46 Mill Plain Rd. Floor 2 Danbury, CT, 06811 P.: 203.797.1112



May 7, 2014

### **VIA OVERNIGHT DELIVERY**

Ms. Melanie A. Bachman Acting Executive Director Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Sprint Spectrum, L.P. – Notice of Exempt Modification 10 Tanner Marsh Road, Guilford, CT

Dear Ms. Bachman:

This letter and attachments are submitted on behalf of Sprint Spectrum, L.P. ("Sprint"). Sprint is undertaking modifications to certain existing sites in its Connecticut network in order to implement updated technology. In order to do so, Sprint will modify antenna and equipment configurations at a number of existing sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the First Selectman of the Town of Guilford.

Sprint plans to modify the existing facility at 10 Tanner Marsh Road, owned by CTI Towers (coordinates 41°17′19.59"N, -72°39′29.87"W). Attached are drawings depicting the planned changes, and documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration. Also included is a power density calculation reflecting the modification to Sprint's operations at the site.

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will be unaffected. Sprint proposes to add three (3) antennas and three (3) remote radio heads, all at a centerline height of approximately 140' above the tower base. Additionally, Sprint will install one (1) new hybrid cable inside the monopole.

Boston Albany Buffalo Danbury Philadelphia Raleigh Atlanta

- 2. The proposed changes will not extend the site boundaries. Sprint will install additional batteries and new rectifiers in existing cabinets. Thus, there will be no effect on the site compound.
- 3. The proposed changes will not increase the noise level at the existing facility by six decibels or more. The incremental effect of the proposed changes will be negligible.
- 4. The changes to the facility will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site. As indicated in the attached power density calculations, Sprint's operations at the site will result in a power density of 20.724%; the combined site operations will result in a total power density of 40.348%.

Please feel free to call me with any questions or concerns regarding this matter. Thank you for your consideration.

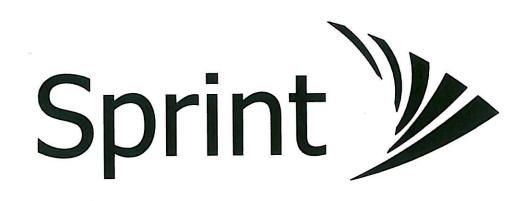
Respectfully submitted, Sprint Spectrum, L.P.

By: \_\_\_\_\_ Eric Dahl, Consultant edahl@comcast.net

860-227-1975

Attachments

cc: Mr. Joseph Mazza, First Selectman, Town of Guilford



PROJECT:

2.5 EQUIPMENT DEPLOYMENT

SITE NAME:

SOUTH GUILFORD

SITE CASCADE:

CT03XC022

SITE ADDRESS:

10 TANNER MARSH ROAD

SOUTH GUILDFORD, CT 06437

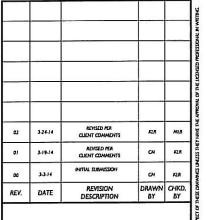
SITE TYPE:

MONOPOLE

**MARKET:** 

SOUTHERN CONNECTICUT

SITE INFORMATION	AREA MAP	PROJECT DISCRIPTION		SHEET INDEX		
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7.52.5	SITE LOCATION	5.8	A-2 A-3	ANTENNA PLAN AND MOUNTING DETAILS	00	-
	st Rid (1) (1) Boston Post Rid (1) Bost	INSTALL (3) PANEL ANTENNAS	A-4	RF DATA SHEET AND EQUIPMENT INFORMATION	00	11
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860-940-9168	Stare Materia					11
GARY.WOOD@SPRINT.COM		)   (				]
					8	14.21





6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



A SAXON DESIGN GROUP

ENGINEER'S LICENSE

### MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26

2.5 GHz

SOUTH GUILFORD IO TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

CT03XC022

COVER SHEET

CHAEL L. BOHUNGER

PROJECT Na: ASDGSP26

T-I

THESE OUTLINE SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT STANDARD CONSTRUCTION SPECIFICATIONS, INCLUDING CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### SECTION 01 100 - SCOPE OF WORK

PART 1 - GENERAL

- THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT CONSTRUCTION STANDARDS FOR WIRELESS SITES, CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- 1.3 PRECEDENCE: SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES INCLUDING THE STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF
- 1.4 NATIONALLY RECOGNIZED CODES AND STANDARDS:
- A. THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO
- 1. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.

  GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY -GENERIC CRITERIA FOR NETWORK TELECOMMUNICATIONS EQUIPMENT.
- NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70 (NATIONAL ELECTRICAL CODE - "NEC") AND NFPA 101 (LIFE SAFETY CODE).
- AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
- INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
- AMERICAN CONCRETE INSTITUTE (ACI)
- AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
- CONCRETE REINFORCING STEEL INSTITUTE (CRSI)
- AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
- 10. PORTLAND CEMENT ASSOCIATION (PCA)
- 11. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
- 12. BRICK INDUSTRY ASSOCIATION (BIA)
- 13. AMERICAN WELDING SOCIETY (AWS)
- 14. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
- 15. SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
- 16. DOOR AND HARDWARE INSTITUTE (DHI)
- 17. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
  18. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING
- CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE. **DEFINITIONS:**
- A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT DOCUMENTS.
- COMPANY: SPRINT CORPORATION
- ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND "A&E". THE DESIGN
- PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT. CONTRACTOR: CONSTRUCTION CONTRACTOR; CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK.
- THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC
- TASKS RELATED TO BUT NOT INCLUDED IN THE WORK.

  OFCI: OWNER FURNISHED, CONTRACTOR INSTALLED EQUIPMENT.

  CONSTRUCTION MANAGER ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT...
- 1.6 SITE FAMILIARITY: CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOWLEDGE OR FIELD CONDITIONS.
- 1.7 POINT OF CONTACT: COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.
- 1.8 ON-SITE SUPERVISION: THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK.
- 1.9 <u>DRAWINGS. SPECIFICATIONS AND DETAILS REQUIRED AT JOBSITE:</u> THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS, STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.
  - THE JOBSITE DRAWINGS, SPECIFICATIONS AND DETAILS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS, AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A&E VENDOR FOR PRODUCTION OF "AS-BUILT" DRAWINGS.
  - DETAILS ARE INTENDED TO SHOW DESIGN INTENT. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK. CONTRACTOR SHALL NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY VARIATIONS PRIOR TO PROCEEDING WITH THE WORK.
  - C . DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO PROCEEDING WITH THE WORK.
- 1.10 <u>USE OF JOB SITE:</u> THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.

- 1.11 <u>UTILITIES SERVICES:</u> WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT AND CAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY COMPANY INVOLVED:
- 1.12 PERMITS / FEES: WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC UTILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND 1.13 CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.
  - METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION: CONTRACTOR SHALL PERFORM WORK AS DESCRIBED IN THE FOLLOWING INSTALLATION AND COMMISSIONING MOPS.
    - TOP HAT HOW TO INSTALL A NEW CABINET

    - BASE BAND UNIT IN EXISTING UNIT INSTALLATION OF HYBRID CABLE
    - INSTALLATION OF RRH'S
    - CABLING
      TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS
      SPRINT CELL SITE ENGINEERING NOTICE EN 2012-001, REV 1.

    - COMMISSIONING MOPS
      SPRINT CELL SITE ENGINEERING NOTICE EN-2013-002

    - SPRINT ENGINEERING LETTER EL-0504 SPRINT ENGINEERING LETTER EL-0568
    - SPRINT TECHNICAL SPECIFICATION TS-0193
  - 1.15 USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:
  - CONTRACTOR WILL UTILIZE ITS BEST EFFORTS TO WORK WITH SPRINT ELECTRONIC PROJECT MANAGEMENT SYSTEMS. CONTRACTOR UNDERSTANDS THAT SUFFICIENT INTERNET ACCESS, EQUIVALENT TO "BROADBAND" OR BETTER, IS REQUIRED TO TIMELY AND EFFECTIVELY UTILIZE SPRINT DATA AND DOCUMENT MANAGEMENT SYSTEMS AND AGREES TO MAINTAIN APPROPRIATE CONNECTIONS FOR CONTRACTOR'S STAFF AND OFFICES THAT ARE COMPATIBLE WITH SPRINT DATA AND DOCUMENT MANAGEMENT SYSTEMS

PART 2 - PRODUCTS (NOT USED)

PART 3 - EXECUTION

- 3.1 TEMPORARY UTILITIES AND FACILITIES: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS. TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE, USE OF THE LESSORS OR SITE OWNER'S UTILITIES OR FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.
- 3.2 ACCESS TO WORK: THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.
- 3.3 TESTING: REQUIREMENTS FOR TESTING BY THIS CONTRACTOR SHALL BE AS INDICATED HEREWITH. ON THE CONSTRUCTION DRAWINGS, AND IN THE INDIVIDUAL SECTIONS OF THESE SPECIFICATIONS. SHOULD COMPANY CHOOSE TO ENGAGE ANY THIRD—PARTY TO CONDUCT THE ANALYSIS OF THE SPECIFICATIONS. ADDITIONAL TESTING, THE CONTRACTOR SHALL COOPERATE WITH AND PROVIDE A WORK AREA FOR COMPANY'S TEST AGENCY.
- 3.4 DIMENSIONS: VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS
- 3.5 EXISTING CONDITIONS: NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERING FROM THOSE INDICATED ON THE DRAWINGS. DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

### SECTION 01 200 - COMPANY FURNISHED MATERIAL AND EQUIPMENT

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- SPRINT 'STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES' ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- PART 2 PRODUCTS (NOT USED)

PART 3 - EXECUTION

#### 3.1 RECEIPT OF MATERIAL AND EQUIPMENT:

- A. COMPANY FURNISHED MATERIAL AND EQUIPMENT IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.
- B. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON

  - ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.

    ACCEPT COMPLETENESS AND CONDITION OF ALL DELIVERIES.

    TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT.
  - AGREEMENT.
    RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY-FOUR HOURS AFTER RECEIPT,
    REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
    PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING.

  - COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SITE.

#### **DELIVERABLES:**

- A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.
- B. IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY.
- C. UPLOAD DOCUMENTATION INTO SPRINT SITE MANAGEMENT SYSTEM (SMS) AND/OR PROVIDE HARD COPY DOCUMENTATION AS REQUESTED.

#### SECTION 01 300 - CELL SITE CONSTRUCTION

PART 1 - GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

- A. NO WORK SHALL COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE
- B. UPON RECEMING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.
- PART 2 PRODUCTS (NOT USED)
- PART 3 EXECUTION

- A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. THE ACTIVITIES DESCRIBED ARE NOT EXHAUSTIVE, AND CONTRACTOR SHALL TAKE ANY AND ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH
- SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED.
- C. MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
- PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
- PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
  PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND
  COMPOUND SURFACE TREATMENTS.
- MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELCO BACKHAUL.
- INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
- INSTALL ABOVE GROUND GROUNDING SYSTEMS.
- PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
  INSTALL "H-FRAMES", CABINETS AND SHELTERS AS INDICATED.
- INSTALL ROADS, ACCESS WAYS, CURBS AND DRAWS AS INDICATED.
  ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.
- PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
- 11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.

  12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS.

  13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
- 14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
  15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
- 16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS
- REQUIRED.

  7. INSTALL CELL SITE RADIOS, MICROWAYE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.

  18. PERFORM, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
- ANTENNAL AND COAX SWEEP TESTING AND MAKE ANY AND ALL NECESSARY
- CORRECTIONS. CURRECTIONS.

  20. REMAIN ON SITE MOBILIZED THROUGHOUT HAND-OFF AND INTEGRATION TO ASSIST AS NEEDED UNTIL SITE IS DEEMED SUBSTANTIALLY COMPLETE AND PLACED "ON AIR."

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED 'BROOM CLEAN' AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS
  - IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN
- THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY
- RETURN THEM TO ORIGINAL CONDITION E. CONDUCT TESTING AS REQUIRED HEREIN.

#### 3.3 DELIVERABLES:

- A. CONTRACTOR SHALL REVIEW, APPROVE, AND SUBMIT TO SPRINT SHOP DRAWINGS, PRODUCT DATA, SAMPLES, AND SIMILAR SUBMITTALS AS REQUIRED HEREINAFTER
- PROVIDE DOCUMENTATION INCLUDING. BUT NOT LIMITED TO, THE FOLLOWING, DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
  - ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
  - PROJECT PROGRESS REPORTS.
- CMIL CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
  ELECTRICAL SERVICE COMPLETION DATE (POPULATE FIELD IN SMS AND/OR FORWARD
- LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- POWER INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION). TELCO READY DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- PPC (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
  TOWER CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD
- 10. TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
- 11. BTS AND RADIO EQUIPMENT DELIVERED AT SITE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION). 12. NETWORK OPERATIONS HANDOFF CHECKLIST (HOC WALK) COMPLETE (UPLOAD FORM IN SMS)
- 13. CIVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION) 14. SITE CONSTRUCTION PROGRESS PHOTOS UNLOADED INTO SMS. CONTINUE SHEET SP-2

REYTLED FER MLB 02 3.24.14 3-19-10 3-3-14 CM KLA REVISION DRAWN CHKD. REV. DATE DESCRIPTION BY BY

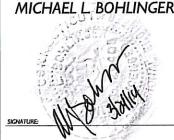


6580 SPRINT PARKWAY





**ENGINEER'S LICENSE** 



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26

CT03XC022

2.5 GHz

DESIGN TYPE

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

SPRINT SPECIFICATIONS (SHEET | OF 3)

3-3-14 PROJECT Na: ASDGSP26 DRAWING BY: CHK BY: SP-I

#### CONTINUED FROM SP-1:

#### SECTION 01 400 - SUBMITTALS, TESTS, AND INSPECTIONS

#### PART 1 - GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.

- A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND
- B. SUBMIT THE FOLLOWING TO COMPANY REPRESENTATIVE FOR APPROVAL
- CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
  SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
- ALL EQUIPMENT AND MATERIALS SO IDENTIFIED ON THE CONSTRUCTION DRAWINGS.
- C. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING NO VERBAL APPROVALS WILL BE CONSIDERED SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

#### 1.4 TESTS AND INSPECTIONS:

- A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
- 1. COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS.
- 2. AGL, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE
- ANTENNA ALIGNMENT TOOL.

  3. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF
- C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING;
- 1. AZIMUTH, DOWNTILT, AGL UPLOAD REPORT FROM ANTENNA ALIGNMENT TOOL TO SITERRA TASK 465. INSTALLED AZIMUTH, DOWNTILT, AND AGL MUST CONFORM TO THE RF DATA SHEETS. SWEEP AND FIBER TESTS
- 2. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
- 3. ALL AVAILABLE JURISDICTIONAL INFORMATION
- 4. PDF SCAN OF REDLINES PRODUCED IN FIELD
- 5. ELECTRONIC AS-BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS. ANY FIELD CHANGE MUST BE REFLECTED BY MODIFYING THE PLANS, ELEVATIONS, AND DETAILS IN THE DRAWING SETS. GENERAL NOTES INDICATING MODIFICATIONS WILL NOT BE ACCEPTED. CHANGES SHALL BE HIGHLIGHTED AS "CLOUDS" IDENTIFIED AS THE "AS-BUILT" CONDITION.
- 7. FINAL PAYMENT APPLICATION
- 8. REQUIRED FINAL CONSTRUCTION PHOTOS
- 9. CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS
- 10. ALL POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLETED IN SITERRA (SPRINTS
- 1.5 COMMISSIONING: PERFORM ALL COMMISSIONING AS REQUIRED BY APPLICABLE MOPS
- 1.5 INTEGRATION: PERFORM ALL INTEGRATION ACTIVITIES AS REQUIRED BY APPLICABLE MOPS
- PART 2 PRODUCTS (NOT USED)

#### PART 3 - EXECUTION

- A. THIRD PARTY TESTING AGENCY: WHEN THE USE OF A THIRD PARTY INDEPENDENT TESTING AGENCY IS REQUIRED, THE AGENCY THAT IS SELECTED MUST PERFORM SUCH WORK ON A REGULAR BASIS IN THE STATE WHERE THE PROJECT IS LOCATED AND HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
  - 1. THE THIRD PARTY TESTING AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
  - 2. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM,
  - ASJTO, AND OTHER METHODS IS NEEDED.

    3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.

#### 3.2 REQUIRED TESTS:

- A. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE 1.1 THE FOLLOWING:
- 1. CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR FOUNDATIONS AS SPECIFIED
- IN SECTION: PORTLAND CEMENT CONCRETE PAVING.

  2. ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED IN SECTION: HOT MIX ASPHALT PAVING.

  3. FIELD QUALITY CONTROL TESTING AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE
- 4. TESTING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS, PADS AND ANCHOR LOCATIONS
- 5. STRUCTURAL BACKFILL COMPACTION TESTS FOR THE TOWER FOUNDATION.
- 6. SITE RESISTANCE TO EARTH TESTING PER EXHIBIT: CELL SITE GROUNDING SYSTEM DESIGN.
  7. ANTENNA AND COAX SWEEP TESTS PER EXHIBIT: ANTENNA TRANSMISSION LINE ACCEPTANCE 3.1 WEEKLY REPORTS:
- STANDARDS.
- B. GROUNDING AT ANTENNA MASTS FOR GPS AND ANTENNAS

  9. ALL OTHER TESTS REQUIRED BY COMPANY OR JURISDICTION.

#### 3.3 REQUIRED INSPECTIONS:

- A. SCHEDULE INSPECTIONS WITH COMPANY REPRESENTATIVE.
- B. CONDUCT INSPECTIONS INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
- GROUNDING SYSTEM INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY AAE OR SPRINT REPRESENTATIVE.
  FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY AAE OR SPRINT REPRESENTATIVE.
  COMPACTION OF BACKFILL MATERIALS; AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS; ASPHALT PAYING; AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
  - PRE- AND POST-CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING
- TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL 3.4 ADDITIONAL REPORTING: FACILITIES.
- PHOTOGRAPHS BY THIRD PARTY AGENCY.
  ANTENNA AZIMUTH , DOWN TILT AND PER SUNLIGHT TOOL SUNSIGHT INSTRUMENTS
- ANTENNALIGN ALIGNMENT TOOL (AAT)
  VERIFICATION DOCUMENTED WITH THE ANTENNA CHECKLIST REPORT, BY A&E, SITE
- DEVELOPMENT REP. OR RF REP. B. FINAL INSPECTION CHECKLIST AND HANDOFF WALK (HOC.). SIGNED FORM SHOWING ACCEPTANCE BY FIELD OPS IS TO BE UPLOADED INTO SMS.
- 9. COAX SWEEP AND FIBER TESTING DOCUMENTS SUBMITTED VIA SMS FOR RF APPROVAL
  10. SCAN-ABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE S INACCESSIBLE SERIALIZED
- 11. ALL AVAILABLE JURISDICTIONAL INFORMATION
  12. PDF SCAN OF REDLINES PRODUCED IN FIELD
- E. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF
- CONSTRUCTION INSPECTIONS AND CORRECTIVE MEASURES SHALL BE DOCUMENTED BY THE CONTRACTOR WITH WRITTEN REPORTS AND PHOTOGRAPHS. PHOTOGRAPHS MUST BE DIGITAL AND OF SUFFICIENT QUALITY TO CLEARLY SHOW THE SITE CONSTRUCTION. PHOTOGRAPHS MUST CLEARLY IDENTIFY THE PHOTOGRAPHED ITEM AND BE LABELED WITH THE SITE CASCADE NUMBER, SITE NAME, DESCRIPTION, AND DATE.
- 3.4 DELIVERABLES: TEST AND INSPECTION REPORTS AND CLOSEOUT DOCUMENTATION SHALL BE UPLOADED TO THE SMS AND/OR FORWARDED TO SPRINT FOR INCLUSION INTO THE
  - THE FOLLOWING TEST AND INSPECTION REPORTS SHALL BE PROVIDED AS APPLICABLE.
  - CONCRETE MIX AND CYLINDER BREAK REPORTS.

  - STRUCTURAL BACKFILL COMPACTION REPORTS.
    SITE RESISTANCE TO EARTH TEST.
    ANTENNA AZIMUTH AND DOWN TILT VERIFICATION
  - TOWER ERECTION INSPECTIONS AND MEASUREMENTS DOCUMENTING TOWER INSTALLED PER SUPPLIER'S REQUIREMENTS AND THE APPLICABLE SECTIONS HEREIN.
  - 6. COAX CABLE SWEEP TESTS PER COMPANY'S "ANTENNA LINE ACCEPTANCE STANDARDS".

#### B. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES THE FOLLOWING;

- TEST WELLS AND TRENCHES: PHOTOGRAPHS OF ALL TEST WELLS; PHOTOGRAPHS SHOWING ALL
  OPEN EXCAVATIONS AND TRENCHING PRIOR TO BACKFILLING SHOWING A TAPE MEASURE
- VISIBLE IN THE EXCAVATIONS INDICATING DEPTH.

  2. CONDUITS, CONDUCTORS AND GROUNDING: PHOTOGRAPHS SHOWING TYPICAL INSTALLATION OF CONDUCTORS AND CONNECTORS; PHOTOGRAPHS SHOWING TYPICAL BEND RADIUS OF INSTALLED GROUND WIRES AND GROUND ROD SPACING;
- CONCRETE FORMS AND REINFORCING: CONCRETE FORMING AT TOWER AND EQUIPMENT/SHELTER PAD/FOUNDATIONS - PHOTOGRAPHS SHOWING ALL REINFORCING STEEL, UTILITY AND CONDUIT STUB OUTS; PHOTOGRAPHS SHOWING CONCRETE POUR OF SHELTER SLAB/FOUNDATION, TOWER FOUNDATION AND GUY ANCHORS WITH VIBRATOR IN USE; PHOTOGRAPHS SHOWING EACH ANCHOR ON GUYED TOWERS, BEFORE CONCRETE POUR.
- ANCHOR ON GUYED TOWERS, BEFORE CONCRETE POUR.

  4. TOWER, ANTENNAS AND MAINLINE: INSPECTION AND PHOTOGRAPHS OF SECTION STACKING; INSPECTION AND PHOTOGRAPHS OF PLATFORM COMPONENT ATTACHMENT POINTS; PHOTOGRAPHS OF TOWER TOP GROUNDING; PHOTOS OF TOWER COAX LINE COLOR CODING AT THE TOP AND AT GROUND LEVEL; INSPECTION AND PHOTOGRAPHS OF OPERATIONAL OF TOWER LIGHTING, AND PLACEMENT OF FAA REGISTRATION SIGN; PHOTOGRAPHS SHOWING ADDITIONAL GROUNDING POINTS FOR TOWERS GREATER THAN 200 FEET.; PHOTOS OF ANTENNA GROUND BAR, EQUIPMENT GROUND BAR, AND MASTER GROUND BAR; PHOTOS OF GPS ANTENNA(S); PHOTOS OF GRAND SECTION OF ANTENNAS; DNE PHOTOGRAPH LODKING AT THE SECTIOR AND ONE FROM OF EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA; PHOTOS OF COAX WEATHERPROOFING — TOP AND BOTTOM; PHOTOS OF COAX GROUNDING—TOP AND BOTTOM; PHOTOS OF ANTENNA TOP AND BOTTOM; PHOTOS OF COAX GROUNDING—TOP AND BOTTOM; PHOTOS OF ANTENNA AND MAST GROUNDING; PHOTOS OF COAX CABLE ENTRY INTO SHELTER; PHOTOS OF PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
- ROOF TOPS: PRE-CONSTRUCTION AND POST-CONSTRUCTION VISUAL INSPECTION AND PHOTOGRAPHS OF THE ROOF AND INTERIOR TO DETERMINE AND DOCUMENT CONDITIONS; ROOF TOP CONSTRUCTION INSPECTIONS AS REQUIRED BY THE JURISDICTION; PHOTOGRAPHS OF CABLE TRAY AND/OR ICE BRIDGE; PHOTOGRAPHS OF DOCHOUSE/CABLE EXIT FROM ROOF;
  SITE LAYOUT — PHOTOGRAPHS OF THE OVERALL COMPOUND, INCLUDING EQUIPMENT PLATFORM
- 7. FINISHED UTILITIES: CLOSE-UP PHOTOGRAPHS OF THE PPC BREAKER PANEL; CLOSE-UP PHOTOGRAPH OF THE INSIDE OF THE TELCO PANEL AND NIU; CLOSE-UP PHOTOGRAPH OF THE POWER METER AND DISCONNECT; PHOTOS OF POWER AND TELCO ENTRANCE TO COMPANY
- ENCLOSURE; PHOTOGRAPHS AT METER BOX AND/OR FACILITY DISTRIBUTION PANEL. 8. REQUIRED MATERIALS CERTIFICATIONS: CONCRETE MIX DESIGNS; MILL CERTIFICATION FOR ALL REINFORCING AND STRUCTURAL STEEL; AND ASPHALT PAYING MIX DESIGN.

  9. ANY AND ALL SUBMITTALS BY THE JURISDICTION OR COMPANY.

#### SECTION 01 500 - PROJECT REPORTING

#### PART 1 - GENERAL

THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

#### 1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITH.
- PART 2 PRODUCTS (NOT USED)
- PART 3 EXECUTION

CONTRACTOR SHALL PROVIDE SPRINT WITH WEEKLY REPORTS SHOWING PROJECT STATUS. THIS STATUS REPORT FORMAT WILL BE PROVIDED TO THE CONTRACTOR BY SPRINT. THE REPORT WILL CONTAIN SITE ID NUMBER, THE MILESTONES FOR EACH SITE, INCLUDING THE B. COMPLY WITH ALL ENVIRONMENTAL REGULATIONS FOR VOLATILE ORGANIC COMPOUNDS. BASELINE DATE, ESTIMATED COMPLETION DATE AND ACTUAL COMPLETION DATE.

B. REPORT INFORMATION WILL BE TRANSMITTED TO SPRINT VIA ELECTRONIC MEANS AS REQUIRED. THIS INFORMATION WILL PROVIDE A BASIS FOR PROGRESS MONITORING AND PAYMENT.

#### 3.2 PROJECT CONFERENCE CALLS:

SPRINT MAY HOLD WEEKLY PROJECT CONFERENCE CALLS. CONTRACTOR WILL BE REQUIRED TO COMMUNICATE SITE STATUS, MILESTONE COMPLETIONS AND UPCOMING MILESTONE PROJECTIONS, AND ANSWER ANY OTHER SITE STATUS QUESTIONS AS NECESSARY.

