



January 28, 2015

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Street
New Britain, CT 06051

Regarding: Notice of Exempt Modification – Addition of 3 radio heads previously approved
Property Address: 5 Perryridge Road, Greenwich, CT (the “Property”)
Applicant: AT&T Mobility (“AT&T”)

Dear Ms. Bachman:

AT&T currently maintains a wireless telecommunications facility on an existing 164 foot Monopole (“tower”) location on the Property. AT&T’s facility consists of nine (9) wireless telecommunications antenna at 134 feet. The is controlled by Greenwich Hospital. The Council approved the previous application on May 31st 2011 reference number EM-CING-057-110506. This application (attached) granted AT&T the use of 6 radio heads at this location. The approval expired one year from the issue date. During that time AT&T made the changes to the site per the approval but only installed three (3) of the six (6) radio heads that they received approval. AT&T would now like to install the additional three(3) radio heads that were originally approved under EM-CING-057-110506.

Please accept this application as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72 (b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the First Selectman, and the Director of Planning and Zoning for the Town of Greenwich. A copy of this letter is also being sent to Greenwich Hospital, the owner of the structure that AT&T is located.

The planned modifications to AT&T’s facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The planned modifications will not result in an increase in the height of the existing structure. AT&T’s additional, previously approved 3 radio heads will be installed at 134 foot level of the 164 foot monopole.
2. The proposed modifications will not involve any changes to ground-mounted equipment and, therefore will not require an extension of the site boundary.
3. The proposed modification will not increase the noise level at the facility by six decibel or more, or to levels that exceed state and local criteria.
4. The operation of the modified facility will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety



standard. An RF emissions calculation (attached) for AT&T's modified facility was provided in the application which led to the May 31st 2011 Decision.

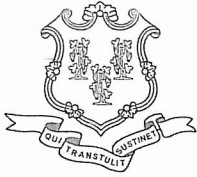
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The tower and its foundation can support AT&T's proposed modifications. (Please see attached Structural analysis completed by Centek Engineering dated April 14, 2011).

For the foregoing reasons AT&T respectfully requests that the proposed addition of 3 radio heads previously approved be allowed within the exempt modifications under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

David P. Cooper
Director of Site Acquisition
Empire Telecom

CC: Peter Tesei, First Selectman, Town of Greenwich
Katie DeLuca, Director, Planning and Zoning, Town of Greenwich
Greenwich Hospital



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
www.ct.gov/csc

CT 2102

May 31, 2011

Douglas L. Culp, Real Estate Consultant
New Cingular Wireless PCS, LLC
500 Enterprise Drive
Rocky Hill, CT 06067-3900

RE: **EM-CING-057-110506** - New Cingular Wireless PCS, LLC notice of intent to modify an existing telecommunications facility located at 5 Perryridge Road, Greenwich, Connecticut.

Dear Mr. Culp:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated May 6, 2011. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

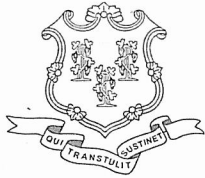
Very truly yours,

Linda Roberts
Executive Director

LR/CDM/laf

c: The Honorable Peter J. Tesei, First Selectman, Town of Greenwich
Diane Fox, Planning & Zoning Director, Town of Greenwich
Greenwich Hospital





STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

May 10, 2011

The Honorable Peter J. Tesei
First Selectman
Town of Greenwich
Town Hall
101 Field Point Road
P. O. Box 2540
Greenwich, CT 06836-2540

RE: **EM-CING-057-110506** - New Cingular Wireless PCS, LLC notice of intent to modify an existing telecommunications facility located at 5 Perryridge Road, Greenwich, Connecticut.

Dear First Selectman Tesei:

The Connecticut Siting Council (Council) received this request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72.

If you have any questions or comments regarding this proposal, please call me or inform the Council by May 24, 2011.

Thank you for your cooperation and consideration.

Very truly yours,

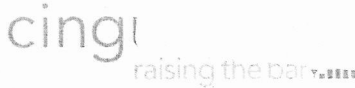
A handwritten signature in cursive script that reads "Linda Roberts".

Linda Roberts
Executive Director

LR/jbw

Enclosure: Notice of Intent

c: Diane Fox, Planning & Zoning Director, Town of Greenwich



EM-CING-057-110506

Wireless PCS, LLC
Drive
Connecticut 06067-3900

Phone: (860) 463-5511
Fax: (860) 513-7190

Douglas L. Culp
Real Estate Consultant

ORIGINAL

HAND DELIVERED

May 6, 2011

RECEIVED
MAY - 6 2011

CONNECTICUT
SITING COUNCIL

Ms. Linda Roberts
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

Re: New Cingular Wireless PCS, LLC notice of intent to modify an existing tele-communications facility located at 5 Perryridge Road Greenwich, CT (owner Greenwich Hospital)

Dear Ms. Roberts:

In order to accommodate technological changes, implement Uniform Mobile Telecommunications System ("UMTS") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the State of Connecticut, New Cingular Wireless PCS, LLC ("AT&T") plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the chief elected official of the municipality in which the affected cell site is located.

UMTS technology offers services to mobile computer and phone users anywhere in the world. Based on the Global System for Mobile ("GSM") communication standard, UMTS is the planned worldwide standard for mobile users. UMTS, fully implemented, gives computer and phone users high-speed access to the Internet as they travel. They have the same capabilities even when they roam, through both terrestrial wireless and satellite transmissions.

LTE is a new high-performance air interface for cellular mobile communications. It is the last step toward the 4th generation (4G) of radio technologies, designed to increase the capacity and speed of mobile telephone networks.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in AT&T's operations at the site. Also included is documentation of the

structural sufficiency of the tower to accommodate the revised antenna configuration.

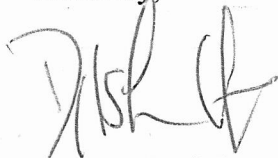
The changes to the facility do not constitute modifications as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will be unaffected.
2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound other than some enlarged equipment pads as may be noted in the attachments.
3. The proposed changes will not increase the noise level at the existing facility by six decibels or more.
4. Radio frequency power density may increase due to use of one or more GSM channel for UMTS transmissions. Moreover, LTE will utilize additional radio frequencies newly-licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons, New Cingular Wireless respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (860) 463-5511 with questions concerning this matter. Thank you for your consideration.

Sincerely,



Douglas L. Culp
Real Estate Consultant

Attachments

NEW CINGULAR WIRELESS PCS, LLC
Equipment Modification

5 Perryridge Ridge Greenwich, CT
 Site Number 2102
 Exempt Mod 08/08

Tower Owner/Manager: Greenwich Hospital

Equipment configuration: Monopole

Current and/or approved: Six PowerWave antennas @ 134 ft
 Six PowerWave TMA's and Diplexers @ 134 ft
 Twelve runs 1 5/8 inch coax to 134 ft
 Equipment Shelter

Planned Modifications: Retain existing PowerWave Antenna's and TMA's at 134 ft
 Retain all Coax Cabling
 Install three PowerWave P65-16 antennas or equivalent @ 134 ft
 Install six remote radio heads and surge arrester @ 134 ft
 Install one new cabinet and surge suppressor equipment in shelter

Power Density:

Worst-case calculations for existing wireless operations at the site, using standard parameters for other carriers, indicate a radio frequency electromagnetic radiation power density, measured at ground level beside the Tower, of approximately 47.7% of the standard adopted by the FCC. As depicted in the second table below, the total radio frequency electromagnetic radiation power density following proposed modifications would be approximately 49.7 % of the standard.

Existing

Other Users							23.70
AT&T UMTS	134	1900 Band	2	500	0.0200	1.0000	2.00
AT&T UMTS	134	800 Band	1	500	0.0100	0.5867	1.71
AT&T GSM	134	800Band	15	296	0.0889	0.5867	15.15
AT&T GSM	134	1900 Band	6	427	0.0513	1.0000	5.13
Total							47.7%

* Data for other users are from Siting Council records - Dave Martin – from Sprint Actual reading at site.

Proposed

Company	Centerline Ht (feet)	Frequency (MHz)	Number of Channels	Power Per Channel (Watts)	Power Density (mW/cm ²)	Standard Limits (mW/cm ²)	Percent of Limit
Other Users							23.70
AT&T UMTS	134	800 Band	1	500	0.0100	0.5867	1.71
AT&T UMTS	134	1900 Band	2	500	0.0200	1.0000	2.00
AT&T GSM	134	1900 Band	6	427	0.0513	1.0000	5.13
AT&T GSM	134	880 - 894	15	296	0.0889	0.5867	15.15
AT&T LTE	134	740 - 746	1	500	0.0100	0.4933	2.03
Total							49.7%

* Data for other users are from Siting Council records - Dave Martin – from Sprint Actual reading at site.

Structural information:

The attached structural analysis demonstrates that the monopole and foundation have adequate structural capacity to accommodate the proposed modifications. (CENTEK dated 4-14-11).

PROJECT INFORMATION

SCOPE OF WORK: UNMANNED TELECOMMUNICATIONS FACILITY MODIFICATIONS
 SITE ADDRESS: 5 PERRYBRIDGE ROAD, GREENWICH, CT 06830
 LATITUDE: 41.034188° N 41° 2' 3"
 LONGITUDE: -73.630856° W -73° 37' 51.08"
 JURISDICTION: NATIONAL, STATE & LOCAL CODES OR ORDINANCES
 CURRENT USE: TELECOMMUNICATIONS FACILITY
 PROPOSED USE: TELECOMMUNICATIONS FACILITY
 NOC#: 886-915-5600



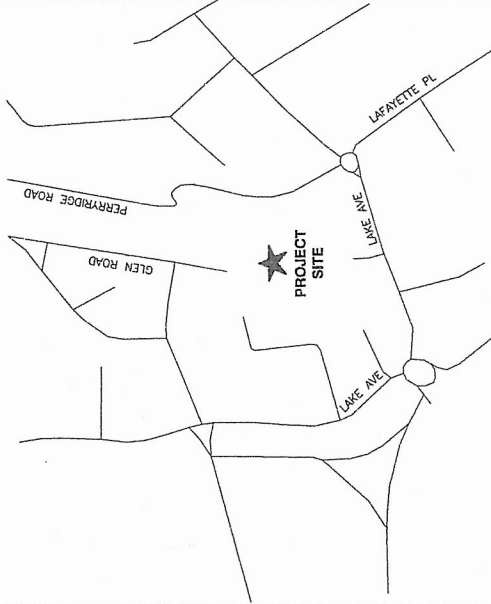
SITE NUMBER: CT2102
SITE NAME: GREENWICH HOSPITAL

DRAWING INDEX

	REV
T-1 TITLE SHEET	2
GN-1 GENERAL NOTES	2
A-1 COMPOUND & EQUIPMENT PLAN	2
A-2 ANTENNA LAYOUT AND ELEVATION	2
A-3 DETAILS	2
G-1 PLUMBING DIAGRAM & DETAILS	2

VICINITY MAP

HEAD NORTHEAST ON ENTERPRISE DR TOWARD CAPITAL BLVD. 0.3 MILES. TURN LEFT AT CAPITAL BLVD. 0.3 MILES. TURN LEFT AT WEST ST. 0.3 MILES. TURN LEFT TO MERGE ONTO I-95 S. TOWARD NEW HAVEN. 9.0 MILES. TAKE EXIT 5A FOR STATE ROUTE 8 S/TOWARD BRIDGEPORT. BRIDGEPORT 0.7 MILES. FOLLOW SIGNS FOR CT-8 S/BRIDGEPORT AND MERGE ONTO CT-8 S/STATE ROUTE 8 S. 5.3 MILES. KEEP RIGHT AT THE FORK. FOLLOW SIGNS FOR I-95 S/N.Y. CITY AND MERGE ONTO I-95 S. 23.4 MILES. TAKE EXIT 5 FOR US-1 TOWARD RIVERSIDE/OLD GREENWICH. 0.1 MILES. TURN LEFT AT US-1 S/E PUTNAM AVE. 2.9 MILES. TURN RIGHT AT MAPLE AVE. 0.4 MILES. TAKE THE 1ST LEFT ONTO PATTERSON AVE. 0.2 MILES. CONTINUE ONTO DEER PARK DR. 495 FT. CONTINUE ONTO GLEN RD. 0.4 MILES.



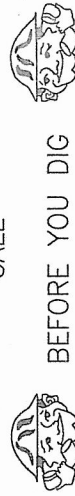
GENERAL NOTES

- THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY TO BE ACCESSSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
- CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T REPRESENTATIVE IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

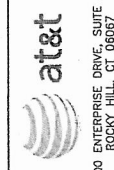
CALL

BEFORE YOU DIG

CALL TOLL FREE 800-922-4455

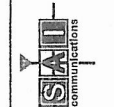


UNDERGROUND SERVICE ALERT



SITE NUMBER: CT2102
SITE NAME: GREENWICH HOSPITAL
 5 PERRYBRIDGE ROAD
 GREENWICH, CT 06830
 FAIRFIELD COUNTY

22 WEEHAWKIN DRIVE
 SALEM, NH 03078

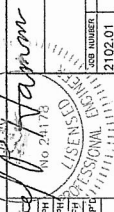


DESIGNED BY: DC
 DRAWN BY: JS
 SCALE: AS SHOWN

NO.	DATE	REVISIONS
2	02/26/11	CONSTRUCTION REVISED
1	02/10/11	ISSUED FOR CONSTRUCTION
0	02/10/11	ISSUED FOR REVIEW

DESIGNED BY: DC
 DRAWN BY: JS
 SCALE: AS SHOWN

AT&T
 TITLE SHEET (LIE)
 DRAWING NUMBER
 T-1

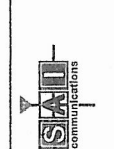
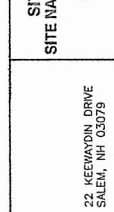


NO.	DATE	REVISIONS
2	02/26/11	CONSTRUCTION REVISED
1	02/10/11	ISSUED FOR CONSTRUCTION
0	02/10/11	ISSUED FOR REVIEW

DESIGNED BY: DC
 DRAWN BY: JS
 SCALE: AS SHOWN

500 ENTERPRISE DRIVE, SUITE 3A
 ROCKY HILL, CT 06067

22 WEEHAWKIN DRIVE
 SALEM, NH 03078



100 GLOUCESTER STREET, SUITE 2410
 NEWTON, MASSACHUSETTS 02459
 TEL: 617-552-5333
 FAX: 617-552-5338

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTNING PROTECTION CODE, AND GENERAL STANDARDS WITH TELDORIDA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND SECURITY) SHALL BE INSTALLED TO THE DEPTH OF OR BELOW GRADE, IN TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NECESSARY TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BITS EQUIPMENT.
5. EACH RIS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES. 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BITS 2 AWG STRANDED COPPER FOR OUTDOOR BITS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTI-OXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CUAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWG COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION, AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50


GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY: CONTRACTOR - SA; SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) OWNER - AT&T MOBILITY
2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF THE CONTRACTOR.
3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL APPLICABLE REGULATIONS, ORDINANCES, AND CODES. THE CONTRACTOR SHALL OBTAIN ALL NECESSARY PERMITS FROM THE PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FINISHING MATERIALS, EQUIPMENT, APPURTENANCES AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
6. NOTHING LISTED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY THE CONTRACTOR. ITEMS NOT LISTED IN THE BID PACKAGE AND NOTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.
14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.

15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILLED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
 16. CONSTRUCTION SHALL COMPLY WITH UNITS SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T MOBILITY SITES."
 17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
 18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT INTERRUPT THE EXISTING NORMAL OPERATION. CONSTRUCTION WORK SHALL BE SCHEDULED FOR OFF-HOURS OF COMMERCIAL OPERATION. ALL WORK SHALL BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
 19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
 20. APPLICABLE BUILDING CODES: SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION OVER THE PROJECT. THE CONTRACTOR SHALL ADOPTED ALL APPLICABLE STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN. BUILDING CODE: 2003 IBC WITH 2005 CT SUPPLEMENT & 2009 CT AMENDMENTS. CODE: REFER TO ELECTRICAL DRAWINGS LIGHTNING CODE: REFER TO ELECTRICAL DRAWINGS
- SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:
- AMERICAN CONCRETE INSTITUTE (ACI) 318: BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE.
 - AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, NINTH EDITION; TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-F, STRUCTURAL STANDARDS FOR STEEL
 - ANTENNA TOWER AND ANTENNA SUPPORTING STRUCTURES, REFER TO ELECTRICAL DRAWINGS FOR SPECIFIC ELECTRICAL STANDARDS.
- FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS

ACL	ABOVE GRADE LEVEL	G.C.	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
AWG	AMERICAN WIRE GAUGE	MGB	MASTER GROUND BUS	TBD	TO BE DETERMINED
BCW	BARE COPPER WIRE	MIN	MINIMUM	TBR	TO BE REMOVED
BITS	BASE TRANSDUCER STATION	PROPOSED	PROPOSED	TBRR	TO BE REMOVED AND REPLACED
EG	EQUIPMENT GROUND	REF. P.	REFERENCE	TYP	TYPICAL
EOR	EQUIPMENT GROUND RING	REQ.	REQUIRED		



500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06867

SITE NUMBER: CT2102
SITE NAME: GREENWICH HOSPITAL
5 PERRYBRIDGE ROAD
GREENWICH, CT 06830
FAIRFIELD COUNTY

22 KEEWAYTON DRIVE
SALEM, NH 03079

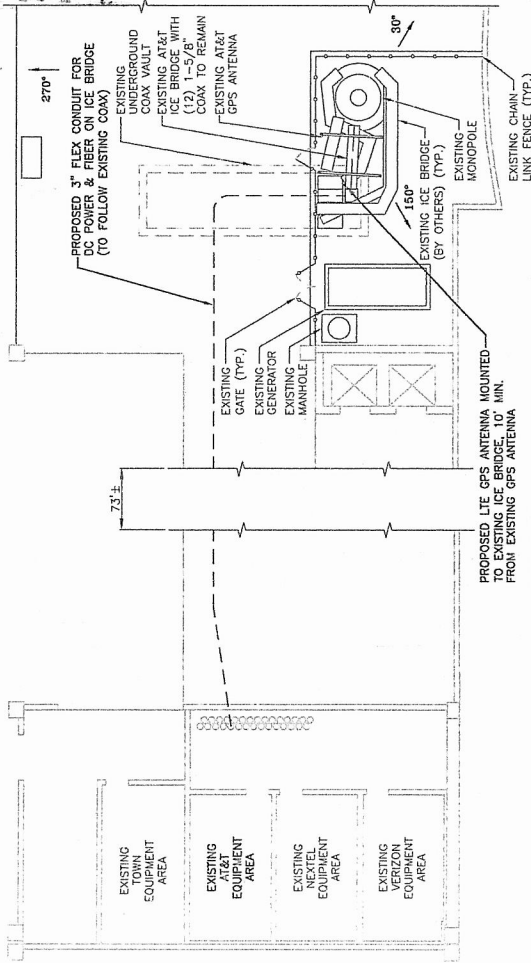


Hudson Design Group
162 CASCAD RIVER ROAD, SUITE 240
ANDOVER, MA 01810
TEL: 978.555.5533

NO.	DATE	REVISIONS	DRAWN BY: JS
1	02/10/11	ISSUED FOR REVIEW	DESIGNED BY: DC
2	02/10/11	ISSUED FOR CONSTRUCTION	
3	02/10/11	CONSTRUCTION REVISED	

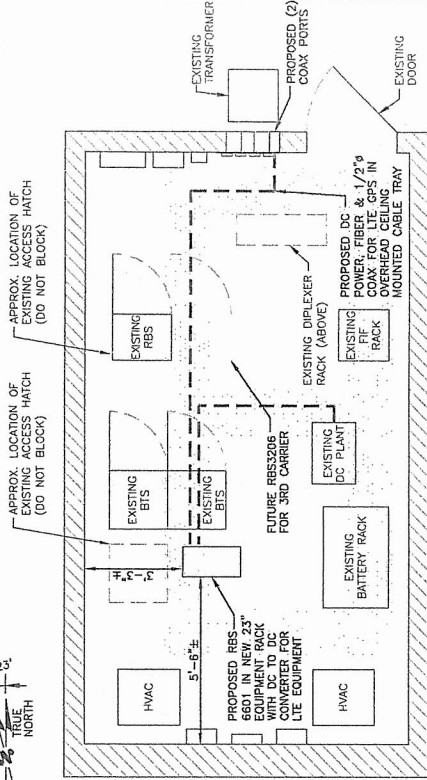
JOB NUMBER	JOB NUMBER	JOB NUMBER	JOB NUMBER	JOB NUMBER	JOB NUMBER
2102.01	2102.01	2102.01	2102.01	2102.01	2102.01

AT&T
GENERAL NOTES
(LITE)
EXPANSION NUMBER
GN-1
2



COMPOUND PLAN
SCALE: 1/8" = 1'-0"

0 4'-0" 8'-0" 16'-0" 24'-0"



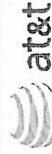
EQUIPMENT ROOM PLAN
SCALE: 1/2" = 1'-0"

0 1'-0" 2'-0" 4'-0" 6'-0"



22 KEEMAYDIN DRIVE
SALEM, NH 03079

SITE NUMBER: CT0102
SITE NAME: GREENWICH HOSPITAL
5 PERRYBRIDGE ROAD
GREENWICH, CT 06830
FAIRFIELD COUNTY



500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06867

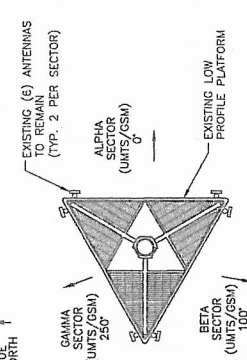
2	03/25/11	CONSTRUCTION REVIEW	AT	DC	DRN	AT&T
1	03/15/11	ISSUED FOR CONSTRUCTION	AT	DC	DRN	AT&T
0	03/09/11	ISSUED FOR REVIEW	AT	DC	DRN	AT&T
NO.	DATE	REVISIONS	BY	CHK	APP'D	
SCALE:	AS SHOWN	DESIGNED BY:	DC	DRAWN BY:	JG	
SER.	2102.01	ISSUED FOR REVIEW	AT&T	COMPONENT & EQUIPMENT PLAN (LIE)	BOONING (ASBELL)	2

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION.

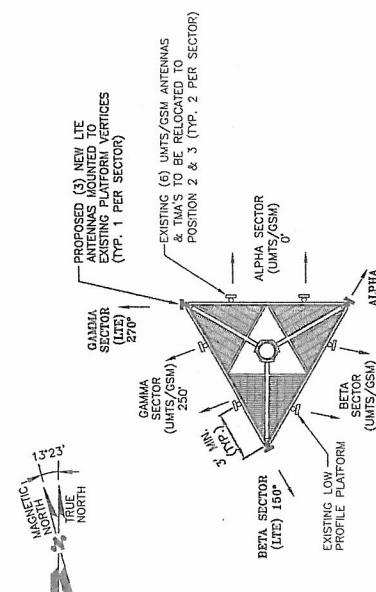
***NOTE:**
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA CONFIGURATION

- EXISTING WHIP ANTENNAS (BY OTHERS) (TYP.)
- TOP OF EXISTING MONOPOLE - ELEV. 164'-0" ± (A.G.L.)
- ☉ OF EXISTING DISH ANTENNAS ELEV. 160'-0" ± (A.G.L.)
- ☉ OF EXISTING ANTENNAS BY OTHERS ELEV. 154'-0" ± (A.G.L.)
- ☉ OF EXISTING ANTENNAS BY OTHERS ELEV. 144'-0" ± (A.G.L.)
- ☉ OF PROPOSED AT&T LTE ANTENNAS ELEV. 134'-0" ± (A.G.L.)
- ☉ OF EXISTING ANTENNAS BY OTHERS ELEV. 124'-0" ± (A.G.L.)
- ☉ OF EXISTING ANTENNAS BY OTHERS ELEV. 114'-0" ± (A.G.L.)

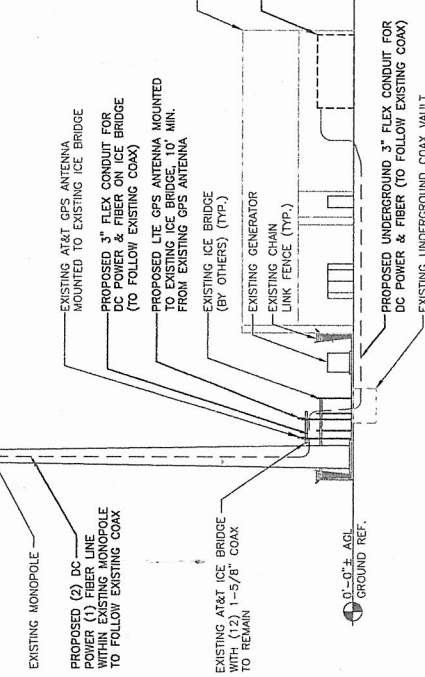
- PROPOSED GRP MOUNTED TO PROPOSED 2-3/8" PIPE (TYP. OF 2 PER SECTOR)
- EXISTING ANTENNAS (BY OTHERS) (TYP.)
- PROPOSED (3) NEW LTE ANTENNAS MOUNTED TO EXISTING PLATFORM VERTICES (TYP. 1 PER SECTOR)
- EXISTING POWERWAVE UMS/GSM ANTENNAS TO REMAIN (TYP. 2 PER SECTOR)
- PROPOSED SURGE ARRESTOR ON 2-3/8" PIPE TO PROPOSED 2-3/8" PIPE
- EXISTING MONOPOLE
- PROPOSED (2) DC POWER (1) FIBER LINE WITHIN EXISTING MONOPOLE TO FOLLOW EXISTING COAX
- EXISTING AT&T GPS ANTENNA MOUNTED TO EXISTING ICE BRIDGE
- PROPOSED 3" FLEX CONDUIT FOR DC POWER & FIBER ON ICE BRIDGE (TO FOLLOW EXISTING COAX)
- PROPOSED LTE GPS ANTENNA MOUNTED TO EXISTING ICE BRIDGE, 10' MIN. FROM EXISTING GPS ANTENNA (BY OTHERS) (TYP.)
- EXISTING GENERATOR
- EXISTING CHAIN LINK FENCE (TYP.)
- PROPOSED UNDERGROUND 3" FLEX CONDUIT FOR DC POWER & FIBER (TO FOLLOW EXISTING COAX)
- EXISTING UNDERGROUND COAX VAULT



EXISTING GSM/UMTS ANTENNA PLAN
SCALE: N.T.S.



PROPOSED LTE ANTENNA PLAN
SCALE: N.T.S.



