



**QC Development**

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April 12, 2019

Melanie A. Bachman  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**Notice of Exempt Modification – New Cingular Wireless PCS, LLC (AT&T) – CT2128**  
**3965 Congress Street, Fairfield, CT 06824**  
**N 41.18834722**  
**W 73.29907222**

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the 128-foot level of the existing 150-foot Monopole at 3965 Congress Street, Fairfield, CT. The tower and property are owned by the Town of Fairfield. AT&T now intends to remove three (3) Powerwave antennas and replace them with three (3) Kathrein 800-10965 antennas. AT&T will also swap (3) Ericsson RRUS-11 for (3) Ericsson 4449-B5/B12s and add (3) Ericsson 4415-B30 Remote Radio Units (RRU). The new antennas and RRUs will also be installed at the 128-foot level of the tower.

AT&T's use of this facility was approved by the Siting Council on March 9, 1999. This approval included no condition(s) that could feasibly be violated by this modification, including total facility height or mounting restrictions. This modification therefore complies with the aforementioned approval.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Michael Tetreau, First Selectman of the Town of Fairfield, and the Fairfield Town Plan & Zoning

Department as well as the property and tower owner.

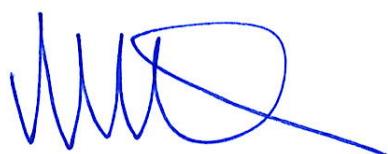
The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Please feel free to call me at (860) 670-9068 with any questions regarding this matter. Thank you for your consideration.

Sincerely,

A handwritten signature in blue ink, appearing to read "Mark Roberts".

Mark Roberts  
QC Development  
Consultant for AT&T

Attachments

Cc: Michael Tetreau - Elected Official, Property Owner & Tower Owner  
Jim Wendt – Planning Director

## Power Density

### Existing Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%MPE
Other Carriers*							14.03%
AT&T GSM	2	552	127	0.0271	850	0.5667	0.25%
AT&T UMTS	2	552	127	0.0271	850	0.5667	0.25%
AT&T UMTS	2	896	127	0.0440	1900	1.0000	0.22%
AT&T LTE	2	940	127	0.0462	700	0.4667	0.81%
AT&T LTE	2	1791	127	0.0880	1900	1.0000	0.66%
Site Total							17.29%

\*Per CSC Records (available upon request, includes calculation formulas)

\*\* If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

### Proposed Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%MPE
Other Carriers*							14.03%
AT&T UMTS	1	252	128	0.0061	850	0.5667	0.11%
AT&T LTE	1	1476	128	0.0357	700	0.4667	0.76%
AT&T LTE	1	1000	128	0.0242	850	0.5667	0.43%
AT&T 5G	1	1000	128	0.0242	850	0.5667	0.43%
AT&T LTE	2	3664	128	0.1771	1900	1.0000	1.77%
AT&T LTE	1	1285	128	0.0310	2300	1.0000	0.31%
Site Total							17.83%

\*Per CSC Records (available upon request, includes calculation formulas)

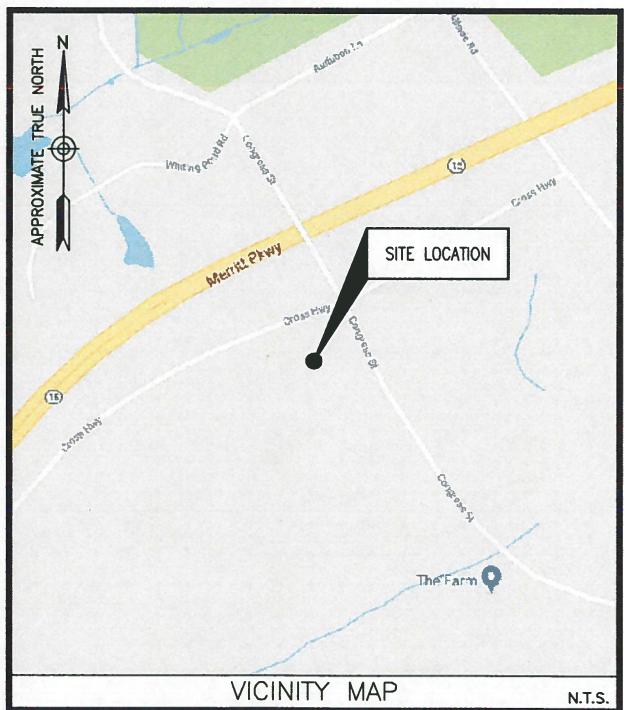
\*\* If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880



**at&t**  
**Mobility**

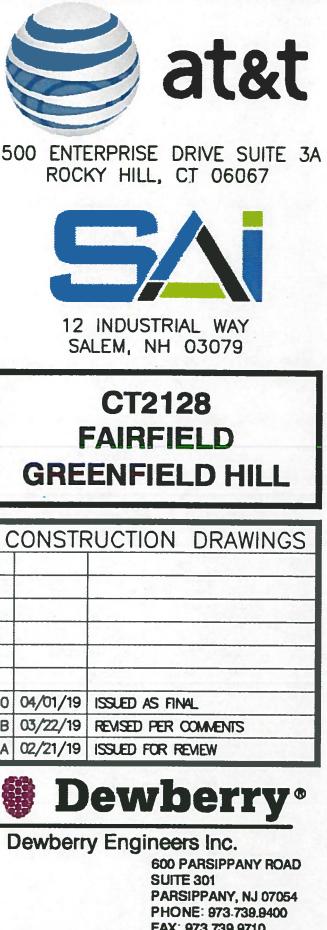
**SITE NAME: FAIRFIELD GREENFIELD HILL  
SITE NUMBER: CT2128  
3965 CONGRESS STREET  
FAIRFIELD, CT 06824  
FA CODE: 10035251**

**PACE ID: MRCTB035112, MRCTB035164, MRCTB035334**  
**PROJECT: LTE 3C, 4C, 5C**



<p><u>SITE COORDINATES:</u></p> <p>LATITUDE: 41°-11'-18.16" N      LONGITUDE: 73°-17'-56.59" W      (PER EXISTING DRAWINGS PROVIDED)</p> <p><u>ELLEVATION DATA:</u></p> <p>GRADE ELEVATION AT TOWER = 271± A.M.S.L.      (PER EXISTING DRAWINGS PROVIDED)</p>	<h2>SITE INFORMATION</h2> <ul style="list-style-type: none"> <li>• SWAP (3) EXISTING GSM ANTENNAS FOR (3) 6' 800-10955 OCTO ANTENNAS</li> <li>• SWAP (3) EXISTING RRUS-11'S FOR (3) B5/B12 4449 RRU'S UP TOP</li> <li>• ADD (3) B30 4415 RRU'S UP TOP</li> <li>• ADD (1) DC/FIBER SQUID WITH (1) 2" CONDUIT FOR 2 DC/1 FIBER</li> <li>• ADD HOMERUN RET TO UMTS ANTENNAS</li> <li>• GROUND - SWAP BB FOR 6630, ADD 5G RBS 6630</li> </ul>
<h2>PROJECT DESCRIPTION</h2>	

<u>SITE NAME:</u> FAIRFIELD GREENFIELD HILL	<u>SITE NUMBER:</u> CT2128
<u>SITE ADDRESS:</u> 3965 CONGRESS STREET FAIRFIELD, CT 06824	
<u>APPLICANT/LESSEE:</u> AT&T MOBILITY 500 ENTERPRISE DRIVE, SUITE 3A ROCKY HILL, CT 06067	
<b>PROJECT INFORMATION</b>	
THIS DOCUMENT WAS DEVELOPED TO REFLECT A SPECIFIC SITE AND ITS SITE CONDITIONS AND IS NOT TO BE USED FOR ANOTHER SITE OR WHEN OTHER CONDITIONS PERTAIN. REUSE OF THIS DOCUMENT IS AT THE SOLE RISK OF THE USER.	
A.D.A. COMPLIANCE: FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION.	



3965 CONGRESS STREET  
FAIRFIELD CT 06824

**SHEET TITLE**

## TITLE SHEET

SHEET NUMBER

T-1

**GENERAL NOTES:**

- FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:  
PROJECT MANAGEMENT - SAI COMMUNICATIONS, INC.  
CONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION)  
OWNER - AT&T MOBILITY  
OEM - ORIGINAL EQUIPMENT MANUFACTURER
- PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING CONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF PROJECT MANAGEMENT.
- ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK.
- ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- DRAWINGS PROVIDED HERE ARE NOT TO SCALE UNLESS OTHERWISE NOTED AND ARE INTENDED TO SHOW OUTLINE ONLY.
- UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY PROJECT MANAGEMENT.
- CONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. CONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. CONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH PROJECT MANAGEMENT.
- THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE OWNER.
- CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- CONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
- THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE PROJECT DESCRIBED HEREIN. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER THE CONTRACT.
- CONTRACTOR SHALL NOTIFY DEWBERRY 48 HOURS IN ADVANCE OF POURING CONCRETE, OR BACKFILLING TRENCHES, SEALING ROOF AND WALL PENETRATIONS & POST DOWNS, FINISHING NEW WALLS OR FINAL ELECTRICAL CONNECTIONS FOR ENGINEER REVIEW.
- CONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. CONTRACTOR SHALL NOTIFY PROJECT MANAGEMENT OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY CONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH LAND LORD. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
- SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.

**SITE WORK GENERAL NOTES:**

- THE CONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
- ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY CONTRACTOR. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO:  
 A) FALL PROTECTION  
 B) CONFINED SPACE  
 C) ELECTRICAL SAFETY  
 D) TRENCHING & EXCAVATION.
- ALL SITE WORK SHALL BE AS INDICATED ON THE DRAWINGS AND PROJECT SPECIFICATIONS.
- IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES, TOP SOIL AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
- ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF CONTRACTOR, OWNER AND/OR LOCAL UTILITIES.
- CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION.
- THE CONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE AT&T SPECIFICATION FOR SITE SIGNAGE.
- THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE TRANSMISSION EQUIPMENT AND TOWER AREAS.
- NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
- THE SUB GRADE SHALL BE COMPAKTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION, SEE SOIL COMPACTION NOTES.
- THE AREAS OF THE OWNER'S PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION.
- EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL JURISDICTION'S GUIDELINES FOR EROSION AND SEDIMENT CONTROL.

**STRUCTURAL STEEL NOTES:**

- ALL STEEL WORK SHALL BE PAINTED OR GALVANIZED IN ACCORDANCE WITH THE DRAWINGS UNLESS NOTED OTHERWISE. STRUCTURAL STEEL SHALL BE ASTM-A-36 UNLESS OTHERWISE NOTED ON THE SITE SPECIFIC DRAWINGS. STEEL DESIGN, INSTALLATION AND BOLTING SHALL BE PERFORMED IN ACCORDANCE WITH THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) "MANUAL OF STEEL CONSTRUCTION".
- ALL WELDING SHALL BE PERFORMED USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION". PAINTED SURFACES SHALL BE TOUCHED UP.
- BOLTED CONNECTIONS SHALL BE ASTM A325 BEARING TYPE (3/4"Ø) CONNECTIONS AND SHALL HAVE MINIMUM OF TWO BOLTS UNLESS NOTED OTHERWISE.
- NON-STRUCTURAL CONNECTIONS FOR STEEL GRATING MAY USE 5/8" Ø DIA. ASTM A 307 BOLTS UNLESS NOTED OTHERWISE.
- INSTALLATION OF CONCRETE EXPANSION/WEDGE ANCHOR, SHALL BE PER MANUFACTURER'S WRITTEN RECOMMENDED PROCEDURE. THE ANCHOR BOLT, DOWEL OR ROD SHALL CONFORM TO MANUFACTURER'S RECOMMENDATION FOR EMBEDMENT DEPTH OR AS SHOWN ON THE DRAWINGS. NO REBAR SHALL BE CUT WITHOUT PRIOR CONTRACTOR APPROVAL WHEN DRILLING HOLES IN CONCRETE. SPECIAL INSPECTIONS, REQUIRED BY GOVERNING CODES, SHALL BE PERFORMED IN ORDER TO MAINTAIN MANUFACTURER'S MAXIMUM ALLOWABLE LOADS. ALL EXPANSION/WEDGE ANCHORS SHALL BE STAINLESS STEEL OR HOT DIPPED GALVANIZED. EXPANSION BOLTS SHALL BE PROVIDED BY RAMSET/REDHEAD OR APPROVED EQUAL.
- CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR ENGINEER REVIEW & APPROVAL ON PROJECTS REQUIRING STRUCTURAL STEEL.
- ALL STRUCTURAL STEEL WORK SHALL BE DONE IN ACCORDANCE WITH AISC SPECIFICATIONS.

**SOIL COMPACTION NOTES FOR SLAB ON GRADE:**

- EXCAVATE AS REQUIRED TO REMOVE VEGETATION & TOPSOIL EXPOSE UNDISTURBED NATURAL SUBLGRADE AND PLACE CRUSHED STONE AS REQUIRED.
- COMPACTION CERTIFICATION: AN INSPECTION AND WRITTEN CERTIFICATION BY A QUALIFIED GEOTECHNICAL TECHNICIAN OR ENGINEER IS ACCEPTABLE.
- AS AN ALTERNATIVE TO INSPECTION AND WRITTEN CERTIFICATION, THE "UNDISTURBED SOIL" BASE SHALL BE COMPACTED WITH "COMPACTION EQUIPMENT", LISTED BELOW, TO AT LEAST 90% MODIFIED PROCTOR MAXIMUM DENSITY PER ASTM D 1557 METHOD C.
- COMPACTED SUBBASE SHALL BE UNIFORM & LEVELED. PROVIDE 6" MINIMUM CRUSHED STONE OR GRAVEL COMPACTED IN 3" LIFTS ABOVE COMPACTED SOIL. GRAVEL SHALL BE NATURAL OR CRUSHED WITH 100% PASSING 1" SIEVE.
- AS AN ALTERNATIVE TO ITEMS 2 AND 3 PROOFROLL THE SUBLGRADE SOILS WITH 5 PASSES OF A MEDIUM SIZED VIBRATORY PLATE COMPACTOR (SUCH AS BOMAG BPR 30/38) OR HAND-OPERATED SINGLE DRUM VIBRATORY ROLLER (SUCH AS BOMAG BW 55E). ANY SOFT AREAS THAT ARE ENCOUNTERED SHOULD BE REMOVED AND REPLACED WITH A WELL-GRADED GRANULAR FILL, AND COMPACTED AS STATED ABOVE.

**COMPACTION EQUIPMENT:**

- HAND OPERATED DOUBLE DRUM, VIBRATORY ROLLER, VIBRATORY PLATE COMPACTOR OR JUMPING JACK COMPACTOR.

**CONSTRUCTION NOTES:**

- FIELD VERIFICATION:**  
CONTRACTOR SHALL FIELD VERIFY SCOPE OF WORK, AT&T ANTENNA PLATFORM LOCATION AND ANTENNAS TO BE REPLACED.
- COORDINATION OF WORK:**  
CONTRACTOR SHALL COORDINATE RF WORK AND PROCEDURES WITH PROJECT MANAGEMENT.
- CABLE LADDER RACK:**  
CONTRACTOR SHALL FURNISH AND INSTALL CABLE LADDER RACK, CABLE TRAY, AND CONDUIT AS REQUIRED TO SUPPORT CABLES TO THE NEW BTS LOCATION.
- ALL POWER AND POWER GROUNDING CONNECTIONS SHALL BE CRIMP-STYLE, COMPRESSION WIRE LUGS AND WIRENUTS BY THOMAS AND BETTS (OR EQUAL). LUGS AND WIRENUTS SHALL BE RATED FOR OPERATION AT NO LESS THAN 75°C (90°C IF AVAILABLE).
- RACEWAY AND CABLE TRAY SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, UL, ANSI/IEEE, AND NEC.
- NEW RACEWAY OR CABLE TRAY WILL MATCH THE EXISTING INSTALLATION WHERE POSSIBLE.
- ELECTRICAL METALLIC TUBING (EMT) OR RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHEDULE 40, OR RIGID PVC SCHEDULE 80 FOR LOCATIONS SUBJECT TO PHYSICAL DAMAGE) SHALL BE USED FOR EXPOSED INDOOR LOCATIONS.
- ELECTRICAL METALLIC TUBING (EMT), ELECTRICAL NONMETALLIC TUBING (ENT), OR RIGID NONMETALLIC CONDUIT (RIGID PVC, SCHEDULE 40) SHALL BE USED FOR CONCEALED INDOOR LOCATIONS.
- GALVANIZED STEEL INTERMEDIATE METALLIC CONDUIT (IMC) SHALL BE USED FOR OUTDOOR LOCATIONS ABOVE GRADE.
- RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHEDULE 40 OR RIGID PVC SCHEDULE 80) SHALL BE USED UNDERGROUND; DIRECT BURIED, IN AREAS OF OCCASIONAL LIGHT VEHICLE TRAFFIC OR ENCASED IN REINFORCED CONCRETE IN AREAS OF HEAVY VEHICLE TRAFFIC.
- Liquid-tight flexible metallic conduit (Liquid-tite flex) shall be used indoors and outdoors, where vibration occurs or flexibility is needed.
- Conduit and tubing fittings shall be threaded or compression-type and approved for the location used. Setscrew fittings are not acceptable.
- CABINETS, BOXES, AND WIREWAYS SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, UL, ANSI/IEEE, AND NEC.
- CABINETS, BOXES, AND WIREWAYS TO MATCH THE EXISTING INSTALLATION WHERE POSSIBLE.
- WIREWAYS SHALL BE EPOXY-COATED (GRAY) AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARD; SHALL BE PANDUIT TYPE E (OR EQUAL); AND RATED NEMA 1 (OR BETTER) INDOORS, OR NEMA 3R (OR BETTER) OUTDOORS.
- EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES, AND PULL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET STEEL, SHALL MEET OR EXCEED UL 50, AND RATED NEMA 1 (OR BETTER) INDOORS, OR NEMA 3R (OR BETTER) OUTDOORS.
- METAL RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED, OR NON-CORRODING; SHALL MEET OR EXCEED UL 514A AND NEMA OS 1; AND RATED NEMA 1 (OR BETTER) INDOORS, OR WEATHER PROTECTED (WP OR BETTER) OUTDOORS.
- NONMETALLIC RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2; AND RATED NEMA 1 (OR BETTER) INDOORS, OR WEATHER PROTECTED (WP OR BETTER) OUTDOORS.
- THE CONTRACTOR SHALL NOTIFY AND OBTAIN NECESSARY AUTHORIZATION FROM PROJECT MANAGEMENT BEFORE COMMENCING WORK ON THE AC POWER DISTRIBUTION PANELS.
- THE CONTRACTOR SHALL PROVIDE NECESSARY TAGGING ON THE BREAKERS, CABLES AND DISTRIBUTION PANELS IN ACCORDANCE WITH THE APPLICABLE CODES AND STANDARDS TO SAFEGUARD AGAINST LIFE AND PROPERTY.

**ELECTRICAL INSTALLATION NOTES:**

- ALL ELECTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS, NEC AND ALL APPLICABLE LOCAL CODES.
- CONTRACTOR SHALL MODIFY EXISTING CABLE TRAY SYSTEM AS REQUIRED TO SUPPORT RF AND TRANSPORT CABLEING TO THE NEW BTS EQUIPMENT. CONTRACTOR SHALL SUBMIT MODIFICATIONS TO PROJECT MANAGEMENT FOR APPROVAL.
- CONDUIT ROUTINGS ARE SCHEMATIC. CONTRACTOR SHALL INSTALL CONDUITS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED.
- WIRING, RACEWAY AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE NEC.
- ALL CIRCUITS SHALL BE SEGREGATED AND MAINTAIN MINIMUM CABLE SEPARATION AS REQUIRED BY THE NEC.
- CABLES SHALL NOT BE ROUTED THROUGH LADDER-STYLE CABLE TRAY RUNGS.
- EACH END OF EVERY POWER, POWER PHASE CONDUCTOR (I.E., HOTS), GROUNDING, AND T1 CONDUCTOR AND CABLE SHALL BE LABELED WITH COLOR-CODED INSULATION OR ELECTRICAL TAPE (3M BRAND, 1/2 INCH PLASTIC ELECTRICAL TAPE WITH UV PROTECTION, OR EQUAL). THE IDENTIFICATION METHOD SHALL CONFORM WITH NEC & OSHA, AND MATCH EXISTING INSTALLATION REQUIREMENTS.
- ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABELED WITH ENGRAVED LAMACOID PLASTIC LABELS. ALL EQUIPMENT SHALL BE LABELED WITH THEIR VOLTAGE RATING, PHASE CONFIGURATION, WIRE CONFIGURATION, POWER OR AMPACITY RATING, AND BRANCH CIRCUIT ID NUMBERS (I.E., PANELBOARD AND CIRCUIT ID'S).
- PANELBOARDS (ID NUMBERS) AND INTERNAL CIRCUIT BREAKERS (CIRCUIT ID NUMBERS) SHALL BE CLEARLY LABELED WITH ENGRAVED LAMACOID PLASTIC LABELS.
- ALL TIE WRAPS SHALL BE CUT FLUSH WITH APPROVED CUTTING TOOL TO REMOVE SHARP EDGES.



500 ENTERPRISE DRIVE SUITE 3A  
ROCKY HILL, CT 06067



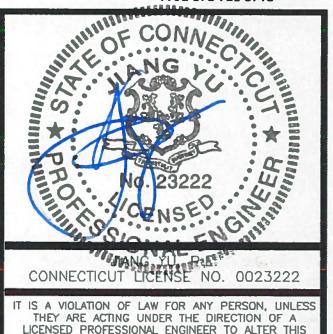
12 INDUSTRIAL WAY  
SALEM, NH 03079

**CT2128**  
**FAIRFIELD**  
**GREENFIELD HILL**

**CONSTRUCTION DRAWINGS**

O 04/01/19 ISSUED AS FINAL  
B 03/22/19 REVISED PER COMMENTS  
A 02/21/19 ISSUED FOR REVIEW

**Dewberry®**  
Dewberry Engineers Inc.  
600 PARISPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973-739-9400  
FAX: 973-739-9710



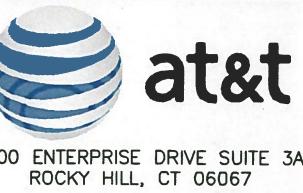
DRAWN BY: BJR  
REVIEWED BY: BSH  
CHECKED BY: GHN  
PROJECT NUMBER: 50055106  
JOB NUMBER: 50093832  
SITE ADDRESS:

3965 CONGRESS STREET  
FAIRFIELD, CT 06824

SHEET TITLE:

GENERAL NOTES

SHEET NUMBER:



00 ENTERPRISE DRIVE SUITE 3A  
ROCKY HILL, CT 06067



12 INDUSTRIAL WAY  
SALEM, NH 03079

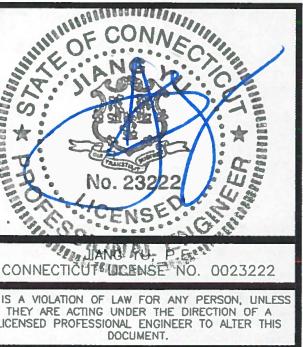
**CT2128  
FAIRFIELD  
GREENFIELD HILL**

## **CONSTRUCTION DRAWINGS**

04/01/19	ISSUED AS FINAL
03/22/19	REVISED PER COMMENTS
02/21/19	ISSUED FOR REVIEW



**Newberry Engineers Inc.**  
600 PARSIPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973.739.9400  
FAX: 973.739.9710



IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS  
THEY ARE ACTING UNDER THE DIRECTION OF A  
LICENSED PROFESSIONAL ENGINEER TO ALTER THIS  
DOCUMENT.

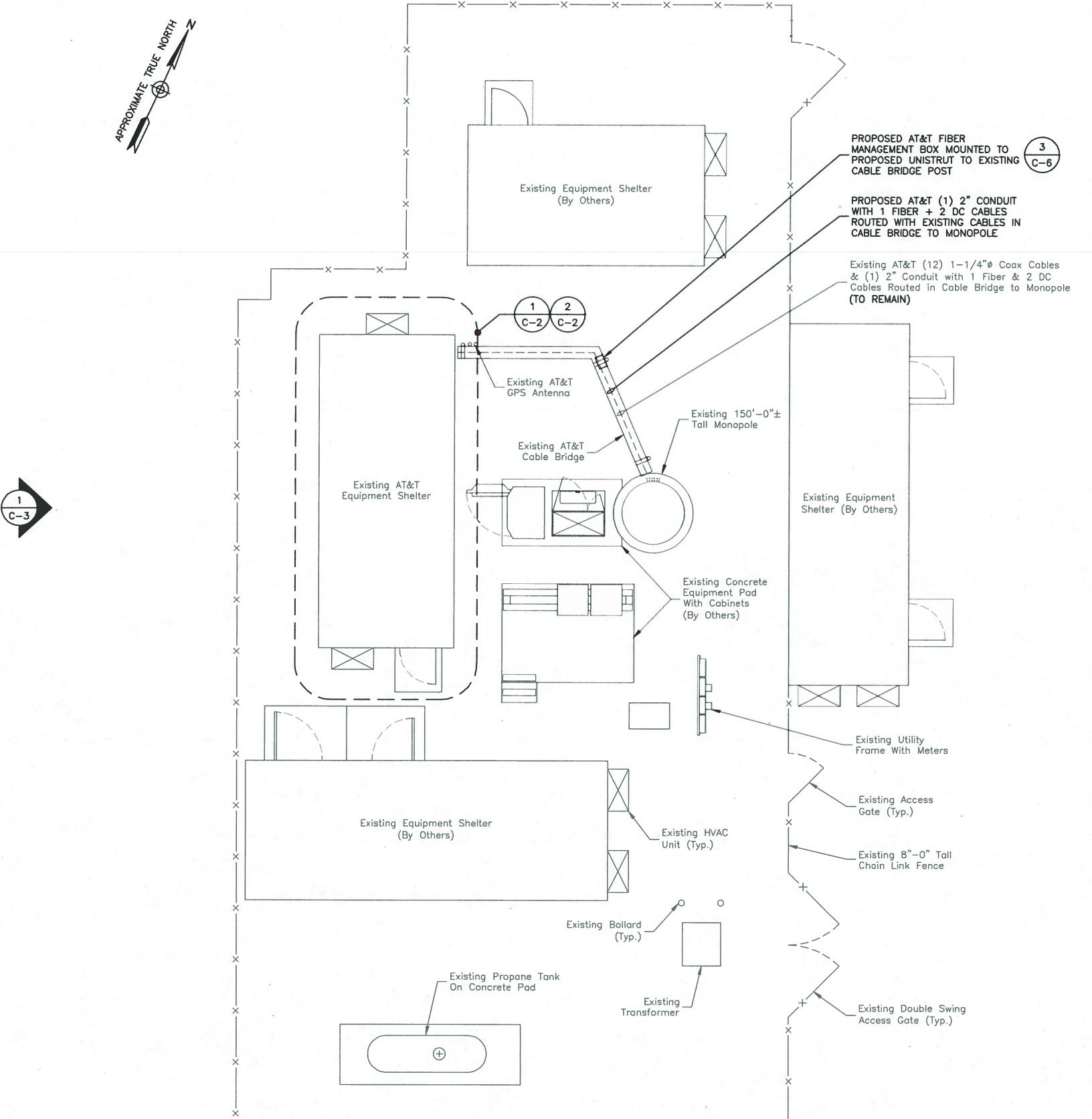
DRAWN BY:	BJR
REVIEWED BY:	BSH
CHECKED BY:	GHN
PROJECT NUMBER:	50055106
JOB NUMBER:	50093832
SITE ADDRESS:	

965 CONGRESS STREET  
FAIRFIELD, CT 06824

SHEET TITLE

## COMPOUND PLAN

SHEET NUMBER



## NOTES:

1. NORTH SHOWN AS APPROXIMATE.
  2. NOT ALL INFORMATION IS SHOWN FOR CLARITY.
  3. ALL PROPOSED EQUIPMENT, INCLUDING ANTENNAS, COAX, SURGE ARRESTORS, TMA'S, RRU'S, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS BY DEWBERRY ENGINEERS INC. DATED 01/29/19 & THE APPURTENANCE MOUNT ANALYSIS BY B+T GROUP DATED 02/08/19.
  4. COMPOUND PLAN BASED ON EXISTING PLANS BY CENTEK ENGINEERING DATED 09/29/16 & A SITE VISIT CONDUCTED BY DEWBERRY ENGINEERS INC. ON 11/28/18.

## **COMPOUND PLAN**

SCALE: 3/32"=1' FOR 11"x17"  
3/16"=1' FOR 22"x34"

1

A horizontal line representing a DNA segment. Above the line, four tick marks are labeled 0', 4', 8', and 12' from left to right. The segments between these labels represent the four nucleotide bases: adenine (A), thymine (T), cytosine (C), and guanine (G).

C-1

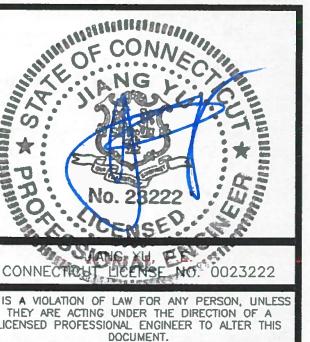
**CT2128**  
**FAIRFIELD**  
**GREENFIELD HILL**

**CONSTRUCTION DRAWINGS**

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REVIEWED BY: BSH  
CHECKED BY: GHN  
PROJECT NUMBER: 50055106  
JOB NUMBER: 50093832  
SITE ADDRESS:

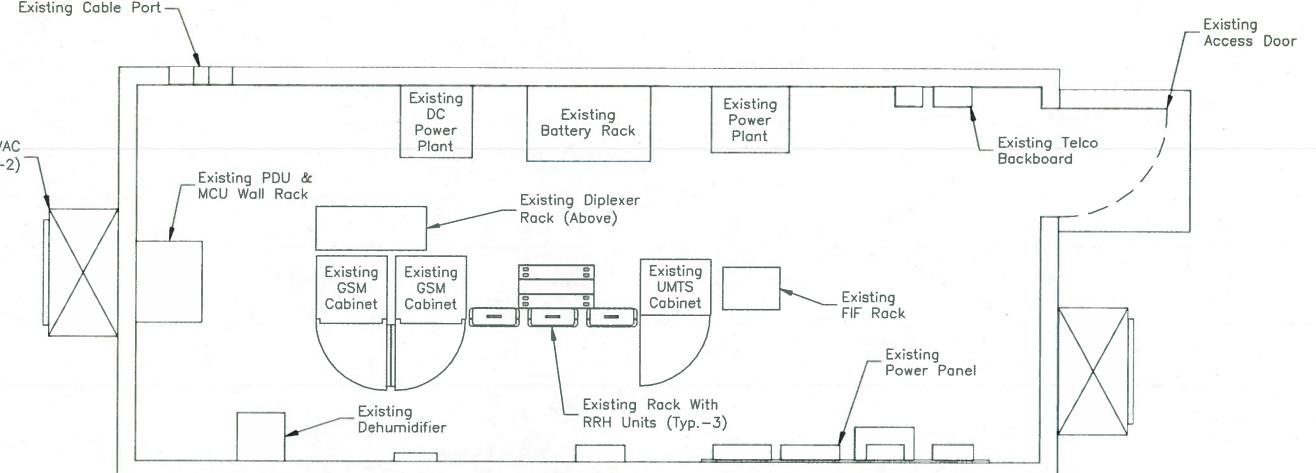
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SHEET TITLE

EXISTING & PROPOSED  
SHELTER LAYOUTS

SHEET NUMBER

APPROXIMATE TRUE NORTH



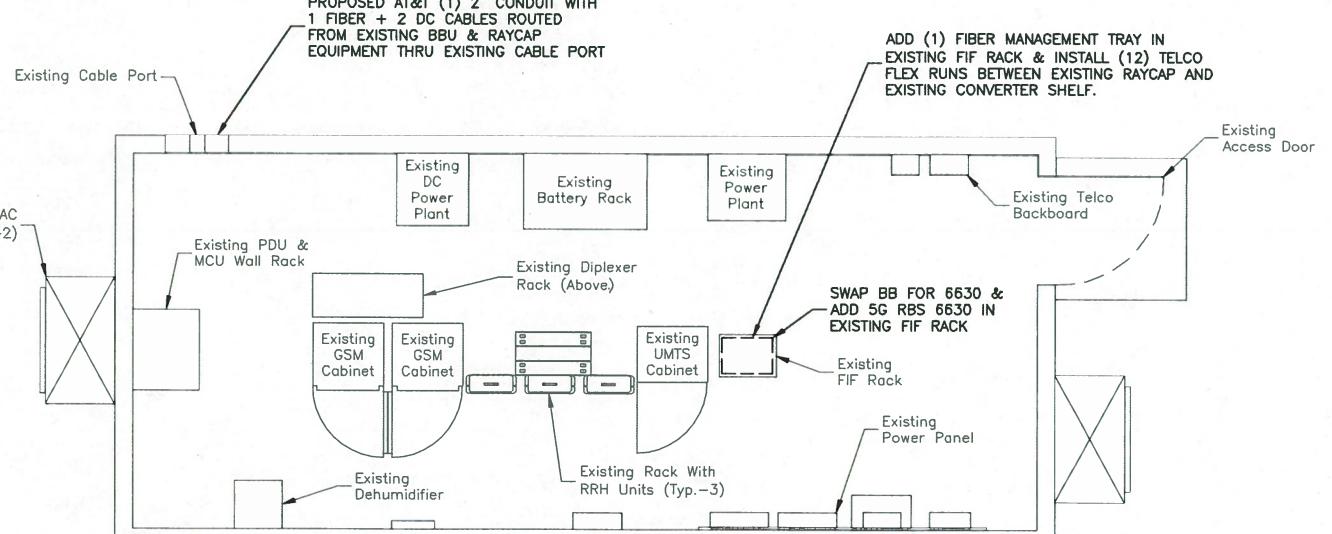
**EXISTING SHELTER LAYOUT**

SCALE: 3/16"=1' FOR 11"x17"  
3/8"=1' FOR 22"x34"

1

0' 2' 4' 6'

APPROXIMATE TRUE NORTH



**PROPOSED SHELTER LAYOUT**

SCALE: 1/8"=1' FOR 11"x17"  
1/4"=1' FOR 22"x34"

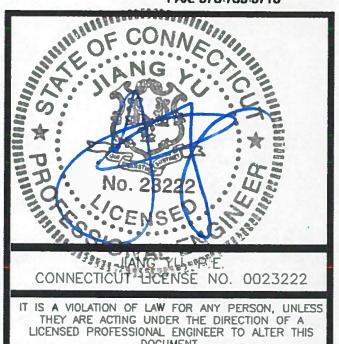
2

0' 2' 4' 8'

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REVIEWED BY: BSH  
CHECKED BY: GHN  
PROJECT NUMBER: 50055106  
JOB NUMBER: 50093832  
SITE ADDRESS:

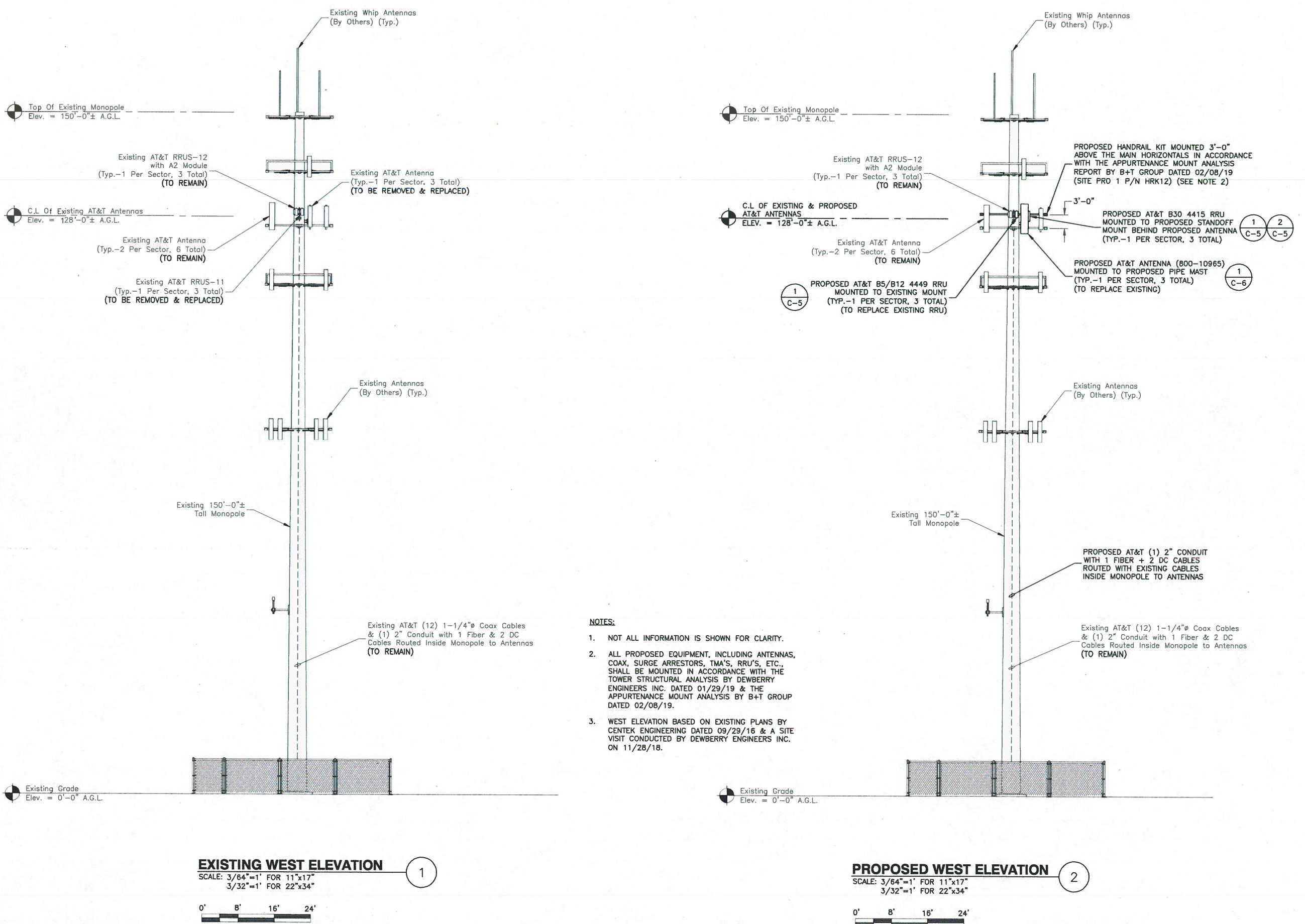
3965 CONGRESS STREET  
FAIRFIELD, CT 06824

SHEET TITLE:

EXISTING & PROPOSED  
WEST ELEVATIONS

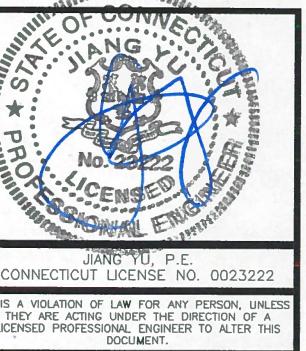
SHEET NUMBER:

C-3

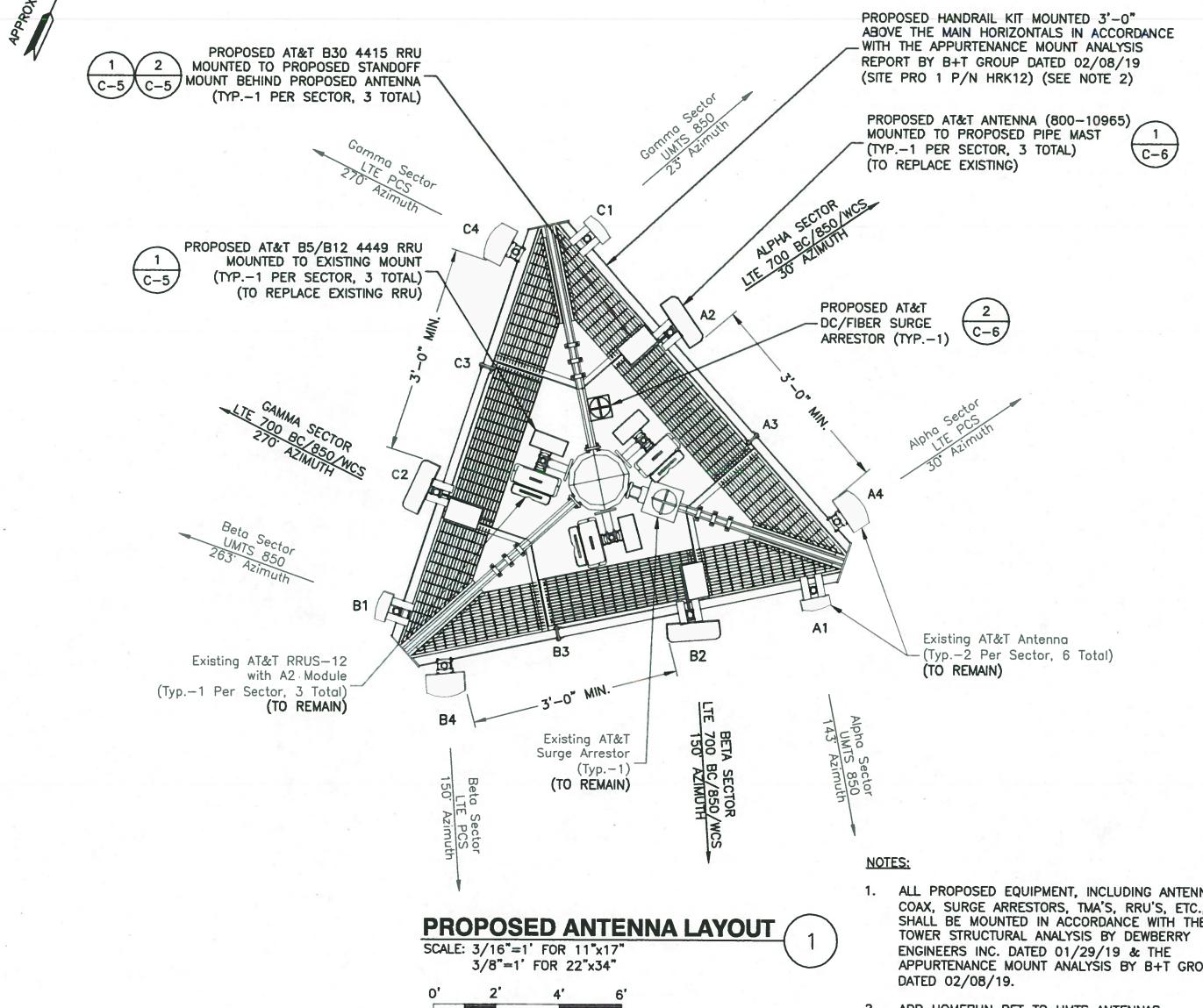
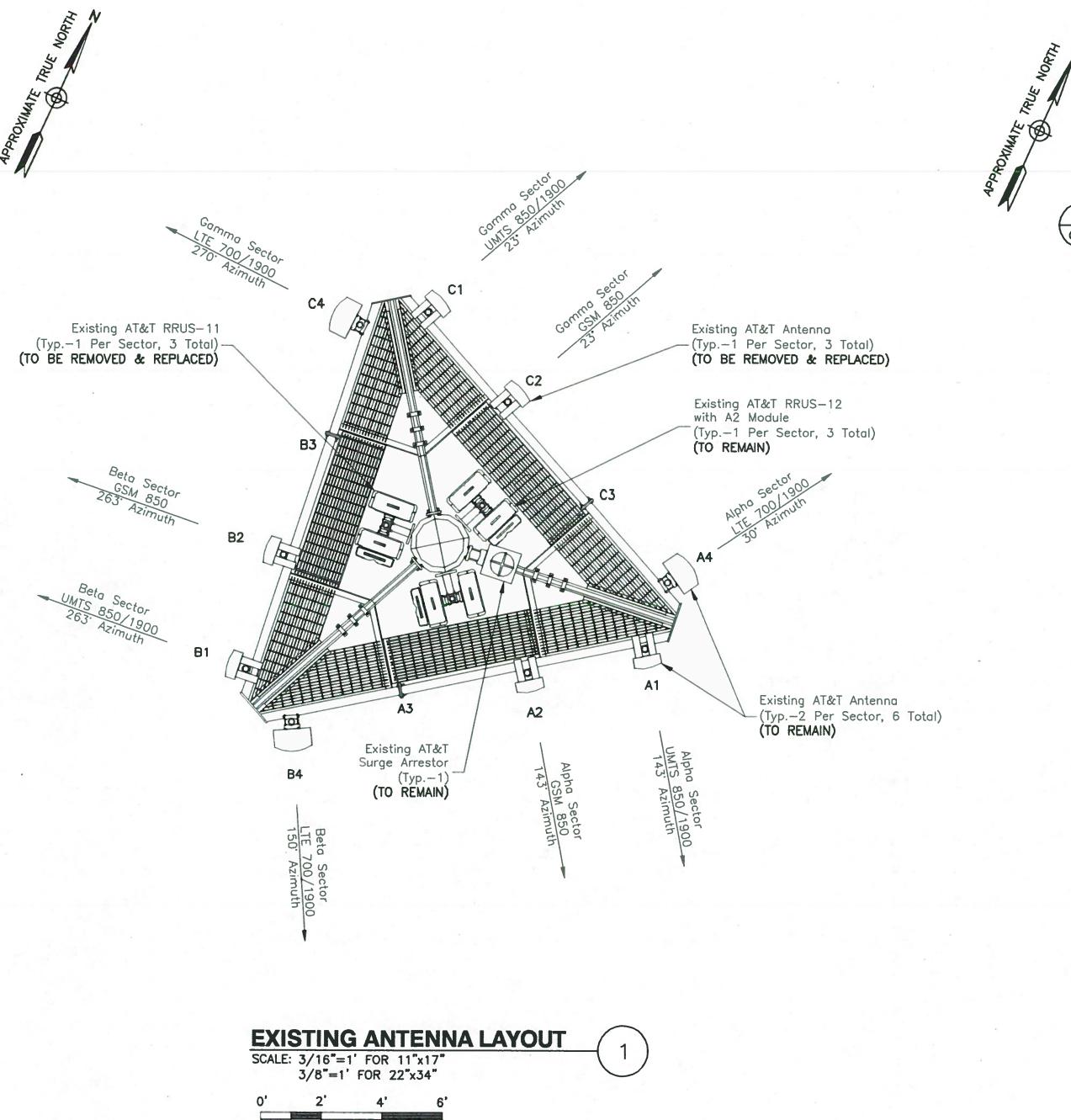


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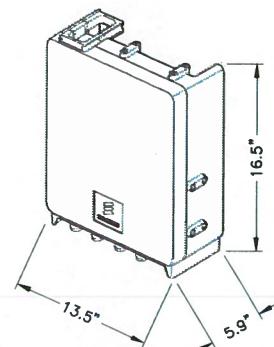
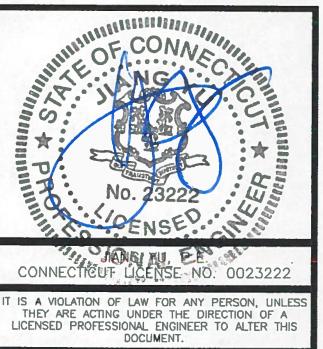
  
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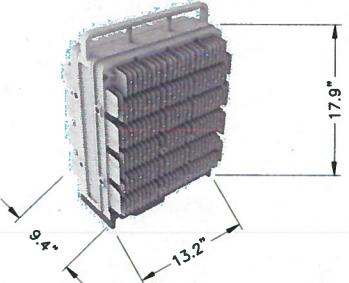
 SHEET TITLE  
 EXISTING & PROPOSED  
 ANTENNA LAYOUTS  
 SHEET NUMBER


**CT2128**  
**FAIRFIELD**  
**GREENFIELD HILL**
**CONSTRUCTION DRAWINGS**

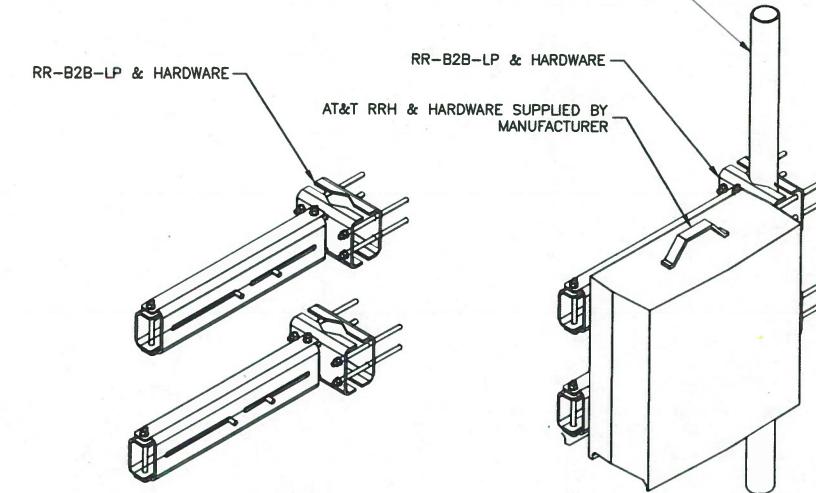
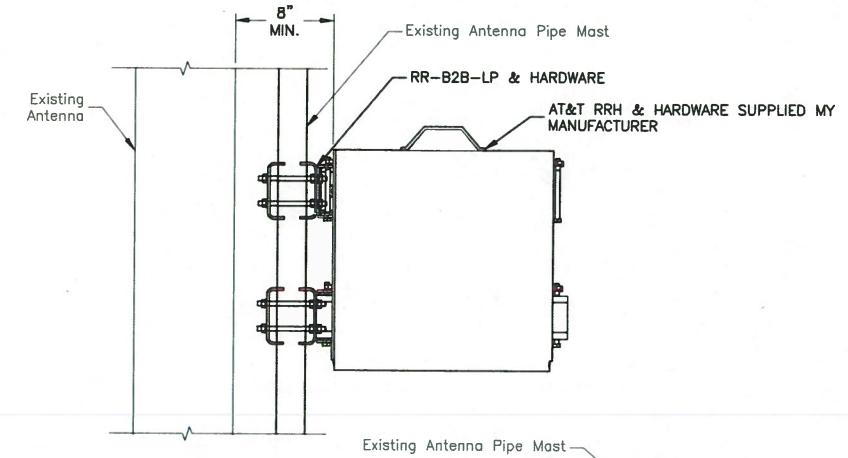
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ERICSSON RRUS-B30 4415



ERICSSON RRUS-B5/B12 4449

**SPECIFICATIONS:**  
 HEIGHT: 17.9"  
 WIDTH: 13.2"  
 DEPTH: 9.4"  
 WEIGHT: 70.4 LBS


- NOTES:**
1. 8" MIN. BETWEEN BACK OF ANTENNA & RRH UNIT.
  2. CONTRACTOR TO COMPLY WITH MANUFACTURER'S INSTRUCTIONS TO ENSURE THAT ALL RRH UNITS RECEIVE ELECTRICAL POWER WITHIN 24 HOURS OF BEING REMOVED FROM THE MANUFACTURER'S PACKAGING. DO NOT OPEN RRH UNITS IN THE RAIN.

**RRH DUAL BRACKET MOUNT DETAIL**

SCALE: N.T.S.

2

**REMOTE RADIO UNIT DETAIL**

SCALE: N.T.S.

1

**ANTENNA SCHEDULE**

SECTOR	EXISTING/PROPOSED	BAND	ANTENNA	ANTENNA CENTERLINE	AZIMUTH	TMA/DIPLEXER	RRU	FEEDER	SURGE ARRESTORS
A1	EXISTING	UMTS 850	POWERWAVE 7770	128°-0"±	143°	(2) POWERWAVE/LGP 21901 (2) 21401 (DB - 850 BYPASS)	-	(2) 1-1/4"Ø COAX + HOMERUN RET	
A2	PROPOSED	LTE 700 BC/850/WCS	KATHREIN 800-10965	128°-0"±	30°	-	(P) ERICSSON RRUS-B5/B12 4449 (P) ERICSSON RRUS-B30 4415	FIBER	
A3	-	-	-	-	-	-	-	-	
A4	EXISTING	LTE PCS	HPA-65R-BUU-H6	128°-0"±	30°		(E) ERICSSON RRUS-12 W/ A2 MODULE	FIBER/ (2) 1-1/4"Ø COAX	
B1	EXISTING	UMTS 850	POWERWAVE 7770	128°-0"±	263°	(2) POWERWAVE/LGP 21901 (2) 21401 (DB - 850 BYPASS)	-	(2) 1-1/4"Ø COAX + HOMERUN RET	
B2	PROPOSED	LTE 700 BC/850/WCS	KATHREIN 800-10965	128°-0"±	150°	-	(P) ERICSSON RRUS-B5/B12 4449 (P) ERICSSON RRUS-B30 4415	FIBER	
B3	-	-	-	-	-	-	-	-	
B4	EXISTING	LTE PCS	HPA-65R-BUU-H6	128°-0"±	150°	-	(E) ERICSSON RRUS-12 W/ A2 MODULE	FIBER/ (2) 1-1/4"Ø COAX	
C1	EXISTING	UMTS 850	POWERWAVE 7770	128°-0"±	23°	(2) POWERWAVE/LGP 21901 (2) 21401 (DB - 850 BYPASS)	-	(2) 1-1/4"Ø COAX + HOMERUN RET	
C2	PROPOSED	LTE 700 BC/850/WCS	KATHREIN 800-10965	128°-0"±	270°	-	(P) ERICSSON RRUS-B5/B12 4449 (P) ERICSSON RRUS-B30 4415	FIBER	
C3	-	-	-	-	-	-	-	-	
C4	EXISTING	LTE PCS	HPA-65R-BUU-H6	128°-0"±	270°	-	(E) ERICSSON RRUS-12 W/ A2 MODULE	FIBER/ (2) 1-1/4"Ø COAX	

 3965 CONGRESS STREET  
 FAIRFIELD, CT 06824

SHEET TITLE

 CONSTRUCTION  
 DETAILS I

SHEET NUMBER

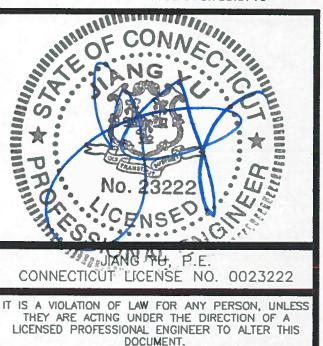
**CT2128  
FAIRFIELD  
GREENFIELD HILL**

**CONSTRUCTION DRAWINGS**

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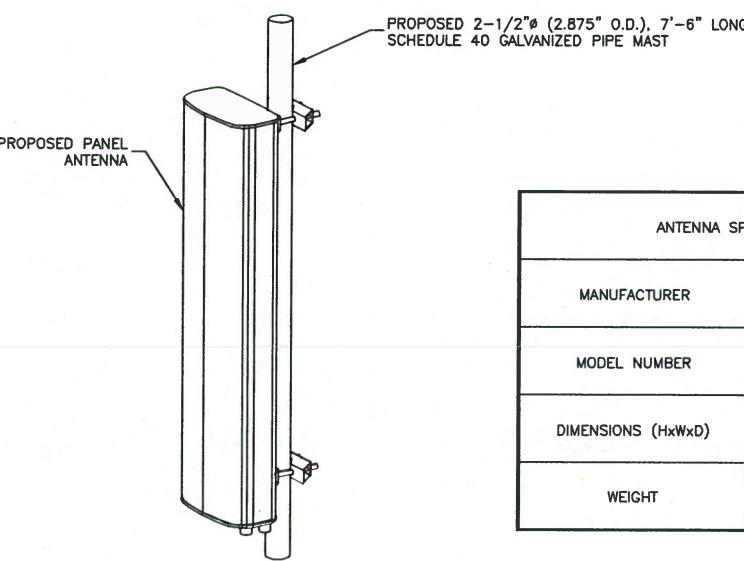
DRAWN BY: BJR  
REVIEWED BY: BSH  
CHECKED BY: GHN  
PROJECT NUMBER: 50055106  
JOB NUMBER: 50093832  
SITE ADDRESS:

3965 CONGRESS STREET  
FAIRFIELD, CT 06824

SHEET TITLE:

CONSTRUCTION  
DETAILS II

SHEET NUMBER:



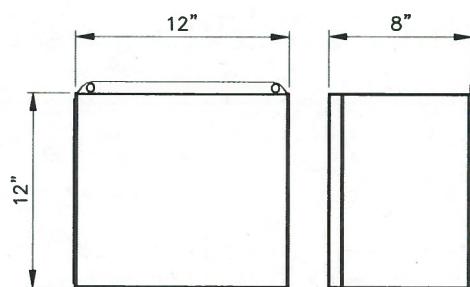
ANTENNA SPECIFICATIONS	
MANUFACTURER	KATHREIN
MODEL NUMBER	800-10965
DIMENSIONS (HxWxD)	78.7" x 20.0" x 6.9"
WEIGHT	108.6 LBS

- NOTES:
1. MOUNT ANTENNA PER MANUFACTURER'S RECOMMENDATIONS.
  2. WEIGHT INCLUDES MOUNTING BRACKETS.

**ANTENNA DETAIL**

SCALE: N.T.S.

