Turnkey Wireless Development

Northeast Site Solutions<br>Denise Sabo<br>4 Angela's Way, Burlington CT 06013<br>203-435-3640<br>denise@northeastsitesolutions.com

October 7, 2021

\author{

Members of the Siting Council \\ Connecticut Siting Council \\ Ten Franklin Square \\ New Britain, CT 06051 \\ | RE: | Tower Share Application |
| :--- | :--- |
| 1455 Forbes Street, East Hartford CT 06118 |  |
| Latitude: 41.731472 |  |
| Longitude: -72.607778 |  |
|  | Site\# 806376_Crown_Dish |

}

Dear Ms. Bachman:

This letter and attachments are submitted on behalf of Dish Wireless LLC. Dish Wireless LLC plans to install antennas and related equipment to the tower site located at 1455 Forbes Street in East Hartford, Connecticut.

Dish Wireless LLC proposes to install three (3) 600/1900 5G MHz antenna and six (6) RRUs, at the 77-foot level of the existing 130 -foot monopole tower, one (1) Fiber cables will also be installed. Dish Wireless LLC equipment cabinets will be placed within $7 x 5$ lease area. Included are plans by Infinigy, dated August 09,2021 Exhibit C. Also included is a structural analysis prepared by Crown Castle, dated June 15,2021 , confirming that the existing tower is structurally capable of supporting the proposed equipment. Attached as Exhibit D. The facility was approved by the Connecticut Siting Council in Docket No. 139 on September 18, 1991. Please see attached Exhibit A.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies 16-50aa, of Dish Wireless LLC intent to share a telecommunications facility pursuant to R.C.S.A. 16-50j-88. In accordance with R.C.S.A., a copy of this letter is being sent to Mayor Marcia A. Leclerc, Elected Official for the Town of East Hartford, Eileen Buckheit, Development Director, as well as the tower owner (Crown Castle) and property owner (Rebecca Handel-Jack)

The planned modifications of the facility fall squarely within those activities explicitly provided for in R.C.S.A. 16-50j-89.

1. The proposed modification will not result in an increase in the height of the existing structure. The top of the tower is 130 -feet; Dish Wireless LLC proposed antennas will be located at a center line height of 77-feet.
2. The proposed modifications will not result in the increase of the site boundary as depicted on the attached site plan.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed local and state criteria. The incremental effect of the proposed changes will be negligent.

Turnkey Wireless Development
4. The operation of the proposed antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. As indicated in the attached power density calculations, the combined site operations will result in a total power density of $59.24 \%$ as evidenced by Exhibit F.

Connecticut General Statutes 16-50aa indicates that the Council must approve the shared use of a telecommunications facility provided it finds the shared use is technically, legally, environmentally, and economically feasible and meets public safety concerns. As demonstrated in this letter, Dish Wireless LLC respectfully indicates that the shared use of this facility satisfies these criteria.
A. Technical Feasibility. The existing monopole has been deemed structurally capable of supporting Dish Wireless LLC proposed loading. The structural analysis is included as Exhibit D.
B. Legal Feasibility. As referenced above, C.G.S. 16-50aa has been authorized to issue orders approving the shared use of an existing tower such as this support tower in East Hartford. Under the authority granted to the Council, an order of the Council approving the requested shared use would permit Dish Wireless LLC to obtain a building permit for the proposed installation. Further, a Letter of Authorization is included as Exhibit G, authorizing Dish Wireless LLC to file this application for shared use.
C. Environmental Feasibility. The proposed shared use of this facility would have a minimal environmental impact. The installation of Dish Wireless LLC equipment at the 77 -foot level of the existing 130 -foot tower would have an insignificant visual impact on the area around the tower. Dish Wireless LLC ground equipment would be installed within the existing facility compound. Dish Wireless LLC shared use would therefore not cause any significant alteration in the physical or environmental characteristics of the existing site. Additionally, as evidenced by Exhibit F, the proposed antennas would not increase radio frequency emissions to a level at or above the Federal Communications Commission safety standard.
D. Economic Feasibility. Dish Wireless LLC will be entering into an agreement with the owner of this facility to mutually agreeable terms. As previously mentioned, the Letter of Authorization has been provided by the owner to assist Dish Wireless LLC with this tower sharing application.
E. Public Safety Concerns. As discussed above, the tower is structurally capable of supporting Dish Wireless LLC proposed loading. Dish Wireless LLC is not aware of any public safety concerns relative to the proposed sharing of the existing guyed tower. Dish Wireless LLC intentions of providing new and improved wireless service through the shared use of this facility is expected to enhance the safety and welfare of local residents and individuals traveling through East Hartford.

Sincerely,

## Denise Sabo

## Denise Sabo

Mobile: 203-435-3640
Fax: 413-521-0558
Office: 4 Angela’s Way, Burlington CT 06013
Email: denise@northeastsitesolutions.com

# NORTHEEST <br> SITE SOLUTIONS 

Turnkey Wireless Development

Attachments cc:

Marcia A. Leclerc, Mayor
Town of East Hartford
740 Main Street East Hartford, CT 06108 860-291-7200

Eileen Buckheit, Development Director
Town of East Hartford
740 Main Street East Hartford, CT 06108

Rebecca Handel-Jack - Property Owner
1455 Forbes Street East Hartford, CT 06118

Crown Castle, Tower Owner

## Exhibit A

## Original Facility Approval

DOCKET NO. 139 - An application of Metro Mobile CTS of Hartford, Inc., for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of cellular facilities in the Towns of Enfield, East Hartford, and Wethersfield, Connecticut.
Connecticut
Siting
Council

September 18, 1991

## Decision and Order

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a cellular telecommunications towers and equipment buildings at the proposed Enfield, Connecticut, alternate site and the proposed East Hartford, Connecticut, prime site including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildife are not disproportionate either alone or cumulatively with other effects when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application and therefore directs that a Certificate of Environmental Compatibility and Public Need as provided by section $16-50 \mathrm{k}$ of the Connecticut General Statutes (CGS), be issued to Metro Mobile CTS of Hartford, Inc., for the construction, operation, and maintenance of a cellular telecommunications tower, associated equipment, and building at the proposed alternate site in Enfield, Connecticut, and the proposed prime site in East Hartford, Connecticut.

The facilities shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter and subject to the following conditions:

1. The self-supporting monopole towers shall be no taller than necessary to provide the proposed communication service and in no event shall the towers exceed a total height of 163 feet above ground level (AGL) at the proposed Enfield alternate site and 123 feet AGI at the proposed East Hartford prime site, with antennas and appurtenances.
2. The Certificate holder shall prepare a Development and Management (D\&M) Plan, for approval by the Council, for these sites in compliance with sections 16-50j-75 through 16-50j-77 of the Regulations of State Agencies. This D\&M plan

Docket No. 139
Decision and Order
Page 2
shall include detailed plans of the towers, tower foundations, soil boring reports, equipment buildings, access roads, security fences, landscaping plans, detailed erosion and sedimentation control plans, and a final schedule. In addition, the $D \& M$ plan shall include for Council consideration, detailed plans and itemized costs for the placement of service utilities underground in order to further mitigate the visual effect of the facilities.
3. The Certificate holder shall comply with any existing and future radio frequency (RF) standards promulgated by State or federal regulatory agencies. Upon the establishment of any new governmental RF standards, the facilities granted herein shall be brought into compliance with such standards.
4. The Certificate holder shall provide the Council with a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels originally calculated and provided in the application.
5. The Certificate holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
6. If the facility does not initially provide or permanently ceases to provide cellular service following completion of construction, this Decision and Order shall be void, and the tower and all associated equipment shall be dismantled and removed or reapplication for any new use shall be made to the Council as soon as practicable before any such new use is made.
7. Unless otherwise approved by the Council, this Decision and Order shall be void if all construction authorized herein is not completed within three years of the effective date of this Decision and Order or within three years after all appeals to this Decision and Order have been resolved.

Pursuant to CGS section 16-50p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of this issuance shall be published in the Hartford Courant and the Journal Inquirer.

Docket No. 139
Decision and Order Page 3

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with section 16-50j-17 of the Regulations of State Agencies.

The parties to this proceeding are:

PARTIES
Metro Mobile CTS of Hartford, Inc. 20 Alexander Drive P.O. Box 5029 Wallingford, CT 06492 Attn: Gary Schulman

The Town of East Hartford

The Town of Enfield

ITS REPRESENTATIVE
Robinson and Cole One Commercial Plaza Hartford, CT 06103-3597 Attn: Earl Phillips, Jr. (203) 275-8200
G. Barry Goodberg Assistant Corporation Counsel Town of East Hartford 740 Main Street East Hartford, CT 06108 (203) 289-2781

Christopher W. Bromson Enfield Town Attorney 47 No. Main Street Enfield, CT 06082 (203) 745-0371 Ext. 290

SMH: bw
5534 E

## CERTIFICATION

The undersigned members of the Connecticut Siting Council hereby certify that they have heard this case in DOCKET NO. 139 - An application of Metro Mobile CTS of Hartford, Inc., for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of cellular facilities in the Towns of Enfield, East Hartford, and Wethersfield, Connecticut, or read the record thereof, and that we voted as follows:

Dated at New Britain, Connecticut the lith day of September, 1991.

Council Members
Vote Cast
$\qquad$

YES
Mortimer A. Gelston
Chairman


Y

Commissioner Clifton d. Leonhardt Designee:
Commissioner Richard G. Patterson

PETITION NO. 535 - AT\&T Wireless PCS, LLC and Crown
Atlantic Company LLC petition for a declaratory ruling that no Certificate of Environmental Compatibility and Public Need is required for proposed modification of an existing telecommunications tower located at 1455 Forbes Street, Eas Hartford, Connecticut.

Connecticut
Siting
Council
May 21, 2002

## Decision and Order

Pursuant to the foregoing Findings of Fact and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the extension of an existing telecommunications tower and installation of associated equipment at an existing facility located at 1455 Forbes Street in East Hartford, Connecticut, are not significant, are not disproportionate either alone or cumulatively with other effects, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny this petition.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The tower extension shall be compatible with and installed on the existing monopole, no taller than necessary to provide the proposed telecommunications services, sufficient to accommodate the antennas of AT\&T Wireless PCS, LLC (AT\&T) and XM Satellite Radio, but such extension shall not exceed a height of 133 feet above ground level, including antennas and appurtenances.
2. The Certificate Holder shall provide a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels calculated and provided pursuant to this Decision and Order.
3. Upon the establishment of any new State or federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
4. The Certificate Holder shall permit public or private entities to share space on the tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
5. If the facility does not initially provide, or permanently ceases to provide cellular services following completion of construction, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapply for any continued or new use to the Council before any such use is made.
6. Any antenna that becomes obsolete and ceases to function shall be removed within 60 days after such antennas become obsolete and ceases to function.
7. Unless otherwise approved by the Council, this Decision and Order shall be void if the facility authorized herein is not completed within one year of the effective date of this Decision and Order or within one year after all appeals to this Decision and Order have been resolved.
8. All other applicable provisions of the Council's September 18, 1991 Decision and Order in Docket No. 139 remain in effect.

Pursuant to General Statutes § 16-50p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in The Hartford Courant, and The East Hartford Gazette.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

The parties and intervenors to this proceeding are:

Crown Atlantic Company LLC and AT\&T Wireless PCS, LLC

Kenneth C. Baldwin, Esq.
Robinson \& Cole LLP
280 Trumbull Street
Hartford, CT 06103-3597

## Exhibit B

## Property Card

| Town of East Hartford Property Summary Report |  |  |  |
| :---: | :---: | :---: | :---: |
| 1455 FORBES ST |  |  |  |
| MAP LOT: | 41-233 | CAMA PID: | 4723 |
| LOCATION: | 1455 FORBES ST |  |  |
| OWNER NAME: | HANDEL-JACK REBECCA |  |  |

## OWNER OF RECORD

HANDEL-JACK REBECCA

1455 FORBES ST

EAST HARTFORD, CT 06118

| LIVING AREA: | 720 | ZONING: | R2 | ACREAGE: | 25.01 |
| :--- | :--- | :--- | :--- | :--- | :--- |


| SALES HISTORY |  |  |  |
| :--- | :--- | :--- | :--- |
| OWNER | BOOK / PAGE | SALE DATE | SALE PRICE |
| HANDEL-JACK REBECCA | $3909 / 186$ | 07-Jul-2020 | $\$ 0.00$ |
| HANDEL ROBERT D | $3582 / 0113$ | 23-Jan-2016 | $\$ 0.00$ |
| HANDEL JESSIE K EST OF C/O ROBERT D HANDEL EXECUTOR | $3534 / 0329$ | 19-May-2015 | $\$ 0.00$ |
| HANDEL JESSIE K | $1874 / 0345$ | 01-Jan-2000 | $\$ 0.00$ |
| HANDEL ALBERT P JR EST OF HANDEL JESSIE K EXEC | $0000 / 0000$ | 30-Dec-1999 | $\$ 0.00$ |


| CURRENT PARCEL ASSESSMENT |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| TOTAL: | $\$ 332,190.00$ | IMPROVEMENTS: | $\$ 291,500.00$ | LAND: | $\$ 40,690.00$ |


| ASSESSING HISTORY |  |  |  |
| :--- | :--- | :--- | :--- |
| FISCAL YEAR | TOTAL VALUE | IMPROVEMENT VALUE | LAND VALUE |
| 2019 | $\$ 332,880.00$ | $\$ 291,500.00$ | $\$ 41,380.00$ |
| 2018 | $\$ 332,880.00$ | $\$ 291,500.00$ | $\$ 41,380.00$ |
| 2017 | $\$ 332,880.00$ | $\$ 291,500.00$ | $\$ 41,380.00$ |
| 2016 | $\$ 332,880.00$ | $\$ 291,500.00$ | $\$ 41,380.00$ |
| 2015 | $\$ 346,650.00$ | $\$ 302,420.00$ | $\$ 44,230.00$ |


| Town of East Hartford Property Summary Report |  |  |  |
| :---: | :---: | :---: | :---: |
| 1455 FORBES ST |  |  |  |
| MAP LOT: | 41-233 | CAMA PID: | 4723 |
| LOCATION: | 1455 FORBES ST |  |  |
| OWNER NAME: | HANDEL-JACK REBECCA |  |  |

## BUILDING \# 1

| YEAR BUILT | 1865 | EXT WALL 1 | Vinyl Siding |
| :--- | :--- | :--- | :--- |
| STYLE | Colonial | INT WALLS 1 | Plaster |
| MODEL | Residential | HEAT FUEL | Hot Water |
| STORIES | 2.0 | HEAT TYPE | 4 |
| OCCUPANCY | One Family | AC TYPE | 1 |
| ROOF | Gable | BEDROOMS | 1 |
| ROOF COVER | Asphalt | FULL BATHS | 9 |
| FLOOR COVER 1 | Hardwood | HALF BATHS | 60 |
| \% BSMT | 100 | TOTAL ROOMS | 0 |
| \% FIN BSMT | 0 | \% REC RM | 0 |
| \% SEMI FIN | 0 | FIREPLACES |  |
| BSMT GARAGE |  |  |  |


| EXTRA FEATURES |  |  |
| :--- | :--- | :--- |
| DESCRIPTION | CODE | UNITS |
| 1 Story Barn | BRN1 | $1 \times 5112(5112.00 \mathrm{SF})$ |
| Shed | SHD1 | $1 \times 64(64.00 \mathrm{S.F})$. |
| 1 Story Barn | BRN1 | $1 \times 3072(3072.00 \mathrm{SF})$ |
| Shed | SHD1 | $1 \times 300(300.00$ S.F. $)$ |
| Shed | SHD1 | $1 \times 561(561.00$ S.F. $)$ |
| 1 Story Barn | BRN1 | $1 \times 4928(4928.00$ SF) |
| Shed | SHD1 | $1 \times 600(600.00$ S.F. $)$ |


| Town of East Hartford Property Summary Report |  |  |  |
| :---: | :---: | :---: | :---: |
| 1455 FORBES ST |  |  |  |
| MAP LOT: | 41-233 | CAMA PID: | 4723 |
| LOCATION: | 1455 FORBES ST |  |  |
| OWNER NAME: | HANDEL-JACK REBECCA |  |  |

## BUILDING \# 2

| YEAR BUILT | 1934 | EXT WALL 1 | Vinyl Siding |
| :--- | :--- | :--- | :--- |
| STYLE | Single Family | INT WALLS 1 | Plaster |
| MODEL | Residential | HEAT FUEL | Other |
| STORIES | 1.0 | HEAT TYPE | None |
| OCCUPANCY | One Family | AC TYPE | 1 |
| ROOF | Gable | BEDROOMS | 1 |
| ROOF COVER | Asphalt | FULL BATHS | 0 |
| FLOOR COVER 1 | Hardwood | HALF BATHS | 4 |
| \% BSMT | 0 | TOTAL ROOMS | 0 |
| \% FIN BSMT | 0 | \% REC RM | 0 |
| \% SEMI FIN | 0 | \% ATTIC FINISH |  |
| BSMT GARAGE |  | FIREPLACES | 0 |


| EXTRA FEATURES |  |  |
| :--- | :--- | :--- |
| DESCRIPTION | CODE | UNITS |
| Shed | SHD1 | $1 \times 105$ (105.00 S.F.) |
| FR/SHED | MSC55 | 30.00 UNIT |
| 1 Story Barn | BRN1 | $1 \times 840$ (840.00 SF) |
| Shed | SHD1 | $1 \times 144(144.00$ S.F. $)$ |
| Shed | SHD1 | $1 \times 308(308.00$ S.F. $)$ |
| 1 Story Barn | BRN1 | $1 \times 3840(3840.00$ SF) |



## Exhibit C

## Construction Drawings

## dEsh wireless.

## DISH Wireless L.L.C. SITE ID:

 BOBDL00047ADISH Wireless L.L.C. SITE ADDRESS:
1455 FORBES STREET EAST HARTFORD, CT 06118

| CTICUT CODE COMPLIANCE |
| :---: |
|  cof mes |
|  |  |



| SHEET INDEX |  |
| :---: | :---: |
| SHEET No. | Sheet title |
| T-1 | TMLE SHEET |
| A-1 | OVERAL AND ENIARGED STE PLAN |
| A-2 | ELEVATON, ANIENNA LYOOUT AND SCHEDLULE |
| A-3 | EQUIPMENT PLATORM AND H-FrRME DEAALS |
| A-4 | EQUIPMENT DEAALS |
| A-5 | Equipment deatls |
| A-6 | EQUIPMENT DEAALS |
| E-1 | Electrical/mer route Plan ano notes |
| E-2 | Electrical dealls |
| E-3 | ELECTRICAL ONE-LNE, FAULT CALCS \& PNEL SCHEDULE |
| 6-1 | GROUNOING PLANS AND NOTES |
| 6-2 | grounoing dealls |
| 6-3 | Grounding detals |
| RF-1 | RF CABE COLOR COOE |
| CN-1 | Legeno and abrrematons |
| CN-2 | GENERLL Notes |
| CN-3 | GENERLL Notes |
| 6N-4 | GENERLL NOTES |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |






$\square$ SITE PHOTO


GENERAL NOTES

11"x17" PLOT WILL BE HALF SCALE UNLESS OTHERWISE NOTED



DIRECTIONS


## dish


CROWN CASTLE zam corborantrinty INFINIGY8 from zero to infinig



|  |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| DRAWN BY: |  |  |  |
|  | RCD | ss | cJw |
| RFDS REv \#: N/A |  |  |  |
| CONSTRUCTION DOCUMENTS |  |  |  |
|  |  |  |  |
| SUBMITALS |  |  |  |
| $\stackrel{1}{0}$ | 00817/2021 | LSSUED For Renew |  |
|  | 08/08/2022 | Lssube for constuectow |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
| A\&E PROJECT NUMBER |  |  |  |
| 2039-Z5555C |  |  |  |
|  |  |  |  |
| BobdL00047A <br> 1455 FORBES STREET <br> EAST HARTFORD, CT 06118 |  |  |  |
| SHEET TTLE |  |  |  |
| title sheet |  |  |  |
| SHEET NUMBER |  |  |  |
| T-1 |  |  |  |














## 



4. Do not instal cable grounong kit at a beno avo alwars direct ground conouctor

6. AlL Grounolng parts and equipment to be suppled and installed er contracter
7. THE CONTRACTOR SHALL BE RESPONSIILE FOR INSTALING ADOTIONLL GROUNO BAR AS
8. EnSure the wre insuaton terminaton is witin $1 / 8^{\circ}$ of the barrel (no shiners).





CROWN CASTLE

INFINIGY8
from zero to infinigy


| TYPICAL GROUNDING NOTES | No Scale | 1 | TYPICAL EXTERIOR TWO HOLE LUG | No SCME | 2 | TYPICAL INTERIOR TWO HOLE LUG | No SCALE | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| LUG DETAIL | No SCALE | 4 | NOT USED | No scale | 5 | NOT USED | No SCALE | 6 |
|  |  |  |  |  |  |  |  |  |
| NOT USED | No SCALE | 7 | NOT USED | No SCALE | 8 | NOT USED | No SCALE | 9 |



[^0]


SITE ACTVITY REQUIREMENTS:

1. NOTTCE TO PROCEED - NO WORK SHALL COMMENEE PRIOR TO CONTRACTOR RECEINING A WRITEN NOTICE TO PROCEED (NTP) AND THE ISSUANCE OF A PURCHASE ORDER. PRIOR TO ACCESSING/ENTERING THE STIE YOU MUST C
L.L.C. AND TOWER OWNER NOC \& THE DISH Wireless LL.C. AND TOWER OWNER CONSTRUCTION MANAGER.
2. "LOOK UP" - DISH Wireless LLL.C. AND TOWER OWNER SAFETY CLIMB REQUIREMENT:

THE INTEGRIT OF THE SAFETY CLIMB AND ALL COMPONENTS OF THE CLIMBING FACLITY SHALL BE CONSIDERED DURING ALL STAGES
OF DESIGN, INSTALLTION, AND INSPECTION. TOWER MODFICATON, MOUNT REINFORCEMENTS, AND/OR EQUPMENT INSTALATIONS SHALL OF DESIGN, NSTALATIN, AND INSPECTION. TOWER MODIFCATON, MOUNT REINFORCEMENTS, AND/OR EQUIPMENT INSTALAATONS SHAL
NOT COMPROMISE THE INTEGRIT OR FUNCTONAL USE OF THE SAFETY CLIMB OR ANY COMPONENTS OF THE CIMBING FACIITTY ON
 ANCHORAGE POINTS IN ANY WAY, OR TO IMPEDE/BLOCK ITS INTENDED USE. ANY COMPROMISED SAFET CLIMB, INCLUDING EXISTING
CONOITIONS MUST BE TAGGED OUT AND REPORTED TO YOUR DISH Wiress LLC. AND DISH Wireless LL.C. AND TOWER OWNER POC P CALL THE NOC TO GENERATE A SAFETY CLIMB MAINTENANCE AND CONTRACTOR NOTICE TICKET.


4. AL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMTED TO, ERECTION PLANS, RIGGING PLANS, CLIMBBING
PLANS, AND RESCUE PLANS SHALL BE THE RESPONSBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF
 PLANS SHALL ADHERE TO ANSI/ASSE A1O.48 (LLTTEST EDITION) AND DISH Wireless LLL.C. AND TOWER OWNER STANDARDS. INCLUDING
THE REQURED INVOLVEMENT OF A QUALIIED ENGINER FOR CLASS IV CONSTRUCTON, TO CERTIFY THE SUPPORTING STRUCTURE(S) IN THE REQUIRED INVOLVEMENT OF A QUALIFIED ENGINE
ACCORDANCE WTH ANSITTA-322 (LATEST EDTION).
5. ALL SITE WORK TO COMPLY WTH DISH Wireless LL..C. AND TOWER OWNER INSTALATION STANDARDS FOR CONSTRUCTION
ACTVMTIEL ON DISH Wireless L.L.C. AND TOWER OWNER TOWER SITE AND LATEST VERSSION OF ANSI/TAA-1019-A-2012 "STANDARD FOR

 AN ALTERNATIE INSTALLA
CHANGE OF INSTALATION.
ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLCABLE CODES, REGLATIONS
AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WTTH ALL LAWS, ORDINANCES, RULESS AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WTH ALL LAWS, ORDINANCES, RULES,
REGLLTONS ATS
RET

8. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS
UNLESS
SPECIFICALYY STATED OTHERWISE.
9. THE CONTRACTOR SHALL CONTACT UTLITY LOCATNG SERVICES INCLUDING PRVATE LOCATES SERVICES PRIOR TO THE START
OF CONSTRUCTION.


 FALL PROTECTIO
PROCEDURES.
11 ALL SITE WORK SHALL BE AS INDICATED ON THE STAMPED CONSTRUCTION DRAWINGS AND DISH PROJECT SPECIFICATIONS,
LATEST APPROVED REVIIION.
12. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULTING WASTE MATERIAL, DEBRIS, AND TRASH AT THE COMPLETION OF
THE WORK. IF NECESARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND THE WORK. IF NECESSAAK
DISPOSED OF LEEALY.
13. ALL Existing inactive sewer, water, gas, electric and other utilties, which interfere with the execution of the WORK, SHAL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WLL NOT INTERFERE WTH
THE EXECUTON OF THE WORK, SUBJECT TO THE APPROVAL OF DISH Wireless L.L.C. AND TOWER OWNER, AND/OR LOCAL UTLITES.
14. THE CONTRACTOR SHALL PROVIDE STE SIENAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIISNAGE
REQUIRED BY LOCAL JURISDCTION AND SIGNAGE REQUIRED ON INDAVIDAL PIECES OF EQUPMENT, ROOMS, AND SHELERS.
15. THE STtE SHALL be graded to Cause surface water to flow away from the carrier's equipment and tower areas.
16. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE
APPLCATON.
17. THE AREAS OF THE OWNERS PROPERT DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUPMENT OR
DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILZED TO PREVENT EROSION AS SPECIFED ON THE CONSTRUCTION DRAWINGS AND/OR PROUECT SPECIFICATIONS
18. CONRACTOR SHAL MINIMIZ DISTURBANCE TT EXIISTING STE DURING CONSTTUCTION. EROSION CONTROL MEASURES, IF
REQURED DURING CONSTRUCTNO, SHALL BE IN CONFORMANCE WITH THE LOCAL GUDELINES FOR EROSION AND SEDMENS CONTRLL
19. THE CONTRACTOR SHALL PROTECT EXISTTNG IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY
20. CONTRACTOR SHELL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER TTEMS 20. CONTRACTOR SHALL LEGALY AND PROPERLY DISPPSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER
REMOVED FROM THE EXISTING FACLILTY. ANTENNAS AND RADIOS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED
LOCATON.
21. CONTRACTOR SHALL LeAvE PREMISES IN CLEAN CONDITION. TRASH AND DEBRIS SHOULD be removed from site on a dally
basis
22. NO FILL OR EMBANKMEN MATERILL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERILLS, SNOW OR ICE SHALL NOT
BE PLACED IN ANY FILL OR EMBANKMENT.

## general notes

1.FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINTIONS SHALL APPLY: CONTRACTOR:GENERAL CONTRACTOR RESPONSIBLE FOR CONSTRUCTION
CARRIER:DISH Wireless L.L.C.
TOWER OWNER:TOWER OWNER
2. THESE DRAWINGS HAVE BEEN PREPARED USING STANDARDS OF PROFESSIONAL CARE AND COMPLETENESS NORMALY
EXERCISED UNDER SIMILAR CIRCUMSTANCES BY REPUTABLE ENGINERS IN THIS OR SIMIAR LOCALTIES. IT IS ASSUMED THAT THE WORK DEPPCTED WLL BE PERFORMED BY AN EXPERENEED CONTRACTOR AND/OR WORKPEOPLE WHO HAVE A WORKING KNOWLEDGE OF THE APPLCALEMENT IS (OR CAN BE) EXPLICITLY SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL USE INDUSTRY ACCEPTE CONDTION OR ELEMENT II (OR CAN BE EXPLCITLY SHOON ON THESE DRAWIN.
STANDRDD GOOD PRACTICE FOR MISELLAEOUS WORK NOT EXPLICTLY SHOWN.
3. THESE DRAWINGS REPRESENT THE FINSHED STRUCTURE. THEY DO NOT INDICATE THE MEANS OR MEEHODS OF

SEQUENCES, AND PROCEDURES. THE CONTRACTOR SHALL PROVIDE ALL MEASURES NECESSARY FOR PROTECTION OF LIFE AND
 SITE VISTTS BY THE ENGINEER OR HIS REPRESENT
OBSERVATON OF THE FINIHED STRUCTURE ONLY.
 THE CONTRACT DOCUMENTS. WHERE DISCREPANCIES OCCUR BETWEEN PLANS, DETALLS, GENERAL NOTES AN AND SPECIICATIONS,
GGEAER, MORE STRICT REQUREMENTS, SHALL GOVERN. IF FURTHER CLARIFCATION IS REQURED CONACT THE ENGINEER OF GRECTER,
SUBSTANTAL EFFORT HAS BEEN MADE TO PROVIDE ACCURATE DIMENSIONS AND MEASUREMENTS ON THE DRAWINGS TO ASSIST
IN THE FABRICATION AND/OR PLACEMENT OF CONSTRUCTION ELEMENTS BUT IT IS THE SELE RESPONSIBILTT OF THE CONTRACTOR TO

 Possibe.

ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGLATIONS
AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WTH ALL LAWS, ORDINANGES, RUUES ANDGULTIONS AND LAWFUL ORDERS OF ANY PUBLLC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED
 8. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MAI
NECESSARY TO COMPLLTE ALL INSTALATIONS AS INDICATED ON THE DRAWINGS.
9. THL CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATION
10. IF THE SPECIFED EQUIPMENT CAN NOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATVE
OF INSTALATION.
Contractor Is to perform a site ivestigation, before submiting bids, to determine the best routing of all
conduts for power, and teco and for grounding cables as show in the power, telco, and grouning plan
DRAWINGS.
12. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY
13. CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEM $14 . \operatorname{contractor~shall~leave~premises~in~clean~condition.~trash~and~debris~should~be~removed~from~site~on~a~dally~}$

5701 SOUTH SANTA FE DRVE
LTILTON, $C$ CO 80120 CASTLE

## CONCRETE FOUNDATIONS. AND REINFORCING STEEL

1. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WTTH THE ACI 301, ACI 318, ACI 336, ASTM A184, ASTM A185 AND THE DESIGN
AND CONSTRUCTON SPECIFCATION FOR CAST-IN-PLACE CONCRETE.
2. UNLESS NOTED OTHERWISE, SOIL BEARING PRESSURE USED FOR DESIGN OF SLABS AND FOUNDATIONS IS ASSUMED TO be 1000
psf.
3. ALL CONCRETE SHALL HAVE A MINMUM COMPRESSIVE STRENGTH (f'c) OF 3000 psi AT 28 DAYS, UNLESS NOTED OTHERWISE. NO
MORE THAN 90 MINUTES SHALL ELAPSE FROM BATCH TIME TO TIME OF PLACEMENT UNLESS APPROVED BY THE ENGINEER OF RECORD. MORE THAN 90 MINUTES SHAL ELAPSE FROM BATCH TIME TO TIME OF PLACE
TEMPERATURE OF CONCREEE SHALL NOT EXCEED $90^{\circ}$ AT TIME OF PLACEMENT.
CONCRETE EXPOSED TO FREEZE-THAW CYCLLES SHALL CONTAIN AIR ENTRANNG ADMIXTURES. AMOUNT OF AR ENTRANMENT TO BE
ASES MAXIMUM WATER-TO-CEMENT RATIO (W/C) OF 0.45.
4. all steel reinforcing shall conform to astm a615. all welded wire fabric (wwf) shall conform to astm a185. all SPLICES SHALL BE CLASS "B" TENSION SPLICES, UNLESS NOTED OTHERWISE. ALL HOOKS SHALL BE STANDARD 90 DEGREE HOOKS, SPLILES SHALL BE CLASS "B" TENSION SSLICES, UNLESS NOTTED OTHERWISE. ALL HOOKS SHALL BE
ULEES NOTED OTHERWISE. YELD STRENTH (Fy) OF STANDARD DEFRMMED AARS ARE AS FOLLOW:
\#4 BARS AND SMALLER 40 ks
\#5 BARS AND LARGER 60 ks
${ }^{6}{ }_{\text {DRAWINGS: }}^{\text {THE }}$
FOLLOWING MINMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON
CONCRETE CAST AGAINST AND PERMANENTLY EXPOSED TO EARTH $3^{\prime \prime}$

- CONCRETE EXPOSED TO EARTH OR WEATHER:
\# ${ }^{\circ}$ bars and larger $2^{n}$
\#5 bars and smaller 1-1/2"
- CONCRETE NOT EXPOSED TO EARTH OR WEATHER:
- slab and walls $3 / 4^{\circ}$
beams and columns $1-1 / 2^{\prime \prime}$

7. A tooled edee or a $3 / 4^{* *}$ chamfer shall be provided at all exposed edges of concrete, unless noted otherwise

## Electrical instalation notes:

1. ALLL ELLCCTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WTH THE PROJECT SPECIFICATIONS, NEC AND ALL APPLCABLE
2. CONDUIT ROUTINGS ARE SCHEMATC. CONTRACTOR SHALL INSTALL CONDUTS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED
3. WIRING, RACEWAY AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WTH THE REQUIREMENTS OF THE NEC.
4. all circuits shall be segregated and maintain minimum cable separation as required by the nec.
4.1. ALL EQUIPMEN SHALL BEAR THE UNDERWRTIERS LABORATORIES LABEL OF APPROVAL, AND SHALL CONFORM TO REQUIREMENT OF
THE NATIONAL ELECTRICAL CODE.
 CURRENT TO WHCH THEY ARE SUBJECTED, 22,000 AIC MNIMUM. VERIFY AVALLABLE SHORT CIRCUIT CURRENT DOES NOT EXCEED TH
RATING OF ELECTRICAL EQUIPMENT IN ACCORDANCE WTH ARTILE 110.24 NEC OR THE MOST CURRENT ADOPTED CODE PRE THE GOVERNING JURISOCTION.
5. EACH END OF EVERY POWER PHASE CONDCTTOR, GROUNDING CONDUCTOR, AND TELCO CONDUCTOR OR CABLE SHALL BE LABELED WTH COLOR-CODED INSULATION OR ELECTRICAL TAPE ( $3 M$ BRAND,
EQUAL). THE IDENTFICATION METHOD SHALL CONFORM WITH NEC AND OSHA.
6. ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABELED WITH LAMCOID TAGS SHOWING THEIR RATED VOLTAGE, PHASE
CONFIGURATIN, WIRE CONFIGURATION, POWER OR AMPACITY RATING AND BRANCH CIRCUIT ID NUMBERS (i.e. PANEL BOARD AND CIRCUIT config
iD's).
7. PANEL boards (ID NUMBERS) SHALL be CLEARLY LABELED with pLASTIC LABELS
8. TIE WRAPS ARE NOT ALLOWED.
9. ALL POWER AND EQUIPMENT GROUND WIRING IN TUBBG OR CONDUIT SHALL BE SINGLE COPPER CONDCTOR (\#14 OR LARGER)
WTTH TTPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATIN UNLESS OTHERWISE SPECFIED. SUPPLEMENTAL EQUIPMENT GROUND WRING LOCATED INDOORS SHALL BE SINGLE COPPER CONDUCTOR (\#6 OR LARGER) WTTH
TVPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATON UNLESS OTHERWISE EPECIFED. POWER AND CONTROL WIRING IN FLEXIBLE CORD SHALL BE MULT-CONDUCTOR, TTPE SOOW CORD (\#14 OR LARGER) UNLESS
OTHERWISE SPECIFIED.
POWER AND CONTROL WIRING FOR USE IN CABLE TRAY SHALL BE MULTI-CONDUCTOR, TTPE TC CABLE (\#14 OR LARGER), WITH
TTPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, 0 RHW-2 INSULATON UNLESS OTHERWISE SPECIFED. TVPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATION UNLESS OTHERWISE (\#PECIFED. 13. AL POWER AND GROUNDING CONNECTIONS SHALL BE CRIMP-STLLE, COMPRESSION WIRE LUGS AND WIRE NUTS BY THOMAS AND
BETS (OR EOUAL). LUGS AND WIRE NUTS SHALL BE RATED FOR PPERATLON NOT ESSS THAN $75^{\circ} \mathrm{C}$ ( $90^{\circ} \mathrm{C}$ IF AVAIIABLE).
10. RACEWAY and cable tray shall be listed or labeled for electrical use in accordance with nema, ul, ansi/IEEE and 15. ELLCTRICAL METALILC TUBING (EMT), INTERMEDIATE METAL CONDUIT (IMC), OR RIGID METAL CONDUT (RMC) SHALL BE USED FOR
EXPOSED INDOOR LCCATIONS.
11. SCHEDULE 40 PVC UNDERGROUND ON STRAGHTS AND SCHEDULE 80 PVC FOR ALL ELBows/90s AND ALL APPROVED ABOVE
GRADE PVC CONDUIT.
12. LIQUID-TIGHT FLEEXBLE MEEALLIC CONDUT (LLQUID-TTIE FLEX) SHALL BE USED INDOORS AND OUTDOORS, WHERE VIBRATION
OCCURS OR FLEXBILITTIS NEEDED. 19. CONDUUT AND tubing fitings shall be threaded or compression-țpe and approved for the location used. set 20. Cabinets, boxes and wire wars shall be labeled for electrical use in accordance with nema, ul, ansi/ieee and the 21. WIREWAYS SHALL BE METAL WITH AN ENAMEL FINISH AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARD (WIREMOLD SPECMATE WIREWAY).
13. SLOTED Wiring duct shall be pvc and include cover (panduit tppe e or equal).
14. CONDUTS SHALL BE FASTENED SECURELY IN PLACE WTH APPROVED NON-PERFORATED STRAPS AND HANGERS. EXPLOSNE
DEVCCS (i.e. POWDER-ACTUATED) FOR ATTACHING HANGERS TO STRUCTURE WIL NOT BE PERMITED. CLOSELY FOLLOW THE LINES

DEVICES (i.e. POWDER-ACTUATED) FOR ATACHING HANGERS TO STRUCTURE WLL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF

 OBSTRUCTIONS. ENDS OF CONDUTS SHALL BE TEMPO
FROM ENERNG CONDUTTS SHAL BE RIIILY CAMME
MALEEABLE IRON LOCKNUT ON OUTSIDE ANO INSIE.
24. EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES AND PUL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET STEEL. SHALL MEET OR EXCEED UL 50 AND BE RATED NEMA 1 (OR BETIER) FOR INTERIOR LOCATIONS AND NEMA 3 (OR BETIER) FOR toations.
25. METAL RECEPTACLE, SWITCH AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED OR NON-CORRODING; SHALL MEET OR
EXCEED 514 AND NEMA OS 1 AND BE RATED NEMA 1 (OR BETER) FOR INTEROR LOCATIONS AND WEATHER PROTECTED (WP OR EXCEED UL 514 A AND NEMA OS
BETER) FOR EXTERIOR LOCATIONS.
26. NONMETALLIC RECEPTACLE, SWITCH AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2 (NEWEST REVISION) AND BE RATED NEMA 1 (OR BETER) FOR INTERIOR LOCATIONS AND WEATHER PROTECTED (WP OR BETIER) FOR EXTERIOR LOCATIONS.
27. THE CONTRACTOR SHALL NOTIFY AND OBTAIN NECESSARY AUTHORIZATION FROM THE CARRIER AND/OR DISH Wireless L.L.C. AND
TOWER OWNER BEFORE COMMENCING WORK ON THE AC POWER DISTRIBUTIN PANEIS
28. THE CONTRACTOR SHALL PROVDE NECESSARY TAGGING ON THE BREAKERS, CABLES AND DISTRBUTION PANELS IN ACCORDANCE
WTTH THE APPLCABLL CODES AND STANDARDS TO SAFEGUARD LIFE AND PROPERTY.
29. Install lamicoid label on the meter center to show "dish wireless l.l.c."
30. all emptr/SPare conduits that are installed are to have a metrred mule tape pull cord installed.