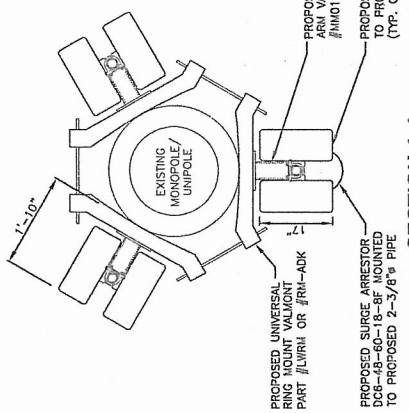
WEST ELEVATION
SCALE: 1/16"=1'-0"



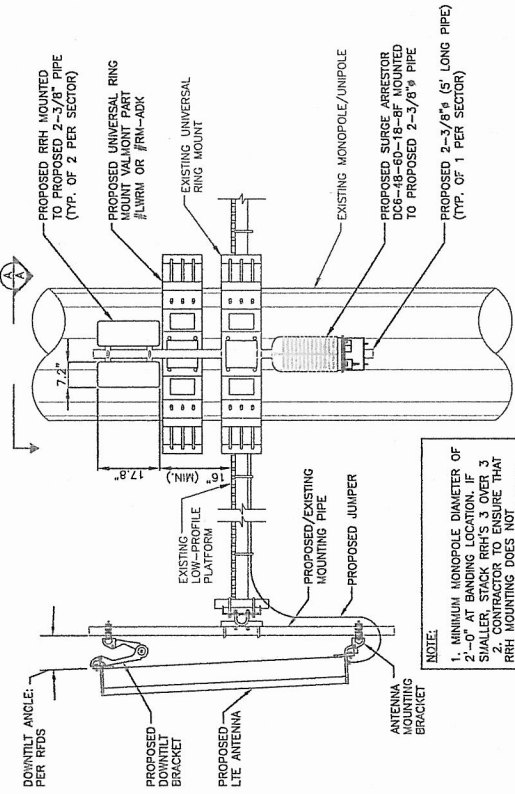
<p>500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067</p>		<p>SITE NUMBER: CT2102 SITE NAME: GREENWICH HOSPITAL 5 PERRYDRIVE ROAD GREENWICH, CT 06830 FAIRFIELD COUNTY</p>		<p>22 KEEWANON DRIVE SALEM, NH 03079</p>		<p>AT&T ANTENNA LAYOUT AND ELEVATION (LTE) DRAWING NUMBER: A-2 JOB NUMBER: 2102.01 REV: 2</p>	
<p>DESIGNED BY: DC</p>	<p>SCALE: AS SHOWN</p>	<p>REVISIONS</p>	<p>BY</p>	<p>CHK</p>	<p>DATE</p>	<p>ISSUED FOR REVIEW</p>	<p>ISSUED FOR CONSTRUCTION</p>
<p>02/10/11</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>
<p>02/10/11</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>
<p>03/29/11</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>
<p>03/29/11</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>	<p>DC</p>

SALEM, NH 03079

1000 CONNOR DRIVE SUITE 3100
N. ANDOVER, MA 01850
TEL: (978) 353-3333
FAX: (978) 354-3388



SECTION A-A



NOTE:
 1. MINIMUM MONOPOLE DIAMETER OF 2'-0" AT BANDING LOCATION. IF SMALLER, STACK RRH'S 3 OVER 3
 2. CONTRACTOR TO ENSURE THAT PROPOSED ANTENNA CLEARANCE INTERFERES WITH CLIMBING LADDER

PART #	V/M PART #	SIZE RANGE
LVRN	801068	12"-45"
RH-ADK	157286	36"-60" ADAPTER KIT

PROPOSED RRH & SURGE ARRESTOR MOUNTING DETAIL
 SCALE: N.T.S.

SITE NUMBER: CT2102
SITE NAME: GREENWICH HOSPITAL
 5 PERRYBRIDGE ROAD
 GREENWICH, CT 06830
 FAIRFIELD COUNTY

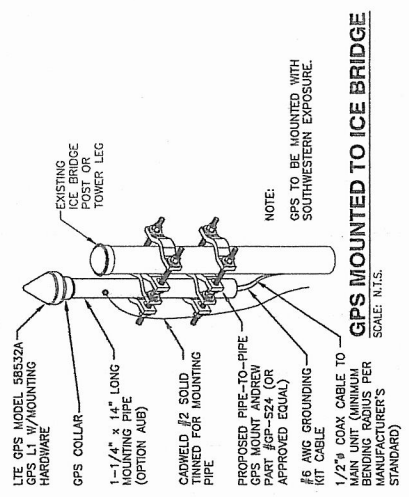
SIAD communications
 22 KEENAVON DRIVE
 SALEM, NH 03079

Hudson Design Group
 1400 COUNCIL STREET
 SUITE 400, WORTHINGTON, NH 03091
 TEL: 603.552.5553
 FAX: 603.552.5558

at&t
 500 ENTERPRISE DRIVE, SUITE 3A
 ROCKY HILL, CT 06867

NO.	DATE	BY	CHK	REVISIONS	DESIGNED BY:	DC
2	03/25/11	CONSTRUCTION REVISED	JC	DC (DPT)		
1	03/10/11	ISSUED FOR CONSTRUCTION	JC	DC (DPT)		
0	02/10/11	ISSUED FOR REVIEW	JC	DC (DPT)		

AT&T
 DETAILS (LIE)
 DRAWING NUMBER: 2102.01
 JOB NUMBER: A-3
 SHEET OF CONNECTICUT STATE PROFESSIONAL ENGINEER
 No. 24176
 P. HARRIS



GPS MOUNTED TO ICE BRIDGE
 SCALE: N.T.S.

Hudson Design Group
 1400 COUNCIL STREET
 SUITE 400, WORTHINGTON, NH 03091
 TEL: 603.552.5553
 FAX: 603.552.5558

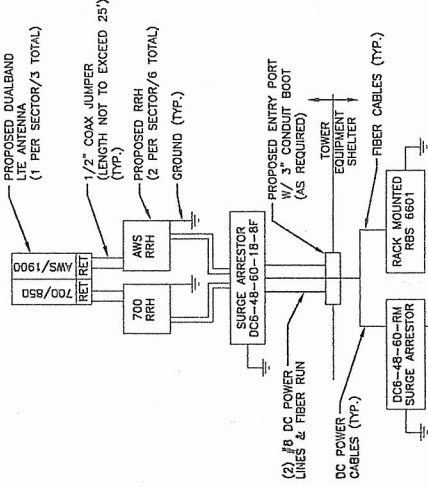
SIAD communications
 22 KEENAVON DRIVE
 SALEM, NH 03079

at&t
 500 ENTERPRISE DRIVE, SUITE 3A
 ROCKY HILL, CT 06867

SITE NUMBER: CT2102
SITE NAME: GREENWICH HOSPITAL
 5 PERRYBRIDGE ROAD
 GREENWICH, CT 06830
 FAIRFIELD COUNTY

SIAD communications
 22 KEENAVON DRIVE
 SALEM, NH 03079

Hudson Design Group
 1400 COUNCIL STREET
 SUITE 400, WORTHINGTON, NH 03091
 TEL: 603.552.5553
 FAX: 603.552.5558



NOTES:

1. CONTRACTOR TO CONFIRM ALL PARTS.
2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS.

3 N.T.S. PLUMBING DIAGRAM

EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS SIZE AND DIRECTION.

SECTION "P" - SURGE PROTECTORS

CABLE ENTRY PORTS (HATCH PLATES) (#2)

GENERATOR FRAMEWORK (IF AVAILABLE) (#2)

INTERNAL POWER COMMON NEUTRAL/GROUND BOND (#2)

+24V POWER SUPPLY RETURN BAR (#2)

-48V POWER SUPPLY RETURN BAR (#2)

RECTIFIER FRAMES.

SECTION "A" - SURGE ARRESTERS

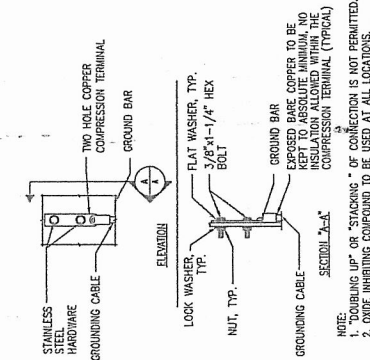
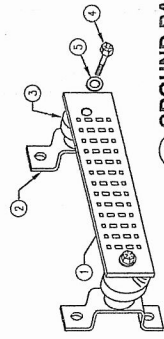
INTERIOR GROUND RING (#2)

EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2)

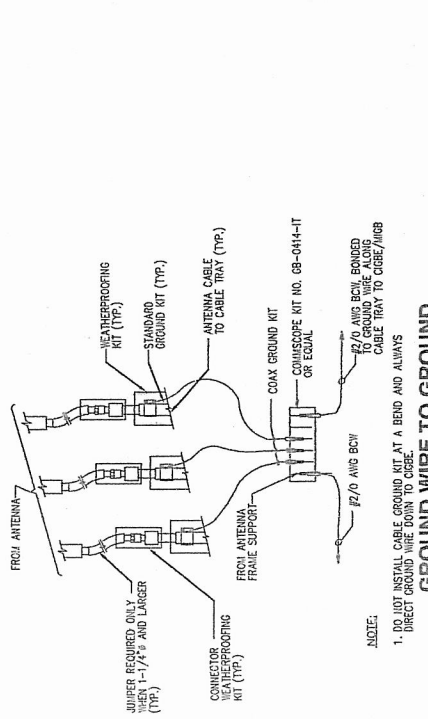
METALLIC COLD WATER PIPE (IF AVAILABLE) (#2)

BUILDING STEEL (IF AVAILABLE) (#2)

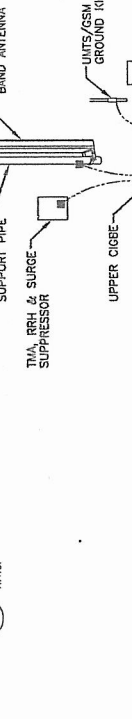
NO.	REQ.	PART NO.	DESCRIPTION
1	1	HUGB-020P-S	SOLID GND. BAR (20"x4"x1/4")
2	2		WALL MTG. BRKT.
3	2		INSULATORS
4	4		5/8"-11x1" HH.G.S.
5	4		5/8" LOCKWASHER



2 N.T.S. TYPICAL GROUND BAR CONNECTION DETAIL



4 N.T.S. GROUNDING RISER DIAGRAM



1 N.T.S. GROUND WIRE TO GROUND BAR CONNECTION DETAIL

NOTE:

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

Hudson
Design Group, Inc.
1400 GARDNER STREET
SADDLE BROOK, NJ 07641
TEL: (201) 349-3333
FAX: (201) 349-3335

SIAD
communications

at&t

500 ENTERPRISE DRIVE, SUITE 3A
ROCKY HILL, CT 06867

SITE NUMBER: CT2102

SITE NAME: GREENWICH HOSPITAL

5 PERRYBROOK ROAD
GREENWICH, CT 06830
FAIRFIELD COUNTY

22 KEEVANDIN DRIVE
SALEM, NH 03079

SCALE: AS SHOWN

DESIGNED BY: DC

DRAWN BY: JS

NO. DATE

0 02/07/01 ISSUED FOR REVIEW

1 03/07/01 ISSUED FOR CONSTRUCTION

2 03/28/01 CONSTRUCTION REVISION

REVISIONS

BY: [Signature]

CHK: [Signature]

JOB NUMBER

2102.01

EXPANSION NUMBER

G-1

PLUMBING DIAGRAM & DETAILS (LTE)

AT&T

CEN TEK engineering

Centered on SolutionsSM

Structural Analysis Report

164-ft Existing EEI Monopole

Proposed AT&T Antenna Upgrade

AT&T Site Ref: CT2102:
Greenwich Hospital

5 Perryridge Road
Greenwich, CT

CEN TEK Project No. 11009.CO12

Date: April 14, 2011



Prepared for:
AT&T Mobility
500 Enterprise Drive, Suite 3A
Rocky Hill, CT 06067

Table of Contents

SECTION 1 - REPORT

- INTRODUCTION.
- ANTENNA AND APPURTENANCE SUMMARY.
- PRIMARY ASSUMPTIONS USED IN THE ANALYSIS.
- ANALYSIS.
- TOWER LOADING.
- TOWER CAPACITY.
- FOUNDATION AND ANCHORS.
- CONCLUSION.

SECTION 2 – CONDITIONS & SOFTWARE

- STANDARD ENGINEERING CONDITIONS.
- GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM.

SECTION 3 – CALCULATIONS

- RISATower INPUT/OUTPUT SUMMARY.
- RISATower DETAILED OUTPUT.
- FLANGE BOLT AND FLANGE PLATE ANALYSIS.
- ANCHOR BOLT AND BASE PLATE ANALYSIS.
- MathCAD CAISSON FOUNDATION ANALYSIS.
- L-PILE CAISSON ANALYSIS.
- L-PILE LATERAL DEFLECTION vs. DEPTH.
- L-PILE BENDING MOMENT vs. DEPTH.
- L-PILE SHEAR FORCE vs. DEPTH.

SECTION 4 – REFERENCE MATERIALS

- AT&T RFDS SHEET.
- ANTENNA CUT SHEETS.

Introduction

The purpose of this report is to summarize the results of the non-linear, P- Δ structural analysis of the antenna installation proposed by AT&T Mobility on the existing monopole (tower) owned and operated by Greenwich Hospital located in Greenwich, Connecticut.

The host tower is a 164-ft tall, five-section, eighteen sided, tapered monopole, originally designed and manufactured by Engineered Endeavors Incorporated (EEI); project no. 11030 dated August 21, 2002. The tower geometry, structure member sizes and foundation system information were obtained from the original manufacturers design documents.

The tower is made up of five (5) tapered vertical sections consisting of A572-65 pole sections. The bottom four (4) vertical tower sections are slip joint connected while the top section is flange connected. The diameter of the pole (flat-flat) is 47.0-in at the top and 76.0-in at the base.

Antenna and appurtenance information were obtained from a previous structural analysis report prepared by CHA; job no; 20621-1037-1203, dated December 29, 2009, an AT&T RFDS sheet and visual verification conducted from grade by Centek personal on April 5, 2011.

AT&T Mobility proposes the installation of three (3) panel antennas on an existing low profile platform, together with six (6) Remote Radio Units (RRU's) and one (1) surge arrestor mounted on a proposed universal ring mount. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna and appurtenance configuration.

Antenna and Appurtenance Summary

The existing tower was designed to support several communication antennas. The existing, proposed and future loads considered in this analysis consist of the following:

- TOWN (EXISTING):
Antennas: One (1) PD1142-1 Omni-directional whip antenna, one (1) PD620-3 Omni-directional whip antenna, one (1) ALR8 Omni-directional whip antenna three (3) BMR10 Omni-directional whip antennas and one (1) camera mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 164-ft above grade level.
Coax Cables: Six (6) 1/2" \varnothing , one (1) 5/8" \varnothing , three (3) 7/8" \varnothing and two (2) 1-1/4" \varnothing coax cables running on the inside of the existing tower.
- TOWN (EXISTING):
Antennas: Two (2) 4 FT Dishes and one (1) 2 Ft Dish mounted on three 4'x4" pipe mounts with a RAD center elevation of 160-ft above grade level.
Coax Cables: Three (3) 1-1/4" \varnothing coax cables running on the inside of the existing tower.
- SPRINT (EXISTING/RESERVED):
Antennas: Three (3) Decibel 950F65T2E-M (2 existing/1 reserved) panel antennas, six (6) Decibel DB980F90E-M (4 existing/2 reserved) panel antennas and one (1) GPS antenna mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 154-ft above grade level.
Coax Cables: Six (6) 1-5/8" \varnothing and one (1) 1/2" \varnothing coax cables running on the inside of the existing tower.

- **CLEARWIRE (EXISTING):**
Antennas: Three (3) Argus LLPX310R panel antennas, three (3) Samsung FDD-R6-RRH, two (2) Dragonwave Horizon ODU's and two (2) Dragonwave A-ANT-23-G-2-C dishes mounted on the Sprint 13-ft low profile platform with a RAD center elevation of 154-ft above the existing tower base plate.
Coax Cables: Two (2) 2" Ø conduits and two (2) 5/8" Ø coax cables running on the inside of the existing tower.
- **T-MOBILE (EXISTING/RESERVED):**
Antennas: Twelve (12) APX16PV-16PVL-X (6 existing/6reserved) panel antennas and twelve (12) G20057A1 TMAs (6 existing/6 reserved) mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 144-ft above grade level.
Coax Cables: Twelve (12) 1-5/8" Ø coax cables running on the inside of the existing tower.
- **AT&T (EXISTING TO REMAIN):**
Antennas: Six (6) Powerwave 7770.00 panel antennas and six (6) LGP21401 tmas mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 134-ft above grade level.
Coax Cables: Twelve (12) 1-5/8" Ø coax cables running on the inside of the existing tower
- **VERIZON (EXISTING):**
Antennas: Six (6) Decibel 844G65T6ZAXY panel antennas, three (3) Andrew LNX-6514DS-T4M panel antennas, three (3) RYMSA MG D3-800T0 panel antennas and six (6) RFS FD(R6004/2C-3L Diplexers mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 124-ft above grade level.
Coax Cables: Twelve (12) 1-5/8" Ø coax cables running on the inside of the existing tower.
- **NEXTEL (EXISTING):**
Antennas: Twelve (12) Decibel DB846G90A-XY panel antennas mounted on a PiROD 13-ft low profile platform with a RAD center elevation of 114-ft above grade level.
Coax Cables: Twelve (12) 1-5/8" Ø coax cables running on the inside of the existing tower.
- **AT&T (PROPOSED):**
Antennas: Three (3) Powerwave P65-16-XLH-RR panel antennas mounted on a 13-ft low profile platform with a RAD center elevation of 134-ft above the existing tower base plate.
- **AT&T (PROPOSED):**
Antennas: Six (6) Ericsson RRUS-11 and one (1) Raycap DC6-48-60-18-8F surge arrestor mounted to one (1) universal ring mount with a RAD center elevation of 138-ft above grade level.
Coax Cables: One (1) fiber cable and two (2) dc control cables running on the inside of the existing tower.

CEN TEK Engineering, Inc.

Structural Analysis – 164-ft EEI Monopole

AT&T Antenna Upgrade – CT2102: Greenwich Hospital

Greenwich, CT

April 14, 2011

- UNKNOWN (EXISTING):
Antennas: Three GPS antennas mounted on three (3) standoffs with a RAD center elevation of 50-ft above grade level.
Coax Cables: Three (3) 7/8" Ø coax cables running on the exterior of the existing tower.

Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents or reinforcement drawings.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- All coax cables to be installed as indicated in this report.
- Refer to construction drawings prepared by Hudson Design Group dated 3.10.11 for RRU and Surge Arrestor mounting details.

Analysis

The existing tower was analyzed using a comprehensive computer program entitled RISATower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower shaft, and the model assumes that the shaft members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for 85 mph basic wind speed (fastest mile) with no ice and 75% reduction of wind force with ½ inch accumulative ice to determine stresses in members as per guidelines of TIA/EIA-222-F-96 entitled “Structural Standards for Steel Antenna Towers and Antenna Supporting Structures”, the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of ½” radial ice tower structure and its components.

Basic Wind Speed:	Fairfield; v = 85 mph (fastest mile) Greenwich; v = 100 mph (3 second gust) equivalent to v = 80 mph (fastest mile) <i>TIA/EIA wind speed criteria controls.</i>	<i>[Section 16 of TIA/EIA-222-F-96]</i> <i>[Appendix K of the 2005 CT Building Code Supplement]</i>
Load Cases:	<u>Load Case 1</u> ; 85 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation. <u>Load Case 2</u> ; 74 mph wind speed w/ ½” radial ice plus gravity load – used in calculation of tower stresses. The 74 mph wind speed velocity represents 75% of the wind pressure generated by the 85 mph wind speed. <u>Load Case 3</u> ; Seismic – not checked	<i>[Section 2.3.16 of TIA/EIA-222-F-96]</i> <i>[Section 2.3.16 of TIA/EIA-222-F-96]</i> <i>[Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type</i>

Tower Capacity

Tower stresses were calculated utilizing the structural analysis software RISATower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

Calculated stresses were found to be within allowable limits. In Load Case 1, per RISATower "Section Capacity Table", this tower was found to be at 47.9% of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Pole Shaft (L5)	1.5'-39.88'	47.9%	PASS

- The tower deflection (tilt) was found to be within allowable limits.

Deflection (degrees)	Proposed	Allowable ⁽¹⁾	Result
Tilt	1.42	1.9	PASS

(1) Allowable tilt taken from original EEI design documents job no. 11030 dated 8/21/02.

Foundation and Anchors

The existing foundation consists of a 9.0 Ø x 28.0-ft long reinforced concrete caisson. The sub-grade conditions used in the analysis of the existing foundation were obtained from the aforementioned EEI design report; project no. 11030 dated August 21, 2002. The base of the tower is connected to the foundation by means of (30) 2.25"Ø, ASTM A615-75 anchor bolts embedded approximately 7-ft into the concrete foundation structure.

Review of the foundation and anchor design consisted of verification of applied loads obtained from the tower design calculations and code checks of allowable stresses:

- The tower base reactions developed from the governing Load Case 1 were used in the verification of the foundation and its anchors:

Base Reactions	Vector	Proposed Load
Base	Shear	45 kips
	Axial	80 kips
	Moment	5000 ft-kips

- The foundation was found to be within allowable limits.

Foundation	Design Limit	Proposed Loading	Result
Reinforced Concrete Caisson	Moment Capacity	56.5%	PASS
	Lateral Deflection	0.59 in. ⁽¹⁾	PASS

(1) Lateral deflection typically limited to 1.0 in. for monopole tower structures.

CEN TEK Engineering, Inc.
Structural Analysis – 164-ft EEI Monopole
AT&T Antenna Upgrade – CT2102: Greenwich Hospital
Greenwich, CT
April 14, 2011

- The anchor bolts and base plate were found to be within allowable limits.

Tower Component	Design Limit	Stress Ratio (percentage of capacity)	Result
Flange Bolts	Tension	58.4%	PASS
Flange Plate	Bending	44.5%	PASS
Anchor Bolts	Compression	49.1%	PASS
Base Plate	Bending	38.5%	PASS

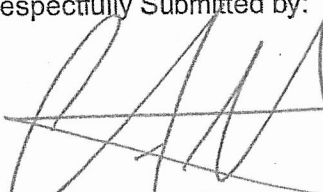
Conclusion

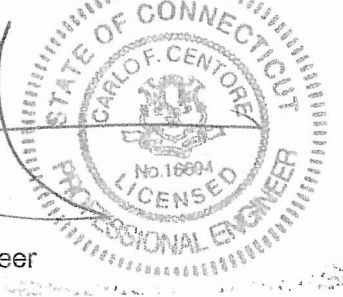
This analysis shows that the subject tower is adequate to support the proposed modified AT&T antenna configuration.

The analysis is based, in part, on the information provided to this office by AT&T Mobility. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:


Carlo F. Centore, PE
Principal ~ Structural Engineer



Prepared by:



Timothy J. Lynn, EIT
Structural Engineer

Standard Conditions for Furnishing of
Professional Engineering Services on
Existing Structures

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of CENTEK engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provide to CENTEK engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. CENTEK engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

CEN TEK Engineering, Inc.
Structural Analysis – 164-ft EEI Monopole
AT&T Antenna Upgrade – CT2102: Greenwich Hospital
Greenwich, CT
April 14, 2011

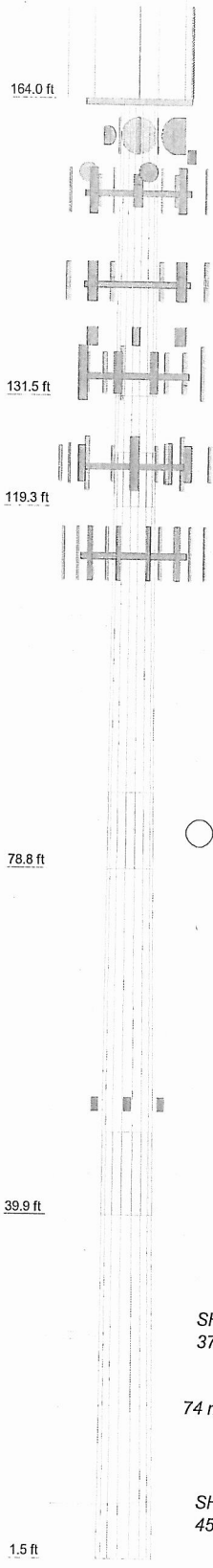
General Description of Structural Analysis Program

RISATower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, RISATower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

RISATower Features:

- RISATower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- RISATower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

Section	1	2	3	4	5
Length (ft)	32.50	12.21	46.50	47.33	47.63
Number of Sides	18	18	18	18	18
Thickness (in)	0.3125	0.3750	0.4375	0.5625	0.5625
Socket Length (ft)		6.00	8.42	9.25	
Top Dia (in)	47.0000	53.4200	54.0585	60.4813	66.7412
Bot Dia (in)	53.4200	56.1500	62.9700	69.6600	76.0000
Grade	A572-65				
Weight (K)	5.5	2.7	12.8	18.5	20.5



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
PD1142-1 (Town Existing)	164	(2) G20057A1 TMA (T-Mobile Existing)	144
PD620-3 (Town Existing)	164	(2) G20057A1 TMA (T-Mobile Reserved)	144
ALR8 (Town Existing)	164	(2) APX16PV-16PVL-X (T-Mobile Existing)	144
BMR10 (Town Existing)	164	(2) RRUS-11 (ATI Proposed)	138
BMR10 (Town Existing)	164	(2) RRUS-11 (ATI Proposed)	138
Camera (Town Existing)	164	(2) RRUS-11 (ATI Proposed)	138
Low Profile Platform (Town Existing)	164	DC6-48-60-18-8F Surge Arrestor (ATI Proposed)	138
4'x4" Pipe Mount (Town Existing)	160	Valmont Uni-Tri Bracket (ATI Proposed)	138
4'x4" Pipe Mount (Town Existing)	160	P65-16-XLH-RR (ATI Proposed)	134
4 FT DISH (Town Existing)	160	7770.00 (ATI Existing)	134
4 FT DISH (Town Existing)	160	7770.00 (ATI Existing)	134
2 FT DISH (Town Existing)	160	7770.00 (ATI Existing)	134
Remote Radio Head FD R6 RRH (Clearwire Existing)	154	P65-16-XLH-RR (ATI Proposed)	134
Remote Radio Head FD R6 RRH (Clearwire Existing)	154	(2) LGP214nn TMA (ATI Existing)	134
Remote Radio Head FD R6 RRH (Clearwire Existing)	154	(2) LGP214nn TMA (ATI Existing)	134
Remote Radio Head FD R6 RRH (Clearwire Existing)	154	(2) LGP214nn TMA (ATI Existing)	134
Horizon ODU (Clearwire Existing)	154	Low Profile Platform (ATI Existing)	134
Horizon ODU (Clearwire Existing)	154	7770.00 (ATI Existing)	134
(2) DB980F90E-M (Sprint Existing)	154	7770.00 (ATI Existing)	134
DB980F90E-M (Sprint Reserved)	154	P65-16-XLH-RR (ATI Proposed)	134
DB980F90E-M (Sprint Existing)	154	7770.00 (ATI Existing)	134
DB980F90E-M (Sprint Reserved)	154	7770.00 (ATI Existing)	134
(2) 950F65T2E-M (Sprint Existing)	154	844G65T6ZAXY (Verizon Existing)	124
950F65T2E-M (Sprint Reserved)	154	MG D3-800TX (Verizon Existing)	124
GPS (Sprint Existing)	154	LNX-6514DS-T0M (Verizon Existing)	124
Low Profile Platform (Sprint Existing)	154	844G65T6ZAXY (Verizon Existing)	124
LLPX310R (Clearwire Existing)	154	(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	124
LLPX310R (Clearwire Existing)	154	844G65T6ZAXY (Verizon Existing)	124
LLPX310R (Clearwire Existing)	154	844G65T6ZAXY (Verizon Existing)	124
A-Ant-23G-2-C (Clearwire Existing)	154	MG D3-800TX (Verizon Existing)	124
A-Ant-23G-2-C (Clearwire Existing)	154	LNX-6514DS-T0M (Verizon Existing)	124
(2) APX16PV-16PVL-X (T-Mobile Reserved)	144	844G65T6ZAXY (Verizon Existing)	124
(2) G20057A1 TMA (T-Mobile Existing)	144	(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	124
(2) G20057A1 TMA (T-Mobile Reserved)	144	Low Profile Platform (Verizon Existing)	124
(2) APX16PV-16PVL-X (T-Mobile Existing)	144	844G65T6ZAXY (Verizon Existing)	124
(2) APX16PV-16PVL-X (T-Mobile Reserved)	144	MG D3-800TX (Verizon Existing)	124
(2) G20057A1 TMA (T-Mobile Existing)	144	LNX-6514DS-T0M (Verizon Existing)	124
(2) G20057A1 TMA (T-Mobile Reserved)	144	844G65T6ZAXY (Verizon Existing)	124
Low Profile Platform (T-Mobile Existing)	144	(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	124
(2) APX16PV-16PVL-X (T-Mobile Existing)	144	(4) DBB46G90A-XY (Nextel Existing)	114
(2) APX16PV-16PVL-X (T-Mobile Reserved)	144	(4) DBB46G90A-XY (Nextel Existing)	114
		(4) DBB46G90A-XY (Nextel Existing)	114
		Low Profile Platform (Nextel Existing)	114
		GPS	51.5
		GPS	51.5
		GPS	51.5

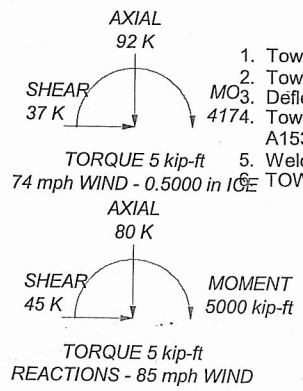
MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

1. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
2. Tower is also designed for a 74 mph basic wind with 0.50 in ice.
3. Deflections are based upon a 50 mph wind.
4. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
5. Welds are fabricated with ER-70S-6 electrodes.