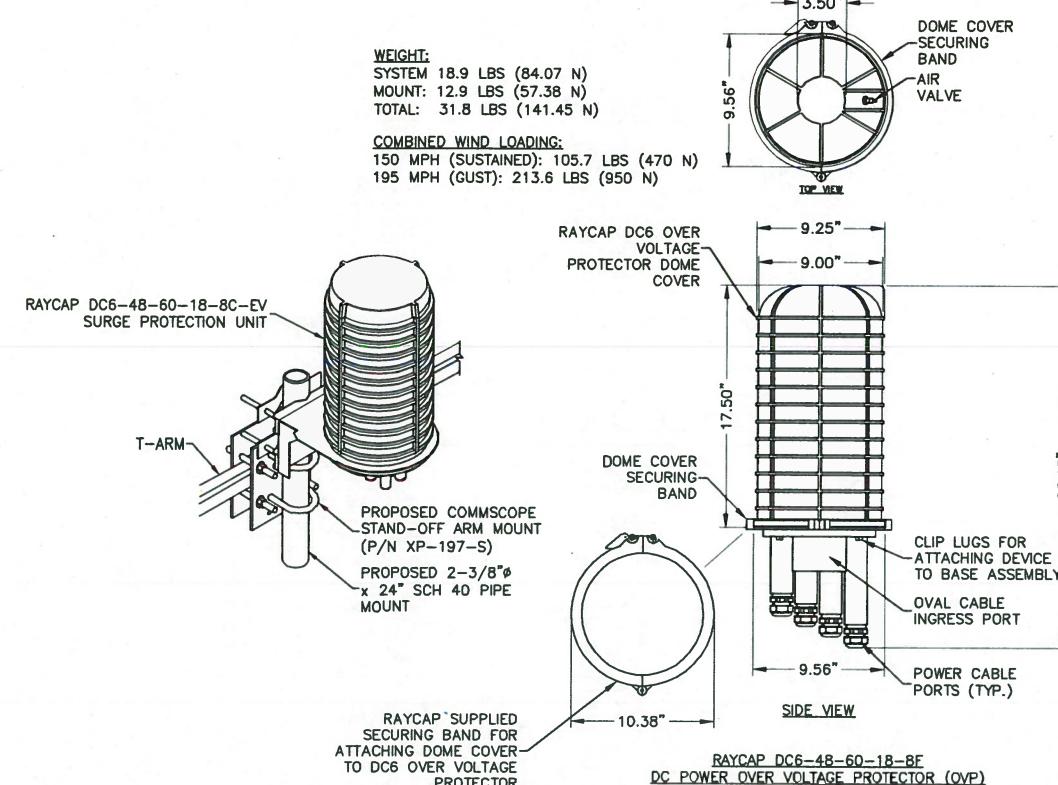
1



**FIBER MANAGEMENT BOX DETAIL**

SCALE: N.T.S.

3



**TOWER MOUNTED SURGE ARRESTOR DETAIL**

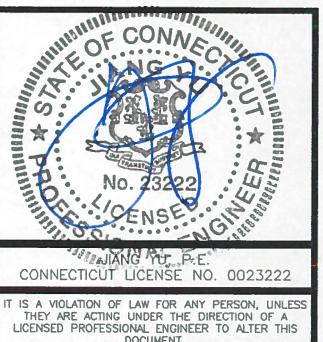
SCALE: N.T.S.

2

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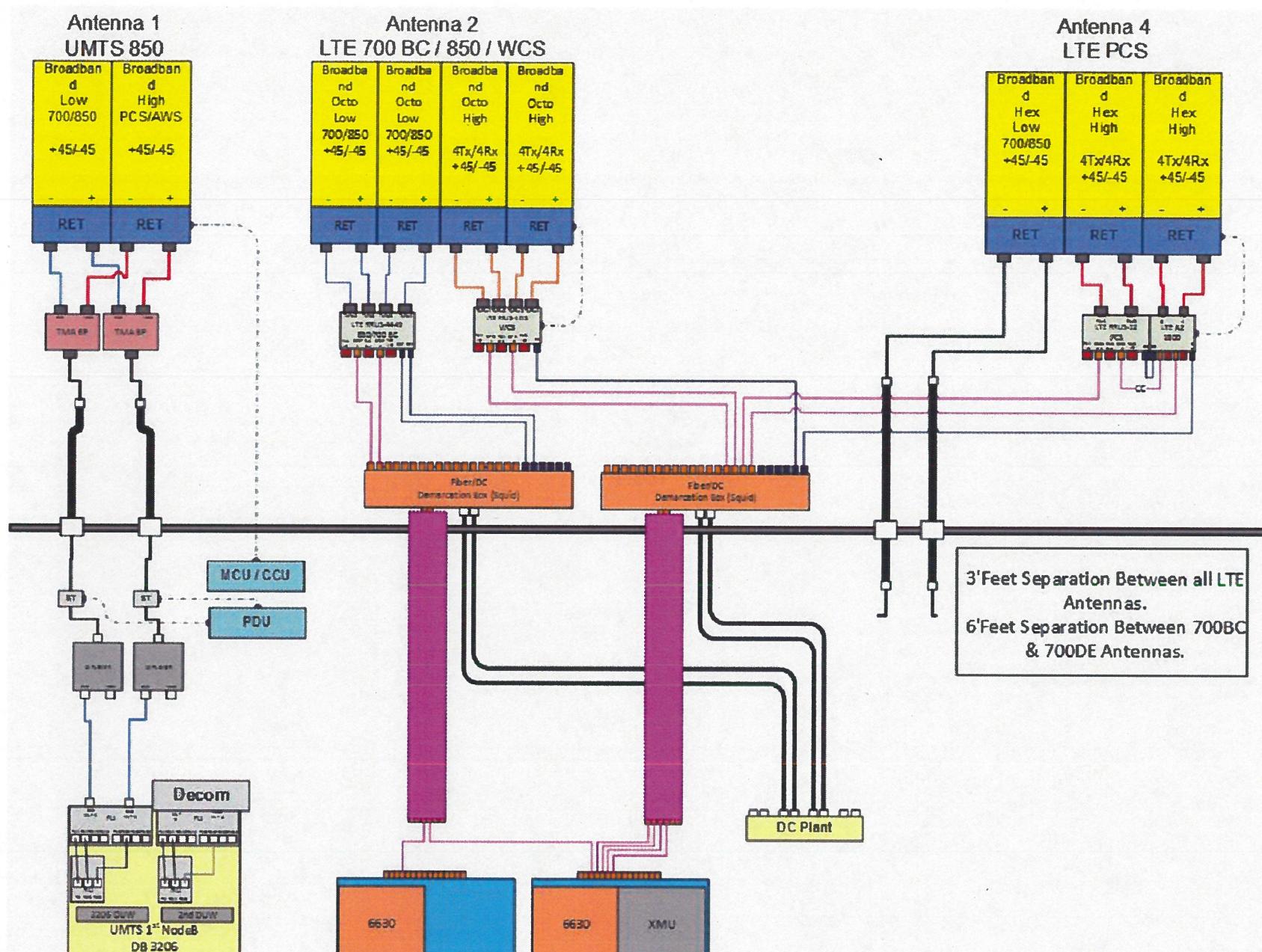
3965 CONGRESS STREET  
FAIRFIELD, CT 06824

**SHEET TITLE**

**PLUMBING DIAGRAM**

**SHEET NUMBER**

C-7



**PLUMBING DIAGRAM**

SCALE: N.T.S.

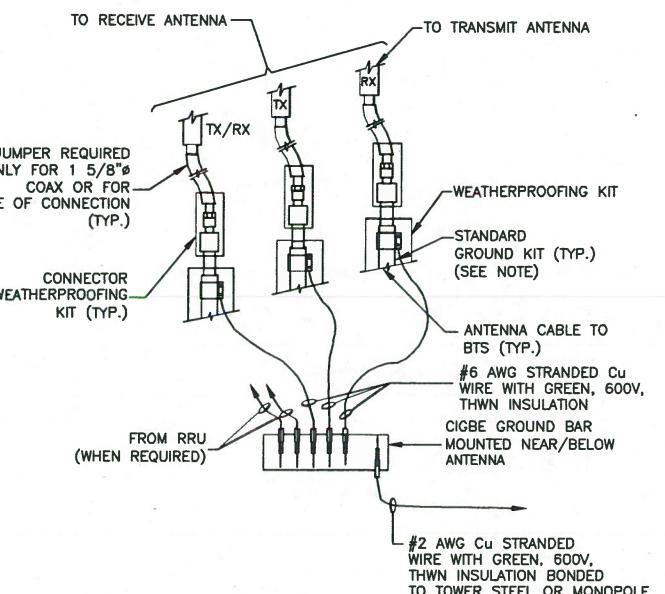
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**NOTES:**

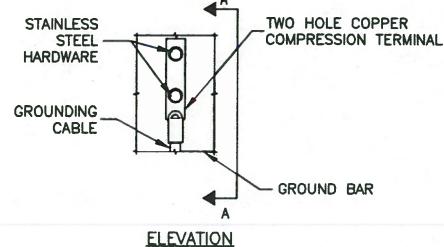
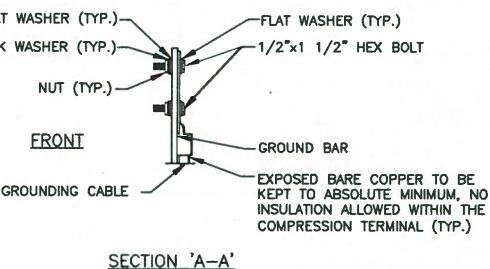
1. PLUMBING DIAGRAM BASED ON RFDS V.2.00 DATED 09/19/2018. CONFIRM FINAL PLUMBING DIAGRAM WITH THE LATEST RFDS.
2. ADD HOMERUN RET TO UMTS ANTENNAS.

**GROUNDING NOTES:**

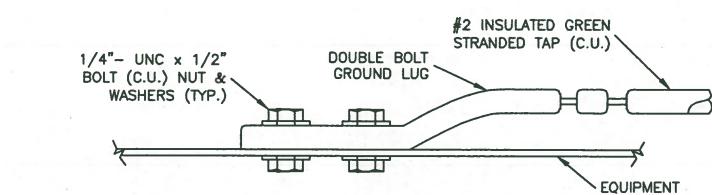
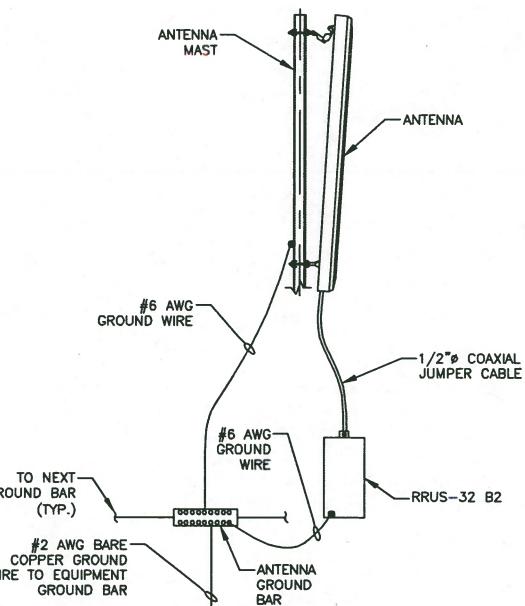
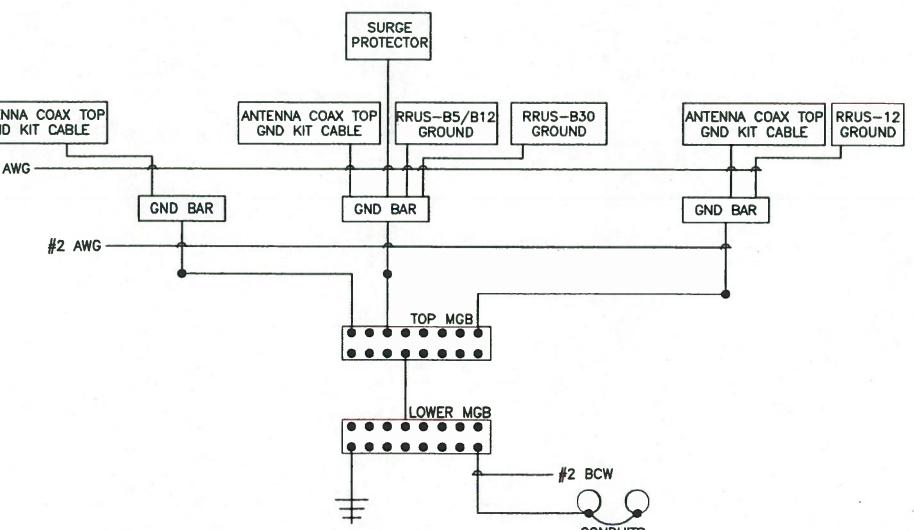
- THE CONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ). THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTNING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE CONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE ENGINEER FOR RESOLUTION.
- ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS. ALL AVAILABLE GROUNDING ELECTRODES SHALL BE CONNECTED TOGETHER IN ACCORDANCE WITH THE NEC.
- THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS. USE OF OTHER METHODS MUST BE PRE-APPROVED BY THE ENGINEER IN WRITING.
- THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS ON TOWER SITES AND 10 OHMS OR LESS ON ROOFTOP SITES. WHEN ADDING ELECTRODES, CONTRACTOR SHALL MAINTAIN A MINIMUM DISTANCE BETWEEN THE ADDED ELECTRODE AND ANY OTHER EXISTING ELECTRODE EQUAL TO THE BURIED LENGTH OF THE ROD. IDEALLY, CONTRACTOR SHALL STRIVE TO KEEP THE SEPARATION DISTANCE EQUAL TO TWICE THE BURIED LENGTH OF THE RODS.
- THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT.
- METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWG COPPER WIRE AND UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO TRANSMISSION EQUIPMENT.
- CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED. BACK-TO-BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
- ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED. IN ALL CASES, BENDS SHALL BE MADE WITH A MINIMUM BEND RADIUS OF 8 INCHES.
- EACH INTERIOR TRANSMISSION CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH 6 AWG STRANDED, GREEN INSULATED EQUIPMENT GROUND WIRE UNLESS NOTED OTHERWISE. EACH OUTDOOR CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER WIRE UNLESS NOTED OTHERWISE IN THE DETAILS.
- ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING, SHALL BE 2 AWG SOLID TIN-PLATED COPPER UNLESS OTHERWISE INDICATED.
- EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE. CONNECTIONS TO ABOVE GRADE UNITS SHALL BE MADE WITH EXOTHERMIC WELDS WHERE PRACTICAL OR WITH 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS. HIGH PRESSURE CRIMP CONNECTORS MAY ONLY BE USED WITH WRITTEN PERMISSION FROM SAI MARKET REPRESENTATIVE.
- EXOTHERMIC WELDS SHALL BE PERMITTED ON TOWERS ONLY WITH THE EXPRESS APPROVAL OF THE TOWER MANUFACTURER OR THE CONTRACTOR'S STRUCTURAL ENGINEER.
- ALL WIRE TO WIRE GROUND CONNECTIONS TO THE INTERIOR GROUND RING SHALL BE FORMED USING HIGH PRESS CRIMPS OR SPLIT BOLT CONNECTORS WHERE INDICATED IN THE DETAILS.
- ON ROOFTOP SITES WHERE EXOTHERMIC WELDS ARE A FIRE HAZARD COPPER COMPRESSION CAP CONNECTORS MAY BE USED FOR WIRE TO WIRE CONNECTORS. 2 HOLE MECHANICAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS SHALL BE USED FOR CONNECTION TO ALL ROOFTOP TRANSMISSION EQUIPMENT AND STRUCTURAL STEEL.
- COAX BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR USING TWO-HOLE MECHANICAL TYPE BRASS CONNECTORS AND STAINLESS STEEL HARDWARE.
- APPROVED ANTICORROSION COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
- MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- BOND ALL METALLIC OBJECTS WITHIN 6 FT OF THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER GROUND CONDUCTOR. DURING EXCAVATION FOR NEW GROUND CONDUCTORS, IF EXISTING GROUND CONDUCTORS ARE ENCOUNTERED, BOND EXISTING GROUND CONDUCTORS TO NEW CONDUCTORS.
- GROUND CONDUCTORS USED IN THE FACILITY GROUND AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC PLASTIC CONDUIT SHALL BE USED, WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (E.G., NON-METALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT WITH LISTED BONDING FITTINGS.


**NOTE:**

- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

**CONNECTION OF GROUND WIRES  
TO GROUNDING BAR (CIGBE)**
**1**

**SECTION 'A-A'**

**NOTES:**

- DOUBLING UP OR STACKING OF CONNECTIONS IS NOT PERMITTED.
- OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

**TYPICAL GROUND BAR  
MECHANICAL CONNECTION DETAIL**
**SCALE: N.T.S.**

**CONNECTION TO EQUIPMENT DETAIL**
**SCALE: N.T.S.**

**TYPICAL ANTENNA  
GROUNDING DETAIL**
**SCALE: N.T.S.**
**4**

**NOTES:**

- BOND ANTENNA GROUNDING KIT CABLE TO TOP CIGBE.
- BOND ANTENNA GROUNDING KIT CABLE TO BOTTOM CIGBE.
- SCHEMATIC GROUNDING DIAGRAM IS TYPICAL FOR EACH SECTOR.
- GROUND ALL EQUIPMENT PER MANUFACTURER RECOMMENDATIONS.

**SCHEMATIC GROUNDING DIAGRAM**
**SCALE: N.T.S.**
**5**

**at&t**  
500 ENTERPRISE DRIVE SUITE 3A  
ROCKY HILL, CT 06067

**SAI**  
12 INDUSTRIAL WAY  
SALEM, NH 03079

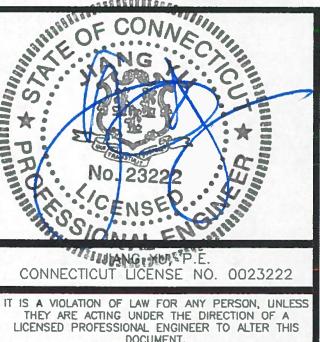
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REVIEWED BY: BSH  
CHECKED BY: GHN  
PROJECT NUMBER: 50055106  
JOB NUMBER: 50093832  
SITE ADDRESS:

3965 CONGRESS STREET  
FAIRFIELD, CT 06824

SHEET TITLE  
GROUNDING NOTES  
& DETAILS

SHEET NUMBER

E - 1

## Tower Analysis Report For a 150 ft. Monopole Tower

Site Name: CT2128  
Site Address: 3965 Congress Street  
Fairfield, CT 06824

*Prepared for:*  
**SAI Communications, Inc.**  
12 Industrial Way  
Salem, NH 03079

January 29, 2019

*Prepared by:*  
**Dewberry Engineers Inc.**  
600 Parsippany Road  
Parsippany, NJ 07054  
Dewberry Project Number: 50093832

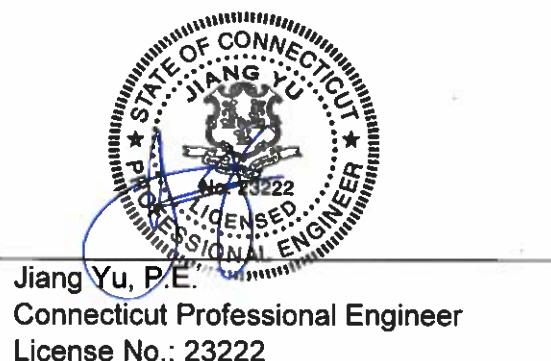
Tower Controlling Member	% Capacity	Pass/Fail
Tower Shaft	62.4	Pass
Tower base Components	52.9	Pass
Tower Foundation	-	Pass

Tower/Foundation Previously Reinforced?	YES <input type="checkbox"/> / NO <input checked="" type="checkbox"/>
Previous Reinforcement Verified?	YES <input type="checkbox"/> / NO <input checked="" type="checkbox"/> Date: <u>N/A</u>
Reinforcement Required?	YES <input type="checkbox"/> / NO <input checked="" type="checkbox"/>

Prepared by:

  
Deep A. Patel  
Graduate Engineer

Reviewed by:



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SAI for AT&T  
Site Name: CT2128  
Project No.: 50093832  
January 29, 2019

## 1.0 INTRODUCTION AND PROJECT SUMMARY

The objective of this report is to provide a structural analysis for the existing 150 ft. tall monopole located in Fairfield, Connecticut to determine the structural capacity of the structure with the existing & proposed equipment. The telecommunication upgrade is proposed by AT&T and managed by SAI Communications, Inc.

Please refer to the appendices for the structural package regarding the structural analysis.

## 2.0 CODES, STANDARDS, AND REFERENCES

The structure was analyzed and the proposed installation designed per the provisions of the following Codes and Standards:

- *2018 Connecticut State Building Code – Amendments to IBC 2015*
- *International Building Code (IBC) 2015, International Code Council.*
- *TIA-222-G-4, Structural Standard for Antenna Supporting Structures and Antennas*
- American Society of Civil Engineers ASCE 7-10 *Minimum Design Loads for Buildings and Other Structure.*

The following site-specific design parameters were considered in this analysis per the provisions of TIA-222-G:

Risk Category:	II
Exposure Category:	B
Design Basic Wind Speed:	95 mph (converted from 122 mph)
Serviceability Wind Speed:	60 mph

*Eqn. 16-33, IBC 2015, NJ Edition*  
*Sect. 2.8.3, TIA*

The tower geometry, member sizes, existing appurtenance loading, and foundation design loading were referenced from the following reports, all of which can be found in appendix B:

- *Structural Analysis by Centek Engineering Inc. dated August 30, 2016*
- *CT2128 Construction Drawings by Centek Engineering Inc. dated September 29, 2016*

SAI for AT&T  
 Site Name: CT2128  
 Project No.: 50093832  
 January 29, 2019

### 3.0 EXISTING AND PROPOSED TOWER LOADING

#### 3.1 Existing Antenna Loading & Cable Information:

CARRIER	ELEV. (ft.)	QTY.	APPURTENANCES DESCRIPTION	FEEDLINE
Town	149	2	10 ft Dipole	(3) 1-5/8" coax
		1	DB810K	
Nextel	149	3	DB844H90E-XY	(12) 1-5/8" coax
		3	Valmont T-Arm	
Sprint	138	3	APXVSPP18-C-A20	(3) Hyrbiflex cables
		3	FD-RRH 4x45 1900	
		3	FD-RRH 2x50 800	
		1	13' Platform w/Rails	
		3	RRUS-11	
AT&T	129	3	RRUS-12	(12) 1-1/4" coax (1) Fiber cable
		3	A2	
		1	DC6-48-60-18-8F Surge Arrestor	
		1	Valmont Uni-Tri Bracket	
		6	7770.00*	
	127	3	HPA-65R-BUU-H6	
		12	LGP214nn TMA**	
		1	Valmont 13' Low Profile Platform	
T-Mobile	113	3	APX16DWV-16DWV-S-E-ACU	(12) 1-1/4" coax
		6	10"x8"x3" TMA	
		1	13' Platform w/Rails	
Town	104	4	4'-6" Standoff	(4) 7/8" coax
		1	1142-2B	
		2	ASPA685	
		1	DB222	
Verizon	80	6	DB846F65ZAXY	(12) 1-5/8" coax (1) 1-5/8" fiber cable
		3	BXA-171063/8BF	
		3	BXA-70063/6CF	
		6	FD9R6004/2C-E3 Diplexer	
		3	BXA-171063/12CF	
		3	RRH2x40-AWS	
		1	DB-T1-6Z-8AB-0Z	
	78	1	Valmont 13' Low Profile Platform	
		1	Stand-off	
		1	GPS	

(\*) 6 to be removed.

(\*\*) 3 to be removed.

SAI for AT&T  
 Site Name: CT2128  
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### 3.2 Proposed Antenna Loading & Cable Information (AT&T):

CARRIER	ELEV. (ft.)	QTY.	APPURTEANCES DESCRIPTION	FEEDLINE
AT&T	127	3	<b>800-10965</b>	(1) Fiber Cable
		3	<b>RRH B5/B12 4449</b>	
		3	<b>RRH 4415 B30</b>	
		1	<b>DC/Fiber Squid</b>	

### 3.3 Final Configuration of Antennas & Equipment Information (AT&T):

CARRIER	ELEV. (ft.)	QTY.	APPURTEANCES DESCRIPTION	FEEDLINE
AT&T	129	3	A2	(12) 1-1/4" coax (2) Fiber cables
		3	RRUS-11	
		3	RRUS-12	
		1	DC6-48-60-18-8F Surge Arrestor	
		1	Valmont Uni-Tri Bracket	
	127	6	7770.00*	
		3	HPA-65R-BUU-H6	
		12	LGP214nn TMA**	
		3	<b>800-10965</b>	
		3	<b>RRH B5/B12 4449</b>	
		3	<b>RRH 4415 B30</b>	
		1	<b>DC/Fiber Squid</b>	
	125	1	Valmont 13' Low Profile Platform	

### 3.4 Method:

tnxTower, a commercially available engineering software program, was used to create a theoretical mathematical model of the tower members and calculate primary member stresses under various loading conditions. Selected output from the analysis is included in Appendix A.

SAI for AT&T  
 Site Name: CT2128  
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 January 29, 2019

## 4.0 TOWER ANALYSIS RESULTS SUMMARY

### 4.1 Tower Structure Results

**Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail
L1	150 - 95.83	Pole	TP33.469x23.61x0.281	1	-17002.30	1938050.00	36.9	Pass
L2	95.83 - 47.83	Pole	TP41.644x31.9661x0.375	2	-31280.80	3318110.00	54.3	Pass
L3	47.83 - 30	Pole	TP41.139x39.7709x0.438	3	-40294.10	4142390.00	62.4	Pass
L4	30 - 0	Pole	TP49.6x41.139x0.58	4	-40321.20	5583380.00	46.6	Pass
Summary								
Pole (L3) 62.4 Pass								
Base Plate 52.9 Pass								
RATING = <b>62.4</b> Pass								

Table above displays the summary of the ratio (as the percentage) of force in the member to their capacities. Values greater than 100% indicate the maximum force in the member exceeds its capacity.

\*Note: Capacities up to 105% are considered acceptable (where applicable)

### 4.2 Foundation Results

The table below displays the previous foundation design reactions according to Centek Engineering Inc.

Reactions	Previous Reactions Centek Engineering Inc.**	Factored Reactions*
Axial	44 kip	59.4 kip
Shear	42 kip	56.7 kip
Moment	3989 kip-ft	5385.2 kip-ft

\* Reactions obtained from Centek Engineering Inc analysis multiplied by a factor of 1.35

The table below displays the foundation design reactions obtained from this analysis.

Reactions	Current Analysis Reactions
Axial	101 kip
Shear	32.4 kip
Moment	3020.6 kip-ft

Previous Centek Engineering Caisson analysis determined the moment capacity of the tower foundation to be at 61.9%. The Dewberry Engineer's analysis determined the moment reaction to be 3020.6 kip-ft, which is less than the previous moment reaction calculated by Centek Engineering. Therefore, the foundation is adequate in moment capacity.

Previous Centek Engineering Caisson analysis determined the lateral deflection to be 0.37 in. The Dewberry analysis determined the shear force to be 32.5 kip and moment to be 3020.6 kip-ft, both of which are less than the previous shear force and moment calculated by Centek Engineering. Therefore, the foundation is adequate for lateral deflection.

## 5.0 CONCLUSIONS, COMMENTARY, AND RECOMMENDATIONS

After analysis, it was determined that the existing tower structure is adequate to support the proposed telecommunication upgrade. Additionally, the existing reinforced foundation is adequate to support the proposed installation.

This engineering analysis is based upon the theoretical capacity of the structure. It is not a condition assessment of the tower and its foundation. Dewberry Engineers Inc. reserves the right to add to or modify this report if more information becomes available. The conclusions reached by Dewberry Engineers Inc. in this report are only applicable to the previously mentioned existing structural elements supporting the proposed wireless telecommunications installation. The results of this report are based on the assumption that existing structural elements have been installed per the original design documents, have been well maintained and are uncompromised. This report does not imply that a thorough inspection of the existing structure has been performed. Any deviation of the support condition, loading, location, placement, equipment configuration, etc, will require Dewberry Engineers Inc. to generate an additional structural analysis.

## 6.0 ASSUMPTIONS

This feasibility structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. Dewberry Engineers Inc. has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analysis of the tower only.
5. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
6. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
7. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and Dewberry Engineering Inc. should be allowed to review any new information to determine its effect on the structural integrity of the tower.

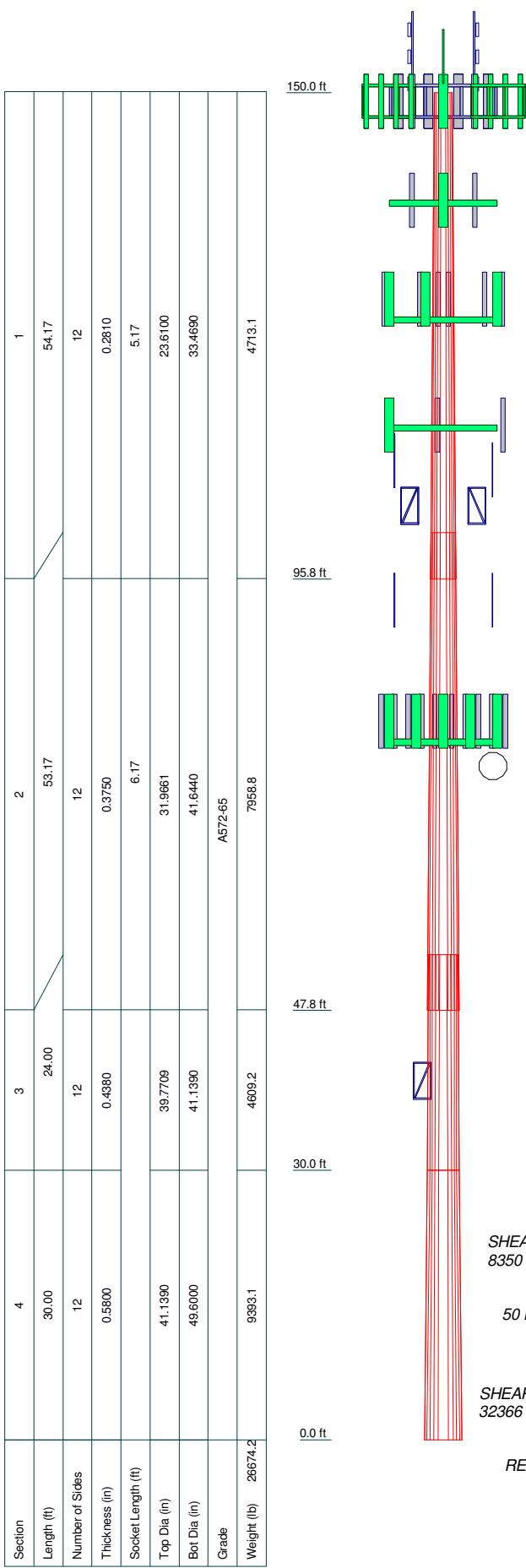
## **7.0 DISCLAIMER OF WARRANTIES**

The engineering services rendered by Dewberry Engineers Inc. in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

Dewberry Engineers Inc. does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. Dewberry Engineers Inc. provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to calculate the structural integrity for the existing tower under existing and proposed loadings.

Dewberry Engineers Inc. makes no warranties, expresses and/or implied in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. Dewberry will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of Dewberry pursuant to this report will be limited to the total fee received for preparation of this report

## **APPENDIX A**



## **DESIGNED APPURTENANCE LOADING**

Type	Elevation	Type	Elevation
10-ft Dipole (Town)	149	Valmont 13' Low Profile Platform (AT&T Existing)	125
10-ft Dipole (Town)	149		
DB810K (Town)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
Valmont T-Arm (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
Valmont T-Arm (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
Valmont T-Arm (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
APXVSPP18-C-A20 (Sprint Existing)	138	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
APXVSPP18-C-A20 (Sprint Existing)	138	13' Platform w/Rails (T-Mobile Existing)	113
APXVSPP18-C-A20 (Sprint Existing)	138	4'-6" Standoff (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	4'-6" Standoff (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	1142-2B (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	ASPA685 (Town - Existing)	104
FD-RRH 2x50 800 (Sprint Existing)	138	DB222 (Town - Existing)	104
FD-RRH 2x50 800 (Sprint Existing)	138	ASPA685 (Town - Existing)	104
FD-RRH 2x50 800 (Sprint Existing)	138	4'-6" Standoff (Town - Existing)	104
13' Platform w/Rails (Sprint Existing)	138	4'-6" Standoff (Town - Existing)	104
RRUS-11 (AT&T Existing)	129	BXA-70063/6CF (Verizon - Existing)	80
RRUS-11 (AT&T Existing)	129	DB846F65ZAXY (Verizon - Existing)	80
RRUS-11 (AT&T Existing)	129	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
RRUS-12 (AT&T Existing)	129		
RRUS-12 (AT&T Existing)	129	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
RRUS-12 (AT&T Existing)	129	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
A2 (AT&T Existing)	129	BXA-171063-12CF (Verizon - Existing)	80
A2 (AT&T Existing)	129	BXA-171063-12CF (Verizon - Existing)	80
A2 (AT&T Existing)	129	BXA-171063-12CF (Verizon - Existing)	80
DC6-48-60-18-8F Surge Arrestor (AT&T Existing)	129	RRH2x40-AWS (Verizon - Existing)	80
Valmont Uni-Tri Bracket (AT&T Existing)	129	RRH2x40-AWS (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	RRH2x40-AWS (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Existing)	127	RRH2x40-AWS (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	DB-T1-6Z-8AB-0Z (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Existing)	127	BXA-70063/6CF (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	DB846F65ZAXY (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Existing)	127	DB846F65ZAXY (Verizon - Existing)	80
(2) LGP214nn TMA (AT&T Existing)	127	BXA-171063/8BF (Verizon Existing)	80
(2) LGP214nn TMA (AT&T Existing)	127	BXA-70063/6CF (Verizon - Existing)	80
(2) LGP214nn TMA (AT&T Existing)	127	DB846F65ZAXY (Verizon - Existing)	80
800-10965	127	DB846F65ZAXY (Verizon - Existing)	80
RRH B5/B12 4449	127	BXA-171063/8BF (Verizon Existing)	80
RRH 4415 B30	127	DB846F65ZAXY (Verizon - Existing)	80
DC/Fiber Squid	127	BXA-171063/8BF (Verizon Existing)	80
800-10965	127	Valmont 13' Low Profile Platform (Verizon - Existing)	78
RRH B5/B12 4449	127	GPS (Existing)	40
RRH 4415 B30	127	Standoff	40
800-10965	127		
RRH B5/B12 4449	127		
RRH 4415 B30	127		

#### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

## ALL REACTIONS ARE FACTOREL

## TOWER DESIGN NOTES

**TOWER DESIGN NOTES**

**AXIAL 101002 lb**

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 95 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase 8 in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.

**TORQUE 892 lb**

**50 mph WIND - 0.750 ft AXIAL 54225 lb**

7. Topographic Category 1 with Crest Height of 0.00 ft
8. Weld together tower sections have flange connections.
9. Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications.
10. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
11. Welds are fabricated with ER-70S-6 electrodes.
12. TOWER RATING: 62.4%

**SHEAR 8350 lb**

**SHEAR 32366 lb**

**TORQUE 1619 lb**

**REACTIONS - 95 mph WIND**

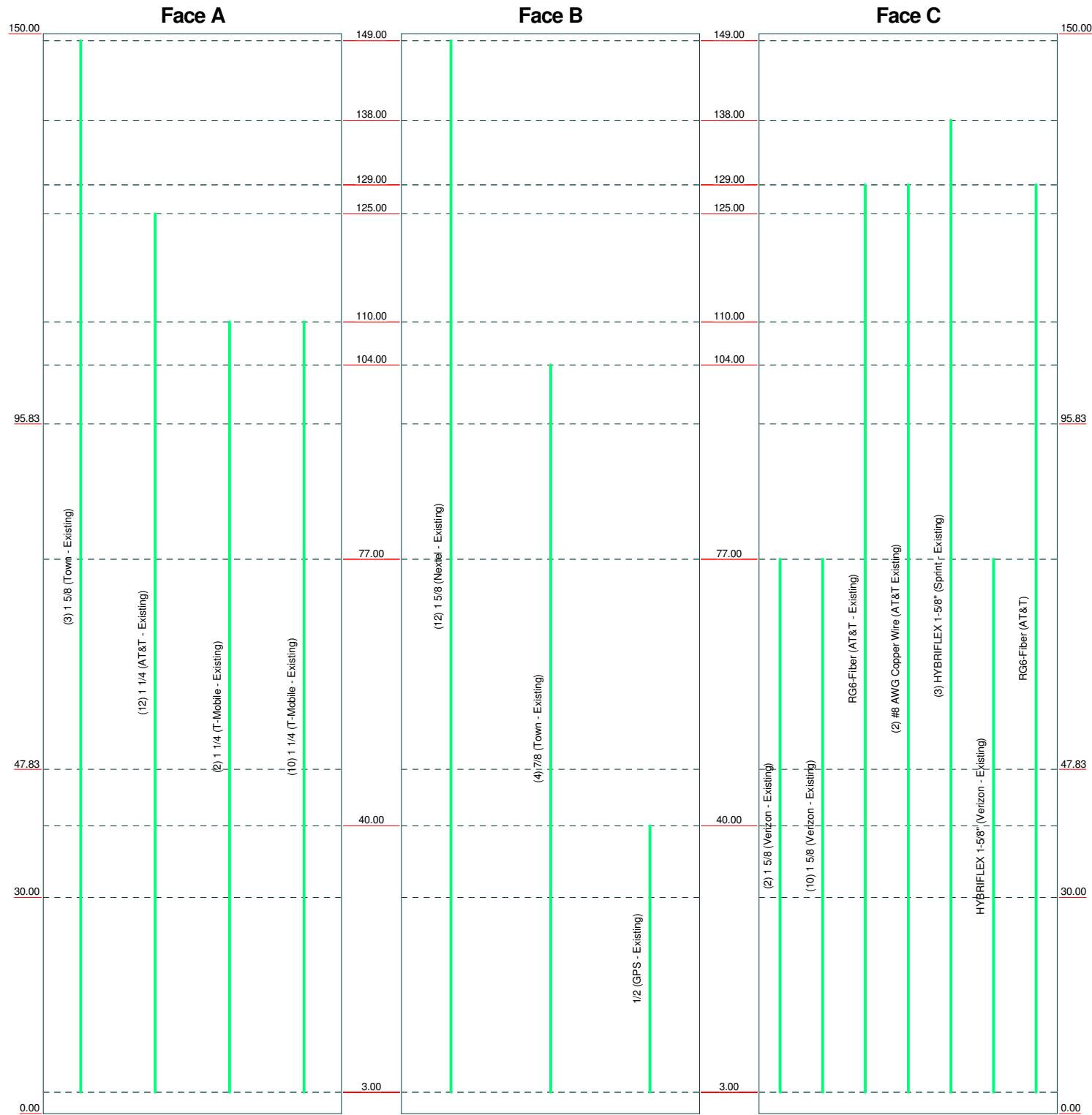
*TORQUE 1619 IL<sup>12</sup>. TO  
REACTIONS - 95 mph WIND*

**Dewberry**  
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FAX: (973) 739-9710

Job: **50093832**  
Project: **CT2128**  
Client: SAI/AT&T Drawn by: DAP App'd:  
Code: TIA-222-G Date: 01/25/19 Scale: NTS  
Path: C:\50055106\50093832\Adm\Reports\TA\lnrx50055106.. CT2128-TA.erl  
Dwg No. E-1

# Feed Line Distribution Chart 0' - 150'

Round      Flat      App In Face      App Out Face      Truss Leg



**Dewberry**  
600 Parsippany Road, Suite 301  
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Job: **50093832**  
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Code: TIA-222-G Date: 01/25/19 Scale: NTS  
Path: O:\500551\06\50093832\Adm\Reports\TA\lnx\50055106 - CT2128-TA.er Dwg No. E-7

<b>tnxTower</b>  <b>Dewberry</b> <i>600 Parsippany Road, Suite 301</i> <i>Parsippany, NJ 07054</i> <i>Phone: (973) 739-9400</i> <i>FAX: (973) 739-9710</i>	<b>Job</b>	50093832	<b>Page</b>
	<b>Project</b>	CT2128	<b>Date</b> 13:56:15 01/25/19
	<b>Client</b>	SAI/AT&T	<b>Designed by</b> DAP

## Tower Input Data

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Fairfield County, Connecticut.

ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).

Basic wind speed of 95 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

Weld together tower sections have flange connections..

Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications..

Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..

Welds are fabricated with ER-70S-6 electrodes..

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |                                     |                                      |   |
|-------------------------------------|--------------------------------------|---|
| Consider Moments - Legs             | Distribute Leg Loads As Uniform      | Use ASCE 10 X-Brace Ly Rules            |
| Consider Moments - Horizontals      | Assume Legs Pinned                   | Calculate Redundant Bracing Forces      |
| Consider Moments - Diagonals        | ✓ Assume Rigid Index Plate           | Ignore Redundant Members in FEA         |
| Use Moment Magnification            | Use Clear Spans For Wind Area        | SR Leg Bolts Resist Compression         |
| ✓ Use Code Stress Ratios            | Use Clear Spans For KL/r             | All Leg Panels Have Same Allowable      |
| ✓ Use Code Safety Factors - Guys    | Retention Guys To Initial Tension    | Offset Girt At Foundation               |
| Escalate Ice                        | ✓ Bypass Mast Stability Checks       | Consider Feed Line Torque               |
| Always Use Max Kz                   | Use Azimuth Dish Coefficients        | Include Angle Block Shear Check         |
| Use Special Wind Profile            | ✓ Project Wind Area of Appurt.       | Use TIA-222-G Bracing Resist. Exemption |
| Include Bolts In Member Capacity    | Autocalc Torque Arm Areas            | Use TIA-222-G Tension Splice Exemption  |
| Leg Bolts Are At Top Of Section     | Add IBC .6D+W Combination            | Poles                                   |
| Secondary Horizontal Braces Leg     | ✓ Sort Capacity Reports By Component | ✓ Include Shear-Torsion Interaction     |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing    | Always Use Sub-Critical Flow            |
| SR Members Have Cut Ends            | Treat Feed Line Bundles As Cylinder  | Use Top Mounted Sockets                 |
| SR Members Are Concentric           |                                      |   |

## Tapered Pole Section Geometry

<b>tnxTower</b>  <b>Dewberry</b> 600 Parsippany Road, Suite 301 Parsippany, NJ 07054 Phone: (973) 739-9400 FAX: (973) 739-9710	Job	50093832	Page
	Project	CT2128	Date 13:56:15 01/25/19
	Client	SAI/AT&T	Designed by DAP

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	150.00-95.83	54.17	5.17	12	23.6100	33.4690	0.2810	1.1250	A572-65 (65 ksi)
L2	95.83-47.83	53.17	6.17	12	31.9661	41.6440	0.3750	1.5000	A572-65 (65 ksi)
L3	47.83-30.00	24.00	0.00	12	39.7709	41.1390	0.4380	1.7500	A572-65 (65 ksi)
L4	30.00-0.00	30.00		12	41.1390	49.6000	0.5800	2.3200	A572-65 (65 ksi)

### Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I <sub>t</sub> /Q in <sup>2</sup>	w in	w/t
L1	24.4429	21.1085	1466.3462	8.3518	12.2300	119.8977	2971.2149	10.3890	5.5744	19.838
	34.6497	30.0292	4221.7391	11.8813	17.3369	243.5112	8554.3879	14.7794	8.2166	29.241
L2	34.0679	38.1462	4859.2074	11.3096	16.5584	293.4585	9846.0716	18.7744	7.5619	20.165
	43.1130	49.8323	10832.9048	14.7743	21.5716	502.1838	21950.4020	24.5260	10.1556	27.082
L3	41.5380	55.4736	10954.3159	14.0812	20.6013	531.7281	22196.4139	27.3024	9.4858	21.657
	42.5902	57.4031	12137.5539	14.5710	21.3100	569.5708	24593.9749	28.2520	9.8525	22.494
L4	42.5902	75.7480	15904.9216	14.5201	21.3100	746.3595	32227.6831	37.2809	9.4709	16.329
	51.3497	91.5498	28079.5237	17.5492	25.6928	1092.8946	56896.7277	45.0580	11.7384	20.239

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L1 150.00-95.83				1	1	1			
L2 95.83-47.83				1	1	1			
L3 47.83-30.00				1	1	1			
L4 30.00-0.00				1.2	1	1.1			

### Monopole Base Plate Data

#### Base Plate Data

Base plate is square	
Base plate is grouted	✓
Anchor bolt grade	A615-75
Anchor bolt size	2.2500 in
Number of bolts	16
Embedment length	60.0000 in
$f_c$	4 ksi
Grout space	3.0000 in
Base plate grade	A633-60
Base plate thickness	2.7500 in
Bolt circle diameter	57.8500 in
Outer diameter	63.8500 in
Inner diameter	40.0000 in
Base plate type	Plain Plate

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## Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C <sub>A</sub> A <sub>A</sub>	Weight
						ft <sup>2</sup> /ft	plf
1 5/8 (Town - Existing)	A	No	Inside Pole	149.00 - 3.00	3	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
1 5/8 (Nextel - Existing)	B	No	Inside Pole	149.00 - 3.00	12	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
1 1/4 (AT&T - Existing)	A	No	CaAa (Out Of Face)	125.00 - 3.00	12	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
1 1/4 (T-Mobile - Existing)	A	No	CaAa (Out Of Face)	110.00 - 3.00	2	No Ice	0.16
						1/2" Ice	0.25
						1" Ice	0.35
1 1/4 (T-Mobile - Existing)	A	No	CaAa (Out Of Face)	110.00 - 3.00	10	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
1 5/8 (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.00 - 3.00	2	No Ice	0.20
						1/2" Ice	0.30
						1" Ice	0.40
1 5/8 (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.00 - 3.00	10	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
7/8 (Town - Existing)	B	No	Inside Pole	104.00 - 3.00	4	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
1/2 (GPS - Existing)	B	No	CaAa (Out Of Face)	40.00 - 3.00	1	No Ice	0.06
						1/2" Ice	0.16
						1" Ice	0.26
RG6-Fiber (AT&T - Existing)	C	No	CaAa (Out Of Face)	129.00 - 3.00	1	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
#8 AWG Copper Wire (AT&T Existing)	C	No	CaAa (Out Of Face)	129.00 - 3.00	2	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
HYBRIFLEX 1-5/8" (Sprint - Existing)	C	No	Inside Pole	138.00 - 3.00	3	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
HYBRIFLEX 1-5/8" (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.00 - 3.00	1	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00
**PROPOSED** RG6-Fiber (AT&T)	C	No	CaAa (Out Of Face)	129.00 - 3.00	1	No Ice	0.00
						1/2" Ice	0.00
						1" Ice	0.00

## Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight lb
			ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	
L1	150.00-95.83	A	0.000	0.000	0.000	4.393	679.59
		B	0.000	0.000	0.000	0.000	670.72
		C	0.000	0.000	0.000	0.000	319.36
L2	95.83-47.83	A	0.000	0.000	0.000	14.880	1296.00
		B	0.000	0.000	0.000	0.000	768.00

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Tower Section	Tower Elevation	Face	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
			ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	lb
L3	47.83-30.00	C	0.000	0.000	0.000	11.551	792.38
		A	0.000	0.000	0.000	5.527	481.41
		B	0.000	0.000	0.000	0.580	295.28
L4	30.00-0.00	C	0.000	0.000	0.000	7.061	392.26
		A	0.000	0.000	0.000	8.370	729.00
		B	0.000	0.000	0.000	1.566	459.00
		C	0.000	0.000	0.000	10.692	594.00

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation	Face or Leg	Ice Thickness	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
			in	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	lb
L1	150.00-95.83	A	1.709	0.000	0.000	0.000	14.080	2457.45
		B	0.000	0.000	0.000	0.000	0.000	670.72
		C	0.000	0.000	0.000	0.000	0.000	546.14
L2	95.83-47.83	A	1.621	0.000	0.000	0.000	47.696	5234.04
		B	0.000	0.000	0.000	0.000	0.000	768.00
		C	0.000	0.000	0.000	0.000	31.494	3613.45
L3	47.83-30.00	A	1.525	0.000	0.000	0.000	17.084	1868.31
		B	0.000	0.000	0.000	0.000	3.821	295.28
		C	0.000	0.000	0.000	0.000	18.618	1952.52
L4	30.00-0.00	A	1.382	0.000	0.000	0.000	23.294	2519.95
		B	0.000	0.000	0.000	0.000	9.029	459.00
		C	0.000	0.000	0.000	0.000	25.616	2608.82

### Shielding Factor K<sub>a</sub>

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
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### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	lb
10-ft Dipole (Town)	A	From Face	3.00	0.0000	149.00	No Ice	3.15	3.15
			0.00			1/2" Ice	5.67	42.00
			5.00			1" Ice	8.19	52.00
10-ft Dipole (Town)	B	From Face	3.00	0.0000	149.00	No Ice	3.15	32.00
			0.00			1/2" Ice	5.67	42.00
			5.00			1" Ice	8.19	52.00
DB810K (Town)	C	From Face	3.00	0.0000	149.00	No Ice	4.08	35.00
			0.00			1/2" Ice	5.73	65.00
			5.00			1" Ice	7.39	95.00
(4) DB844H90E-XY (Nextel Existing)	A	From Face	3.00	0.0000	149.00	No Ice	2.87	10.00
			0.00			1/2" Ice	3.18	35.00

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	Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight lb
(4)	DB844H90E-XY (Nextel Existing)	B	From Face	0.00 3.00 0.00 0.00	0.0000	149.00	1" Ice No Ice 1/2" Ice 1" Ice	3.49 2.87 3.18 3.49	4.47 3.73 4.10 4.47
(4)	DB844H90E-XY (Nextel Existing)	C	From Face	0.00 3.00 0.00 0.00	0.0000	149.00	No Ice 1/2" Ice 1" Ice	2.87 3.18 3.49	10.00 35.00 60.00
	Valmont T-Arm (Nextel Existing)	A	None		0.0000	149.00	No Ice 1/2" Ice 1" Ice	10.54 14.45 18.36	336.00 412.00 488.00
	Valmont T-Arm (Nextel Existing)	B	None		0.0000	149.00	No Ice 1/2" Ice 1" Ice	10.54 14.45 18.36	336.00 412.00 488.00
	Valmont T-Arm (Nextel Existing)	C	None		0.0000	149.00	No Ice 1/2" Ice 1" Ice	10.54 14.45 18.36	336.00 412.00 488.00
	APXVSPP18-C-A20 (Sprint Existing)	A	From Face	3.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	8.26 8.81 9.35	5.28 5.74 6.19
	APXVSPP18-C-A20 (Sprint Existing)	B	From Face	3.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	8.26 8.81 9.35	5.28 5.74 6.19
	APXVSPP18-C-A20 (Sprint Existing)	C	From Face	3.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	8.26 8.81 9.35	5.28 5.74 6.19
	FD-RRH 4x45 1900 (Sprint Existing)	A	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.71 2.94 3.18	2.78 3.02 3.26
	FD-RRH 4x45 1900 (Sprint Existing)	B	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.71 2.94 3.18	2.78 3.02 3.26
	FD-RRH 4x45 1900 (Sprint Existing)	C	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.71 2.94 3.18	2.78 3.02 3.26
	FD-RRH 2x50 800 (Sprint Existing)	A	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.40 2.61 2.83	2.25 2.46 2.67
	FD-RRH 2x50 800 (Sprint Existing)	B	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.40 2.61 2.83	2.25 2.46 2.67
	FD-RRH 2x50 800 (Sprint Existing)	C	From Face	1.00 0.00 0.00	0.0000	138.00	No Ice 1/2" Ice 1" Ice	2.40 2.61 2.83	2.25 2.46 2.67
	13' Platform w/Rails (Sprint Existing)	C	None		0.0000	138.00	No Ice 1/2" Ice 1" Ice	17.20 22.30 27.40	2000.00 3000.00 4000.00
	RRUS-11 (AT&T Existing)	A	From Face	0.50 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	2.99 3.23 3.46	1.25 1.41 1.58
	RRUS-11 (AT&T Existing)	B	From Face	0.50 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	2.99 3.23 3.46	1.25 1.41 1.58
	RRUS-11 (AT&T Existing)	C	From Face	0.50 0.00 0.00	0.0000	129.00	No Ice 1/2" Ice 1" Ice	2.99 3.23 3.46	1.25 1.41 1.58
	RRUS-12 (AT&T Existing)	A	From Face	0.50 0.00	0.0000	129.00	No Ice 1/2" Ice	3.67 3.93	58.00 81.00

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Description	Face or Leg	Offset Type	Offsets: Horz ft	Lateral ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight lb
			Vert ft						
RRUS-12 (AT&T Existing)	B	From Face	0.00						
			0.50		0.0000	129.00	1" Ice	4.18	1.86
			0.00				No Ice	3.67	1.49
			0.00				1/2" Ice	3.93	1.67
			0.00				1" Ice	4.18	1.86
RRUS-12 (AT&T Existing)	C	From Face	0.50		0.0000	129.00	No Ice	3.67	1.49
			0.00				1/2" Ice	3.93	1.67
			0.00				1" Ice	4.18	1.86
A2 (AT&T Existing)	A	From Face	0.50		0.0000	129.00	No Ice	2.42	0.54
			0.00				1/2" Ice	2.63	0.68
			0.00				1" Ice	2.84	0.81
A2 (AT&T Existing)	B	From Face	0.50		0.0000	129.00	No Ice	2.42	0.54
			0.00				1/2" Ice	2.63	0.68
			0.00				1" Ice	2.84	0.81
A2 (AT&T Existing)	C	From Face	0.50		0.0000	129.00	No Ice	2.42	0.54
			0.00				1/2" Ice	2.63	0.68
			0.00				1" Ice	2.84	0.81
DC6-48-60-18-8F Surge Arrestor (AT&T Existing)	C	From Face	0.50		0.0000	129.00	No Ice	2.23	2.23
			0.00				1/2" Ice	2.45	2.45
			0.00				1" Ice	2.67	2.67
Valmont Uni-Tri Bracket (AT&T Existing)	C	None			0.0000	129.00	No Ice	1.75	1.75
							1/2" Ice	1.94	1.94
							1" Ice	2.13	2.13
7770.00 (AT&T Existing)	A	From Face	3.00		0.0000	127.00	No Ice	5.88	2.93
			-6.00				1/2" Ice	6.31	3.27
			0.00				1" Ice	6.75	3.62
HPA-65R-BUU-H6 (AT&T Existing)	A	From Face	3.00		0.0000	127.00	No Ice	10.36	6.45
			6.00				1/2" Ice	10.93	6.91
			0.00				1" Ice	11.49	7.38
7770.00 (AT&T Existing)	B	From Face	3.00		0.0000	127.00	No Ice	5.88	2.93
			-6.00				1/2" Ice	6.31	3.27
			0.00				1" Ice	6.75	3.62
HPA-65R-BUU-H6 (AT&T Existing)	B	From Face	3.00		0.0000	127.00	No Ice	10.36	6.45
			6.00				1/2" Ice	10.93	6.91
			0.00				1" Ice	11.49	7.38
7770.00 (AT&T Existing)	C	From Face	3.00		0.0000	127.00	No Ice	5.88	2.93
			-6.00				1/2" Ice	6.31	3.27
			0.00				1" Ice	6.75	3.62
HPA-65R-BUU-H6 (AT&T Existing)	C	From Face	3.00		0.0000	127.00	No Ice	10.36	6.45
			6.00				1/2" Ice	10.93	6.91
			0.00				1" Ice	11.49	7.38
(2) LGP214nn TMA (AT&T Existing)	A	From Face	3.00		0.0000	127.00	No Ice	0.00	0.23
			0.00				1/2" Ice	0.00	0.31
			0.00				1" Ice	0.00	0.39
(2) LGP214nn TMA (AT&T Existing)	B	From Face	3.00		0.0000	127.00	No Ice	0.00	0.23
			0.00				1/2" Ice	0.00	0.31
			0.00				1" Ice	0.00	0.39
(2) LGP214nn TMA (AT&T Existing)	C	From Face	3.00		0.0000	127.00	No Ice	0.00	0.23
			0.00				1/2" Ice	0.00	0.31
			0.00				1" Ice	0.00	0.39
Valmont 13' Low Profile Platform (AT&T Existing)	C	None			0.0000	125.00	No Ice	15.70	15.70
							1/2" Ice	20.10	20.10
							1" Ice	24.50	24.50
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	A	From Face	3.00		0.0000	113.00	No Ice	6.70	2.00
			6.00				1/2" Ice	7.13	2.33
			0.00				1" Ice	7.56	2.65
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	B	From Face	3.00		0.0000	113.00	No Ice	6.70	2.00
			6.00				1/2" Ice	7.13	2.33

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	C	From Face	0.00 3.00 6.00 0.00	0.0000	113.00	1" Ice No Ice 1/2" Ice 1" Ice	7.56 6.70 7.13 7.56	2.65 2.00 2.33 2.65
(2) 10"x8"x3" TMA (T-Mobile Existing)	A	From Face	3.00 6.00 0.00	0.0000	113.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.29 0.38 0.47
(2) 10"x8"x3" TMA (T-Mobile Existing)	B	From Face	3.00 6.00 0.00	0.0000	113.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.29 0.38 0.47
(2) 10"x8"x3" TMA (T-Mobile Existing)	C	From Face	3.00 6.00 0.00	0.0000	113.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.29 0.38 0.47
13' Platform w/Rails (T-Mobile Existing)	C	None		0.0000	113.00	No Ice 1/2" Ice 1" Ice	17.20 22.30 27.40	2000.00 3000.00 4000.00
4'-6" Standoff (Town - Existing)	A	From Face	3.00 0.00 0.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	2.10 2.48 2.86	0.16 0.21 0.27
4'-6" Standoff (Town - Existing)	A	From Face	3.00 0.00 0.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	2.10 2.48 2.86	0.16 0.21 0.27
4'-6" Standoff (Town - Existing)	B	From Face	3.00 0.00 0.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	2.10 2.48 2.86	0.16 0.21 0.27
4'-6" Standoff (Town - Existing)	C	From Face	3.00 0.00 0.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	2.10 2.48 2.86	0.16 0.21 0.27
1142-2B (Town - Existing)	B	From Face	5.00 0.00 4.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	1.12 2.54 3.95	1.12 2.54 3.95
ASPA685 (Town - Existing)	B	From Face	5.00 0.00 -10.50	0.0000	104.00	No Ice 1/2" Ice 1" Ice	5.25 7.38 9.51	5.25 7.38 9.51
DB222 (Town - Existing)	A	From Face	5.00 0.00 5.00	0.0000	104.00	No Ice 1/2" Ice 1" Ice	1.60 2.88 4.16	1.60 2.88 4.16
ASPA685 (Town - Existing)	A	From Face	5.00 0.00 -10.50	0.0000	104.00	No Ice 1/2" Ice 1" Ice	5.25 7.38 9.51	5.25 7.38 9.51
DB846F65ZAXY (Verizon - Existing)	A	From Face	3.00 -6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
BXA-171063/8BF (Verizon Existing)	A	From Face	3.00 -3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.94 3.25 3.57	2.16 2.46 2.76
BXA-70063/6CF (Verizon - Existing)	A	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.73 8.27 8.80	4.16 4.59 5.03
DB846F65ZAXY (Verizon - Existing)	A	From Face	3.00 6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
DB846F65ZAXY (Verizon - Existing)	B	From Face	3.00 -6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
BXA-171063/8BF (Verizon Existing)	B	From Face	3.00 -3.00 -3.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.94 3.25 3.57	2.16 2.46 2.76

<b>tnxTower</b>  <b>Dewberry</b> 600 Parsippany Road, Suite 301 Parsippany, NJ 07054 Phone: (973) 739-9400 FAX: (973) 739-9710	Job 50093832							Page 8 of 21
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	Client SAI/AT&T							Designed by DAP

