August 20, 2021

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: $\quad$ Notice of Exempt Modifications - AT\&T Site CT1255
AT\&T Telecommunications Facility @ 8 Upper Meadow Lane, Granby, CT 06035

Dear Ms. Bachman,
New Cingular Wireless, PCS, LLC ("AT\&T") is proposing a wireless telecommunications facility on an existing $+/-150$ feet monopole tower at the above referenced address (Latitude $=41.9533$, Longitude $=$ - 71.82984) and within the existing fenced compound. Said monopole tower is owned and operated by American Tower Corporation.

AT\&T desires to modify the existing telecommunications facility by: installing a WIC (Walk-In Cabinet) and a Generator on proposed concrete pads inside a $20^{\prime} \times 10^{\prime}$ ground space within the existing compound and install (9) antennas, (9) RRUS Radios, (2) Squid and mounts/cabling on the existing tower at 134 ' as more particularly detailed and described on the enclosed Construction Drawings prepared by Dewberry Engineers Inc., dated August 4, 2021. The overall height of the existing tower is and will remain at 150 feet and no changes will be made to the compound dimensions.

Please accept this letter as notification pursuant to R.C.S.A §16-50j-73 for construction that constitutes an exempt modification pursuant to R.C.S.A §16-50j-72(b)(2). In accordance with R.C.S.A §16-50j-73, a copy of this letter is being sent to the following individuals: American Tower Corporation as Tower Operator/Owner; Tower Meadow LLC as Property Owners; William Smith as Town Manager of the Town of Granby and Mark Lockwood as Planning \& Zoning Chairman for the Town of Granby.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. §16-50j-72(b)(2). Specifically:

1. The proposed modifications will NOT result in an increase in the height of the existing structure.
2. The proposed modifications will NOT require an extension of the site boundary.
3. The proposed modifications will NOT increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the modified facility will NOT increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. Please see the RF emissions calculation for AT\&T's modified facility enclosed herewith.
5. The proposed modifications will NOT cause an ineligible change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading. Please see the structural analysis dated March 22, 2021 prepared by American Tower Corporation enclosed herewith.

For the foregoing reasons, AT\&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A §16-50j-72(b)(2).

If you have any questions, please feel free to contact me.
Sincerely,

## Kimberly Revak

## Kimberly Revak

Site Acquisition Consultant - Agent for AT\&T
Centerline Communications, LLC
38 Treeline Court
Fishkill, NY 12524
Phone: (845) 242-6152
krevak@clinellc.com

Enclosures: Exhibit 1 - Property Card and GIS
Exhibit 2 - Construction Drawings dated 07/02/21
Exhibit 3 - Structural Analysis Report
Exhibit 4 - Antenna Mount Analysis Report
Exhibit 5 - NIER Study Report
Exhibit 6 - Tower Approval
Exhibit 7 - (4) Notice Confirmations

Cc: $\quad$ American Tower Corporation - Tower Operator/Owner
Tower Meadow LLC - Property Owner
William Smith - Tower Manager of the Town of Granby
Mark Lockwood - Planning \& Zoning Chairman for the Town of Granby

## Exhibit 1

## Property Card and GIS

## 8 UPPER MEADOW

| Location | 8 UPPER MEADOW | Mblu | G-30/69/134// |
| ---: | ---: | ---: | ---: |
| Acct\# | 14750008 | Owner | TOWER MEADOW LLC |
| Assessment | $\$ 221,550$ | Appraisal | $\$ 316,500$ |
| PID 101221 | Building Count | 1 |  |

## Current Value

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2017 | \$129,500 | \$187,000 | \$316,500 |
| Assessment |  |  |  |
| Valuation Year | Improvements | Land | Total |
| 2017 | \$90,650 | \$130,900 | \$221,550 |

## Owner of Record

Owner TOWER MEADOW LLC

Sale Price $\$ 0$
Certificate
Book \& Page 339/0689
Sale Date 12/20/2006

## Ownership History

| Ownership History |  |  |  |  |  |  |
| :--- | ---: | :---: | :---: | :---: | :---: | :---: |
| Owner | Certificate | Boak \& Page | Sale Date |  |  |  |
| TOWER MEADOW LLC | $\$ 0$ |  | $339 / 0689$ | $12 / 20 / 2006$ |  |  |
| TOWER MEADOW LLC | $\$ 0$ |  | $334 / 0976$ | $07 / 20 / 2006$ |  |  |
| GIRARD MEADOW LLC | $\$ 0$ |  | $277 / 0120$ | $01 / 09 / 2003$ |  |  |
| GIRARD ELAINE J | $\$ 0$ |  | $161 / 935$ | $06 / 19 / 1989$ |  |  |

## Building Information

Building 1 : Section 1

## Year Built:

Living Area: 0
Replacement Cost: \$0
Building Percent Good:

## Replacement Cost

## Less Depreciation:

## Building Attributes

| Building Attributes |  |  |
| :---: | :---: | :---: |
| Field | Description |  |
| Style | Outbuildings |  |
| Model |  |  |
| Grade: |  |  |
| Stories: |  |  |
| Occupancy |  |  |
| Exterior Wall 1 |  |  |
| Exterior Wall 2 |  | - |
| Roof Structure: |  | /imas vgsi.cm/photos2/Gran |

(http://images.vgsi.com/photos2/GranbyCTPhotos//^00100197/59.jpg)

## Building Layout

Building Layout
(http://images.vgsi.com/photos2/GranbyCTPhotos//Sketches/101221_1013

| Building Sub-Areas (sq ft) | Legend |
| :---: | :---: |
| No Data for Building Sub-Areas |  |

## Extra Features

| Extra Features | Legend |
| :--- | :--- |
| No Data for Extra Features |  |

## Land

| Land Use |  | Land Line Valuation |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Use Code | 4310 |  | Size (Acres) | 0.79 |
| Description | TEL REL TW | R2A | Frontage |  |
| Zone | Depth |  |  |  |
| Neighborhood |  | Assessed Value | $\$ 130,900$ |  |

Alt Land Appr No
Appraised Value $\$ 187,000$
Category

## Outbuildings

| Outbuildings |  |  |  |  |  |  |  |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Code | Description | Sub Code | Sub Description | Size |  | Value | Bldg \# |
| CELL | CELL TOWER |  |  | 1 UNITS | $\$ 112,500$ |  |  |
| FN4 | FENCE-8' CHAIN |  |  | 320 L.F. | 1 |  |  |
| SHP5 | W/IMPROV GOOD |  |  | $\$ 4,000$ |  | 1 |  |

## Valuation History

| Appraisal |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | Valuation Year | Improvements | Land |  |  |
| 2020 |  | $\$ 129,500$ | $\$ 187,000$ | Total |  |
| 2019 | $\$ 129,500$ | $\$ 187,000$ |  |  |  |
| 2018 | $\$ 129,500$ | $\$ 187,000$ | $\$ 316,500$ |  |  |


| Assessment |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: |
|  | Valuation Year | Improvements |  |  |  |
| 2020 |  | $\$ 90,650$ | Land |  |  |
| 2019 | $\$ 90,650$ | $\$ 130,900$ | Total |  |  |
| 2018 | $\$ 90,650$ | $\$ 130,900$ | $\$ 221,550$ |  |  |

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## Exhibit 2

Construction Drawings





－（2）


|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |




(2) ANTENNA SCHEDULE











(1) PLUMBING DIAGRAM

|  |  |  |  |  |  | (ex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |



## Exhibit 3

## Structural Analysis Report

## AMERICAN TOWVER ${ }^{*}$

CORPORATION
This report was prepared for American Tower Corporation by
TVWER
ENGINEERING
PROFESSIDNALS

## Structural Analysis Report

| Structure | 151 ft Monopole |  |
| :---: | :---: | :---: |
| ATC Site Name | West Granby, CT CT, CT |  |
| ATC Asset Number | : 411186 |  |
| Engineering Number | 13626835_C3_03 |  |
| Proposed Carrier | AT\&T MOBILITY |  |
| Carrier Site Name | : MRCTB050155 |  |
| Carrier Site Number | : CT2393S |  |
| Site Location | : 49 Upper Meadow |  |
|  | Granby, CT 06035 |  |
|  | 41.953300,-72.829800 |  |
| County | : Hartford |  |
| Date | : March 22, 2021 |  |
| Max Usage | : 37\% |  |
| Result | : Pass |  |
| Prepared By: Austin Wilson TEP | Reviewed By: |  |
| tustai Wissar |  | 3/22/2021 |

Eng. Number 13626835_C3_03

## Table of Contents

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Calculations ..... Attached

## Introduction

The purpose of this report is to summarize results of a structural analysis performed on the 151 ft monopole to reflect the change in loading by AT\&T MOBILITY.

## Supporting Documents

| Tower Drawings | EEI Job \#14945, dated June 22, 2007 |
| :--- | :--- |
| Foundation Drawing | EEI Job \#14945, dated June 22, 2007 |
| Geotechnical Report | JGI Project \#04109G, dated January 27, 2004 |

## Analysis

The tower was analyzed using American Tower Corporation's tower analysis software. This program considers an elastic three-dimensional model and second-order effects per ANSI/TIA-222.

| Basic Wind Speed: | $93 \mathrm{mph}\left(3-\right.$-second Gust, $\mathrm{V}_{\text {ASD }}$ ) / 120 mph (3-second Gust, $\mathrm{V}_{\text {ULT }}$ ) |
| :--- | :--- |
| Basic Wind Speed w/ Ice: | $50 \mathrm{mph}(3-$-Second Gust) w/ 1" radial ice concurrent |
| Code: | ANSI/TIA-222-G / 2015 IBC / 2018 Connecticut State Building Code |
| Structure Class: | II |
| Exposure Category: | B |
| Topographic Category: | 1 |
| Crest Height: | 0 ft |
| Spectral Response: | Ss $=0.18, \mathrm{~S}_{1}=0.06$ |
| Site Class: | D - Stiff Soil |

## Conclusion

Based on the analysis results, the structure meets the requirements per the applicable codes listed above. The tower and foundation can support the equipment as described in this report.

If you have any questions or require additional information, please contact American Tower via email at Engineering@americantower.com. Please include the American Tower site name, site number, and engineering number in the subject line for any questions.

Existing and Reserved Equipment

| Elev. ${ }^{1}(\mathrm{ft})$ | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 150.0 | 1 | VZW Unused Reserve (3171.74 sqin) | Low Profile Platform | (18) 1 5/8" Coax <br> (2) 1 1/4" Hybriflex Cable <br> (1) 1/2" Coax | VERIZON WIRELESS |
|  | 6 | $48^{\prime \prime} \times 4$ P Panel |  |  |  |
|  | 2 | $48^{\prime \prime} \times 6$ " Panel |  |  |  |
|  | 3 | 48 " x 12" Panel |  |  |  |
|  | 4 | $48^{\prime \prime} \times 12 \mathrm{c} \times 7$ " Panel |  |  |  |
| 146.0 | 2 | SSB (27lb) |  |  |  |
|  | 3 | RRU |  |  |  |
|  | 9 | 96" x 12" Panel |  |  |  |
|  | 2 | Amphenol Antel LPA-70080/8CF |  |  |  |
|  | 4 | Amphenol Antel LPA-80063-8CF-EDIN-X |  |  |  |

## Equipment to be Removed

| Elev. $^{1}(\mathrm{ft})$ | Qty | Antenna | Mount Type | Lines | Carrier |
| :--- | :--- | :--- | :--- | :--- | :--- |
| No loading was considered as removed as part of this analysis. |  |  |  |  |  |

Proposed Equipment

| Elev. ${ }^{1}(\mathrm{ft})$ | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 135.0 | 3 | Ericsson RRUS 8843 B2, B66A | Sector Frames | (2) 0.39 " $(10 \mathrm{~mm})$ <br> Fiber Trunk <br> (4) 0.92 " ( 23.4 mm ) Cable <br> (2) $21 / 2^{\prime \prime}$ conduit | AT\&T MOBILITY |
|  | 3 | Ericsson RRUS 4478 B14 |  |  |  |
|  | 3 | Ericsson RRUS 4449 B5, B12 |  |  |  |
|  | 3 | Ericsson AIR 6449 B77D |  |  |  |
|  | 2 | Raycap DC9-48-60-24-8C-EV |  |  |  |
|  | 3 | CCI DMP65R-BU8D |  |  |  |
|  | 3 | CCI TPA65R-BU8D |  |  |  |

${ }^{1}$ Contracted elevations are shown for appurtenances within contracted installation tolerances. Appurtenances outside of contract limits are shown at installed elevations.
Install proposed lines inside the pole shaft.

## Structure Usages

| Structural Component | Controlling <br> Usage | Pass/Fail |
| :---: | :---: | :---: |
| Anchor Bolts | $21 \%$ | Pass |
| Shaft | $27 \%$ | Pass |
| Base Plate | $10 \%$ | Pass |

## Foundations

| Reaction Component | Original Design <br> Reactions | Analysis Reactions | \% of Design |
| :---: | :---: | :---: | :---: |
| Moment (Kips-Ft) | $8,029.8$ | $2,621.7$ | $33 \%$ |
| Shear (Kips) | 64.3 | 24.0 | $37 \%$ |

The structure base reactions resulting from this analysis are acceptable when compared to those shown on the original structure drawings, therefore no modification or reinforcement of the foundation will be required.

Deflection and Sway*

| Antenna Elevation (ft) | Antenna | Carrier | Deflection (ft) | Sway (Rotation) ( ${ }^{\circ}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| 135.0 | Ericsson RRUS 8843 B2, B66A | AT\&T MOBILITY | 0.484 | 0.412 |
|  | Ericsson RRUS 4478 B14 |  |  |  |
|  | Ericsson RRUS 4449 B5, B12 |  |  |  |
|  | Ericsson AIR 6449 B77D |  |  |  |
|  | Raycap DC9-48-60-24-8C-EV |  |  |  |
|  | CCI DMP65R-BU8D |  |  |  |
|  | CCI TPA65R-BU8D |  |  |  |

[^0]Standard Conditions
All engineering services performed by A.T. Engineering Service, PLLC are prepared on the basis that the information used is current and correct. This information may consist of, but is not limited to the following:

- Information supplied by the client regarding antenna, mounts and feed line loading
- Information from drawings, design and analysis documents, and field notes in the possession of A.T. Engineering Service, PLLC

It is the responsibility of the client to ensure that the information provided to A.T. Engineering Service, PLLC and used in the performance of our engineering services is correct and complete.

All assets of American Tower Corporation, its affiliates and subsidiaries (collectively "American Tower") are inspected at regular intervals. Based upon these inspections and in the absence of information to the contrary, American Tower assumes that all structures were constructed in accordance with the drawings and specifications.

Unless explicitly agreed by both the client and A.T. Engineering Service, PLLC, all services will be performed in accordance with the current revision of ANSI/TIA-222.

All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. A.T. Engineering Service, PLLC is not responsible for the conclusions, opinions and recommendations made by others based on the information supplied herein.



Load Case : 1.2D + 1.6W

| Max Ratio 26.99\% at 0.0 ft |
| :--- |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :--- | ---: | :--- |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 |  |
| Customer: AT\&T MOBILITY |  |  |

## Analysis Parameters

| Location : | Hartford County, CT | Height (ft) : |
| :--- | :--- | :--- |
| Code : | ANSI/TIA-222-G | Base Diameter (in) : |
| Shape : | 18 Sides | Top Diameter (in) : |
| Pole Type : | Taper | Taper (in/ft) : |
| Pole Manfacturer : |  | Rotation (deg) : |


|  |  | Ice \& Wind Parameters |  |
| :--- | :--- | :--- | :--- |
| Structure Class: | II | Design Wind Speed Without Ice: |  |
| Exposure Category: | B | Design Wind Speed With Ice: |  |
| Topographic Category: | 1 | Operational Wind Speed: |  |
| Crest Height: | 0 ft | Design Ice Thickness: |  |

## Seismic Parameters

| Analysis Method: | Equivalent Modal Analysis \& Equivalent Lateral Force Methods |
| :--- | :--- |
| Site Class: | D - Stiff Soil |

Period Based on Rayleigh Method (sec): 1.53

| $\mathrm{T}_{\mathrm{L}}(\mathrm{sec}):$ | 6 | $\mathrm{p}:$ | 1.3 | $\mathrm{C}_{\mathrm{s}}:$ | 0.045 |
| :--- | ---: | :--- | :--- | :--- | :--- |
| $\mathrm{~S}_{\mathrm{s}}:$ | 0.177 | $\mathrm{~S}_{1}:$ | 0.065 | $\mathrm{C}_{\mathrm{S}}$ Max: | 0.045 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.600 | $\mathrm{~F}_{\mathrm{V}}:$ | 2.400 | $\mathrm{C}_{\mathrm{s}}$ Min: | 0.030 |
| $\mathrm{~S}_{\mathrm{S}}:$ | 0.189 | $\mathrm{~S}_{\mathrm{di}}:$ | 0.104 |  |  |


|  | $\quad$ Load Cases |
| :--- | :--- |
| $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 93 mph with No Ice |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 93 mph with No Ice (Reduced DL) |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ | 50 mph with 1.00 in Radial Ice |
| $(1.2+0.2 \mathrm{Sds})^{*} \mathrm{DL}+$ E ELFM | Seismic Equivalent Lateral Forces Method |
| $(1.2+0.2 \mathrm{Sds})^{*} \mathrm{DL}+$ E EMAM | Seismic Equivalent Modal Analysis Method |
| $(0.9-0.2 \mathrm{Sds})^{*} \mathrm{DL}+$ E ELFM | Seismic (Reduced DL) Equivalent Lateral Forces Method |
| $(0.9-0.2 \mathrm{Sds}) *$ DL + E EMAM | Seismic (Reduced DL) Equivalent Modal Analysis Method |
| $1.0 \mathrm{D}+1.0 \mathrm{~W}$ | Serviceability 60 mph |



## Discrete Appurtenance Properties

| Attach <br> Elev <br> (ft) | Description | Qty | Ка | Vert Ecc (ft) | Weight (lb) | No Ice EPAa (sf) | Orientation Factor | Weight (lb) | EPAa Orientation <br> (sf) Factor |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150.00 | Generic 48" x 4" Panel | 6 | 0.80 | 2.000 | 20.00 | 2.080 | 0.81 | 72.91 | 4.173 | 0.81 |
| 150.00 | Generic 48" x 6" Panel | 2 | 0.80 | 2.000 | 20.00 | 2.867 | 0.80 | 96.57 | 5.043 | 0.80 |
| 150.00 | Generic 48" x 12" Panel | 3 | 0.80 | 2.000 | 30.00 | 5.067 | $7 \quad 0.78$ | 181.16 | 7.565 | 0.78 |
| 150.00 | Generic 48" x 12" x 7" Panel | 4 | 0.80 | 2.000 | 35.00 | 5.067 | $7 \quad 0.82$ | 195.37 | 7.565 | 0.82 |
| 150.00 | VZW Unused Reserve (3171.74 | 1 | 0.80 | 0.000 | 1,226.00 | 22.026 | $6 \quad 0.90$ | 2,366.38 | 42.514 | 0.90 |
| 148.00 | Round Low Profile Platform | 1 | 1.00 | 0.000 | 1,500.00 | 21.700 | $0 \quad 1.00$ | 2,363.88 | 47.300 | 1.00 |
| 146.00 | Generic SSB (27lb) | 2 | 0.80 | 0.000 | 27.00 | 3.200 | 0.79 | 164.88 | 4.786 | 0.79 |
| 146.00 | Generic RRU | 3 | 0.80 | 0.000 | 75.00 | 4.193 | $3 \quad 0.67$ | 233.68 | 5.998 | 0.67 |
| 146.00 | Generic 96" x 12" Panel | 9 | 0.80 | 0.000 | 45.00 | 11.467 | 70.67 | 332.96 | 15.777 | 0.67 |
| 146.00 | Amphenol Antel LPA-70080/8CF | 2 | 0.80 | 0.000 | 24.00 | 12.832 | 20.71 | 331.47 | 17.726 | 0.71 |
| 146.00 | Amphenol Antel LPA-80063-8CF- | 4 | 0.80 | 0.000 | 38.00 | 13.653 | 30.75 | 489.57 | 18.531 | 0.75 |
| 135.00 | Ericsson RRUS 8843 B2, B66A | 3 | 0.80 | 0.000 | 72.00 | 1.639 | 9 0.50 | 152.88 | 2.754 | 0.50 |
| 135.00 | Ericsson RRUS 4478 B14 | 3 | 0.80 | 0.000 | 59.90 | 1.842 | 20.50 | 132.86 | 3.026 | 0.50 |
| 135.00 | Ericsson RRUS 4449 B5, B12 | 3 | 0.80 | 0.000 | 71.00 | 1.969 | 90.50 | 156.05 | 3.200 | 0.50 |
| 135.00 | Ericsson AIR 6449 B77D | 3 | 0.80 | 0.000 | 81.60 | 4.028 | $8 \quad 0.70$ | 235.31 | 5.839 | 0.70 |
| 135.00 | Raycap DC9-48-60-24-8C-EV | 2 | 0.80 | 0.000 | 16.00 | 4.788 | 88.75 | 186.36 | 6.729 | 0.75 |
| 135.00 | CCI DMP65R-BU8D | 3 | 0.80 | 0.000 | 95.70 | 17.871 | 10.63 | 544.21 | 22.734 | 0.63 |
| 135.00 | Generic Flat Light Sector Frame | 3 | 0.75 | 0.000 | 400.00 | 17.900 | 0.75 | 797.14 | 37.811 | 0.75 |
| 135.00 | CCI TPA65R-BU8D | 3 | 0.80 | 0.000 | 82.50 | 18.089 | $9 \quad 0.63$ | 537.48 | 22.961 | 0.63 |
| Totals | Num Loadings:19 | 60 |  |  | 6,620.10 |  |  | 21,374.96 |  |  |

