

Northeast Site Solutions Denise Sabo
4 Angela's Way, Burlington CT 06013
denise@northeastsitesolutions.com
September 30, 2021

Members of the Siting Council<br>Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051<br>RE: Tower Share Application<br>63 Woodland Street, Glastonbury CT 06033<br>Latitude: 41.6608<br>Longitude: -72.5741<br>Site\#: Dish Wireless - BOBDL00104A; Vertical Bridge/Eco-Site: US-CT-5018/Hopewell

Dear Ms. Bachman:
This letter and attachments are submitted on behalf of Dish Wireless LLC. Dish Wireless LLC plans to install antennas and related equipment to the tower site located at 63 Woodland Street, Glastonbury, Connecticut.

Dish Wireless LLC proposes to install three (3) 600/19005G MHz antenna and six (6) RRUs, at the 125 -foot level of the existing 150 -foot monopole tower, one (1) Fiber cables will also be installed. Dish Wireless LLC equipment cabinets will be placed within $7 \times 5$ lease area. Included are plans by Infinigy, dated September 1, 2021 Exhibit C. Also included is a structural analysis prepared by Vertical Bridge Engineering, LLC, dated May 20, 2021, confirming that the existing tower is structurally capable of supporting the proposed equipment. Attached as Exhibit D. This facility was approved by the Connecticut Siting Council, Docket No. 478 on March 29, 2018. Please see attached Exhibit A.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies 16-50aa, of Dish Wireless LLC intent to share a telecommunications facility pursuant to R.C.S.A. 16-50j-88. In accordance with R.C.S.A., a copy of this letter is being sent to Town Manager Richard J. Johnson for the Town of Glastonbury, Rebecca Augur, Director of Planning \& Land Use Services for the Town of Glastonbury, as well as the property owner Paul J Cavanna and Vertical Bridge REIT, LLC tower owner.

The planned modifications of the facility fall squarely within those activities explicitly provided for in R.C.S.A. 16-50j-89.

1. The proposed modifications will not result in an increase in the height of the existing structure. The top of the tower is 150 -feet; Dish Wireless LLC proposed antennas will be located at a center line height of 125 -feet.
2.The proposed modification will not result in the increase of the site boundary as depicted on the attached site plan.
3.The proposed modification will not increase the noise levels at the facility by six decibels or more, or to levels that exceed local and state criteria. The incremental effect of the proposed changes will be negligent.

4.The operation of the proposed antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. As indicated in the attached power density calculations, the combined site operations will result in a total density of $16.47 \%$ as evidenced by Exhibit $F$.

Connecticut General Statutes 16-50-aa indicates that the Council must approve the shared use of a telecommunications facility provided it finds the shared use is technically, legally, environmentally, and economically feasible and meets public safety concerns. As demonstrated in this letter, Dish Wireless LLC respectfully indicates that the shared use of this facility satisfies these criteria.
A. Technical Feasibility. The existing monopole has been deemed structurally capable of supporting Dish Wireless LLC proposed loading. The structural analysis is included in Exhibit D.
B. Legal Feasibility. As referenced above, C.G.S. 16-50aa has been authorized to issue orders approving the shared use of an existing tower such as this support tower in Manchester. Under the authority granted to the Council, an order of the Council approving the requested shared use would permit Dish Wireless LLC to obtain a building permit for the proposed installation. Further, a letter of Authorization is included as Exhibit G, authorizing Dish Wireless LLC to file this application for shared use.
C. Environmental Feasibility. The proposed shared use of this facility would have a minimal environmental impact. The installation of Dish Wireless LLC equipment at the 125 -foot level of the existing 150 -foot tower would have an insignificant visual impact on the area around the tower. Dish Wireless LLC ground equipment would be installed within the existing facility compound. Dish Wireless LLC shared use would therefore not cause any significant alteration in the physical or environmental characteristics of the existing site. Additionally, as evidenced by Exhibit $F$, the proposed antennas would not increase radio frequency emissions to a level at or above the Federal Communications Commission safety standard.
D. Economic Feasibility. Dish Wireless LLC will be entering into an agreement with the owner of this facility to mutually agreeable terms. As previously mentioned, the Letter of Authorization has been provided by the owner to assist Dish Wireless LLC with this tower share application.
E. Public Safety Concerns. As discussed above, the tower is structurally capable of supporting Dish Wireless LLC proposed loading. Dish Wireless LLC is not aware of any public safety concerns relative to the proposed sharing of the existing tower. Dish Wireless LLC intentions of providing new and improved wireless service through the shared use of this facility is expected to enhance the safety and welfare of local residents and individuals traveling through Manchester.

Sincerely,

## Denise sabo

## Denise Sabo

Mobile: 203-435-3640
Fax: 413-521-0558
Office: Angela's Way, Burlington CT 06013
Email: denise@northeastsitesolutions.com


Attachments
Cc: Town Manager, Richard J. Johnson
Town of Glastonbury
$2^{\text {nd }}$ FLoor
2155 Main Street Glastonbury CT 06073

Rebecca Augur, Director of Planning \& Land Use Services
Town of Glastonbury
$3^{\text {rd }}$ Floor
2155 Main Street Glastonbury CT 06073

Paul J Cavanna
80 Woodland Street
S Glastonbury CT 06073

Vertical Bridge, REIT, LLC, Tower Owner
750 Park of Commerce Drive, Suite 200
Boca Raton, FL 33487

## Exhibit A

## Original Facility Approval

DOCKET NO. 478 - Eco-Site, Inc. and T-Mobile Northeast, LLC application for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a telecommunications facility located at 63 Woodland Street, Glastonbury, Connecticut.
\} \}

Connecticut
Siting
Council
March 29, 2018

## Decision and Order

Pursuant to Connecticut General Statutes $\$ 16-50$ p, and the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, maintenance, and operation of a telecommunications facility, including effects on the natural environment, ecological balance, public health and safety, scenic, historic, and recreational values, agriculture, forests and parks, air and water purity, and fish, aquaculture and wildlife are not disproportionate, either alone or cumulatively with other effects, when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application, and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes $\mathbb{S} 16-50 \mathrm{k}$, be issued to Eco-Site, Inc., hereinafter referred to as the Certificate Holder, for a telecommunications facility at 63 Woodland Street, Glastonbury, Connecticut.

Unless otherwise approved by the Council, the facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The tower shall be constructed either as a monopine or monopole at a height of 150 feet above ground level (excluding faux monopine branches) to provide the proposed wireless services, sufficient to accommodate the antennas of T-Mobile Northeast, LLC, the Town of Glastonbury, and other entities, both public and private. The height of the tower may be extended after the date of this Decision and Order pursuant to regulations of the Federal Communications Commission. Prior to submission of the Development and Management Plan to the Council, the Certificate Holder shall consult with the Town of Glastonbury in regards to the Town's emergency communication equipment needs and the appropriateness of a monopine design based on those needs. The final tower design, either a monopole or monopine, shall be determined after this consultation.
2. The Certificate Holder shall prepare a Development and Management (D\&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of Connecticut State Agencies. The D\&M Plan shall be served on the Town of Glastonbury for comment, and all parties and intervenors as listed in the service list, and submitted to and approved by the Council prior to the commencement of facility construction and shall include:
a) final site plan(s) for development of the facility that employ the governing standard in the State of Connecticut for tower design in accordance with the currently adopted International Building Code and include specifications for the tower, tower foundation, antennas, and equipment compound including, but not limited to, fencing, radio equipment, access road, utility line, and emergency backup power source;
b) construction plans for site clearing, grading, utility installation, water drainage and stormwater control, and erosion and sedimentation controls consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control, as amended;
c) schedule for deployment of T-Mobile Northeast LLC's, and the Town of Glastonbury's equipment; and
d) hours of construction.
3. Prior to the commencement of operation, the Certificate Holder shall provide the Council worst-case modeling of the electromagnetic radio frequency power density of all proposed entities' antennas at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin No. 65, August 1997. The Certificate Holder shall ensure a recalculated report of the electromagnetic radio frequency power density be submitted to the Council if and when circumstances in operation cause a change in power density above the levels calculated and provided pursuant to this Decision and Order.
4. Upon the establishment of any new federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
5. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
6. Unless otherwise approved by the Council, if the facility authorized herein is not fully constructed with at least one fully operational wireless telecommunications carrier providing wireless service within eighteen months from the date of the mailing of the Council's Findings of Fact, Opinion, and Decision and Order (collectively called "Final Decision"), this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council before any such use is made. The time between the filing and resolution of any appeals of the Council's Final Decision shall not be counted in calculating this deadline. Authority to monitor and modify this schedule, as necessary, is delegated to the Executive Director. The Certificate Holder shall provide written notice to the Executive Director of any schedule changes as soon as is practicable.
7. Any request for extension of the time period referred to in Condition 6 shall be filed with the Council not later than 60 days prior to the expiration date of this Certificate and shall be served on all parties and intervenors, as listed in the service list, and the Town of Glastonbury.
8. If the facility ceases to provide wireless services for a period of one year, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council within 90 days from the one year period of cessation of service. The Certificate Holder may submit a written request to the Council for an extension of the 90 day period not later than 60 days prior to the expiration of the 90 day period.
9. Any nonfunctioning antenna, and associated antenna mounting equipment, on this facility shall be removed within 60 days of the date the antenna ceased to function.
10. In accordance with Section 16-50j-77 of the Regulations of Connecticut State Agencies, the Certificate Holder shall provide the Council with written notice two weeks prior to the commencement of site construction activities. In addition, the Certificate Holder shall provide the Council with written notice of the completion of site construction, and the commencement of site operation.
11. The Certificate Holder shall remit timely payments associated with annual assessments and invoices submitted by the Council for expenses attributable to the facility under Conn. Gen. Stat. $\$ 16-50 \mathrm{v}$.
12. This Certificate may be transferred in accordance with Conn. Gen. Stat. $\S 16-50 \mathrm{k}(\mathrm{b})$, provided both the Certificate Holder/transferor and the transferee are current with payments to the Council for their respective annual assessments and invoices under Conn. Gen. Stat. §16-50v. In addition, both the Certificate Holder/transferor and the transferee shall provide the Council a written agreement as to the entity responsible for any quarterly assessment charges under Conn. Gen. Stat. $\$ 16-50 \mathrm{v}(\mathrm{b})(2)$ that may be associated with this facility.
13. The Certificate Holder shall maintain the facility and associated equipment, including but not limited to, the tower, tower foundation, antennas, equipment compound, radio equipment, access road, and utility line in a reasonable physical and operational condition that is consistent with this Decision and Order and a Development and Management Plan to be approved by the Council.
14. If the Certificate Holder is a wholly-owned subsidiary of a corporation or other entity and is sold/transferred to another corporation or other entity, the Council shall be notified of such sale and/or transfer and of any change in contact information for the individual or representative responsible for management and operations of the Certificate Holder within 30 days of the sale and/or transfer.
15. This Certificate may be surrendered by the Certificate Holder upon written notification and approval by the Council.

We hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed in the Service List, dated October 26, 2017, and notice of issuance published in the Hartford Courant.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

## Exhibit B

## Property Card




| Building Intormation |  |  |  | Building ID | 1451 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Year Constructed : 1800 |  | Number of Rooms : | 7 |  |  |
| Building Type : | Residential | Number of Bedrooms : | 04 |  |  |
| Style : | Century+ | Number of Bathrooms : | 1 |  |  |
| Occupany : | Single Family | Number of Half-Baths : | 0 |  |  |
| Stories: | 2 | Exterior Wall : | Vinyl |  |  |
| Building Zone: | RR | Interior Wall : | Drywall |  |  |
| Roof Type : | Gable | Interior Floor: | Carpet |  |  |
| Roof Material : | Asphalt Shingl | Interior Floor \#2 : | No entry |  |  |
| Est. Gross S.F. : | 2614 | Air Conditioning Type : | None |  |  |
| Est. Living S.F. : | 1628 | Heat Type : | Hot Water |  |  |
|  |  | Fuel Type : | Oil |  |  |




1C

| Subarea Type | Est. Gross S.F. | Est. Living S.F. | Outbuilding Type | Est. Gross S.F. | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| First Floor | 814 | 814 | Barn 1story | 375.00 |  |
| Porch, Enclosed | 32 | 0 | Barn 1story | 960.00 |  |
| Porch, Open | 140 | 0 | Barn 1story | 4000.00 |  |
| Upper Story, Finished | 814 | 814 | Barn w/Loft | 1250.00 |  |
| Slab | 264 | 0 | Lean-to | 864.00 |  |
| Basement | 550 | 0 | Patio-Concrete | 66.00 |  |
| First Floor | 762 | 762 | Shed-Wood/Comp | 117.00 |  |

[^0]| GIS TOWn of Glastonbury GIS Parcel Report | Report Generated | $9 / 28 / 20219: 50: 38 \mathrm{Am}$ |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Porch, Open | 25 | 0 | Shed-Wood/Comp | 48.00 |
| Basement | 762 | 0 | Shed-Wood/Comp | 176.00 |
| First Floor | 1514 | 1514 | Shed-Wood/Comp | 192.00 |
| Attic, Unfinished | 1514 | 0 | Wood Deck | 192.00 |
| Basement | 1514 | 0 |  |  |

This data \& map is a user generated static output from an Internet mapping site and is for reference only. Data that appears on this form may or may not be accurate, current, or otherwise reliable. Any questions on the data provided above should be directed to the Town of Glastonbury Property Assessment Office 860-652-7600.


## Exhibit C

## Construction Drawings

















5701 SOUTH SANTA FE DRVE
LITLEOON, CO 80120
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INFINIGYZ


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CONSTRUCTION


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2039-Z5555C

BOBDLO0104A
63 WOODLAND ST
GLASTONBURY, CT 06073 GLASTONBURY, CT 06073

SHEET TTTL
RFinging
plumbing diagram
SHEET NUMEER

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## ITE ACTIVTY REQUIREMENTS:

NOTICE TO PROCEED - NO WORK SHALL COMMENCE PRIOR TO CONTRACTOR RECEING A WRITTEN NOTICE TO PROCEED (NTP) AND THE ISSUANCE OF A PURCHASE ORDER. PRRRR TO ACCESSING/ENTERING THE SITE YOU MUST CONTACT THE
WRELESS, LLC. AND TOWER OWNER NOC \& THE DISH WIRELESS, LCI AND TOWER OWNER CONSTRUCTION MANAGER.
2. "LOoK UP" - DISH WIRELESS, LlC. AND TOWER OWNER SAFETY CLIMB REQUIREMENT

THE INTEGRIT OF THE SAFETY CLIMB AND ALL COMPONENTS OF THE CLMBING FACIUTY SHALL BE CONSIDERED DURING ALL STAGES
OF DESIGN, INSTALATION, AND INSPECTION. TOWER MODFICATION, MOUNT REINFORCEMENTS, AND/OR EQUPMENT INSTALATIONS SHM OF DESIGN, INSTALATION, AND INSPECTION. TOWER MODIFICATION, MOUNT REEINORCEMENTS, AND/OR EQUIPMENT INSTALAATIONS SHAL
NOT COMPROMISE THE INTEGRITY OR FUNCTONAL USE OF THE SAEETY CLIMB OR ANY COMPONENTS OF THE CLIMBING FACUIU ON



3. PRIOR TO THE START OF CONSTRUCTION, ALL REOURED JURISOICTIONAL PERMITS SHALL BE OBTAINED. THIS INCLUDES, BUT
IS NOT LIMTED TO, BULING, ELECTRICAL, MECHANLCAL, FIRE, FLOOD ZONE, ENVIRONMENTAL, AND ZONING. ATTER ONSIE ACTVIIIES



 PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION) AND DISH WIRELESS, LLC. AND TOWER OWNER STANDARDS, INCLUDING
THE REQUIRED INVOLVEMENT OF A QUALIFED ENGINEER FOR CLASS IV CONSTRUCTION, TO CERTIFY THE SUPPORTING STRUCTURE(S) iN THE REQUIRED INVOLVEMENT OF A QUALIFED ENGINE
ACCORDANCE WTH ANSITTA-322 (LATEST EDTION).
5. ALL STE WORK TO COMPLY WTH DISH WIRELESS, LlC. AND TOWER OWNER INSTALLATON STANDARDS FOR CONSTRUCTION
ACTVIIES ON DISH WIRELESS, LLC. AND TOWER OWNER TOWER SITE AND LATEST VERSION OF ANSI/TIA-1019-A-2012 STTANDARD


 AND ORDINANCES. CONTRACTOR SHALL ISSUE AL APPROPRATE NOTICES AND COMPLY WITH ALL LALSS, OROINANCES, REULLLSS.
REGULTIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED


9. THE CONTRACTOR SHALL CONTACT UTLITY LOCATING SERVICES INCLUDING PRVATE LOCATES SERVICES PRIOR TO THE START
OF CONSTRUCTION.

 FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING AND EXCAVATION E) CONSTRUCTION SAFETY
11 ALL SITE WORK SHALL
LATEST APPROVED REVIION.
12. CONTRACTOR SHALL KEEP THE STEE FREE FROM ACCUMULTING WASTE MATERIAL, DEBRIS, AND TRASH AT THE COMPLETION OF
TTE WORK IF NCESARY, RUBEISH, STUMPS, DEBRIS, STCKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
13. AL EXISTING INACTVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTLLTIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHAL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WTH
THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF DISH WIRELESS, LLC. AND TOWER OWNER, AND/OR LOCAL UTLITES. 14. THE CONTRACTOR SHALL PROVIDE STEE SIIGNAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIGNAGE
REQURED BY LOCAL JURISDICTON AND SIGNAGE REQURED ON INDIIDUAL PIECES OF EQUIPMENT, ROOMS, AND SHELTERS.
15. THE STtE SHALL be graded to Cause surface water to flow away from the carrier's equipment and tower areas. Th. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE
APPLICATION. 17. THE AREAS OF THE OWNERS PROPERT DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUPMENT OR
DRVVWA, SALL BE GALDE TO A UNIFORM LLOPE, AND STABILZED TO PREVENT EROSION AS SPECIFED ON THE CONSTRUCTON DRAWINGS AND/OR PRONECT SPECIFICATIONS.
 19. THE CONTRACTOR SHALL PROTECC EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY 20. CONTRACTOR SHALL LEGALY AND PROCERIY EXPENSE TO THE SATISFACTION OF OWNER COXIAL CABLES AND OTHER TEES 20. CONTRACTOR SHALL LEGALLY AND PRORERLY DISPOSE OF ALL SCRAP MATERIALL SUCH AS COXXIAL CABLES AND OTH
REMOVED FROM THE EXASTING FACLLITY. ANTENNAS AND RADIOS REMOVED SHALL EE RETURNED TO THE OWNER'S DESIGNATED
LOCATION.
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21. Contractor shall leave premises in clean condition. trash and debris should be removed from site on a dally
basis 22. NO FIL OR EMBANKMENT MATERAL SHALL be placed on frozen ground. Frozen materials, snow or ice shall not
BE PLACED in ANY FIL OR EMBANKMENT.

## general notes

1.FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY CONTRACTOR:GENERAL CONTRACTOR RESPONSIBLE FOR CONSTRUCTION
CARRIER:DISH WIRELESS, LLC.
TOWER OWNER:TOWER OWNER
2. THESE DRAWINGS HAVE BEEN PREPARED USING STANDARDS OF PROFESSIONAL CARE AND COMPLETENESS NORMALYY
EXERCISED UNDER SIMILAR CIRCUMSTANCES BY REPUTABLE ENGINERS IN THIS OR SIMLAR LOCALIIES. IT IS ASSUMED THAT TH
 OF THE ATM
CONDITON OR ELEMENT IS (OR CAN BE) EXPLCITTLY SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL USE INOUSTRY ACCEPTED CONDITION OR ELEMENT IS (OR CAN BE EXPLCITYY SHOWN ON TTESE DRAWING
STANDARD GOOD PRACTICE FOR MISELLAEOUS WORK NOT EXPLICILY SHOWN.


 STEE VSTIS BY THE ENGINEER OR HIS REPRESENTA
OBSERVATION OF THE FINSHED STRUCTURE ONLY.

| NOTTS AND DETALLS IN THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TTPICAL DETALLS |
| :--- |

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GREATER,
RECORD.
5. SUBSTANTAL EFFORT HAS BEEN MADE TO PROVIDE ACCURATE DIMENSIONS AND MEASUREMENTS ON THE DRAWINGS TO ASSIST
IN THE FABRICATION AND/OR PLACEMENT OF CONSTRUCTION ELEMENTS BUT IT IS THE SOLE RESPONSIBLITY OF THE CONTRACTOR TO
 FABRRCATION OR CUTING OF ANY NEW OR EXIISTNG CONSTRUCTION ELEMENTS. IF IT IS DETERMINED THAT THERE ARE
DISRERPANCIES AND/OR CONFLLCTS WTH THE CONSTRUCTION DRAWINGS THE ENGINEER OF RECORD IS TO BE NOTFIED AS SOON AS
POSSIBLE.
 7. AL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLCABLE CODES, REGLATIONS
AND OROINANESS. CONTRACTOR SHALL ISSUE ALL APPROPRATE NOTICES AND COMPLY WTHH ALL LAWS, ORDINANCES, RULES,
 REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORIT REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED
OUT SHAL COOPLY WTH AL APLCALE MUNCIPAL AND UTLITY COMPANY SPECIFCATIONS AND LOCAL UURISICTIONAL CODES,
ORDINANCES AND APLLCABLE REGULATIONS.
8. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MAT
NECESSARY TO COMPLETE ALL INSTALATONS AS INDICATED ON THE DRAWINGS.
9. THL CIESS SPECIFICALALY STATED OTHERTISE.
 11. CONTRACTOR IS TO PERFORM A SITE INVESTIGATION, BEEORE SUBMTTING BIDS, TO DETERMINE THE BEST ROUTING of ALL
CONOTS FOR POWER, AND TELCO AND FOR GROUNDING CABLES AS SHOWN IN THE POWER, TELCO, AND GROUNING PLAN DRAWINGS.

HE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY REPAIRED AT CONTRACTOR'S EXPENSE TO THE 13. CONTRACTOR SHAL LEGALY AND PROPERLY DISPOSE OF ALL SCRAP MATERRALS SUCH AS COAAIAL CABLES AND OTHER ITEMS
REMOVED FROM THE EXISTING FACLITTY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNEP'S DESGNTED 14.
basis.
CONtractor shall leave premises in clean condition. trash and debris should be removed from site on a dally


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| :---: | <br>  <br>  <br> RFDS REV \#: N/A

CONSTRUCTION DOCUMENTS


AKE PROJECT NUMB

63 WOODLAND ST
SHEET TTLLE
general notes

## ations. And reinforcing steel

1. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WTH THE ACI 301, ACI 318, ACI 336, ASTM A184, ASTM A185 AND THE DESIGN
AND CONSTRUCTON SPECIFCATION FOR CAST-IN-PLACE CONCRETE.
2. UNLESS NOTED OTHERWISE, SOIL BEARING PRESSURE USED FOR DESIGN OF SLABS AND FOUNDATIONS IS ASSUMED TO bE 1000
psf.
3. ALL CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH (f'c) OF 3000 psi AT 28 DAYS, UNLESS NOTED OTHERWISE. NO
MORE THAN 90 MINTES SHALL ELAPSE FROM BATCH TIME TO TIME OF PLACEMENT UNLESS APPROVED BY THE ENGINEER OF FRCCOD. MORE THAN 90 MINTES SHALL ELLPSE FROM BATCH TIME TO TIME OF PLACEN
TEMPERATURE OF CONCRETE SHALL NOT EXCEED $90^{\prime}$ AT TIME OF PLACEMENT.
4. CONCRETE EXPOSED TO FREEZE-THAW CYCLES SHALL CONTAN AR ENTRANING ADMIXTURES. AMOUNT OF AR ENTRANMENT TO BE
BASED ON SIZ OF AGGREGATE AND FF CLASS EXPOSURE (VERY SEVERE) CEMENT USED TO BE TPE BASED ON SIZE OF AGGREGATE AND F3 CLASS EXPOSURE (VERY SEVERE). CEMENT USED TO BE TPPE II PORTLAND CEMENT WITH
5. all steel reinforcing shall conform to astm a615. all welded wire fabric (wwf) shall conform to astm alibs. SPLICES SHALL BE CLASS "B" TENSION SPLICES, UNLESS NOTED OTHERWISE. ALL HOOKS SHALL BE STANDARD 90 DEGREE HOOKS,
SPLLCES SHALL BE CLASS "B" TENSION SPLCEES, UNLESS NOTED OTHERWISE. ALL HOOKS SHALL BE
UNLESS NOTED OTHERWISE. YELD STRENGTH (Fy) OF STANDARD DEFORMED BARS ARE AS FOLLOWS:
\#4 BARS AND SMALLER 40 ks
\#5 bars and larger 60 ksi
${ }^{6 .} \stackrel{\text { THE }}{\text { DRAWINGS: }}$
LOLING MINMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON

- concrete cast against and permanently exposed to earth $3^{\prime \prime}$
- CONCRETE EXPOSED TO EARTH OR WEATHER:
- \#g bars and larger $\mathbf{2}^{\prime \prime}$
- \#5 bars and smaller 1-1/2"
- concrete not exposed to earth or weather:
- slab and walls $3 / 4^{-}$
beams and columns $1-1 / 2^{\prime \prime}$

7. A tooled edee or a $3 / 4^{\prime \prime}$ chamfer shall be provided at all exposed edges of concrete, unless noted otherwise,

## Electrical instalation notes:

1. ALL ELECTTICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIIICATIONS, NEC AND ALL APPLCABLE
2. CONDUIT ROUTINGS ARE SCHEMATC. CONTRACTOR SHALL INSTALL CONDUTS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED
3. WIRING, RACEWAY AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE NEC.
4. all circuits shall be segregated and maintain minimum cable separation as required by the nec.
4.1. ALL EQUIPMENT SHALL BEAR THE UNDERWRTERS LABORATORIES LABEL OF APPROVAL, AND SHALL CONFORM TO REQUIREMENT OF
THE NATIONAL ELLCTRICAL COOE.
 CURRENT TO WHICH THEY ARE SUBJECTED, 22,OOO ALC MNMUM. VERIFY AVALLABLE SHORT CIRCUIT CURRENT DDES NOT EXCEED TH
RATING OF ELECTRICL EQUPMENT IN ACCORDANE WTTH ARTCLE 110.24 NEC OR THE MOST CURRNT ADOPTED CODE PRE THE COVERNING JURISDICTION.
5. EACH END OF EVERY POWER PHASE CONDUCTOR, GROUNDING CONDUCTOR, AND TELCO CONDUCTOR OR CABLE SHALL BE LABELED WTH COLOR-CODED INSULATION OR ELLCCTRICAL TAPE ( (3M BRAND,
EQUAL). THE IDENTFICATION METHOD SHALL CONFORM WTH NEC AND OSHA.
6. ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABELED WITH LAMICOID TAGS SHOWING THEIR RATED VOLTAGE, PHASE
CONFIGURATIN, WIRE CONFIGURATON, POWER OR AMPACIY RATNG AND BRANCH CIRUIT ID (D's).
panel boards (id numbers) shall be clearly labeled with plastic labels.
7. TIE WRAPS ARE Not allowed.
8. AL POWER AND EQUIPMENT GROUND WIRRG IN TUBING OR CONDUIT SHALL BE SIIGGLE COPPER CONDUCTOR (\#14 OR LARGER)
WITH TPPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATION UNLESS OTHERWISE SPECIFIED. SUPPLEMENTAL EQUIPMENT GROUND WIRING LOCATED INDOORS SHALL BE SIIGGLE COPPER CONOUCTOR (\#G OR LARGER) WTTH
TOPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATON UNLESS OTHERWISE PPECIFED. 11. POWER AND CONTROL WIRING IN FLEXIBLE CORD SHALL be MULTI-CONDUCTOR, TYPE SOOW CORD (\#14 OR LARGER) UNLESS 11. P POWER AND
OTHERWISE SPECFIFED.
 13. ALP POWER AND GROUNDING CONNECTIONS SHALL BE CRIMP-STILE, COMPRESSION WRE LUGS AND WRE NUTS BY THOMAS AND
BETTS (OR EQUAL). LUGS AND WIRE NUTS SHALL BE RATED FOR OPERATION NOT LESS THAN $75^{\circ} \mathrm{C}$ ( $90^{\circ} \mathrm{C}$ IF AVAIIABLE).
9. raceway and cable tray shall be listed or labeled for electrical use in accordance with nema, ul, ansi/ieee and NEC. 15. ELECTRICAL METALLIC TUBING (EMT), INTERMEDIATE METAL CONDUTT (IMC), OR RIGID METAL CONDUIT (RMC) SHALL BE USED FOR
EXPOSED INDOOR LOCATIONS.
10. SCHEDULE 40 PVC UNDERGROUND ON STRAIGHTS AND SCHEDULE 80 PVC FOR ALL ELBOWS/90s AND ALL APPROVED ABOVE
GRADE PVC CONDUIT. 18. LIQUD-TIGHT FLEXIBLE METALLIC CONDUIT (LIQUID-TTTE FLEX) SHALL BE USED INDOORS AND OUTDOORS, WHERE VBRATION
OCCURS OR FLEXIBLITY IS NEEDED. 19. CONDUUT AND TUBING FFITINGS SHALL BE THREADED OR COMPRESSION-TPPE AND APPROVED FOR THE LOCATION USED. SET
SCREW FITINGS ARE NOT ACEPTABLE. 20. Cabinets, boxes and wire wars shall be labeled for electrical use in accordance with nema, ul, ansi/ieee and the
11. WIREWAYS SHALL BE METAL WITH AN ENAMEL FINISH AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARD (WIREMOLD SPECMATE WIREWAY).
12. SLOTtED WiRIng duct shall be pvc and include cover (panduit tppe e or equal).
13. CONDUTS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED STRAPS AND HANGERS. EXPLOSVE
DEVICES (i.e. POWDER-ACTUATED) FOR ATACHING HANGERS TO STRUCTURE WIL NOT BE PERMITED. CLOSELY FOLLOW THE LINES DEVICES (i.e. POWDER-ACTUATED) FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITED. CLOSELY FOLLOW THE LINES O
THE STRUCTURE, MANTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUTTS IN TIGHT ENVELOPES CHANGES IN DIPECTON



14. EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES AND PULL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET
STEEL. SHALL MEET OR EXCEED UL 50 AND BE RATED NEMA 1 (OR BETER) FOR INTERIOR LOCATONS AND NEMA 3 (OR BETER) FOR SETEELL SHALL MEET OR
EXTERIOR LOCATIONS.
15. METAL RECEPTACLE, SWITCH AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED OR NON-CORRODING; SHALL MEET OR
EXCEED UL $514 A$ AND NEMA OS 1 AND BE RATED NEMA 1 (OR BETER) FOR INTERIOR LOCATIONS AND WEATHER PROTECTED (WP OR EXCEED UL 514 AA AND NEMA OS
BETER) FOR EXTERIOR LOCATIONS.
16. NONMETALLIC RECEPTACLE, SWITCH AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2 (NEWEST REVISION) AND BE RATED ITIR) FOR INTERIOR LOCATIONS AND WEATHER PROTECTED (WP OR BETER) FOR EXTERIOR LOCATIONS.
THE CONTRACTOR SHALL NOTIIY AND OBTAIN NECESSAAY AUTHORIZATION FROM THE CARRIER AND/OR DISH WIRELESS, LLC. AND
TOWER OWNER BEFORE COMANCING WORK ON THE AC PWER DISTRBUITIN PANEIS
${ }^{28}$ 28. THE CONTRACTOR SHALL PROVIDE NECESSARY TAGGING ON THE RREAKERS, CABLES AND DISTRIBUTION PANELS IN ACCORDANCE BREAERERT,
PROPRT.
17. Install lamicoid label on the meter center to show "oish wireless, llc."
18. all empty/SPare conduits that are installed are to have a metered mule tape pull cord installed.

