz | C224 | 7 | 103 | 4 | C227 | 4 | 1: ©3779/26 | 7 | 30293g/24 | 4 | 756: g/25 | 8 |
| 342 |  | 0 p | /@2; | 3 | /06; 4 | 8 | $1 ® 26$ | 8 | /; ¢; 3g/25 | 5 | 14C87; $\mathrm{g} / 25$ | 6 | 1: $0688 \mathrm{~g} / 25$ | 4 |
| 343 | P83 | 0 cz | 2 | 8 | 2 | 8 | 2 | 8 | /; ©: 4g/26 | 7 | 8C28; g/27 | 4 | $8045 \mathrm{~g} / 25$ | 5 |
| 344 |  | 0 p | 2 | 3 | 2 | 3 | 2 | 3 | I; ৫; 6g/25 | 5 | /4063: $\mathrm{g} / 25$ | 6 | 4C34; g/25 | 7 |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

|  | Og@o |  | Eqf g "EOCNqemone |  | Uj gct"EConkajh_ |  | FH |  | rj kRpm | - kROO | j kOp0 | 00 | Ed | Gsp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | O3 | RKRGa4C2 | C26; | 5000 6 | C225 | 8С2: 5 |  | 3 | $42 \mathrm{CB38}$ | 54035 | 3094 | 3094 | 3CB58 | J 3/3d |
| 4 | O4 | RKRGa4®2 | C88; | 802003 | C225 | 8С2:5 |  | 3 | $42 C 338$ | 54035 | 3094 | 3094 | 3CB58 | J 3/3d, |
| 5 | O5 | RKRGa4® | 025 | @@0 6 | O; 3 | 6\% |  | 6 | 670653 | 720937 | 50; 8 | 507; 8 | 40429 | J 5/8 |

C三NT三Kengineering
Centered on Solutions ${ }^{\text {s＂}}$ www．centekeng．com $\begin{array}{ll}\text { 63－2 North Branford Road } & \text { P：（203）488－0580 } \\ \text { Branford，CT 06405 } & \text { F：（203）488－8587 }\end{array}$