CONSTRUCTION

| SUBmitals |  |  |
| :---: | :---: | :---: |
| REv | DATE | DESCRIPTION |
|  | 00/17/2021 | ISSUE Por Remew |
| $\bigcirc$ | 08/80/2021 | SSUL Pror comsmuctow |
|  |  |  |
|  |  |  |
|  |  |  |

2039-75555

BobdLoo047A
1455 FORBES STREET
EAST HARTFORD, CT 06118
SHEET TTLE
GENERAL NOTES
SHEET NUMER

## GROUNDING NOTES:

1. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNNNG PROTECTION AND AC POWER GES'S) SHALL
BE BONDED TOGETHER AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WTTH THE NEC.
2. THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POtENTAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR

GROUND ELECTRODE SYSTEMS, THE CONTRACTOR SH-OF-PURNISH AND INSTALL SUPPIEMENTAL GPOUD EIECTRODES AS NEEDED TO
a hive a test result of 5 OHMS OR LESS.
3. THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUTI INSTALATION AS
PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT AND PROVIDE TESTING RESULTS.
4. METAL CONDUIT AND TRAY SHAL BE GROUNDED AND MADE ELECTRICALY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY
BONDING ACROSS THE DISCONTINUITY WTH \# $\# 6$ COPPER WIRE UL APPROVED GROUNDING TTPE CONDUIT CLAMPS.
5. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS
WTH GREEN NSULTION, SIZED IN ACCORDANCE WTTH THE NEC, SHALL BE FURNISHED AND INSTALED WTH THE POWER CIRCUTTS TO BTS
EQUPMENT
6. EACH CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL
EQUIPMENT GROUND WIRES, \#6 STRANDED COPPER OR LARGER FOR INDOOR BTS; \#2 BARE SOLD TNNED COPPER FOR OUTDOOR BTS.
7. CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED BACK TO BACK CONNECTIONS ON OPPOSITE SIDE
OF THE GROUND BUS ARE PERMITED.

OF THE GROUND BUS ARE PERMITIED.
8. ALL EXTERIOR Ground conductors between equipment/ground bars and the ground ring shall be \#2 sold tinned
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS,
10. USE OF $90^{\circ}$ bends in the protection grounding conductors shall be avoided when $45^{\circ}$ bends can be adequately
Supported.
11. EXOTHERMIC WELDS SHALL be uSEd for all grounding connections below grade.
12. ALL GROUND CONNECTIONS ABOVE GRADE (INTERIOR AND EXTERIOR) SHALL BE FORMED USING HIGH PRESS CRIMPS.
13. COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC WELD CONNECTIONS.
14. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND
15. APPRROVED ANTIOXIDANT COATINGS (i.e. CONDUCTVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
16. ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERILL
17. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND
18. BOND ALL METALLIC OBJECTS WTHIN 6 ft OF MAIN GROUND RING WITH (1) \#2 BARE SOLD TINNED COPPER GROUND
19. GROUND CONDUCTORS USED FOR THE FACIITY GROUNIING AND LGGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED
 SLEEVES THROUGH WALLS OR FLLORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUREMENTS OR LOCAL
CONDTIONS, NON-METALIC MATERAL SUCH AS PVC CONOUT SHALL BE USED. WHERE USE OF MEAL CONDUTT IS UNAVOIDABLE (ie., NONMETALLC CONDUIT PROHBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT.
20. ALL GROUNDS THAT TRANSITION FROM BELOW GRADE TO ABOVE GRADE MUST BE \#2 BARE SOLD TINNED COPPER IN $3 / 4^{\prime \prime}$ NON-METALLIC, FLEXIBLE CONDUIT FROM $24^{4 "}$ BELOW GRADE TO WITHIN $3^{\prime \prime}$ TO $6^{\prime \prime}$ OF CAD-WELD TERMINATIN POINT.
OF THE CONDUIT MUST BE SEALED WITH SILCONE CAULK. (ADD TRANSTIONING GROUND STANDARD DETAIL AS WELI).

 THE EXISTING GROUNDING SYSTEM, THE BULLING STEEL COLUMNS, LIGHTNING PROTECTON SYSTEM, AND BULLDING MAIN WATER LIN (FERROUS OR NONFERROUS METAL PIPING ONLY). DO NOT ATTACH GROUNDING TO FIRE SPRINLLER SYSTEM PIPES.

## Exhibit D

## Structural Analysis Report

Crown Castle
2000 Corporate Drive
Canonsburg, PA 15317
(724) 416-2000

## Subject:

Carrier Designation:

Crown Castle Designation:

Engineering Firm Designation:
Site Data:

Structural Analysis Report
DISH Network Co-Locate
Site Number: BOBDL00047A
Site Name:
BU Number: 806376
Site Name: HRT 100943239
JDE Job Number: 650042
Work Order Number: 1963271

Order Number: 556638 Rev. 1
Crown Castle Project Number: 1963271
1455 FORBES STREET, EAST HARTFORD, HARTFORD County, CT
Latitude $41^{\circ} 43^{\prime} 53.3^{\prime \prime}$, Longitude -72 ${ }^{\circ} 36^{\prime} 28^{\prime \prime}$
130 Foot - Monopole Tower

Crown Castle is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above-mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

## LC7: Proposed Equipment Configuration

Sufficient Capacity - 88.5\%
This analysis utilizes an ultimate 3 -second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - "Analysis Criteria".

Structural analysis prepared by: Daniel Chen
Respectfully submitted by:

Jamal A. Huwel, P.E. Director Engineering


## TABLE OF CONTENTS

## 1) INTRODUCTION

## 2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration
Table 2 - Other Considered Equipment

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided
3.1) Analysis Method
3.2) Assumptions

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)
Table 5 - Tower Component Stresses vs. Capacity - LC7
4.1) Recommendations

## 5) APPENDIX A

tnxTower Output
6) APPENDIX B

Base Level Drawing
7) APPENDIX C

Additional Calculations

## 1) INTRODUCTION

This tower is a 130 ft Monopole tower designed by Valmont.
The tower has been modified multiple times to accommodate additional loading.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Seismic Ss:
Seismic S1:
Service Wind Speed:

TIA-222-H
II
125 mph
C
1
2 in
50 mph
0.18
0.064

60 mph

Table 1 - Proposed Equipment Configuration

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\|\begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}\right\|$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 77.0 | 77.0 | 3 | fujitsu | TA08025-B604 | 1 | 1-3/8 |
|  |  | 3 | fujitsu | TA08025-B605 |  |  |
|  |  | 3 | jma wireless | MX08FRO665-21 w/ Mount Pipe |  |  |
|  |  | 1 | raycap | RDIDC-9181-PF-48 |  |  |
|  |  | 1 | tower mounts | Commscope MC-PK8-DSH |  |  |

Table 2-Other Considered Equipment

| Mounting <br> Level (ft) | Center Line Elevation (ft) | $\left\|\begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}\right\|$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 121.0 | 121.0 | 1 | tower mounts | Platform Mount [LP 602-1] | $\begin{aligned} & 2 \\ & 8 \\ & 6 \end{aligned}$ | $\begin{gathered} 3 / 8 \\ 3 / 4 \\ 1-1 / 4 \end{gathered}$ |
|  |  | 1 | tower mounts | Side Arm Mount [SO 102-3] |  |  |
|  | 120.0 | 3 | ericsson | RRUS 32 B30 |  |  |
|  |  | 3 | ericsson | RRUS 4449 B5/B12 |  |  |
|  |  | 3 | ericsson | RRUS 4478 B14 |  |  |
|  |  | 3 | ericsson | RRUS 8843 B2/B66A |  |  |
|  |  | 3 | ericsson | RRUS E2 B29 |  |  |
|  |  | 3 | kathrein | 80010121 w/ Mount Pipe |  |  |
|  |  | 3 | kathrein | 80010798 w/ Mount Pipe |  |  |
|  |  | 6 | kathrein | 80010965 w/ Mount Pipe |  |  |
|  |  | 6 | powerwave technologies | LGP21401 |  |  |
|  |  | 4 | raycap | DC6-48-60-18-8F |  |  |
| 109.0 | 113.0 | 3 | samsung telecommunications | MT6407-77A w/ Mount Pipe | 2 | 7/8 |
|  | 111.0 | 6 | andrew | SBNHH-1D65B w/ Mount Pipe |  |  |
|  |  | 3 | antel | BXA-80063/4CF w/ Mount Pipe |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 109.0 | 1 | raycap | RUSDC-6267-PF-48 |  |  |
|  |  | 3 | samsung telecommunications | CBRS w/ Mount Pipe |  |  |
|  |  | 3 | samsung telecommunications | RFV01U-D1A |  |  |
|  |  | 3 | samsung telecommunications | RFV01U-D2A |  |  |
|  |  | 1 | tower mounts | Site Pro 1 F3P-12[W] |  |  |
|  |  | 1 | tower mounts | Site Pro 1 F3P-HRK12 |  |  |
| 99.0 | 99.0 | 3 | alcatel lucent | 800MHz 2X50W RRH W/FILTER | - | - |
|  |  | 3 | alcatel lucent | PCS 1900MHz 4x45W-65MHz w/ Mount Pipe |  |  |
|  |  | 1 | tower mounts | Side Arm Mount [SO 101-3] |  |  |
| 97.0 | 103.0 | 1 | andrew | VHLP2-18 | $\begin{aligned} & 4 \\ & 3 \\ & 3 \end{aligned}$ | $\begin{gathered} 1-1 / 4 \\ 5 / 16 \\ 1 / 2 \end{gathered}$ |
|  |  | 1 | andrew | VHLP2.5-18 |  |  |
|  | 98.0 | 3 | argus technologies | LLPX310R-V1 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVSPP18-C-A20 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVTM14-ALU-I20 w/ Mount Pipe |  |  |
|  | 97.0 | 3 | alcatel lucent | TD-RRH8X20-25 |  |  |
|  |  | 2 | dragonwave | HORIZON COMPACT |  |  |
|  |  | 1 | motorola | TIMING 2000 |  |  |
|  |  | 3 | samsung telecommunications | RRH-2WB |  |  |
|  |  | 1 | tower mounts | Platform Mount [LP 713-1] |  |  |
| 87.0 | 87.0 | 3 | ericsson | AIR -32 B2A/B66AA w/ Mount Pipe | $\begin{gathered} 11 \\ 1 \\ 1 \\ 1 \end{gathered}$ | $\begin{gathered} 1-1 / 4 \\ 1-5 / 8 \\ 7 / 8 \\ 1-3 / 8 \end{gathered}$ |
|  |  | 3 | ericsson | ERICSSON AIR 21 B2A B4P w/ Mount Pipe |  |  |
|  |  | 3 | ericsson | KRY 112 144/1 |  |  |
|  |  | 3 | ericsson | RADIO 4449 B12/B71 |  |  |
|  |  | 3 | rfs celwave | APXVAARR24_43-U-NA20 w/ Mount Pipe |  |  |
|  |  | 1 | tower mounts | T-Arm Mount [TA 602-3] |  |  |

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Reference | Source |
| :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | 262381 | CCISITES |
| 4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS | 262389 | CCISITES |
| 4-TOWER MANUFACTURER DRAWINGS | 262386 | CCISITES |


| Document | Reference | Source |
| :---: | :---: | :---: |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 7890057 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 6515906 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 5681337 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 3842355 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 3749907 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 3635976 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 3448150 | CCISITES |
| 4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA | 3249954 | CCISITES |
| 4-POST-MODIFICATION INSPECTION | 8418504 | CCISITES |
| 4-POST-MODIFICATION INSPECTION | 7030743 | CCISITES |
| 4-POST-MODIFICATION INSPECTION | 5921968 | CCISITES |
| 4-POST-MODIFICATION INSPECTION | 5099148 | CCISITES |
| 4-POST-MODIFICATION INSPECTION | 3675451 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 8.1.1.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A. When applicable, Crown Castle has calculated and provided the effective area for panel antennas using approved methods following the intent of the TIA-222 standard.
tnxTower was used to determine the loads on the modified structure. Additional calculations were performed to determine the stresses in the pole and in the reinforcing elements. These calculations are included in Appendix C.

## 3.2) Assumptions

1) Tower and structures were maintained in accordance with the TIA-222 Standard.
2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Crown Castle should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $130-125$ | Pole | TP11.775×10.525x0.1875 | Pole | $0.5 \%$ |  |
| $125-120$ | Pole | TP13.025x11.775x0.1875 | Pole | $4.6 \%$ | Pass |
| $120-115$ | Pole | TP14.275x13.025x0.1875 | Pole | $26.0 \%$ | Pass |
| $115-110$ | Pole | TP15.525x14.275x0.1875 | Pole | $41.8 \%$ | Pass |
| $110-105$ | Pole | TP16.776x15.525x0.25 | Pole | $48.3 \%$ | Pass |
| $105-100$ | Pole | TP18.027x16.776x0.25 | Pole | $60.6 \%$ | Pass |
| $100-95$ | Pole | TP19.277x18.027x0.25 | Pole | $73.4 \%$ | Pass |
| $95-90$ | Pole | TP20.528×19.277x0.25 | Pole | $84.8 \%$ | Pass |


| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 90-89.75 | Pole + Reinf. | TP20.591×20.528x0.5 | Reinf. 12 Tension Rupture | 75.7\% | Pass |
| 89.75-84.75 | Pole + Reinf. | TP21.841×20.591×0.4813 | Reinf. 12 Tension Rupture | 87.3\% | Pass |
| 84.75-84.58 | Pole + Reinf. | TP21.884×21.841×0.475 | Reinf. 12 Tension Rupture | 87.7\% | Pass |
| 84.58-84.33 | Pole + Reinf. | TP21.946x21.884x0.6375 | Reinf. 12 Tension Rupture | 67.8\% | Pass |
| 84.33-83.42 | Pole + Reinf. | TP22.174×21.946x0.625 | Reinf. 12 Tension Rupture | 69.6\% | Pass |
| 83.42-83.17 | Pole + Reinf. | TP22.237x22.174x0.95 | Reinf. 17 Tension Rupture | 48.8\% | Pass |
| 83.17-83 | Pole + Reinf. | TP22.279x22.237×0.95 | Reinf. 17 Tension Rupture | 49.1\% | Pass |
| 83-82.75 | Pole + Reinf. | TP22.342x22.279x0.7 | Reinf. 17 Tension Rupture | 65.2\% | Pass |
| 82.75-77.75 | Pole + Reinf. | TP23.592x22.342x0.6625 | Reinf. 17 Tension Rupture | 73.3\% | Pass |
| 77.75-74 | Pole + Reinf. | TP25.531x23.592x0.65 | Reinf. 17 Tension Rupture | 79.9\% | Pass |
| 74-69 | Pole + Reinf. | TP25.281x24.03x0.7 | Reinf. 17 Tension Rupture | 82.2\% | Pass |
| 69-67.08 | Pole + Reinf. | TP25.761×25.281×0.6875 | Reinf. 17 Tension Rupture | 84.8\% | Pass |
| 67.08-66.83 | Pole + Reinf. | TP25.824×25.761×0.6875 | Reinf. 17 Tension Rupture | 85.1\% | Pass |
| 66.83-64.08 | Pole + Reinf. | TP26.512x25.824x0.675 | Reinf. 17 Tension Rupture | 88.5\% | Pass |
| 64.08-63.83 | Pole + Reinf. | TP26.574x26.512x0.7375 | Reinf. 17 Tension Rupture | 85.0\% | Pass |
| 63.83-62.5 | Pole + Reinf. | TP26.907x26.574x0.7375 | Reinf. 17 Tension Rupture | 86.5\% | Pass |
| 62.5-62.25 | Pole + Reinf. | TP26.969x26.907x0.8625 | Reinf. 17 Tension Rupture | 71.7\% | Pass |
| 62.25-57.25 | Pole + Reinf. | TP28.22x26.969x0.8375 | Reinf. 17 Tension Rupture | 76.4\% | Pass |
| 57.25-53.5 | Pole + Reinf. | TP29.158x28.22x0.8125 | Reinf. 17 Tension Rupture | 79.6\% | Pass |
| 53.5-53.25 | Pole + Reinf. | TP29.22x29.158x0.8375 | Reinf. 10 Tension Rupture | 78.9\% | Pass |
| 53.25-52.58 | Pole + Reinf. | TP29.388x29.22x0.825 | Reinf. 10 Tension Rupture | 79.5\% | Pass |
| 52.58-52.33 | Pole + Reinf. | TP29.45x29.388x0.8625 | Reinf. 10 Tension Rupture | 76.6\% | Pass |
| 52.33-47.33 | Pole + Reinf. | TP30.701x29.45x0.8375 | Reinf. 10 Tension Rupture | 80.5\% | Pass |
| 47.33-44.58 | Pole + Reinf. | TP31.389x30.701×0.8125 | Reinf. 10 Tension Rupture | 82.4\% | Pass |
| 44.58-44.33 | Pole + Reinf. | TP31.451×31.389x0.8125 | Reinf. 10 Tension Rupture | 82.6\% | Pass |
| 44.33-41.92 | Pole + Reinf. | TP32.054×31.451x0.8 | Reinf. 10 Tension Rupture | 84.3\% | Pass |
| 41.92-41.67 | Pole + Reinf. | TP32.117x32.054×0.8125 | Reinf. 9 Tension Rupture | 75.1\% | Pass |
| 41.67-39 | Pole + Reinf. | TP34.015x32.117x0.7875 | Reinf. 9 Tension Rupture | 76.6\% | Pass |
| 39-34 | Pole + Reinf. | TP33.408x32.159x0.8188 | Reinf. 9 Tension Rupture | 78.3\% | Pass |
| 34-29 | Pole + Reinf. | TP34.657x33.408×0.7938 | Reinf. 9 Tension Rupture | 80.6\% | Pass |
| 29-26.92 | Pole + Reinf. | TP35.177×34.657x0.7938 | Reinf. 9 Tension Rupture | 81.5\% | Pass |
| 26.92-26.67 | Pole + Reinf. | TP35.239x35.177x0.8938 | Reinf. 7 Tension Rupture | 76.3\% | Pass |
| 26.67-21.67 | Pole + Reinf. | TP36.488×35.239x0.8688 | Reinf. 7 Tension Rupture | 78.4\% | Pass |
| 21.67-18 | Pole + Reinf. | TP37.404×36.488x0.8563 | Reinf. 7 Tension Rupture | 79.8\% | Pass |
| 18-17.75 | Pole + Reinf. | TP37.467×37.404×0.9938 | Reinf. 16 Tension Rupture | 67.1\% | Pass |
| 17.75-17.5 | Pole + Reinf. | TP37.529x37.467x0.9938 | Reinf. 16 Tension Rupture | 67.2\% | Pass |
| 17.5-17.25 | Pole + Reinf. | TP37.592x37.529x0.9938 | Reinf. 15 Tension Rupture | 67.3\% | Pass |
| 17.25-17.08 | Pole + Reinf. | TP37.634×37.592x0.9938 | Reinf. 15 Tension Rupture | 67.3\% | Pass |
| 17.08-16.83 | Pole + Reinf. | TP37.697x37.634×0.8938 | Reinf. 15 Tension Rupture | 73.5\% | Pass |
| 16.83-13 | Pole + Reinf. | TP38.653x37.697x0.8813 | Reinf. 15 Tension Rupture | 74.8\% | Pass |
| 13-12.75 | Pole + Reinf. | TP38.716x38.653x1.0563 | Reinf. 5 Tension Rupture | 63.5\% | Pass |
| 12.75-11.92 | Pole + Reinf. | TP38.923x38.716x1.0438 | Reinf. 5 Tension Rupture | 63.8\% | Pass |
| 11.92-11.67 | Pole + Reinf. | TP38.985×38.923x0.8188 | Reinf. 15 Tension Rupture | 81.7\% | Pass |
| 11.67-6.67 | Pole + Reinf. | TP40.234×38.985x0.7938 | Reinf. 15 Tension Rupture | 83.3\% | Pass |

tnxTower Report - version 8.1.1.0

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.67-6.5 | Pole + Reinf. | TP40.277x40.234×0.7938 | Reinf. 15 Tension Rupture | 83.4\% | Pass |
| 6.5-6.25 | Pole + Reinf. | TP40.339×40.277×0.9188 | Reinf. 5 Tension Rupture | 77.9\% | Pass |
| 6.25-3.75 | Pole + Reinf. | TP40.963×40.339x0.9063 | Reinf. 5 Tension Rupture | 78.6\% | Pass |
| 3.75-3.5 | Pole + Reinf. | TP41.026x40.963x1.0063 | Reinf. 14 Tension Rupture | 68.1\% | Pass |
| 3.5-3 | Pole + Reinf. | TP41.151x41.026x0.9938 | Reinf. 14 Tension Rupture | 68.3\% | Pass |
| 3-2.75 | Pole + Reinf. | TP41.213x41.151x0.9938 | Reinf. 15 Tension Rupture | 73.2\% | Pass |
| 2.75-0 | Pole + Reinf. | TP41.9×41.213x1.0188 | Reinf. 4 Weldment | 86.8\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 84.8\% | Pass |
|  |  |  | Reinforcement | 88.5\% | Pass |

Table 5 - Tower Component Stresses vs. Capacity - LC7

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 84.7 | Pass |
| 1 | Base Plate | 0 | 57.1 | Pass |
| 1 | Base Foundation (Structure) | 0 | 62.2 | Pass |
| 1 | Base Foundation (Soil Interaction) | 0 | 72.7 | Pass |
| 1 | Flange Bolts | 110 | 38.4 | Pass |
| 1 | Flange Plate | 110 | 20.6 | Pass |

## Structure Rating (max from all components) =

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

TNXTOWER OUTPUT


## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

- Tower base elevation above sea level: 41.0000 ft .
- Basic wind speed of 125 mph .
- Risk Category II.
- Exposure Category C.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- Topographic Category: 1.
- Crest Height: 0.0000 ft .
- Nominal ice thickness of 2.0000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56.00 pcf .
- A wind speed of 50 mph is used in combination with ice.
- Temperature drop of $50^{\circ} \mathrm{F}$.
- Deflections calculated using a wind speed of 60 mph .
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1 .
- Tower analysis based on target reliabilities in accordance with Annex S.
- Load Modification Factors used: $\mathrm{K}_{\mathrm{es}}\left(\mathrm{F}_{\mathrm{w}}\right)=0.95, \mathrm{~K}_{\mathrm{es}}\left(\mathrm{t}_{\mathrm{i}}\right)=0.85$.
- Maximum demand-capacity ratio is: 1.05 .
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

| Options |  |  |
| :---: | :---: | :---: |
| Consider Moments - Legs | Distribute Leg Loads As Uniform | Use ASCE 10 X-Brace Ly Rules |
| Consider Moments - Horizontals | Assume Legs Pinned | Calculate Redundant Bracing Forces |
| Consider Moments - Diagonals | $\checkmark$ Assume Rigid Index Plate | Ignore Redundant Members in FEA |
| Use Moment Magnification | $\checkmark$ Use Clear Spans For Wind Area | SR Leg Bolts Resist Compression |
| Use Code Stress Ratios | Use Clear Spans For KL/r | All Leg Panels Have Same Allowable |
| Use Code Safety Factors - Guys | Retension Guys To Initial Tension | Offset Girt At Foundation |
| Escalate Ice | $\checkmark$ Bypass Mast Stability Checks | $\checkmark$ Consider Feed Line Torque |
| Always Use Max Kz | $\checkmark$ Use Azimuth Dish Coefficients | Include Angle Block Shear Check |
| Use Special Wind Profile | $\checkmark$ Project Wind Area of Appurt. | Use TIA-222-H Bracing Resist. Exemption |
| Include Bolts In Member Capacity | Autocalc Torque Arm Areas | Use TIA-222-H Tension Splice Exemption |
| Leg Bolts Are At Top Of Section | Add IBC . $6 \mathrm{D}+\mathrm{W}$ Combination | Poles |
| Secondary Horizontal Braces Leg | $\checkmark$ Sort Capacity Reports By Component | $\sqrt{ }$ Include Shear-Torsion Interaction |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing | Always Use Sub-Critical Flow |
| SR Members Have Cut Ends | Treat Feed Line Bundles As Cylinder | Use Top Mounted Sockets |
| SR Members Are Concentric | Ignore KL/ry For 60 Deg. Angle Legs | Pole Without Linear Attachments |
|  |  | Pole With Shroud Or No |
|  |  | Appurtenances |
|  |  | Outside and Inside Corner Radii Are |

## Tapered Pole Section Geometry

| Section | Elevation | Section | Splice | Number | Top | Bottom | Wall | Bend | Pole Grade |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | Length | Length <br> ft | of | Diameter | Diameter <br> Thickness | Radius <br> Rides | in | in |


| Section | Elevation <br> ft | Section Length ft | Splice <br> Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $\begin{aligned} & 130.0000- \\ & 125.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 10.5250 | 11.7750 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | $\begin{aligned} & 125.0000- \\ & 120.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 11.7750 | 13.0250 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | $\begin{aligned} & 120.0000- \\ & 115.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 13.0250 | 14.2750 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | $\begin{aligned} & 115.0000- \\ & 110.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 14.2750 | 15.5250 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L5 | $\begin{aligned} & 110.0000- \\ & 105.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 15.5250 | 16.7757 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L6 | $\begin{aligned} & 105.0000- \\ & 100.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 16.7757 | 18.0265 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L7 | $\begin{gathered} 100.0000- \\ 95.0000 \end{gathered}$ | 5.0000 | 0.00 | 12 | 18.0265 | 19.2772 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L8 | $\begin{aligned} & 95.0000- \\ & 90.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 19.2772 | 20.5280 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L9 | $\begin{aligned} & 90.0000- \\ & 89.7500 \end{aligned}$ | 0.2500 | 0.00 | 12 | 20.5280 | 20.5905 | 0.5000 | 2.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L10 | $\begin{gathered} 89.7500- \\ 84.7500 \end{gathered}$ | 5.0000 | 0.00 | 12 | 20.5905 | 21.8413 | 0.4813 | 1.9250 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L11 | $\begin{aligned} & 84.7500- \\ & 84.5800 \end{aligned}$ | 0.1700 | 0.00 | 12 | 21.8413 | 21.8838 | 0.4750 | 1.9000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L12 | $\begin{aligned} & 84.5800- \\ & 84.3300 \end{aligned}$ | 0.2500 | 0.00 | 12 | 21.8838 | 21.9464 | 0.6375 | 2.5500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L13 | $\begin{aligned} & 84.3300- \\ & 83.4200 \end{aligned}$ | 0.9100 | 0.00 | 12 | 21.9464 | 22.1740 | 0.6250 | 2.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L14 | $\begin{gathered} 83.4200- \\ 83.1700 \end{gathered}$ | 0.2500 | 0.00 | 12 | 22.1740 | 22.2365 | 0.9500 | 3.8000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L15 | $\begin{aligned} & 83.1700- \\ & 83.0000 \end{aligned}$ | 0.1700 | 0.00 | 12 | 22.2365 | 22.2791 | 0.9500 | 3.8000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L16 | $\begin{aligned} & 83.0000- \\ & 82.7500 \end{aligned}$ | 0.2500 | 0.00 | 12 | 22.2791 | 22.3416 | 0.7000 | 2.8000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L17 | $\begin{aligned} & 82.7500- \\ & 77.7500 \end{aligned}$ | 5.0000 | 0.00 | 12 | 22.3416 | 23.5923 | 0.6625 | 2.6500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L18 | $\begin{aligned} & 77.7500- \\ & 70.0000 \end{aligned}$ | 7.7500 | 4.00 | 12 | 23.5923 | 25.5310 | 0.6500 | 2.6000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L19 | $\begin{aligned} & 70.0000- \\ & 69.0000 \end{aligned}$ | 5.0000 | 0.00 | 12 | 24.0304 | 25.2810 | 0.7000 | 2.8000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L20 | $\begin{aligned} & 69.0000- \\ & 67.0800 \end{aligned}$ | 1.9200 | 0.00 | 12 | 25.2810 | 25.7612 | 0.6875 | 2.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L21 | $\begin{aligned} & 67.0800- \\ & 66.8300 \end{aligned}$ | 0.2500 | 0.00 | 12 | 25.7612 | 25.8237 | 0.6875 | 2.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L22 | $\begin{aligned} & 66.8300- \\ & 64.0800 \end{aligned}$ | 2.7500 | 0.00 | 12 | 25.8237 | 26.5115 | 0.6750 | 2.7000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L23 | $\begin{aligned} & 64.0800- \\ & 63.8300 \end{aligned}$ | 0.2500 | 0.00 | 12 | 26.5115 | 26.5741 | 0.7375 | 2.9500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L24 | $\begin{aligned} & 63.8300- \\ & 62.5000 \end{aligned}$ | 1.3300 | 0.00 | 12 | 26.5741 | 26.9067 | 0.7375 | 2.9500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L25 | $\begin{aligned} & 62.5000- \\ & 62.2500 \end{aligned}$ | 0.2500 | 0.00 | 12 | 26.9067 | 26.9693 | 0.8625 | 3.4500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L26 | $\begin{aligned} & 62.2500- \\ & 57.2500 \end{aligned}$ | 5.0000 | 0.00 | 12 | 26.9693 | 28.2198 | 0.8375 | 3.3500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L27 | $\begin{aligned} & 57.2500- \\ & 53.5000 \end{aligned}$ | 3.7500 | 0.00 | 12 | 28.2198 | 29.1578 | 0.8125 | 3.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L28 | $\begin{aligned} & 53.5000- \\ & 53.2500 \end{aligned}$ | 0.2500 | 0.00 | 12 | 29.1578 | 29.2203 | 0.8375 | 3.3500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L29 | $\begin{aligned} & 53.2500- \\ & 52.5800 \end{aligned}$ | 0.6700 | 0.00 | 12 | 29.2203 | 29.3879 | 0.8250 | 3.3000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L30 | $\begin{aligned} & 52.5800- \\ & 52.3300 \end{aligned}$ | 0.2500 | 0.00 | 12 | 29.3879 | 29.4504 | 0.8625 | 3.4500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L31 | $\begin{gathered} 52.3300- \\ 47.3300 \end{gathered}$ | 5.0000 | 0.00 | 12 | 29.4504 | 30.7010 | 0.8375 | 3.3500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L32 | $\begin{aligned} & 47.3300- \\ & 44.5800 \end{aligned}$ | 2.7500 | 0.00 | 12 | 30.7010 | 31.3888 | 0.8125 | 3.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L33 | $\begin{aligned} & 44.5800- \\ & 44.3300 \end{aligned}$ | 0.2500 | 0.00 | 12 | 31.3888 | 31.4513 | 0.8125 | 3.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L34 | $\begin{aligned} & 44.3300- \\ & 41.9200 \end{aligned}$ | 2.4100 | 0.00 | 12 | 31.4513 | 32.0541 | 0.8000 | 3.2000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L35 | 41.9200- | 0.2500 | 0.00 | 12 | 32.0541 | 32.1166 | 0.8125 | 3.2500 | A572-65 |

tnxTower Report - version 8.1.1.0

| Section | Elevation ft | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L36 | 41.6700 | 7.5900 | 4.92 | 12 | 32.1166 | 34.0150 | 0.7875 | 3.1500 | (65 ksi) |
|  | 41.6700- |  |  |  |  |  |  |  | A572-65 |
|  | 34.0800 |  |  |  |  |  |  |  | (65 ksi) |
| L37 | 34.0800- | 5.0000 | 0.00 | 12 | 32.1594 | 33.4082 | 0.8187 | 3.2750 | A572-65 |
|  | 34.0000 |  |  |  |  |  |  |  | (65 ksi) |
| L38 | 34.0000- | 5.0000 | 0.00 | 12 | 33.4082 | 34.6570 | 0.7937 | 3.1750 | A572-65 |
|  | 29.0000 |  |  |  |  |  |  |  | (65 ksi) |
| L39 | 29.0000- | 2.0800 | 0.00 | 12 | 34.6570 | 35.1765 | 0.7937 | 3.1750 | A572-65 |
|  | 26.9200 |  |  |  |  |  |  |  | (65 ksi) |
| L40 | 26.9200- | 0.2500 | 0.00 | 12 | 35.1765 | 35.2390 | 0.8938 | 3.5750 | A572-65 |
|  | 26.6700 |  |  |  |  |  |  |  | (65 ksi) |
| L41 | 26.6700- | 5.0000 | 0.00 | 12 | 35.2390 | 36.4877 | 0.8688 | 3.4750 | A572-65 |
|  | 21.6700 |  |  |  |  |  |  |  | (65 ksi) |
| L42 | 21.6700- | 3.6700 | 0.00 | 12 | 36.4877 | 37.4044 | 0.8562 | 3.4250 | A572-65 |
|  | 18.0000 |  |  |  |  |  |  |  | (65 ksi) |
| L43 | 18.0000- | 0.2500 | 0.00 | 12 | 37.4044 | 37.4668 | 0.9938 | 3.9750 | A572-65 |
|  | 17.7500 |  |  |  |  |  |  |  | (65 ksi) |
| L44 | 17.7500- | 0.2500 | 0.00 | 12 | 37.4668 | 37.5292 | 0.9938 | 3.9750 | A572-65 |
|  | 17.5000 |  |  |  |  |  |  |  | (65 ksi) |
| L45 | 17.5000- | 0.2500 | 0.00 | 12 | 37.5292 | 37.5917 | 0.9938 | 3.9750 | A572-65 |
|  | 17.2500 |  |  |  |  |  |  |  | (65 ksi) |
| L46 | 17.2500- | 0.1700 | 0.00 | 12 | 37.5917 | 37.6341 | 0.9938 | 3.9750 | A572-65 |
|  | 17.0800 |  |  |  |  |  |  |  | (65 ksi) |
| L47 | 17.0800- | 0.2500 | 0.00 | 12 | 37.6341 | 37.6966 | 0.8938 | 3.5750 | A572-65 |
|  | 16.8300 |  |  |  |  |  |  |  | (65 ksi) |
| L48 | 16.8300- | 3.8300 | 0.00 | 12 | 37.6966 | 38.6531 | 0.8812 | 3.5250 | A572-65 |
|  | 13.0000 |  |  |  |  |  |  |  | (65 ksi) |
| L49 | 13.0000- | 0.2500 | 0.00 | 12 | 38.6531 | 38.7156 | 1.0562 | 4.2250 | A572-65 |
|  | 12.7500 |  |  |  |  |  |  |  | (65 ksi) |
| L50 | 12.7500- | 0.8300 | 0.00 | 12 | 38.7156 | 38.9229 | 1.0438 | 4.1750 | A572-65 |
|  | 11.9200 |  |  |  |  |  |  |  | (65 ksi) |
| L51 | 11.9200- | 0.2500 | 0.00 | 12 | 38.9229 | 38.9853 | 0.8187 | 3.2750 | A572-65 |
|  | 11.6700 |  |  |  |  |  |  |  | (65 ksi) |
| L52 | 11.6700- | 5.0000 | 0.00 | 12 | 38.9853 | 40.2341 | 0.7937 | 3.1750 | A572-65 |
|  | 6.6700 |  |  |  |  |  |  |  | (65 ksi) |
| L53 | 6.6700-6.5000 | 0.1700 | 0.00 | 12 | 40.2341 | 40.2766 | 0.7937 | 3.1750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L54 | 6.5000-6.2500 | 0.2500 | 0.00 | 12 | 40.2766 | 40.3390 | 0.9187 | 3.6750 | A572-65 <br> (65 ksi) |
|  |  |  |  |  |  |  |  |  |  |
| L55 | 6.2500-3.7500 | 2.5000 | 0.00 | 12 | 40.3390 | 40.9634 | 0.9063 | 3.6250 | A572-65 <br> (65 ksi) |
|  |  |  |  |  |  |  |  |  |  |
| L56 | 3.7500-3.5000 | 0.2500 | 0.00 | 12 | 40.9634 | 41.0258 | 1.0063 | 4.0250 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L57 | 3.5000-3.0000 | 0.5000 | 0.00 | 12 | 41.0258 | 41.1507 | 0.9938 | 3.9750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L58 | 3.0000-2.7500 | 0.2500 | 0.00 | 12 | 41.1507 | 41.2132 | 0.9938 | 3.9750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L59 | 2.7500-0.0000 | 2.7500 |  | 12 | 41.2132 | 41.9000 | 1.0188 | 4.0750 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |

Tapered Pole Properties

| Section | Tip Dia. <br> in | Area <br> $i n^{2}$ | $I$ <br> $i n^{4}$ | $r$ <br> $i n$ | $C$ <br> $i n$ | $I / C$ <br> $i n^{3}$ | $J$ <br> $i n^{4}$ | $I t / Q$ <br> $i n^{2}$ | $w$ <br> $i n$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 10.8301 | 6.2413 | 85.1314 | 3.7008 | 5.4520 | 15.6148 | 172.4993 | 3.0718 | 2.3182 | 12.364 |
|  | 12.1242 | 6.9960 | 119.8981 | 4.1483 | 6.0995 | 19.6572 | 242.9461 | 3.4432 | 2.6532 | 14.15 |
| L2 | 12.1242 | 6.9960 | 119.8981 | 4.1483 | 6.0995 | 19.6572 | 242.9461 | 3.4432 | 2.6532 | 14.15 |
|  | 13.4183 | 7.7506 | 163.0364 | 4.5958 | 6.7470 | 24.1645 | 330.3559 | 3.8146 | 2.9882 | 15.937 |
| L3 | 13.4183 | 7.7506 | 163.0364 | 4.5958 | 6.7470 | 24.1645 | 330.3559 | 3.8146 | 2.9882 | 15.937 |
|  | 14.7124 | 8.5053 | 215.4492 | 5.0433 | 7.3945 | 29.1366 | 436.5585 | 4.1861 | 3.3232 | 17.724 |
| L4 | 14.7124 | 8.5053 | 215.4492 | 5.0433 | 7.3945 | 29.1366 | 436.5585 | 4.1861 | 3.3232 | 17.724 |
|  | 16.0065 | 9.2600 | 278.0397 | 5.4908 | 8.0419 | 34.5737 | 563.3838 | 4.5575 | 3.6582 | 19.51 |
| L5 | 15.9845 | 12.2964 | 366.2060 | 5.4684 | 8.0419 | 45.5370 | 742.0327 | 6.0519 | 3.4907 | 13.963 |
|  | 17.2793 | 13.3032 | 463.7302 | 5.9162 | 8.6898 | 53.3646 | 939.6431 | 6.5474 | 3.8259 | 15.304 |
| L6 | 17.2793 | 13.3032 | 463.7302 | 5.9162 | 8.6898 | 53.3646 | 939.6431 | 6.5474 | 3.8259 | 15.304 |

tnxTower Report - version 8.1.1.0

| Section | Tip Dia. in | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{gathered} r \\ i n \end{gathered}$ | $\begin{aligned} & \text { C } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{aligned} & I t / Q \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & \text { w } \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L7 | 18.5742 | 14.3101 | 577.1924 | 6.3640 | 9.3377 | 61.8129 | 1169.5483 | 7.0430 | 4.1611 | 16.644 |
|  | 18.5742 | 14.3101 | 577.1924 | 6.3640 | 9.3377 | 61.8129 | 1169.5483 | 7.0430 | 4.1611 | 16.644 |
|  | 19.8691 | 15.3169 | 707.7989 | 6.8118 | 9.9856 | 70.8819 | 1434.1925 | 7.5385 | 4.4963 | 17.985 |
| L8 | 19.8691 | 15.3169 | 707.7989 | 6.8118 | 9.9856 | 70.8819 | 1434.1925 | 7.5385 | 4.4963 | 17.985 |
|  | 21.1640 | 16.3238 | 856.7561 | 7.2595 | 10.6335 | 80.5714 | 1736.0201 | 8.0341 | 4.8315 | 19.326 |
| L9 | 21.0758 | 32.2451 | 1650.9145 | 7.1700 | 10.6335 | 155.2559 | 3345.2003 | 15.8700 | 4.1615 | 8.323 |
|  | 21.1405 | 32.3458 | 1666.4278 | 7.1924 | 10.6659 | 156.2389 | 3376.6345 | 15.9196 | 4.1783 | 8.357 |
| L10 | 21.1471 | 31.1619 | 1608.4317 | 7.1991 | 10.6659 | 150.8013 | 3259.1186 | 15.3369 | 4.2285 | 8.787 |
|  | 22.4420 | 33.1000 | 1927.6075 | 7.6469 | 11.3138 | 170.3769 | 3905.8553 | 16.2908 | 4.5637 | 9.483 |
| L11 | 22.4442 | 32.6797 | 1904.2442 | 7.6491 | 11.3138 | 168.3118 | 3858.5150 | 16.0840 | 4.5805 | 9.643 |
|  | 22.4882 | 32.7448 | 1915.6369 | 7.6644 | 11.3358 | 168.9898 | 3881.5997 | 16.1160 | 4.5919 | 9.667 |
| L12 | 22.4309 | 43.6134 | 2512.8857 | 7.6062 | 11.3358 | 221.6767 | 5091.7877 | 21.4652 | 4.1564 | 6.52 |
|  | 22.4956 | 43.7417 | 2535.1408 | 7.6286 | 11.3682 | 223.0026 | 5136.8825 | 21.5284 | 4.1731 | 6.546 |
| L13 | 22.5001 | 42.9092 | 2489.8086 | 7.6330 | 11.3682 | 219.0150 | 5045.0273 | 21.1186 | 4.2066 | 6.731 |
|  | 22.7357 | 43.3673 | 2570.4101 | 7.7145 | 11.4861 | 223.7839 | 5208.3477 | 21.3441 | 4.2676 | 6.828 |
| L14 | 22.6211 | 64.9242 | 3732.8999 | 7.5982 | 11.4861 | 324.9921 | 7563.8672 | 31.9537 | 3.3966 | 3.575 |
|  | 22.6858 | 65.1155 | 3765.9947 | 7.6206 | 11.5185 | 326.9513 | 7630.9263 | 32.0479 | 3.4134 | 3.593 |
| L15 | 22.6858 | 65.1155 | 3765.9947 | 7.6206 | 11.5185 | 326.9513 | 7630.9263 | 32.0479 | 3.4134 | 3.593 |
|  | 22.7298 | 65.2456 | 3788.6105 | 7.6358 | 11.5405 | 328.2869 | 7676.7521 | 32.1119 | 3.4248 | 3.605 |
| L16 | 22.8180 | 48.6392 | 2890.9250 | 7.7253 | 11.5405 | 250.5015 | 5857.7978 | 23.9387 | 4.0948 | 5.85 |
|  | 22.8828 | 48.7801 | 2916.1322 | 7.7477 | 11.5729 | 251.9785 | 5908.8744 | 24.0081 | 4.1115 | 5.874 |
| L17 | 22.8960 | 46.2469 | 2774.2826 | 7.7611 | 11.5729 | 239.7215 | 5621.4487 | 22.7613 | 4.2120 | 6.358 |
|  | 24.1909 | 48.9151 | 3282.6958 | 8.2089 | 12.2208 | 268.6148 | 6651.6316 | 24.0745 | 4.5472 | 6.864 |
| L18 | 24.1953 | 48.0183 | 3226.0283 | 8.2134 | 12.2208 | 263.9778 | 6536.8079 | 23.6332 | 4.5807 | 7.047 |
|  | $26.2023$ | 52.0759 | 4114.8942 | 8.9074 | 13.2251 | 311.1438 | 8337.8912 | 25.6302 | 5.1003 | 7.847 |
| L19 | 25.6669 | 52.5867 | 3653.4773 | 8.3523 | 12.4477 | 293.5051 | 7402.9356 | 25.8816 | 4.5641 | 6.52 |
|  | 25.9259 | 55.4055 | 4273.0428 | 8.8000 | 13.0955 | 326.2974 | 8658.3431 | 27.2689 | 4.8993 | 6.999 |
| L20 | 25.9303 | 54.4438 | 4203.1441 | 8.8045 | 13.0955 | 320.9598 | 8516.7095 | 26.7956 | 4.9328 | 7.175 |
|  | 26.4274 | 55.5069 | 4454.1995 | 8.9764 | 13.3443 | 333.7904 | 9025.4158 | 27.3188 | 5.0615 | 7.362 |
| L21 | 26.4274 | 55.5069 | 4454.1995 | 8.9764 | 13.3443 | 333.7904 | 9025.4158 | 27.3188 | 5.0615 | 7.362 |
|  | 26.4922 | 55.6453 | 4487.6063 | 8.9988 | 13.3767 | 335.4796 | 9093.1071 | 27.3869 | 5.0783 | 7.387 |
| L22 | 26.4966 | 54.6608 | 4412.5900 | 9.0032 | 13.3767 | 329.8716 | 8941.1036 | 26.9024 | 5.1118 | 7.573 |
|  | 27.2087 | 56.1557 | 4784.6350 | 9.2495 | 13.7330 | 348.4047 | 9694.9676 | 27.6381 | 5.2961 | 7.846 |
| L23 | 27.1866 | 61.2069 | 5189.8105 | 9.2271 | 13.7330 | 377.9086 | $\begin{gathered} 10515.963 \\ 0 \end{gathered}$ | 30.1242 | 5.1286 | 6.954 |
|  | 27.2513 | 61.3554 | 5227.6742 | 9.2495 | 13.7654 | 379.7700 | $\begin{gathered} 10592.685 \\ 2 \end{gathered}$ | 30.1973 | 5.1454 | 6.977 |
| L24 | 27.2513 | 61.3554 | 5227.6742 | 9.2495 | 13.7654 | 379.7700 | $\begin{gathered} 10592.685 \\ 2 \end{gathered}$ | 30.1973 | 5.1454 | 6.977 |
|  | 27.5957 | 62.1454 | 5432.2086 | 9.3686 | 13.9377 | 389.7497 | $\begin{gathered} 11007.127 \\ 3 \end{gathered}$ | 30.5861 | 5.2345 | 7.098 |
| L25 | 27.5516 | 72.3313 | 6262.3199 | 9.3238 | 13.9377 | 449.3085 | $\begin{gathered} 12689.157 \\ 9 \end{gathered}$ | 35.5993 | 4.8995 | 5.681 |
|  | 27.6164 | 72.5050 | 6307.5333 | 9.3462 | 13.9701 | 451.5032 | $\begin{gathered} 12780.772 \\ 6 \end{gathered}$ | 35.6847 | 4.9163 | 5.7 |
| L26 | 27.6252 | 70.4708 | 6142.3183 | 9.3552 | 13.9701 | 439.6769 | $\begin{gathered} 12446.002 \\ 2 \end{gathered}$ | 34.6836 | 4.9833 | 5.95 |
|  | 28.9199 | 73.8433 | 7067.0448 | 9.8029 | 14.6179 | 483.4524 | $\begin{gathered} 14319.748 \\ 7 \end{gathered}$ | 36.3434 | 5.3184 | 6.35 |
| L27 | 28.9287 | 71.7044 | 6874.8841 | 9.8118 | 14.6179 | 470.3068 | $\begin{gathered} 13930.379 \\ 1 \end{gathered}$ | 35.2907 | 5.3854 | 6.628 |
|  | 29.8997 | 74.1583 | 7605.1298 | 10.1476 | 15.1037 | 503.5269 | $\begin{gathered} 15410.054 \\ 8 \end{gathered}$ | 36.4985 | 5.6368 | 6.938 |
| L28 | 29.8909 | 76.3727 | 7818.4101 | 10.1387 | 15.1037 | 517.6480 | $\begin{gathered} 15842.218 \\ 6 \end{gathered}$ | 37.5883 | 5.5698 | 6.65 |
|  | 29.9556 | 76.5413 | 7870.3118 | 10.1610 | 15.1361 | 519.9692 | $\begin{gathered} 15947.385 \\ 4 \end{gathered}$ | 37.6713 | 5.5865 | 6.67 |
| L29 | 29.9600 | 75.4321 | 7763.0922 | 10.1655 | 15.1361 | 512.8855 | $\begin{gathered} 15730.129 \\ 4 \end{gathered}$ | 37.1254 | 5.6200 | 6.812 |
|  | 30.1335 | 75.8773 | 7901.3485 | 10.2255 | 15.2229 | 519.0430 | $\begin{gathered} 16010.274 \\ 3 \end{gathered}$ | 37.3445 | 5.6649 | 6.867 |
| L30 | 30.1203 | 79.2221 | 8228.0080 | 10.2121 | 15.2229 | 540.5014 | $\begin{gathered} 16672.174 \\ 9 \end{gathered}$ | 38.9907 | 5.5644 | 6.452 |
|  | 30.1850 | 79.3957 | 8282.2351 | 10.2345 | 15.2553 | 542.9085 | $\begin{gathered} 16782.053 \\ 7 \end{gathered}$ | 39.0762 | 5.5812 | 6.471 |
| L31 | 30.1939 | 77.1618 | 8063.2873 | 10.2434 | 15.2553 | 528.5563 | $\begin{gathered} 16338.406 \\ 1 \end{gathered}$ | 37.9767 | 5.6482 | 6.744 |
|  | 31.4885 | 80.5343 | 9167.4296 | 10.6911 | 15.9031 | 576.4554 | $\begin{gathered} 18575.697 \\ 9 \end{gathered}$ | 39.6365 | 5.9834 | 7.144 |
| L32 | 31.4974 | 78.1957 | 8916.1298 | 10.7001 | 15.9031 | 560.6534 | 18066.496 | 38.4856 | 6.0504 | 7.447 |

tnxTower Report - version 8.1.1.0

| Section | $\begin{gathered} \text { Tip Dia. } \\ \text { in } \end{gathered}$ | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & \text { C } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{aligned} & I t / Q \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | w/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L33 | 32.2094 | 79.9952 | 9545.9589 | 10.9463 | 16.2594 | 587.1043 | $\begin{gathered} 3 \\ 19342.700 \\ 8 \end{gathered}$ | 39.3712 | 6.2347 | 7.673 |
|  | 32.2094 | 79.9952 | 9545.9589 | 10.9463 | 16.2594 | 587.1043 | $\begin{gathered} 19342.700 \\ 8 \end{gathered}$ | 39.3712 | 6.2347 | 7.673 |
| L34 | 32.2742 | 80.1588 | 9604.6435 | 10.9687 | 16.2918 | 589.5391 | $\begin{gathered} 19461.611 \\ 7 \end{gathered}$ | 39.4517 | 6.2515 | 7.694 |
|  | 32.2786 | 78.9578 | 9468.4591 | 10.9732 | 16.2918 | 581.1800 | $\begin{gathered} 19185.665 \\ 2 \end{gathered}$ | 38.8606 | 6.2850 | 7.856 |
| L35 | 32.9026 | 80.5106 | $\begin{gathered} 10038.126 \\ 4 \end{gathered}$ | 11.1890 | 16.6040 | 604.5599 | $\begin{gathered} 20339.965 \\ 5 \end{gathered}$ | 39.6248 | 6.4465 | 8.058 |
|  | 32.8982 | 81.7358 | $\begin{gathered} 10182.744 \\ 6 \end{gathered}$ | 11.1845 | 16.6040 | 613.2698 | $\begin{gathered} 20633.001 \\ 3 \end{gathered}$ | 40.2279 | 6.4130 | 7.893 |
| L36 | 32.9630 | 81.8994 | $\begin{gathered} 10244.008 \\ 2 \end{gathered}$ | 11.2069 | 16.6364 | 615.7583 | $\begin{gathered} 20757.137 \\ 8 \end{gathered}$ | 40.3084 | 6.4298 | 7.914 |
|  | 32.9718 | 79.4428 | 9952.6148 | 11.2158 | 16.6364 | 598.2429 | $\begin{gathered} 20166.696 \\ 0 \end{gathered}$ | 39.0993 | 6.4968 | 8.25 |
| L37 | 34.9371 | 84.2566 | $\begin{gathered} 11873.681 \\ 2 \end{gathered}$ | 11.8954 | 17.6198 | 673.8840 | $\begin{gathered} 24059.297 \\ 2 \end{gathered}$ | 41.4686 | 7.0055 | 8.896 |
|  | 34.2772 | 82.6258 | $\begin{gathered} 10359.016 \\ 1 \end{gathered}$ | 11.2200 | 16.6586 | 621.8424 | $\begin{gathered} 20990.175 \\ 1 \end{gathered}$ | 40.6659 | 6.4245 | 7.847 |
| L38 | 34.2979 | 85.9181 | $\begin{gathered} 11647.297 \\ 7 \end{gathered}$ | 11.6670 | 17.3055 | 673.0418 | $\begin{gathered} 23600.582 \\ 9 \end{gathered}$ | 42.2863 | 6.7592 | 8.255 |
|  | 34.3067 35.5996 | 83.3585 86.5503 | $11317.661$ | 11.6760 12.1230 | 17.3055 17.9523 | 653.9937 | $\begin{gathered} 22932.649 \\ 7 \end{gathered}$ | 41.0265 42.5974 | 6.8262 7.1608 | 8.6 |
| L39 | 35.5996 | 86.5503 | $\begin{gathered} 12668.115 \\ 7 \end{gathered}$ | 12.1230 | 17.9523 | 705.6529 | $\begin{gathered} 25669.037 \\ 0 \end{gathered}$ | 42.5974 | 7.1608 | 9.022 |
|  | 35.5996 | 86.5503 | $\begin{gathered} 12668.115 \\ 7 \end{gathered}$ | 12.1230 | 17.9523 | 705.6529 | $\begin{gathered} 25669.037 \\ 0 \end{gathered}$ | 42.5974 | 7.1608 | 9.022 |
| L40 | 36.1374 | 87.8780 | $\begin{gathered} 13260.131 \\ 0 \end{gathered}$ | 12.3090 | 18.2214 | 727.7216 | $\begin{gathered} 26868.620 \\ 4 \end{gathered}$ | 43.2509 | 7.3001 | 9.197 |
|  | 36.1021 | 98.6615 | $\begin{gathered} 14800.802 \\ 3 \end{gathered}$ | 12.2732 | 18.2214 | 812.2743 | $\begin{gathered} 29990.438 \\ 2 \end{gathered}$ | 48.5582 | 7.0321 | 7.868 |
| L41 | 36.1668 | 98.8412 | $\begin{gathered} 14881.820 \\ 3 \end{gathered}$ | 12.2956 | 18.2538 | 815.2735 | $\begin{gathered} 30154.602 \\ 5 \end{gathered}$ | 48.6466 | 7.0488 | 7.887 |
|  | 36.1756 | 96.1463 | $\begin{gathered} 14497.157 \\ 1 \end{gathered}$ | 12.3045 | 18.2538 | 794.2004 | $\begin{gathered} 29375.170 \\ 7 \end{gathered}$ | 47.3203 | 7.1158 | 8.191 |
| L42 | 37.4684 | 99.6397 | $\begin{gathered} 16135.465 \\ 3 \end{gathered}$ | 12.7516 | 18.9007 | 853.6990 | $\begin{gathered} 32694.827 \\ 1 \end{gathered}$ | 49.0396 | 7.4505 | 8.576 |
|  | 37.4728 | 98.2405 | $\begin{gathered} 15920.049 \\ 3 \end{gathered}$ | 12.7561 | 18.9007 | 842.3017 | $\begin{gathered} 32258.336 \\ 0 \end{gathered}$ | 48.3510 | 7.4840 | 8.74 |
| L43 | 38.4218 | 100.7677 | $\begin{gathered} 17180.545 \\ 6 \end{gathered}$ | 13.0842 | 19.3755 | 886.7170 | $\begin{gathered} 34812.443 \\ 4 \end{gathered}$ | 49.5948 | 7.7296 | 9.027 |
|  | 38.3733 | 116.5094 | $\begin{gathered} 19715.264 \\ 3 \end{gathered}$ | 13.0350 | 19.3755 | 1017.5381 | $\begin{gathered} 39948.470 \\ 6 \end{gathered}$ | 57.3424 | 7.3611 | 7.407 |
| L44 | 38.4379 | 116.7092 | $\begin{gathered} 19816.865 \\ 8 \end{gathered}$ | 13.0573 | 19.4078 | 1021.0774 | $\begin{gathered} 40154.342 \\ 8 \end{gathered}$ | 57.4407 | 7.3779 | 7.424 |
|  | 38.4379 | 116.7092 | $\begin{gathered} 19816.865 \\ 8 \end{gathered}$ | 13.0573 | 19.4078 | 1021.0774 | $\begin{gathered} 40154.342 \\ 8 \end{gathered}$ | 57.4407 | 7.3779 | 7.424 |
| L45 | 38.5026 | 116.9090 | $\begin{gathered} 19918.815 \\ 8 \end{gathered}$ | 13.0797 | 19.4401 | 1024.6229 | $\begin{gathered} 40360.921 \\ 0 \end{gathered}$ | 57.5390 | 7.3946 | 7.441 |
|  | 38.5026 | 116.9090 | $\begin{gathered} 19918.815 \\ 8 \end{gathered}$ | 13.0797 | 19.4401 | 1024.6229 | $\begin{gathered} 40360.921 \\ 0 \end{gathered}$ | 57.5390 | 7.3946 | 7.441 |
| L46 | 38.5672 | 117.1088 | $\begin{gathered} 20021.114 \\ 8 \end{gathered}$ | 13.1021 | 19.4725 | 1028.1746 | $\begin{gathered} 40568.206 \\ 6 \end{gathered}$ | 57.6374 | 7.4113 | 7.458 |
|  | 38.5672 | 117.1088 | $\begin{gathered} 20021.114 \\ 8 \end{gathered}$ | 13.1021 | 19.4725 | 1028.1746 | $\begin{gathered} 40568.206 \\ 6 \end{gathered}$ | 57.6374 | 7.4113 | 7.458 |
| L47 | 38.6112 | 117.2446 | $\begin{gathered} 20090.877 \\ 9 \end{gathered}$ | 13.1173 | 19.4945 | 1030.5932 | $\begin{gathered} 40709.565 \\ 5 \end{gathered}$ | 57.7042 | 7.4227 | 7.469 |
|  | 38.6464 | 105.7342 | $\begin{gathered} 18217.503 \\ 0 \end{gathered}$ | 13.1531 | 19.4945 | 934.4955 | $\begin{gathered} 36913.600 \\ 2 \end{gathered}$ | 52.0392 | 7.6907 | 8.605 |
| L48 | 38.7111 | 105.9139 | $\begin{gathered} 18310.541 \\ 8 \end{gathered}$ | 13.1754 | 19.5268 | 937.7123 | $\begin{gathered} 37102.121 \\ 9 \end{gathered}$ | 52.1276 | 7.7074 | 8.624 |
|  | 38.7155 | 104.4681 | $\begin{gathered} 18072.853 \\ 0 \end{gathered}$ | 13.1799 | 19.5268 | 925.5398 | $\begin{gathered} 36620.500 \\ 0 \end{gathered}$ | 51.4160 | 7.7409 | 8.784 |
| L49 | 39.7058 | 107.1825 | $\begin{gathered} 19518.536 \\ 5 \end{gathered}$ | 13.5223 | 20.0223 | 974.8385 | $\begin{gathered} 39549.846 \\ 7 \end{gathered}$ | 52.7520 | 7.9973 | 9.075 |
|  | 39.6441 | 127.8717 | $\begin{gathered} 23070.895 \\ 9 \end{gathered}$ | 13.4597 | 20.0223 | 1152.2584 | $\begin{gathered} 46747.890 \\ 0 \end{gathered}$ | 62.9346 | 7.5283 | 7.127 |
|  | 39.7087 | 128.0841 | 23186.032 | 13.4820 | 20.0547 | 1156.1412 | 46981.188 | 63.0391 | 7.5450 | 7.143 |


| Section | $\begin{gathered} \text { Tip Dia. } \\ \text { in } \end{gathered}$ | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & \text { C } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & \text { w } \\ & \text { in } \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L50 | 39.7131 | 126.6103 | $\begin{gathered} 8 \\ 22934.464 \\ 2 \end{gathered}$ | 13.4865 | 20.0547 | 1143.5970 | $\begin{gathered} 5 \\ 46471.442 \\ 2 \end{gathered}$ | 62.3138 | 7.5785 | 7.261 |
| L51 | 39.9277 | 127.3070 | $\begin{gathered} 23315.160 \\ 3 \end{gathered}$ | 13.5607 | 20.1621 | 1156.3882 | $\begin{gathered} 47242.835 \\ 8 \end{gathered}$ | 62.6566 | 7.6341 | 7.314 |
|  | 40.0071 | 100.4568 | $\begin{gathered} 18616.986 \\ 9 \end{gathered}$ | 13.6413 | 20.1621 | 923.3676 | $\begin{gathered} 37723.062 \\ 7 \end{gathered}$ | 49.4418 | 8.2371 | 10.061 |
| L52 | 40.0718 | 100.6214 | $\begin{gathered} 18708.657 \\ 4 \end{gathered}$ | 13.6636 | 20.1944 | 926.4281 | $\begin{gathered} 37908.812 \\ 0 \end{gathered}$ | 49.5228 | 8.2538 | 10.081 |
|  | 40.0806 | 97.6129 | $\begin{gathered} 18173.065 \\ 3 \end{gathered}$ | 13.6726 | 20.1944 | 899.9063 | $\begin{gathered} 36823.557 \\ 2 \end{gathered}$ | 48.0421 | 8.3208 | 10.483 |
| L53 | 41.3734 | 100.8046 | $\begin{gathered} 20014.662 \\ 9 \end{gathered}$ | 14.1197 | 20.8413 | 960.3379 | $\begin{gathered} 40555.133 \\ 3 \end{gathered}$ | 49.6130 | 8.6555 | 10.905 |
|  | 41.3734 | 100.8046 | $\begin{gathered} 20014.662 \\ 9 \end{gathered}$ | 14.1197 | 20.8413 | 960.3379 | $\begin{gathered} 40555.133 \\ 3 \end{gathered}$ | 49.6130 | 8.6555 | 10.905 |
| L54 | 41.4174 | 100.9132 | $\begin{gathered} 20079.371 \\ 9 \end{gathered}$ | 14.1349 | 20.8633 | 962.4271 | $\begin{gathered} 40686.251 \\ 3 \end{gathered}$ | 49.6664 | 8.6669 | 10.919 |
|  | 41.3733 | 116.4352 | $\begin{gathered} 23021.432 \\ 9 \end{gathered}$ | 14.0901 | 20.8633 | 1103.4435 | $\begin{gathered} 46647.664 \\ 5 \end{gathered}$ | 57.3059 | 8.3319 | 9.069 |
| L55 | 41.4379 | 116.6199 | $\begin{gathered} 23131.174 \\ 4 \end{gathered}$ | 14.1125 | 20.8956 | 1106.9874 | $\begin{gathered} 46870.030 \\ 6 \end{gathered}$ | 57.3968 | 8.3486 | 9.087 |
|  | 41.4423 | 115.0697 | $\begin{gathered} 22838.176 \\ 5 \end{gathered}$ | 14.1169 | 20.8956 | 1092.9654 | $\begin{gathered} 46276.337 \\ 3 \end{gathered}$ | 56.6338 | 8.3821 | 9.249 |
| L56 | 42.0887 | 116.8918 | $\begin{gathered} 23940.334 \\ 3 \end{gathered}$ | 14.3405 | 21.2190 | 1128.2475 | $\begin{gathered} 48509.607 \\ 8 \end{gathered}$ | 57.5306 | 8.5494 | 9.434 |
|  | 42.0535 | 129.4662 | $\begin{gathered} 26383.442 \\ 2 \end{gathered}$ | 14.3047 | 21.2190 | 1243.3850 | $\begin{gathered} 53460.006 \\ 8 \end{gathered}$ | 63.7193 | 8.2814 | 8.23 |
| L57 | 42.1181 | 129.6685 | $\begin{gathered} 26507.320 \\ 8 \end{gathered}$ | 14.3270 | 21.2514 | 1247.3218 | $\begin{gathered} 53711.018 \\ 4 \end{gathered}$ | 63.8189 | 8.2982 | 8.247 |
|  | 42.1225 | 128.0977 | $\begin{gathered} 26202.574 \\ 8 \end{gathered}$ | 14.3315 | 21.2514 | 1232.9818 | $\begin{gathered} 53093.520 \\ 5 \end{gathered}$ | 63.0458 | 8.3317 | 8.384 |
| L58 | 42.2518 | 128.4973 | $\begin{gathered} 26448.555 \\ 3 \end{gathered}$ | 14.3762 | 21.3161 | 1240.7797 | $\begin{gathered} 53591.943 \\ 6 \end{gathered}$ | 63.2425 | 8.3651 | 8.418 |
|  | 42.2518 | 128.4973 | $\begin{gathered} 26448.555 \\ 3 \end{gathered}$ | 14.3762 | 21.3161 | 1240.7797 | $\begin{gathered} 53591.943 \\ 6 \end{gathered}$ | 63.2425 | 8.3651 | 8.418 |
| L59 | 42.3165 | 128.6971 | $\begin{gathered} 26572.120 \\ 7 \end{gathered}$ | 14.3986 | 21.3484 | 1244.6880 | $\begin{gathered} 53842.320 \\ 6 \end{gathered}$ | 63.3408 | 8.3819 | 8.435 |
|  | 42.3076 | 131.8528 | $\begin{gathered} 27189.835 \\ 8 \end{gathered}$ | 14.3896 | 21.3484 | 1273.6229 | $\begin{gathered} 55093.978 \\ 9 \end{gathered}$ | 64.8939 | 8.3149 | 8.162 |
|  | 43.0187 | 134.1058 | $\begin{gathered} 28607.634 \\ 1 \end{gathered}$ | 14.6355 | 21.7042 | 1318.0690 | $\begin{gathered} 57966.822 \\ 7 \end{gathered}$ | 66.0028 | 8.4990 | 8.343 |


tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

| Tower Elevation <br> ft | Gusset Area (perface) $\mathrm{ft}^{2}$ | Gusset Thickness <br> in | Gusset Grade Adjust. Factor <br> $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle <br> Stitch Bolt Spacing Horizontals in | Double Angle <br> Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { L12 84.5800- } \\ 84.3300 \end{gathered}$ |  |  | 1 | 1 | 0.914408 |  |  |  |
| $\begin{gathered} \text { L13 84.3300- } \\ 83.4200 \end{gathered}$ |  |  | 1 | 1 | 0.926528 |  |  |  |
| $\begin{gathered} \text { L14 83.4200- } \\ 83.1700 \end{gathered}$ |  |  | 1 | 1 | 0.877374 |  |  |  |
| $\begin{gathered} \text { L15 83.1700- } \\ 83.0000 \end{gathered}$ |  |  | 1 | 1 | 0.876149 |  |  |  |
| $\begin{gathered} \text { L16 83.0000- } \\ 82.7500 \end{gathered}$ |  |  | 1 | 1 | 0.895771 |  |  |  |
| $\begin{gathered} \mathrm{L} 1782.7500- \\ 77.7500 \end{gathered}$ |  |  | 1 | 1 | 0.913883 |  |  |  |
| $\begin{gathered} \text { L18 77.7500- } \\ 70.0000 \end{gathered}$ |  |  | 1 | 1 | 0.90949 |  |  |  |
| $\begin{gathered} \text { L19 70.0000- } \\ 69.0000 \end{gathered}$ |  |  | 1 | 1 | 0.921147 |  |  |  |
| $\begin{gathered} \text { L20 69.0000- } \\ 67.0800 \end{gathered}$ |  |  | 1 | 1 | 0.92817 |  |  |  |
| $\begin{gathered} \text { L21 67.0800- } \\ 66.8300 \end{gathered}$ |  |  | 1 | 1 | 0.926992 |  |  |  |
| $\begin{gathered} \text { L22 66.8300- } \\ 64.0800 \end{gathered}$ |  |  | 1 | 1 | 0.930891 |  |  |  |
| $\begin{gathered} \text { L23 64.0800- } \\ 63.8300 \end{gathered}$ |  |  | 1 | 1 | 0.999923 |  |  |  |
| $\begin{gathered} \text { L24 63.8300- } \\ 62.5000 \end{gathered}$ |  |  | 1 | 1 | 0.992599 |  |  |  |
| $\begin{gathered} \text { L25 62.5000- } \\ 62.2500 \end{gathered}$ |  |  | 1 | 1 | 0.913797 |  |  |  |
| $\begin{gathered} \text { L26 62.2500- } \\ 57.2500 \end{gathered}$ |  |  | 1 | 1 | 0.914277 |  |  |  |
| $\begin{gathered} \text { L27 57.2500- } \\ 53.5000 \end{gathered}$ |  |  | 1 | 1 | 0.92312 |  |  |  |
| $\begin{gathered} \text { L28 53.5000- } \\ 53.2500 \end{gathered}$ |  |  | 1 | 1 | 0.934453 |  |  |  |
| $\begin{gathered} \text { L29 53.2500- } \\ 52.5800 \end{gathered}$ |  |  | 1 | 1 | 0.944853 |  |  |  |
| $\begin{gathered} \text { L30 } 52.5800- \\ 52.3300 \end{gathered}$ |  |  | 1 | 1 | 0.917963 |  |  |  |
| $\begin{gathered} \text { L31 52.3300- } \\ 47.3300 \end{gathered}$ |  |  | 1 | 1 | 0.920611 |  |  |  |
| $\begin{gathered} \text { L32 } 47.3300- \\ 44.5800 \end{gathered}$ |  |  | 1 | 1 | 0.935467 |  |  |  |
| $\begin{gathered} \text { L33 } 44.5800- \\ 44.3300 \end{gathered}$ |  |  | 1 | 1 | 0.934343 |  |  |  |
| $\begin{gathered} \text { L34 44.3300- } \\ 41.9200 \end{gathered}$ |  |  | 1 | 1 | 0.937794 |  |  |  |
| $\begin{gathered} \text { L35 } 41.9200- \\ 41.6700 \end{gathered}$ |  |  | 1 | 1 | 0.941001 |  |  |  |
| $\begin{gathered} \text { L36 41.6700- } \\ 34.0800 \end{gathered}$ |  |  | 1 | 1 | 0.958134 |  |  |  |
| $\begin{gathered} \text { L37 34.0800- } \\ 34.0000 \end{gathered}$ |  |  | 1 | 1 | 0.950472 |  |  |  |
| $\begin{gathered} \text { L38 34.0000- } \\ 29.0000 \end{gathered}$ |  |  | 1 | 1 | 0.9595 |  |  |  |
| $\begin{gathered} \text { L39 } 29.0000- \\ 26.9200 \end{gathered}$ |  |  | 1 | 1 | 0.951546 |  |  |  |
| $\begin{gathered} \text { L40 } 26.9200- \\ 26.6700 \end{gathered}$ |  |  | 1 | 1 | 0.968284 |  |  |  |
| $\begin{gathered} \text { L41 } 26.6700- \\ 21.6700 \end{gathered}$ |  |  | 1 | 1 | 0.974397 |  |  |  |
| $\begin{gathered} \text { L42 } 21.6700- \\ 18.0000 \end{gathered}$ |  |  | 1 | 1 | 0.973558 |  |  |  |
| $\begin{gathered} \text { L43 18.0000- } \\ 17.7500 \end{gathered}$ |  |  | 1 | 1 | 0.947355 |  |  |  |
| $\begin{gathered} \text { L44 17.7500- } \\ 17.5000 \end{gathered}$ |  |  | 1 | 1 | 0.946327 |  |  |  |
| L45 17.5000- |  |  | 1 | 1 | 0.945303 |  |  |  |

tnxTower Report - version 8.1.1.0

| Tower Elevation <br> ft | Gusset Area (per face) $f t^{2}$ | Gusset Thickness in | Gusset Grade Adjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 17.2500 |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { L46 17.2500- } \\ 17.0800 \end{gathered}$ |  |  | 1 | 1 | 0.944608 |  |  |  |
| $\begin{gathered} \text { L47 17.0800- } \\ 16.8300 \end{gathered}$ |  |  | 1 | 1 | 0.961219 |  |  |  |
| $\begin{gathered} \text { L48 16.8300- } \\ 13.0000 \end{gathered}$ |  |  | 1 | 1 | 0.959721 |  |  |  |
| $\begin{gathered} \text { L49 13.0000- } \\ 12.7500 \end{gathered}$ |  |  | 1 | 1 | 0.944381 |  |  |  |
| $\begin{gathered} \text { L50 12.7500- } \\ 11.9200 \end{gathered}$ |  |  | 1 | 1 | 0.951948 |  |  |  |
| $\begin{gathered} \text { L51 } 11.9200- \\ 11.6700 \end{gathered}$ |  |  | 1 | 1 | 1.02595 |  |  |  |
| $\begin{gathered} \text { L52 11.6700- } \\ 6.6700 \end{gathered}$ |  |  | 1 | 1 | 1.0378 |  |  |  |
| $\begin{gathered} \text { L53 } 6.6700- \\ 6.5000 \end{gathered}$ |  |  | 1 | 1 | 1.03715 |  |  |  |
| $\begin{gathered} \text { L54 6.5000- } \\ 6.2500 \end{gathered}$ |  |  | 1 | 1 | 0.967827 |  |  |  |
| $\begin{gathered} \text { L55 6.2500- } \\ 3.7500 \end{gathered}$ |  |  | 1 | 1 | 0.971489 |  |  |  |
| $\begin{gathered} \text { L56 3.7500- } \\ 3.5000 \end{gathered}$ |  |  | 1 | 1 | 0.93422 |  |  |  |
| $\begin{gathered} \text { L57 3.5000- } \\ 3.0000 \end{gathered}$ |  |  | 1 | 1 | 0.943811 |  |  |  |
| $\begin{gathered} \text { L58 } 3.0000- \\ 2.7500 \end{gathered}$ |  |  | 1 | 1 | 0.91273 |  |  |  |
| $\begin{gathered} \text { L59 } 2.7500- \\ 0.0000 \end{gathered}$ |  |  | 1 | 1 | 0.881587 |  |  |  |

