

August 27, 2013
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051
Attn: Ms. Melanie Bachman, Executive Director

## Re: 5 Perryridge Road - Greenwich, CT

Dear Ms. Bachman,

On behalf of Sprint Nextel Corporation ("Sprint"), enclosed for filing are One (1) original and two (2) copies of Sprint's Notice of Exempt Modification for Proposed Modifications to an Existing Telecommunications Facility located at the above-referenced site.

I also enclose herewith a check in the amount of $\$ 625.00$ representing the fee for the Notice of Exempt Modification.

If you have any questions, please feel free to contact me.
Thank you,
By: :F.Sagristano
Name: Paul F. Sagristano
Vertical Development LLC, an authorized representative of Sprint Nextel
Vertical Development LLC
20 Commercial Street
Branford, CT 06405
Phone - 917-841-0247
Fax - 401-633-6202
psagristano@verticaldevelopmentllc.com

CC: Mr. Peter Tesei, First Selectman
Greenwich Town Hall
101 Field Point Road
Greenwich, CT 06830

Greenwich Hospital, (Yale New Haven Health System) Property Owner
c/o Stephen Carbery VP Facilities
Yale New Haven Health System
789 Howard St.
New Haven, CT 06519

# Notice of Exempt Modification 5 Perryridge Road, Greenwich, CT 

Sprint Nextel Corporation ("Sprint") submits this Notice of Exempt Modification to the Connecticut Siting Council ("Council") pursuant to Sections 16-50j-73 and 16-50j72(b) of the Regulations of Connecticut State Agencies ("Regulations") in connection with Sprint's planned modification of antennas and associated equipment on an existing 164' Monopole tower located @ 5 Perryridge Road Greenwich, CT. More particularly, Sprint plans to upgrade this site by adding 4G LTE technology to its facilities. The proposed modifications will not increase the tower height, extend the boundaries of the tower site, cause a significant adverse change or alteration in the physical or environmental characteristics of the site, increase noise levels at the tower site boundary by six (6) decibels, add radio frequency sending or receiving capability which increases the total radio frequency electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the Federal Communications Commission pursuant to Section 704 of the Telecommunications Act of 1996, as amended, and the State Department of Energy and Environmental Protection, pursuant to Section 22a-162 of the Connecticut General Statutes, or impair the structural integrity of the facility, as determined in a certification provided by a professional engineer licensed in Connecticut.

To better meet the growing voice and data demands of its wireless customers, Sprint is upgrading their network nationwide to include 4G technology, which will provide faster service and better overall performance. Pursuant to the 4G upgrade at this site, Sprint will add antennas, install RRUs (Remote Radio Units) and install related equipment to its equipment area within the fenced tower compound.

The 164' Monopole located @ 5Perryridge Road Greenwich, CT (lat. $41^{\circ} .03419$ N , long. $73^{\circ} .63082 \mathrm{~W}$, is owned by Greenwich Hospital. It is located on a 7.3274 acre parcel. Sprint currently has three (3) antennas, one (1) antenna on each on three (3) sectors) with a centerline of $155^{\prime} 6^{\prime \prime}$ installed on the tower. Sprint's base station equipment is located inside a building adjacent to the base of the tower. A site plan depicting this is attached.

Sprint plans to add three (3) RFS APXVTM-14-C-I20 panel antennas, one (1) per sector, all with a centerline of 155' 6". Connected to each new RFS antenna will be one (1) ALU TD RRH $8 \times 20$ RRH which will be located behind the antenna. The height of the tower will not be increased. Sprint also plans to install a new 2500 MHz 9929 Growth Cabinet which is to be installed within the existing equipment building. The compound's boundaries will not be extended. The proposed modifications will not cause a significant adverse change or alteration in the physical or environmental characteristics of the site, since it is already a telecommunications installation and the modifications will be compatible with this. Other than brief, construction-related noise, these modifications will not increase noise levels at the tower site boundary by six (6) decibels.

The proposed modifications will not add radio frequency sending or receiving capability which increases the total radio frequency electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the Federal Communications Commission pursuant to Section 704 of the Telecommunications Act of 1996, as amended, and the State Department of Energy and Environmental Protection, pursuant to Section 22a-162 of the Connecticut General Statutes. A radio frequency emissions analysis prepared by EBI Consulting indicates that the proposed final configuration (including other carriers on the tower) will emit 90.29\% of the allowable FCC established general public limit sampled at the ground level (see the 3rd page of Emissions Analysis Report - Evaluation of Human Exposure Potential to Non-lonizing Emissions, August 23, 2014). Emission values for the Sprint antennas have been calculated from the sample point, which is the top of a six foot person standing at the base of the tower. Emissions values for additional carriers were based upon values listed in Connecticut Siting Council active database (see page 5 of Radio Frequency Emissions Analysis Report - Evaluation of Human Exposure Potential to Non-Ionizing Emissions, August 23, 2014). The information used in the report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1 (see the second page of Radio Frequency Emissions Analysis Report - Evaluation of Human Exposure Potential to Non-lonizing Emissions, August 23, 2014).

The proposed modifications will not impair the structural integrity of the facility. Sprint commissioned Infinigy Engineering to perform a structural analysis of the tower to verify that it can support the proposed loading. The structure and foundation were found to be of "Sufficient Capacity" with the proposed modifications (see the first page of Post-Mod Tower Analysis Report, June 12, 2014). The tower is rated at $47.2 \%$ of its capacity with the proposed modifications (see the first page of Post-Mod Tower Analysis Report, June 12, 2014).

In conclusion, Sprint's proposed modifications do not constitute a modification subject to the Council's review because Sprint will not change the height of the tower, will not extend the boundaries of the compound, will not cause a significant adverse change or alteration in the physical or environmental characteristics of the site, will not increase the noise levels at the site, will not increase the total radio frequency electromagnetic radiation power density at the site to levels above applicable standards, and will not impair the structural integrity of the facility. Therefore, Sprint respectfully requests that the Council acknowledge that this Notice of Exempt Modification meets the Council's exemption criteria.
environmental | engineering | due diligence

# RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT 

Sprint Existing Facility

Site ID: CT43XC855

Greenwich Hospital
5 Perryridge Road
Greenwich, CT 06830
August 23, 2014

EBI Project Number: 62144365

August 23, 2014

Sprint
Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495
Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site:
CT43XC855-Greenwich Hospital
Site Total: $\underline{\mathbf{9 0} .29 \%}$ - MPE \% in full compliance
EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 5 Perryridge Road, Greenwich, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm} 2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR $1.1307(b)(1)-(b)(3)$, to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limit for the cellular band ( 850 MHz Band) is approximately $567 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the 1900 MHz and 2500 MHz bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 5 Perryridge Road, Greenwich, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65 . All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

1) 3 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
6) The antennas used in this modeling are the RFS APXVSPP18-C-A20, POWERWAVE P40-16-XLPP-RR-A and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz . The POWERWAVE P40-16-XLPP-RR-A has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz . The RFS APXVTM14-C-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz . The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antenna mounting height centerline for the proposed antennas is $\mathbf{1 5 5}$ feet above ground level (AGL).
8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits


| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| Sprint | $2.53 \%$ |
| Verizon Wireless | $34.38 \%$ |
| AT\&T | $26.02 \%$ |
| MW to Bruce | $6.85 \%$ |
| MW to PD | $0.17 \%$ |
| MW to Putnam | $6.85 \%$ |
| Trunked system | $2.04 \%$ |
| Mutual Aid | $1.13 \%$ |
| CMED | $0.77 \%$ |
| FirePaging | $1.15 \%$ |
| SP Hotine | $1.49 \%$ |
| Clearwire | $0.78 \%$ |
| T-Mobie | $0.17 \%$ |
| Nextel | $5.96 \%$ |
| Total Site MPE \% | $\mathbf{9 0 . 2 9 \%}$ |

## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are $\mathbf{2 . 5 3 \%}$ ( $\mathbf{0 . 8 4 \%}$ from sector $\mathbf{1 , 0 . 8 4 \%}$ from sector $\mathbf{2}$ and $\mathbf{0 . 8 4 \%}$ from sector 3) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{9 0 . 2 9 \%}$ of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

RF Engineering Director

EBI Consulting
21 B Street
Burlington, MA 01803

## Tower Analysis Report

June 12, 2014

| Site Name | Greenwich Hospital - CT43XC855 |
| :--- | :--- |
| Infinigy Job Number | $333-000$ |
| Client | Sprint |
| Proposed Carrier | Sprint |
|  | 5 Perryridge Dr., Greenwich, CT 06830 |
| Site Location | Fairfield County |
|  | $41^{\circ} 2^{\prime} 2.04^{\prime \prime}$ N NAD83 |
|  | $73^{\circ} 37^{\prime} 50.8794^{\prime \prime}$ W NAD83 |
| Structure Type | $164^{\prime}$ Monopole |
| Structural Usage Ratio | $\mathbf{4 7 . 2 \%}$ |
| Overall Result | Pass |

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA code requirements. The tower and foundations are therefore deemed adequate to support the existing and proposed loading as listed in this report.