## Linear Appurtenance Properties

Load Case Azimuth (deg) :

| Elev From (ft) | $\begin{aligned} & \text { Elev } \\ & \text { To } \\ & \text { (ft) } \\ & \hline \end{aligned}$ | Qty Description | Coax Dia (in) | Coax Wt (lb/ft) |  |  | Dist Between Rows (in) | Dist Between Cols (in) | Azimuth (deg) | Dist From Face (in) | $\begin{aligned} & \text { Expose } \\ & \text { To } \\ & \text { Wind } \end{aligned}$ | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 150.00 | $1815 / 8$ " Coax | 1.98 | 0.82 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | VERIZON WIRELESS |
| 0.00 | 146.00 | 21 1/4" Hybriflex Cable | 1.54 | 1.00 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | VERIZON WIRELESS |
| 0.00 | 146.00 | 1 1/2" Coax | 0.63 | 0.15 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | VERIZON WIRELESS |
| 0.00 | 135.00 | 2 0.39" (10mm) Fiber | 0.39 | 0.06 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | AT\&T MOBILITY |
| 0.00 | 135.00 | 4 0.92" (23.4mm) Cable | 0.92 | 0.89 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | AT\&T MOBILITY |
| 0.00 | 135.00 | $221 / 2^{\prime \prime}$ conduit | 2.88 | 5.79 | N | 0 | 0.00 | 0.00 | 0 | 0.00 | N | AT\&T MOBILITY |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| ---: | ---: | ---: | ---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | $3 / 22 / 2021$ 7:18:46 PM |

Customer: AT\&T MOBILITY


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :---: | ---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | $3 / 22 / 2021$ 7:18:46 PM |
| Customer: AT\&T MOBILITY |  |  |

## Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (lb) | Dead Load (lb) | Wind FX <br> (lb) | $\qquad$ | $\begin{gathered} \text { Moment } \\ \text { MZ } \\ (\mathrm{lb}-\mathrm{ft}) \end{gathered}$ | Dead Load <br> (Ib) | Wind FX <br> (Ib) | Dead Load (lb) | Wind FX <br> (lb) | Dead Load <br> (Ib) | Torsion MY <br> (lb-ft) | Moment MZ <br> (lb) |
| 0.00 |  | 239.7 | 0.0 |  |  |  |  | 0.0 | 0.0 | 239.7 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 474.3 | 2,163.6 |  |  |  |  | 0.0 | 193.0 | 474.3 | 2,356.6 | 0.0 | 0.0 |
| 10.00 |  | 464.1 | 2,116.9 |  |  |  |  | 0.0 | 193.0 | 464.1 | 2,309.9 | 0.0 | 0.0 |
| 15.00 |  | 453.8 | 2,070.2 |  |  |  |  | 0.0 | 193.0 | 453.8 | 2,263.2 | 0.0 | 0.0 |
| 20.00 |  | 443.5 | 2,023.5 |  |  |  |  | 0.0 | 193.0 | 443.5 | 2,216.5 | 0.0 | 0.0 |
| 25.00 |  | 433.3 | 1,976.8 |  |  |  |  | 0.0 | 193.0 | 433.3 | 2,169.8 | 0.0 | 0.0 |
| 30.00 |  | 428.0 | 1,930.1 |  |  |  |  | 0.0 | 193.0 | 428.0 | 2,123.2 | 0.0 | 0.0 |
| 35.00 |  | 431.3 | 1,883.4 |  |  |  |  | 0.0 | 193.0 | 431.3 | 2,076.5 | 0.0 | 0.0 |
| 40.00 |  | 437.0 | 1,836.8 |  |  |  |  | 0.0 | 193.0 | 437.0 | 2,029.8 | 0.0 | 0.0 |
| 45.00 |  | 275.9 | 1,790.1 |  |  |  |  | 0.0 | 193.0 | 275.9 | 1,983.1 | 0.0 | 0.0 |
| 46.28 | Bot - Section 2 | 223.9 | 449.4 |  |  |  |  | 0.0 | 49.3 | 223.9 | 498.7 | 0.0 | 0.0 |
| 50.00 |  | 335.8 | 2,612.1 |  |  |  |  | 0.0 | 143.8 | 335.8 | 2,755.8 | 0.0 | 0.0 |
| 53.73 | Top - Section 1 | 225.4 | 2,565.6 |  |  |  |  | 0.0 | 144.1 | 225.4 | 2,709.7 | 0.0 | 0.0 |
| 55.00 |  | 282.3 | 434.2 |  |  |  |  | 0.0 | 49.0 | 282.3 | 483.1 | 0.0 | 0.0 |
| 60.00 |  | 449.4 | 1,682.4 |  |  |  |  | 0.0 | 193.0 | 449.4 | 1,875.4 | 0.0 | 0.0 |
| 65.00 |  | 447.0 | 1,635.7 |  |  |  |  | 0.0 | 193.0 | 447.0 | 1,828.7 | 0.0 | 0.0 |
| 70.00 |  | 443.5 | 1,589.0 |  |  |  |  | 0.0 | 193.0 | 443.5 | 1,782.1 | 0.0 | 0.0 |
| 75.00 |  | 439.0 | 1,542.3 |  |  |  |  | 0.0 | 193.0 | 439.0 | 1,735.4 | 0.0 | 0.0 |
| 80.00 |  | 433.6 | 1,495.7 |  |  |  |  | 0.0 | 193.0 | 433.6 | 1,688.7 | 0.0 | 0.0 |
| 85.00 |  | 427.3 | 1,449.0 |  |  |  |  | 0.0 | 193.0 | 427.3 | 1,642.0 | 0.0 | 0.0 |
| 90.00 |  | 382.7 | 1,402.3 |  |  |  |  | 0.0 | 193.0 | 382.7 | 1,595.3 | 0.0 | 0.0 |
| 94.09 | Bot - Section 3 | 209.0 | 1,112.6 |  |  |  |  | 0.0 | 157.9 | 209.0 | 1,270.5 | 0.0 | 0.0 |
| 95.00 |  | 243.1 | 429.1 |  |  |  |  | 0.0 | 35.1 | 243.1 | 464.2 | 0.0 | 0.0 |
| 99.92 | Top - Section 2 | 208.0 | 2,277.4 |  |  |  |  | 0.0 | 190.1 | 208.0 | 2,467.5 | 0.0 | 0.0 |
| 100.00 |  | 206.8 | 14.9 |  |  |  |  | 0.0 | 2.9 | 206.8 | 17.9 | 0.0 | 0.0 |
| 105.00 |  | 402.8 | 967.9 |  |  |  |  | 0.0 | 193.0 | 402.8 | 1,160.9 | 0.0 | 0.0 |
| 110.00 |  | 393.3 | 932.9 |  |  |  |  | 0.0 | 193.0 | 393.3 | 1,125.9 | 0.0 | 0.0 |
| 115.00 |  | 383.2 | 897.9 |  |  |  |  | 0.0 | 193.0 | 383.2 | 1,090.9 | 0.0 | 0.0 |
| 120.00 |  | 372.6 | 862.9 |  |  |  |  | 0.0 | 193.0 | 372.6 | 1,055.9 | 0.0 | 0.0 |
| 125.00 |  | 361.6 | 827.9 |  |  |  |  | 0.0 | 193.0 | 361.6 | 1,020.9 | 0.0 | 0.0 |
| 130.00 |  | 350.0 | 792.9 |  |  |  |  | 0.0 | 193.0 | 350.0 | 985.9 | 0.0 | 0.0 |
| 135.00 | Appurtenance(s) | 234.7 | 757.8 | 4,130.7 | $7 \quad 0.0$ | 0.0 | 3,144.1 | 0.0 | 193.0 | 4,365.5 | 4,095.0 | 0.0 | 0.0 |
| 136.87 | Bot - Section 4 | 167.7 | 274.0 |  |  |  |  | 0.0 | 37.9 | 167.7 | 311.8 | 0.0 | 0.0 |
| 140.00 |  | 145.2 | 754.5 |  |  |  |  | 0.0 | 63.6 | 145.2 | 818.0 | 0.0 | 0.0 |
| 141.22 | Top - Section 3 | 162.4 | 287.8 |  |  |  |  | 0.0 | 24.8 | 162.4 | 312.5 | 0.0 | 0.0 |
| 145.00 |  | 153.9 | 352.1 |  |  |  |  | 0.0 | 76.7 | 153.9 | 428.8 | 0.0 | 0.0 |
| 146.00 | Appurtenance(s) | 94.3 | 90.9 | 4,624.4 | $4 \quad 0.0$ | 0.0 | 1,060.8 | 0.0 | 20.3 | 4,718.8 | 1,172.0 | 0.0 | 0.0 |
| 148.00 | Appurtenance(s) | 124.2 | 179.1 | 888.0 | 0.0 | 0.0 | 1,800.0 | 0.0 | 35.4 | 1,012.2 | 2,014.5 | 0.0 | 0.0 |
| 150.00 | Appurtenance(s) | 92.0 | 175.3 | 2,075.6 | $6 \quad 0.0$ | 2,848.3 | 1,939.2 | 0.0 | 35.4 | 2,167.6 | 2,149.9 | 0.0 | 0.0 |
| 151.00 |  | 30.4 | 86.3 |  |  |  |  | 0.0 | 0.0 | 30.4 | 86.3 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 24,225.0 | 60,172.8 | 0.00 | 0.00 |

Page: 4
Site Number: $411186 \quad$ Code: ANSI/TIA-222-G © 2007-2021 by ATC IP LLC. All rights reserved.

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:49 PM
Customer: AT\&T MOBILITY

| Load Case: $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 93 mph with No Ice |
| :---: | :---: |
| Gust Response Factor :1.10 |  |
| Dead Load Factor: 1.20 |  |
| Wind Load Factor $: 1.60$ |  |

Calculated Forces

| Seg Elev | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \end{gathered}$ | $\begin{aligned} & \mathrm{Vu} \\ & \mathrm{FX}(-) \end{aligned}$ | Tu <br> MY | Mu MZ | Mu <br> MX | Resultant Moment | $\begin{aligned} & \text { phi } \\ & \text { Pn } \end{aligned}$ | $\begin{aligned} & \text { phi } \\ & \text { Vn } \end{aligned}$ | phi | phi | Total |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (ft) | (kips) | (kips) | (ft-kips) | (ft-kips) | (ft-kips) | (ft-kips) | (kips) | (kips) | (ft-kips) | (ft-kips) | (in) | (deg) | Ratio |
| 0.00 | -60.16 | -24.02 | 0.00 | -2,621.68 | 0.00 | 2,621.68 | 7,216.29 | 3,608.15 | 20,023.1 | 10,026.4 | 0.00 | 0.00 | 0.270 |
| 5.00 | -57.78 | -23.60 | 0.00 | -2,501.60 | 0.00 | 2,501.60 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.03 | -0.06 | 0.267 |
| 10.00 | -55.45 | -23.19 | 0.00 | -2,383.60 | 0.00 | 2,383.60 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.13 | -0.12 | 0.263 |
| 15.00 | -53.16 | -22.79 | 0.00 | -2,267.64 | 0.00 | 2,267.64 | 6,915.90 | 3,457.95 | 17,951.6 | 8,989.14 | 0.28 | -0.18 | 0.260 |
| 20.00 | -50.92 | -22.39 | 0.00 | -2,153.69 | 0.00 | 2,153.69 | 6,810.85 | 3,405.43 | 17,272.5 | 8,649.09 | 0.51 | -0.24 | 0.257 |
| 25.00 | -48.73 | -22.00 | 0.00 | -2,041.73 | 0.00 | 2,041.73 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.80 | -0.31 | 0.253 |
| 30.00 | -46.58 | -21.62 | 0.00 | -1,931.70 | 0.00 | 1,931.70 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 1.15 | -0.37 | 0.249 |
| 35.00 | -44.48 | -21.22 | 0.00 | -1,823.62 | 0.00 | 1,823.62 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 1.57 | -0.44 | 0.245 |
| 40.00 | -42.43 | -20.82 | 0.00 | -1,717.52 | 0.00 | 1,717.52 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 2.07 | -0.50 | 0.241 |
| 45.00 | -40.44 | -20.55 | 0.00 | -1,613.43 | 0.00 | 1,613.43 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 2.63 | -0.57 | 0.237 |
| 46.28 | -39.93 | -20.35 | 0.00 | -1,587.20 | 0.00 | 1,587.20 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 2.78 | -0.59 | 0.236 |
| 50.00 | -37.16 | -20.02 | 0.00 | -1,511.43 | 0.00 | 1,511.43 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 3.26 | -0.64 | 0.232 |
| 53.73 | -34.44 | -19.78 | 0.00 | -1,436.73 | 0.00 | 1,436.73 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 3.78 | -0.69 | 0.221 |
| 55.00 | -33.95 | -19.52 | 0.00 | -1,411.64 | 0.00 | 1,411.64 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 3.97 | -0.71 | 0.220 |
| 60.00 | -32.05 | -19.08 | 0.00 | -1,314.05 | 0.00 | 1,314.05 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 4.75 | -0.78 | 0.215 |
| 65.00 | -30.21 | -18.64 | 0.00 | -1,218.65 | 0.00 | 1,218.65 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 5.60 | -0.84 | 0.209 |
| 70.00 | -28.41 | -18.21 | 0.00 | -1,125.43 | 0.00 | 1,125.43 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 6.51 | -0.91 | 0.204 |
| 75.00 | -26.67 | -17.77 | 0.00 | -1,034.39 | 0.00 | 1,034.39 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 7.50 | -0.98 | 0.199 |
| 80.00 | -24.96 | -17.34 | 0.00 | -945.53 | 0.00 | 945.53 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 8.57 | -1.05 | 0.194 |
| 85.00 | -23.31 | -16.91 | 0.00 | -858.85 | 0.00 | 858.85 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 9.70 | -1.11 | 0.188 |
| 90.00 | -21.71 | -16.52 | 0.00 | -774.31 | 0.00 | 774.31 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 10.90 | -1.18 | 0.181 |
| 94.09 | -20.43 | -16.29 | 0.00 | -706.75 | 0.00 | 706.75 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 11.94 | -1.24 | 0.175 |
| 95.00 | -19.96 | -16.05 | 0.00 | -691.94 | 0.00 | 691.94 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 12.18 | -1.25 | 0.174 |
| 99.92 | -17.49 | -15.80 | 0.00 | -612.89 | 0.00 | 612.89 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 13.50 | -1.32 | 0.215 |
| 100.00 | -17.46 | -15.61 | 0.00 | -611.69 | 0.00 | 611.69 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 13.52 | -1.32 | 0.215 |
| 105.00 | -16.29 | -15.20 | 0.00 | -533.66 | 0.00 | 533.66 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 14.95 | -1.40 | 0.200 |
| 110.00 | -15.16 | -14.80 | 0.00 | -457.68 | 0.00 | 457.68 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 16.45 | -1.48 | 0.183 |
| 115.00 | -14.06 | -14.40 | 0.00 | -383.69 | 0.00 | 383.69 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 18.04 | -1.55 | 0.166 |
| 120.00 | -13.00 | -14.02 | 0.00 | -311.68 | 0.00 | 311.68 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 19.70 | -1.62 | 0.146 |
| 125.00 | -11.97 | -13.64 | 0.00 | -241.60 | 0.00 | 241.60 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 21.44 | -1.68 | 0.124 |
| 130.00 | -10.99 | -13.27 | 0.00 | -173.42 | 0.00 | 173.42 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 23.23 | -1.74 | 0.098 |
| 135.00 | -7.02 | -8.78 | 0.00 | -107.09 | 0.00 | 107.09 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 25.07 | -1.78 | 0.066 |
| 136.87 | -6.72 | -8.61 | 0.00 | -90.69 | 0.00 | 90.69 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 25.77 | -1.79 | 0.058 |
| 140.00 | -5.90 | -8.44 | 0.00 | -63.73 | 0.00 | 63.73 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 26.95 | -1.81 | 0.044 |
| 141.22 | -5.59 | -8.26 | 0.00 | -53.43 | 0.00 | 53.43 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 27.41 | -1.81 | 0.057 |
| 145.00 | -5.17 | -8.10 | 0.00 | -22.20 | 0.00 | 22.20 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 28.85 | -1.82 | 0.027 |
| 146.00 | -4.15 | -3.34 | 0.00 | -14.11 | 0.00 | 14.11 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 29.23 | -1.83 | 0.018 |
| 148.00 | -2.16 | -2.27 | 0.00 | -7.42 | 0.00 | 7.42 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 30.00 | -1.83 | 0.010 |
| 150.00 | -0.09 | -0.03 | 0.00 | -0.03 | 0.00 | 0.03 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 30.76 | -1.83 | 0.000 |
| 151.00 | 0.00 | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 31.15 | -1.83 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | o 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | ---: | ---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | 3/22/2021 7:18:49 PM |
| Customer: AT\&T MOBILITY |  |  |

## Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (lb) | Dead Load (lb) | Wind FX <br> (lb) | ```Torsion MY (lb-ft)``` | $\begin{aligned} & \text { Moment } \\ & \text { MZ } \\ & (\mathrm{lb}-\mathrm{ft}) \end{aligned}$ | Dead <br> Load <br> (Ib) | Wind FX <br> (lb) | Dead Load (lb) | Wind FX <br> (lb) | Dead <br> Load <br> (lb) | $\begin{gathered} \hline \text { Torsion } \\ \text { MY } \\ \text { (lb-ft) } \end{gathered}$ | Moment MZ <br> (lb) |
| 0.00 |  | 239.7 | 0.0 |  |  |  |  | 0.0 | 0.0 | 239.7 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 474.3 | 1,622.7 |  |  |  |  | 0.0 | 144.8 | 474.3 | 1,767.4 | 0.0 | 0.0 |
| 10.00 |  | 464.1 | 1,587.7 |  |  |  |  | 0.0 | 144.8 | 464.1 | 1,732.4 | 0.0 | 0.0 |
| 15.00 |  | 453.8 | 1,552.6 |  |  |  |  | 0.0 | 144.8 | 453.8 | 1,697.4 | 0.0 | 0.0 |
| 20.00 |  | 443.5 | 1,517.6 |  |  |  |  | 0.0 | 144.8 | 443.5 | 1,662.4 | 0.0 | 0.0 |
| 25.00 |  | 433.3 | 1,482.6 |  |  |  |  | 0.0 | 144.8 | 433.3 | 1,627.4 | 0.0 | 0.0 |
| 30.00 |  | 428.0 | 1,447.6 |  |  |  |  | 0.0 | 144.8 | 428.0 | 1,592.4 | 0.0 | 0.0 |
| 35.00 |  | 431.3 | 1,412.6 |  |  |  |  | 0.0 | 144.8 | 431.3 | 1,557.3 | 0.0 | 0.0 |
| 40.00 |  | 437.0 | 1,377.6 |  |  |  |  | 0.0 | 144.8 | 437.0 | 1,522.3 | 0.0 | 0.0 |
| 45.00 |  | 275.9 | 1,342.6 |  |  |  |  | 0.0 | 144.8 | 275.9 | 1,487.3 | 0.0 | 0.0 |
| 46.28 | Bot - Section 2 | 223.9 | 337.1 |  |  |  |  | 0.0 | 36.9 | 223.9 | 374.0 | 0.0 | 0.0 |
| 50.00 |  | 335.8 | 1,959.0 |  |  |  |  | 0.0 | 107.8 | 335.8 | 2,066.9 | 0.0 | 0.0 |
| 53.73 | Top - Section 1 | 225.4 | 1,924.2 |  |  |  |  | 0.0 | 108.0 | 225.4 | 2,032.3 | 0.0 | 0.0 |
| 55.00 |  | 282.3 | 325.6 |  |  |  |  | 0.0 | 36.7 | 282.3 | 362.4 | 0.0 | 0.0 |
| 60.00 |  | 449.4 | 1,261.8 |  |  |  |  | 0.0 | 144.8 | 449.4 | 1,406.6 | 0.0 | 0.0 |
| 65.00 |  | 447.0 | 1,226.8 |  |  |  |  | 0.0 | 144.8 | 447.0 | 1,371.6 | 0.0 | 0.0 |
| 70.00 |  | 443.5 | 1,191.8 |  |  |  |  | 0.0 | 144.8 | 443.5 | 1,336.5 | 0.0 | 0.0 |
| 75.00 |  | 439.0 | 1,156.8 |  |  |  |  | 0.0 | 144.8 | 439.0 | 1,301.5 | 0.0 | 0.0 |
| 80.00 |  | 433.6 | 1,121.7 |  |  |  |  | 0.0 | 144.8 | 433.6 | 1,266.5 | 0.0 | 0.0 |
| 85.00 |  | 427.3 | 1,086.7 |  |  |  |  | 0.0 | 144.8 | 427.3 | 1,231.5 | 0.0 | 0.0 |
| 90.00 |  | 382.7 | 1,051.7 |  |  |  |  | 0.0 | 144.8 | 382.7 | 1,196.5 | 0.0 | 0.0 |
| 94.09 | Bot - Section 3 | 209.0 | 834.4 |  |  |  |  | 0.0 | 118.4 | 209.0 | 952.9 | 0.0 | 0.0 |
| 95.00 |  | 243.1 | 321.9 |  |  |  |  | 0.0 | 26.3 | 243.1 | 348.2 | 0.0 | 0.0 |
| 99.92 | Top - Section 2 | 208.0 | 1,708.1 |  |  |  |  | 0.0 | 142.6 | 208.0 | 1,850.6 | 0.0 | 0.0 |
| 100.00 |  | 206.8 | 11.2 |  |  |  |  | 0.0 | 2.2 | 206.8 | 13.4 | 0.0 | 0.0 |
| 105.00 |  | 402.8 | 725.9 |  |  |  |  | 0.0 | 144.8 | 402.8 | 870.7 | 0.0 | 0.0 |
| 110.00 |  | 393.3 | 699.7 |  |  |  |  | 0.0 | 144.8 | 393.3 | 844.4 | 0.0 | 0.0 |
| 115.00 |  | 383.2 | 673.4 |  |  |  |  | 0.0 | 144.8 | 383.2 | 818.2 | 0.0 | 0.0 |
| 120.00 |  | 372.6 | 647.2 |  |  |  |  | 0.0 | 144.8 | 372.6 | 791.9 | 0.0 | 0.0 |
| 125.00 |  | 361.6 | 620.9 |  |  |  |  | 0.0 | 144.8 | 361.6 | 765.7 | 0.0 | 0.0 |
| 130.00 |  | 350.0 | 594.6 |  |  |  |  | 0.0 | 144.8 | 350.0 | 739.4 | 0.0 | 0.0 |
| 135.00 | Appurtenance(s) | 234.7 | 568.4 | 4,130.7 | 0.0 | 0.0 | 2,358.1 | 0.0 | 144.8 | 4,365.5 | 3,071.2 | 0.0 | 0.0 |
| 136.87 | Bot - Section 4 | 167.7 | 205.5 |  |  |  |  | 0.0 | 28.4 | 167.7 | 233.9 | 0.0 | 0.0 |
| 140.00 |  | 145.2 | 565.8 |  |  |  |  | 0.0 | 47.7 | 145.2 | 613.5 | 0.0 | 0.0 |
| 141.22 | Top - Section 3 | 162.4 | 215.8 |  |  |  |  | 0.0 | 18.6 | 162.4 | 234.4 | 0.0 | 0.0 |
| 145.00 |  | 153.9 | 264.1 |  |  |  |  | 0.0 | 57.5 | 153.9 | 321.6 | 0.0 | 0.0 |
| 146.00 | Appurtenance(s) | 94.3 | 68.2 | 4,624.4 | 40.0 | 0.0 | 795.6 | 0.0 | 15.2 | 4,718.8 | 879.0 | 0.0 | 0.0 |
| 148.00 | Appurtenance(s) | 124.2 | 134.3 | 888.0 | 0.0 | 0.0 | 1,350.0 | 0.0 | 26.6 | 1,012.2 | 1,510.9 | 0.0 | 0.0 |
| 150.00 | Appurtenance(s) | 92.0 | 131.5 | 2,075.6 | 0.0 | 2,848.3 | 1,454.4 | 0.0 | 26.6 | 2,167.6 | 1,612.5 | 0.0 | 0.0 |
| 151.00 |  | 30.4 | 64.7 |  |  |  |  | 0.0 | 0.0 | 30.4 | 64.7 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 24,225.0 | 45,129.6 | 0.00 | 0.00 |

