

June 5, 2020

*Via Electronic Mail*

Melanie A. Bachman, Esq.  
Executive Director/Staff Attorney  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

Re: **Notice of Exempt Modification – Facility Modification  
330 Pokorny Road, Haddam, Connecticut**

Dear Attorney Bachman:

Cellco Partnership d/b/a Verizon Wireless (“Cellco”) currently maintains twelve (12) antennas at the 145-foot level of the existing 280-foot Eversource tower at 330 Pokorny Road in Haddam, Connecticut (the “Property”). The tower and underlying property are owned by Eversource. The existing tower was approved by the Siting Council (“Council”) in Petition No. 1027 in 2012 as a replacement structure for a previously existing tower at the Property. The Council approved Cellco’s shared use of the tower in 2016 (PE1133-VER-20160912). A copy of the Council’s Staff Report for Petition No. 1027 and Council’s 2016 Sub- Petition decision are included in Attachment 1.

Cellco now intends to modify its facility by replacing six (6) of its existing antennas with six (6) new antennas, removing six (6) remote radio heads (“RRHs”) and installing six (6) new RRHs and installing three (3) new fiber optic antenna cables. The existing antenna mounts will be reinforced as part of these proposed facility modifications. A set of project plans showing the proposed facility modifications and the specifications for Cellco’s new antennas, RRHs and fiber optic cables are included in Attachment 2.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Haddam’s First Selectman,

# Robinson+Cole

Melanie A. Bachman, Esq.

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Robert McGarry; Bill Warner, Haddam's Zoning Enforcement Officer; and Eversource, the tower and Property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing tower. Cellco's replacement antennas and RRHs will be installed at the 145-foot level on the 280-foot tower.

2. The proposed modifications will not involve any change to ground-mounted equipment and, therefore, will not require the extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The installation of new antennas and RRHs will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative General Power Density table for the modified facility is included in Attachment 3.

5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.

6. The tower, its foundation and antenna mounts, with certain modifications, can support Cellco's proposed facility modifications. (See Structural Analysis Report and Tower Modification Design Drawings included in Attachment 4 and Mount Structural Analysis Report included in Attachment 5).

A copy of the parcel map and Property owner information is included in Attachment 6. A Certificate of Mailing verifying that this filing was sent to municipal officials and the owner of the Property is included in Attachment 7.

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

# Robinson+Cole

Melanie A. Bachman, Esq.

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Sincerely,

A handwritten signature in black ink, appearing to read "Kenneth C. Baldwin". The signature is fluid and cursive, with a long horizontal stroke at the end.

Kenneth C. Baldwin

Enclosures

Copy to:

Robert McGarry, Haddam First Selectman  
Bill Warner, Haddam Zoning Enforcement Officer  
Eversource  
Tim Parks

# **ATTACHMENT 1**

Petition No. 1027  
Connecticut Light & Power  
Haddam, Connecticut  
Staff Report  
May 10, 2012

On April 5, 2012, the Connecticut Siting Council (Council) received a petition from The Connecticut Light & Power (CL&P) for a declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for the proposed replacement of an existing guyed lattice communications tower in Haddam, Connecticut. Council member Phil Ashton and Siting Analyst David Martin visited the site on May 4, 2012 to review the proposal. John Morissette and Steve Florio represented CL&P at the field review.

CL&P currently owns and operates a 280-foot guyed lattice wireless communications tower at 330 Pokorny Road in Haddam. The tower is host for a number of different antennas for several different users, including CL&P, the Connecticut State Police, Valley Shore Communications, and Sprint/Nextel. It provides critical microwave communication links for both CL&P and the State Police. A detailed structural analysis of the existing tower determined that it was overstressed and that there was no practical way of reinforcing the tower to bring it into compliance with state building code and CL&P engineering requirements.

CL&P proposes to replace the existing tower with a self-supporting lattice tower at the same height. The center of the replacement tower would be located approximately 50 feet to the west of the existing tower, which is the only location where it is possible to erect the new tower between the existing guy wires. CL&P would relocate the antennas on the existing tower onto the replacement tower. The replacement tower would also include a yield point to effectively reduce its potential fall zone and would be lit to comply with FAA requirements.

There are two fence lines on the CL&P property on which the existing tower is located. An outer fence encloses the locations where the guy wires are anchored to the ground. A smaller, inner fence encloses the existing tower and several equipment shelters. This inner fence would have to be extended a short distance to surround the proposed replacement tower. But the outer fence would remain at its current dimensions.

A number of large, single family homes have been built in the area surrounding CL&P's tower within the last twenty years. However, mature deciduous trees around the perimeter of CL&P's property help to minimize the visible impact of the tower on the nearest homes. Council member Ashton recommended that CL&P submit a D&M plan to show additional evergreen trees that would be planted within the facility's outer fence to help augment the existing vegetative screening of the tower.

The proposed replacement tower is not expected to have any substantial adverse environmental impacts. In fact, eliminating the existing guy wires will greatly reduce this wireless communications tower's potential for causing bird fatalities.



# STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

[www.ct.gov/csc](http://www.ct.gov/csc)

October 11, 2016

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **PE1133-VER-20160912** – Cellco Partnership d/b/a Verizon Wireless sub-petition for a declaratory ruling for approval of an eligible facility request for modifications to an existing telecommunications facility located at 330 Pokorny Road, Haddam, Connecticut.

Dear Attorney Baldwin:

The Connecticut Siting Council (Council) hereby approves your Eligible Facilities Request (EFR) to install antennas and associated equipment at the above-referenced facility pursuant to the Federal Communications Commission Wireless Infrastructure Report and Order, with the following conditions:

1. Prior to commencement of installation, Cellco shall provide one copy of the Structural Analysis Report to the Council referencing Revision G of the *Structural Standards for Steel Antenna Towers and Antenna Supporting Structures* as adopted by the Connecticut State Building Code effective October 1, 2016;
2. All coax cables shall be routed as specified in Section 3 of the Structural Analysis Report prepared by Centek Engineering, Inc. dated April 9, 2015 and stamped by Timothy Lynn or subsequent structural analysis report in accordance with Revision G as stated in the condition above;
3. Within 45 days following completion of equipment installation, Cellco shall provide documentation that its installation complied with the recommendations of the structural analysis;
4. Within 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
5. Any nonfunctioning antenna and associated antenna mounting equipment on this facility owned and operated by the Petitioner shall be removed within 60 days of the date the antenna ceased to function;
6. The validity of this action shall expire one year from the date of this letter; and
7. The Petitioner may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration.

This decision is under the exclusive jurisdiction of the Council and is not applicable to any other modification or construction. All work is to be implemented as specified in the EFR dated September 9, 2016.

Thank you for your attention and cooperation.

Very truly yours,

Melanie Bachman  
Acting Executive Director

MB/CW

c: Honorable Lizz Milardo, First Selectman, Town of Haddam  
Elizabeth Glidden, Town Planner, Town of Haddam

S:\PETITIONS\1101-1200\1133\3\_Subpetitions\_ByTown\Haddam\PokornyRd\VERIZON\PE1133-VER-20160912-dctr-pokomyrd-haddam.docx



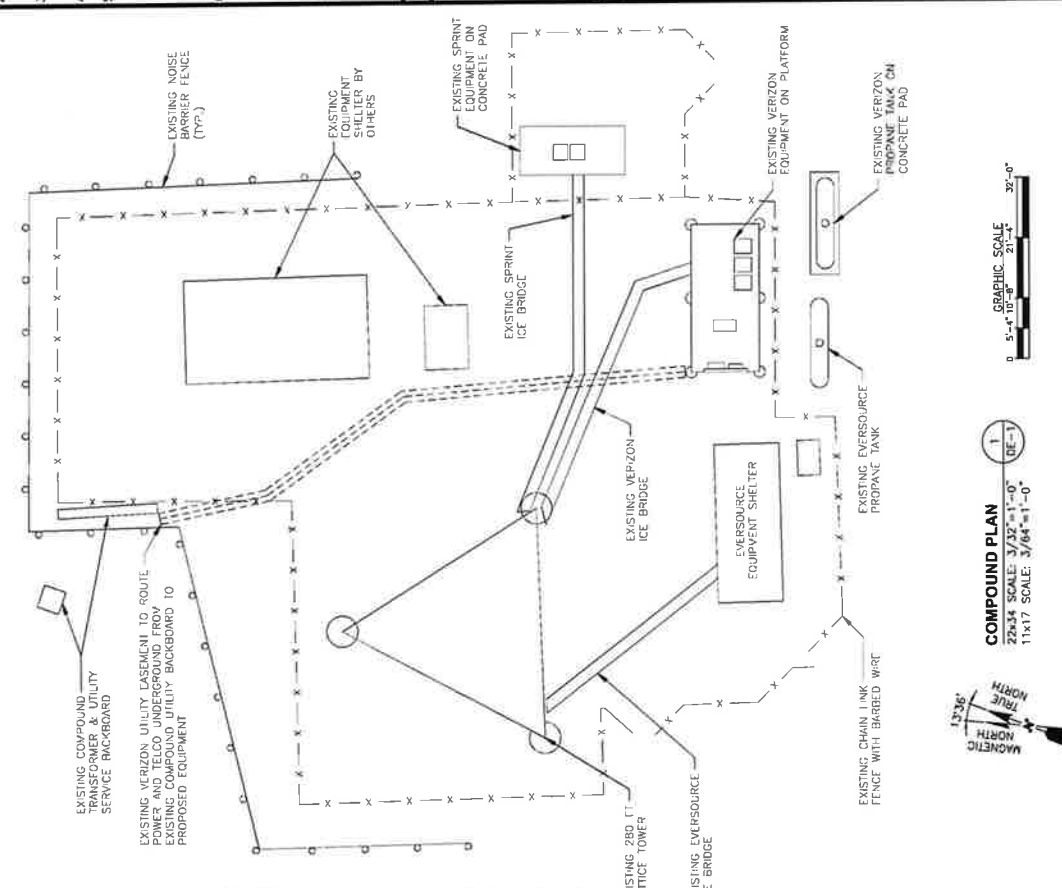
# **ATTACHMENT 2**



**LOCUS MAP**  
 MAP DATA ©2019 GOOGLE  
**SCALE: N.T.S.**  
 APPROXIMATE  
 SITE COORDINATES: LAT: N41° 26' 36.88"  
 LONG: W72° 33' 56.89"

**NOTE**  
 A STRUCTURAL ANALYSIS OF THE CAPACITY OF THE EXISTING MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY HUDSON DESIGN GROUP, LLC DATED: MAY 6, 2019 (REV.1)  
 A STRUCTURAL ANALYSIS OF THE CAPACITY OF THE EXISTING STRUCTURE TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY J. J. FORD & COMPANY DATED: MAY 21, 2020

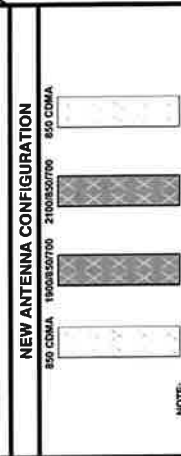
**DESIGN EXHIBIT**  
 THIS PLAN IS DIAGRAMMATIC IN NATURE AND IS INTENDED TO PROVIDE GENERAL INFORMATION REGARDING THE LOCATION AND SIZE OF THE PROPOSED ANTENNA UPGRADE.



**SCOPE**

- EXISTING HBVY-651705-A2M ANTENNAS TO BE REMOVED
- EXISTING LNK-651505-A1M\_ADT ANTENNAS TO BE REMOVED
- EXISTING LNK-651505-A1M\_SDT ANTENNAS TO BE REMOVED
- EXISTING RRHs TO BE REMOVED
- EXISTING ANTENNAS TO REMAIN
- (24) EXISTING 1/2" COAX TO REMAIN
- EXISTING OVP TO REMAIN
- EXISTING HYBRID CABLES TO BE REMOVED.
- EXISTING HYBRID CABLES TO REMAIN
- INSTALL (6) NEW NHH 65C R2B ANTENNAS
- INSTALL (3) NEW RRH B2/B66A
- INSTALL (3) NEW RRH B5/B13
- INSTALL (3) NEW BSAMT-SBS-1-2 MOUNT
- INSTALL (3) NEW HYBRID CABLES
- INSTALL (6) NEW SAMSUNG FIBER JUMPERS
- INSTALL (6) NEW SAMSUNG POWER JUMPERS
- INSTALL (24) NEW 1/2" COAX JUMPERS
- INSTALL (3) NEW SECTOR FRAME STABILIZER KITS SITEPRO1, SFS-V
- INSTALL (3) NEW 2" (2.38 O.D.) PIPE BRACES (SEE S-1)
- INSTALL (3) NEW 2-1/2" (2.88 O.D.) PIPE MASTS (SEE S-1)
- ALL REPLACEMENT ANTENNAS TO MATCH EXISTING CONDITIONS AND HEIGHTS.
- RECONFIGURE / RELOCATE EXISTING ANTENNA MOUNTS AS NECESSARY TO ACCOMMODATE HORIZONTAL SEPARATION, PROPOSED AZIMUTHS, AND ANTENNA CONFIGURATION.

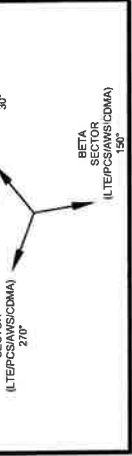
**NEW ANTENNA CONFIGURATION**



**NOTES**

- NORTH SHOWN AS APPROXIMATE.
- SOME EXISTING & PROPOSED INFORMATION NOT SHOWN FOR CLARITY.
- ANTENNAS WILL BE PAINTED PER VERIZON WIRELESS & BUILDING OWNER'S APPROVAL.
- PRIOR TO COMMENCEMENT OF ANY WORK, PROPOSED ANTENNAS SHALL BE SUBMITTED TO THE BUILDING DEPARTMENT FOR STRUCTURAL ANALYSIS. STRUCTURAL ANALYSIS TO VERIFY CAPACITY OF EXISTING STRUCTURE TO ENSURE STRUCTURAL INTEGRITY FOLLOWING INSTALLATION OF PROPOSED ANTENNAS. STRUCTURAL ANALYSIS TO BE SENT TO DESIGN ENGINEER.
- CONTRACTOR SHALL FIELD VERIFY SCOPE OF WORK. VERIZON WIRELESS ANTENNA MOUNT LOCATION AND ANTENNAS TO BE INSTALLED.
- CONTRACTOR SHALL NOTIFY ENGINEERS IF FILED CONDITIONS DIFFER FROM DESIGN.
- RAD CENTERS MEASURED IN THE FIELD WITH LASER BY HDG. RAD CENTERS MAY NOT MATCH RF ANTENNA DESIGN SHEET.

**ANTENNA ORIENTATION**



CHECKED BY: JK  
 APPROVED BY: DPH

**SUBMITTALS**

REV	DATE	DESCRIPTION	BY
1	4/15/20	ISSUE FOR PERMITTING	ST
2	4/15/20	ISSUE FOR PERMITTING	AM
3	7/21/20	ISSUE FOR PERMITTING	ST
4	8/19/20	ISSUE FOR PERMITTING	AM
5	8/19/20	ISSUE FOR PERMITTING	AM

SITE NAME:  
**HIGGANUM SOUTH CT**  
 SITE ADDRESS:  
 330 POKONY ROAD  
 HIGGANUM, CT 06441

SHEET TITLE  
**COMPOUND PLAN**

SHEET NUMBER  
**DE-1**

**DESIGN EXHIBIT**



DESIGN EXHIBIT

FORMED BY: CALICO PARTNERSHIP, L.P.



**H2G**  
**HUDSON**  
 Design Group LLC  
 4500 HIGGANUM ROAD  
 HIGGANUM, MA 01461  
 TEL: 978.527.6500  
 FAX: 978.528.5550



*Daniel Adams*

CHECKED BY: JK

APPROVED BY: DPH

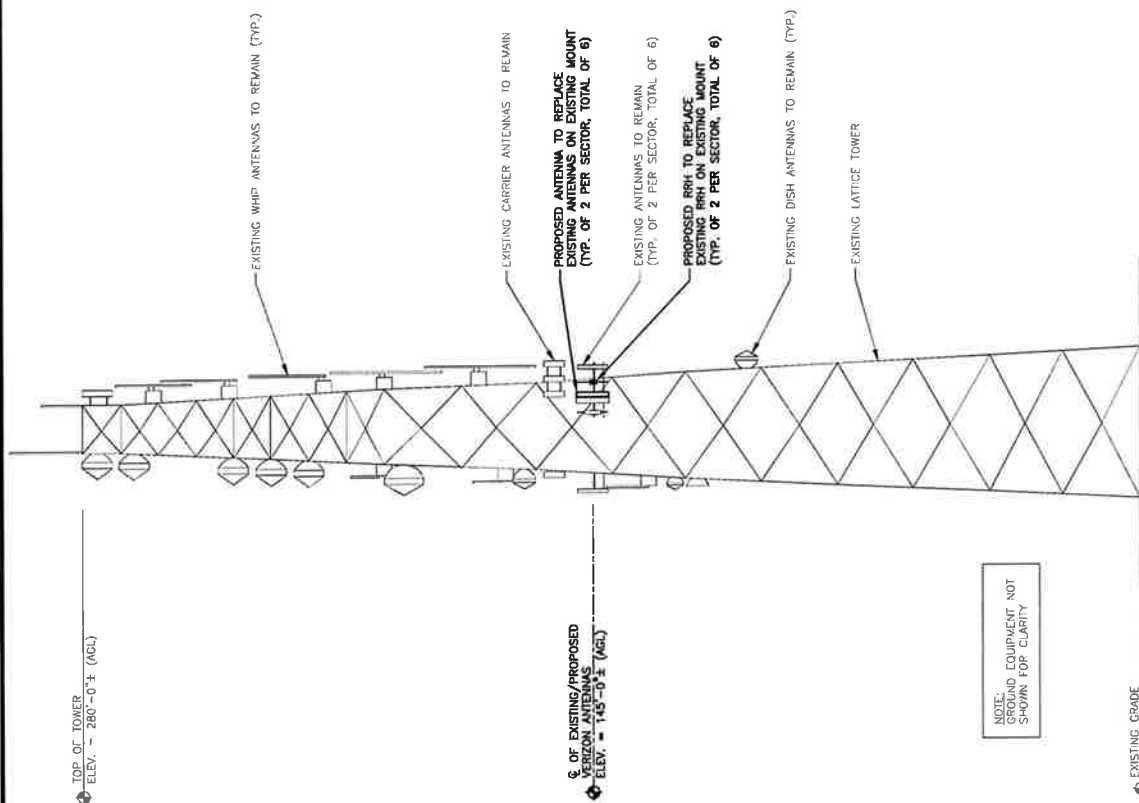
SUBMITTALS

REV.	DATE	DESCRIPTION	BY
1	10/20/19	ISSUED PER COMMENTS	DM
2	11/15/19	ISSUED PER COMMENTS	DM
3	02/27/20	ISSUED PER COMMENTS	DM
4	04/01/20	ISSUED PER COMMENTS	DM
5	04/01/20	ISSUED FOR REVIEW	DM

SITE NAME:  
**HIGGANUM SOUTH CT**  
 SITE ADDRESS:  
 330 POMEROY ROAD  
 HIGGANUM, CT 06441

SHEET TITLE  
**ELEVATION**

SHEET NUMBER  
**DE-2**



**NOTE:**  
 A MOUNT ANALYSIS OF THE CAPACITY OF THE EXISTING MOUNT TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED.  
 DATED: MAY 6, 2018 (REV.1)  
 A STRUCTURAL ANALYSIS OF THE CAPACITY OF THE EXISTING STRUCTURE TO SUPPORT THE PROPOSED LOADING HAS BEEN COMPLETED BY PAUL J. FORD & COMPANY.  
 DATED: MAY 21, 2020

NOTE:  
 SHOWN EQUIPMENT NOT SHOWN FOR CLARITY

ELEVATION  
 22x34 SCALE: 1/16"=1'-0"  
 11x17 SCALE: 1/32"=1'-0"  
 GRAPHIC SCALE  
 0 10 20 30 40 FEET

PROPOSED TYPE: 224534 224534



**H2G HUDSON**  
Design Group LLC  
415 COMMODORE BLVD  
N. ANDOVER, MA 01850  
TEL: 978.237.6400  
FAX: 978.238.5354



CONTRACTOR LICENSES ARE VALID FOR ONE YEAR FROM THE DATE OF EXPIRATION AND MUST BE RENEWED ANNUALLY.

CHECKED BY: JK  
APPROVED BY: DPH

SUBMITTALS

REV	DATE	DESCRIPTION	BY
4	4/15/24	ISSUANCE RETURNING	SVT
3	4/15/24	ISSUE PER COMMENTS	DM
2	2/12/24	ISSUE PER COMMENTS	SVT
1	02/20/24	ISSUE PER COMMENTS	DM
0	01/09/24	ISSUE PER REVIEW	DM

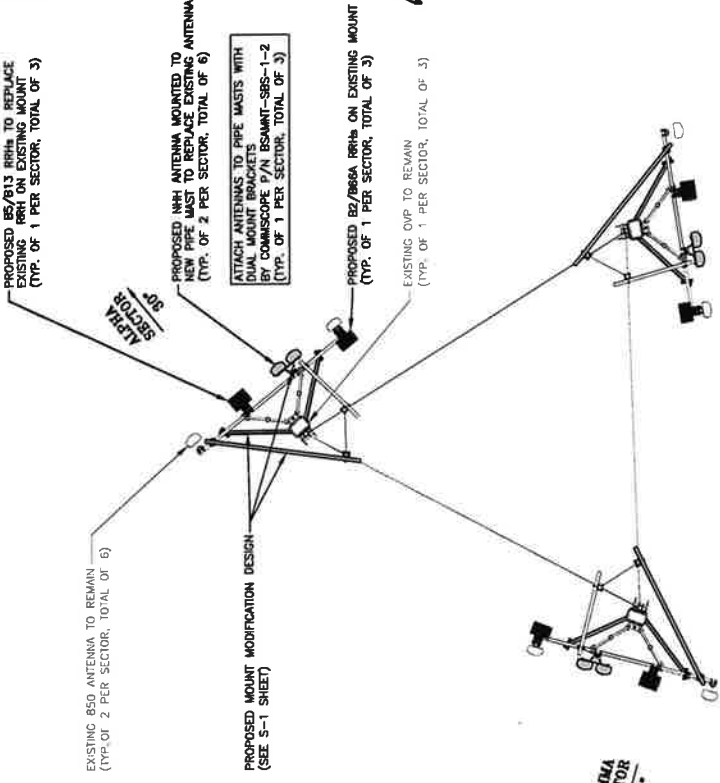
SITE NAME:  
**HIGGANUM SOUTH CT**

SITE ADDRESS:  
330 POKORNY ROAD  
HIGGANUM, CT 06441

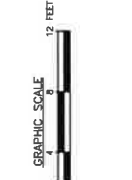
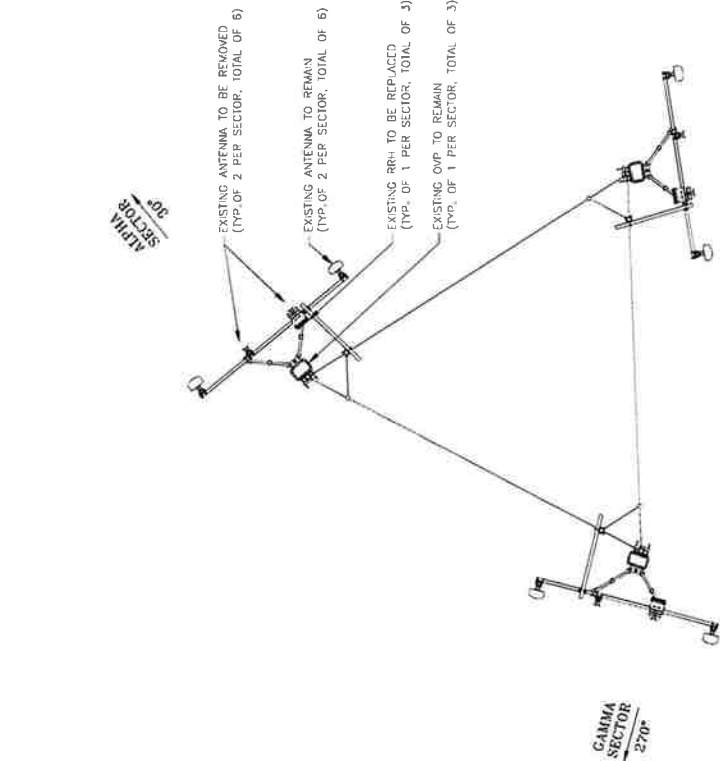
SHEET TITLE  
**ANTENNA CONFIGURATIONS**

SHEET NUMBER  
**DE-3**

**DESIGN EXHIBIT**



**ANTENNA PLAN (AFTER)**  
224534 SCALE: 1/4"=1'-0"  
11x17 SCALE: 1/8"=1'-0"  
DE-3

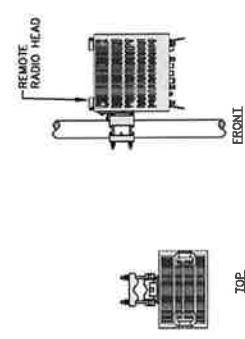
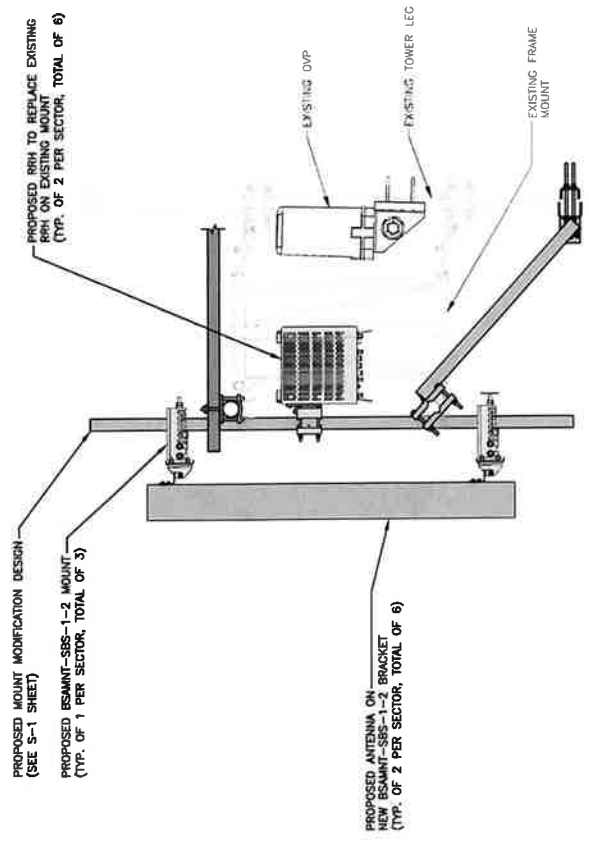


**ANTENNA PLAN (BEFORE)**  
224534 SCALE: 1/4"=1'-0"  
11x17 SCALE: 1/8"=1'-0"  
DE-3

*Daniel P. Hannon*

DESIGN EXHIBIT

			CHECKED BY: JK APPROVED BY: DPH	<table border="1"> <thead> <tr> <th>REF</th> <th>DATE</th> <th>DESCRIPTION</th> <th>BY</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>4/15/09</td> <td>ISSUANCE ATTENDANCE</td> <td>SKT</td> </tr> <tr> <td>2</td> <td>4/15/09</td> <td>ISSUED FOR COMMENTS</td> <td>SKT</td> </tr> <tr> <td>3</td> <td>7/12/09</td> <td>ISSUED FOR COMMENTS</td> <td>SKT</td> </tr> <tr> <td>4</td> <td>02/24/10</td> <td>ISSUED FOR COMMENTS</td> <td>SKT</td> </tr> <tr> <td>5</td> <td>03/10/10</td> <td>ISSUED FOR REVIEW</td> <td>SKT</td> </tr> </tbody> </table>	REF	DATE	DESCRIPTION	BY	1	4/15/09	ISSUANCE ATTENDANCE	SKT	2	4/15/09	ISSUED FOR COMMENTS	SKT	3	7/12/09	ISSUED FOR COMMENTS	SKT	4	02/24/10	ISSUED FOR COMMENTS	SKT	5	03/10/10	ISSUED FOR REVIEW	SKT	SITE NAME: <b>HIGGANUM SOUTH CT</b>	SITE ADDRESS: 330 FOXBORO ROAD HIGGANUM, CT 06441	SHEET TITLE <b>ANTENNA CONFIGURATIONS</b>	SHEET NUMBER <b>DE-4</b>
REF	DATE	DESCRIPTION	BY																													
1	4/15/09	ISSUANCE ATTENDANCE	SKT																													
2	4/15/09	ISSUED FOR COMMENTS	SKT																													
3	7/12/09	ISSUED FOR COMMENTS	SKT																													
4	02/24/10	ISSUED FOR COMMENTS	SKT																													
5	03/10/10	ISSUED FOR REVIEW	SKT																													



**REMOTE RADIO HEAD MOUNTING DETAIL**  
 22x34 SCALE: N.T.S.

**ANTENNA MOUNTING DETAIL**  
 SCALE: N.T.S.

1 DE-4

2 DE-4

**STRUCTURAL NOTES:**

- DESIGN REQUIREMENTS ARE PER STATE BUILDING CODE AND APPLICABLE STANDARDS FOR STEEL ANTENNA, TOWERS AND ANTENNA SUPPORTING STRUCTURES.
- CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION. UNLESS OTHERWISE NOTED, ALL DIMENSIONS AND CONDITIONS SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER AND ENGINEER OF RECORD.
- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO THE REQUIREMENTS OF THE STRUCTURAL STEEL SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS.
- STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 (Fy=50 ksi), UNLESS OTHERWISE INDICATED.
- SEAMLESS CARBON STEEL STRUCTURAL TUBING, GRADE B, OR ASTM A53 PIPE SHALL BE BLACK AND HOT-DIPPED ZINC-COATED WELDED AND SEAMLESS TYPE E OR S. GRADE B PIPE SIZES INDICATED ARE NOMINAL, ACTUAL OUTSIDE DIAMETER IS LARGER.
- STRUCTURAL CONNECTION BOLTS SHALL BE HIGH STRENGTH BOLTS (BEARING TYPE) AND CONFORM TO ASTM A325 TYPE-X "HIGH STRENGTH BOLTS FOR STRUCTURAL JOINTS, INCLUDING SUITABLE NUTS AND PLAIN HARDENED WASHERS". ALL BOLTS SHALL BE 3/4" DIA UDN.
- ALL STEEL MATERIALS SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP GALVANIZED) COATINGS ON IRON AND STEEL PRODUCTS", UNLESS OTHERWISE NOTED.
- ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIP) ON IRON AND STEEL HARDWARE", UNLESS OTHERWISE NOTED.
- FIELD WELDS, DRILL HOLES, SAW CUTS AND ALL DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED WITH AN ORGANIC ZINC REPAIR PAINT WHICH SHALL BE EQUAL TO THE ORIGINAL FINISH. REPAIR SHALL BE PAINTED WITH A MINIMUM OF 65 PERCENT ZINC BY WEIGHT. ZINC REPAIR SHALL BE GALVANIZED PREVIOUSLY BY CROWN OR EQUAL. THICKNESS OF APPLIED GALVANIZING REPAIR PAINT SHALL BE NOT LESS THAN 4 COATS (ALLOW TIME TO DRY BETWEEN COATS) WITH A RESULTING COATING THICKNESS REQUIRED BY ASTM A123 AS APPLICABLE.
- CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES, APPEARANCE AND QUALITY OF WELDS, AND FOR METHODS USED IN CORRECTING WELDING. ALL WELDERS AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS STANDARD QUALIFICATION PROCEDURES. ALL WELDING SHALL BE DONE IN ACCORDANCE WITH THE QUALIFICATION PROCEDURES. WELDING SHALL BE DONE WHERE FLEET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AWS "STEEL CONSTRUCTION MANUAL", 14TH EDITION.
- INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE UNFITTING OR UNUSABLE MATERIAL SHALL BE REPORTED TO THE ATTENTION OF THE CONSTRUCTION MANAGER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE CONSTRUCTION MANAGER APPROVAL.
- UNSTEEL SHALL BE FORMED STEEL CHANNEL STUB FRAMING AS MANUFACTURED BY UNISTRUT CORP. WAYNE MI OR EQUAL. STRUT MEMBERS SHALL BE 1 5/8"x1 5/8"x12GA. UNLESS OTHERWISE NOTED, AND SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION.
- FRAY ANCHOR ASSEMBLY SHALL CONSIST OF STAINLESS STEEL ANCHOR ROD WITH NUTS AND WASHERS; AN INTERNAL THEADED INSERT, A SCREEN TUBE AND AN EPOXY ADHESIVE. THE ANCHORING SYSTEM SHALL BE THE HLT-HIT HY-70 AND OR HY-200 SYSTEMS (AS SPECIFIED IN DWG.) OR ENGINEERS APPROVED EQUAL.
- EXPANSION BOLTS SHALL CONFORM TO FEDERAL SPECIFICATION FF-S-325, GROUP II, TYPE 4, CLASS 1, HLT KWK BOLT III OR APPROVED EQUAL. INSTALLATION SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- LUMBER SHALL COMPLY WITH THE REQUIREMENTS OF THE AMERICAN INSTITUTE OF TIMBER CONSTRUCTION AND THE NATIONAL FOREST PRODUCTS ASSOCIATION'S NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION. ALL LUMBER SHALL BE PRESSURE TREATED AND SHALL BE STRUCTURAL GRADE NO. 2 OR BETTER.
- WHERE ROOF PENETRATIONS ARE REQUIRED, THE CONTRACTOR SHALL CONTACT AND COORDINATE RELATED WORK WITH THE BUILDING OWNER AND THE EXISTING ROOF INSTALLER. WORK SHALL BE PERFORMED IN SUCH A MANNER AS TO NOT VOID THE EXISTING ROOF WARRANTY. ROOF SHALL BE WATERIGHT.
- ALL FIBERGLASS MEMBERS USED ARE AS MANUFACTURED BY STRONGWELL COMPANY OF BRISTOL, VA 24203. ALL DESIGN CRITERIA FOR THESE MEMBERS IS BASED ON INFORMATION PROVIDED IN THE DESIGN MANUAL. ALL REQUIREMENTS PUBLISHED IN SAID MANUAL MUST BE STRICTLY ADHERED TO.
- NO MATERIALS TO BE ORDERED AND NO WORK TO BE COMPLETED UNTIL SHOP DRAWINGS HAVE BEEN REVIEWED AND APPROVED IN WRITING.
- SUBCONTRACTOR SHALL FIREPROOF ALL STEEL TO PRE-EXISTING CONDITIONS.

**SPECIAL INSPECTIONS (REFERENCE IBC CHAPTER 17):**

GENERAL: WHERE APPLICATION IS MADE FOR CONSTRUCTION, THE OWNER OR THE REGISTERED DESIGN PROFESSIONAL IS RESPONSIBLE CHARGE ACTING AS THE OWNER'S AGENT SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM INSPECTIONS DURING CONSTRUCTION ON THE TYPES OF WORK LISTED IN THE INSPECTION CHECKLIST ABOVE. THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND ENGINEERS OF RECORD INVOLVED IN THE DESIGN OF THE SPECIAL INSPECTION WORK SHALL EMPLOY ONE OR MORE APPROVED AGENCIES TO PERFORM THE QUALIFICATION REQUIREMENTS.

STATEMENT OF SPECIAL INSPECTIONS: THE APPLICANT SHALL SUBMIT A STATEMENT OF SPECIAL INSPECTIONS PREPARED BY AN ENGINEER OF RECORD OR REGISTERED DESIGN PROFESSIONAL IN ACCORDANCE WITH SECTION 107.1 AS A CONDITION FOR ISSUANCE. THIS STATEMENT SHALL BE IN ACCORDANCE WITH SECTION 1705.

REPORT REQUIREMENT: SPECIAL INSPECTORS SHALL KEEP RECORDS OF INSPECTIONS. THE SPECIAL INSPECTOR SHALL FURNISH INSPECTION REPORTS TO THE BUILDING OFFICIAL, AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. THE SPECIAL INSPECTOR SHALL REPORT ALL DISCREPANCIES TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE AND TO THE REGISTERED DESIGN PROFESSIONAL IN ATTENTION OF THE CONTRACTOR FOR CORRECTION. IF THEY ARE NOT CORRECTED, THE DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE BUILDING OFFICIAL AND TO THE REGISTERED DESIGN PROFESSIONAL IN RESPONSIBLE CHARGE. A FINAL REPORT DOCUMENTING REQUIRED SPECIAL INSPECTIONS SHALL BE SUBMITTED.

**SPECIAL INSPECTION CHECKLIST**

BEFORE CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
N/A	ENGINEER OF RECORD APPROVED SHOP DRAWINGS
N/A	MATERIAL SPECIFICATIONS REPORT?
N/A	FABRICATOR NODE INSPECTION
N/A	PACKING SUPS?
ADDITIONAL TESTING AND INSPECTIONS:	
DURING CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	STEEL INSPECTIONS
N/A	HIGH STRENGTH BOLT INSPECTIONS
N/A	HIGH WIND ZONE INSPECTIONS *
N/A	FOUNDATION INSPECTIONS
N/A	CONCRETE COMP. STRENGTH, SLUMP TESTS AND PLACEMENT VERIFICATION
N/A	TESTS RELATED TO ANCHOR
N/A	GROUT VERIFICATION
N/A	CERTIFIED WELD INSPECTION
N/A	EARTHWORK, LIFT AND DENSITY VERIFICATION
N/A	ON SITE COLD GALVANIZING VERIFICATION
N/A	CUY WIRE TENSION REPORT
ADDITIONAL TESTING AND INSPECTIONS:	
AFTER CONSTRUCTION	
CONSTRUCTION/INSTALLATION INSPECTIONS AND TESTING REQUIRED (COMPLETED BY ENGINEER OF RECORD)	REPORT ITEM
REQUIRED	MODIFICATION INSPECTION REQUIRE
N/A	POST INSTALLED ANCHOR PULL-OUT TESTING
ADDITIONAL TESTING AND INSPECTIONS:	
PHOTOGRAPHS	

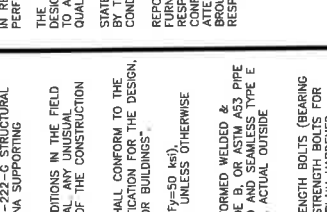
**NOTES:**

- REQUIRED FOR ANY NEW SHOP FABRICATED RRP DP STEEL CONNECTIONS BY MANUFACTURER, REQUIRED IF HIGH STRENGTH BOLTS OR STEEL.
- PROVIDED BY GENERAL CONTRACTOR. PROOF OF MATERIALS.
- HIGH WIND ZONE INSPECTION CATB 120MPH OR CAT C/D FASTENING SCHEDULE
- ADHESIVE FOR REBAR AND ANCHORS SHALL HAVE BEEN TESTED IN ACCORDANCE WITH ASTM C881, C882, C883, C884, C885, C886, C887, C888, C889, C890, C891, C892, C893, C894, C895, C896, C897, C898, C899, C900, C901, C902, C903, C904, C905, C906, C907, C908, C909, C910, C911, C912, C913, C914, C915, C916, C917, C918, C919, C920, C921, C922, C923, C924, C925, C926, C927, C928, C929, C930, C931, C932, C933, C934, C935, C936, C937, C938, C939, C940, C941, C942, C943, C944, C945, C946, C947, C948, C949, C950, C951, C952, C953, C954, C955, C956, C957, C958, C959, C960, C961, C962, C963, C964, C965, C966, C967, C968, C969, C970, C971, C972, C973, C974, C975, C976, C977, C978, C979, C980, C981, C982, C983, C984, C985, C986, C987, C988, C989, C990, C991, C992, C993, C994, C995, C996, C997, C998, C999, C1000.
- AS REQUIRED; FOR ANY FIELD CHANGES TO THE ITEMS IN THIS TABLE.

