

**JULIE D. KOHLER**

PLEASE REPLY TO: Bridgeport  
WRITER'S DIRECT DIAL: (203) 337-4157  
E-Mail Address: jkohler@cohenandwolf.com

June 13, 2014

Attorney Melanie Bachman  
Acting Executive Director  
Connecticut Siting Council  
Ten Franklin Square  
New Britain, CT 06051

**Re: Notice of Exempt Modification  
InSite Wireless Group, LLC/ MetroPCS co-location  
Site ID CTHA536A  
577 Bell Street, Glastonbury, Connecticut**

Dear Attorney Bachman:

This office represents MetroPCS Wireless Inc. ("MetroPCS") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, InSite Wireless Group, LLC owns the existing self-supported lattice tower and related facility located at 577 Bell Street, Glastonbury, Connecticut (Latitude: 41.7336 Longitude: -72.5496). MetroPCS intends to replace three antennas with six new antennas and related equipment at this existing telecommunications facility in Glastonbury ("Glastonbury Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the Town Manager, Richard J. Johnson, and the property owner, Cox Connecticut Telcom LLC.

The existing Glastonbury Facility consists of a 92 foot tall self-supported lattice tower.<sup>1</sup> MetroPCS plans to replace three antennas on single standoff arms with six antennas mounted on dual standoff arms at a centerline of 65 feet. (See the plans revised to May 1, 2014 attached hereto as Exhibit A). MetroPCS will also replace an equipment cabinet and battery backup unit on a new concrete pad, and install fiber cable. The existing Glastonbury Facility is structurally capable of supporting MetroPCS' proposed modifications, as indicated in the structural analysis dated May 29, 2014 and attached hereto as Exhibit B.

The planned modifications to the Glastonbury Facility fall squarely within those activities

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<sup>1</sup> The Glastonbury Facility was first approved by the Council in Docket No. 16. Petition No. 990 was subsequently approved to increase the height of the facility to 104 feet. The Decision and Order in this docket (dated January 11, 1980) and Petition approval (dated June 23, 2011) contain no relevant requirements or limitations on the configuration of the Glastonbury Facility.

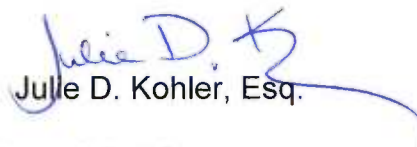
June 13, 2014  
Site ID CTHA536A  
Page 2

explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modification will not increase the height of the tower. MetroPCS' replacement antennas will be installed at a centerline of 65 feet, merely replacing existing antennas located at the same 65 foot elevation. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.
2. The proposed modifications will not require an extension of the site boundaries. MetroPCS' equipment will be located entirely within the existing compound and equipment pad as shown on pages 2 and 3 of Exhibit A.
3. The proposed modification to the Glastonbury Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the replacement antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated June 9, 2014, MetroPCS' operations would add 2.995% of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be 78.595% of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, MetroPCS respectfully submits that the proposed replacement antennas and equipment at the Glastonbury Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, MetroPCS shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,

  
Julie D. Kohler, Esq.

cc: Town of Glastonbury, Town Manager Richard J. Johnson  
InSite Wireless Group, LLC  
Cox Connecticut Telcom LLC  
Northeast Site Solutions, Sheldon J. Freinckle

# **EXHIBIT A**



**KEY PLAN**

N.T.S.

CONFIGURATION

**5A**

SUBMITTALS	
LE REV A	05.01.14

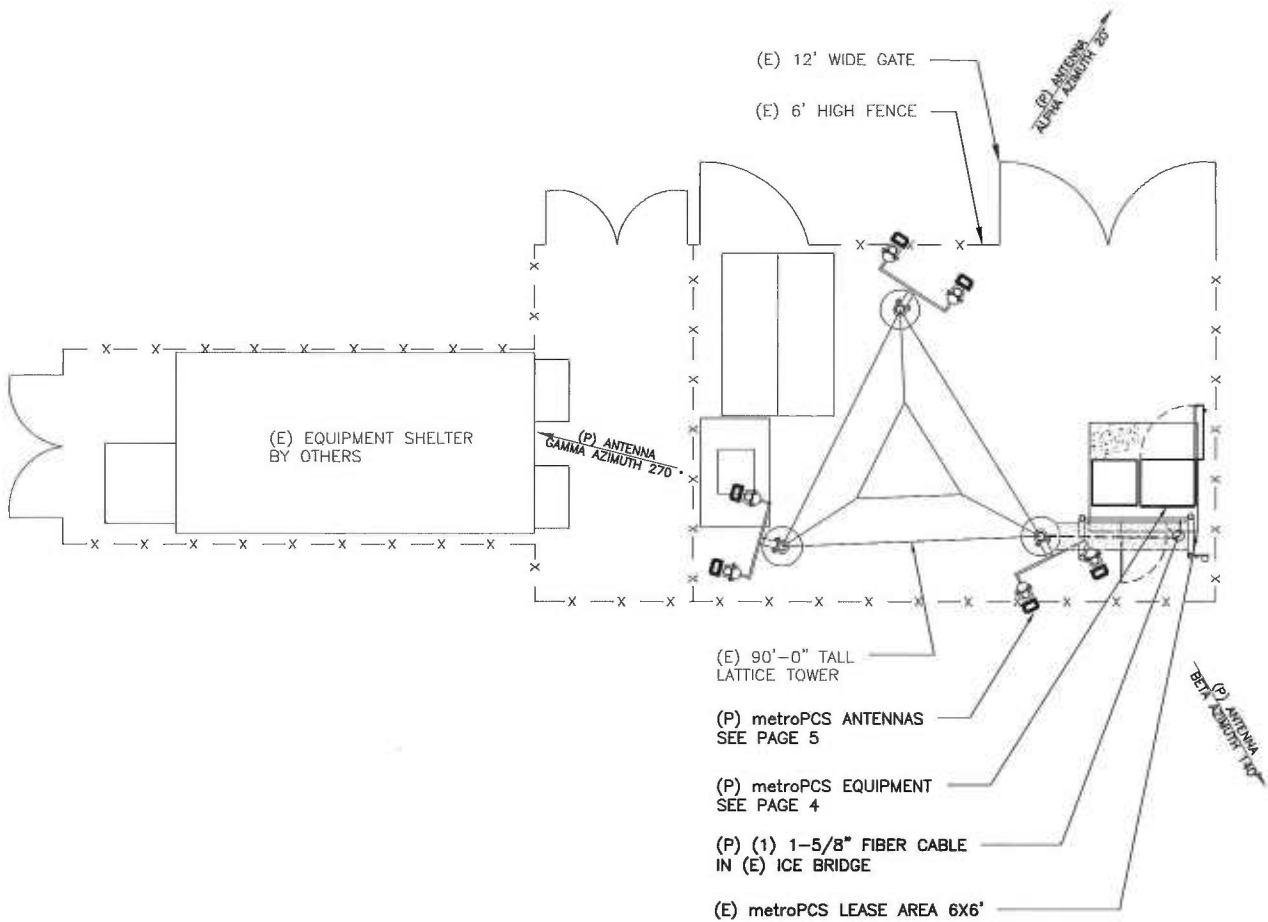
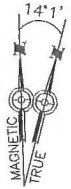
**ATLANTIS GROUP**  
 1340 Centre Street  
 Suite 212  
 Newton, MA 02459  
 Office: 617-965-0789  
 Fax: 617-213-5056

**LEASE EXHIBIT**  
 SITE NUMBER:  
 CTHA536A  
 SITE NAME:  
 INSITE GLASTONBURY LATTICE  
 SITE ADDRESS:  
 577 BELL STREET  
 GLASTONBURY, CT 06033

NORTHEAST SITE SOLUTIONS  
 54 MAIN STREET, UNIT 3  
 STURBRIDGE, MA 01566  
 (508) 434-5237  
 FOR  
**metroPCS.**  
 metroPCS WIRELESS, INC.  
 35 GRIFFIN ROAD SOUTH  
 BLOOMFIELD, CT 06002

DRAWN BY: EB

CHECKED BY: SM



ALL EQUIPMENT LOCATIONS ARE APPROXIMATE AND ARE SUBJECT TO APPROVAL BY LESSEE/LICENSEE'S STRUCTURAL & RF ENGINEERS. LOCATIONS OF POWER & TELEPHONE FACILITIES ARE SUBJECT TO APPROVAL BY UTILITY COMPANIES.

**SITE PLAN**

SCALE: N.T.S.



CONFIGURATION

**5A**

SUBMITTALS	
LE REV A	05.01.14

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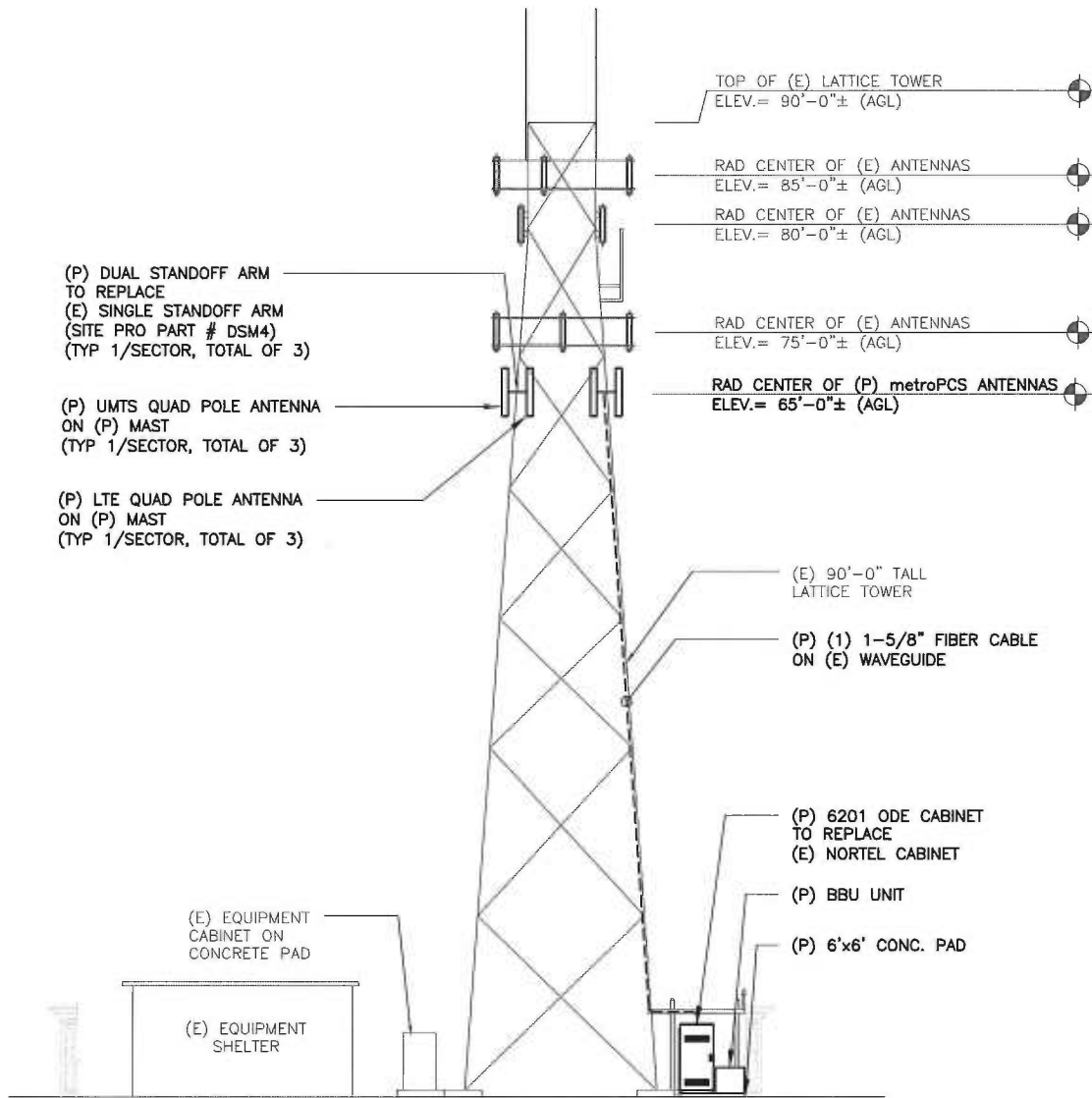
NORTHEAST SITE SOLUTIONS  
 54 MAIN STREET, UNIT 3  
 STURBRIDGE, MA 01566  
 (508) 434-5237

FOR  
**metroPCS.**  
 metroPCS WIRELESS, INC.  
 35 GRIFFIN ROAD SOUTH  
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DRAWN BY: EB

CHECKED BY: SM

PAGE 2 OF 5



ELEVATION  
N.T.S.