5701 SOUTH SANTA FE DRVE
LTTLEEON, CO 80120

## (((虫))


INFINIGY\&
from zero to infinigy
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| :---: | :---: | :---: |
|  <br> Ni |  |  |
|  |  |  |
| RCD | ss | CJW |

## GROUNDING NOTES

1．ALL GROUND ELECTRODE SYSTEMS（INCLUDING TELECOMMUNICATION，RADIO，LIGHTNING PROTECTION AND AC POWER GES＇S）SHALL
BE BONDED TOGETHER AT OR BELOW GRADE，BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WTH THE NEC．
THE CONTRACTOR SHALL PERFORM IEEE FALL－OF－POTENTAL RESISTANCE TO EARTT TESTING（PER IEEE 1100 AND 81）FOR GROUND ELLCTRODE SYSTEMS．THE CONTRACTO
ACHIVVE A TEST RESULT OF 5 OHMS OR LESS．
3．THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO
PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT AND PROVIDE TESTING RESULTS．
4．METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY
BONDING ACROSS THE DISCONTINUITY WTH \＃
5．METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR．STRANDED COPPER CONDUCTORS
WTH GEEN INSULTION，SIZED IN ACCORDANCE WTH THE NEC，SHALL BE FURNISHED AND INSTALED WTH THE POWER CIRCUTS TO BTS
EQUPMENT
6．EACH CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL
EQUPMENT GROUND WRES，\＃6 STRANDED COPPER OR LARGER FOR INDOOR BTS；\＃2 BARE SOLI TINED COPPER FOR OUTDOOR BTS，
7．CONNECTIONS TOTHE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED BACK TO BACK CONNECTIONS ON OPPOSITE SIDE
OF THE GROUND BUS ARE PERMITED．
dictors between equpment／ground baps and the ground ping shal be \＃2 soud tined
9．ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS．
10．USE of $90^{\circ}$ bends in the protection grounding conductors shall be avoided when $45^{\circ}$ bend can be adequately
11．EXOTHERMIC WELDS SHALL be USED FOR ALL GROUNDING CONNECTIONS below grade．
12．ALL GROUND CONNECTIONS ABOVE GRADE（INTERIOR AND EXTERIOR）SHALL BE FORMED USING HIGH PRESS CRIMPS．
13．COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC WELD CONNECTIONS．
14.
BAR．

15．APPROVED ANTIOXIDANT COATINGS（i．e．CONDUCTVE GEL OR PASTE）SHALL bE USED ON ALL COMPRESSION AND BOLTED GROUND
CONNECTIONS．
16．ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERALL
17．MISCELLANEOUS ELECTRICAL AND NON－ELECTRICAL METAL BOXES，FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND
18．BOND ALL METALLIC OBJECTS WTHIN 6 ft OF MAIN GROUND RING WTH（1）\＃2 BARE SOLID TINNED COPPER GROUND
COND
19．GROUND CONDUCTORS USED FOR THE FACILITY GROUNDING AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED
THROUGH MEIALIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR，SUCH AS METALLC CONOUTS，METAL SUPPORT CLPS


20．ALL GROUNDS THAT TRANSTION FROM BELOW GRADE TO ABOVE GRADE MUST BE \＃2 BARE SOLID TINNED COPPER IN $3 / 4^{\prime \prime}$ NON－METALLLC，FLEXIBLE CONDUTT FROM $24^{4 \prime}$ BELOW GRADE TO WTTHIN $3^{\prime \prime}$ TO $6^{\prime \prime \prime}$ OF CAD－WELD TERMINATION POINT．THE EXPOSED END Of The CONDUT MUST be sealed with silicone caulk．（add transitioning ground standard detall as well）．
BULILINGS WHERE THE MAIN GROUNING CONDCTORS ARE REQURED TO BE ROUTED TO GRADE，THE CONTRACTOR SHALL ROUTE
TWO GROUNDING CONDUCTORS FROM THE ROOFTOP，TOWERS，AND WATER TOWERS GROUNDING RING，TO THE EXISTING GROUNDING NS GROUNDING CONDUCTORS FROM THE ROOFTOP，TOWERS，AND WATER TOWERS GROUNDING RING，TO THE EXISTING GROUNDING
SYSTEM，THE GROUNOING CONDCTORS SHALL NOT BE SMALLER THAN $2 / 0$ COPPER．ROOTOO GROUNOING RING SHALL BE BONDED TO THE EXISTNG GROUNDING SYSTEM，THE BULLDING STEEL COLUMNS，LIGHTNING PROTECTION SYSTEM，AND BUULDING MAIN WATER LINE （FERROUS OR NONFERROUS METAL PIPING ONLY）．DO NOT ATACH GROUNOING TO FIRE SPRINKLER SYSTEM PIPES，

5701 SOUTH SANTA FE DRVE
LTTLETON，CO 80120

## Exhibit D

## Structural Analysis Report

# DISH Wireless LLC 

## Structural Analysis Report



VERTICAL BRIDGE ENGINEERING, LLC

## Table of Contents

Introduction ..... 1
Existing Structural Information ..... 1
Final Proposed Equipment Loading for DISH Wireless ..... 1
Design Criteria ..... 2
Analysis Results ..... 2
Assumptions ..... 2
Conclusions ..... 3
Standard Conditions ..... 4
Disclaimer of Warranties ..... 4
Calculations ..... Attached
Collocation Application ..... Attached

## Introduction

We have completed our structural analysis of the proposed equipment installation on the foregoing tower to determine its ability to support the new loads proposed by DISH Wireless. The objective of the analysis was to determine if the tower meets the current structural codes and standards with the proposed equipment installation.

## Existing Structural Information

The following documents for the existing structure were made available for our structural analysis.

| Tower Information | Ehresmann Engineering, Inc., Job No. 102800, dated 12/17/2018 |
| :--- | :--- |
| Foundation Information | Ehresmann Engineering, Inc., Job No. 102800, dated 12/17/2018 |
| Geotechnical Information | FDH Velocitel., Project No. 18PGJC1600, dated 04/10/2018 |
| Existing Equipment Information | Vertical Bridge Collocation Application Version 2. |
| Tower Reinforcement Information | Tower has not been previously reinforced. |

## Final Proposed Equipment Loading for DISH Wireless

The following proposed loading was obtained from the Vertical Bridge Collocation Application:

| Antenna/Equipment |  |  |  |  | Coax |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount <br> (ft) | RAD $(\mathrm{ft})$ | Qty. | Antenna | Type | Qty. | Size/Type |
| 125.0 | - | 1 | Platform with Handrails | Mount | 1 | 1.6" Hybrid |
|  | 125.0 | 6 | Fujitsu TA08025-B605 | RRU |  |  |
|  |  | 3 | JMA MX08FRO665-20_V0F | Panel |  |  |
|  |  | 1 | Raycap RDIDC-9181-PF-48 | DC Box |  |  |

[^1]
## Design Criteria

The tower was analyzed using tnxTower (Version 8.0.9.0) tower analysis software using the following design criteria.

| State | Connecticut |
| :--- | :---: |
| City/County Building Code | Hartford County (IBC 2018) |
| TIA/EIA Standard Code | TIA-222-H |
| Basic Wind Speed | 119 MPH (Vult) |
| Basic Wind Speed w/ Ice | $50 \mathrm{MPH} \mathrm{w} / 1.50 "$ Ice |
| Steel Grade | 65 ksi Pole $/ 50 \mathrm{ksi}$ Base Plate / |
|  | A615-75 Anchor Bolts |
| Exposure Category | C |
| Topographic Category (height) | $1(0.0 \mathrm{ft})$ |
| Risk Category | II |
| $\mathbf{S}_{\mathbf{s}}$ | 0.202 |
| Seismic Design Category | B |

## Analysis Results

Based on the foregoing information, our structural analysis determined that the existing tower is structurally capable of supporting the proposed equipment loads without modification. The existing tower base plate, anchor rods, and foundation have also been evaluated and were found to be structurally capable of supporting the proposed equipment loads. A seismic analysis has been performed on this tower and does not control.

## Assumptions

The below assumptions are true, complete, and accurate.

1. The existing tower has been maintained to manufacturer's specifications and is in good condition.
2. Foundations are considered to have been properly designed for the original design loads.
3. All member connections are considered to have been designed to meet the load carrying capacity of the connected member.
4. Antenna mount loads have been estimated based on generally accepted industry standards.
5. The mounts for the proposed antennas have been analyzed and designed by others.
6. See additional assumptions contained in the report attached.
7. Tower is within acceptable engineering tolerance at $105 \%$.
8. Foundations are within acceptable engineering tolerance at $110 \%$.

## Conclusions

The existing tower described above has sufficient capacity to support the proposed loading based on the governing Building Code. The existing tower base plate, anchor rods, and foundation have also been evaluated and are acceptable. A seismic analysis has been performed on this tower and does not control.

We appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance, please call us anytime at 561-948-6367.

Sincerely,
Analysis by:
Reviewed by:


05/20/2021

Gertha Wesh
Design Engineer II

Michael T. De Boer, P.E.
Vice President of Structural Engineering

## Standard Conditions

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but not necessarily limited, to:

- Information supplied by the client regarding the structure itself, the antenna and transmission line loading on the structure and its components, or relevant information.
- Information from drawings in possession of Vertical Bridge Engineering, LLC, or generated by field inspections or measurements of the structure.

It is the responsibility of the client to ensure that the information provided to Vertical Bridge Engineering, LLC and used in the performance of our engineering services is correct and complete. In the absence of information contrary, we consider that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated; and we, therefore consider that their capacity has not significantly changed from the original design condition.
All services will be performed to the codes and standards specified by the client, and we do not imply to meet any other code and standard requirements unless explicitly agreed to in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes and standards, the client shall specify the exact requirements. In the absence of information to the contrary, all work will be performed in accordance with the revision of ANSI/TIA/EIA-222-H requested.

All services are performed, results obtained, and recommendations made in accordance with the generally accepted engineering principles and practices. Vertical Bridge Engineering LLC, is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

## Disclaimer of Warranties

The engineering services by Vertical Bridge Engineering, LLC in connection with this Structural Analysis are limited to a computer analysis of the tower structure, size, and capacity of its members. Vertical Bridge Engineering, LLC does not analyze the fabrication, including welding, except as may be expressly included in this report.

The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines. Any mention of structural modifications are reasonable estimates and should not be used a precise construction document. Precise modification drawings are obtainable from Vertical Bridge Engineering, LLC but are beyond the scope of this report.

Vertical Bridge Engineering, LLC makes no warranties, express or implied, in connection with this report and disclaims any liability arising from material, fabrication and erection of this tower, or installation and compliance with legal and permitting requirements of the proposed equipment. Vertical Bridge Engineering, LLC will not be responsible whatsoever for or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Vertical Bridge Engineering, LLC pursuant to this report will be limited to the total fee received for preparation of this report.

## Attachment 1: <br> Calculations

150.0 ft
DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| AIR32 KRD901146-1_B66A-B2A w/ Mount Pipe | 150 | SM 602-1 (ATT-E) | 136 |
|  |  | SM 602-1 (ATT-E) | 136 |
| AIR32 KRD901146-1_B66A-B2A w/ Mount Pipe | 150 | SM 602-1 (ATT-E) | 136 |
| AIR32 KRD901146-1_B66A-B2A w/ Mount Pipe | 150 | 1/3 Remaining Reserved Rights (ATT R) | 136 |
|  |  | 1/3 Remaining Reserved Rights (ATT -R) | 136 |
| LNX-6515DS-A1M | 150 | 1/3 Remaining Reserved Rights (ATT(-R) | 136 |
| LNX-6515DS-A1M | 150 |  |  |
| APX16DWV-16DWV-S-E-A20 w/ Mount Pipe | 150 | (2) TPA65R-BU8D w/ Mount Pipe (ATT-E) | 136 |
| APX16DWV-16DWV-S-E-A20 w/ Mount Pipe | 150 | (2) TPA65R-BU8D w/ Mount Pipe (ATT-E) | 136 |
| APX16DWV-16DWV-S-E-A20 w/ Mount Pipe | 150 | (2) TPA65R-BU8D w/ Mount Pipe (ATT-E) | 136 |
| RRUS 11 B12 | 150 | HPA65R-BU8A w/Mount Pipe (ATT-E) | 136 |
| RRUS 11 B12 | 150 | HPA65R-BU8A w/Mount Pipe (ATT-E) | 136 |
| RRUS 11 B12 | 150 | HPA65R-BU8A w/Mount Pipe (ATT-E) | 136 |
| RRUS 11 B4 | 150 | 4478 B14 RRUS(18.1×13.4×8.3×59.4lbs) (ATT-E) | 136 |
| RRUS 11 B4 | 150 |  |  |
| RRUS 11 B4 | 150 | 4478 B14 RRUS(18.1×13.4×8.3x59.4lbs) (ATT-E) | 136 |
| IBR-1300 | 150 |  |  |
| SM 602-1 | 150 | $8^{\prime} \times 2^{\prime \prime}$ STD Pipe Mount (Dish Wireless P) | 125 |
| SM 602-1 | 150 | $8^{\prime} \times 2$ " STD Pipe Mount (Dish Wireless P) | 125 |
| SM 602-1 | 150 |  |  |
| 1/3 Remaining Reserved Rights (TMO -R) | 150 | 8'x2" STD Pipe Mount (Dish Wireless - P) | 125 |
| 1/3 Remaining Reserved Rights (TMO - R) | 150 | 1/3 Remaining Reserved Rights (Dish Wireless - R) | 125 |
| 1/3 Remaining Reserved Rights (TMO $-R)$ | 150 | 1/3 Remaining Reserved Rights (Dish Wireless - R) | 125 |
| 4478 B14 RRUS (18.1 $13.4 \times 8.3 \times 59.4 \mathrm{lbs})$ (ATT-E) | 136 | 1/3 Remaining Reserved Rights (Dish Wireless - R) | 125 |
| E2-700 (ATT-E) | 136 | Platfrom w/Handrails (LP 716) (Dish Wireless - P) | 125 |
| E2-700 (ATT-E) | 136 |  |  |
| E2-700 (ATT-E) | 136 | MX08FRO665-20_V0F w/ Mount Pipe (Dish Wireless - P) | 125 |
| Radio 4415 B30 | 136 |  |  |
| (16.5 $\times 13.4 \times 5.9 \times 46 \mathrm{lbs}$ ) (ATT-E) |  | MX08FRO665-20_V0F w/ Mount Pipe (Dish Wireless - P) | 125 |
| Radio 4415 B30 | 136 |  |  |
| (16.5x13.4×5.9x46lbs) (ATT-E) |  | MX08FRO665-20_V0F w/ Mount Pipe (Dish Wireless - P) | 125 |
| Radio 4415 B30 | 136 |  |  |
| (16.5x13.4×5.9x46lbs) (ATT-E) |  | (2) TA08025-B605 <br> (14.96x15.75x9.06x751bs) (Dish <br> Wireless - P) | 125 |
| $\begin{aligned} & \text { Radio } 4449 \text { ( } 15.0 \times 13.2 \times 9.3 \times 74 \mathrm{lbs}) \\ & \text { (ATT-E) } \end{aligned}$ | 136 |  |  |
| Radio 4449 (15.0×13.2x9.3x74lbs) <br> (ATT-E) | 136 | (2) TA08025-B605 <br> (14.96x15.75x9.06x75lbs) (Dish <br> Wireless - P) | 125 |
| Radio 4449 (15.0×13.2×9.3×74Ibs) (ATT-E) | 136 | (2) TA08025-B605$(14.96 \times 15.75 \times 9.06 \times 75 \mathrm{bs})$ (DishWireless - P) | 125 |
| 8843 (15x13.2×11.1×75Ibs) (ATT-E) | 136 |  |  |
| 8843 ( $15 \times 13.2 \times 11.1 \times 75 \mathrm{lbs}$ ) (ATT-E) | 136 | RDIDC-9181-PF-48 (Dish Wireless P) | 125 |
| 8843 ( $15 \times 13.2 \times 11.1 \times 75 \mathrm{lbs}$ ) (ATT-E) | 136 |  |  |
| Unknown DC (ATT-E) | 136 |  |  |
| Unknown DC (ATT-E) | 136 |  |  |
| Unknown DC (ATT-E) | 136 |  |  |


| ALL REACTIO ARE FACTOR | MATERIAL STRENGTH |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | GRADE | Fy | Fu | GRADE | Fy | Fu |
| AXIAL | A572-65 | 65 ksi | 80 ksi |  |  |  |
| 85 K |  |  |  |  |  |  |
| TOWER DESIGN NOTES |  |  |  |  |  |  |
| SHEAR $11 \mathrm{~K}$ | 1. Tower is <br> 2. Tower <br> 3. Tower | located in signed for signed for | County, Co re C to the mph basic w | ut. <br> -H Standa cordance |  |  |

TORQUE 0 kir 4 . Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to increase 50 mph WIND - 1.50 in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.

| AXIAL | 6. Tower Risk Category II. |
| :---: | :--- |
| 50 K | 7. Topographic Category 1 with Crest Height of 0.000 ft |
| 8. TOWER RATING: $69.5 \%$ |  |



TORQUE 0 kip-ft
REACTIONS - 119 mph WIND

| Vertical Bridge Engineering, LLC |
| ---: |
| 750 Park of Commerce Drive, Suite 200 |

Boca Raton, FL 33487
Phone: 561-948-6367

US-CT-5018
Project: Monopole Structural Analysis

| Cl |
| :--- |
| C |
| C |
| P |


| Client: DISH | Drawn by: GWesh | App'd: |
| :---: | :---: | :---: |
| de: TIA-222-H | Date: 05/20/21 | ale: NTS |
|  |  |  |


| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 Boca Raton, FL 33487 Phone: 561-948-6367 FAX: | Job | US-CT-5018 | $\begin{array}{ll} \hline \text { Page } & \\ & 1 \text { of } 19 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{aligned} & \text { Date } \\ & \text { 10:10:22 05/20/21 } \end{aligned}$ |
|  | Client | DISH | Designed by GWesh |

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:
Tower is located in Hartford County, Connecticut.
Tower base elevation above sea level: 310.000 ft .
Basic wind speed of 119 mph .
Risk Category II.
Exposure Category C.
Simplified Topographic Factor Procedure for wind speed-up calculations is used.
Topographic Category: 1.
Crest Height: 0.000 ft .
Nominal ice thickness of 1.5000 in.
Ice thickness is considered to increase with height.
Ice density of 56.000 pcf .
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50.000^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals Use Moment Magnification
$\sqrt{ }$ Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity
$\sqrt{ }$ Leg Bolts Are At Top Of Section
$\sqrt{ }$ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided)
$\sqrt{ }$ SR Members Have Cut Ends SR Members Are Concentric

Distribute Leg Loads As Uniform Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r
$\sqrt{ }$ Retension Guys To Initial Tension Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
$\sqrt{ }$ Autocalc Torque Arm Areas Add IBC .6D+W Combination
$\sqrt{ }$ Sort Capacity Reports By Component
$\sqrt{ }$ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

[^2]| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 FAX: | Job | US-CT-5018 | Page <br> 2 of 19 |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{aligned} & \text { Date } \\ & \text { 10:10:22 05/20/21 } \end{aligned}$ |
|  | Client | DISH | Designed by GWesh |

$\left.\begin{array}{cccccccccc}\hline \text { Section } & \text { Elevation } & \begin{array}{c}\text { Section } \\ \text { Length } \\ f t\end{array} & \begin{array}{c}\text { Splice } \\ \text { Length } \\ f t\end{array} & \begin{array}{c}\text { Number } \\ \text { of } \\ \text { Sides }\end{array} & \begin{array}{c}\text { Top } \\ \text { Diameter } \\ \text { in }\end{array} & \begin{array}{c}\text { Bottom } \\ \text { Diameter } \\ \text { in }\end{array} & \begin{array}{c}\text { Wall } \\ \text { Thickness } \\ \text { in }\end{array} & \begin{array}{c}\text { Bend } \\ \text { Radius }\end{array} \\ \text { Lt } & \text { ft } & \text { ft }\end{array} \begin{array}{c}\text { Pole Grade }\end{array}\right]$

## Tapered Pole Properties

| Section | Tip Dia. <br> in | Area <br> in $^{2}$ | $I$ <br> $i n^{4}$ | $r$ <br> in | $C$ <br> in | $I / C$ <br> $i n^{3}$ | $J$ <br> $i n^{4}$ | $I t / Q$ <br> $i n^{2}$ | $w$ <br> in |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 26.7672 | 24.8524 | 2138.8836 | 9.2655 | 13.4112 | 159.4849 | 4280.5816 | 12.4286 | 4.1888 |  |
|  | 40.1708 | 37.4215 | 7302.0244 | 13.9515 | 20.1168 | 362.9814 | 14613.6569 | 18.7143 | 6.5120 | 13.963 |
| L2 | 39.5698 | 47.1631 | 8222.6286 | 13.1875 | 19.0744 | 431.0823 | 16456.0768 | 23.5860 | 5.9396 | 14.849 |
|  | 48.9865 | 60.8138 | 17628.3191 | 17.0045 | 24.5364 | 718.4558 | 35279.8341 | 30.4127 | 7.8320 | 19.58 |
| L3 | 48.1435 | 57.4775 | 14883.2580 | 16.0716 | 23.2015 | 641.4794 | 29786.0998 | 28.7442 | 7.2639 | 18.16 |
|  | 57.1006 | 70.9706 | 28018.1714 | 19.8445 | 28.6004 | 979.6426 | 56073.2098 | 35.4921 | 9.1344 | 22.836 |
| L4 | 56.2721 | 67.3238 | 23917.1577 | 18.8248 | 27.1412 | 881.2120 | 47865.7861 | 33.6683 | 8.6289 | 21.572 |
|  | 64.9194 | 80.7466 | 41264.4167 | 22.5780 | 32.5120 | 1269.2057 | 82583.1303 | 40.3810 | 10.4896 | 26.224 |


| Tower Elevation <br> ft | Gusset Area (perface) $f t^{2}$ | Gusset Thickness in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. <br> Factor <br> $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 |  |  |  | 1 | 1 | 1 |  |  |  |
| 150.000-100.0 |  |  |  |  |  |  |  |  |  |
| 00 |  |  |  |  |  |  |  |  |  |
| L2 |  |  |  | 1 | 1 | 1 |  |  |  |
| 100.000-65.50 |  |  |  |  |  |  |  |  |  |
| 0 |  |  |  |  |  |  |  |  |  |
| L3 |  |  |  | 1 | 1 | 1 |  |  |  |
| 65.500-32.300 |  |  |  |  |  |  |  |  |  |
| L4 |  |  |  | 1 | 1 | 1 |  |  |  |
| 32.300-0.000 |  |  |  |  |  |  |  |  |  |

Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> $f t$ | Total Number | Number Per Row | Clear Spacing in | Width or Diameter in | Perimeter <br> in | Weight <br> $k l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| *** |  |  |  |  |  |  |  |  |  |  |  |


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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |


| Description | Face or Leg | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement <br> $f t$ | Total Number |  | $\begin{gathered} C_{A} A_{A} \\ f t^{2} / f t \end{gathered}$ | Weight <br> klf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} * * * \\ \text { 1.6" Hybrid } \\ (\text { Dish - P) } \end{gathered}$ | C | No | No | Inside Pole | 125.000-0.000 | 1 | No Ice <br> 1/2" Ice <br> 1" Ice <br> 2" Ice | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ |
| $\begin{gathered} * * * \\ 5 / 8^{\prime \prime} \text { DC } \\ \text { (ATT-E) } \end{gathered}$ | C | No | No | Inside Pole | 136.000-0.000 | 6 | No Ice <br> 1/2" Ice <br> 1" Ice <br> 2" Ice | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ |
| 3/8" Fiber Cables (ATT-E) | C | No | No | Inside Pole | 136.000-0.000 | 2 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ | $\begin{aligned} & 0.001 \\ & 0.001 \\ & 0.001 \\ & 0.001 \end{aligned}$ |
| 6X12 Hybrid (TMO-E) | C | No | No | Inside Pole | 150.000-0.000 | 3 | No Ice <br> 1/2" Ice <br> 1" Ice <br> 2" Ice | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ | $\begin{aligned} & 0.000 \\ & 0.000 \\ & 0.000 \\ & 0.000 \end{aligned}$ |

## Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower \\
Section
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $C_{A} A_{A}$ Out Face $f t^{2}$ \& Weight
K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{150.000-100.000} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.154 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{100.000-65.500} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.145 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{65.500-32.300} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.139 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{32.300-0.000} \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.136 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation \(f t\) \& \begin{tabular}{l}
Face or \\
Leg
\end{tabular} \& Ice Thickness in \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $C_{A} A_{A}$ Out Face $f t^{2}$ \& Weight
K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{150.000-100.000} \& A \& \multirow[t]{3}{*}{1.712} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.154 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{100.000-65.500} \& A \& \multirow[t]{3}{*}{1.644} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.145 <br>
\hline L3 \& 65.500-32.300 \& A \& 1.560 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.000 <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date <br> 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |


| Tower <br> Section | Tower <br> Elevation <br> $f t$ | Face <br> or | Ice <br> Thickness | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face | $C_{A} A_{A}$ <br> Out Face | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | Leg | in | $f t^{2}$ | $f t^{2}$ | $f t^{2}$ | $f t^{2}$ | K |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| L4 |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.139 |
|  | $32.300-0.000$ | A | 1.397 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.136 |

## Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ | $C P_{Z}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Ice | Ice |  |
|  | $f t$ | in | in | in | in |
| L1 | $150.000-100.000$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L2 | $100.000-65.500$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L3 | $65.500-32.300$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L4 | $32.300-0.000$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight <br>