Feed Line/Linear Appurtenances - Entered As Round Or Flat

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En <br> d <br> Position | Width or Diamete $r$ in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\underset{\substack{3 / 8 *}}{\text { CU12PSM9P8XXX(1- }}$ | B | No | $\begin{aligned} & \text { Surface Ar } \\ & \text { (CaAa) } \end{aligned}$ | $\begin{gathered} 77.0000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.020 \end{aligned}$ | 1.4110 |  | 1.66 |
| 2" Flexible Conduit | B | No | Surface Ar (CaAa) | $\begin{gathered} 121.0000- \\ 0.0000 \end{gathered}$ | 4 | 4 | $\begin{aligned} & -0.200 \\ & -0.100 \end{aligned}$ | 2.0000 |  | 0.34 |
| LDF6-50A(1-1/4) | B | No | Surface Ar (CaAa) | $\begin{gathered} 121.0000- \\ 0.0000 \end{gathered}$ | 6 | 3 | $\begin{gathered} -0.100 \\ 0.000 \end{gathered}$ | 1.5500 |  | 0.60 |
| 2" Flexible Conduit | A | No | Surface Ar (CaAa) | $\begin{gathered} 97.0000- \\ 0.0000 \end{gathered}$ | 2 | 2 | $\begin{aligned} & 0.000 \\ & 0.100 \end{aligned}$ | 2.0000 |  | 0.34 |
|  | B | No | Surface Ar (CaAa) | $\begin{gathered} 87.0000- \\ 0.0000 \end{gathered}$ | 14 | 6 | $\begin{aligned} & -0.500 \\ & -0.350 \end{aligned}$ | 1.6600 |  | 2.40 |
| PL 0.75x4 | A | No | Surface Af (CaAa) | $\begin{gathered} 45.8300- \\ 15.8300 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | B | No | Surface Af (CaAa) | $\begin{gathered} 45.8300- \\ 15.8300 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | C | No | Surface Af (CaAa) | $\begin{gathered} 45.8300- \\ 15.8300 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.000 \\ & 0.000 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | A | No | Surface Af (CaAa) | $\begin{gathered} 68.2500- \\ 43.2500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.250 \\ & 0.250 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | B | No | Surface Af (CaAa) | $\begin{gathered} 68.2500- \\ 43.2500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.250 \\ & 0.250 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | C | No | Surface Af (CaAa) | $\begin{gathered} 68.2500- \\ 43.2500 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.250 \\ & 0.250 \end{aligned}$ | 4.0000 | 9.5000 | 0.00 |
| PL 0.75x4 | A | No | Surface Af | 85.8300 - | 1 | 1 | 0.000 | 4.0000 | 9.5000 | 0.00 |

tnxTower Report - version 8.1.1.0

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En d Position | Width or Diamete $r$ in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (CaAa) | 65.8300 |  |  | 0.000 |  |  |  |
| PL 0.75x4 | B | No | Surface Af | 85.8300 - | 1 | 1 | 0.000 | 4.0000 | 9.5000 | 0.00 |
|  |  |  | (CaAa) | 65.8300 |  |  | 0.000 |  |  |  |
| PL 0.75x4 | C | No | Surface Af | 85.8300 - | 1 | 1 | 0.000 | 4.0000 | 9.5000 | 0.00 |
|  |  |  | (CaAa) | 65.8300 |  |  | 0.000 |  |  |  |
| ** |  |  |  |  |  |  |  |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 15.5000 - | 1 | 1 | 0.000 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 0.0000 |  |  | 0.000 |  |  |  |
| (Area) CCl-65FP- | B | No | Surface Af | $15.5000-$ | 1 | 1 | 0.000 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 0.0000 |  |  | 0.000 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | $15.5000-$ | 1 | 1 | 0.000 | 6.0000 | 14.0000 | 0.00 |
| $060100(\mathrm{H})$ |  |  | (CaAa) | 0.0000 |  |  | 0.000 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | B | No | Surface Af | 20.7500 - | 1 | 1 | 0.500 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 9.4200 |  |  | 0.500 |  |  |  |
| (Area) CCl-65FP- | A | No | Surface Af | 20.7500 - | 1 | 1 | 0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 9.4200 |  |  | 0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | 20.7500 - | 1 | 1 | 0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 9.4200 |  |  | 0.250 |  |  |  |
| (Area) CCl-65FP- | B | No | Surface Af | 44.4200 - | 1 | 1 | 0.500 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 20.7500 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 29.4200 - | 1 | 1 | 0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 20.7500 |  |  | 0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | 29.4200 - | 1 | 1 | 0.250 | 6.0000 | 14.0000 | 0.00 |
|  |  |  |  |  |  |  |  |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 56.0000 - | 1 | 1 | 0.500 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 21.0000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | 56.0000 - | 1 | 1 | 0.500 | 6.0000 | 14.0000 | 0.00 |
| ${ }_{\text {** }}^{060100}(\mathrm{H})$ (CaAa) 21.0000 .500 |  |  |  |  |  |  |  |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 66.0800 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| 045100 (H) |  |  | (CaAa) | 56.0000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | 66.0800 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| 045100 (H) |  |  | (CaAa) | 56.0000 |  |  | 0.500 |  |  |  |
|  | B | No | Surface Af | 64.5000 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| $\underset{* *}{045100}(\mathrm{H})$ |  |  | (CaAa) | 44.5000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 91.5000 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| 045100 (H) |  |  | (CaAa) | 81.5000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | B | No | Surface Af | 91.5000 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| 045100 (H) |  |  | (CaAa) | 81.5000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | 91.5000 - | 1 | 1 | 0.500 | 4.5000 | 11.0000 | 0.00 |
| $045100(\mathrm{H})$ |  |  | (CaAa) | 81.5000 |  |  | 0.500 |  |  |  |
| (Area) CCI-65FP- | A | No | Surface Af | $9.2500-$ | 1 | 1 | 0.250 | 6.5000 | 15.5000 | 0.00 |
| $065125(\mathrm{H})$ |  |  | (CaAa) | 0.0000 |  |  | 0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | B | No | Surface Af | 20.7500 - | 1 | 1 | 0.250 | 6.5000 | 15.5000 | 0.00 |
| 065125 (H) |  |  | (CaAa) | 0.0000 |  |  | 0.250 |  |  |  |
| (Area) CCl-65FP- | A | No | Surface Af | 20.7500 - | 1 | 1 | 0.500 | 6.5000 | 15.5000 | 0.00 |
| 065125 (H) |  |  | (CaAa) | 0.0000 |  |  | 0.500 |  |  |  |
| (Area) CCl-65FP- | C | No | Surface Af | 20.7500 - | 1 | 1 | 0.500 | 6.5000 | 15.5000 | 0.00 |
| $065125(\mathrm{H})$ |  |  | (CaAa) | 0.0000 |  |  | 0.500 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 20.0000 - | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 0.0000 |  |  | -0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | B | No | Surface Af | $20.0000-$ | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 0.0000 |  |  | -0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | C | No | Surface Af | $20.0000-$ | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 0.0000 |  |  | -0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | A | No | Surface Af | 55.0800 - | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 20.0000 |  |  | -0.250 |  |  |  |
| (Area) $\mathrm{CCl}-65 \mathrm{FP}$ - | B | No | Surface Af | 55.0800 - | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 20.0000 |  |  | -0.250 |  |  |  |
| (Area) CCl-65FP- | C | No | Surface Af | 55.0800 - | 1 | 1 | -0.250 | 6.0000 | 14.0000 | 0.00 |
| 060100 (H) |  |  | (CaAa) | 20.0000 |  |  | -0.250 |  |  |  |
| (Area) CCl-65FP- | A | No | Surface Af | 85.1700 - | 1 | 1 | -0.250 | 4.5000 | 11.5000 | 0.00 |
| 045125 (H) |  |  | (CaAa) | 55.0800 |  |  | -0.250 |  |  |  |

tnxTower Report - version 8.1.1.0

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En $d$ Position | Width or Diamete $r$ in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { (Area) CCI-65FP- } \\ 045125(\mathrm{H}) \end{gathered}$ | B | No | Surface Af (CaAa) | $\begin{gathered} 85.1700- \\ 55.0800 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.250 \\ & -0.250 \end{aligned}$ | 4.5000 | 11.5000 | 0.00 |
| $\underset{* * * *}{\text { (Area) CCI-65FP- }} \underset{\substack{\text { (H) }}}{\text { O45125 }}$ | C | No | Surface Af (CaAa) | $\begin{gathered} 85.1700- \\ 55.0800 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.250 \\ & -0.250 \end{aligned}$ | 4.5000 | 11.5000 | 0.00 |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | Face or Leg | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number |  | $\begin{aligned} & C_{A} A_{A} \\ & f t^{2} / f t \end{aligned}$ | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { FB-L98B-002- } \\ & 75000(3 / 8) \end{aligned}$ | B | No | No | Inside Pole | $\begin{gathered} 121.0000- \\ 0.0000 \end{gathered}$ | 2 | No Ice | 0.0000 | 0.06 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.0000 | 0.06 |
|  |  |  |  |  |  |  | 1 " Ice | 0.0000 | 0.06 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 0.06 |
| WR-VG86STBRD(3/4) | B | No | No | Inside Pole | $\begin{gathered} 121.0000- \\ 0.0000 \end{gathered}$ | 8 | No Ice | 0.0000 | 0.58 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.0000 | 0.58 |
|  |  |  |  |  |  |  | 1 " Ice | 0.0000 | 0.58 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 0.58 |
| *** |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { HB158-U12S24- } \\ \text { 160-LI(1-7/8) } \end{gathered}$ | B | No | No | Inside Pole | $\begin{gathered} 109.0000- \\ 0.0000 \end{gathered}$ | 2 | No Ice | 0.0000 | 3.20 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.0000 | 3.20 |
|  |  |  |  |  |  |  | 1 " Ice | 0.0000 | 3.20 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 3.20 |
| $\begin{aligned} & \text { ATCB-B01- } \\ & 005(5 / 16) \end{aligned}$ | A | No | No | Inside Pole | $\begin{gathered} 97.0000- \\ 0.0000 \end{gathered}$ | 3 | No Ice | 0.0000 | 0.07 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.0000 | 0.07 |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.0000 | 0.07 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 0.07 |
| FSJ4-50B(1/2) | A | No | No | Inside Pole | 97.0000 - | 3 | No Ice | 0.0000 | 0.14 |
|  |  |  |  |  | 0.0000 |  | 1/2" Ice | 0.0000 | 0.14 |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.0000 | 0.14 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 0.14 |
| HB158-21U6S24-xxM_TMO(1-5/8) | C | No | No | Inside Pole | $\begin{gathered} 97.0000- \\ 0.0000 \end{gathered}$ | 3 | No Ice | 0.0000 | 2.50 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.0000 | 2.50 |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.0000 | 2.50 |
|  |  |  |  |  |  |  | 2" Ice | 0.0000 | 2.50 |
| **** |  |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio n \& Tower Elevation ft \& Face \& AR

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$

In Face $f^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& 130.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 125.0000 \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L2} \& 125.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 120.0000 \& B \& 0.000 \& 0.000 \& 1.265 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L3} \& 120.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 115.0000 \& B \& 0.000 \& 0.000 \& 6.325 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L4} \& 115.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 110.0000 \& B \& 0.000 \& 0.000 \& 6.325 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L5} \& 110.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 105.0000 \& B \& 0.000 \& 0.000 \& 6.325 \& 0.000 \& 0.07 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline L6 \& 105.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline
\end{tabular}

[^1]130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$t t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow{4}{*}{L7} \& \multirow[t]{2}{*}{100.0000} \& B \& 0.000 \& 0.000 \& 6.325 \& 0.000 \& 0.08 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>

\hline \& \multirow[t]{3}{*}{$$
\begin{gathered}
100.0000- \\
95.0000
\end{gathered}
$$} \& A \& 0.000 \& 0.000 \& 0.800 \& 0.000 \& 0.00 <br>

\hline \& \& B \& 0.000 \& 0.000 \& 6.325 \& 0.000 \& 0.08 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L8} \& \multirow[t]{3}{*}{95.0000-90.0000} \& A \& 0.000 \& 0.000 \& 3.125 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 7.450 \& 0.000 \& 0.08 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.125 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L9} \& \multirow[t]{3}{*}{90.0000-89.7500} \& A \& 0.000 \& 0.000 \& 0.287 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.504 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.188 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L10} \& \multirow[t]{3}{*}{89.7500-84.7500} \& A \& 0.000 \& 0.000 \& 6.785 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 13.351 \& 0.000 \& 0.16 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 4.785 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L11} \& \multirow[t]{3}{*}{84.7500-84.5800} \& A \& 0.000 \& 0.000 \& 0.436 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.753 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.368 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L12} \& \multirow[t]{3}{*}{84.5800-84.3300} \& A \& 0.000 \& 0.000 \& 0.642 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.107 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.542 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L13} \& \multirow[t]{3}{*}{84.3300-83.4200} \& A \& 0.000 \& 0.000 \& 2.336 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 4.029 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.972 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L14} \& \multirow[t]{3}{*}{83.4200-83.1700} \& A \& 0.000 \& 0.000 \& 0.642 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.107 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.542 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L15} \& \multirow[t]{3}{*}{83.1700-83.0000} \& A \& 0.000 \& 0.000 \& 0.436 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.753 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.368 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L16} \& \multirow[t]{3}{*}{83.0000-82.7500} \& A \& 0.000 \& 0.000 \& 0.642 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.107 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.542 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L17} \& \multirow[t]{3}{*}{82.7500-77.7500} \& A \& 0.000 \& 0.000 \& 10.021 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 19.326 \& 0.000 \& 0.25 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.021 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L18} \& \multirow[t]{3}{*}{77.7500-70.0000} \& A \& 0.000 \& 0.000 \& 14.079 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 29.490 \& 0.000 \& 0.40 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 10.979 \& 0.000 \& 0.06 <br>
\hline \multirow[t]{3}{*}{L19} \& \multirow[t]{3}{*}{70.0000-69.0000} \& A \& 0.000 \& 0.000 \& 1.817 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 3.819 \& 0.000 \& 0.05 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.417 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L20} \& \multirow[t]{3}{*}{69.0000-67.0800} \& A \& 0.000 \& 0.000 \& 4.268 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 8.112 \& 0.000 \& 0.10 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 3.500 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L21} \& \multirow[t]{3}{*}{67.0800-66.8300} \& A \& 0.000 \& 0.000 \& 0.621 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.121 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.521 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L22} \& \multirow[t]{3}{*}{66.8300-64.0800} \& A \& 0.000 \& 0.000 \& 7.163 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 11.483 \& 0.000 \& 0.14 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 6.063 \& 0.000 \& 0.02 <br>
\hline \multirow[t]{3}{*}{L23} \& \multirow[t]{3}{*}{64.0800-63.8300} \& A \& 0.000 \& 0.000 \& 0.642 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.142 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.542 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L24} \& \multirow[t]{3}{*}{63.8300-62.5000} \& A \& 0.000 \& 0.000 \& 3.414 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 6.076 \& 0.000 \& 0.07 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 2.882 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L25} \& \multirow[t]{3}{*}{62.5000-62.2500} \& A \& 0.000 \& 0.000 \& 0.642 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.142 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.542 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L26} \& \multirow[t]{3}{*}{62.2500-57.2500} \& A \& 0.000 \& 0.000 \& 12.833 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 22.844 \& 0.000 \& 0.26 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 10.833 \& 0.000 \& 0.04 <br>
\hline \multirow[t]{3}{*}{L27} \& \multirow[t]{3}{*}{57.2500-53.5000} \& A \& 0.000 \& 0.000 \& 10.645 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 17.528 \& 0.000 \& 0.19 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 9.145 \& 0.000 \& 0.03 <br>
\hline \multirow[t]{3}{*}{L28} \& \multirow[t]{3}{*}{53.5000-53.2500} \& A \& 0.000 \& 0.000 \& 0.767 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.205 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 0.667 \& 0.000 \& 0.00 <br>
\hline L29 \& 53.2500-52.5800 \& A \& 0.000 \& 0.000 \& 2.055 \& 0.000 \& 0.00 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& Face \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
f t^{2} \\
\hline
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2} \\
\hline
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow{4}{*}{L30} \& \multirow{4}{*}{52.5800-52.3300} \& B \& 0.000 \& 0.000 \& 3.229 \& 0.000 \& 0.03 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.787 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.767 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.205 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L31} \& \multirow{3}{*}{52.3300-47.3300} \& C \& 0.000 \& 0.000 \& 0.667 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 15.333 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 24.094 \& 0.000 \& 0.26 <br>
\hline \multirow{3}{*}{L32} \& \multirow{3}{*}{47.3300-44.5800} \& C \& 0.000 \& 0.000 \& 13.333 \& 0.000 \& 0.04 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 9.267 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 14.085 \& 0.000 \& 0.14 <br>
\hline \multirow{3}{*}{L33} \& \multirow{3}{*}{44.5800-44.3300} \& C \& 0.000 \& 0.000 \& 8.167 \& 0.000 \& 0.02 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.933 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.334 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L34} \& \multirow{3}{*}{44.3300-41.9200} \& C \& 0.000 \& 0.000 \& 0.833 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.111 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 12.936 \& 0.000 \& 0.12 <br>
\hline \multirow{3}{*}{L35} \& \multirow{3}{*}{41.9200-41.6700} \& C \& 0.000 \& 0.000 \& 7.147 \& 0.000 \& 0.02 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.767 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.267 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L36} \& \multirow{3}{*}{41.6700-34.0800} \& C \& 0.000 \& 0.000 \& 0.667 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 23.276 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 38.472 \& 0.000 \& 0.39 <br>
\hline \multirow{3}{*}{L37} \& \multirow{3}{*}{34.0800-34.0000} \& C \& 0.000 \& 0.000 \& 20.240 \& 0.000 \& 0.06 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.245 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.406 \& 0.000 \& 0.00 <br>
\hline \multirow{3}{*}{L38} \& \multirow{3}{*}{34.0000-29.0000} \& C \& 0.000 \& 0.000 \& 0.213 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 15.698 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 25.344 \& 0.000 \& 0.26 <br>
\hline \multirow{3}{*}{L39} \& \multirow{3}{*}{29.0000-26.9200} \& C \& 0.000 \& 0.000 \& 13.698 \& 0.000 \& 0.04 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 8.185 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 10.543 \& 0.000 \& 0.11 <br>
\hline \multirow{3}{*}{L40} \& \multirow{3}{*}{26.9200-26.6700} \& C \& 0.000 \& 0.000 \& 7.353 \& 0.000 \& 0.02 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.984 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.267 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L41} \& \multirow{3}{*}{26.6700-21.6700} \& C \& 0.000 \& 0.000 \& 0.884 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 19.675 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 25.344 \& 0.000 \& 0.26 <br>
\hline \multirow{3}{*}{L42} \& \multirow{3}{*}{21.6700-18.0000} \& C \& 0.000 \& 0.000 \& 17.675 \& 0.000 \& 0.04 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 14.661 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 21.460 \& 0.000 \& 0.19 <br>
\hline \multirow{3}{*}{L43} \& \multirow{3}{*}{18.0000-17.7500} \& C \& 0.000 \& 0.000 \& 13.193 \& 0.000 \& 0.03 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.026 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.527 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L44} \& \multirow{3}{*}{17.7500-17.5000} \& C \& 0.000 \& 0.000 \& 0.926 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.026 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.527 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L45} \& \multirow{3}{*}{17.5000-17.2500} \& C \& 0.000 \& 0.000 \& 0.926 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.026 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.527 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L46} \& \multirow{3}{*}{17.2500-17.0800} \& C \& 0.000 \& 0.000 \& 0.926 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.698 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.038 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L47} \& \multirow{3}{*}{17.0800-16.8300} \& C \& 0.000 \& 0.000 \& 0.630 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.026 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.527 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L48} \& \multirow{3}{*}{16.8300-13.0000} \& C \& 0.000 \& 0.000 \& 0.926 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 16.339 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 24.007 \& 0.000 \& 0.20 <br>
\hline \multirow{3}{*}{L49} \& \multirow{3}{*}{13.0000-12.7500} \& C \& 0.000 \& 0.000 \& 14.807 \& 0.000 \& 0.03 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.110 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.610 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L50} \& \multirow{3}{*}{12.7500-11.9200} \& C \& 0.000 \& 0.000 \& 1.010 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 3.685 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 5.346 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L51} \& \multirow{3}{*}{11.9200-11.6700} \& C \& 0.000 \& 0.000 \& 3.353 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.110 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.610 \& 0.000 \& 0.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 1.010 \& 0.000 \& 0.00 <br>
\hline L52 \& 11.6700-6.6700 \& A \& 0.000 \& 0.000 \& 21.979 \& 0.000 \& 0.01 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio $n$ \& Tower Elevation ft \& Face \& AR

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
f t^{2} \\
\hline
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{4}{*}{L53} \& \multirow{4}{*}{6.6700-6.5000} \& B \& 0.000 \& 0.000 \& 29.578 \& 0.000 \& 0.26 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 17.567 \& 0.000 \& 0.04 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 0.751 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.933 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L54} \& \multirow{3}{*}{6.5000-6.2500} \& C \& 0.000 \& 0.000 \& 0.524 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.105 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.371 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L55} \& \multirow{3}{*}{6.2500-3.7500} \& C \& 0.000 \& 0.000 \& 0.771 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 11.045 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 13.714 \& 0.000 \& 0.13 <br>
\hline \multirow{3}{*}{L56} \& \multirow{3}{*}{3.7500-3.5000} \& C \& 0.000 \& 0.000 \& 7.708 \& 0.000 \& 0.02 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.105 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.371 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L57} \& \multirow{3}{*}{3.5000-3.0000} \& C \& 0.000 \& 0.000 \& 0.771 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 2.209 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 2.743 \& 0.000 \& 0.03 <br>
\hline \multirow{3}{*}{L58} \& \multirow{3}{*}{3.0000-2.7500} \& C \& 0.000 \& 0.000 \& 1.542 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 1.105 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 1.371 \& 0.000 \& 0.01 <br>
\hline \multirow{4}{*}{L59} \& \multirow{4}{*}{2.7500-0.0000} \& C \& 0.000 \& 0.000 \& 0.771 \& 0.000 \& 0.00 <br>
\hline \& \& A \& 0.000 \& 0.000 \& 12.150 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 15.085 \& 0.000 \& 0.14 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 8.479 \& 0.000 \& 0.02 <br>
\hline
\end{tabular}

## Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
n
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Ice \\
Thickness in
\end{tabular} \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& 130.0000- \& A \& 1.946 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 125.0000 \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L2} \& 125.0000- \& A \& 1.938 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 120.0000 \& B \& \& 0.000 \& 0.000 \& 2.550 \& 0.000 \& 0.05 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L3} \& 120.0000- \& A \& 1.930 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 115.0000 \& B \& \& 0.000 \& 0.000 \& 12.732 \& 0.000 \& 0.23 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>

\hline \multirow[t]{3}{*}{L4} \& $$
115.0000-
$$ \& A \& 1.922 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>

\hline \& $$
110.0000
$$ \& B \& \& 0.000 \& 0.000 \& 12.711 \& 0.000 \& 0.23 <br>

\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L5} \& 110.0000- \& A \& 1.913 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 105.0000 \& B \& \& 0.000 \& 0.000 \& 12.689 \& 0.000 \& 0.25 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L6} \& 105.0000- \& A \& 1.904 \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 100.0000 \& B \& \& 0.000 \& 0.000 \& 12.666 \& 0.000 \& 0.26 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \multirow[t]{3}{*}{L7} \& 100.0000- \& A \& 1.894 \& 0.000 \& 0.000 \& 1.947 \& 0.000 \& 0.03 <br>
\hline \& 95.0000 \& B \& \& 0.000 \& 0.000 \& 12.642 \& 0.000 \& 0.25 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L8} \& 95.0000-90.0000 \& A \& 1.885 \& 0.000 \& 0.000 \& 6.293 \& 0.000 \& 0.09 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 14.055 \& 0.000 \& 0.27 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 1.437 \& 0.000 \& 0.06 <br>
\hline \multirow[t]{3}{*}{L9} \& 90.0000-89.7500 \& A \& 1.879 \& 0.000 \& 0.000 \& 0.482 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.870 \& 0.000 \& 0.02 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.239 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L10} \& 89.7500-84.7500 \& A \& 1.874 \& 0.000 \& 0.000 \& 11.224 \& 0.000 \& 0.15 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 22.827 \& 0.000 \& 0.47 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 6.382 \& 0.000 \& 0.12 <br>
\hline \multirow[t]{3}{*}{L11} \& 84.7500-84.5800 \& A \& 1.868 \& 0.000 \& 0.000 \& 0.695 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.249 \& 0.000 \& 0.03 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.530 \& 0.000 \& 0.01 <br>
\hline \multirow[t]{3}{*}{L12} \& 84.5800-84.3300 \& A \& 1.867 \& 0.000 \& 0.000 \& 1.022 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.837 \& 0.000 \& 0.04 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.780 \& 0.000 \& 0.01 <br>
\hline L13 \& 84.3300-83.4200 \& A \& 1.866 \& 0.000 \& 0.000 \& 3.718 \& 0.000 \& 0.05 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Sectio n \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Ice \\
Thickness in
\end{tabular} \& \(A_{R}\)