TOWER RATING: 47.9%



Centek Engineering Inc.
 63-2 North Branford Road
 Branford, CT 06405
 Phone: 203.488.0580
 FAX: 203.488.8587

Job: 11009.CO12 - CT2102 - Greenwich Hosp
 Project: 164' EEI Monopole - Greenwich, CT
 Client: AT&T Mobility
 Code: TIA/EIA-222-F
 Path:

Drawn by: TJL
 Date: 04/14/11
 App'd:
 Scale: NTS
 Dwg No. E-1

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job 11009.CO12 - CT2102 - Greenwich Hospital	Page 1 of 21
	Project 164' EEI Monopole - Greenwich, CT	Date 11:10:20 04/14/11
	Client AT&T Mobility	Designed by TJL

Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Basic wind speed of 85 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 74 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..

Welds are fabricated with ER-70S-6 electrodes..

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

Options

- | | | |
|--|--|---|
| <ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination | <ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate Use Clear Spans For Wind Area Use Clear Spans For KL/r Retention Guys To Initial Tension Bypass Mast Stability Checks Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends √ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing | <ul style="list-style-type: none"> Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feedline Torque Include Angle Block Shear Check <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets |
|--|--|---|

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	164.00-131.50	32.50	0.00	18	47.0000	53.4200	0.3125	1.2500	A572-65 (65 ksi)
L2	131.50-119.29	12.21	6.00	18	53.4200	56.1500	0.3750	1.5000	A572-65 (65 ksi)
L3	119.29-78.79	46.50	8.42	18	54.0585	62.9700	0.4375	1.7500	A572-65 (65 ksi)
L4	78.79-39.88	47.33	9.25	18	60.4813	69.6600	0.5625	2.2500	A572-65 (65 ksi)
L5	39.88-1.50	47.63		18	66.7412	76.0000	0.5625	2.2500	A572-65 (65 ksi)

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	2 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Tapered Pole Properties

Section	Tip Dia. in	Area in ²	I in ⁴	r in	C in	I/C in ³	J in ⁴	I/O in ²	w in	w/t
L1	47.7251	46.3082	12752.5270	16.5741	23.8760	534.1149	25521.8341	23.1585	7.7220	24.71
	54.2441	52.6760	18769.9004	18.8532	27.1374	691.6627	37564.4987	26.3430	8.8519	28.326
L2	54.2441	63.1368	22444.4518	18.8310	27.1374	827.0684	44918.4365	31.5744	8.7419	23.312
	57.0162	66.3862	26091.2194	19.8001	28.5242	914.7047	52216.7704	33.1994	9.2224	24.593
L3	56.0600	74.4594	27047.4669	19.0354	27.4617	984.9157	54130.5236	37.2368	8.7443	19.987
	63.9414	86.8342	42898.2727	22.1990	31.9888	1341.0421	85852.9920	43.4253	10.3127	23.572
L4	63.0724	106.9776	48524.0652	21.2712	30.7245	1579.3269	97111.9796	53.4990	9.6547	17.164
	70.7346	123.3649	74413.8720	24.5296	35.3873	2102.8424	148925.659	61.6942	11.2702	20.036
L5	69.5966	118.1537	65376.3617	23.4934	33.9045	1928.2498	130838.747	59.0881	10.7564	19.123
	77.1724	134.6842	96834.1984	26.7803	38.6080	2508.1382	193795.813	67.3549	12.3860	22.02

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A _f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft ²	in					in	in
L1 164.00-131.50				1	1	1		
L2 131.50-119.29				1	1	1		
L3 119.29-78.79				1	1	1		
L4 78.79-39.88				1	1	1		
L5 39.88-1.50				1	1	1		

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement	Total Number	C _A A _A	Weight
				ft		ft ² /ft	plf
1/2 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	6	No Ice	0.25
5/8 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	1	1/2" Ice	0.25
7/8 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	3	No Ice	0.40
1 1/4 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	5	1/2" Ice	0.40
1 5/8 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	5	No Ice	0.54
1/2 (Town Existing)	A	No	Inside Pole	164.00 - 4.50	5	1/2" Ice	0.54
1 5/8 (Town Existing)	B	No	Inside Pole	154.00 - 7.50	6	No Ice	0.66
1/2 (Town Existing)	B	No	Inside Pole	154.00 - 7.50	6	1/2" Ice	1.04
2" Rigid Conduit (Clearwire Existing)	B	No	Inside Pole	154.00 - 7.50	1	No Ice	1.04
LDF4.5-50 (5/8 FOAM) (Clearwire Existing)	B	No	Inside Pole	154.00 - 7.50	2	1/2" Ice	0.25
1 5/8 (Clearwire Existing)	B	No	Inside Pole	154.00 - 7.50	2	No Ice	0.25
1 5/8 (Clearwire Existing)	B	No	Inside Pole	154.00 - 7.50	2	1/2" Ice	2.80
1 5/8 (Clearwire Existing)	B	No	Inside Pole	144.00 - 4.50	2	No Ice	2.80
1 5/8 (Clearwire Existing)	B	No	Inside Pole	144.00 - 4.50	12	1/2" Ice	0.15
1 5/8 (Clearwire Existing)	B	No	Inside Pole	144.00 - 4.50	12	No Ice	0.15

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job 11009.CO12 - CT2102 - Greenwich Hospital	Page 3 of 21
	Project 164' EEI Monopole - Greenwich, CT	Date 11:10:20 04/14/11
	Client AT&T Mobility	Designed by TJL

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C _{AA}	Weight
							ft ² /ft	plf
(T-Mobile Existing)								
1 5/8	A	No	Inside Pole	134.00 - 11.50	12	1/2" Ice	0.00	1.04
(AT&T Existing)						No Ice	0.00	1.04
1 5/8	C	No	Inside Pole	124.00 - 7.50	12	1/2" Ice	0.00	1.04
(Verizon Existing)						No Ice	0.00	1.04
1 5/8	C	No	Inside Pole	114.00 - 4.50	12	1/2" Ice	0.00	1.04
(Nextel Existing)						No Ice	0.00	1.04
RG6-Fiber	A	No	Inside Pole	134.00 - 11.50	1	1/2" Ice	0.00	0.00
(AT&T Propsoed)						No Ice	0.00	0.00
#8 AWG Copper Wire	A	No	Inside Pole	134.00 - 11.50	2	1/2" Ice	0.00	0.00
(AT&T Propsoed)						No Ice	0.00	0.00
7/8	B	No	CaAa (Out Of Face)	51.50 - 4.50	3	1/2" Ice	0.11	0.54
						1/2" Ice	0.21	1.52

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
L1	164.00-131.50	A	0.000	0.000	0.000	0.000	0.25
		B	0.000	0.000	0.000	0.000	0.43
		C	0.000	0.000	0.000	0.000	0.00
L2	131.50-119.29	A	0.000	0.000	0.000	0.000	0.24
		B	0.000	0.000	0.000	0.000	0.30
		C	0.000	0.000	0.000	0.000	0.06
L3	119.29-78.79	A	0.000	0.000	0.000	0.000	0.78
		B	0.000	0.000	0.000	0.000	1.01
		C	0.000	0.000	0.000	0.000	0.94
L4	78.79-39.88	A	0.000	0.000	0.000	0.000	0.75
		B	0.000	0.000	0.000	3.869	0.99
		C	0.000	0.000	0.000	0.000	0.97
L5	39.88-1.50	A	0.000	0.000	0.000	0.000	0.60
		B	0.000	0.000	0.000	11.782	0.90
		C	0.000	0.000	0.000	0.000	0.85

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
L1	164.00-131.50	A	0.500	0.000	0.000	0.000	0.000	0.25
		B		0.000	0.000	0.000	0.000	0.43
		C		0.000	0.000	0.000	0.000	0.00
L2	131.50-119.29	A	0.500	0.000	0.000	0.000	0.000	0.24
		B		0.000	0.000	0.000	0.000	0.30
		C		0.000	0.000	0.000	0.000	0.06
L3	119.29-78.79	A	0.500	0.000	0.000	0.000	0.000	0.78
		B		0.000	0.000	0.000	0.000	1.01
		C		0.000	0.000	0.000	0.000	0.94
L4	78.79-39.88	A	0.500	0.000	0.000	0.000	0.000	0.75
		B		0.000	0.000	0.000	7.355	1.02
		C		0.000	0.000	0.000	0.000	0.97
L5	39.88-1.50	A	0.500	0.000	0.000	0.000	0.000	0.60
		B		0.000	0.000	0.000	22.395	1.00
		C		0.000	0.000	0.000	0.000	0.85

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	4 of 21
	Project	Date
164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11	Designed by
Client	AT&T Mobility	TJL

Feed Line Center of Pressure

Section	Elevation	CP _X	CP _Z	CP _X Ice	CP _Z Ice
	ft	in	in	in	in
L1	164.00-131.50	0.0000	0.0000	0.0000	0.0000
L2	131.50-119.29	0.0000	0.0000	0.0000	0.0000
L3	119.29-78.79	0.0000	0.0000	0.0000	0.0000
L4	78.79-39.88	0.1320	0.0762	0.2434	0.1405
L5	39.88-1.50	0.3779	0.2182	0.6797	0.3924

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			ft ft ft	°	ft	ft ²	ft ²	K
4'x4" Pipe Mount (Town Existing)	A	From Face	0.50	0.0000	160.00	No Ice	1.32	0.04
			0.00			1/2" Ice	1.58	0.06
4'x4" Pipe Mount (Town Existing)	B	From Face	0.50	0.0000	160.00	No Ice	1.32	0.04
			0.00			1/2" Ice	1.58	0.06
4'x4" Pipe Mount (Town Existing)	C	From Face	0.50	0.0000	160.00	No Ice	1.32	0.04
			0.00			1/2" Ice	1.58	0.06
PD1142-1 (Town Existing)	A	From Face	4.00	0.0000	164.00	No Ice	1.32	0.01
			0.00			1/2" Ice	3.21	0.02
PD620-3 (Town Existing)	B	From Face	4.00	0.0000	164.00	No Ice	3.83	0.05
			0.00			1/2" Ice	5.99	0.08
ALR8 (Town Existing)	C	From Face	4.00	0.0000	164.00	No Ice	8.10	0.10
			0.00			1/2" Ice	10.80	0.15
BMR10 (Town Existing)	A	From Face	4.00	0.0000	164.00	No Ice	8.64	0.10
			-6.00			1/2" Ice	10.80	0.15
BMR10 (Town Existing)	B	From Face	4.00	0.0000	164.00	No Ice	8.64	0.10
			-6.00			1/2" Ice	10.80	0.15
BMR10 (Town Existing)	C	From Face	4.00	0.0000	164.00	No Ice	8.64	0.10
			-6.00			1/2" Ice	10.80	0.15
Camera (Town Existing)	C	From Face	4.00	0.0000	164.00	No Ice	3.00	0.10
			0.00			1/2" Ice	4.00	0.15
Low Profile Platform (Town Existing)	C	None		0.0000	164.00	No Ice	15.70	1.30
						1/2" Ice	20.10	1.76
LLPX310R (Clearwire Existing)	A	From Face	3.00	0.0000	154.00	No Ice	4.84	0.03
			0.00			1/2" Ice	5.19	0.05

RISATower

Centek Engineering Inc.
63-2 North Branford Road
Branford, CT 06405
Phone: 203.488.0580
FAX: 203.488.8587

Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	5 of 21
Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
Client	AT&T Mobility	Designed by	TJL

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _{AA} Front	C _{AA} Side	Weight K	
LLPX310R (Clearwire Existing)	B	From Face	3.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	4.84 5.19	1.96 2.23	0.03 0.05
LLPX310R (Clearwire Existing)	C	From Face	3.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	4.84 5.19	1.96 2.23	0.03 0.05
Remote Radio Head FD R6 RRH (Clearwire Existing)	A	From Face	3.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	1.80 1.99	0.78 0.92	0.03 0.04
Remote Radio Head FD R6 RRH (Clearwire Existing)	B	From Face	3.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	1.80 1.99	0.78 0.92	0.03 0.04
Remote Radio Head FD R6 RRH (Clearwire Existing)	C	From Face	3.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	1.80 1.99	0.78 0.92	0.03 0.04
Horizon ODU (Clearwire Existing)	A	None		0.0000	154.00	No Ice 1/2" Ice	0.79 0.91	0.17 0.25	0.00 0.00
Horizon ODU (Clearwire Existing)	C	None		0.0000	154.00	No Ice 1/2" Ice	0.79 0.91	0.17 0.25	0.00 0.00
(2) DB980F90E-M (Sprint Existing)	A	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	3.90 4.28	2.29 2.65	0.01 0.03
DB980F90E-M (Sprint Reserved)	A	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	3.90 4.28	2.29 2.65	0.01 0.03
(2) DB980F90E-M (Sprint Existing)	B	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	3.90 4.28	2.29 2.65	0.01 0.03
DB980F90E-M (Sprint Reserved)	B	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	3.90 4.28	2.29 2.65	0.01 0.03
(2) 950F65T2E-M (Sprint Existing)	C	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	6.42 6.88	4.24 4.62	0.02 0.06
950F65T2E-M (Sprint Reserved)	C	From Face	4.00 0.00 0.00	0.0000	154.00	No Ice 1/2" Ice	6.42 6.88	4.24 4.62	0.02 0.06
GPS (Sprint Existing)	C	From Face	4.00 -6.00 3.00	0.0000	154.00	No Ice 1/2" Ice	1.00 1.50	1.00 1.50	0.01 0.01
Low Profile Platform (Sprint Existing)	C	None		0.0000	154.00	No Ice 1/2" Ice	15.70 20.10	15.70 20.10	1.30 1.76
(2) APX16PV-16PVL-X (T-Mobile Existing)	A	From Face	4.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	6.70 7.13	2.00 2.33	0.04 0.07
(2) APX16PV-16PVL-X (T-Mobile Reserved)	A	From Face	4.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	6.70 7.13	2.00 2.33	0.04 0.07
(2) G20057A1 TMA (T-Mobile Existing)	A	From Face	4.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	0.82 0.95	0.39 0.49	0.01 0.02
(2) G20057A1 TMA (T-Mobile Reserved)	A	From Face	4.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	0.82 0.95	0.39 0.49	0.01 0.02
(2) APX16PV-16PVL-X (T-Mobile Existing)	B	From Face	4.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	6.70 7.13	2.00 2.33	0.04 0.07

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job#	11009.CC*12 - CT2102 - Greenwich Hospital	Page	6 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Description	Face or Leg	Offset Type	Offsets:			Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral	Vert					
(2) APX16PV-16PVL-X (T-Mobile Reserved)	B	From Face	4.00	0.0000	144.00	No Ice	6.70	2.00	0.04	
			0.00			1/2" Ice	7.13	2.33	0.07	
(2) G20057A1 TMA (T-Mobile Existing)	B	From Face	4.00	0.0000	144.00	No Ice	0.82	0.39	0.01	
			0.00			1/2" Ice	0.95	0.49	0.02	
(2) G20057A1 TMA (T-Mobile Reserved)	B	From Face	4.00	0.0000	144.00	No Ice	0.82	0.39	0.01	
			0.00			1/2" Ice	0.95	0.49	0.02	
(2) APX16PV-16PVL-X (T-Mobile Existing)	C	From Face	4.00	0.0000	144.00	No Ice	6.70	2.00	0.04	
			0.00			1/2" Ice	7.13	2.33	0.07	
(2) APX16PV-16PVL-X (T-Mobile Reserved)	C	From Face	4.00	0.0000	144.00	No Ice	6.70	2.00	0.04	
			0.00			1/2" Ice	7.13	2.33	0.07	
(2) G20057A1 TMA (T-Mobile Existing)	C	From Face	4.00	0.0000	144.00	No Ice	0.82	0.39	0.01	
			0.00			1/2" Ice	0.95	0.49	0.02	
(2) G20057A1 TMA (T-Mobile Reserved)	C	From Face	4.00	0.0000	144.00	No Ice	0.82	0.39	0.01	
			0.00			1/2" Ice	0.95	0.49	0.02	
Low Profile Platform (T-Mobile Existing)	C	None		0.0000	144.00	No Ice	15.70	15.70	1.30	
(2) RRUS-11 (AT&T Proposed)	A	From Face	0.50	0.0000	138.00	No Ice	20.10	20.10	1.76	
			0.00			1/2" Ice	3.17	1.01	0.04	
			0.00			1/2" Ice	3.41	1.20	0.06	
(2) RRUS-11 (AT&T Proposed)	B	From Face	0.50	0.0000	138.00	No Ice	3.17	1.01	0.04	
			0.00			1/2" Ice	3.41	1.20	0.06	
(2) RRUS-11 (AT&T Proposed)	C	From Face	0.50	0.0000	138.00	No Ice	3.17	1.01	0.04	
			0.00			1/2" Ice	3.41	1.20	0.06	
DC6-48-60-18-8F Surge Arrestor (AT&T Proposed)	C	From Face	0.50	0.0000	138.00	No Ice	1.27	1.27	0.02	
			0.00			1/2" Ice	1.46	1.46	0.04	
Valmont Uni-Tri Bracket (AT&T Proposed)	C	None		0.0000	138.00	No Ice	1.75	1.75	0.29	
7770.00 (AT&T Existing)	A	From Face	3.00	0.0000	134.00	No Ice	1.94	1.94	0.31	
			-2.00			1/2" Ice	5.88	2.93	0.04	
			0.00			1/2" Ice	6.31	3.27	0.07	
7770.00 (AT&T Existing)	A	From Face	3.00	0.0000	134.00	No Ice	5.88	2.93	0.04	
			2.00			1/2" Ice	6.31	3.27	0.07	
			0.00							
P65-16-XLH-RR (AT&T Proposed)	A	From Face	3.00	0.0000	134.00	No Ice	8.40	4.70	0.06	
			6.00			1/2" Ice	8.95	5.15	0.11	
			0.00							
7770.00 (AT&T Existing)	B	From Face	3.00	0.0000	134.00	No Ice	5.88	2.93	0.04	
			-2.00			1/2" Ice	6.31	3.27	0.07	
			0.00							
7770.00 (AT&T Existing)	B	From Face	3.00	0.0000	134.00	No Ice	5.88	2.93	0.04	
			2.00			1/2" Ice	6.31	3.27	0.07	
			0.00							
P65-16-XLH-RR (AT&T Proposed)	B	From Face	3.00	0.0000	134.00	No Ice	8.40	4.70	0.06	
			6.00			1/2" Ice	8.95	5.15	0.11	
			0.00							
7770.00 (AT&T Existing)	C	From Face	3.00	0.0000	134.00	No Ice	5.88	2.93	0.04	
			2.00			1/2" Ice	6.31	3.27	0.07	

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	7 of 21
	Project	Date
164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11	
Client	AT&T Mobility	Designed by
		TJL

Description	Face or Leg	Offset Type	Offsets:			Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral	Vert					
7770.00 (AT&T Existing)	C	From Face	0.00							
			3.00		0.0000	134.00	No Ice	5.88	2.93	0.04
			-2.00				1/2" Ice	6.31	3.27	0.07
			0.00							
P65-16-XLH-RR (AT&T Proposed)	C	From Face	3.00		0.0000	134.00	No Ice	8.40	4.70	0.06
			6.00				1/2" Ice	8.95	5.15	0.11
			0.00							
(2) LGP214nn TMA (AT&T Existing)	A	From Face	3.00		0.0000	134.00	No Ice	1.29	0.23	0.01
			-2.00				1/2" Ice	1.45	0.31	0.02
			0.00							
(2) LGP214nn TMA (AT&T Existing)	B	From Face	3.00		0.0000	134.00	No Ice	1.29	0.23	0.01
			-2.00				1/2" Ice	1.45	0.31	0.02
			0.00							
(2) LGP214nn TMA (AT&T Existing)	C	From Face	3.00		0.0000	134.00	No Ice	1.29	0.23	0.01
			-2.00				1/2" Ice	1.45	0.31	0.02
			0.00							
Low Profile Platform (AT&T Existing)	C	None			0.0000	134.00	No Ice	15.70	15.70	1.30
							1/2" Ice	20.10	20.10	1.76
844G65T6ZAXY (Verizon Existing)	A	From Face	4.00		0.0000	124.00	No Ice	4.67	3.73	0.01
			-6.00				1/2" Ice	5.05	4.10	0.04
			0.00							
MG D3-800TX (Verizon Existing)	A	From Face	4.00		0.0000	124.00	No Ice	3.45	2.22	0.00
			-4.00				1/2" Ice	3.80	2.55	0.02
			0.00							
LNX-6514DS-T0M (Verizon Existing)	A	From Face	4.00		0.0000	124.00	No Ice	8.41	5.41	0.04
			0.00				1/2" Ice	8.96	5.86	0.09
			0.00							
844G65T6ZAXY (Verizon Existing)	A	From Face	4.00		0.0000	124.00	No Ice	4.67	3.73	0.01
			6.00				1/2" Ice	5.05	4.10	0.04
			0.00							
(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	A	From Face	3.00		0.0000	124.00	No Ice	0.37	0.08	0.00
			0.00				1/2" Ice	0.45	0.14	0.01
			0.00							
844G65T6ZAXY (Verizon Existing)	B	From Face	4.00		0.0000	124.00	No Ice	4.67	3.73	0.01
			-6.00				1/2" Ice	5.05	4.10	0.04
			0.00							
MG D3-800TX (Verizon Existing)	B	From Face	4.00		0.0000	124.00	No Ice	3.45	2.22	0.00
			-4.00				1/2" Ice	3.80	2.55	0.02
			0.00							
LNX-6514DS-T0M (Verizon Existing)	B	From Face	4.00		0.0000	124.00	No Ice	8.41	5.41	0.04
			0.00				1/2" Ice	8.96	5.86	0.09
			0.00							
844G65T6ZAXY (Verizon Existing)	B	From Face	4.00		0.0000	124.00	No Ice	4.67	3.73	0.01
			6.00				1/2" Ice	5.05	4.10	0.04
			0.00							
(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	B	From Face	3.00		0.0000	124.00	No Ice	0.37	0.08	0.00
			0.00				1/2" Ice	0.45	0.14	0.01
			0.00							
844G65T6ZAXY (Verizon Existing)	C	From Face	4.00		0.0000	124.00	No Ice	4.67	3.73	0.01
			-6.00				1/2" Ice	5.05	4.10	0.04
			0.00							
MG D3-800TX (Verizon Existing)	C	From Face	4.00		0.0000	124.00	No Ice	3.45	2.22	0.00
			-4.00				1/2" Ice	3.80	2.55	0.02
			0.00							
LNX-6514DS-T0M (Verizon Existing)	C	From Face	4.00		0.0000	124.00	No Ice	8.41	5.41	0.04
			0.00				1/2" Ice	8.96	5.86	0.09
			0.00							

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	8 of 21
	Project	Date
164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11	
Client	AT&T Mobility	Designed by
		TJL

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _A A _A		Weight
			Horz	Lateral			Front	Side	
			Vert						
			ft	ft	°	ft	ft ²	ft ²	K
			ft						
844G65T6ZAXY (Verizon Existing)	C	From Face	4.00	0.0000	124.00	No Ice	4.67	3.73	0.01
			6.00			1/2" Ice	5.05	4.10	0.04
			0.00						
(2) FD9R6004/2C-3L Diplexer (Verizon Existing)	C	From Face	3.00	0.0000	124.00	No Ice	0.37	0.08	0.00
			0.00			1/2" Ice	0.45	0.14	0.01
			0.00						
Low Profile Platform (Verizon Existing)	C	None		0.0000	124.00	No Ice	15.70	15.70	1.30
						1/2" Ice	20.10	20.10	1.76
(4) DB846G90A-XY (Nextel Existing)	A	From Face	4.00	0.0000	114.00	No Ice	4.99	5.87	0.02
			0.00			1/2" Ice	5.44	6.32	0.05
			0.00						
(4) DB846G90A-XY (Nextel Existing)	B	From Face	4.00	0.0000	114.00	No Ice	4.99	5.87	0.02
			0.00			1/2" Ice	5.44	6.32	0.05
			0.00						
(4) DB846G90A-XY (Nextel Existing)	C	From Face	4.00	0.0000	114.00	No Ice	4.99	5.87	0.02
			0.00			1/2" Ice	5.44	6.32	0.05
			0.00						
Low Profile Platform (Nextel Existing)	C	None		0.0000	114.00	No Ice	15.70	15.70	1.30
						1/2" Ice	20.10	20.10	1.76
GPS	A	From Face	1.50	0.0000	51.50	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.01
			0.00						
GPS	B	From Face	1.50	0.0000	51.50	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.01
			0.00						
GPS	C	From Face	1.50	0.0000	51.50	No Ice	1.00	1.00	0.01
			0.00			1/2" Ice	1.50	1.50	0.01
			0.00						