1  
LE-3

CONFIGURATION

5A

SUBMITTALS

LE REV A	05.01.14

**ATLANTIS GROUP**  
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Fax: 617-213-5056

**LEASE EXHIBIT**

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SITE NAME:  
INSITE GLASTONBURY LATTICE  
SITE ADDRESS:  
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GLASTONBURY, CT 06033

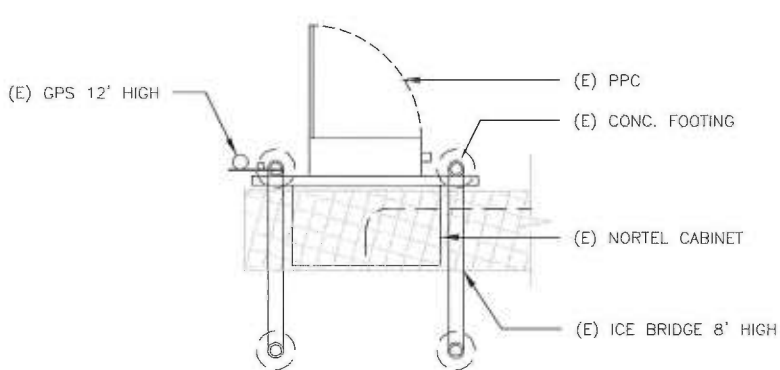
NORTHEAST SITE SOLUTIONS  
54 MAIN STREET, UNIT 8  
STURBRIDGE, MA 01566  
(508) 434-5237

FOR  
**metroPCS.**  
metroPCS WIRELESS, INC.  
35 GRIFFIN ROAD SOUTH  
BLOOMFIELD, CT 06002

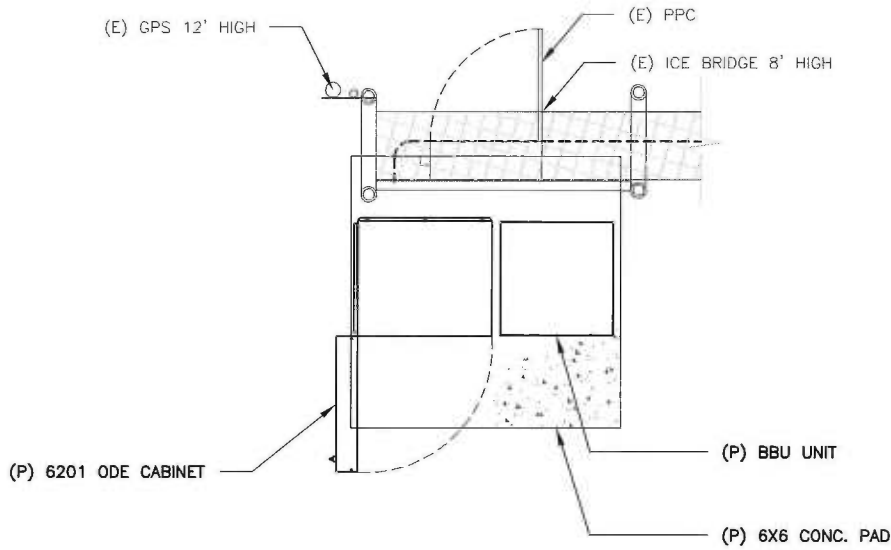
DRAWN BY: EB

CHECKED BY: SM

PAGE 3 OF 5



EXISTING EQUIPMENT



PROPOSED EQUIPMENT

CONFIGURATION

**5A**

SUBMITTALS	
LE REV A	05.01.14

**ATLANTIS GROUP**  
 1340 Centre Street  
 Suite 212  
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 SITE NAME:  
 INSITE GLASTONBURY LATTICE  
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 GLASTONBURY, CT 06033

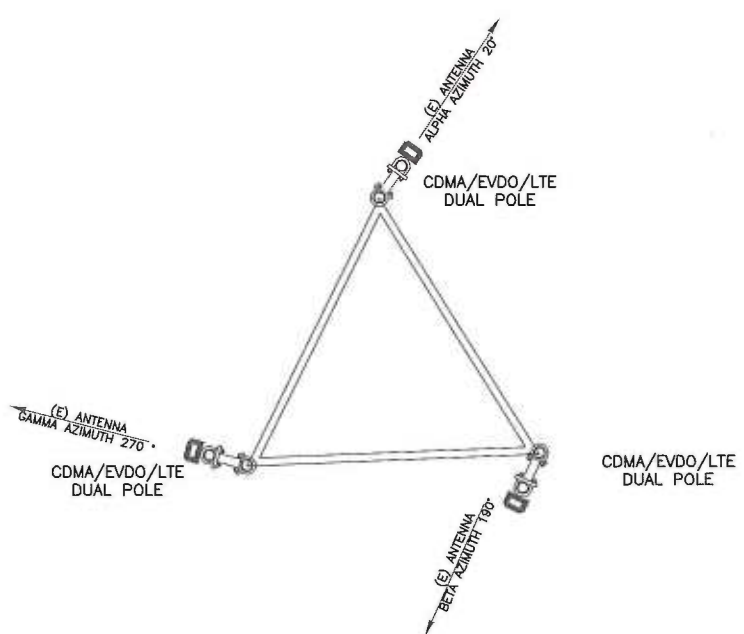
NORTHEAST SITE SOLUTIONS  
 54 MAIN STREET, UNIT 3  
 STURBRIDGE, MA 01566  
 (508) 434-5237

FOR  
**metroPCS.**  
 metroPCS WIRELESS, INC.  
 35 GRIFFIN ROAD SOUTH  
 BLOOMFIELD, CT 06002

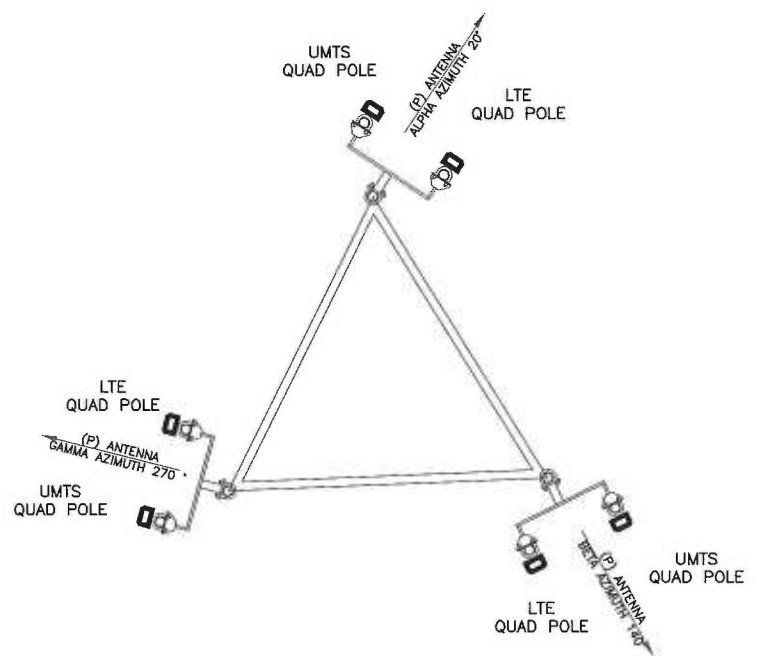
DRAWN BY: EB

CHECKED BY: SM

PAGE 4 OF 5



EXISTING ANTENNA CONFIGURATION



PROPOSED ANTENNA CONFIGURATION

CONFIGURATION  
**5A**

SUBMITTALS	
LE REV A	05.01.14

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FOR  
**metroPCS.**  
metroPCS WIRELESS, INC.  
35 GRIFFIN ROAD SOUTH  
BLOOMFIELD, CT 06002



# **EXHIBIT B**

May 29, 2014

Ms. Tracy Lee  
 Insite Towers, LLC  
 1199 N. Fairfax St., Ste. 700  
 Alexandria, VA 22314

**Re: Tower Structural Analysis- Metro PCS Antenna Installation**

<b>Site Number:</b>	CT901	<b>Site Address:</b>	577 Bell Street Glastonbury, CT
<b>Site Name:</b>	Glastonbury		
<b>Tower Owner:</b>	N/A	<b>Lat/Long:</b>	41.7338/-72.5497
<b>Tower Type:</b>	92-ft Self-Support Tower	<b>B&amp;P Job No:</b>	14060.001
<b>Tower Status:</b>	Passed (99% Capacity)	<b>Foundation Status:</b>	Passed

We have completed our structural analysis of the proposed equipment installation on the foregoing tower to determine its ability to support the new loads proposed by Metro PCS.

The following information was provided for our tower structural analysis:

- Tower: Member sizes and configuration were obtained from the previous structural analysis by the URS Corporation dated 9/7/2010.
- Foundation: Foundation details were obtained from the previous structural analysis listed above.
- Geotechnical: A geotechnical report was not available for this site.
- Antennas: Proposed antenna loading was obtained from the tenant application provided by Insite Towers, LLC dated 4/30/2014. Existing antenna loading was obtained from the structural analysis listed above.
- Other: General photographs of the tower

Table 1 summarizes the antenna, attachment, and transmission line loading proposed and Table 2 summarizes the design criteria used for our structural analysis. Attached is a copy of the structural calculations, which in addition to detailed results of the analysis also includes a tower profile with member sizes and configuration, and the existing/proposed equipment list with types and location.

**Table 1 – Proposed Equipment Loading**

Status	Antennas/Attachments					Transmission Lines <sup>1</sup>	
	Carrier	Rad Center	Qty	Manufacturer	Model	# of Feed lines	Feed line Size (in)
New Antenna	Metro PCS	65'	6	Ericsson	AIR 21	1	1 5/8"

<sup>1</sup>Note: See attachment for transmission line layout

**Table 2 – Design Criteria Used for Structural Analysis**

Criterion	Information Used
State Building Code	Connecticut (IBC 2003)
Tower Standard	EIA/TIA-222-F
County	Montgomery
Basic Wind Speed	80 mph, no ice 69 mph, 1/2" ice
Steel Grade Assumed	50 ksi SR legs, 36 ksi all others, A325 bolts
Tower Analysis Software	tnxTower (version 6.1.3)

Based on the foregoing information, and provided all dead appurtenances and feed lines be removed from the tower, our structural analysis determined that **the existing tower is structurally capable of supporting the proposed equipment loads without modification.** The foundation modifications are assumed to have been completed, and if so the modified foundation is capable of supporting the current and proposed tower loading.

The following assumptions were made in conducting our structural analysis:

1. The existing tower has been maintained to manufacturer's specifications and is in good condition.
2. All member connections are assumed to have been designed to meet the load carrying capacity of the connected member.
3. Antenna mount loads have been estimated based on typical industry standards.
4. The new feed lines for the proposed Metro PCS antennas are assumed to be mounted across one tower face opposite of the existing feed lines.
5. The mounts for the proposed antennas have been analyzed and designed by others.
6. **Existing antennas (2 Omni and 1 dipole) and feed lines at 112' have been removed prior to the Metro PCS Installation.**
7. See additional assumptions contained in the report attached.

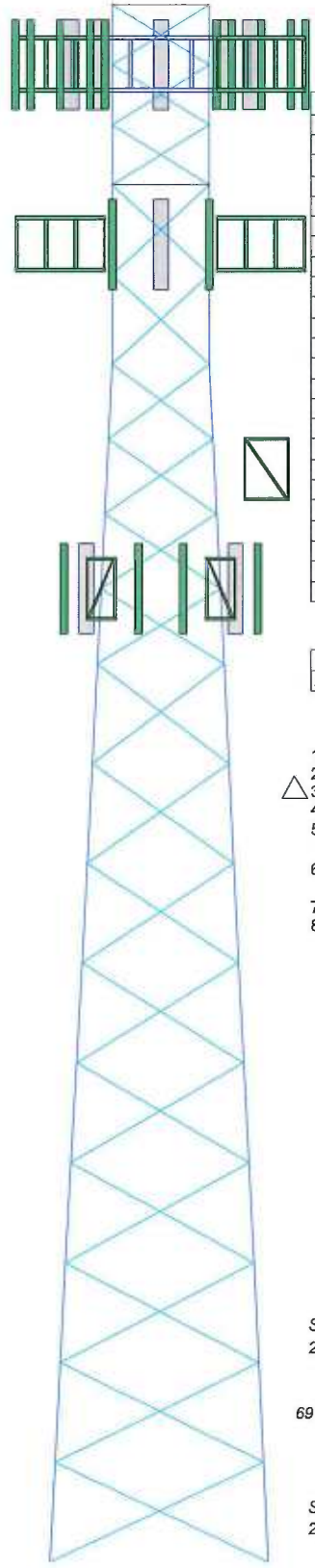
Bennett & Pless, Inc. makes no warranties, expressed or implied, in connection with this report, and disclaims any liability arising from material, fabrication and erection of this tower. Bennett & Pless, Inc. will not be responsible whatsoever for or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Bennett & Pless, Inc. pursuant to this report will be limited to the total fee received for preparation of this report.