**NOTES:**

- ALL CONNECTIONS TO BE SHOP WELDED & FIELD BOLTED USING 3/4" A325-X BOLTS, UNLESS OTHERWISE NOTED.
- SHOP DRAWINGS SHALL BE REVIEWED AND APPROVED BEFORE ORDERING MATERIALS.
- SHOP DRAWING ENGINEER REVIEW & APPROVAL REQUIRED PRIOR TO STEEL FABRICATION.
- CONSTRUCTION OF CONSTRUCTION IS TO APPROVE EXISTING CONDITIONS IN ORDER TO PROCEED WITH FORMWORK SUPPORT COLUMNS TO BE CENTRALLY LOCATED OVER THE EXISTING BUILDING COLUMNS.
- EXISTING BRICK WALLS AND CONCRETE FOUNDATION TO BE MAINTAINED. MASONRY COLUMNS/BOLTS TO BE MAINTAINED. ALL BRICKWORK TO BE REPAIRED. CONSTRUCTION SUPPORT POINTS, ENGINEER OF RECORD TO REVIEW AND APPROVE.

**DESIGN EXHIBIT**



CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE DESIGN MANUAL AND ALL OTHER DOCUMENTS REFERENCED THEREIN.

DATE: 08/20/2024



**HGD HUDSON**  
Design Group LLC  
418704000-046  
14500209 144-2845  
TEL: 203-657-6565  
FAX: 203-657-3358



CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE DESIGN MANUAL AND ALL OTHER DOCUMENTS REFERENCED THEREIN.

CHECKED BY: JK  
APPROVED BY: DPH

**SUBMITTALS**

REV	DATE	DESCRIPTION	BY
4	4/11/2024	ISSUANCE RETENTION	SK
3	4/11/2024	ISSUANCE PER COMMENTS	SK
2	7/10/24	ISSUANCE PER COMMENTS	SK
1	02/28/24	ISSUANCE PER COMMENTS	SK
0	01/07/24	ISSUANCE PER REVIEW	SK

SITE NAME:  
**HIGGANUM SOUTH CT**

SITE ADDRESS:  
330 FOXBORO ROAD  
HIGGANUM, CT 06441

SHEET TITLE  
**NOTES & INSPECTION CHECK LIST**

SHEET NUMBER  
**SN-1**

DESIGN EXHIBIT

PRINTED ON: CALICO PAPER/30% FSC



*Daniel Starnin*

CHECKED BY: JJK  
 APPROVED BY: DPH

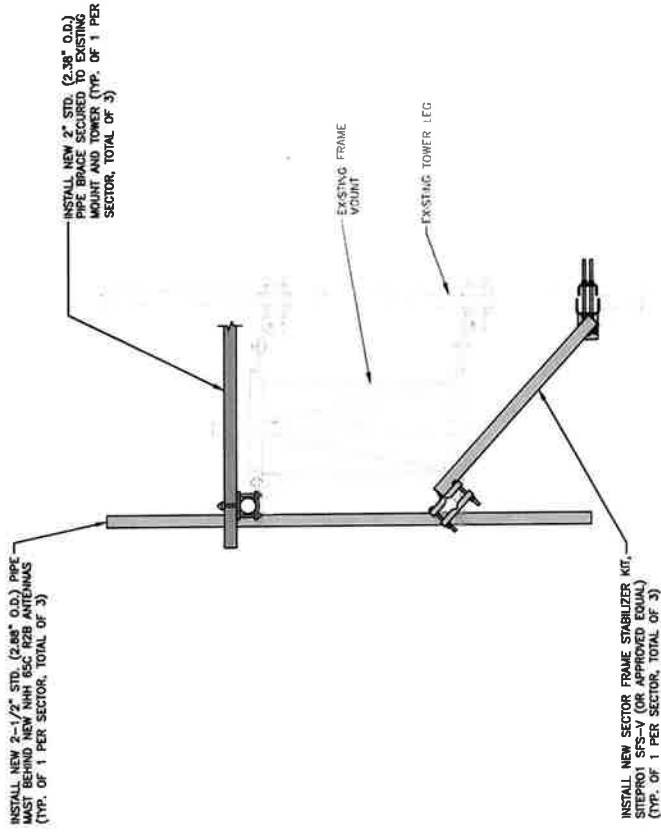
SUBMITTALS

REV	DATE	DESCRIPTION	BY
1	4/15/18	ISSUE FOR BIDDING	DPH
2	7/17/18	REVISED PER COMMENTS	DPH
3	8/24/18	REVISED PER COMMENTS	DPH
4	8/24/18	REVISED PER REVIEW	DPH

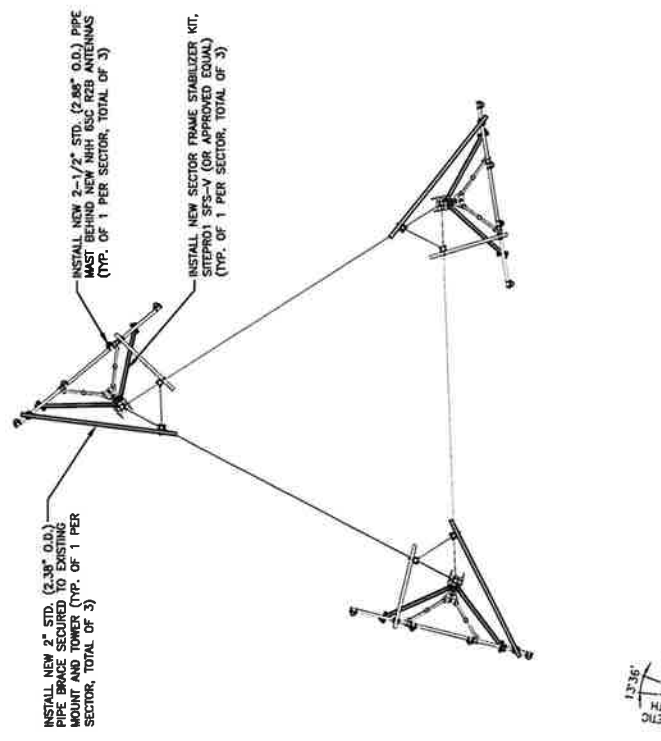
SITE NAME:  
**HIGGANUM SOUTH CT**  
 SITE ADDRESS:  
 330 POKORNY ROAD  
 HIGGANUM, CT 06441

SHEET TITLE  
**MOUNT MODIFICATION DESIGN**

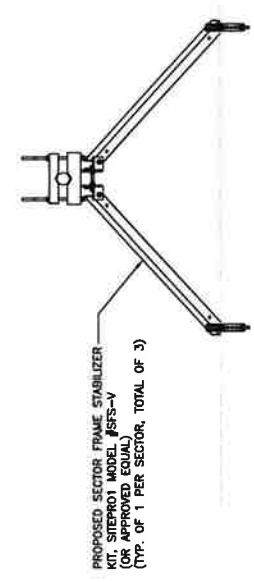
SHEET NUMBER  
**S-1**



**PROPOSED MOUNT MODIFICATION ELEVATION 2**  
 SCALE: N.T.S.



**PROPOSED MOUNT MODIFICATION PLAN 1**  
 SCALE: 1/8"=1'-0"



**SECTOR FRAME STABILIZER KIT 3**  
 SCALE: N.T.S.



4850 WOODDAVE  
N. ANDOVER, MA 01810  
TEL: (978) 522-5333  
FAX: (978) 522-5338

CHECKED BY: JJK  
APPROVED BY: DPH

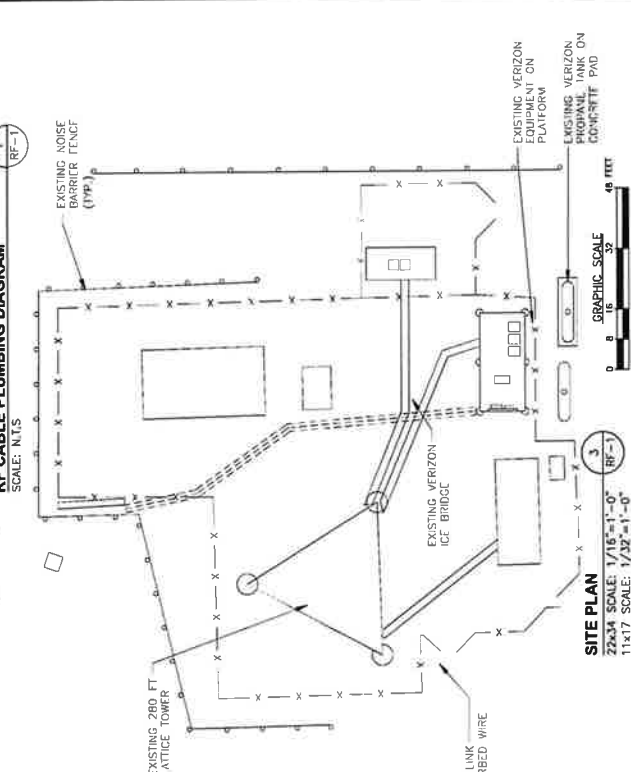
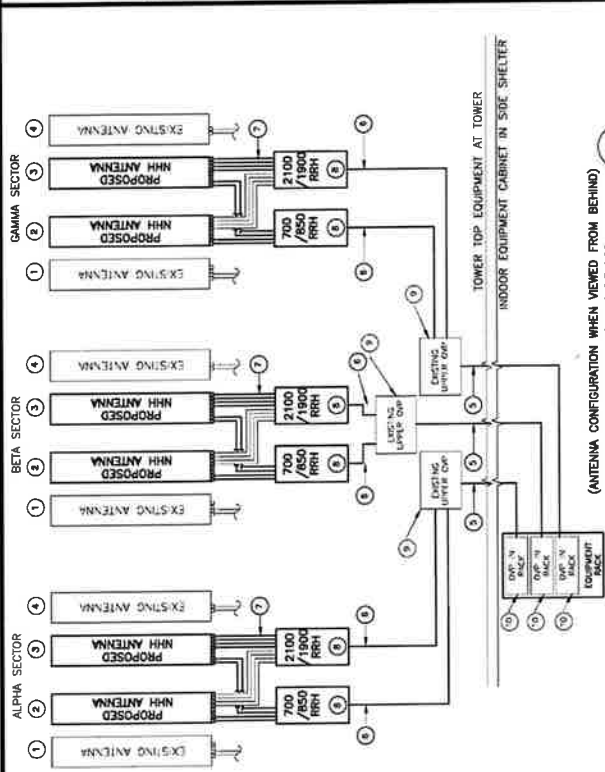
NO.	DATE	DESCRIPTION
1	02/20/17	REVISED PER COMMENTS
2	02/27/17	ISSUED FOR PERMIT

SITE NAME:  
**HIGGANUM SOUTH CT**

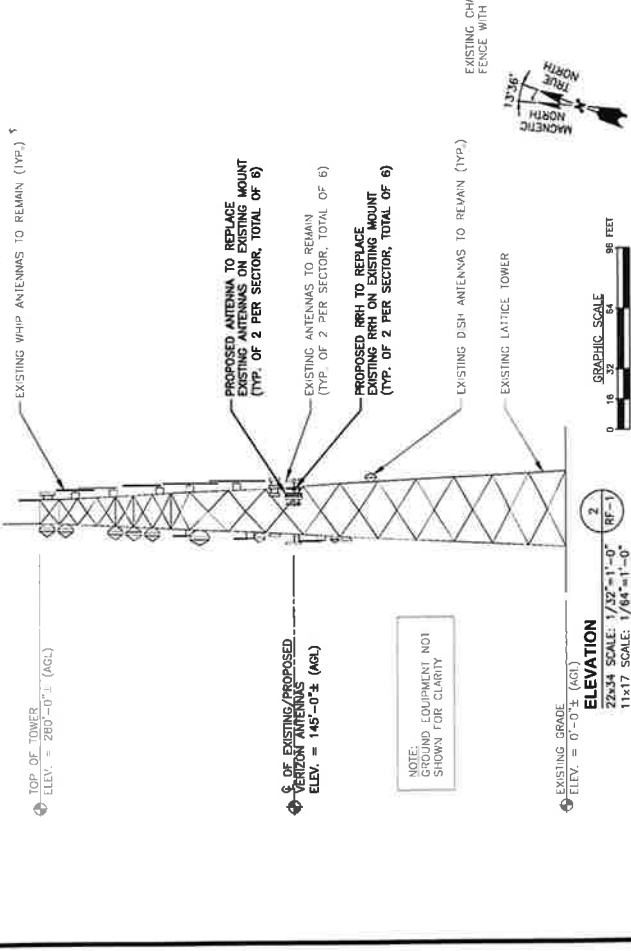
SITE ADDRESS:  
330 POKORNY ROAD  
HIGGANUM, CT 06441

SHEET TITLE  
**RF PLUMBING  
DIAGRAM AND BILL  
OF MATERIALS**

SHEET NUMBER  
**RF-1**



ITEM	DESCRIPTION	QTY	LENGTH	COMMENTS
1	ANTENNA-- (EXISTING) CDMA HBXX-6517DS-A2M	3		MOUNTED TO SECTOR FRAME (EXISTING)
2	ANTENNA-- (PROPOSED) (LTE) NHH-65C-R2B	3		MOUNTED TO SECTOR FRAME (EXISTING)
3	ANTENNA-- (PROPOSED) (AWS/PCS) NHH-65C-R2B	3		MOUNTED TO SECTOR FRAME (EXISTING)
4	ANTENNA-- (EXISTING) CDMA LW-6515DS-A1M	3		MOUNTED TO SECTOR FRAME (EXISTING)
5	6x12 HYBRID CABLE (PROPOSED)	1	185 FT.	ROUTE FROM INDOOR EQUIPMENT TO ANTENNA SECTOR
6	6x12 HYBRID CABLE (PROPOSED)	1	185 FT.	ROUTE FROM INDOOR EQUIPMENT TO ANTENNA SECTOR
7	6x12 HYBRID CABLE (PROPOSED)	1	185 FT.	ROUTE FROM INDOOR EQUIPMENT TO ANTENNA SECTOR
8	SAMSUNG FIBER JUMPERS (PROPOSED)	6	15 FT.	ROUTE FROM UPPER OVP TO RRHs
9	SAMSUNG POWER JUMPERS (PROPOSED)	8	15 FT.	ROUTE FROM UPPER OVP TO RRHs
10	1/2" TOP COAX JUMPERS	8	6 FT.	ROUTE FROM RRH TO ANTENNA
11	1/2" TOP COAX JUMPERS	8	6 FT.	ROUTE FROM RRH TO ANTENNA
12	1/2" TOP COAX JUMPERS	8	6 FT.	ROUTE FROM RRH TO ANTENNA
13	1/2" TOP COAX JUMPERS	24	6 FT.	ROUTE FROM RRH TO ANTENNA
14	LTE RRH	3		(SAMSUNG) 85/813 PIPE MOUNTED
15	PCS/AWS RRH	3		(SAMSUNG) 82/866A PIPE MOUNTED
16	UPPER OVP (EXISTING)	3		MOUNTED TO SECTOR FRAME
17	LOWER OVP (EXISTING)	3		MOUNTED INSIDE EQUIPMENT CABINET



RF BOM IS PER ANTENNA RF COMMENDATION DATE SHEET DATED 03/31/2019

NOTE: GROUND EQUIPMENT NOT SHOWN FOR CLARITY

# MODIFIED 280' SELF SUPPORT TOWER

**SITE: HIGGANUM SOUTH CT**  
 330 PORKORNY STREET  
 HADDAM CONNECTICUT 06441  
 MIDDLESEX COUNTY  
 LAT: 41° 26' 36.9"; LONG: -72° 33' 58.9"

### PROJECT CONTACTS

CLIENT:  
 HUDSON DESIGN GROUP  
 CONTACT: SYLVESTER BHEMBE AT  
 SBHEMBE@HUDSONDESIGNGROUP.LLC.COM  
 PH: (878) 557-5553  
 ENGINEER OF RECORD:  
 PJFTELECOM@PAULJFORD.COM

SHEET INDEX	
SHEET NUMBER	DESCRIPTION
T-1	TITLE SHEET
M-1	MI CHECKLIST AND NOTES
N-1	NOTES
S-1	TOWER ELEVATION
S-2	DIAGONAL STITCH BOLT REINFORCING

TOWER MANUFACTURER: VALMONT  
 TOWER MANUFACTURER #: 2408988  
 QUALIFIED ENGINEERING SERVICES ARE AVAILABLE FROM PAUL J. FORD & COMPANY TO ASSIST CONTRACTORS IN CLASS IV RIGGING PLAN REVIEWS. FOR REQUESTED QUALIFIED ENGINEERING SERVICES, PLEASE CONTACT PJFMOD@PAULJFORD.COM.

### WIND DESIGN DATA

REFERENCE STANDARD	ANSI/TIA-222-G-2-2009
LOCAL CODE	2018 CSBC
ULTIMATE WIND SPEED (3-SECOND GUST)	140 MPH
CONVERTED NOMINAL WIND SPEED (3-SECOND GUST)	108 MPH
ICE THICKNESS	0.75 IN
ICE WIND SPEED	50 MPH
SERVICE WIND SPEED	60 MPH
RISK CATEGORY	III
EXPOSURE CATEGORY	C
MAXIMUM TOPOGRAPHIC FACTOR, $K_{zt}$	1.0



05/21/2020

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**PAUL J. FORD & COMPANY**  
 250 E Broad St, Ste 600 - Columbus, OH 43215  
 Phone 614.221.6679 www.pauljford.com  
**HUDSON DESIGN GROUP**  
 1800 OSBORN ST SUITE 2-101 BUILDING 20 NORTH N ANDOVER, MA 01845  
 PH (978) 557-5553

**SITE: HIGGANUM SOUTH CT**  
 HADDAM CONNECTICUT  
 MODIFIED 280' SELF SUPPORT TOWER

PROJECT NO: 000194111.005.R002  
 DRAWN BY: RAK  
 DESIGNED BY: MFB  
 CHECKED BY: PJF  
 DATE: 5/21/2020

TITLE SHEET

T-1

REV	DATE	DESCRIPTION

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**PAUL J. FORD & COMPANY**  
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 www.pauljford.com

1000 OSBORN RD SUITE 2-101 BUILDING 20 NORTH N ANDOVER, MA 01845  
 PH (978) 557-5575

**HUDSON DESIGN GROUP**

**MODIFIED 280 SELF SUPPORT TOWER**  
**HADDAM CONNECTICUT**  
**SITE: HIGGANUM SOUTH CT**

PROJECT NO: 09170111.005.8800  
 DRAWN BY: RAK  
 CHECKED BY: MTH  
 DATE: 5/21/2020

MI CHECKLIST AND NOTES  
 MI-1

**POST-MODIFICATION CHECKLIST**

**MODIFICATION INSPECTION NOTES**

**GENERAL**

THE M/I TO CONSIDER INSTALLATION, CONSTRUCTION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN ITSELF. WORK DOES NOT INCLUDE THE OWNERSHIP OF THE MODIFICATION DESIGN. THE M/I INSPECTOR SHALL BE RESPONSIBLE FOR VERIFYING THE DESIGN EFFECTIVENESS AND INTEGRITY RESIDES WITH THE GC AT ALL TIMES.

TO ENSURE THAT THE REQUIREMENTS OF THE M ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE M/I INSPECTOR BEGIN COMMUNICATING AND COORDINATING AS SOON AS A PO IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY.

THE M/I INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO FOR THE M/I TO, AT A MINIMUM

- REVIEW THE REQUIREMENTS OF THE M/I CHECKLIST
- WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

THE M/I INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE M/I REPORT TO THE OWNER.

**GENERAL CONTRACTOR**

- THE GC IS REQUIRED TO CONTACT THE M/I INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO, AT A MINIMUM
- REVIEW THE REQUIREMENTS OF THE M/I CHECKLIST
- WORK WITH THE M/I INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
- BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH INDUSTRY STANDARD

**RECOMMENDATIONS**

THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A M/I REPORT

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE M/I INSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE M/I TO BE CONDUCTED
- THE GC AND M/I INSPECTOR COORDINATE CLOSELY THROUGHOUT THE RE-INSPECTION OPERATIONS
- IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION INSPECTIONS TO BE CONDUCTED WITHOUT THE NEED FOR THE GC AND M/I INSPECTOR ON-SITE DURING THE M/I TO HAVE ANY DEFICIENCIES CORRECTED

COORDINATE THE M/I THEREFORE, THE GC MAY CHOOSE TO COORDINATE THE M/I CAREFULLY TO ENSURE ALL CONSTRUCTION ACTIVITIES ARE AT THEIR DISPOSAL WHEN THE M/I INSPECTORS ARE AT THE SITE

**CANCELLATION OR DELAYS IN SCHEDULE**

IF THE GC AND M/I INSPECTOR AGREE TO ADJUTE ON WHICH THE M/I WILL BE CONDUCTED, AND EITHER PARTY CANCELS OR DELAYS, THE TOWER OWNER AND/OR OTHER PARTIES RELATED TO THE CANCELLATION OR DELAY INCURRED BY EITHER PARTY FOR ANY TIME (E.G. TRAVEL AND LOGGING, COSTS OF KEEPING EQUIPMENT ON-SITE, ETC.) IF THE TOWER OWNER CONTRACTS DIRECTLY FOR A THIRD PARTY M/I, COORDINATION MUST BE MADE IN OTHER CONDITIONS THAT MAY COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

**CORRECTION OF FAILING ITEMS**

IF CORRECTION WORK IS REQUIRED, THE M/I INSPECTOR WILL COORDINATE WITH THE GC TO CORRECT THE FAILING ITEMS. THE M/I INSPECTOR WILL COORDINATE WITH THE GC TO CORRECT THE FAILING ITEMS. THE M/I INSPECTOR WILL COORDINATE WITH THE GC TO CORRECT THE FAILING ITEMS.

- CORRECT FAILING ISSUES TO COMPLY WITH THE SPECIFICATIONS
- AS APPLICABLE, THE ORIGINAL CONTRACT DOCUMENTS AND COORDINATE
- OR, WITH OWNERS APPROVAL, THE GC MAY WORK WITH THE GC TO RE-ANALYZE THE MODIFICATION/REINFORCEMENT USING THE AS-BUILT CONDITION

**PHOTOGRAPHS**

BETWEEN THE GC AND THE M/I INSPECTOR THE FOLLOWING PHOTOGRAPHS, AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE M/I REPORT

- PRE-CONSTRUCTION GENERAL SITE CONDITION
- PHOTOGRAPHS DURING THE REINFORCEMENT/ MODIFICATION CONSTRUCTION
- RAW MATERIALS
- POST CONSTRUCTION DETAILS
- FINAL INSPECTION DETAILS
- WELD PREPARATION
- BOLT INSTALLATION AND TORQUE
- FINAL INSTALLED CONDITION
- POST CONSTRUCTION PHOTOGRAPHS
- FINAL IN-FIELD CONDITION

PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS, PLEASE COORDINATE WITH THE M/I

**SHOP DRAWINGS**

IF APPROVED SHOP DRAWINGS CAN BE PROVIDED AS AN ADDITIONAL SCOPE OF SERVICE, IF REQUIRED, PLEASE CONTACT D/F FOR ADDITIONAL INFORMATION

THE M/I INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO FOR THE M/I TO, AT A MINIMUM

- REVIEW THE REQUIREMENTS OF THE M/I CHECKLIST
- WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

THE M/I INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE M/I REPORT TO THE OWNER.

**GENERAL CONTRACTOR**

- THE GC IS REQUIRED TO CONTACT THE M/I INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO, AT A MINIMUM
- REVIEW THE REQUIREMENTS OF THE M/I CHECKLIST
- WORK WITH THE M/I INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
- BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH INDUSTRY STANDARD

**RECOMMENDATIONS**

THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A M/I REPORT

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE M/I INSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE M/I TO BE CONDUCTED
- THE GC AND M/I INSPECTOR COORDINATE CLOSELY THROUGHOUT THE RE-INSPECTION OPERATIONS
- IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO CONDUCTING THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION INSPECTIONS TO BE CONDUCTED WITHOUT THE NEED FOR THE GC AND M/I INSPECTOR ON-SITE DURING THE M/I TO HAVE ANY DEFICIENCIES CORRECTED

COORDINATE THE M/I THEREFORE, THE GC MAY CHOOSE TO COORDINATE THE M/I CAREFULLY TO ENSURE ALL CONSTRUCTION ACTIVITIES ARE AT THEIR DISPOSAL WHEN THE M/I INSPECTORS ARE AT THE SITE

**PRE-CONSTRUCTION**

THIS CHECKLIST SHALL BE INCLUDED IN THE M/I REPORT

FABRICATION DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD FOR REVIEW. THE CONTRACTOR SHALL PROVIDE THE APPROVED SHOP DRAWINGS TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT. SEE SHOP DRAWING NOTES

A LETTER FROM THE FABRICATOR, STATING THAT THE WORK WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THE CONTRACT DOCUMENTS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

CRITICAL SHOP WELDS THAT REQUIRE TESTING ARE NOTED ON THESE CONTRACT DRAWINGS. A CERTIFIED WELD INSPECTOR SHALL PERFORM NON-DESTRUCTIVE TESTING AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

SEPERATION WELDS SHALL BE PROVIDED FOR ALL SITES WITH A WELD STRENGTH GREATER THAN 36 ksi AND THIS DOCUMENTATION SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

A VISUAL OBSERVATION OF A PORTION OF THE EXISTING STRUCTURE (AS NOTED ON THESE DRAWINGS) IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

A VISUAL OBSERVATION OF THE ROLE TO BASE PLATE CONNECTION IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

THE MATERIAL SHIPPING LIST SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

**CONSTRUCTION**

A LETTER FROM THE GENERAL CONTRACTOR STATING THAT THE WORKMANSHIP WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THESE CONTRACT DRAWINGS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

A VISUAL OBSERVATION OF THE EXCAVATION AND REBAR SHALL BE PERFORMED BEFORE PLACING THE CONCRETE. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

THE CONCRETE MIX DESIGN, SLUMP TEST, AND COMPRESSIVE STRENGTH TESTS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

ANCHOR ROD INSTALLATION SHALL INCLUDE VERIFICATION BY LETTER AND PHOTOGRAPHIC DOCUMENTATION

A LETTER FROM THE GENERAL CONTRACTOR SHALL BE PROVIDED TO THE M/I INSPECTOR THAT CERTIFIES THAT THE GROUT WAS INSTALLED IN ACCORDANCE WITH INDUSTRY STANDARD FOR INCLUSION IN THE M/I REPORT.

A CERTIFIED WELD INSPECTOR SHALL INSPECT AND TEST AS NECESSARY ALL FIELD WELDS AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT. PRE-DURING AND POST-WELD INSPECTION IS REQUIRED

FOUNDATION SUB-GRANDES SHALL BE INSPECTED AND APPROVED BY A GEOTECHNICAL ENGINEER AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR VERIFYING THAT ANY ON-SITE COLD GALVANIZING WAS APPLIED FOR FIELD PUNCH-DRILLED HOLES

THE GENERAL CONTRACTOR SHALL PROVIDE A REPORT TO THE M/I INSPECTOR INDICATING THE TEMPERATURE AND TENSION IN EVERY GUY WIRE REPORT

THE GENERAL CONTRACTOR SHALL SUBMIT A COPY OF THE CONTRACT DRAWINGS EITHER STATING "INSTALLED AS DESIGNED" OR NOTING ANY CHANGES THAT WERE REQUIRED AND APPROVED BY THE ENGINEER OF RECORD DUE TO FIELD CONDITIONS

THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR VERIFYING THAT ANY MAGN 565 COATING WAS APPLIED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS FOR INCLUSION IN THE M/I REPORT

THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT

THE M/I INSPECTOR SHALL OBSERVE AND REPORT ANY DISCREPANCIES BETWEEN THE CONTRACTORS REALINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION

POST INSTALLED ANCHOR RODS SHALL BE TESTED IN ACCORDANCE WITH INDUSTRY STANDARD AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

PHOTOGRAPHS SHALL BE SUBMITTED TO THE M/I INSPECTOR DURING ALL PHASES OF THE CONSTRUCTION. THE PHOTOS SHALL BE ORGANIZED IN A MANNER THAT EASILY IDENTIFIES THE EXACT LOCATION OF THE PHOTO

POST INSTALLED ANCHORS SHALL BE TESTED AND INSPECTED IN ACCORDANCE WITH SPECIFICATION STATED ON MICROPIERCE TESTING REPORT. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT

NOTE: A WRITTEN REPORT RECEIVED FROM THE CONTRACTOR FOR THE M/I REPORT

NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE M/I REPORT

THE M/I INSPECTOR SHALL OBSERVE AND REPORT ANY DISCREPANCIES BETWEEN THE CONTRACTORS REALINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION

POST INSTALLED ANCHOR RODS SHALL BE TESTED IN ACCORDANCE WITH INDUSTRY STANDARD AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

PHOTOGRAPHS SHALL BE SUBMITTED TO THE M/I INSPECTOR DURING ALL PHASES OF THE CONSTRUCTION. THE PHOTOS SHALL BE ORGANIZED IN A MANNER THAT EASILY IDENTIFIES THE EXACT LOCATION OF THE PHOTO

POST INSTALLED ANCHORS SHALL BE TESTED AND INSPECTED IN ACCORDANCE WITH SPECIFICATION STATED ON MICROPIERCE TESTING REPORT. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT

NOTE: A WRITTEN REPORT RECEIVED FROM THE CONTRACTOR FOR THE M/I REPORT

NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE M/I REPORT

**POST-CONSTRUCTION**

THE M/I INSPECTOR SHALL OBSERVE AND REPORT ANY DISCREPANCIES BETWEEN THE CONTRACTORS REALINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION

POST INSTALLED ANCHOR RODS SHALL BE TESTED IN ACCORDANCE WITH INDUSTRY STANDARD AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.

PHOTOGRAPHS SHALL BE SUBMITTED TO THE M/I INSPECTOR DURING ALL PHASES OF THE CONSTRUCTION. THE PHOTOS SHALL BE ORGANIZED IN A MANNER THAT EASILY IDENTIFIES THE EXACT LOCATION OF THE PHOTO

POST INSTALLED ANCHORS SHALL BE TESTED AND INSPECTED IN ACCORDANCE WITH SPECIFICATION STATED ON MICROPIERCE TESTING REPORT. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT

NOTE: A WRITTEN REPORT RECEIVED FROM THE CONTRACTOR FOR THE M/I REPORT

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REQUIRED	REPORT ITEM	BRIEF DESCRIPTION
X	MI CHECKLIST DRAWING	THIS CHECKLIST SHALL BE INCLUDED IN THE M/I REPORT
NA	FOR APPROVED SHOP DRAWINGS	FABRICATION DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD FOR REVIEW. THE CONTRACTOR SHALL PROVIDE THE APPROVED SHOP DRAWINGS TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT. SEE SHOP DRAWING NOTES
NA	FABRICATION INSPECTION	A LETTER FROM THE FABRICATOR, STATING THAT THE WORK WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THE CONTRACT DOCUMENTS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	FABRICATOR CERTIFIED WELD INSPECTION	CRITICAL SHOP WELDS THAT REQUIRE TESTING ARE NOTED ON THESE CONTRACT DRAWINGS. A CERTIFIED WELD INSPECTOR SHALL PERFORM NON-DESTRUCTIVE TESTING AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	MATERIAL TEST REPORT (MTR)	SEPERATION WELDS SHALL BE PROVIDED FOR ALL SITES WITH A WELD STRENGTH GREATER THAN 36 ksi AND THIS DOCUMENTATION SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	FABRICATOR MIX INSPECTION	A VISUAL OBSERVATION OF A PORTION OF THE EXISTING STRUCTURE (AS NOTED ON THESE DRAWINGS) IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	ROLE REPORT OF MONOPILE BASE PLATE (AS REQUIRED)	A VISUAL OBSERVATION OF THE ROLE TO BASE PLATE CONNECTION IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
X	PACKING SLIPS	THE MATERIAL SHIPPING LIST SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
<b>CONSTRUCTION</b>		
X	CONSTRUCTION INSPECTIONS	A LETTER FROM THE GENERAL CONTRACTOR STATING THAT THE WORKMANSHIP WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THESE CONTRACT DRAWINGS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	FOUNDATION INSPECTIONS	A VISUAL OBSERVATION OF THE EXCAVATION AND REBAR SHALL BE PERFORMED BEFORE PLACING THE CONCRETE. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	CONCRETE COMP. STRENGTH AND SLUMP TESTS	THE CONCRETE MIX DESIGN, SLUMP TEST, AND COMPRESSIVE STRENGTH TESTS SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
NA	POST INSTALLED ANCHOR ROD VERIFICATION	ANCHOR ROD INSTALLATION SHALL INCLUDE VERIFICATION BY LETTER AND PHOTOGRAPHIC DOCUMENTATION
NA	BASE PLATE GROUT VERIFICATION	A LETTER FROM THE GENERAL CONTRACTOR SHALL BE PROVIDED TO THE M/I INSPECTOR THAT CERTIFIES THAT THE GROUT WAS INSTALLED IN ACCORDANCE WITH INDUSTRY STANDARD FOR INCLUSION IN THE M/I REPORT.
NA	CONTRACTORS CERTIFIED WELD INSPECTION	A CERTIFIED WELD INSPECTOR SHALL INSPECT AND TEST AS NECESSARY ALL FIELD WELDS AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT. PRE-DURING AND POST-WELD INSPECTION IS REQUIRED
NA	EARTHWORK, LIFT AND DENSITY	FOUNDATION SUB-GRANDES SHALL BE INSPECTED AND APPROVED BY A GEOTECHNICAL ENGINEER AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
X	ON SITE COLD GALVANIZING VERIFICATION	THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR VERIFYING THAT ANY ON-SITE COLD GALVANIZING WAS APPLIED FOR FIELD PUNCH-DRILLED HOLES
NA	GUY WIRE TENSION REPORT	THE GENERAL CONTRACTOR SHALL PROVIDE A REPORT TO THE M/I INSPECTOR INDICATING THE TEMPERATURE AND TENSION IN EVERY GUY WIRE REPORT
X	GC AS BUILT DOCUMENTS	THE GENERAL CONTRACTOR SHALL SUBMIT A COPY OF THE CONTRACT DRAWINGS EITHER STATING "INSTALLED AS DESIGNED" OR NOTING ANY CHANGES THAT WERE REQUIRED AND APPROVED BY THE ENGINEER OF RECORD DUE TO FIELD CONDITIONS
NA	MAGN 565 COATING VERIFICATION	THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR VERIFYING THAT ANY MAGN 565 COATING WAS APPLIED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS FOR INCLUSION IN THE M/I REPORT
NA	MICROPILE / ROCK ANCHOR	THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT
<b>POST-CONSTRUCTION</b>		
X	M/I INSPECTOR REVIEW OF RECORD DRAWINGS(S)	THE M/I INSPECTOR SHALL OBSERVE AND REPORT ANY DISCREPANCIES BETWEEN THE CONTRACTORS REALINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION
NA	POST INSTALLED ANCHOR ROD PULL TESTING	POST INSTALLED ANCHOR RODS SHALL BE TESTED IN ACCORDANCE WITH INDUSTRY STANDARD AND A REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT.
X	PHOTOGRAPHS	PHOTOGRAPHS SHALL BE SUBMITTED TO THE M/I INSPECTOR DURING ALL PHASES OF THE CONSTRUCTION. THE PHOTOS SHALL BE ORGANIZED IN A MANNER THAT EASILY IDENTIFIES THE EXACT LOCATION OF THE PHOTO
NA	POST INSTALLED MICROPILE / ROCK ANCHOR TESTING REPORT	POST INSTALLED ANCHORS SHALL BE TESTED AND INSPECTED IN ACCORDANCE WITH SPECIFICATION STATED ON MICROPIERCE TESTING REPORT. A WRITTEN REPORT SHALL BE PROVIDED TO THE M/I INSPECTOR FOR INCLUSION IN THE M/I REPORT

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05 21 2020

REV DATE DESCRIPTION



GENERAL NOTES:

1. THIS TOWER MODIFICATION DRAWING IS BASED UPON A STRUCTURAL ANALYSIS PERFORMED BY PAUL J. FORD AND COMPANY DATED 5/21/2020.
2. PAUL J. FORD AND COMPANY HAS NOT PERFORMED A FIELD VISIT TO VERIFY THE EXISTING TOWER MEMBER SIZES AND DIMENSIONS. THE MODIFICATIONS SHOWN ON THESE PAGES WERE DEVELOPED USING INFORMATION PROVIDED TO US BY HUDSON DESIGN GROUP.
3. THE CONTRACTOR IS EXPECTED TO PERFORM A SITE VISIT BEFORE FABRICATING ANY MATERIAL. IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT ARE NOT AS REPRESENTED ON THESE DRAWINGS, PAUL J. FORD AND COMPANY SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE STRUCTURAL SIGNIFICANCE OF THE DEVIATION.
4. THE CONTRACTOR MUST BE EXPERIENCED IN THE PERFORMANCE OF WORK SIMILAR TO THAT DESCRIBED ON THESE DRAWINGS. BY ACCEPTANCE OF THIS PROJECT, THE CONTRACTOR IS ATTESTING THAT HE DOES HAVE SUFFICIENT EXPERIENCE AND ABILITY, THAT HE IS KNOWLEDGEABLE OF THE WORK TO BE PERFORMED AND THAT HE IS PROPERLY LICENSED TO DO THIS WORK IN THE JURISDICTION IN WHICH THE WORK IS TO BE PERFORMED.
5. THIS DRAWING DOES NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION METHODS, MEANS, TECHNIQUES, SEQUENCES AND PROCEDURES.
6. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR INITIATING, MAINTAINING AND SUPERVISING ALL SAFETY PROGRAMS AND PRECAUTIONS IN CONNECTION WITH THE WORK.
7. INSPECTIONS SHALL BE COMPLETED IN ACCORDANCE WITH LOCAL BUILDING CODES.

CONSTRUCTION NOTES:

1. ALL CONSTRUCTION MEANS AND METHODS, INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN AND SHALL MEET ANSIIASSE A10.48 (LATEST EDITION); FEDERAL, STATE, AND LOCAL REGULATIONS; AND ANY APPLICABLE INDUSTRY CONSENSUS STANDARDS RELATED TO THE CONSTRUCTION ACTIVITIES BEING PERFORMED. ALL RIGGING PLANS SHALL ADHERE TO ANSIIASSE A10.48 (LATEST EDITION)
2. ALL HOLES, EITHER PUNCHED OR DRILLED, IN THE EXISTING STEEL MEMBERS SHALL BE 1/16 INCH LARGER THAN THE BOLT DIAMETER UNLESS NOTED OTHERWISE. SLOTTED OR OVERSIZED HOLES ARE NOT PERMITTED.
3. ANY GALVANIZED SURFACE THAT IS SCRATCHED OR DAMAGED DUE TO THE CONTRACTOR'S EFFORTS, SHALL BE REPAIRED WITH A COLD GALVANIZING COMPOUND CONFORMING TO ASTM A780.

MATERIAL NOTES:

1. PRIOR TO FABRICATION AND INSTALLATION, CONTRACTOR SHALL FIELD VERIFY ALL LENGTHS AND QUANTITIES GIVEN. LENGTH AND QUANTITIES PROVIDED ARE FOR QUOTING PURPOSES ONLY AND SHALL NOT BE USED FOR FABRICATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROPER FIT AND CLEARANCE OF THE REINFORCING MATERIAL IN THE FIELD. THE CONTRACTOR IS EXPECTED TO PERFORM A SITE VISIT BEFORE FABRICATING ANY MATERIAL.
2. ALL STEEL SHALL CONFORM TO THE FOLLOWING (U.N.O.):
  - A. PLATES: ASTM A36 GR 36 (36 KSI YIELD POINT MATERIAL)
3. ALL NEW STEEL SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH THE "SPECIFICATION FOR ZINC (HOT GALVANIZED) COATING ON PRODUCTS FABRICATED FROM ROLLED, PRESSED AND FORGED STEEL SHAPES, PLATES BAR, AND STRIP" ASTM A123.
4. ALL BOLTS SHALL CONFORM TO THE REQUIREMENTS OF ASTM A325. USE BEARING TYPE CONNECTIONS, TIGHTEN TO A SNUG TIGHT CONNECTION, UNO.
5. PAL-NUTS SHALL BE PROVIDED WITH LOCK-WASHERS, OR LOCK-NUTS, OR PAL-NUTS AND SHALL BE GALVANIZED ACCORDING TO ASTM A153/ASTM153M.

