

QC Development
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Mark.Roberts@QCDevelopment.net

September 27, 2019

Melanie A. Bachman Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Notice of Exempt Modification – New Cingular Wireless PCS, LLC (AT&T) – CT2490 886 Main Street, East Hartford, CT 06108 N 41.76944444 W 72.64277778

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the rooftop level (112' and 120' AGL) of the 11-story apartment building at 886 Main Street, East Hartford, CT. The property is owned by Hartford East Associates. AT&T now intends to add three (3) CCI HPA-65R-BU66A antennas and (3) Ericsson B25 4415 Remote Radio Units (RRU).

This facility was approved by the Connecticut Siting Council in Petition # 324 on August 9, 1994 and AT&T's shared use of the facility was approved on September 19, 2014 (TS-CING-043-140822). These approvals included no conditions that could feasibly be violated by this proposed modification, including total facility height and mounting restrictions. This modification therefore complies with the aforementioned approvals.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Ms. Marcia LeClerc, Mayor of the Town of East Hartford, and the East Hartford Development & Planning Department as well as the property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Please feel free to call me at (860) 670-9068 with any questions regarding this matter. Thank you for your consideration.

Sincerely,

Mark Roberts

QC Development

Consultant for AT&T

Attachments

cc: Mayor Marcia LeClerc - Elected Official Jeffrey Cormier – Town Planner

Hartford East Associates - Property Owner

Power Density

Existing Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%МРЕ
Other Carriers*							5.85%
AT&T LTE	1	1476	107	0.0520	700	0.4667	1.12%
AT&T LTE	1	1000	107	0.0353	850	0.5667	0.62%
AT&T 5G	1	1000	107	0.0353	850	0.5667	0.62%
AT&T LTE	2	3664	107	0.2583	1900	1.0000	2.58%
AT&T LTE	1	3837	107	0.1353	2100	1.0000	1.35%
AT&T LTE	1	1285	107	0.0453	2300	1.0000	0.45%
Site Total							12.60%

^{*}Per CSC Records (available upon request, includes calculation formulas)

Proposed Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm^2)	Freq. Band (MHz**)	Limit S (mW /cm^2)	%МРЕ
Other Carriers*							5.85%
AT&T LTE	1	1476	112	0.0472	700	0.4667	1.01%
AT&T LTE	1	1000	112	0.0320	850	0.5667	0.56%
AT&T 5G	1	1000	112	0.0320	850	0.5667	0.56%
AT&T LTE	2	3664	112	0.2345	1900	1.0000	2.35%
AT&T LTE	1	4842	112	0.1550	1900	1.0000	1.55%
AT&T LTE	1	3837	112	0.1228	2100	1.0000	1.23%
AT&T LTE	1	1285	112	0.0411	2300	1.0000	0.41%
Site Total							13.53%

^{*}Per CSC Records (available upon request, includes calculation formulas)

^{**} If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

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SITE NAME: EAST HARTFORD MAIN STREET

SITE NO.: CT2490

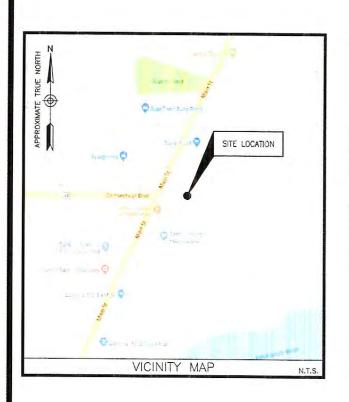
886 MAIN STREET

EAST HARTFORD, CT 06108

FA CODE: 10553970

PACE ID: MRCTB038215

PROJECT: LTE 1900 BWE



SITE COORDINATES:

LATITUDE: 41' 45' 09.99" N

LONGITUDE: 72' 38' 34.00" W

*BASED ON PROVIDED RFDS

ELEVATION DATA:

GRADE ELEVATION AT BUILDING = 38'±

*BASED ON GOOGLE EARTH PRO

SITE INFORMATION

- · ADD (3) NEW ANTENNA PIPE MASTS & MOUNTING HARDWARE
- ADD (3) NEW 6' HPA-65R-BUGAA HEX ANTENNAS
- . ADD (3) NEW B25-4415 RRUS UP TOP

PROJECT DESCRIPTION

PROPERTY OWNER:

TOWN OF EAST HARTFORD
740 MAIN STREET

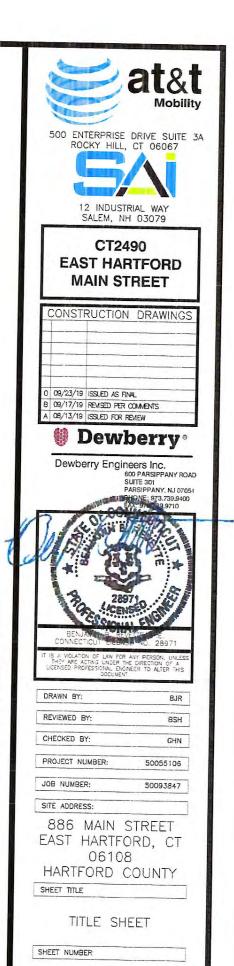
APPLICANT/LESSEE:
AT&T MOBILITY
500 ENTERPRISE DRIVE, SUITE JA
ROCKY HILL, IT 06067

THIS DOCUMENT WAS DEVELOPED TO REFLECT A SPECIFIC SITE AND ITS SITE
CONDITIONS AND IS NOT TO BE USED FOR ANOTHER SITE OR WHEN OTHER
CONDITIONS PERTAIN, REUSE OF THIS DOCUMENT IS AT THE SOLE RISK OF

A.D.A. COMPLIANCE: FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION.

SITE NAME:

SHEET NUMBER	DESCRIPTION
T-1	T/"LE SHEET
G-1	GENERAL NOTES
C-1	ROOF PLAN
C-2	NORTH ELEVATION & EQUIPMENT PLAN
C-3	EXISTING & PROPOSED ANTENNA LAYOUTS
C-4	CONSTRUCTION DETAILS I
C-5	CONSTRUCTION DETAILS II
C-6	P.UMBING DIAGRAM
E-1	GROUNDING NOTES & DETAILS
	SHEET INDEX



1-1

GENERAL NOTES:

- FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY: PROJECT MANAGEMENT SAI COMMUNICATIONS, INC. CONTRACTOR - GINERAL CONTRACTOR (CONSTRUCTION) OWNER - ATAT MOBILITY OEM - ORIGINAL EQUIPMENT MANUFACTURER
- PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING CONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF PROJECT
- ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORD NANCES, CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULLES, RUSULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK.
- ALL WORK CARRIED OU" SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- 5. DRAWINGS PROVIDED HERE ARE NOT TO SCALE UNLESS OTHERWISE NOTED AND ARE INTENDED TO SHOW OUTLINE
- UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FUFNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS IN 3 CATED ON THE DRAWINGS.
- THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATIFICALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY PROJECT MANAGEMENT.
- CONTRACTOR SHALL DE EMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER GROUNDING AND TELCO PLAN DRAWING, CONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. CONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH PROJECT
- THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE OWNER.
- CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF VLL SCRAP MATERIALS SUCH AS CONTIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
- 12. CONTRACTOR SHALL LEGGE PREMISES IN CLEAN CONDITION.
- 13. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE PROJECT DESCRIBED HEREIN. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER THE CONTRACT.
- CONTRACTOR SHALL NOTEY DEWBERRY 48 HOURS IN ADVANCE OF POURING CONCRETE, OR BACKFILLING TRENCHES. SEALING ROOF AND WALL PENETRATIONS & POST DOWNS, FINISHING NEW WALLS OR FINAL ELECTRICAL CONNECTIONS FOR ENGINEER REVIEW.
- 15. CONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK, ALL DIMENSIONS OF EXISTIN 3 CONSTRUCTION SHOWN ON THE CRAWINGS MUST BE VERIFIED, CONTRACTOR SHALL NOTIFY PROJECT MANAGEMENT OF ANY DISCREPANCIES PRIOR TO CRDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 16. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY CONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORL ON EXISTING EQUIPMENT MUST BE COORDINATED WITH LAND LORD. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
- 17. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC FADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER, PERSONAL RF EXPOSL RE MONITORS ARE ADMISED TO BE WORN TO ALERT OF
- CONTRACTOR, SUBCONTRACTORS AND ANY SITE SPECIFIC PART/ PRODUCT/ CONCEALMENT MANUFACTURER TO FIELD VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS PRIOR TO MANUFACTURING, FABRICATION OF CONSTRUCTION.

- THE CONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
- ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY CONTRACTOR. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE S4FETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO:
- B) CONFINED SPACE C) FLECTRICAL SAFETY
- D) TRENCHING & EXCAVATION.
- ALL SITE WORK SHALL BE AS INDICATED ON THE DRAWINGS AND PROJECT SPECIFICATIONS.
- IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES, TOP SOIL AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
- ALL EXISTING INACTIVE SEWER, WATER, CAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLIGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF CONTRACTOR, OWNER
- 6. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION.
- 7. THE CONTRACTOR SHALL PROVIDE SITE SIGNAGE, IN ACCORDANCE WITH THE AT&T SPECIFICATION FOR SITE SIGNAGE.
- THE SITE SHALL BE (RADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE TRANSMISSION EQUIPMENT AND TOWER AREAS.
- NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED DIN FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
- THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION, SEE SOIL COMPACTION NOTES.
- THE AREAS OF THE CWNER'S PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION.
- 12. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL JURISDICTION'S GUIDELINES FOR EROSION AND SEDIMENT CONTROL.

STRUC"URAL STEEL NOTES:

- ALL STEEL WORK SHALL BE PAINTED OR GALVANIZED IN ACCORDANCE WITH THE DRAWINGS UNLESS NOTED OTHERWISE, STRUCTURAL STEEL SHALL BE ASTM-A-36 UNLESS OTHERWISE NOTED ON THE SITE SPECIFIC DRAWINGS. STELL DESIGN, INSTALLATION AND BOLITIC SHALL BE PERFORMED IN ACCORDANCE WITH THE AMERICAN INSTITLE OF STEEL CONSTRUCTION (AISC) "MANUAL OF STEEL CONSTRUCTION".
- ALL WELDING SHALL BE PERFORMED USING ETOXX ELECTRODES AND WELDING SHALL CONFORM TO AISC, WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION". PAINTED SURFACES SHALL BE TOUCHED UP.
- 3. BOLIED CONNECTIONS SHALL BE ASTM 4325 BEARING TYPE (3/4"0) CONNECTIONS AND SHALL HAVE MINIMUM OF
- NOI--STRUCTURAL CONNECTIONS FOR SIEEL GRATING MAY USE 5/8" DIA "STM A 307 BOLTS UNLESS NOTED
- INSTALLATION OF CONCRETE EXPANSION, WEDGE ANCHOR, SHALL BE PER MUNUFACTURER'S WRITTEN RECOMMENDED INSTALLATION OF CONCRETE EXPANSION, WELIGE ANCHOR, SHALL SE PER MANUFACTURER'S WRITTEN RECOMMENDED PROCEDURE. THE ANCHOR BOLT, DOWE. OR ROD SHALL CONFORM TO MANUFACTURER'S RECOMMENDATION FOR EMSEDMENT DEPTH OR AS SHOWN ON THE DRAWINGS. NO REBAR SHALL BE CUT WITHOUT PRIOR CONTRACTOR AFFROVAL WHEN DRILLING HOLES IN CONCRETE. SPECIAL INSPECTIONS, RECUIRED BY GOVERNING CODES, SHALL BE PERFORMED IN ORDER TO MAINTAIN MATUFACTURER'S MAXIMUM ALLOWABLE LOADS, ALL EXPANSION, WEDGE ANCHORS SHALL BE STANLESS STEEL OR HOT DIPPED GALVANIZED. EXPANSION BOLTS SHALL BE PROVIDED BY RAMSET/REDHEAD OR APPROVED FOLIAL
- CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR ENGINEER REVIEW & APPROVAL ON PROJECTS REQUIRING STRUCTURAL STEEL.
- 7. ALL STRUCTURAL STEEL WORK SHALL BE DONE IN ACCORDANCE WITH AISC SPECIFICATIONS.

SOIL COMPACTION NOTES FOR SLAB ON GRADE:

- EXCAVATE AS REQUIRED TO REMOVE VEGETATION & TOPSOIL EXPOSE UNDISTURBED NATURAL SUBGRADE AND PLACE CRUSHED STONE AS REQUIRED.
- CONPACTION CERTIFICATION: AN INSPECTION AND WRITTEN CERTIFICATION BY A QUALIFIED GEOTECHNICAL TECHNICIAN OR ENGINEER IS ACCEPTABLE.
- AS 4N ALTERNATIVE TO INSPECTION AND WRITTEN CERTIFICATION, THE "UND STURBED SOIL" BASE SHALL BE COMPACTED WITH "COMPACTION EQUIPMENT", LISTED BELOW, TO AT LEAST 90% MODIFIED PROCTOR MAXIMUM DENSITY PER ASTM D 1557 METHOD C.
- COMPACTED SUBBASE SHALL BE UNIFORM & LEVELED, PROVIDE 6" MINIMUM CRUSHED STONE OR GRAVEL COMPACTED IN 3" LIFTS ABOVE COMPACTED SOIL GRAVEL SHALL BE NATURAL OR CRUSHED WITH 100% PASSING 1"
- AS AN ALTERNATIVE TO ITEMS 2 AND 3 PROOFROLL THE SUBGRADE SOILS WITH 5 PASSES OF A MEDIUM SIZES MBPATORY PLATE COMPACTOR (SUCH AS BOMAG BPR 30,38) OR HAND-C PERATED SINGLE DRUM VIBRATORY FOLLER (SUCH AS BOMAG BW 55E). ANY SOFT AREAS THAT ARE ENCOUNTERED SHOULD BE REMOVED AND REPLACED MITH A WELL-GRADED GRANULAR FILL, AND COMPACTED AS STATED ABOVE.

COMPACTION EQUIPMENT:

HAND OPERATED DOUBLE DRUM, VIBRATORY ROLLER, VIBRATORY PLATE COMPACTOR OR JUMPING JACK COMPACTOR.

FIELD VERIFICATION:
CONTRACTOR SHALL FIELD VERIFY SCOPE OF WORK, AT&T ANTENNA PLATFORM LOCATION AND ANTENNAS TO BE
REPLACED.

- CONTRACTOR SHALL COORDINATE RF WORK AND PROCEDURES WITH PROJECT MANAGEMENT.
- CABLE LADDER RACK-
- CONTRACTOR SHALL FURNISH AND INSTALL CABLE LADDER RACK, CASLE TRAY, AND CONDUIT AS REQUIRED TO SUPPORT CABLES TO THE NEW BTS LOCATION.

ELECTRICAL INSTALLATION NOTES:

- ALL ELECTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS, NEC AND ALL APPLICABLE LOCAL CODES.
- CONTRACTOR SHALL MODIFY EXISTING CABLE TRAY SYSTEM AS REQUIRED TO SUPPORT RF AND TRANSPORT CABLING TO THE NEW BTS EQUIPMENT, CONTRACTOR SHALL SUBMIT MODIFICATIONS TO PROJECT NAVAGEMENT FOR APPROVAL.
- CONDUIT ROUTINGS ARE SCHEMATIC. CONTRACTOR SHALL INSTALL CONDUITS SO THAT ACCESS TO EQUIPMENT IS NOT
- WIRING, RACEWAY AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE NEC.
- 5. ALL CIRCUITS SHAL. BE SEGREGATED AND MAINTAIN MINIMUM CABLE SEPARATION AS REQUIRED BY THE NEC.
- 6. CABLES SHALL NOT BE ROUTED THROUGH LADDER-ST'LE CABLE TRAY RUNGS
- EACH END OF EVERY POWER, POWER PHASE CONDUCTOR (I.E., HOTS), GROUNDING, AND TI CONDUCTOR AND CABLE SHALL BE LABELED WITH COLOR-CODED INSULATION OF ELECTRICAL TAPE (3M BRAND, 1/2 INCH PLASTIC ELECTRICAL TAPE WITH UV PROTECTION, OR EQUAL). THE IDENTIFICATION METHOD SHALL CONFORM WITH NEC & OSHA, AND MATCH EXISTING INSTALLATION REQUIREMEN'S.
- ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABILED WITH ENGRAVED LAMACOID PLASTIC LABELS. ALL EQUIPMENT SHALL BE LABELED WITH THEIR VOLTAGE RATING, PHASE CONFIGURATION, WIRE CONFIGURATION, POWER OR AMPACITY RATING, AND BRANCH CIRCUIT ID NUMBERS (I.E., PANELBOARD AND CIRCUIT D'S).
- PANELBOARDS (ID NUMBERS) AND INTERNAL CIRCUIT BREAKERS (CIRCUIT ID NUMBERS) SHALL BE CLEARLY LABILED
- 10. ALL TIE WRAPS SHALL BE CUT FLUSH WITH APPROVED CUTTING TOOL TO REMOVE SHARP EDGES.
- 11. POWER, CONTROL, AND EQUIPMENT GROUND WIRING IN TUBING OR CONDUIT SHALL BE SINGLE CONDUCTOR (SIZE 14 AWG OR LARGER), 500V, OIL RESISTANT THINN OR THINN-2, CLASS B STRANDED COPPER LABLE RATED FOR 90 °C (WET AND DRY) OPERATION; USTED OR LABELED FOR "HE LOCATION AND RACEWAY SYSTEM USED, UNLESS OTHERWISE SPECIFILD.
- 12. POWER PHASE CONDUCTORS (I.E., HOTS) SHALL BE LABELED WITH COLOR-CODED INSULATION OR ELECTRICAL TAPE (3M BRAND, 1/2 INCH PLASTIC ELECTRICAL TAPE WITH JV PROTECTION, OR EQUAL) PHASE CONDUCTOR COLOR CODES SHALL CONFORM WITH THE NEC & OSHA AND VATCH EXISTING INSTALLATION REQUIREMENTS.
- SUPPLEMENTAL EQLIPMENT GROUND WIRING LOCATED INDOORS SHALL BE SINGLE CONDUCTOR (SIZE 6 AWG OR LARGER), 600V, CI. RESISTANT THIN OR THINN-2 GREEN INSULATION, CLASS B STRANDED COPPER CABLE RATED FOR 90°C (WET AND DRY) OPERATION; LISTED OR LABSLED FOR THE LOCATION AND RACEWAY SYSTEM USED, UNLESS
- SUPPLEMENTAL EQUIPMENT GROUND WIRING LOCATED CUTDOORS, OR BELOW GRADE, SHALL BE SINGLE CONDUCTOR #2 AWG SOLID TINNED COPPER CABLE, UNLESS OTHERWISE SPECIFIED.
- 15. POWER AND CONTROL WIRING, NOT IN TUBING OR CONDUIT, SHALL BE MULTI-CONDUCTOR, TYPE TO CABLE (SIZE 14 AWG OR LARGER), 200V, OIL RESISTANT THEN OR THWW-2, CLASS B STRANDED COPPER DABLE RATED FOR 90°C (WET AND DRY) OPERATION; WITH OUTER JACKET; LISTED OR LABELED FOR THE LOCATION USED, UNLESS OTHERWISE
- 16. ALL POWER AND POWER GROUNDING CONNECTIONS SHALL BE CRIMP-STYLE, COMPRESSION WIRE LUGS AND WIRENUTS BY THOMAS AND BETTS (OR EQUAL). LUGS AND WIRENUTS SHALL BE RATED FOR OPERATION AT NO LESS THAN 75°C (90°C IF AVAILABLE).
- 17. RACEWAY AND CABLE TRAY SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, U., ANSI/IEEE, AND NEC.
- 18. NEW RACEWAY OR CABLE TRAY WILL MATCH THE EXISTING INSTALLATION WHERE POSSIBLE.
- 19. ELECTRICAL METALLIC TUBING (EMT) OR RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHIZDLE 40, OR RIGID PVC SCHEDULE 80 FOR LOCATIONS SUBJECT TO PHYSICAL DAMAGE) SHALL BE USED FOR EXPOSED INDOOR LOCATIONS.
- 20. ELECTRICAL METALLIC TUBING (EMT), ELECTRICAL NONVETALLIC TUBING (ENT), OR RIGID NONMETALLIC CONDUIT (RIGID PVC, SCHEDULE 40) SHALL BE USED FOR CONCEALED NDOOR LOCATIONS.
- 21. GALVANIZED STEEL INTERMEDIATE METALLIC CONDUIT (IN.C) SHALL BE USED FOR OUTDOOR LOCATIONS ABOVE GRADE.
- RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHEDULE 40 OR RIGID PVC SCHEDULE 80) SHALL BE USED
 UNDERGROUND; DIRECT BURIED, IN AREAS OF OCCASIO VAL LIGHT VEHICLE TRAFFIC OR ENCASED IN REINFORCED
 CONCRETE IN AREAS OF HEAVY VEHICLE TRAFFIC.
- 23. LIQUID-TIGHT FLEXIBLE METALLIC CONDUIT (LIQUID-TITE FLEX) SHALL BE USED INDOORS AND OUTDOORS, WHERE VIBRATION OCCURS OR FLEXIBILITY IS NEEDED.
- 24. CONDUIT AND TUBING FITTINGS SHALL BE THREADED OR COMPRESSION-TYPE AND APPROVED FOR THE LOCATION USED. SETSCREW FITINGS ARE NOT ACCEPTABLE.
- 25. CABINETS, BOXES, AND WIREWAYS SHALL BE LISTED OF LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA,
- 26. CABINETS, BOXES, AND WIREWAYS TO MATCH THE EXISTING INSTALLATION WHERE POSSIBLE
- 27. WIREWAYS SHALL BE EPOXY-COATED (GRAY) AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARD; SHALL BE PANDUIT TYPE E (OR EQUAL); AND RATED NEMA 1 (OR BETTER) INDOORS, OR VEMA 3R (OR BETTER)
- 28. EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES, AND PULL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET STEEL, SHALL MEET OR EXCEED UL 50, AND RATED NEMA 1 (OR HETTER) INDOORS, OF
- 29. METAL RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED, GR NON-CORRODING; SHALL MEET OR EXCEED UL 514A AND NEMA OS 1; AND RATED NEMA 1 (OR BETTER) INDOORS, OR WEATHER PROTECTED (WP OF BETTER) OUTDOORS.
- 30. NONMETALLIC RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2; AND RATED NEMS 1 (OR BETTER) INDOCRS, OR WEATHER PROTECTED (WP OR BETTER) OUTDOORS.
- 31. THE CONTRACTOR SHALL NOTIFY AND OBTAIN NECESSARY AUTHORIZATION FROM PROJECT MANAGEMENT BEFORE COMMENCING WORK ON THE AC POWER DISTRIBUTION PANELS.
- 32. THE CONTRACTOR SHALL PROVIDE NECESSARY TAGGING ON THE BREAKERS, CABLES AND DISTRIBUTION PANELS N ACCORDANCE WITH THE APPLICABLE CODES AND STANDARDS TO SAFEGUARD AGAINST LIFE AND PROPERTY.



