

KENNETH C. BALDWIN

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Also admitted in Massachusetts

November 20, 2019

Melanie A. Bachman, Esq. Executive Director/Staff Attorney Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: Notice of Exempt Modification – Facility Modification Butternut Hollow Road, Greenwich, Connecticut

Dear Ms. Bachman:

Cellco Partnership d/b/a Verizon Wireless ("Cellco") currently maintains twelve (12) antennas at the 130-foot level on the existing 180-foot tower off Butternut Hollow Road in Greenwich, Connecticut (the "Property"). The tower is owned by the State of Connecticut, Department of Emergency Services and Public Protection ("DESPP"). The Siting Council approved Cellco's use of the DESPP tower in 1992 (Docket No. 150). A copy of the Council's Docket No. 150 approval is included in <u>Attachment 1</u>.

Cellco now intends to modify its facility by replacing six (6) of its existing antennas with six (6) new antennas and installing six (6) remote radio heads ("RRHs"), and one (1) HYBRIFLEX<sup>TM</sup> fiber optic antenna cable. A set of project plans showing the proposed facility modifications and equipment specifications are included in <u>Attachment 2</u>.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Greenwich's First Selectman, Peter Tesei; Katie DeLuca, Greenwich's Director of Planning and Zoning; DESPP, the tower owner; and Aquarion Water Company ("Aquarion"), the owner of the Property.

<sup>&</sup>lt;sup>1</sup> It remains unclear whether the building associated with the State Police tower is located in the Route 15 ROW or on property owned by Aquarion. In an excess of caution, we are sending a copy of this notice to both the Connecticut Department of Transportation and Aquarion.

### Robinson+Cole

Melanie A. Bachman, Esq. November 20, 2019 Page 2

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing tower. Cellco's replacement antennas and RRHs will be installed at a centerline height of 130 feet on the 180-foot tower.
- 2. The proposed modifications will not involve any change to ground-mounted equipment and, therefore, will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The installation of six (6) new antennas and six (6) RRHs will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. A cumulative General Power Density table for Cellco's modified facility is included in <u>Attachment 3</u>.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The tower and its foundation, with certain modifications, and antenna mounting brackets can support Cellco's proposed equipment modifications. (*See* Detailed Structural Analysis Report, including Tower Reinforcement Drawings, included in <u>Attachment 4</u>).

A copy of the parcel map and Property owner information is included in <u>Attachment 5</u>. A Certificate of Mailing verifying that this filing was sent to municipal officials and the Property owner is included in <u>Attachment 6</u>.

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

### Robinson+Cole

Melanie A. Bachman, Esq. November 20, 2019 Page 3

Sincerely,

Kenneth C. Baldwin

Enclosures

Copy to:

Peter Tesei, Greenwich First Selectman Katie DeLuca, Greenwich Director of Planning and Zoning Brian Benito, DESPP Aquarion Water Company State of Connecticut Department of Transportation Tim Parks

# **ATTACHMENT 1**



DOCKET NO. 150 - An application of the State of Connecticut, Department of Public Safety, Division of State Police for a Certificate of Environmental Compatibility and Public Need for the construction, operation, and maintenance of a telecommunications facility located on Butternut Hollow Road, in the Town of Greenwich, Connecticut.

Connecticut

Siting

Council

August 4, 1992

#### DECISION AND ORDER

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a telecommunications tower, building, and associated equipment at the proposed site in Greenwich, Connecticut, including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forest and parks; air and water purity; and fish and wildlife are not disproportionate either alone or cumulatively with other effects, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application, and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by 16-50k of the General Statutes of Connecticut (CGS), be issued to the Connecticut Department of Public Safety, Division of State Police, for the construction, operation, and maintenance of a telecommunications tower, building, and associated equipment at the proposed site on Butternut Hollow Road, in Greenwich, Connecticut.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this proceeding, and subject to the following conditions:

- 1. The self-supporting, lattice tower shall be designed no taller than necessary to provide the proposed communications, and in no event shall the tower exceed the proposed tower height of 200 feet above ground level, with antennas and all appurtenances, to maintain a clear microwave path from the Butternut Hollow Road site to the Greenwich Hospital rooftop facility.
- 2. Prior to construction, a Phase 1 archaeological survey of the facility site shall be conducted by a professional archaeologist with results submitted to the Council. All artifacts shall be made available for inspection by the Connecticut Historic Preservation Office and, if necessary, a Phase II archaeological survey shall be prepared and submitted to the Council.
- 3. New connecting utility lines to the facility shall be undergrounded along Butternut Hollow Road.

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- 4. The Certificate Holder shall prepare a Development and Management (D&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of State agencies. The D&M Plan shall be submitted and approved by the Council prior to the commencement of construction and shall also include:
  - A. Final comprehensive site plans detailing the tower location, tower foundation specifications and profiles, tower height and antenna placements, equipment building specifications and profiles, placement of the propane tank, all grading and cut and fill details showing existing and final contour lines and elevations, the security fence, and landscaping and placement of vegetative screening.
  - B. Detailed plans, including grading, for the final route of the site's access road, designed to minimize tree clearing and excessive cutting of earth.
  - C. Detailed plans for the underground utility line from the nearest existing utility pole on Butternut Hollow Road to the tower site. Such plans are to be developed with review by the Connecticut Light and Power Company and the Town of Greenwich.
  - D. Plans for erosion and sedimentation control consistent with the Connecticut Guidelines for Soil Erosion and Sediment Control, as amended, including measures for the protection of wetlands, watercourses, and Putnam Lake.
  - E. Plans for the final disposal of excess excavated material from trenching activities.
  - F. Plans and procedures for blasting, including explosion protection, and notification to adjacent property owners.
  - G. Final construction schedule.
- 5. Selective vegetative clearing shall be allowed prior to approval of the D&M plan to permit reconnaissance necessary to prepare the D&M Plan and the Phase I archaeological survey.
- 6. The Certificate Holder shall comply with existing and future radio frequency (RF) standards promulgated by State or federal regulatory agencies. Upon the establishment of any new governmental RF standards, the facility granted herein shall be brought into compliance with such standards.

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- 7. The Certificate Holder shall provide the Council a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels originally calculated and provided in the application.
- 8. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
- 9. The Certificate Holder shall notify the Council of the commencement of construction no less than seven days prior to construction and shall provide a report to the Council upon completion of construction, including the final construction costs and date of commercial operation.
- 10. If the facility does not initially provide, or permanently ceases to provide telecommunications service following completion of construction, this Decision and Order shall be void, and the tower and all associated equipment shall be dismantled and removed or reapplication for any new use shall be made to the Council before any such new use is made.

Unless otherwise approved by the Council, this Decision and Order shall be void if all construction authorized herein is not completed within five years of the effective date of this Decision and Order or within five years after all appeals to this Decision and Order have been resolved.

Pursuant to CGS Section 16-50p, we hereby directed that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in <a href="https://example.com/The-Greenwich Time">The Greenwich Time</a> and <a href="https://example.com/The-Greenwich News">The Greenwich News</a>.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of State Agencies.

The parties to this proceeding are:

#### PARTIES

Connecticut State Police

#### ITS REPRESENTATIVES

L. D. McCallum and Stephen R. Sarnoski Office of the Attorney General Mackenzie Hall 110 Sherman Street Hartford, CT 06105 (203) 566-7570 Docket No. 150 Decision and Order Page 4

Town of Greenwich

Metro Mobile CTS, Inc.

INTERVENOR

Springwich Cellular Limited Partnership Attorney John K. Wetmore Assistant Town Attorney Town of Greenwich 101 Field Point Road Greenwich, CT 06830

Henry H. Sprague III Robinson and Cole One Commercial Plaza Hartford, CT 06103-3597 (203) 275-8200

ITS REPRESENTATIVES

Peter J. Tyrrell, Esq.
Springwich Cellular Limited
Partnership
227 Church Street
New Haven, CT 06510
(203) 771-7381

TEF/bd

6264E

#### CERTIFICATION

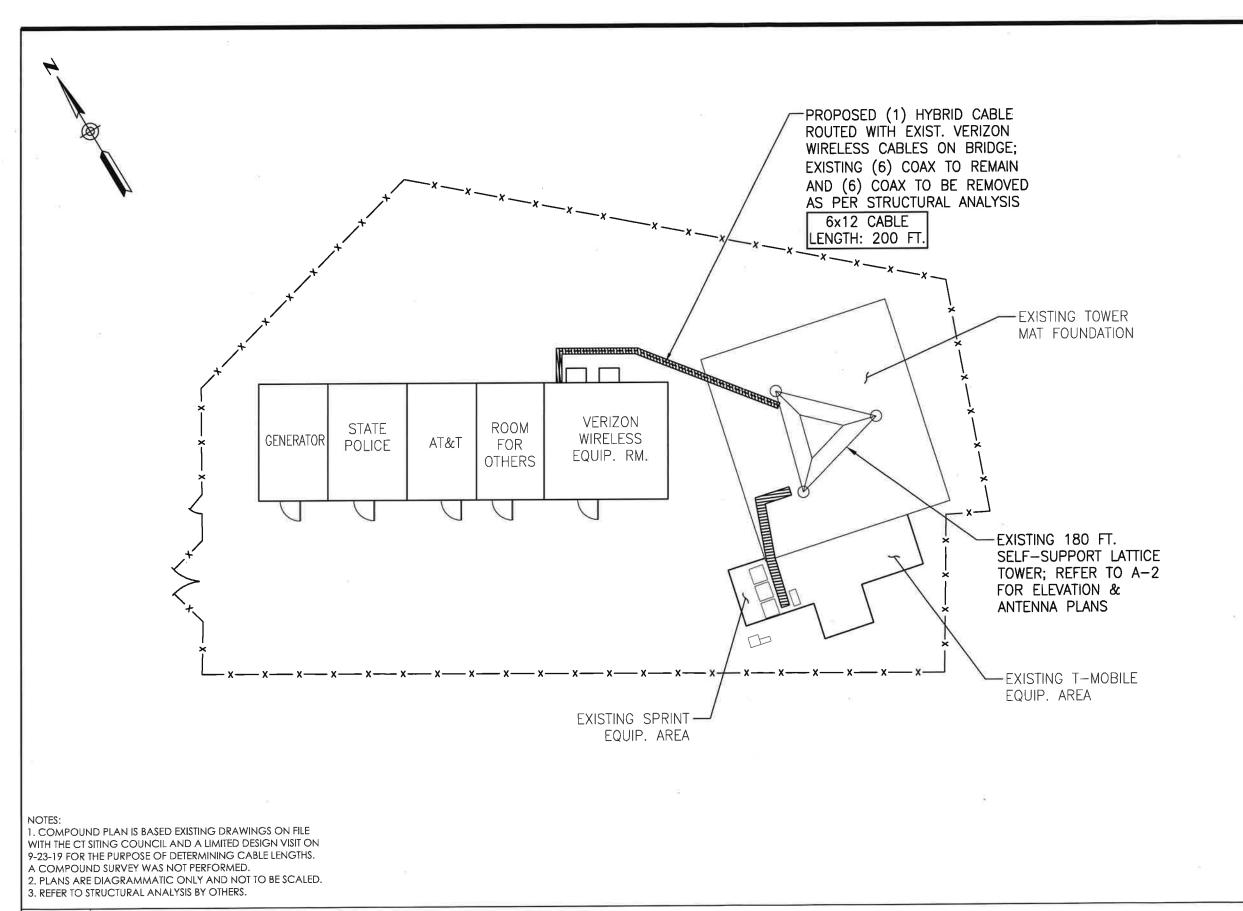
The undersigned members of the Connecticut Siting Council (Council) hereby certify that they have heard this case, or read the record thereof, in DOCKET NO. 150 - An application of the State of Connecticut, Department of Public Safety, Division of State Police for a Certificate of Environmental Compatibility and Public Need for the construction, operation, and maintenance of a telecommunications facility located on Butternut Hollow Road, in the Town of Greenwich, Connecticut, and voted as follows to approve the site:

Council Members	Vote Cast
Mortimer A. Gelston Chairman	YES
Commissioner Clifton A. Leonhardt Designee Gerald J. Heffernan	ABSTAIN
Commissioner Timothy R.E. Keeney Designee: Brian Emerick	YES
Harry E. Govey	YES
Daniel P. Lynch, Jr.	YES
Gloria Dibble Pond	ABSENT
Paulann H. Sheets	YES
William H. Smith	ABSENT
Colin C. Tait	ABSTAIN

Dated at New Britain, Connecticut, August 4, 1992.

6302E-2

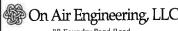
# **ATTACHMENT 2**



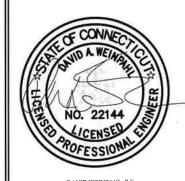
verizon/

WIRELESS COMMUNICATIONS FACILITY

20 ALEXANDER DRIVE WALLINGFORD, CT 06492



88 Foundry Pond Road Cold Spring, NY 10516 201-456-4624 onair@optonlinc.net



		SUBMITTALS
D	10,30,19	REVIEW
_		
_		
_	_	

NO DATE DRAWN BY: DW CHECKED BY:

**ANTMO** AWS-PCS-850-LTE **DESIGN EXHIBITS** 

SITE NAME:

**BUTTERNUT CT** 

SITE ADDRESS:

CT STATE POLICE TOWER BUTTERNUT HOLLOW RD. GREENWICH, CT 06830

SHEET TITLE:

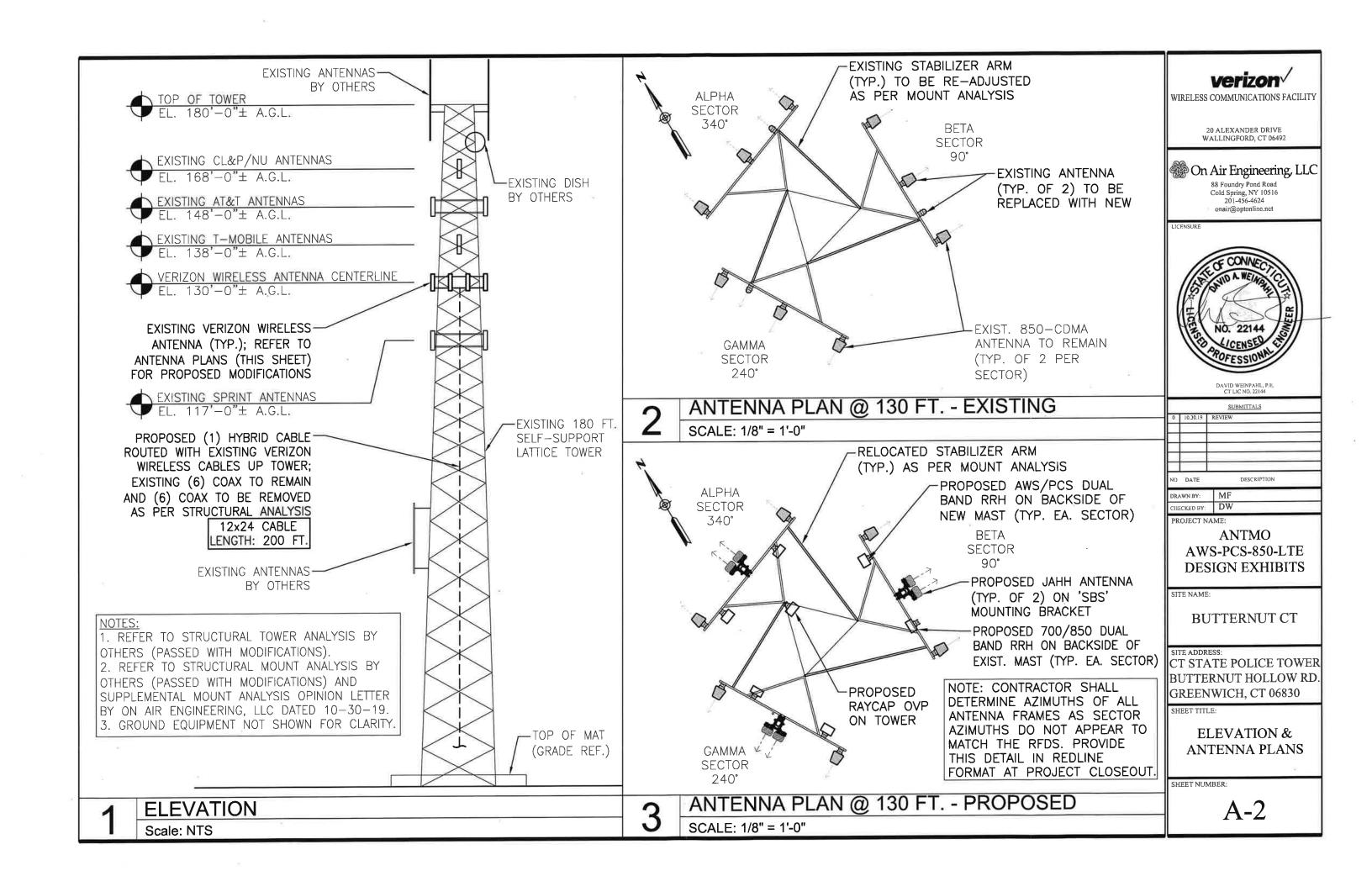
COMPOUND PLAN

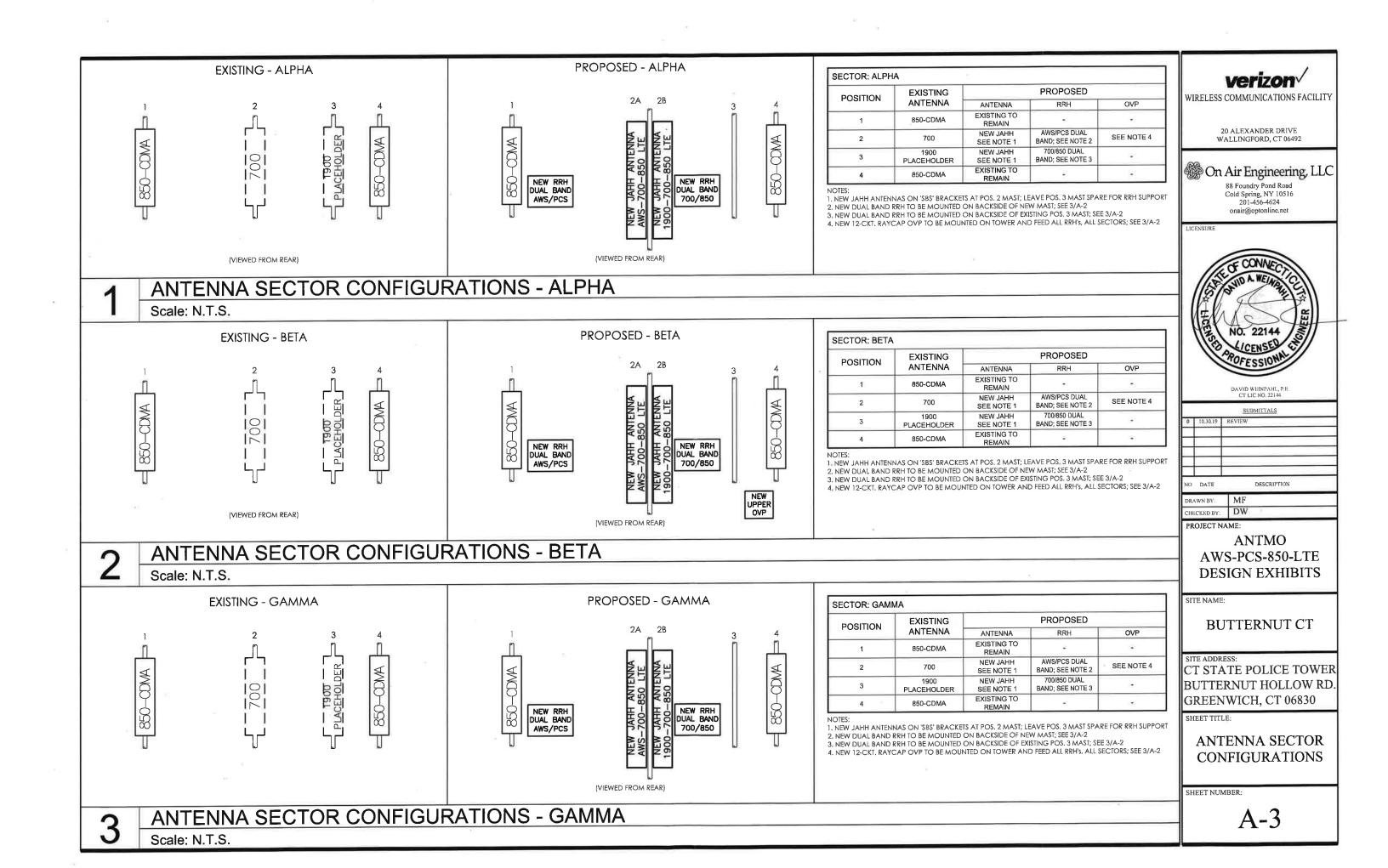
SHEET NUMBER:

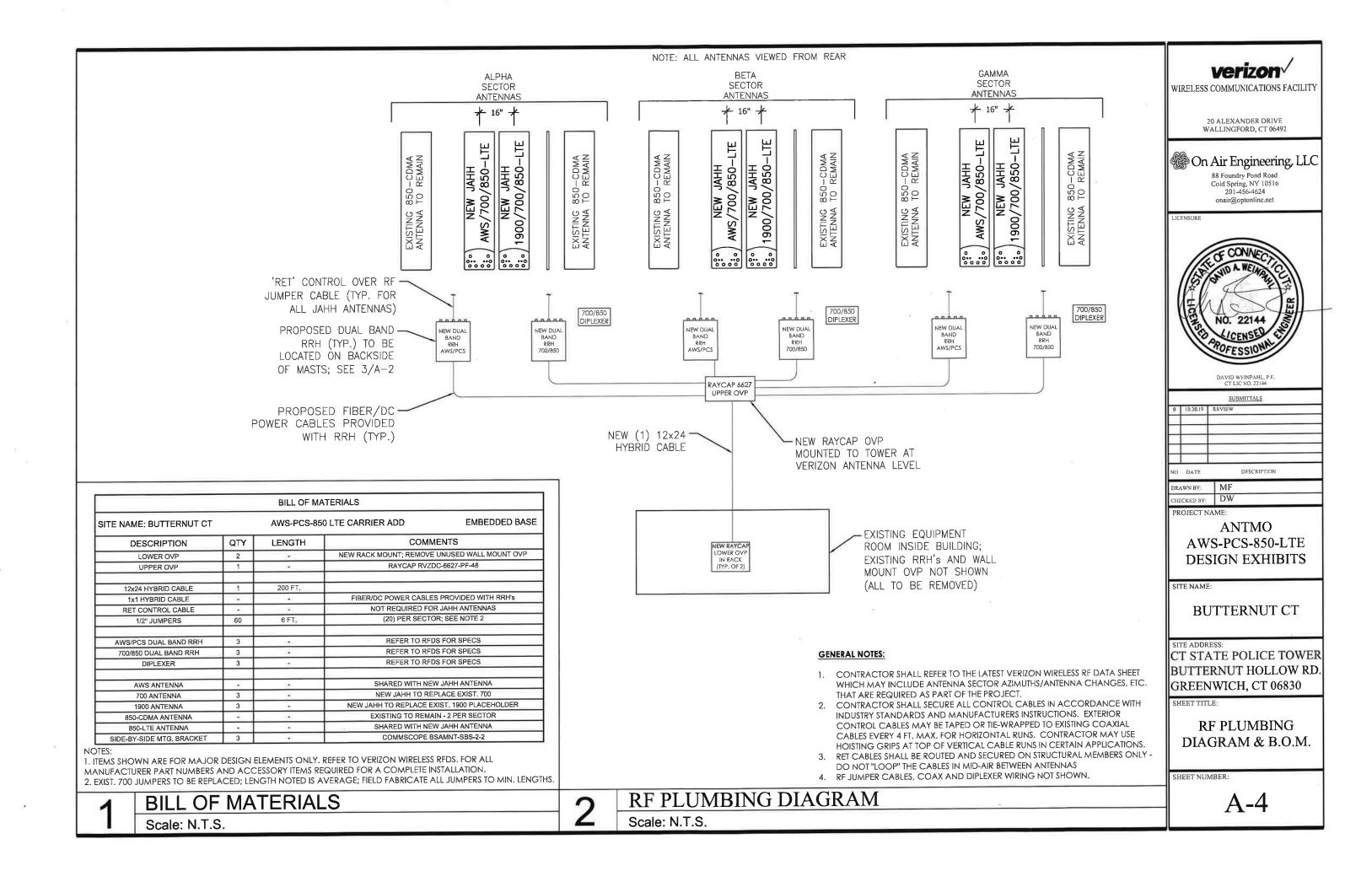
A-1

**COMPOUND PLAN** 

Scale: 1/16" = 1'-0"









8-port sector antenna, 2x 698–787, 2x 824-894 and 4x 1695–2360 MHz, 65° HPBW, 3x RET and low bands have diplexers. Internal SBT's on first LB (Port 1) and first HB(Port 5).

- Internal SBT on low and high band allow remote RET control from the radio over the RF jumper cable
- One RET for 700MHz, one RET for 850MHz, and one RET for both high bands to ensure same tilt level for 4x Rx or 4x MIMO
- Internal filter on low band and interleaved dipole technology providing for attractive, low wind load mechanical package
- Separate RS-485 RET input/output for low and high band

#### **Electrical Specifications**

Frequency Band, MHz	698–787	824-894	1695-1880	1850-1990	1920-2200	2300-2360
Gain, dBi	14.5	15.8	18.0	18.4	18.5	18.8
Beamwidth, Horizontal, degrees	67	65	63	63	65	68
Beamwidth, Vertical, degrees	12.4	10.5	5.7	5.2	4.9	4.4
Beam Tilt, degrees	2-14	2-14	0–10	0–10	0-10	0–10
USLS (First Lobe), dB	18	18	20	20	21	23
Front-to-Back Ratio at 180°, dB	32	34	31	35	36	38
Isolation, Cross Polarization, dB	25	25	25	25	25	25
Isolation, Inter-band, dB	30	30	30	30	30	30
VSWR   Return Loss, dB	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0	1.5   14.0
PIM, 3rd Order, 2 x 20 W, dBc	-153	-153	-153	-153	<b>-</b> 153	-153
Input Power per Port at 50°C, maximum, watts	200	200	300	300	300	250
Polarization	±45°	±45°	±45°	±45°	±45°	±45°
Impedance	50 ohm	50 ohm				

#### Electrical Specifications, BASTA\*

Frequency Band, MHz	698-787	824-894	1695–1880	1850–1990	1920-2200	2300-2360
Gain by all Beam Tilts, average, dBi	14.3	14.9	17.6	18.1	18.2	18.5
Gain by all Beam Tilts Tolerance, dB	±0.3	±0.5	±0.6	±0.4	±0.5	±0.6
	2 °   14.3	2 °   15.0	0 °   17.2	0° 17.6	0 °   17.7	0 9   17.9
Gain by Beam Tilt, average, dBi	8°   14.3	8° 14.9	5° 17.6	5° 18.2	5° 18.3	5 0   18.7
,,,,,,,	14 °   14.3	14 °   15.4	10 °   17.6	10 °   18.2	10 °   18.3	10 0 [ 18.7
Beamwidth, Horizontal Tolerance, degrees	±1.2	±1.4	±4	±2.4	±2.9	±2.7
Beamwidth, Vertical Tolerance, degrees	±0.9	±0.5	±0.3	±0.2	±0.3	±0.1
USLS, beampeak to 20° above beampeak, dB	18	17	17	18	19	18
Front-to-Back Total Power at 180° ± 30°, dB	25	24	26	29	27	29
CPR at Boresight, dB	22	23	20	21	21	24
CPR at Sector, dB	11	12	11	11	11	8

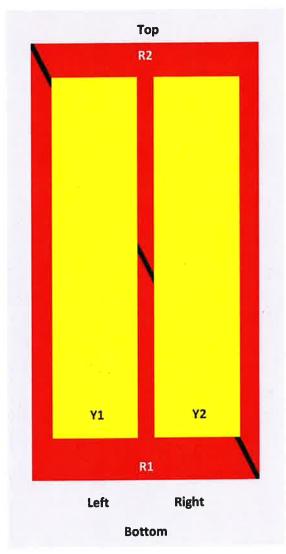
<sup>\*</sup> CommScope® supports NGMN recommendations on Base Station Antenna Standards (BASTA). To learn more about the benefits of BASTA, download the whitepaper Time to Raise the Bar on BSAs.

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#### Array Layout

#### JAHH-65A-R3B JAHH-65B-R3B JAHH-65C-R3B



Array	Freq (MHz)	Conns	RET (SRET)	AISG RET UID
RI	698-798	1-2	1	ANxxxxxxxxxxxxXX
R2	824-894	3-4	2	ANaxanaxaxxxxxxxxxx2
Yl	1695-2360	5-6	3	ANxxxxxxxxxxxxxxxxx
Y2	1695-2360	7-8		

View from the front of the antenna

(Sizes of colored boxes are not true depictions of array sizes)

General Specifications

**Operating Frequency Band** 

1695 – 2360 MHz | 698 – 787 MHz | 824 – 894 MHz

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#### JAHH-65B-R3B

**Antenna Type** 

Sector

**Band** 

Multiband

**Performance Note** 

Outdoor usage | Wind loading figures are validated by wind tunnel measurements

described in white paper WP-112534-EN

Mechanical Specifications

RF Connector Quantity, total 8
RF Connector Quantity, low band 4
RF Connector Quantity, high band 4

RF Connector Interface 4.3-10 Female
Color Light gray

**Grounding Type**RF connector body grounded to reflector and mounting bracket

Radiator Material Aluminum | Low loss circuit board

Radome Material Fiberglass, UV resistant

Reflector MaterialAluminumRF Connector LocationBottom

 Wind Loading, frontal
 301.0 N @ 150 km/h | 67.7 lbf @ 150 km/h

 Wind Loading, lateral
 254.0 N @ 150 km/h | 57.1 lbf @ 150 km/h

 Wind Loading, maximum
 143.4 lbf @ 150 km/h | 638.0 N @ 150 km/h

Effective Projected Area (EPA), frontal0.28 m² | 3.01 ft²Effective Projected Area (EPA), lateral0.24 m² | 2.58 ft²Wind Speed, maximum241 km/h | 150 mph

Dimensions

 Length
 1828.0 mm
 72.0 in

 Width
 350.0 mm
 13.8 in

 Depth
 208.0 mm
 8.2 in

 Net Weight, without mounting kit
 29.2 kg
 64.4 lb

Remote Electrical Tilt (RET) Information

Input Voltage 10–30 Vdc
Internal Bias Tee Port 1 | Port 5

Internal RET High band (1) | Low band (2)

Power Consumption, idle state, maximum  $2~\mathrm{W}$  Power Consumption, normal conditions, maximum  $13~\mathrm{W}$ 

Protocol 3GPP/AISG 2.0 (Single RET)

**RET Interface** 8-pin DIN Female | 8-pin DIN Male

RET Interface, quantity 2 female | 2 male

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#### JAHH-65B-R3B

#### Packed Dimensions

1975.0 mm | 77.8 in Length 456.0 mm | 18.0 in Width

357.0 mm | 14.1 in Depth

42.5 kg | 93.7 lb **Shipping Weight** 

#### Regulatory Compliance/Certifications

**Agency** 

Classification

RoHS 2011/65/EU ISO 9001:2015

Compliant by Exemption

Designed, manufactured and/or distributed under this quality management system China RoHS SJ/T 11364-2014

Above Maximum Concentration Value (MCV)







#### Included Products

BSAMNT-3 — Wide Profile Antenna Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members. Kit contains one scissor top bracket set and one bottom bracket set.

#### \* Footnotes

**Performance Note** 

Severe environmental conditions may degrade optimum performance

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### **SAMSUNG**

# Dual-Band Radio Unit 700/850MHz (B13/B5)

RFV01U-D2A

Samsung's RFV01U-D2A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D2A RU targets dual-band support across Band 13 (700MHz) and Band 5 (850MHz), making it an ideal product for broad coverage footprints across multiple common low-end, long-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributed-and central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

#### Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- · Convection cooled, silent operation

#### **Key Technical Specifications**

Duplex Type: FDD Operating Frequencies:

B13: DL(746-756MHz)/UL(777-787MHz) B5: DL(869-894MHz)/UL(824-849MHz) Instantaneous Bandwidth: 10MHz(B13) + 25MHz(B5)

RF Chain: 4T4R/2T4R/2T2R Output Power: Total 320W DU-RU Interface: CPRI (10Gbps) Dimensions: 380 x 380 x 207mm (29.9L)

Weight: 31.9kg

Input Power: -48V DC

Operating Temp.: -40 - 55°(w/o solar load)

Cooling: Natural convection

### **SAMSUNG**

### Dual-Band Radio Unit AWS/PCS (B66/B2)

RFV01U-D1A

Samsung's RFV01U-D1A is a compact remote Radio Unit (RU) designed for deployments that require flexibility in installation and rapid onlining, without compromising on coverage, capacity or operational expenses.



The RFV01U-D1A RU targets dual-band support across Band 66 (AWS) and Band 2 (PCS), making it an ideal product for broad coverage footprints across multiple common mid-range frequencies.

The RU handles all Radio Frequency (RF) processing in a single, compact unit, and is designed to interface via CPRI with Samsung's CDU baseband offerings, in both distributed-and central-RAN configurations.

In addition to its minimal footprint and ease of installation, the RU is also designed to reduce cost of ownership through its integrated spectrum analyzer, which allows for remote RF monitoring, greatly reducing the need for on-site maintenance visits.

#### Features and Benefits

- Dual-band support for broad frequency coverage
- Minimal footprint reduces site costs
- Rapid, easy installation
- Flexibly deployable in any location
- Remote RF monitoring capability
- Convection cooled, silent operation
- Built-in Broadcast Auxiliary Services (BAS) filter ensures compliant AWS operation without impacting footprint

#### Key Technical Specifications

Duplex Type: FDD Operating Frequencies:

B66: DL(2,110-2,180MHz)/UL(1,710-1,780MHz) B2: DL(1,930-1,990MHz)/UL(1,850-1,910MHz)

Instantaneous Bandwidth:

70MHz(B66) + 60MHz(B2)

RF Chain: 4T4R/2T4R/2T2R

Output Power: Total 320W DU-RU Interface: CPRI (10Gbps)

Dimensions: 380 x 380 x 255mm (36.8L)

Weight: 38.3kg

Input Power: -48V DC

Operating Temp.: -40 - 55°(w/o solar load)

Cooling: Natural convection

# **ATTACHMENT 3**

	General	I OMOL	- Annual					
Site Name: Butternut (Greenwich) Towar Height: 180Et								
lower neight.				CALC.		MAX.		
CARRIER	# OF CHAN.	WATTS ERP	HEIGHT	POWER DENS	FREQ.	PERMISS. EXP.	FRACTION	Total
*State Police	1	1000	180	866.0125	0.0119	0.5773	0.21%	
*Greenwich	1	1000	180	866.7875	0.0119	0.5779	0.21%	
*DOT	1	100	180	42.8	0.0012	0.2000	%90'0	
*Greenwich	1	432	177	18700	0.0053	1.0000	0.05%	
∩N*	1	20	150	928	0.0009	0.6187	0.01%	
nN∗	1	316	150	150	0.0055	0.2000	0.27%	
*NU	1	100	80	37.8	0.0066	0.2000	0.33%	
*NU	1	555	165	944	0.0079	0.6293	0.13%	
*NU	1	316	150	450	0.0055	0.3000	0.18%	
*NU	1	100	130	47.86	0.0023	0.2000	0.12%	
*State Police	1	56	176	0029	0.0007	1.0000	0.01%	
*T-Mobile	2	2334	137	2100	0.0978	1.0000	%86.0	
*T-Mobile	2	2334	137	1900	0.0978	1.0000	0.98%	
*T-Mobile	2	1167	137	2100	0.0489	1.0000	0.49%	
*T-Mobile	2	1167	137	1900	0.0489	1.0000	0.49%	
*T-Mobile	2	1167	137	1900	0.0489	1.0000	0.49%	
*T-Mobile	2	620	137	009	0.0260	0.4000	0.65%	
*T-Mobile	2	629	137	700	0.0285	0.4667	0.61%	
*Sprint	1	438	117	850	0.0128	0.5667	0.23%	
*Sprint	5	623	117	1900	0.0909	1.0000	0.91%	
*Sprint	2	1556	117	1900	0.0908	1.0000	0.91%	
*Sprint	80	640	117	2500	0.1494	1.0000	1.49%	
*Sprint	2	1081	117	850	0.0631	0.5667	1.11%	
*AT&T	2	424	148	850	0.0151	0.5667	0.27%	
*AT&T	2	929	148	1900	0.0234	1.0000	0.23%	
*AT&T	3	585	148	700	0.0313	0.4667	%29.0	
*AT&T	4	1222	148	1900	0.0872	1.0000	0.87%	
*AT&T	2	424	148	850	0.0151	0.5667	0.27%	
VZW PCS	4	1525	130	0.1298	1970	1.0	12.98%	
VZW Cellular	3	498	130	0.0318	880	0.5793	5.49%	
VZW Cellular	4	355	130	0.0302	869	0.5866	5.15%	
VZW AWS	4	1493	130	0.1271	2145	1.0	12.71%	
VZW 700	4	628	130	0.0534	746	0.4973	10.75%	
VZW CBRS	0	31	130	0.000	3550	2.36	%00'0	
								60.29%
* Course Caristian Course								

## **ATTACHMENT 4**



Submitted to Empire Telecom USA, LLC 16 Esquire Road Billerica, MA 01862

Airosmith Development, Inc. 32 Clinton Street Saratoga Springs, NY 12866

Northeast Site Solutions 199 Brickyard Road Farmington, CT 06032

Verizon Wireless 20 Alexander Drive, 2<sup>nd</sup> Floor Wallingford, CT Submitted by AECOM 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 July 31, 2019

DETAILED STRUCTURAL
ANALYSIS AND MODIFICATION
OF AN EXISTING 180' SELF
SUPPORTING LATTICE TOWER
WITH STACK-N-BOLT SYSTEM
AND FOUNDATION FOR
PROPOSED ANTENNA
ARRANGEMENT

AT&T Site No.:

CT2129

Sprint Site No. : T-Mobile Site No. : CT03XC343 CT11070B

Verizon Site No.: Butternut, CT

Site Name : Site Address: Connecticut State Police Tower #74

150 Butternut Hollow Road

CSP Tower # 74

60537397 Revision #4

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#### 1. EXECUTIVE SUMMARY

This report summarizes the controlling load case structural analysis and evaluation of the 180' dual lattice tower, comprised of an exterior tower and an interior tower, located off of Butternut Hollow Road in Greenwich, Connecticut.

The structural analysis was conducted in accordance with the 2018 Connecticut State Building Code which includes the TIA-222-G¹ Standard, 2015 International Building Code, the 2018 Connecticut State Building Code Amendments, the AISC² Load Resistance Factor Design (LRFD), the ASCE 7³ design Code, and the Connecticut State Police Requirements which include the TIA/EIA-222-F⁴.

The antenna loading considered in the analysis consists of all the existing antennas, transmission lines and ancillary items as outlined in the Introduction Section of this report.

The proposed antenna modifications are listed below:

The proposed antenna modifications are listed be	FIQVV.	
Proposed Antenna, Mounts & Cables	Carrier	Antenna Center Elevation
Remove: (3) Windload Dishes	CSP (Existing)	@ 180'
(3) Powerwave P65-16-XLH-RR Panel Antennas	AT&T (Existing)	@ 148'
(3) EMS RR90-17-02DP Panel Antennas (3) GSM TMA Units	T-Mobile (Existing)	@ 136'
(3) Swedcom SLCP 2x6014 Panel Antennas (3) Amphenol BXA-171063-8BF Panel Antennas (3) Commscope HBXX6516DS-A2M Panel Antennas (6) Commscope HBXX6517DS-A2M Panel Antennas (9) 1-5/8" Coaxial Cables (1) (OVP Box) Distribution Box (1) Hybrid Cable	Verizon (Existing)	@ 126'
(3) CCI OPA-65R-LCUU-H6 Panel Antennas (3) Ericsson RRUS-32 B2 RRH Units	AT&T (Proposed)	@ 148'
(3) Ericsson AIR 21 B2A/B4P Panel Antennas (3) Ericsson AIR 32 B66A/B2A Panel Antennas (3) APXVSAA24_43-U-A20 Panel Antennas (3) (AWS) TMA Units (3) Ericsson 4478 B71 RRH Units (3) Ericsson RRUS-11 RRH Units (3) Generic 600/700 Diplexer Units (3) Ericsson Hybriflex Cable 6x12 Fiber Optic Cables	T-Mobile (Proposed)	@ 136'

Proposed Antenna, Mounts & Cables (Cont.)	Carrier	Antenna Center Elevation
(6) Commscope JAHH-65B-R3B-2DT Panel Antennas (3) BSAMNT-SBS-2-2 (JAHH Panel Antenna) Mounting Brackets (3) Samsung B2/B66a (RFV01U-D1A) RRH Units (3) Samsung B5/B13 (RFV01U-D2A) RRH Units (1) RFS DB-C1-12C-24AB-0Z Distribution Box (1) 1-5/8" O.D. Fiber Optic Cable (HB158-	Verizon (Proposed)	@ 126'
13U12S24-270-LI) (3) Commscope CBC78T-DS-43-2X Diplexer Units  (3) Commscope DT465B-2XR Panel Antennas (3) 2x50W (800MHz) RRH Units (3) TD-RRH8x20-25 RRH Units w/ Solar Shield (1) Hybrid Cable (1-1/4" O.D. Cable used for Analysis (3) Stiff-Arm Mount Support Attachments (1 per Sector) (SitePro1 Part # STK-U)	Sprint (Proposed)	@ 115'

The results of an initial assessment analysis indicated the existing exterior and interior tower structures did not have enough capacity for the proposed loading conditions. The existing tower structures require modifications shown on SK-1 through SK-5. Once the modifications indicated on sheets SK-1 through SK-5 are performed, the modified structures are considered structurally adequate with the wind load classification specified with the existing and proposed antenna loading. No installation of proposed antennas shall occur without the required modification being completed.

The results of the analysis indicate the modified tower's sway (deflection) is 0.65 degrees and the modified tower's twist (rotation) is 0.07 degrees. These figures are within the Connecticut State Police requirements of 0.75 degrees for combined twist (rotation) and sway (deflection) when applying the TIA/EIA-222-F design conditions.

<sup>1.</sup> TIA = Telecommunications Industry Association Structural Standard for Antenna Supporting Structures and Antennas (Version G)

<sup>2.</sup> AISC = American Institute of Steel Construction (14th Edition)

<sup>3.</sup> ASCE 7 = American Society of Civil Engineers Standard 7 (2010 Edition)

<sup>4.</sup> TIA/EIA = Telecommunications Industry Association Structural Standard for Antenna Supporting Structures and Antennas (Version F)

#### 1. **EXECUTIVE SUMMARY** (continued)

This analysis is based on:

- 1) The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- 2) Member sizes and tower geometry of the outer tower taken from manufacturers' drawings prepared by Rohn Industries, Inc., file number 28325, dated December 28, 1992.
- Member sizes and tower geometry of the inner tower taken from design calculations and drawings prepared by Towertek Industries Inc., signed and sealed May 9, 2002.
- Foundation modifications taken from drawings prepared by Walker Engineering Incorporated, Job number 0206-237R2, signed and sealed November 26, 2002.
- 5) Tower Mapping and Existing Inventory performed by D&K Nationwide Communications, Inc. on March 31, 2016
- 6) Previous structural analysis performed by AECOM on behalf of the Connecticut State Police, project # 60509756.08 / PNS-608, signed and sealed on September 6, 2016.
- Proposed antenna inventory Radio Frequency Data Sheet (RFDS) and contract drawings provided by AT&T, obtained via e-mail, dated May 5, 2017.
- 8) Proposed antenna inventory RFDS provided by T-Mobile, obtained via e-mail, dated, February 15, 2018, with a revision to proposed inventory obtained via e-mail dated March 26, 2018.
- 9) Proposed antenna inventory RFDS provided by Verizon Wireless, obtained via e-mail, dated March 18, 2019.
- 10) Proposed antenna inventory from site Construction Drawings, signed and sealed October 19, 2018, provided by Sprint, obtained via e-mail, dated July 31, 2019.
- 11) Antenna inventory as specified in section 2 and 6 of this report.

This report is only valid as per the information and data provided by others for antenna inventory, mounts, tower structure, existing foundation and associated cables. The user of this report shall field verify the antenna, cabling and mount configuration used, as well as the physical condition of the tower members, connections and foundations. Notify the engineer in writing immediately if any of the information in this report is found to be other than specified.

If you should have any questions, please call.

Sincerely,

AECOM,

Richard A. Sambor, P.E. Senior Structural Engineer

RAS/mcd

Cc: IA, CF/Book - AECOM

#### 2. INTRODUCTION

The subject tower is located off of Butternut Hollow Road in Greenwich, Connecticut. The original outer structure is a self-supporting three-legged 180' steel tapered lattice tower manufactured by Rohn Industries. A subsequent inner tower structure, a Stack-N-Bolt system, was installed inside the original tower and was designed by Towertek.

The structural analysis was conducted in accordance with the following:

- TIA-222-G Standard for Standard for a wind velocity of range of 90 mph to 110 mph (3-second gust) and 50 mph (3-second gust) concurrent with 0.75" ice thickness, considered to increase in thickness with height
- 2015 International Building Code with 2018 Connecticut State Building Code Amendments for a wind speed of 101 mph (3-second gust)
- 2010 AISC Load Resistance Factor Design (LRFD)
- 2010 ASCE 7 Minimum Design Loads for Buildings and Other Structures for the ice thickness referenced in the TIA-222-G Standard
- Connecticut State Police Requirements for a wind velocity of 90 mph (fastest mile) and 90 mph (fastest mile) concurrent with 0.5" ice. Twist (rotation) and sway (deflection) were determined in accordance with Connecticut State Police Requirements for a wind velocity of 90 mph (fastest mile) concurrent with 0.5" ice, analyzed under the TIA/EIA-222-F design Standard.

The existing structure supports numerous communication antennas. The inventory is summarized below:

Antenna Type	Carrier	Mount	Centerline Elevation / Leg	Cable
(1) Scala OGT9-806 (inverted) * (1) Sinclair SC479- HF1LDF (inverted) (1) TTA/Junction Box *	#27A,27B,27C CSP 2*,4&74* (existing)	3' Stand-Off	175 / B	(2) 1-5/8" (1) 3/8" *
(1) (inverted) Dipole Antenna	#26-A NEU – 20 (existing)	Shared with Above (Omni @ 175')	175 / A	(1) 7/8"
(1) Sinclair SC479- HF1LDF (inverted) (1) Junction Box	#26-B CSP – 67 (existing)	Shared with Above (Omni @ 175')	175 / A	(1) 1-5/8" (1) 1/2"
(1) PD-420 20' Dipole Antenna	#28D NEU – 55 (existing)	3' Stand-Off	174 / C	(1) 7/8"
(1) DB-583 Omni Antenna	#28C TOG – 5 (existing)	Shared with Above	174 / C	(1) 1-5/8"
(1) Scala OGT9-806N * (1) Sinclair SC479- HF1LDF	#28A,28B CSP - 1 * & 3 (existing)	3' Stand-Off	174 / C	(2) 1-5/8"

Antenna Type	Carrier	Mount	Centerline Elevation / Leg	Cable
(1) SC3-W100AC 3' Dish Antenna	#25 Greenwich Police Dep. (existing)	Dish Mount	, 168 / B	(1) Elliptical Cable
(1) Kathrine 197-501 Panel Antenna (1) TMA	#23 Stamford 64 & 65 (existing)	3' Arm	168 / A	(1) 1-5/8" (1) 1/2"
DB-586-Y	#22 TOG - 6 (existing)	Leg Mounted	165 / A	(1) 7/8"
8' (solid) Dish with Radome	#21 SPD - 9 (existing)	Dish Mount	160 / A	(1) EW90
(3) Sinclair SC-479- HF1LDF (1 upright, 2 inverted) (1) TMA	CSP 70 to 73 (reserve)	3' Stand-Off	160	(3) 1-5/8" (1) 1/2"
(1) Kathrine 197-501 Panel Antenna	#20 Unknown (existing)	3' Arm	159.5 / A	(1) 7/8"
(1) Kathrine 197-501 Panel Antenna	#19 Stamford 63 (existing)	3' Arm	159 / B	(1) 7/8"
(3) OPA-65R-LCUU-H6 Panel Antennas (3) RRUS-32 B2 RRH Units	AT&T (Proposed)	Shared with Below Mounts	147.5 / ABC	See Below Cables
(6) Powerwave 7770 (12) TMAs (6) Ericsson RRU (1) Raycap Surge Suppressor	AT&T (existing)	(3) Side Arm Mounts	147.5 / ABC	(12) 1-5/8" (1) Fiber Optic Cable (2) DC Cables
(1) Celwave PD1142	#15 CSP – 21 (existing)	3' Arm	137 / B	(1) 7/8"
(3) AIR 21 B2A/B4P Panels (3) AIR32 B66A/B2A Panels (3) APXVSAA24_43-U- A20 Panel Antennas (3) (AWS) TMA Units (3) 4478 B71 RRH Units (3) RRUS-11 RRH Units (3) Generic Diplexer (600/700)	T-Mobile (Proposed)	Shared with Below Mounts	136 / ABC	(3) 1-1/4" Hybriflex Cables (6x12)
	T-Mobile (existing)	Face Mounted	136 / ABC	(6) 1-5/8"

Antenna Type	Carrier	Mount	Centerline Elevation / Leg	Cable
(1) 6' Dipole Antenna	#12 unknown (existing)	3' Arm	135 / C	(1) 7/8"
(1) Kreco CO41AN	#11 NEU – 18 (existing)	Mounted on Below Frame	130 / A	(1) 1-5/8"
(6) JAHH-65B-R3B-2DT Panels (3) Samsung B2/B66a (RFV01U-D1A) RRH Units (3) Samsung B5/B13 (RFV01U-D2A) RRH Units (1) RFS DB-C1-12C- 24AB-0Z Distribution Box (3) Commscope CBC78T-DS-43-2X Diplexer Units	Verizon (Proposed)	(3) Mount Brackets for JAHH Panels Shared with Below Mounts	126 / ABC	(1) 1-5/8" Fiber Optic Cables
(6) Andrew DB844H80- XY Panels	Verizon (existing)	(3) Boom Gates (existing)	126 / ABC	(6) 1 5/8"
(1) Celwave PD1142	#9 DEP – 54 (existing)	3' Arm	122 / B	(1) 7/8"
(1) Celwave PD1142	#8 CSP – 66 (existing)	Share with (#9) 3' Arm	122 / B	(1) 7/8"
(3) DT465B-2XR Panels (3) 800 MHz RRH Units (3) TD-RRH 8x20-25 RRH Units	Sprint (Proposed)	(3) STK-U Stiff Arm Support to Below Mount	115 / ABC	(1) Hybriflex Cable
(3) APXVSPP18-C Panel Antennas (3) 800 MHz 2x50W RRH Units (3) 1900 MHz 4x45 RRH Units	Sprint (existing)	(3) 12' T-Arm Mount	115 / ABC	(3) Hybriflex Cables
(1) Celwave PD1142	#7 NEU – 17 (existing)	3' Stand-off	110 / A	(1) 7/8"
(1) Celwave PD1142	#5 NEU – 16 (existing)	6' Arm	82 / C	(1) 1-5/8"
(1) 10' Dipole	#4 DOT – 56 (existing)	3' Arm	65 / C	(1) 7/8"
(1) GPS	#3 Sprint - 69 (existing)	3' Arm	60 / C	(1) 7/8"

Antenna Type	Carrier	Mount	Centerline Elevation / Leg	Cable
(1) 4' Dipole Antenna	#1 Unknown (existing)	3' Arm	56 / A	(1) 7/8"
(1) GPS (TMG-26N)	#2 Verizon - 68 (existing)	3' Arm	54 / B	(1) 7/8"

<u>Notes:</u> Antenna elevations and ID numbering obtained from Tower Mapping and Existing Inventory via tower climb, performed by D&K Nationwide Communications, Inc. on March 31, 2016.

This structural analysis and evaluation of the communications tower was performed by AECOM on behalf of AT&T, Sprint, T-Mobile and Verizon Wireless (VZW). The purpose of this analysis was to investigate the structural integrity of the modified tower and existing foundation for existing and proposed antenna loads in compliance with the 2018 Connecticut State Building Code. This analysis was conducted to evaluate stress on the tower and the effect forces to the foundation of the tower resulting from existing and proposed antenna arrangements.

<sup>&</sup>quot; \* " indicated future decommissioning of CSP antennas

#### 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS

The structural analysis was done in accordance with, the TIA-222-G-Structural Standard for Antenna Towers and Antenna Supporting Structures and Antennas, the 2015 International Building Code with 2018 Connecticut State Building Code Amendments and the American Institute of Steel Construction (AISC) Manual of Steel Construction – Load Resistance Factor Design (LRFD)

The analysis was conducted using PLS-Tower (version 10.62) and used the following conditions for this tower review (following the TIA/EIA-222-G Standard):

- Structure Class 3 (Essential Communications)
  - NOTE: ASCE 7 and CT State Building Code Applied Risk Category 4 for design wind loads (see below)
- Topographic Category 3 (Tower location on top of hill rolling wind conditions considered)
  - Crest Height used for analysis: (approximate elevations listed below)
    - Tower Base Elevation = 350 feet
    - High point (2 mile Radius) = 560 feet (Ref. Round Hill West of Tower Site)
    - Low Point (2 mile Radius) = 212 feet (Ref. Near intersection of Grahampton Lane – South of Tower Site)
    - "H" = (Avg of High/Low) Base Elevation = 36 feet
- Exposure Class C (Open Terrain with scattered obstructions)
- Load Conditions:
  - Five load conditions were evaluated as shown which were compared to design stresses according to AISC and TIA-222-G Standard. The load conditions apply TIA-222-G load combinations from Section 2.3.2 (shown at the end of this section)

#### Basic Wind Speed:

- TIA-222-G:
  - Fairfield County (Wind Speed Range): V = 90 mph 110 mph (3-second gust)
     [Annex of TIA/EIA-222-G 2006]
- IBC 2015 w/ 2018 CT State Building Code Amendment:
  - (2015) IBC Section 1609.1.1 Determination of Wind Loads Exception 5 "Designs using TIA-222" applies for determination of Design Wind Load obtained as "V.ult" are to be converted to "V.asd" when applying the TIA-222-G design Standard (under Section 1609.3) for Basic Wind Speed.
  - (2018) CT State Building Code Amendment to the IBC Section 1609.3 wind loads are obtained from Appendix N of the State Building Code.
    - V.asd = 101 mph (3-Second Gust) Wind Design Parameter for the <u>Town of Greenwich</u>, <u>Connecticut</u> for Risk Category four (IV) for essential communications (Connecticut State Police).

Ice thickness used for this analysis is **0.75 inch** (assumed to start at the base of the tower) and is considered to increase in thickness with height. The initial ice thickness for design is referenced in the Annex of TIA-222-G and follows the same design criteria as the ASCE 7 Standard.

The below load condition implements the design requirements of the Connecticut State Police for the tower structures deflection limits with the allowable deflection limit of the combination of the tower's sway (deflection) and twist (rotation) under the TIA-222-F design Standard. This design limit required the design combined value of sway (deflection) and twist (rotation) to be under 0.75 degrees following the TIA-222-F design Standard.

Load Condition (TIA-222-F) = 90 mph (fastest mile) Wind Load (with ice) + Ice Load + Tower Dead Load

#### 3. ANALYSIS METHODOLOGY AND LOADING CONDITIONS (cont.)

Seismic event consideration factors/values for design (and are applied into the PLS-Tower design outputs – see below load combination):

- S.s = 0.259 (2018 CT State Building Code Location Specific Value)
- S.1 = 0.070 (2018 CT State Building Code Location Specific Value)
- Seismic Design Category = "C" (2015 International Building Code)
- F.a = 1.6 (Obtained from TIA-222-G Table 2-12 Considering above conditions)
- F.v = 2.4 (Obtained from TIA-222-G Table 2-13 Considering above conditions)

Strength Limit State Load Combinations (TIA-222-G Section 2.3.2):

The structural analysis herein has considered the following load combinations within the analysis:

- 1. 1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.6 Wind load without ice
- 0.9 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.6 Wind load without ice
- 1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.0 Dead weight of ice due to factored ice thickness + 1.0 Concurrent wind load with factored ice thickness + 1.0 Load effects due to temperature
- 1.2 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.0 Earthquake Load
- 0.9 Dead Load Tower structure + 1.0 Dead Load Guy Assemblies + 1.0 Earthquake Load
- NOTE 1: The above **bolded** load combination is considered to create the governing design loads per the results of the analysis.
- NOTE 2: The above "Dead Load Guy Assemblies" are not considered as part of the analysis and are considered as a value of zero.
- NOTE 3: The "Load effects due to temperature" do not apply for structures that are self-sustaining (from the TIA-222-G Standard)

#### 4. FINDINGS AND EVALUATION

The combined axial and bending stresses on the tower structure were evaluated to compare with the strength design in accordance with AISC (LRFD). The results of an initial analysis indicated that the existing exterior and interior tower structures did not have enough capacity to support the proposed loading conditions. The tower structure requires modifications shown on SK-1 through SK-5. Once the modifications indicated on sheets SK-1 through SK-5 are performed, the modified structure and existing foundation are considered structurally adequate with the wind load specification and with the existing and proposed antenna loading included herein.

The existing dual lattice tower's sway (deflection) is 0.65 degrees, and the existing tower's twist (rotation) is 0.07 degrees. The figures combined ARE within the Connecticut State Police requirement of 0.75 degrees for combined twist and sway.

See the below tables for tower capacity and tower deflection (sway) and rotation (twist) figures:

#### Tower Twist & Sway 90 mph concurrent with ice (TIA-222-F Condition):

Component	Allowable	Actual	
Twist	0.75°	0.07°	
Sway	0.75	0.65°	

#### Proposed Tower Component Stress vs Capacity Summary (TIA-222-G Condition):

Component	Component Size	Controlling Member	Stress (% Capacity)	Pass/Fail
Rohn Diagonal	L3-1/2x3-1/2x1/4	Rohn-DF42	96.34	Pass
Rohn Leg	Rohn 6 EH (Extra Heavy)	Rohn-LG2P	91.06	Pass
Rohn Horizontal	L1-3/4x1-3/4x3/16	Rohn-H2P	16.10	Pass
Rohn Flange Bolts	(6) 1" Diameter A325 Bolts – Tension	Rohn-LH21	84.15	Pass
Interior Tower Diagonal	L6x6x3/8	SNB-DI42	95.44	Pass
Interior Tower Leg	Pipe 8 SCH 80 (Extra Strong)	SNB-LH2P	97.93	Pass
Interior Tower Horizontal	Pipe 4"x0.494" (Pipe 4 XXS)	SNB-H9cP	3.85	Pass
Interior Flange Bolts	(6) 1" Diameter A325 Bolts – Tension	SNB-LG21	96.67	Pass
Tower-to-Tower Connection	A325 Bolt	3/4" Bolt	67.7	Pass
Foundation	36.5' Square	Overturning Moment Resistance	93.8	Pass
Foundation	36.5' Square	Soil Bearing Resistance	72.3	Pass
Foundation	36.5' Square	Punching Shear Capacity	78.9	Pass
Foundation	36.5' Square	Foundation Flexure Capacity	91.4	Pass

Structure Rating (Maximum from all components) =	97.93 %	Pass

#### 5. CONCLUSIONS

The results of an initial assessment analysis indicated the existing Exterior and Interior tower structures did not have enough capacity for the proposed loading conditions. The existing tower structures require modifications shown on SK-1 through SK-5. Once the modifications indicated on sheets SK-1 through SK-5 are performed, the modified structures are considered structurally adequate with the wind load classification specified with the existing and proposed antenna loading. No installation of proposed antennas shall occur without the required modification being completed.

The results of the analysis indicate the modified tower's sway (deflection) is 0.65 degrees and the modified tower's twist (rotation) is 0.07 degrees. These figures are within the Connecticut State Police requirements of 0.75 degrees for combined twist (rotation) and sway (deflection) when applying the TIA/EIA-222-F design conditions.

#### Limitations/Assumptions:

This report is based on the following:

- A. Tower is properly installed and maintained.
- B. All members and their geometry are as specified in the original manufacturer drawings and are in good condition.
- C. All required members are in place.
- All bolts are in place and are properly tightened.
- E. Tower is in plumb condition.
- All member protective coatings are in good condition.
- G. All tower members were properly designed, detailed, fabricated, installed, and have been properly maintained since erection.
- H. Foundations are in good condition without defect and were properly constructed to support original design loads as specified in the original design documents.

AECOM is not responsible for any modifications completed prior to or hereafter in which AECOM is not or was not directly involved. Modifications include but are not limited to:

- A. Adding antennas
- B. Removing/replacing antennas
- C. Adding coaxial cables

AECOM hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations, and conclusions are based upon information contained and set forth herein. If you are aware of any information which conflicts with that which is contained herein, or you are aware of any defects arising from original design, material, fabrication, or erection deficiencies, you should disregard this report and immediately contact AECOM. AECOM disclaims all liability for any representation, recommendation, or conclusion not expressly stated herein.

### Ongoing and Periodic Inspection and Maintenance:

After the Contractor has successfully completed the installation and the work has been accepted, the owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA-222-G Section 14.2 for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at least yearly and more frequently as conditions warrant. It is also recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.

6. ANALYSIS DATA

**TOWER REINFORCEMENT DRAWINGS SK-1 THROUGH SK-5** 

## GENERAL CONSTRUCTION NOTES

- ALL WORK SHALL COMPLY WITH THE CONNECTICUT STATE BUILDING AND LIFE SAFETY CODES, SUPPLEMENTS AND AMENDMENTS.
- CONTRACTOR IS TO REVIEW ALL DRAWINGS AND NOTES IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUB—CONTRACTORS AND ALL RELATED PARTIES. THE SUB—CONTRACTORS SHALL PROVIDED AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD—OUT WITH ALL FINISHES, STRUCTURAL MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON DRAWINGS OR WRITTEN IN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION AND ELECTRICAL SUB-CONTRACTORS SHALL PAY FOR THEIR DEPOLITS
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS ON SITE AT ALL TIMES AND ENSURE THE DISTRIBUTION OF NEW DRAWINGS TO SUB-CONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. CONTRACTOR SHALL FURNISH 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- 7. INSTALLATION OF THIS WIRELESS COMMUNICATIONS EQUIPMENT SITE REQUIRES WORK IN THE IMMEDIATE VICINITY OF EXISTING OPERATING TELECOMMUNICATION SYSTEMS. THE CONTRACTOR SHALL PROVIDE AND COORDINATE THE METHODS OF PROTECTION WITH THE VARIOUS TELECOMMUNICATION CARRIERS AND THE TOWER OWNER. THERE SHALL BE NO INTERRUPTION OF OPERATION WITHOUT TIMELY COORDINATION WITH AND APPROVAL BY THE VARIOUS COMMUNICATIONS OPERATORS INCLUDING THE CONNECTICUT STATE POLICE.
- 8. THE REINFORCEMENT OF PORTIONS OF THIS TOWER STRUCTURE WILL AFFECT CRITICAL CONNECTICUT STATE POLICE ANTENNAS.
- NO MOVEMENT, ALTERATION, OR DISCONNECTION OF CONNECTICUT STATE POLICE ANTENNAS MAY OCCUR WITHOUT THE NOTIFICATION AND APPROVAL OF THE CONNECTICUT STATE POLICE. CONTACT THE NETWORK CONTROL CENTER AT 850-865-8008.
- 10. TOWER REINFORCING WORK AFFECTING CRITICAL CONNECTICUT STATE POLICE ANTENNAS MAY BE REQUIRED TO BE CONDUCTED AT TIMES AS DETERMINED BY THE REQUIREMENTS OF THE CONNECTICUT STATE POLICE.

- 11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUB-CONTRACTORS FOR ANY CONDITION PER MFR'S RECOMMENDATIONS, CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR ARCHITECT.
- 12. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON—SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ARCHITECT FOR REVIEW. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTAL TO THE ARCHITECT FOR REVIEW.
- 14. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA SUBMIT ANY DISCREPANCIES FROM THE DRAWINGS TO THE ARCHITECT.
- 15. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURE AND ITS COMPONENT PARTS DURING CONSTRUCTION, THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- 16. CONTRACTOR TO CONTACT "CALL BEFORE YOU DIG" AT 1-800-922-4455 TO VERIFY AND IDENTIFY THE EXACT LOCATIONS OF ALL UNDERGROUND UTILITIES AND OBSTRUCTIONS IDENTIFIED PRIOR TO COMMENCING WORK IN THE CONTRACT
- 17. CONTRACTOR SHALL COMPLY WITH OWNER ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.
- 18. DIMENSIONS OF EXISTING TOWER ARE BASED ON MANUFACTURER'S DRAWINGS PREPARED BY ROHN INDUSTRIES, INC., DATED DECEMBER 1992, AND ARE NOT GUARANTEED. CONTRACTOR SHALL TAKE FIELD DIMENSIONS AS NECESSARY TO ASSURE PROPER FIT OF ALL FINISHED WORK AND SHALL ASSUME FULL RESPONSIBILITY FOR THEIR ACCURACY. WHEN SHOP DRAWINGS BASED ON FIELD MEASUREMENT ARE SUBMITTED FOR REVIEW, DIMENSIONS ARE PROVIDED FOR THE ENGINEER'S REFERENCE ONLY
- 19. TOWER INVENTORY IS BASED ON INFORMATION OBTAINED BY CONNECTICUT STATE POLICE DATED APRIL 12, 2016. TOWER MAPPING AND EXISTING INVENTORY OBTAINED FROM D&K NATIONWIDE COMMUNICATIONS, INC. DATED MAPCH 2, 2018.
- 20. CONTRACTOR TO VERIFY REQUIRED CLEARANCES INCLUDING BUT NOT LIMITED TO EXISTING BUILDINGS, EQUIPMENT PADS AND SHELTERS PRIOR TO COMMENCING WORK.
- THE CONTRACTOR IS RESPONSIBLE FOR THE STABILITY OF THE STRUCTURE DURING CONSTRUCTION. NO MEMBER OF THE TOWER SHALL BE LEFT DISCONNECTED FOR THE NEXT WORKING DAY. THE CONTRACTOR SHALL BE AWARE OF WEATHER AND WIND CONDITIONS AND NOT PERFORM MEMBER REPLACEMENT IN A WIND.

## STRUCTURAL NOTES

STRUCTURAL STEEL MATERIAL

ALL STRUCTURAL STEEL MEMBERS AND HSS TUBING USED FOR REINFORCING SHALL
BE MINIMUM 50 KSI WITH THE BELOW EXCEPTIONS:
ANGLE SIZE 2-1/2"×2-1/2"×3/16" AND SMALLER
STRUCTURAL PLATES
A36

STRUCTURAL STEEL SHALL CONFORM TO ALL THE REQUIREMENTS OF THE ASTM SPECIFICATION, AS REFERENCED IN THE CODE.

UNLESS OTHERWISE NOTED, ALL STEEL WILL BE GALVANIZED IN ACCORDANCE WITH ASTM 123 AFTER FABRICATION. TOUCH UP ALL DAMAGED GALVANIZED STEEL WITH APPROVED COLD ZINC, "GALVANOX", "DBY GALV", "ZINC-IT", OR APPROVED EQUIVALENT, IN ACCORDANCE WITH MANUFACTURERS GUIDELINES. TOUGH-UP DAMAGED NON GALVANIZED STEEL WITH SAME PAINT APPLIED IN SHOP OR FIELD.

SHOP AND ERECTION DRAWINGS SHALL BE SUBMITTED FOR ALL STRUCTURAL STEEL WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. SUBMIT 2 SETS OF PRINTS FOR THE ENGINEER REVIEW.

MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.

THE OMISSION OF ANY MATERIAL THAT WAS SHOWN ON THE CONTRACT DRAWINGS SHALL NOT RELIEVE THE CONTRACTOR OF PROVIDING THE SAME.

### CONNECTIONS / FIELD ASSEMBLY:

BOLTED CONNECTIONS: UNLESS OTHERWISE NOTED, ALL JOINTS ARE SLIP CRITICAL TYPE, REQUIRING 5/8" & 3/4" DIA. A325-N & A490-X BOLTS, A563 NUTS AND F435 WASHERS. ALL GALVANIZED. BEVELED WASHERS SHALL BE USED ON BEAM FLANGES HAVING A SLOPE GREATER THAN 1:20.

STRUCTURE IS DESIGNED TO BE LEVEL AND PLUMB, SELF-SUPPORTING AND STABLE AFTER WORK IS COMPLETED.

COMMENCEMENT OF WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.

SPECIAL INSPECTIONS ARE REUGH...

OWNER WILL SUPPLY THE SERVICES OF A SPECIAL...
AS REQUIRED, CONTRACTOR SHALL COORDINATE INSPECTIONS ...
ERECTOR'S WORK AND MATERIALS TO MEET THE REQUIREMENTS OF THE OF SPECIAL INSPECTIONS FOR THIS PROJECT.

COPIES OF TESTING AND INSPECTION REPORTS WILL BE PROVIDED TO THE OWNER, BUILDING OFFICIAL, ENGINEER OF RECORD AND CONTRACTOR. No. 9057
CENSE CHARMING

PROJECT NO. 60537397

Designed by:

GAT ICA Approved by: Δ=COM

500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT (880)-529-8882



vertzon

4 07/31/19 RE-ISSUED/NO CHANGE 3 10/11/18 RE-ISSUED 2 10/03/18 RE-ISSUED DESCRIPTION DATE: REV.

SK-1

Scale: AS NOTED Date: 03/20/18

File No Job No.

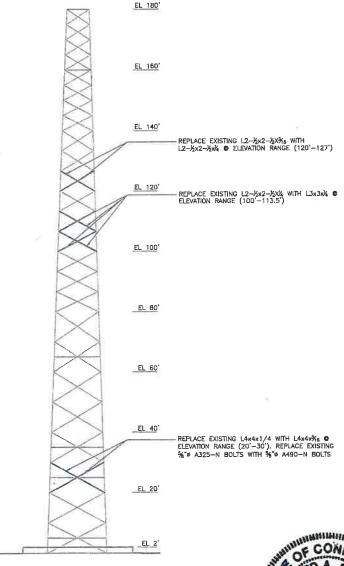
Dwg. 1 of 5

SITE ADDRESS:

BUTTERNUT HOLLOW ROAD **GREENWICH, CONNECTICUT 06831** 

- NOTES:

  1. REFER TO STRUCTURAL NOTES ON SK-1 FOR STEEL GRADE REQUIREMENTS FOR REPLACEMENT MEMBERS,
  2. REINFORCEMENT OF TOWER IS REQUIRED FOR ALL 3 SIDES OF EXISTING EXTERIOR TOWER STRUCTURE.
  3. CONNECTION BOLTS THAT ARE REMOVED DURING MEMBER REPLACEMENT SHALL BE REPLACED IN KIND, UNLESS NOTED OTHERWISE. EXISTING BOLTS SHALL NOT BE RE-USED FOR CONNECTING REPLACEMENT MEMBERS.
  4. CONTRACTOR SHALL COORDINATE WITH ROHN INC. FOR INDICATED TOWER REPLACEMENT MEMBERS AS SHOWN.
  5. CONTRACTOR SHALL VERIFY INCREMENTON SHOWN ON THIS SHEET PRIOR TO ORDERING MATERIALS.
  6. THE BOTTOM 2 FEET OF THE TOWER'S LEGS AND DIAGONAL MEMBERS ARE ENCASED IN CONCRETE, PART OF A PREVIOUS FOUNDATION MODIFICATION.