#### 3.3 PROJECT TRACKING IN SMS:

A. CONTRACTOR SHALL PROVIDE SCHEDULE UPDATES AND PROJECTIONS IN THE SMS SYSTEM ON A WEEKLY BASIS.

ADDITIONAL OR ALTERNATE REPORTING REQUIREMENTS MAY BE ADDED TO THE REPORT AS DETERMINED TO BE REASONABLY NECESSARY BY COMPANY.

#### 3.5 PROJECT PHOTOGRAPHS:

- A. FILE DIGITAL PHOTOGRAPHS OF COMPLETED SITE IN JPEG FORMAT IN THE SMS PHOTO LIBRARY FOR THE RESPECTIVE SITE, PHOTOGRAPHS SHALL BE CLEARLY LABELED WITH SITE NUMBER, NAME AND DESCRIPTION, AND SHALL INCLUDE AT A MINIMUM THE FOLLOWING AS
- SHELTER AND TOWER OVERVIEW
- TOWER FOUNDATION(S) FORMS AND STEEL BEFORE POUR (EACH ANCHOR ON GUYED TOWERS).
- TOWER FOUNDATION(S) POUR WITH VIBRATOR IN USE (EACH ANCHOR ON GUYED TOWERS). TOWER STEEL AS BEING INSTALLED INTO HOLE (SHOW ANCHOR STEEL ON GUYED TOWERS).
- CONCRETE TESTING / SAMPLES. PLACING OF ANCHOR BOLTS IN TOWER FOUNDATION.
- BUILDING WATER TANK FROM ROAD FOR TENANT IMPROVEMENTS OR COMMENTS.
- SHELTER FOUNDATION—FORMS AND STEEL BEFORE POURING
   SHELTER FOUNDATION POUR WITH VIBRATOR IN USE.
- COAX CABLE ENTRY INTO SHELTER. 12. PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
- 13. ROOFTOP PRE AND POST CONSTRUCTION PHOTOS TO INCLUDE PENETRATIONS AND INTERIOR
- CEILING.

  14. PHOTOS OF TOWER TOP COAX LINE COLOR CODING AND COLOR CODING AT GROUND LEVEL.

  15. PHOTOS OF ALL APPROPRIATE COMPANY OR REGULATORY SIGNAGE.

  16. PHOTOS OF EQUIPMENT BOLT DOWN INSIDE SHELTER.

  17. POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE AND POWER AND TELCO SUPPLY
- LOCATIONS INCLUDING METER/DISCONNECT
- 18. ELECTRICAL TRENCH(S) WITH ELECTRICAL / CONDUIT BEFORE BACKFILL
- 19. ELECTRICAL TRENCH(S) WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL.
- 20. TELCO TRENCH WITH TELEPHONE / CONDUIT BEFORE BACKFILL.
  21. TELCO TRENCH WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL.
- 22. SHELTER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
- 23. TOWER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
- 24. FENCE GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND REND RADII).
- ALL BTS GROUND CONNECTIONS
- 26. ALL GROUND TEST WELLS.
  27. ANTENNA GROUND BAR AND EQUIPMENT GROUND BAR.
- 28. ADDITIONAL GROUNDING POINTS ON TOWERS ABOVE 200'
- 29. HVAC UNITS INCLUDING CONDENSERS ON SPLIT SYSTEMS.
- 32. DOGHOUSE/CABLE EXIT FROM ROOF.
  33. EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA.
  34. MASTER BUS BAR.

- 35. TELCO BOARD AND NIU.
  36. ELECTRICAL DISTRIBUTION WALL.
  37. CABLE ENTRY WITH SURGE SUPPRESSION.
- 38. ENTRANCE TO EQUIPMENT ROOM.
  39. COAX WEATHERPROOFING—TOP AND BOTTOM OF TOWER.
- 40. COAX GROUNDING -TOP AND BOTTOM OF TOWER.
- ANTENNA AND MAST GROUNDIN
- 42. LANDSCAPING WHERE APPLICABLE. FINAL PROJECT ACCEPTANCE: COMPLETE ALL REQUIRED REPORTING TASKS PER CONTRACT, CONTRACT DOCUMENTS OR THE SPRINT INTEGRATED CONSTRUCTION STANDARDS FOR WIRELESS SITES AND UPLOAD INTO SITERRA.

### SECTION 07 500 - ROOF CUTTING, PATCHING AND REPAIR

THIS SECTION SPECIFIES CUTTING AND PATCHING EXISTING ROOFING SYSTEMS WHERE CONDUIT OR CABLES EXIT THE BUILDING ONTO THE ROOF OR BUILDING-MOUNTED ANTENNAS, AND AS REQUIRED FOR WATERTIGHT PERFORMANCE. ROOFTOP ENTRY OPENINGS IN MEMBRANE ROOFTOPS SHALL BE CONSTRUCTED TO COMPLY WITH LANDLORD, ANY EXISTING WARRANTY, AND LOCAL JURISDICTIONAL STANDARDS.

#### 1.4 SUBMITTALS:

- A. <u>PRE-CONSTRUCTION ROOF PHOTOS:</u> COMPLETE A ROOF INSPECTION PRIOR TO THE INSTALLATION OF SPRINT EQUIPMENT ON ANY ROOFTOP BUILD. AT A MINIMUM INSPECT AND PHOTOGRAPH (MINIMUM 3 EA.) ALL AREAS IMPACTED BY THE ADDITION OF THE SPRINT EQUIPMENT.
- B. PROVIDE SIMILAR PHOTOGRAPHS SHOWING ROOF CONDITIONS AFTER CONSTRUCTION (MINIMUM 3
- C. ROOF INSPECTION PHOTOGRAPHS SHOULD BE UPLOADED WITH CLOSEOUT PHOTOGRAPHS.

### SECTION 09 900 - PAINTING

#### QUALITY ASSURANCE:

- A. COMPLY WITH GOVERNING CODES AND REGULATIONS. PROVIDE PRODUCTS OF ACCEPTABLE MANUFACTURERS WHICH HAVE BEEN IN SATISFACTORY USE IN SIMILAR SERVICE FOR THREE YEARS. USE EXPERIENCED INSTALLERS. DELIVER, HANDLE, AND STORE MATERIALS IN ACCORDANCE

CONTINUE SHEET SP-3

3-24-14 KLR REVISED PER KLA 3-19-14 CH INITIAL SUBMISSIO 3-3-14 REVISION DESCRIPTION DRAWN CHKD. BY BY DATE REV.







TOMS RIVER, NJ 08755 **FNGINEER'S LICENSE** 

244 RIVERS EDGE LANE

MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

CT03XC022

2.5 GHz

ASDG PROIECT No

ASDGSP26

CLIENT ID No

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

DRAWING TITLE

SPRINT SPECIFICATIONS (SHEET 2 OF 3)

MICHAEL L. BOHUNGER CT LICENSE No. 20405

3-3-14 PROJECT Na: ASDGSP26 DRAWING BY: Ф

SP-2

14"±16" SHEETS - SIGN & SEAL ARE

#### CONTINUED FROM SP-2:

#### MATERIALS:

A. MANUFACTURERS: BENJAMIN MOORE, ICI DEVOE COATINGS, PPG, SHERWIN WILLIAMS OR APPROVED EQUAL. PROVIDE PREMIUM GRADE, PROFESSIONAL—QUALITY PRODUCTS FOR COATING

#### PAINT SCHEDULE:

- A. EXTERIOR ANTENNAE AND ANTENNA MOUNTING HARDWARE: ONE COAT OF PRIMER AND TWO FINISH COATS. PAINT FOR ANTENNAE SHALL BE NON-METALLIC BASED AND CONTAIN NO METALLIC PARTICLES. PROVIDE COLORS AND PATTERNS AS REQUIRED TO MASK APPEARANCE OF ANTENNAE ON ADJACENT BUILDING SURFACES AND AS ACCEPTABLE TO THE OWNER. REFER TO ANTENNA MANUFACTURER'S INSTRUCTIONS WHENEVER POSSIBLE.
- B. ROOF TOP CONSTRUCTION: TOUCH UP PREPARE SURFACES TO BE REPAIRED. FOLLOW INDUSTRY STANDARDS AND REQUIREMENTS OF OWNER TO MATCH EXISTING COATING AND

#### PAINTING APPLICATION:

- INSPECT SURFACES, REPORT UNSATISFACTORY CONDITIONS IN WRITING; BEGINNING WORK MEANS ACCEPTANCE OF SUBSTRATE.
- 2. COMPLY WITH MANUFACTURER'S INSTRUCTIONS AND RECOMMENDATIONS FOR PREPARATION.
- PRIMING AND COATING WORK. COORDINATE WITH WORK OF OTHER SECTIONS.

  3. MATCH APPROVED MOCK-UPS FOR COLOR, TEXTURE, AND PATTERN. RE-COAT OR REMOVE AND REPLACE WORK WHICH DOES NOT MATCH OR SHOWS LOSS OF ADHESION. CLEAN UP, TOUCH UP AND PROTECT WORK.

#### TOUCHUP PAINTING:

- GALVANIZING DAMAGE AND ALL BOLTS AND NUTS SHALL BE TOUCHED UP AFTER TOWER ERECTION WITH "GALVANOX," "DRY GALV," OR "ZINC-IT."
- FIELD TOUCHUP PAINT SHALL BE DONE IN ACCORDANCE WITH THE MANUFACTURER'S
- ALL METAL COMPONENTS SHALL BE HANDLED WITH CARE TO PREVENT DAMAGE TO THE COMPONENTS, THEIR PRESERVATIVE TREATMENT, OR THEIR PROTECTIVE COATINGS.

#### SECTION 11 700 - ANTENNA ASSEMBLY, REMOTE RADIO HEADS AND CABLE INSTALLATION

THIS SECTION SPECIFIES INSTALLATION OF ANTENNAS, RRH'S, AND CABLE EQUIPMENT, INSTALLATION, AND TESTING OF COAXIAL FIBER CABLE.

#### ANTENNAS AND RRH'S:

THE NUMBER AND TYPE OF ANTENNAS AND RRH'S TO BE INSTALLED IS DETAILED ON THE

HYBRID CABLE WILL BE DC/FIBER AND FURNISHED FOR INSTALLATION AT EACH SITE. CABLE SHALL BE INSTALLED PER THE CONSTRUCTION DRAWINGS AND THE APPLICABLE MANUFACTURER'S

#### JUMPERS AND CONNECTORS:

FURNISH AND INSTALL 1/2° COAX JUMPER CABLES BETWEEN THE RRH'S AND ANTENNAS. JUMPERS SHALL BE TYPE LDF 4, FLC 12-50, CR 540, OR FXL 540. SUPER-FLEX CABLES ARE NOT ACCEPTABLE. JUMPERS BETWEEN THE RRH'S AND ANTENNAS OR TOWER TOP AMPLIFIERS SHALL CONSIST OF 1/2 INCH FOAM DIELECTRIC, OUTDOOR RATED COAXIAL CABLE. DO NOT USE SUPERFLEX OUTDOORS, JUMPERS SHALL BE FACTORY FABRICATED IN APPROPRIATE LENGTHS WITH A MAXIMUM OF 4 FEET EXCESS PER JUMPER AND HAVE CONNECTORS AT EACH END, MANUFACTURED BY SUPPLIER. IF JUMPERS ARE FIELD FABRICATED, FOLLOW MANUFACTURER'S REQUIREMENTS FOR INSTALLATION OF CONNECTORS

#### REMOTE ELECTRICAL TILT (RET) CABLES:

#### MISCELLANEOUS:

INSTALL SPLITTERS, COMBINERS, FILTERS PER RF DATA SHEET, FURNISHED BY SPRINT.

- ANTENNA INSTALLATION:
  THE CONTRACTOR SHALL ASSEMBLE ALL ANTENNAS ONSITE IN ACCORDANCE WITH INSTRUCTIONS SUPPLIED BY THE MANUFACTURER. ANTENNA HEIGHT, AZIMUTH, AND FEED ORIENTATION INFORMATION SHALL BE A DESIGNATED ON THE CONSTRUCTION DRAWINGS.
- A. THE CONTRACTOR SHALL POSITION THE ANTENNA ON TOWER PIPE MOUNTS SO THAT THE BOTTOM STRUT IS LEVEL. THE PIPE MOUNTS SHALL BE PLUMB TO WITHIN
- B. ANTENNA MOUNTING REQUIREMENTS: PROVIDE ANTENNA MOUNTING HARDWARE AS INDICATED ON THE DRAWINGS.

#### HYBRID CABLES INSTALLATION:

- A. THE CONTRACTOR SHALL ROUTE, TEST, AND INSTALL ALL CABLES AS INDICATED ON THE CONSTRUCTION DRAWINGS AND IN ACCORDANCE WITH THE MANUFACTURER'S
- B. THE INSTALLED RADIUS OF THE CABLES SHALL NOT BE LESS THAN THE MANUFACTURER'S SPECIFICATIONS FOR BENDING RADII.
- C. EXTREME CARE SHALL BE TAKEN TO AVOID DAMAGE TO THE CABLES DURING HANDLING AND INSTALLATION.
- 1. FASTENING MAIN HYBRID CABLES: ALL CABLES SHALL BE PERMANENTLY FASTENED TO THE COAX LADDER AT 4'-0" OC USING NON-MAGNETIC STAINLESS STEEL CLIPS.
- 2. FASTENING INDIVIDUAL FIBER AND DC CABLES ABOVE BREAKOUT ENCLOSURE (MEDUSA), WITHIN THE MMRTS CARINET AND ANY INTERMEDIATE DISTRIBUTION BOXES:
- MMBIS CABINET AND ANY INTERMEDIAL DISTRIBUTION BOXES:

  0. FIBER: SUPPORT FIBER BUNDLES USING 1/2. YELCRO STRAPS OF THE REQUIRED LENGTH 0 18"

  OC. STRAPS SHALL BE UV, OIL AND WATER RESISTANT AND SUITABLE FOR INDUSTRIAL INSTALLATIONS AS MANUFACTURED BY TEXTOL OR APPROVED EQUAL.

  b. DC: SUPPORT DC BUNDLES WITH ZIP TIES OF THE ADEQUATE LENGTH. ZIP TIES TO BE UV STABILIZED, BLACK NYLON, WITH TENSILE STRENGTH AT 12,000 PSI AS MANUFACTURED BY
- NELCO PRODUCTS OR EQUAL.

  3. FASTENING JUMPERS: SECURE JUMPERS TO THE SIDE ARMS OR HEAD FRAMES USING STAINLESS
- STEEL TIE WRAPS OR STAINLESS STEEL BUTTERFLY CLIPS.
- 4. CABLE INSTALLATION: INSPECT CABLE PRIOR TO USE FOR SHIPPING DAMAGE, NOTIFY THE CONSTRUCTION MANAGER.

  CABLE ROUTING: CABLE INSTALLATION SHALL BE PLANNED TO ENSURE THAT THE LINES WILL BE
  PROPERLY ROUTED IN THE CABLE ENVELOP AS INDICATED ON THE DRAWINGS, AVOID TWISTING
- c. HOIST CABLE USING PROPER HOISTING GRIPS. DO NOT EXCEED MANUFACTURES RECOMMENDED MAXIMUM BEND RADIUS.

- 5. GROUNDING OF TRANSMISSION LINES: ALL TRANSMISSION LINES SHALL BE GROUNDED AS INDICATED SECTION 26 200 ELECTRICAL MATERIALS AND EQUIPMENT
- GROUNDING OF TROMOMISSION CHIEF THE TROMOMISSION COLOR CODING SHALL BE AS REQUIRED IN TS 0200 REV 4.
   HYBRID CABLE COLOR CODING: ALL COLOR CODING SHALL BE AS REQUIRED IN TS 0200 REV 4.
   HYBRID CABLE LABELING: INDIMIDUAL HYBRID AND DC BUNDLES SHALL BE LABELED ALPHA—NUMERICALLY ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE EN 2012—001,

## WEATHERPROOFING EXTERIOR CONNECTORS AND HYBRID CABLE GROUND

- A. ALL FIBER & COAX CONNECTORS AND GROUND KITS SHALL BE WEATHERPROOFED.
- B. WEATHERPROOFED USING ONE OF THE FOLLOWING METHODS. ALL INSTALLATIONS MUST BE DONE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND INDUSTRY BEST PRACTICES.
- COLD SHRINK: ENCOMPASS CONNECTOR IN COLD SHRINK TUBING AND PROVIDE A DOUBLE WRAP OF 2" ELECTRICAL TAPE EXTENDING 2" BEYOND TUBING. PROVIDE 3M COLD SHRINK
- CXS SERIES OR EQUAL.
  2. SELF-AMALGAMATING TAPE: CLEAN SURFACES. APPLY A DOUBLE WRAP OF SELF-AMALGAMATING TAPE: CLEAN SUKFACES. APPLY A DUUBLE WRAP OF SELF-AMALGAMATING TAPE 2 BEYOND CONNECTOR. APPLY A SECOND WRAP OF SELF-AMALGAMATING TAPE IN OPPOSITE DIRECTION. APPLY DOUBLE WRAP OF 2' WIDE ELECTRICAL TAPE EXTENDING 2' BEYOND THE SELF-AMALGAMATING TAPE. 3M SLIM LOCK CLOSURE 716: SUBSTITUTIONS WILL NOT BE ALLOWED.

  OPEN FLAME ON JOB SITE IS NOT ACCEPTABLE

#### SECTION 11 800 - INSTALLATION OF MULTIMODAL BASE STATIONS (MMBS) AND RELATED EQUIPMENT

#### SUMMARY:

- THIS SECTION SPECIFIES MMBS CABINETS, POWER CABINETS, AND INTERNAL EQUIPMENT INCLUDING BY NOT LIMITED TO RECTIFIERS, POWER DISTRIBUTION UNITS, BASE BAND UNITS, SURGE ARRESTORS, BATTERIES, AND SIMILAR EQUIPMENT FURNISHED BY THE COMPANY FOR INSTALLATION BY THE CONTRACTOR (OFCI).
- B. CONTRACTOR SHALL PROVIDE AND INSTALL ALL MISCELLANEOUS MATERIALS AND PROVIDE ALL LABOR REQUIRED FOR INSTALLATION EQUIPMENT IN EXISTING CABINET OR NEW CABINET AS SHOWN ON DRAWINGS AND AS REQUIRE BY THE APPLICABLE
- C. COMPLY WITH MANUFACTURERS INSTALLATION AND START-UP REQUIREMENTS

#### DC CIRCUIT BREAKER LABELING

A. LABEL CIRCUIT BREAKERS ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE - EN 2012-001, REV 1.

#### SECTION 11 800 - INSTALLATION OF MULTIMODAL BASE TRANSCIEVER STATIONS (MMBTS) AND RELATED EQUIPMENT

- A. THIS SECTION SPECIFIES MMBTS CABINETS, POWER CABINETS, AND INTERNAL EQUIPMENT INCLUDING BY NOT LIMITED TO RECTIFIERS, POWER DISTRIBUTION UNITS, BASE BAND UNITS, SURGE ARRESTORS, BATTERIES, AND SIMILAR EQUIPMENT FURNISHED BY THE COMPANY FOR INSTALLATION BY THE CONTRACTOR (OFCI).
- CONTRACTOR SHALL PROVIDE AND INSTALL ALL MISCELLANEOUS MATERIALS AND PROVIDE ALL LABOR REQUIRED FOR INSTALLATION EQUIPMENT IN EXISTING CABINET OR NEW CABINET AS SHOWN ON DRAWINGS AND AS REQUIRE BY THE APPLICABLE INSTALLATION MOPS.
- C. COMPLY WITH MANUFACTURERS INSTALLATION AND START-UP REQUIREMENTS

#### SUPPORTING DEVICES:

- A. MANUFACTURED STRUCTURAL SUPPORT MATERIALS: SUBJECT TO COMPLIANCE WITH REQUIREMENTS, PROVIDE PRODUCTS BY THE FOLLOWING:
  - ALLIED TUBE AND CONDUIT
  - UNISTRUT DIVERSIFIED PRODUCTS
- THOMAS & BETTS
- B. FASTENERS: TYPES, MATERIALS, AND CONSTRUCTION FEATURES AS FOLLOWS:
  - EXPANSION ANCHORS: CARBON STEEL WEDGE OR SLEEVE TYPE.
    POWER-DRIVEN THREADED STUDS: HEAT-TREATED STEEL, DESIGNED SPECIFICALLY FOR THE
  - NITENDED SERVICE

- INTENDED SERVICE.
  FASTEN BY MEANS OF WOOD SCREWS ON WOOD.
  TOGGLE BOLTS ON HOLLOW MASONRY UNITS.
  CONCRETE INSERTS OR EXPANSION BOLTS ON CONCRETE OR SOLID MASONRY.
  MACHINE SCREWS, WELDED THEADED STUDS, OR SPRING—TENSION CLAMPS ON STEEL
  EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE SHALL NOT BE PERMITTED.
  DO NOT WELD CONDUIT, PIPE STRAPS, OR TIEMS OTHER THAN THREADED STUDS TO STEEL
  TERLICITIES
- IN PARTITIONS OF LIGHT STEEL CONSTRUCTION, USE SHEET METAL SCREWS.

#### SUPPORTING DEVICES:

- A. INSTALL SUPPORTING DEVICES TO FASTEN ELECTRICAL COMPONENTS SECURELY AND PERMANENTLY IN ACCORDANCE WITH NEC.
- B. COORDINATE WITH THE BUILDING STRUCTURAL SYSTEM AND WITH OTHER TRADES.
- C. UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FASTEN ELECTRICAL ITEMS AND THEIR SUPPORTING HARDWARE SECURELY TO THE STRUCTURE IN ACCORDANCE WITH
- D. ENSURE THAT THE LOAD APPLIED BY ANY FASTENER DOES NOT EXCEED 25 PERCENT OF THE PROOF TEST LOAD.
- E. USE VIBRATION AND SHOCK-RESISTANT FASTENERS FOR ATTACHMENTS TO CONCRETE

#### **ELECTRICAL IDENTIFICATION:**

- A. UPDATE AND PROVIDE TYPED CIRCUIT BREAKER SCHEDULES IN THE MOUNTING BRACKET, INSIDE DOORS OF AC PANEL BOARDS WITH ANY CHANGES MADE TO THE AC SYSTEM.
- B. BRANCH CIRCUITS FEEDING AVIATION OBSTRUCTION LIGHTING EQUIPMENT SHALL BE CLEARLY IDENTIFIED AS SUCH AT THE BRANCH CIRCUIT PANELBOARD.

#### CONDUIT-

- RIGID GALVANIZED STEEL (RGS) CONDUIT SHALL BE USED FOR EXTERIOR LOCATIONS ABOVE GROUND AND IN UNFINISHED INTERIOR LOCATIONS AND FOR ENCASED RUNS IN CONCRETE. RIGID CONDUIT AND FITTINGS SHALL BE STEEL, COATED WITH ZINC EXTERIOR AND INTERIOR BY THE HOT DIP GALVANIZING PROCESS. CONDUIT SHALL BE PRODUCED TO ANSI SPECIFICATIONS C80.1. FEDERAL SPECIFICATION WW-C-581 AND SHALL BE LISTED WITH THE UNDERWRITERS' LABORATORIES. FITTINGS SHALL BE - SET SCREW OR COMPRESSION FITTINGS WILL NOT BE ACCEPTABLE. RGS CONDUITS SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND.
- B. UNDERGROUND CONDUIT IN CONCRETE SHALL BE POLYVINYLCHLORIDE (PVC) SUITABLE FOR DIRECT BURIAL AS APPLICABLE. JOINTS SHALL BE BELLED, AND FLUSH SOLVENT WELDED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. CONDUIT SHALL BE CARLON ELECTRICAL PRODUCTS OR APPROVED EQUAL.
- C. TRANSITIONS BETWEEN PVC AND RIGID (RGS) SHALL BE MADE WITH PVC COATED METALLIC LONG SWEEP RADIUS ELBOWS.
- D. EMT OR RIGID GALVANIZED STEEL CONDUIT MAY BE USED IN FINISHED SPACES CONCEALED IN WALLS AND CEILINGS. EMT SHALL BE MILD STEEL, ELECTRICALLY WELDED, ELECTRO—GALVANIZED OR HOT—DIPPED GALVANIZED AND PRODUCED TO ANSI SPECIFICATION C80.3, FEDERAL SPECIFICATION WW-C-563, AND SHALL BE UL LISTED. EMT SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND, OR APPROVED EQUAL FITTINGS SHALL BE METALLIC COMPRESSION. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE.
- E. LIQUID TIGHT FLEXIBLE METALLIC CONDUIT SHALL BE USED FOR FINAL CONNECTION TO EQUIPMENT. FITTINGS SHALL BE METALLIC GLAND TYPE COMPRESSION FITTINGS, MAINTAINING THE INTEGRITY OF CONDUIT SYSTEM. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE. MAXIMUM LENGTH OF FLEXIBLE CONDUIT SHALL NOT EXCEED 6-FEET. LFMC SHALL BE PROTECTED AND SUPPORTED AS REQUIRE BY NEC.
  MANUFACTURERS OF FLEXIBLE CONDUITS SHALL BE CAROL, ANACONDA METAL HOSE OR UNIVERSAL METAL HOSE, OR APPROVED EQUAL.
- F. MINIMUM SIZE CONDUIT SHALL BE 3/4 INCH (21MM).

#### HUBS AND BOXES:

- A. AT ENTRANCES TO CABINETS OR OTHER EQUIPMENT NOT HAVING INTEGRAL THREADED HUBS PROVIDE METALLIC THREADED HUBS OF THE SIZE AND CONFIGURATION REQUIRED. HUB SHALL INCLUDE LOCKNUT AND NEOPRENE O-RING SEAL PROVIDE IMPACT RESISTANT 105 DEGREE C PLASTIC BUSHINGS TO PROTECT CABLE INSULATION.
- B. CABLE TERMINATION FITTINGS FOR CONDUIT
- CABLE TERMINATORS FOR RGS CONDUITS SHALL BE TYPE CRC BY 0-Z/GEDNEY OR EQUAL CABLE TERMINATORS FOR LINC SHALL BE ETCO CL2075; OR MADE FOR THE PURPOSE PRODUCTS BY ROXTEC.
- C. EXTERIOR PULL BOXES AND PULL BOXES IN INTERIOR INDUSTRIAL AREAS SHALL BE PLATED CAST ALLOY, HEAVY DUTY, WEATHERPROOF, DUST PROOF, WITH GASKET, PLATED IRON ALLOY COVER AND STAINLESS STEEL COVER SCREWS, CROUSE—HINDS WAB SERIES
- D. CONDUIT OUTLET BODIES SHALL BE PLATED CAST ALLOY WITH SIMILAR GASKETED COVERS. OUTLET BODIES SHALL BE OF THE CONFIGURATION AND SIZE SUITABLE FOR THE APPLICATION. PROVIDE CROUSE—HINDS FORM 8 OR EQUAL.
- E. MANUFACTURER FOR BOXES AND COVERS SHALL BE HOFFMAN, SQUARE "D". CROUSE-HINDS, COOPER, ADALET, APPLETON, O-Z GEDNEY, RACO, OR APPROVED EQUAL.