500 ENTERPRISE DRIVE SUITE 3A ROCKY HILL, CT 06067



12 INDUSTRIAL WAY SALEM, NH 03079

CT2490 EAST HARTFORD MAIN STREET

(CONST	RUCTION DRAWINGS
	_	
-	-	
0	09/23/19	ISSUED AS FINAL
В	09/17/19	REVISED PER COMMENTS
A	08/13/19	ISSUED FOR REVIEW



Dewberry Engineers Inc. 600 PARSIPPANY ROAD SUITE 301 PARSIPPANY, NJ 07054



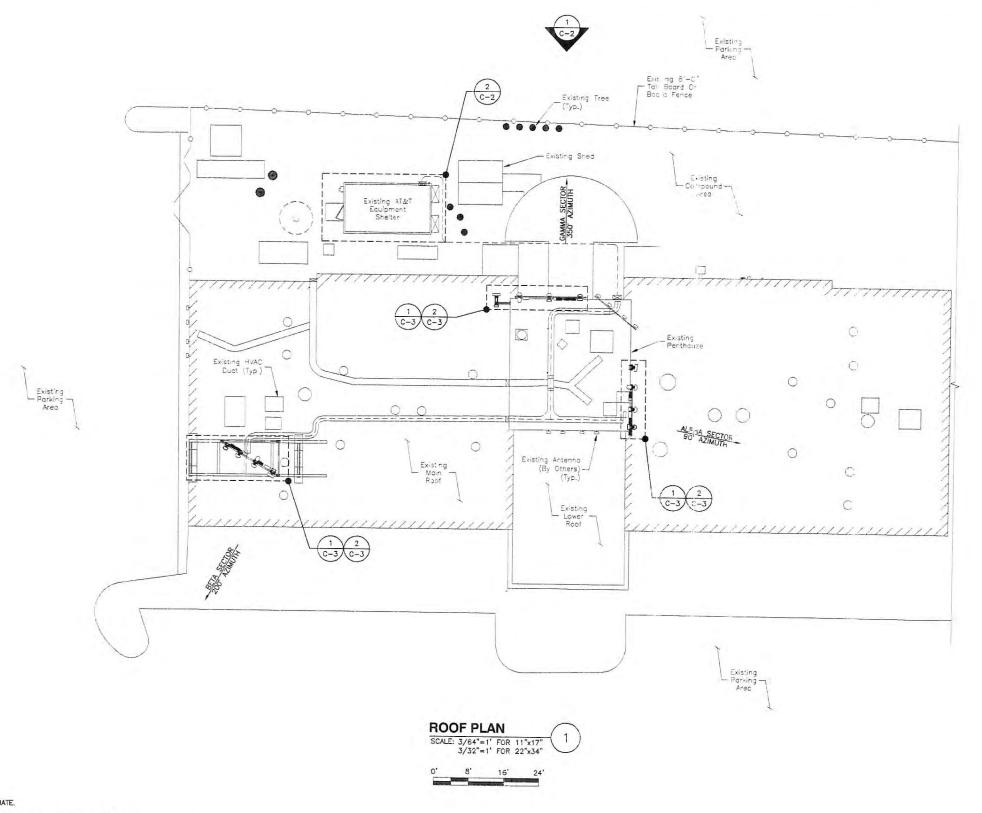
BJR
BSH
GHN
50055106
50093847

886 MAIN STRFFT EAST HARTFORD, CT 06108 HARTFORD COUNTY SHEET TITLE

SHEET NUMBER

SITE ADDRESS:

GENERAL NOTES





- 1. NORTH SHOWN AS APPROXIMATE.
- 2. NOT ALL EXISTING & PROPOSED INFORMATION SHOWN FOR CLARITY.
- ROOF PLAN BASED ON SITE VISIT BY CONDUCTED BY DEWBERRY ENGINEERS INC. ON 12/10/18 AND EXISTING DRAWINGS BY HUDSON DESIGN GROUP LLC DATED 11/08/16 & EXISTING DRAWINGS BY DEWBERRY ENGINEERS INC. REV 0 DATED 04/24/19.
- ALL PROPOSED EQLIPMENT, INCLUDING ANTENNAS, COAX, SURGE ARRESTORS, TMA'S, RRU'S, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS BY DEWBERRY ENGINEERS INC DATED 09/16/19.
- CONTRACTOR TO VERIFY THE ANTENNA FRAMES MATCH THE EXISTING CONSTRUCTION DRAIVINGS BY HUDSON DESIGN GROUP LLC DATED 11/08/16.



500 ENTERPRISE DRIVE SUITE 3A ROCKY HILL, CT 06067



12 INDUSTRIAL WAY SALEM, NH 03079

CT2490 EAST HARTFORD MAIN STREET

	CONST	RUCTION DRAWII	NGS
		TOUTION BRANII	103
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DRAWN BY:	BJR
REVIEWED BY:	BSH
CHECKED BY:	GHN
PROJECT NUMBER:	50055106
JOB NUMBER:	50093847

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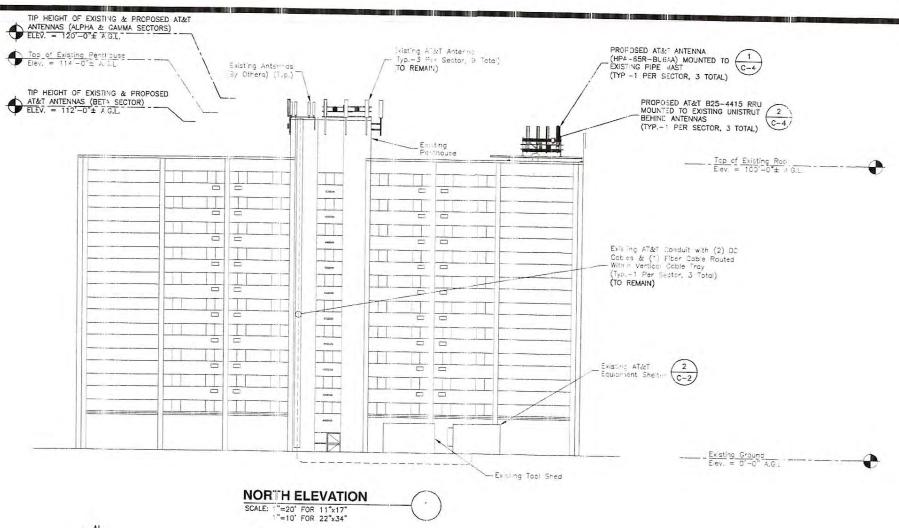
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C-1



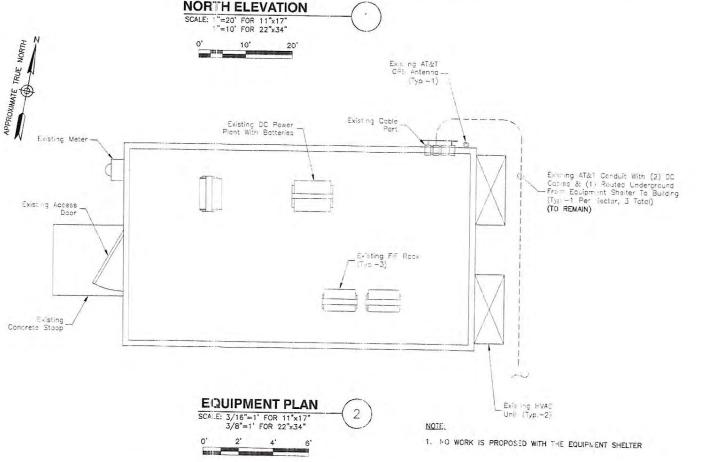
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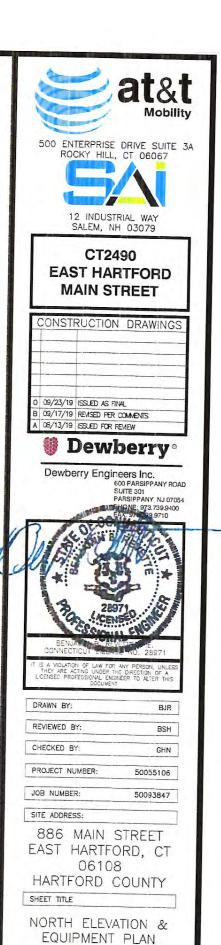
INC. DATED 09/16/19.

1. NOT ALL EXISTING & PROPOSED INFORMATION SHOWN FOR CLARITY.

 ELEVATION BASED ON SITE VISIT BY CONDUCTED BY DEWBERRY ENGINEERS INC. ON 07/26/19 AND EXISTING DRAWINGS BY HUDSON DESIGN GROUP LLC DATED 11/08/16.

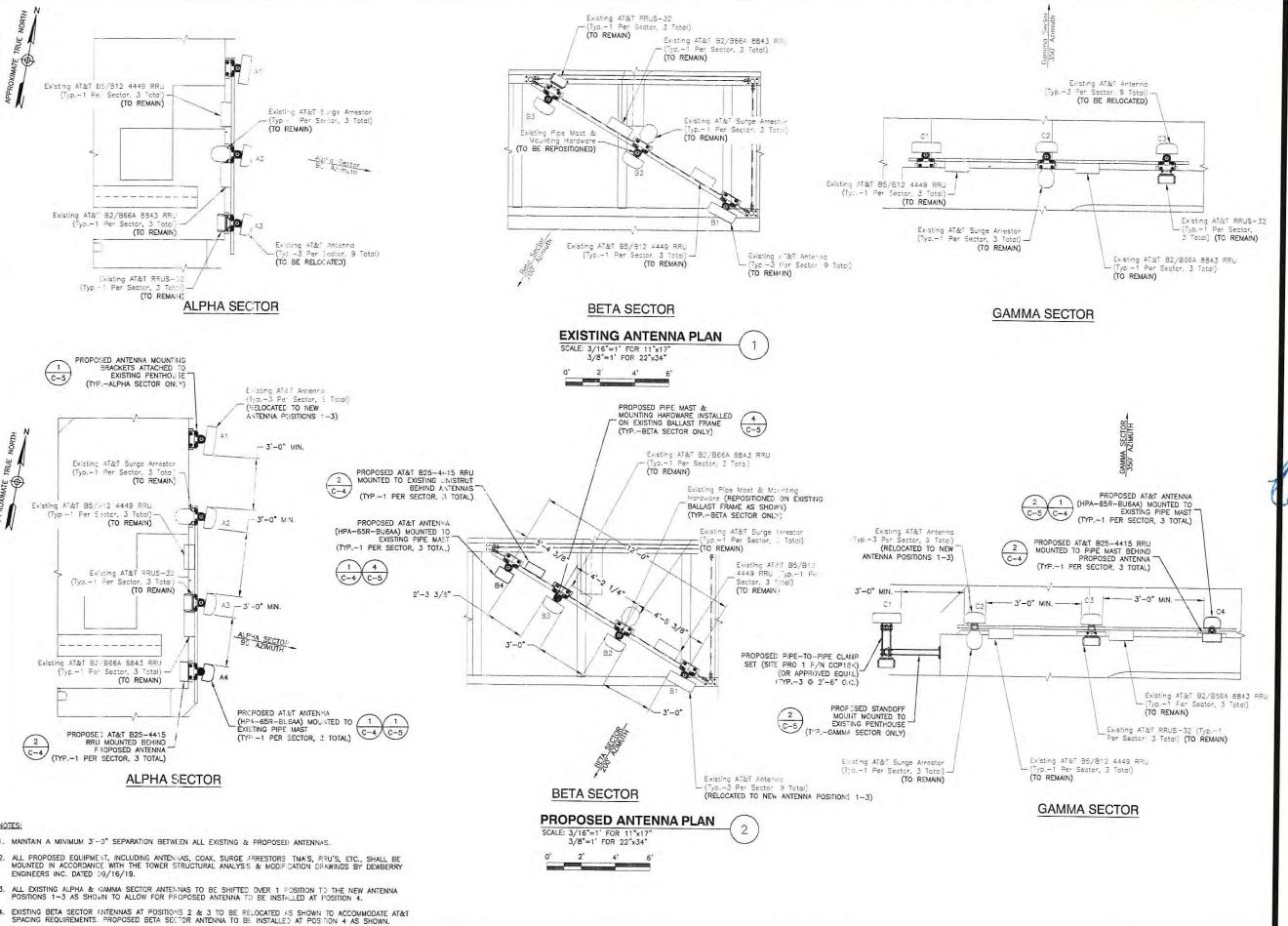
3. ALL PROPOSED EQUIPMENT, INCLUDING ANTENNAS, COAX, SURGE ARRESTORS, TMA'S, RRU'S, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS & MODIFICATION DRAWINGS BY DEWBERRY ENGINEERS





C-2

SHEET NUMBER





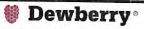
500 ENTERPRISE DRIVE SUITE 3A ROCKY HILL, CT 06067



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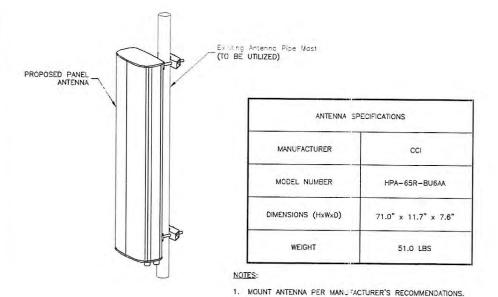
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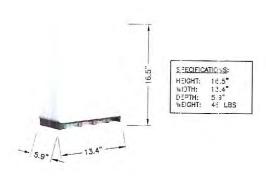
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2. WEIGHT INCLUDES MOUNTING BRACKETS.

SCALE: N.T.S.

ANTENNA DETAIL

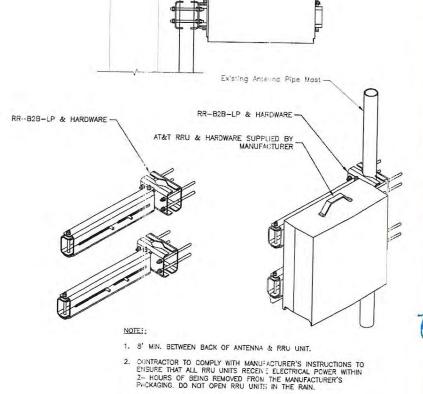


ERICSSON RRUS B25 4415

RRU NOTES:

- 1. MOUNT EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.
- GROUND EQUIPMENT AND MOUNTS PER MANUFACTURER'S RECOMMENDATIONS AND ATTET STANDARDS.
- 3. CONFIRM REQUIRED EQUIPMENT WITH THE LATEST RFDS.

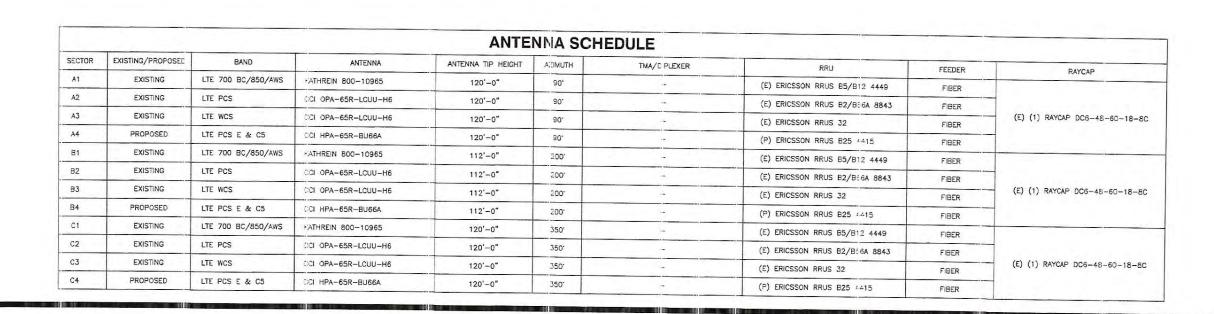




RFIH DUAL BRACKET MOUNT DETAIL

- Existing Antenna Pipe Most

AT&T RRU & HARDWARE SUPPLIED BY MANUFACTURER



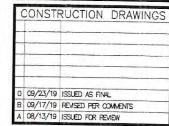


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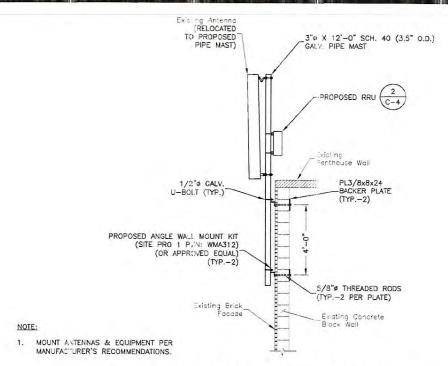
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JOB NUMBER:	50093847
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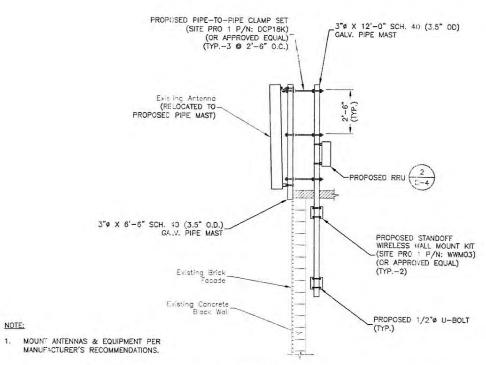
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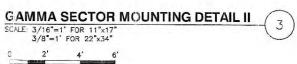
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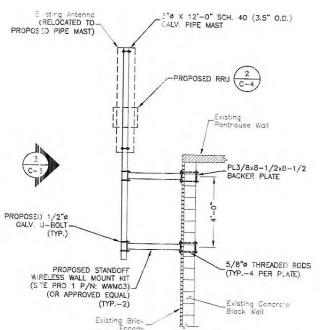






NOTE:





GAMMA SECTOR MOUNTING DETAIL

SCPLE: 3/16"=1' FOR 11"x17" 3/8"=1' FOR 22"x34"

NOTE:

MOUNT ANTENLAS & EQUIPMENT FER MANUFACTUREF'S RECOMMENDATIONS.