Checked by: ICA

**AECOM** 

**500 ENTERPRISE DRIVE** ROCKY HILL, CONNECTICUT (860)-528-8882



Sprint 🥍 ..T. Mobile Verizon



4	07/31/19	RE-ISSUED/NO CHANGE
3	10/11/18	RE-ISSUED
2	10/03/18	RE-ISSUED
REV.	DATE:	DESCRIPTION

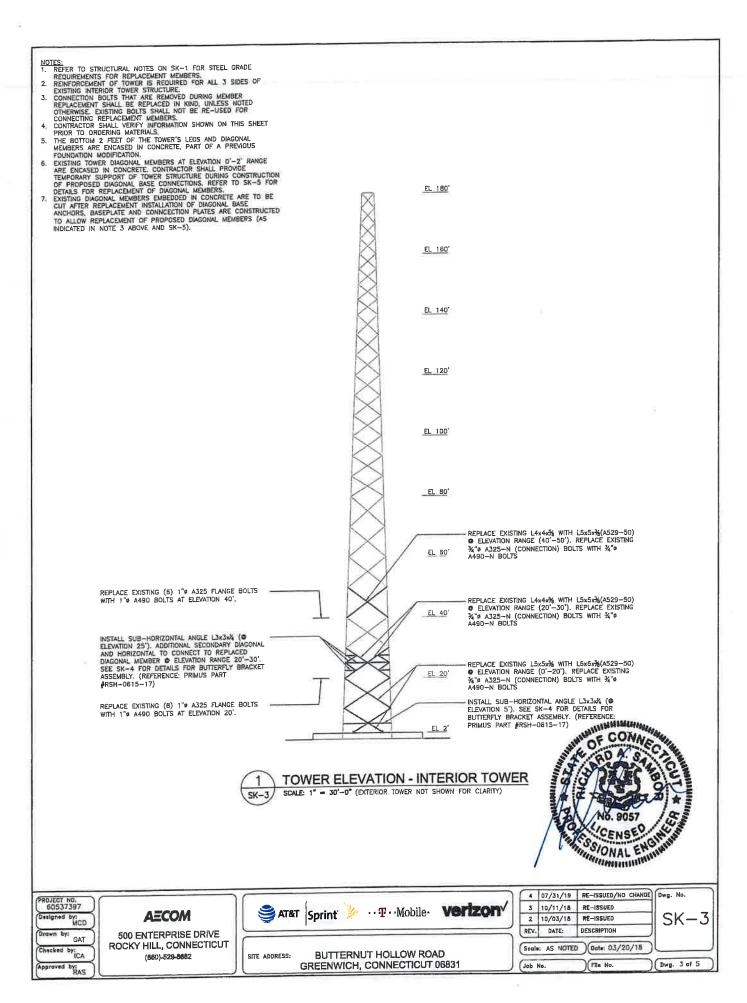
Dwg. No. SK-2

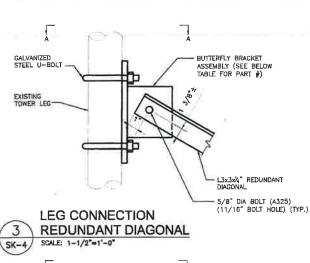
SITE ADDRESS:

**BUTTERNUT HOLLOW ROAD GREENWICH, CONNECTICUT 06831**  Seale: AS NOTED Date: 03/20/18

Job No.

Dwg. 2 of 5 File No.





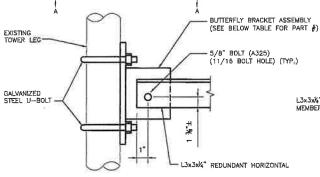
NOTES:

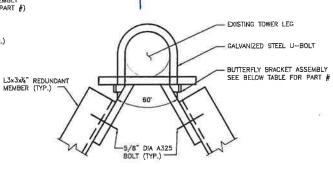
1. REFER TO SK-1 FOR STRUCTURAL NOTES. CODRDINATE SHEET WITH SK-3 FOR SECONDARY HORIZONTAL/DIAGONAL CONNECTION MEMBERS.

2. CONTRACTOR SHALL FIELD VERIFY DIMENSIONS SHOWN PRIOR TO ORDERING SUPPLIES.

3. U-BOLTEO CONNECTION ASSEMBLIES CONNECTING THE EXTERIOR AND INTERIOR TOWERS ARE PERMITTED TO BE ADJUSTED ONE UNIT AT A TIME TO ALLOW THE INSTALLATION OF THE PROPOSED BUTTERFLY BRACKET ASSEMBLIES INDICATED HERE AND ON SHEET SK-3.

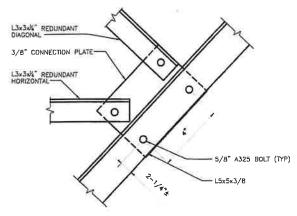


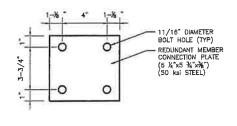














_	J	HOTE LEG BUTTEREY DOLONET APOTHOLY WEGGINATION
ELEVATION	LEG BUTTERFLY BRACKET #	
2'-10'	RSH-0500-00	SHALL USE PRODUCTS SIMILAR TO OR EXCEEDING IN QUALITY FOR CONSTRUCTION.
20'30'	RSH-0500-00	CONDITION CONTINUE TO THE

CONNECTION PLATE SCALE: 1-1/2"=1'-0"

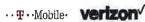
NOTE:
1. DETAILS 2 & 3 ABOVE INDICATE CONNECTIONS OF DIAGONAL AND HORIZONTAL MEMBERS TO TOWER LEGS, BUTTERFLY BRACKET ASSEMBILES USED FOR CONNECTION TO EXISTING LEGS SHALL BE INSTALLED AS CLOSE TO EXISTING ADJOINING HORIZONTAL MEMBER AS POSSIBLE.

PROJE	CT NO. 537397
Design	
Оганп	by: GAT
Check	ed by:
Approv	red by:

### AECOM

500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT (860)-529-8882



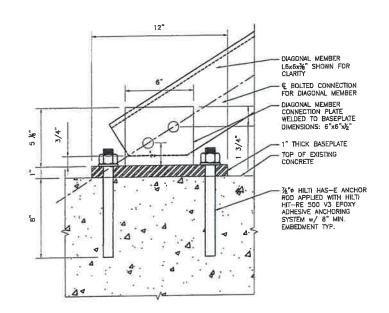


REV.	10/03/18 DATE:	RE-ISSUED DESCRIPTION
3	10/11/18	RE-ISSUED
4	07/31/19	RE-ISSUED/ND CHANGE

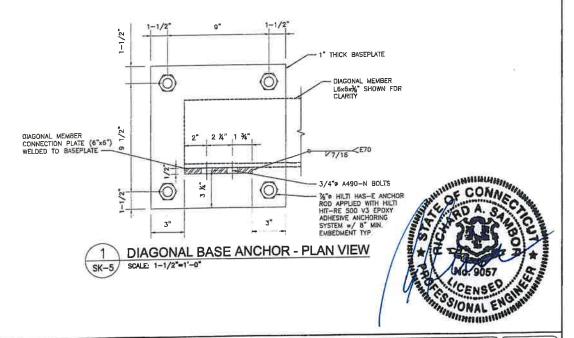
SK-4

Dwg. 4 of 5

BUTTERNUT HOLLOW ROAD SITE ADDRESS: GREENWICH, CONNECTICUT 06831 Scale: AS NOTED | Date: 03/20/18 Job No. (File No.



DIAGONAL BASE ANCHOR - ELEVATION VIEW SCALE: 1-1/2"-1'-0"



PROJECT NO. 60537397

Checked by:

Approved by: RAS

**AECOM** 

500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT (860)-529-8882



3	10/11/18	RE-ISSUED
2	10/03/18	RE-ISSUED
REV.	DATE:	DESCRIPTION

SK-5

Dwg. 5 of 5

Scale: AS NOTED Date: 03/20/18

File No.

Job No.

BUTTERNUT HOLLOW ROAD SITE ADDRESS: **GREENWICH, CONNECTICUT 06831** 

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## **CALCULATIONS COVER PAGE**

## A Note Regarding the Tower Calculations included herein:

The computer program utilized for the structural analysis contained in this report was "PLS-Tower", Version 10.62. This program does not apply multiple wind attack angles to greatest stress. As a result, multiple analyses with different wind attack angles were run in order to arrive at the controlling condition causing he greatest stress. This report includes only the TIA-222-G load case and wind attack angle that causes the greatest stress to the tower members in order to minimize the size of this report. The analyses conducted but not included with this report are available upon request.

PLS-TOWER INPUT / OUTPUT SUMMARY

```
Project Name: Multi-Carrier Analysis
Project Notes: Butternut Hollow
Project Notes: Butternut Hollow
Project File: p:/projects/telcom/structuralsbylocation/connecticut/greenwichcsp#74/14-vzw adds to # 13\_pls_g\pls-tower_wind_0\4-carir.tow
Date run : 3:01:51 PW Medneaday, July 31, 2019
by : Tower Version 10.62
```

: URS Connecticut Licensed to

## Successfully performed nonlinear analysis

```
load: this is nonsensical ??
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             Linear appurtenance "DNK27C-3/8" (§ 175" is included in the face zone (face solidity ratio for kev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK28L-1-5/8" (§ 175" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK28E-1-5/8" (§ 175" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK28C-1-5/8" (§ 175" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK28C-1-5/8" (§ 175" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "CRN-1-Ellipitical (§ 172 (DNK25)" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "CRN-1-Ellipitical (§ 17-Mobile" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "Hybriflex Stl2 Cables" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "Hybriflex Stl2 Cables" (§ T-Mobile" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??
             Unusual number of fixed joints found: 6. Towers normally have from between 1 and 4 fixed joints. ??

Linear appurtenance "DNK1-7/8" @ 56" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "DNK3-7/8" @ 66" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "DNK3-7/8" @ 66" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "DNK6-1-16" @ 82" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "DNK6-Hybriflex Cables @ Sprint" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "DNK6-Hybriflex Cables @ Sprint" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK9-7/8" @ 112" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "DNK9-7/8" @ 122" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "DNK9-7/8" @ 122" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "DNK9-7/8" @ 122" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "DNK9-7/8" @ 122" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical?
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          Linear appurtenance "NRK12-7/8" (§ 137" is included in the face sone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRK12-7/8" (§ 137" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRK15-1/18-1-5/8" (§ 7-Wobile" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRK16-1/18-1-5/8" (§ ATT" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "NRK16-1/18-1-5/8" (§ 150" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "NRK16-1/18-1-5/8" (§ 150" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "CSF70-1/17-1-5/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "CSF70-1/17-1-5/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical?

Linear appurtenance "CSF70-1/17-1-5/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRX2-1-5/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRX2-1-1/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRX2-1-1/8" (§ 160" is included in the face zone (face solidity ratio for Rev. B), but does not contribute to wind load: this is nonsensical??

Linear appurtenance "NRX2-
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       "DNKID-1-5/8" @ VZW" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??
"DNKII-1-5/8" @ 130" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ?
Towers normally have from between 1 and 4 fixed joints. ?? included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ?? included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ?? included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ?? included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         Linear appurtenance
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  Linear appurtenance
```

Member check option: ANSI/TIA 222-G-1

Connection rupture check: ANSI/TIA 222-G-1 [Alternate Unsupported RLOUT = 1]
Crossing diagonal check: ANSI/TIA 222-G-1 [Alternate Unsupported RLOUT = 1]
Loads from file: p:\projects\telcom\structuralsbylocation\connecticut\greenwichcsp#74\14-vzw adds to # 13\\_pls\_g\pls-tower\_wind\_0\4-carir.eia

## \*\* Analysis Results:

Maximum element usage is 97.93% for Angle "SNB-LH2P" in load case "1: 1.2D + 1.0Dg + 1.6Wo"

# Summary of Joint Support Reactions For All Load Cases:

Load Case	- Joint	Long.	Tran.	Vert.	Shear	Tran.	Long.	Vert.	Vert. Shear Tran. Long. Vert. Bending Found.	Found.
	Label.	Force	Force	Force	Force	Moment	Moment	Moment	Moment	Usage
() (eqix) (xix)		(kips)	(kips)	(kips)	(kips)	(ft-k)	(ft-k)	(ft-k)	(kips) (kips) (ft-k) (ft-k) (ft-k) 8	%

00.0	00.00	00.00	00.00	00.00	00.0	00.00	00.00	00.00	00.00	00.0	00.0	00.00	00.00	00.00	00.00	00:00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.0	00.00	00.00	00.00	00.00	0.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	0.00
13.12	2.31	2.33	5.89	5.90	5.32	13.00	2.37	2.39	6.00	6.01	0.56	1.17	0.14	0.14	0.20	0.20	0.49	1.05	0.08	0.08	0.15	0.16	1.38	3.24	0.35	0.35	1.03	1.03	0.28	0.48	0.27	0.27	0.47	0.47	0.21	0.36	0.21	0.21	0.35	0.36
																																						00.0	-0.00	00.0
-13.12	-1.36	-1.46	-2.55	-2.56	-5.32	-13.00	-1.40	-1.50	-2,62	-2.63	-0.56	-1.17	0.11	0.10	0.20	0.20	-0.49	-1.05	0.07	0.07	0.14	0.14	-1.38	-3.24	-0.21	-0.23	-0.41	-0.41	-0,28	-0.48	0.14	0.14	0.24	0.24	-0.21	-0.36	0.10	0.10	0.18	0.18
																																						0.18	-0.31	0.31
49.71	13.39	13.46	24.88	24.91	28.59	49.56	13,65	13.72	25.01	25.04	2.52	3.04	0.34	0.34	0.71	0.71	2.25	2.90	0.10	0.10	0.84	0.84	7.13	11.50	2.35	2.37	5.22	5.23	1.07	0.55	1.06	1.06	0.55	0.55	0.80	0.41	0.80	0.80	0.41	0.41
500.22	-144,29	-144.59	-222.16	-222.63	342.58	495.02	~148.99	-149.32	-226.45	-226.95	41,46	49.20	8.90	8.99	2.94	3.04	36.46	44.53	4.00	4.06	-1.61	-1.54	89.82	122.99	-20.18	-20.19	-38.48	-38.52	19.88	18.52	19.69	19.78	18.28	18.38	14.92	13.89	14.77	14.84	13.71	13,78
0.00	-9.74	9,66	-18.22	18.25			-9.96	9.88	-18.33	18.36	00.00	00.0	0.32	-0.33	-0.54	0.54	0.00	0.00	0.09	-0.10	-0.66	0.66	0.02	0.00	-1.60	1.58	-3.77	3.77	0.00	00.0	0.92	-0.92	0.47	-0.47	0.00	00.00	0.69	-0.69	0.35	-0.36
-49.71	-9.19	-9.38	-16.94	-16.96	-28.59	-49.56	-9.33	-9.51	-17.01	-17.03	-2.52	-3.04	0.11	0.10	-0.46	-0.45	-2.25	-2.90	-0.03	-0.03	-0.52	-0.52	-7.13	-11.50	-1.72	-1.76	-3,62	-3.62	-1.07	-0.55	0.53	0.53	0.27	0.28	-0.80	-0.41	0.40	0.40	0.21	0.21
+ 1.6Wo SNB-JP	+ 1.6Wo RohnJl	+ 1.0Dg + 1.6Wo RohnJ2	+ 1.0Dg + 1.6Wo SNB-J1	+ 1.0Dg + 1.6Wo SNB-J2	+ 1.6Wo RohnJP	# 0.9D + 1.0Dg + 1.6Wo SNB-JP	+ 1.0Dg + 1.6Wo RohnJl	: 0.9D + 1.0Dg + 1.6Wo RohnJ2	: 0.9D + 1.0Dg + 1.6Wo SNB-J1	: 0.9D + 1.0Dg + 1.6Wo SNB-J2	+ 1.0E RohnJP	+ 1.0Dg + 1.0E SNB-JP	+ 1.0Dg + 1.0E RohnJl	+ 1.0Dg + 1.0E RohnJ2	+ 1.0Dg + 1.0E SNB-J1	+ 1.0Dg + 1.0E SNB-J2	+ 1.0Dg + 1.0E RohnJP	+ 1.0Dg + 1.0E SNB-JP	+ 1.0Dg + 1.0E RohnJl	+ 1.0Dg + 1.0E RohnJ2	+ 1.0Dg + 1.0E SNB-J1	+ 1.0Dg + 1.0E SNB-J2	Service 1.0D + 1.0Dg + 1.0 Wo RohnJP	Service 1.0D + 1.0Dg + 1.0 Wo SNB-JP	Service 1.0D + 1.0Dg + 1.0 Wo RohnJl	Rohn J2	Service 1.0D + 1.0Dg + 1.0 Wo SNB-J1	Service 1.0D + 1.0Dg + 1.0 Wo SNB-J2	1.2*DL RohnJP	SNB-JP	RohnJl	RohnJ2	SNB-J1	SNB-J2	RohnJP	0.9DL SNB-JP	RohnJl	RohnJ2	SNB-J1	0.9DL SNB-J2

Summary of Joint Support Reactions For All Load Cases in Direction of Leg:

Load Case S	upport Origin	Leg	Force In Re	Residual Shear B	Residual Shear	Residual Shear	Residual Shear	Total	Tota1	Total
	Joint Join	Member	Leg Dir.	Perpendicular	Horizontal		Horizontal	Long.	Tran.	Vert.
				To Leg	To Leg - Res.	ဥ	To Leg - Tran.	Force	Force	Force
			(kips)	(kips)	(kips)	(kips)	(kips)	(kips)	(kips)	(kips)
1: 1.2D + 1.0Dq + 1.6Wo	RohnJP RohnIaS	Rohn-LI2P	348.846	15.102	15,114			1		347.98
1: 1.2D + 1.0Dg + 1.6Wo	SNB-JP SNB-IaS	SNB-LI2P	501.792	29.999	30.022					500.22
+ 1.6Wo	RohnJl RohnIa	Rohn-LI21	144.691	7.950	7.956	4.803	6.342	-9.19	- 9.74 -	-144.29
+ 1.6Wo	RohnJ2 RohnIa2	Rohn-LI22	144.993	8.041	8.046					144.59
+ 1.6Wo	SNB-J1 SNB-Ial	SNB-LI21	222.944	16.461	16.472	10.646				222.16
+ 1.6Wo	SNB-J2 SNB-Ia2	SNB-LI22	223,417	16.478	16.489	-10.661				222,63
+ 1.6Wo	RohnJP RohnlaS	Rohn-LI2P	343,443	15.047	15.058	860.0-				342.58
+ 1.6Wo	SNB-JP SNB-IaS	SNB-LI2P	496,589	30.060	30.084	-0.001				495.02
_	RohnJl RohnIal	Rohn-LI21	-149,403	8.023	8.028	4.868				148.99
+ 1.6Wo	RohnJ2 RohnI	Rohn-LI22	149,727	8.112	0.117	-4.776				149.32
1.0Dg + 1.6Wo	SNB-J1 SNB-I	SNB-LI21	227,234	16.428	16,439	10.611				226.45
	SNB-J2 SNB-Ia2	SNB-LI22	227,731	16.444	16.456	-10.626				226.95
1.0Dg + 1.0E	RohnJP RohnIaS	04	41,526	0.882	0.883	-0.003				41.46
4: 1.2D + 1.0Dg + 1.0E	SNB-JP SNB-IaS		49,282	1.100	1.101	-0.001				49.20
1.0Dg + 1.0E	RohnJl RohnIal		8,905	0.071	0.071	-0.019				8.90
1.0Dg + 1.0E	RohnJ2 RohnIa2	12 Rohn-LI22	966*8	0.076	0.076	0.020				8.99
1.0Dg + 1.0E	SNB-J1 SNB-Ial		2:908	0.824	0.824	0.644				2,94
1.0Dg + 1.0E	SNB-J2 SNB-Ia2	a2 SNB-LI22	3.009	0.826	0.826	-0.647				3.04
5: 0.9D + 1.0Dg + 1.0E	RohnJP RohnIaS	as Rohn-LI2P	36,518	0.814	0.814	-0.003		-2.25	00.0	36.46
1.0Dg + 1	SNB-JP SNB-IaS	S SNB-LI2P	44.607	1,148	1.148	-0.001		-2.90		44.53

4.00 4.00 1.54 182,82 182,82 182,82 182,82 182,82 183,82 19,83 19,63 19,63 19,63 19,63 19,63 19,63 19,73 113,89	13.78
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.35
-0.03 -0.03 -0.52 -0.52 -1.150 -1.72 -1.72 -1.76	0.21
0.104 0.109 0.493 3.585 6.585 6.585 0.286 0.280 0.085 0.085 0.085	0.064
0.042 0.041 0.041 0.068 0.088 0.988 0.	0.112
0.112 0.117 0.181 0.781 0.783 3.585 6.658 1.658 0.280 0.280 0.280 0.282 0.283 0.284 0.284	0.129 0.129 0.131
0.112 0.781 0.781 0.781 1.603 1.625 3.773 3.773 0.280 0.280 0.280 0.280 0.280 0.281 0.281 0.281 0.281 0.281	0.129 0.129 0.131
3.996 4.064 4.0645 11.5645 10.036 10.036 123,345 123,345 123,345 123,345 123,345 139,911 19,9	13.712
RohnJI RohnIal Rohn-LIZI RohnJZ RohnIaZ Rohn-LIZI SNB-JJ SNB-IAZ SNB-IAZ SNB-IAZ SNB-IAZ SNB-IAZ ROHNJP ROHNIAS ROHN-LIZI ROHNJP ROHNIAS ROHN-LIZI ROHNJF ROHNIAS ROHN-LIZI ROHNJF ROHNIAS ROHN-LIZI ROHNJF ROHNIAZ ROHN-LIZI ROHNJF ROHNIAZ ROHN-LIZI SNB-JZ SNB-IAZ ROHNJF ROHNIAS ROHN-LIZI SNB-JZ SNB-IAZ ROHNJF ROHNIAS ROHN-LIZI SNB-JZ SNB-IAZ SNB-JZ SNB-JZ SNB-JZ SNB-JZ	Konniaz SNB-Ial SNB-Ia2
.009 + 1.0E .009 + 1.0E .009 + 1.0E .009 + 1.0E .009 + 1.0 Wo 09 + 1.0 Wo 1.2*DL	0.9DL 0.9DL 0.9DL

## EIA Sections Information:

. E	Top Z (ft)		Joint	Bottom Joint Member Z Count Count (ft)	Top ] Width (ft)	Bottom Width (ft)	Gross Area (ft^2)	Face Af Adjust Factor	Face Ar Adjust Factor	Dead Load Factor
180.0	000	160.000	36	111	7.50	8.87	163.75	0	0.9000	
160.000 1	000	140,000		93	8.87		191.05	0.9000	0.9000	1.000
140.	000	120,000	27	72	10.23	11.60 2	218.31	0	0.9000	
120.1	000	100.000		72			245.54	0	0.9000	
1001	000	80.000		72			272.78	0	0.9000	
80	000	60,000		51	14.32		300.04	0	0.9000	
09	000	40.000		51	15.68		327.29	0	0	
40	000	20,000	21	51	17,05		354.57	0.9000	0	
20.	000	00000	18	39	18.41		381.92	0	0	

Printed capacities do not include the strength factor entered for each load case. The Group Summary reports on the member and load case that resulted in maximum usage which may not necessarily be the same as that which produces maximum force.

## Group Summary (Compression Portion):

No. Of Bolts Comp.	2000	,000001
Curve N No.	<b>~</b> ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	1444444
L/R Length Comp. Comp. Member (ft)	9.740 10.934 12.798 13.570 15.589 18.315 20.058 5.004 5.004	6.665 6.665 10.008 10.008 7.240
1/R L	170.38 166.50 1 155.13 1 157.99 1 158.34 1 151.38 2 45.67	= = = = = = = = = = = = = = = = = = = =
RLZ	500 1500 1500 1500 1500 1500 1500 1500	7.7
RLY	0.500 0.500	17777
RIX	0 500 0 500 0 0 500 0 0 500 0 0 500 0 0 0 500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1
p. Conn. Bearing Capacity (kips)	13.050 0 13.050 0 13.050 0 17.400 0 19.500 0 19.500 0 0.000 1	
Comp. Conn Bearing Capacity (kips)		
Shear Sapacity (kips)	12 433 12 433 12 433 12 433 0 000 0 000	0.000 0.000 0.000 0.000 0.000
Comp	10 10 m 10 m > = m 10 m	18288000
L/R Capacity (kips)	4,825 5,786 8,468 9,776 13,033 15,227 19,124 103,968	158.870 224.520 243.786 285.178 393.385 8.108
- 1	+++++++++	2D + + 2D
Ă	11: 1: 2D	
Comp. Force (kips)	-1,9241; -4,8991; -6,7821; -9,4791; -11,4341; -9,9501; -11,1471; -38,471;	-127, 7781; -171, 9681; -192, 3891; -259, 6901; -322, 2241; -0, 2061;
Comp.	Rohn-DA61 Rohn-DB61 Rohn-DD21 Rohn-DE61 Rohn-DF32 Rohn-DH12 Rohn-LA4P Rohn-LA4P	
S M		
Max Use In Comp.	39.87 84.67 79.74 84.74 76.24 91.97 80.02 10.72 28.98	
Steel Max ength Usage (ksi) %	36.0 39.87 36.0 84.67 36.0 84.74 36.0 76.24 50.0 91.97 50.0 10.75 50.0 50.0 50.0	50.0 80.43 50.0 76.59 50.0 78.92 50.0 91.06 50.0 81.91 36.0 2.54
ngle Steel Max Size Strength Usage (ksi) %	36.00 36.00 36.00 36.00 36.00	50.05 50.00 50.00 50.00 50.00
Angle Size St	5x0.1875 2x0.1875 2x0.1875 2.5x0.25 3x3x0.25 3.5x0.25 4x4x0.25 4x4x0.25 1pe3EH	Pipe5STD Pipe5EH Pipe6EHS Pipe6EH Pipe8EHS Pipe8EHS
rs I	SAE 1.75X1.75X0.1875 SAE 2.5X2.5X0.1875 SAE 2.5X2.5X0.1875 SAE 3.5X2.5X0.25 SAE 3.5X3.5X0.25 SAE 3.5X3.5X0.25 ipe Pipe3.5EH Pipe3.5EH	PipeSSTD PipeSSTD PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS PipeGEHS
	1.75X1 2.5> 2.3	-
Group Angle Desc. Type		Pipe Pipe Pipe Pipe Pipe SAE SAE
Group Desc.	Rohn Diagonal 1 Rohn Diagonal 2 Rohn Diagonal 4 Rohn Diagonal 4 Rohn Diagonal 5 Rohn Diagonal 6 Rohn Leg 1 Rohn Leg 1	Rohn Leg 5 Rohn Leg 5 Rohn Leg 6 Rohn Leg 6 Rohn Leg 7 Rohn Leg 7 Tizontal 1
	Rohn Diagonal Rohn Diagonal Rohn Diagonal Rohn Diagonal Rohn Diagonal Rohn Diagonal Rohn Diagonal Rohn Leg	Rohn Leg Rohn Leg Rohn Leg Rohn Leg Rohn Leg Rohn Leg Rohn Leg
	R R R S O O O O O O O O O O O O O O O O	Rohn
up 31	D1 D2 D2 D3 D1 D1 D2 D3 D3 D3 D3 D3 D3 D3 D3 D3 D3 D3 D3 D3	LL5 LL7 LL8 D1
Group Label	Rohn-D1 Rohn-D2 Rohn-D3 Rohn-D4 Rohn-D5 Rohn-D7 Rohn-L1 Rohn-L1	Rohn-L5 Rohn-L5 Rohn-L6 Rohn-L7 Rohn-L6 Rohn-H1 SNB-D1

110000000000000000000000000000000000000	
644H40HHHHHHHHHO440044006000HH	Hole (in) (in) (in) (in) (in) (in) (in) (in)
127.05 8.279 140,03 11.412 1121.15 15.529 1132.03 17.142 0.00 0.000 124.46 4.066 124.79 4.060 0.000	Wo. Of No. Of Holes Diameter Tens.  Tens.  (in)  1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.6875 1 1,000 0.8125 1 1,000 0.8125 1 1,000 0.8125 1 1,000 0.8125 1 1,000 0.8125 1 1,000 0.8125 1 1,000 0.8125
\$500 0.500 0.500 1.500 1.500 1.500 1.500 0.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.000 1	Rupture Tens. Com. Length No Rupture Tens. Capacity Mens. (kips) (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft
17.400 0.1.750	Tens. Com. Ten Bearing Capacity (tips)  (tips)  (tips)  13.050  13.050  13.050  13.050  19.500  0.000
12. 433 12. 433 17. 901 17. 901 17. 901 17. 901 0.000	Tens. Gom. Te Shear Gapacity (kips)  (kips)  (kips)  (2,433)  (2,433)  (2,433)  (2,433)  (2,433)  (2,433)  (2,000)  (0,000)  (0,000)  (0,000)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,433)  (1,2,601)  (1,000)  (1,0
13.020 16.821 11.188 57.545 59.660 0.000 115.941 147.353 514.179 167.256 119.859 103.108 0.0000 0.000	Section Capacity (Kips)
-3,5441: 1.2D + 1.2,5441: 1.2D + 1.2,5541: 1.2D + 1.2,5441: 1.2D + 1.2,7852: 0.9D + 0.000   0.	Tension Tension  Force Control  Load Case  (kips)  1,8392: 0.9D + 4.5612: 0.9D + 6.6822: 0.9D + 6.6822: 0.9D + 7.2822: 0.9D + 7.2822: 0.9D + 7.2822: 0.9D + 7.2832: 0.9D +
SNB-DB72 SNB-DD61 SNB-DF12 SNB-DH12 SNB-LIAP SNB-LIAP SNB-LIAP SNB-LIAP SNB-LIAP SNB-HACP SNB-DH32 SNB-DH32	Tension Control Member Rohn-DA19 Rohn-DB19 Rohn-DD19 Rohn-DD19 Rohn-LD32 Rohn-LD32 Rohn-LL342 Rohn-LL342 Rohn-LL342 Rohn-LL342 Rohn-LL32 Rohn-L132
28.50 75.48 68.18 68.18 6.00 0.00 0.01 0.01 0.01 0.01 0.01 0.00 0.	Max. Use II I I I I I I I I I I I I I I I I I
3.6.0 28.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.48.38.0 0 75.49.38.0 0 75	Size Strength Usage (ksi) 8  (ksi) 8  (ksi) 8  (ksi) 8  1875 36.0 39.87  1875 36.0 39.87  0.25 36.0 84.74  0.25 50.0 11.97  0.25 50.0 11.97  0.25 50.0 11.97  0.25 50.0 11.97  0.25 50.0 11.97  0.25 50.0 11.97  0.25 50.0 11.97  0.27 50.0 11.97  0.28 30.0 19.10  1875 36.0 19.10
2.5x2.6x0.25 3.3x0.5 3.3x0.5 4x4x0.625 5x5x0.625 5x5x0.625 84-494 120-625 12	######################################
SAMASAMASAMASAMASAMASAMASAMASAMASAMASAM	Angle She She She She She She She She She Sh
SNB-D2 SNB-D3 SNB-D4 SNB-D5 SNB-D5 SNB-D5 SNB-D5 SNB-D5 SNB-D7 SNB-D7 SNB-D7 SNB-D7 SNB-D7 SNB-D7 SNB-D7 SNB-D8 SNB-L3 SNB-L3 SNB-L6 SNB-L7 SNB-L6 SN	Rohn Diagonal 1 Rohn Diagonal 2 Rohn Diagonal 3 Rohn Diagonal 3 Rohn Diagonal 6 Rohn Diagonal 6 Rohn Leg 1 Rohn Leg 2 Rohn Leg 2 Rohn Leg 3 Rohn Leg 3 Rohn Leg 4 Rohn Leg 5 Rohn Leg 6 Rohn Leg 6 Rohn Leg 5 Rohn Leg 5 Rohn Leg 5 Rohn Leg 5 Rohn Leg 6 Rohn Leg 6 Rohn Leg 6 Rohn Leg 7 Rohn Leg 5 Rohn Leg 7 Rohn Leg 5 Rohn Leg 6 Rohn Leg 7 Rohn Leg 5 Rohn Leg 7 Rohn Leg 8 Rohn Leg 9 Rohn Leg 9 Rohn Leg 5 Rohn Leg 9 Roh
SNB-D2 SNB-D4 SNB-D4 SNB-D6 SNB-D6 SNB-D7 SNB-D7 SNB-L1 SNB-L1 SNB-L1 SNB-L2 SNB-L3 SNB-L4 SN	Group Label Rohn-D1 Rohn-D2 Rohn-D4 Rohn-D6 Rohn-L1 Ro

0	0	0	0	0	0	0	0	0	0.6875	0.6875	0	0	0.6875	0	0	0	0		0	0.8125	0.8125
000.000	000.00	000.00	000.00	000.000	000.00	000.000	000.00	000.000	1 1.000	1 1.000	000.00	000.000	1 1.000	000.000	000.000	000.000	000 0		0 0.000	1 1.000	1 1.000
0.000 10.008	0.000 2.002	0.000 4.066	0.000 7.472	0.000 0.000	0.000 4.066	0.000 7.472	0.000 0.000	0.000 0.000	14.625 13,177	14.625 13.977	0.000 0.000	0.000 0.000	18.281 20.653	0.000 0.000	0000 00000	0000000	000 0 000 0	000.0	0.000 0.000	26,471 16.594	26,471 18,841
0.000	0.000	0.000	000.0	0.000	0.000	0.000	0.000	0.000	19.500	19.500	0.000	0.000	24,375	0.000	000.0	0.000	0000	000	0.000	35.100	35.100
000.0	000.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	12,433	12.433	0.000	000.0	15.542	0.000	0.000	000.0	0000	000.0	0.000	22.376	22.376
521,639	25919,960	133.002	201.204	0.000	30,456	47,304	0.000	0.000	37.225	46.366	0.000	000.0	79.895	000.0	0.00	000 0	000	0.00	000.0	120.850	148.272
+ Q6.0	1.2D +	.2D +	.2D +		1.2D +	1.2D +			7.8602: 0.9D +	1.2D +			+ 06.0							1.2D +	1.2D +
2	۵	<u> </u>	ρ		Б	d.			S.P.	ЭЪ			Д	4						4 P	4 P
SNB-LI2	Connect	SNB-H4e	SNR-H9b	2	SNR-WI,-D	SNB-WI-T			Rohn-DC	Rohn-DD3P			Boho-DH	Thomas Direct						SNB-DG	SNB-DI4P
41.63 SNB-LI2	0.03 Connect 1	1.50 SNB-H4eP	1.81 SNB-H9b	000	1 46 SNR-WI-D	1 32 SNB-WIT3P	0.00	0000	63.22 Rohn-DC			00.0			00.0	000		0.00	0.00		
	0.03	2.13 1.50	3 85 1.81	00.0	1 64 1 46	3 19 1 32	0.00	00 00 00 0	63.22		00 0	00.0	77 10 69 41	15.60 OT.17			000	0.00	50.0 0.00 0.00	64.45 57.78	88.55 76.56
41.63	36.0 60.0 0 35	36.0 2.13 1.50	36.0 3.85 1.81	36.0 0.00 0.00	36.0 0.00	36 0 3 19 1 32	00.00 0.00	000000000000000000000000000000000000000	50.0 85.12 63.22	50 0 79 91 77 76	00 0 00 0 005	00.00	50.0 0.00	15.00 O O O O O O	00.00		00.00	0.00	00.0	50.0 64.45 57.78	50.0 88.55 76.56
36.0 93.12 41.63	בסיס בטיס טיפר נאנ טאני ט	0000 C000 360 20000000000000000000000000000000	DA-A94 36 0 3 85 1 81	36.0 00 0 00 0 00	24240.373 36.0 3.00 24240.25 36.0 1.64 1.46	2 5 5 7 3 1 2 1 3 1 3 1 3 1 3 1 3 1 3 2 3 3 3 3	2.372.372.372.372.3 50.0 0.00 0.00 0.00 0.00	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 5x2 5x0 25 50.0 85.12 63.22	92 LL 16 6L U US 62 0X8X8	00 0 00 0 05 50 0xxxx	2.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30.0 0.00 30.0 0.00 0.00 0.00 0.00 0.00	3×3×0 3135 50.0 77.15 03.41	2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20.00 0.00	2.3AZ.3AU.3IZ3	20.0 0.00	50.0 0.00	SAR 5X5X0.375 50.0 64.45 57.78	SAE 6X6X0.375 50.0 88.55 76.56
CAR Lan 6 Dine 10x3 36.0 93.12 41.63	O 18 18 18 18 18 18 18 18 18 18 18 18 18	COLINGE CAMPAIN DATA CAMPAINT TO THE CAMPAINT	NO INCLUDITION OF THE COLUMN SECTION OF THE	NO HOUSE STATE CARE CONTROL OF THE CANADA STATE OF THE CARE CANADA STATE OF THE CARE CANADA STATE OF THE CARE CANADA STATE OF THE CANADA STATE OF	Notice Designation of the Control of	WILL LACTING 1 OF 2 CV3 KV KV 319 3 C N 3 19 1 30	SAME 2:302:300:3123 30:0 3:13 1:32	MODIFICATION TITLE TOURS TO SAME TO SA	MODIFICATION - LAZAXA) 14 SAF 2AZAVILU/J JULY VILOVA	MODIETICATION 12.22.1/4 can 32.32.7 55 50 0 9 1 77.26	MODITAL CONTROL TO SAID SAND STAND STAND SAND SAND SAND SAND SAND SAND SAND S	MODIFICATION INSTALLY SAND SEVENCES SONS SONS SONS SONS SONS SONS SONS SO	MODIFICATION - LS. 3AS. 3AS. 3AS. 3AS. 3AS. 3AS. 3AS. 3A	MODIFICATION TOXOS:E/15 SAM SAXAO.SIZES SOUN OF COST	MODITALIZATION - LEASTAN IN CARE CARROLLING CONTROLL CONTROL CONTROLL CONTROL CONTROL CONTROL	MODIFICATION - LAXXXXII 4 SAME ACCOUNT OF THE COURT OF TH	MODIFICATION - LZ:5XZ:5X3/18 SAE Z:35XZ:3XU:31Z3 30:0	3.5X3.5X0.375 50.0 0.00	MODIFICATION - 1.4×4×0.5 SAE 4×4×0.5 50.0 0.00	MODIFICENTIAL 15X5x3/8 SAE 5X5X0.375 50.0 64.45 57.78	MODIFICATION - L6X6x3/8 SAE 6X6X0.375 50.0 88.55 76.56

\*\*\* Maximum Stress Summary for Each Load Case

## Summary of Maximum Usages by Load Case:

		Maximum Usage %	Element Label	Element Element Label Type
1 2 2 6: Service	1: 1.2D + 1.0Dg + 1.6Mo 97.93 2: 0.9D + 1.0Dg + 1.6Mo 96.89 4: 1.2D + 1.0Dg + 1.0E 12.42 5: 0.9D + 1.0Dg + 1.0 Mo 24.09 Service 1.0D + 1.0Dg + 1.0 Wo 24.09 0.9DL 4.05	97.93 96.89 12.42 11.00 24.09 5.66	SNB-LHZP SNB-LHZP Rohn-LD3P Rohn-LD3P SNB-LH1P Rohn-LD3P	Angle Angle Angle Angle Angle Angle
Weight Weight Weight Total:	of structure (lbs): of Angles*Section DLF: of Equipment:		61800.0 12631.6 74431.6	

\*\*\* End of Report

**PLS-TOWER NODE LOCATIONS** 

Robnebs SNB-Ebs ROPE P

AECOM Connecticut, Project - Butternut Hollow Greenwich, CT Tower Version 10.62, Wednesday, July 31, 2019 Undeformed geometry displayed RobnEas SNB-Eas Robnebs SNB-Ebs ROMEP SNB-FP RobnEas SNB-Fas RohnGP SNB-GP RohnGaS SNB-GaS ROB-HP RoboHaS SNB-HaS RohnIP SNB-IP RobbiaS SNB-laS

> RohnJP SNB-JP

## PLS-TOWER MEMBER LOCATIONS

180' Self Supporting Tower with Stack-N-Bolt System Greenwich, CT

SNB-H1P Connect AP Rohn-H1R SNB-DA2P Rohn-LA1P Rohn-DA1P SNB-DA1P SNB-DA1P SNB-LA1P

Connect AaP SNB-DA4P Rohn-LA2P Rohn-DA3P Rohn-DA4P SNB-DA3P SNB-LA2P

Connect AbP SNB-DA6P Rohn-LA3P Rohn-DA5P SNB-DA5P SNB-DA5P SNB-LA3P

Connect AcP SNB-DA8P Røhn-LA4P Rohn-DA7P Rohn-DA8P SNB-DA7P SNB-LA4P

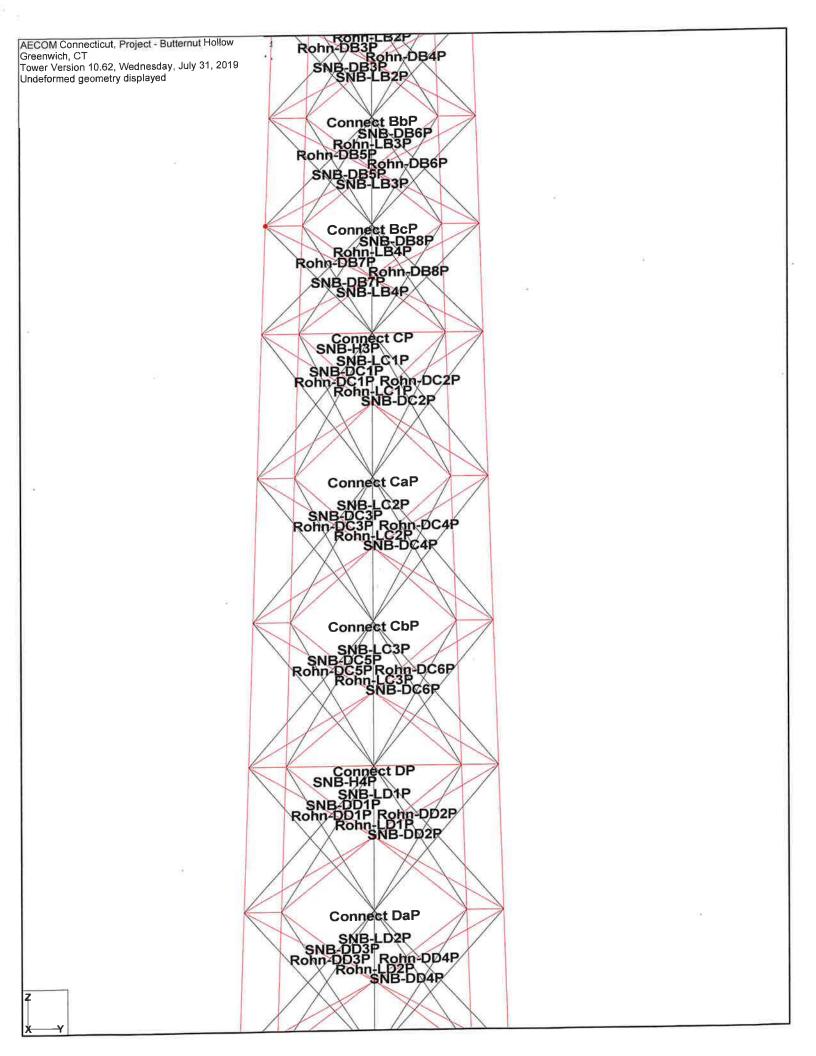
SNB-H2P Connect BP Rohn-H2P SNB-DB2P Rohn-DB1P Rohn-DB1P SNB-DB1P SNB-LB1P

Connect BaP SNB-DB4P Rohn-LB2P Rohn-DB3P SNB-DB3P SNB-LB2P

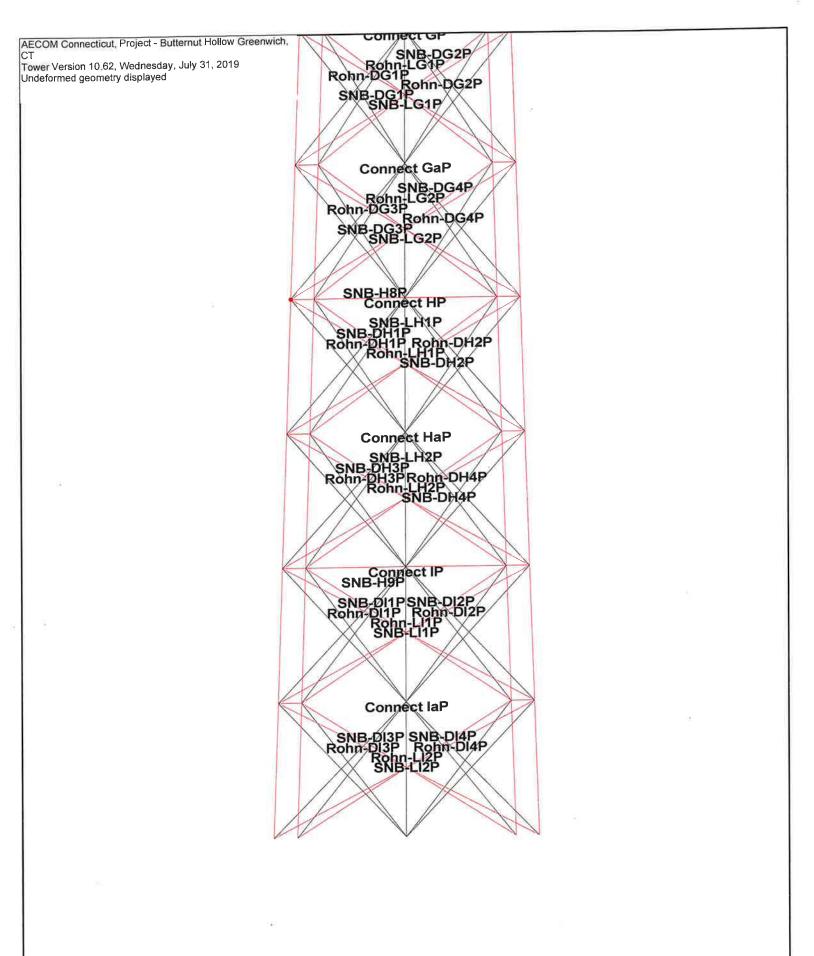
Connect BbP
SNB-DB6P
Rohn-LB3P
Rohn-DB5P
Rohn-DB6P
SNB-DB5R
SNB-LB3P

Connect BcP SNB-DB8P Rohn-LB4P Rohn-DB7P Rohn-DB8P

7



Connect DP SNB-DD2P Rohn-DD1P Rohn-DD2P SNB-DD1P SNB-DD1P AECOM Connecticut, Project - Butternut Hollow Greenwich, CT Tower Version 10.62, Wednesday, July 31, 2019 Undeformed geometry displayed Connect DaP SNB-DD4P Rohn-LD2P Rohn-DD3P Rohn-DD4P SNB-DD3P SNB-LD2P Connect DbP SNB-DD6P Rohn-DD5P Rohn-DD6P SNB-DD5P SNB-DD5P SNB-LD3P SNB-H5P Connect EP SNB-DE2P Rohn-LE1P Rohn-DE2P SNB-DE1P SNB-DE1P Connect EaP SNB-DE4P Refn-LE2P Rohn-DE3P SNB-DE3P SNB-LE2P Connect EbP SNB-DE6P Rohn-LE3P Rohn-DE6P SNB-DE5P SNB-LE3P SNB-H6P Connect FP SNB-DF2P Rohn-DF1P Rohn-DF2P SNB-DF1P SNB-LF1P Connect FaP SNB-DF4P Rohn-DF3P Rohn-DF4P SNB-DF3P SNB-LF2P SNB-H7P Connect GP SNB-DG2P Rohn-LG1P Rohn-DG1P SNB-DG1P SNB-LG1P Connect GaP SNB-DG4P Rohn-LG2P



PLS-TOWER DETAILED OUTPUT

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. * TOWER - Analysis and Design - Copyright Power Line Systems, Inc. 1986-2006 _{\star}^{\star}
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Project Notes: Butternut Hollow
Project File : p:\projects\telcom\structuralsbylocation\connecticut\greenwichcsp#74\14-vzw adds to # 13\\_pls\_g\pls-tower\_wind\_0\4-carir.tow
bate run : 31:151 FW Wednesday, July 31, 2019
by
Licensed to : URS Connecticut

## Successfully performed nonlinear analysis

Duranal number of fixed joints found: A Towers commendate that a transfer personal part of the control toward local this is monomental ?

Linear appurement "NEGL-16" (8 56" is included in the face some (face solidity ratio for Rev ?) but does not contribute to vital local this is monomental ?

Linear appurement "NEGL-16" (8 50" is included in the face some (face solidity ratio for Rev .) but does not contribute to what local this is monomental ?

Linear appurement "NEGL-16" (8 50" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" is included in the face some (face solidity ratio for Rev .) but does not contribute to wind local this is monomental ?

Linear appurement "NEGL-16" (8 12" nonsensical ?? Linear appurtenance "DNKZ8D-7/8" @ 175" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "GRW-1-Ellipitical @ 172 (DNKZ5)" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "WFW-(1) Eybriflax Cables" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "Hybriflax Garles @ T-Mobile" is included in the face zone (face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ??

Linear appurtenance "Hybriflex SA18 Cables @ T-Mobile" is included in the face solidity ratio for Rev. F), but does not contribute to wind load: this is nonsensical ?? normally have from between 1 and 4 fixed joints. ?? number

Nonlinear convergence parameters: Use Standard Parameters Member check option:  $ANSI/TIR_A$  22z-6-1 Connection rupture check:  $ANSI/TIR_A$  22z-6-1 (Connection rupture check:  $ANSI/TIR_A$  22z-6-1 [Alternate Unsupported RLOUT = 1] crossing diagonal check:  $ANSI/TIR_A$  22z-6-1 [Alternate Unsupported RLOUT = 1]

## Joints Geometry:

Joint Symmetry X Coord. Y Coord. X Disp. Y Disp. Z Disp, X Rot., Y Rot., Z Rot., Label. Code (ft) (ft) (ft) Rest. Rest. Rest. Rest. Rest.

Free	Free	Free	Free	Free	Free	Free	Fixed	Free	Free	Free	Free	Free	rree rree	ה ת ה ה ה	Free	Fixed	Free	Free	Free	Free	7 C	Free	Free	Free	Free	Free	Free	Free	Free	ה ה ה ה ה ה	Free	Free	Fixed	Fixed	Free	7 F 10 G 10 G	Free	Free	Free	7 H	Free	Free	Free	Free	ree	7 1 F	Free	Free	Free	Fixed	
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00	0 0	0 0	0	0	0	0	<b>-</b>	0	0	0	0	0	0 0	0 0	0 0	0	-3.752	3.752	-4.435	4.435	-5.11/	7.11.7	5.798	-6.479	6.479	-7.16	7.16	-7.842	7.842	525.8-	902.9	9.206	68.6-	9.89	-2.02	20.2	2.703	-3.384	3.384	990.0	-4 747	4.747	-5.428	5.428	-6.11	6.11 -6.701	6.791	-7.472	7.472	-8.154 8.154	
4.333	7.421	6.005	7.481	8.268	9.055	9.841	11 42	2.333	3.121	3.908	4.695	5.481	6.268	7.055	1.041 R 628	9,415	-2.167	-2.167	-2.561	-2.561	-2.954	2 3 3 A B	-3 34B	-3.741	-3.741	-4.134	-4.134	-4.527	-4.527	-4.921	-4.921 -5.315	-5.315	-5.71	-5.71	-1.167	-1.167	-1.561	-1.954	-1.954	-2.348	-2.340	-2.74	-3.134	-3.134	-3.528	-3.528	-3.921	-4.314	-4.314	-4.708	
ri-Symmetry	TII-Symmetry Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Gen 1		Tri-Gen 1			Tri-Gen 2	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen I	Tri-Gen 2	Tri-Gen 2		Tri-Gen 2		Tri-Gen 2	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1	Tri-Gen Z	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1 Tri-Gen 2	100
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## Secondary Joints:

Z Rot. Rest.		Free
Y Rot. Rest.		Free
X Rot. Rest.		Free
Z Disp. Rest.		Free
Y Disp. Rest.		Free
I Disp. Rest.		Free
End Fraction Elevation X Disp. Joint Rest.	(ft)	00
raction		0.25
End F		RohnBP RohnBP
Origin Joint		RohnAP RohnAP
Symmetry Origin Code Joint		ohnAas Tri-Symmetry RohnAP RohnBP ohnAbs Tri-Symmetry RohnAP RohnBP
Joint Label		RohnAas T RohnAbs T

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0.75 0.25 0.5 0.75	0.667 0.333 0.667	0.333	 	0.0	0.25	0.75	0.5	0.75	0.667	0.333	0.333	0.667	0.5	0.5	0.0	0 0	. c	0.5	0.5	0.5	0.5	0.5	0.0	0.5	0°.0	0.5	0.5	0.5	0.5	0.0	0.5	0.0	0.5	0.5	0.25	0.5	0.5	0.75	0.25	0.25	0.5	0.75
RohnBP RohnCP RohnCP RohnCP	RohnDP RohnEP RohnEP	RohnFP	RohnGP RohnHP	Sohn JP	SNB-BP	SNB-BP	SNB-CP SNB-CP	SNB-CP	SNB-DP	SNB-EP	SNB-FP	SNB-FP	SNB-HP	SNB-IP	SNB-A1	SNB-A2	SNB-AP.	SNB-B2	SNB-BP	SNB-C2		SNB-D1	SNB-D2	SNB-E1				SNB-G1	SNB-G2				SNB-12		RohnBP	RohnB	RohnBP				RohnCP	RohnCP RohnCP
RohnAP RohnBP RohnBP RohnBP	SohnDP SohnDP	AchnEP AchnEP	RohnEP	RohnIP	SNB-AP	SNB-AP	SNB-BP SNB-BP	SNB-BP	SNB-CP	SNB-DP	SNB-EP	SNB-EP	SNB-GP	SNB-HP	SNB-AP	SNB-A1	SNB-A2	SNB-B1	SNB-B2						SNB-E1			SNB-G				SNB-HZ	e SNB-Il		2 RohnAP		2 RohnAP	2 RohnAP	1 RohnBP	2 RohnBP	2 RohnBP	1 RohnBP 2 RohnBP
ri-Symmetry ri-Symmetry ri-Symmetry ri-Symmetry	ri-Symmetry ri-Symmetry ri-Symmetry ri-Symmetry	Tri-Symmetry Tri-Symmetry	ri-Symmetry ri-Symmetry	ri-Symmetry ri-Symmetry	Pri-Symmetry Pri-Symmetry	Tri-Symmetry	rı-Symmetry ri-Symmetry	Tri-Symmetry	ri-Symmetry Pri-Symmetry	Tri-Symmetry	rii-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-Symmetry	Tri-symmetry None	None	None	None		None		None			None		None		2 2	None		None		None		Tri	Tri	Tri-Gen	Tri-Gen	Tri-Gen		Tri-Gen Tri-Gen
RohnBas T. RohnBbs T. RohnBbs T. RohnBcs T.	Robincas I Robincas I Robincas I	RohnEbs T	RohnGaS T	RohnHas T RohnIas T	SNB-Aas 1	SNB-Acs 1	SNB-Bas 1	SNB-Bcs 1	SNB-CBS 5	SNB-Das	SNB-Eas	SNB-Ebs				SNB-WL-A2S	SNB-WL-A3S	SNB-WL-B2S	SNB-WL-B3S	SNB-WL-C1S	SNB-WL-C3S	SNB-WL-DIS	SNB-WL-D3S	SNB-WL-E1S	SNB-WL-E2S SNR-WL-E3S	SNB-WL-F1S	SNB-WL-F2S	SNB-WL-G1S	SNB-WL-G2S	SNB-WL-H1S	SNB-WL-H2S	SNB-WL-H3S	SNB-WL-I2S	SNB-WL-I3S	RohnAa2	RohnAbl	RohnAb2	RohnAc2	RohnBal	RohnBa2	RohnBb2	RohnBc1 RohnBc2

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0.333	0.333	0.667	0.007	0.333	0.667	0.667	0.333	0.333	0.667	0.667	0.5	0.5	0.5	0.5	0.5	0.5	U.U	0.5	0.25	0.25	0.5	0.5	0.75	0.75	0.25	0.25	0.5	0.5	0.75	0.75	0.333	0.333	0.667	0.667	0.333	0,333	0.067	0.667	0.333	0.333	0.667	0.667	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
		KohnDP							_																					-,		P SNB-DP																		P SNB-JP
RohnCP	RohnCP	KohnCF	TOPPE	RohnDP	RohnDP	RohnDP	RohnEP	RohnEP	RohnEP	RohnEP	. RohnFP	RohnFP	. RohnGP	RohnGP	RohnHP	RohnHP	Kohnip	Kohnir	SNB-AP	SNB-AP	SNB-AP	SNB-AP	SNB-AP	SNB-AP	-	2 SNB-BP	L SNB-BP	2 SNB-BP	L SNB-BP	2 SNB-BP	I SNB-CP	2 SNB-CP	1 SNB-CP	SNB-CP	I SNB-DP	SNB-DP	I SNB-DP	SNB-DP	1 SNB-EP	2 SNB-EP	1 SNB-EP	2 SNB-EP	1 SNB-FP	2 SNB-FP	1 SNB-GP	2 SNB-GP	1 SNB-HP	2 SNB-HP	1 SNB-IP	2 SNB-IP
Tri-Gen 1	Tri-Gen 2	Tri-Gen I	Tri-Gen Z	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen J	Tri-Gen 2	Tri-Gen ]	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2	Tri-Gen 1	Tri-Gen 2			Tri-Gen	Tri-Gen 2	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Tri-Gen	Trj-Gen	Tri-Gen	Tri-Gen	Tri-Gen																
RohnCal	RohnCa2	RohnCbl	RohnCD2	Rohn Da 2	RohnDb1	RohnDb2	RohnEal	RohnEa2	RohnEb1	RohnEb2	RohnFal	RohnFa2	RohnGal	RohnGa2	RohnHal	RohnHaZ	Kohnlal	Rohnia2	SNB-Aal	SNB-Aa2	SNB-Abl	SNB-Ab2	SNB-Ac1	SNB-Ac2	SNB-Bal	SNB-Ba2	SNB-Bb1	SNB-Bb2	SNB-Bcl	SNB-Bc2	SNB-Cal	SNB-Ca2	SNB-Cb1	SNB-Cb2	SNB-Dal	SNB-Da2	SNB-DDI	SNB-DD2	SNB-Eal	SNB-Ea2	SNB-Ebl	SNB-Eb2	SNB-Fal	SNB-Fa2	SNB-Gal	SNB-Ga2	SNB-Hal	SNB-Ha2	SNB-Ial	SNB-Ia2

The model contains 60 primary and 123 secondary joints for a total of 183 joints,

Steel Material Properties:

Label	Label Blasticity Fy Fu Hyp. 1 (ksi) (ksi) (ksi)	Stress FY (ksi)	Stress Stress Fu (ksi)	A11.	Member Stress Al Hyp. 1 (ksi)	iss R	Member Member Stress Rupture R Hyp. 2 Hyp. 1 (ksi) (ksi)	wember upture Hyp. 2 (ksi)	Member Bearing Hyp. 1 (ksi)	Member Bearing Hyp. 2 (ksi)
i						 -				
A 36	2.9e+004	36	58		0	0	0	0	0	0
572-50	2.9e+004	50	65		0	0	0	0	0	0

Bolt Properties:

Bolt Bolt Hole Ultimate Default Default Shear Shear Label Diameter Diameter Shear End Bolt Capacity Capacity

Optimize Allow. Add. Group Angle Width For Optimize (in)

Element Type

Material Type

Angle

Group Angle Description Type

Groups:

Angle (

Group Label

Hyp. 2 (kips)	0	0	0	0
Hyp. 1 (kips)	0	0	0	0
Spacing (in)	1,5	1.8	1.5	1.8
apacity Distance (kips) (in)	1.125	1.35	1.125	1.35
Capacity (kips)	16.58	23,87	20.72	29.83
(in)	0.6875	0.8125	0.6875	0.8125
(in)	0.625	0.75	0.625	0.75
	5/8 A325-N	3/4 A325-N	5/8 A490-N	3/4 A490-N

Number Bolts Used By Type:

Bolt Number Type Bolts

5/8 A325-N 228 5/8 A490-N 6 3/4 A325-N 423/4 A490-N 24 Angle Properties:

y Optimize Section
Cost Modulus
Factor Short Long of Edge Edge Dist. Dist. Wind 8 Number of 1 Angles E Radius of N Gyration Rz Rz R Radius of 1 Gyration Ry (in) Gross w/t Radius of Re Area Ratio Gyration of Gyration Unit Weight (in) (lbs/ft) 0.375 0.625 0.625 0.375 0.3125 0.3125 0.3125 0.3125 0.3125 0.1875 0.1875 0.1875 0.1875 0.1875 0.1875 0.1875 0.1875 Long Short Thick. Leg Leg (in) E 6X6X0, 375
E 7X5X0, 625
E 7X4X0, 625
E 7X4X0, 3125
E 7X4X0, 3125
E 7X33, 5X0, 3125
E 7X33, 5X0, 3125
E 7X33, 5X0, 3125
E 7X23, 5X0, 2125
E 7X20, 3125
E Angle Size Angle Type

	000000000000000000000000000000000000000
None None None None None None None None	None None None None None None
Other	Other Other Other Other Other Other
Truss	Truss Truss Truss Truss Truss Truss Truss
A 5 3 4 5 3 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	A572-50 A572-50 A572-50 A572-50 A572-50 A572-50 A572-50
2.5x2 2.5x3 3.5 2.5x1 2.5x3 2.5x3 3.	4X4X0.3125 2X2X0.3125 2X2X0.252 2.5X2.5X0.3125 3.5X3.5X0.375 5X5X0.375 6X6X0.375
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Aggregate Angle Information:

Note: Estimate of surface area reported for painting purposes, not wind loading:

Total Weight (1bs)	592.39	631.49	464.18	324,16		2172.46			1016.15	618,48
Total Surface Area (ft^2)	163.00	172.54	126.00	68.89		443,36	520.96	505.38	165.23	64.05
Total Length (ft)	279.43	258.81	151.20	79.06	81.42	443.36	446.54	379.04	123.92	60.09
Angle Material Size Type	A 36	A 36	A 36	A572-50	A 36	A572-50		A572-50		A572-50
Angle Size	1.75X1.75X0.1875	2X2X0.1875	2.5X2.5X0.1875	2.5X2.5X0.25	2.5x2.5x0.25	3X3X0.25	3.5X3.5X0.25	4X4X0.25	4X4X0.3125	Pipe3EH
Angle Type	SAE	SAE	SAE	SAE	SAE	SAE	SAE	SAE	SAE	Pipe

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Sections: The adjustment factors below only apply to dead load and wind areas that are calculated for members in the model. They do not apply to equipment or to manually input dead load and drag areas.

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174.658 174.858 174.858 174.858 174.858 109.180 169.180 169.180 169.180 163.108 163.10	13.417 23.157 23.157 23.157 23.157 18.587 18.587 14.672 14.672 11.878 11.878 11.878 9.810 9.810
SNB-H2 SN	WLAC-1 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2 WLAC-2
SNB-H7bP SNB-H7cP SNB-H7cP SNB-H7cP SNB-H7cP SNB-H8aP SNB-H8cP SNB-H8cP SNB-H8cP SNB-H8cP SNB-H9cP SNB	SNB-WL-D2P SNB-WL-E1P SNB-WL-E2P SNB-WL-E2P SNB-WL-E3P SNB-WL-E3P SNB-WL-E3P SNB-WL-G3P SNB-WL-G3P SNB-WL-G3P SNB-WL-G3P SNB-WL-G3P SNB-WL-H2P SNB-WL-H2P SNB-WL-H2P SNB-WL-H3P SNB-WL-H3P SNB-WL-H3P

The model contains 612 angle members.