#### SUPPLEMENTAL GROUNDING SYSTEM

- A. FURNISH AND INSTALL A SUPPLEMENTAL GROUNDING SYSTEM AS INDICATED ON THE DRAWINGS, SUPPORT SYSTEM WITH NON-MAGNETIC STAINLESS STEEL CLIPS WITH RUBBER GROMMETS. GROUNDING CONNECTORS SHALL BE TINNED COPPER WIRE, SIZES AS INDICATED ON THE DRAWINGS. PROVIDE STRANDED OR SOLID BARE OR INSULATED CONDUCTORS AS INDICATED.
- B. SUPPLEMENTAL GROUNDING SYSTEM: ALL CONNECTIONS TO BE MADE WITH CAD WELDS, EXCEPT AT EQUIPMENT USE LUGS OR OTHER AVAILABLE GROUNDING MEANS AS REQUIRED BY MANUFACTURER; AT GROUND BARS USE TWO HOLE SPADES WITH NO OX.
- C. STOLEN GROUND—BARS: IN THE EVENT OF STOLEN GROUND BARS, CONTACT SPRINT CM FOR REPLACEMENT INSTRUCTION USING THREADED ROD KITS.

#### **EXISTING STRUCTURE:**

A. EXISTING EXPOSED WIRING AND ALL EXPOSED OUTLETS, RECEPTACLES, SWITCHES, DEVICES, BOXES, AND OTHER EQUIPMENT THAT ARE NOT TO BE UTILIZED IN THE COMPLETED PROJECT SHALL BE REMOVED OR DE-ENERGIZED AND CAPPED IN THE WALL. CEILING, OR FLOOR SO THAT THEY ARE CONCEALED AND SAFE. WALL, CEILING, OR FLOOR SHALL BE PATCHED TO MATCH THE ADJACENT CONSTRUCTION.

#### CONDUIT AND CONDUCTOR INSTALLATION:

- A. CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED CONDUITS SHALL BE FASIENED SECURELT IN PLACE WITH AFFROVED NON-FRONTAIN STRAPS AND HANGERS. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUITS IN TIGHT ENVELOPES. CHANGES IN DIRECTION TO ROUTE AROUND OBSTACLES SHALL BE MADE WITH CONDUIT
  OUTLET BODIES. CONDUIT SHALL BE INSTALLED IN A NEAT AND WORKMANLIKE MANNER, PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES, ALL CONDUIT SHALL BE FISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED TO PREVENT CONCRETE, PLASTER OR DIRT FROM ENTERING. CONDUITS SHALL BE RIGIDLY CLAMPED TO BOXES BY CALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCKNUT ON OUTSIDE AND
- B. CONDUCTORS SHALL BE PULLED IN ACCORDANCE WITH ACCEPTED GOOD PRACTICE.

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EV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY







244 RIVERS EDGE LANE TOMS RIVER, NJ 08755

ENGINEER'S LICENSE



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

CT03XC022

ASDG PROJECT No

ASDGSP26

DESIGN TYPE

2.5 GHz

SITE INFORMATION SOUTH GUILFORD

SOUTH GUILFORD, CT 06437

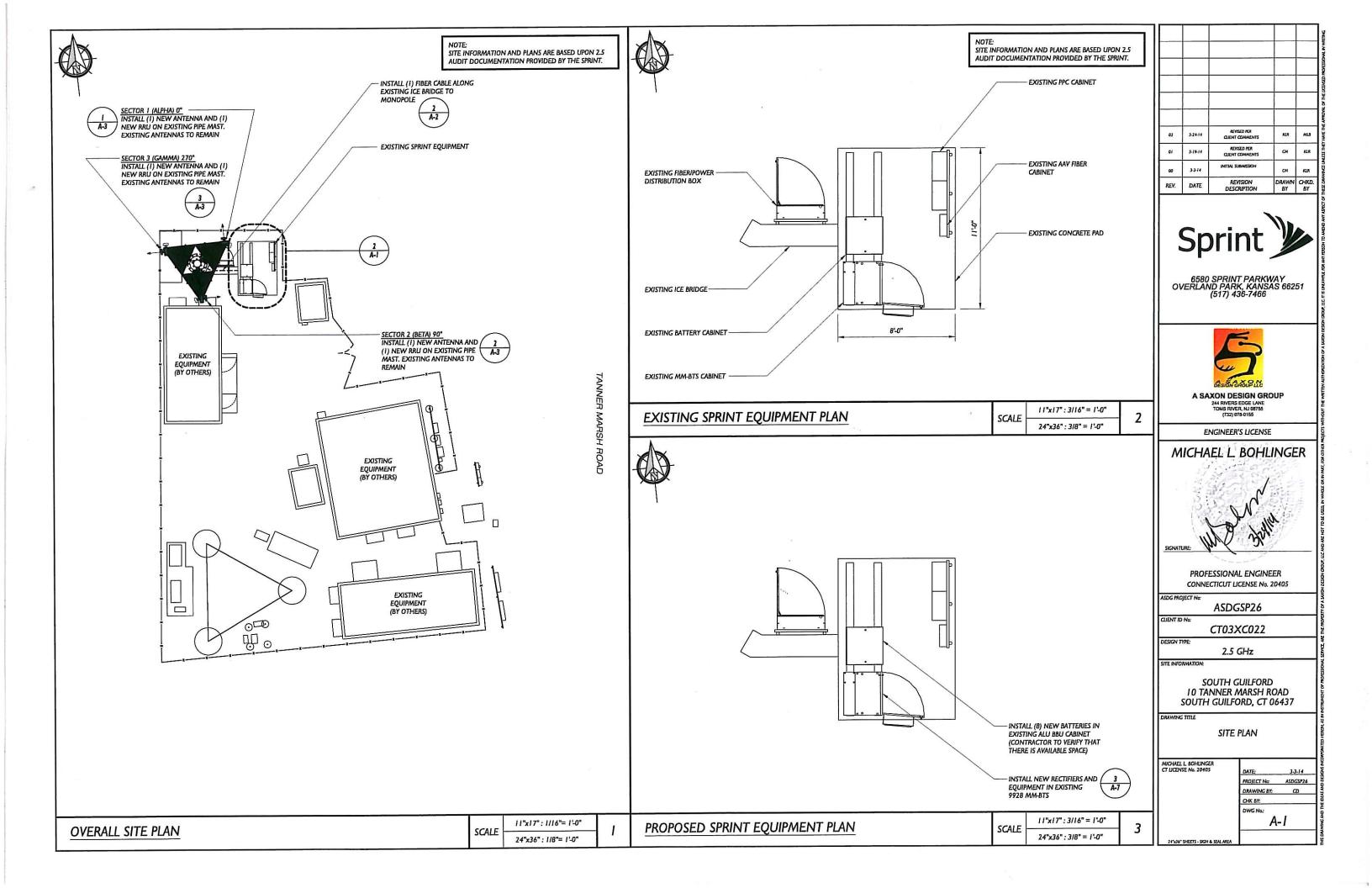
SPRINT SPECIFICATIONS (SHEET 3 OF 3)

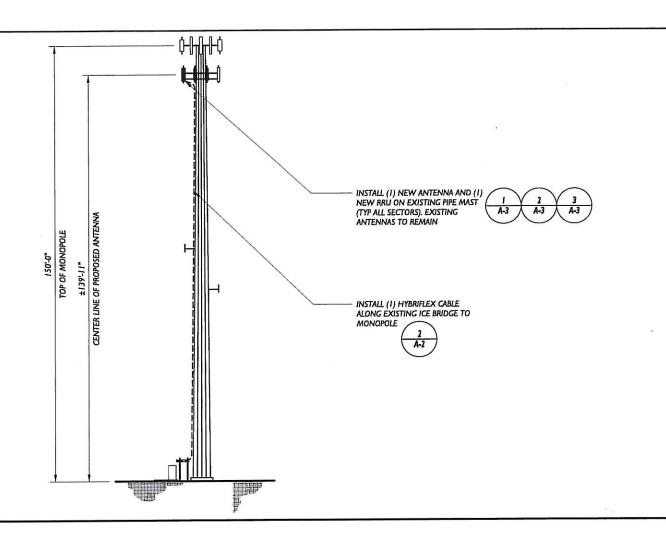
10 TANNER MARSH ROAD

MICHAEL L BOHLINGE

3-3-14 PROJECT Na: ASDGSP26 DRAWING BY: Φ CHK BY:

SP-3





NOTE: SITE INFORMATION AND PLANS ARE BASED UPON 2.5 AUDIT DOCUMENTATION PROVIDED BY THE SPRINT.

11"x17" : 1/32" = 1'-0"

24"x36" : 1/16" = 1'-0"

SCALE

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6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



A SAXON DESIGN GROUP 244 RIVERS EDGE LANE TOMS RIVER, NJ 08755 (732) 678-0155

ENGINEER'S LICENSE

### MICHAEL L BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26

CT03XC022 2.5 GHz

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

**BUILDING ELEVATION** AND CABLE PLAN

DATE:	3-3-14
PROJECT Nat	ASDGSP26
DRAWING BY:	Ф
CHK BY:	
DWG Na: A-2	
	PROJECT No: / DRAWING BY: CHK BY:

11.		HYBRID	CABLE DC CON	NDUCTOR SIZE GU	IIDELINE
	CIRCO ROCAL OLIT	CABLE	LENGTH	DC CONDUCTOR	CABLE DIAMETER
///-	FIBER BREAK OUT (TYP)	FIBER ONLY	VARIES	USE NV HYBRIFLEX	5/8"
	BREAK OUTS TO RRU	HYBRIFLEX	OVER 200'	8 AWG	1 1/4"
	BALAK GOTS TO IMO	HYBRIFLEX	225'-300'	6 AWG	1 1/4"
- 111		HYBRIFLEX	325'-375'	4 AWG	1 1/4"
	INSTALL CABLE TERMINATION ENCLOSE				0] EL FIBER DIST.
	INSTALL CABLE TERMINATION ENCLOSE FURNISHED WITH CABLE INSTALL AND PER MANUFACTURE'S SPECIFICATIONS  INSTALL (I) 518" NV HYBRIFLEX CABLE		[12D] [12D]	217Ø[5.55 12 CHANNE (TYP OF 3)	OJ EL FIBER DIST.

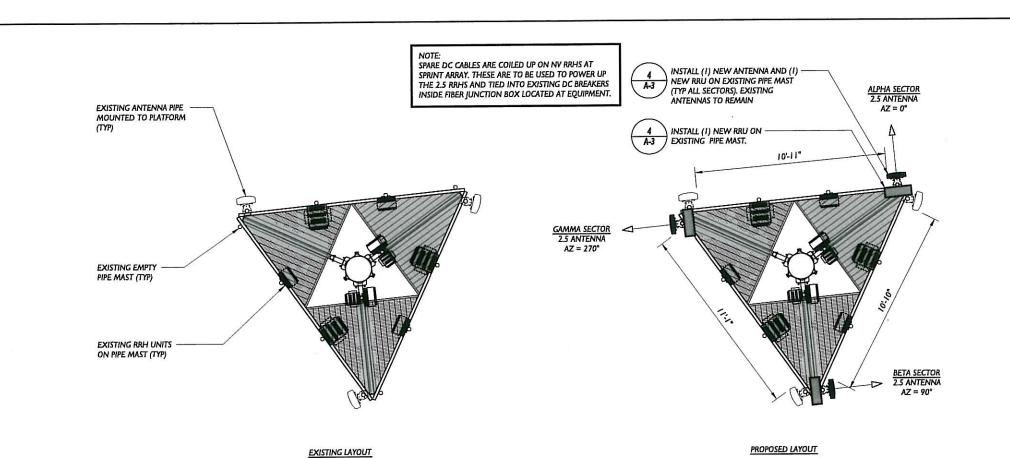
**ELEVATION** 

HYBRID BREAK OUT DETAIL

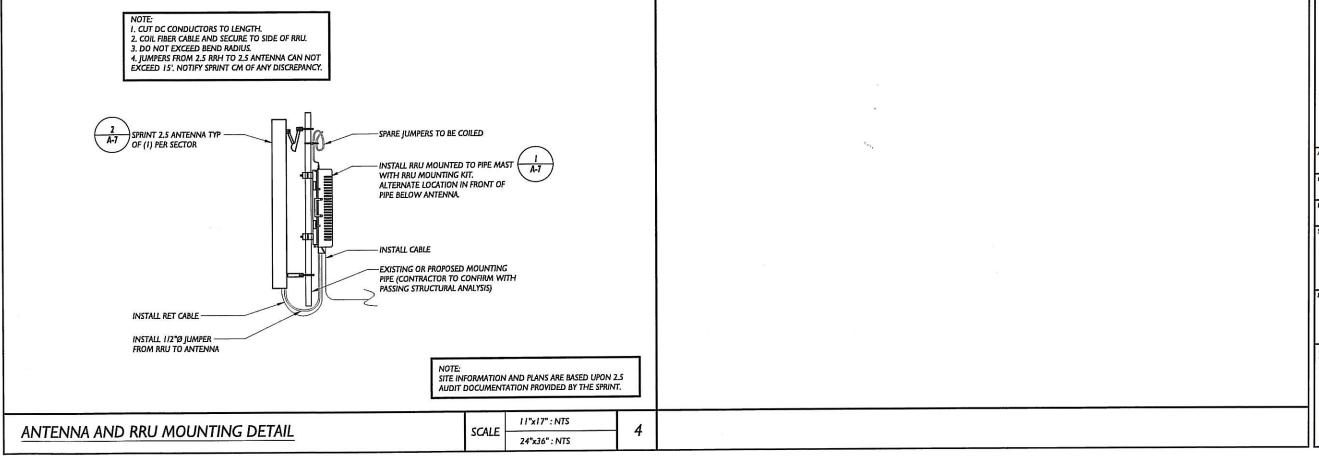
11"x17" : NTS

24"x36" : NTS

**SCALE** 



 $SCALE = \frac{11"x17":31/6" = 1'\cdot0"}{24"x36":3/8" = 1'\cdot0"}$ 



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<b>0</b> 2	32414	REVISED FER CLIENT COMMENTS	KIN	MLB
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REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



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244 RIVERS EDGE LANE
TOMS RIVER, NJ 00755
(732) 678-0155

ENGINEER'S LICENSE

### MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE №. 20405

ASDG PROJECT N

ASDGSP26

DESIGN TYPE:

CT03XC022 2.5 GHz

SITE INFORMATION

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

DRAWING TITL

ANTENNA PLAN AND MOUNTING DETAILS

MICHAEL L BOHLINGER
CT UCENSE No. 20405

DATE: 3-3-14

PROJECT No: ASDGSP26

DRAWING BY: CD

GHK BY:

DWG No:

A-3

GENERAL CONTRACTOR TO VERIFY CURRENT RFDS PRIOR TO CONSTRUCTION START. Sprint 🥦 **RFDS Sheet General Site Information** CT03XC022 Equipment Vandor ALU Site ID Lattitude 41.288773 Southern Connecticut Market -72.558287 EAST Longitude Ragion LL SITE ID N/A N/A MLA Structure Type MONOPOLE BT5 Type N/A Incremental Power Draw Sitema 5R Equipment type N/A needed by added Equipment Solution ID ALU 0 Equipment Vandor **Base Equipment** NONE ALU BBU KIT Top Hat BBU Kit N/A Top Het Qty **BBU Kit Qty** N/A Top Hat Dimenstions N/A Top Hat Weight (ibs) **Growth Cabinet** NONE N/A Growth Cabinet Qty **Growth Cabinat Dimansions** Growth Cabinet Weight **RF Path Information** TD-RRHBx20-25 RRH Qty 25.1in x 18.6 x 5.7 in RRH Dimensions RRH Weight, lbs. TBD RRH Mount Weight, Lbs. ALU Fiber only Power and Fiber Cable Cabla Qty 0.12 Weight per foot. Lbs. Diameter, Inches, (calculated as antenna haight plus 20%) 108 Length Ft. Coax Jumper, Mfg TBD. Coax Jumper 27 Coax Jumper Oty Coax Jumper Length. Feet. Coax Jumper Weight Coax Jumper Diameter. Inches AISG Cable Commscope ATCB-B01-005 3 AISG Cable Qty 0.315 AISG Diameter. Inches. AISG Cable length. Weight of entire AISG cable. Lbs. Antenna Sector Information Sector 1 Sector 2 Sector 3 RFS APXVTM14-C-120 RFS APXVTM14-C-120 RFS APXVTM14-C-120 Antenna make/model Antenna qty 56.3 x 12.6 x 5.3 56.3 x 12.6 x 6.3 55.3 x 12.5 x 5.3 Antenna Dimensions, Inches 56 Antenna Weight, Lbs 11 (estimata) 11 (estimate) 11 (estimate) Antenna Mounting Kit Weight. Lbs. 139'-11" 139'-11" 159'-11" CL Height 270 90 Antenna Azimuth 0 D Antenna Mechanical Downtilt

-2

3/24/2014

-2

Confidential

NO

SITE INFORMATION AND PLANS ARE BASED UPON 2.5
AUDIT DOCUMENTATION PROVIDED BY THE SPRINT.

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02	3-24-14	REVISED PER CLIENT COMMENTS	KIA	MLB
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00	33.14	INITIAL SUBMISSION	СМ	KLA
REV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



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ENGINEER'S LICENSE

### MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER
CONNECTICUT LICENSE No. 20405

ASDG PROJECT

ASDGSP26

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CT03XC022 2.5 GHz

SITE INFORMATION:

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

DRAWING T

RF DATA SHEET AND EQUIPMENT INFORMATION

MICHAEL L. BOHLINGER CT UCENSE № 20405

DATE: 3.3.14

PROJECT No:: ASDGSP26

DRAWING BY: CD

CHK BY:

DWG Na:

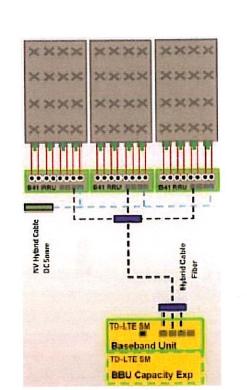
A-4

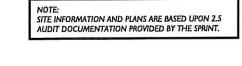
10-10 0000 0000 000 4 000 4904

SCALE 11"x17": NTS
24"x36": NTS

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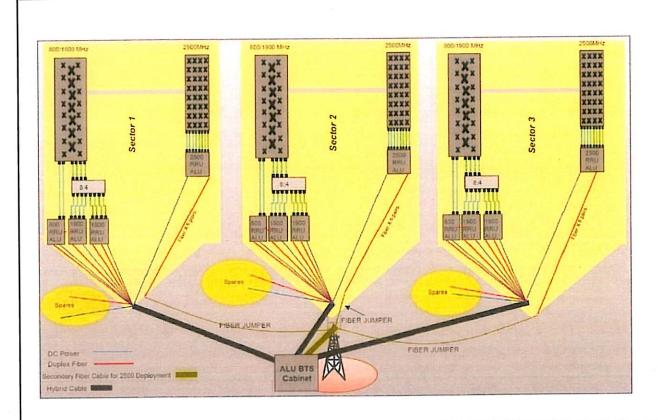
Sprint RFD5 Sheet







ALU 2500MHz ALU SCENARIO I SCALE 11"x17":NTS | 1 | RFS 2500MHz ALU SCENARIO | 1 | 24"x36":NTS | 2 | 24"x36":NTS | 2 |



DANIA MIDING DIA CDAMA ALLI FOLIDAMENT	SCALE	11"x17" : NTS
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3

S 2500MHz ALU SCENARIO I

SCALE

18 pr MM Fiber

SCALE

11"x17": NTS

24"x36": NTS

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TOMS RIVER, NJ 08755

ENGINEER'S LICENSE

MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDG PROJECT

ASDGSP26

CT03XC022

2.5 GHz

SITE INFORMATION

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

DRAWING TITL

WIRING DIAGRAMS

MICHAEL L. BOHUNGER
CT LICENSE No. 20405

DATE: 3-3-14

PROJECT No: ASDGSP26

DRAWING BY:
CD

CHK BY:

DWG No:

A-5

NOTE: SITE INFORMATION AND PLANS ARE BASED UPON 2.5 AUDIT DOCUMENTATION PROVIDED BY THE SPRINT.

		NV CABLES	5	
BAND	INDICA	TOR	PORT	COLOR
800-1	YEL	GRH	NV-1	GRH
1900-1	YEL	RED	NV-2	BLU
1900-2	YEL	BRN	NV-3	BRN
1900-3	YEL	BLU	11V-4	WHT
1900-4	YEL	SLT	IIV-5	RED
800-2	YEL	ORG	NV-6	SLT
SPARE	YEL	WHT	NV-7	PPL
2500	YEL	PPL	NV-8	ORG

HY	BRID
HYBRID	COLOR
1	GRN
2	BLU
3	BRN
4	WHT
5	RED
6	SLT
7	PPL
8	ORG

2.5 Band	
2500 Radio 1	COLOR
YEL WHT	GRN
YEL WHT	BLU
YEL WHT	BRN
YEL WHT	WHT
YEL WHT	RED
YEL WHT	SLT
YEL WHT	PPL
YEL WHT	ORG

#### FIGURE 19.1 CABLE COLOR CODE

			Second	
Sector	Cable	First Ring	Ring	Third Ring
1 Alpha	1	Green	No Tape	No Tape
1	2	III BAR	No Tape	No Tape
1	3	Brown	No Tape	No Tape
1	4	White	No Tape	No Tape
1	5	Red	No Tape	No Tape
1	6	Grey	No Tape	No Tape
1	7	Purple	No Tape	No Tape
1	8	Orange	No Tape	No Tape
2 Beta	1	Green	Green	No Tape
2	2	50.00	Sept.	No Tape
2	3	Brown	Brown	No Tape
2	4	White	White	No Tape
2	5	Red	Red	No Tape
2	6	Grey	Grey	No Tape
2	7	Purple	Purple :	No Tape
2	8	Orange	Orange	No Tape
3 Gamma	1	Green	Green	Green
3	2	10 国际 10 元	150m	THE R. LEWIS CO.
3	3	Brown	Brown	Brown
3	4	White	White	White
3	5	Red	Red	Red
3	6	Grey	Grey	Grey
3	7	Purple	Purple	Fuple
3	8	Orange	Orange	Orange

- 1. All cables shall be marked at the top and bottom with 2" colored tape, stencil tag colored tape, or colored heat shrink tubing
- 2. Colored tape may be obtained from Graybar Electronic. UV stabilized tape or heat shrink are preferred.
- 3. The first ring shall be closest to the end of the cable, and there shall be a 1" space between each ring.
- 4. The cable color code shall be applied in accordance to Table 19-1.
- A. Table 19-1 only shows 3 sectors, but additional sectors are easily supported by adding the appropriate number of colored rings to the cable color code.

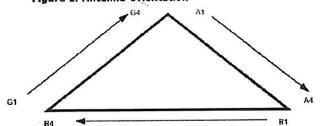
  5. After the cable color code is applied, the frequency color code, Table 19-2, must be applied for the specific frequency band in use on a given line. A.2" gap shall separate the cable color code from the frequency color code. B. The 2" color rings for the frequency code shall be placed next to each other with no spaces.
- 6. Wrap 2" colored tape a minimum of 3 times around the coax, and keep the tape in the same area as much as possible. This will allow removal of tape that fades or discolors due to weather.
- 7. Examples of the cable and frequency color codes are shown in Figure 19-1 and Figure 19-2.