3"¢ (9'-0" SCH. 40 (3.5" O.D.)_ GALV. PIPE MAST WITH CAP Existing Arcenra -(RELOCATED TO PROPOSED FIPE MAST) PFOPOSED L3x3x3/8 (0'-9" LONG) (TYP.-2) Existing .3x3x3/8 Horizontal Ballast Mount Framing (TO BE UTILIZED) PROPOSED 1/2"ø U-BOLT (TYP.) 1/2"ø A325 STRUCTURAL BOLTS

MOUNT ANTENNAS & EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.

BETA SECTOR MOUNTING DETAIL SCALE: 1/4"=1' FOR 11"x1'7" 1/2"=1' FOR 22"x3+"



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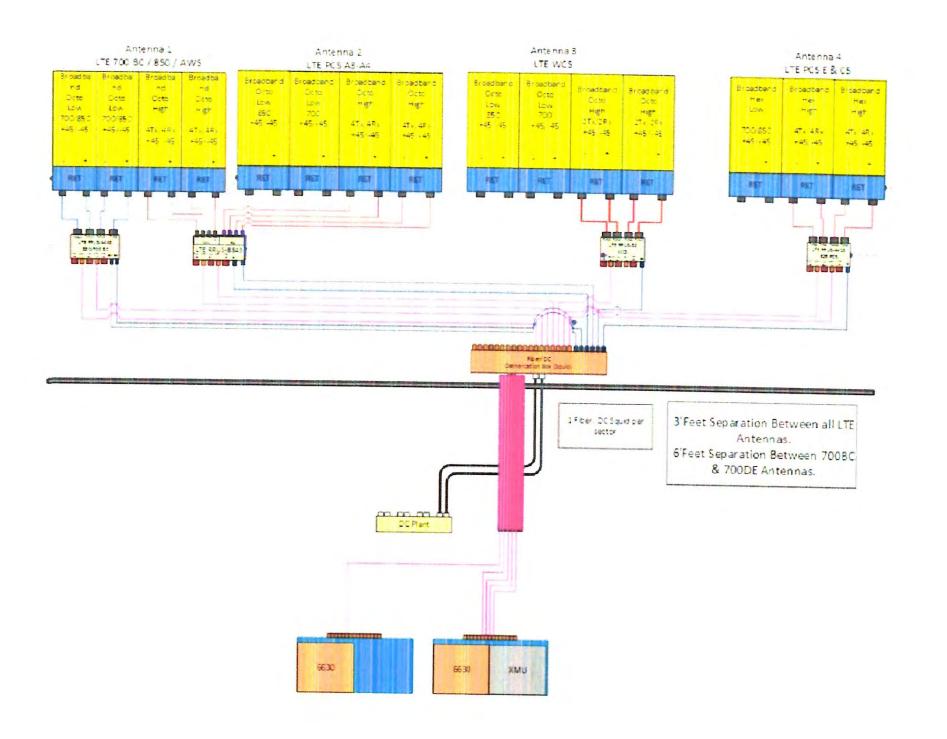
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CHECKED BY:	GHN
PROJECT NUMBER:	50055106
JOB NUMBER:	50093847
SITE ADDRESS:	
886 MAIN	STREET

EAST HARTFORD, CT 06108 HARTFORD COUNTY SHEET TITLE

DETAILS II

CONSTRUCTION

SHEET NUMBER



PLUMBING DIAGRAM

SCALE: N.T.S.

NOTE:

 PLUMBING DIAGRAM BASED ON RFDS V1.00 DATED 02/25/19. CONFIRM FINAL PLUMBING DIAGRAM WITH THE LATEST RFDS.



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DRAWN BY: BJR

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CHECKED BY: GHN

PROJECT NUMBER: 50055106

JOB NUMBER: 50093847

SITE ADDRESS:

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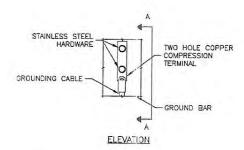
PLUMBING DIAGRAM

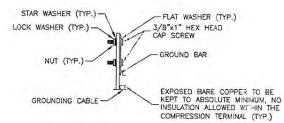
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GROUNDING NOTES:

- 1. THE CONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ). THE SITE—SPECFIC (UL. LPI, OR NFPA) LIGHTING "ROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORPIA AND TIA (ROUNDING STANDARDS. THE CONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE ENGINEER FOR RESOLUTION.
- ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTHINIS PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS, ALL AVAILABLE GROUNDING ELECTRODES SHALL BE CONNECTED TOGETHER IN ACCORDANCE WITH THE NEC.
- THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS. USE OF OTHER METHODS MUST BE PRE-APPROVED BY THE ENGINEER IN WRITING.
- 4. THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 THMS OR LESS ON TOWER SITES AND 10 OHMS OR LESS ON ROOFTOF SITES. WHEN ADDING ELECTRODES, CONTRACTOR SHALL MAINTAIN A WINMUM DISTANCE BETWEEN THE ADDED ELECTRODE AND ANY OTHER EXISTING ELECTRODE EQUAL TO THE BURED LENGTH OF THE ROD. IDEALLY, CONTRACTOR SHALL STRIVE TO KEEP THE SEPARATION DISTANCE EQUAL TO TWICE THE BURIED LENGTH OF THE RODS.
- THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENC 43
 GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TI: PREVENT
 ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO
 THE CONDUIT.
- METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ILECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWG COPPER WIRE AND UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
- 7. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. S'RANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO TRANSMISSION EQUIPMENT.
- CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLET. UP OR STACKED. BACK-TO-BACK CONNECTIONS ON OPPOSITE SIDES OF THE GROUND BUS ARE PERMITTED.
- ALUMINUM CONDUCTOR CR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- USE OF 90' BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45' BEINDS CAN BE ADEQUATELY SUPPORTED, IN ALL CASES, BENDS SHALL BE MADE WITH A MINIMUM BEND RADIL'S OF 8 INCHES.
- 11. EACH INTERIOR TRANSMISSION CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH 6 AWG STRANDED, GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRE UNLESS NOTED OTHERWISE IN THE DETAILS, EACH OUTDOOR CABINET FRAME/PLINTH SHALL BE DIRECTLY CONNECTED TO THE BURIED GROUND RING WITH 2 AWG SOLID TIN-PLATED COPPER WIRE UNLESS NOTED OTHERWISE IN THE DETAILS.
- ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING, SHALL BE 2 AWG SOLID TIN-PLATED COPPER UNLESS OTHERWISE INDICATED.
- 13. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE. CONNECTIONS TO ABOVE GRADE UNITS SHALL BE MADE WITH EXOTHERMIC WELDS WHERE PRACTICAL OR WITH 2 HOLE: MECHANICAL TYPE BRASS CONNECTORS WITH STANLESS STEE. HARDWARE, INCLUDING SET SCREWS. HIGH PRESSURE CRIMP CONNECTORS! MAY ONLY BE USED WITH WRITTEN FERMISSION FROM SAI MARKET REFRESENTATIVE.
- EXOTHERMIC WELDS SHALL BE PERMITTED ON TOWERS ONLY WITH THE EXPRESS APPROVAL OF THE TOWER MANUFACTURER OR THE CONTRACTORS STRUCTURAL ENGINEER.
- ALL WIRE TO WIRE GROUND CONNECTIONS TO THE INTERIOR SROUND RING SHALL BE FORMED USING HIGH PRESS CRIMPS OR SPLIT BOLT CONNECTORS WHERE INDICATED IN THE DETAILS.
- 16. ON ROOFTOP SITES WHERE EXOTHERMIC WELDS ARE A FIRE HAZARD COPPER COMPRESSION CHP CONNECTORS MAY BE USED FOR WIRE TO WIRE CONNECTORS 2 HOLE MICHAINCAL TYPE BRASS CONNECTORS WITH STAINLESS STEEL HARDWARE, INCLUDING SET SCREWS SHALL BE USED FOR CONNECTION TO ALL ROOFTOP TRANSMISSION EQUIPMENT AND STRUCTURAL STEEL.
- 17. COAX BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR USING TWO-HOLE MECHANICAL TYPE BRASS CONNECTORS AND STAINLESS STEEL HARDWARF
- APPROVED ANTIOXIDANT COLATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUNE CONNECTIONS.
- ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.
- 20. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BCKES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
- 21. BOND ALL METALLIC OBJECTS WITHIN 6 FT OF THE BURIED GROUND RING WITH 2 AMG SOLID TIM-PLATED COPPER GROUND CONDUCTOR, DURING EXCAVATION FOR NEW GROUND CONDUCTORS, IF EXISTING GROUND CONDUCTORS ARE ENCOUNTERED, BOND EXISTING GROUND CONDUCTORS TO NEW CONDUCTORS.
- 22. GROUND CONDUCTORS USED IN THE FACILITY GROUND AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A FING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLUPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC PLASTIC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UN AVOIDABLE (E.G., NON-METALLIC CONDUIT PROHIBITED BY LOCAL CODED THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT WITH LISTED BONDING



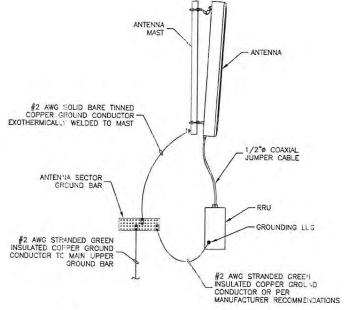


NOTES

- 1. DOUBLING UP OR STACKING OF CONNECTIONS IS NOT PERMITTED.
- 2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATIONS.

TYPICAL GROUND BAR
MECHANICAL CONNECTION DETAIL
SCALE, N.T.S.





NOTES:

- 1. VERIFY EXISTING GROUNDING SYSTEM IS INSTALLED PER AT&T STANDARDS.
- BOND NEW EQUIPMENT INTO EXISTING GROUND SYSTEM IN ACCORDANCE WITH AT&T STANDARDS AND MANUFACTURER'S RECOMMENDATIONS.

TYPICAL ANTENNA GROUNDING DETAIL. 2



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Dewberry Engineers Inc. 600 PARSIPPANY ROAD SUITE 301 PARSIPPANY, NJ 07054



DRAWN BY: BJR

REVIEWED BY: BSH

CHECKED BY: GHN

PROJECT NUMBER: 50055106

JOB NUMBER: 50093847

SITE ADDRESS:

886 MAIN STREET

EAST HARTFORD, CT 06108 HARTFORD COUNTY

SHEET TITLE

GROUNDING NOTES & DETAILS

SHEET NUMBER

E-1



Structural Analysis Report and Design Calculations For a Wireless Telecommunications facility

Site ID #: CT2490 Site Address: 886 Main Street Hartford, CT 06108

Prepared for:

SAI Communications, Inc. 12 Industrial Way Salem, NH 03079

Rev. 1

September 16, 2019

Prepared by:

Dewberry Engineers Inc.

600 Parsippany Road Parsippany, NJ 07054

Dewberry Project Number: 50093847

Analysis Condition	Utilization	Pass/Fail
Existing Mount (Alpha)	24.4% (Strength)	Pass
Existing Mount (Beta)	N/A	Pass
Existing Mount (Gamma)	24.4% (Strength)	Pass
Proposed Mount (Gamma)	37.8% (Strength)	Pass

Prepared by:

Cory Senney/ Graduate Engineer

Reviewed by:

Sahnoune Abed Structural Project Engineer Reviewed by:

Benjamin B. Revette, P.E.
Connecticut Professional Engineer
License No.: 28971

TABLE OF CONTENTS

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2.0	EXISTING	AND PROPOSED ANTENNAS & EQUIPMENT	1
3.0	CODES, S	TANDARDS, AND REFERENCES	2
4.0	LOADING	AND PERFORMANCE CRITERIA	3
5.0	CALCULA	TIONS	3
6.0	CONCLUS	SIONS, COMMENTARY, AND RECOMMENDATIONS	4
APP	ENDIX A	ANALYSIS OF ALPHA AND GAMMA SECTOR MAST PIPE MOUNT	
APPI	ENDIX B	ANALYSIS OF GAMMA SECTOR STAND-OFF FRAME	
APPI	ENDIX C	ANALYSIS OF BETA SECTOR BALLAST MOUNT	
APP	ENDIX D	REFERENCE MATERIAL	
٨٥٥	ENDIX E	SITE PHOTOS	

SAI for AT&T Mobility Site ID: CT2490 Project No. 50093847 September 16, 2019

1.0 INTRODUCTION AND PROJECT SUMMARY

The objective of this report is to assess the structural integrity of the installation of new antennas and associated equipment on existing cantilevered mast pipe mounts in the Alpha and Gamma Sectors, and on a proposed mast pipe mount attached to an existing ballast platform in the Beta Sector. Additionally, the structural integrity of a proposed stand-off mount supporting a relocated antenna will be assessed in this report.

The existing structure is 100 ft tall building located in East Hartford, CT. There are currently existing antennas and support equipment mounted to cantilevered pipe mounts in the Alpha and Gamma Sectors, and to a ballast steel frame in the Beta Sector. The proposed Alpha and Gamma equipment will be attached at an approximate antenna centerline of 117 ft A.G.L. and the proposed Beta equipment will be attached at an approximate antenna centerline of 109 ft A.G.L. The telecommunication upgrade is proposed by AT&T and managed by SAI Communications, Inc.

The installation of all antennas, equipment, cables and accessories are to be performed in accordance with construction drawings prepared by Dewberry Engineers Inc.

2.0 EXISTING AND PROPOSED ANTENNAS & EQUIPMENT

Currently, each sector contains the following equipment:

- Two (2) CCI OPA-65R-LCUU-H6 panel antennas measuring 72"H x 14.8"W x 7.4"D weighing 73 lbs each to remain
- One (1) Kathrein 800-10965 panel antenna measuring 78.7"H x 20.0"W x 6.9"D weighing 108.6 lbs to remain
- One (1) RRUS B5/B12 4449 measuring 17.9"H x 13.2"W x 9.4"D weighing 71 lbs to remain
- One (1) RRUS B2/B66A 8843 measuring 14.9"H x 13.2"W x 10.9"D weighing 72 lbs to be remain
- One (1) RRUS-32 measuring 26.7"H x 12.1" W x 6.7"D weighing 60 lbs each to remain
- One (1) Raycap DC6-48-60-18-8C measuring 26.0"Hx 9.0"D weighing 31.8 lbs to remain

The following equipment is proposed at each sector:

- > One (1) CCI HPA-65R-BU6AA measuring 71"H x 11.7"W x 7.6"D weighing 51 lbs
- One (1) RRUS B25 4415 measuring 16.5"H x 13.4"W x 5.9"D weighing 46 lbs



	Table 1: Appurte	nance Loading at Rooftop
Elev.	Status	Appurtenance Description
109'	Final	(2) CCI OPA-65R-LCUU-H6
109'	Final	(1) Kathrein 800-10965
109'	Final	(1) CCI HPA-65R-BU6AA
109'	Final	(1) RRUS B25 4415
109'	Final	(1) RRUS-32
109'	Final	(1) Raycap DC6-48-60-18-8C
109'	Final	(1) RRUS B5/B12 4449
109'	Final	(1) RRUS B2/B66A 8843
117'	Final	(4) CCI OPA-65R-LCUU-H6
117'	Final	(2) Kathrein 800-10965
117'	Final	(2) CCI HPA-65R-BU6AA
117'	Final	(2) RRUS B25 4415
117'	Final	(2) RRUS-32
117'	Final	(2) Raycap DC6-48-60-18-8C
117'	Final	(2) RRUS B5/B12 4449
117'	Final	(2) RRUS B2/B66A 8843

3.0 CODES, STANDARDS, AND REFERENCES

The structure was analyzed and the proposed installation designed per the provisions of the following Codes and standards:

- International Building Code (IBC) 2015, International Council
- 2018 Connecticut State Building Code Amendments to IBC 2015
- TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
- Steel Construction Manual 14th Edition, American Institute of Steel Construction
- ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
- TMS 402-11/ACI530-11/ASCE 5-11 Building Code Requirements for Masonry Structures
- Construction Drawings by Hudson Design Group, dated November 8th, 2016
- Structural Analysis by Hudson Design Group, dated February 14, 2014
- Radio Frequency Data Sheet (RFDS) by AT&T, dated September 19th, 2018



SAI for AT&T Mobility Site ID: CT2490 Project No. 50093847 September 16, 2019

4.0 LOADING AND PERFORMANCE CRITERIA

The following Code-specified strength limit state load combinations were considered in the analysis of the antenna mounts (TIA-222-H):

- 1. 1.2D + 1.0W
- 2. 1.2D + 1.0Di + 1.0Wi
- 3. 1.4D

The following Code-specified serviceability load combination was considered in the deflection of the antenna mounts (TIA-222-H):

4. 1.0D + 1.0Wservice

The following load combination was considered for the stability of the Beta Sector Ballast Mount (ASCE 7-10):

1. 1.0D + 0.6W

Where:

D = Dead Load
D_i = Ice Dead Load
W = Wind Load
W_i = Ice Wind Load
W_{service} = Service Wind Load

The following site-specific design parameters were considered in this analysis per the provisions of TIA-222-H:

Class. IIExposure: B

Design Wind Speed: 123 mph

 ATC Wind Speed

· Design Ice Wind Speed: 50 mph

. Design Ice Thickness: 1.5 in

Gust Effect Factor: 0.85
 Wind Direction Probability Factor: 0.95
 Serviceability Wind Speed: 60 mph

Section 2.6.9.1
Table 2-2
Sect. 2.8.3

5.0 CALCULATIONS

Calculations for this analysis and the design of the installation are included in the Appendices of this report.



6.0 CONCLUSIONS, COMMENTARY, AND RECOMMENDATIONS

The analysis concludes that the proposed antennas and associated equipment are adequate for the proposed installation with the most unfavorable loading condition.

The existing cantilever pipe mounts used to support the proposed and existing equipment at the Alpha and Gamma sectors are loaded to 24.4% of their strength capacity. The proposed stand-off frame in the Gamma sector is loaded to 37.8% of its strength capacity. The existing steel ballast frame used to support the proposed and existing equipment at the Beta sector passes stability checks, based on a minimum Factor of Safety of 1.5. Based on engineering judgement, the overall stability of the Beta sector governs the design of the ballast frame, not the strength of the steel members.

Existing roof structure appears to be in fair condition at the locations of the proposed equipment.

Dewberry Engineers Inc. reserves the right to add to or modify this report if more information becomes available. The conclusions reached by Dewberry Engineers Inc. in this report are only applicable to the previously mentioned existing structural elements supporting the proposed wireless telecommunications installation. The results of this report are based on the assumption that existing structural elements have been installed per the original design documents, have been well maintained and are uncompromised. This report does not imply that a thorough inspection of the existing structure has been performed. Any deviation of the support condition, loading, location, placement, equipment configuration, etc., will require Dewberry Engineers Inc. to generate an additional structural analysis.



APPENDIX A





Job No. 50093847 Sheet No. A-1 By: CS 9/16/2019 Chk: SA 09/17/2019

Analysis of Alpha and Gamma Sector Mast Pipe Mount

Overview

The Alpha and Gamma Sector antenna frames are composed of three cantilevered pipes, thru-bolted into the existing penthouse wall. The pipes are attached with horizontal unistrut members, which support antenna equipment. Since the unistrut is not a structural member, only the cantilevered pipes shall be checked, with the equipment loads from the unistrut being applied to the cantilevered pipe.