## Section Joint Information:

(±t)	30.	175,000	30.	75.	30.	75.	70.	70.	0	0	165.000	5.0	160,000	160,000	0	180.000	
(ft)	ы	_		RohnAa2				RohnAb2	RohnAbS ]	RohnAc1 1	RohnAc2 ]	RohnAcs	RohnB2	RohnBP	RohnB1	SNB-AP	
	A	A	A	A	A	A	K	A	¥	A	A	A	A	A	А	A	

1175,000 1175,000 175,000 176,000 170,000 170,000 170,000 165,000 165,000 165,000 166,000 160,000	00000000000000000000000000000000000000	140.000 133.340
SNB-Aa1 SNB-Aa2 SNB-Aa2 SNB-Aa3 SNB-Ab2 SNB-Ab2 SNB-Ab2 SNB-Ab2 SNB-Ab2 SNB-Ac		SNB-C1
***************************************	丸丸丸 丸丸 日日	00

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C SNB-C2S 140.000
C SNB-Cb1 126.660
C SNB-Cb2 126.660
C SNB-Cb2 126.660
C SNB-Cb2 126.660
C SNB-D2 120.000
C SNB-D2 120.000
C SNB-ML-D2S 120.000
C SNB-ML-D3S 120.000
C SNB-ML-D3S 120.000
D RohnDa1 120.000
D RohnDa1 113.340
D RohnDa2 113.340
D RohnDa2 113.340
D RohnDa2 113.340
D RohnDa 113.340
D RohnDa 113.340
D RohnDa 113.340
D SNB-DA 113.340
D SNB-DB 100.000
D SNB-BB 100.000
D
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Tall		
80.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000		20.000
RohnF2 RohnG3 RohnG4 RohnG5 RohnG6 SNB-F1 SNB-F1 SNB-F2 SNB-F2 SNB-F2 SNB-G2 SNB-G3 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G3 SN	Robingaz Robingaz Robingaz Robinga Robinga Robinga Robingaz Robing	SNB-IP
[		1 14

0	20.000	0	0	0	0.000	0.000	0.000
SNB-Ial	SNB-I1	SNB-Ia2	SNB-I2	SNB-IaS	SNB-J1	SNB-J2	SNB-JP
H	Н	Н	H	Н	Н	Н	<u></u>

EIA Sections Information:

Bottom Joint Member Z Count Count (ft)
36
33
27
27
27
21
21
21
18

Equipment Library:

10.0 1.32 0.00 Circle 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Equipment Stock Weight Property Label Number (1bs)
1.32 0.00 circle 1.00 0.00 0.054 0.00 0.00 0.00 0.00 0.00	
13.60 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Omni
13.60 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Omri
2.72 0.00 Square 1.00 0.00 1.29 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	
9.17 0.00 circle 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	
1.29 0,00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Dipole
1.00 0.00 Circle 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	TMA
5.88 0,00 Square 1.00 0.00 0.377 0.00 0.00 0.00 0.00 0.00	GPS
1.79 0,00 Circle 1.00 0.00 1.01 1.01 0.00 0.00 0.00 0.0	Panel
3.70 0,00 circle 1.00 0.00 3.95 0,00 circle 1.00 0.00 2.00 0,00 circle 1.00 0.00 2.00 0,00 circle 1.00 0.00 2.27 0,00 circle 1.00 0.00 5.27 0,00 circle 1.00 0.00 6.50 0,00 circle 1.00 0.00 8.26 0,00 circle 1.00 0.00 8.27 0,00 circle 1.00 0.00 8.28 0,00 circle 1.00 0.00 8.29 0,00 circle 1.00 0.00 8.20 0,00 circle 1.00	Other
1.01 0.00	Dipole
3.95 0.00 Circle 1.00 0.00 4.00 0.00 Circle 1.00 0.00 13.60 0.00 Square 1.00 0.00 5.06 0.00 Square 1.00 0.00 5.00 Square 1.00 0.00	Omni
2.00 0,00 Circle 1.00 0.00 13.60 0,00 Circle 1.00 0.00 2.27 0,00 Circle 1.00 0.00 2.27 0,00 Circle 1.00 0.00 8.26 0,00 Circle 1.00 0.00 10.60 0,00 Square 1.00 0.00 5.53 0,00 Square 1.00 0.00 6.53 0,00 Square 1.00 0.00 6.50 0.00 Square 1.00 0.00	Dipole
4.00 0,00 circle 1.00 0.00 2.27 0.00 circle 1.00 0.00 0.00 2.27 0.00 circle 1.00 0.00 0.00 0.00 circle 1.00 0.00 0.00 0.00 circle 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Omnı
13.60 0.00 Square 1.00 0.00 6.90 0.00 6.90 0.00 0.00 0.00 0	Omni
2.27 0.00 Circle 1.00 0.00 8.26 0.00	Mount
5.06 0.00 Circle 1.00 0.00 6.90 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0	Omni
8.26 0.00 Square 1.00 0.00 10.60 0.00 10.60 0.00 0.00 0.	Omni
8,90 0,00 Square 1.00 0,00 3,00 8,00 0,00 0,00 0,00 0,00 0,	Panel
10.60 0.00 Square 1.00 0.00 5.60 0.00 0.00 0.00 0.00 0.00 0	RRH
3.97 0.00 Square 1.00 0.00 6.53 0.00 Square 1.00 0.00 6.53 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Mount
5.60 0.00 Square 1.00 0.00 1.64 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Panel
1.64 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Panel
2.99 9.17 0.00 9.17 0.00 9.18 9.19 0.00 9.65 0.00 9.65 0.00 9.65 0.00 9.65 0.00 9.65 0.00 9.66 0.00 9.66 0.00 9.66 0.00 9.66 0.00 9.66 0.00 9.66 0.00 9.60 9.6	Panel
5.39 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Dipole
6.53 0.00 Square 1.00 0.00 6.90 6.90 6.90 0.00 8 9.65 0.00 8 9.66	Dinole
9.65 0.00 Square 1.00 0.00 4.72 0.00 8quare 1.00 0.00 0.00 0.00 8quare 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Danel
6.90 0.00 Square 1.00 0.00 9.66 0.00 9.66 0.00 9.66 0.00 9.00 9	Panel
4.72 0.00 Square 1.00 0.00 9.66 0.00 3.78 0.00 Square 1.00 0.00 0.00 1.26 0.00 Square 1.00 0.00 0.00 22.38 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	RRH
9.66 0.00 Square 1.00 0.00 1.26 0.00 Square 1.00 0.00 0.00 1.26 0.00 Square 1.00 0.00 0.00 1.26 0.00 Square 1.00 0.00 0.00 1.12 0.00 Square 1.00 0.00 0.00 0.72 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	RRH
3.78 0.00 Square 1.00 0.00 1.26 0.00 5.84 0.00 Square 1.00 0.00 0.00 22.38 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Panel
1.26 0.00 Square 1.00 0.00 5.23 84 0.00 Square 1.00 0.00 0.00 0.00 1.12 0.00 Square 1.00 0.00 0.00 0.72 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Mount
5.84 0.00 Square 1.00 0.00 22:38 0.00 5.00 Square 1.00 0.00 0.00 0.72 0.00 Square 1.00 0.00 1.12 0.00 Square 1.00 0.00 0.00 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	RRH
22.38 0.00 Square 1.00 0.00 1.12 0.00 Square 1.00 0.00 1.22 0.00 Square 1.00 0.00 1.29 0.00 Square 1.00 0.00 1.29 0.00	Panel
1.12 0.00 Square 1.00 0.00 0.72 0.00 Square 1.00 0.00 1.29 0.00 Square 1.00 0.00	Panel
0.72 0.00 Square 1.00 0.00 1.29 0.00 Square 1.00 0.00	Other
1.29 0.00 Square 1.00 0.00	Other
	Other

Square 1.00 0.00 Square 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0																																														
Square Square BIA Microwave MaxCA EIA Microwave Radome MaxCA Square Square Square		tenna ation Angle (deg)	00.00	0,00	120.00	120.00	00,00	00.00	0.00	0.00	0.00	00.00	20.00	0.00	0.00	10.00	00.00	0.00	00:00	0.00	120.00	50.00	240.00	240.00	0.00	20.00	740.00	20.00	240.00	30.00	120.00	0.00	120.00	00.00	0.00	20.00	20.00	240.00	00.0	0.00	120.00	20,00	240.00		0.00	00 00
0000000		EIA Antenna Orientation Angle (deg)			12	12			24	24	12	12	12			120	24							24		12		1		-	-1 (2)															
10.12 3.88 13.10 51.32 3.13 3.13		Equipment EIA Antenna Property Orientation Set Angle	Dipole	Stand-Off	GPS	Stand-Off	and-Off	10 Dipole	ĕ,	Stand-Off	PD1142 w/ ice	Stand-Off	PD1142 w/ ice	12 Ombi	12 T-Arm	12 T-Arm	Ė,	C W/ ice	ALU RRH	-C w/ ice	_		W/ice	ALU RRH	DT465B-2XR-V2	DT465B-2XR-V2	DT465B-ZXR-VZ MH7 RRH Ilnit	RRH Unit	RRH Unit	KRH Unit	RRH Unit	Boom Gate	Boom Gate	XV W/ ice	Y w/ ice	Y w/ ice	Y w/ ice	Y W/ ice	3B Panel	JAHH-65B-R3B Panel	3B Panel	3B Panel	3B Panel	Antonna	JAHH Antenna	
64.0 80.0 120.0 560.0 116.0 98.5		西西	, 5	3, St		3, St	3, St	10,		6,04				7 6		12	12	APXVSPP18-C		APXVSPP18-C			APXVSPP18-C W/		DT4651	DT465	DT465E	00 MHz E	OO MHZ	X20-25	8x20-25	B	ă	A4H80-X	44H80-X	44H80-X	44HB0-X	DB844H80-XY w/ i	H-65B-R	H-65B-R	IH-65B-R	H-65B-R	IH-65B-R	A-GCO-DI	tor JAHH	
Panel Other Dish Dish Panel Panel			1								RES		RFS					RES APX		RFS APX			RFS APX				α	0		D-RRH	TD-RRH 8			Decibel DR9	bel DB8	bel DB8	bel DB8	bel DB8	HAT.	JAH	JAH	JAH	JAH	Ş	Jonne	
OPA-65-LCUU-H6 Panel RRUS-32 RRH Unit 4 Dish B Dish with Radome RRH B2/B66A (RFV01U-D1A) RRH B5B/BB13 (RFV01U-D2A)																															<b>→</b> E→			i CeC	Decibel	Decibel	Decibel	Decibel	1000					C C COLD BIMEROOD	BSAMNT-SBS-Z-Z	
OPA-6 RI 8 D: RH B2/B6 I B5B/BB:	stivity:	Attach Label	BohnGP	RohnGP	RohnG1	RohnGl	RohnG2	RohnG2	RohnG2	RohnF2	RohnD1	RohnD1	RohnDl	RohnDas	RohnDas	RohnDa1	RohnDa2	RohnDas	Ronnbas	RohnDa1	RohnDa1	RohnDal	RohnDa2	Rollinga2 RohnDa2			RohnDa2 RohnDas	RohnDa1		RohnDas	RohnDa2	RohnCbS	RohnCb1	Rounchs Pohnchs	RohnCbS	RohnCb1	RohnCbl	RohnCb2	RohnChs	RohnCbS	RohnCb1	RohnCb1	RohnCb2	Rouncbz	KohnCbS	
RE	Equipment Connectivity	Equipment Label	DNK-1	MT-DNK1	DNK2-GPS68	MT-DNK2	MT-DNK3	DNK4-DOT56	MT-DNK4	DNKS-NEU16	DNK9-DEP54	MT-DNK9			Sprint-A I				Sprint-2	0 4			print-7	Sprint-9			Sprint-12	Sprint-14	Sprint-15	Sprint-16	Sprint-18		Verizon-B	Verizon-U	Verizon-2	Verizon-3	Verizon-4	Verizon-5	Verizon-7	Verizon-8	Verizon-9	Verizon-10	Verizon-11	Verizon-12	Verizon-D	

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0.00	240.00	00.00	120.00	260.00	220.00	120.00	120.00	240.00	240.00	0.00	120.00	240.00	00.00	120.00	240.00	00.00	120.00	240.00	
Andrew DB-583 w/ ice	Decibel PD-420 2 bay - Dipole	6 Stand-Off	6 Stand-Off	6 Stand-Off	6 Stand-Off	Powerwave 7770	Powerwave 7770	Powerwave 7770	Powerwave 7770	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (REV01U-D2A)	CBC78T-DS-43-2X	CBC78T-DS-43-2X	CBC78T-DS-43-2X	
DNK28C-TOG5 RohnAas	DNK28D-NEU55 RohnAa2	Top-A RohnAP	Top-B RohnAl	Top-C1 RohnA2	Top-C2 RohnA2	ATT-B7 RohnBb1	ATT-B8 RohnBb1	ATT-C7 RohnBb2	ATT-C8 RohnBb2	Verizon-25 RohnCbS	Verizon-26 RohnCbl	Verizon-27 RohnCb2	Verizon-28 RohnCbS	Verizon-29 RohnCbl	Verizon-30 RohnCb2	Verizon-31 RohnCbS	Verizon-32 RohnCbl	Verizon-33 RohnCb2	

tenances:	
Appur	
Linear	

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	(ft)	(ft)		Diameter (in)	(in)	(lbs/ft)	Zone	мтиа года
Full Cable Tray 2-150 (wind only)	2	150	2 Flat	24	0	0	Yes	Yes
(wind	150	180	1 Flat	24	0	0	Yes	Yes
DNK1-7/8" @ 56	2	180	1 Round	0	0	1,30128	Yes	No
DNK2-7/8" @ 54	2	180	1 Round	0 1	0	1.30128	Yes	No
О	2	180	1 Round	0	0	1.30128	Yes	No
DNK4-7/8" @ 65	2	180	1 Round	0	0	1.30128	Yes	No
DNK5-1-5/8" @ 82`	2	180	1 Round	1 0	0	2.33495	Yes	No
DNK6-Hybriflex Cables @ Sprint	2	180	4 Round	1	0	0.9	Yes	No
DNK7-7/8" @ 110`	2	180	1 Round	1	0	1.30128	Yes	No
DNK8-7/8" @ 122`	2	180	1 Round	0	0	1.30128	Yes	No
DNK9-7/8" @ 122`	2	180	1 Round	0	0	1.30128	Yes	No
DNK10-1-5/8" @ VZW	2	180	6 Round	0	0	2.33495	Yes	No
DNK11-1-5/8" @ 130`	2	180	1 Round	1 0	0	2.33495	Yes	No
DNK12-7/8" @ 135`	2	180	1 Round	0	0	1,30128	Yes	No
DNK13,14-1-5/8" @ T-Mobile	2	180	6 Round	0	0	2.33495	Yes	No
DNK15-7/8" @ 137`	2	180	1 Round	0	0	1.30128	Yes	No
DNK16,17,18-1-5/8" @ ATT	2	180	12 Round	0	0	2.33495	Yes	No
DNK16,17,18-Optic Fiber Cable @ ATT	2	180	1 Round	0	0	1.3	Yes	No
DNK16,17,18-DC Cable @ AIT	2	180	2 Round	0	0	0.3	Yes	No
DNK19-7/8" @ 159	7	180	1 Round	0	0	1.30128	Yes	No
DNK20-7/8" @ 159.5`	2	180	1 Round	0	0	1.30128	Yes	No
9	2	180	3 Round	0	0	2.33495		No
Ø	2	180	1 Round	1 0	0	0.840278	Yes	No
e	2	180	1 Round	0	0	1.24804		No
0	2	180	1 Round	0	0	1.30128	Yes	No
9	7	180	1 Round	1 0	0			No
©	2	180	1 Round	0	0	0	Yes	No
9	2	180	1 Round	0	0	2,33495	Yes	No
e		180	1 Round	0	0		Yes	No
DNK26C-1/2" @ 175`		180	1 Round	1 0	0	0		No
e		180	1 Round	0	0	2.33495	Yes	No
e		180	1 Round	0	0	1.30128	Yes	No
DNK27C-3/8" @ 175`		180	1 Round	1	0	0.654213	Yes	No
9		180	1 Round	0	0	2.33495	Yes	No
e	2	180	1 Round	0	0	2.33495	Yes	No
9	2	180	1 Round	0	0	2.33495	Yes	No
DNK28D-7/8" @ 175	2	180	1 Round	0	0	1.30128	Yes	No
GRN-1-Ellipitical @ 172 (DNK25)	2	180	1 Round	0	0	1,24804	Yes	No
VZW-(1) Hybriflex Cables	2	180	1 Round	0 [	0	1.3	Yes	No
Cables @	2	180	2 Round	0	0	1.7	Yes	No
Winhriflay Ov18 Cables A T-Mohila	0	180	1 Round	0	0	0.9	YPS	ON

Loads from Tile: p:\projects\telcom\structuralsbylocation\connecticut\greenwichcsp#74\14-vzw adds to # 13\\_pls\_g\pls-tower\_wind\_0\4-carir.eia

Structure Height Summary (used for calculating wind/ice adjust with height):
Structure height above ground
180.00 (ft)
Elevation of structure bottom for wind height adjustment: 0.00 (ft)
Structure height for structure gust response factor: 180.00 (ft)
Structure ust response factor, Gh: 0.8500
Mean wind conversion factor, m: 0.6000
Wind direction probability factor, Kd, for structures: 0.85, for appurtenances: 0.85
Structure fundamental frequency, fi: 2.0199 (Hz)
Guy installation temperature: 60.00 (deg F)
Tower Type: Triangular Latticed

Tower Type: Triangular Latticed
ANSI/TIA 222-G Load Options:
Structure Class
Exposure Category
Topographic Category
Topographic Category 3 (Kzt calculated based on crest height, H, of 36.00 (ft))
Spectral Response SDS 0.276
Spectral Response SDI 0.112

## EIA Rev. G Load Cases:

	Load Case Dead Load	bead Load W	find Load S	strength	Load	BASIC W	LDG Mean	MING ME	STI WITH	)	)	THE PERSON NAMED IN COLUMN	3	1
	Description	Factor	Factor Factor	Factor	Case	Wind D	Ľ.	Start	Stop	Thick.	Density		Loads	Displ.
	•				Type	Speed (Do	Eler	ration El	evation (ft)	(in) (1	Speed Elevation Elevation (in) (lbs/ft^3) (ft) (ft)	(deg F)		
		State							*******					
1 2000 1 6WA + 1 6WA 1 2000	000 + 1 6Wo	1.2000	-	1.0000	Regular	94.000	0	00.0	00.00	0.000 0.0000	0.0000	0*09		
2 T T T T T T T T T T T T T T T T T T T	000 + 1 6MO	00000	1 6000	1 0000	Regular	94.000	0	00.0	0.00	0.000	0.0000	0 09		
1 20 1 7	1 - PGO		1 0000	1 0000	Earthquake	00000	0	0.00	00.00	0.000	0.0000	0.09		
1.120 + 1	. oby + 1.05		1 0000	1 0000	Earthonake	0.00.0	0	00.00	00.00	00000	000000	0 * 09		
1 + 06.0 : 6 :	. UDG + T. UE	0000	00001	1 0000	Service	60.000	0	0.00	00.00	0.000	0.0000	0.09		
6: SELVICE 1:0D + 1:0Dg + 1:0 WG	1 2*DI.		1 0000	1.0000	Requiar	0.000	0	00.0	00.00	0.00 0.0000	000000	0.09		
	O GDI.		1 0000	1.0000	Regular	0.000	0	00.0	00.00	0.000.0	0.0000	0.09		

## Equipment Load Case Information for "1: 1.2D + 1.0Dg + 1.6Wo":

Equipment	Equipment E	Elevation qzGh		Ice 1	Fotal Wind	find 222-G	222-G		Antenna	Antenna	~	Long.	Trans.	Vert.
rabe1	Property	Above	Thi		Wind Incide			3	AXLAL Load FAM	Load FAM Load FSM	MW I	LOZO		9
		(ft) (psf)		(in)		(deg)			(1bs)	(3dT)	(ft-1bs)	(1bs)	(1bs)	(1bs)
DNK-1	מוסהים . ה	86 00 35		į	3,95	0.00						140.22	0.00	60.00
T NING -TM	Stand-Off	60.00 35.				00.00						96.46	00.00	60.00
NNK2-GPS 68	SES	60.00 35.	35.46	0.00		120.00						35.46	0.00	12.00
MT-DNK2	3 Stand-Off	60.00 35.				00.00						96.46	0.00	00.09
DNK3-GPS69	Sab	60,00 35.				00.00						35.46	00.00	12.00
MT-DNK3	3 Stand-Off	60.00 35.				00.00						96.46	00.00	00.09
DNK4-DOT56	10 Dipole	60.00 35.				00.00						325.08	00.00	55.20
MT-DNK4	3 Stand-Off	60.00 35				00.00						96.46	00.00	00.09
DNK5-NEIT16	6 Omni	80.00 36,				00.00						73.49	00.00	00.9
MT-DNK5	6 Stand-Off	80.00 36.				00.00						389.50	00.00	.68.00
DNK9-DEP54	RFS PD1142 w/ ice	120.00 39.				00.00						52.09	00.00	12,00
WT-TM	3 Stand-Off	120.00 39				00.00						107.66	00.00	00.09
DNK8-CSP66	RFS PD1142 w/ ice	120,00 39				00.00						52.09	00 "0	12.00
DNK7-NEU17	12 Omni	113.34 39				00.0						156.52	00.00	90.99
MT-DNK7	3 Stand-Off	113,34 39				00.0						106.43	00.00	00.09
Sprint	12 T-Arm	113.34 39				00.00						532.17	00.00	558.00
Sprint-B	12 T-Arm	113,34 39				0.00						532.17	00.00	558.00
Spring	12 T-Arm	113,34 39				0.00						532.17	00 0	558.00
Sprint-1	RFS APXVSPP18-C w/ ice	113,34 39				0.00						323.21	0.00	108.00
Sprint-2	ALU RRH	113.34 39				0.00						269.87	0.00	72.00
Sprint-3	ALU RRH	113.34 39				0.00						269.87	00.00	72.00

120.00 120.00 120.00 240.00 240.00 240.00 240.00 240.00 240.00 240.00	240.00 240.00 270.00	00000
9009000000044 0000000000000000000000000	133.60 133.60 133.97	5.88 2.99 1.29 1.79
	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	41.44 41.44 41.44 41.44 41.44
	Boom Gate 126,66 66 66 80-XY w/ ice 126,66 66 80-XY w/ ice 126,66 68 80-XY w/ ice 126,66 68 80-XY w/ ice 126,66 59-R3B Panel 126,66 59-R3B Panel 126,66 59-R3B Panel 126,66 59-R3B Panel 126,66 125-R3B Panel 125,23-34 125-R3B Panel 125,23-34 125-R3B Panel 125,23-34 125-R3B Panel 125,23-34 125,24-R3B Panel 125,250.00	7770 Unit 1101) 1101)
RES ADXVSPD18-C w/ ice ALU RRH RES ADXVSPD18-C w/ ice ALU RRH DT465B-2XR-V2 BOO MHZ RRH Unit GOO MHZ RRH Unit TD-RRH 8x20-25 RRH Unit TD-RRH 8x20-25 RRH Unit	cibel DB844H86 JAHH-65E JAHH-6	Powerwave RRHU-11 RRH TWA Unit (LGP2/ TMA Unit (LGP2/ Raycap Surge Suppr
Sprint-4 Sprint-5 Sprint-5 Sprint-7 Sprint-9 Sprint-10 Sprint-12 Sprint-12 Sprint-13 Sprint-13 Sprint-13 Sprint-13 Sprint-13 Sprint-13 Sprint-14 Sprint-15 Sprint-15	BSAMNT-BSSAMNT-RSAMNT-R	ATT-A2 ATT-A3 ATT-A4 ATT-A5 ATT-A6

0.00 108.00 0.00 72.00 0.00 172.00 0.00 172.00 0.00 106.08 0.00 106.08 0.00 106.08 0.00 106.08 0.00 106.08 0.00 106.08 0.00 106.08 0.00 12.00 0.00 12.

2269.987 2269.987 2269.987 2269.987 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.87 2269.73 2269.20 22

1707577071	TMA Unit (LGP24101)	Suppressor	
TITO THAT	TMA Unit	Raycap Surge (	
177 7 777	ATT-A5	ATT-A6	URS Connecticut - 4-carir

419, 44 0.00 76,80 160.74 0.00 96,00 96,00 160.74 0.00 16,92 53,37 0.00 16,92 419,44 0.00 96,00 16,92 419,44 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 16,92 160.74 0.00 96,00 160.76 174.24 0.00 96,00 174.24 0.00 96,00 174.24 0.00 96,00 174.24 0.00 96,00 174.24 0.00 175,00 1	
9 50.04	
1860.78	
0.00 120.00 120.00 120.00 120.00 120.00 240.00	120.00 240.00
10.12 3.88 1.29 1.29 1.29 1.29 1.29 2.30 2.30	0.83
	0.00
150.00 41 150.00 41 150.00 41 150.00 41 150.00 41 150.00 41 150.00 41 150.00 41 150.00 41 160.00 42 160.00 42 175.00 42	126.66 40.02 126.66 40.02
RRUG-32 RRH Unit RRHU-12 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit RRUG-32 RRH Unit RRUG-32 RRH Unit RRHU-11 RRH Unit TWA Unit (LGE24101) OPA-65-LCUU-H6 Panel RRUG-32 RRH Unit Sinclair SC479-HFILDF W/ ice Sinclair SC479-HFILDF W/ ice Sinclair SC479-HFILDF W/ ice Sinclair SC479-HFILDF W/ ice Scala OGT9-806 W/ ice Decibel PD-420 & bay- Dipole Sinclair SC479-HFILDF W/ ice Scala OGT9-806 W/ ice Scala OGT9-806 W/ ice Scala OGT9-806 W/ ice Scala OGT9-806 W/ ice Decibel PD-420 & bay- Dipole 6 & Stand-Off 770 POWERWANG 7770 POWE	CBC78T-DS-43-2X CBC78T-DS-43-2X
ATT-A7 ATT-B1 ATT-B1 ATT-B2 ATT-B2 ATT-B3 ATT-B4 ATT-B4 ATT-C2 ATT-C1 ATT-C1 ATT-C2 ATT-C1 ATT-C3 ATT-C3 ATT-C4 ATT-C4 ATT-C5 CSP-71 CSP-72 CSP-74 DNK23-STAM64 DNK23-STAM64 DNK23-STAM64 DNK23-STAM65 DNK23-STAM65 DNK23-STAM65 DNK23-STAM65 DNK23-CSP2 DNK23-STAM65 DNK23-CSP2 DNK23-CSP2 DNK23-CSP2 DNK23-CSP2 DNK23-CSP2 DNK23-CSP2 DNK28-CSP2 TOP-C2 TOP-C2 ATT-B7 ATT-B7 ATT-C7	Verizon-32 Verizon-33

EIA Section Load Case Information for "1: 1.2D + 1.0Dg + 1.6Wo":

Note: qzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh), Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads)
Face RR is the minimum round reduction factor for all round angles and appurtenances in the section

Total Weight (1bs)	6708 7161 7967 8794 11980
Total T Wind We (1bs)	6777 8732 10521 10805 11081 10864
Note To WA 1 (1bs) (	3403 4973 6437 1 6224 1 5995 1 5769 1
NotF 1 AR*CAR (ft^2) (:	000000
NotF NotF NotF AAR CAR AAR*CAR (ft^2) (ft^2)	0.00 0.60
Noti AAE (ft^2)	
NotF	22.000
NotF AAF (ft^2)	40.00 2.00 60.00 2.00 80.00 2.00 80.00 2.00 80.00 2.00
Face WF (1bs)	3374 3760 4084 4581 5086
Face AE (ft^2)	32.7 37.7 41.7 49.7 58.0
Face Face Face Face Face Face	2 43 2 43 2 43 2 34 2 34
Face	0.58
Face	000000
Face	1 000 1
F B B C B	0.25
Face AG ft^2)	163.7 191.0 218.3 245.5 272.8
Face RR*AR Et^2)	12.12 15.20 15.99 15.99 19.30
Ice Face Face Face Face ick. AF AR RR*AR AG (in) (ft^2) (ft^2) (ft^2)	0.00 22.52 21.02 12.12 163.7 0.25 1.00 1.00 0.58 2.43 0.00 25.52 27.30 15.20 191.0 0.26 1.00 1.00 0.55 2.41 0.00 0.25 73 29.16 15.99 218.3 0.25 1.00 1.00 0.55 2.41 0.00 30.37 36.61 19.30 245.5 0.27 1.00 1.00 0.55 2.37 0.00 37.01 40.26 22.96 272.8 0.28 1.00 1.00 0.50 2.34 0.00 37.01 40.26 20.96 272.8 0.28 1.00 1.00 0.50 2.34 0.00 37.01 40.26 20.96 272.8 0.28 1.00 1.00 0.50 2.34
Face AF ft^2)(	20.58 22.52.52 25.73 30.37 37.01
Ice Face Face Face Thick. AF AR RR*AR (in) (ft^2) (ft^2) (ft^2)	
- 1	70.00 42.54 50.00 41.44 30.00 40.23 10.00 38.90 90.00 37.00
Elev. ve Gnd. (ft)	170.00 42.54 150.00 41.44 130.00 40.23 110.00 38.90 90.00 34.47
Z of Z of Ave. Elev. Top Bottom Above Gnd. (ft) (ft) (ft)	20.00 20.00 20.00 30.00
Z of Top Bo (ft)	A 180.00 160.00 B 160.00 140.00 C 140.00 120.00 D 120.00 100.00 F 100.00 80.00
Section Label	A 180,00 160,00 170,00 42.55 B 150,00 140,00 150,00 41.44 C 140,00 120,00 110,00 40.22 D 120,00 100,00 110,00 38.92 E 100,00 80,00 37.47 F 60,00 60,00 70,00 37.47

. 6Wo"
Η.
1.0Dg +
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0.90
 2
for
Information
Case
Load
Equipment

		Vert. Load	(1bs)	45.00	9.00	45.00	45.00	41.40	45.00	126.00	9.00	9.00	49.50	43.00	418,50	418.50 81.00	54.00	54.00	54 00	54.00	81.00	54.00	79.56	79.56	79.56	54.00	54.00	59.52	59.52	423.90	423.90	9.00	00.6	00.6	9.00	9.00	113.67	113.67	113.67	113.67	104.40	104.40	40.50	49.50	45.00
14075 14983 15101		Trans. Load	(Ed.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	0.00	0.00	00.00	0.00	0.00	00.00	0.00	0.00	00.00	0.00	0.00
11187 11916 15073		Long. Load	(1bs)	140.22	35.46	96.46	35.46	325.08	73.49	389,50	52.09	52.09	156.52	532.17	532.17	323.17	269.87	269.87	323.2I	269.87	323.21	269.87	377.47	377.47	377.47	269.87	269.87	184.68	184.68	544.21	544.21	158.73	158.73	158.73	158.73	158.73	386.55	386.55	386.55	386.55	151,42	151.42	224.08	160.06	53.22 109.99
5612 5716 6256		ntenna Moment MM	ps)																																										
00.0		4	(ft-1bs)																																										
0.60		Antenna Side	(1bs)																																										
0.00		nna ial waw	ps)																																										
2.00		-G Ante																																											
80.00 80.00 72.00		222																																											
5575 6200 8816		222-G CS																																											
67.9 73.7 89.2		222-G CA																																											
0 2.34 9 2.35 1 2.28		Wind	(deg)	00.	00.	00.	00.	00.0	00.0	00.0	00.	00.00	00.0	00.00	00.0	00.00	00.	00.00	00.00	00.0	00.0	00.00	00.0	00.00	00.00	00.00	00.0	00.00	00.00	00.00	00.0	00.00	00.0	00.0	00.00	00.0	00.0	00.00	00.0	00.0	00.00	00.0	00.00	00.00	120.00
1.00 0.50 1.00 0.49 1.00 0.51		Wind Incidence	20																																										
1.00 1. 1.00 1. 1.00 1.			(£t^2)	3.95																																									
0.28 0.28 0.31		Ice Thick.	(in)	0.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	0.00	0.00	0.00	00.00	0.00	0.00	00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
327.3 354.6 381.9		qzGh	(bsf)	35.46	35.46	35.46	35.46	35.46	35.46	36.75	39.58	39.58	39.13	39.13	39.13	39. L3	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	39.13	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.02	40.44
37 25.59 83 25.68 17 29.86	1.6Wo":	Above		60.00	60.00	60.00	00.09	60.00	80.00	80.00	120.00	120.00	113.34	113.34	113.34	113.34	113.34	113.34	113 34	113.34	113.34	113.34	113.34	113.34	113.34	113.34	113.34	113.34	113.34	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	126.66	133.34
28 50 37 05 50 83 30 58 17	Dg + 1	回	ָ ֓֞֞֜֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓														RRH		1Ce																										
0.00 42.2 0.00 48.0	0.90 + 1.0	Equipment Property	2	5 Dipole	o called G	Stand-0	Stand-0	10 Dipo	Stand-C	Stand-C	PD1142 w/ i	PD1142 w/ i	12 Omni	12 T-P	12 T-P	1 3	ALU		APXVSPPI8-C W/			ALU F	65B-2XR-	65B-2XR-	65B-2XR-	IZ RRH Ur	Z RRH Ur	S RRH Ur	5 RRH Ur	Boom Ga	Boom Ga	-XY w/	-XX w/	/M XX-(	/w XX-(	/M XX-(	3-R3B Par 3-R3B Par	3-R3B Par	3-R3B Par	3-K3B Par 3-R3B Par	WHH Anter	WHH Anter	1-5B5-2-2 Mount 10r JARR Anter Raycap DB-T1-62-8AB-02 Dist. P	12` Or	RES PDII42 w/ ice 3` Stand-Off
	"2: 0.			ć	1	'n	'n		'n	,9	RFS PD1	RFS PD1	ć	า		LZ APXVSPD18-C	11000	0	XVSPPI		XVSPP1		DT4	DT4	DT4	800 ME	800 MF	8x20-2	8×20-2			844H8(	844H8(	844H8( 844H8(	844HB(	844HB	.HH-65E	HH-65E	HH-65E	HH-651	for JA	for J	8AB-02		3.50
50.00 35.08 30.00 35.73 10.00 43.45											25	K				PFC AP			RES AP		RES AP							O-RRH	O-RRH			sel DB	bel DB	oel DB	oel DB	bel DB	AD.	A.D.	J.A.	AU.	Mount	Mount	Mount T1-6Z-	'	x,
30	mation																-	,	-4		ш							E	1 2			Decil	Decil	Decil	Decil	Deci					5-2-2	3-2-2	ap DB-	4	
40.00 20.00 0.00	Case Information for																																								SAMNT-SB	-E BSAMNT-SBS-2-2 Mount for JAHH Antenna	SAMINI-SB Rayo		
60.00 40.00 20.00		pment Label		DNK-1	368 S	NK2	869 8K3	T56	NK4	NK5	P54	.P66	U17	t-A	ıt-B	1t-C	it 2 it-2	1t-3	1t-4 +-5	1t-6	1t-7	1t-8	-10	:-11	-12	-14	:-15	-16	:-18	A-uc	Nn−B N−r∨	un-1	2-uc	on-3	2-uc	9-uc	7-400	0-IIC	1-10	n-11 n-12	on-D B	B 3-uc	21-12 1-22	7-18	SPZ1 WK15
G H H A 2	Equipment Load	Equipment Label		DNK-1	DNK2-GPS68	MT-DNK2	DNK3-GPS69 MT-DNK3	DNK4-DOT56	MT-DNK4	MT-DNK5	DNK9-DEP54	DNK8-CSP66	DNK7-NEU17	Sprint-A	Sprint-B	Sprint-C	Sprint-2	Sprint-3	Sprint-4	Sprint-6	Sprint-7	Sprint-8	Sprint-10	Sprint-11	Sprint-12	Sprint-14	Sprint-15	Sprint-16	Sprint-10	Verizon-A	Verizon-B	Verizo	Verizon-2	Verizo	Verizon-5	Verizon-6	Verizon-/	Verizon-9	Verizo	Verizon-II	Verizon-D	Verizon-E	Verizon-22	NEU-18	DNKIS-CSFZI MT-DNK15
	Eq.																																												

	0.00 504 0.0
159.89 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.20 264.34 45.46 45.46 45.46 45.46 121.07 121.07 121.09 29.31 29.31 29.31 29.31 29.31 419.40 419.40 610.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74 160.74	1869.10 274.26 274.26 114.24 114.24 114.24 42.85 276.03 392.30 138.21 216.84 97.29 97.29 97.29 97.29 126.44 22.99 456.33
	50.04
	927.29
ž	.66410 0.08980 -0.06910
240.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	240.00 240.00 120.00 120.00 120.00 240.00 50.00 1.20.00 1.20.00 1.20.00 1.20.00 1.20.00 1.20.00 1.20.00
3.955 2.725 6.533 6.533 6.533 7.384 7.	
133, 34 40, 44 135, 00 41, 44 150, 0	160.00 42.00 160.00 42.00 160.00 42.00 160.00 42.00 160.00 42.00 160.00 42.00 165.00 42.27 165.00 42.27 175.00 42.80
5. Dipole 3. Stand-Off Ericsson AIR B2A/B4P ARR32 B66/B2A TWIN TWA Unit - Generic DIPOLESSON 4478 (B71) RRH Unit Ericsson 4478 (B71) RRH Unit Ericsson 4478 (B71) RRH Unit Ericsson 4478 (B71) RRH Unit DIPOLESSON UNIT - Generic DIPOLESSON UNIT (LGEP24101) TWA UNIT (LGEP24101)	A A A A A A A A A A A A A A A A A A A
DNK-12 MT-DNK12 T-Mobile-3 T-Mobile-3 T-Mobile-5 T-Mobile-6 T-Mobile-9 T-Mobile-9 T-Mobile-10 T-Mobile	CSP-73  DWK21-STPM63  DWK19-STPM63  DWK21-STPM63  159-B  160  DWK23-STPM64  DWK23-STPM65  GRW-1 (DWK25)  DWK23-STPM65  DWK26-CSP 74  DWK27B-CSP 74  DWK28C-TCG 59  DWK28C-TCG 59  DWK28C-TCG 59  DWK28C-TCG 59  DWK28C-TCG 50  DWK28C-T

456.33 0.00 126.00 456.33 0.00 126.00	0.00	0.00	0.00	00.00	00.0	00.00	00.00	00.00	00.00	00.00	00.00	00.00
4 4	24	24	24	12	12	12	12	12	12			
260.00	120.00	120.00	240.00	00.00	120.00	240.00	00.00	120.00	240.00	0.00	120.00	240.00
10.60	5.88	5.88	5.88	3.13	3.13	3,13	3.13	3.13	3.13	0.83	0.83	0.83
0.00	00.00	0.00	0.00	00.0	00.0	0.00	00.00	00.0	0.00	0.00	00.00	00.0
180.00 43.05	150.00	150.00	150.00	126.66	126.66	126,66	126.66	126,66	126,66	126.66	126,66	126.66
6 Stand-Off 6 Stand-Off	Powerwave 7770	Powerwave 7770	Powerwave 7770	RRH B2/B66A (REV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	CBC78T-DS-43-2X	CBC78T-DS-43-2X	CBC78T-DS-43-2X
Top-C1 Top-C2	ATT-B7	ATT-B8	ATT-C8	Verizon-25	Verizon-26	Verizon-27	Verizon-28	Verizon-29	Verizon-30	Verizon-31	Verizon-32	Verizon-33

ELA Section Load Case Information for "2: 0.9D + 1.0Dg + 1.6Wo":

Note: qzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh), Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads)
Face RR is the minimum round reduction factor for all round angles and appurtenances in the section

Н	ų	_	n	Į	S	9	2	S	9	7	,
Total			100				8985				
Total	Wind	(1ps)	6777	8732	10521	10805	11081	10864	11187	11916	000
Note							5995				
Note			0.00	00.00	00.0	00.00	00.00	00.00	00.00	00.0	0
NotF	CAR A		09.0	09.0	09.0	09.0	09.0	09.0	09.0	09:0	
NotF 1		(ft^2)	0.00	00.0	00.00	00.00	0.00	00.0	0.00	0.00	-
NotF	CAF	_	2.00	2.00	5.00	2.00	2,00	2.00	2.00	2,00	
Note 1	_	(ft^2)	40.00 2	60.00	80.00	80.00	80.00	80.00	80.00	80.00	
Face	WE	(1bs)	3374	3760	4084	4581	9809	5095	5575	6200	
Face	AE	(ft^2)	32.7	37.7	41.7	49.7	58.0	59.5	67.9	73.7	
Face	CE		2.43	2.41	2.43	2.37	2.34	2.38	2.34	2.35	
Face	RR		0.58	0.55	0.55	0.52	0.50	0.50	0.50	0.49	
Face Face	DR		1.00	1,00	1.00	1:00	1,00	1,00	1.00	1.00	-
Face	DF		1.00	1.00	1.00	1,00	1,00	1,00	1.00	1,00	
Face	a		0.25	0.26	0.25	0.27	0.28	0.27	0.28	0.28	
Face	AG	ft^2)	163.7	191.0	218.3	245.5	5 272.8 0.28	300.0	327.3	354.6	
ace	Z*AR		12.12	15.20 1	15.99 2	9.30 2	3.96.0	2.14 3	5.59	5.68	1
ace I	AR RE	^2) (£1	.02 12	27.30 15	29.16 15	.61 19	0 37.01 40.26 20.96 2	.90 22	.37 25	.83 2!	1
Se Fa	F	2) (ft,			73 29.	37 36.	01 40.	32 43.	28 50,	05 50.	1
Fac	7	(ft,	0 20.58	) 22.52	0 25.73	30.3	37.(	37.	7 42.2	7 48.(	
Ice Face Face Face	Thick,	(in)	00.0	00.00	0.0	0.0	0.0	0.0	0.0	0.0	-
dzGh	£*1	(psf)	170.00 42.54	11.44	10.23	38.90	37.47	36.06	35.08	35.73	
lev.	3nd.	(£t)	170.00 4	0.00	00.0	00.0	00.0	00.0	00.0	00.0	1
ve. E.	bove (		17(	15(	13(	11(	ര്	71	5	ĕ	
Z of An	ottom Al	(ft) (ft) (ft) (psf)	A 180.00 160.00	40.00	20.00	00.00	80.00	60.00	40.00	20.00	4
z of	Top B	(ft)	0.00 1	0.00 1	0.00 1	0.001	00.0	00.00	00.0	00.0	4
			A 180	B 160	C 14(	D 12(	E 10(	F 8(	G 61	H 4(	1
Section	Label										

Equipment Load Case Information for "4: 1.2D + 1.0Dg + 1.0E":

(ft) (psf) (in) (ft^2)  (ft) (psf) (in) (ft^2)  60.00 0.00 0.00 3.95  60.00 0.00 0.00 1.72  60.00 0.00 0.00 1.72  60.00 0.00 0.00 2.72  60.00 0.00 0.00 2.72  80.00 0.00 0.00 2.72  80.00 0.00 0.00 2.72  80.00 0.00 0.00 2.72  120.00 0.00 0.00 2.72  120.00 0.00 0.00 2.72  120.00 0.00 0.00 2.72  120.00 0.00 0.00 2.72  120.00 0.00 0.00 1.32  113.34 0.00 0.00 13.60  113.34 0.00 0.00 13.60  113.34 0.00 0.00 13.60  113.34 0.00 0.00 13.60  113.34 0.00 0.00 8.26  113.34 0.00 0.00 8.26  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90  113.34 0.00 0.00 6.90	Equipment Label	Equipment Elevation Property Above	levation Above	qzGh	Ice Thick.	Total Wind I	otal Wind Wind Incidence	222-G CA	222-G CS	222-G CM	Antenna Axial	Antenna Side	Antenna Long. Moment Load	Long.	Trans. Load	Vert. Load
Pole 60.00 0.00 0.00 3.95 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0		Set	Ground (ft)	(psd)	(in)	Area (ft^2)	Angle (deg)				Load FAM (1bs)	Load FSM (1bs)	MW (ft-1bs)	_	(lbs)	(1bs)
Color   Colo		5` Dipole	60.00	0.00	00.00	3.95	0.00					1		0.00	#S	60.00
GES 60.00 0.00 0.00 1.00 120.00 0.00 0.00 0.0		3 Stand-Off	60.00	00.00	0.00	2.72	00.00							0.00		00.09
H-Off 60.00 0.00 0.00 2.72 120.00 0.00 0.00 0.00 0.00 0.00 0.00 0		GPS	60.00	00.00	0.00	1.00	120.00							00.0		12.00
Control   Cont		Stan	60.00	0.00	0.00	2.72	120.00							00.0		60.00
H-Off 60.00 0.00 0.00 2.72 240.00 0.00 0.00 0.00 0.00 0.00 0.00 0		GPS	60.00	00.0	0.00	1.00	240.00							0.00		12.00
Post		3 Stand-Off	00.09	0.00	0.00	2.72	240.00							00.0	_	60.00
1.5   1.5		10 Dipole	60.00	00.0	00.00	9.17	240.00							0.00		55.20
Omni 80.00 0.00 0.00 240.00 0.00 0.00 0.00 0.0		3 Stand-Off	60.00	0.00	00.0	2.72	240.00							00.00		60.00
		8 Omni	80.00	00.00	00.00	2.00	240.00							0.00		6.00
12.00   0.00   0.00   1.32   120.00   0.00   1.32   120.00   0.		6 Stand-Off	80.00	00.00	00.00	10.60	240.00							0.00		168.00
		RFS PD1142 w/ ice	120.00	00.00	00.00	1.32	120.00							0.00		12.00
13.34   0.00   0.00   1.32   120.00   0.00		3 Stand-Off	120.00	00.0	0.00	2.72	120.00							0.00		60.00
Omni 113.34 0.00 0.00 4.00 0.00 0.00 0.00 0.00		RFS PD1142 w/ ice	120.00	00.0	0.00	1.32	120.00							0.00		12.00
13.34 0.00 0.00 0.00 0.00 0.00 0.00 0.00		12 Omni	113.34	0.00	00.0	4.00	00.00							00.00		66.00
Arm 113.34 0.00 0.00 13.60 0.00 0.00 0.00 0.00 0.00 0.00 0.00		3 Stand-Off	113.34	0.00	00.0	2.72	00.00							00.00	00.0	60.00
Arm 113.34 0.00 0.00 13.60 120.00 0.00 0.00 0.00 0.00 0.00 0.00 0		12 T-Arm	113.34	0.00	0.00	13.60	00.00							0.00	00.0	558.00
		12 T-Arm	113.34	0.00	00.0	13.60	120.00							0.00		558.00
13.34   0.00   0.00   8.26   0.00		12 T-Arm	113.34	0.00	00.00	13.60	240.00							0.00		558,00
J RRH 113.34 0.00 0.00 6.90 0.00 0.00 0.00 0.00 0.00		RFS APXVSPP18-C w/ ice	113.34	0.00	00.0	8.26	00.00							00.00		108.00
NEW   113.34   0.00   0.00   6.90   0.00		ALU RRH	113.34	0.00	00.0	6.90	00.00							0.00		72.00
/ ice 113.34 0.00 0.00 8.26 120.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		ALU RRH	113.34	0.00	00.00	6.90	00.00							00.00		72.00
J RRH 113.34 0.00 0.00 6.90 120.00 0.00 0.00 0.00 0.00 0.00 0.00 0		RFS APXVSPP18-C w/ ice	113.34	00.0	00.00	8.26	120.00							0.00		108.00
7 RRH 113.34 0.00 0.00 6.90 120.00 7 0.00 0.00 0.00 0.00 0.00 0.00 0.		ALU RRH	113.34	0.00	00.00	6.90	120,00							00.00		72.00
/ ice 113.34 0.00 0.00 8.26 240.00 0.00 13.34 0.00 0.00 6.90 240.00 0.00		ALU RRH	113.34	00.0	0.00	6.90	120.00	880						00.00		72.00
J RRH 113.34 0.00 0.00 6.90 240.00		RFS APXVSPP18-C w/ ice	113.34	00.0	0.00	8.26	240.00							0.00		108.00
		ALU RRH	113,34	0.00	0.00	6.90	240.00							00.00		72.00

240.00 120.00	120.00 240.00 240.00 120.00 240.00 120.00 240.00 0.00 0.00 0.00 0.00 0.00 0.
6.55 6.50	1.26 1.26 0.72 0.72 0.72 0.72 13.60 13.60 13.60 1.29 1.29 1.29 1.29 1.29
1113.34 1113.34 1113.34 1113.34 1113.34 1113.34 1113.34 1126.66 66	
Dec Dec Dec Dec SAMNT—SBS—2— SAMNT—SBS—2— SSAMNT—SBS—2— SSAMNT—SBS—2—	Ericsson 4478 (871) RRH Unit Ericsson 4478 (871) RRH Unit Ericsson 4478 (871) RRH Unit Diplexer Unit - Generic Diplexer Unit - Generic Diplexer Unit - Generic 12 'T-Arm Powerwave 7770 Powerwave 7770 Powerwave 7770 Powerwave 7770 Powerwave 7770 Powerwave 7770 RRHU-11 RRH Unit TWA Unit (LGP24101) RAYORD Surge Suppressor OPA-65-LCUU-H6 Panel RRUS-32 RRH Unit
Sprint-9 Sprint-12 Sprint-12 Sprint-13 Sprint-15 Sprint-15 Sprint-15 Sprint-16 Sprint-16 Sprint-16 Sprint-17 Sprint-17 Sprint-17 Sprint-17 Sprint-17 Sprint-17 Sprint-17 Verizon-2 Verizon-2 Verizon-10 Verizon-1	T-Mobile-16 T-Mobile-17 T-Mobile-19 T-Mobile-19 T-Mobile-20 T-Mobile-20 T-Mobile-20 ATT-8 ATT-8 ATT-A4 ATT-A4 ATT-A5 ATT-A6 ATT-A7 ATT-A7 ATT-A8 ATT-B2

72.00 106.08 106.08 72.00 72.00 72.00 79.36 79.3

0.00 0.00 16.92 0.00 0.00 16.92 0.00 0.00 16.92 0.00 0.00 16.92 0.00 0.00 16.92 0.00 0.00 16.92 0.00 0.00 18.00 0.00 0.00 40.80 0.00 0.00 672 0.00 0.00 672 0.00 0.00 672 0.00 0.00 672 0.00 0.00 672 0.00 0.00 18.00 0.00 0.00 18.00 0.00 0.00 144.00 0.00 0.00 144.00 0.00 0.00 168.00 0.00 0.00 188.00 0.00 0.00 188.78	0.00
1.66410 0.08980 -0.06910	
120.00 240.00	120.00
10.12 3.88 2.99 10.12 10.1	0.83
	0.00
	0.00
150.00 150.00 150.00 150.00 150.00 150.00 150.00 160.00 175.00 17	126.66 126.66
OPA-65-LCUU-H6 Panel RRNB-32 RRH Unit RRNB-32 RRH Unit RRNB-32 RRH Unit Sinclair SC479-HFLIDF W, ice 3° Stand-Off 3° Stand-Off 3° Stand-Off 3° Stand-Off 3° Stand-Off 4° XI' Panel 4° XI' Panel 4° XI' Panel 5° Stand-Off 8° Sinclair SC479-HFLIDF W, ice Scala OGT9-806 W, ice Decibel PD-420 2 bay Dipole 6° Stand-Off 770 POWERWAVE 7770 PO	CBC78T-DS-43-2X CBC78T-DS-43-2X
ATT-B4 ATT-B5 ATT-C2 ATT-C2 ATT-C3 ATT-C3 ATT-C3 ATT-C4 ATT-C4 ATT-C3 ATT-C4 ATT-C3 ATT-C3 ATT-C4 ATT-C3 ATT-C4 ATT-C3 ATT-C4 ATT-C4 ATT-C6 CSP-71 CSP-71 CSP-72 CSP-72 CSP-73 CSP-73 CSP-73 DNK20-UNKNOWN DNK21-STPAM63 DNK22-STPAM64 DNK22-STPAM64 DNK22-STPAM64 DNK22-STPAM64 DNK22-STPAM64 DNK22-CSP1 DNK23-STPAM65 CSP1 DNK22-CSP1 DNK23-STPAM65 CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP1 DNK28-CSP2 DNK28-CSP3 DNK28-CSP1 DNK28-CSP3 DNK28-CSP3 UNC28-CSP3 DNK28-CSP3 UNC28-CSP3 UNC28	Verizon-32 Verizon-33

EIA Section Load Case Information for "4: 1.2D + 1.0Dg + 1.0E":

Note: gzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh), Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/ELA Loads)
Face RR is the minimum round reduction factor for all round angles and appurtenances in the section

Label Top Bottom Above Gnd. Thick. AF AR RR*AR AG e (ft) (ft) (ft) (ft) (in) (ft^2) (ft^2) (ft^2)
0.00 20.58 21.02 12.32 163.7 0.25 1.
0.00 22.52 27.30 16
0.00 25.73 29.16 17
0.00 30.37 36.61 21
0.00 37.01 40.26 23
0.00 37.32 43.90 25
0.00 42.28 50.37 29
0.00 48.05 50.83 30
0.00 59.30 58.17

Equipment Load Case Information for "5: 0.9D + 1.0Dg + 1.0E":

Vert. Load (1bs)	45.00 45.00 45.00 45.00 45.00 45.00 45.00 45.00 418.50
Trans. Load (1bs)	
· 10 ~	
Antenna Long Moment Loam MM (ft-lbs) (lbs	
Antenna Side Load FSM (1bs)	
Antenna Axial Load FAM 1	
222-G Ar CM Los	
222-G CS	
222-G CA	
Wind Incidence Angle (deg)	0.00 240.00
Total Wind In Area (ft^2)	13.95 1.02 1.02 1.03
Ice Thick. (in)	
qzGh T (psf)	
Elevation Above Ground (ft)	60.00 60
Equipment El Property Set	5. Dipole 3. Stand-Off 10. Dipole 3. Stand-Off 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 13. Stand-Off 14. Stand-Off 15. Stand-Off 16. Stand-Off 17. Ombi 18. Stand-Off 19. T-Arm 19.
Equipment Label	DNK-1 DNK-2GS88 NT-DNK2 DNK-GP869 NT-DNK3 DNK4-GP869 NT-DNK5 NT-DNK5 DNK4-DNF9 NT-DNK5 DNK4-DNF9 NT-DNK7-NEU17 NT-DNK7-NEU17 NT-DNK7-NEU17 NT-DNK7-NEU17 NT-DNK7-NEU17 Sprint-1 Sprint-

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	Grē		-0.06910
000000000000000000000000000000000000000	\$ 000000000000000000000000000000000000	000 000 000 000 000 000 000 000 000 00	1.66410 0.08980
	1,26 0,000 1,26 242,000 0,72 120,000 0,72 240,000 13,60 120,000 13,60 120,000 5,88 0,000 5,88 0,000 1,29 0,000 1,29 0,000 1,29 0,000 1,29 1,20,000 1,29 1,20,000		50 50 50 50 50 50 50 50 50 50
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	1333333344 13333333444 150000000000000000000000000000000000	15000000000000000000000000000000000000	165.00 175.00
Ericsson AIR B2A/B4P ARXVAA24 43-U-A20 (RES) Ericsson AIR B2A/B4P ARX23 B6/B2A APXVAA24 43-U-A20 (RES) Twin TWA Unit - Generic Twin TWA Unit - Generic Twin TWA Unit - Generic Twin TWA Unit - RRHU-11 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit	Ericsson 4478 (B71) RRH Unit Ericsson 4478 (B71) RRH Unit Ericsson 4478 (B71) RRH Unit Diplexer Unit - Generic TAXTM	RRUS-32 RRH Unit RRHU-11 RRH Unit RRHU-11 RRH Unit TMA Unit (LGE24101) OPA-65-LCUU-46 Panel RRUS-32 RRH Unit Sinclaix SC479-HFILDF w/ ice Sinclaix SC479-HFILDF w	4'x1' Panel TMA 4' Dish Dipole 4' Disole Sinclair SC479-HFILDF W/ ice Scala OGT9-806 W/ ice Stala OGT9-806 W/ ice Scala OGT9-806 W/ ice Andrew DB-583 W/ ice Decibel PO-420 2 bay - Dipole 6' Stand-Off 6' Stand-Off 6' Stand-Off 6' Stand-Off 6' Stand-Off 7700 POWEYWAVE 7770 POWEYWAVE 7770
T-Mobile-4 T-Mobile-5 T-Mobile-6 T-Mobile-8 T-Mobile-9 T-Mobile-10 T-Mobile-11 T-Mobile-12 T-Mobile-13 T-Mobile-13 T-Mobile-13 T-Mobile-13 T-Mobile-13 T-Mobile-13 T-Mobile-13	Trwobile-16 Trwobile-17 Trwobile-19 Trwobile-20 Trwobi	ATT-85 ATT-61 ATT-C1 ATT-C2 ATT-C3 ATT-C3 ATT-C4 ATT-C5 CSP-70 CSP-70 CSP-71 CSP-72 CSP-73 DNK21-SRD9 DNK20-UNKNOWN DNK19-STAMG3 159-A 159-B 159-B DNK22-TOG-6	DNK22-STAM64 DNK22-STAM65 GRN-1 (DNK25) DNK26ACSP-67 DNK26ANCGP-67 DNK27A-CSP4 DNK27A-CSP14 DNK28A-CSP14 DNK28B-CSP3 DNK28C-TCGP74 TOP-C T

0,00 0.00 31.50	0.00	0.00	00.00	00.00	0.00	00.00	0.00	00.00	00.00
240.00	00.00	120.00	240.00	0.00	120.00	240.00	00.00	120.00	240.00
5.88	3.13	3.13	3,13	3.13	3,13	3.13	0.83	0.83	0.83
00.00	00.0	00.0	00.0	00.0	00.0	0.00	00.0	00.0	00.0
00.00									
150.00	126.66	126.66	126.66	126,66	126.66	126.66	126.66	126.66	126,66
Powerwave 7770	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B5B/BB13 (RFV010-D2A)	RRH RSR/BR13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	CBC78T-DS-43-2X	CBC78T-DS-43-2X	CBC78T-DS-43-2X
ATT-C8	Verizon-25	Verizon-26	Verizon-27	Verizon-28	Verizon-29	Verizon-30	Verizon-31	Verizon-32	Verizon-33

EIA Section Load Case Information for "5: 0.9D + 1.0Dg + 1.0E":

Note: gzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh), Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads)
Face RR is the minimum round reduction factor for all round anches and assertanted in the section

Face RR	kisth	e minimum	Face RR is the minimum round reduction factor for all round angles and appurtenances in the section	iction f	actor	for al.	round	l angle	s and	appur	cenance	ss in t	he secti	Top								
Section Z Label T	of 2 Top Bot	<b>&amp; &amp;</b>	qzGh (psf)	Ice Face Face Face Thick, AF AR RR*AR (in) (ft^2) (ft^2) (ft^2)	Face AF (ft^2) (	Face AR 1 ft^2) (	Face R*AR ft^2) (f	Face F AG (ft^2)	ace F	or Fa	Se Face	Face Face Face Face Face Face Face Face	Face AE (ft^2)	Face WF (1bs)	NotF 1 AAF (ft^2)	NotF CAF	NotF N AAR (ft^2)	NotF NotF CAR AAR*CAR (ft^2)		NotF T WA (1bs) (	Total Wind W	Total Weight (1bs)
A 180.00 160.00	00 160	i	70.00 0.00	0.00	20.58	21.02	12.32 1	63.7 (	.25 1	00 1.	00 0.59	3 2.43	32.9	0	24.00	2.00	0.00	.20	0.00	0	0	5031
B 160	00 140		150.00 0.00		22.52	27.30	16.04 1	0.161	0.26 1	.00 1.	00 0.5	3 2,41	38.6	0	36.00	2.00	0.00 1	.20	00.0	0	0	5371
C 140.00 120.00	.00 120		130,00 0.00		0.00 25.73 29.16 17.07 218.3 0.25 1.00 1.00 0.59 2	29.16	17.07	218.3 (	).25 1	.00 1.	00 0.59	3 2.43	42.8	0	48.00 2.00	2.00	0.00	1.20	00.0	0	0	5975
D 120.	00 100		110.00 0.00		30.37	36.61	21,63	245.5 (	0.27 1	.00 1.	00 0.59	9 2.37	52.0	0	48.00	2,00	0.00	.20	00.0	0	0	9659
E 100	00 80		90.00 0.00		37.01	40.26	23,91	272.8 (	0,28 1	.00 1.	00 0.59	9 2.34	6.09	0	48.00	2.00	0.00	.20	00.0	0	0	8985
E 80	00 00		70.00 0.00		37.32	43.90	25.92	300.00	0.27 1	.00 1.	00 0.59	9 2.38	63.2	0	48.00	2.00	0.00	.20	00.0	0	0	9449
.09 5	60.00 40		50.00 0.00		42,28	50.37	29.91	327.3	0.28 1	.00 1.	00 0.5	9 2,34	72.2	0	48.00	2.00	0,00	.20	00.0	0	0	10556
H 40			30.00 0.00		48.05	50.83	30,12	354.6	0.28 1	.00 1.	00 0.5	9 2.35	78.2	0	48.00 2.00	2.00	0.00	.20	00.0	0	0	11237
I 20		0.00	10.00 0.00		59.30	58.17	59.30 58.17 34.98 381.9 0.31 1.00 1.00	381.9	0.31 1	.00 1.	00 0.60	0 2.28	94.3	0	43.20	2.00	0.00	.20	00.0	0	0	11326

Equipment Load Case Information for "6: Service 1.0D + 1.0Dg + 1.0 Wo":

. Vert. d Load ) (lbs)	50.00 10
Trans. Load (1bs)	
Long. Load (1bs)	31.05 21.36 21.36 21.36 21.36 21.36 22.36 22.36 22.36 23.34 111.53 33.56 23.57
Antenna Moment MM (ft-lbs)	1 1 1 1 1 1 1 1 1
Antenna Side Load FSM (1bs)	
Antenna Antenne Axial Side Load FAM Load FSM (lbs) (lbs)	
222-G CM	# # # # # # # # # # # # # # # # # # #
222-G CS	# # # # # # # # # # # # # # # # # # #
222-G CA	
Fotal Wind Wind Wind Wind Incidence Area Angle Ft^2) (deg)	120.00 120.00 120.00 120.00 240.00 240.00 240.00 240.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00
Total Wind D Area (ft^2)	2.75 2.75 2.72 2.72 2.72 2.72 2.72 2.72
Ice Thick. (in)	
qzGh (psf)	77.88.7 77.88.5 77.88.5 77.88.5 77.88.5 88.114 8
levation Above Ground (ft)	60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 120.00 120.00 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34
Equipment Elevation Property Above Set Ground (ft)	5. Dipole 3. Stand-Off GPS 3. Stand-Off GPS 3. Stand-Off 10. Dipole 3. Stand-Off 10. Dipole 3. Stand-Off RFS PD1142 W/ ice 3. Stand-Off RFS PD1142 W/ ice 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 13. Stand-Off RFS APXVSPP18-C W/ ice ALU RRH
W.	
Equipment Label	DNK-1 DNK-1 DNK-1 DNK-2-GPS6B MT-DNKS DNK-3-GPS6B MT-DNKS DNK-1 DN

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120.00 240.00	240.00 240.00 240.00 240.00 240.00 240.00 240.00 0.00
22. 22. 23. 24. 24. 25. 25. 25. 25. 25. 25. 25. 25. 25. 25	2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99
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1113.3.3.4 1113.3.3.4 1113.3.3.4 1113.3.3.4 1113.3.3.4 1126.6.6.6 1126.6.6.6 1126.6.6.6 1126.6.6.6 1128.6.6.6 1128.6.6.6 1128.6.6 1128.3.3.3.4 128.3.3.3.4 128.3.3.4 128.3.3.4 128.3.3.4 128.3.3.4 128.3.	133.34 133.34 133.34 133.34 133.34 133.34 133.34 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00
BSAMNT - SBS BSAMNT - SBS BSAMNT - SBS	RRHU-11 RRH Unit 13  RRHU-11 RRH Unit 13  Ericsson 4478 (B71) RRH Unit 13  Ericsson 4478 (B71) RRH Unit 13  Ericsson 4478 (B71) RRH Unit 15  Ericsson 4478 (B71) RRH Unit 15  Diplexer Unit - Generic 17  12 'T-Arm 12' T-Arm 12' T-Arm 12' T-Arm 14'  RRHU-11 RRH Unit 16  POWETWAVE 7770 16  RAM Unit (LGG24101) 17MA Unit (LGG24101) 11 TWA Unit (LGG24101) 11 TWA Unit (LGG24101) 11 TWA Unit (LGG24101) 11 TWA Unit (LGG24101) 11
Sprint-16 Sprint-16 Sprint-16 Sprint-17 Sprint-18 Verizon-19 Verizon-20 Verizon-19 Veriz	Trwobile-13 Trwobile-14 Trwobile-16 Trwobile-18 Trwobile-19 Trwobi

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10.12	5.06	200	1.29	51.32	6.53	6.53	2.72	2.72	2.72	1,01	6,53	1.29	13.10	9.17	3,70	30.0	2.27	1.29	2.27	2.06	0.54	1.64	10.60	10.60	10.60	10.60	5.88	5,88	5.88	5.88	3.13	3.13	3,13	3.13	J. I.3	3.13	0.83	0,83	0.83
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9.18																																							
150.00																																							
OPA-65-LCUU-H6 Panel RRUS-32 RRH Unit	Sinclair SC479-HFILDF w/ ice	Sinclair SC479-HFLLDF w/ ice	SINCIALE SC4/9-DFILDE W/ ICE	8 Dish with Radome	4 x1 Panel	4'x1' Panel	3 Stand-Off	3 Stand-Off	3 Stand-Off	DB586-Y	4`x1` Panel	TMA	4 Dish	Dipole	4 Dipole	Sinclair SC479-HF1LDF w/ ice	Scala OGT9-806 w/ ice	AMT	Scala OGT9-806 w/ ice	Sinclair SC479-HF1LDF w/ ice	Andrew DB-583 w/ ice	Decibel PD-420 2 bay - Dipole	6 Stand-Off	6 Stand-Off	6 Stand-Off	6 Stand-Off	Powerwave 7770	Powerwave 7770	Powerwave 7770	Powerwave 7770	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B2/B66A (RFV01U-D1A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	RRH B5B/BB13 (RFV01U-D2A)	CBC78T-DS-43-2X	CBC78T-DS-43-2X	CBC78T-DS-43-2X
ATT-C4 ATT-C5	CSP-70	CSP-71	CSP-72	CSF=73	DNK20=INKNOWN	DNK19-STAM63	159-A	159-1	160	DNK22-TOG-6	DNK23-STAM64	DNK23-STAM65	GRN-1 (DNK25)	DNK26aCSP-67	DNK26bNEU-20	DNK27A-CSP4	DNK278-CSP2	DNK27C-CSP74	DNK28A-CSP1	DNK28B-CSP3	DNK28C-TOG5	DNK28D-NEUSS	Ton-A	Top-B	LD-GOL	Top-C2	ATT-B7	ATT-B8	ATT-C7	ATT-CB	Verizon-25	Verizon-26	Verizon-27	Verizon-28	Verizon-29	Verizon-30	Verizon-31	Verizon-32	Verizon-33

EIA Section Load Case Information for "6: Service 1.0D + 1.0Dg + 1.0 Wo":

Note: qzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh), Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads) Face RR is the minimum round reduction factor for all round angles and appurtenances in the section

пной	0 <del>0</del> <del>0</del> <del>0</del> <del>0</del> <del>0</del> <del>0</del> <del>0</del> <del>0</del>	
Total Weight (1bs)	5590 5968 6639 7329 9983 10499 11729 12486	
Total Wind (1bs)	1505 1952 2353 2440 2505 2468 2531 2695 3356	
NotF WA (1bs)	753 1101 1425 1378 1327 1243 1266 1385	
NotF AAR*CAR (ft^2)	0000000000	
NotF	0.60 0.60 0.60 0.60 0.60 0.60	
NotF AAR (ft^2)	000000000000000000000000000000000000000	
NOLF	22.00	
Note 3AE (ft^2)	40.00 80.00 80.00 80.00 80.00 80.00 80.00	
Face WE (1bs)	751 851 928 1062 1178 1190 1289 1429	
Face AE (ft^2)	32 38 42 42 60 60 70 70 80 76 70	
Face	22.43 22.43 22.34 22.34 22.38 22.38	
Face Face Face Face Face (E	0.59 0.59 0.59 0.58 0.58 0.55	
Face	1.000	1
Face	1.000	1 0 4
Face	0.25 0.25 0.25 0.28 0.28 0.28	
Face AG (ft^2)	63.7 91.0 118.3 45.5 72.8 300.0 327.3 354.6	1 . + 0
Face RR*AR (ft^2) (f	2.32 1.63 2.04 1.63 2.62 2.41 3.62 2.41 3.56 3.70 3.70	)
ace F AR Ru ^2) (ft		
Ice Face Face Face Face hick. AF AR RR*AR (in) (ft^2) (ft^2) (ft^2)	0.00 20.58 21.02 12.32 163.7 0.25 1.00 1.00 0.59 2.43 0.00 25.52 27.30 16.04 191.0 0.26 1.00 1.00 0.59 2.41 0.00 25.73 291.6 17.07 218.3 0.25 1.00 1.00 0.59 2.41 0.00 35.73 291.6 17.07 218.3 0.25 1.00 1.00 0.59 2.41 0.00 37.31 36.61 21.63 245.5 0.27 1.00 1.00 0.59 2.37 0.00 37.32 43.90 25.41 300.0 0.27 1.00 1.00 0.58 2.38 0.00 42.28 50.37 28.56 271 0.00 1.00 0.55 2.34 0.00 48.05 50.83 28.73 0.28 1.00 1.00 0.55 2.38 0.00 48.05 50.83 28.70 35.46 0.28 1.00 1.00 0.55 2.38 0.00 48.05 50.83 28.70 35.40 0.28 0.28 1.00 1.00 0.55 2.38 0.00 48.05 50.83 28.70 35.40 0.28 0.28 1.00 1.00 0.55 2.38 0.00 48.05 50.83 28.70 35.40 0.28 0.28 1.00 1.00 0.55 2.35 0.00 48.05 50.83 28.70 35.40 0.28 0.28 1.00 1.00 0.55 2.35 0.00 48.05 50.83 28.70 35.40 0.28 1.00 1.00 0.55 2.35 0.00 48.05 50.83 28.70 35.40 0.28 0.28 1.00 1.00 0.55 2.35 0.00 48.05 50.83 28.70 35.40 0.28 0.28 0.20 0.25 0.25 0.28 0.20 0.25 0.28 0.20 0.25 0.28 0.20 0.25 0.28 0.20 0.25 0.25 0.25 0.25 0.25 0.28 0.20 0.25 0.25 0.25 0.25 0.25 0.25 0.25	200
e Fa	10 20. 10 22. 10 25. 10 30. 10 37. 10 42.	100
Ice Thick. (in) (	000000000	,
(jsd)	9 42 9 18 8 91 8 61 8 61 7 77 7 77 7 77 7 91	10.0
Elev. e Gnd. (ft)	110.00 110.00 110.00 110.00 90.00 70.00 50.00	,,,,
Ave.		
Z of Jottom (ft)	160.00 120.00 120.00 100.00 80.00 60.00 40.00	, ,
Z of Top E (ft)	00.00	20.00
ection Label	A 180.00 160.00 170.00 9,42 18 160.00 140.00 150.00 9,18 160.00 120.00 110.00 891 10.00 80	4
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Equipment Load Case Information for "1.2\*DL":

Vert.	rd Load		(Ibs)
rans.	Load		(1ps)
rond.	Load		(1ps)
Antenna	Moment Load Load	M	ps)
Antenna	CM Axial Side Mom	Load FSM	(1ps)
Antenna	Axial	Load FAM	(1bs)
5-777	뀰		
	CS		
	CA		
Wind	Incidence	Angle	(ft^2) (deg)
Total	Wind 1	Area	(ft^2)
ICE	hick.		(in)
dzgh	,		(psf)
<b>Elevation</b>	Above	Ground	(ft)
Equipment F	Property	Set	(ft) (psf)
Equipment	Label		

0,00 60.00 0,00 60.00 0,00 12.00 0,00 60.00 0,00 60.00 0,00 60.00 0,00 60.00	0.00 12.00 0.00 12.00 0.00 65.00 0.00 65.00 0.00 558.00 0.00 558.00 0.00 72.00	0.00 565.20 0.00 565.20 0.00 565.20 0.00 12.00 0.00 139.20 0.00 139.20 0.
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600.000 600.000 600.000 600.000 600.000	10000000000000000000000000000000000000	126.066666666666666666666666666666666666
5. Dipole 3. Stand-Off (GPS) 3. Stand-Off (GPS) 3. Stand-Off (10. Dipole 3. Stand-Off (SPS) 4. Oppole (SPS) 5. Stand-Off (SPS) 6. Oppole (SPS) 7. Oppole (SPS)	6 Stand-Off  RFS PD1142 W/ ice  3 Stand-Off  12 Omni  12 Omni  12 T-Arm  12 T-Arm  12 T-Arm  12 T-Arm  13 T-Arm  14 T-Arm  15 T-Arm  16 ARVSPP18-C W/ ice  ALU RRH  RFS APXVSPP18-C W/ ice  ALU RRH  RFS APXVSPP18-C W/ ice  ALU RRH  ALU RRH  DT465B-2XR-V2  DT465B-	0x20-25 RRH 0x20-25 RRH 0x30-25 RRH 0x30-
DNK-1 MYZ-GSE 68 MY-DNKZ DNK2-GSE 69 MY-DNK2 MY-DNK3 DNK4-DOT 56 MY-DNK4	MY-DBKS MK9-DEPS4 MK9-DEPS4 MK9-DEPS54 MK7-NEU17 MT-DBK7 Sprint-A Sprint-A Sprint-A Sprint-A Sprint-A Sprint-A Sprint-A Sprint-A Sprint-B Sprint-A Sprint-B Sprint-II	

0.00 0.00 180.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 60.00 0.00 0.00 60.00 0.00 0.00 36.00 0.00 0.00 144.00 0.00 0.00 44.00 0.00 0.00 22.20 0.00 0.00 22.20 0.00 0.00 128.00 0.00 0.00 128.00 0.00 0.00 128.00 0.00 0.00 168.00 0.00 0.00 189.20 0.00 0.00 139.20 0.00 0.00 139.20 0.00 0.00 139.20 0.00 0.00 139.20 0.00 0.00 139.20
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86330	.66410 0.08980 -0.06910
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133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 133.34 135.00 150.00	160.00 160.00 165.00 165.00 17
	FEF FFF Y MAA MAA MAA MAA MAA MAA MAA MA
T-Mobile-9 T-Mobile-10 T-Mobile-13 T-Mobile-13 T-Mobile-14 T-Mobile-15 T-Mobile-17 T-Mobile-19 T-Mobile-19 T-Mobile-19 T-Mobile-19 T-Mobile-20 T-Mobile-20 T-Mobile-21 ATT-A ATT-B ATT-B ATT-C ATT-B ATT-C ATT-B ATT-C ATT-B ATT-C ATT-C ATT-B ATT-C A	DNK19-374M03  159-B  160  DNK23-STAM64  DNK23-STAM65  GRN-1 (DNK25)  DNK26aCSP-67  DNK26aCSP-67  DNK27A-CSP 14  DNK27B-CSP 14  DNK28B-CSP 14  DNK28B-CSP 14  DNK28B-CSP 14  DNK28B-CSP 14  DNK28B-CSP 14  DNK2B-CSP 14  DNK2B-CSP 14  TOP-C  TOP-B  TOP-C  ATT-B8  ATT-B8  ATT-C  ATT-C  Verizon-25  Verizon-26  Verizon-26  Verizon-27

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00-0	00.00	00.0	00.0	00.00
0.00	00.0	0.00	00.0	00.0
126.66	126.66 0.00	126,66	126.66	126,66
RRH BSB/BB13 (RFV010-D2A)	RRH B5B/BB13 (REV01U-D2A)	CBC78T-DS-43-2X	CBC78T-DS-43-2X	CBC78T-DS-43-2X
Werison-20	Verizon-30	Verizon-31	Verizon-32	Verizon-33

118.20 118.20 18.78 18.78 18.78

EIA Section Load Case Information for "1.2\*DL":

Note; gzGh (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor (Gh) Wind Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads)
Face RR is the minimum round reduction factor for all round angles and appurtenances in the section

6708 7161 7967 8794 11980 12598 14075 14075 Total Weight (1bs) Total Wind (1bs) 000000000 NotF 7 WA (1bs) 000000000 NotF NotF CAR AAR\*CAR (ft^2) 1.20 1.20 1.20 1.20 1.20 1.20 NotF 1 AAR (ft^2) NotF NotF AAF CAF (ft^2) 24.00 2.00 488.00 2.00 488.00 2.00 488.00 2.00 488.00 2.00 488.00 2.00 43.20 2.00 Face WF (1bs) 000000000 Face AE (ft^2) 32.9 32.9 42.8 52.0 60.9 72.2 748.2 | Ice | Face | F 2.43 2.34 2.34 2.34 2.34 2.35 5 1.00 1.00 0.59 2 5 1.00 1.00 0.59 2 5 1.00 1.00 0.59 2 8 1.00 1.00 0.59 2 8 1.00 1.00 0.59 2 8 1.00 1.00 0.59 2 8 1.00 1.00 0.59 2 8 1.00 1.00 0.59 2 1 1.00 1.00 0.59 2 1 1.00 1.00 0.59 2 1 1.00 1.00 0.60 2 2 12.32 163.7 0.25 1 5 16.04 191.0 0.26 1 6 17.07 218.3 0.25 1 121.63 245.5 0.27 1 6 23.91 272.8 0.28 1 0 25.92 300.0 0.27 1 2 3 30.12 354.6 0.28 1 3 3 0.12 354.7 0.28 1 3 3 0.12 354.7 0.28 1 0.00 20.58 21.02 1 0.00 22.52 27.30 1 0.00 25.73 29.16 1 0.00 37.31 36.61 2 0.00 37.32 43.90 2 0.00 48.05 50.83 2 0.00 48.05 50.83 2 1770.00 1150.00 1130.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 Z of Ave. Elev. qzGh Bottom Above Gnd. (ft) (ft) (psf) 160.00 140.00 120.00 100.00 80.00 60.00 20.00 Z of Top 1 (ft) 180.00 140.00 120.00 120.00 100.00 60.00 40.00 20.00 Label HEGERDCBA Section

"0.9DL": Equipment Load Case Information for

. Vert. d Load ) (1bs)	45.00 45.00 45.00 45.00 47
Trans. Load (1bs)	
Long. Load (1bs)	
Antenna Long. Moment Load MM (ft-lbs) (lbs)	
Antenna Side Load FSM (1bs)	
Antenna Axial Load FAM (1bs)	
222-G CM	
222-G CS	
222-G CA	
otal Wind Wind Incidence Area Angle t^2) (deg)	0.00 240.00
Total Wind Area (ft^2)	13.95 10.00
Ice Thick. (in)	
qzGh 1 (psf)	
levation Above Ground (ft)	60.00 60
Equipment Elevation Property Above Set Ground (ft)	5. Dipole 3. Stand-Off 6. Stand-Off 10. Dipole 3. Stand-Off 10. Dipole 3. Stand-Off 10. Dipole 4. Stand-Off 8. Omni 6. Stand-Off 11. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 12. T-Arm 13. Stand-Off 12. T-Arm 14. T-Arm 15. T-Arm 16. T-Arm 17. TArm 18. ApxVSPP18-C w/ ice ALU RRH RFS ApxVSPP18-C w/ ice ALU RRH RFS ApxVSPP18-C w/ ice ALU RRH RFS ApxVSPP18-C w/ ice ALU RRH ALU RRH DT465B-2XR-V2 ROD MHZ RRH UNIT TD-RRH 9X20-25 RRH UNIT TD-RRH 9X20-25 RRH UNIT TD-RRH 9X20-25 RRH UNIT
Equipment Label	DNK-1  WT-DNK1  WT-DNK2  DNK3-GPS69  WT-DNK3  DNK3-GPS69  WT-DNK3  DNK4-DOT56  WT-DNK5  DNK5-WEU16  WT-DNK5  DNK9-DEP56  DNK9-DEP56  DNK9-DEP56  DNK9-DEP66  DNK7-NEU17  WT-DNK7  SPLINT-A

240.00 240.00	120.00
13.3.60 13.3.60 13.3.60 13.3.60 13.3.97 13.97 13.97 13.97 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129 10.129	5.06
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126.66.66.66.66.66.66.66.66.66.66.66.66.6	160.00
Boom Gate Boom Gate Boom Gate Bochbel DB844480-xx w/ ice Decibel DB844480-xx w/ ice JAHH-65B-R3B Panel JAHH-65B-R3B RH Unit JAHH-65B	Sinclair SC479-HFILDF w/ ice Sinclair SC479-HFILDF w/ ice
Verizon-A Verizon-B Verizon-1 Verizon-3 Verizon-3 Verizon-9 Verizon-0 Verizon-0 Verizon-0 Verizon-1 Verizo	CSP-71 CSP-72

423.90 423.90 423.90 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 1113.67 113.67 114.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 118.98 122.50 222.5

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240.00 240.00 240.00 240.00 0.00 0.00 0.
51.32 6,533 6,533 6,533 1.29 1.29 1.29 1.29 1.29 1.29 1.29 1.29
160.00 160.00 160.00 160.00 160.00 165.00 165.00 17
## Dish with Radome    Axi Panel     Axi Panel     Axi Panel     3 Stand-Off     3 Stand-Off     4 Dish     BBS6-Y     4 Dish     5 Dish     6 Dish     7 Dish     8 Dish     9 Dish     10 Dish     1
CSP-73  DNK21-SPD9  DNK19-STAM63  159-B  159-B  159-B  159-B  160  DNK22-TGG-6  DNK23-STAM64  DNK23-STAM65  GRN-1 (DNK25)  DNK26-SPD9  DNK26-SPD9  DNK26-SPD9  DNK26-SPD9  DNK26-SPD9  DNK28-CSP1  DNK28A-CSP1  DNK28A-CSP1  DNK28B-CSP1  DNK28B-CSP1  DNK28C-TGG5  DNK28C-TGG5  DNK28C-TGG5  DNK28C-TGG5  DNK28C-TGG5  DNK28D-NEU55  VETIZOR-25  VETIZOR-25  VETIZOR-25  VETIZOR-26  VETIZOR-27  VETIZOR-30  VETIZOR-31  VETIZOR-31  VETIZOR-32

EIA Section Load Case Information for "0.9DL":

(gp) (adjusted wind pressure) includes: Velocity Pressure Coefficient (Kz), Topographic Factor (Kzt), Gust Effect Factor Direction Probability Factor (Kd), Wind Importance Factor (Table 2-3), Wind Load Factor (from Loads/EIA Loads) RR is the minimum round reduction factor for all round angles and appurtenances in the section Note: qzGh ( Wind I Face F

Notf WA WA (1bs) 000000000 NotF AAR\*CAR (ft^2) 000000000 Note 1.20 1.20 1.20 1.20 1.20 1.20 1.20 000000000 NotF AAR (ft^2) NotF 2.00 2.00 2.00 2.00 2.00 2.00 2.00 NotF N AAF (ft^2) 24.00 36.00 48.00 48.00 48.00 48.00 48.00 Face WF (1bs) 000000000 Face AE (ft^2) 32.9 38.6 42.8 52.0 60.9 72.2 78.2 2.43 2.43 2.37 2.34 2.38 2.38 2.38 2.38 Face Face 000000000 00000000 Face 2 163.7 0.25 1.00 1 191.0 0.25 1.00 1 191.0 0.25 1.00 1 1 27.8 0.28 1.00 1 2 300.0 0.27 1.00 1 1 327.3 0.28 1.00 1 2 354.6 0.28 1.00 1 8 381.9 0.31 1.00 1 Face Face e DF ## Above Gnd.