Eqo rcp\｛＜Egpıgm
Fgukipgt＜HLR
Lqd＂Pwo dgt＜3； 249036
Oqf griPcog＜EV33696CaCOC

Crt＂46．＂423；
4\＆7＂RO
Ej gengf＂ $\mathrm{D}\{2 \mathrm{E} \mathrm{ECl}$

Envelope AISC 14th（360－10）：LRFD Steel Code Checks（Continued）

|  | Ogø | Uj cr g | Eqf g＂EONVqeOONE |  | Uj gct＂EComadilv＿ |  | FH |  | rj kRpmom kRoor j | j kOp | mjkm | Ed | Gsp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | O6 | RIRGa407 | 043 | ：©00 6 | Б525 | ：C389 |  | 6 | 6706537209375 | 50； 8 | 5\％；8 | 4012： | J 5／8 |
| 7 | O7 | RIRGa407 | （962 | 3 | 0928 | 7ら55 |  | 3 | $69 C 8947209375$ | 5\％； 8 | 50； 8 | 4C378 | J 3／3d |
| 8 | 08 | RIRGa407 | （95： | 3 | 0663 | ： |  | 3 | $69 C 8947209375$ | 5\％； 8 | 5\％；8 | 3085 | J 3／3d |
| 9 | O9 | RIRGa407 | 973 | 3 | © ； 7 | 3 |  | 3 | 6：©： 87209375 | 50； 8 | 50； 8 | 4C88： | J 3／3d |
| ： | O： | RKRGa407 | 958 | 3 | 0446 | 78 |  | 3 | 6：©： 87209375 | 5\％； 8 | 50； 8 | 4®36 | J 3／3d |
| ； | O； | RKRGa4C2 | \％24 | 66 | C33： | 48 |  | 6 | 4208954035 | 3094 | 3094 | 4C2； 5 | J 3／3d |
| 32 | O32 | RIRGa4®2 | C8： 4 | 65 | （57） | 6 |  | 6 | 4208954035 | 3094 | 3094 | 60 6； | J 3／3d |
| 33 | O33 | RKRGa4C2 | 693 | 45 | （2； 5 | 4 |  | 8 | 4208954035 | 3094 | 3094 | 6077 | J 3／3d |
| 34 | O34 | RIRGa4®2 | （55； | 65 | ¢86 | 4 |  | 8 | 4208954035 | 3094 | 3094 | 68857 | J 3／3d |
| 35 | O35 | RIRGa4C2 | 67： | 65 | C353 | 40 |  | 3 | 4208954035 | 3094 | 3094 | 5＠49 | J 3／3d |
| 36 | O36 | RIRGa4C2 | C85； | 48 | ¢524 | 6 |  | 3 | 4208954035 | 3094 | 3094 | $603 ;$ | J 3／3d |
| 37 | O37 | RIRGa4C2 | 693 | 65 | （2； 5 | 4 |  | 5 | 4208954035 | 3094 | 3094 | 6964 | J 3／3d |
| 38 | O38 | RKRGa4®2 | C628 | 45 | （29： | 4 |  | 5 | 4208954035 | 3094 | 3094 | 5®8； 8 | J 3／3d |
| 39 | O39 | RIRGa4C2 | \％：7 | 65 | C333 | 4 |  | 8 | 4208954035 | 3094 | 3094 | 6\％2； | J 3／3d |
| 3： | O3： | RIRGa4C2 | C858 | 68 | 0444 | 6 |  | 3 | 4208954035 | 3094 | 3094 | 6083 | J 3／3d |
| 3； | O3； | RIRGa4C2 | ©685 | 65 | （2； 3 | 4 |  | 5 | 4208954035 | 3094 | 3094 | 608 | J 3／3d |
| 42 | O42 | RIRGa4C2 | C645 | 45 | ®2： 3 | 4 |  | 5 | 4208954035 | 3094 | 3094 | 6C654 | J 3／3d |
| 43 | O43 | RKRGa3047 | ［296 | 5セ20 6 | Q26 | 2 |  | 6 | 9＠； 7 3；©：： | 023 | 023 | 3C358 | J 3／3d |



Member Code Checks Displayed (Enveloped)

| Centek | CT11474A_AMA <br> Member Unity Check |  |
| :---: | :---: | :---: |
| FJP |  | Apr 24, 2019 at 2:24 PM |
| 19027.14 |  | CT11474A_AMA.R3D |

# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility
Site ID: CTII474A
WTNH Hamden
IOI Talmadge Road
Hamden, Connecticut 065I8
May 28, 2019
EBI Project Number: 6219001816

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population allowable <br> limit: | $\mathbf{0 . 9 6 \%}$ |

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May 28, 2019
T-Mobile
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, Connecticut 06002

Emissions Analysis for Site: CTII474A - WTNH Hamden

EBI Consulting was directed to analyze the proposed T-Mobile facility located at IOI Talmadge Road in Hamden, Connecticut for the purpose of determining whether the emissions from the Proposed TMobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-Oland ANSI/IEEE Std C95.I. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR I.I307(b)(I) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and II GHz frequency bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.
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Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at IOI Talmadge Road in Hamden, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6 -foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 LTE channels ( 600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
2) 2 LTE channels ( 700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 4 GSM channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
4) 2 LTE channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
5) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
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6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-0I recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antennas used in this modeling are the for the channel(s), the for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the $1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \mathrm{MHz}$ / 1900 MHz channel(s) in Sector A, , the RFS APXI6DWV-I6DWV-S-E-A20 for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the $1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \mathrm{MHz} /$ 1900 MHz channel(s) in Sector B, , the RFS APXI6DWV-I6DWV-S-E-A20 for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the $1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \mathrm{MHz} /$ 1900 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
9) The antenna mounting height centerline of the proposed antennas is feet above ground level (AGL).
10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
11) All calculations were done with respect to uncontrolled / general population threshold limits.