#### FIGURE 19.2 COLOR CODE

FREQUENC	INDICATOR	ID
800-1	YEL	GRN
1900-1	YEL	RED
1900-2	YEL	BRN
1900-3	YEL	BLU
1900-4	YEL	SLT
800-1	YEL	ORG
RESERVED	YEL	WHT
RESERVED	YEL	PPL

FREQUENCY	INDICATOR		ID
2500 -1	YEL	WHT	GRN
2500 -2	YEL	WHT	RED
2500 -3	YEL	WHT	BRN
2500 -4	YEL	WHT	BLU
2500 -5	YEL	WHT	SLT
2500 -6	YEL	WHT	ORG
2500 -7	YEL	WHT	WHT
2500 -8	YEL	WHT	PPL

Figure 1: Antenna Orientation



3-19-14 REV. DATE



6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



A SAXON DESIGN GROUP 244 RIVERS EDGE LANE TOMS RIVER, NJ 08755 (732) 678-0155

**ENGINEER'S LICENSE** 

MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26

CT03XC022 2.5 GHz

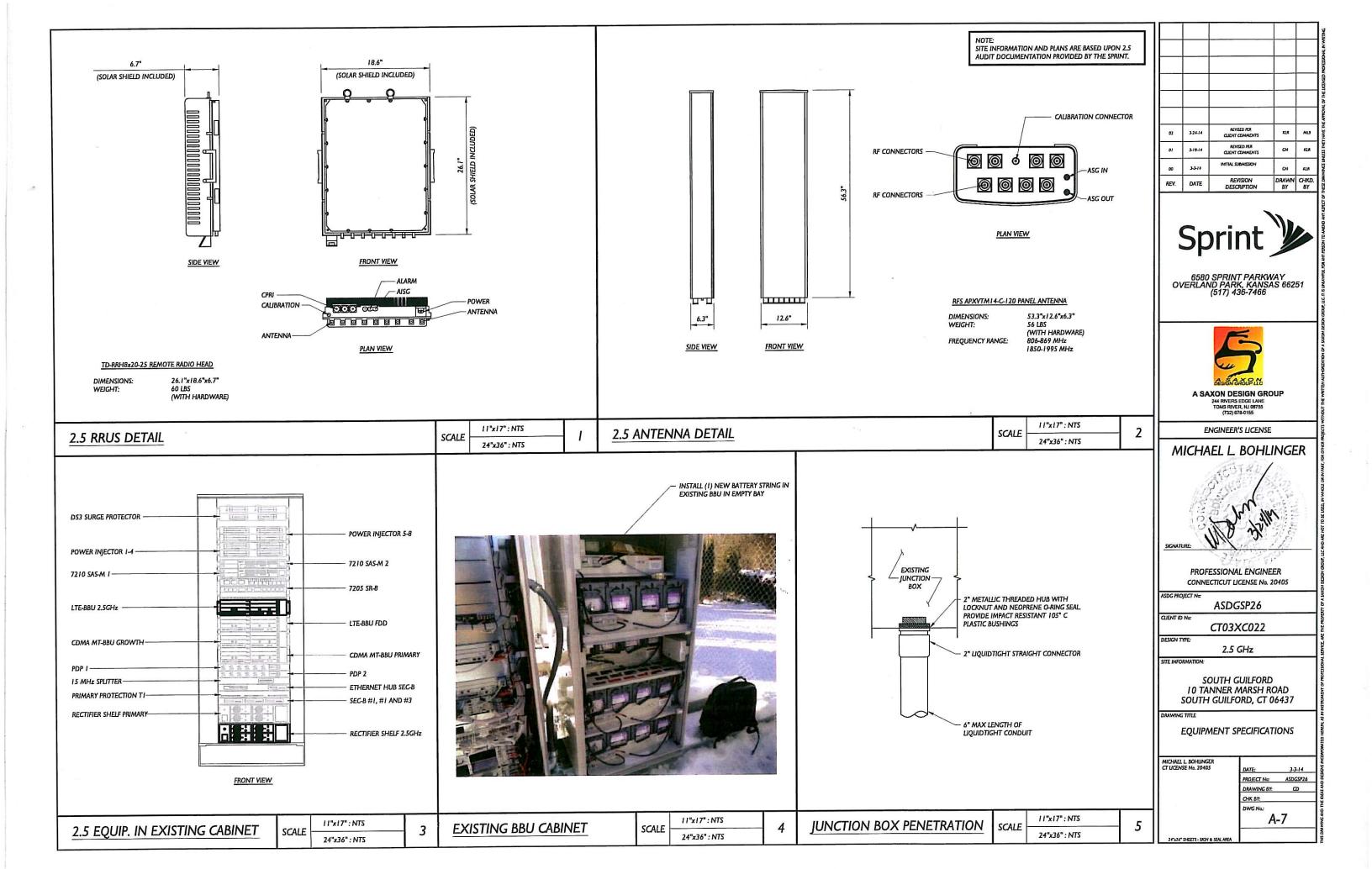
SOUTH GUILFORD **10 TANNER MARSH ROAD** SOUTH GUILFORD, CT 06437

RF DATA SHEET

A-6

MICHAEL L. BOHLINGER CT LICENSE No. 20405 PROJECT No: ASDGSP26 DRAWING BY: DWG Na.:

11"x17" : NTS SCALE 24"x36" : NTS



#### SPECIAL WORK NOTE:

- 1. G.C. TO FURNISH AND INSTALL ALL COMPONENTS TO UPGRADE EXISTING ELECTRICAL SERVICE, CONDUIT, CONDUCTOR, PPC AND MCB IN ACCORDANCE WITH SPRINT CONSTRUCTION STANDARDS NV 2.5 ADDENDUM "ENGINEERING NOTICE 2013—002 (POWER LIPGRADES) REV.O"
- UPGRADES) REV.U

  2. G.C. TO FURNISH AND INSTALL UPGRADE THE EXISTING MMBTS

  BREAKER, CONDUCTOR, AND CONDUIT TO A MINIMUM NEC RATING

  FOR A 100—AMP, 240V CIRCUIT.

  3. FOR NEW OR REPAIRED GROUNDING EQUIPMENT, REFER TO SPRINT
- GROUNDING STANDARDS AND FOLLOWING (SUPPLEMENTS):

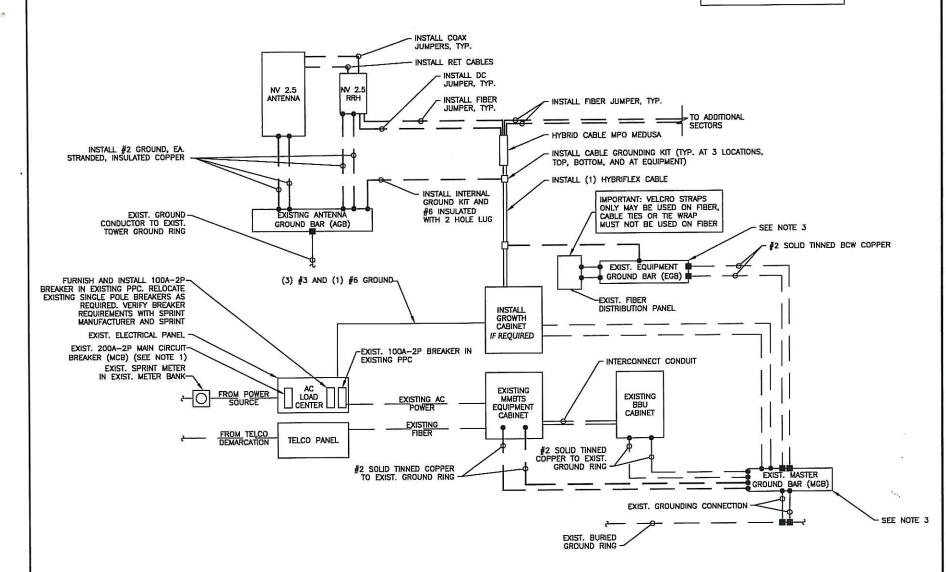
  -ANTI-THEFT UPDATE TO SPRINT GROUNDING DATED 08-24-12

  -SPRINT ENGINEERING LETTER EL-0504 DATED 04-20-12

NOTE-MAXIMUM LENGTH OF LIQUID TIGHT CONDUIT IS TO BE 6 FEET

SYMBOL LEGEND SPECIAL WORK NOTE

- EXOTHERMIC CONNECTION
- MECHANICAL CONNECTION
- CABLE GROUNDING KIT



#### **ELECTRICAL NOTES**

- 1) ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) AS WELL AS APPLICABLE STATE AND LOCAL CODES.
- 2) THE ELECTRICAL CONTRACTOR SHALL COORDINATE ALL CONDUIT ROUTING WITH LOCAL UTILITY COMPANIES AND SPRINT CONSTRUCTION MANAGER.
- 3) ALL CONDUITS ROUTED BELOW GRADE SHALL TRANSITION TO RIGID GALVANIZED ELBOWS WITH RIGID GALVANIZED STEEL CONDUIT ABOVE
- 4) ALL METAL CONDUITS SHALL BE PROVIDED WITH GROUNDING BUSHINGS.
- 5) GENERAL CONTRACTOR SHALL PROVIDE ALL DIRECT BURIED CONDUITS WITH PLASTIC WARNING TAPE IDENTIFYING CONTENTS. TAPE COLORS SHALL BE ORANGE FOR TELEPHONE AND RED FOR ELECTRIC.
- 6) ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED AND PROCURED PER SPECIFICATION REQUIREMENTS.
- 7) THE ELECTRICAL WORK INCLUDES ALL LABOR AND MATERIALS DESCRIBED BY DRAWINGS AND SPECIFICATIONS INCLUDING INCIDENTAL WORK TO PROVIDE COMPLETE OPERATING AND APPROVED ELECTRICAL
- 8) GENERAL CONTRACTOR SHALL PAY FEES FOR PERMITS, AND IS RESPONSIBLE FOR OBTAINING SAID PERMITS AND COORDINATION OF
- 9) ELECTRICAL AND TELCO WIRING OUTSIDE A BUILDING AND EXPOSED TO WEATHER SHALL BE IN WATER TICHT GALVANIZED RIGID STEEL CONDUITS OR SCHEDULE BO PVC (AS PERMITTED BY CODE) AND WHERE REQUIRED IN LIQUID TICHT FLEXIBLE METAL OR NONMETALLIC CONDUITS.
- 10) BURIED CONDUIT SHALL BE SCHEDULE 40 PVC.
- 11) ELECTRICAL WIRING SHALL BE COPPER WITH TYPE XHHW, THWN, OR THIN INSULATION.
- 12) RUN ELECTRICAL CONDUIT OR CABLE BETWEEN ELECTRICAL UTILITY DEMARCATION POINT AND PROJECT OWNER CELL SITE PPC AS INDICATED ON THIS DRAWING. PROVIDE FULL LENGTH PULL ROPE. COORDINATE INSTALLATION WITH UTILITY COMPANY.
- 13) RUN TELCO CONDUIT OR CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT AND PROJECT OWNER CELL SITE TELCO CABINET AND BTS CABINET AS INDICATED ON THIS DRAWING PROVIDE FULL LENGTH PULL ROPE IN INSTALLED TELCO CONDUIT. PROVIDE GREENLEE CONDUIT MEASURING TAPE AT EACH END.
- 14) FIBER OPTIC CIRCUITS SHALL BE IN ACCORDANCE WITH NEC ARTICLE 770-OPTICAL FIBER CABLES AND RACEWAYS.
- 15) COMMUNICATIONS CIRCUITS SHALL BE IN ACCORDANCE WITH NEC ARTICLE 800-COMMUNICATIONS SYSTEMS.

		REVISED FER		
02	3-24-14	CLIENT COMMENTS  REVISED FER CLIENT COMMENTS	KIA CH	MLB
00	3-3-14	NORZEMBLIZ JAITINE	CM	KIA.
ŒV.	DATE	REVISION DESCRIPTION	DRAWN BY	CHKD. BY



6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



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**ENGINEER'S LICENSE** 

MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26 CT03XC022

CLIENT ID No:

2.5 GHz

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

DRAWING TITLE

ONE-LINE DIAGRAM

DRAWING BY: Θ CHK BY: E-I

PROJECT No: ASDGSP26

3-3-14

NOTE: SITE INFORMATION AND PLANS ARE BASED UPON 2.5 AUDIT DOCUMENTATION PROVIDED BY THE SPRINT.

**ELECTRICAL ONE-LINE DIAGRAM** 

11"x17":NTS SCALE 24"x36" : NTS

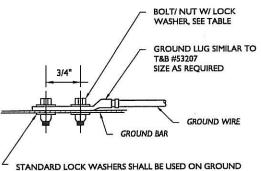
**ELECTRICAL NOTES** 

SCALE

11"x17" : NTS 24"x36" : NTS

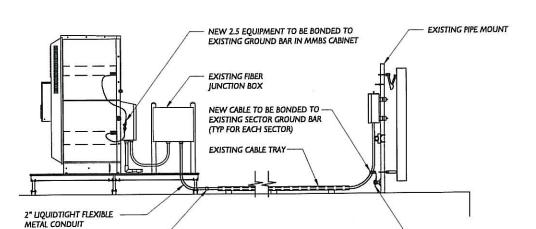


NOTE: SITE INFORMATION AND PLANS ARE BASED UPON 2.5 AUDIT DOCUMENTATION PROVIDED BY THE SPRINT.



BARS, SSERRATED "DRAGON TOOTH" LOCK WASHERS SHALL BE USED ON CONNECTIONS TO BUILDING STEEL AND MISCELLANEOUS METALS.

		TABLE
WIRE SIZE	LUG #	BOLT SIZE
#4/0	53212	1/2" - 20 NC x 1/2" S.S. BOLT & NUT W/ LOCK WASHERS
#2	53207	1/4" - 20 NC x 1/2" S.S. BOLT & NUT W/ LOCK WASHERS
#6	53205	1/4 - 20 NO X 1/2 3.3. BOLT & NOT NY COOK MASHERS



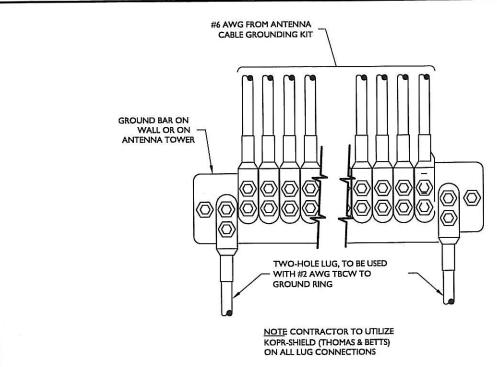
**EXISTING SECTOR** GROUND BAR

SCALE

11"x17" : NTS

24"x36" : NTS

11"x17" : NTS **GROUND LUG CONNECTION** 2 SCALE 24"x36" : NTS



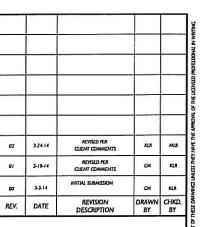
(6' MAX)

USE CONDUIT SEAL PRODUCT -BY ETCO OR ROXTEC

TYPICAL EQUIPMENT GROUNDING SCHEMATIC

GROUND LUG CONNECTION TO GROUND BAR

			q			SITE IN
			-	8		
						DRAW
						MICH CT U.C
SCALE	11"x17" : NTS	3				
JUILL	24"x36" : NTS					262





6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251 (517) 436-7466



A SAXON DESIGN GROUP

ENGINEER'S LICENSE

### MICHAEL L. BOHLINGER



PROFESSIONAL ENGINEER CONNECTICUT LICENSE No. 20405

ASDGSP26

CT03XC022 2.5 GHz

SOUTH GUILFORD 10 TANNER MARSH ROAD SOUTH GUILFORD, CT 06437

GROUNDING DETAILS

MICHAEL L. BOHLINGER CT LICENSE No. 20405	DATE: 3-3-14
	PROJECT Na: ASDGSP26
	DRAWING BY: CD
	CHK BY:
	DWG No.: <b>G-1</b>



# RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

**Sprint Existing Facility** 

Site ID: CT03XC022

Rte 1 TCI Tower 10 Tanner Marsh Road South Guilford, CT 06437

May 7, 2014

EBI Project Number: 62142630

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



May 7, 2014

Sprint Attn: RF Engineering Manager 1 International Boulevard, Suite 800 Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:

CT03XC022 - Rte 1 TCI Tower

Site Total: 40.348% - MPE% in full compliance

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 10 Tanner Marsh Road, South Guilford, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm2). The number of  $\mu$ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm<sup>2</sup>). The general population exposure limit for the cellular band is approximately 567  $\mu$ W/cm<sup>2</sup>, and the general population exposure limit for the 1900 MHz and 2500 MHz bands band is 1000  $\mu$ W/cm<sup>2</sup>. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

### **CALCULATIONS**

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 10 Tanner Marsh Road, South Guilford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario. Actual values seen from this site will be dramatically less than those shown in this report. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 2 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications was used in this direction.



- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20 and the RFS APXVTMM-C-120. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXVTMM-C-120 has a 15.9 dBd gain value at its main lobe at 2500 MHz. All calculations were performed assuming the main lobe of the antenna was focused at the base of the tower to present a worst case scenario.
- 7) The antenna mounting height centerlines for the proposed antennas are **140 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

	Site ID CT03XC022 - Rte 1 TCl Tower				1												
	Site Addresss			uilford, CT 06437													
	Site Type	20 10111101 11101311	Monopole	umora, er ee is:													
					ı												
							Secto	or 1									
						D			A A								
						Power Out Per			Antenna Gain in direction							Power	Power
Antenna						Channel	Number of	Composite	of sample	Antenna	analysis		Cable Loss	Additional		Density	Density
	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power		Height (ft)	height	Cable Size		Loss	ERP	Value	Percentage
1a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	140	134	1/2 "	0.5	0	1386.9474	27.76875	2.77688%
1a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	140	134	1/2 "	0.5	0	389.96892	7.807759	1.37703%
1B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	40	1	40	13.4	140	134	1/2 "	0.5	0	779.93784	15.61552	2.75406%
												Sector tot	al Power De	ensity Value:	6.908%		
	Sector 2																
							Section	or Z									
						Power			Antenna Gain								
						Out Per			in direction							Power	Power
Antenna						Channel	Number of	Composite	of sample	Antenna	analysis		Cable Loss	Additional		Density	Density
	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	point (dBd)			Cable Size		Loss	ERP	Value	Percentage
2a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	140	134	1/2 "	0.5	0	1386.9474	27.76875	2.77688%
2a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	13.4	140	134	1/2 "	0.5	0	389.96892	7.807759	1.37703%
2B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	40	1	40	13.4	140	134	1/2 "	0.5	0	779.93784	15.61552	2.75406%
												Sector tot	al Power De	ensity Value:	6.908%		
							Secto	or 3									
						Power			Antenna Gain								
						Out Per			in direction							Power	Power
Antenna						Channel		Composite	of sample	Antenna	analysis		Cable Loss			Density	Density
	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	point (dBd)		height	Cable Size		Loss	ERP	Value	Percentage
3a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	2	40	15.9	140	134	1/2 "	0.5	0	1386.9474	27.76875	2.77688%
3a 3B	RFS RFS	APXVSPP18-C-A20 APXVTMM14-C-120	RRH RRH	850 MHz 2500 MHz	CDMA / LTE CDMA / LTE	40	1	20 40	13.4 13.4	140 140	134 134	1/2 "	0.5	0	389.96892 779.93784	7.807759 15.61552	1.37703% 2.75406%
38	RFS	APAV HVIIVI14-C-120	KKH	ZOUU IVIHZ	CDIVIA / LTE	40	1	40	13.4	140	134				6.908%	15.01552	2.75406%
	Sector total Power Density Value: 6.908%																

Site Composite MPE %				
Carrier	MPE %			
Sprint	20.724%			
Verizon Wireless PCS	4.920%			
Verizon Wireless Cellular	7.210%			
Verizon Wireless AWS	3.214%			
Verizon Wireless 700 MH:	3.280%			
TCI	0.01			
Total Site MPE %	40.348%			



### **Summary**

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are 20.724% (6.908% from each sector) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **40.348**% of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Scott Heffernan

RF Engineering Director

**EBI Consulting** 

21 B Street

Burlington, MA 01803



FDH Engineering, Inc., 6521 Meridien Drive Raleigh, NC 27616, Ph. 919.755.1012

## Structural Analysis for CTI Towers

150' Monopole Tower

CTI Towers Site Name: Guilford CTI Towers Site ID: 10110 Sprint Site ID: CT03XC022 Sprint Site Name: Rte. 1 TCI Tower

FDH Project Number 1426101400

**Analysis Results** 

	,, o.o	
Tower Components	69.0%	Sufficient
Foundation	37.7%	Sufficient

Prepared By:

Cary J Webb, PE Project Engineer Bradley Newman, PE Senior Project Engineer CT PE License No. 29630

Reviewed By:

FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 (919) 755-1012 info@fdh-inc.com

April 8, 2014

Prepared pursuant to TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the 2005 Connecticut State Building Code

Document No. ENG-RPT-501S

na the 2005 Connecticut State Building Code

Revision Date: 06/17/11

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Conclusions	
Recommendations	3
APPURTENANCE LISTING	4
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GENERAL COMMENTS	6
LIMITATIONS	6
APPENDIX	7

#### **EXECUTIVE SUMMARY**

At the request of CTI Towers, FDH Engineering, Inc. performed a structural analysis of the monopole located in Guilford, CT to determine whether the tower is structurally adequate to support both the existing and proposed loads pursuant to the Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, TIA/EIA-222-F and the 2005 Connecticut State Building Code. Information pertaining to the existing/proposed antenna loading, current tower geometry, geotechnical data, foundation dimensions, and member sizes was obtained from:

Daley Tower Service, Inc. (Job No. 23513-0317) original design drawings dated July 29, 2013
Terracon (Project No. J2135125) Geotechnical Engineering Report dated April 9, 2013
Vertical Solutions, Inc. (Project No 130479, Rev. 0) Structural Review Letter dated May 22, 2013
CTI Towers

The basic design wind speed per the TIA/EIA-222-F standards and the 2005 Connecticut State Building Code is 85 mph without ice and 38 mph with 3/4" radial ice. Ice is considered to increase in thickness with height.

#### Conclusions

With the existing and proposed antennas from Sprint in place at 140 ft, the tower meets the requirements of the *TIA/EIA-222-F* standards and the *2005 Connecticut State Building Code* provided the **Recommendations** listed below are satisfied. Furthermore, provided the foundations were designed and constructed per the original design drawings (see Daley Tower Service, Inc. Job No. 23513-0317), and provided the soil parameters (see Terracon Project No. J2135125), the foundations should have the necessary capacity to support the existing and proposed loading. For a more detailed description of the analysis of the tower, see the **Results** section of this report.

Our structural analysis has been performed assuming all information provided to FDH Engineering, Inc. is accurate (i.e., the steel data, tower layout, existing antenna loading, and proposed antenna loading) and that the tower has been properly erected and maintained per the original design drawings.

#### Recommendations

To ensure the requirements of the *TIA/EIA-222-F* standards and the *2005 Connecticut State Building Code* are met with the existing and proposed loading in place, we have the following recommendations:

- 1. The proposed feedlines should be installed inside the pole shaft.
- 2. RRU/RRH Stipulation: The proposed and existing equipment may be installed in any arrangement as determined by the client.

### **APPURTENANCE LISTING**

The proposed and existing antennas with their corresponding cables/coax lines are shown in **Table 1**. *If the actual layout determined in the field deviates from the layout, FDH Engineering, Inc. should be contacted to perform a revised analysis.* 

### **Table 1 - Appurtenance Loading**

### **Existing Loading:**

Antenna Elevation (ft)	Description	Feedlines <sup>1</sup>	Carrier	Mount Elevation (ft)	Mount Type
150	(6) Antel BXA-70063/6CF (6) Antel BXA-171063/12CF (6) Alcatel Lucent RRH2X40-AWS (6) Alcatel Lucent RRH2x40 LTE (1) RFS 24"x24"x10"	(18) 1-5/8"	Verizon	150	(1) Platform w/ Handrails (Assumed CaAa = 33.02 ft²)
140	(3) RFS APXVSPP18-C-A20 (3) Alcatel Lucent 800 MHz RRH (3) Alcatel Lucent 1900MHz RRH Notch Filters	(3) 1-1/4"	Sprint	140	(1) Platform w/ Handrails

Feedlines installed inside the pole shaft unless otherwise noted

### **Proposed Loading:**

Antenna Elevation (ft)	Description	Feedlines	Carrier	Mount Elevation (ft)	Mount Type
140	(3) RFS APXVTM14-C-120 (3) RFS APXVSPP18-C-A20 (3) Alcatel Lucent 800 MHz RRH (3) Alcatel Lucent 1900MHz RRH (3) Alcatel Lucent TD-RRH8x20-25 (3) Andrew 800 MHz 2x50W External Notch Filter	(3) 1-1/4" (1) .7"	Sprint	140	(1) Platform w/ Handrails

#### **RESULTS**

The following yield strength of steel for individual members was used for analysis:

**Table 2 - Material Strength** 

Member Type	Yield Strength
Tower Shaft Sections	65 ksi
Base Plate	60 ksi
Anchor Bolts	75 ksi

**Table 3** displays the summary of the ratio (as a percentage) of force in the member to their capacities. Values greater than 100% indicate locations where the maximum force in the member exceeds its capacity. *Note: Capacities up to 105% are considered acceptable.* **Table 4** displays the maximum foundation reactions.

If the assumptions outlined in this report differ from actual field conditions, FDH Engineering, Inc. should be contacted to perform a revised analysis. Furthermore, as no information pertaining to the allowable twist and sway requirements for the existing or proposed appurtenances was provided, deflection and rotation were not taken into consideration when performing this analysis.

See the **Appendix** for detailed modeling information

Table 3 - Summary of Working Percentage of Structural Components

Section No.	Elevation ft	Component Type	Size	% Capacity	Pass Fail
L1	150 - 113	Pole	TP30.48x20x0.1875	69.0	Pass
L2	113 - 91.25	Pole	TP36.27x28.9012x0.25	66.1	Pass
L3	91.25 - 46.25	Pole	TP48.52x34.3529x0.3125	62.3	Pass
L4	46.25 - 0	Pole	TP61x45.9824x0.375	56.5	Pass
		Anchor Bolts	(16) 2.25" Ø w/ BC = 68"	42.5	Pass
		Base Plate	74" Ø x 2" thk.	38.9	Pass

**Table 4 - Maximum Base Reactions** 

Base Reactions	Current Analysis* (TIA/EIA-222-F)	Original Design (ANSI/TIA-222-G)
Axial	37 k	44 k
Shear	23 k	49 k
Moment	2.520 k-ft	5.150 k-ft

<sup>\*</sup>Foundation determined adequate per independent analysis.

#### **GENERAL COMMENTS**

This engineering analysis is based upon the theoretical capacity of the structure. It is not a condition assessment of the tower and its foundation. It is the responsibility of CTI Towers to verify that the tower modeled and analyzed is the correct structure (with accurate antenna loading information) modeled. If there are substantial modifications to be made or the assumptions made in this analysis are not accurate, FDH Engineering, Inc. should be notified immediately to perform a revised analysis.

#### **LIMITATIONS**

All opinions and conclusions are considered accurate to a reasonable degree of engineering certainty based upon the evidence available at the time of this report. All opinions and conclusions are subject to revision based upon receipt of new or additional/updated information. All services are provided exercising a level of care and diligence equivalent to the standard and care of our profession. No other warranty or guarantee, expressed or implied, is offered. Our services are confidential in nature and we will not release this report to any other party without the client's consent. The use of this engineering work is limited to the express purpose for which it was commissioned and it may not be reused, copied, or distributed for any other purpose without the written consent of FDH Engineering, Inc.

## **APPENDIX**

113.0 R  113			-		
22 22 22 22 22 22 22 22 22 22 22 22 22	Section	4	3	2	1
81 0 0000 00 00 00 00 00 00 00 00 00 00 0	Length (ft)	53.00	90.00	26.00	37.00
94840 00000 00000 00000 0000 0000 0000 0	Number of Sides		18	18	18
97 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Thickness (in)	0.3750	0.3125	0.2500	0.1875
113.0 R	Socket Length (ft)		6.75	5.00	4.25
000 6 6 7 113.0 ft	Top Dia (in)	45.9824	34.3529	28.9012	20.0000
913ft 13.0ft AXIAL 43 K  913ft 1. 2. 3. 4. 5.   92	Bot Dia (in)	61.0000	48.5200	36.2700	30.4800
113.0 ft  113.0 ft  113.0 ft  113.0 ft  AXIAL  43 K  SHEAR  5 K  TORQUE 0 kip-ft 38 mph WIND 0 x7500 in ICE AXIAL 31 K  SHEAR  23 K  TORQUE 1 kip-ft REACTIONS - 85 mph WIND	Grade		A572-65		
113.0 ft  AXIAL 46.3 ft  AXIAL 43 K  SHEAR TOROUE 0 kip-ft 38 mph WIND - 0.7500 in ICE AXIAL 31 K  SHEAR 23 K  MOME 25 20 k  TOROUE 1 kip-ft  TOROUE 1 kip-ft  TOROUE 1 kip-ft		10	6.0	2.3	1.9
(C)	REACTIONS - 85 mph WIND	AXIAL 43 K  SHEAR 5 K  TORQUE 0 kip-ft 38 mph WIND - 0.7500 in ICE AXIAL 31 K  SHEAR 23 K  MOMEN 2520 kip		APX APX  G A572  1	Ligh (2) E (2) F (

### **DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
Lightning Rod	150	APXVSPP18-C-A20 w/Mount Pipe	140
(2) BXA-70063/6CF w/ Mount Pipe	150	APXVTM14-C-120 w/Mount Pipe	140
(2) BXA-70063/6CF w/ Mount Pipe	150	APXVTM14-C-120 w/Mount Pipe	140
(2) BXA-70063/6CF w/ Mount Pipe	150	APXVTM14-C-120 w/Mount Pipe	140
(2) BXA-171063/12CF w/ Mount Pipe	150	800 MHz RRH	140
(2) BXA-171063/12CF w/ Mount Pipe	150	800 MHz RRH	140
(2) BXA-171063/12CF w/ Mount Pipe	150	800 MHz RRH	140
(2) RRH2X40-AWS	150	1900MHz RRH	140
(2) RRH2X40-AWS	150	1900MHz RRH	140
(2) RRH2X40-AWS	150	1900MHz RRH	140
(2) RRH2x40 LTE	150	TD-RRH8x20-25	140
(2) RRH2x40 LTE	150	TD-RRH8x20-25	140
(2) RRH2x40 LTE	150	TD-RRH8x20-25	140
24"x24"x10"	150	800 MHz 2x50W External Notch Filter	140
Platform With Handrails MNT	150	800 MHz 2x50W External Notch Filter	140
APXVSPP18-C-A20 w/Mount Pipe	140	800 MHz 2x50W External Notch Filter	140
APXVSPP18-C-A20 w/Mount Pipe	140	Platform With Handrails MNT	140

#### **MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

#### **TOWER DESIGN NOTES**

- Tower is located in New Haven County, Connecticut.

  Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.

  Tower is also designed for a 38 mph basic wind with 0.75 in ice. Ice is considered to ncrease in thickness with height.

  Deflections are based upon a 50 mph wind.

  TOWER RATING: 69%



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## **Tower Input Data**

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in New Haven County, Connecticut.

Basic wind speed of 85 mph.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 38 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

### **Options**

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification

- Use Code Stress Ratios
- Use Code Safety Factors Guys

Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform Assume Legs Pinned

- Assume Rigid Index Plate
- Use Clear Spans For Wind Area
- Use Clear Spans For KL/r Retension Guys To Initial Tension
- Bypass Mast Stability Checks
- Use Azimuth Dish Coefficients
- Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

- Consider Feedline Torque Include Angle Block Shear Check
  - Poles
- Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets

## **Tapered Pole Section Geometry**

Section	Elevation	Section	Splice	Number	Тор	Bottom	Wall	Bend	Pole Grade
		Length	Length	of	Diameter	Diameter	Thickness	Radius	
	ft	ft	ft	Sides	in	in	in	in	
L1	150.00-113.00	37.00	4.25	18	20.0000	30.4800	0.1875	0.7500	A572-65
									(65 ksi)
L2	113.00-91.25	26.00	5.00	18	28.9012	36.2700	0.2500	1.0000	A572-65
									(65 ksi)
L3	91.25-46.25	50.00	6.75	18	34.3529	48.5200	0.3125	1.2500	A572-65
									(65 ksi)
L4	46.25-0.00	53.00		18	45.9824	61.0000	0.3750	1.5000	A572-65
									(65 ksi)

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## **Tapered Pole Properties**

Section	Tip Dia.	Area	I	r	С	I/C	J	It/Q	w	w/t
	in	$in^2$	$in^4$	in	in	$in^3$	$in^4$	in <sup>2</sup>	in	
L1	20.3085	11.7909	584.7409	7.0334	10.1600	57.5532	1170.2512	5.8966	3.1900	17.013
	30.9502	18.0278	2090.0227	10.7538	15.4838	134.9809	4182.7954	9.0156	5.0345	26.851
L2	30.5702	22.7347	2357.8359	10.1712	14.6818	160.5956	4718.7742	11.3695	4.6466	18.586
	36.8295	28.5819	4685.0638	12.7871	18.4252	254.2753	9376.2923	14.2937	5.9435	23.774
L3	36.3214	33.7638	4942.8720	12.0844	17.4513	283.2383	9892.2479	16.8851	5.4961	17.588
	49.2685	47.8158	14039.0663	17.1137	24.6482	569.5787	28096.6055	23.9125	7.9895	25.566
L4	48.6339	54.2843	14265.3644	16.1906	23.3591	610.6988	28549.4996	27.1473	7.4329	19.821
	61.9410	72.1589	33506.6412	21.5219	30.9880	1081.2780	67057.3713	36.0863	10.0760	26.869

Tower	Gusset	Gusset	Gusset Grade	Adjust. Factor	Adjust.	Weight Mult.	Double Angle	Double Angle
Elevation	Area	Thickness		$A_f$	Factor		Stitch Bolt	Stitch Bolt
	(per face)				$A_r$		Spacing	Spacing
							Diagonals	Horizontals
ft	ft <sup>2</sup>	in					in	in
L1				1	1	1		
150.00-113.00								
L2				1	1	1		
113.00-91.25								
L3 91.25-46.25				1	1	1		
L4 46.25-0.00				1	1	1		

## Feed Line/Linear Appurtenances - Entered As Area

Description	Face or	Allow Shield	Component Type	Placement	Total Number		$C_A A_A$	Weight
	Leg		• •	ft			ft²/ft	plf
1-1/4"	С	No	Inside Pole	140.00 - 0.00	3	No Ice	0.00	0.66
						1/2" Ice	0.00	0.66
						1" Ice	0.00	0.66
						2" Ice	0.00	0.66
						4" Ice	0.00	0.66
.7''	C	No	Inside Pole	140.00 - 0.00	1	No Ice	0.00	0.47
						1/2" Ice	0.00	0.47
						1" Ice	0.00	0.47
						2" Ice	0.00	0.47
						4" Ice	0.00	0.47
**								
1-5/8"	C	No	Inside Pole	150.00 - 0.00	18	No Ice	0.00	1.04
						1/2" Ice	0.00	1.04
						1" Ice	0.00	1.04
						2" Ice	0.00	1.04
						4" Ice	0.00	1.04

## Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation	Face	$A_R$	$A_F$	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
Decitor	ft		$ft^2$	ft²	ft <sup>2</sup>	ft <sup>2</sup>	K
L1	150.00-113.00	A	0.000	0.000	0.000	0.000	0.00

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Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		$ft^2$	ft <sup>2</sup>	ft <sup>2</sup>	$ft^2$	K
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.76
L2	113.00-91.25	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.46
L3	91.25-46.25	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.95
L4	46.25-0.00	A	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.98

## Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	$ft^2$	$ft^2$	$ft^2$	$ft^2$	K
L1	150.00-113.00	A	0.884	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.76
L2	113.00-91.25	A	0.859	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.46
L3	91.25-46.25	A	0.818	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.95
L4	46.25-0.00	A	0.750	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.98

## **Feed Line Center of Pressure**

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
				Ice	Ice
	ft	in	in	in	in
L1	150.00-113.00	0.0000	0.0000	0.0000	0.0000
L2	113.00-91.25	0.0000	0.0000	0.0000	0.0000
L3	91.25-46.25	0.0000	0.0000	0.0000	0.0000
L4	46.25-0.00	0.0000	0.0000	0.0000	0.0000

## Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft	o	ft	ft²	ft <sup>2</sup>	K

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Description	Face or	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
	Leg		Lateral Vert ft ft	٥	ft		ft²	ft²	K
			ft						
Lightning Rod	С	From Leg	0.00	0.0000	150.00	No Ice	0.25	0.25	0.03
			0.00			1/2" Ice	0.66	0.66	0.03
			2.00			1" Ice 2" Ice	0.97 1.49	0.97 1.49	0.04 0.06
						4" Ice	2.68	2.68	0.06
**						1 100	2.00	2.00	0.11
(2) BXA-70063/6CF w/	A	From Leg	4.00	0.0000	150.00	No Ice	7.98	5.41	0.04
Mount Pipe			0.00			1/2" Ice	8.62	6.56	0.10
			0.00			1" Ice	9.23	7.42	0.17
						2" Ice	10.47	9.20	0.33
						4" Ice	13.08	12.95	0.79
(2) BXA-70063/6CF w/	В	From Leg	4.00	0.0000	150.00	No Ice	7.98	5.41	0.04
Mount Pipe			0.00			1/2" Ice	8.62	6.56	0.10
			0.00			1" Ice	9.23	7.42	0.17
						2" Ice	10.47	9.20	0.33
(2) DVA 70062/6CE/	C	E I	4.00	0.0000	150.00	4" Ice	13.08	12.95	0.79
(2) BXA-70063/6CF w/	С	From Leg	4.00 0.00	0.0000	150.00	No Ice 1/2" Ice	7.98 8.62	5.41 6.56	0.04 0.10
Mount Pipe			0.00			1/2 Ice 1" Ice	9.23	7.42	0.10
			0.00			2" Ice	10.47	9.20	0.17
						4" Ice	13.08	12.95	0.55
(2) BXA-171063/12CF w/	A	From Leg	4.00	0.0000	150.00	No Ice	5.03	5.29	0.79
Mount Pipe	11	Trom Leg	0.00	0.0000	150.00	1/2" Ice	5.58	6.46	0.04
Would Tipe			0.00			1" Ice	6.10	7.35	0.14
			0.00			2" Ice	7.17	9.15	0.27
						4" Ice	9.44	12.95	0.68
(2) BXA-171063/12CF w/	В	From Leg	4.00	0.0000	150.00	No Ice	5.03	5.29	0.04
Mount Pipe		· ·	0.00			1/2" Ice	5.58	6.46	0.09
•			0.00			1" Ice	6.10	7.35	0.14
						2" Ice	7.17	9.15	0.27
						4" Ice	9.44	12.95	0.68
(2) BXA-171063/12CF w/	C	From Leg	4.00	0.0000	150.00	No Ice	5.03	5.29	0.04
Mount Pipe			0.00			1/2" Ice	5.58	6.46	0.09
			0.00			1" Ice	6.10	7.35	0.14
						2" Ice	7.17	9.15	0.27
						4" Ice	9.44	12.95	0.68
(2) RRH2X40-AWS	A	From Leg	4.00	0.0000	150.00	No Ice	2.52	1.59	0.04
			0.00			1/2" Ice	2.75	1.80	0.06
			0.00			1" Ice	2.99	2.01	0.08
						2" Ice	3.50	2.46	0.13
(2) PRIJAVAO ANIG	ъ	Б. Т	4.00	0.0000	150.00	4" Ice	4.61	3.48	0.28
(2) RRH2X40-AWS	В	From Leg	4.00	0.0000	150.00	No Ice	2.52	1.59	0.04
			0.00			1/2" Ice 1" Ice	2.75 2.99	1.80	0.06
			0.00			2" Ice	3.50	2.01 2.46	0.08 0.13
						4" Ice	4.61	3.48	0.13
(2) RRH2X40-AWS	C	From Leg	4.00	0.0000	150.00	No Ice	2.52	1.59	0.28
(2) KKH274-0-71W3	C	1 Ioni Leg	0.00	0.0000	150.00	1/2" Ice	2.75	1.80	0.04
			0.00			1" Ice	2.99	2.01	0.08
			0.00			2" Ice	3.50	2.46	0.13
						4" Ice	4.61	3.48	0.13
(2) RRH2x40 LTE	A	From Leg	4.00	0.0000	150.00	No Ice	2.25	1.23	0.05
(=)	- •	228	0.00		3.00	1/2" Ice	2.45	1.39	0.07
			0.00			1" Ice	2.66	1.55	0.09
			=			2" Ice	3.10	1.91	0.13
						4" Ice	4.10	2.73	0.27
						- ICC	7.10		

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_AA_A$ Front	$C_AA_A$ Side	Weight
	Leg		Vert ft ft ft	۰	ft		ft <sup>2</sup>	ft²	K
			0.00			1/2" Ice	2.45	1.39	0.07
			0.00			1" Ice	2.66	1.55	0.09
						2" Ice	3.10	1.91	0.13
						4" Ice	4.10	2.73	0.27
(2) RRH2x40 LTE	С	From Leg	4.00	0.0000	150.00	No Ice	2.25	1.23	0.05
			0.00			1/2" Ice	2.45	1.39	0.07
			0.00			1" Ice	2.66	1.55	0.09
						2" Ice 4" Ice	3.10 4.10	1.91 2.73	0.13 0.27
24"x24"x10"	A	From Leg	4.00	0.0000	150.00	No Ice	5.60	2.73	0.27
24 X24 X10	А	110iii Leg	0.00	0.0000	150.00	1/2" Ice	5.92	2.56	0.04
			0.00			1" Ice	6.24	2.79	0.12
			0.00			2" Ice	6.91	3.28	0.21
						4" Ice	8.37	4.37	0.45
Platform With Handrails	С	None		0.0000	150.00	No Ice	33.03	33.03	1.71
MNT						1/2" Ice	44.60	44.60	2.19
						1" Ice	56.17	56.17	2.68
						2" Ice	79.31	79.31	3.65
**						4" Ice	125.59	125.59	5.58
APXVSPP18-C-A20		F I	4.00	0.0000	140.00	NI. I	8.50	6.95	0.08
w/Mount Pipe	A	From Leg	0.00	0.0000	140.00	No Ice 1/2" Ice	9.15	8.13	0.08
w/wount i ipc			0.00			1" Ice	9.77	9.02	0.13
			0.00			2" Ice	11.03	10.84	0.41
						4" Ice	13.68	14.85	0.91
APXVSPP18-C-A20	В	From Leg	4.00	0.0000	140.00	No Ice	8.50	6.95	0.08
w/Mount Pipe		, ,	0.00			1/2" Ice	9.15	8.13	0.15
•			0.00			1" Ice	9.77	9.02	0.23
						2" Ice	11.03	10.84	0.41
						4" Ice	13.68	14.85	0.91
APXVSPP18-C-A20	С	From Leg	4.00	0.0000	140.00	No Ice	8.50	6.95	0.08
w/Mount Pipe			0.00			1/2" Ice	9.15	8.13	0.15
			0.00			1" Ice	9.77	9.02	0.23
APXVTM14-C-120 w/Mount						2" Ice 4" Ice	11.03 13.68	10.84 14.85	0.41 0.91
	A	From Leg	4.00	0.0000	140.00	No Ice	7.13	4.96	0.91
Pipe	11	1 Ioni Leg	0.00	0.0000	140.00	1/2" Ice	7.66	5.75	0.13
			0.00			1" Ice	8.18	6.47	0.19
						2" Ice	9.26	8.01	0.34
						4" Ice	11.53	11.41	0.75
APXVTM14-C-120 w/Mount	В	From Leg	4.00	0.0000	140.00	No Ice	7.13	4.96	80.0
Pipe			0.00			1/2" Ice	7.66	5.75	0.13
			0.00			1" Ice	8.18	6.47	0.19
						2" Ice	9.26	8.01	0.34
ADVINTENTAL CLASS OF	C	Б. Т	4.00	0.0000	1.40.00	4" Ice	11.53	11.41	0.75
APXVTM14-C-120 w/Mount	С	From Leg	4.00	0.0000	140.00	No Ice	7.13	4.96	0.08
Pipe			0.00 0.00			1/2" Ice 1" Ice	7.66 8.18	5.75 6.47	0.13 0.19
			0.00			2" Ice	9.26	8.01	0.19
						4" Ice	11.53	11.41	0.75
800 MHz RRH	A	From Leg	4.00	0.0000	140.00	No Ice	2.49	2.07	0.75
		2-6	0.00		2 0	1/2" Ice	2.71	2.27	0.07
			0.00			1" Ice	2.93	2.48	0.10
						2" Ice	3.41	2.93	0.16
						4" Ice	4.46	3.93	0.32
800 MHz RRH	В	From Leg	4.00	0.0000	140.00	No Ice	2.49	2.07	0.05
			0.00			1/2" Ice	2.71	2.27	0.07

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Client	CTI Towers	Designed by Cary Webb

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weigh
			Vert ft ft	٥	ft		ft²	ft²	K
			ft					- 10	
			0.00			1" Ice	2.93	2.48	0.10
						2" Ice	3.41	2.93	0.16
000 MI DDII	0	г т	4.00	0.0000	1.40.00	4" Ice	4.46	3.93	0.32
800 MHz RRH	C	From Leg	4.00	0.0000	140.00	No Ice	2.49	2.07	0.05
			0.00			1/2" Ice 1" Ice	2.71 2.93	2.27 2.48	0.07
			0.00			2" Ice	3.41	2.48	0.10 0.16
						4" Ice	4.46	3.93	0.10
1900MHz RRH	Α.	Enom Loo	4.00	0.0000	140.00	No Ice	2.70	3.93 2.77	0.32
1900MHZ RRH	A	From Leg	0.00	0.0000	140.00	1/2" Ice	2.70	3.01	0.08
			0.00			1" Ice	3.18	3.26	0.08
			0.00			2" Ice	3.70	3.78	0.11
						4" Ice	4.85	4.93	0.18
1900MHz RRH	В	From Leg	4.00	0.0000	140.00	No Ice	2.70	2.77	0.06
1900WIIIZ KKII	ь	110III Leg	0.00	0.0000	140.00	1/2" Ice	2.70	3.01	0.08
			0.00			1" Ice	3.18	3.26	0.00
			0.00			2" Ice	3.70	3.78	0.11
						4" Ice	4.85	4.93	0.35
1900MHz RRH	C	From Leg	4.00	0.0000	140.00	No Ice	2.70	2.77	0.06
	_		0.00			1/2" Ice	2.94	3.01	0.08
			0.00			1" Ice	3.18	3.26	0.11
						2" Ice	3.70	3.78	0.18
						4" Ice	4.85	4.93	0.35
TD-RRH8x20-25	A	From Leg	4.00	0.0000	140.00	No Ice	4.72	1.70	0.07
			0.00			1/2" Ice	5.01	1.92	0.10
			0.00			1" Ice	5.32	2.14	0.13
						2" Ice	5.95	2.62	0.20
						4" Ice	7.31	3.68	0.40
TD-RRH8x20-25	В	From Leg	4.00	0.0000	140.00	No Ice	4.72	1.70	0.07
			0.00			1/2" Ice	5.01	1.92	0.10
			0.00			1" Ice	5.32	2.14	0.13
						2" Ice	5.95	2.62	0.20
	~					4" Ice	7.31	3.68	0.40
TD-RRH8x20-25	C	From Leg	4.00	0.0000	140.00	No Ice	4.72	1.70	0.07
			0.00			1/2" Ice	5.01	1.92	0.10
			0.00			1" Ice	5.32	2.14	0.13
						2" Ice 4" Ice	5.95	2.62	0.20
	Α.	Enom Loo	4.00	0.0000	140.00	No Ice	7.31 0.78	3.68 0.29	0.40 0.01
800 MHz 2x50W External Notch Filter	A	From Leg	0.00	0.0000	140.00	1/2" Ice	0.78	0.29	0.01
			0.00			1" Ice	1.03	0.38	0.01
			0.00			2" Ice	1.31	0.48	0.02
						4" Ice	1.99	1.24	0.10
00 MHz 2x50W External	В	From Leg	4.00	0.0000	140.00	No Ice	0.78	0.29	0.01
Notch Filter	ь	Trom Leg	0.00	0.0000	110.00	1/2" Ice	0.90	0.38	0.01
			0.00			1" Ice	1.03	0.48	0.02
			0.00			2" Ice	1.31	0.70	0.04
						4" Ice	1.99	1.24	0.10
800 MHz 2x50W External Notch Filter	C	From Leg	4.00	0.0000	140.00	No Ice	0.78	0.29	0.01
		3	0.00			1/2" Ice	0.90	0.38	0.01
			0.00			1" Ice	1.03	0.48	0.02
						2" Ice	1.31	0.70	0.04
						4" Ice	1.99	1.24	0.10
Platform With Handrails MNT	C	None		0.0000	140.00	No Ice	33.03	33.03	1.71
						1/2" Ice	44.60	44.60	2.19
						1" Ice	56.17	56.17	2.68
						2" Ice	79.31	79.31	3.65

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	CTI Towers	Cary Webb

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_AA_A$ Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft	o	ft		ft <sup>2</sup>	ft <sup>2</sup>	K
**						4" Ice	125.59	125.59	5.58

## **Load Combinations**

Comb.	Description
No.	
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

## **Maximum Member Forces**

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	CTI Towers	Cary Webb

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axi Moment kip-ft
L1	150 - 113	Pole	Max Tension	14	0.00	-0.00	-0.00
	150 110	1 0.0	Max. Compression	14	-13.38	0.03	0.53
			Max. Mx	11	-7.03	356.59	0.17
			Max. My	2	-7.01	0.02	362.04
			Max. Vy	11	-13.48	356.59	0.17
			Max. Vx	2	-13.64	0.02	362.04
			Max. Torque	11			-0.55
L2	113 - 91.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-16.75	0.03	0.53
			Max. Mx	11	-9.65	656.11	0.18
			Max. My	2	-9.64	0.02	664.97
			Max. Vy	11	-15.06	656.11	0.18
			Max. Vx	2	-15.22	0.02	664.97
			Max. Torque	5			0.55
L3	91.25 - 46.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-26.06	0.03	0.53
			Max. Mx	11	-17.20	1385.47	0.19
			Max. My	2	-17.19	0.02	1401.34
			Max. Vy	11	-18.69	1385.47	0.19
			Max. Vx	2	-18.85	0.02	1401.34
			Max. Torque	5			0.55
L4	46.25 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-42.66	0.03	0.53
			Max. Mx	11	-31.18	2495.44	0.19
			Max. My	2	-31.18	0.02	2519.79
			Max. Vy	11	-23.25	2495.44	0.19
			Max. Vx	2	-23.41	0.02	2519.79
			Max. Torque	5			0.55

## **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, 2
		Load	K	K	K
		Comb.			
Pole	Max. Vert	14	42.66	-0.00	-0.00
	$Max. H_x$	11	31.19	23.23	0.00
	$Max. H_z$	2	31.19	0.00	23.39
	$Max. M_x$	2	2519.79	0.00	23.39
	$Max. M_z$	5	2495.40	-23.23	0.00
	Max. Torsion	5	0.55	-23.23	0.00
	Min. Vert	2	31.19	0.00	23.39
	Min. H <sub>x</sub>	5	31.19	-23.23	0.00
	Min. H <sub>z</sub>	8	31.19	0.00	-23.39
	$Min. M_x$	8	-2519.41	0.00	-23.39
	$Min. M_z$	11	-2495.44	23.23	0.00
	Min. Torsion	11	-0.55	23.23	0.00

## **Tower Mast Reaction Summary**

Load Combination	Vertical	$Shear_x$	$Shear_z$	Overturning $Moment, M_x$	Overturning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	31.19	0.00	-0.00	-0.18	0.02	0.00

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Load	Vertical	Shear <sub>x</sub>	$Shear_z$	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, $M_z$	
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 0 deg - No Ice	31.19	0.00	-23.39	-2519.79	0.02	-0.01
Dead+Wind 30 deg - No Ice	31.19	11.62	-20.26	-2182.36	-1247.75	-0.28
Dead+Wind 60 deg - No Ice	31.19	20.12	-11.70	-1260.08	-2161.20	-0.48
Dead+Wind 90 deg - No Ice	31.19	23.23	-0.00	-0.19	-2495.40	-0.55
Dead+Wind 120 deg - No Ice	31.19	20.12	11.70	1259.70	-2161.19	-0.47
Dead+Wind 150 deg - No Ice	31.19	11.62	20.26	2181.99	-1247.74	-0.27
Dead+Wind 180 deg - No Ice	31.19	0.00	23.39	2519.41	0.02	0.01
Dead+Wind 210 deg - No Ice	31.19	-11.62	20.26	2181.99	1247.79	0.28
Dead+Wind 240 deg - No Ice	31.19	-20.12	11.70	1259.70	2161.24	0.48
Dead+Wind 270 deg - No Ice	31.19	-23.23	-0.00	-0.19	2495.44	0.55
Dead+Wind 300 deg - No Ice	31.19	-20.12	-11.70	-1260.08	2161.24	0.47
Dead+Wind 330 deg - No Ice	31.19	-11.62	-20.26	-2182.36	1247.79	0.26
Dead+Ice+Temp	42.66	0.00	0.00	-0.53	0.03	0.00
Dead+Wind 0 deg+Ice+Temp	42.66	0.00	-5.40	-619.21	0.03	-0.01
Dead+Wind 30 deg+Ice+Temp	42.66	2.68	-4.68	-536.33	-306.75	-0.07
Dead+Wind 60 deg+Ice+Temp	42.66	4.65	-2.70	-309.89	-531.34	-0.12
Dead+Wind 90 deg+Ice+Temp	42.66	5.37	0.00	-0.57	-613.54	-0.13
Dead+Wind 120 deg+Ice+Temp	42.66	4.65	2.70	308.74	-531.34	-0.11
Dead+Wind 150 deg+Ice+Temp	42.66	2.68	4.68	535.18	-306.75	-0.06
Dead+Wind 180 deg+Ice+Temp	42.66	0.00	5.40	618.06	0.03	0.01
Dead+Wind 210 deg+Ice+Temp	42.66	-2.68	4.68	535.18	306.81	0.07
Dead+Wind 240 deg+Ice+Temp	42.66	-4.65	2.70	308.74	531.40	0.12
Dead+Wind 270 deg+Ice+Temp	42.66	-5.37	0.00	-0.57	613.60	0.13
Dead+Wind 300 deg+Ice+Temp	42.66	-4.65	-2.70	-309.89	531.40	0.11
Dead+Wind 330 deg+Ice+Temp	42.66	-2.68	-4.68	-536.33	306.81	0.06
Dead+Wind 0 deg - Service	31.19	0.00	-8.09	-872.52	0.02	-0.00
Dead+Wind 30 deg - Service	31.19	4.02	-7.01	-755.74	-432.00	-0.10
Dead+Wind 60 deg - Service	31.19	6.96	-4.05	-436.41	-748.26	-0.17
Dead+Wind 90 deg - Service	31.19	8.04	0.00	-0.19	-863.92	-0.19
Dead+Wind 120 deg - Service	31.19	6.96	4.05	436.03	-748.26	-0.16
Dead+Wind 150 deg - Service	31.19	4.02	7.01	755.36	-432.00	-0.09
Dead+Wind 180 deg - Service	31.19	0.00	8.09	872.14	0.02	0.00
Dead+Wind 210 deg - Service	31.19	-4.02	7.01	755.36	432.04	0.10
Dead+Wind 240 deg - Service	31.19	-6.96	4.05	436.03	748.31	0.17
Dead+Wind 270 deg - Service	31.19	-8.04	0.00	-0.19	863.97	0.19
Dead+Wind 300 deg - Service	31.19	-6.96	-4.05	-436.41	748.31	0.16
Dead+Wind 330 deg - Service	31.19	-4.02	-7.01	-755.74	432.04	0.09