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight lb
BXA-70063/6CF (Verizon - Existing)	B	From Face	0.00 3.00 0.00 0.00	0.0000	80.00	1" Ice No Ice 1/2" Ice 1" Ice	3.57 7.73 8.27 8.80	2.76 4.16 4.59 5.03
DB846F65ZAXY (Verizon - Existing)	B	From Face	3.00 6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
DB846F65ZAXY (Verizon - Existing)	C	From Face	3.00 -6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
BXA-171063/8BF (Verizon Existing)	C	From Face	3.00 -3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.94 3.25 3.57	2.16 2.46 2.76
BXA-70063/6CF (Verizon - Existing)	C	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.73 8.27 8.80	4.16 4.59 5.03
DB846F65ZAXY (Verizon - Existing)	C	From Face	3.00 6.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	7.03 7.54 8.04	6.16 6.62 7.08
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	A	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.09 0.14 0.19
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	B	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.09 0.14 0.19
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	C	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	0.00 0.00 0.00	0.09 0.14 0.19
BXA-171063-12CF (Verizon - Existing)	A	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	4.79 5.24 5.69	3.62 4.06 4.50
BXA-171063-12CF (Verizon - Existing)	B	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	4.79 5.24 5.69	3.62 4.06 4.50
BXA-171063-12CF (Verizon - Existing)	C	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	4.79 5.24 5.69	3.62 4.06 4.50
RRH2x40-AWS (Verizon - Existing)	A	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.52 2.75 2.98	1.59 1.79 2.00
RRH2x40-AWS (Verizon - Existing)	B	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.52 2.75 2.98	1.59 1.79 2.00
RRH2x40-AWS (Verizon - Existing)	C	From Face	3.00 3.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	2.52 2.75 2.98	1.59 1.79 2.00
DB-T1-6Z-8AB-0Z (Verizon - Existing)	A	From Face	3.00 0.00 0.00	0.0000	80.00	No Ice 1/2" Ice 1" Ice	5.60 5.92 6.23	2.33 2.56 2.78
Valmont 13' Low Profile Platform (Verizon - Existing)	C	None		0.0000	78.00	No Ice 1/2" Ice 1" Ice	15.70 20.10 24.50	1300.00 20.10 2230.00
Standoff	A	From Face	1.00 0.00 0.00	0.0000	40.00	No Ice 1/2" Ice 1" Ice	0.75 0.95 1.15	27.00 36.00 45.00
GPS (Existing)	A	From Face	2.00 0.00	0.0000	40.00	No Ice 1/2" Ice	1.00 1.50	10.00 15.00

<b>tnxTower</b>  <b>Dewberry</b> 600 Parsippany Road, Suite 301 Parsippany, NJ 07054 Phone: (973) 739-9400 FAX: (973) 739-9710	Job	50093832	Page
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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
**PROPOSED**			0.00		1" Ice	2.00	2.00	20.00
800-10965	A	From Face	3.00 2.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	5.46 5.81 6.16	1.89 2.19 2.49
RRH B5/B12 4449	A	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	1.86 2.12 2.37	0.87 1.06 1.26
RRH 4415 B30	A	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	2.69 3.02 3.36	1.57 1.85 2.13
DC/Fiber Squid	A	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	2.10 2.39 2.69	19.00 39.65 60.30
800-10965	B	From Face	3.00 2.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	5.46 5.81 6.16	1.89 2.19 2.49
RRH B5/B12 4449	B	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	1.97 2.24 2.50	1.40 1.64 1.87
RRH 4415 B30	B	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	2.69 3.02 3.36	60.00 80.40 100.80
800-10965	C	From Face	3.00 2.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	5.46 5.81 6.16	1.89 2.19 2.49
RRH B5/B12 4449	C	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	1.97 2.24 2.50	1.40 1.64 1.87
RRH 4415 B30	C	From Face	0.50 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice 1" Ice	2.69 3.02 3.36	60.00 80.40 100.80

## Tower Pressures - No Ice

$$G_H = 1.100$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 150.00-95.83	121.78	1.045	23	133.377	A B C	0.000 0.000 0.000	133.377 133.377 133.377	133.377	100.00	0.000	4.393
L2 95.83-47.83	71.47	0.898	20	154.362	A B C	0.000 0.000 0.000	154.362 154.362 154.362	154.362	100.00	0.000	14.880
L3 47.83-30.00	38.88	0.754	17	62.500	A B C	0.000 0.000 0.000	62.500 62.500 62.500	62.500	100.00	0.000	11.551
										5.527	5.527
										0.580	0.580
										7.061	7.061

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Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L4 30.00-0.00	14.53	0.7	15	117.425	A	0.000	117.425	117.425	100.00	0.000	8.370
					B	0.000	117.425		100.00	0.000	1.566
					C	0.000	117.425		100.00	0.000	10.692

### Tower Pressure - With Ice

$$G_H = 1.100$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>Z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 150.00-95.83	121.78	1.045	6	1.7092	148.808	A	0.000	148.808	148.808	100.00	0.000	14.080
						B	0.000	148.808		100.00	0.000	0.000
						C	0.000	148.808		100.00	0.000	0.000
L2 95.83-47.83	71.47	0.898	5	1.6205	168.036	A	0.000	168.036	168.036	100.00	0.000	47.696
						B	0.000	168.036		100.00	0.000	0.000
						C	0.000	168.036		100.00	0.000	31.494
L3 47.83-30.00	38.88	0.754	5	1.5248	67.316	A	0.000	67.316	67.316	100.00	0.000	17.084
						B	0.000	67.316		100.00	0.000	3.821
						C	0.000	67.316		100.00	0.000	18.618
L4 30.00-0.00	14.53	0.7	4	1.3819	124.334	A	0.000	124.334	124.334	100.00	0.000	23.294
						B	0.000	124.334		100.00	0.000	9.029
						C	0.000	124.334		100.00	0.000	25.616

### Tower Pressure - Service

$$G_H = 1.100$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>	e	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
L1 150.00-95.83	121.78	1.045	8	133.377	A	0.000	133.377	133.377	100.00	0.000	4.393
					B	0.000	133.377		100.00	0.000	0.000
					C	0.000	133.377		100.00	0.000	0.000
L2 95.83-47.83	71.47	0.898	7	154.362	A	0.000	154.362	154.362	100.00	0.000	14.880
					B	0.000	154.362		100.00	0.000	0.000
					C	0.000	154.362		100.00	0.000	11.551
L3 47.83-30.00	38.88	0.754	6	62.500	A	0.000	62.500	62.500	100.00	0.000	5.527
					B	0.000	62.500		100.00	0.000	0.580
					C	0.000	62.500		100.00	0.000	7.061
L4 30.00-0.00	14.53	0.7	5	117.425	A	0.000	117.425	117.425	100.00	0.000	8.370
					B	0.000	117.425		100.00	0.000	1.566
					C	0.000	117.425		100.00	0.000	10.692

### Tower Forces - No Ice - Wind Normal To Face

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
									ft <sup>2</sup>	lb		
L1 150.00-95.83	1669.67	4713.09	A B C	1 1 1	1 1 1	23	1 1 1	1 1 1	133.377 133.377 133.377	3469.69	64.05	C
L2 95.83-47.83	2856.38	7958.82	A B C	1 1 1	1.128 1.128 1.128	20	1 1 1	1 1 1	154.362 154.362 154.362	4324.80	90.10	C
L3 47.83-30.00	1168.95	4609.15	A B C	1 1 1	1.2 1.2 1.2	17	1 1 1	1 1 1	62.500 62.500 62.500	1606.01	90.07	C
L4 30.00-0.00	1782.00	9393.11	A B C	1 1 1	1.139 1.139 1.139	15	1 1 1	1 1 1	117.425 117.425 117.425	2609.38	86.98	C
Sum Weight:	7477.00	26674.17					OTM		831998.57 lb·ft	12009.88		

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
									ft <sup>2</sup>	lb		
L1 150.00-95.83	1669.67	4713.09	A B C	1 1 1	1 1 1	23	1 1 1	1 1 1	133.377 133.377 133.377	3469.69	64.05	C
L2 95.83-47.83	2856.38	7958.82	A B C	1 1 1	1.128 1.128 1.128	20	1 1 1	1 1 1	154.362 154.362 154.362	4324.80	90.10	C
L3 47.83-30.00	1168.95	4609.15	A B C	1 1 1	1.2 1.2 1.2	17	1 1 1	1 1 1	62.500 62.500 62.500	1606.01	90.07	C
L4 30.00-0.00	1782.00	9393.11	A B C	1 1 1	1.139 1.139 1.139	15	1 1 1	1 1 1	117.425 117.425 117.425	2609.38	86.98	C
Sum Weight:	7477.00	26674.17					OTM		831998.57 lb·ft	12009.88		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
									ft <sup>2</sup>	lb		
L1 150.00-95.83	1669.67	4713.09	A B C	1 1 1	1 1 1	23	1 1 1	1 1 1	133.377 133.377 133.377	3469.69	64.05	C
L2 95.83-47.83	2856.38	7958.82	A B C	1 1 1	1.128 1.128 1.128	20	1 1 1	1 1 1	154.362 154.362 154.362	4324.80	90.10	C
L3 47.83-30.00	1168.95	4609.15	A	1	1.2	17	1	1	62.500	1606.01	90.07	C

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
47.83-30.00			B	1	1.2			1	1	62.500		
L4 30.00-0.00	1782.00	9393.11	C	1	1.2			1	1	62.500		
			A	1	1.139		15	1	1	117.425		
			B	1	1.139			1	1	117.425	2609.38	
			C	1	1.139			1	1	117.425	86.98	C
Sum Weight:	7477.00	26674.17						OTM	831998.57 lb-ft	12009.88		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
L1 150.00-95.83	3674.31	8220.16	A	1	1.2	6	1	1	148.808	1344.00	24.81	C
			B	1	1.2		1	1	148.808			
			C	1	1.2		1	1	148.808			
L2 95.83-47.83	9615.49	11747.44	A	1	1.2	5	1	1	168.036	1677.46	34.95	C
			B	1	1.2		1	1	168.036			
			C	1	1.2		1	1	168.036			
L3 47.83-30.00	4116.11	6044.30	A	1	1.2	5	1	1	67.316	607.02	34.04	C
			B	1	1.2		1	1	67.316			
			C	1	1.2		1	1	67.316			
L4 30.00-0.00	5587.76	11820.14	A	1	1.2	4	1	1	124.334	969.75	32.32	C
			B	1	1.2		1	1	124.334			
			C	1	1.2		1	1	124.334			
Sum Weight:	22993.67	37832.04					OTM	321255.74 lb-ft	4598.23			

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w plf	Ctrl. Face
L1 150.00-95.83	3674.31	8220.16	A	1	1.2	6	1	1	148.808	1344.00	24.81	C
			B	1	1.2		1	1	148.808			
			C	1	1.2		1	1	148.808			
L2 95.83-47.83	9615.49	11747.44	A	1	1.2	5	1	1	168.036	1677.46	34.95	C
			B	1	1.2		1	1	168.036			
			C	1	1.2		1	1	168.036			
L3 47.83-30.00	4116.11	6044.30	A	1	1.2	5	1	1	67.316	607.02	34.04	C
			B	1	1.2		1	1	67.316			
			C	1	1.2		1	1	67.316			
L4 30.00-0.00	5587.76	11820.14	A	1	1.2	4	1	1	124.334	969.75	32.32	C
			B	1	1.2		1	1	124.334			
			C	1	1.2		1	1	124.334			
Sum Weight:	22993.67	37832.04					OTM	321255.74 lb-ft	4598.23			

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### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F ft <sup>2</sup>	w lb	Ctrl. Face plf
L1 150.00-95.83	3674.31	8220.16	A	1	1.2	6	1	1	148.808	1344.00	24.81	C
			B	1	1.2		1	1	148.808			
			C	1	1.2		1	1	148.808			
L2 95.83-47.83	9615.49	11747.44	A	1	1.2	5	1	1	168.036	1677.46	34.95	C
			B	1	1.2		1	1	168.036			
			C	1	1.2		1	1	168.036			
L3 47.83-30.00	4116.11	6044.30	A	1	1.2	5	1	1	67.316	607.02	34.04	C
			B	1	1.2		1	1	67.316			
			C	1	1.2		1	1	67.316			
L4 30.00-0.00	5587.76	11820.14	A	1	1.2	4	1	1	124.334	969.75	32.32	C
			B	1	1.2		1	1	124.334			
			C	1	1.2		1	1	124.334			
Sum Weight:	22993.67	37832.04					OTM		321255.74 lb-ft	4598.23		

### Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F ft <sup>2</sup>	w lb	Ctrl. Face plf
L1 150.00-95.83	1669.67	4713.09	A	1	1	8	1	1	133.377	1238.34	22.86	C
			B	1	1		1	1	133.377			
			C	1	1		1	1	133.377			
L2 95.83-47.83	2856.38	7958.82	A	1	1.128	7	1	1	154.362	1543.54	32.16	C
			B	1	1.128		1	1	154.362			
			C	1	1.128		1	1	154.362			
L3 47.83-30.00	1168.95	4609.15	A	1	1.2	6	1	1	62.500	573.19	32.15	C
			B	1	1.2		1	1	62.500			
			C	1	1.2		1	1	62.500			
L4 30.00-0.00	1782.00	9393.11	A	1	1.139	5	1	1	117.425	931.30	31.04	C
			B	1	1.139		1	1	117.425			
			C	1	1.139		1	1	117.425			
Sum Weight:	7477.00	26674.17					OTM		296943.07 lb-ft	4286.37		

### Tower Forces - Service - Wind 60 To Face

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Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F ft <sup>2</sup>	w lb	Ctrl. Face plf
L1 150.00-95.83	1669.67	4713.09	A B C	1 1 1	1 1 1	8	1 1 1	1 1 1	133.377 133.377 133.377	1238.34	22.86	C
L2 95.83-47.83	2856.38	7958.82	A B C	1 1 1	1.128 1.128 1.128	7	1 1 1	1 1 1	154.362 154.362 154.362	1543.54	32.16	C
L3 47.83-30.00	1168.95	4609.15	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	62.500 62.500 62.500	573.19	32.15	C
L4 30.00-0.00	1782.00	9393.11	A B C	1 1 1	1.139 1.139 1.139	5	1 1 1	1 1 1	117.425 117.425 117.425	931.30	31.04	C
Sum Weight:	7477.00	26674.17					OTM		296943.07 lb-ft	4286.37		

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight lb	Self Weight lb	F a c e	e	C <sub>F</sub>	q <sub>z</sub> psf	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F ft <sup>2</sup>	w lb	Ctrl. Face plf
L1 150.00-95.83	1669.67	4713.09	A B C	1 1 1	1 1 1	8	1 1 1	1 1 1	133.377 133.377 133.377	1238.34	22.86	C
L2 95.83-47.83	2856.38	7958.82	A B C	1 1 1	1.128 1.128 1.128	7	1 1 1	1 1 1	154.362 154.362 154.362	1543.54	32.16	C
L3 47.83-30.00	1168.95	4609.15	A B C	1 1 1	1.2 1.2 1.2	6	1 1 1	1 1 1	62.500 62.500 62.500	573.19	32.15	C
L4 30.00-0.00	1782.00	9393.11	A B C	1 1 1	1.139 1.139 1.139	5	1 1 1	1 1 1	117.425 117.425 117.425	931.30	31.04	C
Sum Weight:	7477.00	26674.17					OTM		296943.07 lb-ft	4286.37		

### Force Totals

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, M <sub>x</sub> lb-ft	Sum of Overturning Moments, M <sub>z</sub> lb-ft	Sum of Torques lb-ft
Leg Weight	26674.17					
Bracing Weight	0.00					
Total Member Self-Weight	26674.17			-413.72	443.25	
Total Weight	45187.17			-413.72	443.25	
Wind 0 deg - No Ice		-50.61	-20171.20	-1807399.82	5031.84	-415.29
Wind 90 deg - No Ice		20229.64	50.61	4174.87	-1811841.30	-1016.10
Wind 180 deg - No Ice		50.61	20171.20	1806572.38	-4145.34	415.29

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Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments, $M_x$ lb-ft	Sum of Overturning Moments, $M_z$ lb-ft	Sum of Torques lb-ft
Member Ice	11157.87					
Total Weight Ice	91060.21			-1501.09	1201.26	
Wind 0 deg - Ice		-17.45	-8330.61	-775482.71	2816.01	-159.22
Wind 90 deg - Ice		8350.76	17.45	113.66	-774644.92	-885.37
Wind 180 deg - Ice		17.45	8330.61	772480.52	-413.50	159.22
Total Weight	45187.17			-413.72	443.25	
Wind 0 deg - Service		-18.06	-7199.17	-645333.09	2080.93	-148.22
Wind 90 deg - Service		7220.03	18.06	1223.96	-646367.16	-362.65
Wind 180 deg - Service		18.06	7199.17	644505.65	-1194.43	148.22

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 90 deg - No Ice
5	0.9 Dead+1.6 Wind 90 deg - No Ice
6	1.2 Dead+1.6 Wind 180 deg - No Ice
7	0.9 Dead+1.6 Wind 180 deg - No Ice
8	1.2 Dead+1.0 Ice+1.0 Temp
9	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
10	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
11	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
12	Dead+Wind 0 deg - Service
13	Dead+Wind 90 deg - Service
14	Dead+Wind 180 deg - Service

## Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L1	150 - 95.83	Pole	Max Tension	2	0.12	-0.83	-0.02
			Max. Compression	8	-38438.51	398.79	1069.39
			Max. Mx	4	-16998.30	-458304.18	-8.62
			Max. My	2	-17002.31	507.97	458457.76
			Max. Vy	4	16010.02	-458304.18	-8.62
			Max. Vx	2	-15971.54	507.97	458457.76
			Max. Torque	4			1354.63
L2	95.83 - 47.83	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	8	-66424.71	1063.21	1453.06
			Max. Mx	4	-31280.81	-1445200.1	-2708.26
					0		
			Max. My	2	-31286.29	3592.61	1442283.97
			Max. Vy	4	25749.49	-1445200.1	-2708.26
					0		
L3	47.83 - 30	Pole	Max. Vx	2	-25651.37	3592.61	1442283.97
			Max. Torque	4			1540.52
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	8	-81359.42	1290.11	1584.10
			Max. Mx	4	-40294.10	-2102660.0	-4632.59

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L4	30 - 0	Pole	Max. My	2	-40297.15	5712.27	2097556.49
			Max. Vy	4	28931.18	-2102660.0	-4632.59
			Max. Vx	2	-28835.33	5712.27	2097556.49
			Max. Torque	4			1620.62
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	8	-101002.34	1290.19	1584.21
			Max. Mx	4	-54211.47	-3020617.0	-7091.04
						1	
			Max. My	2	-54211.42	8171.22	3012594.83
			Max. Vy	4	32387.93	-3020617.0	-7091.04
			Max. Vx	2	-32291.73	8171.22	3012594.83
			Max. Torque	4			1619.95

## Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
Pole	Max. Vert	8	101002.34	0.00	0.00
	Max. H <sub>x</sub>	3	40668.33	80.97	32271.19
	Max. H <sub>z</sub>	3	40668.33	80.97	32271.19
	Max. M <sub>x</sub>	2	3012594.83	80.97	32269.90
	Max. M <sub>z</sub>	4	3020617.00	-32366.04	-80.97
	Max. Torsion	4	1619.39	-32366.04	-80.97
	Min. Vert	5	40668.33	-32364.69	-80.96
	Min. H <sub>x</sub>	4	54224.54	-32366.04	-80.97
	Min. H <sub>z</sub>	7	40668.33	-80.97	-32271.20
	Min. M <sub>x</sub>	6	-3011539.29	-80.97	-32269.90
	Min. M <sub>z</sub>	2	-8171.14	80.97	32269.90
	Min. Torsion	6	-661.99	-80.97	-32269.90

## Tower Mast Reaction Summary

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub>	Overturning Moment, M <sub>z</sub>	Torque
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead Only	45187.17	-0.00	-0.00	-413.72	443.26	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	54224.42	-80.97	-32269.90	-3012594.83	8171.14	-664.04
0.9 Dead+1.6 Wind 0 deg - No Ice	40668.33	-80.97	-32271.19	-2980428.63	7953.71	-663.72
1.2 Dead+1.6 Wind 90 deg - No Ice	54224.54	32366.04	80.97	7091.23	-3020617.00	-1619.39
0.9 Dead+1.6 Wind 90 deg - No Ice	40668.33	32364.69	80.96	7155.64	-2988317.00	-1618.85
1.2 Dead+1.6 Wind 180 deg - No Ice	54224.42	80.97	32269.90	3011539.29	-7048.47	661.99
0.9 Dead+1.6 Wind 180 deg - No Ice	40668.33	80.97	32271.20	2979649.92	-7124.55	661.69
1.2 Dead+1.0 Ice+1.0 Temp	101002.34	-0.00	-0.00	-1584.21	1290.19	0.00

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Load Combination	Vertical lb	Shear <sub>x</sub> lb	Shear <sub>z</sub> lb	Overspinning Moment, M <sub>x</sub> lb-ft	Overspinning Moment, M <sub>z</sub> lb-ft	Torque lb-ft
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	101002.33	-17.45	-8330.25	-851196.11	3224.25	-161.12
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	101002.33	8350.40	17.45	-71.34	-849917.92	-892.05
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	101002.33	17.45	8330.26	847544.96	-276.98	160.98
Dead+Wind 0 deg - Service	45187.16	-18.06	-7198.45	-668063.04	2153.98	-148.52
Dead+Wind 90 deg - Service	45187.16	7219.30	18.06	1251.55	-669109.07	-363.10
Dead+Wind 180 deg - Service	45187.16	18.06	7198.45	667189.73	-1221.77	148.41

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX lb	PY lb	PZ lb	PX lb	PY lb	PZ lb	
1	0.00	-45187.17	0.00	0.00	45187.17	0.00	0.000%
2	-80.97	-54224.60	-32273.92	80.97	54224.42	32269.90	0.006%
3	-80.97	-40668.45	-32273.92	80.97	40668.33	32271.19	0.005%
4	32367.42	-54224.60	80.97	-32366.04	54224.54	-80.97	0.002%
5	32367.42	-40668.45	80.97	-32364.69	40668.33	-80.96	0.005%
6	80.97	-54224.60	32273.92	-80.97	54224.42	-32269.90	0.006%
7	80.97	-40668.45	32273.92	-80.97	40668.33	-32271.20	0.005%
8	0.00	-101002.34	0.00	0.00	101002.34	0.00	0.000%
9	-17.45	-101002.34	-8330.61	17.45	101002.33	8330.25	0.000%
10	8350.76	-101002.34	17.45	-8350.40	101002.33	-17.45	0.000%
11	17.45	-101002.34	8330.61	-17.45	101002.33	-8330.26	0.000%
12	-18.06	-45187.17	-7199.17	18.06	45187.16	7198.45	0.002%
13	7220.03	-45187.17	18.06	-7219.30	45187.16	-18.06	0.002%
14	18.06	-45187.17	7199.17	-18.06	45187.16	-7198.45	0.002%

## Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	12	0.00012362	0.00012403
3	Yes	12	0.00008241	0.00010806
4	Yes	13	0.00004356	0.00005847
5	Yes	12	0.00008240	0.00013133
6	Yes	12	0.00012362	0.00011706
7	Yes	12	0.00008241	0.00010265
8	Yes	6	0.00000001	0.00000001
9	Yes	14	0.00000001	0.00012320
10	Yes	14	0.00000001	0.00012285
11	Yes	14	0.00000001	0.00012238
12	Yes	12	0.00000001	0.00003014
13	Yes	12	0.00000001	0.00003072
14	Yes	12	0.00000001	0.00003005

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## Maximum Tower Deflections - Service Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
L1	150 - 95.83	17.755	13	0.9535	0.0004
L2	101 - 47.83	8.537	13	0.7783	0.0003
L3	54 - 30	2.405	13	0.4301	0.0002
L4	30 - 0	0.684	13	0.2253	0.0001

## Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
149.00	10-ft Dipole (Town)	13	17.555	0.9508	0.0010	83650
138.00	APXVSPP18-C-A20 (Sprint Existing)	13	15.368	0.9212	0.0011	34854
129.00	RRUS-11 (AT&T Existing)	13	13.608	0.8945	0.0011	19916
127.00	7770.00 (AT&T Existing)	13	13.223	0.8881	0.0012	18184
125.00	Valmont 13' Low Profile Platform (AT&T Existing)	13	12.840	0.8815	0.0012	16729
113.00	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	13	10.612	0.8362	0.0012	11303
104.00	4'-6" Standoff (Town - Existing)	13	9.039	0.7942	0.0012	9100
80.00	DB846F65ZAXY (Verizon - Existing)	13	5.386	0.6416	0.0009	7992
78.00	Valmont 13' Low Profile Platform (Verizon - Existing)	13	5.119	0.6266	0.0008	7944
40.00	Standoff	13	1.260	0.3090	0.0003	5853

## Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
L1	150 - 95.83	80.304	4	4.3159	0.0017
L2	101 - 47.83	38.610	4	3.5231	0.0015
L3	54 - 30	10.871	4	1.9451	0.0007
L4	30 - 0	3.089	4	1.0181	0.0003

## Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
149.00	10-ft Dipole (Town)	4	79.401	4.3040	0.0041	18670
138.00	APXVSPP18-C-A20 (Sprint Existing)	4	69.508	4.1699	0.0046	7778
129.00	RRUS-11 (AT&T Existing)	4	61.545	4.0492	0.0050	4443
127.00	7770.00 (AT&T Existing)	4	59.803	4.0202	0.0051	4056

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Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
125.00	Valmont 13' Low Profile Platform (AT&T Existing)	4	58.072	3.9903	0.0051	3731
113.00	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	4	47.995	3.7851	0.0053	2519
104.00	4'-6" Standoff (Town - Existing)	4	40.879	3.5949	0.0052	2027
80.00	DB846F65ZAXY (Verizon - Existing)	4	24.352	2.9034	0.0039	1774
78.00	Valmont 13' Low Profile Platform (Verizon - Existing)	4	23.148	2.8355	0.0037	1763
40.00	Standoff	4	5.695	1.3969	0.0012	1295

## Base Plate Design Data

Plate Thickness in	Number of Anchor Bolts	Anchor Bolt Size	Actual Allowable Ratio	Actual Allowable Ratio	Actual Allowable Ratio	Actual Allowable Ratio	Controlling Condition	Critical Ratio
			Bolt Tension lb	Concrete Stress ksi	Plate Stress ksi	Stiffener Stress ksi		
2.7500	16	2.2500	118397.00 223654.40 0.53	2.124 4.080 0.52	28.516 54.000 0.53		Bolt T	0.53

## Compression Checks

## Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> lb	ϕP <sub>n</sub> lb	Ratio P <sub>u</sub> ϕP <sub>n</sub>
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	54.17	0.00	0.0	29.1778	-17002.30	1938050.00	0.009
L2	95.83 - 47.83 (2)	TP41.644x31.9661x0.375	53.17	0.00	0.0	48.4762	-31280.80	3318110.00	0.009
L3	47.83 - 30 (3)	TP41.139x39.7709x0.438	24.00	0.00	0.0	57.4031	-40294.10	4142390.00	0.010
L4	30 - 0 (4)	TP49.6x41.139x0.58	30.00	0.00	0.0	75.7480	-40321.20	5583380.00	0.007

## Pole Bending Design Data

Section No.	Elevation ft	Size	M <sub>ux</sub> lb·ft	ϕM <sub>nx</sub> lb·ft	Ratio M <sub>ux</sub> ϕM <sub>nx</sub>	M <sub>uy</sub> lb·ft	ϕM <sub>ny</sub> lb·ft	Ratio M <sub>uy</sub> ϕM <sub>ny</sub>
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	458458.33	1272216.67	0.360	0.00	1272216.67	0.000
L2	95.83 - 47.83 (2)	TP41.644x31.9661x0.375	1445200.00	2710000.00	0.533	0.00	2710000.00	0.000

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Section No.	Elevation ft	Size	$M_{ux}$ lb-ft	$\phi M_{nx}$ lb-ft	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	$M_{uy}$ lb-ft	$\phi M_{ny}$ lb-ft	Ratio $\frac{M_{uy}}{\phi M_{ny}}$
L3	47.83 - 30 (3)	TP41.139x39.7709x0.438	2102666.67	3425175.00	0.614	0.00	3425175.00	0.000
L4	30 - 0 (4)	TP49.6x41.139x0.58	2102666.67	4584516.67	0.459	0.00	4584516.67	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ lb	$\phi V_n$ lb	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ lb-ft	$\phi T_n$ lb-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	15971.60	969023.00	0.016	196.33	2579658.33	0.000
L2	95.83 - 47.83 (2)	TP41.644x31.9661x0.375	25749.60	1659060.00	0.016	1538.48	5495041.67	0.000
L3	47.83 - 30 (3)	TP41.139x39.7709x0.438	28931.30	2071200.00	0.014	1620.02	6945183.33	0.000
L4	30 - 0 (4)	TP49.6x41.139x0.58	29093.70	2820810.00	0.010	1619.95	9296000.00	0.000

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $P_u$ $\phi P_n$	Ratio $M_{ux}$ $\phi M_{nx}$	Ratio $M_{uy}$ $\phi M_{ny}$	Ratio $V_u$ $\phi V_n$	Ratio $T_u$ $\phi T_n$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	150 - 95.83 (1)	0.009	0.360	0.000	0.016	0.000	0.369	1.000	4.8.2
L2	95.83 - 47.83 (2)	0.009	0.533	0.000	0.016	0.000	0.543	1.000	4.8.2
L3	47.83 - 30 (3)	0.010	0.614	0.000	0.014	0.000	0.624	1.000	4.8.2
L4	30 - 0 (4)	0.007	0.459	0.000	0.010	0.000	0.466	1.000	4.8.2

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	$\phi P_{allow}$ lb	% Capacity	Pass Fail
L1	150 - 95.83	Pole	TP33.469x23.61x0.281	1	-17002.30	1938050.00	36.9	Pass
L2	95.83 - 47.83	Pole	TP41.644x31.9661x0.375	2	-31280.80	3318110.00	54.3	Pass
L3	47.83 - 30	Pole	TP41.139x39.7709x0.438	3	-40294.10	4142390.00	62.4	Pass
L4	30 - 0	Pole	TP49.6x41.139x0.58	4	-40321.20	5583380.00	46.6	Pass
Summary								
Pole (L3)      62.4      Pass								
Base Plate      52.9      Pass								
<b>RATING = 62.4      Pass</b>								

### Element Map

<p><b>tnxTower</b></p> <p><b>Dewberry</b></p> <p>600 Parsippany Road, Suite 301</p> <p>Parsippany, NJ 07054</p> <p>Phone: (973) 739-9400</p> <p>FAX: (973) 739-9710</p>	<b>Job</b>	50093832	<b>Page</b>
	<b>Project</b>	CT2128	<b>Date</b> 13:56:15 01/25/19
	<b>Client</b>	SAI/AT&T	<b>Designed by</b> DAP

<i>Section No.</i>	<i>Section Elevation ft</i>	<i>Component Type</i>	<i>Element List</i>
L1	150.00-95.83	Pole	1
L2	95.83-47.83	Pole	2
L3	47.83-30.00	Pole	3
L4	30.00-0.00	Pole	4 Total number of elements: 4

---

Program Version 7.0.8.5 - 9/29/2017 File:Q:/50055106/50093832/Adm/Reports/TA/tnx/50055106 - CT2128-TA.erl

## **APPENDIX B**

**⚠ This is a beta release of the new ATC Hazards by Location website. Please contact us with feedback.**

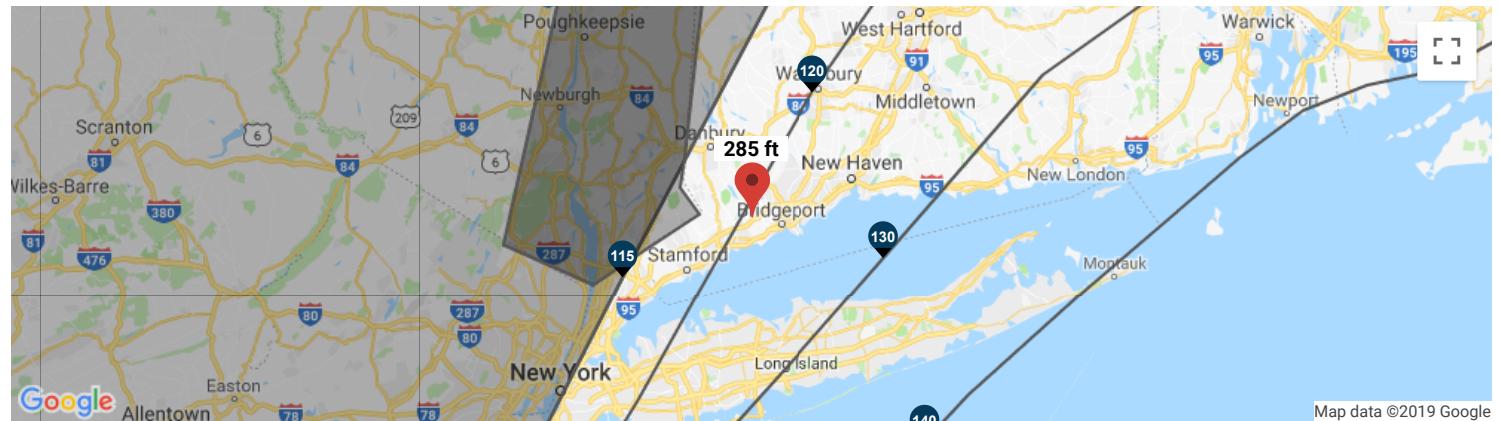


## Hazards by Location

### Search Information

Address:	3965 Congress St, Fairfield, CT 06824, USA
Coordinates:	41.1884172, -73.29858009999998
Timestamp:	2019-01-23T15:12:15.866Z
Hazard Type:	Wind

### Map Results



### Text Results

#### ASCE 7-16

MRI 10-Year	75 mph
MRI 25-Year	84 mph
MRI 50-Year	90 mph
MRI 100-Year	97 mph
Risk Category I	108 mph
Risk Category II	118 mph
Risk Category III	128 mph
Risk Category IV	132 mph <span style="color: orange;">⚠</span>

You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.

#### ASCE 7-10

MRI 10-Year	76 mph
MRI 25-Year	86 mph
MRI 50-Year	93 mph
MRI 100-Year	99 mph
Risk Category I	111 mph
<b>Risk Category II</b>	<b>122 mph</b>

 131 mph**Risk Category III-IV**

If the structure under consideration is a healthcare facility, you are in a wind-borne debris region. If other occupancy, use the Risk Category II basic wind speed contours to determine if you are in a wind-borne debris region.

**ASCE 7-05****ASCE 7-05 Wind Speed** 110 mph

You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.

*The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.*

**Disclaimer**

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

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**8-Port Antenna**

R1	R2	Y1	Y2
----	----	----	----

**Frequency Range**

698–960	698–960	1695–2690	1695–2690
---------	---------	-----------	-----------

**Dual Polarization**

X	X	X	X
---	---	---	---

**HPBW**

65°	65°	65°	65°
-----	-----	-----	-----

**Adjust. Electr. DT**

2°–12°	2°–12°	2.5°–12°	2.5°–12°
--------	--------	----------	----------

set by **FlexRET****KATHREIN**

**8-Port Antenna 698–960/698–960/1695–2690/1695–2690 65°/65°/65°/65° 15.5/15.5/18/18dBi  
2°–12°/2°–12°/2.5°–12°/2.5°–12°T**

Type No.	<b>80010965</b>				
Left side, lowband	<b>R1, connector 1–2</b>				
		<b>698–960</b>			
Frequency Range	MHz	698 – 806	790 – 862	824 – 894	880 – 960
Gain at mid Tilt	dBi	14.8	15.4	15.6	15.9
Gain over all Tilts	dBi	14.8 ± 0.6	15.4 ± 0.4	15.6 ± 0.2	15.8 ± 0.2
<b>Horizontal Pattern:</b>					
Azimuth Beamwidth	°	62 ± 3.9	61 ± 3.2	60 ± 2.7	60 ± 2.1
Front-to-Back Ratio, Total Power, ± 30°	dB	> 22	> 25	> 27	> 25
<b>Vertical Pattern:</b>					
Elevation Beamwidth	°	11.9 ± 0.8	11.0 ± 0.8	10.5 ± 0.4	10.2 ± 0.4
Electrical Downtilt continuously adjustable	°	2.0 – 12.0			
Tilt Accuracy	°	< 0.7	< 0.7	< 0.7	< 0.7
First Upper Side Lobe Suppression	dB	> 14	> 14	> 15	> 14
Cross Polar Isolation	dB	> 30			
Port to Port Isolation	dB	> 27 (R1 // R2) > 30 (R1 // Y1, Y2)			
Max. Effective Power per Port	W	400 (at 50 °C ambient temperature)			
Max. Effective Power Port 1–2	W	800 (at 50 °C ambient temperature)			

Values based on NGMN-P-BASTA (version 9.6) requirements.



Right side, lowband		R2, connector 3–4			
		698–960			
Frequency Range	MHz	698 – 806	790 – 862	824 – 894	880 – 960
Gain at mid Tilt	dBi	14.8	15.3	15.5	15.8
Gain over all Tilts	dBi	14.8 ± 0.6	15.3 ± 0.3	15.5 ± 0.3	15.7 ± 0.3
<b>Horizontal Pattern:</b>					
Azimuth Beamwidth	°	63 ± 3.6	62 ± 1.8	62 ± 2.1	60 ± 3.7
Front-to-Back Ratio, Total Power, ± 30°	dB	> 22	> 24	> 26	> 27
<b>Vertical Pattern:</b>					
Elevation Beamwidth	°	11.6 ± 0.7	11.0 ± 0.6	10.7 ± 0.4	10.2 ± 0.5
Electrical Downtilt continuously adjustable	°	2.0 – 12.0			
Tilt Accuracy	°	< 0.7	< 0.6	< 0.6	< 0.5
First Upper Side Lobe Suppression	dB	> 14	> 16	> 16	> 16
Cross Polar Isolation	dB	> 30			
Port to Port Isolation	dB	> 27 (R2 // R1) > 30 (R2 // Y1, Y2)			
Max. Effective Power per Port	W	400 (at 50 °C ambient temperature)			
Max. Effective Power Port 3–4	W	800 (at 50 °C ambient temperature)			

Values based on NGMN-P-BASTA (version 9.6) requirements.

Left side, highband		Y1, connector 5–6			
		1695–2690			
Frequency Range	MHz	1695 – 1880	1850 – 1990	1920 – 2180	2300 – 2400
Gain at mid Tilt	dBi	17.6	17.9	18.3	18.1
Gain over all Tilts	dBi	17.5 ± 0.4	17.8 ± 0.4	18.1 ± 0.5	18.0 ± 0.6
<b>Horizontal Pattern:</b>					
Azimuth Beamwidth	°	62 ± 5.1	65 ± 4.1	62 ± 7.2	56 ± 4.1
Front-to-Back Ratio, Total Power, ± 30°	dB	> 22	> 25	> 25	> 25
<b>Vertical Pattern:</b>					
Elevation Beamwidth	°	6.4 ± 0.5	5.9 ± 0.3	5.5 ± 0.4	4.8 ± 0.3
Electrical Downtilt continuously adjustable	°	2.5 – 12.0			
Tilt Accuracy	°	< 0.2	< 0.1	< 0.2	< 0.3
First Upper Side Lobe Suppression	dB	> 19	> 18	> 16	> 18
Cross Polar Isolation	dB	> 28			
Port to Port Isolation	dB	> 30 (Y1 // R1, R2, Y2)			
Max. Effective Power per Port	W	200 (at 50 °C ambient temperature)			
Max. Effective Power Port 5–6	W	400 (at 50 °C ambient temperature)			

Values based on NGMN-P-BASTA (version 9.6) requirements.

Right side, highband		Y2, connector 7-8				
		1695–2690				
Frequency Range	MHz	1695 – 1880	1850 – 1990	1920 – 2180	2300 – 2400	2490 – 2690
Gain at mid Tilt	dBi	17.5	18.0	18.3	18.2	17.9
Gain over all Tilts	dBi	17.4 ± 0.4	17.8 ± 0.4	18.1 ± 0.6	18.0 ± 0.7	17.8 ± 0.7
<b>Horizontal Pattern:</b>						
Azimuth Beamwidth	°	65 ± 4.7	66 ± 4.7	62 ± 7.8	57 ± 3.8	59 ± 7.1
Front-to-Back Ratio, Total Power, ± 30°	dB	> 24	> 26	> 26	> 25	> 24
<b>Vertical Pattern:</b>						
Elevation Beamwidth	°	6.4 ± 0.4	5.9 ± 0.3	5.5 ± 0.5	4.8 ± 0.3	4.4 ± 0.3
Electrical Downtilt continuously adjustable	°	2.5 – 12.0				
Tilt Accuracy	°	< 0.2	< 0.2	< 0.2	< 0.3	< 0.2
First Upper Side Lobe Suppression	dB	> 18	> 18	> 15	> 17	> 16
Cross Polar Isolation	dB	> 28				
Port to Port Isolation	dB	> 30 (Y2 // R1, R2, Y1)				
Max. Effective Power per Port	W	200 (at 50 °C ambient temperature)				
Max. Effective Power Port 7-8	W	400 (at 50 °C ambient temperature)				

Values based on NGMN-P-BASTA (version 9.6) requirements.

Electrical specifications, all systems		
Impedance	Ω	50
VSWR		< 1.5
Return Loss	dB	> 14
Interband Isolation	dB	> 27
Passive Intermodulation	dBc	< -153 (2 x 43 dBm carrier)
Polarization	°	+45, -45
Max. Effective Power for the Antenna	W	1200 (at 50 °C ambient temperature)

Values based on NGMN-P-BASTA (version 9.6) requirements.

Mechanical specifications		
Input	8 x 4.3-10 female	
Connector Position		bottom
Adjustment Mechanism		FlexRET, continuously adjustable
Wind load (at Rated Wind Speed: 150 km/h (93 mph))	N   lbf	Frontal: 1130   254 Maximal: 1140   256
Max. Wind Velocity	km/h mph	241 150
Height / Width / Depth	mm inches	1999 / 508 / 175 78.7 / 20.0 / 6.9
Category of Mounting Hardware		XH (X-Heavy)
Weight	kg lb	44.3 / 49.3 (clamps incl.) 97.6 / 108.6 (clamps incl.)
Packing Size	mm inches	2200 / 542 / 268 86.6 / 21.3 / 10.6
Scope of Supply		Panel, FlexRET and clamps for 55–115 mm   2.2–4.5 inches diameter

## Accessories (order separately if required)

Type No.	Description	Remarks mm   inches	Weight approx. kg   lb	Units per antenna
85010097	2 clamps	Mast diameter: 110 – 220   4.3 – 8.7	9.4   20.7	1
85010099	1 downtilt kit	Downtilt angle: 0° – 13°	10.6   23.4	1
86010154	Site Sharing Adapter	3-way (see figure below)	0.7   1.5	
86010155	Site Sharing Adapter	6-way (see figure below)	1.4   3.1	
86010162	Gender Adapter	Solely to be used in combination with the FlexRET module 86010153v01	0.045   0.099	1
86010163	Port Extender		0.16   0.35	1

## Accessories (included in the scope of supply)

85010096	2 clamps	Mast diameter: 55 – 115   2.2 – 4.5	5.0   11.0	1
86010153v01	FlexRET			1

For downtilt mounting use the clamps for an appropriate mast diameter together with the downtilt kit.  
Wall mounting: No additional mounting kit needed.

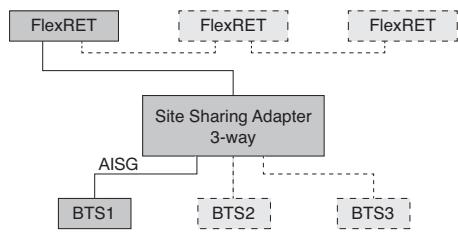
**Material:** Reflector screen: Aluminum.

Fiberglass housing: It covers totally the internal antenna components. The special design reduces the sealing areas to a minimum and guarantees the best weather protection. Fiberglass material guarantees optimum performance with regards to stability, stiffness, UV resistance and painting. The color of the radome is light grey.

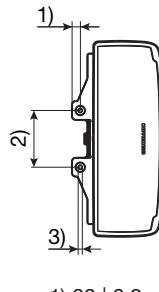
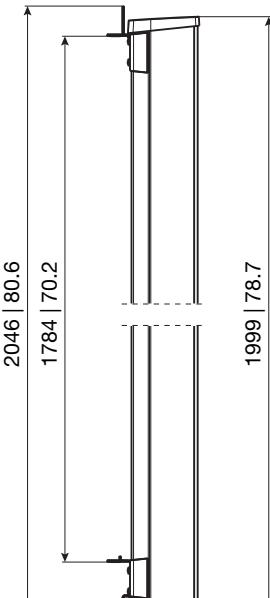
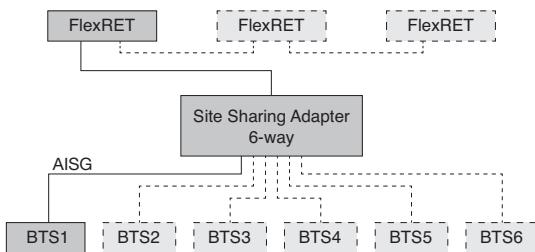
All nuts and bolts: Stainless steel or hot-dip galvanized steel.

**Grounding:** The metal parts of the antenna including the mounting kit and the inner conductors are DC grounded.

## Configuration example with Site Sharing Adapter 86010154

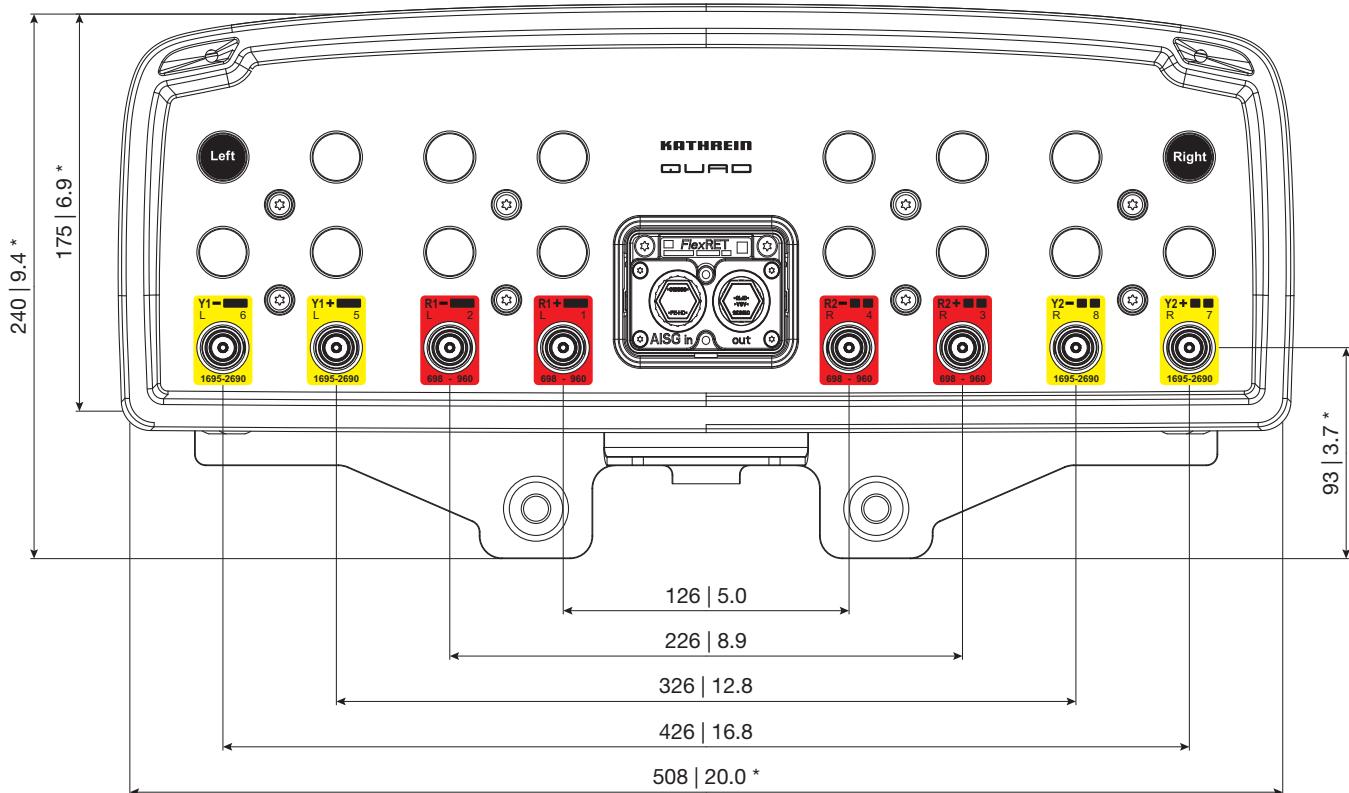


## Configuration example with Site Sharing Adapter 86010155



1) 22 | 0.9  
2) 150 | 5.9  
3) Ø 11 | 0.4  
All dimensions in mm | inches

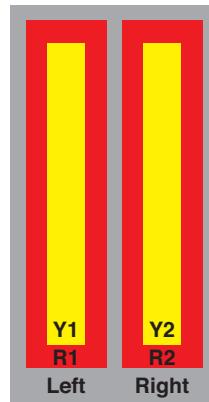
For more information please refer to the respective data sheets.

**Layout of interface:**

Bottom view  
 \* Dimensions refer to radome  
 All dimensions in mm | inches

**Correlation Table**

Frequency range	Array	Connector
698– 960 MHz	R1	1–2
698– 960 MHz	R2	3–4
1695–2690 MHz	Y1	5–6
1695–2690 MHz	Y2	7–8

**Order Information**

Model	Description
80010965	8-Port antenna with mounting bracket
80010965K	8-Port antenna with mounting bracket and mechanical tilt bracket

Section 1 - RFDS GENERAL INFORMATION												
RFDS NAME:	CT2128	DATE:	9/19/2018	RF DESIGN ENG:	Mohammed Rahman	RF PERF ENG:		RFDS PROGRAM TYPE:	2019 LTE Next Carrier			
ISSUE:	Bronze Standard	Approved? (Y/N):	Yes	RF DESIGN PHONE:	860-258-6350	RF PERF PHONE:		RFDS TECHNOLOGY:	LTE			
REVISION:	Preliminary	RF MANAGER:	John Benedetto	RF DESIGN EMAIL:	mr673a@att.com	RF PERF EMAIL:		STATE/STATUS:	Preliminary/Approved			
INITIATIVE / PROJECT:	LTE 3C[WCS], LTE 4C[850 B(U)], 4TX4RX Software Retrofit[700 B-C]											
RFDs Version:	1.00		RFDs ID:	2571812			GSM FREQUENCY:	Created By:	mr673a	Updated By:	mr673a	
UMTS FREQUENCY:	850		Created:	9/19/2018			LTE FREQUENCY:	Created:	9/19/2018	Updated:	10/18/2018	
5G FREQUENCY:	850		IPLAN JOB # 1:	NER-RCTB-18-07131			PRD    SUB GRP #1:	LTE Next Carrier    LTE 3C				
			IPPLAN JOB # 2:	NER-RCTB-18-07200			PRD    SUB GRP #2:	LTE Next Carrier    LTE 4C				
			IPPLAN JOB # 3:	NER-RCTB-18-07467			PRD    SUB GRP #3:	Antenna Modifications    4TX4RX Software Retrofit				
			IPPLAN JOB # 4:				PRD    SUB GRP #4:					
			IPPLAN JOB # 5:				PRD    SUB GRP #5:					
			IPPLAN JOB # 6:				PRD    SUB GRP #6:					
			IPPLAN JOB # 7:				PRD    SUB GRP #7:					
			IPPLAN JOB # 8:				PRD    SUB GRP #8:					
Section 2 - LOCATION INFORMATION												
USID:	5787	FA LOCATION CODE:	10035251	LOCATION NAME:	FAIRFIELD GREENFIELD HILL	ORACLE PRJT # 1:	2051A0KPJV	PACE JOB #1:	MRCTB035112			
REGION:	NORTHEAST	MARKET CLUSTER:	NEW ENGLAND	MARKET:	CONNECTICUT	ORACLE PRJT # 2:	2051A0KPH8	PACE JOB #2:	MRCTB035164			
ADDRESS:	3965 CONGRESS STREET	CITY:	FAIRFIELD	STATE:	CT	ORACLE PRJT # 3:	2051A0KQB3	PACE JOB #3:	MRCTB035334			
ZIP CODE:	06824	COUNTY:	FAIRFIELD	LONG (DEC. DEG.):	-73.2990550	ORACLE PRJT # 4:		PACE JOB #4:				
LATITUDE (D-M-S):	41d 11m 18.17196s	LONGITUDE (D-M-S):	-73d 17m 56.598s	LAT (DEC. DEG.):	41.1883811	ORACLE PRJT # 5:		PACE JOB #5:				
DIRECTIONS, ACCESS AND EQUIPMENT LOCATION:	UPDATED 4/04 CT-083 FAIRFIELD-GREENFIELD HILL TAKE RT. 17 NORTH TO GARDEN STATE PARKWAY NORTH TO I-87 SOUTH. GO ACROSS TAPPAN ZEE BRIDGE; FOLLOW SIGNS TO I-287 EAST; ONCE ON I-287 YOU WILL GET OFF EXIT 9N FOR THE HUTCHINSON AND MERRITT PARKWAY YOU NEED TO											
FREQ COORD:			BTA:		MSA / RSA:							
OPS DISTRICT:	CT-South		LAC(GSM):									
OPS ZONE:	NE_CT_S_FRFD_CTL_CS		LAC(UMTS):	05989								
RF DISTRICT:	NPO Triage		BSC(GSM):									
RF ZONE:	Hotseat		RNC(UMTS):	BRIDGEPORT RNC06 ERICSSON 3820								
PARENT NAME(GSM):			MME POOL ID(LTE):	FF01								
PARENT NAME(UMTS):	BRPTCT04CRBR06											
Section 3 - LICENSE COVERAGE/FILING INFORMATION												
CGSA - NO FILING TRIGGERED (Yes/No):	No	CGSA LOSS:		PCS REDUCED - UPS ZIP:		CGSA CALL SIGNS:						
CGSA - MINOR FILING NEEDED (Yes/No):	No	CGSA EXT AGMT NEEDED:		PCS POPS REDUCED:								
CGSA - MAJOR FILING NEEDED (Yes/No):	Yes	CGSA SCORECARD UPDATED:										
Section 4 - TOWER/REGULATORY INFORMATION												
STRUCTURE AT&T OWNED?:	Yes	GROUND ELEVATION (ft):		STRUCTURE TYPE:	MONOPOLE	MARKET LOCATION 700 MHz Band:						
ADDITIONAL REGULATORY?:	Yes	HEIGHT OVERALL (ft):	90.00	FCC ASR NUMBER:	NR	MARKET LOCATION 850 MHz Band:						
SUB-LEASE RIGHTS?:	Yes	STRUCTURE HEIGHT (ft):	90.00			MARKET LOCATION 1900 MHz Band:						
LIGHTING TYPE:	NOT REQUIRED					MARKET LOCATION AWS Band:						
						MARKET LOCATION WCS Band:						
						MARKET LOCATION Future Band:						
Section 5 - E-911 INFORMATION - existing												
SECTOR A E-911	PSAP NAME:	PSAP ID:	E911 PHASE:	MPC SVC PROVIDER:	LMU REQUIRED:	ESRN:	DATE LIVE PH1:	DATE LIVE PH2:				
SECTOR B				INTRADO_MIAAMI	0							
SECTOR C				INTRADO_MIAAMI	0							
SECTOR D				INTRADO_MIAAMI	0							
SECTOR E												
SECTOR F												
OMNI												
Section 5 - E-911 INFORMATION - final												
SECTOR A E-911	PSAP NAME:	PSAP ID:	E911 PHASE:	MPC SVC PROVIDER:	LMU REQUIRED:	ESRN:	DATE LIVE PH1:	DATE LIVE PH2:				
SECTOR B				INTRADO_MIAAMI	0							
SECTOR C				INTRADO_MIAAMI	0							
SECTOR D				INTRADO_MIAAMI	0							
SECTOR E												

SECTOR F								
OMNI								

## **Section 6 - RBS GENERAL INFORMATION - existing**

## **Section 6 - RBS GENERAL INFORMATION - final**

**Section 7 - RBS SPECIFIC INFORMATION - existing**

	UMTS 1ST RBS	UMTS 2ND RBS	UMTS 3RD RBS	LTE 1ST RBS	5G 1ST RBS																	
<b>RAC:</b>																						
<b>EQUIPMENT VENDOR:</b>	ERICSSON	ERICSSON	ERICSSON	ERICSSON																		
<b>EQUIPMENT TYPE:</b>	3206 INDOOR	3206 INDOOR	6601 MAIN UNIT UMTS	6601 INDOOR MU																		
<b>BASEBAND CONFIGURATION:</b>																						
<b>LOCATION:</b>																						
<b>CABINET LOCATION:</b>																						
<b>MARKET STATE CODE:</b>					CT																	
<b>AGPS:</b>	Yes	Yes	Yes	Yes																		
<b>NODE B NUMBER:</b>	0	0	0	2128																		

**Section 7 - RBS SPECIFIC INFORMATION - final**

	UMTS 1ST RBS	UMTS 2ND RBS	UMTS 3RD RBS	LTE 1ST RBS	5G 1ST RBS																		
<b>RAC:</b>																							
<b>EQUIPMENT VENDOR:</b>	ERICSSON	ERICSSON	ERICSSON	ERICSSON	ERICSSON																		
<b>EQUIPMENT TYPE:</b>	3206 INDOOR	3206 INDOOR	6601 MAIN UNIT UMTS	6601 INDOOR MU	6601 INDOOR MU																		
<b>BASEBAND CONFIGURATION:</b>					1x6601 / 1x6630 / 1xXMU03	xxxxx / 1x6630 / xxxx																	
<b>LOCATION:</b>																							
<b>CABINET LOCATION:</b>																							
<b>MARKET STATE CODE:</b>					CT	CT																	
<b>AGPS:</b>	Yes	Yes	Yes	Yes	Yes																		
<b>NODE B NUMBER:</b>	0	0	0	2128	2128																		