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Total
Weight (1bs)
(1bs)
5371
5371
5975
6596
8985
9449
10257

000000000

Total Wind Wind (1bs)

\*\*\* Analysis Results:

Maximum element usage is 97.93% for Angle "SNB-LH2P" in load case "1: 1.2D + 1.0Dg + 1.6Wo" Angle Forces For All Load Cases:

### (Atjac) (A	## (Atjus) (At	Group Label	Angle Label	Max. Usage For All LC	Max. Tens. For All LC	Max. Comp. For All LC	rc 1	IC 2	rc 3	LC 4	r C T	rc e	· ·
Reht-Marie 11.77 0.865 0.006 0.1855 0.181 0.114 0.029 0.001 0.001 0.1014 0.012 0.001 0.1014 0.1014 0.1012 0.1014 0	Robin-Dalip   11.17				- 10	(kips)	(kips)	(kips)	(kips)	(kips)	(kips)	(kips)	(kips)
Roth-Dall   1.37   0.107   0.000   0.100   0.101   0.011   0.012   0.025   0.001   0	Rohn-DAL         1.37         0.107         0.107         0.117         0.017         0.017         0.017         0.017         0.017         0.017         0.017         0.017         0.017         0.017         0.017         0.018         0.028         <	Rohn-D1	Rohn-DA1P		0.865		0.865	0.865	0.141	0.144	0.189	900.0-	-0.003
Robin-Dayle   1.5   1.5   1.0   1.0   1.1   1.0   1.1   1.0   1.1   1.0   1.	Rothr-DAL2         25.67         0.000         -1.400         -1.333         -0.213         -0.213         -0.159           Rothr-DAL2         1.5.15         0.000         -0.1400         -0.286         -0.151         -0.159           Rothr-DAL2         1.5.15         0.000         -0.019         0.086         0.155         -0.163           Rothr-DAL2         1.5.15         0.000         -0.019         0.866         0.821         -0.163           Rothr-DAL3         1.0.44         0.089         -0.012         0.386         0.025         0.015           Rothr-DAL2         1.0.40         0.089         0.012         0.168         0.022         0.022           Rothr-DAL2         1.0.00         0.000         0.013         1.06         0.022         0.022           Rothr-DAL2         1.0.000         0.013         0.000         0.022         0.022         0.022           Rothr-DAL2         1.0.000         0.013         0.000         0.022         0.022         0.022           Rothr-DAL2         1.0.000         0.010         0.022         0.022         0.022         0.022           Rothr-DAL2         1.0.000         0.010         0.022         0.022         0.	Rohn-Dl	Rohn-DAll		0.107		0.105	0.107	0.011	0.012	0.025	0.001	0.003
Roth-Park   1.2	Rother-Dark	Rohn-Dl	Rohn-DA12		000.0		-1.400	-1.393	-0.213	-0.209	-0.314	600.0-	-0.00.0
Roth-Park 1	Rohn-DAZ         1.5.15         0.000         -0.826         -0.826         -0.821         -0.185         -0.185           Rohn-DAZ         1.0.44         0.809         -0.011         0.386         0.384         -0.185         -0.155           Rohn-DAZ         1.2.2         0.000         -1.706         -1.69         0.224         -0.224           Rohn-DAZ         1.3.29         0.000         -1.706         -1.69         0.224         0.224           Rohn-DAZ         1.0.70         0.022         0.022         0.022         0.022         0.022           Rohn-DAZ         1.0.70         0.022         0.022         0.022         0.022         0.022           Rohn-DAZ         1.0.70         0.000         0.013         0.022         0.024         0.022           Rohn-DAZ         1.0.70         0.000         0.024         0.024         0.024         0.024           Rohn-DAZ         1.0.70         0.000         0.024         1.0.70         0.024         0.025         0.026           Rohn-DAZ         1.0.70         0.000         0.024         1.445         1.445         1.445         0.022           Rohn-DAZ         1.0.70         0.000         0.024 </td <td>Rohn-D1</td> <td>Rohn-DA2P</td> <td></td> <td>776.0</td> <td></td> <td>0.977</td> <td>0.976</td> <td>0.168</td> <td>U.169</td> <td>0.217</td> <td>-0.001</td> <td>0.00</td>	Rohn-D1	Rohn-DA2P		776.0		0.977	0.976	0.168	U.169	0.217	-0.001	0.00
ROME-DAZA   1.47		Rohn-Dl	Rohn-DA21		0.00.0		-0.826	-0.82I	-0.165	-U.163	-0.183	-0.003	-0.000
ROBIN DALFA   1.2.4   0.095   0.007		Rohn-Dl	Rohn-DA22		0.364		0.360	0.364	0.031	0.035	0.0/4	-0.011	-0.006
Notice Date   1.70		Rohn-Dl	Rohn-DA3P	10	608.0		0.800	0.808	0.100	10.10	0.100	-0.019	-0.013
Rolling   March 2012   March	Rohn-Da32   31.28   0.000   -1.41   -1.46   -1.599   -1.254   -1.214   -1.465   -1.225   -1	Rohn-Dl	Rohn-DA31		0.095		260.0	0.095	0.009	0.012	0.UI/	-0.00	10.004
Rother Dark   20   20   20   20   20   20   20   2	Roth-DA4P         17.93         -0.013         0.686         0.690         0.020           Roth-DA4P         17.93         -1.390         -0.013         0.686         0.690         0.020           Roth-DA5P         18.79         -0.024         1.471         1.139         -0.204         0.013           Roth-DA5P         4.03         0.312         -0.000         -0.138         0.031         0.010         0.010           Roth-DA5P         4.03         0.312         -0.000         -0.138         0.031         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.010         0.011         0.021         0.011         0.021         0.011         0.021         0.011         0.021	Rohn-D1	Rohn-DA32		000.00		-I.706	-1.698	-0.254	-0.249	-0.383	-0.011	0000
Roth-Date 2	Nother-Day 1	Rohn-Dl	Rohn-DA4P		1.390		1.389	1.39U	0.200	0.205	0.300	-0.013	0000
Rohn-Data         B 9.1         U. 990         U. 100         U. 10	Nother Data   1.49	Rohn-Dl	Rohn-DA41		0.000		-1.4/I	-I.463	-0.229	C22.U-		-0.011	0000
Rohn-DAS         1,1,7         1,449         0.101         0.001         0.001           Rohn-DAS         2,2,5         0.001         1,449         0.144         0.124         0.124         0.124         0.001           Rohn-DAS         2,2,5         0.001         1,504         1,504         1,504         1,504         0.001         0.002         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001         0.000         0.001 <t< td=""><td>Rohn-Days         18.70         0.342         0.024         1.449         0.131         0.005           Rohn-Days         4.0         0.342         0.001         1.590         1.590         1.514         0.012           Rohn-Days         3.2         9.001         1.590         1.590         1.514         0.024         0.024           Rohn-Days         2.0         3.8         0.000         1.1024         1.917         0.024         0.025           Rohn-Days         2.0         3.9         0.000         1.1024         1.917         0.023         0.021           Rohn-Days         2.0         3.0         0.0<td>Rohn-Dl</td><td>Rohn-DA42</td><td></td><td>0.690</td><td></td><td>0.686</td><td>0.690</td><td>0.040</td><td>0.045</td><td></td><td>-0.013</td><td>0.006</td></td></t<>	Rohn-Days         18.70         0.342         0.024         1.449         0.131         0.005           Rohn-Days         4.0         0.342         0.001         1.590         1.590         1.514         0.012           Rohn-Days         3.2         9.001         1.590         1.590         1.514         0.024         0.024           Rohn-Days         2.0         3.8         0.000         1.1024         1.917         0.024         0.025           Rohn-Days         2.0         3.9         0.000         1.1024         1.917         0.023         0.021           Rohn-Days         2.0         3.0         0.0 <td>Rohn-Dl</td> <td>Rohn-DA42</td> <td></td> <td>0.690</td> <td></td> <td>0.686</td> <td>0.690</td> <td>0.040</td> <td>0.045</td> <td></td> <td>-0.013</td> <td>0.006</td>	Rohn-Dl	Rohn-DA42		0.690		0.686	0.690	0.040	0.045		-0.013	0.006
Non-Day 1   4 .03   0 .312   0 .312   0 .314	Rohn-Dall   Rohn	Rohn-Dl	Rohn-DA5P		1.449		1.445	1.449	161.0	0.196		-0.024	0.010
Roth-Dake   32,95   1,616   0.101   0.1,590   0.1,294   0.1,284	Rothin-Daka         32.95         0.001         -1,590         -1,590         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,594         -1,518         -1,516         -0,213         -0,213         -0,213         -0,213         -0,213         -0,213         -0,213         -0,213         -0,214         -0,214         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,215         -0,214         -0,2	Rohn-D1	Rohn-DA51		0.312		0.308	0.312	100.0			0000	-0.003
Non-Dake   30, 85   10, 85	Rohn-DAG         39.87         1.010         -1.024         1.024         1.024         1.024         1.024         1.024         1.024         1.024         1.027         1.028         1.026         1.027         1.028         1.028         1.006         0.012         0.011         0.018	Rohn-DI	Rohn-DA52		100.0		-1.590	-1.584	-0.246			000.0-	100.0
Non-Darke   39.34   Non-Darke   39.32   Non-Darke   39.34   Non-	Rohn-Dakel 20.20 0.000 11.244 1.256 1.277 0.023 0.015 Rohn-Dakel 20.20 0.000 0	Rohn-D1	Rohn-DA6P		0.010.1		1.612	1.016	0.213			0.024	10.010
Rohn-DRAF         0.02         0.1155         0.005	Rohn-Da76         0.20         0.00	Rohn-DI	Rohn-DA61		0.00.0		-1.924	-1.91/	-0.24I			0000	100.00
National Part   Control Part   Con	Rother_DAY1         20.34         1.370         -0.043         -0.025         -0.257         -0.257           Rother_DAY1         20.34         -0.29         -0.018         -0.257         -0.257         -0.257           Rother_DAY2         0.41         0.029         -0.018         0.229         0.007         0.019         0.029           Rother_DAY3         3.700         0.000         -0.054         3.104         0.029         0.007         0.019           Rother_DBAR         3.700         0.000         -0.054         2.104         0.137         0.029           Rother_DBAL         3.700         0.000         -0.124         -0.029         0.017         0.029           Rother_DBAL         4.35         0.000         -0.124         -0.136         0.304         0.028           Rother_DBAL         4.35         0.000         -0.248         -0.280         0.373         0.028           Rother_DBAL         5.0         0.000         -0.218         0.027         0.027         0.027           Rother_DBAL         5.0         0.000         -0.280         0.027         0.027         0.027           Rother_DBAL         5.0         0.000         -0.280         0.028 <td>Rohn-D1</td> <td>Rohn-DA62</td> <td></td> <td>0.015</td> <td></td> <td>0.003</td> <td>0.000</td> <td>0.012</td> <td></td> <td>1.7</td> <td>0.000</td> <td>00.00</td>	Rohn-D1	Rohn-DA62		0.015		0.003	0.000	0.012		1.7	0.000	00.00
Roth-Date         Control         0.029         -0.018         0.029         0.039	Rothin-Day 2  Rothin-Day 8  Rothin-Day 9  Ro	Kohn-DI	Kohn-DA/F		0.000		1.300	1.07 L	0.203			10.044	10.00
Non-Dark	ROMIN-DAY         0.023         0.023         0.023         0.023         0.023         0.023         0.023         0.026         0.0273         0.026         0.036	Konn-Di	Konn-DA/I		000.0		00/:TI	00/.T-	10.00			000	0.01
Rohn-DB1   2.70   0.173   0.023   0.154   0.171   0.010   0.003   0.023   0.023   0.023   0.023   0.023   0.023   0.023   0.024   0.027   0.024   0.	RODIT - DARGE         2.7.0         0.103         0.104         0.105         0.105           RODIT - DARGE         2.7.0         0.100         - 1.682         - 1.682         - 1.682         - 1.675         - 0.268         - 0.265           Rohn - DBBI         3.7.00         0.100         - 1.682         - 1.682         - 1.675         - 0.268         - 0.205           Rohn - DBBI         42.36         0.100         - 2.745         - 2.745         - 2.745         - 0.299         - 0.019           Rohn - DBBI         48.51         0.000         - 0.026         0.029         0.011         0.029         0.011           Rohn - DBBI         48.51         0.000         - 0.246         0.284         0.834         - 0.024         0.834         0.011         0.029         0.011           Rohn - DBBI         5.00         0.000         - 0.246         0.028         2.642         0.029         0.034           Rohn - DBBI         46.53         0.004         - 2.86         2.76         2.979         0.374         0.371           Rohn - DBBI         5.00         0.004         - 2.828         2.642         0.029         0.034           Rohn - DBSI         46.53         0.004 <th< td=""><td>Konn-DI</td><td>Konn-DA/Z</td><td></td><td></td><td></td><td>1 832</td><td>0.020</td><td>0.00</td><td></td><td></td><td>-0.010</td><td>-0.012</td></th<>	Konn-DI	Konn-DA/Z				1 832	0.020	0.00			-0.010	-0.012
Continue	Rohn-DB1P   35.39   3.104   -0.054   3.096   3.104   0.258   0.258   0.314   Conno-DB1P   35.39   3.104   -0.054   3.096   3.104   0.299   0.314   Conno-DB1P   35.39   3.104   -0.054   3.096   3.104   0.299   0.314   Conno-DB1P   31.39   3.104   -0.056   3.104   0.299   0.314   Conno-DB1P   31.39   2.805   -0.2745   -2.745   -2.745   -2.735   -0.364   -0.360   Conno-DB2P   31.39   2.805   -0.280   -0.280   -0.280   -0.364   -0.360   Conno-DB2P   30.12   2.642   -0.280   -0.280   -0.227   -0.364   -0.360   Conno-DB3P   30.12   2.642   -0.280   -0.280   -0.272   -0.021   -0.012   Conno-DB3P   30.12   2.642   -0.280   -0.280   -0.272   -0.021   -0.012   Conno-DB3P   Conno-DB3P   2.805   -0.024   Conno-DB3P   Conno-DB3P   Conno-DB4P   Con	Rollin-Di					150	17.0	-0.50			ECO 0-	0.01
Rohn-DB1         35.39         3.104         -0.054         3.104         0.299         0.314         0.654         -0.054           Rohn-DB1         1.45         0.127         -0.054         3.104         0.299         0.314         0.056         -0.054         0.004           Rohn-DB1         42.36         0.000         -0.127         -0.056         2.745         -0.273         0.036         -0.054         0.004         -0.056         2.745         -0.027         0.036         -0.056         0.004         -0.056         2.745         -0.027         0.014         0.004         -0.056         2.745         -0.027         0.021         0.004         -0.056         0.004         0.027         0.005         0.004         0.028         0.027         0.021         0.007         0.006         0.028         0.027         0.021         0.007         0.006         0.007         0.028         0.027         0.028         0.007         0.007         0.008         0.007         0.008         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002<	Rohn-DB17         35.39         3.104         -0.054         3.104         0.296         0.314           Rohn-DB18         35.39         3.104         -0.056         3.104         0.296         0.316           Rohn-DB18         1.45         0.127         -0.056         2.796         2.805         -0.364         -0.369           Rohn-DB2P         31.98         2.805         -0.056         2.796         2.805         0.318           Rohn-DB3P         48.51         0.000         -2.143         -2.784         -0.272         -0.021           Rohn-DB3P         30.12         2.642         -0.034         2.888         2.888         2.895         0.317           Rohn-DB3P         48.83         0.004         -2.988         -2.988         -2.999         0.374         0.037           Rohn-DB4         2.32         0.004         -2.988         -2.988         -2.999         0.374         0.037           Rohn-DB4         2.33         0.044         -2.988         2.976         0.373         0.374           Rohn-DB5         46.53         4.081         -0.058         2.746         -0.031         0.372           Rohn-DB5         4.081         0.000         -0.04	Pohn-D1					1 682	-1.675	-0.268			-0.004	-0.001
Rohn-Dall         1.45         0.127         -0.036         0.118         0.127         -0.028         -0.019         0.009           Rohn-Dall         1.45         0.127         -0.036         2.745         2.745         2.746         0.009         -0.036           Rohn-Dall         48.51         0.000         -2.745         2.746         2.805         0.336         0.138         0.009         -0.036           Rohn-Dall         48.51         0.000         -2.80         -2.796         2.805         0.332         0.012         0.006           Rohn-Dall         9.50         0.000         -0.289         2.642         0.291         0.021         0.007         0.028           Rohn-Dall         9.50         0.003         -0.288         2.276         2.297         0.021         0.007         0.005           Rohn-Dall         9.50         0.003         -0.288         2.276         2.281         0.237         0.012         0.005           Rohn-Dall         9.50         0.003         -0.024         0.028         0.027         0.017         0.023         0.031         0.003           Rohn-Dall         9.50         0.003         0.024         0.028         0.023	Rohn-DBI         1.45         0.127         -0.030         0.118         0.127         -0.028         -0.018           Rohn-DBI         42.36         0.000         -2.745         -2.735         -0.364         -0.360           Rohn-DBI         48.51         0.000         -0.280         -0.272         0.364         -0.360           Rohn-DBI         48.51         0.000         -0.280         -0.272         0.027         0.030           Rohn-DBI         48.51         0.000         -0.280         -0.272         0.027         0.030           Rohn-DBI         48.51         0.000         -0.280         -0.291         0.037         0.037           Rohn-DBI         2.000         0.833         -0.024         0.029         0.037         0.037           Rohn-DBI         2.000         0.024         0.024         0.024         0.037           Rohn-DBI         2.000         0.024         0.024         0.037         0.037           Rohn-DBI         2.000         0.057         0.057         0.057         0.037         0.037           Rohn-DBI         3.740         0.057         0.057         0.057         0.057         0.037           Rohn-DBI	Rohn-D2	4 14				3.096	3.104	0.299			-0.054	-0.03
Rohn-DB12         42.36         0.000         -2.745         -2.735         -0.364         -0.360         -0.004           Rohn-DB12         43.36         0.000         -2.745         -2.735         -0.364         -0.364         -0.056           Rohn-DB22         48.51         0.000         -0.280         -0.280         -0.021         -0.056         -0.005           Rohn-DB23         48.51         0.000         -0.280         -0.280         -0.021         -0.021         -0.036         -0.005           Rohn-DB31         9.50         0.003         -0.280         -0.280         -0.021         -0.035         -0.026         -0.003           Rohn-DB31         48.83         0.003         -2.988         -2.979         -0.371         -0.024         -0.036           Rohn-DB41         54.33         0.003         -2.988         -2.979         -0.371         -0.024         -0.025           Rohn-DB42         5.32         0.003         -2.325         -3.325         -3.316         -0.373         -0.024         -0.025           Rohn-DB51         9.91         0.003         -0.064         4.054         0.046         -0.055         -0.371         -0.371         -0.024         -0.036 <td>Rohn-DB12         42.36         0.000         -2.745         -2.735         -0.364         -0.360           Rohn-DB2P         31.98         2.000         -2.745         -2.745         -2.735         -0.364         -0.360           Rohn-DB2P         48.51         0.000         -3.143         -3.143         -0.364         -0.369           Rohn-DB3P         48.51         0.000         -0.240         -0.280         -0.272         -0.021         -0.030           Rohn-DB3P         48.83         0.004         -2.988         -2.979         -0.374         -0.024           Rohn-DB4P         2.01         0.004         -2.988         -2.979         -0.376         -0.301           Rohn-DB4P         2.01         0.004         -2.988         -2.979         -0.374         -0.021           Rohn-DB4P         2.01         0.004         -0.235         -3.281         -0.373         -0.374           Rohn-DB5P         4.053         0.003         -0.221         -0.021         -0.036         -0.374           Rohn-DB5P         4.051         0.000         4.266         -0.021         -0.016         -0.016         -0.016           Rohn-DB5P         2.01         0.000         4.2</td> <td>Rohn-D2</td> <td>Rohn-DB11</td> <td></td> <td></td> <td></td> <td>0.118</td> <td>0.127</td> <td>-0.028</td> <td></td> <td></td> <td>-0.030</td> <td>-0.021</td>	Rohn-DB12         42.36         0.000         -2.745         -2.735         -0.364         -0.360           Rohn-DB2P         31.98         2.000         -2.745         -2.745         -2.735         -0.364         -0.360           Rohn-DB2P         48.51         0.000         -3.143         -3.143         -0.364         -0.369           Rohn-DB3P         48.51         0.000         -0.240         -0.280         -0.272         -0.021         -0.030           Rohn-DB3P         48.83         0.004         -2.988         -2.979         -0.374         -0.024           Rohn-DB4P         2.01         0.004         -2.988         -2.979         -0.376         -0.301           Rohn-DB4P         2.01         0.004         -2.988         -2.979         -0.374         -0.021           Rohn-DB4P         2.01         0.004         -0.235         -3.281         -0.373         -0.374           Rohn-DB5P         4.053         0.003         -0.221         -0.021         -0.036         -0.374           Rohn-DB5P         4.051         0.000         4.266         -0.021         -0.016         -0.016         -0.016           Rohn-DB5P         2.01         0.000         4.2	Rohn-D2	Rohn-DB11				0.118	0.127	-0.028			-0.030	-0.021
Rohn-DB2P         31.98         2.805         -0.056         2.796         0.302         0.318         0.517         -0.056           Rohn-DB2P         31.98         2.805         -0.056         2.796         2.805         0.318         0.518         -0.056         -0.006           Rohn-DB2P         48.51         0.000         -0.2143         -2.133         -0.324         -0.024         -0.024         -0.026         -0.009           Rohn-DB3P         30.12         2.642         -0.035         2.638         -0.024         0.027         0.034         -0.024         -0.026         -0.009         -0.024         -0.0	Rohn-DB2P         31.98         2.865         -0.056         2.796         2.805         0.302         0.3143         -0.3143         -0.3144         -0.316         0.0316         0.0316         0.0316         0.0317         0.0316         0.0317<	Rohn-D2	Rohn-DB12				-2.745	-2.735	-0.364			-0.004	-0.001
Rohn-DB21         48.51         0.000         -3.143         -3.143         -3.143         -3.143         -3.143         -3.143         -3.143         -3.143         -3.143         -3.143         -0.364         -0.360         -0.020         Rohn-DB32         4.35         0.000         -0.280         -0.272         -0.021         -0.027         -0.020         -0.020         Rohn-DB33         -0.024         0.833         -0.024         0.833         -0.024         0.833         -0.024         0.833         -0.024         0.833         -0.024         0.833         -0.024         0.833         -0.024         0.024 </td <td>Rohn-DB21         48.51         0.000         -3.143         -3.133         -0.364         -0.360           Rohn-DB32         4.32         0.000         -0.280         -0.272         -0.301         -0.304           Rohn-DB31         9.50         0.004         -0.988         2.683         0.027         0.020           Rohn-DB32         48.83         0.004         -2.988         2.988         2.991         0.037           Rohn-DB42         54.33         0.003         -2.988         2.296         2.291         0.304           Rohn-DB42         54.33         0.003         -2.988         2.276         0.281         0.037           Rohn-DB42         54.33         0.003         -0.021         0.029         0.037         0.037           Rohn-DB54         5.33         0.003         -0.021         0.029         0.037         0.037           Rohn-DB54         4.653         4.081         -0.065         0.025         0.324         0.037           Rohn-DB55         9.91         0.000         -4.566         -4.566         -4.561         0.010           Rohn-DB56         8.01         0.000         -4.566         -4.566         -4.876         0.010</td> <td>Rohn-D2</td> <td>Rohn-DB2P</td> <td></td> <td></td> <td></td> <td>2.796</td> <td>2.805</td> <td>0.302</td> <td></td> <td></td> <td>-0.056</td> <td>-0.040</td>	Rohn-DB21         48.51         0.000         -3.143         -3.133         -0.364         -0.360           Rohn-DB32         4.32         0.000         -0.280         -0.272         -0.301         -0.304           Rohn-DB31         9.50         0.004         -0.988         2.683         0.027         0.020           Rohn-DB32         48.83         0.004         -2.988         2.988         2.991         0.037           Rohn-DB42         54.33         0.003         -2.988         2.296         2.291         0.304           Rohn-DB42         54.33         0.003         -2.988         2.276         0.281         0.037           Rohn-DB42         54.33         0.003         -0.021         0.029         0.037         0.037           Rohn-DB54         5.33         0.003         -0.021         0.029         0.037         0.037           Rohn-DB54         4.653         4.081         -0.065         0.025         0.324         0.037           Rohn-DB55         9.91         0.000         -4.566         -4.566         -4.561         0.010           Rohn-DB56         8.01         0.000         -4.566         -4.566         -4.876         0.010	Rohn-D2	Rohn-DB2P				2.796	2.805	0.302			-0.056	-0.040
Rohn-DB32         4.32         0.000         -0.280         -0.272         -0.021         -0.012<	Rohn-DB32         4.32         0.000         -0.280         -0.227         -0.021         -0.021           Rohn-DB34         9.50         0.833         -0.024         0.834         -0.024         -0.831         -0.027           Rohn-DB34         9.50         0.833         -0.024         0.824         0.833         0.017         0.024           Rohn-DB4P         26.01         2.281         -0.024         0.824         0.834         -0.374           Rohn-DB4P         26.01         -0.031         -0.288         -2.788         -2.979         -0.376         0.034           Rohn-DB4D         5.32         0.003         -3.325         -3.316         -0.373         -0.371           Rohn-DB5D         9.91         0.003         -0.024         0.057         0.051         0.035         0.037           Rohn-DB6D         9.91         0.000         -0.057         0.055         0.059         -0.016         0.000           Rohn-DB6D         3.749         0.057         0.055         0.059         -0.016         0.000           Rohn-DB7         3.749         0.057         0.053         0.011         0.010           Rohn-DB7         3.749         0.000         -0	Rohn-D2	Rohn-DB21				-3.143	-3.133	-0.364			-0.006	-0.003
Rohn-DB3P         30.12         2.642         0.035         2.643         0.034         0.050         0.054         0.050	Rohn-DB3P         30.12         2.642         0.035         2.643         0.2407         0.031           Rohn-DB3P         30.12         2.643         0.034         0.524         0.533         0.024         0.034           Rohn-DB31         48.83         0.004         -2.986         -2.987         -2.973         0.0374           Rohn-DB4P         26.01         2.281         -2.986         -2.979         -0.374         0.024           Rohn-DB4P         5.32         0.003         -3.325         -3.326         -3.336         -0.373         0.037           Rohn-DB4P         5.32         0.466         -0.021         0.024         0.037         0.373         0.037           Rohn-DB5P         46.53         40.81         -0.068         4.075         0.466         0.023         0.037           Rohn-DB5P         78.91         0.000         -4.566         -4.566         -4.543         -0.504         0.016           Rohn-DB7         3.749         -0.069         3.749         -4.866         -4.543         -0.504         -0.016           Rohn-DB7         3.89         0.000         -4.869         -4.866         -4.543         -0.504         -0.610 <th< td=""><td>Rohn-D2</td><td>Rohn-DB22</td><td></td><td>0</td><td></td><td>-0.280</td><td>-0.272</td><td>-0.021</td><td></td><td></td><td>-0.026</td><td>-0.017</td></th<>	Rohn-D2	Rohn-DB22		0		-0.280	-0.272	-0.021			-0.026	-0.017
Rohn-DB31         9.30         0.833         -0.024         0.827         0.834         0.014         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.017         0.024         0.018	Rohn-DB47         9.50         0.0833         -0.024         0.0824         0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.084         -0.034         -0.034         -0.037         -0.036         -0.037         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.036         -0.037         -0.037         -0.037<	Rohn-D2	Rohn-DB3F		2.		2.638	2.642	0.297			-0.035	-0.025
Rohn-DB42         48.78         0.0004         -2.988         -2.988         -2.988         -2.989         -2.999         -2.999         -2.99	Rohn-DB42         48.83         0.004         -2.988         -2.2979         -0.574           Rohn-DB41         26.83         0.003         -2.988         -2.2979         -0.574           Rohn-DB42         2.281         0.003         -3.325         -3.325         -3.316         -0.373         -0.371           Rohn-DB51         9.91         0.069         4.075         0.657         0.869         -0.016         0.023         0.036           Rohn-DB52         78.91         0.060         -0.057         0.865         -0.016         0.0	Rohn-D2	Rohn-DB31		0 0		128.0	0.833	0.01/			-0.024	-0.01¢
Rohn-DB47         54.33         0.003         -2.70	ROMIN-DB4F         5.00         1.00	Rohn-DZ	Rohn-DB32		0.004	-2.988	12,988	12.9.0	0.070			0.003	0.00
Rohn-DBS         46.53         4.081         -0.068         4.072         0.068         -0.068         -0.068           Rohn-DBS         46.53         4.081         -0.068         4.072         0.035         0.036         0.058         0.068           Rohn-DBS         46.53         4.081         -0.068         4.085         -0.068         0.068	Rohn-DB52 (6.53 4.081 0.066 4.072 0.466 0.023 0.036 Rohn-DB54 (6.53 4.081 0.068 4.072 0.466 0.002 0.006 Rohn-DB54 (6.53 4.081 0.068 4.072 0.466 0.002 0.006 Rohn-DB54 1.0 0.000	Konn-DZ	Ronn-UB4F		V C	10.038	2.2.2	102.2	-0.373			0.03	0.00
Rohn-DBS         46.53         4.081         -0.057         4.081         -0.057         -0.068         -0.061         -0.041         -0.041         -0.041         -0.041         -0.063         -0.014         -0.041         -0.041         -0.063         -0.014         -0.063         -0.071         -0.063         -0.071         -0.063         -0.071         -0.063         -0.071         -0.063         -0.071         -0.063         -0.071         -0.063         -0.071         -0.063         -0.072         -0.063         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073         -0.073 </td <td>Rohn-DB5 46.53 4.081 -0.068 4.072 4.081 0.350 0.368 Rohn-DB5 9.91 0.869 -0.057 0.855 0.869 -0.010 0.000 0.000 0.000 0.368 0.000 0.368 0.000 0.000 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.374 0.3749 0.352 0.3748 0.352 0.3748 0.352 0.3748 0.352 0.3749 0.3749 0.374</td> <td>Pohn-D2</td> <td>Pohn-Da43</td> <td></td> <td></td> <td>-0.025</td> <td>0.35.0</td> <td>3,310</td> <td>0.00</td> <td></td> <td></td> <td>-0.02</td> <td>-0.0</td>	Rohn-DB5 46.53 4.081 -0.068 4.072 4.081 0.350 0.368 Rohn-DB5 9.91 0.869 -0.057 0.855 0.869 -0.010 0.000 0.000 0.000 0.368 0.000 0.368 0.000 0.000 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.000 0.368 0.374 0.3749 0.352 0.3748 0.352 0.3748 0.352 0.3748 0.352 0.3749 0.3749 0.374	Pohn-D2	Pohn-Da43			-0.025	0.35.0	3,310	0.00			-0.02	-0.0
Rohn-DB5         9.91         0.869         -0.057         0.869         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.067         0.069         -0.069 <th< td=""><td>Rohn-DB51         9.91         0.869         -0.057         0.865         -0.869         -0.016         -0.018<!--</td--><td>Rohn-D2</td><td>Pohn-DB5</td><td></td><td>180 V</td><td>130.0 -0 068</td><td>4.072</td><td>4 081</td><td>0.350</td><td></td><td></td><td>-0.068</td><td>-0.04</td></td></th<>	Rohn-DB51         9.91         0.869         -0.057         0.865         -0.869         -0.016         -0.018 </td <td>Rohn-D2</td> <td>Pohn-DB5</td> <td></td> <td>180 V</td> <td>130.0 -0 068</td> <td>4.072</td> <td>4 081</td> <td>0.350</td> <td></td> <td></td> <td>-0.068</td> <td>-0.04</td>	Rohn-D2	Pohn-DB5		180 V	130.0 -0 068	4.072	4 081	0.350			-0.068	-0.04
Rohn-DB52         78.91         0.000         -4.566         -4.556         -4.543         -0.504         -0.491         -1.037         -0.041           Rohn-DB54         42.74         3.749         -0.069         3.749         -4.876         -0.502         0.350         0.709         -0.068           Rohn-DB62         5.90         0.517         -0.055         0.503         0.517         -0.010         0.005         -0.055           Rohn-DB7         3.89         0.000         -4.899         -4.861         -0.010         0.005         -0.059           Rohn-DB7         3.89         0.000         -4.046         -4.046         -4.021         -0.089         -0.070           Rohn-DB7         4.364         -0.070         -4.046         -4.021         -0.089         -0.070           Rohn-DB8         4.45         -0.070         -4.249         -4.046         -4.049         -0.070         -0.059         -0.053           Rohn-DB8         4.45         4.046         -4.021         -0.488         -0.063         -0.053         -0.053         -0.070         -0.089         -0.053         -0.070         -0.099         -0.053         -0.053         -0.010         -0.089         -0.099         -	Rohin-DB52         78.91         0.000         -4.566         -4.543         -0.504         -0.491           Rohin-DB62         42.74         3.749         -0.069         3.749         -0.069         -0.089         -0.502         -0.370           Rohin-DB62         5.90         4.899         -4.899         -4.876         -0.552         0.037           Rohin-DB72         5.90         4.561         -0.075         4.551         -0.019         -0.185         -0.379           Rohin-DB72         73.88         0.000         -4.046         -4.021         -0.081         -0.063           Rohin-DB82         9.99         0.000         -4.046         -4.021         -0.332         0.073           Rohin-DB82         9.99         0.000         -4.368         -4.368         -4.343         -0.488         -0.473           Rohin-DC12         0.000         -4.368         -4.368         -4.343         -0.061         -0.073           Rohin-DC12         0.000         -4.368         -4.368         -4.343         -0.081         -0.033           Rohin-DC12         0.000         -6.547         -0.547         -0.229         -0.071           Rohin-DC2         0.000         -6.347	Rohn-D2					0,855	0.869	-0.016			-0.057	-0.04
Rohn-DB6P         42.74         3.749         -0.069         3.749         -0.352         0.370         0.788         -0.069           Rohn-DB61         84.67         0.000         -4.899         -4.876         -0.552         0.370         0.779         -0.059           Rohn-DB7         52.01         4.561         -0.070         4.553         4.561         -0.030         0.079         -0.055           Rohn-DB7         3.89         0.000         -4.046         -4.021         -0.188         -0.379         0.059         -0.057           Rohn-DB7         48.45         4.249         -0.015         -0.015         -0.081         -0.059         -0.057           Rohn-DB8         48.45         4.249         -0.070         4.249         -0.070         4.249         -0.070         -0.052         -0.071         -0.053         -0.052         -0.071         -0.053         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052         -0.071         -0.052	Rohn-DB6P         42.74         3.749         -0.069         3.740         3.749         0.352         0.370           Rohn-DB6I         84.67         0.000         -4.899         -4.899         -4.895         -0.202         -0.489           Rohn-DB7P         52.01         4.561         -0.075         0.503         0.517         -0.010         0.005           Rohn-DB7P         52.01         4.561         -0.070         4.553         4.561         0.379         0.397           Rohn-DB7         73.89         0.000         -4.046         -4.046         -4.021         -0.063           Rohn-DB8         48.45         4.249         -0.074         -4.249         0.381         0.400           Rohn-DB8         48.45         4.249         -0.074         -0.073         -0.063           Rohn-DC1P         46.08         4.510         -0.124         4.348         4.510         0.371         0.064           Rohn-DC1P         45.09         0.000         -0.124         4.488         4.510         0.004           Rohn-DC2P         42.65         4.174         -0.124         4.188         4.174         0.337           Rohn-DC2P         5.69         0.000         -	Rohn-D2			0		-4.566	-4.543	-0.504			-0.041	-0.02
Rehn-DB61         84 67         0.000         -4.899         -4.819         -6.819         -6.010         -6.929         -6.070         -6.929         -6.070         -6.929         -6.070         -6.929         -6.070         -6.929         -6.070         -6.929         -6.010         -6.929         -6.010	Rohn-DB61         84.67         0.000         -4.899         -4.899         -4.876         -0.502         -0.489           Rohn-DB62         5.90         0.517         -0.055         0.503         -0.010         0.005           Rohn-DB7         3.89         0.000         -4.013         -0.195         -0.010         0.005           Rohn-DB7         73.89         0.000         -4.046         -4.046         -4.011         0.063           Rohn-DB8         79.75         0.000         -4.368         -4.368         -4.349         0.182         0.407           Rohn-DB8         79.75         0.000         -4.368         -4.368         -4.349         0.188         0.408           Rohn-DB8         46.08         4.510         -0.547         -0.547         0.060         -0.647         0.060           Rohn-DC1         10.10         0.980         -0.124         4.488         4.510         0.304         0.061           Rohn-DC2         6.6         0.000         -5.47         -0.524         0.510         0.003           Rohn-DC2         6.5         0.014         -0.124         4.183         4.174         0.340         0.340           Rohn-DC2         6.5	Rohn-D2			(C)		3.740	3.749	0.352			-0.069	-0.05
Rohn-DB62         5.90         0.517         -0.055         0.553         4.561         -0.055         0.009         0.009         0.005         0.005         0.005         0.005         0.005         0.007         0.005         0.007         0.005         0.007         0.007         0.008         0.007         0.008         0.007         0.008         0.009         0.009         0.009         0.009         0.009         0.009         0.009         0.000         0.000         0.002         0.000	Rohn-DBAC         5,90         0.517         -0.055         0.503         0.517         -0.055           Rohn-DBAC         3.89         0.517         -0.053         0.517         -0.053         0.517         -0.063           Rohn-DBAC         3.89         0.000         -4.046         -4.021         -0.195         -0.081         -0.063           Rohn-DBAC         4.249         0.000         -4.046         -4.046         -4.049         -0.379         0.067           Rohn-DBBIC         9.75         0.000         -4.368         -4.346         -4.349         0.486         -0.470           Rohn-DCID         10.01         0.80         -0.547         -0.529         -0.077         -0.060           Rohn-DCID         10.01         0.980         -0.114         0.951         0.980         -0.061           Rohn-DCID         46.08         4.510         -0.124         -4.488         4.510         0.337           Rohn-DCID         62.60         0.000         -5.346         -5.346         -5.365         -0.034           Rohn-DCID         62.61         0.000         -5.44         -5.645         -5.603         -0.610         -0.031           Rohn-DCID         5.63	Rohn-D2	ш		0		-4.899	-4.876	-0.502			-0.042	-0.03(
Rohn-DB7P         52.01         4.551         -0.070         4.553         -0.070         4.553         -0.070         0.379         0.397         0.096         -0.070           Rohn-DB71         3.89         0.000         -4.046         -4.021         -0.488         -0.433         -0.928         -0.056           Rohn-DB81         79.75         0.000         -4.046         -4.021         -0.488         -0.473         -0.928         -0.0570           Rohn-DB81         79.75         0.000         -4.046         -4.249         -0.470         -0.929         -0.0570           Rohn-DB82         9.99         0.000         -0.547         -0.547         -0.529         -0.077         -0.060         -0.160         -0.052           Rohn-DC11         10.01         0.980         -0.124         4.488         4.510         0.060         -0.160         -0.162         -0.067           Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.305         -0.064         -0.034         0.124         -0.124           Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.305         -0.624         -0.595         -1.250         -0.104	Rohn-DB7P         52.01         4.561         -0.070         4.553         4.561         0.037           Rohn-DB72         3.89         0.000         -0.213         -0.213         -0.195         -0.081         -0.063           Rohn-DB8P         48.45         4.249         -0.070         4.246         -4.021         -0.488         -0.473           Rohn-DB8P         48.45         0.000         -4.046         -4.021         -0.488         -0.470           Rohn-DB8P         48.45         0.000         -4.369         -4.349         -0.347         -0.529         0.378           Rohn-DC1P         46.08         4.510         -0.124         4.488         4.510         0.369           Rohn-DC1P         46.08         4.510         -0.124         4.488         4.510         0.364         -0.064           Rohn-DC2P         42.65         4.174         -0.124         4.153         4.174         0.346         -0.594           Rohn-DC2P         6.26         0.000         -5.46         5.305         -0.624         -0.591           Rohn-DC2P         6.26         0.100         -5.46         5.645         5.630         0.061         -0.591           Rohn-DC3P	Rohn-D2					0.503	0.517	-0.010			-0.055	-0.04
Rohn-DBA         4.00         -4.01         -4.01         -0.01         -0.02         -0.02         -0.02         -0.03         -0.06         -0.03         -0.05         -0.03         -0.05         -0.03         -0.05         -0.03         -0.05         -0.03         -0.05         -0.03         -0.06         -0.03         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.05         -0.06         -0.05         -0.05         -0.05         -0.05         -0.05         -0.06         -0.05         -0.05         -0.05         -0.06         -0.05         -0.05         -0.06         -0.05         -0.06         -0.05         <	Rohn-DB4         3:89         0.000         -0.213         -0.214         -0.18         -0.473           Rohn-DB4         48.45         4.249         -0.070         4.249         -0.488         -0.473           Rohn-DB4         49.75         0.000         -4.364         -4.249         0.382         0.400           Rohn-DB4         46.08         4.510         -0.077         -0.547         -0.529         0.077         -0.470           Rohn-DC1P         46.08         4.510         -0.124         4.488         4.510         0.337         0.369           Rohn-DC1P         46.08         4.510         -0.124         4.488         4.510         0.337         0.369           Rohn-DC1P         45.09         0.000         -5.346         -5.346         -5.305         0.064         -0.034           Rohn-DC2P         42.65         4.174         4.153         4.174         0.340         0.375           Rohn-DC2P         6.260         0.000         -5.445         -5.455         -5.645         -5.645         -5.645         -5.645         -5.645         -5.61         0.031           Rohn-DC2P         6.260         0.000         -5.645         -5.645         -5.645	Rohn-D2					4.553	4.561	0,379			-0.070	-0.05
Rohn-DBM         73.78         0.000         -4.048         -4.049         -0.378         -0.458         -0.070           Rohn-DBM         79.75         0.000         -0.436         -4.349         0.382         0.400         0.899         -0.070           Rohn-DBM         79.75         0.000         -0.547         -0.587         -0.662         0.062           Rohn-DCIP         46.08         4.510         -0.124         4.88         4.510         0.359         -0.052           Rohn-DCIP         46.08         4.510         -0.124         4.88         4.510         0.359         -0.124         0.980         -0.062           Rohn-DCIP         46.08         4.510         -0.124         0.980         -0.064         -0.034         0.112         0.022           Rohn-DCIP         4.08         4.511         0.980         -0.064         -0.034         0.112         0.112           Rohn-DCIP         4.09         -0.114         0.981         -5.365         -5.365         -0.595         -1.250         -0.104           Rohn-DCIP         6.26         0.000         -5.465         -5.635         -6.62         0.059         -1.124         0.114           Rohn-DCIP	Rohn-DBH         73.83         0.000         -4.146         -4.124         0.486         -0.410           Rohn-DBH         79.75         0.000         -4.368         -4.349         0.382         0.400           Rohn-DBH         79.75         0.000         -4.368         -4.349         0.382         0.400           Rohn-DCH         46.08         4.510         -0.124         4.88         4.343         -0.486         -0.410           Rohn-DC1         9.99         0.000         -4.368         -0.547         -0.529         -0.077         -0.060           Rohn-DC1         10.01         0.980         -0.124         4.488         4.510         0.364         -0.369           Rohn-DC2         42.65         4.174         -0.124         4.183         4.174         0.340         -0.372           Rohn-DC2         62.60         0.000         -5.446         -5.63         -0.621         -0.034           Rohn-DC2         62.90         0.616         -0.113         0.587         -5.63         -0.61         -0.031           Rohn-DC2         62.90         0.616         -0.113         0.587         -0.611         -0.611         -0.611         -0.611         -0.611	Rohn-D2					-0.213	-U.195	-0.08I			-0.063	-0.046
Rohn-DB81         79.75         0.000         -4.368         -4.343         -0.486         -0.470         -0.999         -0.052           Rohn-DB82         9.99         0.000         -0.547         -0.589         -0.529         -0.052         -0.160         -0.160         -0.160         -0.062           Rohn-DC1P         46.08         4.510         -0.124         4.981         4.510         0.037         -0.060         -0.160         -0.162           Rohn-DC1P         46.09         4.510         -0.124         4.981         -0.581         0.380         -0.034         0.142         -0.124           Rohn-DC1P         59.29         0.000         -5.346         -5.346         -5.365         -0.624         -0.595         -1.250         -0.104           Rohn-DC2P         42.65         4.114         -0.124         4.115         -0.124         -0.112           Rohn-DC2P         6.20         0.000         -5.645         -5.63         -0.62         -0.591         -1.213           Rohn-DC2P         6.29         0.616         -0.113         0.587         0.616         -0.013         0.012         0.011           Rohn-DC3P         57.60         0.009         0.021         0.011 </td <td>  Rohn-DB81   79.75   0.000   -4.368   -4.368   -4.343   0.486   -0.470   Condensity   79.75   0.000   -4.368   -4.368   -4.368   -4.343   -0.486   -0.470   Condensity   6.000   -0.547   -0.547   -0.559   -0.077   -0.060   Condensity   Con</td> <td>Rohn-D2</td> <td></td> <td></td> <td></td> <td></td> <td>4.046</td> <td>-4.02I</td> <td>0.488</td> <td></td> <td></td> <td>0.020</td> <td>-0.03</td>	Rohn-DB81   79.75   0.000   -4.368   -4.368   -4.343   0.486   -0.470   Condensity   79.75   0.000   -4.368   -4.368   -4.368   -4.343   -0.486   -0.470   Condensity   6.000   -0.547   -0.547   -0.559   -0.077   -0.060   Condensity   Con	Rohn-D2					4.046	-4.02I	0.488			0.020	-0.03
Rohn-DB82         9.99         0.000         0.547         -0.547         -0.529         -0.077         -0.060         -0.160         -0.062           Rohn-DC11         46.08         4.510         -0.124         4.488         4.510         0.337         0.369         0.032         0.124           Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.305         -0.624         -0.595         -1.250         -0.104           Rohn-DC12         59.29         0.000         -5.346         -5.305         -0.624         -0.595         -1.250         -0.104           Rohn-DC1         6.26         0.000         -5.445         -5.36         -5.305         -0.624         -0.595         -1.24         -0.104           Rohn-DC2         6.29         0.000         -5.445         -5.645         -5.63         -0.621         -0.591         -1.124         -0.104           Rohn-DC2         6.29         0.616         -0.013         0.567         -0.616         -0.617         -0.113           Rohn-DC3         6.29         0.616         -0.017         5.630         -0.621         -0.113         0.616         -0.011           Rohn-DC3         6.270         0.011	Rohn-DB82         9.99         0.000         -0.547         -0.547         -0.529         -0.077         -0.060           Rohn-DC1         46.08         4.510         -0.124         4.488         4.510         0.359           Rohn-DC1         10.01         0.980         -0.114         0.951         0.980         -0.034           Rohn-DC1         59.29         0.000         -5.346         -5.305         -0.624         -0.595           Rohn-DC2         42.65         4.174         -0.124         4.153         4.174         0.340         0.372           Rohn-DC2         62.9         0.000         -5.465         -5.645         -5.630         -0.629         0.031           Rohn-DC2         62.9         0.616         -0.113         0.587         0.616         -0.031           Rohn-DC2         62.9         0.616         -0.113         0.587         0.616         -0.031           Rohn-DC2         62.9         0.616         -0.113         0.587         0.616         -0.031           Rohn-DC2         62.9         0.616         -0.111         1.257         -6.617         -0.617         0.616         -0.031           Rohn-DC3         7.4         0.007 <td>Rohn-D2</td> <td></td> <td></td> <td></td> <td></td> <td>-4.368</td> <td>-4.343</td> <td>-0.486</td> <td></td> <td></td> <td>-0.052</td> <td>-0.03</td>	Rohn-D2					-4.368	-4.343	-0.486			-0.052	-0.03
Rohn-DCIP         46.08         4.510         -0.124         4.488         4.510         0.337         0.369         0.922         -0.124           Rohn-DCII         10.01         0.980         -0.114         0.951         0.980         -0.064         0.034         0.104         0.114           Rohn-DCIP         42.65         4.174         -0.124         4.153         4.174         -0.124         4.153         4.174         -0.124         7.174         -0.124         7.174         -0.124         4.134         -0.124         4.134         -0.124         4.134         -0.124         0.340         0.340         0.372         0.347         0.124           Rohn-DCI2         6.29         0.616         -0.113         0.587         0.616         -0.061         -0.131         0.016           Rohn-DCI3         5.76         5.63         0.616         -0.061         -0.113         0.587         0.616         -0.031         0.011           Rohn-DCI3         1.286         5.63         0.017         0.017         0.572         -0.017           Rohn-DCI3         1.286         0.011         1.259         0.001         0.012         0.011	Rohn-DCIP         46.08         4.510         -0.124         4.488         4.510         0.337         0.369           Rohn-DCII         10.01         0.980         -0.114         0.951         0.034         -0.034           Rohn-DCIP         42.65         4.174         -0.124         4.153         4.174         0.340         0.375           Rohn-DC2P         42.65         4.174         -0.124         4.153         4.174         0.340         0.372           Rohn-DC2P         62.0         0.000         -5.645         -5.633         -0.621         -0.591           Rohn-DC2P         6.29         0.616         -0.113         0.587         0.616         -0.031           Rohn-DC2P         5.637         -0.017         5.637         5.637         0.048         0.048           Rohn-DC3P         57.60         5.637         -0.017         5.637         5.630         0.482         0.487           Rohn-DC3P         7.29         0.001         -6.546         -6.546         -6.540         0.051           Rohn-DC3P         57.60         5.637         -0.017         5.637         5.630         0.482         0.481           Rohn-DC3P         7.25         6.567	Rohn-D2			0.0		-0.547	-0.529	-0.077			-0.062	-0.04
Rohn-DC11         10.01         0.980         -0.114         0.951         0.980         -0.064         -0.034         0.142         -0.114           Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.305         -0.624         -0.597         -1.250         -0.106           Rohn-DC2P         42.65         4.174         -0.124         4.134         0.340         0.372         0.847         -0.124           Rohn-DC2P         62.60         0.000         -5.645         -5.645         -5.603         -0.620         -0.591         -1.317         -0.106           Rohn-DC2P         6.29         0.616         -0.113         0.587         0.616         -0.051         -0.113           Rohn-DC3P         57.60         5.637         -0.017         5.637         0.001         -0.113           Rohn-DC3P         57.60         0.001         -0.017         5.637         0.009         0.012         0.017	Rohn-DC11         10.01         0.980         -0.114         0.951         0.980         -0.064         -0.064         -0.064         -0.034           Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.346         -0.595           Rohn-DC21         62.60         0.000         -5.645         -5.633         -0.629         -0.372           Rohn-DC22         62.90         0.616         -0.113         0.587         -0.621         -0.631           Rohn-DC3P         5.63         0.616         -0.113         0.587         -0.061         -0.031           Rohn-DC3P         5.63         0.017         5.637         5.630         0.482         0.487           Rohn-DC3P         5.63         0.011         1.259         -0.011         5.637         0.061         0.011           Rohn-DC3P         7.2         0.000         -6.656         -6.656         0.001         -6.657         0.001	Rohn-D3	_		4.			4.510	0.337			-0.124	-0.09
Rohn-DC12         59.29         0.000         -5.346         -5.346         -5.346         -5.346         -0.124         -0.105         -0.106           Rohn-DC2P         42.65         4.174         -0.124         4.174         0.340         0.342         0.347         0.347         0.124           Rohn-DC2P         62.60         0.000         -5.645         -5.633         -0.620         -0.591         -1.134           Rohn-DC2P         6.29         0.616         -0.113         0.587         0.616         -0.061         -0.101           Rohn-DC3P         57.60         5.637         -0.017         5.637         -0.017         0.017           Rohn-DC3P         12.86         1.259         -0.011         1.259         0.009         0.012         0.012	Rohn-DC12 59.29 0.000 -5.346 -5.305 -0.624 -0.595 Rohn-DC2P 42.65 4.174 -0.124 4.153 4.174 0.340 0.372 Rohn-DC2L 62.60 0.000 -5.645 -5.645 -5.603 -0.620 -0.591 Rohn-DC3Z 6.29 0.616 -0.113 0.587 0.616 -0.061 -0.031 Rohn-DC3P 57.60 5.637 -0.017 5.637 5.630 0.482 0.487 Rohn-DC3 7.20 0.000 0.011 1.259 -0.001 1.259 0.009 0.012 Rohn-DC3 7.20 0.000 0.012	Rohn-D3			0.			0.980	-0.064			-0.114	-0.08
Ronn-DC2P 42.65 4.174 -0.124 4.155 4.177 -0.124 -0.124 8.056 0.000 -5.656 0.000 -5.655 -5.603 -0.620 -0.591 -1.317 -0.106 Rohn-DC22 6.29 0.616 -0.113 0.597 0.616 -0.061 -0.031 0.061 -0.113 Rohn-DC3P 57.60 5.637 -0.017 5.637 0.616 -0.061 -0.031 0.061 -0.113 Rohn-DC3P 57.60 5.637 -0.017 1.244 -0.017 Rohn-DC3P 0.009 0.012 0.272 -0.017 0.009 0.012 0.272 -0.011	Rohn-DC2P 42.65 4.174 -0.124 4.153 4.174 0.340 0.372 Rohn-DC21 62.60 0.000 -5.645 -5.645 -5.633 -0.620 -0.551 Rohn-DC22 6.29 0.616 -0.113 0.587 0.616 -0.031 Rohn-DC3P 57.60 5.637 -0.017 5.637 5.630 0.482 0.487 Rohn-DC31 12.86 1.259 -0.011 1.257 1.259 0.009 0.012 Rohn-DC31 7.42 0.001 -6.546 -6.540 -0.578 0.596	Rohn-D3							-0.624			-0.106	-0.07
AOMIT-DC22 6.29 0.616 -0.113 0.587 0.616 -0.061 0.061 -0.113 0.587 0.616 -0.061 -0.031 0.061 -0.113 Rohn-DC3P 57.60 5.637 -0.017 5.637 5.630 0.482 0.487 1.244 -0.017 Rohn-DC3I 12.86 1.259 -0.011 1.257 1.259 0.009 0.012 0.272 -0.011	Rohn-DC22 6.29 0.616 -0.113 0.587 0.616 -0.031 Rohn-DC3P 57.60 5.637 -0.017 5.637 5.630 0.482 0.487 Rohn-DC31 12.86 1.259 -0.017 1.259 0.009 0.012 Rohn-DC31 7.42 0.000 -6.556 -6.540 0.528 0.556	Rohn-Da			4.0				0.340			-0.124 -0.106	90.01
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0.01234 0.0244 0.024	-0.213 -0.212 -0.209 -0.218
1.181 1.199 1.	-2.499 2.065 -2.439 -0.069
0.0 4 4 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-0.693 0.369 -0.684 -0.153
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5.349 1.008 1.	-10.606 9.838 -10.342 0.388
	-10.665 9.792 -10.400 0.332
-0.0172 -0.0172 -0.0236 -0.236 -0.236 -0.237	
5. 357 1. 1008 1. 1008 1. 1008 1. 1008 1. 1000 1. 1	0.000 9.838 0.000 0.388
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Rohn-DC4P Rohn-DC4P Rohn-DC4P Rohn-DC52 Rohn-DC52 Rohn-DC61 Rohn-DD10 Rohn-DD11 Rohn-DD12 Rohn-DD13 Rohn-DD13 Rohn-DD14 Rohn-DD13 Rohn-DD14 Rohn-DD14 Rohn-DD14 Rohn-DD14 Rohn-DD12 Rohn-DD14 Rohn-DD13 Rohn-DD14 Rohn-DD13 Rohn-DD14 Rohn-DD14 Rohn-DD13 Rohn-DD14 Rohn-DD12 Rohn-DD13 Rohn-DD14 Rohn-DD13 Rohn-DD14 Rohn-DD13 Rohn-D	Rohn-DG32 Rohn-DG4P Rohn-DG41 Rohn-DG42
Rohn-D3 Rohn-D3 Rohn-D3 Rohn-D3 Rohn-D3 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D4 Rohn-D5 Rohn-D5 R-D4-M0D	Rohn-D6 Rohn-D6 Rohn-D6 Rohn-D6

0.134 0.1149 0.1149 0.1149 0.1194	
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1. 915 -0. 219 -0. 219 -0. 169 -0. 169 -0. 169 -0. 169 -0. 169 -0. 169 -0. 169 -0. 191 -0. 192 -0. 191 -0.	
0.260 0.260 0.263 0.263 0.177 0.177 0.193 0.193 0.105 0.106 0.107 0.107 0.108 0.	
0.200 0.236 0.236 0.236 0.236 0.236 0.237 0.237 0.237 0.237 0.252 0.150 0.147 0.150 0.137 0.	
9.123 -0.231 -0.231 0.018 0.018 10.0525 10.0526 0.05776 0.0576 0.0576 0.0576 0.05776 0.05776 0.05776 0.05776 0.	
9.068 -0.290 9.328 -9.671 -0.043 -0.043 -0.043 -0.043 -0.043 -0.043 -0.023 -0.273 -0.2	
-0.240 -0.290 -0.290 -0.290 -0.291 -0.231 -0.233 -0.283 -0.2833 -0.182 -0.183 -0.183 -0.193 -	
9.123 0.000 0.000 0.000 0.000 0.018 0.000	
73.38 2.338 75.46 77.746 77.746 75.402 75.403 75.403 75.403 75.403 75.403 75.403 75.403 75.403 75.403 75.603 76.203 7	
Rohn-DH1P Rohn-DH11 Rohn-DH11 Rohn-DH11 Rohn-DH12 Rohn-DH21 Rohn-DH32 Rohn-DH32 Rohn-DH32 Rohn-DH32 Rohn-DH32 Rohn-DH31 Rohn-DH31 Rohn-DH31 Rohn-DH31 Rohn-DH112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D1112 Rohn-D131 Rohn-D131 Rohn-D131 Rohn-D131 Rohn-D131 Rohn-LB12 Rohn-LB12 Rohn-LB12 Rohn-LB12 Rohn-LB13 Rohn-LD12 Rohn-LD12 Rohn-LD12 Rohn-LD13 Rohn-LE12	
Rohn-D7	

-7.5739 -7.5739 -7.5739 -7.7373 -7.7373 -7.7373 -9.0228	0.010 0.031 0.026 0.014
-100.09999999999999999999999999999999999	0.015 0.045 0.038 0.021
44.430 4	0.030 0.650 0.018 -0.587
20.0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.032 0.361 0.025 -0.315
13. 4949 13. 49	0.037 0.375 0.036 -0.309
1154 - 823 166 - 182 167 - 182 168 - 182 173 - 123 189 - 122 189 - 123 189 - 123	0.094 2.796 -0.027 -2.699
1.7.722 63.7.722 64.071 1.1968 1.29.132 1.29.132 1.29.132 1.29.132 1.29.132 1.29.133 1.29.133 1.29.133 1.29.133 1.29.133 1.30.133 1	0.099 2.816 -0.016 -2.699
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25.0.31 25.0.31 26.0.31 27.0.02 28.0.25 28.	0.85 24.08 0.32 21.71
Rohn-LE2P Rohn-LE2P Rohn-LE21 Rohn-LE31 Rohn-LE31 Rohn-LE31 Rohn-LE31 Rohn-LE31 Rohn-LE31 Rohn-LE31 Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI42P Rohn-LI41P Rohn-LI41P Rohn-LI42P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-LI41P Rohn-H11P Rohn-H11P Rohn-H11P Rohn-H11P Rohn-H12P	SNB-DB22 SNB-DB3P SNB-DB31 SNB-DB31
Rohn-L5 Rohn-L5 Rohn-L5 Rohn-L5 Rohn-L6 Rohn-L6 Rohn-L6 Rohn-L7 Rohn-L	SNB-D2 SNB-D2 SNB-D2 SNB-D2

0.033 0.0143 0.0222 0.0222 0.0222 0.0222 0.0222 0.0133 0.0134 0.0135 0.0134 0.0135 0.0135 0.0222 0.0135 0.0135 0.0231 0.0
0.0025 0.0035 0.0035 0.0035 0.0031 0.0031 0.0025 0.
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0.3377 0.3377 0.33788 0.33788 0.3378 0.3378 0.3378 0.3378 0.3378 0.3378 0.3378 0.33
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24.13 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 28.095 4.812 4.812 4.812 4.812 4.812 4.812 4.812 4.813 4.812 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 4.813 6.914 6.916
SNB-DB4P SNB-DB41 SNB-DB41 SNB-DB41 SNB-DB42 SNB-DB42 SNB-DB5P SNB-DB52 SNB-DB62 SNB-DB63
SNB-D2 SNB-D3 SNB-D4

0.145 0.145 0.1543 0.1543 0.1543 0.1549 0.1655 0.1655 0.1657 0.1657 0.1673 0.1773 0.17	-1.269 -1.261 -1.657 -1.426
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2. 634 -2. 348 -2. 554 -2. 554 -3. 179 -3. 179 -4. 179 -5. 179 -6. 179 -7.	0.692 0.724 -7.744 1.392
0.780 0.239 0.2539 0.2539 0.2539 0.2583	-4.100 0.196 0.204 -5.456 0.474 0.484
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SNB-DF1P SNB-DF12 SNB-DF22 SNB-DF22 SNB-DF22 SNB-DF23 SNB-DF23 SNB-DF31 SNB-DF31 SNB-DF41 SNB-DF41 SNB-DG11 SNB-DG22 SNB-DG22 SNB-DG22 SNB-DG33 SNB-DG42 SNB-DG42 SNB-DG42 SNB-DG42 SNB-DG42 SNB-DG42 SNB-DG12 SNB-DH12 SNB-DH13 SNB-DH13 SNB-DH13 SNB-DH13 SNB-DH13 SNB-DH13 SNB-DH12 SNB-DH13 SNB	SNB-LB27 SNB-LB21 SNB-LB22 SNB-LB3P SNB-LB31
SNB-D5 SNB-D6 SNB-L1	SNB-L2 SNB-L2 SNB-L2 SNB-L2 SNB-L2 SNB-L2

1. 816 1. 1. 580 1. 1. 560 1. 1. 560 1. 2. 502 2. 502 2. 502 2. 502 2. 502 2. 503 1. 3. 213 1. 3. 2	0.021 0.000 0.000 0.003 0.031 0.013 0.013 0.018 0.018
22,429 -2,103 -2,104 -2	00000000000000
2.048 2.048 2.048 2.1493 2.720 3.881 3.881 3.881 3.881 3.881 3.881 3.881 5.337 5.337 6.610 6.525 6.610 6.525 6.610 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 8.317 9.32 10.383	0.060 0.124 -0.0129 -0.092 0.063 -0.014 0.038 -0.038 0.280 0.280 0.173
-6.453 0.745 0.745 0.746 0.746 0.746 0.746 0.746 0.746 0.746 0.746 0.746 0.746 0.746 0.746 1	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
-7 069 0.215 0.216 0.119 0.119 0.119 0.189 0.189 0.666 0.393 0.416 0.416 0.435 0.657 0.657 0.657 0.657 0.7113 0.725	0.088 0.050 0.050 0.078 0.078 0.002 0.027 0.027 0.0129 0.129
36.169 15.575 15.575 20.625 20.625 20.625 27.512 27.512 27.512 27.512 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 34.263 36.273 37.262 36.103 36	0.160 0.160 0.510 0.0150 0.0376 0.0478 0.063 0.063 0.063
36.865 15.086 15.086 17.5.086 17	1.00-1-00-1-00-1-00-1-00-1-00-1-00-1-00
-36.863 -2.109 -47.958 -2.718 -2.718 -3.340 -3.340 -3.408 -3.408 -3.408 -4.286 -4.286 -4.286 -4.286 -4.286 -4.264 -118.038 -9.382 -9.382 -9.382 -9.382 -9.382 -11.066 -11	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 15.575 15.765 0.000 20.427 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00	0.190 0.120 0.012 0.012 0.012 0.023 0.035 0.045 0.045 0.045 0.045 0.045 0.045 0.045 0.045
20.113 27.74 27.74 113.67 113.	
SNB-LB412 SNB-LB412 SNB-LB412 SNB-LC112 SNB-LC12 SNB-LC22 SNB-LC22 SNB-LC22 SNB-LC23 SNB-LC23 SNB-LC23 SNB-LC23 SNB-LC23 SNB-LC23 SNB-LC23 SNB-LC34 SNB-LC34 SNB-LC34 SNB-LC34 SNB-LC34 SNB-LC35 SNB-LC35 SNB-LC35 SNB-LC37	
SNB-112 SNB-113 SNB-114 SNB-114 SNB-114 SNB-114 SNB-114 SNB-114 SNB-114 SNB-114 SNB-115 SNB-114 SNB-114 SNB-115 SNB-116 SNB-116 SNB-116 SNB-117 SNB-11	Connect

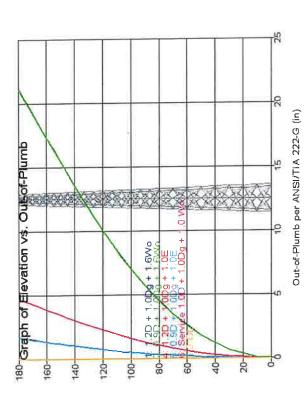
00000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
00.00 00	0.50	0.599 0.099	00000000000000000000000000000000000000
0.202 -0.0033 -0.0033 -0.011 -0.011 -0.011 0.102 0.102 0.103 0.103 0.178 0.178	0.000	0.000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.0022 0.0032 0.0032 0.0032 0.0033 0.0033 0.0033 0.0033 0.0033	00000000000000000000000000000000000000	00000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
00000000000000000000000000000000000000	0.000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000000000000000000000000000000000000
0.781 0.314 0.295 0.295 0.0295 0.0397 0.039 0.0158 0.0168	0.134 0.134 0.145 0.145 0.1425 0.1225 0.1227 0.1464 0.1464 0.1464 0.1681	11.54 11.58	2.2.2.2.3.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.
0.2699 0.2669 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.017 0.018 0.01	0.000 0.000	1.569 1.7569 1.7569 0.710 0.720 0.622 0.623 0.623 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.03	1 1 9 9 5 8 8 9 8 9 8 9 8 9 8 9 8 9 9 8 9 9 9 9
0.0000000000000000000000000000000000000	0.000 0.000	11, 735 0,000 0,000 0,000 0,000 0,000 1,1,562 1,1,362 1,1,362 0,000 0,00	2.2.2.2 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.0599 0.0599 0.0810 0.0810 0.087 0.087 0.166 0.166 0.166 0.135	0.323 0.323 3.440 0.440 0.673 0.673 0.437 2.193 0.521 5.296 0.826 0.495	0.590 1.769 1.769 0.858 0.815 0.610 0.630 0.702 0.583 1.178 0.583 0.674 0.583	0.654 1.9558 6.988 6.688 9.658 9.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
Connect Bap Connect Bap Connect Bab Connect Bbp Connect Bbp Connect Bbc Connect Bcp Connect Cp Connect Cp Connect Cc Conn			
Connect Connec	Connect Connec	Connect Connec	Connect Connect Connect Connect Connect Connect Connect Connect Connect Connect Connect SNB-H1 SNB-H1 SNB-H1 SNB-H1 SNB-H1 SNB-H1 SNB-H1 SNB-H1 SNB-H1

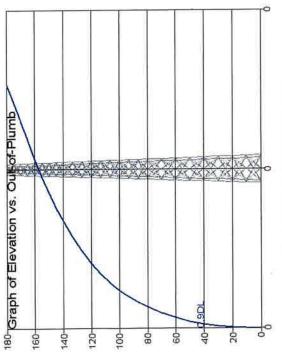
0.015 0.015 0.0124 0.01288 0.0388 0.0388	
0.025 0.026 0.026 0.175	ŀ
0.0549 0.0165 0.0267 0.0267 0.0267 0.0267 0.0268 0.0268 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.02688 0.026888 0.026888 0.026888 0.026888 0.026888 0.026888 0.026888 0.0268888 0.0268888 0.02688888 0.02688888 0.026888888 0.02688888888888888888888888888888888888	N
0.0530 0.0530 0.0530 0.0532 0.	1
0.000	1
0.5588 0.0588 0.0588 0.0588 0.0589 0.0589 0.0589 0.0588	)
0.299 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599 0.599	)
0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	
0.222 0.2220 0.2220 0.2220 0.1255 0.1255 0.1255 0.1375 1.389 1.316 1.	)    - 
00000000000000000000000000000000000000	1
SNB-H2GP SNB-H2GP SNB-H3GP SNB-H3GP SNB-H3GP SNB-H3GP SNB-H3GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H4GP SNB-H6GP SNB-M1-G2P	1
SNB-H1 SNB-H2 SN	11 days a week