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| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :---: | :---: | :---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | 3/22/2021 7:18:52 PM |
| Customer: AT\&T MOBILITY |  |  |
| Load Case: $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 93 mph with No Ice (Reduced DL) | 20 Iterations |
| Gust Response Factor :1.10 |  | Wind Importance Factor : 1.00 |
| Dead Load Factor : 0.90 <br> Wind Load Factor : 1.60 |  |  |

Calculated Forces

| Seg <br> Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \text { FY (-) } \\ \text { (kips) } \end{gathered}$ | Vu <br> FX (-) (kips) | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $M u$ $M X$ (ft-kips) | Resultant Moment (ft-kips) | $\begin{aligned} & \text { phi } \\ & \text { Pn } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ |  | phi Mn (ft-kips) | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -45.12 | -24.01 | 0.00 | -2,608.42 | 0.00 | 2,608.42 | 7,216.29 | 3,608.15 | 20,023.1 | 0,026.4 | 0.00 | 0.00 | 0.266 |
| 5.00 | -43.33 | -23.58 | 0.00 | -2,488.38 | 0.00 | 2,488.38 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.03 | -0.06 | 0.263 |
| 10.00 | -41.57 | -23.16 | 0.00 | -2,370.49 | 0.00 | 2,370.49 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.13 | -0.12 | 0.260 |
| 15.00 | -39.85 | -22.74 | 0.00 | -2,254.72 | 0.00 | 2,254.72 | 6,915.90 | 3,457.95 | 17,951.6 | 8,989.14 | 0.28 | -0.18 | 0.257 |
| 20.00 | -38.16 | -22.33 | 0.00 | -2,141.02 | 0.00 | 2,141.02 | 6,810.85 | 3,405.43 | 17,272.5 | 8,649.09 | 0.50 | -0.24 | 0.253 |
| 25.00 | -36.51 | -21.93 | 0.00 | -2,029.36 | 0.00 | 2,029.36 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.79 | -0.30 | 0.250 |
| 30.00 | -34.90 | -21.53 | 0.00 | -1,919.71 | 0.00 | 1,919.71 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 1.14 | -0.37 | 0.246 |
| 35.00 | -33.32 | -21.13 | 0.00 | -1,812.05 | 0.00 | 1,812.05 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 1.57 | -0.43 | 0.242 |
| 40.00 | -31.78 | -20.72 | 0.00 | -1,706.41 | 0.00 | 1,706.41 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 2.05 | -0.50 | 0.238 |
| 45.00 | -30.28 | -20.45 | 0.00 | -1,602.83 | 0.00 | 1,602.83 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 2.61 | -0.57 | 0.234 |
| 46.28 | -29.90 | -20.24 | 0.00 | -1,576.73 | 0.00 | 1,576.73 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 2.77 | -0.58 | 0.233 |
| 50.00 | -27.81 | -19.91 | 0.00 | -1,501.36 | 0.00 | 1,501.36 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 3.24 | -0.63 | 0.229 |
| 53.73 | -25.77 | -19.67 | 0.00 | -1,427.08 | 0.00 | 1,427.08 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 3.76 | -0.69 | 0.218 |
| 55.00 | -25.40 | -19.41 | 0.00 | -1,402.13 | 0.00 | 1,402.13 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 3.95 | -0.70 | 0.217 |
| 60.00 | -23.98 | -18.97 | 0.00 | -1,305.10 | 0.00 | 1,305.10 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 4.72 | -0.77 | 0.212 |
| 65.00 | -22.59 | -18.53 | 0.00 | -1,210.28 | 0.00 | 1,210.28 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 5.56 | -0.84 | 0.207 |
| 70.00 | -21.24 | -18.09 | 0.00 | -1,117.65 | 0.00 | 1,117.65 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 6.48 | -0.90 | 0.202 |
| 75.00 | -19.92 | -17.65 | 0.00 | -1,027.22 | 0.00 | 1,027.22 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 7.46 | -0.97 | 0.197 |
| 80.00 | -18.65 | -17.22 | 0.00 | -938.97 | 0.00 | 938.97 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 8.51 | -1.04 | 0.192 |
| 85.00 | -17.40 | -16.79 | 0.00 | -852.89 | 0.00 | 852.89 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 9.64 | -1.11 | 0.186 |
| 90.00 | -16.20 | -16.40 | 0.00 | -768.96 | 0.00 | 768.96 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 10.83 | -1.17 | 0.179 |
| 94.09 | -15.24 | -16.18 | 0.00 | -701.88 | 0.00 | 701.88 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 11.87 | -1.23 | 0.173 |
| 95.00 | -14.88 | -15.94 | 0.00 | -687.17 | 0.00 | 687.17 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 12.10 | -1.24 | 0.171 |
| 99.92 | -13.03 | -15.70 | 0.00 | -608.70 | 0.00 | 608.70 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 13.42 | -1.31 | 0.213 |
| 100.00 | -13.01 | -15.50 | 0.00 | -607.51 | 0.00 | 607.51 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 13.44 | -1.31 | 0.212 |
| 105.00 | -12.13 | -15.09 | 0.00 | -530.02 | 0.00 | 530.02 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 14.85 | -1.39 | 0.198 |
| 110.00 | -11.27 | -14.69 | 0.00 | -454.56 | 0.00 | 454.56 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 16.35 | -1.47 | 0.181 |
| 115.00 | -10.45 | -14.30 | 0.00 | -381.10 | 0.00 | 381.10 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 17.93 | -1.54 | 0.163 |
| 120.00 | -9.65 | -13.92 | 0.00 | -309.60 | 0.00 | 309.60 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 19.58 | -1.61 | 0.144 |
| 125.00 | -8.88 | -13.54 | 0.00 | -240.02 | 0.00 | 240.02 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 21.30 | -1.67 | 0.122 |
| 130.00 | -8.14 | -13.18 | 0.00 | -172.30 | 0.00 | 172.30 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 23.08 | -1.72 | 0.096 |
| 135.00 | -5.20 | -8.72 | 0.00 | -106.41 | 0.00 | 106.41 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 24.91 | -1.76 | 0.065 |
| 136.87 | -4.97 | -8.55 | 0.00 | -90.13 | 0.00 | 90.13 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 25.60 | -1.78 | 0.057 |
| 140.00 | -4.36 | -8.39 | 0.00 | -63.34 | 0.00 | 63.34 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 26.78 | -1.79 | 0.043 |
| 141.22 | -4.13 | -8.22 | 0.00 | -53.11 | 0.00 | 53.11 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 27.24 | -1.80 | 0.056 |
| 145.00 | -3.81 | -8.05 | 0.00 | -22.05 | 0.00 | 22.05 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 28.67 | -1.81 | 0.026 |
| 146.00 | -3.08 | -3.31 | 0.00 | -14.00 | 0.00 | 14.00 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 29.05 | -1.81 | 0.017 |
| 148.00 | -1.61 | -2.25 | 0.00 | -7.38 | 0.00 | 7.38 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 29.81 | -1.82 | 0.009 |
| 150.00 | -0.06 | -0.03 | 0.00 | -0.03 | 0.00 | 0.03 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 30.57 | -1.82 | 0.000 |
| 151.00 | 0.00 | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 30.95 | -1.82 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | O 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :---: | ---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | 3/22/2021 7:18:52 PM |
| Customer: AT\&T MOBILITY |  |  |

## Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (lb) | Dead Load (lb) | Wind FX <br> (lb) | ```Torsion MY (lb-ft)``` | Moment MZ (lb-ft) | Dead Load <br> (lb) | Wind FX <br> (Ib) | Dead Load (lb) | Wind FX <br> (lb) | Dead <br> Load <br> (lb) | $\begin{gathered} \hline \text { Torsion } \\ \text { MY } \\ \text { (lb-ft) } \end{gathered}$ | Moment <br> MZ <br> (lb) |
| 0.00 |  | 83.6 | 0.0 |  |  |  |  | 0.0 | 0.0 | 83.6 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 165.9 | 2,822.8 |  |  |  |  | 0.0 | 193.0 | 165.9 | 3,015.8 | 0.0 | 0.0 |
| 10.00 |  | 163.1 | 2,839.0 |  |  |  |  | 0.0 | 193.0 | 163.1 | 3,032.0 | 0.0 | 0.0 |
| 15.00 |  | 160.0 | 2,814.7 |  |  |  |  | 0.0 | 193.0 | 160.0 | 3,007.8 | 0.0 | 0.0 |
| 20.00 |  | 156.8 | 2,777.3 |  |  |  |  | 0.0 | 193.0 | 156.8 | 2,970.3 | 0.0 | 0.0 |
| 25.00 |  | 153.6 | 2,733.0 |  |  |  |  | 0.0 | 193.0 | 153.6 | 2,926.0 | 0.0 | 0.0 |
| 30.00 |  | 152.1 | 2,684.4 |  |  |  |  | 0.0 | 193.0 | 152.1 | 2,877.4 | 0.0 | 0.0 |
| 35.00 |  | 153.7 | 2,632.8 |  |  |  |  | 0.0 | 193.0 | 153.7 | 2,825.8 | 0.0 | 0.0 |
| 40.00 |  | 156.1 | 2,578.9 |  |  |  |  | 0.0 | 193.0 | 156.1 | 2,772.0 | 0.0 | 0.0 |
| 45.00 |  | 98.7 | 2,523.4 |  |  |  |  | 0.0 | 193.0 | 98.7 | 2,716.4 | 0.0 | 0.0 |
| 46.28 | Bot - Section 2 | 80.2 | 636.8 |  |  |  |  | 0.0 | 49.3 | 80.2 | 686.0 | 0.0 | 0.0 |
| 50.00 |  | 120.4 | 3,161.0 |  |  |  |  | 0.0 | 143.8 | 120.4 | 3,304.8 | 0.0 | 0.0 |
| 53.73 | Top - Section 1 | 80.9 | 3,109.5 |  |  |  |  | 0.0 | 144.1 | 80.9 | 3,253.6 | 0.0 | 0.0 |
| 55.00 |  | 101.6 | 618.7 |  |  |  |  | 0.0 | 49.0 | 101.6 | 667.7 | 0.0 | 0.0 |
| 60.00 |  | 162.0 | 2,395.0 |  |  |  |  | 0.0 | 193.0 | 162.0 | 2,588.1 | 0.0 | 0.0 |
| 65.00 |  | 161.6 | 2,335.3 |  |  |  |  | 0.0 | 193.0 | 161.6 | 2,528.3 | 0.0 | 0.0 |
| 70.00 |  | 160.8 | 2,274.8 |  |  |  |  | 0.0 | 193.0 | 160.8 | 2,467.9 | 0.0 | 0.0 |
| 75.00 |  | 159.6 | 2,213.7 |  |  |  |  | 0.0 | 193.0 | 159.6 | 2,406.8 | 0.0 | 0.0 |
| 80.00 |  | 158.2 | 2,152.1 |  |  |  |  | 0.0 | 193.0 | 158.2 | 2,345.1 | 0.0 | 0.0 |
| 85.00 |  | 156.4 | 2,089.9 |  |  |  |  | 0.0 | 193.0 | 156.4 | 2,282.9 | 0.0 | 0.0 |
| 90.00 |  | 140.5 | 2,027.2 |  |  |  |  | 0.0 | 193.0 | 140.5 | 2,220.3 | 0.0 | 0.0 |
| 94.09 | Bot - Section 3 | 76.9 | 1,613.2 |  |  |  |  | 0.0 | 157.9 | 76.9 | 1,771.2 | 0.0 | 0.0 |
| 95.00 |  | 89.6 | 541.9 |  |  |  |  | 0.0 | 35.1 | 89.6 | 577.0 | 0.0 | 0.0 |
| 99.92 | Top - Section 2 | 76.7 | 2,870.9 |  |  |  |  | 0.0 | 190.1 | 76.7 | 3,061.0 | 0.0 | 0.0 |
| 100.00 |  | 76.5 | 24.1 |  |  |  |  | 0.0 | 2.9 | 76.5 | 27.0 | 0.0 | 0.0 |
| 105.00 |  | 149.4 | 1,553.2 |  |  |  |  | 0.0 | 193.0 | 149.4 | 1,746.2 | 0.0 | 0.0 |
| 110.00 |  | 146.5 | 1,500.8 |  |  |  |  | 0.0 | 193.0 | 146.5 | 1,693.8 | 0.0 | 0.0 |
| 115.00 |  | 143.4 | 1,448.1 |  |  |  |  | 0.0 | 193.0 | 143.4 | 1,641.1 | 0.0 | 0.0 |
| 120.00 |  | 140.1 | 1,395.1 |  |  |  |  | 0.0 | 193.0 | 140.1 | 1,588.1 | 0.0 | 0.0 |
| 125.00 |  | 136.7 | 1,341.9 |  |  |  |  | 0.0 | 193.0 | 136.7 | 1,534.9 | 0.0 | 0.0 |
| 130.00 |  | 133.1 | 1,288.4 |  |  |  |  | 0.0 | 193.0 | 133.1 | 1,481.4 | 0.0 | 0.0 |
| 135.00 | Appurtenance(s) | 89.6 | 1,234.6 | 1,163.4 | 0.0 | 0.0 | 7,974.9 | 0.0 | 193.0 | 1,253.0 | 9,402.6 | 0.0 | 0.0 |
| 136.87 | Bot - Section 4 | 64.3 | 449.5 |  |  |  |  | 0.0 | 37.9 | 64.3 | 487.4 | 0.0 | 0.0 |
| 140.00 |  | 55.7 | 1,046.1 |  |  |  |  | 0.0 | 63.6 | 55.7 | 1,109.7 | 0.0 | 0.0 |
| 141.22 | Top - Section 3 | 62.6 | 400.4 |  |  |  |  | 0.0 | 24.8 | 62.6 | 425.1 | 0.0 | 0.0 |
| 145.00 |  | 59.4 | 689.3 |  |  |  |  | 0.0 | 76.7 | 59.4 | 766.0 | 0.0 | 0.0 |
| 146.00 | Appurtenance(s) | 36.6 | 179.5 | 1,151.8 | 0.0 | 0.0 | 6,204.2 | 0.0 | 20.3 | 1,188.4 | 6,404.0 | 0.0 | 0.0 |
| 148.00 | Appurtenance(s) | 48.3 | 353.0 | 349.7 | 0.0 | 0.0 | 2,570.9 | 0.0 | 35.4 | 398.0 | 2,959.3 | 0.0 | 0.0 |
| 150.00 | Appurtenance(s) | 35.8 | 346.2 | 649.5 | 0.0 | 844.6 | 4,354.2 | 0.0 | 35.4 | 685.3 | 4,735.8 | 0.0 | 0.0 |
| 151.00 |  | 11.9 | 170.9 |  |  |  |  | 0.0 | 0.0 | 11.9 | 170.9 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 7,873.37 | 92,477.1 | 0.00 | 0.00 |

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Site Number: 411186 Code: ANSI/TIA-222-G © 2007-2021 by ATC IP LLC. All rights reserved.

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:54 PM
Customer: AT\&T MOBILITY

| Load Case: 1.2D + 1.0Di + 1.0Wi | 50 mph with 1.00 in Radial Ice | 19 Iterations |
| :---: | :---: | :---: |
| Gust Response Factor :1.10 | Ice Dead Load Factor :1.00 | Wind Importance Factor :1.00 |
| Dead Load Factor :1.20 |  | Ice Importance Factor :1.00 |
| Wind Load Factor :1.00 |  |  |

Calculated Forces

| Seg Elev | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \end{gathered}$ | $\begin{aligned} & \mathrm{Vu} \\ & \mathrm{FX}(-) \end{aligned}$ | Tu <br> MY | Mu <br> MZ | Mu <br> MX | Resultant Moment | $\begin{aligned} & \text { phi } \\ & \text { Pn } \end{aligned}$ | phi | $\begin{aligned} & \text { phi } \\ & \text { Tr } \end{aligned}$ | $\begin{aligned} & \text { phi } \\ & \text { Mn } \end{aligned}$ | Total |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (ft) | (kips) | (kips) | (ft-kips) | (ft-kips) | (ft-kips) | (ft-kips) | (kips) | (kips) | (ft-kips) | (ft-kips) | (in) | (deg) | Ratio |
| 0.00 | -92.48 | -7.80 | 0.00 | -836.42 | 0.00 | 836.42 | 7,216.29 | 3,608.15 | 20,023.1 | 10,026.4 | 0.00 | 0.00 | 0.096 |
| 5.00 | -89.46 | -7.67 | 0.00 | -797.40 | 0.00 | 797.40 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.01 | -0.02 | 0.095 |
| 10.00 | -86.42 | -7.53 | 0.00 | -759.06 | 0.00 | 759.06 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.04 | -0.04 | 0.094 |
| 15.00 | -83.41 | -7.40 | 0.00 | -721.40 | 0.00 | 721.40 | 6,915.90 | 3,457.95 | 17,951.6 | 8,989.14 | 0.09 | -0.06 | 0.092 |
| 20.00 | -80.44 | -7.27 | 0.00 | -684.41 | 0.00 | 684.41 | 6,810.85 | 3,405.43 | 17,272.5 | 8,649.09 | 0.16 | -0.08 | 0.091 |
| 25.00 | -77.51 | -7.14 | 0.00 | -648.08 | 0.00 | 648.08 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.25 | -0.10 | 0.090 |
| 30.00 | -74.63 | -7.00 | 0.00 | -612.41 | 0.00 | 612.41 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 0.37 | -0.12 | 0.088 |
| 35.00 | -71.80 | -6.87 | 0.00 | -577.39 | 0.00 | 577.39 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 0.50 | -0.14 | 0.087 |
| 40.00 | -69.03 | -6.73 | 0.00 | -543.03 | 0.00 | 543.03 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 0.66 | -0.16 | 0.085 |
| 45.00 | -66.31 | -6.64 | 0.00 | -509.37 | 0.00 | 509.37 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 0.84 | -0.18 | 0.083 |
| 46.28 | -65.63 | -6.57 | 0.00 | -500.89 | 0.00 | 500.89 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 0.89 | -0.19 | 0.083 |
| 50.00 | -62.32 | -6.46 | 0.00 | -476.42 | 0.00 | 476.42 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 1.04 | -0.20 | 0.081 |
| 53.73 | -59.07 | -6.38 | 0.00 | -452.32 | 0.00 | 452.32 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 1.20 | -0.22 | 0.077 |
| 55.00 | -58.40 | -6.29 | 0.00 | -444.24 | 0.00 | 444.24 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 1.26 | -0.22 | 0.077 |
| 60.00 | -55.81 | -6.13 | 0.00 | -412.81 | 0.00 | 412.81 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 1.51 | -0.25 | 0.075 |
| 65.00 | -53.28 | -5.98 | 0.00 | -382.14 | 0.00 | 382.14 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 1.78 | -0.27 | 0.073 |
| 70.00 | -50.81 | -5.83 | 0.00 | -352.24 | 0.00 | 352.24 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 2.07 | -0.29 | 0.071 |
| 75.00 | -48.40 | -5.67 | 0.00 | -323.11 | 0.00 | 323.11 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 2.38 | -0.31 | 0.070 |
| 80.00 | -46.05 | -5.52 | 0.00 | -294.75 | 0.00 | 294.75 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 2.72 | -0.33 | 0.068 |
| 85.00 | -43.77 | -5.36 | 0.00 | -267.16 | 0.00 | 267.16 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 3.07 | -0.35 | 0.066 |
| 90.00 | -41.55 | -5.22 | 0.00 | -240.34 | 0.00 | 240.34 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 3.45 | -0.37 | 0.063 |
| 94.09 | -39.78 | -5.14 | 0.00 | -218.98 | 0.00 | 218.98 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 3.78 | -0.39 | 0.061 |
| 95.00 | -39.20 | -5.06 | 0.00 | -214.30 | 0.00 | 214.30 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 3.85 | -0.39 | 0.061 |
| 99.92 | -36.14 | -4.97 | 0.00 | -189.40 | 0.00 | 189.40 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 4.27 | -0.41 | 0.075 |
| 100.00 | -36.11 | -4.90 | 0.00 | -189.02 | 0.00 | 189.02 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 4.28 | -0.41 | 0.075 |
| 105.00 | -34.36 | -4.75 | 0.00 | -164.54 | 0.00 | 164.54 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 4.73 | -0.44 | 0.070 |
| 110.00 | -32.67 | -4.60 | 0.00 | -140.79 | 0.00 | 140.79 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 5.20 | -0.46 | 0.065 |
| 115.00 | -31.03 | -4.46 | 0.00 | -117.78 | 0.00 | 117.78 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 5.70 | -0.49 | 0.059 |
| 120.00 | -29.44 | -4.31 | 0.00 | -95.49 | 0.00 | 95.49 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 6.22 | -0.51 | 0.053 |
| 125.00 | -27.90 | -4.17 | 0.00 | -73.92 | 0.00 | 73.92 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 6.76 | -0.53 | 0.046 |
| 130.00 | -26.42 | -4.03 | 0.00 | -53.06 | 0.00 | 53.06 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 7.32 | -0.54 | 0.038 |
| 135.00 | -17.03 | -2.69 | 0.00 | -32.90 | 0.00 | 32.90 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 7.90 | -0.56 | 0.026 |
| 136.87 | -16.55 | -2.62 | 0.00 | -27.88 | 0.00 | 27.88 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 8.12 | -0.56 | 0.023 |
| 140.00 | -15.44 | -2.56 | 0.00 | -19.66 | 0.00 | 19.66 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 8.49 | -0.56 | 0.019 |
| 141.22 | -15.01 | -2.49 | 0.00 | -16.54 | 0.00 | 16.54 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 8.63 | -0.57 | 0.026 |
| 145.00 | -14.25 | -2.43 | 0.00 | -7.12 | 0.00 | 7.12 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 9.08 | -0.57 | 0.017 |
| 146.00 | -7.85 | -1.17 | 0.00 | -4.70 | 0.00 | 4.70 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 9.20 | -0.57 | 0.010 |
| 148.00 | -4.90 | -0.75 | 0.00 | -2.35 | 0.00 | 2.35 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 9.44 | -0.57 | 0.006 |
| 150.00 | -0.17 | -0.01 | 0.00 | -0.01 | 0.00 | 0.01 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 9.68 | -0.57 | 0.000 |
| 151.00 | 0.00 | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 9.80 | -0.57 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :---: | ---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | 3/22/2021 7:18:54 PM |
| Customer: AT\&T MOBILITY |  |  |

## Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (lb) | Dead Load <br> (Ib) | Wind FX <br> (Ib) | Torsion MY <br> (lb-ft) | $\begin{aligned} & \hline \text { Moment } \\ & \text { MZ } \\ & \text { (lb-ft) } \end{aligned}$ | Dead Load (lb) | Wind FX <br> (lb) | Dead Load <br> (lb) | Wind FX <br> (Ib) | Dead Load <br> (lb) | Torsion MY <br> (lb-ft) | Moment MZ <br> (Ib) |
| 0.00 |  | 55.8 | 0.0 |  |  |  |  | 0.0 | 0.0 | 55.8 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 110.4 | 1,803.0 |  |  |  |  | 0.0 | 160.9 | 110.4 | 1,963.8 | 0.0 | 0.0 |
| 10.00 |  | 108.0 | 1,764.1 |  |  |  |  | 0.0 | 160.9 | 108.0 | 1,924.9 | 0.0 | 0.0 |
| 15.00 |  | 105.6 | 1,725.2 |  |  |  |  | 0.0 | 160.9 | 105.6 | 1,886.0 | 0.0 | 0.0 |
| 20.00 |  | 103.2 | 1,686.3 |  |  |  |  | 0.0 | 160.9 | 103.2 | 1,847.1 | 0.0 | 0.0 |
| 25.00 |  | 100.8 | 1,647.3 |  |  |  |  | 0.0 | 160.9 | 100.8 | 1,808.2 | 0.0 | 0.0 |
| 30.00 |  | 99.6 | 1,608.4 |  |  |  |  | 0.0 | 160.9 | 99.6 | 1,769.3 | 0.0 | 0.0 |
| 35.00 |  | 100.4 | 1,569.5 |  |  |  |  | 0.0 | 160.9 | 100.4 | 1,730.4 | 0.0 | 0.0 |
| 40.00 |  | 101.7 | 1,530.6 |  |  |  |  | 0.0 | 160.9 | 101.7 | 1,691.5 | 0.0 | 0.0 |
| 45.00 |  | 64.2 | 1,491.7 |  |  |  |  | 0.0 | 160.9 | 64.2 | 1,652.6 | 0.0 | 0.0 |
| 46.28 | Bot - Section 2 | 52.1 | 374.5 |  |  |  |  | 0.0 | 41.1 | 52.1 | 415.6 | 0.0 | 0.0 |
| 50.00 |  | 78.2 | 2,176.7 |  |  |  |  | 0.0 | 119.8 | 78.2 | 2,296.5 | 0.0 | 0.0 |
| 53.73 | Top - Section 1 | 52.5 | 2,138.0 |  |  |  |  | 0.0 | 120.0 | 52.5 | 2,258.1 | 0.0 | 0.0 |
| 55.00 |  | 65.7 | 361.8 |  |  |  |  | 0.0 | 40.8 | 65.7 | 402.6 | 0.0 | 0.0 |
| 60.00 |  | 104.6 | 1,402.0 |  |  |  |  | 0.0 | 160.9 | 104.6 | 1,562.9 | 0.0 | 0.0 |
| 65.00 |  | 104.0 | 1,363.1 |  |  |  |  | 0.0 | 160.9 | 104.0 | 1,524.0 | 0.0 | 0.0 |
| 70.00 |  | 103.2 | 1,324.2 |  |  |  |  | 0.0 | 160.9 | 103.2 | 1,485.0 | 0.0 | 0.0 |
| 75.00 |  | 102.2 | 1,285.3 |  |  |  |  | 0.0 | 160.9 | 102.2 | 1,446.1 | 0.0 | 0.0 |
| 80.00 |  | 100.9 | 1,246.4 |  |  |  |  | 0.0 | 160.9 | 100.9 | 1,407.2 | 0.0 | 0.0 |
| 85.00 |  | 99.5 | 1,207.5 |  |  |  |  | 0.0 | 160.9 | 99.5 | 1,368.3 | 0.0 | 0.0 |
| 90.00 |  | 89.1 | 1,168.6 |  |  |  |  | 0.0 | 160.9 | 89.1 | 1,329.4 | 0.0 | 0.0 |
| 94.09 | Bot - Section 3 | 48.6 | 927.2 |  |  |  |  | 0.0 | 131.6 | 48.6 | 1,058.8 | 0.0 | 0.0 |
| 95.00 |  | 56.6 | 357.6 |  |  |  |  | 0.0 | 29.2 | 56.6 | 386.9 | 0.0 | 0.0 |
| 99.92 | Top - Section 2 | 48.4 | 1,897.8 |  |  |  |  | 0.0 | 158.4 | 48.4 | 2,056.3 | 0.0 | 0.0 |
| 100.00 |  | 48.1 | 12.5 |  |  |  |  | 0.0 | 2.4 | 48.1 | 14.9 | 0.0 | 0.0 |
| 105.00 |  | 93.8 | 806.6 |  |  |  |  | 0.0 | 160.9 | 93.8 | 967.5 | 0.0 | 0.0 |
| 110.00 |  | 91.5 | 777.4 |  |  |  |  | 0.0 | 160.9 | 91.5 | 938.3 | 0.0 | 0.0 |
| 115.00 |  | 89.2 | 748.2 |  |  |  |  | 0.0 | 160.9 | 89.2 | 909.1 | 0.0 | 0.0 |
| 120.00 |  | 86.7 | 719.1 |  |  |  |  | 0.0 | 160.9 | 86.7 | 879.9 | 0.0 | 0.0 |
| 125.00 |  | 84.2 | 689.9 |  |  |  |  | 0.0 | 160.9 | 84.2 | 850.7 | 0.0 | 0.0 |
| 130.00 |  | 81.5 | 660.7 |  |  |  |  | 0.0 | 160.9 | 81.5 | 821.6 | 0.0 | 0.0 |
| 135.00 | Appurtenance(s) | 54.6 | 631.5 | 961.5 | 0.0 | 0.0 | 2,620.1 | 0.0 | 160.9 | 1,016.1 | 3,412.5 | 0.0 | 0.0 |
| 136.87 | Bot - Section 4 | 39.0 | 228.3 |  |  |  |  | 0.0 | 31.6 | 39.0 | 259.9 | 0.0 | 0.0 |
| 140.00 |  | 33.8 | 628.7 |  |  |  |  | 0.0 | 53.0 | 33.8 | 681.7 | 0.0 | 0.0 |
| 141.22 | Top - Section 3 | 37.8 | 239.8 |  |  |  |  | 0.0 | 20.6 | 37.8 | 260.4 | 0.0 | 0.0 |
| 145.00 |  | 35.8 | 293.4 |  |  |  |  | 0.0 | 63.9 | 35.8 | 357.3 | 0.0 | 0.0 |
| 146.00 | Appurtenance(s) | 22.0 | 75.8 | 1,076.4 | 0.0 | 0.0 | 884.0 | 0.0 | 16.9 | 1,098.3 | 976.7 | 0.0 | 0.0 |
| 148.00 | Appurtenance(s) | 28.9 | 149.2 | 206.7 | 0.0 | 0.0 | 1,500.0 | 0.0 | 29.5 | 235.6 | 1,678.7 | 0.0 | 0.0 |
| 150.00 | Appurtenance(s) | 21.4 | 146.1 | 483.1 | 0.0 | - 663.0 | 1,616.0 | 0.0 | 29.5 | 504.5 | 1,791.6 | 0.0 | 0.0 |
| 151.00 |  | 7.1 | 71.9 |  |  |  |  | 0.0 | 0.0 | 7.1 | 71.9 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 5,638.6 | 50,144.0 | 0.00 | 0.00 |

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Site Number: $411186 \quad$ Code: ANSI/TIA-222-G © 2007-2021 by ATC IP LLC. All rights reserved.

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:58 PM
Customer: AT\&T MOBILITY

| Load Case: 1.0D +1.0 W | Serviceability 60 mph |
| :---: | :---: |
| Gust Response Factor: 1.10 |  |
| Dead Load Factor: 1.00 |  |
| Wind Load Factor :1.00 | Wind Importance Factor 1.00 |

Calculated Forces

| Seg Elev | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \end{gathered}$ | $\begin{aligned} & \mathrm{Vu} \\ & \mathrm{FX}(-) \end{aligned}$ | Tu <br> MY | Mu MZ | Mu <br> MX | Resultant Moment | $\begin{aligned} & \text { phi } \\ & \text { Pn } \end{aligned}$ | phi | $\begin{aligned} & \text { phi } \\ & \text { Tr } \end{aligned}$ | $\begin{aligned} & \text { phi } \\ & \text { Mn } \end{aligned}$ | Total |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (ft) | (kips) | (kips) | (ft-kips) | (ft-kips) | (ft-kips) | (ft-kips) | (kips) | (kips) | (ft-kips) | (ft-kips) | (in) | (deg) | Ratio |
| 0.00 | -50.14 | -5.59 | 0.00 | -608.18 | 0.00 | 608.18 | 7,216.29 | 3,608.15 | 20,023.1 | 10,026.4 | 0.00 | 0.00 | 0.068 |
| 5.00 | -48.18 | -5.49 | 0.00 | -580.24 | 0.00 | 580.24 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.01 | -0.01 | 0.067 |
| 10.00 | -46.25 | -5.39 | 0.00 | -552.79 | 0.00 | 552.79 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.03 | -0.03 | 0.066 |
| 15.00 | -44.36 | -5.30 | 0.00 | -525.84 | 0.00 | 525.84 | 6,915.90 | 3,457.95 | 17,951.6 | 8,989.14 | 0.07 | -0.04 | 0.065 |
| 20.00 | -42.52 | -5.20 | 0.00 | -499.35 | 0.00 | 499.35 | 6,810.85 | 3,405.43 | 17,272.5 | 8,649.09 | 0.12 | -0.06 | 0.064 |
| 25.00 | -40.71 | -5.11 | 0.00 | -473.34 | 0.00 | 473.34 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.18 | -0.07 | 0.063 |
| 30.00 | -38.94 | -5.02 | 0.00 | -447.79 | 0.00 | 447.79 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 0.27 | -0.09 | 0.062 |
| 35.00 | -37.21 | -4.92 | 0.00 | -422.70 | 0.00 | 422.70 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 0.37 | -0.10 | 0.061 |
| 40.00 | -35.51 | -4.83 | 0.00 | -398.08 | 0.00 | 398.08 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 0.48 | -0.12 | 0.060 |
| 45.00 | -33.86 | -4.77 | 0.00 | -373.93 | 0.00 | 373.93 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 0.61 | -0.13 | 0.059 |
| 46.28 | -33.44 | -4.72 | 0.00 | -367.85 | 0.00 | 367.85 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 0.65 | -0.14 | 0.059 |
| 50.00 | -31.15 | -4.64 | 0.00 | -350.28 | 0.00 | 350.28 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 0.76 | -0.15 | 0.057 |
| 53.73 | -28.89 | -4.59 | 0.00 | -332.96 | 0.00 | 332.96 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 0.88 | -0.16 | 0.055 |
| 55.00 | -28.48 | -4.53 | 0.00 | -327.14 | 0.00 | 327.14 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 0.92 | -0.16 | 0.054 |
| 60.00 | -26.92 | -4.42 | 0.00 | -304.51 | 0.00 | 304.51 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 1.10 | -0.18 | 0.053 |
| 65.00 | -25.40 | -4.32 | 0.00 | -282.40 | 0.00 | 282.40 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 1.30 | -0.20 | 0.052 |
| 70.00 | -23.91 | -4.22 | 0.00 | -260.79 | 0.00 | 260.79 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 1.51 | -0.21 | 0.050 |
| 75.00 | -22.46 | -4.12 | 0.00 | -239.69 | 0.00 | 239.69 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 1.74 | -0.23 | 0.049 |
| 80.00 | -21.05 | -4.02 | 0.00 | -219.11 | 0.00 | 219.11 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 1.99 | -0.24 | 0.048 |
| 85.00 | -19.69 | -3.92 | 0.00 | -199.02 | 0.00 | 199.02 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 2.25 | -0.26 | 0.046 |
| 90.00 | -18.36 | -3.83 | 0.00 | -179.44 | 0.00 | 179.44 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 2.53 | -0.27 | 0.045 |
| 94.09 | -17.30 | -3.77 | 0.00 | -163.79 | 0.00 | 163.79 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 2.77 | -0.29 | 0.043 |
| 95.00 | -16.91 | -3.72 | 0.00 | -160.36 | 0.00 | 160.36 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 2.82 | -0.29 | 0.043 |
| 99.92 | -14.85 | -3.66 | 0.00 | -142.04 | 0.00 | 142.04 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 3.13 | -0.31 | 0.053 |
| 100.00 | -14.84 | -3.62 | 0.00 | -141.77 | 0.00 | 141.77 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 3.13 | -0.31 | 0.053 |
| 105.00 | -13.87 | -3.52 | 0.00 | -123.68 | 0.00 | 123.68 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 3.47 | -0.32 | 0.049 |
| 110.00 | -12.93 | -3.43 | 0.00 | -106.08 | 0.00 | 106.08 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 3.81 | -0.34 | 0.045 |
| 115.00 | -12.02 | -3.34 | 0.00 | -88.93 | 0.00 | 88.93 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 4.18 | -0.36 | 0.041 |
| 120.00 | -11.14 | -3.25 | 0.00 | -72.25 | 0.00 | 72.25 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 4.57 | -0.38 | 0.037 |
| 125.00 | -10.29 | -3.16 | 0.00 | -56.01 | 0.00 | 56.01 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 4.97 | -0.39 | 0.031 |
| 130.00 | -9.47 | -3.08 | 0.00 | -40.21 | 0.00 | 40.21 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 5.39 | -0.40 | 0.025 |
| 135.00 | -6.06 | -2.04 | 0.00 | -24.83 | 0.00 | 24.83 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 5.81 | -0.41 | 0.017 |
| 136.87 | -5.80 | -1.99 | 0.00 | -21.03 | 0.00 | 21.03 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 5.97 | -0.41 | 0.015 |
| 140.00 | -5.12 | -1.96 | 0.00 | -14.78 | 0.00 | 14.78 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 6.25 | -0.42 | 0.012 |
| 141.22 | -4.86 | -1.92 | 0.00 | -12.39 | 0.00 | 12.39 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 6.35 | -0.42 | 0.015 |
| 145.00 | -4.51 | -1.88 | 0.00 | -5.15 | 0.00 | 5.15 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 6.69 | -0.42 | 0.008 |
| 146.00 | -3.54 | -0.77 | 0.00 | -3.27 | 0.00 | 3.27 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 6.78 | -0.42 | 0.006 |
| 148.00 | -1.86 | -0.53 | 0.00 | -1.72 | 0.00 | 1.72 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 6.95 | -0.42 | 0.003 |
| 150.00 | -0.07 | -0.01 | 0.00 | -0.01 | 0.00 | 0.01 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 7.13 | -0.42 | 0.000 |
| 151.00 | 0.00 | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 7.22 | -0.42 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | ---: | ---: | :--- |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | 3/22/2021 7:18:58 PM |
| Customer: AT\&T MOBILITY |  |  |

## Equivalent Lateral Forces Method Analysis

(Based on ASCE7-10 Chapters 11, 12, 15)

| Spectral Response Acceleration for Short Period (S ${ }_{\mathrm{s}}$ ): | 0.18 |
| :---: | :---: |
| Spectral Response Acceleration at 1.0 Second Period ( $\mathrm{S}_{1}$ ) : | 0.06 |
| Long-Period Transition Period ( $\mathrm{T}_{\mathrm{L}}$ ) : | 6 |
| Importance Factor ( $\mathrm{I}_{\mathrm{E}}$ ): | 1.00 |
| Site Coefficient F ${ }_{\mathrm{a}}$ : | 1.60 |
| Site Coeffiecient F ${ }_{\mathrm{v}}$ : | 2.40 |
| Response Modification Coefficient (R): | 1.50 |
| Design Spectral Response Acceleration at Short Period (S ds ): | 0.19 |
| Design Spectral Response Acceleration at 1.0 Second Period (S di): | 0.10 |
| Seismic Response Coefficient ( C s): | 0.05 |
| Upper Limit $\mathrm{C}_{\text {s }}$ | 0.05 |
| Lower Limit C s | 0.03 |
| Period based on Rayleigh Method (sec): | 1.53 |
| Redundancy Factor (p): | 1.30 |
| Seismic Force Distribution Exponent (k): | 1.51 |
| Total Unfactored Dead Load: | 50.14 |
| Seismic Base Shear (E): | 2.96 |

$\underline{\text { Load Case }} \underline{(1.2+0.2 S d s) ~ * D L ~+~ E ~ E L F M ~}$
Seismic Equivalent Lateral Forces Method

| Segment | Height Above Base (ft) | Weight <br> (Ib) | $\begin{gathered} \mathrm{W}_{\mathrm{z}} \\ (\mathrm{lb}-\mathrm{ft}) \end{gathered}$ | $\mathrm{C}_{\mathrm{vx}}$ | Horizontal Force <br> (lb) | Vertical Force <br> (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 150.50 | 72 | 142 | 0.004 | 11 | 89 |
| 38 | 149.00 | 176 | 341 | 0.009 | 26 | 217 |
| 37 | 147.00 | 179 | 340 | 0.009 | 26 | 221 |
| 36 | 145.50 | 93 | 174 | 0.005 | 13 | 115 |
| 35 | 143.11 | 357 | 653 | 0.017 | 51 | 442 |
| 34 | 140.61 | 260 | 463 | 0.012 | 36 | 322 |
| 33 | 138.43 | 682 | 1,185 | 0.031 | 92 | 844 |
| 32 | 135.93 | 260 | 439 | 0.012 | 34 | 322 |
| 31 | 132.50 | 792 | 1,289 | 0.034 | 100 | 981 |
| 30 | 127.50 | 822 | 1,261 | 0.033 | 98 | 1,017 |
| 29 | 122.50 | 851 | 1,229 | 0.032 | 95 | 1,053 |
| 28 | 117.50 | 880 | 1,193 | 0.031 | 93 | 1,089 |
| 27 | 112.50 | 909 | 1,154 | 0.030 | 90 | 1,125 |
| 26 | 107.50 | 938 | 1,112 | 0.029 | 86 | 1,161 |
| 25 | 102.50 | 967 | 1,067 | 0.028 | 83 | 1,197 |
| 24 | 99.96 | 15 | 16 | 0.000 | 1 | 18 |
| 23 | 97.46 | 2,056 | 2,101 | 0.055 | 163 | 2,545 |
| 22 | 94.55 | 387 | 378 | 0.010 | 29 | 479 |
| 21 | 92.05 | 1,059 | 992 | 0.026 | 77 | 1,310 |
| 20 | 87.50 | 1,329 | 1,154 | 0.030 | 89 | 1,646 |
| 19 | 82.50 | 1,368 | 1,087 | 0.028 | 84 | 1,694 |
| 18 | 77.50 | 1,407 | 1,017 | 0.027 | 79 | 1,742 |
| 17 | 72.50 | 1,446 | 944 | 0.025 | 73 | 1,790 |

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:59 PM
Customer: AT\&T MOBILITY

| 16 | 67.50 | 1,485 | 870 | 0.023 | 68 | 1,838 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 62.50 | 1,524 | 795 | 0.021 | 62 | 1,886 |
| 14 | 57.50 | 1,563 | 719 | 0.019 | 56 | 1,934 |
| 13 | 54.37 | 403 | 170 | 0.004 | 13 | 498 |
| 12 | 51.87 | 2,258 | 888 | 0.023 | 69 | 2,795 |
| 11 | 48.14 | 2,297 | 807 | 0.021 | 63 | 2,843 |
| 10 | 45.64 | 416 | 135 | 0.004 | 10 | 514 |
| 9 | 42.50 | 1,653 | 481 | 0.013 | 37 | 2,045 |
| 8 | 37.50 | 1,691 | 407 | 0.011 | 32 | 2,094 |
| 7 | 32.50 | 1,730 | 336 | 0.009 | 26 | 2,142 |
| 6 | 27.50 | 1,769 | 267 | 0.007 | 21 | 2,190 |
| 5 | 22.50 | 1,808 | 201 | 0.005 | 16 | 2,238 |
| 4 | 17.50 | 1,847 | 140 | 0.004 | 11 | 2,286 |
| 3 | 12.50 | 1,886 | 86 | 0.002 | 7 | 2,334 |
| 2 | 7.50 | 1,925 | 41 | 0.001 | 3 | 2,383 |
| 1 | 2.50 | 1,964 | 8 | 0.000 | 1 | 2,431 |
| Generic 48" x 4" Pan | 150.00 | 120 | 235 | 0.006 | 18 | 149 |
| Generic 48" x 6" Pan | 150.00 | 40 | 78 | 0.002 | 6 | 50 |
| Generic 48" $\times 12 \mathrm{~Pa}$ | 150.00 | 90 | 177 | 0.005 | 14 | 111 |
| Generic 48" x 12" x | 150.00 | 140 | 275 | 0.007 | 21 | 173 |
| VZW Unused Reserve ( | 150.00 | 1,226 | 2,406 | 0.063 | 187 | 1,517 |
| Round Low Profile PI | 148.00 | 1,500 | 2,884 | 0.076 | 224 | 1,857 |
| Generic SSB (27lb) | 146.00 | 54 | 102 | 0.003 | 8 | 67 |
| Generic RRU | 146.00 | 225 | 424 | 0.011 | 33 | 278 |
| Generic 96" x 12" Pa | 146.00 | 405 | 763 | 0.020 | 59 | 501 |
| Amphenol Antel LPA-7 | 146.00 | 48 | 90 | 0.002 | 7 | 59 |
| Amphenol Antel LPA-8 | 146.00 | 152 | 286 | 0.007 | 22 | 188 |
| Ericsson RRUS 8843 B | 135.00 | 216 | 361 | 0.009 | 28 | 267 |
| Ericsson RRUS 4478 B | 135.00 | 180 | 301 | 0.008 | 23 | 222 |
| Ericsson RRUS 4449 B | 135.00 | 213 | 356 | 0.009 | 28 | 264 |
| Ericsson AIR 6449 B7 | 135.00 | 245 | 410 | 0.011 | 32 | 303 |
| Raycap DC9-48-60-24- | 135.00 | 32 | 54 | 0.001 | 4 | 40 |
| CCI DMP65R-BU8D | 135.00 | 287 | 480 | 0.013 | 37 | 355 |
| Generic Flat Light S | 135.00 | 1,200 | 2,008 | 0.053 | 156 | 1,485 |
| CCI TPA65R-BU8D | 135.00 | 248 | 414 | 0.011 | 32 | 306 |
|  |  | 50,144 | 38,184 | 1.000 | 2,961 | 62,066 |

