



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

December 19, 2000

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

Sandy M. Carter
Verizon Wireless
20 Alexander Drive
P.O. Box 5029
Wallingford, CT 06492

RE: **TS-VER-039-001117** - Cellco Partnership d/b/a Verizon Wireless request for an order to approve tower sharing at an existing telecommunications facility located at 35 Old Route 44, Eastford, Connecticut.

Dear Ms. Carter:

At a public meeting held December 14, 2000, the Connecticut Siting Council (Council) ruled that the shared use of this existing tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility to avoid the unnecessary proliferation of tower structures. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

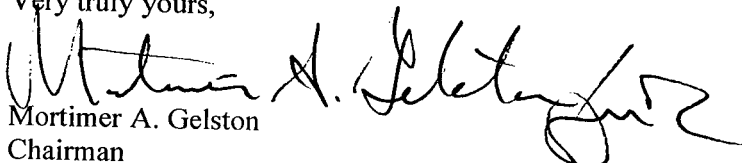
This decision is under the exclusive jurisdiction of the Council. Any additional change to this facility may require an explicit request to this agency pursuant to General Statutes § 16-50aa or notice pursuant to Regulations of Connecticut State Agencies Section 16-50j-73, as applicable. Such request or notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

This decision applies only to this request for tower sharing and is not applicable to any other request or construction.

The proposed shared use is to be implemented as specified in your letter dated November 16, 2000.

Thank you for your attention and cooperation.

Very truly yours,


Mortimer A. Gelston
Chairman

MAG/FOC/laf

c: Honorable Richard L. Woodward, First Selectman, Town of Eastford
Robert J. Francis, Cordless Data Transfer, Inc.
Ronald C. Clark, Nextel Communications
Julie M. Cashin, Esq., Hurwitz & Sagarin, LLC

Network Dept.

RECEIVED

NOV 17 2000

CONNECTICUT
SITING COUNCIL



verizon wireless

Verizon Wireless
20 Alexander Drive
Wallingford, Connecticut 06492

November 16, 2000

Mr. Mortimer A. Gelston, Chairman
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

HAND DELIVERED

Re: **Request by Cellco Partnership d/b/a Verizon Wireless for an Order to Approve the Shared Use of a Tower Facility located at 35 Old Route 44, Eastford, Connecticut.**

Dear Chairman Gelston:

Pursuant to Connecticut General Statutes (C.G.S.) Sec. 16-50aa, Cellco Partnership d/b/a Verizon Wireless hereby requests an order from the Connecticut Siting Council ("Council") to approve the proposed shared use by Verizon Wireless of an existing tower located at 35 Old Route 44, Eastford, Connecticut. The property is owned by Priscilla Armitage and the tower is owned by Cordless Data Transfer which is located in Marlborough, Connecticut. As shown on the attached drawing and as further described below, Verizon Wireless proposes to install antennas on the existing tower and to locate an equipment shelter at the base of the tower. Verizon Wireless requests that the Council finds that the proposed shared use of the tower facility satisfy the criteria stated in C.G.S. Sec. 16-50aa, and to issue an order approving the proposed shared use.

Background

Verizon Wireless is licensed by the Federal Communications Commission to provide cellular telephone service in the Windham County New England County Metropolitan Area (NECMA), which includes the area to be served by the proposed Eastford installation.

The facility at 35 Old Route 44 in Eastford, consists of an approximately 193 foot AGL guyed steel tower built by Cordless Data Transfer. The guyed tower can structurally support multiple carriers and there other carriers located on the tower which are shown on the attached site plan. Verizon Wireless and Cordless Data transfer have agreed to the proposed-shared use of this tower pursuant to mutually acceptable terms and conditions. Cordless data Transfer has authorized Verizon Wireless to apply for all necessary permits, approvals and authorizations which may be required for the proposed shared use of this facility.

Mr. Mortimer A. Gelston
November 16, 2000
Page 2

Verizon Wireless proposes to install twelve (12) Swedcom Model ALP-9011 antennas, approximately 43 inches in height, on a platform with their center of radiation at approximately 194 feet above ground level ("AGL"). Verizon Wireless will also install one (1) GPS antenna on the tower. Equipment associated with these antennas, as well as a 40 KW diesel-fueled emergency stand-by generator, would be located in a new approximately 12-foot x 30-foot equipment building located at the base of the tower.

C.G.S. Sec. 16-50aa provides that, upon written request for approval of a proposed shared use, "if the Council finds that the proposed shared use of the facility is technically, legally, environmentally and economically feasible and meets public safety concerns, the Council shall issue an order approving such shared use" (C.G.S. Sec. 16-50aa(c)(1).)

Discussion

A. Technical Feasibility. The existing tower is structurally sound and capable of supporting the proposed Verizon Wireless antennas. The tower will not require any structural modification to support the proposed attachments. Verizon Wireless engineers have determined that the proposed antenna installations present minimal potential for interference to or from existing radio transmissions from this location. In addition, the applicant is unaware of any occasion where its operations have caused interference with AM, FM or television reception. The proposed-shared use of this tower therefore is technically feasible. A copy of the structural analysis is attached to this application.

B. Legal Feasibility. Under C.G.S. Sec. 16-50aa, the Council has been authorized to issue an order approving the proposed-shared use of an existing communications tower facility such as the facility at 35 Old Route 44. (C.G.S. Sec. 16-50aa(c)(1).) This authority complements the Council's prior-existing authority under C.G.S. Sec. 16-50p to issue orders approving the construction of new towers that are subject to the Council's jurisdiction. C.G.S. Sec. 16-50x(a) directs the Council to "give consideration to other state laws and municipal regulations as it shall deem appropriate" in ruling on requests for the shared use of existing tower facilities. Under the authority vested in the Council by C.G.S. Sec. 16-50aa, an order by the Council approving the shared use would permit the applicant to obtain a building permit for the proposed installations.

C. Environmental Feasibility. The proposed shared use would have a minimal environmental effect, for the following reasons:

1. The proposed installations would have an insignificant incremental visual impact, and would not cause any significant change or alteration in the physical or environmental characteristics of the existing site. The addition of the proposed antennas would not increase the height of the tower, although a portion of the antennas themselves would extend above the tower. The proposed installation would not extend the boundaries of the tower site, including the placement of the equipment building near the base of the existing tower.

2. The proposed installation would not increase the noise levels at the existing facility by six decibels or more. The only additional noise will occur during emergency use or periodic exercising of the generator.

3. Operation of the additional antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base to a level at or above the applicable standard. "Worst-case" exposure calculation for a point at the base of the tower in relation to the operation of Verizon Wireless's and other existing antenna arrays are as follows:

	<u>Applicable ANSI Stnd</u>	<u>Calculated "Worst-Case"</u>	<u>Percentage of Stnd.</u>
Verizon Wireless	0.583 mW/cm ²	0.0181 mW/cm ²	3.11%
Nextel	0.5673 mW/cm ²	0.0117 mW/cm ²	2.05%
Sprint PCS	1.000 mW/cm ²	0.0149 mW/cm ²	<u>1.49%</u>
		Total	6.65%

The "worst-case" exposure would be only 6.65 % of the ANSI standard, as calculated for mixed frequency sites. Power density levels from shared use of the tower facility would thus be well below applicable ANSI standards

4. The proposed installations would not require any water or sanitary facilities, or generate discharges to water bodies. Operation of the emergency back-up generator will result in limited air emissions; pursuant to R.C.S.A. Section 22a-174-3, the generator will require the issuance of a permit from the Department of Environmental Protection Bureau of Air Management. After construction is complete, the proposed installation would not generate any traffic other than periodic maintenance visits.

The proposed use of this facility would therefore have a minimal environmental effect, and is environmentally feasible.

D. Economic Feasibility. As previously mentioned, the tower owner and the applicant have entered into a mutual agreement to share the use of the existing tower on terms agreeable to the parties, and the proposed tower sharing is thus economically feasible.

E. Public Safety Concerns. As stated above, the existing tower is structurally capable of supporting the proposed Verizon Wireless antennas. The Applicant is not aware of any other public safety concerns relative to the proposed tower sharing of the existing tower. In fact, the provision of new or improved cellular phone service in the Eastford area, including 5 miles of Route 44 and 3.5 miles of Route 198 and the surrounding area, through shared use of the tower is expected to enhance the safety and welfare of area residents and travelers. The public safety benefits of wireless service are further illustrated by the decision of local authorities elsewhere in Connecticut to provide cellular phones to residents to improve local public safety and emergency communications. The proposed-shared use of this facility would likewise improve public safety in the Eastford area.

Conclusion

For the reasons discussed above, the proposed shared use of the existing telecommunications tower facility at 35 Old Route 44 satisfies the criteria stated in C.G.S. Sec. 16-50aa, and advances the General Assembly's and the Council's goal of preventing the proliferation of towers in Connecticut. The Applicant therefore requests that the Council issue an order approving the proposed shared use.

Mr. Mortimer A. Gelston
November 16, 2000
Page 5

Thank you for your consideration of this matter.

Pursuant to Connecticut General Statutes Sec. 16-50v and Section 16-50v-1(a) of the Regulations of Connecticut State Agencies, Verizon Wireless has enclosed a check in the amount of \$500.00 for the required filing fee.

Respectfully yours,



Sandy M. Carter
Manager – Regulatory
Verizon Wireless

Attachments

cc: Honorable Richard Woodward, First Selectman

Network Dept.



Verizon Wireless
20 Alexander Drive
Wallingford, Connecticut 06492

November 16, 2000

Honorable Richard Woodward,
First Selectman
Town Office Building
16 Westford Road
Eastford, Connecticut 06242

Dear Mr. Woodward:

This letter is to inform you that Celco Partnership d/b/a Verizon Wireless plans to install antennas and associated equipment at the existing tower facility located at 35 Old Route 44, Eastford, Connecticut. I am enclosing a copy of Verizon Wireless's tower sharing application to the Connecticut Siting Council.

The application fully sets forth the Company's proposal. However, if you have any questions or require further information on our plans or the Siting Council's procedures, please contact me at (203) 294-8519 or Mr. Joel Rinebold, Executive Director of the Connecticut Siting Council at (860) 827-2935.

Sincerely,

A handwritten signature in cursive script that reads "Sandy M. Carter".

Sandy M. Carter
Manager- Regulatory
Verizon Wireless

Enclosure



P. O. Box 363
August 3, 2000

Marlborough, Connecticut 06447

(860) 295-0445 FAX -1473

Ms. Sandy M. Carter
Manager Regulatory
Verizon Wireless
20 Alexander Drive
P.O. Box 5029
Wallingford, Connecticut 06492-2430

RE: Eastford Tower (35 Old Route 44, Eastford, Connecticut)
VIA USPS Overnight Service

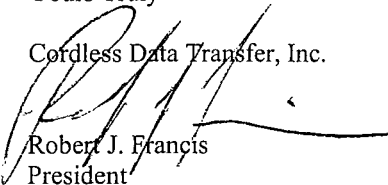
Dear Ms. Carter

Please consider this letter to be authorization to proceed with your installation of a wireless telephone facility at our tower site located at the above referenced address. I have included with this letter an original Connecticut Licensed Professional Engineer's Stamped plan of the tower which includes a structural analysis of the structure including your proposed antenna and all existing and planned for antenna on the tower as of this date.

If I may be of any further assistance please feel free to call anytime.

Yours Truly

Cordless Data Transfer, Inc.

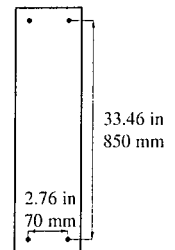
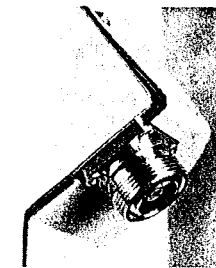
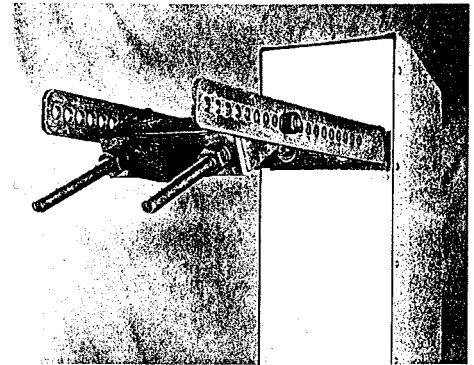
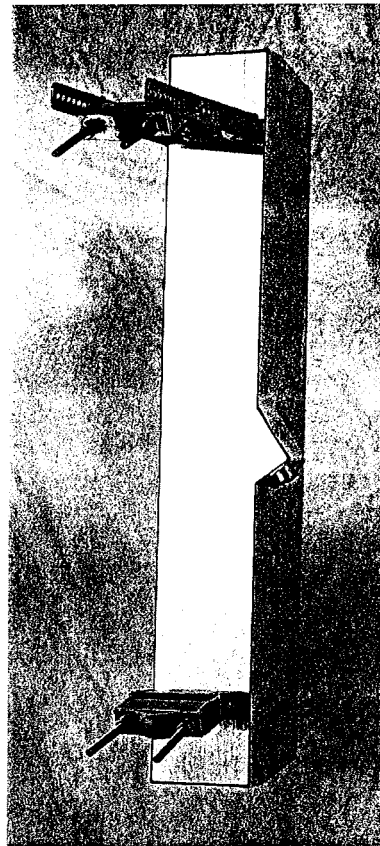

Robert J. Francis
President

ALP-E 9011-Din

Enhanced Log-Periodic Antenna

Features:

- Small Size
- Aesthetically Pleasing
- Suitable For TDMA/CDMA
- High Return Loss
- Low Intermodulation
- High FTB
- Broadbanded
- Side-lobe Suppression
- Sturdy Design
- Down-Tilt Brackets Incl.



