## CC CROWN CASTLE

Crown Castle 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065

July 17, 2019

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

#### RE: Notice of Exempt Modification for T-Mobile: 871584 - T-Mobile Site ID: CT11189E 115 Birch Mountain Road, Glastonbury, CT 06033 Latitude: 41° 42′ 32.24″ / Longitude: -72° 28′ 24.41″

Dear Ms. Bachman:

T-Mobile currently maintains six (6) total antennas at the 182-foot mount on the existing 200-foot Self Support Tower, located at 115 Birch Mountain Road, Glastonbury, CT. The tower is owned by Crown Castle and the property is owned by Scarrone Park LLC . T-Mobile now intends to replace three (3) existing antennas with three (3) new 600/700 MHz antennas at the 182-foot mount. T-Mobile is also proposing tower mount modifications as shown on the enclosed mount analysis.

#### **Planned Modifications:**

Tower:

Remove: (3) 1 5/8" Coax (3) Diplexers

<u>Remove and Replace</u>: (3) LNX 6515DS-A1M Antenna (**REMOVE**) - (3) RFS-APXVAARR24\_43-U-NA20 Antenna 600/700 MHz (**REPLACE**)

(3) RRUS11 B12 (REMOVE) – (3) Radio 4449 B71/B12 (REPLACE)

Install New: (3) 1 5/8" Hybrid Fiber Line

Existing to Remain: (9) 1 5/8" Coax (3) RFS-APXV18-209015-C-A20 Antenna 1900 MHz (3) TMA Ground:

The Foundation for a Wireless World.

CrownCastle.com

Page 2

Upgrade: Internal upgrade to existing ground cabinet.

The facility was approved by the Town of Glastonbury Zoning Board of Appeals on August 7, 1998. This approval was made without conditions.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Richard Johnson, Town of Glastonbury Town Manager, Peter Carey, Building Official, Crown Castle as the tower owner, and Scarrone Park LLC, the property owner.

- 1. The proposed modifications will not result in an increase in the height of the existing tower.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Anne Marie Zsamba.

Sincerely,

Anne Marie Zsamba Real Estate Specialist 3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065 (201) 236-9224 AnneMarie.Zsamba@crowncastle.com

Attachments

Melanie A. Bachman

Page 3

cc:

Richard Johnson, Town Manager Town of Glastonbury Town Hall – 2<sup>nd</sup> Floor 2155 Main Street Glastonbury, CT 06033 860.652.7500

Peter Carey, Building Official Town of Glastonbury Town Hall – 2<sup>nd</sup> Floor 2155 Main Street Glastonbury, CT 06033 860.652.7524

Scarrone Park LLC, Property Owner C/O Maria A. Toczyska 3385 Hebron Avenue Glastonbury, CT 06033 860.306.3849

Crown Castle, Tower Owner



1. Use the 'Print' button on this page to print your label to your laser or inkjet printer.

2. Fold the printed page along the horizontal line.

3. Place label in shipping pouch and affix it to your shipment so that the barcode portion of the label can be read and scanned.

Warning: Use only the printed original label for shipping. Using a photocopy of this label for shipping purposes is fraudulent and could result in additional billing charges, along with the cancellation of your FedEx account number.

Use of this system constitutes your agreement to the service conditions in the current FedEx Service Guide, available on fedex.com.FedEx will not be responsible for any claim in excess of \$100 per package, whether the result of loss, damage, delay, non-delivery,misdelivery,or misinformation, unless you declare a higher value, pay an additional charge, document your actual loss and file a timely claim.Limitations found in the current FedEx Service Guide apply. Your right to recover from FedEx for any loss, including intrinsic value of the package, loss of sales, income interest, profit, attorney's fees, costs, and other forms of damage whether direct, incidental,consequential, or special is limited to the greater of \$100 or the authorized declared value. Recovery cannot exceed actual documented loss.Maximum for items of extraordinary value is \$1,000, e.g. jewelry, precious metals, negotiable instruments and other items listed in our ServiceGuide. Written claims must be filed within strict time limits, see current FedEx Service Guide.



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# Exhibit A

**Property Card** 

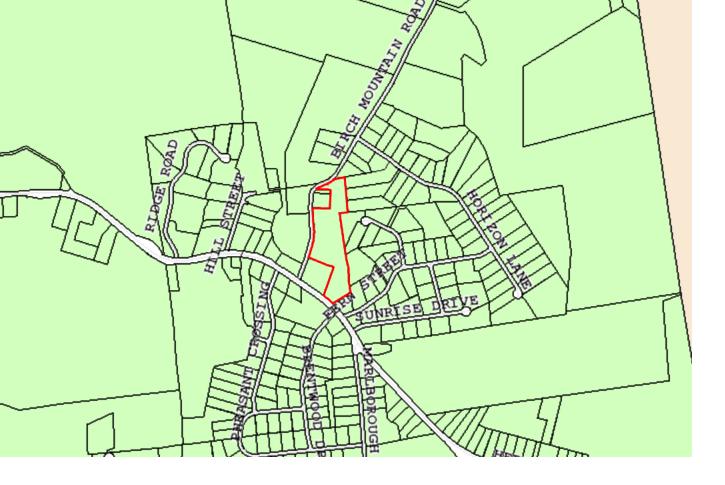
## Town of Glastonbury GIS Parcel Report

(GIS)

Owner o	f Record			Αςςοι	int Number: 29	203387	
GIS ID:	04200115			– Prope	rty Address: 11	5 BIRCH MOU	JNTAIN RD
Owner:	SCARRONE PARK I	LC		}	}	15	
Co-Owner:	C/O TOCZYSKA MA	RIA A		_ L		$\leq$ $\vdash$	/
Address:	3385 HEBRON AVE			3	71 IF		
	GLASTONBURY, CI	06033-2806					
Parcel I	nformation				7	-	$\mathbf{T}$
Map/Street/Lot	t N6 / 2920	/ E0001C Property	<b>ID:</b> 13487	-	/ 11		$\nabla \mathcal{A}$
Developer Lot I	<b>D:</b> B	Water:	Well	$\gamma$			
Parcel Acreage:	11.54	Sewer:	Septic			- V ,	(l+
Zoning Code:	RR	Census:	5202.01	4	$\rightarrow \parallel$		5 -11
Valuatio	n Summary				HIP.		$\times / \mathbb{N}$
Item	Appraised	Value As	ssessed Value		HEBROM	7	AK
Buildings	0	0		$\sim$	A AKE		$( \setminus \mathbb{Y} / )$
Land	808600	56	6000			An I	
Appurtenances	800	60	00				XL
Total	809400	50	66600	Property	highlighted in blue		
		Owner of Record			Deed / Page	Sale Date	Sale Price
		SCARRONE PARK LLC	2		3525/0218	11/15/2018	0
		TOCZYSKA MARIA A			3525/0216	11/15/2018	0
Ru	ilding	SCARRONE CAROLYN	N R REVOCABLE TRUST		3468/0328	01/22/2018	0
	U	SCARRONE CAROLYN	N R REVOCABLE TRUST		1829/0101	06/03/2003	0
Pi	cture	SCARRONE CAROLYN	N R		1261/0312	07/29/1999	0
	Not	SCARRONE CAROLYN	N R		0544/0017	04/10/1990	0
App	olicable						

Building Information			Building 1	<b>D</b> 0	
Year Constructed : Building Type : Style : Occupany : Stories : Building Zone : Roof Type : Roof Material : Est. Gross S.F. : Est. Living S.F. :	Nur Nur Ext Inte Inte Air Hea	mber of Rooms : mber of Bedrooms : mber of Bathrooms : mber of Half-Baths : erior Wall : erior Wall : erior Floor : erior Floor #2 : Conditioning Type : at Type :		Building Sketch Not Applicabl	e
Subarea Type Est. (	Gross S.F.	Est. Living S.F.	Outbuilding Type	Est. Gross S.F.	Comments
			Shed-Metal-Storage	168.00	

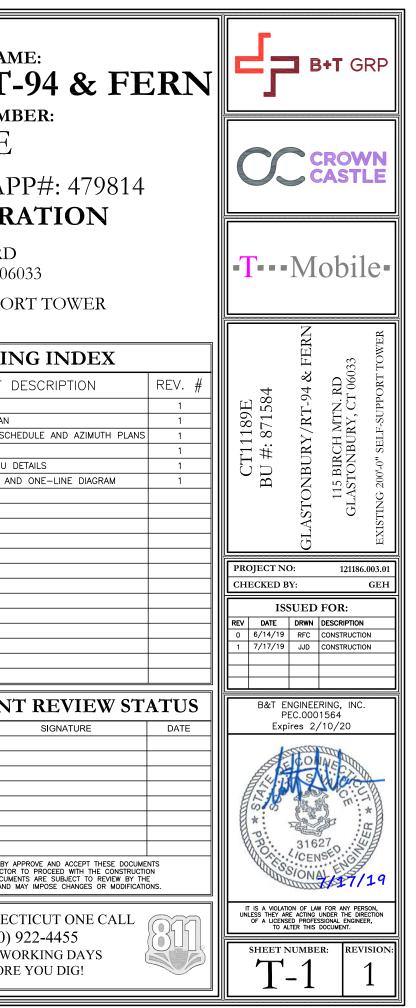
This data & map is a user generated static output from an Internet mapping site and is for reference only. Data that appears on this form may or may not be accurate, current, or otherwise reliable. Any questions on the data provided above should be directed to the Town of Glastonbury Property Assessment Office 860-652-7600.

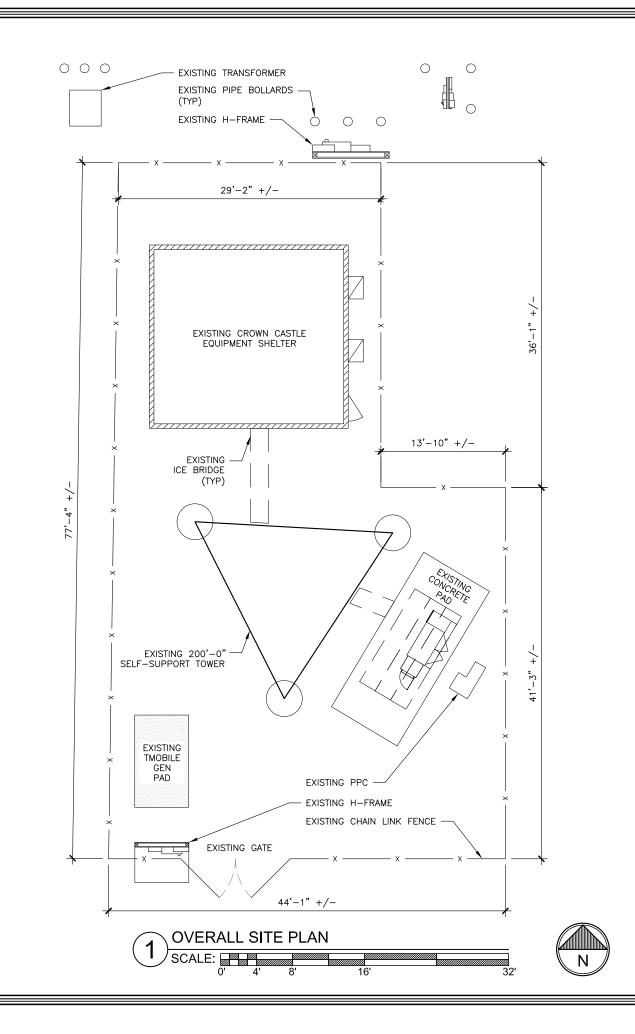


# Exhibit B

**Construction Drawings** 

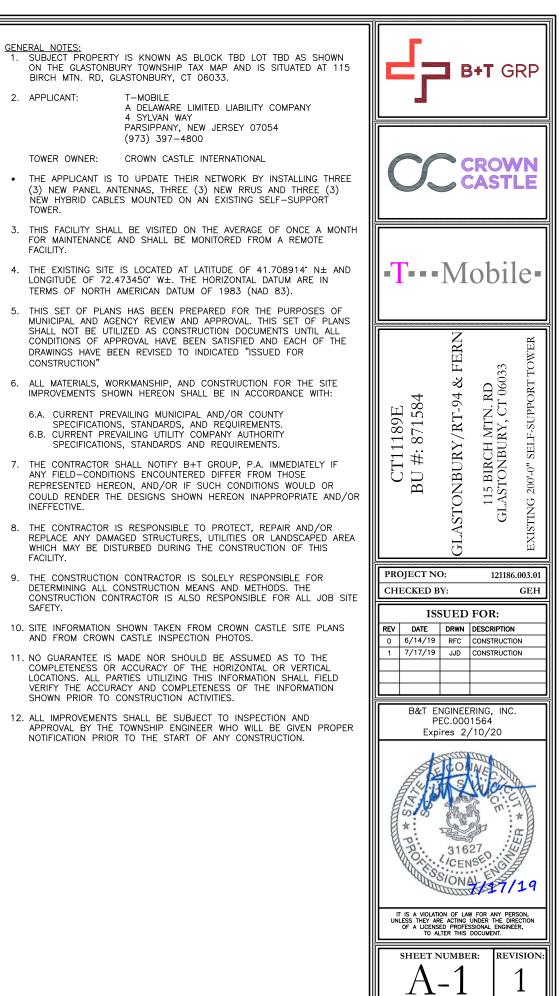
	Aobil	GLASTON T CROWN 67D04	T-MOBILE SITE NA BURY/RT -MOBILE SITE NUM CT11189E BU: 871584 / A G CONFIGUI 115 BIRCH MTN. R GLASTONBURY, CT ( NG 200'-0" SELF-SUPPO
PROJECT SUMMARY	LOCATI	ON MAP	DRAW
SITE TYPE: EXISTING EQUIPMENT UPGRADE SITE ADDRESS: 115 BIRCH MTN. RD GLASTONBURY, CT 06033 JURISDICTION: HARTFORD COUNTY	Reservoir	DH TOM HILL	SHEET # SHEET T-1 TITLE SHEET A-1 OVERALL SITE PLA A-2 ANTENNA/CABLE S A-3 TOWER ELEVATION A-4 ANTENNA AND RRL E-1 PANEL SCEHDULE
NAD83         LATITUDE:       41.708914* N         LONGITUDE:       72.473450* W         TOWER OWNER:       CROWN CASTLE         3200 HORIZON DHIVE, SUITE 150         KING OF PRUSSIA, PA 19406         JASON SMITH         (610)         635–3225         CUSTOMER/APPLICANT:       T-MOBILE         4 SYLVAN WAY         PARSIPPANY, NJ 07054         (973)       397–4800         OCCUPANCY TYPE:       UNMANNED         A.D.A. COMPLIANCE:       FACILITY IS UNMANNED AND NOT		He Bailey St.	
CONTACT INFORMATION		IRECTIONS	A/E DOCUMEN
A&E FIRM: B+T GROUP 1717 S. BOULDER, STE. 300 TULSA, OK 74119 CONTACT: MIKE OAKES PHONE: (918) 587-4630 BELECTRIC N/A PROVIDER: N/A TELCO AT&T PROVIDER: 855-637-9527	DEPART FROM BRADLEY INTERNATIONAL AIRPORT ON TERMINAL RD. RC	DAD NAME CHANGES TO BRADLEY FIELD CONNECTOR. ROAD NAME T) ONTO I—91 [RICHARD P HORAN MEMORIAL HWY]. AT EXIT 30, TAKE IT—2 [VETERANS OF FOREIGN WARS MEM'L HWY]. AT EXIT 8, KEEP	TITLE T-MOBILE PROP: T-MOBILE R.F. MGR.: T-MOBILE NetOps: T-MOBILE CONST. MGR.:
	<b>PROJECT DESCRIPTION</b>	<b>DO NOT SCALE DRAWINGS</b>	INTERCONNECT:
CODE COMPLIANCE         ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN         ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES         AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE         PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO         THESE CODES: <u>CODE TYPE</u> BUILDING/DWELLING         BUILDING/DWELLING         IBC 2015         STRUCTURAL         MECHANICAL         IMC 2015         ELECTRICAL	THE PROPOSED PROJECT INCLUDES: • REMOVE (3) EXISTING ANTENNAS AT 177'-0". • REMOVE (3) 1 5/8" COAX. • REMOVE (3) 1 5/8" COAX. • REMOVE (3) EXISTING RRUS AT 177'-0". • REPLACE (1) DUS41 WITH (2) BB6630s • INSTALL (3) NEW ANTENNAS AT 177'-0". • INSTALL (3) NEW RRUS AT 177'-0". • INSTALL (3) NEW RRUS AT 177'-0". • INSTALL (1) NEW SSC • INSTALL (3) NEW HYBRID CABLES. • MODIFY EXISTING MOUNTS PER MOUNT ANALYSIS BY PAUL J. FORD DATED 5/2/19.	ALL DRAWINGS CONTAINED HEREIN ARE FORMATTED FOR 11X17. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.	PROPERTY OWNER: PLANNING: THE FOLLOWING PARTIES HEREE AND AUTHORIZE THE CONTRAC DESCRIBED HEREIN. ALL DOC LOCAL BUILDING DEPARTMENT AN CALL CONNI (800) CALL 3 V BEFO





BIRCH MTN. RD. GLASTONBURY, CT 06033. 2. APPLICANT: T-MOBILE TOWER OWNER:

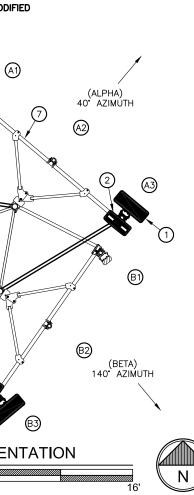
- TOWER
- FACILITY.
- CONSTRUCTION'
- INEFFECTIVE.
- FACILITY.
- SAFETY
- AND FROM CROWN CASTLE INSPECTION PHOTOS.

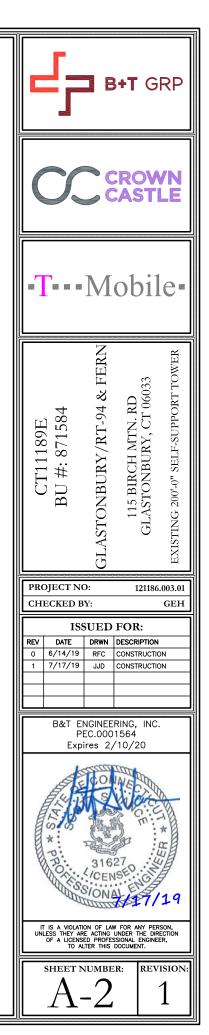


	I	END	
	EXISTING/DEMOLITION NOTES		INSTALLATION NOTES
	EXISTING RFS-APXV18-209015-C-A20 ANTENNA TO REMAIN (TOTAL OF 3)	1	INSTALL RFS APXVAARR24_43-U-NA20 (8 FT ANTENNAS. PROVIDE NEW 2 7/8" OD SCH.40 PIPE MAST (LENGTH TO BE V.I.F) (TYP. OF 1 PER SECTOR, TOTAL OF 3)
B	EXISTING RRUS11 B12 TO BE REMOVED (TOTAL OF 3)	2	INSTALL RADIO 4449 B12/B71 (TYP. OF 1 PER SECTOR, TOTAL OF 3)
⊘	REMOVE (3) 1 5/8" COAX	3	INSTALL (3) NEW 6X12 HCS
	EXISTING DUS41 TO BE REMOVED	4	INSTALL (2) NEW BB6630
(E)	EXISTING TWIN STYLE 1A TMAS TO REMAIN (TOTAL OF 3)	5	INSTALL NEW SSC
F	EXISTING RBS 6201 ODE CABINET TO REMAIN	6	INSTALL SITEPRO1 STK-U STIFF ARM KIT OR EOR APPROVED EQUIVALENT
6	EXISTING LNX-6515DS-A1M ANTENNA TO BE REMOVED (TOTAL OF 3)	0	REPLACE EXISTING MOUNT PIPES WITH NEW 8FT LONG P2.0 X-STR (2.38" O.D. x .204") WHERE REQUIRED
(H)	EXISTING DIPLEXERS TO BE REMOVED		

ANTENNA AND CABLE SCHEDULE											
SECTOR	POSITION	EXISTING ANTENNAS	PROPOSEE CONFIGI		E-TILT	M-TILT	ANTENNA CENTERLINE	TMA/RRU	CABLES	JUMPER TYPE	CABLE LENGTH
	A1	RFS APXV18-209015-C-A20	G19 L19	_	2*	0°		1/0	(2) 1 5/8" COAX	_	215'-0"
40° – ALPHA	A2	-	-	-	-	-	177'-0"	-	-	-	-
	A3	RFS APXVAARR24_43-U-NA20	L600 L700	B71 + B12	2./2.	°,		0/1	(1) 1 5/8" HYBRID	(4) COAX	215'–0"
	B1	RFS APXV18-209015-C-A20	G19 L19	I	2*	0°		1/0	(2) 1 5/8" COAX	_	215'-0"
140° – BETA	B2	_	-	-	-	I	177'-0"	_	-	-	_
	B3	RFS APXVAARR24_43-U-NA20	L600 L700	B71 + B12	2°/2°	0°		0/1	(1) 1 5/8" HYBRID	(4) COAX	215'–0"
	G1	RFS APXV18-209015-C-A20	G19 L19	-	2*	0°		1/0	(2) 1 5/8" COAX	-	215'-0"
260° – GAMMA	G2	-	-	1	-	I	177'–0"	_	-	-	-
	G3	RFS APXVAARR24_43-U-NA20	L600 L700	B71 + B12	2./2.	ð		0/1	(1) 1 5/8" HYBRID	(4) COAX	215'–0"