\hline \multicolumn{10}{|l|}{***} <br>

\hline \multirow[t]{4}{*}{$$
\begin{gathered}
\text { LP } 716 \\
\text { (Dish Wireless - P) }
\end{gathered}
$$} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 26.800 \& 26.800 \& 1.509 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 32.200 \& 32.200 \& 1.811 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 37.600 \& 37.600 \& 2.113 <br>
\hline \& \& \& \& \& \& 2" Ice \& 48.400 \& 48.400 \& 2.717 <br>
\hline \multirow[t]{4}{*}{MX08FRO665-20_V0F w/ Mount Pipe (Dish Wireless - P)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 12.964 \& 7.767 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.668 \& 9.053 \& 0.178 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.340 \& 10.191 \& 0.282 <br>
\hline \& \& \& \& \& \& 2" Ice \& 15.618 \& 12.139 \& 0.519 <br>
\hline \multirow[t]{4}{*}{MX08FRO665-20 V0F w/ Mount Pipe (Dish Wireless - P)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 12.964 \& 7.767 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.668 \& 9.053 \& 0.178 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.340 \& 10.191 \& 0.282 <br>
\hline \& \& \& \& \& \& 2" Ice \& 15.618 \& 12.139 \& 0.519 <br>
\hline \multirow[t]{4}{*}{MX08FRO665-20_V0F w/ Mount Pipe (Dish Wireless - P)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 12.964 \& 7.767 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 13.668 \& 9.053 \& 0.178 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 14.340 \& 10.191 \& 0.282 <br>
\hline \& \& \& \& \& \& 2" Ice \& 15.618 \& 12.139 \& 0.519 <br>
\hline (2) TA08025-B605 \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 1.964 \& 1.129 \& 0.075 <br>
\hline (14.96x15.75x9.06x75lbs) \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.138 \& 1.267 \& 0.093 <br>
\hline \multirow[t]{2}{*}{(Dish Wireless - P)} \& \& \& 0.000 \& \& \& $1{ }^{1 \prime}$ Ice \& 2.320 \& 1.411 \& 0.114 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.705 \& 1.723 \& 0.164 <br>
\hline (2) TA08025-B605 \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Leg} \& 3.000 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{125.000} \& No Ice \& 1.964 \& 1.129 \& 0.075 <br>
\hline (14.96x15.75x9.06x75lbs) \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.138 \& 1.267 \& 0.093 <br>
\hline (Dish Wireless - P) \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.320 \& 1.411 \& 0.114 <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date $10: 10: 22 \text { 05/20/21 }$ |
|  | Client | DISH | Designed by GWesh |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
-
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight <br>

\hline \multirow{5}{*}{(2) TA08025-B605 (14.96x15.75x9.06x75lbs) (Dish Wireless - P)} \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& 2" Ice \& 2.705 \& 1.723 \& 0.164 <br>
\hline \& \& \& 3.000 \& \& \& No Ice \& 1.964 \& 1.129 \& 0.075 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.138 \& 1.267 \& 0.093 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.320 \& 1.411 \& 0.114 <br>
\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& 2" Ice \& 2.705 \& 1.723 \& 0.164 <br>

\hline \multirow[t]{4}{*}{| RDIDC-9181-PF-48 |
| :--- |
| (Dish Wireless - P) |} \& \& \& 3.000 \& \& \& No Ice \& 2.561 \& 1.342 \& 0.022 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.760 \& 1.498 \& 0.043 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 2.967 \& 1.662 \& 0.067 <br>
\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& 2" Ice \& 3.402 \& 2.012 \& 0.125 <br>
\hline \multirow[t]{4}{*}{8'x2" STD Pipe Mount (Dish Wireless - P)} \& \& \& 3.000 \& \& \& No Ice \& 1.900 \& 1.900 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.728 \& 2.728 \& 0.044 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.401 \& 3.401 \& 0.063 <br>
\hline \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& $2^{\prime \prime}$ Ice \& 4.396 \& 4.396 \& 0.119 <br>
\hline \multirow[t]{4}{*}{8'x2" STD Pipe Mount (Dish Wireless - P)} \& \& \& 3.000 \& \& \& No Ice \& 1.900 \& 1.900 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.728 \& 2.728 \& 0.044 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.401 \& 3.401 \& 0.063 <br>
\hline \& \multirow{4}{*}{C} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& 2" Ice \& 4.396 \& 4.396 \& 0.119 <br>
\hline \multirow[t]{4}{*}{8'x2" STD Pipe Mount (Dish Wireless - P)} \& \& \& 3.000 \& \& \& No Ice \& 1.900 \& 1.900 \& 0.029 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.728 \& 2.728 \& 0.044 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 3.401 \& 3.401 \& 0.063 <br>
\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{125.000} \& 2" Ice \& 4.396 \& 4.396 \& 0.119 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (Dish Wireless - R)} \& \& \& 3.000 \& \& \& No Ice \& 5.885 \& 5.885 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 6.905 \& 6.905 \& 0.094 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.925 \& 7.925 \& 0.126 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{125.000} \& 2 " Ice \& 9.965 \& 9.965 \& 0.188 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (Dish Wireless - R)} \& \multirow[t]{4}{*}{B} \& \& 3.000 \& \& \& No Ice \& 5.885 \& 5.885 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 6.905 \& 6.905 \& 0.094 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 7.925 \& 7.925 \& 0.126 <br>
\hline \& \& \& \& \& \& 2" Ice \& 9.965 \& 9.965 \& 0.188 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (Dish Wireless - R)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 5.885 \& 5.885 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 6.905 \& 6.905 \& 0.094 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.925 \& 7.925 \& 0.126 <br>
\hline \& \& \& \& \& \& 2" Ice \& 9.965 \& 9.965 \& 0.188 <br>
\hline *** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{4}{*}{(2) TPA65R-BU8D w/ Mount Pipe (ATT-E)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{136.000} \& No Ice \& 18.089 \& 10.100 \& 0.112 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 18.722 \& 11.522 \& 0.232 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{1 \prime}$ Ice \& 19.362 \& 12.796 \& 0.362 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 20.662 \& 15.017 \& 0.658 <br>
\hline \multirow[t]{4}{*}{(2) TPA65R-BU8D w/ Mount Pipe (ATT-E)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{136.000} \& No Ice \& 18.089 \& 10.100 \& 0.112 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 18.722 \& 11.522 \& 0.232 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 19.362 \& 12.796 \& 0.362 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 20.662 \& 15.017 \& 0.658 <br>
\hline \multirow[t]{4}{*}{(2) TPA65R-BU8D w/ Mount Pipe (ATT-E)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 4.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{136.000} \& No Ice \& 18.089 \& 10.100 \& 0.112 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 18.722 \& 11.522 \& 0.232 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 19.362 \& 12.796 \& 0.362 <br>
\hline \& \& \& \& \& \& 2" Ice \& 20.662 \& 15.017 \& 0.658 <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& \text { HPA65R-BU8A w/Mount } \\
& \text { Pipe } \\
& \text { (ATT-E) }
\end{aligned}
$$} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 0.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{136.000} \& No Ice \& 18.564 \& 10.575 \& 0.094 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 19.402 \& 12.197 \& 0.219 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 20.251 \& 13.843 \& 0.355 <br>
\hline \& \& \& \& \& \& 2" Ice \& 21.844 \& 16.531 \& 0.665 <br>

\hline \multirow[t]{4}{*}{$$
\begin{gathered}
\text { HPA65R-BU8A w/Mount } \\
\text { Pipe } \\
\text { (ATT-E) }
\end{gathered}
$$} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 0.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{136.000} \& No Ice \& 18.564 \& 10.575 \& 0.094 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 19.402 \& 12.197 \& 0.219 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 20.251 \& 13.843 \& 0.355 <br>
\hline \& \& \& \& \& \& 2" Ice \& 21.844 \& 16.531 \& 0.665 <br>
\hline \multirow[t]{3}{*}{HPA65R-BU8A w/Mount Pipe (ATT-E)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 0.000 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{136.000} \& No Ice \& 18.564 \& 10.575 \& 0.094 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 19.402 \& 12.197 \& 0.219 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 20.251 \& 13.843 \& 0.355 <br>
\hline
\end{tabular}

| tnxTower <br> Vertical Bridge Engineering, <br> LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 <br> FAX: | Job | US-CT-5018 | $\begin{array}{ll} \hline \text { Page } & \\ & 6 \text { of } 19 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |


| Description | Face or Leg | Offset <br> Type |  | Azimuth Adjustment <br> 0 | Placement $f t$ |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight <br> K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 4478 \text { B14 RRUS } \\ (18.1 \times 13.4 \times 8.3 \times 59.4 \mathrm{lbs}) \\ \text { (ATT-E) } \end{gathered}$ | A | From Leg |  | 0.0000 | 136.000 | 2" Ice | 21.844 | 16.531 | 0.665 |
|  |  |  | 3.000 |  |  | No Ice | 2.021 | 1.252 | 0.059 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 2.200 | 1.402 | 0.077 |
|  |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 2.386 | 1.560 | 0.097 |
|  |  | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 2.780 | 1.898 | 0.147 |
| 4478 B14 RRUS | B |  | 3.000 |  |  | No Ice | 2.021 | 1.252 | 0.059 |
| (18.1x13.4x8.3x59.4lbs) |  |  | 0.000 |  |  | 1/2" Ice | 2.200 | 1.402 | 0.077 |
| (ATT-E) |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 2.386 | 1.560 | 0.097 |
|  | C | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 2.780 | 1.898 | 0.147 |
| 4478 B14 RRUS |  |  | 3.000 |  |  | No Ice | 2.021 | 1.252 | 0.059 |
| (18.1x13.4x8.3x59.4lbs) |  |  | 0.000 |  |  | 1/2" Ice | 2.200 | 1.402 | 0.077 |
| (ATT-E) |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 2.386 | 1.560 | 0.097 |
|  | A | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 2.780 | 1.898 | 0.147 |
| $\begin{gathered} \text { E2-700 } \\ \text { (ATT-E) } \end{gathered}$ |  |  | 3.000 |  |  | No Ice | 3.083 | 1.243 | 0.052 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 3.301 | 1.392 | 0.075 |
|  |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 3.526 | 1.553 | 0.101 |
|  | B | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 3.998 | 1.901 | 0.163 |
| E2-700 |  |  | 3.000 |  |  | No Ice | 3.083 | 1.243 | 0.052 |
| (ATT-E) |  |  | 0.000 |  |  | 1/2" Ice | 3.301 | 1.392 | 0.075 |
|  |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 3.526 | 1.553 | 0.101 |
| $\begin{gathered} \text { E2-700 } \\ \text { (ATT-E) } \end{gathered}$ | C | From Leg |  | 0.0000 | 136.000 | $2^{\prime \prime}$ Ice | 3.998 | 1.901 | 0.163 |
|  |  |  | 3.000 |  |  | No Ice | 3.083 | 1.243 | 0.052 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 3.301 | 1.392 | 0.075 |
|  |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 3.526 | 1.553 | 0.101 |
| $\begin{gathered} \text { Radio } 4415 \mathrm{~B} 30 \\ (16.5 \times 13.4 \times 5.9 \times 46 \mathrm{lbs}) \\ (\text { ATT-E) } \end{gathered}$ | A | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 3.998 | 1.901 | 0.163 |
|  |  |  | 3.000 |  |  | No Ice | 0.000 | 0.000 | 0.000 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 0.000 | 0.000 | 0.000 |
|  |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 0.000 | 0.000 | 0.000 |
|  | B | From Leg |  | 0.0000 | 136.000 | 2 " Ice | 0.000 | 0.000 | 0.000 |
| Radio 4415 B30 |  |  | 3.000 |  |  | No Ice | 0.000 | 0.000 | 0.000 |
| (16.5x13.4x5.9x46lbs) |  |  | 0.000 |  |  | 1/2" Ice | 0.000 | 0.000 | 0.000 |
| (ATT-E) |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 0.000 | 0.000 | 0.000 |
|  | C | From Leg |  | 0.0000 | 136.000 | 2 " Ice | 0.000 | 0.000 | 0.000 |
| Radio 4415 B30 |  |  | 3.000 |  |  | No Ice | 0.000 | 0.000 | 0.000 |
| (16.5x13.4x5.9x46lbs) |  |  | 0.000 |  |  | 1/2" Ice | 0.000 | 0.000 | 0.000 |
| (ATT-E) |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 0.000 | 0.000 | 0.000 |
|  | A | From Leg |  | 0.0000 | 136.000 | $2{ }^{\prime \prime}$ Ice | 0.000 | 0.000 | 0.000 |
| Radio 4449 |  |  | 3.000 |  |  | No Ice | 1.650 | 1.163 | 0.074 |
| (15.0x13.2×9.3×74lbs) |  |  | 0.000 |  |  | 1/2" Ice | 1.810 | 1.301 | 0.090 |
| (ATT-E) |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 1.978 | 1.447 | 0.109 |
| $\begin{gathered} \text { Radio } 4449 \\ (15.0 \times 13.2 \times 9.3 \times 74 \mathrm{lbs}) \\ \text { (ATT-E) } \end{gathered}$ | B | From Leg |  | 0.0000 | 136.000 | 2 " Ice | 2.336 | 1.762 | 0.155 |
|  |  |  |  |  |  | No Ice | 1.650 | 1.163 | 0.074 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 1.810 | 1.301 | 0.090 |
|  |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 1.978 | 1.447 | 0.109 |
|  | C | From Leg |  | 0.0000 | 136.000 | 2 " Ice | 2.336 | 1.762 | 0.155 |
| $\begin{gathered} \text { Radio } 4449 \\ (15.0 \times 13.2 \times 9.3 \times 74 \mathrm{lbs}) \\ \text { (ATT-E) } \end{gathered}$ |  |  | 3.000 |  |  | No Ice | 1.650 | 1.163 | 0.074 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 1.810 | 1.301 | 0.090 |
|  |  |  | 0.000 |  |  | 1 " Ice | 1.978 | 1.447 | 0.109 |
|  | A | From Leg |  | 0.0000 | 136.000 | 2 " Ice | 2.336 | 1.762 | 0.155 |
| $\begin{aligned} & 8843 \text { ( } 15 \times 13.2 \times 11.1 \times 75 \mathrm{lbs}) \\ & \text { (ATT-E) } \end{aligned}$ |  |  | 3.000 |  |  | No Ice | 1.650 | 1.388 | 0.075 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 1.810 | 1.536 | 0.093 |
|  |  |  | 0.000 |  |  | $1^{\prime \prime}$ Ice | 1.978 | 1.692 | 0.113 |
|  | B | From Leg |  | 0.0000 | 136.000 | 2" Ice | 2.336 | 2.027 | 0.164 |
| $\begin{gathered} 8843(15 \times 13.2 \times 11.1 \times 75 \mathrm{lbs}) \\ \text { (ATT-E) } \end{gathered}$ |  |  | 3.000 |  |  | No Ice | 1.650 | 1.388 | 0.075 |
|  |  |  | 0.000 |  |  | 1/2" Ice | 1.810 | 1.536 | 0.093 |
|  |  |  | 0.000 |  |  | $1{ }^{\prime \prime}$ Ice | 1.978 | 1.692 | 0.113 |
|  |  |  |  |  |  | 2 " Ice | 2.336 | 2.027 | 0.164 |


| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 FAX: | Job | US-CT-5018 | $\begin{array}{ll} \hline \text { Page } \\ & 7 \text { of } 19 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date <br> 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight <br>

\hline \multirow[t]{4}{*}{$$
\begin{aligned}
& 8843 \text { (15x13.2x11.1x75lbs)} \\
& \text { (ATT-E) }
\end{aligned}
$$} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.650 \& 1.388 \& 0.075 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.810 \& 1.536 \& 0.093 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.978 \& 1.692 \& 0.113 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.336 \& 2.027 \& 0.164 <br>

\hline \multirow[t]{4}{*}{| Unknown DC |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.547 \& 4.762 \& 0.026 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.708 \& 5.042 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.877 \& 5.328 \& 0.104 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.237 \& 5.924 \& 0.199 <br>

\hline \multirow[t]{4}{*}{| Unknown DC |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.547 \& 4.762 \& 0.026 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.708 \& 5.042 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& 1" Ice \& 1.877 \& 5.328 \& 0.104 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.237 \& 5.924 \& 0.199 <br>

\hline \multirow[t]{4}{*}{| Unknown DC |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.547 \& 4.762 \& 0.026 <br>

\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 1.708 \& 5.042 \& 0.063 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.877 \& 5.328 \& 0.104 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 2.237 \& 5.924 \& 0.199 <br>

\hline \multirow[t]{4}{*}{| SM 602-1 |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{None} \& \& 0.0000 \& 136.000 \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 24.070 \& 11.090 \& 0.707 <br>
\hline \& \& \& \& \& \& 1" Ice \& 28.330 \& 13.630 \& 0.947 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 37.820 \& 18.640 \& 1.562 <br>

\hline \multirow[t]{4}{*}{| SM 602-1 |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{None} \& \& 0.0000 \& 136.000 \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>

\hline \& \& \& \& \& \& 1/2" Ice \& 24.070 \& 11.090 \& 0.707 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 28.330 \& 13.630 \& 0.947 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 37.820 \& 18.640 \& 1.562 <br>

\hline \multirow[t]{4}{*}{| SM 602-1 |
| :--- |
| (ATT-E) |} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{None} \& \& 0.0000 \& 136.000 \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>

\hline \& \& \& \& \& \& 1/2' Ice \& 24.070 \& 11.090 \& 0.707 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 28.330 \& 13.630 \& 0.947 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 37.820 \& 18.640 \& 1.562 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (ATT - R)} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.149 \& 1.149 \& 0.012 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.300 \& 1.300 \& 0.018 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.451 \& 1.451 \& 0.024 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 1.753 \& 1.753 \& 0.035 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (ATT - R)} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.149 \& 1.149 \& 0.012 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.300 \& 1.300 \& 0.018 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.451 \& 1.451 \& 0.024 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 1.753 \& 1.753 \& 0.035 <br>
\hline \multirow[t]{4}{*}{1/3 Remaining Reserved Rights (ATT - R)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& 0.0000 \& 136.000 \& No Ice \& 1.149 \& 1.149 \& 0.012 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 1.300 \& 1.300 \& 0.018 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.451 \& 1.451 \& 0.024 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 1.753 \& 1.753 \& 0.035 <br>
\hline \multicolumn{8}{|l|}{***} \& \& <br>
\hline AIR32 \& A \& From Leg \& 3.000 \& 0.0000 \& 150.000 \& No Ice \& 7.290 \& 6.612 \& 0.161 <br>
\hline KRD901146-1_B66A-B2A \& \& \& 0.000 \& \& \& 1/2' Ice \& 8.007 \& 7.796 \& 0.228 <br>
\hline \multirow[t]{2}{*}{w/ Mount Pipe} \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.667 \& 8.832 \& 0.303 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 9.865 \& 10.574 \& 0.477 <br>
\hline AIR32 \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 150.000 \& No Ice \& 7.290 \& 6.612 \& 0.161 <br>
\hline KRD901146-1_B66A-B2A \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.007 \& 7.796 \& 0.228 <br>
\hline \multirow[t]{2}{*}{w/ Mount Pipe} \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.667 \& 8.832 \& 0.303 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 9.865 \& 10.574 \& 0.477 <br>
\hline AIR32 \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 150.000 \& No Ice \& 7.290 \& 6.612 \& 0.161 <br>
\hline KRD901146-1_B66A-B2A \& \& \& 0.000 \& \& \& 1/2" Ice \& 8.007 \& 7.796 \& 0.228 <br>
\hline w/ Mount Pipe \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.667 \& 8.832 \& 0.303 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 9.865 \& 10.574 \& 0.477 <br>
\hline \multirow[t]{4}{*}{LNX-6515DS-A1M} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& 0.0000 \& 150.000 \& No Ice \& 11.912 \& 10.071 \& 0.087 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 12.733 \& 11.692 \& 0.179 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 13.564 \& 13.337 \& 0.281 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 15.104 \& 16.021 \& 0.521 <br>
\hline
\end{tabular}

| tnxTower <br> Vertical Bridge Engineering, <br> LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 <br> FAX: | Job | US-CT-5018 | $\begin{array}{ll} \hline \text { Page } & \\ & 8 \text { of } 19 \end{array}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side

$f t^{2}$ \& Weight <br>
\hline \multirow[t]{4}{*}{LNX-6515DS-A1M} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 11.912 \& 10.071 \& 0.087 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 12.733 \& 11.692 \& 0.179 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 13.564 \& 13.337 \& 0.281 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 15.104 \& 16.021 \& 0.521 <br>
\hline \multirow[t]{4}{*}{LNX-6515DS-A1M} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 11.912 \& 10.071 \& 0.087 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 12.733 \& 11.692 \& 0.179 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 13.564 \& 13.337 \& 0.281 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 15.104 \& 16.021 \& 0.521 <br>
\hline \multirow[t]{4}{*}{APX16DWV-16DWV-S-E-A $20 \mathrm{w} /$ Mount Pipe} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 9.055 \& 6.507 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 9.778 \& 7.722 \& 0.157 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 10.449 \& 8.776 \& 0.239 <br>
\hline \& \& \& \& \& \& $2{ }^{\prime \prime}$ Ice \& 11.679 \& 10.545 \& 0.429 <br>
\hline \multirow[t]{4}{*}{APX16DWV-16DWV-S-E-A 20 w/ Mount Pipe} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 9.055 \& 6.507 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 9.778 \& 7.722 \& 0.157 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 10.449 \& 8.776 \& 0.239 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 11.679 \& 10.545 \& 0.429 <br>
\hline \multirow[t]{4}{*}{APX16DWV-16DWV-S-E-A 20 w/ Mount Pipe} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 9.055 \& 6.507 \& 0.083 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 9.778 \& 7.722 \& 0.157 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 10.449 \& 8.776 \& 0.239 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 11.679 \& 10.545 \& 0.429 <br>

\hline \multirow[t]{4}{*}{RRUS 11 B12} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& $$
3.000
$$ \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.833 \& 1.182 \& 0.051 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.043 \& 1.330 \& 0.072 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.259 \& 1.485 \& 0.095 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.715 \& 1.826 \& 0.153 <br>
\hline \multirow[t]{4}{*}{RRUS 11 B12} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.833 \& 1.182 \& 0.051 <br>
\hline \& \& \& 0.000 \& \& \& 1/2' Ice \& 3.043 \& 1.330 \& 0.072 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.259 \& 1.485 \& 0.095 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.715 \& 1.826 \& 0.153 <br>
\hline \multirow[t]{4}{*}{RRUS 11 B 12} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.833 \& 1.182 \& 0.051 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 3.043 \& 1.330 \& 0.072 <br>
\hline \& \& \& 0.000 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.259 \& 1.485 \& 0.095 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.715 \& 1.826 \& 0.153 <br>
\hline \multirow[t]{4}{*}{RRUS 11 B4} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.784 \& 1.187 \& 0.051 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.992 \& 1.334 \& 0.071 <br>
\hline \& \& \& 0.000 \& \& \& 1 " Ice \& 3.207 \& 1.490 \& 0.095 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.658 \& 1.833 \& 0.153 <br>
\hline \multirow[t]{4}{*}{RRUS 11 B4} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.784 \& 1.187 \& 0.051 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.992 \& 1.334 \& 0.071 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.207 \& 1.490 \& 0.095 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 3.658 \& 1.833 \& 0.153 <br>
\hline \multirow[t]{4}{*}{RRUS 11 B4} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 2.784 \& 1.187 \& 0.051 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 2.992 \& 1.334 \& 0.071 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 3.207 \& 1.490 \& 0.095 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 3.658 \& 1.833 \& 0.153 <br>
\hline \multirow[t]{4}{*}{IBR-1300} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 0.672 \& 0.307 \& 0.008 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" Ice \& 0.776 \& 0.384 \& 0.013 <br>
\hline \& \& \& 0.000 \& \& \& $1^{\prime \prime}$ Ice \& 0.888 \& 0.470 \& 0.020 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 1.133 \& 0.668 \& 0.040 <br>
\hline \multirow[t]{4}{*}{SM 602-1} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>
\hline \& \& \& \& \& \& 1/2' Ice \& 24.070 \& 11.090 \& 0.707 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 28.330 \& 13.630 \& 0.947 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 37.820 \& 18.640 \& 1.562 <br>
\hline \multirow[t]{4}{*}{SM 602-1} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{None} \& \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{150.000} \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 24.070 \& 11.090 \& 0.707 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 28.330 \& 13.630 \& 0.947 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 37.820 \& 18.640 \& 1.562 <br>
\hline SM 602-1 \& C \& None \& \& 0.0000 \& 150.000 \& No Ice \& 20.000 \& 8.530 \& 0.513 <br>
\hline
\end{tabular}



## Tower Pressures - No Ice

$$
G_{H}=1.100
$$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Section Elevation
\(\qquad\) \\
ft
\end{tabular} \& \(z\)
\(f t\) \& \(K_{Z}\) \& \(q_{z}\)

$k s f$ \& $A_{G}$

$f t^{2}$ \& | $F$ |
| :--- |
| $a$ |
| $c$ |
| $e$ | \& $A_{F}$

$f t^{2}$ \& $A_{R}$

$f t^{2}$ \& $A_{l e g}$

$f t^{2}$ \& \[
$$
\begin{array}{r}
\text { Leg } \\
\%
\end{array}
$$

\] \& | $C_{A} A_{A}$ |
| :--- |
| In |
| Face |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Out |
| Face |
| $f t^{2}$ | <br>

\hline L1 \& 123.592 \& 1.323 \& 0.045 \& 139.454 \& A \& 0.000 \& 139.454 \& 139.454 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 150.000-100.0 \& \& \& \& \& B \& 0.000 \& 139.454 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline 00 \& \& \& \& \& C \& 0.000 \& 139.454 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline L2 \& 82.328 \& 1.215 \& 0.041 \& 127.300 \& A \& 0.000 \& 127.300 \& 127.300 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 100.000-65.50 \& \& \& \& \& B \& 0.000 \& 127.300 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline 0 \& \& \& \& \& C \& 0.000 \& 127.300 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline L3 \& 48.729 \& 1.088 \& 0.037 \& 145.588 \& A \& 0.000 \& 145.588 \& 145.588 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 65.500-32.300 \& \& \& \& \& B \& 0.000 \& 145.588 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 145.588 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline L4 \& 16.164 \& 0.862 \& 0.030 \& 163.104 \& A \& 0.000 \& 163.104 \& 163.104 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 32.300-0.000 \& \& \& \& \& B \& 0.000 \& 163.104 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 163.104 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline
\end{tabular}

## Tower Pressure - With Ice

$$
G_{H}=1.100
$$

| Section Elevation $f t$ | ft | $K_{Z}$ | $q_{z}$ <br> ksf | $t_{Z}$ <br> in | $A_{G}$ $f t^{2}$ | $\begin{aligned} & \hline F \\ & a \\ & c \\ & e \end{aligned}$ | $\overline{A_{F}}$ $f t^{2}$ | $A_{R}$ $f t^{2}$ | $A_{l e g}$ $f t^{2}$ | $\begin{gathered} \text { Leg } \\ \% \end{gathered}$ | $\begin{gathered} \hline C_{A} A_{A} \\ \text { In } \\ \text { Face } \\ {f t^{2}}^{2} \end{gathered}$ | $C_{A} A_{A}$ <br> Out <br> Face <br> $f t^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 123.592 | 1.323 | 0.008 | 1.7117 | 153.719 | A | 0.000 | 153.719 | 153.719 | 100.00 | 0.000 | 0.000 |


| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 FAX: | Job | US-CT-5018 | $\begin{aligned} & \text { Page } \\ & 10 \text { of } 19 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{aligned} & \text { Date } \\ & \text { 10:10:22 05/20/21 } \end{aligned}$ |
|  | Client | DISH | Designed by GWesh |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Section Elevation
\(\qquad\) \\
\(f t\)
\end{tabular} \& \(z\)
\(f t\) \& \(K_{Z}\) \& \(q_{z}\)
\(k s f\) \& \(t_{Z}\)
in \& \(A_{G}\)

$f t^{2}$ \& | $F$ |
| :--- |
| $a$ |
| $c$ |
| $e$ | \& $A_{F}$

$f t^{2}$ \& $A_{R}$

$f t^{2}$ \& $A_{l e g}$

$f t^{2}$ \& \[
$$
\begin{gathered}
L e g \\
\%
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { In } \\
\text { Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& | $C_{A} A_{A}$ |
| :--- |
| Out |
| Face |
| $f t^{2}$ | <br>