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz	Lateral						
			Vert		°	°	ft	ft	ft ²	K	
			ft								
4 FT DISH (Town Existing)	A	Paraboloid w/Shroud (HP)	From Leg	1.00	0.00	Worst		160.00	4.00	No Ice	0.17
				0.00						1/2" Ice	0.24
				0.00							
4 FT DISH (Town Existing)	B	Paraboloid w/Shroud (HP)	From Leg	1.00	0.00	Worst		160.00	4.00	No Ice	0.17
				0.00						1/2" Ice	0.24
				0.00							
2 FT DISH (Town Existing)	C	Paraboloid w/Shroud (HP)	From Leg	1.00	0.00	Worst		160.00	2.00	No Ice	0.03
				0.00						1/2" Ice	0.04
				0.00							
A-Ant-23G-2-C (Clearwire Existing)	A	Paraboloid w/Radome	From Face	3.10	-2.52	Worst		154.00	2.17	No Ice	0.03
				2.00						1/2" Ice	0.05
				2.00							
A-Ant-23G-2-C (Clearwire Existing)	C	Paraboloid w/Radome	From Face	3.80	-1.24	Worst		154.00	2.17	No Ice	0.03
				2.00						1/2" Ice	0.05
				2.00							

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	9 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Tower Pressures - No Ice

$G_H = 1.690$

Section Elevation	z	K_z	q_z	A_G	Face	A_F	A_R	A_{leg}	Leg %	$C_A A_A$ In Face	$C_A A_A$ Out Face
ft	ft		psf	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
L1 164.00-131.50	147.53	1.534	28	135.985	A	0.000	135.985	135.985	100.00	0.000	0.000
					B	0.000	135.985	100.00	0.000	0.000	
					C	0.000	135.985	100.00	0.000	0.000	
L2 131.50-119.29	125.34	1.464	27	55.744	A	0.000	55.744	55.744	100.00	0.000	0.000
					B	0.000	55.744	100.00	0.000	0.000	
					C	0.000	55.744	100.00	0.000	0.000	
L3 119.29-78.79	98.89	1.368	25	199.426	A	0.000	199.426	199.426	100.00	0.000	0.000
					B	0.000	199.426	100.00	0.000	0.000	
					C	0.000	199.426	100.00	0.000	0.000	
L4 78.79-39.88	59.42	1.183	22	213.639	A	0.000	213.639	213.639	100.00	0.000	0.000
					B	0.000	213.639	100.00	0.000	3.869	
					C	0.000	213.639	100.00	0.000	0.000	
L5 39.88-1.50	20.36	1	18	231.142	A	0.000	231.142	231.142	100.00	0.000	0.000
					B	0.000	231.142	100.00	0.000	11.782	
					C	0.000	231.142	100.00	0.000	0.000	

Tower Pressure - With Ice

$G_H = 1.690$

Section Elevation	z	K_z	q_z	t_z	A_G	Face	A_F	A_R	A_{leg}	Leg %	$C_A A_A$ In Face	$C_A A_A$ Out Face
ft	ft		psf	in	ft ²	e	ft ²	ft ²	ft ²		ft ²	ft ²
L1 164.00-131.50	147.53	1.534	21	0.5000	138.694	A	0.000	138.694	138.694	100.00	0.000	0.000
						B	0.000	138.694	100.00	0.000	0.000	
						C	0.000	138.694	100.00	0.000	0.000	
L2 131.50-119.29	125.34	1.464	20	0.5000	56.761	A	0.000	56.761	56.761	100.00	0.000	0.000
						B	0.000	56.761	100.00	0.000	0.000	
						C	0.000	56.761	100.00	0.000	0.000	
L3 119.29-78.79	98.89	1.368	19	0.5000	202.801	A	0.000	202.801	202.801	100.00	0.000	0.000
						B	0.000	202.801	100.00	0.000	0.000	
						C	0.000	202.801	100.00	0.000	0.000	
L4 78.79-39.88	59.42	1.183	16	0.5000	216.881	A	0.000	216.881	216.881	100.00	0.000	0.000
						B	0.000	216.881	100.00	0.000	7.355	
						C	0.000	216.881	100.00	0.000	0.000	
L5 39.88-1.50	20.36	1	14	0.5000	234.341	A	0.000	234.341	234.341	100.00	0.000	0.000
						B	0.000	234.341	100.00	0.000	22.395	
						C	0.000	234.341	100.00	0.000	0.000	

Tower Pressure - Service

$G_H = 1.690$

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	10 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Section Elevation	z	K _z	q _z	A _G	F a c e	A _F	A _R	A _{leg}	Leg %	C _{AA} _{In} Face	C _{AA} _{Out} Face
ft	ft		psf	ft ²		ft ²	ft ²	ft ²		ft ²	ft ²
L1 164.00-131.50	147.53	1.534	10	135.985	A	0.000	135.985	135.985	100.00	0.000	0.000
					B	0.000	135.985	100.00	0.000	0.000	
					C	0.000	135.985	100.00	0.000	0.000	
L2 131.50-119.29	125.34	1.464	9	55.744	A	0.000	55.744	55.744	100.00	0.000	0.000
					B	0.000	55.744	100.00	0.000	0.000	
					C	0.000	55.744	100.00	0.000	0.000	
L3 119.29-78.79	98.89	1.368	9	199.426	A	0.000	199.426	199.426	100.00	0.000	0.000
					B	0.000	199.426	100.00	0.000	0.000	
					C	0.000	199.426	100.00	0.000	0.000	
L4 78.79-39.88	59.42	1.183	8	213.639	A	0.000	213.639	213.639	100.00	0.000	0.000
					B	0.000	213.639	100.00	0.000	3.869	
					C	0.000	213.639	100.00	0.000	0.000	
L5 39.88-1.50	20.36	1	6	231.142	A	0.000	231.142	231.142	100.00	0.000	0.000
					B	0.000	231.142	100.00	0.000	11.782	
					C	0.000	231.142	100.00	0.000	0.000	

Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	4.24	130.34	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	1.66	135.82	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-78.79	2.73	12.76	A	1	0.65	1	1	1	199.426	5.53	136.63	C
			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	5.25	134.97	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	5.06	131.96	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	1762.61 kip-ft	21.74		

Tower Forces - No Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	4.24	130.34	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	1.66	135.82	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-	2.73	12.76	A	1	0.65	1	1	1	199.426	5.53	136.63	C

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	11 of 21
	Project	Date
	164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11
	Client	Designed by
	AT&T Mobility	TJL

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K	e						ft ²	K	plf	
78.79			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	5.25	134.97	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	5.06	131.96	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	1762.61 kip-ft	21.74		

Tower Forces - No Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K	e						ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	4.24	130.34	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	1.66	135.82	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-78.79	2.73	12.76	A	1	0.65	1	1	1	199.426	5.53	136.63	C
			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	5.25	134.97	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	5.06	131.96	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	1762.61 kip-ft	21.74		

Tower Forces - With Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K	e						ft ²	K	plf	
L1 164.00-131.50	0.69	6.49	A	1	0.65	1	1	1	138.694	3.24	99.70	C
			B	1	0.65	1	1	1	138.694			
			C	1	0.65	1	1	1	138.694			
L2 131.50-119.29	0.60	3.11	A	1	0.65	1	1	1	56.761	1.27	103.72	C
			B	1	0.65	1	1	1	56.761			
			C	1	0.65	1	1	1	56.761			
L3 119.29-78.79	2.73	14.25	A	1	0.65	1	1	1	202.801	4.22	104.21	C
			B	1	0.65	1	1	1	202.801			
			C	1	0.65	1	1	1	202.801			
L4 78.79-	2.74	20.14	A	1	0.65	1	1	1	216.881	4.09	105.20	C

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	Project	Date
	Client	Designed by
	11009.CO12 - CT2102 - Greenwich Hospital	12 of 21
	164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11
	AT&T Mobility	TJL

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
39.88			B	1	0.65	1	1	1	216.881			
L5 39.88-1.50	2.45	22.21	C	1	0.65	1	1	1	216.881	4.10	106.72	C
			A	1	0.65	1	1	1	234.341			
			B	1	0.65	1	1	1	234.341			
			C	1	0.65	1	1	1	234.341			
Sum Weight:	9.21	66.20						OTM	1355.40	16.92		
									kip-ft			

Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	6.49	A	1	0.65	1	1	1	138.694	3.24	99.70	C
			B	1	0.65	1	1	1	138.694			
			C	1	0.65	1	1	1	138.694			
L2 131.50-119.29	0.60	3.11	A	1	0.65	1	1	1	56.761	1.27	103.72	C
			B	1	0.65	1	1	1	56.761			
			C	1	0.65	1	1	1	56.761			
L3 119.29-78.79	2.73	14.25	A	1	0.65	1	1	1	202.801	4.22	104.21	C
			B	1	0.65	1	1	1	202.801			
			C	1	0.65	1	1	1	202.801			
L4 78.79-39.88	2.74	20.14	A	1	0.65	1	1	1	216.881	4.09	105.20	C
			B	1	0.65	1	1	1	216.881			
			C	1	0.65	1	1	1	216.881			
L5 39.88-1.50	2.45	22.21	A	1	0.65	1	1	1	234.341	4.10	106.72	C
			B	1	0.65	1	1	1	234.341			
			C	1	0.65	1	1	1	234.341			
			C	1	0.65	1	1	1	234.341			
Sum Weight:	9.21	66.20						OTM	1355.40	16.92		
									kip-ft			

Tower Forces - With Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	6.49	A	1	0.65	1	1	1	138.694	3.24	99.70	C
			B	1	0.65	1	1	1	138.694			
			C	1	0.65	1	1	1	138.694			
L2 131.50-119.29	0.60	3.11	A	1	0.65	1	1	1	56.761	1.27	103.72	C
			B	1	0.65	1	1	1	56.761			
			C	1	0.65	1	1	1	56.761			
L3 119.29-78.79	2.73	14.25	A	1	0.65	1	1	1	202.801	4.22	104.21	C
			B	1	0.65	1	1	1	202.801			
			C	1	0.65	1	1	1	202.801			
L4 78.79-39.88	2.74	20.14	A	1	0.65	1	1	1	216.881	4.09	105.20	C
			B	1	0.65	1	1	1	216.881			
			C	1	0.65	1	1	1	216.881			
L5 39.88-1.50	2.45	22.21	C	1	0.65	1	1	1	216.881	4.10	106.72	C
			A	1	0.65	1	1	1	234.341			

RISA Tower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	13 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
			B	1	0.65	1	1	1	234.341			
			C	1	0.65	1	1	1	234.341			
Sum Weight:	9.21	66.20						OTM	1355.40 kip-ft	16.92		

Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	1.47	45.10	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	0.57	47.00	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-78.79	2.73	12.76	A	1	0.65	1	1	1	199.426	1.91	47.28	C
			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	1.82	46.70	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	1.75	45.66	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	609.90 kip-ft	7.52		

Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K							ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	1.47	45.10	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	0.57	47.00	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-78.79	2.73	12.76	A	1	0.65	1	1	1	199.426	1.91	47.28	C
			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	1.82	46.70	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	1.75	45.66	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	609.90	7.52		

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	14 of 21
	Project	Date
	164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11
	Client	Designed by
	AT&T Mobility	TJL

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K	e						ft ²	K	plf	
									kip-ft			

Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C _F	R _R	D _F	D _R	A _E	F	w	Ctrl. Face
ft	K	K	e						ft ²	K	plf	
L1 164.00-131.50	0.69	5.47	A	1	0.65	1	1	1	135.985	1.47	45.10	C
			B	1	0.65	1	1	1	135.985			
			C	1	0.65	1	1	1	135.985			
L2 131.50-119.29	0.60	2.69	A	1	0.65	1	1	1	55.744	0.57	47.00	C
			B	1	0.65	1	1	1	55.744			
			C	1	0.65	1	1	1	55.744			
L3 119.29-78.79	2.73	12.76	A	1	0.65	1	1	1	199.426	1.91	47.28	C
			B	1	0.65	1	1	1	199.426			
			C	1	0.65	1	1	1	199.426			
L4 78.79-39.88	2.71	18.55	A	1	0.65	1	1	1	213.639	1.82	46.70	C
			B	1	0.65	1	1	1	213.639			
			C	1	0.65	1	1	1	213.639			
L5 39.88-1.50	2.34	20.49	A	1	0.65	1	1	1	231.142	1.75	45.66	C
			B	1	0.65	1	1	1	231.142			
			C	1	0.65	1	1	1	231.142			
Sum Weight:	9.07	59.96						OTM	609.90	7.52		
									kip-ft			

Force Totals

Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Z	Sum of Overturning Moments, M _x	Sum of Overturning Moments, M _z	Sum of Torques
	K	K	K	kip-ft	kip-ft	kip-ft
Leg Weight	59.96					
Bracing Weight	0.00					
Total Member Self-Weight	59.96			1.39	-0.70	
Total Weight	80.36			1.39	-0.70	
Wind 0 deg - No Ice		0.00	-44.54	-4928.15	-0.70	1.98
Wind 30 deg - No Ice		22.23	-38.58	-4267.72	-2459.08	4.11
Wind 60 deg - No Ice		38.50	-22.27	-2463.38	-4258.73	5.14
Wind 90 deg - No Ice		44.46	0.00	1.39	-4917.45	4.79
Wind 120 deg - No Ice		38.50	22.27	2466.17	-4258.73	3.16
Wind 150 deg - No Ice		22.23	38.58	4270.51	-2459.08	0.68
Wind 180 deg - No Ice		0.00	44.54	4930.94	-0.70	-1.98
Wind 210 deg - No Ice		-22.23	38.58	4270.51	2457.67	-4.11
Wind 240 deg - No Ice		-38.50	22.27	2466.17	4257.32	-5.14
Wind 270 deg - No Ice		-44.46	0.00	1.39	4916.04	-4.79
Wind 300 deg - No Ice		-38.50	-22.27	-2463.38	4257.32	-3.16
Wind 330 deg - No Ice		-22.23	-38.58	-4267.72	2457.67	-0.68
Member Ice	6.24					
Total Weight Ice	92.26			2.43	-1.23	
Wind 0 deg - Ice		0.00	-36.63	-4099.19	-1.23	1.79

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	Project	Date
	Client	Designed by
	11009.CO12 - CT2102 - Greenwich Hospital	15 of 21
	164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11
	AT&T Mobility	TJL

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M_x kip-ft	Sum of Overturning Moments, M_z kip-ft	Sum of Torques kip-ft
Wind 30 deg - Ice		18.28	-31.72	-3549.68	-2046.72	3.66
Wind 60 deg - Ice		31.66	-18.31	-2048.38	-3544.12	4.56
Wind 90 deg - Ice		36.56	0.00	2.43	-4092.21	4.23
Wind 120 deg - Ice		31.66	18.31	2053.24	-3544.12	2.77
Wind 150 deg - Ice		18.28	31.72	3554.54	-2046.72	0.56
Wind 180 deg - Ice		0.00	36.63	4104.06	-1.23	-1.79
Wind 210 deg - Ice		-18.28	31.72	3554.54	2044.26	-3.66
Wind 240 deg - Ice		-31.66	18.31	2053.24	3541.67	-4.56
Wind 270 deg - Ice		-36.56	0.00	2.43	4089.75	-4.23
Wind 300 deg - Ice		-31.66	-18.31	-2048.38	3541.67	-2.77
Wind 330 deg - Ice		-18.28	-31.72	-3549.68	2044.26	-0.56
Total Weight	80.36			1.39	-0.70	
Wind 0 deg - Service		0.00	-15.41	-1704.44	-0.51	0.68
Wind 30 deg - Service		7.69	-13.35	-1475.92	-851.16	1.42
Wind 60 deg - Service		13.32	-7.71	-851.58	-1473.87	1.78
Wind 90 deg - Service		15.38	0.00	1.28	-1701.80	1.66
Wind 120 deg - Service		13.32	7.71	854.14	-1473.87	1.09
Wind 150 deg - Service		7.69	13.35	1478.48	-851.16	0.24
Wind 180 deg - Service		0.00	15.41	1707.01	-0.51	-0.68
Wind 210 deg - Service		-7.69	13.35	1478.48	850.14	-1.42
Wind 240 deg - Service		-13.32	7.71	854.14	1472.86	-1.78
Wind 270 deg - Service		-15.38	0.00	1.28	1700.79	-1.66
Wind 300 deg - Service		-13.32	-7.71	-851.58	1472.86	-1.09
Wind 330 deg - Service		-7.69	-13.35	-1475.92	850.14	-0.24

Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	16 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Comb. No.	Description
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	164 - 131.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-19.18	-0.68	-2.12
			Max. Mx	5	-13.95	-371.29	-1.20
			Max. My	8	-13.95	-0.48	-373.97
			Max. Vy	5	20.31	-371.29	-1.20
			Max. Vx	8	20.40	-0.48	-373.97
			Max. Torque	4			-4.95
			Max Tension	1	0.00	0.00	0.00
L2	131.5 - 119.29	Pole	Max. Compression	14	-21.04	-0.68	-2.12
			Max. Mx	5	-15.60	-500.10	-1.21
			Max. My	8	-15.59	-0.48	-503.31
			Max. Vy	5	21.18	-500.10	-1.21
			Max. Vx	8	21.26	-0.48	-503.31
			Max. Torque	4			-4.95
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-41.32	-0.68	-2.12
L3	119.29 - 78.79	Pole	Max. Mx	5	-32.64	-1627.57	-1.27
			Max. My	8	-32.64	-0.51	-1634.04
			Max. Vy	5	33.44	-1627.57	-1.27
			Max. Vx	8	33.53	-0.51	-1634.04
			Max. Torque	4			-4.95
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-62.72	-0.78	-2.17
			Max. Mx	5	-52.64	-3002.22	-1.32
L4	78.79 - 39.88	Pole	Max. My	8	-52.64	-0.55	-3011.95
			Max. Vy	5	38.73	-3002.22	-1.32
			Max. Vx	8	38.81	-0.55	-3011.95
			Max. Torque	4			-4.99
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-92.26	-1.23	-2.43
			Max. Mx	5	-80.35	-4986.30	-1.42
			Max. My	8	-80.35	-0.72	-5000.01
L5	39.88 - 1.5	Pole	Max. Vy	5	44.48	-4986.30	-1.42
			Max. Vx	8	44.56	-0.72	-5000.01
			Max. Torque	4			-5.16

Maximum Reactions

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	17 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	21	92.26	0.00	-36.63
	Max. H _x	11	80.36	44.46	-0.00
	Max. H _z	2	80.36	0.00	44.54
	Max. M _x	2	4997.15	0.00	44.54
	Max. M _z	5	4986.30	-44.46	-0.00
	Max. Torsion	10	5.16	38.50	-22.27
	Min. Vert	33	80.36	0.00	-15.41
	Min. H _x	5	80.36	-44.46	-0.00
	Min. H _z	8	80.36	0.00	-44.54
	Min. M _x	8	-5000.01	0.00	-44.54
	Min. M _z	11	-4984.87	44.46	-0.00
	Min. Torsion	4	-5.16	-38.50	22.27

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overtuning Moment, M _x kip-ft	Overtuning Moment, M _z kip-ft	Torque kip-ft
Dead Only	80.36	0.00	0.00	1.39	-0.70	0.00
Dead+Wind 0 deg - No Ice	80.36	0.00	-44.54	-4997.15	-0.72	1.98
Dead+Wind 30 deg - No Ice	80.36	22.23	-38.58	-4327.47	-2493.51	4.12
Dead+Wind 60 deg - No Ice	80.36	38.50	-22.27	-2497.87	-4318.36	5.16
Dead+Wind 90 deg - No Ice	80.36	44.46	0.00	1.42	-4986.30	4.82
Dead+Wind 120 deg - No Ice	80.36	38.50	22.27	2500.72	-4318.36	3.19
Dead+Wind 150 deg - No Ice	80.36	22.23	38.58	4330.32	-2493.51	0.70
Dead+Wind 180 deg - No Ice	80.36	0.00	44.54	5000.01	-0.72	-1.98
Dead+Wind 210 deg - No Ice	80.36	-22.23	38.58	4330.32	2492.08	-4.12
Dead+Wind 240 deg - No Ice	80.36	-38.50	22.27	2500.71	4316.92	-5.16
Dead+Wind 270 deg - No Ice	80.36	-44.46	0.00	1.42	4984.87	-4.82
Dead+Wind 300 deg - No Ice	80.36	-38.50	-22.27	-2497.87	4316.92	-3.19
Dead+Wind 330 deg - No Ice	80.36	-22.23	-38.58	-4327.47	2492.07	-0.70
Dead+Ice+Temp	92.26	0.00	0.00	2.43	-1.23	0.00
Dead+Wind 0 deg+Ice+Temp	92.26	0.00	-36.63	-4170.62	-1.25	1.79
Dead+Wind 30 deg+Ice+Temp	92.26	18.28	-31.72	-3611.53	-2082.39	3.68
Dead+Wind 60 deg+Ice+Temp	92.26	31.66	-18.31	-2084.06	-3605.88	4.59
Dead+Wind 90 deg+Ice+Temp	92.26	36.56	0.00	2.50	-4163.52	4.27
Dead+Wind 120 deg+Ice+Temp	92.26	31.66	18.31	2089.06	-3605.89	2.80
Dead+Wind 150 deg+Ice+Temp	92.26	18.28	31.72	3616.53	-2082.39	0.58
Dead+Wind 180 deg+Ice+Temp	92.26	0.00	36.63	4175.62	-1.25	-1.79
Dead+Wind 210 deg+Ice+Temp	92.26	-18.28	31.72	3616.53	2079.88	-3.68
Dead+Wind 240 deg+Ice+Temp	92.26	-31.66	18.31	2089.06	3603.38	-4.59
Dead+Wind 270 deg+Ice+Temp	92.26	-36.56	0.00	2.50	4161.02	-4.27
Dead+Wind 300 deg+Ice+Temp	92.26	-31.66	-18.31	-2084.06	3603.38	-2.80
Dead+Wind 330 deg+Ice+Temp	92.26	-18.28	-31.72	-3611.53	2079.88	-0.58
Dead+Wind 0 deg - Service	80.36	0.00	-15.41	-1728.35	-0.72	0.68
Dead+Wind 30 deg - Service	80.36	7.69	-13.35	-1496.60	-863.35	1.43
Dead+Wind 60 deg - Service	80.36	13.32	-7.71	-863.46	-1494.85	1.79
Dead+Wind 90 deg - Service	80.36	15.38	0.00	1.43	-1725.99	1.67
Dead+Wind 120 deg - Service	80.36	13.32	7.71	866.31	-1494.85	1.10
Dead+Wind 150 deg - Service	80.36	7.69	13.35	1499.45	-863.35	0.24
Dead+Wind 180 deg - Service	80.36	0.00	15.41	1731.20	-0.72	-0.68
Dead+Wind 210 deg - Service	80.36	-7.69	13.35	1499.45	861.92	-1.43
Dead+Wind 240 deg - Service	80.36	-13.32	7.71	866.31	1493.41	-1.79
Dead+Wind 270 deg - Service	80.36	-15.38	0.00	1.43	1724.55	-1.67
Dead+Wind 300 deg - Service	80.36	-13.32	-7.71	-863.46	1493.41	-1.10
Dead+Wind 330 deg - Service	80.36	-7.69	-13.35	-1496.60	861.92	-0.24

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	11009.CO12 - CT2102 - Greenwich Hospital	18 of 21
	Project	Date
164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11	Client
AT&T Mobility	Designed by	TJL

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-80.36	0.00	0.00	80.36	0.00	0.000%
2	0.00	-80.36	-44.54	0.00	80.36	44.54	0.000%
3	22.23	-80.36	-38.58	-22.23	80.36	38.58	0.000%
4	38.50	-80.36	-22.27	-38.50	80.36	22.27	0.000%
5	44.46	-80.36	0.00	-44.46	80.36	-0.00	0.000%
6	38.50	-80.36	22.27	-38.50	80.36	-22.27	0.000%
7	22.23	-80.36	38.58	-22.23	80.36	-38.58	0.000%
8	0.00	-80.36	44.54	0.00	80.36	-44.54	0.000%
9	-22.23	-80.36	38.58	22.23	80.36	-38.58	0.000%
10	-38.50	-80.36	22.27	38.50	80.36	-22.27	0.000%
11	-44.46	-80.36	0.00	44.46	80.36	-0.00	0.000%
12	-38.50	-80.36	-22.27	38.50	80.36	22.27	0.000%
13	-22.23	-80.36	-38.58	22.23	80.36	38.58	0.000%
14	0.00	-92.26	0.00	0.00	92.26	0.00	0.000%
15	0.00	-92.26	-36.63	0.00	92.26	36.63	0.000%
16	18.28	-92.26	-31.72	-18.28	92.26	31.72	0.000%
17	31.66	-92.26	-18.31	-31.66	92.26	18.31	0.000%
18	36.56	-92.26	0.00	-36.56	92.26	0.00	0.000%
19	31.66	-92.26	18.31	-31.66	92.26	-18.31	0.000%
20	18.28	-92.26	31.72	-18.28	92.26	-31.72	0.000%
21	0.00	-92.26	36.63	0.00	92.26	-36.63	0.000%
22	-18.28	-92.26	31.72	18.28	92.26	-31.72	0.000%
23	-31.66	-92.26	18.31	31.66	92.26	-18.31	0.000%
24	-36.56	-92.26	0.00	36.56	92.26	0.00	0.000%
25	-31.66	-92.26	-18.31	31.66	92.26	18.31	0.000%
26	-18.28	-92.26	-31.72	18.28	92.26	31.72	0.000%
27	0.00	-80.36	-15.41	0.00	80.36	15.41	0.000%
28	7.69	-80.36	-13.35	-7.69	80.36	13.35	0.000%
29	13.32	-80.36	-7.71	-13.32	80.36	7.71	0.000%
30	15.38	-80.36	0.00	-15.38	80.36	0.00	0.000%
31	13.32	-80.36	7.71	-13.32	80.36	-7.71	0.000%
32	7.69	-80.36	13.35	-7.69	80.36	-13.35	0.000%
33	0.00	-80.36	15.41	0.00	80.36	-15.41	0.000%
34	-7.69	-80.36	13.35	7.69	80.36	-13.35	0.000%
35	-13.32	-80.36	7.71	13.32	80.36	-7.71	0.000%
36	-15.38	-80.36	0.00	15.38	80.36	0.00	0.000%
37	-13.32	-80.36	-7.71	13.32	80.36	7.71	0.000%
38	-7.69	-80.36	-13.35	7.69	80.36	13.35	0.000%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00006550
3	Yes	4	0.00000001	0.00057312
4	Yes	4	0.00000001	0.00044568
5	Yes	4	0.00000001	0.00015644
6	Yes	4	0.00000001	0.00055794
7	Yes	4	0.00000001	0.00048902
8	Yes	4	0.00000001	0.00006556

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	Page
	Project	Date
	Client	Designed by
	11009.CO12 - CT2102 - Greenwich Hospital	19 of 21
	164' EEI Monopole - Greenwich, CT	11:10:20 04/14/11
	AT&T Mobility	TJL