Design Criteria and References

- 1. International Building Code (IBC) 2015, International Code Council
- 2. 2018 Connecticut State Building Code Amendments to IBC 2015
- 3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
- 4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
- 5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
- 6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
- 7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
- 8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

Equipment Dead Loads

		Dimension	s (in)	Weight (lb)
Description	W	D	Н	weight (ib)
CCI HPA-65R-BU6AA	11.70	7.60	71.00	51.00
Ericsson RRUS B25 4415	13.40	5.90	16.50	46.00
Ericsson RRUS B2/B66A 8843	13.20	10.90	14.90	72.00

^{*}Bold = Proposed

Structural Members

			Dir	nensions (in)		Weight (lb/ft)
Member	d	b _f	t _f	t _w	I.D.	O.D.	weight (ib/ft)
3" XS Pipe					3.07	3.50	7.55



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Analysis of Alpha and Gamma Sector Mast Pipe Mount

Wind Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
V _{max} =	123.00	Design Wind Speed	ASCE 7-10, Appendix D
V _i =	50.00	Design Ice Wind Speed	TIA-222-H, Annex B-9
K _d =	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	11	Risk Category	TIA-222-H, Table 2-1
=	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
I ice thick =	1.00	Importance Factor (Ice Thickness)	TIA-222-H, Table 2-3
z = h =	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	В	Exposure Category	TIA-222-H, Section 2.6.5.1.2
z _g =	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
a =	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
$K_{z \text{ (min)}} =$	0.70	Minimum Value for K_z	TIA-222-H, Table 2-4
K _c =	0.90	Terrain Constant	TIA-222-H, Table 2-4
K _t =	N/A	Topographic Constant	TIA-222-H, Table 2-5
K _z =	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
e =	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
f =	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
H =	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
K _h =	N/A	e ^{((f*z)/H)} Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
K _{zt} =	1.00	= $[1+((K_c*K_t)/K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
K _{iz} =	1.13	$= (z/33)^{0.10} \le 1.4$ Height Escalation Factor	TIA-222-H, Section 2.6.10
G _h =	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
K _a =	0.9	Shielding Factor	TIA-222-H, Section 16.6
t _i =	1.50	Design Ice Thickness (in)	TIA-222-H, Annex B-9
t _{iz} =	3.40	$2 t_i(I_{ice thick})K_{iz}(K_{zt})^{0.35}$ Thickness of Radial Glaze Ice	TIA-222-H, Section 2.6.10
q _{z design} =	34.23	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{max}^2)(1)$	TIA-222-H, Section 2.6.11.6
q _{z ice} =	5.66	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_i^2)$	TIA-222-H, Section 2.6.11.6



Job No. 50093847 Sheet No. A-1 By: CS 9/16/2019 Chk: SA 09/17/2019

Analysis of Alpha and Gamma Sector Mast Pipe Mount

Wind Service Load and Maintenance Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
V _{service} =	60.00	Design Service Wind Speed	TIA-222-H, Section 2.8.3
V _{maintenance} =	30.00	Design Maintenance Wind Speed	TIA-222-H, Section 16.3
K _d =	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	II.	Risk Category	TIA-222-H, Table 2-1
Total State	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
z = h =	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	В	Exposure Category	TIA-222-H, Section 2.6.5.1.2
z _g =	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
a =	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
K _{z (min)} =	0.70	Minimum Value for K ₂	TIA-222-H, Table 2-4
K _c =	0.90	Terrain Constant	TIA-222-H, Table 2-4
K _t =	N/A	Topographic Constant	TIA-222-H, Table 2-5
K _z =	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
e =	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
f =	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
H =	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
K _h =	N/A	e ^{((f*z)/H)} Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
K _{zt} =	1.00	= $[1+((K_c*K_t)/K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
G _h =	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
K _a =	0.9	Shielding Factor	TIA-222-H, Section 16.6
q _{z service} =	8.14	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{service}^2)(I)$	TIA-222-H, Section 2.6.11.6
q _{z maintenance} =	2.04	= $0.00256(K_z)(K_{zt})(K_d)(V_{maintenance}^2)(I)$	TIA-222-H, Section 2.6.11.6



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Analysis of Alpha and Gamma Sector Mast Pipe Mount

Force Coefficients for Appurtenances, Without Ice (TIA-222-H)

	O	Dimensions (ft)	(托)		Area (A _s),				ڻ ن	ئ
Equipment	Width (Normal)	Length (tangent)	0	(Normal) (sf) $(Tangent)$	(Tangent) (sf)	Aspect Katio (Normal)	Aspect Ratio (Tangent)	C Table 2-9	(Normal) Table 2-9	(Tangent) Table 2-9
CCI HPA-65R-BU6AA	0.98	0.63	5.92	5.77	3.75	6.07	9.34		1.36	1.48
Ericsson RRUS B25 4415	1.12	0.49	1.38	1.54	0.68	1.23	2.80		1.20	1.21
Ericsson RRUS B2/B66A 8843	1.10	0.91	1.24	1.37	1.13	1.13	1.37		1.20	1.20
seu										

Force Coefficients for Appurtenances, With Ice (TIA-222-H)

-		Di	Dimensions (ft)	(ft)		Area (A ₃),					ٿ
	Equipment	Width (Normal)	Length (tangent)	Height (Or (Normal) Span)	Area (A _a) _n (Normal) (sf)	Jahn (Tangent) (sf) (sf)	Aspect Katio (Normal)	Aspect Katio (Tangent)	C Table 2-9	(Normal) Table 2-9	(Tangent) Table 2-9
	CCI HPA-65R-BU6AA	1.23	0.88	6.17	7.55	5.45	5.03	6.98		1.31	1.40
SLI	Ericsson RRUS B25 4415	1.37	0.74	1.63	2.22	1.21	1.19	2.19		1.20	1.20
VV/	Ericsson RRUS B2/B66A 8843	1.35	1.16	1.49	2.01	1.73	1.10	1.29		1.20	1.20
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Job No. 50093847

Analysis of Alpha and Gamma Sector Mast Pipe Mount

Equipment Wind Loads (TIA-222-H)

 $F_A = q_z _{design} G_h(EPA)_A$ $(EPA)_A = C_a A_a$

 $F_A = q_z i_{ce} G_h (EPA)_{A ice}$

(EPA)_{A ice} = C_aA_{a ice}

TIA-222-H, Section 2.6.11.2, Applies to Strength, Service & Maintenance Conditions

Ice Condition

		No	No Ice	2	lce	240	141) de	-	(150)		1941)
			(sf)	if)		Streng	Strength (Ibs)	20	ice (ibs)	Service	service (IDS)
-	Farripmont	(EPA) _A	(EPA) _A	(EPA) _A	(EPA) _A	FA	T.	π _A	ТA	Ā	
- mpuret	רלמולוויייי	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)		(Tangent)
-	CCI HPA-65R-BU6AA	7.84	5.54	9.92	7.62	268.24	189.57	56.08	43.11	63.83	45.11
CLI	Ericsson RRUS B25 4415	1.84	0.82	2.67	1.45	90.89	28.07	15.07	8.18	15.01	89.9
ARIA	Ericsson RRUS B2/B66A 8843	1.64	1.35	2.42	2.07	56.10	46.32	13.67	11.73	13.35	11.02
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The proposed antenna frame layout consists of two RRH's, one of which is mounted directly behind the proposed antenna, and the other to unistrut spanning in between the antennas. For simplicity, the loads of 1.5 RRUS will be applied to the pipe STAAD model

Structure Wind Loads (TIA-222-H)

Wind loads on structural elements will be applied linearly: $\omega_{wnd} = q_2 _{design} C_a G_n d$, with d being the structure depth or diameter. A conservative Ca value of 1.2 will be used for pipes. This same equation will be used for the service condition, with the service wind load being used, and ice condition, with the ice wind load and ice structure depth/diameter being used.

Member	d (ft)	d _{ice} (ft)	ڻ	ω _{wind} (lb/ft)	windice (Ib/ft)	ω _{wind ser} (lb/ft)	
3" XS Pipe	0.38	0.63	1.2	15.40	4.24	3.66	



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Analysis of Alpha and Gamma Sector Mast Pipe Mount

Ice Dead Loads

Equipment	Volume (cf)	Volume _{w/ice} (cf)	Volume _{ice} (cf)	W _{ice} (lb)
CCI HPA-65R-BU6AA	3.65	6.67	3.02	169.08
Ericsson RRUS B25 4415	0.75	1.65	0.89	49.96
Ericsson RRUS B2/B66A 8843	1.24	2.33	1.09	61.15
100 110 Mary 100 100 100 100 100 100 100 100 100 10				

Structural Member	Perimeter (If)	Perimeter _{w/ ice} (lf)	Area _{ice} (sf)	W _{ice} (lb/ft)
3" XS Pipe	1.18	1.96	0.20	11.00

Load Combinations (TIA-222-H)

1. $1.2D + 1.0W_o$

2. $1.2D + 1.0D_i + 1.0W_i$

3. 1.4D

4. $1.0D + 1.0W_s$

Strength Limit State

Strength Limit State

Strength Limit State

Service Limit State

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Job Information

	Engineer	Checked	Approved
Name:	CS	SA	
Date:	9/16/2019	9/17/2019	

Project ID	
Project Name	

Structure Type | SPACE FRAME

Number of Nodes	7	Highest Node	7
Number of Elements	6	Highest Beam	6

Number of Basic Load Cases	8
Number of Combination Load Cases	7

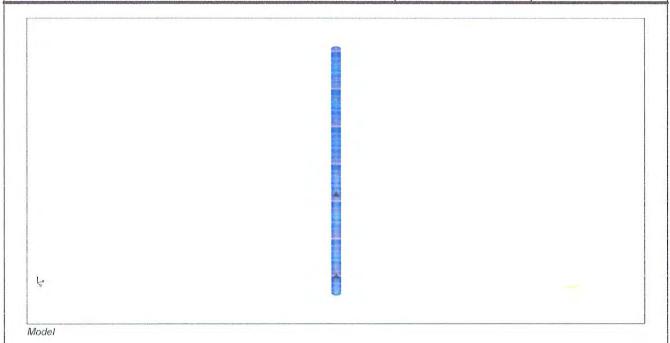
Included in this printout are data for:

porturate to the second or the	NEW COLUMN TO THE PARTY OF THE
All	The Whole Structure

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	DI
Primary	3	W(X)O
Primary	4	W(Z)O
Primary	5	W(X)I
Primary	6	W(Z)I
Primary	7	W(X)S
Primary	8	W(Z)S
Combination	9	1.2D + 1.0W(X)O
Combination	10	1.2D + 1.0W(Z)O
Combination	11	1.2D + 1.0DI + 1.0W(X)I
Combination	12	1.2D + 1.0DI + 1.0W(Z)I
Combination	13	1.4D
Combination	14	1.0D + 1.0W(X)S
Combination	15	1.0D + 1.0W(Z)S

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Nodes

Node	Х	Υ	Z
	(ft)	(ft)	(ft)
1	0	0	0
2	0	1.000	0
3	0	5.000	0
4	0	6.000	0
5	0	8.500	0
6	0	9.500	0
7	0	12.000	0

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Nodes

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	2	1.000	1	0
2	2	3	4.000	1	0
3	3	4	1.000	1	0
4	4	5	2.500	1	0
5	5	6	1.000	1	0
6	6	7	2.500	1	0

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Members

Section Properties

Prop	Section	Area (in²)	l _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in⁴)	Material
1	PIPS30	2.100	2.850	2.850	5.689	STEEL

Materials

Mat	Name	E (kip/in²)	ν	Density (kip/in³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E -6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E -6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
7	STEEL	29E+3	0.300	0.000283	6E -6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6

Supports

Node	Х	Y	Z	rX	rY	rZ
	(kip/in)	(kip/in)	(kip/in)	(kip ft/deg)	(kip ft/deg)	(kip ⁻ ft/deg)
2	Fixed	Fixed	Fixed	-	-	-
3	Fixed	Fixed	Fixed	-	-	-

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Releases

There is no data of this type.

Primary Load Cases

Number	Name	Туре
1	DL	Dead
2	DI	Dead
3	W(X)O	Wind
4	W(Z)O	Wind
5	W(X)I	Wind
6	W(Z)I	Wind
7	W(X)S	Wind
8	W(Z)S	Wind

1 DL: Node Loads

Node	FX	FY	FZ	MX	MY	MZ
	(kip)	(kip)	(kip)	(kip in)	(kipʻin)	(kip in)
4	**	-0.0255	74	-	-	-
5	-	-0.059		-	-	-
6	-	-0.059	-	-	-	-
7	-	-0.0255	-	-	-	-

1 DL: Selfweight

Direction	Factor	Assigned Geometry	
	-1.000	11 I	

2 DI: Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip⁻in)	MZ (kip in)
4	-	-0.08454	-	-	-	-
5	-	-0.0556	-	-	-	-
6	-	-0.0556	-	-	-	-
7		-0.08454	-	-	-	-

2	Job No Sheet No 6 Rev
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2 DI: Beam Loads

Beam	Туре		Direction	Fa	Da (ft)	Fb	Db	Ecc.
1	UNI	lbf/ft	GY	-1.100	-		-	-
2	UNI	lbf/ft	GY	-1.100	-	-	-	-
3	UNI	lbf/ft	GY	-1.100	-	-	-	-
4	UNI	lbf/ft	GY	-1.100			-	-
5	UNI	lbf/ft	GY	-1.100	-	-	-	-
6	UNI	lbf/ft	GY	-1.100	-	-	-	-

3 W(X)O: Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip*in)	MZ (kip ⁻ in)
4	0.095	A STATE OF THE PARTY OF THE PAR		**	And the Control of th	-
5	0.0372	-	-	-	-	-
6	0.0372	-	-	-	-	-
7	0.095	-	-	-	-	-

3 W(X)O : Beam Loads

Beam	Туре		Direction	Fa	Da (ft)	Fb	Db	Ecc.
1	UNI	lbf/ft	GX	15.400	-	-	-	-
2	UNI	lbf/ft	GX	15.400	-	-	-	-
3	UNI	lbf/ft	GX	15.400	-	-	-	-
4	UNI	lbf/ft	GX	15.400	**	-	-	-
5	UNI	lbf/ft	GX	15.400	-	-	-	-
6	UNI	lbf/ft	GX	15.400	-	-	-	-

4 W(Z)O: Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip⁻in)	MZ (kip⁻in)
4	40.134			-	-	
7	-	-	-0.134	-	-4	-

5 W(X)I: Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kipʻin)	MZ (kip in)
4	0.02156	-	-	-	-	-
5	0.01	-	-	-	-	-
6	0.01		-	-	-	-
7	0.02156	-	-	-	~	-

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5 W(X)I : Beam Loads

Beam	Ty	/pe	Direction	Fa	Da (ft)	Fb	Db	Ecc.
1	UNI	lbf/ft	GX	4.240	-			-
2	UNI	lbf/ft	GX	4.240	-	-	-	-
3	UNI	lbf/ft	GX	4.240	-	-	-	-
4	UNI	lbf/ft	GX	4.240	*	-	-	-
5	UNI	lbf/ft	GX	4.240	-	-	-	-
6	UNI	lbf/ft	GX	4.240	-	-	-	-

6 W(Z)I: Node Loads

Node	FX	FY	FZ	MX	MY	MZ
	(kip)	(kip)	(kip)	(kip in)	(kip⁻in)	(kip in)
4	-	-	-0.02804	_	-	-
7	-	-	-0.02804	-	-	-

7 W(X)S: Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip*in)	MY (kip in)	MZ (kip in)
4	0.02256	-	-	-	-	-
5	0.00885	11-1	-	-	-	-
6	0.00885	-	-	-	-	-
7	0.02256	-		-	-	-

7 W(X)S: Beam Loads

Beam	Туре		Direction	Fa	Da (ft)	Fb	Db	Ecc.
1	UNI	lbf/ft	GX	3.660	-	-	-	-
2	UNI	lbf/ft	GX	3.660	-	-		-
3	UNI	lbf/ft	GX	3.660	-	-	-	-
4	UNI	lbf/ft	GX	3.660	-	-	-	-
5	UNI	lbf/ft	GX	3.660	-	-	-	-
6	UNI	lbf/ft	GX	3.660	-	-	-	-

8 W(Z)S: Node Loads

Node	FX	FY	FZ	MX	MY	MZ
4	(kip)	(kip)	(kip) -0.03192	(kip in)	(kip in)	(kip in)
7	-		-0.03192	-	*	-

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Load Case 8						

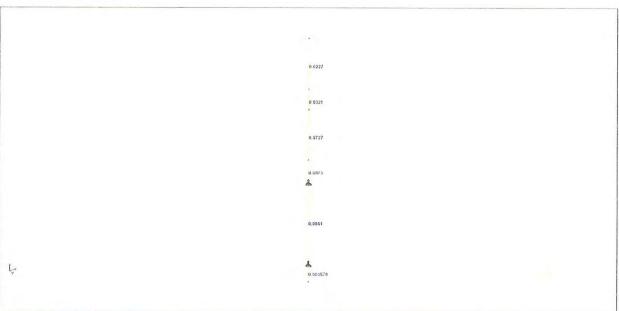
	Job No Sheet No 12 Rev
Software licensed to STAAD Pro CONNECTED User. Cory Senney	Part Alpha & Gamma Sectors
Job Title CT2490 - East Hampton Main Street	Ref
	By CS Dateg/16/2019 Chd SA
Client AT&T	File Alpha & Gamma Sector.s Date/Time 16-Sep-2019 11:42

Utilization Ratio

Beam	Analysis	Design	Actual	Allowable	Ratio	Clause	L/C	Ax	lz	ly	lx
	Property	Property	Ratio	Ratio	(Act./Allow.)			(in ²)	(in ⁴)	(in ⁴)	(in ⁴)
1	PIPS30	PIPS30	0.001	1.000	0.001	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
2	PIPS30	PIPS30	0.243	1.000	0.243	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
3	PIPS30	PIPS30	0.244	1.000	0.244	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
4	PIPS30	PIPS30	0.183	1.000	0.183	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
5	PIPS30	PIPS30	0.080	1.000	0.080	LRFD-H1-1B-	10	2.100	2.850	2.850	5.700
6	PIPS30	PIPS30	0.057	1.000	0.057	LRFD-H1-1B-	10	2.100	2.850	2.850	5.700

Failed Members

There is no data of this type.

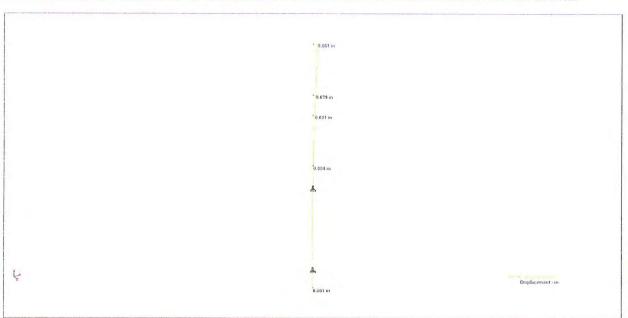


Envelope Utilization Ratio

	Job No Sheet No 13	Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamma Sectors	
Job Title CT2490 - East Hampton Main Street	Ref	***************************************
	By CS Date9/16/2019	Chd SA
Client AT&T	Fite Alpha & Gamma Sector.s Date/Time 1	6-Sep-2019 11:42

Node Displacement Summary

	Node	L/C	X	Y	Z	Resultant	rX	rY	rZ
			(in)	(in)	(in)	(in)	(rad)	(rad)	(rad)
Max X	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010
Min X	1	1:DL	0	-0.000	0	0.000	0	0	0
Max Y	2	1:DL	0	0	0	0	0	0	0
Min Y	7	11:1.2D + 1.0D	0.168	-0.000	0	0.168	0	0	-0.002
Max Z	1	1:DL	0	-0.000	0	0.000	0	0	0
Min Z	7	4:W(Z)O	0	0	-0.542	0.542	-0.008	0	0
Max rX	1	4:W(Z)O	0	0	-0.015	0.015	0.001	0	0
Min rX	7	4:W(Z)O	0	0	-0.542	0.542	-0.008	0	0
Max rY	1	1:DL	0	-0.000	0	0.000	0	0	0
Min rY	1	1:DL	0	-0.000	0	0.000	0	0	0
Max rZ	1	3:W(X)O	0.019	0	0	0.019	0	0	0.002
Min rZ	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010
Max Rst	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010



Displacement

Displacement Check
Antenna Pipe Mast (3 1/2" O.D. Pipe):
Max Displacement = 0.679"

(Node 7)

Allowable Displacement = 1.5% cantilever = 1.08" 0.697" < 1.26" -- OK

	Job No Sheet No 14 Rev
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Job Title CT2490 - East Hampton Main Street	Ref
	By CS Date9/16/2019 Chd SA
Client AT&T	File Alpha & Gamma Sector.s Date/Time 16-Sep-2019 11:

Reaction Summary

			Horizontal	Vertical	Horizontal		Moment	
	Node	L/C	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip in)	MZ (kip in)
Max FX	2	3:W(X)O	0.310	0	0	0	0	0
Min FX	3	3:W(X)O	-0.759	0	0	0	0	0
Max FY	3	11:1.2D + 1.0D	-0.190	0.570	0	0	0	0
Min FY	2	3:W(X)O	0.310	0	0	0	0	0
Max FZ	3	4:W(Z)O	0	0	0.536	0	0	0
Min FZ	2	4:W(Z)O	0	0	-0.268	0	0	0
Max MX	2	1:DL	0	0.021	0	0	0	0
Min MX	2	1:DL	0	0.021	0	0	0	0
Max MY	2	1:DL	0	0.021	0	0	0	0
Min MY	2	1:DL	0	0.021	0	0	0	0
Max MZ	2	1:DL	0	0.021	0	0	0	0
Min MZ	2	1:DL	0	0.021	0	0	0	0



Job No. 50093847 Sheet No. A-29 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Alpha and Gamma Sector Mast Pipe Mount

Design Criteria

- 1. TMS 402-11/ACI 530-11/ASCE 5-11 Building Code Requirements for Masonry Structures
- 2. ACI -318-11 Building Code Requirements for Structural Concrete
- 3. AISC 360-10 Specifications for Structural Steel Buildings

References

Refer to construction drawings by Hudson Design Group, dated November 8, 2016 for pipe mount connection details (Bolt diameter field verified by Dewberry Engineers Inc. on 07/26/2019)

Thru Bolt Check

M =	2.28 kip-in	Fx * (1/2 Angle depth), See Appendix A-28 for Fx
d =	9.50 in	Spacing of Thru Bolts
T =	0.24 kip	Tension in 5/8" Thru Bolt
$f_{y \text{ thru bolt}} =$	0.78 ksi	Tensile Stress in Thru Bolt> OK BY INSPECTION
F _x =	0.759	See Appendix A-28
V _{thru bolt} =	0.38 kip	Shear at 5/8" Thru Bolt
$f_{v \text{ thru bolt}} =$	1.24 ksi	Shear Stress in Thru Bolt> OK BY INSPECTION

Penthouse Wall Global Check

Based on Engineering Judgement, the loads produced by the antenna mounting pipes is negligible on the penthouse CMU and steel stud walls

APPENDIX B





Job No. 50093847 Sheet No. B-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Gamma Sector Stand-off Frame

Overview

The existing C1 position antenna in the gamma sector is going to be relocated to a proposed 3'-0" stand-off frame. The antenna will be mounted to a 3" diameter sch. 40 pipe, which will be U-bolted to the proposed stand-off frame, and proposed stand-off frame will be thru-bolted to the existing penthouse wall. Only the 4" diameter pipe will be checked for strength.