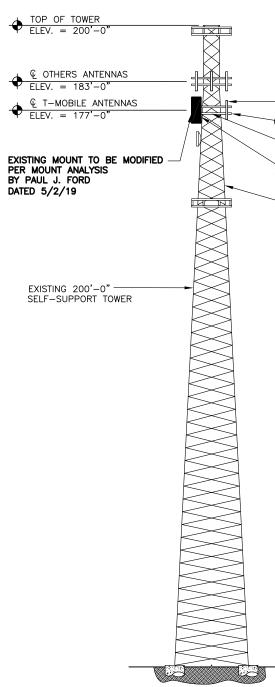
EXISTING MOUNT TO BE MODIFIED PER MOUNT ANALYSIS BY PAUL J. FORD DATED 5/2/19 A1)  $\langle A \rangle$  $\langle E \rangle$ (ALPHA) 40° AZIMUTH EXISTING CROWN CASTLE EQUIPMENT SHELTER (A2) (B) 6  $\langle \circ \rangle$ E. A3 © 3 Ó É É Ĥ 3 4 5 ×9 >P 8 - EXISTING T-MOBILE ICE BRIDGE **B1** (GAMMA) 260° AZIMUTH ©2 (GAMMA) 260° AZIMUTH **D** (DA) 82 ©1 ©1) (BETA) 140° AZIMUTH EXISTING 200'-0" SELF-SUPPORT TOWER B3 **EXISTING ANTENNA ORIENTATION** PROPOSED ANTENNA ORIENTATION ENLARGED AREA PLAN 3 2 1 SCALE: SCALE: SCALE: Ν 16'





LEGEND							
	EXISTING/DEMOLITION NOTES		INSTALLATION NOTES				
A	EXISTING RFS-APXV18-209015-C-A20 ANTENNA TO REMAIN (TOTAL OF 3)	1	INSTALL RFS APXVAARR24_43-U-NA20 (8 FT) ANTENNAS. PROVIDE NEW 2 7/8" OD SCH.40 PIPE MAST (LENGTH TO BE V.I.F) (TYP. OF 1 PER SECTOR, TOTAL OF 3)				
∕₿〉	EXISTING RRUS11 B12 TO BE REMOVED (TOTAL OF 3)	2	INSTALL RADIO 4449 B12/B71 (TYP. OF 1 PER SECTOR, TOTAL OF 3)				
⊘	REMOVE (3) 1 5/8" COAX	3	INSTALL (3) NEW 6X12 HCS				
	EXISTING DUS41 TO BE REMOVED	4	INSTALL (2) NEW BB6630				
E	EXISTING TWIN STYLE 1A TMAS TO REMAIN (TOTAL OF 3)	5	INSTALL NEW SSC				
F	EXISTING RBS 6201 ODE CABINET TO REMAIN	6	INSTALL SITEPRO1 STK-U STIFF ARM KIT OR EOR APPROVED EQUIVALENT				
6	EXISTING LNX-6515DS-A1M ANTENNA TO BE REMOVED (TOTAL OF 3)	0	REPLACE EXISTING MOUNT PIPES WITH NEW 8FT LONG P2.0 X-STR (2.38" O.D. x .204") WHERE REQUIRED				
(H)	EXISTING DIPLEXERS TO BE REMOVED						

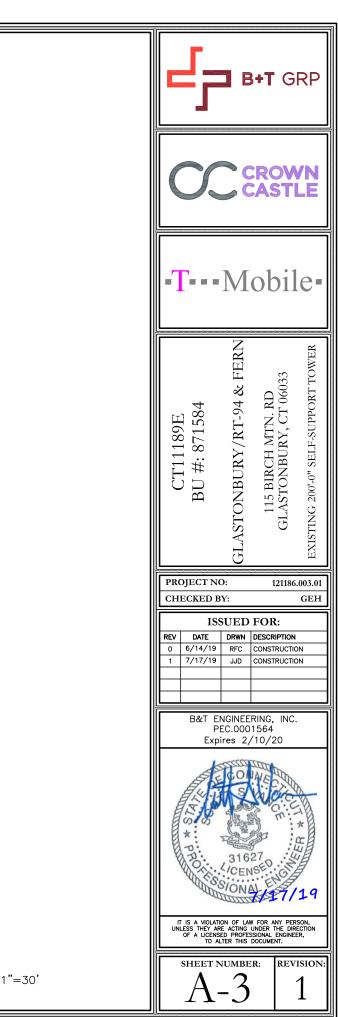
EXISTING MOUNT IS SUFFICIENT PER STRUCTURAL ANALYSIS BY PIER STRUCTURAL ENGINEERING GROUP DATED 5/22/19.

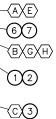


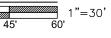
TOWER ELEVATION

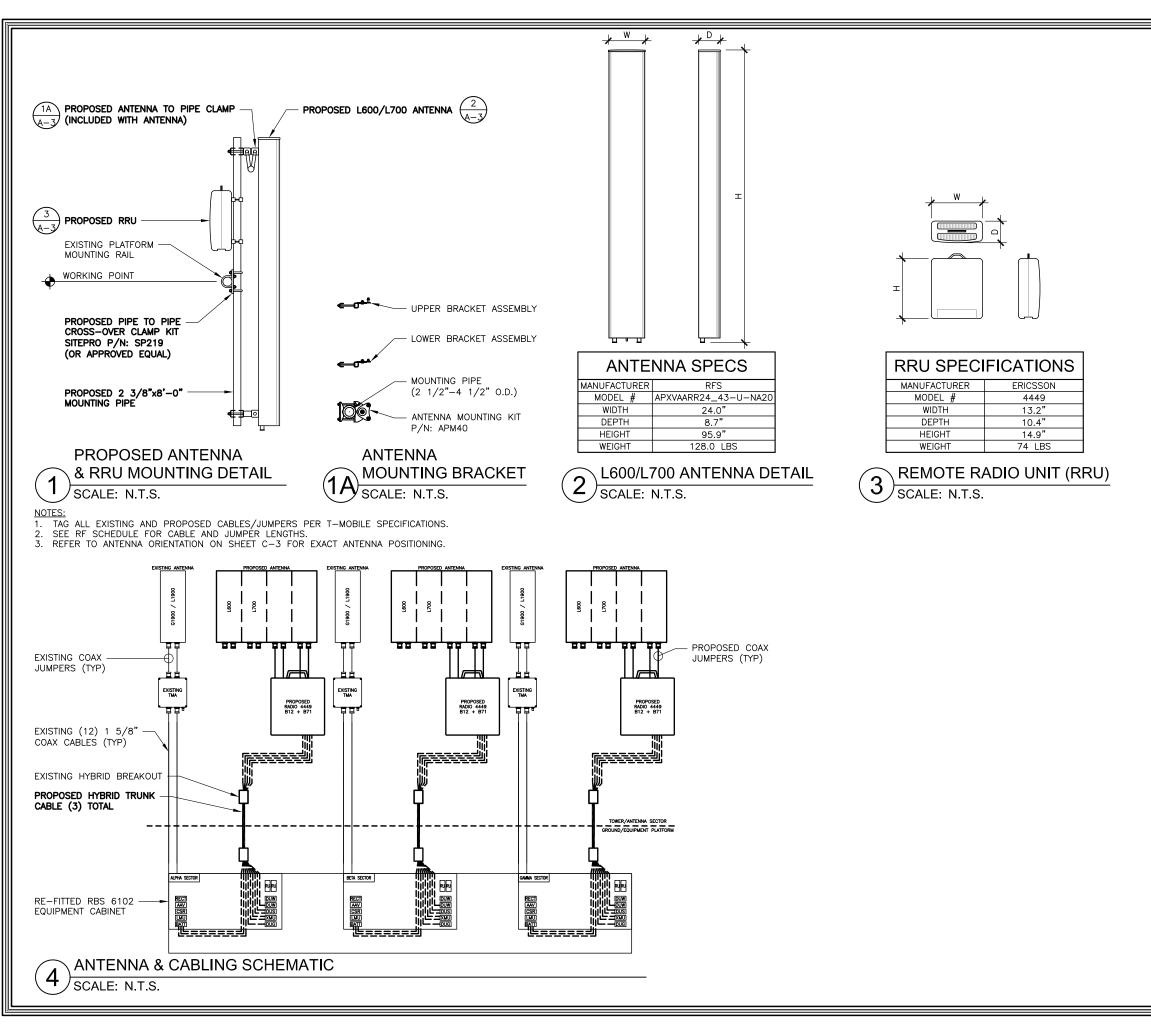
SCALE:

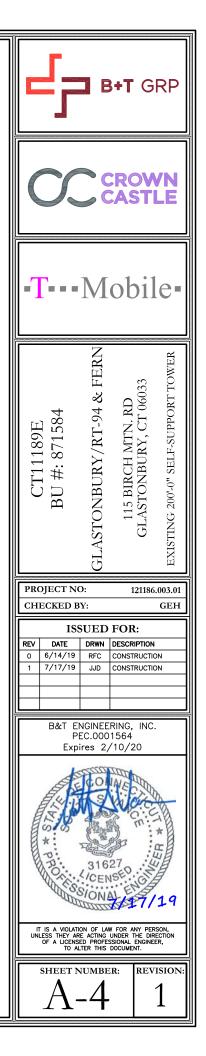
1











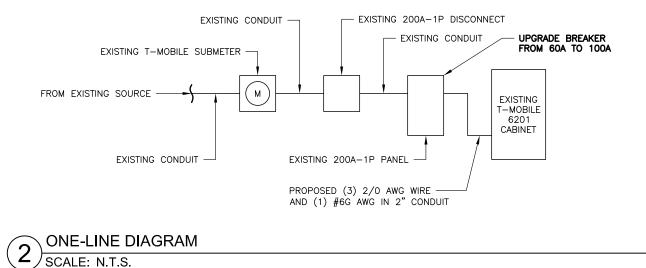
FINAL PANEL SCHEDULE									
LOAD	POLES	AMPS	L1	BUS L2	L3	AMPS	POLES	LOAD	
EQUIPMENT	2	_	1		2	100	2	RBS 6201	
			3		4				
			5		6	20	1	EQUIPMENT	
			7		8				
			9		10				
			11		12				
			13		14				
			15		16				
			17		18				
RATED VOLTAGE: ■120/240 □	3 PHASE	E, 4 WIRE	BRA	NCH	POLES	: 🗆 12 🛛	24 🗆 30	□42 APPROVED MF'RS	
RATED AMPS: □100 ■225 □400 □				BINET:	SU	RFACE 🗆	FLUSH	NEMA □1 🖬 3R □4X	
□ MAIN LUGS ONLY MAIN 200 AMPS ■ BREAKER □ FUSED SWITCH				INGED	DOOF			KEYED DOOR LATCH	
□FUSED ■CIRCUIT BREAKER BRANCH DEVICES				□ TO BE GFCI BREAKERS FULL NEUTRAL BUS GROUND BAR					
ALL BREAKERS MUST BE RATED TO INTERRUF	PT A SHOR	T CIRCUIT	ISC (	OF 10	,000	AMPS SYN	IMETRICAL		

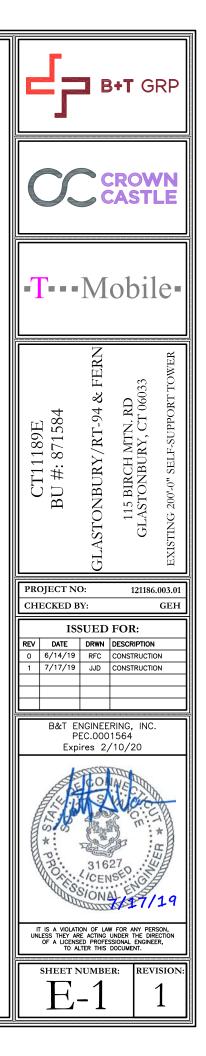
REPLACE EXISTING 60A BREAKER IN POSITION 2 AND 4 W/ NEW 100A BREAKER INSIDE PANEL

REPLACE EXISTING WIRES FOR EXISTING 6201 CABINET WITH (3) 2/0 AWG THWN (COPPER) AND (1) #6G AWG. MINIMUM CONDUIT SIZE TO BE 2" FINAL PANEL DESIGN AND CALCULATIONS FOR WIRE SIZE WERE BASED OFF OF EXISTING PHOTOS

#### FINAL T-MOBILE PANEL DETAIL 1







# Exhibit C

**Structural Analysis Report** 



July 16, 2019

Pier Structural Engineering Corp. 55 Northfield Drive E, Suite 198 Waterloo, ON N2K 3T6 Tel: 519-885-3806 Fax: 519-884-3806 www.p-sec.ca

Heather Simeone, Tower Structural Analyst Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277

Subject:	Structural Analysis Report	
Carrier Designation:	Carrier Co-Locate: Carrier Site Number: Carrier Site Name:	T-Mobile CT11189E Glastonbury/ Rt-94 & Fern
Crown Castle Designation:	Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number: Crown Castle WO Number: Crown Castle Order Number:	871584 John Tom Hill 559293 1729843 479814 Rev. 0
Engineering Firm Designation:	P-SEC Project Number:	19994
Site Data:	115 Birch Mtn. Road, GLASTONBL Latitude <i>41° 42' 32.24"</i> , Longitude 200-ft Self Support Tower	

Dear Heather Simeone,

Pier Structural Engineering Corp. (P-SEC) is pleased to submit this "**Structural Analysis Report**" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1378321, in accordance with order 479814, revision 0.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration

#### Sufficient Capacity-92.3%

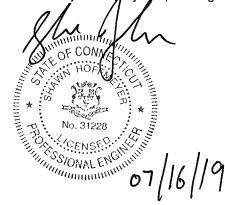
This analysis has been performed in accordance with the 2018 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 125 mph. Exposure Category C and Risk Category II were used in this analysis.

We at P-SEC appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared by: Tariq Hasan, E.I.T.

Respectfully submitted by:

Shawn Hoffmeyer, P.E., P.Eng. *CT PE# 31228* tnxTower Report - version 8.0.5.0





July 16, 2019

Pier Structural Engineering Corp. 55 Northfield Drive E, Suite 198 Waterloo, ON N2K 3T6 Tel: 519-885-3806 Fax: 519-884-3806 www.p-sec.ca

Heather Simeone, Tower Structural Analyst Crown Castle 3530 Toringdon Way Suite 300 Charlotte, NC 28277

Subject:	Structural Analysis Report	
Carrier Designation:	Carrier Co-Locate: Carrier Site Number: Carrier Site Name:	T-Mobile CT11189E Glastonbury/ Rt-94 & Fern
Crown Castle Designation:	Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number: Crown Castle WO Number: Crown Castle Order Number:	871584 John Tom Hill 559293 1729843 479814 Rev. 0
Engineering Firm Designation:	P-SEC Project Number:	19994 Rev. 2
Site Data:	115 Birch Mtn. Road, GLASTONBU Latitude <i>41° 42' 32.24"</i> , Longitude 200-ft Self Support Tower	

Dear Heather Simeone,

Pier Structural Engineering Corp. (P-SEC) is pleased to submit this "**Structural Analysis Report**" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 1378321, in accordance with order 479814, revision 0.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration

#### Sufficient Capacity-92.3%

This analysis has been performed in accordance with the 2018 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 125 mph. Exposure Category C and Risk Category II were used in this analysis.

We at P-SEC appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared by: Tariq Hasan, E.I.T.

Respectfully submitted by:

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tnxTower Output

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#### 1) INTRODUCTION

This tower is a 200-ft Self Support tower originally designed by SABRE COMMUNICATIONS in November of 1998 for a wind speed of 85 mph per TIA/EIA-222-F.

#### 2) ANALYSIS CRITERIA

The following design para	ameters have	been used in our analysis:
Design Standard:		TIA-222-H Standard
County/State:		Hartford County, CT
Wind Speeds:	CASE 1	125 mph (3-second gust)
	CASE 2	50 mph (3-second gust) with 2" radial solid ice
	CASE 3	60 mph (3-second gust) for serviceability
Exposure Category:		С
Topographic Category:		1
Risk Category:		II

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)			
	183	3	ericsson	KRY 112 489/2					
	182	182	100	100	3	SitePro1	15' Sector Frame		
182			3	SitePro1	STK-U Stiff Arm Kit	12	1-5/8		
102		3	rfs celwave	APXV18-209015-C-A20	12	1-5/6			
	177	3	rfs celwave	APXVAARR24_43-U-NA20	-				
		3	ericsson	RADIO 4449 B12/B71					

#### **Table 1 - Proposed Equipment Configuration**

#### Table 2 - Other Considered Equipment

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
	208	1	rfs celwave	ALR10-O		
		1	decibel	DB225-A		
198	205	1	rfs celwave	PD1107-1	3	7/8
190		1	rfs celwave	PD201-7	2	1/2
	204	1	scala OGB6-928N			1
	198	1		Sector Mount [SM 702-3]		
		3	commscope	NNVV-65B-R4	4	
	171	3	rfs celwave	APXVTM14-ALU-I20		1-1/4
170		3	alcatel lucent	PCS 1900MHZ 4X45W- 65MHZ		
		6	alcatel lucent	RRH2X50-800		
		3	alcatel lucent	TD-RRH8X20-25		
	170	1		Sector Mount [SM 506-3]		
400	400	1	kathrein	PR-850		4/0
163	163	1		Pipe Mount [PM 601-1]	1	1/2
	155	1	sinclair	SRL480N1DT4		7/0
144	152	2	rfs celwave	PD1109-1	2	7/8 1/2
	144	1		Sector Mount [SM 702-3]	3	1/2

	inting el (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
Ę	53	55	1	lucent	KS24019-L112A	1	1/2

#### 3) ANALYSIS PROCEDURE

#### Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	C Welti Assoc. dated 8/21/1998	1404208	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Sabre, Proj. No. 98-10044 dated 11/3/1998	2068370	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Sabre, Proj. No. 98-10044 dated 11/24/1998	1403674	CCISITES
APPLICATION	T-Mobile, Revision #0 dated 4/17/2019	479814	CCISITES

#### 3.1) Analysis Method

tnxTower (8.0.5.0), a commercially available analysis software package, was used to create a threedimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower\structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) P-SEC did not analyze antenna supporting mounts as part of this analysis report and assumed they are structurally sufficient. It is the carrier's responsibility to ensure structural compliance of their existing and/or proposed antenna supporting mounts.
- 5) The existing base plate grout was not considered in this analysis.
- 6) All equipment model numbers, quantities, and centerline elevations are as provided in the CCI CAD package dated 04/22/2019.

This analysis may be affected if any assumptions are not valid or have been made in error. P-SEC should be notified to determine the effect on the structural integrity of the tower.

#### 4) ANALYSIS RESULTS

Section No.	Elevation (ft)	Component Type	Size	Critical Element	Р (К)	SF*P_allow (K)	% Capacity	Pass / Fail
T1	200 - 180	Leg	Sabre 2.875x.375	2	-17.997	100.371	17.9	Pass
T2	180 - 160	Leg	Sabre 3.5 x .3	31	-59.264	116.342	50.9	Pass
Т3	160 - 140	Leg	Sabre 4 x .318	58	-100.568	149.087	67.5	Pass
T4	140 - 120	Leg	Sabre 4.5 x .438	85	-138.479	211.276	65.5	Pass
T5	120 - 100	Leg	Sabre 5.5625 x .375	106	-174.468	251.617	69.3	Pass
T6	100 - 80	Leg	Sabre 5.5625 x .375	127	-208.709	251.617	82.9	Pass

#### Table 4 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	Р (К)	SF*P_allow (K)	% Capacity	Pass / Fail
T7	80 - 60	Leg	Sabre 6.625 x .432	148	-239.282	319.517	74.9	Pass
T8	60 - 40	Leg	Sabre 8.625 x .322	163	-271.672	351.500	77.3	Pass
Т9	40 - 20	Leg	Sabre 8.625 x .5	178	-304.055	531.396	57.2	Pass
T10	20 - 0	Leg	Sabre 8.625 x .5	193	-335.569	531.396	63.1	Pass
T1	200 - 180	Diagonal	L1 3/4x1 3/4x3/16	10	-3.678	13.849	26.6 42.0 (b)	Pass
T2	180 - 160	Diagonal	L1 3/4x1 3/4x3/16	34	-5.312	9.465	56.1 64.5 (b)	Pass
Т3	160 - 140	Diagonal	L1 3/4x1 3/4x3/16	61	-5.873	6.536	89.9	Pass
T4	140 - 120	Diagonal	L2 1/2x2 1/2x3/16	88	-6.537	12.361	52.9 62.7 (b)	Pass
T5	120 - 100	Diagonal	L2 1/2x2 1/2x3/16	109	-6.776	9.610	70.5	Pass
Т6	100 - 80	Diagonal	L3x3x3/16	130	-7.202	13.184	54.6 64.7 (b)	Pass
Τ7	80 - 60	Diagonal	L3 1/2x3 1/2x1/4	151	-8.531	18.994	44.9 54.9 (b)	Pass
T8	60 - 40	Diagonal	L3 1/2x3 1/2x1/4	166	-9.356	16.226	57.7	Pass
Т9	40 - 20	Diagonal	L3 1/2x3 1/2x1/4	181	-9.909	13.726	72.2	Pass
T10	20 - 0	Diagonal	L4x4x1/4	196	-10.995	17.670	62.2 65.7 (b)	Pass
T1	200 - 180	Top Girt	L1 3/4x1 3/4x3/16	5	-0.138	7.657	1.8	Pass
							Summary	
						Leg (T6)	82.9	Pass
						Diagonal (T3)	89.9	Pass
						Top Girt (T1)	1.8	Pass
						Bolt Checks	69.8	Pass
						RATING =	89.9	Pass

#### Table 5 - Tower Component Stresses vs. Capacity

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail				
2	Anchor Rods		62.0	Pass				
2	Base Foundation - Soil		52.2	Pass				
2	Base Foundation - Structural		92.3	Pass				
	Structure Rating (max from all components) = 92.3%							
Notes:	Notes: 1) See full member breakdown and section capacities in Appendix A.							