0.000

0.000

-0.071 -0.071 0.142





Elevation (fl)

Out-of-Plumb per ANSI/T!A 222-G (in)

Twist and Out-of-Plumb for "1: 1.2D + 1.0Dg + 1.6Wo":

Out of Flumb (in)	0.00 0.03 0.03 0.03 0.63 0.63 1.18 1.18 1.20 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23
Sway (deg)	0.00 0.05 0.15 0.15 0.37 0.37 0.59 0.68 0.88 0.88 0.90 0.90 0.90 0.90 0.90
Twist (deg)	000000000000000000000000000000000000000
Elevation (ft)	0.00 22000 30.00 40.00 50.00 60.00 10.00 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.34 113.00 1150.00 1150.00

Twist and Out-of-Plumb for "2: 0.9D + 1.0Dg + 1.6Wo":

Out of Plumb (in)	0.00 0.00 0.06 0.03 0.03 1.18 1.18 1.18 1.19 1.19 1.19 1.19 1.19
Sway (deg)	0.00 0.00 0.01 0.01 0.03 0.03 0.03 0.05 0.05 0.05 0.05 0.05
Twist (deg)	00.000000000000000000000000000000000000
Elevation Twist (ft) (deg)	0.00 10.00 30.00 30.00 40.00 60.00 60.00 80.00 80.00 80.00 110.00 113.34 140.00 120.00

Twist and Out-of-Plumb for "4: 1.2D + 1.0Dg + 1.0E":

Out of Plumb (in)	0.00 0.000 0.000 0.000 0.117 0.117 0.017 0
Sway (deg)	0.00 0.00 0.01 0.01 0.01 0.03 0.04 0.05 0.05 0.05 0.05 0.05 0.05 0.05
Twist (deg)	
Elevation (ft)	0.00 20.00 30.00 50.00 60.00 60.00 100.00 113.36 113.66 11

Twist and Out-of-Plumb for "5: 0.9D + 1.0Dg + 1.0E";

Out of Plumb	(ai)	0.00	0	0.02	°.	٥.	0.12	۲.	ď	Э.	E,	4.	4	.5	9.	. 7	8	9	0.	0.	۲.	2	۳.	4	5	1.58	۰.
Sway (	(deg)	0.00	0	0.	0.	0.	0.	0	0.	0.	0.	0.	0.	0.	0.	0.	0	٥.	0.	٥.	0.	0.	9	0.	0.08	-	0.08
Twist	(deg)	0.00	0.	0.		-0.00				-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00
Elevation	(ft)	0.00	0.0	0.0	0.0	0	0.0	0.0	0.0	80.00	6.6	3,3	0.00	9.90	13.3	20.0	26.6	33,3	40.0	45.	50.0	55.0	0.09	65.0	170.00	75.0	180.00

Twist and Out-of-Plumb for "6: Service 1.0D + 1.0Dg + 1.0 Wo":

Out of Plumb	(in)	00.0	0.01	0.07	0.14	0.26	0.40	0.58	17.0	0		m			2.01	2.25	2.50	2.76	3.03	3.24	3.45	3.66		4.08	4.29	4.51	4.72
Sway	(deg)	0.00	0.01	0.03	0.04	0.06	0.07	0.08	0.09	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.19	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
Twist	(ded)	0.00	00 * 0-	0	0	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	0.	0.	0.	0.	٥.	°.	0.	0.00	0.	0.00	0.	0.00	0.00	0.00		0.00
Elevation	(ft)	0		0.0	30.00				70.00	0.0	9.9	3.3	00.00	9.90	13.3	20.02	26.6	33.3	40.0	45.0	50.0	155.00	0.09	65.0	70.0	75.0	180.00

Twist and Out-of-Plumb for "1.2\*DL";

Out of Plumb	(in)	00.00	0	0	0	0	0	0	0	0	0	0	0	0	٠.	٧.	~	٧.	٠.	~	٠.	۳.	٦.	٠.	0.02	0.02	0.02
5u	(ded)	0.	°.	-0.00	0.	0,	00.00	°.	0	O	O	$\circ$	$\circ$	$^{\circ}$	$\overline{}$	$\overline{}$	_	~	Υ.	۳.	٠.	Ξ.	Ξ.	-	0.00		0.00
Twist	(deb)	0.0	-0.0	-0.0	-0.0	-0.0	-0.0	0.0-	0.0	0.0	0.0	0.0	0 0	0	0	0	0	0	0	0,0	0.0	0	0	0	0.00	0	-0.00
ď	(ft)	00.00	0	0.	0.	0.	°.	٥.	0:	0.	9	E.	00.0	9.90	13.3	20.0	26.6	33.	10.0	15.0	50.0	55.	90.	65.1	0	5	

Twist and Out-of-Plumb for "0.9DL":

Out of Plumb	<u>E</u>	0	0	0	0	0	0	0	0	0	0	9	0	٥.	٥.	٥.	0.00	٥.	٠,	٠.	٠.	9	٧,	٧,	٧.	0.01	0.02
Sway	(deg)	0.0	0.0	-0.0	0.0	0.0-	0.0	-0.0	0.0	-0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0
Twist	(deg)	0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		-0.
ä	(ft)	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.6	3.3	0.00	9.90	13.3	20.0	26.6	33.3	40.0	45.0	50.0	55.0	60.0	65.0	70.0	175.00	80.0

Equilibrium Joint Positions and Rotations for Load Case "1: 1.2D  $\pm$  1.0Dg  $\pm$  1.6Mo":

\*\*\* Analysis Results for Load Case No. 1 "1: 1.2D + 1.0Dg + 1.6Wo" - Number of iterations in SAPS 13

os ft)	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
-Pos Z-P (ft) (f	113399999	888004400
-X	11.386 10.00	χ σ- 
X-Pos (ft)	1	9.4159 9.4159 9.4159 1.1.11824
Z-Rot (deg)	100000000000000000000000000000000000000	
Y-Rot (deg)	0.9062 0.9062 0.9042 0.9742 0.7904 0.7904 0.7904 0.7904 0.7906 0.7706 0.	
X-Rot (deg)		
Z-Displ (ft)	1 1 4 6 4 0 5 8 8 8 9 0 0 8 8 9 8 8 8 8 8 8 8 8 8 8 8	
Y-Displ (ft)	0.0008174 -0.0008174 -0.0002756 -0.0003763 -0.0006282 -0.0004123 -0.000423 -0.000423 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284 -0.0006284	1.488-000 1.00254-000254-0002524-000254-000252
X-Displ	1.76 1.131 0.02163 0.02163 0.02163 0.02792 0.02792 0.02792 0.02792 0.02792 0.02792 0.02792 0.02792 0.02792	7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Joint	RODIAP RO	SNB-JP SNB-JP SNB-JP Rohn42 Rohn42 Rohn62 Rohn61 Rohn62 Ro

1174.9 1169.9 1169.9 1173.1 1173.1 1173.2 1175.6 1175.6 1175.6 1175.6 1175.7 11	
0.0003848 0.2000318 0.2001032 0.00010332 0.0003322 0.0003322 0.0003322 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003221 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.0003222 0.00032 0.000322 0.000322 0.00032	
6.211 6.329 6.6847 7.329 7.329 7.329 7.367	
0.001111 0.001111 0.001111 0.001111 0.00125 0.0025 0.0025 0.00025 0.00025 0.00000 0.00	
0.9106 0.90268 0.90268 0.88955 0.88955 0.08263 0.09268 0.09	
000017 0000017 0000017 0000017 0000017 0000017 0000017 0000017	
0.09285 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
-0.0003818	
1.681 1.562 1.562 1.562 0.05335 0.05335 0.05335 0.05935 1.563 1.365 1.366 1.378 1.366 1	
RohnAdas RohnAdas RohnAdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas RohnBdas SNB-Adas SNB-Adas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Bdas SNB-Rdas SNB	

948 945 345 13 343 13 343 13 572 12 5.57 12 025 11 024 11 025 11		3355778888995588
		1.283 1.283 1.283 1.283 1.283 1.283 1.283 1.294 1.394 1.294 1.394
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	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	-0.00154 -0.0006172 -0.0006172 -0.000724 -0.00224 -0.00226 -0.00226 -0.00226 -0.00159 -0.00118 -0.00118 -0.00118 -0.00118	
1.208 1.208 1.032 1.032 0.934 0.934 0.7496	0.5629 0.5115 0.5117 0.5117 0.1283 0.1283 0.05375 0.05375 0.05375 0.05375 0.05375 0.05371	0.933 0.933 0.933 0.7486 0.7486 0.6627 0.6627 0.6511 0.4418 0.288 0.288 0.1494 0.05833
RohnBc1 RohnCa1 RohnCa1 RohnCa2 RohnCb1 RohnCb2 RohnDa2 RohnDa2	RohnDb2 RohnEa1 RohnEa1 RohnEb1 RohnEb1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa1 RohnEa2 SNB-Aa2 SNB-Aa2 SNB-AA2 SNB-AA2 SNB-AA2 SNB-AA2 SNB-AA2 SNB-AA2 SNB-AA2 SNB-BA	Control of the contro

Joint Support Reactions for Load Case "1: 1.2D + 1.0Dg + 1.6Wo":

Joint	X Force (kips)	X Usage %	Y Force Us (kips)	Y Usage	Z Force (kips)	Comp. Usage	Uplift Usage %	Result. Force (kips)	Result. Usage	X Moment (ft-k)	X-M. Usage	Y Moment (ft-k)	Y-M. Usage	Z Moment (ft-k)	Z-M. Usage	Max. Usage
пJР	-28.86	0.0	0.10		347.98					-0.05	0.0	-5.4		-0.01	0.0	0.0
-JP	-49.71	0.0	0.00	0.0	500.22	0.0	0.0	502.69	0.0	00.00	0.0	-13,1	0.0	0.00	0.0	0.0
InJ1	-9.19	0.0	-9.74		-144.29					1.86	0.0	-1.4		00.00	0.0	0.0
RohnJ2	-9.38	0.0	9,66		-144,59					-1.81	0.0	-1.5		-0.01	0.0	0.0
3-71	-16.94	0.0	-18.22		-222.16					5,30	0.0	-2.6		-0.04	0.0	0.0
3-12	-16.96	0.0	18.25		-222,63					-5.31	0.0	-2.6		0.04	0.0	0.0

| Columbia 1.6Wo" + 1.0Dg "1: 1.2D Joint Displacements, Loads and Member Forces on Joints for Load Case # Member # Postes | P \*\*Member N Forces (CAps) | CAps) | CAps | Ca × N External Load (kips) 3.0.6446 3.0.6289 0.0.6543 0.0.6543 0.0.9277 1.1001 1.4048 0.6543 0.6563 0.6663 × External Y Load (kips) Rohmap Rohmap Rohmap Rohmap Rohmap Rohmap Rohmap Rohmap Rohmap SNB-4P SN × Joint

URS Connecticut - 4-carir

-0.09993 -0.09997 -0.099997 -0.09997	
0.000000000000000000000000000000000000	'
1. 364 1. 285 1. 285 1. 285 0. 93311 0. 94312 0. 94311 1. 2864 0. 2934 1. 2862 1. 3660 1. 3	i.
0.2170 0.1580 0.2170 0.2577 0.4437 0.10863 0.18630 0.18630 0.2170 0.2170 0.2257	
-0.2646 -0.2646 -0.2005 -0.200	
0.1170 0.105977 0.105977 0.1059999 0.1059999 0.1059999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.1059999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.10599 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.1059999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.105999 0.10	
0.2646 0.2646 0.26466 0.26466 0.4104 0.517344 0.51734 0.51734 0.51734 0.51734 0.51734 0.51734 0.517	l E
Rohnbbs Rohnbb	

	7
000000000000000000000000000000000000000	0.0248 0.0247 0.0247 0.0230 0.0231 0.0188 0.0124 0.0044
	0,0003 1,0000 1,
	77 0.5110 77 0.5111 77 0.4118 79 0.2880 79 0.2880 72 0.1494 72 0.1494 73 0.0543 74 0.058
444400000000000000000000000000000000000	0.4437 0.4437 0.4437 0.5999 0.5999 0.6702 0.7135 0.7135 0.8390
-2. 3119 -2. 4592 -2. 4592 -2. 6273 -0. 4002 -0. 4104 -0. 4104 -0. 4104 -0. 5327 -0. 53	-0.4104 -0.4104 -0.4104 -0.5173 -0.5327 -0.5327 -0.5674 -0.5674 -0.8374
	-0.4437 -0.4437 -0.4437 -0.5999 -0.5999 -0.6702 -0.7135 -0.7135
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44440000000
RohnCa2 RohnCb2 RohnCb2 RohnDa1 RohnDa1 RohnDb3 RohnDb3 RohnCb2 RohnCb3 RohnCb3 RohnCb3 RohnCb3 RohnCb3 RohnCb3 RohnCa2 RohnCa3 RohnCa	SNB-Ea1 SNB-Ea2 SNB-Eb1 SNB-Eb2 SNB-Fa1 SNB-Fa2 SNB-Ga2 SNB-Ga2 SNB-Ha1 SNB-Ha2 SNB-Ha2 SNB-Ha2 SNB-Ha2

Moments for Angles Modeled as Beams:

Torsion (ft-lbs)	Origin X Moment (ft-lbs)	Origin Y Moment (ft-1bs)	Origin End Y Moment X Moment (ft-1bs) (ft-1bs)	End Y Moment (ft-1bs)	X Shear (1bs)	Y Shear (1bs)
0.01		4.68	26.06		5.42	-2.62
2.04	-1.59	2.69	11.25	38.00	1.93	8.13
-2.16		2.88	6.55		1.55	-2.78
0.01					-11.76	8.74
2.04	-11.25	-38.00		-88.05	-9.27	-25.19
-2.16					-1,08	4.14
0.01					13.69	-7.82
2.04					15.15	38.69
-2.16					-5.07	9.39
0.01					-10.89	7.59
2.04		,			-20.49	-44.68

-25.76 -3.29 -3.29 -3.29 -11.78 -11.78 -11.38 -11.38 -11.38 -11.38 -1.138 -2.3.18 -2.3	2237 2237 2258 000
14.06 3.5136 43.04 43.104 43.104 43.104 43.104 43.106	000000000000000000000000000000000000000
-78.04 -78.04 -2.36 -2.36 -2.10.95 -2.10.45 -2.10.45 -2.10.45 -2.10.45 -2.10.45 -2.10.45 -1.0.39 -1.0.	383. 363. 363. 457. -1.0
46.17 10.94 110.94 141.26 141.26 141.26 141.26 141.26 14.08 17.72 19.86 19.632 19.86 19.632 19.86 19.632 19.86 19.632 19.86 19.632 19.86 19.632 19.86 19.632 19.86 19.	0.000
-50.89 -14.09 124.09 133.82 -2.36 -2.26 -2.36 -2.36 -2.26 -3.36 -3.36 -3.36 -3.36 -1.65 -1.65 -1.65 -1.65 -1.17 -1.09	652 1189 717 717 10 1
	16402049
2.16 3.16	
Rohn-LM2 Rohn-LB1P Rohn-LB1P Rohn-LB1P Rohn-LB2P Rohn-LB3P Rohn-LB3P Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB41 Rohn-LB12 Rohn-LB13	ohn-LI ohn-LI ohn-LI Sohn-H Rohn-H Rohn-H Rohn-H

11.27 11.27 11.27 11.27 11.27 11.27 12.35 12.35 12.36 12.37 12.36 12.37 13.36 13.37	0.00000
1.4.5 1.1.4.5 1.1.6.68 1.1.6.68 1.1.6.68 1.1.6.6.09 1.1.6.10 1.0.6.10	30 91 30
-1.11 -9.89 -9.89 -9.89 -9.89 -9.89 -143.28 -143.28 -17.766 -1	1565. -224. 6398. 7035.
-6.16 14.54 14.54 16.85 16.85 16.85 16.85 16.85 10.43 10.43 10.43 10.43 10.43 10.43 10.43 10.43 10.43 10.95 10	166 3 198 194 -1
0.49 -0.65.28 -23.3.2 -35.3.2 -35.3.2 -35.3.2 -36.80 -36.80 -36.80 -37.28 -37.28 -10.02 -37.28 -10.02 -10.03 -10.0	799 942 814 817 224 398
-6.69 -6.69 -71.19 -71.19 -71.19 -71.19 -71.6.20 -76.85	691 725 724 -3
0.03 0.03	-60.89 0.08 60.29 -60.51 0.08
Rohn-H22 SNB-LA1P SNB-LA1P SNB-LA1P SNB-LA12 SNB-LA2P SNB-LA2P SNB-LA3P SNB-LB1D SNB-LB1D SNB-LB2P SNB-LB2P SNB-LB3P SNB-LB3P SNB-LB3P SNB-LB3P SNB-LD1D SNB-LE2D SNB	18-17 18-17 18-17 18-17 18-17 18-17

\*\*\* Analysis Results for Load Case No. 2 "2: 0.9D + 1.0Dg + 1.6Mo" - Number of iterations in SAPS 13

Equilibrium Joint Positions and Rotations for Load Case "2: 0.9D + 1.0Dg + 1.6Mo":

m - 1		00		-	\1 =	r \C	o co	0	O	6	on o	0 4	7	D.	9	<b></b>		0	0	0.	0	0 0	0.0	00	0	3	33	E 6	200	200	)1	01	0	0 9	000	20	50	10	40	20	01	000	02	03	02	02	7 0	01	01	0	>
Z-Pos (ft)	79.	159.9	19.	9.9	ა. ა. ი		, 0		79.	59	139.	6	0	9	5	6	-		-			-	٦,		-	80.	80.	90	90.	40.	20.	20.					-				, .		80	80	09	9	7	20	20		41
Y-Pos (ft)	-0.00085	1.944e-00	-0.00040	-0.000545	-0.000702	-0.000415	-0.000205		-0.00172	-0.0013	-0.000944	-0.000404	-0.000248	-0.000136	5.785e-00	-1.49e-00	, I	ז	<b>b</b> -	4	- 5	יטי	7	1		511#11	. 11	ī		1	, 01		'		1	1		1		1	Ĭ		Ĩ,					ì		-8.154	
X-Pos (ft)	2	6.562 -		-	~ •												- 1				1			- 1	1	- 1		1		, ,				,			~	~	_												
Z-Rot (deg)	0.0112	0.0110	0.0048	0.0032	0.0021	0.0009	0.0003	0.000.0	-0.000.0	-0.0000	0.0000	0.000	0 0000	0.0000	000000	0,0000	0.0000	0.0178	0.000	0.0222	6800 0-	0:0234	-0.0132	-0.0130	0.0195	-0.0128	0.0170	-0.0097	0.0071	00000	-0.0040	0.0046	000000	0,0000	0.0018	-0.0021	0.0023	-0.0029	0.0030	0500.0-	-0.0030	0.0040	-0.0038	0.0038	-0.0047	0.0046	-0.0045	-0.0042	0.0042	00000	>>>>>
Y-Rot (deg)	9042	9022	7889	6499	5153	2682	1220	0000	9006	.8964	8635	6358	5159	,3745	0.2606	0.1192	00000	0.9059	0,9086	0,9067	0.8635	0.8601	0.7846	6490	0.6466	0.5371	0.5361	0.3975	0.3977	0.2751	0.1346	0.1354	0.0000	0.0000	0.9100	0.9037	0.9039	0,8716	0.8716	0.7921	0.6441	0.6440	0.5398	0.5397	0.4010	0.4010	12/21	0.1399	0.1399	0.0000	00000
X-Rot (deg)	0.0063	0.0011	0.0002	0.0005	0.0003	0.0000	0.0006	0.0000	0.0020	0.0009	0.0010	0.000	0.0004	0.0003	0.0002	-			_	7	ĭ	0.0	ī	0 0	0	0	9	0	ř	2	, 0	Ÿ			ī	, _	_	ĭ	_	ĭ	7	_	_	ī	_	ī	1		- 1	0.0000	
Z-Displ (ft)	-0.08	-0.0942	-0.09815	~0.08804	-0.0764		-0.02		-0.05	-0.06	-0.06		-0.0	-0.0-	-0.0	-0.0	0		0.0	0.0	0	0.0	0 6	000	0.0	0.0	0.0	0	0.0	0.0	0.00	00.00		0		0.0	0	0	0.0	0			0.0	0 0	0	0 0	0 0	0.00	0.0		
Y-Displ (ft)	0.000856	-4.944e-005	0.000404	0.000545	0.000702	0.000031	0.00020		-0.00172	-0.0013	-0.00094	-0.00063	-0.000248	-0.00013	-5.785e-0	-1.49e-0		-0.0020	-0.0020	-0.0019	-0.00096	-0.0015	-0.00022	-0.0013	-0.00048	0.00051	-0.00043	0.0003	-1./51e-U	-0.00041	0.00018	-2.775e-0		0	-0.001/	-0.0013	-0.0013	-0.00093	-0.0009	-0.00054	1,000.01	-0.0004	-0.00015	-0.00034	9.501e-(	-0.00028	0.0001	0.0002	-0.0002		
X-Displ (ft)	1.757	1.441 -		0.5836	٠٠,	50	0.02794				Ξ,	u.			ö	.0		1 757			1.13		٠,	0.83/4					5	0.09842	. 0	0.	0	0 0	1.738	1.441	1.441	1.13		0.8384		, _	0	0		_ <	5 0	0	0	0	
Joint Label	huho	RohnBP	RohnDP	RohnEP	ohn	Rohner	RohnTP	RohnJP	SNB-AP	SNB-BP	SNB-CP	SNB-DE	SNB-FP	H	$\equiv$	SNB-IP	SNB-UF	Rohna2	RohnBl	RohnB2	RohnC1	RohnC2	RohnD1	RohnE1	RohnE2	RohnFl	RohnF2	RohnGl	RohnG2	ROUNTI PohoH2	RohnI1	Rohn I 2	RohnJl	RohnJ2	SNB-AI	SNB-B1	SNB-B2	SNB-C1	SNB-C2	SNB-DI	SNB-E1	SNB-ES	SNB-F1	SNB-F2	SNB-G1	SNB-G2	TH-HNS	SNB-11	SNB-12	SNB-J1	DIVID OF
	į																																																		

E V	
1175 - 17	170 165 165 155 150 150
-0.00042 -0.0003 -0	4 - 4 - 26 0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
6.228 6.325 6.325 6.325 6.325 6.325 6.326 6.318 8.425 8.952	I I was a
0,001111 0,011111 0,011111 0,011111 0,0011111 0,0011111 0,0011111111	0000000
0.9084 0.9069 0.9069 0.90743 0.8478 0.8478 0.7478	0000000
	-0.001 0.002 -0.000 0.006 0.002
9999991799797979797979799999	
0.461	
1.598 1.598 1.283 1.283 1.206 1.206 1.206 1.206 1.206 1.206 1.206 1.529 1.529 1.529 1.529 1.529 1.529 1.529 1.529 1.529 1.539 1.	
RohnAas RohnBas RohnBas RohnBas RohnBas RohnBas RohnCas SNB-Aas SNB-Aas SNB-Aas SNB-Aas SNB-Aas SNB-Aas SNB-Bas SNB-Bas SNB-Bas SNB-Bas SNB-Bas SNB-Bas SNB-Cas SNB-Ca	RohnAb2 RohnAc1 RohnBa1 RohnBa2 RohnBa2 RohnBb1

-4.948 145	4,945 145	-5.345 133.4	5.343 133.4	-5.572 126.7	5.57 126.7	-6.025 113.4	6.024 113.4	-6.251 106.7	6.25 106.7	-6.705 93.37	6.705 93.37	-6.933 86.69	6.932 86.69	-7.498 70.03	7.499 70.03	-8.18 50.02	8.18 50.02	-8.861 30.01	8.861 30.01	-9.546 10											3.042 150				3.6I	3000	200	7.22.		.518	.973	.973	.201	5.2		.766	.448	.448	. 129	.129	7.81 10	
-1.649	-1,651	-2.055	-2.056	-2.284	-2.285	-2.73	-2.73	-2.948	-2.948	-3.362	-3.361	-3.562	-3.562	-4.043	-4.042	-4.575	-4.574	-5.064	-5.064	-5.506	-5.506	0.4134	0.4135	0.2359	0.2358	0.05806	0.05812	-0.2963	-0.2963	-0.4731	-0.4731	-0.6494	-0.6494	-1.056	-1.056	-1.285	C87.1-	1.731	-1.948	-1,948	-2.361	-2.361	-2.562	-2.562	-3.043	-3.043	-3.575	-3.575	-4.063	-4.063	5 -4.505	
0.0079	0.0243	0.0108	0.0237	0.0128	0.0241	0,0141	0,0226	0.0136	0,0211	0.0133	0,0190	0.0123	0.0172	0.0106	0.0142	0.0083	0.0107	0.0054	0.0065	-0,002€	0.0029	-0,0020	0.0022	-0,0022	0.0023	-0.0021	0,0023	-0,0026	0,0028	-0.0029	0,0030	-0,003	0,003	-0,004	0.004	-0.004	0.004	0000	-0.004	0.004	-0.004	0.004	-0.003	0.003	-0:003	0.003	-0.004	0,004	-0.004	0.004	0.002	Craolity
0.9020	0.8979	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O	0	0	0	0	0	_	_	_	_		_	_	_																6 0 0823	
0	-0.0050	0.0015	0.0023	0.0070	-0.0040	0.0068	-0,0037	0.0009	0.0017					0.0	Ö	Ö	0	0	0	0	Ö	o'	0.0001	0	0	0	0	0	-0.0004	0	0	0.000	0	0	0	0 0	0 0	5 0	0	0	0	0	0	0	0	0	0	0	0	0	0.0000	6
0.0295	0.0297	0.0325	0.0327	0	0.0340	0.0349	0.0350	0.0346	0.0347	0.03305	0.03316	0.0321	0.0322	0,02861	0.02868	0.02257	0.02261	0.01445	0.01448	0.004905	0.004916	0.006401	0.006486	0.008556	0.008655	0.01067	0.01077	0.01474	0.01485	0.01667	0.01678	0.01847	0.01859	0.0221	0.02221	0.02371	0.02382	0.02362	0.02572	0.02581	0.02554	0.02562	0.02542	0.02549	0.02357	0.02363	0.0191	0.01922	0.0126	0.0126	0.00445	
-0.001153	-0.001735	-0.001164	-0.0009826	-0.0006493	-0.001173	-0.0004198	-0.0007927	0.0006696	-0.0016	0.0006182	-0.001034	0,0007201	-0.0008992	0.002603	-0.002418	0.00262	-0.002337	0.002953	-0.002752	0.002096	-0.002012	-0.001625	-0.001653	-0.001504	-0.001517	-0.001354	-0.001514	-0.001122	-0,001335	-0.001027	-0.001235	-0.0008482	-0.001228	-0.0002982	-0,00138	-0.0001264	-0.001341	0.0001697	0.0007747	-0.001718	0.0002847	-0.0009757	0.0004192	-0.001001	0.002671	-0.003032	0.002439	-0.002619	0.002637	-0.002702	-0.002362	F 1 2 2
1 207	1 205	1.031	1.03	0.9323	0,9317	0.7483	0.7482	0.6618	0.6618	0.5097	0.5102	0.4406	0.4413	0.2877	0.2887	0.149	0.1498	0.05373	0.0542	0.006317	0.00648	1.678	1.679	1.599	1.599	1.52	1.52	1.363	1,363	1.284	1.284	1.206	1.206	1.029	1.029	0.9314	0.9314	0.74/3	0.6616	0.6616	0.5102	0.5102	0.4411	0.4411	0.2876	0.2876	0.1493	0.1493	0.05428	0.05428	. uu 005	ŕ
PohnBcl	RohnBC2	RohnCal	RohnCa2	RohnCb1	RohnCb2	RohnDal	RohnDa2	RohnDbl	RohnDb2	RohnEal	RohnEa2	RohnEb1																	SNB-Ba2			301	Bc2	-Cal	-Ca2	-G	-Cb2	Dal	A-Dhi	-Db2	-Eal	B-Ea2	-Ep]	<b>b</b> 2	-Fal	-Fa2	$\vdash$	-Ga2	-Hal	-Ha2	SNB-1al SNB-1a2	

Joint Support Reactions for Load Case "2: 0.9D + 1.0Dg + 1.6Wo":

	×	×	¥	X	2	Comp.		_		×	X-M.	Ħ	Y-M.	12	Z-M.	Max.
Force	ce Usage	ge ]	Force	Usage	Force	Usage	Usage	Force	Usage Mc	ment	Usage	Moment	Usage 1	Moment	Usage	Usage
(kip			kips)	dР	(kips)					(t-k)	96	(ft-k)	o)(0	(£t-k)	dφ	dΨ
		:	0.10	0.0	:			i ' '		'			0.0	1		
-49.56		0.0	0.00	0 .0	495:02	0.0	0.0	497.50	0.0	00.0	0.0	-13.0	0.0	00.0	0.0	0.0
			-9.96	0.0									0.0			
RohnJ2 -9.			9.88	0.0									0.0			
		-20	18.33	0.0									0.0	,		
			18.36	0.0									0.0			

Joint X Label	r External Y Load (kips)	(External Z Load (kips)	External Load (kips)	X Member Force (kips)	Y Member Force (kips)	Z Member Force (kips)	X Disp. (ft)	Y Disp. (ft)	Disp. (ft)
tohnAP	0.6446	0.0000	-0.2657	-0.6446	-0.0000	0.2657	1-7569 -(	- 60000 0-	-0.0856
tohnCP	0.6543		-0.3841	-0.6543	0	0.3841	1,1288	-0.0003	, φ
RohnDP	0.7898	0.	-0.4656	-0.7898	0	0.4656	0.8377	-0.0004	-
OhnEP	0.810		-0.7827	-0.8106 -0.9277	7 9	0.7827	0.3774	-0.0003	
ohnGP	1.2867	0.	-1.0426	-1.2867	9	1.0426	0.2160	-0.0006	$\sim$
RohnHP	1.1001	0.0	-1.0378	-1.1001	9	1.0378	0.0991	-0.0004	
Ohn IP	1.4048 0.8374		-I.1643 -N 6292	27 7526	7 7	-341 9525	0.0279	0.000	
NR-AP	0.1882	ò	-0.1397	-0.1882		יי ר	1.7572	~0.0017	~ ~
NB-BP	0.4529	0	-0.3025	-0.4529	0	0.3025	1.4409	-0.0013	$\sim$
NB-CP	0.6543	0	-0.3841	-0.6543	0	0.3841	1.1291	-0.0009	~ .
NB-DP	0.7898	0.0	-0.4656	-0.7898	00	0.4656	0.83/9	-0.0006	7 7
NB-EF	0.8106		7827	-0.8100	<i>,</i> C	0.7827	0.3775	-0.000	~ ~
NB-GP	1.0500	0	-0.9526	-1,0500		0.9526	0.2161	-0.0001	Ÿ
NB-HP	1,1001	0	-1.0378	-1.1001	0	1.0378	0,0991	-0.0001	Ť
SNB-IP	1.4048	0 0	-1.1643	-1.4048		1.1643	0.0279	00000	7 ~
SNB-UF BOhnal	0.83/4	<b>&gt;</b> C	-0.6592	48.723	1	ם, צי	1 7585	-0.0022	
RohnA2	1.1009	. 0	-0.3917	-1.1009	Υ Υ	0.3917	1.7571	-0.0021	_
RohnB1	1.0538	0	-0.4051	-1.0538	Ĩ	0.4051	1.4427	-0.0020	_
ohnB2	0.7194	0 0	-0.3466	-0.7194	Y	0.3466	1.4404	-0.0020	
tohnC1	0.6543	<b>&gt;</b> C	-0.3841	-0.6543	1	0.3841	1,1290	0.0016	
Rohn D1	1.0017	<i>&gt;</i> C	-0.5286	-1.0017		0.5286	0.8379	-0.0002	_
RohnD2	0.7898		-0.4656	-0.7898	ĭ	0.4656	0.8374	-0,0013	_
tohnE1	0.8106	0 0	-0.5771	-0.8106		0.5771	0.5838	-0,0002	
RohnE2	0.8106 7779		-0.5//1	-0.810e	īī	0.587	0.3766	0.000.0	
Sohn F2	1.3907		-0.9132	-1.3907	Ť	0.9132	0,3776	-0.0004	
lohngl	1.1820		-1.0066	-1.1820		1.0066	0.2154	0.0004	
RohnG2	1.6035	000	-1.0930	-I.6035	ĭ	1.0930	0.2165	0000	
Sohn H2	1.1001		-1.0378	-1,1001	1	1.0378	0.0991	-0.0002	
RohnIl	1.4048	0	-1.1643	-1,4048	Ī	1.1643	0.0276	0.0002	
3ohnI2	1,4048	0.0	-1,1643	-1.4048	0	-	0.0280	0000 0-	
RohnJl	0.8374		-0.6292	8.4889 8.6753	20	14	0000	0000	
SNB-A1	0.1882	0	-0.1397	-0.1882	0	-	1.7576	-0,0017	
SNB-A2	0,1882	0.000	-0.1397	-0.1882	0		1,7576	-0,0017	
SNB-B1	0.4529	0	-0.3025	-0.4529	9		1,4415	-0.0013	
SNB-BZ	0,4329	jc	-0.3023	-0.4329	9 0		1 1297	0000	
SNB-C2	0.6543		-0,3841	-0.6543	0		1,1297	-0.0010	
SNB-D1	0.7898	0	-0.4656	-0.7898	0-		0,8384	-0,0005	
SNB-D2	0.7898	0	-0.4656	-0.7898	0		0.8384	-0.0007	
SNB-E1	0.8106	o c	-0.5771	-0.8106	0 0		0.5840	-0.0003	
1 1	0.9277	ò	-0.7827	-0.8100	0		0.3777	-0.0002	
댇	0.9277	0	-0.7827	-0.9277	0		0.3777	-0.0003	
9	1.0500	0	-0.9526	-1.0500	0		0.2160	0.000	
9	1.0500	0	-0.9526	-1.0500	0		0.2160	-0.0003	
SNB-H1	1,1001	00	-1.03/8	-1.1001	7		0.0989	1000.00	
1 1	1 4048	o c	-1.1643	-1.404B			0.0275	0.0002	
SNB-T2	1.4048	0	-1.1643	-1.404B	0		0.0275	-0.0000	
SNB-J1	0.8374		-0.6292	16,1746		22	0.000	0.0000	
SNB-J2	0.8374	0	-0.6292	16.1929	-18	22	0.0000	0.0000	
RonnAas	0.6035	0	-0.1868	-0.6035	>		8/19	-0.0004	ı
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-2,3119	-24592	-2.6273	-2.6273	-0,4002	-0.4002	-0,4104	-0,4104	-0.4104	-0.4104	-0.5173	-0.5173	-0,5327	-0.5327	-0.5674		-0.8374	0 0	5 0		00	-0.1882	-0,1882		264	10	-0.2646	-0.2646	389	.389	e,	-0.3896	2, 0	4	-0.4002	-0.4104	-0.4104	-0.4104	-0+4104	0.5173	-0.5327	-0.5327	-0.5674	567
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Torsion (ft-lbs)	Torsion Origin X Moment (ft-lbs) (ft-lbs)	Origin Y Moment (ft-1bs)	End X Moment (ft-lbs)	End Y Moment (ft-1bs)	X Shear (1bs)	Y Shear (1bs)
0.0		4.70	26.18	-16.78	5.44	-2.41
2.0		2.67	12.14	37.60	2.12	8.05
-2.1				-17.25	1.38	-2.88
0.0				24.59	-11.79	8.27
2.04	4 -12.15	-37,59	-36.29	-87.35	-9.68	-24.97
-2.1				4.59	-0.68	4.36
0.0				-11.36	13.69	-7.18
2.0				104.60	15.69	38.36
-2.1				50.01	-5.61	9.08
0.0				22.27	-10.88	6.72
2.0				-116.68	-21.17	-44.22

0886700884008740	-120.79 -130.852 -130.852 -130.852 -130.852 -130.852 -124.86 -125.886 -125.887 -126.888	420. 721. 721. 886.
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100184010101000	-2.33 -40.47 1980.98 1980.98 1980.36 56.96 56.96 56.96 57.70 336.35 180.33 336.35 180.33 336.35 180.33 336.35 180.33 175.10 175.10 183.36 183.	6339. 6337. 6729.
2.5.13.5.2.13.5.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.13.5.5.5.13.5.5.13.5.5.13.5.5.13.5.5.5.13.5.5.5.13.5.5.5.13.5.5.5.5	-39.54 -39.54 -31.74 -21.74 -23.60 -39.08 -39.08 -39.08 -9.19.08 -9.19.08 -9.19.08 -9.19.08 -9.10.08 -	271.2 266.3 -1.9
0.4 442.5 113.2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-101.68 -12.93 -1.94.04 -1.94.04 -1.95.04 -1.99.08 -1.90.38	4072. 881.0 883. 130.2 6339.9
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-48.42 -48.42 -41.68 -5.168 -41.15 -5.9.52 -5.9.52 -6.10 -1.09	595 594.6 -4.1
100000000000000000000000000000000000000	3.22 -0.06 -0.06 -0.07 -0.08 -0.09 -0.	0000
n-H2 -LA1 -LA1 -LA2 -LA2 -LA3 -LA3 -LA4 -LA4	SNB-LB21 SNB-LB22 SNB-LB32 SNB-LB32 SNB-LB32 SNB-LB42 SNB-LB42 SNB-LB41 SNB-LB41 SNB-LB41 SNB-LC21 SNB-LC21 SNB-LC22 SNB-LC22 SNB-LC22 SNB-LC32 SNB-LC32 SNB-LC32 SNB-LC32 SNB-LC32 SNB-LC32 SNB-LC32 SNB-LD32 SNB-LB22 SNB-LB22 SNB-LB23 SNB-LB23 SNB-LE23 SNB-LE23 SNB-LE23 SNB-LE23 SNB-LE33 SNB	8-1H) 8-1H) 8-1H) 8-1H)

\*\*\* Analysis Results for Load Case No. 3 "4: 1.2D + 1.0Dg + 1.0E" - Number of iterations in SAPS 12 Equilibrium Joint Positions and Rotations for Load Case "4: 1.2D + 1.0Dg + 1.0E":

Z-Pos (ft)	180 180 180 180 180 180 180 180
Y-Pos (ft)	9.999e-005 9.00011227 9.869e-005 1.7468e-005 1.7468e-005 1.7468e-005 1.753e-006 9.0001350 9.0001350 9.0001350 9.0001350 9.182e-005 1.716e-
X-Pos (ft)	5.233 5.233 5.233 7.5222 7.52222 7.5222 7.5222 7.5222 7.5222 7.5222 7.5222 7.5222 7.
Z-Rot (deg)	00000000000000000000000000000000000000
Y-Rot (deg)	0.0731 0.0631 0.0631 0.0632 0.0635 0.0635 0.0636 0.
X-Rot (deg)	0.000000000000000000000000000000000000
Z-Displ (ft)	0.01534 0.01536 0.01536 0.01036 0.002609 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986 0.0009986
Y-Displ (ft)	9.9999-005 9.0001227 9.869-005 9.869-005 1.7468-005 1.7176-005 9.0001365 9.0001365 9.0001365 9.00011366
X-Displ (ft)	0.11395 0.08464 0.01112 0.002392 0.001312 0.01312 0.013135 0.025913 0.025913 0.025913 0.025913 0.025913 0.01395
Joint	Rohnapp Rohnapp Rohnapp Rohnapp Rohnapp Rohnapp SinB-n
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Joint Support Reactions for Load Case "4: 1.2D + 1.0Dg + 1.0E":

Joint X Label Force (kips)	X Se Usaç 3)	X Y Usage Force U %(kips)	Y Z Usage Force %(kips)		Comp. Usage	Uplift Usage %	Result. Force (kips)	Result. Usage	Momen (ft-k	x-m. Usage	X X-M. Y ) t Usage Moment Us ) % (ft-k)	Y-M. Usage	Y-M. Z Usage Moment % (ft-k)	Z-M. Usage	Max. Usage
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				8.90					,						0.0
				B 99											0.0
				2.94									,		0.0
SNB-J2 -0.4				3.04											0.0

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1,0777 1,6028 1,9028 1,3931 0,3257 0,4437 0,4437 0,4437 0,4437 0,4437 0,6437	0.6702 0.7135 0.7135 0.8390 0.8390 0.1863 0.1863 0.1863 0.1863 0.1863 0.1863 0.2170	888888888888888888
-0.0817 -0.0817 -0.1065 -0.1065 -0.0764 -0.0166 -0.0200 -0.0200 -0.0186 -0.0200 -0.0200	-0.0153 -0.0164 -0.0164 -0.0169 -0.0059 -0.0450 -0.0390 -0.0397 -0.0397 -0.0292	-0.0252 -0.0219 -0.0214 -0.0224 -0.0196 -0.0179 -0.0179 -0.0179 -0.0179 -0.0186 -0.0186 -0.0186 -0.0186 -0.0186 -0.0186 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187 -0.0187
-1.0777 -1.6028 -1.3931 -1.3931 -0.3257 -0.4437 -0.4437 -0.4437 -0.5999	-0.6702 -0.6702 -0.7135 -0.7135 -0.8390 -0.1863 -0.1863 -0.1863 -0.1863 -0.1863 -0.1863 -0.1863	-0.2170 -0.2170 -0.2951 -0.2951 -0.2951 -0.2951 -0.3257 -0.3257 -0.4437 -0.4437 -0.5999 -0.5999 -0.5999 -0.5999 -0.5999 -0.5999 -0.5999 -0.6702 -0.6702 -0.63396 -0.8390
000000000000000000000000000000000000000		
0.0817 0.1065 0.1065 0.0764 0.0764 0.0166 0.0200 0.0200 0.0200 0.0200 0.0200	0.0153 0.0154 0.0104 0.0059 0.0059 0.0450 0.0450 0.0330 0.0337 0.0337 0.0337	0.0252 0.0219 0.0224 0.0224 0.0126 0.0136 0.0179 0.0179 0.0166 0.0166 0.0200 0.0200 0.0200 0.0200 0.0153 0.0153
RohnCa2 RohnCb1 RohnCb2 RohnDa2 RohnDa2 RohnCa1 RohnCa2 RohnCa2 RohnCa2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb2 RohnCb3 RohnCb	RohnGal RohnBal RohnHal RohnLal RohnLal RohnLal SNB-Aal SNB-Abl SNB-Abl SNB-Abl SNB-Abl SNB-Abl SNB-Acl SNB-Acl SNB-Acl SNB-Acl SNB-Bal	SNB-Bb2 SNB-Ca1 SNB-Ca2 SNB-Ca2 SNB-Ca2 SNB-Cb3 SNB-Da1 SNB-Db2 SNB-Db2 SNB-Ea1 SNB-Ea2 SNB-Ea2 SNB-Ea2 SNB-Fa1 SNB-Fa1 SNB-Fa2 SNB-Fa

Moments for Angles Modeled as Beams:

Angle	Angle Torsion Label (ft-1bs)	Origin X Moment (ft-1bs)	Origin Y Moment (ft-1bs)	Enc X Momen (ft-1bs)	f End F Y Moment SI (ft-lbs) (	X Shear (1bs)	Y Shear (1bs)
Nohn-LAIP	-0.19					00.0	-0.68
hn-LAll						-0.74	0.36
hn-LA12						0.74	0.24
Rohn-LA2P	-0.19	0.08	4.17	-0.64	6.74	-0,11	2.18
Rohn-LA21						1.25	-1.14
hn-LA22						-1.45	-0.48
hn-LA3P						0.33	-2.57
hn-LA31						-1.22	2.69
hn-LA32						1.51	1,8
hn-LA4P						-0.30	3.78
Sohn-TA41						1.22	-3.78

-3. 13 -6. 55 -6. 55	-, -, -,
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-8.23 -9.07	
1.55 1.55	
1.1. 56 1.1. 56 1.1. 56 1.1. 56 1.1. 56 1.2. 134 1.2. 134 1.3. 133 1.3. 133 1	
-3.63 -3.63 -3.63 -0.49 -0.49 -0.49 -0.10	000
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Rohn-Lid12 Rohn-Lid11 Rohn-Lid11 Rohn-Lid12 Rohn-Lid21 Rohn-Lid21 Rohn-Lid32 Rohn-Lid33 Rohn-Lid34 Rohn-Lid34 Rohn-Lid34 Rohn-Lid34 Rohn-Lid21 Rohn-Lid22 Rohn-Lid22 Rohn-Lid23	<b>并并</b>

10.03 18.63 18.63 19.84 19.86 10.03 10	224 229 229 322 111 111 322 333 331
25.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.	-52.49 -0.17 75.44 -75.44 0.19 96.89 -96.91 -0.19 65.58 -65.56 0.20
0.06 13.32 -6.97 -7.84 -4.08 18.32 17.84 -4.08 18.22 17.83 17.83 17.83 -1.05 -	MUNDONO HONDE
-0.72 0.35 12.12 -0.62 -2.21 13.16 -0.12 -0.12 -0.13 -0.12 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.13 -0.04 -0.05 -0.	-464.87 -1.42 -65.22 -65.31 0.44 903.42 -904.56 -91.46 -63.68.76 68.76
76.46 -35.28 -36.28 -36.28 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.32 -13.33 -13.83 -14.83 -16.84 -16.84 -16.84 -16.84 -16.84 -16.84 -17.83 -17	30 30 30 30 30 30
-0.85 -0.08 -0.08 -0.08 -0.08 -0.35 -0.35 -0.35 -0.42 -0.42 -0.13 -0.09	-60.41 -0.27 821.20 -920.32 1.42 66.22 -65.31 -05.31 -724.88 -724.88
0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.	-2.75 -4.42 -4.45 -4.45 -4.45 -4.16 -4.16 -4.16 -4.16
Rohn-H22 SNB-LA1P SNB-LA11 SNB-LA12 SNB-LA2P SNB-LA2P SNB-LA32 SNB-LA33 SNB	B-16 B-16 B-16 B-16 B-16 B-17 B-17 B-17 B-17 B-17 B-17

\*\*\* Analysis Results for Load Case No. 4 "5: 0.9D + 1.0Dg + 1.0E" - Number of iterations in SAPS 12 Equilibrium Joint Positions and Rotations for Load Case "5: 0.9D + 1.0Dg + 1.0E":

(ft) (ft)	8e-005	475e-005 1	008e-005	915e-005	136e-005 95	851e-005 /9	294e-006 55	012e-007	446e-006		0001254	* 000 T C C C C C C C C C C C C C C C C C	JOOTIZB	. UUUTUZZ	/84e-005	877e-005 9	05 7	.36e-005		721e-006	0	752	753	435	435	1117	5.117	798	5.798	670	671	7.16									,	П	-					7 .		_	-3.428 80 5 428 80							
X-Pos (ft)	4.472	5.232 8	5.993	6.756 6	7.522 5	8.294 2	9.069	9.847 -4	10.63 -3	11 42	0770	2/6/2	3.232	3.992	4.756 8	5.522 6	6.294 4	7.069		8.63		- 1			- 1			- 1	,				,	, ,	-4.914	-4-914	-5.313	-5,313	-5.71	-5.71	-1.028	-1.028	-1.449	-1,449	-1.87	-1.87	-2.287	-2.287	1.7-	1.2.	J 4	-3,513	-3.513	-3.914	-3.91	-4,31	-4.31	75-1-
Z-Rot (deg)	-0.0008	-0.0004	-0.0003	-0.0002	-0.0001	-0.0001	-0.0001	-0.0000	-0.0000	0000	0000	0000.0-	-0.0000	-0.0000	-0.0000-	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	-0.0012	-0.0004	-0.0012	0.0004	-0.0015	0,0010	-0.0015	0.0011	-0.0012	0.0010	-0.0011	0.0009	2000.01	-0 0005	0.0005	-0.0003	0.0002	000000	0.000	-0.0001	0.0001	-0*0001	0.0001	-0:0005	0.0002	-0.0003	0.0003	-0.0003	0.0003	-0.000	-0.0003	0.0003	5 -0.0003	0.0003	3 -0.0002	3 0.0002	0000
Y-Rot (deg)	0.0793	0.0783	0.0727	0:0620	0.0484	0.0359	0.0270	0.0178	0.0069		0.00	0.0743	0.0746	6890 0	0,0560	0.0440	0.0318	0.0191	0,0115	0,0026	000000	0.0796	0.0800	0.0792	0.0793	0.0725	0.0725	0.0624	0.0625	0.0485	0.0485	0.0392	0.0392	0.0278	0.0273	0.0185	3 0.0090	0.0090	0000.00	0 0 0 0 00	4 0.0823	3 0.0823	8 0.0802	7 0.0802	1 0.0747	0 0.0747	1 0.0656	0 0.0656	1 0.0498	0.0.0498	3 0 0417	9 0.0314	8 0.0314	6 0.0215	5 0.0215	2 0.0113	2 0.0113	0000
X-Rot (deg)	100	0.000	000	000	001	001	000	000	000			00000	000000	000	000000	0.0001	0.0001	0,0001	000	0.0000	0.000	-0.0006	0.0002	0,0001	-0.0002	-0.0002	0.0001	-0.000-	0.000	-0.000	0000	-0.000	0000	000	000	000	-0.000	0.000	00000	000.0	-0.004	0.004	-0.002	0.002	-0.003	0.003	-0.005	0.005	-0.003	0.003	00.00	-0.005	0.005	-0.005	0.005	-0.004	0.004	000
Z-Displ (ft)	5	-0.01373	0.01	0.0	-0.	00.	0.00	00	Ċ		9	5	ō	00.0	00.0	00	9	00.0	-0.003534	30173	0	-0.004076	-0.004094	-0.003469	-0.00347	-0.00287	-0.002876	-0.002296	-0.002303	-0.001692	-0.001707	-0.001228	-0.001251	-0.0008624	-0 0005537	-0 000565	-0.0002615	-0,0002664	0	0					67	78	0.000314	-0.00032	0.000138	0.000148	-1.133e-UU6 -1 28e-OO5	173e-00	.147e-00	.698e-00	.978e-00	.617e-00	ŏ	
Y-Displ (ft)	5 718p-	8.475	8.008e-	6.915e-	5.136e-	2.851e-	9.294e-	.A 012e-	-9 445 F.	0055.0	0	0.000	0.000	0000.0	8.784e	6.877e	4.505e	2.36e	9.146e	1.721e		0.00	0.000	0.000	000.0	00.00	8.51e	0.000	5.67	9.786	5.8316	9.135e	1.808e-005	5.5126	7.000	-1 3426	2.4466	-1.622			0.000124	0.000126	0.000112	0.000113	0.000101	0.000103	8.826e-00	8.786e-00	7.103e-00	6.687e-00	4.48e-005	3.242e-00	1.495e-00	2.037e-00	-1,845e-00	1.659e-00	-1.299e-0(	
X-Displ (ft)	0 1388	0,111	0.0843	0.06055	0.04099	0.02586	0.01439	996900	- 225000.0	7/0700.	0 000	0.1388	0.111	0.08431	0.06056	0.04099	0.02586	0.01439		0.001672		0.1387	0.1389	0.111	0.111	0.08424	0.08428	0.06045	0.06048	0.04092	0.04095	0.02575	0.02579	0.01433	0 006299	0.000233	0.001622	0.00163	0	0	38	38	Π	0.11	.0843	0.0843	0.0605	0.0605	0.0409	0.0409	0.02583	0.0143	0.0143	0,00633	0.00633	0.00163	0.0016	
Joint	Ochulo	20	RohnCP	RohnDP	RohnEP	RohnFP	RohnGP	Dohnun	Dobnin	NOTHITE I	Konnor	SNB-AP	SNB-BP	SNB-CP	SNB-DP	SNB-EP	SNB-FP	SNB-GP	SNB-HP	SNB-IP	SNB-JP	Rohnal	RohnA2	RohnBl	RohnB2	RohnCl	RohnC2	RohnD1	RohnD2	RohnE1	RohnE2	RobnF1	RohnF2	KohnGI	Pohori	PohoH2	Rohn I 1	Rohn12	Rohn J1	RohnJ2	SNB-A1	SNB-A2	SNB-B1	SNB-B2	SNB-C1	SNB-C2	SNB-D1	SNB-D2	SNB-E1	SNB-E2	SNB-FI	SNB-G1	SNB-G2	SNB-H1	SNB-H2	SNB-I1	SNB-I2	-

-4.947 145 -5.344 133.3 5.344 133.3 5.344 133.3 6.025 113.3 6.025 113.3 6.025 113.3 6.025 113.3 6.025 113.3 6.025 113.3 6.025 113.3 6.025 106.7 6.706 93.34 6.706 93.34 6.707 93.34 6.707 93.34 6.708 93.34 6.708 93.34 6.708 93.34 6.708 93.34 6.708 93.34 9.548 175 2.362 170 2.362 170 3.364 150 3.374 145	3.611 133.3 -3.839 126.7 -4.293 113.3 -4.293 113.3 -4.52 106.7 -4.974 93.34 -5.201 86.66 -5.201 86.66 -5.769 66 -5.769 70 -6.45 50 -6.45 50 -7.813 10
	-0.0003 -0.000
0.0003 0.0 0.0004 0.0 0.0004 0.0 0.0004 0.0 0.0005 0.0 0.0003 0.0	3329 0,0005 0,0007 0,00
0.000145 0.0001145 0.0001145 0.000129 0.325e-005 0.0001111 0.0001112 0.0001102 0.0001103 0.0001103 0.0001103 0.0001104 0.0001104 0.0001105 0.0001107 0.00011	-0.0005 -0.0005 -0.0007 -0.00007 -0.0007 -0.0007 -0.0007 -0.0007 -0.0007 -0.0007 -0.0007 -0.00
0.09074 0.09074 0.07597 0.06793 0.06793 0.06793 0.06793 0.06794 0.06798 0.06798 0.06798 0.0979 0.0979 0.0979 0.0979 0.0979 0.0979 0.0979 0.0979 0.0979 0.0979	0.07589 0.06792 0.06792 0.06332 0.06332 0.04673 0.04673 0.03345 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545 0.03545
RohnBc1 RohnCa1 RohnCa2 RohnCa2 RohnCb1 RohnDa2 RohnDa2 RohnDa2 RohnDa2 RohnDa2 RohnEa1 RohnEa2 RohnIa1 RohnIa1 RohnIa2 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnIa3 RohnEa2 RohnIa3 RohnEa2 RohnIa3 RohnEa2 RohnEa	SNB-Ca1 SNB-Ca2 SNB-Cb2 SNB-Cb2 SNB-Da1 SNB-Da2 SNB-Db1 SNB-Ea2 SNB-Ea2 SNB-Eb1 SNB-Eb

Joint Support Reactions for Load Case "5: 0.9D + 1.0Dg + 1.0E":

Toint abel	X Force (kips)	P	X Y Y sage Force U % (kips)	Y Z Usage Force %(kips)	Z Force kips)	Comp. Usage	Uplift Usage Usage	Result. Force (kips)	. Result. B Usage	X Moment (ft-k)	X-M. Usage 1	Y Moment (ft-k)	Y-M. Usage	Z foment (ft-k)	Z-M. Usage	Max. Usage
nJP	-2.25	0.0	0.00		36.46	0.0		1						i		0.0
3-JP	-2.90	0.0	0.00	0.0	44.53	0.0	0.0	44.62	0.0	00.0- 0	0.0	=1.1	0.0	-0.00	0.0	0.0
SohnJl	-0.03	0.0	0.09		4.00	0.0										0.0
Lu JZ	-0.03	0.0	-0.10		4.06	0.0										0.0
- L.J.	-0.52	0.0	-0.66		-1.61	0.0										0.0
CT E	-0.52	0.0	0.66		-1.54	0.0										0.0

| Coint Displacement, Loads and Namber Forces on Jointe for Load Gase "S: 0.D + 1.00 +

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0.0292 0.0219 0.0219 0.0219 0.0219 0.02092	Ť
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0.0292 0.0219 0.0219 0.0219 0.0126 0.0200 0.0334 0.0128 0.0128 0.0129	0.0781
Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas Rohnbas SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Abs SNB-Acs SNB-Bas SNB-Bas SNB-Bas SNB-Bas SNB-Acs SNB-Ba	ohnCa

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	0.0000
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ROHACOL SNB-ACOL SNB-ACOL SNB-ACOL SNB-ACOL SNB-BCOL	SNB-Ial SNB-Ia2

Beams
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Angle Label (	Torsion (ft-lbs)	Origin X Moment (ft-1bs)	Origin Y Moment (ft-1bs)	End X Moment (ft-1bs)	End Y Moment (ft-lbs)	X Shear (1bs)	Y Shear (1bs)
Rohn-LA1P	-0.19	0.10				0.03	-0.4
tohn-LA11	0.01	-0.37				-0.56	0.28
Sohn-LA12		0.33				0.57	0.1
Rohn-LA2P	-0.19	90"0-	3.18	-0.67	5,37	-0.15	1.71
Nobn-LA21		2.41				0.83	-0.93
Sohn-LA22		-2.51				-1.04	-0.25
Nohn-LA3P		0.67				0.33	-1.94
Nohn-LA31		-1.75				-0.66	2,4(
Rohn-LA32		2.72				0.95	1.55
Rohn-LA4P		-1.00				-0.29	2.91
Rohn-LA41	0.01	1.57				0.50	-3.38

-2.74 -2.999 -2.999 -4.10 -1.143 -1.15 -2.	0.06
0.018 0.010 0.	9 9 9
-7.05 -5.98 -5.98 -114.69 -114.60 -114	0.18
10.50 10.50 10.51 10.51 10.52 10.53 10.53 10.53 10.54 10.55	-0.52
-6.64 -8.97 -8.97 -8.97 -8.97 -8.98 -2.2.33 -2.2.33 -2.2.33 -2.2.13	0.24
-2.06 -1.041 -1.	000
0.0111133111331113311133111331113311133	0000
Rohn-LA42 Rohn-LB1P Rohn-LB1P Rohn-LB1P Rohn-LB21 Rohn-LB21 Rohn-LB3P Rohn-LB3P Rohn-LB4P Rohn-LB4P Rohn-LB4P Rohn-LC1P Rohn-LC3P Rohn-LD1P Rohn-LE2P Rohn-LD1P Rohn-LE2P Rohn-LE3P Rohn-LH1P Rohn-LH2P Rohn-L	Rohn-H12 Rohn-H2P Rohn-H2I

10.03 -6.25 -7.25 -7	12. 15. 45. 53.
0.018 1.181 1.	61 61 61 47
0.06 0.07 0.08 0.09	70 - 50 - 50 - 50 - 50 - 50 - 50 - 50 -
-0.75 -0.17 -0.18 -0.18 -0.198 -0.98	8.0000
0.17 -26.87 -26.87 -26.87 -26.87 -26.87 -26.87 -4.59 -115.67 -115.67 -116.79 -116.79 -117.	551. 100. 128. 127. 258. 583.
0.86  488.64  488.64  10.10  10.14  10.14  10.14  10.14  10.14  10.15	111111111
00000000000000000000000000000000000000	40000
Rohn-H22 SNB-LA12 SNB-LA12 SNB-LA13 SNB-LA22 SNB-LA33 SNB-LA33 SNB-LA33 SNB-LA34 SNB-LA34 SNB-LA34 SNB-LA35 SNB-LA36 SNB-LA36 SNB-LA36 SNB-LA37	WB-LG WB-LH WB-LH WB-LH WB-LH

\*\*\* Analysis Results for Load Case No. 5 "6: Service 1.0D + 1.0Dg + 1.0 Wo" - Number of iterations in SAPS 12 Equilibrium Joint Positions and Rotations for Load Case "6: Service 1.0D + 1.0Dg + 1.0 Wo":

Z-Pos (ft)	199.998 199.998 199.998 199.998 199.998 199.998 199.998 190
Y-Pos (ft)	9.938e-005 1.1328e-005 5.869e-005 5.869e-005 4.403e-005 1.1328e-005 4.403e-005 1.1328e-005 1.1328e-005 1.138e-005 1.138e-005 1.138e-005 1.138e-005 1.138e-005 1.138e-005 1.138e-005 1.138e-006 1.138e-
X-Pos (ft)	7.4 4.12 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 4.2 6.8 6.8 4.2 6.8 4.2 6.8 6.8 4.2 6.8 6.8 4.2 6.8 6.8 6.8 4.2 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8
Z-Rot (deg)	0.0014 0.0014 0.0016 0.0017
Y-Rot (deg)	7. 2022 7. 2022 7. 1945 7.
X-Rot (deg)	0.00033 0.0003 0.00
Z-Displ (ft)	-0.02351 -0.02561 -0.02681 -0.02681 -0.02681 -0.01165 -0.001174
Y-Displ (ft)	-7.69e-005 8.938e-005 -2.1238e-005 -3.28e-005 -0.0001146 -0.0001146 -0.0001131 -0.0001187 -0.000118
X-Displ (ft)	0.3232 0.3234 0.1305 0.08451 0.08451 0.08221 0.08221 0.0833 0.08325 0.08325 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08422 0.08423 0.08423 0.08422 0.08423 0.08423 0.08423 0.08423 0.08423 0.08448 0.08448 0.08448 0.08448 0.08448 0.08448 0.08448 0.08448 0.08448
Joint	Rohnade Rohnade Rohnade Rohnade Rohnade Rohnade Rohnade SNB-Ap SNB-Cp Rohnad Ro

175 170 170 170 170 170 170 170 170 170 170
1.071e-005 1.705e-005 8.58e-005 8.58e-005 8.58e-005 1.341e-005 1.341e-005 1.332e-005 1.332e-005 1.00147 40 1.00147 40 1.00147 40 1.00173 40 1.00173 40 1.00173 40 40 40 40 40 40 40 40 40 40 40 40 40
4 9 9 0 6 6 9 9 9 6 6 9 9 9 9 9 9 9 9 9 9
0.0025 0.0025
7.2036 7.2030 7.2030 7.2030 7.2030 7.2030 7.2031
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0.02414 0.02473 0.02615 0.02619 0.02631 0.02631 0.02631 0.02631 0.02631 0.02631 0.01283 0.01283 0.002864 0.01283 0.01283 0.002864 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678 0.0028678
1.071e-005 1.705e-005 6.496e-005 6.496e-005 1.41a1e-006 1.801e-006 1.801e-006 1.801e-006 1.901e-005 1.0001447 1.0001447 1.0001443 1.0001446 1.0001443 1.0001443 1.0001443 1.0001443 1.0001444 1.0001444 1.0001444 1.0001446 1.0001466 1
0.3756 0.3758 0.3758 0.3758 0.28472 0.28472 0.28473 0.3758 0.1485 0.1485 0.1675 0.3478 0.28473 0.3758
Rohnabs

145 1133.3 1133.3 1126.7 1126.7 1113.3 1106.7 106.7 106.7 106.7 106.7 106.7 106.7 106.7 106.7 106.7 106.7 106.7 110.3 11	
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	-7.131 7.131 -7.812 7.812
2.5.586 2.6.786 2.6.786 2.7.886 2.7.986 2.8.886 2.7.986 2.8.886 2.886 2.	
0.0051 0.0051 0.0051 0.0051 0.0052 0.0052 0.0053	0.0009
7.2019 7.2010 7.2010 7.2010 7.11861	0.0439 0.0439 0.0179
0.00011 0.0001	
0.001911 0.001946 0.002959 0.002959 0.003486 0.003486 0.003486 0.003524 0.003742 0.003742 0.003742 0.003742 0.003742 0.003742 0.003742 0.003742 0.003742 0.003742 0.002868 0.0028682 0.0028682 0.0028682 0.0028282 0.0028298 0.001077 0.001827 0.001837 0	0.002092 0.002092 0.0007519 0.0007527
-0.0001909 -0.0002621 -0.0002189 -0.0001121 -0.0001122 -0.0001132 -0.0001314 -0.0003425 -0.000345 -0.0003425 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.000345 -0.0003438	-0.0003604 -0.0003604 -0.0003616
	0.03329 0.01202 0.01202 0.001206
BBC2 CC21 CC21 CC21 CC21 CC21 CC21 CC21	SNB-Ga2 SNB-Ha1 SNB-Ha2 SNB-Ia1 SNB-Ia2

Joint Support Reactions for Load Case "6: Service 1.0D + 1.0Dg + 1.0 Wo":

Max. Usage	000000
Z-M. Usage U	000000
Y-M. Z Usage Moment % (ft-k)	-0.00 -0.00 -0.00 -0.01
Y-M. Usage b	000000
K X-M. Y E Usage Moment % (ft-k)	-1.3.0
X-M. Usage 1	000000
Moment (ft-k)	-0.01 -0.00 0.28 -0.27 0.95
Result. Usage 1	000000
Result. Force (kips)	90.11 123.52 20.32 20.33 38.83 38.83
Uplift Usage	000000
Comp. Usage	000000
Z Force (kips)	89.82 122.99 -20.18 -20.19 -38.48
Y Usage	000000
X Y Jsage Force % (kips)	0.02 0.00 -1.60 1.58 -3.77
X Usage %(	000000
X Force Us (kips)	-7.13 -11.50 -1.72 -1.76 -3.62
Joint Label	RobnJP SNB-JP RobnJI RobnJ2 SNB-J1 SNB-J2

Joint	Displ Joint Label	E X	" ¥	Forces xternal Load	rn	for Load Y Member Force	Z Member Force	Service X Disp.	1.0D + 1  Y Disp.	ODg + 1. Z Disp. (f+)	0 Wo":
		(kips)	(kips)	(Kips)	(Kips)	(KIPS)	(sqty)	77	(34)	(24)	
	RohnAP	0.1428	0.0000	-0.2953	-0.1428 -	-0.0000	0,2953	3932	0001	-0.0235	
	RohnBP	0.6/13		-1.000.I-	-0.6/13	0000	0.4267	2526	0000	-0.0268	
	RohnDP	0.1775		-0.5173	-0.1775	0.0000	0.5173	1875	0000	-0,0265	
	RohnEP	0.1832		-0.6412	-0.1832	-0.0000	0,6412	1306	.0001	-0.0235	
	RohnFP	0.2103		-0.8697	-0.2103	-0.0000	0.8697	0845	0001	0.0203	
	RohnGP	0.2904		-1.1585	-0.2904	-0.0000	CRCIT	0222	1000	0.0103	
	KohnhP	0.2489		-1.1331	-0.2469	-0.000	1 2937	0063	0000	-0.0057	
	Ronnir Pohn TB	0.3140		-0.6991	6 9463	-0.0226	89.1251	0000	0000	000000	
	SNR-AP	0.0418		-0.1553	-0.0418	0.0000	0.1553	3933	00003	-0.0125	
	SNB-BP	0.1010		-0.3361	-0.1010	0.0000	0.3361	3224	0.0002	-0.0149	
	SNB-CP	0.1463		-0.4267	-0.1463	0.0000	0.4267	.252	1,000.0	-0.0168	
	SNB-DP	0.1775		-0.5173	-0.1775	0.0000	0.5173	187	0.0001	-0.0175	
	SNB-EP	0.1832		-0.6412	-0.1832	0000	0.6412 0.8697	084	0000	-0.0161 -0.0149	
	SNB-EP	0.2103		-1.0585	-0.2380	0000	1.0585	.048	00000	-0.0123	
	SNB-HD	0.2300		-1.1531	-0.2489	-0.0000	1.1531	.022	00000.0	-0.0091	
	SNB-IP	0.3148		-1,2937	-0.3148	0.0000	1.2937	.006	0.000.0	-0.0046	
	SNB-JP	0.1865		-0.6991	11.3114	-0.0010	122.2891	000.	0.000.0	0.000.0	
	RohnA1	0.1428		-0.2953	-0.1428	0.0000	0.2953	.393	0.0004	-0.0007	
	RohnA2	0.2439		-0.4353	-0.2439	-0.0000	0.4353	200	0.0004	-0.00.0-	
	RohnB1	0.2340		-0.4501	-0.2340	0.0000	0.4501	322	5000	0.000	
	RohnB2	0.1463		-0.3851	-0.1600	0000	0.000	252	0.000	0.0022	
	RohnC1	0.1463		-0.4267	-0.1463	-0.0000	0.4267	,252	0.0003	0.0023	
	RohnD1	0.2244		-0.5873	-0.2244	0.0000	0.5873	1.187	0.000.0	0.0033	
	RohnD2	0.1775		-0.5173	-0.1775	-0.0000	0.517	1.187	0.0002	0.0033	
	RohnE1	0.1832		-0.6412	-0.1832	0.0000	0.6412	130	0.0000	0.0037	
	RohnE2	0.1832		-0.6412	-0.1832	-0.0000	0.641	. I30	0,0000	0.0037	
	RohnFl	0.2103		-0.8697	-0.2103	0.0000	1 014	0.084	0.000	0.0037	
0	PohnG1	0.3120		-1 1185	-0 2673	00000	1.118	0.048	0.0001	0.0032	
	RohnG2	0.3606		-1.2145	-0.3606	-0.0000	1,214	0.048	0.0000	0.0032	
	RohnHl	0.2489		-111531	-0.2489	0.0000	1,153	0.022	0.0001	0.0025	
	RohnH2	0.2489		-1,1531	-0.2489	-0.0000	1.153	0.022	00000.0	0.0025	
	RohnIl	0.3148		-1.2937	-0.3148	0.000	1.293	900.0	0.0000	0.0012	
	Rohniz	0.3148		7567.T-	-0.514d	1 5986	20.880		0.000	0.0000	
	RohnJ2	0.1865		-0.6991	1.5735	-1.5799	20.892	000.0	0.0000	0.0000	
	SNB-A1	0.0418		-0.1553	-0.0418	-0.0000	0.155	0.393	-0.0003	-0.0001	
	SNB-A2			-0.1553	-0.0418	0.0000	0.155	0.393	-0.0003	-0.0001	
	SNB-B1			-0.3361	-0.1010	0000	0.336	7777	2000.0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	0.0014	
	SNB-C1			-0.4267	-0.1463	-0.0000	0.426	0.252	-0.0001	0.0028	
	SNB-C2			-0.4267	-0.1463	0.0000	0.426	0,252	-0,0001	0,0028	
	SNB-D1			-0.5173	-0.1775	-0.0000	0.517	0,187	-0.0001	0.0037	
	SNB-D2			-0.5173	-0.1775	0.0000	0.517	0.18	1000 0-0	0.0038	
	SNB-EL			-0.6412	-0.1832	0000	0.641	0.130	0.000	0.0039	
	SNB-F1			-0.8697	-0.2103	-0.0000	0.869	0.084	-0.000	0.0040	
	SNB-F2			-0.8697	-0.2103	0.000	0.869	0.084	0000.0-	0.0040	
	SNB-G1			-1.058	-0,2380	-0.000	1.058	0.048	0.000	0.0035	
	SNR-H1			-1.1531	-0.2489	-0.0000	1.153	0.022	0 000	0.0027	
	SNB-H2			-1.1531	-0.2489	0.0000	1,153	0.023	0000 0-	0.0027	
	SNB-I1			-1.2937	, -0.3148	-0.000	1.293	00.00	0.000	0.0014	
	SNB-I2			-1.2937	-0.3148	0.0000	1,293	000	0000	0.0014	
	SNB-J2			-0.699.	3.4352	-3.7736	39.219	00.0	0.000	0.0000	
	RohnAaS			-0.207	5 -0.1338	0.0000	0.207	0,37	0.000	-0.0241	
	RohnAbS			-0.155	3 -0.0418	-0.0000	0.155	0,35	0000	-0.0247	
	ROHINCS			007.01	-0.164	000.0			*	200	

URS Connecticut - 4-carir

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RohnBass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass Rohnbass SNB-Aass SNB	RohnBb1 RohnBb2 RohnBc1 RohnBc2 RohnCa1