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**PJF**  
**PAUL J. FORD**  
**& COMPANY**  
250 E Broad St, Ste 600 - Columbus, OH 43215  
Phone 614.221.6679 www.pauljford.com

**HUDSON DESIGN GROUP**  
1000 OSAGOOD ST SUITE 2-101 BUILDING 20 NORTH N ANDOVER, MA 01845  
PH (978) 557-5553

**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

PROJECT No.	0019-0111.005.0506
DRAWN BY	RAK
DESIGNED BY	MTE
CHECKED BY	JPJ
DATE	5/21/2020

NOTES

N-1



REV. DATE DESCRIPTION

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**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

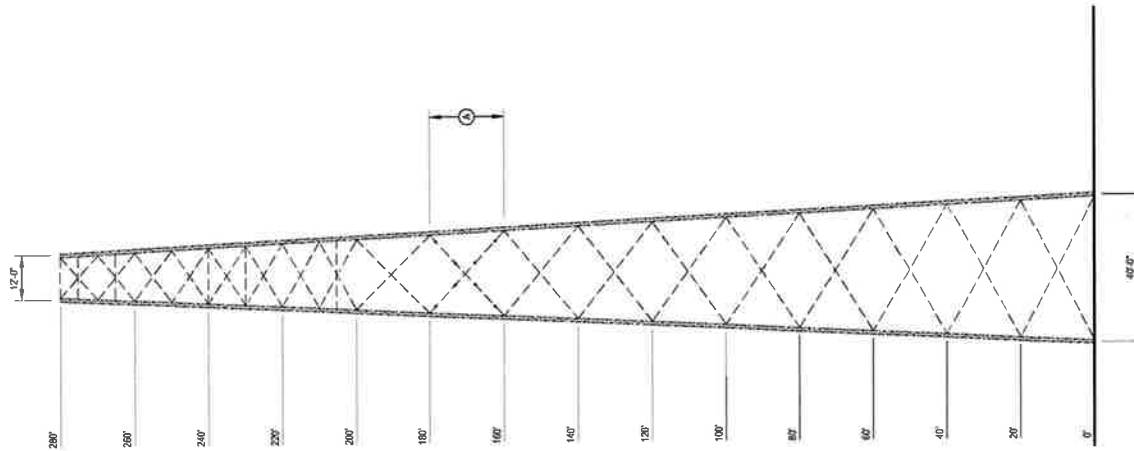
PROJECT No: 00019-0111-005-8802  
 DRAWN BY: RJK  
 DESIGNED BY: MTB  
 CHECKED BY: PJF  
 DATE: 5/21/2020

**TOWER  
 ELEVATION**

**S-1**

TOWER MODIFICATION SCHEDULE		
ELEVATION	TOWER MODIFICATION DESCRIPTION	REFERENCE SHEETS
180' TO 187'	INSTALL STITCH BOLTS AND SPACER PLATES IN EXISTING DIAGONALS	S-2

① PRIOR TO FABRICATION AND INSTALLATION, CONTRACTOR SHALL VERIFY ALL LENGTHS AND QUANTITIES GIVEN. LENGTH AND QUANTITIES PROVIDED ARE FOR QUOTING PURPOSE ONLY AND SHALL NOT BE USED FOR FABRICATION.



**TOWER ELEVATION 1**  
**S-1**



REV	DATE	DESCRIPTION

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**SITE: HIGGANUM SOUTH CT**  
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**MODIFIED 280' SELF SUPPORT TOWER**

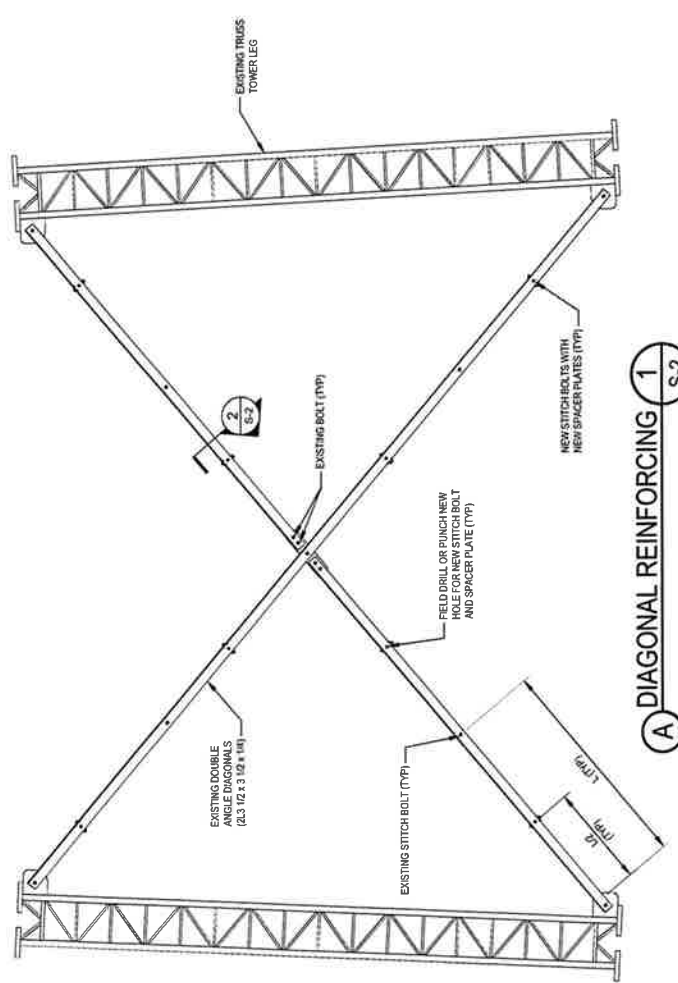
PROJECT No 001190111 005 8806  
 DRAWN BY RAK  
 DESIGNED BY MTH  
 CHECKED BY PJF  
 DATE 5/21/2020

**DIAGONAL STITCH  
 BOLT  
 REINFORCING**

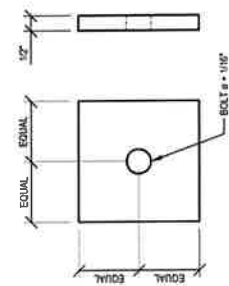
**S-2**

**MATERIAL LIST**

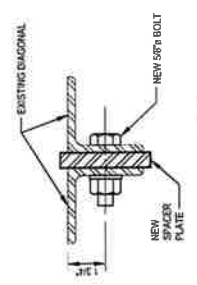
ELEVATION	QTY	MATERIAL	LENGTH
1876 TO 1882	24	SPACERPLATE 1/2" x 4"	0'-2 1/2"
	24	SF70 BOLTS	2'-1 1/4"



**A** **DIAGONAL REINFORCING** **1** **S-2**



**SPACER PLATE**



**SECTION** **2** **S-2**



REV	DATE	DESCRIPTION

# NHH-65C-R2B



6-port sector antenna, 2x 698–896 and 4x 1695–2360 MHz, 65° HPBW, 2x RET. Both high bands share the same electrical tilt.

- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- Separate RS-485 RET input/output for low and high band
- One RET for low band and one RET for both high bands to ensure same tilt level for 4x Rx or 4x MIMO

## General Specifications

<b>Antenna Type</b>	Sector
<b>Band</b>	Multiband
<b>Color</b>	Light gray
<b>Effective Projective Area (EPA), frontal</b>	0.37 m <sup>2</sup>   3.983 ft <sup>2</sup>
<b>Effective Projective Area (EPA), lateral</b>	0.31 m <sup>2</sup>   3.337 ft <sup>2</sup>
<b>Grounding Type</b>	RF connector body grounded to reflector and mounting bracket
<b>Performance Note</b>	Outdoor usage   Wind loading figures are validated by wind tunnel measurements described in white paper WP-112534-EN
<b>RF Connector Interface</b>	7-16 DIN Female
<b>RF Connector Location</b>	Bottom
<b>RF Connector Quantity, high band</b>	4
<b>RF Connector Quantity, low band</b>	2
<b>RF Connector Quantity, total</b>	6

## Remote Electrical Tilt (RET) Information, General

<b>RET Interface</b>	8-pin DIN Female   8-pin DIN Male
<b>RET Interface, quantity</b>	2 female   2 male

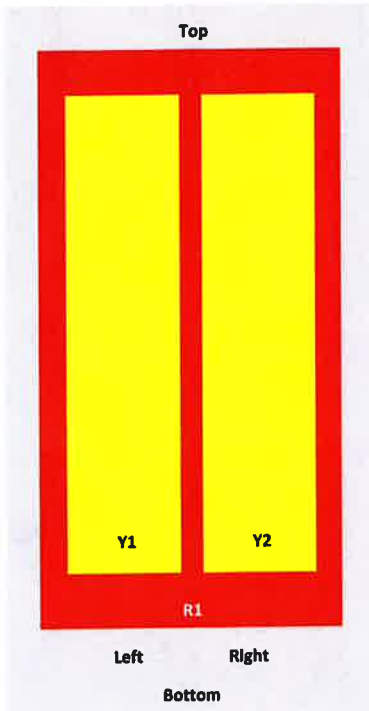
## Dimensions

<b>Width</b>	301 mm   11.85 in
<b>Length</b>	2438 mm   95.984 in
<b>Depth</b>	180 mm   7.087 in

## Array Layout

# NHH-65C-R2B

NHH



Array	Freq (MHz)	Comps	RET (dBET)	AISG RET UID
R1	698-896	1-2	1	ANXXXXXXXXXXXXX1
Y1	1695-2360	1-4	2	ANXXXXXXXXXXXXX2
Y2	1695-2360	5-8		

View from the front of the antenna  
(Sizes of colored boxes are not true depictions of array sizes)

## Electrical Specifications

<b>Impedance</b>	50 ohm
<b>Operating Frequency Band</b>	1695 – 2360 MHz   698 – 896 MHz
<b>Total Input Power, maximum</b>	900 W @ 50 °C

## Remote Electrical Tilt (RET) Information, Electrical

<b>Protocol</b>	3GPP/AISG 2.0 (Single RET)
<b>Power Consumption, idle state, maximum</b>	2 W
<b>Power Consumption, normal conditions, maximum</b>	13 W
<b>Input Voltage</b>	10–30 Vdc
<b>Internal Bias Tee</b>	Port 1   Port 3
<b>Internal RET</b>	High band (1)   Low band (1)

# NHH-65C-R2B

## Electrical Specifications

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain, dBi	16	16.1	17.3	17.7	18.3	18.2
Beamwidth, Horizontal, degrees	65	62	74	66	62	59
Beamwidth, Vertical, degrees	9	7.9	5.6	5.2	4.9	4.5
Beam Tilt, degrees	0–11	0–11	0–7	0–7	0–7	0–7
USLS (First Lobe), dB	21	18	19	20	22	18
Front-to-Back Ratio at 180°, dB	35	31	33	29	29	30
Isolation, Cross Polarization, dB	25	25	25	25	25	25
Isolation, Inter-band, dB	30	30	30	30	30	30
VSWR   Return loss, dB	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	-153	-153
Input Power per Port, maximum, watts	400	400	350	350	350	300

## Electrical Specifications, BASTA

Frequency Band, MHz	698–806	806–896	1695–1880	1850–1990	1920–2200	2300–2360
Gain by all Beam Tilts, average, dBi	15.8	15.9	16.9	17.5	18	17.9
Gain by all Beam Tilts Tolerance, dB	±0.4	±0.4	±0.4	±0.3	±0.6	±0.4
Gain by Beam Tilt, average, dBi	0°   15.9 5°   15.9 11°   15.5	0°   15.8 5°   16.0 11°   15.7	0°   16.9 4°   17.0 7°   16.9	0°   17.4 4°   17.5 7°   17.4	0°   17.9 4°   18.0 7°   18.0	0°   17.8 4°   17.9 7°   17.9
Beamwidth, Horizontal Tolerance, degrees	±1.2	±1.6	±5.3	±3.4	±6	±3.1
Beamwidth, Vertical Tolerance, degrees	±0.6	±0.4	±0.3	±0.2	±0.2	±0.2
USLS, beampeak to 20° above beampeak, dB	15	14	17	16	17	15
Front-to-Back Total Power at 180° ± 30°, dB	25.6	23.8	28	25	25	24
CPR at Boresight, dB	18	26	20	25	20	17
CPR at Sector, dB	15	9	11	10	8	2

## Material Specifications

Radiator Material

Copper | Low loss circuit board

# NHH-65C-R2B

**Reflector Material** Aluminum

## Mechanical Specifications

<b>Wind Loading at Velocity, frontal</b>	393.0 N @ 150 km/h   88.8 lbf @ 150 km/h
<b>Wind Loading at Velocity, lateral</b>	330.0 N @ 150 km/h   74.2 lbf @ 150 km/h
<b>Wind Loading at Velocity, maximum</b>	170.2 lbf @ 150 km/h   757.0 N @ 150 km/h
<b>Wind Speed, maximum</b>	241 km/h   149.75 mph

## Packaging and Weights

<b>Width, packed</b>	409 mm   16.102 in
<b>Depth, packed</b>	299 mm   11.772 in
<b>Length, packed</b>	2561 mm   100.827 in
<b>Net Weight, without mounting kit</b>	23.4 kg   51.588 lb
<b>Weight, gross</b>	36.1 kg   79.587 lb

## Regulatory Compliance/Certifications

<b>Agency</b>	<b>Classification</b>
CHINA-ROHS	Above maximum concentration value
ISO 9001:2015	Designed, manufactured and/or distributed under this quality management system
REACH-SVHC	Compliant as per SVHC revision on <a href="http://www.commscope.com/ProductCompliance">www.commscope.com/ProductCompliance</a>
ROHS	Compliant/Exempted



## Included Products

**BSAMNT-3** — Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.

## \* Footnotes

**Performance Note** Severe environmental conditions may degrade optimum performance

# SAMSUNG

## Dual-Band Radio Unit AWS/PCS (B66/B2)

RFV01U-D1A

Samsung's RFV01U-D1A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D1A RU targets dual-band support across Band 66 (AWS) and Band 2 (PCS), making it an ideal product for broad coverage footprints across multiple common mid-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributed- and central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

### Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- Convection cooled, silent operation
- Built-in Broadcast Auxiliary Services (BAS) filter ensures compliant AWS operation without impacting footprint

### Key Technical Specifications

Duplex Type: FDD

Operating Frequencies:

B66: DL(2,110-2,180MHz)/UL(1,710-1,780MHz)

B2: DL(1,930-1,990MHz)/UL(1,850-1,910MHz)

Instantaneous Bandwidth:

70MHz(B66) + 60MHz(B2)

RF Chain: 4T4R/2T4R/2T2R

Output Power: Total 320W

DU-RU Interface: CPRI (10Gbps)

Dimensions: 380 x 380 x 255mm (36.8L)

Weight: 38.3kg

Input Power: -48V DC

Operating Temp.: -40 - 55°(w/o solar load)

Cooling: Natural convection



# SAMSUNG

## Dual-Band Radio Unit 700/850MHz (B13/B5)

RFV01U-D2A

Samsung's RFV01U-D2A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D2A RU targets dual-band support across Band 13 (700MHz) and Band 5 (850MHz), making it an ideal product for broad coverage footprints across multiple common low-end, long-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributed- and central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

### Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- Convection cooled, silent operation

### Key Technical Specifications

Duplex Type: FDD

Operating Frequencies:

B13: DL(746-756MHz)/UL(777-787MHz)

B5: DL(869-894MHz)/UL(824-849MHz)

Instantaneous Bandwidth: 10MHz(B13) + 25MHz(B5)

RF Chain: 4T4R/2T4R/2T2R

Output Power: Total 320W

DU-RU Interface: CPRI (10Gbps)

Dimensions: 380 x 380 x 207mm (29.9L)

Weight: 31.9kg

Input Power: -48V DC

Operating Temp.: -40 - 55°(w/o solar load)

Cooling: Natural convection



# HYBRIFLEX® RRH Hybrid Cable Solution 6x12, 6AWG Low-Inductance, 1-1/4", Single-Mode Fiber With DLC Connectors



HYBRIFLEX Series



DC Wire Insulator

RFS' HYBRIFLEX Remote Radio Head (RRH) hybrid feeder cabling solution combines optical fiber and DC power for RRHs in a single lightweight aluminum corrugated cable, making it the world's most innovative solution for RRH deployments.

This low-inductance version of HYBRIFLEX allows mobile operators deploying an RRH architecture to deploy >400ft sites without the danger of power-cycling their RRHs due to voltage swings, which could occur in some specific instances. It combines bend-insensitive single-mode fiber (12 pairs of DLC connectors), 6 pairs of low-inductance DC wires and 9 pairs of 18AWG wires used to carry alarm signals. The package also includes special RFS-designed DC insulating boot, used to properly protect and insulate the DC wires after stripping the jacket, avoiding possible short-circuits while wiring it to the distribution boxes. Standard RFS CELLFLEX® accessories can be used with HYBRIFLEX cable.

### FEATURES / BENEFITS

- ➔ DC Wire Insulator (Patent pending) – Used at the DC wire connection in distribution boxes, prevents potential short circuits
- ➔ Aluminum corrugated armor with outstanding bending characteristics – Minimizes installation time and enables mechanical protection and shielding
- ➔ Same accessories as 1-1/4" coaxial cable – Saves installation costs and time
- ➔ Outer conductor grounding – Eliminates typical grounding requirements and saves on installation costs
- ➔ Lightweight solution and compact design – Decreases tower loading
- ➔ Robust cabling – Eliminates need for expensive cable trays and ducts
- ➔ Optical fiber and power cables housed in single corrugated cable – Saves CAPEX by standardizing RRH cable installation and reducing installation requirements
- ➔ Outdoor, flame-retardant jacket – Ensures long-lasting cable protection

### Technical Features

#### STRUCTURE

Cable Type		HYBRIFLEX® Low Inductance
Size		1-1/4"
Fire Performance		Flame Retardant
Length	m (ft)	36.57 (120)

#### MECHANICAL SPECIFICATIONS

Outer Diameter Nominal	mm (in)	39 (1.54)
Cable Weight	kg/m (lb/ft)	2.52 (1.7)
Minimum Bending Radius, Single Bend	mm (in)	152 (6)
Minimum Bending Radius, Multi Bends	mm (in)	254 (10)
Recommended / Maximum Clamp Spacing	m (ft)	1 / 1.2 (3.25 / 4)

#### DC POWER CABLE SPECIFICATIONS

Number of DC Pairs		6
Maximum DC-Resistance Power Cable	Ω/km (Ω/kft)	1.4 (0.42)
Cross Section of Power Cable	mm² (AWG)	13.3 (6)
DC Wire Jacket Material		PVC/Nylon
DC Cable Diameter	mm (in)	9.3 (0.365)
DC Cable Jacket		PVC/Nylon
DC Standards (Meets or Exceeds)		For use in Type RHC per UL 2882, PVC/Nylon, RoHS/REACH Compliant
Break-out length	mm(in)	812.8
DC Cable sealing method		Semi-rigid flame-retarded polyolefin, with hot melt adhesive
Alarm Wire		18 (9 twisted pairs), 0.8mm2 (18AWG)

#### CABLE JACKET

UV-Protection Individual and External Jacket		Yes
--	--	-----

#### ARMOR SPECIFICATIONS

Armor Type		Corrugated Aluminum
Maximum DC-Resistance of Armor	Ω/km (Ω/kft)	0.9 (0.27)
Diameter Corrugated Armor	mm (in)	36 (1.42)

#### F/O CABLE SPECIFICATIONS

F/O Cable Type		Single-Mode, Bend Tolerant
Number of F/O Pairs		12
Core/Clad	µm	9 / 125
Secondary Protection Nominal	µm (in)	900 (0.035)
Single Bending Radius	mm (in)	137 (5.4)
F/O Standards (Meets or Exceeds)		UL Listed Type OFNR (UL1666), RoHS Compliant
Optical Loss	dB/Km	0.5 @ 1310 nm 0.5 @ 1550 nm
Fiber Termination End 1		DLC Connectors
Fiber Termination End 2		DLC Connectors
FO Break-out length	mm(in)	939.8 +/-50.8 (37 +/-2)
Cable sealing method		Semi-rigid flame-retarded polyolefin, with hot melt adhesive

#### TESTING AND ENVIRONMENTAL

Storage Temperature	°C (°F)	-40 to 70 (-40 to 158 )
Operation Temperature	°C (°F)	-40 to 65 (-40 to 158 )
Installation Temperature	°C (°F)	-20 to 65 (-4 to 149 )
Jacket Specifications		UL2882 Type RHC, UL listed
Alarm Wire Standards (Meets or Exceeds)		UL Standard 1063, 1581 VW-1, MTW Oil and Gasoline RES1 SUNRES (Cable meets UL requirements), RoHS/REACH Compliant



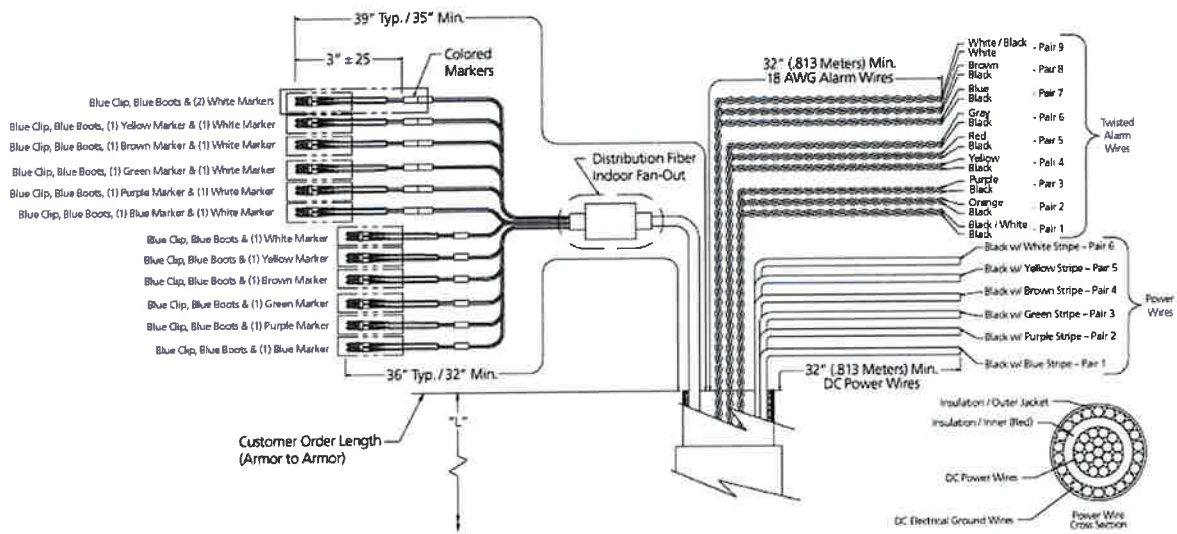
# HYBRIFLEX<sup>®</sup> RRH Hybrid Cable Solution 6x12, 6AWG Low-Inductance, 1-1/4", Single-Mode Fiber With DLC Connectors

**External Document Links**

- Installation Guidelines
- Quick Ship 2.0 Program Information

**Notes**

**External Link Reference**



Drawing

# **ATTACHMENT 3**

Site Name: Higganum S (Haddam)		General		Power		Density		CALC.		MAX.		FRACTIO	
Tower Height: 280 Ft		# OF CHAN.	WATTS ERP	HEIGHT	POWER DENS	FREQ.	PERMISS. EXP.	N MPE	Total				
*Eversource Energy	1	3428	240	6256	0.0225	1.0000	0.23%						
*Eversource Energy	1	776	123	2145	0.0204	1.0000	0.20%						
*Sprint	8	778	144	2500	0.1175	1.0000	1.18%						
*Sprint	4	859	144	800	0.0649	0.5333	1.22%						
*Sprint	4	1440	144	1900	0.1088	1.0000	1.09%						
*Northeast	1	501	251	37.1	0.0010	0.2000	0.05%						
*Northeast	1	335	274	150	0.0006	0.2000	0.03%						
*Northeast	1	335	274	166	0.0006	0.2000	0.03%						
*Northeast	1	2500	274	450	0.0011	0.3000	0.04%						
*Northeast	1	335	154	157	0.0018	0.2000	0.09%						
*Northeast	1	1005	214	150	0.0028	0.2000	0.14%						
*Northeast	1	100	74	47.96	0.0024	0.2000	0.12%						
*Middlesex Fire	1	100	274	45.98	0.0002	0.2000	0.01%						
*Haddam Fire	1	316	64	46.24	0.0100	0.2000	0.50%						
*Operations	1	178	214	42.06	0.0005	0.2000	0.03%						
*NL County Fire	1	316	111	33.76	0.0033	0.2000	0.17%						
*MED 9	1	150	244	460	0.0001	0.3067	0.00%						
*Hi-Band TRP-TRP	1	878	144	150	0.0055	0.2000	0.27%						
*Operations	1	398	114	450	0.0010	0.3000	0.03%						
*MS to Talcott	1	9927	269	6805	0.0005	1.0000	0.00%						
*MW to CT Yankee	1	9957	269	6815	0.0005	1.0000	0.00%						
*MW to Madison	1	9869	269	6785	0.0005	1.0000	0.00%						
*MW to Talcott	1	845	194	6000	0.0001	1.0000	0.00%						
*MW to Millstone	2	9782	194	6000	0.0019	1.0000	0.02%						
*MW to Troop F	1	5413	187	6525	0.0006	1.0000	0.01%						
*MW to Mt. Beseck	1	5413	185	6525	0.0006	1.0000	0.01%						
*MW to Jenks Hill	1	18741	94	17700	0.0076	1.0000	0.08%						
*Troop F 800 MHz	5	200	169	866	0.0005	0.5773	0.01%						
*Troop K 800 MHz	5	200	234	866	0.0005	0.5773	0.01%						
*Interop 800 MHz	5	200	169	866	0.0005	0.5773	0.01%						
*Educational TV	1	151	234	2500	0.0000	1.0000	0.00%						
*VoiceStream	8	208	125	1930	0.0423	1.0000	0.42%			5.99%			
*Northeast Utilities	6-foot dish owned by State Police was proposed to be added but no power density was provided.												
<b>VZW PCS</b>	<b>4</b>	<b>1531</b>	<b>145</b>	<b>0.1047</b>	<b>1970</b>	<b>1.0</b>	<b>10.47%</b>						
<b>VZW Cellular</b>	<b>4</b>	<b>460</b>	<b>145</b>	<b>0.0315</b>	<b>880</b>	<b>0.58666</b>	<b>5.36%</b>						
<b>VZW AWS</b>	<b>4</b>	<b>1702</b>	<b>145</b>	<b>0.1164</b>	<b>2145</b>	<b>1.0</b>	<b>11.64%</b>						
<b>VZW 700</b>	<b>4</b>	<b>965</b>	<b>145</b>	<b>0.0660</b>	<b>746</b>	<b>0.4973333</b>	<b>13.27%</b>			<b>46.74%</b>			
* Source: Siting Council													

# **ATTACHMENT 4**

**Report Date:** May 21, 2020

**Client:** Hudson Design Group  
110 Washington Ave, Fourth Floor  
North Haven, CT 06473  
Attn: Sylvester Bhembe  
978.557.5553  
sbhembe@hudsondesigngrouppllc.com

**Structure:** Modified 280-ft Self Support Tower  
**FCC ASR #:** 1285236  
**Site Name:** Higganum South CT  
**Site Address:** 330 Porkorny St  
**City, County, State:** Haddam, Middlesex County, CT  
**Latitude, Longitude:** 41° 26' 36.9", -72 ° 33' 58.9"

**PJF Project:** A00019-0111.005.8800

Paul J. Ford and Company is pleased to submit this "**Structural Modification Report**" to determine the tower stress level.

**Analysis Criteria:**

**Reference Standard:** 2018 Connecticut State Building Code with the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1.

**Ultimate Wind Speed:** 140 mph 3-second gust wind speed without ice  
**Nominal Wind Speed:** 108 mph 3-second gust wind speed without ice  
**Ice Wind Speed:** 50 mph 3-second gust wind speed with 0.75" ice  
**Service Wind Speed:** 60.0 mph (Serviceability) without ice  
**TIA-222 Criteria:** Structure Class III, Topographic Category I, Exposure Category C

**Proposed Appurtenance Loads:**

The structure was analyzed with the addition of the proposed appurtenance loads shown in Table 1 combined with the existing and reserved loads shown in Table 2 of this report.

**Summary of Analysis Results:**

**Modified Structure:** Pass – 98.6%  
**Existing Foundation:** Pass – 86.0%

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and Hudson Design Group. If you have any questions or need further assistance on this or any other projects, please give us a call.

Respectfully Submitted by:  
Paul J. Ford and Company

*Michael T Bange*

Michael Bange, EI  
Structural Designer  
mbange@pauljford.com

*PJF*



*Joseph Pachicarah Jacobs*

05.21.2020

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**1) INTRODUCTION**

This tower is a 280 ft Self Support tower designed by Valmont in February of 2012.

**2) ANALYSIS CRITERIA**

**TIA-222 Revision:** TIA-222-G  
**Risk Category:** III  
**Nominal Wind Speed:** 108 mph  
**Exposure Category:** C  
**Topographic Factor:** 1  
**Ice Thickness:** 0.75 in  
**Wind Speed with Ice:** 50 mph  
**Service Wind Speed:** 60 mph

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
145.0	145.0	3	Sitepro1	(3) VFA12-RRU Sector Frame	48	1/2" – 6' jumper	-
		3	-	2 Std. Stabilizing Pipe			
		3	-	2.5 STD Pipe Mount Reinforcing			
		3	commscope	BSAMNT-SBS-1-2 (Mount Bracket)			
		6	commscope	NHH-65C-R2B			
		3	samsung telecommunications	B2/B66A RRH-BR049			
		3	samsung telecommunications	B5/B13 RRH-BR04C			
		3	Sitepro1	SFS-V Sector Frame Stabilizer			

**Table 2 – Existing Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
280.0	280.0	1	-	FAA L-864 Beacon	1	½	1
279.0	279.0	1	-	ANT150F6-3	1	1-5/8 7/8	1
		1	-	DB538-G			
		1	kreco	Kreco CO-35A			
		3	tower mounts	4' x 2" Std. Pipe Mount			
276.0	276.0	3	rfs celwave	PAL8	3	EW63	1
		4	tower mounts	8' x 2" Sch 40 Pipe Mount			
266.0	266.0	1	rfs celwave	PAL8	1	EW63	1
261.0	261.0	1	-	10' 8-Bay Dipole	2	7/8	1
		1	tower mounts	6' Side Arm Mount			
260.0	265.5	1	decibel	DB589-Y	2	1-5/8 3/8	1
	260.0	1	-	12" x 12" x 6" TMA			
		1	tower mounts	6' Side Arm Mount			
	254.5	1	decibel	DB589-Y			
255.0	255.0	1	-	DB212-C	1	7/8	1
		1	tower mounts	6' Side Arm Mount			
241.0	241.0	1	sinclair	SD110-SFXPASNM	1	7/8	1
		1	tower mounts	6' Side Arm Mount			
240.0	240.0	1	rfs celwave	PADX6-59AC	1	7/8 EW63	1
		1	kreco	CO-36A			
		1	tower mounts	6' Side Arm Mount			
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
235.2	240.8	1	-	SE419-SF3P4LDF w/ Mount Pipe	2	1-5/8	1
	235.2	1	tower mounts	6' Side Arm Mount	1	1/2	
	229.5	1	-	SE419-SF3P4LDF w/ Mount Pipe	1	3/8	
230.0	230.0	1	tower mounts	3' Side Arm Mount	1	WE63	1
		1	rfs celwave	PAL8			
		1	comprod	Comprod 531-70HD			
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
220.0	220.0	1	rfs celwave	PAL8	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
216.0	216.0	1	sinclair	SD110-SFXPASNM	2	7/8	1
		1	telewave	ANT450F10			
		2	tower mounts	6' Side Arm Mount			
205.5	205.5	1	rfs celwave	PA10-59	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
204.0	204.0	1	tower mounts	3' Side Arm Mount	1	1-5/8	1
	200.0	1	sinclair	SC479-HF1LDF			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
200.0	206.0	1	sinclair	SC479-HF1LDF	3	1-5/8 1/2	1
	200.0	2	tower mounts	3' Side Arm Mount			
		1	-	TMA (16" x 12" x 6")			
		1	telewave	Telewave ANT900D6-9			
		1	tower mounts	6' Side Arm Mount			
194.0	1	sinclair	SC479-HF1LDF				
197.0	197.0	1	rfs celwave	PAL6-59	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
195.0	195.0	1	rfs celwave	PA10-59	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
175.0	181.0	1	antel	BCR-80010:90	4	1-5/8 1/2 3/8	1
		1	sinclair	SC479-HF1LDF			
	175.0	1	-	TMA (16" x 12" x 6")			
		2	tower mounts	6' Side Arm Mount			
		1	antel	BCR-80010:90			
169.0	1	sinclair	SC479-HF1LDF				
168.0	168.0	1	tower mounts	3' Side Arm Mount	1	7/8	1
		1	telewave	ANT450F6			
163.0	163.0	1	rfs celwave	PAD6-65AC	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
155.0	155.0	3	tower mounts	12' V Frame	6	1-5/8	1
		6	alcatel lucent	FD RRH 2x50 800	4	1-1/4	2
		3	commscope	NNVV-65B-R4			
		3	nokia	FZHN (TD-RRH8 x 20-25)			
		3	rfs celwave	APXVTM14-C			
		3	rfs celwave	APXVSP18-C	-	-	3
		3	alcatel lucent	FD-RRH-4x45-1900			
145.0	145.0	3	commscope	HBXX-6517DS-A2M	3	6 x 12 Hybrid Cables	1
		3	commscope	LNx-6515DS-A1M			
		3	raycap	RC3DC-3315-PF-48			
		3	alcatel lucent	B13 RRH4X30-4R	-	-	3
		3	commscope	HBXX-6517DS-A2M			
		3	commscope	LNx-6515DS-A1M			
		1	rfs celwave	DB-T1-6Z-8AB-0Z			
3	tower mounts	Generic Sector Frame					
140.0	140.0	3	-	FAA L-810 Sidelight	1	3/8	1
130.0	130.0	1	kreco	CO-36A	1	7/8	1
		1	tower mounts	6' Side Arm Mount			
128.0	128.0	1	telewave	ANT450F6	1	7/8	1
		1	tower mounts	6' Side Arm Mount			
126.0	126.0	1	kathrein	PRF-950	1	7/8	1
		1	tower mounts	6' Side Arm Mount			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
124.0	124.0	1	telewave	ANT450F6	1	7/8	1
		1	tower mounts	6' Side Arm Mount			
123.0	123.0	1	rfs celwave	SBX4-W60AC2	1	E60	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
117.0	117.0	1	tower mounts	3' Side Arm Mount	1	7/8	1
		1	kathrein	PRF-950			
116.0	116.0	2	tower mounts	3' Side Arm Mount	1	7/8	1
		1	browning	BR6155			
	113.0	1	telewave	ANT400D			
104.0	104.0	1	rfs celwave	PAD6-65AC	1	EW63	1
		1	tower mounts	8' x 2" Sch 40 Pipe Mount			
97.0	97.0	1	Tower mounts	3' Side Arm Mount	1	7/8	1
		1	Browning	BR6155			
55.0	55.0	1	tower mounts	3' Side Arm Mount	1	7/8	1
		1	astron wireless	V-1500			
50.0	50.0	1	Tower mounts	3' Side Arm Mount	1	1/2	1
		1	telewave	ANT790-S2			

- Notes:  
 1) Existing Equipment  
 2) Reserved Equipment  
 3) Equipment to be Removed. Not considered in this analysis.

### 3) ANALYSIS PROCEDURE

**Table 3 - Documents Provided**

Document	Remarks	Reference
Tower Manufacturer Drawings	Valmont, 2/29/2012	240898
Geotechnical Report	8/1/2011	-
Structural Analysis	Centek, 10/31/2018	17159.10
Mount Modifications	HDG, 4/15/2020	Higganum
Mount Analysis	HDG, 5/6/2019	-

#### 3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

### 4) ANALYSIS RESULTS

**Table 4 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
T1	280 - 270	Leg	Valmont 207628 (12x1.25)	2	-4.91	142.49	26.7	Pass
T2	270 - 260	Leg	Valmont 207628 (12x1.25)	18	-10.50	142.49	20.4	Pass
T3	260 - 240	Leg	Valmont 207628 (12x1.25)	28	-38.91	142.49	27.3	Pass
T4	240 - 220	Leg	Valmont 207628 (12x1.25)	43	-54.37	142.49	53.6	Pass
T5	220 - 210	Leg	Valmont 195557 (12x1.75)	64	-97.23	301.49	46.6	Pass
T6	210 - 200	Leg	Valmont 195557 (12x1.75)	73	-120.43	301.49	51.9	Pass
T7	200 - 180	Leg	Valmont 211843 (12x2)	85	-161.25	356.29	75.6	Pass
T8	180 - 160	Leg	Valmont 208334 (12x2.25)	94	-221.84	451.15	49.2	Pass
T9	160 - 140	Leg	Valmont 208334 (12x2.25)	103	-282.34	451.15	76.2	Pass
T10	140 - 120	Leg	Valmont 208335 (12x2.5)	112	-352.18	557.27	63.2	Pass
T11	120 - 100	Leg	Valmont 208337 (12x2.75)	121	-422.72	674.68	62.7	Pass
T12	100 - 80	Leg	Valmont 208338 (12x3)	130	-495.05	803.44	61.6	Pass
T13	80 - 60	Leg	Valmont 208338 (12x3)	139	-567.48	803.44	70.6	Pass
T14	60 - 40	Leg	Valmont 208339 (12x3.25)	148	-639.38	943.57	67.8	Pass
T15	40 - 20	Leg	Valmont 208339 (12x3.25)	157	-713.20	943.57	75.6	Pass
T16	20 - 0	Leg	Valmont 208339 (12x3.25)	167	-782.36	943.57	82.9	Pass
T1	280 - 270	Diagonal	L 3 x 3 x 5/16	7	-3.78	17.33	21.8	Pass
T2	270 - 260	Diagonal	L 3 x 3 x 5/16	20	-6.15	15.59	39.4	Pass
T3	260 - 240	Diagonal	L 3 x 3 x 5/16	32	-8.06	12.75	63.3	Pass
T4	240 - 220	Diagonal	L 4 x 4 x 1/4	53	-13.52	20.95	64.5	Pass
T5	220 - 210	Diagonal	L 4 x 4 x 1/4	68	-15.71	19.15	82.0	Pass
T6	210 - 200	Diagonal	L 4 x 4 x 1/4	77	-15.68	17.55	89.3	Pass
T7	200 - 180	Diagonal	2L 3.5 x 3.5 x 1/4 (1/2)	89	-25.35	29.00	87.4	Pass
T8	180 - 160	Diagonal	2L 3.5 x 3.5 x 1/4 (1/2)	98	-26.57	27.90	95.2	Pass
T9	160 - 140	Diagonal	2L 4 x 4 x 3/8 (1/2)	107	-31.45	51.86	60.6	Pass
T10	140 - 120	Diagonal	2L 4 x 4 x 3/8 (1/2)	116	-34.92	47.03	74.3	Pass
T11	120 - 100	Diagonal	2L 4 x 4 x 3/8 (1/2)	125	-36.51	43.07	84.8	Pass
T12	100 - 80	Diagonal	2L 5 x 5 x 5/16 (1/2)	134	-38.50	63.83	60.3	Pass
T13	80 - 60	Diagonal	2L 5 x 5 x 5/16 (1/2)	143	-39.77	58.27	68.3	Pass
T14	60 - 40	Diagonal	2L 5 x 5 x 5/16 (1/2)	152	-41.65	53.32	78.1	Pass
T15	40 - 20	Diagonal	2L 5 x 5 x 5/16 (1/2)	161	-42.05	48.93	85.9	Pass
T16	20 - 0	Diagonal	2L 5 x 5 x 5/16 (1/2)	170	-44.37	45.01	98.6	Pass
T1	280 - 270	Secondary Horizontal	L 2.5 x 2.5 x 5/16	13	-2.02	10.72	18.9	Pass

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail	
T2	270 - 260	Secondary Horizontal	L 2.5 x 2.5 x 5/16	25	-0.93	9.03	10.3	Pass	
T6	210 - 200	Secondary Horizontal	L 5 x 5 x 3/8	82	-2.09	41.61	5.0	Pass	
T1	280 - 270	Top Girt	L 3.5 x 3.5 x 5/16	6	-0.44	13.72	3.2	Pass	
T4	240 - 220	Top Girt	L 5 x 5 x 3/8	47	-1.65	25.80	6.4	Pass	
T4	240 - 220	Mid Girt	L 5 x 5 x 3/8	50	-2.30	22.62	10.2	Pass	
							Summary		
							Leg (T16)	82.9	Pass
							Diagonal (T16)	98.6	Pass
							Secondary Horizontal (T1)	18.9	Pass
							Top Girt (T4)	6.4	Pass
							Mid Girt (T4)	10.2	Pass
							Bolt Checks	89.7	Pass
							Rating =	98.6	Pass

**Table 5 - Tower Component Stresses vs. Capacity**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	74.1	Pass
1	Base Foundation Structural	0	86.0	Pass
1	Base Foundation Soil Interaction	0	60.0	Pass

<b>Structure Rating (max from all components) =</b>	<b>98.6%</b>
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Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

#### 4.1) Recommendations

Install the proposed modifications per the attached drawings.