Maxwell R. Becker, E.I.T. Structural Engineer I

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## Introduction

Infinigy Engineering has been requested to perform a structural analysis on the existing $164^{\prime}$ Monopole. All supporting documents have been obtained from the client and are assumed to be accurate and applicable to this site. The tower was analyzed using tnxTower version 6.1.3.1 tower analysis software.

## Supporting Documentation

| Construction Drawings | Infinigy Engineering, Job \# 333-000, dated October 01, 2013 |
| :--- | :--- |
| Previous Analysis | Salient Associates Site \# CT43XC855, dated January 18, 2013 |

## Analysis Code Requirements

| Wind Speed | 100 mph (3-Second Gust) |
| :--- | :--- |
| Wind Speed w/ ice | 50 mph (3-Second Gust) w/ 3/4" ice |
| TIA Revision | ANSI/TIA-222-G |
| Adopted IBC | $2003 \mathrm{IBC} \mathrm{w} / 2005$ CT Supplement \& 2009 CT Amendment |
| Structure Class | 2 |
| Exposure Category | B |
| Topographic Category | 1 |
| Calculated Crest Height | 0 ft |

## Conclusion

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA code requirements. The tower and foundations are therefore deemed adequate to support the existing and proposed loading as listed in this report.

If you have any questions, require additional information, or actual conditions differ from those as detailed in this report please contact me via the information below:

Maxwell R. Becker, E.I.T.
Structural Engineer I | Infinigy
1033 Watervliet Shaker Road, Albany, NY 12205
(O) (518) 690-0790 | (M) (518) 221-4665
mbecker@infinigy.com | www.infinigy.com

## Existing and Reserved Loading

| Mount <br> Height (ft) | Qty. | Appurtenance | Mount Type | Coax\& Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 165.0 | 1 | Camera | Platform | (6) 1-5/8" | Town of Greenwich |
|  | 1 | GPS |  |  |  |
|  | 3 | RFS BMR12 |  |  |  |
|  | 1 | Celwave PD1142-1 |  |  |  |
|  | 1 | Celwave PD620-3 |  |  |  |
|  | 1 | Celwave ALR8-0 |  |  |  |
| 160.0 | 2 | 4 ft . STD Dish | Pipes | (3) 1-5/8" |  |
|  | 1 | Andrew VP2-180A | Pipe |  |  |
| 155.0 | 1 | GPS | Platform | (1) 2-1/4" <br> (2) $1 / 2^{\prime \prime}$ | Clearwire |
|  | 3 | Commscope LLPX310R |  |  |  |
|  | 2 | Dragonwave 24" Dish |  |  |  |
|  | 2 | RFS APXVSPP18-C |  |  |  |
|  | 1 | Powerwave P4-16-XLPP-RR-A |  | (1) $1 / 2$ " | Sprint |
| 152.0 | 3 | Alcatel-Lucent 800 MHz RRH |  | (3) $1-1 / 4$ " |  |
|  | 3 | Alcatel-Lucent 1900 MHz RRH |  | Hybriflex |  |
| 145.0 | 6 | RFS APX16PV-16PVL-C | Platform | (12) 1-5/8" | T-Mobile |
|  | 6 | Ericsson KRY 11271 |  |  |  |
| 135.0 | 6 | Powerwave 7770.00 | Platform | (12) 1-5/8" | AT\&T |
|  | 4 | Powerwave LGP 21401 TMA |  |  |  |
|  | 2 | Powerwave LGP 17201 TMA |  |  |  |
| 125.0 | 6 | Decibel DB844G45ZAXY | Platform | (18) 1-5/8" | Verizon Wireless |
|  | 3 | LNX-6514DS-T0M |  |  |  |
| 115.0 | 12 | Decibel DB846G90A-XY | Platform | (12) 1-5/8" | Nextel |

## Proposed Loading

| Mount <br> Height (ft) | Qty. | Appurtenance | Mount Type |  <br> Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 155.5 | 3 | RFS APXVTM14-C-120 | Platform | (3) 1-1/4" <br> Fiber | Sprint |
|  | 3 | Alcatel Lucent TD-RRH8X20 |  |  |  |

## Structure Usages

| Pole (T5) | 35.5 | Pass |
| :---: | :---: | :---: |
| Base Plate | 47.2 | Pass |
| RATING $=$ | $\mathbf{4 7 . 2}$ | Pass |

## Foundation Reactions

| Reaction Data | Design Reactions | Analysis Reactions | Result |
| :---: | :---: | :---: | :---: |
| Moment (kip) | -- | 4760.9 | -- |
| Shear (kip) | -- | 41.5 | -- |
| Axial (kip) | -- | 136.3 | -- |

The existing foundation was not evaluated because no information was made available at the time of this analysis.

## Deflection, Twist, and Sway

| Antenna Elevation (ft) | Deflection (in) | Twist $\left({ }^{\circ}\right)$ | Sway $\left({ }^{\circ}\right)$ |
| :---: | :---: | :---: | :---: |
| 155.5 | 5.71 | 0.00 | 0.29 |

*Per ANSI/TIA-222-G Section 2.8 .2 maximum serviceability structural deflection limit is $3 \%$ of structure height.
*Per ANSI/TIA-222-G Section 2.8.2 maximum serviceability structural twist and sway limit is 4 degrees.
*Per ANSI/TIA-222-G Section 2.8.3 deflection, Twist, and sway values were calculated using a basic 3-second gust wind speed of 60 mph .
*It is the responsibility of the client to ensure their proposed and/or existing equipment will meet ANSI/TIA-222-G Annex D or other appropriate microwave signal degradation limits based on the provided values above.

## Assumptions and Limitations

All engineering services are completed assuming all information provided to Infinigy Engineering is current and correct. If actual conditions differ from those described in this report we should be notified immediately to complete a revised evaluation.

It is the responsibility of the client to ensure that the information provided to Infinigy Engineering is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the design drawings and specifications that have been supplied.

All calculations are completed in accordance with generally accepted engineering principles and practices. Infinigy Engineering is not responsible the conclusions, opinions, and recommendations made by others based on the information we supply.

This report is an evaluation of the tower structure only and does not reflect adequacy of any existing antenna mounts, mount connections, or coax mounting attachments. These elements are assumed to be adequate for the purposes of this analysis and are assumed to have been installed per their manufacturer requirements.


DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :--- | :--- | :--- | :--- |
| Angle Low Profile Platform (Town of <br> Greenwich) | 165 | 1900 MHz RRH (Sprint) | 152 |
| BMR12-A (Town of Greenwich) | 165 | 1900 MHz RRH (Sprint) | 152 |
| BMR12-A (Town of Greenwich) | 165 | 1900 MHz RRH (Sprint) | 152 |
| BMR12-A (Town of Greenwich) | 165 | 800 MHz RRH (Sprint) | 152 |
| GPS (Town of Greenwich) | 165 | 800 MHz RRH (Sprint) | 152 |
| ALR8 (Town of Greenwich) | 165 | (2) KRY11271/2 (T-Mobile) | 145 |
| PD1142-1 (Town of Greenwich) | 165 | Angle Low Profile Platform (T-Mobile) | 145 |
| PD620 (Town of Greenwich) | 165 | (2) APX16PV-16PVL (T-Mobile) | 145 |
| Camera (Town of Greenwich) | 165 | (2) APX16PV-16PVL (T-Mobile) | 145 |
| Dish Pipe Mount (Town of Greenwich) | 160 | (2) APX16PV-16PVL (T-Mobile) | 145 |
| Dish Pipe Mount (Town of Greenwich) | 160 | (2) KRY11271/2 (T-Mobile) | 145 |
| Dish Pipe Mount (Town of Greenwich) | 160 | (2) KRY11271/2 (T-Mobile) | 145 |
| 4' Std. Dish (Town of Greenwhich) | 160 | (2) LGP21401 (ATI) | 135 |
| 4' Std. Dish (Town of Greenwhich) | 160 | (2) LGP17201 (ATI) | 135 |
| VP2-180A (Town of Greenwhich) | 160 | (2) 7700.00 (ATI) | 135 |
| APXVTM14-C-120 (Sprint) | 155.5 | (2) 7700.00 (ATI) | 135 |
| APXVTM14-C-120 (Sprint) | 155.5 | (2) 7700.00 (ATI) | 135 |
| APXVTM14-C-120 (Sprint) | 155.5 | (2) LGP21401 (ATI) | 135 |
| TD-RRH8X20 (Sprint) | 155.5 | Angle Low Profile Platform (ATI) | 135 |
| TD-RRH8X20 (Sprint) | 155.5 | DB844G45ZAXY (Verizon Wireless) | 125 |
| TD-RRH8X20 (Sprint) | 155.5 | DB844G45ZAXY (Verizon Wireless) | 125 |
| DB980F90E-M (Sprint) | 155 | LNX-6514DS-VTM (Verizon Wireless) | 125 |
| DB980F90E-M (Sprint) | 155 | LNX-6514DS-VTM (Verizon Wireless) | 125 |
| DB950F65T2E-M (Sprint) | 155 | LNX-6514DS-VTM (Verizon Wireless) | 125 |
| LLPX310R (Sprint) | 155 | Angle Low Profile Platform (Verizon | 125 |
| LLPX310R (Sprint) | 155 | Wireless) |  |
| LLPX310R (Sprint) | DB844G45ZAXY (Verizon Wireless) | 125 |  |
| P40-16-XLPP-RR-A (Sprint) | 155 | DB844G45ZAXY (Verizon Wireless) | 125 |
| Angle Low Profile Platform (Sprint) | 155 | DB844G45ZAXY (Verizon Wireless) | 125 |
| APXVSPP18-C-A20 (Sprint) | 155 | DB844G45ZAXY (Verizon Wireless) | 125 |
| APXVSPP18-C-A20 (Sprint) | 155 | (4) DB846G90A-XY (Nextel) | 115 |
| A-ANT-23G-24 (Sprint) | 155 | (4) DB846G90A-XY (Nextel) | 115 |
| A-ANT-23G-24 (Sprint) | 155 | (4) DB846G90A-XY (Nextel) | 115 |
| 800 MHz RRH (Sprint) | 152 | Angle Low Profile Platform (Nextel) | 115 |
|  |  |  |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A572-65 | 65 ksi | 80 ksi |  |  |  |  |

TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $80 \%$

ALL REACTIONS ARE FACTORED


TORQUE 5458 lb -ft
50 mph WIND - 0.7500 in ICE


TORQUE 21038 lb-ft
REACTIONS - 100 mph WIND

| Infinigy Engineering 2255 Sewell Mill Road, Suite 130 Marietta, GA 30062 | 1ob: 333-000 |  |  |
| :---: | :---: | :---: | :---: |
|  | Project: Greenwich Hospital |  |  |
|  | Client: Sprint | Drawn by: MBecker | App'd: |
| Phone: (678) 444-4463 | Code: TIA-222-G | Date: 06/09/14 | Scale: NTS |
| FAX: (678)444-4472 | Path: |  | ${ }^{\text {No. }}$ |


| tnxTower <br> Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Job | 333-000 | $\begin{array}{ll} \hline \text { Page } \\ & \\ \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |

## Tower Input Data

There is a pole section.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in Fairfield County, Connecticut.
Basic wind speed of 100 mph .
Structure Class II.
Exposure Category B.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 0.7500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf .
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
$\sqrt{ }$ Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile
$\sqrt{ }$ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section
$\sqrt{ }$ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform
Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r
$\sqrt{ }$ Retension Guys To Initial Tension Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
$\sqrt{ }$ Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component
$\sqrt{ }$ Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
$\sqrt{ }$ All Leg Panels Have Same Allowable Offset Girt At Foundation
$\sqrt{ }$ Consider Feedline Torque
$\sqrt{ }$ Include Angle Block Shear Check Poles
Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets

## Tapered Pole Section Geometry

| Section | Elevation <br> ft | Section <br> Length <br> ft | Splice <br> Length <br> ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 164.00-131.50 | 32.50 | 0.00 | 18 | 47.0000 | 53.4200 | 0.3125 | 1.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | 131.50-119.29 | 12.21 | 6.00 | 18 | 53.4200 | 56.1500 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |


| tnxTower <br> Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Job 333-000 |  | Page |
| :---: | :---: | :---: | :---: |
|  |  |  | 2 of 13 |
|  | Greenwich Hospital |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \\ \hline \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |


| Section | Elevation <br> $f t$ | Section Length $f t$ | Splice Length $f t$ | Number of Sides | Top <br> Diameter in | Bottom Diameter in | Wall Thickness in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 119.29-78.79 | 46.50 | 8.42 | 18 | 54.0585 | 62.9700 | 0.4375 | 1.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 78.79-39.88 | 47.33 | 9.25 | 18 | 60.4813 | 69.6600 | 0.5625 | 2.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L5 | 39.88-0.00 | 49.13 |  | 18 | 66.7412 | 76.0000 | 0.5625 | 2.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

## Tapered Pole Properties



## Monopole Base Plate Data

| Base Plate Data |  |
| :---: | :---: |
| Base plate is square |  |
| Base plate is grouted | A615-75 |
| Anchor bolt grade | 2.2500 in |
| Anchor bott size | 30 |
| Number of bolts | 48.0000 in |
| Embedment length | 3 ksi |
| $\mathrm{f}_{\mathrm{c}}$ | 2.0000 in |
| Grout space | A 36 |
| Base plate grade | 3.0000 in |


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| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | Date $14: 11: 52 \text { 06/09/14 }$ |
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| Base Plate Data |  |
| :---: | :---: |
| Bolt circle diameter | 86.0000 in |
| Outer diameter | 92.0000 in |
| Inner diameter | 74.5000 in |
| Base plate type | Plain Plate |

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow <br> Shield | Component Type | Placement <br> ft | Total Number | Number <br> Per Row | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & * * * \\ & * * * \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Area

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Allow Shield \& Component Type \& Placement
ft \& Total Number \& \& $C_{A} A_{A}$

$f t^{2} / f t$ \& Weight
plf <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{164.00-4.50} \& \multirow[t]{3}{*}{6} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{160.00-4.50} \& \multirow[t]{3}{*}{3} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{1/2} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{154.00-4.50} \& \multirow[t]{3}{*}{1} \& No Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.25 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{114.00-4.50} \& \multirow[t]{3}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$11 / 4$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{154.00-4.50} \& \multirow[t]{3}{*}{3} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.00 \& 0.66 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{124.00-6.00} \& \multirow[t]{3}{*}{6} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{124.00-6.00} \& \multirow[t]{3}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{134.00-8.00} \& \multirow[t]{3}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{144.00-10.00} \& \multirow[t]{3}{*}{12} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$15 / 8$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{154.00-4.50} \& \multirow[t]{3}{*}{6} \& No Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.04 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 1.04 <br>
\hline \multirow[t]{3}{*}{$21 / 4$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{154.00-4.50} \& \multirow[t]{3}{*}{1} \& No Ice \& 0.00 \& 1.16 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 1.16 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 0.00 \& 1.16 <br>
\hline \multirow[t]{3}{*}{1/2} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{154.00-4.50} \& \multirow[t]{3}{*}{2} \& No Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.25 <br>
\hline \multicolumn{9}{|l|}{***} <br>
\hline *** \& \& \& \& \& \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Allow Shield \& Component Type \& Placement
ft \& Total Number \& \& $C_{A} A_{A}$

$f t^{2} / f t$ \& Weight
plf <br>
\hline \multirow[t]{3}{*}{$11 / 4$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{155.50-4.50} \& \multirow[t]{3}{*}{3} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.66 <br>
\hline \multirow[t]{3}{*}{1-1/4" Hybrid} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{No} \& \multirow[t]{3}{*}{Inside Pole} \& \multirow[t]{3}{*}{155.50-4.50} \& \multirow[t]{3}{*}{3} \& No Ice \& 0.00 \& 0.83 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.83 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.83 <br>
\hline
\end{tabular}

## Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation ft \& Face \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $C_{A} A_{A}$ Out Face $f t^{2}$ \& Weight
lb <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{164.00-131.50} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 227.93 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 244.92 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 341.50 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{131.50-119.29} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 182.47 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 219.87 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 283.26 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{119.29-78.79} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 915.71 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 884.52 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1378.98 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{78.79-39.88} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 879.76 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 849.79 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1388.27 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{39.88-0.00} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 781.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 694.70 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1218.64 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower \\
Section
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Ice Thickness in \& \(A_{R}\)
\(f t^{2}\) \& \(A_{F}\)

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $C_{A} A_{A}$ Out Face $f t^{2}$ \& | Weight |
| :--- |
| $l b$ | <br>

\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{164.00-131.50} \& A \& \multirow[t]{3}{*}{1.742} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 227.93 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 244.92 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 341.50 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{131.50-119.29} \& A \& \multirow[t]{3}{*}{1.714} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 182.47 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 219.87 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 283.26 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{119.29-78.79} \& A \& \multirow[t]{3}{*}{1.674} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 915.71 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 884.52 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1378.98 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{78.79-39.88} \& A \& \multirow[t]{3}{*}{1.591} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 879.76 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 849.79 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1388.27 <br>
\hline \multirow[t]{3}{*}{L5} \& \multirow[t]{3}{*}{39.88-0.00} \& A \& \multirow[t]{3}{*}{1.424} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 781.22 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 694.70 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1218.64 <br>
\hline
\end{tabular}

## Feed Line Center of Pressure

| tnxTOWer | Job | Page |  |
| :---: | :--- | :--- | :--- |
|  | Project | Client | Greenwich Hospital |


| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ <br> Ice | $C P_{Z}$ <br> Ice |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | in | in | in |
| ft | in | in | 0.0000 | 0.0000 | 0.0000 |
| L1 | $164.00-131.50$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L3 | $131.50-119.29$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L4 | $119.29-78.79$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L5 | $78.79-39.88$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

## Shielding Factor Ka

| Tower |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Feed Line |
| Record No. |  |$\quad$ Description | Feed Line | $K_{a}$ |
| :---: | :---: |
| Segment Elev. | No Ice | | $K_{a}$ |
| :---: |
| Ice |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ Front |
| :--- |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight

$l b$ <br>
\hline \multirow[t]{3}{*}{Angle Low Profile Platform (Town of Greenwich)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 0.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 26.10 \& 26.10 \& 1500.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 31.60 \& 31.60 \& 1700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 37.10 \& 37.10 \& 1900.00 <br>