\hline 150.000-100.000 \& \& \& \& \& \& B \& 0.000 \& 153.719 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& \& C \& 0.000 \& 153.719 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline L2 \& 82.328 \& 1.215 \& 0.007 \& 1.6436 \& 137.142 \& A \& 0.000 \& 137.142 \& 137.142 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 100.000-65.500 \& \& \& \& \& \& B \& 0.000 \& 137.142 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& \& C \& 0.000 \& 137.142 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& 48.729 \& 1.088 \& 0.007 \& 1.5596 \& 154.682 \& A \& 0.000 \& 154.682 \& 154.682 \& 100.00 \& 0.000 \& 0.000 <br>
\hline 65.500-32.300 \& \& \& \& \& \& B \& 0.000 \& 154.682 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& \& C \& 0.000 \& 154.682 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline L4 32.300-0.000 \& 16.164 \& 0.862 \& 0.005 \& 1.3967 \& 171.500 \& A \& 0.000 \& 171.500 \& 171.500 \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& \& B \& 0.000 \& 171.500 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline \& \& \& \& \& \& C \& 0.000 \& 171.500 \& \& 100.00 \& 0.000 \& 0.000 <br>
\hline
\end{tabular}

## Tower Pressure - Service

$$
G_{H}=1.100
$$

$\left.\begin{array}{|r|c|c|c|c|c|c|c|c|c|c|c|}\hline \begin{array}{c}\text { Section } \\ \text { Elevation }\end{array} & z & K_{Z} & q_{z} & A_{G} & F & A_{F} & A_{R} & A_{\text {leg }} & \begin{array}{c}\text { Leg } \\ \% \\ \%\end{array} & \begin{array}{c}C_{A} A_{A} \\ \text { In }\end{array} & \begin{array}{c}C_{A} A_{A} \\ \text { Out } \\ \text { Face }\end{array} \\ \text { Face }\end{array}\right]$

Tower Forces - No Ice - Wind Normal To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Section \\
Elevation \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Add \\
Weight \\
K
\end{tabular} \& Self Weight K \& \(F\)
\(a\)
\(c\)
\(e\) \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
\(k s f\)
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.045 \& 1 \& 1 \& 139.454 \& 5.040 \& 0.101 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.041 \& 1 \& 1 \& 127.300 \& 4.223 \& 0.122 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>

\hline $$
0
$$ \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>

\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.037 \& 1 \& 1 \& 145.588 \& 4.315 \& 0.130 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.030 \& 1 \& 1 \& 163.104 \& 3.981 \& 0.123 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline Sum Weight: \& 0.574 \& 31.490 \& \& \& \& \& \& OTM \& 1245.225 \& 17.559 \& \& <br>
\hline
\end{tabular}

| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 FAX: | Job | US-CT-5018 | $\begin{aligned} & \text { Page } 11 \text { of } 19 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |


| Section Elevation <br> ft | Add Weight | Self Weight K | $F$ $a$ $c$ $c$ $e$ | $e$ | $C_{F}$ | $q_{z}$ <br> ksf | $D_{F}$ | $D_{R}$ | $A_{E}$ <br> $f t^{2}$ | $F$ $K$ | ${ }^{w}$ | Ctrl. Face |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | kip-ft |  |  |  |

Tower Forces - No Ice - Wind 60 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation
\[
f t
\] \& Add Weight
\[
K
\] \& Self Weight
\(\qquad\) \& \begin{tabular}{l}
\(F\) \\
\(a\) \\
\(c\) \\
\(e\) \\
\hline
\end{tabular} \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
\(k s f\)
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& Ctrl. Face <br>
\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.045 \& 1 \& 1 \& 139.454 \& 5.040 \& 0.101 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.041 \& 1 \& 1 \& 127.300 \& 4.223 \& 0.122 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.037 \& 1 \& 1 \& 145.588 \& 4.315 \& 0.130 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.030 \& 1 \& 1 \& 163.104 \& 3.981 \& 0.123 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline Sum Weight: \& 0.574 \& 31.490 \& \& \& \& \& \& OTM \& 1245.225 \& 17.559 \& \& <br>
\hline \& \& \& \& \& \& \& \& \& kip-ft \& \& \& <br>
\hline
\end{tabular}

Tower Forces - No Ice - Wind 90 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Section Elevation \\
ft
\end{tabular} \& Add Weight
\[
K
\] \& \begin{tabular}{l}
Self Weight \\
K
\end{tabular} \& \(F\)
\(a\)
\(c\)
\(e\)
\(e\) \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
ksf
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.045 \& 1 \& 1 \& 139.454 \& 5.040 \& 0.101 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.041 \& 1 \& 1 \& 127.300 \& 4.223 \& 0.122 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.037 \& 1 \& 1 \& 145.588 \& 4.315 \& 0.130 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.030 \& 1 \& 1 \& 163.104 \& 3.981 \& 0.123 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline Sum Weight: \& 0.574 \& 31.490 \& \& \& \& \& \& OTM \& 1245.225 \& 17.559 \& \& <br>
\hline \& \& \& \& \& \& \& \& \& kip-ft \& \& \& <br>
\hline
\end{tabular}

| tnxTower <br> Vertical Bridge Engineering, LLC <br> 750 Park of Commerce Drive, Suite 200 <br> Boca Raton, FL 33487 <br> Phone: 561-948-6367 FAX: | Job | US-CT-5018 | $\begin{aligned} & \text { Page } 12 \text { of } 19 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |

## Tower Forces - With Ice - Wind Normal To Face

| Section Elevation $f t$ | Add Weight K | Self Weight K | $F$ $a$ $c$ $e$ | $e$ | $C_{F}$ | $q_{z}$ <br> $k s f$ | $D_{F}$ | $D_{R}$ | $\overline{A_{E}}$ $f t^{2}$ | $F$ $K$ | $w$ $k l f$ | Ctrl. <br> Face |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 0.154 | 8.965 | A | 1 | 1.2 | 0.008 | 1 | 1 | 153.719 | 1.612 | 0.032 | C |
| 150.000-100.0 |  |  | B | 1 | 1.2 |  | 1 | 1 | 153.719 |  |  |  |
| 00 |  |  | C | 1 | 1.2 |  | 1 | 1 | 153.719 |  |  |  |
| L2 | 0.145 | 10.520 | A | 1 | 1.2 | 0.007 | 1 | 1 | 136.750 | 1.317 | 0.038 | C |
| 100.000-65.50 |  |  | B | 1 | 1.2 |  | 1 | 1 | 136.750 |  |  |  |
| 0 |  |  | C | 1 | 1.2 |  | 1 | 1 | 136.750 |  |  |  |
| L3 | 0.139 | 12.158 | A | 1 | 1.2 | 0.007 | 1 | 1 | 154.218 | 1.326 | 0.040 | C |
| 65.500-32.300 |  |  | B | 1 | 1.2 |  | 1 | 1 | 154.218 |  |  |  |
|  |  |  | C | 1 | 1.2 |  | 1 | 1 | 154.218 |  |  |  |
| L4 | 0.136 | 13.507 | A | 1 | 1.2 | 0.005 | 1 | 1 | 170.622 | 1.209 | 0.037 | C |
| 32.300-0.000 |  |  | B | 1 | 1.2 |  | 1 | 1 | 170.622 |  |  |  |
|  |  |  | C | 1 | 1.2 |  | 1 | 1 | 170.622 |  |  |  |
| Sum Weight: | 0.574 | 45.149 |  |  |  |  |  | OTM | $\begin{array}{r} 391.830 \\ \text { kip-ft } \end{array}$ | 5.464 |  |  |

## Tower Forces - With Ice - Wind 60 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Section Elevation \\
ft
\end{tabular} \& Add Weight \& Self Weight K \& \(F\)
\(a\)
\(c\)
\(c\)
\(e\) \& \(e\) \& \(C_{F}\) \& \(q_{z}\) \(k s f\) \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$
$k l f$ \& Ctrl. Face <br>
\hline L1 \& 0.154 \& 8.965 \& A \& 1 \& 1.2 \& 0.008 \& 1 \& 1 \& 153.719 \& 1.612 \& 0.032 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 153.719 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 153.719 \& \& \& <br>
\hline L2 \& 0.145 \& 10.520 \& A \& 1 \& 1.2 \& 0.007 \& 1 \& 1 \& 136.750 \& 1.317 \& 0.038 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 136.750 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 136.750 \& \& \& <br>
\hline L3 \& 0.139 \& 12.158 \& A \& 1 \& 1.2 \& 0.007 \& 1 \& 1 \& 154.218 \& 1.326 \& 0.040 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 154.218 \& \& \& <br>
\hline \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 154.218 \& \& \& <br>
\hline L4 \& 0.136 \& 13.507 \& A \& 1 \& 1.2 \& 0.005 \& 1 \& 1 \& 170.622 \& 1.209 \& 0.037 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 170.622 \& \& \& <br>
\hline \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 170.622 \& \& \& <br>

\hline Sum Weight: \& 0.574 \& 45.149 \& \& \& \& \& \& OTM \& $$
\begin{array}{r}
391.830 \\
\text { kip-ft }
\end{array}
$$ \& 5.464 \& \& <br>

\hline
\end{tabular}

## Tower Forces - With Ice - Wind 90 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation
\(\qquad\) \& \begin{tabular}{l}
Add Weight
\(\qquad\) \\
K
\end{tabular} \& Self Weight
\(\qquad\) K \& \[
\begin{aligned}
\& \hline F \\
\& a \\
\& c \\
\& e
\end{aligned}
\] \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
ksf
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline L1 \& 0.154 \& 8.965 \& A \& 1 \& 1.2 \& 0.008 \& 1 \& 1 \& 153.719 \& 1.612 \& 0.032 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 153.719 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 153.719 \& \& \& <br>
\hline L2 \& 0.145 \& 10.520 \& A \& 1 \& 1.2 \& 0.007 \& 1 \& 1 \& 136.750 \& 1.317 \& 0.038 \& C <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation \& Add Weight
$\qquad$ \& Self Weight
$\qquad$ \& $F$
$a$
$c$
$c$
$e$ \& $e$ \& $C_{F}$ \& $q_{z}$ $k s f$ \& $D_{F}$ \& $D_{R}$ \& $A_{E}$

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline 100.000-65.50 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 136.750 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 136.750 \& \& \& <br>
\hline L3 \& 0.139 \& 12.158 \& A \& 1 \& 1.2 \& 0.007 \& 1 \& 1 \& 154.218 \& 1.326 \& 0.040 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 154.218 \& \& \& <br>
\hline \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 154.218 \& \& \& <br>
\hline L4 \& 0.136 \& 13.507 \& A \& 1 \& 1.2 \& 0.005 \& 1 \& 1 \& 170.622 \& 1.209 \& 0.037 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 1.2 \& \& 1 \& 1 \& 170.622 \& \& \& <br>
\hline \& \& \& C \& 1 \& 1.2 \& \& 1 \& 1 \& 170.622 \& \& \& <br>

\hline Sum Weight: \& 0.574 \& 45.149 \& \& \& \& \& \& OTM \& $$
391.830
$$ \& 5.464 \& \& <br>

\hline
\end{tabular}

Tower Forces - Service - Wind Normal To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation
\(\qquad\) \& Add Weight
\(\qquad\)
\[
K
\] \& \begin{tabular}{l}
Self Weight
\(\qquad\) \\
K
\end{tabular} \& \begin{tabular}{l}
\(F\) \\
\(a\) \\
\(c\) \\
\(e\) \\
\hline
\end{tabular} \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
ksf
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.010 \& 1 \& 1 \& 139.454 \& 1.146 \& 0.023 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.009 \& 1 \& 1 \& 127.300 \& 0.961 \& 0.028 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.008 \& 1 \& 1 \& 145.588 \& 0.981 \& 0.030 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.007 \& 1 \& 1 \& 163.104 \& 0.906 \& 0.028 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>

\hline Sum Weight: \& 0.574 \& 31.490 \& \& \& \& \& \& OTM \& $$
\begin{array}{r}
283.238 \\
\text { kip-ft }
\end{array}
$$ \& 3.994 \& \& <br>

\hline
\end{tabular}

Tower Forces - Service - Wind 60 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation
\[
f t
\] \& \begin{tabular}{l}
Add \\
Weight \\
K
\end{tabular} \& Self Weight K \& \begin{tabular}{l}
\(F\) \\
\(a\) \\
\(c\) \\
\(e\) \\
\hline
\end{tabular} \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\[
q_{z}
\] \\
ksf
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$

$k l f$ \& | Ctrl. |
| :--- |
| Face | <br>

\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.010 \& 1 \& 1 \& 139.454 \& 1.146 \& 0.023 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.009 \& 1 \& 1 \& 127.300 \& 0.961 \& 0.028 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>

\hline $$
0
$$ \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>

\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.008 \& 1 \& 1 \& 145.588 \& 0.981 \& 0.030 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.007 \& 1 \& 1 \& 163.104 \& 0.906 \& 0.028 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline
\end{tabular}

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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |


| Section Elevation <br> ft | Add Weight <br> K | Self Weight K | $\begin{aligned} & \hline F \\ & a \\ & c \\ & e \end{aligned}$ | $e$ | $C_{F}$ | $q_{z}$ <br> $k s f$ | $D_{F}$ | $D_{R}$ | $A_{E}$ $f t^{2}$ | $F$ $K$ | w $k l f$ | Ctrl. Face |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sum Weight: | 0.574 | 31.490 | C | 1 | 0.73 |  | 1 | $\begin{array}{r} 1 \\ \text { OTM } \end{array}$ | 163.104 283.238 <br> kip-ft | 3.994 |  |  |

Tower Forces - Service - Wind 90 To Face

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation
\[
f t
\] \& Add Weight K \& Self Weight K \& \begin{tabular}{l}
\(F\) \\
\(a\) \\
\(c\) \\
\(e\) \\
\hline
\end{tabular} \& \(e\) \& \(C_{F}\) \& \begin{tabular}{l}
\(q_{z}\) \\
ksf
\end{tabular} \& \(D_{F}\) \& \(D_{R}\) \& \(A_{E}\)

$f t^{2}$ \& $F$
$K$ \& $w$
$k l f$ \& Ctrl. Face <br>
\hline L1 \& 0.154 \& 5.298 \& A \& 1 \& 0.73 \& 0.010 \& 1 \& 1 \& 139.454 \& 1.146 \& 0.023 \& C <br>
\hline 150.000-100.0 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline 00 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 139.454 \& \& \& <br>
\hline L2 \& 0.145 \& 7.348 \& A \& 1 \& 0.73 \& 0.009 \& 1 \& 1 \& 127.300 \& 0.961 \& 0.028 \& C <br>
\hline 100.000-65.50 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline 0 \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 127.300 \& \& \& <br>
\hline L3 \& 0.139 \& 8.742 \& A \& 1 \& 0.73 \& 0.008 \& 1 \& 1 \& 145.588 \& 0.981 \& 0.030 \& C <br>
\hline 65.500-32.300 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 145.588 \& \& \& <br>
\hline L4 \& 0.136 \& 10.102 \& A \& 1 \& 0.73 \& 0.007 \& 1 \& 1 \& 163.104 \& 0.906 \& 0.028 \& C <br>
\hline 32.300-0.000 \& \& \& B \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>
\hline \& \& \& C \& 1 \& 0.73 \& \& 1 \& 1 \& 163.104 \& \& \& <br>

\hline Sum Weight: \& 0.574 \& 31.490 \& \& \& \& \& \& OTM \& $$
\begin{array}{r}
283.238 \\
\text { kip- } \mathrm{ft}
\end{array}
$$ \& 3.994 \& \& <br>

\hline
\end{tabular}

Force Totals

| Load Case | Vertical Forces $K$ | Sum of Forces X K | Sum of Forces Z K | Sum of Overturning Moments, $M_{x}$ kip-ft | Sum of Overturning Moments, $M_{z}$ kip-ft | Sum of Torques $k i p-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Leg Weight | 31.490 |  |  |  |  |  |
| Bracing Weight | 0.000 |  |  |  |  |  |
| Total Member Self-Weight | 31.490 |  |  | 0.065 | 0.055 |  |
| Total Weight | 41.578 |  |  | 0.065 | 0.055 |  |
| Wind 0 deg - No Ice |  | 0.014 | -39.657 | -4341.758 | -1.588 | -0.157 |
| Wind 90 deg - No Ice |  | 39.689 | -0.014 | -1.579 | -4345.926 | 0.143 |
| Wind 180 deg - No Ice |  | -0.014 | 39.657 | 4341.887 | 1.698 | 0.157 |
| Member Ice | 13.659 |  |  |  |  |  |
| Total Weight Ice | 74.196 |  |  | 0.309 | 0.286 |  |
| Wind 0 deg - Ice |  | 0.003 | -11.466 | -1235.932 | -0.017 | -0.035 |
| Wind 90 deg - Ice |  | 11.473 | -0.003 | 0.005 | -1236.802 | 0.039 |
| Wind 180 deg - Ice |  | -0.003 | 11.466 | 1236.550 | 0.590 | 0.035 |
| Total Weight | 41.578 |  |  | 0.065 | 0.055 |  |
| Wind 0 deg - Service |  | 0.003 | -9.020 | -987.524 | -0.319 | -0.036 |
| Wind 90 deg - Service |  | 9.028 | -0.003 | -0.309 | -988.479 | 0.032 |
| Wind 180 deg - Service |  | -0.003 | 9.020 | 987.653 | 0.429 | 0.036 |


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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | Date <br> 10:10:22 05/20/21 |
|  | Client | DISH | Designed by GWesh |

## Load Combinations

| Comb. No. |  | Description |
| :---: | :---: | :---: |
| 1 | Dead Only |  |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |  |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |  |
| 4 | 1.2 Dead+1.0 Wind 90 deg - No Ice |  |
| 5 | 0.9 Dead+1.0 Wind 90 deg - No Ice |  |
| 6 | 1.2 Dead+1.0 Wind 180 deg - No Ice |  |
| 7 | 0.9 Dead+1.0 Wind 180 deg - No Ice |  |
| 8 | 1.2 Dead+1.0 Ice+1.0 Temp |  |
| 9 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |  |
| 10 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |  |
| 11 | 1.2 Dead+1.0 Wind $180 \mathrm{deg}+1.0$ Ice+1.0 Temp |  |
| 12 | Dead+Wind 0 deg - Service |  |
| 13 | Dead+Wind 90 deg - Service |  |
| 14 | Dead+Wind 180 deg - Service |  |


| Maximum Member Forces |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Condition | Gov. <br> Load <br> Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| L1 | 150-100 | Pole | Max Tension | 13 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 8 | -39.336 | 0.297 | -0.322 |
|  |  |  | Max. Mx | 4 | -15.584 | -889.242 | 0.052 |
|  |  |  | Max. My | 6 | -15.587 | 0.190 | -888.554 |
|  |  |  | Max. Vy | 4 | 27.458 | -889.242 | 0.052 |
|  |  |  | Max. Vx | 6 | 27.425 | 0.190 | -888.554 |
|  |  |  | Max. Torque | 7 |  |  | -0.154 |
| L2 | 100-65.5 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 8 | -50.938 | 0.297 | -0.322 |
|  |  |  | Max. Mx | 4 | -24.069 | -1867.185 | 0.540 |
|  |  |  | Max. My | 6 | -24.071 | 0.685 | -1865.413 |
|  |  |  | Max. Vy | 4 | 31.460 | -1867.185 | 0.540 |
|  |  |  | Max. Vx | 6 | 31.427 | 0.685 | -1865.413 |
|  |  |  | Max. Torque | 7 |  |  | -0.153 |
| L3 | 65.5-32.3 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 8 | -64.966 | 0.297 | -0.322 |
|  |  |  | Max. Mx | 4 | -34.613 | -2945.175 | 1.014 |
|  |  |  | Max. My | 6 | -34.615 | 1.162 | -2942.354 |
|  |  |  | Max. Vy | 4 | 35.406 | -2945.175 | 1.014 |
|  |  |  | Max. Vx | 6 | 35.374 | 1.162 | -2942.354 |
|  |  |  | Max. Torque | 7 |  |  | -0.153 |
| L4 | 32.3-0 | Pole | Max Tension | 1 | 0.000 | 0.000 | 0.000 |
|  |  |  | Max. Compression | 8 | -84.539 | 0.297 | -0.322 |
|  |  |  | Max. Mx | 4 | -49.875 | -4455.377 | 1.600 |
|  |  |  | Max. My | 6 | -49.875 | 1.749 | -4451.266 |
|  |  |  | Max. Vy | 4 | 39.710 | -4455.377 | 1.600 |
|  |  |  | Max. Vx | 6 | 39.679 | 1.749 | -4451.266 |
|  |  |  | Max. Torque | 7 |  |  | -0.153 |

## Maximum Reactions

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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |


| Location | Condition | Gov. <br> Load <br> Comb. | Vertical K | $\begin{gathered} \text { Horizontal, } X \\ K \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 8 | 84.539 | 0.000 | 0.000 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 7 | 37.420 | 0.014 | -39.656 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 3 | 37.420 | -0.014 | 39.656 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 4451.104 | -0.014 | 39.656 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 4 | 4455.377 | -39.688 | 0.014 |
|  | Max. Torsion | 3 | 0.153 | -0.014 | 39.656 |
|  | Min. Vert | 5 | 37.420 | -39.688 | 0.014 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | 37.420 | -39.688 | 0.014 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 7 | 37.420 | 0.014 | -39.656 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 6 | -4451.266 | 0.014 | -39.656 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 6 | -1.749 | 0.014 | -39.656 |
|  | Min. Torsion | 7 | -0.153 | 0.014 | -39.656 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $_{x}$ $K$ | Shear ${ }_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 41.578 | 0.000 | 0.000 | 0.065 | 0.055 | 0.000 |
| 1.2 Dead+1.0 Wind 0 deg - No | 49.893 | 0.014 | -39.656 | -4451.104 | -1.613 | -0.151 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 0 deg - No | 37.420 | 0.014 | -39.656 | -4422.307 | -1.620 | -0.153 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg - No | 49.893 | 39.688 | -0.014 | -1.600 | -4455.377 | 0.142 |
| Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 90 deg - No | 37.420 | 39.688 | -0.014 | -1.611 | -4426.548 | 0.142 |
| Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 deg - | 49.893 | -0.014 | 39.656 | 4451.266 | 1.749 | 0.152 |
| No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 180 deg - | 37.420 | -0.014 | 39.656 | 4422.426 | 1.721 | 0.153 |
| No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Ice+1.0 Temp | 84.539 | 0.000 | 0.000 | 0.322 | 0.297 | 0.000 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 | 84.539 | 0.003 | -11.466 | -1306.226 | 0.010 | -0.029 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 deg+1.0 | 84.539 | 11.473 | -0.003 | 0.039 | -1307.152 | 0.039 |
| Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 | 84.539 | -0.003 | 11.466 | 1306.941 | 0.648 | 0.029 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| Dead+Wind 0 deg - Service | 41.578 | 0.003 | -9.019 | -1008.649 | -0.324 | -0.035 |
| Dead+Wind 90 deg - Service | 41.578 | 9.026 | -0.003 | -0.314 | -1009.626 | 0.032 |
| Dead+Wind 180 deg - Service | 41.578 | -0.003 | 9.019 | 1008.783 | 0.438 | 0.035 |

Solution Summary

| Load | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PX | PY | $P Z$ | PX | PY | PZ |  |
| Comb. | K | K | K | K | K | K |  |
| 1 | 0.000 | -41.578 | 0.000 | 0.000 | 41.578 | 0.000 | 0.000\% |
| 2 | 0.014 | -49.893 | -39.657 | -0.014 | 49.893 | 39.656 | 0.002\% |
| 3 | 0.014 | -37.420 | -39.657 | -0.014 | 37.420 | 39.656 | 0.002\% |
| 4 | 39.689 | -49.893 | -0.014 | -39.688 | 49.893 | 0.014 | 0.002\% |
| 5 | 39.689 | -37.420 | -0.014 | -39.688 | 37.420 | 0.014 | 0.002\% |
| 6 | -0.014 | -49.893 | 39.657 | 0.014 | 49.893 | -39.656 | 0.002\% |


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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |


|  | Sum of Applied Forces |  |  |  |  | Sum of Reactions |  |  |  | $P Z$ | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $R$ | $P Z$ | $P X$ | $P Y$ | $K$ |  |  |  |  |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |  |  |  |  |
| 7 | -0.014 | -37.420 | 39.657 | 0.014 | 37.420 | -39.656 | $0.002 \%$ |  |  |  |  |
| 8 | 0.000 | -84.539 | 0.000 | 0.000 | 84.539 | 0.000 | $0.000 \%$ |  |  |  |  |
| 9 | 0.003 | -84.539 | -11.466 | -0.003 | 84.539 | 11.466 | $0.000 \%$ |  |  |  |  |
| 10 | 11.473 | -84.539 | -0.003 | -11.473 | 84.539 | 0.003 | $0.000 \%$ |  |  |  |  |
| 11 | -0.003 | -84.539 | 11.466 | 0.003 | 84.539 | -11.466 | $0.000 \%$ |  |  |  |  |
| 12 | 0.003 | -41.578 | -9.020 | -0.003 | 41.578 | 9.019 | $0.003 \%$ |  |  |  |  |
| 13 | 9.028 | -41.578 | -0.003 | -9.026 | 41.578 | 0.003 | $0.003 \%$ |  |  |  |  |
| 14 | -0.003 | -41.578 | 9.020 | 0.003 | 41.578 | -9.019 | $0.003 \%$ |  |  |  |  |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00000001 |
| 2 | Yes | 5 | 0.00000001 | 0.00005723 |
| 3 | Yes | 5 | 0.00000001 | 0.00004805 |
| 4 | Yes | 5 | 0.00000001 | 0.00005695 |
| 5 | Yes | 5 | 0.00000001 | 0.00004780 |
| 6 | Yes | 5 | 0.00000001 | 0.00006041 |
| 7 | Yes | 5 | 0.00000001 | 0.00005040 |
| 8 | Yes | 4 | 0.00000001 | 0.00000001 |
| 9 | Yes | 7 | 0.00000001 | 0.00008491 |
| 10 | Yes | 7 | 0.00000001 | 0.00008498 |
| 11 | Yes | 7 | 0.00000001 | 0.00008501 |
| 12 | Yes | 4 | 0.00000001 | 0.00009667 |
| 13 | Yes | 4 | 0.00000001 | 0.00009674 |
| 14 | Yes | 4 | 0.00000001 | 0.00009676 |

## Maximum Tower Deflections - Service Wind

| Section No. | Elevation <br> $f t$ | Horz. Deflection in | Gov. Load Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 150-100 | 16.222 | 13 | 0.9439 | 0.0001 |
| L2 | 105.5-65.5 | 8.129 | 13 | 0.7247 | 0.0001 |
| L3 | 72.3-32.3 | 3.833 | 13 | 0.4929 | 0.0000 |
| L4 | 40.1-0 | 1.203 | 13 | 0.2675 | 0.0000 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150.000 | AIR32 KRD901146-1_B66A-B2A w/ Mount Pipe | 13 | 16.222 | 0.9439 | 0.0001 | 61020 |
| 136.000 | (2) TPA65R-BU8D w/ Mount Pipe | 13 | 13.512 | 0.8827 | 0.0001 | 21792 |
| 125.000 | LP 716 | 13 | 11.453 | 0.8313 | 0.0001 | 12203 |


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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | (wist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | 71.591 | 4 | 0 | $\circ$ |
| L1 | $150-100$ | 35.882 | 4 | 4.1677 | 0.0005 |
| L2 | $105.5-65.5$ | 16.919 | 4 | 2.1999 | 0.0003 |
| L3 | $72.3-32.3$ | 5.308 | 4 | 1.1811 | 0.0001 |
| L4 | $40.1-0$ |  |  |  | 0.0001 |
|  |  |  |  |  |  |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. Load <br> Comb. | Deflection in | Tilt | Twist | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150.000 | AIR32 KRD901146-1_B66A-B2A w/ Mount Pipe | 4 | 71.591 | 4.1677 | 0.0005 | 13946 |
| 136.000 | (2) TPA65R-BU8D w/ Mount Pipe | 4 | 59.635 | 3.8976 | 0.0004 | 4979 |
| 125.000 | LP 716 | 4 | 50.551 | 3.6706 | 0.0004 | 2787 |

## Compression Checks

| Pole Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
|  | $f t$ |  | $f t$ | $f t$ |  | in ${ }^{2}$ | K | K | $\phi P_{n}$ |
| L1 | 150-100 (1) | TP39.6x26.4x0.3 | 50.000 | 150.000 | 134.0 | 36.0389 | -15.584 | 453.637 | 0.034 |
| L2 | 100-65.5 (2) | TP48.3x37.548x0.4 | 40.000 | 150.000 | 110.1 | 58.4932 | -24.069 | 1091.020 | 0.022 |
| L3 | 65.5-32.3 (3) | TP56.3x45.6722x0.4 | 40.000 | 150.000 | 94.2 | 68.3395 | -34.613 | 1720.030 | 0.020 |
| L4 | 32.3-0 (4) | TP64x53.4276x0.4 | 40.100 | 150.000 | 79.7 | 80.7466 | -49.875 | 2581.700 | 0.019 |