The distance between the center of the bolts (on the back of the antenna) are shown in the drawing above.

Bolt diameter is: **3/8-16**
[comes with lock nut].

Electrical Specifications

Frequency Range:	800-900 MHz
Impedance:	50 ohm
Connector Type:	7/16 Din
Return Loss:	20 dB
Polarization:	Vertical
Gain:	> 11 dBd
Front To Back Ratio:	> 30 dB
Side-Lobe Suppression:	18 dB
Intermodulation (2x25W):	IM3 > 146 dB
	IM5 > 153 dB
	IM7/9 > 163 dB
Power Rating:	500 W
H-Plane (-3 dB point):	85 - 92°
V-Plane (-3 dB point):	16 - 18°
Lightning Protection:	DC Grounded

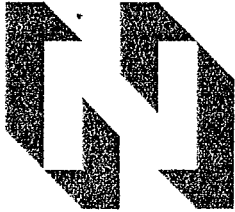
Mechanical Specifications

Overall Height:	43 in	[1092 mm]
Width:	6.5 in	[165 mm]
Depth:	8 in	[203 mm]
Weight Including Tilt-Brackets:	20 lbs	[9.1 Kg]
Rated Wind Velocity:	113 mph	[180 Km/h]
Wind Area (CxA/Side):	2.3 sq. ft.	[0.22 sq.m]
Lateral Thrust At Rated Wind Worst Case:	112 lbs	[500 N]

Materials

Radiating Elements:	Aluminum
Extrusion:	Aluminum
Radome:	Grey PVC
Tilt-Bracket:	Hot Dip Galvanized Steel
Antenna Bolts:	Stainless Steel

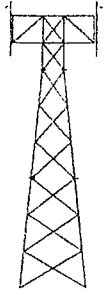
The ALP-E 9011-Din is made in U.S.A.



FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524 -2531 FAX (315) 524-4249

www.nuddtowers.com



July 31, 2000

Bob Francis
CDT
PO Box 363
17 Ridgewood Drive
Marlborough, CT 06447

Bob,

We have completed the analysis of your Eastford tower and have found it adequate within the scope of this analysis to support the proposed antenna loading. The analysis was performed using 85 mph wind speed with 1/2" radial ice per EIA/TIA 222-F recommended standard.

The tower we analyzed is a 180' Nudd G42 guyed tower consisting of pipe legs and angle bracing. Tower sections are all-welded with a face dimension of 3'-6". Foundation capacities were predicated on original design criteria.

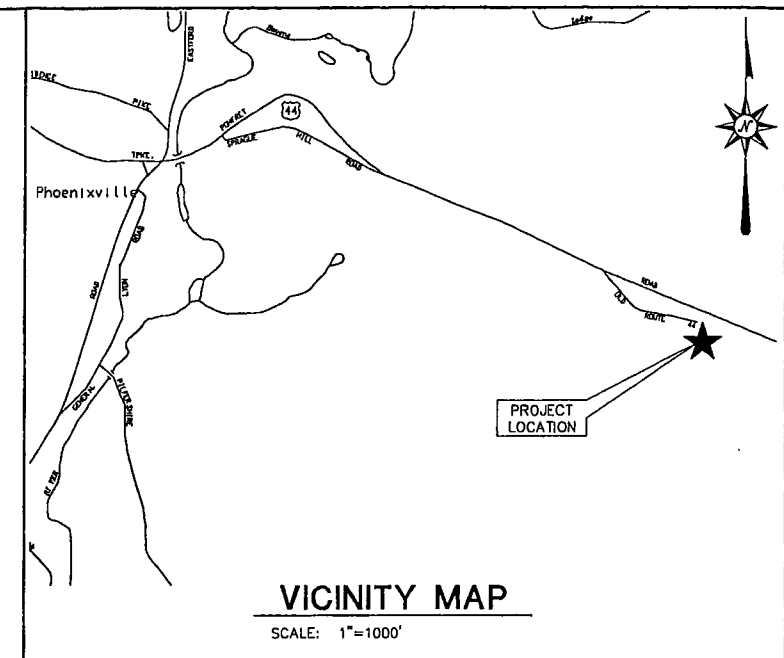
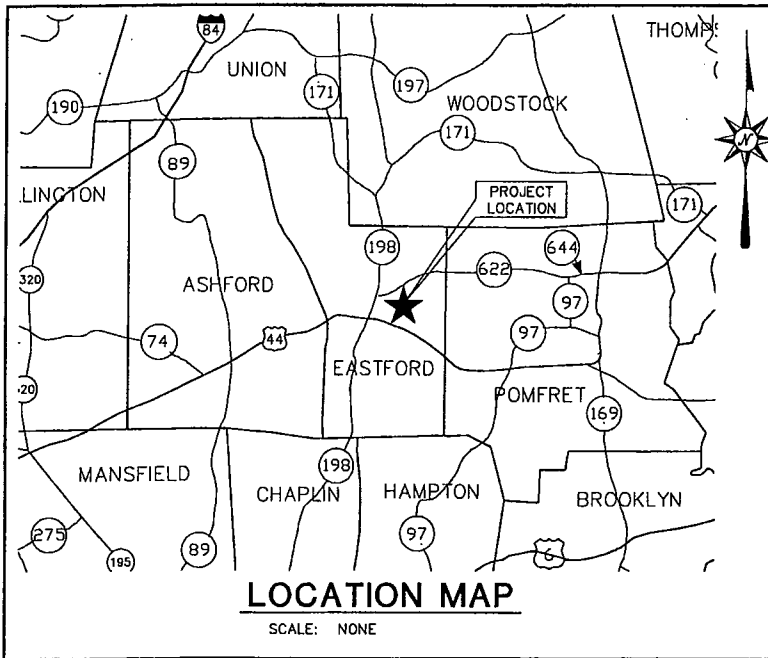
The antenna loading used in the analysis consisted of the configuration shown on drawing #00-5874A-1. The results of the analysis showed with the addition of the 10' section and new guy cable, all tower & foundation elements were loaded within allowable limits.

If you have any questions concerning this analysis, please contact me.

Sincerely,

FRED A. NUDD CORPORATION

Patrick Botimer
Engineer



SITING COUNCIL SUBMISSION

EASTFORD

TELECOMMUNICATION FACILITY

35 OLD ROUTE 44
EASTFORD, CONNECTICUT 06242

PREPARED FOR:
CELLCO PARTNERSHIP DBA
VERIZON WIRELESS
20 ALEXANDER DRIVE
WALLINGFORD, CONNECTICUT 06492

CONTENTS

	TITLE SHEET
SC-1	SITE PLAN AND ELEVATION

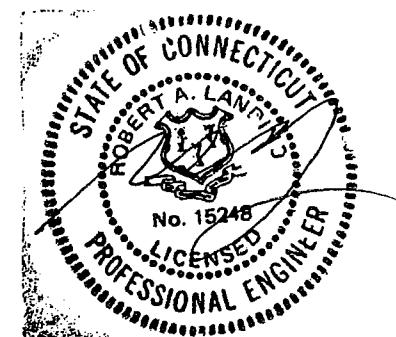
PREPARED BY:



Companies

ARCHITECTURE ENGINEERING PLANNING LANDSCAPE ARCHITECTURE
LAND SURVEYING ENVIRONMENTAL SCIENCES ANALYTICAL SERVICES

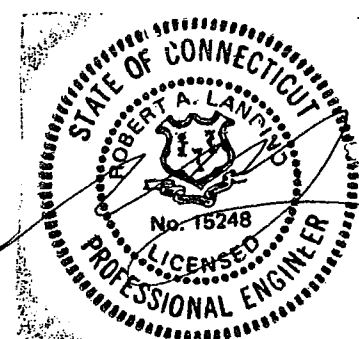
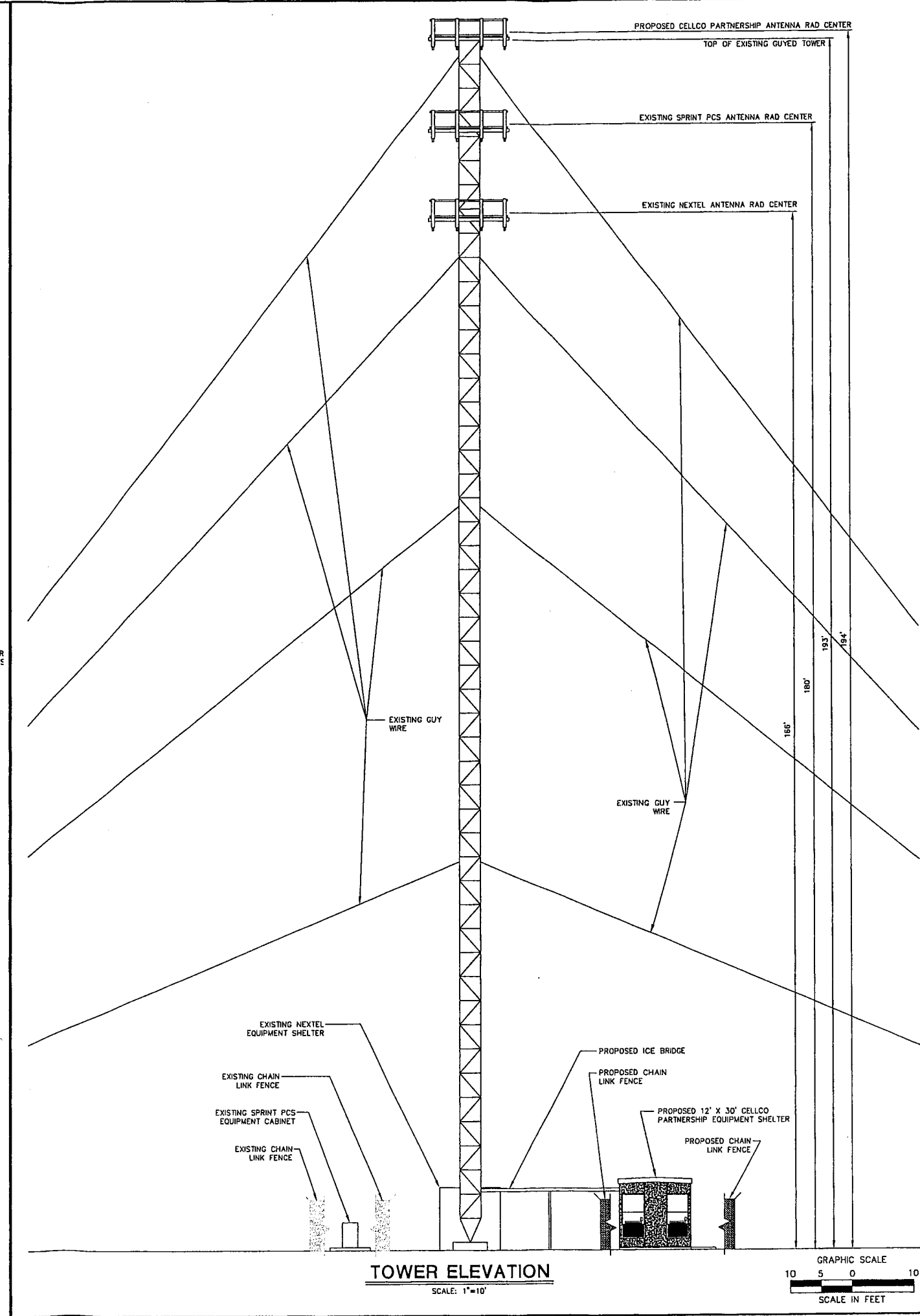
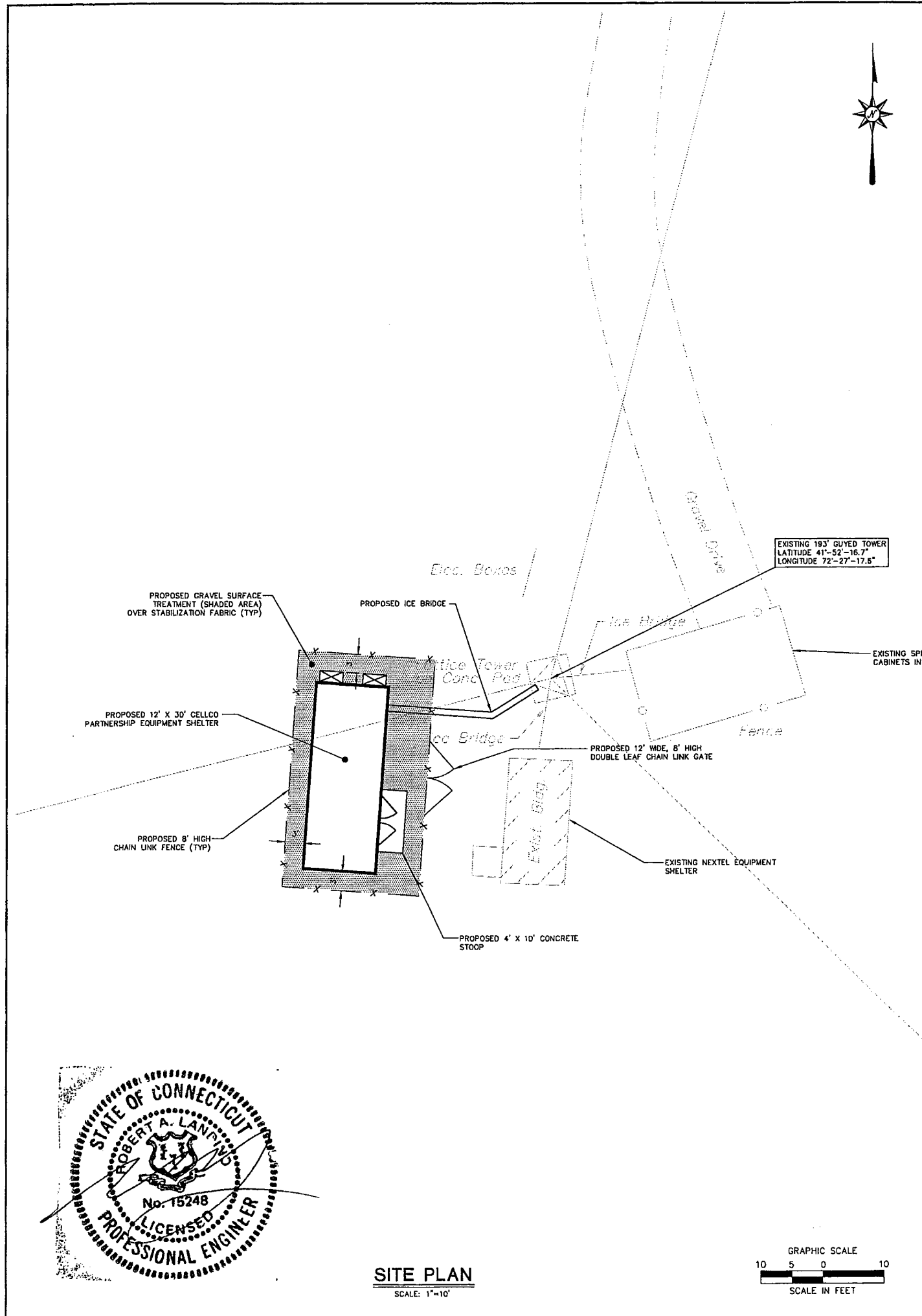
355 RESEARCH PARKWAY
MERIDEN, CONNECTICUT 06450
(203) 630-1406
(203) 630-2615 Fax