**Table 6 - Microwave Dish Tilt (Sway) Results for 60 mph Rev G Service**

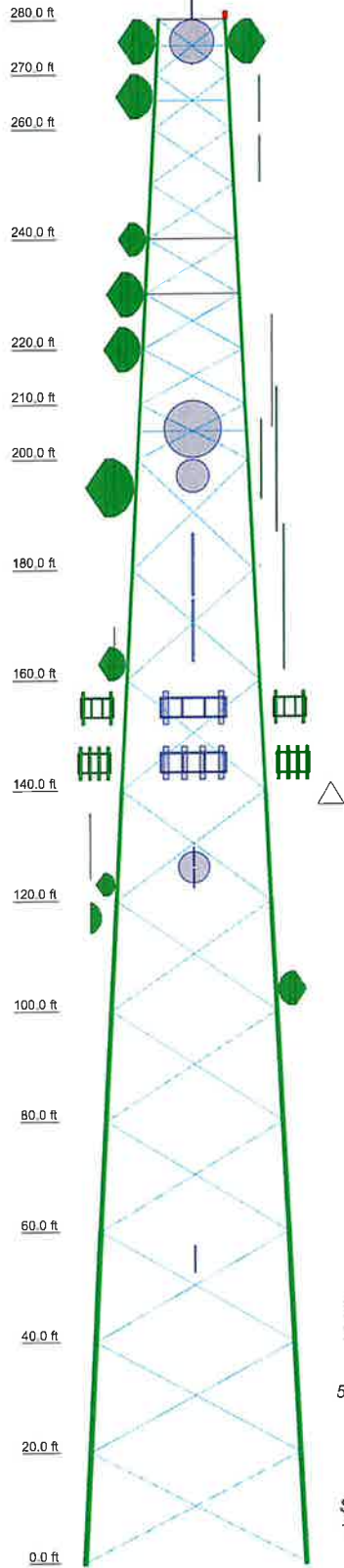
**Critical Deflections and Radius of Curvature - Service Wind**

<i>Elevation</i>	<i>Appurtenance</i>	<i>Gov. Load Comb.</i>	<i>Deflection</i>	<i>Tilt</i>	<i>Twist</i>	<i>Radius of Curvature</i>
<i>ft</i>			<i>in</i>	<i>°</i>	<i>°</i>	<i>ft</i>
276.00	PAL8	47	4.165	0.1287	0.0276	778479
266.00	PAL8	47	3.892	0.1282	0.0275	Inf
240.00	PADX6-59AC	47	3.194	0.1206	0.0263	144254
230.00	PAL8	47	2.939	0.1142	0.0250	110070
220.00	PAL8	47	2.694	0.1081	0.0230	97658
205.50	PA10-59	47	2.357	0.1016	0.0197	147333
197.00	PAL6-59	47	2.166	0.0972	0.0184	80190
195.00	PA10-59	47	2.123	0.0961	0.0181	83604
163.00	RFS PAD6-65AC	47	1.495	0.0807	0.0136	92794
126.00	PRF-950	47	0.921	0.0598	0.0102	113341
123.00	SBX4-W60AC2	47	0.881	0.0583	0.0099	114333
117.00	PRF-950	47	0.804	0.0552	0.0094	116244
104.00	RFS PAD6-65AC	47	0.650	0.0487	0.0083	120308

**APPENDIX A**  
**TNXTOWER OUTPUT**



Section	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40					
Legs	Valmont 207628 (12x1.25)		Valmont 208334 (12x2.25)		Valmont 208338 (12x3)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)		Valmont 208339 (12x3.25)					
Log Grade	L 3 x 3 x 5/16		L 4 x 4 x 1/4		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)			
Diagonals	L 3 x 3 x 5/16		L 4 x 4 x 1/4		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)		L 4 x 4 x 3/8 (1/2)			
Diagonal Grade	A572-50		A36		A36		A36		A36		A36		A36		A36		A36		A36		A36		A36		A36		A36			
Top Girts	L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8		L 5 x 5 x 3/8			
Mid Girts	N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.		N.A.			
Sec. Horizontals	L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16		L 2.5 x 2.5 x 5/16			
Face Width (ft)	40		40		40		40		40		40		40		40		40		40		40		40		40		40			
# Panels @ (ft)	12		12		12		12		12		12		12		12		12		12		12		12		12		12			
Weight (K)	113.3		12.8		12.6		12.4		11.3		11.3		11.1		10 @ 20		9.6		8.5		7.7		5.9		5.3		2.8		1.9	



### SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	Valmont 195557 (12x1.75)	D	Valmont 208337 (12x2.75)
B	Valmont 211843 (12x2)	E	L 3.5 x 3.5 x 5/16
C	Valmont 208335 (12x2.5)	F	L 5 x 5 x 3/8

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

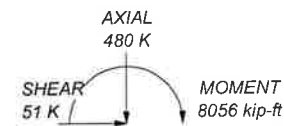
- ### TOWER DESIGN NOTES
1. Tower is located in Middlesex County, Connecticut.
  2. Tower designed for Exposure C to the TIA-222-G Standard.
  3. Tower designed for a 108 mph wind in accordance with the TIA-222-G Standard.
  4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
  5. Deflections are based upon a 60 mph wind.
  6. Tower Structure Class III.
  7. Topographic Category 1 with Crest Height of 0.00 ft
  8. TOWER RATING: 98.6%

ALL REACTIONS  
ARE FACTORED

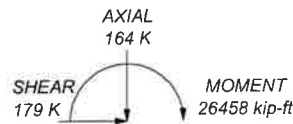
MAX. CORNER REACTIONS AT BASE:

DOWN: 618 K  
SHEAR: 108 K

UPLIFT: -686 K  
SHEAR: 94 K



TORQUE 108 kip-ft  
50 mph WIND - 0.7500 in ICE



TORQUE 360 kip-ft  
REACTIONS - 108 mph WIND

<b>Paul J. Ford and Company</b> 250 E. Broad St., Ste 600 Columbus, OH 43215 Phone: 614-221-6679 FAX:	<b>Job: 280-ft Self Support Tower Haddam, CT</b>		
	Project: <b>00019-0111</b>		
	Client: Hudson Design Group	Drawn by: Michael Bange	App'd:
	Code: TIA-222-G	Date: 05/21/20	Scale: NTS
	Path: G:\TOWER\200_Mar30\19\00019-0111_Haddam\Sub\CT\001-6805-020-10X\00019-0111-021-8602.dwg		Dwg No. <b>E-1</b>

## Tower Input Data

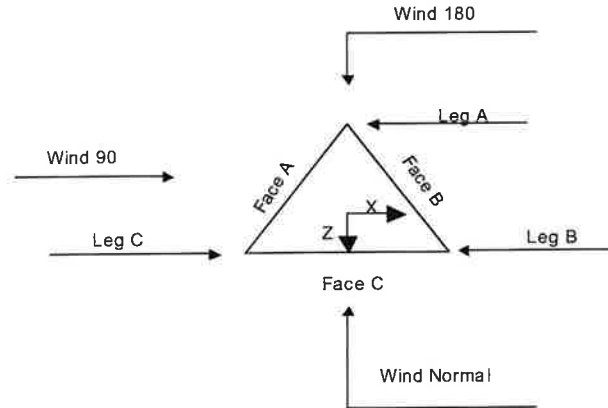
The main tower is a 3x free standing tower with an overall height of 280.00 ft above the ground line.  
 The base of the tower is set at an elevation of 0.00 ft above the ground line.  
 The face width of the tower is 12.00 ft at the top and 40.00 ft at the base.  
 This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- 1) Tower is located in Middlesex County, Connecticut.
- 2) ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
- 3) Basic wind speed of 108 mph.
- 4) Structure Class III.
- 5) Exposure Category C.
- 6) Topographic Category 1.
- 7) Crest Height 0.00 ft.
- 8) Nominal ice thickness of 0.7500 in.
- 9) Ice thickness is considered to increase with height.
- 10) Ice density of 56 pcf.
- 11) A wind speed of 50 mph is used in combination with ice.
- 12) Deflections calculated using a wind speed of 60 mph.
- 13) Pressures are calculated at each section.
- 14) Stress ratio used in tower member design is 1.
- 15) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification ✓ Use Code Stress Ratios ✓ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile  Include Bolts In Member Capacity  Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric	Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate Use Clear Spans For Wind Area ✓ Use Clear Spans For KL/r Retension Guys To Initial Tension Bypass Mast Stability Checks ✓ Use Azimuth Dish Coefficients ✓ Project Wind Area of Appurt.  Autocalc Torque Arm Areas  Add IBC .6D+W Combination ✓ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs	Use ASCE 10 X-Brace Ly Rules ✓ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation ✓ Consider Feed Line Torque ✓ Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption  <div style="text-align: center; background-color: #e0e0e0; padding: 2px;"><b>Poles</b></div> Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
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**Triangular Tower**

**Tower Section Geometry**

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	280.00-270.00			12.00	1	10.00
T2	270.00-260.00			13.00	1	10.00
T3	260.00-240.00			14.00	1	20.00
T4	240.00-220.00			16.00	1	20.00
T5	220.00-210.00			18.00	1	10.00
T6	210.00-200.00			19.00	1	10.00
T7	200.00-180.00			20.00	1	20.00
T8	180.00-160.00			22.00	1	20.00
T9	160.00-140.00			24.00	1	20.00
T10	140.00-120.00			26.00	1	20.00
T11	120.00-100.00			28.00	1	20.00
T12	100.00-80.00			30.00	1	20.00
T13	80.00-60.00			32.00	1	20.00
T14	60.00-40.00			34.00	1	20.00
T15	40.00-20.00			36.00	1	20.00
T16	20.00-0.00			38.00	1	20.00

**Tower Section Geometry (cont'd)**

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	280.00-270.00	10.00	X Brace	No	Yes	0.0000	0.0000
T2	270.00-260.00	10.00	X Brace	No	Yes	0.0000	0.0000
T3	260.00-240.00	10.00	X Brace	No	No	0.0000	0.0000
T4	240.00-220.00	10.00	X Brace	No	No	0.0000	0.0000
T5	220.00-210.00	10.00	X Brace	No	No	0.0000	0.0000
T6	210.00-200.00	10.00	X Brace	No	Yes	0.0000	0.0000
T7	200.00-180.00	20.00	X Brace	No	No	0.0000	0.0000

Tower Section	Tower Elevation ft	Diagonal Spacing ft	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset in	Bottom Girt Offset in
T8	180.00-160.00	20.00	X Brace	No	No	0.0000	0.0000
T9	160.00-140.00	20.00	X Brace	No	No	0.0000	0.0000
T10	140.00-120.00	20.00	X Brace	No	No	0.0000	0.0000
T11	120.00-100.00	20.00	X Brace	No	No	0.0000	0.0000
T12	100.00-80.00	20.00	X Brace	No	No	0.0000	0.0000
T13	80.00-60.00	20.00	X Brace	No	No	0.0000	0.0000
T14	60.00-40.00	20.00	X Brace	No	No	0.0000	0.0000
T15	40.00-20.00	20.00	X Brace	No	No	0.0000	0.0000
T16	20.00-0.00	20.00	X Brace	No	No	0.0000	0.0000

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 280.00-270.00	Truss Leg	Valmont 207628 (12x1.25)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 5/16	A36 (36 ksi)
T2 270.00-260.00	Truss Leg	Valmont 207628 (12x1.25)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 5/16	A36 (36 ksi)
T3 260.00-240.00	Truss Leg	Valmont 207628 (12x1.25)	A572-50 (50 ksi)	Single Angle	L 3 x 3 x 5/16	A36 (36 ksi)
T4 240.00-220.00	Truss Leg	Valmont 207628 (12x1.25)	A572-50 (50 ksi)	Single Angle	L 4 x 4 x 1/4	A36 (36 ksi)
T5 220.00-210.00	Truss Leg	Valmont 195557 (12x1.75)	A572-50 (50 ksi)	Single Angle	L 4 x 4 x 1/4	A36 (36 ksi)
T6 210.00-200.00	Truss Leg	Valmont 195557 (12x1.75)	A572-50 (50 ksi)	Single Angle	L 4 x 4 x 1/4	A36 (36 ksi)
T7 200.00-180.00	Truss Leg	Valmont 211843 (12x2)	A572-50 (50 ksi)	Double Angle	2L 3.5 x 3.5 x 1/4 (1/2)	A36 (36 ksi)
T8 180.00-160.00	Truss Leg	Valmont 208334 (12x2.25)	A572-50 (50 ksi)	Double Angle	2L 3.5 x 3.5 x 1/4 (1/2)	A36 (36 ksi)
T9 160.00-140.00	Truss Leg	Valmont 208334 (12x2.25)	A572-50 (50 ksi)	Double Angle	2L 4 x 4 x 3/8 (1/2)	A36 (36 ksi)
T10 140.00-120.00	Truss Leg	Valmont 208335 (12x2.5)	A572-50 (50 ksi)	Double Angle	2L 4 x 4 x 3/8 (1/2)	A36 (36 ksi)
T11 120.00-100.00	Truss Leg	Valmont 208337 (12x2.75)	A572-50 (50 ksi)	Double Angle	2L 4 x 4 x 3/8 (1/2)	A36 (36 ksi)
T12 100.00-80.00	Truss Leg	Valmont 208338 (12x3)	A572-50 (50 ksi)	Double Angle	2L 5 x 5 x 5/16 (1/2)	A36 (36 ksi)
T13 80.00-60.00	Truss Leg	Valmont 208338 (12x3)	A572-50 (50 ksi)	Double Angle	2L 5 x 5 x 5/16 (1/2)	A36 (36 ksi)
T14 60.00-40.00	Truss Leg	Valmont 208339 (12x3.25)	A572-50 (50 ksi)	Double Angle	2L 5 x 5 x 5/16 (1/2)	A36 (36 ksi)
T15 40.00-20.00	Truss Leg	Valmont 208339 (12x3.25)	A572-50 (50 ksi)	Double Angle	2L 5 x 5 x 5/16 (1/2)	A36 (36 ksi)
T16 20.00-0.00	Truss Leg	Valmont 208339 (12x3.25)	A572-50 (50 ksi)	Double Angle	2L 5 x 5 x 5/16 (1/2)	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 280.00-270.00	Equal Angle	L 3.5 x 3.5 x 5/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T4 240.00-220.00	Single Angle	L 5 x 5 x 3/8	A36 (36 ksi)	Single Angle		A36 (36 ksi)

**Tower Section Geometry (cont'd)**

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T4 240.00-220.00	1	Single Angle	L 5 x 5 x 3/8	A36 (36 ksi)	Single Angle		A36 (36 ksi)

**Tower Section Geometry (cont'd)**

Tower Elevation ft	Secondary Horizontal Type	Secondary Horizontal Size	Secondary Horizontal Grade	Inner Bracing Type	Inner Bracing Size	Inner Bracing Grade
T1 280.00-270.00	Single Angle	L 2.5 x 2.5 x 5/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T2 270.00-260.00	Single Angle	L 2.5 x 2.5 x 5/16	A36 (36 ksi)	Single Angle		A36 (36 ksi)
T6 210.00-200.00	Single Angle	L 5 x 5 x 3/8	A36 (36 ksi)	Single Angle		A36 (36 ksi)

**Tower Section Geometry (cont'd)**

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>r</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontal in	Double Angle Stitch Bolt Spacing Redundants in
T1 280.00-270.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T2 270.00-260.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T3 260.00-240.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T4 240.00-220.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T5 220.00-210.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T6 210.00-200.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T7 200.00-180.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T8 180.00-160.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Third-Pt	Mid-Pt	Mid-Pt
T9 160.00-140.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T10 140.00-120.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T11 120.00-100.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T12 100.00-80.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T13 80.00-60.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T14 60.00-40.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T15 40.00-20.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt
T16 20.00-0.00	0.00	0.5000	A36 (36 ksi)	1	1	1.1	Mid-Pt	Mid-Pt	Mid-Pt

### Tower Section Geometry (cont'd)

Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors <sup>1</sup>										
				X Brace Diags		K Brace Diags		Single Diags		Girts		Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y	X Y	X Y		
T1 280.00-270.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T2 270.00-260.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T3 260.00-240.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T4 240.00-220.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T5 220.00-210.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T6 210.00-200.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T7 200.00-180.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T8 180.00-160.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T9 160.00-140.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T10 140.00-120.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T11 120.00-100.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T12 100.00-80.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T13 80.00-60.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T14 60.00-40.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T15 40.00-20.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	
T16 20.00-0.00	Yes	Yes	1	1	1	1	1	1	1	1	1	1	1	

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Panels	Truss-Leg K Factors				
		Truss-Legs Used As Leg Members		Leg Panels	Truss-Legs Used As Inner Members	
		X Brace Diagonals	Z Brace Diagonals		X Brace Diagonals	Z Brace Diagonals
T1 280.00-270.00	1	0.5	0.85	1	1	1
T2 270.00-260.00	1	0.5	0.85	1	1	1
T3 260.00-240.00	1	0.5	0.85	1	1	1
T4 240.00-220.00	1	0.5	0.85	1	1	1
T5 220.00-210.00	1	0.5	0.85	1	1	1
T6 210.00-200.00	1	0.5	0.85	1	1	1
T7 200.00-180.00	1	0.5	0.85	1	1	1

Truss-Leg K Factors						
Tower Elevation ft	Truss-Legs Used As Leg Members			Truss-Legs Used As Inner Members		
	Leg Panels	X Brace Diagonals	Z Brace Diagonals	Leg Panels	X Brace Diagonals	Z Brace Diagonals
T8 180.00-160.00	1	0.5	0.85	1	1	1
T9 160.00-140.00	1	0.5	0.85	1	1	1
T10 140.00-120.00	1	0.5	0.85	1	1	1
T11 120.00-100.00	1	0.5	0.85	1	1	1
T12 100.00-80.00	1	0.5	0.85	1	1	1
T13 80.00-60.00	1	0.5	0.85	1	1	1
T14 60.00-40.00	1	0.5	0.85	1	1	1
T15 40.00-20.00	1	0.5	0.85	1	1	1
T16 20.00-0.00	1	0.5	0.85	1	1	1

**Tower Section Geometry (cont'd)**

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 280.00-270.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 270.00-260.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 260.00-240.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 240.00-220.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 220.00-210.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 210.00-200.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 200.00-180.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T8 180.00-160.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T9 160.00-140.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T10 140.00-120.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T11 120.00-100.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T12 100.00-80.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T13 80.00-60.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T14 60.00-40.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T15 40.00-20.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T16 20.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

**Tower Section Geometry (cont'd)**

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 280.00-270.00	Flange	1.0000 A325N	0	1.0000 A325N	1	1.0000 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	1.0000 A325N	1
T2 270.00-260.00	Flange	1.0000 A325N	6	1.0000 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	1.0000 A325N	1
T3 260.00-240.00	Flange	1.0000 A325N	6	1.0000 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T4 240.00-220.00	Flange	1.0000 A325N	6	1.0000 A325N	1	1.0000 A325N	1	0.6250 A325N	0	1.0000 A325N	1	0.6250 A325N	0	0.6250 A325N	0
T5 220.00-210.00	Flange	1.0000 A325N	0	1.0000 A325N	1	0.6250 A325N	0	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T6 210.00-200.00	Flange	1.0000 A325N	12	1.0000 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	1.0000 A325N	1
T7 200.00-180.00	Flange	1.0000 A325N	12	0.8750 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T8 180.00-160.00	Flange	1.0000 A325N	12	0.8750 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T9 160.00-140.00	Flange	1.0000 A325N	12	0.8750 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T10 140.00-120.00	Flange	1.0000 A325N	12	0.8750 A325N	1	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T11 120.00-100.00	Flange	1.0000 A325N	12	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T12 100.00-80.00	Flange	1.2500 A325N	12	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T13 80.00-60.00	Flange	1.2500 A325N	12	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T14 60.00-40.00	Flange	1.2500 A325N	12	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T15 40.00-20.00	Flange	1.2500 A325N	12	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0
T16 20.00-0.00	Flange	0.0000 A615-75	0	0.8750 A325N	2	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0

**Feed Line/Linear Appurtenances - Entered As Round Or Flat**

Description	Face or Shield Leg	Allow	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
**** Safety Line 3/8	C	No	No	Ar (CaAa)	280.00 - 0.00	0.0000	0	1	1	0.3750	0.3750		0.22
LDF4-50A (1/2" foam)	C	No	No	Ar (CaAa)	280.00 - 0.00	0.0000	0.45	1	1	0.6300	0.6300		0.15
LDF2-50 (3/8" foam)	C	No	No	Ar (CaAa)	140.00 - 0.00	0.0000	0.45	1	1	0.4400	0.4400		0.08
****FACE A****													
LDF6-50 (1 1/4" foam)	A	No	No	Ar (CaAa)	155.00 - 0.00	0.0000	0.4	4	4	1.0000 0.5000	1.5500		0.66
LDF7-50A (1 5/8" foam)	A	No	No	Ar (CaAa)	155.00 - 0.00	0.0000	0.4	6	6	1.0000 0.5000	1.9800		0.92
1.5" flat Cable Ladder Rail	A	No	No	Af (CaAa)	155.00 - 0.00	0.0000	0.4	2	2	24.000 0	1.5000		1.80
**													
EW63(ELLIP TICAL)	A	No	No	Ar (CaAa)	195.00 - 0.00	0.0000	-0.45	1	1	1.0000 0.5000	2.0100		0.51



Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
EW63(ELLIP TICAL)	A	No	No	Ar (CaAa)	163.00 - 0.00	0.0000	-0.43	1	1	1.0000 0.5000	2.0100		0.51
EW63(ELLIP TICAL)	A	No	No	Ar (CaAa)	104.00 - 0.00	0.0000	-0.42	1	1	1.0000 0.5000	2.0100		0.51
LDF7-50A (1 5/8" foam)	A	No	No	Ar (CaAa)	235.17 - 0.00	0.0000	-0.38	2	2	1.0000 0.5000	1.9800		0.92
LDF2-50 (3/8" foam)	A	No	No	Ar (CaAa)	235.17 - 0.00	0.0000	-0.38	1	1	0.4400	0.4400		0.08
LDF4-50A (1/2" foam)	A	No	No	Ar (CaAa)	235.17 - 0.00	0.0000	-0.38	1	1	0.6300	0.6300		0.15
LDF7-50A (1 5/8" foam)	A	No	No	Ar (CaAa)	200.00 - 0.00	0.0000	-0.36	3	3	1.0000 0.5000	1.9800		0.92
LDF7-50A (1 5/8" foam)	A	No	No	Ar (CaAa)	175.00 - 0.00	0.0000	-0.34	4	2	1.0000 0.5000	1.9800		0.92
LDF5-50A (7/8" foam)	A	No	No	Ar (CaAa)	116.00 - 0.00	0.0000	-0.32	2	2	1.0000 0.5000	1.0900		0.33
LDF5-50A (7/8" foam)	A	No	No	Ar (CaAa)	55.00 - 0.00	0.0000	-0.32	1	1	1.0900	1.0900		0.33
LDF4-50A (1/2" foam)	A	No	No	Ar (CaAa)	175.00 - 0.00	0.0000	-0.4	1	1	0.6300	0.6300		0.15
LDF2-50 (3/8" foam)	A	No	No	Ar (CaAa)	175.00 - 0.00	0.0000	-0.4	1	1	0.4400	0.4400		0.08
LDF4-50A (1/2" foam)	A	No	No	Ar (CaAa)	200.00 - 0.00	0.0000	-0.36	1	1	0.6300	0.6300		0.15
1.5" flat Cable Ladder Rail	A	No	No	Af (CaAa)	235.00 - 0.00	0.0000	-0.4	2	2	36.000 0 1.5000	1.5000		1.80
****FACE B****													
EW63(ELLIP TICAL)	B	No	No	Ar (CaAa)	276.00 - 266.00	0.0000	0.47	3	3	0.5000	2.0100		0.51
EW63(ELLIP TICAL)	B	No	No	Ar (CaAa)	266.00 - 168.00	0.0000	0.46	4	4	0.5000	2.0100		0.51
EW63(ELLIP TICAL)	B	No	No	Ar (CaAa)	220.00 - 0.00	0.0000	0.45	5	5	0.5000	2.0100		0.51
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	168.00 - 0.00	0.0000	0.43	1	1	1.0000 0.5000	1.0900		0.33
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	255.00 - 0.00	0.0000	0.41	1	1	1.0900 0.5000	1.0900		0.33
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	240.00 - 0.00	0.0000	0.42	1	1	1.0000 0.5000	1.0900		0.33
LDF2-50 (3/8" foam)	B	No	No	Ar (CaAa)	260.00 - 0.00	0.0000	0.41	1	1	0.4400	0.4400		0.08
LDF7-50A (1 5/8" foam)	B	No	No	Ar (CaAa)	260.00 - 0.00	0.0000	0.39	2	2	1.0000 0.5000	1.9800		0.92
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	230.00 - 0.00	0.0000	0.38	1	1	1.0900	1.0900		0.33
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	216.00 - 0.00	0.0000	0.38	1	1	1.0900	1.0900		0.33
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	280.00 - 0.00	0.0000	0.37	2	1	1.0900	1.0900		0.33
LDF5-50A (7/8" foam)	B	No	No	Ar (CaAa)	130.00 - 0.00	0.0000	0.44	1	1	1.0900	1.0900		0.33
LDF6-50 (1 1/4" foam)	B	No	No	Ar (CaAa)	145.00 - 0.00	0.0000	0.44	1	1	1.5500	1.5500		0.66
Hybrid Cables	B	No	No	Ar (CaAa)	145.00 - 0.00	0.0000	0.44	3	3	1.5500	1.5500		0.66
1.5" flat Cable Ladder Rail	B	No	No	Af (CaAa)	280.00 - 0.00	0.0000	0.4	2	2	36.000 0 1.5000	1.5000		1.80
****FACE C****													
LDF7-50A (1 5/8" foam)	C	No	No	Ar (CaAa)	279.00 - 0.00	0.0000	0.46	1	1	1.0000 0.5000	1.9800		0.92
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	117.00 - 97.00	0.0000	0.45	5	5	1.0000 0.5000	1.0900		0.33
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	97.00 - 0.00	0.0000	0.43	4	4	1.0000 0.5000	1.0900		0.33

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	261.00 - 241.00	0.0000	0.43	2	2	1.0000 0.5000	1.0900		0.33
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	241.00 - 117.00	0.0000	0.43	3	3	1.0000 0.5000	1.0900		0.33
EW63(ELLIP TICAL)	C	No	No	Ar (CaAa)	240.00 - 230.00	0.0000	0.4	2	2	0.5000	2.0100		0.51
EW63(ELLIP TICAL)	C	No	No	Ar (CaAa)	230.00 - 205.50	0.0000	0.4	3	3	0.5000	2.0100		0.51
EW63(ELLIP TICAL)	C	No	No	Ar (CaAa)	205.50 - 197.00	0.0000	0.4	4	4	0.5000	2.0100		0.51
EW63(ELLIP TICAL)	C	No	No	Ar (CaAa)	197.00 - 0.00	0.0000	0.4	5	5	0.5000	2.0100		0.51
E60(ELLIPTICAL)	C	No	No	Ar (CaAa)	123.00 - 0.00	0.0000	0.4	1	1	2.2000	2.2000		0.68
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	128.00 - 0.00	0.0000	0.4	1	1	1.0900	1.0900		0.33
LDF5-50A (7/8" foam)	C	No	No	Ar (CaAa)	126.00 - 0.00	0.0000	0.4	1	1	1.0900	1.0900		0.33
LDF4-50A (1/2" foam)	C	No	No	Ar (CaAa)	50.00 - 0.00	0.0000	0.4	1	1	0.6300	0.6300		0.15
1.5" flat Cable Ladder Rail	C	No	No	Af (CaAa)	280.00 - 0.00	0.0000	0.42	2	2	36.000 0 1.5000	1.5000		1.80
***													
LDF4-50A (1/2" foam)	A	No	No	Ar (CaAa)	148.00 - 142.00	0.0000	0	16	8	0.5000	0.6300		0.15
LDF4-50A (1/2" foam)	B	No	No	Ar (CaAa)	148.00 - 142.00	0.0000	0	16	8	0.5000	0.6300		0.15
LDF4-50A (1/2" foam)	C	No	No	Ar (CaAa)	148.00 - 142.00	0.0000	0	16	8	0.5000	0.6300		0.15
***													

**Discrete Tower Loads**

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAAA Front ft²	CAAA Side ft²	Weight K	
Kreco CO-35A	A	From Leg	0.50	0.0000	279.00	No Ice	3.26	3.26	0.01
			0.00			1/2" Ice	4.74	4.74	0.03
			0.00			Ice	6.23	6.23	0.06
						1" Ice			
4' x 2" Std. Pipe Mount	A	From Leg	0.00	0.0000	279.00	No Ice	0.87	0.87	0.01
			0.00			1/2" Ice	1.11	1.11	0.02
			0.00			Ice	1.36	1.36	0.03
						1" Ice			
***									
ANT150F6-3	C	From Leg	0.50	0.0000	279.00	No Ice	4.80	4.80	0.03
			0.00			1/2" Ice	6.83	6.83	0.07
			0.00			Ice	8.87	8.87	0.11
						1" Ice			
4' x 2" Std. Pipe Mount	C	From Leg	0.00	0.0000	279.00	No Ice	0.87	0.87	0.01
			0.00			1/2" Ice	1.11	1.11	0.02
			0.00			Ice	1.36	1.36	0.03
						1" Ice			
**									
DB538-G	B	From Leg	0.50	0.0000	279.00	No Ice	3.64	3.64	0.02
			0.00			1/2" Ice	5.13	5.13	0.04
			0.00			Ice	6.63	6.63	0.08
						1" Ice			
4' x 2" Std. Pipe Mount	B	From Leg	0.00	0.0000	279.00	No Ice	0.87	0.87	0.01
			0.00			Ice	1.11	1.11	0.02

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement ft	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight K
			Horz Lateral ft	Vert ft			ft <sup>2</sup>	ft <sup>2</sup>	
				0.00			1.36	1.36	0.03
						1/2" Ice			
						1" Ice			
** FAA L-864 Beacon	B	From Leg	0.00	0.0000	280.00	No Ice	1.20	1.20	0.05
			0.00			1/2"	2.20	2.20	0.08
			0.00			Ice	3.20	3.20	0.12
						1" Ice			
** 8' x 2" Sch 40 Pipe Mount	A	From Leg	0.00	0.0000	276.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
						1" Ice			
8' x 2" Sch 40 Pipe Mount	B	From Leg	0.00	0.0000	276.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
						1" Ice			
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	276.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
						1" Ice			
**** 8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	276.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
						1" Ice			
**** 10' 8-Bay Dipole	A	From Leg	3.00	0.0000	261.00	No Ice	8.00	8.00	0.06
			0.00			1/2"	10.00	10.00	0.10
			0.00			Ice	12.00	12.00	0.14
						1" Ice			
6' Side Arm Mount	A	From Leg	1.50	0.0000	261.00	No Ice	4.54	1.23	0.05
			0.00			1/2"	7.80	2.55	0.08
			0.00			Ice	11.06	3.88	0.10
						1" Ice			
**** DB589-Y	B	From Leg	6.00	0.0000	260.00	No Ice	2.13	2.13	0.01
			0.00			1/2"	3.00	3.00	0.03
			5.50			Ice	3.76	3.76	0.05
						1" Ice			
DB589-Y	B	From Leg	6.00	0.0000	260.00	No Ice	2.13	2.13	0.01
			0.00			1/2"	3.00	3.00	0.03
			-5.50			Ice	3.76	3.76	0.05
						1" Ice			
12" x 12" x 6" TMA	B	From Leg	6.00	0.0000	260.00	No Ice	1.20	0.60	0.03
			0.00			1/2"	1.34	0.70	0.04
			0.00			Ice	1.48	0.81	0.05
						1" Ice			
6' Side Arm Mount	B	From Leg	3.00	0.0000	260.00	No Ice	4.54	1.23	0.05
			0.00			1/2"	7.80	2.55	0.08
			0.00			Ice	11.06	3.88	0.10
						1" Ice			
*** DB212-C	C	From Leg	6.00	0.0000	255.00	No Ice	3.10	3.10	0.03
			0.00			1/2"	6.22	6.22	0.06
			0.00			Ice	9.35	9.35	0.10
						1" Ice			
6' Side Arm Mount	C	From Leg	3.00	0.0000	255.00	No Ice	4.54	1.23	0.05
			0.00			1/2"	7.80	2.55	0.08
			0.00			Ice	11.06	3.88	0.10
						1" Ice			
*** CO-36A	A	From Leg	6.00	0.0000	240.00	No Ice	0.75	0.75	0.01
			0.00			1/2"	1.96	1.96	0.02
			0.00			Ice	3.19	3.19	0.04

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz Lateral	Vert					
							ft <sup>2</sup>	ft <sup>2</sup>	K
6' Side Arm Mount	A	From Leg	3.00	0.0000	240.00	1" Ice No Ice 1/2" Ice 1" Ice	4.54 7.80 11.06	1.23 2.55 3.88	0.05 0.08 0.10
***									
Comprod 531-70HD	A	From Leg	3.00	0.0000	230.00	1" Ice No Ice 1/2" Ice 1" Ice	4.98 6.22 7.47	4.98 6.22 7.47	0.04 0.05 0.06
3' Side Arm Mount	A	From Leg	1.50	0.0000	230.00	1" Ice No Ice 1/2" Ice 1" Ice	0.94 1.48 2.02	1.41 2.17 2.93	0.03 0.04 0.06
***									
SD110-SFXPASNM	B	From Leg	6.00	0.0000	241.00	1" Ice No Ice 1/2" Ice 1" Ice	7.50 15.00 22.50	7.50 15.00 22.50	0.03 0.03 0.04
6' Side Arm Mount	B	From Leg	3.00	0.0000	241.00	1" Ice No Ice 1/2" Ice 1" Ice	4.54 7.80 11.06	1.23 2.55 3.88	0.05 0.08 0.10
***									
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	240.00	1" Ice No Ice 1/2" Ice 1" Ice	1.90 2.73 3.40	1.90 2.73 3.40	0.03 0.04 0.06
***									
SE419-SF3P4LDF w/ Mount Pipe	C	From Leg	6.00	0.0000	235.17	1" Ice No Ice 1/2" Ice 1" Ice	4.36 5.45 6.53	11.82 13.45 15.10	0.06 0.13 0.20
SE419-SF3P4LDF w/ Mount Pipe	C	From Leg	6.00	0.0000	235.17	1" Ice No Ice 1/2" Ice 1" Ice	4.36 5.45 6.53	11.82 13.45 15.10	0.06 0.13 0.20
6' Side Arm Mount	C	From Leg	3.00	0.0000	235.17	1" Ice No Ice 1/2" Ice 1" Ice	4.54 7.80 11.06	1.23 2.55 3.88	0.05 0.08 0.10
***									
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	230.00	1" Ice No Ice 1/2" Ice 1" Ice	1.90 2.73 3.40	1.90 2.73 3.40	0.03 0.04 0.06
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	220.00	1" Ice No Ice 1/2" Ice 1" Ice	1.90 2.73 3.40	1.90 2.73 3.40	0.03 0.04 0.06
***									
ANT450F10	B	From Leg	6.00	0.0000	216.00	1" Ice No Ice 1/2" Ice 1" Ice	5.59 7.66 9.74	5.59 7.66 9.74	0.04 0.08 0.14
6' Side Arm Mount	B	From Leg	3.00	0.0000	216.00	1" Ice No Ice 1/2" Ice 1" Ice	4.54 7.80 11.06	1.23 2.55 3.88	0.05 0.08 0.10
***									
SD110-SFXPASNM	A	From Leg	6.00	0.0000	216.00	1" Ice No Ice 1/2" Ice 1" Ice	7.50 15.00 22.50	7.50 15.00 22.50	0.03 0.03 0.04
6' Side Arm Mount	A	From Leg	3.00	0.0000	216.00	1" Ice No Ice	4.54	1.23	0.05

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustmen t °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K	
			0.00			1/2"	7.80	2.55	0.08
			0.00			Ice	11.06	3.88	0.10
			0.00			1" Ice			
***									
8' x 2" Sch 40 Pipe Mount	A	From Leg	0.00	0.0000	205.50	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
			0.00			1" Ice			
***									
SC479-HF1LDF	B	From Leg	6.00	0.0000	200.00	No Ice	4.21	4.21	0.03
			0.00			1/2"	6.51	6.51	0.07
			6.00			Ice	8.00	8.00	0.11
			6.00			1" Ice			
SC479-HF1LDF	B	From Leg	6.00	0.0000	200.00	No Ice	4.21	4.21	0.03
			0.00			1/2"	6.51	6.51	0.07
			-6.00			Ice	8.00	8.00	0.11
			-6.00			1" Ice			
TMA (16" x 12" x 6")	B	From Leg	6.00	0.0000	200.00	No Ice	1.70	0.86	0.03
			0.00			1/2"	1.86	0.99	0.04
			0.00			Ice	2.04	1.12	0.06
			0.00			1" Ice			
6' Side Arm Mount	B	From Leg	3.00	0.0000	200.00	No Ice	4.54	1.23	0.05
			0.00			1/2"	7.80	2.55	0.08
			0.00			Ice	11.06	3.88	0.10
			0.00			1" Ice			
***									
SC479-HF1LDF	B	From Leg	3.00	0.0000	204.00	No Ice	4.20	4.20	0.03
			0.00			1/2"	6.51	6.51	0.07
			-4.00			Ice	8.00	8.00	0.11
			-4.00			1" Ice			
3' Side Arm Mount	B	From Leg	1.50	0.0000	204.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
			0.00			1" Ice			
***									
Telewave ANT900D6-9	C	From Leg	3.00	0.0000	200.00	No Ice	0.80	0.80	0.01
			0.00			1/2"	1.60	1.60	0.02
			0.00			Ice	2.40	2.40	0.03
			0.00			1" Ice			
(2) 3' Side Arm Mount	C	From Leg	1.50	0.0000	200.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
			0.00			1" Ice			
***									
8' x 2" Sch 40 Pipe Mount	A	From Leg	0.00	0.0000	197.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
			0.00			1" Ice			
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	195.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
			0.00			1" Ice			
***									
SC479-HF1LDF	B	From Leg	6.00	0.0000	175.00	No Ice	4.27	4.27	0.03
			0.00			1/2"	6.51	6.51	0.07
			6.00			Ice	8.00	8.00	0.11
			6.00			1" Ice			
SC479-HF1LDF	B	From Leg	6.00	0.0000	175.00	No Ice	4.27	4.27	0.03
			0.00			1/2"	6.51	6.51	0.07
			-6.00			Ice	8.00	8.00	0.11
			-6.00			1" Ice			
TMA (16" x 12" x 6")	B	From Leg	6.00	0.0000	175.00	No Ice	1.70	0.86	0.03
			0.00			1/2"	1.86	0.99	0.04
			0.00			Ice	2.04	1.12	0.06
			0.00			1" Ice			