$t^{2}$ \& $A_{F}$

$f t^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& $C_{A} A_{A}$

Out Face
$f t^{2}$ \& Weight
K <br>
\hline \multirow{4}{*}{L14} \& \multirow{5}{*}{83.4200-83.1700} \& B \& \multirow{4}{*}{1.865} \& 0.000 \& 0.000 \& 6.684 \& 0.000 \& 0.14 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 2.839 \& 0.000 \& 0.04 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.021 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.836 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L15} \& \& C \& \& 0.000 \& 0.000 \& 0.780 \& 0.000 \& 0.01 <br>
\hline \& \multirow[t]{2}{*}{83.1700-83.0000} \& A \& 1.864 \& 0.000 \& 0.000 \& 0.694 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.248 \& 0.000 \& 0.03 <br>
\hline \multirow{3}{*}{L16} \& \multirow{3}{*}{83.0000-82.7500} \& C \& \& 0.000 \& 0.000 \& 0.530 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.864 \& 0.000 \& 0.000 \& 1.021 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.836 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L17} \& \multirow{3}{*}{82.7500-77.7500} \& C \& \& 0.000 \& 0.000 \& 0.780 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.858 \& 0.000 \& 0.000 \& 16.816 \& 0.000 \& 0.21 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 33.092 \& 0.000 \& 0.70 <br>
\hline \multirow{3}{*}{L18} \& \multirow{3}{*}{77.7500-70.0000} \& C \& \& 0.000 \& 0.000 \& 11.993 \& 0.000 \& 0.18 <br>
\hline \& \& A \& 1.843 \& 0.000 \& 0.000 \& 24.136 \& 0.000 \& 0.30 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 52.872 \& 0.000 \& 1.11 <br>
\hline \multirow{3}{*}{L19} \& \multirow{3}{*}{70.0000-69.0000} \& C \& \& 0.000 \& 0.000 \& 16.691 \& 0.000 \& 0.25 <br>
\hline \& \& A \& 1.831 \& 0.000 \& 0.000 \& 3.114 \& 0.000 \& 0.04 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 6.871 \& 0.000 \& 0.14 <br>
\hline \multirow{3}{*}{L20} \& \multirow{3}{*}{69.0000-67.0800} \& C \& \& 0.000 \& 0.000 \& 2.154 \& 0.000 \& 0.03 <br>
\hline \& \& A \& 1.828 \& 0.000 \& 0.000 \& 7.168 \& 0.000 \& 0.09 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 14.362 \& 0.000 \& 0.29 <br>
\hline \multirow{3}{*}{L21} \& \multirow{3}{*}{67.0800-66.8300} \& C \& \& 0.000 \& 0.000 \& 5.331 \& 0.000 \& 0.08 <br>
\hline \& \& A \& 1.825 \& 0.000 \& 0.000 \& 1.034 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.970 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L22} \& \multirow{3}{*}{66.8300-64.0800} \& C \& \& 0.000 \& 0.000 \& 0.795 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.820 \& 0.000 \& 0.000 \& 11.464 \& 0.000 \& 0.14 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 20.313 \& 0.000 \& 0.41 <br>
\hline \multirow{3}{*}{L23} \& \multirow{3}{*}{64.0800-63.8300} \& C \& \& 0.000 \& 0.000 \& 8.837 \& 0.000 \& 0.13 <br>
\hline \& \& A \& 1.816 \& 0.000 \& 0.000 \& 1.013 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.987 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L24} \& \multirow{3}{*}{63.8300-62.5000} \& C \& \& 0.000 \& 0.000 \& 0.774 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.814 \& 0.000 \& 0.000 \& 5.385 \& 0.000 \& 0.07 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 10.568 \& 0.000 \& 0.21 <br>
\hline \multirow{3}{*}{L25} \& \multirow{3}{*}{62.5000-62.2500} \& C \& \& 0.000 \& 0.000 \& 4.117 \& 0.000 \& 0.06 <br>
\hline \& \& A \& 1.812 \& 0.000 \& 0.000 \& 1.012 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.986 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L26} \& \multirow{3}{*}{62.2500-57.2500} \& C \& \& 0.000 \& 0.000 \& 0.774 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.804 \& 0.000 \& 0.000 \& 20.208 \& 0.000 \& 0.25 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 39.650 \& 0.000 \& 0.77 <br>
\hline \multirow{3}{*}{L27} \& \multirow{3}{*}{57.2500-53.5000} \& C \& \& 0.000 \& 0.000 \& 15.453 \& 0.000 \& 0.22 <br>
\hline \& \& A \& 1.790 \& 0.000 \& 0.000 \& 16.530 \& 0.000 \& 0.19 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 30.054 \& 0.000 \& 0.58 <br>
\hline \multirow{3}{*}{L28} \& \multirow{3}{*}{53.5000-53.2500} \& C \& \& 0.000 \& 0.000 \& 12.977 \& 0.000 \& 0.17 <br>
\hline \& \& A \& 1.784 \& 0.000 \& 0.000 \& 1.171 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.037 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L29} \& \multirow{3}{*}{53.2500-52.5800} \& C \& \& 0.000 \& 0.000 \& 0.934 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.782 \& 0.000 \& 0.000 \& 3.137 \& 0.000 \& 0.04 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 5.458 \& 0.000 \& 0.10 <br>
\hline \multirow{3}{*}{L30} \& \multirow{3}{*}{52.5800-52.3300} \& C \& \& 0.000 \& 0.000 \& 2.503 \& 0.000 \& 0.03 <br>
\hline \& \& A \& 1.781 \& 0.000 \& 0.000 \& 1.170 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.036 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L31} \& \multirow{3}{*}{52.3300-47.3300} \& C \& \& 0.000 \& 0.000 \& 0.934 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.771 \& 0.000 \& 0.000 \& 23.362 \& 0.000 \& 0.26 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 40.649 \& 0.000 \& 0.77 <br>
\hline \multirow{3}{*}{L32} \& \multirow{3}{*}{47.3300-44.5800} \& C \& \& 0.000 \& 0.000 \& 18.648 \& 0.000 \& 0.24 <br>
\hline \& \& A \& 1.757 \& 0.000 \& 0.000 \& 14.088 \& 0.000 \& 0.16 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 23.569 \& 0.000 \& 0.43 <br>
\hline \multirow{3}{*}{L33} \& \multirow{3}{*}{44.5800-44.3300} \& C \& \& 0.000 \& 0.000 \& 11.505 \& 0.000 \& 0.14 <br>
\hline \& \& A \& 1.751 \& 0.000 \& 0.000 \& 1.418 \& 0.000 \& 0.02 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.213 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L34} \& \multirow{3}{*}{44.3300-41.9200} \& C \& \& 0.000 \& 0.000 \& 1.184 \& 0.000 \& 0.01 <br>
\hline \& \& A \& 1.746 \& 0.000 \& 0.000 \& 12.306 \& 0.000 \& 0.14 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 21.198 \& 0.000 \& 0.38 <br>
\hline \multirow{4}{*}{L35} \& \multirow{3}{*}{41.9200-41.6700} \& C \& \& 0.000 \& 0.000 \& 10.049 \& 0.000 \& 0.12 <br>
\hline \& \& A \& 1.741 \& 0.000 \& 0.000 \& 1.162 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.083 \& 0.000 \& 0.04 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.928 \& 0.000 \& 0.01 <br>
\hline L36 \& 41.6700-34.0800 \& A \& 1.723 \& 0.000 \& 0.000 \& 35.154 \& 0.000 \& 0.38 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
\(n\)
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Ice Thickness in \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow{4}{*}{L37} \& \multirow{4}{*}{34.0800-34.0000} \& B \& \multirow{4}{*}{1.705} \& 0.000 \& 0.000 \& 63.037 \& 0.000 \& 1.16 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 28.088 \& 0.000 \& 0.35 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 0.371 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.664 \& 0.000 \& 0.01 <br>
\hline \multirow{3}{*}{L38} \& \multirow{3}{*}{34.0000-29.0000} \& C \& \multirow{3}{*}{1.692} \& 0.000 \& 0.000 \& 0.296 \& 0.000 \& 0.00 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 23.465 \& 0.000 \& 0.25 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 41.283 \& 0.000 \& 0.75 <br>
\hline \multirow{3}{*}{L39} \& \multirow{3}{*}{29.0000-26.9200} \& C \& \multirow{3}{*}{1.672} \& 0.000 \& 0.000 \& 18.850 \& 0.000 \& 0.23 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 11.720 \& 0.000 \& 0.13 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 17.109 \& 0.000 \& 0.31 <br>
\hline \multirow{3}{*}{L40} \& \multirow{3}{*}{26.9200-26.6700} \& C \& \multirow{3}{*}{1.665} \& 0.000 \& 0.000 \& 9.810 \& 0.000 \& 0.12 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.407 \& 0.000 \& 0.02 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.054 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L41} \& \multirow{3}{*}{26.6700-21.6700} \& C \& \multirow{3}{*}{1.648} \& 0.000 \& 0.000 \& 1.178 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 28.056 \& 0.000 \& 0.30 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 40.940 \& 0.000 \& 0.74 <br>
\hline \multirow{3}{*}{L42} \& \multirow{3}{*}{21.6700-18.0000} \& C \& \multirow{3}{*}{1.616} \& 0.000 \& 0.000 \& 23.497 \& 0.000 \& 0.28 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 20.613 \& 0.000 \& 0.22 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 33.192 \& 0.000 \& 0.57 <br>
\hline \multirow{3}{*}{L43} \& \multirow{3}{*}{18.0000-17.7500} \& C \& \multirow{3}{*}{1.599} \& 0.000 \& 0.000 \& 17.296 \& 0.000 \& 0.20 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.433 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.330 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L44} \& \multirow{3}{*}{17.7500-17.5000} \& C \& \multirow{3}{*}{1.597} \& 0.000 \& 0.000 \& 1.208 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.433 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.329 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L45} \& \multirow{3}{*}{17.5000-17.2500} \& C \& \multirow{3}{*}{1.594} \& 0.000 \& 0.000 \& 1.208 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.432 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.328 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L46} \& \multirow{3}{*}{17.2500-17.0800} \& C \& \multirow{3}{*}{1.592} \& 0.000 \& 0.000 \& 1.208 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 0.974 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.583 \& 0.000 \& 0.03 <br>
\hline \multirow{3}{*}{L47} \& \multirow{3}{*}{17.0800-16.8300} \& C \& \multirow{3}{*}{1.590} \& 0.000 \& 0.000 \& 0.821 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.431 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.326 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L48} \& \multirow{3}{*}{16.8300-13.0000} \& C \& \multirow{3}{*}{1.570} \& 0.000 \& 0.000 \& 1.207 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 22.214 \& 0.000 \& 0.23 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 35.874 \& 0.000 \& 0.60 <br>
\hline \multirow{3}{*}{L49} \& \multirow{3}{*}{13.0000-12.7500} \& C \& \multirow{3}{*}{1.547} \& 0.000 \& 0.000 \& 18.796 \& 0.000 \& 0.21 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.490 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.378 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L50} \& \multirow{3}{*}{12.7500-11.9200} \& C \& \multirow{3}{*}{1.541} \& 0.000 \& 0.000 \& 1.268 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 4.942 \& 0.000 \& 0.05 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 7.885 \& 0.000 \& 0.13 <br>
\hline \multirow{3}{*}{L51} \& \multirow{3}{*}{11.9200-11.6700} \& C \& \multirow{3}{*}{1.534} \& 0.000 \& 0.000 \& 4.208 \& 0.000 \& 0.05 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.487 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.372 \& 0.000 \& 0.04 <br>
\hline \multirow{3}{*}{L52} \& \multirow{3}{*}{11.6700-6.6700} \& C \& \multirow{3}{*}{1.495} \& 0.000 \& 0.000 \& 1.266 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 29.344 \& 0.000 \& 0.29 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 44.089 \& 0.000 \& 0.73 <br>
\hline \multirow{3}{*}{L53} \& \multirow{3}{*}{6.6700-6.5000} \& C \& \multirow{3}{*}{1.447} \& 0.000 \& 0.000 \& 22.149 \& 0.000 \& 0.24 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 0.996 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 1.402 \& 0.000 \& 0.02 <br>
\hline \multirow{3}{*}{L54} \& \multirow{3}{*}{6.5000-6.2500} \& C \& \multirow{3}{*}{1.442} \& 0.000 \& 0.000 \& 0.664 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.463 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.060 \& 0.000 \& 0.03 <br>
\hline \multirow{3}{*}{L55} \& \multirow{3}{*}{6.2500-3.7500} \& C \& \multirow{3}{*}{1.408} \& 0.000 \& 0.000 \& 0.976 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 14.557 \& 0.000 \& 0.13 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 20.474 \& 0.000 \& 0.34 <br>
\hline \multirow{3}{*}{L56} \& \multirow{3}{*}{3.7500-3.5000} \& C \& \multirow{3}{*}{1.363} \& 0.000 \& 0.000 \& 9.712 \& 0.000 \& 0.10 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.446 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.031 \& 0.000 \& 0.03 <br>
\hline \multirow{3}{*}{L57} \& \multirow{3}{*}{3.5000-3.0000} \& C \& \multirow{3}{*}{1.348} \& 0.000 \& 0.000 \& 0.966 \& 0.000 \& 0.01 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 2.886 \& 0.000 \& 0.03 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 4.052 \& 0.000 \& 0.06 <br>
\hline \multirow{3}{*}{L58} \& \multirow{3}{*}{3.0000-2.7500} \& C \& \multirow{3}{*}{1.332} \& 0.000 \& 0.000 \& 1.928 \& 0.000 \& 0.02 <br>
\hline \& \& A \& \& 0.000 \& 0.000 \& 1.440 \& 0.000 \& 0.01 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 2.020 \& 0.000 \& 0.03 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.962 \& 0.000 \& 0.01 <br>
\hline L59 \& 2.7500-0.0000 \& A \& 1.237 \& 0.000 \& 0.000 \& 15.611 \& 0.000 \& 0.13 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Sectio $n$ \& Tower Elevation ft \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Ice
Thickness
in \& AR

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $\mathrm{ft}^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multicolumn{2}{|l|}{\multirow[t]{2}{*}{}} \& B \& \& 0.000 \& 0.000 \& 21.840 \& 0.000 \& 0.34 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 10.449 \& 0.000 \& 0.10 <br>
\hline
\end{tabular}

## Feed Line Center of Pressure

| Section | Elevation ft | $C P_{X}$ in | $C P_{z}$ in | $\begin{gathered} C P_{x} \\ \text { Ice } \\ \text { in } \end{gathered}$ | $\begin{gathered} C P_{z} \\ \text { Ice } \\ \text { in } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $\begin{aligned} & 130.0000- \\ & 125.0000 \end{aligned}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L2 | $\begin{aligned} & 125.0000- \\ & 120.0000 \end{aligned}$ | 1.1072 | -1.0467 | 1.1637 | -1.0768 |
| L3 | $\begin{aligned} & 120.0000- \\ & 115.0000 \end{aligned}$ | 3.0857 | -2.9183 | 2.6045 | -2.4110 |
| L4 | $\begin{aligned} & 115.0000- \\ & 110.0000 \end{aligned}$ | 3.1879 | -3.0164 | 2.7443 | -2.5418 |
| L5 | $\begin{aligned} & 110.0000- \\ & 105.0000 \end{aligned}$ | 3.2842 | -3.1089 | 2.8789 | -2.6678 |
| L6 | $\begin{aligned} & 105.0000- \\ & 100.0000 \end{aligned}$ | 3.3712 | -3.1923 | 3.0067 | -2.7875 |
| L7 | 100.0000-95.0000 | 2.8025 | -3.4276 | 2.3409 | -2.9652 |
| L8 | 95.0000-90.0000 | 1.6763 | -3.0849 | 1.3459 | -2.8494 |
| L9 | 90.0000-89.7500 | 1.2241 | -2.2540 | 1.1232 | -2.3791 |
| L10 | 89.7500-84.7500 | 1.1866 | -2.8061 | 1.0914 | -2.8275 |
| L11 | 84.7500-84.5800 | 0.8513 | -2.4236 | 0.8302 | -2.5157 |
| L12 | 84.5800-84.3300 | 0.8531 | -2.4286 | 0.8319 | -2.5209 |
| L13 | 84.3300-83.4200 | 0.8570 | -2.4398 | 0.8361 | -2.5334 |
| L14 | 83.4200-83.1700 | 0.8617 | -2.4529 | 0.8407 | -2.5474 |
| L15 | 83.1700-83.0000 | 0.8632 | -2.4570 | 0.8423 | -2.5519 |
| L16 | 83.0000-82.7500 | 0.8641 | -2.4594 | 0.8434 | -2.5553 |
| L17 | 82.7500-77.7500 | 1.0413 | -2.9629 | 0.9659 | -2.9256 |
| L18 | 77.7500-70.0000 | 1.3031 | -3.3353 | 1.3269 | -3.2817 |
| L19 | 70.0000-69.0000 | 1.3392 | -3.3924 | 1.3786 | -3.3486 |
| L20 | 69.0000-67.0800 | 1.1928 | -3.0208 | 1.2597 | -3.0601 |
| L21 | 67.0800-66.8300 | 1.1126 | -2.8171 | 1.1965 | -2.9064 |
| L22 | 66.8300-64.0800 | 0.9296 | -3.5664 | 1.1007 | -3.4596 |
| L23 | 64.0800-63.8300 | 1.1126 | -2.8159 | 1.2678 | -2.8401 |
| L24 | 63.8300-62.5000 | 1.1190 | -2.8316 | 1.2749 | -2.8561 |
| L25 | 62.5000-62.2500 | 1.1256 | -2.8479 | 1.2824 | -2.8726 |
| L26 | 62.2500-57.2500 | 1.1465 | -2.8998 | 1.3060 | -2.9254 |
| L27 | 57.2500-53.5000 | 1.0390 | -3.0931 | 1.2212 | -3.1418 |
| L28 | 53.5000-53.2500 | 0.9662 | -3.1146 | 1.1645 | -3.2042 |
| L29 | 53.2500-52.5800 | 0.9690 | -3.1233 | 1.1679 | -3.2139 |
| L30 | 52.5800-52.3300 | 0.9718 | -3.1324 | 1.1715 | -3.2238 |
| L31 | 52.3300-47.3300 | 0.9873 | -3.1823 | 1.1912 | -3.2790 |
| L32 | 47.3300-44.5800 | 0.9443 | -3.0437 | 1.1496 | -3.1661 |
| L33 | 44.5800-44.3300 | 0.8307 | -3.0949 | 1.0328 | -3.2431 |
| L34 | 44.3300-41.9200 | 1.0534 | -2.6585 | 1.2225 | -2.9659 |
| L35 | 41.9200-41.6700 | 1.1324 | -2.8576 | 1.3055 | -3.1671 |
| L36 | 41.6700-34.0800 | 1.1571 | -2.9187 | 1.3353 | -3.2395 |
| L37 | 34.0800-34.0000 | 1.1655 | -2.9395 | 1.3459 | -3.2648 |
| L38 | 34.0000-29.0000 | 1.0740 | -2.9928 | 1.2855 | -3.3170 |
| L39 | 29.0000-26.9200 | 0.0532 | -3.1829 | 0.5239 | -3.4557 |
| L40 | 26.9200-26.6700 | 0.0531 | -3.2030 | 0.5263 | -3.4782 |
| L41 | 26.6700-21.6700 | 0.0529 | -3.2466 | 0.5311 | -3.5273 |
| L42 | 21.6700-18.0000 | 0.9019 | -2.7631 | 1.2097 | -3.2407 |
| L43 | 18.0000-17.7500 | 1.1229 | -2.7268 | 1.3883 | -3.2422 |
| L44 | 17.7500-17.5000 | 1.1243 | -2.7302 | 1.3899 | -3.2461 |
| L45 | 17.5000-17.2500 | 1.1257 | -2.7335 | 1.3915 | -3.2500 |
| L46 | 17.2500-17.0800 | 1.1269 | -2.7363 | 1.3929 | -3.2532 |
| L47 | 17.0800-16.8300 | 1.1279 | -2.7387 | 1.3940 | -3.2560 |
| L48 | 16.8300-13.0000 | 1.1080 | -2.6899 | 1.3920 | -3.2524 |
| L49 | 13.0000-12.7500 | 1.0872 | -2.6390 | 1.3764 | -3.2175 |
| L50 | 12.7500-11.9200 | 1.0901 | -2.6457 | 1.3794 | -3.2249 |
| L51 | 11.9200-11.6700 | 1.0926 | -2.6516 | 1.3819 | -3.2313 |

tnxTower Report - version 8.1.1.0

| Section | Elevation | $C P_{x}$ | $C P_{z}$ | $C P_{x}$ <br> Ice <br> in | $C P_{z}$ <br> Ice <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lt | in | in | -4.3385 |  |  |
| L53 | $11.6700-6.6700$ | 1.5228 | -4.0427 | 1.7287 | -4.3 .0345 |
| L54 | $6.6700-6.5000$ | 1.9116 | -5.4011 | -5.3963 |  |
| L55 | $6.5000-6.2500$ | 1.9139 | -5.4075 | 2.0365 | -5.4023 |
| L56 | $6.2500-3.7500$ | 1.9263 | -5.4417 | 2.0467 | -5.4347 |
| L57 | $3.7500-3.5000$ | 1.9390 | -5.4767 | 2.0561 | -5.4668 |
| L58 | $3.5000-3.0000$ | 1.9423 | -5.4859 | 2.0582 | -5.4749 |
| L59 | $3.0000-2.7500$ | 1.9456 | -5.4952 | 2.0602 | -5.4830 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | 3 | 2" Flexible Conduit | $\begin{array}{r} \hline 120.00- \\ 121.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 120.00- \\ 121.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 3 | 2" Flexible Conduit | $\begin{array}{r} 115.00- \\ 120.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 115.00- \\ 120.00 \end{array}$ | 1.0000 | 1.0000 |
| L4 | 3 | 2" Flexible Conduit | $\begin{array}{r} 110.00- \\ 115.00 \end{array}$ | 1.0000 | 1.0000 |
| L4 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 110.00- \\ 115.00 \end{array}$ | 1.0000 | 1.0000 |
| L5 | 3 | 2" Flexible Conduit | $\begin{array}{r} 105.00- \\ 110.00 \end{array}$ | 1.0000 | 1.0000 |
| L5 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 105.00- \\ 110.00 \end{array}$ | 1.0000 | 1.0000 |
| L6 | 3 | 2" Flexible Conduit | $\begin{array}{r} 100.00- \\ 105.00 \end{array}$ | 1.0000 | 1.0000 |
| L6 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 100.00- \\ 105.00 \end{array}$ | 1.0000 | 1.0000 |
| L7 | 3 | 2" Flexible Conduit | $\begin{aligned} & 95.00- \\ & 100.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L7 | 4 | LDF6-50A(1-1/4) | $\begin{aligned} & 95.00- \\ & 100.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L7 | 10 | 2" Flexible Conduit | $\begin{array}{r} 95.00- \\ 97.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 3 | 2" Flexible Conduit | $\begin{array}{r} 90.00- \\ 95.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 90.00- \\ 95.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 10 | 2" Flexible Conduit | $\begin{array}{r} 90.00- \\ 95.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 90.00- \\ 91.50 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 48 | (Area) CCI-65FP-045100 | $\begin{array}{r} 90.00- \\ 91.50 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 90.00- \\ 91.50 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 3 | 2" Flexible Conduit | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 10 | 2" Flexible Conduit | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 47 | (Area) CCI-65FP-045100 | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L9 | 48 | (Area) CCI-65FP-045100 | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 3 | 2" Flexible Conduit | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 4 | LDF6-50A(1-1/4) | $84.75$ $89.75$ | 1.0000 | 1.0000 |
| L10 | 10 | 2" Flexible Conduit | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 84.75- \\ 87.00 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 25 | PL 0.75x4 | $\begin{array}{r} 84.75- \\ 85.83 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 26 | PL 0.75x4 | $\begin{array}{r} 84.75- \\ 85.83 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 27 | PL 0.75x4 | $\begin{array}{r} 84.75- \\ 85.83 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 47 | (Area) CCl -65FP-045100 | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 3 | 2" Flexible Conduit | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 10 | 2" Flexible Conduit | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 25 | PL 0.75x4 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 26 | PL 0.75x4 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 27 | PL 0.75x4 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 3 | 2" Flexible Conduit | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 10 | 2" Flexible Conduit | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 25 | PL 0.75x4 | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 26 | PL 0.75x4 | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 27 | PL 0.75x4 | $84.33-$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L12 | 47 | (Area) CCl-65FP-045100 | 84.58 | 1.0000 | 1.0000 |
|  |  |  | 84.33 - |  |  |
| L12 | 48 | (Area) CCl-65FP-045100 | 84.58 $84.33-$ | 1.0000 | 1.0000 |
|  |  | (H) | 84.58 |  |  |
| L12 | 49 | (Area) CCl-65FP-045100 | 84.33 - | 1.0000 | 1.0000 |
|  |  |  | 84.58 |  |  |
| L12 | 62 | (Area) CCl -65FP-045125 | $84.33-$ 84.58 | 1.0000 | 1.0000 |
|  |  |  | 84.58 $84.33-$ |  |  |
| L12 | 63 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-045125$ | 84.58 | 1.0000 | 1.0000 |
| L12 | 64 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-045125$ | 84.33 - | 1.0000 | 1.0000 |
|  |  |  | 84.58 |  |  |
| L13 | 3 | 2" Flexible Conduit | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 $83.42-$ |  |  |
| L13 | 4 | LDF6-50A(1-1/4) | $83.42-$ 84.33 | 1.0000 | 1.0000 |
| L13 | 10 | 2" Flexible Conduit | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 16 | HCS 6X12 4AWG(1-5/8) | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 25 | PL 0.75x4 | $83.42-$ 84.33 | 1.0000 | 1.0000 |
| L13 | 26 | PL 0.75x4 | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 27 | PL 0.75x4 | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 47 | (Area) CCl-65FP-045100 | 83.42 - | 1.0000 | 1.0000 |
|  |  | (H) | 84.33 |  |  |
| L13 | 48 | (Area) CCl -65FP-045100 | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 49 | (Area) CCl-65FP-045100 | 83.42 - | 1.0000 | 1.0000 |
|  |  | (H) | 84.33 $83.42-$ |  |  |
| L13 | 62 | (Area) CCI-65FP-045125 | 83.42 - | 1.0000 | 1.0000 |
| L13 | 63 | (Area) CCl -65FP-045125 | 83.42 - | 1.0000 | 1.0000 |
|  |  |  | 84.33 |  |  |
| L13 | 64 | (Area) CCI-65FP-045125 | 83.42 - | 1.0000 | 1.0000 |
|  | 3 |  | 84.33 |  |  |
| L14 |  | 2" Flexible Conduit | 83.17 - | 1.0000 | 1.0000 |
| L14 | 4 | LDF6-50A(1-1/4) | 83.42 $83.17-$ |  | 1.0000 |
|  |  |  | 83.42 | 1.0000 |  |
| L14 | 10 | 2" Flexible Conduit | 83.17 - | 1.0000 | 1.0000 |
|  |  |  | 83.42 |  |  |
| L14 | 16 | HCS 6X12 4AWG(1-5/8) | 83.17 - | 1.0000 | 1.0000 |
|  |  |  | 83.42 |  |  |
| L14 | 25 | PL 0.75x4 | 83.17 - | 1.0000 | 1.0000 |
|  | 26 |  | 83.42 |  |  |
| L14 |  | PL 0.75x4 | 83.17 - | 1.0000 | 1.0000 |
|  |  |  | 83.42 |  |  |
| L14 | 27 | PL 0.75x4 | 83.17 - | 1.0000 | 1.0000 |
|  | 47 |  | 83.42 |  |  |
| L14 |  | (Area) CCI-65FP-045100 | 83.17 - | 1.0000 | 1.0000 |
|  |  | (H) | 83.42 |  |  |
| L14 | 48 | (Area) CCl-65FP-045100 | 83.17 - | 1.0000 | 1.0000 |
|  |  |  | 83.42 |  |  |
| L14 | 49 | (Area) CCl-65FP-045100 | 83.17 - | 1.0000 | 1.0000 |
|  |  | (H) | 83.42 |  |  |
| L14 | 62 | (Area) CCI-65FP-045125 | 83.17 - | 1.0000 | 1.0000 |
|  |  | (H) | 83.42 |  |  |
| L14 | 63 | (Area) CCl-65FP-045125 | 83.17 - | 1.0000 | 1.0000 |
| L14 |  |  | 83.42 |  |  |
|  | 64 | (Area) CCl -65FP-045125 | 83.17 - | 1.0000 | 1.0000 |
| L15 |  |  | 83.42 |  |  |
|  | 3 | 2" Flexible Conduit | $83.00-17$ | 1.0000 | 1.0000 |
| L15 | 4 | LDF6-50A(1-1/4) | 83.17 | 1.0000 | 1.0000 |
|  |  |  | 83.17 |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L15 | 10 | 2" Flexible Conduit | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 25 | PL $0.75 \times 4$ | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 26 | PL 0.75x4 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 27 | PL 0.75x4 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 48 | (Area) CCl-65FP-045100 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 64 | (Area) CCl-65FP-045125 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 3 | 2" Flexible Conduit | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 10 | 2" Flexible Conduit | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 25 | PL 0.75x4 | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 26 | PL 0.75x4 | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 27 | PL 0.75x4 | $82.75-$ 83.00 | 1.0000 | 1.0000 |
| L16 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 63 | (Area) CCl-65FP-045125 <br> (H) | $82.75-$ 83.00 | 1.0000 | 1.0000 |
| L16 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 3 | 2" Flexible Conduit | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 10 | 2" Flexible Conduit | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 25 | PL 0.75x4 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 26 | PL 0.75x4 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 27 | PL 0.75x4 | $77.75-$ 82.75 | 1.0000 | 1.0000 |
| L17 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 81.50- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 81.50- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 81.50- \\ 82.75 \end{array}$ | 1.0000 | 1.0000 |
| L17 | 62 | (Area) CCl-65FP-045125 | $77.75-$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (H) | 82.75 |  |  |
| L17 | 63 | (Area) CCI-65FP-045125 | $77.75-$ | 1.0000 | 1.0000 |
|  |  | (H) | 82.75 |  |  |
| L17 | 64 | (Area) CCI-65FP-045125 | $77.75-$ | 1.0000 | 1.0000 |
|  |  | (H) | 82.75 |  |  |
| L18 | 1 | CU12PSM9P8XXX(1-3/8) | $70.00-1$ | 1.0000 | 1.0000 |
| L18 | 3 | 2" Flexible Conduit | $70.00-$ | 1.0000 | 1.0000 |
|  |  |  | 77.75 |  |  |
| L18 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 70.00- \\ 7775 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 10 | 2" Flexible Conduit | 77.75 $70.00-$ | 1.0000 | 1.0000 |
|  |  | 2 Flexible Condur | $77.75$ |  |  |
| L18 | 16 | HCS 6X12 4AWG(1-5/8) | $70.00-$ | 1.0000 | 1.0000 |
|  |  |  | 77.75 |  |  |
| L18 | 25 | PL 0.75x4 | $\begin{array}{r} 70.00- \\ 7775 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 26 | PL 0.75x4 | 70.00- | 1.0000 | 1.0000 |
|  |  |  | 77.75 |  |  |
| L18 | 27 | PL 0.75x4 | 70.00- | 1.0000 | 1.0000 |
|  |  |  | 77.75 |  |  |
| L18 | 62 | (Area) CCI-65FP-045125 | $70.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 77.75 |  |  |
| L18 | 63 | (Area) CCI-65FP-045125 | $70.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 77.75 |  |  |
| L18 | 64 | (Area) CCI-65FP-045125 | $70.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 77.75 |  |  |
| L19 | 1 | CU12PSM9P8XXX(1-3/8) | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 3 | 2" Flexible Conduit | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 4 | LDF6-50A(1-1/4) | $69.00-1$ | 1.0000 | 1.0000 |
| L19 | 10 | 2" Flexible Conduit | 69.00 - | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 16 | HCS 6X12 4AWG(1-5/8) | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 25 | PL 0.75x4 | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 26 | PL $0.75 \times 4$ | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 27 | PL 0.75x4 | $69.00-$ | 1.0000 | 1.0000 |
|  |  |  | 70.00 |  |  |
| L19 | 62 | (Area) CCI-65FP-045125 | $69.00-$ 70.00 | 1.0000 | 1.0000 |
| L19 | 63 | (Area) CCI-65FP-045125 | 70.00 $69.00-$ |  |  |
| L19 | 63 | (Area) CCl-65FP-045125 | $69.00-$ 70.00 | 1.0000 | 1.0000 |
| L19 | 64 | (Area) CCI-65FP-045125 | $69.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 70.00 |  |  |
| L20 | 1 | CU12PSM9P8XXX(1-3/8) | 67.08 - | 1.0000 | 1.0000 |
|  |  |  | 69.00 |  |  |
| L20 | 3 | 2" Flexible Conduit | 67.08 - | 1.0000 | 1.0000 |
|  |  | LDF6-50A(1-1/4) | 69.00 |  |  |
| L20 | 4 | LDF6-50A(1-1/4) | 67.08 - | 1.0000 | 1.0000 |
| L20 | 10 | 2" Flexible Conduit | 67.08 - | 1.0000 | 1.0000 |
|  |  |  | 69.00 |  |  |
| L20 | 16 | HCS 6X12 4AWG(1-5/8) | 67.08 - | 1.0000 | 1.0000 |
|  |  |  | 69.00 |  |  |
| L20 | 22 | PL 0.75x4 | $67.08$ | 1.0000 | 1.0000 |
| L20 | 23 | PL 0.75x4 | 68.25 $67.08-$ | 1.0000 | 1.0000 |
| L20 | 23 | PL $0.75 \times 4$ | $68.25$ | 1.0000 | 1.0000 |
| L20 | 24 | PL 0.75x4 | 67.08 - | 1.0000 | 1.0000 |
|  |  |  | 68.25 |  |  |
| L20 | 25 | PL 0.75x4 | $67.08-$ | 1.0000 | 1.0000 |
| L20 | 26 | PL 0.75x4 | 69.00 | 1.0000 | 1.0000 |
|  |  |  | 69.00 |  |  |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L20 | 27 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 3 | 2" Flexible Conduit | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 10 | 2" Flexible Conduit | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 22 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 23 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 24 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 25 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 26 | PL $0.75 \times 4$ | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 27 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 64 | (Area) CCI-65FP-045125 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 3 | 2" Flexible Conduit | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 10 | 2" Flexible Conduit | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 22 | PL 0.75x4 | $\begin{array}{r} 64.08-1 \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 23 | PL 0.75x4 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 24 | PL 0.75x4 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 25 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 26 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 27 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 64.08- \\ 66.08 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 44 | (Area) CCl-65FP-045100 <br> (H) | $\begin{array}{r} 64.08- \\ 66.08 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 64.08- \\ 64.50 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 63 | (Area) CCI-65FP-045125 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 64 | (Area) CCI-65FP-045125 | 64.08-1 | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | Ka No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L23 | 1 | CU12PSM9P8XXX(1-3/8) | 66.83 63.83 64.08 | 1.0000 | 1.0000 |
| L23 | 3 | 2" Flexible Conduit | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 10 | 2" Flexible Conduit | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 22 | PL 0.75x4 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 23 | PL 0.75x4 | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 24 | PL 0.75x4 | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 43 | (Area) CCl-65FP-045100 | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 3 | 2" Flexible Conduit | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 10 | 2" Flexible Conduit | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 22 | PL 0.75x4 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 23 | PL 0.75x4 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 24 | PL 0.75x4 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 3 | 2" Flexible Conduit | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 10 | 2" Flexible Conduit | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 22 | PL 0.75x4 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L25 | 23 | PL 0.75x4 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 24 | PL $0.75 \times 4$ | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 43 | (Area) CCl -65FP-045100 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 44 | (Area) CCl-65FP-045100 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.25 \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 64 | (Area) CCI-65FP-045125 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 3 | 2" Flexible Conduit | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 10 | 2" Flexible Conduit | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 22 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 23 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 24 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 3 | 2" Flexible Conduit | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 10 | 2" Flexible Conduit | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 22 | PL 0.75x4 | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 23 | PL 0.75x4 | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 24 | PL 0.75x4 | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 56.00 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 56.00 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 56.00- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 44 | (Area) CCI-65FP-045100 | $\begin{array}{r} 56.00- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 45 | (Area) CCI-65FP-045100 | 53.50-1 | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Segment Elev. | No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L27 | 59 |  | 57.25 | 1.0000 | 1.0000 |
|  |  | (Area) CCI-65FP-060100 | $53.50-$ |  |  |
| L27 | 60 | (H) | 55.08 |  |  |
|  |  | (Area) CCl-65FP-060100 | 53.50-1 | 1.0000 | 1.0000 |
| L27 | 61 | (Area) CCl-65FP-060100 | $53.50-$ | 1.0000 | 1.0000 |
|  |  | (H) | 55.08 |  |  |
| L27 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 55.08- \\ 57.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 63 | (Area) CCI-65FP-045125 | 55.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 57.25 |  |  |
| L27 | 64 | (Area) CCl-65FP-045125 | 55.08 - | 1.0000 | 1.0000 |
|  |  | CU12PSM9P8XXX(1-3/8) | 57.25 |  |  |
| L28 | 1 | CU12PSM9P8XXX(1-3/8) | 53.25- | 1.0000 | 1.0000 |
| L28 | 3 | 2" Flexible Conduit | $53.25-$ | 1.0000 | 1.0000 |
|  | 4 | LDF6-50A(1-1/4) | 53.50 |  |  |
| L28 |  |  | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 10 | 2" Flexible Conduit | 53.25 - | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L28 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 22 | PL 0.75x4 | 53.25 - | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L28 | 2324 | PL 0.75x4 | $53.25-$ | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L28 | 24 | PL 0.75x4 | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 40 | (Area) CCl -65FP-060100 | 53.25 - | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L28 | 41 | (Area) CCl -65FP-060100 | $53.25-$ | 1.0000 | 1.0000 |
|  | 45 | (H) | 53.50 $53.25-$ |  |  |
| L28 |  | (Area) CCI-65FP-045100 | 53.25- | 1.0000 | 1.0000 |
| L28 | 59 | (Area) CCl -65FP-060100 | $53.25-$ | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L28 | 60 | (Area) CCI-65FP-060100 | 53.25- | 1.0000 | 1.0000 |
| L28 | 61 | (Area) CCI-65FP-060100 | 53.50 $53.25-$ | 1.0000 | 1.0000 |
|  |  |  | 53.50 |  |  |
| L29 | 1 | CU12PSM9P8XXX(1-3/8) | 52.58 - | 1.0000 | 1.0000 |
|  |  |  | 53.25 |  |  |
| L29 | 3 | 2" Flexible Conduit | $\begin{array}{r} 52.58 \\ 53.25 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 4 | LDF6-50A(1-1/4) | 52.58 - | 1.0000 | 1.0000 |
| L29 |  |  | 53.25 |  |  |
|  | 10 | 2" Flexible Conduit | 52.58- | 1.0000 | 1.0000 |
| L29 | 16 | HCS 6X12 4AWG(1-5/8) | 52.58 - | 1.0000 | 1.0000 |
|  |  |  | 53.25 |  |  |
| L29 | 22 | PL 0.75x4 | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 23 | PL 0.75x4 | 52.58 - | 1.0000 | 1.0000 |
|  |  |  | 53.25 |  |  |
| L29 | 24 | PL 0.75x4 | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 40 | (Area) CCl-65FP-060100 | 52.58- | 1.0000 | 1.0000 |
|  |  | (H) | 53.25 |  |  |
| L29 | 41 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | 52.58 - | 1.0000 | 1.0000 |
| L29 |  |  | 53.25 |  |  |
|  | 45 | (Area) CCI-65FP-045100 | 52.58 - | 1.0000 | 1.0000 |
| L29 |  |  | 53.25 52.58 |  |  |
|  | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 60 | (Area) CCI-65FP-060100 <br> (H) | 52.58 - | 1.0000 | 1.0000 |
|  |  |  | 53.25 |  |  |
| L29 | 61 | (Area) CCI-65FP-060100 | 52.58 - | 1.0000 | 1.0000 |
|  |  |  | 53.25 |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L30 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 52.33 \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 3 | 2" Flexible Conduit | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 10 | 2" Flexible Conduit | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 22 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 23 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 24 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 40 | (Area) CCl-65FP-060100 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 45 | (Area) CCl-65FP-045100 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 3 | 2" Flexible Conduit | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 10 | 2" Flexible Conduit | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 22 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 23 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 24 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 41 | (Area) CCl-65FP-060100 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 3 | 2" Flexible Conduit | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 10 | 2" Flexible Conduit | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 19 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 45.83 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 20 | PL 0.75x4 | 44.58-1 | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L32 | 21 | PL 0.75x4 | $\begin{array}{r} 45.83 \\ 44.58- \\ 45.83 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 22 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 23 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 24 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 40 | (Area) CCl-65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 41 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 60 | (Area) CCl -65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L32 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 3 | 2" Flexible Conduit | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 10 | 2" Flexible Conduit | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 19 | PL 0.75x4 | $\begin{array}{r} 44.33 \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 20 | PL 0.75x4 | $\begin{array}{r} 44.33 \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 21 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 22 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 23 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 24 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.42 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 44.50- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33 \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 3 | 2" Flexible Conduit | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 10 | 2" Flexible Conduit | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 19 | PL 0.75x4 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L34 | 20 | PL 0.75x4 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 21 | PL 0.75x4 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 22 | PL 0.75x4 | $\begin{array}{r} 43.25- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 23 | PL 0.75x4 | $\begin{array}{r} 43.25- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 24 | PL 0.75x4 | $\begin{array}{r} 43.25- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 36 | (Area) CCI-65FP-060100 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 4433 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 41 | (Area) CCI-65FP-060100 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 60 | (Area) CCl -65FP-060100 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 1 | CU12PSM9P8XXX (1-3/8) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 3 | 2" Flexible Conduit | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 10 | 2" Flexible Conduit | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 19 | PL 0.75x4 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 20 | PL 0.75x4 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 21 | PL 0.75x4 | $41.67-$ 41.92 | 1.0000 | 1.0000 |
| L35 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 40 | (Area) CCI-65FP-060100 <br> (H) | $41.67-9$ 41.92 | 1.0000 | 1.0000 |
| L35 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 1 | CU12PSM9P8XXX(1-3/8) | 34.08-1 41.67 | 1.0000 | 1.0000 |
| L36 | 3 | 2" Flexible Conduit | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 10 | 2" Flexible Conduit | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 19 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 20 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 21 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 36 | (Area) CCI-65FP-060100 | $34.08 \text { - }$ | 1.0000 | 1.0000 |
| L36 | 40 | (Area) CCI-65FP-060100 | 41.67 | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L36 | 41 | (H) | 41.67 | 1.0000 | 1.0000 |
|  |  | (Area) CCI-65FP-060100 | 34.08 - |  |  |
|  |  | (H) | 41.67 |  |  |
| L36 | 59 | (Area) CCI-65FP-060100 | 34.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 41.67 |  |  |
| L36 | 60 | (Area) CCI-65FP-060100 | $34.08-$ 41.67 | 1.0000 | 1.0000 |
| L36 | 61 | (Area) CCl-65FP-060100 | 41.67 $34.08-$ | 1.0000 | 1.0000 |
|  |  | (H) | 41.67 |  |  |
| L37 | 1 | CU12PSM9P8XXX(1-3/8) | $34.00-$ | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 3 | 2" Flexible Conduit | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 4 | LDF6-50A(1-1/4) | $34.00-$ | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 10 | 2" Flexible Conduit | $34.00-$ 34.08 | 1.0000 | 1.0000 |
| L37 | 16 | HCS 6X12 4AWG(1-5/8) | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 19 | PL 0.75x4 | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 20 | PL 0.75x4 | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 21 | PL 0.75x4 | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 36 | (Area) CCl-65FP-060100 | $34.00-$ | 1.0000 | 1.0000 |
|  |  |  | 34.08 34.00 |  |  |
| L37 | 40 | (Area) CCl -65FP-060100 | $34.00-$ 34.08 | 1.0000 | 1.0000 |
| L37 | 41 | (Area) CCI-65FP-060100 | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 59 | (Area) CCI-65FP-060100 | 34.00 - | 1.0000 | 1.0000 |
|  |  | (H) | 34.08 |  |  |
| L37 | 60 | (Area) CCI-65FP-060100 | 34.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.08 |  |  |
| L37 | 61 | (Area) CCl-65FP-060100 | $34.00-$ 34.08 | 1.0000 | 1.0000 |
| L38 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r}34.08 \\ 29.00- \\ \hline\end{array}$ |  |  |
|  |  |  | $29.00-$ 34.00 | 1.0000 | 1.0000 |
| L38 | 3 | 2" Flexible Conduit | 29.00 - | 1.0000 | 1.0000 |
|  | 4 |  | 34.00 |  |  |
| L38 |  | LDF6-50A(1-1/4) | $29.00-$ 34.00 | 1.0000 | 1.0000 |
| L38 | 10 | 2" Flexible Conduit | 29.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.00 |  |  |
| L38 | 16 | HCS 6X12 4AWG(1-5/8) | 29.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.00 |  |  |
| L38 | 19 | PL 0.75x4 | 29.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.00 |  |  |
| L38 | 20 | PL 0.75x4 | 29.00 - | 1.0000 | 1.0000 |
|  | 21 |  | 34.00 |  |  |
| L38 |  | PL 0.75x4 | $29.00-$ 34.00 | 1.0000 | 1.0000 |
| L38 | 36 | (Area) CCI-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
|  |  | (H) | 34.00 |  |  |
| L38 | 37 | (Area) CCl-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
| L38 | 38 | $(\mathrm{H})$ | 29.42 |  |  |
|  |  | (Area) CCI-65FP-060100 | $29.00-$ 29.42 | 1.0000 | 1.0000 |
| L38 | 40 | (Area) CCl-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
|  |  |  | 34.00 |  |  |
| L38 | 41 | (Area) CCI-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
|  |  | (H) | 34.00 |  |  |
| L38 | 59 | (Area) CCI-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
| L38 |  | $(\mathrm{H})$ | 34.00 |  |  |
|  | 60 | (Area) CCI-65FP-060100 | 29.00 - | 1.0000 | 1.0000 |
|  | $61$ |  | 34.00 | $1.0000$ |  |
| L38 |  | (Area) CCI-65FP-060100 <br> (H) | 29.00 - |  | $1.0000$ |
|  |  |  | 34.00 |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L39 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 3 | 2" Flexible Conduit | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 10 | 2" Flexible Conduit | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 19 | PL 0.75x4 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 20 | PL 0.75x4 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 21 | PL 0.75x4 | $26.92-1$ | 1.0000 | 1.0000 |
| L39 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 37 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 40 | (Area) CCl-65FP-060100 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 41 | (Area) CCI-65FP-060100 <br> (H) | $26.92-$ 29.00 | 1.0000 | 1.0000 |
| L39 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 60 | (Area) CCl -65FP-060100 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 61 | (Area) CCI-65FP-060100 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 3 | 2" Flexible Conduit | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 10 | 2" Flexible Conduit | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 19 | PL 0.75x4 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 20 | PL 0.75x4 | $26.67-1$ 26.92 | 1.0000 | 1.0000 |
| L40 | 21 | PL 0.75x4 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 36 | (Area) CCl -65FP-060100 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 59 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 61 | (Area) CCI-65FP-060100 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 3 | 2" Flexible Conduit | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 4 | LDF6-50A(1-1/4) | 21.67-1 | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 26.67 |  |  |
| L41 | 10 | 2" Flexible Conduit | $21.67-$ 26.67 | 1.0000 | 1.0000 |
| L41 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 19 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 20 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 21 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 36 | (Area) CCI-65FP-060100 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 40 | (Area) CCI-65FP-060100 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 2667 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 3 | 2" Flexible Conduit | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 10 | 2" Flexible Conduit | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 19 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 20 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 21 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 57 | (Area) CCI-65FP-060100 | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L42 | 58 | (Area) CCl-65FP-060100 | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 3 | 2" Flexible Conduit | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 10 | 2" Flexible Conduit | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 19 | PL 0.75x4 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 20 | PL 0.75x4 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 21 | PL 0.75x4 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 33 | (Area) CCl -65FP-060100 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 58 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 3 | 2" Flexible Conduit | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 10 | 2" Flexible Conduit | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 19 | PL 0.75x4 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 20 | PL 0.75x4 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 21 | PL 0.75x4 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | 1.0000 | 1.0000 |
| L44 | 53 | (Area) CCI-65FP-065125 | $17.50-$ | 1.0000 | 1.0000 |
| L44 | 54 | (Area) CCI-65FP-065125 | $\begin{array}{r} 17.75 \\ 17.50- \end{array}$ | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 56 | (H) | 17.75 |  |  |
| L44 |  | (Area) CCI-65FP-060100 | 17.50 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.75 |  |  |
| L44 | 57 | (Area) CCI-65FP-060100 | $17.50-$ | 1.0000 | 1.0000 |
|  |  | (H) | 17.75 |  |  |
| L44 | 58 | (Area) CCI-65FP-060100 | 17.50 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.75 |  |  |
| L45 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | 1.0000 | 1.0000 |
| L45 | 3 | 2" Flexible Conduit | $17.25-$ | 1.0000 | 1.0000 |
|  |  |  | 17.50 |  |  |
| L45 | 4 | LDF6-50A(1-1/4) | $17.25-$ | 1.0000 | 1.0000 |
| L45 |  | 2" Flexible Conduit | 17.50 $17.25-$ | 1.0000 | 1.0000 |
|  | 10 | dut | 17.50 | 1.0000 | 1.0000 |
| L45 | 16 | HCS 6X12 4AWG(1-5/8) | $17.25-$ | 1.0000 | 1.0000 |
|  |  |  | 17.50 |  |  |
| L45 | 19 | PL 0.75x4 | 17.25 - | 1.0000 | 1.0000 |
|  |  |  | 17.50 |  |  |
| L45 | 20 | PL 0.75x4 | $17.25-$ | 1.0000 | 1.0000 |
|  |  |  | 17.50 |  |  |
| L45 | 21 | PL 0.75x4 | $17.25-$ | 1.0000 | 1.0000 |
|  |  |  | 17.50 |  |  |
| L45 | 33 | (Area) CCI-65FP-060100 | $17.25-$ | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 34 | (Area) CCl-65FP-060100 | 17.25 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 35 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | 1.0000 | 1.0000 |
| L45 | 52 | (Area) CCl-65FP-065125 | 17.25- | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 53 | (Area) CCl-65FP-065125 | 17.25 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 54 | (Area) CCI-65FP-065125 | $17.25-$ | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 56 | (Area) CCl-65FP-060100 | 17.25- | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L45 | 57 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | 1.0000 | 1.0000 |
| L45 | 58 | (Area) CCl-65FP-060100 | 17.50 $17.25-$ | 1.0000 | 1.0000 |
|  |  | (H) | 17.50 |  |  |
| L46 | 1 | CU12PSM9P8XXX(1-3/8) | $17.08$ | 1.0000 | 1.0000 |
| L46 | 3 |  | $\begin{array}{r} 17.25 \\ 17.08 \end{array}$ |  |  |
|  |  | 2 " Flexible Conduit | $\begin{array}{r} 17.08 \\ 17.25 \end{array}$ | 1.0000 | 1.0000 |
| L46 | 4 | LDF6-50A(1-1/4) | 17.08 - | 1.0000 | 1.0000 |
|  |  |  | 17.25 |  |  |
| L46 | 10 | 2" Flexible Conduit | 17.08- | 1.0000 | 1.0000 |
| L46 | 16 | HCS 6X12 4AWG(1-5/8) | 17.25 $17.08-$ | 1.0000 | 1.0000 |
|  |  | HCS 6X12 4AWG(1-5/8) | $17.25$ | 1.0000 | 1.0000 |
| L46 | 19 | PL 0.75x4 | 17.08 - | 1.0000 | 1.0000 |
|  |  |  | 17.25 |  |  |
| L46 | 20 | PL 0.75x4 | $\begin{array}{r} 17.08- \\ 1705 \end{array}$ | 1.0000 | 1.0000 |
| L46 | 21 | PL 0.75x4 | 17.25 $17.08-$ | 1.0000 | 1.0000 |
|  |  |  | 17.25 |  |  |
| L46 | 33 | (Area) CCI-65FP-060100 | 17.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 34 | (Area) CCl-65FP-060100 | 17.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 35 | (Area) CCI-65FP-060100 | 17.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 52 | (Area) CCl-65FP-065125 | 17.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 53 | (Area) CCI-65FP-065125 | 17.08 - | 1.0000 | 1.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 54 | (Area) CCl-65FP-065125 | 17.08 - | 1.0000 | 1.0000 |
|  |  |  | 17.25 |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | Ka No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L46 | 56 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | 1.0000 | 1.0000 |
| L46 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | 1.0000 | 1.0000 |
| L46 | 58 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 3 | 2" Flexible Conduit | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 10 | 2" Flexible Conduit | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 19 | PL 0.75x4 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 20 | PL 0.75x4 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 21 | PL 0.75x4 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 33 | (Area) CCl-65FP-060100 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 47$ | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L47 | 58 | (Area) CCl -65FP-060100 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 3 | 2" Flexible Conduit | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 10 | 2" Flexible Conduit | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 19 | PL 0.75x4 | $\begin{array}{r} 15.83- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 20 | PL 0.75x4 | $\begin{array}{r} 15.83- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 21 | PL 0.75x4 | $15.83-$ 16.83 | 1.0000 | 1.0000 |
| L48 | 29 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 30 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 31 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 15.50 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | 1.0000 | 1.0000 |
| L48 | 52 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-065125$ | $13.00-$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No Ice | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 53 | (H) | 16.83 |  |  |
| L48 |  | (Area) CCI-65FP-065125 | 13.00 - | 1.0000 | 1.0000 |
|  |  | (H) | 16.83 |  |  |
| L48 | 54 | (Area) CCI-65FP-065125 | 13.00 16.83 | 1.0000 | 1.0000 |
| L48 | 56 | (Area) CCI-65FP-060100 | 16.83 $13.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 16.83 |  |  |
| L48 | 57 | (Area) CCI-65FP-060100 | 13.00 - | 1.0000 | 1.0000 |
|  |  | (H) | 16.83 |  |  |
| L48 | 58 | (Area) CCl-65FP-060100 | $13.00-$ | 1.0000 | 1.0000 |
|  |  | (H) | 16.83 |  |  |
| L49 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 12.75- \\ 13.00 \end{array}$ | 1.0000 | 1.0000 |
| L49 | 3 | 2" Flexible Conduit | 12.75- | 1.0000 | 1.0000 |
|  |  |  | 13.00 |  |  |
| L49 | 4 | LDF6-50A(1-1/4) | 12.75 - | 1.0000 | 1.0000 |
|  |  |  | 13.00 |  |  |
| L49 | 10 | 2" Flexible Conduit | $\begin{array}{r} 12.75- \\ 13.00 \end{array}$ | 1.0000 | 1.0000 |
| L49 | 16 | HCS 6X12 4AWG(1-5/8) | 12.75 - | 1.0000 | 1.0000 |
|  |  |  | 13.00 |  |  |
| L49 | 29 | (Area) CCl-65FP-060100 | $12.75$ | 1.0000 | 1.0000 |
|  | 30 | (Area) (H) | 13.00 |  |  |
| L49 |  | (Area) CCI-65FP-060100 | $\begin{array}{r} 12.75- \\ 13.00 \end{array}$ | 1.0000 | 1.0000 |
| L49 | 31 | (Area) CCl-65FP-060100 | 12.75- | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 33 | (Area) CCI-65FP-060100 | 12.75 - | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 34 | (Area) CCI-65FP-060100 | 12.75 - | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 35 | (Area) CCl-65FP-060100 | $12.75-$ | 1.0000 | 1.0000 |
| L49 | 52 | ( ${ }^{(\mathrm{H})}$ | $\begin{array}{r} 13.00 \\ 12.75- \end{array}$ |  |  |
|  |  | (Area) CCI-65FP-065125 | $12.75-$ 13.00 | 1.0000 | 1.0000 |
| L49 | 53 | (Area) CCl-65FP-065125 | 12.75 - | 1.0000 | 1.0000 |
|  | 54 | (H) | 13.00 |  |  |
| L49 |  | (Area) CCI-65FP-065125 | $\begin{array}{r} 12.75- \\ 130 \end{array}$ | 1.0000 | 1.0000 |
| L49 | 56 | (Area) CCI-65FP-060100 | 13.00 | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 57 | (Area) CCI-65FP-060100 | 12.75 - | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 58 | (Area) CCI-65FP-060100 | 12.75 - | 1.0000 | 1.0000 |
|  |  | (H) | 13.00 |  |  |
| L50 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 11.92- \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 3 | 2" Flexible Conduit | 11.92- | 1.0000 | 1.0000 |
|  |  |  | 12.75 |  |  |
| L50 | 4 | LDF6-50A(1-1/4) | 11.92 - | 1.0000 | 1.0000 |
|  |  |  | 12.75 |  |  |
| L50 | 10 | 2" Flexible Conduit | 11.92 - | 1.0000 | 1.0000 |
|  |  |  | 12.75 |  |  |
| L50 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 11.92- \\ 1075 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 29 | (Area) CCl-65FP-060100 | 12.75 $11.92-$ | 1.0000 | 1.0000 |
|  |  | (H) | 12.75 |  |  |
| L50 | 30 | (Area) CCI-65FP-060100 | 11.92 - | 1.0000 | 1.0000 |
|  |  | (H) | 12.75 |  |  |
| L50 | 31 | (Area) CCl-65FP-060100 | 11.92 - | 1.0000 | 1.0000 |
| L50 |  | (H) | 12.75 |  |  |
|  | 33 | (Area) CCI-65FP-060100 | 11.92 - | 1.0000 | 1.0000 |
| L50 | 34 | (H) | 12.75 |  |  |
|  |  | (Area) CCI-65FP-060100 | $\begin{array}{r} 11.92- \\ 1275 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 35 | (Area) CCI-65FP-060100 | 12.75 | 1.0000 | 1.0000 |
|  |  | (H) | 12.75 |  |  |
| L50 | 52 | (Area) CCI-65FP-065125 | 11.92- | 1.0000 | 1.0000 |
|  |  |  | 12.75 |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L50 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 11.92-75 \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 54 | (Area) CCI-65FP-065125 | $\begin{array}{r} 11.92- \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 56 | (Area) CCl -65FP-060100 | $\begin{array}{r} 11.92- \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.92- \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L50 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.92- \\ 12.75 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 1 | CU12PSM9P8XXX(1-3/8) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 3 | 2" Flexible Conduit | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 4 | LDF6-50A(1-1/4) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 10 | 2" Flexible Conduit | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 16 | HCS 6X12 4AWG(1-5/8) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 29 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 30 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 31 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 33 | (Area) CCI-65FP-060100 <br> (H) | $11.67-9$ 11.92 | 1.0000 | 1.0000 |
| L51 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 52 | (Area) CCI-65FP-065125 <br> (H) | $11.67-9$ 11.92 | 1.0000 | 1.0000 |
| L51 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 11.67 \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 54 | (Area) CCI-65FP-065125 <br> (H) | 11.67-1 11.92 | 1.0000 | 1.0000 |
| L51 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L51 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 11.67- \\ 11.92 \end{array}$ | 1.0000 | 1.0000 |
| L52 | 1 | CU12PSM9P8XXX(1-3/8) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 3 | 2" Flexible Conduit | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 4 | LDF6-50A(1-1/4) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 10 | 2" Flexible Conduit | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 16 | HCS 6X12 4AWG(1-5/8) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 29 | (Area) CCI-65FP-060100 <br> (H) | $6.67-11.67$ $6.67-11.67$ | 1.0000 | 1.0000 1.0000 |
| L52 | 30 | (Area) CCI-65FP-060100 <br> (H) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 31 33 | (Area) CCI-65FP-060100 <br> (H) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 33 | (Area) CCI-65FP-060100 <br> (H) | 9.42-11.67 | 1.0000 | 1.0000 |
| L52 | 34 | (Area) CCI-65FP-060100 <br> (H) | 9.42-11.67 | 1.0000 | 1.0000 |
| L52 | 35 | (Area) CCI-65FP-060100 <br> (H) | 9.42-11.67 | 1.0000 | 1.0000 |
| L52 | 51 | (Area) CCI-65FP-065125 | 6.67-9.25 | 1.0000 | 1.0000 |
| L52 | 52 | (Area) CCl-65FP-065125 | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 53 | (Area) CCI-65FP-065125 | 6.67-11.67 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L52 | 54 | (Area) CCl -65FP-065125 | 6.67-11.67 | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L52 | 56 | (Area) CCI-65FP-060100 | 6.67-11.67 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L52 | 57 | (Area) CCI-65FP-060100 <br> (H) | 6.67-11.67 | 1.0000 | 1.0000 |
| L52 | 58 | (Area) CCI-65FP-060100 | 6.67-11.67 | 1.0000 | 1.0000 |
| L53 | 1 | CU12PSM9P8XXX(1-3/8) | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 3 | 2" Flexible Conduit | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 4 | LDF6-50A(1-1/4) | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 10 | 2" Flexible Conduit | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 16 | HCS 6X12 4AWG(1-5/8) | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 29 | (Area) CCI-65FP-060100 | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 30 | (Area) CCI-65FP-060100 | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 31 | $(\mathrm{H})$ | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 31 | $(\mathrm{H})$ | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 51 | (Area) CCl-65FP-065125 | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 52 | (Area) CCI-65FP-065125 | 6.50-6.67 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L53 | 53 | (Area) CCI-65FP-065125 | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 54 | $\begin{array}{r} (\mathrm{H}) \\ \text { (Area) CCI-65FP-065125 } \end{array}$ | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 54 | $(\mathrm{H})$ | 6.50-6.67 | 1.0000 | 1.0000 |
| L53 | 56 | (Area) CCI-65FP-060100 | 6.50-6.67 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L53 | 57 | (Area) CCI-65FP-060100 | 6.50-6.67 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L53 | 58 | (Area) CCI-65FP-060100 <br> (H) | 6.50-6.67 | 1.0000 | 1.0000 |
| L54 | 1 | CU12PSM9P8XXX(1-3/8) | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 3 | 2" Flexible Conduit | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 4 | LDF6-50A(1-1/4) | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 10 | 2" Flexible Conduit | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 16 | HCS 6X12 4AWG(1-5/8) | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 29 | (Area) CCI-65FP-060100 | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 30 | (Area) CCI-65FP-060100 | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 31 | (H) |  |  |  |
| L54 | 31 | (Area) CCl-65FP-060100 | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 51 | (Area) CCI-65FP-065125 | 6.25-6.50 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L54 | 52 | (Area) CCI-65FP-065125 | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 53 | (Area) CCI-65FP-065125 | 6.25-6.50 | 1.0000 | 1.0000 |
| L54 | 54 | (Area) CCI-65FP-065125 | 6.25-6.50 | 1.0000 | 1.0000 |
|  |  | $(\mathrm{H})$ |  |  |  |
| L54 | 56 | (Area) CCI-65FP-060100 | 6.25-6.50 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L54 | 57 | (Area) CCI-65FP-060100 | 6.25-6.50 | 1.0000 | 1.0000 |
|  |  | (Area) CCI-65FP-060100 |  |  |  |
| L54 | 58 | (Area) CCI-65FP-060100 <br> (H) | 6.25-6.50 | 1.0000 | 1.0000 |
| L55 | 1 | CU12PSM9P8XXX(1-3/8) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 3 | 2" Flexible Conduit | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 4 | LDF6-50A(1-1/4) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 10 | 2" Flexible Conduit | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 16 | HCS 6X12 4AWG(1-5/8) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 29 | (Area) CCI-65FP-060100 | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 30 | (Area) CCI-65FP-060100 | 3.75-6.25 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L55 | 31 | (Area) CCI-65FP-060100 | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 51 | (Area) CCI-65FP-065125 | 3.75-6.25 | 1.0000 | 1.0000 |
|  |  |  |  |  |  |