\hline \multirow[t]{3}{*}{| BMR12-A |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 13.25 \& 13.25 \& 92.00 <br>

\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 15.31 \& 15.31 \& 180.53 <br>
\hline \& \& \& 5.00 \& \& \& $1{ }^{1 /}$ Ice \& 17.39 \& 17.39 \& 282.10 <br>

\hline \multirow[t]{3}{*}{| BMR12-A |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 13.25 \& 13.25 \& 92.00 <br>

\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 15.31 \& 15.31 \& 180.53 <br>
\hline \& \& \& 5.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 17.39 \& 17.39 \& 282.10 <br>

\hline \multirow[t]{3}{*}{| BMR12-A |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 13.25 \& 13.25 \& 92.00 <br>

\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 15.31 \& 15.31 \& 180.53 <br>
\hline \& \& \& 5.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 17.39 \& 17.39 \& 282.10 <br>

\hline \multirow[t]{3}{*}{| GPS |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 0.50 \& 0.50 \& 10.00 <br>

\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 0.63 \& 0.63 \& 15.96 <br>
\hline \& \& \& 3.00 \& \& \& 1" Ice \& 0.78 \& 0.78 \& 23.49 <br>

\hline \multirow[t]{3}{*}{| ALR8 |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 8.10 \& 8.10 \& 70.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 9.29 \& 9.29 \& 80.00 <br>
\hline \& \& \& 5.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 10.48 \& 10.48 \& 90.00 <br>
\hline \multirow[t]{3}{*}{PD1142-1
(Town of Greenwich)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 1.86 \& 1.86 \& 10.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.76 \& 3.76 \& 27.21 <br>
\hline \& \& \& 5.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.67 \& 5.67 \& 56.16 <br>
\hline \multirow[t]{3}{*}{PD620
(Town of Greenwich)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{165.00} \& No Ice \& 4.27 \& 4.27 \& 53.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.68 \& 7.68 \& 95.00 <br>
\hline \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 11.09 \& 11.09 \& 137.00 <br>

\hline \multirow[t]{3}{*}{| Camera |
| :--- |
| (Town of Greenwich) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{165.00} \& No Ice \& 1.40 \& 2.80 \& 15.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.56 \& 3.04 \& 39.92 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 1.73 \& 3.28 \& 68.15 <br>
\hline \multicolumn{6}{|l|}{***} \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Dish Pipe Mount (Town of Greenwich)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{160.00} \& No Ice \& 2.09 \& 2.09 \& 54.66 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.46 \& 2.46 \& 80.59 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.85 \& 2.85 \& 110.49 <br>
\hline \multirow[t]{3}{*}{Dish Pipe Mount (Town of Greenwich)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 1.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{160.00} \& No Ice \& 2.09 \& 2.09 \& 54.66 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.46 \& 2.46 \& 80.59 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.85 \& 2.85 \& 110.49 <br>
\hline
\end{tabular}

| tnxTower <br> Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Job | 333-000 | Page 6 of 13 |
| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | Date 14:11:52 06/09/14 |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |



| tnxTower | Job | 333-000 | Page |
| :---: | :---: | :---: | :---: |
|  |  |  | 7 of 13 |
| Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
ft \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

ft \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight

$l b$ <br>
\hline \multirow[t]{2}{*}{(T-Mobile)} \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.27 \& 3.94 \& 93.66 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.75 \& 4.58 \& 147.19 <br>
\hline \multirow[t]{3}{*}{(2) APX16PV-16PVL (T-Mobile)} \& C \& From Leg \& 4.00 \& 0.0000 \& 145.00 \& No Ice \& 6.80 \& 3.31 \& 46.95 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.27 \& 3.94 \& 93.66 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.75 \& 4.58 \& 147.19 <br>

\hline \multirow[t]{3}{*}{| (2) KRY11271/2 |
| :--- |
| (T-Mobile) |} \& A \& From Leg \& 4.00 \& 0.0000 \& 145.00 \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.80 \& 0.56 \& 18.38 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.93 \& 0.68 \& 25.16 <br>

\hline \multirow[t]{3}{*}{| (2) KRY11271/2 |
| :--- |
| (T-Mobile) |} \& B \& From Leg \& 4.00 \& 0.0000 \& 145.00 \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.80 \& 0.56 \& 18.38 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.93 \& 0.68 \& 25.16 <br>
\hline \multirow[t]{3}{*}{(2) KRY11271/2 (T-Mobile)} \& C \& From Leg \& 4.00 \& 0.0000 \& 145.00 \& No Ice \& 0.68 \& 0.45 \& 13.20 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.80 \& 0.56 \& 18.38 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.93 \& 0.68 \& 25.16 <br>
\hline \multirow[t]{3}{*}{Angle Low Profile Platform (T-Mobile)} \& C \& From Leg \& 0.00 \& 0.0000 \& 145.00 \& No Ice \& 26.10 \& 26.10 \& 1500.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 31.60 \& 31.60 \& 1700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 37.10 \& 37.10 \& 1900.00 <br>
\hline \multirow[t]{2}{*}{(2) $77 * * *$} \& \& \& \& \& \& \& \& \& <br>
\hline \& A \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 1.58 \& 0.82 \& 22.00 <br>
\hline \multirow[t]{2}{*}{(AT\&T)} \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.00 \& 31.66 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.02 \& 1.19 \& 43.84 <br>

\hline \multirow[t]{3}{*}{| (2) 7700.00 |
| :--- |
| (AT\&T) |} \& B \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 1.58 \& 0.82 \& 22.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.00 \& 31.66 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.02 \& 1.19 \& 43.84 <br>

\hline \multirow[t]{3}{*}{| (2) 7700.00 |
| :--- |
| (AT\&T) |} \& C \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 1.58 \& 0.82 \& 22.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.79 \& 1.00 \& 31.66 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.02 \& 1.19 \& 43.84 <br>

\hline \multirow[t]{3}{*}{| (2) LGP21401 |
| :--- |
| (AT\&T) |} \& A \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 0.95 \& 0.37 \& 17.50 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.09 \& 0.48 \& 23.31 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.24 \& 0.60 \& 30.86 <br>

\hline \multirow[t]{3}{*}{| (2) LGP21401 |
| :--- |
| (AT\&T) |} \& C \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 0.95 \& 0.37 \& 17.50 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.09 \& 0.48 \& 23.31 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.24 \& 0.60 \& 30.86 <br>

\hline \multirow[t]{3}{*}{| (2) LGP17201 |
| :--- |
| (AT\&T) |} \& B \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 1.95 \& 0.50 \& 31.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.13 \& 0.62 \& 41.95 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.33 \& 0.75 \& 55.17 <br>
\hline \multirow[t]{3}{*}{Angle Low Profile Platform (AT\&T)} \& C \& From Leg \& 4.00 \& 0.0000 \& 135.00 \& No Ice \& 26.10 \& 26.10 \& 1500.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 31.60 \& 31.60 \& 1700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 37.10 \& 37.10 \& 1900.00 <br>
\hline \multirow[t]{2}{*}{DB844G457AXY} \& \& \& \& \& \& \& \& \& <br>
\hline \& A \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>
\hline \multirow[t]{2}{*}{(Verizon Wireless)} \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline \& \& \& 6.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \multirow[t]{3}{*}{| DB844G45ZAXY |
| :--- |
| (Verizon Wireless) |} \& B \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline \& \& \& 6.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \multirow[t]{3}{*}{| DB844G45ZAXY |
| :--- |
| (Verizon Wireless) |} \& C \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline \& \& \& 6.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \multirow[t]{3}{*}{| DB844G45ZAXY |
| :--- |
| (Verizon Wireless) |} \& A \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline \& \& \& -6.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \multirow[t]{3}{*}{| DB844G45ZAXY |
| :--- |
| (Verizon Wireless) |} \& B \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline \& \& \& -6.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \multirow[t]{2}{*}{| DB844G45ZAXY |
| :--- |
| (Verizon Wireless) |} \& C \& From Leg \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 7.00 \& 3.97 \& 21.00 <br>

\hline \& \& \& 0.00 \& \& \& $1 / 2$ Ice \& 7.41 \& 4.34 \& 64.04 <br>
\hline
\end{tabular}

| tnxTower | Job | 333-000 | Page |
| :---: | :---: | :---: | :---: |
|  |  |  | 8 of 13 |
| Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
ft \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
f t^{2}
$$ \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight

$l b$ <br>

\hline \multirow{4}{*}{| LNX-6514DS-VTM |
| :--- |
| (Verizon Wireless) |} \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& -6.00 \& \& \& 1" Ice \& 7.83 \& 4.72 \& 111.90 <br>

\hline \& \& \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 8.41 \& 5.88 \& 38.30 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.96 \& 6.34 \& 91.03 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 9.52 \& 6.81 \& 149.94 <br>

\hline \multirow[t]{3}{*}{| LNX-6514DS-VTM |
| :--- |
| (Verizon Wireless) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 8.41 \& 5.88 \& 38.30 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.96 \& 6.34 \& 91.03 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 9.52 \& 6.81 \& 149.94 <br>