0.0026 0.0035 0.0035 0.0037	0.0040 0.0040 0.0040 0.0038 0.0031 0.0031 0.0031 0.0021
7. 2303 7. 2084 7. 2084 7. 2084 7. 1673 7. 1673 7. 1673 7. 1113 7.	00000000000
0.8981 0 0 8981 0 0 1 3356 0 1 1 3356 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.369 0.369 0.369 0.598 0.558 0.598
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	-0.0928 -0.0928 -0.1175 -0.1175 -0.1205 -0.1205 -0.1283 -0.1865
-0.8981 -1.3356 -1.3356 -1.1610 -0.2714 -0.3697 -0.3699 -0.3699 -0.3699 -0.5986 -0.5986 -0.5986 -0.1553 -0.155	-0.3697 -0.3697 -0.49999 -0.4999999999999999999999999999999999999
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0.5128 0.5835 0.5835 0.5835 0.0904 0.0928 0.0928 0.0928 0.1175 0.1283 0.1283 0.1283 0.1283 0.0418 0.0418 0.0418 0.0418 0.0592 0.0592 0.0592 0.0592 0.0592 0.0592 0.0592 0.0592 0.0592 0.0592	0.0928 0.0928 0.0928 0.1175 0.1175 0.1205 0.1283 0.1283
RohnCa2 RohnCb1 RohnCb2 RohnDa1 RohnDb1 RohnDb1 RohnEa1 RohnEa1 RohnEa2 RohnEb2 RohnEb2 RohnEb1 RohnEa1 RohnEa1 RohnHa2 SNB-Ab2 SNB-Ab2 SNB-Bb1 SNB-Bb2 SNB-Bc2 SNB-Ca	SNB-Ea2 SNB-Eb1 SNB-Eb2 SNB-Fa1 SNB-Fa2 SNB-Ga2 SNB-Ga2 SNB-Ha1 SNB-Ha1 SNB-Ha2 SNB-Ha2

Moments for Angles Modeled as Beams:

0.00 0.52 0.00 0.00 0.00 0.00 0.00 0.00	X Moment (ft-1bs)	Origin K Moment (ft-lbs)	End X Moment Moment (ft-1bs)	End Y Moment (ft-1bs)	X Shear (1bs)	Y Shear (1bs)
0.49 0.52 0.00 0.49 0.49 0.52 0.52 0.52	0.27	1.01		*	1.14	-1.01
0.52 0.00 0.49 0.52 0.49 0.49	-0.45	0.62	0.47	9.27	00.00	1.98
0.00 0.49 0.52 0.00 0.49 0.52	0.39	0.76			0.72	-0.37
0.49 0.00 0.00 0.49 0.52	-5.44	6.08			-2.52	2.97
-0.52 0.00 0.49 -0.52	-0.47	-9.27			-1.10	-6.04
0.00 0.49 -0.52 0.00	-3,21	2.60			-1.12	0.39
0.49	7.17	-8.79			3.00	-3.16
-0.52	5.05	20.95			2.07	9.23
00.00	2.41	0.66			0.12	2.75
	-7.86	7.01			-2.36	3.67
	-5.32	-25.22			-2.80	-10,83

-6.65 -1.3.34 -1.3.	1000000
1. 49 1. 23 1.	00000
-20.05 -21.68 -21.68 -21.30 -21.31 -23.00 -21.10 -21.10 -21.10 -21.10 -21.10 -21.10 -22.11.18	100000
5.67 19.40 19.40 19.40 10.94 10.94 10.98 10.	12.0
13.08 19.04 20.04 21.32 21.32 21.33 21.33 21.33 21.33 21.33 21.33 21.33 21.33 21.33 21.33 21.31 21.33 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 21.31 22.31 23	100-
1.81 8.18 8.18 8.18 8.18 9.18 1.00	
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11.2 12.2 11.1	-32.13 -30.05 10.05 -113.97 -113.97 -113.97 -10.75 -10.75 -10.27 -10.27 -10.27 -10.27 -10.27 -10.27 -2.27 -10.27 -2.27 -10.27 -2.27 -2.27 -2.27 -2.27 -39.55 -3
V404LL 8 V W B O V 9 L O O O L V V V V V V V V V V V V V V V	-28.09 -21.00 -21.00 -20.01 -2
11.00 11.00 13.00 13.00 13.00 14.00 10.00	-37.23 -57.23 -50.25 -50.25 -50.138 -208.43 -60.12 -10.02 -10.02 -10.02 -10.03
0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03	1, 90 0, 00 0, 00 0, 00 1, 91 1,
hn-H2 B-LA1 B-LA1 B-LA2 B-LA2 B-LA2 B-LA3 B-LB3 B-	######################################

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11.555.87 1.383.59 1.383.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.03.55.87 1.045 1.05.17 1	
531.13 1705.32 1705.32 1705.32 1072.99 1072.99 1072.91 35.20 102.00 103.00 1	133. 038. 143.
13.48 - 4.4.4 - 4.4.4 - 4.4.4 - 4.4.4 - 6.5.58 - 6	9
SNB-LH22 SNB-LI112 SNB-LI112 SNB-LI112 SNB-LI122 SNB-H102 SNB-H103	9-H9 6H-E

Service Loads Check:

Max. Usage	7.3
Disp. Usage	7.3
Actual Allowable Disp. Disp. Disp. Usage U	5.40
Actual Disp. (ft)	0.39
wa <u>y</u> age	5.1
Actual Allowable S Sway Sway Us (deg) (deg)	4.00
Actual Sway (deg)	0.20
Twist Usage	0.1
Allowable Twist Twist Usage (deg)	4.00
Actual Twist (deg)	0.00
Elevation (ft)	180.00
Joint I Label	SNB-A2
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180.000 180.000 180.000 180.000 179.999 175.999 175.000 175.000 175.000 175.000 176.00
SNB-A13 SNB-M1-A25 ROMAA2 ROMAA2 ROMAA2 ROMAA2 ROMAA2 ROMAA2 ROMAA3 SNB-AA2 ROMAA3 SNB-AA2 ROMAA3 SNB-AA2 ROMAA3 SNB-AA2 SNB-BA2 SNB-AA2 SNB-BA2 SNB-CA2

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000000000000000000000000000000000000000			0.20 0.20 0.20 0.20 0.19 0.19 0.19 0.17 0.17
000000000			111110000000000000000000000000000000000
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126.66 126.66 126.66 126.64 126.63 120.00 120.00	1120.00 1119.99 1119.99 1119.99 1113.34 1113.34 1113.34 1113.34 1113.34 1113.34 1106.66 106.66 106.66 106.66 106.66	00000000000000000000000000000000000000	80.00 779.99 779.99 779.99 770.00 770.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00
SNB-Cb1 RohnCb2 RohnCb1 SNB-CbS RohnCb2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D2 SNB-D3 SNB-D4 RohnD2	SNB-WID2S SNB-WID3S SNB-WID3S SNB-DP ROHDD2 SNB-DD1 SNB-DD1 ROHDD3 SNB-DD2 SNB-DD3 SNB-DD3 SNB-DD3 SNB-DD3 SNB-DD3 SNB-DD3 SNB-DD3 SNB-E1 SNB-DD5 SNB-E1	NNB-WL-E2S SNB-WL-E1S SNB-EE SNB-EE SNB-EE SNB-EE SNB-EE SNB-E2Z SNB-EZ	SNB-WIL-F2S SNB-WIL-F3S SNB-WIL-F3S SNB-WIL-F3S SNB-F2 SNB-F2 SNB-F2 SNB-F2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-G2 SNB-MI-G2S SNB-WIL-G3S

4.1	4.1	3.5	3.5	3.5	3.5	3,3	3.3	2.8	2.8	2.8	2.8	2.4	2.4	2.4	2.4	2.4	2.1	2.1	2.1	2.1	1.7	1.7	1.4	1.4	1.4	1.4	0.9	0.9	0.9	0.9	0.9	0.6	9.0	9.0	9.0	0.3	0.3
0.9	0.9	9.0	9.0	9.0	9.0	9.0	9.0	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0,4	0.2	0.2	0.2	0.2	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0
5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40	5.40
0.05	0.05	0.03	0.03	0.03	0.03	0.03	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	00.00	00.00	00.00	00.00	00.00	0.00
4.1	4.1	3.5	3.5	3.5	3.5	3,3	3,3	2.8	2.8	2.8	2.8	2.4	2.4	2.4	2.4	2.4	2.1	2.1	2.1	2.1	1.7	1.7	1.4	1,4	1.4	1,4	0.9	0.9	0.9	0.9	0.9	9.0	0.6	0.6	0.6	0.3	0.3
4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00
0,16	0.16	0.14	0.14	0.14	0.14	0.13	0.13	0.11	0.11	0.11	0.11	0.09	0.09	0.09	0.09	0.09	0.08	0.08	0.08	0.08	0.07	0.07	90.0	90.0	90.0	90.0	0.04	0.04	0.04	0.04	0.04	0.03	0.03	0.03	0.03	0.01	0.01
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00
00.00	00.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00
59.99	59.98	50.00	50.00	50.00	50.00	49.99	49.99	40.00	40.00	40.00	40.00	40.00	39.99	39.99	39.99	39.99	30.00	30.00	30.00	30.00	29.99	29.99	20.00	20.00	20.00	20.00	20.00	20.00	19.99	19,99	19.99	10.00	10.00	10.00	10.00	10.00	10,00
SNB-GP	RohnGP	SNB-Ga2	SNB-Gal	RohnGa1	RohnGa2	SNB-GaS	RohnGaS	SNB-H2	SNB-H1	RohnH1	RohnH2	SNB-WL-H2S	SNB-WL-H3S	SNB-WL-H1S	SNB-HP	RohnHP	SNB-Ha2	SNB-Ha1	RohnHa2	RohnHal	SNB-HaS	RohnHaS	SNB-I2	SNB-II	RohnI2	RohnIl	SNB-WL-I2S	SNB-IP	RohnIP	SNB-WL-I3S	SNB-WL-I1S	SNB-Ia2	SNB-Ial	RohnIa2	RohnIal	SNB-IaS	RohnlaS

\*\*\* Analysis Results for Load Case No. 6 "1.2\*DL" - Number of iterations in SAPS  $\, 9 \,$ 

Equilibrium Joint Positions and Rotations for Load Case "1.2\*DL";

| (deg) (ft) (ft) (ft)                          | 4.335 0.000<br>5.122 0.000         | 5.91 0.0001364<br>6.695 0.0001169 | 7.481 9.238e-005 99 | 9.055 3.119e-005 |               | 10.63 1.85e-006 | 10.63 1.85e-006<br>11.42 0.63 1.85e-006 | 9,841 1,198e-009<br>10,63 1,85e-006<br>11,42 0,0001676<br>3,132 0,0001498 | 9.841 1.1688-005<br>10.63 1.85e-006<br>11.42 0.0001676<br>3.122 0.0001498<br>3.909 0.000136 | 9 9 841 1.1588-005<br>1 10 63 1.856-006<br>1 1.42 0.0001676<br>3 3.122 0.0001498<br>3 3.99 0.000136 | 10.84 1.1188e-003<br>11.42 1.85e-006<br>2.335 0.0001676<br>3.309 0.0001498<br>4.695 0.0001169<br>5.481 9.164e-005<br>6.268 6.0128 | 10.63 1.158e-005<br>11.42 0.001676<br>3.122 0.0001498<br>4.695 0.0001498<br>5.481 9.164e-005<br>6.688 6.022e-005<br>7.055 3.151e-005 | 10.63 1.188e-005<br>11.42 0.001676<br>3.122 0.0001498<br>3.909 0.0001169<br>4.695 0.0001169<br>5.481 9.164e-005<br>7.055 3.111e-005<br>7.841 1.223e-005 | 10.63 1.188e-005<br>11.42 0.001676<br>3.122 0.0001498<br>3.909 0.000136<br>4.695 0.000136<br>5.481 9.16-005<br>5.288 6.012e-005<br>7.055 3.151e-005<br>7.055 3.151e-005<br>6.288 6.22e-005<br>7.055 3.151e-005<br>7.055 3.151e-005<br>7.055 3.151e-005 | 19.63 1.188e-005<br>11.42 0.001476<br>3.122 0.0001488<br>3.909 0.000136<br>5.481 9.164e-005<br>5.481 1.225e-005<br>7.055 3.151e-005<br>7.842 1.225e-005<br>8.628 2.321e-005<br>7.841 1.225e-005<br>9.415005  | 10.63 1.180e-005 11.05 1 | 19.63 1.180e-005<br>11.42 0.00176<br>3.122 0.000148<br>3.909 0.000136<br>4.695 0.0001469<br>5.481 9.164e-005<br>6.268 6.002e-005<br>7.055 3.151e-005<br>9.415 -2.359<br>-2.165 3.752<br>-2.165 4.435  | 10.63 1.180e-005 11.40 11.42 1.80 11.42 1.80 11.42 1.80 11.42 1.80 11.40 | 10.63 1.1898-005 11.408 11.42 11.42 11.42 11.42 10.63 11.42 10.63 13.90 10.00148 13.90 10.00148 14.695 10.00148 15.28 14.15 12.28 12.165 13.75 12.295 14.435 12.295 11.75 11.75 11.75 12.295 14.435 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 11.75 12.295 12.295 11.75 12.295 12.295 11.75 12.295 12.295 11.75 12.295 12.295 12.295 11.75 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295 12.295
12.295 12. | 10.63 1.1808-005 11.42 0.00136 | 10.63 1.188e-005 11.42 0.00136 0.00136 0.000148 0.000136 0.000136 0.000148 0.000136 0.000148 0.000136 0.000148 0.000136 0.000136 0.000148 0.000136 0.000148 0.000136  | 10.63   1.1898-005   1.1898-005   11.42   1.1898-006   11.42   1.1898-005   1.1888-005   1.1888- |
10.63<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.42<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11.43<br>11 | 10.63<br>11.42<br>11.42<br>11.42<br>11.42<br>10.00101676<br>3.122<br>0.0001169<br>4.695<br>0.0001169<br>1.001169<br>0.0001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1.001169<br>1 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| 10.63   1.180e-005   11.42   1.180e-005   11.42   1.180e-005   11.42   1.180e-005   11.42   1.180e-005   1.18   | 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RohnBc2 RohnCa1 RohnCa1 RohnCb1 RohnDb2 RohnDb2 RohnDb2 RohnDb2 RohnDb2		SNB-1aZ

Joint Support Reactions for Load Case "1.2\*DL":

	X Usage %(	X Y sage Force %(kips)	Z C B Usage Force U R(kips)	Z orce ips)	Comp. Usage	Uplift Usage	Result. Force (kips)	Result. X X Usage Moment Us % (ft-k)	X Moment (ft-k)	X-M. Usage	X X-M. Y nt Usage Moment U k) % (ft-k)	Y-M. Usage	Y-M. Z Usage Moment (	Z-M. Usage	Max. Usage
ř.	0.0	0.00	0.0	9.88	0.0	0.0					"	0.0			
	0.0	0.00	0.0 16	3.52	0.0	0.0					117	0.0	Ċ		
	0.0	0.92	0.0 15	69 6	0 0	0.0						0.0	,		
_	0.0	-0.92	0.0 15	9.78	0 0	0.0						0.0			
0.27	0.0	0.47	0.0	18,28	0.0	0.0	18.29	0.0	-0.41	0.0	0.2	0.0	-0.00	0.0	0.0
~	0	-0.47	0.0	9.38	0.0	0.0						0.0			

Joint Displacements, Loads and Member Forces on Joints for Load Case "1.2\*DL":

Disp. (ft)	-0.0094	$\circ$	-0.0078	-0.0064	-0.0039	-0.0027	-0.0013	0.0000	-0.0043	-0.0042	-0.0038	-0.0032	-0.0028	-0.0022						0 0	,	-0	-0.0077	$\circ$	0	0	-0.0039	1	7	7	ï		0	0.0	-0.0043	-0-	-0-	99		-0.0031	-0.0027	-0.0027	- 1	-0.0015	-0.0015	-0.0007	0.000	- 1	-0.00
Disp. (ft)	0.0002	0	0.	0.0001	0			0.0000		0.0001	0.0001	0.0001	10000	0000	0.000.0	0.000.0	0.0002	0.0002	0.0002	0.0001	0.0001	0.0001	0.0001	. 0	0	0	0 0																					0.0000	0.0002
Disp. (ft)	0.0017		0	o c	0	0	0	0 0	0.0017	0	0	0	$\supset$	) C	0	0	0	O 0	) (				0.0004																	0.0002		-	0	0	· ·	0.000	0	0.00	0
Z Member Force (kips)	0.3543	0.5121	0.6208	1.0436	1,3901	1.3837	1.5524	-19.0455	0.4033	0.5121	0.6208	0.7694	1.0436	1 3837	1.5524	-17.6794	0.3543	0.5223	0.5401	0.5121	0.5121	0.7048	0.6208	0.7694	1.0436	1.2176	1.3421	1.3837	1,3837	1.5524	-																,	,	
Member Force (kips)	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	-0.0007	0.0000	0.0000	0.0000	0.0000	00000	0000	0.0000	-0.0012	0.0000	0.0000	0.0000	0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0,0000	0.0000	0.9202	0.0000	0000	0000			0.0000		0.0000		· c	0	0.	0.0000				0.0000
Member Y Force (kips)	0.0000		0.		0.0000		0.0000	1.0658	0.000	0.0000	0.000.0	0.000.0	0.0000	0000	0.0000		0.	0.0		0.0000			0.0000			0.0000	0.0000	0.000	0.0000	0.0000	0.0000	-0.5329	0.0000	0.0000	00000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	o c	0.0000	0.	0.0	0.0	10.2	0 0	0.000
External X Load (kips)	-0.3543	. 0	0		i	i.	i,	-0.8390			0	0	i.	-1.2701		Ö	0	o o		-0.5121	0		-0.6208				-1.3421	-1.3837	-1,3837	-1	-1.5524	0	-0.1863	-0.1863	-0.4033	-0.5121	-0.5121	-0.6208	-0.7694	-0.7694	-1.0436	-i -		d,	.i.	-1.5524	-0.8390	-0.8390	-0.1863
External Z Load (kips)		0.0000		0.0000				0.0	00000	0.0000				0000	0.0000	0.000.0	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000			0.0000			0.0000			0.0000		00000			0.0000					0.0000	0,					0.0000
External Y Load (kips)	0.0000	0.0000	0.000.0	0.0000	0,0000	0.000.0	0.0000	0,0	0.0000	0.0000		0.000.0	0.0000	0000	0.0000	0.0000	0.0000	0.000.0	0.0000	0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000.0	0.0000		0,	0.	00000	9	0	0 0	0000		000000	00000			10.0	0000		0	00000	0		0000	0.0000
Joint X Label	RohnAP	RohnCP	RohnDP	RohnEP	RohnGP	RohnHP	RohnIP	RohnJP	SNB-AP	SNB-CP	SNB-DP	SNB-EP	SNB-FP	SNB-GP	SNB-IP	SNB-JP	RohnA1	RohnA2	KonnB1	RohnC1	RohnC2	RohnDl	RohnD2	RohnE2	Rohn F1	Rohn F2	RohnG1	RohuH1	RohnH2	RohnIl	RohnI2	RohnJ2	SNB-A1	SNB-A2	SNB-B1	( )	SNB-C2	SNB-D1	SNB-E1	SNB~E2	SNB-F1	SNB-FZ		SNB-H1	SNB-HZ	SNB-I2	SNB-J1	SNB-UZ	RohnAbs

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0000	0.0002 -0.0073 0.0000 -0.0068	000	0.0000 -0.0055	0.0002 -0.0045		0.0002 -0.0033		0.0003 -0.0020	0.0003 -0.0006					0.0001 -0.0043					0.0001 -0.0041				0.0002 -0.0038	0.0002 -0.0035	0000	0002 -0.	0.0000 -0.0030	0.0000 -0.0028		-0.0002 -0.0024		1	0-	0-0	0.0003 -0.0004	
00006 00005 00005 00003	0.0003	'		-0.0001 -0		-0.0001 -0	-0.0002 -		-0.0001	0.0016	0.0016	0.001		0.0013	, 0	0			0.0008			0	0.0005				0.0002	0	0	0		- 1	-0	0-	0 -0 0001	
1.0777 1.6028 1.6028 1.3931	1.3931	0.4437	. 4.	0.5999	0.5999	0.6702	0.7135	0.7135	0.8390	0.1863	0.1863	0.1863	0.1863	0.1863 0.1863	0.2170	0.2170	.217	0.2170	0.2170	0.2951	0.2951	0.2951	0.2951	0.3257	0.3257	0.3257	0.4437	0.4437	0.4437	0.5999	0.1999	0.6702	0.7135	0.7135	0.8390	
0.0000	0.0000	00000	0.0000	0.0000	0.0000	0.0000	00000.0	0.000.0	0.0000	0.0000	0.0000	0.0000	0.0000	00000	0.0000	0.000.0	0.000.0		0.0000			0.000.0	0.0000		0.000		0.0000	0,0000		0.0000	0000	0.0000	0.0000	0.0000	0.0000	
0.0000	0.0000		0.0000	0.0000	0.000.0	0.0000	0.0000	0.0000	0.0000	0,0000	0.0000	0.0000	0.0000	0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	0.000		0.0000	0.0000		0.0000	0.0000	0.0000	0.0000	0.0000	00000	0.0000	0.0000	0.0000	0.0000	
-1.0777 -1.6028 -1.6028 -1.3931	-1.3931	-0.4437	-0.4437	-0.443/	-0.5999	-0.6702	-0.7135	-0.7135	0.8390	-0.1863	-0.1863	-0.1863	-0.1863	-0.1863 -0.1863	-0.2170	-0.2170	-0.2170	-0.2170	-0.2170	-0.2951	-0.2951	-0.2951	-0.2951	-0.3257	-0.3257	-0.3257	-0.4437	-0.4437	-0.4437	-0.5999	10.1999	-0.6702	-0,7135	-0.7135	-0.8390 -0.8390	
0.0000	0.0000	0000	0.0000	0.0000	0.000.0	0.0000	0.0000	0.000.0	0.0000		0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000.0			0.000		000000	00000	0,0000	0.000	0.0000	00000	0.0000	0.0000	0.0000	0.0000	
0.0000	0.0000		0.0000	0.0000	0.0000	00000		0.0000	0.000	0.000	0.0000	0.000.0	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.000.0		0.000	0.0000		0.0000			0.0000	00000	0.0000	0.0000	0.0000	0.00000	
RohnCa2 RohnCb1 RohnCb2 RohnDa1	RohnDa2 RohnDb1	RohnEa1	RohnEbl	RohnEb2 RohnFa1	RohnFa2	RohnGal	RohnHa1	RohnHa2	RohnIal	SNB-Aal	SNB-Aa2	SNB-Abl	SNB-Ab2	SNB-ACI	SNB-Bal	SNB-Ba2	SNB-Bb1	SNB-Bb2	SNB-Bcl	SNB-Cal	SNB-Ca2	SNB-Cb1	SNB-Cb2	SNB-Dal	SNB-Db1	SNB-Db2	SNB-Eal	SNB-ED1	SNB-Eb2	SNB-Fal	SNB-FaZ	SNB-Ga2	SNB-Hal	SNB-Ha2	SNB-Ial SNB-Ia2	

Beams	
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Modeled	
Angles	
HOH	
oments	

Angle Label	Angle Torsion Label (ft-lbs)	Origin X Moment (ft-lbs)	Origin Y Moment (ft-lbs)	End X Moment Y (ft-lbs) (	End Y Moment (ft-lbs)	X Shear (1bs)	Y Shear (1bs)
n-LAlP	1					-0.11	-0.7
Rohn-LA11	00.00	-0.08	0.05	-3.33	1.42	-0.68	0.29
Rohn-LA12	·					0.62	0.3
nn-LA2P						0.13	1.7
n-LA21						1.57	-0.7
1-LA22						-1.49	-0.B
n-LA3P						-0.02	-2.3
1-LA31						-2.10	1.0
Rohn-LA32						2.09	1.0
Rohn-LA4P						-0.02	3.2
hn-T.A41						27.75	-1.4

URS Connecticut - 4-carir

10.03 10.04 10.05 10	00000
-2.75 -2.75	
-4.41 -1.76 -1.34 -1.3.56	00000
-7.80 -9.14 -9.71 -9.72 -9.73 -9.73 -9.73 -10.66 -11.26 -11.21 -9.06 -3.26 -3.26 -3.29 -10.15 -	
-2.93 -4.46 -1.1.76 -1.1.76 -1.3.56 -1.3.56 -1.3.31	00000
-5.94 -0.07 -0.07 -0.07 -0.07 -0.07 -0.02 -0.02 -0.02 -0.02 -0.03 -0	
Rohn-LA42 Rohn-LB12 Rohn-LB13 Rohn-LB21 Rohn-LB32 Rohn-LC12 Rohn-LB32 Rohn-LC12 Rohn-LD12 Rohn-LC22 Rohn-LD12 Rohn-LD22 Rohn-LD22 Rohn-LD22 Rohn-LD22 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LD32 Rohn-LE29 Rohn-LE39 Rohn-LE31 Rohn-LE39 Rohn-LE31	Rohn-H1P Rohn-H11 Rohn-H2P Rohn-H2P Rohn-H2P

0.00 1.933 -8.96 -8.96 -8.96 -8.96 -9.88 -9.37 -7.79 -7.79 -8.54 -8.54 -11.07 -11.07 -11.07 -2.44 -2.45 -2.45 -2.45 -2.55	48.88 -24.22 -24.22 -25.33 -25.33 -25.34 -25.34 -34.40 -34.40 -34.40 -34.52 -34.52 -34.52 -34.52 -34.53 -35.40 -48.01 -33.20 -48.01 -13.20 -20.56 -20
0.00 15.00 1.10	7.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.00 14.16 -7.12 -7.22 -2.83 -2.83 -2.83 -11.03 -11.03 -11.03 -11.03 -11.38 -1	73.48 -34.71 -97.40 50.50 50.50 50.50 -118.45 -110.78 -47.80 -47.93
0.14 0.05 12.53 -0.12 -0.12 -0.12 -0.13 18.14 18.14 18.14 0.03 0.04 -5.61 -5.61 -5.61 -5.61 -7.61	63.017 63.017 63.017 90.08 84.64 84.64 84.64 86.72 86.72 86.72 86.73 87.73
	255.32 -126.83 -13.65 -126.83 -13.65 -50.50 -50.50 -182.10 -182.10 -182.10 -182.10 -182.10 -182.10 -182.10 -182.10 -193.53 -111.12 -97.23 -97.23 -97.61 -97.
0.04 64.89 -65.22 0.05 -12.53 12.53 12.53 12.53 12.53 12.63 12.63 12.73 13.73 14.73 15.73 16.73 17	210.03 -219.06 -219.06 -0.17 -0.219.06 -0.08 -0.08 -0.09 -0.
PB-LAA	

\*\*\* Analysis Results for Load Case No. 7 "0.9DL" - Number of iterations in SAPS 9

Equilibrium Joint Positions and Rotations for Load Case "0.9DL":

Rehmer   Condition   Conditi	Label	A-Dispi (ft)	(ft)	4-Dispi	(deg)	(deg)	(deg)	(£t)	(££)	(£f)
0.0003348	RohnAP	0.00126	000	100	0.0		0	4.334	0.0	7
0.0003573 0.0001022 -0.000565 -0.0000 0.0000 0.591 0.00001022 1.0000134	RohnBP	0.000877	000	0.006952	-0.0000		0	5.122	0.0	
0.0003484 6.7526-005 -0.003495 -0.0001 0.0002 -0.0000 0.481 4.7556-005 0.0001334 4.5588-005 -0.0001349 4.5588-005 -0.0001349 0.00012 0.0001344 6.5286-005 -0.0001349 0.00012 0.000134 4.5588-005 0.000134 0.0002 0.00013 4.5588-006 0.000134 0.0002 0.00013 4.5588-006 0.000135 0.00034 0.0000 0.0000 0.4001 0.0002 0.00013 0.000135 0.000135 0.000135 0.0000 0.00013 0.0000 0.00013 0.0000 0.00013 0.000135 0.00013 0.00013 0.00013 0.00000 0.00000 0.00000 0.00000 0.0000 0.00000 0.0000 0.0000 0.00000	RohnCP	0.000557	0.000	0.006523	-0.0000	7.7	$\circ$	5.91	0.0	
0.001249 4.5242-005 -0.003749 -0.0001 -0.0012 -0.0000 0.0013 1.335-005 1.335	RohnDP	0.000340	. (35	2002869 201700	-0.000	200	$\supset$ $\subset$	7 481	0,0	, ,
\$\text{2.132} \text{2.000} \text{2.137} \text{2.000} \text{2.137} \text{2.100} \text{2.137} \text{2.100} \text{2.137} \text{2.137} \text{2.100} \text{2.137} \text{2.100} \text{2.137} \text{2.100} \text{2.137} \text{2.100} \text{2.137} \text{2.100} \text{2.1000} \text{2.100} \text{2.1000} \text{2.100} \text{2.1000} 2.1	ROHIEF	0.000134	550	004500	1000.01	а.	, ,	200	75.0	•
7.335e-005 1.755-005 -0.002374 -0.0000 -0.0000 1.0.3 1.385e-006 1.385e-006 1.385e-006 1.0000125		712016	7376	0000000	-0 0001	· _	, _	9.055	3	
0.001266 0.0001285 0.0039788 -0.0000 0.0000 0.1342 0.0001285 0.0003562 0.0000348 0.0001285 0.000349 0.00001285 0.000349 0.00001285 0.0000349 0.00001285 0.0000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.00001281 0.000349 0.0000128 0.00001289 0.00001 0.00034 0.00001 0.00001 0.00001 0.00034 0.00001 0.0	DohnHD	3370-06	745	7 00207	0000 0-	111	, ,	9.841	8.74	
0.001268 0.0001125 0.003344 -0.0001 0.0000 0.3125 0.0001125 1 0.000125 0.0000138 0.00001121 0.000344 -0.0000 0.0003 3.125 0.00001121 0.0003124 -0.0000 0.0003 3.125 0.00001121 0.0003124 0.0000125 0.0000138 0.00001121 0.0003124 0.000013 3.125 0.0000138 0.00000138 0.00001 0.0000	RohnTP	339e-00	3856	.0009708	-0.0000	-	, 0	10.63	1.38	
0.0001266 0.0001125 0.0003364 0.0001 0.0004 0.0000 3.122 0.0001125 1 0.0005862 0.0001138 0.0003333 0.0001293 0.0001138 0.000333 0.0001394 0.0001394 0.00013 0.00013 0.00013 0.00013 0.00013 0.0001394 0.0001394 0.0001394 0.0001394 0.0001394 0.00013 0.000013 0.00013 0.00013 0.00013 0.00013 0.00013 0.00013 0.00013 0.000	Rohn,TP			0	0.0000	-	0.0000	11.42		
0.000343 8.7526-005 0.0001018 0.00253 -0.0000 -0.0024 0.0000 3.929 0.0001018 0.000343 8.7526-005 0.00001414 4.9526-005 0.0001018 1.000343 8.6566-005 0.0001018 1.00034 0.000343 8.6566-005 0.0001014 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 4.9526-005 0.00001414 0.000014 0.00	SNB-AP	0.00126	.000	0.003364	-0.0001	-0.0040	$\sim$	2.334	0.0	
0.0001356 6.864e-005 -0.0001018 -0.00133 -0.0000 -0.0005 -0.0000 5.909 8.752e-005 0.0001141 4.504e-005 -0.002598 -0.0001 -0.00259 -0.0000 5.481 6.864e-005 0.0001141 4.504e-005 -0.002598 -0.0001 -0.0034 -0.0000 5.481 6.864e-005 0.0001141 4.504e-005 -0.001617 -0.0001 -0.0034 -0.0000 5.481 6.864e-005 0.0001141 4.504e-005 -0.001617 -0.0001 -0.0034 -0.0000 5.481 6.864e-005 0.0001141 4.504e-005 -0.001141 -0.0001 -0.0035 -0.0000 7.841 9.135e-006 7.335e-006 7.0001 0.00012 0	SNB-BP	0.000880	.000	0.003294	-0.0000	-0.0024		3.122	0.0	
0.0001343 8.752e-005 1.002455 0.0000 0.0000 5.481 6.864e-005 1.0001141 4.504e-005 1.0001141 4.504e-005 1.0001141 4.504e-005 1.002455 0.0001 0.00014 0.0000 5.481 6.864e-005 1.0001141 4.504e-005 0.001141 0.00014 0.00014 0.0001 0.0001 0.0000 0.25 2.33e-005 2.33e-005 1.139e-006 0.001141 0.00014 0.0001 0.0001 0.0000 0.15 2.33e-005 1.139e-006 0.00014 0.00012 0.0	SNB-CP	0.000560	.000	0.003133	-0.0000	-0:0030		3.909	0	
0.0001328 6.8464-005 -0.002298 0.0001 -0.0057 -0.000 6.268 4.5046-005 5.3516-005 0.0001141 4.5046-005 -0.002665 -0.001141 4.5046-005 -0.002665 -0.00167 -0.0005 0.000 6.268 4.5046-005 5.3516-005 0.2002665 -0.00017 -0.0005 0.0000 0.000	SNB-DP	0.00034	.752	0.002853	-0.0000	-0.0056	0.0000	4.695	8.7	
0.0001181 4.504e-005 -0.000165 -0.0001 -0.0007 -0.0000 6.268 4.204e-005 2.35e-005 -0.000165 -0.0001 -0.0005 -0.0000 0.2165 -0.000 0.000	SNB-EP	0.00019	.864	0.002398	-0.0001	-0.0034	-0.0000	5.481	9 . 9	
2.351e=-005	SNB-FP	0.00011	. 504	0.002065	-0.0001	-0.0057	-0.000	6.268	4.5	
7.336e-006 1.738e-006 -0.0005603 -0.0000 0.0003 -0.0000 8.628 1.738e-006	SNB-GP	.351e-0	2.36	0.001617	-0.0001	-0.0074	0000.0-	7.055	, ,	
0.0001819 0.0001289 0.006579 0.0000 0.0000 0.2.165 0.3.752 0.00001819 0.0001289 0.006579 0.00013 0.00000 0.2.165 0.3.752 0.00001819 0.00011289 0.006579 0.00013 0.00000 0.2.165 0.3.753 0.000101289 0.006579 0.00013 0.00000 0.2.165 0.3.753 0.000101289 0.000539 0.00013 0.00000 0.2.165 0.3.753 0.00010119 0.000539 0.00000 0.0000 0.0000 0.2.954 0.3.117 0.0001253 0.0001019 0.006539 0.0000 0.0000 0.0000 0.2.954 0.3.117 0.0001253 0.00011019 0.006539 0.0000 0.0000 0.0000 0.2.954 0.3.117 0.0001253 0.00011019 0.006539 0.0000 0.0000 0.0000 0.0000 0.2.954 0.3.117 0.0001253 0.00011019 0.0005375 0.0000 0.0000 0.0000 0.0000 0.3.37 0.3.47 0.0001253 0.4.6000 0.0000 0.0000 0.0000 0.0000 0.3.37 0.00011019 0.0005375 0.0000 0.0000 0.0000 0.0000 0.3.37 0.3.47 0.0001224 0.000775 0.000775 0.0000 0.0000 0.0000 0.3.37 0.00011019 0.0007775 0.0000 0.0000 0.0000 0.3.37 0.0001224 0.0007775 0.0001279 0.0000 0.0000 0.0000 0.3.37 0.0001224 0.0007775 0.0001270 0.0000 0.0000 0.0000 0.3.74 0.4.79 0.0001224 0.0007775 0.0001270 0.0000 0.0000 0.3.74 0.4.79 0.0001224 0.0007270 0.0000 0.0000 0.3.74 0.4.79 0.0001224 0.0002204 0.0000 0.0000 0.0000 0.3.74 0.4.79 0.0001224 0.0002204 0.0000 0.0000 0.0000 0.3.74 0.2.20 0.0002204 0.0000 0.0000 0.3.74 0.2.20 0.0002204 0.0000 0.0000 0.0000 0.3.74 0.2.20 0.0002204 0.0000 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.3.74 0.0002 0.000129 0.0000 0.0000 0.0000 0.3.74 0	SNB-HP	.352e-U	129	U.UUII44	-0.000	0000	-0.0000	0 620	y -	
0.00127 0.0001289	SNB-IP	7.33be-U	./38e-	.000000.0-	0000	000	0000	0 0 0 0 0	, , ,	
0.000127 0.0001228 0.00037 0.0003 0.0013 0.0000 -2.165	SINDION	Ċ	0000	10200	2000			79.0		-
0.0008819 0.0001124 0.006779 0.0002 0.0013 0.0000 2.56 4.435 0.0000553 0.00010184 0.006779 0.0002 0.0018 0.0000 2.56 4.435 0.00001818 0.00010199 0.0006419 0.0000 0.0008 0.0000 2.56 4.435 0.00001818 0.00010199 0.0006410 0.0000 0.0008 0.0000 2.56 4.435 0.0000182 0.00001019 0.000578 0.0000 0.0008 0.0000 2.347 5.117 0.0003254 8.00896-005 0.000778 0.0000 0.0008 0.0000 0.347 5.798 0.000182 4.2820 0.000182 4.00077 0.0000 0.0000 0.347 6.479 0.000182 4.2870-0.000182 4.0000 0.00018 4.0000 0.000018 4.0000 0.00018 4.0000 0.00018 4.0000 0.00018 4.0000 0.00000	Konnal		0000	100000	0000			-2 165		
0.0008818 0.0001098 -0.00678 0.0002 0.0013 0.0000 -2.56 4.435 0.0000853 0.00010199 -0.006678 0.0002 0.0008 0.0000 -2.554 5.117 10.0000853 0.00010199 -0.00678 0.0002 0.0003 0.0000 -2.347 -5.798 0.0001825 0.4066-005 -0.005775 0.0002 0.0003 0.0000 -3.47 -5.798 0.000182	Pohnel	0.00	1000	-0.00.0-	-0 00002			17.56	,	-
0.0003253 0.0001019 0.0066395 0.0000 0.0008 0.0000 0.2.954 -5.117 10.0003253 0.0001019 0.0066395 0.0000 0.0008 0.0000 0.2.954 -5.117 10.0003254 0.0001119 0.0066395 0.0000 0.0009 0.0000 0.2.947 -5.798 10.0003254 0.0088 0.0001182 0.0004725 0.0000 0.0000 0.0000 0.0000 0.3.74 -5.798 10.0001824 0.0091824 0.009725 0.0094725 0.0000 0.0000 0.0000 0.0000 0.3.74 -5.798 10.0001824 0.0091824 0.0093117 0.00018 0.0000 0.0000 0.0000 0.3.74 -5.798 10.0001824 0.0091824 0.0093117 0.00018 0.0000 0.0000 0.0000 0.3.74 -5.798 10.0001824 0.0003117 0.00018 0.0000 0.0000 0.3.74 -5.716 0.0001824 0.000210 0.00018 0.0000 0.0000 0.3.74 -5.716 0.0001824 0.00021 0.00018 0.0000 0.0000 0.0000 0.3.74 -5.716 0.000210 0.00021 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0	Dohna2	9000	0 0001	-0 00676	0.000			-2.56		_
0.0003254 8.089e-005 -0.005788 0.0000 0.0008 0.0000 -3.347 5.117 10.0003255 8.089e-005 -0.005788 0.00001 0.0003255 8.089e-005 -0.005788 0.00001 0.0003 0.0000 -3.347 5.798 10.00013255 8.2416e-005 -0.005788 0.00001 0.0003 0.0000 -3.347 5.798 10.00013255 8.2416e-005 -0.005787 0.00001 0.0003 0.0000 -3.347 5.798 10.00013255 9.268e-005 -0.003717 -0.0011 0.0003 0.0000 -4.134 7.16 7.16 9.788e-005 2.5678e-005 -0.003217 -0.0011 0.0003 0.0000 -4.134 7.16 7.16 9.788e-005 2.568e-005 0.002291 0.0002 0.0003 0.0000 -4.527 7.842 1.558e-005 2.568e-005 0.002291 0.0002 0.0003 0.0000 -4.527 7.842 1.558e-005 2.788e-006 0.002204 0.0002 0.0002 0.0000 -4.92 8.523 1.558e-005 0.002204 0.0002 0.0000 0.0000 -4.92 8.523 1.558e-006 0.000201 0.0000 0.0000 0.0000 -4.92 8.523 1.558e-006 0.000201 0.00000 0.00000 0.0000 0.00000 0.0000 0.0000 0.00000 0.0000 0.00000 0	Dobne		0.0001	1000000	-0 0000			-2.954		-
0.00018254 8.089e-005 -0.005768 -0.0003 0.0007 -0.0000 -3.347 -5.798 0.00001825 9.416e-005 -0.005775 0.0002 0.00003 -0.0000 -3.74 -6.479 0.0001825 9.416e-005 -0.00474 0.0000 0.0003 -0.0000 -3.74 -6.479 0.0001824 7.42e-005 -0.00474 0.0001 0.0003 -0.0000 -4.74 -6.479 0.0001824 7.42e-005 -0.00474 0.0001 0.0003 0.0000 -4.134 7.16 9.708e-005 -0.003817 -0.0019 0.0000 0.0000 -4.134 7.16 9.708e-005 -0.003817 -0.0039 0.0000 0.0000 -4.134 7.16 9.708e-005 2.142e-005 -0.002929 0.0001 0.0003 0.0000 -4.527 7.842 1.655e-005 1.246e-005 -0.002929 0.0002 0.0003 0.0000 -4.92 8.523 1.655e-005 1.246e-005 -0.002015 0.0002 0.0000 -4.92 8.523 1.655e-006 1.198e-006 -0.002015 0.0000 -4.92 8.523 1.655e-006 1.198e-006 -0.002015 0.0000 0.0000 -5.315 -9.206 1.298e-006 -0.002015 0.0000 0.0000 -5.315 -9.206 0.0001269 0.0001269 0.0000 0.0000 -5.315 -9.206 0.0000 0.0000 0.0000 -5.315 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00	PohnC2	0000	000.0	-0.00640	-0.0000			-2.954		
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0.000182	Rohn D2	0.000	9.416e-	-0.00577	0.0002			-3.347		
0.001884 7.42e-005 -0.00474 0.0000 0.0003 0.0000 -3.74 6.479 19.66e-005 3.677e-005 -0.003817 0.0010 0.0008 0.0000 -4.134 7.16 9.66e-005 3.677e-005 -0.003817 0.0010 0.0008 0.0000 -4.134 7.16 4.871e-005 2.142e-005 -0.003817 0.0010 0.0003 0.0000 -4.527 7.842 7.86e-005 2.68e-005 -0.00229 0.0002 0.0003 0.0000 -4.527 7.842 7.85e-005 1.246e-005 -0.002204 0.0003 0.0002 0.0000 -4.92 8.523 1.655e-005 1.246e-005 -0.002205 0.0002 0.0002 0.0000 -4.92 8.523 1.655e-005 1.246e-005 0.002015 0.0002 0.0000 -4.92 8.523 1.655e-005 1.246e-005 0.002015 0.0002 0.0000 0.0000 -4.92 8.523 1.655e-005 1.246e-005 0.002054 0.0000 0.0000 0.0000 -5.315 9.206 0.00000 0.0000 0.0000 0.0000 0.0000 0.00	RohnEl	0.000	6.336e-	-0.00472	-0.0001	0.000	-0.0000	-3.74		
9.66e-005 3.677e-005 -0.003817 -0.0011 0.0008 0.0000 -4.134 -7.16   4.85e-005 5.357e-005 -0.003839 0.0010 0.0008 0.0000 -4.527 7.842   4.85e-005 5.357e-005 -0.002929 0.0010 0.0003 0.0000 -4.527 7.842   1.656-005 5.737e-006 -0.002929 0.0002 0.0000 -4.922 8.523   1.656-005 1.246e-005 -0.002049 0.0002 0.0000 -4.922 8.523   1.656-006 1.198e-006 -0.002064 -0.0007 0.0004 0.0000 -5.315 9.206   1.298e-006 -1.198e-006 -0.002064 -0.0007 0.0004 0.0000 -5.315 9.206   1.298e-006 -1.198e-006 -0.002064 -0.0007 0.0004 0.0000 -5.315 9.206   1.298e-006 -1.009604 -0.0009604 -0.0007 0.0004 0.0000 -5.315 9.206   1.298e-006 -1.009604 -0.0009604 0.0004 0.0000 -5.315 9.206   1.298e-006 -1.009604 -0.0009604 0.0004 0.0000 -5.315 9.206   0.001269 0.0001254 -0.003299 0.0004 0.0000 -1.165 -2.021   0.0001269 0.0001254 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001254 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001138 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001257 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001125 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001125 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.000125 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001125 -0.003299 0.0004 0.0000 -1.165 -2.703   0.0001269 0.0001125 -0.003299 0.0002 -1.165 -2.703   0.0001269 0.000125 -0.003299 0.0002 -1.165 -2.703   0.0001269 0.000125 -0.003299 0.0002 -1.165 -2.703   0.0001269 0.0001269 0.000329 0.0000 -1.165 -2.703   0.000182 0.000125 -0.00329 0.0003 0.0000 -2.347   0.000182 0.0001269 0.000320 0.0003 0.0000 -3.134   0.000182 0.000326 0.000320 0.0003 0.0000 -3.134   0.000182 0.000320 0.000320 0.0003 0.0000 -3.134   0.000182 0.000320 0.000320 0.0003 0.0000 -3.134   0.000182 0.000320 0.000320 0.0003 0.0000 -3.134   0.000182 0.000320 0.000320 0.0003 0.0000 0.3.134   0.000182 0.000320 0.000320 0.0003 0.0000 0.3.134   0.000182 0.000320 0.000320 0.000320 0.0000 0.3.134   0.000182 0.000320 0.000320 0.000320 0.0000 0.3.134   0.000182 0.000320 0.000320 0.000320 0.0000 0.3.134   0.000320 0.00032	RohnE2	00000	7.42e-	-0.0047	0.0000	0.000	0.0000	-3.74		
9.7086-005 5.357e-005 -0.003839 0.0010 0.0008 0.0000 -4.134 7.16 4.871e-005 2.142e-005 -0.00291-0.0003 0.0002 4.527 7.842 1.862e-005 2.142e-005 -0.002291 0.0002 0.0002 0.0000 -4.527 7.842 1.862e-005 5.737e-006 -0.002203 0.0002 0.0002 0.0000 -4.92 8.523 1.652e-006 -1.198e-006 -0.002204 0.0007 0.0002 0.0000 -4.92 8.523 1.652e-006 -1.198e-006 -0.002204 0.0007 0.0004 0.0000 -5.315 9.206 1.298e-006 0.0001254 0.000205 0.0000 0.0000 0.0000 0.5.315 9.206 0.0001269 0.0001257 0.00029 0.0004 0.0000 0.0000 0.0000 -5.315 9.206 0.0001269 0.0001257 0.00029 0.0004 0.0000 0.0000 0.0000 -5.315 9.89 0.0001269 0.0001257 0.00029 0.0004 0.0007 0.0000 0.0000 0.0000 -5.315 9.89 0.0001269 0.0001257 0.00029 0.0004 0.0000 0.0000 0.0000 -5.315 9.89 0.00008 0.0001254 0.000229 0.0004 0.0007 0.0000 0.0000 0.0000 -1.165 0.0002 0.00008 0.0001189 0.00032 0.0003 0.0002 0.0003 0.	RohnF1	9.666	3.677e-	-0.00381	-0.0011	0		-4.134		
4.871e-005 2.142e-005 -0.00291 -0.0003 0.0000 -4.527 -7.842 4.85e-005 5.737e-006 -0.002292 0.0002 0.0002 0.0000 -4.92 -6.523 1.655e-005 1.246e-005 -0.002204 -0.0003 0.0002 0.0000 -4.92 -6.523 1.655e-005 1.246e-005 -0.002204 -0.0003 0.0002 0.0000 -4.92 -6.523 1.655e-006 -1.198e-006 -0.002015 0.0002 0.0000 -5.315 9.206 1.298e-006 -0.0030504 -0.0007 0.0004 0.0000 -5.315 9.206 1.298e-006 -0.0030504 -0.0037 0.0000 0.0000 -5.315 9.89 0.0001269 0.0001254 -0.00329 0.0004 0.0000 -5.315 9.89 0.0001269 0.0001254 -0.00329 0.0004 0.0000 -1.165 -2.02 0.0001268 0.0001184 -0.00329 0.0004 0.0000 -1.165 -2.703 0.00038 0.000118 -0.00329 0.0004 0.0002 -1.165 -2.703 0.00038 0.000118 -0.00329 0.0004 0.0002 -1.165 -2.703 0.00038 0.000118 -0.00329 0.0004 0.0002 -1.165 -2.703 0.000353 0.0001253 -0.00329 0.0004 0.0002 -1.156 -2.703 0.000353 0.0001253 0.00035 0.0003 0.0028 0.0000 -1.156 -2.703 0.000353 0.000135 0.00035 0.00035 0.00035 0.0003 0.0028 0.0000 -1.156 -2.703 0.000358 0.0001253 0.00035 0.0003	Rohn F2	9.708e-	5.357e-	-0.00383	0,0010	0		-4.134		
4.85e-005 2.568e-005 -0.002929 0.0002 0.0000 -4.527 7.842 1.696e-005 5.737e-006 -0.002044 0.0003 0.0000 -4.92 8.523 1.652e-006 1.196e-006 -0.002044 0.0002 0.0000 -4.92 8.523 1.652e-006 1.196e-006 -0.0020504 0.0002 0.0000 -5.315 9.206 1.296e-006 -1.966-006 -0.0009604 0.0000 0.0000 -5.315 9.206 1.296e-006 -1.096e-006 -0.0009604 0.0000 0.0000 0.5.71 9.89 0.001269 0.0001257 0.003299 0.0044 0.0037 0.0000 1.165 2.021 0.00088 0.0001187 0.003299 0.0044 0.0037 0.0000 1.165 2.021 0.00088 0.000118 0.000118 0.003299 0.0044 0.0037 0.0000 1.165 2.021 0.0005537 0.0001259 0.00329 0.0038 0.0026 0.0000 1.156 2.703 0.000358 0.000125 0.003299 0.0034 0.0026 0.0000 1.165 2.021 0.000358 0.000118 0.000118 0.00329 0.0039 0.0028 0.0000 1.166 2.703 0.000358 0.000125 0.00329 0.0039 0.0026 0.0000 1.166 2.703 0.000358 0.000125 0.00329 0.0039 0.0026 0.0000 1.167 4.066 0.000182 0.000125 0.00329 0.0039 0.0026 0.0000 2.347 4.066 0.000182 0.00205 0.00239 0.0039 0.0000 2.347 4.747 0.000182 0.00326 0.00239 0.0039 0.0000 2.347 4.747 0.000182 0.00205 0.00239 0.0039 0.0000 3.324 4.869-005 2.5516-006 0.000134 0.0056 0.0039 0.0000 3.324 4.869-005 2.5516-006 0.00134 0.0056 0.0039 0.0000 3.327 4.611 4.869-005 2.5516-006 0.000134 0.0056 0.0039 0.0000 0.3327 4.8729 1.8828-006 0.00134 0.0056 0.0039 0.0000 0.3327 4.8729 1.8828-006 0.00134 0.0056 0.0039 0.0000 0.3327 4.4729 1.8828-006 0.000134 0.0056 0.0039 0.0000 0.3327 4.8729 1.8828-006 0.000134 0.0056 0.0039 0.0000 0.3327 4.4729 1.8828-006 0.000134 0.0056 0.0039 0.0000 0.3327 4.4729 1.8828-006 0.000134 0.0005 0.0003 0.0000 0.3327 4.4729 1.8828-006 0.000134 0.0056 0.0003 0.0000 0.3327 4.4729 1.8828-006 0.0000558 0.0003 0.0000 0.3327 4.4729 1.8728-006 0.0000558 0.0003 0.0000 0.3327 4.4729 1.8728-006 0.0000558 0.0003 0.0000 0.3327 4.4729 1.8728-006 0.0000558 0.0003 0.0000 0.3327 4.4729 1.8728-006 0.0000558 0.0003 0.0000 0.3327 4.4729 1.8728-006 0.0000558 0.0003 0.0000 0.3327 4.4729 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.	RohnG1	4.871e	2.142e-	-0.0029	-0.0003	0		-4.527		
1.696=-005 5.737=-006 -0.002014 0.0002 0.0000 -4.92 8.523 1.655=-006 -1.1246=-005 -0.002015 0.0002 0.0000 -5.315 9.206 1.298=-006 -1.0246=-005 -0.002015 0.0007 0.0004 0.0000 -5.315 9.206 1.298=-006 -1.0246=-006 -0.0009652 0.0007 0.0004 0.0000 -5.315 9.206 0.001269 0.0001257 -0.002296 0.0004 0.0007 0.0000 -1.165 -2.703 0.001269 0.0001254 -0.002299 0.0004 0.0007 0.0000 -1.165 -2.703 0.000288 0.0001254 -0.002299 0.0004 0.0007 0.0000 -1.165 -2.703 0.000389 0.0001181 -0.003219 0.0004 0.0002 0.1165 -2.703 0.0003537 0.0001053 -0.00321 0.0003 0.0002 0.1953 -3.384 0.000354 0.000155 -0.003212 0.0003 0.0002 0.1953 -3.384 0.000358 0.000155 -0.002010 0.0002 0.0000 0.1953 0.0000 0.000182 0.000358 0.000159 0.00035 0.0003 0.0000 0.1953 0.0000 0.000182 0.0001828 0.133=-005 -0.00231 0.0003 0.0000 0.2347 4.066 0.0001828 0.133=-005 -0.00231 0.0003 0.0000 0.2347 4.006 0.0001828 0.133=-005 -0.00231 0.0003 0.0000 0.2347 4.747 0.0001828 0.133=-005 -0.00231 0.0003 0.0000 0.3134 -5.428 4.876=-005 2.551=-006 -0.000352 0.0003 0.0000 0.3134 -5.428 1.696=-005 2.625=-005 -0.001137 0.0005 0.0000 0.3134 -0.0000 0.3134 0.0000 0.00000 0.00000 0.00000 0.00000 0.000000	RohnG2	4.85e	2.568e-	-0.00292	0.0002	0.000	0.0000	-4.527		
1.655e-005 1.246e-005 -0.002015 0.0002 0.0000 -4.92 8.523 1.528e-006 -1.198e-006 -0.0009604 -0.0007 0.0004 0.0000 -5.315 9.206 1.298e-006 -0.0009604 -0.0007 0.0000 0.0000 -5.315 9.206 1.298e-006 -0.0009604 -0.0007 0.0000 0.0000 -5.71 9.89 0.0001269 0.0001257 -0.003299 0.0004 0.0000 -1.165 -2.02 0.000188 0.0001184 -0.003299 0.0004 0.0003 -1.165 -2.02 0.000188 0.0001185 -0.003299 0.0004 0.0003 -1.165 -2.703 0.00038 0.000118 -0.003299 0.0004 0.0003 -1.165 -2.703 0.00038 0.000118 -0.00329 0.0004 0.0003 0.0002 -1.165 -2.703 0.0003537 9.89e-005 -0.003293 0.0026 0.0000 -1.155 -2.703 0.0003537 9.89e-005 -0.003293 0.0026 0.0000 -1.155 -2.703 0.000328 0.0001828 0.000325 -0.00329 0.00035 0.0026 0.0000 -1.353 -0.3384 0.000328 0.000328 0.000329 0.00035 0.0003 0	RohnHl	1,696e	5.737e-	-0.00200	-0.0003	0.000	0.000	-4.92		
1.652e-006 -1.198e-006 -0.0009604 -0.0007 0.0004 0.0000 -5.315 -9.206	RohnH2	1.655e	1.246e-	-0.00201	0.0002	0.000	0.0000	-4.92		
1.298e-066 4.58e-066 -0.0009652 0.0007 0.0004 0.0000 -5.315 9.206 0.0001269 0.0001257 -0.00329 0.0000 0.0000 0.0000 -5.71 9.89 0.0001268 0.0001257 -0.003296 -0.0045 0.0037 0.0000 -1.165 -2.02 0.000188 0.0001125 -0.003299 -0.0034 0.0002 0.0000 -1.165 -2.02 0.00088 0.0001118 -0.003299 -0.0039 0.0028 0.0000 -1.56 -2.703 0.00038 0.0001125 -0.003212 0.0039 0.0028 0.0000 -1.56 -2.703 0.0003537 9.83e-005 -0.003312 0.0033 0.0026 0.0000 -1.56 -2.703 0.0003537 9.83e-005 -0.00332 0.0032 0.0002 0.0003 0.0029 0.0003 0.0028 0.0000 -1.56 -2.703 0.000326 0.00010537 0.0032 0.0023 0.0025 0.0000 -1.55 0.0032 0.00032 0.0003 0.0028 0.0000 -1.59 3.385 0.000326 0.0001828 0.0000 -2.347 0.0023 0.00032 0.00032 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0000 -2.74 0.0003 0.0003 0.0000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.0000 0.0000 0.00000 0.00000 0.0000	RohnIl	1.652e	-1.198e~	-0.000960	-0.0007	0		-5.315		
0.001269 0.0001257 -0.003299 0.0044 0.0000 -5.71 9.89 0.0001269 0.0001269 0.0001264 -0.003299 0.0044 0.0007 0.1165 -2.02 0.000088 0.000118 -0.003299 0.0044 0.0037 0.0000 -1.165 -2.02 0.000088 0.000118 -0.003299 0.0044 0.0037 0.0000 -1.165 -2.703 0.00038 0.000118 -0.00329 0.0039 0.0028 0.0000 -1.56 -2.703 0.0003837 0.0001053 -0.00353 0.0028 0.0000 -1.56 -2.703 0.000326 0.000326 0.00035 0.0028 0.0000 -1.56 -2.703 0.000326 0.000326 0.0000 -1.56 -2.703 0.000326 0.000326 0.00035 0.00295 0.00035 0.0029 0.0000 -1.358 0.000326 0.000326 0.00035 0.00032 0.00029 0.0000 -2.347 -4.066 0.0001828 0.0028 0.00023 0.0023 0.0000 -2.347 -4.066 0.0001828 0.0000 -2.347 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.00032 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.00032 0.00032 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.00032 0.0000 -2.347 0.00032 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.0003 0.0000 -2.347 0.00032 0.00032 0.0003 0.0000 -2.347 0.00032 0.0003 0.0000 -2.347 0.0003 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	RohnI2	1,298e	4.58e-	-0.000965	0,0007	0		-5,315		
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	-2.485=-005 0.0007764 -9.338e-005 0.0001315 0.0001023 -0.0001789 -0.0001789 -0.0001789 -0.0002178 -0.0002178
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	SNB-Db1 SNB-cb2 SNB-ca2 SNB-ca2 SNB-cb1 SNB-cb1 SNB-cb1 SNB-ca1 SNB-da1 SNB-da2 SNB-da1 SNB-da1 SNB-da1 SNB-da1 SNB-da1 SNB-da1 SNB-da2 SNB-da

Joint Support Reactions for Load Case "0.9DL":

Joint	×	X	Y	Y	ZOLOG	Comp.	Uplift Heage	Result.	Result. X X-M. Y	X + remont	X-M.	Y Momont	Y-M.	Z	Z-M.	Max.
	kips)	9 AP	kips)	% (kips) % (kips)	kips)	) % D		(kips)		(ft-k)	) de	(£t-k)	) %	(ft-k)	) % ) )	
nJP		0.0			14.92	0.0		14.94		1		1	0.0	-0.00	1	
SNB-JP	-0.41	0.0	00.0	0.0	13.89	0.0	0.0	13.89	0.0	-0.00	0.0	-0.4	0.0	-0.00	0.0	0.0
nnJ1		0.0			14.77	0.0		14,79					0.0	-0.00		
hnJ2		0.0			14.84	0.0		14.86					0.0	00.0		
B-J1		0.0			13.71	0.0		13.71					0.0	-0.00		
R-,T2		0.0			13.78	0		13.79					0.0	0.00		

Joint Displacements, Loads and Member Forces on Joints for Load Case "0.9DL":

	0.007	-0.0065	0	-0.0039	-0.0029	-0.0010	0 0	-0.0033	0	-0,0029	-0,0024	-0.0016	-0.0011	9000 0-	00000	-0.000	-0.0068	-0,0068	-0.0064	-0.0064	-0.0058	-0.0047	-0.0047	-0.0038	-0.0029	,	,	-0.0020				0.0033			,									0-	000	0.00	000*0	-0.007	-0.0070
Y Disp. (ft)	0.0001	0.0001	0,0001	0,000	0000000	0000 0	0.000	0.0001	0.0001	000	0.0001	0.000	0.0000	0.0000	0.0000	0.0001	0.0001	0,0001	0,0001	0.0001	0.0001	0.0001	0.0001	0.0000	0000	0 0000 0	000000	00000			000			0.0001			0.0001		0.0001		0000	0.000		0.0000		0.0000			0.0001
x Disp. (ft)	0.0013	000			0.0000											0.0013			000	000	0.0003	000		0,0001	0000	0.0000	000000		00000		0 0000	0.0013	0.0009	0.0009	000	000	0.0003	000	0.0002	0.0001	0000	000	000000	000	0000	0.0000	000	001	0.0010
Z Member Force (kips)	0.2657	0,3841	0,5771	0.7827	1.0378		-14.2863	0.1397	0.3841	0.4656	0.5771	0.9526	1,0378		-13,2569	71697.0	0.4051	0.3466	0.3841	0.3841	0.4656	0.5771	0,5771	0.7827	1.0066	1.0930	1.0378	1.0378	1,1643	-14,1385		0.1397	0.3025	0.3025	0.3841	0.4656	0.4656	0.5771	0.5771	0.7827	0.9526	0.9526	1.0378	1.0378	1,1643	-13,0774	-13,1534	0.1868	0.1877
Member Force (kips)	0.0000	0000	000000	00000	00000	000000	.0005	00000	000000	000000	00000	0000	0		600	0000	0000	0 0000	000000	0.000	0000	0.000	0.0000	0.0000	0000	0.0000	0.0000	0.0000	-0.0000	-0.6901	0.6908	0.000	0.0000	0.0000	0.0000	0000	0.0000	0.0000	0.0000	0.0000	0000	0.000	0.0000	0,0000	0000	-0.3546	0.3552	0.0000	0.0000
Member Y Force (kips)	0.0000	0.0000	0.000.0	000000	0.0000	0	0.8002	0,000	0.0000	0.000.0	0.0000	0000	0.000.0	0.000.0	0.4124	0.0000	0.0000	0.000.0	0.0000	000000			0.0000	0,0	٠ .			0.0000			-0.4001					0000			0.000.0						0.0000		-0.2075		0.0000
External X Load (kips)	-0.2657	-0.3841			-1.0426									-1.1643	-0.6292	7195 0-	-0.4051	-0.3466	-0.3841	-0.3841	-0.3266 -0.4656	-0.5771	-0.5771	-0.7827	-1.9132	-1.0930	-1.0378	-1.0378	-1.1643	-0.6292		-0.1397	-0.3025	-0.3025	-0.3841	-0.384I -0.4656	-0.4656	-0.5771	-0.5771	-0.7827	10.1827	-0.9526	-1.0378	-1.0378	-1.1643	-0.6292	-0.6292	-0.1868	-0.1397
External Z Load (kips)	0.0000	0,0		0.0				0000					0.0000			0.0000		0.0000		0.0000		0.000.0			0.000					0.0000			0.000	0,0000	,	00000			0	٠.	. c	. 0				0.0000		,	0.0000
External Y Load (kips)	0.0000			0.0	0000.0		0,0	0.0000				0.0000			0.0000			0.0000		0.0000	0000			00000				0000			0,0000		0.0000	0.000.0	0.0000	0.000		0.000					°.	0.0000		0.0000			0.0000
Joint X Label	RohnaP	RohnCP	RohnEP	RohnFP	RohnGP	RohnIP	RohnJP	SNB-AP	SNB-CP	Ω	SNB-EP	SNBIFF	SNB-HP	SNB-IP	SNB-JP	RohnAl	Rohn B1	RohnB2	RohnC1	RohnC2	Rohnu1	RohnEl	RohnE2	RohnFl	Ronn F.Z	RohnG2	RohnH1	RohnH2	Rohn 12	RohnJl	RohnJ2	SNB-AI	SNB-B1	SNB-B2	SNB-C1	SNB-CZ	SNB-D2	SNB-E1	SNB-E2	SNB-F1	SNB-FZ	SNB-G2	SNB-H1	SNB-H2	SNB-II	SNB-JZ	SNB-J2	RohnAaS	RohnAbs
	1																																																

0.0069 0.0069 0.0064 0.0064 0.0064 0.0064 0.0064 0.0064 0.0069	
	0000000000
0.000098 0.000099 0.000099 0.000099 0.000099 0.00099 0	38888888888
0.1628 0.01628 1.2921 1.2921 1.2921 0.3328 0.62351 0.62351 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.1337 0.2213	0.1397 0.1397 0.1397 0.1628 0.1628 0.8442 0.8442 0.1628
0.1628 0.1628 0.1628 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1394 1.1397	0.1397 -0.1397 -0.1397 -0.1628 -0.1628 -0.8442 -0.1628 -0.1628
RohnBas RohnBas RohnCas RohnCas RohnCas RohnDas RohnCas RohnDas RohnCas RohnDas RohnCas RohnCas RohnCas RohnCas RohnCas SNB-Aas SNB-Aas SNB-Aas SNB-Bas SNB-WL-C3S SNB-WL-C3S SNB-WL-G3S SNB-WL-	RohnAb2 RohnAc2 RohnBa1 RohnBa1 RohnBa1 RohnBb1 RohnBb2 RohnBc2 RohnBc2

0.0002 -0.0002 -0.0000000000000000000000	0002 0,0002 0001 -0,000 0001 0,000 1001 0,000 0001 -0,0002 0001 -0,0002	0001	0,0008 0,0001 -0,0032 0,0032 0,0008 0,0001 -0,0032 0,0008 0,0001 -0,0031 0,0009 0,0001 -0,0031 0,0006 0,0001 -0,0031 0,0004 0,0000 -0,0030 0,0004 0,0000 -0,0030 0,0004 0,0000 -0,0030 0,0004 0,0000 0,0002 0	0,0002 0,0002 0,0002 0,0002 0,0002 0,0001 0,0001 0,0001 0,0001 0,0001 0,0001 0,0001 0,0001 0,0001 0,0001 0,0002 0,
0.8083 1.2021 1.2021 1.0449 1.0449	0.2443 0.3328 0.3328 0.3328 0.4499 0.4499	0.5027 0.5351 0.5351 0.6292 0.6292 0.1397 0.1397 0.1397	0.1397 0.1628 0.1628 0.1628 0.1628 0.1628 0.2213	0 2 4 4 1 3 3 3 4 4 4 3 3 3 4 4 4 4 3 3 3 4 4 4 4 3 3 3 4
0.0000.00000.00000.00000.00000.00000.0000	00000.000000.00000000000000000000000000			
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-0.8083 -1.2021 -1.0021 -1.0449 -0.2443	-0.2443 -0.3328 -0.3328 -0.3328 -0.3328 -0.4499	-0.5027 -0.5351 -0.65351 -0.6292 -0.1397 -0.1397 -0.1397	-0.1397 -0.1628 -0.1628 -0.1628 -0.1628 -0.1628 -0.1628	0,24413 0,24413 0,24433 0,24433 0,3328 0,3328 0,3328 0,4499 0,5027 0,5027 0,5027 0,5027 0,5027 0,5027
0.0000		000000000000000000000000000000000000000		
000000000000000000000000000000000000000		000000000000000000000000000000000000000		
RohnCa2 RohnCb1 RohnCa1 RohnDa1 RohnDa2	Rohnbb2 RohnEal RohnEal RohnEbl RohnEb2 RohnFal RohnFal	RohnGa2 RohnHa1 RohnIa1 RohnIa2 SNB-Aa1 SNB-Aa2 SNB-AA2 SNB-AA5 SNB-AA5 SNB-AAC1	SNB-ACZ SNB-Ba1 SNB-Ba1 SNB-Bb1 SNB-Bb2 SNB-Bc2 SNB-Ca1 SNB-Ca2	SNB-CD2 SNB-Da1 SNB-Da2 SNB-Db2 SNB-Eb2 SNB-Eb2 SNB-Eb2 SNB-Eb2 SNB-Eb2 SNB-Eb2 SNB-Eb2 SNB-Fa2 SNB-Fa2 SNB-Ha2 SNB-Ha2 SNB-Ha2 SNB-Ha2

Beams	
D S	
Modered	
Angles	
HOH	
STUBMIC	

0.08	in Origin at Y Moment s) (ft-lbs)	Torsion Origin X Moment ft-lbs) (ft-lbs)
-2.43 1.02 -0.50 2.13 0.45 0.10 3.31 -1.73 1.15 -1.08 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0		00.00
2.13 0.45 0.10 3.71 0.10 3.31 1.13 0.15 -3.29 1.83 -1.08 0.02 -4.90 2.19 -1.54 4.37 2.15 1.53 -0.05 7.00 5.74 -3.30 2.02		-0.06
3.31		0.13
3.31 -1.73 1.15 -3.29 -1.83 -1.08 0.02 -4.40 2.19 -1.54 -4.37 2.15 1.53 -0.05 7.08 -0.01 5.74 -3.30 2.02		0.41
-3.29 -1.83 -1.08 -4.40 2.19 -1.54 -4.37 2.15 -1.53 -0.05 7.08 -0.01 5.74 -3.30 2.02		2,43
0.02 -4.97 -0.02 -4.40 2.19 -1.54 4.37 2.15 1.53 -0.05 7.08 -0.01 5.74 -3.30 2.02		-2.13
-4.40 2.19 -1.54 4.37 2.15 1.53 -0.05 7.08 -0.01 5.74 -3.30 2.02		-0.10
4.37 2.15 1.53 -0.05 7.08 -0.01 5.74 -3.30 2.02		-3,31
-0.05 7.08 -0.01 5.74 -3.30 2.02		3.29
5.74 -3.30 2.02		-0.02
		4.40

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-1.08 -3.18	-0.00
2.03 2.03 2.03 3.01 3.01 3.02 3.36 3.37 3.38	-0.00
-3.24 -8.674 -8.674 -9.633 -10.022 -10.023 -10	0.00
-5.74 -0.10 -0.10 -0.10 -0.10 -0.10 -0.00	0.02
-2.15 -7.26 -7.26 -7.26 -7.28 -7.28 -7.28 -7.51 -7.00	-0.00
-4.37 -5.745 -5.745 -6.005 -7.155 -7.	0
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0.02 1.1.60 1.26 0.02 0.02 0.02 0.02 0.02 0.03	
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0.00 2.56.37 10.75 10.75 2.3.79 2.3.79 2.3.79 2.05 2	272116272146
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	1.1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2

Hole

Net Tens. Conn. Tens. Conn. Tens. Conn. Length No. Of No. Of

Tension Tension Tension

Max

Angle Steel Max

Group Angle

Group Summary (Tension Portion):

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Group

Printed capacities do not include the strength factor entered for each load case. The Group Summary reports on the member and load case that resulted in maximum usage which may not necessarily be the same as that which produces maximum force.