tnxTower Report - version 8.1.1.0

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L55 | 52 | (Area) CCI-65FP-065125 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 53 | (Area) CCI-65FP-065125 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 54 | (Area) CCI-65FP-065125 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 56 | (Area) CCI-65FP-060100 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 57 | (Area) CCI-65FP-060100 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L55 | 58 | (Area) CCI-65FP-060100 <br> (H) | 3.75-6.25 | 1.0000 | 1.0000 |
| L56 | 1 | CU12PSM9P8XXX(1-3/8) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 3 | 2" Flexible Conduit | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 4 | LDF6-50A(1-1/4) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 10 | 2" Flexible Conduit | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 16 | HCS 6X12 4AWG(1-5/8) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 29 | (Area) CCI-65FP-060100 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 30 | (Area) CCI-65FP-060100 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 31 | (Area) CCI-65FP-060100 | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 51 | (Area) CCI-65FP-065125 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 52 | (Area) CCI-65FP-065125 | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 53 | (Area) CCI-65FP-065125 | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 54 | (Area) CCI-65FP-065125 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 56 | (Area) CCI-65FP-060100 | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 57 | (Area) CCI-65FP-060100 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L56 | 58 | (Area) CCI-65FP-060100 <br> (H) | 3.50-3.75 | 1.0000 | 1.0000 |
| L57 | 1 | CU12PSM9P8XXX(1-3/8) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 3 | 2" Flexible Conduit | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 4 | LDF6-50A(1-1/4) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 10 | 2" Flexible Conduit | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 16 | HCS 6X12 4AWG(1-5/8) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 29 | (Area) CCI-65FP-060100 | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 30 | (Area) CCI-65FP-060100 <br> (H) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 31 | (Area) CCI-65FP-060100 | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 51 | (Area) CCI-65FP-065125 | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 52 | (Area) CCI-65FP-065125 | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 53 | (Area) CCI-65FP-065125 <br> (H) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 54 | (Area) CCI-65FP-065125 <br> (H) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 56 | (Area) CCI-65FP-060100 <br> (H) | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 57 | (Area) CCI-65FP-060100 | 3.00-3.50 | 1.0000 | 1.0000 |
| L57 | 58 | (Area) CCI-65FP-060100 <br> (H) | 3.00-3.50 | 1.0000 | 1.0000 |
| L58 | 1 | CU12PSM9P8XXX(1-3/8) | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 3 | 2" Flexible Conduit | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 4 | LDF6-50A(1-1/4) | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 10 | 2" Flexible Conduit | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 16 | HCS 6X12 4AWG(1-5/8) | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 29 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | 2.75-3.00 | 1.0000 | 1.0000 |

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L58 | 30 | (Area) CCI-65FP-060100 | 2.75-3.00 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L58 | 31 | (Area) CCI-65FP-060100 <br> (H) | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 51 | (Area) CCI-65FP-065125 | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 52 | (Area) CCI-65FP-065125 | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 52 | $(\mathrm{H})$ | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 53 | (Area) CCI-65FP-065125 | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 54 | (Area) CCI-65FP-065125 | 2.75-3.00 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L58 | 56 | (Area) CCI-65FP-060100 | 2.75-3.00 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L58 | 57 | (Area) CCI-65FP-060100 | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 58 | (Area) CCl (H) ${ }^{\text {(H) }}$ | 2.75-3.00 | 1.0000 | 1.0000 |
| L58 | 5 | (H) |  |  |  |
| L59 | 1 | CU12PSM9P8XXX(1-3/8) | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 3 | 2" Flexible Conduit | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 4 | LDF6-50A(1-1/4) | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 10 | 2" Flexible Conduit | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 16 | HCS 6X12 4AWG(1-5/8) | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 29 | (Area) CCI-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  |  |  |  |  |
| L59 | 30 | (Area) CCI-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 31 | (Area) CCI-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L59 | 51 | (Area) CCI-65FP-065125 | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 52 | (Area) CCl-65FP-065125 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L59 | 53 | (Area) CCI-65FP-065125 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L59 | 54 | (Area) CCl-65FP-065125 | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 56 | (Area) CCI-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |
| L59 | 57 | (Area) CCl-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
| L59 | 58 | (Area) CCl-65FP-060100 | 0.00-2.75 | 1.0000 | 1.0000 |
|  |  | (H) |  |  |  |

## Effective Width of Flat Linear Attachments / Feed Lines

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective Width Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L8 | 47 | (Area) CCI-65FP-045100 | $\begin{array}{r} 90.00- \\ 91.50 \end{array}$ | Auto | 0.0000 |
| L8 | 48 | (Area) CCI-65FP-045100 | $90.00-$ 91.50 | Auto | 0.0000 |
| L8 | 49 | (Area) CCI-65FP-045100 | $\begin{array}{r} 90.00- \\ 91.50 \end{array}$ | Auto | 0.0000 |
| L9 | 47 | (Area) CCI-65FP-045100 | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | Auto | 0.0734 |
| L9 | 48 | (Area) CCI-65FP-045100 | $\begin{array}{r} 89.75- \\ 90.00 \end{array}$ | Auto | 0.0734 |
| L9 | 49 | (Area) CCI-65FP-045100 | 89.75-1 | Auto | 0.0734 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L10 | 25 | $(\mathrm{H})$ PL 0.75x4 | $\begin{array}{r} 90.00 \\ 84.75- \\ 85.83 \end{array}$ | Auto | 0.0000 |
| L10 | 26 | PL 0.75x4 | $\begin{array}{r} 84.75- \\ 85.83 \end{array}$ | Auto | 0.0000 |
| L10 | 27 | PL 0.75x4 | $\begin{array}{r} 84.75- \\ 85.83 \end{array}$ | Auto | 0.0000 |
| L10 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | Auto | 0.0244 |
| L10 | 48 | (Area) CCl-65FP-045100 | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | Auto | 0.0244 |
| L10 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.75- \\ 89.75 \end{array}$ | Auto | 0.0244 |
| L10 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | Auto | 0.0000 |
| L10 | 63 | (Area) CCI-65FP-045125 | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | Auto | 0.0000 |
| L10 | 64 | (Area) CCl -65FP-045125 | $\begin{array}{r} 84.75- \\ 85.17 \end{array}$ | Auto | 0.0000 |
| L11 | 25 | PL $0.75 \times 4$ | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 26 | PL 0.75x4 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 27 | PL 0.75x4 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 47 | (Area) CCl -65FP-045100 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L11 | 64 | (Area) CCI -65FP-045125 | $\begin{array}{r} 84.58- \\ 84.75 \end{array}$ | Auto | 0.0000 |
| L12 | 25 | PL 0.75×4 | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0000 |
| L12 | 26 | PL 0.75x4 | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0000 |
| L12 | 27 | PL $0.75 \times 4$ | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0000 |
| L12 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L12 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L12 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L12 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.33 \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L12 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L12 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 84.33- \\ 84.58 \end{array}$ | Auto | 0.0745 |
| L13 | 25 | $\text { PL } 0.75 \times 4$ | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0000 |
| L13 | 26 | PL 0.75x4 | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0000 |
| L13 | 27 | PL 0.75x4 | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0000 |
| L13 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0584 |
| L13 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0584 |
| L13 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.42- \\ 84.33 \end{array}$ | Auto | 0.0584 |
| L13 | 62 | (Area) CCI-65FP-045125 | 83.42 - | Auto | 0.0584 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective Width Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L13 | 63 | (Area) CCI-65FP-045125 | $\begin{array}{r} 84.33 \\ 83.42- \\ 84.33 \end{array}$ | Auto | 0.0584 |
| L13 | 64 | (Area) CCI-65FP-045125 | $83.42-3$ | Auto | 0.0584 |
| L14 | 25 | PL 0.75x4 | $\begin{array}{r} 83.17- \\ 83.42 \end{array}$ | Auto | 0.1487 |
| L14 | 26 | PL 0.75x4 | $83.17-1$ 83.42 | Auto | 0.1487 |
| L14 | 27 | PL 0.75x4 | $\begin{array}{r} 83.17- \\ 83.42 \end{array}$ | Auto | 0.1487 |
| L14 | 47 | (Area) CCI-65FP-045100 <br> (H) | $83.17-1$ 83.42 | Auto | 0.2433 |
| L14 | 48 | (Area) CCI-65FP-045100 <br> (H) | $83.17-1$ 83.42 | Auto | 0.2433 |
| L14 | 49 | (Area) CCI-65FP-045100 <br> (H) | $83.17-1$ 83.42 | Auto | 0.2433 |
| L14 | 62 | (Area) CCI-65FP-045125 (H) | $83.17-1$ 83.42 | Auto | 0.2433 |
| L14 | 63 | (Area) CCI-65FP-045125 <br> (H) | $83.17-1$ | Auto | 0.2433 |
| L14 | 64 | (Area) CCl-65FP-045125 | 83.17-1 83.42 | Auto | 0.2433 |
| L15 | 25 | PL 0.75x4 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.1452 |
| L15 | 26 | PL 0.75x4 | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.1452 |
| L15 | 27 | PL 0.75x4 | $83.00-17$ | Auto | 0.1452 |
| L15 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L15 | 48 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L15 | 49 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L15 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L15 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L15 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 83.00- \\ 83.17 \end{array}$ | Auto | 0.2402 |
| L16 | 25 | PL 0.75x4 | $82.75-$ 83.00 | Auto | 0.0000 |
| L16 | 26 | PL 0.75x4 | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | Auto | 0.0000 |
| L16 | 27 | PL 0.75x4 | $82.75-$ 83.00 | Auto | 0.0000 |
| L16 | 47 | (Area) CCI-65FP-045100 <br> (H) | $82.75-$ 83.00 | Auto | 0.0882 |
| L16 | 48 | (Area) CCI-65FP-045100 (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | Auto | 0.0882 |
| L16 | 49 | (Area) CCI-65FP-045100 <br> (H) | $82.75-$ 83.00 | Auto | 0.0882 |
| L16 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | Auto | 0.0882 |
| L16 | 63 | (Area) CCI-65FP-045125 <br> (H) | $82.75-$ 83.00 | Auto | 0.0882 |
| L16 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 82.75- \\ 83.00 \end{array}$ | Auto | 0.0882 |
| L17 | 25 | PL 0.75x4 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0000 |
| L17 | 26 | PL 0.75x4 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0000 |
| L17 | 27 | PL 0.75x4 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0000 |
| L17 | 47 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 81.50- \\ 82.75 \end{array}$ | Auto | 0.0547 |
| L17 | 48 | (Area) CCI-65FP-045100 | $81.50-$ | Auto | 0.0547 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L17 | 49 | $(\mathrm{H})$ (Area) CCI-65FP-045100 (H) | 82.75 81.50 82.75 | Auto | 0.0547 |
| L17 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0275 |
| L17 | 63 | (Area) CCl-65FP-045125 | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0275 |
| L17 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 77.75- \\ 82.75 \end{array}$ | Auto | 0.0275 |
| L18 | 25 | $\text { PL } 0.75 \times 4$ | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L18 | 26 | PL 0.75x4 | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L18 | 27 | PL 0.75x4 | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L18 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L18 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L18 | 64 | (Area) CCl-65FP-045125 | $\begin{array}{r} 70.00- \\ 77.75 \end{array}$ | Auto | 0.0000 |
| L19 | 25 | PL 0.75x4 | $\begin{array}{r} 69.00- \\ 70.00 \end{array}$ | Auto | 0.0000 |
| L19 | 26 | PL 0.75x4 | $\begin{array}{r} 69.00- \\ 70.00 \end{array}$ | Auto | 0.0000 |
| L19 | 27 | PL 0.75x4 | $69.00-$ 70.00 | Auto | 0.0000 |
| L19 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 69.00- \\ 70.00 \end{array}$ | Auto | 0.0000 |
| L19 | 63 | (Area) CCl-65FP-045125 | $\begin{array}{r} 69.00- \\ 70.00 \end{array}$ | Auto | 0.0000 |
| L19 | 64 | (Area) CCl-65FP-045125 | $\begin{array}{r} 69.00- \\ 70.00 \end{array}$ | Auto | 0.0000 |
| L20 | 22 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 68.25 \end{array}$ | Auto | 0.0000 |
| L20 | 23 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 68.25 \end{array}$ | Auto | 0.0000 |
| L20 | 24 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 68.25 \end{array}$ | Auto | 0.0000 |
| L20 | 25 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L20 | 26 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L20 | 27 | PL 0.75x4 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L20 | 62 | (Area) CCl-65FP-045125 | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L20 | 63 | (Area) CCl-65FP-045125 <br> (H) | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L20 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 67.08- \\ 69.00 \end{array}$ | Auto | 0.0000 |
| L21 | 22 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 23 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 24 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 25 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 26 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 27 | PL 0.75x4 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 63 | (Area) CCl-65FP-045125 | $\begin{array}{r} 66.83- \\ 67.08 \end{array}$ | Auto | 0.0000 |
| L21 | 64 | (Area) CCl-65FP-045125 | 66.83 - | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L22 | 22 | $(\mathrm{H})$ PL 0.75x4 | $\begin{array}{r} 67.08 \\ 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 23 | PL 0.75x4 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 24 | PL 0.75x4 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 25 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 26 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 27 | PL 0.75x4 | $\begin{array}{r} 65.83- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 43 | (Area) CCl-65FP-045100 | $\begin{array}{r} 64.08- \\ 66.08 \end{array}$ | Auto | 0.0000 |
| L22 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 64.08- \\ 66.08 \end{array}$ | Auto | 0.0000 |
| L22 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 64.08- \\ 64.50 \end{array}$ | Auto | 0.0000 |
| L22 | 62 | (Area) CCl -65FP-045125 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 63 | (Area) CCl-65FP-045125 <br> (H) | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L22 | 64 | (Area) CCl -65FP-045125 | $\begin{array}{r} 64.08- \\ 66.83 \end{array}$ | Auto | 0.0000 |
| L23 | 22 | PL 0.75x4 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 23 | PL 0.75x4 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 24 | PL 0.75x4 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 44 | (Area) CCl -65FP-045100 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 63.83 \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 63 | (Area) CCl -65FP-045125 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L23 | 64 | (Area) CCl-65FP-045125 | $\begin{array}{r} 63.83- \\ 64.08 \end{array}$ | Auto | 0.0000 |
| L24 | 22 | PL $0.75 \times 4$ | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 23 | PL 0.75x4 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 24 | PL 0.75x4 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 43 | (Area) CCl-65FP-045100 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L24 | 64 | (Area) CCl -65FP-045125 | $\begin{array}{r} 62.50- \\ 63.83 \end{array}$ | Auto | 0.0000 |
| L25 | 22 | PL 0.75x4 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | Auto | 0.0000 |
| L25 | 23 | PL 0.75x4 | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | Auto | 0.0000 |
| L25 | 24 | PL 0.75x4 | $62.25-$ 62.50 | Auto | 0.0000 |
| L25 | 43 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-045100$ | 62.25 - | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L25 | 44 | (H) (Area) CCI-65FP-045100 (H) | 62.50 62.25 62.50 | Auto | 0.0000 |
| L25 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | Auto | 0.0000 |
| L25 | 62 | (Area) CCI-65FP-045125 <br> (H) | $62.25-$ 62.50 | Auto | 0.0000 |
| L25 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | Auto | 0.0000 |
| L25 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 62.25- \\ 62.50 \end{array}$ | Auto | 0.0000 |
| L26 | 22 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 23 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 24 | PL 0.75x4 | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 45 | (Area) CCl-65FP-045100 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L26 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 57.25- \\ 62.25 \end{array}$ | Auto | 0.0000 |
| L27 | 22 | $\text { PL } 0.75 \times 4$ | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 23 | PL 0.75x4 | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 24 | PL 0.75x4 | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 56.00 \end{array}$ | Auto | 0.0745 |
| L27 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 56.00 \end{array}$ | Auto | 0.0745 |
| L27 | 43 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 56.00- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 44 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 56.00- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 53.50- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 55.08 \end{array}$ | Auto | 0.0694 |
| L27 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 55.08 \end{array}$ | Auto | 0.0694 |
| L27 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.50- \\ 55.08 \end{array}$ | Auto | 0.0694 |
| L27 | 62 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 55.08- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 63 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 55.08- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L27 | 64 | (Area) CCI-65FP-045125 <br> (H) | $\begin{array}{r} 55.08- \\ 57.25 \end{array}$ | Auto | 0.0000 |
| L28 | 22 | PL $0.75 \times 4$ | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0000 |
| L28 | 23 | PL 0.75x4 | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0000 |
| L28 | 24 | PL 0.75x4 | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0000 |
| L28 | 40 | (Area) CCI-65FP-060100 | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0703 |
| L28 | 41 | (Area) CCl-65FP-060100 | $53.25-$ | Auto | 0.0703 |
| L28 | 45 | (Area) CCl-65FP-045100 | $\begin{array}{r} 53.50 \\ 53.25- \end{array}$ | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L28 | 59 | (H) (Area) CCI-65FP-060100 (H) | 53.50 53.25 53.50 | Auto | 0.0703 |
| L28 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0703 |
| L28 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 53.25- \\ 53.50 \end{array}$ | Auto | 0.0703 |
| L29 | 22 | PL $0.75 \times 4$ | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0000 |
| L29 | 23 | PL 0.75x4 | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0000 |
| L29 | 24 | PL 0.75x4 | 52.58-1 | Auto | 0.0000 |
| L29 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0596 |
| L29 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0596 |
| L29 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0000 |
| L29 | 59 | (Area) CCl-65FP-060100 | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0596 |
| L29 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0596 |
| L29 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.58- \\ 53.25 \end{array}$ | Auto | 0.0596 |
| L30 | 22 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0000 |
| L30 | 23 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0000 |
| L30 | 24 | PL 0.75x4 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0000 |
| L30 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0712 |
| L30 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0712 |
| L30 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0000 |
| L30 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0712 |
| L30 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0712 |
| L30 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 52.33- \\ 52.58 \end{array}$ | Auto | 0.0712 |
| L31 | 22 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0000 |
| L31 | 23 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0000 |
| L31 | 24 | PL 0.75x4 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0000 |
| L31 | 40 | (Area) CCl-65FP-060100 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0307 |
| L31 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0307 |
| L31 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0000 |
| L31 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0307 |
| L31 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0307 |
| L31 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 47.33- \\ 52.33 \end{array}$ | Auto | 0.0307 |
| L32 | 19 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 45.83 \end{array}$ | Auto | 0.0000 |
| L32 | 20 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 45.83 \end{array}$ | Auto | 0.0000 |
| L32 | 21 | PL 0.75x4 | $\begin{array}{r} 44.58- \\ 45.83 \end{array}$ | Auto | 0.0000 |
| L32 | 22 | PL 0.75x4 | 44.58-1 | Auto | 0.0000 |