\hline \multirow[t]{3}{*}{| LNX-6514DS-VTM |
| :--- |
| (Verizon Wireless) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 125.00 \& No Ice \& 8.41 \& 5.88 \& 38.30 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.96 \& 6.34 \& 91.03 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 9.52 \& 6.81 \& 149.94 <br>
\hline \multirow[t]{3}{*}{Angle Low Profile Platform (Verizon Wireless)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 0.00 \& 0.0000 \& 125.00 \& No Ice \& 26.10 \& 26.10 \& 1500.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 31.60 \& 31.60 \& 1700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 37.10 \& 37.10 \& 1900.00 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Angle Low Profile Platform (Nextel)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 0.00 \& 0.0000 \& 115.00 \& No Ice \& 26.10 \& 26.10 \& 1500.00 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 31.60 \& 31.60 \& 1700.00 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 37.10 \& 37.10 \& 1900.00 <br>
\hline \multirow[t]{3}{*}{(4) DB846G90A-XY (Nextel)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 115.00 \& No Ice \& 4.99 \& 5.87 \& 15.40 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.44 \& 6.32 \& 53.75 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 5.90 \& 6.79 \& 97.91 <br>
\hline \multirow[t]{3}{*}{(4) DB846G90A-XY (Nextel)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 115.00 \& No Ice \& 4.99 \& 5.87 \& 15.40 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.44 \& 6.32 \& 53.75 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 5.90 \& 6.79 \& 97.91 <br>
\hline \multirow[t]{3}{*}{(4) DB846G90A-XY (Nextel)} \& \multirow[t]{6}{*}{C} \& \multirow[t]{6}{*}{From Leg} \& 4.00 \& 0.0000 \& 115.00 \& No Ice \& 4.99 \& 5.87 \& 15.40 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 5.44 \& 6.32 \& 53.75 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 5.90 \& 6.79 \& 97.91 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{| APXVTM14-C-120 |
| :--- |
| (Sprint) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 6.53 \& 3.38 \& 52.90 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.96 \& 3.72 \& 90.49 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.40 \& 4.07 \& 132.96 <br>

\hline \multirow[t]{3}{*}{| APXVTM14-C-120 |
| :--- |
| (Sprint) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 6.53 \& 3.38 \& 52.90 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.96 \& 3.72 \& 90.49 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 7.40 \& 4.07 \& 132.96 <br>

\hline \multirow[t]{3}{*}{| APXVTM14-C-120 |
| :--- |
| (Sprint) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 6.53 \& 3.38 \& 52.90 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.96 \& 3.72 \& 90.49 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 7.40 \& 4.07 \& 132.96 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { TD-RRH8X20 } \\
& \text { (Sprint) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 4.32 \& 1.41 \& 66.14 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 4.60 \& 1.61 \& 90.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 4.89 \& 1.83 \& 117.36 <br>
\hline \multirow[t]{3}{*}{TD-RRH8X20 (Sprint)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 4.32 \& 1.41 \& 66.14 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 4.60 \& 1.61 \& 90.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 /}$ Ice \& 4.89 \& 1.83 \& 117.36 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { TD-RRH8X20 } \\
& \text { (Sprint) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& 0.0000 \& 155.50 \& No Ice \& 4.32 \& 1.41 \& 66.14 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 4.60 \& 1.61 \& 90.08 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{1 \prime}$ Ice \& 4.89 \& 1.83 \& 117.36 <br>
\hline
\end{tabular}

| tnxTower <br> Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Job |  | Page 9 of 13 |
| :---: | :---: | :---: | :---: |
|  | Greenwich Hospital |  | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or Leg
\end{tabular} \& \[
\begin{aligned}
\& \text { Dish } \\
\& \text { Type }
\end{aligned}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft
\end{tabular} \& Azimuth Adjustment \& \begin{tabular}{l}
\(3 d B\) \\
Beam \\
Width \\
。
\end{tabular} \& Elevation \& \begin{tabular}{l}
Outside Diameter \\
ft
\end{tabular} \& \& \begin{tabular}{l}
Aperture \\
Area \\
\(f t^{2}\)
\end{tabular} \& Weight

$l b$ <br>
\hline 4' Std. Dish \& A \& Paraboloid w/o \& From \& 1.00 \& 0.0000 \& \& 160.00 \& 4.00 \& No Ice \& 12.57 \& 190.00 <br>
\hline (Town of \& \& Radome \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 13.10 \& 260.00 <br>
\hline Greenwhich) \& \& \& \& 0.00 \& \& \& \& \& 1" Ice \& 13.62 \& 320.00 <br>
\hline 4' Std. Dish \& B \& Paraboloid w/o \& From \& 1.00 \& 0.0000 \& \& 160.00 \& 4.00 \& No Ice \& 12.57 \& 190.00 <br>
\hline (Town of \& \& Radome \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 13.10 \& 260.00 <br>
\hline Greenwhich) \& \& \& \& 0.00 \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 13.62 \& 320.00 <br>
\hline VP2-180A \& C \& Paraboloid w/o \& From \& 1.00 \& 0.0000 \& \& 160.00 \& 2.50 \& No Ice \& 4.91 \& 64.00 <br>
\hline (Town of \& \& Radome \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 5.24 \& 90.90 <br>
\hline $\underset{* * *}{\text { Greenwhich }}$ \& \& \& \& 0.00 \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.57 \& 117.80 <br>

\hline \multirow[t]{3}{*}{| A-ANT-23G-24 |
| :--- |
| (Sprint) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{Paraboloid w/Radome} \& \multirow[t]{3}{*}{From Leg} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{2.17} \& No Ice \& 3.72 \& 12.30 <br>

\hline \& \& \& \& 0.00 \& \& \& \& \& 1/2" Ice \& 4.01 \& 32.88 <br>
\hline \& \& \& \& -6.50 \& \& \& \& \& 1" Ice \& 4.30 \& 53.47 <br>

\hline \multirow[t]{3}{*}{| A-ANT-23G-24 |
| :--- |
| (Sprint) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{Paraboloid w/Radome} \& From \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \& \multirow[t]{3}{*}{155.00} \& \multirow[t]{3}{*}{2.17} \& No Ice \& 3.72 \& 12.30 <br>

\hline \& \& \& Leg \& 0.00 \& \& \& \& \& 1/2" Ice \& 4.01 \& 32.88 <br>
\hline \& \& \& \& 6.50 \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 4.30 \& 53.47 <br>
\hline
\end{tabular}

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.6 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.6 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.6 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.6 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.6 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.6 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.6 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.6 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.6 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.6 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.6 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.6 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.6 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.6 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.6 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.6 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.6 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.6 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.6 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.6 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.6 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.6 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.6 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.6 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind $90 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind $180 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind $210 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind $240 \mathrm{deg}+1.0$ Ice+1.0 Temp |


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| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | Date $14: 11: 52 \text { 06/09/14 }$ |
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| Comb. <br> No. |  | Description |
| :---: | :--- | :--- |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice +1.0 Temp |  |
| 37 | 1.2 Dead+1.0 Wind 300 deg +1.0 Ice +1.0 Temp |  |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice +1.0 Temp |  |
| 39 | Dead+Wind 0 deg - Service |  |
| 40 | Dead+Wind 30 deg - Service |  |
| 41 | Dead+Wind 60 deg - Service |  |
| 42 | Dead+Wind 90 deg - Service |  |
| 43 | Dead+Wind 120 deg - Service |  |
| 44 | Dead+Wind 150 deg - Service |  |
| 45 | Dead+Wind 180 deg - Service |  |
| 46 | Dead+Wind 210 deg - Service |  |
| 47 | Dead+Wind 240 deg - Service |  |
| 48 | Dead+Wind 270 deg - Service |  |
| 49 | Dead+Wind 300 deg - Service |  |
| 50 | Dead+Wind 330 deg - Service |  |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 165.00 | Angle Low Profile Platform | 47 | 6.363 | 0.3033 | 0.0047 | 272990 |
| 161.50 | A-ANT-23G-24 | 47 | 6.205 | 0.3022 | 0.0046 | 272990 |
| 160.00 | 4' Std. Dish | 47 | 6.109 | 0.3016 | 0.0046 | 272990 |
| 155.50 | APXVTM14-C-120 | 47 | 5.824 | 0.2995 | 0.0045 | 160583 |
| 155.00 | Angle Low Profile Platform | 47 | 5.793 | 0.2993 | 0.0045 | 151661 |
| 152.00 | 1900 MHz RRH | 47 | 5.604 | 0.2977 | 0.0044 | 113746 |
| 148.50 | A-ANT-23G-24 | 47 | 5.384 | 0.2957 | 0.0043 | 88061 |
| 145.00 | (2) APX16PV-16PVL | 47 | 5.167 | 0.2935 | 0.0042 | 71839 |
| 135.00 | (2) 7700.00 | 47 | 4.557 | 0.2848 | 0.0038 | 47101 |
| 125.00 | DB844G45ZAXY | 47 | 3.973 | 0.2721 | 0.0033 | 41110 |
| 115.00 | Angle Low Profile Platform | 47 | 3.418 | 0.2562 | 0.0029 | 38002 |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $164-131.5$ | 30.496 | 18 | 1.4316 |
| L1 | $131.5-119.29$ | 20.965 | 18 | 1.3357 | 0.0233 |
| L2 |  |  |  | 0.0181 |  |