Load Case (0.9-0.2Sds) * DL + E ELFM
Seismic (Reduced DL) Equivalent Lateral Forces Method

| Segment | Height <br> Above Base <br> (ft) | Weight <br> (Ib) | $\begin{gathered} \mathrm{W}_{\mathrm{z}} \\ (\mathrm{lb}-\mathrm{ft}) \end{gathered}$ | C vx | Horizontal Force <br> (lb) | Vertical Force <br> (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 150.50 | 72 | 142 | 0.004 | 11 | 62 |
| 38 | 149.00 | 176 | 341 | 0.009 | 26 | 151 |
| 37 | 147.00 | 179 | 340 | 0.009 | 26 | 154 |
| 36 | 145.50 | 93 | 174 | 0.005 | 13 | 80 |
| 35 | 143.11 | 357 | 653 | 0.017 | 51 | 308 |
| 34 | 140.61 | 260 | 463 | 0.012 | 36 | 225 |
| 33 | 138.43 | 682 | 1,185 | 0.031 | 92 | 588 |
| 32 | 135.93 | 260 | 439 | 0.012 | 34 | 224 |
| 31 | 132.50 | 792 | 1,289 | 0.034 | 100 | 683 |
| 30 | 127.50 | 822 | 1,261 | 0.033 | 98 | 708 |
| 29 | 122.50 | 851 | 1,229 | 0.032 | 95 | 734 |
| 28 | 117.50 | 880 | 1,193 | 0.031 | 93 | 759 |
| 27 | 112.50 | 909 | 1,154 | 0.030 | 90 | 784 |
| 26 | 107.50 | 938 | 1,112 | 0.029 | 86 | 809 |
| 25 | 102.50 | 967 | 1,067 | 0.028 | 83 | 834 |
| 24 | 99.96 | 15 | 16 | 0.000 | 1 | 13 |
| 23 | 97.46 | 2,056 | 2,101 | 0.055 | 163 | 1,773 |
| 22 | 94.55 | 387 | 378 | 0.010 | 29 | 334 |
| 21 | 92.05 | 1,059 | 992 | 0.026 | 77 | 913 |

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03 3/22/2021 7:18:59 PM
Customer: AT\&T MOBILITY

| 20 | 87.50 | 1,329 | 1,154 | 0.030 | 89 | 1,146 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 82.50 | 1,368 | 1,087 | 0.028 | 84 | 1,180 |
| 18 | 77.50 | 1,407 | 1,017 | 0.027 | 79 | 1,213 |
| 17 | 72.50 | 1,446 | 944 | 0.025 | 73 | 1,247 |
| 16 | 67.50 | 1,485 | 870 | 0.023 | 68 | 1,280 |
| 15 | 62.50 | 1,524 | 795 | 0.021 | 62 | 1,314 |
| 14 | 57.50 | 1,563 | 719 | 0.019 | 56 | 1,348 |
| 13 | 54.37 | 403 | 170 | 0.004 | 13 | 347 |
| 12 | 51.87 | 2,258 | 888 | 0.023 | 69 | 1,947 |
| 11 | 48.14 | 2,297 | 807 | 0.021 | 63 | 1,980 |
| 10 | 45.64 | 416 | 135 | 0.004 | 10 | 358 |
| 9 | 42.50 | 1,653 | 481 | 0.013 | 37 | 1,425 |
| 8 | 37.50 | 1,691 | 407 | 0.011 | 32 | 1,458 |
| 7 | 32.50 | 1,730 | 336 | 0.009 | 26 | 1,492 |
| 6 | 27.50 | 1,769 | 267 | 0.007 | 21 | 1,526 |
| 5 | 22.50 | 1,808 | 201 | 0.005 | 16 | 1,559 |
| 4 | 17.50 | 1,847 | 140 | 0.004 | 11 | 1,593 |
| 3 | 12.50 | 1,886 | 86 | 0.002 | 7 | 1,626 |
| 2 | 7.50 | 1,925 | 41 | 0.001 | 3 | 1,660 |
| 1 | 2.50 | 1,964 | 8 | 0.000 | 1 | 1,693 |
| Generic 48" x 4" Pan | 150.00 | 120 | 235 | 0.006 | 18 | 103 |
| Generic 48" x 6" Pan | 150.00 | 40 | 78 | 0.002 | 6 | 34 |
| Generic 48" x 12" Pa | 150.00 | 90 | 177 | 0.005 | 14 | 78 |
| Generic 48" x 12" x | 150.00 | 140 | 275 | 0.007 | 21 | 121 |
| VZW Unused Reserve ( | 150.00 | 1,226 | 2,406 | 0.063 | 187 | 1,057 |
| Round Low Profile PI | 148.00 | 1,500 | 2,884 | 0.076 | 224 | 1,293 |
| Generic SSB (27lb) | 146.00 | 54 | 102 | 0.003 | 8 | 47 |
| Generic RRU | 146.00 | 225 | 424 | 0.011 | 33 | 194 |
| Generic 96" x 12" Pa | 146.00 | 405 | 763 | 0.020 | 59 | 349 |
| Amphenol Antel LPA-7 | 146.00 | 48 | 90 | 0.002 | 7 | 41 |
| Amphenol Antel LPA-8 | 146.00 | 152 | 286 | 0.007 | 22 | 131 |
| Ericsson RRUS 8843 B | 135.00 | 216 | 361 | 0.009 | 28 | 186 |
| Ericsson RRUS 4478 B | 135.00 | 180 | 301 | 0.008 | 23 | 155 |
| Ericsson RRUS 4449 B | 135.00 | 213 | 356 | 0.009 | 28 | 184 |
| Ericsson AIR 6449 B7 | 135.00 | 245 | 410 | 0.011 | 32 | 211 |
| Raycap DC9-48-60-24- | 135.00 | 32 | 54 | 0.001 | 4 | 28 |
| CCI DMP65R-BU8D | 135.00 | 287 | 480 | 0.013 | 37 | 248 |
| Generic Flat Light S | 135.00 | 1,200 | 2,008 | 0.053 | 156 | 1,035 |
| CCI TPA65R-BU8D | 135.00 | 248 | 414 | 0.011 | 32 | 213 |
|  |  | 50,144 | 38,184 | 1.000 | 2,961 | 43,236 |

Load Case ( $1.2+0.2$ Sds) * DL + E ELFM Seismic Equivalent Lateral Forces Method Calculated Forces

| Seg <br> Elev <br> (ft) |  | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ |  | Resultant Moment (ft-kips) | phi Pn (kips) | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ |  | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -59.64 | -2.96 | 0.00 | -329.63 | 0.00 | 329.63 | 7,216.29 | 3,608.15 | 20,023.1 | 10,026.4 | 0.00 | 0.00 | 0.041 |
| 5.00 | -57.25 | -2.97 | 0.00 | -314.82 | 0.00 | 314.82 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.00 | -0.01 | 0.041 |
| 10.00 | -54.92 | -2.97 | 0.00 | -299.98 | 0.00 | 299.98 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.02 | -0.02 | 0.040 |
| 15.00 | -52.63 | -2.96 | 0.00 | -285.14 | 0.00 | 285.14 | 6,915.90 | 3,457.95 | 17,951 | 8,989.14 | 0.04 | -0.02 | 0.039 |
| 20.00 | -50.39 | -2.95 | 0.00 | -270.33 | 0.00 | 270.33 | 6,810.85 | ,405.43 | 17,27 | ,649.09 | 0.06 | -0.03 | 0.039 |
| 25.00 | -48.20 | -2.94 | 0.00 | -255.56 | 0.00 | 255.56 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.10 | -0.04 | 0.038 |
| 30.00 | -46.06 | -2.92 | 0.00 | -240.87 | 0.00 | 240.87 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 0.14 | -0.05 | 0.037 |
| 35.00 | -43.97 | -2.89 | 0.00 | -226.29 | 0.00 | 226.29 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 0.20 | -0.05 | 0.036 |
| 40.00 | -41.92 | -2.86 | 0.00 | -211.84 | 0.00 | 211.84 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 0.26 | -0.06 | 0.036 |
| 45.00 | -41.41 | -2.85 | 0.00 | -197.56 | 0.00 | 197.56 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 0.33 | -0.07 | 0.035 |
| 46.28 | -38.56 | -2.79 | 0.00 | -193.92 | 0.00 | 193.92 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 0.35 | -0.07 | 0.034 |
| 50.00 | -35.77 | -2.72 | 0.00 | -183.55 | 0.00 | 183.55 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 0.41 | -0.08 | 0.033 |
| 53.73 | -35.27 | -2.71 | 0.00 | -173.41 | 0.00 | 173.41 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 0.47 | -0.09 | 0.032 |
| 55.00 | -33.33 | -2.65 | 0.00 | -169.98 | 0.00 | 169.98 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 0.50 | -0.09 | 0.031 |
| 60.00 | -31.45 | -2.59 | 0.00 | -156.73 | 0.00 | 156.73 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 0.59 | -0.10 | 0.030 |
| 65.00 | -29.61 | -2.52 | 0.00 | -143.78 | 0.00 | 143.78 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 0.70 | -0.10 | 0.029 |
| 70.00 | -27.82 | -2.45 | 0.00 | -131.17 | 0.00 | 131.17 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 0.81 | -0.11 | 0.028 |
| 75.00 | -26.08 | -2.37 | 0.00 | -118.91 | 0.00 | 118.91 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 0.93 | -0.12 | 0.027 |
| 80.00 | -24.38 | -2.29 | 0.00 | -107.06 | 0.00 | 107.06 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 1.06 | -0.13 | 0.026 |
| 85.00 | -22.74 | -2.20 | 0.00 | -95.62 | 0.00 | 95.62 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 1.20 | -0.14 | 0.025 |
| 90.00 | -21.43 | -2.12 | 0.00 | -84.64 | 0.00 | 84.64 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 1.35 | -0.14 | 0.024 |
| 94.09 | -20.95 | -2.09 | 0.00 | -75.97 | 0.00 | 75.97 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 1.47 | -0.15 | 0.023 |
| 95.00 | -18.40 | -1.92 | 0.00 | -74.07 | 0.00 | 74.07 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 1.50 | -0.15 | 0.022 |
| 99.92 | -18.39 | -1.92 | 0.00 | -64.60 | 0.00 | 64.60 | 3,494.98 | ,747.49 | 5,818.92 | 2,913.79 | 1.66 | -0.16 | 0.027 |
| 100.00 | -17.19 | -1.84 | 0.00 | -64.46 | 0.00 | 64.46 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 1.66 | -0.16 | 0.027 |
| 105.00 | -16.03 | -1.75 | 0.00 | -55.27 | 0.00 | 55.27 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 1.83 | -0.17 | 0.025 |
| 110.00 | -14.90 | -1.66 | 0.00 | -46.52 | 0.00 | 46.52 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 2.01 | -0.17 | 0.023 |
| 115.00 | -13.81 | -1.57 | 0.00 | -38.23 | 0.00 | 38.23 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 2.19 | -0.18 | 0.020 |
| 120.00 | -12.76 | -1.47 | 0.00 | -30.40 | 0.00 | 30.40 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 2.39 | -0.19 | 0.018 |
| 125.00 | -11.74 | -1.37 | 0.00 | -23.06 | 0.00 | 23.06 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 2.59 | -0.19 | 0.015 |
| 130.00 | -10.76 | -1.27 | 0.00 | -16.22 | 0.00 | 16.22 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 2.79 | -0.20 | 0.013 |
| 135.00 | -7.20 | -0.88 | 0.00 | -9.90 | 0.00 | 9.90 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 3.00 | -0.20 | 0.009 |
| 136.87 | -6.36 | -0.78 | 0.00 | -8.25 | 0.00 | 8.25 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 3.08 | -0.20 | 0.007 |
| 140.00 | -6.03 | -0.75 | 0.00 | -5.80 | 0.00 | 5.80 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 3.22 | -0.21 | 0.006 |
| 141.22 | -5.59 | -0.70 | 0.00 | -4.88 | 0.00 | 4.88 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 3.27 | -0.21 | 0.008 |
| 145.00 | -5.48 | -0.68 | 0.00 | -2.25 | 0.00 | 2.25 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 3.44 | -0.21 | 0.006 |
| 146.00 | -4.16 | -0.52 | 0.00 | -1.57 | 0.00 | 1.57 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 3.48 | -0.21 | 0.004 |
| 148.00 | -2.09 | -0.26 | 0.00 | -0.53 | 0.00 | 0.53 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 3.57 | -0.21 | 0.002 |
| 150.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 3.65 | -0.21 | 0.000 |
| 151.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 3.70 | -0.21 | 0.000 |


| Seg Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \text { FY (-) } \\ \text { (kips) } \\ \hline \end{gathered}$ | Vu FX (-) (kips) | Tu MY (ft-kips) | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi <br> Pn <br> (kips) | phi Vn (kips) | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \mathrm{Mn} \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -41.54 | -2.96 | 0.00 | -327.76 | 0.00 | 327.76 | 7,216.29 | 3,608.15 | 20,023. | 10,026.4 | 0.00 | 0.00 | 0.038 |
| 5.00 | -39.88 | -2.96 | 0.00 | -312.95 | 0.00 | 312.95 | 7,118.62 | 3,559.31 | 19,327.3 | 9,678.04 | 0.00 | -0.01 | 0.038 |
| 10.00 | -38.26 | -2.96 | 0.00 | -298.13 | 0.00 | 298.13 | 7,018.49 | 3,509.25 | 18,636.6 | 9,332.20 | 0.02 | -0.01 | 0.037 |
| 15.00 | -36.66 | -2.96 | 0.00 | -283.32 | 0.00 | 283.32 | 6,915.90 | 3,457.95 | 17,951.6 | 8,989.14 | 0.04 | -0.02 | 0.037 |
| 20.00 | -35.10 | -2.94 | 0.00 | -268.54 | 0.00 | 268.54 | 6,810.85 | 3,405.43 | 17,272.5 | 8,649.09 | 0.06 | -0.03 | 0.036 |
| 25.00 | -33.58 | -2.93 | 0.00 | -253.82 | 0.00 | 253.82 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.10 | -0.04 | 0.036 |
| 30.00 | -32.09 | -2.90 | 0.00 | -239.19 | 0.00 | 239.19 | 6,593.37 | 3,296.69 | 15,934.1 | 7,978.90 | 0.14 | -0.05 | 0.035 |
| 35.00 | -30.63 | -2.88 | 0.00 | -224.67 | 0.00 | 224.67 | 6,480.94 | 3,240.47 | 15,275.6 | 7,649.19 | 0.20 | -0.05 | 0.034 |
| 40.00 | -29.20 | -2.84 | 0.00 | -210.29 | 0.00 | 210.29 | 6,366.05 | 3,183.02 | 14,625.0 | 7,323.38 | 0.26 | -0.06 | 0.033 |
| 45.00 | -28.84 | -2.83 | 0.00 | -196.08 | 0.00 | 196.08 | 6,248.70 | 3,124.35 | 13,982.5 | 7,001.67 | 0.33 | -0.07 | 0.033 |
| 46.28 | -26.86 | -2.77 | 0.00 | -192.47 | 0.00 | 192.47 | 6,218.35 | 3,109.18 | 13,819.9 | 6,920.25 | 0.35 | -0.07 | 0.032 |
| 50.00 | -24.91 | -2.70 | 0.00 | -182.15 | 0.00 | 182.15 | 6,128.89 | 3,064.44 | 13,348.7 | 6,684.30 | 0.41 | -0.08 | 0.031 |
| 53.73 | -24.57 | -2.69 | 0.00 | -172.07 | 0.00 | 172.07 | 6,122.55 | 3,061.27 | 13,315.8 | 6,667.80 | 0.47 | -0.09 | 0.030 |
| 55.00 | -23.22 | -2.63 | 0.00 | -168.66 | 0.00 | 168.66 | 6,091.73 | 3,045.87 | 13,156.5 | 6,588.07 | 0.49 | -0.09 | 0.029 |
| 60.00 | -21.91 | -2.57 | 0.00 | -155.49 | 0.00 | 155.49 | 5,968.71 | 2,984.35 | 12,534.7 | 6,276.69 | 0.59 | -0.10 | 0.028 |
| 65.00 | -20.62 | -2.51 | 0.00 | -142.63 | 0.00 | 142.63 | 5,843.22 | 2,921.61 | 11,922.5 | 5,970.14 | 0.69 | -0.10 | 0.027 |
| 70.00 | -19.38 | -2.43 | 0.00 | -130.10 | 0.00 | 130.10 | 5,697.45 | 2,848.72 | 11,285.1 | 5,650.96 | 0.81 | -0.11 | 0.026 |
| 75.00 | -18.16 | -2.35 | 0.00 | -117.93 | 0.00 | 117.93 | 5,527.55 | 2,763.78 | 10,618.8 | 5,317.30 | 0.93 | -0.12 | 0.025 |
| 80.00 | -16.98 | -2.27 | 0.00 | -106.16 | 0.00 | 106.16 | 5,357.66 | 2,678.83 | 9,972.76 | 4,993.79 | 1.06 | -0.13 | 0.024 |
| 85.00 | -15.84 | -2.18 | 0.00 | -94.81 | 0.00 | 94.81 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 1.19 | -0.13 | 0.023 |
| 90.00 | -14.93 | -2.10 | 0.00 | -83.92 | 0.00 | 83.92 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 1.34 | -0.14 | 0.022 |
| 94.09 | -14.59 | -2.07 | 0.00 | -75.31 | 0.00 | 75.31 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 1.46 | -0.15 | 0.021 |
| 95.00 | -12.82 | -1.91 | 0.00 | -73.43 | 0.00 | 73.43 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 1.49 | -0.15 | 0.021 |
| 99.92 | -12.81 | -1.91 | 0.00 | -64.04 | 0.00 | 64.04 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 1.65 | -0.16 | 0.026 |
| 100.00 | -11.97 | -1.82 | 0.00 | -63.90 | 0.00 | 63.90 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 1.65 | -0.16 | 0.025 |
| 105.00 | -11.16 | -1.74 | 0.00 | -54.79 | 0.00 | 54.79 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 1.82 | -0.16 | 0.023 |
| 110.00 | -10.38 | -1.64 | 0.00 | -46.11 | 0.00 | 46.11 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 1.99 | -0.17 | 0.021 |
| 115.00 | -9.62 | -1.55 | 0.00 | -37.88 | 0.00 | 37.88 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 2.18 | -0.18 | 0.019 |
| 120.00 | -8.89 | -1.45 | 0.00 | -30.13 | 0.00 | 30.13 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 2.37 | -0.19 | 0.017 |
| 125.00 | -8.18 | -1.36 | 0.00 | -22.85 | 0.00 | 22.85 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 2.57 | -0.19 | 0.014 |
| 130.00 | -7.50 | -1.25 | 0.00 | -16.08 | 0.00 | 16.08 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 2.77 | -0.20 | 0.011 |
| 135.00 | -5.01 | -0.87 | 0.00 | -9.81 | 0.00 | 9.81 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 2.98 | -0.20 | 0.008 |
| 136.87 | -4.43 | -0.78 | 0.00 | -8.18 | 0.00 | 8.18 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 3.06 | -0.20 | 0.007 |
| 140.00 | -4.20 | -0.74 | 0.00 | -5.74 | 0.00 | 5.74 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 3.20 | -0.20 | 0.005 |
| 141.22 | -3.89 | -0.69 | 0.00 | -4.84 | 0.00 | 4.84 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 3.25 | -0.20 | 0.007 |
| 145.00 | -3.81 | -0.68 | 0.00 | -2.23 | 0.00 | 2.23 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 3.41 | -0.21 | 0.005 |
| 146.00 | -2.90 | -0.52 | 0.00 | -1.56 | 0.00 | 1.56 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 3.45 | -0.21 | 0.004 |
| 148.00 | -1.45 | -0.26 | 0.00 | -0.52 | 0.00 | 0.52 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 3.54 | -0.21 | 0.002 |
| 150.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 3.63 | -0.21 | 0.000 |
| 151.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 3.67 | -0.21 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :--- | ---: | :--- |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 | $3 / 22 / 20217: 18: 59$ PM |
| Customer: AT\&T MOBILITY |  |  |

## Equivalent Modal Analysis Method

(Based on ASCE7-10 Chapters 11, 12 \& 15 and ANSI/TIA-G, section 2.7)

| Spectral Response Acceleration for Short Period (S ${ }_{\mathrm{s}}$ ) : | 0.18 |
| :---: | :---: |
| Spectral Response Acceleration at 1.0 Second Period (S ${ }_{1}$ ): | 0.06 |
| Importance Factor ( $\mathrm{I}_{\mathrm{E}}$ ) : | 1.00 |
| Site Coefficient $\mathrm{F}_{\mathrm{a}}$ : | 1.60 |
| Site Coefficient F v | 2.40 |
| Response Modification Coefficient (R): | 1.50 |
| Design Spectral Response Acceleration at Short Period (S ds): | 0.19 |
| Desing Spectral Response Acceleration at 1.0 Second Period (S d1 ) : | 0.10 |
| Period Based on Rayleigh Method (sec): | 1.53 |
| Redundancy Factor (p): | 1.30 |