| Tower <br> Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L32 | 23 | PL 0.75x4 | $\begin{array}{r} \hline 47.33 \\ 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 24 | PL $0.75 \times 4$ | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 40 | (Area) CCI-65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 41 | (Area) CCl -65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 60 | (Area) CCl-65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L32 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 44.58- \\ 47.33 \end{array}$ | Auto | 0.0000 |
| L33 | 19 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 20 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 21 | PL $0.75 \times 4$ | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 22 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 23 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 24 | PL 0.75x4 | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 36 | (Area) CCI-65FP-060100 | $\begin{array}{r} 44.33- \\ 44.42 \end{array}$ | Auto | 0.0000 |
| L33 | 40 | (Area) CCI-65FP-060100 (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 45 | (Area) CCI-65FP-045100 <br> (H) | $\begin{array}{r} 44.50- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L33 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 44.33- \\ 44.58 \end{array}$ | Auto | 0.0000 |
| L34 | 19 | PL 0.75x4 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 20 | PL 0.75x4 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 21 | PL 0.75x4 | $41.92-$ 44.33 | Auto | 0.0000 |
| L34 | 22 | PL 0.75x4 | $\begin{array}{r} 43.25- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 23 | PL 0.75x4 | $\begin{array}{r} 43.25- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 24 | PL 0.75x4 | $43.25-$ 44.33 | Auto | 0.0000 |
| L34 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 41 | (Area) CCl-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 60 | (Area) CCI-65FP-060100 | $\begin{array}{r} 41.92- \\ 44.33 \end{array}$ | Auto | 0.0000 |
| L34 | 61 | (Area) CCl-65FP-060100 | 41.92- | Auto | 0.0000 |
| L35 | 19 | PL $0.75 \times 4$ | 44.33 | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective Width Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L35 | 20 | PL 0.75x4 | 41.92 41.67 41.92 | Auto | 0.0000 |
| L35 | 21 | PL 0.75x4 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 36 | (Area) CCl -65FP-060100 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 40 | (Area) CCl-65FP-060100 | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 59 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L35 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 41.67- \\ 41.92 \end{array}$ | Auto | 0.0000 |
| L36 | 19 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 20 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 21 | PL 0.75x4 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L36 | 61 | (Area) CCl-65FP-060100 | $\begin{array}{r} 34.08- \\ 41.67 \end{array}$ | Auto | 0.0000 |
| L37 | 19 | PL 0.75x4 | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 20 | PL 0.75x4 | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 21 | PL 0.75x4 | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 36 | (Area) CCl-65FP-060100 | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L37 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 34.00- \\ 34.08 \end{array}$ | Auto | 0.0000 |
| L38 | 19 | PL 0.75x4 | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 20 | PL 0.75x4 | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 21 | PL 0.75x4 | 29.00- | Auto | 0.0000 |
| L38 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 29.00- \\ 29.42 \end{array}$ | Auto | 0.0000 |
| L38 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 29.00- \\ 29.42 \end{array}$ | Auto | 0.0000 |
| L38 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 41 | (Area) CCI-65FP-060100 | 29.00-1 | Auto | 0.0000 |


| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L38 | 59 | (H) (Area) CCI-65FP-060100 (H) | $\begin{array}{r} 34.00 \\ 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | Auto | 0.0000 |
| L38 | 61 | (Area) CCI-65FP-060100 <br> (H) | 29.00- | Auto | 0.0000 |
| L39 | 19 | PL 0.75x4 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 20 | PL 0.75x4 | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 21 | PL 0.75x4 | $26.92-$ 29.00 | Auto | 0.0000 |
| L39 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 59 | (Area) CCI-65FP-060100 <br> (H) | $26.92-1$ 29.00 | Auto | 0.0000 |
| L39 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L39 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.92- \\ 29.00 \end{array}$ | Auto | 0.0000 |
| L40 | 19 | PL 0.75x4 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 20 | PL 0.75x4 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 21 | PL 0.75x4 | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67 \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67 \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67- \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L40 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 26.67 \\ 26.92 \end{array}$ | Auto | 0.0000 |
| L41 | 19 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 20 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 21 | PL 0.75x4 | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 41 | (Area) CCI-65FP-060100 <br> (H) | 21.67-67 | Auto | 0.0000 |
| L41 | 59 | (Area) CCI-65FP-060100 | 21.67-1 | Auto | 0.0000 |


| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L41 | 60 | (H) (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ $(\mathrm{H})$ | $\begin{array}{r} 26.67 \\ 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L41 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.67- \\ 26.67 \end{array}$ | Auto | 0.0000 |
| L42 | 19 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 20 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 21 | PL 0.75x4 | $\begin{array}{r} 18.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 36 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 37 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 38 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.75- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 40 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 41 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 21.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 18.00- \\ 20.75 \end{array}$ | Auto | 0.0000 |
| L42 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | Auto | 0.0000 |
| L42 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | Auto | 0.0000 |
| L42 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 18.00- \\ 20.00 \end{array}$ | Auto | 0.0000 |
| L42 | 59 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 60 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L42 | 61 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 20.00- \\ 21.67 \end{array}$ | Auto | 0.0000 |
| L43 | 19 | $\text { PL } 0.75 \times 4$ | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 20 | PL 0.75x4 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 21 | PL 0.75x4 | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.75- \\ 18.00 \end{array}$ | Auto | 0.0000 |
| L43 | 58 | (Area) CCI-65FP-060100 | $17.75-$ | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L44 | 19 | $(\mathrm{H})$ PL $0.75 \times 4$ | $\begin{array}{r} 18.00 \\ 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 20 | PL 0.75x4 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 21 | PL 0.75x4 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 33 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 34 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 56 | (Area) CCl-65FP-060100 | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 57 | (Area) $\mathrm{CCl}-65 \mathrm{FP}-060100$ | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L44 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.50- \\ 17.75 \end{array}$ | Auto | 0.0000 |
| L45 | 19 | PL 0.75x4 | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 20 | PL 0.75x4 | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 21 | PL 0.75x4 | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 54 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 56 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 57 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L45 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.25- \\ 17.50 \end{array}$ | Auto | 0.0000 |
| L46 | 19 | $\text { PL } 0.75 \times 4$ | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 20 | PL 0.75x4 | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 21 | PL 0.75x4 | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 33 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 34 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 35 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 52 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 53 | (Area) CCI-65FP-065125 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L46 | 54 | (Area) CCI-65FP-065125 | $17.08-$ | Auto | 0.0000 |
| L46 | 56 | (Area) CCI-65FP-060100 | $\begin{array}{r} 17.25 \\ 17.08- \end{array}$ | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L46 | 57 | (H) | $17.25$ |  |  |
|  |  | (Area) CCI-65FP-060100 | 17.08 - |  | 0.0000 |
|  |  | (H) | 17.25 |  |  |
| L46 | 58 | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 17.08- \\ 17.25 \end{array}$ | Auto | 0.0000 |
| L47 | 19 |  |  |  |  |
|  |  | PL 0.75x4 | $17.08$ | Auto | 0.0000 |
| L47 | 20 | PL 0.75x4 | $17.08$ | Auto | 0.0000 |
| L47 |  | PL 0.75x4 |  | Auto |  |
|  | 21 |  | $\begin{array}{r} 17.08 \\ 1683 \end{array}$ |  | 0.0000 |
| $\llcorner 47$ | 33 | (Area) CCl -65FP-060100 |  | Auto | 0.0000 |
|  |  |  | $17.08$ |  |  |
| L47 | 34 | (Area) CCI-65FP-060100 | $16.83-$ | Auto | 0.0000 |
| $\llcorner 47$ |  |  | $\begin{array}{r} 17.08 \\ 16.83 \end{array}$ |  |  |
|  | 35 | (Area) CCl-65FP-060100 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | Auto | 0.0000 |
| L47 | 52 | (Area) CCl -65FP-065125 | $16.83-$ | Auto | 0.0000 |
|  |  |  | $17.08$ |  |  |
| L47 | 53 | (Area) CCl -65FP-065125 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | Auto | 0.0000 |
| L47 | 54 | (Area) CCl-65FP-065125 |  | Auto | 0.0000 |
|  |  |  | $\begin{array}{r} 16.83 \\ 17.08 \end{array}$ |  |  |
| L47 | 56 | (Area) CCl -65FP-060100 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | Auto | 0.0000 |
| L47 |  |  |  |  |  |
|  | 57 | (Area) CCI-65FP-060100 | $\begin{array}{r} 16.83 \\ 17.08 \end{array}$ | Auto | 0.0000 |
| L47 | 58 | (Area) CCl -65FP-060100 | $\begin{array}{r} 16.83- \\ 17.08 \end{array}$ | Auto | 0.0000 |
|  |  |  |  |  |  |
| L48 | 19 | PL 0.75x4 | $16.83$ | Auto | 0.0000 |
| L48 | 20 | PL 0.75x4 | $\begin{array}{r} 16.83 \\ 15.83 \end{array}$ | Auto | 0.0000 |
|  | 21 |  | $\begin{array}{r} 15.83- \\ 16.83 \end{array}$ |  |  |
| L48 |  | PL $0.75 \times 4$ | $\begin{array}{r} 15.83- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 29 | (Area) CCI-65FP-060100 | $13.00-$ | Auto | 0.0000 |
|  |  | (H) | $15.50$ |  |  |
| L48 | 30 | (Area) CCl -65FP-060100 | $\begin{array}{r} 13.00- \\ 15.50 \end{array}$ | Auto | 0.0000 |
|  | 31 |  |  |  |  |
| L48 |  | (Area) CCI-65FP-060100 <br> (H) | $\begin{array}{r} 13.00- \\ 15.50 \end{array}$ | Auto | 0.0000 |
| L48 | 33 |  |  |  | 0.0000 |
|  |  | (H) | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto |  |
| L48 | 34 | (Area) CCI-65FP-060100 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 35 |  |  |  |  |
|  |  | (Area) CCI-65FP-060100 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 52 | (Area) CCl-65FP-065125 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
|  |  |  |  |  |  |
| L48 | 53 | (Area) CCI-65FP-065125 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 54 | (Area) CCI -65FP-065125 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 |  |  |  |  |  |
|  | 56 | (Area) CCI-65FP-060100 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 57 |  |  |  |  |
|  |  | (Area) CCI-65FP-060100 | $\begin{array}{r} 13.00- \\ 16.83 \end{array}$ | Auto | 0.0000 |
| L48 | 58 | (Area) CCl-65FP-060100 | 13.00- | Auto | 0.0000 |
|  |  | (H) | 16.83 |  |  |
| L49 | 29 | (Area) CCI-65FP-060100 | $12.75-13$ | Auto | 0.0000 |
| $\llcorner 49$ | 30 | (H) <br> (Area) | 13.00 $12.75-$ | Auto | 0.0000 |
| L49 | 30 | $(H)$ | 12.75-00 | Auto | 0.0000 |
| L49 | 31 | (Area) CCI-65FP-060100 | 12.75 - | Auto | 0.0000 |
|  |  | (H) | 13.00 |  |  |
| L49 | 33 | (Area) CCl-65FP-060100 | 12.75 - | Auto | 0.0000 |
|  |  |  | 13.00 |  |  |
| L49 | 34 | (Area) CCI-65FP-060100 | $12.75-$ | Auto | 0.0000 |

\begin{tabular}{|c|c|c|c|c|c|}
\hline Tower Section \& Attachment Record No. \& Description \& Attachment Segment Elev. \& Ratio Calculatio \(n\) Method \& \begin{tabular}{l}
Effective \\
Width \\
Ratio
\end{tabular} \\
\hline L49 \& 35 \& (H)
(Area) CCI-65FP-060100

(H) \& $$
\begin{array}{r}
13.00 \\
12.75- \\
13.00
\end{array}
$$ \& Auto \& 0.0000 <br>

\hline L49 \& 52 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
12.75- \\
13.00
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L49 \& 53 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& $12.75-$

13.00 \& Auto \& 0.0000 <br>

\hline L49 \& 54 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
12.75- \\
13.00
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L49 \& 56 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
12.75- \\
13.00
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L49 \& 57 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
12.75- \\
13.00
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L49 \& 58 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
12.75- \\
13.00
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 29 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 30 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 31 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 33 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& 11.92- \& Auto \& 0.0000 <br>


\hline L50 \& 34 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 35 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 52 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 53 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 54 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 56 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 57 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L50 \& 58 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.92- \\
12.75
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 29 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.67- \\
11.92
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 30 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& $11.67-1$

11.92 \& Auto \& 0.0000 <br>

\hline L51 \& 31 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.67- \\
11.92
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 33 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& $11.67-1$

11.92 \& Auto \& 0.0000 <br>

\hline L51 \& 34 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.67- \\
11.92
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 35 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& $11.67-$

11.92 \& Auto \& 0.0000 <br>

\hline L51 \& 52 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& 11.67-1 \& Auto \& 0.0000 <br>


\hline L51 \& 53 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.67- \\
11.92
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 54 \& | (Area) CCI-65FP-065125 |
| :--- |
| (H) | \& 11.67-1 \& Auto \& 0.0000 <br>


\hline L51 \& 56 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& \[

$$
\begin{array}{r}
11.67- \\
11.92
\end{array}
$$
\] \& Auto \& 0.0000 <br>

\hline L51 \& 57 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& $11.67-$

11.92 \& Auto \& 0.0000 <br>

\hline L51 \& 58 \& | (Area) CCI-65FP-060100 |
| :--- |
| (H) | \& 11.67-1 \& Auto \& 0.0000 <br>

\hline L52 \& 29 \& (Area) CCI-65FP-060100 \& 6.67-11.67 \& Auto \& 0.0000 <br>
\hline L52 \& 30 \& (Area) CCl-65FP-060100 \& 6.67-11.67 \& Auto \& 0.0000 <br>
\hline L52 \& 31 \& (Area) CCl-65FP-060100 \& 6.67-11.67 \& Auto \& 0.0000 <br>
\hline
\end{tabular}

tnxTower Report - version 8.1.1.0

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective Width Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L52 | 33 | $\begin{array}{rr} (\mathrm{H}) \\ \text { (Area) CCI-65FP-060100 } \\ & (\mathrm{H}) \end{array}$ | 9.42-11.67 | Auto | 0.0000 |
| L52 | 34 | (Area) CCI-65FP-060100 <br> (H) | 9.42-11.67 | Auto | 0.0000 |
| L52 | 35 | (Area) CCI-65FP-060100 <br> (H) | 9.42-11.67 | Auto | 0.0000 |
| L52 | 51 | (Area) CCI-65FP-065125 <br> (H) | 6.67-9.25 | Auto | 0.0000 |
| L52 | 52 | (Area) CCI-65FP-065125 | 6.67-11.67 | Auto | 0.0000 |
| L52 | 53 | (Area) CCI-65FP-065125 | 6.67-11.67 | Auto | 0.0000 |
| L52 | 54 | (Area) CCI-65FP-065125 <br> (H) | 6.67-11.67 | Auto | 0.0000 |
| L52 | 56 | (Area) CCI-65FP-060100 <br> (H) | 6.67-11.67 | Auto | 0.0000 |
| L52 | 57 | (Area) CCl-65FP-060100 <br> (H) | 6.67-11.67 | Auto | 0.0000 |
| L52 | 58 | (Area) CCI-65FP-060100 | 6.67-11.67 | Auto | 0.0000 |
| L53 | 29 | (Area) CCl-65FP-060100 | 6.50-6.67 | Auto | 0.0000 |
| L53 | 30 | (Area) CCI-65FP-060100 <br> (H) | 6.50-6.67 | Auto | 0.0000 |
| L53 | 31 | (Area) CCI-65FP-060100 <br> (H) | 6.50-6.67 | Auto | 0.0000 |
| L53 | 51 | (Area) CCI-65FP-065125 <br> (H) | 6.50-6.67 | Auto | 0.0000 |
| L53 | 52 | (Area) CCI-65FP-065125 | 6.50-6.67 | Auto | 0.0000 |
| L53 | 53 | (Area) CCI-65FP-065125 | 6.50-6.67 | Auto | 0.0000 |
| L53 | 54 | (Area) CCI-65FP-065125 <br> (H) | 6.50-6.67 | Auto | 0.0000 |
| L53 | 56 | (Area) CCI-65FP-060100 | 6.50-6.67 | Auto | 0.0000 |
| L53 | 57 | (Area) CCI-65FP-060100 | 6.50-6.67 | Auto | 0.0000 |
| L53 | 58 | (Area) CCI-65FP-060100 <br> (H) | 6.50-6.67 | Auto | 0.0000 |
| L54 | 29 | (Area) CCI-65FP-060100 <br> (H) | 6.25-6.50 | Auto | 0.0000 |
| L54 | 30 | (Area) CCI-65FP-060100 <br> (H) | 6.25-6.50 | Auto | 0.0000 |
| L54 | 31 | (Area) CCI-65FP-060100 | 6.25-6.50 | Auto | 0.0000 |
| L54 | 51 | (Area) CCI-65FP-065125 | 6.25-6.50 | Auto | 0.0000 |
| L54 | 52 | (Area) CCI-65FP-065125 <br> (H) | 6.25-6.50 | Auto | 0.0000 |
| L54 | 53 | (Area) CCI-65FP-065125 | 6.25-6.50 | Auto | 0.0000 |
| L54 | 54 | (Area) CCI-65FP-065125 <br> (H) | 6.25-6.50 | Auto | 0.0000 |
| L54 | 56 | (Area) CCI-65FP-060100 | 6.25-6.50 | Auto | 0.0000 |
| L54 | 57 | (Area) CCI-65FP-060100 | 6.25-6.50 | Auto | 0.0000 |
| L54 | 58 | (Area) CCI-65FP-060100 <br> (H) | 6.25-6.50 | Auto | 0.0000 |
| L55 | 29 | (Area) CCI-65FP-060100 <br> (H) | 3.75-6.25 | Auto | 0.0000 |
| L55 | 30 | (Area) CCI-65FP-060100 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 31 | (Area) CCI-65FP-060100 <br> (H) | 3.75-6.25 | Auto | 0.0000 |
| L55 | 51 | (Area) CCl-65FP-065125 | 3.75-6.25 | Auto | 0.0000 |


| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L55 | 52 | (Area) CCI-65FP-065125 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 53 | (Area) CCI-65FP-065125 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 54 | (Area) CCI-65FP-065125 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 56 | (Area) CCI-65FP-060100 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 57 | (Area) CCI-65FP-060100 | 3.75-6.25 | Auto | 0.0000 |
| L55 | 58 | (Area) CCI-65FP-060100 | 3.75-6.25 | Auto | 0.0000 |
| L56 | 29 | (Area) CCI-65FP-060100 <br> (H) | 3.50-3.75 | Auto | 0.0000 |
| L56 | 30 | (Area) CCI-65FP-060100 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 31 | (Area) CCI-65FP-060100 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 51 | (Area) CCI-65FP-065125 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 52 | (Area) CCl-65FP-065125 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 53 |  | 3.50-3.75 | Auto | 0.0000 |
| L56 | 5 | (H) | 3.50-3.75 | Auto | 0.0000 |
| L56 | 54 | (Area) CCI-65FP-065125 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 56 | $\begin{array}{r} (\mathrm{H}) \\ \text { (Area) CCI-65FP-060100 } \end{array}$ | 3.50-3.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L56 | 57 | (Area) CCI-65FP-060100 | 3.50-3.75 | Auto | 0.0000 |
| L56 | 58 | (Area) CCl-65FP-060100 | 3.50-3.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L57 | 29 |  | 3.00-3.50 | Auto | 0.0000 |
|  | 30 | (Area) CCI-65FP-060100 |  |  |  |
| L57 | 30 | (Area) CCl-65FP-060100 | 3.00-3.50 | Auto | 0.0000 |
| L57 | 31 | (Area) CCl-65FP-060100 | 3.00-3.50 | Auto | 0.0000 |
| L57 | 51 | (Area) CCI-65FP-065125 | 3.00-3.50 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L57 | 52 | (Area) CCl-65FP-065125 | 3.00-3.50 | Auto | 0.0000 |
| L57 | 53 | (Area) CCI-65FP-065125 | 3.00-3.50 | Auto | 0.0000 |
| L57 | 53 | (H) | 3.00-3.50 | Auto | 0.0000 |
| L57 | 54 | (Area) CCI-65FP-065125 | 3.00-3.50 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L57 | 56 | (Area) CCI-65FP-060100 | 3.00-3.50 | Auto | 0.0000 |
| L57 | 57 | (Area) CCI-65FP-060100 | 3.00-3.50 | Auto | 0.0000 |
|  |  |  |  |  |  |
| L57 | 58 | (Area) CCI-65FP-060100 | 3.00-3.50 | Auto | 0.0000 |
| L58 | 29 | $(\mathrm{H})$ | 2.75-3.00 | Auto | 0.0000 |
|  | 29 | $(\mathrm{H})$ | 2.75-3.00 | Auto | 0.0000 |
| L58 | 30 | (Area) CCl-65FP-060100 | 2.75-3.00 | Auto | 0.0000 |
|  |  | $(\mathrm{H})$ |  |  |  |
| L58 | 31 | (Area) CCI-65FP-060100 <br> (H) | 2.75-3.00 | Auto | 0.0000 |
| L58 | 51 | (Area) CCI-65FP-065125 | 2.75-3.00 | Auto | 0.0000 |
| L58 | 52 | (Area) CCI-65FP-065125 | 2.75-3.00 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L58 | 53 | (Area) CCI-65FP-065125 | 2.75-3.00 | Auto | 0.0000 |
| L58 | 54 | (Area) CCI-65FP-065125 | 2.75-3.00 | Auto | 0.0000 |
|  |  |  |  |  |  |
| L58 | 56 | (Area) CCI-65FP-060100 | 2.75-3.00 | Auto | 0.0000 |

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

| Tower Section | Attachment Record No. | Description | Attachment Segment Elev. | Ratio Calculatio $n$ Method | Effective <br> Width <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (H) |  |  |  |
| L58 | 57 | (Area) CCI-65FP-060100 | 2.75-3.00 | Auto | 0.0000 |
| L58 | 58 | (H) | 2.75-3.00 | Auto | 0.0000 |
|  |  |  |  |  |  |
| L59 | 29 | (Area) CCl-65FP-060100 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L59 | 30 | (Area) CCI-65FP-060100 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (Area) CCI-65FP-060100 |  |  |  |
| L59 | 31 | (Area) CCI-65FP-060100 <br> (H) | 0.00-2.75 | Auto | 0.0000 |
| L59 | 51 | (Area) CCI-65FP-065125 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L59 | 52 | (Area) CCI-65FP-065125 | 0.00-2.75 | Auto | 0.0000 |
| L59 | 53 | (Area) CCl-65FP-065125 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L59 | 54 | (Area) CCl-65FP-065125 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L59 | 56 | (Area) CCl-65FP-060100 | 0.00-2.75 | Auto | 0.0000 |
| L59 | 57 | (Area) CCl-65FP-060100 | 0.00-2.75 | Auto | 0.0000 |
|  |  | (H) |  |  |  |
| L59 | 58 | (Area) CCI-65FP-060100 | 0.00-2.75 | Auto | 0.0000 |


| Discrete Tower Loads |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: | Azimuth | Placement |
|  |  |  | Horz | Adjustment |  |
|  |  |  | Lateral |  |  |
|  |  |  | Vert |  |  |
|  |  |  | ft ft | - | $f$ |
|  |  |  | ft |  |  |
| 80010798 w/ Mount Pipe | A | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| 80010798 w/ Mount Pipe | B | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| 80010798 w/ Mount Pipe | C | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| (2) $80010965 \mathrm{w} / \mathrm{Mount}$ Pipe | A | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| (2) $80010965 \mathrm{w} / \mathrm{Mount}$ Pipe | B | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| (2) $80010965 \mathrm{w} / \mathrm{Mount}$ Pipe | C | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| 80010121 w/ Mount Pipe | A | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| 80010121 w/ Mount Pipe | B | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |
|  |  |  | -1.00 |  |  |
| 80010121 w/ Mount Pipe | C | From Leg | 4.0000 | 0.00 | 121.0000 |
|  |  |  | 0.00 |  |  |

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|}
\hline Description \& \[
\begin{aligned}
\& \text { Face } \\
\& \text { or } \\
\& \text { Leg }
\end{aligned}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert \\
ft \\
\(f t\)
\end{tabular} \& Azimuth Adjustment \& Placement

ft <br>

\hline RRUS E2 B29 \& A \& From Leg \& | -1.00 4.0000 0.00 |
| :--- |
| -1.00 | \& 0.00 \& 121.0000 <br>

\hline RRUS E2 B29 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS E2 B29 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 8843 B2/B66A \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 8843 B2/B66A \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 8843 B2/B66A \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline DC6-48-60-18-8F \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline DC6-48-60-18-8F \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline (2) DC6-48-60-18-8F \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 32 B30 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 32 B30 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 32 B30 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4478 B14 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4478 B14 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4478 B14 \& c \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4449 B5/B12 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4449 B5/B12 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline RRUS 4449 B5/B12 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline (2) LGP21401 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline (2) LGP21401 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline (2) LGP21401 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
-1.00
\end{gathered}
$$ \& 0.00 \& 121.0000 <br>

\hline (2) 2.4" Dia $\times 6$-ft Pipe (Horizontal) \& A \& From Leg \& 4.0000 \& 0.00 \& 121.0000 <br>
\hline
\end{tabular}

130 Ft Monopole Tower Structural Analysis

| Description | Face or Leg | Offset <br> Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustment | Placement <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 0.00 \\ & 0.00 \end{aligned}$ |  |  |
| (2) 2.4" Dia $\times 6$-ft Pipe (Horizontal) | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 121.0000 |
| (2) 2.4" Dia x 6-ft Pipe (Horizontal) | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 121.0000 |
| Side Arm Mount [SO 102-3] | C | None |  | 0.00 | 121.0000 |
| Platform Mount [LP 602-1] | C | None |  | 0.00 | 121.0000 |
| (2) SBNHH-1D65B w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| (2) SBNHH-1D65B w/ Mount Pipe | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| (2) SBNHH-1D65B w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| BXA-80063/4CF w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| BXA-80063/4CF w/ Mount Pipe | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| BXA-80063/4CF w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 | 109.0000 |
| CBRS w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| CBRS w/ Mount Pipe | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| CBRS w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| MT6407-77A w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 4.00 \end{gathered}$ | 0.00 | 109.0000 |
| MT6407-77A w/ Mount Pipe | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 4.00 \end{gathered}$ | 0.00 | 109.0000 |
| MT6407-77A w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 4.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D1A | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D1A | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D1A | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D2A | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D2A | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |
| RFV01U-D2A | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 109.0000 |

\begin{tabular}{|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustment \& Placement

ft <br>

\hline RUSDC-6267-PF-48 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 109.0000 <br>

\hline | Site Pro 1 F3P-HRK12 |
| :--- |
| Site Pro 1 F3P-12[W] | \& \[

$$
\begin{aligned}
& C \\
& C
\end{aligned}
$$

\] \& None None \& \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 109.0000 \\
& 109.0000
\end{aligned}
$$
\] <br>

\hline 800MHz 2X50W RRH W/FILTER \& A \& From Leg \&  \& 0.00 \& 99.0000 <br>

\hline 800MHz 2X50W RRH W/FILTER \& B \& From Leg \& $$
\begin{gathered}
2.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 99.0000 <br>

\hline 800MHz 2X50W RRH W/FILTER \& C \& From Leg \& $$
\begin{gathered}
2.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 99.0000 <br>

\hline PCS 1900MHz 4x45W-65MHz w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
2.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 99.0000 <br>

\hline PCS 1900MHz 4x45W-65MHz w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
2.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 99.0000 <br>

\hline PCS 1900MHz 4x45W-65MHz w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
2.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 99.0000 <br>

\hline Side Arm Mount [SO 101-3] \& C \& None \& \& 0.00 \& 99.0000 <br>

\hline LLPX310R-V1 w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline LLPX310R-V1 w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline LLPX310R-V1 w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline TIMING 2000 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline RRH-2WB \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline RRH-2WB \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline RRH-2WB \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline HORIZON COMPACT \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline HORIZON COMPACT

$* *$ \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline APXVSPP18-C-A20 w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline APXVSPP18-C-A20 w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline APXVSPP18-C-A20 w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
1.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline APXVTM14-ALU-I20 w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00
\end{gathered}
$$ \& 0.00 \& 97.0000 <br>

\hline
\end{tabular}

| Description | Face or Leg | Offset <br> Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustment | Placement <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: |
| APXVTM14-ALU-I20 w/ Mount Pipe | B | From Leg | $\begin{gathered} 1.00 \\ 4.0000 \\ 0.00 \\ 1.00 \end{gathered}$ | 0.00 | 97.0000 |
| APXVTM14-ALU-I20 w/ Mount Pipe | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 1.00 \end{gathered}$ | 0.00 | 97.0000 |
| TD-RRH8X20-25 | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 97.0000 |
| TD-RRH8X20-25 | B | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 97.0000 |
| TD-RRH8X20-25 | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 97.0000 |
| Platform Mount [LP 713-1] | C | None |  | 0.00 | 97.0000 |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe | A | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe | B | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| ERICSSON AIR 21 B2A B4P w/ Mount Pipe | C | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| APXVAARR24_43-U-NA20 w/ Mount Pipe | A | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| APXVAARR24_43-U-NA20 w/ Mount Pipe | B | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| APXVAARR24_43-U-NA20 w/ Mount Pipe | C | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| AIR -32 B2A/B66AA w/ Mount Pipe | A | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| AIR -32 B2A/B66AA w/ Mount Pipe | B | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| AIR -32 B2A/B66AA w/ Mount Pipe | C | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| KRY 112 144/1 | A | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| KRY 112 144/1 | A | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| KRY 112 144/1 | B | From Face | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| RADIO 4449 B12/B71 | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| (2) RADIO 4449 B12/B71 | C | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 87.0000 |
| T-Arm Mount [TA 602-3] | C | None |  | 0.00 | 87.0000 |
| MX08FRO665-21 w/ Mount Pipe | A | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 0.00 \end{gathered}$ | 0.00 | 77.0000 |

130 Ft Monopole Tower Structural Analysis

\begin{tabular}{|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustment \& Placement

ft <br>

\hline MX08FRO665-21 w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline MX08FRO665-21 w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B604 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B604 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B604 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B605 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B605 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline TA08025-B605 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline RDIDC-9181-PF-48 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline (2) 8' x 2" Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline (2) 8' x 2" Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline (2) 8' x 2" Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 77.0000 <br>

\hline Commscope MC-PK8-DSH \& C \& None \& \& 0.00 \& 77.0000 <br>
\hline
\end{tabular}

## Dishes

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Dish Type \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft \& Azimuth Adjustment \& \begin{tabular}{l}
\(3 d B\) \\
Beam \\
Width
\end{tabular} \& Elevation

ft \& | Outside Diameter |
| :--- |
| ft | <br>

\hline VHLP2.5-18 \& B \& Paraboloid w/Shroud (HP) \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
6.00
\end{gathered}
$$ \& 0.00 \& \& 97.0000 \& 2.5000 <br>

\hline VHLP2-18

**** \& C \& Paraboloid w/o Radome \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
6.00
\end{gathered}
$$ \& 0.00 \& \& 97.0000 \& 2.1750 <br>

\hline
\end{tabular}

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

## Maximum Member Forces

| Sectio <br> $n$ | Elevation <br> ft | Component <br> Type | Condition | Gov. <br> Load | Axial | Major Axis <br> Moment | Minor Axis <br> Moment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  |  |  | Comb. | K | kip-ft |  |