NOT FOR CONSTRUCTION

DATES

ISSUE DATE: NOVEMBER 15, 2000
REVISION:



BL Companies
ARCHITECTURE
ENGINEERING
PLANNING
LANDSCAPE ARCHITECTURE
LAND SURVEYING
ENVIRONMENTAL SCIENCES
ANALYTICAL SERVICES

355 Research Parkway
Meriden, CT 06450
(203) 630-1406
(203) 630-2615 Fax

EASTFORD TELECOMMUNICATION FACILITY
35 OLD ROUTE 44
EASTFORD, CONNECTICUT

REVISIONS	No.	Date	Desc.

Designed: R.C.B.
Drawn: R.C.B.
Checked: R.C.B.
Approved: R.A.L.
Scale: AS SHOWN
Project No.: 00C751
Date: 11/15/00
CAD File: SCC75101

Title: **SITE PLAN AND TOWER ELEVATION**

Sheet No.: **SC-1**

TOWER DESIGN CONDITIONS

This tower has been designed to conform to the requirements of ANSI/EIA/TIA 222-F recommended standard for 85 mph wind speed with 1/2" radial ice. Worst case load condition is wind with ice with load reduction. Allowable steel stresses per AISC ASD 9th Edition. Allowable concrete stresses per ACI 318-89.

MATERIAL SPECIFICATIONS

Tower Legs: ASTM A500-C, Fy > 58 ksi.
 All other Steel: ASTM A36, Fy > 36 ksi
 Hardware: ASTM A325 Hot Dipped Galvanized Bolts with Anco Nuts.
 Galvanizing: ASTM A123
 Guy Anchor Shaft: ASTM A36M, Fy > 48 ksi

TOWER LOADING CONDITIONS

QTY	Antenna	Elevation	Windload	Deadload	
3	12' Cellular Boom	191	290	170	
12	ALP 9011	191	116	20	Verizon Wireless
3	8' Cellular Boom	178	226	130	
9	ALP 9011	178	114	20	Nextel
3	12' Cellular Boom	158	275	170	
9	ALP 9011	158	110	20	Sprint PCS
1	G42 Torque Arm	160	527	262	
3	12' Cellular Boom	150	271	170	
12	ALP 9011	150	109	20	Future
1	G42 Torque Arm	120	485	262	

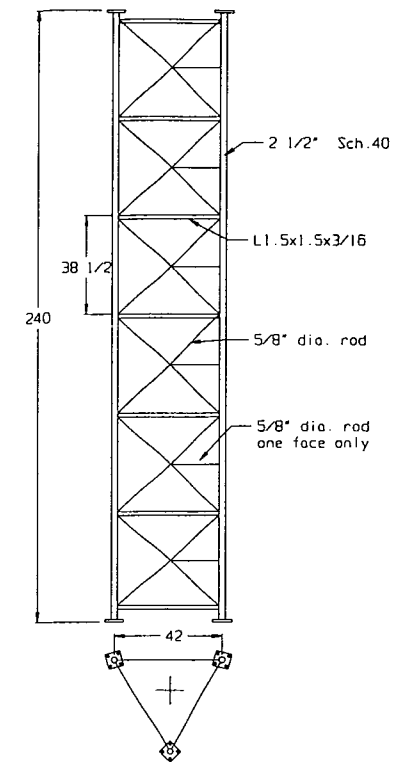
QTY	Type	Elevation		#/ft	
		Start	Stop	Windload	Deadload
1	Tower Span 4	160	190	249.0	57.8
1	Tower Span 3	120	160	233.7	57.8
1	Tower Span 2	60	120	206.3	57.8
1	Tower Span 1	0	60	154.4	63.9

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

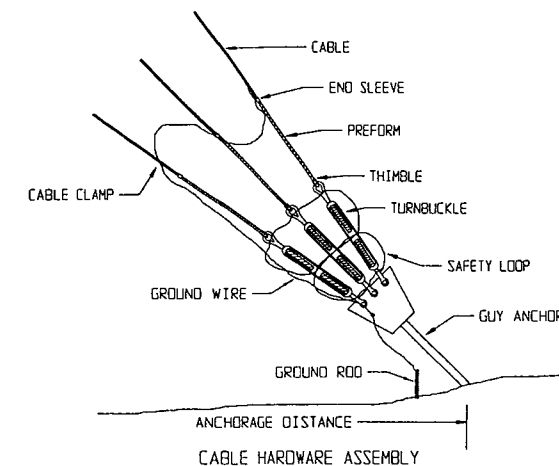
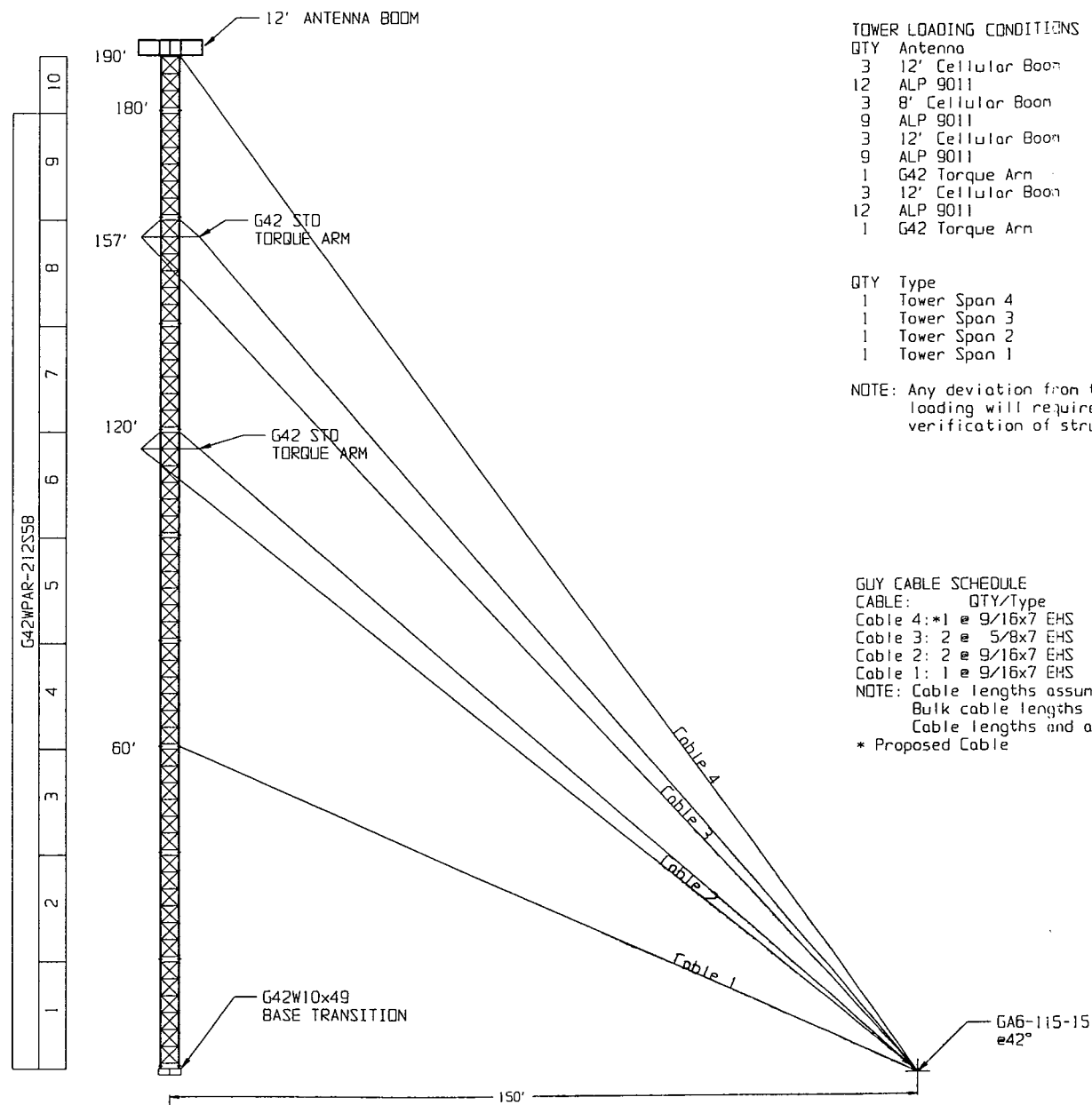
GUY CABLE SCHEDULE

CABLE:	QTY/Type	Length	Ti	Turnbuckle	Preform	Thnbl	Endslve	Shckl
Cable 4:	1 @ 9/16x7 EHS	239'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"
Cable 3:	2 @ 5/8x7 EHS	216'	6360#	1"x18" J-J	5/8" BG	3/4"	65268	3/4"
Cable 2:	2 @ 9/16x7 EHS	188'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"
Cable 1:	1 @ 9/16x7 EHS	157'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"

NOTE: Cable lengths assume anchors at elevation 0'.
 Bulk cable lengths assume 20' tails.
 Cable lengths and anchor layout must compensate for site topography.
 * Proposed Cable



G42WPAR TOWER SECTION



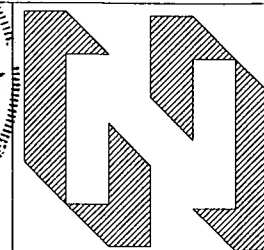
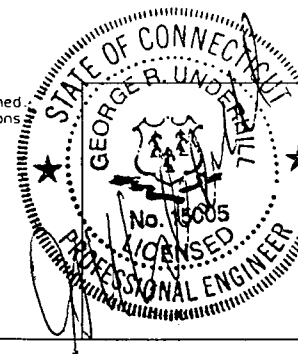
NOTE: Install cable hardware per manufacturer's specifications.