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| :---: | :---: | :---: | :---: |
|  | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |


| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in in | Tilt | Twist 。 | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 165.00 | Angle Low Profile Platform | 18 | 30.496 | 1.4316 | 0.0233 | 63256 |
| 161.50 | A-ANT-23G-24 | 18 | 29.746 | 1.4270 | 0.0230 | 63256 |
| 160.00 | 4' Std. Dish | 18 | 29.297 | 1.4243 | 0.0228 | 63256 |
| 155.50 | APXVTM14-C-120 | 18 | 27.950 | 1.4155 | 0.0222 | 37209 |
| 155.00 | Angle Low Profile Platform | 18 | 27.801 | 1.4145 | 0.0222 | 35142 |
| 152.00 | 1900 MHz RRH | 18 | 26.908 | 1.4080 | 0.0218 | 26356 |
| 148.50 | A-ANT-23G-24 | 18 | 25.870 | 1.3995 | 0.0213 | 20405 |
| 145.00 | (2) APX16PV-16PVL | 18 | 24.840 | 1.3898 | 0.0207 | 16646 |
| 135.00 | (2) 7700.00 | 18 | 21.952 | 1.3528 | 0.0189 | 10912 |
| 125.00 | DB844G45ZAXY | 18 | 19.172 | 1.2976 | 0.0165 | 9308 |
| 115.00 | Angle Low Profile Platform | 18 | 16.522 | 1.2265 | 0.0142 | 8443 |

## Base Plate Design Data

| Plate Thickness | Number of Anchor Bolts | Anchor Bolt | Actual | Actual | Actual | Actual | Controlling Condition | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Size | Allowable | Allowable | Allowable | Allowable |  |  |
|  |  |  | Ratio | Ratio | Ratio | Ratio |  |  |
|  |  |  | Bolt | Bolt | Plate | Stiffener |  |  |
|  |  |  | Tension | Compression | Stress | Stress |  |  |
| in |  | in | $l b$ | $l b$ | ksi | ksi |  |  |
| 3.0000 | 30 | 2.2500 | 86580.37 | 92882.78 | 25.935 |  | Plate | 0.80 |
|  |  |  | 223654.40 | 371266.30 | 32.400 |  |  | 1 |
|  |  |  | 0.39 | 0.25 | 0.80 |  |  |  |

## Compression Checks

## Pole Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $\mathrm{in}^{2}$ | $l b$ | $l b$ | $\phi P_{n}$ |
| L1 | 164-131.5 (1) | TP53.42x47x0.3125 | 32.50 | 164.00 | 104.4 | 52.6760 | -17514.80 | 1092120.00 | 0.016 |
| L2 | $\begin{gathered} 131.5-119.29 \\ \text { (2) } \end{gathered}$ | TP56.15x53.42x0.375 | 12.21 | 164.00 | 101.8 | 64.7894 | -19548.00 | 1411180.00 | 0.014 |
| L3 | $\begin{gathered} 119.29-78.79 \\ \text { (3) } \end{gathered}$ | TP62.97x54.0585x0.4375 | 46.50 | 164.00 | 91.0 | 84.5934 | -40955.70 | 2300840.00 | 0.018 |
| L4 | 78.79-39.88 | TP69.66x60.4813x0.5625 | 47.33 | 164.00 | 82.4 | 120.162 | -65357.30 | 3896170.00 | 0.017 |


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|  | Project | Greenwich Hospital | Date $14: 11: 52 \text { 06/09/14 }$ |
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| Section <br> No. | Elevation ft | Size | ft | $\begin{gathered} L_{u} \\ f t \end{gathered}$ | Kl/r | A $i n^{2}$ | $P_{u}$ <br> lb | $\phi P_{n}$ <br> lb | $\begin{gathered} \hline \text { Ratio } \\ P_{u} \\ \hline \phi P_{n} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L5 | $\begin{gathered} (4) \\ 39.88-0(5) \end{gathered}$ | TP76x66.7412x0.5625 | 49.13 | 164.00 | 73.5 | $\begin{gathered} 0 \\ 134.684 \\ 0 \end{gathered}$ | -99818.40 | 5041620.00 | 0.020 |

## Pole Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \\ \hline \end{gathered}$ | $M_{u y}$ | $\phi M_{n y}$ | Ratio $M_{u y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | $l b-f t$ | $l b-f t$ | $\phi M_{n x}$ | $l b-f t$ | $l b-f t$ | $\phi M_{n y}$ |
| L1 | 164-131.5 (1) | TP53.42x47x0.3125 | 420606.67 | 3531850.00 | 0.119 | 0.00 | 3531850.00 | 0.000 |
| L2 | $\begin{gathered} 131.5-119.29 \\ (2) \end{gathered}$ | TP56.15x53.42x0.375 | 538480.00 | 4783283.33 | 0.113 | 0.00 | 4783283.33 | 0.000 |
| L3 | 119.29-78.79 <br> (3) | TP62.97x54.0585x0.4375 | 1606866.67 | 7104258.00 | 0.226 | 0.00 | 7104258.00 | 0.000 |
| L4 | $78.79-39.88$ <br> (4) | TP69.66x60.4813x0.5625 | 2904400.00 | 11742749.33 | 0.247 | 0.00 | 11742749.33 | 0.000 |
| L5 | 39.88-0 (5) | TP76x66.7412x0.5625 | 4840125.00 | 14202666.67 | 0.341 | 0.00 | 14202666.67 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | Actual $T_{u}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | $l b$ | $l b$ | $\phi V_{n}$ | $l b-f t$ | $l b-f t$ | $\phi T_{n}$ |
| L1 | 164-131.5 (1) | TP53.42x47x0.3125 | 18550.60 | 1613880.00 | 0.011 | 391.61 | 7072341.33 | 0.000 |
| L2 | $131.5-119.29$ <br> (2) | TP56.15x53.42x0.375 | 19420.50 | 2134620.00 | 0.009 | 391.61 | 9578250.00 | 0.000 |
| L3 | $119.29-78.79$ <br> (3) | TP62.97x54.0585x0.4375 | 31456.70 | 2833690.00 | 0.011 | 391.57 | 14225916.00 | 0.000 |
| L4 | $78.79-39.88$ <br> (4) | TP69.66x60.4813x0.5625 | 36529.30 | 4244460.00 | 0.009 | 391.49 | 23514165.33 | 0.000 |
| L5 | 39.88-0 (5) | TP76x66.7412x0.5625 | 41952.30 | 4576000.00 | 0.009 | 18087.58 | 28440082.67 | 0.001 |

## Pole Interaction Design Data

| Section No. | Elevation | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u x} \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ M_{u y} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ | Comb. <br> Stress | Allow. <br> Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  | ${ }_{\phi} P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ |  | Ratio |  |
| L1 | 164-131.5 (1) | 0.016 | 0.119 | 0.000 | 0.011 | 0.000 | ${ }^{0.135}$ | 1.000 | 4.8.2 |
| L2 | $\begin{aligned} & 131.5-119.29 \\ & \text { (2) } \end{aligned}$ | 0.014 | 0.113 | 0.000 | 0.009 | 0.000 | ${ }^{0.127}$ | 1.000 | 4.8.2 |
| L3 | $\begin{aligned} & 119.29-78.79 \\ & \text { (3) } \end{aligned}$ | 0.018 | 0.226 | 0.000 | 0.011 | 0.000 | $0.244$ | 1.000 | 4.8.2 |
| L4 | $78.79-39.88$ <br> (4) | 0.017 | 0.247 | 0.000 | 0.009 | 0.000 | ${ }^{0.264}$ | 1.000 | 4.8.2 |


| tnxTower | Job |  | $\begin{array}{\|l\|l\|} \hline \text { Page } \\ & \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: |
|  |  | 333-000 |  |
| Infinigy Engineering 2255 Sewell Mill Road, Suite 130 | Project | Greenwich Hospital | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:11:52 06/09/14 } \\ \hline \end{array}$ |
| Marietta, GA 30062 <br> Phone: (678) 444-4463 <br> FAX: (678)444-4472 | Client | Sprint | Designed by MBecker |


| Section No. | Elevation <br> $f t$ | Ratio $\frac{P_{u}}{\phi P_{n}}$ | $\begin{gathered} \begin{array}{c} \text { Ratio } \\ M_{u x} \end{array} \\ \hline \phi M_{n x} \end{gathered}$ | Ratio <br> $M_{u y}$ <br> $\phi M_{n y}$ | Ratio $V_{u}$ $\phi V_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \phi T_{n} \\ \hline \end{gathered}$ | Comb. <br> Stress <br> Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L5 | 39.88-0 (5) | 0.020 | 0.341 | 0.000 | 0.009 | 0.001 | $0.361$ | 1.000 | 4.8.2 |