$\underline{\text { Load Case }} \underline{(1.2+0.2 S d s) ~ * ~ D L ~+~ E ~ E M A M ~ S e i s m i c ~ E q u i v a l e n t ~ M o d a l ~ A n a l y s i s ~ M e t h o d ~}$

| Segment | Height Above Base <br> (ft) | Weight <br> (lb) | a | b | C | Saz | Horizontal Force (lb) | Vertical Force (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 150.50 | 72 | 1.878 | 1.915 | 1.116 | 0.365 | 23 | 89 |
| 38 | 149.00 | 176 | 1.840 | 1.728 | 1.048 | 0.342 | 52 | 217 |
| 37 | 147.00 | 179 | 1.791 | 1.499 | 0.962 | 0.313 | 48 | 221 |
| 36 | 145.50 | 93 | 1.755 | 1.341 | 0.901 | 0.292 | 23 | 115 |
| 35 | 143.11 | 357 | 1.698 | 1.113 | 0.811 | 0.260 | 80 | 442 |
| 34 | 140.61 | 260 | 1.639 | 0.904 | 0.724 | 0.228 | 52 | 322 |
| 33 | 138.43 | 682 | 1.589 | 0.743 | 0.655 | 0.203 | 120 | 844 |
| 32 | 135.93 | 260 | 1.532 | 0.582 | 0.581 | 0.175 | 39 | 322 |
| 31 | 132.50 | 792 | 1.455 | 0.397 | 0.491 | 0.140 | 96 | 981 |
| 30 | 127.50 | 822 | 1.347 | 0.192 | 0.380 | 0.097 | 69 | 1,017 |
| 29 | 122.50 | 851 | 1.244 | 0.050 | 0.289 | 0.062 | 46 | 1,053 |
| 28 | 117.50 | 880 | 1.144 | -0.041 | 0.215 | 0.035 | 26 | 1,089 |
| 27 | 112.50 | 909 | 1.049 | -0.094 | 0.157 | 0.015 | 12 | 1,125 |
| 26 | 107.50 | 938 | 0.958 | -0.118 | 0.111 | 0.003 | 2 | 1,161 |
| 25 | 102.50 | 967 | 0.871 | -0.121 | 0.077 | -0.003 | -3 | 1,197 |
| 24 | 99.96 | 15 | 0.828 | -0.117 | 0.062 | -0.004 | 0 | 18 |
| 23 | 97.46 | 2,056 | 0.787 | -0.109 | 0.050 | -0.003 | -5 | 2,545 |
| 22 | 94.55 | 387 | 0.741 | -0.099 | 0.039 | -0.001 | 0 | 479 |
| 21 | 92.05 | 1,059 | 0.702 | -0.088 | 0.030 | 0.002 | 2 | 1,310 |
| 20 | 87.50 | 1,329 | 0.635 | -0.065 | 0.019 | 0.008 | 10 | 1,646 |
| 19 | 82.50 | 1,368 | 0.564 | -0.040 | 0.011 | 0.017 | 20 | 1,694 |
| 18 | 77.50 | 1,407 | 0.498 | -0.015 | 0.007 | 0.025 | 31 | 1,742 |
| 17 | 72.50 | 1,446 | 0.436 | 0.006 | 0.006 | 0.032 | 41 | 1,790 |
| 16 | 67.50 | 1,485 | 0.378 | 0.025 | 0.007 | 0.038 | 49 | 1,838 |
| 15 | 62.50 | 1,524 | 0.324 | 0.040 | 0.010 | 0.041 | 54 | 1,886 |
| 14 | 57.50 | 1,563 | 0.274 | 0.051 | 0.015 | 0.043 | 58 | 1,934 |
| 13 | 54.37 | 403 | 0.245 | 0.056 | 0.018 | 0.043 | 15 | 498 |
| 12 | 51.87 | 2,258 | 0.223 | 0.060 | 0.020 | 0.043 | 84 | 2,795 |
| 11 | 48.14 | 2,297 | 0.192 | 0.064 | 0.024 | 0.043 | 85 | 2,843 |
| 10 | 45.64 | 416 | 0.173 | 0.066 | 0.027 | 0.042 | 15 | 514 |
| 9 | 42.50 | 1,653 | 0.150 | 0.068 | 0.030 | 0.041 | 59 | 2,045 |
| 8 | 37.50 | 1,691 | 0.117 | 0.070 | 0.035 | 0.040 | 58 | 2,094 |
| 7 | 32.50 | 1,730 | 0.088 | 0.071 | 0.039 | 0.038 | 57 | 2,142 |
| 6 | 27.50 | 1,769 | 0.063 | 0.072 | 0.041 | 0.036 | 56 | 2,190 |

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Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:59 PM
Customer: AT\&T MOBILITY

| 5 | 22.50 | 1,808 | 0.042 | 0.070 | 0.042 | 0.035 | 54 | 2,238 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 17.50 | 1,847 | 0.025 | 0.067 | 0.040 | 0.032 | 51 | 2,286 |
| 3 | 12.50 | 1,886 | 0.013 | 0.059 | 0.034 | 0.028 | 46 | 2,334 |
| 2 | 7.50 | 1,925 | 0.005 | 0.044 | 0.025 | 0.021 | 35 | 2,383 |
| 1 | 2.50 | 1,964 | 0.001 | 0.018 | 0.010 | 0.009 | 16 | 2,431 |
| Generic 48" x 4" Pan | 150.00 | 120 | 1.865 | 1.851 | 1.093 | 0.357 | 37 | 149 |
| Generic 48" x 6" Pan | 150.00 | 40 | 1.865 | 1.851 | 1.093 | 0.357 | 12 | 50 |
| Generic 48" $\times 12 \mathrm{~Pa}$ | 150.00 | 90 | 1.865 | 1.851 | 1.093 | 0.357 | 28 | 111 |
| Generic 48" $\times 12 \mathrm{l}$ x | 150.00 | 140 | 1.865 | 1.851 | 1.093 | 0.357 | 43 | 173 |
| VZW Unused Reserve ( | 150.00 | 1,226 | 1.865 | 1.851 | 1.093 | 0.357 | 380 | 1,517 |
| Round Low Profile PI | 148.00 | 1,500 | 1.816 | 1.611 | 1.004 | 0.327 | 426 | 1,857 |
| Generic SSB (27lb) | 146.00 | 54 | 1.767 | 1.392 | 0.921 | 0.299 | 14 | 67 |
| Generic RRU | 146.00 | 225 | 1.767 | 1.392 | 0.921 | 0.299 | 58 | 278 |
| Generic 96" x 12" Pa | 146.00 | 405 | 1.767 | 1.392 | 0.921 | 0.299 | 105 | 501 |
| Amphenol Antel LPA-7 | 146.00 | 48 | 1.767 | 1.392 | 0.921 | 0.299 | 12 | 59 |
| Amphenol Antel LPA-8 | 146.00 | 152 | 1.767 | 1.392 | 0.921 | 0.299 | 39 | 188 |
| Ericsson RRUS 8843 B | 135.00 | 216 | 1.511 | 0.528 | 0.556 | 0.165 | 31 | 267 |
| Ericsson RRUS 4478 B | 135.00 | 180 | 1.511 | 0.528 | 0.556 | 0.165 | 26 | 222 |
| Ericsson RRUS 4449 B | 135.00 | 213 | 1.511 | 0.528 | 0.556 | 0.165 | 30 | 264 |
| Ericsson AIR 6449 B7 | 135.00 | 245 | 1.511 | 0.528 | 0.556 | 0.165 | 35 | 303 |
| Raycap DC9-48-60-24- | 135.00 | 32 | 1.511 | 0.528 | 0.556 | 0.165 | 5 | 40 |
| CCI DMP65R-BU8D | 135.00 | 287 | 1.511 | 0.528 | 0.556 | 0.165 | 41 | 355 |
| Generic Flat Light S | 135.00 | 1,200 | 1.511 | 0.528 | 0.556 | 0.165 | 172 | 1,485 |
| CCI TPA65R-BU8D | 135.00 | 248 | 1.511 | 0.528 | 0.556 | 0.165 | 35 | 306 |
|  |  | 50,144 | 61.352 | 32.512 | 24.682 | 8.105 | 3,106 | 62,066 |

Load Case (0.9-0.2Sds) * DL + E EMAM Seismic (Reduced DL) Equivalent Modal Analysis Method
Height
Above
Base

Segment
(ft)
Weight

Horizontal
Force
(Ib)
Vertical
Force
(lb)

| 39 | 150.50 | 72 | 1.878 | 1.915 | 1.116 | 0.365 | 23 | 62 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 38 | 149.00 | 176 | 1.840 | 1.728 | 1.048 | 0.342 | 52 | 151 |
| 37 | 147.00 | 179 | 1.791 | 1.499 | 0.962 | 0.313 | 48 | 154 |
| 36 | 145.50 | 93 | 1.755 | 1.341 | 0.901 | 0.292 | 23 | 80 |
| 35 | 143.11 | 357 | 1.698 | 1.113 | 0.811 | 0.260 | 80 | 308 |
| 34 | 140.61 | 260 | 1.639 | 0.904 | 0.724 | 0.228 | 52 | 225 |
| 33 | 138.43 | 682 | 1.589 | 0.743 | 0.655 | 0.203 | 120 | 588 |
| 32 | 135.93 | 260 | 1.532 | 0.582 | 0.581 | 0.175 | 39 | 224 |
| 31 | 132.50 | 792 | 1.455 | 0.397 | 0.491 | 0.140 | 96 | 683 |
| 30 | 127.50 | 822 | 1.347 | 0.192 | 0.380 | 0.097 | 69 | 708 |
| 29 | 122.50 | 851 | 1.244 | 0.050 | 0.289 | 0.062 | 46 | 734 |
| 28 | 117.50 | 880 | 1.144 | -0.041 | 0.215 | 0.035 | 26 | 759 |
| 27 | 112.50 | 909 | 1.049 | -0.094 | 0.157 | 0.015 | 12 | 784 |
| 26 | 107.50 | 938 | 0.958 | -0.118 | 0.111 | 0.003 | 2 | 809 |
| 25 | 102.50 | 967 | 0.871 | -0.121 | 0.077 | -0.003 | -3 | 834 |
| 24 | 99.96 | 15 | 0.828 | -0.117 | 0.062 | -0.004 | 0 | 13 |
| 23 | 97.46 | 2,056 | 0.787 | -0.109 | 0.050 | -0.003 | -5 | 1,773 |
| 22 | 94.55 | 387 | 0.741 | -0.099 | 0.039 | -0.001 | 0 | 334 |
| 21 | 92.05 | 1,059 | 0.702 | -0.088 | 0.030 | 0.002 | 2 | 913 |
| 20 | 87.50 | 1,329 | 0.635 | -0.065 | 0.019 | 0.008 | 10 | 1,146 |
| 19 | 82.50 | 1,368 | 0.564 | -0.040 | 0.011 | 0.017 | 20 | 1,180 |
| 18 | 77.50 | 1,407 | 0.498 | -0.015 | 0.007 | 0.025 | 31 | 1,213 |
| 17 | 72.50 | 1,446 | 0.436 | 0.006 | 0.006 | 0.032 | 41 | 1,247 |
| 16 | 67.50 | 1,485 | 0.378 | 0.025 | 0.007 | 0.038 | 49 | 1,280 |
| 15 | 62.50 | 1,524 | 0.324 | 0.040 | 0.010 | 0.041 | 54 | 1,314 |
| 14 | 57.50 | 1,563 | 0.274 | 0.051 | 0.015 | 0.043 | 58 | 1,348 |
| 13 | 54.37 | 403 | 0.245 | 0.056 | 0.018 | 0.043 | 15 | 347 |
| 12 | 51.87 | 2,258 | 0.223 | 0.060 | 0.020 | 0.043 | 84 | 1,947 |
| 11 | 48.14 | 2,297 | 0.192 | 0.064 | 0.024 | 0.043 | 85 | 1,980 |

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:59 PM
Customer: AT\&T MOBILITY

| 10 | 45.64 | 416 | 0.173 | 0.066 | 0.027 | 0.042 | 15 | 358 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 42.50 | 1,653 | 0.150 | 0.068 | 0.030 | 0.041 | 59 | 1,425 |
| 8 | 37.50 | 1,691 | 0.117 | 0.070 | 0.035 | 0.040 | 58 | 1,458 |
| 7 | 32.50 | 1,730 | 0.088 | 0.071 | 0.039 | 0.038 | 57 | 1,492 |
| 6 | 27.50 | 1,769 | 0.063 | 0.072 | 0.041 | 0.036 | 56 | 1,526 |
| 5 | 22.50 | 1,808 | 0.042 | 0.070 | 0.042 | 0.035 | 54 | 1,559 |
| 4 | 17.50 | 1,847 | 0.025 | 0.067 | 0.040 | 0.032 | 51 | 1,593 |
| 3 | 12.50 | 1,886 | 0.013 | 0.059 | 0.034 | 0.028 | 46 | 1,626 |
| 2 | 7.50 | 1,925 | 0.005 | 0.044 | 0.025 | 0.021 | 35 | 1,660 |
| 1 | 2.50 | 1,964 | 0.001 | 0.018 | 0.010 | 0.009 | 16 | 1,693 |
| Generic 48" x 4" Pan | 150.00 | 120 | 1.865 | 1.851 | 1.093 | 0.357 | 37 | 103 |
| Generic 48" x 6" Pan | 150.00 | 40 | 1.865 | 1.851 | 1.093 | 0.357 | 12 | 34 |
| Generic 48" x 12" Pa | 150.00 | 90 | 1.865 | 1.851 | 1.093 | 0.357 | 28 | 78 |
| Generic 48" x 12" x | 150.00 | 140 | 1.865 | 1.851 | 1.093 | 0.357 | 43 | 121 |
| VZW Unused Reserve ( | 150.00 | 1,226 | 1.865 | 1.851 | 1.093 | 0.357 | 380 | 1,057 |
| Round Low Profile PI | 148.00 | 1,500 | 1.816 | 1.611 | 1.004 | 0.327 | 426 | 1,293 |
| Generic SSB (27lb) | 146.00 | 54 | 1.767 | 1.392 | 0.921 | 0.299 | 14 | 47 |
| Generic RRU | 146.00 | 225 | 1.767 | 1.392 | 0.921 | 0.299 | 58 | 194 |
| Generic 96" x 12" Pa | 146.00 | 405 | 1.767 | 1.392 | 0.921 | 0.299 | 105 | 349 |
| Amphenol Antel LPA-7 | 146.00 | 48 | 1.767 | 1.392 | 0.921 | 0.299 | 12 | 41 |
| Amphenol Antel LPA-8 | 146.00 | 152 | 1.767 | 1.392 | 0.921 | 0.299 | 39 | 131 |
| Ericsson RRUS 8843 B | 135.00 | 216 | 1.511 | 0.528 | 0.556 | 0.165 | 31 | 186 |
| Ericsson RRUS 4478 B | 135.00 | 180 | 1.511 | 0.528 | 0.556 | 0.165 | 26 | 155 |
| Ericsson RRUS 4449 B | 135.00 | 213 | 1.511 | 0.528 | 0.556 | 0.165 | 30 | 184 |
| Ericsson AIR 6449 B7 | 135.00 | 245 | 1.511 | 0.528 | 0.556 | 0.165 | 35 | 211 |
| Raycap DC9-48-60-24- | 135.00 | 32 | 1.511 | 0.528 | 0.556 | 0.165 | 5 | 28 |
| CCI DMP65R-BU8D | 135.00 | 287 | 1.511 | 0.528 | 0.556 | 0.165 | 41 | 248 |
| Generic Flat Light S | 135.00 | 1,200 | 1.511 | 0.528 | 0.556 | 0.165 | 172 | 1,035 |
| CCI TPA65R-BU8D | 135.00 | 248 | 1.511 | 0.528 | 0.556 | 0.165 | 35 | 213 |
|  |  | 50,144 | 61.352 | 32.512 | 24.682 | 8.105 | 3,106 | 43,236 |

$\underline{\text { Load Case }}$ (1.2+0.2Sds) * DL + E EMAM Seismic Equivalent Modal Analysis Method Calculated Forces

| Seg Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \\ (\mathrm{kips}) \end{gathered}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \mathrm{Tu} \\ \mathrm{MY} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Mu } \\ \text { MX } \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{aligned} & \text { phi } \\ & \text { Vn } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{phi} \\ \mathrm{Mn} \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -59.64 | -3.09 | 0.00 | -358.43 | 0.00 | 358.43 | 7,216.29 | , 608 | ,023 | 26.4 | 0.00 | 0.00 | 0.044 |
| 5.00 | -57.25 | -3.07 | 0.00 | -342.96 | 0.00 | 342.96 | 7,118.62 | 3,559.311 | 19,327.35 | 9,678.04 | 0.00 | -0.01 | 0.043 |
| 10.00 | -54.92 | -3.03 | 0.00 | -327.62 | 0.00 | 327.62 | 7,018.49 | 3,509.251 | 18,636.69 | 9,332.20 | 0.02 | -0.02 | 0.043 |
| 15.00 | -52.63 | -2.98 | 0.00 | -312.48 | 0.00 | 312.48 | 6,915.90 | 3,457.951 | 17,951.60 | 8,989.14 | 0.04 | -0.02 | 0.042 |
| 20.00 | -50.39 | -2.94 | 0.00 | -297.55 | 0.00 | 297.55 | 6,810.85 | 3,405.431 | 17,272.51 | 8,649.09 | 0.07 | -0.03 | 0.042 |
| 25.00 | -48.20 | -2.89 | 0.00 | -282.87 | 0.00 | 282.87 | 6,703.34 | 3,351.671 | 16,599.8 | 8,312.27 | 0.11 | -0.04 | 0.041 |
| 30.00 | -46.06 | -2.84 | 0.00 | -268.43 | 0.00 | 268.43 | 6,593.37 | 3,296.691 | 15,934.1 | 7,978.90 | 0.16 | -0.05 | 0.041 |
| 35.00 | -43.97 | -2.78 | 0.00 | -254.25 | 0.00 | 254.25 | 6,480.94 | 3,240.471 | 15,275.68 | 7,649.19 | 0.22 | -0.06 | 0.040 |
| 40.00 | -41.92 | -2.73 | 0.00 | -240.34 | 0.00 | 240.34 | 6,366.05 | 3,183.021 | 14,625.01 | 7,323.38 | 0.28 | -0.07 | 0.039 |
| 45.00 | -41.41 | -2.72 | 0.00 | -226.70 | 0.00 | 226.70 | 6,248.70 | 3,124.3513, | 13,982.56 | 7,001.67 | 0.36 | -0.08 | 0.039 |
| 46.28 | -38.56 | -2.63 | 0.00 | -223.23 | 0.00 | 223.23 | 6,218.35 | 3,109.1813, | 13,819.95 | 6,920.25 | 0.38 | -0.08 | 0.038 |
| 50.00 | -35.77 | -2.55 | 0.00 | -213.43 | 0.00 | 213.43 | 6,128.89 | 3,064.44 1 | 13,348.75 | 6,684.30 | 0.45 | -0.09 | 0.038 |
| 53.73 | -35.27 | -2.53 | 0.00 | -203.93 | 0.00 | 203.93 | 6,122.55 | 3,061.2713, | 13,315.81 | 6,667.80 | 0.52 | -0.10 | 0.036 |
| 55.00 | -33.33 | -2.48 | 0.00 | -200.72 | 0.00 | 200.72 | 6,091.73 | 3,045.8713,1 | 13,156.5 | 6,588.07 | 0.55 | -0.10 | 0.036 |
| 60.00 | -31.45 | -2.42 | 0.00 | -188.33 | 0.00 | 188.33 | 5,968.7 | 2,984.3 | 12,534. | 6,276.69 | 0.66 | -0.11 | 0.035 |
| 65.00 | -29.61 | -2.38 | 0.00 | -176.21 | 0.00 | 176.21 | 5,843.2 | 2,921.6 | 11,922.5 | 5,970.14 | 0.78 | -0.12 | 0.035 |
| 70.00 | -27.82 | -2.34 | 0.00 | -164.33 | 0.00 | 164.33 | 5,697.4 | 2,848.72 | 11,285. 1 | 5,650.96 | 0.90 | -0.13 | 0.034 |
| 75.00 | -26.08 | -2.31 | 0.00 | -152.65 | 0.00 | 152.65 | 5,527.5 | 2,763.781 | 10,618 | 5,317.30 | 1.04 | -0.14 | 0.033 |
| 80.00 | -24.38 | -2.29 | 0.00 | -141.11 | 0.00 | 141.11 | 5,357.66 | 2,678.83 | 9,972.7 | 4,993.79 | 1.19 | -0.15 | 0.033 |
| 85.00 | -22.74 | -2.28 | 0.00 | -129.68 | 0.00 | 129.68 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 1.35 | -0.16 | 0.032 |
| 90.00 | -21.43 | -2.28 | 0.00 | -118.29 | 0.00 | 118.29 | 5,017.88 | 2,508.94 | 8,741.48 | 4,377.24 | 1.52 | -0.17 | 0.031 |
| 94.09 | -20.95 | -2.28 | 0.00 | -108.99 | 0.00 | 108.99 | 4,878.88 | 2,439.44 | 8,261.16 | 4,136.72 | 1.67 | -0.18 | 0.031 |
| 95.00 | -18.40 | -2.28 | 0.00 | -106.92 | 0.00 | 106.92 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 1.70 | -0.18 | 0.030 |
| 99.92 | -18.38 | -2.28 | 0.00 | -95.71 | 0.00 | 95.71 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 1.89 | -0.19 | 0.038 |
| 100.00 | -17.19 | -2.28 | 0.00 | -95.54 | 0.00 | 95.54 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 1.90 | -0.19 | 0.038 |
| 105.00 | -16.02 | -2.28 | 0.00 | -84.15 | 0.00 | 84.15 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 2.10 | -0.20 | 0.035 |
| 110.00 | -14.90 | -2.26 | 0.00 | -72.78 | 0.00 | 72.78 | 3,309.66 | 1,654.83 | 5,112.41 | 2,560.00 | 2.32 | -0.21 | 0.033 |
| 115.00 | -13.81 | -2.23 | 0.00 | -61.47 | 0.00 | 61.47 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 2.55 | -0.23 | 0.030 |
| 120.00 | -12.75 | -2.19 | 0.00 | -50.29 | 0.00 | 50.29 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 2.79 | -0.24 | 0.027 |
| 125.00 | -11.74 | -2.12 | 0.00 | -39.36 | 0.00 | 39.36 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 3.05 | -0.25 | 0.023 |
| 130.00 | -10.76 | -2.02 | 0.00 | -28.78 | 0.00 | 28.78 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 3.31 | -0.26 | 0.019 |
| 135.00 | -7.19 | -1.59 | 0.00 | -18.70 | 0.00 | 18.70 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 3.58 | -0.26 | 0.014 |
| 136.87 | -6.35 | -1.46 | 0.00 | -15.74 | 0.00 | 15.74 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 3.69 | -0.26 | 0.012 |
| 140.00 | -6.03 | -1.41 | 0.00 | -11.15 | 0.00 | 11.15 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 3.86 | -0.27 | 0.010 |
| 141.22 | -5.59 | -1.33 | 0.00 | -9.43 | 0.00 | 9.43 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 3.93 | -0.27 | 0.013 |
| 145.00 | -5.47 | -1.30 | 0.00 | -4.41 | 0.00 | 4.41 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 4.14 | -0.27 | 0.008 |
| 146.00 | -4.16 | -1.02 | 0.00 | -3.11 | 0.00 | 3.11 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 4.20 | -0.27 | 0.006 |
| 148.00 | -2.09 | -0.53 | 0.00 | -1.07 | 0.00 | 1.07 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 4.32 | -0.27 | 0.003 |
| 150.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 4.43 | -0.27 | 0.000 |
| 151.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 4.49 | -0.27 | 0.000 |

Site Number: $411186 \quad$ Code: ANSI/TIA-222-G $\quad \odot 2007$ - 2021 by ATC IP LLC. All rights reserved.