1) See full member breakdown and section capacities in Appendix A.

2) See additional documentation in Appendix C for supporting calculations. .

#### 4.1) Recommendations

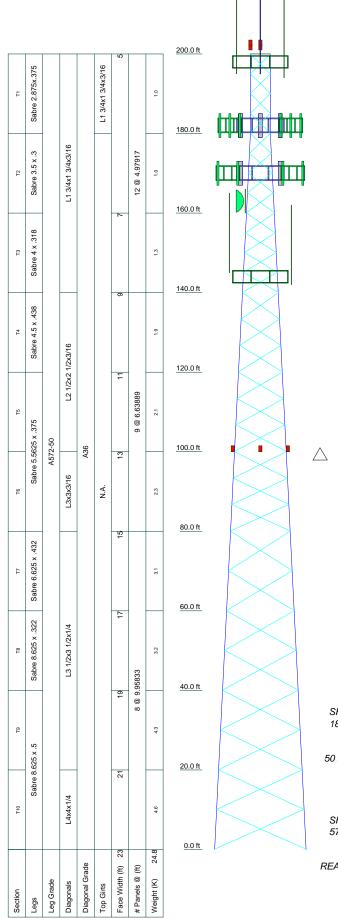
The tower and its foundation have sufficient capacity to carry the proposed loading configuration.

No modifications are required at this time.

Should you have any questions, please call us anytime at 519-885-3806.

encl. 871584\_479814 SA Report\_20190716.doc APPENDIX A

#### **TNXTOWER OUTPUT**



	MATERIAL STRENGTH							
	GRADE	Fy	Fu	GRADE	Fy	Fu		
A	4572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi		

#### **TOWER DESIGN NOTES**

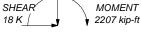
- 1. Tower is located in Hartford County, Connecticut.
- Tower designed for Exposure C to the TIA-222-H Standard. 2.
- 3. Tower designed for a 125 mph basic wind in accordance with the TIA-222-H Standard. 4. Tower is also designed for a 50 mph basic wind with 2.00 in ice. Ice is considered to increase in thickness with height.
- 5
- Deflections are based upon a 60 mph wind. Tower Risk Category II. 6. Topographic Category 1 with Crest Height of 0' 7.
- 8. TheTIA-222-H Annex S
- 9.
- 10. E - Existing, R/MLA - Reserved, P - Proposed
- 11. Proposed loading at 182ft elevation
- 12. Reserved loading at 170ft elevation
- 13. TOWER RATING: 89.9%

ALL REACTIONS ARE FACTORED

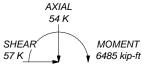
MAX. CORNER REACTIONS AT BASE: DOWN: 343 K SHEAR: 35 K

> UPLIFT: -299 K SHEAR: 31 K





TORQUE 21 kip-ft 50 mph WIND - 2.000 in ICE



TORQUE 49 kip-ft REACTIONS - 125 mph WIND



**Pier Structural Engineering** 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

5	<sup>••••</sup> PSEC 19994 (for T	-MOBILE)	
	Project: BU 871584 - JOHN T	OM HILL	
	Client: CROWN CASTLE	<sup>Drawn by:</sup> thasan	App'd:
	<sup>Code:</sup> TIA-222-H	Date: 05/09/19	Scale: NTS
	Path:	1 - 871584 - John Tom Hills71584   CZ 2019050	Dwg No. E-1

*tnxTower* 

PSEC 19994 (for T-MOBILE)

Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

**CROWN CASTLE** 

Designed by thasan

10:25:57 05/09/19

#### **Tower Input Data**

The main tower is a 3x free standing tower with an overall height of 200' above the ground line.

The base of the tower is set at an elevation of 0' above the ground line.

The face width of the tower is 5' at the top and 23' at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in Hartford County, Connecticut.

Job

Project

Client

Tower base elevation above sea level: 878'.

Basic wind speed of 125 mph.

Risk Category II.

Exposure Category C.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0'. Nominal ice thickness of 2.000 in.

Ice thickness is considered to increase with height.

Ice density of 56.000 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50.000 °F.

Deflections calculated using a wind speed of 60 mph.

TheTIA-222-H Annex S.

. . . . . . . . . . . . . . . . . . .

E - Existing, R/MLA - Reserved, P - Proposed.

Proposed loading at 182ft elevation.

Reserved loading at 170ft elevation.

A non-linear (P-delta) analysis was used. Pressures are calculated at each section.

Tower analysis based on target reliabilities in accordance with Annex S.

Load Modification Factors used:  $K_{es}(F_w) = 0.95$ ,  $K_{es}(t_i) = 0.85$ .

Stress ratio used in tower member design is 1.05.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

#### Options

Distribute Leg Loads As Uniform Consider Moments - Horizontals Assume Legs Pinned Consider Moments - Diagonals Assume Rigid Index Plate Use Clear Spans For Wind Area Use Moment Magnification  $\sqrt{}$ Use Code Stress Ratios Use Clear Spans For KL/r Retension Guys To Initial Tension Use Code Safety Factors - Guys Escalate Ice Bypass Mast Stability Checks Always Use Max Kz Use Azimuth Dish Coefficients Use Special Wind Profile Project Wind Area of Appurt. Include Bolts In Member Capacity Autocalc Torque Arm Areas Leg Bolts Are At Top Of Section Add IBC .6D+W Combination Secondary Horizontal Braces Leg

Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs Use ASCE 10 X-Brace Ly Rules

- $\sqrt{}$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA
- SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
- Consider Feed Line Torque
- Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption Poles

Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known

Consider Moments - Legs

SR Members Are Concentric

 $\sqrt{}$ Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends

*tnxTower* 

Project

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PSEC 19994 (for T-MOBILE)

Page 2 of 18

Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

**CROWN CASTLE** 

Designed by thasan

10:25:57 05/09/19

### **Tower Section Geometry**

Tower	Tower	Assembly	Description	Section	Number	Section
Section	Elevation	Database		Width	of	Length
					Sections	
	ft			ft		ft
T1	200'-180'			5'	1	20'
T2	180'-160'			5'	1	20'
T3	160'-140'			7'	1	20'
T4	140'-120'			9'	1	20'
T5	120'-100'			11'	1	20'
T6	100'-80'			13'	1	20'
T7	80'-60'			15'	1	20'
T8	60'-40'			17'	1	20'
Т9	40'-20'			19'	1	20'
T10	20'-0'			21'	1	20'

### Tower Section Geometry (cont'd)

Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Girt
Section	Elevation	Spacing	Type	K Brace	Horizontals	Offset	Offset
				End			
	ft	ft		Panels		in	in
T1	200'-180'	4'11-3/4"	X Brace	No	No	0.000	1.000
T2	180'-160'	4'11-3/4"	X Brace	No	No	0.000	1.000
T3	160'-140'	4'11-3/4"	X Brace	No	No	0.000	1.000
T4	140'-120'	6'7-21/32"	X Brace	No	No	0.000	1.000
T5	120'-100'	6'7-21/32"	X Brace	No	No	0.000	1.000
T6	100'-80'	6'7-21/32"	X Brace	No	No	0.000	1.000
T7	80'-60'	9'11-1/2"	X Brace	No	No	0.000	1.000
T8	60'-40'	9'11-1/2"	X Brace	No	No	0.000	1.000
Т9	40'-20'	9'11-1/2"	X Brace	No	No	0.000	1.000
T10	20'-0'	9'11-1/2"	X Brace	No	No	0.000	1.000

### Tower Section Geometry (cont'd)

Tower	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
Elevation ft	Type	Size	Grade	Type	Size	Grade
T1 200'-180'	Pipe	Sabre 2.875x.375	A572-50 (50 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)
T2 180'-160'	Pipe	Sabre 3.5 x .3	A572-50 (50 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)
T3 160'-140'	Pipe	Sabre 4 x .318	A572-50 (50 ksi)	Equal Angle	L1 3/4x1 3/4x3/16	A36 (36 ksi)
T4 140'-120'	Pipe	Sabre 4.5 x .438	A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T5 120'-100'	Pipe	Sabre 5.5625 x .375	A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 100'-80'	Pipe	Sabre 5.5625 x .375	A572-50 (50 ksi)	Equal Angle	L3x3x3/16	A36 (36 ksi)
T7 80'-60'	Pipe	Sabre 6.625 x .432	A572-50 (50 ksi)	Equal Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)
T8 60'-40'	Pipe	Sabre 8.625 x .322	A572-50 (50 ksi)	Equal Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)
T9 40'-20'	Pipe	Sabre 8.625 x .5	A572-50	Equal Angle	L3 1/2x3 1/2x1/4	A36

tnxTower	Job	PSEC 19994 (for T-MOBILE)	Page 3 of 18
<b>Pier Structural Engineering</b> 198-55 Northfield Drive East	Project	BU 871584 - JOHN TOM HILL	Date 10:25:57 05/09/19
Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806	Client	CROWN CASTLE	Designed by thasan

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T10 20'-0'	Pipe	Sabre 8.625 x .5	(50 ksi) A572-50 (50 ksi)	Equal Angle	L4x4x1/4	(36 ksi) A36 (36 ksi)

## Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 200'-180'	Equal Angle	L1 3/4x1 3/4x3/16	A36	Solid Round		A36
			(36 ksi)			(36 ksi)

## Tower Section Geometry (cont'd)

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	$ft^2$	in					in	in	in
T1 200'-180'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T2 180'-160'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T3 160'-140'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T4 140'-120'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T5 120'-100'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T6 100'-80'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T7 80'-60'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T8 60'-40'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T9 40'-20'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt
T10 20'-0'	0.000	0.000	A36 (36 ksi)	1.05	1	1.025	Mid-Pt	Mid-Pt	Mid-Pt

## Tower Section Geometry (cont'd)

						K Fa	ctors <sup>1</sup>			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
C.	Angles	Rounds		X	X	X	X	X	X	X
<u>Jt</u> T1 200'-180'	Yes	No	1	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>
T2 180'-160'	Yes	No	1	1 1	1 1	1 1	1 1	1 1	1 1	1 1

*tnxTower* 

Project

Client

PSEC 19994 (for T-MOBILE)

Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

10:25:57 05/09/19 Designed by thasan

		_				K Fa	ctors <sup>1</sup>			
Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
ft	Angles	Rounds		X Y	X Y	X Y	X Y	X Y	X Y	X Y
<i>J</i> *				1	1	1	1	1	1	1
T3 160'-140'	Yes	No	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T4 140'-120'	Yes	No	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T5 120'-100'	Yes	No	1	1	1	1	1	1	1	1
T6 100'-80'	Yes	No	1	1 1 1	1	1	1 1 1	1 1 1	1 1 1	1
T7 80'-60'	Yes	No	1	1	1	1	1	1	1	1
T8 60'-40'	Yes	No	1	1 1	1	1	1	1	1	1
T9 40'-20'	Yes	No	1	1 1	1 1	1 1	1 1	1 1	1 1	1 1
				1	1	1	1	1	1	1
T10 20'-0'	Yes	No	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1

## Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagor	ıal	Top G	irt	Botton	ı Girt	Mid	Girt	Long Ho	rizontal	Short Ho	orizontal
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 200'-180'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T2 180'-160'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T3 160'-140'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T4 140'-120'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T5 120'-100'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T6 100'-80'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T7 80'-60'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T8 60'-40'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T9 40'-20'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75
T10 20'-0'	0.000	1	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75	0.000	0.75

## Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagor	nal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hori	zontal	Short Hori	izontal
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T1 200'-180'	Flange	0.750	4	0.625	1	0.625	1	0.000	0	0.625	0	0.000	0	0.625	0
	-	A325X		A325X		A325X		A325N		A325N		A325N		A325N	
T2 180'-160'	Flange	1.000	4	0.625	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T3 160'-140'	Flange	1.000	4	0.625	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
	-	A325X		A325X		A325N		A325N		A325N		A325N		A325N	

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PSEC 19994 (for T-MOBILE)

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Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

#### BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

Designed by thasan

10:25:57 05/09/19

Tower	Leg	Leg		Diagor	ıal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hori	zontal	Short Hori	izontal
Elevation ft	Connection Type														
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T4 140'-120'	Flange	1.250	4	0.625	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T5 120'-100'	Flange	1.250	4	0.625	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
	-	A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T6 100'-80'	Flange	1.250	6	0.750	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T7 80'-60'	Flange	1.250	6	0.750	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T8 60'-40'	Flange	1.375	6	0.750	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T9 40'-20'	Flange	1.375	6	0.750	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A325X		A325X		A325N		A325N		A325N		A325N		A325N	
T10 20'-0'	Flange	0.000	0	0.750	1	0.000	0	0.000	0	0.625	0	0.000	0	0.625	0
		A572-50		A325X		A325N		A325N		A325N		A325N		A325N	

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight klf
*** LDF4-50A(1/ 2) (Carrier 198'	В	No	No	Ar (CaAa)	198' - 163'	0.000	0.45	1	1	0.500	0.625		0.000
E) LDF4-50A(1/ 2) (Carrier 198' E)	С	No	No	Ar (CaAa)	198' - 0'	-2.000	0.03	1	1	0.500	0.625		0.000
LDF5-50A(7/ 8) (Carrier 198' E) ***	В	No	No	Ar (CaAa)	198' - 144'	0.000	0.42	3	2	0.500	1.030		0.000
AVA7-50(1-5/ 8) (Carrier 182' E)	В	No	No	Ar (CaAa)	182' - 0'	0.000	-0.1	12	8	0.500	2.010		0.001
Feedline Ladder (Af) (Carrier 182' E) ***	В	No	No	Af (CaAa)	200' - 0'	0.000	-0.1	1	1	3.000	3.000		0.008
HB114-1-081 3U4-M5J(1-1/ 4) (Carrier 170'	С	No	No	Ar (CaAa)	170' - 0'	-2.000	0.02	4	4	0.500	1.540		0.001
R) Feedline Ladder (Af) (Carrier 170' E) ***	С	No	No	Af (CaAa)	170' - 0'	-1.000	0.03	1	1	3.000	3.000		0.008
FLC 12-50J(1/2)	В	No	No	Ar (CaAa)	163' - 144'	0.000	0.45	2	2	0.500	0.640		0.000

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

**CROWN CASTLE** 

Designed by thasan

10:25:57 05/09/19

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight klf
(Carrier 163' E) ***													
LDF5-50A(7/ 8) (Carrier 144' E)	В	No	No	Ar (CaAa)	144' - 0'	0.000	0.42	5	5	0.500	1.030		0.000
LDF4-50A(1/ 2) (Carrier 144' E) ****	В	No	No	Ar (CaAa)	144' - 56'	0.000	0.45	5	5	0.625	0.625		0.000
LDF4-50A(1/ 2) (Carrier 53' E) ***	С	No	No	Ar (CaAa)	53' - 0'	-1.500	0.03	1	1	0.630	0.625		0.000
LDF4-50A(1/ 2) (Lighting Cable 56' E)	В	No	No	Ar (CaAa)	56' - 0'	0.000	0.45	6	6	0.630	0.625		0.000
LDF2-50(3/8") (Lighting Cable 100' E)		No	No	Ar (CaAa)	100' - 0'	0.000	0.4	1	1	0.500	0.440		0.000
50-AC-208-8S M( 3/4") (Lighting Cable 200' ABN) ***	В	No	No	Ar (CaAa)	200' - 0'	0.000	0.4	1	1	0.740	0.740		0.000
Feedline Ladder (Af) (Carrier 200' E)	В	No	No	Af (CaAa)	200' - 0'	0.000	0.35	1	1	3.000	3.000		0.008
Safety Line 3/8 (Carrier 200' E)	С	No	No	Ar (CaAa)	200' - 0'	1.000	0	1	1	0.375	0.375		0.000
Thin Flat Bar Climbing Ladder (Carrier 200' E) ***	С	No	No	Af (CaAa)	200' - 0'	0.000	0	1	1	2.000	2.000		0.004
1 1/2" Rigid Conduit (Carrier 215' E)	В	No	No	Ar (CaAa)	200' - 0'	0.000	0.43	1	1	1.500	1.500		0.001

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

**CROWN CASTLE** 

Designed by thasan

10:25:57 05/09/19

## **Discrete Tower Loads**

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	0	ft		ft <sup>2</sup>	$ft^2$	K
Flash Beacon Lighting	А	From Leg	0.000	0.000	200'	No Ice	1.563	1.563	0.050
(Carrier 200'E)		U	0'			1/2" Ice	2.411	2.411	0.080
			1'			1" Ice	2.644	2.644	0.114
						2" Ice	3.140	3.140	0.191
12' x 2" Pipe Mount	А	From Leg	0.000	0.000	200'	No Ice	2.400	2.400	0.100
(Carrier 200' E)			0'			1/2" Ice	3.625	3.625	0.119
			2'			1" Ice	4.867	4.867	0.145
						2" Ice	7.354	7.354	0.221
Flash Beacon Lighting	С	From Leg	0.000	0.000	200'	No Ice	1.563	1.563	0.050
(Carrier 200' E)			0'			1/2" Ice	2.411	2.411	0.080
			1'			1" Ice	2.644	2.644	0.114
	~					2" Ice	3.140	3.140	0.191
12' x 2" Pipe Mount	С	From Leg	0.000	0.000	200'	No Ice	2.400	2.400	0.100
(Carrier 200' E)			0'			1/2" Ice	3.625	3.625	0.119
			2'			1" Ice	4.867	4.867	0.145
0'1 I'1'		гт	0.500	0.000	100	2" Ice	7.354	7.354	0.221
Side Lighting (Carrier 100' E)	А	From Leg	0.500	0.000	100'	No Ice	0.133	0.133	0.005
(Carrier 100 E)			0' 0'			1/2" Ice 1" Ice	0.194 0.267	0.194 0.267	0.007 0.010
			0			2" Ice	0.267	0.267	0.010
Side Lighting	В	From Leg	0.500	0.000	100'	No Ice	0.133	0.133	0.019
(Carrier 100' E)	D	110iii Leg	0.500	0.000	100	1/2" Ice	0.194	0.194	0.005
(Carrier 100 E)			0'			1" Ice	0.194	0.194	0.007
			0			2" Ice	0.444	0.444	0.019
Side Lighting	С	From Leg	0.500	0.000	100'	No Ice	0.133	0.133	0.005
(Carrier 100'E)	C	110m Leg	0'	01000	100	1/2" Ice	0.194	0.194	0.007
(**************************************			<u>0</u> '			1" Ice	0.267	0.267	0.010
						2" Ice	0.444	0.444	0.019
**		г I	4 000	0.000	1001	NT T	2 2 1 0	2 2 10	0.027
DB225-A	А	From Leg	4.000	0.000	198'	No Ice	3.210	3.210	0.037
(Carrier 198' E)			0' 7'			1/2" Ice	5.778	5.778	0.048
			/			1" Ice 2" Ice	8.346 13.482	8.346	0.059 0.081
ALR10-O	В	From Leg	4.000	0.000	198'	No Ice	6.625	13.482 6.625	0.081
(Carrier 198' E)	D	110iii Leg	4.000	0.000	198	1/2" Ice	15.314	15.314	0.092
(Carrier 198 E)			10'			1" Ice	17.394	17.394	0.282
			10			2" Ice	20.790	20.790	0.525
OGB6-928N	В	From Leg	4.000	0.000	198'	No Ice	0.967	0.967	0.009
(Carrier 198'E)	2		0'		-20	1/2" Ice	1.329	1.329	0.017
(************************			6'			1" Ice	1.630	1.630	0.028
						2" Ice	2.258	2.258	0.060
PD1107-1	С	From Leg	4.000	0.000	198'	No Ice	2.180	2.180	0.008
(Carrier 198' E)		Ũ	0'			1/2" Ice	3.295	3.295	0.025
			7'			1" Ice	4.427	4.427	0.049
						2" Ice	6.424	6.424	0.118
PD201-7	С	From Leg	4.000	0.000	198'	No Ice	1.015	1.015	0.004
(Carrier 198' E)			0'			1/2" Ice	1.809	1.809	0.013
			7'			1" Ice	2.620	2.620	0.026
		_				2" Ice	3.757	3.757	0.070
(4) 6' x 2" Mount Pipe	А	From Leg	4.000	0.000	198'	No Ice	1.425	1.425	0.022
(Carrier 198' E)			0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
	P	<b>F I</b>	4 000	0.000	1001	2" Ice	3.060	3.060	0.090
(4) 6' x 2" Mount Pipe	В	From Leg	4.000	0.000	198'	No Ice	1.425	1.425	0.022

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PSEC 19994 (for T-MOBILE)