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## T-Mobile Site Inventory and Power Data

| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Make / Model: | $\begin{gathered} \text { RFS APXI6DWV-16DWV-S- } \\ \text { E-A20 } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { RFS APXI6DWV-16DWV-S- } \\ \text { E-A20 } \end{gathered}$ | Make / Model: | RFS APXI6DWV-I6DWV-S- <br> E-A20 |
| Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 315 feet | Height (AGL): | 315 feet | Height (AGL): | 315 feet |
| Channel Count: | 2 | Channel Count: | 2 | Channel Count: | 2 |
| Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts |
| ERP (W): | 4,668.54 | ERP (W): | 4,668.54 | ERP (W): | 4,668.54 |
| Antenna A2 MPE \%: | 0.17\% | Antenna B2 MPE \%: | 0.17\% | Antenna C2 MPE \%: | 0.17\% |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna \#: | 3 |
| Make / Model: | RFS APXVAARR24_43-UNA2O | Make / Model: | RFS APXVAARR24_43-UNA20 | Make / Model: | $\begin{aligned} & \text { RFS APXVAARR24_43-U- } \\ & \text { NA20 } \end{aligned}$ |
| Frequency Bands: | $\begin{gathered} 1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \\ \mathrm{MHz} / 1900 \mathrm{MHz} \end{gathered}$ | Frequency Bands: | $\begin{gathered} 1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \\ \mathrm{MHz} / 1900 \mathrm{MHz} \end{gathered}$ | Frequency Bands: | $\begin{gathered} \hline 1900 \mathrm{MHz} / 600 \mathrm{MHz} / 700 \\ \mathrm{MHz} / 1900 \mathrm{MHz} \end{gathered}$ |
| Gain: | $15.65 \mathrm{dBd} / 12.95 \mathrm{dBd} / 13.35$ $\mathrm{dBd} / 15.65 \mathrm{dBd}$ | Gain: | $15.65 \mathrm{dBd} / 12.95 \mathrm{dBd} / 13.35$ $\mathrm{dBd} / 15.65 \mathrm{dBd}$ | Gain: | $15.65 \mathrm{dBd} / 12.95 \mathrm{dBd} / 13.35$ $\mathrm{dBd} / 15.65 \mathrm{dBd}$ |
| Height (AGL): | 315 feet | Height (AGL): | 315 feet | Height (AGL): | 315 feet |
| Channel Count: | 10 | Channel Count: | 10 | Channel Count: | 10 |
| Total TX Power (W): | 360 Watts | Total TX Power (W): | 360 Watts | Total TX Power (W): | 360 Watts |
| ERP (W): | 11,295.86 | ERP (W): | 11,295.86 | ERP (W): | 11,295.86 |
| Antenna A3 MPE \%: | 0.53\% | Antenna B3 MPE \%: | 0.53\% | Antenna C3 MPE \%: | 0.53\% |

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| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| T-Mobile (Max at Sector A): | $0.70 \%$ |
| Sprint | $0.26 \%$ |
| Site Total MPE \%: | $0.96 \%$ |


| T-Mobile Sector A Total: | $0.70 \%$ |
| :---: | :---: |
| T-Mobile Sector B Total: | $0.70 \%$ |
| T-Mobile Sector C Total: | $0.70 \%$ |
| Site Total: |  |
| $0.96 \%$ |  |

## T-Mobile Maximum MPE Power Values (Sector A)

| T-Mobile Frequency Band / Technology (Sector A) | \# Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-Mobile 2100 MHz LTE | 2 | 2334.27 | 315.0 | 1.69 | 2100 MHz LTE | 1000 | 0.17\% |
| T-Mobile 1900 MHz GSM | 4 | 1101.85 | 315.0 | 1.60 | 1900 MHz GSM | 1000 | 0.16\% |
| T-Mobile 600 MHz LTE | 2 | 591.73 | 315.0 | 0.43 | 600 MHz LTE | 400 | 0.11\% |
| T-Mobile 700 MHz LTE | 2 | 648.82 | 315.0 | 0.47 | 700 MHz LTE | 467 | 0.10\% |
| T-Mobile 1900 MHz LTE | 2 | 2203.69 | 315.0 | 1.60 | 1900 MHz LTE | 1000 | 0.16\% |
|  |  |  |  |  |  | Total: | 0.70\% |

- NOTE: Totals may vary by approximately $0.01 \%$ due to summation of remainders in calculations.
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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| :---: | :---: |
| Sector A: | $0.70 \%$ |
| Sector B: | $0.70 \%$ |
| Sector C: | $0.70 \%$ |
| T-Mobile Maximum <br> MPE \% (Sector A): | $0.70 \%$ |
| Site Total: |  |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{0 . 9 6 \%}$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.