9	Yes	4	0.00000001	0.00045320
10	Yes	4	0.00000001	0.00059581
11	Yes	4	0.00000001	0.00015638
12	Yes	4	0.00000001	0.00045846
13	Yes	4	0.00000001	0.00051235
14	Yes	4	0.00000001	0.00000001
15	Yes	5	0.00000001	0.00002182
16	Yes	5	0.00000001	0.00002892
17	Yes	5	0.00000001	0.00002816
18	Yes	5	0.00000001	0.00002201
19	Yes	5	0.00000001	0.00002886
20	Yes	5	0.00000001	0.00002843
21	Yes	5	0.00000001	0.00002187
22	Yes	5	0.00000001	0.00002824
23	Yes	5	0.00000001	0.00002911
24	Yes	5	0.00000001	0.00002199
25	Yes	5	0.00000001	0.00002818
26	Yes	5	0.00000001	0.00002849
27	Yes	4	0.00000001	0.00001493
28	Yes	4	0.00000001	0.00004426
29	Yes	4	0.00000001	0.00003368
30	Yes	4	0.00000001	0.00002563
31	Yes	4	0.00000001	0.00004200
32	Yes	4	0.00000001	0.00003293
33	Yes	4	0.00000001	0.00001498
34	Yes	4	0.00000001	0.00003234
35	Yes	4	0.00000001	0.00004796
36	Yes	4	0.00000001	0.00002560
37	Yes	4	0.00000001	0.00003169
38	Yes	4	0.00000001	0.00003539

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	164 - 131.5	10.579	33	0.4930	0.0026
L2	131.5 - 119.29	7.283	33	0.4648	0.0015
L3	125.29 - 78.79	6.686	33	0.4532	0.0014
L4	87.21 - 39.88	3.430	33	0.3441	0.0007
L5	49.13 - 1.5	1.156	33	0.2097	0.0003

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
164.00	PD1142-1	33	10.579	0.4930	0.0026	210712
160.00	4 FT DISH	33	10.165	0.4911	0.0025	210712
156.00	A-Ant-23G-2-C	33	9.752	0.4890	0.0023	131695
154.00	LLPX310R	33	9.546	0.4878	0.0023	105356
144.00	(2) APX16PV-16PVL-X	33	8.526	0.4804	0.0019	52678
138.00	(2) RRUS-11	33	7.924	0.4740	0.0017	40521
134.00	7770.00	33	7.528	0.4687	0.0016	35149
124.00	844G65T6ZAXY	33	6.564	0.4505	0.0013	27944
114.00	(4) DB846G90A-XY	33	5.643	0.4264	0.0011	24691

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	20 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
51.50	GPS	33	1.258	0.2189	0.0004	11247

Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
L1	164 - 131.5	30.531	8	1.4217	0.0076
L2	131.5 - 119.29	21.027	8	1.3412	0.0045
L3	125.29 - 78.79	19.303	8	1.3081	0.0040
L4	87.21 - 39.88	9.904	8	0.9936	0.0021
L5	49.13 - 1.5	3.337	8	0.6056	0.0010

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
164.00	PD1142-1	8	30.531	1.4217	0.0076	73805
160.00	4 FT DISH	8	29.339	1.4162	0.0072	73805
156.00	A-Ant-23G-2-C	8	28.148	1.4103	0.0068	46128
154.00	LLPX310R	8	27.555	1.4071	0.0066	36902
144.00	(2) APX16PV-16PVL-X	8	24.611	1.3861	0.0056	18450
138.00	(2) RRUS-11	8	22.874	1.3678	0.0050	14192
134.00	7770.00	8	21.732	1.3524	0.0047	12308
124.00	844G65T6ZAXY	8	18.951	1.3003	0.0039	9717
114.00	(4) DB846G90A-XY	8	16.292	1.2309	0.0033	8577
51.50	GPS	8	3.632	0.6322	0.0010	3896

Compression Checks

Pole Design Data

Section No.	Elevation	Size	L	L _n	Kl/r	F _a	A	Actual P	Allow. P _a	Ratio P/P _a
	ft		ft	ft		ksi	in ²	K	K	
L1	164 - 131.5 (1)	TP53.42x47x0.3125	32.50	162.50	103.4	13.959	52.6760	-13.95	735.30	0.019
L2	131.5 - 119.29 (2)	TP56.15x53.42x0.375	12.21	162.50	100.9	14.665	64.7894	-15.59	950.11	0.016
L3	119.29 - 78.79 (3)	TP62.97x54.0585x0.4375	46.50	162.50	90.2	18.264	84.5934	-32.64	1545.03	0.021
L4	78.79 - 39.88 (4)	TP69.66x60.4813x0.5625	47.33	162.50	81.6	21.155	120.1620	-52.64	2542.07	0.021
L5	39.88 - 1.5 (5)	TP76x66.7412x0.5625	47.63	162.50	72.8	23.922	134.6840	-80.35	3221.92	0.025

RISATower Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11009.CO12 - CT2102 - Greenwich Hospital	Page	21 of 21
	Project	164' EEI Monopole - Greenwich, CT	Date	11:10:20 04/14/11
	Client	AT&T Mobility	Designed by	TJL

Pole Bending Design Data

Section No.	Elevation ft	Size	Actual	Actual	Allow.	Ratio	Actual	Actual	Allow.	Ratio
			M_x kip-ft	f_{bx} ksi	F_{bx} ksi	$\frac{f_{bx}}{F_{bx}}$	M_y kip-ft	f_{by} ksi	F_{by} ksi	$\frac{f_{by}}{F_{by}}$
L1	164 - 131.5 (1)	TP53.42x47x0.3125	373.97	-6.488	36.775	0.176	0.00	0.000	36.775	0.000
L2	131.5 - 119.29 (2)	TP56.15x53.42x0.375	503.31	-6.934	39.000	0.178	0.00	0.000	39.000	0.000
L3	119.29 - 78.79 (3)	TP62.97x54.0585x0.4375	1634.04	-15.410	39.000	0.395	0.00	0.000	39.000	0.000
L4	78.79 - 39.88 (4)	TP69.66x60.4813x0.5625	3011.95	-18.120	39.000	0.465	0.00	0.000	39.000	0.000
L5	39.88 - 1.5 (5)	TP76x66.7412x0.5625	5000.01	-23.922	39.000	0.613	0.00	0.000	39.000	0.000

Pole Interaction Design Data

Section No.	Elevation ft	Size	Ratio	Ratio	Ratio	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
			$\frac{P}{P_a}$	$\frac{f_{bx}}{F_{bx}}$	$\frac{f_{by}}{F_{by}}$			
L1	164 - 131.5 (1)	TP53.42x47x0.3125	0.019	0.176	0.000	0.195 ✓	1.333	H1-3 ✓
L2	131.5 - 119.29 (2)	TP56.15x53.42x0.375	0.016	0.178	0.000	0.194 ✓	1.333	H1-3 ✓
L3	119.29 - 78.79 (3)	TP62.97x54.0585x0.4375	0.021	0.395	0.000	0.416 ✓	1.333	H1-3 ✓
L4	78.79 - 39.88 (4)	TP69.66x60.4813x0.5625	0.021	0.465	0.000	0.485 ✓	1.333	H1-3 ✓
L5	39.88 - 1.5 (5)	TP76x66.7412x0.5625	0.025	0.613	0.000	0.638 ✓	1.333	H1-3 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF* P_{allow} K	% Capacity	Pass Fail
L1	164 - 131.5	Pole	TP53.42x47x0.3125	1	-13.95	980.15	14.7	Pass
L2	131.5 - 119.29	Pole	TP56.15x53.42x0.375	2	-15.59	1266.50	14.6	Pass
L3	119.29 - 78.79	Pole	TP62.97x54.0585x0.4375	3	-32.64	2059.52	31.2	Pass
L4	78.79 - 39.88	Pole	TP69.66x60.4813x0.5625	4	-52.64	3388.58	36.4	Pass
L5	39.88 - 1.5	Pole	TP76x66.7412x0.5625	5	-80.35	4294.82	47.9	Pass
Summary								
Pole (L5)							47.9	Pass
RATING =							47.9	Pass

Flange Bolt and Plate Analysis:

Input Data:

Tower Reactions:

Overturning Moment =	OM := 374ft-kips	(Input From RisaTower)
Shear Force =	Shear := 20.4-kips	(Input From RisaTower)
Axial Force =	Axial := 19.2-kips	(Input From RisaTower)

Flange Bolt Data:

Use ASTM A325

Number of Flange Bolts =	N := 12	(User Input)
Diameter of Bolt Circle =	$D_{bc} := 58.00\text{-in}$	(User Input)
Bolt Ultimate Strength =	$F_u := 120\text{-ksi}$	(User Input)
Bolt Yield Strength =	$F_y := 92\text{-ksi}$	(User Input)
Bolt Modulus =	E := 29000-ksi	(User Input)
Diameter of Flange Bolts =	D := 1.00-in	(User Input)

Flange Plate Data:

Use ASTM A36

Plate Yield Strength =	$F_{y_{bp}} := 36.00\text{-ksi}$	(User Input)
Flange Plate Thickness =	$t_{bp} := 1.00\text{-in}$	(User Input)
Flange Plate Diameter =	$D_{bp} := 61.00\text{-in}$	(User Input)
Outer Pole Diameter =	$D_{pole} := 53.42\text{-in}$	(User Input)

Geometric Layout Data:

Distance from Bolts to Centroid of Pole:

Radius of Bolt Circle =: $R_{bc} := \frac{D_{bc}}{2} = 29\text{-in}$

Distance to Bolts = $i := 1..N$

$$d_i := \begin{cases} \theta \leftarrow 2 \cdot \pi \cdot \left(\frac{i}{N}\right) \\ d \leftarrow R_{bc} \cdot \sin(\theta) \end{cases}$$

$d_1 = 14.50\text{-in}$	$d_7 = -14.50\text{-in}$
$d_2 = 25.11\text{-in}$	$d_8 = -25.11\text{-in}$
$d_3 = 29.00\text{-in}$	$d_9 = -29.00\text{-in}$
$d_4 = 25.11\text{-in}$	$d_{10} = -25.11\text{-in}$
$d_5 = 14.50\text{-in}$	$d_{11} = -14.50\text{-in}$
$d_6 = 0.00\text{-in}$	etc.

Critical Distances For Bending in Plate:

Outer Pole Radius = $R_{pole} := \frac{D_{pole}}{2} = 26.7\text{-in}$

Moment Arms of Bolts about Neutral Axis = $MA_i := \text{if}(d_i \geq R_{pole}, d_i - R_{pole}, 0\text{in})$

$MA_1 = 0.00\text{-in}$	$MA_7 = 0.00\text{-in}$
$MA_2 = 0.00\text{-in}$	$MA_8 = 0.00\text{-in}$
$MA_3 = 2.29\text{-in}$	$MA_9 = 0.00\text{-in}$
$MA_4 = 0.00\text{-in}$	$MA_{10} = 0.00\text{-in}$
$MA_5 = 0.00\text{-in}$	$MA_{11} = 0.00\text{-in}$
$MA_6 = 0.00\text{-in}$	etc

Effective Width of Plate for Bending = $B_{eff} := .8 \cdot \sqrt{\left(\frac{D_{bp}}{2}\right)^2 - \left(\frac{D_{pole}}{2}\right)^2} = 23.6\text{-in}$

Flange Bolt Analysis:

Calculated Flange Bolt Properties:

Polar Moment of Inertia = $I_p := \sum_i (d_i)^2 = 5.046 \times 10^3 \cdot \text{in}^2$

Gross Area of Bolt = $A_g := \frac{\pi}{4} \cdot D^2 = 0.785 \cdot \text{in}^2$

Check Flange Bolt Tension Force:

Maximum Tensile Force = $T_{\text{Max}} := OM \cdot \frac{R_{bc}}{I_p} - \frac{\text{Axial}}{N} = 24.2 \cdot \text{kips}$

Allowable Tensile Force = $T_{\text{ALL.Gross}} := 1.333 \cdot (0.33 \cdot A_g \cdot F_u) = 41.5 \cdot \text{kips}$ (1.333 increase allowed per TIA/EIA)

Bolt Tension % of Capacity = $\frac{T_{\text{Max}}}{T_{\text{ALL.Gross}}} = 58.4 \cdot \%$

Condition1 = $\text{Condition1} := \text{if} \left(\frac{T_{\text{Max}}}{T_{\text{ALL.Gross}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Condition1 = "OK"

Flange Plate Analysis:

Force from Bolts = $C_i := \frac{OM \cdot d_i}{I_p} + \frac{Axial}{N}$

$C_1 = 14.5 \cdot \text{kips}$

$C_7 = -11.3 \cdot \text{kips}$

$C_2 = 23.9 \cdot \text{kips}$

$C_8 = -20.7 \cdot \text{kips}$

$C_3 = 27.4 \cdot \text{kips}$

$C_9 = -24.2 \cdot \text{kips}$

$C_4 = 23.9 \cdot \text{kips}$

$C_{10} = -20.7 \cdot \text{kips}$

$C_5 = 14.5 \cdot \text{kips}$

$C_{11} = -11.3 \cdot \text{kips}$

$C_6 = 1.6 \cdot \text{kips}$

etc.

Maximum Bending Stress in Plate = $f_{bp} := \sum_i \frac{6 \cdot C_i \cdot M A_i}{(B_{eff} t_{bp})^2} = 16 \cdot \text{ksi}$

Allowable Bending Stress in Plate = $F_{bp} := 1.33 \cdot 0.75 \cdot F_y = 35.9 \cdot \text{ksi}$

Plate Bending Stress % of Capacity = $\frac{f_{bp}}{F_{bp}} = 44.5 \cdot \%$

Condition3 = $\text{Condition2} := \text{if} \left(\frac{f_{bp}}{F_{bp}} < 1.00, \text{"Ok"}, \text{"Overstressed"} \right)$

Condition2 = "Ok"

Anchor Bolt and Base Plate Analysis:

Input Data:

Tower Reactions:

Overturning Moment =	OM := 5000-ft-kips	(Input From RisaTower)
Shear Force =	Shear := 45-kips	(Input From RisaTower)
Axial Force =	Axial := 80-kips	(Input From RisaTower)

Anchor Bolt Data:

Use ASTM A615 Grade 75

Number of Anchor Bolts =	N := 30	(User Input)
Diameter of Bolt Circle =	$D_{bc} := 86.00$ -in	(User Input)
Bolt "Column" Distance =	l := 3.0-in	(User Input)
Bolt Ultimate Strength =	$F_u := 100$ -ksi	(User Input)
Bolt Yield Strength =	$F_y := 75$ -ksi	(User Input)
Bolt Modulus =	E := 29000-ksi	(User Input)
Diameter of Anchor Bolts =	D := 2.25-in	(User Input)
Threads per Inch =	n := 4.5	(User Input)

Base Plate Data:

Use ASTM A572 GR 60

Plate Yield Strength =	$F_{y_{bp}} := 60$ -ksi	(User Input)
Base Plate Thickness =	$t_{bp} := 3.0$ -in	(User Input)
Base Plate Diameter =	$D_{bp} := 92.00$ -in	(User Input)
Outer Pole Diameter =	$D_{pole} := 76.00$ -in	(User Input)

Geometric Layout Data:

Distance from Bolts to Centroid of Pole:

Radius of Bolt Circle =: $R_{bc} := \frac{D_{bc}}{2} = 43\text{-in}$

Distance to Bolts = $i := 1..N$

$$d_i := \begin{cases} \theta \leftarrow 2 \cdot \pi \cdot \left(\frac{i}{N}\right) \\ d \leftarrow R_{bc} \cdot \sin(\theta) \end{cases}$$

$d_1 = 8.94\text{-in}$	$d_7 = 42.76\text{-in}$
$d_2 = 17.49\text{-in}$	$d_8 = 42.76\text{-in}$
$d_3 = 25.27\text{-in}$	$d_9 = 40.90\text{-in}$
$d_4 = 31.96\text{-in}$	$d_{10} = 37.24\text{-in}$
$d_5 = 37.24\text{-in}$	$d_{11} = 31.96\text{-in}$
$d_6 = 40.90\text{-in}$	etc.

Critical Distances For Bending in Plate:

Outer Pole Radius = $R_{pole} := \frac{D_{pole}}{2} = 38\text{-in}$

Moment Arms of Bolts about Neutral Axis = $MA_i := \text{if}(d_i \geq R_{pole}, d_i - R_{pole}, 0\text{in})$

$MA_1 = 0.00\text{-in}$	$MA_7 = 4.76\text{-in}$
$MA_2 = 0.00\text{-in}$	$MA_8 = 4.76\text{-in}$
$MA_3 = 0.00\text{-in}$	$MA_9 = 2.90\text{-in}$
$MA_4 = 0.00\text{-in}$	$MA_{10} = 0.00\text{-in}$
$MA_5 = 0.00\text{-in}$	$MA_{11} = 0.00\text{-in}$
$MA_6 = 2.90\text{-in}$	etc

Effective Width of Baseplate for Bending = $B_{eff} := .82 \cdot \sqrt{\left(\frac{D_{bp}}{2}\right)^2 - \left(\frac{D_{pole}}{2}\right)^2} = 41.5\text{-in}$

Anchor Bolt Analysis:

Calculated Anchor Bolt Properties:

Polar Moment of Inertia =

$$I_p := \sum_i (d_i)^2 = 2.773 \times 10^4 \cdot \text{in}^2$$

Gross Area of Bolt =

$$A_g := \frac{\pi}{4} \cdot D^2 = 3.976 \cdot \text{in}^2$$

Net Area of Bolt =

$$A_n := \frac{\pi}{4} \cdot \left(D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 = 3.248 \cdot \text{in}^2$$

Net Diameter =

$$D_n := \frac{2 \cdot \sqrt{A_n}}{\sqrt{\pi}} = 2.033 \cdot \text{in}$$

Radius of Gyration of Bolt =

$$r := \frac{D_n}{4} = 0.508 \cdot \text{in}$$

Section Modulus of Bolt =

$$S_x := \frac{\pi \cdot D_n^3}{32} = 0.826 \cdot \text{in}^3$$

Check Anchor Bolt Tension Force:

Maximum Tensile Force =

$$T_{\text{Max}} := OM \cdot \frac{R_{bc}}{I_p} - \frac{\text{Axial}}{N} = 90.4 \cdot \text{kips}$$

Allowable Tensile Force =

$$T_{\text{ALL.Gross}} := 1.333 \cdot (0.33 \cdot A_g \cdot F_u) = 174.9 \cdot \text{kips} \quad (1.333 \text{ increase allowed per TIA/EIA})$$

$$T_{\text{ALL.Net}} := 1.333 \cdot (0.60 \cdot A_n \cdot F_y) = 194.812 \cdot \text{kips} \quad (1.333 \text{ increase allowed per TIA/EIA})$$

Bolt Tension % of Capacity =

$$\frac{T_{\text{Max}}}{T_{\text{ALL.Net}}} = 46.4\% \quad \text{Bolts are "upset bolts". Use net area per AISC}$$

Condition1 =

$$\text{Condition1} := \text{if} \left(\frac{T_{\text{Max}}}{T_{\text{ALL.Net}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition1 = "OK"

Check Anchor Bolt Bending Stress:

Maximum Bending Moment =

$$M_x := \left(\frac{\text{Shear}}{N} \right) \cdot l = 0.375 \cdot \text{ft} \cdot \text{kips}$$

Maximum Bending Stress =

$$f_{bx} := \frac{M_x}{S_x} = 5.5 \cdot \text{ksi}$$

Allowable Bending Stress =

$$F_{Dx} := 1.333 \cdot 0.6 \cdot F_y = 60 \cdot \text{ksi} \quad (1.333 \text{ increase allowed per TIA/EIA})$$

Check Combined Stress Requirement:

Per ASCE Manual 72: "If the clearance between the base plate and concrete does not exceed two times the bolt diameter a bending stress analysis of the bolts is NOT normally required."

$$l := \begin{cases} l & \text{if } l > 2 \cdot D_n \\ 0 & \text{otherwise} \end{cases} = 0 \text{ in}$$

$$f_{bx} := \begin{cases} f_{bx} & \text{if } l > 2 \cdot D_n \\ 0 & \text{otherwise} \end{cases} = 0 \text{ ksi}$$

Check Anchor Bolt Compression/Combined Stress:

Maximum Compressive Force =

$$C_{Max} := OM \cdot \frac{R_{bc}}{I_p} + \frac{Axial}{N} = 95.7 \text{ kips}$$

Maximum Compressive Stress =

$$f_a := \frac{C_{Max}}{A_n} = 29.5 \text{ ksi}$$

$$K := 0.65$$

$$C_c := \sqrt{\frac{2 \cdot \pi^2 \cdot E}{F_y}} = 87.364$$

$$F_a := \begin{cases} \frac{\left[1 - \frac{\left(\frac{K \cdot l}{r}\right)^2}{2 \cdot C_c^2} \right] \cdot F_y}{\frac{5}{3} + \frac{3 \cdot \left(\frac{K \cdot l}{r}\right)}{8 \cdot C_c} - \frac{\left(\frac{K \cdot l}{r}\right)^3}{8 \cdot C_c^3}} & \text{if } \frac{K \cdot l}{r} \leq C_c \\ \frac{12 \cdot \pi^2 \cdot E}{23 \cdot \left(\frac{K \cdot l}{r}\right)^2} & \text{if } \frac{K \cdot l}{r} > C_c \end{cases} = 45 \text{ ksi}$$

Allowable Compressive Stress =

$$F_a := 1.333 \cdot F_a = 60 \text{ ksi} \quad (1.333 \text{ increase allowed per TIA/EIA})$$

Combined Stress % of Capacity =

$$\left(\frac{f_a}{F_a} + \frac{f_{bx}}{F_{bx}} \right) = 49.1 \%$$

Condition 2 =

$$\text{Condition2} := \text{if} \left(\frac{f_a}{F_a} + \frac{f_{bx}}{F_{bx}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition2 = "OK"

Base Plate Analysis:

Force from Bolts =

$$C_i := \frac{OM \cdot d_i}{I_p} + \frac{Axial}{N}$$

$C_1 = 22.0 \cdot \text{kips}$

$C_7 = 95.2 \cdot \text{kips}$

$C_2 = 40.5 \cdot \text{kips}$

$C_8 = 95.2 \cdot \text{kips}$

$C_3 = 57.3 \cdot \text{kips}$

$C_9 = 91.1 \cdot \text{kips}$

$C_4 = 71.8 \cdot \text{kips}$

$C_{10} = 83.2 \cdot \text{kips}$

$C_5 = 83.2 \cdot \text{kips}$

$C_{11} = 71.8 \cdot \text{kips}$

$C_6 = 91.1 \cdot \text{kips}$

etc.

Maximum Bending Stress in Plate =

$$f_{bp} := \sum_i \frac{6 \cdot C_i \cdot MA_i}{(B_{eff} t_{bp})^2} = 23.1 \cdot \text{ksi}$$

Allowable Bending Stress in Plate =

$F_{bp} := 1.33 \cdot 0.75 \cdot F_y = 59.9 \cdot \text{ksi}$

Plate Bending Stress % of Capacity =

$\frac{f_{bp}}{F_{bp}} = 38.5 \cdot \%$

Condition3 =

Condition3 := $\left(\text{if} \left(\frac{f_{bp}}{F_{bp}} < 1.00, \text{"Ok"}, \text{"Overstressed"} \right) \right)$

Condition3 = "Ok"

Caisson Foundation:

Input Data:

Shear Force =	S := 44.5k	USER INPUT-FROM RISATower
Overturing Moment =	M := 5000ft-k	USER INPUT-FROM RISATower
Applied Axial Load =	A1 := 80k	USER INPUT-FROM RISATower
Bending Moment =	Mu := 5238ft-k	USER INPUT-FROM LPILE
Moment Capacity =	Mn := 12301ft-k	USER INPUT-FROM LPILE
Foundation Diameter =	d := 9.0ft	USER INPUT
Overall Length of Caisson =	L _c := 28.0ft	USER INPUT
Depth From Top of Caisson to Grade =	L _{pag} := 1.0ft	USER INPUT
Number of Rebar =	n := 33	USER INPUT
Area of Rebar =	Ar := 1.560in ²	USER INPUT
Rebar Yield Strength =	fy := 60ksi	USER INPUT
Concrete Comp Strength =	fc := 3ksi	USER INPUT

Check Foundation Depth:

Depth of Caisson Below Ground Level = LD := L_c - L_{pag} = 27ft (TIA/EIA-222-F 7.2.5)

Depth Required = LD1 := 2.0ft + $\left(\frac{S \cdot \text{ft}^2}{3k \cdot d}\right) + 2\text{ft} \cdot 5 \left(\frac{M \cdot \text{ft}}{3 \cdot kd} + \frac{S \cdot \text{ft}}{2k} + \frac{S^2 \cdot \text{ft}^3}{18k^2 \cdot d^2}\right)^{.5} = 32.55\text{ft}$

DepthCheck := if(LD1 ≤ LD, "OK", "NO GOOD")

DepthCheck = "NO GOOD" Note: Result not applicable. Actual soil is better than normal soil as defined in TIA/EIA 222 F. Refer to L-Pile analysis.

Check Moment Capacity:

Factor of Safety = FS := $\frac{Mn}{Mu} = 2.3$

Factor of Safety Required = FS_{reqd} := 1.3

FOSCheck := if(FS ≥ FS_{reqd}, "OK", "NO GOOD")

FOSCheck = "OK"

Check Axial Capacity:

Concrete Weight = A2 := $.150 \frac{k}{\text{ft}^3} \cdot LD \cdot \pi \frac{d^2}{4} = 257.6 \text{ kips}$

Total Axial Load = AT := A1 + A2 = 337.6 kips

Area of Concrete = Ag := $\pi \frac{d^2}{4} = 63.62 \text{ ft}^2$

Axial Capacity = Po := n · Ar · fy + (Ag - n · Ar) · 0.85 · fc = 26317.8 kips

AxialCheck := if(AT ≤ Po, "OK", "NO GOOD")

AxialCheck = "OK"

Greenwich Hospital Caisson Analysis.lpo

LPILE Plus for Windows, Version 5.0 (5.0.39)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

(c) 1985-2007 by Ensoft, Inc.
All Rights Reserved

This program is licensed to:

Staff
Natcomm, Inc.

Path to file locations: J:\Jobs\1100900.WI\CO12 - CT2102 - Greenwich
Hospital - 5 Perryridge Road Greenwich, CT\Calcs\Foundation\
Name of input data file: Greenwich Hospital Caisson Analysis.lpd
Name of output file: Greenwich Hospital Caisson Analysis.lpo
Name of plot output file: Greenwich Hospital Caisson Analysis.lpp
Name of runtime file: Greenwich Hospital Caisson Analysis.lpr

Time and Date of Analysis

Date: April 14, 2011 Time: 10:15:41

Problem Title

11009.CO12 - CT2102: Greenwich Hospital

Program Options

Units Used in Computations - US Customary Units: Inches, Pounds

Basic Program Options:

Analysis Type 3:

- Computation of Nonlinear Bending Stiffness and Ultimate Bending Moment Capacity with Pile Response Computed Using Nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis does not use p-y multipliers (individual pile or shaft action only)
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- Analysis includes computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No additional p-y curves to be computed at user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100

Greenwich Hospital Caisson Analysis.lpo

- Deflection tolerance for convergence = 1.0000E-04 in
- Maximum allowable deflection = 1.0000E+02 in

Printing Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (spacing of output points) = 8

 Pile Structural Properties and Geometry

Pile Length = 336.00 in
 Depth of ground surface below top of pile = 12.00 in
 Slope angle of ground surface = .00 deg.