# Group Summary (Compression Portion):

lo. Of Bolts Comp.			000	00	00	00	HH	pH #	4 11 1	0	00	00	00	00	0	00	0	00	0		0.0	) H	0	00	0	) H	ef:
Curve No. No. Bo	****			om on		et 47	H 42	्य अ	e et s	. 0	ed e	(ete	111	et et	-	- 0	· e	F C	0	v v	00	0 4	01	00	0	D rt	-
	40 34 98 70	115	004 104 565	565	800	. 505	240	112	529	000	004	565	800	008	990	7.472	4.066	7.472	000	111	000	553	0.000	0.000	0.000	000	941
L/R Length Comp. Member (ft)	8 9.740 0 10.934 3 12.798 3 13.570	1 1 2	7 5.004 4 5.004 4 6.665			10	r 8			-	3 6 665	-		4 10.008	4	- 0		1- C		5 13.177		(4					9 18.6
17/1	170.38 166.50 155.13 165.83	158.34	.52.67 45.84 54.04	42.54	54.10		111.38		119.15	00.00	55.09	43.23	10.42	16.54	44.41	63.14	12	183.36		141.66		156.66	0.00	00.00	00.00	107.27	94.99
RLZ	0.500		1.000	1.000	1.000	1.000	0.500	0.500	0.500	0.000	1.000	1.000	0.250	0.500	1.000	1.000	1.000	1.000	0.000	0.500	0.000	0.500	0.000	0.000	0.000	0.500	0.500
RLY	500	. 500	0000	0000	0000	.000	.500	500	. 500	0000.	000	0000	.250	0.500	000.1	000	000.1	000	0.000	0.500	0000	0.500	0.000	000.0	000.0	0.000	0.500
RLX	0.500 00.5	500 0	000	.000	.000	.500	.500	.500	.500	0000	000.	0000	.250	.500	.000	000	0000	000		5000				0000	000.	. 5000	. 500
Conn. earing pacity (kips)		000	1 000	0.000 1	0.000 1	0.000 1	21.750 0	750 0	41.760 0	0.000.0	0.000 1	0.000 1	0.000.0	0.000 0	0.000 1	0.000 1	0.0001	0.000 1	0.000	19.500 0	0.000	4.375 0	0.000.0	0.000.0	0.000	35.100 0	35.100 0
Comp. Conn. Bearing Capacity (kips)	13. 13. 17.	9 6 6	000	00	00	00	21.	21.	44.	0	00	00	0	00	0	0 0	0	00	0	2 5	00	24	0 0	0	0 0	35	35
	33 33 33 33 33 33 33	888	0000	000	0.000	0.000.0	133	133	301	0.000	0.000	0.000	0.000	0.000	0.000	000	000	0.000	000	433	0.000	542	000	000	0.000	376	376
Comp. Conn. Shear Capacity (kips)	12.433 12.433 12.433 12.433	12.433	0.000.0	0.000	0.0	0.000	12,433	12,433	17.901	0.0	0 0	0.0	0.0	00	0	0 0	00	00	0	12.	0.0	15.	0	0	0	22.	22.
CO	5888	7 7	968 756 478	0.70	36	35	31	21	0 10 0	200	37	200	53	7.9	50	80	17	00	00	68 11	00	91	000	200	00	32	ω Μ
L/R Capacity (kips)	4 825 5 786 8 468 9 776	15.227	103.968 132.756 150.478	158.870 224.520	243, 786 285, 178	393,385 8,108	19,391	16,821	57,545	0.000	115,987	167,960	412.353	514.179	119,859	163,108	13,417	9.810	0.000	16.211	0.000	22.091	0.0	0.000	0.000	70.032	95.638
	+++++	++	+ + +	+ +	+ +	+ +	+ +	+ +	+ + -	+	+ +	+ +		+ +	+	+	+	+		+ +		+				+	+
Comp. Control Load Case	22.22.2	1.20	1.20			1.20	1.2b	1,20	0.90		1.25		1.25	125		0.90	0.90	ri.		1.2D		1.2D					0.90
Comp. Force L (kips)	-1,9241: -4,8991: -6,7521: -8,2851:	-11.4341:	-11,1471: -38,4671: -76,3891:	-127.7781:	-192.3891:	-322.2241: -0.2061:	-1,4681:	-9,3851:	-12.0732:	0.000	-8,8351:	-136,3791:	-403.8181:	478,7921:	2,5502:	6.2802:	0.2212:	0.3131:	0.000	9.9361:	0.000	.9831:	000.	000.	0.000	-14.4222:	.8132:
S F S	1 4 9 8 9							1 5					ı ı	1		1	1	1		1 1		'	00	00	0 0		
· H H																											-0
Comp.	n-DA6 n-DB6 n-DC4 n-DD2	n-DF32	n-LA4F n-LB4F n-LC3F	n-LD3E n-LE3E	n-LF1F n-LG2E	n-LI1E hn-H12	B-DA72 B-DB72	B-DD61	B-DE12	D-Dul.	B-LA4	B-LD3	B-LH21	B-LI21 ect I	B-H4c	В-Н9с]	WL-D2	WL-12		n-DC6.		n-DH32				B-DH3	B-DI3
ບິ	Rohn-DA61 Rohn-DB61 Rohn-DC41 Rohn-DD21		Rohn-LA4P Rohn-LB4P Rohn-LC3P			M.					SNB-LA4P			2 SNB-LI2P 1 Connect I2		SNB-H9CP		9 SNB-WL-I2P		Z Rohn-DC61		0 Rohn-DH32	0		77	S SNB-DH32	
	39.87 Rohn-DA66 84.67 Rohn-DB6 79.74 Rohn-DD2 84.74 Rohn-DD2 76.24 Rohn-DD2		10.72 Rohn-LA4F 28.98 Rohn-LB4F 50.76 Rohn-LC3F								7.62 SNB-LA41			93.12 SNB-LI21 0.01 Connect I			.64				0.00		00.00	0.00	0.00		88.55 SNB-DI3
k Max re Use In Comp.	7 39.87 7 84.67 4 79.74 4 84.74	97 91.97	72 10.72 98 28.98 76 50.76	43 80.43 59 76.59	32 78.92 36 91.06	31 81.91 54 2.54	36 11.81 50 28.50	18 75.48	14 67.44	00.00	62 7.62 68 45 68	20 81,20	93 97.93	12 93.12 03 0.01 Co	13 2.13	00 0 00	64 1.64		00 0 00	12 85.12 91 79.91	00.00	10 77.10	00.	0.00 0.00	00.	.45 64.45	.55 88.55
k Max re Use In Comp.	39.87 39.87 84.67 84.67 79.74 79.74 84.74 84.74	91.97 91.97 80.02	10.72 10.72 28.98 28.98 50.76 50.76	80.43 80.43 76.59 76.59	78.92 78.92 91.06	81.91 81.91 2.54 2.54	11.96 11.81 28.50 28.50	75.48 75.48	67.44 67.44	00.00 00.00	7.62 7.62	81.20 81.20	97.93 97.93	93.12 93.12 0.03 0.01 Co	2.13 2.13	3.85 3.85	64 1.64	3,19 3,19	0.00 0.00	12 85.12 91 79.91	0.00	77.10 77.10	0.00	0.00	00.	64.45 64.45	88.55 88.55
Steel Max Max Strength Usage Use In Comp. (Ksi) %	36.0 39.87 39.87 36.0 36.0 84.67 84.67 85.0 79.74 84.74 84.74 50.0 76.24	50.0 91.97 91.97	50.0 10.72 10.72 50.0 28.98 28.98 50.0 50.76 50.76	50.0 80.43 80.43 50.0 76.59	50.0 78.92 78.92 50.00 91.00	50,0 81.91 81.91 36,0 2.54 2.54	36.0 11.96 11.81 36.0 28.50 28.50	36.0 75.48 75.48	36.0 67.44 67.44	36.0 0.00 0.00	36.0 7.62 7.62	36.0 81.20 81.20	36.0 97.93 97.93	36:0 93.12 93.12 36:0 0.03 0.01 Co	36.0 2.13 2.13	36.0 3.85 3.85 36.0 0.00 0.00	36.0 1.64 1.64	36.0 3.19 3.19	20.0 0.00 0.00	50.0 85.12 85.12 50.0 79.91 79.91	50.0 0.00 0.00	50.0 77.10 77.10	50.0 0.00	50.0 0.00	50.0 0.00	5 50.0 64.45 64.45	5 50,0 88.55 88.55
Max Max Usage Use In Comp.	36.0 39.87 39.87 36.0 36.0 84.67 84.67 85.0 79.74 84.74 84.74 50.0 76.24	50.0 91.97 91.97	50.0 10.72 10.72 50.0 28.98 28.98 50.0 50.76 50.76	50.0 80.43 80.43 50.0 76.59	50.0 78.92 78.92 50.00 91.00	50,0 81.91 81.91 36,0 2.54 2.54	36.0 11.96 11.81 36.0 28.50 28.50	36.0 75.48 75.48	36.0 67.44 67.44	36.0 0.00 0.00	7.62 7.62	36.0 81.20 81.20	36.0 97.93 97.93	36:0 93.12 93.12 36:0 0.03 0.01 Co	36.0 2.13 2.13	36.0 3.85 3.85 36.0 0.00 0.00	36.0 1.64 1.64	36.0 3.19 3.19	20.0 0.00 0.00	50.0 85.12 85.12 50.0 79.91 79.91	50.0 0.00 0.00	50.0 77.10 77.10	50.0 0.00	50.0 0.00	50.0 0.00	5 50.0 64.45 64.45	5 50,0 88.55 88.55
Steel Max Max Strength Usage Use In Comp. (Ksi) %	36.0 39.87 39.87 36.0 36.0 84.67 84.67 85.0 79.74 84.74 84.74 50.0 76.24	5X3.5X0.25 4X4X0.25 50.0 80.02 80.02	10.72 10.72 28.98 28.98 50.76 50.76	50.0 80.43 80.43 50.0 76.59	50.0 78.92 78.92 50.00 91.00	50,0 81.91 81.91 36,0 2.54 2.54	36.0 11.96 11.81 36.0 28.50 28.50	36.0 75.48 75.48	36.0 67.44 67.44	36.0 0.00 0.00	36.0 7.62 7.62	36,0 81,20 81,20	36.0 97.93 97.93	93.12 93.12 0.03 0.01 Co	36.0 2.13 2.13	36.0 3.85 3.85 36.0 0.00 0.00	36.0 1.64 1.64	36.0 3.19 3.19	20.0 0.00 0.00	50.0 85.12 85.12 50.0 79.91 79.91	50.0 0.00 0.00	50.0 77.10 77.10	50.0 0.00	50.0 0.00	50.0 0.00	5 50.0 64.45 64.45	50,0 88,55 88,55
Angle Steel Max Max Size Strength Usage Use In Comp.	2.5X2.5X0.1875 36.0 39.87 39.87 2.5X2.5X0.1875 36.0 84.67 84.67 2.5X2.5X0.1875 36.0 84.74 84.74 2.5X2.5X0.25 56.0 84.74 84.74	3.5x3.5x0.25 4x4x0.25 50.0 80.02 80.02	Pipe3EH 50,0 10.72 10.72 Pipe3.5EH 50,0 28.98 28.98 Pipe4EH 50,0 50,76 50,76	Pipe5STD 50.0 80.43 80.43 Pipe5EH 50.0 76.59	Pipe6EHS 50.0 78.92 78.92 Pipe6EH 50.0 91.06 91.06	1.75X1.75X0.1875 36,0 81.91 81.91 1.75X1.75X0.1875 36,0 2.54	2X2X0.3125 36.0 11.96 11.81 2X2X0.25 36.0 28.50 28.50	2.5X2.5X0.3125 36.0 75.48 75.48	4X4X0.5 36.0 67.44 67.44 67.44	5x5x0.625 36.0 0.00 0.00	P3-437 36.0 7.62 7.62 D4-494 36.0 45.68	Pipe5EH 36.0 81.20 81.20	Pipe8XS 36.0 97.93 97.93	PipelOXS 36:0 93.12 93.12 0.1X0.1X1 36:0 0.03 0.01 Co	P3-425 36.0 2.13 2.13	2x2x0.375 36.0 3.85 3.85	2X2X0.25 36.0 1.64 1.64	2.5X2.5X0.3125 36.0 3.19 3.19	2X2X0.1875 50.0 0.00 0.00	2.5X2.5XU.Z5 50,0 85.1Z 85.1Z 3X3X0.25 50.0 79.91	3X3X0.25 50.0 0.00 0.00	4X4X0.3125 50.0 77.10 77.10	2x2x0.3125 50.0 0.00	2.5x2.5x0.3125 50.0 0.00	3.5x3.5x0.375 50.0 0.00	5X5X0.375 50.0 64.45 64.45	6x6x0.375 50.0 88.55 88.55
Angle Steel Max Max Size Strength Usage Use In Comp.	36.0 39.87 39.87 36.0 36.0 84.67 84.67 85.0 79.74 84.74 84.74 50.0 76.24	3.5x3.5x0.25 4x4x0.25 50.0 80.02 80.02	50.0 10.72 10.72 50.0 28.98 28.98 50.0 50.76 50.76	Pipe5STD 50.0 80.43 80.43 Pipe5EH 50.0 76.59	Pipe6EHS 50.0 78.92 78.92 Pipe6EH 50.0 91.06 91.06	1.75X1.75X0.1875 36.0 2.54 2.54	2X2X0.3125 36.0 11.96 11.81 2X2X0.25 36.0 28.50 28.50	2.5X2.5X0.3125 36.0 75.48 75.48	4X4X0.5 354.0 67.44 67.44 67.44	5x5x0.625 36.0 0.00 0.00	36.0 7.62 7.62	Pipe5EH 36.0 81.20 81.20	Fipe F0-362 50,0 50,37 90,37 Pipe Pipe 8XS 36,0 97,93 97,93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	Pipe P3-425 36.0 2.13 2.13	36.0 3.85 3.85 36.0 0.00 0.00	SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	SAE 5X5X0.375 50.0 64.45 64.45	SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Size Strength Usage Use In Comp.	1 SAE 1.75X1.75X0.1875 36,0 39.87 39.87 2 SAE 2.X2X0.1875 36,0 84.67 84.67 3 SAE 2.5X2.5X0.1875 36,0 84.74 4 SAE 2.5X2.5X0.25 36,0 84.74 84.74 84.74 84.74	6 SAE 3.5X3.5X0.25 50.0 91.97 91.97 7 SAE 4X4X0.25 50.0 80.02 80.02	Leg 1 Pipe Pipe3EH 50,0 10.72 10.72 Leg 2 Pipe Pipe3.5EH 50,0 28.98 28.98 Leg 3 Pipe Pipe4EH 50,0 50.76 50.76	Leg 4 Pipe Pipe5STD 50.0 80.43 80.43 Leg 5 Pipe Pipe5EH 50.0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 sAE 1.75x1.75x0.1875 36,0 2.54 2.54	1 SAE 2X2X0.3125 36.0 11.96 11.81 2 SAE 2X2X0.25 36.0 28.50 28.50	3 SAE 2.5X2.5X0.3125 36.0 75.48 75.48	5 SAE 4X4X0.5 36.0 67.44 67.44	7 SAE 5X5X0.625 36.0 0.00 0.00	1 Pipe P3-437 36.0 7.62 7.62 2 Pipe P4-494 36.0 45.68 45.68	3 Pipe Pipe5EH 36,0 81.20 81.20	4 Lipe F0-362 3040 90.97 50.97 5 Pipe 5 Pipe 8XS 3640 97.93 97.93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	1 Pipe P3-425 36.0 2.13 2.13	2 Pipe P4-494 36.0 3.85 3.85 8 3.85 8 3.85 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	SAE 5X5X0.375 50.0 64.45 64.45	SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Type Size Strength Usage Use In Comp.	Diagonal 1 SAE 1.75X1.75X0.1875 36.0 39.87 39.87 Diagonal 2 SAE 2.5X2.5X0.1875 36.0 84.67 84.67 Diagonal 3 SAE 2.5X2.5X0.1875 36.0 84.74 79.74 Diagonal 4 SAE 2.5X2.5X0.25 36.0 84.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74	Diagonal 6 SAE 3.5%3.2%0.25 50.0 91.97 91.97 biagonal 7 SAE 4%4%0.25 50.0 80.02 80.02	1 Pipe Pipe3EH 50.0 10.72 10.72 2 Pipe Pipe3.EH 50.0 28.98 28.98 3 Pipe Pipe4EH 50.0 50.76	Leg 4 Pipe Pipe5STD 50.0 80.43 80.43 Leg 5 Pipe Pipe5EH 50.0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 sAE 1.75x1.75x0.1875 36,0 2.54 2.54	1 SAE 2X2X0.3125 36.0 11.96 11.81 2 SAE 2X2X0.25 36.0 28.50 28.50	Diagonal 3 SAE 2.5X2.5X0.3125 36.0 75.48 75.48	Diagonal 5 SAE 5A5X0.5 36,0 67,44 67,44	Diagonal 7 SAE 5X5X0.625 36,0 0.00 0.00	P3-437 36.0 7.62 7.62 D4-494 36.0 45.68	3 Pipe Pipe5EH 36,0 81.20 81.20	4 Lipe F0-362 3040 90.97 50.97 5 Pipe 5 Pipe 8XS 3640 97.93 97.93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	1 Pipe P3-425 36.0 2.13 2.13	2 Pipe P4-494 36.0 3.85 3.85 8 3.85 8 3.85 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	SAE 5X5X0.375 50.0 64.45 64.45	- L6X6x3/8 SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Type Size Strength Usage Use In Comp.	1 SAE 1.75X1.75X0.1875 36,0 39.87 39.87 2 SAE 2.X2X0.1875 36,0 84.67 84.67 3 SAE 2.5X2.5X0.1875 36,0 84.74 4 SAE 2.5X2.5X0.25 36,0 84.74 84.74 84.74 84.74	Diagonal 6 SAE 3.5%3.2%0.25 50.0 91.97 91.97 biagonal 7 SAE 4%4%0.25 50.0 80.02 80.02	Leg 1 Pipe Pipe3EH 50,0 10.72 10.72 Leg 2 Pipe Pipe3.5EH 50,0 28.98 28.98 Leg 3 Pipe Pipe4EH 50,0 50.76 50.76	Leg 4 Pipe Pipe5STD 50.0 80.43 80.43 Leg 5 Pipe Pipe5EH 50.0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 sAE 1.75x1.75x0.1875 36,0 2.54 2.54	1 SAE 2X2X0.3125 36.0 11.96 11.81 2 SAE 2X2X0.25 36.0 28.50 28.50	Diagonal 3 SAE 2.5X2.5X0.3125 36.0 75.48 75.48	Diagonal 5 SAE 5A5X0.5 36,0 67,44 67,44	7 SAE 5X5X0.625 36.0 0.00 0.00	1 Pipe P3-437 36.0 7.62 7.62 2 Pipe P4-494 36.0 45.68 45.68	3 Pipe Pipe5EH 36,0 81.20 81.20	4 Lipe F0-362 3040 90.97 50.97 5 Pipe 5 Pipe 8XS 3640 97.93 97.93	6 Pipe Pipe10XS 36:0 93.12 93.12 8:18 0.1X0.1X1 36:0 0.03 0.01 Co	1 Pipe P3-425 36.0 2.13 2.13	2x2x0.375 36.0 3.85 3.85	1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	SAE 5X5X0.375 50.0 64.45 64.45	- L6X6x3/8 SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Type Size Strength Usage Use In Comp.	Diagonal 1 SAE 1.75X1.75X0.1875 36.0 39.87 39.87 Diagonal 2 SAE 2.5X2.5X0.1875 36.0 84.67 84.67 Diagonal 3 SAE 2.5X2.5X0.1875 36.0 84.74 79.74 Diagonal 4 SAE 2.5X2.5X0.25 36.0 84.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74	Diagonal 6 SAE 3.5%3.2%0.25 50.0 91.97 91.97 biagonal 7 SAE 4%4%0.25 50.0 80.02 80.02	Leg 1 Pipe Pipe3EH 50,0 10.72 10.72 Leg 2 Pipe Pipe3.5EH 50,0 28.98 28.98 Leg 3 Pipe Pipe4EH 50,0 50.76 50.76	Leg 4 Pipe Pipe5STD 50.0 80.43 80.43 Leg 5 Pipe Pipe5EH 50.0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 SAE 1.75X1.75X0.1875 36,0 2.54 2.54	1 SAE 2X2X0.3125 36.0 11.96 11.81 2 SAE 2X2X0.25 36.0 28.50 28.50	Diagonal 3 SAE 2.5X2.5X0.3125 36.0 75.48 75.48	Diagonal 5 SAE 5A5X0.5 36,0 67,44 67,44	Diagonal 7 SAE 5X5X0.625 36,0 0.00 0.00	1 Pipe P3-437 36.0 7.62 7.62 2 Pipe P4-494 36.0 45.68 45.68	3 Pipe Pipe5EH 36,0 81.20 81.20	4 Lipe F0-362 3040 90.97 50.97 5 Pipe 5 Pipe 8XS 3640 97.93 97.93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	1 Pipe P3-425 36.0 2.13 2.13	2 Pipe P4-494 36.0 3.85 3.85 8 3.85 8 3.85 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	SAE 5X5X0.375 50.0 64.45 64.45	- L6X6x3/8 SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Type Size Strength Usage Use In Comp.	Diagonal 1 SAE 1.75X1.75X0.1875 36.0 39.87 39.87 Diagonal 2 SAE 2.5X2.5X0.1875 36.0 84.67 84.67 Diagonal 3 SAE 2.5X2.5X0.1875 36.0 84.74 79.74 Diagonal 4 SAE 2.5X2.5X0.25 36.0 84.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74	Diagonal 6 SAE 3.5%3.2%0.25 50.0 91.97 91.97 biagonal 7 SAE 4%4%0.25 50.0 80.02 80.02	Leg 1 Pipe Pipe3EH 50,0 10.72 10.72 Leg 2 Pipe Pipe3.5EH 50,0 28.98 28.98 Leg 3 Pipe Pipe4EH 50,0 50.76 50.76	Leg 4 Pipe Pipe5STD 50.0 80.43 80.43 Leg 5 Pipe Pipe5EH 50.0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 sAE 1.75x1.75x0.1875 36,0 2.54 2.54	1 SAE 2X2X0.3125 36.0 11.96 11.81 2 SAE 2X2X0.25 36.0 28.50 28.50	Diagonal 3 SAE 2.5X2.5X0.3125 36.0 75.48 75.48	Diagonal 5 SAE 5A5X0.5 36,0 67,44 67,44	Diagonal 7 SAE 5X5X0.625 36,0 0.00 0.00	1 Pipe P3-437 36.0 7.62 7.62 2 Pipe P4-494 36.0 45.68 45.68	3 Pipe Pipe5EH 36,0 81.20 81.20	4 Lipe F0-362 3040 90.97 50.97 5 Pipe 5 Pipe 8XS 3640 97.93 97.93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	1 Pipe P3-425 36.0 2.13 2.13	2 Pipe P4-494 36.0 3.85 3.85 8 3.85 8 3.85 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 85.12 84.01	SAE 3X3X0.25 50.0 0.00 0.00	SAE 4X4X0.3125 50.0 77.10 77.10	SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	SAE 3.5X3.5X0.375 50.0 0.00	- L5X5x3/8 SAE 5X5X0.375 50.0 64.45 64.45	SAE 6X6X0.375 50.0 88.55 88.55
Group Angle Angle Steel Max Max Desc. Type Size Strength Usage Use In Comp.	Rohn Diagonal 1 SAE 1.75X1.75X0.1875 36.0 39.87 39.87 84.67 84.74	Rohn Diagonal 7 SAE 3.5X3.5X0.25 50.0 91.97 91.97 Rohn Diagonal 7 SAE 4X4X0.25 50.0 80.02	Rohn Leg 1   Pipe   Pipe3EH 50,0 10.72 10.72   Rohn Leg 2 Pipe   Pipe3.5EH 50,0 28.98   Rohn Leg 3 Pipe   Pipe4EH 50,0 50.76 50.76   Rohn Leg 3 Pipe   Pipe4EH 50,0 50.76 50.76   Rohn Leg 3 Pipe   Pipe4EH 50,0 50.76   Rohn Leg 3 Pipe4EH 50,0 50.76   Rohn Leg 4 Pipe4EH 50,0 50.76   Rohn Leg 5 Pipe4EH 50,0 5 P	Rohn Leg 4 Pipe Pipe5STP 50,0 80.43 80.43 Rohn Leg 5 Pipe Pipe5EH 50,0 76.59 76.59	Rohn Leg 6 Pipe Pipe6EHS 50,0 78.92 78.92 Rohn Leg 7 Pipe Pipe6EH 50,0 91.06 91.06	Rohn Leg 8 Pipe Pipe8EHS 50,0 81.91 81.91 Rohn Horizontal 1 SAE 1.75X1.75X0.1875 36,0 2.54 2.54	SNB Diagonal 1 SAE 2X2X0.3125 36,0 11.96 11.81 SNB Diagonal 2 SAE 2X2X0.25 36,0 28.50 28.50	SNB Diagonal 3 SAE 2.5X2.5X0.3125 36,0 75.48 75.48	SNB Diagonal 5 SAE 4X4X0.5 36,0 67.44 67.44	SNB Diagonal 7 SAE 44444,023 36,0 06.10 00.10 SNB Diagonal 7 SAE 5X5X0.625 36,0 0.00 0.00	SNB Leg 1 Pipe P3-437 36,0 7.62 7.62 80 81 1.00 2 Pipe P4-494 36,0 45,68 45,68	SNB Leg 3 Pipe Pipe5EH 36,0 81.20 81.20 81.20 81.20 81.20	SNB Leg 5 Pipe Pipe8XS 36,0 97.93 97.93	SNB Leg 6 Pipe Pipe10XS 36:0 93:12 93:12 Connect Towers BIG 0.1X0.1X1 36:0 0.03 0.01 Co	SNB Horizontal 1 Pipe P3-425 36.0 2.13 2.13	SNB Horizontal 2 Pipe P4-494 36.0 3.85 3.85 Robn Diagonal 8 SAE 2X2X0.375 36.0 0.00 0.00	Wind Lacing 1 SAE 2X2X0.25 36.0 1.64 1.64	SAE 2.5X2.5X0.3125 36.0 3.19 3.19 3.19 3.19	SAE 2X2X0.1875 50.0 0.00 0.00	MODIFICATION = L2.5X2.5x1/4 SAE 2.5X2.5X0.25 50,0 85.12 85.12 MODIFICATION = L3x3x1/4 SAE 3X3X0.25 50.0 79.91 79.91	MODIFICATION - L3X3x1/4 SAE 3X3X0.25 50.0 0.00 0.00	MODIFICATION - L4X4x5/16 SAE 4X4X0.3125 50,0 77.10 77.10	MODIFICATION - L2X2x5/16 SAE 2X2X0.3125 50.0 0.00	MODIFICATION - 12.5x2.5x1/4 SAE 2.5x2.5x0.25 50.00 MODIFICATION - 12.5x2.5x2.5x6/16 SAE 2.5x2.5x0.3125 50.0	MODIFICATION - L3.5x3.5x3/8 SAE 3.5x3.5x0.375 50.0 0.00	MODIFICATION - LAX4XU,5 SAE 5X2XU,3 50,0 0,00 0.00 MODIFICATION - L5X5x3/8 SAE 5X5X0.375 50,0 64.45 64.45	MODIFICATION - L6X6x3/8 SAE 6X6X0.375 50.0 88.55 88.55
Angle Steel Max Max Type Size Strength Usage Use In Comp.	Diagonal 1 SAE 1.75X1.75X0.1875 36.0 39.87 39.87 Diagonal 2 SAE 2.5X2.5X0.1875 36.0 84.67 84.67 Diagonal 3 SAE 2.5X2.5X0.1875 36.0 84.74 79.74 Diagonal 4 SAE 2.5X2.5X0.25 36.0 84.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74 Diagonal 5 SAE 2.5X2.5X0.25 56.0 87.74 84.74	Rohn Diagonal 7 SAE 3.5X3.5X0.25 50.0 91.97 91.97 Rohn Diagonal 7 SAE 4X4X0.25 50.0 80.02	Leg 1 Pipe Pipe3EH 50,0 10.72 10.72 Leg 2 Pipe Pipe3.5EH 50,0 28.98 28.98 Leg 3 Pipe Pipe4EH 50,0 50.76 50.76	Rohn Leg 4 Pipe Pipe5STP 50,0 80.43 80.43 Rohn Leg 5 Pipe Pipe5EH 50,0 76.59 76.59	6 Pipe Pipe6EHS 50.0 78.92 78.92 7 Pipe Pipe6EH 50.0 91.06 91.06	8 Pipe Pipe8EHS 50,0 81.91 81.91 1 sAE 1.75x1.75x0.1875 36,0 2.54 2.54	SNB Diagonal 1 SAE 2X2X0.3125 36,0 11.96 11.81 SNB Diagonal 2 SAE 2X2X0.25 36,0 28.50 28.50	SNB Diagonal 3 SAE 2.5X2.5X0.3125 36,0 75.48 75.48	SNB Diagonal 5 SAE 4X4X0.5 36,0 67.44 67.44	SNB Diagonal 7 SAE 5X5X0.625 36,0 0.00 0.00	1 Pipe P3-437 36.0 7.62 7.62 2 Pipe P4-494 36.0 45.68 45.68	SNB Leg 3 Pipe Pipe5EH 36,0 81.20 81.20 81.20 81.20 81.20	SNB Leg 5 Pipe Pipe8XS 36,0 97.93 97.93	Pipe Pipe10XS 36;0 93.12 93.12 BIG 0.1X0.1X1 36.0 0.03 0.01 Co	SNB Horizontal 1 Pipe P3-425 36.0 2.13 2.13	2 Pipe P4-494 36.0 3.85 3.85 8 3.85 8 3.85 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Wind Lacing 1 SAE 2X2X0.25 36.0 1.64 1.64	2 SAE 2.5X2.5X0.3125 36.0 3.19 3.19 6 SAE 1.75X1.75X0.1875 50.0 0.00	SAE 2X2X0.1875 50.0 0.00 0.00	SAE 2.5X2.5X0.25 50.0 85.12 85.12 SAE 3X3X0.25 50.0 79.91 79.91	MODIFICATION - L3X3x1/4 SAE 3X3X0.25 50.0 0.00 0.00	MODIFICATION - L4X4x5/16 SAE 4X4X0.3125 50,0 77.10 77.10	MODIFICATION - L2X2x5/16 SAE 2X2X0.3125 50.0 0.00	SAE 2.5X2.5X0.3125 50.0 0.00	MODIFICATION - L3.5x3.5x3/8 SAE 3.5x3.5x0.375 50.0 0.00	MODIFICATION - L4X4XU.5 SAE 5X2XU.375 50,0 0.00 0.00 MODIFICATION - L5X5x3/8 SAE 5X2XU.375 50,0 64.45 64.45	- L6X6x3/8 SAE 6X6X0.375 50.0 88.55 88.55

umeter (in)	0.6875 0.6875 0.6875 0.6875 0.6875 0.6875 0.6875 0.6875 0.0875	0.8125
Holes Diameter (in)	11.1.1.0000 1.1	1.000
Bolts H Tens.		н
Tens. ] Member (ft)	110,034 112,238 112,798 112,519 117,748 5,004 6,665 6,665 6,665 110,008 110,008 111,059 112,112 111,059 112,012 113,117 113,017 113,11	18.841
Rupture Capacity M (kips)	7.750 8.770 13.050 14.625 14.625 14.625 10.000 0.00	26,471
Bearing Capacity (kips)	13. 050 13. 050 13. 050 13. 050 17. 050 19. 500 0. 000 0. 000	35.100
Shear Capacity (kips)	12. 433 12. 433 13. 600 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.00	22,376
Section Capacity (kips)	16.022 18.958 18.5222 33.216 46.366 55.506 64.6366 127.350 1127.35	148.272
Force Control Load Case kips)	1.8392: 0.90 + 4.5612: 0.90 + 6.6822: 0.90 + 6.6822: 0.90 + 6.6822: 0.90 + 6.2822	17.1321: 1.2D +
Control Member	Rohn-DB4P Rohn-DB7P Rohn-DB7P Rohn-DB1P Rohn-DB1P Rohn-DB2P Rohn-DB2P Rohn-LB32 5 Rohn-LB32 5 Rohn-LB4P 5 SNB-DB4P 5 SNB-DB4P 5 SNB-DB4P 5 SNB-DB4P 5 SNB-DB4P 5 SNB-DB4P 5 SNB-LB22 12 SNB-LB22 12 SNB-LB22 12 SNB-LB32 5 SNB-LB32 5 SNB-LB32 5 SNB-LB32 5 SNB-LB32 5 SNB-HB4P 5 SNB-ML-D33 5 SNB-ML-D34 8 SNB-ML-D38 5 SNB-ML-D38 5 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8 Rohn-DD39 8	SNB-DI4P
Use In Tens.	23.73 55.70 55.70 55.70 66.10 78.158 78.158 78.160 78.18	76.56
age *	39.81 84.74 84.74 84.74 84.74 84.74 84.74 86	0 88.55
Size Strength Us (ksi)		50.
Size S	1.75x1.75x0.1875 2.5x2.5x0.1875 2.5x2.5x0.1875 2.5x2.5x0.25 3.5x3.5x0.25 3.5x3.5x0.25 3.5x3.5x0.25 Pipe3EHF Pipe4EHF Pip	6X6X0.375
Туре	SAE 1. SAE 1. SAE 1. SAE 1. SAE 2. SAE 2. SAE 2. SAE 3. SA	SAE
Desc.	Rohn Diagonal   Rohn List   Rohn Diagonal   Rohn List   Rohn Leg   Rohn List   Rohn List   Rohn Leg   Rohn List   Rohn List   Rohn Leg   Rohn List   Rohn Leg   Rohn List   Rohn List   Rohn Leg   Rohn List   Rohn Lis	MODIFICATION - L6X6x3/8
Label	Rohn-D1 Rohn-D2 Rohn-D3 Rohn-D4 Rohn-D5 Rohn-D6 Rohn-D7 Rohn-L1 SNB-D1 SNB-D2 SNB-D3 SNB-D1 SNB-D1 SNB-D2 SNB-L1 SNB-L1 SNB-L5 SNB-L1	S-D7-MOD

<sup>\*\*\*</sup> Maximum Stress Summary for Each Load Case

Summary of Maximum Usages by Load Case:
Load Case Maximum

Load Case Maximum	Maximum	Element Element	Element
	Usage %	Label	Type
	1		
1: 1.2D + 1.0Dg + 1.6Wo	97.93	SNB-LHZP	
2: 0.9D + 1.0Dg + 1.6Wo		SNB-LH2P	
4: 1.2D + 1.0Dg + 1.0E	12.42	Rohn-LD3P	
5: 0.9D + 1:0Dg + 1.0E		Rohn-LD3P	
6: Service 1.0D + 1.0Dg + 1.0 Wo		SNB-LH1P	Angle

URS Connecticut - 4-carir

Angle Angle
Rohn-LD3P Rohn-LD3P
5.66
1,2*DL 0,9DL

61800.0 12631.6 74431.6 \*\*\* Weight of structure (lbs):
Weight of Angles\*Section DLF:
Weight of Equipment:
Total:

\*\*\* End of Report

"0 DEG" "+60 DEG" "-60 DEG" "+90 DEG" "-90 DEG" "180 DEG" Max Tension

(Kips)

							(0)					
Rohn-L1 Rohn-LA1P	0	0	0	0	0	0.724	0.724				2	
Rohn-L1 Rohn-LA11	0.136	0.544	0	0.457	0	0	0.544					
Rohn-L1 Rohn-LA12	0.19	0	0.681	0	0.541	0	0.681					
Rohn-L1 Rohn-LA2P	0	0	0	0	0	2.866	2.866					
Rohn-L1 Rohn-LA21	1,337	3.058	0	2,623	0	0	3.058					
Rohn-L1 Rohn-LA22	1.103	0	2.769	0	2.379	0	2.769					
Rohn-L1 Rohn-LA3P	0	0	0	0	0	5.911	5.911					
Rohn-L1 Rohn-LA31	2.729	6.009	0	5.174	0	0	600.9					
Rohn-L1 Rohn-LA32	2.566	0	5.745	0	4.959	0	5.745					
Rohn-L1 Rohn-LA4P	0	0	0	0	0	9.192	9.192		. Bolt	Bolt Tension Factored Tensile	d Tensile	
Rohn-L1 Rohn-LA41	4.146	8.712	0	7.475	0	0	8.712		Capacity	city Capacity	>	Cap Percentage
Rohn-L1 Rohn-LA42	4.244	0	8.805	0	7.522	0	8.805 # B	solts Dia	8.805 # Boits Dia Bolt LRFD			
Rohn-L2 Rohn-LB1P	0	0	0	0	0	12.811	12.811	4	-0.75	29.8	119.2 OK	11%
Rohn-L2 Rohn-LB11	6.153	13.063	0	11.245	0	0	13.063	4	0.75	29.8	119.2 OK	11%
Rohn-L2 Rohn-LB12	6.245	0	13.06	0	11.207	0	13.06	4	0.75	29.8	119.2 OK	11%
Rohn-L2 Rohn-LB2P	0	0	0	0	0	17.68	17.68	4	0.75	29.8	119.2 OK	15%
Rohn-L2 Rohn-LB21	8.54	18.046	0	15.64	0	0	18.046	4	0.75	29.8	119.2 OK	15%
Rohn-L2 Rohn-LB22	8.695	0	18.086	0	15.612	0	18.086	4	0.75	29.8	119.2 OK	15%
Rohn-L2 Rohn-LB3P	0	0	0	0	0	23,309	23.309	4	0.75	29.8	119.2 OK	20%
Rohn-L2 Rohn-LB31	11.034	23.605	0	20.383	0	0	23.605	4	0.75	29.8	119.2 OK	20%
Rohn-L2 Rohn-LB32	11.2	0	23.628	0	20.328	0	23,628	4	0.75	29.8	119.2 OK	20%
Rohn-L2 Rohn-LB4P	0	0	0	0	0	31.258	31.258	4	0.75	29.8	119.2 OK	76%
Rohn-L2 Rohn-LB41	15.015	31.542	0	27.281	0	0	31.542	4	0.75	29.8	119.2 OK	76%
Rohn-L2 Rohn-LB42	15.195	0	31.558	0	27.208	0	31.558	4	0.75	29.8	119.2 OK	26%
Rohn-L3 Rohn-LC1P	0	0	0	0	0	39,147	39.147	4	0.875	40.6	162.4 OK	24%
Rohn-L3 Rohn-LC11	18.931	39.503	0	34.212	0	0	39,503	4	0.875	40.6	162.4 OK	24%
Rohn-L3 Rohn-LC12	19.156	0	39.549	0	34.147	0	39.549	4	0.875	40.6	162.4 OK	24%
Rohn-L3 Rohn-LC2P	0	0	0	0	0	49.616	49.616	4	0.875	40.6	162.4 OK	31%
Rohn-L3 Rohn-LC21	23.834	49.756	0	43.058	0	0	49.756	4	0.875	40.6	162.4 OK	31%
Rohn-L3 Rohn-LC22	24.067	0	49.783	0	42.95	0	49.783	4	0.875	40.6	162.4 OK	31%
Rohn-L3 Rohn-LC3P	0	0	0	0	0	63.24	63.24	4	0.875	40.6	162.4 OK	39%
Rohn-L3 Rohn-LC31	30.324	63.434	0	54.85	0	0	63.434	4	0.875	40.6	162.4 OK	36%
Rohn-L3 Rohn-LC32	30.504	0	63.369	0	54.666	0	63.369	4	0.875	40.6	162.4 OK	36%

37%	37%	44%	44%	44%	25%	25%	52%	28%	28%	28%	64%	64%	64%	71%	71%	71%	23%	23%	23%	%09	%09	%09	%99	%99	%99	72%	72%	72%	78%	78%	78%	84.10%	84.15%	84.12%	%29	%29	%29	71%	71%	710/
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212 OK 212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	318 OK	424 OK	424 OK	424 OK	424 OK	424 OK	424 OK
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77.52	77.73	92.759	92.927	92.978	109.448	109.722	109.749	123.139	123,351	123.389	136.363	136.571	136.575	149.74	149.932	150.057	168.17	168.362	168.332	189.868	190.015	190.001	209.98	210.148	210.117	229.354	229.543	229.392	248.08	248.247	248.154	267.443	267.604	267.513	284.562	284.715	284.634	299.567	299.715	200 638
77.52	0	92.759	0	0	109,448	0	0	123.139	0	0	136.363	0	0	149.74	0	0	168.17	0	0	189.868	0	0	209.98	0	0	229.354	0	0	248,08	0	0	267.443	0	0	284.562	0	0	299.567	0	_
00	67.135	0	0	80.246	0	0	94,858	0	0	106.676	0	0	118.124	0	0	129.869	0	0	145.689	0	0	164.565	0	0	182.002	0	0	198.799	0	0	215.082	0	0	231.962	0	0	246.827	0	0	250 887
0 67.265	0	0	80.358	0	0	94,994	0	0	106.809	0	0	118.283	0	0	129.956	0	0	145.923	0	0	164.79	0	0	182.269	0	0	199.142	0	0	215.39	0	0	232.272	0	0	247.133	0	0	260.19	c
00	77.73	0	0	92.978	0	0	109.749	0	0	123.389	0	0	136.575	0	0	150.057	0	0	168.332	0	0	190.001	0	0	210.117	0	0	229,392	0	0	248.154	0	0	267.513	0	0	284.634	0	0	200 638
0 77.728	0	0	92.927	0	0	109.722	0	0	123.351	0	0	136.571	0	0	149.932	0	0	168.362	0	0	190.015	0	0	210.148	0	0	229,543	0	0	248.247	0	0	267.604	0	0	284.715	0	0	299.715	_
0 37.384	37.645	0	44.646	44.968	0	53.182	53.493	0	59.91	60.236	0	66,505	808.99	0	73.271	73,691	0	82.359	82.64	0	93.387	93.698	0	103.297	103.599	0	113.159	113.365	0	122.383	122.655	0	132.224	132,51	0	140.643	140.949	0	148.151	118 160
Rohn-LD1P Rohn-LD11	Rohn-LD12	Rohn-LD2P	Rohn-LD21	Rohn-LD22	Rohn-LD3P	Rohn-LD31	Rohn-LD32	Rohn-LE1P	Rohn-LE11	Rohn-LE12	Rohn-LE2P	Rohn-LE21	Rohn-LE22	Rohn-LE3P	Rohn-LE31	Rohn-LE32	ohn-LF1P	Rohn-LF11	Rohn-LF12	Rohn-LF2P	Rohn-LF21	Rohn-LF22	Rohn-LG1P	Rohn-LG11	Rohn-LG12	Rohn-LG2P	Rohn-LG21	Rohn-LG22	Rohn-LH1P	Rohn-LH11	Rohn-LH12	Rohn-LH2P	Rohn-LH21	Rohn-LH22	ohn-LI1P	ohn-Ll11	Rohn-Li12	Rohn-LI2P	Rohn-L121	Col 1 100
Rohn-L4 Ro				Rohn-L4 Ro		Rohn-L4 R	Rohn-L4 Ro	Rohn-L5 Ro	Rohn-L5 R			Rohn-L6 Rohn-LF1P	Rohn-L6 R					Rohn-L7 R	Rohn-L7 R					Rohn-L7 R	Rohn-L7 R					Rohn-L8 Rohn-L11P	Rohn-L8 Rohn-Li11	Rohn-L8 R		Rohn-L8 R						

84%	Cap Percentage	%6 %6	14%	14%	20%	20%	27%	27%	26% 26%	26%	34%	35%	35%	43%	43%	40%	40%	40%	20%	20%	20%	%89	29%	29%
ed Tensile	ity 119.2 OK	119.2 OK 119.2 OK	119.2 OK 119.2 OK	119.2 OK	119.2 OK	119.2 OK 119.2 OK	119.2 OK	119.2 OK	162.4 OK	162.4 OK	162.4 OK	162.4 OK	162.4 OK 162.4 OK	162.4 OK	162.4 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK		212 OK
Bolt Tension Factored Tensile	Capacity Capacity LRFD 29.8	29.8 29.8	29.8 29.8	29.8	29.8	29.8 29.8	29.8	29.8	40.6	40.6	40.6	40.6	40.6	40.6	40.6	53	53	53	53	53	53	53	53	53
Boit	6.723 Capar 6.949 # Bolts Dia Bolt LRFD 0.924 4 0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.875	0.875	0.875	0.875	0.875	0.875	0.875	-	<b>э</b> т	T.	<del>.</del>	ਲ	-	-		
	Bolts 4	4 4	4 4	4 <	1 4	4 4	4	4	4 4	4	4	4	4 <	14	4	4	4	4	4	4	4	4	4	4
0.175 0.204 1.265 1.36 1.262 3.664 3.84 3.639 6.836	6.723 6.949 # 10.924	11.149	17.03	17.168	24.369	24.363	31.896	31.904	41.432	41.75	55.894	56.104	56.11	69.393	69.408	85.465	85.595	85,626	106.052	106.256	106.269	123.904	124.169	124.176
0.175 0 1.265 0 3.664 0 0 0 0 0 0	0 0 10.924	00	17.03 0	0 00 700	0	31,664	0	0	41.432	0	55.894	0	0	00	0	85.465	0	0	106.052	0	0	123.904	0 (	5
0 0.173 0.987 0.987 0 3.043	6.047	0 9.587	00	14.784	0	21.041	0	27.599	0 0	36.112	0	0	48.587	0	60.174	0	0	74.21	0	0	92.131	0	0	107.731
0 0 0 1.113 0 3.295 0	5.859	9.651 0	0 14.859	00	21.133	0 0	27.696	0	36.21	0	0	48.71	0 0	60.316	0	0	74.35	0	0	92.295	0	0	107.911	0
0.204 0.204 0.262 0.00 0.00 3.639	0 6.949 0	011.143	0 0	17.168	00	24.363	0	31.904	0 0	41.75	0	0	56.11	0	69,408	0	0	85.626	0	0	106.269	0	0	124.176
0 0 1.36 0 0 0 0 0	6.723	11.149	0 17.175	0	24.369	00	31,896	0	0 41 737	0	0	56,104	0	69.393	0	0	85.595	0	0	106.256	0	0	124.169	5
0 0 0 0 0.543 0.542 0.542 1.706	3.05	5.154 5.245	0 8.248	8.359	11,845	11.993	15.618	15.803	0 20 491	20.69	0	27.606	27.833	34.38	34.663	0	42.393	42.707	0	52.664	52.985	0	61.874	62.212
SNB-LA1P SNB-LA11 SNB-LA21 SNB-LA22 SNB-LA22 SNB-LA32 SNB-LA32 SNB-LA32 SNB-LA32	SNB-LA41 SNB-LA42 SNB-LB1P	SNB-LB11 SNB-LB12	SNB-LB2P SNB-1 B21	SNB-LB22	SNB-LB31	SNB-LB32	SNB-LB41	SNB-LB42	SNB-LC1P	SNB-LC12	SNB-LC2P	SNB-LC21	SNB-LC22	SNB-LC31	SNB-LC32	SNB-LD1P	SNB-LD11	SNB-LD12	SNB-LD2P	SNB-LD21	SNB-LD22	SNB-LD3P	SNB-LD31	SNB-LD32
SNB-L1 SN	SNB-L1 SNB-L1 SNB-L2	SNB-L2 SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L2	SNB-L3	SNB-L3	SNB-L3	SNB-L3	SNB-L3	SNB-L3	SNB-L3	SNB-L3	SNB-L3

%69	%69	%69	81%	81%	81%	%06	%06	%06	%89	%89	%89	%//	41%	41%	%98	%98	%98	%09.96	%29.96	%59.96	106%	106%	106%	116%	116%	116%	%36	95%	95%	103%	103%	103%	
212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	212 OK	318 No Good - Replace Bolt	424 OK	424 OK	424 OK	424 No Good - Replace Bolt	424 No Good - Replace Bolt	424 No Good - Replace Bolt																		
53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	
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4	4	4	4	4	4	4	4	4	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	9	œ	80	∞	∞	80	ø	
145.588	145.812	145.844	171.097	171.323	171.33	190.836	191.056	191.009	215.579	215.797	215.746	244.856	245.079	245.003	274.497	274.712	274.634	307.203	307.405	307.342	337.988	338,182	338.122	369.807	369.997	369.928	402.128	402.309	402.24	438.404	438.578	438.51	
145.588	0	0	171.097	0	0	190.836	0	0	215.579	0	0	244.856	0	0	274.497	0	0	307.203	0	0	337.988	0	0	369.807	0	0	402,128	0	0	438.404	0	0	
0	0	126.519	0	0	148.663	0	0	165.844	0	0	187,229	0	0	212,733	0	0	238.469	0	0	267.003	0	0	293.733	0	0	321.51	0	0	349.63	0	0	381.346	
0	126.699	0	0	148.884	0	0	166.104	0	0	187.515	0	0	213.056	0	0	238.804	0	0	267.358	0	0	294.091	0	0	321.885	0	0	350.012	0	0	381.735	0	
0	0	145.844	0	0	171.33	0	0	191.009	0	0	215.746	0	0	245.003	0	0	274,634	0	0	307.342	0	0	338.122	0	0	369.928	0	0	402.24	0	0	438.51	
0	145.812	0	0	171.323	0	0	191.056	0	0	215.797	0	0	245.079	0	0	274.712	0	0	307.405	0	0	338.182	0	0	369.997	0	0	402,309	0	0	438.578	0	
0	72.584	72.966	0	85.41	85.809	0	95.634	95.978	0	107.641	108.006	0	122.568	122.933	0	137.317	137.685	0	154.035	154.464	0	169.299	169.739	0	185.64	186.092	0	201.804	202.272	0	220.514	221.001	
SNB-LE1P	SNB-LE11	SNB-LE12	SNB-LE2P	SNB-LE21	SNB-LE22	SNB-LE3P	SNB-LE31	SNB-LE32	SNB-LF1P	SNB-LF11	SNB-LF12	SNB-LF2P	SNB-LF21	SNB-LF22	SNB-LG1P	SNB-LG11	SNB-LG12	SNB-LG2P	SNB-LG21	SNB-LG22	SNB-LH1P	SNB-LH11	SNB-LH12	SNB-LH2P	SNB-LH21	SNB-LH22	SNB-LI1P	SNB-LI11	SNB-LI12	SNB-LI2P	SNB-LI21	SNB-LI22	
SNB-L4			SNB-L4	SNB-L4	SNB-L4	SNB-L4	SNB-L4		SNB-L4	SNB-L4	SNB-L4	SNB-L4	SNB-L4		SNB-L5	SNB-L5	SNB-L5	SNB-L5	SNB-L5		SNB-L5	SNB-L5	SNB-L5	SNB-L5	SNB-L5	SNB-L5	SNB-L6	SNB-L6	SNB-L6	SNB-L6	SNB-L6	SNB-L6	

Bolt
A490
with
Bolts
A325
Existing
Replaced

		Cap Percentage	85%	85%	82%	%86	%86	%66	75%	%92	75%	82%	82%	82%
	Factored Tensile	ity	399.6 OK	532.8 OK	532.8 OK	532.8 OK	532.8 OK	532.8 OK	532.8 OK					
Bolt Tension	Sapacity Factor	Capacity	9.99	9.99	9.99	9.99	9.99	9.99	9.99	9-99	9.99	9.99	9.99	9.99
Bolt	Cap	# Bolts Dia Bolt LRFD			-	•	•	-	-	•	-	÷		-
		3olts Dia	9	9	9	9	9	9	80	80	œ	00	89	œ
		#	337.988	338.182	338.122	369.807	369.997	369.928	402.128	402.309	402.24	438.404	438,578	438.51
			337.988	0	0	369.807	0	0	402.128	0	0	438.404	0	0
			0	0	293.733	0	0	321.51	0	0	349.63	0	0	381.346
			0	294.091	0	0	321.885	0	0	350.012	0	0	381.735	0
490 Bolts			0	0	338.122	0	0	369.928	0	0	402,24	0	0	438.51
ts with A			0	338.182	0	0	369.997	0	0	402.309	0	0	438.578	0
A325 Bol			0	169.299	169.739	0	185.64	186.092	0	201.804	202.272	0	220.514	221.001
Replaced Existing A325 Bolts with A490 Bolts		3	SNB-LH1P	SNB-LH11	SNB-LH12	SNB-LH2P	SNB-LH21	SNB-L5 SNB-LH22 186.092	SNB-L6 SNB-L11P	SNB-L6 SNB-L111	SNB-L6 SNB-Li12	SNB-L6 SNB-LI2P	SNB-L(21	SNB-L6 SNB-L122
Replace			SNB-L5		SNB-L5	SNB-L5	SNB-L5	SNB-L5	SNB-L6	SNB-L6	SNB-L6	SNB-L6	SNB-L6	SNB-L6

CONNECTION BETWEEN TOWERS EVALUATION

Δ	-	-	A	A
A	C	u	//	И

Job Description

			Page	OT
180' ROHN SSV Tower w/ SNB Reinf Greenwich	Project No.	Revision 4	Sheet	of
Tower to Tower Connection Force	Computed by	MCD	_ Date	07/31/19
TIA-222-G All Load Cases and with Ice Forces	_Checked by _		Date	

# SUMMARY OF CONNECTION FORCES FOR ALL WIND ANGLES AND LOAD COMBINATIONS

Loads Without Ice (V.asd wind Speed = 101 MPH)

Wind Angle	Force @ "C	
0 Deg	7.1481	
+60 Deg	5.5872	kips
-60 Deg	5.5922	
+90 Deg	6.0271	kips
-90 Deg	6.0291	kips

Loads With Design Ice 2.25 inch ("V" wind Speed = 50 MPH)

Wind Angle	Force @ "C	
0 Deg	8.9903	
+60 Deg	8.1373	
-60 Deg	8.1383	
+90 Deg	8.6773	
-90 Deg	8.6823	kips



Job

180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Tower Connection - TIA-222-G Loads on Conection Computed by

Checked by

Page

**Bolt Diameter** 

$$Dia_{bolt} := \frac{3}{4}in$$

**Bolt Shear Capacity** 

Capacitybolt := 6.64kip

Per AISC 15th Edition p. 7-24 for 3/4" A325 slip critical bolt

(Considered as Long Slotted Hole) - LRFD

Shear Plane Area

Area<sub>plate</sub> := 
$$\frac{3}{8}$$
in· $\left(\frac{3}{4}$ in + 1in $\right)$ 

 $Area_{plate} = 0.6563 in^2$ 

Yield Strength of Plate

$$Fy_{plate} := 36ksi$$

$$\phi := 1.0$$

 $\varphi := \ 1.0 \hspace{1cm} \text{LRFD Reduction Factor - AISC Chapter J}$ 

Plate Capacity

$$Capacity_{plate} := 0.6Area_{plate} \cdot Fy_{plate} \cdot \phi$$

 $Capacity_{plate} = 14.175 kip$ 

**U-Bolt Size** 

$$Dia_{ubolt} := \frac{1}{2}in$$

U-Bolt Area

$$Area_{ubolt} := 2 \cdot \pi \left( \frac{Dia_{ubolt}}{2} \right)^2$$

$$Area_{ubolt} = 0.3927 in^2$$

 $Fy_{ubolt} := 58ksi$ 

ф.:= 0.75

LRFD Reduction Factor - AISC Chapter J

 $Capacity_{ubolt} := (0.75Area_{ubolt} \cdot Fy_{ubolt}) \cdot \phi \qquad Capacity_{ubolt} = 12.8118kip$ 

Connection Capacity

 $Capacity_{connection} := \min \! \! \left( \text{Capacity}_{bolt}, \text{Capacity}_{plate}, \text{Capacity}_{ubolt} \right)$ 

Capacity<sub>connection</sub> = 6.64 kip

Max Connection Spacing

Spacing := 5ft

Connection Capacity per Foot

$$Capacity_{LF} := \frac{Capacity_{connection}}{Spacing}$$

Capacity<sub>LF</sub> =  $1.328 \frac{\text{kip}}{\Omega}$ 

Max Connection Force (Tension):

$$F_{\text{max}} := 8.9903 \text{kip}$$

NOTE: Force obtained from TIA-222-G Load Combination #3

(PLS-TOWER program)

Connection Spacing in PLS-Tower

Spacing<sub>PLS</sub>.Tower := 10ft

Connection Force per Foot

$$\mathsf{Force}_{LF} \coloneqq \frac{\mathsf{F}_{max}}{\mathsf{Spacing}_{PLS.Tower}}$$

 $Force_{LF} = 0.899 \cdot kip$ 

Percent Capacity

$$Percent_{capacity} := \frac{Force_{LF}}{Capacity_{LF}}$$

 $Percent_{capacity} = 67.7.\%$ 

#### **FOUNDATION EVALUATION**



	A V X			rage	· ·
Job	180' ROHN SSV Tower w/ SNB Reinf Greenwich	Project No.	Revision 4	Sheet	of
	Overturning Moment Calculation	Computed by	MCD	Date	07/31/19
Description	TIA-222-G Load Case #2	Checked by		Date	

From PLS-Tower Output Summary

Summary of Joint Support Reactions For All Load Cases:

	Load Case	Joint Label	Long. Force (kips)	Tran. Force (kips)	Vert. Force (kips)	Shear Force (kips)	Tran. Moment (ft-k)	Long. Moment (ft-k)	Vert. Moment (ft-k)	Bending Moment (ft-k)	Found. Usage %
	0.000 : 4.00- : 4.600	RohnJP	-0.64	3.89	14.64	3.95	-0.36	-0.21	0.01	0.42	0
"-90"	2: 0.9D + 1.0Dg + 1.6Wo	SNB-JP	-0.26	6.4	13.63				0.05	0.74	0
	2: 0.9D + 1.0Dg + 1.6Wo		10.99	22.09	295.57			2.44	0.01	4.61	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ1	-10.29	20.94	-265.94			-2.04	0.02	4.23	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ2	18.56	38.53	426.37					11.24	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J1	-18.3	38.08	-398.37						0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J2	-14.32	3.35	175.32			-2.73		2.74	0
"-60"	2: 0.9D + 1.0Dg + 1.6Wo	RohnJP	-24.45	5.46	249.58	-				6.63	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-JP	4.76	13.82	175.56					2.74	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ1	-13.59	22.96	-306.61					4.87	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ2	7.53	23.93	249.98					6.64	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J1	-24.08	41.7	-457.94					12.16	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J2	-24.00	0.11	347.71					5.45	0
"0"	2: 0.9D + 1.0Dg + 1.6Wo	RohnJP	-50.83	0.11	503.36					13.3	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-JP	-9.58		-151.56					2.44	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ1	-9.78		-151.89					2.46	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ2	-17.53	-18.77	-230.61					6.14	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J1 SNB-J2	-17.55		-231.11					6.16	0
	2: 0.9D + 1.0Dg + 1.6Wo		-17.35		175.73				-0.02	2.74	0
"60"	2: 0.9D + 1.0Dg + 1.6Wo	RohnJP	-14.33		250.14					6.64	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-JP RohnJ1	-24,43		-306.69				-0.01	4.86	0
	2: 0.9D + 1.0Dg + 1.6Wo		4.66		175.23				-0.01	2.73	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ2	-24.08		-458.01					12.16	0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J1 SNB-J2	7.51	-23.9	249.49					6.63	0
	2: 0.9D + 1.0Dg + 1.6Wo		-0.67		15.12					0.42	0
"90"	2: 0.9D + 1.0Dg + 1.6Wo	RohnJP SNB-JP	-0.3				-0.65			0.75	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ1	-10.3		-266.25					4.23	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJ2	10.98		295.4				-0.01	4.61	0
	2: 0.9D + 1.0Dg + 1.6Wo		-18.31	-38.1	-398.77					10.6	Y2 0
	2: 0.9D + 1.0Dg + 1.6Wo	SNB-J1 SNB-J2	18.55		426.13					11.24	0
	2: 0.9D + 1.0Dg + 1.6Wo	RohnJP	-0.8						0	0.21	0
"0.9*DL"	0.9DL	SNB-JP	-0.41		13.89				0	0.36	0
	0.9DL		0.4						0	0.21	0
	0.9DL	RohnJ1 RohnJ2	0.4						0	0,21	0
	0.9DL	SNB-J1	0.4						0	0.35	0
	0.9DL		0.21	-0.36						0.36	0
	0.9DL	SNB-J2	0.21	-0.50	13.70	. J. 71	2.01				



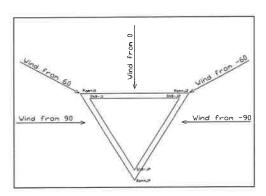
Job 180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Revision 4 Sheet of Description Overturning Moment Calculation Computed by MCD Date 07/31/19

TIA-222-G Load Case #2 Checked by Date

Load Case	Joint	Vert,	Leg		Total	Shear	Total
	Label	Tower	Moment	Moment	Moment		Shear
		Forces (k)	Arm (ft)	(ft-k)	(ft-k)	(k)	(k)
-90 deg	RohnJP	-0.28	0.00	0.00		3.95	
-90 deg	SNB-JP	-0.26	0.00			6.41	
-90 deg	RohnJ1	280.8	11.42		14183.0	24.67	143.4
-90 deg	RohnJ2	-280.78	-11.42	3206.51	14100.0	23.33	140.4
-90 deg	SNB-J1	412.66	9.42			42.77	
-90 deg	SNB-J2	-412.15	-9.42	3882.45		42.25	
-60 deg	RohnJP	160.4	6.60	1058.64		14.71	
-60 deg	SNB-JP	235.69	5.44	1282.15		25.05	
-60 deg	RohnJ1	160.79	6.60	1061.21	14056.3	14.61	154.3
-60 deg	RohnJ2	-321.45	-13.18	4236.71	14000.5	26.68	154.3
-60 deg	SNB-J1	236.27	5.44			25.09	
-60 deg	SNB-J2	-471.72	-10.88	5132.31		48.16	
0 deg	RohnJP	332.79	13.18	4386.17		29.23	159.5
0 deg	SNB-JP	489.47	10.88	5325.43	l	50.83	
0 deg	RohnJ1	-166.33	-6.60	1097.78	14571.1	13.99	
0 deg	RohnJ2	-166.73	-6.60	1100.42	1457 1.1	14.07	
0 deg	SNB-J1	-244.32	-5.44	1329.10	]	25.69	
0 deg	SNB-J2	-244.89	-5.44	1332.20		25.72	
+60 deg	RohnJP	160.81	6.60	1061.35		14.71	
+60 deg	SNB-JP	236.25	5.44	1285.20		25.09	
+60 deg	RohnJ1	-321.46	-13.18	4236.84	14056.5	26.68	154.3
+60 deg	RohnJ2	160.39	6.60	1058.57	14050.5	14.61	104.3
+60 deg	SNB-J1	-471.72	-10.88	5132.31		48.16	
+60 deg	SNB-J2	235.71	5.44	1282.26		25.05	
+90 deg	RohnJP	0.2	0.00	0.00		3.95	
+90 deg	SNB-JP	0.37	0.00	0.00		6.41	
+90 deg	RohnJ1	-281.02	-11.42	3209.25	14183.1	23.34	143.4
+90 deg	RohnJ2	280.56	11.42	3204.00	14 183.1	24.66	143.4
+90 deg	SNB-J1	-412.48	-9.42	3885.56		42.27	
+90 deg	SNB-J2	412.35		3884.34		42.75	

Forces taken from PLS-Tower output with 0.9\*DL Only load case subtracted from Vertical Tower Forces

Dimensions taken from CAD drawing





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lab	180' ROHN SSV Tower w/ SNB Reinf Greenwich	Project No.	Revision 4	Sheet	of
Job	Overturning Moment Calculation	Computed by	MCD	Date	07/31/19
Description		Checked by		Date	
	TIA-222-G Load Case #3	Officered by			

From PLS-Tower Output Summary

Summary of Joint Support Reactions For All Load Cases:

	Load Case	Joint Label	Long. Force (kips)	Tran. Force (kips)	Vert. Force (kips)		Shear Force (kips)	Tran. Moment (ft-k)	Long. Moment (ft-k)	Vert. Moment (ft-k)	Bending Moment (ft-k)	
	3: 1,2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJP	-1.09	1.54		188.79	1.88	0.03	1.15	0.01	1.15	0
"-90"	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-JP	2.4	2.16		218.94		0.44	3.46	0,02	3.49	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ1	4.68	9.53		294.91	10.62	-0.37	0.28	0	0.46	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ2	-3.59	7.64		82.38	8.44	-2.38	-1.4	0	2.76	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J1	5.44	11.56		372.08	12.78	-0.31	0.47	-0.01	0.56	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J2	-7.84	15.73		65.45	17.57	-6.35	-3.89	-0.01	7.45	0
"-60"	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJP	-6.57	1.32		250.15	6.7	0.05	0.22	0.01	0.23	0
-60	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-JP	-6.32	1.86		307.44	6.59	0.41	1.17	0.02	1.24	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ1	2.19	6.32		249.93	6.69	0.23	-0.05	0	0.24	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ2	-4.95	8.53		66	9.86	-2.6	-1.51	0	3	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J1	1.56	6.4		307.18	6.59	1.22		-0.02	1.25	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J2	-9.92	17.19		41.85	19.85	-6.98	-4.03	0		0
"0"	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJP	-12.28	-0.01		313.75	12.28	0	-0.73	0	0.73	0
U	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-JP	-15.27	0		398.14	15.27	0	-1.19	0	1.19	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ1	-3.35	-3.15		127.28	4.6	1.82		0	2.08	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ2	-3,33	3.16		127,4	4.59	-1.82		0	2.08	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J1	-7.28	-8.83		129.15	11.44	5.18	-2.58	-0.01	5.79	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J2	-7.28	8.83		129.26	11.44	-5.18	-2.57	0.01	5.79	0
"60"	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJP	-6.57	-1.33		250.22	6.7	-0.05	0.22	-0.01	0.23	0
00	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-JP	-6.33	-1.86		307.54	6.59	-0.41	1.17	-0.02	1.24	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ1	-4.96	-8.52		65.81	9.86	2.59	-1.52	0	3	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ2	2.19	-6.31		250.05	6.68	-0.23	-0.04	0	0.24	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J1	-9.93	-17.19		41.64	19.85	6.98	-4.03	0	8.06	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J2	1.56	-6.4		307.29	6.58	-1.23	-0.23	0.01	1.25	0
"90"	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJP	-1.09	-1.53		188.88	1.88	-0.04	1.15	-0.01	1.15	0 0
00	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-JP	2.4	-2.16		219.05	3.22	-0.44	3.46	-0.02	3.49	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ1	-3.59	-7.65		82.15	8.45	2.38	-1.4	0	2.76	
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	RohnJ2	4.68	-9.53		295.06	10.62	0.36	0.28	0	0.46	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J1	-7.85	-15.73		65.18	17.58	6.35	-3.9	0.01	7.45	0
	3: 1.2D + 1.0Dg + 1.0 Di + 1.0 Wi + 1.0 Ti	SNB-J2	5.44	-11.56		372.23	12.78	0.31	0.47	0.01	0.56	0
"1.2*DL"	1.2*DL	RohnJP	-2.09	0		30.92		0	-0.35	0	0.35	0
	1.2*DL	SNB-JP	-0.06	0		18.69	0.06	0		0	0.67 0.34	0
	1.2*DL	RohnJ1	1.05	1.81		30.73		-0.3	0.17	0		0
	1.2*DL	RohnJ2	1.05	-1.81		30.92		0.3	0.17	0	0:35 0.67	0
	1.2*DL	SNB-J1	0.03	0.05		18.46	0.06	-0.58	0.33	0	0.67	0
	1.2*DL	SNB-J2	0.03	-0.05		18.66	0.06	0.58	0.34	U	0.07	U



 Job
 180° ROHN SSV Tower w/ SNB Reinf. - Greenwich
 Project No.
 Revision 4
 Sheet
 of

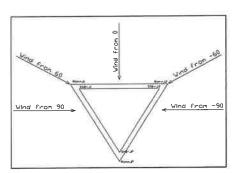
 Description
 Overturning Moment Calculation
 Computed by MCD
 Date
 07/31/19

 TIA-222-G Load Case #3
 Checked by
 Date

Load Case	Joint	Vert.	Leg		Total	Shear	Total
25	Label	Tower	Moment	Moment	Moment		Shear
		Forces (k)	Arm (ft)	(ft-k)	(ft-k)	(k)	(k)
-90 deg	RohnJP	157.87	0.00			1.88	
-90 deg	SNB-JP	200.25				3.23	
-90 deg	RohnJ1	264.18			5319.6	10.62	54.5
-90 deg	RohnJ2	51.46				8.44	01.0
-90 deg	SNB-J1	353.62	9.42			12.78	
-90 deg	SNB-J2	46.79		-440.76		17.57	
-60 deg	RohnJP	219.23				6.70	
-60 deg	SNB-JP	288.75				6.59	56.3
-60 deg	RohnJ1	219.2			5320.4	6.69	
-60 deg	RohnJ2	35.08				9.86	
-60 deg	SNB-J1	288.72	5.44			6.59	
-60 deg	SNB-J2	23.19	-10.88	-252.31		19.85	
0 deg	RohnJP	282.83	13.18	3727.70		12.28	59.6
0 deg	SNB-JP	379.45	10.88			15.27	
0 deg	RohnJ1	96.55			5378.3	4.60	
0 deg	RohnJ2	96.48				4.59	
0 deg	SNB-J1	110.69				11.44	
0 deg	SNB-J2	110.6				11.44	
+60 deg	RohnJP	219.3				6.70	
+60 deg	SNB-JP	288.85				6.59	
+60 deg	RohnJ1	35.08	-13.18			9.86	56.3
+60 deg	RohnJ2	219.13	6.60	1446.26	3320.0	6.68	50.5
+60 deg	SNB-J1	23.18	-10.88			19.85	
+60 deg	SNB-J2	288.63	5.44	1570.15		6.58	
+90 deg	RohnJP	157.96	0.00	0.00		1.88	
+90 deg	SNB-JP	200.36				3.22	
+90 deg	RohnJ1	51.42	-11.42		5319.8	8.45	54.5
+90 deg	RohnJ2	264.14	11.42	3016.48	0.519.0	10.62	
+90 deg	SNB-J1	46.72	-9.42			17.58	
+90 deg	SNB-J2	353.57	9.42	3330.63	1	12.78	

Forces taken from PLS-Tower output with 1.2\*DL Only load case subtracted from Vertical Tower Forces

Dimensions taken from CAD drawing



Job	
Description	

И			Page	of
180' ROHN SSV Tower w/ SNB Reinf, - Greenwich	Project No.	Revision 4	Sheet	of
Overturning Moment Calculation	Computed by	MCD	Date	07/31/19
TIA-222-G Load Case #4	Checked by		Date	

From PLS-Tower Output Summary

Summary of Joint Support Reactions For All Load Cases:

	Load Case	Joint Label	Long Force (kips)	Tran. Force (kips)	Vert. Force (kips)	3	Shear Force (kips)	Tran. Moment (ft-k)	Long. Moment (ft-k)	Vert. Moment (ft-k)	Bending Moment (ft-k)	
"-90"	4: 1.2D + 1.0Dg + 1.0E	RohnJP	-1.07	0.1		19.89	1.07	0.04	-0.28	0	0.28	0
~-90 <sup>~</sup>	4: 1.2D + 1.0Dg + 1.0E	SNB-JP	-0.55			18.52	0.57	0.18	-0.48	0.01	0.51	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ1	1.14			38.37	2.32	-0.43	0.29	0	0.52	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ2	-0.07	0.19		1.1	0.2	0.04	-0.01	0	0.04	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J1	1.29			44.84	2.7	-0.89	0.62	0	1.08	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J2	-0.74			-8.19	1.61	-0.07	-0.14	0	0.15	0
"-60"	4: 1.2D + 1.0Dg + 1.0E	RohnJP	-1.79			30.67	1.79	0.04	-0.42	0	0.42	0
-00	4: 1.2D + 1.0Dg + 1.0E	SNB-JP	-1.79			33.86	1.8	0.15	-0.82	0,01	0.84	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ1	0.84			30.47	1.79	-0.33	0.25	0	0.42	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ2	-0.21	0.33		-1.79	0.39	0	-0.01	0	0.01	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J1	0.79	1.61		33.62	1.79	-0.63	0.55	-0.01	0.84	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J2	-0.97	1.68		-12.3	1.94	-0.19	-0.11	0	0.22	0
"O"	4: 1.2D + 1.0Dg + 1.0E	RohnJP	-2.52	0		41.46	2.52	0	-0.56	0	0.56	0
U	4: 1.2D + 1.0Dg + 1.0E	SNB-JP	-3.04			49.2	3.04	0	<i>-</i> 1.17	0	1.17	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ1	0.11	0.32		8.9	0.34	-0.09	0.11	0	0.14	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ2	0.1	-0.33		8.99	0.34	0.1	0.1	0	0.14	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J1	-0.46	-0.54		2.94	0.71	-0.03	0.2			0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J2	-0.45	0.54		3.04	0.71	0.03	0.2	0.01	0.2	0
"60"	4: 1.2D + 1.0Dg + 1.0E	RohnJP	-1.79	-0.08		30.67	1.79	-0.04	-0.42	0	0.42	0
00	4: 1.2D + 1.0Dg + 1.0E	SNB-JP	-1.79	-0.12		33.86	1.8	-0.16	-0.82	-0.01	0.84	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ1	-0.21	-0.34		-1.89	0.39	0	-0.01	0	0.01	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ2	0.84	-1.58		30.56	1.79	0.33	0.25	0	0.42	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J1	-0.97	-1.68		-12.4	1.94		-0.11	0	0.22	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J2	0.79	-1.61		33.72	1.8	0.63	0.55	0.01	0.84	0
"90"	4: 1.2D + 1.0Dg + 1.0E	RohnJP	-1.07	-0.1		19.89	1.07	-0.04	-0.28	0	0.28	0
50	4: 1.2D + 1.0Dg + 1.0E	SNB-JP	-0.55	-0.14		18.52	0.57	-0.18	-0.48	-0.01	0.51	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ1	-0.07	-0.19		1	0.2	-0.04	-0.01	0	0.04	0
	4: 1.2D + 1.0Dg + 1.0E	RohnJ2	1.14	-2.02		38.46	2.32		0.29	0	0.52	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J1	-0.74	-1.43		-8.29	1.61	0.07	-0.14	0	0.16	0
	4: 1.2D + 1.0Dg + 1.0E	SNB-J2	1.29	-2.37		44.95	2.7	0.89	0.62	0	1.08	0
"1.2*DL"	1.2*DL	RohnJP	-1.07	0		19.88	1.07	0	-0.28	0	0.28	0
1.2 DL	1.2*DL	SNB-JP	-0.55	0		18.52	0.55	0	-0.48	0	0.48	0
	1.2*DL	RohnJ1	0.53	0.92		19.69	1.06	-0.24	0.14	0	0.27	0
	1.2*DL	RohnJ2	0.53	-0.92		19.78	1.06	0.24	0.14	0	0.27	0
	1.2*DL	SNB-J1	0.27	0.47		18.28	0.55	-0.41	0.24	0	0.47	0
	1.2*DL	SNB-J2	0.28	-0.47		18.38	0.55	0.41	0.24	0	0.47	0