**Section 8 - RBS/SECTOR ASSOCIATION - existing**

	UMTS 1ST RBS	UMTS 2ND RBS	UMTS 3RD RBS	LTE 1ST RBS	5G 1ST RBS																
<b>CTS Common ID</b>	CTU2128	CTV2128	CTU6128	CTL02128																	
<b>Soft Sector IDs</b>	CTU21287	CTV21281	CTV6128A	CTL02128_7A_1																	
	CTU21288	CTV21282	CTV6128B	CTL02128_7B_1																	
	CTU21289	CTV21283	CTV6128C	CTL02128_7C_1																	
				CTL02128_9A_1																	
				CTL02128_9A_2																	
				CTL02128_9B_1																	
				CTL02128_9B_2																	
				CTL02128_9C_1																	
				CTL02128_9C_2																	

**Section 8 - RBS/SECTOR ASSOCIATION - final**

	UMTS 1ST RBS	UMTS 2ND RBS	UMTS 3RD RBS	LTE 1ST RBS	5G 1ST RBS																
<b>CTS Common ID</b>	CTU2128	CTV2128	CTU6128	CTL02128	CTN0002128																
<b>Soft Sector IDs</b>	CTU21287	CTV21281		CTL02128_3A_1	CTN0002128_F1NSA_1																
	CTV21282			CTL02128_3B_1	CTN0002128_F1NSB_1																
	CTV21283			CTL02128_3C_1	CTN0002128_F1NSC_1																
				CTL02128_7A_1																	
				CTL02128_7B_1																	
				CTL02128_7C_1																	
				CTL02128_8A_1																	
				CTL02128_8B_1																	
				CTL02128_8C_1																	
				CTL02128_9A_1																	
				CTL02128_9A_2																	
				CTL02128_9B_1																	
				CTL02128_9B_2																	
				CTL02128_9C_1																	
				CTL02128_9C_2																	

**Section 9 - SOFT SECTOR ID - existing**

	UMTS 1ST 850	UMTS 1ST 1900	UMTS 2ND 850	LTE 1ST 700	LTE 1ST 850	LTE 1ST 1900	LTE 1ST WCS	LTE 2ND 1900	5G 1ST 850																	
USEID (excluding Hard Sector)	5787.850.3G.1	5787.1900.3G.1	5787.850.3G.2																							
SECTOR A SOFT SECTOR ID	CTV21281	CTU21287	CTV6128A	CTL02128_7A_1		CTL02128_9A_1		CTL02128_9A_2																		
SECTOR B	CTV21282	CTU21288	CTV6128B	CTL02128_7B_1		CTL02128_9B_1		CTL02128_9B_2																		
SECTOR C	CTV21283	CTU21289	CTV6128C	CTL02128_7C_1		CTL02128_9C_1		CTL02128_9C_2																		
SECTOR D																										
SECTOR E																										
SECTOR F																										
OMNI																										

**Section 9 - SOFT SECTOR ID - final**

	UMTS 1ST 850	UMTS 1ST 1900	UMTS 2ND 850	LTE 1ST 700	LTE 1ST 850	LTE 1ST 1900	LTE 1ST WCS	LTE 2ND 1900	5G 1ST 850																	
USEID (excluding Hard Sector)	5787.850.3G.1																									
SECTOR A SOFT SECTOR ID	CTV21281			CTL02128_7A_1	CTL02128_8A_1	CTL02128_9A_1	CTL02128_3A_1	CTL02128_9A_2	CTN0002128_F1NSA_1																	
SECTOR B	CTV21282			CTL02128_7B_1	CTL02128_8B_1	CTL02128_9B_1	CTL02128_3B_1	CTL02128_9B_2	CTN0002128_F1NSB_1																	
SECTOR C	CTV21283			CTL02128_7C_1	CTL02128_8C_1	CTL02128_9C_1	CTL02128_3C_1	CTL02128_9C_2	CTN0002128_F1NSC_1																	
SECTOR D																										
SECTOR E																										
SECTOR F																										
OMNI																										













**Section 15A - CURRENT TOWER CONFIGURATION - SECTOR A (OR OMNI)**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
<b>ANTENNA MAKE - MODEL</b>	7770	7770		HPA-65R-BUU-H6			
<b>ANTENNA VENDOR</b>	Powerwave	Powerwave		CCI			
<b>ANTENNA SIZE (H x W x D)</b>	55X11X5	55X11X5		72X14.8X9			
<b>ANTENNA WEIGHT</b>	35	35		50.7			
<b>AZIMUTH</b>	143	143		30			
<b>MAGNETIC DECLINATION</b>							
<b>RADIATION CENTER (feet)</b>	128.03	128.03		128.03			
<b>ANTENNA TIP HEIGHT</b>							
<b>MECHANICAL DOWNTILT</b>	0	0		0			
<b>FEEDER AMOUNT</b>	2	2					
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>							
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>							
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>							
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>							
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>							
<b>Antenna RET Motor (QTY/MODEL)</b>	2	Powerwave 7020	2	Powerwave 7020		Internal	
<b>SURGE ARRESTOR (QTY/MODEL)</b>				1	DC/Fiber Squid		
<b>DIPLEXER (QTY/MODEL)</b>	2	Powerwave / LGP 21901	2	Powerwave / LGP 21901			
<b>DUPLEXER (QTY/MODEL)</b>							
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>			1	Kathrein / 860-10006		LTE RRH	
<b>DC BLOCK (QTY/MODEL)</b>							
<b>TMA/LNA (QTY/MODEL)</b>	2	21401 (Dual Band - 850)	2	21401 (Dual Band - 850)			
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>	2	Polyphaser 1000860	2	Polyphaser 1000860			
<b>PDU FOR TMAS (QTY/MODEL)</b>	1	LGP 12104 ( 850 Bypass TMA )	1	LGP 12104 ( 850 Bypass TMA )			
<b>FILTER (QTY/MODEL)</b>							
<b>SQUID (QTY/MODEL)</b>							
<b>FIBER TRUNK (QTY/MODEL)</b>							
<b>DC TRUNK (QTY/MODEL)</b>							
<b>REPEATER (QTY/MODEL)</b>							
<b>RRH - 700 band (QTY/MODEL)</b>				1	RRUS-11 (REUSE ONLY)		
<b>RRH - 850 band (QTY/MODEL)</b>							
<b>RRH - 1900 band (QTY/MODEL)</b>				1	RRUS-12+RRUS-A2		
<b>RRH - AWS band (QTY/MODEL)</b>							
<b>RRH - WCS band (QTY/MODEL)</b>							
<b>Additional RRH #1 - any band (QTY/MODEL)</b>							
<b>Additional RRH #2 - any band (QTY/MODEL)</b>							
<b>Additional Component 1 (QTY/MODEL)</b>							
<b>Additional Component 2 (QTY/MODEL)</b>							
<b>Additional Component 3 (QTY/MODEL)</b>							
<b>Local Market Note 1</b>							
<b>Local Market Note 2</b>							
<b>Local Market Note 3</b>							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 1	PORT 1		5787.A.850.3G.1	CTV21281	CTV21281		UMTS 850	7770.00.850.07	13.5	143	7	None	Commscope 1-1/4 (850)	155.039685						252.35		1	
	PORT 2		5787.A.850.3G.1	CTV6128A	CTV6128A		UMTS 850	7770.00.850.07	13.5	143	7	None	Commscope 1-1/4 (850)	155.039685						252.35		1	
	PORT 3		5787.A.1900.3G.1	CTU21287	CTU21287		UMTS 1900	7770.00.1900.03	15.5	143	3	None	Commscope 1-1/4 (1900)	155.039685						323.59		2	

ANTENNA POSITION 2	PORT 1	5787.A.850.25G.1	321G21281	321G21281		GSM 850	7770.00.850.07	13.5	143	7	None	1-1/4 at 850 MHz	155.039685							11.22	131.21		3
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ANTENNA POSITION 4	PORT 1		5787.A.700.4G.1	CTL02128_7A_1	CTL02128_7A_1		LTE 700	H6_719MHz_02 DT	14.27	30	2	TOP	FIBER	0						1475.7065		7	
	PORT 3		5787.A.1900.4G.1	1	CTL02128_9A_1	CTL02128_9A_1	LTE 1900	H6_1930MHz_03 DT	17	30	3	TOP	FIBER	0						3664.3757		8	

	PORT 4	5787.A.1900.4G. 2	CTL02128_9A_2	CTL02128_9A_2	LTE 1900	H6_1930MHz_03 DT	17	30	3	TOP	FIBER	0						3664.3757		8	
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**Section 15B - CURRENT TOWER CONFIGURATION - SECTOR B**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7	
<b>ANTENNA MAKE - MODEL</b>	7770	7770		HPA-65R-BUU-H6				
<b>ANTENNA VENDOR</b>	Powerwave	Powerwave		CCI				
<b>ANTENNA SIZE (H x W x D)</b>	55X11X5	55X11X5		72X14.8X9				
<b>ANTENNA WEIGHT</b>	35	35		50.7				
<b>AZIMUTH</b>	263	263		150				
<b>MAGNETIC DECLINATION</b>								
<b>RADIATION CENTER (feet)</b>	128.03	128.03		128.03				
<b>ANTENNA TIP HEIGHT</b>								
<b>MECHANICAL DOWNTILT</b>	0	0		0				
<b>FEEDER AMOUNT</b>	2	2						
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>								
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>								
<b>Antenna RET Motor (QTY/MODEL)</b>	2	Powerwave 7020	2	Powerwave 7020		Internal		
<b>SURGE ARRESTOR (QTY/MODEL)</b>								
<b>DIPLEXER (QTY/MODEL)</b>	2	Powerwave / LGP 21901	2	Powerwave / LGP 21901				
<b>DUPLEXER (QTY/MODEL)</b>								
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>					LTE RRH			
<b>DC BLOCK (QTY/MODEL)</b>								
<b>TMA/LNA (QTY/MODEL)</b>	2	21401 (Dual Band - 850)	2	21401 (Dual Band - 850)				
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>	2	Polyphaser 1000860	2	Polyphaser 1000860				
<b>PDU FOR TMAS (QTY/MODEL)</b>								
<b>FILTER (QTY/MODEL)</b>								
<b>SQUID (QTY/MODEL)</b>								
<b>FIBER TRUNK (QTY/MODEL)</b>								
<b>DC TRUNK (QTY/MODEL)</b>								
<b>REPEATER (QTY/MODEL)</b>								
<b>RRH - 700 band (QTY/MODEL)</b>				1	RRUS-11 (REUSE ONLY)			
<b>RRH - 850 band (QTY/MODEL)</b>				1	RRUS-12+RRUS-A2			
<b>RRH - 1900 band (QTY/MODEL)</b>				1				
<b>RRH - AWS band (QTY/MODEL)</b>								
<b>RRH - WCS band (QTY/MODEL)</b>								
<b>Additional RRH #1 - any band (QTY/MODEL)</b>								
<b>Additional RRH #2 - any band (QTY/MODEL)</b>								
<b>Additional Component 1 (QTY/MODEL)</b>								
<b>Additional Component 2 (QTY/MODEL)</b>								
<b>Additional Component 3 (QTY/MODEL)</b>								
<b>Local Market Note 1</b>								
<b>Local Market Note 2</b>								
<b>Local Market Note 3</b>								

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 1	PORT 1		5787.B.850.3G.1	CTV21282	CTV21282		UMTS 850	7770.00.850.07	13.5	263	7	None	Commscope 1-1/4 (850)	155.039685						252.35		9	
	PORT 2		5787.B.850.3G.1	CTV6128B	CTV6128B		UMTS 850	7770.00.850.07	13.5	263	7	None	Commscope 1-1/4 (850)	155.039685						252.35		9	
	PORT 3		5787.B.1900.3G.1	CTU21288	CTU21288		UMTS 1900	7770.00.1900.06	15.5	263	6	None	Commscope 1-1/4 (1900)	155.039685						323.59		10	

ANTENNA POSITION 2	PORT 1	5787.B.850.25G.1	321G21282	321G21282		GSM 850	7770.00.850.07	13.5	263	7	None	1-1/4 at 850 MHz	155.039685							12.58	147.23		11	
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ANTENNA POSITION 4	PORT 1		5787.B.700.4G.1	CTL02128_7B_1	CTL02128_7B_1		LTE 700	H6_719MHz_07 DT	14.02	150	7	TOP	FIBER	0						1475.7065		15		
	PORT 3		5787.B.1900.4G.1	CTL02128_9B_1	CTL02128_9B_1		LTE 1900	H6_1930MHz_02 DT	16.85	150	2	TOP	FIBER	0						3664.3757		16		

	PORT 4	5787.B.1900.4G. 2	CTL02128_9B_2	CTL02128_9B_2	LTE 1900	H6_1930MHz_02 DT	16.85	150	2	TOP	FIBER	0					3664.3757		16	
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**Section 15C - CURRENT TOWER CONFIGURATION - SECTOR C**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7															
<b>ANTENNA MAKE - MODEL</b>	7770	7770			HPA-65R-BUU-H6																	
<b>ANTENNA VENDOR</b>	Powerwave	Powerwave			CCI																	
<b>ANTENNA SIZE (H x W x D)</b>	55X11X5	55X11X5			72X14.8X9																	
<b>ANTENNA WEIGHT</b>	35	35			50.7																	
<b>AZIMUTH</b>	23	23			270																	
<b>MAGNETIC DECLINATION</b>																						
<b>RADIATION CENTER (feet)</b>	128.03	128.03			128.03																	
<b>ANTENNA TIP HEIGHT</b>																						
<b>MECHANICAL DOWNTILT</b>	0	0			0																	
<b>FEEDER AMOUNT</b>	2	2																				
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>																						
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>																						
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>																						
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>																						
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>																						
<b>Antenna RET Motor (QTY/MODEL)</b>	2	Powerwave 7020	2	Powerwave 7020			Internal															
<b>SURGE ARRESTOR (QTY/MODEL)</b>																						
<b>DIPLEXER (QTY/MODEL)</b>	2	Powerwave / LGP 21901	2	Powerwave / LGP 21901																		
<b>DUPLEXER (QTY/MODEL)</b>																						
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>							LTE RRH															
<b>DC BLOCK (QTY/MODEL)</b>																						
<b>TMA/LNA (QTY/MODEL)</b>	2	21401 (Dual Band - 850	2	21401 (Dual Band - 850																		
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>	2	Polyphaser 1000860	2	Polyphaser 1000860																		
<b>PDU FOR TMAS (QTY/MODEL)</b>																						
<b>FILTER (QTY/MODEL)</b>																						
<b>SQUID (QTY/MODEL)</b>																						
<b>FIBER TRUNK (QTY/MODEL)</b>																						
<b>DC TRUNK (QTY/MODEL)</b>																						
<b>REPEATER (QTY/MODEL)</b>																						
<b>RRH - 700 band (QTY/MODEL)</b>					1	RRUS-11 (REUSE ONLY)																
<b>RRH - 850 band (QTY/MODEL)</b>																						
<b>RRH - 1900 band (QTY/MODEL)</b>					1	RRUS-12+RRUS-A2																
<b>RRH - AWS band (QTY/MODEL)</b>																						
<b>RRH - WCS band (QTY/MODEL)</b>																						
<b>Additional RRH #1 - any band (QTY/MODEL)</b>																						
<b>Additional RRH #2 - any band (QTY/MODEL)</b>																						
<b>Additional Component 1 (QTY/MODEL)</b>																						
<b>Additional Component 2 (QTY/MODEL)</b>																						
<b>Additional Component 3 (QTY/MODEL)</b>																						
<b>Local Market Note 1</b>																						
<b>Local Market Note 2</b>																						
<b>Local Market Note 3</b>																						

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/ Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIR KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
<b>ANTENNA POSITION 1</b>	<b>PORT 1</b>	5787.C.850.3G.1	CTV21283	CTV21283			UMTS 850	7770.00.850.06	13.5	23	6	None	Commscope 1-1/4 (850)	155.039685						252.35		17	
	<b>PORT 2</b>	5787.C.850.3G.1	CTV6128C	CTV6128C			UMTS 850	7770.00.850.06	13.5	23	6	None	Commscope 1-1/4 (850)	155.039685						252.35		17	
	<b>PORT 3</b>	5787.C.1900.3G.1	CTU21289	CTU21289			UMTS 1900	7770.00.1900.02	15.5	23	2	None	Commscope 1-1/4 (1900)	155.039685						323.59		18	

<b>ANTENNA POSITION 2</b>	<b>PORT 1</b>	5787.C.850.25G.1	321G21283	321G21283			GSM 850	7770.00.850.06	13.5	23	6	None	1-1/4 at 850 MHz	155.039685						17.78	207.96		19	
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<b>ANTENNA POSITION 4</b>	<b>PORT 1</b>	5787.C.700.4G.1	CTL02128_7C_1	CTL02128_7C_1			LTE 700	H6_719MHz_02 DT	14.27	270	2	TOP	FIBER</
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	PORT 4	5787.C.1900.4G. 2	CTL02128_9C_2	CTL02128_9C_2	LTE 1900	H6_1930MHz_02 DT	16.85	270	2	TOP	FIBER	0					3664.3757		24	
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**Section 16A - PLANNED/PROPOSED TOWER CONFIGURATION - SECTOR A (OR OMNI)**

ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7										
Existing Antenna?																	
ANTENNA MAKE - MODEL		800-10965															
ANTENNA VENDOR		Kathrein															
ANTENNA SIZE (H x W x D)		78.7X20X6.9															
ANTENNA WEIGHT		108.6															
AZIMUTH		30															
MAGNETIC DECLINATION																	
RADIATION CENTER (feet)		128.03															
ANTENNA TIP HEIGHT																	
MECHANICAL DOWNTILT		0															
FEEDER AMOUNT																	
VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)																	
VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)																	
HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)																	
HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)																	
HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)																	
Antenna RET Motor (QTY/MODEL)				Internal													
SURGE ARRESTOR (QTY/MODEL)		1	DC/Fiber Squid														
DIPLEXER (QTY/MODEL)																	
DUPLEXER (QTY/MODEL)																	
Antenna RET CONTROL UNIT (QTY/MODEL)			LTE RRH														
DC BLOCK (QTY/MODEL)																	
TMA/LNA (QTY/MODEL)																	
CURRENT INJECTORS FOR TMA (QTY/MODEL)																	
PDU FOR TMAS (QTY/MODEL)																	
FILTER (QTY/MODEL)																	
SQUID (QTY/MODEL)																	
FIBER TRUNK (QTY/MODEL)																	
DC TRUNK (QTY/MODEL)																	
REPEATER (QTY/MODEL)																	
RRH - 700 band (QTY/MODEL)		1	B5/B12 4449														
RRH - 850 band (QTY/MODEL)				RRH is shared with another band													
RRH - 1900 band (QTY/MODEL)																	
RRH - AWS band (QTY/MODEL)																	
RRH - WCS band (QTY/MODEL)			1	4415 B30													
Additional RRH #1 - any band (QTY/MODEL)																	
Additional RRH #2 - any band (QTY/MODEL)																	
Additional Component 1 (QTY/MODEL)																	
Additional Component 2 (QTY/MODEL)																	
Additional Component 3 (QTY/MODEL)																	
Local Market Note 1			Radio positions according to PD														
Local Market Note 2																	
Local Market Note 3			1xxMU03& xxxx														
			/ 1x630 / xxxx														

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/ Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 2	PORT 2		5787.A.850.4G.1	CTL02128_8A_1	CTL02128_8A_1		LTE 850	80010965_849M Hz_02DT	15.4	30	2	TOP	FIBER	0						1000		3	
	PORT 3		5787.A.WCS.4G	1	CTL02128_3A_1	CTL02128_3A_1		80010965_2355 MHz_03DT	18.1	30	3	TOP	FIBER	0						1285.2866		4	
	PORT 5			CTN0002128_F1	N5A_1	CTN0002128_F1	5G 850	80010965_849M Hz															

**Section 16B - PLANNED/PROPOSED TOWER CONFIGURATION - SECTOR B**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7	
<b>Existing Antenna?</b>								
<b>ANTENNA MAKE - MODEL</b>		800-10965						
<b>ANTENNA VENDOR</b>		Kathrein						
<b>ANTENNA SIZE (H x W x D)</b>		78.7X20X6.9						
<b>ANTENNA WEIGHT</b>		108.6						
<b>AZIMUTH</b>		150						
<b>MAGNETIC DECLINATION</b>								
<b>RADIATION CENTER (feet)</b>		128.03						
<b>ANTENNA TIP HEIGHT</b>								
<b>MECHANICAL DOWNTILT</b>		0						
<b>FEEDER AMOUNT</b>								
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>								
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>								
<b>Antenna RET Motor (QTY/MODEL)</b>			Internal					
<b>SURGE ARRESTOR (QTY/MODEL)</b>								
<b>DIPLEXER (QTY/MODEL)</b>								
<b>DUPLExER (QTY/MODEL)</b>								
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>			LTE RRH					
<b>DC BLOCK (QTY/MODEL)</b>								
<b>TMA/LNA (QTY/MODEL)</b>								
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>								
<b>PDU FOR TMAS (QTY/MODEL)</b>								
<b>FILTER (QTY/MODEL)</b>								
<b>SQUID (QTY/MODEL)</b>								
<b>FIBER TRUNK (QTY/MODEL)</b>								
<b>DC TRUNK (QTY/MODEL)</b>								
<b>REPEATER (QTY/MODEL)</b>								
<b>RRH - 700 band (QTY/MODEL)</b>	1	B5/B12 4449						
<b>RRH - 850 band (QTY/MODEL)</b>			RRH is shared with another band					
<b>RRH - 1900 band (QTY/MODEL)</b>								
<b>RRH - AWS band (QTY/MODEL)</b>								
<b>RRH - WCS band (QTY/MODEL)</b>	1	4415 B30						
<b>Additional RRH #1 - any band (QTY/MODEL)</b>								
<b>Additional RRH #2 - any band (QTY/MODEL)</b>								
<b>Additional Component 1 (QTY/MODEL)</b>								
<b>Additional Component 2 (QTY/MODEL)</b>								
<b>Additional Component 3 (QTY/MODEL)</b>								
<b>Local Market Note 1</b>	- Add Homerun RET to UMTS antenna - Replace GSM antenna with LTE 8 port							
<b>Local Market Note 2</b>								
<b>Local Market Note 3</b>	xxxxx / 1x6630 / 1xXMU03& xxxx / 1x6630 / xxxx							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/ Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
<b>ANTENNA POSITION 2</b>	<b>PORT 2</b>		5787.B.850.4G.1	CTL02128_8B_1	CTL02128_8B_1		LTE 850	80010965_849M Hz_07DT	15.5	150	7	TOP	FIBER	0						1000		11	
	<b>PORT 3</b>		5787.B.WCS.4G	1	CTL02128_3B_1	CTL02128_3B_1		80010965_2355 MHz_03DT	18.1	150	3	TOP	FIBER	0						1285.2866		12	
	<b>PORT 5</b>			CTN0002128_F1	N5B_1	CTN0002128_F1	5G 850	80010965_849M Hz_07DT	15.5	150	7	TOP	FIBER	0						1000		11	

**Section 16C - PLANNED/PROPOSED TOWER CONFIGURATION - SECTOR C**

ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7																				
Existing Antenna?																											
ANTENNA MAKE - MODEL		800-10965																									
ANTENNA VENDOR		Kathrein																									
ANTENNA SIZE (H x W x D)		78.7X20X6.9																									
ANTENNA WEIGHT		108.6																									
AZIMUTH		270																									
MAGNETIC DECLINATION																											
RADIATION CENTER (feet)		128.03																									
ANTENNA TIP HEIGHT																											
MECHANICAL DOWNTILT		0																									
FEEDER AMOUNT																											
VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)																											
VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)																											
HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)																											
HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)																											
HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)																											
Antenna RET Motor (QTY/MODEL)			Internal																								
SURGE ARRESTOR (QTY/MODEL)																											
DIPLEXER (QTY/MODEL)																											
DUPLEXER (QTY/MODEL)																											
Antenna RET CONTROL UNIT (QTY/MODEL)			LTE RRH																								
DC BLOCK (QTY/MODEL)																											
TMA/LNA (QTY/MODEL)																											
CURRENT INJECTORS FOR TMA (QTY/MODEL)																											
PDU FOR TMAS (QTY/MODEL)																											
FILTER (QTY/MODEL)																											
SQUID (QTY/MODEL)																											
FIBER TRUNK (QTY/MODEL)																											
DC TRUNK (QTY/MODEL)																											
REPEATER (QTY/MODEL)																											
RRH - 700 band (QTY/MODEL)	1	B5/B12 4449																									
RRH - 850 band (QTY/MODEL)			RRH is shared with another band																								
RRH - 1900 band (QTY/MODEL)																											
RRH - AWS band (QTY/MODEL)																											
RRH - WCS band (QTY/MODEL)	1	4415 B30																									
Additional RRH #1 - any band (QTY/MODEL)																											
Additional RRH #2 - any band (QTY/MODEL)																											
Additional Component 1 (QTY/MODEL)																											
Additional Component 2 (QTY/MODEL)																											
Additional Component 3 (QTY/MODEL)																											
Local Market Note 1	- Add Homerun RET to UMTS antenna - Replace GSM antenna with LTE 8 port																										
Local Market Note 2																											
Local Market Note 3	xxxxx / 1x6630 / 1xXMU03& xxxx / 1x6630 / xxxx																										

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/ Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 2	PORT 2		5787.C.850.4G.1	CTL02128_8C_1	CTL02128_8C_1		LTE 850	80010965_849M Hz_02DT	15.4	270	2	TOP	FIBER	0						1000		19	
	PORT 3		5787.C.WCS.4G	1	CTL02128_3C_1	CTL02128_3C_1	LTE WCS	80010965_2355 MHz_03DT	18.1	270	3	TOP	FIBER	0						1285.2866		20	
	PORT 5			CTN0002128_F1	N5C_1	CTN0002128_F1	5G 850	80010965_849M Hz_02DT	15.4														

## Section 16.5A - SCOPING TOWER CONFIGURATION - SECTOR A (OR OMNI)

## Section 17A - FINAL TOWER CONFIGURATION - SECTOR A (OR OMNI)

ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
ANTENNA MAKE - MODEL	7770	800-10965		HPA-65R-BUU-H6			
ANTENNA VENDOR	Powerwave	Kathrein		CCI			
ANTENNA SIZE (H x W x D)	55X11X5	78.7X20X6.9		72X14.8X9			
ANTENNA WEIGHT	35	108.6		50.7			
AZIMUTH	143	30		30			
MAGNETIC DECLINATION							
RADIATION CENTER (feet)	128.03	128.03		128.03			
ANTENNA TIP HEIGHT							
MECHANICAL DOWNTILT	0	0		0			
FEEDER AMOUNT	2			Fiber + 2 Coax			
VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)							
VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)							
HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)							
HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)							
Antenna RET Motor (QTY/MODEL)	2	Powerwave 7020	Internal		Internal		
SURGE ARRESTOR (QTY/MODEL)		1	DC/Fiber Squid		1	DC/Fiber Squid	
DIPLEXER (QTY/MODEL)	2	Powerwave / LGP 21901					
DUPLEXER (QTY/MODEL)							
Antenna RET CONTROL UNIT (QTY/MODEL)	1	Kathrein / 860-10006	LTE RRH		LTE RRH		
DC BLOCK (QTY/MODEL)							
TMA/LNA (QTY/MODEL)	2	21401 (Dual Band - 850)					
CURRENT INJECTORS FOR TMA (QTY/MODEL)	2	Polyphaser 1000860					
PDU FOR TMAS (QTY/MODEL)	1	LGP 12104 ( 850 Bypass TMA )					
FILTER (QTY/MODEL)							
SQUID (QTY/MODEL)							
FIBER TRUNK (QTY/MODEL)							
DC TRUNK (QTY/MODEL)							
REPEATER (QTY/MODEL)							
RRH - 700 band (QTY/MODEL)		1	B5/B12 4449				
RRH - 850 band (QTY/MODEL)			RRH is shared with another band				
RRH - 1900 band (QTY/MODEL)				1	RRUS-12+RRUS-A2		
RRH - AWS band (QTY/MODEL)							
RRH - WCS band (QTY/MODEL)		1	4415 B30				
Additional RRH #1 - any band (QTY/MODEL)							
Additional RRH #2 - any band (QTY/MODEL)							
Additional Component 1 (QTY/MODEL)							
Additional Component 2 (QTY/MODEL)							
Additional Component 3 (QTY/MODEL)							
Local Market Note 1	- Add Homerun RET to UMTS antenna - Replace GSM antenna with LTE 8 port						
Local Market Note 2							
Local Market Note 3	xxxxx / 1x6630 / 1xXMU03& xxxx / 1x6630 / xxxxx						

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/ Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIR KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 1	PORT 1	5787.A.850.3G.1	5787.A.850.3G.1	CTV21281	CTV21281		UMTS 850	7770.00.850.07	13.5	143	7	None	Commscope 1-1/4 (850)	155.039685						252.35		1	

ANTENNA POSITION 2	PORT 1	5787.A.700.4G.1	5787.A.700.4G.1	CTL02128_7A_1	CTL02128_7A_1		LTE 700	80010965_716M Hz_02DT	14.9	30	2	TOP	FIBER	0						1475.7065		3	
	PORT 2	5787.A.850.4G.t	5787.A.850.4G.t	CTL02128_8A_1	CTL02128_8A_1		LTE 850	80010965_849M Hz_02DT	15.4	30	2	TOP	FIBER	0						1000		3	
	PORT 3	5787.A.WCS.4G.	5787.A.WCS.4G.	CTL02128_3A_1	CTL02128_3A_1		LTE WCS	80010965_2355 MHz_03DT	18.1	30	3	TOP	FIBER	0						1285.2866		4	
	PORT 4	5787.A.850.5G.t	5787.A.850.5G.t	CTN0002128_F1	CTN0002128_F1		5G 850	80010965_849M Hz_02DT	15.4	30	2	TOP	FIBER	0						1000		3	
	PORT 5	5787.A.850.5G.t	5787.A.850.5G.t	N5A_1	N5A_1																		

ANTENNA POSITION 4	PORT 3	5787.A.1900.4G. 1	5787.A.1900.4G. 1	CTL02128_9A_1	CTL02128_9A_1	LTE 1900	H6_1930MHz_03 DT	17	30	3	TOP	FIBER	0						3664.3757		8	
	PORT 4	5787.A.1900.4G. 2	5787.A.1900.4G. 4	CTL02128_9A_2	CTL02128_9A_2	LTE 1900	H6_1930MHz_03 DT	17	30	3	TOP	FIBER	0						3664.3757		8	

**Section 17B - FINAL TOWER CONFIGURATION - SECTOR B**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7	
<b>ANTENNA MAKE - MODEL</b>	7770	800-10965		HPA-65R-BUU-H6				
<b>ANTENNA VENDOR</b>	Powerwave	Kathrein		CCI				
<b>ANTENNA SIZE (H x W x D)</b>	55X11X5	78.7X20X6.9		72X14.8X9				
<b>ANTENNA WEIGHT</b>	35	108.6		50.7				
<b>AZIMUTH</b>	263	150		150				
<b>MAGNETIC DECLINATION</b>								
<b>RADIATION CENTER (feet)</b>	128.03	128.03		128.03				
<b>ANTENNA TIP HEIGHT</b>								
<b>MECHANICAL DOWNTILT</b>	0	0		0				
<b>FEEDER AMOUNT</b>	2			Fiber + 2 Coax				
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>								
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>								
<b>Antenna RET Motor (QTY/MODEL)</b>	2	Powerwave 7020		Internal		Internal		
<b>SURGE ARRESTOR (QTY/MODEL)</b>								
<b>DIPLEXER (QTY/MODEL)</b>	2	Powerwave / LGP 21901						
<b>DUPLEXER (QTY/MODEL)</b>								
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>			LTE RRH		LTE RRH			
<b>DC BLOCK (QTY/MODEL)</b>								
<b>TMA/LNA (QTY/MODEL)</b>	2	21401 (Dual Band - 850)						
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>	2	Polyphaser 1000860						
<b>PDU FOR TMAS (QTY/MODEL)</b>								
<b>FILTER (QTY/MODEL)</b>								
<b>SQUID (QTY/MODEL)</b>								
<b>FIBER TRUNK (QTY/MODEL)</b>								
<b>DC TRUNK (QTY/MODEL)</b>								
<b>REPEATER (QTY/MODEL)</b>								
<b>RRH - 700 band (QTY/MODEL)</b>		1	B5/B12 4449					
<b>RRH - 850 band (QTY/MODEL)</b>			RRH is shared with another band					
<b>RRH - 1900 band (QTY/MODEL)</b>				1	RRUS-12+RRUS-A2			
<b>RRH - AWS band (QTY/MODEL)</b>								
<b>RRH - WCS band (QTY/MODEL)</b>		1	4415 B30					
<b>Additional RRH #1 - any band (QTY/MODEL)</b>								
<b>Additional RRH #2 - any band (QTY/MODEL)</b>								
<b>Additional Component 1 (QTY/MODEL)</b>								
<b>Additional Component 2 (QTY/MODEL)</b>								
<b>Additional Component 3 (QTY/MODEL)</b>								
<b>Local Market Note 1</b>	- Add Homerun RET to UMTS antenna - Replace GSM antenna with LTE 8 port							
<b>Local Market Note 2</b>								
<b>Local Market Note 3</b>	xxxxx / 1x6630 / 1xMU038 xxxx / 1x6630 / xxxx							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXA/IT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 1	PORT 1	5787.B.850.3G.1	5787.B.850.3G.1	CTV21282	CTV21282		UMTS 850	7770.00.850.07	13.5	263	7	None	Commscope 1-1/4 (850)	155.039685						252.35		9	

ANTENNA POSITION 2	PORT 1	5787.B.700.4G.1	5787.B.700.4G.1	CTL02128_7B_1	CTL02128_7B_1		LTE 700	80010965_716M Hz_07DT	14.6	150	7	TOP	FIBER	0						1475.7065		11	
	PORT 2	5787.B.850.4G.t	5787.B.850.4G.t	CTL02128_8B_1	CTL02128_8B_1		LTE 850	80010965_849M Hz_07DT	15.5	150	7	TOP	FIBER	0						1000		11	
	PORT 3	5787.B.WCS.4G.1	5787.B.WCS.4G.1	CTL02128_3B_1	CTL02128_3B_1		LTE WCS	80010965_2355 MHz_03DT	18.1	150	3	TOP	FIBER	0						1285.2866		12	
	PORT 5	5787.B.850.5G.t	5787.B.850.5G.t	CTN0002128_F1	CTN0002128_F1		5G 850	80010965_849M Hz_07DT	15.5	150	7	TOP	FIBER	0						1000		11	

ANTENNA POSITION 4	PORT 3	5787.B.1900.4G.1	5787.B.1900.4G.1	CTL02128_9B_1	CTL02128_9B_1		LTE 1900	H6_1930MHz_02 DT	16.85	150	2	TOP	FIBER	0						3664.3757		16	
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ANTENNA PORTS		5787.B.1900.4G.	5787.B.1900.4G.	4	LTE 1900	H6_1930MHz_02	DT	16.85	150	2	TOP	FIBER	0					3664.3757		16	
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**Section 17C - FINAL TOWER CONFIGURATION - SECTOR C**

<b>ANTENNA POSITION is LEFT to RIGHT from BACK of ANTENNA (unless otherwise specified)</b>	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7	
<b>ANTENNA MAKE - MODEL</b>	7770	800-10965		HPA-65R-BUU-H6				
<b>ANTENNA VENDOR</b>	Powerwave	Kathrein		CCI				
<b>ANTENNA SIZE (H x W x D)</b>	55X11X5	78.7X20X6.9		72X14.8X9				
<b>ANTENNA WEIGHT</b>	35	108.6		50.7				
<b>AZIMUTH</b>	23	270		270				
<b>MAGNETIC DECLINATION</b>								
<b>RADIATION CENTER (feet)</b>	128.03	128.03		128.03				
<b>ANTENNA TIP HEIGHT</b>								
<b>MECHANICAL DOWNTILT</b>	0	0		0				
<b>FEEDER AMOUNT</b>	2			Fiber + 2 Coax				
<b>VERTICAL SEPARATION from ANTENNA ABOVE (TIP to TIP)</b>								
<b>VERTICAL SEPARATION from ANTENNA BELOW (TIP to TIP)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to LEFT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from CLOSEST ANTENNA to RIGHT (CENTERLINE to CENTERLINE)</b>								
<b>HORIZONTAL SEPARATION from ANOTHER ANTENNA (which antenna # / # of inches)</b>								
<b>Antenna RET Motor (QTY/MODEL)</b>	2	Powerwave 7020		Internal		Internal		
<b>SURGE ARRESTOR (QTY/MODEL)</b>								
<b>DIPLEXER (QTY/MODEL)</b>	2	Powerwave / LGP 21901						
<b>DUPLEXER (QTY/MODEL)</b>								
<b>Antenna RET CONTROL UNIT (QTY/MODEL)</b>			LTE RRH		LTE RRH			
<b>DC BLOCK (QTY/MODEL)</b>								
<b>TMA/LNA (QTY/MODEL)</b>	2	21401 (Dual Band - 850						
<b>CURRENT INJECTORS FOR TMA (QTY/MODEL)</b>	2	Polyphaser 1000860						
<b>PDU FOR TMAS (QTY/MODEL)</b>								
<b>FILTER (QTY/MODEL)</b>								
<b>SQUID (QTY/MODEL)</b>								
<b>FIBER TRUNK (QTY/MODEL)</b>								
<b>DC TRUNK (QTY/MODEL)</b>								
<b>REPEATER (QTY/MODEL)</b>								
<b>RRH - 700 band (QTY/MODEL)</b>		1	B5/B12 4449					
<b>RRH - 850 band (QTY/MODEL)</b>			RRH is shared with another band					
<b>RRH - 1900 band (QTY/MODEL)</b>				1	RRUS-12+RRUS-A2			
<b>RRH - AWS band (QTY/MODEL)</b>								
<b>RRH - WCS band (QTY/MODEL)</b>		1	4415 B30					
<b>Additional RRH #1 - any band (QTY/MODEL)</b>								
<b>Additional RRH #2 - any band (QTY/MODEL)</b>								
<b>Additional Component 1 (QTY/MODEL)</b>								
<b>Additional Component 2 (QTY/MODEL)</b>								
<b>Additional Component 3 (QTY/MODEL)</b>								
<b>Local Market Note 1</b>	- Add Homerun RET to UMTS antenna - Replace GSM antenna with LTE 8 port							
<b>Local Market Note 2</b>								
<b>Local Market Note 3</b>	xxxxx / 1x6630 / 1xMU038 xxxx / 1x6630 / xxxx							

PORT SPECIFIC FIELDS	PORT NUMBER	USEID (CSSng)	USEID (Atoll)	ATOLL TXID	ATOLL CELL ID	TX/RX?	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RRH LOCATION (Top/Bottom/Integrated/None )	FEEDERS TYPE	FEEDER LENGTH (feet)	RXAIT KIT MODULE?	TRIPLEXER or LLC (QTY)	TRIPLEXER or LLC (MODEL)	SCPA/MCPA MODULE?	HATCHPLATE POWER (Watts)	ERP (Watts)	Antenna RET Name	CABLE NUMBER	CABLE ID(cssng)
ANTENNA POSITION 1	POR T 1	5787.C.850.3G.1	5787.C.850.3G.1	CTV21283	CTV21283		UMTS 850	7770.00.850.06	13.5	23	6	None	Commscope 1-1/4 (850)	155.039685						252.35		17	

ANTENNA POSITION 2	POR T 1	5787.C.700.4G.1	5787.C.700.4G.1	CTL02128_7C_1	CTL02128_7C_1		LTE 700	80010965_716M Hz_02DT	14.9	270	2	TOP	FIBER	0						1475.7065		19	
	POR T 2	5787.C.850.4G.tmp1	5787.C.850.4G.1	CTL02128_8C_1	CTL02128_8C_1		LTE 850	80010965_849M Hz_02DT	15.4	270	2	TOP	FIBER	0						1000		19	
	POR T 3	5787.C.WCS.4G.1	5787.C.WCS.4G.1	CTL02128_3C_1	CTL02128_3C_1		LTE WCS	80010965_2355 MHz_03DT	18.1	270	3	TOP	FIBER	0						1285.2866		20	
	POR T 5	5787.C.850.5G.tmp1	5787.C.850.5G.t	CTN0002128_F1	CTN0002128_F1		5G 850	80010965_849M Hz_02DT	15.4	270	2	TOP	FIBER	0						1000		19	

ANTENNA POSITION 4	POR T 3	5787.C.1900.4G.1	5787.C.1900.4G.1	CTL02128_9C_1	CTL02128_9C_1		LTE 1900	H6_1930MHz_02 DT	16.85	270	2	TOP	FIBER	0						3664.3757		24	
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ANTENNA PORTS		5787.C.1900.4G.	5787.C.1900.4G.	4	LTE 1900	H6_1930MHz_02	DT	16.85	270	2	TOP	FIBER	0					3664.3757		24	
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Centered on Solutions<sup>SM</sup>

## Structural Analysis Report

150-ft Existing Valmont Monopole

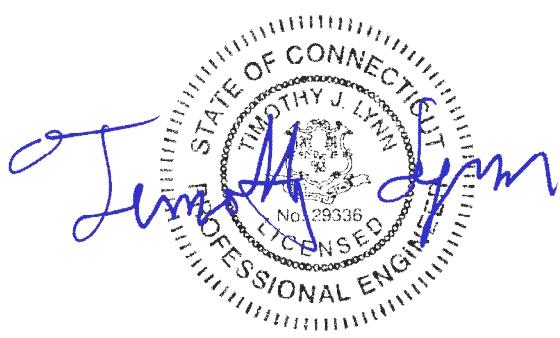
Proposed AT&T Mobility  
Antenna Upgrade

AT&T Site Ref: CT2128

3965 Congress Street  
Fairfield, CT

Centek Project No. 16071.42

Date: August 30, 2016



**Prepared for:**  
AT&T Mobility  
500 Enterprise Drive, Suite 3A  
Rocky Hill, CT 06067

**CENTEK** Engineering, Inc.  
Structural Analysis - 150-ft Valmont Monopole  
AT&T Antenna Upgrade ~ CT2128  
Fairfield, CT  
August 30, 2016

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- PRIMARY ASSUMPTIONS USED IN THE ANALYSIS
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- TOWER LOADING
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- FOUNDATION AND ANCHORS
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### **SECTION 2 – CONDITIONS & SOFTWARE**

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- ANTENNA CUT SHEETS

**CENTEK** Engineering, Inc.

*Structural Analysis - 150-ft Valmont Monopole*

*AT&T Antenna Upgrade ~ CT2128*

*Fairfield, CT*

*August 30, 2016*

## Introduction

The purpose of this report is to summarize the results of the non-linear, P-Δ structural analysis of the antenna upgrade proposed by AT&T Mobility on the existing monopole (tower) located in Fairfield, CT.

The host tower is a 150-ft tall, three-section, twelve sided, tapered monopole, originally designed and manufactured by Valmont Structures. The manufacturer's drawings and calculations were unavailable for use in this report. The tower geometry, structure member sizes and foundation system information were obtained from a previous structural analysis report prepared by Centek Engineering job no; 13001.101, dated December 5, 2013.

Antenna and appurtenance information were obtained from the aforementioned Centek structural report, visual verification from grade conducted by Centek personnel on August 18, 2016 and a AT&T RF data sheet.

The tower is made up of three (3) tapered vertical sections consisting of A572-65 pole sections. The vertical tower sections are slip joint connected. The diameter of the pole (flat-flat) is 23.61-in at the top and 49.6-in at the base.

AT&T proposes the replacement of three (3) panel antennas and the installation of three (3) three (3) remote radio heads and one (1) main distribution box mounted to the existing low profile platform. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna and appurtenance configuration.

## Antenna and Appurtenance Summary

The existing, proposed and future loads considered in this analysis consist of the following:

- **TOWN (Existing):**  
Antennas: One (1) DB810K Omni-directional whip antenna and two (2) 10-ft Dipole antennas mounted on the Nextel T-Arms with respective RAD center elevations of 157-ft and 154-ft above grade.  
Coax Cables: Three (3) 1-5/8"Ø coax cables running on the inside of the existing tower.
- **NEXTEL (Existing):**  
Antennas: Twelve (12) Andrew DB844H90E-XY panel antennas mounted on three (3) 12-ft T-Arms with a RAD center elevation of 149-ft above grade.  
Coax Cables: Twelve (12) 1-5/8" coax cables running on the inside of the existing tower.
- **SPRINT (Existing):**  
Antennas: Three (3) RFS APXVSPP18-C-A20 panel antennas mounted on a 13-ft platform with hand rails with a RAD center elevation of 138-ft above grade. Three (3) ALU 1900 MHz RRH's and three (3) ALU 800 MHz RRH's mounted on a universal tr-bracket above the existing platform.  
Coax Cables: Three (3) 1-5/8" Ø Hybriflex cables running on the inside of the existing tower.

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*Structural Analysis - 150-ft Valmont Monopole*

*AT&T Antenna Upgrade ~ CT2128*

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- **T-MOBILE (Existing):**  
Antennas: Three (3) RFS APX16DWV-16DWV-S panel antennas and six (6) 10" by 8" by 3" TMA's mounted on a 13-ft platform with rails with a RAD center elevation of 113-ft above grade.  
Coax Cables: Twelve (12) 1-1/4"  $\varnothing$  coax cables running on the exterior of the existing tower.
- **TOWN (Existing):**  
Antennas: Two (2) Andrew APSA685 Omni-directional whip antennas (inverted), one (1) DB-222 dipole antenna and one (1) PD1142-2B Omni-directional whip antenna mounted on two (2) standoffs with an elevation of 104-ft above grade.  
Coax Cables: Four (4) 1-5/8"  $\varnothing$  coax cables running on the inside of the existing tower.
- **TOWN (Existing):**  
Antennas: Two (2) empty standoffs with a RAD center elevation of 104-ft above grade.
- **VERIZON (EXISTING TO REMAIN):**  
Antennas: Three (3) Antel BXA-70063-6CF panel antennas, six (6) Andrew DB846F65ZAXY panel antennas, three (3) Antel BXA-171063-8BF panel antennas, three (3) BXA-171063-12CF panel antennas, three (3) Alcatel-Lucent RRH2x40-AWS Remote Radio Heads, six (6) RFS FD9R6004/2C-3L Diplexers and one (1) RFS DB-T1-6Z-8AB-0Z main distribution mounted on an existing low profile platform with a RAD center elevation of 80-ft above grade.  
Coax Cables: Twelve (12) 1-5/8"  $\varnothing$  coax cables and one (1) 1-5/8"  $\varnothing$  fiber cable running on the exterior of the existing tower.
- **UNKNOWN (Existing):**  
Antennas: One (1) GPS antenna on a GPS Stand-off mount with a RAD center elevation of 40-ft above grade.  
Coax Cables: One (1) 1/2"  $\varnothing$  coax cable running on the exterior of the existing tower.
- **AT&T (Existing to Remain):**  
Antennas: Six (6) Powerwave 7770 panel antennas and twelve (12) Powerwave LGP21401 TMA's mounted on an existing low profile platform with a RAD center elevation of 127-ft above grade.  
Appurtenances: Three (3) Ericsson RRUS-11 and one (1) Raycap DC6-48-60-18-8F surge arrestor mounted to one (1) universal ring mount with a RAD center elevation of 129-ft above grade.  
Coax Cables: Twelve (12) 1-1/4"  $\varnothing$  coax cables, one (1) fiber cable and two (2) dc control cables running on the exterior of the existing tower.
- **AT&T (Existing to Remove):**  
Antennas: Three (3) Powerwave P65-16-XLH-RR panel antennas a mounted on an existing low profile platform with a RAD center elevation of 127-ft above grade.

- **AT&T (Proposed):**

**Antennas:** Three (3) CCI HPA-65R-BUU-H6 panel antennas mounted on an existing low profile platform with a RAD center elevation of 127-ft above grade.

**Appurtenances:** Three (3) Ericsson RRUS-12 and three (3) Ericsson A2s mounted to one (1) universal ring mount with a RAD center elevation of 129-ft above grade.

### Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents or reinforcement drawings.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- All existing coax cables to be installed as indicated in this report.

## Analyses

The existing tower was analyzed using a comprehensive computer program entitled tnxTower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower shaft, and the model assumes that the shaft members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for the controlling basic wind speed (fastest mile) with no ice and a 75% reduction of wind force with  $\frac{1}{2}$  inch accumulative ice to determine stresses in members as per guidelines of TIA/EIA-222-F-96 entitled "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures", the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

The controlling wind speed is determined by evaluating the local available wind speed data as provided in Appendix K of the CSBC<sup>1</sup> and the wind speed data available in the TIA/EIA-222-F-96 Standard. The higher of the two wind speeds is utilized in preparation on the tower analysis.

## Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of  $\frac{1}{2}$ " radial ice on the tower structure and its components.

Basic Wind Speed:	New Haven; $v = 85$ mph (fastest mile)  Fairfield; $v = 110$ mph (3 second gust) equivalent to $v = 90$ mph (fastest mile)	[Section 16 of TIA/EIA-222-F-96]  [Appendix K of the 2005 CT Building Code Supplement]
Load Cases:	<u>Load Case 1</u> ; 90 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation.  <u>Load Case 2</u> ; 78 mph wind speed w/ $\frac{1}{2}$ " radial ice plus gravity load – used in calculation of tower stresses. The 78 mph wind speed velocity represents 75% of the wind pressure generated by the 90 mph wind speed.	[Section 2.3.16 of TIA/EIA-222-F-96]  [Section 2.3.16 of TIA/EIA-222-F-96]
	<u>Load Case 3</u> ; Seismic – not checked	[Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type

<sup>1</sup> The 2005 Connecticut State Building Code as amended by the 2009 CT State Supplement. (CSBC)

## Tower Capacity

Tower stresses were calculated utilizing the structural analysis software tnxC Tower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

- Calculated stresses were found to be within allowable limits. In Load Case 1, per tnxC Tower "Section Capacity Table", this tower was found to be at **99.6%** of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Pole Shaft (L3)	30.00'-47.83'	99.6%	<b>PASS</b>

Note 1: Equivalent thickness of 0.58" used for section L4 of pole shaft with reinforcement.

## Foundation and Anchors

The existing foundation consists of a 6.6 Ø x 26.6-ft long reinforced concrete caisson. The sub-grade conditions used in the analysis of the existing foundation were obtained from the design documents prepared by SAC, dated May 18, 1994. The base of the tower is connected to the foundation by means of (16) 2.25"Ø, ASTM A615-75 anchor bolts embedded approximately 5-ft into the concrete foundation structure.

- The tower base reactions developed from the governing Load Case 1 were used in the verification of the foundation and its anchors:

Location	Vector	Proposed Reactions
Base	Shear	42 kips
	Compression	44 kips
	Moment	3989 kip-ft

- The foundation was found to be within allowable limits.

Foundation	Design Limit	Proposed Loading	Result
Reinforced Concrete Caisson	Moment Capacity	61.9%	<b>PASS</b>
	Lateral Deflection	0.37 in. <sup>(1)</sup>	<b>PASS</b>

(1) Lateral deflection typically limited to 1.0 in. for monopole tower structures. Based on service loads ( $V = 50$  mph)

**CENTEK** Engineering, Inc.

Structural Analysis - 150-ft Valmont Monopole

AT&T Antenna Upgrade ~ CT2128

Fairfield, CT

August 30, 2016

- The anchor bolts and base plate were found to be within allowable limits.

Tower Component	Design Limit	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Tension	90.8%	<b>PASS</b>
Base Plate	Bending	93.8%	<b>PASS</b>

### Conclusion

This analysis shows that the subject tower **is adequate** to support the proposed antenna configuration.

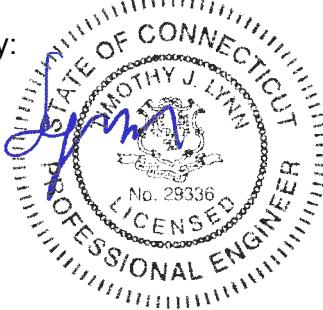
The analysis is based, in part, on the information provided to this office by AT&T. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:



Timothy J. Lynn, PE  
Structural Engineer



**CENTEK** Engineering, Inc.

*Structural Analysis - 150-ft Valmont Monopole*

*AT&T Antenna Upgrade ~ CT2128*

*Fairfield, CT*

*August 30, 2016*

**Standard Conditions for Furnishing of  
Professional Engineering Services on  
Existing Structures**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of CENTEK engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to CENTEK engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. CENTEK engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

**CENTEK** Engineering, Inc.

*Structural Analysis - 150-ft Valmont Monopole*

*AT&T Antenna Upgrade ~ CT2128*

*Fairfield, CT*

*August 30, 2016*

## General Description of Structural Analysis Program

tnxTower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, tnxTower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

### tnxTower Features:

- tnxTower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- tnxTower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

## DESIGNED APPURTENANCE LOADING

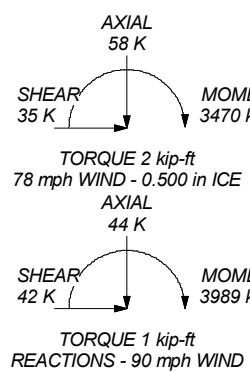
TYPE	ELEVATION	TYPE	ELEVATION
10-ft Dipole (Town)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
10-ft Dipole (Town)	149	APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113
DB810K (Town)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
(4) DB844H90E-XY (Nextel Existing)	149	(2) 10"x8"x3" TMA (T-Mobile Existing)	113
Valmont T-Arm (1) (Nextel Existing)	149	13' Platform w/Rail (T-Mobile Existing)	113
Valmont T-Arm (1) (Nextel Existing)	149	4'6" Standoff (Town - Existing)	104
Valmont T-Arm (1) (Nextel Existing)	149	4'6" Standoff (Town - Existing)	104
APXVSPP18-C-A20 (Sprint Existing)	138	4'6" Standoff (Town - Existing)	104
APXVSPP18-C-A20 (Sprint Existing)	138	4'6" Standoff (Town - Existing)	104
APXVSPP18-C-A20 (Sprint Existing)	138	1142-2B (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	ASPA685 (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	DB222 (Town - Existing)	104
FD-RRH 4x45 1900 (Sprint Existing)	138	ASPA685 (Town - Existing)	104
FD-RRH 2x50 800 (Sprint Existing)	138	DB846F65ZAXY (Verizon - Existing)	80
FD-RRH 2x50 800 (Sprint Existing)	138	BXA-171063/8BF (Verizon - Existing)	80
FD-RRH 2x50 800 (Sprint Existing)	138	BXA-70063/6CF (Verizon - Existing)	80
13' Platform w/Rails (Sprint Existing)	138	DB846F65ZAXY (Verizon - Existing)	80
RRUS-11 (AT&T Existing)	129	DB846F65ZAXY (Verizon - Existing)	80
RRUS-11 (AT&T Existing)	129	DB846F65ZAXY (Verizon - Existing)	80
RRUS-11 (AT&T Existing)	129	BXA-171063/8BF (Verizon - Existing)	80
RRUS-12 (AT&T Proposed)	129	BXA-70063/6CF (Verizon - Existing)	80
RRUS-12 (AT&T Proposed)	129	DB846F65ZAXY (Verizon - Existing)	80
RRUS-12 (AT&T Proposed)	129	DB846F65ZAXY (Verizon - Existing)	80
A2 (AT&T Proposed)	129	BXA-171063/6BF (Verizon - Existing)	80
A2 (AT&T Proposed)	129	BXA-70063/6CF (Verizon - Existing)	80
A2 (AT&T Proposed)	129	DB846F65ZAXY (Verizon - Existing)	80
DC6-48-60-18-8F Surge Arrestor (AT&T Existing)	129	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
Valmont Uni-Tri Bracket (AT&T Existing)	129	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	BXA-171063-12CF (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	BXA-171063-12CF (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Proposed)	127	RRHx240-AWS (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	RRHx240-AWS (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	RRHx240-AWS (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Proposed)	127	RRHx240-AWS (Verizon - Existing)	80
7770.00 (AT&T Existing)	127	RRHx240-AWS (Verizon - Existing)	80
HPA-65R-BUU-H6 (AT&T Proposed)	127	DB-T1-6Z-BAB-0Z (Verizon - Existing)	80
(4) LGP214nn TMA (AT&T Existing)	127	Valmont 13' Low Profile Platform (Verizon - Existing)	78
(4) LGP214nn TMA (AT&T Existing)	127	Stand-off	40
(4) LGP214nn TMA (AT&T Existing)	127	GPS (Existing)	40
Valmont 13' Low Profile Platform (AT&T Existing)	125		
APX16DWV-16DWV-S-E-ACU (T-Mobile Existing)	113		

## MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

## TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for a 90 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 78 mph basic wind with 0.50 in ice.
4. Deflections are based upon a 50 mph wind.
5. Weld together tower sections have flange connections.
6. Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications.
7. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
8. Welds are fabricated with ER-70S-6 electrodes.
9. TOWER RATING: 99.6%



**Centek Engineering Inc.**

63-2 North Branford Rd.

Branford, CT 06405

Phone: (203) 488-0580

FAX: (203) 488-8587

Job: 16071.42 - CT2128

Project: 150-ft Valmont Monopole - Fairfield, CT

Client: AT&T Mobility Drawn by: TJL App'd:

Code: TIA/EIA-222-F Date: 08/30/16 Scale: NTS

Path: Dwg No. E-11

2008-08712WMS\_Faulted GroundWire Shaded Drawing Documentation CapEx Plan/ISI Monopole, Fairfield CT

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Job</b>	16071.42 - CT2128	<b>Page</b>
	<b>Project</b>	150-ft Valmont Monopole - Fairfield, CT	<b>Date</b> 10:42:33 08/30/16
	<b>Client</b>	AT&T Mobility	<b>Designed by</b> TJL

## Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Fairfield County, Connecticut.

Basic wind speed of 90 mph.

Nominal ice thickness of 0.500 in.

Ice density of 56 pcf.

A wind speed of 78 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

Weld together tower sections have flange connections..

Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC Specifications..

Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..

Welds are fabricated with ER-70S-6 electrodes..