# **Solution Summary**

	Sui	n of Applied Force.	S		Sum of Reaction	ıs	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-31.19	0.00	0.00	31.19	0.00	0.000%
2	0.00	-31.19	-23.39	0.00	31.19	23.39	0.003%
3	11.62	-31.19	-20.26	-11.62	31.19	20.26	0.000%
4	20.12	-31.19	-11.70	-20.12	31.19	11.70	0.000%
5	23.23	-31.19	0.00	-23.23	31.19	0.00	0.003%
6	20.12	-31.19	11.70	-20.12	31.19	-11.70	0.000%
7	11.62	-31.19	20.26	-11.62	31.19	-20.26	0.000%
8	0.00	-31.19	23.39	0.00	31.19	-23.39	0.003%
9	-11.62	-31.19	20.26	11.62	31.19	-20.26	0.000%
10	-20.12	-31.19	11.70	20.12	31.19	-11.70	0.000%
11	-23.23	-31.19	0.00	23.23	31.19	0.00	0.003%
12	-20.12	-31.19	-11.70	20.12	31.19	11.70	0.000%
13	-11.62	-31.19	-20.26	11.62	31.19	20.26	0.000%
14	0.00	-42.66	0.00	-0.00	42.66	-0.00	0.000%
15	0.00	-42.66	-5.40	-0.00	42.66	5.40	0.000%

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	Sui	m of Applied Forces	3				
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
16	2.69	-42.66	-4.68	-2.68	42.66	4.68	0.000%
17	4.65	-42.66	-2.70	-4.65	42.66	2.70	0.000%
18	5.37	-42.66	0.00	-5.37	42.66	-0.00	0.000%
19	4.65	-42.66	2.70	-4.65	42.66	-2.70	0.000%
20	2.69	-42.66	4.68	-2.68	42.66	-4.68	0.000%
21	0.00	-42.66	5.40	-0.00	42.66	-5.40	0.000%
22	-2.69	-42.66	4.68	2.68	42.66	-4.68	0.000%
23	-4.65	-42.66	2.70	4.65	42.66	-2.70	0.000%
24	-5.37	-42.66	0.00	5.37	42.66	-0.00	0.000%
25	-4.65	-42.66	-2.70	4.65	42.66	2.70	0.000%
26	-2.69	-42.66	-4.68	2.68	42.66	4.68	0.000%
27	0.00	-31.19	-8.09	-0.00	31.19	8.09	0.004%
28	4.02	-31.19	-7.01	-4.02	31.19	7.01	0.001%
29	6.96	-31.19	-4.05	-6.96	31.19	4.05	0.001%
30	8.04	-31.19	0.00	-8.04	31.19	-0.00	0.004%
31	6.96	-31.19	4.05	-6.96	31.19	-4.05	0.001%
32	4.02	-31.19	7.01	-4.02	31.19	-7.01	0.001%
33	0.00	-31.19	8.09	-0.00	31.19	-8.09	0.004%
34	-4.02	-31.19	7.01	4.02	31.19	-7.01	0.001%
35	-6.96	-31.19	4.05	6.96	31.19	-4.05	0.001%
36	-8.04	-31.19	0.00	8.04	31.19	-0.00	0.004%
37	-6.96	-31.19	-4.05	6.96	31.19	4.05	0.001%
38	-4.02	-31.19	-7.01	4.02	31.19	7.01	0.001%

## **Non-Linear Convergence Results**

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	13	0.00003886	0.00006834
3	Yes	16	0.00000001	0.00008889
4	Yes	16	0.00000001	0.00009048
5	Yes	13	0.00003889	0.00008245
6	Yes	16	0.00000001	0.00008806
7	Yes	16	0.00000001	0.00009023
8	Yes	13	0.00003886	0.00006832
9	Yes	16	0.00000001	0.00009029
10	Yes	16	0.00000001	0.00008804
11	Yes	13	0.00003889	0.00008245
12	Yes	16	0.00000001	0.00009046
13	Yes	16	0.00000001	0.00008895
14	Yes	6	0.00000001	0.00000001
15	Yes	14	0.00000001	0.00008209
16	Yes	14	0.00000001	0.00009849
17	Yes	14	0.00000001	0.00009846
18	Yes	14	0.00000001	0.00008113
19	Yes	14	0.00000001	0.00009765
20	Yes	14	0.00000001	0.00009824
21	Yes	14	0.00000001	0.00008168
22	Yes	14	0.00000001	0.00009828
23	Yes	14	0.00000001	0.00009767
24	Yes	14	0.00000001	0.00008115
25	Yes	14	0.00000001	0.00009847
26	Yes	14	0.00000001	0.00009853
27	Yes	12	0.00010731	0.00008397
28	Yes	13	0.00000001	0.00008322

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29	Yes	13	0.00000001	0.00008844
30	Yes	12	0.00010727	0.00008487
31	Yes	13	0.00000001	0.00008116
32	Yes	13	0.0000001	0.00008726
33	Yes	12	0.00010729	0.00008387
34	Yes	13	0.0000001	0.00008743
35	Yes	13	0.00000001	0.00008112
36	Yes	12	0.00010728	0.00008488
37	Yes	13	0.00000001	0.00008838
38	Yes	13	0.00000001	0.00008337

## **Maximum Tower Deflections - Service Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
L1	150 - 113	23.336	27	1.6135	0.0032
L2	117.25 - 91.25	13.243	27	1.2218	0.0009
L3	96.25 - 46.25	8.478	27	0.9201	0.0005
L4	53 - 0	2.362	27	0.4194	0.0002

## Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	in	٥	۰	ft
150.00	Lightning Rod	27	23.336	1.6135	0.0032	19449
140.00	APXVSPP18-C-A20 w/Mount Pipe	27	20.054	1.5018	0.0023	9724

## **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	٥	0
L1	150 - 113	67.290	2	4.6507	0.0091
L2	117.25 - 91.25	38.211	2	3.5246	0.0027
L3	96.25 - 46.25	24.468	2	2.6553	0.0015
L4	53 - 0	6.820	2	1.2108	0.0005

## Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
150.00	Lightning Rod	2	67.290	4.6507	0.0091	6826
140.00	APXVSPP18-C-A20 w/Mount Pipe	2	57.836	4.3298	0.0068	3412

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Client	Designed by
CTI Towers	Cary Webb

# Compression Checks

No. $\frac{f}{f}$ $\frac{f}{f}$ $\frac{f}{f}$ $\frac{f}{f}$ $\frac{f}{f}$ $\frac{f}{f}$ $\frac{h}{h}$				Pol	e Des	sign D	ata				
fr	Section	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A			Ratio
The content of the	No.	Č.		C.	C.		, .	. 2			<i>P</i>
148.276											
146.553	L1		TP30.48x20x0.1875	37.00	0.00	0.0					
146.553							39.000	12.3720	-2.47	482.51	0.00
144 829 144 829 143 105 143 105 143 105 141 1382							39.000	12.6626	-2.57	493.84	0.00
143.105 143.105 141.382 141.487 141.488 141.48											
143.105 - 141.382   39.000   13.2437   2.79   516.50   0.00   141.382   39.000   13.5342   -5.27   527.84   0.01   139.658   39.000   13.8248   -5.38   539.17   0.01   137.934   39.000   14.1153   -5.50   550.50   0.01   136.211   36.211   39.000   14.4059   -5.62   561.83   0.01   134.487   39.000   14.4059   -5.62   561.83   0.01   132.763   39.000   14.6964   -5.75   573.16   0.01   132.763   39.000   14.9870   -5.88   584.49   0.01   131.039   39.000   15.2776   -6.01   595.83   0.01   129.316   39.000   15.5681   -6.15   607.16   0.01   127.592   39.000   15.5681   -6.15   607.16   0.01   127.592   123.868   125.868   39.000   16.1492   -6.42   629.82   0.01   124.145   39.000   16.4398   -6.57   641.15   0.01   124.145   39.000   16.7303   -6.71   652.48   0.01   120.697   131.974   118.974   38.433   17.3114   -7.01   665.33   0.01   117.25   113   TP36.27x28.9012x0.25   26.00   0.00   0.0   39.000   23.9260   -7.81   933.11   0.00   110.906   110.906   39.000   24.3968   -8.05   951.48   0.00   110.906   110.906   39.000   24.3968   -8.05   951.48   0.00   110.9859   109.							39.000	12.9531	-2.68	505.17	0.00
141382 141382 141382 141382 139.658 139.658 139.658 137.934 137.934 137.934 136.211 136.211 136.211 136.211 136.211 136.211 136.211 137.763 139.000 14.4059 15.62 15.75 157.316 0.01 132.763 132.763 131.039 130.000 15.2776 6.01 595.83 0.01 122.316 0.01 127.592 0.01 127.592 127.592 0.01 128.68 0.01 129.316 0.01 127.592 0.01 120.697 120.697 120.697 138.744 118.974 119.93							20.000	10.0105	2.50	516.50	0.00
141382							39.000	13.2437	-2.79	516.50	0.00
139.658   136.658   39.000   13.8248   -5.38   539.17   0.01   137.934   39.000   14.1153   -5.50   550.50   0.01   137.934   39.000   14.1153   -5.50   550.50   0.01   136.211   36.211   39.000   14.4059   -5.62   561.83   0.01   134.487   39.000   14.6964   -5.75   573.16   0.01   132.763   39.000   14.9870   -5.88   584.49   0.01   132.763   39.000   15.2776   -6.01   595.83   0.01   131.039   39.000   15.2776   -6.01   595.83   0.01   127.592   39.000   15.5681   -6.15   607.16   0.01   127.592   127.592   39.000   15.8587   -6.28   618.49   0.01   125.868   124.145   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   122.421   127.592   38.734   17.0209   -6.86   659.12   0.01   118.974   118.974   118.974   118.974   118.974   119.53   117.25   113   TP36.27x28.9012x0.25   26.00   0.00   0.0   39.000   23.9050   -4.35   23.39   0.00   10.9859   109.859   10							39,000	13 53/12	5 27	527.84	0.01
139.658							37.000	13.3342	-5.21	321.04	0.01
137.934							39.000	13.8248	-5.38	539.17	0.01
136.211											
136,211 -   39,000							39.000	14.1153	-5.50	550.50	0.01
134.487 134.487 134.487 132.763 132.763 132.763 131.039 131.039 131.039 129.316 120.412 121.592 121.592 122.592 127.592 121.5988 125.868 125.868 125.868 125.868 125.868 125.868 125.868 126.368 127.368 128.39000 16.1492 6.42 629.82 0.01 120.697 120.697 120.697 120.697 120.697 120.697 120.697 120.697 120.697 120.697 120.697 120.597 120.597 120.597 120.597 138.714 118.974 117.25 117.25 117.25 117.25 117.25 117.25 117.25 119.30 117.25 110.906 110.906 110.906 110.906 110.906 110.906 110.906 110.905 110.813 108.813 107.766 107.766 107.766 107.766 107.766 107.766 107.766							20,000	14 4050	5.62	561 92	0.01
134,487							39.000	14.4039	-3.02	301.03	0.01
132.763 -   39.000   14.9870   -5.88   584.49   0.01							39.000	14.6964	-5.75	573.16	0.01
131.039											
131,039 - 129,316							39.000	14.9870	-5.88	584.49	0.01
129.316 129.316 129.316 129.316 127.592 127.592 125.868 125.868 125.868 125.868 125.869 124.145 124.145 124.145 122.421 122.421 1120.697 120.697 1218.974 118.974 118.974 118.974 118.974 118.974 118.975 117.25 - 113 17.3113 17.3114 18.974 119.53 117.25 - 113 17.3113 17.3114 18.974 119.953 110.906 110.906 110.906 110.906 110.906 110.906 110.9859 109.859 - 109.859 - 109.859 - 109.859 - 109.859 - 109.859 - 109.859 - 107.766 107.766 107.766 107.766 - 107.766 107.766 - 107.766 107.766 -							20,000	15 2776	6.01	505.02	0.01
129.316 - 127.592 - 39.000 15.5681 -6.15 607.16 0.01 127.592 - 125.868 125.868 - 39.000 15.8587 -6.28 618.49 0.01 125.868 125.868 - 39.000 16.1492 -6.42 629.82 0.01 124.145 124.145 - 39.000 16.4398 -6.57 641.15 0.01 122.421 122.421 120.697 120.697 120.697 118.974 118.974 118.974 117.25 113 TP36.27x28.9012x0.25 26.00 0.00 0.0 39.000 23.6905 -4.35 923.93 0.00 113 -111.953 - 110.906 110.906 110.906 110.906 110.906 110.906 109.859 109.859 109.859 - 108.813 108.813 - 107.766 100.7166 107.766 100.7166 107.766 107.766 100.7169							39.000	15.2776	-0.01	393.83	0.01
127.592							39.000	15.5681	-6.15	607.16	0.01
125.868 125.868 124.145 124.145 124.145 122.421 122.421 120.697 120.697 118.974 118.974 1117.25 117.25 - 113 129.697 120.697 110.906 110.906 110.906 110.906 110.906 110.906 110.906 110.905 108.813 108.813 108.813 108.813 108.813 107.766											
125.868 - 124.145 - 24.145 - 24.145 - 24.145 - 122.421 - 24.145 -							39.000	15.8587	-6.28	618.49	0.01
124.145 124.145 -							20.000	161100	ć 10	(20.02	0.01
124.145 - 122.421 - 39.000 16.4398 -6.57 641.15 0.01 122.421 - 39.000 16.7303 -6.71 652.48 0.01 120.697 - 38.724 17.0209 -6.86 659.12 0.01 118.974 - 117.25 - 113							39.000	16.1492	-6.42	629.82	0.01
122.421 122.421 120.697 120.697 118.974 118.974 117.25 117.25 - 113 12							39 000	16 4398	-6.57	641 15	0.01
122.421 - 39.000 16.7303 -6.71 652.48 0.01 120.697 120.697 - 38.724 17.0209 -6.86 659.12 0.01 118.974 118.974 - 38.433 17.3114 -7.01 665.33 0.01 117.25 113 TP36.27x28.9012x0.25 26.00 0.00 0.0 39.000 23.6905 -4.35 923.93 0.00 113 - 111.953 - 39.000 24.1614 -7.93 942.29 0.00 110.906 110.906 110.906 110.906 110.906 110.9859 109.859 - 108.813 108.813 - 107.766 107.766 107.766 107.766 107.766 106.719							27.000	10.1570	0.57	011.13	0.01
120.697 - 118.974 118.974 118.974 117.25 - 113 122 - 113 123 - 111.953 111.953 - 110.906 110.906 110.906 - 109.859 - 108.813 108.813 - 107.766 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 107.766 - 106.719							39.000	16.7303	-6.71	652.48	0.01
118.974 118.974 117.25 117.25 - 113 12											
118.974 - 117.25 117.25 - 113 12							38.724	17.0209	-6.86	659.12	0.01
117.25 117.25 - 113 12							38 /33	17 3114	7.01	665 33	0.01
117.25 - 113 L2 117.25 - 113 TP36.27x28.9012x0.25 26.00 0.00 0.0 39.000 23.6905 -4.35 923.93 0.00 113 - 111.953 39.000 23.9260 -7.81 933.11 0.00 110.906 110.906 1109.859 39.000 24.3968 -8.05 951.48 0.00 108.813 108.813 - 107.766 107.766 - 106.719							30.433	17.5114	7.01	005.55	0.01
113 - 111.953       39.000       23.9260       -7.81       933.11       0.00         111.953 -       39.000       24.1614       -7.93       942.29       0.00         110.906       39.000       24.3968       -8.05       951.48       0.00         109.859       39.000       24.6322       -8.16       960.66       0.00         108.813       39.000       24.8677       -8.28       969.84       0.00         107.766       39.000       25.1031       -8.40       979.02       0.00         106.719		117.25 - 113					37.714	18.0278	-3.34	679.90	0.00
111.953 - 39.000 24.1614 -7.93 942.29 0.00 110.906 110.906 - 39.000 24.3968 -8.05 951.48 0.00 109.859 - 39.000 24.6322 -8.16 960.66 0.00 108.813 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719	L2		TP36.27x28.9012x0.25	26.00	0.00	0.0					0.00
110.906 110.906 - 39.000 24.3968 -8.05 951.48 0.00 109.859 - 39.000 24.6322 -8.16 960.66 0.00 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719											
110.906 - 39.000 24.3968 -8.05 951.48 0.00 109.859 109.859 - 39.000 24.6322 -8.16 960.66 0.00 108.813 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 107.766 39.000 25.1031 -8.40 979.02 0.00 106.719							39.000	24.1614	-7.93	942.29	0.00
109.859 109.859 - 39.000 24.6322 -8.16 960.66 0.00 108.813 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719							39,000	24 3968	8.05	951 48	0.00
109.859 - 39.000 24.6322 -8.16 960.66 0.00 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719							37.000	27.5700	-0.03	751.10	0.00
108.813 108.813 - 39.000 24.8677 -8.28 969.84 0.00 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719							39.000	24.6322	-8.16	960.66	0.00
107.766 107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719											
107.766 - 39.000 25.1031 -8.40 979.02 0.00 106.719							39.000	24.8677	-8.28	969.84	0.00
106.719							20,000	25 1021	0 40	070.02	0.00
							39.000	23.1031	-0.40	9/9.02	0.00
		106.719 -					39.000	25.3385	-8.52	988.20	0.00

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Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. $P_a$	Ratio P
110.	ft		ft	ft		ksi	$in^2$	K	K	$P_a$
	105.672					20.000	25.57.40	0.64	007.00	0.000
	105.672 - 104.625					39.000	25.5740	-8.64	997.38	0.009
	104.625 -					39.000	25.8094	-8.76	1006.57	0.009
	103.578									
	103.578 -					39.000	26.0448	-8.88	1015.75	0.009
	102.531 102.531 -					39.000	26.2803	-9.01	1024.93	0.009
	102.331 -					39.000	20.2603	-9.01	1024.93	0.009
	101.484 -					39.000	26.5157	-9.13	1034.11	0.009
	100.438					20.000	0 ( 5511	0.26	10.10.20	0.000
	100.438 - 99.3906					39.000	26.7511	-9.26	1043.29	0.009
	99.3906 -					39.000	26.9866	-9.38	1052.48	0.009
	98.3438					271000	20,5000	,,,,	1002110	0.005
	98.3438 -					39.000	27.2220	-9.51	1061.66	0.009
	97.2969					20,000	27 4574	0.64	1070.04	0.000
	97.2969 - 96.25 96.25 - 91.25					39.000 39.000	27.4574 28.5819	-9.64 -4.87	1070.84 1114.69	0.009 0.004
L3	96.25 - 91.25	TP48.52x34.3529x0.3125	50.00	0.00	0.0	39.000	35.1690	-4.87 -5.94	1371.59	0.004
LJ	91.25 - 89.125	1146.32834.332980.3123	30.00	0.00	0.0	39.000	35.7663	-11.13	1394.88	0.004
	89.125 - 87					39.000				
							36.3635	-11.45	1418.18	0.008
	87 - 84.875					39.000	36.9607	-11.77	1441.47	0.008
	84.875 - 82.75					39.000	37.5579	-12.10	1464.76	0.008
	82.75 - 80.625					39.000	38.1551	-12.43	1488.05	0.008
	80.625 - 78.5					39.000	38.7523	-12.77	1511.34	0.008
	78.5 - 76.375					39.000	39.3495	-13.12	1534.63	0.009
	76.375 - 74.25					39.000	39.9467	-13.46	1557.92	0.009
	74.25 - 72.125					39.000	40.5439	-13.81	1581.21	0.009
	72.125 - 70					39.000	41.1411	-14.17	1604.50	0.009
	70 - 67.875					39.000	41.7383	-14.53	1627.80	0.009
	67.875 - 65.75					39.000	42.3355	-14.90	1651.09	0.009
	65.75 - 63.625					39.000	42.9328	-15.27	1674.38	0.009
	63.625 - 61.5					39.000	43.5300	-15.64	1697.67	0.009
	61.5 - 59.375					39.000	44.1272	-16.02	1720.96	0.009
	59.375 - 57.25					39.000	44.7244	-16.41	1744.25	0.009
	57.25 - 55.125					39.000	45.3216	-16.80	1767.54	0.010
	55.125 - 53					39.000	45.9188	-17.19	1790.83	0.010
	53 - 46.25					38.531	47.8158	-9.06	1842.39	0.005
L4	53 - 46.25	TP61x45.9824x0.375	53.00	0.00	0.0	39.000	56.5607	-10.64	2205.87	0.005
	46.25 - 43.8158					39.000	57.3817	-20.24	2237.89	0.009
	43.8158 -					39.000	58.2027	-20.79	2269.90	0.009
	41.3816									
	41.3816 -					39.000	59.0236	-21.35	2301.92	0.009
	38.9474									
	38.9474 -					39.000	59.8446	-21.91	2333.94	0.009
	36.5132					20.000	60.6655	22.40	2265.06	0.010
	36.5132 -					39.000	60.6655	-22.48	2365.96	0.010
	34.0789 34.0789 -					39.000	61.4865	-23.06	2397.97	0.010
	31.6447					39.000	01.4603	-23.00	2391.91	0.010
	31.6447 -					39.000	62.3074	-23.64	2429.99	0.010
	29.2105									
	29.2105 -					39.000	63.1284	-24.23	2462.01	0.010
	26.7763									
	26.7763 -					39.000	63.9493	-24.83	2494.02	0.010
	24.3421									
	24.3421 -					39.000	64.7703	-25.43	2526.04	0.010
	21.9079									
	21.9079 -					39.000	65.5913	-26.04	2558.06	0.010

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Client		Designed by
	CTI Towers	Cary Webb

Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	$Allow. \ P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	K	K	$P_a$
	19.4737									
	19.4737 -					39.000	66.4122	-26.66	2590.08	0.010
	17.0395									
	17.0395 -					38.938	67.2332	-27.29	2617.90	0.010
	14.6053									
	14.6053 -					38.732	68.0541	-27.92	2635.85	0.011
	12.1711									
	12.1711 -					38.526	68.8751	-28.56	2653.47	0.011
	9.73684									
	9.73684 -					38.320	69.6960	-29.20	2670.74	0.011
	7.30263									
	7.30263 -					38.114	70.5170	-29.86	2687.68	0.011
	4.86842									
	4.86842 -					37.908	71.3380	-30.52	2704.28	0.011
	2.43421									
	2.43421 - 0					37.702	72.1589	-31.18	2720.54	0.011

Pole Bending Des	sign Data
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Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.			$M_{\scriptscriptstyle X}$	$f_{bx}$	$F_{bx}$	$f_{bx}$	$M_{y}$	$f_{by}$	$F_{by}$	$f_{by}$
	ft		kip-ft	ksi	ksi	$F_{bx}$	kip-ft	ksi	ksi	$F_{by}$
L1	150 - 148.276	TP30.48x20x0.1875	11.67	2.317	39.000	0.059	0.00	0.000	39.000	0.000
	148.276 -		23.30	4.411	39.000	0.113	0.00	0.000	39.000	0.000
	146.553									
	146.553 -		35.11	6.343	39.000	0.163	0.00	0.000	39.000	0.000
	144.829									
	144.829 -		47.10	8.130	39.000	0.208	0.00	0.000	39.000	0.000
	143.105									
	143.105 -		59.26	9.784	39.000	0.251	0.00	0.000	39.000	0.000
	141.382									
	141.382 -		73.30	11.586	39.000	0.297	0.00	0.000	39.000	0.000
	139.658									
	139.658 -		94.37	14.293	39.000	0.366	0.00	0.000	39.000	0.000
	137.934									
	137.934 -		115.63	16.796	39.000	0.431	0.00	0.000	39.000	0.000
	136.211									
	136.211 -		137.06	19.112	39.000	0.490	0.00	0.000	39.000	0.000
	134.487									
	134.487 -		158.69	21.258	39.000	0.545	0.00	0.000	39.000	0.000
	132.763									
	132.763 -		180.50	23.248	39.000	0.596	0.00	0.000	39.000	0.000
	131.039									
	131.039 -		202.50	25.096	39.000	0.643	0.00	0.000	39.000	0.000
	129.316									
	129.316 -		224.70	26.813	39.000	0.688	0.00	0.000	39.000	0.000
	127.592									
	127.592 -		247.09	28.411	39.000	0.728	0.00	0.000	39.000	0.000
	125.868		260.60	20.000	20.000	0.565	0.00	0.000	20.000	0.000
	125.868 -		269.68	29.899	39.000	0.767	0.00	0.000	39.000	0.000
	124.145		202.47	21 205	20,000	0.003	0.00	0.000	20.000	0.000
	124.145 -		292.47	31.285	39.000	0.802	0.00	0.000	39.000	0.000
	122.421		215 45	22 570	20,000	0.025	0.00	0.000	20.000	0.000
	122.421 -		315.45	32.578	39.000	0.835	0.00	0.000	39.000	0.000
	120.697		229.64	22.706	20.724	0.073	0.00	0.000	20.724	0.000
	120.697 -		338.64	33.786	38.724	0.872	0.00	0.000	38.724	0.000

**FDH Engineering, Inc.** 6521 Meridien Drive, Suite 107

Job		Page
	Guilford, 10110	15 of 22
Project		Date
	1426101400	11:14:00 04/08/14
Client	CTI Towers	Designed by Cary Webb