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Horz Lateral	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
6' Side Arm Mount	B	From Leg	3.00	0.0000	175.00	No Ice	4.54	1.23	0.05
			0.00	0.00		1/2" Ice	7.80	2.55	0.08
			0.00	0.00		1" Ice	11.06	3.88	0.10
			***						
BCR-80010:90	A	From Leg	6.00	0.0000	175.00	No Ice	3.35	3.35	0.04
			0.00	0.00		1/2" Ice	6.03	6.03	0.07
			6.00	0.00		1" Ice	6.80	6.80	0.11
			***						
BCR-80010:90	A	From Leg	6.00	0.0000	175.00	No Ice	3.35	3.35	0.04
			0.00	0.00		1/2" Ice	6.03	6.03	0.07
			-6.00	0.00		1" Ice	6.80	6.80	0.11
			***						
6' Side Arm Mount	A	From Leg	3.00	0.0000	175.00	No Ice	4.54	1.23	0.05
			0.00	0.00		1/2" Ice	7.80	2.55	0.08
			0.00	0.00		1" Ice	11.06	3.88	0.10
			***						
ANT450F6	C	From Leg	3.00	0.0000	168.00	No Ice	0.79	0.79	0.01
			0.00	0.00		1/2" Ice	1.01	1.01	0.02
			0.00	0.00		1" Ice	1.23	1.23	0.03
			***						
3' Side Arm Mount	C	From Leg	1.50	0.0000	168.00	No Ice	0.94	1.41	0.03
			0.00	0.00		1/2" Ice	1.48	2.17	0.04
			0.00	0.00		1" Ice	2.02	2.93	0.06
			***						
8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00	0.0000	163.00	No Ice	1.90	1.90	0.03
			0.00	0.00		1/2" Ice	2.73	2.73	0.04
			0.00	0.00		1" Ice	3.40	3.40	0.06
			***						
FAA L-810 Sidelight	A	From Leg	0.50	0.0000	140.00	No Ice	0.20	0.20	0.00
			0.00	0.00		1/2" Ice	0.40	0.40	0.01
			0.00	0.00		1" Ice	0.60	0.60	0.01
			***						
FAA L-810 Sidelight	B	From Leg	0.50	0.0000	140.00	No Ice	0.20	0.20	0.00
			0.00	0.00		1/2" Ice	0.40	0.40	0.01
			0.00	0.00		1" Ice	0.60	0.60	0.01
			***						
FAA L-810 Sidelight	C	From Leg	0.00	0.0000	140.00	No Ice	0.20	0.20	0.00
			0.00	0.00		1/2" Ice	0.40	0.40	0.01
			0.00	0.00		1" Ice	0.60	0.60	0.01
			***						
(3) 12' V Frame	C	None		0.0000	155.00	No Ice	29.82	29.82	1.67
				0.0000		1/2" Ice	42.21	42.21	2.27
				0.0000		1" Ice	54.43	54.43	3.05
			***						
APXVTM14-C-120_TIA w/ Mount Pipe	A	From Leg	4.00	0.0000	155.00	No Ice	6.58	4.96	0.08
			0.00	0.00		1/2" Ice	7.03	5.75	0.13
			0.00	0.00		1" Ice	7.47	6.47	0.19
			***						
APXVTM14-C-120_TIA w/ Mount Pipe	B	From Leg	4.00	0.0000	155.00	No Ice	6.58	4.96	0.08
			0.00	0.00		1/2" Ice	7.03	5.75	0.13
			0.00	0.00		1" Ice	7.47	6.47	0.19
			***						
APXVTM14-C-120_TIA w/ Mount Pipe	C	From Leg	4.00	0.0000	155.00	No Ice	6.58	4.96	0.08
			0.00	0.00		1/2" Ice	7.03	5.75	0.13
			0.00	0.00		1" Ice	7.47	6.47	0.19
			***						
NNVV-65B-R4_TIA w/ Mount Pipe	A	From Leg	4.00	0.0000	155.00	No Ice	12.51	7.41	0.10
			0.00	0.00		1/2" Ice	13.11	8.60	0.19
			0.00	0.00		1" Ice	13.67	9.50	0.29
			***						

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub>		Weight
			Horz Lateral	Vert			Front	Side	
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
NNVV-65B-R4_TIA w/ Mount Pipe	B	From Leg	4.00	0.0000	155.00	No Ice	12.51	7.41	0.10
			0.00	0.00		1/2"	13.11	8.60	0.19
			0.00	0.00		Ice	13.67	9.50	0.29
						1" Ice			
NNVV-65B-R4_TIA w/ Mount Pipe	C	From Leg	4.00	0.0000	155.00	No Ice	12.51	7.41	0.10
			0.00	0.00		1/2"	13.11	8.60	0.19
			0.00	0.00		Ice	13.67	9.50	0.29
						1" Ice			
(2) FD RRH 2x50 800	A	From Leg	4.00	0.0000	155.00	No Ice	1.70	1.32	0.05
			0.00	0.00		1/2"	1.87	1.46	0.07
			0.00	0.00		Ice	2.04	1.62	0.09
						1" Ice			
(2) FD RRH 2x50 800	B	From Leg	4.00	0.0000	155.00	No Ice	1.70	1.32	0.05
			0.00	0.00		1/2"	1.87	1.46	0.07
			0.00	0.00		Ice	2.04	1.62	0.09
						1" Ice			
(2) FD RRH 2x50 800	C	From Leg	4.00	0.0000	155.00	No Ice	1.70	1.32	0.05
			0.00	0.00		1/2"	1.87	1.46	0.07
			0.00	0.00		Ice	2.04	1.62	0.09
						1" Ice			
FZHN	A	From Leg	4.00	0.0000	155.00	No Ice	2.02	0.61	0.04
			0.00	0.00		1/2"	2.20	0.71	0.06
			0.00	0.00		Ice	2.38	0.83	0.07
						1" Ice			
FZHN	B	From Leg	4.00	0.0000	155.00	No Ice	2.02	0.61	0.04
			0.00	0.00		1/2"	2.20	0.71	0.06
			0.00	0.00		Ice	2.38	0.83	0.07
						1" Ice			
FZHN	C	From Leg	4.00	0.0000	155.00	No Ice	2.02	0.61	0.04
			0.00	0.00		1/2"	2.20	0.71	0.06
			0.00	0.00		Ice	2.38	0.83	0.07
						1" Ice			
***									
HBXX-6517DS-A2M_TIA w/ Mount Pipe	A	From Leg	0.00	0.0000	145.00	No Ice	8.77	6.96	0.08
			0.00	0.00		1/2"	9.34	8.18	0.15
			0.00	0.00		Ice	9.89	9.14	0.23
						1" Ice			
HBXX-6517DS-A2M_TIA w/ Mount Pipe	B	From Leg	0.00	0.0000	145.00	No Ice	8.77	6.96	0.08
			0.00	0.00		1/2"	9.34	8.18	0.15
			0.00	0.00		Ice	9.89	9.14	0.23
						1" Ice			
HBXX-6517DS-A2M_TIA w/ Mount Pipe	C	From Leg	0.00	0.0000	145.00	No Ice	8.77	6.96	0.08
			0.00	0.00		1/2"	9.34	8.18	0.15
			0.00	0.00		Ice	9.89	9.14	0.23
						1" Ice			
LNX-6515DS-A1M_TIA w/ Mount Pipe	A	From Leg	0.00	0.0000	145.00	No Ice	11.71	9.87	0.08
			0.00	0.00		1/2"	12.43	11.39	0.17
			0.00	0.00		Ice	13.17	12.94	0.27
						1" Ice			
LNX-6515DS-A1M_TIA w/ Mount Pipe	B	From Leg	0.00	0.0000	145.00	No Ice	11.71	9.87	0.08
			0.00	0.00		1/2"	12.43	11.39	0.17
			0.00	0.00		Ice	13.17	12.94	0.27
						1" Ice			
LNX-6515DS-A1M_TIA w/ Mount Pipe	C	From Leg	0.00	0.0000	145.00	No Ice	11.71	9.87	0.08
			0.00	0.00		1/2"	12.43	11.39	0.17
			0.00	0.00		Ice	13.17	12.94	0.27
						1" Ice			
RC3DC-3315-PF-48	A	From Leg	4.00	0.0000	145.00	No Ice	3.79	2.51	0.03
			0.00	0.00		1/2"	4.04	2.72	0.06
			0.00	0.00		Ice	4.30	2.94	0.10
						1" Ice			
RC3DC-3315-PF-48	B	From Leg	4.00	0.0000	145.00	No Ice	3.79	2.51	0.03
			0.00	0.00		1/2"	4.04	2.72	0.06
			0.00	0.00		Ice	4.30	2.94	0.10
						1" Ice			

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement ft	C <sub>AA</sub>			Weight K
			Horz Lateral ft	Vert ft			Front ft <sup>2</sup>	Side ft <sup>2</sup>		
RC3DC-3315-PF-48	C	From Leg	4.00	0.00	0.0000	145.00	No Ice	3.79	2.51	0.03
							1/2" Ice	4.04	2.72	0.06
							Ice	4.30	2.94	0.10
							1" Ice			
(2) NHH-65C-R2B_TIA w/ Mount Pipe	A	From Leg	0.00	0.00	0.0000	145.00	No Ice	11.63	9.79	0.08
							1/2" Ice	12.35	11.31	0.17
							Ice	13.07	12.85	0.27
							1" Ice			
(2) NHH-65C-R2B_TIA w/ Mount Pipe	B	From Leg	0.00	0.00	0.0000	145.00	No Ice	11.63	9.79	0.08
							1/2" Ice	12.35	11.31	0.17
							Ice	13.07	12.85	0.27
							1" Ice			
(2) NHH-65C-R2B_TIA w/ Mount Pipe	C	From Leg	0.00	0.00	0.0000	145.00	No Ice	11.63	9.79	0.08
							1/2" Ice	12.35	11.31	0.17
							Ice	13.07	12.85	0.27
							1" Ice			
B2/B66A RRH-BR049	A	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
B2/B66A RRH-BR049	B	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
B2/B66A RRH-BR049	C	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
B5/B13 RRH-BR04C	A	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
B5/B13 RRH-BR04C	B	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
B5/B13 RRH-BR04C	C	From Leg	4.00	0.00	0.0000	145.00	No Ice	1.88	1.01	0.07
							1/2" Ice	2.05	1.14	0.09
							Ice	2.22	1.28	0.11
							1" Ice			
(3) VFA12-RRU Sector Frame	C	None			0.0000	145.00	No Ice	33.02	33.02	1.67
							1/2" Ice	47.36	47.36	2.22
							Ice	61.70	61.70	2.77
							1" Ice			
BSAMNT-SBS-1-2 (Mount Bracket)	A	From Leg	0.00	0.00	0.0000	145.00	No Ice	0.00	0.00	0.07
							1/2" Ice	0.00	0.00	0.09
							Ice	0.00	0.00	0.11
							1" Ice			
BSAMNT-SBS-1-2 (Mount Bracket)	B	From Leg	0.00	0.00	0.0000	145.00	No Ice	0.00	0.00	0.07
							1/2" Ice	0.00	0.00	0.09
							Ice	0.00	0.00	0.11
							1" Ice			
BSAMNT-SBS-1-2 (Mount Bracket)	C	From Leg	0.00	0.00	0.0000	145.00	No Ice	0.00	0.00	0.07
							1/2" Ice	0.00	0.00	0.09
							Ice	0.00	0.00	0.11
							1" Ice			
2 Std. Mount Pipe Stabilizer	A	From Leg	0.00	0.00	0.0000	145.00	No Ice	2.38	2.38	0.04
							1/2" Ice	3.40	3.40	0.05
							Ice	4.45	4.45	0.08
							1" Ice			
2 Std. Mount Pipe Stabilizer	B	From Leg	0.00	0.00	0.0000	145.00	No Ice	2.38	2.38	0.04
							1/2" Ice	3.40	3.40	0.05
							Ice	4.45	4.45	0.08
							1" Ice			



Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement ft	C <sub>A</sub> A		Weight K
			Horz Lateral ft ft	Vert ft			Front ft <sup>2</sup>	Side ft <sup>2</sup>	
2 Std. Mount Pipe Stabilizer	C	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	2.38	2.38	0.04
						1/2" Ice	3.40	3.40	0.05
						Ice	4.45	4.45	0.08
						1" Ice			
2.5 STD x Mount Pipe	A	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	0.97	0.97	0.05
						1/2" Ice	1.22	1.22	0.06
						Ice	1.48	1.48	0.07
						1" Ice			
2.5 STD x Mount Pipe	B	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	0.97	0.97	0.05
						1/2" Ice	1.22	1.22	0.06
						Ice	1.48	1.48	0.07
						1" Ice			
2.5 STD x Mount Pipe	C	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	0.97	0.97	0.05
						1/2" Ice	1.22	1.22	0.06
						Ice	1.48	1.48	0.07
						1" Ice			
(2) L 3 x 3 x 1/4 x 3' Mount Angle (Horiz)	A	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	1.18	0.01	0.01
						1/2" Ice	1.40	0.35	0.02
						Ice	1.63	0.71	0.03
						1" Ice			
(2) L 3 x 3 x 1/4 x 3' Mount Angle (Horiz)	B	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	1.18	0.01	0.01
						1/2" Ice	1.40	0.35	0.02
						Ice	1.63	0.71	0.03
						1" Ice			
(2) L 3 x 3 x 1/4 x 3' Mount Angle (Horiz)	C	From Leg	0.00 0.00 0.00	0.0000	145.00	No Ice	1.18	0.01	0.01
						1/2" Ice	1.40	0.35	0.02
						Ice	1.63	0.71	0.03
						1" Ice			
*** 8' x 2" Sch 40 Pipe Mount	C	From Leg	0.00 0.00 0.00	0.0000	123.00	No Ice	1.90	1.90	0.03
1/2" Ice						2.73	2.73	0.04	
Ice						3.40	3.40	0.06	
1" Ice									
*** CO-36A	C	From Leg	6.00 0.00 0.00	0.0000	130.00	No Ice	0.75	0.75	0.01
1/2" Ice						1.96	1.96	0.02	
Ice						3.19	3.19	0.04	
1" Ice									
6' Side Arm Mount	C	From Leg	3.00 0.00 0.00	0.0000	130.00	No Ice	4.54	1.23	0.05
						1/2" Ice	7.80	2.55	0.08
						Ice	11.06	3.88	0.10
						1" Ice			
*** ANT450F6	A	From Leg	6.00 0.00 0.00	0.0000	128.00	No Ice	0.79	0.79	0.01
1/2" Ice						1.01	1.01	0.02	
Ice						1.23	1.23	0.03	
1" Ice									
6' Side Arm Mount	A	From Leg	3.00 0.00 0.00	0.0000	128.00	No Ice	4.54	1.23	0.05
						1/2" Ice	7.80	2.55	0.08
						Ice	11.06	3.88	0.10
						1" Ice			
*** 6' Side Arm Mount	A	From Leg	3.00 0.00 0.00	0.0000	126.00	No Ice	4.54	1.23	0.05
1/2" Ice						7.80	2.55	0.08	
Ice						11.06	3.88	0.10	
1" Ice									
*** ANT450F6	A	From Leg	6.00 0.00 0.00	0.0000	124.00	No Ice	0.79	0.79	0.01
1/2" Ice						1.01	1.01	0.02	
Ice						1.23	1.23	0.03	
1" Ice									
6' Side Arm Mount	A	From Leg	3.00 0.00 0.00	0.0000	124.00	No Ice	4.54	1.23	0.05
						1/2" Ice	7.80	2.55	0.08
						Ice	11.06	3.88	0.10
						1" Ice			

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Horz Lateral	Vert					
***									
3' Side Arm Mount	C	From Leg	1.50	0.0000	117.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
						1" Ice			
***									
BR6155	A	From Leg	3.00	0.0000	116.00	No Ice	1.00	1.00	0.02
			0.00			1/2"	1.39	1.39	0.02
			0.00			Ice	1.70	1.70	0.03
						1" Ice			
ANT400D	A	From Leg	0.00	0.0000	116.00	No Ice	0.95	0.95	0.01
			0.00			1/2"	1.19	1.19	0.02
			-3.00			Ice	1.45	1.45	0.03
						1" Ice			
3' Side Arm Mount	A	From Leg	1.50	0.0000	116.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
						1" Ice			
***									
8' x 2" Sch 40 Pipe Mount	B	From Leg	0.00	0.0000	104.00	No Ice	1.90	1.90	0.03
			0.00			1/2"	2.73	2.73	0.04
			0.00			Ice	3.40	3.40	0.06
						1" Ice			
***									
BR6155	A	From Leg	3.00	0.0000	97.00	No Ice	1.00	1.00	0.02
			0.00			1/2"	1.39	1.39	0.02
			0.00			Ice	1.70	1.70	0.03
						1" Ice			
3' Side Arm Mount	A	From Leg	1.50	0.0000	97.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
						1" Ice			
***									
V-1500	A	From Leg	3.00	0.0000	55.00	No Ice	0.55	0.55	0.00
			0.00			1/2"	1.07	1.07	0.01
			0.00			Ice	1.45	1.45	0.02
						1" Ice			
3' Side Arm Mount	A	From Leg	1.50	0.0000	55.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
						1" Ice			
***									
Telewave ANT790-S2	C	From Leg	3.00	0.0000	50.00	No Ice	1.58	1.58	0.02
			0.00			1/2"	2.29	2.29	0.04
			0.00			Ice	2.60	2.60	0.06
						1" Ice			
3' Side Arm Mount	A	From Leg	1.50	0.0000	50.00	No Ice	0.94	1.41	0.03
			0.00			1/2"	1.48	2.17	0.04
			0.00			Ice	2.02	2.93	0.06
						1" Ice			
***									

**Dishes**

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area		Weight
				Horz	Lateral					ft <sup>2</sup>	K	
				ft	ft	°	°	ft	ft			K
PAL8	A	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		-15.0000		276.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
PAL8	B	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		-37.0000		276.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
PAL8	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		2.0000		276.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
***												
PAL8	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		2.0000		266.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
PADX6-59AC	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		50.0000		240.00	6.00	No Ice 1/2" Ice 1" Ice	28.27 29.07 29.86	0.19 0.33 0.48
PAL8	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		10.0000		230.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
***												
PAL8	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		2.0000		220.00	8.00	No Ice 1/2" Ice 1" Ice	50.27 51.32 52.37	0.29 0.55 0.81
PA10-59	A	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		14.0000		205.50	10.44	No Ice 1/2" Ice 1" Ice	85.63 87.00 88.38	0.79 1.24 1.69
***												
PAL6-59	A	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		46.0000		197.00	6.00	No Ice 1/2" Ice 1" Ice	28.27 29.07 29.86	0.19 0.33 0.48
PA10-59	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		35.0000		195.00	10.44	No Ice 1/2" Ice 1" Ice	85.63 87.00 88.38	0.79 1.24 1.69
***												
RFS PAD6-65AC	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		35.0000		163.00	6.00	No Ice 1/2" Ice 1" Ice	28.27 29.07 29.86	0.07 0.15 0.23
SBX4-W60AC2	C	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		-16.5000		123.00	4.14	No Ice 1/2" Ice 1" Ice	13.47 14.02 14.57	0.08 0.15 0.22
***												
PRF-950	A	Grid	From Leg	6.00 0.00 0.00		0.0000		126.00	5.67	No Ice 1/2" Ice 1" Ice	25.22 25.97 26.71	0.04 0.17 0.31
PRF-950	C	Grid	From Leg	3.00 0.00 0.00		0.0000		117.00	5.67	No Ice 1/2" Ice 1" Ice	25.22 25.97 26.71	0.04 0.17 0.31
RFS PAD6-65AC	B	Paraboloid w/Radome	From Leg	0.50 0.00 0.00		37.0000		104.00	6.00	No Ice 1/2" Ice 1" Ice	28.27 29.07 29.86	0.07 0.15 0.23
***												

### Truss-Leg Properties

Section Designation	Area	Area Ice	Self Weight	Ice Weight	Equiv. Diamete r	Equiv. Diamete r Ice	Leg Area
	in <sup>2</sup>	in <sup>2</sup>	K	K	in	in	in <sup>2</sup>
Valmont 207628 (12x1.25)	2161.7740	6558.0008	0.48	2.07	7.5062	22.7708	3.6816
Valmont 207628 (12x1.25)	2161.7740	6551.9048	0.48	2.06	7.5062	22.7497	3.6816

Section Designation	Area in <sup>2</sup>	Area Ice in <sup>2</sup>	Self Weight K	Ice Weight K	Equiv. Diamete r in	Equiv. Diamete r Ice in	Leg Area in <sup>2</sup>
Valmont 207628 (12x1.25)	2161.7740	6542.3611	0.48	2.04	7.5062	22.7165	3.6816
Valmont 207628 (12x1.25)	2161.7740	6528.8005	0.48	2.01	7.5062	22.6694	3.6816
Valmont 195557 (12x1.75)	1998.1590	5797.2605	0.78	2.01	6.9381	20.1294	7.2158
Valmont 195557 (12x1.75)	1998.1590	5791.0711	0.78	2.00	6.9381	20.1079	7.2158
Valmont 211843 (12x2)	2279.9276	5853.2574	1.02	1.91	7.9164	20.3238	9.4248
Valmont 208334 (12x2.25)	2264.8364	5911.0263	1.20	1.98	7.8640	20.5244	11.9282
Valmont 208334 (12x2.25)	2264.8364	5895.2000	1.20	1.94	7.8640	20.4694	11.9282
Valmont 208335 (12x2.5)	2550.6273	5949.3467	1.41	1.92	8.8563	20.6575	14.7262
Valmont 208337 (12x2.75)	2786.4655	6000.8255	1.69	1.93	9.6752	20.8362	17.8187
Valmont 208338 (12x3)	3229.8584	6887.7536	2.03	1.94	11.2148	23.9158	21.2058
Valmont 208338 (12x3)	3229.8584	6851.1588	2.03	1.87	11.2148	23.7887	21.2058
Valmont 208339 (12x3.25)	3392.5998	6875.5819	2.30	1.78	11.7799	23.8735	24.8873
Valmont 208339 (12x3.25)	3392.5998	6806.3434	2.30	1.62	11.7799	23.6331	24.8873
Valmont 208339 (12x3.25)	3392.5998	6668.8943	2.30	1.31	11.7799	23.1559	24.8873

### Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice

Comb. No.	Description
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	280 - 270	4.273	47	0.1286	0.0275
T2	270 - 260	4.001	47	0.1285	0.0276
T3	260 - 240	3.729	47	0.1273	0.0273
T4	240 - 220	3.194	47	0.1206	0.0263
T5	220 - 210	2.694	47	0.1081	0.0230
T6	210 - 200	2.460	47	0.1038	0.0206
T7	200 - 180	2.232	47	0.0987	0.0188
T8	180 - 160	1.815	47	0.0888	0.0160
T9	160 - 140	1.443	47	0.0791	0.0132
T10	140 - 120	1.119	47	0.0675	0.0114
T11	120 - 100	0.842	47	0.0567	0.0097
T12	100 - 80	0.606	47	0.0468	0.0080
T13	80 - 60	0.409	47	0.0377	0.0064
T14	60 - 40	0.249	47	0.0278	0.0048
T15	40 - 20	0.130	43	0.0190	0.0032
T16	20 - 0	0.042	43	0.0096	0.0016

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
280.00	FAA L-864 Beacon	47	4.273	0.1286	0.0275	778479
279.00	Kreco CO-35A	47	4.246	0.1287	0.0276	778479
276.00	PAL8	47	4.165	0.1287	0.0276	778479
266.00	PAL8	47	3.892	0.1282	0.0275	Inf
261.00	10' 8-Bay Dipole	47	3.756	0.1275	0.0273	431713
260.00	DB589-Y	47	3.729	0.1273	0.0273	371328
255.00	DB212-C	47	3.593	0.1263	0.0271	253191
241.00	SD110-SFXPASNM	47	3.221	0.1211	0.0264	148662
240.00	PADX6-59AC	47	3.194	0.1206	0.0263	144254
235.17	SE419-SF3P4LDF w/ Mount Pipe	47	3.070	0.1177	0.0257	125557
230.00	PAL8	47	2.939	0.1142	0.0250	110070
220.00	PAL8	47	2.694	0.1081	0.0230	97658
216.00	ANT450F10	47	2.599	0.1063	0.0220	138023
205.50	PA10-59	47	2.357	0.1016	0.0197	147333
204.00	SC479-HF1LDF	47	2.322	0.1008	0.0195	116925

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
200.00	SC479-HF1LDF	47	2.232	0.0987	0.0188	82136
197.00	PAL6-59	47	2.166	0.0972	0.0184	80190
195.00	PA10-59	47	2.123	0.0961	0.0181	83604
175.00	SC479-HF1LDF	47	1.718	0.0865	0.0153	117729
168.00	ANT450F6	47	1.586	0.0832	0.0143	101679
163.00	RFS PAD6-65AC	47	1.495	0.0807	0.0136	92794
155.00	(3) 12' V Frame	47	1.357	0.0763	0.0126	92415
145.00	HBXX-6517DS-A2M_TIA w/ Mount Pipe	47	1.196	0.0704	0.0118	102800
140.00	FAA L-810 Sidelight	47	1.119	0.0675	0.0114	108098
130.00	CO-36A	47	0.975	0.0619	0.0105	112042
128.00	ANT450F6	47	0.948	0.0609	0.0104	112688
126.00	PRF-950	47	0.921	0.0598	0.0102	113341
124.00	ANT450F6	47	0.894	0.0588	0.0100	114002
123.00	SBX4-W60AC2	47	0.881	0.0583	0.0099	114333
117.00	PRF-950	47	0.804	0.0552	0.0094	116244
116.00	BR6155	47	0.791	0.0546	0.0093	116548
104.00	RFS PAD6-65AC	47	0.650	0.0487	0.0083	120308
97.00	BR6155	47	0.574	0.0454	0.0077	123737
55.00	V-1500	47	0.216	0.0255	0.0044	121933
50.00	Telewave ANT790-S2	47	0.185	0.0234	0.0040	146121

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	280 - 270	21.880	18	0.6549	0.1428
T2	270 - 260	20.497	18	0.6544	0.1432
T3	260 - 240	19.107	18	0.6484	0.1414
T4	240 - 220	16.384	18	0.6146	0.1362
T5	220 - 210	13.829	18	0.5520	0.1190
T6	210 - 200	12.633	18	0.5307	0.1067
T7	200 - 180	11.467	18	0.5049	0.0977
T8	180 - 160	9.331	18	0.4548	0.0831
T9	160 - 140	7.420	11	0.4053	0.0684
T10	140 - 120	5.764	11	0.3461	0.0590
T11	120 - 100	4.339	11	0.2910	0.0501
T12	100 - 80	3.127	11	0.2402	0.0412
T13	80 - 60	2.113	11	0.1935	0.0330
T14	60 - 40	1.291	11	0.1430	0.0248
T15	40 - 20	0.673	11	0.0978	0.0166
T16	20 - 0	0.217	11	0.0496	0.0083

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
280.00	FAA L-864 Beacon	18	21.880	0.6549	0.1428	152540
279.00	Kreco CO-35A	18	21.742	0.6550	0.1429	152540
276.00	PAL8	18	21.328	0.6551	0.1432	152540
266.00	PAL8	18	19.941	0.6527	0.1427	368193
261.00	10' 8-Bay Dipole	18	19.246	0.6492	0.1416	89885
260.00	DB589-Y	18	19.107	0.6484	0.1414	76209
255.00	DB212-C	18	18.416	0.6432	0.1405	50988
241.00	SD110-SFXPASNM	18	16.517	0.6173	0.1366	29562
240.00	PADX6-59AC	18	16.384	0.6146	0.1362	28698
235.17	SE419-SF3P4LDF w/ Mount Pipe	18	15.748	0.5999	0.1334	25134
230.00	PAL8	18	15.080	0.5826	0.1294	22184

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
220.00	PAL8	18	13.829	0.5520	0.1190	19854
216.00	ANT450F10	18	13.346	0.5431	0.1140	27617
205.50	PA10-59	18	12.103	0.5197	0.1022	28000
204.00	SC479-HF1LDF	18	11.928	0.5157	0.1009	22707
200.00	SC479-HF1LDF	18	11.467	0.5049	0.0977	16104
197.00	PAL6-59	18	11.129	0.4969	0.0954	15735
195.00	PA10-59	18	10.908	0.4917	0.0939	16422
175.00	SC479-HF1LDF	18	8.832	0.4430	0.0793	23267
168.00	ANT450F6	18	8.156	0.4261	0.0739	19934
163.00	RFS PAD6-65AC	11	7.690	0.4134	0.0703	18112
155.00	(3) 12' V Frame	11	6.982	0.3911	0.0656	18038
145.00	HBXX-6517DS-A2M_TIA w/ Mount Pipe	11	6.155	0.3610	0.0611	20178
140.00	FAA L-810 Sidelight	11	5.764	0.3461	0.0590	21268
130.00	CO-36A	11	5.025	0.3178	0.0547	21961
128.00	ANT450F6	11	4.883	0.3123	0.0538	22067
126.00	PRF-950	11	4.744	0.3070	0.0529	22173
124.00	ANT450F6	11	4.607	0.3016	0.0519	22280
123.00	SBX4-W60AC2	11	4.539	0.2990	0.0515	22324
117.00	PRF-950	11	4.144	0.2831	0.0487	22680
116.00	BR6155	11	4.080	0.2805	0.0483	22741
104.00	RFS PAD6-65AC	11	3.353	0.2499	0.0429	23504
97.00	BR6155	11	2.962	0.2331	0.0400	24173
55.00	V-1500	11	1.120	0.1313	0.0227	23762
50.00	Telewave ANT790-S2	11	0.961	0.1201	0.0207	28474

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Allowable	Allowable Ratio	Criteria
T1	280	Diagonal	A325N	1.0000	1	3.53	19.47	0.181 ✓	1	Member Block Shear
		Secondary Horizontal	A325N	1.0000	1	1.80	15.24	0.118 ✓	1	Member Block Shear
		Top Girt	A325N	1.0000	1	0.37	20.34	0.018 ✓	1	Member Block Shear
T2	270	Leg	A325N	1.0000	6	1.32	53.01	0.025 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	5.85	19.47	0.301 ✓	1	Member Block Shear
		Secondary Horizontal	A325N	1.0000	1	0.92	15.24	0.060 ✓	1	Member Block Shear
T3	260	Leg	A325N	1.0000	6	5.18	53.01	0.098 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	7.91	19.47	0.406 ✓	1	Member Block Shear
T4	240	Leg	A325N	1.0000	6	10.06	53.01	0.190 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	13.05	18.30	0.713 ✓	1	Member Block Shear
		Top Girt	A325N	1.0000	1	2.06	25.45	0.081 ✓	1	Member Bearing
		Mid Girt	A325N	1.0000	1	2.78	25.45	0.109 ✓	1	Member Bearing
T5	220	Diagonal	A325N	1.0000	1	15.60	18.30	0.853 ✓	1	Member Block Shear
T6	210	Leg	A325N	1.0000	12	8.42	53.01	0.159 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	15.99	18.30	0.874 ✓	1	Member Block Shear
		Secondary Horizontal	A325N	1.0000	1	2.09	25.45	0.082 ✓	1	Member Bearing
T7	200	Leg	A325N	1.0000	12	11.28	53.01	0.213 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	1	24.79	29.58	0.838 ✓	1	Gusset Bearing

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio	Allowable Ratio	Criteria
								Load Allowable		
T8	180	Leg	A325N	1.0000	12	15.66	53.01	0.295 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	1	26.52	29.58	0.897 ✓	1	Gusset Bearing
T9	160	Leg	A325N	1.0000	12	19.89	53.01	0.375 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	1	31.45	48.71	0.646 ✓	1	Bolt Shear
T10	140	Leg	A325N	1.0000	12	24.77	53.01	0.467 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	1	34.98	48.71	0.718 ✓	1	Bolt Shear
T11	120	Leg	A325N	1.0000	12	29.86	53.01	0.563 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	2	18.07	39.15	0.462 ✓	1	Gusset Bearing
T12	100	Leg	A325N	1.2500	12	34.98	82.83	0.422 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	2	19.10	39.15	0.488 ✓	1	Gusset Bearing
T13	80	Leg	A325N	1.2500	12	40.06	82.83	0.484 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	2	19.80	39.15	0.506 ✓	1	Gusset Bearing
T14	60	Leg	A325N	1.2500	12	45.06	82.83	0.544 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	2	20.55	39.15	0.525 ✓	1	Gusset Bearing
T15	40	Leg	A325N	1.2500	12	50.11	82.83	0.605 ✓	1	Bolt Tension
		Diagonal	A325N	0.8750	2	21.10	39.15	0.539 ✓	1	Gusset Bearing
T16	20	Diagonal	A325N	0.8750	2	21.73	39.15	0.555 ✓	1	Gusset Bearing

**Compression Checks**

**Leg Design Data (Compression)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio
									$\frac{P_u}{\phi P_n}$
T1	280 - 270	Valmont 207628 (12x1.25)	10.02	10.02	45.4 K=1.00	3.6816	-4.91	142.49	0.034 <sup>1</sup> ✓
T2	270 - 260	Valmont 207628 (12x1.25)	10.02	10.02	45.4 K=1.00	3.6816	-11.85	142.49	0.083 <sup>1</sup> ✓
T3	260 - 240	Valmont 207628 (12x1.25)	20.03	10.02	45.4 K=1.00	3.6816	-38.91	142.49	0.273 <sup>1</sup> ✓
T4	240 - 220	Valmont 207628 (12x1.25)	20.03	10.02	45.4 K=1.00	3.6816	-74.43	142.49	0.522 <sup>1</sup> ✓
T5	220 - 210	Valmont 195557 (12x1.75)	10.02	10.02	31.9 K=1.00	7.2158	-97.23	301.49	0.322 <sup>1</sup> ✓
T6	210 - 200	Valmont 195557 (12x1.75)	10.02	10.02	31.9 K=1.00	7.2158	-120.43	301.49	0.399 <sup>1</sup> ✓
T7	200 - 180	Valmont 211843 (12x2)	20.03	20.03	48.8 K=1.00	9.4248	-161.25	356.29	0.453 <sup>1</sup> ✓
T8	180 - 160	Valmont 208334 (12x2.25)	20.03	20.03	48.8 K=1.00	11.928 2	-221.84	451.15	0.492 <sup>1</sup> ✓
T9	160 - 140	Valmont 208334 (12x2.25)	20.03	20.03	48.8 K=1.00	11.928 2	-282.34	451.15	0.626 <sup>1</sup> ✓
T10	140 - 120	Valmont 208335 (12x2.5)	20.03	20.03	48.7 K=1.00	14.726 2	-352.18	557.27	0.632 <sup>1</sup> ✓
T11	120 - 100	Valmont 208337 (12x2.75)	20.03	20.03	48.6 K=1.00	17.818 7	-422.72	674.68	0.627 <sup>1</sup> ✓



Section No.	Elevation ft	Size	L ft	$L_u$ ft	$Kl/r$	A in <sup>2</sup>	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T12	100 - 80	Valmont 208338 (12x3)	20.03	20.03	48.5 K=1.00	21.205 7	-495.05	803.44	0.616 <sup>1</sup> ✓
T13	80 - 60	Valmont 208338 (12x3)	20.03	20.03	48.5 K=1.00	21.205 7	-567.48	803.44	0.706 <sup>1</sup> ✓
T14	60 - 40	Valmont 208339 (12x3.25)	20.03	20.03	48.4 K=1.00	24.887 3	-639.38	943.57	0.678 <sup>1</sup> ✓
T15	40 - 20	Valmont 208339 (12x3.25)	20.03	20.03	48.4 K=1.00	24.887 3	-713.20	943.57	0.756 <sup>1</sup> ✓
T16	20 - 0	Valmont 208339 (12x3.25)	20.03	20.03	48.4 K=1.00	24.887 3	-782.36	943.57	0.829 <sup>1</sup> ✓

<sup>1</sup>  $P_u / \phi P_n$  controls

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	$L_d$ ft	$Kl/r$	$\phi P_n$ K	A in <sup>2</sup>	$V_u$ K	$\phi V_n$ K	Stress Ratio
T1	280 - 270	0.5	1.48	121.0	165.67	0.1963	0.88	3.29	0.267 ✓
T2	270 - 260	0.5	1.48	121.0	165.67	0.1963	0.67	3.29	0.204 ✓
T3	260 - 240	0.5	1.48	121.0	165.67	0.1963	0.58	3.29	0.178 ✓
T4	240 - 220	0.5	1.48	121.0	165.67	0.1963	1.76	3.29	0.536 ✓
T5	220 - 210	0.5	1.44	117.6	324.71	0.1963	1.69	3.62	0.466 ✓
T6	210 - 200	0.5	1.44	117.6	324.71	0.1963	1.88	3.62	0.519 ✓
T7	200 - 180	0.5	1.39	113.2	424.12	0.1963	2.84	3.76	0.756 ✓
T8	180 - 160	0.5	1.38	112.2	536.77	0.1963	1.63	3.80	0.428 ✓
T9	160 - 140	0.5	1.38	112.2	536.77	0.1963	2.90	3.80	0.762 ✓
T10	140 - 120	0.5	1.36	111.2	662.68	0.1963	1.16	3.85	0.300 ✓
T11	120 - 100	0.625	1.35	88.2	801.84	0.3068	1.22	7.66	0.160 ✓
T12	100 - 80	0.625	1.34	87.4	954.26	0.3068	0.91	7.71	0.119 ✓
T13	80 - 60	0.625	1.34	87.4	954.26	0.3068	0.99	7.71	0.128 ✓
T14	60 - 40	0.625	1.33	86.7	1119.93	0.3068	1.18	7.77	0.153 ✓
T15	40 - 20	0.625	1.33	86.7	1119.93	0.3068	1.34	7.77	0.172 ✓
T16	20 - 0	0.625	1.33	86.7	1119.93	0.3068	1.32	7.77	0.170 ✓