## Section Capacity Table

| Section <br> No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} \phi P_{\text {allow }} \\ l b \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 164-131.5 | Pole | TP53.42x47x0.3125 | 1 | -17514.80 | 1092120.00 | 13.5 | Pass |
| L2 | 131.5-119.29 | Pole | TP56.15x53.42x0.375 | 2 | -19548.00 | 1411180.00 | 12.7 | Pass |
| L3 | 119.29-78.79 | Pole | TP62.97x54.0585x0.4375 | 3 | -40955.70 | 2300840.00 | 24.4 | Pass |
| L4 | 78.79-39.88 | Pole | TP69.66x60.4813x0.5625 | 4 | -65357.30 | 3896170.00 | 26.4 | Pass |
| L5 | 39.88-0 | Pole | TP76x66.7412x0.5625 | 5 | -99818.40 | 5041620.00 | 36.1 | Pass |
|  |  |  |  |  |  | Summary |  |  |
|  |  |  |  |  |  | Pole (L5) | 36.1 | Pass |
|  |  |  |  |  |  | Base Plate | 80.0 | Pass |
|  |  |  |  |  |  | RATING = | 80.0 | Pass |




THESE OUTLINE SPECIILCATIONS IN CONUUNCTION WITH THE SPRINT STANDARD CONSTRUCTION SPECIFICATIONS, INCLUOING CONTRACT DOCUMENTS
ANO THE CONSTRUCTION DRAWINGS DESCRBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

SECTION 01100 - SCOPE OF WORK


1.2 related documents:
A. THE RECQUREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS

1.3 PRECEDENCEE SHOULD CONFLLTSS OCCUR BETWEEN THE STANAARD CONSTRUCTION
SPECFICCATONS FOR WRELESS SITES INCLUONG THE STANOARO CONSTRUCTON DETALS

. 4 NATIONALIY RECOGNIZED CODES AND STANDARDS:


1. GR-63-CORE NEBS REQuirements: phrsical Protection
2. GR-78-CORE GENERCR REOUREMENTS FOR THE PHVSICAL DESIGN AND
3. GR-1089 CORE, ELECTROMAGNETC COMPATBLIUTY AND ELECTRICAL SAEET
 INCLLDING NFPA 70
(LIFE SAFETY COOE).
4. AMERICAN SOCIETY FOR TESTING OF MATERILLS (ASTM)
5. Institute of electronic and electrical engineers (ieee)
6. AMERICAN CONCRETE INSTTUTE (ACI)
7. American wire producers association (awpa)
8. CONCRETE REINFORCING STEEL INSTTUTE (CRSI)
9. AMERICAN ASSOCIATION of STATE HIGHWAY AND TRANSPORTATION OFFICILLS
10. portland cement association (pCA)
11. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
12. BRICK INDUSTRY ASSOCITION (BAA)
13. AMERICAN WELING SOCIETY (AWS)
14. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA
15. SHEET METAL AND AR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION
(SMACNA)
16. DOOR AND HARDWARE INSTTUTE (OHI)
17. occupational safect and heaith act (osha)
18. APPLCABEE BULLDNG COOES INCLUDING UNIFORM BUILDNG CODE, SOUTHERM
1.5 defintions:
A. Work: THE SUM of tasks and responsibuties IDentified in the contract
b. COMPANY: SPRINT CORPORATION


E. THIRD PARTV VENOR OR AGENCY: VENOOR OR AGENCY ENGAGED SEPARTELY

ACCOMPLISH SPECIFICC TASKS RELATED TO BUT NOT NCLLDEED IN THE WORK
. OFCl: OUNER FURNISHED, CONTRACTOR INSTALLED EQUPMEN
G. CONSTRUCTION MANAGER - AL PROJECTS RELATED COMMUNCATION TO FLOw

 KNRK. NO COMPENSATION WILL


















14 METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION: CONTRACTOR SHALL
PERFORM WORK AS DESCRIED IN THE FOLOWING INSTALATION ANO COMMSSINNG
MOPS

15 USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:
PART 2 - PRODUCTS (NOT USED)
PART 3 - EXECUTION





3. 3 TESTING REOUREMENTS FFR TIESTING BY THIS CONTRACTOR SHALL BE AS INDICATED




## SECTION 01200 - COMPANY FURNISHED MATERIAL AND EQUIPMENT ART 1 - GENERAL


1.2 ReLated documents:
A. THE REOQUREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS
SPECIFICATON.
B. SPRIN "STANDARD CONSTRUCTION DEEALS FOR MIRELESS STES" ARE INCLUDED IN PART 2 - PRODUCTS (NOT USED)
PART 3 - EXECUTION
3.1 RECEIPT OF MATERIL AND EQUIPMENT:

B. THE CONTRACTOR IS RESPONSILEE FOR SPRINT PRovioed MATERAL AND
EQUIPMENT AND UPON RECEITT SHALL:

1 ACCEPT delmeries as shipped and take receipt.
2. verrir completeness and conotion of all delveries.
3. TASE RESPONSIBLIT FOR EQUUPMENT AND PROVIDE INSURANCE PROTECTION

5. PRovide secure and necessary weather protected warehousina
6. COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND
3.2 Delverables:
A. COMCLETE: SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WTH COMPANr
PACICE.
B. If APPLLCABEE, COMPLETE LOST/STTLEN/DAMAGED DOCUMENTATION REPPRTT AS
c. UPLOAD DOCUMENTATION INTO SPRINT STIE MANAGEMENT SYSTEM (SMS) AND/OR SECTION 01300 - CELL SITE CONSTRUCTION CO.

1.2 RELATED DOCUMENTS:
A. THE REQUREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS
B. SPRIN "STANDARD Constructor degals for mineless sites Are included in
. 3 Notice to proceed
A. NO WORK SHAL COMMENCE PRIOR TO COMPAN'S WRITEN NOTICE TO PROCEED
ANO THE ISSUANCE OF THE WORK OREER.


## PART 2 - PRODUCTS (NOT USED) PART 3 - EXECUTION

3.1 FUNCTIONAL REQUIREMENTS:
A. THE ACTVMTIES DEECRRBED IN THIS PARAGRAPH REPRESENT MINMUM ACTIONS AND



c. Manage and conouct all field construction service reated actuties


## Sprint

658 Spinit Parkway
verland Park, Kansas 662
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CONTINUE FROM SP-1

1. Perform any required site environmental mitiation.
2. PREPARE GROUND STIES; PRovot oe-grubgng; and rough and final
3. MANAGE ANO Conouct All Actuties for instalation of UTLITIES
4. INSTAL UNDERGROUND FACLITIES INCLUOING UNDERGROUND PowER AND
5. Install above ground grounding syttems.
6. INSTALL ABOVE GROUND GROUNOING STSEMS.
7. INSTALL "H-FRAMES", cabinets and Shelters as indicated.
8. INSTALL ROADS, ACCESS WATs, CURBS AND DRAANS AS INOICated.
9. ACCOMPLSH REQUIRED MOOIFCATION OF EXISTNG FACLITIES.
10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
11. Provide slabs and equipment platrorms.
12. INSTALL COMPOUND FENCING, SIGHT SHIELLING, LANOSCAPING AND ACCESS
13. PERFORM Inspection and materill testing as required hereinatter.
14. CONOUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON

17. PERRORN, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL
18. PRRFORM AATENNAL AND COOX SWEEP TESTING AND MAKE ANY AND ALL
 PLACED "ON ARR."
3.2 GENERAL REQUIREMENTS FOR CINL CONSTRUCTION:


B. EQUipment roons shall at all times be maintaned "broom cleana and
c. CONTRACTOR SHALL TARE ALL REASONABLE PRECAUTIONS TO DISCOVER AND




e. conouct testing as required herein.
3.3 delinerables:
A. CONTRACTOR SHALL REMEW, APPROVE, AND SUBMIT TO SPRINT SHO DRAWNGS,
B. PROVIDE DOCUMENTATION INCLLDDNG, BUT NOT LIMTED TO. THE FOLLOWING.
DCOUMENTAION SHALL BE FORWARDED IN ORIGNAL FORMAT AND/OR UPLOADED

> 1. ALL CORRESPONDENCE AND PRELMINARY CONSTRUCTION REPORTS.
2. PROJECT PROGRESS REPORTS.
3. CIVL Construction start date (populate fill in sms andor forward
4. ELECTRCCLL SERYCE COMPLETION DATE (POPULATE FELLD IN SMS ANO/OR
FORWARD NOTIFCAGOON).
5. LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS ANO/OR
FORWARD NOTIFCATON).
6. Power install date (populate fiel in sms and/or forward
7. TELLO Readr date (populate fielo in sms and/or forward
8. $\operatorname{PpC}$ (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD
NOTFCGATIN).
9. TOWER CONSTRPCTION START DATE (POPULATE FIELD IN SMS AND/OR
10. TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR
11. BTS AND RaOD EGUIPMENT DELINERD AT STte date (populate field in
SMS AND/OR ForWARD Notrication).
12. NETWORK OPERATONS HANDOFF CHECKLIST (HOC WALK) COMPLLETE (UPLOAD
13. CVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR
FORWARD NOTFICATION).
14. Stie construction progress photos unloaded into sms.