We appreciate the opportunity of providing our continuing professional services to you. If you have any questions or need further assistance on this please call us anytime.

Yours very truly,  
**Bennett & Pless, Inc.**

Mike De Boer, P.E.  
Director of Telecom

Section	T1	T2	T3	T4	T5	T6
Legs	P2x-154	P2.5x-203	Pipe 2.875 x 0.276 w/ 3/8 Plate	Pipe 2.875 x 0.276 w/ 3/8 Plate	Pipe 2.875 x 0.276 w/ 3/8 Plate	Pipe 3 x 0.3 w/ 3/8 Plate
Leg Grade	L1 1/2x1 1/2x3/16	L1 1/2x1 1/2x1/4	A618-50	A618-50	A618-50	A618-50
Diagonals	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16
Diagonal Grade	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16
Top Girts	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16	L2x2x3/16
Face Width (ft)	6.52	6.56	8.56	10.56	12.6	14.85
# Panels @ (ft)	3 @ 4	2 @ 6	4 @ 5	9 @ 6.6667	0.8	3.2
Weight (K)	0.3	0.3	0.5	0.7	0.8	3.2



**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
12' T-Frame Sector Mount (Verizon)	100	KMW AX-X-CD-1665-OOT (ATI)	88
12' T-Frame Sector Mount (Verizon)	100	KMW AX-X-CD-1665-OOT (ATI)	88
12' T-Frame Sector Mount (Verizon)	100	Andrew SBNH-1D6565C (ATI)	88
BXA-70063/8CF (Verizon)	100	Andrew SBNH-1D6565C (ATI)	88
BXA-70063/8CF (Verizon)	100	Andrew SBNH-1D6565C (ATI)	88
BXA-70063/8CF (Verizon)	100	(2) TMA (ATI)	88
LPA-80063/8CF (Verizon)	100	(2) TMA (ATI)	88
LPA-80063/8CF (Verizon)	100	(2) TMA (ATI)	88
LPA-80063/8CF (Verizon)	100	(2) RRU-11 (ATI)	88
LPA-80063/8CF (Verizon)	100	(2) RRU-11 (ATI)	88
LPA-80063/8CF (Verizon)	100	(2) RRU-11 (ATI)	88
LPA-80063/8CF (Verizon)	100	Demarcation Box DC6-4880-188F (ATI)	88
LPA-185063/16CF (Verizon)	100	DB806-XT (Town of Glastonbury)	79
LPA-185063/12CH-2 (Verizon)	100	PR-950 (Town of Glastonbury)	73
LPA-185063/12CH-2 (Verizon)	100	PIROD 6' Side Mount Standoff (Town of Glastonbury)	73
LPA-185063/16CF (Verizon)	100	PIROD 6' Side Mount Standoff (Town of Glastonbury)	73
LPA-185063/12CH-2 (Verizon)	100	3' Stand-Off (Metro PCS)	65
LPA-185063/12CH-2 (Verizon)	100	3' Stand-Off (Metro PCS)	65
12' T-Frame Sector Mount (ATI)	88	3' Stand-Off (Metro PCS)	65
12' T-Frame Sector Mount (ATI)	88	(2) AIR 21 (Metro PCS)	65
Powerwave P65-17-XLH-RR (ATI)	88	(2) AIR 21 (Metro PCS)	65
Powerwave P65-17-XLH-RR (ATI)	88	(2) AIR 21 (Metro PCS)	65
Powerwave P65-17-XLH-RR (ATI)	88	3' Stand-Off (Metro PCS)	65
Powerwave P65-17-XLH-RR (ATI)	88		
KMW AX-X-CD-1665-OOT (ATI)	88		

**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A618-50	50 ksi	70 ksi	A36	36 ksi	58 ksi

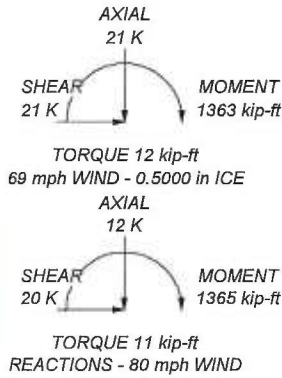
**TOWER DESIGN NOTES**

1. Tower designed for a 80 mph basic wind in accordance with the TIA/EIA-222-F Standard.
2. Tower is also designed for a 69 mph basic wind with 0.50 in ice.
3. Deflections are based upon a 60 mph wind.
4. Weld together tower sections have flange connections.
5. Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications.
6. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
7. Welds are fabricated with ER-70S-6 electrodes.
8. TOWER RATING: 98.8%

**MAX. CORNER REACTIONS AT BASE:**

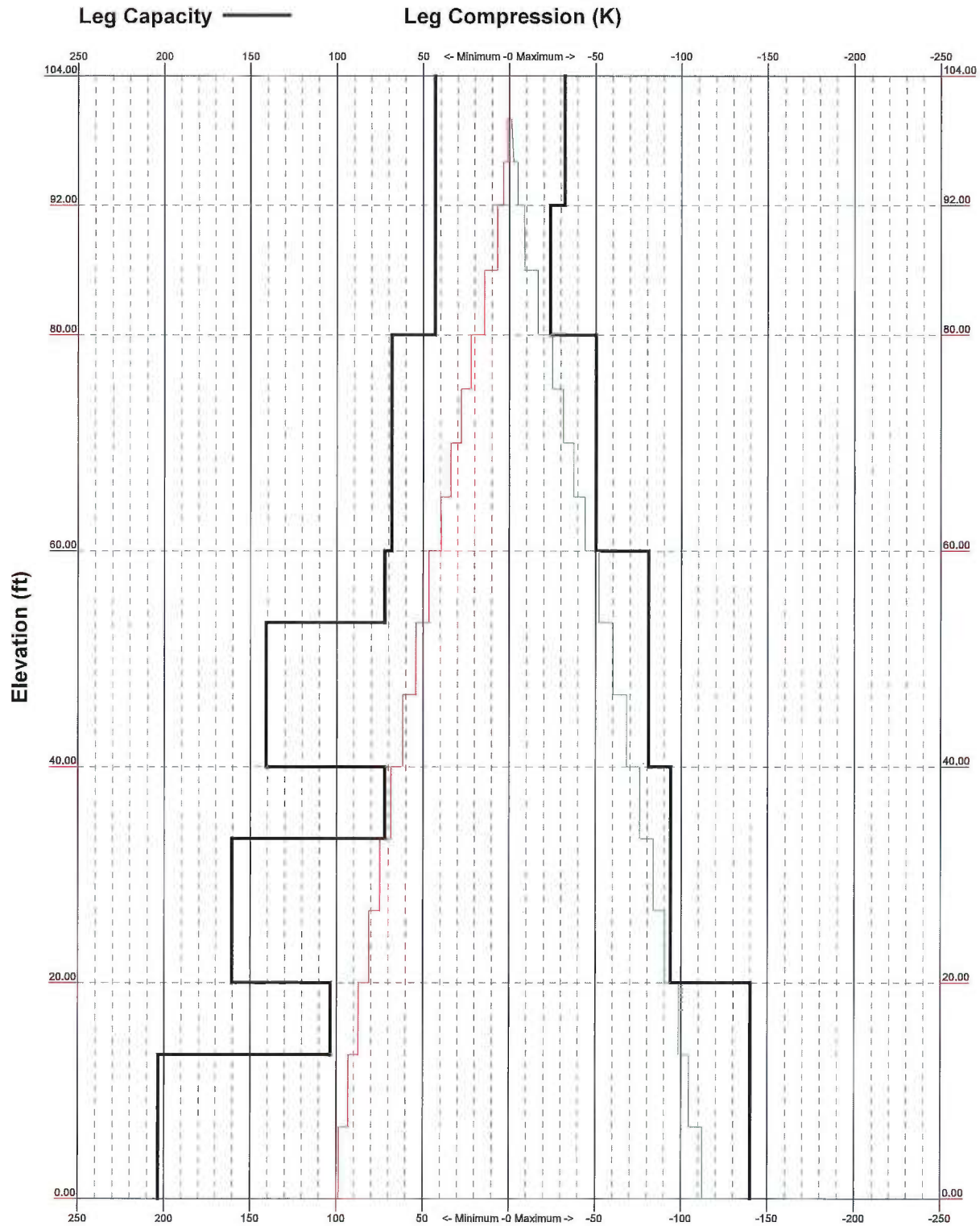
DOWN: 114 K  
SHEAR: 12 K

UPLIFT: -101 K  
SHEAR: 11 K



Job:	<b>CT901 Glastonbury</b>		
Project:	<b>SST Analysis</b>		
Client:	Insite Towers, LLC	Drawn by:	LETS America, Inc.
Code:	TIA/EIA-222-F	Date:	06/03/14
Path:	Y:\2014\14013.xxx - InSite Wireless\14013.002 - CT901 Glastonbury\Design\CT901 Glastonbury.dwg		
Phone:		Scale:	NTS
FAX:		Dwg No.:	E-1

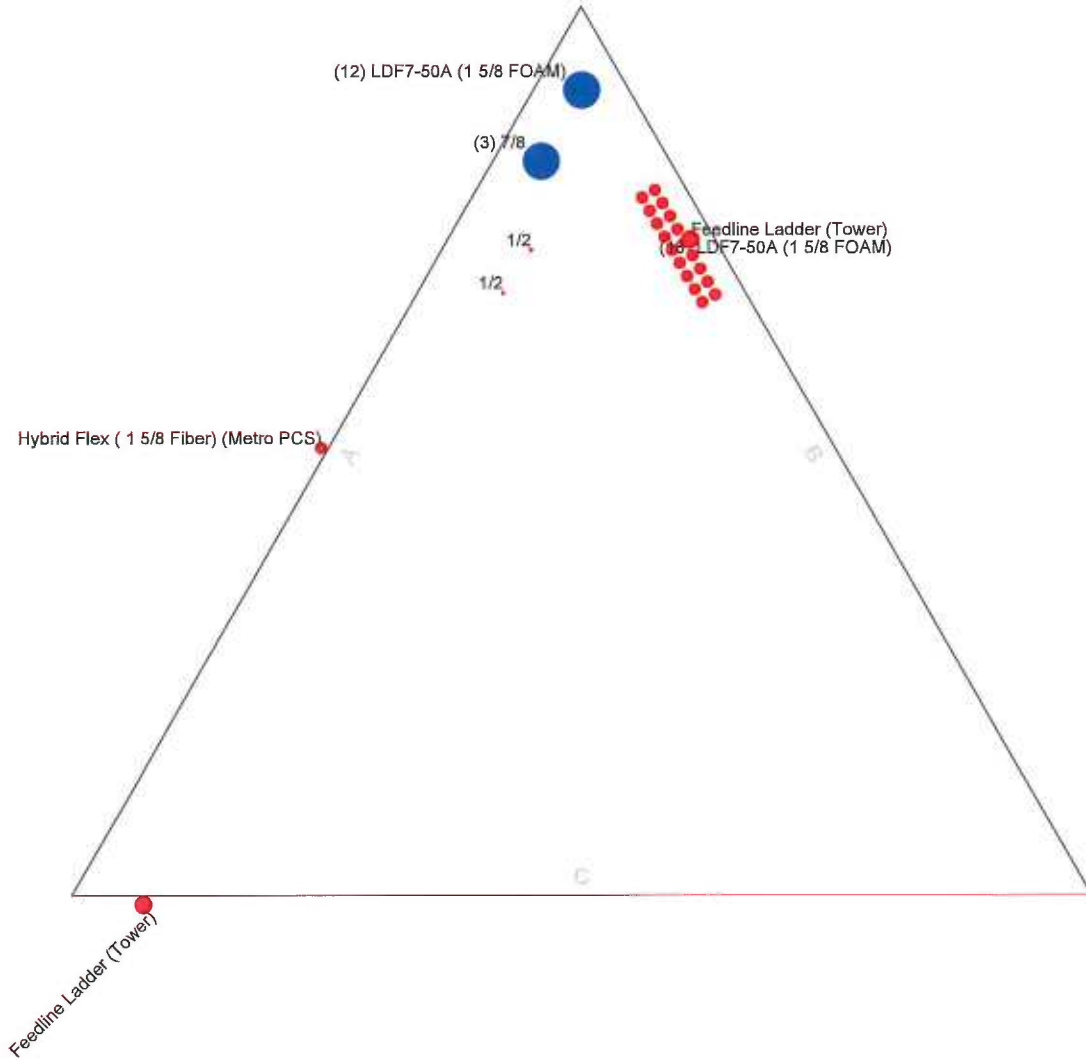
TIA/EIA-222-F - 80 mph/69 mph 0.5000 in Ice



Job: <b>CT901 Glastonbury</b>			
Project: <b>SST Analysis</b>			
Client: <b>Insite Towers, LLC</b>	Drawn by: <b>LETS America, Inc.</b>	App'd:	
Code: <b>TIA/EIA-222-F</b>	Date: <b>06/03/14</b>	Scale: <b>NTS</b>	
Phone:	Path:	Dwg No. <b>E-3</b>	
FAX:	<small>Y:\2014\14013.xxx - InSite Wireless\14013.002 - CT901 Glastonbury\Design\CT901 Glastonbury.dwg</small>		

# Feed Line Plan

Round    
  Flat    
  App In Face    
  App Out Face



	Job: <b>CT901 Glastonbury</b>		
	Project: <b>SST Analysis</b>		
	Client: <b>Insite Towers, LLC</b>	Drawn by: <b>LETS America, Inc.</b>	App'd:
Phone:	Code: <b>TIA/EIA-222-F</b>	Date: <b>06/03/14</b>	Scale: <b>NTS</b>
FAX:	Path: <small>Y:\32014\414013\www - InSite Wireless\14013_002 - CT901 Glastonbury\Design\CT901 Glastonbury.dwg</small>		
			Dwg No. <b>E-7</b>

<b><i>tnxTower</i></b>  Phone: FAX:	<b>Job</b> CT901 Glastonbury	<b>Page</b> 1 of 24
	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

## Tower Input Data

The main tower is a 3x free standing tower with an overall height of 104.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 6.52 ft at the top and 14.65 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Basic wind speed of 80 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 69 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Weld together tower sections have flange connections..

Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications..

Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..

Welds are fabricated with ER-70S-6 electrodes..

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

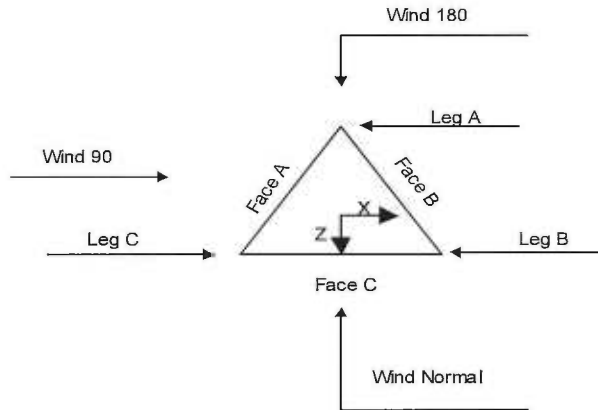
Stress ratio used in tower member design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

<ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>√ Include Bolts In Member Capacity</li> <li>√ Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>Add IBC .6D+W Combination</li> </ul>	<ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>SR Members Have Cut Ends</li> <li>√ Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Use TIA-222-G Tension Splice Capacity Exemption</li> </ul>	<ul style="list-style-type: none"> <li>Treat Feedline Bundles As Cylinder</li> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>√ Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>√ All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feedline Torque</li> <li>Include Angle Block Shear Check</li> <li style="text-align: center;">Poles</li> <li>Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul>
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<b>tnxTower</b>  Phone: FAX:	<b>Job</b> CT901 Glastonbury	<b>Page</b> 2 of 24
	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.



Triangular Tower

### Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	ft			ft		ft
T1	104.00-92.00			6.52	1	12.00
T2	92.00-80.00			6.52	1	12.00
T3	80.00-60.00			6.56	1	20.00
T4	60.00-40.00			8.56	1	20.00
T5	40.00-20.00			10.56	1	20.00
T6	20.00-0.00			12.60	1	20.00

### Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	104.00-92.00	4.00	X Brace	No	No	0.0000	0.0000
T2	92.00-80.00	6.00	X Brace	No	No	0.0000	0.0000
T3	80.00-60.00	5.00	X Brace	No	No	0.0000	0.0000
T4	60.00-40.00	6.67	X Brace	No	No	0.0000	0.0000
T5	40.00-20.00	6.67	X Brace	No	No	0.0000	0.0000
T6	20.00-0.00	6.67	X Brace	No	No	0.0000	0.0000



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### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 104.00-92.00	Pipe	P2x.154	A618-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x3/16	A36 (36 ksi)
T2 92.00-80.00	Pipe	P2x.154	A618-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/4	A36 (36 ksi)
T3 80.00-60.00	Pipe	P2.5x.203	A618-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/4	A36 (36 ksi)
T4 60.00-40.00	Arbitrary Shape	Pipe 2.875 x .203 w/ 3/8 Plate	A618-50 (50 ksi)	Single Angle	L2x2x3/16	A36 (36 ksi)
T5 40.00-20.00	Arbitrary Shape	Pipe 2.875 x 0.276 w/ 3/8 Plate	A618-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 20.00-0.00	Arbitrary Shape	Pipe 3 x 0.3 w/ 3/8 Plate	A618-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 104.00-92.00	Single Angle	L2x2x3/16	A36 (36 ksi)	Solid Round		A36 (36 ksi)
T2 92.00-80.00	Single Angle	L2x2x3/16	A36 (36 ksi)	Solid Round		A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
T1 104.00-92.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000
T2 92.00-80.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000
T3 80.00-60.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000
T4 60.00-40.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000
T5 40.00-20.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000
T6 20.00-0.00	0.00	0.2500	A36 (36 ksi)	1.02	1	1	36.0000	36.0000

### Tower Section Geometry (cont'd)

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Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors <sup>1</sup>							
				X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
				X Y	X Y	X Y	X Y	X Y	X Y	X Y	
T1 104.00-92.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T2 92.00-80.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T3 80.00-60.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T4 60.00-40.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T5 40.00-20.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T6 20.00-0.00	Yes	Yes	1	1	1	1	1	1	1	1	1

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U	Net Width Deduct in	U
T1 104.00-92.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T2 92.00-80.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T3 80.00-60.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T4 60.00-40.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 40.00-20.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 20.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T1 104.00-92.00	Flange	0.6250	4	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T2 92.00-80.00	Flange	0.6250	4	0.5000	1	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T3 80.00-60.00	Flange	0.6250	4	0.5000	1	0.0000	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T4 60.00-40.00	Flange	0.6250	4	0.5000	1	0.0000	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
T5 40.00-20.00	Flange	0.6250	4	0.5000	1	0.0000	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0

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Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.
T6 20.00-0.00	Flange	0.7500 A325N	4	0.5000 A325N	1	0.0000 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0	0.6250 A325N	0

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1/2	A	Yes	Ar (CfAe)	73.00 - 6.00	-12.5000	0.27	1	1	0.5000	0.5800		0.25
1/2	A	Yes	Ar (CfAe)	73.00 - 6.00	-12.0000	0.22	1	1	0.5000	0.5800		0.25
Feedline Ladder (Tower)	C	Yes	Ar (CfAe)	65.00 - 6.00	0.0000	0.43	1	1	0.5000	3.0000		8.40
LDF7-50A (1 5/8 FOAM)	B	Yes	Ar (CfAe)	100.00 - 6.00	-6.0000	-0.25	18	9	0.5000	1.9800		0.82
Feedline Ladder (Tower)	B	Yes	Ar (CfAe)	100.00 - 6.00	-2.0000	-0.25	1	1	0.5000	3.0000		8.40
Hybrid Flex (1 5/8 Fiber) (Metro PCS)	A	Yes	Ar (CfAe)	65.00 - 6.00	0.0000	0	1	1	1.9800	1.9800		0.82

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight plf
7/8	A	No	CaAa (In Face)	102.00 - 6.00	-4.0000	0.35	3	No Ice 1/2" Ice	0.00 0.00
LDF7-50A (1 5/8 FOAM)	A	No	CaAa (In Face)	92.00 - 6.00	-4.0000	0.43	12	No Ice 1/2" Ice	0.16 0.26

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
T1	104.00-92.00	A	0.000	0.000	0.000	0.000	0.02
		B	13.880	0.000	0.000	0.000	0.19
		C	0.000	0.000	0.000	0.000	0.00
T2	92.00-80.00	A	0.000	0.000	23.401	0.000	0.14
		B	20.820	0.000	0.000	0.000	0.28
		C	0.000	0.000	0.000	0.000	0.00
T3	80.00-60.00	A	2.082	0.000	39.001	0.000	0.24
		B	34.700	0.000	0.000	0.000	0.46
		C	1.250	0.000	0.000	0.000	0.04
T4	60.00-40.00	A	5.233	0.000	39.001	0.000	0.26

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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T5	40.00-20.00	B	34.700	0.000	0.000	0.000	0.46
		C	5.000	0.000	0.000	0.000	0.17
		A	5.233	0.000	39.001	0.000	0.26
T6	20.00-0.00	B	34.700	0.000	0.000	0.000	0.46
		C	5.000	0.000	0.000	0.000	0.17
		A	3.663	0.000	27.301	0.000	0.18
		B	24.290	0.000	0.000	0.000	0.32
		C	3.500	0.000	0.000	0.000	0.12

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T1	104.00-92.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		4.653	13.227	0.000	0.000	0.41
		C		0.000	0.000	0.000	0.000	0.00
T2	92.00-80.00	A	0.500	0.000	0.000	37.800	0.000	0.29
		B		6.980	19.840	0.000	0.000	0.62
		C		0.000	0.000	0.000	0.000	0.00
T3	80.00-60.00	A	0.500	4.665	0.000	63.000	0.000	0.53
		B		11.633	33.067	0.000	0.000	1.03
		C		1.667	0.000	0.000	0.000	0.05
T4	60.00-40.00	A	0.500	10.233	0.000	63.000	0.000	0.57
		B		11.633	33.067	0.000	0.000	1.03
		C		6.667	0.000	0.000	0.000	0.21
T5	40.00-20.00	A	0.500	10.233	0.000	63.000	0.000	0.57
		B		11.633	33.067	0.000	0.000	1.03
		C		6.667	0.000	0.000	0.000	0.21
T6	20.00-0.00	A	0.500	7.163	0.000	44.100	0.000	0.40
		B		8.143	23.147	0.000	0.000	0.72
		C		4.667	0.000	0.000	0.000	0.15

### Feed Line Shielding

Section	Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_R$ Ice ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$A_F$ Ice ft <sup>2</sup>
T1	104.00-92.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.998	1.211	1.559
		C	0.000	0.000	0.000	0.000
T2	92.00-80.00	A	0.000	0.000	0.000	0.000
		B	0.000	1.197	1.466	1.889
		C	0.000	0.000	0.000	0.000
T3	80.00-60.00	A	0.000	0.187	0.125	0.280
		B	0.000	1.790	2.085	2.686
		C	0.000	0.067	0.075	0.100
T4	60.00-40.00	A	0.000	0.312	0.319	0.625
		B	0.000	1.364	2.118	2.728
		C	0.000	0.203	0.305	0.407
T5	40.00-20.00	A	0.000	0.295	0.378	0.739
		B	0.000	1.290	2.504	3.226
		C	0.000	0.192	0.361	0.481
T6	20.00-0.00	A	0.000	0.199	0.255	0.499

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Section	Elevation	Face	$A_R$	$A_R$	$A_F$	$A_F$
	ft		ft <sup>2</sup>	Ice ft <sup>2</sup>	ft <sup>2</sup>	Ice ft <sup>2</sup>
		B	0.000	0.871	1.691	2.178
		C	0.000	0.130	0.244	0.325

### Feed Line Center of Pressure

Section	Elevation	$CP_X$	$CP_Z$	$CP_X$	$CP_Z$
	ft	in	in	Ice in	Ice in
T1	104.00-92.00	1.3649	-6.8550	0.9992	-4.9724
T2	92.00-80.00	0.8057	-9.7336	0.6054	-8.9705
T3	80.00-60.00	0.6306	-11.0652	0.4123	-10.3434
T4	60.00-40.00	-0.1603	-14.8036	-0.3875	-13.9615
T5	40.00-20.00	-0.1822	-16.9491	-0.5032	-16.2286
T6	20.00-0.00	-0.1862	-17.4274	-0.5556	-16.8470