Structural properties of pile defined using 2 points

Point	Depth X in	Pile Diameter in	Moment of Inertia in**4	Pile Area Sq.in	Modulus of Elasticity lbs/Sq.in
1	0.0000	108.00000	6678285.	9160.9000	3600000.
2	336.0000	108.00000	6678285.	9160.9000	3600000.

Please note that because this analysis makes computations of ultimate moment capacity and pile response using nonlinear bending stiffness that the above values of moment of inertia and modulus of are not used for any computations other than total stress due to combined axial loading and bending.

 Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 12.000 in
 Distance from top of pile to bottom of layer = 48.000 in
 p-y subgrade modulus k for top of soil layer = 20.000 lbs/in**3
 p-y subgrade modulus k for bottom of layer = 20.000 lbs/in**3

Layer 2 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 48.000 in
 Distance from top of pile to bottom of layer = 72.000 in
 p-y subgrade modulus k for top of soil layer = 90.000 lbs/in**3
 p-y subgrade modulus k for bottom of layer = 90.000 lbs/in**3

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 72.000 in
 Distance from top of pile to bottom of layer = 132.000 in
 p-y subgrade modulus k for top of soil layer = 150.000 lbs/in**3
 p-y subgrade modulus k for bottom of layer = 150.000 lbs/in**3

Layer 4 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 132.000 in
 Distance from top of pile to bottom of layer = 360.000 in
 p-y subgrade modulus k for top of soil layer = 250.000 lbs/in**3
 p-y subgrade modulus k for bottom of layer = 250.000 lbs/in**3

 Effective Unit weight of Soil vs. Depth

Effective unit weight of soil with depth defined using 8 points

Point No.	Depth X in	Eff. Unit weight lbs/in**3
1	12.00	.05800
2	48.00	.05800
3	48.00	.06900
4	72.00	.06900
5	72.00	.06900
6	132.00	.06900
7	132.00	.07500
8	360.00	.07500

 Shear Strength of Soils

Shear strength parameters with depth defined using 8 points

Point No.	Depth X in	Cohesion c lbs/in**2	Angle of Friction Deg.	E50 or k _{rm}	RQD %
1	12.000	.00000	20.00	-----	-----
2	48.000	.00000	20.00	-----	-----
3	48.000	.00000	30.00	-----	-----
4	72.000	.00000	30.00	-----	-----
5	72.000	.00000	35.00	-----	-----
6	132.000	.00000	35.00	-----	-----
7	132.000	.00000	42.00	-----	-----
8	360.000	.00000	42.00	-----	-----

Notes:

- (1) Cohesion = uniaxial compressive strength for rock materials.
- (2) Values of E50 are reported for clay strata.
- (3) Default values will be generated for E50 when input values are 0.
- (4) RQD and k_{rm} are reported only for weak rock strata.

 Loading Type

Static loading criteria was used for computation of p-y curves.

 Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load Case Number 1

Greenwich Hospital Caisson Analysis.lpo

Pile-head boundary conditions are Shear and Moment (BC Type 1)
 Shear force at pile head = 44540.000 lbs
 Bending moment at pile head = 60003818.000 in-lbs
 Axial load at pile head = 80390.000 lbs

Non-zero moment at pile head for this load case indicates the pile-head may rotate under the applied pile-head loading, but is not a free-head (zero moment) condition.

 Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Number of sections = 1

Pile Section No. 1

The sectional shape is a circular drilled shaft (bored pile).

Outside Diameter = 108.0000 in

Material Properties:

Compressive Strength of Concrete = 3.000 kip/in**2
 Yield Stress of Reinforcement = 60. kip/in**2
 Modulus of Elasticity of Reinforcement = 29000. kip/in**2
 Number of Reinforcing Bars = 33
 Area of Single Bar = 1.56000 in**2
 Number of Rows of Reinforcing Bars = 33
 Area of Steel = 51.480 in**2
 Area of Shaft = 9160.884 in**2
 Percentage of Steel Reinforcement = .562 percent
 Cover Thickness (edge to bar center) = 4.000 in

Unfactored Axial Squash Load Capacity = 26317.78 kip

Distribution and Area of Steel Reinforcement

Row Number	Area of Reinforcement in**2	Distance to Centroidal Axis in
1	1.560	49.943
2	1.560	49.491
3	1.560	48.591
4	1.560	47.250
5	1.560	45.482
6	1.560	43.301
7	1.560	40.729
8	1.560	37.787
9	1.560	34.504
10	1.560	30.908
11	1.560	27.032
12	1.560	22.911
13	1.560	18.583
14	1.560	14.087
15	1.560	9.463
16	1.560	4.753
17	1.560	0.000
18	1.560	-4.753
19	1.560	-9.463

Greenwich Hospital Caisson Analysis.lpo

20	1.560	-14.087
21	1.560	-18.583
22	1.560	-22.911
23	1.560	-27.032
24	1.560	-30.908
25	1.560	-34.504
26	1.560	-37.787
27	1.560	-40.729
28	1.560	-43.301
29	1.560	-45.482
30	1.560	-47.250
31	1.560	-48.591
32	1.560	-49.491
33	1.560	-49.943

Axial Thrust Force = 80390.00 lbs

Bending Concrete Stress	Bending Max. Steel Stress	Bending Steel Stiffness	Bending Curvature	Maximum Strain	Neutral Axis Position	Max. psi
in-lbs	psi	lb-in ²	rad/in	in/in	inches	psi
11414083.	2.282817E+13	804.36668	5.000000E-07	.00002977	59.53019732	
91.48943069	2.271332E+13	1532.23118	.00000100	.00005689	56.89219111	
173.29339	2.259280E+13	2259.00164	.00000150	.00008398	55.98770517	
253.60051	2.247503E+13	2987.97456	.00000200	.00011115	55.57343584	
332.75050	2.235550E+13	3715.29335	.00000250	.00013826	55.30205852	
410.34789	1.862958E+13	6592.01910	.00000300	.00008452	28.17303246	
251.17167	1.596822E+13	7744.67465	.00000350	.00009674	27.64115363	
286.24720	1.397219E+13	8896.91512	.00000400	.00010898	27.24582285	
321.09522	1.241972E+13	10041.10960	.00000450	.00012150	26.99999839	
356.48342	1.117775E+13	11192.92676	.00000500	.00013375	26.75076860	
390.82676	1.016159E+13	12345.73409	.00000550	.00014597	26.54064542	
424.80096	9.314792E+12	13498.08861	.00000600	.00015821	26.36814505	
458.55028	8.598270E+12	14649.98885	.00000650	.00017046	26.22459322	
492.07379	7.984108E+12	15801.43069	.00000700	.00018273	26.10380691	
525.37082	7.451834E+12	16952.41161	.00000750	.00019501	26.00124460	
558.44051	6.986094E+12	18102.92742	.00000800	.00020731	25.91350740	
591.28216	6.575148E+12	19252.97586	.00000850	.00021962	25.83798820	
623.89489	6.209862E+12	20402.55303	.00000900	.00023195	25.77266568	
656.27793	5.883027E+12	21551.65519	.00000950	.00024430	25.71594340	
688.43052	5.588875E+12	22700.28066	.00001000	.00025667	25.66653711	
720.35166						

Greenwich Hospiatl Caisson Analysis.lpo

55888754.	5.322738E+12	.00001050	.00026905	25.62342006
752.04073	23848.42383			
55888754.	5.080796E+12	.00001100	.00028144	25.58574253
783.49679	24996.08219			
55888754.	4.859892E+12	.00001150	.00029386	25.55280608
814.71902	26143.25205			
55888754.	4.657396E+12	.00001200	.00030629	25.52402490
845.70644	27289.93104			
55888754.	4.471100E+12	.00001250	.00031874	25.49891621
876.45838	28436.11340			
55888754.	4.299135E+12	.00001300	.00033120	25.47706157
906.97382	29581.79713			
55888754.	4.139908E+12	.00001350	.00034368	25.45811015
937.25191	30726.97804			
56827996.	4.059143E+12	.00001400	.00035618	25.44176263
967.29184	31871.65136			
58739118.	4.050974E+12	.00001450	.00036870	25.42775506
997.09257	33015.81480			
60648045.	4.043203E+12	.00001500	.00038124	25.41586214
1026.65319	34159.46460			
62554782.	4.035792E+12	.00001550	.00039379	25.40589398
1055.97300	35302.59410			
64459300.	4.028706E+12	.00001600	.00040636	25.39767355
1085.05085	36445.20174			
66361583.	4.021914E+12	.00001650	.00041895	25.39104956
1113.88578	37587.28387			
68261629.	4.015390E+12	.00001700	.00043156	25.38589329
1142.47699	38728.83452			
70159409.	4.009109E+12	.00001750	.00044419	25.38208240
1170.82330	39869.85191			
72054923.	4.003051E+12	.00001800	.00045683	25.37951714
1198.92394	41010.32961			
73948155.	3.997198E+12	.00001850	.00046949	25.37810415
1226.77788	42150.26350			
75839089.	3.991531E+12	.00001900	.00048218	25.37775975
1254.38412	43289.64957			
77727700.	3.986036E+12	.00001950	.00049488	25.37840670
1281.74151	44428.48502			
81497929.	3.975509E+12	.00002050	.00052034	25.38242358
1335.70607	46704.48084			
85258717.	3.965522E+12	.00002150	.00054588	25.38969451
1388.66321	48978.21477			
89009950.	3.955998E+12	.00002250	.00057150	25.39984614
1440.60455	51249.64734			
92751483.	3.946872E+12	.00002350	.00059720	25.41256303
1491.52113	53518.74288			
96483199.	3.938090E+12	.00002450	.00062298	25.42759091
1541.40421	55785.45889			
1.002050E+08	3.929606E+12	.00002550	.00064884	25.44471091
1590.24448	58049.75615			
1.038781E+08	3.919929E+12	.00002650	.00067470	25.46047908
1637.86972	60000.00000			
1.067779E+08	3.882832E+12	.00002750	.00069891	25.41483861
1681.23936	60000.00000			
1.092085E+08	3.831878E+12	.00002850	.00072209	25.33656424
1721.72044	60000.00000			
1.113281E+08	3.773835E+12	.00002950	.00074459	25.24019784
1760.02623	60000.00000			
1.135610E+08	3.723312E+12	.00003050	.00076860	25.20000011
1800.02423	60000.00000			
1.149472E+08	3.649118E+12	.00003150	.00079050	25.09528452
1835.46534	60000.00000			
1.165172E+08	3.585145E+12	.00003250	.00081144	24.96743006
1868.48416	60000.00000			
1.178852E+08	3.518962E+12	.00003350	.00083180	24.82998723
1899.80478	60000.00000			

Greenwich Hospiatl Caisson Analysis.lpo

1.192124E+08	3.455433E+12	.00003450	.00085209	24.69828647
1930.26945	60000.00000			
1.203683E+08	3.390656E+12	.00003550	.00087186	24.55935019
1959.21478	60000.00000			
1.215207E+08	3.329333E+12	.00003650	.00089166	24.42915577
1987.52883	60000.00000			
1.225052E+08	3.266804E+12	.00003750	.00091092	24.29118508
2014.35115	60000.00000			
1.234781E+08	3.207225E+12	.00003850	.00093018	24.16059154
2040.52960	60000.00000			
1.243960E+08	3.149266E+12	.00003950	.00094928	24.03246027
2065.82727	60000.00000			
1.252097E+08	3.091599E+12	.00004050	.00096802	23.90182167
2090.00229	60000.00000			
1.260206E+08	3.036642E+12	.00004150	.00098680	23.77834457
2113.60502	60000.00000			
1.268033E+08	2.983607E+12	.00004250	.00100551	23.65899378
2136.49538	60000.00000			
1.274751E+08	2.930463E+12	.00004350	.00102379	23.53534931
2158.24408	60000.00000			
1.281444E+08	2.879650E+12	.00004450	.00104210	23.41802949
2179.44628	60000.00000			
1.288288E+08	2.831402E+12	.00004550	.00106470	23.39999861
2205.03779	60000.00000			
1.295259E+08	2.785504E+12	.00004650	.00108295	23.28927058
2224.84393	60000.00000			
1.300597E+08	2.738099E+12	.00004750	.00110023	23.16278082
2243.00533	60000.00000			
1.305913E+08	2.692605E+12	.00004850	.00111754	23.04215866
2260.67839	60000.00000			
1.311208E+08	2.648906E+12	.00004950	.00113489	22.92705327
2277.86031	60000.00000			
1.316482E+08	2.606894E+12	.00005050	.00115227	22.81714278
2294.54833	60000.00000			
1.321100E+08	2.565244E+12	.00005150	.00116930	22.70487303
2310.37895	60000.00000			
1.325351E+08	2.524478E+12	.00005250	.00118616	22.59353667
2325.53926	60000.00000			
1.329582E+08	2.485199E+12	.00005350	.00120305	22.48692530
2340.23138	60000.00000			
1.333793E+08	2.447326E+12	.00005450	.00121997	22.38478464
2354.45280	60000.00000			
1.337984E+08	2.410783E+12	.00005550	.00123692	22.28687328
2368.20068	60000.00000			
1.342156E+08	2.375497E+12	.00005650	.00125390	22.19297558
2381.47257	60000.00000			
1.345566E+08	2.340115E+12	.00005750	.00127042	22.09423381
2393.87830	60000.00000			
1.348894E+08	2.305801E+12	.00005850	.00128692	21.99862379
2405.79911	60000.00000			
1.352203E+08	2.272611E+12	.00005950	.00130345	21.90671843
2417.26754	60000.00000			
1.358768E+08	2.209379E+12	.00006150	.00133660	21.73330718
2438.83695	60000.00000			
1.367504E+08	2.153550E+12	.00006350	.00137160	21.60000032
2459.59723	60000.00000			
1.371781E+08	2.094323E+12	.00006550	.00141000	21.52674383
2479.99903	60000.00000			
1.376597E+08	2.039403E+12	.00006750	.00144110	21.34970194
2494.45465	60000.00000			
1.381353E+08	1.987558E+12	.00006950	.00147232	21.18444675
2507.28554	60000.00000			
1.386048E+08	1.938529E+12	.00007150	.00150365	21.03001910
2518.47338	60000.00000			
1.390440E+08	1.891755E+12	.00007350	.00153484	20.88210922
2527.92497	60000.00000			

Greenwich Hospiatl Caisson Analysis.lpo

1.393978E+08	1.846329E+12	.00007550	.00156530	20.73245484
2535.52568	60000.00000			
1.397461E+08	1.803176E+12	.00007750	.00159587	20.59192854
2541.54804	60000.00000			
1.400887E+08	1.762122E+12	.00007950	.00162656	20.45985764
2545.97395	60000.00000			
1.404256E+08	1.723013E+12	.00008150	.00165735	20.33564347
2548.78499	60000.00000			
1.407566E+08	1.685708E+12	.00008350	.00168826	20.21874207
2549.96222	60000.00000			
1.410490E+08	1.649696E+12	.00008550	.00171896	20.10474068
2546.02690	60000.00000			
1.412857E+08	1.614693E+12	.00008750	.00174910	19.98977047
2541.05419	60000.00000			
1.415199E+08	1.581228E+12	.00008950	.00177937	19.88117641
2543.51902	60000.00000			
1.415199E+08	1.546665E+12	.00009150	.00181170	19.79999882
2547.09008	60000.00000			
1.417490E+08	1.516032E+12	.00009350	.00185130	19.79999882
2549.59126	60000.00000			
1.423302E+08	1.490369E+12	.00009550	.00188497	19.73793358
2548.63742	60000.00000			
1.425367E+08	1.461914E+12	.00009750	.00191439	19.63478547
2544.42434	60000.00000			
1.427417E+08	1.434590E+12	.00009950	.00194390	19.53667778
2540.19566	60000.00000			
1.429352E+08	1.408228E+12	.00010150	.00197330	19.44139928
2539.72329	60000.00000			
1.430795E+08	1.382411E+12	.00010350	.00200187	19.34169191
2543.26246	60000.00000			
1.432226E+08	1.357561E+12	.00010550	.00203051	19.24655503
2546.06762	60000.00000			
1.433645E+08	1.333624E+12	.00010750	.00205924	19.15574080
2548.12928	60000.00000			
1.435052E+08	1.310550E+12	.00010950	.00208806	19.06903034
2549.43786	60000.00000			
1.436445E+08	1.288292E+12	.00011150	.00211696	18.98620802
2549.98339	60000.00000			
1.437806E+08	1.266789E+12	.00011350	.00214605	18.90797228
2547.20221	60000.00000			
1.439153E+08	1.246020E+12	.00011550	.00217524	18.83321911
2543.66216	60000.00000			
1.440492E+08	1.225951E+12	.00011750	.00220448	18.76153010
2540.11140	60000.00000			
1.441825E+08	1.206548E+12	.00011950	.00223378	18.69275719
2536.54982	60000.00000			
1.443149E+08	1.187777E+12	.00012150	.00226315	18.62675875
2535.60881	60000.00000			
1.444347E+08	1.169512E+12	.00012350	.00229228	18.56097597
2539.25390	60000.00000			
1.445264E+08	1.151605E+12	.00012550	.00232077	18.49218696
2542.25689	60000.00000			
1.446174E+08	1.134254E+12	.00012750	.00234932	18.42601150
2544.77715	60000.00000			
1.447078E+08	1.117435E+12	.00012950	.00237792	18.36233371
2546.80938	60000.00000			
1.447976E+08	1.101122E+12	.00013150	.00240659	18.30104738
2548.34816	60000.00000			
1.448867E+08	1.085293E+12	.00013350	.00243531	18.24204630
2549.38790	60000.00000			
1.449751E+08	1.069927E+12	.00013550	.00246410	18.18523711
2549.92298	60000.00000			
1.450620E+08	1.054996E+12	.00013750	.00249301	18.13098353
2548.70099	60000.00000			
1.451472E+08	1.040482E+12	.00013950	.00252204	18.07914072
2545.81908	60000.00000			

Greenwich Hospiatl Caisson Analysis.lpo

1.455127E+08	1.014026E+12	.00014350	.00258300	18.00000054
2539.54654	60000.00000			
1.466286E+08	9.940921E+11	.00014750	.00265500	18.00000054
2531.33751	60000.00000			
1.476109E+08	9.743296E+11	.00015150	.00272700	18.00000054
2536.11274	60000.00000			
1.476109E+08	9.492664E+11	.00015550	.00279117	17.94963831
2542.51490	60000.00000			
1.476109E+08	9.254604E+11	.00015950	.00284857	17.85938090
2546.17322	60000.00000			
1.476109E+08	9.028191E+11	.00016350	.00290515	17.76850551
2548.55472	60000.00000			
1.476109E+08	8.812593E+11	.00016750	.00296191	17.68306965
2549.80428	60000.00000			
1.476109E+08	8.607051E+11	.00017150	.00301998	17.60919517
2547.98766	60000.00000			
1.476109E+08	8.410879E+11	.00017550	.00307897	17.54397887
2543.32336	60000.00000			
1.476109E+08	8.223450E+11	.00017950	.00313808	17.48233205
2538.63819	60000.00000			
1.476109E+08	8.044192E+11	.00018350	.00319731	17.42403585
2533.93168	60000.00000			
1.476109E+08	7.872583E+11	.00018750	.00325667	17.36888748
2529.20345	60000.00000			
1.476109E+08	7.708143E+11	.00019150	.00331615	17.31671315
2524.45271	60000.00000			
1.476109E+08	7.550431E+11	.00019550	.00337576	17.26733905
2519.67915	60000.00000			
1.476109E+08	7.399044E+11	.00019950	.00343645	17.22532600
2525.73942	60000.00000			
1.476109E+08	7.253608E+11	.00020350	.00349791	17.18876213
2531.99010	60000.00000			
1.476109E+08	7.113780E+11	.00020750	.00355955	17.15447062
2537.35110	60000.00000			
1.476109E+08	6.979240E+11	.00021150	.00362069	17.11911696
2541.67787	60000.00000			
1.476109E+08	6.849695E+11	.00021550	.00368033	17.07809526
2544.89240	60000.00000			
1.476109E+08	6.724872E+11	.00021950	.00374012	17.03927833
2547.34202	60000.00000			
1.476109E+08	6.604516E+11	.00022350	.00380007	17.00256640
2549.00865	60000.00000			

Unfactored (Nominal) Moment Capacity at Concrete Strain of 0.003 =
147610.93014 in-kip

Computed Values of Load Distribution and Deflection
for Lateral Loading for Load Case Number 1

Pile-head boundary conditions are Shear and Moment (BC Type 1)
Specified shear force at pile head = 44540.000 lbs
Specified moment at pile head = 60003818.000 in-lbs
Specified axial load at pile head = 80390.000 lbs

Non-zero moment for this load case indicates the pile-head may rotate under the applied pile-head loading, but is not a free-head (zero moment) condition.

Depth	Deflect.	Moment	Shear	Slope	Total	Flx. Rig.	Soil Res.
Es*h	y	M	V	S	Stress	EI	p
X							
F/L							

in	in	Greenwich lbs-in	Hospiatl lbs	Caisson Rad.	Analysis.lpo lbs/in**2	lbs-in**2	lbs/in
0.000	.593914	6.00E+07	44540.	-.004061	493.961	4.05E+12	0.000
0.000							
26.880	.490141	6.12E+07	43401.	-.003658	503.663	4.04E+12	-145.866
999.936							
53.760	.397309	6.23E+07	34744.	-.003247	512.496	4.04E+12	-788.794
6670.753							
80.640	.315619	6.29E+07	1641.888	-.002830	517.002	4.03E+12	-1769.440
18837.							
107.520	.245165	6.21E+07	-59495.	-.002413	511.261	4.04E+12	-2747.204
37651.							
134.400	.185802	5.95E+07	-1.36E+05	-.002007	490.182	4.05E+12	-3522.375
63698.							
161.280	.136438	5.46E+07	-2.32E+05	-.001742	450.186	2.24E+13	-3503.413
86277.							
188.160	.090470	4.71E+07	-3.20E+05	-.001680	389.994	2.24E+13	-2931.007
1.09E+05							
215.040	.046013	3.76E+07	-3.84E+05	-.001629	312.943	2.25E+13	-1799.936
1.31E+05							
241.920	.002759	2.68E+07	-4.11E+05	-.001591	225.636	2.27E+13	-126.480
1.54E+05							
268.800	-.039640	1.60E+07	-3.86E+05	-.001566	137.847	2.28E+13	2083.361
1.77E+05							
295.680	-.081528	6.64E+06	-2.95E+05	-.001553	62.487	2.28E+13	4832.764
1.99E+05							
322.560	-.123196	8.47E+05	-1.22E+05	-.001549	15.624	2.28E+13	8130.664
2.22E+05							

Please note that because this analysis makes computations of ultimate moment capacity and pile response using nonlinear bending stiffness that the above values of total stress due to combined axial stress and bending may not be representative of actual conditions.

Output Verification:

Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = .59391430 in
 Computed slope at pile head = -.00406135
 Maximum bending moment = 62853315. lbs-in
 Maximum shear force = -411502.03834 lbs
 Depth of maximum bending moment = 80.64000000 in
 Depth of maximum shear force = 245.28000 in
 Number of iterations = 66
 Number of zero deflection points = 1

Summary of Pile Response(s)

Definition of Symbols for Pile-Head Loading Conditions:

Type 1 = Shear and Moment, y = pile-head displacement in
 Type 2 = Shear and Slope, M = Pile-head Moment lbs-in
 Type 3 = Shear and Rot. Stiffness, V = Pile-head Shear Force lbs
 Type 4 = Deflection and Moment, S = Pile-head Slope, radians

Greenwich Hospital Caisson Analysis.lpo

Type 5 = Deflection and Slope, R = Rot. Stiffness of Pile-head in-lbs/rad

Load Type	Pile-Head Condition 1	Pile-Head Condition 2	Axial Load lbs	Pile-Head Deflection in	Maximum Moment in-lbs	Maximum Shear lbs
1	V= 44540.	M= 6.00E+07	80390.0000	.5939143	6.2853E+07	-411502.