Site Name: West Granby, CT CT, CT
Engineering Number:13626835_C3_03
3/22/2021 7:18:59 PM
Customer: AT\&T MOBILITY

Load Case (0.9-0.2Sds) * DL + E EMAM Seismic (Reduced DL) Equivalent Modal Analysis Method Calculated Forces

| $\begin{aligned} & \text { Seg } \\ & \text { Elev } \\ & (\mathrm{ft}) \end{aligned}$ | $\begin{gathered} \mathrm{Pu} \\ \text { FY (-) } \\ \text { (kips) } \\ \hline \end{gathered}$ | $\begin{aligned} & V \mathrm{Vu} \\ & \text { FX }(-) \\ & \text { (kips) } \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{Tu} \\ \mathrm{MY} \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MXX} \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{phi} \\ \mathrm{Mn} \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -41.54 | -3.09 | 0.00 | -356.23 | 0.00 | 356.23 | 7,216.29 | 3,608.1520,0 | 0,023.14 | ,026.4 | 0.00 | 0.00 | 0.041 |
| 5.00 | -39.88 | -3.06 | 0.00 | -340.77 | 0.00 | 340.77 | 7,118.62 | 3,559.31 | 19,327.35 | 9,678.04 | 0.00 | -0.01 | 0.041 |
| 10.00 | -38.26 | -3.02 | 0.00 | -325.45 | 0.00 | 325.45 | 7,018.49 | 3,509.25 | 18,636.69 | 9,332.20 | 0.02 | -0.02 | 0.040 |
| 15.00 | -36.66 | -2.98 | 0.00 | -310.33 | 0.00 | 310.33 | 6,915.90 | 3,457.95 | 17,951.60 | 8,989.14 | 0.04 | -0.02 | 0.040 |
| 20.00 | -35.10 | -2.93 | 0.00 | -295.45 | 0.00 | 295.45 | 6,810.85 | 3,405.4317 | 17,272.51 | 8,649.09 | 0.07 | -0.03 | 0.039 |
| 25.00 | -33.58 | -2.88 | 0.00 | -280.82 | 0.00 | 280.82 | 6,703.34 | 3,351.67 | 16,599.8 | 8,312.27 | 0.11 | -0.04 | 0.039 |
| 30.00 | -32.08 | -2.82 | 0.00 | -266.44 | 0.00 | 266.44 | 6,593.37 | 3,296.69 | 15,934.11 | 7,978.90 | 0.16 | -0.05 | 0.038 |
| 35.00 | -30.63 | -2.77 | 0.00 | -252.33 | 0.00 | 252.33 | 6,480.94 | 3,240.47 | 15,275.68 | 7,649.19 | 0.22 | -0.06 | 0.038 |
| 40.00 | -29.20 | -2.71 | 0.00 | -238.49 | 0.00 | 238.49 | 6,366.05 | 3,183.02 | 14,625.01 | 7,323.38 | 0.28 | -0.07 | 0.037 |
| 45.00 | -28.84 | -2.70 | 0.00 | -224.94 | 0.00 | 224.94 | 6,248.70 | 3,124.35 | 13,982.56 | 7,001.67 | 0.36 | -0.08 | 0.037 |
| 46.28 | -26.86 | -2.61 | 0.00 | -221.49 | 0.00 | 221.49 | 6,218.35 | 3,109.1813, | 13,819.95 | 6,920.25 | 0.38 | -0.08 | 0.036 |
| 50.00 | -24.91 | -2.53 | 0.00 | -211.76 | 0.00 | 211.76 | 6,128.89 | 3,064.44 | 13,348.75 | 6,684.30 | 0.45 | -0.09 | 0.036 |
| 53.73 | -24.57 | -2.52 | 0.00 | -202.32 | 0.00 | 202.32 | 6,122.55 | 3,061.27 | 13,315.81 | 6,667.80 | 0.52 | -0.10 | 0.034 |
| 55.00 | -23.22 | -2.46 | 0.00 | -199.13 | 0.00 | 199.13 | 6,091.73 | 3,045.87 | 13,156.59 | 6,588.07 | 0.54 | -0.10 | 0.034 |
| 60.00 | -21.91 | -2.40 | 0.00 | -186.84 | 0.00 | 186.84 | 5,968.71 | 2,984. | 12,534. | 6,276.69 | 0.65 | -0.11 | 0.033 |
| 65.00 | -20.62 | -2.36 | 0.00 | -174.82 | 0.00 | 174.82 | 5,843.22 | 2,921. | 11,922 | 5,970.14 | . 77 | -0.12 | 0.033 |
| 70.00 | -19.38 | -2.32 | 0.0 | -163.03 | 00 | 163.03 | 5,697. | 2,848 | 11,28 | 5,650.96 | 0.90 | -0.13 | . 032 |
| 75.00 | -18.16 | -2.29 | 0.00 | -151.45 | 00 | 151.45 | 5,52 | 2,763 | 10,61 | 317.30 | . 04 | -0.14 | . 032 |
| 80.00 | -16.98 | -2.27 | 0.00 | -140.01 | 0.00 | 140.01 | 5,357 | 2,678.83 | 9,972. | 4,993.79 | 18 | -0.15 | 0.031 |
| 85.00 | -15.84 | -2.26 | 0.00 | -128.68 | 0.00 | 128.68 | 5,187.77 | 2,593.89 | 9,346.98 | 4,680.44 | 1.34 | -0.16 | 0.031 |
| 90.00 | -14.92 | -2.26 | 0.00 | -117.39 | 0.00 | 117.39 | 5,017.8 | 2,508.94 | 8,741.48 | 4,377.24 | 1.51 | -0.17 | 0.030 |
| 94.09 | -14.59 | -2.26 | 0.00 | -108.17 | 0.00 | 108.17 | 4,878 | 2,439.44 | 8,261. | 4,136.72 | 66 | -0.18 | 0.029 |
| 95.00 | -12.82 | -2.26 | 0.00 | -106.12 | 0.00 | 106.12 | 4,847.98 | 2,423.99 | 8,156.25 | 4,084.19 | 1.69 | -0.18 | 0.029 |
| 99.92 | -12.80 | -2.26 | 0.00 | -95.00 | 0.00 | 95.00 | 3,494.98 | 1,747.49 | 5,818.92 | 2,913.79 | 1.88 | -0.19 | 0.036 |
| 100.00 | -11.97 | -2.26 | 0.00 | -94.83 | 0.00 | 94.83 | 3,493.62 | 1,746.81 | 5,813.50 | 2,911.07 | 1.88 | -0.19 | 0.036 |
| 105.00 | -11.16 | -2.26 | 0.00 | -83.53 | 0.00 | 83.53 | 3,402.87 | 1,701.43 | 5,459.44 | 2,733.78 | 2.09 | -0.20 | 0.034 |
| 110.00 | -10.38 | -2.24 | 0.00 | -72.25 | 0.00 | 72.25 | 3,309.66 | 1,654.83 | 5,112.4 | 2,560.00 | 2.30 | -0.21 | 0.031 |
| 115.00 | -9.62 | -2.22 | 0.00 | -61.03 | 0.00 | 61.03 | 3,203.68 | 1,601.84 | 4,757.55 | 2,382.31 | 2.53 | -0.22 | 0.029 |
| 120.00 | -8.88 | -2.17 | 0.00 | -49.94 | 0.00 | 49.94 | 3,076.27 | 1,538.13 | 4,384.77 | 2,195.65 | 2.77 | -0.24 | 0.026 |
| 125.00 | -8.17 | -2.10 | 0.00 | -39.09 | 0.00 | 39.09 | 2,948.85 | 1,474.42 | 4,027.21 | 2,016.60 | 3.03 | -0.25 | 0.022 |
| 130.00 | -7.49 | -2.00 | 0.00 | -28.59 | 0.00 | 28.59 | 2,821.43 | 1,410.71 | 3,684.84 | 1,845.16 | 3.29 | -0.25 | 0.018 |
| 135.00 | -5.01 | -1.58 | 0.00 | -18.58 | 0.00 | 18.58 | 2,694.01 | 1,347.00 | 3,357.69 | 1,681.34 | 3.56 | -0.26 | 0.013 |
| 136.87 | -4.42 | -1.45 | 0.00 | -15.64 | 0.00 | 15.64 | 2,646.44 | 1,323.22 | 3,239.45 | 1,622.13 | 3.66 | -0.26 | 0.011 |
| 140.00 | -4.20 | -1.40 | 0.00 | -11.08 | 0.00 | 11.08 | 2,566.59 | 1,283.29 | 3,045.74 | 1,525.14 | 3.83 | -0.27 | 0.009 |
| 141.22 | -3.89 | -1.32 | 0.00 | -9.37 | 0.00 | 9.37 | 1,643.42 | 821.71 | 1,977.14 | 990.04 | 3.90 | -0.27 | 0.012 |
| 145.00 | -3.81 | -1.30 | 0.00 | -4.39 | 0.00 | 4.39 | 1,600.53 | 800.26 | 1,853.36 | 928.06 | 4.11 | -0.27 | 0.007 |
| 146.00 | -2.90 | -1.01 | 0.00 | -3.09 | 0.00 | 3.09 | 1,588.94 | 794.47 | 1,820.98 | 911.84 | 4.17 | -0.27 | 0.005 |
| 148.00 | -1.45 | -0.53 | 0.00 | -1.06 | 0.00 | 1.06 | 1,565.48 | 782.74 | 1,756.72 | 879.67 | 4.28 | -0.27 | 0.002 |
| 150.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,541.62 | 770.81 | 1,693.16 | 847.84 | 4.40 | -0.27 | 0.000 |
| 151.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1,529.54 | 764.77 | 1,661.64 | 832.05 | 4.45 | -0.27 | 0.000 |


| Site Number: 411186 | Code: ANSI/TIA-222-G | © 2007-2021 by ATC IP LLC. All rights reserved. |
| :--- | :---: | :---: | :---: |
| Site Name: West Granby, CT CT, CT | Engineering Number:13626835_C3_03 |  |
| Customer: AT\&T MOBILITY |  |  |

## Analysis Summary

| Load Case | Reactions |  |  |  |  |  | Max Usage |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Shear } \\ & \text { FX } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { Shear } \\ \text { FZ } \\ \text { (kips) } \\ \hline \end{gathered}$ | Axial FY (kips) | $\begin{aligned} & \text { Moment } \\ & \text { MX } \\ & \text { (ft-kips) } \end{aligned}$ | Moment MY (ft-kips) | $\begin{gathered} \text { Moment } \\ \text { MZ } \\ \text { (ft-kips) } \end{gathered}$ |  | teraction Ratio |
| 1.2D + 1.6W | 24.02 | 0.00 | 60.16 | 0.00 | 0.00 | 2621.68 | 0.00 | 0.27 |
| 0.9D + 1.6W | 24.01 | 0.00 | 45.12 | 0.00 | 0.00 | 2608.42 | 0.00 | 0.27 |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ | 7.80 | 0.00 | 92.48 | 0.00 | 0.00 | 836.42 | 0.00 | 0.10 |
| $(1.2+0.2$ Sds ) * DL + E ELFM | 2.96 | 0.00 | 59.64 | 0.00 | 0.00 | 329.63 | 0.00 | 0.04 |
| (1.2 + 0.2Sds) * DL + E EMAM | 3.09 | 0.00 | 59.64 | 0.00 | 0.00 | 358.43 | 0.00 | 0.04 |
| (0.9-0.2Sds) * DL + E ELFM | 2.96 | 0.00 | 41.54 | 0.00 | 0.00 | 327.76 | 0.00 | 0.04 |
| (0.9-0.2Sds) * DL + E EMAM | 3.09 | 0.00 | 41.54 | 0.00 | 0.00 | 356.23 | 0.00 | 0.04 |
| 1.0D + 1.0W | 5.59 | 0.00 | 50.14 | 0.00 | 0.00 | 608.18 | 0.00 | 0.07 |

## Base Plate \& Anchor Rod Analysis

| Pole Dimensions |  |
| :--- | :--- |
| Number of Sides | 18 |
| - |  |
| Diameter | 68 |
| in |  |
| Thickness | $1 / 2$ | in | Orientation Offset |  | ${ }^{\circ}$ |
| :--- | :--- | :--- |


| Base Reactions |  |  |
| :--- | :---: | :--- |
| Moment, Mu | $2,621.7$ | $\mathrm{k}-\mathrm{ft}$ |
| Axial, Pu | 60.2 | k |
| Shear, Vu | 24.0 | k |
| Neutral Axis | 270 | ${ }^{\circ}$ |


| Report Capacities |  |  |
| :---: | :---: | :---: |
| Component | Capacity | Result |
| Base Plate | $10 \%$ | Pass |
| Anchor Rods | $21 \%$ | Pass |
| Dwyidag | - | - |


| Base Plate |  |  |
| :--- | :---: | :--- | :--- |
| Shape | Round | - |
| Diameter, $\varnothing$ | 82 | in |
| Thickness | $31 / 4$ | in |
| Grade | A572-60 |  |
| Yield Strength, Fy | 60 | ksi |
| Tensile Strength, Fu | 75 | ksi |
| Clip | $\mathrm{N} / \mathrm{A}$ | in |
| Orientation Offset |  | $\circ$ |
| Anchor Rod Detail | d | $\mathrm{\eta}=0.5$ |
| Clear Distance | 3 | in |
| Applied Moment, Mu | 363.4 | k |
| Bending Stress, $\phi \mathrm{Mn}$ | 3505.7 | k |


| Original Anchor Rods |  |  |
| :--- | :---: | :--- |
| Arrangement | Radial | - |
| Quantity | 32 | - |
| Diameter, $\varnothing$ | $21 / 4$ | in |
| Bolt Circle | 76 | in |
| Grade | A615-75 |  |
| Yield Strength, Fy | 75 | ksi |
| Tensile Strength, Fu | 100 | ksi |
| Spacing | 7.5 | in |
| Orientation Offset |  | $\circ$ |
| Applied Force, Pu | 55.3 | k |
| Anchor Rods, $\phi$ Pn | 259.8 | k |



## Calculations for Monopole Base Plate \& Anchor Rod Analysis

Reaction Distribution

| Reaction | Shear <br> Vu | Moment <br> Mu | Factor |
| :--- | :---: | :---: | :---: |
|  | k | $\mathrm{k}-\mathrm{ft}$ | - |
| Base Forces | 24.0 | 2621.7 | 1.00 |
| Anchor Rod Forces | 24.0 | 2621.7 | 1.00 |
| Additional Bolt (Grp1) Forces |  |  |  |
| Additional Bolt (Grp2) Forces |  |  |  |
| Dywidag Forces |  |  |  |
| Stiffener Forces |  |  |  |

Geometric Properties

| Section | Gross <br> Area | Net Area | Individual <br> Inertia | Threads <br> per Inch | Moment <br> of Inertia |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Pole | 105.4913 | 5.8606 | 0.4902 |  | 60089.40 |
| Bolt | 3.9761 | 3.2477 | 0.8393 | 4.5 | 70445.09 |
| Bolt1 |  |  |  |  |  |
| Bolt2 |  |  |  |  |  |
| Dywidag | $00004 n^{2}$ |  |  |  |  |
| Stiffener |  |  |  |  |  |


| Base Plate |  |  |
| ---: | :---: | :--- |
| Shape | Round | - |
| Diameter, D | 82 | in |
| Thickness, t | 3.25 | in |
| Yield Strength, Fy | 60 | ksi |
| Tensile Strength, Fu | 75 | ksi |
| Base Plate Chord | 45.826 | in |
| Detail Type | d | - |
| Detail Factor | 0.50 | - |
| Clear Distance | 3 | - |


| Anchor Rods |  |  |
| ---: | :---: | :--- |
| Anchor Rod Quantity, N | 32 | - |
| Rod Diameter, d | 2.25 | in |
| Bolt Circle, BC | 76 | in |
| Yield Strength, Fy | 75 | ksi |
| Tensile Strength, Fu | 100 | ksi |
| Applied Axial, Pu | 55.3 | k |
| Applied Shear, Vu | 0.2 | k |
| Compressive Capacity, $\phi \mathrm{Pn}$ | 259.8 | k |
| Tensile Capacity, $\phi R n t$ | 0.213 | OK |
| Interaction Capacity | 0.215 | OK |

External Base Plate
Chord Length AA 38.784 in Additional AA 6.000 in Section Modulus, Z 118.257 in $^{3}$ Applied Moment, Mu 363.4 k-ft Bending Capacity, $\phi \mathrm{Mn} \quad 6385.9$ k-ft Capacity, $\mathrm{Mu} / \phi \mathrm{Mn} \quad 0.057$ OK

| Chord Length AB | 36.870 | in |
| ---: | :---: | :--- |
| Additional AB | 6.000 | in |
| Section Modulus, Z | 113.202 | $\mathrm{in}^{3}$ |
| Applied Moment, Mu | 277.2 | $\mathrm{k}-\mathrm{ft}$ |
| Bending Capacity, $\phi \mathrm{Mn}$ | 6112.9 | $\mathrm{k}-\mathrm{ft}$ |
| Capacity, $\mathrm{Mu} / \phi \mathrm{Mn}$ | 0.045 | OK |


| Bend Line Length | 24.585 | in |
| ---: | :---: | :--- |
| Additional Bend Line | 0.000 | in |
| Section Modulus, Z | 64.921 | $\mathrm{in}^{3}$ |
| Applied Moment, Mu | 363.4 | $\mathrm{k}-\mathrm{ft}$ |
| Bending Capacity, $\phi \mathrm{Mn}$ | 3505.7 | $\mathrm{k}-\mathrm{ft}$ |
| Capacity, $\mathrm{Mu} / \phi \mathrm{Mn}$ | 0.104 | OK |

## Internal Base Plate

Arc Length 0.000 in
Section Modulus, Z $0.000 \mathrm{in}^{3}$
Moment Arm 0.000 in
Applied Moment, Mu 0.0 k-ft
Bending Capacity, $\phi \mathrm{Mn} \quad 0.0$ k-ft
Capacity, $\mathrm{Mu} / \phi \mathrm{Mn}$

## Exhibit 4

## Antenna Mount Analysis Report



## AMERICAN TOWER ${ }^{\circ}$

CORPORATION
This report was prepared for American Tower Corporation by


## Antenna M ount Analysis Report

| ATC Site Name | : 411186 |  |
| :---: | :---: | :---: |
| ATC Site Number | : West Granby, CT |  |
| Engineering Number | : 13626835_C8_01 |  |
| Mount Elevation | 135 ft |  |
| Carrier | : AT\&T M obility |  |
| Carrier Site Name | M RCTB050155 |  |
| Carrier Site Number | CT2393S |  |
| Site Location | : 49 Upper M eadow |  |
|  | Granby, CT 06035 |  |
|  | 41.953300, -72.929800 |  |
| County | : Hartford |  |
| Date | April 1, 2021 |  |
| Max Usage | : 46\% |  |
| Result | Pass |  |
| Prepared By: <br> Pedro Lopez <br> TEP No. 68991.516108 | Reviewed By: |  |

Eng. Number 13626835_C8_01 April 1, 2021

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## Introduction

The purpose of this report is to summarize results of the antenna mount analysis performed for AT\&T Mobility at 257 ft .

## Supporting Documents

| Spec. Sheet | Spec Sheet for Sabre C10857801C |
| :--- | :--- |
| RFDS | RFDS dated March 5, 2021 |
| Photos | Site photos from 2018 |

## Analysis

This antenna mount was analyzed using RISA-3D v17 analysis software

| Basic Wind Speed: | 115 mph (3-Second Gust) |
| :--- | :--- |
| Basic Wind Speed w/ Ice: | $50 \mathrm{mph}(3-$ Second Gust) w/ 1.5-inch radial ice |
| Codes: | ANSI/TIA-222-H/ 2018 IBC |
| Risk Category: | II |
| Exposure Category: | B |
| Topographic Category: | Method 2 |
| Kzt: | 1.000 |
| Spectral Response: | Ss $=, \mathrm{S}_{1}=\left[\mathrm{s} \_1\right]$ |
| Site Class: | D - Stiff Soil |
| Live Loads: | Lm =500 lbs, Lv = 250 lbs |

## Conclusion

Based on the analysis results, the antenna mount meets the requirements per the applicable codes listed above. The mount can support the equipment as described in this report. If the load differs from that described in this report or the provisions of this analysis are found to be invalid, another structural analysis should be performed.

If you have any questions or require additional information, please contact American Tower via email at Engineering@americantower.com. Please include the American Tower site name, site number, and engineering number in the subject line for any questions.