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	$C_{AA}$ Front ft <sup>2</sup>	$C_{AA}$ Side ft <sup>2</sup>	Weight K
12' T-Frame Sector Mount (Verizon)	A	From Leg	4.00	0.0000	100.00	No Ice	11.00	0.47
			0.00			1/2" Ice	11.30	0.60
			0.00					
12' T-Frame Sector Mount (Verizon)	B	From Leg	4.00	0.0000	100.00	No Ice	11.00	0.47
			0.00			1/2" Ice	11.30	0.60
			0.00					
12' T-Frame Sector Mount (Verizon)	C	From Leg	4.00	0.0000	100.00	No Ice	11.00	0.47
			0.00			1/2" Ice	11.30	0.60
			0.00					
BXA-70063/8CF (Verizon)	A	From Leg	4.00	0.0000	100.00	No Ice	7.40	0.02
			0.00			1/2" Ice	8.00	0.08
			0.00					
BXA-70063/6CF (Verizon)	B	From Leg	4.00	0.0000	100.00	No Ice	5.50	0.04
			0.00			1/2" Ice	6.50	0.09
			0.00					
BXA-70063/6CF (Verizon)	C	From Leg	4.00	0.0000	100.00	No Ice	5.50	0.04
			0.00			1/2" Ice	6.50	0.09
			0.00					
LPA-80063/8CF (Verizon)	A	From Leg	4.00	0.0000	100.00	No Ice	10.00	0.04
			-6.00			1/2" Ice	10.75	0.14
			0.00					
LPA-80063/6CF (Verizon)	B	From Leg	4.00	0.0000	100.00	No Ice	7.40	0.03
			-6.00			1/2" Ice	8.00	0.04
			0.00					
LPA-80063/6CF (Verizon)	C	From Leg	4.00	0.0000	100.00	No Ice	7.40	0.03
			-6.00			1/2" Ice	8.00	0.04
			0.00					
LPA-80063/8CF	A	From Leg	4.00	0.0000	100.00	No Ice	10.00	0.04

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
(Verizon)			6.00		1/2" Ice	10.75	9.50	0.14
LPA-80063/6CF (Verizon)	B	From Leg	4.00 6.00 0.00	0.0000	100.00 No Ice 1/2" Ice	7.40 8.00	6.50 7.00	0.03 0.04
LPA-80063/6CF (Verizon)	C	From Leg	4.00 6.00 0.00	0.0000	100.00 No Ice 1/2" Ice	7.40 8.00	6.50 7.00	0.03 0.04
LPA-185063/16CF (Verizon)	A	From Leg	4.00 -4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	2.59 3.20	4.53 5.10	0.02 0.03
LPA-185063/12CH-2 (Verizon)	B	From Leg	4.00 -4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	4.97 5.42	4.51 4.95	0.01 0.05
LPA-185063/12CH-2 (Verizon)	C	From Leg	4.00 -4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	4.97 5.42	4.51 4.95	0.01 0.05
LPA-185063/16CF (Verizon)	A	From Leg	4.00 4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	2.59 3.20	4.53 5.10	0.02 0.03
LPA-185063/12CH-2 (Verizon)	B	From Leg	4.00 4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	4.97 5.42	4.51 4.95	0.01 0.05
LPA-185063/12CH-2 (Verizon)	C	From Leg	4.00 4.00 0.00	0.0000	100.00 No Ice 1/2" Ice	4.97 5.42	4.51 4.95	0.01 0.05
12' T-Frame Sector Mount (AT&T)	B	From Leg	4.00 0.00 0.00	0.0000	88.00 No Ice 1/2" Ice	11.00 11.30	11.00 11.30	0.47 0.60
12' T-Frame Sector Mount (AT&T)	C	From Leg	4.00 0.00 0.00	0.0000	88.00 No Ice 1/2" Ice	11.00 11.30	11.00 11.30	0.47 0.60
DB806-XT (Town of Glastonbury)	B	From Leg	4.00 0.00 0.00	0.0000	79.00 No Ice 1/2" Ice	1.14 1.68	1.14 1.68	0.02 0.03
PR-950 (Town of Glastonbury)	B	From Leg	4.00 0.00 0.00	0.0000	73.00 No Ice 1/2" Ice	6.35 11.43	6.35 11.43	0.04 0.05
PiROD 6' Side Mount Standoff (Town of Glastonbury)	B	From Leg	4.00 0.00 0.00	0.0000	73.00 No Ice 1/2" Ice	4.97 6.12	4.97 6.12	0.07 0.13
(2) AIR 21 (Metro PCS)	A	From Leg	0.00 0.00 0.00	0.0000	65.00 No Ice 1/2" Ice	6.53 6.98	5.72 6.42	0.12 0.18
(2) AIR 21 (Metro PCS)	B	From Leg	0.00 0.00 0.00	0.0000	65.00 No Ice 1/2" Ice	6.53 6.98	5.72 6.42	0.12 0.18
(2) AIR 21 (Metro PCS)	C	From Leg	0.00 0.00 0.00	0.0000	65.00 No Ice 1/2" Ice	6.53 6.98	5.72 6.42	0.12 0.18
3' Stand-Off (Metro PCS)	A	From Leg	0.00 0.00 0.00	0.0000	65.00 No Ice 1/2" Ice	4.00 4.25	8.00 8.50	0.05 0.07
3' Stand-Off (Metro PCS)	B	From Leg	0.00 0.00 0.00	0.0000	65.00 No Ice 1/2" Ice	4.00 4.25	8.00 8.50	0.05 0.07
3' Stand-Off	C	From Leg	0.00	0.0000	65.00 No Ice	4.00	8.00	0.05

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	<b>Project</b>		SST Analysis					<b>Date</b>	
							12:06:49 06/03/14		
<b>Client</b>		Insite Towers, LLC					<b>Designed by</b>		
							LETS America, Inc.		

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight	
			Horz	Lateral						
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
(Metro PCS)			0.00			1/2" Ice	4.25	8.50	0.07	
			0.00							
Powerwave P65-17-XLH-RR (AT&T)	A	From Leg	0.00		0.0000	88.00	No Ice	11.70	8.94	0.09
			0.00			1/2" Ice	12.42	10.45	0.12	
			0.00							
Powerwave P65-17-XLH-RR (AT&T)	B	From Leg	0.00		0.0000	88.00	No Ice	11.70	8.94	0.09
			0.00			1/2" Ice	12.42	10.45	0.12	
			0.00							
Powerwave P65-17-XLH-RR (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	11.70	8.94	0.09
			0.00			1/2" Ice	12.42	10.45	0.12	
			0.00							
KMW AX-X-CD-1665-OOT (AT&T)	A	From Leg	0.00		0.0000	88.00	No Ice	8.50	6.30	0.07
			0.00			1/2" Ice	9.15	7.48	0.09	
			0.00							
KMW AX-X-CD-1665-OOT (AT&T)	B	From Leg	0.00		0.0000	88.00	No Ice	8.50	6.30	0.07
			0.00			1/2" Ice	9.15	7.48	0.09	
			0.00							
KMW AX-X-CD-1665-OOT (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	8.50	6.30	0.07
			0.00			1/2" Ice	9.15	7.48	0.09	
			0.00							
Andrew SBNH-1D6565C (AT&T)	A	From Leg	0.00		0.0000	88.00	No Ice	11.64	9.84	0.09
			0.00			1/2" Ice	12.37	11.37	0.18	
			0.00							
Andrew SBNH-1D6565C (AT&T)	B	From Leg	0.00		0.0000	88.00	No Ice	11.64	9.84	0.09
			0.00			1/2" Ice	12.37	11.37	0.18	
			0.00							
Andrew SBNH-1D6565C (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	11.64	9.84	0.09
			0.00			1/2" Ice	12.37	11.37	0.18	
			0.00							
(2) TMA (AT&T)	A	From Leg	0.00		0.0000	88.00	No Ice	1.69	0.85	0.02
			0.00			1/2" Ice	1.87	0.98	0.03	
			0.00							
(2) TMA (AT&T)	B	From Leg	0.00		0.0000	88.00	No Ice	1.69	0.85	0.02
			0.00			1/2" Ice	1.87	0.98	0.03	
			0.00							
(2) TMA (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	1.69	0.85	0.02
			0.00			1/2" Ice	1.87	0.98	0.03	
			0.00							
(2) RRU-11 (AT&T)	A	From Leg	0.00		0.0000	88.00	No Ice	4.42	1.19	0.06
			0.00			1/2" Ice	4.71	1.35	0.08	
			0.00							
(2) RRU-11 (AT&T)	B	From Leg	0.00		0.0000	88.00	No Ice	4.42	1.19	0.06
			0.00			1/2" Ice	4.71	1.35	0.08	
			0.00							
(2) RRU-11 (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	4.42	1.19	0.06
			0.00			1/2" Ice	4.71	1.35	0.08	
			0.00							
Demarcation Box DC6-4860-188F (AT&T)	C	From Leg	0.00		0.0000	88.00	No Ice	4.45	0.89	0.02
			0.00			1/2" Ice	4.76	1.04	0.05	
			0.00							

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	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

**Tower Pressures - No Ice**

$G_H = 1.159$

Section Elevation ft	z ft	$K_Z$	$q_z$ psf	$A_G$ ft <sup>2</sup>	F a c e	$A_F$ ft <sup>2</sup>	$A_R$ ft <sup>2</sup>	$A_{leg}$ ft <sup>2</sup>	Leg %	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>
T1 104.00-92.00	98.00	1.365	22	80.615	A	6.749	4.750	4.750	41.31	0.000	0.000
					B	5.538	18.630	19.65	0.000	0.000	
					C	6.749	4.750	41.31	0.000	0.000	
T2 92.00-80.00	86.00	1.315	22	80.855	A	5.464	4.750	4.750	46.50	23.401	0.000
					B	3.998	25.570	16.06	0.000	0.000	
					C	5.464	4.750	46.50	0.000	0.000	
T3 80.00-60.00	70.00	1.24	20	155.998	A	8.840	11.681	9.599	46.78	39.001	0.000
					B	6.880	44.299	18.76	0.000	0.000	
					C	8.890	10.849	48.63	0.000	0.000	
T4 60.00-40.00	50.00	1.126	18	197.250	A	11.243	5.233	0.000	0.00	39.001	0.000
					B	9.445	34.700	0.00	0.000	0.000	
					C	11.258	5.000	0.00	0.000	0.000	
T5 40.00-20.00	30.00	1	16	237.659	A	16.265	5.233	0.000	0.00	39.001	0.000
					B	14.138	34.700	0.00	0.000	0.000	
					C	16.282	5.000	0.00	0.000	0.000	
T6 20.00-0.00	10.00	1	16	279.593	A	18.643	3.663	0.000	0.00	27.301	0.000
					B	17.207	24.290	0.00	0.000	0.000	
					C	18.654	3.500	0.00	0.000	0.000	

**Tower Pressure - With Ice**

$G_H = 1.159$

Section Elevation ft	z ft	$K_Z$	$q_z$ psf	$t_z$ in	$A_G$ ft <sup>2</sup>	F a c e	$A_F$ ft <sup>2</sup>	$A_R$ ft <sup>2</sup>	$A_{leg}$ ft <sup>2</sup>	Leg %	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>
T1 104.00-92.00	98.00	1.365	17	0.5000	81.615	A	6.749	10.985	6.750	38.06	0.000	0.000
						B	18.416	14.640	20.42	0.000	0.000	
						C	6.749	10.985	38.06	0.000	0.000	
T2 92.00-80.00	86.00	1.315	16	0.5000	81.855	A	5.464	10.146	6.750	43.24	37.800	0.000
						B	23.415	15.928	17.16	0.000	0.000	
						C	5.464	10.146	43.24	0.000	0.000	
T3 80.00-60.00	70.00	1.24	15	0.5000	157.666	A	8.684	23.276	12.938	40.48	63.000	0.000
						B	39.346	28.640	19.03	0.000	0.000	
						C	8.865	20.397	44.22	0.000	0.000	
T4 60.00-40.00	50.00	1.126	14	0.5000	198.919	A	10.938	15.589	0.000	0.00	63.000	0.000
						B	41.901	15.937	0.00	0.000	0.000	
						C	11.156	12.131	0.00	0.000	0.000	
T5 40.00-20.00	30.00	1	12	0.5000	239.328	A	15.904	16.464	0.000	0.00	63.000	0.000
						B	46.483	16.869	0.00	0.000	0.000	
						C	16.161	13.001	0.00	0.000	0.000	
T6 20.00-0.00	10.00	1	12	0.5000	281.262	A	18.399	14.375	0.000	0.00	44.100	0.000
						B	39.866	14.683	0.00	0.000	0.000	
						C	18.573	11.948	0.00	0.000	0.000	