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

# BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

Designed by thasan

10:25:57 05/09/19

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft	0	ft		ft <sup>2</sup>	$ft^2$	K
			ft						
(Carrier 198' E)			0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
						2" Ice	3.060	3.060	0.090
(4) 6' x 2" Mount Pipe	С	From Leg	4.000	0.000	198'	No Ice	1.425	1.425	0.022
(Carrier 198'E)			0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
(2) 4' y 2" Pine Mount	•	Enom Lag	4 000	0.000	198'	2" Ice No Ice	3.060 0.785	3.060 0.785	0.090 0.029
(2) 4' x 2" Pipe Mount (Carrier 198' E)	А	From Leg	4.000 0'	0.000	198	1/2" Ice	1.028	1.028	0.029
(Carrier 198 E)			0'			172 ICC 1" Icc	1.281	1.281	0.033
			0			2" Ice	1.814	1.814	0.072
(2) 4' x 2" Pipe Mount	В	From Leg	4.000	0.000	198'	No Ice	0.785	0.785	0.029
(Carrier 198'E)		U	0'			1/2" Ice	1.028	1.028	0.035
			0'			1" Ice	1.281	1.281	0.044
						2" Ice	1.814	1.814	0.072
(2) 4' x 2" Pipe Mount	С	From Leg	4.000	0.000	198'	No Ice	0.785	0.785	0.029
(Carrier 198'E)			0'			1/2" Ice	1.028	1.028	0.035
			0'			1" Ice	1.281	1.281	0.044
	G			0.000	1001	2" Ice	1.814	1.814	0.072
Sector Mount [SM 702-3]	С	None		0.000	198'	No Ice	37.400	37.400	1.551
(Carrier 198' E)						1/2" Ice 1" Ice	54.200 71.000	54.200 71.000	2.352 3.153
						2" Ice	104.600	104.600	4.755
***						2 100	104.000	104.000	4.755
APXVAARR24_43-U-NA20	А	From Leg	4.000	0.000	182'	No Ice	20.480	11.024	0.161
w/ Mount Pipe			0'			1/2" Ice	21.231	12.550	0.297
(Carrier 182' P)			-5'			1" Ice	21.990	14.099	0.444
	_					2" Ice	23.444	16.451	0.775
APXVAARR24_43-U-NA20	В	From Leg	4.000	0.000	182'	No Ice	20.480	11.024	0.161
w/ Mount Pipe			0'			1/2" Ice	21.231	12.550	0.297
(Carrier 182' P)			-5'			1" Ice 2" Ice	21.990 23.444	14.099 16.451	0.444 0.775
APXVAARR24_43-U-NA20	С	From Leg	4.000	0.000	182'	No Ice	20.480	11.024	0.161
w/ Mount Pipe	C	110ill Leg	4.000 0'	0.000	102	1/2" Ice	21.231	12.550	0.297
(Carrier 182' P)			-5'			1" Ice	21.990	14.099	0.444
( · · · · · · · · · · · · · · · · · · ·						2" Ice	23.444	16.451	0.775
RADIO 4449 B12/B71	А	From Leg	4.000	0.000	182'	No Ice	1.650	1.163	0.074
(Carrier 182' P)			0'			1/2" Ice	1.810	1.301	0.090
			-5'			1" Ice	1.978	1.447	0.109
	-					2" Ice	2.336	1.762	0.155
RADIO 4449 B12/B71	В	From Leg	4.000	0.000	182'	No Ice	1.650	1.163	0.074
(Carrier 182' P)			0'			1/2" Ice	1.810	1.301	0.090
			-5'			1" Ice 2" Ice	1.978 2.336	1.447	0.109
RADIO 4449 B12/B71	С	From Leg	4.000	0.000	182'	No Ice	2.550	1.762 1.163	0.155 0.074
(Carrier 182' P)	C	110ill Leg	4.000 0'	0.000	102	1/2" Ice	1.810	1.301	0.074
(Carrier 102 T)			-5'			1" Ice	1.978	1.447	0.109
			U			2" Ice	2.336	1.762	0.155
APXV18-209015-C-A20 w/	А	From Leg	4.000	0.000	182'	No Ice	4.184	3.556	0.048
Mount Pipe		9	0'			1/2" Ice	4.629	4.352	0.084
(Carrier 182' E)			-5'			1" Ice	5.065	5.061	0.127
	_	_				2" Ice	5.931	6.529	0.234
APXV18-209015-C-A20 w/	В	From Leg	4.000	0.000	182'	No Ice	4.184	3.556	0.048
Mount Pipe			0'			1/2" Ice	4.629	4.352	0.084
(Carrier 182'E)			-5'			1" Ice	5.065	5.061	0.127
APXV18-209015-C-A20 w/	С	From Leg	4.000	0.000	182'	2" Ice No Ice	5.931 4.184	6.529 3.556	0.234 0.048
1 A V 10-207013-C-A20 W/	U	rioni Leg	4.000	0.000	102	INO ICE	4.104	5.550	0.048

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

## BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

Designed by thasan

10:25:57 05/09/19

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weight
	0		Vert ft ft	0	ft		ft <sup>2</sup>	$ft^2$	K
			ft						
Mount Pipe			0'			1/2" Ice	4.629	4.352	0.084
(Carrier 182' E)			-5'			1" Ice	5.065	5.061	0.127
						2" Ice	5.931	6.529	0.234
(2) KRY 112 489/2 (Carrier 182' E)	В	From Leg	4.000	0.000	182'	No Ice	0.559	0.365	0.015
			0'			1/2" Ice	0.658	0.448	0.020
			1'			1" Ice	0.764	0.542	0.027
	C	<b>Б</b> Т	1 000	0.000	102	2" Ice	0.998	0.752	0.046
KRY 112 489/2 (Carrier 182' E)	С	From Leg	4.000	0.000	182'	No Ice 1/2" Ice	0.559 0.658	0.365 0.448	0.015
			0' 1'			1/2 ICe 1" Ice	0.038	0.448	0.020 0.027
			1			2" Ice	0.998	0.752	0.027
(3) 15' Sector Frame (Carrier 182' E)	С	None		0.000	182'	No Ice	41.388	41.388	1.926
	e	110110		01000	102	1/2" Ice	56.125	56.125	2.698
						1" Ice	70.862	70.862	3.471
						2" Ice	100.338	100.338	5.017
(3) 8' x 3" Mount Pipe (Carrier 182' P)	А	From Leg	4.000	0.000	182'	No Ice	2.400	2.400	0.041
			0'			1/2" Ice	3.188	3.188	0.058
			0'			1" Ice	3.675	3.675	0.081
						2" Ice	4.676	4.676	0.143
6' x 2" Horizontal Mount Pipe (Carrier 182' P)	Α	From Leg	4.000	0.000	182'	No Ice	0.500	0.500	0.028
			0'			1/2" Ice	1.065	1.065	0.171
			0'			1" Ice 2" Ice	1.439 2.217	1.439 2.217	0.322 0.646
(3) 8' x 3" Mount Pipe	В	From Leg	4.000	0.000	182'	No Ice	2.217 2.400	2.217 2.400	0.040
(Carrier 182' P)	Б	110III Leg	4.000	0.000	162	1/2" Ice	3.188	3.188	0.041
			0'			1" Ice	3.675	3.675	0.081
			Ű			2" Ice	4.676	4.676	0.143
6' x 2" Horizontal Mount Pipe (Carrier 182' P)	В	From Leg	4.000	0.000	182'	No Ice	0.500	0.500	0.028
			0'			1/2" Ice	1.065	1.065	0.171
			0'			1" Ice	1.439	1.439	0.322
						2" Ice	2.217	2.217	0.646
<ul><li>(3) 8' x 3" Mount Pipe (Carrier 182' P)</li><li>5' x 2" Horizontal Mount Pipe</li></ul>	С	From Leg	4.000	0.000	182'	No Ice	2.400	2.400	0.041
			0'			1/2" Ice	3.188	3.188	0.058
			0'			1" Ice 2" Ice	3.675	3.675	0.081
	С	From Leg	4.000	0.000	182'	2" Ice No Ice	4.676 0.500	4.676 0.500	0.143 0.028
(Carrier 182' P)	C	From Leg	4.000	0.000	162	1/2" Ice	1.065	1.065	0.028
			0'			172 ICC 1" ICC	1.439	1.439	0.322
			0			2" Ice	2.217	2.217	0.646
6' x 2" Mount Pipe (Carrier 182' E)	А	From Leg	4.000	0.000	182'	No Ice	1.425	1.425	0.022
		Ũ	0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
						2" Ice	3.060	3.060	0.090
6' x 2" Mount Pipe (Carrier 182' E)	В	From Leg	4.000	0.000	182'	No Ice	1.425	1.425	0.022
			0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
6' x 2" Mount Pipe (Carrier 182' E)	C	From Leg	4.000	0.000	182'	2" Ice No Ice	3.060	3.060	0.090 0.022
	С	From Leg	4.000	0.000	162	1/2" Ice	1.425 1.925	1.425 1.925	0.022
			0'			1/2 ICC 1" ICC	2.294	2.294	0.033
			U			2" Ice	3.060	3.060	0.048
**							2.200	2.200	2.020
APXVTM14-ALU-I20 w/	А	From Leg	4.000	0.000	170'	No Ice	6.580	4.959	0.077
Mount Pipe (Carrier 170' R)		5	0'			1/2" Ice	7.031	5.754	0.132
			1'			1" Ice	7.473	6.472	0.193
						2" Ice	8.385	7.941	0.339
APXVTM14-ALU-I20 w/	В	From Leg	4.000	0.000	170'	No Ice	6.580	4.959	0.077

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PSEC 19994 (for T-MOBILE)

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

#### BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

Designed by thasan

10:25:57 05/09/19

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_A A_A$ Side	Weigh
	0		Vert				- 2	- 2	
			ft ft	0	ft		$ft^2$	$ft^2$	K
Mount Pipe			<u>ft</u> 0'			1/2" Ice	7.031	5.754	0.132
(Carrier 170' R)			0 1'			172 ICe 1" Ice	7.473	6.472	0.132
			1			2" Ice	8.385	7.941	0.339
APXVTM14-ALU-I20 w/	С	From Leg	4.000	0.000	170'	No Ice	6.580	4.959	0.077
Mount Pipe	-		0'			1/2" Ice	7.031	5.754	0.132
(Carrier 170' R)			1'			1" Ice	7.473	6.472	0.193
						2" Ice	8.385	7.941	0.339
NNVV-65B-R4 w/ Mount	А	From Leg	4.000	0.000	170'	No Ice	12.509	7.413	0.103
Pipe			0'			1/2" Ice	13.108	8.598	0.194
(Carrier 170' R)			1'			1" Ice	13.672	9.496	0.293
						2" Ice	14.822	11.328	0.520
NNVV-65B-R4 w/ Mount	В	From Leg	4.000	0.000	170'	No Ice	12.509	7.413	0.103
Pipe			0'			1/2" Ice	13.108	8.598	0.194
(Carrier 170' R)			1'			1" Ice	13.672	9.496	0.293
						2" Ice	14.822	11.328	0.520
NVV-65B-R4 w/ Mount	С	From Leg	4.000	0.000	170'	No Ice	12.509	7.413	0.103
Pipe			0'			1/2" Ice	13.108	8.598	0.194
(Carrier 170' R)			1'			1" Ice	13.672	9.496	0.293
						2" Ice	14.822	11.328	0.520
PCS 1900MHZ	А	From Leg	4.000	0.000	170'	No Ice	2.322	2.238	0.060
4X45W-65MHZ			0'			1/2" Ice	2.527	2.441	0.083
(Carrier 170' R)			1'			1" Ice	2.739	2.651	0.110
	D	г т	1 000	0.000	170	2" Ice	3.185	3.093	0.173
PCS 1900MHZ	В	From Leg	4.000	0.000	170'	No Ice	2.322	2.238	0.060
4X45W-65MHZ			0' 1'			1/2" Ice 1" Ice	2.527 2.739	2.441 2.651	0.083
(Carrier 170' R)			1			2" Ice	3.185	3.093	0.110 0.173
PCS 1900MHZ	С	From Leg	4.000	0.000	170'	No Ice	2.322	2.238	0.175
4X45W-65MHZ	C	110III Leg	4.000 0'	0.000	170	1/2" Ice	2.522	2.238	0.000
(Carrier 170' R)			0 1'			172 ICe 1" Ice	2.739	2.651	0.082
(Carrier 170 R)			1			2" Ice	3.185	3.093	0.173
TD-RRH8X20-25	А	From Leg	4.000	0.000	170'	No Ice	4.045	1.535	0.070
(Carrier 170' R)	11	110III Log	0'	0.000	170	1/2" Ice	4.298	1.714	0.097
			1'			1" Ice	4.557	1.901	0.128
			-			2" Ice	5.098	2.295	0.201
TD-RRH8X20-25	В	From Leg	4.000	0.000	170'	No Ice	4.045	1.535	0.070
(Carrier 170' R)			0'			1/2" Ice	4.298	1.714	0.097
(1			1'			1" Ice	4.557	1.901	0.128
						2" Ice	5.098	2.295	0.201
TD-RRH8X20-25	С	From Leg	4.000	0.000	170'	No Ice	4.045	1.535	0.070
(Carrier 170' R)		U	0'			1/2" Ice	4.298	1.714	0.097
			1'			1" Ice	4.557	1.901	0.128
						2" Ice	5.098	2.295	0.201
(2) RRH2X50-800	А	From Leg	4.000	0.000	170'	No Ice	1.701	1.282	0.053
(Carrier 170' R)			0'			1/2" Ice	1.864	1.428	0.070
			1'			1" Ice	2.035	1.580	0.090
						2" Ice	2.398	1.908	0.138
(2) RRH2X50-800	В	From Leg	4.000	0.000	170'	No Ice	1.701	1.282	0.053
(Carrier 170' R)			0'			1/2" Ice	1.864	1.428	0.070
			1'			1" Ice	2.035	1.580	0.090
				0.0		2" Ice	2.398	1.908	0.138
(2) RRH2X50-800	С	From Leg	4.000	0.000	170'	No Ice	1.701	1.282	0.053
(Carrier 170' R)			0'			1/2" Ice	1.864	1.428	0.070
			1'			1" Ice	2.035	1.580	0.090
2.511.01.01		<b>F F</b>	4 000	0.000	170	2" Ice	2.398	1.908	0.138
3.5"x8' Pipe (Carrier 170' R)	А	From Leg	4.000	0.000	170'	No Ice	2.800	2.800	0.061
(Carrier E/() R)			0'			1/2" Ice	3.405	3.405	0.081

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PSEC 19994 (for T-MOBILE)

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Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

## BU 871584 - JOHN TOM HILL

#### CROWN CASTLE

Designed by thasan

10:25:57 05/09/19

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
	Ū		Vert ft ft	0	ft		ft <sup>2</sup>	$ft^2$	K
			<u>ft</u> 0'			1" Ice	3.894	3.894	0.106
			0			2" Ice	4.900	4.900	0.174
3.5"x8' Pipe	В	From Leg	4.000	0.000	170'	No Ice	2.800	2.800	0.061
(Carrier 170' R)		U	0'			1/2" Ice	3.405	3.405	0.081
			0'			1" Ice	3.894	3.894	0.106
						2" Ice	4.900	4.900	0.174
3.5"x8' Pipe	С	From Leg	4.000	0.000	170'	No Ice	2.800	2.800	0.061
(Carrier 170' R)			0'			1/2" Ice	3.405	3.405	0.081
			0'			1" Ice	3.894	3.894	0.106
			4 0 0 0	0.000	1.501	2" Ice	4.900	4.900	0.174
6' x 2" Mount Pipe	А	From Leg	4.000	0.000	170'	No Ice	1.425	1.425	0.022
(Carrier 170'E)			0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice 2" Ice	2.294 3.060	2.294 3.060	$0.048 \\ 0.090$
6' x 2" Mount Pipe	В	From Leg	4.000	0.000	170'	No Ice	1.425	1.425	0.090
(Carrier 170'E)	Б	Hom Leg	4.000	0.000	170	1/2" Ice	1.925	1.925	0.022
(Currer 170 E)			0'			1" Ice	2.294	2.294	0.048
			0			2" Ice	3.060	3.060	0.090
6' x 2" Mount Pipe	С	From Leg	4.000	0.000	170'	No Ice	1.425	1.425	0.022
(Carrier 170' E)		8	0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
						2" Ice	3.060	3.060	0.090
Sector Mount [SM 506-3]	С	None		0.000	170'	No Ice	35.470	35.470	1.742
(Carrier 170' E)						1/2" Ice	50.600	50.600	2.348
						1" Ice	65.730	65.730	2.953
***						2" Ice	95.990	95.990	4.164
Pipe Mount [PM 601-1]	С	From Leg	0.500	0.000	163'	No Ice	3.000	0.900	0.065
(Carrier 163'E)		6	0'			1/2" Ice	3.740	1.120	0.079
( )			0'			1" Ice	4.480	1.340	0.093
						2" Ice	5.960	1.780	0.122
***	р	Г. Т.	4.000	0.000	1.4.4	N7 7	2 0 2 2	2 0 2 2	0.017
(2) PD1109-1	В	From Leg	4.000	0.000	144'	No Ice	2.833	2.833	0.017
(Carrier 144'E)			0' 8'			1/2" Ice 1" Ice	3.894 4.972	3.894 4.972	0.038 0.065
			0			2" Ice	4.972 6.367	4.972 6.367	0.063
SRL480N1DT4	С	From Leg	4.000	0.000	144'	No Ice	3.813	3.813	0.030
(Carrier 144'E)	C	110III Leg	4.000 0'	0.000	144	1/2" Ice	5.367	5.367	0.058
(Currer III E)			11'			1" Ice	6.938	6.938	0.096
						2" Ice	10.129	10.129	0.202
(4) 6' x 2" Mount Pipe	А	From Leg	4.000	0.000	144'	No Ice	1.425	1.425	0.022
(Carrier 144' E)		C	0'			1/2" Ice	1.925	1.925	0.033
			0'			1" Ice	2.294	2.294	0.048
						2" Ice	3.060	3.060	0.090
(4) 6' x 2" Mount Pipe	В	From Leg	4.000	0.000	144'	No Ice	1.425	1.425	0.022
(Carrier 144' E)			0'			1/2" Ice	1.925	1.925	0.033
· · · · ·			0'			1" Ice	2.294	2.294	0.048
		E. J	4 000	0.000	1.4.4	2" Ice	3.060	3.060	0.090
	C	From Leg	4.000	0.000	144'	No Ice	1.425	1.425	0.022
(4) 6' x 2" Mount Pipe	С					1/2" Ice	1.925	1.925	0.033
	С		0' 0'			1" 100	2 204	2 204	
(4) 6' x 2" Mount Pipe	С		0' 0'			1" Ice 2" Ice	2.294	2.294	0.048
(4) 6' x 2" Mount Pipe (Carrier 144' E)		-	0'	0.000	144'	2" Ice	3.060	3.060	0.090
<ul> <li>(4) 6' x 2" Mount Pipe (Carrier 144' E)</li> <li>(2) 4' x 2" Pipe Mount</li> </ul>	C A	From Leg	0' 4.000	0.000	144'	2" Ice No Ice	3.060 0.785	3.060 0.785	0.090 0.029
(4) 6' x 2" Mount Pipe (Carrier 144' E)		-	0' 4.000 0'	0.000	144'	2" Ice No Ice 1/2" Ice	3.060 0.785 1.028	3.060 0.785 1.028	0.090 0.029 0.035
<ul> <li>(4) 6' x 2" Mount Pipe (Carrier 144' E)</li> <li>(2) 4' x 2" Pipe Mount</li> </ul>		-	0' 4.000	0.000	144'	2" Ice No Ice	3.060 0.785	3.060 0.785	0.090 0.029

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<b>Pier Structural Engineering</b> 198-55 Northfield Drive East	Project	BU 871584 - JOHN TOM HILL	Date 10:25:57 05/09/19
Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806	tinx TowerProjectPier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806Client	CROWN CASTLE	Designed by thasan

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_A A_A$ Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft ft	o	ft		ft <sup>2</sup>	$ft^2$	Κ
(Carrier 144' E)			0' 0'			1/2" Ice 1" Ice 2" Ice	1.028 1.281 1.814	1.028 1.281 1.814	0.035 0.044 0.072
(2) 4' x 2" Pipe Mount (Carrier 144' E)	C	From Leg	4.000 0' 0'	0.000	144'	No Ice 1/2" Ice 1" Ice 2" Ice	0.785 1.028 1.281 1.814	0.785 1.028 1.281 1.814	0.029 0.035 0.044 0.072
Sector Mount [SM 702-3] (Carrier 144'E) ***	С	None		0.000	144'	No Ice 1/2" Ice 1" Ice 2" Ice	37.400 54.200 71.000 104.600	37.400 54.200 71.000 104.600	1.551 2.352 3.153 4.755
KS24019-L112A (Carrier 53' E) ***	С	From Leg	4.000 0' 2'	0.000	53'	No Ice 1/2" Ice 1" Ice 2" Ice	0.141 0.198 0.262 0.415	0.141 0.198 0.262 0.415	0.005 0.007 0.009 0.018

### Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	0	0	ft	ft		$ft^2$	Κ
PR-850 Carrier 163' E)	С	Grid	From Leg	1.000 0' 0'	60.000		163'	5.667	No Ice 1/2" Ice 1" Ice 2" Ice	25.220 25.970 26.710 28.210	0.038 0.170 0.300 0.570
***											

## Load Combinations

Comb.	Description
No.	
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 60 deg - No Ice
7	0.9 Dead+1.0 Wind 60 deg - No Ice
8	1.2 Dead+1.0 Wind 90 deg - No Ice
9	0.9 Dead+1.0 Wind 90 deg - No Ice
10	1.2 Dead+1.0 Wind 120 deg - No Ice
11	0.9 Dead+1.0 Wind 120 deg - No Ice
12	1.2 Dead+1.0 Wind 150 deg - No Ice
13	0.9 Dead+1.0 Wind 150 deg - No Ice
14	1.2 Dead+1.0 Wind 180 deg - No Ice
15	0.9 Dead+1.0 Wind 180 deg - No Ice

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PSEC 19994 (for T-MOBILE)

Date

Pier Structural Engineering 198-55 Northfield Drive East Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806

BU 871584 - JOHN TOM HILL

**CROWN CASTLE** 

Designed by thasan

10:25:57 05/09/19

Comb.	. Description	
No.		
16	1.2 Dead+1.0 Wind 210 deg - No Ice	
17	0.9 Dead+1.0 Wind 210 deg - No Ice	
18	1.2 Dead+1.0 Wind 240 deg - No Ice	
19	0.9 Dead+1.0 Wind 240 deg - No Ice	
20	1.2 Dead+1.0 Wind 270 deg - No Ice	
21	0.9 Dead+1.0 Wind 270 deg - No Ice	
22	1.2 Dead+1.0 Wind 300 deg - No Ice	
23	0.9 Dead+1.0 Wind 300 deg - No Ice	
24	1.2 Dead+1.0 Wind 330 deg - No Ice	
25	0.9 Dead+1.0 Wind 330 deg - No Ice	
26	1.2 Dead+1.0 Ice+1.0 Temp	
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	
39	Dead+Wind 0 deg - Service	
40	Dead+Wind 30 deg - Service	
41	Dead+Wind 60 deg - Service	
42	Dead+Wind 90 deg - Service	
43	Dead+Wind 120 deg - Service	
44	Dead+Wind 150 deg - Service	
45	Dead+Wind 180 deg - Service	
46	Dead+Wind 210 deg - Service	
47	Dead+Wind 240 deg - Service	
48	Dead+Wind 270 deg - Service	
49	Dead+Wind 300 deg - Service	
50	Dead+Wind 330 deg - Service	

### **Maximum Reactions**

Location	Condition	Gov.	Vertical	Horizontal, X	Horizontal, Z
		Load	Κ	Κ	K
		Comb.			
Leg C	Max. Vert	18	343.442	30.960	-17.036
-	Max. H <sub>x</sub>	18	343.442	30.960	-17.036
	Max. Hz	7	-299.171	-27.504	15.045
	Min. Vert	7	-299.171	-27.504	15.045
	Min. H <sub>x</sub>	7	-299.171	-27.504	15.045
	Min. Hz	18	343.442	30.960	-17.036
Leg B	Max. Vert	10	319.793	-27.830	-16.276
-	Max. H <sub>x</sub>	23	-272.061	24.305	14.235
	Max. Hz	23	-272.061	24.305	14.235
	Min. Vert	23	-272.061	24.305	14.235
	Min. H <sub>x</sub>	10	319.793	-27.830	-16.276
	Min. Hz	10	319.793	-27.830	-16.276
Leg A	Max. Vert	2	320.027	0.938	32.532
	Max. H <sub>x</sub>	21	13.250	3.424	1.014
	Max. H <sub>z</sub>	2	320.027	0.938	32.532
	Min. Vert	15	-275.073	-0.941	-28.478
	Min. H <sub>x</sub>	9	13.039	-3.392	0.997
	Min. Hz	15	-275.073	-0.941	-28.478

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<b>Pier Structural Engineering</b> 198-55 Northfield Drive East	Project BU 871584 - JOHN TOM HILL	Date 10:25:57 05/09/19
Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806	Client CROWN CASTLE	Designed by thasan

Location Condition Gov. Vertical Horizontal, X Horizontal, Z Load K K K Comb.