Design Criteria and References

- 1. International Building Code (IBC) 2015, International Code Council
- 2. 2018 Connecticut State Building Code Amendments to IBC 2015
- 3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
- 4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
- 5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
- 6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
- 7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
- 8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

Equipment Dead Loads

Description		Dimension	ıs (in)	
Description	W	D	Н	weight (ib)
Kathrein 800-10965	20.00	6.90	78.70	108.60
RRU 4415 B25	13.40	5.90	16.50	46.00
S. III C. II				

^{*}Bold = Proposed

Structural Members

0.4			Dir	mensions (in)			Weight /lb/ft\
Member	d	b_f	t _f	t _w	I.D.	O.D.	Weight (lb/ft)
3" STD Pipe					3.07	3.50	7.58
HSS4X4X1/4*	4.00	4.00		0.233			12.21

^{*}Approximate member size for Site Pro 1 Standoff Arm



Job No. 50093847 Sheet No. B-1 By: CS 09/16/2019

Chk: SA 09/17/2019

Analysis of Gamma Sector Stand-off Frame

Wind Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
V _{max} =	123.00	Design Wind Speed	ASCE 7-10, Appendix D
V _i =	50.00	Design Ice Wind Speed	TIA-222-H, Annex B-9
K _d =	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	11	Risk Category	TIA-222-H, Table 2-1
name.	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
I ice thick =	1.00	Importance Factor (Ice Thickness)	TIA-222-H, Table 2-3
z = h =	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	В	Exposure Category	TIA-222-H, Section 2.6.5.1.2
z _g =	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
a =	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
K _{z (min)} =	0.70	Minimum Value for K _z	TIA-222-H, Table 2-4
K _c =	0.90	Terrain Constant	TIA-222-H, Table 2-4
K _t =	N/A	Topographic Constant	TIA-222-H, Table 2-5
K _z =	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
e =	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
f =	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
H =	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
K _h =	N/A	e ^{((f*z)/H)} Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
K _{zt} =	1.00	= $[1+((K_c*K_t)/K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
K _{iz} =	1.13	$= (z/33)^{0.10} \le 1.4$ Height Escalation Factor	TIA-222-H, Section 2.6.10
G _h =	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
K _a =	0.9	Shielding Factor	TIA-222-H, Section 16.6
t _i =	1.50	Design Ice Thickness (in)	TIA-222-H, Annex B-9
t _{iz} =	3.40	$2 t_i(I_{ice thick})K_{iz}(K_{zt})^{0.35}$ Thickness of Radial Glaze Ice	TIA-222-H, Section 2.6.10
q _{z design} =	34.23	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{max}^2)(I)$	TIA-222-H, Section 2.6.11.6
q _{z ice} =	5.66	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_i^2)$	TIA-222-H, Section 2.6.11.6



Job No. 50093847 Sheet No. B-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Gamma Sector Stand-off Frame

Wind Service Load and Maintenance Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
V _{service} =	60.00	Design Service Wind Speed	TIA-222-H, Section 2.8.3
V _{maintenance} =	30.00	Design Maintenance Wind Speed	TIA-222-H, Section 16.3
K _d =	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	11	Risk Category	TIA-222-H, Table 2-1
=	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
z = h =	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	В	Exposure Category	TIA-222-H, Section 2.6.5.1.2
z _g =	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
a =	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
K _{z (min)} =	0.70	Minimum Value for K ₂	TIA-222-H, Table 2-4
K _c =	0.90	Terrain Constant	TIA-222-H, Table 2-4
K _t =	N/A	Topographic Constant	TIA-222-H, Table 2-5
K _z =	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
e =	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
f =	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
H =	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
K _h =	N/A	e ^{((f*z)/H)} Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
K _{zt} =	1.00	= $[1+((K_c*K_t)/K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
G _h =	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
K _a =	0.9	Shielding Factor	TIA-222-H, Section 16.6
q _{z service} =	8.14	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{service}^2)(I)$	TIA-222-H, Section 2.6.11.6
q _{z maintenance} =	2.04	= $0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{maintenance}^2)(I)$	TIA-222-H, Section 2.6.11.6



Job No. 50093847 Sheet No. B-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Gamma Sector Stand-off Frame

Force Coefficients for Appurtenances, Without Ice (TIA-222-H)

MARKEDSKA		Dimensions (ft)			Area (A.).	statement of the last				ن
Equipment	Width (Normal)	Length (tangent)		Area $(A_a)_n$ (formal) (sf) (sf)	(Tangent) (sf)	THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER.	Aspect Ratio Aspect Ratio C (Normal) (Tangent) Tobl	C Table 2-9	(Normal) Table 2-9	(Tangent) Table 2-9
Kathrein 800-10965	1.67	0.58	6.56	10.93	3.77	3.94	11.41		1.26	1.55
RRU 4415 825	1.12	0.49	1.38	1.54	0.68	1.23	2.80		1.14	1.26

Force Coefficients for Appurtenances, With Ice (TIA-222-H)

							-				
		Ö	Dimensions (ft)	(ft)	1 41	Area (A ₃),					ن
	Equipment	Width	Length	Height (or	Height (Or (Normal) (sf) (Tangent)	(Tangent)	Aspect Ratio (Normal)	Aspect Ratio Aspect Ratio (Normal) (Tangent)	C Table 2-9	(Normal)	(Tangent)
		(Normal)	(tangent)	Span)		(st)					Table 2-9
	Kathrein 800-10965	1.92	0.83		13.05	5.62	3.55	8.25		1.25	1.46
SH	RRU 4415 B25	1.37	0.74	1.63	2.22	1.21	1.19	2.19		1.14	1.19
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SAI Communications

East Hartford Main Street CT2490

Sheet No. B-1 By: CS 09/16/2019

Chk: SA 09/17/2019 Job No. 50093847

Analysis of Gamma Sector Stand-off Frame Equipment Wind Loads (TIA-222-H)

 $F_A = q_z design G_h (EPA)_A$ $(EPA)_A = C_aA_a$

TIA-222-H, Section 2.6.11.2, Applies to Strength, Service & Maintenance Conditions

 $F_A = q_z _{ice} G_h (EPA)_A _{ice}$ (EPA)A Ice = CaAa ice

Ice Condition

	ž	No Ice		Ice	i	11 111 1		1 11/		, , ,	
		5)	(sf)		- streng	strength (lbs)	93	Ice (Ibs)	Servic	Service (Ibs)	
Equipment	(EPA) _A (Normal)	(EPA) _A (Tangent)	(EPA) _A (Normal)	(EPA) _A (Tangent,	F _A F _A (Normal) (Tangent)	F _A (Tangent)	F _A (Normal)	F _A (Tangent)	F _A F _A F _A (Normal)	F _A (Tangent)	
Kathrein 800-10965	13.81	5.83	16.27	8.18	472.79	199.65	92.01	46.24	112.50	47.51	
은 RRU 4415 B25	1.76	0.85	2.54	1.43	60.10	29.15	14.34	8.09	14.30	6.94	
אא											
seu											
ten											-
nA											

Structure Wind Loads (TIA-222-H)

used for pipes and 2.0 for HSS. This same equation will be used for the service condition, with the service wind load being used, and ice condition, with the ice wind Wind loads on structural elements will be applied linearly: $\omega_{wind} = q_2 a_{esign} C_a G_n d$, with d being the structure depth or diameter. A conservative Ca value of 1.2 will be load and ice structure depth/diameter being used.

ω _{wind ice} (lb/ft) ω _{wi}	nd ser (Ib/ft)
3.68 2.85	2



Job No. 50093847 Sheet No. B-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Gamma Sector Stand-off Frame

Ice Dead Loads

Equipment	Volume (cf)	Volume _{w/ice} (cf)	Volume _{ice} (cf)	W _{ice} (lb)
Kathrein 800-10965	6.29	10.77	4.48	250.91
RRU 4415 B25	0.75	1.65	0.89	49.96
Belong House and the Control of the				
termine and an experience of the common problems of the common probl				

Structural Member	Perimeter (If)	Perimeter _{w/ice} (lf)	Area _{ice} (sf)	W _{ice} (lb/ft)
3" STD Pipe	0.92	1.70	0.16	9.16
HSS4X4X1/4*	1.33	2.33	0.23	12.83

Load Combinations (TIA-222-H)

1. $1.2D + 1.0W_o$

2. $1.2D + 1.0D_i + 1.0W_i$

3. 1.4D

4. 1.0D + 1.0W_s

Strength Limit State

Strength Limit State

Strength Limit State

Service Limit State

	Job No Sheet I 50093840	B - 1	
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamma Secto	ors	
Job Title CT2490 - East Hampton Main Street	Ref		-
	By CS Dategy	10/2019 ^{Chd} BK	
Client AT&T	File Gamma Sector Stando	off.: Date/Time 10-Sep-2019 13:30	0

Job Information

	Engineer	Checked	Approved
Name:	CS	ВК	
Date:	9/10/2019	9/12/2019	8/15/2019

Project ID	
Project Name	

Structure Type | SPACE FRAME

Number of Nodes	9	Highest Node	12
Number of Elements	6	Highest Beam	10

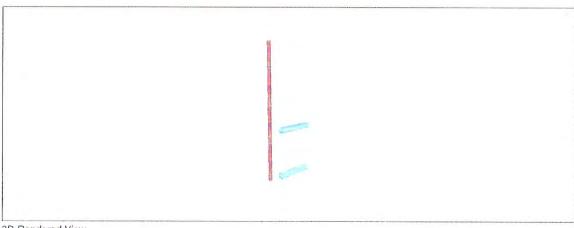
Number of Basic Load Cases	5
Number of Combination Load Cases	5

Included in this printout are data for:

All	The Whole Structure

Included in this printout are results for load cases:

Туре	L/C	Name	
Primary	1	DL	THE PARTY OF THE P
Primary	2	DI	
Primary	3	W	
Primary	4	W(I)	
Primary	5	W(S)	
Combination	6	1.2D + 1.0W	
Combination	7	1.2D + 1.0DI + 1.0W(i)	
Combination	8	1.4D	
Combination	9	1.0D + 1.0W(S)	

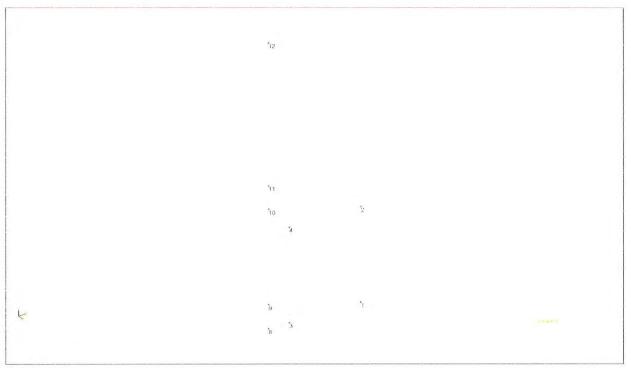


3D Rendered View

	Job No Sheet No B - 2				
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Job Title CT2490 - East Hampton Main Street	Ref				
	By CS Date9/10/2019 Chd BK				
Client AT&T	File Gamma Sector Standoff.: Date/Time 10-Sep-2019 13:				

<u>Nodes</u>

Node	X	Y	Z
	(ft)	(ft)	(ft)
1	0	0	0
2	0	4.000	0
3	-3.000	0	0
4	-3.000	4.000	0
8	-3.000	-1.000	-1.500
9	-3.000	0	-1.500
10	-3.000	4.000	-1.500
11	-3.000	5.000	-1.500
12	-3.000	11.000	-1.500

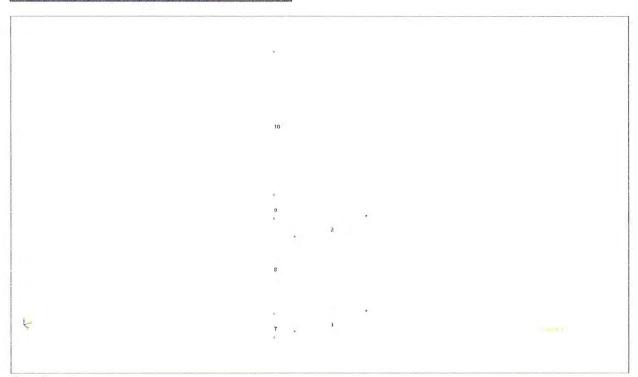


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	Job No Sheet No B - 3	
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Alpha & Gamma Sectors	-
Job Title CT2490 - East Hampton Main Street	Ref	-
	By CS Dateg/10/2019 Chd BK	
Client AT&T	File Gamma Sector Standoff.: Date/Time 10-Sep-2019 13:3	30

<u>Beams</u>

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	3	3.000	2	0
2	2	4	3.000	2	0
7	8	9	1.000	1	0
8	9	10	4.000	1	0
9	10	11	1.000	1	0
10	11	12	6.000	1	0



Beam Layout

Section Properties

Prop	Section	Area (in²)	l _{yy} (in ⁴)	l _{zz} (in ⁴)	J (in ⁴)	Material
1	PIPS30	2.100	2.850	2.850	5.689	STEEL
2	HSST4X4X0.125	1.770	4.400	4.400	6.797	STEEL

	Job No				
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamma Sectors				
lob Title CT2490 - East Hampton Main Street	Ref				
	By CS Dateg/10/2019 Chd BK				
Client AT&T	File Gamma Sector Standoff.s Date/Time 10-Sep-2019 13:30				

Materials

Mat	Name	E (kip/in²)	ν	Density (kip/in³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E-6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E-6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
7	STEEL	29E+3	0.300	0.000283	6E -6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6

Supports

Node	Х	Y	Z	rX	rY	rZ
	(kip/in)	(kip/in)	(kip/in)	(kip ft/deg)	(kip ft/deg)	(kip ⁻ ft/deg)
1	Fixed	Fixed	Fixed		Fixed	-
2	Fixed	Fixed	Fixed	-	Fixed	

Releases

There is no data of this type.

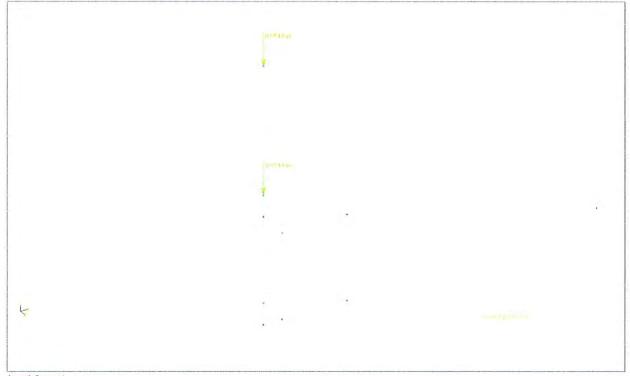
Primary Load Cases

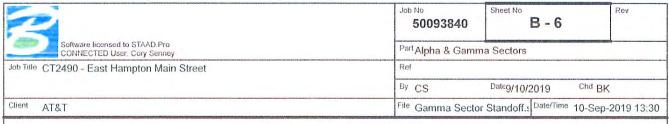
Number	Name	Туре
1	DL	Dead
2	DI	Dead
3	W	Wind
4	W(I)	Wind
5	W(S)	Wind

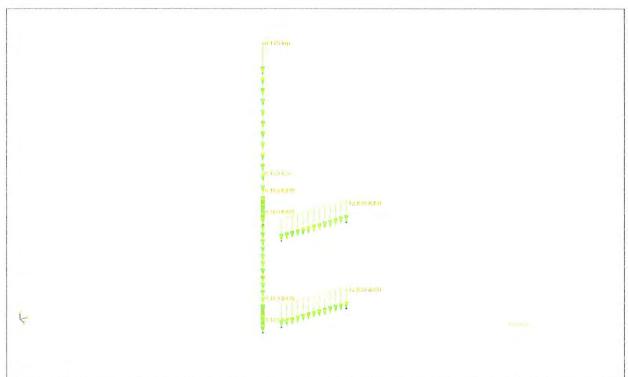
	Job No
Software licensed to STAAD.Pro CONNECTED User, Cory Senney	Part Alpha & Gamma Sectors
Job Title CT2490 - East Hampton Main Street	Ref
	By CS Date9/10/2019 Chd BK
Client AT&T	File Gamma Sector Standoff. Date/Time 10-Sep-2019 13:30

Combination Load Cases

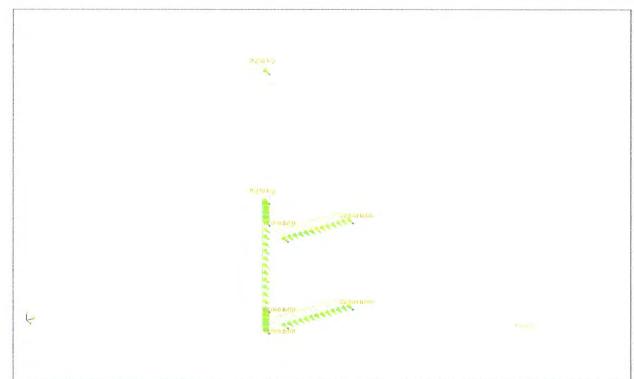
Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
6	1.2D + 1.0W	1	DL.	1.20
		3	W	1.00
7 1.2D + 1.0DI + 1.0W(I)	1	DL	1.20	
		2	DI	1.00
		4	W(I)	1.00
8	1.4D	1	DL.	1.40
9	1.0D + 1.0W(S)	1	DL	1.00
		5	W(S)	1.00
10	1D+1WL(Z)	1	DL.	1.00
		3	W	1.00







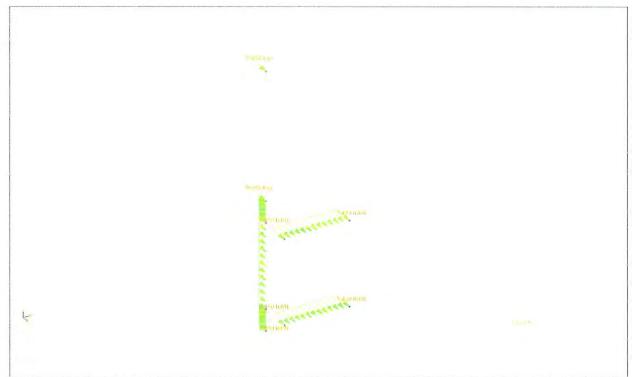
	Job No Sheet No B - 7 Rev				
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Alpha & Gamma Sectors				
Job Title CT2490 - East Hampton Main Street	Ref				
	By CS Date9/10/2019 Chd BK				
Client AT&T	File Gamma Sector Standoff.s Date/Time 10-Sep-2019 13:30				
AI&I	Gamma Sector Standoff.s Date Inne 10-Sep-2019 1				



Load Case 3

2		Job No 50093840	Sheet No B - 8	Rev				
Software licensed to STAAD.Pri CONNECTED User: Cory Senn	o ey	Part Alpha & Gamma Sectors						
lob Title CT2490 - East Hampton Ma		Ref						
		By CS	Date 9/10/2019 Ch	d BK				
Client AT&T		File Gamma Secto	r Standoff.s Date/Time 10-	Sep-2019 13:30				
Load Case 4	OLIANA LIA							

	Job No 50093840 Sheet No B - 9	Rev			
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Alpha & Gamma Sectors				
Job Title CT2490 - East Hampton Main Street	Ref				
	By CS Date9/10/2019 CI	hd BK			
Client AT&T	File Gamma Sector Standoff.s Date/Time 10-	-Sep-2019 13:30			



Load Case 5

Utilization Ratio

Beam	Analysis	Design	Actual	Allowable	Ratio	Clause	L/C	Ax	lz	ly	lx
	Property	Property	Ratio	Ratio	(Act./Allow.)			(in ²)	(in ⁴)	(in ⁴)	(in ⁴)
1	HSST4X4X0	HSST4X4X0	0.209	1.000	0.209	HSS FLEX+A	7	1.770	4.400	4.400	6.910
2	HSST4X4X0	HSST4X4X0	0.378	1.000	0.378	HSS BEND Y	3	1.770	4.400	4.400	6.910
7	PIPS30	PIPS30	0.001	1.000	0.001	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700
8	PIPS30	PIPS30	0.301	1.000	0.301	LRFD-H1-1B-	3	2.100	2.850	2.850	5.700
9	PIPS30	PIPS30	0.322	1.000	0.322	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700
10	PIPS30	PIPS30	0.241	1.000	0.241	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700

Failed Members

There is no data of this type.