## Pole Bending Design Data

| Section | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio <br> No. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $M_{u x}$ |  |  |  |  |  |  |  |  |


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| :---: | :---: | :---: | :---: |
|  | Project | Monopole Structural Analysis | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 10:10:22 05/20/21 } \end{array}$ |
|  | Client | DISH | Designed by GWesh |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual <br> $T_{u}$ | $\phi T_{n}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | K | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | 150-100 (1) | TP39.6x26.4x0.3 | 27.458 | 632.482 | 0.043 | 0.142 | 2096.383 | 0.000 |
| L2 | 100-65.5 (2) | TP48.3x37.548x0.4 | 31.460 | 1026.560 | 0.031 | 0.142 | 4141.917 | 0.000 |
| L3 | 65.5-32.3 (3) | TP56.3x45.6722x0.4 | 35.406 | 1199.360 | 0.030 | 0.142 | 5653.708 | 0.000 |
| L4 | 32.3-0 (4) | TP64x53.4276x0.4 | 39.710 | 1417.100 | 0.028 | 0.142 | 7892.933 | 0.000 |


| Pole Interaction Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Ratio $P_{u}$ | Ratio $M_{u x}$ | Ratio $M_{u y}$ | $\begin{gathered} \text { Ratio } \\ V_{u} \end{gathered}$ | $\begin{aligned} & \text { Ratio } \\ & T_{u} \end{aligned}$ | Comb. <br> Stress | Allow. <br> Stress | Criteria |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L1 | 150-100 (1) | 0.034 | 0.463 | 0.000 | 0.043 | 0.000 | $\begin{gathered} 0.499 \\ \end{gathered}$ | 1.000 | 4.8.2 |
| L2 | 100-65.5 (2) | 0.022 | 0.478 | 0.000 | 0.031 | 0.000 | $0.501$ | 1.000 | $4.8 .2$ |
| L3 | 65.5-32.3 (3) | 0.020 | 0.581 | 0.000 | 0.030 | 0.000 | $0.602$ | 1.000 | 4.8.2 |
| L4 | 32.3-0 (4) | 0.019 | 0.675 | 0.000 | 0.028 | 0.000 | $0.695$ | 1.000 | 4.8.2 |

## Section Capacity Table

| Section No. | $\begin{gathered} \text { Elevation } \\ f t \end{gathered}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} ø P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 150-100 | Pole | TP39.6x26.4x0.3 | 1 | -15.584 | 453.637 | 49.9 | Pass |
| L2 | 100-65.5 | Pole | TP48.3x $37.548 \times 0.4$ | 2 | -24.069 | 1091.020 | 50.1 | Pass |
| L3 | 65.5-32.3 | Pole | TP56.3x45.6722x0.4 | 3 | -34.613 | 1720.030 | 60.2 | Pass |
| L4 | 32.3-0 | Pole | TP64x53.4276x0.4 | 4 | -49.875 | 2581.700 | 69.5 | Pass |
|  |  |  |  |  |  | Pole (L4) RATING = | $\begin{gathered} \text { Summary } \\ 69.5 \\ \mathbf{6 9 . 5} \end{gathered}$ | $\begin{aligned} & \text { Pass } \\ & \text { Pass } \end{aligned}$ |

Program Version 8.0.9.0-4/12/2021 File:C:/Users/gwesh/Documents/SA/US-CT-5018/tnx Files/US-CT-5018_SA_051921_DISH.eri

## Monopole Base Plate Connection

| Site Info |  |
| ---: | ---: |
| BU \# | US-CT-5018 |
| Site Name |  |
| Order \# |  |



## Connection Properties

## Analysis Results

## Anchor Rod Data

(22) 2-1/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 72" BC

Base Plate Data
79" OD x 2" Plate (A572-50; Fy=50 ksi, Fu=65 ksi)
Stiffener Data
N/A

Pole Data
64" x 0.4" 18-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)

| Anchor Rod Summary |  | (units of kips, kip-in) |
| :---: | :--- | :---: |
| $\mathrm{Pu} \_\mathrm{c}=137.22$ | $\phi \mathrm{Pn} \_\mathrm{c}=268.39$ | Stress Rating |
| $\mathrm{Vu}=1.81$ | $\phi \mathrm{Vn}=120.77$ | $\mathbf{5 1 . 2 \%}$ |
| $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |


| Base Plate Summary |  |  |
| :--- | :--- | :---: |
| Max Stress (ksi): | 36.95 | (Flexural) |
| Allowable Stress (ksi): | 45 |  |
| Stress Rating: | $\mathbf{8 2 . 1 \%}$ | Pass |

## Drilled Pier Foundation

| BU \# : | US-CT-5018 |  |
| ---: | :--- | :---: |
| Site Name: |  |  |
| Order Number: |  |  |
| TIA-222 Revison: | H |  |
| Tower Type: | Monopole |  |
| Applied Loads |  |  |
| Comp. |  |  |
| Moment (kip-ft) | 4455 |  |
| Axial Force (kips) | 50 |  |
| Shear Force (kips) | 40 |  |

Report File: $\square$

| Material Properties |  |
| ---: | ---: | ---: |
| Concrete Strength, f'c: | 4.5 ksi |
| Rebar Strength, Fy: | 60 ksi |
| Tie Yield Strength, Fyt: | 60 ksi |


| Pier Design Data |  |  |
| :---: | :---: | :---: |
| Depth | 24 | ft |
| Ext. Above Grade | 0.5 | ft |
| Pier Section 1 |  |  |
| From 0.5' above grade to 24 ' below grad |  |  |
| Pier Diameter | 8 | ft |
| Rebar Quantity | 38 |  |
| Rebar Size | 10 |  |
| Clear Cover to Ties | 3 | in |
| Tie Size | 5 |  |
| Tie Spacing | 12 | in |

Embedded Pole Inputs

| Analysis Results |  |  |
| :---: | :---: | :---: |
| Soil Lateral Check | Compression | Uplift |
| $\mathrm{D}_{\mathrm{v}=0}$ (ft from TOC) | 7.90 | - |
| Soil Safety Factor | 5.49 | - |
| Max Moment (kip-ft) | 4917.17 | - |
| Rating | 24.2\% | - |
| Soil Vertical Check | Compression | Uplift |
| Skin Friction (kips) | 933.05 | - |
| End Bearing (kips) | 2365.56 | - |
| Weight of Concrete (kips) | 168.97 | - |
| Total Capacity (kips) | 3298.61 | - |
| Axial (kips) | 218.97 | - |
| Rating | 6.6\% | - |
| Reinforced Concrete Flexure | Compression | Uplift |
| Critical Depth (ft from TOC) | 7.45 | - |
| Critical Moment (kip-ft) | 4915.53 | - |
| Critical Moment Capacity | 9124.40 | - |
| Rating | 53.9\% | - |
| Reinforced Concrete Shear | Compression | Uplift |
| Critical Depth (ft from TOC) | 19.49 | - |
| Critical Shear (kip) | 876.04 | - |
| Critical Shear Capacity | 1050.65 | - |
| Rating | 83.4\% | - |
|  |  |  |
| Soil Interaction Rating | 24.2\% |  |
| Structural Foundation Rating | 83.4\% |  |



## Pier and Pad Foundation

BU \# : US-CT-5018
Site Name: App. Number: $\qquad$

| TIA-222 Revision: | H |
| ---: | :--- |
| Tower Type: | Monopole |


| Top \& Bot. Pad Rein. Different?: | $\square$ |
| ---: | :---: |
| Block Foundation?: | $\square$ |
| Rectangular Pad?: | $\square$ |


| Superstructure Analysis Reactions |  |  |  |
| ---: | :---: | :--- | :---: |
| Compression, $\mathbf{P}_{\text {comp }}:$ |  |  |  |
| Base Shear, Vu_comp: | 40 | kips |  |
|  |  | kips |  |
|  |  |  |  |
| Moment, $\mathbf{M}_{\mathbf{u}}:$ | 4455 | ft -kips |  |
| Tower Height, $\mathbf{H}:$ | 150 | ft |  |
|  |  |  |  |
| BP Dist. Above Fdn, $\mathbf{b p}_{\text {dist }}:$ | 0 | in |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 382.77 | 40.00 | $\mathbf{1 0 . 5 \%}$ | Pass |
| Bearing Pressure (ksf) | 22.50 | 2.14 | $\mathbf{9 . 5 \%}$ | Pass |
| Overturning (kip*ft) | 9475.38 | 4775.00 | $\mathbf{5 0 . 4 \%}$ | Pass |
| Pier Flexure (Comp.) (kip*ft) | 8998.47 | 4655.00 | $\mathbf{5 1 . 7 \%}$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 35992.10 | 95.24 | $\mathbf{0 . 3 \%}$ | Pass |
| Pad Flexure (kip*f) | 8139.63 | 1585.81 | $\mathbf{1 9 . 5 \%}$ | Pass |
| Pad Shear - 1-way (kips) | 1051.30 | 226.69 | $\mathbf{2 1 . 6 \%}$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.201 | 0.039 | $\mathbf{1 9 . 6 \%}$ | Pass |
| Flexural 2-way (Comp) (kip*f) | 9891.57 | 2793.00 | $\mathbf{2 8 . 2} \%$ | Pass |


| Pier Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Pier Shape: | Circular |  |  |
| Pier Diameter, dpier: | 8 | ft |  |
| Ext. Above Grade, E: | 0.5 | ft |  |
| Pier Rebar Size, Sc: | 10 |  |  |
| Pier Rebar Quantity, mc: | 38 |  |  |
| Pier Tie/Spiral Size, St: | 5 |  |  |
| Pier Tie/Spiral Quantity, mt: | 8 |  |  |
| Pier Reinforcement Type: | Tie |  |  |
| Pier Clear Cover, $\mathbf{c} \mathbf{c}_{\text {pier: }}:$ | 3 | in |  |

2-way (Comp) (kip 1 )

| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 7.5 | ft |
| Pad Width, $\mathbf{W}_{1}:$ | 28 | ft |
| Pad Thickness, T: | 3 | ft |
| Pad Rebar Size (Bottom dir. 2), $\mathbf{S p}_{\mathbf{2}}:$ | 10 |  |
| Pad Rebar Quantity (Bottom dir. 2), $\mathbf{m p}_{\mathbf{2}}:$ | 48 |  |
| Pad Clear Cover, $\mathbf{c c}_{\text {pad }}:$ | 3 | in |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 5 | ksi |
| Dry Concrete Density, ठc: | 150 | pcf |


| Soil Properties |  |  |  |  |
| ---: | :---: | :--- | :---: | :---: |
| Total Soil Unit Weight, $\mathbf{y}$ | 105 | pcf |  |  |
| Ultimate Gross Bearing, Qult: | 30.000 | ksf |  |  |
| Cohesion, $\mathbf{C u}:$ |  | ksf |  |  |
| Friction Angle, $\boldsymbol{\phi}:$ | 38 | degrees |  |  |
| SPT Blow Count, $\mathbf{N}_{\text {blows }}:$ |  |  |  |  |
| Base Friction, $\boldsymbol{\mu}:$ | 0.4 |  |  |  |
| Neglected Depth, $\mathbf{N}:$ | 4.00 | ft |  |  |
| Foundation Bearing on Rock? | No |  |  |  |
| Groundwater Depth, gw: | $\mathrm{N} / \mathrm{A}$ | ft |  |  |


| $\begin{gathered} \text { BU: } \\ \text { WO: } \\ \text { Order: } \end{gathered}$ |  | Structure: <br> Rev: | A |
| :---: | :---: | :---: | :---: |
|  | US-CT-2018 |  |  |
|  |  |  |  |
|  |  |  |  |
| Location |  |  |  |
| Lat: $\begin{aligned} & \text { Decimal Degrees } \\ & \text { Long: } \\ &\end{aligned}$ | Deg | Min | Sec |
|  |  |  |  |
|  |  |  |  |
| Code and Site Parameters |  |  |  |
| Seismic Design Code: <br> Site Soil: <br> Risk Category: | TIA-222-H | Default |  |
|  | D (Default) |  |  |
|  | 11 |  |  |
| USGS Seismic Reference | $0.2020$ |  |  |
|  |  |  |  |
|  | 0.0560 |  |  |
|  | 6 |  |  |
| Seismic Design Category Determination |  |  |  |
| Importance Factor, $\mathrm{I}_{\mathrm{e}}$ : | 1 |  |  |
| Acceleration-based site coefficient, $\mathrm{F}_{\mathrm{a}}$ : | 1.6000 |  |  |
| Velocity-based site coefficient, $\mathrm{F}_{\mathrm{v}}$ : | 2.4000 |  |  |
| Design spectral response acceleration short period, $\mathrm{S}_{\mathrm{DS}}$ : <br> Design spectral response acceleration 1 s period, $\mathrm{S}_{\mathrm{D} 1}$ : | 0.2155 |  |  |
|  | 0.0896 |  |  |
| $\begin{aligned} & \text { Seismic Design Category Based on } \mathrm{S}_{\mathrm{DS}}: \\ & \text { Seismic Design Category Based on } \mathrm{S}_{\mathrm{D} 1}: \\ & \text { Seismic Design Category Based on } \mathrm{S}_{1}: \end{aligned}$ | B |  |  |
|  | B |  |  |
|  | N/A |  |  |
| Controlling Seismic Design Category: | B |  |  |


| BU: | US-CT-2018 |
| ---: | :--- |
| WO: |  |
| Otructure: |  |
| Order: | $\square$ |



## Address:

No Address at This Location

## ASCE 7 Hazards Report

## Wind

## Results:

| Wind Speed: | 119 Vmph |
| :--- | :--- |
| 10 -year MRI | 75 Vmph |
| 25 -year MRI | 84 Vmph |
| 50 -year MRI | 90 Vmph |
| 100 -year MRI | 98 Vmph |

Data Source:
Date Accessed:

Standard: ASCE/SEI 7-16 Elevation: 310.29 ft (NAVD 88)
Risk Category: II
Soil Class: D - Default (see
Section 11.4.3)

Latitude: 41.660792
Longitude: -72.574097


Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2. Glazed openings need not be protected against wind-borne debris.

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## Seismic

## Site Soil Class:

D - Default (see Section 11.4.3)
Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.202 | $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.089 |
| :--- | :--- | :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.056 | $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 | $\mathrm{PGA}:$ | 0.111 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 | $\mathrm{PGA}_{\mathrm{M}}:$ | 0.175 |
| $\mathrm{~S}_{\mathrm{MS}}:$ | 0.323 | $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.578 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.133 | $\mathrm{I}_{\mathrm{e}}:$ | 1 |
| $\mathrm{~S}_{\mathrm{DS}}:$ | 0.216 | $\mathrm{C}_{\mathrm{V}}:$ | 0.704 |

Seismic Design Category
B





Data Accessed:
Date Source:

Wed May 192021
USGS Seismic Design Maps based on ASCE/SEI 7-16 and ASCE/SEI 7-16 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-16 Ch. 21 are available from USGS.

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Ice

Results:

Ice Thickness:
Concurrent Temperature:
Gust Speed:
Data Source:
Date Accessed:
1.50 in .

15 F
50 mph
Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8
Wed May 192021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 500 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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## Attachment 2: Collocation Application

COLOCATION APPLICATION
US-CT-5018
Vertical Bridge REIT, LLC. 750 Park of Commerce Drive

## SUMMARY

## PRIMARY INFO

Application \#: P-006914
Application Version: 2 (Submitted: 3/3/2021 10:12:00 PM)
Application Type: Broadband
Application Name: DISH Wireless BOBDL00104A
Lease Type: New Lease

## Description:

Dish proposes to place 3 antennas, 6 RRUs, 1 junction box(s), and 1 cable(s) at the 125 foot RAD. Dish will require a $5^{\prime} \times 7^{\prime}$ lease area for ground equipment

VERTICAL BRIDGE SITE INFO
VB Site \#:
VB Site Name:

Latitude: $\quad 41.66079166$
Longitude: -72.57409722
Structure Type: Monopole
Structure Height:
152.1600

Site Address: 63 Woodland St -
Glastonbury, CT 06073

## VERTICAL BRIDGE DEAL TEAM

RLM: Floyd Jenkins FJenkins@verticalbridge.com (301) 667-0069

RLS: Sam Bowden
SBowden@verticalbridge.com

ROM:Joe Bascelli
JBascelli@verticalbridge.com (484) 288-9586

## TENANT LEGAL INFO

| Tenant Legal Name: | DISH Wireless L.L.C. |
| :--- | :--- |
| State of Registration: | Colorado |
| Type of Entity: | LLC |
| Carrier NOC \#: | 2039274317 |
| Tenant Site \#: | BOBDL00104A |
| Tenant Site Name: | BOBDL00104A |

## APPLICANT

| Name: | Mai Conaway |
| :--- | :--- |
| Address | 1053 Farmington Avenue |

Farmington, CT 06032
Phone Number:: (410) 409-3822
Email Address: mai@northeastsitesolutions.com

## FINAL LEASED RIGHTS CONFIGURATION TOTALS

This is a summary of your remaining existing equipment plus the new equipment.

## FINAL EQUIPMENT

| Qty | Equipment Type |
| :--- | :--- |
| 1 | Junction Box |
| 3 | Panel |
| 6 | RRU |

## FINAL LINES

| Qty | Line Type |
| :--- | :--- |
| 1 | Hybrid |

## FREQUENCY \& TECHNOLOGY INFO

| Type of Technology: | Broadband Wireless |
| ---: | :--- |
| Is TX Frequency Licensed: | Yes |
| TX Frequency: | 82.1884683 |
| Is RX Frequency Licensed: | Yes |
| RX Frequency: | 9085.919815 |

## MOUNT \& STRUCTURAL ANALYSIS

## MOUNT ANALYSIS

Provided by Tenant: No
To Be Run by VB: Yes
Include Mount Mapping: Yes

## STRUCTURAL HARD COPIES

```
Required: No
```

Number of Hard Copies

## CONTACTS

INVOICE CONTACT

| Attention To | Name | Address | Phone Number 1 | Phone Number 2 | Email 1 | Email 2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Real Estate | Jeanne Cottrell | 5701 South Sante <br> Fe Blvd <br> Littleton, CO <br> 80120 | $(203) 927-4317$ |  | jean.cottrell@dish <br> .$c o m$ |  |


| PO CONTACT |  |  |
| :--- | :--- | :--- |
| Name | Phone Number | Email |
| Jeanne Cottrell | $(203) 927-4317$ | jean.cottrell@dish.com |

## LEASING CONTACT

| Name | Phone Number | Email |
| :--- | :--- | :--- |
| Mai Conaway | $(410) 409-3822$ | mai@northeastsitesolutions.com |


| RF CONTACT |  |  |
| :--- | :--- | :--- |
| Name | Phone Number | Email |
| Jared Robinson | $(978) 855-5870$ | jared.robinson@dish.com |

## TENANT CONSTRUCTION MANAGER CONTACT

| Name | Phone Number | Email |
| :--- | :--- | :--- |
| Javier Soto | $(617) 839-6514$ | javier.soto@dish.com |

## LINE \& EQUIPMENT

| NEW LINE(S) |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| Qty | Line Type | Line Size(in.) | Line Location | Comments |  |  |
| 1 | Hybrid | 1.6 | Interior |  |  |  |


| NEW EQUIPMENT |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Qty | Equipment <br> Type | RAD <br> Height | Mount (H') | Mount Type | Manufacturer | Model <br> Number | Dimensions <br> (H"xW"xD") | Weight <br> (Lbs.) | Azimuth | Comments <br> 3 |
| Panel | 125.00 | 125.00 | Platform | JMA | MX08F <br> RO665- <br> $20 \_V 0 F$ | $72.00 \times$ <br> $20.00 \times 8.00$ | 54.00 | $0,120,24$ <br> 0 |  |  |
| 1 | Junction <br> Box | 125.00 | 125.00 | Platform | Raycap | RDIDC- <br> $9181-P F$ <br> -48 | $16.00 \times$ <br> $14.00 \times 8.00$ | 21.85 | na |  |
| 6 | RRU | 125.00 | 125.00 | Platform | Fujitsu | TA0802 <br> $5-B 605$ | $15.75 \times$ <br> $14.96 \times 9.06$ | 74.95 | 0,120, <br> 240 |  |


| NEW EQUIPMENT CABINET(S) |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| Quantity of Cabinets | Cabinet Dimensions (H x W x D) | Manufacturer | Comments |  |  |  |
| 1 | $32.00 \times 32.00 \times 74.00$ | Charles(Amphenol) -H/EX |  |  |  |  |

## ADDITIONAL SITE REQUIREMENTS

## GROUND \& INTERIOR SPACE REQUIREMENTS

| Requirement <br> Type | Total Lease Area <br> $(\mathrm{Lx}$ W) | Cabinet <br> Required | Cabinet Area (L x <br> W) | Shelter Required | Shelter Pad (L x <br> W) | Comments |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| New | $5.00 \times 7.00$ | No | x |  | x |  |

## GENERATOR REQUIREMENTS

| Requirement <br> Type | Fuel Type | Kilowatt Size | Pad Dimensions <br> $(L \times$ D $)$ | Generator <br> Manufacturer | Fuel Tank <br> Manufacturer | Comments |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Not Required |  |  | x |  |  |  |

## AC POWER REQUIREMENTS

| Meter Type | Additional Details | Comments |
| :--- | :--- | :--- |
| New Tenant Meter |  |  |


| BACKHAUL REQUIREMENTS |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: |
| Requirement Type | Cable Type | Number Of Points Of <br> Entry | Riser Size (Inches) | Comments |  |
| New | Fiber | 1 |  |  |  |

## Exhibit E

## Mount Analysis

FROM ZERO TO INFINIGY

## Mount Analysis Report

July 30, 2021

| Dish Wireless Site Number | BOBDL00104A |
| :--- | :--- |
| Infinigy Job Number | 2039-Z5555C |
| Client | Crown Castle |
| Carrier | Dish Wireless |
|  | 63 Woodland Street, |
| Site Location | Glastonbury, CT 06073 |
|  | 41.6608 N NAD83 |
|  | 72.5741 W NAD83 |
| Mount Centerline EL. | 125 ft |
| Mount Classification | Platform |
| Structural Usage Ratio | $\mathbf{6 6 \%}$ |
| Overall Result | Pass |

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA and ASCE code requirements. The proposed platform for the proposed carrier is therefore deemed adequate to support the final loading configuration as listed in this report.


Dmitriy Albul, P.E.
Engineering Consultant to Infinigy

## Contents

Introduction ..... 3
Supporting Documentation ..... 3
Analysis Code Requirements ..... 3
Conclusion. ..... 3
Final Configuration Loading ..... 4
Structure Usages ..... 4
Assumptions and Limitations ..... 4
Calculations Appended

## Introduction

Infinigy Engineering has been requested to perform a mount analysis of proposed antenna mount from the Dish Wireless equipment. All supporting documents have been obtained from the client and are assumed to be accurate and applicable to this site. The mount was analyzed using RISA3D Version 19.0.3 analysis software.

## Supporting Documentation

| Platform Drawings | SiteProl Assembly Drawings No. SNP8HR-3XX |
| :--- | :--- |
| Construction Drawings | Infinigy Engineering PLLC, Job No. 2039-Z5555C, dated <br> June 7, 2021 |
| RF Design Sheet | Dish Wireless, dated February 15, 2021 |

## Analysis Code Requirements

| Wind Speed | 125 mph (3-second Gust, Vult.) |
| :--- | :--- |
| Wind Speed w/ ice | 50 mph (3-Second Gust) w/ " ice |
| TIA Revision | ANSI/TIA-222-G |
| TIA Revision | 2018 Connecticut Building Code (2015 IBC) |
| Structure Class | II |
| Exposure Category | C |
| Topographic Method | Method 2 |
| Topographic Category | 1 |
| Spectral Response | Ss $=0.181, \mathrm{~S}_{1}=0.064$ |
| Site Class | $\mathrm{D}-$ Stiff Soil (Assumed) |
| HMSL | 310.29 ft. |

## Conclusion

Upon reviewing the results of this analysis, it is our opinion that the structure meets the specified TIA code requirements. The proposed platform is therefore deemed adequate to support the final loading configuration as listed in this report.

If you have any questions, require additional information, or actual conditions differ from those as detailed in this report please contact me via the information below:

Dmitriy Albul, P.E.
Professional Engineer | Engineering Consultant to Infinigy
1033 Watervliet Shaker Road, Albany, NY 12205
(O) (518) 690-0790 | (M) (518) 699-4428
www.infinigy.com

## Final Configuration Loading

| $\begin{array}{\|c} \hline \text { Mount } \\ \text { CL } \\ \text { (ft) } \\ \hline \end{array}$ | Rad. HT <br> (ft) | Vert. O/S <br> (ft) | Horiz. O/S <br> (ft)* | Qty | Appurtenance | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 125.0 | 125.0 | ( | 4 | 3 | JMA MX08FRO665-20 | Dish <br> Wireless |
|  |  |  | 4 | 3 | Fujitsu TA08025-B605 |  |
|  |  |  | 4 | 3 | Fujitsu TA08025-B604 |  |
|  |  |  | - | 1 | Raycap RDIDC-9181-PF-48 |  |

## Structure Usages

| Plates | $66 \%$ | Pass |
| :---: | :--- | :--- |
| Cross Arms | $55 \%$ | Pass |
| Mount Pipes | $52 \%$ | Pass |
| Arms | $40 \%$ | Pass |
| Connections | $33 \%$ | Pass |
| Handrails | $22 \%$ | Pass |
| Frame Rails | $18 \%$ | Pass |
| Rating | $\underline{\mathbf{6 6 \%}} \mathbf{0}$ | Pass |

## Assumptions and Limitations

Our structural calculations are completed assuming all information provided to Infinigy Engineering is accurate and applicable to this site. For the purposes of calculations, we assume an overall structure condition of "like new" and all members and connections to be free of corrosion and/or structural defects. The structure owner and/or contractor shall verify the structure's condition prior to installation of any proposed equipment. If actual conditions differ from those described in this report Infinigy Engineering should be notified immediately to complete a revised evaluation.

Our evaluation is completed using standard TIA, AISC, ACI, and ASCE methods and procedures. Our structural results are proprietary and should not be used by others as their own. Infinigy Engineering is not responsible for decisions made by others that are or are not based on our supplied assumptions and conclusions.

This report is an evaluation of the proposed carriers mount structure only and does not reflect adequacy of the existing tower, other mounts, or coax mounting attachments. These elements are assumed to be adequate for the purposes of this analysis and are assumed to have been installed per their manufacturer requirements.