INSTALLATION NOTES

1. Installation of tower must be performed by a qualified tower erector.
2. Install sections with section number on the bottom, and climbing device is aligned.
3. Install safety climb, lights, cable attachments per manufacturer's recommendations.
4. Do not lift more than 100' of assembled tower sections.
5. Install "sharp" edge of adapter plates against face of tower.
6. Plumb and tension tower and cables as erected.
7. "Ti"-Initial tension of cable.

G42 Section Weights: 785/685 +/-
 Top Frame: 1000 +/-

SECTION DESIGNATION:
 G42WPAR-212S55 = 2-1/2"; (212), (S)Sch.40/(EH)Sch.80, (55)ksi strength
 96-47-xx = Year-(47) ksi strength-xx



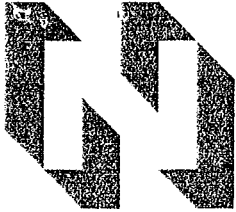
FRED A. NUDD CORPORATION
 Route 104*Ontario, New York 14519*315/524-2531

SCALE: N/S
 DATE: 7/31/00

DRAWN BY: PCB
 APPROVED BY: [Signature]

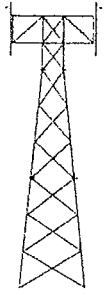
180' TOWER MT. EXTENSION

COT EASTFORD, CT
 DRAWING NUMBER: 00-5874A-1



FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524 -2531 FAX (315) 524-4249
www.nuddtowers.com



July 31, 2000

Bob Francis
CDT
PO Box 363
17 Ridgewood Drive
Marlborough, CT 06447

Bob,

We have completed the analysis of your Eastford tower and have found it adequate within the scope of this analysis to support the proposed antenna loading. The analysis was performed using 85 mph wind speed with 1/2" radial ice per EIA/TIA 222-F recommended standard.

The tower we analyzed is a 180' NuDD G42 guyed tower consisting of pipe legs and angle bracing. Tower sections are all-welded with a face dimension of 3'-6". Foundation capacities were predicated on original design criteria.

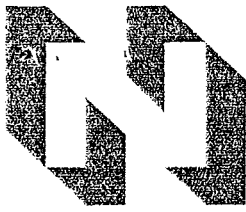
The antenna loading used in the analysis consisted of the configuration shown on drawing #00-5874A-1. The results of the analysis showed with the addition of the 10' section and new guy cable, all tower & foundation elements were loaded within allowable limits.

If you have any questions concerning this analysis, please contact me.

Sincerely,

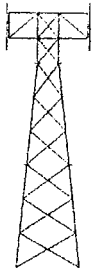
FRED A. NUDD CORPORATION

Patrick Botimer
Engineer



FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524-2531 FAX (315) 524-4249
www.nuddtowers.com



Analysis of
190' Guyed Tower

MODEL #: G42WPAR

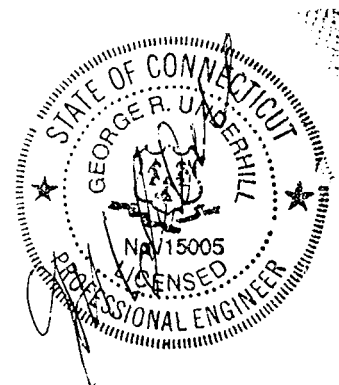
PROJECT #: 5874A

LOCATION: Eastford, Ct

for

CDT
Box 363
17 Ridgewood Dr.
Marlborough, CT 06447

July, 2000



SYNOPSIS OF TOWER ANALYSIS

1. Wind loading conditions considered:
75% wind load with concurrent 1/2" ice.
100% wind with no ice.
Worst wind load case is wind with ice.

- | | |
|----------------------|------------|
| 2. Maximum Leg Load: | 66% loaded |
| 3. Tower Bracing: | 78% loaded |
| 4. Foundations: | 89% loaded |
| 5. Guy Cables: | 91% loaded |

PRIMARY ASSUMPTIONS USED IN THE ANALYSIS

1. Allowable steel stresses are defined by AISC-ASD 9th Edition.
2. All tower members adequately galvanized to prevent corrosion of steel members.
3. All proposed antenna mounts are modeled as Nudd manufactured.
4. No residual stresses due to incorrect tower erection.
5. All bolts are appropriately tightened providing the necessary connection continuity.
6. All welds conform to the requirements of AWS D1.1.
7. We have assumed an allowable wind speed of 85 mph per EIA/TIA 222-F standard for analysis purposes.
8. The acceptability of the analyzed antenna loading is the responsibility of CDT to confirm with the other carriers.
9. Any deviation from the analyzed antenna loading will require a tower analysis for verification of structural integrity.
10. This analysis has been commissioned by Bob Francis of CDT who has provided information about the proposed antennas and location.

TOWER DESIGN CONDITIONS

This tower has been designed to conform to the requirements of ANSI/EIA/TIA 222-F recommended standard for 65 mph wind speed with 1/2" radial ice. Worst case load condition is wind with ice with load reduction. Allowable steel stresses per AISC ASD 9th Edition. Allowable concrete stresses per ACI 318-89.

MATERIAL SPECIFICATIONS

Tower Legs: ASTM A500-C, Fy > 58 ksi.
 All other Steel: ASTM A36, Fy > 36 ksi
 Hardware: ASTM A325 Hot Dipped Galvanized Bolts with Anco Nuts.
 Galvanizing: ASTM A123
 Guy Anchor Shaft: ASTM A304, Fy > 48 ksi

TOWER LOADING CONDITIONS

Qty	Antenna	Windload	Deadload	Verizon Wireless
3	12' Cellular Boom	116	20	
12	ALP 9011	226	130	
3	8' Cellular Boom	175	70	
3	ALP 9011	175	70	
9	12' Cellular Boom	527	262	
1	G42 Torque Arm	271	176	Sprint PCS
3	12' Cellular Boom	109	20	Future
12	ALP 9011	485	262	
1	G42 Torque Arm			

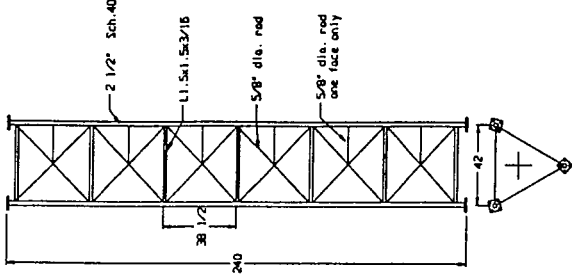
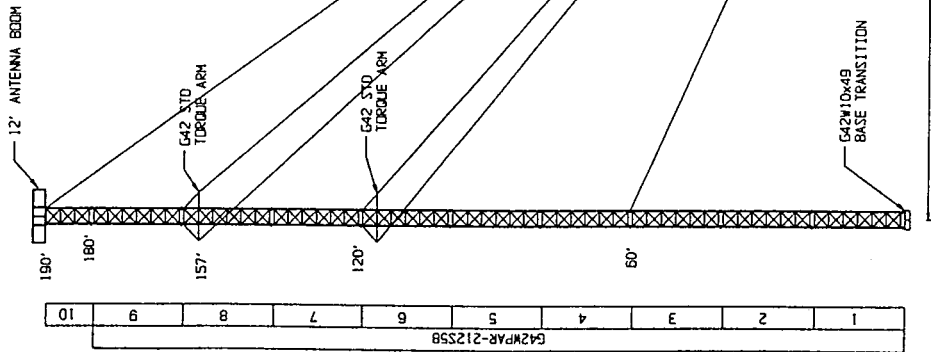
Elevation	Start	Stop	Windload	Deadload	#/ft
191	190	190	249.0	57.8	
191	120	160	233.7	57.8	
178	60	120	206.3	57.8	
158	0	60	154.4	63.9	

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

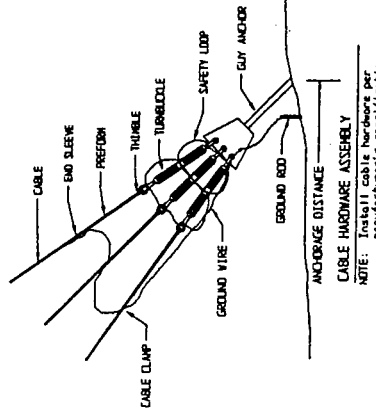
GUY CABLE SCHEDULE

Cable	Qty	Type	Length	Ti	Turnbuckle	Preform	Thobl	Endsize	Shckl
Cable 4	1	9/16x7 EHS	239'	5250#	7/8"x12" J-J	9/16" BG	5-8"	65267	3/4"
Cable 3	2	5/8x7 EHS	216'	6360#	1"x18" J-J	5/8" BG	3-4"	65268	3/4"
Cable 2	2	9/16x7 EHS	188'	5250#	7/8"x12" J-J	9/16" BG	5-8"	65267	3/4"
Cable 1	1	9/16x7 EHS	157'	5250#	7/8"x12" J-J	9/16" BG	5-8"	65267	3/4"

NOTE: Cable lengths assume anchors at elevation 0'.
 Bulk cable lengths assume 20' tails.
 Cable lengths and anchor layout must compensate for site topography.
 * Proposed Cable



ELEVATION TOWER SECTION



- INSTALLATION NOTES**
1. Installation of tower must be performed by a qualified tower erector.
 2. Do not install cable on tower until the bottom and clamping device is aligned.
 3. Install safety chain links on cable after the tower is erected.
 4. Do not lift more than 100' of assembled tower sections.
 5. Install sharp edge of adapter plates against face of tower.
 6. Do not use any other hardware or materials not specified in this drawing.
 7. Final tension of cables as erected.

G42 Section Weights: 785/885 +/-
 Top Frame: 1000 +/-

SECTION DESIGNATION:
 G42MPAR-2125SB = 2-1/2" (212), (3.88ch.-40) EHS Sch. 40, (55 ksi) strength
 86-47-14 = 1/4" (47) ksi strength-xx

FRED A. NUDD CORPORATION
 Route 104-Ontonio, New York 14519-315-524-2531

SCALE: N/S
 DATE: 7/31/00
 PROJECT NO: PCB

180' TOWER MT. EXTENSION

DOT EASTFORD, CT
 DRAWING NUMBER: 00-5874A-1

7/31/00
 8:03:41 AM
 CDT
 Eastford, NY
 Project #: 5874A

GUY CABLE DATA		ft, lbf			Wind	Total	Cable
	Elev	Horiz	Length	Angle	Length	Length	Type
Cable 4:	190	145	240	52.79	419	719	EHS
Cable 3:	160	145	217	47.99	728	1300	EHS
Cable 2:	120	145	189	39.84	589	1133	EHS
Cable 1:	60	145	157	22.81	200	472	EHS

CABLE LOADS		-lbf			Cable Size	%Loaded
	Shear	Download	Cable Load			
Cable 4:	7135	10853	13626	1 - 9/16x7	77.9	
Cable 3:	15973	20480	27561	2 - 5/8x7	65.0	
Cable 2:	13618	13122	20481	2 - 9/16x7	58.5	
Cable 1:	12737	6187	15956	1 - 9/16x7	91.2	

Cable Safety Factor: 2.00
 Shear at 0': 3492 lbf
 Shear on Guy Anchors: 493 lbf

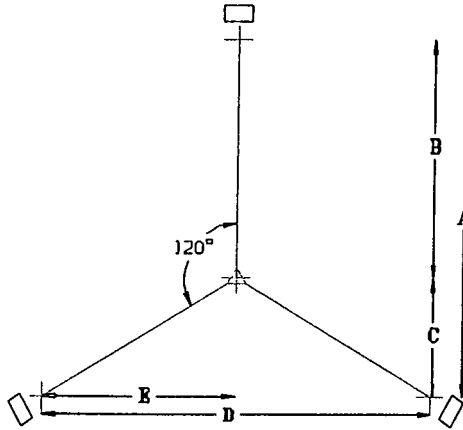
ACCUMULATED DOWN LOADS	
Elevation	Down load (lbf)
193	0
191	750
190	12085
175	13522
160	36187
140	38783
120	54083
90	55816
60	64054
30	65970
0	67886

GUY ANCHOR REACTIONS

Anchor Radius (ft):	145
Vertical Reaction (lbf):	50642
Horizontal Reaction (lbf):	57116
Resultant (lbf):	76333
Horizontal Angle (°):	41.56

TOWER PLOT DIMENSIONS

A=	218 ft
B=	145 ft
C=	73 ft
D=	251 ft
E=	126 ft



TOWER PLOT PLAN

7/31/00
 8:03:55 AM
 CDT
 Eastford, NY
 Project #: 5874A

MOMENT DISTRIBUTION OUTPUT

Beam Configuration:

5 Spans

SPAN	FEMB	FEMT	VB	VT	dfB	dfT
1	-46309	46308	4630	4630	1.0000	0.5000
2	-61877	61876	6187	6672	0.5000	0.4000
3	-35303	46334	5294	8511	0.6000	0.4286
4	-23585	26038	4417	4757	0.5714	1.0000
5	-2265	0	2264	0	0.0000	0.0000