			Job No 50093840	Sheet No B - 10	Rev
4	Software licensed to STAAD.Pro CONNECTED User, Cory Senney		Part Alpha & Gamm	a Sectors	
Job Tit	CT2490 - East Hampton Main Street		Ref		
			By CS	Date9/10/2019 Chd BK	
Client	AT&T		File Gamma Sector	Standoff.: Date/Time 10-Sep-	2019 13:30
ſ			mine the court of the control of the		
		Y			
		0.241			
		3,241			
		0,322			
		0.378			
		0.301			
			į.		
	4	0.00108 0.209		Load 5	
Ū	Itilization Ratio				

	Job No Sheet No B - 11 Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamma Sectors
Job Title CT2490 - East Hampton Main Street	Ref
	By CS Date9/10/2019 Chd BK
Client AT&T	File Gamma Sector Standoff.s Date/Time 10-Sep-2019 13:3

Node Displacements

Node	L/C	X	Υ	Z	Resultant	rX	rY	rZ
		(in)	(in)	(in)	(in)	(rad)	(rad)	(rad)
11	1:DL	-0.012	-0.036	0.001	0.038	-0.000	0.000	0.001
	2:DI	-0.022	-0.068	0.002	0.07118	-0.000	0.000	0.001
	3:W	-0.095	0.011	0.194	0.217	0.009	0.004	0.003
	4:W(I)	-0.019	0.002	0.038596	0.043	0.002	0.001	0.000
	5:W(S)	-0.023	0.003	0.046	0.052	0.002	0.001	0.001
	6:1.2D + 1.0W	-0.109	-0.032	0.196	0.226	0.009	0.004	0.003
	7:1.2D + 1.0DI	-0.055	-0.109	0.042	0.129	0.002	0.002	0.002
	8:1.4D	-0.016	-0.050	0.001	0.053	-0.000	0.000	0.001
	9:1.0D + 1.0W(-0.034	-0.033	0.047	0.067	0.002	0.001	0.001
12	1:DL	-0.053	-0.036	-0.006	0.064	-0.000	0.000	0.001
	2:DI	-0.100	-0.068	-0.009	0.121	-0.000	0.000	0.001
	3:W	-0.280	0.011	1.222	1.254	0.017	0.004	0.003
	4:W(I)	-0.055	0.002	0.238	0.245	0.003	0.001	0.000
	5:W(S)	-0.067	0.003	0.291	0.298	0.004	0.001	0.001
	6:1.2D + 1.0W	-0.344	-0.033	1.216	1.264	0.017	0.004	0.003
and the terminal way	7:1.2D + 1.0DI	-0.219	-0.109	0.222	0.330	0.003	0.002	0.002
	8:1.4D	-0.074	-0.050	-0.008	0.090	-0.000	0.000	0.001
	9:1.0D + 1.0W(-0.120	-0.034	0.285	0.311	0.004	0.001	0.001

Relative Displacement Check
Antenna Pipe Mast (3 1/2" O.D. Pipe):
Max Displacement = 1.038"
(Node 12 with respect to 11)
Allowable Displacement = 1.5% cantilever = 1.260"
1.038" < 1.26" -- OK

	Job No 50093840	B - 12	Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamn	na Sectors	
Title CT2490 - East Hampton Mair	Ref	***************************************	
	By CS	Date9/10/2019 Cho	BK
ent AT&T	File Gamma Secto	r Standoff.s Date/Time 10-S	Sep-2019 13:3
4			
Y		Load 5 Displacement	
Displacement			

	Job No Sheet No B - 13 Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Alpha & Gamma Sectors
Job Title CT2490 - East Hampton Main Street	Ref
	By CS Date9/10/2019 Chd BK
Client AT&T	File Gamma Sector Standoff.s Date/Time 10-Sep-2019 13:30

Reactions

		Horizontal	Vertical	Horizontal		Moment	
Node	L/C	FX	FY	FZ	MX	MY	MZ
Sancia Decounty control		(kip)	(kip)	(kip)	(kip in)	(kip in)	(kip in)
1	1:DL	-0.159	0.115	-0.073	0	-0.421	military and solds made
	2:DI	-0.300	0.219	-0.135	0	-0.745	
	3:W	0.000	-0.098	0.368	0	9.034	
	4:W(I)	0.000	-0.019	0.06116	0	1.496	
	5:W(S)	0.000	-0.023	0.08766	0	2.150	
	6:1.2D + 1.0W	-0.191	0.040	0.281	0	8.528	
	7:1.2D + 1.0DI	-0.491	0.338	-0.162	0	0.246	
	8:1.4D	-0.223	0.161	-0.102	0	-0.590	
	9:1.0D + 1.0W(-0.159	0.092	0.015	0	1.729	
2	1:DL	0.159	0.115	0.073	0	0.421	***************************************
	2:DI	0.300	0.219	0.135	0	0.745	
	3:W	-0.000	0.098	-1.050	0	-31.109	
	4:W(I)	-0.000	0.019	-0.215	0	-6.315	
	5:W(S)	0	0.023	-0.250	0	-7.402	
	6:1.2D + 1.0W	0.191	0.237	-0.963	0	-30.603	
-	7:1.2D + 1.0DI	0.491	0.376	0.008	0	-5.065	
	8:1.4D	0.223	0.161	0.102	0	0.590	
	9:1.0D + 1.0W(0.159	0.139	-0.177	0	-6.981	



Job No. 50093847 Sheet No. B-14 By: CS 09/11/2019 Chk: BK 09/13/2019

Analysis of Gamma Sector Stand-off Frame

Design Criteria

- 1. TMS 402-11/ACI 530-11/ASCE 5-11 Building Code Requirements for Masonry Structures
- 2. ACI -318-11 Building Code Requirements for Structural Concrete
- 3. AISC 360-10 Specifications for Structural Steel Buildings

References

Refer to construction drawings by Dewberry Engineers Inc.

Thru Bolt Check

$M_y =$	2.59 kip-ft	Max moment at thru-bolt connection (4 Bolts)
d =	6.00 in	Bolt Spacing
$F_{\times} =$	0.19 kip	Tensile Reaction at thru-bolt connection (4 Bolts)
T =	2.64 Kip	Tension at critical bolt (5/8"dia)
F _v =	0.24 kip	Vertical Shear Reaction at thru-Bolt connection (4 bolts)
$F_z =$	0.98 kip	Hor. Shear Reaction at thru-Bolt connection (4 bolts)
V =	1.00 kip	Shear at critical bolt (5/8"dia)
f _t =	8.61 ksi	Tensile Stress at critical bolt (5/8"dia)
f _v =	3.27 ksi	Shear Stress at critical bolt (5/8"dia)

Thru-Bolts OK by Inspection

Penthouse Wall Check

Based on Engineering Judgement, the loads produced by the antenna mounting pipes is negligible on the penthouse CMU and steel stud walls

7:14 PM

APPENDIX C





Job No. 50093847 Sheet No. C-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Beta Sector Ballast Frame

Overview

The existing equipment on the ballast frame consists of (3) antennas, (3) RRUS and (1) surge arrestor. New equipment, which consists of (1) antenna and (1) RRU, will be mounted to a new 3" diameter pipe, which will be attached to the existing ballast frame.

Design Criteria and References

- 1. International Building Code (IBC) 2015, International Code Council
- 2. 2018 Connecticut State Building Code Amendments to IBC 2015
- 3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
- 4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
- 5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
- 6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
- 7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
- 8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

STAAD Model Assumptions

- Wind pressure applied normal to the short and long sides of the ballast frame governs for sliding and overturning
- 2. Although the antenna frame is oriented roughly 30° from the direction of wind, the calculated wind forces will be applied normal to the longspan side of the frame for simplicity (slightly conservative)
- 3. Since the proposed pipe mast that the new antenna and RRU are going to be mounted to is braced in two directions, and the weight of the additional equipment and new steel is negligible with regard to the strength and serviceability of the ballast frame, only the global stability needs to be investigated.
- 4. The RAD center for the Beta Sector is 109', which is 8 feet lower than the Alpha/Gamma Sector RAD centers (117'). Since the difference in wind pressure is less than 1 psf, the design wind pressures calculated in Appendices A & B will be used for the Beta Sector Analysis:

 $q_{z \text{ design}} = 34.23 \text{ psf}$ See Appendices A&B

Use ASCE 7-10 ASD Load Combo 1.0D + 0.6W for stability check:

 $q_{z \text{ design}} = 20.54 \text{ psf}$ 0.6*W, to be used for Beta Sector Stability Check

Minimum F.S. = 1.5 for Overturning and Sliding

Existing frame rests on load bearing walls. Based on engineering judgement, the existing load bearing walls are OK



Job No. 50093847 Sheet No. C-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Beta Sector Ballast Frame

Equipment Dead Loads

	Description		Mainle (Uh)		
	Description	W	D	Н	
edia per	CCI HPA-65R-BU6AA	11.70	7.60	71.00	51.00
	Kathrein 800-10965	20.00	6.90	78.70	108.60
RHS	CCI OPA-65R-LCUU-H6	14.80	7.40	72.00	73.00
as/R	RRUS B25 4415	13.40	5.90	16.50	46.00
nn	RRUS B2/B12 4449	13.20	9.40	17.90	71.00
Ante	RRUS B2/B66A 8843	13.20	10.90	14.90	72.00
1	RRUS-32	12.10	6.70	26.70	60.00
	Raycap DC6-48-60-18-8C		9.00	26.00	31.80

^{*}Bold = Proposed

Structural Members

N. 0		Dimensions (in)							
Member	d	b _f	t _f	t _w	I.D.	O.D.	Weight (lb/ft)		
W12X19	12.2	4.01	0.35	0.235		Water and Deliver and Delivery of Street, or other Delivery or oth	19.00		
W6X25	6.38	6.08	0.455	0.32			25.00		
L3X3X3/8	3	3	0.375	0.375			7.20		
3" STD Pipe					3.07	3.50	7.58		

^{*}Bold = Proposed



Job No. 50093847 Sheet No. C-1 By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Beta Sector Ballast Frame

Force Coefficients for Appurtenances, Without Ice (TIA-222-H)

and the second					-		enumbus	
(Tangent) Table 2-9	1.48	1.55	1.49	1.21	1.20	1.20	1.27	1.22
(Normal) Table 2-9	1.36	1.26	1.31	1.20	1.20	1.20	1.20	
ble 2-9								
Aspect Katlo (Tangent)	9.34	11.41	9.73	2.80	1.90	1.37	3.99	2.89
Aspect Katio (Normal)	6.07	3.94	4.86	1.23	1.36	1.13	2.21	
(Tangent) (sf)	3.75	3.77	3.70	0.68	1.17	1.13	1.24	1.63
Area (A _{aln} (Normal) (sf)		10.93		1.54	1.64	1.37	2.24	
Height (or Span)	5.92	6.56	6.00	1.38	1.49	1.24	2.23	2.17
Length (tangent)	0.63	0.58	0.62	0.49	0.78	0.91	0.56	0.75
Width (Normal)	96.0	1.67	1.23	1.12	1.10	1.10	1.01	
Equipment	CCI HPA-65R-BU6AA	Kathrein 800-10965	CCI OPA-65R-LCUU-H6	RRUS B25 4415	RRUS B2/B12 4449	RRUS B2/B66A 8843	RRUS-32	Raycap DC6-48-60-18-8C
	Width Length Height (or (Normal) (sf) (Tangent) (Normal) (Tangent) (Tangent) (Tangent) (Tangent) (Tangent) (Table 2-9 (Normal) (tangent)	Width Length Height (or (Normal)) (sf) (Tangent) (Tangent) Table 2-9 (Normal) (Normal) (1.36 0.98 0.63 5.92 5.77 3.75 6.07 9.34 1.36	Equipment Width Length Height (or Normal) (sf) (Normal) (Tangent) (Tangent) (Tangent) (Normal) (Normal) (Normal) (Tangent) (Normal) (Normal) (Normal) (Tangent) (Normal) (Normal) (Normal) (Tangent) (Normal) (Normal)	Equipment Width Length Height for (Normal) (Normal) (sf) (forment) (Normal) (forment) (Normal) (sf) (Normal) (forment) (Normal) (forment)	Equipment Width Length Height (or normal) (Normal) (sf) (Normal) (Tangent) (Normal) (Normal)	Equipment Width Length Height (or Mormal) (Normal) (sf) (Tangent) Aspect National (normal) Aspect National (normal) Common (normal) (Normal)	Equipment Width Length Height (or Normal) (Normal) (S) (Normal) (S) (Normal) (S) (S)	Equipment Width Length Height (or Mormal) (Normal) (sf) (Tangent) Aspect Ratio (normal) Cable 2-9 (normal) (Normal) (sf) (Normal) (sf) (Normal) (sf) (Tangent) Cable 2-9 (normal) (Normal) (sf) (Normal) (sf

SAI Communications

East Hartford Main Street

By: CS 09/16/2019 Chk: SA 09/17/2019 Job No. 50093847 Sheet No. C-1

Analysis of Beta Sector Ballast Frame

Equipment Wind Loads (TIA-222-H)

 $F_A = q_z design G_h(EPA)_A$ $(EPA)_A = C_a A_a$

TIA-222-H, Section 2.6.11.2,

 $G_h = 1.0$ (See Appendices A & B)

		No	No Ice	γ	lce	Chron	Ctrongeth (Ibe)	C	(160)	Condi	Contino (Ibe)	Mainton	(Jdl) opacactaich
			(st)	f)		אוובווכ	Stil (105)	ט	(SOI)	אור מבו	(sqı) a	Maille	מווכב (ווחא)
i.	Farriament	(EPA) _A	(EPA) _A	(EPA) _A	(EPA) _A	T A	LL.	П. A	Ā	FA	FA	FA	T. A
2	pilicit	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)	(Normal)	(Tangent)
CCI HP.	CCI HPA-65R-BU6AA	7.84	5.54			160.96	113.75						
	Kathrein 800-10965	13.81	5.83			283.71	119.80						
CCI OP	CI OPA-65R-LCUU-H6	99.6	5.52			198.35	113.30						
	RRUS B25 4415	1.84	0.82			37.84	16.84						
	RRUS B2/B12 4449	1.97	1.40			40.44	28.80						
	RRUS B2/B66A 8843	1.64	1.35			33.66	27.80						
RRUS-32	32	2.69	1.57			55.29	32.30						
Raycap	Raycap DC6-48-60-18-8C		1.98				40.63						

*Wind loads shown reflect 0.6*W

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East Hartford Main Street

Job No. 50093847 Sheet No. C-1

By: CS 09/16/2019 Chk: SA 09/17/2019

Analysis of Beta Sector Ballast Frame

Structure Wind Loads (TIA-222-H)

Wind loads on structural elements will be applied linearly: $\omega_{wind} = q_z_{design} C_a G_h d$, with d being the structure depth or diameter. A conservative Ca value of 1.2 will be used for pipes, and 2/0 for W-Shapes and Angles.

Member	d (ft)	dice (ft)	رءً	ω _{wind} (lb/ft)	w _{wind ice} (Ib/ft)	$ \omega_{wind} _{loe}$ (lb/ft) $ \omega_{wind} _{loop}$ (lb/ft) $ \omega_{wind} _{loop}$ (lb/ft)	$\omega_{wind m}$ (lb/ft)
W12X19	1.02		2.0	41.76			
W6X25	0.53		2.0	21.84			
L3X3X3/8	0.25		2.0	10.27			
3" STD Pipe	0.29		1.2	7.19	Cal market		

*Wind loads shown reflect 0.6*W

	Job No 50093847	Sheet No C - 6	Rev
Software licensed to STAAD Pro CONNECTED User: Cory Senney	Part Beta Sector		
Job Title CT2490 - East Hampton Main Street	Ref		
	By CS	Date9/10/2019 Cho	^d BK
Client AT&T	File Beta Sector.std	Date/Time 11-S	Sep-2019 10:37

Job Information

	Engineer	Checked	Approved
Name:	CS	BK	
Date:	9/10/2019	9/12/2019	

Project ID	
Project Name	

Structure Type | SPACE FRAME

Number of Nodes	61	Highest Node	66
Number of Elements	92	Highest Beam	102

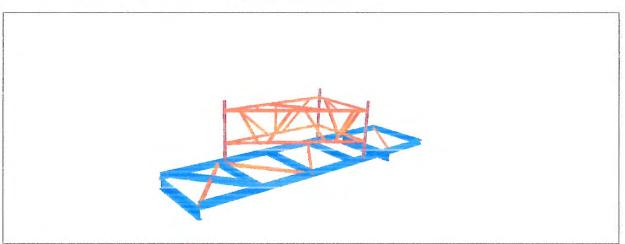
Number of Basic Load Cases	3
Number of Combination Load Cases	2

Included in this printout are data for:

All	The Whole Structure
Residence and the second second	

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	WIND(Z)
Primary	3	WIND(X)
Combination	4	1.0D + 1.5W(Z)
Combination	5	1.0D + 1.5W(X)



3D Rendered View

	Job No 50093847	Sheet No C - 7	Rev
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Beta Sector	- Emilian de la company de la	
Job Title CT2490 - East Hampton Main Street	Ref		
	By CS	Date 9/10/2019	Chd BK
Client AT&T	File Beta Sector.std	Date/Time 11	I-Sep-2019 10:37

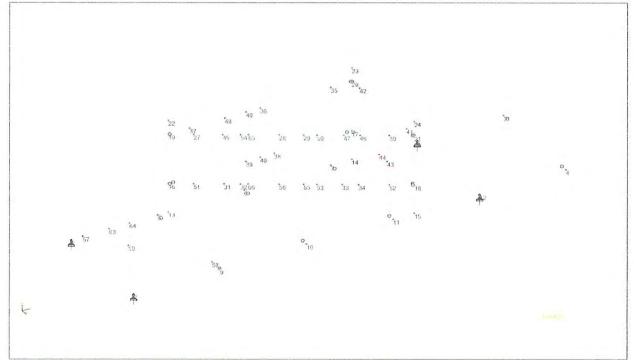
Nodes

Node	X	Υ	Z	
	(ft)	(ft)	(ft)	
1	0	0	C	
2	0	0	7.667	
3	30.625	0	0	
4	30.625	0	7.667	
5	6.125	0	0	
6	12.250	0	0	
7	18.375	0	C	
8	24.500	0	C	
9	6.125	0	7.667	
10	12.250	0	7.667	
11	18.375	0	7.667	
12	24.500	0	7.667	
13	6.875	0	(
14	19.875	0	C	
15	19.875	0	7.667	
16	6.875	2.000	0	
17	19.875	2.000	C	
18	19.875	2.000	7.667	
19	6.875	5.500	(
20	19.875	5.500	(
21	19.875	5.500	7.667	
22	6.875	6.500	(
23	19.875	6.500	(
24	19.875	6.500	7.667	
27	8.207	5.500	0.785	
28	12.729	5.500	3.452	
29	14.021	5.500	4.214	
30	18.543	5.500	6.88	
31	9.822	2.000	1.738	
32	10.683	2.000	2.246	
33	16.067	2.000	5.421	
34	16.928	2.000	5.929	
35	18.375	5.500	(
36	13.375	5.500	(
37	8.375	5.500	(
38	14.375	2.000	(
39	12.375	2.000	(
40	13.375	2.000	(
41	19.875	5.500	6.708	
42	19.875	5.500	0.958	
43	19.875	2.000	4.333	
44	19.875	2.000	3.333	
45	9.746	5.500	1.693	
46	17.004	5.500	5.973	
47	16.142	5.500	5.465	

	Job No 50093847	C - 8	Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Beta Sector		
Job Title CT2490 - East Hampton Main Street	Ref		
	By CS Date9/10/2019 Chd BK		BK
Client AT&T	File Beta Sector.std	Date/Time 11-S	Sep-2019 10:37

Nodes Cont...