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Section No.	Elevation	Size	Actual M <sub>x</sub>	Actual f.	Allow. $F_{bx}$	Ratio	Actual M <sub>v</sub>	Actual f.	$Allow.$ $F_{by}$	Ratio
118.974	NO.	ft									$\frac{f_{by}}{F}$
118.974				кір-јі	KSI	KSI	F <sub>bx</sub>	кір-јі	KSt	KS1	$F_{by}$
11725   11725   113				362.04	3/1 01/	38 /33	0.008	0.00	0.000	38 /33	0.000
117.25 - 113				302.04	34.914	36.433	0.908	0.00	0.000	36.433	0.000
117.25 - 113				184 96	16 443	37 714	0.436	0.00	0.000	37 714	0.000
113 - 111 - 953	1.2		TP36 27x28 9012x0 25								0.000
111933			110012/112013 012110120								0.000
110.906											0.000
109.859   109.859   109.859   109.859   109.859   109.859   109.8513   494.80   30.879   39.000   0.792   0.00   0.000   39.000   107.766   509.86   31.223   39.000   0.801   0.00   0.000   39.000   107.766   509.86   31.223   39.000   0.801   0.00   0.000   39.000   106.719   525.00   31.553   39.000   0.807   0.000   39.000   105.672   105.672   104.625   104.625   104.625   104.625   103.578   102.531   102.531   102.531   102.531   586.37   32.752   39.000   0.840   0.00   0.000   39.000   100.438   101.484   101.484   101.484   101.484   101.484   101.484   101.483   100.438   617.56   33.285   39.000   0.853   0.00   0.000   39.000   99.3006   99.3006   99.3006   99.3006   633.27   33.538   39.000   0.860   0.00   0.000   39.000   99.3438   98.3438   98.3438   98.3438   98.3438   98.2438											
109.859		110.906 -		464.92	30.150	39.000	0.773	0.00	0.000	39.000	0.000
108.813		109.859									
108.813 -		109.859 -		479.82	30.522	39.000	0.783	0.00	0.000	39.000	0.000
107.766   107.766   107.766   107.766   106.719   525.00   31.553   39.000   0.801   0.00   0.000   39.000   106.719   105.672   105.672   105.672   104.625   104.6		108.813									
107.766				494.80	30.879	39.000	0.792	0.00	0.000	39.000	0.000
106.719											
106.719				509.86	31.223	39.000	0.801	0.00	0.000	39.000	0.000
105.672				525.00	21.552	20.000	0.000	0.00	0.000	20.000	0.000
105.672				525.00	31.553	39.000	0.809	0.00	0.000	39.000	0.000
104.625				540.22	21.970	20,000	0.017	0.00	0.000	20.000	0.000
104,625   555,52   32,175   39,000   0.825   0.00   0.000   39,000   103,578   570,90   32,469   39,000   0.833   0.00   0.000   39,000   102,531   586,37   32,752   39,000   0.840   0.00   0.000   39,000   101,484   101,484   101,484   101,484   104,388   100,438				340.22	31.670	39.000	0.817	0.00	0.000	39.000	0.000
103.578				555 52	32 175	39,000	0.825	0.00	0.000	39,000	0.000
103.578				333.32	32.173	37.000	0.025	0.00	0.000	37.000	0.000
102.531				570.90	32,469	39.000	0.833	0.00	0.000	39.000	0.000
102.531											
101.484				586.37	32.752	39.000	0.840	0.00	0.000	39.000	0.000
100.438		101.484									
100.438		101.484 -		601.92	33.024	39.000	0.847	0.00	0.000	39.000	0.000
99.3906 99.3906 99.3906 98.3438 98.3438 98.3438 97.2969 97.2969 97.2969 96.25 96.25 - 91.25  TP48.52x34.3529x0.3125 843.39 15.746 899.51 29.549 87.84.875 843.71 29.806 84.875 - 82.75 86.625 913.20 82.75 - 80.625 913.20 82.75 - 80.625 98.625 - 78.5 98.425 - 78.5 98.416 30.669 30.400 30.400 30.0000 30.0000 30.00000000											
99.3906 - 98.3438 - 649.08 33.781 39.000 0.860 0.00 0.000 39.000 98.3438 - 97.2969 - 664.97 34.014 39.000 0.872 0.00 0.000 39.000 96.25 - 91.25				617.56	33.285	39.000	0.853	0.00	0.000	39.000	0.000
98.3438				622 <b>25</b>	22.520	20.000	0.060	0.00	0.000	20.000	0.000
98.3438 - 97.2969 97.2969 - 664.97 34.014 39.000 0.872 0.00 0.000 39.000 96.25 96.25 - 91.25 TP48.52x34.3529x0.3125 403.39 15.746 39.000 0.410 0.00 0.000 39.000 91.25 - 89.125 89.125 775.67 29.271 39.000 0.751 0.00 0.000 39.000 89.125 - 87 80.951 29.549 39.000 0.751 0.00 0.000 39.000 87 - 84.875 80.951 29.549 39.000 0.758 0.00 0.000 39.000 88.4875 - 82.75 80.825 913.20 30.265 39.000 0.770 0.00 0.000 39.000 80.625 - 78.5 948.49 30.469 39.000 0.776 0.00 0.000 39.000 80.625 - 78.5 948.49 30.469 39.000 0.776 0.00 0.000 39.000 78.5 - 76.375 984.16 30.659 39.000 0.786 0.00 0.000 39.000 76.375 - 74.25 1020.19 30.835 39.000 0.796 0.00 0.000 39.000 76.375 - 74.25 1020.19 30.835 39.000 0.791 0.00 0.000 39.000 76.375 - 75.25 1056.60 30.998 39.000 0.795 0.00 0.000 39.000 70 - 67.875 1130.55 31.289 39.000 0.795 0.00 0.000 39.000 67.875 - 63.75 1168.08 31.419 39.000 0.799 0.00 0.000 39.000 67.875 - 65.75 1168.08 31.419 39.000 0.790 0.00 0.000 39.000 67.875 - 65.75 1168.08 31.419 39.000 0.806 0.00 0.000 39.000 63.625 - 61.5 1244.30 31.651 39.000 0.812 0.00 0.000 39.000 63.625 - 61.5 1244.30 31.651 39.000 0.814 0.00 0.000 39.000 59.375 - 57.25 1322.05 31.851 39.000 0.817 0.00 0.000 39.000 59.375 - 57.25 1322.05 31.851 39.000 0.817 0.00 0.000 39.000 55.125 - 53 1401.34 32.022 39.000 0.817 0.00 0.000 39.000 55.125 - 53 1401.34 32.022 39.000 0.811 0.00 0.000 39.000 53.3 - 46.25 712.67 15.015 38.531 0.390 0.00 0.000 38.531				633.27	33.538	39.000	0.860	0.00	0.000	39.000	0.000
97.2969 97.2969 - 664.97 34.014 39.000 0.872 0.00 0.000 39.000 96.25 96.25 - 91.25				640.00	22 701	20,000	0.066	0.00	0.000	20.000	0.000
97.2969 - 96.25 96.25 - 91.25 96.25 - 91.25 TP48.52x34.3529x0.3125 403.39 15.746 39.000 0.410 0.00 0.000 39.000 89.125 - 89.125 775.67 29.271 39.000 0.751 0.00 0.000 39.000 89.125 - 87 809.51 29.549 39.000 0.758 0.00 0.000 39.000 87 - 84.875 843.71 29.806 878.27 30.044 39.000 0.764 0.00 0.000 39.000 82.75 - 80.625 913.20 80.625 - 78.5 948.49 30.469 39.000 0.776 0.00 0.000 39.000 78.5 - 76.375 984.16 30.659 39.000 0.786 0.00 0.000 39.000 76.375 - 74.25 1020.19 30.835 31.149 39.000 0.795 0.00 0.000 39.000 70 - 67.875 1168.08 31.149 39.000 0.781 0.00 0.000 39.000 70 - 67.875 1168.08 31.149 39.000 0.781 0.00 0.000 39.000 70 - 67.875 1168.08 31.149 39.000 0.781 0.00 0.000 39.000 0.795 0.00 0.000 39.000 0.700 0.000 39.000 0.700 0.000 39.000 0.700 0.000 39.000 0.000 39.000 0.700 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 39.000 0.000 0.000 39.000 0.000 39.000 0.000 0.000 39.000 0.000 0.000 39.000 0.000 0.000 39.000 0.000 0.000 39.000 0.				049.06	33.761	39.000	0.800	0.00	0.000	39.000	0.000
96.25 - 91.25				664 97	34 014	39 000	0.872	0.00	0.000	39 000	0.000
L3       96.25 - 91.25       TP48.52x34.3529x0.3125       403.39       15.746       39.000       0.410       0.00       0.000       39.000         91.25 - 89.125       TP48.52x34.3529x0.3125       403.39       15.746       39.000       0.404       0.00       0.000       39.000         89.125 - 87       809.51       29.549       39.000       0.758       0.00       0.000       39.000         87 - 84.875       843.71       29.806       39.000       0.764       0.00       0.000       39.000         82.75 - 80.625       878.27       30.044       39.000       0.770       0.00       0.000       39.000         80.625 - 78.5       913.20       30.265       39.000       0.776       0.00       0.000       39.000         78.5 - 76.375       984.16       30.659       39.000       0.776       0.00       0.000       39.000         76.375 - 74.25       1020.19       30.835       39.000       0.786       0.00       0.000       39.000         72.125 - 70       1093.38       31.49       39.000       0.799       0.00       0.000       39.000         70 - 67.875       1130.55       31.289       39.000       0.806       0.00       0.000<				001.57	51.011	57.000	0.072	0.00	0.000	57.000	0.000
L3       96.25 - 91.25       TP48.52x34.3529x0.3125       403.39       15.746       39.000       0.404       0.00       0.000       39.000         891.25 - 87       809.51       29.271       39.000       0.751       0.00       0.000       39.000         87 - 84.875       843.71       29.806       39.000       0.764       0.00       0.000       39.000         82.75 - 80.625       878.27       30.044       39.000       0.770       0.00       0.000       39.000         80.625 - 78.5       913.20       30.265       39.000       0.776       0.00       0.000       39.000         78.5 - 76.375       984.16       30.659       39.000       0.781       0.00       0.000       39.000         76.375 - 74.25       1020.19       30.835       39.000       0.786       0.00       0.000       39.000         72.125 - 70       1093.38       31.149       39.000       0.795       0.00       0.000       39.000         67.875 - 63.625       1168.08       31.419       39.000       0.802       0.00       0.000       39.000         70 - 67.875       1168.08       31.419       39.000       0.806       0.00       0.000       39.000 <td></td> <td></td> <td></td> <td>338.80</td> <td>15.989</td> <td>39.000</td> <td>0.410</td> <td>0.00</td> <td>0.000</td> <td>39.000</td> <td>0.000</td>				338.80	15.989	39.000	0.410	0.00	0.000	39.000	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	L3	96.25 - 91.25	TP48.52x34.3529x0.3125	403.39	15.746	39.000	0.404	0.00	0.000	39.000	0.000
87 - 84.875       843.71       29.806       39.000       0.764       0.00       0.000       39.000         84.875 - 82.75       878.27       30.044       39.000       0.770       0.00       0.000       39.000         82.75 - 80.625       913.20       30.265       39.000       0.776       0.00       0.000       39.000         80.625 - 78.5       948.49       30.469       39.000       0.781       0.00       0.000       39.000         78.5 - 76.375       984.16       30.659       39.000       0.786       0.00       0.000       39.000         76.375 - 74.25       1020.19       30.835       39.000       0.791       0.00       0.000       39.000         74.25 - 72.125       1056.60       30.998       39.000       0.795       0.00       0.000       39.000         72.125 - 70       1093.38       31.149       39.000       0.799       0.00       0.000       39.000         67.875 - 65.75       1168.08       31.419       39.000       0.802       0.00       0.000       39.000         65.75 - 63.625       1206.00       31.540       39.000       0.806       0.00       0.000       39.000         61.5 - 59.375 <td< td=""><td></td><td>91.25 - 89.125</td><td></td><td>775.67</td><td>29.271</td><td>39.000</td><td>0.751</td><td>0.00</td><td>0.000</td><td>39.000</td><td>0.000</td></td<>		91.25 - 89.125		775.67	29.271	39.000	0.751	0.00	0.000	39.000	0.000
84.875 - 82.75       878.27       30.044       39.000       0.770       0.00       0.000       39.000         82.75 - 80.625       913.20       30.265       39.000       0.776       0.00       0.000       39.000         80.625 - 78.5       948.49       30.469       39.000       0.781       0.00       0.000       39.000         78.5 - 76.375       984.16       30.659       39.000       0.786       0.00       0.000       39.000         76.375 - 74.25       1020.19       30.835       39.000       0.791       0.00       0.000       39.000         74.25 - 72.125       1056.60       30.998       39.000       0.795       0.00       0.000       39.000         70 - 67.875       1130.55       31.289       39.000       0.799       0.00       0.000       39.000         67.875 - 65.75       1168.08       31.419       39.000       0.802       0.00       0.000       39.000         65.75 - 63.625       1206.00       31.540       39.000       0.806       0.00       0.000       39.000         61.5 - 59.375       1244.30       31.651       39.000       0.812       0.00       0.000       39.000         65.75 - 61.5       <		89.125 - 87		809.51	29.549	39.000	0.758	0.00	0.000	39.000	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		87 - 84.875				39.000	0.764	0.00	0.000	39.000	0.000
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67.875 - 65.75       1168.08       31.419       39.000       0.806       0.00       0.000       39.000         65.75 - 63.625       1206.00       31.540       39.000       0.809       0.00       0.000       39.000         63.625 - 61.5       1244.30       31.651       39.000       0.812       0.00       0.000       39.000         61.5 - 59.375       1282.98       31.755       39.000       0.814       0.00       0.000       39.000         59.375 - 57.25       1322.05       31.851       39.000       0.817       0.00       0.000       39.000         57.25 - 55.125       1361.50       31.940       39.000       0.819       0.00       0.000       39.000         55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
65.75 - 63.625       1206.00       31.540       39.000       0.809       0.00       0.000       39.000         63.625 - 61.5       1244.30       31.651       39.000       0.812       0.00       0.000       39.000         61.5 - 59.375       1282.98       31.755       39.000       0.814       0.00       0.000       39.000         59.375 - 57.25       1322.05       31.851       39.000       0.817       0.00       0.000       39.000         57.25 - 55.125       1361.50       31.940       39.000       0.819       0.00       0.000       39.000         55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
63.625 - 61.5       1244.30       31.651       39.000       0.812       0.00       0.000       39.000         61.5 - 59.375       1282.98       31.755       39.000       0.814       0.00       0.000       39.000         59.375 - 57.25       1322.05       31.851       39.000       0.817       0.00       0.000       39.000         57.25 - 55.125       1361.50       31.940       39.000       0.819       0.00       0.000       39.000         55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
61.5 - 59.375       1282.98       31.755       39.000       0.814       0.00       0.000       39.000         59.375 - 57.25       1322.05       31.851       39.000       0.817       0.00       0.000       39.000         57.25 - 55.125       1361.50       31.940       39.000       0.819       0.00       0.000       39.000         55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
59.375 - 57.25       1322.05       31.851       39.000       0.817       0.00       0.000       39.000         57.25 - 55.125       1361.50       31.940       39.000       0.819       0.00       0.000       39.000         55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
57.25 - 55.125     1361.50     31.940     39.000     0.819     0.00     0.000     39.000       55.125 - 53     1401.34     32.022     39.000     0.821     0.00     0.000     39.000       53 - 46.25     712.67     15.015     38.531     0.390     0.00     0.000     38.531											0.000
55.125 - 53       1401.34       32.022       39.000       0.821       0.00       0.000       39.000         53 - 46.25       712.67       15.015       38.531       0.390       0.00       0.000       38.531											0.000
		55.125 - 53		1401.34	32.022	39.000	0.821	0.00	0.000	39.000	0.000
L4 53 - 46.25 TP61x45.9824x0.375 818.03 14.801 39.000 0.380 0.00 0.000 39.000						38.531	0.390	0.00	0.000	38.531	0.000
	L4	53 - 46.25	TP61x45.9824x0.375	818.03	14.801	39.000	0.380	0.00	0.000	39.000	0.000
46.25 - 1578.38 27.744 39.000 0.711 0.00 0.000 39.000				1578.38	27.744	39.000	0.711	0.00	0.000	39.000	0.000
43.8158		43.8158									

**FDH Engineering, Inc.** 6521 Meridien Drive, Suite 107

Job		Page
	Guilford, 10110	16 of 22
Project		Date
	1426101400	11:14:00 04/08/14
Client	CTI Towers	Designed by Cary Webb

Section No.	Elevation	Size	Actual $M_x$	Actual f <sub>bx</sub>	Allow. $F_{bx}$	Ratio $f_{bx}$	Actual M <sub>v</sub>	Actual f <sub>by</sub>	Allow. $F_{bv}$	Ratio $f_{by}$
	ft		kip-ft	ksi	ksi	$F_{bx}$	kip-ft	ksi	ksi	$F_{by}$
	43.8158 -		1626.50	27.786	39.000	0.712	0.00	0.000	39.000	0.000
	41.3816									
	41.3816 -		1675.10	27.823	39.000	0.713	0.00	0.000	39.000	0.000
	38.9474									
	38.9474 -		1724.18	27.855	39.000	0.714	0.00	0.000	39.000	0.000
	36.5132									
	36.5132 -		1773.72	27.882	39.000	0.715	0.00	0.000	39.000	0.000
	34.0789									
	34.0789 -		1823.74	27.906	39.000	0.716	0.00	0.000	39.000	0.000
	31.6447									
	31.6447 -		1874.26	27.925	39.000	0.716	0.00	0.000	39.000	0.000
	29.2105									
	29.2105 -		1925.26	27.941	39.000	0.716	0.00	0.000	39.000	0.000
	26.7763		1076.75	27.054	20.000	0.717	0.00	0.000	20.000	0.000
	26.7763 -		1976.75	27.954	39.000	0.717	0.00	0.000	39.000	0.00
	24.3421 24.3421 -		2028.74	27.964	39.000	0.717	0.00	0.000	39.000	0.000
	24.3421 - 21.9079		2028.74	27.904	39.000	0./1/	0.00	0.000	39.000	0.00
	21.9079 -		2081.23	27.972	39.000	0.717	0.00	0.000	39.000	0.00
	19.4737		2001.23	21.912	39.000	0./1/	0.00	0.000	39.000	0.00
	19.4737 -		2134.23	27.977	39.000	0.717	0.00	0.000	39.000	0.00
	17.0395		2134.23	21.511	37.000	0.717	0.00	0.000	37.000	0.000
	17.0395 -		2187.74	27.980	38.938	0.719	0.00	0.000	38.938	0.00
	14.6053		210,	27.1500	20020	01, 15	0.00	0.000	20000	0.00
	14.6053 -		2241.77	27.981	38.732	0.722	0.00	0.000	38.732	0.000
	12.1711									
	12.1711 -		2296.32	27.981	38.526	0.726	0.00	0.000	38.526	0.000
	9.73684									
	9.73684 -		2351.38	27.979	38.320	0.730	0.00	0.000	38.320	0.00
	7.30263									
	7.30263 -		2406.98	27.975	38.114	0.734	0.00	0.000	38.114	0.00
	4.86842									
	4.86842 -		2463.12	27.970	37.908	0.738	0.00	0.000	37.908	0.00
	2.43421									
	2.43421 - 0		2519.78	27.965	37.702	0.742	0.00	0.000	37.702	0.000

Pole Shear Design Data										
			•			•			•	
Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio

No.			V	$f_{v}$	$F_{\nu}$	$f_{v}$	T	$f_{vt}$	$F_{vt}$	$f_{vt}$
	ft		K	ksi	ksi	$\overline{F_v}$	kip-ft	ksi	ksi	$F_{vt}$
L1	150 - 148.276	TP30.48x20x0.1875	6.70	0.555	26.000	0.043	0.01	0.001	26.000	0.000
	148.276 -		6.80	0.550	26.000	0.042	0.01	0.001	26.000	0.000
	146.553									
	146.553 -		6.90	0.545	26.000	0.042	0.01	0.001	26.000	0.000
	144.829									
	144.829 -		7.01	0.541	26.000	0.042	0.01	0.001	26.000	0.000
	143.105									
	143.105 -		7.11	0.537	26.000	0.041	0.01	0.001	26.000	0.000
	141.382									
	141.382 -		12.17	0.899	26.000	0.069	0.01	0.001	26.000	0.000
	139.658				•				•	
	139.658 -		12.28	0.888	26.000	0.068	0.01	0.001	26.000	0.000
	137.934		12.00	0.055	26.000	0.065	0.01	0.004	26000	0.000
	137.934 -		12.39	0.877	26.000	0.067	0.01	0.001	26.000	0.000
	136.211									

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Section	Elevation	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
No.	ft		V K	f <sub>v</sub> ksi	F <sub>v</sub> ksi	$\frac{f_v}{F_v}$	T kip-ft	f <sub>vt</sub> ksi	F <sub>vt</sub> ksi	$\frac{f_{vt}}{F_{vt}}$
	136.211 -		12.49	0.867	26.000	0.067	0.01	0.001	26.000	$\frac{F_{vt}}{0.000}$
	134.487		12	0.007	20,000	0.007	0.01	0.001		0.000
	134.487 -		12.60	0.858	26.000	0.066	0.01	0.001	26.000	0.000
	132.763		10.71	0.040	26,000	0.065	0.01	0.001	26,000	0.000
	132.763 - 131.039		12.71	0.848	26.000	0.065	0.01	0.001	26.000	0.000
	131.039 -		12.83	0.839	26.000	0.065	0.01	0.001	26.000	0.000
	129.316									
	129.316 -		12.94	0.831	26.000	0.064	0.01	0.001	26.000	0.000
	127.592 127.592 -		13.05	0.823	26.000	0.063	0.01	0.001	26.000	0.000
	125.868		15.05	0.023	20.000	0.005	0.01	0.001	20.000	0.000
	125.868 -		13.17	0.815	26.000	0.063	0.01	0.001	26.000	0.000
	124.145		12.20	0.000	2 < 000	0.062	0.01	0.004	2 ( 000	0.000
	124.145 - 122.421		13.28	0.808	26.000	0.062	0.01	0.001	26.000	0.000
	122.421 -		13.40	0.801	26.000	0.062	0.01	0.001	26.000	0.000
	120.697									
	120.697 -		13.52	0.794	26.000	0.061	0.01	0.001	26.000	0.000
	118.974 118.974 -		13.64	0.788	26.000	0.061	0.01	0.000	26.000	0.000
	117.25		15.04	0.766	20.000	0.001	0.01	0.000	20.000	0.000
	117.25 - 113		6.23	0.346	26.000	0.027	0.00	0.000	26.000	0.000
L2	117.25 - 113	TP36.27x28.9012x0.25	7.75	0.327	26.000	0.025	0.01	0.000	26.000	0.000
	113 - 111.953		14.05	0.587	26.000	0.045	0.01	0.000	26.000	0.000
	111.953 - 110.906		14.12	0.585	26.000	0.045	0.01	0.000	26.000	0.000
	110.906 -		14.20	0.582	26.000	0.045	0.01	0.000	26.000	0.000
	109.859									
	109.859 -		14.27	0.579	26.000	0.045	0.01	0.000	26.000	0.000
	108.813 108.813 -		14.35	0.577	26.000	0.044	0.01	0.000	26.000	0.000
	107.766		14.55	0.577	20.000	0.044	0.01	0.000	20.000	0.000
	107.766 -		14.43	0.575	26.000	0.044	0.01	0.000	26.000	0.000
	106.719		14.50	0.550	26,000	0.044	0.01	0.000	26,000	0.000
	106.719 - 105.672		14.50	0.572	26.000	0.044	0.01	0.000	26.000	0.000
	105.672 -		14.58	0.570	26.000	0.044	0.01	0.000	26.000	0.000
	104.625									
	104.625 -		14.66	0.568	26.000	0.044	0.01	0.000	26.000	0.000
	103.578 103.578 -		14.74	0.566	26.000	0.044	0.01	0.000	26.000	0.000
	102.531		14.74	0.500	20.000	0.011	0.01	0.000	20.000	0.000
	102.531 -		14.82	0.564	26.000	0.043	0.01	0.000	26.000	0.000
	101.484		14.00	0.560	26,000	0.042	0.01	0.000	26,000	0.000
	101.484 - 100.438		14.90	0.562	26.000	0.043	0.01	0.000	26.000	0.000
	100.438 -		14.98	0.560	26.000	0.043	0.01	0.000	26.000	0.000
	99.3906									
	99.3906 -		15.06	0.558	26.000	0.043	0.01	0.000	26.000	0.000
	98.3438 98.3438 -		15.14	0.556	26.000	0.043	0.01	0.000	26.000	0.000
	97.2969		13.17	0.550	20.000	0.075	0.01	0.000	20.000	0.000
	97.2969 -		15.22	0.554	26.000	0.043	0.01	0.000	26.000	0.000
	96.25		7.27	0.254	26,000	0.020	0.00	0.000	26,000	0.000
L3	96.25 - 91.25 96.25 - 91.25	TP48.52x34.3529x0.3125	7.27 8.41	0.254 0.239	26.000 26.000	0.020 0.018	0.00 0.01	0.000	26.000 26.000	0.000
LJ	91.25 - 89.125	11'40.54854.55478U.5145	15.85	0.239	26.000	0.018	0.01	0.000	26.000	0.000
	89.125 - 87		16.02	0.440	26.000	0.034	0.01	0.000	26.000	0.000
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Section No.	Elevation	Size	Actual V	Actual $f_v$	Allow. $F_v$	Ratio $f_v$	Actual T	Actual $f_{vt}$	$Allow.$ $F_{vt}$	Ratio $f_{vt}$
1,0.	ft		K	ksi	ksi	$\frac{f_v}{F_v}$	kip-ft	ksi	ksi	$F_{vt}$
	84.875 - 82.75		16.36	0.436	26.000	0.033	0.01	0.000	26.000	0.000
	82.75 - 80.625		16.53	0.433	26.000	0.033	0.01	0.000	26.000	0.000
	80.625 - 78.5		16.71	0.431	26.000	0.033	0.01	0.000	26.000	0.000
	78.5 - 76.375		16.88	0.429	26.000	0.033	0.01	0.000	26.000	0.000
	76.375 - 74.25		17.05	0.427	26.000	0.033	0.01	0.000	26.000	0.000
	74.25 - 72.125		17.23	0.425	26.000	0.033	0.01	0.000	26.000	0.000
	72.125 - 70		17.41	0.423	26.000	0.033	0.01	0.000	26.000	0.000
	70 - 67.875		17.59	0.421	26.000	0.032	0.01	0.000	26.000	0.000
	67.875 - 65.75		17.76	0.420	26.000	0.032	0.01	0.000	26.000	0.000
	65.75 - 63.625		17.94	0.418	26.000	0.032	0.01	0.000	26.000	0.000
	63.625 - 61.5		18.12	0.416	26.000	0.032	0.01	0.000	26.000	0.000
	61.5 - 59.375		18.30	0.415	26.000	0.032	0.01	0.000	26.000	0.000
	59.375 - 57.25		18.49	0.413	26.000	0.032	0.01	0.000	26.000	0.000
	57.25 - 55.125		18.67	0.412	26.000	0.032	0.01	0.000	26.000	0.000
	55.125 - 53		18.85	0.411	26.000	0.032	0.01	0.000	26.000	0.000
	53 - 46.25		9.25	0.193	26.000	0.032	0.00	0.000	26.000	0.000
L4	53 - 46.25	TP61x45.9824x0.375	10.26	0.181	26.000	0.013	0.01	0.000	26.000	0.000
	46.25 -	11 017 13.502 170.573	19.69	0.343	26.000	0.026	0.01	0.000	26.000	0.000
	43.8158		17.07	010.10	20,000	0.020	0.01	0.000	20,000	0.000
	43.8158 -		19.88	0.342	26.000	0.026	0.01	0.000	26.000	0.000
	41.3816		17.00	0.0.12	20,000	0.020	0.01	0.000	20,000	0.000
	41.3816 -		20.07	0.340	26.000	0.026	0.01	0.000	26.000	0.000
	38.9474		20.07	0.510	20.000	0.020	0.01	0.000	20.000	0.000
	38.9474 -		20.27	0.339	26.000	0.026	0.01	0.000	26.000	0.000
	36.5132		20.27	0.557	20.000	0.020	0.01	0.000	20.000	0.000
	36.5132 -		20.46	0.337	26.000	0.026	0.01	0.000	26.000	0.000
	34.0789		20.40	0.551	20.000	0.020	0.01	0.000	20.000	0.000
	34.0789 -		20.66	0.336	26.000	0.026	0.01	0.000	26.000	0.000
	31.6447		20.00	0.550	20.000	0.020	0.01	0.000	20.000	0.000
	31.6447 -		20.86	0.335	26.000	0.026	0.01	0.000	26.000	0.000
	29.2105		20.00	0.555	20.000	0.020	0.01	0.000	20.000	0.000
	29.2105 -		21.07	0.334	26.000	0.026	0.01	0.000	26.000	0.000
	26.7763		21.07	0.554	20.000	0.020	0.01	0.000	20.000	0.000
	26.7763 -		21.27	0.333	26.000	0.026	0.01	0.000	26.000	0.000
	24.3421		21.27	0.555	20.000	0.020	0.01	0.000	20.000	0.000
	24.3421 -		21.47	0.332	26.000	0.025	0.01	0.000	26.000	0.000
	21.9079		21.47	0.552	20.000	0.023	0.01	0.000	20.000	0.000
	21.9079 -		21.68	0.331	26.000	0.025	0.01	0.000	26.000	0.000
	19.4737		21.00	0.551	20.000	0.023	0.01	0.000	20.000	0.000
	19.4737 -		21.89	0.330	26.000	0.025	0.01	0.000	26.000	0.000
	17.0395		21.09	0.550	20.000	0.023	0.01	0.000	20.000	0.000
	17.0395 -		22.10	0.329	26.000	0.025	0.01	0.000	26.000	0.000
	14.6053		22.10	0.329	20.000	0.023	0.01	0.000	20.000	0.000
	14.6053 -		22.31	0.328	26.000	0.025	0.01	0.000	26.000	0.000
	12.1711		22.31	0.326	20.000	0.023	0.01	0.000	20.000	0.000
	12.1711 -		22.53	0.327	26.000	0.025	0.01	0.000	26.000	0.000
	9.73684		22.33	0.327	20.000	0.023	0.01	0.000	20.000	0.000
	9.73684 9.73684 -		22.75	0.326	26.000	0.025	0.01	0.000	26.000	0.000
	7.30263		44.13	0.320	20.000	0.023	0.01	0.000	20.000	0.000
			22.06	0.226	26,000	0.025	0.01	0.000	26,000	0.00
	7.30263 -		22.96	0.326	26.000	0.025	0.01	0.000	26.000	0.00
	4.86842		22.10	0.225	26,000	0.025	0.01	0.000	26,000	0.000
	4.86842 -		23.18	0.325	26.000	0.025	0.01	0.000	26.000	0.00
	2.43421		22.41	0.224	26,000	0.025	0.01	0.000	26,000	0.000
	2.43421 - 0		23.41	0.324	26.000	0.025	0.01	0.000	26.000	0.000

FDH Engineering, Inc.