10 Iterations

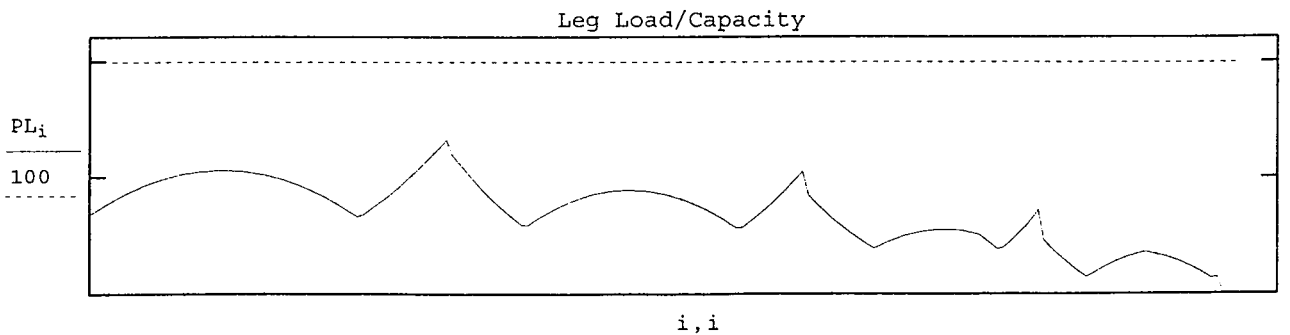
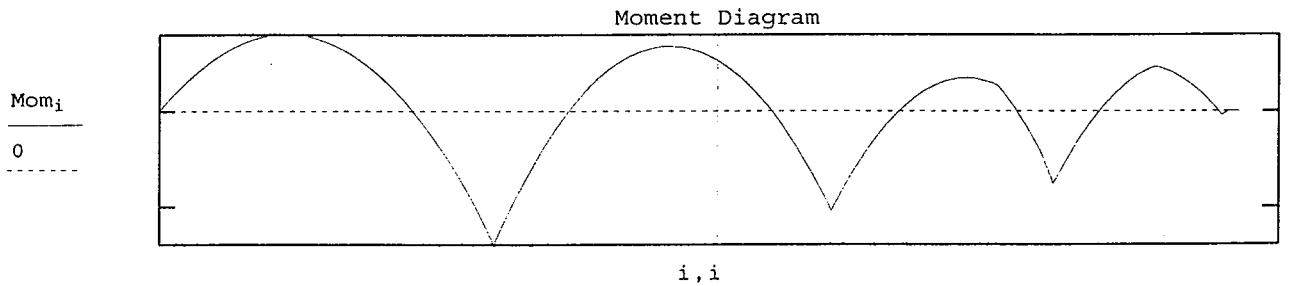
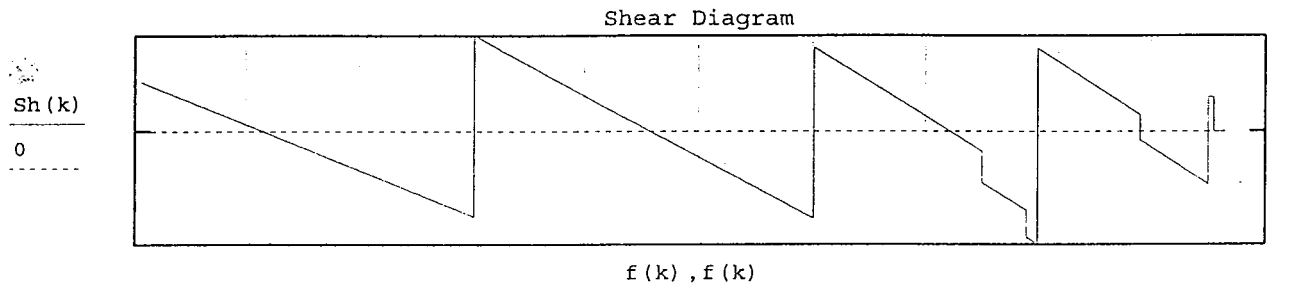
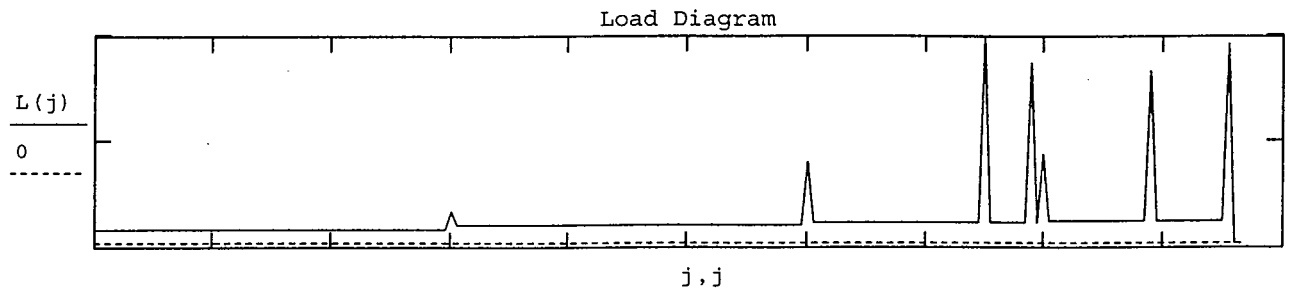
SPAN #	DISTRIBUTED MOMENTS (ft-lb)			SHEARS (lb)		REACTIONS (lb)
	MOM B	MOM T	VB	VT		
1	0	68354	3492	5770		3492
2	-68354	51141	6475	6386		12245
3	-51141	37154	5644	8162		12030
4	-37154	2265	5580	3595		13742
5	-2265	0	2265	0		5859
						0

Project: CDT
 Location: Eastford, CT
 Date: 7/00

Maximum_Download = 67885.6

Maximum_Load = 2348

Top := 200 ft High



PL_i = % Loaded

Elevation = 180

Moment = 21232.7

Leg_Load = 11226

Mom_i = Moment

DownLoad = 12663.1

Percent_Loaded₁ = 16.8%

max (PL) = 66.4

Check Girts at Guy Pulls:

Tensile capacity of (1) L1.5x1.5x3/16:

$$\text{Area} := \left[1.5^2 - (1.5 - .1875)^2 - .4375 \cdot .1875 \right] \cdot \text{in}^2$$

$$\text{Capacity} := .6 \cdot \text{FYgirt} \cdot \frac{4}{3} \cdot \text{Area} \cdot 1 \cdot \text{bars}$$

Maximum Single cable shear is 12800 lb, resolved into each brace.

$$\text{Percent_Loaded}_2 := \frac{\frac{12800 \cdot \text{lbF}}{2 \cdot \text{girt} \cdot \cos(30 \cdot \text{deg})}}{\text{Capacity}}$$

Steel Properties:

$$E := 29 \cdot 10^6 \cdot \text{psi}$$

$$\text{FYgirt} := 36000 \cdot \text{psi}$$

$$\text{FYdiag} := 36000 \cdot \text{psi}$$

$$\text{Capacity} = 12825 \text{ lbf}$$

$$\text{Percent_Loaded}_2 = 57.6\%$$

Check compression capacity of girts against maximum shear:

$$l := (42 - 2.875) \cdot \text{in} \quad \text{Area} := \left[1.5^2 - (1.5 - .1875)^2 \right] \cdot \text{in}^2$$

$$\text{Area} = 0.527 \text{ in}^2$$

$$r := .293 \cdot \text{in} \quad \text{L1.5x1.5x.1875"} \quad \text{K} := .70 \quad \text{All welded}$$

$$\text{klr} := \frac{K \cdot l}{r}$$

$$\text{Cc} := \sqrt{\frac{2 \cdot \pi^2 \cdot E}{\text{FYgirt}}}$$

$$\text{klr} = 93.5$$

$$\text{Cc} = 126.1$$

$$\text{Fa}(\text{klr}, \text{Cc}, \text{FY}) := \frac{\left[1 - \frac{\left(\frac{\text{klr}}{\text{Cc}} \right)^2}{2} \right] \cdot \text{FY}}{\frac{5}{3} + \frac{3}{8} \cdot \frac{\text{klr}}{\text{Cc}} - \left(\frac{\text{klr}}{2 \cdot \text{Cc}} \right)^3} \cdot (\text{klr} < \text{Cc}) + \frac{12 \cdot \pi^2 \cdot E}{23 \cdot \text{klr}^2} \cdot (\text{klr} \geq \text{Cc})$$

$$\text{Fa1} := \text{Fa}(\text{klr}, \text{Cc}, \text{FYgirt})$$

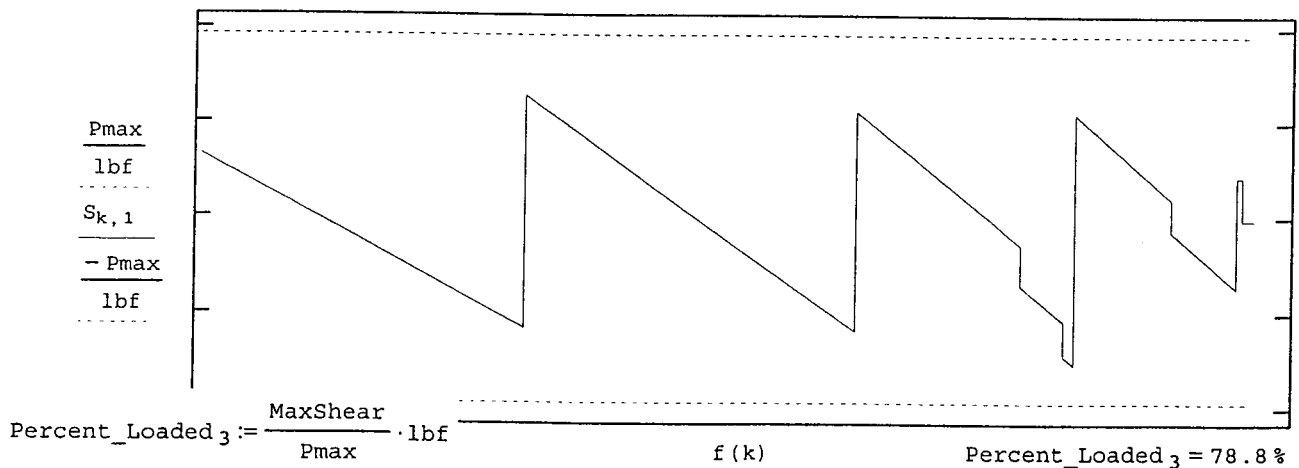
$$\text{Fa1} = 13787.4 \text{ psi}$$

Maximum allowable compression load:

$$\text{Pmax} := \text{Fa1} \cdot \frac{4}{3} \cdot \text{Area}$$

$$\text{Pmax} = 9694.3 \text{ lbf}$$

$$\text{MaxShear} = 7635.3$$

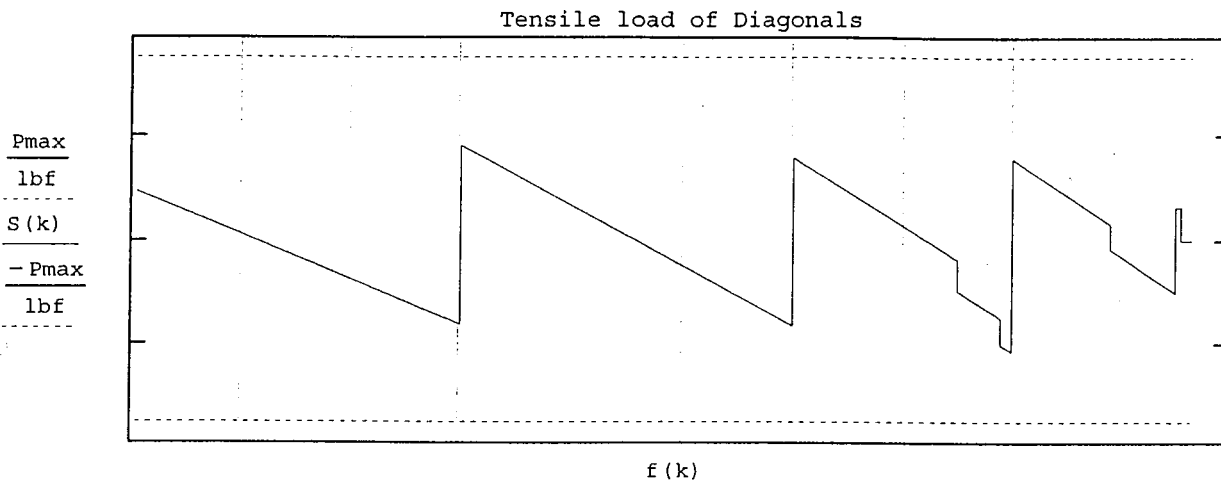


Check tension capacity of diagonals:

$$S(k) := \frac{Sh(k)}{2 \cdot \text{braces} \cdot \cos(45 \cdot \text{deg})}$$

$$P_{\max} := \frac{\pi}{4} \cdot \left(\frac{5}{8} \cdot \text{in}\right)^2 \cdot .6 \cdot F_{y\text{diag}} \cdot \frac{4}{3}$$

$$P_{\max} = 8835.7 \text{ lbf}$$



Bracing:
 Use 5/8" diagonals throughout tower,
 3/4" at guypull panels.
 Use L1.5x1.5x.1875" Horizontals.
 Legs: 2-1/2" pipe

All allowable stresses per
 American Institute of Steel Construction 9th edition and
 Electronics Industry Association 222-F recommended standard.