### **Maximum Tower Deflections - Service Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	0
T1	200 - 180	5.782	47	0.273	0.046
T2	180 - 160	4.636	47	0.264	0.042
T3	160 - 140	3.557	47	0.232	0.035
T4	140 - 120	2.630	47	0.190	0.029
T5	120 - 100	1.871	47	0.157	0.023
T6	100 - 80	1.248	47	0.123	0.017
T7	80 - 60	0.770	47	0.088	0.012
T8	60 - 40	0.432	47	0.062	0.009
Т9	40 - 20	0.203	47	0.035	0.006
T10	20 - 0	0.064	47	0.018	0.003

## **Critical Deflections and Radius of Curvature - Service Wind**

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load				Curvature
ft		Comb.	in	0	0	ft
200'	Flash Beacon Lighting	47	5.782	0.273	0.046	289969
198'	DB225-A	47	5.666	0.273	0.046	289969
182'	APXVAARR24_43-U-NA20 w/	47	4.749	0.266	0.043	80053
	Mount Pipe					
170'	APXVTM14-ALU-I20 w/ Mount	47	4.083	0.251	0.039	40084
	Pipe					
163'	PR-850	47	3.711	0.238	0.036	30583
144'	(2) PD1109-1	47	2.802	0.198	0.030	27123
100'	Side Lighting	47	1.248	0.123	0.017	32658
53'	KS24019-L112A	47	0.341	0.052	0.008	49029

### **Bolt Design Data**

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Ratio Load	Allowable Ratio	Criteria
	ft			in	Bolts	per Bolt K	per Bolt K	Allowable		
T1	200	Leg	A325X	0.750	4	4.163	30.101	0.138	1.05	Bolt Tension
		Diagonal	A325X	0.625	1	3.476	7.875	0.441	1.05	Member Block Shear
		Top Girt	A325X	0.625	1	0.138	13.050	0.011	1.05	Member Bearing
T2	180	Leg	A325X	1.000	4	13.863	54.517	0.254	1.05	Bolt Tension
		Diagonal	A325X	0.625	1	5.330	7.875	0.677	1.05	Member Block Shear
T3	160	Leg	A325X	1.000	4	23.197	54.517	0.425	1.05	Bolt Tension
		Diagonal	A325X	0.625	1	5.769	7.875	0.733	1.05	Member Block Shear
T4	140	Leg	A325X	1.250	4	32.188	87.220	0.369	1.05	Bolt Tension

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BU 871584 - JOHN TOM HILL

#### **CROWN CASTLE**

Designed by thasan

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load	Allowable Load	Ratio Load	Allowable Ratio	Criteria
110.	ft	Type	Grude	in	Bolts	per Bolt K	per Bolt K	Allowable	nuno	
		Diagonal	A325X	0.625	1	6.522	9.914	0.658	1.05	Member Block Shear
T5	120	Leg	A325X	1.250	4	40.227	87.220	0.461	1.05	Bolt Tension
		Diagonal	A325X	0.625	1	6.618	9.914	0.668	1.05	Member Block Shear
T6	100	Leg	A325X	1.250	6	31.843	87.220	0.365	1.05	Bolt Tension
		Diagonal	A325X	0.750	1	7.080	10.424	0.679	1.05	Member Block Shear
T7	80	Leg	A325X	1.250	6	36.650	87.220	0.420	1.05	Bolt Tension
		Diagonal	A325X	0.750	1	8.269	14.355	0.576	1.05	Member Bearing
T8	60	Leg	A325X	1.375	6	41.287	103.939	0.397	1.05	Bolt Tension
		Diagonal	A325X	0.750	1	8.666	14.355	0.604	1.05	Member Bearing
T9	40	Leg	A325X	1.375	6	45.746	103.939	0.440	1.05	Bolt Tension
		Diagonal	A325X	0.750	1	9.219	14.355	0.642	1.05	Member Bearing
T10	20	Diagonal	A325X	0.750	1	9.907	14.355	0.690	1.05	Member Bearing

### **Compression Checks**

### Leg Design Data (Compression)

Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	Κ	Κ	$\phi P_n$
T1	200 - 180	Sabre 2.875x.375	20'	4'11-3/4'	66.9 K=1.00	2.945	-17.997	95.591	0.188 1
T2	180 - 160	Sabre 3.5 x .3	20'13/32	4'11-27/ 32''	52.7 K=1.00	3.016	-59.264	110.802	0.535 1
T3	160 - 140	Sabre 4 x .318	20'13/32	4'11-27/ 32''	45.8 K=1.00	3.678	-100.568	141.988	0.708 1
T4	140 - 120	Sabre 4.5 x .438	20'13/32	6'7-13/1 6''	55.2 K=1.00	5.589	-138.479	201.215	0.688 1
T5	120 - 100	Sabre 5.5625 x .375	20'13/32	6'7-13/1 6''	43.4 K=1.00	6.111	-174.468	239.635	0.728 1
T6	100 - 80	Sabre 5.5625 x .375	20'13/32	6'7-13/1 6''	43.4 K=1.00	6.111	-208.709	239.635	0.871 1
T7	80 - 60	Sabre 6.625 x .432	20'13/32	9'11-11/ 16"	54.5 K=1.00	8.405	-239.282	304.302	0.786 1
T8	60 - 40	Sabre 8.625 x .322	20'13/32	9'11-11/ 16"	40.7 K=1.00	8.399	-271.672	334.762	0.812 1
T9	40 - 20	Sabre 8.625 x .5	20'13/32	9'11-11/ 16"	41.6 K=1.00	12.763	-304.055	506.091	0.601 1
T10	20 - 0	Sabre 8.625 x .5	20'13/32	9'11-11/ 16"	41.6 K=1.00	12.763	-335.569	506.091	0.663 1

## tnxTower

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g		BU 871584 - JOHN TOM HILL	10:25:57 05/09/19
	Client	CROWN CASTLE	Designed by thasan

## **Diagonal Design Data (Compression)**

Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	$Ratio P_u$
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T1	200 - 180	L1 3/4x1 3/4x3/16	7'11/16"	3'2-9/16'	114.2 K=1.02	0.621	-3.678	13.190	0.279 1
T2	180 - 160	L1 3/4x1 3/4x3/16	8'4-19/3 2''	4'7/32''	140.4 K=1.00	0.621	-5.312	9.014	0.589 1
T3	160 - 140	L1 3/4x1 3/4x3/16	10'3/4"	4'10-1/3 2"	169.0 K=1.00	0.621	-5.873	6.225	0.944 1
T4	140 - 120	L2 1/2x2 1/2x3/16	12'6-23/ 32''	6'1-5/16'	148.1 K=1.00	0.902	-6.537	11.773	0.555 1
T5	120 - 100	L2 1/2x2 1/2x3/16	14'3-9/1 6''	6'11-1/8'	168.0 K=1.00	0.902	-6.776	9.153	0.740 1
T6	100 - 80	L3x3x3/16	16'1-1/8'	7'9-15/1 6''	157.6 K=1.00	1.090	-7.202	12.556	0.574 1
T7	80 - 60	L3 1/2x3 1/2x1/4	19'3-7/3 2''	9'5-15/3 2''	163.5 K=1.00	1.690	-8.531	18.090	0.472 1
T8	60 - 40	L3 1/2x3 1/2x1/4	21'1/16"	10'2-25/ 32''	176.9 K=1.00	1.690	-9.356	15.453	0.605 1
Т9	40 - 20	L3 1/2x3 1/2x1/4	22'9-7/1 6''	11'1-1/2'	192.4 K=1.00	1.690	-9.909	13.072	0.758 1
T10	20 - 0	L4x4x1/4	24'7-7/3 2''	12'13/32	181.6 K=1.00	1.940	-10.995	16.829	0.653 1

		Top Gi	irt De	sign D	ata (C	compr	ession)		
Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	P <sub>u</sub>	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	Κ	Κ	$\phi P_n$
T1	200 - 180	L1 3/4x1 3/4x3/16	5'	4'5-5/8"	156.1 K=1.00	0.621	-0.138	7.292	0.019 1

### **Tension Checks**

		L	.eg Des	ign [	Data (	Tensio	on)		
Section No.	Elevation	Size	L	$L_u$	Kl/r	A	P <sub>u</sub>	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	Κ	K	$\phi P_n$
T1	200 - 180	Sabre 2.875x.375	20'	1"	1.1	2.945	16.652	132.536	0.126 1
T2	180 - 160	Sabre 3.5 x .3	20'13/32	1"	0.9	3.016	55.450	135.717	0.409 1
T3	160 - 140	Sabre 4 x .318	20'13/32	1"	0.8	3.678	92.788	165.529	0.561 1
T4	140 - 120	Sabre 4.5 x .438	20'13/32	1"	0.7	5.589	128.752	251.522	0.512 1
T5	120 - 100	Sabre 5.5625 x .375	20'13/32	1"	0.5	6.111	160.909	275.012	0.585 1
T6	100 - 80	Sabre 5.5625 x .375	20'13/32	1"	0.5	6.111	191.061	275.012	0.695 1

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<b>Pier Structural Engineering</b> 198-55 Northfield Drive East	Project	BU 871584 - JOHN TOM HILL	Date 10:25:57 05/09/19
Waterloo, Ontario, N2K 3T6 Phone: (519)885-3806 FAX: (519)884-3806	Client	CROWN CASTLE	Designed by thasan

Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	K	K	$\phi P_n$
T7	80 - 60	Sabre 6.625 x .432	20'13/32	1"	0.5	8.405	219.898	378.222	0.581 1
T8	60 - 40	Sabre 8.625 x .322	20'13/32	1"	0.3	8.399	247.722	377.967	0.655 1
Т9	40 - 20	Sabre 8.625 x .5	20'13/32	1"	0.3	12.763	274.479	574.322	0.478 1
T10	20 - 0	Sabre 8.625 x .5	20'13/32	1"	0.3	12.763	300.495	574.322	0.523 1

## Diagonal Design Data (Tension)

Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	Ratio P <sub>u</sub>
	ft		ft	ft		$in^2$	Κ	Κ	$\phi P_n$
T1	200 - 180	L1 3/4x1 3/4x3/16	7'11/16"	3'2-9/16'	75.1	0.360	3.476	15.675	0.222 1
T2	180 - 160	L1 3/4x1 3/4x3/16	8'4-19/3 2''	4'7/32''	93.1	0.360	5.330	15.675	0.340 1
T3	160 - 140	L1 3/4x1 3/4x3/16	10'3/4"	4'10-1/3 2"	111.4	0.360	5.769	15.675	0.368 1
T4	140 - 120	L2 1/2x2 1/2x3/16	11'5-7/1 6''	5'6-25/3 2''	88.1	0.571	6.522	24.840	0.263 1
T5	120 - 100	L2 1/2x2 1/2x3/16	14'3-9/1 6''	6'11-1/8'	109.1	0.571	6.618	24.840	0.266 1
T6	100 - 80	L3x3x3/16	16'1-1/8'	7'9-15/1 6''	101.9	0.694	7.080	30.209	0.234 1
T7	80 - 60	L3 1/2x3 1/2x1/4	19'3-7/3 2''	9'5-15/3 2''	105.7	1.103	8.269	47.999	0.172 1
T8	60 - 40	L3 1/2x3 1/2x1/4	21'1/16"	10'2-25/ 32''	114.3	1.103	8.666	47.999	0.181 1
Т9	40 - 20	L3 1/2x3 1/2x1/4	21'10-3/ 4''	10'8-3/1 6''	119.2	1.103	9.219	47.999	0.192 1
T10	20 - 0	L4x4x1/4	24'7-7/3 2''	12'13/32	116.9	1.291	9.907	56.156	0.176 <sup>1</sup>

## Top Girt Design Data (Tension)

Section No.	Elevation	Size	L	$L_u$	Kl/r	Α	$P_u$	$\phi P_n$	Ratio $P_u$
	ft		ft	ft		$in^2$	Κ	K	$\phi P_n$
	200 - 180	L1 3/4x1 3/4x3/16	<b>C1</b>	4'5-5/8"	106.4	0.360	0.072	15.675	0.005 1

## Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow} \ K$	% Capacity	Pass Fail
T1	200 - 180	Leg	Sabre 2.875x.375	2	-17.997	100.371	17.9	Pass
T2	180 - 160	Leg	Sabre 3.5 x .3	31	-59.264	116.342	50.9	Pass

*tnxTower* 

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### CROWN CASTLE

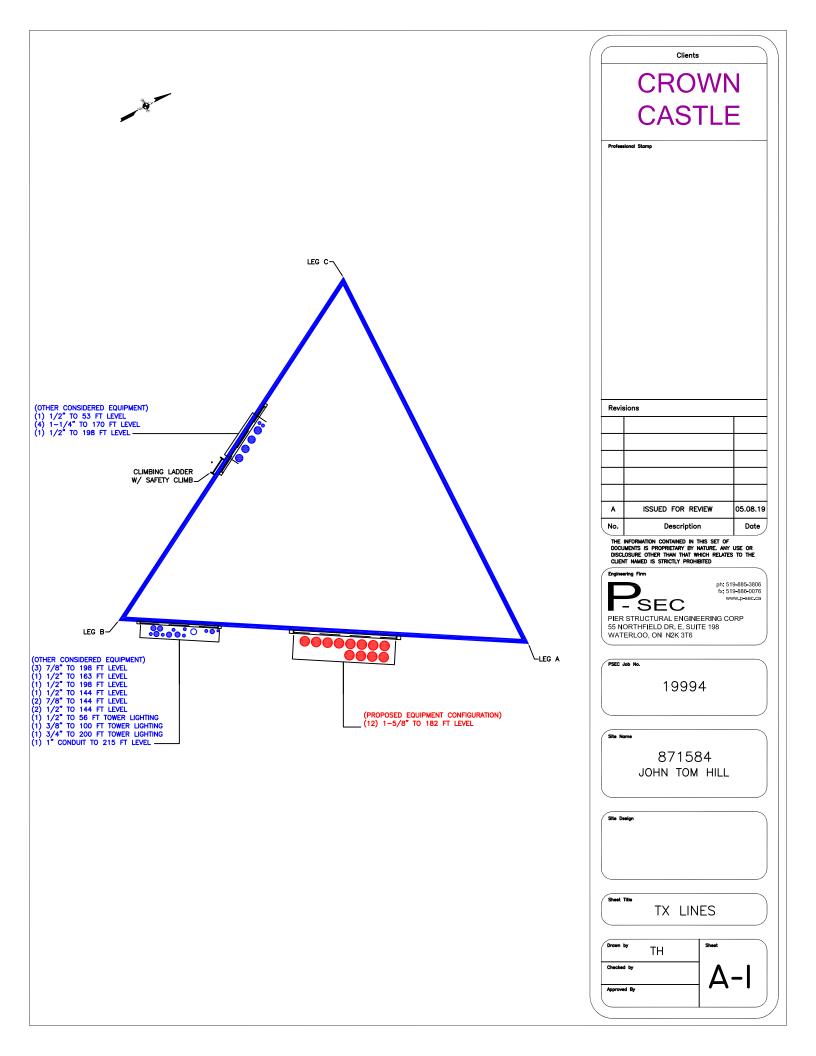
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Section	Elevation	Component	Size	Critical	Р	$\phi P_{allow}$	%	Pass
No.	ft	Type		Element	K	Κ	Capacity	Fail
T3	160 - 140	Leg	Sabre 4 x .318	58	-100.568	149.087	67.5	Pass
T4	140 - 120	Leg	Sabre 4.5 x .438	85	-138.479	211.276	65.5	Pass
T5	120 - 100	Leg	Sabre 5.5625 x .375	106	-174.468	251.617	69.3	Pass
T6	100 - 80	Leg	Sabre 5.5625 x .375	127	-208.709	251.617	82.9	Pass
T7	80 - 60	Leg	Sabre 6.625 x .432	148	-239.282	319.517	74.9	Pass
T8	60 - 40	Leg	Sabre 8.625 x .322	163	-271.672	351.500	77.3	Pass
T9	40 - 20	Leg	Sabre 8.625 x .5	178	-304.055	531.396	57.2	Pass
T10	20 - 0	Leg	Sabre 8.625 x .5	193	-335.569	531.396	63.1	Pass
T1	200 - 180	Diagonal	L1 3/4x1 3/4x3/16	10	-3.678	13.849	26.6 42.0 (b)	Pass
T2	180 - 160	Diagonal	L1 3/4x1 3/4x3/16	34	-5.312	9.465	56.1 64.5 (b)	Pass
T3	160 - 140	Diagonal	L1 3/4x1 3/4x3/16	61	-5.873	6.536	89.9	Pass
T4	140 - 120	Diagonal	L2 1/2x2 1/2x3/16	88	-6.537	12.361	52.9 62.7 (b)	Pass
T5	120 - 100	Diagonal	L2 1/2x2 1/2x3/16	109	-6.776	9.610	70.5	Pass
T6	100 - 80	Diagonal	L3x3x3/16	130	-7.202	13.184	54.6	Pass
		U U					64.7 (b)	
T7	80 - 60	Diagonal	L3 1/2x3 1/2x1/4	151	-8.531	18.994	44.9 54.9 (b)	Pass
T8	60 - 40	Diagonal	L3 1/2x3 1/2x1/4	166	-9.356	16.226	57.7	Pass
T9	40 - 20	Diagonal	L3 1/2x3 1/2x1/4	181	-9.909	13.726	72.2	Pass
T10	20 - 0	Diagonal	L4x4x1/4	196	-10.995	17.670	62.2 65.7 (b)	Pass
T1	200 - 180	Top Girt	L1 3/4x1 3/4x3/16	5	-0.138	7.657	1.8 Summary	Pass
						Leg (T6)	82.9	Pass
						Diagonal (T3)	89.9	Pass
						Top Girt (T1)	1.8	Pass
						Bolt Checks	69.8	Pass
						RATING =	89.9	Pass

APPENDIX B

#### **BASE LEVEL DRAWING**



APPENDIX C

#### ADDITIONAL CALCULATIONS



Project Information				
BU #	871584			
Site Name	JOHN TOM HILL			
Order #	479814 Rev 0			

Tower Information				
Tower Type	Self Support			
TIA-222 Rev	Н			

Apply TIA-222-H Section 15.5

Applied Loads					
	Comp.	Uplift			
Axial (k)	343.00	299.00			
Shear (k)	35.00	31.00			

Anchor Rod Data			
Quantity:	8		
Diameter (in):	1.5		
Material Grade:	A572-50	Fy=50 ksi	Fu=65 ksi
Grout Considered:	No	Not Conside	ered, lar<=1(d)
I <sub>ar</sub> (in):	1.125		
Eta Factor, η:			
Thread Type:	N-Included		
Configuration:	Symmetrical		

Anchor Rod Results				
Axial, Pu_c (kips)	42.88			
Shear, Vu (kips)	4.38			
Moment, Mu (kip-in)	-			
Axial Cap., φPn_c (kips)	70.50			
Shear Cap., φVn (kips)	21.15			
Moment Cap., φMn (kip-in)	-			
Stress Rating	62.0%			

Pass

### **Pier and Pad Foundation**

BU # :	871584
	JOHN TOM HILL
App. Number:	479814 Rev 0

TIA-222 Revision: H Tower Type: Self Support

	Top & Bot. Pad Rein. Different?:	
	Block Foundation?:	