Computed Pile-head Stiffness Matrix Members
K22, K23, K32, K33 for Superstructure

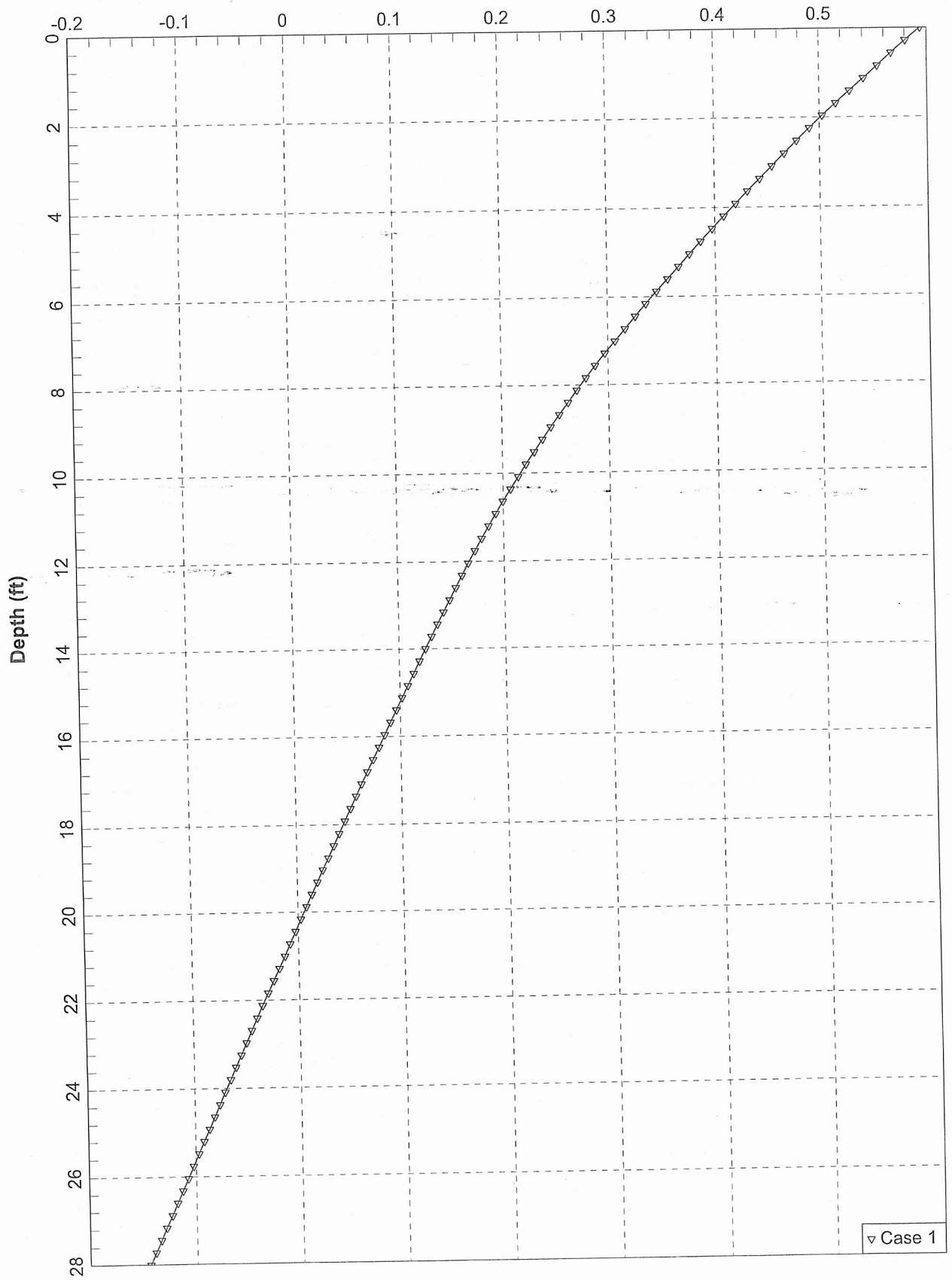
Top y in	Shear React. lbs	Mom. React. in-lbs	K22 lbs/in	K32 in-lbs/in
.00118833	4454.00007	900238.67670	3748109.	7.575646E+08
.00357724	13407.87601	2709988.	3748109.	7.575646E+08
.00566979	21250.98068	4295230.	3748109.	7.575646E+08
.00715447	26815.75201	5419977.	3748109.	7.575646E+08
.00830609	31132.12399	6292398.	3748109.	7.575646E+08
.00924702	34658.85669	7005218.	3748109.	7.575646E+08
.01004257	37640.66670	7607899.	3748109.	7.575646E+08
.01073171	40223.62802	8129965.	3748109.	7.575646E+08
.01133957	42501.96137	8590460.	3748109.	7.575646E+08
.01188332	44540.00000	9002387.	3748109.	7.575646E+08

Top Rota. rad	Shear React. lbs	Mom. React. in-lbs	K23 lbs/rad	K33 in-lbs/rad
.00003241	24553.90891	6000382.	7.575646E+08	1.851305E+11
.00009769	73917.20324	18062949.	7.566833E+08	1.849087E+11
.00015516	117170.05630	28629097.	7.551385E+08	1.845090E+11
.00019612	147866.82133	36125898.	7.539529E+08	1.842011E+11
.00022800	171681.91043	41940869.	7.529864E+08	1.839501E+11
.00025411	191143.42358	46692046.	7.522207E+08	1.837506E+11
.00027623	207600.10754	50709109.	7.515457E+08	1.835751E+11
.00029543	221857.23202	54188847.	7.509594E+08	1.834226E+11
.00031316	234436.23842	57258194.	7.486076E+08	1.828383E+11
.00033533	245712.19045	60003818.	7.327531E+08	1.789410E+11

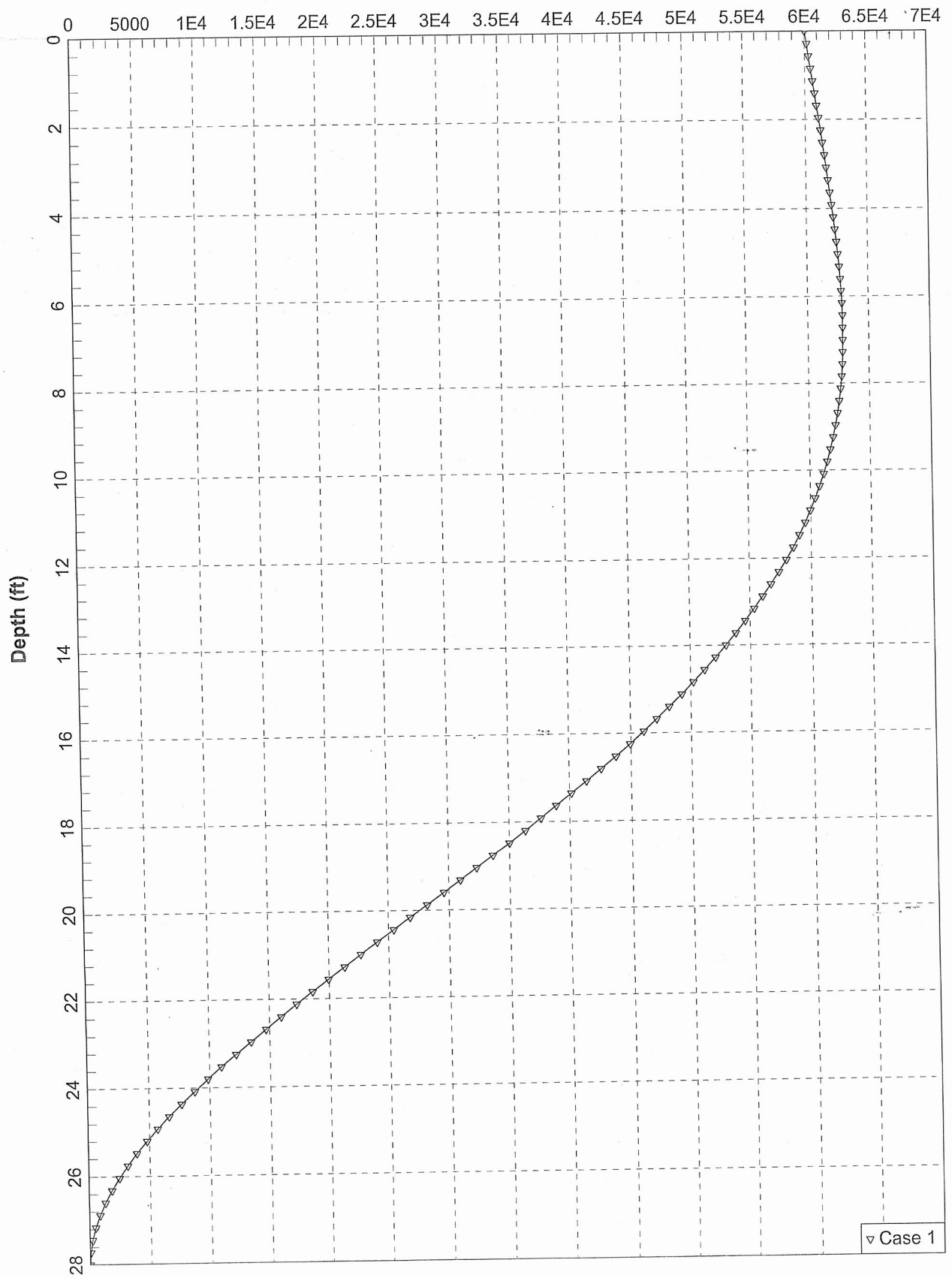
K22 = abs(Shear Reaction/Top y)
 K23 = abs(Shear Reaction/Top Rotation)
 K32 = abs(Moment Reaction/Top y)
 K33 = abs(Moment Reaction/Top Rotation)

The analysis ended normally.

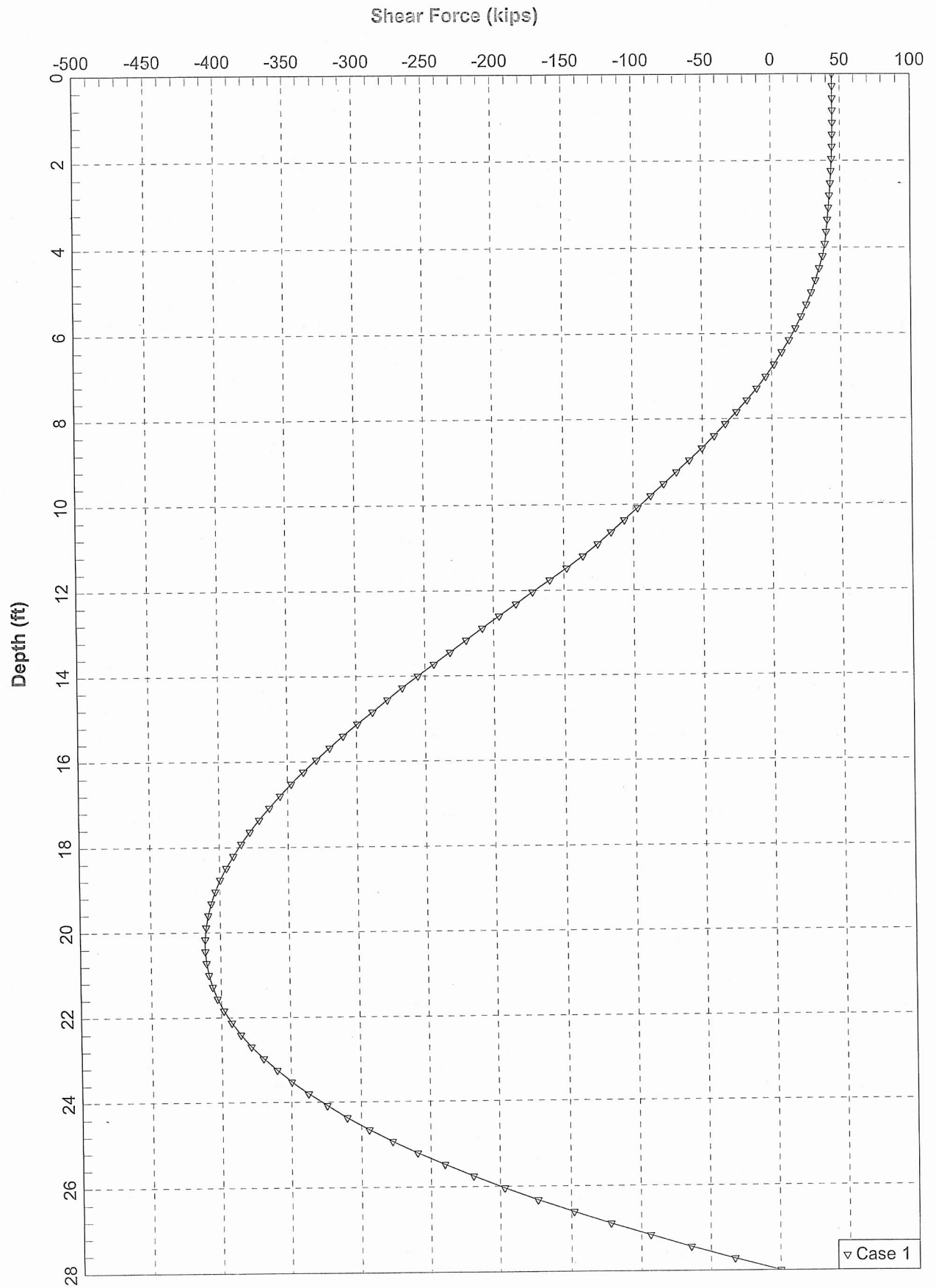
Lateral Deflection (in)



Bending Moment (in-kips)



▽ Case 1



▽ Case 1

Section 15A - CURRENT SECTOR/CELL INFORMATION - ALPHA (OR DELTA)						
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	
	Tx/Rx / TxRx GSM / 850	TxRx / TxRx N/A				
TECHNOLOGY						
RRH LOCATION (Top/Bottom/None)						
FEEDERS TYPE	1 5/8" - CommScope					
Feeder Length (feet)	160'					
ANTENNA ATOLL	7770					
ANTENNA MAKE - MODEL	Powerwave					
ANTENNA VENDOR	55.0 x 11.0 x 5.0					
ANTENNA SIZE (H x W x D)	35					
ANTENNA WEIGHT	13.5 dBi	16.5 dBi			13.5 dBi	16.5 dBi
ANTENNA GAIN						
AZIMUTH	0°	71°			0°	71°
RADIATION CENTER (feet)	71'	73'			73'	73'
ANTENNA TIP HEIGHT						
ELECTRICAL TILT (700/850/1900/AWS)	0°	0°			0°	0°
MECHANICAL DOWNTILT						
FEEDER AMOUNT	2				2	
Antenna RET Motor (QTY/MODEL)	1 / Powerwave / 7020 (DB)				1 / Powerwave / 7020 (DB)	
Antenna RET Splitter (QTY/MODEL)						
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)						
Antenna RET Surge Arrester (QTY/MODEL)						
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site						
DC BLOCK (QTY/MODEL)	N/A				N/A	
TMA/LNA (TYPE/MODEL)	2 / Powerwave / LGP 21401 (Dual Band -				N/A	
CURRENT INJECTORS FOR TMA (QTY/MODEL)	Polyphaser / 1000860				N/A	
PDU FOR TMA (QTY/MODEL) usually per site	LGP 12104 (1800 AND 850 Bypass TMA)				N/A	
SURGE ARRESTOR (QTY/MODEL)	N/A				1 / Polyphaser / 1000860	
DIPLEXER (QTY/MODEL)	0 + 2 / Powerwave / LGP 21901				2 + 2 / Powerwave / LGP 21901	
HYBRID COMBINER (QTY/MODEL)	N/A				N/A	
DUPLEXER (QTY/MODEL)	N/A				N/A	
FILTER (QTY/MODEL)	N/A				N/A	
ISXAIT KIT MODULE?	N/A				N/A	
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)	N/A				N/A	
SCPA/MCPA MODULE?	N/A				N/A	
Additional Component1	Powerwave				N/A	
Additional Component2	N/A				N/A	
Additional Component3	Daisy chain to ANT4				Daisy chain to CILOC from ANT4	
MAGNETIC DECLINATION	-14°				-14°	
HATCHPLATE POWER (Watts)	TBD	TBD			TBD	TBD
ERP (Watts)	TBD	TBD			TBD	TBD
Local Market Note1						
Local Market Note2						
Local Market Note3						

Section 15B - CURRENT SECTOR/CELL INFORMATION - BETA						
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	
	Tx/Rx / TxRx GSM / 850	TxRx / TxRx GSM / 1900				
TECHNOLOGY						
RRH LOCATION (Top/Bottom/None)						
FEEDERS TYPE	1 5/8" - CommScope					
Feeder Length (feet)	160'					
ANTENNA ATOLL	7770					
ANTENNA MAKE - MODEL	Powerwave					
ANTENNA VENDOR	55.0 x 11.0 x 5.0					
ANTENNA SIZE (H x W x D)	35					
ANTENNA WEIGHT	13.5 dBi	16.5 dBi			13.5 dBi	16.5 dBi
ANTENNA GAIN						
AZIMUTH	100°	71°			100°	71°
RADIATION CENTER (feet)	71'	73'			73'	73'
ANTENNA TIP HEIGHT						
ELECTRICAL TILT (700/850/1900/AWS)	2°	2°			2°	2°
MECHANICAL DOWNTILT						
FEEDER AMOUNT	2				2	
Antenna RET Motor (QTY/MODEL)	1 / Powerwave / 7020 (DB)				1 / Powerwave / 7020 (DB)	
Antenna RET Splitter (QTY/MODEL)						
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)						
Antenna RET Surge Arrester (QTY/MODEL)						
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site						
DC BLOCK (QTY/MODEL)	N/A				N/A	
TMA/LNA (TYPE/MODEL)	2 / Powerwave / LGP 21401 (Dual Band -				N/A	
CURRENT INJECTORS FOR TMA (QTY/MODEL)	Polyphaser / 1000860				N/A	
PDU FOR TMA (QTY/MODEL) usually per site	LGP 12104 (1800 AND 850 Bypass TMA)				N/A	
SURGE ARRESTOR (QTY/MODEL)	N/A				1 / Polyphaser / 1000860	
DIPLEXER (QTY/MODEL)	0 + 2 / Powerwave / LGP 21901				2 + 2 / Powerwave / LGP 21901	
HYBRID COMBINER (QTY/MODEL)	N/A				N/A	
DUPLEXER (QTY/MODEL)	N/A				N/A	
FILTER (QTY/MODEL)	N/A				N/A	
ISXAIT KIT MODULE?	N/A				N/A	
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)	N/A				N/A	
SCPA/MCPA MODULE?	N/A				N/A	
Additional Component1	Powerwave				N/A	
Additional Component2	N/A				N/A	
Additional Component3	Daisy chain to ANT4				Daisy chain to CILOC from ANT4	
MAGNETIC DECLINATION	-14°				-14°	
HATCHPLATE POWER (Watts)	TBD	TBD			TBD	TBD
ERP (Watts)	TBD	TBD			TBD	TBD
Local Market Note1						
Local Market Note2						
Local Market Note3						

Section 15C - CURRENT SECTOR/CELL INFORMATION - GAMMA						
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)		ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	
	Tx/Rx / TxRx GSM / 850	TxRx / TxRx N/A				
TECHNOLOGY						
RRH LOCATION (Top/Bottom/None)						
FEEDERS TYPE	1 5/8" - CommScope					
Feeder Length (feet)	160'					
ANTENNA ATOLL	7770					
ANTENNA MAKE - MODEL	Powerwave					
ANTENNA VENDOR	55.0 x 11.0 x 5.0					
ANTENNA SIZE (H x W x D)	35					
ANTENNA WEIGHT	13.5 dBi	16.5 dBi			13.5 dBi	16.5 dBi
ANTENNA GAIN						
AZIMUTH	250°	71°			250°	71°
RADIATION CENTER (feet)	71'	73'			73'	73'
ANTENNA TIP HEIGHT						
ELECTRICAL TILT (700/850/1900/AWS)	4°	2°			4°	2°
MECHANICAL DOWNTILT						
FEEDER AMOUNT	2				2	
Antenna RET Motor (QTY/MODEL)	1 / Powerwave / 7020 (DB)				1 / Powerwave / 7020 (DB)	
Antenna RET Splitter (QTY/MODEL)						
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)						
Antenna RET Surge Arrester (QTY/MODEL)						
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site						
DC BLOCK (QTY/MODEL)	N/A				N/A	
TMA/LNA (TYPE/MODEL)	2 / Powerwave / LGP 21401 (Dual Band -				N/A	
CURRENT INJECTORS FOR TMA (QTY/MODEL)	Polyphaser / 1000860				N/A	
PDU FOR TMA (QTY/MODEL) usually per site	LGP 12104 (1800 AND 850 Bypass TMA)				N/A	
SURGE ARRESTOR (QTY/MODEL)	N/A				1 / Polyphaser / 1000860	
DIPLEXER (QTY/MODEL)	0 + 2 / Powerwave / LGP 21901				2 + 2 / Powerwave / LGP 21901	
HYBRID COMBINER (QTY/MODEL)	N/A				N/A	
DUPLEXER (QTY/MODEL)	N/A				N/A	
FILTER (QTY/MODEL)	N/A				N/A	
ISXAIT KIT MODULE?	N/A				N/A	
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)	N/A				N/A	
SCPA/MCPA MODULE?	N/A				N/A	
Additional Component1	Powerwave				N/A	
Additional Component2	N/A				N/A	
Additional Component3	Daisy chain to ANT4				Daisy chain to CILOC from ANT4	
MAGNETIC DECLINATION	-14°				-14°	
HATCHPLATE POWER (Watts)	TBD	TBD			TBD	TBD
ERP (Watts)	TBD	TBD			TBD	TBD
Local Market Note1						
Local Market Note2						
Local Market Note3						

Section 150 - CURRENT SECTOR/CELL INFORMATION - DELTA					
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWNTILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLEXER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
EXACT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					
Section 15E - CURRENT SECTOR/CELL INFORMATION - EPSILON					
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWNTILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLEXER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
EXACT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					
Section 15F - CURRENT SECTOR/CELL INFORMATION - ZETA					
ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWNTILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLEXER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
EXACT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TBD		TxRx / Rx UMTS / 850	TxRx / TxRx UMTS / MC 1900	TxRx / TxRx GSM / 850
TECHNOLOGY	LTE / 700		UMTS / MC 1900		
RRH LOCATION (Top/Bottom/None)	TOP				
FEEDERS TYPE	er & 2 DC cables with RAYCAP kit		1 5/8" - CommScope		1 5/8" - CommScope
Feeder Length (feet)			160'		160'
ANTENNA ATOLL			7770		7770
ANTENNA MAKE - MODEL	P65-16-XLH-RR		Powerwave		Powerwave
ANTENNA VENDOR	Powerwave		55.0 x 11.0 x 5.0		55.0 x 11.0 x 5.0
ANTENNA SIZE (H x W x D)	72.0 x 12.0 x 6.0		35		35
ANTENNA WEIGHT	64		13.5 dBi		13.5 dBi
ANTENNA GAIN	14.0 dBi		0*		0*
AZIMUTH	30*		71'		71'
RADIATION CENTER (feet)	135'		73'		73'
ANTENNA TIP HEIGHT	138'		0*		0*
ELECTRICAL TILT (700/850/1900/AWS)	2*		0*		0*
MECHANICAL DOWNTILT	0*		0*		0*
FEEDER AMOUNT			2		2
Antenna RET Motor (QTY/MODEL)	N/A / Powerwave / Built-in RET Equipment		1 / Powerwave / 7020 (DB)		1 / Powerwave / 7020 (DB)
Antenna RET Splitter (QTY/MODEL)	N/A				
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)	N/A				
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)	2 Ericsson RRU (S/L)		N/A		N/A
CURRENT INJECTORS FOR TMA (QTY/MODEL)			2 / Powerwave / LGP 21401 (Dual Band - Polyphaser / 1000860		N/A
PDU FOR TMA (QTY/MODEL) usually per site			LG 12104 (1900 AND 850 Bypass TMA)		N/A
SURGE ARRESTOR (QTY/MODEL)			N/A		1 / Polyphaser / 1000860
DIPLEXER (QTY/MODEL)			0 + 2 / Powerwave / LGP 21901		2 + 2 / Powerwave / LGP 21901
HYBRID COMBINER (QTY/MODEL)			N/A		N/A
DUPLEXER (QTY/MODEL)			N/A		N/A
FILTER (QTY/MODEL)			N/A		N/A
RKAIT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?			Powerwave		N/A
Additional Component1			N/A		N/A
Additional Component2			Daisy chain to ANT4		Daisy chain to CILOC from ANT4
Additional Component3			-14*		-14*
MAGNETIC DECLINATION			TBD		TBD
HATCHPLATE POWER (Watts)			TBD		TBD
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

Section 16B - NEW/PROPOSED SECTOR/CELL INFORMATION - BETA

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TBD		TxRx / Rx UMTS / 850	TxRx / TxRx UMTS / MC 1900	TxRx / TxRx GSM / 850
TECHNOLOGY	LTE / 700		UMTS / MC 1900		
RRH LOCATION (Top/Bottom/None)	TOP				
FEEDERS TYPE	er & 2 DC cables with RAYCAP kit		1 5/8" - CommScope		1 5/8" - CommScope
Feeder Length (feet)			160'		160'
ANTENNA ATOLL			7770		7770
ANTENNA MAKE - MODEL	P65-16-XLH-RR		Powerwave		Powerwave
ANTENNA VENDOR	Powerwave		55.0 x 11.0 x 5.0		55.0 x 11.0 x 5.0
ANTENNA SIZE (H x W x D)	72.0 x 12.0 x 6.0		35		35
ANTENNA WEIGHT	64		13.5 dBi		13.5 dBi
ANTENNA GAIN	14.0 dBi		100*		100*
AZIMUTH	150*		71'		71'
RADIATION CENTER (feet)	135'		73'		73'
ANTENNA TIP HEIGHT	138'		2*		2*
ELECTRICAL TILT (700/850/1900/AWS)	8*		0*		0*
MECHANICAL DOWNTILT	0*		2		2
FEEDER AMOUNT			1 / Powerwave / 7020 (DB)		1 / Powerwave / 7020 (DB)
Antenna RET Motor (QTY/MODEL)	N/A / Powerwave / Built-in RET Equipment				
Antenna RET Splitter (QTY/MODEL)	N/A				
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)	N/A				
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)	2 Ericsson RRU (S/L)		N/A		N/A
CURRENT INJECTORS FOR TMA (QTY/MODEL)			2 / Powerwave / LGP 21401 (Dual Band - Polyphaser / 1000860		N/A
PDU FOR TMA (QTY/MODEL) usually per site			LG 12104 (1900 AND 850 Bypass TMA)		N/A
SURGE ARRESTOR (QTY/MODEL)			N/A		1 / Polyphaser / 1000860
DIPLEXER (QTY/MODEL)			0 + 2 / Powerwave / LGP 21901		2 + 2 / Powerwave / LGP 21901
HYBRID COMBINER (QTY/MODEL)			N/A		N/A
DUPLEXER (QTY/MODEL)			N/A		N/A
FILTER (QTY/MODEL)			N/A		N/A
RKAIT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?			Powerwave		N/A
Additional Component1			N/A		N/A
Additional Component2			Daisy chain to ANT4		Daisy chain to CILOC from ANT4
Additional Component3			-14*		-14*
MAGNETIC DECLINATION			TBD		TBD
HATCHPLATE POWER (Watts)			TBD		TBD
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

Section 16C - NEW/PROPOSED SECTOR/CELL INFORMATION - GAMMA

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?	TBD		TxRx / Rx UMTS / 850	TxRx / TxRx UMTS / MC 1900	TxRx / TxRx GSM / 850
TECHNOLOGY	LTE / 700		UMTS / MC 1900		
RRH LOCATION (Top/Bottom/None)	TOP				
FEEDERS TYPE	er & 2 DC cables with RAYCAP kit		1 5/8" - CommScope		1 5/8" - CommScope
Feeder Length (feet)			160'		160'
ANTENNA ATOLL			7770		7770
ANTENNA MAKE - MODEL	P65-16-XLH-RR		Powerwave		Powerwave
ANTENNA VENDOR	Powerwave		55.0 x 11.0 x 5.0		55.0 x 11.0 x 5.0
ANTENNA SIZE (H x W x D)	72.0 x 12.0 x 6.0		35		35
ANTENNA WEIGHT	64		13.5 dBi		13.5 dBi
ANTENNA GAIN	14.0 dBi		16.5 dBi		16.5 dBi
AZIMUTH	270*		250*		250*
RADIATION CENTER (feet)	135'		71'		71'
ANTENNA TIP HEIGHT	138'		73'		73'
ELECTRICAL TILT (700/850/1900/AWS)	2*		4*		4*
MECHANICAL DOWNTILT	0*		0*		0*
FEEDER AMOUNT			2		2
Antenna RET Motor (QTY/MODEL)	N/A / Powerwave / Built-in RET Equipment		1 / Powerwave / 7020 (DB)		1 / Powerwave / 7020 (DB)
Antenna RET Splitter (QTY/MODEL)	N/A				
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)	N/A				
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)	2 Ericsson RRU (S/L)		N/A		N/A
CURRENT INJECTORS FOR TMA (QTY/MODEL)			2 / Powerwave / LGP 21401 (Dual Band - Polyphaser / 1000860		N/A
PDU FOR TMA (QTY/MODEL) usually per site			LG 12104 (1900 AND 850 Bypass TMA)		N/A
SURGE ARRESTOR (QTY/MODEL)			N/A		1 / Polyphaser / 1000860
DIPLEXER (QTY/MODEL)			0 + 2 / Powerwave / LGP 21901		2 + 2 / Powerwave / LGP 21901
HYBRID COMBINER (QTY/MODEL)			N/A		N/A
DUPLEXER (QTY/MODEL)			N/A		N/A
FILTER (QTY/MODEL)			N/A		N/A
RKAIT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?			Powerwave		N/A
Additional Component1			N/A		N/A
Additional Component2			Daisy chain to ANT4		Daisy chain to CILOC from ANT4
Additional Component3			-14*		-14*
MAGNETIC DECLINATION			TBD		TBD
HATCHPLATE POWER (Watts)			TBD		TBD
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