INNER GUY ANCHOR DESIGN CALCULATIONS

Customer: CDT
 Project: Eastford, NY
 7/31/00 8:22 AM

REACTIONS:

Vertical 50.6 kips
 Horizontal 57.1 kips
 Resultant 76.3 kips
 Hor. Angle 41.6 °
 Submerged? 0 No
 Water Depth: 0 ft

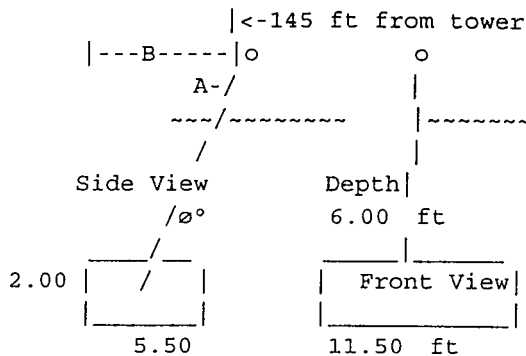
Soil Wt: 100.0 lb/ft³
 Soil Gs: 2.65
 Subm Soil Wt 62.3 lb/ft³
 H.Bearing 400.0 psf/ft
 Rebar Fy: 60.0 ksi
 Conc. Wt: 150.0 lb/ft³
 Conc f'c: 3.0 ksi

CONCRETE WEIGHT:

Block Volume 4.7 cu yds
 Block Wt 19.0 kips

SOIL FRUSTUM WEIGHT:

Frustum: 30 °
 Block: 38.0 kips
 Edges: 35.3 kips
 Corners: 9.6 kips
 Total Wt: 82.9 kips
 Excavation: 506 cuft



HORIZONTAL CAPACITY: EIA 7.1.2

Check anchor shaft embedment? OK

Load @ 7 ft
 Load: 64400 lb

Uplift 50.64
 Horizontal 57.12 kips

GUY ANCHOR ROD:

Resultant 76.33 kips
 Hole QTY 6 holes

Design Loads: 50.64
 Capacity*: 56.62
 % Loaded: 89%
 * EIA 7.2.4

of rods 1

Concrete Volume: 14.1 cu yds

Fy 48000 psi
 Min. Area 1.988 in²/bar
 Min. Dia. 1.591 in
 Act. Area 2.405 in²/bar
 Act. Dia. 1.75 in, 82.6% Loaded

ANCHOR ROD LENGTH:
 Minimum: 13.30 ft
 Maximum: 15.07 ft
 Recommend: 14.00 ft
 Actual: 15 ft

Anchor ID: GA6-115-15

BLOCK REINFORCEMENT: Cover: 6 in

Vertical Horizontal

Factored Loads: 65.8 74.3 kips EIA 3.1.13
 Factored Moment: 1261.8 1423.1 kip-inch
 Minimum As: 1.583 0.529 in² ACI 10.5.1
 Minimum Qty: 9 3 Bar #:
 Actual Qty: 9 4 4
 Actual As: 1.767 0.785 in² OK

ANCHOR DIMENSIONS:

REBAR DIMENSIONS:

MASTER CHECK: OK

Length - 11'- 6" RBL: 121"
 Width - 5'- 6" RBH: 12"
 Height - 2'- 0" RBW: 56"
 Depth - 6'- 0" Bent OAL: 68"
 OADepth- 8'- 0" QTY Long: 14 Bars ea
 Dim. A: 7'- 0" QTY Bent: 14 Bars ea
 Dim. B: 12'- 6" Rebar Wt. 164 lb ea
 ø: 41°

SQUARE FOOTING AND PIER DESIGN

Customer: CDT
 Project: Eastford, NY
 7/31/00 8:22 AM

Dead Load 20 kips
 Wind Load 55 kips
 Live Load 0 kips

ASSUMED DIMENSIONS:

Width 5.50 ft OK f'c: 3000 psi
 Thickness 1.00 ft Fy: 60000 psi
 Pier OD 2.00 ft Soil: 4000 psf net bearing capacity
 Sqr Pier 0
 Rnd Pier 1 Pier Area: 452 inch²
 Depth 4.00 ft Ht. above Grade: 3 inches
 Cover 3 inches
 Bar # 4 0.5 G42W10x49 Base Transition ID
 Eff. Depth 8.500 inches

CALCULATIONS: Minimum Width: 4.330 ft 62% loaded
 Ultimate Load: 43.0 kips ACI 9.2.2
 Ultimate Stress 1421 psf (factored)

CHECK SHEAR

Two Way Action: Assumes βc=1 One Way Action Load Area: 5.729 ft²
 Vu: 34799 lbs Vu: 8141 lbs
 Vc: 161619 lbs Vc: 52236 lbs
 21.53% <= OK => 15.59%

LOAD TRANSFER

Pier Capacity/Pu ACI 15.8

@ Pad/Pier interface 5% OK - Dowels not required.

Pivot Pin Bearing Stress: ACI 10.15.1

Minimum Area 12 inch²
 Minimum plate OD 3.92 inchø, 3.47" ea. side square
 Distance "d" to edge 0.5 inch -> d
 Minimum Plate Thickness: 0.2230 inch

Bearing Plate-- ^ |<--Pivot Pin

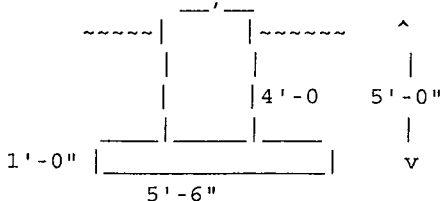
MINIMUM PIER REINFORCING ACI 15.8.2.1, 7.10.5

.5% Req. 2.262 inch² Steel Area:
 8 Bars of # 5 2.454 inch² OK
 Bar Length: 54 inch
 Pier Tie bar #: 3 10 " tie bar spacing

|<-->| 2'-0"

PAD BENDING MOMENT REINFORCEMENT

Mn: 13297 ft-lbs
 Ratio: 0.000561 ACI 10.5.1
 Steel: 0.315 inch²
 Bar #: 5
 Req'd QTY: 2
 Act'l QTY: 5 OK
 Act. Stl: 1.534 inch²
 Act. d: 8.500 inches
 Ldb: 11.25 inches OK



Mat Bars: Concrete:
 10 @ 13.50" spacing 1.6 cuyd
 84 lb 6422.5 lb

MASTER CHECK: OK

TOWER LOADS

Point Loads

QTY	Antenna	Elevation		Windload	Deadload	
		(ft)	(lb)			
3	12' Cellular Boom	191	290	170		
12	ALP 9011	191	116	20		Verizon Wirelss
3	8' Cellular Boom	178	226	130		
9	ALP 9011	178	114	20		Nextel
3	12' Cellular Boom	158	275	170		
9	ALP 9011	158	110	20		Sprint PCS
1	G42 Torque Arm	160	527	262		
3	12' Cellular Boom	150	271	170		
12	ALP 9011	150	109	20		Future
1	G42 Torque Arm	120	485	262		

Uniform Loads

QTY	Type	Elevation		#/ft	
		Start	Stop	Windload	Deadload
1	Tower Span 4	160	190	249.0	57.8
1	Tower Span 3	120	160	233.7	57.8
1	Tower Span 2	60	120	206.3	57.8
1	Tower Span 1	0	60	154.4	63.9

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, NY

Guyed Tower

7/31/00 8:19 AM

Wind Angle 0,60,90 90 °

Span: 1

Elevation of Foundation: 1 ft

Elev@Top 40 feet

Wind Speed 85 mph

Elev@Base 20 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 193 feet

Wind Pres. 20.6 psf EIA 2.3.3

Top Face 42.00 inches 3.50

Radial Ice 0.5 inch

Bot Face 42.00 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper/Se 0.00 in.

ANSI/EIA Overstress Factor: Yes

Ave Face 42.00 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY >

Section Ixx,Iyy > 1508 in^4

ITEM DL WL

Face Vert. Angle 0.000 °

Ladder: 100 10

Leg Angle in face 0.000 °

Misc. 159 0

Leg/Axis Angle 0.000 °

Total lbf: 259 10

Brace Angle 42.138 °

SECTION 1 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Ag: 76 ft² Total Weigh 682 336 lbs

Af: 3 ft² Df: 0.850

Ar: 22 ft² Rr: 0.625

SR(e): 0.328 ft² Dr: 1.000

Cf: 2.225

K 1.00

Legs: KL/r 40.1 OK

Fy 58000 psi

EIA 3.1.1, Cc 99.3

AISC E2 Fa 39247 psi

fMax.Compresn.Force 66879 lbs

Area: 16.30 ft²

Shear: 571 28.6 lbf,lbf/ft

CnMoment: 5713 ft-lbf

Deadload: 1277 63.9 lbf,lbf/ft

K 1.00

Solid Area Windloads:

Diagonals: KL/r 153.0 OK

Shear: 3087 154.4 lbf,lbf/ft

Fy 36000 psi

Cc 126.1

feet²

EIA 3.1.1 Fa 8502 psi

Ae 0° 16.73

Max.Compresn.Force 2608 lbs

Ae 45° 20.07

Max.Tension.Force* 8836 lbs

Ae 60° 16.16

*Verify Net Section on member.

Ae 90° 16.30

K 1

Horizontals: KL/r 133.4 OK

Span Length 60 ft

Cc 126.1

Span Capacity 66121 lbf/leg

EIA 3.1.1 Fa 11193 psi

Max.Compresn.Force 5903 lbs

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, NY

Guyed Tower

7/31/00 8:19 AM

Wind Angle 0,60,90 90 °

Span: 2

Elevation of Foundation: 1 ft Elev@Top 100 feet

Wind Speed 85 mph Elev@Base 80 feet

Gh 1.12 EIA 2.3.4 Tower Ht. 193 feet

Wind Pres. 27.6 psf EIA 2.3.3 Top Face 42.00 inches 3.50

Radial Ice 0.5 inch Bot Face 42.00 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes Taper/Se 0.00 in.

ANSI/EIA Overstress Factor: Yes Ave Face 42.00 inches
Length 240 inches

LEGS OD,L1 ID,L2 wall FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203 # Panel 6 panels

DIAGONALS Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313 Br/Panel 2 |x|

HORIZONTALS Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188 # Horiz 7 7

Density 0.283 lb/in³

Dbl Angle Gap: 0 in Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY »

Section Ixx,Iyy » 1508 in⁴

Face Vert. Angle 0.000 °

Leg Angle in face 0.000 °

Leg/Axis Angle 0.000 °

Brace Angle 42.138 °

ITEM	DL	WL
Ladder:	100	10
Misc.	38	0
Total lbf:	138	10

SECTION 2 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Ag: 76 ft² Total Weigh 682 336 lbs

Af: 3 ft² Df: 0.850

Ar: 22 ft² Rr: 0.625

SR(e): 0.328 ft² Dr: 1.000

Cf: 2.225

Legs: K 1.00

KL/r 40.1 OK

Fy 58000 psi

EIA 3.1.1, Cc 99.3

AISC E2 Fa 39247 psi

Max.Compresn.Force 66879 lbs

Area: 16.30 ft²

Shear: 760 38.0 lbf,lbf/ fMax.Compresn.Force

CnMoment: 7600 ft-lbf

Deadload: 1156 57.8 lbf,lbf/ft K 1.00

Solid Area Windloads: Diagonals : KL/r 142.2 OK

Shear: 4125 206.3 lbf,lbf/ft Fy 36000 psi

Cc 126.1

feet² EIA 3.1.1 Fa 9848 psi

Ae 0° 16.73 Max.Compresn.Force 3021 lbs

Ae 45° 20.07 Max.Tension.Force* 8836 lbs

Ae 60° 16.16 *Verify Net Section on member.

Ae 90° 16.30 K 1

Horizontals: KL/r 133.4 OK

Cc 126.1

Span Length 60 ft

Span Capacity 66121 lbf/leg EIA 3.1.1 Fa 11193 psi

Max.Compresn.Force 5903 lbs

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, NY

Guyed Tower

7/31/00 8:19 AM

Wind Angle 0,60,90 90 °

Span: 3

Elevation of Foundation: 1 ft

Elev@Top 150 feet

Wind Speed 85 mph

Elev@Base 130 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 193 feet

Wind Pres. 31.3 psf EIA 2.3.3

Top Face 42.00 inches 3.50

Radial Ice 0.5 inch

Bot Face 42.00 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper/Se 0.00 in.