Superstructure Analysis Reactions				
Compression, P <sub>comp</sub> :	343	kips		
Compression Shear, Vu_comp:	35	kips		
Uplift, <b>P<sub>uplift</sub></b> :	299	kips		
Uplift Shear, V <sub>u_uplift</sub> :	31	kips		
Tower Height, H:	200	ft		
Base Face Width, BW:	23	ft		
BP Dist. Above Fdn, <b>bp<sub>dist</sub>:</b>	2.635	in		

Pier Properties				
Pier Shape:	Circular			
Pier Diameter, dpier:	3.5	ft		
Ext. Above Grade, E:	0.5	ft		
Pier Rebar Size, <b>Sc</b> :	7			
Pier Rebar Quantity, <b>mc</b> :	14			
Pier Tie/Spiral Size, St:	3			
Pier Tie/Spiral Quantity, mt:	10			
Pier Reinforcement Type:	Tie			
Pier Clear Cover, <b>cc</b> <sub>pier</sub> :	3	in		

Pad Properties				
Depth, D:	10	ft		
Pad Width, <b>W</b> :	15	ft		
Pad Thickness, <b>T</b> :	1.8	ft		
Pad Rebar Size (Bottom), Sp:	7			
Pad Rebar Quantity (Bottom), mp:	20			
Pad Clear Cover, <b>cc</b> <sub>pad</sub> :	3	in		

Material Properties				
Rebar Grade, <b>Fy</b> :	60	ksi		
Concrete Compressive Strength, F'c:	3	ksi		
Dry Concrete Density, $\delta c$ :	150	pcf		

Soil Properties				
Total Soil Unit Weight, $m{\gamma}$ :	135	pcf		
Ultimate Gross Bearing, Qult:	16.000	ksf		
Cohesion, <b>Cu</b> :	0.000	ksf		
Friction Angle, $oldsymbol{arphi}$ :	36	degrees		
SPT Blow Count, Notes	28			
Base Friction, $\mu$ :	0.6			
Neglected Depth, N:	3.30	ft		
Foundation Bearing on Rock?	No			
Groundwater Depth, gw:	8	ft		

Foundation Analysis Checks					
	Capacity	Demand	Rating*	Check	
Uplift (kips)	545.59	299.00	52.2%	Pass	
Lateral (Sliding) (kips)	128.91	31.00	22.9%	Pass	
Bearing Pressure (ksf)	12.00	3.04	24.1%	Pass	
Pier Flexure (Comp.) (kip*ft)	957.79	304.50	30.3%	Pass	
Pier Flexure (Tension) (kip*ft)	278.14	269.70	92.3%	Pass	
Pier Compression (kip)	4592.74	357.92	7.4%	Pass	
Pad Flexure (kip*ft)	891.17	380.53	40.7%	Pass	
Pad Shear - 1-way (kips)	255.66	99.20	37.0%	Pass	
Pad Shear - 2-way (Comp) (ksi)	0.164	0.101	58.4%	Pass	
Flexural 2-way (Comp) (kip*ft)	1045.15	182.70	16.6%	Pass	
Pad Shear - 2-way (Uplift) (ksi)	0.164	0.107	62.0%	Pass	
Flexural 2-way (Tension) (kip*ft)	1045.15	161.82	14.7%	Pass	

\*Rating per TIA-222-H Section 15.5

Soil Rating*:	52.2%
Structural Rating*:	92.3%

<--Toggle between Gross and Net





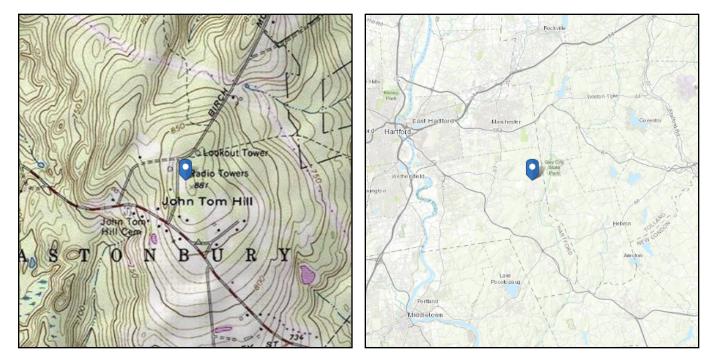
## ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

 Elevation:
 877.95 ft (NAVD 88)

 Latitude:
 41.708956

 Longitude:
 -72.473447



### Wind

#### **Results:**

Wind Speed:	125 Vmph
10-year MRI	77 Vmph
25-year MRI	87 Vmph
50-year MRI	94 Vmph
100-year MRI	102 Vmph
Data Source:	ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of
Date Accessed:	March 12, 2014 Thu Aug 30 2018

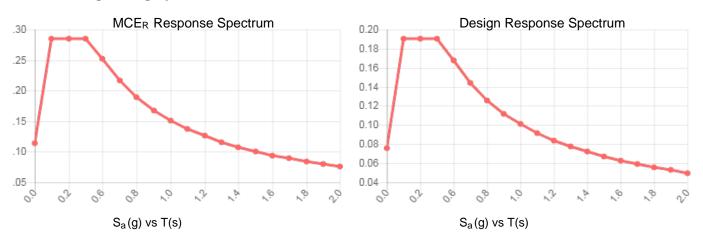
Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



Site Soil Class: Results:	D - Stiff Soil			
S <sub>s</sub> :	0.178	S <sub>DS</sub> :	0.190	
<b>S</b> <sub>1</sub> :	0.063	<b>S</b> <sub>D1</sub> :	0.101	
F <sub>a</sub> :	1.600	Τ <sub>L</sub> :	6.000	
$F_v$ :	2.400	PGA :	0.090	
S <sub>MS</sub> :	0.285	PGA M:	0.143	
S <sub>M1</sub> :	0.151	F <sub>PGA</sub> :	1.600	
		l <sub>e</sub> :	1	

#### Seismic Design Category B



Data Accessed: Date Source:

Thu Aug 30 2018

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



#### Ice

#### Results:

Ice Thickness:	1.00 in.
Concurrent Temperature:	5 F
Gust Speed:	50 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Thu Aug 30 2018

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

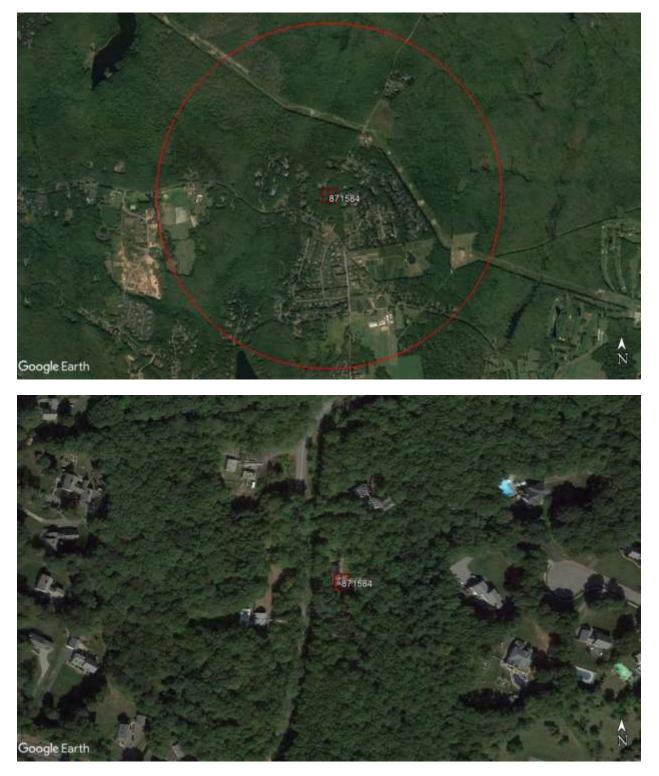
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

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#### 871584 – John Tom Hill Exposure C, Topographic Category 1



# Exhibit D

**Mount Analysis** 



Date: May 2, 2019

Kevin Morrow Crown Castle 3530 Toringdon Way Charlotte, NC 28277		Paul J Ford and 250 E. Broad S Columbus, OH 614.221.6679	treet, Suite 600
Subject:	Mount Analysis Report		
Carrier Designation:	<i>T-Mobile</i> Equipment Change-o Carrier Site Number: Carrier Site Name:	ut	CT11189E Glastonbury/Rt-94 & Fern
Crown Castle Designation:	Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number Crown Castle Purchase Order Crown Castle Order Number:	-	871584 John Tom Hill 559293 1370719 479814 Rev. 0
Engineering Firm Designation:	Paul J Ford and Company Proj	ect Number:	A37519-1779.001.8190
Site Data:	115 Birch Mtn. Road, Glastonb Latitude 41.708956°, Longitude		ounty, CT
Structure Information:	Tower Height & Type: Mount Elevation: Mount Type:	182 Foot	elf Support t Sector Frame
Dear Kevin Morrow,	mount rype.	(3) 13 F001	

Paul J Ford and Company is pleased to submit this "Mount Analysis Report" to determine the structural integrity of the T-Mobile antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

#### 15' Sector Frame (typical)

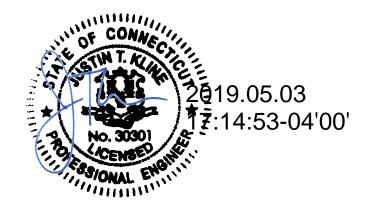
SUFFICIENT\* \*The mount has sufficient capacity once the changes, as described in Section 4.1 Recommendations of this report, are completed.

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Respectfully submitted by:

elekah lon

Rebekah M. Dorris, El Structural Designer RDorris@pauljford.com



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- 9) APPENDIX D SUPPLEMENTAL MODIFICATION INFORMATION

#### **10) APPENDIX E**

MANUFACTURER DRAWINGS (FOR REFERENCE ONLY)

#### 1) INTRODUCTION

The existing mounts under consideration are (3) 15' Sector Frame mounts estimated based on photos and models of previously analyzed mounts of similar type.

#### 2) ANALYSIS CRITERIA

TIA-222 Revision: Risk Category:	TIA-222-H II
Ultimate Wind Speed:	 125 mph
Exposure Category:	С
Topographic Factor at Base:	1.0
Topographic Factor at Mount:	1.0
Ice Thickness:	2.0
Wind Speed with Ice:	50 mph
Live Loading Wind Speed:	30 mph
Man Live Load at Mid/End-Points:	250 lb
Man Live Load at Mount Pipes:	500 lb

Mount Centerline (ft)		Number of Antennas	Antenna Manufacturer	Antenna Model	Mount / Modification Details
	183	3	Ericsson	KRY 112 489/2	
100		3	RFS	APXVAARR24_43-U-NA20	(3) 15' Sector Frame
182 177		3	RFS	APXV18-209015-C-A20	(3) 15 Sector Frame
		3	Ericsson	RADIO 4449 B12/B71	

#### 3) ANALYSIS PROCEDURE

#### Table 2 - Documents Provided

Document	Remarks	Reference	Source
Mount Manufacturer Drawings	Antenna Mounting T-Boom (4 Pipe) Dated: 07/07/97	-	Sabre Communications
TIA Inspection	Dated: 01/28/19	-	CCISites
Order	ID: 479814 Rev. 0 Dated: 04/17/19	-	CCISites

#### 3.1) Analysis Method

RISA-3D (version 17.0.2), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 *Tower Mount Analysis* (Revision C).

#### 3.2) Assumptions

- 1) The analysis of the existing tower or the effect of the mount attachment to the tower is not within the current scope of work.
- 2) The antenna mounting system was properly fabricated, installed and maintained in good condition, twist free and plumb in accordance with its original design and manufacturer's specifications and all bolts are tightened as specified by the manufacturer and AISC requirements.
- 3) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1.
- 4) All member connections have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report. All U-Bolt connections have been properly tightened. This analysis will be required to be revised if the existing conditions in the field differ from those shown in the above referenced documents or assumed in this analysis. No allowance was made for any damaged, missing, or rusted members.
- 5) Steel grades are as follows, unless noted otherwise:

	-
a) Channel, Solid Round, Angle, Plate, Unistrut	ASTM A36 (GR 36)
b) Pipe	ASTM A53 (GR 35)
c) HSS (Rectangular)	ASTM 500 (GR B-46)
d) HSS (Round)	ASTM 500 (GR B-42)
e) Threaded Rods	ASTM F1554 (GR 36)
f) Connection Bolts	ASTM A325
g) U-Bolts	SAE J429 (GR 2)
Proposed againment is to be installed in the leasting	no apposified in Appondix A

- 6) Proposed equipment is to be installed in the locations specified in Appendix A. Any changes to the proposed equipment locations will render this report invalid.
- 7) Mount has been modeled based on photographs and the TIA inspection referenced in Table 2, indicating a match to the Sabre Communications Antenna Mounting T-Boom (4 Pipes). Member information and dimensions not provided have been assumed to match those specified in the manufacturer drawings referenced in Table 2. No guarantee can be made as to the accuracy of these assumptions without a complete mount mapping.
- 8) Existing mount pipes are replaced with 8-ft long, P2.0 X-STR (2.38" O.D. x 0.204") mount pipes where required.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the mount.

#### 4) ANALYSIS RESULTS

#### **Table 3 - Mount Component Capacity**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1, 2	Face Horizontals		55.1	Pass
1, 2	Standoff Members		78.5	Pass
1, 2	Tie Backs	182	13.8	Pass
1, 2	Bracing Members	102	28.3	Pass
1, 2	Mount Pipes		70.0	Pass
1, 2	Mount to Tower Connection		22.8	Pass

#### Mount Rating (max from all components) =

78.5%

Notes:

See additional documentation in "Appendix C – Software Analysis Output" for calculations supporting the % capacity consumed.

2) All sectors are typical.

#### Table 4 - Tieback Connection Data Table

Tower Connection Node No.	Existing / Proposed	Resultant End Reaction (Ib)	Connected Member Type	Connected Member Size	Member Compressive Capacity (lb) <sup>3</sup>	Notes
N76	Existing	823	Leg	Pipe 3.5 x 0.3	5817	1, 3
N75A	Proposed	1143	Leg	Pipe 3.5 x 0.3	1745	2, 3

Notes:

1) Tieback connection point is within 25% of either end of the connected tower member

2) Tieback connection point is NOT within 25% of either end of the connected tower member

3) Reduced member compressive capacity according to CED-STD-10294 *Standard for Installation of Mounts and Appurtenances* 

#### 4.1) Recommendations

The mount will have sufficient capacity to carry the proposed loading configuration. In order for the results of the analysis to be considered valid, modification listed below must be completed:

- Install SitePro1 STK-U Stiff Arm Kit or EOR approved equivalent in accordance with attached manufacturer drawings. The new tieback is to be installed as shown in "Appendix D – Supplemental Modification Information". Connection to tower must be to adjacent tower leg.
- Replace existing mount pipes with new 8-ft. long P2.0 X-STR (2.38" O.D. x 0.204") where required. See Appendix A/D details.

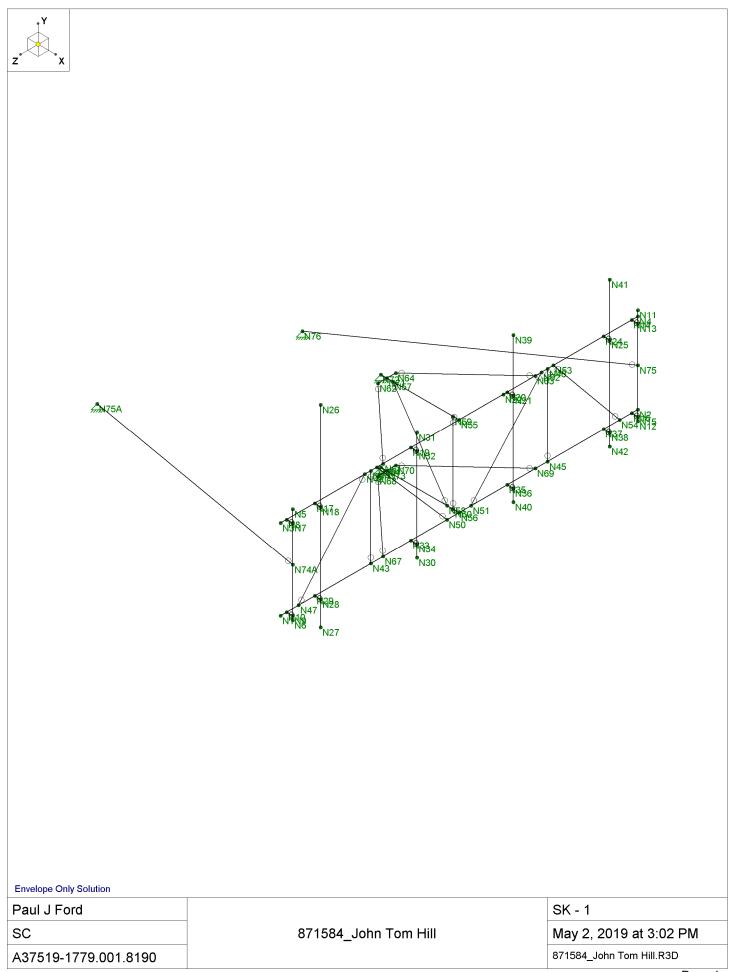
No structural modifications are required at this time, provided that the above-listed changes are implemented.

### STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON EXISTING MOUNTS BY PAUL J. FORD AND COMPANY

- 1) It is the responsibility of the client to ensure that the information provided to Paul J. Ford and Company is accurate and complete. Paul J. Ford and Company will rely on the accuracy and completeness of such information in performing or furnishing services under this project.
- 2) If the existing conditions are not as represented on the referenced drawings and/or documents, Paul J. Ford and Company should be contacted immediately to evaluate the significance of the deviation.
- 3) The mount has been analyzed according to the minimum design loads recommended by the Reference Standard. If additional design loads are required, Paul J. Ford and Company should be made aware of this prior to the start of the project.
- 4) The standard of care for all Professional Engineering Services performed or furnished by Paul J. Ford and Company under this project will be the skill and care used by members of the Consultant's profession practicing under similar circumstances at the same time and in the same locality.
- 5) All Services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Paul J. Ford and Company is not responsible for the conclusions, opinions and/or recommendations made by others based on the information supplied herein.

## APPENDIX A

## WIRE FRAME AND RENDERED MODELS



Add (1) APXVAARR24_		roposed 8-ft long P2.0 X-STR ipe mount
Envelope Only Solution Paul J Ford SC A37519-1779.001.8190	871584_John Tom Hill	SK - 2 May 2, 2019 at 3:02 PM 871584_John Tom Hill.R3D

## APPENDIX B

## SOFTWARE INPUT CALCULATION

### ANSI/TIA-222H - WIND & ICE LOAD CALCULATIONS

Site Code/Name	871584 - John Tom Hill
State	Connecticut
County	Hartford
V	125 mph
Vi	50 mph
t <sub>i</sub>	2.0 in
Z <sub>s</sub>	880 ft
Z	182 ft

Structure Class	II
Exposure Category	С
Topographic Category	1
Wind direction probability factor	0.95
Gust factor	1
Wind Pressure (including Ka = 0.9)	47.56 psf
t <sub>iz</sub>	2.37 in

Dead and Wind Forces for Equipment									
Manufacturer	Model	L [in]	W [in]	D [in]	0º [lbs]	30 <sup>o</sup> [lbs]	60° [lbs]	90° [lbs]	Weight [lbs]
RFS	APXV18-209015-C-A20	72	6.65	3.15	241.6	217.3	168.7	144.5	25.3
RFS	APXVAARR24_43-U-NA20	95.9	24	8.7	962.7	827.7	557.7	422.7	128.0
Ericsson	KRY 112 489/2	11	6.1	3.94	26.6	24.3	19.7	17.4	15.4
Ericsson	RADIO 4449 B12/B71	14.95	13.19	9.25	78.2	72.3	60.6	54.8	75.0



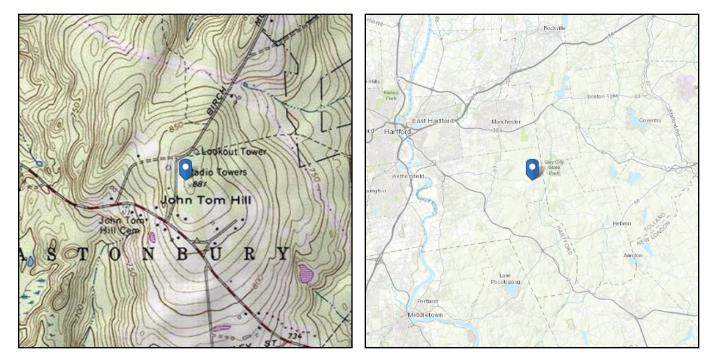
## ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

 Elevation:
 879.67 ft (NAVD 88)

 Latitude:
 41.708889

 Longitude:
 -72.473333



### Wind

#### **Results:**

Wind Speed: 10-year MRI 25-year MRI 50-year MRI 100-year MRI	125 Vmph 77 Vmph 87 Vmph 94 Vmph 102 Vmph
Data Source:	ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of March 12, 2014
Date Accessed:	Thu May 02 2019

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

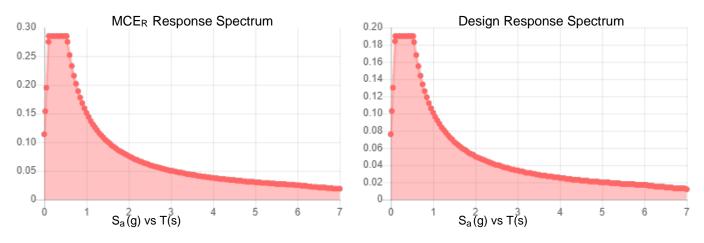
Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