Section 160 - NEW/PROPOSED SECTOR/CELL INFORMATION - DELTA

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWN TILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
RSAT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

Section 166 - NEW/PROPOSED SECTOR/CELL INFORMATION - EPSILON

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWN TILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
RSAT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

Section 169 - NEW/PROPOSED SECTOR/CELL INFORMATION - ZETA

ANTENNA CONFIG (FROM BACK):	ANTENNA 1 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 2 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 3 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 4 GSM, UMTS (850 / 1900) or LTE (700 / AWS)	ANTENNA 5 GSM, UMTS (850 / 1900) or LTE (700 / AWS)
TX/RX?					
TECHNOLOGY					
RRH LOCATION (Top/Bottom/None)					
FEEDERS TYPE					
Feeder Length (feet)					
ANTENNA ATOLL					
ANTENNA MAKE - MODEL					
ANTENNA VENDOR					
ANTENNA SIZE (H x W x D)					
ANTENNA WEIGHT					
ANTENNA GAIN					
AZIMUTH					
RADIATION CENTER (feet)					
ANTENNA TIP HEIGHT					
ELECTRICAL TILT (700/850/1900/AWS)					
MECHANICAL DOWN TILT					
FEEDER AMOUNT					
Antenna RET Motor (QTY/MODEL)					
Antenna RET Splitter (QTY/MODEL)					
Antenna RET Earth (Grounding) Clamp (QTY/MODEL)					
Antenna RET Surge Arrestor (QTY/MODEL)					
Antenna RET CONTROL UNIT (QTY/MODEL) usually per site					
DC BLOCK (QTY/MODEL)					
TMA/LNA (TYPE/MODEL)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)					
PDU FOR TMA (QTY/MODEL) usually per site					
SURGE ARRESTOR (QTY/MODEL)					
DIPLER (QTY/MODEL)					
HYBRID COMBINER (QTY/MODEL)					
DUPLEXER (QTY/MODEL)					
FILTER (QTY/MODEL)					
RSAT KIT MODULE?					
TRIPLEXER or NARROW BAND LLC (QTY/MODEL)					
SCPA/MCPA MODULE?					
Additional Component1					
Additional Component2					
Additional Component3					
MAGNETIC DECLINATION					
HATCHPLATE POWER (Watts)					
ERP (Watts)					
Local Market Note1					
Local Market Note2					
Local Market Note3					

P65-16-XLH-RR Dual Broadband Antennas

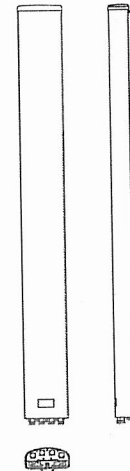
POLARIZATION: Dual linear $\pm 45^\circ$
 FREQUENCY (MHz): 698-894, 1710-2170
 HORIZONTAL BEAM WIDTH ($^\circ$): 65, 65
 GAIN (dBi/dBd): 15.5/13.4 17.5/15.4
 TILT: 1-12, 0-8
 LENGTH: 72"

ELECTRICAL SPECIFICATIONS*

	698-894		1710-2170	
	698-806	806-894	1710-1880	1850-1990
Frequency range (MHz)	698-894		1710-2170	
Frequency band (MHz)	698-806	806-894	1710-1880	1850-1990
Gain (dBi/dBd)	14.8/12.7	15.5/13.4	16.9/14.8	17.2/15.1
Polarization	Dual Linear +/- 45		Dual Linear +/- 45	
Nominal Impedance (Ω)	50		50	
VSWR	< 1.5:1		< 1.5:1	
Horizontal beam width, -3 dB ($^\circ$)	66	65	60	63
Vertical beam width, -3 dB ($^\circ$)	14.7	12.5	6.8	6.4
Electrical down tilt ($^\circ$)	1 to 12		0 to 8	
Side lobe suppression, vertical 1st upper (dB)	> 16	> 16	> 16	> 16
Isolation between inputs (dB)	> 30	> 30	> 30	> 30
Inter band Isolation (dB)	> 40		> 40	
Tracking, horizontal plane $\pm 60^\circ$ (dB)	< 2	< 2	< 2	< 2
First null fill (dB)	> 20	> 20	> 20	> 20
Vertical beam squint ($^\circ$)	< 0.8	< 0.8	< 0.5	< 0.5
Front to back ratio (dB) $180^\circ \pm 30^\circ$ copolar	> 24	> 24	> 30	> 30
Front to back ratio (dB) $180^\circ \pm 30^\circ$ total power	> 15	> 15	> 15	> 15
Cross polar discrimination (XPD) 0° (dB)	> 10	> 10	> 10	> 10
Cross polar discrimination (XPD) $\pm 60^\circ$ (dB)	> 10	> 10	> 10	> 10
Far field coupling	< -153		< -153	
IM3, 2xTx@43dBm (dBc)	< -153		< -153	
IM7, 2xTx@43dBm (dBc)	< -153		< -153	
Power handling, average per input (W)	500		250	
Power handling, average total (W)	1000		500	

MECHANICAL SPECIFICATIONS*

Connector	4 X 7/16 DIN Female, IP67
Connector position	Bottom
Dimensions, HxWxD, mm (ft)	72" x 12" x 6" (1829 x 305 x 152)
Mounting	Pre-mounted Tilt Brackets
Weight, with brackets, kg (lbs)	29 (64)
Weight, without brackets, kg (lbs)	24 (53)
Wind load, frontal/lateral/rear side 42 m/s Cd=1.6 (N)	1380
Maximum operational wind speed, m/s (mph)	100 (45)
Survival wind speed, m/s (mph)	150 (67)
Lightning protection	DC Ground
Operating Temperature	-40C to +60C
Radome material	PVC, IP55
Packet size, HxWxD, mm (ft)	87" x 16" x 10" (2225 x 400 x 225)
Radome colour	Light Grey
Shipping weight, kg (lbs)	34 (75)
RET	iRET AISGv1.1, MET and AISGv2.0
Brackets	7256.00, 7454.00



*All specifications subject to change without notice. Please contact your Powerwave representative for complete performance data.

ANTENNA PATTERNS*

For detailed patterns visit <http://www.powerwave.com/rpa/>.

7770.00A

DBB90 Broadband Cross Polarized

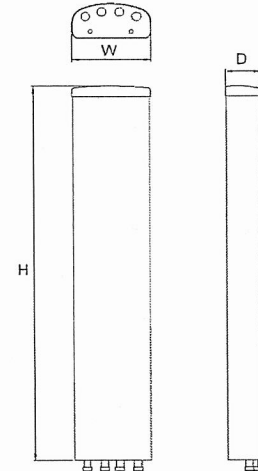
POLARIZATION: XX-Pol
 FREQUENCY (MHz): 824-896, 1710-2170
 HORIZONTAL BEAM WIDTH (°): 90
 GAIN (dBi/dBd): 13.5/11.4, 15.5/13.4
 TILT: MET
 LENGTH: 1.4m (4'7")

ELECTRICAL SPECIFICATIONS*

	824-896		1710-2170		
	824-896	1710-1880	1850-1990	1900-2170	
Frequency range (MHz)	824-896	1710-1880	1850-1990	1900-2170	
Frequency band (MHz)	824-896	1710-1880	1850-1990	1900-2170	
Gain (dBi/dBd)	13.5/11.4	15.5/13.4	15.5/13.4	15.5/13.4	
Polarization	Dual linear $\pm 45^\circ$		Dual linear $\pm 45^\circ$		
Nominal Impedance (Ω)	50		50		
VSWR	<1.5:1		<1.5:1		
Horizontal beam width, -3 dB (°)	85	90	90	90	
Vertical beam width, -3 dB (°)	15	7	7	7	
Electrical down tilt (°)	0 to 10		0 to 8		
Side lobe suppression, vertical 1st upper (dB)	>18	>18	>18	>18	
Isolation between inputs (dB)	>30	>30	>30	>25	
Inter band Isolation (dB)	>36	>36	>36	>36	
Tracking, horizontal plane $\pm 60^\circ$ (dB)	<2	<2	<2	<2	
First null fill (dB)	-	-	-	-	
Vertical beam squint (°)	<1.0	<0.5	<0.5	<0.5	
Front to back ratio (dB) $180^\circ \pm 30^\circ$ copolar	>25	>25	>25	>25	
Front to back ratio (dB) $180^\circ \pm 30^\circ$ total power	>22	>21	>21	>21	
Cross polar discrimination (XPD) 0° (dB)	-	-	-	-	
Cross polar discrimination (XPD) $\pm 60^\circ$ (dB)	>10	>10	>10	>10	
Far field coupling	-	-	-	-	
IM3, 2xTx@43dBm (dBc)	<-153	-	<-153	-	
IM7, 2xTx@43dBm (dBc)	-	-	<-160	-	
Power handling, average per input (W)	500	-	250	-	
Power handling, average total (W)	800	-	500	-	

MECHANICAL SPECIFICATIONS*

Connector	4 x 7/16 DIN Female
Connector position	Bottom
Dimensions, HxWxD, mm (ft)	1408x280x125mm
Mounting	Pre-mounted heavy duty brackets
Weight, with brackets, kg (lbs)	17.6 (39)
Weight, without brackets, kg (lbs)	12.1 (27)
Wind load, frontal/lateral/rear side 42 m/s Cd=1.6 (N)	415.
Maximum operational wind speed, m/s (mph)	42 (93)
Survival wind speed, m/s (mph)	55 (123)
Lightning protection	DC grounded
Operating Temperature	-40°C to +60°C
Radome material	GRP
Package size, HxWxD, mm (ft)	1550x355x255 (61"x1'2"x10")
Radome colour	Light Grey
Shipping weight, kg (lbs)	21.5 (47.4)
RET	8220.10, 8220.40, 8210.10, 8210.40
Brackets	7256.00, 7454.00



*All specifications subject to change without notice. Please contact your Powerwave representative for complete performance data.

ANTENNA PATTERNS*

For detailed patterns visit <http://www.powerwave.com/rpa/>.

Tower Mounted Amplifier



1900/850 MHz

Technical Specifications

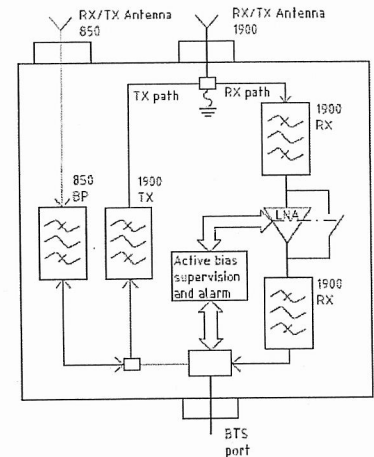
Product Number	LGP214nn	
850 MHz	Bypass (MHz)	824-894
	Return loss* (dB)	> 20
	Insertion loss* (dB)	< 0.3
1900 MHz		
Up-link	Frequency range, full band (60 MHz)	1850-1910
	Nominal gain (dB)	12
	Return loss* (dB)	> 20
	Noise figure* (dB)	< 1.7
	Output 3rd order Intercept Point* (dBm)	> +23
Down-link	Frequency range, full band (60 MHz)	1930-1990
	Insertion loss* (dB)	< 0.6
	Return loss* (dB)	> 20
Intermodulation	2 Tx@x43 dBm (dBc)	<-158
Alarm Functionality	Two levels, individually supervised LNAs	
Power Consumption	@12 VDC	1.2 W

* Typical

All specifications subject to change without notice. Please contact your Powerwave representative for complete performance data.

Mechanical Specifications

Size, W x H x D (without mounting plate)	235 x 366 x 66 mm (9.2 x 14.4 x 2.6 in)
Weight	6.4 kg (14.1 lbs)
Color	Off white (NCS 1502-R)
Housing	Aluminum
RF-connectors	DIN 7/16 female.
Mounting kit	Mounting kit for pole and wall is included
Temperature range	-40 °C to +65 °C (-40 °F to +149 °F)
MTBF	>1 million hours
Safety	UL 60 950
Ingress protection, IP 65	EN 60 529
Environmental	ETS 300 019
EMC	FCC Part 15



D031-08422 Rev. A Pg. 2 of 2

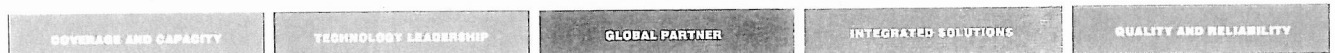
Corporate Headquarters
 Powerwave Technologies, Inc.
 1801 East St. Andrew Place
 Santa Ana, CA 92705 USA
 Tel: 714-466-1000
 Fax: 714-466-5800
 www.powerwave.com

Main European Office
 Antennvägen 6
 SE-187 80 Täby
 Sweden
 Tel: +46 8 540 822 00
 Fax: +46 8 540 823 40

Main Asia-Pacific Office
 23 F Tai Yau Building
 181 Johnston Road
 Wanchai, Hong Kong
 Tel: +852 2512 6123
 Fax: +852 2575 4860



©Copyright 2006, Powerwave Technologies, Inc. All Rights reserved. Powerwave, Powerwave Technologies, The Power in Wireless and the Powerwave logo are registered trademarks of Powerwave Technologies, Inc.



P65-16-XLH-RR Dual Broadband Antennas

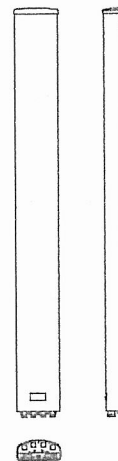
POLARIZATION: Dual linear $\pm 45^\circ$
 FREQUENCY (MHz): 698-894, 1710-2170
 HORIZONTAL BEAM WIDTH ($^\circ$): 65, 65
 GAIN (dBi/dBd): 15.5/13.4 17.5/15.4
 TILT: 1-12, 0-8
 LENGTH: 72"

ELECTRICAL SPECIFICATIONS*

	698-894		1710-1880	1710-2170	
	698-806	806-894		1850-1990	1900-2170
Frequency range (MHz)					
Frequency band (MHz)					
Gain (dBi/dBd)	14.8/12.7	15.5/13.4	16.9/14.8	17.2/15.1	17.5/15.4
Polarization	Dual Linear +/- 45			Dual Linear +/- 45	
Nominal Impedance (Ω)	50			50	
VSWR	< 1.5:1			< 1.5:1	
Horizontal beam width, -3 dB ($^\circ$)	66	65	60	63	63
Vertical beam width, -3 dB ($^\circ$)	14.7	12.5	6.8	6.4	5.7
Electrical down tilt ($^\circ$)	1 to 12			0 to 8	
Side lobe suppression, vertical 1st upper (dB)	> 16	> 16	> 16		
	> 16	> 16			
Isolation between inputs (dB)	> 30	> 30	> 30	> 30	
Inter band Isolation (dB)	> 40			> 40	
Tracking, horizontal plane $\pm 60^\circ$ (dB)	< 2		< 2	< 2	< 2
First null fill (dB)			> -20	> -20	> -20
Vertical beam squint ($^\circ$)	< 0.8	< 0.8	< 0.5	< 0.5	< 0.5
Front to back ratio (dB) $180^\circ \pm 30^\circ$ copolar	> 24	> 24	> 30	> 30	> 28
Front to back ratio (dB) $180^\circ \pm 30^\circ$ total power					
Cross polar discrimination (XPD) 0° (dB)	> 15	> 15	> 15	> 15	> 15
Cross polar discrimination (XPD) $\pm 60^\circ$ (dB)	> 10	> 10	> 10	> 10	> 10
Far field coupling					
IM3, 2xTx@43dBm (dBc)	< -153			< -153	
IM7, 2xTx@43dBm (dBc)					
Power handling, average per input (W)	500			250	
Power handling, average total (W)	1000			500	

MECHANICAL SPECIFICATIONS*

Connector	4 X 7/16 DIN Female, IP67
Connector position	Bottom
Dimensions, HxWxD, mm (ft)	72" x 12" x 6" (1829 x 305 x 152)
Mounting	Pre-mounted Tilt Brackets
Weight, with brackets, kg (lbs)	29 (64)
Weight, without brackets, kg (lbs)	24 (53)
Wind load, frontal/lateral/rear side 42 m/s Cd=1.6 (N)	1380
Maximum operational wind speed, m/s (mph)	100 (45)
Survival wind speed, m/s (mph)	150 (67)
Lightning protection	DC Ground
Operating Temperature	-40C to +60C
Radome material	PVC, IP55
Packet size, HxWxD, mm (ft)	87" x 16" x 10" (2225 x 400 x 225)
Radome colour	Light Grey
Shipping weight, kg (lbs)	34 (75)
RET	iRET AISGv1.1, MET and AISGv2.0
Brackets	7256.00, 7454.00A



*All specifications subject to change without notice. Please contact your Powerwave representative for complete performance data.

ANTENNA PATTERNS*

For detailed patterns visit <http://www.powerwave.com/rpa/>.



RRUS 11 – Dual PA RRU.

Technical Data

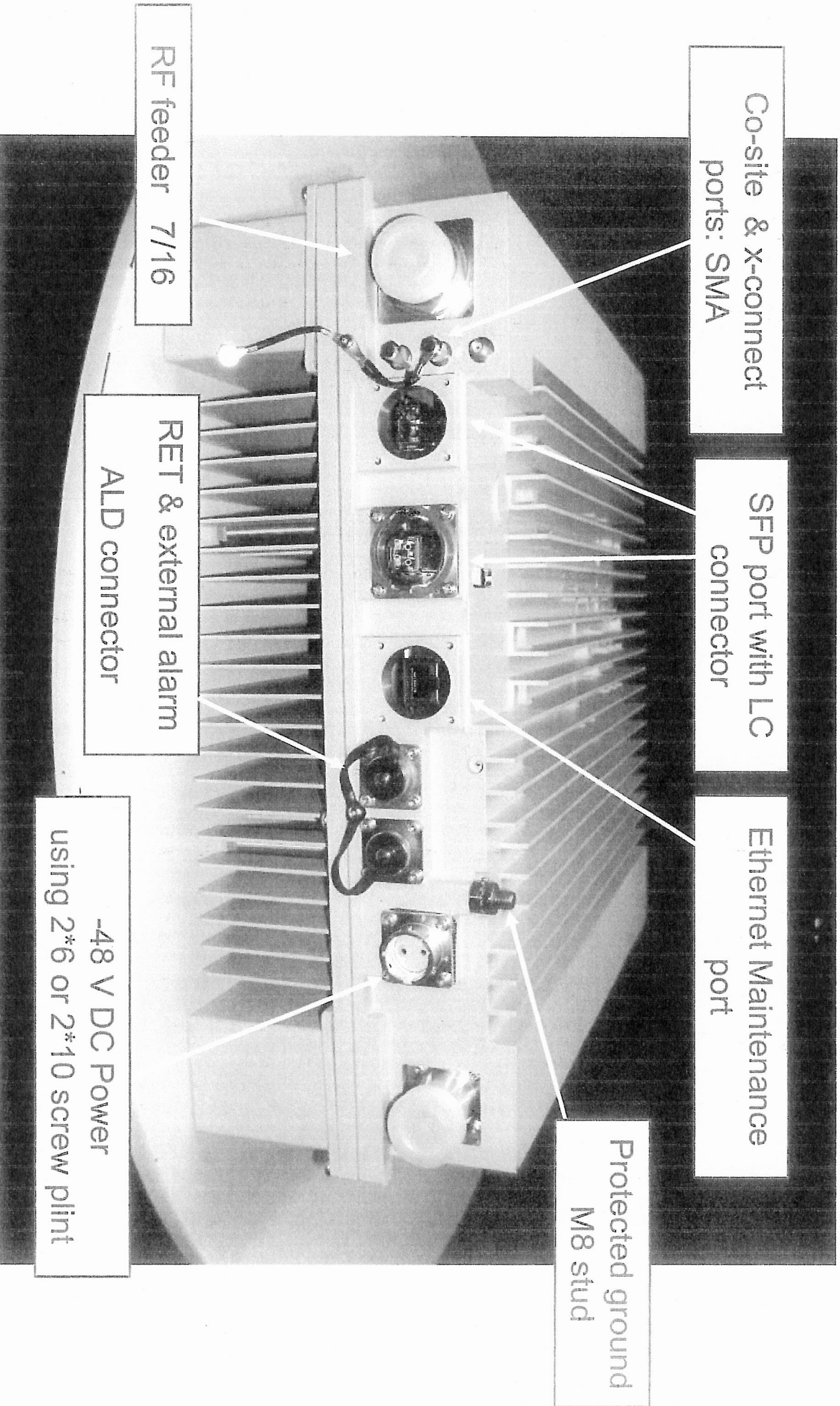
RBS6000

- > Multi standard
- > RF: 2x30 Watts
- > Carrier BW: 1.4 – 20 MHz
- > Alarms: 2
- > Dimensions (with sunshield):
 - Width: 17.0 in
 - Height: 17.8 in
 - Depth: 7.2 in
 - Weight: 55 lbs (Band 12)
 - Weight: 50 lbs (Band 4)
- > Temperature: -40 to +131 F
- > Cooling: Self convection
- > Power: -48 VDC
- > Rec. fuse size 20 Amp
 - Rec. DC cable:
 - 6 mm² up to 60 meters
 - 10 mm² over 60 meters
- > Shielded
- > Power Cons: 200 Watts typ.



RRUS-11 I/F

RBS6000



POWER

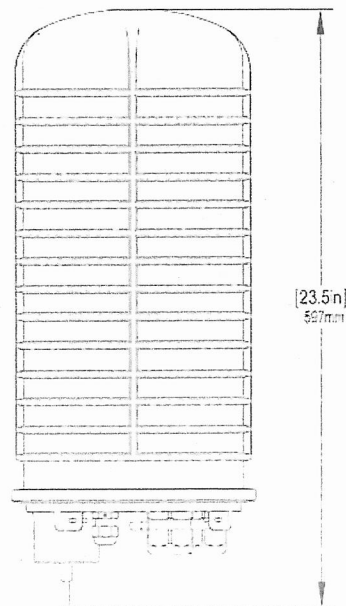
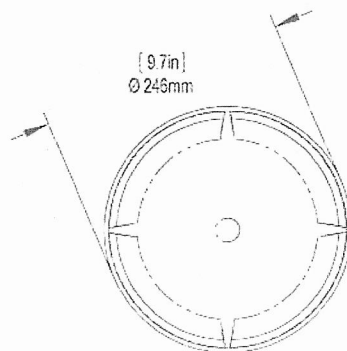
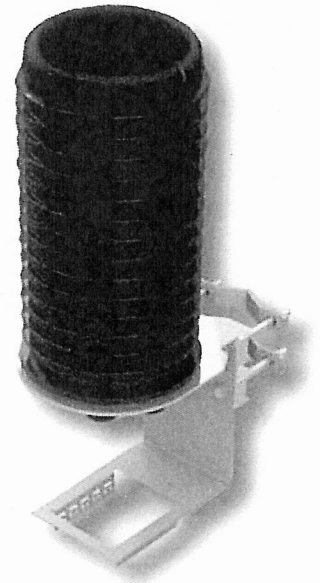
DC6-48-60-18-8F

DC Surge Suppression Solution

The DC6-48-60-18 is a dual chambered, DC surge suppression system for use in multi-circuit, Distributed Antenna Systems. The system will protect up to 6 Remote Radio Heads from voltage surges and lightning, and connect up to 18 fiber pairs. The system is enclosed in a NEMA 4 rated, waterproof enclosure.

FEATURES

- Protects up to 6 Remote Radio Heads, each with its own protection circuit.
- Flexible design allows for installation at the top of a tower for Remote Radio Head protection.
- Includes fiber connections for up to 18 pairs of fiber.
- LED indicators on individual circuits provide visual indication of suppressor status.
- Form 'C' relays allow for remote monitoring of the suppressor status.
- Patented Strikesorb technology provides over 60 kA of surge current capacity per circuit.
- Strikesorb suppression modules are fully recognized to UL 1449-3rd Edition Safety Standard, meeting all intermediate and high current fault requirements to facilitate use in OEM applications.
- Raycap recommends that DC protection system be installed within 2 meters or 6 feet of the radio.
- Dome design is lightweight and aerodynamic providing maximum flexibility for installation on top of towers.



Raycap

DC6-48-60-18-8F

DC Power Surge Protection

Electrical Specifications	
Model Number	DC6-48-60-18-8F
Nominal Operating Voltage	48 VDC
Nominal Discharge Current (I_n)	20 kA 8/20 μ s
Maximum Discharge Current (I_{max}) per NEMA LS-1	60 kA 8/20 μ s
Maximum Continuous Operating Voltage (U_c)	75 VDC
Voltage Protection Rating	400 V

Mechanical Specifications	
Suppression Connection Method	Compression lug, #2-#14 AWG Copper, #2-#12 Aluminum
Fiber Connection Method	LC-LC Single mode duplex
Environmental Rating	IP 68, 7m 72hrs
Operating Temperature	-40° C to + 80° C
Storage Temperature	-70° C to + 80° C
Cold Temperature Cycling	IEC 61300-2-22e -30° C to + 60° C 200 hrs @ 5 psi
Resistance to Aggressive Materials	CEI IEC 61073-2 including acids and bases
UV Protection	ISO 4892-2 Method A Xenon-Arc 2160 hrs
Weight	20 lbs without Mounting Bracket

STANDARDS

Strikesorb modules are compliant to the following Surge Protection Device (SPD) Standards:

- ANSI/UL 1449 - 3rd Edition
- IEEE C62.41
- NEMA LS-1, IEC 61643-1:2005 2nd Edition:2005
- IEC 61643-12
- EN 61643-11:2002 (including A11:2007)



Raycap

G02-00-068 REV 050610



GS-07F-0435V



Certified to
ISO 9001:2000



TUV Rheinland
of North America



New Cingular Wireless PCS, LLC
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 463-5511
Fax: (860) 513-7190

Douglas L. Culp
Real Estate Consultant

May 6, 2011

Honorable Peter Tesei
1st Selectman, Town of Greenwich
Greenwich Town Hall
101 Field Point Road
Greenwich, CT 06830

Re: Telecommunications Facility – 5 Perryridge Road Greenwich, CT

Dear First Selectman Tesei:

In order to accommodate technological changes, implement Uniform Mobile Telecommunications System (“UMTS”) and Long Term Evolution (“LTE”) capabilities, and enhance system performance in the State of Connecticut, New Cingular Wireless PCS, LLC (“AT&T”) will be changing its equipment configuration at certain cell sites.

As required by Regulations of Connecticut State Agencies (“R.C.S.A.”) Section 16-50j-73, the Connecticut Siting Council has been notified of the changes and will review AT&T’s proposal. Please accept this letter as notification under Section 16-50j-73 of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2).

The accompanying letter to the Siting Council fully describes Cingular’s proposal for the referenced cell site. However, if you have any questions or require any further information on our plans or the Siting Council’s procedures; please call me at (860) 463-5511 or Ms. Linda Roberts, Executive Director, Connecticut Siting Council at (860) 827-2935.

Sincerely,

Douglas L. Culp
Real Estate Consultant

Enclosure