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs	Distribute Leg Loads As Uniform
Consider Moments - Horizontals	Assume Legs Pinned
Consider Moments - Diagonals	✓ Assume Rigid Index Plate
Use Moment Magnification	Use Clear Spans For Wind Area
✓ Use Code Stress Ratios	Use Clear Spans For KL/r
Use Code Safety Factors - Guys	Retension Guys To Initial Tension
Escalate Ice	✓ Bypass Mast Stability Checks
Always Use Max Kz	Use Azimuth Dish Coefficients
Use Special Wind Profile	✓ Project Wind Area of Appurt.
Include Bolts In Member Capacity	Autocalc Torque Arm Areas
Leg Bolts Are At Top Of Section	Add IBC .6D+W Combination
Secondary Horizontal Braces Leg	✓ Sort Capacity Reports By Component
Use Diamond Inner Bracing (4 Sided)	Triangulate Diamond Inner Bracing
SR Members Have Cut Ends	Treat Feed Line Bundles As Cylinder
SR Members Are Concentric	
	Use ASCE 10 X-Brace Ly Rules
	Calculate Redundant Bracing Forces
	Ignore Redundant Members in FEA
	SR Leg Bolts Resist Compression
	All Leg Panels Have Same Allowable
	Offset Girt At Foundation
	Consider Feed Line Torque
	Include Angle Block Shear Check
	Use TIA-222-G Bracing Resist. Exemption
	Use TIA-222-G Tension Splice Exemption
	Poles
	✓ Include Shear-Torsion Interaction
	Always Use Sub-Critical Flow
	Use Top Mounted Sockets

## Tapered Pole Section Geometry

Section	Elevation	Section	Splice	Number	Top	Bottom	Wall	Bend	Pole Grade
	ft	Length	Length	of	Diameter	Diameter	Thickness	Radius	
		ft	ft	Sides	in	in	in	in	
L1	150.000-95.830	54.170	5.170	12	23.610	33.469	0.281	1.125	A572-65 (65 ksi)
L2	95.830-47.830	53.170	6.170	12	31.965	41.644	0.375	1.500	A572-65 (65 ksi)

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Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L3	47.830-30.000	24.000	0.000	12	39.771	44.139	0.438	1.750	A572-65 (65 ksi)
L4	30.000-0.000	30.000		12	44.139	49.600	0.580	2.320	A572-65 (65 ksi)

### Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	It/Q in <sup>2</sup>	w in	w/t
L1	24.443	21.131	1467.855	8.352	12.230	120.021	2974.272	10.400	5.574	19.814
	34.650	30.061	4226.132	11.881	17.337	243.765	8563.288	14.795	8.216	29.207
L2	34.067	38.145	4858.931	11.309	16.558	293.447	9845.511	18.774	7.562	20.165
	43.113	49.832	10832.905	14.774	21.572	502.184	21950.402	24.526	10.156	27.082
L3	42.336	55.411	10942.170	14.081	20.601	531.139	22171.804	27.272	9.486	21.683
	45.696	61.564	15007.519	15.645	22.864	656.382	30409.303	30.300	10.657	24.358
L4	45.696	81.351	19701.692	15.594	22.864	861.690	39920.969	40.038	10.275	17.715
	51.350	91.550	28079.524	17.549	25.693	1092.895	56896.728	45.058	11.738	20.239

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
L1				1	1	1			
150.000-95.83									
0									
L2				1	1	1			
95.830-47.830									
L3				1	1	1			
47.830-30.000									
L4				1.2	1	1.1			
30.000-0.000									

### Monopole Base Plate Data

#### Base Plate Data

Base plate is square	
Base plate is grouted	✓
Anchor bolt grade	A615-75
Anchor bolt size	2.250 in
Number of bolts	16
Embedment length f <sub>c</sub>	60.000 in 4.000 ksi
Grout space	3.000 in
Base plate grade	A633-60
Base plate thickness	2.750 in
Bolt circle diameter	57.850 in
Outer diameter	63.850 in
Inner diameter	40.000 in
Base plate type	Plain Plate

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### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C <sub>A</sub> A <sub>A</sub>	Weight
						ft <sup>2</sup> /ft	klf
1 5/8 (Town - Existing)	A	No	Inside Pole	149.000 - 3.000	3	No Ice 1/2" Ice	0.000 0.000
1 5/8 (Nextel - Existing)	B	No	Inside Pole	149.000 - 3.000	12	No Ice 1/2" Ice	0.000 0.000
1 1/4 (AT&T - Existing)	A	No	CaAa (Out Of Face)	125.000 - 3.000	12	No Ice 1/2" Ice	0.000 0.000
1 1/4 (T-Mobile - Existing)	A	No	CaAa (Out Of Face)	110.000 - 3.000	2	No Ice 1/2" Ice	0.155 0.255
1 1/4 (T-Mobile - Existing)	A	No	CaAa (Out Of Face)	110.000 - 3.000	10	No Ice 1/2" Ice	0.000 0.000
1 5/8 (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.000 - 3.000	2	No Ice 1/2" Ice	0.198 0.298
1 5/8 (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.000 - 3.000	10	No Ice 1/2" Ice	0.000 0.000
7/8 (Town - Existing)	B	No	Inside Pole	104.000 - 3.000	4	No Ice 1/2" Ice	0.000 0.000
1/2 (GPS - Existing)	B	No	CaAa (Out Of Face)	40.000 - 3.000	1	No Ice 1/2" Ice	0.058 0.158
#8 AWG Copper WIRE (AT&T - Existing)	C	No	CaAa (Out Of Face)	129.000 - 3.000	2	No Ice 1/2" Ice	0.000 0.000
HYBRIFLEX 1-5/8" (Sprint - Existing)	C	No	Inside Pole	138.000 - 3.000	3	No Ice 1/2" Ice	0.000 0.000
HYBRIFLEX 1-5/8" (Verizon - Existing)	C	No	CaAa (Out Of Face)	77.000 - 3.000	1	No Ice 1/2" Ice	0.000 0.000

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
			ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	K
L1	150.000-95.830	A	0.000	0.000	0.000	4.393	0.509
		B	0.000	0.000	0.000	0.000	0.681
		C	0.000	0.000	0.000	0.000	0.277
L2	95.830-47.830	A	0.000	0.000	0.000	14.880	0.910
		B	0.000	0.000	0.000	0.000	0.703
		C	0.000	0.000	0.000	11.551	0.746
L3	47.830-30.000	A	0.000	0.000	0.000	5.527	0.338
		B	0.000	0.000	0.000	0.580	0.264
		C	0.000	0.000	0.000	7.061	0.378
L4	30.000-0.000	A	0.000	0.000	0.000	8.370	0.512
		B	0.000	0.000	0.000	1.566	0.402
		C	0.000	0.000	0.000	10.692	0.572

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub>	A <sub>F</sub>	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face	Weight
			in	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	K
L1	150.000-95.830	A	0.500	0.000	0.000	0.000	7.227	1.159

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
L2	95.830-47.830	B		0.000	0.000	0.000	0.000	0.681
		C		0.000	0.000	0.000	0.000	0.323
L3	47.830-30.000	A	0.500	0.000	0.000	0.000	24.480	2.350
		B		0.000	0.000	0.000	0.000	0.703
		C		0.000	0.000	0.000	17.385	1.385
L4	30.000-0.000	A	0.500	0.000	0.000	0.000	9.093	0.873
		B		0.000	0.000	0.000	1.580	0.270
		C		0.000	0.000	0.000	10.627	0.752
		A	0.500	0.000	0.000	0.000	13.770	1.322
		B		0.000	0.000	0.000	4.266	0.420
		C		0.000	0.000	0.000	16.092	1.139

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	$C_A A_A$ Front ft <sup>2</sup>	$C_A A_A$ Side ft <sup>2</sup>	Weight K
10-ft Dipole (Town)	A	From Face	3.000 0.000 5.000	0.000	149.000	No Ice 1/2" Ice	3.150 5.670	3.150 5.670 0.032 0.042
10-ft Dipole (Town)	B	From Face	3.000 0.000 5.000	0.000	149.000	No Ice 1/2" Ice	3.150 5.670	3.150 5.670 0.032 0.042
DB810K (Town)	C	From Face	3.000 0.000 5.000	0.000	149.000	No Ice 1/2" Ice	4.075 5.734	4.075 5.734 0.035 0.065
(4) DB844H90E-XY (Nextel Existing)	A	From Face	3.000 0.000 0.000	0.000	149.000	No Ice 1/2" Ice	2.867 3.177	3.733 4.101 0.010 0.035
(4) DB844H90E-XY (Nextel Existing)	B	From Face	3.000 0.000 0.000	0.000	149.000	No Ice 1/2" Ice	2.867 3.177	3.733 4.101 0.010 0.035
(4) DB844H90E-XY (Nextel Existing)	C	From Face	3.000 0.000 0.000	0.000	149.000	No Ice 1/2" Ice	2.867 3.177	3.733 4.101 0.010 0.035
Valmont T-Arm (1) (Nextel Existing)	A	None		0.000	149.000	No Ice 1/2" Ice	10.540 14.450	10.540 14.450 0.336 0.412
Valmont T-Arm (1) (Nextel Existing)	B	None		0.000	149.000	No Ice 1/2" Ice	10.540 14.450	10.540 14.450 0.336 0.412
Valmont T-Arm (1) (Nextel Existing)	C	None		0.000	149.000	No Ice 1/2" Ice	10.540 14.450	10.540 14.450 0.336 0.412
APXVSPP18-C-A20 (Sprint Existing)	A	From Face	3.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	8.260 8.807	5.283 5.736 0.057 0.107
APXVSPP18-C-A20 (Sprint Existing)	B	From Face	3.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	8.260 8.807	5.283 5.736 0.057 0.107
APXVSPP18-C-A20 (Sprint Existing)	C	From Face	3.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	8.260 8.807	5.283 5.736 0.057 0.107
FD-RRH 4x45 1900 (Sprint Existing)	A	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.705 2.944	2.781 3.022 0.060 0.084

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C4A Front	C4A Side	Weight K
FD-RRH 4x45 1900 (Sprint Existing)	B	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.705 2.944	2.781 3.022
FD-RRH 4x45 1900 (Sprint Existing)	C	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.705 2.944	2.781 3.022
FD-RRH 2x50 800 (Sprint Existing)	A	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.401 2.613	2.254 2.460
FD-RRH 2x50 800 (Sprint Existing)	B	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.401 2.613	2.254 2.460
FD-RRH 2x50 800 (Sprint Existing)	C	From Face	1.000 0.000 0.000	0.000	138.000	No Ice 1/2" Ice	2.401 2.613	2.254 2.460
13' Platform w/Rails (Sprint Existing)	C	None		0.000	138.000	No Ice 1/2" Ice	17.200 22.300	17.200 22.300
RRUS-11 (AT&T Existing)	A	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.994 3.226	1.246 1.412
RRUS-11 (AT&T Existing)	B	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.994 3.226	1.246 1.412
RRUS-11 (AT&T Existing)	C	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.994 3.226	1.246 1.412
RRUS-12 (AT&T Proposed)	A	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	3.669 3.926	1.488 1.673
RRUS-12 (AT&T Proposed)	B	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	3.669 3.926	1.488 1.673
RRUS-12 (AT&T Proposed)	C	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	3.669 3.926	1.488 1.673
A2 (AT&T Proposed)	A	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.424 2.633	0.542 0.675
A2 (AT&T Proposed)	B	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.424 2.633	0.542 0.675
A2 (AT&T Proposed)	C	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.424 2.633	0.542 0.675
DC6-48-60-18-8F Surge Arrestor (AT&T Existing)	C	From Face	0.500 0.000 0.000	0.000	129.000	No Ice 1/2" Ice	2.228 2.447	2.228 2.447
Valmont Uni-Tri Bracket (AT&T Existing)	C	None		0.000	129.000	No Ice 1/2" Ice	1.750 1.940	1.750 1.940
7770.00 (AT&T Existing)	A	From Face	3.000 -6.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
7770.00 (AT&T Existing)	A	From Face	3.000 2.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
HPA-65R-BUU-H6 (AT&T Proposed)	A	From Face	3.000 6.000	0.000	127.000	No Ice 1/2" Ice	10.360 10.927	6.450 6.913

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	<b>Client</b>	AT&T Mobility	<b>Designed by</b> TJL

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
7770.00 (AT&T Existing)	B	From Face	0.000 3.000 -6.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
7770.00 (AT&T Existing)	B	From Face	3.000 2.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
HPA-65R-BUU-H6 (AT&T Proposed)	B	From Face	3.000 6.000 0.000	0.000	127.000	No Ice 1/2" Ice	10.360 10.927	6.450 6.913
7770.00 (AT&T Existing)	C	From Face	3.000 -6.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
7770.00 (AT&T Existing)	C	From Face	3.000 2.000 0.000	0.000	127.000	No Ice 1/2" Ice	5.882 6.314	2.928 3.273
HPA-65R-BUU-H6 (AT&T Proposed)	C	From Face	3.000 6.000 0.000	0.000	127.000	No Ice 1/2" Ice	10.360 10.927	6.450 6.913
(4) LGP214nn TMA (AT&T Existing)	A	From Face	3.000 0.000 0.000	0.000	127.000	No Ice 1/2" Ice	0.000 0.000	0.233 0.313
(4) LGP214nn TMA (AT&T Existing)	B	From Face	3.000 0.000 0.000	0.000	127.000	No Ice 1/2" Ice	0.000 0.000	0.233 0.313
(4) LGP214nn TMA (AT&T Existing)	C	From Face	3.000 0.000 0.000	0.000	127.000	No Ice 1/2" Ice	0.000 0.000	0.233 0.313
Valmont 13' Low Profile Platform (AT&T Existing)	C	None		0.000	125.000	No Ice 1/2" Ice	15.700 20.100	15.700 20.100
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	A	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	6.699 7.131	2.003 2.326
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	B	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	6.699 7.131	2.003 2.326
APX16DWV-16DWV-S-E-A CU (T-Mobile Existing)	C	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	6.699 7.131	2.003 2.326
(2) 10"x8"x3" TMA (T-Mobile Existing)	A	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	0.000 0.000	0.292 0.380
(2) 10"x8"x3" TMA (T-Mobile Existing)	B	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	0.000 0.000	0.292 0.380
(2) 10"x8"x3" TMA (T-Mobile Existing)	C	From Face	3.000 6.000 0.000	0.000	113.000	No Ice 1/2" Ice	0.000 0.000	0.292 0.380
13' Platform w/Rails (T-Mobile Existing)	C	None		0.000	113.000	No Ice 1/2" Ice	17.200 22.300	17.200 22.300
4'-6" Standoff (Town - Existing)	A	From Face	3.000 0.000 0.000	0.000	104.000	No Ice 1/2" Ice	2.100 2.480	0.156 0.212
4'-6" Standoff (Town - Existing)	A	From Face	3.000 0.000 0.000	0.000	104.000	No Ice 1/2" Ice	2.100 2.480	0.156 0.212

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
4'-6" Standoff (Town - Existing)	B	From Face	3.000 0.000 0.000	0.000	104.000	No Ice 1/2" Ice 2.100 2.480 0.156 0.212 0.040 0.057		
4'-6" Standoff (Town - Existing)	C	From Face	3.000 0.000 0.000	0.000	104.000	No Ice 1/2" Ice 2.100 2.480 0.156 0.212 0.040 0.057		
1142-2B (Town - Existing)	B	From Face	5.000 0.000 4.000	0.000	104.000	No Ice 1/2" Ice 1.120 2.535 1.120 2.535 0.010 0.021		
ASPA685 (Town - Existing)	B	From Face	5.000 0.000 -10.500	0.000	104.000	No Ice 1/2" Ice 5.250 7.379 5.250 7.379 0.022 0.060		
DB222 (Town - Existing)	A	From Face	5.000 0.000 5.000	0.000	104.000	No Ice 1/2" Ice 1.600 2.880 1.600 2.880 0.016 0.021		
ASPA685 (Town - Existing)	A	From Face	5.000 0.000 -10.500	0.000	104.000	No Ice 1/2" Ice 5.250 7.379 5.250 7.379 0.022 0.060		
DB846F65ZAXY (Verizon - Existing)	A	From Face	3.000 -6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
BXA-171063/8BF (Verizon - Existing)	A	From Face	3.000 -3.000 0.000	0.000	80.000	No Ice 1/2" Ice 2.941 3.255 2.156 2.458 0.011 0.029		
BXA-70063/6CF (Verizon - Existing)	A	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.731 8.268 4.158 4.595 0.012 0.054		
DB846F65ZAXY (Verizon - Existing)	A	From Face	3.000 6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
DB846F65ZAXY (Verizon - Existing)	B	From Face	3.000 -6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
BXA-171063/8BF (Verizon - Existing)	B	From Face	3.000 -3.000 0.000	0.000	80.000	No Ice 1/2" Ice 2.941 3.255 2.156 2.458 0.011 0.029		
BXA-70063/6CF (Verizon - Existing)	B	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.731 8.268 4.158 4.595 0.012 0.054		
DB846F65ZAXY (Verizon - Existing)	B	From Face	3.000 6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
DB846F65ZAXY (Verizon - Existing)	C	From Face	3.000 -6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
BXA-171063/8BF (Verizon - Existing)	C	From Face	3.000 -3.000 0.000	0.000	80.000	No Ice 1/2" Ice 2.941 3.255 2.156 2.458 0.011 0.029		
BXA-70063/6CF (Verizon - Existing)	C	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.731 8.268 4.158 4.595 0.012 0.054		
DB846F65ZAXY (Verizon - Existing)	C	From Face	3.000 6.000 0.000	0.000	80.000	No Ice 1/2" Ice 7.033 7.536 6.158 6.619 0.021 0.070		
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	A	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice 0.000 0.000 0.085 0.136 0.003 0.005		

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	B	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice	0.000 0.000	0.085 0.136
(2) FD9R6004/2C-3L Diplexer (Verizon - Existing)	C	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice	0.000 0.000	0.085 0.136
BXA-171063-12CF (Verizon - Existing)	A	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	4.791 5.242	3.618 4.058
BXA-171063-12CF (Verizon - Existing)	B	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	4.791 5.242	3.618 4.058
BXA-171063-12CF (Verizon - Existing)	C	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	4.791 5.242	3.618 4.058
RRH2x40-AWS (Verizon - Existing)	A	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	2.522 2.753	1.589 1.795
RRH2x40-AWS (Verizon - Existing)	B	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	2.522 2.753	1.589 1.795
RRH2x40-AWS (Verizon - Existing)	C	From Face	3.000 3.000 0.000	0.000	80.000	No Ice 1/2" Ice	2.522 2.753	1.589 1.795
DB-T1-6Z-8AB-0Z (Verizon - Existing)	C	From Face	3.000 0.000 0.000	0.000	80.000	No Ice 1/2" Ice	5.600 5.915	2.333 2.558
Valmont 13' Low Profile Platform (Verizon - Existing)	C	None		0.000	78.000	No Ice 1/2" Ice	15.700 20.100	15.700 20.100
Stand-off	A	From Face	1.000 0.000 0.000	0.000	40.000	No Ice 1/2" Ice	0.750 0.950	0.750 0.950
GPS (Existing)	A	From Face	2.000 0.000 0.000	0.000	40.000	No Ice 1/2" Ice	1.000 1.500	1.000 1.500

### Tower Pressures - No Ice

$$G_H = 1.690$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L1 150.000-95.83	121.781	1.452	0.030	128.832	A B C	0.000 0.000 0.000	128.832 128.832 128.832	128.832	100.00	0.000	4.393
0											
L2 95.830-47.830	71.470	1.247	0.026	149.101	A B	0.000 0.000	149.101 149.101	149.101	100.00	0.000	14.880

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Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L3 47.830-30.000	38.802	1.047	0.022	63.172	C	0.000	149.101	63.172	100.00	0.000	11.551
					A	0.000	63.172		100.00	0.000	5.527
					B	0.000	63.172		100.00	0.000	0.580
					C	0.000	63.172		100.00	0.000	7.061
L4 30.000-0.000	14.709	1	0.021	117.174	A	0.000	117.174	117.174	100.00	0.000	8.370
					B	0.000	117.174		100.00	0.000	1.566
					C	0.000	117.174		100.00	0.000	10.692

## Tower Pressure - With Ice

$$G_H = 1.690$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub>	t <sub>Z</sub> in	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L1 150.000-95.830	121.781	1.452	0.023	0.500	133.346	A	0.000	133.346	133.346	100.00	0.000	7.227
						B	0.000	133.346		100.00	0.000	0.000
						C	0.000	133.346		100.00	0.000	0.000
L2 95.830-47.830	71.470	1.247	0.019	0.500	153.101	A	0.000	153.101	153.101	100.00	0.000	24.480
						B	0.000	153.101		100.00	0.000	0.000
						C	0.000	153.101		100.00	0.000	17.385
L3 47.830-30.000	38.802	1.047	0.016	0.500	64.658	A	0.000	64.658	64.658	100.00	0.000	9.093
						B	0.000	64.658		100.00	0.000	1.580
						C	0.000	64.658		100.00	0.000	10.627
L4 30.000-0.000	14.709	1	0.016	0.500	119.674	A	0.000	119.674	119.674	100.00	0.000	13.770
						B	0.000	119.674		100.00	0.000	4.266
						C	0.000	119.674		100.00	0.000	16.092

## Tower Pressure - Service

$$G_H = 1.690$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L1 150.000-95.83	121.781	1.452	0.009	128.832	A	0.000	128.832	128.832	100.00	0.000	4.393
					B	0.000	128.832		100.00	0.000	0.000
					C	0.000	128.832		100.00	0.000	0.000
L2 95.830-47.830	71.470	1.247	0.008	149.101	A	0.000	149.101	149.101	100.00	0.000	14.880
					B	0.000	149.101		100.00	0.000	0.000
					C	0.000	149.101		100.00	0.000	11.551
L3 47.830-30.000	38.802	1.047	0.007	63.172	A	0.000	63.172	63.172	100.00	0.000	5.527
					B	0.000	63.172		100.00	0.000	0.580
					C	0.000	63.172		100.00	0.000	7.061
L4 30.000-0.000	14.709	1	0.006	117.174	A	0.000	117.174	117.174	100.00	0.000	8.370
					B	0.000	117.174		100.00	0.000	1.566
					C	0.000	117.174		100.00	0.000	10.692

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### Tower Forces - No Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1 150.000-95.83	1.467	4.718	A	1	1.03	1	1	1	128.832	6.961	0.128	C
0			B	1	1.03	1	1	1	128.832			
L2 95.830-47.830	2.359	7.959	C	1	1.03	1	1	1	128.832	7.826	0.163	C
			A	1	1.03	1	1	1	149.101			
			B	1	1.03	1	1	1	149.101			
			C	1	1.03	1	1	1	149.101			
L3 47.830-30.000	0.979	4.777	A	1	1.03	1	1	1	63.172	2.872	0.161	C
			B	1	1.03	1	1	1	63.172			
			C	1	1.03	1	1	1	63.172			
L4 30.000-0.000	1.486	9.708	A	1	1.03	1	1	1	117.174	4.952	0.165	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
Sum Weight:	6.291	27.161						OTM	1591.247 kip-ft	22.610		

### Tower Forces - No Ice - Wind 45 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1 150.000-95.83	1.467	4.718	A	1	1.03	1	1	1	128.832	6.961	0.128	C
0			B	1	1.03	1	1	1	128.832			
L2 95.830-47.830	2.359	7.959	C	1	1.03	1	1	1	128.832	7.826	0.163	C
			A	1	1.03	1	1	1	149.101			
			B	1	1.03	1	1	1	149.101			
			C	1	1.03	1	1	1	149.101			
L3 47.830-30.000	0.979	4.777	A	1	1.03	1	1	1	63.172	2.872	0.161	C
			B	1	1.03	1	1	1	63.172			
			C	1	1.03	1	1	1	63.172			
L4 30.000-0.000	1.486	9.708	A	1	1.03	1	1	1	117.174	4.952	0.165	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
Sum Weight:	6.291	27.161						OTM	1591.247 kip-ft	22.610		

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1 150.000-95.83	1.467	4.718	A	1	1.03	1	1	1	128.832	6.961	0.128	C
0			B	1	1.03	1	1	1	128.832			
L2 95.830-47.830	2.359	7.959	C	1	1.03	1	1	1	128.832	7.826	0.163	C
			A	1	1.03	1	1	1	149.101			
			B	1	1.03	1	1	1	149.101			
			C	1	1.03	1	1	1	149.101			

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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L3 47.830-30.000	0.979	4.777	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	63.172 63.172 63.172	2.872	0.161	C
L4 30.000-0.000	1.486	9.708	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	117.174 117.174 117.174	4.952	0.165	C
Sum Weight:	6.291	27.161						OTM	1591.247 kip-ft	22.610		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1 150.000-95.83	1.467	4.718	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	128.832 128.832 128.832	6.961	0.128	C
0 95.830-47.830	2.359	7.959	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	149.101 149.101 149.101	7.826	0.163	C
L2 47.830-30.000	0.979	4.777	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	63.172 63.172 63.172	2.872	0.161	C
L3 30.000-0.000	1.486	9.708	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	117.174 117.174 117.174	4.952	0.165	C
Sum Weight:	6.291	27.161						OTM	1591.247 kip-ft	22.610		

### Tower Forces - With Ice - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1 150.000-95.83	2.163	5.703	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	133.346 133.346 133.346	5.506	0.102	C
0 95.830-47.830	4.438	9.094	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	153.101 153.101 153.101	6.507	0.136	C
L2 47.830-30.000	1.895	5.257	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	64.658 64.658 64.658	2.420	0.136	C
L3 30.000-0.000	2.881	10.597	A B C	1 1 1	1.03 1.03 1.03	1 1 1	1 1 1	1 1 1	119.674 119.674 119.674	4.137	0.138	C
Sum Weight:	11.377	30.651						OTM	1290.244 kip-ft	18.569		

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### Tower Forces - With Ice - Wind 45 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
L1 150.000-95.83	2.163	5.703	A	1	1.03	1	1	1	133.346	5.506	0.102	C
0			B	1	1.03	1	1	1	133.346			
L2 95.830-47.830	4.438	9.094	C	1	1.03	1	1	1	133.346	6.507	0.136	C
			A	1	1.03	1	1	1	153.101			
			B	1	1.03	1	1	1	153.101			
			C	1	1.03	1	1	1	153.101			
L3 47.830-30.000	1.895	5.257	A	1	1.03	1	1	1	64.658	2.420	0.136	C
			B	1	1.03	1	1	1	64.658			
			C	1	1.03	1	1	1	64.658			
L4 30.000-0.000	2.881	10.597	A	1	1.03	1	1	1	119.674	4.137	0.138	C
			B	1	1.03	1	1	1	119.674			
			C	1	1.03	1	1	1	119.674			
Sum Weight:	11.377	30.651						OTM	1290.244 kip-ft	18.569		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
L1 150.000-95.83	2.163	5.703	A	1	1.03	1	1	1	133.346	5.506	0.102	C
0			B	1	1.03	1	1	1	133.346			
L2 95.830-47.830	4.438	9.094	C	1	1.03	1	1	1	133.346	6.507	0.136	C
			A	1	1.03	1	1	1	153.101			
			B	1	1.03	1	1	1	153.101			
			C	1	1.03	1	1	1	153.101			
L3 47.830-30.000	1.895	5.257	A	1	1.03	1	1	1	64.658	2.420	0.136	C
			B	1	1.03	1	1	1	64.658			
			C	1	1.03	1	1	1	64.658			
L4 30.000-0.000	2.881	10.597	A	1	1.03	1	1	1	119.674	4.137	0.138	C
			B	1	1.03	1	1	1	119.674			
			C	1	1.03	1	1	1	119.674			
Sum Weight:	11.377	30.651						OTM	1290.244 kip-ft	18.569		

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w klf	Ctrl. Face
L1 150.000-95.83	2.163	5.703	A	1	1.03	1	1	1	133.346	5.506	0.102	C
0			B	1	1.03	1	1	1	133.346			
L2 95.830-47.830	4.438	9.094	C	1	1.03	1	1	1	133.346	6.507	0.136	C

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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
95.830-47.830			B	1	1.03	1	1	1	153.101			
L3	1.895	5.257	C	1	1.03	1	1	1	153.101			
47.830-30.000			A	1	1.03	1	1	1	64.658	2.420	0.136	C
L4	2.881	10.597	B	1	1.03	1	1	1	64.658			
30.000-0.000			C	1	1.03	1	1	1	64.658			
Sum Weight:	11.377	30.651	A	1	1.03	1	1	1	119.674	4.137	0.138	C
			B	1	1.03	1	1	1	119.674			
			C	1	1.03	1	1	1	119.674			
								OTM	1290.244			
									kip-ft	18.569		

### Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1	1.467	4.718	A	1	1.03	1	1	1	128.832	2.148	0.040	C
150.000-95.83			B	1	1.03	1	1	1	128.832			
0			C	1	1.03	1	1	1	128.832			
L2	2.359	7.959	A	1	1.03	1	1	1	149.101	2.415	0.050	C
95.830-47.830			B	1	1.03	1	1	1	149.101			
L3	0.979	4.777	C	1	1.03	1	1	1	149.101			
47.830-30.000			A	1	1.03	1	1	1	63.172	0.886	0.050	C
L4	1.486	9.708	B	1	1.03	1	1	1	63.172			
30.000-0.000			C	1	1.03	1	1	1	63.172			
Sum Weight:	6.291	27.161	A	1	1.03	1	1	1	117.174	1.528	0.051	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
								OTM	491.126			
									kip-ft	6.978		

### Tower Forces - Service - Wind 45 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	klf	
L1	1.467	4.718	A	1	1.03	1	1	1	128.832	2.148	0.040	C
150.000-95.83			B	1	1.03	1	1	1	128.832			
0			C	1	1.03	1	1	1	128.832			
L2	2.359	7.959	A	1	1.03	1	1	1	149.101	2.415	0.050	C
95.830-47.830			B	1	1.03	1	1	1	149.101			
L3	0.979	4.777	C	1	1.03	1	1	1	149.101			
47.830-30.000			A	1	1.03	1	1	1	63.172	0.886	0.050	C
L4	1.486	9.708	B	1	1.03	1	1	1	63.172			
30.000-0.000			C	1	1.03	1	1	1	63.172			
Sum Weight:	6.291	27.161	A	1	1.03	1	1	1	117.174	1.528	0.051	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
								OTM	491.126			
									kip-ft	6.978		

<b>tnxTower</b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	16071.42 - CT2128	Page
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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	kN	

### Tower Forces - Service - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
L1 150.000-95.83	1.467	4.718	A	1	1.03	1	1	1	128.832	2.148	0.040	C
0			B	1	1.03	1	1	1	128.832			
L2 95.830-47.830	2.359	7.959	C	1	1.03	1	1	1	128.832			
			A	1	1.03	1	1	1	149.101	2.415	0.050	C
			B	1	1.03	1	1	1	149.101			
			C	1	1.03	1	1	1	149.101			
L3 47.830-30.000	0.979	4.777	A	1	1.03	1	1	1	63.172	0.886	0.050	C
			B	1	1.03	1	1	1	63.172			
			C	1	1.03	1	1	1	63.172			
L4 30.000-0.000	1.486	9.708	A	1	1.03	1	1	1	117.174	1.528	0.051	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
Sum Weight:	6.291	27.161						OTM	491.126	6.978		
									kip-ft			

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
L1 150.000-95.83	1.467	4.718	A	1	1.03	1	1	1	128.832	2.148	0.040	C
0			B	1	1.03	1	1	1	128.832			
L2 95.830-47.830	2.359	7.959	C	1	1.03	1	1	1	128.832			
			A	1	1.03	1	1	1	149.101	2.415	0.050	C
			B	1	1.03	1	1	1	149.101			
			C	1	1.03	1	1	1	149.101			
L3 47.830-30.000	0.979	4.777	A	1	1.03	1	1	1	63.172	0.886	0.050	C
			B	1	1.03	1	1	1	63.172			
			C	1	1.03	1	1	1	63.172			
L4 30.000-0.000	1.486	9.708	A	1	1.03	1	1	1	117.174	1.528	0.051	C
			B	1	1.03	1	1	1	117.174			
			C	1	1.03	1	1	1	117.174			
Sum Weight:	6.291	27.161						OTM	491.126	6.978		
									kip-ft			

### Force Totals

<b><i>tnxTower</i></b>  <b>Centek Engineering Inc.</b> 63-2 North Branford Rd. Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Job</b>	16071.42 - CT2128	<b>Page</b>
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	<b>Client</b>	AT&T Mobility	<b>Designed by</b> TJL

Load Case	Vertical Forces <i>K</i>	Sum of Forces <i>X</i> <i>K</i>	Sum of Forces <i>Z</i> <i>K</i>	Sum of Overturning Moments, <i>M<sub>x</sub></i> kip-ft	Sum of Overturning Moments, <i>M<sub>z</sub></i> kip-ft	Sum of Torques kip-ft
Leg Weight	27.161					
Bracing Weight	0.000					
Total Member Self-Weight	27.161			-0.122	0.280	
Total Weight	43.964			-0.122	0.280	
Wind 0 deg - No Ice		-0.041	-41.689	-3869.746	4.540	-0.346
Wind 30 deg - No Ice		20.759	-36.083	-3349.185	-1927.405	-0.927
Wind 45 deg - No Ice		29.379	-29.449	-2733.347	-2728.083	-1.132
Wind 60 deg - No Ice		35.996	-20.809	-1931.245	-3342.828	-1.259
Wind 90 deg - No Ice		41.589	0.041	4.138	-3862.468	-1.254
Wind 120 deg - No Ice		36.037	20.880	1938.379	-3347.088	-0.913
Wind 135 deg - No Ice		29.437	29.507	2739.128	-2734.107	-0.642
Wind 150 deg - No Ice		20.830	36.124	3353.201	-1934.783	-0.327
Wind 180 deg - No Ice		0.041	41.689	3869.502	-3.979	0.346
Wind 210 deg - No Ice		-20.759	36.083	3348.941	1927.965	0.927
Wind 225 deg - No Ice		-29.379	29.449	2733.104	2728.644	1.132
Wind 240 deg - No Ice		-35.996	20.809	1931.001	3343.388	1.259
Wind 270 deg - No Ice		-41.589	-0.041	-4.382	3863.028	1.254
Wind 300 deg - No Ice		-36.037	-20.880	-1938.623	3347.648	0.913
Wind 315 deg - No Ice		-29.437	-29.507	-2739.372	2734.668	0.642
Wind 330 deg - No Ice		-20.830	-36.124	-3353.445	1935.343	0.327
Member Ice	3.490					
Total Weight Ice	57.968			-0.197	0.345	
Wind 0 deg - Ice		-0.036	-35.477	-3321.914	4.072	-0.299
Wind 30 deg - Ice		17.672	-30.706	-2875.025	-1654.892	-1.191
Wind 45 deg - Ice		25.010	-25.061	-2346.370	-2342.443	-1.529
Wind 60 deg - Ice		30.644	-17.708	-1657.827	-2870.337	-1.763
Wind 90 deg - Ice		35.405	0.036	3.531	-3316.584	-1.863
Wind 120 deg - Ice		30.680	17.770	1663.890	-2874.064	-1.464
Wind 135 deg - Ice		25.061	25.112	2351.248	-2347.714	-1.106
Wind 150 deg - Ice		17.734	30.742	2878.359	-1661.348	-0.673
Wind 180 deg - Ice		0.036	35.477	3321.521	-3.382	0.299
Wind 210 deg - Ice		-17.672	30.706	2874.631	1655.582	1.191
Wind 225 deg - Ice		-25.010	25.061	2345.977	2343.133	1.529
Wind 240 deg - Ice		-30.644	17.708	1657.434	2871.027	1.763
Wind 270 deg - Ice		-35.405	-0.036	-3.924	3317.275	1.863
Wind 300 deg - Ice		-30.680	-17.770	-1664.283	2874.754	1.464
Wind 315 deg - Ice		-25.061	-25.112	-2351.641	2348.404	1.106
Wind 330 deg - Ice		-17.734	-30.742	-2878.752	1662.038	0.673
Total Weight	43.964			-0.122	0.280	
Wind 0 deg - Service		-0.013	-12.867	-1194.450	1.595	-0.107
Wind 30 deg - Service		6.407	-11.137	-1033.783	-594.684	-0.286
Wind 45 deg - Service		9.067	-9.089	-843.710	-841.807	-0.349
Wind 60 deg - Service		11.110	-6.423	-596.148	-1031.543	-0.389
Wind 90 deg - Service		12.836	0.013	1.193	-1191.926	-0.387
Wind 120 deg - Service		11.123	6.444	598.181	-1032.858	-0.282
Wind 135 deg - Service		9.085	9.107	845.325	-843.667	-0.198
Wind 150 deg - Service		6.429	11.149	1034.854	-596.961	-0.101
Wind 180 deg - Service		0.013	12.867	1194.206	-1.035	0.107
Wind 210 deg - Service		-6.407	11.137	1033.539	595.245	0.286
Wind 225 deg - Service		-9.067	9.089	843.466	842.368	0.349
Wind 240 deg - Service		-11.110	6.423	595.904	1032.104	0.389
Wind 270 deg - Service		-12.836	-0.013	-1.437	1192.486	0.387
Wind 300 deg - Service		-11.123	-6.444	-598.425	1033.418	0.282
Wind 315 deg - Service		-9.085	-9.107	-845.569	844.227	0.198
Wind 330 deg - Service		-6.429	-11.149	-1035.098	597.522	0.101

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<b>Client</b>	AT&T Mobility	<b>Designed by</b>	TJL

## Load Combinations

<i>Comb. No.</i>	<i>Description</i>
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 45 deg - No Ice
5	Dead+Wind 60 deg - No Ice
6	Dead+Wind 90 deg - No Ice
7	Dead+Wind 120 deg - No Ice
8	Dead+Wind 135 deg - No Ice
9	Dead+Wind 150 deg - No Ice
10	Dead+Wind 180 deg - No Ice
11	Dead+Wind 210 deg - No Ice
12	Dead+Wind 225 deg - No Ice
13	Dead+Wind 240 deg - No Ice
14	Dead+Wind 270 deg - No Ice
15	Dead+Wind 300 deg - No Ice
16	Dead+Wind 315 deg - No Ice
17	Dead+Wind 330 deg - No Ice
18	Dead+Ice+Temp
19	Dead+Wind 0 deg+Ice+Temp
20	Dead+Wind 30 deg+Ice+Temp
21	Dead+Wind 45 deg+Ice+Temp
22	Dead+Wind 60 deg+Ice+Temp
23	Dead+Wind 90 deg+Ice+Temp
24	Dead+Wind 120 deg+Ice+Temp
25	Dead+Wind 135 deg+Ice+Temp
26	Dead+Wind 150 deg+Ice+Temp
27	Dead+Wind 180 deg+Ice+Temp
28	Dead+Wind 210 deg+Ice+Temp
29	Dead+Wind 225 deg+Ice+Temp
30	Dead+Wind 240 deg+Ice+Temp
31	Dead+Wind 270 deg+Ice+Temp
32	Dead+Wind 300 deg+Ice+Temp
33	Dead+Wind 315 deg+Ice+Temp
34	Dead+Wind 330 deg+Ice+Temp
35	Dead+Wind 0 deg - Service
36	Dead+Wind 30 deg - Service
37	Dead+Wind 45 deg - Service
38	Dead+Wind 60 deg - Service
39	Dead+Wind 90 deg - Service
40	Dead+Wind 120 deg - Service
41	Dead+Wind 135 deg - Service
42	Dead+Wind 150 deg - Service
43	Dead+Wind 180 deg - Service
44	Dead+Wind 210 deg - Service
45	Dead+Wind 225 deg - Service
46	Dead+Wind 240 deg - Service
47	Dead+Wind 270 deg - Service
48	Dead+Wind 300 deg - Service
49	Dead+Wind 315 deg - Service
50	Dead+Wind 330 deg - Service

## Maximum Member Forces

<i>Section No.</i>	<i>Elevation ft</i>	<i>Component Type</i>	<i>Condition</i>	<i>Gov. Load Comb.</i>	<i>Force K</i>	<i>Major Axis Moment kip-ft</i>	<i>Minor Axis Moment kip-ft</i>
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<b><i>tnxTower</i></b> <b>Centek Engineering Inc.</b> <i>63-2 North Branford Rd.</i> <i>Branford, CT 06405</i> <i>Phone: (203) 488-0580</i> <i>FAX: (203) 488-8587</i>	<b>Job</b>	16071.42 - CT2128	<b>Page</b>	17 of 23
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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	150 - 95.83	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	18	-20.059	0.210	0.479
			Max. Mx	14	-12.603	633.997	0.338
			Max. My	2	-12.606	0.332	633.951
			Max. Vy	14	-21.591	633.997	0.338
			Max. Vx	2	-21.544	0.332	633.951
			Max. Torque	31			-2.142
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	18	-35.523	0.210	0.119
			Max. Mx	14	-24.265	1943.395	2.196
L2	95.83 - 47.83	Pole	Max. My	2	-24.259	2.329	1944.808
			Max. Vy	14	-33.691	1943.395	2.196
			Max. Vx	2	-33.792	2.329	1944.808
			Max. Torque	31			-2.141
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	18	-44.489	0.345	0.197
			Max. Mx	14	-31.968	2796.863	3.264
			Max. My	2	-31.965	3.432	2800.668
			Max. Vy	14	-37.339	2796.863	3.264
			Max. Vx	2	-37.440	3.432	2800.668
L3	47.83 - 30	Pole	Max. Torque	31			-1.859
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	18	-57.968	0.345	0.197
			Max. Mx	14	-43.942	3980.291	4.504
			Max. My	2	-43.942	4.674	3987.119
			Max. Vy	14	-41.612	3980.291	4.504
			Max. Vx	2	-41.712	4.674	3987.119
			Max. Torque	31			-1.858
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	18	-43.942	3980.291	4.504
L4	30 - 0	Pole	Max. Mx	2	-43.942	4.674	3987.119
			Max. My	14	-43.942	4.674	3987.119
			Max. Vy	14	-41.612	3980.291	4.504
			Max. Vx	2	-41.712	4.674	3987.119
			Max. Torque	31			-1.858

## Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	19	57.968	0.036	35.477
	Max. H <sub>x</sub>	14	43.964	41.589	0.041
	Max. H <sub>z</sub>	2	43.964	0.041	41.689
	Max. M <sub>x</sub>	2	3987.119	0.041	41.689
	Max. M <sub>z</sub>	6	3979.709	-41.589	-0.041
	Max. Torsion	23	1.856	-35.405	-0.036
	Min. Vert	1	43.964	0.000	0.000
	Min. H <sub>x</sub>	6	43.964	-41.589	-0.041
	Min. H <sub>z</sub>	10	43.964	-0.041	-41.689
	Min. M <sub>x</sub>	10	-3986.864	-0.041	-41.689
	Min. M <sub>z</sub>	14	-3980.291	41.589	0.041
	Min. Torsion	31	-1.857	35.405	0.036

## Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overshoring Moment, M <sub>x</sub> kip-ft	Overshoring Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	43.964	0.000	0.000	-0.122	0.280	0.000

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overswing Moment, M <sub>x</sub>	Overswing Moment, M <sub>z</sub>	Torque
	K	K	K	kip·ft	kip·ft	kip·ft
Dead+Wind 0 deg - No Ice	43.964	-0.041	-41.689	-3987.119	4.674	-0.346
Dead+Wind 30 deg - No Ice	43.964	20.759	-36.083	-3450.786	-1985.921	-0.922
Dead+Wind 45 deg - No Ice	43.964	29.379	-29.449	-2816.269	-2810.908	-1.125
Dead+Wind 60 deg - No Ice	43.964	35.996	-20.809	-1989.834	-3444.314	-1.251
Dead+Wind 90 deg - No Ice	43.964	41.589	0.041	4.262	-3979.709	-1.244
Dead+Wind 120 deg - No Ice	43.964	36.037	20.880	1997.170	-3448.674	-0.905
Dead+Wind 135 deg - No Ice	43.964	29.437	29.507	2822.203	-2817.083	-0.636
Dead+Wind 150 deg - No Ice	43.964	20.830	36.124	3454.900	-1993.497	-0.324
Dead+Wind 180 deg - No Ice	43.964	0.041	41.689	3986.864	-4.092	0.344
Dead+Wind 210 deg - No Ice	43.964	-20.759	36.083	3450.534	1986.497	0.921
Dead+Wind 225 deg - No Ice	43.964	-29.379	29.449	2816.021	2811.483	1.124
Dead+Wind 240 deg - No Ice	43.964	-35.996	20.809	1989.589	3444.890	1.251
Dead+Wind 270 deg - No Ice	43.964	-41.589	-0.041	-4.503	3980.291	1.246
Dead+Wind 300 deg - No Ice	43.964	-36.037	-20.880	-1997.415	3449.262	0.906
Dead+Wind 315 deg - No Ice	43.964	-29.437	-29.507	-2822.452	2817.673	0.637
Dead+Wind 330 deg - No Ice	43.964	-20.830	-36.124	-3455.152	1994.085	0.324
Dead+Ice+Temp	57.968	0.000	0.000	-0.197	0.345	0.000
Dead+Wind 0 deg+Ice+Temp	57.968	-0.036	-35.477	-3467.791	4.246	-0.299
Dead+Wind 30 deg+Ice+Temp	57.968	17.672	-30.706	-3001.286	-1727.623	-1.188
Dead+Wind 45 deg+Ice+Temp	57.968	25.010	-25.061	-2449.416	-2445.389	-1.525
Dead+Wind 60 deg+Ice+Temp	57.968	30.644	-17.708	-1730.634	-2996.477	-1.757
Dead+Wind 90 deg+Ice+Temp	57.968	35.405	0.036	3.684	-3462.318	-1.856
Dead+Wind 120 deg+Ice+Temp	57.968	30.680	17.770	1736.949	-3000.334	-1.458
Dead+Wind 135 deg+Ice+Temp	57.968	25.061	25.112	2454.487	-2450.853	-1.101
Dead+Wind 150 deg+Ice+Temp	57.968	17.734	30.742	3004.740	-1734.327	-0.670
Dead+Wind 180 deg+Ice+Temp	57.968	0.036	35.477	3467.369	-3.517	0.298
Dead+Wind 210 deg+Ice+Temp	57.968	-17.672	30.706	3000.871	1728.340	1.187
Dead+Wind 225 deg+Ice+Temp	57.968	-25.010	25.061	2449.008	2446.104	1.524
Dead+Wind 240 deg+Ice+Temp	57.968	-30.644	17.708	1730.233	2997.194	1.757
Dead+Wind 270 deg+Ice+Temp	57.968	-35.405	-0.036	-4.079	3463.048	1.857
Dead+Wind 300 deg+Ice+Temp	57.968	-30.680	-17.770	-1737.351	3001.077	1.459
Dead+Wind 315 deg+Ice+Temp	57.968	-25.061	-25.112	-2454.895	2451.597	1.102
Dead+Wind 330 deg+Ice+Temp	57.968	-17.734	-30.742	-3005.156	1735.069	0.669
Dead+Wind 0 deg - Service	43.964	-0.013	-12.867	-1232.234	1.647	-0.107
Dead+Wind 30 deg - Service	43.964	6.407	-11.137	-1066.486	-613.507	-0.287
Dead+Wind 45 deg - Service	43.964	9.067	-9.089	-870.401	-868.452	-0.350
Dead+Wind 60 deg - Service	43.964	11.110	-6.423	-615.008	-1064.193	-0.389
Dead+Wind 90 deg - Service	43.964	12.836	0.013	1.226	-1229.651	-0.387
Dead+Wind 120 deg - Service	43.964	11.123	6.444	617.097	-1065.546	-0.282
Dead+Wind 135 deg - Service	43.964	9.085	9.107	872.059	-870.366	-0.198
Dead+Wind 150 deg - Service	43.964	6.429	11.149	1067.582	-615.851	-0.101
Dead+Wind 180 deg - Service	43.964	0.013	12.867	1231.976	-1.061	0.107
Dead+Wind 210 deg - Service	43.964	-6.407	11.137	1066.229	614.092	0.286
Dead+Wind 225 deg - Service	43.964	-9.067	9.089	870.144	869.037	0.350
Dead+Wind 240 deg - Service	43.964	-11.110	6.423	614.752	1064.779	0.389
Dead+Wind 270 deg - Service	43.964	-12.836	-0.013	-1.482	1230.237	0.388
Dead+Wind 300 deg - Service	43.964	-11.123	-6.444	-617.353	1066.133	0.282
Dead+Wind 315 deg - Service	43.964	-9.085	-9.107	-872.316	870.952	0.198
Dead+Wind 330 deg - Service	43.964	-6.429	-11.149	-1067.840	616.438	0.101

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-43.964	0.000	0.000	43.964	0.000	0.000%
2	-0.041	-43.964	-41.689	0.041	43.964	41.689	0.000%
3	20.759	-43.964	-36.083	-20.759	43.964	36.083	0.000%

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
4	29.379	-43.964	-29.449	-29.379	43.964	29.449	0.000%
5	35.996	-43.964	-20.809	-35.996	43.964	20.809	0.000%
6	41.589	-43.964	0.041	-41.589	43.964	-0.041	0.000%
7	36.037	-43.964	20.880	-36.037	43.964	-20.880	0.000%
8	29.437	-43.964	29.507	-29.437	43.964	-29.507	0.000%
9	20.830	-43.964	36.124	-20.830	43.964	-36.124	0.000%
10	0.041	-43.964	41.689	-0.041	43.964	-41.689	0.000%
11	-20.759	-43.964	36.083	20.759	43.964	-36.083	0.000%
12	-29.379	-43.964	29.449	29.379	43.964	-29.449	0.000%
13	-35.996	-43.964	20.809	35.996	43.964	-20.809	0.000%
14	-41.589	-43.964	-0.041	41.589	43.964	0.041	0.000%
15	-36.037	-43.964	-20.880	36.037	43.964	20.880	0.000%
16	-29.437	-43.964	-29.507	29.437	43.964	29.507	0.000%
17	-20.830	-43.964	-36.124	20.830	43.964	36.124	0.000%
18	0.000	-57.968	0.000	0.000	57.968	0.000	0.000%
19	-0.036	-57.968	-35.477	0.036	57.968	35.477	0.000%
20	17.672	-57.968	-30.706	-17.672	57.968	30.706	0.000%
21	25.010	-57.968	-25.061	-25.010	57.968	25.061	0.000%
22	30.644	-57.968	-17.708	-30.644	57.968	17.708	0.000%
23	35.405	-57.968	0.036	-35.405	57.968	-0.036	0.000%
24	30.680	-57.968	17.770	-30.680	57.968	-17.770	0.000%
25	25.061	-57.968	25.112	-25.061	57.968	-25.112	0.000%
26	17.734	-57.968	30.742	-17.734	57.968	-30.742	0.000%
27	0.036	-57.968	35.477	-0.036	57.968	-35.477	0.000%
28	-17.672	-57.968	30.706	17.672	57.968	-30.706	0.000%
29	-25.010	-57.968	25.061	25.010	57.968	-25.061	0.000%
30	-30.644	-57.968	17.708	30.644	57.968	-17.708	0.000%
31	-35.405	-57.968	-0.036	35.405	57.968	0.036	0.000%
32	-30.680	-57.968	-17.770	30.680	57.968	17.770	0.000%
33	-25.061	-57.968	-25.112	25.061	57.968	25.112	0.000%
34	-17.734	-57.968	-30.742	17.734	57.968	30.742	0.000%
35	-0.013	-43.964	-12.867	0.013	43.964	12.867	0.000%
36	6.407	-43.964	-11.137	-6.407	43.964	11.137	0.000%
37	9.067	-43.964	-9.089	-9.067	43.964	9.089	0.000%
38	11.110	-43.964	-6.423	-11.110	43.964	6.423	0.000%
39	12.836	-43.964	0.013	-12.836	43.964	-0.013	0.000%
40	11.123	-43.964	6.444	-11.123	43.964	-6.444	0.000%
41	9.085	-43.964	9.107	-9.085	43.964	-9.107	0.000%
42	6.429	-43.964	11.149	-6.429	43.964	-11.149	0.000%
43	0.013	-43.964	12.867	-0.013	43.964	-12.867	0.000%
44	-6.407	-43.964	11.137	6.407	43.964	-11.137	0.000%
45	-9.067	-43.964	9.089	9.067	43.964	-9.089	0.000%
46	-11.110	-43.964	6.423	11.110	43.964	-6.423	0.000%
47	-12.836	-43.964	-0.013	12.836	43.964	0.013	0.000%
48	-11.123	-43.964	-6.444	11.123	43.964	6.444	0.000%
49	-9.085	-43.964	-9.107	9.085	43.964	9.107	0.000%
50	-6.429	-43.964	-11.149	6.429	43.964	11.149	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00024531
3	Yes	5	0.00000001	0.00032979
4	Yes	5	0.00000001	0.00037148

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5	Yes	5	0.00000001	0.00033948
6	Yes	4	0.00000001	0.00034531
7	Yes	5	0.00000001	0.00033095
8	Yes	5	0.00000001	0.00037261
9	Yes	5	0.00000001	0.00033671
10	Yes	4	0.00000001	0.00023299
11	Yes	5	0.00000001	0.00033763
12	Yes	5	0.00000001	0.00037155
13	Yes	5	0.00000001	0.00032851
14	Yes	4	0.00000001	0.00038182
15	Yes	5	0.00000001	0.00033969
16	Yes	5	0.00000001	0.00037278
17	Yes	5	0.00000001	0.00033334
18	Yes	4	0.00000001	0.00000001
19	Yes	5	0.00000001	0.00041612
20	Yes	5	0.00000001	0.00090824
21	Yes	6	0.00000001	0.00005488
22	Yes	5	0.00000001	0.00092742
23	Yes	5	0.00000001	0.00041756
24	Yes	5	0.00000001	0.00090940
25	Yes	6	0.00000001	0.00005502
26	Yes	5	0.00000001	0.00092344
27	Yes	5	0.00000001	0.00041601
28	Yes	5	0.00000001	0.00092294
29	Yes	6	0.00000001	0.00005488
30	Yes	5	0.00000001	0.00090504
31	Yes	5	0.00000001	0.00041793
32	Yes	5	0.00000001	0.00092970
33	Yes	6	0.00000001	0.00005505
34	Yes	5	0.00000001	0.00091436
35	Yes	4	0.00000001	0.00010806
36	Yes	4	0.00000001	0.00049962
37	Yes	4	0.00000001	0.00058778
38	Yes	4	0.00000001	0.00053032
39	Yes	4	0.00000001	0.00011522
40	Yes	4	0.00000001	0.00050114
41	Yes	4	0.00000001	0.00058983
42	Yes	4	0.00000001	0.00051971
43	Yes	4	0.00000001	0.00010782
44	Yes	4	0.00000001	0.00052478
45	Yes	4	0.00000001	0.00058817
46	Yes	4	0.00000001	0.00049554
47	Yes	4	0.00000001	0.00011612
48	Yes	4	0.00000001	0.00052953
49	Yes	4	0.00000001	0.00059101
50	Yes	4	0.00000001	0.00050948

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 95.83	31.290	50	1.728	0.001
L2	101 - 47.83	14.694	50	1.382	0.001
L3	54 - 30	4.026	50	0.717	0.000
L4	30 - 0	1.182	50	0.377	0.000

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## Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
149.000	10-ft Dipole	50	30.928	1.723	0.001	42894
138.000	APXVSPP18-C-A20	50	26.972	1.665	0.001	17872
129.000	RRUS-11	50	23.793	1.613	0.001	10212
127.000	7770.00	50	23.098	1.600	0.001	9324
125.000	Valmont 13' Low Profile Platform	50	22.408	1.587	0.001	8578
113.000	APX16DWV-16DWV-S-E-ACU	50	18.401	1.497	0.001	5795
104.000	4'-6" Standoff	50	15.587	1.414	0.001	4665
80.000	DB846F65ZAXY	50	9.138	1.110	0.001	4168
78.000	Valmont 13' Low Profile Platform	50	8.674	1.081	0.001	4149
40.000	Stand-off	50	2.129	0.513	0.000	3492

## Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 95.83	100.973	2	5.583	0.007
L2	101 - 47.83	47.465	17	4.465	0.006
L3	54 - 30	13.017	17	2.319	0.002
L4	30 - 0	3.825	17	1.218	0.001

## Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
149.000	10-ft Dipole	2	99.809	5.566	0.007	13503
138.000	APXVSPP18-C-A20	17	87.053	5.379	0.007	5625
129.000	RRUS-11	17	76.804	5.211	0.007	3212
127.000	7770.00	17	74.564	5.170	0.007	2932
125.000	Valmont 13' Low Profile Platform	17	72.340	5.128	0.007	2697
113.000	APX16DWV-16DWV-S-E-ACU	17	59.423	4.838	0.007	1820
104.000	4'-6" Standoff	17	50.348	4.568	0.007	1463
80.000	DB846F65ZAXY	17	29.533	3.587	0.004	1301
78.000	Valmont 13' Low Profile Platform	17	28.035	3.493	0.004	1295
40.000	Stand-off	17	6.886	1.661	0.001	1082

## Base Plate Design Data

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Plate Thickness	Number of Anchor Bolts	Anchor Bolt Size	Actual Allowable Ratio Bolt Tension K	Actual Allowable Ratio Concrete Stress ksi	Actual Allowable Ratio Plate Stress ksi	Actual Allowable Ratio Stiffener Stress ksi	Controlling Condition	Critical Ratio
in	in							
2.750	16	2.250	158.398	2.804	56.468		Plate	1.25
			131.211	2.800	45.000			✓
			1.21	1.00	1.25			

## Compression Checks

## Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	54.170	0.000	0.0	39.000	29.209	-12.599	1139.140	0.011
L2	95.83 - 47.83 (2)	TP41.644x31.965x0.375	53.170	0.000	0.0	39.000	48.476	-24.258	1890.570	0.013
L3	47.83 - 30 (3)	TP44.139x39.771x0.438	24.000	0.000	0.0	39.000	61.564	-31.964	2401.020	0.013
L4	30 - 0 (4)	TP49.6x44.139x0.58	30.000	0.000	0.0	39.000	91.550	-43.942	3570.440	0.012

## Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M <sub>x</sub> kip-ft	Actual f <sub>bx</sub> ksi	Allow. F <sub>bx</sub> ksi	Ratio F <sub>bx</sub> / F <sub>bx</sub>	Actual M <sub>y</sub> kip-ft	Actual f <sub>by</sub> ksi	Allow. F <sub>by</sub> ksi	Ratio f <sub>by</sub> / F <sub>by</sub>
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	634.217	33.078	39.000	0.848	0.000	0.000	39.000	0.000
L2	95.83 - 47.83 (2)	TP41.644x31.965x0.375	1946.35	49.160	39.000	1.261	0.000	0.000	39.000	0.000
L3	47.83 - 30 (3)	TP44.139x39.771x0.438	2802.52	51.236	39.000	1.314	0.000	0.000	39.000	0.000
L4	30 - 0 (4)	TP49.6x44.139x0.58	3989.29	43.803	39.000	1.123	0.000	0.000	39.000	0.000

## Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f <sub>v</sub> ksi	Allow. F <sub>v</sub> ksi	Ratio f <sub>v</sub> / F <sub>v</sub>	Actual T kip-ft	Actual f <sub>t</sub> ksi	Allow. F <sub>t</sub> ksi	Ratio f <sub>t</sub> / F <sub>t</sub>
L1	150 - 95.83 (1)	TP33.469x23.61x0.281	21.610	0.740	26.000	0.058	1.030	0.025	26.000	0.001
L2	95.83 - 47.83 (2)	TP41.644x31.965x0.375	33.804	0.697	26.000	0.054	0.431	0.005	26.000	0.000
L3	47.83 - 30 (3)	TP44.139x39.771x0.438	37.451	0.608	26.000	0.048	0.324	0.003	26.000	0.000
L4	30 - 0 (4)	TP49.6x44.139x0.58	41.723	0.456	26.000	0.036	0.324	0.002	26.000	0.000

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### Pole Interaction Design Data

Section No.	Elevation ft	Ratio P P <sub>a</sub>	Ratio f <sub>bx</sub> F <sub>bx</sub>	Ratio f <sub>by</sub> F <sub>by</sub>	Ratio f <sub>v</sub> F <sub>v</sub>	Ratio f <sub>vt</sub> F <sub>vt</sub>	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	150 - 95.83 (1)	0.011	0.848	0.000	0.058	0.001	0.860	1.333	H1-3+VT ✓
L2	95.83 - 47.83 (2)	0.013	1.261	0.000	0.054	0.000	1.274	1.333	H1-3+VT ✓
L3	47.83 - 30 (3)	0.013	1.314	0.000	0.048	0.000	1.328	1.333	H1-3+VT ✓
L4	30 - 0 (4)	0.012	1.123	0.000	0.036	0.000	1.136	1.333	H1-3+VT ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
L1	150 - 95.83	Pole	TP33.469x23.61x0.281	1	-12.599	1518.474	64.5	Pass
L2	95.83 - 47.83	Pole	TP41.644x31.965x0.375	2	-24.258	2520.130	95.6	Pass
L3	47.83 - 30	Pole	TP44.139x39.771x0.438	3	-31.964	3200.560	99.6	Pass
L4	30 - 0	Pole	TP49.6x44.139x0.58	4	-43.942	4759.396	85.2	Pass
						Summary		
						Pole (L3)	99.6	Pass
						Base Plate	94.1	Pass
						<b>RATING =</b>	<b>99.6</b>	<b>Pass</b>

**Caisson Foundation:**Input Data:Shear Force =  $S := 42k$  USER INPUT-FROM RisaTowerOverturning Moment =  $M := 3989\text{ft}\cdot\text{k}$  USER INPUT-FROM RisaTowerApplied Axial Load =  $A1 := 44k$  USER INPUT-FROM RisaTowerBending Moment =  $Mu := 4112\text{ft}\cdot\text{k}$  USER INPUT-FROM LPILEMoment Capacity =  $Mn := 9378\text{ft}\cdot\text{k}$  USER INPUT-FROM LPILEFoundation Diameter =  $d := 6.6\text{ft}$  USER INPUTOverall Length of Caisson =  $L_c := 26.5\text{ft}$  USER INPUTDepth From Top of Caisson to Grade =  $L_{pag} := 1\text{ft}$  USER INPUTNumber of Rebar =  $n := 40$  USER INPUTArea of Rebar =  $Ar := 1.56\text{in}^2$  USER INPUTRebar Yield Strength =  $f_y := 60\text{ksi}$  USER INPUTConcrete Comp Strength =  $f_c := 3.0\text{ksi}$  USER INPUTCheck Moment Capacity:Factor of Safety =  $FS := \frac{0.9Mn}{Mu} = 2.1$ Factor of Safety Required =  $FS_{reqd} := 1.3$  $FOSCheck := \text{if}(FS \geq FS_{reqd}, \text{"OK"}, \text{"NO GOOD"})$ 

FOSCheck = "OK"

Caisson Analysis.lpo

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LPILE Plus for Windows, Version 5.0 (5.0.47)

Analysis of Individual Piles and Drilled Shafts  
Subjected to Lateral Loading Using the p-y Method

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This program is licensed to:

TJL  
Centek Engineering

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Files Used for Analysis

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Path to file locations: J:\Jobs\1607100.WI\42\_Fairfield Greenfield  
Hill\04\_Structural\Backup Documentation\Calcs\Foundation\  
Name of input data file: Caisson Analysis.lpd  
Name of output file: Caisson Analysis.lpo  
Name of plot output file: Caisson Analysis.lpp  
Name of runtime file: Caisson Analysis.lpr

---

Time and Date of Analysis

---

Date: August 30, 2016 Time: 10:48:31

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Problem Title

---

16071.42 - CT2128

---

Program Options

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Units Used in Computations - US Customary Units: Inches, Pounds

## Caisson Analysis.lpo

### Basic Program Options:

#### Analysis Type 3:

- Computation of Nonlinear Bending Stiffness and Ultimate Bending Moment Capacity with Pile Response Computed Using Nonlinear EI

#### Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis does not use p-y multipliers (individual pile or shaft action only)
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- Analysis includes computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No additional p-y curves to be computed at user-specified depths

#### Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-04 in
- Maximum allowable deflection = 1.0000E+02 in

#### Printing Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (spacing of output points) = 8

---

### Pile Structural Properties and Geometry

---

Pile Length = 318.00 in

Depth of ground surface below top of pile = 12.00 in

Slope angle of ground surface = 0.00 deg.