Site Soil Class: Results:	D - Stiff Soil			
S <sub>S</sub> :	0.178	S <sub>DS</sub> :	0.19	
S <sub>1</sub> :	0.063	<b>S</b> <sub>D1</sub> :	0.101	
F <sub>a</sub> :	1.6	T <sub>L</sub> :	6	
F <sub>v</sub> :	2.4	PGA :	0.09	
S <sub>MS</sub> :	0.285	PGA M:	0.143	
S <sub>M1</sub> :	0.151	F <sub>PGA</sub> :	1.6	
		l <sub>e</sub> :	1	

#### Seismic Design Category B



Data Accessed: Date Source:

#### Thu May 02 2019

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



#### Ice

#### Results:

Ice Thickness:	1.00 in.
Concurrent Temperature:	5 F
Gust Speed:	50 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Thu May 02 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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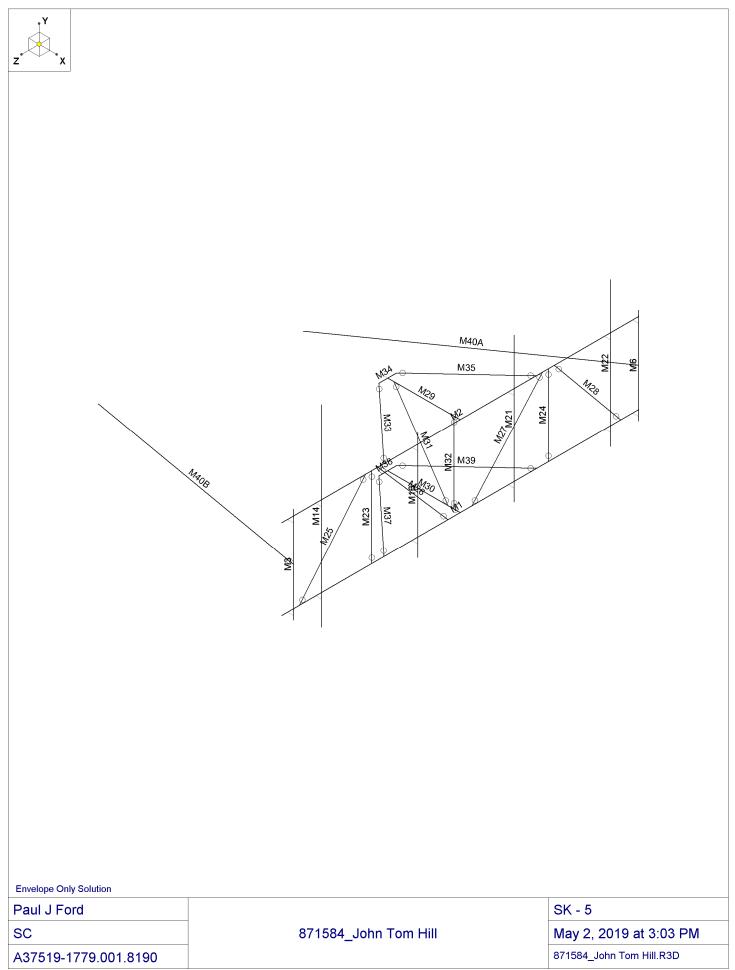
In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

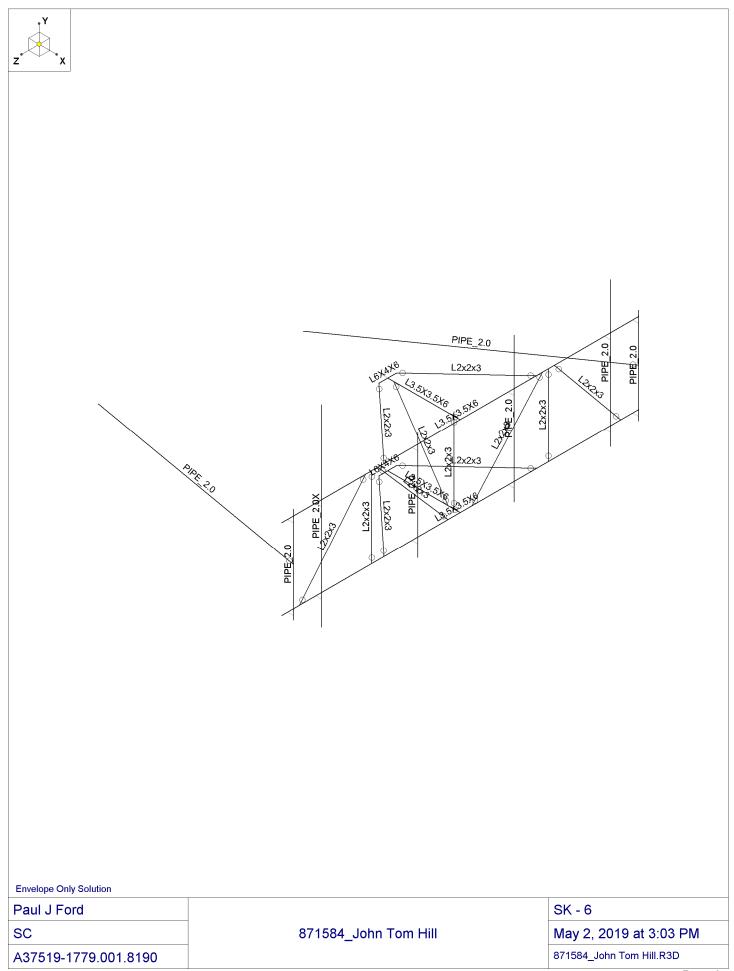
## APPENDIX C

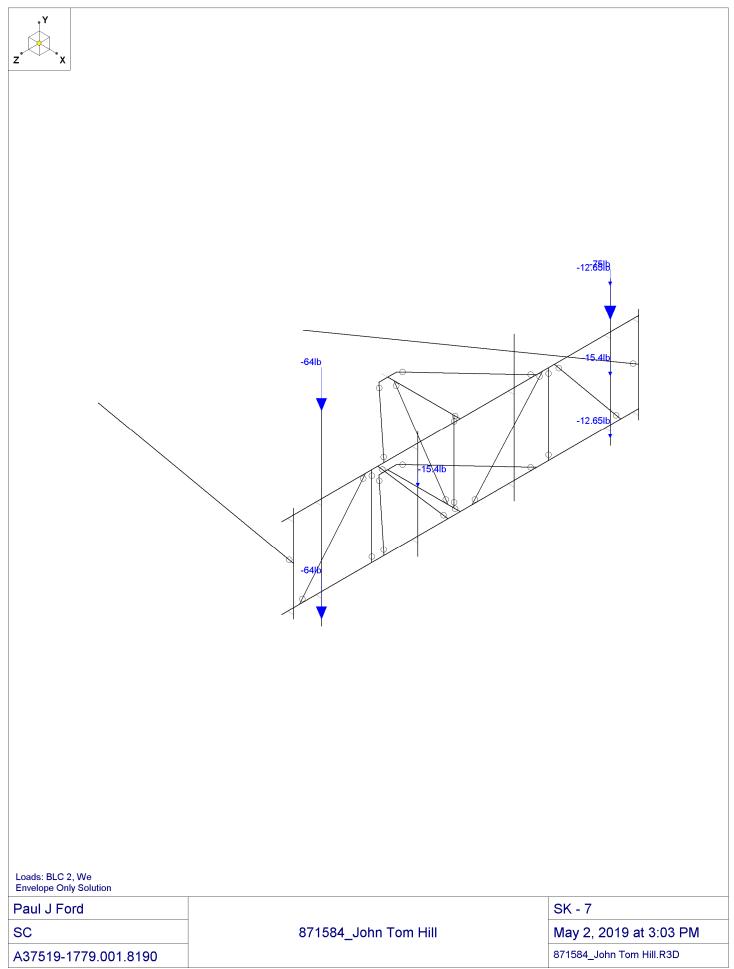
## SOFTWARE ANALYSIS OUTPUT

Member Code Checks Displayed (Enveloped) Envelope Only Solution
Paul J Ford         SK - 3           SC         871584_John Tom Hill         May 2, 2019 at 3:02 PM

		Shear Check (Erv) 9-0-10 50-75 0-50
Member Shear Checks Displayed (En Envelope Only Solution	nveloped)	
Paul J Ford		SK - 4
SC	871584_John Tom Hill	May 2, 2019 at 3:02 PM
A37519-1779.001.8190		871584_John Tom Hill.R3D





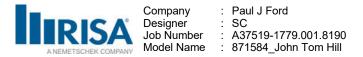




## (Global) Model Settings

	-
Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	24
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): LRFD
Cold Formed Steel Code	AISI S100-16: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None
Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR SET ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8
	v

May 2, 2019 3:03 PM Checked By:\_



## (Global) Model Settings, Continued

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1

## Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (\1E	Density[k/ft	Yield[ksi]	Rv	Fu[ksi]	Rt
1	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	1.1
4	A500 Gr.B 42	29000	11154	.3	.65	.49	42	1.4	58	1.3
5	A500 Gr.B 46	29000	11154	.3	.65	.49	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	.3	.65	.49	35	1.6	60	1.2
7	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3

## Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N1	N2		270	L3.5X3.5X6	Beam	Single Angle	A36 Gr.36	Typical
2	M2	N3	N4		180	L3.5X3.5X6	Beam	Single Angle	A36 Gr.36	Typical
3	M3	N5	N6			PIPE 2.0	Column	Pipe	A53 Gr.B	Typical
4	M4	N7	N8			RIGID	None	None	RIGID	Typical
5	M5	N9	N10			RIGID	None	None	RIGID	Typical
6	M6	N11	N12			PIPE 2.0	Column	Pipe	A53 Gr.B	Typical
7	M7	N13	N14			RIGĪD	None	None	RIGID	Typical
8	M8	N15	N16			RIGID	None	None	RIGID	Typical
9	M9	N17	N18			RIGID	None	None	RIGID	Typical
10	M10	N19	N32			RIGID	None	None	RIGID	Typical
11	M11	N20	N21			RIGID	None	None	RIGID	Typical
12	M13	N24	N25			RIGID	None	None	RIGID	Typical
13	M14	N26	N27			PIPE 2.0X	Column	Pipe	A53 Gr.B	Typical
14	M15	N28	N29			RIGID	None	None	RIGID	Typical
15	M16	N31	N30			PIPE 2.0	Column	Pipe	A53 Gr.B	Typical
16	M18	N33	N34			RIGID	None	None	RIGID	Typical
17	M19	N35	N36			RIGID	None	None	RIGID	Typical
18	M20	N37	N38			RIGID	None	None	RIGID	Typical
19	M21	N39	N40			PIPE 2.0	Column	Pipe	A53 Gr.B	Typical

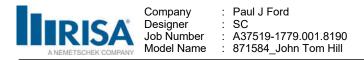


## Member Primary Data (Continued)

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Туре	Design List	Material	Design Rules
20	M22	N41	N42			PIPE 2.0	Column	Pipe	A53 Gr.B	Typical
21	M23	N43	N44		270	L2x2x3	Column	Single Angle	A36 Gr.36	Typical
22	M24	N45	N46			L2x2x3	Column	Single Angle	A36 Gr.36	Typical
23	M25	N47	N48		180	L2x2x3	VBrace	Single Angle	A36 Gr.36	Typical
24	M26	N49	N50		180	L2x2x3	VBrace	Single Angle	A36 Gr.36	Typical
25	M27	N51	N52		180	L2x2x3	VBrace	Single Angle	A36 Gr.36	Typical
26	M28	N53	N54		180	L2x2x3	VBrace	Single Angle	A36 Gr.36	Typical
27	M29	N55	N71		90	L3.5X3.5X6	Beam	Single Angle	A36 Gr.36	Typical
28	M30	N56	N73			L3.5X3.5X6	Beam	Single Angle	A36 Gr.36	Typical
29	M31	N57	N58		90	L2x2x3	VBrace	Single Angle	A36 Gr.36	Typical
30	M32	N59	N60			L2x2x3	Column	Single Angle	A36 Gr.36	Typical
31	M33	N61	N62		90	L2x2x3	Beam	Single Angle	A36 Gr.36	Typical
32	M34	N62	N64			L6X4X6	Beam	Single Angle	A36 Gr.36	Typical
33	M35	N63	N64		180	L2x2x3	Beam	Single Angle	A36 Gr.36	Typical
34	M37	N67	N68			L2x2x3	Beam	Single Angle	A36 Gr.36	Typical
35	M38	N70	N68		180	L6X4X6	Beam	Single Angle	A36 Gr.36	Typical
36	M39	N69	N70		270	L2x2x3	Beam	Single Angle	A36 Gr.36	Typical
37	M40	N71	N72			RIGID	None	None	RIGID	Typical
38	M41	N73	N74			RIGID	None	None	RIGID	Typical
39	M40A	N75	N76			PIPE 2.0	Beam	Pipe	A53 Gr.B	Typical
40	M40B	N74A	N75A			PIPE_2.0	Beam	Pipe	A53 Gr.B	

## Member Advanced Data

	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Defl Rat	Analysis	Inactive	Seismic
1	M1						Yes	Default			None
2	M2						Yes				None
3	M3						Yes	** NA **			None
4	M4		000X00				Yes	** NA **			None
5	M5		000X00				Yes	** NA **			None
6	M6						Yes	** NA **			None
7	M7		000X00				Yes	** NA **			None
8	M8		000X00				Yes	** NA **			None
9	M9	OOOXOX					Yes	** NA **			None
10	M10	000X0X					Yes	** NA **			None
11	M11	000X0X					Yes	** NA **			None
12	M13	000X0X					Yes	** NA **			None
13	M14						Yes	** NA **			None
14	M15		000X00				Yes	** NA **			None
15	M16						Yes	** NA **			None
16	M18	000X0X					Yes	** NA **			None
17	M19	000X0X					Yes	** NA **			None
18	M20	000X0X					Yes	** NA **			None
19	M21						Yes	** NA **			None
20	M22						Yes	** NA **			None
21	M23	BenPIN	BenPIN				Yes	** NA **			None
22	M24	BenPIN	BenPIN				Yes	** NA **			None
23	M25	BenPIN	BenPIN				Yes	** NA **			None
24	M26	BenPIN	BenPIN				Yes	** NA **			None
25	M27	BenPIN	BenPIN				Yes	** NA **			None
26	M28	BenPIN	BenPIN				Yes	** NA **			None
27	M29	BenPIN					Yes	Default			None
28	M30	BenPIN					Yes	Default			None
29	M31	BenPIN	BenPIN				Yes	** NA **			None
30	M32	BenPIN	BenPIN				Yes	** NA **			None
31	M33	BenPIN	BenPIN				Yes	Default			None



## Member Advanced Data (Continued)

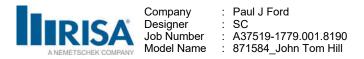
	Label	I Release	J Release	I Offset[in]	J Offset[in]	T/C Only	Physical	Defl Rat	.Analysis	Inactive	Seismic
32	M34						Yes				None
33	M35	BenPIN	BenPIN				Yes	Default			None
34	M37	BenPIN	BenPIN				Yes	Default			None
35	M38						Yes				None
36	M39	BenPIN	BenPIN				Yes	Default			None
37	M40						Yes	** NA **			None
38	M41						Yes	** NA **			None
39	M40A	BenPIN					Yes	Default			None
40	M40B	BenPIN					Yes	Default			None

## Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in] L-torgu	. Kvv	Kzz	Cb	Function
1	M1	L3.5X3.5X6	178	51	51	Lbyy					Lateral
2	M2	L3.5X3.5X6	178	51	51	Lbyy					Lateral
3	M3	PIPE 2.0	48			Lbyy					Lateral
4	M6	PIPE 2.0	48			Lbyy					Lateral
5	M14	PIPE 2.0X	96			Lbyy					Lateral
6	M16	PIPE 2.0	54			Lbyy					Lateral
7	M21	PIPE 2.0	72			Lbyy					Lateral
8	M22	PIPE 2.0	72			Lbyy					Lateral
9	M23	L2x2x3	40			Lbyy					Lateral
10	M24	L2x2x3	40			Lbyy					Lateral
11	M25	L2x2x3	51.856			Lbyy					Lateral
12	M26	L2x2x3	53.151			Lbyy					Lateral
13	M27	L2x2x3	53.151			Lbyy					Lateral
14	M28	L2x2x3	51.856			Lbyy					Lateral
15	M29	L3.5X3.5X6	36			Lbyy					Lateral
16	M30	L3.5X3.5X6	36			Lbyy					Lateral
17	M31	L2x2x3	48.26			Lbyy					Lateral
18	M32	L2x2x3	40			Lbyy					Lateral
19	M33	L2x2x3	49.176			Lbyy					Lateral
20	M34	L6X4X6	9			Lbyy					Lateral
21	M35	L2x2x3	49.176			Lbyy					Lateral
22	M37	L2x2x3	49.176			Lbyy					Lateral
23	M38	L6X4X6	9			Lbyy					Lateral
24	M39	L2x2x3	49.176			Lbyy					Lateral
25	M40A	PIPE 2.0	120			Lbyy					Lateral
26	M40B	PIPE_2.0	120			Lbyy					Lateral

## **Basic Load Cases**

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(Me	Surface(P
1	Self We	DĽ		-1.1						,
2	We	DL					7			
3	Ice We	DL					7	24		
4	W0	WL					7	24		
5	W30	WL					14	48		
6	W60	WL					14	48		
7	W90	WL					7	24		
8	W120	WL					14	48		
9	W150	WL					14	48		
10	W0 + Ice	WL					7	24		
11	W30 + Ice	WL					14	48		
12	W60 + Ice	WL					14	48		
13	W90 + Ice	WL					7	24		



## Basic Load Cases (Continued)

_	<b>BLC</b> Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(Me	Surface(P
14	W120 + Ice	WL					14	48		
15	W150 + Ice	WL					14	48		
16	500lbs LM 1	LL				1				
17	500lbs LM 2	LL				1				
18	500lbs LM 3	LL				1				
19	500lbs LM 4	LL				1				
20	250lbs LV 5	LL				1				
21	250lbs LV 6	LL				1				

## Load Combinations

$\begin{array}{c c c c c c c c c c c c c c c c c c c $		
2       Dead + Wind 0°       Yes       Y       1       1.2       2       1.2       4       1		
3       Dead + Wind 30°       Yes       Y       1       1.2       2       1.2       5       1		
4       Dead + Wind 60°       Yes       Y       1       1.2       2       1.2       6       1       Image: constraint of the state		
5       Dead + Wind 90°       Yes       Y       1       1.2       2       1.2       7       1            6       Dead + Wind 120°       Yes       Y       1       1.2       2       1.2       8       1 <td< td=""><td></td><td></td></td<>		
6       Dead + Wind 120°       Yes       Y       1       1.2       2       1.2       8       1		
7       Dead + Wind 150°       Yes       Y       1       1.2       2       1.2       9       1         8       Dead + Wind 180°       Yes       Y       1       1.2       2       1.2       4       -1         9       Dead + Wind 210°       Yes       Y       1       1.2       2       1.2       5       -1         10       Dead + Wind 240°       Yes       Y       1       1.2       2       1.2       6       -1		
8         Dead + Wind 180°         Yes         Y         1         1.2         2         1.2         4         -1         Image: Constraint of the state		
9         Dead + Wind 210°         Yes         Y         1         1.2         2         1.2         5         -1         Image: Constraint of the second s		
10         Dead + Wind 240°         Yes         Y         1         1.2         2         1.2         6         -1	_	
12 Dead + Wind 300° Yes Y 1 1.2 2 1.2 8 -1		
13 Dead + Wind 330° Yes Y 1 1.2 2 1.2 9 -1		
14 Dead + Ice + Wind Ice 0° Yes Y 1 1 1.2 2 1.2 10 1 3 1		
15 Dead + Ice + Wind Ice 30° Yes Y 1 1.2 2 1.2 11 1 3 1		
16         Dead + Ice + Wind Ice 60° Yes         Y         1         1.2         2         1.2         1         3         1		
17         Dead + Ice + Wind Ice 90° Yes         Y         1         1.2         2         1.2         13         1         3         1		
18 Dead + Ice + Wind Ice 1 Yes Y 1 1 1.2 2 1.2 14 1 3 1		
19         Dead + Ice + Wind Ice 1 Yes         Y         1         1.2         2         1.2         1         3         1		
20 Dead + Ice + Wind Ice 1 Yes Y 1 1 1.2 2 1.2 10 -1 3 1		
21         Dead + Ice + Wind Ice 2 Yes         Y         1         1.2         2         1.2         11         -1         3         1		
22         Dead + Ice + Wind Ice 2 Yes         Y         1         1.2         2         1.2         12         -1         3         1		
23 Dead + Ice + Wind Ice 2 Yes Y 1 1.2 2 1.2 13 -1 3 1		
24         Dead + Ice + Wind Ice 3         Yes         Y         1         1.2         2         1.2         14         -1         3         1		
25 Dead + Ice + Wind Ice 3 Yes Y 1 1.2 2 1.2 15 -1 3 1		
26 Dead + LM5001 + Wred 0°Yes Y 1 1.2 2 1.2 16 1.5 4 .08		
27 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 5 .08		
28 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 6 .08		
29 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 7 .08		
30 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 8 .08		
31 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 9 .08		
32 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 408		
33         Dead + LM5001 + Wred Yes         Y         1         1.2         2         1.2         16         1.5         5        08		
34         Dead + LM5001 + Wred Yes         Y         1         1.2         2         1.2         16         1.5         6        08		
35 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 708		
36 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 808		
37 Dead + LM5001 + Wred Yes Y 1 1.2 2 1.2 16 1.5 908		
38 Dead + LM5002 + Wred 0°Yes Y 1 1.2 2 1.2 17 1.5 4 .08		
39 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 5 .08		
40 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 6 .08		
41 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 7 .08		
42 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 8 .08		
43 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 9 .08		
44 Dead + LM5002 + Wred Yes Y 1 1.2 2 1.2 17 1.5 408		