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio P <sub>u</sub> / φP <sub>n</sub>
T1	280 - 270	L 3 x 3 x 5/16	16.01	7.48	152.3 K=1.00	1.7800	-3.78	17.33	0.218 <sup>1</sup> ✓
T2	270 - 260	L 3 x 3 x 5/16	16.80	7.88	160.6 K=1.00	1.7800	-6.15	15.59	0.394 <sup>1</sup> ✓
T3	260 - 240	L 3 x 3 x 5/16	18.45	8.72	177.6 K=1.00	1.7800	-8.06	12.75	0.633 <sup>1</sup> ✓
T4	240 - 220	L 4 x 4 x 1/4	20.16	9.58	144.6 K=1.00	1.9400	-13.52	20.95	0.645 <sup>1</sup> ✓
T5	220 - 210	L 4 x 4 x 1/4	21.03	10.02	151.3 K=1.00	1.9400	-15.71	19.15	0.820 <sup>1</sup> ✓
T6	210 - 200	L 4 x 4 x 1/4	21.92	10.47	158.0 K=1.00	1.9400	-15.68	17.55	0.893 <sup>1</sup> ✓
T7	200 - 180	2L 3.5 x 3.5 x 1/4 (1/2)	29.01	14.29	162.2 K=1.00	3.3750	-25.35	29.00	0.874 <sup>1</sup> ✓
T8	180 - 160	2L 'a' > 81.7665 in - 89 2L 3.5 x 3.5 x 1/4 (1/2)	30.49	15.03	165.3 K=1.00	3.3750	-26.57	27.90	0.952 <sup>1</sup> ✓
T9	160 - 140	2L 4 x 4 x 3/8 (1/2)	32.02	15.80	157.8 K=1.00	5.7188	-31.45	51.86	0.606 <sup>1</sup> ✓
T10	140 - 120	2L 'a' > 90.7220 in - 107 2L 4 x 4 x 3/8 (1/2)	33.61	16.59	165.7 K=1.00	5.7188	-34.92	47.03	0.743 <sup>1</sup> ✓
T11	120 - 100	2L 'a' > 95.2708 in - 116 2L 4 x 4 x 3/8 (1/2)	35.23	17.34	173.2 K=1.00	5.7188	-36.51	43.07	0.848 <sup>1</sup> ✓
T12	100 - 80	2L 'a' > 92.7523 in - 125 2L 5 x 5 x 5/16 (1/2)	36.90	18.17	146.4 K=1.00	6.0547	-38.50	63.83	0.603 <sup>1</sup> ✓
T13	80 - 60	2L 'a' > 100.4316 in - 134 2L 5 x 5 x 5/16 (1/2)	38.59	19.02	153.2 K=1.00	6.0547	-39.77	58.27	0.683 <sup>1</sup> ✓
T14	60 - 40	2L 'a' > 104.1226 in - 143 2L 5 x 5 x 5/16 (1/2)	40.32	19.88	160.2 K=1.00	6.0547	-41.65	53.32	0.781 <sup>1</sup> ✓
T15	40 - 20	2L 'a' > 107.8743 in - 152 2L 5 x 5 x 5/16 (1/2)	42.06	20.76	167.2 K=1.00	6.0547	-42.05	48.93	0.859 <sup>1</sup> ✓
T16	20 - 0	2L 'a' > 111.6793 in - 161 2L 5 x 5 x 5/16 (1/2)  2L 'a' > 115.5312 in - 170	43.83	21.64	174.3 K=1.00	6.0547	-44.37	45.01	0.986 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Secondary Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio P <sub>u</sub> / φP <sub>n</sub>
T1	280 - 270	L 2.5 x 2.5 x 5/16	12.48	11.15	175.4 K=1.00	1.4600	-2.02	10.72	0.189 <sup>1</sup> ✓
T2	270 - 260	L 2.5 x 2.5 x 5/16	13.48	12.15	191.2 K=1.00	1.4600	-0.93	9.03	0.103 <sup>1</sup> ✓
T6	210 - 200	L 5 x 5 x 3/8	19.49	18.15	140.0 K=1.00	3.6100	-2.09	41.61	0.050 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	280 - 270	L 3.5 x 3.5 x 5/16	12.00	10.67	185.5 K=1.00	2.0900	-0.44	13.72	0.032 <sup>1</sup> ✓
T4	240 - 220	L 5 x 5 x 3/8	16.00	14.67	177.8 K=1.00	3.6100	-1.65	25.80	0.064 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Mid Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T4	240 - 220	L 5 x 5 x 3/8	17.00	15.67	189.9 K=1.00	3.6100	-2.30	22.62	0.102 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	280 - 270	Valmont 207628 (12x1.25)	10.02	10.02	45.4	3.6816	0.95	165.67	0.006 <sup>1</sup> ✓
T2	270 - 260	Valmont 207628 (12x1.25)	10.02	10.02	45.4	3.6816	7.92	165.67	0.048 <sup>1</sup> ✓
T3	260 - 240	Valmont 207628 (12x1.25)	20.03	10.02	45.4	3.6816	31.07	165.67	0.188 <sup>1</sup> ✓
T4	240 - 220	Valmont 207628 (12x1.25)	20.03	10.02	45.4	3.6816	60.34	165.67	0.364 <sup>1</sup> ✓
T5	220 - 210	Valmont 195557 (12x1.75)	10.02	10.02	31.9	7.2158	80.63	324.71	0.248 <sup>1</sup> ✓
T6	210 - 200	Valmont 195557 (12x1.75)	10.02	10.02	31.9	7.2158	101.02	324.71	0.311 <sup>1</sup> ✓
T7	200 - 180	Valmont 211843 (12x2)	20.03	20.03	48.8	9.4248	135.40	424.12	0.319 <sup>1</sup> ✓
T8	180 - 160	Valmont 208334 (12x2.25)	20.03	20.03	48.8	11.928 2	187.95	536.77	0.350 <sup>1</sup> ✓
T9	160 - 140	Valmont 208334 (12x2.25)	20.03	20.03	48.8	11.928 2	238.71	536.77	0.445 <sup>1</sup> ✓
T10	140 - 120	Valmont 208335 (12x2.5)	20.03	20.03	48.7	14.726 2	297.18	662.68	0.448 <sup>1</sup> ✓
T11	120 - 100	Valmont 208337 (12x2.75)	20.03	20.03	48.6	17.818 7	358.29	801.84	0.447 <sup>1</sup> ✓

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T12	100 - 80	Valmont 208338 (12x3)	20.03	20.03	48.5	21.205 7	419.80	954.26	0.440 <sup>1</sup>
T13	80 - 60	Valmont 208338 (12x3)	20.03	20.03	48.5	21.205 7	480.71	954.26	0.504 <sup>1</sup>
T14	60 - 40	Valmont 208339 (12x3.25)	20.03	20.03	48.4	24.887 3	540.77	1119.93	0.483 <sup>1</sup>
T15	40 - 20	Valmont 208339 (12x3.25)	20.03	20.03	48.4	24.887 3	601.30	1119.93	0.537 <sup>1</sup>
T16	20 - 0	Valmont 208339 (12x3.25)	20.03	20.03	48.4	24.887 3	657.86	1119.93	0.587 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

### Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L <sub>d</sub> ft	Kl/r	φP <sub>n</sub> K	A in <sup>2</sup>	V <sub>u</sub> K	φV <sub>n</sub> K	Stress Ratio
T1	280 - 270	0.5	1.48	121.0	165.67	0.1963	0.88	3.29	0.267
T2	270 - 260	0.5	1.48	121.0	165.67	0.1963	0.67	3.29	0.204
T3	260 - 240	0.5	1.48	121.0	165.67	0.1963	0.58	3.29	0.178
T4	240 - 220	0.5	1.48	121.0	165.67	0.1963	1.76	3.29	0.536
T5	220 - 210	0.5	1.44	117.6	324.71	0.1963	1.69	3.62	0.466
T6	210 - 200	0.5	1.44	117.6	324.71	0.1963	1.88	3.62	0.519
T7	200 - 180	0.5	1.39	113.2	424.12	0.1963	2.84	3.76	0.756
T8	180 - 160	0.5	1.38	112.2	536.77	0.1963	1.63	3.80	0.428
T9	160 - 140	0.5	1.38	112.2	536.77	0.1963	2.90	3.80	0.762
T10	140 - 120	0.5	1.36	111.2	662.68	0.1963	1.16	3.85	0.300
T11	120 - 100	0.625	1.35	88.2	801.84	0.3068	1.22	7.66	0.160
T12	100 - 80	0.625	1.34	87.4	954.26	0.3068	0.91	7.71	0.119
T13	80 - 60	0.625	1.34	87.4	954.26	0.3068	0.99	7.71	0.128
T14	60 - 40	0.625	1.33	86.7	1119.93	0.3068	1.18	7.77	0.153
T15	40 - 20	0.625	1.33	86.7	1119.93	0.3068	1.34	7.77	0.172
T16	20 - 0	0.625	1.33	86.7	1119.93	0.3068	1.32	7.77	0.170

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	$L_u$ ft	$Kl/r$	A $in^2$	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	280 - 270	L 3 x 3 x 5/16	16.01	7.48	100.1	1.0713	3.53	46.60	0.076 <sup>1</sup>
T2	270 - 260	L 3 x 3 x 5/16	16.80	7.88	105.4	1.0713	5.85	46.60	0.126 <sup>1</sup>
T3	260 - 240	L 3 x 3 x 5/16	18.45	8.72	116.3	1.0713	7.91	46.60	0.170 <sup>1</sup>
T4	240 - 220	L 4 x 4 x 1/4	20.16	9.58	93.9	1.2441	13.05	54.12	0.241 <sup>1</sup>
T5	220 - 210	L 4 x 4 x 1/4	21.03	10.02	98.1	1.2441	15.60	54.12	0.288 <sup>1</sup>
T6	210 - 200	L 4 x 4 x 1/4	21.92	10.47	102.4	1.2441	15.99	54.12	0.296 <sup>1</sup>
T7	200 - 180	2L 3.5 x 3.5 x 1/4 (1/2)	29.01	14.29	159.5	2.1563	24.79	93.80	0.264 <sup>1</sup>
T8	180 - 160	2L 'a' > 81.7665 in - 88 2L 3.5 x 3.5 x 1/4 (1/2)	30.49	15.03	167.6	2.1563	26.52	93.80	0.283 <sup>1</sup>
T9	160 - 140	2L 4 x 4 x 3/8 (1/2)	32.02	15.80	155.6	3.7266	30.50	162.10	0.188 <sup>1</sup>
T10	140 - 120	2L 'a' > 90.7220 in - 106 2L 4 x 4 x 3/8 (1/2)	33.61	16.59	163.3	3.7266	34.98	162.10	0.216 <sup>1</sup>
T11	120 - 100	2L 'a' > 95.2708 in - 115 2L 4 x 4 x 3/8 (1/2)	35.23	17.34	171.2	3.7266	36.15	162.10	0.223 <sup>1</sup>
T12	100 - 80	2L 'a' > 92.7523 in - 124 2L 5 x 5 x 5/16 (1/2)	36.90	18.17	141.4	4.0723	38.21	177.14	0.216 <sup>1</sup>
T13	80 - 60	2L 'a' > 100.4316 in - 133 2L 5 x 5 x 5/16 (1/2)	38.59	19.02	147.9	4.0723	39.60	177.14	0.224 <sup>1</sup>
T14	60 - 40	2L 'a' > 104.1226 in - 142 2L 5 x 5 x 5/16 (1/2)	40.32	19.88	154.5	4.0723	41.11	177.14	0.232 <sup>1</sup>
T15	40 - 20	2L 'a' > 107.8743 in - 151 2L 5 x 5 x 5/16 (1/2)	42.06	20.76	161.2	4.0723	42.19	177.14	0.238 <sup>1</sup>
T16	20 - 0	2L 'a' > 111.6793 in - 160 2L 5 x 5 x 5/16 (1/2)	43.83	21.64	168.0	4.0723	43.45	177.14	0.245 <sup>1</sup>
		2L 'a' > 115.5312 in - 169							

<sup>1</sup>  $P_u / \phi P_n$  controls

### Secondary Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	$L_u$ ft	$Kl/r$	A $in^2$	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
T1	280 - 270	L 2.5 x 2.5 x 5/16	12.48	11.15	180.7	0.8313	1.80	36.16	0.050 <sup>1</sup>
T2	270 - 260	L 2.5 x 2.5 x 5/16	13.48	12.15	196.4	0.8313	0.92	36.16	0.025 <sup>1</sup>
T6	210 - 200	L 5 x 5 x 3/8	19.49	18.15	142.6	2.3911	2.09	104.01	0.020 <sup>1</sup>

<sup>1</sup>  $P_u / \phi P_n$  controls

**Top Girt Design Data (Tension)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	280 - 270	L 3.5 x 3.5 x 5/16	12.00	10.67	122.2	1.3038	0.37	56.72	0.006 <sup>1</sup> ✓
T4	240 - 220	L 5 x 5 x 3/8	16.00	14.67	115.7	2.3911	2.06	104.01	0.020 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

**Mid Girt Design Data (Tension)**

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T4	240 - 220	L 5 x 5 x 3/8	17.00	15.67	123.4	2.3911	2.78	104.01	0.027 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / φP<sub>n</sub> controls

**Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	φP <sub>allow</sub> K	% Capacity	Pass Fail
T1	280 - 270	Leg	Valmont 207628 (12x1.25)	2	-4.91	142.49	26.7	Pass
T2	270 - 260	Leg	Valmont 207628 (12x1.25)	18	-10.50	142.49	20.4	Pass
T3	260 - 240	Leg	Valmont 207628 (12x1.25)	28	-38.91	142.49	27.3	Pass
T4	240 - 220	Leg	Valmont 207628 (12x1.25)	43	-54.37	142.49	53.6	Pass
T5	220 - 210	Leg	Valmont 195557 (12x1.75)	64	-97.23	301.49	46.6	Pass
T6	210 - 200	Leg	Valmont 195557 (12x1.75)	73	-120.43	301.49	51.9	Pass
T7	200 - 180	Leg	Valmont 211843 (12x2)	85	-161.25	356.29	75.6	Pass
T8	180 - 160	Leg	Valmont 208334 (12x2.25)	94	-221.84	451.15	49.2	Pass
T9	160 - 140	Leg	Valmont 208334 (12x2.25)	103	-282.34	451.15	76.2	Pass
T10	140 - 120	Leg	Valmont 208335 (12x2.5)	112	-352.18	557.27	63.2	Pass
T11	120 - 100	Leg	Valmont 208337 (12x2.75)	121	-422.72	674.68	62.7	Pass
T12	100 - 80	Leg	Valmont 208338 (12x3)	130	-495.05	803.44	61.6	Pass
T13	80 - 60	Leg	Valmont 208338 (12x3)	139	-567.48	803.44	70.6	Pass
T14	60 - 40	Leg	Valmont 208339 (12x3.25)	148	-639.38	943.57	67.8	Pass
T15	40 - 20	Leg	Valmont 208339 (12x3.25)	157	-713.20	943.57	75.6	Pass
T16	20 - 0	Leg	Valmont 208339 (12x3.25)	167	-782.36	943.57	82.9	Pass
T1	280 - 270	Diagonal	L 3 x 3 x 5/16	7	-3.78	17.33	21.8	Pass
T2	270 - 260	Diagonal	L 3 x 3 x 5/16	20	-6.15	15.59	39.4	Pass
T3	260 - 240	Diagonal	L 3 x 3 x 5/16	32	-8.06	12.75	63.3	Pass
T4	240 - 220	Diagonal	L 4 x 4 x 1/4	53	-13.52	20.95	64.5	Pass
T5	220 - 210	Diagonal	L 4 x 4 x 1/4	68	-15.71	19.15	82.0	Pass
T6	210 - 200	Diagonal	L 4 x 4 x 1/4	77	-15.68	17.55	89.3	Pass
T7	200 - 180	Diagonal	2L 3.5 x 3.5 x 1/4 (1/2)	89	-25.35	29.00	87.4	Pass
T8	180 - 160	Diagonal	2L 3.5 x 3.5 x 1/4 (1/2)	98	-26.57	27.90	95.2	Pass
T9	160 - 140	Diagonal	2L 4 x 4 x 3/8 (1/2)	107	-31.45	51.86	60.6	Pass
T10	140 - 120	Diagonal	2L 4 x 4 x 3/8 (1/2)	116	-34.92	47.03	74.3	Pass
T11	120 - 100	Diagonal	2L 4 x 4 x 3/8 (1/2)	125	-36.51	43.07	84.8	Pass
T12	100 - 80	Diagonal	2L 5 x 5 x 5/16 (1/2)	134	-38.50	63.83	60.3	Pass
T13	80 - 60	Diagonal	2L 5 x 5 x 5/16 (1/2)	143	-39.77	58.27	68.3	Pass
T14	60 - 40	Diagonal	2L 5 x 5 x 5/16 (1/2)	152	-41.65	53.32	78.1	Pass
T15	40 - 20	Diagonal	2L 5 x 5 x 5/16 (1/2)	161	-42.05	48.93	85.9	Pass
T16	20 - 0	Diagonal	2L 5 x 5 x 5/16 (1/2)	170	-44.37	45.01	98.6	Pass

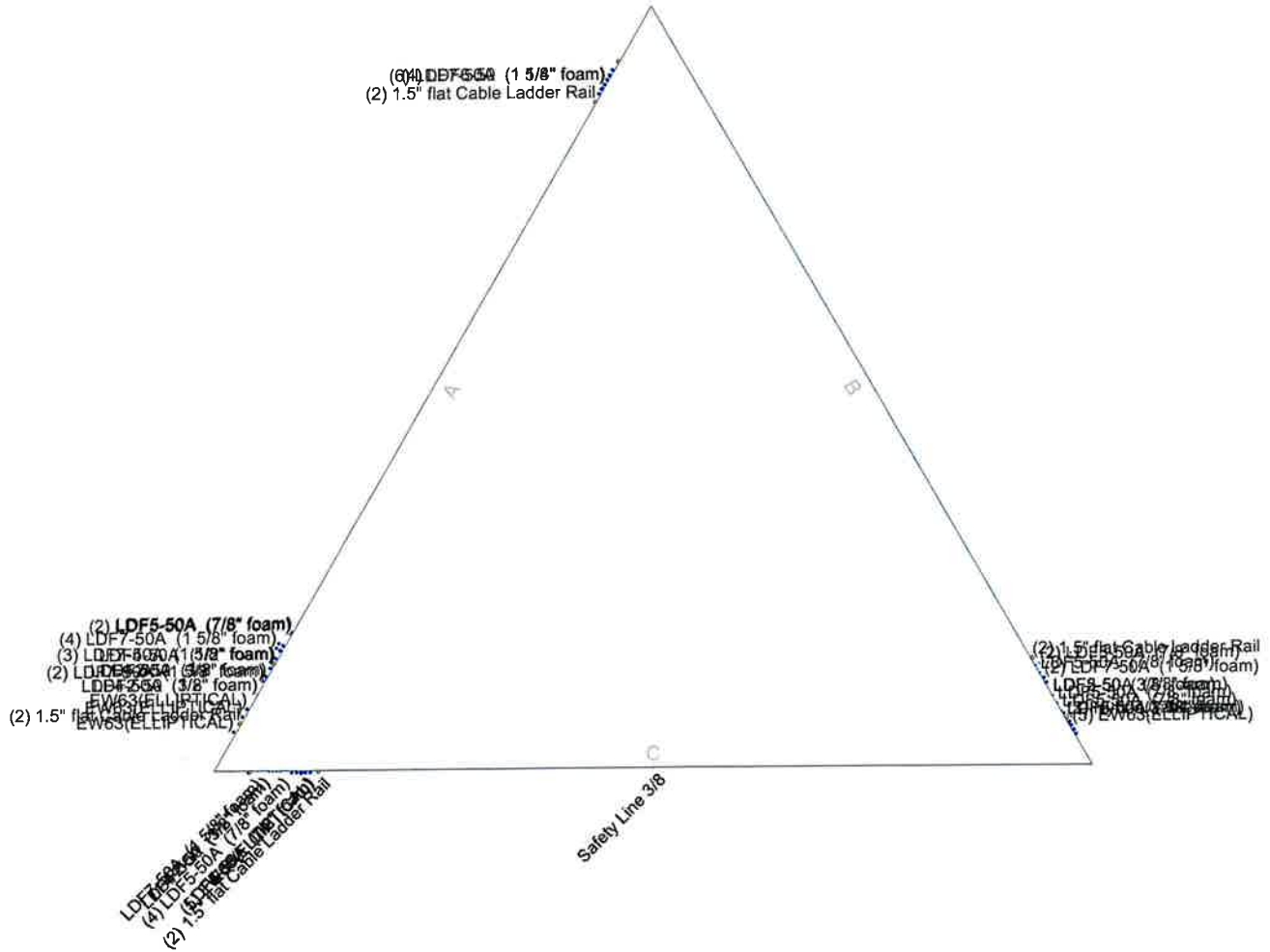
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail	
T1	280 - 270	Secondary Horizontal	L 2.5 x 2.5 x 5/16	13	-2.02	10.72	18.9	Pass	
T2	270 - 260	Secondary Horizontal	L 2.5 x 2.5 x 5/16	25	-0.93	9.03	10.3	Pass	
T6	210 - 200	Secondary Horizontal	L 5 x 5 x 3/8	82	-2.09	41.61	5.0	Pass	
T1	280 - 270	Top Girt	L 3.5 x 3.5 x 5/16	6	-0.44	13.72	3.2	Pass	
T4	240 - 220	Top Girt	L 5 x 5 x 3/8	47	-1.65	25.80	6.4	Pass	
T4	240 - 220	Mid Girt	L 5 x 5 x 3/8	50	-2.30	22.62	10.2	Pass	
							Summary		
							Leg (T16)	82.9	Pass
							Diagonal (T16)	98.6	Pass
							Secondary Horizontal (T1)	18.9	Pass
							Top Girt (T4)	6.4	Pass
							Mid Girt (T4)	10.2	Pass
							Bolt	89.7	Pass
							Checks		
							<b>RATING =</b>	<b>98.6</b>	<b>Pass</b>

**APPENDIX B**  
**BASE LEVEL DRAWING**



# Feed Line Plan

— Round   
 — Flat   
 — App In Face   
 — App Out Face   
 — Truss-Leg



<b>Paul J. Ford and Company</b> 250 E. Broad St., Ste 600 Columbus, OH 43215 Phone: 614-221-6679 FAX:	<b>Job: 280-ft Self Support Tower Haddam, CT</b>		
	Project: <b>00019-0111</b>		
	Client: Hudson Design Group	Drawn by: Michael Bange	App'd:
	Code: TIA-222-G	Date: 05/06/20	Scale: NTS
	Path:	Dwg No. E-7	

G:\TOWER\00019-0111 - Haddam\South CT\004-8700 - SAIT\00019-0111-004-8700.dwg

**APPENDIX C**  
**ADDITIONAL CALCULATIONS**

**Self-Support Tower Anchor Rod Capacity - TIA-G**

**Loads**

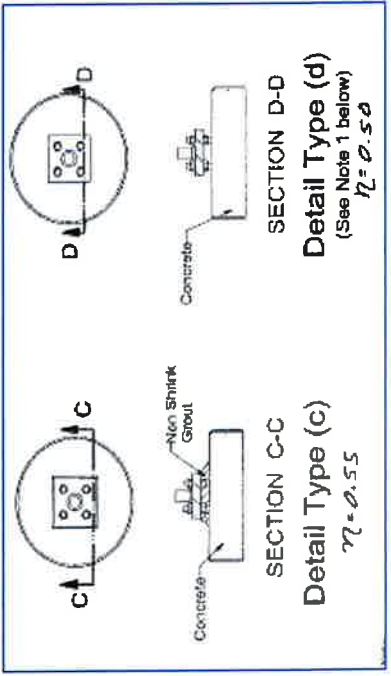
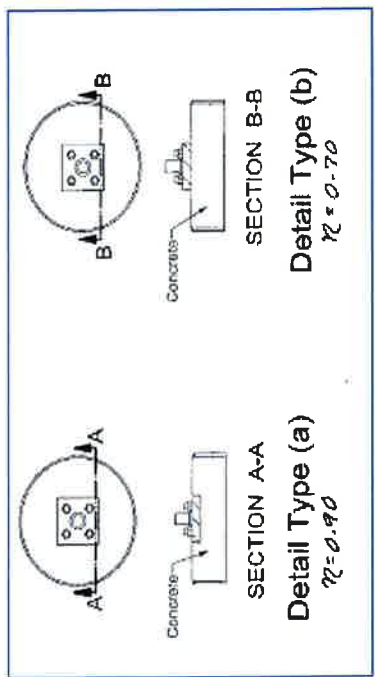
Compression:	818 kips	1.00	Maximum Ratio
Shear:	108 kips		

**Existing Anchor Rods**

Anchor Rod Condition (n):	0.5
Anchor Rod $\phi$ :	1 1/4 in
Anchor Rod Quantity:	12
Anchor Rod Grade:	F1554 Gr. 105

$F_y$ : 105 ksi  
 $F_u$ : 150 ksi  
 Threads per Inch: 7  
 Total Net Tensile Area: 11.63 in<sup>2</sup>  
 $\phi$ : 0.8  
 Total Anchor Rod Capacity  $\phi R_{nt}$ : 1395.52 kip  
 Anchor Rod Ratio: 0.741

$l_{ar}$ :  inches  
 Moment:  k-in



**Combined Footing Foundation**

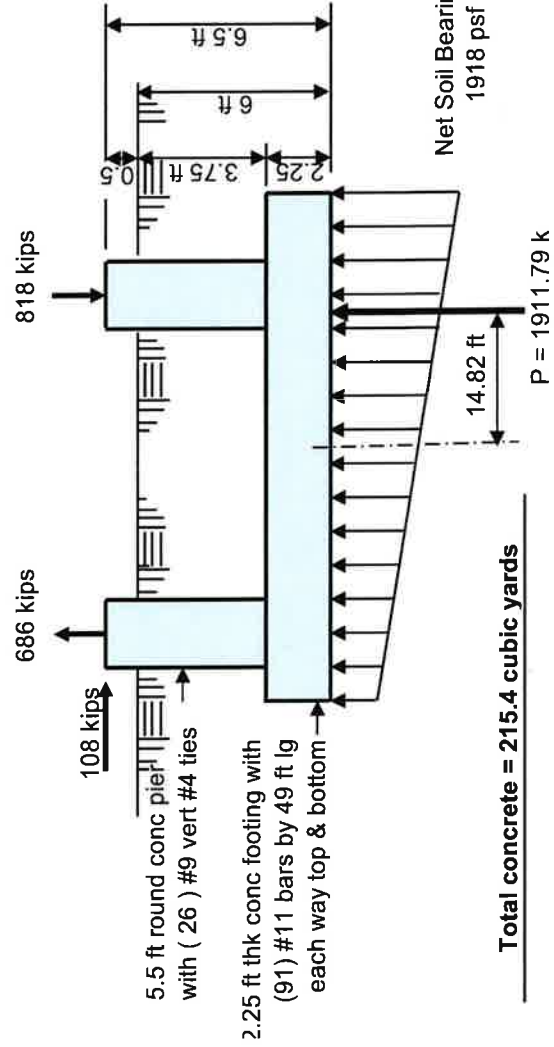
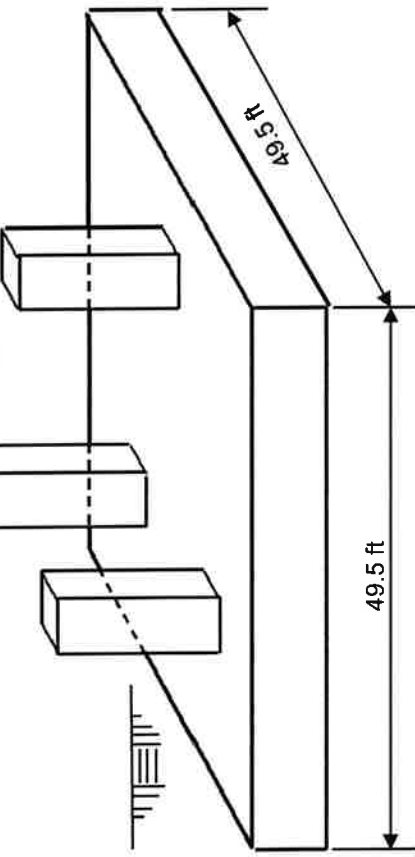
- Concrete strength  $F'_c = 4$  (ksi)
- Rebar Strength  $F_y = 60$  (ksi)
- Soil Density = **125** (pcf)
- Depth to Water Table = **9** (ft)
- minimum cover over vert rebar = **3** inches

Overturning Moment = 26458 ft-k

Total Horizontal Load = 179 k

1.2D => Tower

Wt = 164 k



**Total concrete = 215.4 cubic yards**

818 kips

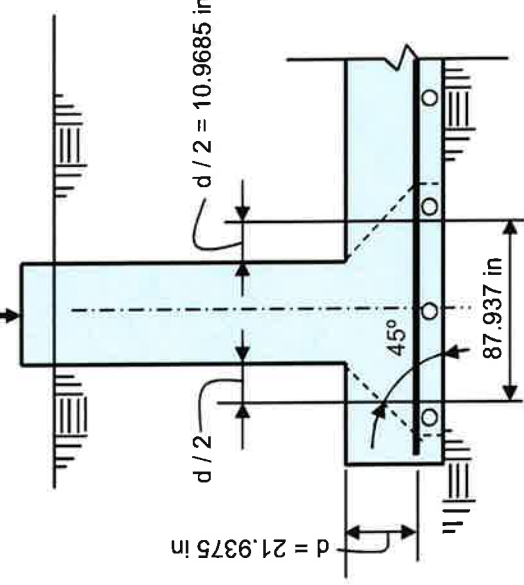


Fig Overturning Resistance = 47316.7 ft-kips  
 Total Overturning Moment = 28331.9 ft-kips  
 Required Overturning Safety Factor = 1  
 Overturning Safety Factor = 1.67  
**Ratio = 0.6 OK**

Maximum Net Soil Bearing = 2.689 ksf  
 Ultimate Net Soil Bearing = 9 ksf  
**Soil Bearing Stress Ratio = 0.3 OK**

Ult Punching Shear Capacity = 253 psi  
 Ult Punching Shear Force = 217 psi  
**Punching Shear Stress Ratio = 0.86 OK**

Pad Bending Moment Capacity = 6619 ft-k  
 Pad Bending Moment = 3432 ft-k  
**Bending Moment Stress Ratio = 0.52 OK**

Pier Rebar Capacity = -1404 kips  
 Pier Rebar Required = -686 kips  
**Pier Rebar Stress Ratio = 0.49 OK**

Pad Bending Shear Capacity = 1236 ft-k  
 Pad Bending Shear = 246 ft-k  
**Bending Shear Stress Ratio = 0.2 OK**

STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON  
EXISTING STRUCTURES BY PAUL J. FORD AND COMPANY

- 1) Paul J. Ford and Company has not made a field inspection to verify the tower member sizes or the antenna/coax loading. If the existing conditions are not as represented on these drawings, we should be contacted immediately to evaluate the significance of the deviation.
- 2) No allowance was made for any damaged, missing, or rusted members. The analysis of this tower assumes that no physical deterioration has occurred in any of the structural components of the tower and that all the tower members have the same load carrying capacity as the day the tower was erected.
- 3) It is not possible to have all the detailed information to perform a thorough analysis of every structural sub-component of an existing tower. The structural analysis by Paul J. Ford and Company verifies the adequacy of the main structural members of the tower. Paul J. Ford and Company provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc.
- 4) The structural integrity of the existing tower foundation can only be verified if exact foundation sizes and soil conditions are known. Paul J. Ford and Company will not accept any responsibility for the adequacy of the existing foundations unless the foundation sizes and a soils report are provided.
- 5) This tower has been analyzed according to the minimum design wind loads recommended by the Telecommunications Industry Association Standard ANSI/TIA-222-G. If the owner or local or state agencies require a higher design wind load, Paul J. Ford and Company should be made aware of this requirement.
- 6) The enclosed sketches are a schematic representation of the tower that we have analyzed. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions and for the proper fit and clearance in the field.
- 7) Miscellaneous items such as antenna mounts etc. have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

**APPENDIX D**  
**MODIFICATION DRAWINGS**

# MODIFIED 280' SELF SUPPORT TOWER

## SITE: HIGGANUM SOUTH CT

330 PORKORNY STREET  
 HADDAM CONNECTICUT 06441  
 MIDDLESEX COUNTY

LAT: 41° 26' 36.9"; LONG: -72° 33' 58.9"

### PROJECT CONTACTS

CLIENT:  
 HUDSON DESIGN GROUP  
 CONTACT: SYLVESTER BHEMBE AT  
 SBHEMBE@HUDSONDESIGNGROUP.LLC.COM  
 PH: (978) 357-5553

ENGINEER OF RECORD:  
 P.J.FORD@PAULJFORD.COM

SHEET INDEX	
SHEET NUMBER	DESCRIPTION
T-1	TITLE SHEET
M-1	MI CHECKLIST AND NOTES
N-1	NOTES
S-1	TOWER ELEVATION
S-2	DIAGONAL STITCH BOLT REINFORCING

TOWER MANUFACTURER: VALMONT  
 TOWER MANUFACTURER #: 240898

QUALIFIED ENGINEERING SERVICES ARE AVAILABLE FROM PAUL J. FORD & COMPANY TO ASSIST CONTRACTORS IN CLASS IV RIGGING PLAN REVIEWS. FOR REQUESTED QUALIFIED ENGINEERING SERVICES, PLEASE CONTACT P.J.FORD@PAULJFORD.COM.

### WIND DESIGN DATA

REFERENCE STANDARD	ANSI/TIA-222-G-2-2009
LOCAL CODE	2018 CSBC
ULTIMATE WIND SPEED (3-SECOND GUST)	140 MPH
CONVERTED NOMINAL WIND SPEED (3-SECOND GUST)	108 MPH
ICE THICKNESS	0.75 IN.
ICE WIND SPEED	50 MPH
SERVICE WIND SPEED	60 MPH
RISK CATEGORY	III
EXPOSURE CATEGORY	C
MAXIMUM TOPOGRAPHIC FACTOR, $K_{zt}$	1.0



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**PAUL J. FORD & COMPANY**  
 250 E Broad St, Ste 600, Columbus, OH 43215  
 Phone 614.221.6679  
 www.pauljford.com

**HUDSON DESIGN GROUP**  
 1800 OGDON ST SUITE 2-101 BUILDING 20 NORTH N ANDOVER, MA 01845  
 PH (978) 557-5553

**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

PROJECT No. 00079-0111-005-8502  
 DRAWN BY: RJK  
 DESIGNED BY: MTS  
 CHECKED BY: JPI  
 DATE: 5/1/2020

TITLE SHEET

T-1

REV	DATE	DESCRIPTION

1800 080000 87 SUITE 2-101 BUILDING 20 NORTH N ANDOVER MA 01845  
 PH (978) 552-5553  
**HUDSON DESIGN GROUP**  
 Phone 614.221.6679 www.pauljford.com  
 230 E Broad St, 5th Fl, 600 Columbus, OH 43215  
**PAUL J. FORD & COMPANY**

PROJECT No. 00019-0111 006 8800  
 DRAWN BY: MFB  
 DESIGNED BY: JPL  
 CHECKED BY: JPL  
 DATE: 5/21/2020

**MI CHECKLIST AND NOTES**

**MI-1**

**SITE: HIGGANUM SOUTH CT  
 HADDAM CONNECTICUT  
 MODIFIED 280 SELF SUPPORT TOWER**

**POST-MODIFICATION CHECKLIST**

**REQUIREMENT REPORT ITEM BRIEF DESCRIPTION**

**PRE-CONSTRUCTION**

THIS CHECKLIST SHALL BE INCLUDED IN THE MI REPORT

FABRICATION DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD FOR REVIEW. THE CONTRACTOR SHALL PROVIDE THE APPROVED SHOP DRAWINGS TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT. SEE SHOP DRAWING NOTES

A LETTER FROM THE FABRICATOR, STATING THAT THE WORK WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THE CONTRACT DOCUMENTS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

CENTRAL SHOP WELDS THAT REQUIRE TESTING ARE NOTED ON THESE CONTRACT DRAWINGS. A CERTIFIED WELD INSPECTOR SHALL PERFORM NON DESTRUCTIVE TESTING AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

ALL CERTIFICATION SHALL BE PROVIDED FOR ALL STEEL WITH A WELD STRENGTH GREATER THAN 36 KSI AND THIS DOCUMENTATION SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

A VISUAL OBSERVATION OF A PORTION OF THE EXISTING STRUCTURE (AS NOTED ON THESE DRAWINGS) IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

A VISUAL OBSERVATION OF THE ROLE TO BASE PLATE CONNECTION IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

THE MATERIAL SHIPPING LIST SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

**CONSTRUCTION**

A LETTER FROM THE GENERAL CONTRACTOR STATING THAT THE WORKMANSHIP WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THESE CONTRACT DRAWINGS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

A VISUAL OBSERVATION OF THE EXCAVATION AND REBAR SHALL BE PERFORMED BEFORE PLACING THE CONCRETE. A WRITTEN REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

THE CONCRETE MIX DESIGN, SLUMP TEST, AND COMPRESSIVE STRENGTH TESTS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

ANCHOR ROD INSTALLATION SHALL INCLUDE VERIFICATION BY LETTER AND PHOTOGRAPHIC DOCUMENTATION

A LETTER FROM THE GENERAL CONTRACTOR SHALL BE PROVIDED TO THE MI INSPECTOR THAT CERTIFIES THAT THE GROUT WAS INSTALLED IN ACCORDANCE WITH INDUSTRY STANDARDS FOR INCLUSION IN THE MI REPORT.

A CERTIFIED WELD INSPECTOR SHALL INSPECT AND TEST AS NECESSARY ALL FIELD WELDS AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT. THE DURING AND POST WELD INSPECTION IS REQUIRED

FOUNDATION SUB-GRADES SHALL BE INSPECTED AND APPROVED BY A GEOTECHNICAL ENGINEER AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE MI INSPECTOR VERIFYING THAT ANY ON-SITE COLD GALVANIZING WAS APPLIED FOR FIELD PUNCH-DRILLED HOLES

THE GENERAL CONTRACTOR SHALL PROVIDE A REPORT TO THE MI INSPECTOR INDICATING THE TEMPERATURE AND TENSION IN EVERY GUY WIRE FOR INCLUSION IN THE MI REPORT.

THE GENERAL CONTRACTOR SHALL PROVIDE THE CONTRACT DRAWINGS EITHER STATING INSTALLED AS DESIGNED OR NOTING ANY CHANGES THAT WERE REQUIRED AND APPROVED BY THE ENGINEER OF RECORD TO FIELD CONDITIONS

THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE MI INSPECTOR VERIFYING THAT ANY MAGN. SEC COATING WAS APPLIED IN ACCORDANCE PER ASTM F1188

THE GENERAL CONTRACTOR SHALL PROVIDE INSTALLER'S DRILLING AND INSTALLATION LOGS AND QA/QC DOCUMENTATION TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

**POST-CONSTRUCTION**

THE MI INSPECTOR SHALL OBSERVE AND REPORT ANY DISCREPANCIES BETWEEN THE CONTRACTORS REDLINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION

POST INSTALLED ANCHOR RODS SHALL BE TESTED IN ACCORDANCE WITH INDUSTRY STANDARD AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

PHOTOGRAPHS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT. THE PHOTOS SHALL BE ORGANIZED IN A MANNER THAT EASILY DENOTES THE EXACT LOCATION OF THE PHOTO

POST INSTALLED ANCHORS SHALL BE TESTED AND INSPECTED IN ACCORDANCE WITH SPECIFICATION STATED ON MICROPIER/ROCK ANCHOR NOTES

NOTE: X DENOTES A DOCUMENT REQUESTED FROM THE CONTRACTOR FOR THE MI REPORT  
 NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE MI REPORT

**MODIFICATION INSPECTION NOTES:**

**GENERAL**

THE MODIFICATION INSPECTION (MI) IS A VISUAL INSPECTION OF TOWER MODIFICATIONS AND A REVIEW OF CONSTRUCTION INSPECTIONS AND OTHER DOCUMENTS. THE MI IS TO BE CONDUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, NAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF RECORD (EOR).

THE MI IS TO CONTROL INSTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A REVIEW OF THE MODIFICATION DESIGN ITSELF. NOR DOES THE MI INSPECTOR TAKE OWNERSHIP OF THE MODIFICATION DESIGN. OWNERSHIP OF THE STRUCTURAL MODIFICATION DESIGN EFFECTIVENESS AND INTEGRITY RESIDES WITH THE EOR AT ALL TIMES.