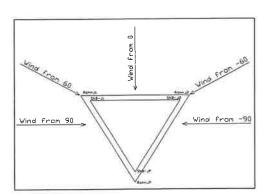
Job 180' ROHN SSV Tower w/ SNB Reinf, - Greenwich Project No. Revision 4 Sheet of
Description Overturning Moment Calculation Computed by MCD Date 07/31/19

TIA-222-G Load Case #4 Checked by Date

Load Case	Joint	Vert.	Leg		Total	Shear	Total
	Label	Tower	Moment	Moment	Moment		Shear
		Forces (k)	Arm (ft)	(ft-k)	(ft-k)	.(k)	(k)
-90 deg	RohnJP	0.01	0.00			1.07	
-90 deg	SNB-JP	0	0.00	0.00		0.57	
90 deg	RohnJ1	18.68	11.42	213.33	927.1	2.32	8.5
90 deg	RohnJ2	-18.68	-11.42	213.33	327	0.20	0.0
90 deg	SNB-J1	26.56	9.42	250.20		2.70	
90 deg	SNB-J2	-26.57	-9.42	250.29		1.61	
-60 deg	RohnJP	10.79	6.60	71.21		1.79	
60 deg	SNB-JP	15.34	5.44	83.45		1.80	
60 deg	RohnJ1	10.78	6.60	71.15	927.4	1.79	9.5
60 deg	RohnJ2	-21.57	-13.18		321.4	0.39	0.0
60 deg	SNB-J1	15.34	5.44	83.45		1.79	
60 deg	SNB-J2	-30.68	-10.88	333.80		1.94	
) deg	RohnJP	21.58	13.18	284.42		2.52	
) deg	SNB-JP	30.68	10.88	333.80		3.04	7,7
) deg	RohnJ1	-10.79	-6.60	71.21	927.6	0.34	
) deg	RohnJ2	-10.79	-6.60	71.21	921.0	0.34	
O deg	SNB-J1	-15.34	-5.44	83.45		0.71	
O deg	SNB-J2	-15.34	-5.44	83.45		0.71	
+60 deg	RohnJP	10.79	6.60	71.21		1.79	
+60 deg	SNB-JP	15.34	5.44	83.45		1.80	
+60 deg	RohnJ1	-21.58	-13.18		927.5	0.39	9.5
+60 deg	RohnJ2	10.78	6.60	71.15	921.5	1.79	3.0
+60 deg	SNB-J1	-30.68	-10.88			1.94	
+60 deg	SNB-J2	15.34	5.44	83.45		1.80	
+90 deg	RohnJP	0.01	0.00	0.00		1.07	
+90 deg	SNB-JP	0	0.00			0.57	
+90 deg	RohnJ1	-18.69	-11.42		927.3	0.20	8.5
+90 deg	RohnJ2	18.68	11.42		921.3	2.32	0.0
+90 deg	SNB-J1	-26.57	-9.42			1.61	
+90 dea	SNB-J2	26.57	9.42	250.29	l	2.70	

Forces taken from PLS-Tower output with 1.2\*DL Only load case subtracted from Vertical Tower Forces

Dimensions taken from CAD drawing



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Job	180' ROHN SSV Tower w/ SNB Reinf, - Greenwich	Project No.	Revision 4	Sheet	of
Description	Overturning Moment Calculation	Computed by	MCD	Date	07/31/19
	TIA-222-G Load Case #5	Checked by		Date	

From PLS-Tower Output Summary

Summary of Joint Support Reactions For All Load Cases:

	Load Case	Joint Label	Long. Force (kips)	Tran. Force (kips)	Vert. Force (kips)		Shear Force (kips)	Tran. Moment (ft-k)	Long. Moment (ft-k)	Vert. Moment (ft-k)	Bending Moment (ft-k)	
" 00"	5.0.0D + 1.0D  + 1.0E	RohnJP	-0.8	0.1		14.92	0.81	0.04	-0.21	0	0.21	0
"-90"	5: 0.9D + 1.0Dg + 1.0E	SNB-JP	-0.41	0.15		13.89	0.44		-0.36	0.01	0.4	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ1	1	1.79		33.42	2,06	-0.37	0.25	0	0.45	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ2	-0.21	0.41		-3.82	0.46	-0.02	-0.04	0	0.05	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J1	1.22			40.24	2.57	-0.78	0.56	0	0.96	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J2	-0.81	1.55		-12.75	1.75	-0.17	-0.2	0	0.26	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJP	-1.53			25.69	1,53	0.03	-0.35	0	0.35	0
"-60"	5: 0.9D + 1.0Dg + 1.0E	SNB-JP	-1.66			29.21	1.66	0.15	-0.7	0.01	0.72	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ1	0.71	1.35		25.54	1.52	-0.27	0.22	0	0.35	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ2	-0.34			-6.7	0.66	-0.06	-0.04	0	0.07	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J1	0.72			29.02	1.66	-0.53	0.49	-0.01	0.72	0
	5: 0.9D + 1.0Dg + 1.0E 5: 0.9D + 1.0Dg + 1.0E	SNB-J2	-1.04			-16.85	2.08	-0.3	-0.17	0	0.34	0
"0"	5: 0.9D + 1.0Dg + 1.0E 5: 0.9D + 1.0Dg + 1.0E	RohnJP	-2.25			36.46	2.25	0	-0.49	0	0.49	0
.0	5: 0.9D + 1.0Dg + 1.0E	SNB-JP	-2.9			44.53	2.9	0	-1.05	0	1.05	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ1	-0.03			4	0.1	-0.04	0.07	0	0.08	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ2	-0.03			4.06	0.1	0.04	0.07	0	0.08	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J1	-0.52			-1.61	0.84	0.07	0.14	-0.01	0.15	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J2	-0.52			-1.54	0.84	-0.07	0.14	0.01	0.16	0
"60"	5: 0.9D + 1.0Dg + 1.0E	RohnJP	-1.53			25.69	1.53	-0.04	-0.35	0	0.35	0
00	5: 0.9D + 1.0Dg + 1.0E	SNB-JP	-1.66			29.21	1.66	-0.16	-0.7	-0.01	0.72	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ1	-0.34			-6.77	0.66	0.06	-0.04	0	0.07	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ2	0.71	-1.35		25.6	1.53	0.27	0.22	0	0.35	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J1	-1.04	-1.8		-16.93	2.08	0.3	-0.17	0	0.34	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J2	0.72			29.1	1.66	0.53	0.49	0.01	0.72	0
"90"	5: 0.9D + 1.0Dg + 1.0E	RohnJP	-0.8	-0.1		14.92	0.81	-0.04	-0.21	0	0.21	0
30	5: 0.9D + 1.0Dg + 1.0E	SNB-JP	-0.41	-0.14		13.89	0.44	-0.18	-0.36	-0.01	0.4	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ1	-0.21	-0.42		-3.89	0.46	0.02	-0.05	0	0.05	0
	5: 0.9D + 1.0Dg + 1.0E	RohnJ2	1.01	-1.8		33.49	2.06	0.37	0.25	0	0.45	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J1	-0.81	-1.55		-12.83	1.75	0.17	-0.2	0	0.26	0
	5: 0.9D + 1.0Dg + 1.0E	SNB-J2	1.22	-2.26		40.31	2.57	0.78	0.56	0	0.96	0
"0.9*DL"	0.9DL	RohnJP	-0.8	0		14.92	0.8	0	-0.21	0	0.21	0
0.5 DL	0.9DL	SNB-JP	-0.41	0		13.89	0.41	0	-0.36	0	0.36	0
	0.9DL	RohnJ1	0.4	0.69		14.77	0.8	-0.18	0.1	0	0.21	0
	0.9DL	RohnJ2	0.4	-0.69		14.84	8.0	0.18	0.1	0	0.21	0
	0.9DL	SNB-J1	0.21	0.35		13.71	0.41	-0.31	0.18	0	0.35	0
	0.9DL	SNB-J2	0.21	-0.36		13.78	0.41	0.31	0.18	0	0.36	0

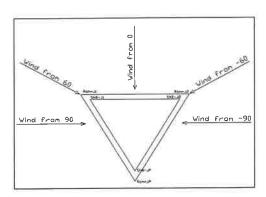


Job 180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Revision 4 Sheet of
Description Overturning Moment Calculation Computed by MCD Date 07/31/19
TIA-222-G Load Case #5 Checked by Date

Load Case	Joint	Vert.	Leg		Total	Shear	Total
	Label	Tower	Moment	Moment	Moment		Shear
		Forces (k)	Arm (ft)	(ft-k)	(ft-k)	(k)	(k)
-90 deg	RohnJP	0	0.00	0.00		0.81	
-90 deg	SNB-JP	0	0.00			0.44	
-90 deg	RohnJ1	18.65			925.9	2,06	8.1
-90 deg	RohnJ2	-18.66			020.0	0.46	0.,
-90 deg	SNB-J1	26.53				2.57	
-90 deg	SNB-J2	-26.53				1.75	
-60 deg	RohnJP	10,77	6.60			1.53	
-60 deg	SNB-JP	15.32	5.44	83.34		1.66	
-60 deg	RohnJ1	10.77	6.60	71.08	925.9	1.52	9.1
-60 deg	RohnJ2	-21.54	-13.18	283.90	325.5	0.66	J.,
-60 deg	SNB-J1	15.31	5.44			1.66	
-60 deg	SNB-J2	-30.63	-10.88	333.25		2.08	
0 deg	RohnJP	21.54	13.18	283.90		2.25	
0 deg	SNB-JP	30.64	10.88	333.36		2.90	7.0
0 deg	RohnJ1	-10.77	-6.60	71.08	926.2	0.10	
0 deg	RohnJ2	-10.78	-6.60	71.15	920.2	0.10	
0 deg	SNB-J1	-15.32	-5.44			0.84	
0 deg	SNB-J2	-15.32	-5.44	83.34		0.84	
+60 deg	RohnJP	10.77	6.60	71.08		1.53	
+60 deg	SNB-JP	15.32				1.66	
+60 deg	RohnJ1	-21.54	-13.18		926.0	0.66	9.1
+60 deg	RohnJ2	10.76	6.60	71.02	320.0	1.53	0.1
+60 deg	SNB-J1	-30.64				2.08	
+60 deg	SNB-J2	15.32	5.44	83.34		1.66	
+90 deg	RohnJP	0	0.00	0.00		0.81	
+90 deg	SNB-JP	0				0.44	
+90 deg	RohnJ1	-18.66				0.46	8.1
+90 deg	RohnJ2	18.65	11.42	212.98	920.0	2.06	0.1
+90 deg	SNB-J1	-26.54				1.75	
+90 dea	SNB-J2	26.53	9.42	249.91	l	2.57	

Forces taken from PLS-Tower output with 0.9\*DL Only load case subtracted from Vertical Tower Forces

Dimensions taken from CAD drawing





Job Description Page of

180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Revision 4 Sheet of

Overturning Moment Calculation Computed by MCD Date 07/31/19

Maximum Forces - All 5 Load Cases Checked by Date

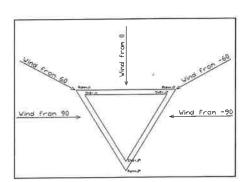
	Load Case 1	Load Case 1	Load Case 2	Load Case 2	Load Case 3	Load Case 3	Load Case 4	Load Case 4	Load Case 5	Load Case 5
Load Case	Total Moment (ft-k)	Total Shear (k)								
Wo -90 deg	14201	143.5	14183	143.4	5320	54.5	927.1	8.5	925.9	8.1
Wo -60 deg	14074	154.7	14056,3	154.3	5320	56.3	927.4	9.5	925.9	9.1
Wo 0 deg	14589	159.2	14576.1	159.5	5378	59.6	927.6	7.7	926.2	7
Wo 60 deg	14074	154.7	14056.5	154.3	5321	56.3	927.5	9.5	926	9.1
Wo 90 deg	- 14201	143.4	14183.1	143.4	5320	54.5	927.3	8.5	926	8,1

Maximum Moment =

14<u>589</u> kip\*ft

Maximum Shear =

159.5 kip



Description

Sheet 1 180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Revision 4 Date 07/31/19 Computed by MCD Foundation Analysis (TIA-222-G) Date Checked by

#### PIER AND MAT FOUNDATION ANALYSIS - 3 PIERS

#### **TOWER FORCES:**

Shear at Base of Tower

#### **FOOTING DIMENSIONS:**

Overall Depth of Footing

Thickness of Footing

Width of Footing

Moment Caused by Tower M<sub>t</sub> := 14589 kip ft

 $S_{+} := 159.5 \text{ kip}$ 

Max Compressive Force  $C_t := 814 \text{kip}$ 

Max Uplift

 $U_t := 738 \text{ kip}$ 

Height of Tower Width of Tower at Base  $H_t := 180 \, ft$  $W_t := 22.833 \, ft$ 

Weight of Tower

Reinforement Cover:

 $T_f := 6.0 \, \text{ft}$ Cvr := 3in

 $W_f := 36.5 \, ft$ 

 $D_{f} := 3.5 \text{ft}$ 

Page

 $WT_{t. 0.9} := 86.21 \cdot kip$ WTt. 0.9 - 80.2 Fkp

NOTE: Information for "Weight of Tower" obtained from Load

WTt. 1.2 := 114.95 kip

Combination Calculation Excel Sheets Summation of Factored DL.

#### **MATERIAL PROPERTIES:**

Compressive Strength of Concrete

fc := 3000 psi

Unit Weight of Soil

 $\gamma_s := 130 \, \text{pcf}$ 

Yield Strength of Steel Reinforcement fy := 60000 psi

Unit Weight of Concrete

 $\gamma_c := 150 \,\mathrm{pcf}$ 

Internal Friction Angle of Soil

 $\phi_s := 36 \cdot \deg$ 

Depth to Neglect

 $n := 0 \cdot ft$ 

Allowable Bearing Capacity

 $q_s := 4000 \, psf$ 

Cohesion of Clay Type Soil Note: Use 0 for Sandy Soil

 $c := 0 \cdot ksf$ 

Ultimate Bearing Capacity

 $R_s := 2 \cdot q_s$ 

Coefficient of Lateral Soil Pressure

 $K_p := \frac{1 + \sin(\phi_s)}{1 - \sin(\phi_s)}$   $K_p = 3.8518$ 

What is Position of Center of Tower with respect to Center of Pad?

1=Offset

2=Not Offset

 $Pos_{tower} := 2$ 

#### STEEL REINFORCING:

#### PAD REINFORCEMENT (Considering Uplift Moment Resistance):

Bar Size

 $BS_{pad} := 8$ 

**Bar Diameter** 

 $d_{bpad} := 1.00 \cdot in$ 

Number of Bars

 $NB_{pad} := 44$ 

Bar Area

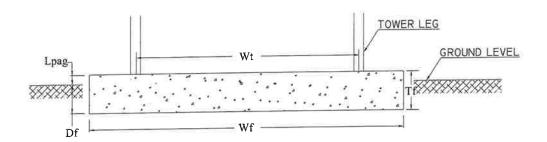
 $A_{bnad} := 0.95 \cdot in^2$ 

NOTE: Area is for #8 @ 10in for uplift control ONLY.

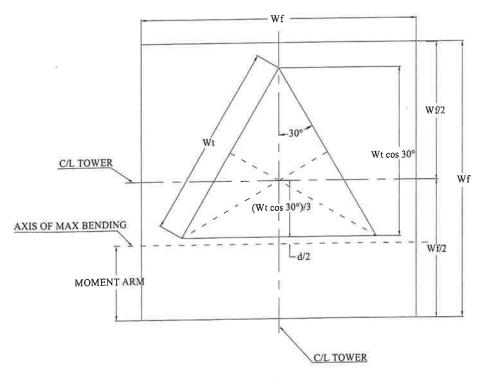
Job

Page Sheet 2 of 7 180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Revision 4 Date 07/31/19 Computed by MCD Description Foundation Analysis (TIA-222-G) Date Checked by

#### **FOUNDATION OVERVIEW**



#### **ELEVATION**



**PLAN** 

Job Description

180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Foundation Analysis (TIA-222-G)

Computed by Checked by

Revision 4

Page of Sheet 3 of 7 Date 07/31/19 Date

#### STABILITY OF FOOTING

NOTE: Reduction factor is implemented as 0.75 for pull-out/uplift of foundation. Reduction factor shall be applied to Overturning Moment in this

Passive Pressure:

$$P_{pn} := K_p \cdot \gamma_s \cdot n + c \cdot 2 \cdot \sqrt{K_p}$$

$$P_{pn} = 0 \cdot ksf$$

$$P_{pt} := K_p \cdot \gamma_s \cdot (D_f - T_f) + c \cdot 2 \cdot \sqrt{K_p}$$

$$P_{ton} := if \left[ n < (D_f - T_f), P_{pt}, P_{pn} \right]$$

$$P_{pt} = -1.2518 \cdot ksf$$

$$P_{top} = 0 \cdot ksf$$

$$P_{hot} := K_p \cdot \gamma_s \cdot D_f + c \cdot 2 \cdot \sqrt{K_p}$$

$$P_{hot} = 1.7526 \cdot ksf$$

$$P_{ave} := \frac{P_{top} + P_{bot}}{2}$$

$$P_{ave} = 0.8763 \cdot ksf$$

Shear:

$$\mathsf{T}_{\mathsf{pp}} \coloneqq \mathsf{if} \Big[ \mathsf{n} < \Big( \mathsf{D}_{\mathsf{f}} - \mathsf{T}_{\mathsf{f}} \Big), \mathsf{T}_{\mathsf{f}}, \Big( \mathsf{D}_{\mathsf{f}} - \mathsf{n} \Big) \Big]$$

$$T_{pp} = 3.5 \cdot ft$$

$$A_{pp} := W_f \cdot T_{pp}$$

$$A_{op} = 127.75 \cdot ft^2$$

Ultimate Shear:

$$S_u := P_{ave} \cdot A_{pp}$$

$$A_{pp} = 127.75 \text{ ft}$$
  
 $S_{tt} = 111.9465 \cdot \text{kip}$ 

Weight of Concrete Pad:

$$WT_c := (W_f^2 \cdot T_f) \cdot \gamma_c$$

$$WT_c = 1199.025 \cdot kip$$

Weight of Soil:

$$WT_{e1} := 0$$

$$WT_{e1} = 0 \cdot kip$$

above Footing:

$$WT_{s2} := \left[ \frac{\left(D_f - n\right)^2 \cdot tan(\phi_s)}{2} \cdot W_f \right] \cdot \gamma_s$$

Distance to center of Tower Leg from Edge of Footing:

Wedge at back face:

$$X_{t1} := \frac{W_f}{2} - \frac{W_t \cdot \cos(30 \cdot \deg)}{2}$$

$$X_{t2} := \frac{W_f}{2} - \frac{W_t \cdot \cos(30 \cdot \deg)}{3}$$

$$X_t := if(Pos_{tower} = 1, X_{t1}, X_{t2})$$

$$X_t = 11.6587 \cdot ft$$

Additional Offset of Footing:

$$X_{off1} := \frac{W_f}{2} - \left(\frac{W_t \cdot \cos(30 \cdot \deg)}{3} + X_t\right) \qquad X_{off2} := 0$$

 $X_{off} := if(Pos_{tower} = 1, X_{off1}, X_{off2})$ 

$$X_{off} = 0 \cdot ft$$

Resisting Moment:

$$\begin{aligned} \mathbf{M_r} &\coloneqq \left[0.9 \left(\mathbf{WT_c} + \mathbf{WT_{s1}}\right)\right] \cdot \frac{\mathbf{W_f}}{2} + \left[\mathbf{WT_{t.\_0.9}} \cdot \left(\frac{\mathbf{W_f}}{2} - \mathbf{X_{off}}\right)\right] + 0.90 \cdot \left(\mathbf{S_u} \cdot \frac{\mathbf{T_{pp}}}{3}\right) \dots \\ &+ \mathbf{WT_{s2}} \cdot 0.90 \cdot \left(\mathbf{W_f} + \frac{\mathbf{T_{pp}} \cdot \tan(\phi_s)}{3}\right) \end{aligned}$$

$$\phi_{OT} := 0.75$$

### φ<sub>OT</sub> := 0.75 ANSI/TIA-222-G REDUCTION FACTOR

$$M_r = 22094.6177 \cdot \text{kip} \cdot \text{ft}$$

$$\mathsf{M}_{ot} \coloneqq \mathsf{M}_t + \mathsf{S}_t \cdot \left(\mathsf{T}_f\right) + \mathsf{WT}_{t.\_1.2} \cdot \mathsf{X}_{off}$$

$$M_{ot} = 15546 \cdot \text{kip} \cdot \text{ft}$$

Ratio<sub>Stability</sub> := 
$$\frac{M_{ot}}{M_r \cdot \phi_{OT}}$$

StabilityCheck := 
$$if(M_r, \phi_{OT} > M_{ot}, "Okay", "No Good")$$

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180' ROHN SSV Tower w/ SNB Reinf. - Greenwich Project No. Foundation Analysis (TIA-222-G)

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# BEARING PRESSURE CHECK:

$$LOAD_{tot} := (WT_c + WT_{s1}) \cdot 0.9 + WT_{t.\_0.9}$$

$$LOAD_{tot} = 1165.3325 \cdot kip$$

$$A_{\text{mat}} := W_f^2$$

$$A_{mat} = 1332.25 \cdot ft^2$$

$$S = \frac{W_f^3}{6}$$

$$S = 8104.5208 \cdot ft^3$$

$$P_{\text{max}} := \frac{\text{LOAD}_{\text{tot}}}{A_{\text{mat}}} + \frac{M_{\text{ot}}}{S}$$

$$P_{\text{max}} = 2.7929 \cdot \text{ksf}$$

$$P_{min} := \frac{LOAD_{tot}}{A_{mat}} - \frac{M_{ot}}{S}$$

$$P_{\min} = -1.0435 \cdot ksf$$

$$MinPressure := if \left\lceil \left(P_{min} \geq 0\right) \cdot \left(P_{min} < 0.75 \cdot R_{s}\right), "Okay", "No Good" \right\rceil$$

Distance to Resultant of Pressure Distribution:

$$X_{p} := \frac{P_{max}}{\frac{P_{max} - P_{min}}{W_{f}}} \cdot \frac{1}{3}$$

$$X_p = 8.8574 \cdot \text{ft}$$

$$X_k := \frac{W_f}{3}$$

$$X_k = 12.1667 \cdot ft$$

Since Resultant Force is Not in Kern, Area to which Pressure is Applied Must be Reduced.

Eccentricity:

$$e := \frac{M_{ot}}{LOAD_{tot}}$$

Adjusted Soil Pressure:

$$q_a := \frac{2 \cdot LOAD_{tot}}{3 \cdot W_f \cdot \left(\frac{W_f}{2} - e\right)}$$

$$q_a = 4.3353 \cdot ksf$$

Revised Maximum:

$$q_{max} := if(X_p < X_k, q_a, P_{max})$$

$$q_{\text{max}} = 4.3353 \cdot \text{ksf}$$

$$PressureCheck := if \Big( q_{max} < 0.75 \cdot R_{s}, "Okay", "No Good" \Big)$$

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Job	180' ROHN SSV Tower w/ SNB Reinf Greenwich	Project No.	Revision 4	_Sheet	5 of 7
Description	Foundation Analysis (TIA-222-G)	Computed by	MCD	_Date	07/31/19
		Checked by		Date	

# CHECK PUNCHING AND BEAM SHEAR:

Beam Shear: (Critical section located at a distance d from the face of Pier) (ACI 11.3.1.1)

$$\phi_c := 0.75$$
 (ACI 9.3.2.3)

$$d := T_f - Cvr - .5 \cdot in$$
  $d = 44.5 \cdot in$ 

Factored load: 
$$FL := \frac{C_t}{W_f^2}$$
 
$$FL = 0.611 \cdot ksf$$

$$V_{\text{req}} := \frac{\text{FL} \cdot (X_t - d) \cdot W_f}{\Phi_c}$$

$$V_{\text{req}} = 236.4048 \cdot \text{kip}$$

ACI 11.3.1.1 
$$V_{Avail} := 2 \cdot \sqrt{fc \cdot psi} \cdot W_{f} \cdot d$$
  $V_{Avail} = 2135.1321 \cdot kip$ 

$$\label{eq:beamShearCheck} \begin{aligned} \text{BeamShearCheck} &:= \text{if} \Big( \text{$V_{req} < V_{Avail}$, "Okay" , "No Good"} \Big) \end{aligned} \qquad \begin{aligned} &\text{BeamShearCheck} &= \text{"Okay"} \end{aligned}$$

Punching Shear: (Critical Section Located at a distance of d/2 from the face of pier) (ACI 11.12.2.1)

$$\boldsymbol{b}_0 \coloneqq (\boldsymbol{d}) \cdot \boldsymbol{\pi} \qquad \qquad \boldsymbol{b}_0 = 11.6501 \cdot \boldsymbol{f} \boldsymbol{t}$$

$$V_{req} := FL \cdot \frac{W_f^2 - (d)^2 \cdot \frac{\pi}{4}}{\varphi_c}$$

$$V_{req} = 1076.5345 \cdot kip$$

$$V_{Avail} := 4 \cdot \sqrt{fc \cdot psi} \cdot b_o \cdot d$$

$$V_{Avail} = 1362.9832 \cdot kip$$

PunchingShearCheck := 
$$if(V_{req} < V_{Avail}, "Okay", "No Good")$$

PunchingShearCheck = "Okay"

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Description Foundation Analysis (TIA-222-G)

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# TENSILE REINFORCEMENT IN PAD:

$$\phi_{\rm m} := 0.90$$

per ACI 9.3.2.2

Applied Moments: NOTE: Existing 2 feet of concrete over original foundation considered in uplift reduction for design

 $0.9 \cdot \frac{\gamma_{\rm c} \cdot (2\text{ft} \cdot 32.5\text{ft} \cdot 32.5\text{ft})}{2} = 95.0625 \cdot \text{kip}$ 

calculations shown below

$$\textit{Calculations shown below} \\ \text{M}_{nT} := \left[ \left( \textbf{U}_t - 95 \text{kip} \right) \cdot \left( \textbf{W}_t \cdot \sin(60 \cdot \text{deg}) \right) + \textbf{S}_t \cdot \left( \textbf{D}_f \right) \right] - \textbf{WT}_{t.\_1.2} \cdot \textbf{X}_{off} \\ \text{Thickness} \\ \text{Thickness}$$

$$M_{nS} := -1 \cdot \left[ \frac{1}{2} \cdot \left( \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30 \cdot \deg) \right)^2 \cdot 0.9W_t \cdot \left[ \gamma_s \cdot \left( T_{pp} - T_f \right) \right] + 0.9WT_{s2} \cdot \left[ \left( \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30 \cdot \deg) \right) + \left( D_f - n \right) \cdot \tan(\varphi_s) \right] \right]$$

$$M_{nC} \coloneqq -1 \cdot \left[ \frac{1}{2} \cdot \left( \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30 \cdot \text{deg}) \right)^2 \cdot 0.9 \cdot W_t \cdot \left( \gamma_c \cdot T_f \right) \right] \qquad \text{a.s.} = 56.5 \text{in}$$

Design Moment:

$$M_n := \frac{M_{nT} + M_{nS} + M_{nC}}{\Phi_m} \qquad M_n = 10400.3519 \cdot \text{kips} \cdot \text{ft}$$

$$M_n = 10400.3519 \cdot \text{kips} \cdot \text{ft}$$

# Required Reinforcement:

ACI 10.2.7.3

 $\beta := \text{if} \left| \text{fc} \le 4000 \cdot \text{psi}, .85, \text{if} \right| \text{fc} \ge 8000 \cdot \text{psi}, .65, .85 - \left( \frac{\text{fc}}{\text{psi}} - 4000}{1000} \right) \cdot .05 \right| \qquad \beta = 0.85$ 

Effective Width:

 $b_{eff} := W_t \cdot \cos(30 \cdot \deg) + 0 \text{ ft}$ 

 $b_{eff} = 237.2875 \cdot in$ 

$$A_{s} := \frac{M_{n}}{\phi_{m} \cdot fy \cdot d}$$

$$A_{S} = 40.906 \cdot in^{2}$$

$$a := \frac{A_{S} \cdot fy}{\beta \cdot f c \cdot b_{eff}}$$

$$\text{Ass} = \frac{M_n}{\text{fy-}\left(d - \frac{a}{2}\right)}$$

$$A_{S} = 38.1861 \cdot in^{2}$$

$$\rho := \frac{A_{s}}{b_{eff} \cdot d}$$

$$\rho = 0.0028$$

Temperature and Shrinkage:

$$\rho_{sh} \coloneqq \mathrm{if}(\mathrm{fy} \geq 60000 \cdot \mathrm{psi}, 0.0018, 0.0020)$$

$$\rho_{sh} = 0.0018$$

(ACI 7.12.2.1b)

$$\mathsf{As} \coloneqq \mathrm{if} \left( \, \rho \geq \rho_{sh}, \mathsf{A}_s, \rho_{sh} . \frac{\mathsf{beff}}{2} . \mathsf{d} \, \right)$$

$$As = 38.1861 \cdot in^2$$

$$As_{prov} := A_{bpad} \cdot NB_{pad}$$

$$As_{prov} = 41.8 \cdot in^2$$

PadReinforcement := if(As<sub>prov</sub> > As, "Okay", "No Good")

PadReinforcement = "Okay"

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# DEVELOPMENT LENGTH OF PAD REINFORCEMENT:

TENSION (ACI 12.2.3)

$$B_{sPad} := \frac{W_f - 2 \cdot Cvr - NB_{pad} \cdot d_{bpad}}{NB_{pad} - 1}$$

$$B_{sPad} = 9.0233 \cdot in$$

$$\alpha := 1.0$$

$$\beta := 1.0$$

$$\lambda := 1.0$$

$$\gamma := 1.0$$

$$c := if \left( Cvr < \frac{B_{sPad}}{2}, Cvr, \frac{B_{sPad}}{2} \right) \quad c = 3 \cdot in$$

$$k_{tr} := 0$$

$$L_{dbt} := \frac{3}{40} \cdot \frac{fy}{\sqrt{f'c \cdot psi}} \cdot \frac{\alpha \cdot \beta \cdot \gamma \cdot \lambda}{\frac{c + k_{tr}}{dt}} \cdot d_{bpad}$$

$$L_{dbt} = 27.3861 \cdot in$$

$$L_{dbmin} := 12 \cdot in$$

$$\label{eq:loss_loss} \mbox{Minimum Development Length: } L_{dbtCheck} \coloneqq if \Big( L_{dbt} \ge L_{dbmin}, "Use L.dbt" \ , "Use L.dbmin" \Big)$$
 (ACI 12.2.1)

$$L_{\text{Pad}} := \frac{W_{\text{f}}}{2} - \frac{W_{\text{t}}}{2} - \text{Cvr}$$

$$L_{Pad} = 79.002 \cdot in$$

$$\texttt{LpadTension} := \text{if} \left( \texttt{L}_{\texttt{Pad}} > \texttt{L}_{\texttt{dbt}}, \texttt{"Okay"}, \texttt{"No Good"} \right)$$

LpadTension = "Okay"

AECOM:  Job Greenwich (SP modification Analysis  Description Custom Anchorage Design  Check For Anchor Bolts	Project No. Revision 4  Computed by McD  Checked by	Page of 2 Sheet of 3 Date 7/31/19 Date Reference
Diagonal Members SNI	· Compre ss ion force	= 21.030 Kif
· Convert to "X y" Plane forces 21.355 t. ρ Θ=32.06° (CAD) · 21.355 t. ρ · sin (32.06) · 21.355 t. ρ · cos (32.06)	neasuled from PLS-tou	
- for Conservative consideration Compressive force.  Convert to "xy" Plane forces		is (cn +/01/11/19
21.030 Kip. Sin (32.06)  21.030 Kip. Cos (32.06)	5°) = 11.16 287 K:P5 °) = 17.8228 K:P5	2
- for conservative considerations, tension force		

Z (I) 74 A 490 N Single Shar Assumed Printo tower Modification - Bolt shear a neck

22.5 k:P5 > 18,0982 k:P5 .. Bolt@connection 36+

AECOM"		Page of
Job Greenwich CSP Medification Analysis Description CUSTOM Anchorage Design Check	Project No. Revision 4 Computed by MCD	Page of Sheet \( \geq \frac{2}{7/31/19} \)
For Ancher Boits	Checked by	Date
· For Anchorage Details, the f		Reference
-V(Shear) = 18,0982 kips / 4An (conservative values) -1(uplift) = 17,8228 kips / 4 And		

· Apply (4) HILT HIT-RESOOVS Epoxy Anchoring System

- · for 78" Anchor @ 7%" effective embedment & Scooncrete = 3000PS;
  - epoxy tension capacity lanchor= 13,375 lbs (Priorto Reduction factor)
     epoxy Shear Capacity lanchor= 28,810 lbs (priorto Reduction factor)
- · APPly "HAS-E" Anchor Bolts (table 29) (Steel)
  - Tension Capacity / Ancher = 21,755 165 (LRFD Capacity ACT 17. 4.1.28)
  - Shear capacity/Anchor = 12,050165 (LEFD (apacity) -Act 17.5.1.26
- · Apply Hilli Reductions to epoxy Anchers [table 39] & S=6:1.
  - tension (apacity = 13,375 lb + x0.61=8,158 lb =/anchor = F/n
  - Shear capacity = 28,8 10 165 x Oist = 15,845 165/anchor = \$000
- · Apply Anchers Per Interaction Equation -Act 17.6,3 & HILTER 3,1,6,7

- Note: HILLI applications follow the Design or teris from IBC 2015, Section 1901. & BACT 318-14 (Reference: ICC-ESReport "ESR-3814" - January 2017)

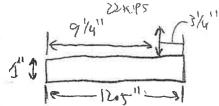
# AECOM'

AECUNI		Page of
Job Green wich CSP MoDification Analysis	Project No. Revision 4	Sheet 3 of 3
Description Custom Anchorage Design Check	Computed by MCD	Date 7/31/19
Baseplate for anchor Bolts	Checked by	Date

Reference

· tension/compression force applied to Baseplate = 22 tips

-Per Design Sketch SK-5- Determine Plastic Bending Capacity of
Baseplate



mapplied = Pab = 22 KiPS X 9,25" x 3,25" = 52.91 KiFA

- Plate Plastic capacity = mr = 0x2 = 0.9x50ksix bdi
= 8,9x50ksi xlatin (lin)2

mr = 14c. 625 kin

· Note: Plate LTBis Not considered for Plate "miner" axisbend:

# 3.2.4 HIT-RE 500 V3 Epoxy Adhesive Anchoring System

Table 26 - Hilti HIT-RE 500 V3 adhesive design strength with concrete / bond failure for threaded rod

Mandaul			Tension	- ON			Shear	ΦV.	
Nominal anchor diameter	Effective embedment	f' = 2,500 psi (17.2 MPa)	f' = 3,000 рві (20.7 МРа)	27.6 MPa)	f* = 6,000 psi (41.4 MPa)	f' = 2,500 pri (17.2 MPs)	f' = 3,000 ps (20.7 MPa)	" = 4,000 psi (27.6 MPa)	f = 6,000 ps (41.4 MPa)
ln.	In. (mm)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	Ib (kN)	lb (kN)	lb (kN)	Ib (kN)
	2-3/8	2,020	2,215	2,500	2,655	2,180	2,385	2,690	2,880
L	(60)	(9.0)	(9.9)	(11.1)	(11.8)	(9.7)	(10.6)	(12.0)	(12.7)
	3-3/8	3,310	3,400	3,550	3,770	7,125	7,325	7,645	8,125
3/8	(88)	(14.7)	(15.1)	(15.8)	(16.8)	(31.7)	(32.6)	(34.0)	(36.1)
5/5	4-1/2	4,410	4,535	4,735	5,030	9,500	9,765	10,195	10,835
	(114)	(3.61)	(20.2)	(21.1)	(22.4)	(42.3)	(43.4)	(45.3)	(48.2)
	7-1/2	7,350	7,555	7,890	8,385	15,835	16,275	16,990	18,055
	(191)	(32.7)	(33.6)	(35.1)	(37.3)	(70.4)	(72.4)	(75.6)	(80.3)
	2-3/4	2,520	2,760	3,185	3,905	5,425	5,845	6,865	8,405
	(70)	(11,2)	(12.3)	(14.2)	(17.4)	(24.1)	(28.4)	(30.5)	(37.4)
-	4-1/2	5,275	5,780	6,260	6,655	11,360	12,445	13,485	14,33D
1/2	(114)	(23.5)	(25.7)	(27.8)	(29.6)	(50.5)	(55.4)	(0.0)	(63.7)
1/2	6	7,780	7,895	8,350	8,870	16,755	17,220	17,980	19,110
L	(152)	(34.6)	(35.6)	(37.1)	(39.5)	(74.5)	(76.6)	(0.03)	(95.0)
f	10	12,985	13,325	13,915	14,785	27,930	28,705	29,970	31,850
	(254)	(57.7)	(59.3)	(61.9)	(65.8)	(124.2)	(127.7)	(133.3)	(141.7)
	3-1/8	3,050	3,345	3,860	4,730	8,575	7,200	8,315	10,185
Į.	(79)	(13.6)	(14.9)	(17.2)	(21.0)	(29.2)	(32.0)	(37.0)	(45.3)
	5-5/8	7,370	8,075	9,325	10,315	15,875	17,390	20,080	22,215
5/8	(143)	(32.8)	(35.9)	(41.5)	(45.9)	(70.6)	(77.4)	(89.3)	(8.89)
3/6	7-1/2	11,350	12,395	12,940	13,755	24,440	26,895	27,875	29,620
	(191)	(50.5)	(55.1)	(57.6)	(61.2)	(108.7)	(118.7)	(124.0)	(131.8)
	12-1/2	20,100	20,660	21,570	22,920	43,295	44,495	46,460	49,370
	(318)	(89.4)	(91.9)	(95.9)	(102.0)	(192.6)	(197.9)	(208.7)	(219.6)
	3-1/2	3,620	3,865	4,575	5,605	7,790	8,535	9,855	12,070
L	(89)	(16.1)	(17.6)	(20.4)	(24.9)	(34.7)	(38.0)	(43.8)	(53.7)
	6-3/4	9,690	10,615	12,255	14,735	20,870	22,860	28,395	31,740
3/410	(171)	(43.1)	(47.2)	(54.5)	(85.5)	(92.8)	(101.7)	(117.4)	(141.2)
5/4	8	14,920	16,340	18,490	19,650	32,130	35,195	39,820	42,320
	(229)	(66.4)	(72.7)	(82.2)	(87.4)	(142.9)	(156.6)	(177.1)	(188.2)
	15	28,715	29,510	30,815	32,745	61,850	63,565	66,370	70,530
	(381)	(127.7)	(131.3)	(137.1)	(145.7)	(275.1)	(282.7)	(295.2)	(313.7)
	3-1/2	3,620	3,965	4,575	5,605	7,790	8,535	9,855	12,070
	(89)	(16.1)	(17.6)	(20.4)	(24.9)	(34.7)	(38.0)	(43.8)	(53.7)
	7-7/8	12,210	13,375	15,445	18,915	26,300	28,810	33,265	40,740
7/810	(200)	(54.3)	(59.5)	(68.7)	(64.1)	(117.0)	(128.2)	(148.0)	(181.2)
,,e	10-1/2	18,800	20,590	23,780	26,530	40,490	44,355	51,215	57,140
	(287)	(83.6)	(91.6)	(105.8)	(118.0)	(180.1)	(197.3)	(227.8)	(254.2)
	17-1/2	38,775	39,B5D	41,605	44,215	83,510	85,825	89,610	95,230
	(445)	(172.5)	(177.3)	(185.1)	(196.7)	(371.5)	(381.6)	(398.6)	(423.6)
	4	4,420	4,840	5,590	6,845	9,520	10,430	12,040	14,750
L	(102)	(19.7)	(21.5)	(24.9)	(30.4)	(42.3)	(48.4)	(53.6)	(65.6)
F	9	14,920	16,340	18,870	23,110	32,130	35,195	40,640	49,775
1 -	(229)	(66.4)	(72.7)	(83.9)	(102.8)	(142.9)	(156.5)	(180.8)	(221.4)
	12	22,965	25,160	29,050	34,650	49,485	54,190	62,570	74,630
	(305)	(102.2)	(111.9)	(129.2)	(154.1)	(220.0)	(241.0)	(278.3)	(332.0)
	20	49,415	52,045	54,340	57,750	106,435	112,100	117,045	124,385
	(508)	(219.8)	(231.5)	(241.7)	(256.9)	(473.4)	(498.5)	(520.6)	(553.3)
	5	8,175	6,785	7,815	9,670	13,305	14,575	16,830	20,610
	(127)	(27.5)	(30.1)	(34.8)	(42.8)	(59.2)	(64.8)	(74.9)	(91.7)
Г	11-1/4	20,850	22,840	26,370	32,295	44,905	49,190	56,800	89,565
1-1/410	(286)	(82.7)	(101.6)	(117.3)	(143.7)	(199.7)	(218.8)	(252.7)	(309.4)
1-1/4	15	32,095	35,160	40,600	49,725	69,135	75,730	87,445	107,100
	(381)	(142.8)	(155.4)	(180.6)	(221.2)	(307.5)	(336.9)	(0.986)	(476.4)
Ī	25	69,060	76,666	80,800	85,865	148,750	162,945	174,030	184,945
	(635)	(307.2)	(336.5)	(359.4)	(381.9)	(661.7)	(724.8)	(774.1)	(822.7)

- See Section 3.1.8 for explanation on development of load values.

  See Section 3.1.8 for explanation on development of load values.

  See Section 3.1.8 for explanation on development of load values.

  Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

  Apply specing, edge distance, and concrete thickness factors in tables 30-41 as necessary to the above values. Compare to the steel values in table 29. The leaser of the values is to be used for the design.

  Data is for temperature range 8: Max. short term temperature = 130°F (55°C), max. long term temperature = 110°F (43°C).

  For temperature range 8: Max. short term temperature = 178°F (80°C), max. long term temperature = 110°F (43°C) multiply above values by 0.99.

  Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over least the second of the concrete temperature are roughly constant over Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

  Tabular values are for dry or water saturated concrete conditions.

  For water-filled drilled holes multiply design strength by 0.51.

  Tabular values are for short term loads only. For sustained loads including overhead use, see Section 3.1.8.8.

  Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by \(\lambda\), as follows:

  For sand-lightweight, \(\lambda\), = 0.51. For all-lightweight concrete multiply design strength by \(\lambda\), as follows:

  For sand-lightweight, \(\lambda\), = 0.51. For all-lightweight concrete multiply design strength by \(\lambda\), as follows:

  For sand-lightweight, \(\lambda\), = 0.51. For all-lightweight concrete with carbide tipped hammer drill bit. Diamond core drilling is not permitted in cracked concrete conditions except as indicated in note 10.

  10 Diamond core drilling with Hill TE-YRT roughening tool is permitted for 3/4\*, 7/8\*, and 1 1/4\* diameter anchors for dry and water-saturated concrete conditions. See Table 28

  11 Tabular values are for tholes drilling with Hill TE-YRT roughening tool is permitted for 3/4\*, 7/8\*, and 1 1/4\* diameter anchors for dry and water-saturated concrete conditions. See Table 28

  12 Inc. diameter - 0... = 0.58

  12 Inc. diameter - 0... = 0.59

  13/4-in. diameter - 0... = 0.71

  3/4-in. diameter - 0... = 0.71

  3/4-in. diameter - 0... = 0.71

# HIT-RE 500 V3 Epoxy Adhesive Anchoring System 3.2.4

Table 38 - Load adjustment factors for 7/8-in. diameter threaded rods in uncracked concrete<sup>1,2,3</sup>

																	Edge	dista	nce in	shear						
	7/B-ii uncrac	ked	٤	Spacin In te	g facto nsion	or	Edg	e dista In te	ance fa nsion	actor	1	•	g facti hear	or		Towar	⊥ d edg	9	1	To ar	d awa edge	ıy		actor I	thick n shea	
	CONCR	ete		f	AN				RW		_		W				RV		_	J	RV				HV.	145.4
Em	bedment	in.	3-1/2	7-7/8	10-1/2	17-1/2	3-1/2	7-7/8	10-1/2	17-1/2	3-1/2	7-7/8	10-1/2	17-1/2												1000
	h,	(mm)	(89)	(200)	(287)	(445)	(89)	(200)	(267)	(445)	(89)	(200)	(267)	(445)		(200)	-	_		(200)		1 /	(89)		(267)	-
	1-3/4	(44)	n/a	n/a	n/a	n/a	0.39	0.24	0.18	0.10	n/a	n/a	n/a	n/a	0.09	0.03	0.02	0.01	0.18	0.05	0.04	0.02	n/a	n/a	n/a	n/a
ê	4-3/8	(111)	0.58	0.58	0.57	0.54	0.53	0.31	0.23	0.13	0.58	0.54	0.53	0.52	0.35	0.11	0.07	0.03	0.63	-	0.14	0.07	n/a	n/a	n/a	n/a
(IIII)	5	(127)	0.59	0.59	0.58	0.55	0.56	0.33	0.24	0.13	0.59	0.54	0.53	0.52	0.43	0.13		0.04	0.70			0.08	n/a	n/a	n/a	n/a
ċ	5-1/2	(140)	0.60	0.60	0.59	0.55	0.58	0.34	0.25	0.14	0.60	0.55	0.54	0.52	0.50	0.15	0.10	0.05	0.76		0.20	0.09	0.65	n/a	n/a	n/a
٦.	6	(152)	0.61	0.61	0.60	0.56	0.61	0.36	0.26	0.15	0.61	0.55	0.54	0.52	0.57	0.17	0.11	0.05	0.83	0.35	0.23	0.11	0.68	n/a	π/a	n/a
Ê	7	(178)	0.63	0.63	0.61	0.57	0.65	0.39	0.28	0.16	0.63	0.56	0.55	0.53	0.71	0.22	0.14	0.07	0.97	0.39	0.29	0.13	0.73	n/a	n/a	n/a
8	8	(203)	0.65	0.65	0.63	0.58	0.71	0.42	0.31	0.17	0.65	0.57	0.55	0.53	0.87	0.27	0.17	0.08	1.00	0.42	0.33	0.16	0,78	n/a	n/a	n/a
₹	9	(229)	0.67	0.67	0.64	0.59	0.76	0.45	0.33	0.18	0.67	0.58	0.56	0.54	1.00	0.32	0.21	0.10			0.35	0.19	0.83	n/a	n/a	n/a
Thickness	9-7/8	(251)	0.69	0.69	0.66	0.59	0.80	0.48	0.35	0.19	0.69	0.59	0.56	0.54		0.37	0.24	0.11		0.48	0.37	0.22	0.87	0.59	n/a	n/a
	10	(254)	0.69	0.69	0.66	0.60	0.81	0.49	0.35	0.19	0.69	0.59	0.57	0.54		0.38	0.24	0.11		0.49	0.37	0.23	0.87	0.59	n/a	n/a
Ē	11	(279)	0.71	0.71	0.67	0.60	0.87	0.52	0.38	0.21	0.71	0.60	0.57	0.54		0.43	0.28	0.13		0.52	0.40	0.26	0.91	0.62	n/a	n/a
Concrete	12	(305)	0.73	0.73	0.69	0.61	0.92	0.56	0.40	0.22	0.73	0.60	0.58	0.55		0.49	0.32	0.15		0.56	0.42	0.29	0.95		n/a	n/a
ŏ	12-1/2	(318)	0.74	0.74	0.70	0.62	0.95	0.59	0.41	0.23	0.74	0.61	0.58	0.55		0.52	0.34	0.16		0.59	0.43	0.29	0.97	0.66	0.57	n/a
(0)	14	(356)	0.76	0.76	0.72	0.63	1.00	0.66	0.46	0.25	0.77	0.62	0.59	0.55		0.62	0.40	0.19		0.66	0.47	0.31	1.00	0.70	0.60	n/a
<u>ی</u>	16	(406)	0.80	0.80	0.75	0.65		0.75	0.52	0.29	0.80	0.64	0.60	0.56		0.76	0.49	0.23		0.75	0.52	D.34		0.75	0.65	n/a
ğ	18	(457)	0.84	0.84	0.79	0.67		0.84	0.59	0.32	0.84	0.66	0.62	0.57		0.91	0.59	0.27		0.84	0.59	0.36		0.79	0.68	n/a
Dista	19-1/2	(495)	0.87	0.87	0.81	0.69		0.92	0.64	0.35	0.87	0.67	0.63	0.58		1.00	0.66	0.31		0.92	0.64	0.38		0.82	0.71	0.55
	20	(508)	0.88	0.88	0.82	0.69		0.94	0.65	0.36	0.88	0.67	0.63	0.58			0.69	0.32		0.94	0.65	0.39		0.83	0.72	0.58
Edge	22	(559)	0.91	0.91	0.85	0.71		1.00	0.72	0.40	0.92	0.69	0.64	0.59			0.80	0.37		1.00	0.72	0.41		0.87	0.76	0.58
/E	24	(610)	0.95	0.95		0.73			0.78	0.43	0.96	0.71	0.66	0.59		- 1	0.91	0.42			0.78	0.44		0.91	0.79	0.61
(8)	26	(660)	0.99	0.99	0.91	0.75			0.85	0.47	0.99	0.73	0.67	0.60			1.00	0.48			0.85	0.47		0.95	0.82	0.64
8	28	(711)	1.00	1.00	0.94	0.77			0.91	0.50	1.00	0.74	0.68	0.61				0.53			0.91	0.50		0.99	0.85	0.66
BC	30	(762)				0.79			0.98	0.54		0.76	0.70	0.62		(c1)		0.59			0.98	0.54		1.00	0.88	0.68
Sp	36	(914)			-	0.84			1.00	0.65		0.81	0.73	0.64				0.77			1.00	0.65			0.97	0.75
-		(1219)	_			0.96				0.86		0.92	0.81	0.69				1.00				0.86			1.00	0.87

Table 39 - Load adjustment factors for 7/8-in. diameter threaded rods in cracked concrete<sup>1,2,3</sup>

F										2011		-				_	Edge	dista	ice in	ड्रांख्य						
	7/8-i crack concr	ed	5		g factonsion	or	Edg		ince fa nslon	actor	5		g facto hear <sup>4</sup>	or		1134	L d edge	Э	H	from	edge	y		actor i	thickn n shea	
-			2 10	7-7/8	10.10	17.10	2.10			17.10	3-1/2			17-1/2	3-1/2			17-1/2	3-1/2			17-1/2	3-1/2	1-1-1	***	17-1/2
150	ibedment		000000		1000000000	2000000000	No. of the North	25 40 40 40 40	100000000000000000000000000000000000000	(445)	V 10 2 10 1						(267)				(267)			(200)		(445)
-	h,	(mm)	(89)	-	(267)	-			0.41	0.38	n/a	n/a	n/a	n/a	0.09	0.03	-	0.01	0.18	0.08	-	0.02	n/a	n/a	n/a	n/a
	1-3/4	(44)	n/a	n/a	n/a	n/a	0.42	0.53	0.50	0.44	0.58	-	0.53	0.52	0.36	0.11	0.07	0.03	0.71	0.22	_	0.07	n/a	n/a	n/a	n/a
(mm)	4-3/8	(111)	0.58	0.58	-	0.54		0.56	0.50	_	0.60	-	0.53	0.52	0.43	0.13	0.09	0.04	0.87	0.27	0.17	0.08	n/a	n/a	n/a	n/a
١٤		(127)	0.59	0.59	0.58	0.55	0.58	0.58		-	0.61	_	0.54		0.50	0.15	0.10	-	1.00	0.31	0.20	0.10	0.65	n/a	n/a	n/a
1.5	5 1/2	(140)	0.61		0.60	0.56	0.56	0.61	0.56	0.47	0.61	_	0.54	0.52		0.18		0.06	1.00	0.35	_	0.11	0.68	n/a	n/a	n/a
2	6	(152)	0.63	-	0.61	0.57	0.65	0.65	0.60	0.49		_	0.55	0.53	0.72	0.22	0.14	0.07		0.44	0.29	0.14	0.73	n/a	n/a	n/a
1 9		(203)	0.65	0.65	0.63	0.58	0.71	-	0.64	_	0.65	0.57	0.55	0.53	0.88	0.27	0.18	0.09		0.54		0.17	0.78	n/a	n/a	n/a
Į	9	(229)	0.67	0.67	0.64		0.76	0.76		0.54	0.67	0.58	0.56	-	1.00	0.32	-	0.10		0.65	0.42	0.20	0.83	n/a	n/a	n/a
ÌŽ	9-7/8	(251)	0.69	0.69	_		0.80	0.80	0.72	0.56	0.69		0.56	0.54		0.37	0.24	0.12		0.74	0.48	0.23	0.87	0.59	n/a	n/a
Ē	10	(254)	0.69	0.69	0.66		0.81	-	-	0.56	0.69	_	0.57	0.54		0.38	0.25	0.12		0.76	0.49	0.24	0.87	0.59	n/a	n/a
	11	(279)	0.08	0.71	0.67	0.60	0.87	0.87	0.77	0.59	0.71	0.60	-	0.54		0.44	-	0.14		0.87	0.57	0.28	0.92	0.62	n/a	n/a
Concrete	12	(305)	0.73	0.73	0.69	40.00	0.92		0.82	0.61	0.73	0.60	0.58	0.55		0.50	0.32	0.16		1.00	0.65	0.31	0.96	0.65	n/a	n/a
8	12-1/2	-	0.74	0.74	0.70				_	0.62	0.74	0.61	0.58	0.55		0.53	0.34	0.17			0.69	0.33	0.98	0.66	0.57	n/a
12	-	(356)	0.76		-	0.63	-	1.00	0.91	0.66	0.77	0.62	0.59	_		0.63	0.41	0.20			0.82	0.40	1.00	0.70	0.61	n/a
1 -	16	(406)	0.80	0.80	-	0.65			1.00	0.71	0.81	0.64	0.60	0.56		0.77	0.50	0.24			1.00	0.48		0.75	0.65	n/a
180	18	(457)	0.84	0.84		0.67	-			0.76	0.84	0.66	0.62	0.57		0.91	0.59	0.29				0.58		0.79	0.69	n/a
1 #	19-1/2	(495)	0.87		0.81	0.69				0.80	0.87	0.67	0.63	0.58		1.00	0.67	0.32				0.65		0.82	0.71	0.56
	20	(508)	0.88	0.88	_	0.69				0.82	0.88	0.67	0.63	0.58			0.70	0.34				0.67		0.84	0.72	0.57
Edoa	22	(559)	0.91	0.91	0.85	-				0.87	0.92	0.69	0.64	0.59			0.80	0.39				0.78		88.0	0.76	0.60
ŭ	24	(610)	0.95	0.95		0.73				0.93	0.96	0.71	0.66	0.60			0.91	0.44		250		0.89		0.92	0.79	0.62
100		(66D)	0.99	0.99	0.91	0.75				0.99	1.00	0.73	0.67	0.61			1.00	0.50				0.99		0.95	0.82	0.65
18	28	(711)	1.00	1.00	-	0.77				1.00		0.74	0.68	0.61				0.56				1.00		0.99		0.67
10	30	(762)	1.00		0.98	0.79						0.76	0.70	0.62				0.62						1.00	0.89	0.70
S	36	(914)			1.00	0.84						0.81	0.74	0.65				0.81							-	0.76
1.0	> 48	(1219)				0.96						0.92	0.81	0.69				1.00							1.00	0.88

<sup>1</sup> Linear interpolation not permitted.

Linear interpolation not permitted.
 Shaded area with reduced edge distance is permitted provided the installation torque is reduced to 0.30 T<sub>max</sub> for 5d ≤ s ≤ 16-in. and to 0.5 T<sub>max</sub> for s > 16-in.
 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with a thin concrete member) the design can become very conservative. To optimize the design, use Hill PROFIS Anchor Design software or perform anchor calculation using the design equations from ACI 318 Chapter 17.
 Spacing factor reduction in shear, f<sub>NY</sub> assumes an influence of a nearby edge. If no edge exists, then f<sub>NY</sub> = f<sub>NY</sub>.
 Concrete thickness reduction factor in shear, f<sub>NY</sub> assumes an influence of a nearby edge. If no edge exists, then f<sub>NY</sub> = 1.0.

# 3.2.4 HIT-RE 500 V3 Epoxy Adhesive Anchoring System

Table 29 - Steel design strength for Hilti HIT-V and HAS threaded rods

	ASTN	HIT-V M A307 Gra	ide A²	ISO	HAS-E 898 Class	5.B <sup>2</sup>	AS	HAS-E-B STM A193 I	37³	HAS-R stainless steel ASTM F593 - AISI 304/316 SS <sup>2</sup>		
Nominal anchor diameter in.	Tensile <sup>4</sup> \$\phi N_{\text{s}}\$  Ib (kN)	Shear <sup>6</sup> $\phi V_{\underline{M}}$ Ib (kN)	Seismite Shear <sup>4</sup> $\phi V_{\underline{a}, eq}$ Ib (kN)	Tensile <sup>4</sup>	Shear <sup>5</sup> φV <sub>ss</sub> Ib (kN)	Seismic Shear <sup>d</sup> $\phi V_{al,eq}$ Ib (kN)	Tensile <sup>4</sup> \$\phi \text{N}_{\text{s}}  \$\text{Ib (kN)}\$	Shear <sup>6</sup> $\phi V_{\underline{\underline{}}}$ (b (kN)	Seismic Shear <sup>e</sup> $\phi V_{u_{n}eq}$ Ib (kN)	Tensile <sup>4</sup>	Shear <sup>6</sup> $\phi V_{aa}$ Ib (kN)	Seismic Shear <sup>6</sup> $\phi V_{sa,sc}$ Ib (kN)
0.00	3,025	1,675	1,175	3,655	2,020	1,415	7,265	3,775	2,645	5,040	2,790	1,955
3/8	(13.5)	(7.5)	(5.2)	(16.3)	(9.0)	(6.3)	(32.3)	(16.8)	(11.8)	(22.4)	(12.4)	(8.7)
1/2	5,535 (24.6)	3,065 (13.6)	2,145 (9.5)	6,690 (29.8)	3,705 (16.5)	2,595 (11.5)	13,300 (59.2)	6,915 (30.8)	4,840 (21.5)	9,225 (41.0)	5,110 (22.7)	3,575 (15.9)
5/8	8,815 (39.2)	4,880 (21.7)	3,415 (15.2)	10,650 (47.4)	5,900 (26.2)	4,130 (18.4)	21,190 (94.3)	11,020 (49.0)	7,715 (34.3)	14,690 (65.3)	8,135 (36.2)	5,695 (25.3)
3/4	13,045 (58.0)	7,225 (32.1)	5,060 (22.5)	15,765 (70.1)	8,730 (38.8)	6,110 (27.2)	31,360 (139.5)	16,305 (72.5)	11,415 (50.8)	18,480 (82.2)	10,235 (45.5)	7,165 (31.9)
7/8			-	21,755 (96.8)	12,050 (53.6)	8,435 (37.5)	43,285 (192.5)	22,505 (100.1)	15,755 (70.1)	25,510 (113.5)	14,125 (62.8)	9,890 (44.0)
1	23,620 (105.1)	13,085 (58.2)	9,16 <del>0</del> (40.7)	<del>28,540</del> (127.0)	15,805 (70.3)	11,065 (49.2)	56,785 (252.6)	29,525 (131.3)	20,670 (91.9)	33,465 (148.9)	18,535 (82.4)	12,975 (57.7)
1-1/4	93		.5	45,670 (203.1)	25,295 (112.5)	17,705 (78.8)	90,850 (404.1)	47,240 (210.1)	33,070 (147.1)	53,540 (238.2)	29,655 (131.9)	20,760 (92.3)

<sup>1</sup> See Section 3.1.8.6 to convert design strength value to ASD value.

<sup>2</sup> HIT-V, HAS-E, and HAS-R threaded rods are considered brittle steel elements. HIT-V does not comply with % elongation requirements of ASTM A307 Grade A steel. HAS-E does not comply with % elongation requirements of ISO 898-1.

3 HAS-E-B7 rods are considered ductile steel elements.

HAS-E-57 rods are considered ductile steel elements.
 Tensile = φ A<sub>so,N</sub> f<sub>tre</sub> as noted in ACI 318 Chapter 17.
 Shear = φ 0.60 A<sub>so,V</sub> f<sub>tre</sub> as noted in ACI 318 Chapter 17.
 Selsmic Shear = α<sub>Vasis</sub> φV<sub>Vas</sub>: Reduction for selsmic shear only. See section 3.1.8.7 for additional information on seismic applications.

# L=15' / ; tobe field

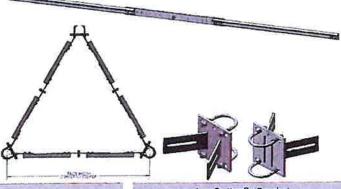


Structural Reinforcement



# **Tapered Self-Support Tower Sub-Horizontals**

- Designed to strengthen tower legs by reducing their KL/r value
- · Complete kits contain (6) Angles, (3) Brackets, (3) Center Plates, (6) 5/8" U-bolts, (27) 5/8" Bolts
- All material is minimum A36, Hardware is A325X, Hot-Dip Galvanized
- Connections use Squirter\* F959 DTI washers to ensure proper installed bolt tension
- · Double bolted angle connections at both ends
- Brackets center themselves on legs with the welded solid rods on backside
- Specify leg butterfly bracket kit + angle / center plate kit [Qtv: (3) per Kit]



		Sub I	Horizontal Angle & Cent	er Plate		
Mfr	Tower Face Width Range (ft)	Center Plate Size	Sub-Horizontal Size	Φ Pn (kips)	Leg Pu* (kips)	Kit#
	5 - 6	3/8" x 3"	2" x 2" x 3/16"	20.00	800	RSH-0605-06
	6-7	3/8" x 3"	2" x 2" x 3/16"	18.00	720	RSH-0606-07
nts	7-9	3/8" x 3"	2" x 2" x 1/4"	13.75	550	RSH-0607-09
Components	9-11	3/8" x 3"	2" x 2" x 1/4"	9.50	380	RSH-0609-11
ď	11 - 13	3/8" x 3"	2-1/2" x 2-1/2" x 1/4"	12.13	485	RSH-0611-13
Ö	13 - 15	1/2" x 4"	2-1/2" x 2-1/2" x 1/4"	8.50	340	RSH-0613-15
-	15 17	1/2" x 4"	3" x 3" x 1/4"	16.50	660	RSH-0615-17
Đ,	17 - 19	1/2" x 4"	3" x 3" x 1/4"	12.50	500	RSH-0617-19
Structura	19 - 21	5/8" x 4"	3-1/2" x 3-1/2" x 1/4"	16.00	640	RSH-0619-21
S	21 - 23	5/8" x 4"	3-1/2" x 3-1/2" x 1/4"	12.88	515	RSH-0621-23
	23 - 25	5/8" x 4"	4" x 4" x 1/4"	15.88	635	RSH-0623-25

Leg Ø Range	U-Bolt	
(O.D.) (in)	Size	Kit#
1.5 - 2.5	5/8" x 2-9/16"	RSH-0515-25
2.5 - 3.5	5/8" x 3-9/16"	RSH-0525-35
3.5 - 4.5	5/8" x 4-9/16"	RSH-0535-45
4.5 - 6.75	5/8" x 6-13/16"	RSH-0545-68
6.75 - 8.625	5/8" x 8-11/16"	RSH-0568-86
8.625 - 10.75	5/8" x 10-13/16"	RSH-0586-00

\*CAPACITY BASED ON FULLY LOADING HORIZONTAL WITH 2.5% OF LEG COMPRESSION NOTE: Order (1) RSH-05##-## kit and (1) RSH-06##-## kit for (1) full sub-horizontal assembly

# **Guyed Tower Torque Arm**

18

24

30

33

36

39

41

42

45

48

54

57

60

72

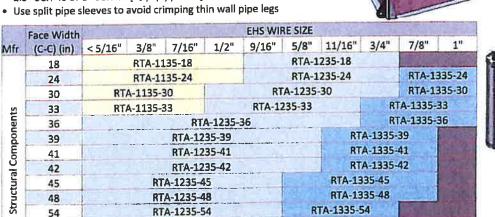
Structural Components

- Designed to provide torsion resistance to guyed towers when needed
- · Kits contain all materials to bolt torque arm onto tower
- All material is minimum A572-50, Hardware is A325X, Hot-Dip Galvanized
- Connections use Squirter F959 DTI washers to ensure proper installed bolt tension
- Fits guyed towers with 1.25" 3.5" OD Legs
- Add split pipe sleeve kit if tower leg is 2" SCH 40, 2.5" SCH 40 or 3" SCH 40 [Qty: (3) per kit]

RTA-1235-57

RTA-1235-60

RTA-1235-72



RTA-1335-72

RTA-1335-57

RTA-1335-60

ì		h SCH 40 Pipe Legs: Pipe Sleeves
	Leg OD	Kit #
и	2.375"	RGA-1000-23
и	2.875"	RGA-1000-28
Ų,	3.5"	RGA-1000-35

LIGHT MEDIUN	HEAVY
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## About AECOM

AECOM (NYSE: AGM) is a global provider of professional technical and management support services to a broad range of markets, including transportation, facilities, environmental, energy, water and government. With approximately 45,000 employees around the world, AECOM is a leader in all of the key markets that it serves. AECOM provides a blend of global reach, local knowledge, innovation, and collaborative technical excellence in delivering solutions that enhance and sustain the world's built, natural, and social environments. A Fortune 500 company, AECOM serves clients in more than 100 countries and has annual revenue in excess of \$6 billion.

More information on AECOM and its services can be found at www.aecom.com.

500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 860-529-8882 Fax: 860-529-3991

# **ATTACHMENT 5**

# AQUARION WATER COMPANY OF

# BUTTERNUT HOLLOW ROAD 0024 Tax ID 199/018

AQUARION WATER COMPANY OF CONNECTICUE OWNERSHIP

ADMINISTRATIVE INFORMATION

11-1142

Property Address HUTTERNUT HOLLOW RCAD 0024

Parent Parcel Number

PARCEL NUMBER

PARKMAY NORTH

2800

Neighborheed

TAXING DISTRICT (NFORMATION

Property Class 430 Hydro Plant

LOT NO 37 BUTTERNUT HOLLOW RD E 11 600 LINDLEY STREET BRIDGEFORT, CT 06606

TRANSFER OF OWNERSHIP

Printed 05/10/2018 Card No. 1

Of

Ek/Pg: 3862, 102 Bk/rg: 1012, 120 20 \$0 CONNECTICUT-AMERICAN WATER CO Ž

> 05/21/2002 04/12/1977

		,	1	1	_						
Jurisdiction 57	Greenwich, CT										
Arca 601	1					VALUATION RECORD	RECORD				
Corporation 057	7	Assessment Year	11/30/2010		10/01/2012	10/01/2013	10/01/2015	015 10/01/2015		10/01/2016	10/01/2017
District 11:	:17	Reason for Change		2010 BAA	2012 List	2013 List	2015 Prelim	lim 2015 Minal	inal	2016 List	2017 bist
	000000000000000000000000000000000000000	VALUATION	I 6798700		12421000	10239700	9672500	00 9672500	500	9672500	9672500
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		Rating	Measured	Table	Fred, Factor						
street or Road:		Soil ID	Acreage		-or-						
Neighborhood:		-or- Actual	-or- Actual Effective	Rifective	Depth Factor	Base	Adjusted	Extended	Influence	ence	
	Land Type	Frontage	Frontage Frontage	Depth	Square Reet	Rate	Rate	Value	Factor	tor	Value
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Bst. Cost Field Visit Est. SqFt FilingDate Permir Number Type 

Supplemental Cards

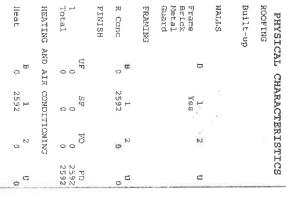
TRUE TAX VALUE

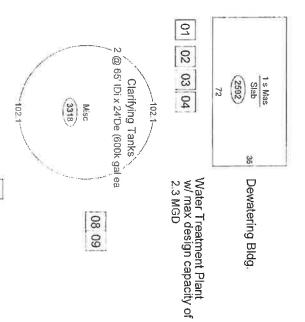
Supplemental Cards TOTAL LAND VALUE

P: 20 aprs

9672500

BUTTERNUT HOLLOW ROAD GOZA





1 Thickening Tank samas clarifying tanks 06
2-540k gal retention basins07

# SUMMARY OF IMPROVEMENTS

(LCM: 150.00)

SPECIAL FEATURES

ID	51									C : Remod 2012		Description :
HSTLSTOR 0.00 Avg 1999 2005 V3 0.00 N 0.00 2592 0 0 0 150 100 ELEVITANK 123.00 Avg 1970 1985 AV 44.50 N 4.62 500000 2310000 3 0 100 100 FENCECL 8.00 Avg 1999 2000 V3 0.00 N 0.00 0 0 0 SV 100 100 C1ft. Tk 0.00 Avg 1999 2000 V3 0.00 N 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0												Value
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bd 04/19/2012 Data Collector/Date

TOG 10/01/2015 Appraiser/Date

Neighborhood

Neigh 2800 AV

Supplemental Cards

Place: Ct - Fairfield Map: Parcel Outline (Default) Date rendered: // Wyckham Places: 0 Medium City Minor City O Small City Towns & Villages
Of Dr

Office Villages Interstates Highways Merritt Pkwy Roads Railways General: Butternut Hollow Rd Default Land Agriculture Merritt PkW Parks Forests Water

Property Shark

Butternut Hollow Rd

Add notes here ...

Tinker Ly

# **ATTACHMENT 6**

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Kenneth C. Baldwin, Esq. Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103				neopost# 11/20/2019 US POSTA	画\$003.159	2
	Postmaster, per (name of receiving employee)	(трюуее)			ZIP 06103 041L12203937	03937
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USPS® Tracking Number Firm-specific Identifier	Add (Name, Street, City, 8	Address (Name, Street, City, State, and ZiP Code™)	Postage	Fee	Special Handling	Parcel Airlift
1,	Peter Tesei, First Selectman Town of Creenviel 101 Field Point Road Greenwich, CT 06830					
2.	Katie DeLuca, Director of Planning and Zoning Town of Greenwich 101 Field Point Road Greenwich, CT 06830	ning				
3.	Aquarion Water Company of Connecticut 600 Lindley Street Bridgeport, CT 06606	ticut		AOUSF		
4.	State of Connecticut Department of Transportation 2800 Berlin Tumpike Newington, CT 06131		970	0610 000 0 7 NON	ATION 0610	
5,		(Cc)		)   Call	3	
6.			9			