ANSI/EIA Overstress Factor: Yes

Ave Face 42.00 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY »

Section Ixx,Iyy » 1508 in^4

ITEM DL WL

Face Vert. Angle 0.000 °

Ladder: 100 10

Leg Angle in face 0.000 °

Misc. 38 0

Leg/Axis Angle 0.000 °

Total lbf: 138 10

Brace Angle 42.138 °

SECTION 3 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

 Ag: 76 ft² Total Weigh 682 336 lbs

Af: 3 ft² Df: 0.850

Ar: 22 ft² Rr: 0.625

SR(e): 0.328 ft² Dr: 1.000

Cf: 2.225

Legs: K 1.00

KL/r 40.1 OK

Fy 58000 psi

EIA 3.1.1, Cc 99.3

AISC E2 Fa 39247 psi

Max.Compresn.Force 66879 lbs

Area: 16.30 ft²

Shear: 860 43.0 lbf,lbf/ f

CnMoment: 8599 ft-lbf

Deadload: 1156 57.8 lbf,lbf/ft

Diagonals : K 1.00

KL/r 142.2 OK

Fy 36000 psi

Cc 126.1

EIA 3.1.1 Fa 9848 psi

Max.Compresn.Force 3021 lbs

Max.Tension.Force* 8836 lbs

*Verify Net Section on member.

K 1

Horizontals: KL/r 133.4 OK

Cc 126.1

EIA 3.1.1 Fa 11193 psi

Max.Compresn.Force 5903 lbs

feet²

Ae 0° 16.73

Ae 45° 20.07

Ae 60° 16.16

Ae 90° 16.30

Span Length 40 ft

Span Capacity 71530 lbf/leg

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, NY

Guyed Tower

7/31/00 8:19 AM

Wind Angle 0,60,90 90 °

Span: 4

Elevation of Foundation: 1 ft Elev@Top 185 feet

Wind Speed 85 mph Elev@Base 165 feet

Gh 1.12 EIA 2.3.4 Tower Ht. 193 feet

Wind Pres. 33.3 psf EIA 2.3.3 Top Face 42.00 inches 3.50

Radial Ice 0.5 inch Bot Face 42.00 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes Taper/Se 0.00 in.

ANSI/EIA Overstress Factor: Yes Ave Face 42.00 inches
Length 240 inches

LEGS OD,L1 ID,L2 wall FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203 # Panel 6 panels

DIAGONALS Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313 Br/Panel 2 |x|

HORIZONTALS Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188 # Horiz 7 7

Density 0.283 lb/in³

Dbl Angle Gap: 0 in Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY »

Section Ixx,Iyy » 1508 in⁴

Face Vert. Angle 0.000 °

Leg Angle in face 0.000 °

Leg/Axis Angle 0.000 °

Brace Angle 42.138 °

ITEM DL WL

Ladder: 100 10

Misc. 38 0

Total lbf: 138 10

SECTION 4 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Ag: 76 ft² Total Weigh 682 336 lbs

Af: 3 ft² Df: 0.850

Ar: 22 ft² Rr: 0.625 K 1.00

SR(e): 0.328 ft² Dr: 1.000 Legs: KL/r 40.1 OK

Cf: 2.225 Fy 58000 psi

EIA 3.1.1, Cc 99.3

Area: 16.30 ft² AISC E2 Fa 39247 psi

Shear: 916 45.8 lbf, lbf/ f Max.Compresn.Force 66879 lbs

CnMoment: 9155 ft-lbf

Deadload: 1156 57.8 lbf, lbf/ft K 1.00

Solid Area Windloads: Diagonals : KL/r 142.2 OK

Shear: 4981 249.0 lbf, lbf/ft Fy 36000 psi

Cc 126.1

feet² EIA 3.1.1 Fa 9848 psi

Ae 0° 16.73 Max.Compresn.Force 3021 lbs

Ae 45° 20.07 Max.Tension.Force* 8836 lbs

Ae 60° 16.16 *Verify Net Section on member.

Ae 90° 16.30 K 1

Horizontals: KL/r 133.4 OK

Cc 126.1

Span Length 30 ft

Span Capacity 73853 lbf/leg

EIA 3.1.1 Fa 11193 psi

Max.Compresn.Force 5903 lbs

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Eastford, NY

Guyed Tower

7/31/00 8:19 AM

Wind Angle 0,60,90 90 °

Span: 5

Elevation of Foundation: 1 ft

Elev@Top 201 feet

Wind Speed 85 mph

Elev@Base 181.5 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 193 feet

Wind Pres. 34.2 psf EIA 2.3.3

Top Face 42.00 inches 3.50

Radial Ice 0.5 inch

Bot Face 42.00 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper/Se 0.00 in.

ANSI/EIA Overstress Factor: Yes

Ave Face 42.00 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY »

Section Ixx,Iyy » 1508 in^4

Face Vert. Angle 0.000 °

Leg Angle in face 0.000 °

Leg/Axis Angle 0.000 °

Brace Angle 42.138 °

ITEM DL WL

Ladder: 100 10

Misc. 38 0

Total lbf: 138 10

SECTION 5 WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

 Ag: 76 ft^2 Total Weigh 682 336 lbs

Af: 3 ft^2 Df: 0.850

Ar: 22 ft^2 Rr: 0.625

SR(e): 0.328 ft^2 Dr: 1.000

Cf: 2.225

K 1.00

Legs: KL/r 40.1 OK

Fy 58000 psi

EIA 3.1.1, Cc 99.3

AISC E2 Fa 39247 psi

fMax.Compresn.Force 66879 lbs

Area: 16.30 ft^2

Shear: 939 46.9 lbf,lbf/ft

CnMoment: 9390 ft-lbf

Deadload: 1156 57.8 lbf,lbf/ft

K 1.00

Solid Area Windloads: Diagonals : KL/r 142.2 OK

Shear: 5110 255.5 lbf,lbf/ft

Fy 36000 psi

Cc 126.1

feet^2 EIA 3.1.1 Fa 9848 psi

Ae 0° 16.73 Max.Compresn.Force 3021 lbs

Ae 45° 20.07 Max.Tension.Force* 8836 lbs

Ae 60° 16.16 *Verify Net Section on member.

Ae 90° 16.30

K 1

Horizontals: KL/r 133.4 OK

Cc 126.1

Span Length 6 ft

Span Capacity 78255 lbf/leg

EIA 3.1.1 Fa 11193 psi

Max.Compresn.Force 5903 lbs

Eleva- tion	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
0	0	67886	22629	66121	66121	34.2
1	3414	67822	23734	66121	66121	35.9
2	6675	67758	24788	66121	66121	37.5
3	9780	67694	25791	66121	66121	39.0
4	12732	67630	26744	66121	66121	40.4
5	15529	67566	27645	66121	66121	41.8
6	18171	67502	28496	66121	66121	43.1
7	20660	67439	29295	66121	66121	44.3
8	22993	67375	30044	66121	66121	45.4
9	25173	67311	30742	66121	66121	46.5
10	27198	67247	31389	66121	66121	47.5
11	29069	67183	31985	66121	66121	48.4
12	30785	67119	32530	66121	66121	49.2
13	32348	67055	33024	66121	66121	49.9
14	33755	66991	33467	66121	66121	50.6
15	35009	66928	33859	66121	66121	51.2
16	36108	66864	34200	66121	66121	51.7
17	37052	66800	34491	66121	66121	52.2
18	37843	66736	34730	66121	66121	52.5
19	38479	66672	34919	66121	66121	52.8
20	38960	66608	35056	66121	66121	53.0
21	39287	66544	35143	66121	66121	53.1
22	39460	66481	35179	66121	66121	53.2
23	39479	66417	35163	66121	66121	53.2
24	39343	66353	35097	66121	66121	53.1
25	39053	66289	34980	66121	66121	52.9
26	38608	66225	34812	66121	66121	52.6
27	38009	66161	34593	66121	66121	52.3
28	37256	66097	34324	66121	66121	51.9
29	36348	66033	34003	66121	66121	51.4
30	35286	65970	33631	66121	66121	50.9
31	34069	65906	33209	66121	66121	50.2
32	32699	65842	32735	66121	66121	49.5
33	31174	65778	32211	66121	66121	48.7
34	29494	65714	31635	66121	66121	47.8
35	27660	65650	31009	66121	66121	46.9
36	25672	65586	30332	66121	66121	45.9
37	23529	65523	29604	66121	66121	44.8
38	21232	65459	28824	66121	66121	43.6
39	18781	65395	27994	66121	66121	42.3
40	16176	65331	27114	66121	66121	41.0
41	13415	65267	26182	66121	66121	39.6
42	10501	65203	25199	66121	66121	38.1
43	7432	65139	24165	66121	66121	36.5
44	4209	65075	23081	66121	66121	34.9
45	832	65012	21945	66121	66121	33.2
46	-2700	64948	22540	66121	66121	34.1
47	-6386	64884	23735	66121	66121	35.9
48	-10227	64820	24981	66121	66121	37.8
49	-14222	64756	26277	66121	66121	39.7

Eleva- tion	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
50	-18371	64692	27625	66121	66121	41.8
51	-22675	64628	29024	66121	66121	43.9
52	-27133	64565	30473	66121	66121	46.1
53	-31745	64501	31973	66121	66121	48.4
54	-36512	64437	33525	66121	66121	50.7
55	-41433	64373	35127	66121	66121	53.1
56	-46508	64309	36780	66121	66121	55.6
57	-51738	64245	38484	66121	66121	58.2
58	-57122	64181	40239	66121	66121	60.9
59	-62661	64117	42045	66121	66121	63.6
60	-68354	64054	43902	66121	66121	66.4
61	-61982	57492	39613	66121	66121	59.9
62	-55817	57434	37560	66121	66121	56.8
63	-49858	57376	35574	66121	66121	53.8
64	-44106	57319	33657	66121	66121	50.9
65	-38559	57261	31808	66121	66121	48.1
66	-33219	57203	30027	66121	66121	45.4
67	-28085	57145	28314	66121	66121	42.8
68	-23158	57087	26669	66121	66121	40.3
69	-18436	57030	25092	66121	66121	37.9
70	-13921	56972	23584	66121	66121	35.7
71	-9612	56914	22143	66121	66121	33.5
72	-5510	56856	20770	66121	66121	31.4
73	-1614	56799	19465	66121	66121	29.4
74	2077	56741	19599	66121	66121	29.6
75	5560	56683	20729	66121	66121	31.4
76	8838	56625	21791	66121	66121	33.0
77	11909	56567	22785	66121	66121	34.5
78	14774	56510	23711	66121	66121	35.9
79	17433	56452	24569	66121	66121	37.2
80	19886	56394	25359	66121	66121	38.4
81	22132	56336	26081	66121	66121	39.4
82	24172	56279	26734	66121	66121	40.4
83	26006	56221	27320	66121	66121	41.3
84	27633	56163	27838	66121	66121	42.1
85	29055	56105	28287	66121	66121	42.8
86	30270	56047	28669	66121	66121	43.4
87	31279	55990	28982	66121	66121	43.8
88	32081	55932	29228	66121	66121	44.2
89	32677	55874	29405	66121	66121	44.5
90	33067	55816	29515	66121	66121	44.6
91	33251	55759	29556	66121	66121	44.7
92	33229	55701	29530	66121	66121	44.7
93	33000	55643	29435	66121	66121	44.5
94	32565	55585	29272	66121	66121	44.3
95	31924	55527	29041	66121	66121	43.9
96	31076	55470	28742	66121	66121	43.5
97	30022	55412	28375	66121	66121	42.9
98	28762	55354	27940	66121	66121	42.3
99	27296	55296	27437	66121	66121	41.5

Elevation	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
100	25623	55239	26866	66121	66121	40.6
101	23745	55181	26227	66121	66121	39.7
102	21659	55123	25520	66121	66121	38.6
103	19368	55065	24745	66121	66121	37.4
104	16871	55007	23902	66121	66121	36.1
105	14167	54950	22990	66121	66121	34.8
106	11257	54892	22011	66121	66121	33.3
107	8140	54834	20964	66121	66121	31.7
108	4818	54776	19848	66121	66121	30.0
109	1289	54719	18665	66121	66121	28.2
110	-2446	54661	19027	66121	66121	28.8
111	-6388	54603	20308	66121	66121	30.7
112	-10535	54545	21657	66121	66121	32.8
113	-14889	54487	23075	66121	66121	34.9
114	-19449	54430	24560	66121	66121	37.1
115	-24216	54372	26113	66121	66121	39.5
116	-29188	54314	27734	66121	66121	41.9
117	-34367	54256	29424	66121	66121	44.5
118	-39752	54199	31181	66121	66121	47.2
119	-45344	54141	33006	66121	66121	49.9
120	-51141	54083	34900	66121	66121	52.8
121	-45614	39881	28342	66879	66879	42.4
122	-40321	39823	26577	66879	66879	39.7
123	-35261	39765	24888	66879	66879	37.2
124	-30436	39707	23277	66879	66879	34.8
125	-25844	39649	21743	66879	66879	32.5
126	-21485	39592	20286	66879	66879	30.3
127	-17361	39534	18906	66879	66879	28.3
128	-13470	39476	17603	66879	66879	26.3
129	-9813	39418	16377	66879	66879	24.5
130	-6390	39361	15228	66879	66879	22.8
131	-3200	39303	14157	66879	66879	21.2
132	-244	39245	13162	66879	66879	19.7
133	2478	39187	13880	66879	66879	20.8
134	4966	39129	14682	66879	66879	22.0
135	7221	39072	15406	66879	66879	23.0
136	9242	39014	16054	66879	66879	24.0
137	11029	38956	16624	66879	66879	24.9
138	12582	38898	17117	66879	66879	25.6
139	13902	38841	17533	66879	66879	26.2
140	14988	38783	17872	66879	66879	26.7
141	15840	38725	18134	66879	66879	27.1
142	16458	38667	18319	66879	66879	27.4
143	16843	38609	18426	66879	66879	27.6
144	16994	38552	18457	66879	66879	27.6
145	16911	38494	18410	66879	66879	27.5
146	16594	38436	18287	66879	66879	27.3
147	16044	38378	18086	66879	66879	27.0
148	15260	38321	17808	66879	66879	26.6
149	14242	38263	17453	66879	66879	26.1