TO ENSURE THAT THE REQUIREMENTS OF THE MI ARE MET, IT IS VITAL THAT THE GENERAL CONTRACTOR (GC) AND THE MI INSPECTOR BEGIN COMMUNICATING AND COORDINATING AS SOON AS A PO IS RECEIVED. IT IS EXPECTED THAT EACH PARTY WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY.

THE MI INSPECTOR IS REQUIRED TO CONTACT THE GC AS SOON AS RECEIVING A PO FOR THE MI TO, AT A MINIMUM

- REVIEW THE REQUIREMENTS OF THE MI CHECKLIST
- WORK WITH THE GC TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS

THE MI INSPECTOR IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) INSPECTION AND TEST REPORTS, REVIEWING THE DOCUMENTS FOR ADHERENCE TO THE CONTRACT DOCUMENTS, CONDUCTING THE IN-FIELD INSPECTIONS, AND SUBMITTING THE MI REPORT TO THE OWNER

**GENERAL CONTRACTOR**

THE GC IS REQUIRED TO CONTACT THE MI INSPECTOR AS SOON AS RECEIVING A PO FOR THE MODIFICATION INSTALLATION OR TURNKEY PROJECT TO, AT A MINIMUM

- REVIEW THE REQUIREMENTS OF THE MI CHECKLIST
- WORK WITH THE MI INSPECTOR TO DEVELOP A SCHEDULE TO CONDUCT ON-SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS
- BETTER UNDERSTAND ALL INSPECTION AND TESTING REQUIREMENTS IN ACCORDANCE WITH INDUSTRY STANDARD

THE GC SHALL PERFORM AND RECORD THE TEST AND INSPECTION RESULTS IN ACCORDANCE WITH INDUSTRY STANDARD

**RECOMMENDATIONS**

THE FOLLOWING RECOMMENDATIONS AND SUGGESTIONS ARE OFFERED TO ENHANCE THE EFFICIENCY AND EFFECTIVENESS OF DELIVERING A MI REPORT

- IT IS SUGGESTED THAT THE GC PROVIDE A MINIMUM OF 5 BUSINESS DAYS NOTICE, PREFERABLE 10, TO THE MI INSPECTOR AS TO WHEN THE SITE WILL BE READY FOR THE MI TO BE CONDUCTED
- THE GC AND MI INSPECTOR COORDINATE CLOSELY THROUGHOUT THE MI PROCESS
- WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MI INSPECTOR ON-SITE SIMULTANEOUSLY FOR ANY GUY WIRE TENSIONING OR RE-TENSIONING OPERATIONS
- IT MAY BE BENEFICIAL TO INSTALL ALL TOWER MODIFICATIONS PRIOR TO THE MI INSPECTION
- THE GC AND MI INSPECTOR SHALL COORDINATE WITH THE SITE VISIT AND MI INSPECTIONS TO COMMENCE WITH ONE SITE VISIT
- WHEN POSSIBLE, IT IS PREFERRED TO HAVE THE GC AND MI INSPECTOR ON-SITE DURING THE MI TO HAVE ANY DEFICIENCIES CORRECTED DURING THE INITIAL MI. THEREFORE, THE GC MAY CHOOSE TO FACILITATE THE MI INSPECTION AT THE GENERAL CONTRACTOR'S FACILITIES ARE AT THEIR DISPOSAL WHEN THE MI INSPECTORS ON SITE

**CANCELLATION OR DELAYS IN SCHEDULED MI**

IF THE GC AND MI INSPECTOR AGREE TO ADJUTE ON WHICH THE MI WILL BE CONDUCTED AND EITHER PARTY WANTS TO CANCEL OR DELAYS, THE OWNER OWNER AND OTHER PARTIES RELATED TO THE CANCELLATION OR DELAY INCURRED BY EITHER PARTY FOR ANY TIME (E.G. TRAVEL AND LOGGING, COSTS OF KEEPING EQUIPMENT ON-SITE, ETC.) IF THE TOWER OWNER CONTRACTS DIRECTLY FOR A THIRD PARTY TO CONDUCT THE MI, THE MI INSPECTOR SHALL BE ADVISED OF ANY SUCH ARRANGEMENTS AND OTHER CONDITIONS THAT MAY COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

**CORRECTION OF FINDINGS**

IF THE MI INSPECTOR IDENTIFIES ANY FINDINGS THAT WOULD FAIL THE MI, THE GC SHALL WORK WITH THE EOR TO COORDINATE A REMEDIATION PLAN IN ONE OF TWO WAYS

- CORRECT FINDINGS (ISSUES TO CORRECT) WITH THE SPECIFICATIONS CONTAINED IN THE ORIGINAL CONTRACT DOCUMENTS AND COORDINATE A SUPPLEMENT MI
- OR, WITH OWNERS APPROVAL, THE GC MAY WORK WITH THE EOR TO RE-ANALYZE THE MODIFICATION/REINFORCEMENT USING THE AS-BUILT PHOTOGRAPHS

BEFORE THE MI, THE GC AND THE MI INSPECTOR THE FOLLOWING PHOTOGRAPHS AT A MINIMUM, ARE TO BE TAKEN AND INCLUDED IN THE MI REPORT:

- PRE-CONSTRUCTION GENERAL SITE CONDITION
- PHOTOGRAPHS DURING THE REINFORCEMENT MODIFICATION
- CONSTRUCTION INSPECTION AND INSPECTION
- RAW MATERIALS
- FOUNDATIONAL DETAIL DETAILS
- FOUNDATION MODIFICATIONS
- WELD PREPARATION
- BOLT INSTALLATION AND TORQUE
- FINAL INSTALLED CONDITION
- POST CONSTRUCTION PHOTOGRAPHS
- FINAL INFELD CONDITION

PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED INADEQUATE.

THIS IS NOT A COMPLETE LIST OF REQUIRED PHOTOS. PLEASE COORDINATE WITH THE MI

SHOP DRAWINGS

EOR APPROVED SHOP DRAWINGS CAN BE PROVIDED AS AN ADDITIONAL SCOPE OF SERVICE. IF REQUIRED, PLEASE CONTACT P.J.F. FOR ADDITIONAL INFORMATION

**CONSTRUCTION**

A LETTER FROM THE GENERAL CONTRACTOR STATING THAT THE WORKMANSHIP WAS PERFORMED IN ACCORDANCE WITH INDUSTRY STANDARDS AND THESE CONTRACT DRAWINGS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

A VISUAL OBSERVATION OF THE EXCAVATION AND REBAR SHALL BE PERFORMED BEFORE PLACING THE CONCRETE. A WRITTEN REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

THE CONCRETE MIX DESIGN, SLUMP TEST, AND COMPRESSIVE STRENGTH TESTS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.

ANCHOR ROD INSTALLATION SHALL INCLUDE VERIFICATION BY LETTER AND PHOTOGRAPHIC DOCUMENTATION

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 NA DENOTES A DOCUMENT THAT IS NOT REQUIRED FOR THE MI REPORT

PROJECT No. 00019-0111 006 8800  
 DRAWN BY: MFB  
 DESIGNED BY: JPL  
 CHECKED BY: JPL  
 DATE: 5/21/2020

**MI CHECKLIST AND NOTES**

**MI-1**

**SITE: HIGGANUM SOUTH CT  
 HADDAM CONNECTICUT  
 MODIFIED 280 SELF SUPPORT TOWER**



REV	DATE	DESCRIPTION



GENERAL NOTES:

1. THIS TOWER MODIFICATION DRAWING IS BASED UPON A STRUCTURAL ANALYSIS PERFORMED BY PAUL J. FORD AND COMPANY DATED 5/21/2020.
2. PAUL J. FORD AND COMPANY HAS NOT PERFORMED A FIELD VISIT TO VERIFY THE EXISTING TOWER MEMBER SIZES AND DIMENSIONS. THE MODIFICATIONS SHOWN ON THESE PAGES WERE DEVELOPED USING INFORMATION PROVIDED TO US BY HUDSON DESIGN GROUP.
3. THE CONTRACTOR IS EXPECTED TO PERFORM A SITE VISIT BEFORE FABRICATING ANY MATERIAL. IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT ARE NOT AS REPRESENTED ON THESE DRAWINGS, PAUL J. FORD AND COMPANY SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE STRUCTURAL SIGNIFICANCE OF THE DEVIATION.
4. THE CONTRACTOR MUST BE EXPERIENCED IN THE PERFORMANCE OF WORK SIMILAR TO THAT DESCRIBED ON THESE DRAWINGS. BY ACCEPTANCE OF THIS PROJECT, THE CONTRACTOR IS ATTESTING THAT HE DOES HAVE SUFFICIENT EXPERIENCE AND ABILITY, THAT HE IS KNOWLEDGEABLE OF THE WORK TO BE PERFORMED AND THAT HE IS PROPERLY LICENSED TO DO THIS WORK IN THE JURISDICTION IN WHICH THE WORK IS TO BE PERFORMED.
5. THIS DRAWING DOES NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION METHODS, MEANS, TECHNIQUES, SEQUENCES AND PROCEDURES.
6. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR INITIATING, MAINTAINING, AND SUPERVISING ALL SAFETY PROGRAMS AND PRECAUTIONS IN CONNECTION WITH THE WORK.
7. INSPECTIONS SHALL BE COMPLETED IN ACCORDANCE WITH LOCAL BUILDING CODES.

CONSTRUCTION NOTES:

1. ALL CONSTRUCTION MEANS AND METHODS, INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN AND SHALL MEET ANSI/ASSE A10.48 (LATEST EDITION), FEDERAL, STATE, AND LOCAL REGULATIONS; AND ANY APPLICABLE INDUSTRY CONSENSUS STANDARDS RELATED TO THE CONSTRUCTION ACTIVITIES BEING PERFORMED. ALL RIGGING PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION)
2. ALL HOLES, EITHER PUNCHED OR DRILLED, IN THE EXISTING STEEL MEMBERS SHALL BE 1/16 INCH LARGER THAN THE BOLT DIAMETER UNLESS NOTED OTHERWISE. SLOTTED OR OVERSIZED HOLES ARE NOT PERMITTED.
3. ANY GALVANIZED SURFACE THAT IS SCRATCHED OR DAMAGED DUE TO THE CONTRACTOR'S EFFORTS, SHALL BE REPAIRED WITH A COLD GALVANIZING COMPOUND CONFORMING TO ASTM A780.

MATERIAL NOTES:

1. PRIOR TO FABRICATION AND INSTALLATION, CONTRACTOR SHALL FIELD VERIFY ALL LENGTHS AND QUANTITIES GIVEN. LENGTH AND QUANTITIES PROVIDED ARE FOR QUOTING PURPOSES ONLY AND SHALL NOT BE USED FOR FABRICATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROPER FIT AND CLEARANCE OF THE REINFORCING MATERIAL IN THE FIELD. THE CONTRACTOR IS EXPECTED TO PERFORM A SITE VISIT BEFORE FABRICATING ANY MATERIAL.
2. ALL STEEL SHALL CONFORM TO THE FOLLOWING (U.N.O.):
  - A. PLATES: ASTM A36 GR 36 (36 KSI YIELD POINT MATERIAL)
3. ALL NEW STEEL SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH THE SPECIFICATION FOR ZINC (HOT GALVANIZED) COATING ON PRODUCTS FABRICATED FROM ROLLED, PRESSED AND FORGED STEEL SHAPES, PLATES BAR, AND STRIP" ASTM A123.
4. ALL BOLTS SHALL CONFORM TO THE REQUIREMENTS OF ASTM A325. USE BEARING TYPE CONNECTIONS. TIGHTEN TO A SNUG TIGHT CONNECTION, UNO.
5. ALL BOLTS SHALL BE PROVIDED WITH LOCK-WASHERS, OR LOCK-NUTS, OR PAL-NUTS AND SHALL BE GALVANIZED ACCORDING TO ASTM A153/ASTM153M.



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**PJF PAUL J. FORD & COMPANY**  
 250 E Broad St, Ste 600  
 Columbus, OH 43215  
 Phone 614.221.6679  
 www.pjford.com

**HUDSON DESIGN GROUP**  
 1800 OSWEGO RD SUITE 2101 BUILDING 20 NORTH ANDOVER, MA 01845  
 PH: (978) 557-5553

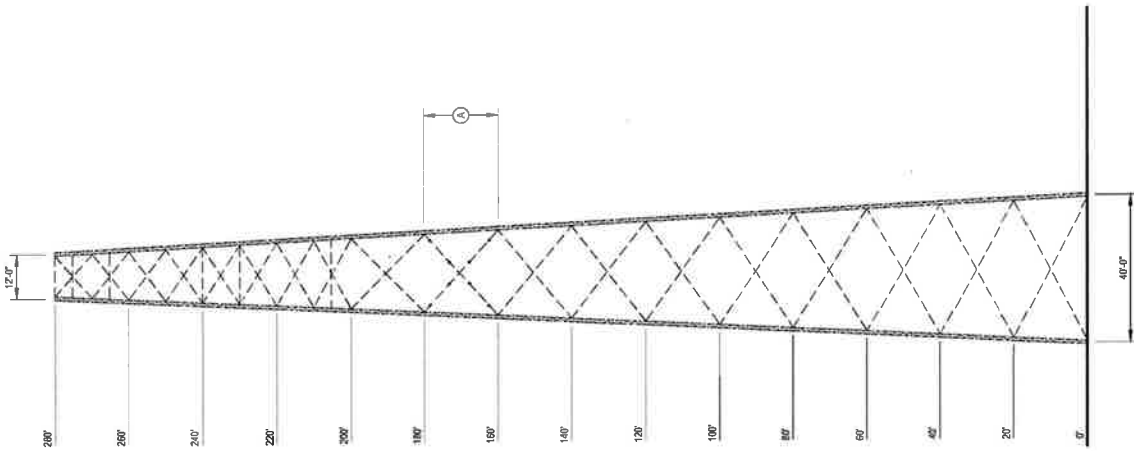
**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

PROJECT No.	00019-0111 005 8000
DRAWN BY:	RAM
DESIGNED BY:	MTM
CHECKED BY:	JPL
DATE	5/21/2020

NOTES

N-1

REV	DATE	DESCRIPTION



TOWER ELEVATION 1  
S-1

TOWER MODIFICATION SCHEDULE		
ELEVATION	TOWER MODIFICATION DESCRIPTION	REFERENCE SHEETS
A	INSTALL STITCH BOLTS AND SPACER PLATES EXISTING DIAGONALS	S-2

PRIOR TO FABRICATION AND INSTALLATION, CONTRACTOR SHALL VERIFY ALL LENGTHS AND QUANTITIES GIVEN LENGTH AND QUANTITIES PROVIDED ARE FOR QUOTING PURPOSE ONLY AND SHALL NOT BE USED FOR FABRICATION



REV	DATE	DESCRIPTION

**RJF PAUL J. FORD & COMPANY**  
 250 E Broad St, Ste 600 - Columbus, OH 43215  
 Phone 614.221.6679 www.pauljford.com

**HUDSON DESIGN GROUP**  
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**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

PROJECT No. 0001903111.005.8000  
 DRAWN BY: RANK  
 DESIGNED BY: MFB  
 CHECKED BY: JPL  
 DATE 5/21/2020

TOWER  
 ELEVATION

S-1

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**SITE: HIGGANUM SOUTH CT**  
**HADDAM CONNECTICUT**  
**MODIFIED 280' SELF SUPPORT TOWER**

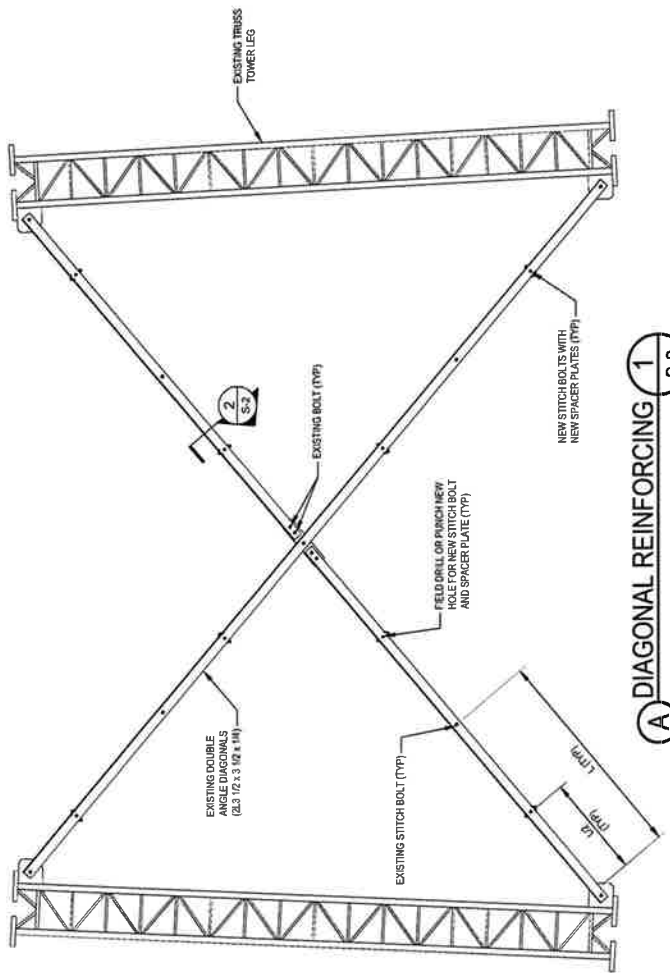
PROJECT No. 00019-0111-006-8800  
 DRAWN BY: RAK  
 DESIGNED BY: MTH  
 CHECKED BY: JPL  
 DATE: 5/21/2020

**DIAGONAL STITCH  
 BOLT  
 REINFORCING**

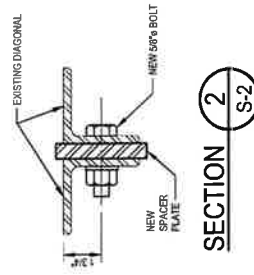
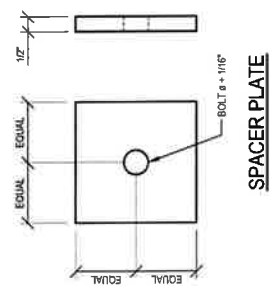
**S-2**

**MATERIAL LIST**

ELEVATION	QTY	MATERIAL	LENGTH
1875 TO 1872	24	SPACER PLATE 1/2" x 4"	0'-4"
	24	5/8" BOLTS	2'-11"



**A** **DIAGONAL REINFORCING** **1** **S-2**



05.21.2020

REV	DATE	DESCRIPTION

# **ATTACHMENT 5**



February 25, 2019  
May 6, 2019 (Rev.1)



20 Alexander Drive  
Wallingford, CT 06492

RE: Site Name: HIGGANUM SOUTH CT  
Site Address: 330 Pokorny Road  
Haddam, CT 06441

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by Verizon to perform a mount analysis on the existing Verizon antenna mounts to determine their capability of supporting the following equipment loading:

- (3) HBXX-6517DS-A2M Antennas (75.0"x12.0"x6.5" – Wt. = 41 lbs. /each)
- (3) LNX-6515DS-A1M Antennas (96.6"x11.9"x7.1" – Wt. = 44 lbs. /each)
- (3) RC3DC-3315-PF-48 Junction Boxes (28.9"x15.7"x10.3" – Wt. 32 lbs. /each)
- **(6) NHH 65C R2B Antennas (96.0"x11.9"x7.1" – Wt. = 52 lbs. /each)**
- **(3) B2/B66 RRH-BR049 RRH's (15.0"x15.0"x10.0" – Wt. = 85 lbs. /each)**
- **(3) B5/B13 RRH-BR04C RRH's (15.0"x15.0"x8.1" – Wt. = 82 lbs. /each)**

*\*Proposed equipment shown in bold.*

A survey climb and mapping of the antenna mount was not performed at this site. Mount fabrication drawings prepared by SitePro1 (P/N VFA12-RRU) dated April 7, 2014 were used to perform this analysis.

Based on our analysis, we have determined that the existing antenna mounts **ARE NOT CAPABLE** of supporting the proposed antenna installation. HDG recommends the following modifications:

- **Install new Sector Frame Stabilizer Kit, SitePro1 SFS-V (or approved equal) (typ. of 1 per sector, total of 3).**
- **Install new 2" std. (2.38" O.D.) pipe brace secured to existing mount and tower (typ. of 1 per sector, total of 3).**
- **Install new 2-1/2" std. (2.88" O.D.) pipe masts behind new NHH 65C R2B antennas (typ. of 1 per sector, total of 3).**

	Member	Controlling Load Case	Stress Ratio	Pass/Fail
Existing Mount Rating	37	LC3	171%	<b>FAIL</b>
Modified Mount Rating	37	LC1	86%	<b>PASS</b>

This analysis was conducted in accordance with EIA/TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the International Building Code 2015 with 2018 Connecticut State Building Code Amendments (See the attached analysis).

**Reference Documents:**

- Fabrication drawings prepared by SitePro1, P/N VFA12-RRU, dated April 7, 2014.

**This determination was based on the following limitations and assumptions:**

1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities. Contractor to perform pre-inspection prior to construction.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mounts have been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to Verizon's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,  
Hudson Design Group LLC



Michael Cabral  
Structural Dept. Head



Daniel P. Hamm, PE  
Principal



**FIELD PHOTOS:**





**HUDSON**  
Design Group LLC

**Wind & Ice  
Calculations**



Date: 5/6/2019  
 Project Name: HIGGANUM SOUTH CT  
 Designed By: JP Checked By: MSC



**2.6.5.2 Velocity Pressure Coeff:**

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$K_z =$  **1.107**       $z =$  149 (ft)  
 $z_g =$  1200 (ft)  
 $\alpha =$  7.0

$K_{zmin} \leq K_z \leq 2.01$

**Table 2-4**

Exposure	$Z_g$	$\alpha$	$K_{zmin}$	$K_e$
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

**2.6.6.4 Topographic Factor:**

**Table 2-5**

Topo. Category	$K_t$	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_e K_t / K_h)]^2$$

$$K_h = e^{(fz/H)}$$

$K_{zt} =$  #DIV/0!

$K_h =$  #DIV/0!

$K_e =$  0.9 (from Table 2-4)

$K_t =$  0 (from Table 2-5)

$f =$  0 (from Table 2-5)

$z =$  149

$H =$  0 (Ht. of the crest above surrounding)

$K_{zt} =$  1.00

$K_{iz} =$  1.16 (from Sec. 2.6.8)

*(If Category 1 then  $K_{zt} = 1.0$ )*

Category= **1**

**2.6.8 Design Ice Thickness**

Max Ice Thickness =

$t_i =$  0.75 in

$$t_{iz} = 2.0 * t_i * I * K_{iz} * (K_{zt})^{0.35}$$

$t_{iz} =$  1.74 in



**Determine Ca:**

**Table 2-8**

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Round	C < 32 (Subcritical)	0.7	0.8	1.2
	32 ≤ C ≤ 64 (Transitional)	$3.76/(C^{0.485})$	$3.37/(C^{0.415})$	$38.4/(C^{1.0})$
	C > 64 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.  
 (Aspect ratio is independent of the spacing between support points of a linear appurtenance.)

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness =

1.74 in

Angle = 0 (deg)

Equivalent Angle = 180 (deg)

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)
HBXX-6517DS-A2M Antenna	75.0	12.0	6.5	6.25	6.25	1.37	296	70
NHH 65C R2B Antenna	96.0	11.9	7.1	7.93	8.07	1.44	395	92
LNX-6515DS-A1M Antenna	96.6	11.9	7.1	7.98	8.12	1.44	398	93
B2/B66 RRH-BR049 RRH	15.0	15.0	10.0	1.56	1.00	1.20	65	17
B5/B13 RRH-BR04C RRH	15.0	15.0	8.1	1.56	1.00	1.20	65	17
RC3DC-3315-PF-48 Junction Box	28.9	15.7	10.3	3.15	1.84	1.20	131	31

Date: 5/6/2019

Project Name: HIGGANUM SOUTH CT

Designed By: JP Checked By: MSC



### ICE WEIGHT CALCULATIONS

Thickness of ice: 1.74 in.  
Density of ice: 56 pcf

#### HBXX-6517DS-A2M Antenna

Weight of ice based on total radial SF area:  
Height (in): 75.0  
Width (in): 12.0  
Depth (in): 6.5  
Total weight of ice on object: 204 lbs  
Weight of object: 41.0 lbs  
Combined weight of ice and object: 245 lbs

#### NHH 65C R2B Antenna

Weight of ice based on total radial SF area:  
Height (in): 96.0  
Width (in): 11.9  
Depth (in): 7.1  
Total weight of ice on object: 265 lbs  
Weight of object: 52.0 lbs  
Combined weight of ice and object: 317 lbs

#### LNX-6515DS-A1M Antenna

Weight of ice based on total radial SF area:  
Height (in): 96.6  
Width (in): 11.9  
Depth (in): 7.1  
Total weight of ice on object: 267 lbs  
Weight of object: 44.0 lbs  
Combined weight of ice and object: 311 lbs

#### B2/B66 RRH-BR049 RRH

Weight of ice based on total radial SF area:  
Height (in): 15.0  
Width (in): 15.0  
Depth (in): 10.0  
Total weight of ice on object: 53 lbs  
Weight of object: 85.0 lbs  
Combined weight of ice and object: 138 lbs

#### B5/B13 RRH-BR04C RRH

Weight of ice based on total radial SF area:  
Height (in): 15.0  
Width (in): 15.0  
Depth (in): 8.1  
Total weight of ice on object: 50 lbs  
Weight of object: 82.0 lbs  
Combined weight of ice and object: 132 lbs

#### RC3DC-3315-PF-48 Junction Box

Weight of ice based on total radial SF area:  
Height (in): 28.9  
Width (in): 15.7  
Depth (in): 10.3  
Total weight of ice on object: 105 lbs  
Weight of object: 32.0 lbs  
Combined weight of ice and object: 137 lbs

#### 1-1/4" Pipe

Per foot weight of ice:  
diameter (in): 1.66  
Per foot weight of ice on object: 7 plf

#### 2" pipe

Per foot weight of ice:  
diameter (in): 2.38  
Per foot weight of ice on object: 9 plf

#### 2-1/2" pipe

Per foot weight of ice:  
diameter (in): 2.88  
Per foot weight of ice on object: 10 plf

#### 3" Pipe

Per foot weight of ice:  
diameter (in): 3.5  
Per foot weight of ice on object: 11 plf

#### 5/8" Round Bar

Per foot weight of ice:  
diameter (in): 0.625  
Per foot weight of ice on object: 5 plf

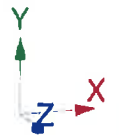
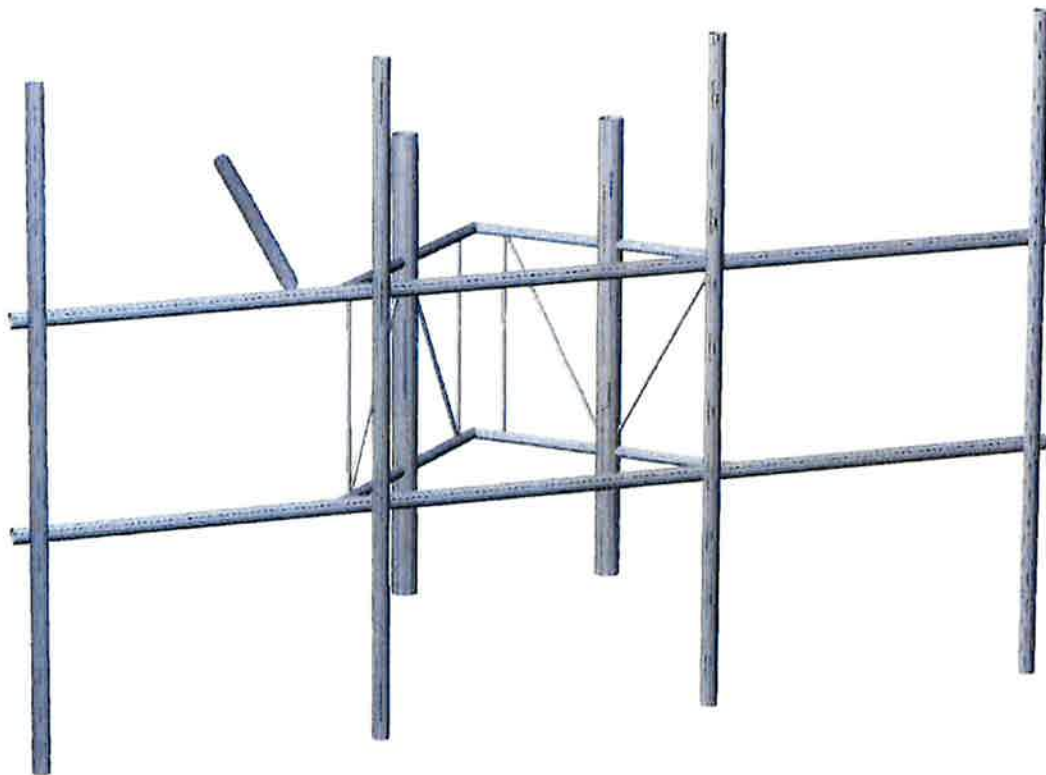
#### L 2-1/2x2-1/2 Angles

Weight of ice based on total radial SF area:  
Height (in): 2.5  
Width (in): 2.5  
Per foot weight of ice on object: 11 plf



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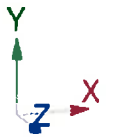
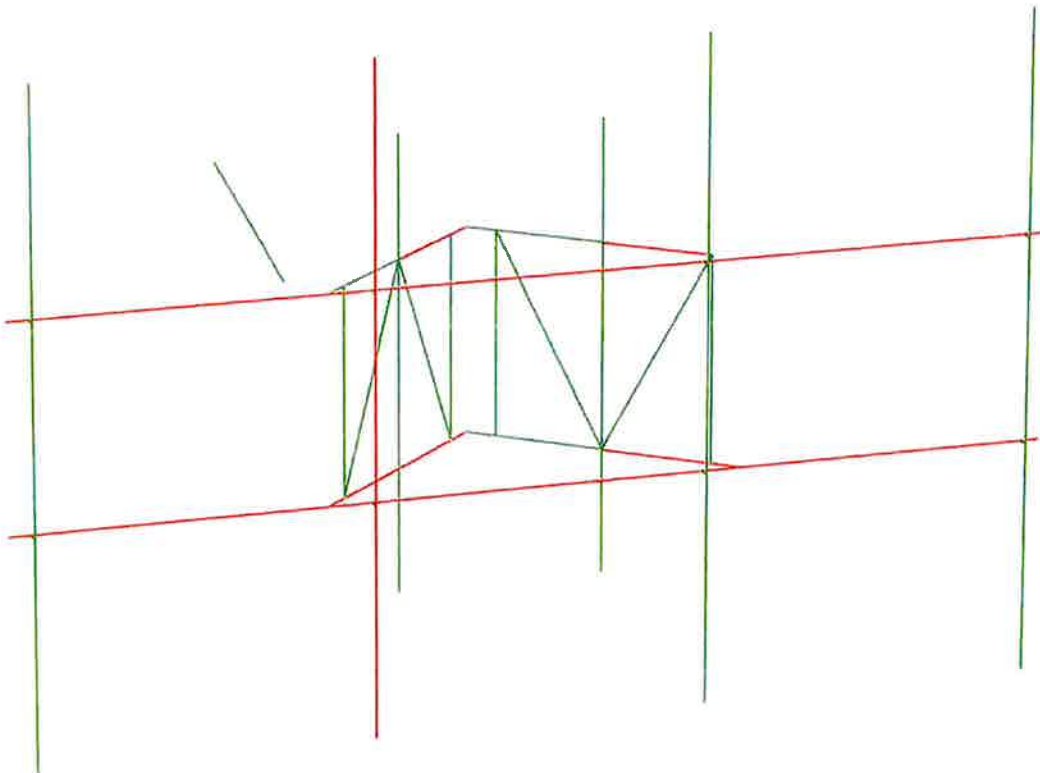
**ANTMO 2019 Mount Calculations  
(Existing Conditions)**



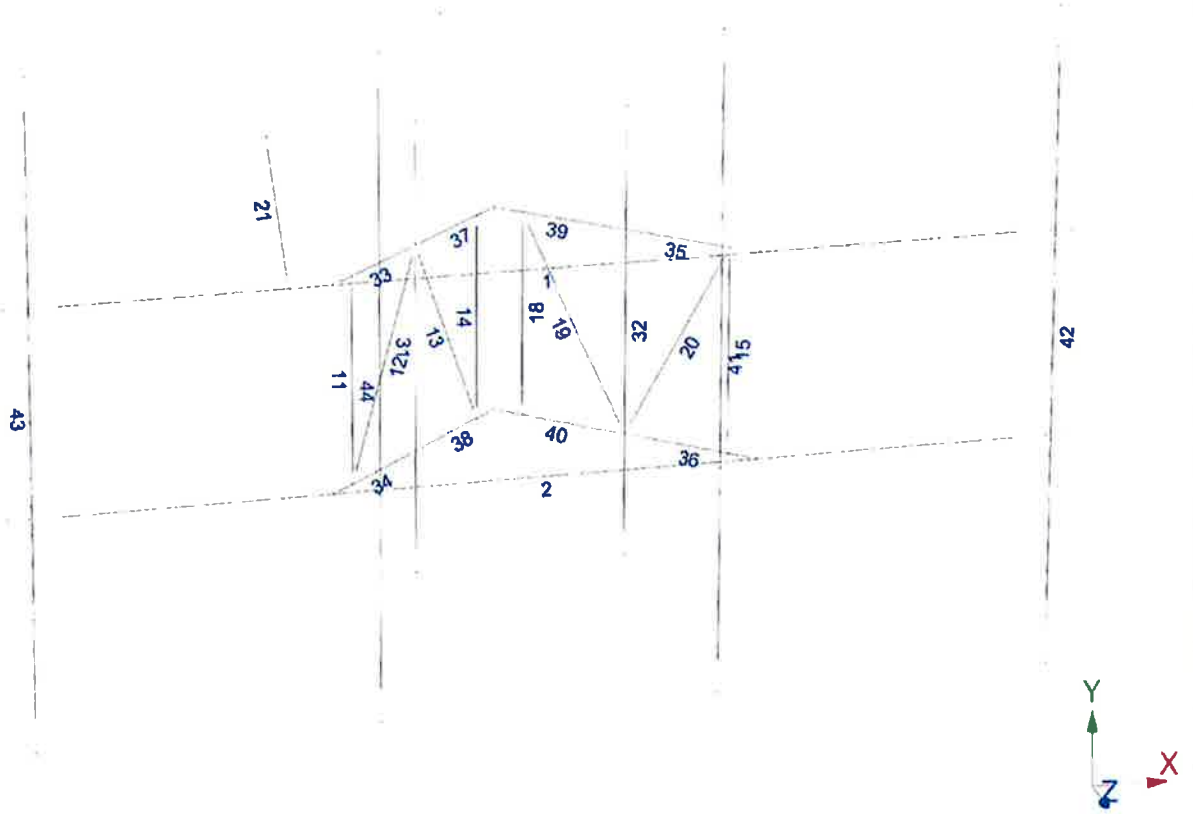


Design status

- Not designed
- Error on design
- Design O.K.
- With warnings







## Load data

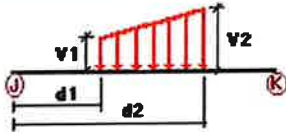
### GLOSSARY

Comb : Indicates if load condition is a load combination

### Load Conditions

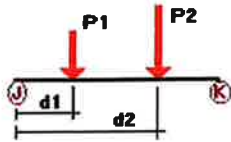
Condition	Description	Comb.	Category
DL	Dead Load	No	DL
Wo	Wind Load (No Ice)	No	WIND
Wi	Wind Load (With Ice)	No	WIND
Di	Ice Load	No	LL

### Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Di	1	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	2	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	11	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	12	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	13	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	14	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	15	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	18	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	19	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	20	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	21	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	31	Y	-0.011	-0.011	0.00	Yes	100.00	Yes
	32	Y	-0.011	-0.011	0.00	Yes	100.00	Yes
	41	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	42	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	43	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	44	Y	-0.009	-0.009	0.00	Yes	100.00	Yes

### Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%	
DL	31	y	-0.032	0.50	No	
		y	-0.085	2.00	No	
		y	-0.082	4.00	No	
	32	y	-0.085	2.00	No	
		y	-0.082	4.00	No	
	42	y	-0.022	0.50	No	
		y	-0.022	7.50	No	
	43	y	-0.021	0.50	No	
		y	-0.021	7.50	No	
	44	y	-0.052	0.50	No	
		y	-0.052	7.50	No	
		y	-0.026	4.00	No	
	Wo	31	z	-0.131	0.50	No
			z	-0.065	2.00	No
			z	-0.065	4.00	No
32		z	-0.065	2.00	No	
		z	-0.065	4.00	No	
42		z	-0.20	0.50	No	
		z	-0.20	7.50	No	
43		z	-0.149	0.50	No	
		z	-0.149	7.50	No	
44		z	-0.396	0.50	No	
		z	-0.396	7.50	No	
Wi		31	z	-0.031	0.50	No
	z		-0.017	2.00	No	
	z		-0.017	4.00	No	
	32	z	-0.017	2.00	No	
		z	-0.017	4.00	No	
	42	z	-0.047	0.50	No	
		z	-0.047	7.50	No	
	43	z	-0.035	0.50	No	
		z	-0.035	7.50	No	
	44	z	-0.092	0.50	No	
		z	-0.092	7.50	No	
	DI	14	y	-0.105	2.00	No
y			-0.105	0.50	No	
y			-0.053	2.00	No	
31		y	-0.05	4.00	No	
		y	-0.053	2.00	No	
32		y	-0.05	4.00	No	
		y	-0.053	2.00	No	
42		y	-0.133	0.50	No	
		y	-0.133	7.50	No	
43		y	-0.102	0.50	No	
		y	-0.102	7.50	No	
44		y	-0.265	0.50	No	
	y	-0.265	7.50	No		

### Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (No Ice)	No	0.00	0.00	0.00
Wi	Wind Load (With Ice)	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00

### Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
Wo	0.00	0.00	0.00
Wi	0.00	0.00	0.00
Di	0.00	0.00	0.00



Current Date: 2/22/2019 5:44 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\VERIZON\CT\Higganum South CT\ANTMO 2019\Higganum South CT.etz

## Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2DL+1.6Wo

LC2=0.9DL+1.6Wo

LC3=1.2DL+Wi+Di

LC4=1.2DL

LC5=0.9DL

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
<i>PIPE 1-1_4x0.140</i>		33	LC2 at 0.00%	0.84	OK	Eq. H1-1b
		34	LC2 at 0.00%	1.26	N.G.	Eq. H1-1b
		35	LC3 at 100.00%	1.08	N.G.	Eq. H1-1b
		36	LC1 at 0.00%	1.57	N.G.	Eq. H1-1b
		37	LC3 at 100.00%	1.71	N.G.	Eq. H1-1b
		38	LC3 at 100.00%	1.68	N.G.	Eq. H1-1b
		39	LC3 at 100.00%	0.84	OK	Eq. H1-1b
		40	LC1 at 0.00%	0.43	OK	Eq. H1-1b
		<i>PIPE 2x0.154</i>		1	LC2 at 30.47%	1.09
2	LC2 at 70.54%			1.19	N.G.	Eq. H1-1b
21	LC1 at 0.00%			0.31	OK	Eq. H1-1b
41	LC1 at 64.58%			0.65	OK	Eq. H1-1b
42	LC1 at 64.58%			0.73	OK	Eq. H1-1b
43	LC1 at 35.42%			0.59	OK	Eq. H1-1b
44	LC1 at 33.33%			1.56	N.G.	Eq. H1-1b
<i>PIPE 3x0.216</i>		31	LC3 at 29.17%	0.24	OK	Eq. H1-1b
		32	LC3 at 70.83%	0.15	OK	Eq. H1-1b
<i>RndBar 5_8</i>		11	LC3 at 100.00%	0.26	OK	Eq. H1-1b
		12	LC3 at 0.00%	0.41	OK	Eq. H1-1a
		13	LC3 at 100.00%	0.11	OK	Eq. H1-1b
		14	LC3 at 100.00%	0.54	OK	Eq. H1-1b
		15	LC3 at 100.00%	0.80	OK	Eq. H1-1b
		18	LC3 at 0.00%	0.09	OK	Eq. H1-1b
		19	LC3 at 100.00%	0.30	OK	Eq. H1-1a
		20	LC3 at 100.00%	0.27	OK	Eq. H1-1b