SECTION 01400 - SUBMITTALS \& TESTS
 1.2 RELTED DOCUMENTS:
A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS
 1.3 submitals:
A. THE WORK IN ALL ASPECTS SHALL COMPLY WTH THE CONSTRUCTION DRAWINGS
b. SUBmt the following to compant representative for approval. 1. CONCRETE MX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND
CONCEEEE PANING.
2. CONcrett break tests as specified herein.
3. SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
4. ALL Equipment and materals so identified on the construction
5. Chemical grounoling design
D. ALTERNATES: AT THE COMPAN'S REQUEST, ANY ALTERNATNES TO THE MATERALS

1.4 TESTS AND INSPECTIONS:
A. THE CONTRACTOR SHALL BE RESPONSBLEE FOR ALL CONSTRUCTION TESTS,
B. Contractor shall accomplish testing incluoing but not lmited to the

1. COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE
2. AGL. AIMUUTH AND DOWWNLL USING EEECTRONCC COMMMECIAL

c. REOURED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMTED TO THE

3. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIILLE
4. AlL AVAILABLE JURISOICTIONAL INoormation
5. pdf scan of redines produced in fieLo
6. ELECTRONC AS BUIT DEAWNGS IN AUTOCAD AN PDF FORMATS. AN FIEL
 WIL NOT BE ACCEP NED COHANGES SHAL
IDENTIELED AS THE AS-BULT CONOTION.
7. LIEN WAVERS

Sprint

| $\begin{array}{c}6580 \text { Spint Parkway } \\ \text { Overland Park, Kansas } 66251\end{array}$ |
| :---: |

8. RELNAL PAMMENT APPLLCATION
9. Construction and commissioning checklist complete wit no deficient
10. ALL POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLEEED in STEERRA
(SPRINT DOCUMENT REPOSTORY OF RECORD).
1.5 Commissioning: Perform all commissioning as reaured by applicable
MOPs
1.6 Integration: Perform all integration actutites as reoured by applcable
mops

PART 2 - PRODUCTS (NOT USED)
PART 3 - EXECUTION
3.1 Requirements for testina:
A. THIRD PARTY TESTING AGENCY:



3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT
4. EXPERENENE IN SOILS, CONCRETE MASONRY, AGGREGATE, AND ASPHALT
3.2 REQUIRED TESTS:
A. CoNTOACTIO: SHALL ACCOMPLISH TESTING INCLUODG BUT NOT LIMTED TO THE

1. CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR
FOUNOATIONS AS SPECIFED IN SECTION: PORTANO CEMENT CONCRETE PAVING.
2. ASPHALT ROADNAY COMPACTED THICNNESS, SURFACE SMOOTHNESS, AND
3. FiEL oualir conntol testing as specified in section: portand cement
4. TEETING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS,
5. Structural backfil compaction tests for the tower foundation.
6. SITE RESIITANCE TO EARTH TESTNG PER EXHBTI: CELL STIE GROUNOING
7. ANTENNA AND COAX SWEEP TESTS PER EXHIITT: ANTENNA TRANSMISSION LINE
8. GROUNDING At ANTENNA MASTS FOR GPS AND antennas
9. ALL OTHER TESTS REQUIRED by COMPANY OR JURISOICTION.
3.3 REQUIRED INSPECTIONS
A. SCHEDULE INSPECTIONS WTH COMPANY REPRESENTATVE.
B. CONDUCT INSPECTONS INCLUDING BUT Not LIMTED to the FOLLowing:



10. PRE- AND POST-CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON
11. TOWER ERECTION SECTION STACKING AND PLATTORM ATTACHMENT DOCUMENTED
12. ANTENNA AZIMUTH ADOWN TLT AND PER SUNLIGHT TOOL SUNSIGHT

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SPRINT SPECIFICATIONS
SP-2
7. VERIFICATION DOCUMENTED WTH THE ANTENNA CHECKLIST REPORT, BY A\&E,
STEE DEVELOPMENT REP, OR RF REP.

9. COAA SWEEP AND FIBER TESTING DOCUMENTS SUBMITED VA SMS FOR RF
10. SCAN-ABEE RARCOOE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE
11. AlL AVallable jurisolctional information
12. PDF SCAN of redlines produced in fieLo

D. CONSTRUCTION INPECTIONS AND CORRECTVE MEAURES SHALL RE DOCUMENTED


A. THE FOLLOWING TEST AND Inspection reports shall be provided as

1. CONCRETE MIX AND CYIINDER BREAK REPORTS.
2. STRUCTURAL BACKFIL COMPACTION REPORTS.
3. SIte resistance to earth test
4. antenna azimuth and down tlit verification

5. COAX CABLE SWEEP TESTS PER COMPANY'S "ANTENNA LINE ACCEPTANCE
b. reguried closeout documentation includes the following
 BACKGLILGM SHHWN
INOICATING DEPT.
6. CONDUIS, CONDUCTORS AND GROUNOING: PHOTOGRAPHS SHOWNG TYICAL THPACAL
TPPACING:
St
7. CONCRETE FORMS AND REINFORCING: CONCRETE FORMING TITMER AND

8. TOWER ANTENNAS AND MANLINE: INSPECTION AND PHOTOGRAPHS OF SECTION ATACHMENT POINT: PHOOOGRAPHS OF TOWER TP GROUNDNG: PHOTOS



TOWER/MONOPOLE.
9. ROOF TOPS: PRE-CONSTRUCTION AND POST-CONSTRUCTION VIUAL INSPECTION
俗
10. SITE LAYOUT- PHOTOGRAPHS OF THE OVERAL COMPOUND, INCLUDING



11. any and all submitals by the jurisolction or companr.

SECTION 01400 - SUBMITTALS \& TESTS
Nan

. 2 RELATED DOCuments:
A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS
B. SPRNT "STANOARD CONSTRUCTION DETALLS FOR WIRELESS STIES" ARE INCLUDED in PART 2 - PRODUCTS (NOT USED)
PART 3 - EXECUTIO
. 1 WEEKLY REPORTS:

 3.2 PROJECT CONFERENCE CALLS:
 MILESTONE PROJECTIONS,
NEEESARYY
3.3 PROUECT TRACKING IN SMS:
A. CoNTRACCROR SHAAL RROVIDE SCHEDLLE UPDATES AND PROJECTONS IN THE SMS
SYSTEM OM A WEEKLY BASI. 3.4 Adoitional reporting:
A. ADOITONAL RR ALTERNATE REPORTING REOURRMENTS MAY BE ADDED TO THE
REPORT AS DEEERMNED TO BE REASONABLY NECESSARY BY COMPANY. 3.5 PROJECT PHOTOGRAPHS:
 1. ISHELTER AND TOWER OVERVEW.

1. ISHELTER AND TOWER OVERVEW.
2. TOWER FOUNDATION(S) - FORMS AND STEEL BEFORE POUR (EACH ANCHOR
ON GUYED TOWERS).
3. TOWER FOUNOATION(S) POUR WTH VBRATOR IN USE (EACH ANCHOR ON
GUUED TOWERS).
4. Tower stel as being installed into hole (show anchor steel on
GuYed towers).
5. Photos of tower secton stacking.
6. Concrete testing / Samples.
7. PLacing of anchor bolts in tower foundation.
8. BULLDING/WATER TANK FROM ROAD FOR TENANT IMPROVEMENTS OR COMMENTS.
9. Shelter foundation--forms and steel before pouring.
10. Shelter foundation pour with vibator in use.
11. coax cable entry into shelter.
12. PLATFORM MECHANICAL CONNECTONS To TOWER/MONOPOLE

13. Photos of tower top coax line color cooing and color cooing at
grouno level.
14. photos of all approprate company or regulatory signage.
15. PHOTOS OF EQUPMENT BOLT DOWN INSIDE SHELTER.

16. ELECTRICAL TRENCH(S) wTH ELECTRICAL / CONOUT BEFORE BACKFLL.
17. ELECTRICAL TRENCH(S) wTH FOLL-BACKED TAPE BEFORE FURTHER BACKFILL 20. TELCO TRENCH WTH TELEPHONE / CONOUIT BEFORE BACKFIL.
18. TELCO TRENCH WIH FOLL-BACKED TAPE BEFORE FURTHER BACKFLLL.
19. SHELTER GROUND-RING TRENCH WTTH GROUND-WRE before backFIL (show
20. TOWER GROUND-RING TRENCH WTHH GROUND-WIRE BEFORE BACKFILL (SHOW
ALL CLDS AND BEND RAOIII.
21. FENCE GROUND-RNG TRENCH WTH GROUND-WRE BEFORE BACKFILL (SHow 25. Al BTS Ground connccions.
22. ALL GRound test wells.

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658 Spint. Parkway
overiand Pakk, Kansas 66251
27. antenna ground bar and equipment ground bar.
28. ADDITIONAL GROUNOING POINTS on towers above 200'.
29. hVac units including condensers on splt systems.
30. GPS ANTENNAS.
31. CABLE TRAY AND/OR WavEGUIDE bRIDGE.
32. Dochouse/cable Ext from roof.
33. EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND
34. master bus bar.
35. telco board and nu.
36. ELECTRICAL DISTRBUTION WALL.
37. CABLE ENTRY with surge suppression.
38. ENTRANCE TO EQUIPMENT ROOM.
39. COAX WEATHERPROOFING-TOP AND BOTTOM OF TOWER
40. Coax grounding -top and bottom of tower.
41. antenna and mast grounoing.
42. LANOSCAPING - WHERE APPLCABLE.


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RAN WIRING DIAGRAM