**Tower Pressure - Service**



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	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

$$G_H = 1.159$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
T1 104.00-92.00	98.00	1.365	13	80.615	A	6.749	4.750	4.750	41.31	0.000	0.000
					B	5.538	18.630		19.65	0.000	0.000
					C	6.749	4.750		41.31	0.000	0.000
T2 92.00-80.00	86.00	1.315	12	80.855	A	5.464	4.750	4.750	46.50	23.401	0.000
					B	3.998	25.570		16.06	0.000	0.000
					C	5.464	4.750		46.50	0.000	0.000
T3 80.00-60.00	70.00	1.24	11	155.998	A	8.840	11.681	9.599	46.78	39.001	0.000
					B	6.880	44.299		18.76	0.000	0.000
					C	8.890	10.849		48.63	0.000	0.000
T4 60.00-40.00	50.00	1.126	10	197.250	A	11.243	5.233	0.000	0.00	39.001	0.000
					B	9.445	34.700		0.00	0.000	0.000
					C	11.258	5.000		0.00	0.000	0.000
T5 40.00-20.00	30.00	1	9	237.659	A	16.265	5.233	0.000	0.00	39.001	0.000
					B	14.138	34.700		0.00	0.000	0.000
					C	16.282	5.000		0.00	0.000	0.000
T6 20.00-0.00	10.00	1	9	279.593	A	18.643	3.663	0.000	0.00	27.301	0.000
					B	17.207	24.290		0.00	0.000	0.000
					C	18.654	3.500		0.00	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	1	1	9.506	1.01	84.39	B
			B	0.3	2.297	0.616	1	1	17.011			
			C	0.143	2.799	0.58	1	1	9.506			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	1	1	8.210	1.67	139.00	B
			B	0.366	2.136	0.638	1	1	20.317			
			C	0.126	2.861	0.578	1	1	8.210			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	1	1	15.601	2.73	136.41	B
			B	0.328	2.224	0.625	1	1	34.562			
			C	0.127	2.86	0.578	1	1	15.162			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	1	1	14.245	2.46	122.80	B
			B	0.224	2.518	0.596	1	1	30.110			
			C	0.082	3.036	0.573	1	1	14.125			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	1	1	19.270	2.44	121.90	B
			B	0.205	2.578	0.592	1	1	34.665			
			C	0.09	3.006	0.574	1	1	19.152			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	1	1	20.743	2.17	108.55	B
			B	0.148	2.777	0.581	1	1	31.325			
			C	0.079	3.049	0.573	1	1	20.660			
Sum Weight:	3.76	3.19						OTM	651.31 kip-ft	12.47		

### Tower Forces - No Ice - Wind 60 To Face

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	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	0.8	1	8.156	0.95	78.89	B
			B	0.3	2.297	0.616	0.8	1	15.904			
			C	0.143	2.799	0.58	0.8	1	8.156			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	0.8	1	7.118	1.63	135.45	B
			B	0.366	2.136	0.638	0.8	1	19.517			
			C	0.126	2.861	0.578	0.8	1	7.118			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	0.8	1	13.833	2.66	132.81	B
			B	0.328	2.224	0.625	0.8	1	33.186			
			C	0.127	2.86	0.578	0.8	1	13.384			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	0.8	1	11.996	2.35	117.71	B
			B	0.224	2.518	0.596	0.8	1	28.221			
			C	0.082	3.036	0.573	0.8	1	11.873			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	0.8	1	16.017	2.30	114.97	B
			B	0.205	2.578	0.592	0.8	1	31.837			
			C	0.09	3.006	0.574	0.8	1	15.896			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	0.8	1	17.014	1.99	99.47	B
			B	0.148	2.777	0.581	0.8	1	27.884			
			C	0.079	3.049	0.573	0.8	1	16.929			
Sum Weight:	3.76	3.19						OTM	625.08 kip-ft	11.87		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	0.85	1	8.493	0.96	80.27	B
			B	0.3	2.297	0.616	0.85	1	16.181			
			C	0.143	2.799	0.58	0.85	1	8.493			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	0.85	1	7.391	1.64	136.34	B
			B	0.366	2.136	0.638	0.85	1	19.717			
			C	0.126	2.861	0.578	0.85	1	7.391			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	0.85	1	14.275	2.67	133.71	B
			B	0.328	2.224	0.625	0.85	1	33.530			
			C	0.127	2.86	0.578	0.85	1	13.829			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	0.85	1	12.558	2.38	118.98	B
			B	0.224	2.518	0.596	0.85	1	28.693			
			C	0.082	3.036	0.573	0.85	1	12.436			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	0.85	1	16.830	2.33	116.70	B
			B	0.205	2.578	0.592	0.85	1	32.544			
			C	0.09	3.006	0.574	0.85	1	16.710			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	0.85	1	17.946	2.03	101.74	B
			B	0.148	2.777	0.581	0.85	1	28.744			
			C	0.079	3.049	0.573	0.85	1	17.862			
Sum Weight:	3.76	3.19						OTM	631.63 kip-ft	12.02		

### Tower Forces - With Ice - Wind Normal To Face

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	<b>Project</b> SST Analysis	<b>Date</b> 12:06:49 06/03/14
	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.41	0.61	A	0.217	2.539	0.594	1	1	13.275	1.12	93.13	B
			B	0.405	2.054	0.654	1	1	27.986			
			C	0.217	2.539	0.594	1	1	13.275			
T2 92.00-80.00	0.91	0.56	A	0.191	2.627	0.589	1	1	11.435	1.95	162.34	B
			B	0.481	1.926	0.688	1	1	34.371			
			C	0.191	2.627	0.589	1	1	11.435			
T3 80.00-60.00	1.61	0.97	A	0.203	2.587	0.591	1	1	22.439	3.18	159.02	B
			B	0.431	2.006	0.665	1	1	58.387			
			C	0.186	2.645	0.588	1	1	20.849			
T4 60.00-40.00	1.81	0.92	A	0.133	2.834	0.579	1	1	19.965	2.93	146.71	B
			B	0.291	2.321	0.613	1	1	51.672			
			C	0.117	2.896	0.577	1	1	18.155			
T5 40.00-20.00	1.81	1.30	A	0.135	2.827	0.579	1	1	25.442	2.83	141.56	B
			B	0.265	2.394	0.606	1	1	56.702			
			C	0.122	2.878	0.578	1	1	23.670			
T6 20.00-0.00	1.27	1.47	A	0.117	2.899	0.577	1	1	26.692	2.44	121.82	B
			B	0.194	2.616	0.589	1	1	48.517			
			C	0.109	2.93	0.576	1	1	25.455			
Sum Weight:	7.83	5.83						OTM	755.69 kip-ft	14.45		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.41	0.61	A	0.217	2.539	0.594	0.8	1	11.925	0.97	80.88	B
			B	0.405	2.054	0.654	0.8	1	24.303			
			C	0.217	2.539	0.594	0.8	1	11.925			
T2 92.00-80.00	0.91	0.56	A	0.191	2.627	0.589	0.8	1	10.343	1.78	148.26	B
			B	0.481	1.926	0.688	0.8	1	29.688			
			C	0.191	2.627	0.589	0.8	1	10.343			
T3 80.00-60.00	1.61	0.97	A	0.203	2.587	0.591	0.8	1	20.702	2.90	145.08	B
			B	0.431	2.006	0.665	0.8	1	50.518			
			C	0.186	2.645	0.588	0.8	1	19.076			
T4 60.00-40.00	1.81	0.92	A	0.133	2.834	0.579	0.8	1	17.778	2.62	131.11	B
			B	0.291	2.321	0.613	0.8	1	43.292			
			C	0.117	2.896	0.577	0.8	1	15.924			
T5 40.00-20.00	1.81	1.30	A	0.135	2.827	0.579	0.8	1	22.262	2.51	125.71	B
			B	0.265	2.394	0.606	0.8	1	47.405			
			C	0.122	2.878	0.578	0.8	1	20.438			
T6 20.00-0.00	1.27	1.47	A	0.117	2.899	0.577	0.8	1	23.012	2.14	106.96	B
			B	0.194	2.616	0.589	0.8	1	40.544			
			C	0.109	2.93	0.576	0.8	1	21.740			
Sum Weight:	7.83	5.83						OTM	679.16 kip-ft	12.93		

### Tower Forces - With Ice - Wind 90 To Face

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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.41	0.61	A	0.217	2.539	0.594	0.85	1	12.263	1.01	83.94	B
			B	0.405	2.054	0.654	0.85	1	25.224			
			C	0.217	2.539	0.594	0.85	1	12.263			
T2 92.00-80.00	0.91	0.56	A	0.191	2.627	0.589	0.85	1	10.616	1.82	151.78	B
			B	0.481	1.926	0.688	0.85	1	30.859			
			C	0.191	2.627	0.589	0.85	1	10.616			
T3 80.00-60.00	1.61	0.97	A	0.203	2.587	0.591	0.85	1	21.137	2.97	148.57	B
			B	0.431	2.006	0.665	0.85	1	52.485			
			C	0.186	2.645	0.588	0.85	1	19.520			
T4 60.00-40.00	1.81	0.92	A	0.133	2.834	0.579	0.85	1	18.325	2.70	135.01	B
			B	0.291	2.321	0.613	0.85	1	45.387			
			C	0.117	2.896	0.577	0.85	1	16.482			
T5 40.00-20.00	1.81	1.30	A	0.135	2.827	0.579	0.85	1	23.057	2.59	129.67	B
			B	0.265	2.394	0.606	0.85	1	49.729			
			C	0.122	2.878	0.578	0.85	1	21.246			
T6 20.00-0.00	1.27	1.47	A	0.117	2.899	0.577	0.85	1	23.932	2.21	110.68	B
			B	0.194	2.616	0.589	0.85	1	42.537			
			C	0.109	2.93	0.576	0.85	1	22.669			
Sum Weight:	7.83	5.83						OTM	698.29 kip-ft	13.31		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	1	1	9.506	0.57	47.47	B
			B	0.3	2.297	0.616	1	1	17.011			
			C	0.143	2.799	0.58	1	1	9.506			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	1	1	8.210	0.94	78.19	B
			B	0.366	2.136	0.638	1	1	20.317			
			C	0.126	2.861	0.578	1	1	8.210			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	1	1	15.601	1.53	76.73	B
			B	0.328	2.224	0.625	1	1	34.562			
			C	0.127	2.86	0.578	1	1	15.162			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	1	1	14.245	1.38	69.07	B
			B	0.224	2.518	0.596	1	1	30.110			
			C	0.082	3.036	0.573	1	1	14.125			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	1	1	19.270	1.37	68.57	B
			B	0.205	2.578	0.592	1	1	34.665			
			C	0.09	3.006	0.574	1	1	19.152			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	1	1	20.743	1.22	61.06	B
			B	0.148	2.777	0.581	1	1	31.325			
			C	0.079	3.049	0.573	1	1	20.660			
Sum Weight:	3.76	3.19						OTM	366.36 kip-ft	7.02		

### Tower Forces - Service - Wind 60 To Face

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Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	0.8	1	8.156	0.53	44.38	B
			B	0.3	2.297	0.616	0.8	1	15.904			
			C	0.143	2.799	0.58	0.8	1	8.156			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	0.8	1	7.118	0.91	76.19	B
			B	0.366	2.136	0.638	0.8	1	19.517			
			C	0.126	2.861	0.578	0.8	1	7.118			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	0.8	1	13.833	1.49	74.70	B
			B	0.328	2.224	0.625	0.8	1	33.186			
			C	0.127	2.86	0.578	0.8	1	13.384			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	0.8	1	11.996	1.32	66.21	B
			B	0.224	2.518	0.596	0.8	1	28.221			
			C	0.082	3.036	0.573	0.8	1	11.873			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	0.8	1	16.017	1.29	64.67	B
			B	0.205	2.578	0.592	0.8	1	31.837			
			C	0.09	3.006	0.574	0.8	1	15.896			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	0.8	1	17.014	1.12	55.95	B
			B	0.148	2.777	0.581	0.8	1	27.884			
			C	0.079	3.049	0.573	0.8	1	16.929			
Sum Weight:	3.76	3.19						OTM	351.61 kip-ft	6.68		

### Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 104.00-92.00	0.20	0.29	A	0.143	2.799	0.58	0.85	1	8.493	0.54	45.15	B
			B	0.3	2.297	0.616	0.85	1	16.181			
			C	0.143	2.799	0.58	0.85	1	8.493			
T2 92.00-80.00	0.42	0.30	A	0.126	2.861	0.578	0.85	1	7.391	0.92	76.69	B
			B	0.366	2.136	0.638	0.85	1	19.717			
			C	0.126	2.861	0.578	0.85	1	7.391			
T3 80.00-60.00	0.75	0.51	A	0.132	2.841	0.579	0.85	1	14.275	1.50	75.21	B
			B	0.328	2.224	0.625	0.85	1	33.530			
			C	0.127	2.86	0.578	0.85	1	13.829			
T4 60.00-40.00	0.89	0.51	A	0.084	3.031	0.574	0.85	1	12.558	1.34	66.93	B
			B	0.224	2.518	0.596	0.85	1	28.693			
			C	0.082	3.036	0.573	0.85	1	12.436			
T5 40.00-20.00	0.89	0.74	A	0.09	3.003	0.574	0.85	1	16.830	1.31	65.65	B
			B	0.205	2.578	0.592	0.85	1	32.544			
			C	0.09	3.006	0.574	0.85	1	16.710			
T6 20.00-0.00	0.62	0.84	A	0.08	3.047	0.573	0.85	1	17.946	1.14	57.23	B
			B	0.148	2.777	0.581	0.85	1	28.744			
			C	0.079	3.049	0.573	0.85	1	17.862			
Sum Weight:	3.76	3.19						OTM	355.29 kip-ft	6.76		