Eleva- tion	Moment	Accum. Download	Resolved Legload	Panel / Span Capacity		% Loaded
150	12990	38205	17021	66879	66879	25.4
151	9391	37397	15564	66879	66879	23.3
152	5557	37339	14280	66879	66879	21.4
153	1490	37282	12919	66879	66879	19.3
154	-2811	37224	13335	66879	66879	19.9
155	-7345	37166	14812	66879	66879	22.1
156	-12114	37108	16366	66879	66879	24.5
157	-17116	37051	17997	66879	66879	26.9
158	-22351	36993	19705	66879	66879	29.5
159	-29636	36245	21859	66879	66879	32.7
160	-37154	36187	24320	66879	66879	36.4
161	-31699	14331	15235	66879	66879	22.8
162	-26492	14273	13498	66879	66879	20.2
163	-21535	14215	11843	66879	66879	17.7
164	-16826	14158	10271	66879	66879	15.4
165	-12367	14100	8780	66879	66879	13.1
166	-8157	14042	7372	66879	66879	11.0
167	-4195	13984	6046	66879	66879	9.0
168	-483	13926	4802	66879	66879	7.2
169	2980	13869	5606	66879	66879	8.4
170	6195	13811	6647	66879	66879	9.9
171	9160	13753	7606	66879	66879	11.4
172	11876	13695	8483	66879	66879	12.7
173	14343	13638	9278	66879	66879	13.9
174	16562	13580	9990	66879	66879	14.9
175	18531	13522	10621	66879	66879	15.9
176	20251	13464	11169	66879	66879	16.7
177	21722	13406	11635	66879	66879	17.4
178	22944	13349	12019	66879	66879	18.0
179	22213	12721	11569	66879	66879	17.3
180	21233	12663	11226	66879	66879	16.8
181	20004	12605	10801	66879	66879	16.2
182	18526	12548	10294	66879	66879	15.4
183	16798	12490	9705	66879	66879	14.5
184	14822	12432	9034	66879	66879	13.5
185	12597	12374	8281	66879	66879	12.4
186	10123	12316	7445	66879	66879	11.1
187	7400	12259	6527	66879	66879	9.8
188	4427	12201	5528	66879	66879	8.3
189	1206	12143	4446	66879	66879	6.6
190	-2265	12085	4776	66879	66879	7.1
191	0	750	250	66879	66879	0.4
192	0	0	0	66879	66879	0.0
193	0	0	0	66879	66879	0.0

TOWER DESIGN CONDITIONS

This tower has been designed to conform to the requirements of ANSI/EIA/TIA 222-F recommended standard for 85 mph wind speed with 1/2" radial ice. Worst case load condition is wind with ice with load reduction. Allowable steel stresses per AISC ASD 9th Edition Allowable concrete stresses per ACI 318-89.

MATERIAL SPECIFICATIONS

Tower Legs: ASTM A500-C, Fy > 58 ksi.
 All other Steel: ASTM A36, Fy > 36 ksi
 Hardware: ASTM A325 Hot Dipped Galvanized Bolts with Anco Nuts.
 Galvanizing: ASTM A123
 Guy Anchor Shaft: ASTM A36M, Fy > 48 ksi

TOWER LOADING CONDITIONS

QTY	Antenna	Elevation	Windload	Deadload	
3	12' Cellular Boom	191	290	170	Verizon Wireless
12	ALP 9011	191	116	20	
3	8' Cellular Boom	178	226	130	Nextel
9	ALP 9011	178	114	20	
3	12' Cellular Boom	158	275	170	Sprint PCS
9	ALP 9011	158	110	20	
1	G42 Torque Arm	160	527	262	Future
3	12' Cellular Boom	150	271	170	
12	ALP 9011	150	109	20	
1	G42 Torque Arm	120	485	262	

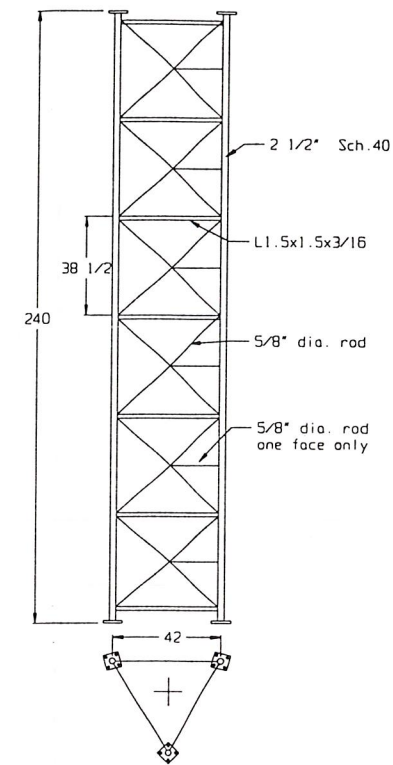
QTY	Type	Elevation Start	Elevation Stop	#/ft	Windload	Deadload
1	Tower Span 4	160	190	249.0	57.8	
1	Tower Span 3	120	160	233.7	57.8	
1	Tower Span 2	60	120	206.3	57.8	
1	Tower Span 1	0	60	154.4	63.9	

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

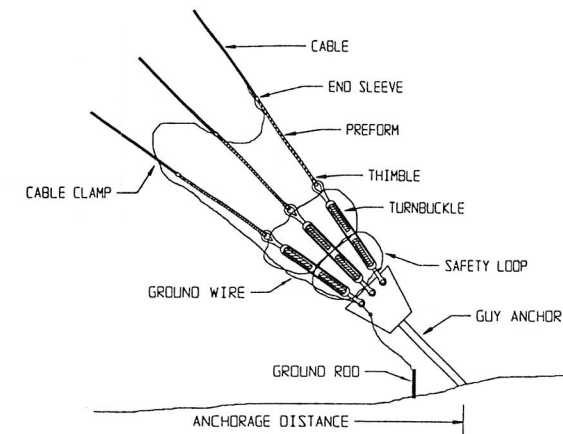
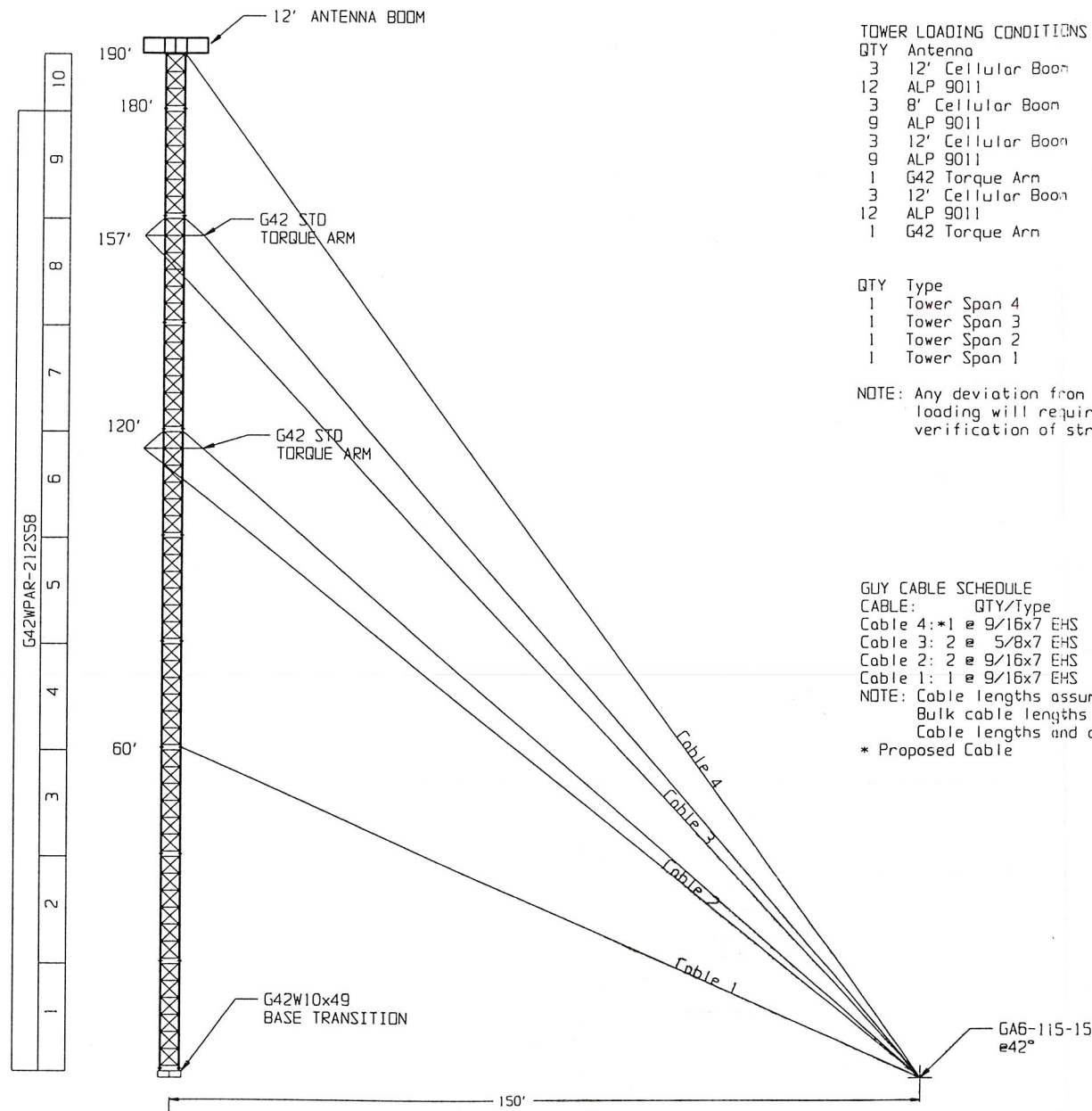
GUY CABLE SCHEDULE

CABLE	QTY/Type	Length	Ti	Turnbuckle	Preform	Thnbl	Endslve	Shckl
Cable 4	*1 @ 9/16x7 EHS	239'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"
Cable 3	2 @ 5/8x7 EHS	216'	6360#	1"x18" J-J	5/8" BG	3/4"	65268	3/4"
Cable 2	2 @ 9/16x7 EHS	188'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"
Cable 1	1 @ 9/16x7 EHS	157'	5250#	7/8"x12" J-J	9/16" BG	5/8"	65267	3/4"

NOTE: Cable lengths assume anchors at elevation 0'. Bulk cable lengths assume 20' tails. Cable lengths and anchor layout must compensate for site topography.
 * Proposed Cable



G42WPAR TOWER SECTION



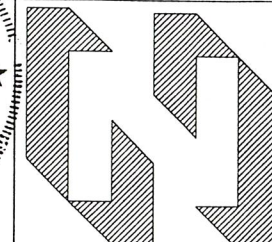
CABLE HARDWARE ASSEMBLY
 NOTE: Install cable hardware per manufacturer's specifications.

INSTALLATION NOTES

1. Installation of tower must be performed by a qualified tower erector.
2. Install sections with section number on the bottom, and climbing device is aligned.
3. Install safety climb, lights, cable attachments per manufacturer's recommendations.
4. Do not lift more than 100' of assembled tower sections.
5. Install "sharp" edge of adapter plates against face of tower.
6. Plumb and tension tower and cables as erected.
7. *Ti*=Initial tension of cable.

G42 Section Weights: 785/695 +/-
 Top Frame: 1000 +/-

SECTION DESIGNATION:
 G42WPAR-212S55 = 2-1/2"; (212), (S)Sch.40/(EH)Sch.80, (55)ksi, strength
 96-47-xx = Year-(47) ksi strength-xx



FRED A. NUDD CORPORATION		
Route 104*Ontario, New York 14519*315/524-2531		
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DATE: 7/31/00	180' TOWER MT. EXTENSION	
COT EASTFORD, CT	DRAWING NUMBER: 00-5874A-1	