Node	Х	Υ	Z
	(ft)	(ft)	(ft)
48	10.875	5.500	0
49	12.375	5.500	0
50	14.721	5.500	4.627
51	8.207	2.000	0.785
52	18.543	2.000	6.881
53	14.721	2.000	4.627
54	10.683	5.500	2.246
55	14.021	2.000	4.214
56	12.729	2.000	3.453
57	0.830	0	0
58	6.125	0	6.667
59	2.696	0	2.349
63	2.696	0	0
64	4.125	0	0
65	11.105	5.500	2.495
66	11.087	2.000	2.484



	Job No 50093847	Sheet No C - 9	Rev	
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Beta Sector			
Job Title CT2490 - East Hampton Main Street	Ref			
	By CS Date9/10/2019 Chd BK			
Client AT&T	File Beta Sector.std	Date/Time 11-S	Sep-2019 10:37	

Beams

Beam	Node A	Node B	Length	Property	β
			(ft)		(degrees)
1	1	57	0.830	1	0
2	2	9	6.125	1	0
3	1	2	7.667	2	0
4	3	4	7.667	1	0
5	5	13	0.750	1	0
6	6	7	6.125	1	0
7	7	14	1.500	1	0
8	8	3	6.125	1	0
9	9	10	6.125	1	0
10	10	11	6.125	1	0
11	11	15	1.500	1	0
12	12	4	6.125	1	0
13	5	58	6.667	1	0
14	6	10	7.667	1	0
15	7	11	7.667	1	0
16	8	12	7.667	2	0
17	2	5	9.813	3	45
18	5	10	9.813	3	45
19	10	7	9.813	3	45
21	12	3	9.813	3	45
22	13	6	5.375	1	0
23	14	8	4.625	1	0
24	15	12	4.625	1	0
25	13	16	2.000	4	0
26	16	19	3.500	4	0
27	19	22	1.000	4	0
28	14	17	2.000	4	0
29	17	20	3.500	4	0
30	20	23	1.000	4	0
31	15	18	2.000	4	0
32	18	21	3.500	4	0
33	21	24	1.000	4	0
35	18	43	3.333	3	45
36	17	38	5.500	3	45
37	19	27	1.546	3	45
38	21	41	0.958	3	45
39	20	35	1.500	3	45
43	28	29	1.500	3	45
44	29	50	0.813	3	45
45	30	21	1.546	3	45
46	16	51	1.546	3	45
47	31	32	1.000	3	45
48	32	66	0.469	3	45
49	33	34	1.000	3	45
50	34	52	1.875	3	45

	Job No 50093847	C - 10	Rev		
Software licensed to STAAD.Pro CONNECTED User, Cory Senney	Part Beta Sector				
Job Title CT2490 - East Hampton Main Street	Ref				
	By CS	Date9/10/2019 Chd	вк		
Client AT&T	File Beta Sector.std	Date/Time 11-S	ep-2019 10:37		

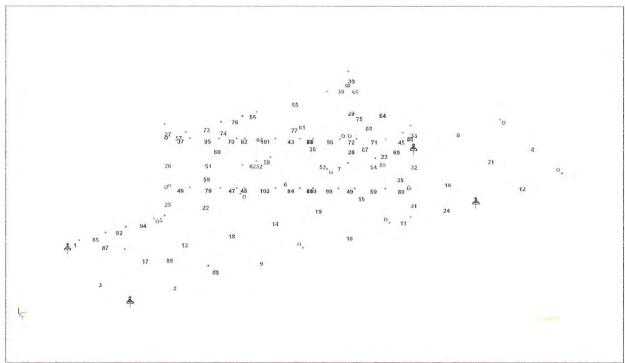
Beams Cont...

Beam	Node A	Node B	Length	Property	β
			(ft)		(degrees
51	27	31	3.971	3	45
52	32	28	4.230	3	45
53	29	33	4.230	3	45
54	34	30	3.971	3	45
55	35	36	5.000	3	45
56	36	49	1.000	3	45
57	37	19	1.500	3	45
58	38	40	1.000	3	45
59	39	16	5.500	3	45
60	37	39	5.315	3	45
61	35	38	5.315	3	45
62	40	39	1.000	3	45
63	36	40	3.500	3	45
64	41	42	5.750	3	45
65	42	20	0.958	3	45
66	43	44	1.000	3	45
67	44	17	3.333	3	45
68	42	44	4.230	3	45
69	41	43	4,230	3	45
70	45	54	1.088	3	45
71	46	30	1.787	3	45
72	47	46	1.000	3	45
73	48	37	2.500	3	45
74	45	48	2.035	3	45
75	46	42	5.779	3	45
76	49	48	1.500	3	45
77	49	47	6.638	3	45
78	50	29	0.813	3	45
79	51	31	1.875	3	0
80	52	18	1.546	3	0
81	53	55	0.813	3	0
82	54	65	0.490	3	45
83	55	53	0.813	3	0
84	56	55	1.499	3	45
85	57	63	1.866	1	0
86	58	9	1.000	1	0
87	57	59	3.000	5	0
88	59	58	5.514	5	0
92	63	64	1.429	1	0
94	64	5	2.000	1	0
95	27	45	1.787	3	45
96	50	47	1.650	3	45
97	29	50	0.813	3	45
99	53	33	1.563	3	0
100	55	53	0.813	3	45

	Job No 50093847	Sheet No C - 11	Rev		
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Beta Sector				
Job Title CT2490 - East Hampton Main Street	Ref				
	By CS	Date9/10/2019 Ch	d BK		
Client AT&T	File Beta Sector.std	Date/Time 11-	Sep-2019 10:37		

Beams Cont...

Beam	Node A	Node B	Length	Property	β
			(ft)		(degrees)
101	65	28	1.885	3	45
102	66	56	1.907	3	45



Beam Layout

Section Properties

Prop	Section	Area (in²)	l _{yy} (in ⁴)	l _{zz} (in ⁴)	J (in ⁴)	Material
1	W6X25	7.340	17.100	53.400	0.461	STEEL
2	W12X19	5.570	3.760	130.000	0.180	STEEL
3	L30306	2.110	2.793	0.727	0.102	STEEL
4	PIPS30	2.100	2.850	2.850	5.689	STEEL
5	W6X15	4.430	9.320	29.100	0.101	STEEL

2	Job No 50093847	Sheet No C - 12	Rev		
Software licensed to STAAD.Pro CONNECTED User, Cory Senney	Part Beta Sector				
Job Title CT2490 - East Hampton Main Street	Ref				
	By CS Date9/10/2019 Chd BK				
Client AT&T	File Beta Sector.std	Date/Time 1	1-Sep-2019 10:37		

Materials

Mat	Name	E (kip/in²)	ν	Density (kip/in³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E -6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E -6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
7	STEEL	29E+3	0.300	0.000283	6E -6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6

Supports

Node	Х	Υ	Z	rX	rY	rZ
	(kip/in)	(kip/in)	(kip/in)	(kip ft/deg)	(kip ⁻ ft/deg)	(kip ⁻ ft/deg)
1	Fixed	Fixed	Fixed	-	-	-
2	Fixed	Fixed	Fixed	-	-	-
8	Fixed	Fixed	Fixed	-	-	-
12	Fixed	Fixed	Fixed	-	-	-

Releases

Beam ends not shown in this table are fixed in all directions.

Beam	Node	Х	У	Z	rx	ry	rz
4	3	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
4	4	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
13	5	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
14	6	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
14	10	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
15	7	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
15	11	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
35	18	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
36	17	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
37	19	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
38	21	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
39	20	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
45	21	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
46	16	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
57	19	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
59	16	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
65	20	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
67	17	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
80	18	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
86	9	Fixed	Fixed	Fixed	Pin	Fixed	Fixed

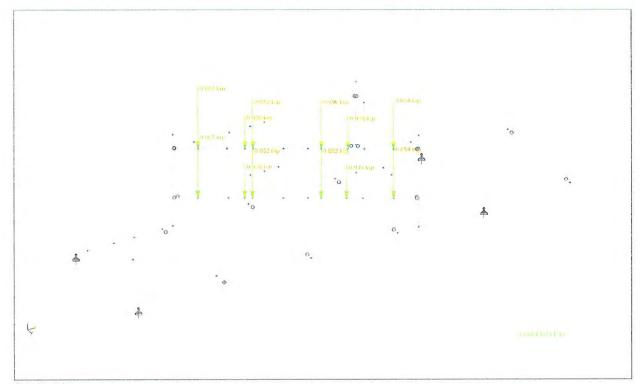
	Job No 50093847	C - 13
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Beta Sector	
Job Title CT2490 - East Hampton Main Street	Ref	
	By CS	Date9/10/2019 Chd BK
Client AT&T	File Beta Sector.std	Date/Time 11-Sep-2019 10:37

Primary Load Cases

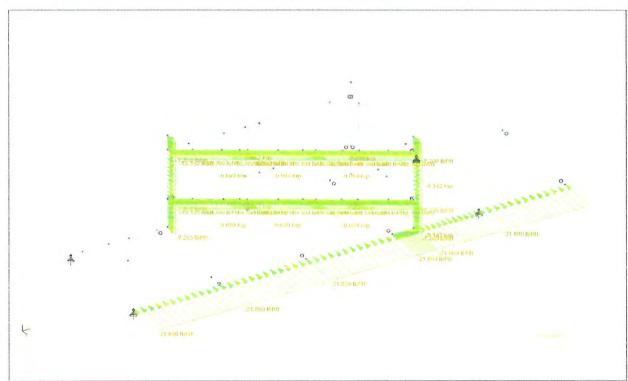
Number	Name	Туре	
1	DL	Dead	
2	WIND(Z)	Wind	
3	WIND(X)	Wind	

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	1.0D + 1.5W(Z)	1	портобрать по при	1.00
		2	WIND(Z)	1.50
5 1.0	1.0D + 1.5W(X)	1	DL	1.00
		3	WIND(X)	1.50

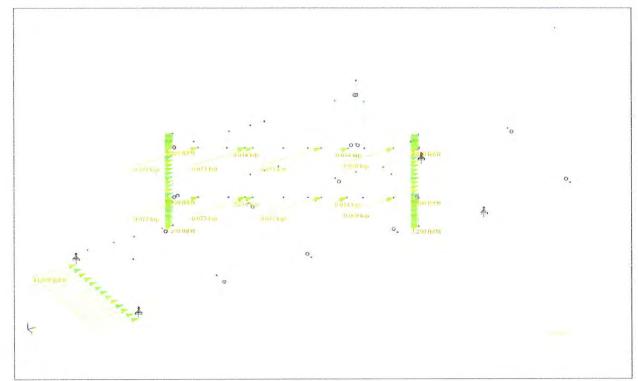


	Job No 50093847	C - 14	Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Beta Sector		
Job Title CT2490 - East Hampton Main Street	Ref		CONTRACTOR
	By CS	Date9/10/2019 Cho	ⁱ BK
Client AT&T	File Beta Sector.std	Date/Time 11-S	Sep-2019 10:37



Wind Load (Z)

	Job No 50093847	C - 15	Rev
Software licensed to STAAD.Pro CONNECTED User. Cory Senney	Part Beta Sector		on the same of the
^{b Title} CT2490 - East Hampton Main Street	Ref		
	By CS	Date9/10/2019 Chd	BK
Client AT&T	File Beta Sector.std	Date/Time 11-S	ep-2019 10:37



Wind Load (X)

Reactions

		Horizontal	Vertical	Horizontal		Moment	
Node	L/C	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip in)	MZ (kip in)
2 3 4 5 2 1 2 3 4 5 8 1 2 3 4 5 1 2 1 2 1 1 2 1 1 1 2 1 1 1 1 1 1 1 1	1:DL	0.683	1.213	-0.110	0	0	
	2:WIND(Z)	1.722	0.107	0.448	0	0	
	3:WIND(X)	-0.381	-0.088	-0.096	0	0	
	4:1.0D + 1.5W(3.266	1.373	0.562	0	0	
	5:1.0D + 1.5W(0.111	1.080	-0.253	0	0	
2	1:DL	-0.012	0.669	0.163	0	0	
	2:WIND(Z)	-1.788	-0.107	1.110	0	0	
	3:WIND(X)	-0.250	-0.009	0.090	0	0	
	4:1.0D + 1.5W(-2.693	0.509	1.828	0	0	
	5:1.0D + 1.5W(-0.387	0.655	0.297	0	0	
8	1:DL	-0.513	1.314	-0.164	0	0	
	2:WIND(Z)	0.479	0.567	0.287	0	0	
8	3:WIND(X)	-0.179	0.088	0.014	0	0	
8 2	4:1.0D + 1.5W(0.205	2.165	0.267	0	0	
	5:1.0D + 1.5W(-0.782	1.446	-0.142	0	0	
12	1:DL	-0.158	1.447	0.111	0	0	
	2:WIND(Z)	-0.414	-0.567	0.213	0	0	

	Јор No 50093847	C - 16	Rev
Software licensed to STAAD.Pro CONNECTED User: Cory Senney	Part Beta Sector	•	
Job Title CT2490 - East Hampton Main Street	Ref		
	By CS	Date 9/10/2019 Che	d BK
Client AT&T	File Beta Sector.std	Date/Time 11-9	Sep-2019 10:37

Reactions Cont...

		Horizontal	Vertical	Horizontal		Moment	
Node	L/C	FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip ⁻ in)	MZ (kip ⁻ in)
	3:WIND(X)	-0.225	0.009	-0.008	0	0	0
	4:1.0D + 1.5W(-0.778	0.596	0.431	0	0	0
	5:1.0D + 1.5W(-0.496	1.461	0.098	0	0	0

Z-Direction Wind governs for Sliding and Overturning

Per Construction Drawings by Hudson Design Group dated 11/08/2016, ballast is adhered to roof paver

Coef. of Friction = 0.8

Total weight 4.643 kip

Total sliding force = 3.088 kip (Sum of Fz Reactions)

0.8)*(4.643) = 3.715 > 3.088 kip --> Sliding OK

APPENDIX D





ASCE 7 Hazards Report

Address:

886 Main St

East Hartford, Connecticut

06108

ASCE/SEI 7-10 Standard:

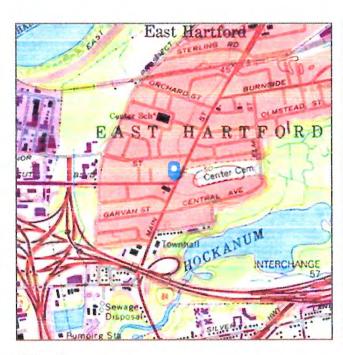
Risk Category: II

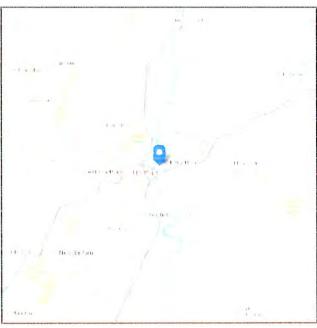
Soil Class:

Elevation: 40.7 ft (NAVD 88)

Latitude: 41.769404

Longitude: -72.64371





Wind

Results:

Wind Speed:	123 Vmph
10-year MRI	77 Vmph
25-year MRI	86 Vmph
50-year MRI	93 Vmph
100-year MRI	100 Vmph

ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of Data Source:

March 12, 2014

Wed Sep 11 2019 Date Accessed:

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

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Section 15C - CURRENT TOWER CONFIGURATION - SECTOR stows rottens Antensa rottens Antensa rottens																																							FINH LOCATION (Top/Bellers Integrated/Nems)	8	8	.8	100
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rvice specified	_		ANTERSA SIZE OF W. W. D.	ANTENNA WEIGHT 108.6	ATTAUTH	-	RADIATION CENTER (1641) 140	ANTENNA TIP HEIGHT 120	MECHANICAL DOMITLE	PEEDER AMOUNT	OVE (TIP to TIP)	ST ANTENNA to	o CENTERLINE	CENTERLINE	ast # of inches	TOTA MODES	DIPLECER (QTV MODEL)	DUPLEXER (GTY/MODEL)	T (QTYMODEL)	DC BLOCK (GTY MODEL)	TMALMA (QTYMODEL)	A (OTY MODEL)	PDU FOR TMAS (OTYTHODEL)	FLIER (GTY MODEL)	SQUD (GTY3/ODEL	DO TRUNK (GTYNSODEL)	REPEATER (OTYMODEL)	RIBH - 780 band (QTY MODEL)	PARH - 850 band (GTY MODEL)	(divisobel)	d (QTY MODEL)	d (OTYMODEL	S (OTV MODEL.	1 (GTVRADBEL)	ment 2 (QTY MODEL)	mpenent 3 (QTY MODEL)	Local Market Note 1	Local Market Note 3	n (fuggo) eastn	5 -	10 40	2.0	1
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	ANTERNA YENDOR				5									
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The color	ANTENNA WEIGHT				51									
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	FADIATION CENTER (feet)				140									
	THORN ATTENDED A				143									
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	HOSEONYAL SEPARATION from CLOSEST ANTERNA to													
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	Antenna NET CONTROL UNIT (QTV MODEL)				H4017					T				
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The color of the	RRH - AWS band (GTY ASDEL)													
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The property The	Additional ROth 61 - any band (OTY MODEL)													
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	AL SEPARATION from ANTERNA ABOVE (TIP to T.P.)											
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	Antenna NET CONTROL UNIT (GTV 1400EL)			を出まれ								
	DC BLOCK (GTVMODEL)											
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	CUMMENT INJECTORS FOR TWA (QTV MODEL)											
	POUFOR TMAS (GTV NODEL.											
	FLTER (GTYMODEL)						1					
	SQUID (QTVANOBEL)											
	FIRET TRUNK (GTV NODEL)						1					
	DC TRUNK (GTVANODEL)											
	REPEATER (QTYNODES)											
	Riffet - 706 band (GTV/skopel.)											
	FIRM - 800 band /GTV NODEL.											
MINIST See of OTT WHOCH A MARKET SEE OF THE	FIRSH - 1900 band (QTY/MODEL)			4415 025								
Address PDN FT - EVY bed (OTV WOOD) Address PDN FT - EVY bed (OTV WOOD)	Mith - AWS band OTY MODEL											
Additional PRINTS - any band (OTV'NOOR). Additional PRINTS - any band (OTV'NOOR).	FRM-WCS bard/OTYMODEL							I				
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	Additional Fifth #2 - pry band (QTYMODEL)											
	Appending Composition 1 (A. V. VOULL.)											
Additional Common of Official And Additional A												
	Local Market Note 1,400 hargord artenna	ano 4415 R 25										
Constitute Notes	Local Markel Note 3											
FEDGRE PRINCE PR	PORT NUMBER USED (CSGng) USED (Aloit)	ATOLL CELL ID	TECHNOLOGY - PREQUENCY		ELECTRICAL AZMUTH	PRE-LOCATION (Top-Bottom) Integrated Nane)	FEEDER LPVGTH (feet)	**********	THIPLEXER or LLC (MODEL)			CABLE CABLE NUMBER ID(coorg)
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The control of the					Section 15C - PLA	MINED PROPOSE	D TOWER COM	FIGURATION - SE	STORC					
Column C		JAWA POSITION 1	ANTENIA POSITION 2	AMTENNA POSITION 3	400	ANTENNA	POSITIONS	AVCTEVNA POSTEON 6	AATDWA	POSITION?				
Column C						-								
	Existing Antenna?													
	ANTERNA MAKE - WODEL													
	AUTENIA YENDOR				100									
	ANTEMA SIZE HAWED				71X11 7X 6									
	ANTENNA VIENOHT				-51									
Column C	AZBRUTH				350									
	MAGNETIC DECUNATION													
	FADIATION CENTER (feet				140									
	ANTERNATIP HEGHT				143									
Column C	WECHANGAL DOWNTET				0									
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	TICAL SEPARATION from ANTENNA ABOVE (TIP to TIP).													
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	Antoma RET Meter (GTV MODEL)				100									
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	DIPLEXER (GTYANDEL)					-								
	DUPLEMER (STYMODEL)					1			-					
Part	Antonna RET CONTROL UNIT (GTV1800EL:				He 3.1	-								
	DC SLOCK (GTY MODEL)													
	THALMA (GTV MODEL)				-		1							
Part	CURRENT INLECTIONS FOR TMA (OTY MODEL.													
	POU FOR TMAS (QTY MODEL)													
	FILTER (GTYMODEL)													
Figure 19 Figu	SQUID (GLAYMODEL)													
Part	FIBER TRUTH CATY MODEL													
Provision Prov	DC TRUNK (QTY MODEL)													
Principles Contribution Principles P	REPEATER (GTYSMODEL).													
Procession Pro	FIRM: 700 band (QTYAAODEL)		-											
This bill control of the control o	FIRM - 686 band (QTV) NODEL)								-					
Triangle And Part P	RIPN - 1900 band (QTYMODIEL)				1 4415 825									
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This is the supplication of the control of the co	MRH - WCS band (GTY NODEL)													
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RRUS 4415 B25