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Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\VERIZON\CT\Higganum South CT\ANTMO 2019\Higganum South CT.et\

## Geometry data

### GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member    0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

### Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	0.00	0.00	-2.60	0
2	-6.25	0.00	0.00	0
3	6.25	0.00	0.00	0
5	2.00	2.75	0.20	0
6	-6.25	-2.50	0.00	0
7	0.00	-2.50	-2.60	0
8	6.25	-2.50	0.00	0
9	-2.50	0.00	0.00	0
10	-2.50	-2.50	0.00	0
11	2.50	0.00	0.00	0
12	2.50	-2.50	0.00	0
13	-2.00	2.75	0.20	0
14	6.00	2.75	0.20	0
16	2.00	-5.25	0.20	0
17	-2.00	-5.25	0.20	0
18	6.00	-5.25	0.20	0
19	-0.2778	0.00	-2.3111	0
26	-2.2222	0.00	-0.2889	0
27	-1.25	0.00	-1.30	0
28	-2.2222	-2.50	-0.2889	0
29	-0.2778	-2.50	-2.3111	0

30	2.2222	-2.50	-0.2889	0
32	1.25	0.00	-1.30	0
33	0.2778	-2.50	-2.3111	0
34	0.2778	0.00	-2.3111	0
35	-2.00	0.00	-6.2889	0
51	1.25	-2.50	-1.30	0
52	-1.25	-2.50	-1.30	0
53	-6.00	2.75	0.20	0
54	-6.00	-5.25	0.20	0
59	-1.25	1.50	-1.30	0
60	1.25	1.50	-1.30	0
61	-1.25	-4.00	-1.30	0
62	1.25	-4.00	-1.30	0
63	-3.00	0.00	0.00	0
31	2.2222	0.00	-0.2889	0

**Restraints**

Node	TX	TY	TZ	RX	RY	RZ
1	1	1	1	1	1	1
7	1	1	1	1	1	1
35	1	1	1	0	0	0

**Members**

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	2	3		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
2	6	8		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
11	26	28		RndBar 5_8	A36	0.00	0.00	0.00
12	28	27		RndBar 5_8	A36	0.00	0.00	0.00
13	27	29		RndBar 5_8	A36	0.00	0.00	0.00
14	19	29		RndBar 5_8	A36	0.00	0.00	0.00
15	31	30		RndBar 5_8	A36	0.00	0.00	0.00
18	34	33		RndBar 5_8	A36	0.00	0.00	0.00
19	34	51		RndBar 5_8	A36	0.00	0.00	0.00
20	51	31		RndBar 5_8	A36	0.00	0.00	0.00
21	63	35		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
31	59	61		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
32	60	62		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
33	9	27		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
34	10	52		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
35	31	32		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
36	12	51		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
37	27	1		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
38	52	7		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
39	32	1		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
40	51	7		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
41	5	16		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
42	14	18		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	53	54		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

**Orientation of local axes**

---

Member	Rotation [Deg]	Axis23	NX	NY	NZ
31	45.00	0	0.00	0.00	0.00
32	45.00	0	0.00	0.00	0.00
41	45.00	0	0.00	0.00	0.00
43	45.00	0	0.00	0.00	0.00
44	45.00	0	0.00	0.00	0.00

---

**Rigid end offsets**

---

Member	DJX [in]	DJY [in]	DJZ [in]	DKX [in]	DKY [in]	DKZ [in]
21	0.00	2.00	0.00	0.00	2.00	0.00

---

**Hinges**

---

Member	Node-J				Node-K				TOR	AXL	Axial rigidity
	M33	M22	V3	V2	M33	M22	V3	V2			
11	0	0	0	0	0	0	0	0	0	0	Tension only
12	0	0	0	0	0	0	0	0	0	0	Tension only
13	0	0	0	0	0	0	0	0	0	0	Tension only
14	0	0	0	0	0	0	0	0	0	0	Tension only
15	0	0	0	0	0	0	0	0	0	0	Tension only
18	0	0	0	0	0	0	0	0	0	0	Tension only
19	0	0	0	0	0	0	0	0	0	0	Tension only
20	0	0	0	0	0	0	0	0	0	0	Tension only

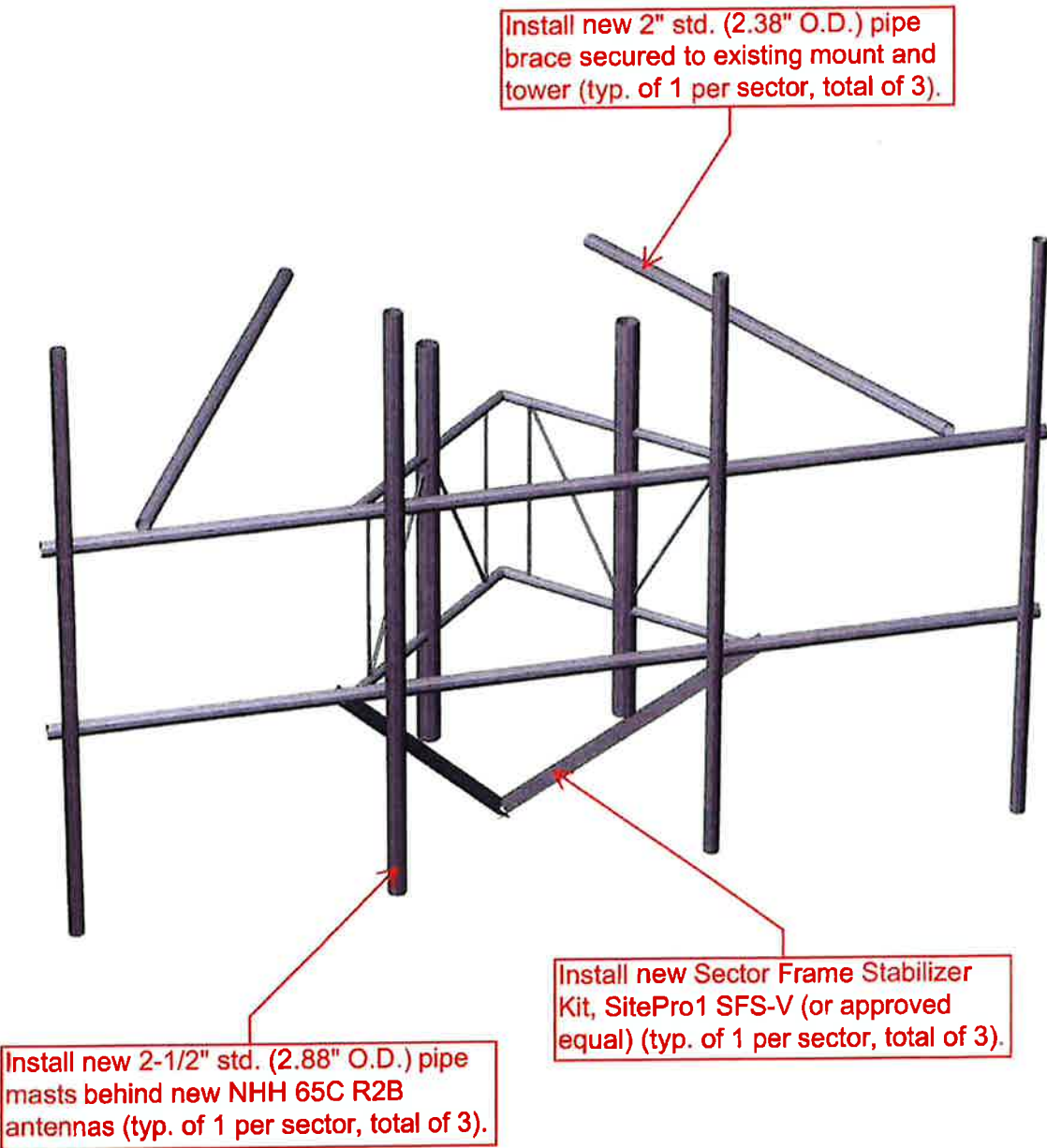
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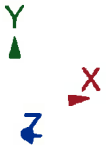
**ANTMO 2019 Mount Calculations  
(Modified Conditions)**

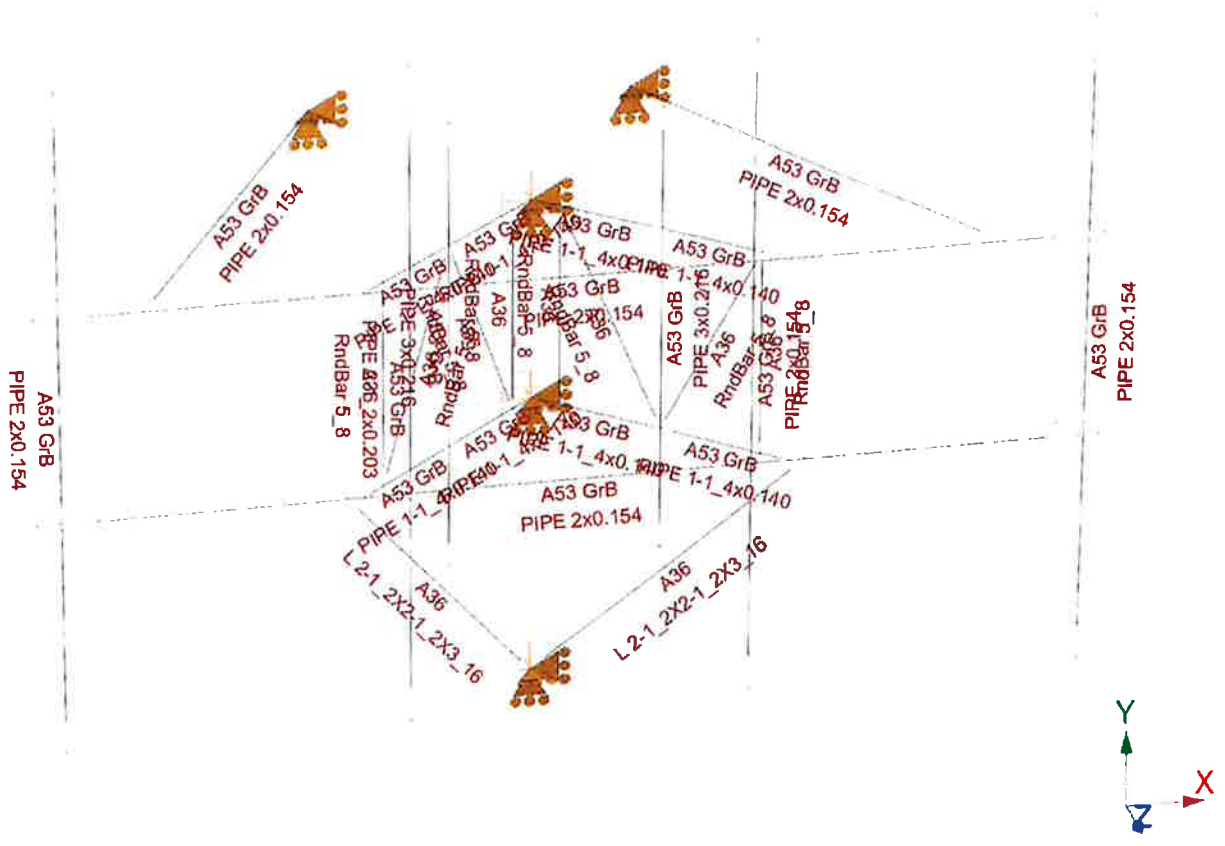


Install new 2" std. (2.38" O.D.) pipe brace secured to existing mount and tower (typ. of 1 per sector, total of 3).

Install new 2-1/2" std. (2.88" O.D.) pipe masts behind new NHH 65C R2B antennas (typ. of 1 per sector, total of 3).

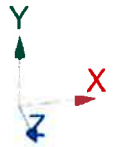
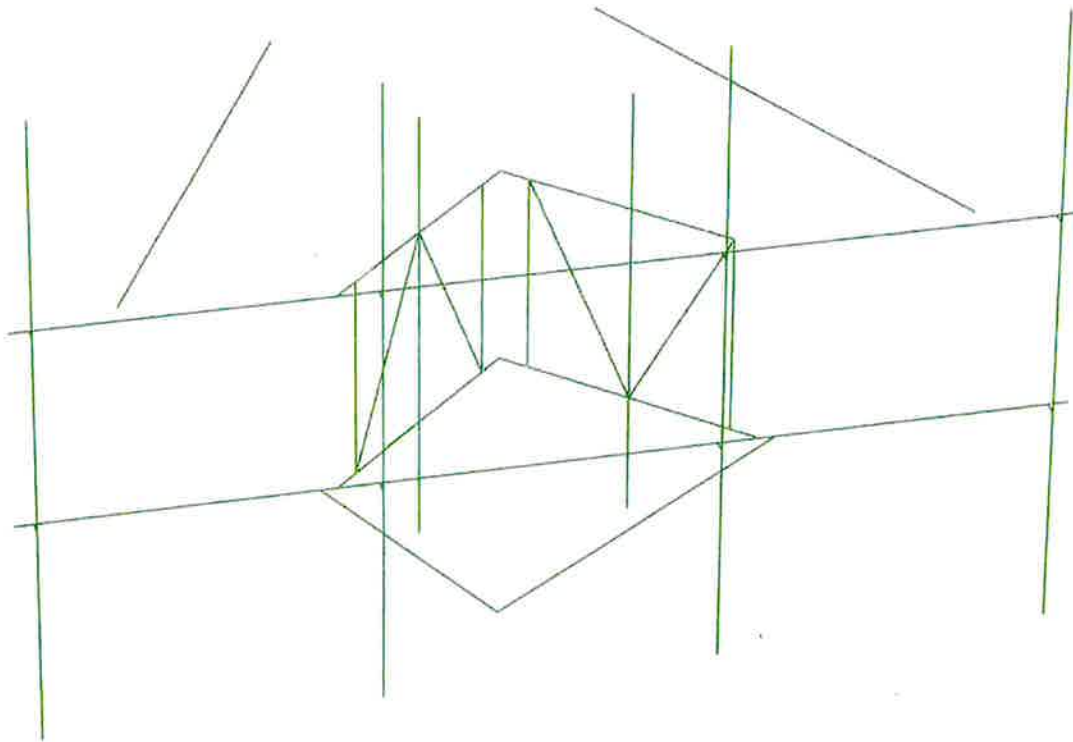
Install new Sector Frame Stabilizer Kit, SitePro1 SFS-V (or approved equal) (typ. of 1 per sector, total of 3).

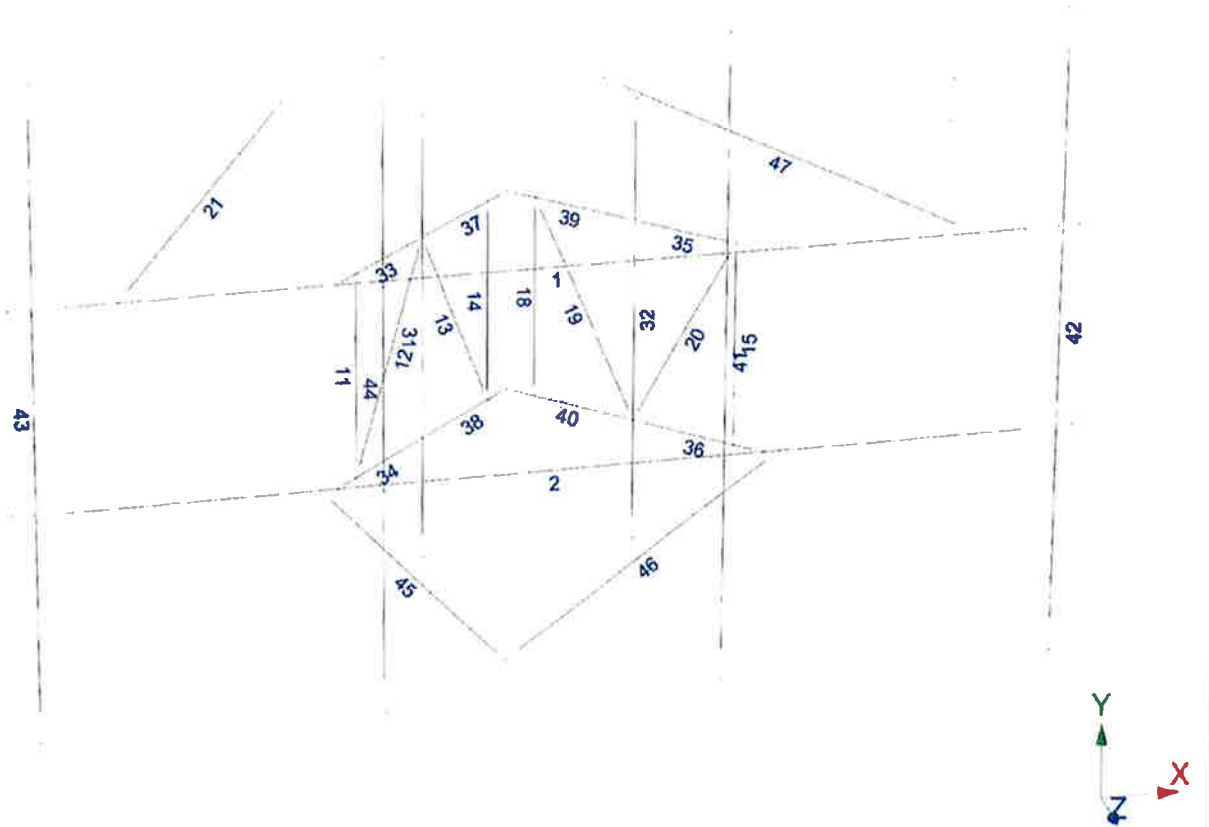




Design status

-  Not designed
-  Error on design
-  Design O.K.
-  With warnings





Current Date: 2/22/2019 5:43 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\VERIZON\CT\Higganum South CT\ANTMO 2019\Higganum South CT (MOD).etz

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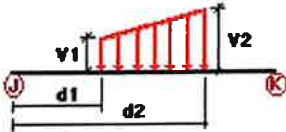
### GLOSSARY

Comb : Indicates if load condition is a load combination

### Load Conditions

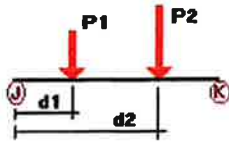
Condition	Description	Comb.	Category
DL	Dead Load	No	DL
Wo	Wind Load (No Ice)	No	WIND
Wi	Wind Load (With Ice)	No	WIND
Di	Ice Load	No	LL

### Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Di	1	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	2	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	11	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	12	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	13	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	14	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	15	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	18	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	19	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	20	Y	-0.005	-0.005	0.00	Yes	100.00	Yes
	21	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	31	Y	-0.011	-0.011	0.00	Yes	100.00	Yes
	32	Y	-0.011	-0.011	0.00	Yes	100.00	Yes
	41	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	42	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	43	Y	-0.009	-0.009	0.00	Yes	100.00	Yes
	44	Y	-0.01	-0.01	0.00	Yes	100.00	Yes
45	Y	-0.011	-0.011	0.00	Yes	100.00	Yes	
46	Y	-0.011	-0.011	0.00	Yes	100.00	Yes	
47	Y	-0.009	-0.009	0.00	Yes	100.00	Yes	

**Concentrated forces on members**



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
DL	31	y	-0.032	0.50	No
		y	-0.085	2.00	No
		y	-0.082	4.00	No
	32	y	-0.085	2.00	No
		y	-0.082	4.00	No
	42	y	-0.022	0.50	No
		y	-0.022	7.50	No
	43	y	-0.021	0.50	No
		y	-0.021	7.50	No
	44	y	-0.052	0.50	No
		y	-0.052	7.50	No
		y	-0.026	4.00	No
Wo	31	z	-0.131	0.50	No
		z	-0.065	2.00	No
		z	-0.065	4.00	No
	32	z	-0.065	2.00	No
		z	-0.065	4.00	No
	42	z	-0.20	0.50	No
		z	-0.20	7.50	No
	43	z	-0.149	0.50	No
		z	-0.149	7.50	No
	44	z	-0.396	0.50	No
		z	-0.396	7.50	No
	Wi	31	z	-0.031	0.50
z			-0.017	2.00	No
z			-0.017	4.00	No
32		z	-0.017	2.00	No
		z	-0.017	4.00	No
42		z	-0.047	0.50	No
		z	-0.047	7.50	No
43		z	-0.035	0.50	No
		z	-0.035	7.50	No
44		z	-0.092	0.50	No
		z	-0.092	7.50	No
Di		31	y	-0.053	2.00
	y		-0.05	4.00	No
	y		-0.105	0.50	No
	32	y	-0.053	2.00	No
		y	-0.05	4.00	No
	42	y	-0.133	0.50	No
		y	-0.133	7.50	No
	43	y	-0.102	0.50	No
		y	-0.102	7.50	No
	44	y	-0.265	0.50	No
		y	-0.265	7.50	No

**Self weight multipliers for load conditions**

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
DL	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (No Ice)	No	0.00	0.00	0.00
Wi	Wind Load (With Ice)	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00

### Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
DL	0.00	0.00	0.00
Wo	0.00	0.00	0.00
Wi	0.00	0.00	0.00
Di	0.00	0.00	0.00





Current Date: 2/22/2019 5:43 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\VERIZON\CT\Higganum South CT\ANTMO 2019\Higganum South CT (MOD).et3

## Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2DL+1.6Wo

LC2=0.9DL+1.6Wo

LC3=1.2DL+Wl+Di

LC4=1.2DL

LC5=0.9DL

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	<i>L 2-1_2X2-1_2X3_16</i>	45	LC1 at 0.00%	0.38	OK	Eq. H2-1
		46	LC3 at 100.00%	0.30	OK	Eq. H2-1
	<i>PIPE 1-1_4x0.140</i>	33	LC2 at 0.00%	0.60	OK	Eq. H1-1b
		34	LC1 at 0.00%	0.46	OK	Eq. H1-1b
		35	LC3 at 100.00%	0.04	OK	Eq. H1-1b
		36	LC2 at 0.00%	0.69	OK	Eq. H1-1b
		37	LC1 at 100.00%	0.86	OK	Eq. H1-1b
		38	LC3 at 100.00%	0.48	OK	Eq. H1-1b
		39	LC3 at 100.00%	0.25	OK	Eq. H1-1b
		40	LC1 at 100.00%	0.33	OK	Eq. H1-1b
	<i>PIPE 2-1_2x0.203</i>	44	LC1 at 33.33%	0.81	OK	Eq. H1-1b
	<i>PIPE 2x0.154</i>	1	LC1 at 90.28%	0.46	OK	Eq. H1-1b
		2	LC1 at 72.22%	0.65	OK	Eq. H1-1b
		21	LC2 at 100.00%	0.14	OK	Eq. H1-1b
		41	LC1 at 64.58%	0.25	OK	Eq. H1-1b
		42	LC1 at 35.42%	0.62	OK	Eq. H1-1b
		43	LC1 at 35.42%	0.70	OK	Eq. H1-1b
		47	LC2 at 0.00%	0.22	OK	Eq. H1-1b
	<i>PIPE 3x0.216</i>	31	LC1 at 27.08%	0.08	OK	Eq. H1-1b
		32	LC2 at 70.83%	0.03	OK	Eq. H1-1b
	<i>RndBar 5_8</i>	11	LC3 at 0.00%	0.10	OK	Eq. H1-1b
		12	LC2 at 0.00%	0.08	OK	Eq. H1-1b
		13	LC1 at 100.00%	0.05	OK	Eq. H1-1b
		14	LC3 at 0.00%	0.12	OK	Eq. H1-1b
		15	LC2 at 100.00%	0.12	OK	Eq. H1-1b
		18	LC3 at 0.00%	0.03	OK	Eq. H1-1b
		19	LC3 at 100.00%	0.08	OK	Eq. H1-1b
		20	LC3 at 100.00%	0.04	OK	Eq. H1-1b



Current Date: 2/22/2019 5:43 PM

Units system: English

File name: W:\STRUCTURAL DEPARTMENT\ANALYSIS SOFTWARE\RAM Elements\RAM Projects\VERIZON\CT\Higganum South CT\ANTMO 2019\Higganum South CT (MOD).etx

## Geometry data

### GLOSSARY

Cb22, Cb33 : Moment gradient coefficients  
 Cm22, Cm33 : Coefficients applied to bending term in interaction formula  
 d0 : Tapered member section depth at J end of member  
 DJX : Rigid end offset distance measured from J node in axis X  
 DJY : Rigid end offset distance measured from J node in axis Y  
 DJZ : Rigid end offset distance measured from J node in axis Z  
 DKX : Rigid end offset distance measured from K node in axis X  
 DKY : Rigid end offset distance measured from K node in axis Y  
 DKZ : Rigid end offset distance measured from K node in axis Z  
 dL : Tapered member section depth at K end of member  
 Ig factor : Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members  
 K22 : Effective length factor about axis 2  
 K33 : Effective length factor about axis 3  
 L22 : Member length for calculation of axial capacity  
 L33 : Member length for calculation of axial capacity  
 LB pos : Lateral unbraced length of the compression flange in the positive side of local axis 2  
 LB neg : Lateral unbraced length of the compression flange in the negative side of local axis 2  
 RX : Rotation about X  
 RY : Rotation about Y  
 RZ : Rotation about Z  
 TO : 1 = Tension only member 0 = Normal member  
 TX : Translation in X  
 TY : Translation in Y  
 TZ : Translation in Z

### Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	0.00	0.00	-2.60	0
2	-6.25	0.00	0.00	0
3	6.25	0.00	0.00	0
5	2.00	2.75	0.20	0
6	-6.25	-2.50	0.00	0
7	0.00	-2.50	-2.60	0
8	6.25	-2.50	0.00	0
9	-2.50	0.00	0.00	0
10	-2.50	-2.50	0.00	0
11	2.50	0.00	0.00	0
12	2.50	-2.50	0.00	0
13	-2.00	2.75	0.20	0
14	6.00	2.75	0.20	0
16	2.00	-5.25	0.20	0
17	-2.00	-5.25	0.20	0
18	6.00	-5.25	0.20	0
19	-0.2778	0.00	-2.3111	0
26	-2.2222	0.00	-0.2889	0
27	-1.25	0.00	-1.30	0
28	-2.2222	-2.50	-0.2889	0
29	-0.2778	-2.50	-2.3111	0

30	2.2222	-2.50	-0.2889	0
32	1.25	0.00	-1.30	0
33	0.2778	-2.50	-2.3111	0
34	0.2778	0.00	-2.3111	0
35	-2.00	0.00	-6.2889	0
51	1.25	-2.50	-1.30	0
52	-1.25	-2.50	-1.30	0
53	-6.00	2.75	0.20	0
54	-6.00	-5.25	0.20	0
59	-1.25	1.50	-1.30	0
60	1.25	1.50	-1.30	0
61	-1.25	-4.00	-1.30	0
62	1.25	-4.00	-1.30	0
63	-5.00	0.00	0.00	0
64	0.00	-6.00	-2.60	0
65	-2.70	-2.50	0.00	0
66	2.70	-2.50	0.00	0
67	5.00	0.00	0.00	0
68	2.00	0.00	-6.2889	0
31	2.2222	0.00	-0.2889	0

### Restraints

Node	TX	TY	TZ	RX	RY	RZ
1	1	1	1	1	1	1
7	1	1	1	1	1	1
35	1	1	1	0	0	0
64	1	1	1	1	1	1
68	1	1	1	0	0	0

### Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	Ig factor
1	2	3		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
2	6	8		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
11	26	28		RndBar 5_8	A36	0.00	0.00	0.00
12	28	27		RndBar 5_8	A36	0.00	0.00	0.00
13	27	29		RndBar 5_8	A36	0.00	0.00	0.00
14	19	29		RndBar 5_8	A36	0.00	0.00	0.00
15	31	30		RndBar 5_8	A36	0.00	0.00	0.00
18	34	33		RndBar 5_8	A36	0.00	0.00	0.00
19	34	51		RndBar 5_8	A36	0.00	0.00	0.00
20	51	31		RndBar 5_8	A36	0.00	0.00	0.00
21	63	35		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
31	59	61		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
32	60	62		PIPE 3x0.216	A53 GrB	0.00	0.00	0.00
33	9	27		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
34	10	52		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
35	31	32		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
36	12	51		PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00

37	27	1	PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
38	52	7	PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
39	32	1	PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
40	51	7	PIPE 1-1_4x0.140	A53 GrB	0.00	0.00	0.00
41	5	16	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
42	14	18	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
43	53	54	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
44	13	17	PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
45	64	65	L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
46	64	66	L 2-1_2X2-1_2X3_16	A36	0.00	0.00	0.00
47	67	68	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

### Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
31	45.00	0	0.00	0.00	0.00
32	45.00	0	0.00	0.00	0.00
41	45.00	0	0.00	0.00	0.00
43	45.00	0	0.00	0.00	0.00
44	45.00	0	0.00	0.00	0.00
45	270.00	0	0.00	0.00	0.00

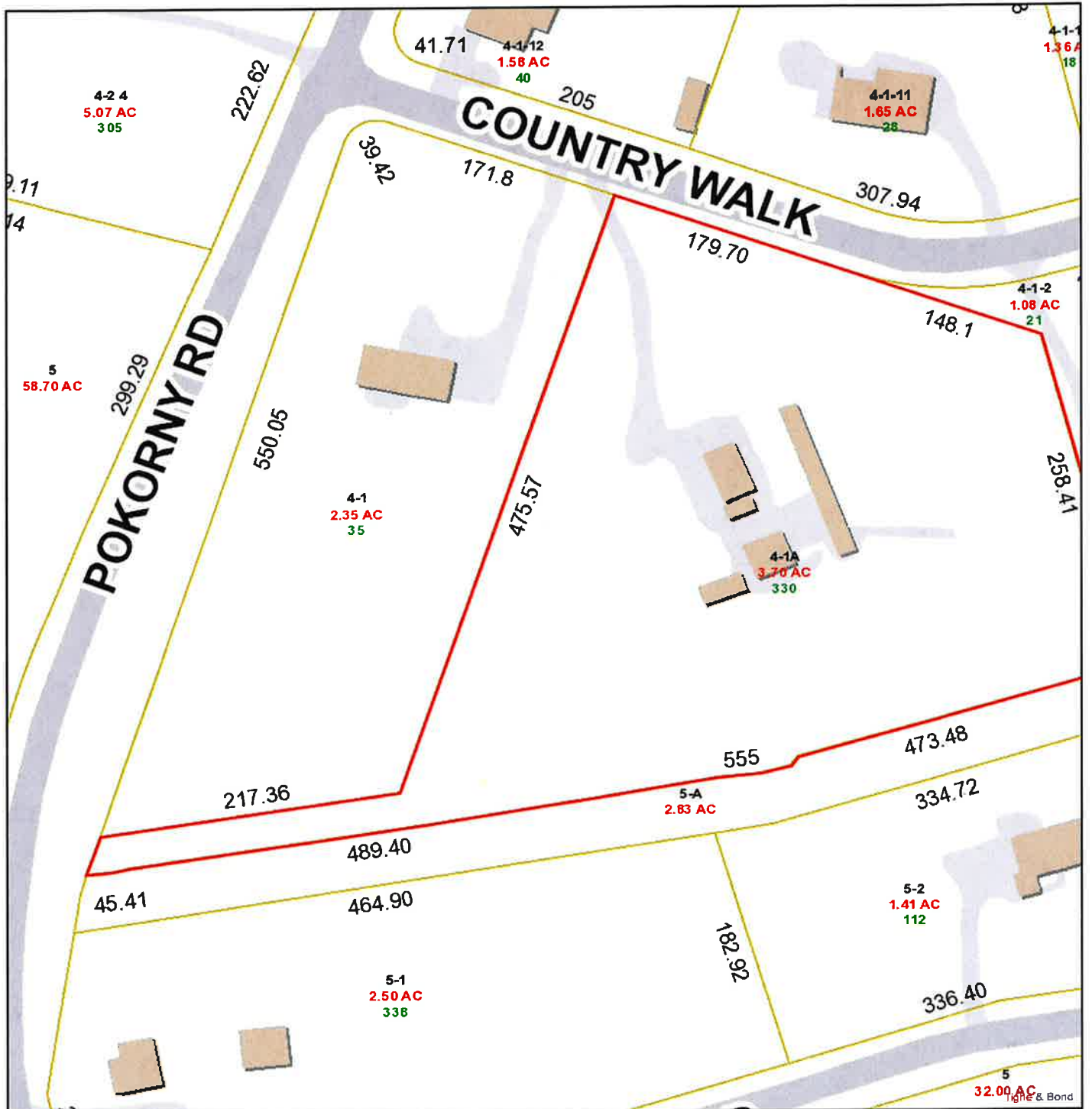
### Rigid end offsets

Member	DJX [in]	DJY [in]	DJZ [in]	DKX [in]	DKY [in]	DKZ [in]
21	0.00	2.00	0.00	0.00	2.00	0.00
47	0.00	2.00	0.00	0.00	2.00	0.00

### Hinges

Member	Node-J				Node-K				TOR	AXL	Axial rigidity
	M33	M22	V3	V2	M33	M22	V3	V2			
11	0	0	0	0	0	0	0	0	0	0	Tension only
12	0	0	0	0	0	0	0	0	0	0	Tension only
13	0	0	0	0	0	0	0	0	0	0	Tension only
14	0	0	0	0	0	0	0	0	0	0	Tension only
15	0	0	0	0	0	0	0	0	0	0	Tension only
18	0	0	0	0	0	0	0	0	0	0	Tension only
19	0	0	0	0	0	0	0	0	0	0	Tension only
20	0	0	0	0	0	0	0	0	0	0	Tension only

# **ATTACHMENT 6**



**330 POKORNY RD**

10/3/2019 10:04:07

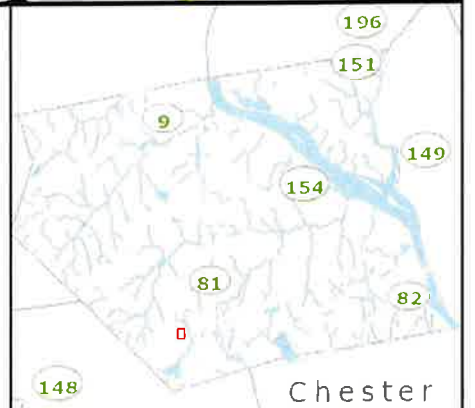
1"=100'

**Property Information**

<b>Parcel_ID</b>	55 004 1A
<b>Street Address</b>	330 POKORNY RD
<b>Sale Price</b>	null



The information depicted on this map is for planning purposes only. It is not adequate for legal boundary definition, regulatory interpretation, or parcel-level analyses.



Chester

CURRENT OWNER		TOPO.	UTILITIES	STRT./ROAD	LOCATION	CURRENT ASSESSMENT	
Code	Description	Code	Appraised Value	Assessed Value	Code	Appraised Value	Assessed Value
10	CONN LIGHT + POWER CO	6	1	2 Suburban	4-1	227,950	159,570
03	TAX DEPT	7			4-3	5,740	4,020
	PO BOX 270						
HARTFORD, CT 06141 Additional Owners:							
Other ID: Dev Lot 3.7 Census Tract R-2A 490 Penalty Section 2 Town Line? Callback Ltr ASSOC PID#							

RECORD OF OWNERSHIP		BK-VOL/PAGE	SALE DATE	U/V	SALE PRICE	V.C.	PREVIOUS ASSESSMENTS (HISTORY)	
Yr.	Code	Assessed Value	Yr.	Code	Assessed Value	Yr.	Code	Assessed Value
2017	4-1	159,570	2016	4-1	89,570	2015	4-1	89,570
2017	4-3	4,020	2016	4-3	4,020	2015	4-3	4,020
<b>Total:</b>		<b>163,590</b>	<b>Total:</b>		<b>93,590</b>	<b>Total:</b>		<b>93,590</b>

**EXEMPTIONS**

Description	Code	Amount	Number	Comm. Int.
<b>Total:</b>				

OTHER ASSESSMENTS		Amount	Comm. Int.
<b>Total:</b>			

ASSESSING NEIGHBORHOOD		Street Index Name	Batch
0001/A			
<b>NOTES</b>			
CELL TOWER LOT AND T-MOBILE AS TENANTS			
VACANT W/OB -R2010 GATED			
2014 I&E: NA			
2017-BP TO ADD VERIZON ANTENNA; ADDED LAND LINE TO BE IN LINE W/ OTHER C-TOWERS			
SITTING-COUNCIL INDICATES SPRINT, VERIZON			

BUILDING PERMIT RECORD		Amount	Insp. Date	% Comp.	Date Comp.	Comments
13480	BP Permit	85,000		100	09/25/2017	ADD VZW ANTENNA, 08/17/2015
<b>Net Total Appraised Parcel Value</b>						
<b>233,690</b>						

LAND LINE VALUATION SECTION															
B Use Code	Use Description	Zone	D	Front	Depth	Units	Unit Price	I Factor	S.A. Factor	C ST. Factor	Idx Adj.	Notes-Adj	S Adj Fact	Unit Price	Land Value
1	350 Cell Tower	R-2A				2.00 AC	113,750.00	0.5385	C	1.00	CEL1	1.00	1.00	1,000	122,510
1	350 Cell Tower					1.70 AC	3,200.00	1.0000	0	1.00	0.00		1.00	5,440	
1	350 Cell Tower					1.00 BL	100,000.00	1.0000	0	1.00	CEL1	1.00	1.00	1,000	100,000
<b>Total Card Land Units: 3.70 AC Parcel Total Land Area: 3.7 AC</b>															
<b>Total Land Value: 227,950</b>															

**APPROXIMATE VALUE SUMMARY**

Appraised Bldg. Value (Card) 0

Appraised XF (B) Value (Bldg) 0

Appraised OB (L) Value (Bldg) 5,740

Appraised Land Value (Bldg) 227,950

Special Land Value 0

Total Appraised Parcel Value 233,690

Valuation Method: C

Adjustment: 0

**APPROXIMATE VALUE SUMMARY**

Appraised Bldg. Value (Card) 0

Appraised XF (B) Value (Bldg) 0

Appraised OB (L) Value (Bldg) 5,740

Appraised Land Value (Bldg) 227,950

Special Land Value 0

Total Appraised Parcel Value 233,690

Valuation Method: C

Adjustment: 0

**APPROXIMATE VALUE SUMMARY**

Appraised Bldg. Value (Card) 0

Appraised XF (B) Value (Bldg) 0

Appraised OB (L) Value (Bldg) 5,740

Appraised Land Value (Bldg) 227,950

Special Land Value 0

Total Appraised Parcel Value 233,690

Valuation Method: C

Adjustment: 0





# **ATTACHMENT 7**



**Certificate of Mailing — Firm**

Name and Address of Sender	TOTAL NO. of Pieces Listed by Sender	TOTAL NO. of Pieces Received at Post Office™	Affix Stamp Here Postmark with Date of Receipt.			
<b>Kenneth C. Baldwin, Esq.</b> <b>Robinson &amp; Cole LLP</b> <b>280 Trumbull Street</b> <b>Hartford, CT 06103</b>	3	3				
Postmaster, per (name of receiving employee)						
USPS® Tracking Number Firm-specific Identifier	Address (Name, Street, City, State, and ZIP Code)™ USPS	Postage	Fee	Special Handling	Parcel Airlift	
1.	Robert McGarry, First Selectman Town of Haddam 30 Field Park Drive Haddam, CT 06348					
2.	Bill Warner, Zoning Enforcement Officer Town of Haddam 30 Field Park Drive Haddam, CT 06348					
3.	The Connecticut Light & Power Company (Eversource) 107 Seidon Street Berlin, CT 06037					
4.						
5.						
6.						