## INFINIGY8

FROM ZERO TO INFINIGY


| the solutions are endless |
| :--- |
| Date: 7/30/2021 <br> Site Name: BOBDLOO104A <br> Project Engineer: DVA <br> Project No: 2039--25555C <br> Customer: Northeast Site Solutions <br> Carrier: Dish Wireless |
| Building Code: 2015 <br> ASCE Standard: ASCE 7-10 <br> TIA Standard: G- <br> Mount Type: Platform <br> Mount Centerline: 125 <br> Superstructure Height: 150 <br> Structure Type: Tower |



| Factors |  |  |
| :---: | :---: | :---: |
| Gh: | 1.000 |  |
| $K_{z \text { min }}$ : | 0.850 |  |
| $K_{z}$ : | 1.326 |  |
| $K_{d}$ : | 0.950 |  |
| $K_{z t}$ : | 1.000 |  |
|  |  |  |
| Ka: | 0.900 |  |
|  |  |  |
| I wind: | 1.000 |  |
| lice: | 1.000 |  |
| $q_{z}$ : | 30.24 | psf |
| Surface Wind Pressure: | 0.00 | psf |


| Run Seismic? Yes <br> Site Soil: (Defautt) <br> Short-Period Accel. (Ss): 0.1800 <br> 1-Second Accel. (S1): 0.0630 <br> Short-Period Design (SDS): 0.1920 <br> 1-Second Design (SD1): 0.1010 <br> Short-Period Coeff. (Fa): 1.6000 <br> 1-Second Coeff. (Fv): 2.4000 <br> Cs 0.0960 <br> Cs min 0.0300 <br> Amplification Factor (ap): 1.00 <br> Response Mod. (Rp): 2.50 <br> Overstrength (Ro): 1.00 <br>   <br> Service Wind: 30.0 <br> Lm (man live load) ) 500.0 <br> Lv (man live load) $=$ 250.0 |
| :--- |

PLAN VIEW

Table 1. Equipment Specifications and Wind Pressure

| Manufacturer | Model | Elevation | Pipe Label | Weight (lb) | Height (in) | Width (in) | Depth (in) | $E P A_{N}$ | $E P A_{\text {T }}$ | $E P A_{N w / i c e}$ | $E P A_{\text {T w/ ice }}$ | $\mathrm{q}_{2}$ : | $q_{\text {zice: }}$ | $q_{\text {zlive }}$ : |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| JMA | MX08FRO665-20 | 125 | 4, 74, 42 | 54.00 | 72 | 20 | 8 | 8.01 | 3.21 | 9.08 | 4.15 | 30.24 | 8.07 | 2.90 |
| Fujitsu | TA08025-B605 | 125 | 4, 74, 42 | 74.90 | 14.9 | 15.7 | 9 | 1.84 | 1.08 | 3.10 | 2.11 | 30.24 | 8.07 | 2.90 |
| Fujitsu | TA08025-B604 | 125 | 4, 74, 42 | 63.90 | 14.9 | 15.7 | 7.8 | 1.84 | 0.95 | 3.10 | 1.94 | 30.24 | 8.07 | 2.90 |
| Raycap | RDIDC-9181-PF-48 | 125 | 125 | 21.82 | 18.98 | 14.39 | 8.15 | 2.18 | 1.28 | 3.55 | 2.44 | 30.24 | 8.07 | 2.90 |


| Manufacturer | Model | Wind Load ( $F_{\text {A }}$ ), lb |  | Wind Load lce Case ( $F_{\text {A }}$ ) , Ib |  |  | Wind Load Service Case ( $F_{\text {A }}$ ), |  | Seismic Load, |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| JMA | MX08FRO665-20 | 218 | 87 | 66 | 30 | 408 | 21 | 8 | 5.2 |
| Fujitsu | TA08025-B605 | 50 | 29 | 23 | 15 | 72 | 5 |  | 7.2 |
| Fujitsu | TA08025-B604 | 50 | 26 | 23 | 14 | 70 | 5 | 2 | 6.1 |
| Raycap | RDIDC-9181-PF-48 | 59 | 35 | 26 | 18 | 85 | 6 | 3 | 2.1 |


| Member Name | Member Shape | $\begin{gathered} \text { Wind load } \\ \text { (plf) } \end{gathered}$ | Wind Load Ice (plf) | $\begin{aligned} & \text { Weight Ice } \\ & \text { (plf) } \end{aligned}$ | Bending Check | Shear Check | Total Capacity | Controlling Capacity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Arm | HSS4x4x4 | 20.16 | 5.38 | 2.04 | 40\% | 18\% | 40\% | 66\% |
| Arm 2 | HSS4.5x4.5x | 22.68 | 6.05 | 2.16 | 7\% | 16\% | 16\% |  |
| Cross Arm | L4×4x4 | 20.16 | 5.38 | 2.04 | 55\% | 12\% | 55\% |  |
| Frame Rail | PIPE_3.0 | 10.59 | 2.82 | 1.92 | 12\% | 18\% | 18\% |  |
| Handrail | PIPE_2.5 | 8.71 | 2.32 | 1.77 | 15\% | 22\% | 22\% |  |
| Mount Pipe | PIPE_2.0 | 7.20 | 1.92 | 1.65 | 52\% | 22\% | 52\% |  |
| Plate | 6"x0.375" Plate | 30.24 | 8.07 | 2.51 | 61\% | 66\% | 66\% |  |
| Angle | L3 $\times 3 \times 3$ | 15.12 | 4.03 | 1.80 | 34\% | 4\% | 34\% |  |






| Model Settings |
| :--- |
| Solution |
| $\quad$ Members |
| Number of Reported Sections |
| Number of Internal Sections |
| Member Area Load Mesh Size $\left(\mathrm{in}^{2}\right)$ |
| Consider Shear Deformation |
| Consider Torsional Warping |

Wall Panels

| Approximate Mesh Size (in) | 12 |
| :--- | :--- |
| Transfer Forces Between Intersecting Wood Walls | Yes |
| Increase Wood Wall Nailing Capacity for Wind Loads | Yes |
| Include P-Delta for Walls | Yes |
| Optimize Masonry and Wood Walls | Yes |
| Maximum Number of Iterations | 3 |

Processor Core Utilization

| Single | No |
| :--- | :--- |
| Multiple (Optimum) | Yes |
| Maximum | No |

## Axis

Vertical Global Axis

| Global Axis corresponding to vertical direction | Y |
| :--- | :--- |
| Convert Existing Data | Yes |

Default Member Orientation

| Default Global Plane for z-axis | XZ |
| :--- | :--- |

Plate Axis

| Plate Local Axis Orientation | Nodal |
| :--- | :--- |

Codes

| Hot Rolled Steel | AISC 14th (360-10): LRFD |
| :--- | :--- |
| Stiffness Adjustment | Yes (Iterative) |
| Notional Annex | None |
| Connections | AISC 14th (360-10): LRFD |
| Cold Formed Steel | AISI S100-12: LRFD |
| Stiffness Adjustment | Yes (Iterative) |
| Wood | AWC NDS-12: ASD |
| Temperature | < 100F |
| Concrete | ACI 318-11 |
| Masonry | ACI 530-11: Strength |
| Aluminum | AAADM1-10: LRFD |
| Structure Type | Building |
| Stiffness Adjustment | Yes (Iterative) |
| Stainless | AISC 14th (360-10): LRFD |
| Stiffness Adjustment | Yes (Iterative) |

## Concrete

Column Design

| Analysis Methodology | Exact Integration Method |
| :--- | :--- |
| Parme Beta Factor | 0.65 |


| Compression Stress Block | Rectangular Stress Block |
| :--- | :--- |
| Analyze using Cracked Sections | Yes |
| Leave room for horizontal rebar splices (2*d bar spacing) | No |

Model Settings (Continued)

| List forces which were ignored for design in the Detail Report | Yes |
| :--- | :--- |

## Rebar

| Column Min Steel | 1 |
| :--- | :--- |
| Column Max Steel | 8 |
| Rebar Material Spec | ASTM A615 |
| Warn if beam-column framing arrangement is not understood | No |

Shear Reinforcement

| Number of Shear Regions | 4 |
| :--- | :--- |
| Region 2 \& 3 Spacing Increase Increment (in) | 4 |

## Seismic

RISA-3D Seismic Load Options

| Code | ASCE 7-10 |
| :--- | :--- |
| Risk Category | I or II |
| Drift Cat | Other |
| Base Elevation (ft) |  |
| Include the weight of the structure in base shear calcs | Yes |

Site Parameters

| $\mathrm{S}_{1}(\mathrm{~g})$ | 1 |
| :--- | :--- |
| $\mathrm{SD}(\mathrm{g})$ | 1 |
| $\mathrm{SD}(\mathrm{g})$ | 1 |
| $\mathrm{~T}_{\mathrm{L}}(\mathrm{sec})$ | 5 |

## Structure Characteristics

| $\mathrm{T} Z(\mathrm{sec})$ |  |
| :--- | :--- |
| $\mathrm{T} X(\mathrm{sec})$ |  |
| $\mathrm{C}_{\mathrm{t}} \mathrm{X}$ | 0.02 |
| $\mathrm{C}_{\mathbf{t}}$ Exp. $Z$ | 0.75 |
| $\mathrm{C}_{\mathbf{t}}$ Exp. X | 0.75 |
| $\mathrm{R} Z$ | 3 |
| $\mathrm{R} X$ | 3 |
| $\Omega_{0} Z$ | 1 |
| $\Omega_{0} X$ | 1 |
| $\mathrm{C}_{\mathrm{d}} Z$ | 4 |
| $\mathrm{C}_{\mathrm{d}} X$ | 4 |
| $\rho Z$ | 1 |
| $\rho X$ | 1 |

$\qquad$
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Member Primary Data

|  | Label | I Node | J Node | Rotate(deg) | Section/Shape | Type | Design List | Material | Design Rule |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  | Arm | Beam | Tube | A500 Gr.B Rect | Typical |
| 2 | M2 | N5 | N6 |  | Frame Rail | Beam | Pipe | A53 Gr.B | Typical |
| 3 | M3 | N7 | N8 |  | Handrail | HBrace | Pipe | A53 Gr.B | Typical |
| 4 | M4 | N10 | N11 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 5 | M5 | N4 | N3 |  | Arm 2 | Beam | Tube | A500 Gr.B Rect | Typical |
| 6 | M6 | N15 | N35 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 7 | M7 | N33 | N13 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 8 | M8 | N12 | N34 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 9 | M9 | N36 | N14 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 10 | M10 | N18 | N20 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 11 | M11 | N17 | N19 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 12 | M12 | N21 | N22 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 13 | M13 | N23 | N24 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 14 | M14 | N28 | N25 | 90 | Angle | HBrace | Single Angle | A36 Gr. 36 | Typical |
| 15 | M15 | N26 | N27 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 16 | M16 | N29 | N30 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 17 | M17 | N31 | N9 |  | RIGID | None | None | RIGID | Typical |
| 18 | M18 | N32 | N16 |  | RIGID | None | None | RIGID | Typical |
| 19 | M19 | N4 | N35 |  | RIGID | None | None | RIGID | Typical |
| 20 | M20 | N4 | N33 |  | RIGID | None | None | RIGID | Typical |
| 21 | M21 | N3 | N34 |  | RIGID | None | None | RIGID | Typical |
| 22 | M22 | N36 | N3 |  | RIGID | None | None | RIGID | Typical |
| 23 | M23 | N19 | N37 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 24 | M24 | N22 | N38 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 25 | M25 | N39 | N41 |  | RIGID | None | None | RIGID | Typical |
| 26 | M26 | N40 | N42 |  | RIGID | None | None | RIGID | Typical |
| 27 | M27 | N27 | N43 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 28 | M28 | N44 | N45 |  | RIGID | None | None | RIGID | Typical |
| 29 | M29 | N20 | N46 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 30 | M30 | N24 | N47 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 31 | M31 | N48 | N50 |  | RIGID | None | None | RIGID | Typical |
| 32 | M32 | N49 | N51 |  | RIGID | None | None | RIGID | Typical |
| 33 | M33 | N30 | N52 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 34 | M34 | N53 | N54 |  | RIGID | None | None | RIGID | Typical |
| 35 | M35 | N56 | N57 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 36 | M36 | N59 | N55 |  | RIGID | None | None | RIGID | Typical |
| 37 | M37 | N60 | N58 |  | RIGID | None | None | RIGID | Typical |
| 38 | M38 | N62 | N63 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 39 | M39 | N65 | N61 |  | RIGID | None | None | RIGID | Typical |
| 40 | M40 | N66 | N64 |  | RIGID | None | None | RIGID | Typical |
| 41 | M41 | N67 | N68 |  | Arm | Beam | Tube | A500 Gr.B Rect | Typical |
| 42 | M42 | N72 | N73 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 43 | M43 | N70 | N69 |  | Arm 2 | Beam | Tube | A500 Gr.B Rect | Typical |
| 44 | M44 | N77 | N97 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 45 | M45 | N95 | N75 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 46 | M46 | N74 | N96 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 47 | M47 | N98 | N76 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 48 | M48 | N80 | N82 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 49 | M49 | N79 | N81 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 50 | M50 | N83 | N84 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 51 | M51 | N85 | N86 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 52 | M52 | N90 | N87 | 90 | Angle | HBrace | Single Angle | A36 Gr. 36 | Typical |
| 53 | M53 | N88 | N89 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 54 | M54 | N91 | N92 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 55 | M55 | N93 | N71 |  | RIGID | None | None | RIGID | Typical |
| 56 | M56 | N94 | N78 |  | RIGID | None | None | RIGID | Typical |
| 57 | M57 | N70 | N97 |  | RIGID | None | None | RIGID | Typical |
| 58 | M58 | N70 | N95 |  | RIGID | None | None | RIGID | Typical |

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Member Primary Data (Continued)

|  | Label | I Node | J Node | Rotate(deg) | Section/Shape | Type | Design List | Material | Design Rule |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 59 | M59 | N69 | N96 |  | RIGID | None | None | RIGID | Typical |
| 60 | M60 | N98 | N69 |  | RIGID | None | None | RIGID | Typical |
| 61 | M61 | N81 | N99 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 62 | M62 | N84 | N100 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 63 | M63 | N101 | N103 |  | RIGID | None | None | RIGID | Typical |
| 64 | M64 | N102 | N104 |  | RIGID | None | None | RIGID | Typical |
| 65 | M65 | N89 | N105 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 66 | M66 | N106 | N107 |  | RIGID | None | None | RIGID | Typical |
| 67 | M67 | N82 | N108 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 68 | M68 | N86 | N109 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 69 | M69 | N110 | N112 |  | RIGID | None | None | RIGID | Typical |
| 70 | M70 | N111 | N113 |  | RIGID | None | None | RIGID | Typical |
| 71 | M71 | N92 | N114 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 72 | M72 | N115 | N116 |  | RIGID | None | None | RIGID | Typical |
| 73 | M73 | N117 | N118 |  | Arm | Beam | Tube | A500 Gr.B Rect | Typical |
| 74 | M74 | N122 | N123 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 75 | M75 | N120 | N119 |  | Arm 2 | Beam | Tube | A500 Gr.B Rect | Typical |
| 76 | M76 | N127 | N147 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 77 | M77 | N145 | N125 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 78 | M78 | N124 | N146 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 79 | M79 | N148 | N126 | 90 | Cross Arm | Beam | Single Angle | A36 Gr. 36 | Typical |
| 80 | M80 | N130 | N132 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 81 | M81 | N129 | N131 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 82 | M82 | N133 | N134 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 83 | M83 | N135 | N136 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 84 | M84 | N140 | N137 | 90 | Angle | HBrace | Single Angle | A36 Gr. 36 | Typical |
| 85 | M85 | N138 | N139 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 86 | M86 | N141 | N142 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 87 | M87 | N143 | N121 |  | RIGID | None | None | RIGID | Typical |
| 88 | M88 | N144 | N128 |  | RIGID | None | None | RIGID | Typical |
| 89 | M89 | N120 | N147 |  | RIGID | None | None | RIGID | Typical |
| 90 | M90 | N120 | N145 |  | RIGID | None | None | RIGID | Typical |
| 91 | M91 | N119 | N146 |  | RIGID | None | None | RIGID | Typical |
| 92 | M92 | N148 | N119 |  | RIGID | None | None | RIGID | Typical |
| 93 | M93 | N131 | N149 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 94 | M94 | N134 | N150 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 95 | M95 | N151 | N153 |  | RIGID | None | None | RIGID | Typical |
| 96 | M96 | N152 | N154 |  | RIGID | None | None | RIGID | Typical |
| 97 | M97 | N139 | N155 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 98 | M98 | N156 | N157 |  | RIGID | None | None | RIGID | Typical |
| 99 | M99 | N132 | N158 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 100 | M100 | N136 | N159 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 101 | M101 | N160 | N162 |  | RIGID | None | None | RIGID | Typical |
| 102 | M102 | N161 | N163 |  | RIGID | None | None | RIGID | Typical |
| 103 | M103 | N142 | N164 |  | Plate | Beam | BAR | A36 Gr. 36 | Typical |
| 104 | M104 | N165 | N166 |  | RIGID | None | None | RIGID | Typical |
| 105 | M105 | N167 | N168 |  | Frame Rail | Beam | Pipe | A53 Gr.B | Typical |
| 106 | M106 | N169 | N170 |  | Handrail | HBrace | Pipe | A53 Gr.B | Typical |
| 107 | M107 | N172 | N173 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 108 | M108 | N175 | N171 |  | RIGID | None | None | RIGID | Typical |
| 109 | M109 | N176 | N174 |  | RIGID | None | None | RIGID | Typical |
| 110 | M110 | N178 | N179 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 111 | M111 | N181 | N177 |  | RIGID | None | None | RIGID | Typical |
| 112 | M112 | N182 | N180 |  | RIGID | None | None | RIGID | Typical |
| 113 | M113 | N183 | N184 |  | Frame Rail | Beam | Pipe | A53 Gr.B | Typical |
| 114 | M114 | N185 | N186 |  | Handrail | HBrace | Pipe | A53 Gr.B | Typical |
| 115 | M115 | N188 | N189 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 116 | M116 | N191 | N187 |  | RIGID | None | None | RIGID | Typical |

FROM ZERO TO INFINIGY the solutions are endless

Company
Designer Job Number Model Name

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
12:53:50 AM
Checked By : $\qquad$
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Member Primary Data (Continued)

|  | Label | I Node | J Node | Rotate(deg) | Section/Shape | Type | Design List | Material | Design Rule |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 117 | M117 | N192 | N190 |  | RIGID | None | None | RIGID | Typical |
| 118 | M118 | N194 | N195 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |
| 119 | M119 | N197 | N193 |  | RIGID | None | None | RIGID | Typical |
| 120 | M120 | N198 | N196 |  | RIGID | None | None | RIGID | Typical |
| 121 | M121 | N199 | N200 |  | RIGID | None | None | RIGID | Typical |
| 122 | M122 | N201 | N199 |  | RIGID | None | None | RIGID | Typical |
| 123 | M123 | N200 | N202 |  | RIGID | None | None | RIGID | Typical |
| 124 | M124 | N201 | N203 |  | RIGID | None | None | RIGID | Typical |
| 125 | M125 | N204 | N205 |  | Mount Pipe | Column | Pipe | A53 Gr.B | Typical |

Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm. Coeff. [ $1 \mathrm{e}^{50} \mathrm{~F}^{-1}$ ] | Density [ $\left.\mathrm{lb} / \mathrm{ft}^{3}\right]$ | Yield [ksi] | Ry | Fu [ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | 0.3 | 0.65 | 490 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | 0.3 | 0.65 | 490 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 0.3 | 0.65 | 490 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | 0.3 | 0.65 | 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | 0.3 | 0.65 | 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | 0.3 | 0.65 | 490 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 0.3 | 0.65 | 490 | 50 | 1.4 | 65 | 1.3 |

## Basic Load Cases

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Point | Distributed | Area(Member) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Self Weight | DL |  | -1 |  | 20 |  | 3 |
| 2 | Wind Load AZI 0 | WLX |  |  |  | 40 | 258 |  |
| 3 | Wind Load AZI 30 | None |  |  |  | 40 | 258 |  |
| 4 | Wind Load AZI 60 | None |  |  |  | 40 | 258 |  |
| 5 | Wind Load AZI 90 | WLZ |  |  |  | 40 | 258 |  |
| 6 | Wind Load AZI 120 | None |  |  |  | 40 | 258 |  |
| 7 | Wind Load AZI 150 | None |  |  |  | 40 | 258 |  |
| 8 | Wind Load AZI 180 | None |  |  |  | 40 | 258 |  |
| 9 | Wind Load AZI 210 | None |  |  |  | 40 | 258 |  |
| 10 | Wind Load AZI 240 | None |  |  |  | 40 | 258 |  |
| 11 | Wind Load AZI 270 | None |  |  |  | 40 | 258 |  |
| 12 | Wind Load AZI 300 | None |  |  |  | 40 | 258 |  |
| 13 | Wind Load AZI 330 | None |  |  |  | 40 | 258 |  |
| 14 | Ice Weight | OL1 |  |  |  | 20 | 125 | 3 |
| 15 | Ice Wind Load AZI 0 | OL2 |  |  |  | 40 | 258 |  |
| 16 | Ice Wind Load AZI 30 | None |  |  |  | 40 | 258 |  |
| 17 | Ice Wind Load AZI 60 | None |  |  |  | 40 | 258 |  |
| 18 | Ice Wind Load AZI 90 | OL3 |  |  |  | 40 | 258 |  |
| 19 | Ice Wind Load AZI 120 | None |  |  |  | 40 | 258 |  |
| 20 | Ice Wind Load AZI 150 | None |  |  |  | 40 | 258 |  |
| 21 | Ice Wind Load AZI 180 | None |  |  |  | 40 | 258 |  |
| 22 | Ice Wind Load AZI 210 | None |  |  |  | 40 | 258 |  |
| 23 | Ice Wind Load AZI 240 | None |  |  |  | 40 | 258 |  |
| 24 | Ice Wind Load AZI 270 | None |  |  |  | 40 | 258 |  |
| 25 | Ice Wind Load AZI 300 | None |  |  |  | 40 | 258 |  |
| 26 | Ice Wind Load AZI 330 | None |  |  |  | 40 | 258 |  |
| 27 | Seismic Load X | ELX |  |  | -0.096 | 20 |  |  |
| 28 | Seismic Load Z | ELZ | -0.096 |  |  | 20 |  |  |
| 29 | Service Live Loads | LL |  |  |  |  |  |  |
| 30 | Maintenance Load 1 | LL |  |  |  | 1 |  |  |
| 31 | Maintenance Load 2 | LL |  |  |  | 1 |  |  |
| 32 | Maintenance Load 3 | LL |  |  |  | 1 |  |  |
| 33 | Maintenance Load 4 | LL |  |  |  | 1 |  |  |
| 34 | Maintenance Load 5 | LL |  |  |  | 1 |  |  |
| 35 | Maintenance Load 6 | LL |  |  |  | 1 |  |  |

the solutions are endless
Company
Designer Job Number Model Name

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
12:53:50 AM
Checked By :

Basic Load Cases (Continued)

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Point | Distributed | Area(Member) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 36 | Maintenance Load 7 | LL |  |  |  | 1 |  |  |
| 37 | Maintenance Load 8 | LL |  |  |  | 1 |  |  |
| 38 | Maintenance Load 9 | LL |  |  |  | 1 |  |  |
| 39 | Maintenance Load 10 | LL |  |  |  | 1 |  |  |
| 40 | Maintenance Load 11 | LL |  |  |  | 1 |  |  |
| 41 | Maintenance Load 12 | LL |  |  |  | 1 |  |  |
| 42 | Maintenance Load 13 | LL |  |  |  | 1 |  |  |
| 43 | Maintenance Load 14 | LL |  |  |  | 1 |  |  |
| 44 | Maintenance Load 15 | LL |  |  |  |  |  |  |
| 45 | Maintenance Load 16 | LL |  |  |  | 1 |  |  |
| 46 | Maintenance Load 17 | LL |  |  |  | 1 |  |  |
| 47 | Maintenance Load 18 | LL |  |  |  | 1 |  |  |
| 52 | BLC 1 Transient Area Loads | None |  |  |  |  | 141 |  |
| 53 | BLC 14 Transient Area Loads | None |  |  |  |  | 141 |  |

Load Combinations

|  | Description | Solve | PDelta | BLC | Factor | BLC | Factor | BLC | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4DL | Yes | Y | 1 | 1.4 |  |  |  |  |
| 2 | 1.2DL + 1.6WL AZI 0 | Yes | Y | 1 | 1.2 | 2 | 1.6 |  |  |
| 3 | 1.2DL + 1.6WL AZI 30 | Yes | Y | 1 | 1.2 | 3 | 1.6 |  |  |
| 4 | 1.2DL + 1.6WL AZI 60 | Yes | Y | 1 | 1.2 | 4 | 1.6 |  |  |
| 5 | 1.2DL + 1.6WL AZI 90 | Yes | Y | 1 | 1.2 | 5 | 1.6 |  |  |
| 6 | 1.2DL + 1.6WL AZI 120 | Yes | Y | 1 | 1.2 | 6 | 1.6 |  |  |
| 7 | 1.2DL + 1.6WL AZI 150 | Yes | Y | 1 | 1.2 | 7 | 1.6 |  |  |
| 8 | 1.2DL + 1.6WL AZI 180 | Yes | Y | 1 | 1.2 | 8 | 1.6 |  |  |
| 9 | 1.2DL + 1.6WL AZI 210 | Yes | Y | 1 | 1.2 | 9 | 1.6 |  |  |
| 10 | 1.2DL + 1.6WL AZI 240 | Yes | Y | 1 | 1.2 | 10 | 1.6 |  |  |
| 11 | 1.2DL + 1.6WL AZI 270 | Yes | Y | 1 | 1.2 | 11 | 1.6 |  |  |
| 12 | 1.2DL + 1.6WL AZI 300 | Yes | Y | 1 | 1.2 | 12 | 1.6 |  |  |
| 13 | 1.2DL + 1.6WL AZI 330 | Yes | Y | 1 | 1.2 | 13 | 1.6 |  |  |
| 14 | 0.9DL + 1.6WL AZI 0 | Yes | Y | 1 | 0.9 | 2 | 1.6 |  |  |
| 15 | 0.9DL + 1.6WL AZI 30 | Yes | Y | 1 | 0.9 | 3 | 1.6 |  |  |
| 16 | 0.9DL + 1.6WL AZI 60 | Yes | Y | 1 | 0.9 | 4 | 1.6 |  |  |
| 17 | 0.9DL + 1.6WL AZI 90 | Yes | Y | 1 | 0.9 | 5 | 1.6 |  |  |
| 18 | 0.9DL + 1.6WL AZI 120 | Yes | Y | 1 | 0.9 | 6 | 1.6 |  |  |
| 19 | 0.9DL + 1.6WL AZI 150 | Yes | Y | 1 | 0.9 | 7 | 1.6 |  |  |
| 20 | 0.9DL + 1.6WL AZI 180 | Yes | Y | 1 | 0.9 | 8 | 1.6 |  |  |
| 21 | 0.9DL + 1.6WL AZI 210 | Yes | Y | 1 | 0.9 | 9 | 1.6 |  |  |
| 22 | 0.9DL + 1.6WL AZI 240 | Yes | Y | 1 | 0.9 | 10 | 1.6 |  |  |
| 23 | 0.9DL + 1.6WL AZI 270 | Yes | Y | 1 | 0.9 | 11 | 1.6 |  |  |
| 24 | 0.9DL + 1.6WL AZI 300 | Yes | Y | 1 | 0.9 | 12 | 1.6 |  |  |
| 25 | 0.9DL + 1.6WL AZI 330 | Yes | Y | 1 | 0.9 | 13 | 1.6 |  |  |
| 26 | 1.2D + 1.0Di | Yes | Y | 1 | 1.2 | 14 | 1 |  |  |
| 27 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ AZI 0 | Yes | Y | 1 | 1.2 | 14 | 1 | 15 | 1 |
| 28 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ AZI 30 | Yes | Y | 1 | 1.2 | 14 | 1 | 16 | 1 |
| 29 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} \mathrm{AZI} 60$ | Yes | Y | 1 | 1.2 | 14 | 1 | 17 | 1 |
| 30 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ AZI 90 | Yes | Y | 1 | 1.2 | 14 | 1 | 18 | 1 |
| 31 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ AZI 120 | Yes | Y | 1 | 1.2 | 14 | 1 | 19 | 1 |
| 32 | 1.2D + 1.0Di +1.0Wi AZI 150 | Yes | Y | 1 | 1.2 | 14 | 1 | 20 | 1 |
| 33 | 1.2D + 1.0Di +1.0Wi AZI 180 | Yes | Y | 1 | 1.2 | 14 | 1 | 21 | 1 |
| 34 | 1.2D + 1.0Di +1.0Wi AZI 210 | Yes | Y | 1 | 1.2 | 14 | 1 | 22 | 1 |
| 35 | 1.2D + 1.0Di +1.0Wi AZI 240 | Yes | Y | 1 | 1.2 | 14 | 1 | 23 | 1 |
| 36 | 1.2D + 1.0Di +1.0Wi AZI 270 | Yes | Y | 1 | 1.2 | 14 | 1 | 24 | 1 |
| 37 | 1.2D + 1.0Di +1.0Wi AZI 300 | Yes | Y | 1 | 1.2 | 14 | 1 | 25 | 1 |
| 38 | 1.2D + 1.0Di +1.0Wi AZI 330 | Yes | Y | 1 | 1.2 | 14 | 1 | 26 | 1 |
| 39 | (1.2 + 0.2Sds) DL + 1.0E AZI 0 | Yes | Y | 1 | 1.238 | 27 | 1 | 28 |  |
| 40 | (1.2 + 0.2Sds)DL + 1.0E AZI 30 | Yes | Y | 1 | 1.238 | 27 | 0.866 | 28 | 0.5 |
| 41 | (1.2 + 0.2Sds)DL + 1.0E AZI 60 | Yes | Y | 1 | 1.238 | 27 | 0.5 | 28 | 0.866 |