DA Engineering, in	c.
21 Meridien Drive, Suite	107
Raleigh, NC 27616	
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# Pole Interaction Design Data

lection No.	Elevation	Ratio P	Ratio $f_{bx}$	Ratio $f_{by}$	Ratio $f_v$	Ratio $f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	$F_{bx}$	$F_{by}$	$\frac{f_v}{F_v}$	$\frac{-F_{vt}}{F_{vt}}$	Ratio	Ratio	
L1	150 - 148.276	0.005	0.059	0.000	0.043	0.000	0.065	1.333	H1-3+VT ✔
	148.276 - 146.553	0.005	0.113	0.000	0.042	0.000	0.119	1.333	H1-3+VT ✔
	146.553 - 144.829	0.005	0.163	0.000	0.042	0.000	0.168	1.333	H1-3+VT 🗸
	144.829 - 143.105	0.005	0.208	0.000	0.042	0.000	0.214	1.333	H1-3+VT 🗸
	143.105 - 141.382	0.005	0.251	0.000	0.041	0.000	0.257	1.333	H1-3+VT 🗸
	141.382 - 139.658	0.010	0.297	0.000	0.069	0.000	0.308	1.333	H1-3+VT 🗸
	139.658 - 137.934	0.010	0.366	0.000	0.068	0.000	0.378	1.333	H1-3+VT 🗸
	137.934 - 136.211	0.010	0.431	0.000	0.067	0.000	0.442	1.333	H1-3+VT 🗸
	136.211 - 134.487	0.010	0.490	0.000	0.067	0.000	0.501	1.333	H1-3+VT 🗸
	134.487 - 132.763	0.010	0.545	0.000	0.066	0.000	0.556	1.333	H1-3+VT 🗸
	132.763 - 131.039	0.010	0.596	0.000	0.065	0.000	0.607	1.333	H1-3+VT 🗸
	131.039 - 129.316	0.010	0.643	0.000	0.065	0.000	0.655	1.333	H1-3+VT ✔
	129.316 - 127.592	0.010	0.688	0.000	0.064	0.000	0.699	1.333	H1-3+VT 🗸
	127.592 - 125.868	0.010	0.728	0.000	0.063	0.000	0.740	1.333	H1-3+VT 🗸
	125.868 - 124.145	0.010	0.767	0.000	0.063	0.000	0.778	1.333	H1-3+VT 🗸
	124.145 - 122.421	0.010	0.802	0.000	0.062	0.000	0.813	1.333	H1-3+VT 🗸
	122.421 - 120.697	0.010	0.835	0.000	0.062	0.000	0.847	1.333	H1-3+VT 🗸
	120.697 - 118.974	0.010	0.872	0.000	0.061	0.000	0.884	1.333	H1-3+VT 🗸
	118.974 - 117.25	0.011	0.908	0.000	0.061	0.000	0.920	1.333	H1-3+VT 🗸
	117.25 - 113	0.005	0.436	0.000	0.027	0.000	0.441	1.333	H1-3+VT 🗸
L2	117.25 - 113	0.005	0.416	0.000	0.025	0.000	0.421	1.333	H1-3+VT 🗸
	113 - 111.953	0.008	0.753	0.000	0.045	0.000	0.762	1.333	H1-3+VT ✔
	111.953 - 110.906	0.008	0.763	0.000	0.045	0.000	0.772	1.333	H1-3+VT 🗸
	110.906 - 109.859	0.008	0.773	0.000	0.045	0.000	0.782	1.333	H1-3+VT 🗸
	109.859 - 108.813	0.008	0.783	0.000	0.045	0.000	0.792	1.333	H1-3+VT 🗸

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Client	Designed by
CTI Towers	Cary Webb

ection No.	Elevation	Ratio P	Ratio $f_{bx}$	$Ratio \ f_{by}$	Ratio $f_v$	Ratio $f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	$F_{bx}$	$F_{by}$	$\frac{f_{v}}{F_{v}}$	$\frac{f_{vt}}{F_{vt}}$	Ratio	Ratio	
	108.813 - 107.766	0.009	0.792	0.000	0.044	0.000	0.801	1.333	H1-3+VT ▶
	107.766 - 106.719	0.009	0.801	0.000	0.044	0.000	0.810	1.333	H1-3+VT ▶
	106.719 - 105.672	0.009	0.809	0.000	0.044	0.000	0.818	1.333	H1-3+VT ▶
	105.672 - 104.625	0.009	0.817	0.000	0.044	0.000	0.826	1.333	H1-3+VT ▶
	104.625 - 103.578	0.009	0.825	0.000	0.044	0.000	0.834	1.333	H1-3+VT ▶
	103.578 - 102.531	0.009	0.833	0.000	0.044	0.000	0.842	1.333	H1-3+VT ▶
	102.531 - 101.484	0.009	0.840	0.000	0.043	0.000	0.849	1.333	H1-3+VT ▶
	101.484 - 100.438	0.009	0.847	0.000	0.043	0.000	0.856	1.333	H1-3+VT ▶
	100.438 - 99.3906	0.009	0.853	0.000	0.043	0.000	0.863	1.333	H1-3+VT ▶
	99.3906 - 98.3438	0.009	0.860	0.000	0.043	0.000	0.869	1.333	H1-3+VT ▶
	98.3438 - 97.2969	0.009	0.866	0.000	0.043	0.000	0.876	1.333	H1-3+VT ▮
	97.2969 - 96.25	0.009	0.872	0.000	0.043	0.000	0.882	1.333	H1-3+VT <b>↓</b>
	96.25 - 91.25	0.004	0.410	0.000	0.020	0.000	0.414	1.333	H1-3+VT ┡
L3	96.25 - 91.25	0.004	0.404	0.000	0.018	0.000	0.408	1.333	H1-3+VT ▶
	91.25 - 89.125	0.008	0.751	0.000	0.034	0.000	0.759	1.333	H1-3+VT <b>↓</b>
	89.125 - 87	0.008	0.758	0.000	0.034	0.000	0.766	1.333	H1-3+VT ▮
	87 - 84.875	0.008	0.764	0.000	0.034	0.000	0.773	1.333	H1-3+VT ▮
	84.875 - 82.75	0.008	0.770	0.000	0.033	0.000	0.779	1.333	H1-3+VT ▮
	82.75 - 80.625	0.008	0.776	0.000	0.033	0.000	0.785	1.333	H1-3+VT ▮
	80.625 - 78.5	0.008	0.781	0.000	0.033	0.000	0.790	1.333	H1-3+VT ▮
	78.5 - 76.375	0.009	0.786	0.000	0.033	0.000	0.795	1.333	H1-3+VT ▮
	76.375 - 74.25	0.009	0.791	0.000	0.033	0.000	0.800	1.333	H1-3+VT <b>↓</b>
	74.25 - 72.125	0.009	0.795	0.000	0.033	0.000	0.804	1.333	H1-3+VT ▮
	72.125 - 70	0.009	0.799	0.000	0.033	0.000	0.808	1.333	H1-3+VT ▶
	70 - 67.875	0.009	0.802	0.000	0.032	0.000	0.811	1.333	H1-3+VT ▮
	67.875 - 65.75	0.009	0.806	0.000	0.032	0.000	0.815	1.333	H1-3+VT ▮

FDH Engineering, Inc. 6521 Meridien Drive, Suite 107

Job		Page
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Project		Date
	1426101400	11:14:00 04/08/14
Client	CTI Towers	Designed by Cary Webb

Section No.	Elevation	Ratio P	Ratio $f_{bx}$	Ratio $f_{by}$	Ratio $f_v$	Ratio $f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	$\frac{f_{bx}}{F_{bx}}$	$\frac{f_{by}}{F_{by}}$	$\frac{F_{v}}{F_{v}}$	$F_{vt}$	Ratio	Ratio	
	65.75 - 63.625	0.009	0.809	0.000	0.032	0.000	0.818	1.333	H1-3+VT 🗸
	63.625 - 61.5	0.009	0.812	0.000	0.032	0.000	0.821	1.333	H1-3+VT ✔
	61.5 - 59.375	0.009	0.814	0.000	0.032	0.000	0.824	1.333	H1-3+VT 🗸
	59.375 - 57.25	0.009	0.817	0.000	0.032	0.000	0.826	1.333	H1-3+VT 🗸
	57.25 - 55.125	0.010	0.819	0.000	0.032	0.000	0.829	1.333	H1-3+VT 🗸
	55.125 - 53	0.010	0.821	0.000	0.032	0.000	0.831	1.333	H1-3+VT 🗸
	53 - 46.25	0.005	0.390	0.000	0.015	0.000	0.395	1.333	H1-3+VT ✓
L4	53 - 46.25	0.005	0.380	0.000	0.014	0.000	0.384	1.333	H1-3+VT
	46.25 - 43.8158	0.009	0.711	0.000	0.026	0.000	0.721	1.333	H1-3+VT
	43.8158 - 41.3816 41.3816 -	0.009	0.712 0.713	0.000	0.026	0.000	0.722 0.723	1.333 1.333	H1-3+VT
	38.9474 38.9474 -	0.009	0.713	0.000	0.026	0.000	0.724	1.333	H1-3+VT
	36.5132 36.5132 -	0.010	0.714	0.000	0.026	0.000	0.725	1.333	H1-3+VT
	34.0789 34.0789 -	0.010	0.716	0.000	0.026	0.000	0.725	1.333	H1-3+VT H1-3+VT
	31.6447 31.6447 -	0.010	0.716	0.000	0.026	0.000	0.726	1.333	H1-3+VT 🗸
	29.2105 29.2105 -	0.010	0.716	0.000	0.026	0.000	0.726	1.333	H1-3+VT 🗸
	26.7763 26.7763 -	0.010	0.717	0.000	0.026	0.000	0.727	1.333	H1-3+VT ✔
	24.3421 24.3421 - 21.9079	0.010	0.717	0.000	0.025	0.000	0.727	1.333	H1-3+VT ✔
	21.9079 - 19.4737	0.010	0.717	0.000	0.025	0.000	0.728	1.333	H1-3+VT 🗸
	19.4737 - 17.0395	0.010	0.717	0.000	0.025	0.000	0.728	1.333	H1-3+VT 🗸
	17.0395 - 14.6053	0.010	0.719	0.000	0.025	0.000	0.729	1.333	H1-3+VT 🗸
	14.6053 - 12.1711	0.011	0.722	0.000	0.025	0.000	0.733	1.333	H1-3+VT 🗸
	12.1711 - 9.73684	0.011	0.726	0.000	0.025	0.000	0.737	1.333	H1-3+VT ✔
	9.73684 - 7.30263	0.011	0.730	0.000	0.025	0.000	0.741	1.333	H1-3+VT ✔
	7.30263 - 4.86842	0.011	0.734	0.000	0.025	0.000	0.745	1.333	H1-3+VT
	4.86842 - 2.43421	0.011	0.738	0.000	0.025	0.000	0.749	1.333	H1-3+VT 🗸

**FDH Engineering, Inc.** 6521 Meridien Drive, Suite 107

Raleigh, NC 27616 Phone: 9197551012 FAX: 9197551031

Job		Page
	Guilford, 10110	22 of 22
Project		Date
	1426101400	11:14:00 04/08/14
Client	CTI Towers	Designed by Cary Webb

Section No.	Elevation	Ratio P	Ratio $f_{bx}$	Ratio $f_{by}$	Ratio $f_v$	Ratio $f_{vt}$	Comb. Stress	Allow. Stress	Criteria
	ft	$P_a$	$F_{bx}$	$F_{by}$	$F_{v}$	$F_{vt}$	Ratio	Ratio	
	2.43421 - 0	0.011	0.742	0.000	0.025	0.000	0.753	1.333	H1-3+VT 🖊

Section Capacity Table								
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
L1	150 - 113	Pole	TP30.48x20x0.1875	1	-7.01	886.88	69.0	Pass
L2	113 - 91.25	Pole	TP36.27x28.9012x0.25	2	-9.64	1427.43	66.1	Pass
L3	91.25 - 46.25	Pole	TP48.52x34.3529x0.3125	3	-17.19	2387.18	62.3	Pass
L4	46.25 - 0	Pole	TP61x45.9824x0.375	4	-31.18	3626.48	56.5	Pass
							Summary	
						Pole (L1)	69.0	Pass
						RATING =	69.0	Pass

 $Program\ Version\ 6.1.4.1\ -\ 12/17/2013\ File://FDH-SERVER/Projects/2014\ Effective\ -\ Client\ Jobs/CTITOW\_CTI\ Towers/CT/10110\_Guilford/1426101400/Analysis/Tower/Guilford,\ 10110.eri$ 

### Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

TIA Rev G Assumption: Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)\*(Rod Diameter)

Site Data

BU#: Site Name: Guilford App #:

Pole Manufacturer: Other

Anchor Rod Data							
Qty:	16						
Diam:	2.25	in					
Rod Material:	A615-J						
Strength (Fu):	105	ksi					
Yield (Fy):	75	ksi					
Bolt Circle:	68	in					

Plate Data				
Diam:	74	in		
Thick:	2	in		
Grade:	60	ksi		
Single-Rod B-eff:	12.10	in		

Stiffener Data (Welding at both sides)					
Config:	0	*			
Weld Type:	Both				
Groove Depth:	0.3125	in **			
Groove Angle:	45	degrees			
Fillet H. Weld:	0.3125	in			
Fillet V. Weld:	0.3125	in			
Width:	10	in			
Height:	12	in			
Thick:	1	in			
Notch:	0.5	in			
Grade:	50	ksi			
Weld str.:	70	ksi			

Pole Data					
Diam:	61	in			
Thick:	0.375	in			
Grade:	65	ksi			
# of Sides:	18	"0" IF Round			
Fu	80	ksi			
Reinf. Fillet Weld	0	"0" if None			

Reactions					
Mu: 2520 ft-kips					
Axial, Pu:	31	kips			
Shear, Vu:	23	kips			
Eta Factor, η	0.5	TIA G (Fig. 4-4)			

If No stiffeners, Criteria:	AISC LRFD	<-Only Applcable to Unstiffened Cases
-----------------------------	-----------	---------------------------------------

**Anchor Rod Results** 

Max Rod (Cu+ Vu/ή): 116.0 Kips Allowable Axial, Φ\*Fu\*Anet: 273.0 Kips Anchor Rod Stress Ratio: 42.5% Pass

Rigid
AISC LRFD
φ*Tn

Base Plate ResultsFlexural CheckBase Plate Stress:21.0 ksiAllowable Plate Stress:54.0 ksiBase Plate Stress Ratio:38.9% Pass

Rigid	
AISC LRFD	
φ*Fy	
Y.L. Length:	
30.05	

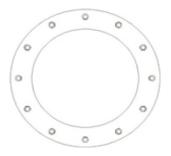
### n/a

### Stiffener Results

Horizontal Weld: n/a
Vertical Weld: n/a
Plate Flex+Shear, fb/Fb+(fv/Fv)^2: n/a
Plate Tension+Shear, ft/Ft+(fv/Fv)^2: n/a
Plate Comp. (AISC Bracket): n/a

### **Pole Results**

Pole Punching Shear Check: n/a





Analysis Date: 4/8/2014

<sup>\* 0 =</sup> none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

<sup>\*\*</sup> Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

CAISSON Version 10.61 5:00:18 PM Tuesday, April 08, 2014

FDH Engineering

\* CAISSON - Pier Foundations Analysis and Design - Copyright Power Line Systems, Inc. 1993-2010 \*

Project Title: Guilford - 1426101400 Project Notes:

Calculation Method: Full 8CD

\*\*\*\*\* I N P U T D A T A

### Pier Properties

Diameter (ft)	Distance of Top of Pier above Ground (ft)	Concrete Strength (ksi)	Steel Yield Strength (ksi)
8.00	0 - 5 0	4 - 00	60.00

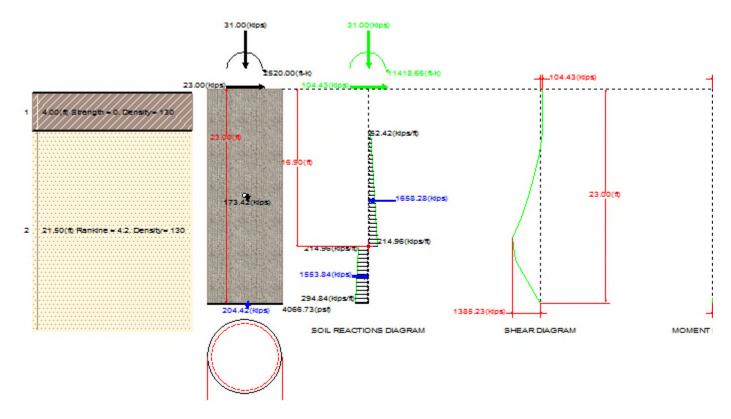
### Soil Properties

Layer	Type	Thickness	Depth at Top of Layer	Density	CU	KP	PHI
		(ft)	(ft)	(lbs/ft^3)	(psf)		(deg)
1 2	Clay Sand	4.00 21.50	0.00 4.00	130.0 130.0		4.200	37.98

### Design (Factored) Loads at Top of Pier

Additional Safety Factor Against Soil Failure	Shear Load	Axial Load	Moment
SOII FAILURE	(kips)	(kips)	(ft-k)
4.50	23.00	31.0	2520.0

\*\*\*\*\* R E S U L T S



Calculated Pier Properties

FDH Engineering Page 1/2

Total End-Bearing	Pressure Due To	Pressure Due To	Weight	Length
Pressure (psf)	Weight (psf)	Axial Load (psf)	(kips)	(ft)
4066.7	3450.0	616.7	173.416	23.000

### Ultimate Resisting Forces Along Pier

Туре	Distance of Top of Layer to Top of Pier	Thickness	Density	CU	KP	Force	Arm
	(ft)	(ft)	(lbs/ft^3)	(psf)		(kips)	(ft)
Clay	0.50	4.00	130.0			0.00	2.50
Sand	4.50	12.40	130.0		4.200	1658.28	11.96
Sand	16.90	6.10	130.0		4.200	-1553.84	20.11

### Shear and Moments Along Pier

Distance below Top of Pier (ft)	Shear (with Safety Factor) (kips)	Moment (with Safety Factor) (ft-k)	Shear (without Safety Factor) (kips)	Moment (without Safety Factor) (ft-k)
0.00	104.4	11418.7	23.2	2537.5
2.30	104.4	11658.9	23.2	2590.9
4.60	99.1	11898.8	22.0	2644.2
6.90	-59.1	11958.1	-13.1	2657.4
9.20	-286.7	11573.8	-63.7	2571.9
11.50	-583.5	10586.3	-129.7	2352.5
13.80	-949.7	8836.4	-211.0	1963.6
16.10	-1385.2	6164.5	-307.8	1369.9
18.40	-1217.6	2906.8	-270.6	646.0
20.70	-643.5	753.3	-143.0	167.4
23.00	0.0	0.0	0.0	0.0

### Reinforcement and Capacity

Total	Reinforcement	Usable	Usable
Reinforcement	Area	Axial	Moment
Percent		Capacity	Capacity
	(in^2)	(kips)	(ft-k)
0.44	31.85	31.0	5715.3

### US Standard Re-Bars (Select one of the following)

Quantity	Name	Area (in^2)	Diameter (in)	Spacing (in)
160 103 73 54 41 32 26	#4 #5 #6 #7 #8 #9	0.20 0.31 0.44 0.60 0.79 1.00	0.500 0.625 0.750 0.875 1.000 1.128	1.69 2.62 3.70 5.00 6.59 8.44 10.39
21 15	#11 #14	1.56 2.25	1.410 1.693	12.87 18.01

FDH Engineering Page 2/2

### Moment Capacity of Drilled Concrete Shaft (Caisson) for TIA Rev F or G

Note: Shaft assumed to have ties, not spiral, transverse reinforcing

### Site Data

Site Name: Guilford

Loads Already Factored			
For M (WL)	1.3	<disregard< td=""></disregard<>	
For P (DL)	1.3	<disregard< td=""></disregard<>	

Pier Properties			
Concrete:		_	
Pier Diameter =	8.0	ft	
Concrete Area =	7238.2	in <sup>2</sup>	
Reinforcement:			
Clear Cover to <b>Tie</b> =	3.00	in	
Horiz. <b>Tie</b> Bar Size=	5		
Vert. Cage Diameter =	7.28	ft	
Vert. Cage Diameter =	87.34	in	
<b>Vertical</b> Bar Size =	11		
Bar Diameter =	1.41	in	
Bar Area =	1.56	in <sup>2</sup>	
Number of Bars =	24		
As Total=	37.44	in <sup>2</sup>	
A s/ Aconc, Rho:	0.0052	0.52%	

ACI 10.5 , ACI 21.10.4, and IBC 1810.

Min As for Flexural, Tension Controlled, Shafts:

(3)\*(Sqrt(f'c)/Fy: 0.0032

200 / Fy: 0.0033

### Minimum Rho Check:

Actual Req'd Min. Rho:	0.33%	Flexural
Provided Rho:	0.52%	OK

Ref. Shaft Max Axial Capacities, φ Max(Pn or Tn):				
Max Pu = $(\phi = 0.65)$ Pn.				
Pn per ACI 318 (10-2)	13899.12	kips		
at Mu=(φ=0.65)Mn=	9742.13	ft-kips		
Max Tu, (φ=0.9) Tn =	2021.76	kips		
at Mu=φ=(0.90)Mn=	0.00	ft-kips		

Maximum Shaft Superimposed Forces			
TIA Revision: G			
Max. Factored Shaft Mu:	2657.4	ft-kips (* Note)	
Max. Factored Shaft Pu:	31	kips	
Max Axial Force Type: Comp.			

(\*) Note: Max Shaft Superimposed Moment does not necessarily equal to the shaft top reaction moment

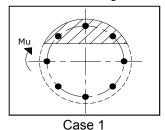
Load Factor	Shaft Factored Loads		
1.00	Mu:	2657.4	ft-kips
1.00	Pu:	31	kips

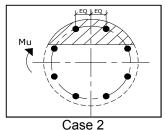
Material Properties				
Concrete Comp. strength, f'c =	4000	psi		
Reinforcement yield strength, Fy =	60	ksi		
Reinforcing Modulus of Elasticity, E =	29000	ksi		
Reinforcement yield strain =	0.00207	_		
Limiting compressive strain =	0.003			
ACI 318 Code				
Select Analysis ACI Code=	2005			
Seismic Properties				
Seismic Design Category =	Ċ			
Seismic Risk =	Moderate			

Solve	< Press Upon Completing All Input
(Run)	

### Results:

### Governing Orientation Case: 1





Dist. From Edge to Neutral Axis: 12.42 in Extreme Steel Strain, et: 0.0191

ct > 0.0050, Tension Controlled

Reduction Factor, $\varphi$ : **0.900** 

Output Note: Negative Pu=Tension

For Axial Compression,  $\varphi$  Pn = Pu: 31.00 kips Drilled Shaft Moment Capacity,  $\varphi$ Mn: 7037.43 ft-kips Drilled Shaft Superimposed Mu: 2657.40 ft-kips

(Mu/φMn, Drilled Shaft Flexure CSR: 37.8%