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April 1, 2021
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## Antenna Loading

| Mount <br> Centerline <br> $(\mathrm{ft})$ | Antenna <br> Centerline <br> $(\mathrm{ft})$ | Qty | Antenna Model |
| :---: | :---: | :---: | :---: |
| 135.0 | 135.0 | 3 | CCI TPA65R-BU8D |
|  |  | 3 | CCI DMP65R-BU8D |
|  |  | 3 | Ericsson AIR 6449 B77D |
|  |  | 3 | Ericsson RRUS 4449 B5/B12 |
|  |  | 3 | Ericsson RRUS 4478 B14 |
|  |  | 3 | Ericsson RRUS 8843 B2/B66A |
|  |  |  | Raycap DC9-48-60-24-8C-EV |

## Structure Usages

| Structural Component | Controlling <br> Usage | Pass/Fail |
| :---: | :---: | :---: |
| Horizontals | $23 \%$ | Pass |
| Verticals | $24 \%$ | Pass |
| Diagonals | $14 \%$ | Pass |
| Tie-Backs | $7 \%$ | Pass |
| Mount Pipes | $46 \%$ | Pass |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MFR | Model | Qty | Shape | Member Label | Location \#1 (ft,\%) | Location \#2 (ft,\%) |
| CCI ANTENNAS | TPA65R-BU8D | 1 | Flat | MP-1 | 0.50 | 7.50 |
| Ericsson | RRUS 4478 B14 | 1 | Flat | MP-1 | 2.00 |  |
| Ericsson | AIR 6449 B77D | 1 | Flat | MP-3 | 2.00 | 4.50 |
| CCI ANTENNAS | DMP65R-BU8D | 1 | Flat | MP-4 | 0.50 | 7.50 |
| Ericsson | RRUS 4449 B5/B12 | 1 | Flat | MP-4 | 2.00 |  |
| Ericsson | RRUS 8843 B2/B66A | 1 | Flat | MP-4 | 2.00 |  |
|  |  |  |  |  |  |  |
| Raycap | DC9-48-60-24-8C-EV | 1 | Flat | SF2-TH | 1.00 |  |


| 411186-West Granby, CT |
| :--- |

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## Standard Conditions

All engineering services performed by TEP are prepared on the basis that the information used is current and correct. This information may consist of, but is not limited to the following:

- Information supplied by the client regarding antenna, mounts and feed line loading
- Information from drawings, design and analysis documents, and field notes in the possession of TEP

It is the responsibility of the client to ensure that the information provided to TEP and used in the performance of our engineering services is correct and complete.

TEP assumes that all structures were constructed in accordance with the drawings and specifications.

TEP assumes that the mount has been maintained in accordance with the manufacturer's specification.

TEP assumes that all mount components are in sufficient condition to carry their full design capacity for this analysis.

Serviceability with respect to antenna twist, tilt, roll, or lateral translation, is not checked and is left to the carrier or tower owner to ensure conformance.

All material grades used for this analysis, unless verified by mount manufacturer design, were assumed per AISC Table 2-4, $15^{\text {th }}$ Edition. See RISA 3-D output for confirmation on grades used in this analysis.

All connections are to be verified for condition and tightness by the installation contractor preceding any changes to the appurtenance mounting system and/or equipment attached to it.

Unless explicitly agreed by both the client and TEP, all services will be performed in accordance with the current revision of ANSI/TIA-222.

All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. TEP is not responsible for the conclusions, opinions and recommendations made by others based on the information supplied herein.

## Exhibit 5

NIER Study Report

## NIER Study Report

# SITE NAME: <br> 411186 West Granby CT 

LOCATION:<br>Granby, Connecticut

COMPANY:
American Tower
Woburn, Massachusetts

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## Disclaimer Notice

This work is based upon our best interpretation of available information. However, these data and their interpretation are constantly changing. Therefore, we do not warrant that any undertaking based on this report will be successful, or that others will not require further research or actions in support of this proposal or future undertaking. In the event of errors, our liability is strictly limited to replacement of this document with a corrected one. Liability for consequential damages is specifically disclaimed. Any use of this document constitutes an agreement to hold Tower Engineering Professionals and its employees harmless and indemnify it for all liability, claims, demands, and litigation expenses and attorney's fees arising out of such use.

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## NIER STUDY REPORT <br> 411186 West Granby CT <br> Granby, Connecticut

INTRODUCTION
Tower Engineering Professionals (TEP) has been retained by American Tower (ATC) of Woburn, Massachusetts to evaluate the RF emissions of an existing tower at this location.

## SITE AND FACILITY CONSIDERATIONS

Site West Granby CT is located at 49 Upper Meadow in Granby, CT at coordinates $41.953300,-72.829842$. The support structure is a $150^{\prime}$ monopole. The installation consists of two antenna levels with radiation centers of $150^{\prime} \& 135^{\prime}$ above ground level. All antennae will have a radiation center as described above. All data used in this study was provided by one or more of the following sources:

1. ATC furnished data
2. Compiled from carrier and manufacturer standard configurations
3. Empirical data collected by TEP

A topographic map of the study area is located in Appendix 1. A satellite view of the study area is located in Appendix 2.

## POWER DENSITY CALCULATIONS

Graphs of the power density at different distances from the transmitter, compared to FCC MPE general population and occupational limits, may be seen in Appendix 3. These limits are based upon the Information Relating to MPE Standards found in Appendix 5. Study methodology may be seen in Appendix 6, which describes the Non-Ionizing Radiation Prediction Models. Approximate radiation patterns may be found in Appendix 4. This site $\underline{I S}$ in compliance with FCC OET-65 MPE limits.

April 8th, 2021
Michael W. Hayden NCE CPBE CBNT AMD CPI Director, RF Design \& Services Tower Engineering Professionals


## APPENDIX 1 Topographic Map





| Maximum Power Density (@40'): | $0.0007 \mathrm{~mW} / \mathrm{cm}^{2}$ |
| ---: | :---: |
| General Population MPE (@40'): | $0.07 \%$ |
| Occupational MPE (@40'): | $0.01 \%$ |

## APPENDIX 4 Tower Radiation Patterns



## APPENDIX 5 Information Pertaining to MPE Studies

In 1985, the FCC first adopted guidelines to be used for evaluating human exposure to RF emissions. The FCC revised and updated these guidelines on August 1, 1996, as a result of a rule-making proceeding initiated in 1993. The new guidelines incorporate limits for Maximum Permissible Exposure (MPE) in terms of electric and magnetic field strength and power density for transmitters operating at frequencies between 300 kHz and 100 GHz .

The FCC's MPE limits are based on exposure limits recommended by the National Council on Radiation Protection and Measurements (NCRP) and, over a wide range of frequencies, the exposure limits were developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI) to replace the 1982 ANSI guidelines. Limits for localized absorption are based on recommendations of both ANSI/IEEE and NCRP.

The FCC's limits, and the NCRP and ANSI/IEEE limits on which they are based, are derived from exposure criteria quantified in terms of specific absorption rate (SAR). The basis for these limits is a whole-body averaged SAR threshold level of 4 watts per kilogram ( $4 \mathrm{~W} / \mathrm{kg}$ ), as averaged over the entire mass of the body, above which expert organizations have determined that potentially hazardous exposures may occur. The MPE limits are derived by incorporating safety factors that lead, in some cases, to limits that are more conservative than the limits originally adopted by the FCC in 1985. Where more conservative limits exist, they do not arise from a fundamental change in the RF safety criteria for whole-body averaged SAR, but from a precautionary desire to protect subgroups of the general population who, potentially, may be more at risk.

The FCC exposure limits are also based on data showing that the human body absorbs RF energy at some frequencies more efficiently than at others. The most restrictive limits occur in the frequency range of $30-300 \mathrm{MHz}$ where whole-body absorption of RF energy by human beings is most efficient. At other frequencies, whole-body absorption is less efficient, and consequently, the MPE limits are less restrictive.

MPE limits are defined in terms of power density (units of milliwatts per centimeter squared: $\mathrm{mW} / \mathrm{cm}^{2}$ ), electric field strength (units of volts per meter: $\mathrm{V} / \mathrm{m}$ ) and magnetic field strength (units of amperes per meter: $\mathrm{A} / \mathrm{m}$ ). The far-field of a transmitting antenna is where the electric field vector (E), the magnetic field vector ( H ), and the direction of propagation can be considered to be all mutually orthogonal ("plane-wave" conditions).

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment-related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area. Additional details can be found in FCC OET 65.

## APPENDIX 6 MPE Standards Methodology

This study predicts RF field strength and power density levels that emanate from communications system antennae. It considers all transmitter power levels (less filter and line losses) delivered to each active transmitting antenna at the communications site. Calculations are performed to determine power density and MPE levels for each antenna as well as composite levels from all antennas. The calculated levels are based on where a human (Observer) would be standing at various locations at the site. The point of interest where the MPE level is predicted is based on the height of the Observer.

Compliance with the FCC limits on RF emissions are determined by spatially averaging a person's exposure over the projected area of an adult human body, that is approximately six-feet or two-meters, as defined in the ANSI/IEEE C95.1 standard. The MPE limits are specified as time-averaged exposure limits. This means that exposure is averaged over an identifiable time interval. It is 30 minutes for the general population/uncontrolled RF environment and 6 minutes for the occupational/controlled RF environment. However, in the case of the general public, time averaging should not be applied because the general public is typically not aware of RF exposure and they do not have control of their exposure time. Therefore, it should be assumed that any RF exposure to the general public will be continuous.

The FCC's limits for exposure at different frequencies are shown in the following Tables.

| Limits for Occupational/Controlled Exposure |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Frequency Range (MHz) | Electric Field <br> Strength (E) ( $\mathrm{V} / \mathrm{m}$ ) | $\begin{aligned} & \text { Magnetic } \\ & \text { Field } \\ & \text { Strength }(\mathrm{H}) \\ & (\mathrm{A} / \mathrm{m}) \end{aligned}$ | Power <br> Density (S) <br> (mW/cm ${ }^{2}$ ) | Averaging Time $\|E\|^{2}$, $\|\mathrm{H}\|^{2}$ or $S$ (minutes) |
| 0.3-3.0 | 614 | 1.63 | 100* | 6 |
| 3.0-30 | 1842/f | 4.89/f | 900/F2 | 6 |
| 30-300 | 61.4 | 0.163 | 1.0 | 6 |
| 300-1500 | -- | -- | f/300 | 6 |
| $\begin{aligned} & 1500- \\ & 100,000 \end{aligned}$ | -- | -- | 5 | 6 |

$\mathrm{f}=$ frequency

* = Plane-wave equivalent power density

Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure.

| Limits for General Population/Uncontrolled Exposure |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Frequency Range (MHz) | Electric Field Strength (E) (V/m) | Magnetic Field Strength (H) (A/m) | $\begin{gathered} \text { Power Density } \\ \text { (S) } \\ \left(\mathrm{mW} / \mathrm{cm}^{2}\right) \end{gathered}$ | Averaging Time $\|\mathbf{E}\|^{2},\|\mathbf{H}\|^{2}$ or $\mathbf{S}$ (minutes) |
| 0.3-1.34 | 614 | 1.63 | 100* | 30 |
| 1.34-30 | 824/f | 2.19/f | 180/F2 | 30 |
| 30-300 | 27.5 | 0.073 | 0.2 | 30 |
| 300-1500 | -- | -- | f/1500 | 30 |
| 1500-100,000 | -- | -- | 1.0 | 30 |

$\mathrm{f}=$ frequency

* = Plane-wave equivalent power density

General population/uncontrolled exposures apply in situations in which the general public may be exposed or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

It is important to understand that these limits apply cumulatively to all sources of RF emissions affecting a given area. For example, if several different communications system antennas occupy a shared facility such as a tower or rooftop, then the total exposure from all systems at the facility must be within compliance of the FCC guidelines.

The field strength emanating from an antenna can be estimated based on the characteristics of an antenna radiating in free space. There are basically two field areas associated with a radiating antenna. When close to the antenna, the region is known as the Near Field. Within this region, the characteristics of the RF fields are very complex and the wave front is extremely curved. As you move further from the antenna, the wave front has less curvature and becomes planar. The wave front still has a curvature but it appears to occupy a flat plane in space (plane-wave radiation). This region is known as the Far Field.

[^1]Two models are utilized to predict Near and Far field power densities. They are based on the formulae in FCC OET 65. As this study is concerned only with Near Field calculations, we will only describe the model used for this study. For additional details, refer to FCC OET Bulletin 65.

## Cylindrical Model (Near Field Predictions)

Spatially averaged plane-wave equivalent power densities parallel to the antenna may be estimated by dividing the antenna input power by the surface area of an imaginary cylinder surrounding the length of the radiating antenna. While the actual power density will vary along the height of the antenna, the average value along its length will closely follow the relation given by the following equation:

$$
S=P \div 2 \pi R L
$$

Where:
S = Power Density
$\mathrm{P}=$ Total Power into antenna
$\mathrm{R}=$ Distance from the antenna
$\mathrm{L}=$ Antenna aperture length
For directional-type antennas, power densities can be estimated by dividing the input power by that portion of a cylindrical surface area corresponding to the angular beam width of the antenna. For example, for the case of a 120 -degree azimuthal beam width, the surface area should correspond to $1 / 3$ that of a full cylinder. This would increase the power density near the antenna by a factor of three over that for a purely omni-directional antenna. Mathematically, this can be represented by the following formula:

$$
S=\left(180 / \theta_{B W}\right) P \div \pi R L
$$

Where:
S = Power Density
$\theta_{\mathrm{BW}}=$ Beam width of antenna in degrees ( 3 dB half-power point)
$\mathrm{P}=$ Total Power into antenna
$\mathrm{R}=$ Distance from the antenna
$\mathrm{L}=$ Antenna aperture length
If the antenna is a 360-degree omni-directional antenna, this formula would be equivalent to the previous formula.

## Spherical Model (Far Field Predictions)

Spatially averaged plane-wave power densities in the Far Field of an antenna may be estimated by considering the additional factors of antenna gain and reflective waves that would contribute to exposure.

The radiation pattern of an antenna has developed in the Far Field region and the power gain needs to be considered in exposure predictions. Also, if the vertical radiation pattern of the antenna is considered, the exposure predictions would most likely be reduced significantly at ground level, resulting in a more realistic estimate of the actual exposure levels.

Additionally, to model a truly "worst case" prediction of exposure levels at or near a surface, such as at ground-level or on a rooftop, reflection off the surface of antenna radiation power can be assumed, resulting in a potential four-fold increase in power density.

These additional factors are considered and the Far Field prediction model is determined by the following equation:

$$
S=E I R P \times R c \div 4 \pi R^{2}
$$

Where:
S = Power Density
EIRP = Effective Radiated Power from antenna
$\mathrm{Rc}=$ Reflection Coefficient (2.56)
$R=$ Distance from the antenna
The EIRP includes the antenna gain. If the antenna pattern is considered, the antenna gain is relative based on the horizontal and vertical pattern gain values at that particular location in space, on a rooftop or on the ground. However, it is recommended that the antenna radiation pattern characteristics not be considered to provide a conservative "worst case" prediction. This is the equation is utilized for the Far Field exposure predictions herein.

## Exhibit 6

## Original Facility Approval

DOCKET NO. 263 - AT\&T Wireless PCS, LLC d/b/a AT\&T
Wireless application for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance and operation of two telecommunications facilities in the West Granby section of the Town of Granby, Connecticut.

December 22, 2003

## Decision and Order:

Granby Site CT-812

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a telecommunications facility including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildlife are not disproportionate either alone or cumulatively with other effects when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the proposed Site A located at 8 Upper Meadow Road, Granby, Connecticut. The Council denies certification of proposed Site B located at 10 Day Street South, Granby, Connecticut.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The tower shall be constructed no taller than necessary to provide the proposed telecommunications services, sufficient to accommodate the antennas of AT\&T and other entities, both public and private, but such tower shall not exceed a height of 150 feet above ground level.
2. The tower and facility compound shall be moved in a southerly or southeasterly direction within the lease area to minimize the area of the adjacent property to the north that is encompassed within the tower's setback radius; and the tower shall be designed with a yield point to effectively reduce the radius of said setback area.
3. The Certificate Holder shall prepare a Development and Management (D\&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of Connecticut State Agencies. The D\&M Plan shall be submitted to and approved by the Council prior to the commencement of facility construction and shall include:
a) a final site plan(s) of site development to include specifications for the tower, tower foundation, antennas, equipment building, fencing without razor wire on top, access road, utility line, and landscaping (including a screen of evergreen plantings around the facility compound); and
b) construction plans for site clearing, water drainage, and erosion and sedimentation control consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control, as amended.
4. The Certificate Holder shall, prior to the commencement of operation, provide the Council worst-case modeling of electromagnetic radio frequency power density of all proposed entities' antennas at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin No. 65, August 1997. The Certificate Holder shall ensure a recalculated report of electromagnetic radio frequency power density is submitted to the Council if and when circumstances in operation cause a change in power density above the levels calculated and provided pursuant to this Decision and Order.
5. Upon the establishment of any new State or federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
6. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
7. The Certificate Holder shall provide reasonable space on the tower for no compensation for any municipal antennas, provided such antennas are compatible with the structural integrity of the tower.
8. If the facility does not initially provide wireless services within one year of completion of construction or ceases to provide wireless services for a period of one year, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council before any such use is made.
9. Any antenna that becomes obsolete and ceases to function shall be removed within 60 days after such antennas become obsolete and cease to function.
10. Unless otherwise approved by the Council, this Decision and Order shall be void if the facility authorized herein is not operational within one year of the effective date of this Decision and Order or within one year after all appeals to this Decision and Order have been resolved.

Pursuant to General Statutes § 16-50p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in The Hartford Courant.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

Docket 263 - AT\&T
Decision \& Order: CT-812
Page 3

The parties and intervenors to this proceeding are:

## Applicant

AT\&T Wireless PCS, LLC d/b/a AT\&T Wireless

## Its Representative

Christopher B. Fisher, Esq. Cuddy \& Feder LLP
90 Maple Avenue
White Plains, New York 10601

## Exhibit 7

## (4) Notice Confirmations



$$
\begin{aligned}
& \text { IH } 15 \text { RECEIPT LISTS EACH PACKAGE RECEIUED BY THE UPS STORE \#4839 AND } \\
& \text { NDICATES THE INFORMATION FOR EACH PACKAGE HAS BEEN TRANSMITTED TO EACH } \\
& \text { ARRIER'S DATG SYSTEM. PACKAGES HITH OFFL INE LABELS HILL BE UPDATED AND } \\
& \text { SYSTEM AFTER A CONNECTION IS REESTABLISHED. THIS RECEIDT IS NOT CONFIRMATIO } \\
& \text { he carrier has picked up the package, to verify the status of a package, go } \\
& \text { CO HTTP://THEUPSSTORE, COM, SELECT TRACKING, THEN ENTER TRACKING \#. IF YOU } \\
& \text { SELECTED A NO PACKAGIMG OPTIOL FOR YOUR RETURNED ITEH. THE TRACKING \# MAY } \\
& \text { HOT PROUIDE TRACK1NG RESULTS. PLEASE CONTACI THE UENDOR'S WEBSIIE FOR MORE } \\
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& \text { ETURNPREFUND STATUS FOR UENDORS. YOU ACKHOWLEDGE THAI THE SHIPMENT SERUYCES } \\
& \text { ROUDDED BY THE UPS SIORE \#4839 FOR THE LISTED PHCKAGES ARE SUBJECT TO AND } \\
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& \text { participating locations only }
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From:
Sent:
To:
Subject:

UPS [pkginfo@ups.com](mailto:pkginfo@ups.com)
Saturday, September 4, 2021 1:35 PM
Kimberly Revak
UPS Delivery Notification, Tracking Number 1Z9Y45030335286195


Hello, your package has been delivered.
Delivery Date: Saturday,09/04/2021
Delivery Time: 1:27 PM
Left At: FRONTDOOR

## Experience UPS My Choice ${ }^{\circledR}$ Premium Today

Be in total control of how, when and where your packages are delivered.

## Upgrade to Premlum Now



## Set Delivery <br> Instructions <br> CENTERLINE SITE ACQUISITION

Manage Preferences
View My Packages

Tracking Number:

Ship To:

Number of Packages:
UPS Service:
Package Weight:
Reference Number:

## 1Z9Y45030335286195

TOWER MEADOW LLC
40 SIMSBURYROAD
WEST GRANBY, CT060901401
US
1

UPS Ground
1.0 LBS

GRANBY - LL

From:
Sent:
To:
Subject:

UPS [pkginfo@ups.com](mailto:pkginfo@ups.com)
Friday, September 3, 2021 10:38 PM
Kimberly Revak
UPS Schedule Delivery Update, Tracking Number 1Z9Y45030305448272

Your scheduled delivery date has changed.
Scheduled Delivery Date: Wednesday,09/08/2021

## Important Delivery Information

## From: <br> Tracking Number: <br> Shipment Details

CENTERLINE SITEACQUISITION
1Z9Y45030305448272

|  | Gary Waitt - Site Development <br> American Tower Corporation <br> Ship To: <br>  <br>  <br> Io Presidential Way <br> WOBURN, MA O18011053 <br> US |
| :--- | :--- |
| Number of Packages: | 1 |
| Weight: | 1.0 LBS |
| Reference Number 1: | Granby-ATC |
|  |  |

Download the UPS mobile app

From:
Sent: To: Subject:

UPS [pkginfo@ups.com](mailto:pkginfo@ups.com)
Friday, September 3, 2021 10:38 PM
Kimberly Revak
UPS Schedule Delivery Update, Tracking Number 129Y45030328912584


Your scheduled delivery date has changed.
Scheduled Delivery Date: Tuesday,09/07/2021

## Important Delivery Information

From:
Tracking Number:
Shipment Decails

Mark Lockwood - Planning \& Zoning Town of Granby Town Hall
15 North Granby Road GRANBY, CT 060352102
US
Number of Packages: 1
Weight: 1.0LBS
Reference Number 1:
Granby - Planning


Download the UPS mobile app

From:
Sent:
To:
Subject:

UPS [pkginfo@ups.com](mailto:pkginfo@ups.com)
Friday, September 3, 2021 10:38 PM
Kimberly Revak
UPS Schedule Delivery Update, Tracking Number 129Y45030337331971


Your scheduled delivery date has changed.
Scheduled Delivery Date: Tuesday, 09/07/2021

## Important Delivery Information

## From: <br> Tracking Number: <br> Shipment Details

CENTERLINE SITE ACQUISITION
1Z9Y45030337331971

Ship To:
William Smith - Town Manager
Town of Granby
Town Hall
15 North Gramby Road
GRANBY, CT 060352102
US
Number of Packages:
1
Weight:
1.0 LBS

Reference Number 1:
Granby - Town

It's the thought that counts

Download the UPS mobile app


[^0]:    *Deflection and Sway was evaluated considering a design wind speed of 60 mph (3-Second Gust) per ANSI/TIA-222-G

[^1]:    RF Design \& Services | Tower Engineering Professionals, Inc. (www.tepgroup.net) 105 W Caswell Street | Kinston, NC 28501