Structural properties of pile defined using 2 points

Point No.	Point Depth in	Pile Diameter in	Moment of Inertia in**4	Pile Area Sq.in	Modulus of Elasticity lbs/Sq.in
1	0.0000	78.00000000	1816972.	4778.4000	3122018.
2	318.0000	78.00000000	1816972.	4778.4000	3122018.

Please note that because this analysis makes computations of ultimate moment capacity and pile response using nonlinear bending stiffness

Caisson Analysis.lpo

that the above values of moment of inertia and modulus of are not used for any computations other than total stress due to combined axial loading and bending.

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Soil and Rock Layering Information

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The soil profile is modelled using 3 layers

Layer 1 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 12.000 in  
Distance from top of pile to bottom of layer = 48.000 in  
p-y subgrade modulus k for top of soil layer = 10.000 lbs/in\*\*3  
p-y subgrade modulus k for bottom of layer = 10.000 lbs/in\*\*3

Layer 2 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 48.000 in  
Distance from top of pile to bottom of layer = 114.000 in  
p-y subgrade modulus k for top of soil layer = 90.000 lbs/in\*\*3  
p-y subgrade modulus k for bottom of layer = 90.000 lbs/in\*\*3

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 114.000 in  
Distance from top of pile to bottom of layer = 318.000 in  
p-y subgrade modulus k for top of soil layer = 27.000 lbs/in\*\*3  
p-y subgrade modulus k for bottom of layer = 27.000 lbs/in\*\*3

(Depth of lowest layer extends 0.00 in below pile tip)

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Effective Unit Weight of Soil vs. Depth

---

Effective unit weight of soil with depth defined using 6 points

Point No.	Depth X in	Eff. Unit Weight lbs/in**3
1	12.00	0.05700
2	48.00	0.05700
3	48.00	0.06900
4	114.00	0.06900
5	114.00	0.06100
6	318.00	0.06100

Caisson Analysis.lpo

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Shear Strength of Soils  
-----

Shear strength parameters with depth defined using 6 points

Point No.	Depth X in	Cohesion c lbs/in**2	Angle of Friction Deg.	E50 or k_rm	RQD %
1	12.000	0.00000	30.00	-----	-----
2	48.000	0.00000	30.00	-----	-----
3	48.000	0.00000	35.00	-----	-----
4	114.000	0.00000	35.00	-----	-----
5	114.000	0.00000	30.00	-----	-----
6	318.000	0.00000	30.00	-----	-----

Notes:

- (1) Cohesion = uniaxial compressive strength for rock materials.
- (2) Values of E50 are reported for clay strata.
- (3) Default values will be generated for E50 when input values are 0.
- (4) RQD and k\_rm are reported only for weak rock strata.

-----  
Loading Type  
-----

Static loading criteria was used for computation of p-y curves.

-----  
Pile-head Loading and Pile-head Fixity Conditions  
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Number of loads specified = 2

Load Case Number 1

Pile-head boundary conditions are Shear and Moment (BC Type 1)

Shear force at pile head = 42000.000 lbs

Bending moment at pile head = 47868000.000 in-lbs

Axial load at pile head = 44000.000 lbs

Caisson Analysis.lpo

Non-zero moment at pile head for this load case indicates the pile-head may rotate under the applied pile-head loading, but is not a free-head (zero moment) condition.

Load Case Number 2

Pile-head boundary conditions are Shear and Moment (BC Type 1)

Shear force at pile head = 13000.000 lbs

Bending moment at pile head = 14796000.000 in-lbs

Axial load at pile head = 44000.000 lbs

Non-zero moment at pile head for this load case indicates the pile-head may rotate under the applied pile-head loading, but is not a free-head (zero moment) condition.

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Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

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Number of sections = 1

Pile Section No. 1

The sectional shape is a circular drilled shaft (bored pile).

Outside Diameter = 78.0000 in

Material Properties:

Compressive Strength of Concrete = 3.000 kip/in\*\*2

Yield Stress of Reinforcement = 60. kip/in\*\*2

Modulus of Elasticity of Reinforcement = 29000. kip/in\*\*2

Number of Reinforcing Bars = 40

Area of Single Bar = 1.56000 in\*\*2

Number of Rows of Reinforcing Bars = 21

Area of Steel = 62.400 in\*\*2

Area of Shaft = 4778.362 in\*\*2

Percentage of Steel Reinforcement = 1.306 percent

Cover Thickness (edge to bar center) = 4.000 in

Unfactored Axial Squash Load Capacity = 15769.70 kip

Distribution and Area of Steel Reinforcement

Row	Area of	Distance to
-----	---------	-------------

Caisson Analysis.lpo

Number	Reinforcement in**2	Centroidal Axis in
1	1.560	35.000
2	3.120	34.569
3	3.120	33.287
4	3.120	31.185
5	3.120	28.316
6	3.120	24.749
7	3.120	20.572
8	3.120	15.890
9	3.120	10.816
10	3.120	5.475
11	3.120	0.000
12	3.120	-5.475
13	3.120	-10.816
14	3.120	-15.890
15	3.120	-20.572
16	3.120	-24.749
17	3.120	-28.316
18	3.120	-31.185
19	3.120	-33.287
20	3.120	-34.569
21	1.560	-35.000

Axial Thrust Force = 44000.00 lbs

Bending Max. Steel Moment Stress in-lbs psi	Bending Stiffness lb-in2	Bending Curvature rad/in	Maximum Strain in/in	Neutral Axis Position inches	Max. Concrete Stress psi
5671609.	6.805931E+12	8.333333E-07	0.00003525	42.29798439	108.13396
925.53462					
11278189.	6.766913E+12	0.00000167	0.00006787	40.72204855	206.00102
1774.89901					
16820316.	6.728126E+12	0.00000250	0.00010053	40.21376958	301.99249
2625.49829					
22296606.	6.688982E+12	0.00000333	0.00013316	39.94675192	395.85287
3474.85269					
22296606.	5.351185E+12	0.00000417	0.00010050	24.12084773	298.69647
6027.06423					
22296606.	4.459321E+12	0.00000500	0.00011911	23.82194844	351.83587
7275.81748					
22296606.	3.822275E+12	0.00000583	0.00013775	23.61385891	404.43178

Caisson Analysis.lpo

8523.65553					
22296606.	3.344491E+12	0.00000667	0.00015642	23.46256819	456.48168
9770.57015					
22296606.	2.972881E+12	0.00000750	0.00017537	23.38323721	508.70279
11009.14591					
22296606.	2.675593E+12	0.00000833	0.00019410	23.29158130	559.61073
12254.53452					
22296606.	2.432357E+12	0.00000917	0.00021285	23.22035381	609.97060
13498.92261					
22296606.	2.229661E+12	0.00001000	0.00023164	23.16448250	659.77969
14742.30007					
22790768.	2.103763E+12	0.00001083	0.00025047	23.12045494	709.03519
15984.65707					
24464552.	2.096962E+12	0.00001167	0.00026933	23.08576754	757.73441
17225.98198					
26135262.	2.090821E+12	0.00001250	0.00028823	23.05857459	805.87427
18466.26671					
27802879.	2.085216E+12	0.00001333	0.00030717	23.03750226	853.45200
19705.49913					
29467377.	2.080050E+12	0.00001417	0.00032614	23.02149752	900.46468
20943.66810					
31128726.	2.075248E+12	0.00001500	0.00034515	23.00973746	946.90918
22180.76420					
32786901.	2.070752E+12	0.00001583	0.00036419	23.00157818	992.78254
23416.77535					
34441875.	2.066512E+12	0.00001667	0.00038328	22.99650362	1038.08169
24651.68992					
36093620.	2.062493E+12	0.00001750	0.00040240	22.99409536	1082.80348
25885.49661					
37742108.	2.058660E+12	0.00001833	0.00042156	22.99401167	1126.94470
27118.18380					
39387309.	2.054990E+12	0.00001917	0.00044076	22.99597129	1170.50213
28349.73929					
41029193.	2.051460E+12	0.00002000	0.00045999	22.99973944	1213.47247
29580.15113					
42667734.	2.048051E+12	0.00002083	0.00047927	23.00512084	1255.85243
30809.40616					
44302896.	2.044749E+12	0.00002167	0.00049859	23.01194814	1297.63854
32037.49259					
45934653.	2.041540E+12	0.00002250	0.00051795	23.02008185	1338.82744
33264.39659					
47562975.	2.038413E+12	0.00002333	0.00053735	23.02940342	1379.41571
34490.10369					
49187819.	2.035358E+12	0.00002417	0.00055680	23.03980359	1419.39949
35714.60431					
50809168.	2.032367E+12	0.00002500	0.00057628	23.05120102	1458.77556
36937.87926					
52426977.	2.029431E+12	0.00002583	0.00059581	23.06351200	1497.53993
38159.91893					

Caisson Analysis.lpo					
54041215.	2.026546E+12	0.00002667	0.00061538	23.07667145	1535.68896
39380.70741					
55651848.	2.023704E+12	0.00002750	0.00063499	23.09062126	1573.21889
40600.22954					
57258839.	2.020900E+12	0.00002833	0.00065465	23.10530797	1610.12573
41818.47195					
58862157.	2.018131E+12	0.00002917	0.00067435	23.12068972	1646.40573
43035.41661					
60461761.	2.015392E+12	0.00003000	0.00069410	23.13672468	1682.05477
44251.04953					
62057616.	2.012679E+12	0.00003083	0.00071390	23.15337798	1717.06879
45465.35452					
63649678.	2.009990E+12	0.00003167	0.00073374	23.17061707	1751.44355
46678.31665					
65237914.	2.007320E+12	0.00003250	0.00075362	23.18841639	1785.17493
47889.91755					
68402746.	2.002032E+12	0.00003417	0.00079354	23.22560039	1850.69022
50308.96761					
71551773.	1.996794E+12	0.00003583	0.00083365	23.26476261	1913.57902
52722.36752					
74684666.	1.991591E+12	0.00003750	0.00087397	23.30577984	1973.80487
55129.96442					
77801052.	1.986410E+12	0.00003917	0.00091448	23.34854516	2031.32918
57531.61078					
80900567.	1.981238E+12	0.00004083	0.00095521	23.39298418	2086.11240
59927.14123					
83472928.	1.964069E+12	0.00004250	0.00099377	23.38280252	2135.08247
60000.00000					
85599826.	1.938109E+12	0.00004417	0.00103042	23.33034602	2179.04155
60000.00000					
87359822.	1.906032E+12	0.00004583	0.00106542	23.24547789	2218.65749
60000.00000					
88990574.	1.873486E+12	0.00004750	0.00109989	23.15565839	2255.48271
60000.00000					
90402656.	1.838698E+12	0.00004917	0.00113334	23.05106387	2289.10690
60000.00000					
91788236.	1.805670E+12	0.00005083	0.00116680	22.95351747	2320.70273
60000.00000					
92891535.	1.769363E+12	0.00005250	0.00119872	22.83278802	2348.89818
60000.00000					
93988620.	1.735175E+12	0.00005417	0.00123075	22.72150335	2375.33454
60000.00000					
95079397.	1.702915E+12	0.00005583	0.00126289	22.61885217	2399.99358
60000.00000					
95934310.	1.668423E+12	0.00005750	0.00129357	22.49680004	2421.74953
60000.00000					
96762584.	1.635424E+12	0.00005917	0.00132420	22.38081971	2441.77097
60000.00000					
97585613.	1.604147E+12	0.00006083	0.00135493	22.27283826	2460.15338

Caisson Analysis.lpo

60000.00000					
98403314.	1.574453E+12	0.00006250	0.00138576	22.17223969	2476.88025
60000.00000					
99263122.	1.546958E+12	0.00006417	0.00141808	22.10000101	2492.58936
60000.00000					
99734738.	1.514958E+12	0.00006583	0.00144816	21.99739400	2505.47366
60000.00000					
1.003254E+08	1.486302E+12	0.00006750	0.00147710	21.88299438	2516.31220
60000.00000					
1.009119E+08	1.458967E+12	0.00006917	0.00150614	21.77546391	2525.67037
60000.00000					
1.014941E+08	1.432858E+12	0.00007083	0.00153527	21.67433766	2533.53324
60000.00000					
1.020720E+08	1.407890E+12	0.00007250	0.00156449	21.57919720	2539.88555
60000.00000					
1.025497E+08	1.382693E+12	0.00007417	0.00159282	21.47623685	2544.56787
60000.00000					
1.029582E+08	1.357690E+12	0.00007583	0.00162056	21.36998489	2547.75136
60000.00000					
1.033631E+08	1.333717E+12	0.00007750	0.00164838	21.26942351	2549.55689
60000.00000					
1.037637E+08	1.310700E+12	0.00007917	0.00167629	21.17420635	2549.03904
60000.00000					
1.041588E+08	1.288562E+12	0.00008083	0.00170429	21.08401957	2544.86234
60000.00000					
1.045511E+08	1.267286E+12	0.00008250	0.00173238	20.99857262	2547.77391
60000.00000					
1.049407E+08	1.246820E+12	0.00008417	0.00176057	20.91760513	2549.48952
60000.00000					
1.053273E+08	1.227114E+12	0.00008583	0.00178885	20.84091720	2549.62886
60000.00000					
1.055803E+08	1.206632E+12	0.00008750	0.00182000	20.79999992	2544.73421
60000.00000					
1.060158E+08	1.188962E+12	0.00008917	0.00184946	20.74157390	2546.53561
60000.00000					
1.062692E+08	1.169936E+12	0.00009083	0.00187576	20.65059909	2548.53620
60000.00000					
1.065210E+08	1.151578E+12	0.00009250	0.00190214	20.56368300	2549.69065
60000.00000					
1.067710E+08	1.133851E+12	0.00009417	0.00192860	20.48072335	2549.43778
60000.00000					
1.070180E+08	1.116709E+12	0.00009583	0.00195518	20.40188983	2545.72565
60000.00000					
1.072638E+08	1.100141E+12	0.00009750	0.00198182	20.32637581	2543.59522
60000.00000					
1.075084E+08	1.084118E+12	0.00009917	0.00200852	20.25402090	2546.25745
60000.00000					
1.079939E+08	1.053599E+12	0.00010250	0.00206212	20.11820725	2549.45790
60000.00000					

Caisson Analysis.lpo					
1.084730E+08 60000.00000	1.024942E+12	0.00010583	0.00211602	19.99384680	2547.34798
1.089068E+08 60000.00000	9.976198E+11	0.00010917	0.00216945	19.87286165	2542.37954
1.092152E+08 60000.00000	9.708014E+11	0.00011250	0.00222069	19.73949346	2546.86437
1.095209E+08 60000.00000	9.455045E+11	0.00011583	0.00227211	19.61533526	2549.39866
1.095209E+08 60000.00000	9.190568E+11	0.00011917	0.00232375	19.49999884	2548.72474
1.101868E+08 60000.00000	8.994841E+11	0.00012250	0.00238525	19.47142741	2541.35765
1.104724E+08 60000.00000	8.779268E+11	0.00012583	0.00243579	19.35725793	2543.25677
1.107567E+08 60000.00000	8.574710E+11	0.00012917	0.00248646	19.25000176	2546.90278
1.110394E+08 60000.00000	8.380332E+11	0.00013250	0.00253726	19.14914981	2549.15575
1.113206E+08 60000.00000	8.195384E+11	0.00013583	0.00258820	19.05425110	2549.99466
1.115912E+08 60000.00000	8.018528E+11	0.00013917	0.00263976	18.96835783	2545.55047
1.118202E+08 60000.00000	7.847031E+11	0.00014250	0.00269117	18.88542143	2540.71344
1.119503E+08 60000.00000	7.676591E+11	0.00014583	0.00274177	18.80069974	2538.26009
1.120704E+08 60000.00000	7.513098E+11	0.00014917	0.00279301	18.72410014	2542.67351
1.121896E+08 60000.00000	7.356693E+11	0.00015250	0.00284437	18.65157786	2546.06503
1.123079E+08 60000.00000	7.206922E+11	0.00015583	0.00289583	18.58288416	2548.41978
1.124252E+08 60000.00000	7.063366E+11	0.00015917	0.00294741	18.51778892	2549.72243
1.125394E+08 60000.00000	6.925502E+11	0.00016250	0.00299928	18.45710573	2548.80721
1.126217E+08 60000.00000	6.791260E+11	0.00016583	0.00305338	18.41233662	2544.25842
1.127033E+08 60000.00000	6.662265E+11	0.00016917	0.00310758	18.36994556	2539.69142
1.127841E+08 60000.00000	6.538211E+11	0.00017250	0.00316189	18.32980236	2535.10597
1.128642E+08 60000.00000	6.418816E+11	0.00017583	0.00321631	18.29179314	2536.59239
1.129434E+08 60000.00000	6.303820E+11	0.00017917	0.00327083	18.25580862	2541.15055
1.130219E+08 60000.00000	6.192980E+11	0.00018250	0.00332547	18.22175118	2544.78116
1.131580E+08	6.089218E+11	0.00018583	0.00338217	18.20000008	2547.65936

Caisson Analysis.lpo

60000.00000						
1.134064E+08	5.995052E+11	0.00018917	0.00344283	18.20000008	2549.57550	
60000.00000						
1.136443E+08	5.903599E+11	0.00019250	0.00350350	18.20000008	2548.72471	
60000.00000						
1.138690E+08	5.814588E+11	0.00019583	0.00356417	18.20000008	2543.78409	
60000.00000						
1.140886E+08	5.728299E+11	0.00019917	0.00362483	18.20000008	2538.84346	
60000.00000						
1.140886E+08	5.634006E+11	0.00020250	0.00368480	18.19653413	2534.02595	
60000.00000						
1.140886E+08	5.542767E+11	0.00020583	0.00374265	18.18290046	2529.57959	
60000.00000						
1.140886E+08	5.454436E+11	0.00020917	0.00379781	18.15686515	2532.84163	
60000.00000						
1.140886E+08	5.368877E+11	0.00021250	0.00385194	18.12677810	2537.01904	
60000.00000						

Unfactored (Nominal) Moment Capacity at Concrete Strain of 0.003 = 112540.50458  
in-kip

Computed Values of Load Distribution and Deflection  
for Lateral Loading for Load Case Number 1

Pile-head boundary conditions are Shear and Moment (Pile-head Condition Type 1)  
Specified shear force at pile head = 42000.000 lbs  
Specified moment at pile head = 47868000.000 in-lbs  
Specified axial load at pile head = 44000.000 lbs

Depth Es*h F/L	Deflect. X in	Moment M lbs-in	Shear V lbs	Slope S Rad.	Total Stress lbs/in**2	Flx. Rig. EI	Soil Res. p lbs/in
0.000	2.028	4.79E+07	42000.	-0.011970	1036.660	2.04E+12	0.000
0.000							
25.440	1.731	4.89E+07	40376.	-0.011365	1059.721	2.04E+12	-232.653
427.392							
50.880	1.450	4.99E+07	28627.	-0.010747	1079.585	2.03E+12	-1399.986
3070.824							
76.320	1.184	5.00E+07	-23386.	-0.010121	1082.804	2.03E+12	-2683.732
7206.078							

Caisson Analysis.lpo

101.760	0.934741	4.84E+07	-1.07E+05	-0.009503	1048.901	2.04E+12	-3826.926
13019.							
127.200	0.700492	4.46E+07	-1.86E+05	-0.008921	966.443	2.04E+12	-2342.177
10633.							
152.640	0.480323	3.92E+07	-2.41E+05	-0.008400	849.601	2.06E+12	-1935.940
12817.							
178.080	0.272449	3.25E+07	-2.82E+05	-0.007957	706.131	2.07E+12	-1285.246
15001.							
203.520	0.074699	2.50E+07	-3.04E+05	-0.007606	545.060	2.10E+12	-403.692
17186.							
228.960	-0.116678	1.72E+07	-3.01E+05	-0.007480	378.637	6.72E+12	710.699
19370.							
254.400	-0.306266	9.93E+06	-2.66E+05	-0.007429	222.371	6.77E+12	2075.874
21554.							
279.840	-0.494894	4.01E+06	-1.93E+05	-0.007404	95.230	6.81E+12	3694.328
23738.							
305.280	-0.683121	4.89E+05	-75904.	-0.007396	19.700	6.81E+12	5568.650
25923.							

Please note that because this analysis makes computations of ultimate moment capacity and pile response using nonlinear bending stiffness that the above values of total stress due to combined axial stress and bending may not be representative of actual conditions.

#### Output Verification:

Computed forces and moments are within specified convergence limits.

#### Output Summary for Load Case No. 1:

Pile-head deflection	=	2.02789291 in
Computed slope at pile head	=	-0.01196952
Maximum bending moment	=	50120832. lbs-in
Maximum shear force	=	-306385.08079 lbs
Depth of maximum bending moment	=	66.78000000 in
Depth of maximum shear force	=	213.06000 in
Number of iterations	=	21
Number of zero deflection points	=	1

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Computed Values of Load Distribution and Deflection  
for Lateral Loading for Load Case Number 2

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Caisson Analysis.lpo

Pile-head boundary conditions are Shear and Moment (Pile-head Condition Type 1)  
 Specified shear force at pile head = 13000.000 lbs  
 Specified moment at pile head = 14796000.000 in-lbs  
 Specified axial load at pile head = 44000.000 lbs

Depth Es*h F/L	Depth	Deflect.	Moment	Shear	Slope	Total	Flx.	Rig.	Soil Res.
	X in	y in	M lbs-in	V lbs	S Rad.	Stress lbs/in**2	EI lbs-in**2	p lbs/in	
<hr/>									
0.000	0.000	0.373013	1.48E+07	13000.	-0.002086	326.794	6.74E+12	0.000	
25.440	427.392	0.320649	1.51E+07	12700.	-0.002030	333.913	6.74E+12	-43.095	
50.880	9749.945	0.269739	1.54E+07	9615.875	-0.001972	340.441	6.74E+12	-827.025	
76.320	17031.	0.220308	1.54E+07	-16371.	-0.001914	339.065	6.74E+12	-1179.888	
101.760	24312.	0.172348	1.46E+07	-48579.	-0.001857	321.541	6.74E+12	-1317.641	
127.200	10633.	0.125779	1.30E+07	-69493.	-0.001805	287.805	6.75E+12	-420.556	
152.640	12817.	0.080452	1.11E+07	-79089.	-0.001760	247.166	6.77E+12	-324.260	
178.080	15001.	0.036183	8.99E+06	-85502.	-0.001722	202.087	6.78E+12	-170.689	
203.520	17186.	-0.007228	6.78E+06	-87293.	-0.001692	154.700	6.79E+12	39.064	
228.960	19370.	-0.049994	4.60E+06	-83039.	-0.001671	107.918	6.81E+12	304.517	
254.400	21554.	-0.092320	2.62E+06	-71323.	-0.001658	65.430	6.81E+12	625.745	
279.840	23738.	-0.134394	1.05E+06	-50720.	-0.001651	31.698	6.81E+12	1003.237	
305.280	25923.	-0.176363	1.29E+05	-19791.	-0.001649	11.968	6.81E+12	1437.674	

Please note that because this analysis makes computations of ultimate moment capacity and pile response using nonlinear bending stiffness that the above values of total stress due to combined axial stress and bending may not be representative of actual conditions.

#### Output Verification:

Computed forces and moments are within specified convergence limits.

### Caisson Analysis.lpo

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.37301266 in
Computed slope at pile head	=	-0.00208645
Maximum bending moment	=	15484522. lbs-in
Maximum shear force	=	-87370.88607 lbs
Depth of maximum bending moment	=	60.42000000 in
Depth of maximum shear force	=	200.34000 in
Number of iterations	=	5
Number of zero deflection points	=	1

---

#### Summary of Pile Response(s)

---

Definition of Symbols for Pile-Head Loading Conditions:

Type 1 = Shear and Moment,	y = pile-head displacement in
Type 2 = Shear and Slope,	M = Pile-head Moment lbs-in
Type 3 = Shear and Rot. Stiffness,	V = Pile-head Shear Force lbs
Type 4 = Deflection and Moment,	S = Pile-head Slope, radians
Type 5 = Deflection and Slope,	R = Rot. Stiffness of Pile-head in-lbs/rad

Load Type	Pile-Head Condition 1	Pile-Head Condition 2	Axial Load lbs	Pile-Head Deflection in	Maximum Moment in-lbs	Maximum Shear lbs
1	V= 42000. M= 4.79E+07	44000.0000	2.0279	5.0121E+07	-306385.	
1	V= 13000. M= 1.48E+07	44000.0000	0.3730127	1.5485E+07	-87370.8861	

---

#### Computed Pile-head Stiffness Matrix Members K22, K23, K32, K33 for Superstructure

---

Top y in	Shear React. lbs	Mom. React. in-lbs	K22 lbs/in	K32 in-lbs/in
0.00410508	4200.00006	725989.75631	1023123.	1.768516E+08
0.01235752	12643.25982	2185447.	1023123.	1.768516E+08
0.01958620	20039.09270	3463851.	1023123.	1.768516E+08
0.02471503	25286.51964	4370894.	1023123.	1.768516E+08
0.02869327	29356.74018	5074451.	1023123.	1.768516E+08

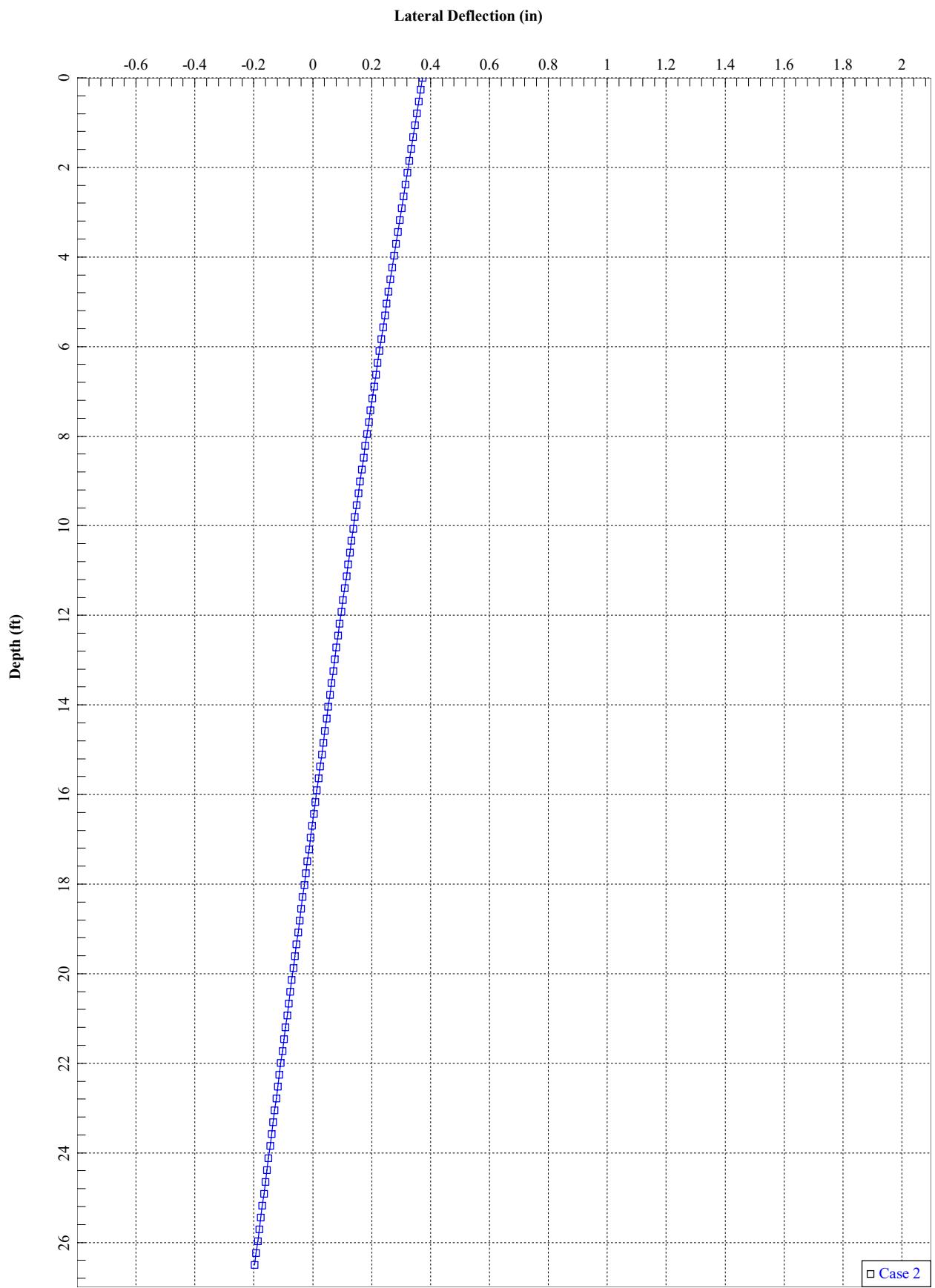
Caisson Analysis.lpo

0.03194372	32682.35252	5649298.	1023123.	1.768516E+08
0.03469286	35494.11768	6135280.	1023096.	1.768456E+08
0.03707551	37929.77945	6556194.	1023041.	1.768335E+08
0.03917790	40078.18540	6927426.	1022979.	1.768197E+08
0.04105904	42000.00000	7259476.	1022917.	1.768058E+08

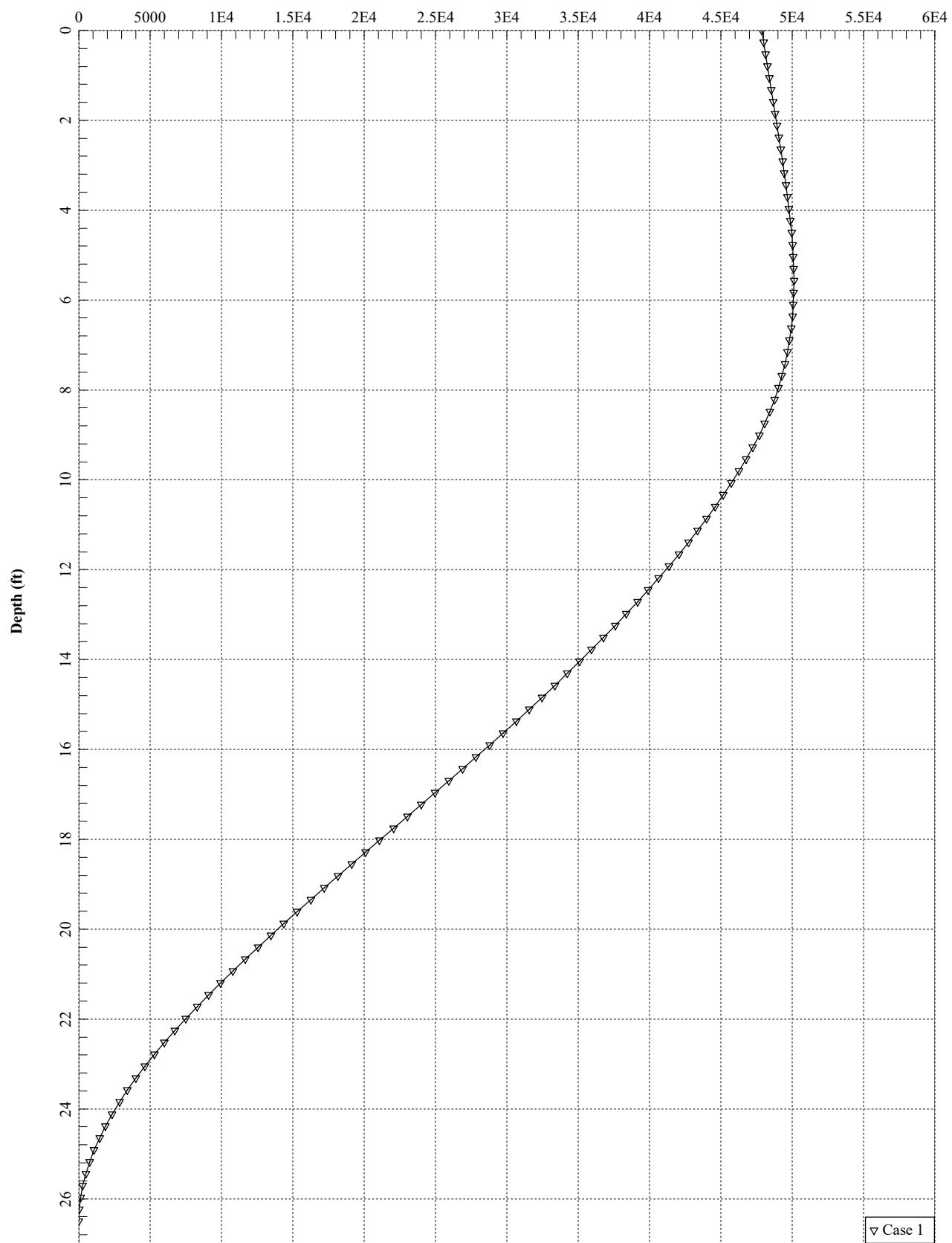
Top Rota. rad	Shear React. lbs	Mom. React. in-lbs	K23 lbs/rad	K33 in-lbs/rad
0.00012353	21846.36785	4786800.	1.768516E+08	3.875030E+10
0.00037278	65773.60589	14409704.	1.764398E+08	3.865450E+10
0.00059320	104270.04511	22838840.	1.757767E+08	3.850133E+10
0.00108054	133229.68904	28819408.	1.232992E+08	2.667131E+10
0.00140527	156978.75645	33458296.	1.117073E+08	2.380918E+10
0.00164047	176425.28223	37248544.	1.075454E+08	2.270599E+10
0.00183931	193108.26864	40453153.	1.049895E+08	2.199365E+10
0.00200008	207349.54639	43229111.	1.036707E+08	2.161370E+10
0.00214211	219970.05671	45677680.	1.026887E+08	2.132372E+10
0.00227051	231341.85862	47868000.	1.018899E+08	2.108250E+10

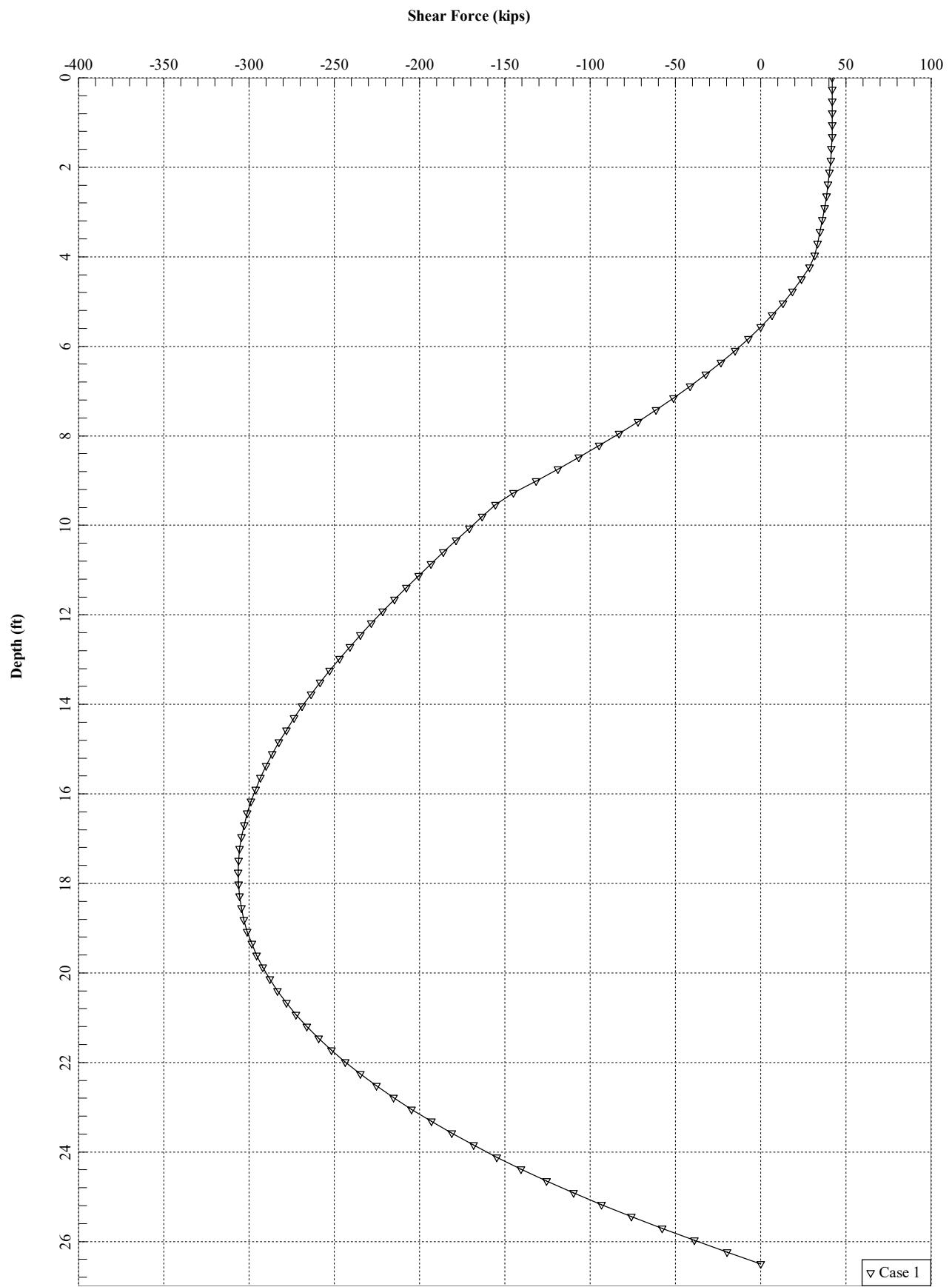
K22 = abs(Shear Reaction/Top y)  
 K23 = abs(Shear Reaction/Top Rotation)  
 K32 = abs(Moment Reaction/Top y)  
 K33 = abs(Moment Reaction/Top Rotation)

The analysis ended normally.



### Bending Moment (in-kips)







February 8, 2019

Angie Bruce  
SAI Communications, Inc.  
12 Industrial Way  
Salem, NH 03079  
(603) 952-8468

B+T Group  
1717 S. Boulder, Suite 300  
Tulsa, OK 74119  
(918) 587-4630  
btwo@btgrp.com

<b>Subject:</b>	<b>Appurtenance Mount Analysis Report</b>	
<b>Carrier Designation:</b>	<b>Site Number:</b>	CT2128
	<b>FA Number:</b>	10035251
	<b>Site Name:</b>	Fairfield Greenfield Hill
<b>Engineering Firm Designation:</b>	<b>B+T Group Project Number:</b>	130656.002.01
<b>Site Data:</b>	<b>3965 Congress Street, Fairfield, CT, 06824, Fairfield County</b> <b>Latitude 41.18838°, Longitude -73.29905°</b> <b>Monopole</b> <b>13' Platform Mount</b>	

Dear Angie Bruce,

*B+T Group* is pleased to submit this "**Appurtenance Mount Analysis Report**" to determine the structural integrity of the antenna mount on the above-mentioned structure.

The purpose of the analysis is to determine acceptability of the mount's stress level. Based on our analysis we have determined the stress level for the mount under the following load case to be:

**Existing + Proposed Equipment**  
Note: See Table 1 for the final loading configuration

**Sufficient Capacity**  
(Failing AS IS over 150%)  
(Passing at 58.2% with  
Recommendations in Section 5)

This analysis has been performed in accordance with the 2018 International Building Code based upon an ultimate 3-second gust wind speed of 118 mph. Exposure Category C and Risk Category II were used in this analysis.

All the equipment proposed in this report shall be installed in accordance with the drawings for the determined available structural capacity to be effective.

We at *B+T Group* appreciate the opportunity of providing our continuing professional services to you and *SAI Communications, Inc.* If you have any questions or need further assistance on this or any other projects, please give us a call.

Mount structural analysis prepared by: Siva Tellakula, E.I.T.

Respectfully submitted by: B&T Engineering, Inc.  
COA: PEC.0001564 Expires: 02/10/2020



Scott S. Vance, P.E.

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## 1) INTRODUCTION

The appurtenance mount consists of platform mount at 126ft., attached to monopole at 3965 Congress Street, Fairfield, CT, 06824, Fairfield County. The proposed antenna loading information was obtained from SAI Communications, Inc. All information provided to B+T Group was assumed accurate and complete.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this mount in accordance with the ANSI/TIA-222-H-2017 Structural Standard for Antenna Supporting Structures and Antennas and Small Wind Turbine Support Structures using a 3-second gust wind speed of 118 mph with no ice and 50 mph with 1inch escalated ice thickness Exposure Category C with topographic factor 1 and Risk Category II were used in this analysis. In addition, the platform mount has been analyzed for various live loading conditions consisting of a 250-lb man live load applied individually at the midpoint and cantilevered ends of horizontal members as well as a 250-pound man live load applied individually at mount pipe locations using a 3-second gust of 30mph. The mount was analyzed under 30° increments in the wind direction. The analyzed loading is detailed in Table 1.

**Table 1 – Proposed and Existing Equipment Information**

Loading	RAD Center Elev. (ft.)	Position	Qty.	Manufacturer	Model / Type	Note
Proposed	127	2	3	Kathrein	800-10965	1
			3	Ericsson	B5/B12 4449	2
			3	Ericsson	4415 B30	
		-	1	Raycap	DC6-48-60-18-8F	3
Existing	127	1	3	Powerwave	7770	4
			5	CCI	HPA-65R-BUU-H6	
		1	6	Powerwave	LGP 21401	
		-	3	Ericsson	RRUS-12+RRUS-A2	5
			1	Raycap	DC6-48-60-18-8F	

Note:

- (1) Proposed Antenna to be installed on the existing Mount Pipe.
- (2) Proposed Equipment to be installed side by side with RRUS Support, directly behind the Antenna
- (3) Proposed Equipment to be installed on the mount
- (4) Existing Equipment installed on the Mount.
- (5) Existing Equipment installed on the Tower

**Table 2 - Documents Provided**

Documents	Remarks	Reference	Source
RFDS	Existing Loading Proposed Loading	Date: 10/18/2018	SAI Communications, Inc.
Scoping Details	Existing Loading Proposed Loading	Date: 01/07/2019	SAI Communications, Inc.
Mount Mapping	B+T Group	Date: 12/12/2018	On File

## 3) ANALYSIS PROCEDURE

### 3.1) Analysis Method

RISA-3D (Version 17.0.2), a commercially available analysis software package, was used to create a three-dimensional model of the mount and calculate member stresses and deflections for various loading cases. Selected output from the analysis is included in Appendix A.

### 3.2) Assumptions

1. The mount was built in accordance with the manufacturer's specifications.
2. The mount has been maintained in accordance with the manufacturer's specifications and is free of damage.
3. The configuration of antennas and other appurtenances are as specified in Table 1.
4. All mount components have been assumed to be in sufficient condition to carry their full design capacity for the analysis.
5. Mount areas and weights are determined from field measurements, standard material properties, and/or manufacturer product data.
6. Serviceability with respect to antenna twist, tilt, roll or lateral translation is not checked and is left to the carrier or tower owner to ensure conformance.
7. All prior structural modifications, if any are assumed to be correctly installed and fully effective.
8. All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
9. The following material grades were assumed (Unless Noted Otherwise):
  - a) Connection Bolts : ASTM A325
  - b) Steel Pipe : ASTM A53 (GR. 35)
  - c) HSS (Round) : ASTM 500 (GR. B-42)
  - d) HSS (Rectangular) : ASTM 500 (GR. B-46)
  - e) Channel : ASTM A36 (GR. 36)
  - f) Steel Solid Rod : ASTM A36 (GR. 36)
  - g) Steel Plate : ASTM A36 (GR. 36)
  - h) Steel Angle : ASTM A36 (GR. 36)
  - i) UNISTRUT : ASTM A570 (GR. 33)

This analysis may be affected if any assumptions are not valid or have been made in error. B+T Group should be notified to determine the effect on the structural integrity of the antenna mounting system.

## 4) ANALYSIS RESULTS

**Table 3 (a)– (AS IS) Mount Component Stresses vs. Capacity**

Notes	Component	Elevation (ft.)	% Capacity*	Pass / Fail
-	Main Horizontals	126	Over 150	Fail
-	Supporting Tubes	126	35.1	Pass
-	Supporting Angles	126	99.0	Pass
-	Connection Angles	126	36.3	Pass
-	Mount Pipes	126	82.1	Pass

**Table 3 (b)– Mount Component Stresses vs. Capacity**

Notes	Component	Elevation (ft.)	% Capacity*	Pass / Fail
-	Main Horizontals	126	42.4	Pass
-	Supporting Tubes	126	35.1	Pass
-	Supporting Angles	126	23.8	Pass
-	Connection Angles	126	10.7	Pass
-	Mount Pipes	126	58.2	Pass
Proposed	Additional Site Pro Handrail Kit (HRK12)	126	34.8	Pass

Note: \*Member Capacity based on Recommended Modification on Section 5

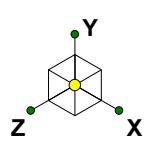
## **5) RECOMMENDATIONS**

The mount will have sufficient capacity to carry the existing and proposed loads and be in compliance with the ANSI/TIA-222-H Standard for the proposed and existing loading, with the modifications described below. (Refer to the RISA output for the specific members).