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
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| Description |  | Solve | PDelta | BLC | Factor | BLC | Factor | BLC | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 42 | (1.2 + 0.2Sds)DL + 1.0E AZI 90 | Yes | Y | 1 | 1.238 | 27 |  | 28 | 1 |
| 43 | $(1.2+0.2$ Sds) DL + 1.0E AZI 120 | Yes | Y | 1 | 1.238 | 27 | -0.5 | 28 | 0.866 |
| 44 | (1.2 + 0.2Sds)DL + 1.0E AZI 150 | Yes | Y | 1 | 1.238 | 27 | -0.866 | 28 | 0.5 |
| 45 | (1.2 + 0.2Sds) DL + 1.0E AZI 180 | Yes | Y | 1 | 1.238 | 27 | -1 | 28 |  |
| 46 | (1.2 + 0.2Sds)DL + 1.0E AZI 210 | Yes | Y | 1 | 1.238 | 27 | -0.866 | 28 | -0.5 |
| 47 | (1.2 + 0.2Sds) DL + 1.0E AZI 240 | Yes | Y | 1 | 1.238 | 27 | -0.5 | 28 | -0.866 |
| 48 | (1.2 + 0.2Sds)DL + 1.0E AZI 270 | Yes | Y | 1 | 1.238 | 27 |  | 28 | -1 |
| 49 | $(1.2+0.2$ Sds) DL + 1.0E AZI 300 | Yes | Y | 1 | 1.238 | 27 | 0.5 | 28 | -0.866 |
| 50 | $(1.2+0.2$ Sds) DL + 1.0E AZI 330 | Yes | Y | 1 | 1.238 | 27 | 0.866 | 28 | -0.5 |
| 51 | (0.9-0.2Sds)DL + 1.0E AZI 0 | Yes | Y | 1 | 0.862 | 27 | 1 | 28 |  |
| 52 | (0.9-0.2Sds)DL + 1.0E AZI 30 | Yes | Y | 1 | 0.862 | 27 | 0.866 | 28 | 0.5 |
| 53 | (0.9-0.2Sds)DL + 1.0E AZI 60 | Yes | Y | 1 | 0.862 | 27 | 0.5 | 28 | 0.866 |
| 54 | (0.9-0.2Sds)DL + 1.0E AZI 90 | Yes | Y | 1 | 0.862 | 27 |  | 28 | 1 |
| 55 | (0.9-0.2Sds)DL + 1.0E AZI 120 | Yes | Y | 1 | 0.862 | 27 | -0.5 | 28 | 0.866 |
| 56 | (0.9-0.2Sds)DL + 1.0E AZI 150 | Yes | Y | 1 | 0.862 | 27 | -0.866 | 28 | 0.5 |
| 57 | (0.9-0.2Sds)DL + 1.0E AZI 180 | Yes | Y | 1 | 0.862 | 27 | -1 | 28 |  |
| 58 | (0.9-0.2Sds)DL + 1.0E AZI 210 | Yes | Y | 1 | 0.862 | 27 | -0.866 | 28 | -0.5 |
| 59 | (0.9-0.2Sds)DL + 1.0E AZI 240 | Yes | Y | 1 | 0.862 | 27 | -0.5 | 28 | -0.866 |
| 60 | (0.9-0.2Sds)DL + 1.0E AZI 270 | Yes | Y | 1 | 0.862 | 27 |  | 28 | -1 |
| 61 | (0.9-0.2Sds)DL + 1.0E AZI 300 | Yes | Y | 1 | 0.862 | 27 | 0.5 | 28 | -0.866 |
| 62 | (0.9-0.2Sds)DL + 1.0E AZI 330 | Yes | Y | 1 | 0.862 | 27 | 0.866 | 28 | -0.5 |
| 63 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 0 | Yes | Y | 1 | 1 | 2 | 0.096 | 29 | 1.5 |
| 64 | 1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 30 | Yes | Y | 1 | 1 | 3 | 0.096 | 29 | 1.5 |
| 65 | 1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 60 | Yes | Y | 1 | 1 | 4 | 0.096 | 29 | 1.5 |
| 66 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 90 | Yes | Y | 1 | 1 | 5 | 0.096 | 29 | 1.5 |
| 67 | 1.0DL + 1.5LL + 1.0SWL (30 mph) AZI 120 | Yes | Y | 1 | 1 | 6 | 0.096 | 29 | 1.5 |
| 68 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ (30 mph) AZI 150 | Yes | Y | 1 | 1 | 7 | 0.096 | 29 | 1.5 |
| 69 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1 | 8 | 0.096 | 29 | 1.5 |
| 70 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 210 | Yes | Y | 1 | 1 | 9 | 0.096 | 29 | 1.5 |
| 71 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 240 | Yes | Y | 1 | 1 | 10 | 0.096 | 29 | 1.5 |
| 72 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ (30 mph) AZI 270 | Yes | Y | 1 | 1 | 11 | 0.096 | 29 | 1.5 |
| 73 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1 | 12 | 0.096 | 29 | 1.5 |
| 74 | $1.0 \mathrm{DL}+1.5 \mathrm{LL}+1.0 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1 | 13 | 0.096 | 29 | 1.5 |
| 75 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 0 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 2 | 0.154 |
| 76 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 3 | 0.154 |
| 77 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1$ + 1.6SWL ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 4 | 0.154 |
| 78 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 5 | 0.154 |
| 79 | 1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 6 | 0.154 |
| 80 | 1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 7 | 0.154 |
| 81 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 8 | 0.154 |
| 82 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}$ (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 9 | 0.154 |
| 83 | 1.2DL + 1.5LM1 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 10 | 0.154 |
| 84 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 270 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 11 | 0.154 |
| 85 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 12 | 0.154 |
| 86 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 1+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 34 | 1.5 | 13 | 0.154 |
| 87 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}(30 \mathrm{mph}) \mathrm{AZI} 0$ | Yes | Y | 1 | 1.2 | 35 | 1.5 | 2 | 0.154 |
| 88 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 3 | 0.154 |
| 89 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 4 | 0.154 |
| 90 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 90 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 5 | 0.154 |
| 91 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 6 | 0.154 |
| 92 | 1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 7 | 0.154 |
| 93 | 1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 8 | 0.154 |
| 94 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 9 | 0.154 |
| 95 | 1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 10 | 0.154 |
| 96 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 11 | 0.154 |
| 97 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 2+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 12 | 0.154 |
| 98 | 1.2DL + 1.5LM2 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 35 | 1.5 | 13 | 0.154 |
| 99 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 3+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 0 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 2 | 0.154 |

Company Designer Job Number Model Name

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
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Checked By

| Description |  | Solve | PDelta <br> Y | $\frac{\text { BLC }}{1}$ | $\begin{gathered} \text { Factor } \\ \hline 1.2 \end{gathered}$ | $\frac{\text { BLC }}{36}$ | $\begin{gathered} \text { Factor } \\ \hline 1.5 \end{gathered}$ | $\begin{gathered} \text { BLC } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Factor } \\ \hline 0.154 \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 30 | Yes |  |  |  |  |  |  |  |
| 101 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 3+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 4 | 0.154 |
| 102 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 5 | 0.154 |
| 103 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 6 | 0.154 |
| 104 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 7 | 0.154 |
| 105 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 8 | 0.154 |
| 106 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 9 | 0.154 |
| 107 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 10 | 0.154 |
| 108 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 11 | 0.154 |
| 109 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 3+1.6 \mathrm{SWL}$ (30 mph) AZI 300 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 12 | 0.154 |
| 110 | 1.2DL + 1.5LM3 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 36 | 1.5 | 13 | 0.154 |
| 111 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 4+1.6 \mathrm{SWL}(30 \mathrm{mph}) \mathrm{AZI} 0$ | Yes | Y | 1 | 1.2 | 37 | 1.5 | 2 | 0.154 |
| 112 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 4+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 3 | 0.154 |
| 113 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 4+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 4 | 0.154 |
| 114 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 4+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 90 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 5 | 0.154 |
| 115 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 6 | 0.154 |
| 116 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 7 | 0.154 |
| 117 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 8 | 0.154 |
| 118 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 9 | 0.154 |
| 119 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 10 | 0.154 |
| 120 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 11 | 0.154 |
| 121 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 4+1.6 \mathrm{SWL}$ (30 mph) AZI 300 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 12 | 0.154 |
| 122 | 1.2DL + 1.5LM4 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 37 | 1.5 | 13 | 0.154 |
| 123 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 5+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 0 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 2 | 0.154 |
| 124 | 1.2DL + 1.5LM5 + 1.6SWL ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 3 | 0.154 |
| 125 | 1.2DL + 1.5LM5 + 1.6SWL ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 4 | 0.154 |
| 126 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 5 | 0.154 |
| 127 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 6 | 0.154 |
| 128 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 7 | 0.154 |
| 129 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 8 | 0.154 |
| 130 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 9 | 0.154 |
| 131 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 10 | 0.154 |
| 132 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 11 | 0.154 |
| 133 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 300 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 12 | 0.154 |
| 134 | 1.2DL + 1.5LM5 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 38 | 1.5 | 13 | 0.154 |
| 135 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 6+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 0 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 2 | 0.154 |
| 136 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 6+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 3 | 0.154 |
| 137 | 1.2DL + 1.5LM6 + 1.6SWL ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 4 | 0.154 |
| 138 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 5 | 0.154 |
| 139 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 6 | 0.154 |
| 140 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 7 | 0.154 |
| 141 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 8 | 0.154 |
| 142 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 9 | 0.154 |
| 143 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 10 | 0.154 |
| 144 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 11 | 0.154 |
| 145 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 300 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 12 | 0.154 |
| 146 | 1.2DL + 1.5LM6 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 39 | 1.5 | 13 | 0.154 |
| 147 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 7+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 0 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 2 | 0.154 |
| 148 | 1.2DL + 1.5LM7 + 1.6SWL ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 3 | 0.154 |
| 149 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 7+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 4 | 0.154 |
| 150 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 7+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 90 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 5 | 0.154 |
| 151 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 6 | 0.154 |
| 152 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 7 | 0.154 |
| 153 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 8 | 0.154 |
| 154 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 9 | 0.154 |
| 155 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 10 | 0.154 |
| 156 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 11 | 0.154 |
| 157 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 300 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 12 | 0.154 |

Company Designer Job Number Model Name

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
12:53:50 AM
Checked By

|  | Description | Solve | PDelta | BLC | Factor | BLC | Factor | BLC | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 158 | 1.2DL + 1.5LM7 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 40 | 1.5 | 13 | 0.154 |
| 159 | 1.2DL + 1.5LM8 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 2 | 0.154 |
| 160 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 30 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 3 | 0.154 |
| 161 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}(30 \mathrm{mph}) \mathrm{AZI} 60$ | Yes | Y | 1 | 1.2 | 41 | 1.5 | 4 | 0.154 |
| 162 | 1.2DL + 1.5LM8 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 5 | 0.154 |
| 163 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 6 | 0.154 |
| 164 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 150 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 7 | 0.154 |
| 165 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 8 | 0.154 |
| 166 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 9 | 0.154 |
| 167 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 240 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 10 | 0.154 |
| 168 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 270 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 11 | 0.154 |
| 169 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 300 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 12 | 0.154 |
| 170 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 8+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 41 | 1.5 | 13 | 0.154 |
| 171 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 2 | 0.154 |
| 172 | 1.2DL + 1.5LM9 + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 3 | 0.154 |
| 173 | 1.2DL + 1.5LM9 + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 4 | 0.154 |
| 174 | 1.2DL + 1.5LM9 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 5 | 0.154 |
| 175 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 6 | 0.154 |
| 176 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 150 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 7 | 0.154 |
| 177 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 8 | 0.154 |
| 178 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 9 | 0.154 |
| 179 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 10 | 0.154 |
| 180 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 270 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 11 | 0.154 |
| 181 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 12 | 0.154 |
| 182 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 9+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 42 | 1.5 | 13 | 0.154 |
| 183 | 1.2DL + 1.5LM10 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 2 | 0.154 |
| 184 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 3 | 0.154 |
| 185 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 4 | 0.154 |
| 186 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 5 | 0.154 |
| 187 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 6 | 0.154 |
| 188 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 7 | 0.154 |
| 189 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 8 | 0.154 |
| 190 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10$ + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 9 | 0.154 |
| 191 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 240 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 10 | 0.154 |
| 192 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 270 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 11 | 0.154 |
| 193 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 10+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 12 | 0.154 |
| 194 | 1.2DL + 1.5LM10 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 43 | 1.5 | 13 | 0.154 |
| 195 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL ( 30 mph ) AZI 0 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 2 | 0.154 |
| 196 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 3 | 0.154 |
| 197 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 4 | 0.154 |
| 198 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 5 | 0.154 |
| 199 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 120 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 6 | 0.154 |
| 200 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 7 | 0.154 |
| 201 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 8 | 0.154 |
| 202 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 9 | 0.154 |
| 203 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 10 | 0.154 |
| 204 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 11 | 0.154 |
| 205 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 12 | 0.154 |
| 206 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 11$ + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 44 | 1.5 | 13 | 0.154 |
| 207 | 1.2DL + 1.5LM12 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 2 | 0.154 |
| 208 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 3 | 0.154 |
| 209 | 1.2DL + 1.5LM12 + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 4 | 0.154 |
| 210 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 5 | 0.154 |
| 211 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 120 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 6 | 0.154 |
| 212 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 150 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 7 | 0.154 |
| 213 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 8 | 0.154 |
| 214 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 210 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 9 | 0.154 |
| 215 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12$ + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 10 | 0.154 |

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
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| Description |  | Solve | PDelta | BLC | Factor | BLC | Factor | BLC | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 216 | 1.2DL + 1.5LM12 + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 11 | 0.154 |
| 217 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 12 | 0.154 |
| 218 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 12+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 45 | 1.5 | 13 | 0.154 |
| 219 | 1.2DL + 1.5LM13 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 2 | 0.154 |
| 220 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 3 | 0.154 |
| 221 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 4 | 0.154 |
| 222 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 90 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 5 | 0.154 |
| 223 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 120 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 6 | 0.154 |
| 224 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 150 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 7 | 0.154 |
| 225 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 8 | 0.154 |
| 226 | 1.2DL + 1.5LM13 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 9 | 0.154 |
| 227 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 240 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 10 | 0.154 |
| 228 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 270 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 11 | 0.154 |
| 229 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 13+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 300 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 12 | 0.154 |
| 230 | 1.2DL + 1.5LM13 + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 46 | 1.5 | 13 | 0.154 |
| 231 | 1.2DL + 1.5LM14 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 2 | 0.154 |
| 232 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 3 | 0.154 |
| 233 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14$ + 1.6 SWL ( 30 mph ) AZI 60 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 4 | 0.154 |
| 234 | 1.2DL + 1.5LM14 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 5 | 0.154 |
| 235 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 6 | 0.154 |
| 236 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 150 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 7 | 0.154 |
| 237 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 8 | 0.154 |
| 238 | 1.2DL + 1.5LM14 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 9 | 0.154 |
| 239 | 1.2DL + 1.5LM14 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 10 | 0.154 |
| 240 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 270 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 11 | 0.154 |
| 241 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 12 | 0.154 |
| 242 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 14+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 330 | Yes | Y | 1 | 1.2 | 47 | 1.5 | 13 | 0.154 |
| 243 | 1.2DL + 1.5LM15 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 2 | 0.154 |
| 244 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 30 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 3 | 0.154 |
| 245 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}$ (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 4 | 0.154 |
| 246 | 1.2DL + 1.5LM15 + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 5 | 0.154 |
| 247 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 120 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 6 | 0.154 |
| 248 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 150 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 7 | 0.154 |
| 249 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 180 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 8 | 0.154 |
| 250 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 210 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 9 | 0.154 |
| 251 | 1.2DL + 1.5LM15 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 10 | 0.154 |
| 252 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 270 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 11 | 0.154 |
| 253 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 48 | 1.5 | 12 | 0.154 |
| 254 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 15+1.6 \mathrm{SWL}(30 \mathrm{mph}) \mathrm{AZI} 330$ | Yes | Y | 1 | 1.2 | 48 | 1.5 | 13 | 0.154 |
| 255 | 1.2DL + 1.5LM16 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 2 | 0.154 |
| 256 | 1.2DL + 1.5LM16 + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 3 | 0.154 |
| 257 | 1.2DL + 1.5LM16 + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 4 | 0.154 |
| 258 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 5 | 0.154 |
| 259 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16$ + 1.6SWL ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 6 | 0.154 |
| 260 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16$ + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 7 | 0.154 |
| 261 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 8 | 0.154 |
| 262 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 210 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 9 | 0.154 |
| 263 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16$ + 1.6SWL ( 30 mph ) AZI 240 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 10 | 0.154 |
| 264 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16$ + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 11 | 0.154 |
| 265 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 300 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 12 | 0.154 |
| 266 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 16+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 49 | 1.5 | 13 | 0.154 |
| 267 | 1.2DL + 1.5LM17 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 2 | 0.154 |
| 268 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17$ + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 3 | 0.154 |
| 269 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17$ + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 4 | 0.154 |
| 270 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 5 | 0.154 |
| 271 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 120 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 6 | 0.154 |
| 272 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17$ + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 7 | 0.154 |
| 273 | 1.2DL + 1.5LM17 + 1.6SWL (30 mph) AZI 180 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 8 | 0.154 |

Company Designer
Job Number Model Name

Infinigy Engineering, PLLC
DVA
2039-Z5555C
BOBDL00104A

7/28/2021
12:53:50 AM
Checked By

| Description |  | Solve | PDelta | BLC | Factor | BLC | Factor | BLC | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 274 | 1.2DL + 1.5LM17 + 1.6SWL (30 mph) AZI 210 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 9 | 0.154 |
| 275 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 240 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 10 | 0.154 |
| 276 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17$ + 1.6SWL (30 mph) AZI 270 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 11 | 0.154 |
| 277 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 12 | 0.154 |
| 278 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 17+1.6 \mathrm{SWL}$ ( 30 mph ) AZI 330 | Yes | Y | 1 | 1.2 | 50 | 1.5 | 13 | 0.154 |
| 279 | 1.2DL + 1.5LM18 + 1.6SWL (30 mph) AZI 0 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 2 | 0.154 |
| 280 | 1.2DL + 1.5LM18 + 1.6SWL (30 mph) AZI 30 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 3 | 0.154 |
| 281 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL (30 mph) AZI 60 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 4 | 0.154 |
| 282 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL (30 mph) AZI 90 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 5 | 0.154 |
| 283 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL ( 30 mph ) AZI 120 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 6 | 0.154 |
| 284 | 1.2DL + 1.5LM18 + 1.6SWL (30 mph) AZI 150 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 7 | 0.154 |
| 285 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL ( 30 mph ) AZI 180 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 8 | 0.154 |
| 286 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL ( 30 mph ) AZI 210 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 9 | 0.154 |
| 287 | 1.2DL + 1.5LM18 + 1.6SWL (30 mph) AZI 240 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 10 | 0.154 |
| 288 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18+1.6 \mathrm{SWL}(30 \mathrm{mph})$ AZI 270 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 11 | 0.154 |
| 289 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL ( 30 mph ) AZI 300 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 12 | 0.154 |
| 290 | $1.2 \mathrm{DL}+1.5 \mathrm{LM} 18$ + 1.6SWL (30 mph) AZI 330 | Yes | Y | 1 | 1.2 | 51 | 1.5 | 13 | 0.154 |

## Envelope Node Reactions

| Node Label |  |  | X [lb] | LC | Y [lb] | LC | Z [lb] | LC | MX [lb-in] | LC | MY [lb-in] | LC | MZ [lb-in] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | max | 1329.767 | 25 | 1722.877 | 27 | 1293.144 | 6 | 23174.84 | 108 | 27189.445 | 6 | 21079.197 | 20 |
| 2 |  | min | -1456.606 | 8 | -198.177 | 20 | -1294.11 | 12 | -23162.683 | 90 | -27467.341 | 12 | -66649.248 | 2 |
| 3 | N67 | max | 1662.784 | 2 | 1857.939 | 35 | 1528.917 | 5 | 19245.927 | 16 | 35008.981 | 13 | 34968.491 | 143 |
| 4 |  | min | -1571.738 | 20 | -164.019 | 16 | -1380.866 | 24 | -59380.677 | 10 | -28600.827 | 6 | -10983.775 | 16 |
| 5 | N117 | max | 1565.311 | 2 | 1723.589 | 31 | 1279.79 | 16 | 66885.017 | 127 | 27704.97 | 10 | 34602.146 | 209 |
| 6 |  | min | -1474.269 | 20 | -218.015 | 24 | -1487.207 | 12 | -19286.117 | 24 | -27447.646 | 4 | -11147.264 | 24 |
| 7 | Totals: | max | 4478.45 | 14 | 4876.205 | 35 | 3923.808 | 16 |  |  |  |  |  |  |
| 8 |  | min | -4478.457 | 20 | 1679.354 | 52 | -4140.921 | 24 |  |  |  |  |  |  |

## Envelope AISC 14TH (360-10): LRFD Member Steel Code Checks

| Member |  |  |  |  |  |  |  |  |  |  |  |  | Cb Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M12 | 6"x0.375" Plate | 0.602 | 2.036 | 2 | 0.664 | 2.036 | y | 11062722.329 | 72900 | 6834.391 | 109350 | $2.529 \mathrm{H} 1-1 \mathrm{~b}$ |
| 2 | M83 | 6"x0.375" Plate | 0.605 | 2.036 | 6 | 0.661 | 2.036 | v | 12762722.329 | 72900 | 6834.391 | 109350 | $2.527 \mathrm{H} 1-1 \mathrm{~b}$ |
| 3 | M13 | 6"x0.375" Plate | 0.602 | 2.036 | 2 | 0.661 | 2.036 | y | 8762722.329 | 72900 | 6834.391 | 109350 | $2.527 \mathrm{H} 1-1 \mathrm{~b}$ |
| 4 | M82 | 6 "x0.375" Plate | 0.597 | 2.036 | 6 | 0.516 | 2.036 | y | 662722.329 | 72900 | 6834.391 | 109350 | $2.527 \mathrm{H} 1-1 \mathrm{~b}$ |
| 5 | M51 | 6"x0.375" Plate | 0.595 | 2.036 | 10 | 0.515 | 2.036 | y | 1062722.329 | 72900 | 6834.391 | 109350 | $2.525 \mathrm{H} 1-1 \mathrm{~b}$ |
| 6 | M50 | 6"x0.375" Plate | 0.604 | 2.036 | 10 | 0.515 | 2.036 | y | 1062722.329 | 72900 | 6834.391 | 109350 | $2.528 \mathrm{H} 1-1 \mathrm{~b}$ |
| 7 | M81 | 6"x0.375" Plate | 0.372 | 2.036 | 10 | 0.353 | 2.036 | y | 3762722.329 | 72900 | 6834.391 | 109350 | $2.19 \mathrm{H} 1-1 \mathrm{~b}$ |
| 8 | M49 | 6"x0.375" Plate | 0.367 | 2.036 | 2 | 0.352 | 2.036 | y | 2962722.329 | 72900 | 6834.391 | 109350 | 2.187H1-1b |
| 9 | M80 | 6"x0.375" Plate | 0.374 | 2.036 | 13 | 0.351 | 2.036 | y | 3762722.329 | 72900 | 6834.391 | 109350 | 2.24 H1-1b |
| 10 | M10 | 6"x0.375" Plate | 0.365 | 2.036 | 10 | 0.351 | 2.036 | y | 3362722.329 | 72900 | 6834.391 | 109350 | 2.187H1-1b |
| 11 | M11 | 6"x0.375" Plate | 0.365 | 2.036 | 6 | 0.351 | 2.036 | y | 3362722.329 | 72900 | 6834.391 | 109350 | 2.187H1-1b |
| 12 | M48 | 6"x0.375" Plate | 0.371 | 2.036 | 6 | 0.35 | 2.036 | y | 2962722.329 | 72900 | 6834.391 | 109350 | $2.188 \mathrm{H} 1-1 \mathrm{~b}$ |
| 13 | M24 | 6"x0.375" Plate | 0.304 | 0 | 2 | 0.347 | 0 | y | 11071110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 14 | M100 | 6"x0.375" Plate | 0.305 | 0 | 6 | 0.345 | 0 | y | 12771110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 15 | M30 | 6"x0.375" Plate | 0.304 | 0 | 2 | 0.345 | 0 | y | 8771110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 16 | M94 | 6"x0.375" Plate | 0.301 | 0 | 6 | 0.265 | 0 | y | 671110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 17 | M62 | 6"x0.375" Plate | 0.305 | 0 | 10 | 0.264 | 0 | y | 1071110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 18 | M68 | 6"x0.375" Plate | 0.3 | 0 | 10 | 0.264 | 0 | y | 1071110.261 | 72900 | 6834.391 | 109350 | $1.353 \mathrm{H} 1-1 \mathrm{~b}$ |
| 19 | M42 | PIPE_2.0 | 0.386 | 30 | 13 | 0.22 | 38 |  | 1314916.096 | 32130 | 22459.5 | 22459.5 | 3 H1-1b |
| 20 | M106 | PIPE_2.5 | 0.152 | 90 | 13 | 0.219 | 6 |  | 1330038.461 | 50715 | 43155 | 43155 | $1.782 \mathrm{H} 1-1 \mathrm{~b}$ |
| 21 | M110 | PIPE_2.0 | 0.483 | 30 | 25 | 0.212 | 30 |  | 1314916.096 | 32130 | 22459.5 | 22459.5 | 3 H1-1b |
| 22 | M107 | PIPE_2.0 | 0.516 | 30 | 13 | 0.211 | 30 |  | 1314916.096 | 32130 | 22459.5 | 22459.5 | $2.556 \mathrm{H} 1-1 \mathrm{~b}$ |
| 23 | M3 | PIPE_2.5 | 0.139 | 90 | 6 | 0.207 | 6 |  | 1030038.461 | 50715 | 43155 | 43155 | $1.792 \mathrm{H} 1-1 \mathrm{~b}$ |
| 24 | M114 | PIPE_2.5 | 0.139 | 6 | 2 | 0.207 | 90 |  | 1030038.461 | 50715 | 43155 | 43155 | $1.792 \mathrm{H} 1-1 \mathrm{~b}$ |
| 25 | M115 | PIPE_2.0 | 0.456 | 30 | 9 | 0.202 | 30 |  | 414916.096 | 32130 | 22459.5 | 22459.5 | 3 H1-1b |
| 26 | M38 | PIPE_2.0 | 0.454 | 30 | 10 | 0.202 | 30 |  | 414916.096 | 32130 | 22459.5 | 22459.5 | 3 H1-1b |