- , B25
- TX = 1930 1995 MHz
- RX = 1850 1915 MHz
- CPRI 2 ports x 2.5/4.9/9.8/10.1 Gbps. Install 2 SFPs and connect 2 fiber pair to the RRUS 4415 during initial install
- Only use Ericsson supplied and approved SFPs RDH10265/25

Exception SFP7 RDH 1(265.3 for CPRI * 4km to 10km Exception SPP7 (pa.), RDH 102 70/1 and RDH 102 70/2 for CPRI > 10km

- 2 external alarm inputs
- Max wind load @ 50m/sec = 260N
- Breaker size = 25A, DC Power Consumption = 670 W (for dimensioning)
- 200mm horizontal separation required for side by side mounting
- 200mm separation required from antenna backplane to radio
- 400mm vertical outdoor/indoor separation required between 2 radios
- 500mm vertical separation below antenna
- Min, Max DC cable size from squid to radio = 10,8 AWG
 - Adapter is required for 2-wire connection
- Shielded DC cable is required
- Ground cable size = 2AWG
- Dimensions (incl. handles, feet and sunshield, w/o fan unit)
- Height: 16.5" (420 mm)
 - Width 13.4" (342 mm)
- Depth: 5.9" (149 mm)
- Weight, excl. mounting hardware = 46 lbs (21 kg)





SPECIFICATIONS OctoPort Multi-Band Antenna

OPA-65R-LCUU-H6

- 10	- 1					
-	- 1	0	0	r	10	a

Ports	2 × Low Band Ports for 698-787 MHz	2 x Low Band Ports for 824-894 MHz	4	× High Band Ports	for 1710-2360 MI	-iz
Frequency Range	698-787 MHz	824-894 MHz	1850-1990 MHz	1710-1755/21	10-2170 MHz	2305-2360 MHz
Gain	13.8 dBi	14.6 dBi	17.0 dBi	16.3 dBi	17.4 dBi	17.6 dBi
Azimuth Beamwidth (-3dB)	66°	61°	60°	68°	64°	60°
Elevation Beamwidth (-3dB)	12.2°	10.3°	5.7°	6.3°	5.1°	4.5°
Electrical Downtilt	0° to 10°	0° to 10°	0° to 8°	0° to 8°	0° to 8°	0° to 8°
Elevation Sidelobes (1st Upper)	< -17 dB	< -18 dB	< -19 dB	< -19 dB	< -18 dB	< -18 dB
Front-to-Back Ratio @180°	> 30 dB	> 27 dB	> 32 dB	> 32 dB	> 35 dB	> 35 dB
Front-to-Back Ratio over ± 20°	> 27 dB	> 25 dB	> 27 dB	> 27 dB	> 28 dB	> 28 dB
Cross-Polar Discrimination (at Peak)	> 22 dB	> 22 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Cross-Polar Discrimination (at ± 60°)	> 16 dB	> 14 dB	> 17 dB	> 17 dB	> 17 dB	> 17 dB
Cross-Polar Port-to-Port Isolation	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Voltage Standing Wave Ratio (VSWR)	< 1.5.1	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5 1	< 1.5:1
Passive Intermodulation (2×20W)	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc
Input Power Continuous Wave (CW)	500 watts	500 watts	300 watts	300 watts	300 watts	300 watts
Polarization	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°
Input Impedance	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms
Lightning Protection	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground

Mechanical

Dimensions (L×W×D) 72.3×14.4×7.3 in (1836×366×185 mm)

Survival Wind Speed > 150 mph (> 241 kph)

Front Wind Load 243 lbs (1081 N) @ 100 mph (161 kph) Side Wind Load 140 lbs (622 N) @ 100 mph (161 kph)

Equivalent Flat Plate Area 9.5 ft² (0.9 m²)

Weight * 56.9 lbs (25.8 kg)

RET System Weight 6.6 lbs (3.0 kg)

Connector 8 x 7-16 DIN female long neck

Mounting Pole 2 to 5 in (5 to 12 cm)

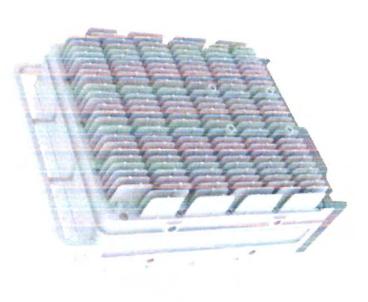
* Weight excludes mounting and RET

RRUS 4449 B5, B12

- B5, B12
- B5 TX = 869 894 MHz, B12 TX = 729 746 MHz
- B5 RX = 824 849 MHz B12 RX = 699 716 MHz

Both frequency bands are combined to transmit/receive out the same RF connectors.

- CPRI 2 ports x 2.5/4 9/9.8/10.1 Gbps. Install 2 SFP7s and connect 2 fiber pair to the RRUS 4449 during initial install. 2nd CPRI is reserved for 5G NR deployment later. Do not connect SFP7 to DUL20.
 - Only use Ericsson supplied and approved SFP7s RDH10265/25
- install 2 SFP RDH 10285/3 to CPR/Length 1.4 km ± 10 km install SFP7 (part) RDH102 70/1 and RDH 102 70/2 (priorectional SFP7 for CPRI length > 10 km
- 2 external alarm inputs
- Max wind load @ 50m/sec = 260 N
- connections must be connected and operational for the radio to operate. Each power feed must support Breaker size = 2x25A, DC Power Consumption = 1440 W (for dimensioning). Both DC power AWG Y DC split jumper cable connected from the surge suppressor to the 4449 DC po
- 40mm horizontal separation required for side by side mounting
- 200mm separation required from antenna backplane to radio
- 400mm vertical outdoor/indoor separation required between 2 radios
- 500mm vertical separation below antenna
- Min, Max DC cable size from squid to radio = 10,8 AWG
- Adapter is required for 2-wire connection
- Shielded DC cable is required
- Ground cable size = 2AWG
- Dimensions (incl. handles, feet and sunshield, w/o fan unit)
 - Height 17.9" (455 mm)
- Width 13.19" (335 mm)
- Depth: 9.44" (240 mm)
- Weight, excl. mounting hardware = 71 lbs (32 kg)



RRUS 8843 B2, B66A



- B2 TX=1930-1990 MHz, B66A TX=2110-2180 MHz
- B2 RX = 1850 1910 MHz, B66A RX = 1710-1780 MHz
- during initial install, 2nd CPRI is reserved for 5G NR deployment later. Do not connect SFP7 to DUL20 CPR1 2 ports x 2.5/4.9/9.8/10.1 Gbps. Install 2 SFP7s and connect 2 fiber pair to the RRUS 8843
- Only use Ericsson supplied and approved SFP7s RDH10265/25
 - nstall 2 SFP FDH 10266/3 for CPRI length 1 4 km 10 wm
- install SPP7 (pair) RDH 102 70/1 and RDH 102 70/2 (b)-directional SFP7 for CPR llength > 10 km

2 external alarminouts

connections must be connected and operational for the radio to operate. Each DC Feed must support 1100W individually for cable size, voltage drop engineering. A single DC trunk cable that can handle Breaker size = 2x30A, DC Power Consumption = 1520 W (for dimensioning), Both DC power Max wind load @ 50m/sec = 260 N

1520W and #10AWG Y DC splitter cable from the surge suppressor to the 2 DC power connections

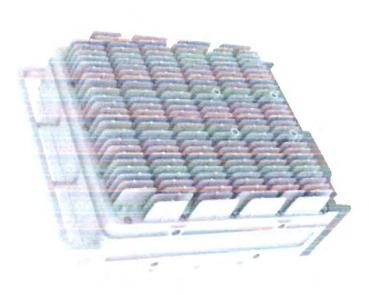
40 mm horizontal separation required between radios mounted side by side

can be used with a single 40A breaker.

- 200mm separation required from antenna backplane to radio
- 400mm vertical outdoor/indoor separation required between 2 radios
- 500mm vertical separation below antenna
- 200mm horizontal separation between radio and side edge of antenna
- Min, Max DC cable size from squid to radio = 10,8 AWG
- Adapter is required for 2-wire connection
- Shielded DC cable is required

Ground cable size = 2AWG

- Dimensions (incl. handles, feet and sunshield, w/o fan unit)
- Height 14.9" (380 mm
- Width: 13.2" (335 mm)
- Weight, excl. mounting hardware = 72 lbs (32.6 kg)



RRUS 32 B30





- WCS A+B blocks
- -TX = 2350 2360 MHz
- -RX = 2305 2315 MHz
- > RF output 4 x 25 Watts
- 4T4R FDD
- 10 MHz IBW for LTE
- CPRI 2 ports x 10 Gbps
- > Dimensions (incl. feet and sunshield)
- Height: 26.7" (678 mm)
- Width: 12.1" (306 mm)
- Depth: 6.7" (171 mm)
- > Weight, excl. mounting hardware
- 60 lbs (23 kg)

APPENDIX E







Town of East Hartford Property Summary Report

886 MAIN ST

MAP LOT: 13-332 **CAMA PID:** 8733

LOCATION: 886 MAIN ST

OWNER NAME: HARTFORD EAST ASSOCIATION



OWNER OF RECORD

HARTFORD EAST ASSOCIATION

954 WARWICK AVE

WARWICK, RI 02888

8733 03/27/2016

LIVING AREA: 97981 ZONING: B5 ACREAGE: 1.19

SALES HISTORY				
OWNER BOOK / PAGE SALE DATE SALE PRICE			SALE PRICE	
HARTFORD EAST ASSOCIATION	27/ 37	01-Jan-1900	\$0.00	

CURRENT PARCEL ASSESSMENT					
TOTAL:	\$6,440,000.00	IMPROVEMENTS:	\$6,076,700.00	LAND:	\$363,300.00

ASSESSING HISTORY				
FISCAL YEAR	TOTAL VALUE	IMPROVEMENT VALUE	LAND VALUE	
2018	\$6,440,000.00	\$6,076,700.00	\$363,300.00	
2017	\$5,390,000.00	\$5,026,700.00	\$363,300.00	
2016	\$4,760,000.00	\$4,396,700.00	\$363,300.00	
2015	\$4,760,000.00	\$4,396,700.00	\$363,300.00	
2014	\$5,943,560.00	\$5,580,260.00	\$363,300.00	

Town of East Hartford Property Summary Report

886 MAIN ST

MAP LOT: 13-332 CAMA PID:	8733
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LOCATION: 886 MAIN ST

OWNER NAME: HARTFORD EAST ASSOCIATION

BUILDING #1

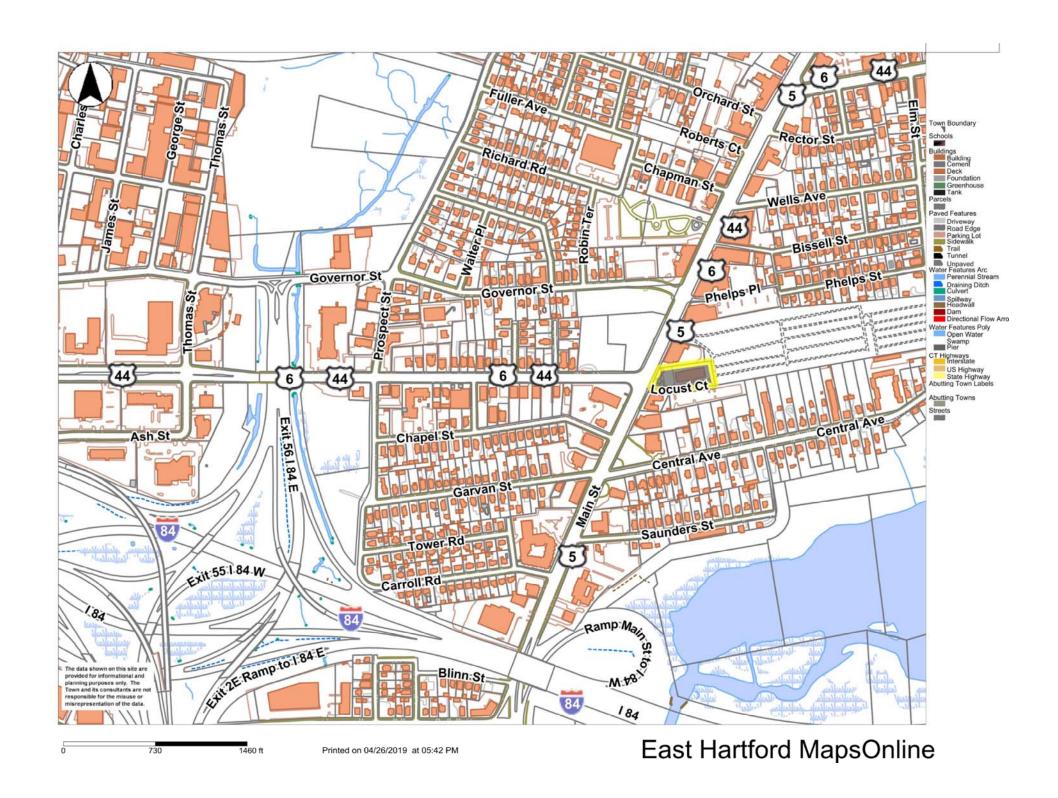
YEAR BUILT	1983	EXT WALL 1	Brick
STYLE	High Rise	INT WALLS 1	Drywall
MODEL	Comm/Ind	HEAT FUEL	Gas
STORIES	11	HEAT TYPE	Forced Hot Air
OCCUPANCY	Apt w/ Elevator	AC TYPE	Unit
ROOF	Flat	BEDROOMS	
ROOF COVER	Rubber	FULL BATHS	0
FLOOR COVER 1	Mixed	HALF BATHS	
% BSMT	null	TOTAL ROOMS	120
% FIN BSMT	null	% REC RM	null
% SEMI FIN	null	% ATTIC FINISH	null
BSMT GARAGE	null	FIREPLACES	null



8733 03/27/2016

EXTRA FEATURES			
DESCRIPTION	CODE	UNITS	
Sprinklers-Wet	SPR1	97981 S.F.	
Elevator Pass	ELV1	2 UNITS	

OUTBUILDINGS				
DESCRIPTION CODE UNITS				
FR/SHED		90 SF		





STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401 New Britain, Connecticut 06051-4225 Phone: 827-7682

Petition No. 324

Metro Mobile CTS of Hartford, Inc. 886 Main Street East Hartford, CT

> Staff Report August 9, 1994

On July 29, 1994, Connecticut Siting Council (Council) member Daniel P. Lynch, Jr., Council staff member Stephen M. Howard, and Thomas Krummenacker representing Metro Mobile CTS of Hartford, Inc. (Metro Mobile), met at the site of the proposed cellular telecommunications facility at 886 Main Street, East Hartford, Connecticut.

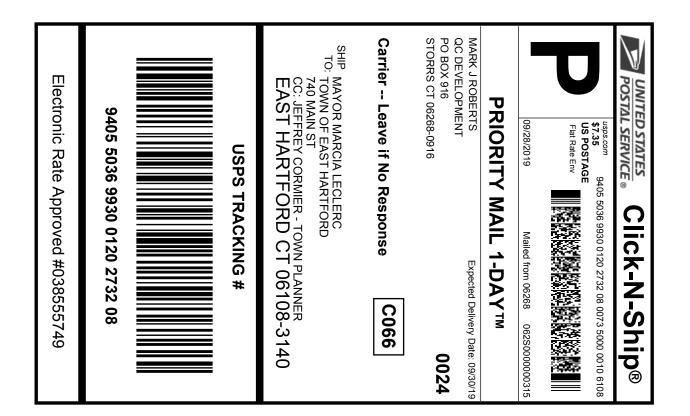
Metro Mobile is proposing to install nine panel antennas, three each at three locations on the building. Each antenna is approximately 35 inches in height, 12 inches wide, and five inches deep. Three of the nine antennas would be attached to the building facade just below the roof line. Three additional antennas would be attached to the facade of the elevator penthouse on the roof of the building, below the penthouse roof line. The remaining three antennas would be mounted on pipes, approximately five feet in length, to be attached to the top of the elevator penthouse. Equipment associated with antennas would be located inside an 18-foot by 25-foot equipment room which would be constructed within a leased area on the ground floor of the building. The antennas would be attached at levels ranging from 99 feet above ground level to approximately 117 feet above ground level. The antennas would not extend beyond the height of the existing chimneys, vents, and television antennas on the penthouse roof. The building is not listed on any historical or architectural register, nor would it require any structural modification to support the proposed installations.

The maximum (i.e., "worst case") radio frequency power density calculations, assuming 19 channels operating simultaneously at 100 watts effective radiated power in an omni directional pattern, at the closest occupied floor of the building which is approximately 15 feet below the lowest antenna mounting point, indicate that the cellular antennas would emit 0.1186 milliwatts per square centimeter or 20.3 percent of the current ANSI standard. This calculation does not take into account the directional nature of the proposed antennas, which would likely result in a lower actual radio frequency power density at this occupied level.

Metro Mobile contends that the proposed construction would not have a substantial adverse environmental effect and therefore would not require a Certificate of Environmental Compatibility and Public Need from the Council.

Stephen M. Howard Siting Analyst

SMH:mmb SP324sr.doc





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Instructions

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USPS TRACKING #: 9405 5036 9930 0120 2732 08

473274652 09/25/2019 Trans. #: Print Date: Ship Date: 09/28/2019 09/30/2019 Delivery Date:

Priority Mail® Postage: Total

From: MARK J ROBERTS

QC DEVELOPMENT

PO BOX 916

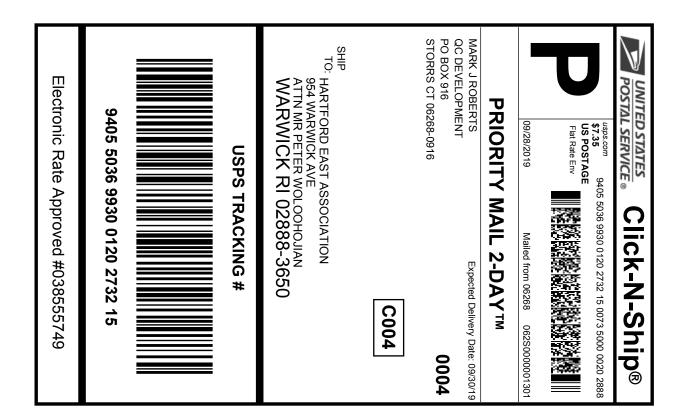
STORRS CT 06268-0916

MAYOR MARCIA LECLERC TOWN OF EAST HARTFORD

740 MAIN ST

CC: JEFFREY CORMIER - TOWN PLANNER EAST HARTFORD CT 06108-3140

* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.





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QC DEVELOPMENT

PO BOX 916

STORRS CT 06268-0916

HARTFORD EAST ASSOCIATION

954 WARWICK AVE

ATTN MR PETER WOLOOHOJIAN

WARWICK RI 02888-3650

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Shipment Confirmation Acceptance Notice

A. Mailer Action

Note To Mailer: The labels and volume associated to this form online, **must** match the labeled packages being presented to the USPS® employee with this form.

Shipment Date: 09/25/19

Shipped From:

MARK J ROBERTS QC DEVELOPMENT PO BOX 916 STORRS CT 06268-0916

Type of Mail	Volume		
Priority Mail®	2		
Priority Mail Express™*	0		
International Mail*	0		
Other	0		
Total Volume	2		

^{*}Start time for products with service guarantees will begin when mail arrives at the local Post Office™ and items receive individual processing and acceptance scans.

B. USPS Action

- USPS EMPLOYEE: Please scan upon pickup or receipt of mail. Leave form with customer or in customer's mail receptacle.
- Employee verifies the package volume count on the Package Pickup Carrier Manifest.
 - If the volume on the manifest matches the volume being collected from the customer, the employee should make the **1:YES** selection by pressing the number 1 on the keypad of the handheld scanner, or on the keyboard of the POS ONE terminal.
 - If the volume on the manifest does not match the volume being collected from the customer, the employee should make the **2:NO** selection. The mail should still be collected and dispatched as normal.

USPS SCAN

9475 7036 9930 0327 6300 12