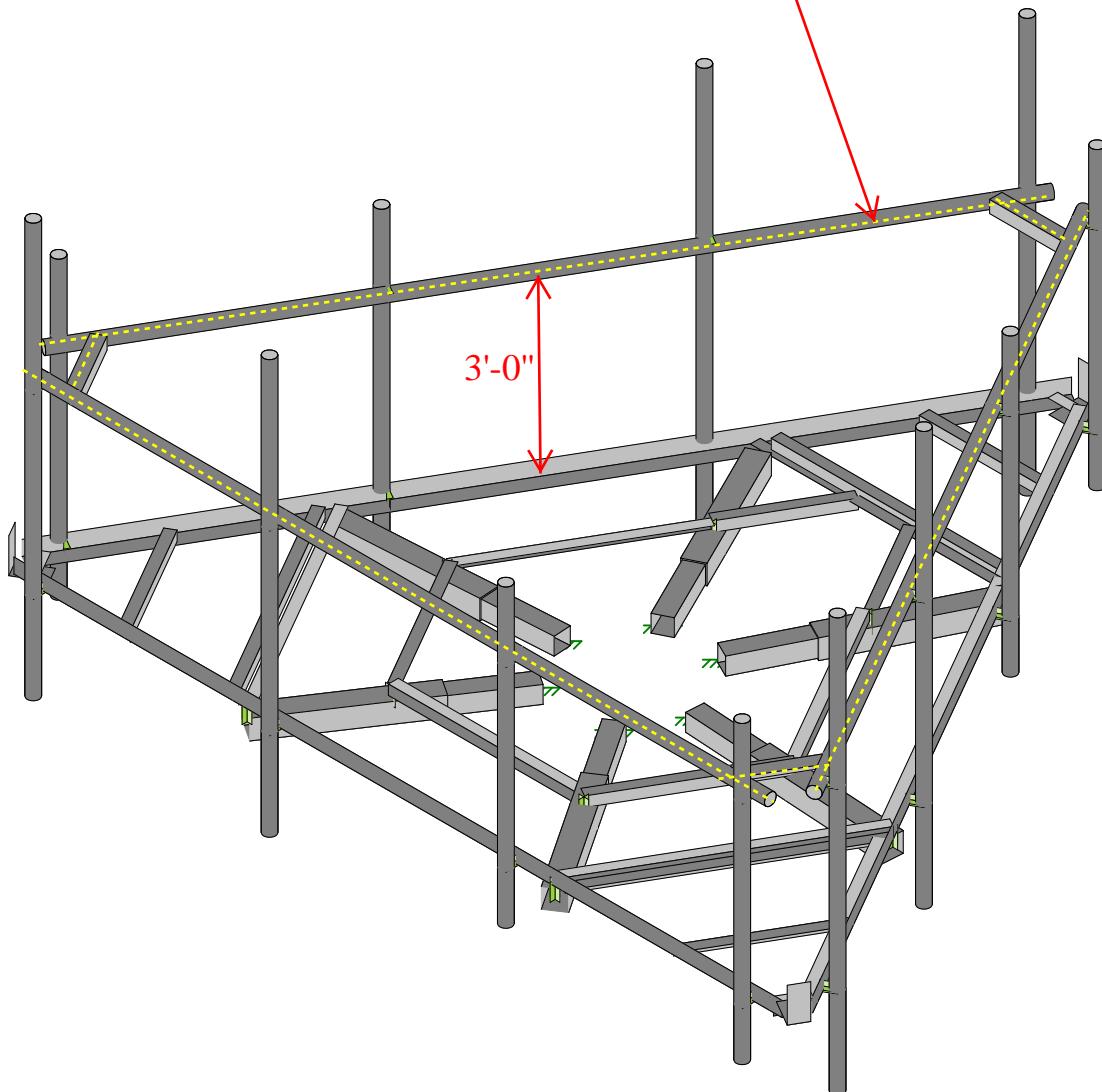
**Install (1) Site Pro handrail kit (HRK12), 3ft. above the main horizontals as shown in SK-1 of APPENDIX A**

## **APPENDIX A**

(RISA-3D Output)



NEW HANDRAIL KIT  
SITEPRO #HRK-12



Envelope Only Solution

B+T Group

SP

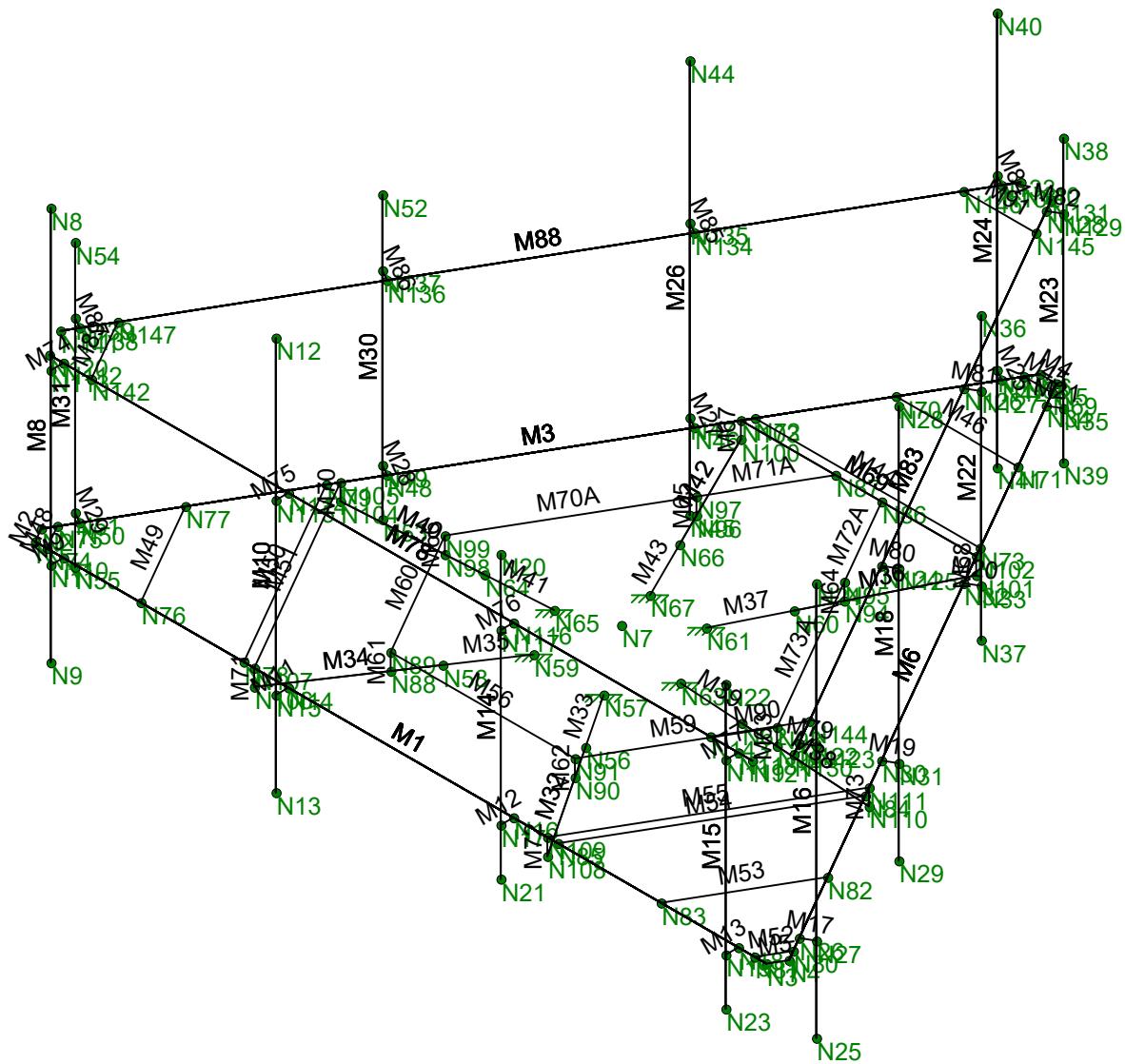
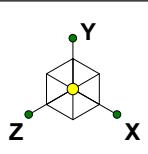
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CT2128 - Fairfield Greenfield Hill

SK - 1

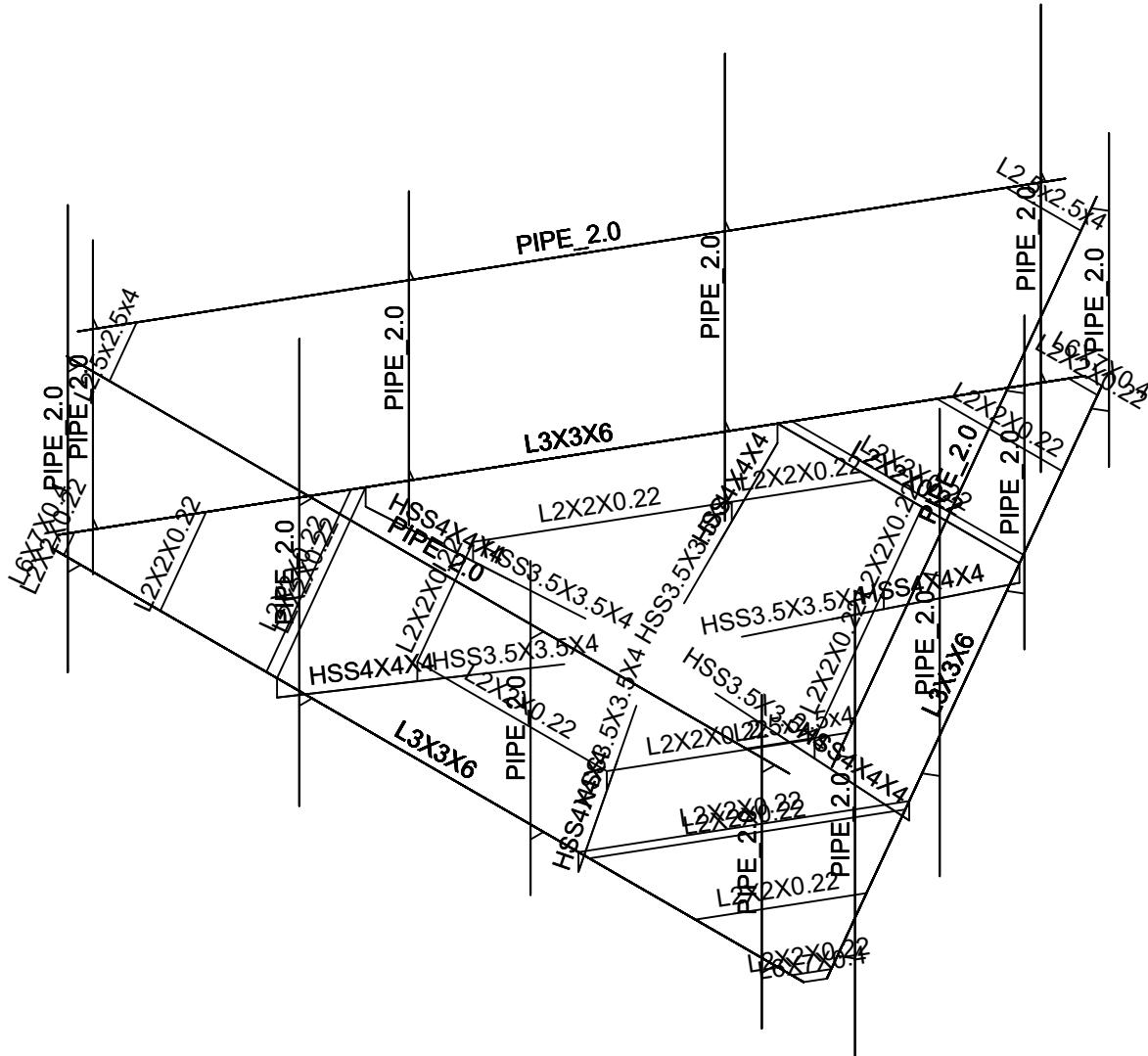
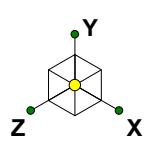
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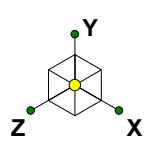
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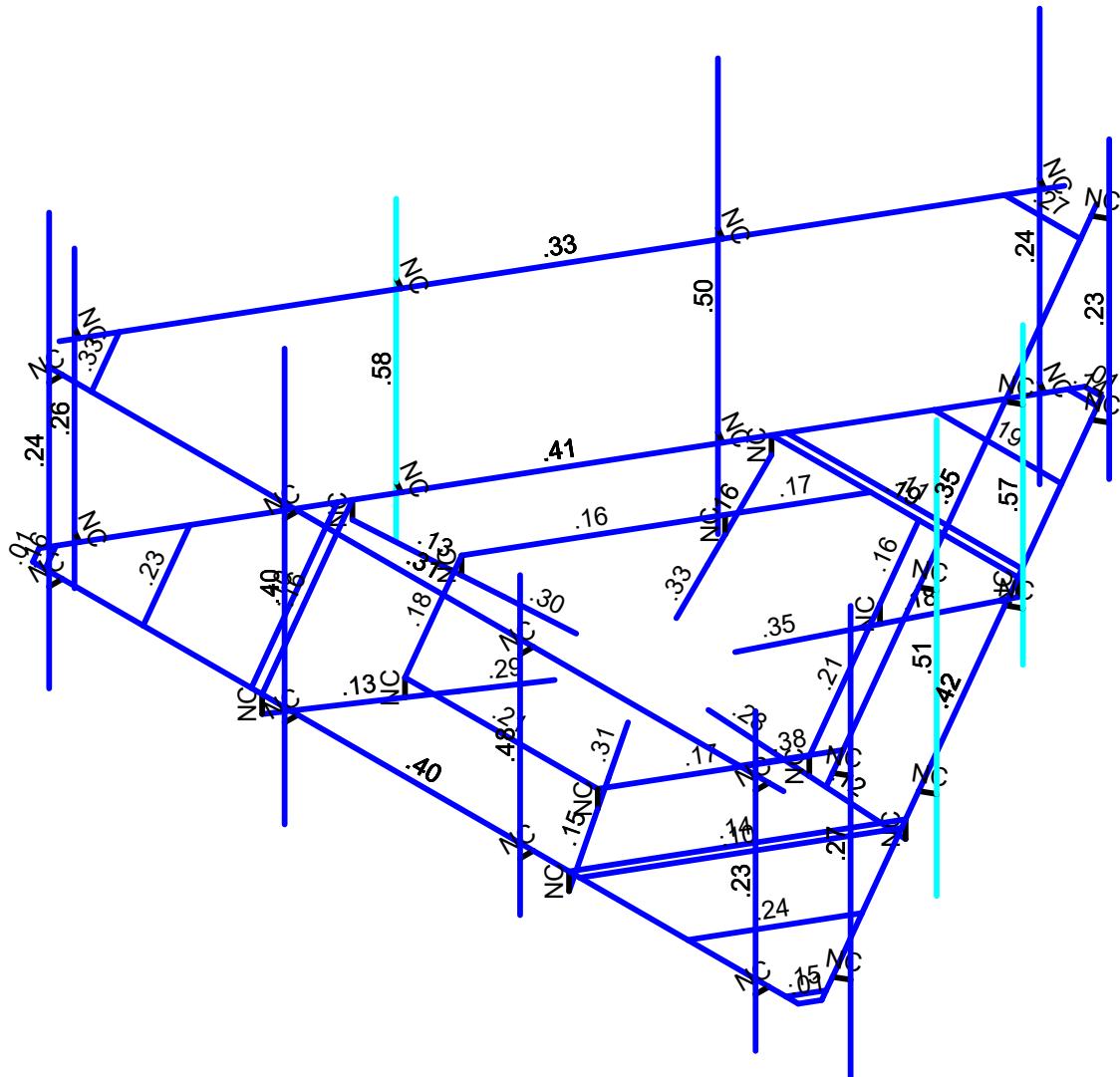


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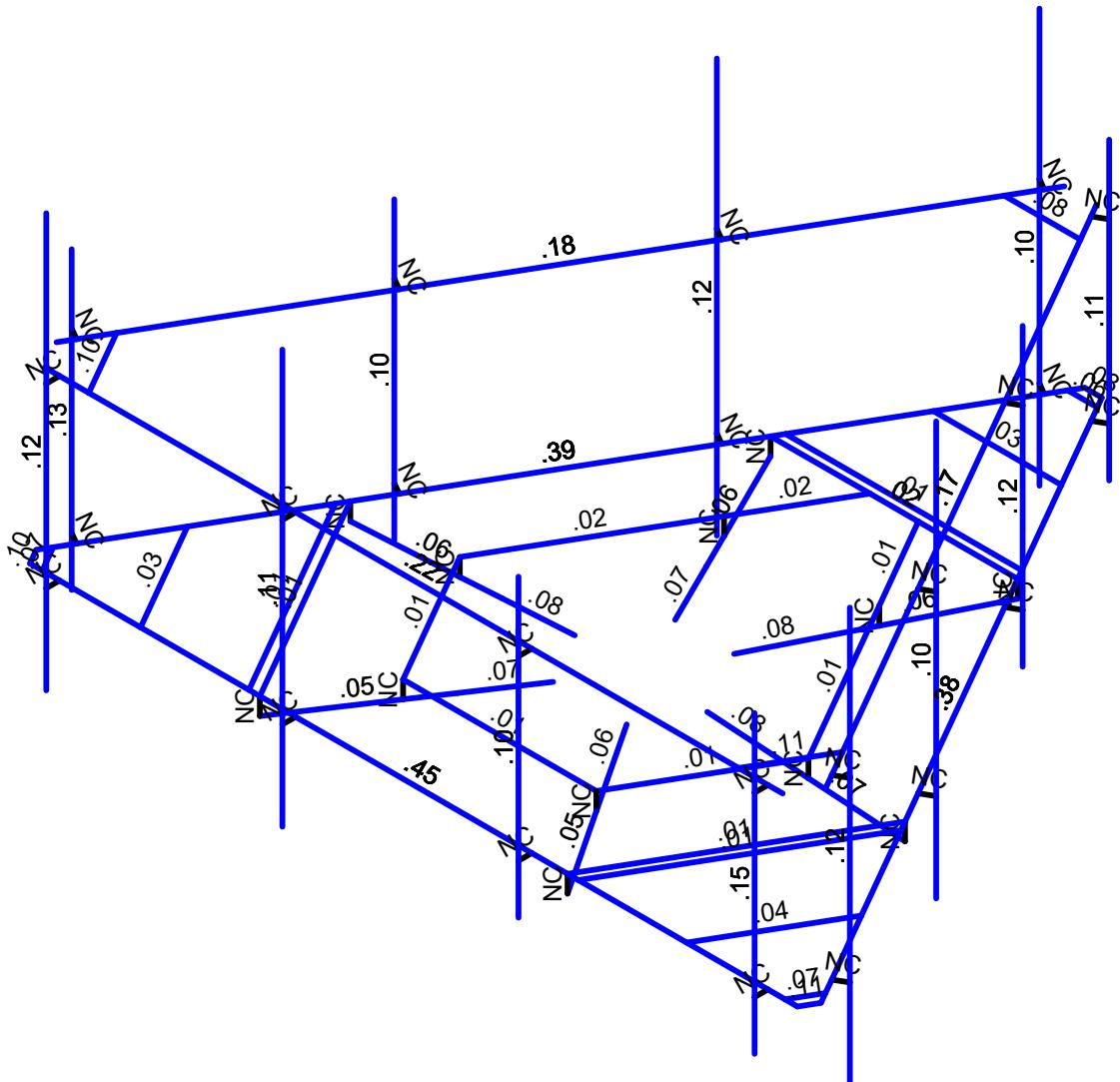
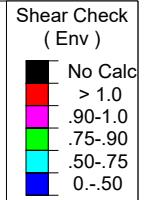
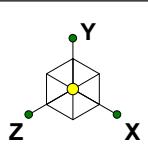


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IH	PJH	EEGJH	EE	HJGFFHG	€
II	PJI	EEJF	EE	EIIEH	€
II	PJI	EEJF	EE	HJGFFHG	€
II	PJI	EEUJF	EE	EEUJH	€
II	PJI	EEUJF	EE	EEUJH	€
II	PJI	EEHIGG	EFGF	GEIH	€
IJ	PJL	EEHIGG	EFGF	GEIH	€
J€	PJ€	FEGHIGG	EFGF	GEIH	€

>cJbh7ccfXjbUhYgUbXHYa dYfUi fYg fTcbhbi YXŁ

>cJbh7ccfXjbUhYgUbXHYa dYfUi fYg fVcbhjbi YXŁ

Še&vacute;	Ý&zacute;a	Ý&zacute;a	Z&á&zacute;a	V&gt;&gt; Á&zacute;a	Ö&gt;&gt; cas&gt;&gt; Ö&gt;&gt; ä&gt;&gt;
F I H	þF I H	í ē e F i ï	H	H ð G F F H G	€
F I I	þF I I	í ē i i i i H	H	G ð e F i G	€
F I Í	þF I Í	é ð e i H ð F	H	H ð G H F I	€
F I Ï	þF I Ï	é ð e i H ð F	H	H ð G H F I	€
F I ï	þF I ï	é ð e i i i i H	H	G ð e F i G	€

## A Ya VYf'DfJa Ufm8 Uh

Sākums	DR āc	RĀ āc	SĀ āc	Ū āc Ā āc * D Ā āc * I āc	V āc	Ō āc Ā āc	T āc Ā āc	Ō āc Ā āc
F	TF	PF	PH		Ģ ē	T ØEPF	Ó āf	Ū ā * Ā āf * ā
G	TG	PF	P G			ØFEÖAF	Ó āf	Ū ā * Ā āf * ā
H	TH	PF	P ī			T ØEPF	Ó āf	Ū ā * Ā āf * ā
I	TI	P ī	P ī			ØFEÖAF	Ó āf	Ū ā * Ā āf * ā
Í	TÍ	P I	P H			ØFEÖAF	Ó āf	Ū ā * Ā āf * ā
Ī	TÍ	P I	P ī	Ģ ē	T ØEPF	Ó āf	Ū ā * Ā āf * ā	OH ÄO: Eī
Ī	TÍ	P ī	P J		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
Ī	TJ	P F ē	P FF			ÜWÖÖ	P [ } ā	ÜWÖÖ
J	TF ē	P FG	P FH		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
FĒ	TF F	P F	P F ī			ÜWÖÖ	P [ } ā	ÜWÖÖ
FF	TF G	P F ī	P F ī			ÜWÖÖ	P [ } ā	ÜWÖÖ
FG	TF H	P F ī	P F J			ÜWÖÖ	P [ } ā	ÜWÖÖ
FH	TF I	P G ē	P GF		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
FI	TF Í	P GG	P GH		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
FÍ	TF ī	P G	P G		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
FÎ	TF ī	P G	P G			ÜWÖÖ	P [ } ā	ÜWÖÖ
FÎ	TF ī	P G	P GI		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
FÎ	TF J	P H ē	P HF			ÜWÖÖ	P [ } ā	ÜWÖÖ
FJ	TG ē	P HG	P HH			ÜWÖÖ	P [ } ā	ÜWÖÖ
GĒ	TGF	P H	P H			ÜWÖÖ	P [ } ā	ÜWÖÖ
GF	TGG	P H ī	P H ī		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
GG	TGH	P H ī	P H J		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
GH	TG	P I ē	P IF		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
G	TG	P IG	P IH			ÜWÖÖ	P [ } ā	ÜWÖÖ
G	TG	P II	P II		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
G	TG	P II	P II			ÜWÖÖ	P [ } ā	ÜWÖÖ
G	TG	P II	P IJ			ÜWÖÖ	P [ } ā	ÜWÖÖ
G	TG	P I ē	P IF			ÜWÖÖ	P [ } ā	ÜWÖÖ
GI	TH ē	P I G	P IH		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
HĒ	TH F	P II	P II		T ØEFU	Ó[ ī ī { }	Ū ā ā	OE HÄO: Eō
HF	TH G	P F ē	P II			ØFEÜVF	Ó āf	V ā ā
HG	TH H	P II	P II			ØFEÜVG	Ó āf	V ā ā
HH	TH	P F ē	P II			ØFEÜVF	Ó āf	V ā ā
H	TH	P II	P IJ			ØFEÜVG	Ó āf	V ā ā
H	TH	P F ē F	P I ē			ØFEÜVF	Ó āf	V ā ā
H	TH	P I ē	P F ī			ØFEÜVG	Ó āf	V ā ā
H	TH	P F F ē	P I G			ØFEÜVF	Ó āf	V ā ā
H	TH	P I G	P IH			ØFEÜVG	Ó āf	V ā ā
HJ	TI ē	P F ē I	P II			ØFEÜVF	Ó āf	V ā ā
I ē	TIF	P II	P II			ØFEÜVG	Ó āf	V ā ā
IF	TIG	P F F ē	P II			ØFEÜVF	Ó āf	V ā ā
IG	TIH	P II	P II			ØFEÜVG	Ó āf	V ā ā

*A Ya VYf'DfJa Ufm8 UUfV cbHbi YXŁ*

S&eacute;	C&acute;	R&acute;	S&acute;	U&gt;C&gt;D	U&gt;C&gt;E	V]&	Ö&gt;A&gt;C	T&gt;A&gt;C	Ö&gt;A&gt;C
I H	T I I	P I G	P I H	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P I I	P I J	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P I I	P I F	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P I I	P I I	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I J	P I I	P I I	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P I I	P I J	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I J	T I F	P F E I	P F E I	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I €	T I G	P I €	P I F	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I F	T I H	P I G	P I H	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I G	T I I	P I I	P I I	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I H	T I I	P F F F	P F E U	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P J F	P I J	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I J	P J F	P J H	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I €	P J J	P I J	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I F	P I I	P I J			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I G	P J €	P J F			Ü W W	P [ ] &	P [ ] &	Ü W W
I J	T I H	P J G	P J H			Ü W W	P [ ] &	P [ ] &	Ü W W
I €	T I I	P J I	P J I			Ü W W	P [ ] &	P [ ] &	Ü W W
I F	T I I	P J I	P J I			Ü W W	P [ ] &	P [ ] &	Ü W W
I G	T I I	P J I	P J J			Ü W W	P [ ] &	P [ ] &	Ü W W
I H	T I I	P F E E	P F E H			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F E F	P F E G			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I J	P F E G	P F E H	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I €	P F E I	P F E I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I F	P F E I	P F E I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I G	P F E I	P F E U			Ü W W	P [ ] &	P [ ] &	Ü W W
I J	T I H	P F F €	P F F F			Ü W W	P [ ] &	P [ ] &	Ü W W
I €	T I € O E	P J J	P J I	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I F	T I F O E	P J I	P I I	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I G	T I G O E	P I I	P J I	F I E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I H	T I H O E	P J I	P J H	J E	Ö F E U O E	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P F F G	P F F H			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F F I	P F F I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F F I	P F F I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F F I	P F F J			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F G €	P F G F		P Ö Y Ä Ö Ö P Ö Ü	Ö A &gt;	Ü ä &	Ö H Ä Ö I E	V > A &gt; C
I J	T I J	P F G G	P F G H			Ü W W	P [ ] &	P [ ] &	Ü W W
I €	T I €	P F G I	P F G I			Ü W W	P [ ] &	P [ ] &	Ü W W
I F	T I F	P F G I	P F G I			Ü W W	P [ ] &	P [ ] &	Ü W W
I G	T I G	P F G I	P F G J			Ü W W	P [ ] &	P [ ] &	Ü W W
I H	T I H	P F H €	P F H F		P Ö Y Ä Ö Ö P Ö Ü	Ö A &gt;	Ü ä &	Ö H Ä Ö I E	V > A &gt; C
I I	T I I	P F H G	P F H H			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F H I	P F H I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F H I	P F H I			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F H I	P F H J			Ü W W	P [ ] &	P [ ] &	Ü W W
I I	T I I	P F H €	P F H F		P Ö Y Ä Ö Ö P Ö Ü	Ö A &gt;	Ü ä &	Ö H Ä Ö I E	V > A &gt; C
I J	T I J	P F G	P F I I	F I E	Ö P Ö U	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
J €	T J €	P F I I	P F H	F I E	Ö P Ö U	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C
J F	T J F	P F I I	P F I I	F I E	Ö P Ö U	Ö A &gt;	Ü ä *   &gt; Ö E *   &	Ö H Ä Ö I E	V > A &gt; C

6 UgW@ UX'7 UgYg

ÓŠÓÁÖ·&í	Óæ·* ·	ÝÁÖ æ·	ÝÁÖ æ·	ZÓÖ æ·	R á c	Ú[á]c	Öädä·çåCE^æ·	ÜÜ æ·çü
F	Ö^æ·	ÖŠ		Ë			Í€	
G	€ÁY ä åÄÖP  ÁÖ·	Y SZ					Í€	ÍÍ
H	JÉÁY ä åÄÖP  ÁÖ·	Y SÝ					Í€	ÍÍ
I	ÉÁY ä åÄÖP	Y SZ					Í€	ÍÍ
Í	JÉÁY ä åÄÖP	Y SÝ					Í€	ÍÍ
Î	ÉÁY ä åÄÖP íçä·	Y SZ					Í€	ÍÍ
Ï	JÉÁY ä åÄÖP íçä·	Y SÝ					Í€	ÍÍ
	Q^	UŠF					Í€	ÍÍ
J	Šä^ÄSI æ Åe	ŠŠ			H			
F€	Šä^ÄSI æ Å	ŠŠ			H			
FF	Šä^ÄSI æ Å&	ŠŠ			H			
FG	Šä^ÄSI æ Å·	ŠŠ			H			
FH	T æ öSSÄF	ŠŠ					F	
FI	T æ öSSÄG	ŠŠ					F	
FÍ	T æ öSSÄH	ŠŠ					F	
FÎ	T æ öSSÄ	ŠŠ					F	
FÎ	T æ öSSÄ	ŠŠ					F	
FÍ	T æ öSSÄ	ŠŠ					F	
FJ	T æ öSSÄ	ŠŠ					F	
G€	T æ öSSÄ	ŠŠ					F	
GF	T æ öSSÄ	ŠŠ					F	
GG	T æ öSSÄF€	ŠŠ					F	
GH	T æ öSSÄFF	ŠŠ					F	
G	T æ öSSÄFG	ŠŠ					F	
Í	T æ öSSÄFH	ŠŠ						
Î	T æ öSSÄFI	ŠŠ						
Ï	T æ öSSÄFI	ŠŠ						
G	ÓŠÓÁFÁ!æ·&í) ãOE^æ·	þ[·] ^					F€	
GJ	ÓŠÓÁFÁ!æ·&í) ãOE^æ·	þ[·] ^					F€	

@UX7ca VjbUhcbg

@UX7ca VjbUhjcbg'fTc b h jbi YXŁ

@UX7ca VjbUhcbg fTc bHbi YXŁ

A Ya VYf'DcJbh@UXg'f6 @% 8 YUXŁ

	T ^ { à ^ { Á } á ^ { Á } }	Ö á ^ { & ö }	T æ } ã á ^ { Ä } ß É cá	Š & ž } Ž Ě Á
F	T FÍ	Ý	EEFÍ	ÁÍ
G	T FÍ	Ŷ	EEFÍ	ÁJÍ
H	T FÍ	Ÿ	EEG	ÁÍÍ
I	T FÍ	Ÿ	€	€
Í	T FÍ	Ÿ	€	€
Í	T FI	Ý	EEI	ÁÍ
Í	T FI	Ŷ	EEI	ÁJÍ
Í	T FI	Ÿ	EEH	ÁÍ€
J	T FI	Ÿ	EEI	ÁÍ€
F€	T FI	Ý	€	€
FF	T Í	Ŷ	EEG	ÁHE
FG	T Í	Ÿ	EEG	ÁÍÍ
FH	T Í	Ÿ	€	€
FI	T Í	Ÿ	€	€
FÍ	T Í	Ý	€	€
FÍ	T HÍ	Ý	EEH	ÁÍ€
FÍ	T HÍ	Ŷ	€	€
FÍ	T HÍ	Ÿ	€	€
FJ	T HÍ	Ý	€	€
G€	T HÍ	Ŷ	€	€
GF	T HF	Ý	EEFÍ	ÁÍ
GG	T HF	Ŷ	EEFÍ	ÁJÍ
GH	T HF	Ÿ	EEG	ÁÍÍ
G	T HF	Ÿ	€	€
G	T HF	Ŷ	€	€
G	T HE	Ý	EEI	ÁÍ
G	T HE	Ŷ	EEI	ÁJÍ
G	T HE	Ÿ	EEH	ÁÍ€

A Ya VYf'DcJbh@UXg'f6 @%.'8 YUXLfVcbh]bi YXŁ

GJ	T <sup>À</sup> T <sup>È</sup> T <sup>Í</sup>	Ö T <sup>Å</sup> T <sup>Å</sup>	T <sup>Æ</sup> T <sup>Ø</sup> T <sup>Å</sup> T <sup>É</sup> T <sup>Á</sup>	Š T <sup>Å</sup> T <sup>É</sup> T <sup>Å</sup>
H€	T H€	Ÿ	€	ÃÍ €
HF	T G	Ÿ	EG	Ã H€
HG	T G	Ÿ	EG	Ã ÍÍ
HH	T G	Ÿ	€	€
HI	T G	Ÿ	€	€
HÍ	T G	Ÿ	€	€
HÍ	T GH	Ÿ	EFG	ÃÍ
HÍ	T GH	Ÿ	EFG	Ã JÍ
HÍ	T GH	Ÿ	EG	Ã ÍÍ
HJ	T GH	Ÿ	€	€
I €	T GH	Ÿ	€	€
I F	T GG	Ÿ	EÍ	ÃÍ
I G	T GG	Ÿ	EÍ	Ã JÍ
I H	T GG	Ÿ	E H	ÃÍ €
I I	T GG	Ÿ	EÍ	ÃÍ €
I Í	T GG	Ÿ	€	€
I Í	T FÍ	Ÿ	EG	Ã H€
I Í	T FÍ	Ÿ	EG	Ã ÍÍ
I Í	T FÍ	Ÿ	€	€
I J	T FÍ	Ÿ	€	€
I €	T FÍ	Ÿ	€	€

A Ya VYf Dc Jbh@ UXg f6 @& \$K JbX! Bc ƎWŁ

T ^ { à ^ { Á } }	T ð ^ { ð }	T ð ^ { ð }	T æ ^ { ð }	š ^ { & eacute; }
F	T FÍ	Z	ÜFG	ÁÍ
G	T FÍ	Z	ÜFG	ÁJÍ
H	T FÍ	Z	ÜHF	ÁÍÍ
I	T FÍ	Z	€	€
Í	T FÍ	Z	€	€
Î	T FI	Z	ÜFG	ÁÍ
Ï	T FI	Z	ÜFG	ÁJÍ
Ì	T FI	Z	ÜJ	ÁÍ€
J	T FI	Z	ÜH	ÁÍ€
F€	T FI	Z	€	€
FF	T Ì	Z	ÜGFI	ÁHE
FG	T Ì	Z	ÜGFI	ÁÍÍ
FH	T Ì	Z	€	€
FI	T Ì	Z	€	€
FÍ	T Ì	Z	€	€
FÍ	T HÍ	Z	ÜÍ	ÁÍ€
FÍ	T HÍ	Z	€	€
FÍ	T HÍ	Z	€	€
FJ	T HÍ	Z	€	€
GE	T HÍ	Z	€	€
GF	T HF	Z	ÜG	ÁÍ
GG	T HF	Z	ÜG	ÁJÍ
GH	T HF	Z	ÜHF	ÁÍÍ
G	T HF	Z	€	€
Ğ	T HF	Z	€	€
Ğ	T HE	Z	ÜFG	ÁÍ

A Ya VYf'DcJbh@UXg'f6 @' & \$ K JbX!'Bc =WŁfV cbhjbi YXŁ

T <sup>h</sup>	á	é	ö	ü	ö	ü
G	T H E	Z	Ü FG	Ä JÍ		
G	T H E	Z	Ü É J	Ä Í È		
GJ	T H E	Z	Ü Ü H	Ä Í È		
H E	T H E	Z	Ü Ü	Ä È		
H F	T G	Z	Ü FG	Ä H È		
H G	T G	Z	Ü FG	Ä Í Í		
H H	T G	Z	Ü Ü	Ä È		
H I	T G	Z	Ü Ü	Ä È		
H Í	T G	Z	Ü Ü	Ä È		
H Ï	T GH	Z	Ü FG	Ä Í		
H Ï	T GH	Z	Ü FG	Ä JÍ		
H Ï	T GH	Z	Ü Ü F	Ä Í Í		
H Ï	T GH	Z	Ü Ü	Ä È		
I €	T GH	Z	Ü Ü	Ä È		
I F	T GG	Z	Ü FG	Ä Í		
I G	T GG	Z	Ü FG	Ä JÍ		
I H	T GG	Z	Ü É J	Ä Í È		
I I	T GG	Z	Ü Ü H	Ä Í È		
I Í	T GG	Z	Ü Ü	Ä È		
I Ï	T F Ï	Z	Ü FG	Ä H È		
I Ï	T F Ï	Z	Ü FG	Ä Í Í		
I Ï	T F Ï	Z	Ü Ü	Ä È		
I J	T F Ï	Z	Ü Ü	Ä È		
I €	T F Ï	Z	Ü Ü	Ä È		

A Ya VYf'DcJbh@UXg'f6 @" :- \$'K JbX!'Bc 'WYz

	T <sup>À</sup> Í	ÖÅÍ	TÆÍ	ŠÍ
F	T FÍ	Ý	ÅÍ	ÁÍ
G	T FÍ	Ý	ÅÍ	ÁJÍ
H	T FÍ	Ý	ÅÍ	ÁÍÍ
I	T FÍ	Ý	€	€
Í	T FÍ	Ý	€	€
Î	T FI	Ý	ÅHG	ÁÍ
Ï	T FI	Ý	ÅHG	ÁJÍ
Ì	T FI	Ý	ÅÍ	ÁÍ€
J	T FI	Ý	ÅÍ	ÁÍ€
F€	T FI	Ý	€	€
FF	T Í	Ý	ÅÍ	ÁHE
FG	T Í	Ý	ÅÍ	ÁÍÍ
FH	T Í	Ý	€	€
FI	T Í	Ý	€	€
FÍ	T Í	Ý	€	€
FÍ	THÍ	Ý	ÅÍ	ÁÍ€
FÍ	THÍ	Ý	€	€
FÍ	THÍ	Ý	€	€
FJ	THÍ	Ý	€	€
G€	THÍ	Ý	€	€
GF	THF	Ý	ÅÍ	ÁÍ
GG	THF	Ý	ÅÍ	ÁJÍ
GH	THF	Ý	ÅÍ	ÁÍÍ
G	THF	Ý	€	€

A Ya VYf Dc Jbh@UXg f6 @ " :- \$ K JbX ! Bc =WYf7 cbhjbi YXŁ

T <sup>À</sup>	T <sup>À</sup>	Ó	T <sup>Æ</sup>	Š
G	THF	Ý	€	€
G	THE	Ý	ÞFHG	ÃÍ
G	THE	Ý	ÞFHG	ÃJÍ
G	THE	Ý	ÞFI	ÃÍ€
GJ	THE	Ý	ÞFI	ÃÍ€
H€	THE	Ý	€	€
HF	TG	Ý	ÞFI	ÃHE
HG	TG	Ý	ÞFI	ÃII
HH	TG	Ý	€	€
H	TG	Ý	€	€
H	TG	Ý	€	€
H	TGH	Ý	ÞFI	ÃÍ
H	TGH	Ý	ÞFI	ÃJÍ
H	TGH	Ý	ÞF	ÃII
HJ	TGH	Ý	€	€
I€	TGH	Ý	€	€
IF	TGG	Ý	ÞFHG	ÃÍ
IG	TGG	Ý	ÞFHG	ÃJÍ
IH	TGG	Ý	ÞFI	ÃÍ€
II	TGG	Ý	ÞFI	ÃÍ€
II	TGG	Ý	€	€
II	TFI	Ý	ÞFI	ÃHE
II	TFI	Ý	ÞFI	ÃII
II	TFI	Ý	€	€
IJ	TFI	Ý	€	€
I€	TFI	Ý	€	€

A Ya VYf'DcJbh@UXg'f6 @ ( : \$ K JbX! -WYt

	T ^ { à ^ { Á } è ^ { Ă } }	Ö å ^ { & ö }	T æ ) ã ^ { á } ũ ^ { ā } ă ^ { Ě }	Ş ş ^ { & ş }
F	T FÍ	Z	EEGG	ÁÍ
G	T FÍ	Z	EEGG	ÁJÍ
H	T FÍ	Z	EEG	ÁÍÍ
I	T FÍ	Z	€	€
Í	T FÍ	Z	€	€
Î	T FI	Z	EEÍ	ÁÍ
Ï	T FI	Z	EEÍ	ÁJÍ
Ì	T FI	Z	EEFF	ÁÍ€
J	T FI	Z	EEâ	ÁÍ€
F€	T FI	Z	€	€
FF	T Ì	Z	EEH	ÁHE
FG	T Ì	Z	EEH	ÁÍÍ
FH	T Ì	Z	€	€
FI	T Ì	Z	€	€
FÍ	T Ì	Z	€	€
FÎ	THÍ	Z	EEF	ÁÍ€
FÏ	THÍ	Z	€	€
FÌ	THÍ	Z	€	€
FJ	THÍ	Z	€	€
G€	THÍ	Z	€	€
GF	THF	Z	EEGG	ÁÍ
GG	THF	Z	EEGG	ÁJÍ

A Ya VYf'DcJbh@UXg'f6 @' ( . '\$K JbX! =WYŁf7 c bHjbi YXŁ

	T <sup>æ</sup> { à^{ } Áéé^{ }}	Öä^{ } &ç{	T æ } Á { à^{ } Áéé^{ }	Š { &š{ } Žééá
GH	T HF	Z	HEÉ	ÁÍ
G	T HF	Z	€	€
Ğ	T HF	Z	€	€
Ğ	T HE	Z	HEÍ	ÁÍ
Ğ	T HE	Z	HEÍ	ÁJÍ
Ğ	T HE	Z	HEFF	ÁÍ€
GJ	T HE	Z	HEÉ	ÁÍ€
H€	T HE	Z	€	€
HF	T G	Z	HEH	ÁHE
HG	T G	Z	HEH	ÁÍÍ
HH	T G	Z	€	€
HI	T G	Z	€	€
HÍ	T G	Z	€	€
HÍ	T GH	Z	HEGG	ÁÍ
HÍ	T GH	Z	HEGG	ÁJÍ
HÍ	T GH	Z	HEÉ	ÁÍÍ
HJ	T GH	Z	€	€
I €	T GH	Z	€	€
I F	T GG	Z	HEÍ	ÁÍ
I G	T GG	Z	HEÍ	ÁJÍ
I H	T GG	Z	HEFF	ÁÍ€
II	T GG	Z	HEÉ	ÁÍ€
ÍÍ	T GG	Z	€	€
ÍÍ	T FÍ	Z	HEÍ	ÁHE
ÍÍ	T FÍ	Z	HEÍ	ÁÍÍ
ÍÍ	T FÍ	Z	€	€
I J	T FÍ	Z	€	€
Í €	T FÍ	Z	€	€

A Ya VYf'DcJbh@UXg'ff @' ) :- \$K JbX! -WYt

A Ya VYf Dc Jbh@ UXg f6 @ ) :- \$'K JbX ! =WŁfV c bhjbi YXŁ

T <sup>æ</sup>	à^ áéí	Öä^&çí	T æ	á ã ž ē é á	š & ž   ž á
G F	T HF	Ý	HEFG	ÁÍ	
G G	T HF	Ý	HEFG	Á JÍ	
G H	T HF	Ý	HEFI	Á ÍÍ	
G	T HF	Ý	€	€	
Ğ	T HF	Ý	€	€	
Ğ	T HE	Ý	HEG	ÁÍ	
Ğ	T HE	Ý	HEG	Á JÍ	
Ğ	T HE	Ý	HEFH	ÁÍ€	
G J	T HE	Ý	HEFI	ÁÍ€	
H €	T HE	Ý	€	€	
H F	T G	Ý	HEG	Á H€	
H G	T G	Ý	HEG	Á ÍÍ	
H H	T G	Ý	€	€	
H I	T G	Ý	€	€	
H Í	T G	Ý	€	€	
H İ	T GH	Ý	HEFG	ÁÍ	
H İ	T GH	Ý	HEFG	Á JÍ	
H İ	T GH	Ý	HEFI	Á ÍÍ	
H J	T GH	Ý	€	€	
I €	T GH	Ý	€	€	
I F	T GG	Ý	HEG	ÁÍ	
I G	T GG	Ý	HEG	Á JÍ	
I H	T GG	Ý	HEFH	ÁÍ€	
I I	T GG	Ý	HEFI	ÁÍ€	
I Í	T GG	Ý	€	€	
I İ	T FÍ	Ý	HEG	Á H€	
I İ	T FÍ	Ý	HEG	Á ÍÍ	
I İ	T FÍ	Ý	€	€	
I J	T FÍ	Ý	€	€	
I €	T FÍ	Ý	€	€	

A Ya VYf'DcJbh@UXg'f6 @\* : \$KJbX!GYfj JWŁ

	T <sup>À</sup> T <sup>Á</sup> T <sup>Ã</sup>	Ö T <sup>Å</sup> T <sup>Å</sup>	T <sup>Æ</sup> T <sup>Ø</sup> T <sup>Å</sup> T <sup>Ë</sup>	Š T <sup>Œ</sup> T <sup>Œ</sup> T <sup>Œ</sup>
F	T FÍ	Z	HEE	ÁÍ
G	T FÍ	Z	HEE	ÁJÍ
H	T FÍ	Z	HEEG	ÁÍÍ
I	T FÍ	Z	€	€
Í	T FÍ	Z	€	€
Î	T FI	Z	HEEG	ÃÍ
Ï	T FI	Z	HEEG	ÃJÍ
Ì	T FI	Z	HEE	ÃÍ€
J	T FI	Z	HEEG	ÃÍ€
F€	T FI	Z	€	€
FF	T Ì	Z	HEFI	ÃHE
FG	T Ì	Z	HEFI	ÃÍÍ
FH	T Ì	Z	€	€
FI	T Ì	Z	€	€
FÍ	T Ì	Z	€	€
FÍ	T HÍ	Z	HEE	ÃÍ€
FÍ	T HÍ	Z	€	€
FÍ	T HÍ	Z	€	€

A Ya VYf'DcJbh@UXg'f6 @\* : \$KJbX!GYfjJWŁfVcbHjbi YXŁ

	T ^ { à ^ { Á ã ã }	Ö ã ^ & ö }	T æ { á ã ã Ÿ ß é á }	Š & œ { Ÿ ß é á }
FJ	THÍ	Z	€	€
GE	THÍ	Z	€	€
GF	THF	Z	‰€	ÃÍ
GG	THF	Z	‰€	ÃJÍ
GH	THF	Z	‰€G	ÃÍÍ
G	THF	Z	€	€
Ğ	THF	Z	€	€
Ğ	THE	Z	‰€G	ÃÍ
Ğ	THE	Z	‰€G	ÃJÍ
Ğ	THE	Z	‰€I	ÃÍ€
GJ	THE	Z	‰€G	ÃÍ€
H€	THE	Z	€	€
HF	TG	Z	‰€FI	ÃH€
HG	TG	Z	‰€FI	ÃÍÍ
HH	TG	Z	€	€
H	TG	Z	€	€
HÍ	TG	Z	€	€
HÍ	TGH	Z	‰€	ÃÍ
HÍ	TGH	Z	‰€	ÃJÍ
HÍ	TGH	Z	‰€G	ÃÍÍ
HJ	TGH	Z	€	€
I€	TGH	Z	€	€
IF	TGG	Z	‰€G	ÃÍ
IG	TGG	Z	‰€G	ÃJÍ
IH	TGG	Z	‰€I	ÃÍ€
II	TGG	Z	‰€G	ÃÍ€
ÍÍ	TGG	Z	€	€
ÍÍ	TFÍ	Z	‰€FI	ÃH€
ÍÍ	TFÍ	Z	‰€FI	ÃÍÍ
IJ	TFÍ	Z	€	€
Í€	TFÍ	Z	€	€

A Ya VYf'Dc Jbh@UXq'f6 @7 + :- -\$'K JbX?'GYfj JWZ

## A Ya VYf Dc Jbh@UXg ff @ ; - \$K JbX! GYfj JWŁ fV cbHjbi YXŁ

T^{ à^ ÁÖ! }	Öä^ &{ }	T æ } ß à^ Ä EÉá	Š &{ } ŽÉA á
FÍ	THÍ	Ý	€
FÍ	THÍ	Ý	€
FJ	THÍ	Ý	€
G€	THÍ	Ý	€
GF	THF	Ý	‰€
GG	THF	Ý	‰€
GH	THF	Ý	‰€
G	THF	Ý	€
GÍ	THF	Ý	€
GÍ	THE	Ý	‰€
GÍ	THE	Ý	‰€
GÍ	THE	Ý	‰€
H€	THE	Ý	€
HF	TG	Ý	‰€
HG	TG	Ý	‰€
HH	TG	Ý	€
HI	TG	Ý	€
HÍ	TG	Ý	€
HÍ	TGH	Ý	‰€
HÍ	TGH	Ý	‰€
HÍ	TGH	Ý	‰€
HÍ	TGH	Ý	‰€
HÍ	TGH	Ý	‰€
I€	T GH	Ý	€
IF	T GG	Ý	‰€
IG	T GG	Ý	‰€
IH	T GG	Ý	‰€
II	T GG	Ý	‰€
II	T GG	Ý	€
II	TFÍ	Ý	‰€
II	TFÍ	Ý	‰€
II	TFÍ	Ý	€
IJ	TFÍ	Ý	€
I€	TFÍ	Ý	€

## A Ya VYf Dc Jbh@UXg ff @ ; : JWŁ

T^{ à^ ÁÖ! }	Öä^ &{ }	T æ } ß à^ Ä EÉá	Š &{ } ŽÉA á
F	TFÍ	Ý	‰€ G
G	TFÍ	Ý	‰€ G
H	TFÍ	Ý	‰€ H
I	TFÍ	Ý	€
I	TFÍ	Ý	€
I	TFÍ	Ý	‰€ G
I	TFÍ	Ý	‰€ G
I	TFÍ	Ý	‰€ HF
J	TFÍ	Ý	‰€ H
F€	TFÍ	Ý	€
FF	TÍ	Ý	‰€ I
FG	TÍ	Ý	‰€ I
FH	TÍ	Ý	€
FI	TÍ	Ý	€

A Ya VYf'DcJbh@UXg'f6 @ ; : =WŁfVcbh]bi YXŁ

T <sup>À</sup> <sup>Á</sup> <sup>Ã</sup>	T <sup>È</sup> <sup>É</sup> <sup>Ë</sup>	T <sup>Ã</sup> <sup>Ã</sup> <sup>Ã</sup>	T <sup>Ã</sup> <sup>Ã</sup> <sup>Ã</sup>	T <sup>Ã</sup> <sup>Ã</sup> <sup>Ã</sup>
FÍ	TÍ	Ý	€	€
FÍ	THÍ	Ý	Ã€I	ÃÍ€
FÍ	THÍ	Ý	€	€
FÍ	THÍ	Ý	€	€
FJ	THÍ	Ý	€	€
GE	THÍ	Ý	€	€
GF	THF	Ý	Ã€G	ÃÍ
GG	THF	Ý	Ã€G	ÃJÍ
GH	THF	Ý	Ã€H	ÃÍÍ
GI	THF	Ý	€	€
GI	THF	Ý	€	€
GI	THE	Ý	Ã€G	ÃÍ
GI	THE	Ý	Ã€G	ÃJÍ
GI	THE	Ý	Ã€F	ÃÍ€
GJ	THE	Ý	Ã€H	ÃÍ€
HE	THE	Ý	€	€
HF	TG	Ý	Ã€I	ÃHE
HG	TG	Ý	Ã€I	ÃÍÍ
HH	TG	Ý	€	€
HI	TG	Ý	€	€
HÍ	TG	Ý	€	€
HÍ	TGH	Ý	Ã€G	ÃÍ
HÍ	TGH	Ý	Ã€G	ÃJÍ
HÍ	TGH	Ý	Ã€H	ÃÍÍ
HJ	TGH	Ý	€	€
I€	TGH	Ý	€	€
I F	TGG	Ý	Ã€G	ÃÍ
I G	TGG	Ý	Ã€G	ÃJÍ
I H	TGG	Ý	Ã€F	ÃÍ€
II	TGG	Ý	Ã€H	ÃÍ€
II	TGG	Ý	€	€
II	TFÍ	Ý	Ã€I	ÃHE
II	TFÍ	Ý	Ã€I	ÃÍÍ
II	TFÍ	Ý	€	€
I J	TFÍ	Ý	€	€
I €	TFÍ	Ý	€	€

A Ya VYf'Dc Jbh@ UXq f6 @ % : A UJbh@@%t

T<sup>æ</sup>{ à:| Å:œ:| Ö:ä:&ö:} T æ } à: à: Ä: È: É:á Š: &ä: } Ž: Ë: Á:

A Ya VYf'DcJbh@UXg'f6 @ % : A UJbh@@&L

T<sup>æ</sup>{ à|ä|ɛ̄|ɛ̄| Öä{ ä&gt;} T æ} å^ä^ž ß ēá ř&gt; } žč á F TF Ÿ ũ Á JÍ

A Ya VYf Dc Jbh@ UXg ff @ % : A UJbh@@' t

T <sup>h</sup>	TH	Ö	Ä	Å
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### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@ L

T^{ à^ ÁS&a^   F	Öä^&q{   TH	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
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### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@ L

T^{ à^ ÁS&a^   F	Öä^&q{   TÍ	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	-------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@\* L

T^{ à^ ÁS&a^   F	Öä^&q{   TÍ	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁJÍ
------------------	-------------	-----------------------	---------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@+ L

T^{ à^ ÁS&a^   F	Öä^&q{   TI€	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	--------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@- L

T^{ à^ ÁS&a^   F	Öä^&q{   TIG	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	--------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@- L

T^{ à^ ÁS&a^   F	Öä^&q{   THI	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	--------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@%\$L

T^{ à^ ÁS&a^   F	Öä^&q{   THI	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	--------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@%&L

T^{ à^ ÁS&a^   F	Öä^&q{   THG	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
------------------	--------------	-----------------------	--------------------

### A Ya VYf Dc Jbh@UXg f6 @% : A Ujh@@%&

T^{ à^ ÁS&a^   F	Öä^&q{   TH	T æ } ß à^ Ź Èçá   ÙG	Š &a^ } ŽdÁ á   ÁÍ
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### >cJbh@UXg UbX'9 bZcfWX'8 Jgd'UWYa YbIg f6 @ - : @j Y@UX'UŁ

R à ÁS&a^   F	ŠDÈ   PFE	Öä^&q{   Š	T æ } ß à^ Ź Èçá   ÙG
G	PIG	Š	ÙG
H	PG	Š	ÙG

### >cJbh@UXg UbX'9 bZcfWX'8 Jgd'UWYa YbIg f6 @ %\$ : @j Y@UX'VŁ

R à ÁS&a^   F	ŠDÈ   PFI	Öä^&q{   Š	T æ } ß à^ Ź Èçá   ÙG
G	PII	Š	ÙG
H	PHE	Š	ÙG

>c]bh@UXgUbX'9bZcfWx'8Jgd`UWwA Ybhg'f6 @ '%. @j Y@UX.WL

Rāga Sāh	ŠEH	Öä^&çä}	Tæ} ß å^&ZEH DÄG Eaa DÄG E äGHE
F	PF	Š	EE
G	PÍ	Š	EE
H	PHG	Š	EE

>cJbh@UXgUbX'9bZcfWVX'8Jgd`UWVa Ybhg'f6 @ %.: @j Y@UX'XŁ

F Å G Å H Å		S Ö	Ö Å	T Å
F	þí€	þ	ÿ	þ
G	þF	þ	ÿ	þ
H	þH	þ	ÿ	þ

A Ya VYf'8 Jglf]Vi hYX'@ UXg f6 @' & \$ K JbX! Bc -Wt

## A Ya VYf'8]glf]Vi hYX@UXg'f6 @T' & \$'K]bX!'Bc 'WŁt c b h p i YXL

T^{ à^ ^ Ás^ ^ }	Öä^ & ^ }	ÚcetoÁt æ } ß à^ ^ Z Döfifl Ö) à Át æ } ß à^ ^ Z Döfifl	ÚcetoÁt & ^ } Zd Á á	Ó) à Ás^ & ^ } Zd Á á
HJ	TÍH	Z	ßEF	€
I €	TÍI	Z	ßEF	€
I F	TÍI	Z	ßEF	€
I G	TÍI	Z	ßEF	€
I H	TÍJ	Z	ßFH	€
I I	TÍ€	Z	ßFH	€
I I	TÍJ	Z	ßFI	€
I I	TÍ EOE	Z	ßFI	€
I I	TÍ FOE	Z	ßFF	€
I I	TÍ OOE	Z	ßFF	€
I J	TÍ HOE	Z	ßFI	€
I €	TÍI	Z	ßFF	€
I F	TÍH	Z	ßFF	€
I G	TÍI	Z	ßFF	€
I H	TÍJ	Z	ßF	€
I I	TJ€	Z	ßF	€
I I	TJF	Z	ßF	€

## A Ya VYf'8]glf]Vi hYX@UXg'f6 @T' :- \$'K]bX!'Bc 'WŁ

T^{ à^ ^ Ás^ ^ }	Öä^ & ^ }	ÚcetoÁt æ } ß à^ ^ Z Döfifl Ö) à Át æ } ß à^ ^ Z Döfifl	ÚcetoÁt & ^ } Zd Á á	Ó) à Ás^ & ^ } Zd Á á
F	TF	Ý	ßECH	€
G	TG	Ý	ßEHG	€
H	TH	Ý	ßECH	€
I	TI	Ý	ßEHG	€
I	TÍ	Ý	ßEHG	€
I	TÍ	Ý	ßECH	€
I	TÍ	Ý	ßEFG	€
I	T F€	Ý	ßEFF	€
J	T FI	Ý	ßEFF	€
F€	T FI	Ý	ßEFF	€
FF	T FÍ	Ý	ßEFF	€
FG	T FÍ	Ý	ßEFF	€
FH	T GG	Ý	ßEFF	€
FI	T GH	Ý	ßEFF	€
FÍ	T G	Ý	ßEFF	€
FÍ	T G	Ý	ßEFF	€
FÍ	T HG	Ý	ßEGF	€
G€	T HH	Ý	ßEF	€
GF	T HI	Ý	ßEGF	€
GG	T HÍ	Ý	ßEF	€
GH	T HÍ	Ý	ßEGF	€
G	T HÍ	Ý	ßEF	€
G	T HÍ	Ý	ßEGF	€
G	T HÍ	Ý	ßEF	€
G	T I €	Ý	ßEGF	€
G	T IF	Ý	ßEF	€
GJ	T IG	Ý	ßEGF	€
H€	T IH	Ý	ßEF	€
HF	T II	Ý	ßFI	€

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @Y' : - \$' K JbX'! Bc' -WŁfV cbhjbi YXŁ

T^ { à^ { Áséé{ }	Öä^ &ç{ }	ÙçæöÁt æ{ } ß à^ Z Ðæéé{ } Ò) à Át æ{ } ß à^ Z Ðæéé{ }	ÙçæöÁt &ç{ } ß à^ Z Ðæéé{ }	ÙçæöÁt &ç{ } ß à^ Z Ðæéé{ }	Ó) à Áséé{ } ß à^ Z Ðæéé{ }
HG	TÍI	Ý	ßEEJ	ßEEJ	€
HH	TÍÍ	Ý	ßFG	ßFG	€
HI	TÍI	Ý	ßEJ	ßEJ	€
HÍ	TÍJ	Ý	ßFG	ßFG	€
HÍ	TÍ€	Ý	ßFI	ßFI	€
HÍ	TÍF	Ý	ßFI	ßFI	€
HÍ	TÍG	Ý	ßEJ	ßEJ	€
HJ	TÍH	Ý	ßFG	ßFG	€
I€	TÍI	Ý	ßFI	ßFI	€
IF	TÍI	Ý	ßFI	ßFI	€
IG	TÍI	Ý	ßFI	ßFI	€
IH	TÍJ	Ý	ßFH	ßFH	€
II	TÍ€	Ý	ßFH	ßFH	€
II	TÍJ	Ý	ßFI	ßFI	€
II	TÍ€OE	Ý	ßFI	ßFI	€
II	TÍFOE	Ý	ßFF	ßFF	€
II	TÍGOE	Ý	ßFF	ßFF	€
IJ	TÍHŒ	Ý	ßFI	ßFI	€
I€	TÍI	Ý	ßFF	ßFF	€
IF	TÍH	Ý	ßFF	ßFF	€
IG	TÍI	Ý	ßFF	ßFF	€
IH	TÍJ	Ý	ßF	ßF	€
II	TJ€	Ý	ßF	ßF	€
II	TJF	Ý	ßF	ßF	€

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @Y' ( : \$' K JbX'! -WŁ

T^ { à^ { Áséé{ }	Öä^ &ç{ }	ÙçæöÁt æ{ } ß à^ Z Ðæéé{ } Ò) à Át æ{ } ß à^ Z Ðæéé{ }	ÙçæöÁt &ç{ } ß à^ Z Ðæéé{ }	ÙçæöÁt &ç{ } ß à^ Z Ðæéé{ }	Ó) à Áséé{ } ß à^ Z Ðæéé{ }
F	TF	Z	ßeei	ßeei	€
G	TG	Z	ßFG	ßFG	€
H	TH	Z	ßei	ßei	€
I	TI	Z	ßFG	ßFG	€
I	TÍ	Z	ßFG	ßFG	€
I	TÍ	Z	ßei	ßei	€
I	TÍ	Z	ßEG	ßEG	€
I	TF€	Z	ßEG	ßEG	€
J	T FI	Z	ßEG	ßEG	€
F€	T FÍ	Z	ßEG	ßEG	€
FF	T FÍ	Z	ßEG	ßEG	€
FG	T FÍ	Z	ßEG	ßEG	€
FH	T GG	Z	ßEG	ßEG	€
FI	T GH	Z	ßEG	ßEG	€
FÍ	T G	Z	ßEG	ßEG	€
FÍ	T G	Z	ßEG	ßEG	€
FÍ	T H€	Z	ßEG	ßEG	€
FÍ	T HF	Z	ßEG	ßEG	€
FJ	T HG	Z	ßei	ßei	€
G€	T HH	Z	ßei	ßei	€
GF	T HI	Z	ßei	ßei	€
GG	T HÍ	Z	ßei	ßei	€
GH	T HÍ	Z	ßei	ßei	€
G	THÍ	Z	ßei	ßei	€

A Ya VYf'8 Jgkf]Vi hYX@ UXg'f6 @' ( : \$ K JbX! =WYf7 cbHbi YXŁ

T <small>À</small> T <small>Á</small>	O <small>Ã</small> O <small>É</small>	Ú <small>Ç</small> Ú <small>Å</small>	Ó <small>À</small> Ó <small>Á</small>	È <small>À</small> È <small>Á</small>	Í <small>À</small> Í <small>Á</small>	Ó <small>À</small> Ó <small>Á</small>	È <small>À</small> È <small>Á</small>
G	T <small>Ì</small>	Z	€	€	€	€	€
G	T <small>H</small>	Z	€	€	€	€	€
G	T <small>I</small> €	Z	€	€	€	€	€
G	T <small>I</small> F	Z	€	€	€	€	€
G	T <small>I</small> G	Z	€	€	€	€	€
H€	T <small>I</small> H	Z	€	€	€	€	€
HF	T <small>I</small> I	Z	€	€	€	€	€
HG	T <small>I</small> I	Z	€	€	€	€	€
HH	T <small>I</small> I	Z	€	€	€	€	€
H	T <small>I</small> I	Z	€	€	€	€	€
H	T <small>I</small> J	Z	€	€	€	€	€
H	T <small>I</small> €	Z	€	€	€	€	€
H	T <small>I</small> F	Z	€	€	€	€	€
H	T <small>I</small> G	Z	€	€	€	€	€
HJ	T <small>I</small> H	Z	€	€	€	€	€
I€	T <small>I</small> I	Z	€	€	€	€	€
IF	T <small>I</small> I	Z	€	€	€	€	€
IG	T <small>I</small> I	Z	€	€	€	€	€
IH	T <small>I</small> J	Z	€	€	€	€	€
II	T <small>I</small> €	Z	€	€	€	€	€
II	T <small>I</small> J	Z	€	€	€	€	€
II	T <small>I</small> FCE	Z	€	€	€	€	€
II	T <small>I</small> FCE	Z	€	€	€	€	€
II	T <small>I</small> GCE	Z	€	€	€	€	€
IJ	T <small>I</small> HCE	Z	€	€	€	€	€
I€	T <small>I</small> I	Z	€	€	€	€	€
IF	T <small>I</small> H	Z	€	€	€	€	€
IG	T <small>I</small> I	Z	€	€	€	€	€
IH	T <small>I</small> J	Z	€	€	€	€	€
II	T <small>J</small> €	Z	€	€	€	€	€
II	T <small>J</small> F	Z	€	€	€	€	€

A Ya VYf'8Jgkf]Vi hYX'@UXg'fs @?') :- \$'K JbX! =WŁ

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @T' ) :- \$ K JbX'! WKLfV cbIjbi YXk

T^{ à^ ^ }	Öä^ &ç }	ÙçæñT æ } ß à^ ^ DæññO) à ÁT æ } ß à^ ^ DæññE	ÙçæñT &ç } ß à^ ^ DæññE	ÙçæñT &ç } ß à^ ^ DæññE	Ó) à^ ^ &ç } ß à^ ^ DæññE
FI	THF	Ý	ßeeG	ßeeG	€
FJ	THG	Ý	ßeeI	ßeeI	€
GE	THH	Ý	ßeeI	ßeeI	€
GF	THI	Ý	ßeeI	ßeeI	€
GG	THÍ	Ý	ßeeI	ßeeI	€
GH	THÍ	Ý	ßeeI	ßeeI	€
GI	THÍ	Ý	ßeeI	ßeeI	€
GÍ	THÍ	Ý	ßeeI	ßeeI	€
GÍ	THÍ	Ý	ßeeI	ßeeI	€
GÍ	TI €	Ý	ßeeI	ßeeI	€
GÍ	TI F	Ý	ßeeI	ßeeI	€
GJ	TI G	Ý	ßeeI	ßeeI	€
HE	TI H	Ý	ßeeI	ßeeI	€
HF	TI I	Ý	ßeeI	ßeeI	€
HG	TI I	Ý	ßeeI	ßeeI	€
HH	TI I	Ý	ßeeI	ßeeI	€
HI	TI I	Ý	ßeeI	ßeeI	€
HÍ	TI J	Ý	ßeeI	ßeeI	€
HÍ	TI €	Ý	ßeeI	ßeeI	€
HÍ	TI F	Ý	ßeeI	ßeeI	€
HÍ	TI G	Ý	ßeeI	ßeeI	€
HJ	TI H	Ý	ßeeI	ßeeI	€
I €	TI I	Ý	ßeeI	ßeeI	€
I F	TI I	Ý	ßeeI	ßeeI	€
I G	TI I	Ý	ßeeI	ßeeI	€
I H	TI J	Ý	ßeeI	ßeeI	€
II	TI €	Ý	ßeeI	ßeeI	€
II	TI J	Ý	ßeeI	ßeeI	€
II	TI FOE	Ý	ßeeI	ßeeI	€
II	TI FOE	Ý	ßeeI	ßeeI	€
II	TI GOE	Ý	ßeeI	ßeeI	€
I J	TI HOE	Ý	ßeeI	ßeeI	€
I €	TI I	Ý	ßeeG	ßeeG	€
I F	TI H	Ý	ßeeG	ßeeG	€
I G	TI I	Ý	ßeeG	ßeeG	€
I H	TI J	Ý	ßeeI	ßeeI	€
II	TJ €	Ý	ßeeI	ßeeI	€
II	TJF	Ý	ßeeI	ßeeI	€