Infinigy Engineering, PLLC
DVA
2039-Z5555C

7/28/2021
12:53:50 AM
Checked By

## Envelope AISC 14TH (360-10): LRFD Member Steel Code Checks (Continued)

| Member |  | Shape | Code CheckLoc[in] |  | LC Shear CheckLoc[in]D |  |  | $\begin{aligned} & \text { DirLC phi*Pnc [lb]pl } \\ & \hline 1214916.096 \end{aligned}$ |  | $\begin{gathered} \text { phi*Pnt [lb] } \\ 32130 \end{gathered}$ | phi*Mn y-y [lb-in] phi*Mn z-z [lb-in]  <br> 22459.5 22459.5 |  | $\begin{array}{c\|c} \hline \mathrm{Cb} & \text { Eqn } \\ \hline 3 & \mathrm{H} 1-1 \mathrm{~b} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | M35 | PIPE_2.0 | 0.454 | 30 | 6 | 0.202 | 30 |  |  |  |  |  |  |
| 28 | M118 | PIPE_2.0 | 0.457 | 30 | 3 | 0.202 | 30 |  | 814916.096 | 32130 | 22459.5 | 22459.5 | $2.216 \mathrm{H} 1-1 \mathrm{~b}$ |
| 29 | M74 | PIPE_2.0 | 0.342 | 30 | 8 | 0.195 | 38 |  | 314916.096 | 32130 | 22459.5 | 22459.5 | $3 \mathrm{H} 1-1 \mathrm{~b}$ |
| 30 | M4 | PIPE_2.0 | 0.35 | 30 | 12 | 0.193 | 38 |  | 1214916.096 | 32130 | 22459.5 | 22459.5 | $2.263 \mathrm{H} 1-1 \mathrm{~b}$ |
| 31 | M1 | HSS4X4X4 | 0.395 | 0 | 13 | 0.184 | 0 | y | 109133649.326 | 139518 | 194166 | 194166 | $1.659 \mathrm{H} 1-1 \mathrm{~b}$ |
| 32 | M73 | HSS4X4X4 | 0.383 | 0 | 4 | 0.184 | 0 | y 1 | 129133649.326 | 139518 | 194166 | 194166 | $1.703 \mathrm{H} 1-1 \mathrm{~b}$ |
| 33 | M105 | PIPE_3.0 | 0.121 | 90 | 13 | 0.175 | 90 |  | 1360482.561 | 65205 | 68985 | 68985 | $1.767 \mathrm{H} 1-1 \mathrm{~b}$ |
| 34 | M93 | 6"x0.375" Plate | 0.154 | 0 | 12 | 0.167 | 0 | y | 3771110.261 | 72900 | 6834.391 | 109350 | $1.351 \mathrm{H} 1-1 \mathrm{~b}$ |
| 35 | M99 | 6"x0.375" Plate | 0.157 | 0 | 13 | 0.166 | 0 | v | 3771110.261 | 72900 | 6834.391 | 109350 | $1.35 \mathrm{H1-1b}$ |
| 36 | M61 | 6"x0.375" Plate | 0.153 | 0 | 4 | 0.166 | 0 | v | 2971110.261 | 72900 | 6834.391 | 109350 | $1.351 \mathrm{H} 1-1 \mathrm{~b}$ |
| 37 | M29 | 6"x0.375" Plate | 0.154 | 0 | 8 | 0.166 | 0 | y | 3371110.261 | 72900 | 6834.391 | 109350 | $1.351 \mathrm{H} 1-1 \mathrm{~b}$ |
| 38 | M23 | 6"x0.375" Plate | 0.154 | 0 | 8 | 0.166 | 0 | y | 3371110.261 | 72900 | 6834.391 | 109350 | $1.351 \mathrm{H} 1-1 \mathrm{~b}$ |
| 39 | M67 | 6"x0.375" Plate | 0.154 | 0 | 4 | 0.166 | 0 | y | 2971110.261 | 72900 | 6834.391 | 109350 | $1.351 \mathrm{H} 1-1 \mathrm{~b}$ |
| 40 | M5 | HSS4.5X4.5X3 | 0.069 | 20 | 2 | 0.159 | 8.958 | y | 109120246.398 | 121302 | 194994 | 194994 | $1.494 \mathrm{H} 1-1 \mathrm{~b}$ |
| 41 | M75 | HSS4.5X4.5X3 | 0.069 | 20 | 6 | 0.158 | 8.958 | y | 129120246.398 | 121302 | 194994 | 194994 | $1.494 \mathrm{H} 1-1 \mathrm{~b}$ |
| 42 | M113 | PIPE_3.0 | 0.114 | 48 | 75 | 0.157 | 6 |  | 360482.561 | 65205 | 68985 | 68985 | 1 H1-1b |
| 43 | M2 | PIPE_3.0 | 0.112 | 90 | 6 | 0.157 | 90 |  | 660482.561 | 65205 | 68985 | 68985 | $1.786 \mathrm{H} 1-1 \mathrm{~b}$ |
| 44 | M41 | HSS4X 4 X4 | 0.397 | 0 | 12 | 0.131 | 12.017 | z | 13133649.326 | 139518 | 194166 | 194166 | $1.717 \mathrm{H} 1-1 \mathrm{~b}$ |
| 45 | M7 | L4X4X4 | 0.549 | 0 | 110 | 0.124 | 0 | z | 10954411.715 | 62532 | 37651.159 | 80578.632 | $1.5 \mathrm{H} 2-1$ |
| 46 | M6 | L4X4X4 | 0.547 | 24.375 | 89 | 0.123 | 24.375 | z | 8954411.715 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 47 | M76 | L4X4X4 | 0.547 | 24.375 | 129 | 0.123 | 24.375 | z | 12954411.715 | 62532 | 37651.159 | 80578.632 | $1.5 \mathrm{H} 2-1$ |
| 48 | M43 | HSS4.5X4.5X3 | 0.069 | 20 | 10 | 0.098 | 8.958 | z | 13120246.398 | 121302 | 194994 | 194994 | $1.494 \mathrm{H} 1-1 \mathrm{~b}$ |
| 49 | M44 | L4X4X4 | 0.368 | 24.375 | 12 | 0.089 | 24.375 | z | 1254411.715 | 62532 | 37651.159 | 80578.632 | $1.469 \mathrm{H} 2-1$ |
| 50 | M77 | L4X4X4 | 0.363 | 0 | 4 | 0.089 | 24.375 | z | 1054411.715 | 62532 | 37651.159 | 80578.632 | $1.468 \mathrm{H} 2-1$ |
| 51 | M45 | L4X4X4 | 0.362 | 0 | 8 | 0.088 | 24.375 | z | 254411.715 | 62532 | 37651.159 | 80578.632 | $1.467 \mathrm{H} 2-1$ |
| 52 | M8 | L4X4X4 | 0.378 | 36.125 | 30 | 0.055 | 36.125 | z | 10951466.784 | 62532 | 37651.159 | 80578.632 | $1.5 \mathrm{H} 2-1$ |
| 53 | M79 | L4X4X4 | 0.379 | 0 | 28 | 0.054 | 0 | z 1 | 12951466.784 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 54 | M9 | L4X4X4 | 0.379 | 0 | 36 | 0.054 | 0 | z | 8951466.784 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 55 | M47 | L4X4X4 | 0.377 | 0 | 32 | 0.037 | 3.01 | y | 1351466.784 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 56 | M46 | L4X4X4 | 0.38 | 36.125 | 38 | 0.036 | 36.125 | z | 22551466.784 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 57 | M78 | L4X4X4 | 0.38 | 36.125 | 34 | 0.036 | 36.125 | z 2 | 20951466.784 | 62532 | 37651.159 | 80578.632 | 1.5 H2-1 |
| 58 | M84 | L3X3X3 | 0.34 | 27.5 | 12 | 0.036 | 55 | z 1 | 13021109.581 | 35316 | 15841.16 | 29030.935 | $1.018 \mathrm{H} 2-1$ |
| 59 | M14 | L3X3X3 | 0.334 | 27.5 | 8 | 0.035 | 0 | z 1 | 10821109.581 | 35316 | 15841.16 | 29033.525 | $1.018 \mathrm{H} 2-1$ |
| 60 | M52 | L3X3X3 | 0.334 | 27.5 | 4 | 0.033 | 0 | y | 1321109.581 | 35316 | 15841.16 | 29033.512 | $1.018 \mathrm{H} 2-1$ |
| 61 | M15 | 6"x0.375" Plate | 0.555 | 1.557 | 2 | 0.022 | 5.75 | y | 1362722.329 | 72900 | 6834.391 | 109350 | $2.198 \mathrm{H} 1-1 \mathrm{~b}$ |
| 62 | M53 | 6"x0.375" Plate | 0.555 | 1.557 | 10 | 0.022 | 5.75 | z | 1062722.329 | 72900 | 6834.391 | 109350 | $2.197 \mathrm{H} 1-1 \mathrm{~b}$ |
| 63 | M86 | 6"x0.375" Plate | 0.555 | 1.557 | 6 | 0.022 | 5.75 | z | 662722.329 | 72900 | 6834.391 | 109350 | 2.196H1-1b |
| 64 | M54 | 6"x0.375" Plate | 0.555 | 1.557 | 10 | 0.022 | 5.75 | z | 1062722.329 | 72900 | 6834.391 | 109350 | $2.202 \mathrm{H} 1-1 \mathrm{~b}$ |
| 65 | M85 | 6"x0.375" Plate | 0.555 | 1.557 | 6 | 0.022 | 5.75 | z | 662722.329 | 72900 | 6834.391 | 109350 | $2.203 \mathrm{H} 1-1 \mathrm{~b}$ |
| 66 | M16 | 6"x0.375" Plate | 0.555 | 1.557 | 2 | 0.022 | 5.75 | z | 262722.329 | 72900 | 6834.391 | 109350 | $2.201 \mathrm{H} 1-1 \mathrm{~b}$ |
| 67 | M65 | 6"x0.375" Plate | 0.14 | 0 | 10 | 0.015 | 0 | z | 1071110.261 | 72900 | 6834.391 | 109350 | $1.349 \mathrm{H} 1-1 \mathrm{~b}$ |
| 68 | M71 | 6"x0.375" Plate | 0.14 | 0 | 10 | 0.015 | 0 | z | 1071110.261 | 72900 | 6834.391 | 109350 | $1.35 \mathrm{H} 1-1 \mathrm{~b}$ |
| 69 | M103 | 6"x0.375" Plate | 0.14 | 0 | 6 | 0.015 | 0 | z | 671110.261 | 72900 | 6834.391 | 109350 | $1.349 \mathrm{H} 1-1 \mathrm{~b}$ |
| 70 | M97 | 6"x0.375" Plate | 0.14 | 0 | 6 | 0.015 | 0 | z | 671110.261 | 72900 | 6834.391 | 109350 | $1.35 \mathrm{H1-1b}$ |
| 71 | M27 | 6"x0.375" Plate | 0.14 | 0 | 2 | 0.015 | 0 | z | 271110.261 | 72900 | 6834.391 | 109350 | $1.349 \mathrm{H} 1-1 \mathrm{~b}$ |
| 72 | M33 | 6"x0.375" Plate | 0.14 | 0 | 2 | 0.015 | 0 | z | 271110.261 | 72900 | 6834.391 | 109350 | $1.35 \mathrm{H} 1-1 \mathrm{~b}$ |
| 73 | M125 | PIPE_2.0 | 0.059 | 18 | 10 | 0.011 | 18 |  | 1026521.424 | 32130 | 22459.5 | 22459.5 | $2.401 \mathrm{H} 1-1 \mathrm{~b}$ |

FROM ZERO TO INFINIGY
the solutions are endless

## BOLT CONNECTION CALCULATION

## BOLT PROPERTIES

| Date: | $7 / 28 / 2021$ |
| :--- | :--- |
| Site: | BOBDL00104A |
| Engineer: | DVA |
| Infinigy Job No: | $2039-Z 5555 C$ |
| Connection Location: | Arm to Collar |

Bolt Capacity Equation
Connection Type
Bolt Size, d
Threads per Inch, n
Steel Grade
Bolt Ultimate Tensile Stress, $\mathbf{F}_{\mathbf{u}}$
Threads Exclusion
Shear Plane

| TIA-222-H |
| :---: |
| Steel |
| $5 / 8$ |
| 11 |
| A325 |
| 120 |
| N |
| 1 |

in
ksi
$i n^{2}$
$i n^{2}$
lbs
lbs

## INFINIGY8

FROM ZERO TO INFINIGY the solutions are endless

## BOLT CONNECTION CALCULATION

## BOLT GROUP CHECK

| Date: | 7/28/2021 |
| :--- | :--- |
| Site: | BOBDL00104A |
| Engineer: | DVA |
| Infinigy Job No: | $2039-Z 5555 C$ |
| Connection Location: | Arm to Collar |


| Loads Properties |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Controlling LC: | 13 |  |  |  |  |
| Load Point Number: | N1 |  |  |  |  |
| X-Coordinate (in.) | 4.00 |  |  |  |  |
| Y-Coordinate (in.) | 4.00 |  |  |  |  |
| Z-Coordinate (in.) | 0.00 |  |  |  |  |
| Shear Load, Px (lbs) | -695.000 | 0 | 0 | 0 | 0 |
| Shear Load, Py (lbs) | 1455.000 | 0 | 0 | 0 | 0 |
| Axial Load, Pz (lbs) | 1305.000 | 0 | 0 | 0 | 0 |
| Moment, Mx (lb-in) | 62199.000 | 0 | 0 | 0 | 0 |
| Moment, My (lb-in) | -13585.000 | 0 | 0 | 0 | 0 |
| Moment, Mz (lb-in) | 6724.000 | 0 | 0 | 0 | 0 |


| Member Properties |  |  |
| :--- | :---: | :---: |
| Start Coordinates: <br> Dimentions: | $\boldsymbol{X}$ | $\boldsymbol{Y}$ |
|  | 0.0 | 0.0 |
|  | 8.0 | 8.0 |



Number of Bolts

|  | 4 |  |
| :---: | :---: | :---: |
| No. | Bolt Type | Xo (in) |
| 1 | Main Type | 1.0 |
| 2 | Main Type | 7.0 |
| 3 | Main Type | 1.0 |
| 4 | Main Type | 7.0 |
| Bolt Group Properties: |  |  |
| Xc $=$ | 4.00 | in. |
| $\mathrm{Yc}=$ | 4.00 | in. |
| Ic. $\mathrm{y}=$ | 11.04 | in.^2 |
| Ic. $\mathrm{x}=$ | 11.04 | in.^2 |
| lc. $\mathrm{xy}=$ | 22.09 | in.^2 |

Bolt Loads

Loads Shear 787.83 | 787.83 | Tensio |
| ---: | ---: |
| 461.55 | $0.0 \%$ |
| 652.65 | $21.5 \%$ |
| 135.32 | $32.7 \%$ |

Loads at Center of Gravity of Bolt Group:

| $\mathrm{Pz}=$ | 1305.00 |
| :---: | :---: |
| $P \mathrm{x}=$ | -695.00 |
| $P y=$ | 1455.00 |
| $\mathrm{Mx}=$ | 62199.00 |
| $\mathrm{My}=$ | -13585.00 |
| $\mathrm{Mz}=$ | 6724.00 |

PARTS LIST

| ITEM | QTY | PART NO. | PART DESCRIPTION | LENGTH | UNIT WT. | NET WT. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 3 | X-LWRM | RING MOUNT WELDMENT |  | 68.81 | 206.42 |
| 2 | 3 | X-SNP-ST8 | SNB8 TELESCOPING ARM FOR GRATING |  | 60.39 | 181.16 |
| 3 | 3 | X-SNPC | CORNER GRATING WELDMENT |  | 194.33 | 582.99 |
| 4 | 3 | P396 | 3" SCH. 40 PIPE (3.5" O.D. $\times 0.216 "$ WALL) A500 | 96.000 in | 60.75 | 182.25 |
| 5 | 3 | P3096 | 2-7/8" OD X 96" Sch 40 Galvanized Pipe |  | 46.45 | 139.36 |
| 6 | 3 | X-SNP-HRA | CORNER BRACKET FOR SNPX PLATFORMS |  | 25.95 | 77.86 |
| 7 | 3 | X-SNPP1G | CLAMP PLATE | 7.250 in | 2.03 | 6.10 |
| 8 | 9 | X-SP219 | SMALL SUPPORT CROSS PLATE | 8.250 in | 8.61 | 77.50 |
| 9 | 9 | SCX2 | CROSSOVER PLATE | 7.000 in | 4.80 | 43.17 |
| 10 | 9 | G58R-48 | 5/8" $\times 48$ " THREADED ROD (HDG.) |  | 0.55 | 4.94 |
| 10 | 9 | G58R-24 | $5 / 8$ " $\times 24$ " THREADED ROD (HDG.) |  | 0.55 | 4.94 |
| 11 | 12 | A58234 | 5/8" $\times 2$-3/4" HDG A325 HEX BOLT | 2.75 | 0.36 | 4.27 |
| 12 | 30 | A58FW | 5/8" HDG A325 FLATWASHER |  | 0.03 | 1.02 |
| 13 | 30 | G58LW | 5/8" HDG LOCKWASHER |  | 0.03 | 0.78 |
| 14 | 18 | A58NUT | 5/8" HDG A325 HEX NUT |  | 0.13 | 2.34 |
| 15 | 12 | G58NUT | 5/8" HDG HEAVY 2H HEX NUT |  | 0.13 | 1.56 |
| 16 | 12 | X-UB1358 | 1/2" $\times 3$-5/8" $\times 5-1 / 2^{\prime \prime} \times 3$ " U-BOLT (HDG.) |  | 0.73 | 8.78 |
| 17 | 24 | X-UB1300 | 1/2" $\times 3$ " $\times 5$ " $\times 2$ " U-BOLT (HDG.) |  | 0.73 | 17.56 |
| 18 | 36 | X-UB1212 | 1/2" $\times 2-1 / 2^{\prime \prime} \times 4-1 / 2^{\prime \prime} \times 2$ " U-BOLT (HDG.) |  | 0.73 | 26.34 |
| 19 | 6 | G12065 | $1 / 2^{\prime \prime} \times 6-1 / 2$ " HDG HEX BOLT GR5 FULL THREAD | 7-1/2 | 0.41 | 2.46 |
| 20 | 18 | X-UB1306 | 1/2" $\times 3-5 / 8$ " $\times 6$ " $\times 3$ " U-BOLT (HDG.) |  | 0.73 | 13.17 |
| 21 | 186 | G12NUT | 1/2" HDG HEAVY 2H HEX NUT |  | 0.07 | 13.32 |
| 22 | 180 | G12FW | 1/2" HDG USS FLATWASHER |  | 0.03 | 6.13 |
| 23 | 186 | G12LW | 1/2" HDG LOCKWASHER |  | 0.01 | 2.59 |
| 24 | 9 | A | 2" SCH. 40 PIPE (2.375" O.D. x 0.154" WALL) A500 | B | C | D |

$15{ }^{x} 2_{2}$
$13 x^{2}$
$12 x^{2}$
11
$21 x 2$
23
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${ }^{22} x^{x 2} x 2$
(21) $x 2$


21
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$x 2$
DETAIL C

| 2-3/8" O.D. VERTICAL MOUNTING PIPES |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ASSEMBLY NO. | PART NO. "A" | LENGTH "B" | UNIT WEIGHT "C | NET WEIGHT "D" | TOTAL WEIGHT |
| SNP8HR-372 | P272 | $6^{\prime}$ '0" | 23.07 | 207.63 | 1717.07 |
| SNP8HR-384 | P284 | $7^{\prime}-0 "$ | 26.91 | 242.19 | 1751.63 |
| SNP8HR-396 | P296 | $8^{\prime}-0 "$ | 30.76 | 276.84 | 1786.28 |
| SNP8HR-3126 | P2126 | $10^{\prime}-6 "$ | 40.75 | 366.75 | 1876.19 |


| TOLERANCE NOTES |  |
| :---: | :---: |
| tolerances on dimensions, unless otherwise noted are: SAWED, SHEARED AND GAS CUT EDGES ( $\pm 0.030^{\prime \prime}$ ) <br> DRILLED AND GAS CUT HOLES ( $\pm 0.030^{\prime \prime}$ ) - NO CONING OF HOLES LASER CUT EDGES AND HOLES ( $\pm 0.010^{\prime \prime}$ ) - NO CONING OF HOLES BENDS ARE $\pm 1 / 2$ DEGREE <br> ALL OTHER MACHINING ( $\pm 0.030^{\prime \prime}$ ) <br> ALL OTHER ASSEMBLY ( $\pm \mathbf{0 . 0 6 0 " )}$ |  |
|  |  |
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|  |  |
|  |  |
| PROPRIETARY NOTE: THE DATA AND TECHNIQUES CONTAINED IN THI INDUSTRIES AND CONSIDERED A TRADE SECRE | PROPRIETARY INFORMATION OF VALMONT SCLOSURE WITHOUT THE CONSENT OF |






## Exhibit F

## Power Density/RF Emissions Report

# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

Dish Wireless Existing Facility

Site ID: BOBDL00104A
63 Woodland Street
Glastonbury, Connecticut 06033
September I, 202 I
EBI Project Number: 6221004688

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population <br> allowable limit: | $\mathbf{1 6 . 4 7 \%}$ |

environmental | engineering | due diligence

September I, 202I

Dish Wireless

Emissions Analysis for Site: BOBDL00 I04A

EBI Consulting was directed to analyze the proposed Dish Wireless facility located at 63 Woodland Street in Glastonbury, Connecticut for the purpose of determining whether the emissions from the Proposed Dish Wireless Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-Oland ANSI/IEEE Std C95.I. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR I.I307(b)(I) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, respectively. The general population exposure limit for the $1900 \mathrm{MHz}(\mathrm{PCS}), 2100 \mathrm{MHz}(\mathrm{AWS})$ and II GHz frequency bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure.
environmental | engineering | due diligence
Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed Dish Wireless Wireless antenna facility located at 63 Woodland Street in Glastonbury, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since Dish Wireless is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6 -foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 4 n 7 I channels ( 600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
2) 4 n 70 channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
3) 4 n 66 channels (AWS Band -2190 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
5) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative
environmental | engineering | due diligence
estimate as gain reductions for these particular antennas are typically much higher in this direction.
6) The antennas used in this modeling are the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900$ $\mathrm{MHz} / 2190 \mathrm{MHz}$ channel(s) in Sector A, the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900$ MHz / 2190 MHz channel(s) in Sector B, the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900$ $\mathrm{MHz} / 2190 \mathrm{MHz}$ channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antenna mounting height centerline of the proposed antennas is 125 feet above ground level (AGL).
8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
9) All calculations were done with respect to uncontrolled / general population threshold limits.
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## Dish Wireless Site Inventory and Power Data

$\left.\begin{array}{|r|c|r|r|r|}\hline \text { Sector: } & \text { A } & \text { Sector: } & \text { B } & \text { Sector: }\end{array}\right]$ C
environmental | engineering | due diligence

| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| Dish Wireless (Max at Sector A): | $1.67 \%$ |
| AT\&T | $10.06 \%$ |
| T-Mobile | $4.74 \%$ |
| Site Total MPE \%: | $16.47 \%$ |


| Dish Wireless MPE \% Per Sector |  |
| :---: | :---: |
| Dish Wireless Sector A Total: | $1.67 \%$ |
| Dish Wireless Sector B Total: | $1.67 \%$ |
| Dish Wireless Sector C Total: | $1.67 \%$ |
| Site Total MPE \%: |  |
| $16.47 \%$ |  |

## Dish Wireless Maximum MPE Power Values (Sector A)

| Dish Wireless Frequency <br> Band / <br> Technology <br> (Sector A) | \# Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE <br> ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dish Wireless $600 \mathrm{MHz} \mathrm{n7I}$ | 4 | 223.68 | 125.0 | 2.27 | $600 \mathrm{MHz} \mathrm{n71}$ | 400 | 0.57\% |
| Dish Wireless $1900 \mathrm{MHz} \mathrm{n70}$ | 4 | 542.70 | 125.0 | 5.51 | $1900 \mathrm{MHz} \mathrm{n70}$ | 1000 | 0.55\% |
| Dish Wireless 2190 MHz n 66 | 4 | 542.70 | 125.0 | 5.51 | $2190 \mathrm{MHz} \mathrm{n66}$ | 1000 | 0.55\% |
|  |  |  |  |  |  | Total: | 1.67\% |

- NOTE: Totals may vary by approximately $0.01 \%$ due to summation of remainders in calculations.
environmental | engineering | due diligence


## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the Dish Wireless facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| Dish Wireless Sector | Power Density Value (\%) |
| :---: | :---: |
| Sector A: | $1.67 \%$ |
| Sector B: | $1.67 \%$ |
| Sector C: | $1.67 \%$ |
| Dish Wireless <br> Maximum MPE \% <br> (Sector A): | $1.67 \%$ |
| Site Total: |  |
| $16.47 \%$ |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{1 6 . 4 7 \%}$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.

## Exhibit G

## Letter of Authorization

Eco-Site, LLC - Letter of Authorization

CT - CONNECTICUT SITING COUNCIL<br>Melanie A. Bachman<br>Executive Director<br>Connecticut Siting Council<br>10 Franklin Square<br>New Britain, CT 06051

## Re: Tower Share Application

Eco-Site, LLC - telecommunications site at:
63 WOODLAND ST., GLASTONBURY, CT 06073

Eco-Site, LLC, a Delaware limited liability company, d/b/a Vertical Bridge ("Eco Site") hereby authorizes DISH Wireless LLC, including their Agent, to act as our Agent in the processing of all zoning applications, building permits and approvals through the CT - CONNECTICUT SITING COUNCIL for the existing wireless communications site described below:

Eco Site ID/Name: US-CT-5018/Hopewell
Customer Site ID: BOBDL00104A / ECO - Woodland St
Site Address: 63 WOODLAND ST., GLASTONBURY, CT 06073

Eco-Site, LLC


Name: ${ }^{\text {Tim }}{ }^{\text {Túlk }}$
Title: Vice President - Lease Administration

## Exhibit H

## Recipient Mailings



## Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
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3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage ${ }^{B}$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {Tm }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

| USPS TRACKING \# : 9405503699300019758694 |  |  |  |
| :---: | :---: | :---: | :---: |
| Trans. \#: Print Date: | 544897384 | Priority Mail(8) Postage: | \$7.95 |
|  | : 09/30/2021 |  | \$7.95 |
| Ship Date: | : 10/01/2021 |  |  |
| Defivery Date: | Date: 10/04/2021 |  |  |
| From: $\begin{array}{ll}\text { CH } \\ & \mathrm{NO} \\ & 10 \\ & \mathrm{FA}\end{array}$ | CHUCK REGULBUTO |  |  |
|  | NORTHEAST SITE SOLUTIONS |  |  |
|  | 1053 FARMINGTON AVE STE G |  |  |
|  | FARMINGTON CT 06032-1574 |  |  |
| To: VER | VERTICAL BRIDGE, REIT, LLC, TOWER OWNER |  |  |
|  | 750 PARK OF COMMERCE DR |  |  |
|  | STE 200 |  |  |
|  | BOCA RATON FL 33487-3650 |  |  |
| * Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking (8) servic on Prierity Mall service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date. |  |  |  |



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## Click-N-Ship® Label Record

| USPS TRACKING \# : 9405503699300019740842 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Trans. \#: Print Dat Ship Dat Expected Delivery |  | 544895944 | Priority Mail® Postage: | \$7.95 |
|  |  | 09/30/2021 | Total: | \$7.95 |
|  |  | 10/01/2021 |  |  |
|  | Date: | 10/02/2021 |  |  |
| From: | CHU | K REGULBU |  |  |
|  | NOR | HEAST SITE | OLUTIONS |  |
|  | 1053 | FARMINGTO | AVE STE G |  |
|  | FAR | IINGTON CT | 032-1574 |  |
| To: | RICH | ARD J JOHN |  |  |
|  | TOW | N MANAGER | OWN OF GLASTONBUR |  |
|  | 2155 | MAIN ST |  |  |
|  | \# 2 |  |  |  |
|  | GLA | TONBURY | 06033-2282 |  |
| * Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date. |  |  |  |  |



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4. To mail your package with PC Postage $®^{\circledR}$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {tm }}$, or drop in a USPS collection box.
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## Click-N-Ship® Label Record

## USPS TRACKING \# :

 9405503699300019740859| Trans. \#: |  | 544895944 | Priority Mail® Postage: Total: | $\frac{\$ 7.95}{\$ 7.95}$ |
| :---: | :---: | :---: | :---: | :---: |
| Print Date: |  | 09/30/2021 |  |  |
| Ship Date: Expected |  | 10/01/2021 |  |  |
| Delivery Date: |  | 10/02/2021 |  |  |
| From: | CHUCK REGULBUTO |  |  |  |
|  | NORTHEAST SITE SOLUTIONS |  |  |  |
|  | 1053 FARMINGTON AVE STE G |  |  |  |
|  | FARMINGTON CT 06032-1574 |  |  |  |
| To: | REBECCA AUGUR |  |  |  |
|  | DIRECTOR OF PLANNING \& LAND USE SERVICES |  |  |  |
|  | 2155 MAIN ST |  |  |  |
|  | \# 3 |  |  |  |
|  | GLASTONBURY CT 06033-2282 |  |  |  |
| * Retail Pricing Priarity Mail rates apply. There is no fee for USPS Tracking(®) service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date. |  |  |  |  | on Prority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date


|  | 9405503699300019740866 |  |  |  | $\begin{array}{\|l\|} \hline \boldsymbol{0} \\ \mathbf{N} \\ \mathbf{\omega} \\ \hline \end{array}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Instructions

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4. To mail your package with PC Postage ${ }^{\text {® }}$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {TM }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

## Click-N-Ship® Label Record

## USPS TRACKING \#:

 9405503699300019740866| Trans.\#: |  | 544895944 | Priority Mail® Postage: | \$7.95 |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 09/30/2021 |  | \$7.95 |
| Expected $10102 / 2021$ |  |  |  |  |
| Delivery Date: 10/02/2021 |  |  |  |  |
| From: | CHUCK REGULBUTO |  |  |  |
|  | NORTHEAST SITE SOLUTIONS |  |  |  |
|  | 1053 FARMINGTON AVE STE G |  |  |  |
|  | FARMINGTON CT 06032-1574 |  |  |  |
| To: | PAUL J CAVANNA |  |  |  |
|  | 80 WOODLAND ST |  |  |  |
|  | S GLASTONBURY CT 06073-2715 |  |  |  |
| * Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking(B) service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date. |  |  |  |  |




[^0]:    This data \& map is a user generated static output from an Internet mapping site and is for reference only. Data that appears on this form may or may not be accurate, current, or otherwise reliable. Any questions on the data provided above should be directed to the Town of Glastonbury Property Assessment Office 860-652-7600.

[^1]:    Note: Proposed equipment shown in bold.
    Note: Other existing loading can be found on the tower profile attached.
    Note: All proposed feedlines for DISH Wireless are to be placed inside the monopole tower.
    Note: The remainder of $\mathbf{8 , 5 0 0} \mathbf{s q}$. in. for DISH Wireless have been included in this analysis.

[^2]:    Use ASCE 10 X-Brace Ly Rules
    $\sqrt{ }$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression
    $\sqrt{ }$ All Leg Panels Have Same Allowable Offset Girt At Foundation
    $\sqrt{ }$ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption Poles
    $\sqrt{ }$ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