### Force Totals

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Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>z</sub> kip-ft	Sum of Torques kip-ft
Leg Weight	0.00					
Bracing Weight	3.19					
Total Member Self-Weight	3.19					
Total Weight	11.91			-6.24	-0.04	
Wind 0 deg - No Ice		0.04	-20.44	-1362.15	-3.45	2.30
Wind 90 deg - No Ice		20.11	-0.04	-9.65	-1347.78	-11.19
Wind 180 deg - No Ice		-0.04	19.84	1323.44	3.37	-2.29
Member Ice	2.64					
Total Weight Ice	20.98			-19.90	-1.70	
Wind 0 deg - Ice		0.03	-21.06	-1358.61	-4.37	2.34
Wind 90 deg - Ice		20.01	-0.03	-22.57	-1292.04	-11.85
Wind 180 deg - Ice		-0.03	19.54	1242.27	0.97	-2.35
Total Weight	11.91			-6.24	-0.04	
Wind 0 deg - Service		0.02	-11.50	-758.64	-2.77	1.29
Wind 90 deg - Service		11.31	-0.02	2.15	-758.95	-6.29
Wind 180 deg - Service		-0.02	11.16	752.01	1.07	-1.29

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 90 deg - No Ice
4	Dead+Wind 180 deg - No Ice
5	Dead+Ice+Temp
6	Dead+Wind 0 deg+Ice+Temp
7	Dead+Wind 90 deg+Ice+Temp
8	Dead+Wind 180 deg+Ice+Temp
9	Dead+Wind 0 deg - Service
10	Dead+Wind 90 deg - Service
11	Dead+Wind 180 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	104 - 92	Leg	Max Tension	4	3.21	-0.00	0.12
			Max. Compression	6	-5.08	-0.01	0.41
			Max. Mx	3	-4.23	-0.51	0.04
			Max. My	2	-4.88	-0.01	0.49
			Max. Vy	3	-1.17	0.01	0.00
			Max. Vx	2	1.08	0.00	0.04
		Diagonal	Max Tension	4	1.36	0.00	0.00
			Max. Compression	2	-1.36	0.00	0.00
			Max. Mx	7	0.89	0.01	0.00
			Max. My	4	-1.12	0.00	0.00
			Max. Vy	7	-0.01	0.01	0.00
			Max. Vx	4	0.00	0.00	0.00
		Top Girt	Max Tension	4	0.43	0.00	0.00
			Max. Compression	2	-0.43	0.00	0.00
			Max. Mx	5	-0.01	-0.02	0.00

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T2	92 - 80	Leg	Max. My	7	-0.01	0.00	0.00
			Max. Vy	5	0.01	0.00	0.00
			Max. Vx	7	-0.00	0.00	0.00
			Max Tension	4	14.21	-0.60	-0.01
			Max. Compression	2	-16.75	-0.17	-0.00
			Max. Mx	2	-8.93	-0.97	0.01
			Max. My	4	-5.68	0.28	-0.86
			Max. Vy	4	0.79	-0.60	-0.01
		Diagonal	Max. Vx	3	-0.70	0.00	0.54
			Max Tension	3	4.04	0.00	0.00
			Max. Compression	3	-4.18	0.00	0.00
			Max. Mx	6	2.88	0.02	0.00
			Max. My	4	-1.89	0.00	0.00
			Max. Vy	6	-0.01	0.02	0.00
			Max. Vx	4	0.00	0.00	0.00
			Max Tension	2	0.21	0.00	0.00
Top Girt	Max. Compression	8	-0.26	0.00	0.00		
	Max. Mx	5	-0.05	-0.02	0.00		
	Max. My	7	-0.06	0.00	0.00		
	Max. Vy	5	0.01	0.00	0.00		
	Max. Vx	7	-0.00	0.00	0.00		
	Max Tension	4	39.60	-0.08	-0.01		
	Max. Compression	2	-44.38	0.05	-0.00		
	Max. Mx	8	17.64	-0.18	0.07		
T3	80 - 60	Leg	Max. My	8	-16.35	0.05	-0.18
			Max. Vy	4	-0.47	-0.08	-0.01
			Max. Vx	3	0.44	0.00	0.02
			Max Tension	3	3.51	0.00	0.00
			Max. Compression	3	-3.55	0.00	0.00
			Max. Mx	8	2.79	0.02	0.00
			Max. My	8	-3.10	0.01	0.00
			Max. Vy	8	0.01	0.02	0.00
		Diagonal	Max. Vx	8	-0.00	0.00	0.00
			Max Tension	4	61.44	-0.06	-0.00
			Max. Compression	2	-68.22	0.12	-0.00
			Max. Mx	8	53.31	-0.22	0.00
			Max. My	3	-2.63	-0.01	0.16
			Max. Vy	8	0.04	-0.22	0.00
			Max. Vx	3	0.05	-0.01	0.16
			Max Tension	3	3.76	0.00	0.00
T4	60 - 40	Leg	Max. Compression	6	-3.81	0.00	0.00
			Max. Mx	8	3.02	0.03	0.00
			Max. My	8	-3.45	0.01	0.00
			Max. Vy	8	0.02	0.03	0.00
			Max. Vx	8	-0.00	0.00	0.00
			Max Tension	4	80.85	-0.10	-0.00
			Max. Compression	6	-90.38	0.41	0.00
			Max. Mx	6	-90.38	0.41	0.00
		Diagonal	Max. My	3	-4.03	-0.01	0.17
			Max. Vy	8	-0.09	-0.31	-0.00
			Max. Vx	3	-0.04	-0.01	0.17
			Max Tension	6	3.80	0.00	0.00
			Max. Compression	6	-4.10	0.00	0.00
			Max. Mx	6	3.06	0.06	-0.00
			Max. My	7	-2.63	0.04	0.01
			Max. Vy	8	0.03	0.06	0.00
Leg	Max. Vx	7	-0.00	0.00	0.00		
	Max Tension	4	97.97	-0.11	-0.00		
	Max. Compression	6	-111.85	0.00	0.00		
	Max. Mx	8	84.00	-0.71	-0.00		
Diagonal	Max. My	3	-4.61	-0.02	0.30		

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
		Diagonal	Max. Vy	8	-0.18	-0.71	-0.00
			Max. Vx	3	-0.07	-0.02	0.30
			Max Tension	8	4.43	0.00	0.00
			Max. Compression	6	-4.36	0.00	0.00
			Max. Mx	8	2.58	0.07	0.00
			Max. My	7	-3.15	0.06	0.01
			Max. Vy	8	0.03	0.07	0.00
			Max. Vx	7	-0.00	0.00	0.00

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	4	56.48	4.67	-4.16
	Max. H <sub>x</sub>	4	56.48	4.67	-4.16
	Max. H <sub>z</sub>	7	-82.40	-9.63	5.16
	Min. Vert	3	-88.62	-8.81	4.68
	Min. H <sub>x</sub>	7	-82.40	-9.63	5.16
	Min. H <sub>z</sub>	4	56.48	4.67	-4.16
Leg B	Max. Vert	3	95.80	-9.27	-4.94
	Max. H <sub>x</sub>	6	-46.43	5.19	4.78
	Max. H <sub>z</sub>	6	-46.43	5.19	4.78
	Min. Vert	2	-49.60	4.19	4.15
	Min. H <sub>x</sub>	3	95.80	-9.27	-4.94
	Min. H <sub>z</sub>	3	95.80	-9.27	-4.94
Leg A	Max. Vert	6	114.44	0.09	11.64
	Max. H <sub>x</sub>	6	114.44	0.09	11.64
	Max. H <sub>z</sub>	2	111.58	0.09	12.28
	Min. Vert	4	-100.58	-0.09	-11.38
	Min. H <sub>x</sub>	7	8.78	-2.06	-0.68
	Min. H <sub>z</sub>	8	-91.26	-0.09	-12.17

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	11.91	0.00	-0.00	-6.24	-0.04	-0.00
Dead+Wind 0 deg - No Ice	11.91	0.04	-20.44	-1365.27	-3.47	2.30
Dead+Wind 90 deg - No Ice	11.91	20.11	-0.04	-9.68	-1350.89	-11.19
Dead+Wind 180 deg - No Ice	11.91	-0.04	19.84	1326.50	3.36	-2.29
Dead+Ice+Temp	20.98	-0.00	0.00	-19.94	-1.70	0.00
Dead+Wind 0 deg+Ice+Temp	20.98	0.03	-21.06	-1363.25	-4.41	2.36
Dead+Wind 90 deg+Ice+Temp	20.98	20.01	-0.03	-22.65	-1296.52	-11.91
Dead+Wind 180 deg+Ice+Temp	20.98	-0.03	19.54	1246.59	0.96	-2.36
Dead+Wind 0 deg - Service	11.91	0.02	-11.50	-770.70	-1.97	1.29
Dead+Wind 90 deg - Service	11.91	11.31	-0.02	-8.17	-759.90	-6.30
Dead+Wind 180 deg - Service	11.91	-0.02	11.16	743.43	1.87	-1.29



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### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-11.91	0.00	-0.00	11.91	0.00	0.000%
2	0.04	-11.91	-20.44	-0.04	11.91	20.44	0.001%
3	20.11	-11.91	-0.04	-20.11	11.91	0.04	0.001%
4	-0.04	-11.91	19.84	0.04	11.91	-19.84	0.002%
5	0.00	-20.98	0.00	0.00	20.98	-0.00	0.000%
6	0.03	-20.98	-21.06	-0.03	20.98	21.06	0.002%
7	20.01	-20.98	-0.03	-20.01	20.98	0.03	0.002%
8	-0.03	-20.98	19.54	0.03	20.98	-19.54	0.002%
9	0.02	-11.91	-11.50	-0.02	11.91	11.50	0.001%
10	11.31	-11.91	-0.02	-11.31	11.91	0.02	0.001%
11	-0.02	-11.91	11.16	0.02	11.91	-11.16	0.001%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	8	0.00000001	0.00007088
3	Yes	8	0.00000001	0.00008004
4	Yes	8	0.00000001	0.00008792
5	Yes	6	0.00000001	0.00010110
6	Yes	8	0.00000001	0.00012054
7	Yes	8	0.00000001	0.00012995
8	Yes	8	0.00000001	0.00013695
9	Yes	8	0.00000001	0.00007425
10	Yes	8	0.00000001	0.00007960
11	Yes	8	0.00000001	0.00008422

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist "
T1	104 - 92	3.849	10	0.3204	0.0278
T2	92 - 80	3.037	9	0.3146	0.0245
T3	80 - 60	2.265	9	0.2759	0.0228
T4	60 - 40	1.248	9	0.1808	0.0196
T5	40 - 20	0.566	9	0.1177	0.0137
T6	20 - 0	0.160	9	0.0533	0.0073

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
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	<b>Client</b> Insite Towers, LLC	<b>Designed by</b> LETS America, Inc.