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @T' \* : \$ K JbX'! GYfj JWk

T^{ à^ ^ }	Öä^ &ç }	ÙçæñT æ } ß à^ ^ DæññO) à ÁT æ } ß à^ ^ DæññE	ÙçæñT &ç } ß à^ ^ DæññE	ÙçæñT &ç } ß à^ ^ DæññE	Ó) à^ ^ &ç } ß à^ ^ DæññE
F	TF	Z	ßeeG	ßeeG	€
G	TG	Z	ßeeG	ßeeG	€
H	TH	Z	ßeeG	ßeeG	€
I	TI	Z	ßeeG	ßeeG	€
I	TÍ	Z	ßeeG	ßeeG	€
I	TÍ	Z	ßeeG	ßeeG	€
I	TÍ	Z	ßeeH	ßeeH	€
I	TÍ	Z	ßeeH	ßeeH	€
I	TF€	Z	ßeeH	ßeeH	€
J	TFI	Z	ßeeH	ßeeH	€
F€	TFÍ	Z	ßeeH	ßeeH	€

A Ya VYf'8JglfJVi hYX'@UXg'f6 @T'\*'. \$'K JbX!'GYfj JWM'fV cbhjbi YXŁ

T{ à^í Áéúéí}	Öä^&ö{ }	Ùçáó Á{ æ} ë á^ž Dëññò{ } ã Á{ æ} ë á^ž Dëññé{ }	Ùçáó Á{ &æ{ } } Zéñ á{ }	Ò{ } ã Á{ &æ{ } } Zéñ á{ }
FF	T FÌ	Z	ßéééH	€
FG	T FÌ	Z	ßéééH	€
FH	T GG	Z	ßéééH	€
FI	T GH	Z	ßéééH	€
FÍ	T G	Z	ßéééH	€
FÎ	T GÌ	Z	ßéééH	€
FÏ	T HÈ	Z	ßéééH	€
FÌ	T HF	Z	ßéééH	€
FJ	T HG	Z	ßééF	€
G€	T HH	Z	ßééF	€
GF	T H	Z	ßééF	€
GG	T HÌ	Z	ßééF	€
GH	T HÌ	Z	ßééF	€
G	T HÌ	Z	ßééF	€
GÍ	T HÌ	Z	ßééF	€
GÌ	T HU	Z	ßééF	€
GÏ	T I €	Z	ßééF	€
G	T IF	Z	ßééF	€
GJ	T IG	Z	ßééF	€
H€	T IH	Z	ßééF	€
HF	T II	Z	ßééF	€
HG	T II	Z	ßééâ	€
HH	T II	Z	ßééâ	€
H	T II	Z	ßééâ	€
HÍ	T IJ	Z	ßééâ	€
HÌ	T I €	Z	ßééF	€
HÌ	T IF	Z	ßééF	€
HÌ	T ÍG	Z	ßééâ	€
HJ	T IH	Z	ßééâ	€
I€	T ÍI	Z	ßééF	€
IF	T ÍI	Z	ßééF	€
IG	T ÍI	Z	ßééU	€
IH	T ÍJ	Z	ßééâ	€
II	T Í €	Z	ßééâ	€
ÍI	T Í J	Z	ßééF	€
ÍI	T Í EO	Z	ßééU	€
ÍI	T Í FOE	Z	ßééâ	€
ÍI	T Í OOE	Z	ßééâ	€
IJ	T Í HOE	Z	ßééU	€
Í€	T Í I	Z	ßééH	€
ÍF	T Í H	Z	ßééH	€
ÍG	T Í I	Z	ßééH	€
ÍH	T IJ	Z	ßééâ	€
ÍI	T JE	Z	ßééâ	€
ÍÍ	T JF	Z	ßééâ	€

A Ya VYf'8Jglf]Vi hYX'@UXg'f6 @? '+' - \$'K JbX!'GYfj JWŁ

A Ya VYf'8JgHJM hYX@UXg'f6 @? +:- \$'K JbX!GYfj JWŁf7 cbHbi YXŁ

T ^{ à^{\wedge} Á^{\wedge} }	Ö^{\wedge} & ö^{\wedge}	Ú^{\wedge} c^{\wedge} Á^{\wedge} z^{\wedge} ã^{\wedge} á^{\wedge} Ž^{\wedge} ð^{\wedge} é^{\wedge} ö^{\wedge}	Ú^{\wedge} c^{\wedge} Á^{\wedge} z^{\wedge} ã^{\wedge} á^{\wedge} Ž^{\wedge} ð^{\wedge} é^{\wedge} ö^{\wedge}	Ú^{\wedge} c^{\wedge} Á^{\wedge} z^{\wedge} ã^{\wedge} á^{\wedge} Ž^{\wedge} ð^{\wedge} é^{\wedge} ö^{\wedge}	Ó^{\wedge} á^{\wedge} Á^{\wedge} z^{\wedge} ã^{\wedge} á^{\wedge} Ž^{\wedge} ð^{\wedge} é^{\wedge} ö^{\wedge}	Ó^{\wedge} á^{\wedge} Á^{\wedge} z^{\wedge} ã^{\wedge} á^{\wedge} Ž^{\wedge} ð^{\wedge} é^{\wedge} ö^{\wedge}
I	T I	Ý	EEEG	EEEG	€	€
Í	T Í	Ý	EEEG	EEEG	€	€
Î	T Î	Ý	EEEG	EEEG	€	€
Ï	T Ï	Ý	EEEH	EEEH	€	€
Ì	T F€	Ý	EEEH	EEEH	€	€
J	T FI	Ý	EEEH	EEEH	€	€
F€	T FÍ	Ý	EEEH	EEEH	€	€
FF	T FÍ	Ý	EEEH	EEEH	€	€
FG	T FÍ	Ý	EEEH	EEEH	€	€
FH	T CG	Ý	EEEH	EEEH	€	€
FI	T GH	Ý	EEEH	EEEH	€	€
FÍ	T G	Ý	EEEH	EEEH	€	€
FÎ	T G	Ý	EEEH	EEEH	€	€
FÏ	T H€	Ý	EEEH	EEEH	€	€
FÌ	T HF	Ý	EEEH	EEEH	€	€
FJ	T HG	Ý	EEEF	EEEF	€	€
G€	T HH	Ý	EEEF	EEEF	€	€
GF	T HI	Ý	EEEF	EEEF	€	€
GG	T HÍ	Ý	EEEF	EEEF	€	€
GH	T HÎ	Ý	EEEF	EEEF	€	€
GI	T HÍ	Ý	EEEF	EEEF	€	€
GI	T HÍ	Ý	EEEF	EEEF	€	€
GI	T HU	Ý	EEEF	EEEF	€	€
Ĝ	T I €	Ý	EEEF	EEEF	€	€
ĜI	T IF	Ý	EEEF	EEEF	€	€
GJ	T IG	Ý	EEEF	EEEF	€	€
H€	T IH	Ý	EEEF	EEEF	€	€
HF	T II	Ý	EEEF	EEEF	€	€
HG	T II	Ý	EECA	EECA	€	€
HH	T II	Ý	EECD	EECD	€	€
HI	T II	Ý	EECD	EECD	€	€
HÍ	T IJ	Ý	EECD	EECD	€	€
HÎ	T I €	Ý	EECF	EECF	€	€
HÎ	T I F	Ý	EECF	EECF	€	€
HÎ	T I G	Ý	EECD	EECD	€	€
HJ	T I H	Ý	EECD	EECD	€	€
I €	T II	Ý	EECF	EECF	€	€
I F	T II	Ý	EECF	EECF	€	€
I G	T II	Ý	EECJ	EECJ	€	€
I H	T IJ	Ý	EECD	EECD	€	€
II	T I €	Ý	EECD	EECD	€	€
II	T I J	Ý	EECF	EECF	€	€
II	T I EOE	Ý	EECJ	EECJ	€	€
II	T I FOE	Ý	EECD	EECD	€	€
II	T I GOE	Ý	EECD	EECD	€	€
I J	T I HOE	Ý	EECJ	EECJ	€	€
I €	T II	Ý	EECH	EECH	€	€
I F	T I H	Ý	EECH	EECH	€	€
I G	T II	Ý	EECH	EECH	€	€
I H	T I J	Ý	EECD	EECD	€	€
II	T J €	Ý	EECD	EECD	€	€
II	T JF	Ý	EECD	EECD	€	€

A Ya VYf'8JgHJVi hYX'@UXg'f6 @ ; : =Wt

T	A	E	S	E	S	E	S
F	T F	Y	E E	E E	E	E	E
G	T G	Y	E E	E E	E	E	E
H	T H	Y	E E	E E	E	E	E
I	T I	Y	E E	E E	E	E	E
I	T I	Y	E E	E E	E	E	E
I	T I	Y	E E	E E	E	E	E
I	T I	Y	E E	E E	E	E	E
I	T F E	Y	E E	E E	E	E	E
J	T F I	Y	E E	E E	E	E	E
F E	T F I	Y	E E	E E	E	E	E
F F	T F I	Y	E E	E E	E	E	E
F G	T F I	Y	E E	E E	E	E	E
F H	T G G	Y	E E	E E	E	E	E
F I	T G H	Y	E E	E E	E	E	E
F I	T G	Y	E E	E E	E	E	E
F I	T G	Y	E E	E E	E	E	E
F I	T H E	Y	E E	E E	E	E	E
F I	T H F	Y	E E	E E	E	E	E
F J	T H G	Y	E E	E E	E	E	E
G E	T H H	Y	E E	E E	E	E	E
G F	T H	Y	E E	E E	E	E	E
G G	T H	Y	E E	E E	E	E	E
G H	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
G I	T H	Y	E E	E E	E	E	E
H E	T H	Y	E E	E E	E	E	E
H F	T I I	Y	E E	E E	E	E	E
H G	T I I	Y	E E	E E	E	E	E
H H	T I I	Y	E E	E E	E	E	E
H I	T I I	Y	E E	E E	E	E	E
H I	T I J	Y	E E	E E	E	E	E
H I	T I J	Y	E E	E E	E	E	E
H I	T I J	Y	E E	E E	E	E	E
H I	T I J	Y	E E	E E	E	E	E
H I	T I F	Y	E E	E E	E	E	E
H I	T I G	Y	E E	E E	E	E	E
H J	T I H	Y	E E	E E	E	E	E
I E	T I I	Y	E E	E E	E	E	E
I F	T I I	Y	E E	E E	E	E	E
I G	T I I	Y	E E	E E	E	E	E
I H	T I J	Y	E E	E E	E	E	E
I I	T I J	Y	E E	E E	E	E	E
I I	T I J	Y	E E	E E	E	E	E
I I	T I E O E	Y	E E	E E	E	E	E
I I	T I F O E	Y	E E	E E	E	E	E
I I	T I G O E	Y	E E	E E	E	E	E
I J	T I H O E	Y	E E	E E	E	E	E
I E	T I I	Y	E E	E E	E	E	E
I F	T I H	Y	E E	E E	E	E	E
I G	T I I	Y	E E	E E	E	E	E

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @T ; : -WLFfV cbhjbi YXŁ

T^ { à^ ^ ÁSéé^ }	Öä^ &ç }	Úçéöñ æ } ß à^ ^ Z DÉÉÉÖ) à ÁT æ } ß à^ ^ Z DÉÉÉÜ) Úçéöñ &ç } Žéá á	Ó) à ÁSéé } Žéá á
I H	T I J	Ý	€
I I	T J €	Ý	€
I I	T J F	Ý	€

## A Ya VYf'8 Jglf]Vi hYX'@ UXg'f6 @T & : 6 @T %HfUbg]Ybh5 f YU@ UXgŁ

T^ { à^ ^ ÁSéé^ }	Öä^ &ç }	Úçéöñ æ } ß à^ ^ Z DÉÉÉÖ) à ÁT æ } ß à^ ^ Z DÉÉÉÜ) Úçéöñ &ç } Žéá á	Ó) à ÁSéé } Žéá á
F	T H	Ý	Í ÈI
G	T H	Ý	J ÈI
H	T H	Ý	F ÈJG
I	T H	Ý	F ÈJG
I	T H	Ý	FH
I	T I	Ý	Í ÈI
I	T I	Ý	J ÈI
I	T I	Ý	F ÈJG
J	T I	Ý	F ÈJG
F€	T I	Ý	FH
FF	T G	Ý	ÈG
FG	T II	Ý	È
FH	T II	Ý	FÈ
FI	T II	Ý	GÈ
FÍ	T II	Ý	HÈ
FÎ	T II	Ý	I
FÏ	T II	Ý	È
FÌ	T II	Ý	È HH
FJ	T II	Ý	È HH
G€	T II	Ý	FÈ
GF	T II	Ý	F ÈHH
GG	T II	Ý	G ÈHH
GH	T I J	Ý	È HH
G	T I J	Ý	F ÈHH
GÍ	T I J	Ý	G ÈFF
Gî	T I J	Ý	H ÈHH
GÏ	T I J	Ý	I ÈHH
Gì	T I J	Ý	I ÈHH
GJ	T I FOE	Ý	F ÈJJ
H€	T I J	Ý	F ÈF
HF	T I GÖE	Ý	F ÈIG
HG	T H	Ý	Í ÈHH
HH	T H	Ý	Í ÈHH
H	T H	Ý	J È
HÍ	T I €	Ý	È EF
Hî	T I GÖE	Ý	H ÈGÍ
HÏ	T I	Ý	Í ÈHH
HÌ	T I	Ý	Í ÈHH
HJ	T I	Ý	J È
I €	T I GÖE	Ý	F ÈF
I F	T I HÖE	Ý	H ÈGÍ
I G	T I F	Ý	F ÈUÍ
I H	T I F	Ý	G ÈJ
II	T I F	Ý	I ÈHH
I I	T I €	Ý	F ÈHH

A Ya VYf'8 JglfJvI HYX' @ UXg fb @ & 6 @ %HfUbglYbh5 f YU @ UXgLfr c bhjbi YXL

T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>	T <small>À</small> T <small>À</small> T <small>À</small>
I <small>À</small>	T <small>Ì</small> €	Y	E <small>È</small>	E <small>È</small>	F <small>È</small> H <small>Ì</small>	G <small>È</small> H
I <small>È</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small> H	€	F <small>È</small> I
I <small>È</small>	T <small>Ì</small> F	Y	E <small>È</small> H	E <small>È</small>	F <small>È</small> I	G <small>È</small> I
I <small>J</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small>	G <small>È</small>	H <small>È</small> G
I <small>€</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small> D JH	H <small>È</small> G	I <small>È</small> I
I <small>F</small>	T <small>Ì</small> F	Y	E <small>È</small> D JH	I <small>È</small> ^H	I <small>È</small> I	I <small>È</small> G
I <small>G</small>	T <small>Ì</small> H	Y	E <small>È</small> G	E <small>È</small>	€	F <small>È</small> I
I <small>H</small>	T <small>Ì</small> H	Y	E <small>È</small>	E <small>È</small>	F <small>È</small> I	G <small>È</small> I
I <small>I</small>	T <small>Ì</small> H	Y	E <small>È</small>	E <small>È</small> H	G <small>È</small>	H <small>È</small> G
I <small>I</small>	T <small>Ì</small> H	Y	E <small>È</small> H	E <small>È</small> D I G	H <small>È</small> G	I <small>È</small> I
I <small>I</small>	T <small>Ì</small> H	Y	E <small>È</small> D I G	I <small>È</small> ^H	I <small>È</small> I	I <small>È</small> G
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small> G	E <small>È</small> G	€	È
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small> F	E <small>È</small>	€	ÈHH
I <small>J</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small> F	ÈHH	ÈII
I <small>€</small>	T <small>Ì</small> I	Y	E <small>È</small> F	E <small>È</small> I	ÈII	F <small>È</small> H
I <small>F</small>	T <small>Ì</small> I	Y	E <small>È</small> I	E <small>È</small>	F <small>È</small> H	F <small>È</small> HH
I <small>G</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small> D H	F <small>È</small> H	G <small>È</small> II
I <small>H</small>	T <small>Ì</small> €	Y	E <small>È</small> F	E <small>È</small>	€	È
I <small>I</small>	T <small>Ì</small> €	Y	E <small>È</small>	E <small>È</small>	È	F <small>È</small> E
I <small>I</small>	T <small>Ì</small> €	Y	E <small>È</small>	E <small>È</small>	F <small>È</small>	G <small>È</small>
I <small>I</small>	T <small>Ì</small> €	Y	E <small>È</small>	E <small>È</small>	G <small>È</small>	H <small>È</small> G
I <small>I</small>	T <small>Ì</small> €	Y	E <small>È</small>	E <small>È</small> D I H	H <small>È</small> G	I
I <small>I</small>	T <small>Ì</small> F	Y	E <small>È</small> D FJ	E <small>È</small> D I J	€	ÈH
I <small>J</small>	T <small>Ì</small> F	Y	E <small>È</small> D I J	E <small>È</small> D GF	ÈH	F <small>È</small> II
I <small>€</small>	T <small>Ì</small> F	Y	E <small>È</small> D GF	E <small>È</small> D HU	F <small>È</small> II	G <small>È</small> FF
I <small>F</small>	T <small>Ì</small> F	Y	E <small>È</small> D HU	E <small>È</small> D I G	G <small>È</small> FF	HEH
I <small>G</small>	T <small>Ì</small> F	Y	E <small>È</small> D I G	E <small>È</small> D JI	HEH	I <small>È</small> I
I <small>H</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small>	€	F <small>È</small> UI
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small>	F <small>È</small> UI	G <small>È</small> J
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small> J	G <small>È</small> J	I <small>È</small> I
I <small>I</small>	T <small>Ì</small> J	Y	E <small>È</small>	E <small>È</small> F	€	F <small>È</small> F <small>Ì</small>
I <small>I</small>	T <small>Ì</small> J	Y	E <small>È</small> F	E <small>È</small> I	F <small>È</small> F <small>Ì</small>	G <small>È</small> H
I <small>I</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small> D I I	È	I <small>È</small> I
I <small>J</small>	T <small>Ì</small> F	Y	E <small>È</small> D I I	E <small>È</small>	È	J <small>È</small> I
I <small>€</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small>	J <small>È</small> I	F <small>È</small> JG
I <small>F</small>	T <small>Ì</small> F	Y	E <small>È</small>	E <small>È</small> H	F <small>È</small> JG	FFJ <small>Ì</small>
I <small>G</small>	T <small>Ì</small> F	Y	E <small>È</small> H	E <small>È</small> G	FFJ <small>Ì</small>	F <small>È</small> H
I <small>H</small>	T <small>Ì</small> I	Y	E <small>È</small> G	E <small>È</small>	€	F <small>È</small> I
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small>	F <small>È</small> I	G <small>È</small> I
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small> H	G <small>È</small>	H <small>È</small> G
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small> H	E <small>È</small> D H	H <small>È</small> G	I <small>È</small> I
I <small>I</small>	T <small>Ì</small> I	Y	E <small>È</small> D H	I <small>È</small> ^H	I <small>È</small> I	I <small>È</small> G
I <small>I</small>	T <small>Ì</small> FH	Y	E <small>È</small> I	E <small>È</small>	€	E <small>È</small> G
I <small>J</small>	T <small>Ì</small> G	Y	E <small>È</small> G	E <small>È</small> G	€	È
J <small>€</small>	T <small>Ì</small> H	Y	E <small>È</small> D JI	E <small>È</small>	€	ÈHH
JF	T <small>Ì</small> H	Y	E <small>È</small>	E <small>È</small> I	ÈHH	ÈII
JG	T <small>Ì</small> H	Y	E <small>È</small> I	E <small>È</small> I	ÈII	F <small>È</small> H
JH	T <small>Ì</small> H	Y	E <small>È</small> I	E <small>È</small>	F <small>È</small> H	F <small>È</small> HH
JI	T <small>Ì</small> H	Y	E <small>È</small>	E <small>È</small> H	F <small>È</small> H	G <small>È</small> II
JÍ	T <small>Ì</small> I	Y	E <small>È</small> D I J	E <small>È</small>	€	È
JÍ	T <small>Ì</small> I	Y	E <small>È</small>	E <small>È</small> J	È	F <small>È</small> E
JÍ	T <small>Ì</small> I	Y	E <small>È</small> J	E <small>È</small>	F <small>È</small>	G <small>È</small> E

A Ya VYf'8 JglfJvI HYX' @ UXg fb @ & 6 @ %HfUbglYbh5 f YU @ UXgLfr c bhjbi YXL

T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>	Ó <small>ó</small>
J <small>i</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
J <small>jj</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>ee</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>ef</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>eg</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>eh</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>e</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>f</small>	T <small>f</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>é</small>	T <small>f</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>é</small>	T <small>f</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>é</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>
F <small>é</small>	T <small>í</small>	Ö <small>ö</small>	Ü <small>ü</small>	Á <small>á</small>	É <small>é</small>	Í <small>í</small>

A Ya VYf'8 Jghf]Vi hYX'@ UXg'f6 @' & '6 @' ; HfUbglYbh5 f YU'@ UXg'f

T ^{ à^{\circ} \& ö^{\circ}}		Öö^{\circ} & ö^{\circ}	Üü^{\circ} ö^{\circ} ð^{\circ} ä^{\circ} å^{\circ} ũ^{\circ} ö^{\circ}	Öö^{\circ} å^{\circ} ð^{\circ} ä^{\circ} å^{\circ} ũ^{\circ} ö^{\circ}	Üü^{\circ} ö^{\circ} & ö^{\circ}	žž^{\circ} á^{\circ}	Öö^{\circ} å^{\circ} ö^{\circ} & ö^{\circ}	žž^{\circ} á^{\circ}
F	TH	Ý	EEH	EECH	EEH	EEH	EEH	EEH
G	TH	Ý	EECH	EEG	EEH	EEH	EEH	EEH
H	TH	Ý	EEG	EEG	EEH	JEEH	EEG	EEH
I	TH	Ý	EEG	EEF	EEH	FEJG	FFEJ	EEH
Í	TH	Ý	EEF	EEF	EEH	FFEJ	FH	EEH
Î	TÎ	Ý	EEH	EECHFH	EEH	EEH	EEH	EEH
Ï	TÎ	Ý	EECHFH	EEG	EEH	EEH	EEH	EEH
Ì	TÎ	Ý	EEG	EECH	EEH	JEEH	EEG	EEH
J	TÎ	Ý	EECH	EEG	EEH	FEJG	FFEJ	EEH
F€	TÎ	Ý	EEG	EEF	EEH	FFEJ	FH	EEH
FF	TG	Ý	EEH	EEH	EEH	€	EGG	EEH
FG	TII	Ý	EEcd G	EECH	EEH	€	EE	EEH
FH	TII	Ý	EECH	EEC	EEH	EE	FE	EEH
FI	TII	Ý	EEC	EEC	EEH	FE	GE	EEH
FÍ	TII	Ý	EEC	EEH	EEH	GE	HEG	EEH
FÎ	TII	Ý	EECH	EEcd J	EEH	HIG	-	EEH
FÏ	TII	Ý	EEF	EEF	EEH	€	EE	EEH
FJ	TII	Ý	EECH	EEC	EEH	EEHH	EEII	EEH
G€	TII	Ý	EEC	EEC	EEH	EEII	FEH	EEH
GF	TII	Ý	EEC	EEC	EEH	FEH	FEHH	EEH
GG	TII	Ý	EEC	EEF	EEH	FEHH	GEII	EEH
GH	TÎJ	Ý	EEcd U	EEcd F	EEH	€	EEHI	EEH
G	TÎJ	Ý	EEcd F	EEcd G	EEH	EEII	FEII	EEH
G	TÎJ	Ý	EEcd G	EEcd I	EEH	EEII	GEFF	EEH
G	TÎJ	Ý	EEcd I	EEcd H	EEH	GEFF	HEHI	EEH
G	TÎJ	Ý	EEcd H	EEcd II	EEH	HEHI	I EII	EEH
G	TÎJ	Ý	EEG	EEG	EEH	HEII	I EII	EEH
GJ	TÎ FOE	Ý	EECH	EEH	EEH	GI	FE	EEH
H€	TÎ J	Ý	EEG	EEG	EEH	EEF	FEF	EEH
HF	TÎ OOE	Ý	EECH	EEH	EEH	EGF	FEIG	EEH
HG	TH	Ý	EEG	EEH	EEH	HB	FEH	EEH
HH	TH	Ý	EECH	EEH	EEH	IEH	IEII	EEH
H	TH	Ý	EEC	EEH	EEH	IEII	JEE	EEH
H	TÎ €	Ý	EEC	EEH	EEH	€	EEF	EEH
H	TÎ OOE	Ý	EEC	EEH	EEH	EH	HEG	EEH

A Ya VYf'8 JglfJvI HYX @ UXg f6 @ & 6 @ , HfUbglYbh5 f YU @ UXgLfr c bhjbi YXL

A Ya VYf'8 JglfJvI HYX @ UXg fb @ & 6 @ , HfUbglYbh5 f YU @ UXgLfr c bhjbi YXL

T <small>À</small> T <small>Á</small>	T <small>Í</small> G	Ö <small>Å</small> & Ö	Ü <small>Ü</small> Ö <small>Ö</small>	À <small>À</small> Á <small>Á</small> Ä <small>Ä</small> Ö <small>Ö</small>	À <small>À</small> Á <small>Á</small> Ä <small>Ä</small> Ö <small>Ö</small>	Ü <small>Ü</small> Ö <small>Ö</small> & Ö	Ž <small>Ž</small> Á	Ö <small>Ö</small> Å <small>Å</small> & Ö	Ž <small>Ž</small> Á
Í J	TÍG	Ý	EEF	EEF	EEF	€	Ě		
J€	TÍH	Ý	EEEGU	EECH	EECH	€	ĚHH		
JF	TÍH	Ý	EECH	EECH	EECH	€	ĚHH		
JG	TÍH	Ý	EECH	EECH	EECH	€	ĚHH		
JH	TÍH	Ý	EECH	EECH	EECH	F	FHH		
JI	TÍH	Ý	EECH	EECF	EECF	FĚHH	GĚI		
JÍ	TÍI	Ý	EECH H	EECH	EECH	€	Ě		
JÍ	TÍI	Ý	EECH	EECI	EECI	€	FĚ		
JÍ	TÍI	Ý	EECI	EECI	EECI	FĚ	GĚ		
JÌ	TÍI	Ý	EECI	EECH	EECH	GĚ	HĚG		
JJ	TÍI	Ý	EECH	EECD J	EECD J	HĚG	I		
F€€	TÍI	Ý	EECH H	EECH F	EECH F	€	ĚH		
F€F	TÍI	Ý	EECH F	EECD FF	EECD FF	€	FĚII		
F€G	TÍI	Ý	EECD FF	EECD FJ	EECD FJ	FĚII	GĚFF		
F€H	TÍI	Ý	EECD FJ	EECH J	EECH J	GĚFF	HĚII		
F€	TÍI	Ý	EECH J	EECH G	EECH G	HĚII	I		
F€	TF	Ý	EECI	EECI	EECI	HĚ	I		
F€	TF	Ý	EECI	EECH	EECH	I	ĚHH		
F€	TF	Ý	EECH	EECG	EECG	I	ĚII	J	
F€	TÍI	Ý	EECI	EECI	EECI	€	FĚH		
F€	TÍI	Ý	EECI	EECH	EECH	FĚH	HĚG		

9bj YcdY>cJbhFYUWcbg

Rāc	ÝÁá	ŠÓ	ÝÁá	ŠÓ	ZÁá	ŠÓ	TÝÁÉá	ŠÓ	TÝÁÉá	ŠÓ	TZÁÉá	ŠÓ		
F	PÍJ	{ æ	田€J	Í	FÙ€	FJ	IÈÍÍ	Í	FÈ€	FH	ÈÍÍ	I	ÈÍ	FG
G		{ à	田ÈÍÍ	G	ÈÍ	FH	È€J	Í	È€ÍÍ	Í	田HG	F€	È€ÍÍ	Í
H	PÍÍ	{ æ	田GH	Í	FÙÍ	FÍ	ÈÍÍ	G	ÈÍH	FH	È€F	G	ÈÍJÍ	FG
I		{ à	田ÈÍ	GH	ÈÍÍ	FG	田ÍÍ	Í	田JF	Í	田ÍG	I	田ÈÍF	Í
J	PÍÍ	{ æ	ÈÍÍ	H	FÙÍJ	FI	ÈÍG	G	ÈÍÍI	G	ÈÍG	FG	ÈÍF	J
K		{ à	田ÈÍÍ	J	ÈÍF	I	ÈÍÍÍ	Œ	ÈÍÍÍ	I	田II	FÍ	ÈÍÍÍ	H
L	PÍF	{ æ	FÈÍG	Í	FÙÍFF	FI	ÈÍÍÍ	G	HEÍG	G	ÈÍH	GG	FÈÍG	FH
M		{ à	田JÍ	FH	ÈÍHG	I	ÈÍÍÍ	Œ	ÈÍÍFG	I	田HÍ	I	田HÍ	Í
N	PÍH	{ æ	ÍÈ	FÍ	FÈÍÍ	GG	ÈÍÍG	G	ÈÍG	H	ÈÍÍ	I	GEÍÍ	F€
O		{ à	ÈÍÍ	FF	È€G	I	田ÍF	Í	田ÍÍ	J	田€F	G	ÈÍÍÍ	I
P	PÍÍ	{ æ	HÈÍÍ	FÍ	FÙÍÍ	GF	IÈ€G	FÍ	FÈ	H	È€H	I	GEÍI	F€
R	FG	{ à	ÈÍH	F€	ÈÍJF	H	ÈÍG	J	È€ÍHG	J	田GJ	FG	田JG	I
S	FH	VÍCÍK	{ æ	ÍÈG	Í	ÍÈÍÍ	FÍ	ÍÈÍÍ	G					
T	FI		{ à	ÈÍÈG	FF	HÈÍH	F€	ÈÍÍÍ	I					

9bj YcdY5=G7 % H fl \* \$!%\* £ @: 8 GhYY 7cXY7\ YWg

T	A	U	O	S	S	S	S	S	F	G	H	I	J	K	L	M	N	O
F	T H E	Ú Ó Ó G E	É É G	I È È I	F H	È È F	I È È I	F G	G H È È J	H G È F H	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G
G	T G G	Ú Ó Ó G E	É È I	I È È I	J	È È G E	I È È I	I	G H È È J	H G È F H	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G
H	T F I	Ú Ó Ó G E	É F I	I È È I	J	È È F	I È È I	F H	F I È È I	H G È F H	F È È G	F È È G	G	F I È È I	H G È F H	F È È G	F È È G	F È È G
I	T G I	Ú Ó Ó G E	É J J	I È È I	F H	È È F J	I È È I	G	F I È È I	H G È F H	F È È G	F È È G	F È È G	F I È È I	H G È F H	F È È G	F È È G	F È È G
Í	T F I	Ú Ó Ó G E	È È I	I È È I	Í	È È F	I È È I	I	G H È È J	H G È F H	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G	F È È G
Í	T Í	Š H Y H Y Í	È G	É I G	G	È È I	H È D	^	F H	È È F G	I È È I	G È È	I È È G	F È È P G F	I È È G	F È È P G F	I È È G	F È È P G F
Í	T H	Š H Y H Y Í	È F I	É I G	G	È È I J	H È D	:	H	È È F G	I È È I	G È È	I È È J	F È È P G F	I È È J	F È È P G F	I È È J	F È È P G F
Í	T F È	Ú Ó Ó G E	È È H	I È È I	F F	È È È	I È È I	I	F I È È I	H G È F H	F È È G	F È È G	G	F I È È I	H G È F H	F È È G	F È È G	F È È G

9bj YcdY5=G7 %& H fl \*\$!%&L @E:8 GhyY7cXY7\ YWg fTcbhbi YXt

T	A	U	O	S	S	U	S	S	C	U	C	U	C	C	C	
J	T	F	ŠHÝHÝ	ÈJ	ÈIG	J	ÈI	ÈI	H	Ì	ÌÈFG	ÌÈH	ÈH	IÈIJ	FEPGF	
F€	T	J€	ŠGÉGÉ	ÈJ	FEI	G	ÈE	ÈE	^	FH	HÈG	HÈI	FEFI	GÈH	GPGF	
FF	T	H	PÙUHÉY	ÈF	FEI	FH	ÈJ	FEI	:	F€	FFJE	FEI	FEFI	FGÉ	FPFÈF	
FG	T	I	ÚQÓGÉ	ÈI	ÈIF	G	ÈI	ÈI	FH	ÌÈGJ	HÈFH	FEIG	FEIG	HÈF	GPGF	
FH	T	I	ÚQÓGÉ	ÈHE	FFÈI	J	ÈI	FFÈE	J	ÌÈGJ	HÈFH	FEIG	FEIG	HÈF	GPGF	
FI	T	I	H	ÈHE	FEI	H	ÈH	FEI	:	Ì	FFJE	FEI	FEFI	FGÉ	FPFÈF	
FÍ	T	I	J	SGÉGÉ	ÈG	È	G	ÈEH	È	J	HÈG	HÈI	FEFI	GÈH	GPGF	
FÍ	T	I	J	ÚQÓGÉ	ÈFG	ÈI	F	J	ÈGF	FFÈE	G	ÌÈGJ	HÈFH	FEIG	FEIG	GPGF
FÍ	T	H	PÙUHÉY	ÈFE	FEI	J	ÈI	FEI	^	FF	FFJE	FEI	FEFI	FGÉ	FPFÈF	
FÍ	T	I	F	PÙUHÉY	ÈGJ	FEI	ÈI	FEI	^	Ì	FFJE	FEI	FEFI	FGÉ	FPFÈF	
FJ	T	H	PÙUHÉY	ÈGJ	FEI	ÈI	ÈJ	FEI	^	Í	FFJE	FEI	FEFI	FGÉ	FPFÈF	
G€	T	H	PÙUHÉY	ÈGJ	FEI	ÈI	FEI	FEI	^	J	FFJE	FEI	FEFI	FGÉ	FPFÈF	
GF	T	J	SGÉGÉ	ÈGJ	FEI	ÈI	ÈI	ÈI	È	Í	HÈG	HÈI	FEFI	GÈH	GPGF	
GG	T	F	ÚQÓGÉ	ÈGJ	FEI	ÈI	ÈJ	ÈGF	ÈI	JH	ÈI	ÈI	FEIG	FEIG	GPGF	
GH	T	H	ÚQÓGÉ	ÈGJ	FEI	ÈI	ÈG	ÈHG	ÈI	H	GÈEJ	HÈFH	FEIG	FEIG	GPGF	
G	T	I	ÚQÓGÉ	ÈGU	FEI	ÈI	FEI	ÈGF	ÈI	J	FIEI	HÈFH	FEIG	FEIG	GPGF	
GÍ	T	H	SGYGYEGG	ÈGI	GEI	FH	ÈH	GEI	ÈI	FH	GFÈH	GÈJI	ÈHF	FE GH	GPGF	
GÍ	T	G	ÚQÓGÉ	ÈGI	FEI	ÈI	ÈJ	FEI	ÈI	Í	FEI	ÈI	HÈFH	FEIG	FEIG	GPGF
GÍ	T	I	J	SGYGYEGG	ÈGI	GEI	J	ÈH	È	J	GFÈH	GÈJI	ÈHF	FE GH	GPGF	
GÍ	T	G	H	ÚQÓGÉ	ÈGI	FEI	ÈI	FEI	ÈI	FG	GÈEJ	HÈFH	FEIG	FEIG	GPGF	
GJ	T	F	ÚQÓGÉ	ÈGH	FEI	ÈI	ÈI	ÈI	ÈI	Í	GÈEJ	HÈFH	FEIG	FEIG	GPGF	
HE	T	I	SGYGYEGG	ÈGJ	HEG	I	FEI	FEI	È	FF	FIEI	HÈJI	ÈHF	FE GG	GPGF	
HF	T	I	H	SGYGYEGG	ÈGJ	HEG	I	GG	FEI	ÈGJ	: J	FIEI	HÈJI	ÈHF	FE GH	GPGF
HG	T	I	J	SGYGYEGG	ÈJG	GEI	I	FEI	FEI	FF	FFÈH	GÈJI	ÈHF	FEI	GPGF	
HH	T	I	I	SGYGYEGG	ÈJF	GEI	Í	ÈG	È	Í	GFÈH	GÈJI	ÈHF	FE GH	GPGF	
HI	T	I	E	SGYGYEGG	ÈJF	GEI	I	FEI	È	H	FJÈI	GÈJI	ÈHF	FE GH	GPGF	
HÍ	T	H	I	PÙUIYIYI	ÈJF	GEI	G	ÈI	FEI	F	FHÈI	FHÈF	ÈHF	FEI	GPGF	
HÍ	T	I	F	SGYGYEGG	ÈJF	È	G	ÈF	È	FH	ÈI	FHÈF	ÈHF	FE GH	GPGF	
HÍ	T	I	J	SGYGYEGG	ÈJF	È	J	ÈG	È	G	ÈI	ÈI	J	GFÈH	GÈJI	ÈHF
I€	T	I	I	SGYGYEGG	ÈJF	È	J	ÈI	È	ÈEJ	ÈI	ÈI	ÈHF	FE GH	GPGF	
IF	T	I	F	SGYGYEGG	ÈJF	È	J	ÈI	È	ÈEJ	ÈI	ÈI	H	FFÈH	GÈJI	ÈHF
IG	T	I	O	SGYGYEGG	ÈJF	FEF	G	ÈFG	FEF	: F	FGÈG	GÈJI	ÈHF	FE GH	GPGF	
IH	T	I	G	SGYGYEGG	ÈJG	È	FH	ÈI	È	FH	ÈF	ÈI	J	GFÈH	GÈJI	ÈHF
II	T	H	G	PÙUIYIYI	ÈJF	È	J	ÈI	È	ÈF	ÈI	ÈI	FF	FHÈI	FHÈF	ÈHF
II	T	I	I	SGYGYEGG	ÈJF	È	H	ÈI	È	ÈE	ÈI	ÈI	ÈHF	FE F	GPGF	
II	T	I	I	SGYGYEGG	ÈJF	È	H	ÈI	È	ÈE	ÈI	ÈI	ÈHF	FE F	GPGF	
II	T	H	I	PÙUIYIYI	ÈJF	È	H	ÈI	È	ÈF	ÈI	ÈI	ÈHF	FE F	GPGF	
II	T	I	E	PÙUIYIYI	ÈHH	ÈF	I	ÈI	È	ÈF	ÈI	ÈI	ÈHF	FE F	GPGF	
IJ	T	H	I	PÙUIYIYI	ÈGG	ÈF	FF	ÈI	È	ÈF	ÈI	ÈI	J	FHÈI	FHÈF	ÈHF
I€	T	I	I	SGYGYEGG	ÈFF	È	F	ÈE	È	ÈE	ÈI	ÈI	ÈHF	FE GH	GPGF	
IF	T	I	E	SGYGYEGG	ÈEG	È	F	ÈE	È	ÈE	ÈI	ÈI	ÈHF	FE GH	GPGF	
IG	T	I	I	SGYGYEGG	ÈJ	È	GG	ÈE	È	ÈI	ÈI	ÈI	ÈHF	FE GH	GPGF	
IH	T	I	I	ŠYIYI	ÈEJ	È	I	ÈE	È	ÈGJ	È	FHÈJG	FHÈJG	ÈHF	FE E	GPGF
II	T	G	I	ŠYIYI	ÈEJ	È	GJ	ÈJ	È	ÈE	ÈGJ	È	J	FHÈJG	FHÈJG	ÈHF
II	T	I	I	ŠYIYI	ÈEJ	È	G	ÈE	È	ÈGJ	È	FHÈJG	FHÈJG	ÈHF	FE E	GPGF

## **APPENDIX B**

(Force calculation tables)

## INPUT

[REF: ANSI/TIA-222-H]

Tower Type	:	MP		
Tower Height	:	150	ft	
Mount Elevation	:	126	ft	
Antenna Elevation	:	127	ft	
Crest Height	:	0	ft	
Risk Category	:	II		[Table 2-1 ]
Exposure Category	:	C		[Sec. 2.6.5.1.2]
Topography Category	:	1		[Sec. 2.6.6.2]
Wind Velocity	V	118	mph	[Annex B ]
Ice wind Velocity	V <sub>i</sub>	50	mph	[Annex B ]
Service Velocity	V <sub>s</sub>	30	mph	[Annex B ]
Base Ice thickness	t <sub>i</sub>	1	in	[Annex B ]

## ANTENNAS

	Manufacturer	Model	Height (in)	Front Width (in)	Side Width (in)	Weight (lbs)	Shape	Quantity	Location (%)
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Mount Pipe M15

**Mount Pipe**

Mount Pipe

**Mount Pipe** **M35**

Mount Pipe M31

Powerwave	7770	55.00	11.00	5.00	35.00	Flat	0.5	5
Powerwave	7770	55.00	11.00	5.00	35.00	Flat	0.5	95
Powerwave	LGP 21401	14.40	2.60	9.20	14.10	Flat	2	65

Mount Pipe M30

PROJECT	<b>130656.002.01 - FAIRFIELD C</b>	SP
SUBJECT	<b>Platform Mount - Mount Analysis</b>	
DATE	<b>02/08/19</b>	PAGE OF



**B+T Group**  
 1717 S. Boulder, Suite 300  
 Tulsa, OK 74119  
 (918) 587-4630

**B+T GRP**

Manufacturer	Model	Qty	Aspect Ratio	C <sub>a</sub> flat/round	A <sub>A</sub> (ft <sup>2</sup> ) Normal	A <sub>A</sub> (ft <sup>2</sup> ) Trans.	A <sub>A-Ice</sub> (ft <sup>2</sup> ) Normal	A <sub>A-Ice</sub> (ft <sup>2</sup> ) Trans.	F <sub>A</sub> No Ice (N)	F <sub>A</sub> No Ice (T)	F <sub>A</sub> Ice (N)	F <sub>A</sub> Ice (T)
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.12	0.07	0.02	0.01
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.12	0.07	0.02	0.01
Powerwave	LGP 21401	2	5.54	1.34	0.52	1.84	1.13	2.66	0.03	0.10	0.01	0.02
<hr/>												
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.31	0.13	0.06	0.02
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.31	0.13	0.06	0.02
ERICSSON	B5/B12 4449	1	1.43	1.20	1.08	1.37	1.52	1.85	0.06	0.07	0.01	0.01
ERICSSON	4415 B30	1	3.07	1.23	0.62	1.55	1.00	2.06	0.03	0.08	0.01	0.02
<hr/>												
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.22	0.15	0.04	0.03
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.22	0.15	0.04	0.03
<hr/>												
RAYCAP	DC6-48-60-18-8F	1	2.84	0.51	2.39	2.39	3.09	3.09	0.05	0.05	0.01	0.01
<hr/>												
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.12	0.07	0.02	0.01
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.12	0.07	0.02	0.01
Powerwave	LGP 21401	2	5.54	1.34	0.52	1.84	1.13	2.66	0.03	0.10	0.01	0.02
<hr/>												
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.31	0.13	0.06	0.02
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.31	0.13	0.06	0.02
ERICSSON	B5/B12 4449	1	1.43	1.20	1.08	1.37	1.52	1.85	0.06	0.07	0.01	0.01
ERICSSON	4415 B30	1	3.07	1.23	0.62	1.55	1.00	2.06	0.03	0.08	0.01	0.02

PROJECT	130656.002.01 - FAIRFIELD C		
SUBJECT	Platform Mount - Mount Analysis		
DATE	02/08/19	PAGE	OF



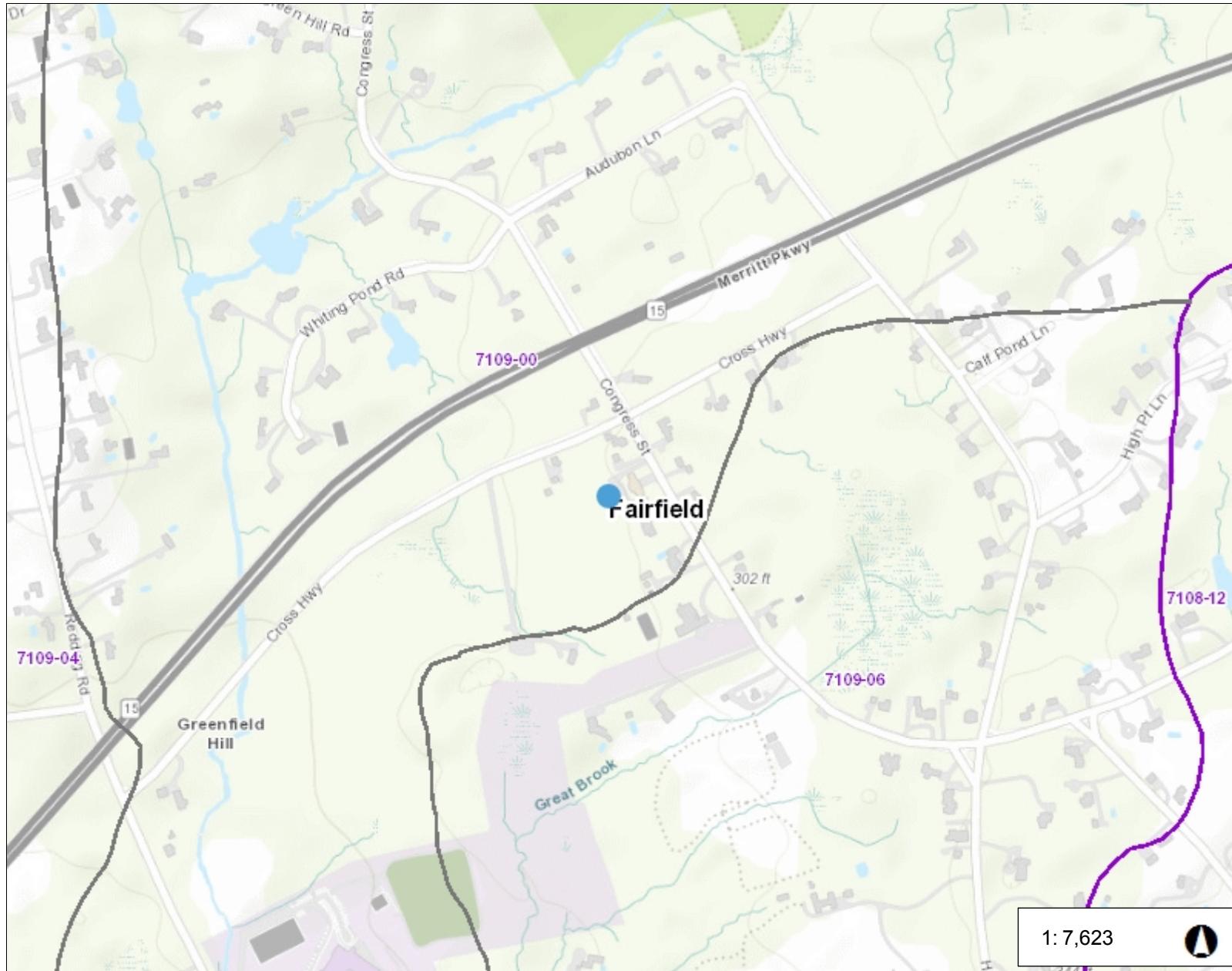
**B+T Group**  
1717 S. Boulder, Suite 300  
Tulsa, OK 74119  
(918) 587-4630

Manufacturer	Model	Qty	Aspect Ratio	C <sub>a</sub> flat/round	A <sub>A</sub> (ft <sup>2</sup> ) Normal	A <sub>A</sub> (ft <sup>2</sup> ) Trans.	A <sub>A-Ice</sub> (ft <sup>2</sup> ) Normal	A <sub>A-Ice</sub> (ft <sup>2</sup> ) Trans.	F <sub>A</sub> No Ice (N)	F <sub>A</sub> No Ice (T)	F <sub>A</sub> Ice (N)	F <sub>A</sub> Ice (T)
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.00	0.15	0.04	0.03
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.00	0.15	0.04	0.03
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.00	0.07	0.02	0.01
Powerwave	7770	0.5	5.00	1.31	2.10	0.95	2.64	1.45	0.00	0.07	0.02	0.01
Powerwave	LGP 21401	2	5.54	1.34	0.52	1.84	1.13	2.66	0.00	0.10	0.01	0.02
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.00	0.13	0.06	0.02
Kathrein	800-10965	0.5	3.94	1.26	5.47	1.89	6.27	2.58	0.00	0.13	0.06	0.02
ERICSSON	B5/B12 4449	1	1.43	1.20	1.08	1.37	1.52	1.85	0.00	0.07	0.01	0.01
ERICSSON	4415 B30	1	3.07	1.23	0.62	1.55	1.00	2.06	0.00	0.08	0.01	0.02
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.00	0.15	0.04	0.03
CCI	HPA-65R-BUU-H6	0.5	4.86	1.31	3.70	2.25	4.41	2.91	0.00	0.15	0.04	0.03



# Town of Fairfield

3965 CONGRESS ST



## Legend

Local Basin Boundary

- Major
- Regional
- Subregional
- Local

Local Basin Area

Town Boundary

1,270.5                  0                  635.23                  1,270.5 Feet

WGS\_1984\_Web\_Mercator\_Auxiliary\_Sphere  
Created by Greater Bridgeport Regional Council

This map is a user generated static output from an Internet mapping site and is for reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable.  
THIS MAP IS NOT TO BE USED FOR NAVIGATION

## **3965 CONGRESS STREET**

**Location** 3965 CONGRESS STREET

**Mblu** 170/ 41/ / /

Acct# 05308

**Owner** FAIRFIELD TOWN OF

**Assessment** \$939,330

**Appraisal** \$1,341,900

**PID** 14189

**Building Count** 1

### **Current Value**

<b>Appraisal</b>			
<b>Valuation Year</b>	<b>Improvements</b>	<b>Land</b>	<b>Total</b>
2017	\$508,400	\$833,500	\$1,341,900
<b>Assessment</b>			
<b>Valuation Year</b>	<b>Improvements</b>	<b>Land</b>	<b>Total</b>
2017	\$355,880	\$583,450	\$939,330

**Owner of Record**

**Owner** FAIRFIELD TOWN OF  
**Co-Owner**  
**Address** 725 OLD POST ROAD  
FAIRFIELD, CT 06824

**Sale Price** \$0  
**Certificate**  
**Book & Page** 395/ 523  
**Sale Date**

#### **Ownership History**

Ownership History				
Owner	Sale Price	Certificate	Book & Page	Sale Date
FAIRFIELD TOWN OF	\$0		395/ 523	

## **Building Information**

Building 1 : Section 1

<b>Year Built:</b>	1959
<b>Living Area:</b>	3,848
<b>Replacement Cost:</b>	\$670,756
<b>Building Percent Good:</b>	60
<b>Replacement Cost Less Depreciation:</b>	\$402,500

**Building Attributes**

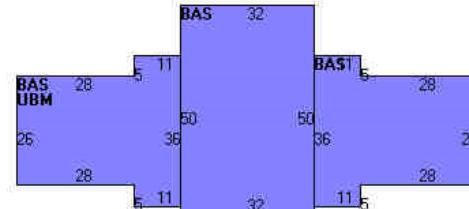
Building Attributes	
Field	Description
STYLE	Fire Station
MODEL	Ind/Comm
Stories:	1
Occupancy	1
Exterior Wall 1	Vinyl Siding
Exterior Wall 2	Brick/Masonry
Roof Structure	Gable/Hip
Roof Cover	Asphalt
Interior Wall 1	Minim/Masonry
Interior Wall 2	Plywood Panel
Interior Floor 1	Concr-Finished
Interior Floor 2	Vinyl/Asphalt
Heating Fuel	Gas
Heating Type	Hot Water
AC Type	None
Bldg Use	Fire Dept
Total Rooms	
Total Bedrms	00
Total Baths	0
Liv Area	
Effect Area	
1st Floor Use:	9032
Heat/AC	None
Frame Type	Masonry
Baths/Plumbing	Average

## **Building Photo**



(<http://images.vgsi.com/photos2/FairfieldCTPhotos/\02\03\13\91.jpg>)

## **Building Layout**



(<http://images.vgsi.com/photos2/FairfieldCTPhotos//Sketches/14>)

**Building Sub-Areas (sq ft)**

Building Sub Areas (sq ft)			
Code	Description	Gross Area	Living Area
BAS	First Floor	3,848	3,848
UBM	Basement, Unfinished	1,124	0

## **Extra Features**

Extra Features				
Code	Description	Size	Value	Bldg #

SPR1	SPRINKLERS-WET	4972 S.F.	\$6,900	1
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## Land

Land Use		Land Line Valuation	
Use Code	9032	Size (Acres)	1.2
Description	Fire Dept	Depth	0
Zone		Assessed Value	\$583,450
Neighborhood	C6	Appraised Value	\$833,500
Alt Land Appr	No		
Category			

## Outbuildings

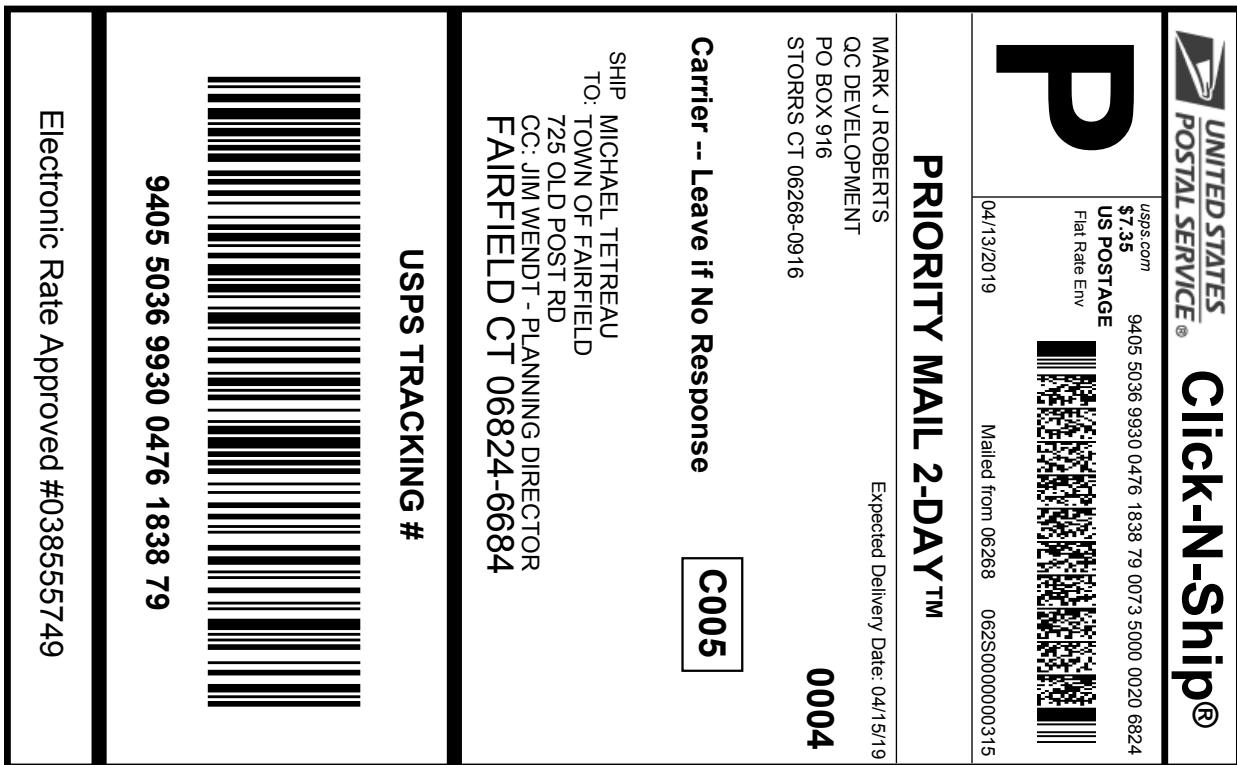
Outbuildings					Legend	
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
PAV1	PAVING-ASPHALT			5000 S.F.	\$15,800	1
LT1	LIGHTS-IN W/PL			1 UNITS	\$700	1
SHD2	W/LIGHTS ETC			80 S.F.	\$1,200	1
GEN1	GENERATOR			1 UNITS	\$10,000	1
SHD5	CELL SHED			300 SF	\$16,200	1
SHD5	CELL SHED			300 SF	\$16,200	1
SHD5	CELL SHED			300 SF	\$16,200	1
SHD5	CELL SHED			300 SF	\$16,200	1
FN4	FENCE-8' CHAIN			600 L.F.	\$6,500	1

## Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2018	\$508,400	\$833,500	\$1,341,900
2017	\$508,400	\$833,500	\$1,341,900
2016	\$508,400	\$833,500	\$1,341,900

Assessment			
Valuation Year	Improvements	Land	Total
2018	\$355,880	\$583,450	\$939,330
2017	\$355,880	\$583,450	\$939,330
2016	\$355,880	\$583,450	\$939,330

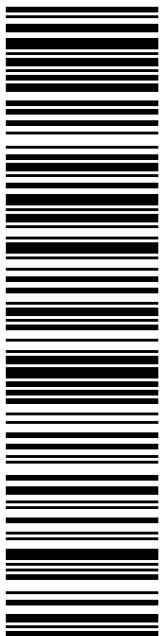
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—X— *Cut on dotted line.*

## Instructions

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2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.



**9405 5036 9930 0476 1838 79**

Electronic Rate Approved #038555749

## Click-N-Ship® Label Record

**USPS TRACKING #:**  
**9405 5036 9930 0476 1838 79**

Trans. #:	461509641	Priority Mail® Postage:	\$7.35
Print Date:	04/12/2019	Total	\$7.35
Ship Date:	04/13/2019		
Expected			
Delivery Date:	04/15/2019		

**From:** MARK J ROBERTS  
QC DEVELOPMENT  
PO BOX 916  
STORRS CT 06268-0916

**To:** MICHAEL TETREAU  
TOWN OF FAIRFIELD  
725 OLD POST RD  
CC: JIM WENDT - PLANNING DIRECTOR  
FAIRFIELD CT 06824-6684

\* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.



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