### Load Combinations (Continued)

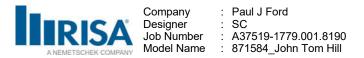
	Description	SoP	S	BLC	Fac																		
45	Dead + LM5002 + Wred	Yes Y		1	1.2	2	1.2	17	1.5	5	08												
46	Dead + LM5002 + Wred	Yes Y		1	1.2	2	1.2	17	1.5	6	08												
47	Dead + LM5002 + Wred	Yes Y		1	1.2	2	1.2	17	1.5	7	08												
48	Dead + LM5002 + Wred	Yes Y		1	1.2	2	1.2	17	1.5	8	08												
49	Dead + LM5002 + Wred	Yes Y		1	1.2	2	1.2	17	1.5	9	08												
50	Dead + LM5003 + Wred 0	°Yes Y		1	1.2	2	1.2	18	1.5	4	.08												
51	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	5	.08												
52	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2		1.5		.08												
53	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	7	.08												
54	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	8	.08												
55	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	9	.08												
56	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	4	08												
57	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	5	08												
58	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	6	08												
59	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	7	08												
60	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	8	08												
61	Dead + LM5003 + Wred	Yes Y		1	1.2	2	1.2	18	1.5	9	08												
62	Dead + LM5004 + Wred 0	°Yes Y		1	1.2	2	1.2	19	1.5	4	.08												
63	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	5	.08												
64	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	6	.08												
65	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	7	.08												
66	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	8	.08												
67	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	9	.08												
68	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	4	08												
69	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	5	08												
70	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2		1.5	6	08												
71	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	7	08												
72	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2	19	1.5	8	08												
73	Dead + LM5004 + Wred	Yes Y		1	1.2	2	1.2		1.5		08												
74	Dead + LV2505	Yes Y		1	1.2	2	1.2		1.5														
75	Dead + LV2506	Yes Y		1	1.2	2	1.2	21	1.5														
76	Service 60mph Wind 0°	Yes Y		1	1	2	1	4	.32														

## Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-in]	LC	MY [k-in]	LC	MZ [k-in]	LC
1	N72	max	493.429	2	4763.204	17	1455.366	12	Ō	76	Ō	76	Ō	76
2		min	-4341.472	20	1038.458	76	-1607.872	6	0	1	0	1	0	1
3	N74	max	4164.715	14	-121.637	76	1471.337	72	0	76	0	76	0	76
4		min	570.688	8	-617.981	25	-1333.973	30	0	1	0	1	0	1
5	N76	max	682.54	13	95.449	25	430.954	7	0	76	0	76	0	76
6		min	-701.25	7	19.559	76	-421.22	13	0	1	0	1	0	1
7	N75A	max	1126.898	3	97.271	21	188.469	3	0	76	0	76	0	76
8		min	-1141.527	9	9.505	3	-187.862	9	0	1	0	1	0	1
9	Totals:	max	3236.535	2	4328.462	23	1933.339	12						
10		min	-3236.519	8	954.428	76	-1933.338	6						

#### Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Member	Shape	Code	Loc[in]	LC	Shear	.Loc[in]	Dir L	.C phi*Pnc [	.phi*Pnt [l	phi*Mn y	.phi*Mn z(	<u>Cb Egn</u>
1	M29	L3.5X3.5X6	.785	33	17	.183	36	zí	869978.801	81000	40.078	89.424	H2-1
2	M14	PIPE 2.0X	.700	44	8	.339	44	e	32 19844.858	44100	30.366	30.366	IH1-1b
3	M30	L3.5X3.5X6	.642	6	15	.191	6	y 2	2 <mark>4</mark> 69978.801	81000	40.078	89.424	I H2-1
4	M2	L3.5X3.5X6	.551	50.063	7	.068	46.354	y 2	2 <mark>1</mark> 60395.819	81000	40.078	62.061	1 H2-1
5	M16	PIPE 2.0	.498	8.438	63	.691	47.813	6	3 <mark>25203.832}}</mark>	32130	22.459	22.459	I H3-6
6	M3	PIPE 2.0	.494	24	3	.278	24	3	3 <mark>3</mark> 26521.424	32130	22.459	22.459	IH1-1b



## Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)

	Member	Shape	Code	Loc[in]	LC	Shear	.Loc[in]	Dir L	LCp	hi*Pnc [	phi*Pnt [l	phi*Mn y	.phi*Mn z	.Cb	Egn
7	M1	L3.5X3.5X6	.474	66.75	73	.076	89	ΖĹ	176	0395.819	81000	40.078	62.061	1	H2-1
8	M26	L2x2x3	.434	27.129	17	.055	53.151	y (	62 8	8736.909	23392.8	6.693	12.692	1	H2-1
9	M21	PIPE 2.0	.432	26.25	63	.692	66	Ē	632	0866.733	32130	22.459	22.459	1	H3-6
10	M31	L2x2x3	.348	24.13	15	.062	0	z	331	0403.802	23392.8	6.693	12.991	1	H2-1
11	M6	PIPE 2.0	.329	24	13	.321	46	6	632	6521.424	32130	22.459	22.459	1	H1-1b
12	M27	L2x2x3	.283	26.022	35	.052	0				23392.8		12.692	1	H2-1
13	M33	L2x2x3	.205	24.588	13	.011	49.176	zź	241	0085.728	23392.8	6.693	12.933	1	H2-1
14	M22	PIPE 2.0	.188	66	63	.387	66		00	0866.733	02100	22.459	22.459	1	H3-6
15	M37	L2x2x3	.182	24.588	25	.012	0				23392.8		12.933	1	H2-1
16	M35	L2x2x3	.179	24.588	15	.011	49.176				23392.8		12.933	1	H2-1
17	M32	L2x2x3	.154	21.25	25	.098	0	y e	631	3407.172	23392.8	6.693	13.532	1	H2-1
18	M28	L2x2x3	.145	25.928	16	.036	0	y (	63 9	9179.087	23392.8	6.693	12.769	1	H2-1
19	M40B	PIPE 2.0	.138	60	16	.010	120		23 9	9836.597	32130	22.459	22.459	1	H1-1b
20	M40A	PIPE 2.0	.138	60	25	.010	0		25 9	9836.597	32130	22.459	22.459	1	H1-1b
21	M34	L6X4X6	.127	4.5	7	.051	4.5	Z	7 1	07464	116964	61.31	184.212	1	H2-1
22	M25	L2x2x3	.126	25.928	24	.032	0	y (	33 9	9179.087	23392.8	6.693	12.769	1	H2-1
23	M39	L2x2x3	.115	24.588	28	.010	49.176	zź	231	0085.728	23392.8	6.693	12.933	1	H2-1
24	M38	L6X4X6	.076	4.5	72	.031	4.5	z	721	07464	116964	61.31	176.892	1	H2-1
25	M23	L2x2x3	.061	20	2	.077	40	z	621	3407.172	23392.8	6.693	13.532	1	H2-1
26	M24	L2x2x3	.049	20	2	.078	0	y (	631	3407.172	23392.8	6.693	13.532	1	H2-1

SITE DETAILS			
Site Name/Code	871584	4 - John Tom Hill	
Date	0	2/05/2019	
Engineer		SC	
CONNECTION PARAMETERS			
Loadcase #		17	
Number of bolts		4	
Bolt Diameter	d	<b>1/2</b> in	
Tensile Area	A <sub>b</sub>	0.20 in $^{2}$	
Tensile Area	A <sub>n</sub>	0.14 in <sup>2</sup>	
Grade	J4	29 Grade 2	A State of the second
Bolt Ultimate Strength	F <sub>ub</sub>	74 <i>ksi</i>	
Connection length reduction factor	Rb	1	Connection Sketch/Photo
CONNECTION LOADS			
Develop Managet	N 4	0.00 literation	

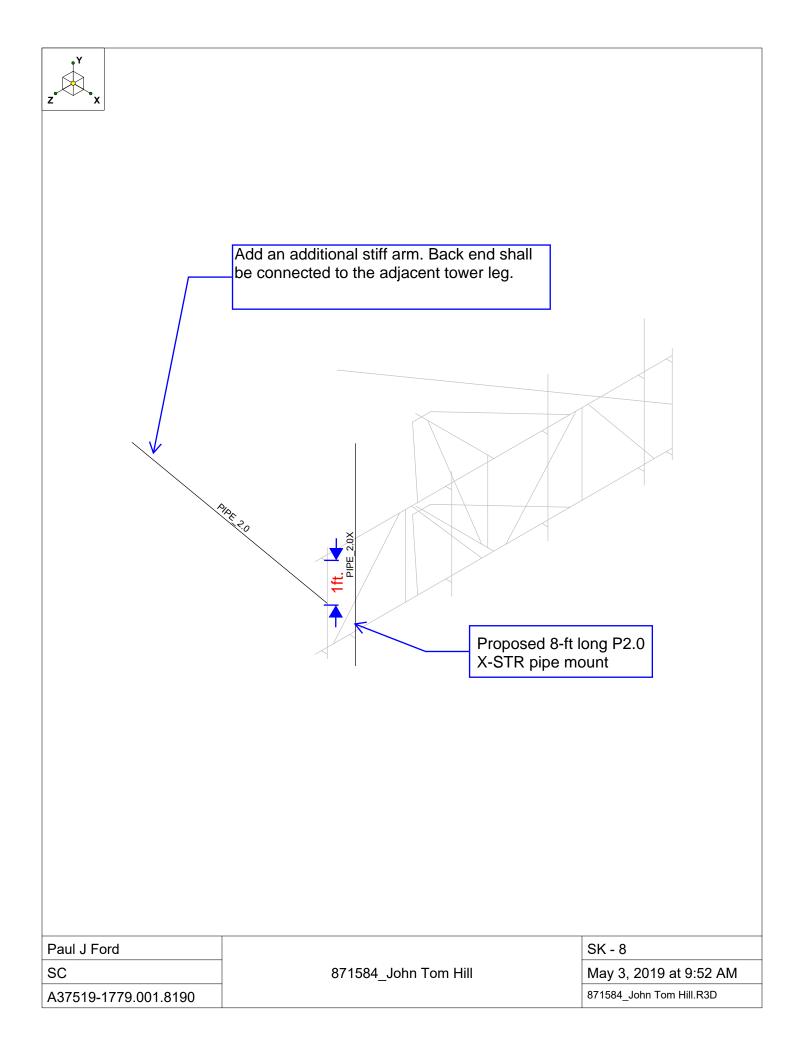
Bending Moment	Мхх	0.00 kips-in
Bending Moment	Mzz	0.00 kips-in
Torsional Moment	Муу	0.00 kips-in
Shear Force	Vx	<b>4.76</b> kips
Shear Force	Vz	<b>1.44</b> kips
Axial Force	Ту	<b>3.89</b> kips

SOF	OFTWARE REACTIONS TABLE										
L	Joint Label	X [lb]	Y [lb]	Z [lb]	MX [k-in]	MY [k-in]	MZ [k-in]				
17	N72	-3893.766	4763.204	-1437.85	0	0	0				
17	N74	3902.776	-610.113	525.789	0	0	0				
17	N76	-207.576	87.547	142.652	0	0	0				
17	N75A	198.649	87.815	11.169	0	0	0				

BOLT CHECK Bolt Tension Capacity			Bolt Shear Capacity				
¢	$R_{nt} = 0.75 F_{ub} A_n$	 φR <sub>nv</sub> = 0.75*0.625*0.8*Fub*Ab*Rb					
	$\phi R_{nt} =$	<b>7.9</b> kips	φR <sub>nv</sub> =	<b>5.4</b> kips			
Maximum Bolt Tension			Maximum Bolt Shear				
	$T_{ub} = F_{Mxx} + F_{Mzz} + 7$	Г <sub>у</sub> /4	$V_{ub} = sqrt ((V_x/4)^2 + (V_y/4)^2) + F_{Myy}$				
	T <sub>ub</sub> =	<b>0.97</b> kips	V <sub>ub</sub> =	<b>1.24</b> kips			
Tension Ratio:		12.4% PASS	Shear Ratio:	22.8% PASS			
$(T_{ub} / \varphi R_{nt})^2 + (V_{ub} / \varphi R_{nv})^2 < 1.0$	Ratio	6.7% PASS					

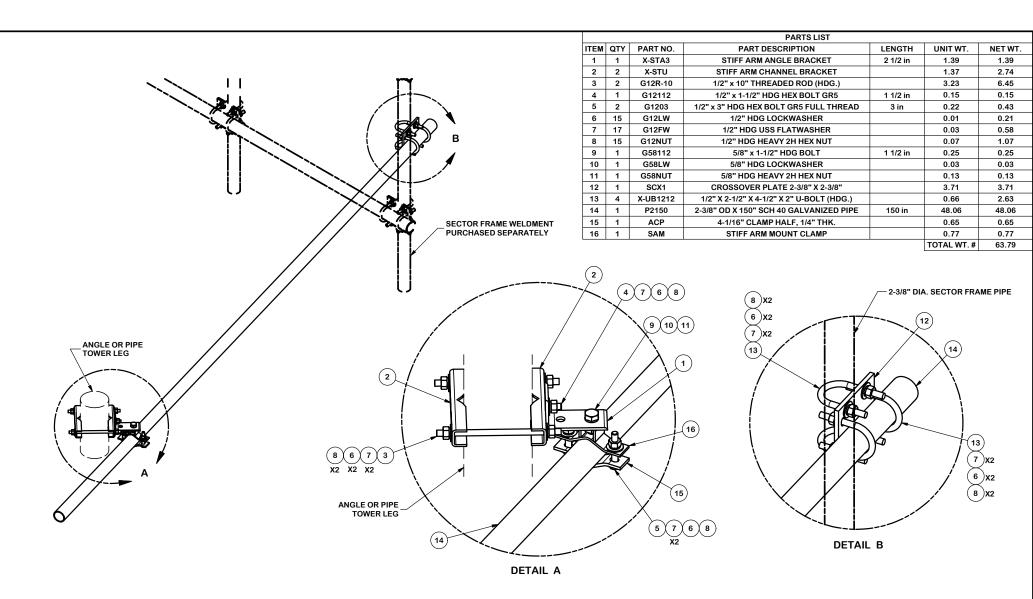
# APPENDIX D

# SUPPLEMENTAL MODIFICATION INFORMATION



# APPENDIX E

# MANUFACTURER DRAWINGS (FOR REFERENCE ONLY)



TOLERANCE NOTES TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE: SAWED, SHEARED AND GAS CUT EDGES (± 0.0307) DRILLED AND GAS CUT HOLES (± 0.0307) - NO CONING OF HOLES LASER CUT EDGES AND HOLES (± 0.0107) - NO CONING OF HOLES BENDS ARE ± 1/2 DEGREE	DESCRIPT	ION SECTOR FRA STIFF ARM P		A valmont V comment	Location: New York Engineering Atlanta, C Support Team: Los Ange 1-888-753-7446 Plymouth Salem, O Dallas, T	k, NY GA eles, CA h, IN DR
ALL OTHER MACHINING (± 0.030") ALL OTHER ASSEMBLY (± 0.060")	CPD NO. 4647	DRAWN BY KC8 8/16/2012	ENG. APPROVAL	PART NO.	STK-U	- 1
PROPRIETARY NOTE: THE DATA AND TECHNIQUER CONTAINED IN THIS DRAWING ARE PROPRIETARY INFORMATION OF VALMONT INDUSTRIES AND CONSIDERED A TRADE SECRET. ANY USE OR DISCLOSURE WITHOUT THE CONSENT OF VALMONT INDUSTRIES IS STRUCTLY PROVINTED.	CLASS SU	B DRAWING USAGE	СНЕСКЕД ВУ СЕК 2/18/2013	DWG. NO.	STK-U	

# Exhibit E

**Power Density/RF Emissions Report** 

Wireless Network Design and Deployment

# Radio Frequency Emissions Analysis Report

# **T-MOBILE** Existing Facility

# Site ID: CT11189E

Glastonbury/ Rt-94 & Fern 115 Birch Mountain Road Glastonbury, CT 06033

May 28, 2019

**Transcom Engineering Project Number: 737001-0047** 

Site Compliance Summary							
Compliance Status:	COMPLIANT						
Site total MPE% of FCC general population allowable limit:	6.84 %						

Wireless Network Design and Deployment

May 28, 2019

T-MOBILE Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, CT 6009

### Emissions Analysis for Site: CT11189E - Glastonbury/ Rt-94 & Fern

Transcom Engineering, Inc ("Transcom") was directed to analyze the proposed upgrades to the T-MOBILE facility located at **115 Birch Mountain Road, Glastonbury, CT**, for the purpose of determining whether the emissions from the Proposed T-MOBILE Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm2). The number of  $\mu$ W/cm<sup>2</sup> calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

<u>General population/uncontrolled exposure</u> limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm<sup>2</sup>). The general population exposure limits for the 600 & 700 MHz bands are approximately 400  $\mu$ W/cm<sup>2</sup> and 467  $\mu$ W/cm<sup>2</sup> respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is 1000  $\mu$ W/cm<sup>2</sup>. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

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<u>Occupational/controlled exposure</u> limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over this or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

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## CALCULATIONS

Calculations were performed for the proposed upgrades to the T-MOBILE antenna facility located at **115 Birch Mountain Road, Glastonbury, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-MOBILE is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in *Table 1*:

Technology	Frequency Band	Channel Count	Transmit Power per Channel (W)
LTE	1900 MHz (PCS)	4	40
GSM	1900 MHz (PCS)	1	15
LTE / 5G NR	600 MHz	2	40
LTE	700 MHz	2	20

Table 1: Channel Data Table

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The following antennas listed in *Table 2* were used in the modeling for transmission in the 600, 700 MHz, 1900 MHz (PCS) and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

			Antenna
	Antenna		Centerline
Sector	Number	Antenna Make / Model	(ft)
А	1	RFS APXV18-209015-C-A20	177
А	2	RFS APXVAARR24_43-U-NA20	177
В	1	RFS APXV18-209015-C-A20	177
В	2	RFS APXVAARR24_43-U-NA20	177
С	1	RFS APXV18-209015-C-A20	177
С	2	RFS APXVAARR24_43-U-NA20	177

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

Cable losses were factored in the calculations for this site. Since all **1900 MHz (PCS)** radios are ground mounted the following cable loss values were used. For each ground mounted **1900 MHz (PCS)** radio there was **1.82 dB** of cable loss calculated into the system gains / losses for this site. These values were calculated based upon the manufacturers specifications for **215 feet** of **1-5/8**" coax.

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## RESULTS

Per the calculations completed for the proposed T-MOBILE configurations *Table 3* shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

					Total TX					
Antenna			Antenna Gain	Channel	Power					
ID	Antenna Make / Model	Frequency Bands	(dBd)	Count	(W)	ERP (W)	MPE %			
Antenna	RFS									
A1	APXV18-209015-C-A20	1900 MHz (PCS)	15.55	5	175	4,130.84	0.50			
Antenna	RFS									
A2	APXVAARR24_43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	4	120	2,443.03	0.72			
Sector A Composite MPE%										
Antenna	RFS									
B1	APXV18-209015-C-A20	1900 MHz (PCS)	15.55	5	175	4,130.84	0.50			
Antenna	RFS									
B2	APXVAARR24_43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	4	120	2,443.03	0.72			
				Se	ector B Comp	osite MPE%	1.22			
Antenna	RFS									
C1	APXV18-209015-C-A20	1900 MHz (PCS)	15.55	5	175	4,130.84	0.50			
Antenna	RFS									
C2	APXVAARR24_43-U-NA20	600 MHz / 700 MHz	12.95 / 13.35	4	120	2,443.03	0.72			
				Se	ector C Comp	osite MPE%	1.22			

Table 3: T-MOBILE Emissions Levels

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The Following table (*table 4*) shows all additional carriers on site and their MPE% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum T-MOBILE MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. *Table 5* below shows a summary for each T-MOBILE Sector as well as the composite MPE value for the site.

Site Composite MPE%					
Carrier	MPE%				
T-MOBILE – Max Per Sector Value	1.22 %				
Tilcon Tomasso	0.12 %				
Arch Cmens	0.09 %				
SkyTel	0.08 %				
Arch Cmcns	0.16 %				
US Drug	0.08 %				
Internal Revenue	0.08 %				
Connecticut Radio	0.12 %				
Federal Express	0.08 %				
Northeast Paging	0.45 %				
Stamm Const.	0.15 %				
Unknown	2.16 %				
Sprint	2.05 %				
Site Total MPE %:	6.84 %				

Table 4: All Carrier MPE Contributions

T-MOBILE Sector A Total:	1.22 %		
T-MOBILE Sector B Total:	1.22 %		
T-MOBILE Sector C Total:	1.22 %		
Site Total:	6.84 %		

Table 5: Site MPE Summary

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FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. *Table 6* below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated T-MOBILE sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

T-MOBILE _ Frequency Band / Technology Max Power Values (Per Sector)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm <sup>2</sup> )	Frequency (MHz)	Allowable MPE (µW/cm <sup>2</sup> )	Calculated % MPE
T-Mobile 1900 MHz (PCS) LTE	4	944.19	177	4.64	1900 MHz (PCS)	1000	0.46%
T-Mobile 1900 MHz (PCS) GSM	1	354.07	177	0.44	1900 MHz (PCS)	1000	0.04%
T-Mobile 600 MHz LTE / 5G NR	2	788.97	177	1.94	600 MHz	400	0.49%
T-Mobile 700 MHz LTE	2	432.54	177	1.06	700 MHz	467	0.23%
						Total:	1.22%

Table 6: T-MOBILE Maximum Sector MPE Power Values

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### Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-MOBILE facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-MOBILE Sector	Power Density Value (%)
Sector A:	1.22 %
Sector B:	1.22 %
Sector C:	1.22 %
T-MOBILE Maximum Total (per sector):	1.22 %
Site Total:	6.84 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **6.84** % of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

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