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
100.00	12' T-Frame Sector Mount	10	3.577	0.3206	0.0266	321983
88.00	12' T-Frame Sector Mount	9	2.772	0.3055	0.0238	29808
79.00	DB806-XT	9	2.205	0.2715	0.0227	12064
73.00	PR-950	9	1.867	0.2425	0.0219	12334
65.00	(2) AIR 21	9	1.468	0.2028	0.0206	13250

### Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
T1	104 - 92	6.835	3	0.5686	0.0515
T2	92 - 80	5.395	2	0.5585	0.0469
T3	80 - 60	4.019	2	0.4898	0.0437
T4	60 - 40	2.213	2	0.3207	0.0372
T5	40 - 20	1.004	2	0.2085	0.0260
T6	20 - 0	0.288	6	0.0944	0.0138

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
100.00	12' T-Frame Sector Mount	3	6.353	0.5691	0.0498	177613
88.00	12' T-Frame Sector Mount	2	4.922	0.5422	0.0457	16811
79.00	DB806-XT	2	3.913	0.4818	0.0434	6866
73.00	PR-950	2	3.312	0.4304	0.0418	6960
65.00	(2) AIR 21	2	2.604	0.3600	0.0392	7476

### Bolt Design Data

Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of Bolts	Maximum Load per Bolt	Allowable Load	Ratio	Allowable Ratio	Criteria	
	ft			in		K	K	Allowable			
T1	104	Leg	A325N	0.6250	4	0.05	13.50	0.004	✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	1.36	4.08	0.333	✓	1.333	Member Bearing
		Top Girt	A325N	0.5000	1	0.43	4.12	0.105	✓	1.333	Bolt Shear
T2	92	Leg	A325N	0.6250	4	1.68	13.49	0.124	✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	4.18	4.12	1.014	✓	1.333	Bolt Shear
		Top Girt	A325N	0.5000	1	0.26	4.12	0.063	✓	1.333	Bolt Shear
T3	80	Leg	A325N	0.6250	4	5.52	13.50	0.409	✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	3.55	4.12	0.860	✓	1.333	Bolt Shear
T4	60	Leg	A325N	0.6250	4	11.65	13.50	0.863	✓	1.333	Bolt Tension

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T5	40	Diagonal	A325N	0.5000	1	3.81	4.12	0.924 ✓	1.333	Bolt Shear
		Leg	A325N	0.6250	4	17.05	13.50	1.263 ✓	1.333	Bolt Tension
T6	20	Diagonal	A325N	0.5000	1	4.10	4.12	0.994 ✓	1.333	Bolt Shear
		Leg	A325N	0.7500	4	21.69	19.44	1.116 ✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	4.43	4.08	1.085 ✓	1.333	Member Bearing

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>n</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	104 - 92	P2x.154	12.00	4.00	61.0 K=1.00	22.549	1.0745	-5.08	24.23	0.210 ✓
T2	92 - 80	P2x.154	12.00	6.00	91.5 K=1.00	16.619	1.0745	-16.75	17.86	0.938 ✓
T3	80 - 60	P2.5x.203	20.03	5.01	63.4 K=1.00	22.122	1.7040	-44.38	37.70	1.177 ✓
T4	60 - 40	Pipe 2.875 x .203 w/ 3/8 Plate	20.03	6.68	88.5 K=1.00	17.258	3.5180	-68.22	60.71	1.124 ✓
T5	40 - 20	Pipe 2.875 x 0.276 w/ 3/8 Plate	20.03	6.68	87.0 K=1.00	17.572	4.0080	-90.38	70.43	1.283 ✓
T6	20 - 0	Pipe 3 x 0.3 w/ 3/8 Plate	20.03	6.68	71.4 K=1.00	20.671	5.0840	-111.85	105.09	1.064 ✓

### Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>n</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	104 - 92	L1 1/2x1 1/2x3/16	7.65	3.60	147.4 K=1.00	6.869	0.5273	-1.36	3.62	0.374 ✓
T2	92 - 80	L1 1/2x1 1/2x1/4	8.88	4.21	173.0 K=1.00	4.990	0.6875	-4.18	3.43	1.218 ✓
T3	80 - 60	L1 1/2x1 1/2x1/4	9.70	4.75	195.3 K=1.00	3.917	0.6875	-3.55	2.69	1.317 ✓
T4	60 - 40	L2x2x3/16	12.21	6.04	183.9 K=1.00	4.416	0.7150	-3.63	3.16	1.150 ✓
T5	40 - 20	L2 1/2x2 1/2x3/16	13.96	6.91	167.6 K=1.00	5.316	0.9020	-4.10	4.80	0.855 ✓
T6	20 - 0	L2 1/2x2 1/2x3/16	15.17	7.49	181.6	4.526	0.9020	-4.36	4.08	1.069 ✓

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
K=1.00										
✓										

### Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	104 - 92	L2x2x3/16	6.52	6.11	186.2 K=1.00	4.307	0.7150	-0.43	3.08	0.141
T2	92 - 80	L2x2x3/16	6.52	6.11	186.2 K=1.00	4.307	0.7150	-0.26	3.08	0.084

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	104 - 92	P2x.154	12.00	4.00	61.0	30.000	1.0745	3.21	32.24	0.100
T2	92 - 80	P2x.154	12.00	6.00	91.5	30.000	1.0745	14.21	32.24	0.441
T3	80 - 60	P2.5x.203	20.03	5.01	63.4	30.000	1.7040	39.33	51.12	0.769
T4	60 - 40	Pipe 2.875 x .203 w/ 3/8 Plate	20.03	6.68	88.5	30.000	3.5180	61.44	105.54	0.582
T5	40 - 20	Pipe 2.875 x 0.276 w/ 3/8 Plate	20.03	6.68	87.0	30.000	4.0080	80.85	120.24	0.672
T6	20 - 0	Pipe 3 x 0.3 w/ 3/8 Plate	20.03	6.68	71.4	30.000	5.0840	97.97	152.52	0.642

### Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	104 - 92	L1 1/2x1 1/2x3/16	7.65	3.60	97.4	29.000	0.3076	1.36	8.92	0.152
T2	92 - 80	L1 1/2x1 1/2x1/4	8.88	4.21	115.3	29.000	0.3984	4.04	11.55	0.350
T3	80 - 60	L1 1/2x1 1/2x1/4	9.70	4.75	129.8	29.000	0.3984	3.51	11.55	0.304

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T4	60 - 40	L2x2x3/16	11.12	5.50	109.0	29.000	0.4484	3.76	13.00	0.289 ✓
T5	40 - 20	L2 1/2x2 1/2x3/16	13.36	6.62	103.7	29.000	0.5886	3.80	17.07	0.223 ✓
T6	20 - 0	L2 1/2x2 1/2x3/16	15.79	7.80	121.9	29.000	0.5886	4.43	17.07	0.259 ✓

### Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio $\frac{P}{P_a}$
T1	104 - 92	L2x2x3/16	6.52	6.11	123.0	29.000	0.4484	0.43	13.00	0.033 ✓
T2	92 - 80	L2x2x3/16	6.52	6.11	123.0	29.000	0.4484	0.21	13.00	0.016 ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	104 - 92	Leg	P2x.154	3	-5.08	32.30	15.7	Pass
T2	92 - 80	Leg	P2x.154	27	-16.75	23.80	70.4	Pass
T3	80 - 60	Leg	P2.5x.203	45	-44.38	50.25	88.3	Pass
T4	60 - 40	Leg	Pipe 2.875 x .203 w/ 3/8 Plate	72	-68.22	80.93	84.3	Pass
T5	40 - 20	Leg	Pipe 2.875 x 0.276 w/ 3/8 Plate	93	-90.38	93.88	96.3	Pass
T6	20 - 0	Leg	Pipe 3 x 0.3 w/ 3/8 Plate	114	-111.85	140.09	79.8	Pass
							83.7 (b)	
T1	104 - 92	Diagonal	L1 1/2x1 1/2x3/16	16	-1.36	4.83	28.1	Pass
T2	92 - 80	Diagonal	L1 1/2x1 1/2x1/4	32	-4.18	4.57	91.4	Pass
T3	80 - 60	Diagonal	L1 1/2x1 1/2x1/4	47	-3.55	3.59	98.8	Pass
T4	60 - 40	Diagonal	L2x2x3/16	74	-3.63	4.21	86.3	Pass
T5	40 - 20	Diagonal	L2 1/2x2 1/2x3/16	97	-4.10	6.39	64.1	Pass
							74.6 (b)	
T6	20 - 0	Diagonal	L2 1/2x2 1/2x3/16	124	-4.36	5.44	80.2	Pass
							81.4 (b)	
T1	104 - 92	Top Girt	L2x2x3/16	4	-0.43	4.10	10.6	Pass
T2	92 - 80	Top Girt	L2x2x3/16	28	-0.26	4.10	6.3	Pass
						Summary	ELC:	Existing+Proposed
						Leg (T5)	96.3	Pass
						Diagonal (T3)	98.8	Pass
						Top Girt (T1)	10.6	Pass
						Bolt Checks	94.8	Pass
						Rating =	98.8	Pass

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# **EXHIBIT C**

RADIO FREQUENCY EMISSIONS ANALYSIS REPORT  
EVALUATION OF HUMAN EXPOSURE POTENTIAL  
TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CTHA536A

Insite Glastonbury Lattice

577 Bell Street  
Glastonbury, CT 06033

**June 9, 2014**

**EBI Project Number: 62143318**



June 9, 2014

T-Mobile USA  
Attn: Jason Overbey, RF Manager  
35 Griffin Road South  
Bloomfield, CT 06002

Re: Emissions Values for Site: **CTHA536A - Insite Glastonbury Lattice**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 577 Bell Street, Glastonbury, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the cellular band is  $567 \mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the PCS and AWS bands is  $1000 \mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 577 Bell Street, Glastonbury, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, the actual antenna pattern gain value in the direction of the sample area was used. For this report the sample point is a 6 foot person standing at the base of the tower

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (1935.000 MHz—to 1945.000 MHz) were considered for each sector of the proposed installation.
- 2) 2 UMTS channels (2110.000 MHz to 2120.000 MHz / 2140.000 MHz to 2145.000 MHz) were considered for each sector of the proposed installation.
- 3) 2 LTE channels (2110.000 MHz to 2120.000 MHz / 2140.000 MHz to 2145.000 MHz) were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The actual gain in this direction was used per the manufactures supplied specifications.
- 6) The antenna used in this modeling is the Ericsson AIR21 for LTE, UMTS and GSM. This is based on feedback from the carrier with regards to anticipated antenna selection. This antenna has a 15.6 dBd gain value at its main lobe. Actual antenna gain values were used for all calculations as per the manufacturers specifications.

- 7) The antenna mounting height centerline of the proposed antennas is **65 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

Site ID	CTHA5356A - InSite Glastonbury Lattice
Site Address	577 Bell Street, Glastonbury, CT 06033
Site Type	Self Support Tower

Antenna Number	Antenna Make	Antenna Model	Status	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBi)	Antenna Height (ft)	Antenna analysis height (ft)	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
1a	Ericsson	AIR21 B4A/B2P	Active	AWS - 2100 MHz	LTE	60	2	120	-3.95	65	59	None	0	0	48.326044	4.99095	0.49909%
1b	Ericsson	AIR21 B4A/B2P	Not Used	-	-	0	0	0	-3.95	65	59	None	0	0	0	0	0.00000%
2a	Ericsson	AIR21 B2A / B4P	Active	PCS - 1950 MHz	GSM / UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
2b	Ericsson	AIR21 B2A / B4P	Passive	AWS - 2100 MHz	UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
Sector total Power Density Value: 0.998%																	

Antenna Number	Antenna Make	Antenna Model	Status	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBi)	Antenna Height (ft)	Antenna analysis height (ft)	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
1a	Ericsson	AIR21 B4A/B2P	Active	AWS - 2100 MHz	LTE	60	2	120	-3.95	65	59	None	0	0	48.326044	4.99095	0.49909%
1b	Ericsson	AIR21 B4A/B2P	Not Used	-	-	0	0	0	-3.95	65	59	None	0	0	0	0	0.00000%
2a	Ericsson	AIR21 B2A / B4P	Active	PCS - 1950 MHz	GSM / UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
2b	Ericsson	AIR21 B2A / B4P	Passive	AWS - 2100 MHz	UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
Sector total Power Density Value: 0.998%																	

Antenna Number	Antenna Make	Antenna Model	Status	Frequency Band	Technology	Power Out Per Channel (Watts)	Number of Channels	Composite Power	Antenna Gain in direction of sample point (dBi)	Antenna Height (ft)	Antenna analysis height (ft)	Cable Size	Cable Loss (dB)	Additional Loss	ERP	Power Density Value	Power Density Percentage
1a	Ericsson	AIR21 B4A/B2P	Active	AWS - 2100 MHz	LTE	60	2	120	-3.95	65	59	None	0	0	48.326044	4.99095	0.49909%
1b	Ericsson	AIR21 B4A/B2P	Not Used	-	-	0	0	0	-3.95	65	59	None	0	0	0	0	0.00000%
2a	Ericsson	AIR21 B2A / B4P	Active	PCS - 1950 MHz	GSM / UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
2b	Ericsson	AIR21 B2A / B4P	Passive	AWS - 2100 MHz	UMTS	30	2	60	-3.95	65	59	1-5/8"	0	0	24.163022	2.495475	0.24955%
Sector total Power Density Value: 0.998%																	

Site Composite MPE %	
Carrier	MPE %
T-Mobile	2.995%
Town	0.170%
Clearwire	6.150%
MetroPCS	16.110%
AT&T	5.550%
COX	15.960%
Verizon Wireless	31.660%
<b>Total Site MPE %</b>	<b>78.595%</b>

## Summary

All calculations performed for this analysis yielded results that were well within the allowable limits for general public exposure to RF Emissions.

The anticipated Maximum Composite contributions from the T-Mobile facility are **2.995% (0.998% from each sector)** of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **78.595%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



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