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

| Sectio $n$ No. | Elevation $f t$ | Component Type | Condition | Gov. <br> Load <br> Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 120-115 | Pole | Max. Vy | 8 | 8.03 | -5.04 | -0.04 |
|  |  |  | Max. Vx | 2 | -8.02 | 0.06 | 5.07 |
|  |  |  | Max. Torque | 24 |  |  | 0.24 |
|  |  |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -15.72 | 0.27 | -0.17 |
|  |  |  | Max. Mx | 20 | -4.36 | 46.10 | -0.00 |
|  |  |  | Max. My | 14 | -4.38 | 0.01 | -46.00 |
|  |  |  | Max. Vy | 8 | 8.33 | -45.97 | -0.03 |
|  |  |  | Max. Vx | 2 | -8.32 | 0.04 | 45.93 |
|  | 115-110 |  | Max. Torque | 24 |  |  | 0.24 |
| L4 |  | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -16.34 | 0.08 | -0.07 |
|  |  |  | Max. Mx | 20 | -4.62 | 88.49 | 0.03 |
|  |  |  | Max. My | 14 | -4.64 | -0.05 | -88.34 |
|  |  |  | Max. Vy | 8 | 8.64 | -88.42 | -0.02 |
|  |  |  | Max. Vx | 2 | -8.63 | 0.01 | 88.31 |
|  |  |  | Max. Torque | 2 |  |  | 0.21 |
| L5 | 110-105 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -28.05 | -2.73 | 1.07 |
|  |  |  | Max. Mx | 8 | -9.02 | -156.62 | 0.25 |
|  |  |  | Max. My | 2 | -9.06 | -0.78 | 155.83 |
|  |  |  | Max. Vy | 8 | 13.53 | -156.62 | 0.25 |
|  |  |  | Max. Vx | 2 | -13.50 | -0.78 | 155.83 |
|  |  |  | Max. Torque | 24 |  |  | -0.97 |
| L6 | 105-100 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -29.05 | -2.95 | 0.67 |
|  |  |  | Max. Mx | 8 | -9.52 | -226.84 | -0.22 |
|  |  |  | Max. My | 2 | -9.57 | -0.56 | 225.27 |
|  |  |  | Max. Vy | 8 | 14.41 | -226.84 | -0.22 |
|  |  |  | Max. Vx | 2 | -14.28 | -0.56 | 225.27 |
|  |  |  | Max. Torque | 4 |  |  | -1.58 |
| L7 | 100-95 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -40.97 | -3.17 | 0.65 |
|  |  |  | Max. Mx | 8 | -13.48 | -312.22 | -0.46 |
|  |  |  | Max. My | 2 | -13.54 | -0.35 | 309.89 |
|  |  |  | Max. Vy | 8 | 19.43 | -312.22 | -0.46 |
|  |  |  | Max. Vx | 2 | -19.27 | -0.35 | 309.89 |
|  |  |  | Max. Torque | 4 |  |  | -1.60 |
| L8 | 95-90 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -41.99 | -3.37 | 0.82 |
|  |  |  | Max. Mx | 8 | -14.14 | -410.00 | -0.65 |
|  |  |  | Max. My | 2 | -14.19 | -0.12 | 406.90 |
|  |  |  | Max. Vy | 8 | 19.71 | -410.00 | -0.65 |
|  |  |  | Max. Vx | 2 | -19.56 | -0.12 | $406.90$ |
|  |  |  | Max. Torque | 4 |  |  | -1.60 |
| L9 | 90-89.75 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -42.07 | -3.38 | 0.83 |
|  |  |  | Max. Mx | 8 | -14.20 | -414.93 | -0.65 |
|  |  |  | Max. My | 2 | -14.26 | -0.11 | 411.79 |
|  |  |  | Max. Vy | 8 | 19.71 | -414.93 | -0.65 |
|  |  |  | Max. Vx | 2 | -19.56 | -0.11 | 411.79 |
|  |  |  | Max. Torque | 4 |  |  | -1.60 |
| L10 | $\begin{gathered} 89.75- \\ 84.75 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -51.43 | -2.20 | 1.32 |
|  |  |  | Max. Mx | 8 | -17.92 | -520.85 | -0.67 |
|  |  |  | Max. My | 2 | -17.98 | 0.72 | 517.53 |
|  |  |  | Max. Vy | 8 | 23.23 | -520.85 | -0.67 |
|  |  |  | Max. Vx | 2 | -22.99 | 0.72 | $517.53$ |
|  |  |  | Max. Torque | 4 |  |  | -1.60 |
| L11 | $\begin{gathered} 84.75- \\ 84.58 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -51.50 | -2.22 | 1.34 |
|  |  |  | Max. Mx | 8 | -17.97 | -524.81 | -0.67 |
|  |  |  | Max. My | 2 | -18.03 | 0.72 | 521.44 |
|  |  |  | Max. Vy | 8 | 23.25 | -524.81 | -0.67 |
|  |  |  | Max. Vx | 2 | -23.00 | 0.72 | 521.44 |
|  |  |  | Max. Torque | 4 |  |  | -1.22 |
| L12 | 84.58 - | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1


130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1


130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1


130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis
Project Number 1963271, Order 556638, Revision 1


130 Ft Monopole Tower Structural Analysis

| $\begin{gathered} \text { Sectio } \\ n \\ \text { No. } \\ \hline \end{gathered}$ | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L59 | 2.75-0 | Pole | Max. Mx | 8 | -56.31 | -3142.36 | -1.15 |
|  |  |  | Max. My | 2 | -56.32 | -0.25 | 2952.14 |
|  |  |  | Max. Vy | 8 | 37.01 | -3142.36 | -1.15 |
|  |  |  | Max. Vx | 24 | -35.10 | 1692.92 | 2904.55 |
|  |  |  | Max. Torque | 10 |  |  | 2.16 |
|  |  |  | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -115.61 | -13.74 | 9.29 |
|  |  |  | Max. Mx | 8 | -57.87 | -3244.73 | -1.14 |
|  |  |  | Max. My | 2 | -57.88 | -0.32 | 3044.56 |
|  |  |  | Max. Vy | 8 | 37.32 | -3244.73 | -1.14 |
|  |  |  | Max. Vx | 24 | -35.38 | 1749.27 | 3001.55 |
|  |  |  | Max. Torque | 10 |  |  | 2.23 |

## Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical K | $\begin{gathered} \text { Horizontal, } X \\ K \end{gathered}$ | $\begin{gathered} \text { Horizontal, Z } \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 31 | 115.61 | -8.95 | -5.11 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 20 | 57.89 | 37.29 | 0.21 |
|  | Max. $\mathrm{Hz}_{\mathrm{z}}$ | 24 | 57.89 | 20.65 | 35.36 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 3044.56 | 0.05 | 33.68 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 8 | 3244.73 | -37.29 | -0.04 |
|  | Max. Torsion | 10 | 2.23 | -36.73 | -20.95 |
|  | Min. Vert | 17 | 43.42 | 16.84 | -29.27 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 57.89 | -37.29 | -0.04 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 12 | 57.89 | -20.58 | -35.30 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -3026.87 | -0.19 | -33.58 |
|  | Min. $\mathrm{Mz}_{\mathrm{z}}$ | 20 | -3231.90 | 37.29 | 0.21 |
|  | Min. Torsion | 22 | -1.95 | 36.63 | 21.13 |

Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $_{x}$ $K$ | Shear ${ }_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 48.24 | 0.00 | 0.00 | -3.03 | -5.08 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg - | 57.89 | -0.05 | -33.68 | -3044.56 | -0.32 | 0.83 |
| No Ice 0.9 Dead+1.0 Wind 0 deg No Ice | 43.42 | -0.05 | -33.68 | -3013.21 | 1.22 | 0.80 |
| 1.2 Dead+1.0 Wind 30 deg No Ice | 57.89 | 17.07 | -29.24 | -2637.53 | -1547.07 | 1.46 |
| 0.9 Dead+1.0 Wind 30 deg No Ice | 43.42 | 17.07 | -29.24 | -2610.30 | -1530.10 | 1.43 |
| 1.2 Dead+1.0 Wind 60 deg No Ice | 57.89 | 30.62 | -17.45 | -1547.67 | -2722.35 | 0.93 |
| 0.9 Dead+1.0 Wind 60 deg No Ice | 43.42 | 30.62 | -17.45 | -1531.45 | -2693.88 | 0.92 |
| 1.2 Dead+1.0 Wind 90 deg No Ice | 57.89 | 37.29 | 0.04 | 1.14 | -3244.73 | -0.14 |
| 0.9 Dead+1.0 Wind 90 deg No Ice | 43.42 | 37.29 | 0.04 | 2.04 | -3211.50 | -0.14 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice | 57.89 | 36.73 | 20.95 | 1743.96 | -3080.61 | -2.23 |
| 0.9 Dead+1.0 Wind 120 deg <br> - No Ice | 43.42 | 36.73 | 20.95 | 1728.13 | -3049.44 | -2.20 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No Ice | 57.89 | 20.58 | 35.30 | 2987.96 | -1754.47 | -1.84 |
| 0.9 Dead+1.0 Wind 150 deg <br> - No Ice | 43.42 | 20.58 | 35.30 | 2959.95 | -1735.92 | -1.81 |


| Load Combination | Vertical | Shear $_{x}$ K | Shear $_{z}$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 Dead+1.0 Wind 180 deg <br> - No Ice | 57.89 | 0.19 | 33.58 | 3026.87 | -26.48 | -0.75 |
| 0.9 Dead+1.0 Wind 180 deg <br> - No Ice | 43.42 | 0.19 | 33.58 | 2997.54 | -24.66 | -0.72 |
| 1.2 Dead+1.0 Wind 210 deg <br> - No Ice | 57.89 | -16.84 | 29.27 | 2633.56 | 1509.92 | -1.03 |
| 0.9 Dead+1.0 Wind 210 deg <br> - No Ice | 43.42 | -16.84 | 29.27 | 2608.20 | 1496.41 | -1.00 |
| 1.2 Dead+1.0 Wind 240 deg <br> - No Ice | 57.89 | -30.59 | 17.34 | 1528.80 | 2707.33 | -0.73 |
| 0.9 Dead+1.0 Wind 240 deg <br> - No Ice | 43.42 | -30.59 | 17.34 | 1514.62 | 2682.10 | -0.72 |
| 1.2 Dead+1.0 Wind 270 deg <br> - No Ice | 57.89 | -37.29 | -0.21 | -26.56 | 3231.90 | -0.28 |
| 0.9 Dead+1.0 Wind 270 deg <br> - No Ice | 43.42 | -37.29 | -0.21 | -25.36 | 3201.88 | -0.29 |
| 1.2 Dead+1.0 Wind 300 deg <br> - No Ice | 57.89 | -36.63 | -21.13 | -1771.58 | 3057.24 | 1.95 |
| 0.9 Dead+1.0 Wind 300 deg <br> - No lce | 43.42 | -36.63 | -21.13 | -1753.62 | 3029.40 | 1.93 |
| 1.2 Dead+1.0 Wind 330 deg <br> - No Ice | 57.89 | -20.65 | -35.36 | -3001.55 | 1749.27 | 1.84 |
| 0.9 Dead+1.0 Wind 330 deg <br> - No Ice | 43.42 | -20.65 | -35.36 | -2971.57 | 1733.87 | 1.81 |
| 1.2 Dead+1.0 Ice+1.0 Temp | 115.61 | 0.00 | -0.00 | -9.29 | -13.74 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp | 115.61 | -0.01 | -8.63 | -841.30 | -13.02 | 0.19 |
| 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp | 115.61 | 4.34 | -7.45 | -726.77 | -432.54 | 0.32 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp | 115.61 | 7.53 | -4.30 | -423.35 | -739.55 | 0.20 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 115.61 | 9.06 | 0.01 | -8.64 | -877.20 | -0.07 |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 115.61 | 8.95 | 5.11 | 454.04 | -827.10 | -0.62 |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp | 115.61 | 5.08 | 8.73 | 789.71 | -479.51 | -0.53 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp | 115.61 | 0.04 | 8.61 | 820.30 | -17.95 | -0.17 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp | 115.61 | -4.30 | 7.46 | 708.75 | 399.45 | -0.23 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp | 115.61 | -7.53 | 4.28 | 402.16 | 711.20 | -0.16 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp | 115.61 | -9.05 | -0.04 | -14.04 | 849.33 | -0.02 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp | 115.61 | -8.93 | -5.15 | -477.19 | 796.91 | 0.56 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp | 115.61 | -5.09 | -8.74 | -809.73 | 453.36 | 0.53 |
| Dead+Wind 0 deg - Service | 48.24 | -0.01 | -7.32 | -660.43 | -3.90 | 0.17 |
| Dead+Wind 30 deg - Service | 48.24 | 3.71 | -6.35 | -572.45 | -338.26 | 0.31 |
| Dead+Wind 60 deg - Service | 48.24 | 6.65 | -3.79 | -336.86 | -592.34 | 0.20 |
| Dead+Wind 90 deg - Service | 48.24 | 8.10 | 0.01 | -2.04 | -705.30 | -0.03 |
| Dead+Wind 120 deg Service | 48.24 | 7.98 | 4.55 | 374.79 | -669.89 | -0.48 |
| Dead+Wind 150 deg Service | 48.24 | 4.47 | 7.67 | 643.73 | -383.15 | -0.39 |
| Dead+Wind 180 deg Service | 48.24 | 0.04 | 7.30 | 652.04 | -9.54 | -0.16 |
| Dead+Wind 210 deg Service | 48.24 | -3.66 | 6.36 | 567.02 | 322.58 | -0.22 |
| Dead+Wind 240 deg Service | 48.24 | -6.65 | 3.77 | 328.22 | 581.43 | -0.16 |
| Dead+Wind 270 deg Service | 48.24 | -8.10 | -0.05 | -8.01 | 694.87 | -0.07 |
| Dead+Wind 300 deg Service | 48.24 | -7.96 | -4.59 | -385.32 | 657.19 | 0.42 |
| Dead+Wind 330 deg Service | 48.24 | -4.48 | -7.68 | -651.24 | 374.37 | 0.39 |

## Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ | PY | $P Z$ |  |
| Comb. | K | K | K | K | K | K |  |
| 1 | 0.00 | -48.24 | 0.00 | 0.00 | 48.24 | 0.00 | 0.000\% |
| 2 | -0.05 | -57.89 | -33.68 | 0.05 | 57.89 | 33.68 | 0.000\% |
| 3 | -0.05 | -43.42 | -33.68 | 0.05 | 43.42 | 33.68 | 0.000\% |
| 4 | 17.07 | -57.89 | -29.24 | -17.07 | 57.89 | 29.24 | 0.000\% |
| 5 | 17.07 | -43.42 | -29.24 | -17.07 | 43.42 | 29.24 | 0.000\% |
| 6 | 30.62 | -57.89 | -17.45 | -30.62 | 57.89 | 17.45 | 0.000\% |
| 7 | 30.62 | -43.42 | -17.45 | -30.62 | 43.42 | 17.45 | 0.000\% |
| 8 | 37.29 | -57.89 | 0.04 | -37.29 | 57.89 | -0.04 | 0.000\% |
| 9 | 37.29 | -43.42 | 0.04 | -37.29 | 43.42 | -0.04 | 0.000\% |
| 10 | 36.73 | -57.89 | 20.95 | -36.73 | 57.89 | -20.95 | 0.000\% |
| 11 | 36.73 | -43.42 | 20.95 | -36.73 | 43.42 | -20.95 | 0.000\% |
| 12 | 20.58 | -57.89 | 35.30 | -20.58 | 57.89 | -35.30 | 0.000\% |
| 13 | 20.58 | -43.42 | 35.30 | -20.58 | 43.42 | -35.30 | 0.000\% |
| 14 | 0.19 | -57.89 | 33.58 | -0.19 | 57.89 | -33.58 | 0.000\% |
| 15 | 0.19 | -43.42 | 33.58 | -0.19 | 43.42 | -33.58 | 0.000\% |
| 16 | -16.84 | -57.89 | 29.27 | 16.84 | 57.89 | -29.27 | 0.000\% |
| 17 | -16.84 | -43.42 | 29.27 | 16.84 | 43.42 | -29.27 | 0.000\% |
| 18 | -30.59 | -57.89 | 17.34 | 30.59 | 57.89 | -17.34 | 0.000\% |
| 19 | -30.59 | -43.42 | 17.34 | 30.59 | 43.42 | -17.34 | 0.000\% |
| 20 | -37.29 | -57.89 | -0.21 | 37.29 | 57.89 | 0.21 | 0.000\% |
| 21 | -37.29 | -43.42 | -0.21 | 37.29 | 43.42 | 0.21 | 0.000\% |
| 22 | -36.63 | -57.89 | -21.13 | 36.63 | 57.89 | 21.13 | 0.000\% |
| 23 | -36.63 | -43.42 | -21.13 | 36.63 | 43.42 | 21.13 | 0.000\% |
| 24 | -20.65 | -57.89 | -35.36 | 20.65 | 57.89 | 35.36 | 0.000\% |
| 25 | -20.65 | -43.42 | -35.36 | 20.65 | 43.42 | 35.36 | 0.000\% |
| 26 | 0.00 | -115.61 | 0.00 | -0.00 | 115.61 | 0.00 | 0.000\% |
| 27 | -0.01 | -115.61 | -8.63 | 0.01 | 115.61 | 8.63 | 0.000\% |
| 28 | 4.34 | -115.61 | -7.45 | -4.34 | 115.61 | 7.45 | 0.000\% |
| 29 | 7.53 | -115.61 | -4.30 | -7.53 | 115.61 | 4.30 | 0.000\% |
| 30 | 9.06 | -115.61 | 0.01 | -9.06 | 115.61 | -0.01 | 0.000\% |
| 31 | 8.95 | -115.61 | 5.11 | -8.95 | 115.61 | -5.11 | 0.000\% |
| 32 | 5.08 | -115.61 | 8.73 | -5.08 | 115.61 | -8.73 | 0.000\% |
| 33 | 0.04 | -115.61 | 8.61 | -0.04 | 115.61 | -8.61 | 0.000\% |
| 34 | -4.30 | -115.61 | 7.46 | 4.30 | 115.61 | -7.46 | 0.000\% |
| 35 | -7.53 | -115.61 | 4.28 | 7.53 | 115.61 | -4.28 | 0.000\% |
| 36 | -9.05 | -115.61 | -0.04 | 9.05 | 115.61 | 0.04 | 0.000\% |
| 37 | -8.93 | -115.61 | -5.15 | 8.93 | 115.61 | 5.15 | 0.000\% |
| 38 | -5.09 | -115.61 | -8.74 | 5.09 | 115.61 | 8.74 | 0.000\% |
| 39 | -0.01 | -48.24 | -7.32 | 0.01 | 48.24 | 7.32 | 0.000\% |
| 40 | 3.71 | -48.24 | -6.35 | -3.71 | 48.24 | 6.35 | 0.000\% |
| 41 | 6.65 | -48.24 | -3.79 | -6.65 | 48.24 | 3.79 | 0.000\% |
| 42 | 8.10 | -48.24 | 0.01 | -8.10 | 48.24 | -0.01 | 0.000\% |
| 43 | 7.98 | -48.24 | 4.55 | -7.98 | 48.24 | -4.55 | 0.000\% |
| 44 | 4.47 | -48.24 | 7.67 | -4.47 | 48.24 | -7.67 | 0.000\% |
| 45 | 0.04 | -48.24 | 7.30 | -0.04 | 48.24 | -7.30 | 0.000\% |
| 46 | -3.66 | -48.24 | 6.36 | 3.66 | 48.24 | -6.36 | 0.000\% |
| 47 | -6.65 | -48.24 | 3.77 | 6.65 | 48.24 | -3.77 | 0.000\% |
| 48 | -8.10 | -48.24 | -0.05 | 8.10 | 48.24 | 0.05 | 0.000\% |
| 49 | -7.96 | -48.24 | -4.59 | 7.96 | 48.24 | 4.59 | 0.000\% |
| 50 | -4.48 | -48.24 | -7.68 | 4.48 | 48.24 | 7.68 | 0.000\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 4 | 0.00000001 | 0.00001188 |
| 2 | Yes | 5 | 0.00000001 | 0.00060782 |
| 3 | Yes | 5 | 0.00000001 | 0.00024556 |
| 4 | Yes | 6 | 0.00000001 | 0.00075608 |

tnxTower Report - version 8.1.1.0

| 5 | Yes | 6 | 0.00000001 | 0.00024215 |
| :---: | :---: | :---: | :---: | :---: |
| 6 | Yes | 6 | 0.00000001 | 0.00072486 |
| 7 | Yes | 6 | 0.00000001 | 0.00022958 |
| 8 | Yes | 5 | 0.00000001 | 0.00039397 |
| 9 | Yes | 5 | 0.00000001 | 0.00013813 |
| 10 | Yes | 6 | 0.00000001 | 0.00083181 |
| 11 | Yes | 6 | 0.00000001 | 0.00025252 |
| 12 | Yes | 6 | 0.00000001 | 0.00087223 |
| 13 | Yes | 6 | 0.00000001 | 0.00026763 |
| 14 | Yes | 5 | 0.00000001 | 0.00083910 |
| 15 | Yes | 5 | 0.00000001 | 0.00035795 |
| 16 | Yes | 6 | 0.00000001 | 0.00069845 |
| 17 | Yes | 6 | 0.00000001 | 0.00022355 |
| 18 | Yes | 6 | 0.00000001 | 0.00073864 |
| 19 | Yes | 6 | 0.00000001 | 0.00023617 |
| 20 | Yes | 5 | 0.00000001 | 0.00041322 |
| 21 | Yes | 5 | 0.00000001 | 0.00014581 |
| 22 | Yes | 6 | 0.00000001 | 0.00087700 |
| 23 | Yes | 6 | 0.00000001 | 0.00026776 |
| 24 | Yes | 6 | 0.00000001 | 0.00082836 |
| 25 | Yes | 6 | 0.00000001 | 0.00025233 |
| 26 | Yes | 5 | 0.00000001 | 0.00064639 |
| 27 | Yes | 7 | 0.00000001 | 0.00052425 |
| 28 | Yes | 7 | 0.00000001 | 0.00057550 |
| 29 | Yes | 7 | 0.00000001 | 0.00057759 |
| 30 | Yes | 7 | 0.00000001 | 0.00054038 |
| 31 | Yes | 7 | 0.00000001 | 0.00062174 |
| 32 | Yes | 7 | 0.00000001 | 0.00061698 |
| 33 | Yes | 7 | 0.00000001 | 0.00051279 |
| 34 | Yes | 7 | 0.00000001 | 0.00054591 |
| 35 | Yes | 7 | 0.00000001 | 0.00054808 |
| 36 | Yes | 7 | 0.00000001 | 0.00051948 |
| 37 | Yes | 7 | 0.00000001 | 0.00061213 |
| 38 | Yes | 7 | 0.00000001 | 0.00061018 |
| 39 | Yes | 5 | 0.00000001 | 0.00007799 |
| 40 | Yes | 5 | 0.00000001 | 0.00023649 |
| 41 | Yes | 5 | 0.00000001 | 0.00021324 |
| 42 | Yes | 5 | 0.00000001 | 0.00007679 |
| 43 | Yes | 5 | 0.00000001 | 0.00025900 |
| 44 | Yes | 5 | 0.00000001 | 0.00028933 |
| 45 | Yes | 5 | 0.00000001 | 0.00007749 |
| 46 | Yes | 5 | 0.00000001 | 0.00019608 |
| 47 | Yes | 5 | 0.00000001 | 0.00021940 |
| 48 | Yes | 5 | 0.00000001 | 0.00007583 |
| 49 | Yes | 5 | 0.00000001 | 0.00028896 |
| 50 | Yes | 5 | 0.00000001 | 0.00025450 |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | o |
| :---: | :---: | :---: | :---: | :---: | :---: | | ft | 20.91 | 43 | 1.64 | 0.00 |
| :---: | :---: | :---: | :---: | :---: |
| L1 | $130-125$ | 19.19 | 43 | 1.64 |
| L2 | $125-120$ | 17.47 | 43 | 1.64 |
| L3 | $120-115$ | 15.77 | 43 | 1.60 |
| L4 | $115-110$ | 14.13 | 43 | 1.52 |
| L5 | $110-105$ | 12.59 | 43 | 1.42 |
| L6 | $105-100$ | $100-95$ | $95-90$ | 9.87 |
| L8 | $90-89.75$ | 8.72 | 43 | 1.30 |
| L9 | $89.75-84.75$ | 8.67 | 43 | 1.17 |
| L10 | $84.75-84.58$ | 7.65 | 43 | 1.02 |
| L11 | $84.58-84.33$ | 7.62 | 43 | 1.01 |
| L12 | $84.33-83.42$ | 7.57 | 43 | 0.93 |
| L13 | $83.42-83.17$ | 7.40 | 43 | 0.92 |
| L15 | $83.17-83$ | 7.35 | 43 | 0.92 |
| L16 | $83-82.75$ | 7.32 | 43 | 0.91 |


| Section No. | Elevation ft | Horz. Deflection in | Gov. Load Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L17 | 82.75-77.75 | 7.27 | 43 | 0.90 | 0.00 |
| L18 | 77.75-70 | 6.36 | 43 | 0.83 | 0.00 |
| L19 | 74-69 | 5.73 | 43 | 0.78 | 0.00 |
| L20 | 69-67.08 | 4.93 | 43 | 0.74 | 0.00 |
| L21 | 67.08-66.83 | 4.64 | 43 | 0.71 | 0.00 |
| L22 | 66.83-64.08 | 4.60 | 43 | 0.71 | 0.00 |
| L23 | 64.08-63.83 | 4.21 | 43 | 0.67 | 0.00 |
| L24 | 63.83-62.5 | 4.17 | 43 | 0.66 | 0.00 |
| L25 | 62.5-62.25 | 3.99 | 43 | 0.65 | 0.00 |
| L26 | 62.25-57.25 | 3.96 | 43 | 0.64 | 0.00 |
| L27 | 57.25-53.5 | 3.31 | 43 | 0.58 | 0.00 |
| L28 | 53.5-53.25 | 2.88 | 43 | 0.54 | 0.00 |
| L29 | 53.25-52.58 | 2.85 | 43 | 0.53 | 0.00 |
| L30 | 52.58-52.33 | 2.77 | 43 | 0.53 | 0.00 |
| L31 | 52.33-47.33 | 2.75 | 43 | 0.52 | 0.00 |
| L32 | 47.33-44.58 | 2.23 | 43 | 0.47 | 0.00 |
| L33 | 44.58-44.33 | 1.97 | 43 | 0.43 | 0.00 |
| L34 | 44.33-41.92 | 1.95 | 43 | 0.43 | 0.00 |
| L35 | 41.92-41.67 | 1.74 | 43 | 0.40 | 0.00 |
| L36 | 41.67-34.08 | 1.72 | 43 | 0.40 | 0.00 |
| L37 | 39-34 | 1.50 | 43 | 0.37 | 0.00 |
| L38 | 34-29 | 1.13 | 43 | 0.34 | 0.00 |
| L39 | 29-26.92 | 0.81 | 43 | 0.28 | 0.00 |
| L40 | 26.92-26.67 | 0.69 | 43 | 0.26 | 0.00 |
| L41 | 26.67-21.67 | 0.68 | 43 | 0.25 | 0.00 |
| L42 | 21.67-18 | 0.44 | 43 | 0.20 | 0.00 |
| L43 | 18-17.75 | 0.30 | 43 | 0.16 | 0.00 |
| L44 | 17.75-17.5 | 0.29 | 43 | 0.16 | 0.00 |
| L45 | 17.5-17.25 | 0.28 | 43 | 0.16 | 0.00 |
| L46 | 17.25-17.08 | 0.27 | 43 | 0.16 | 0.00 |
| L47 | 17.08-16.83 | 0.27 | 43 | 0.16 | 0.00 |
| L48 | 16.83-13 | 0.26 | 43 | 0.15 | 0.00 |
| L49 | 13-12.75 | 0.15 | 43 | 0.12 | 0.00 |
| L50 | 12.75-11.92 | 0.15 | 43 | 0.12 | 0.00 |
| L51 | 11.92-11.67 | 0.13 | 43 | 0.11 | 0.00 |
| L52 | 11.67-6.67 | 0.12 | 43 | 0.11 | 0.00 |
| L53 | 6.67-6.5 | 0.04 | 43 | 0.05 | 0.00 |
| L54 | 6.5-6.25 | 0.04 | 43 | 0.05 | 0.00 |
| L55 | 6.25-3.75 | 0.03 | 43 | 0.05 | 0.00 |
| L56 | 3.75-3.5 | 0.01 | 43 | 0.03 | 0.00 |
| L57 | 3.5-3 | 0.01 | 43 | 0.03 | 0.00 |
| L58 | 3-2.75 | 0.01 | 43 | 0.02 | 0.00 |
| L59 | 2.75-0 | 0.01 | 43 | 0.02 | 0.00 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 121.0000 | 80010798 w/ Mount Pipe | 43 | 17.81 | 1.64 | 0.00 | 25121 |
| 109.0000 | (2) SBNHH-1D65B w/ Mount Pipe | 43 | 13.82 | 1.50 | 0.00 | 3077 |
| 103.0000 | VHLP2.5-18 | 43 | 12.01 | 1.38 | 0.00 | 2482 |
| 99.0000 | 800MHz 2X50W RRH W/FILTER | 43 | 10.89 | 1.28 | 0.00 | 2195 |
| 97.0000 | LLPX310R-V1 w/ Mount Pipe | 43 | 10.37 | 1.23 | 0.00 | 2089 |
| 87.0000 | ERICSSON AIR 21 B2A B4P w/ Mount Pipe | 43 | 8.10 | 0.97 | 0.00 | 3231 |
| 77.0000 | MX08FRO665-21 w/ Mount Pipe | 43 | 6.23 | 0.82 | 0.00 | 4443 |

## Maximum Tower Deflections - Design Wind

| Section No. | Elevation ft | Horz. <br> Deflection in | Gov. Load Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 130-125 | 96.17 | 10 | 7.58 | 0.02 |
| L2 | 125-120 | 88.28 | 10 | 7.57 | 0.02 |
| L3 | 120-115 | 80.40 | 10 | 7.56 | 0.02 |
| L4 | 115-110 | 72.59 | 10 | 7.37 | 0.02 |
| L5 | 110-105 | 65.10 | 10 | 6.98 | 0.02 |
| L6 | 105-100 | 58.03 | 10 | 6.55 | 0.02 |
| L7 | 100-95 | 51.47 | 10 | 6.01 | 0.02 |
| L8 | 95-90 | 45.52 | 10 | 5.39 | 0.01 |
| L9 | 90-89.75 | 40.25 | 10 | 4.70 | 0.01 |
| L10 | 89.75-84.75 | 40.00 | 10 | 4.68 | 0.01 |
| L11 | 84.75-84.58 | 35.31 | 10 | 4.28 | 0.01 |
| L12 | 84.58-84.33 | 35.16 | 10 | 4.27 | 0.01 |
| L13 | 84.33-83.42 | 34.94 | 10 | 4.25 | 0.01 |
| L14 | 83.42-83.17 | 34.14 | 10 | 4.20 | 0.01 |
| L15 | 83.17-83 | 33.92 | 10 | 4.18 | 0.01 |
| L16 | 83-82.75 | 33.77 | 10 | 4.18 | 0.01 |
| L17 | 82.75-77.75 | 33.55 | 10 | 4.16 | 0.01 |
| L18 | 77.75-70 | 29.36 | 10 | 3.85 | 0.00 |
| L19 | 74-69 | 26.44 | 10 | 3.61 | 0.00 |
| L20 | 69-67.08 | 22.75 | 10 | 3.41 | 0.00 |
| L21 | 67.08-66.83 | 21.41 | 10 | 3.28 | 0.00 |
| L22 | 66.83-64.08 | 21.24 | 10 | 3.27 | 0.00 |
| L23 | 64.08-63.83 | 19.41 | 10 | 3.08 | 0.00 |
| L24 | 63.83-62.5 | 19.25 | 10 | 3.06 | 0.00 |
| L25 | 62.5-62.25 | 18.41 | 10 | 2.98 | 0.00 |
| L26 | 62.25-57.25 | 18.25 | 10 | 2.97 | 0.00 |
| L27 | 57.25-53.5 | 15.30 | 10 | 2.69 | 0.00 |
| L28 | 53.5-53.25 | 13.27 | 10 | 2.48 | 0.00 |
| L29 | 53.25-52.58 | 13.14 | 10 | 2.46 | 0.00 |
| L30 | 52.58-52.33 | 12.80 | 10 | 2.43 | 0.00 |
| L31 | 52.33-47.33 | 12.67 | 10 | 2.41 | 0.00 |
| L32 | 47.33-44.58 | 10.28 | 10 | 2.15 | 0.00 |
| L33 | 44.58-44.33 | 9.09 | 10 | 2.00 | 0.00 |
| L34 | 44.33-41.92 | 8.98 | 10 | 1.98 | 0.00 |
| L35 | 41.92-41.67 | 8.02 | 10 | 1.85 | 0.00 |
| L36 | 41.67-34.08 | 7.92 | 10 | 1.84 | 0.00 |
| L37 | 39-34 | 6.93 | 10 | 1.70 | 0.00 |
| L38 | 34-29 | 5.22 | 10 | 1.56 | 0.00 |
| L39 | 29-26.92 | 3.73 | 10 | 1.29 | 0.00 |
| L40 | 26.92-26.67 | 3.19 | 10 | 1.18 | 0.00 |
| L41 | 26.67-21.67 | 3.13 | 10 | 1.17 | 0.00 |
| L42 | 21.67-18 | 2.03 | 10 | 0.93 | 0.00 |
| L43 | 18-17.75 | 1.38 | 10 | 0.76 | 0.00 |
| L44 | 17.75-17.5 | 1.34 | 10 | 0.75 | 0.00 |
| L45 | 17.5-17.25 | 1.31 | 10 | 0.74 | 0.00 |
| L46 | 17.25-17.08 | 1.27 | 10 | 0.73 | 0.00 |
| L47 | 17.08-16.83 | 1.24 | 10 | 0.72 | 0.00 |
| L48 | 16.83-13 | 1.20 | 10 | 0.71 | 0.00 |
| L49 | 13-12.75 | 0.70 | 10 | 0.54 | 0.00 |
| L50 | 12.75-11.92 | 0.67 | 10 | 0.53 | 0.00 |
| L51 | 11.92-11.67 | 0.58 | 10 | 0.50 | 0.00 |
| L52 | 11.67-6.67 | 0.56 | 10 | 0.49 | 0.00 |
| L53 | 6.67-6.5 | 0.17 | 10 | 0.25 | 0.00 |
| L54 | 6.5-6.25 | 0.16 | 10 | 0.25 | 0.00 |
| L55 | 6.25-3.75 | 0.15 | 10 | 0.24 | 0.00 |
| L56 | 3.75-3.5 | 0.05 | 10 | 0.13 | 0.00 |
| L57 | 3.5-3 | 0.05 | 10 | 0.13 | 0.00 |
| L58 | 3-2.75 | 0.03 | 10 | 0.11 | 0.00 |
| L59 | 2.75-0 | 0.03 | 10 | 0.10 | 0.00 |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Load |  |  |  |  |
| ft | Comb. | in | $\circ$ |  | 0 | $f t$ |


| Elevation <br> ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 121.0000 | 80010798 w/ Mount Pipe | 10 | 81.97 | 7.57 | 0.02 | 5796 |
| 109.0000 | (2) SBNHH-1D65B w/ Mount Pipe | 10 | 63.65 | 6.90 | 0.02 | 693 |
| 103.0000 | VHLP2.5-18 | 10 | 55.34 | 6.34 | 0.02 | 559 |
| 99.0000 | 800MHz 2X50W RRH W/FILTER | 10 | 50.23 | 5.89 | 0.01 | 491 |
| 97.0000 | LLPX310R-V1 w/ Mount Pipe | 10 | 47.82 | 5.66 | 0.01 | 466 |
| 87.0000 | ERICSSON AIR 21 B2A B4P w/ Mount Pipe | 10 | 37.37 | 4.47 | 0.01 | 711 |
| 77.0000 | MX08FRO665-21 w/ Mount Pipe | 10 | 28.76 | 3.80 | 0.00 | 971 |

## Compression Checks

## Pole Design Data

| Section No. | Elevation | Size | L | $L_{u}$ | Kl/r | $A$ | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | ft | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| L1 | 130-125 (1) | TP11.775 $\times 10.525 \times 0.1875$ | 5.0000 | 0.0000 | 0.0 | 6.9960 | -0.10 | 409.26 | 0.000 |
| L2 | 125-120 (2) | TP13.025x11.775x0.1875 | 5.0000 | 0.0000 | 0.0 | 7.7506 | -15.07 | 453.41 | 0.033 |
| L3 | 120-115 (3) | TP14.275x13.025x0.1875 | 5.0000 | 0.0000 | 0.0 | 8.5053 | -4.27 | 497.56 | 0.009 |
| L4 | 115-110 (4) | TP15.525x14.275x0.1875 | 5.0000 | 0.0000 | 0.0 | 9.2600 | -4.50 | 541.71 | 0.008 |
| L5 | 110-105 (5) | TP16.7758×15.525x0.25 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 13.303 \\ 2 \end{gathered}$ | -8.84 | 778.24 | 0.011 |
| L6 | 105-100 (6) | TP18.0265x16.7758×0.25 | 5.0000 | 0.0000 | 0.0 | $14.310$ | -9.33 | 837.14 | 0.011 |
| L7 | 100-95 (7) | TP19.2773x18.0265×0.25 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 15.316 \\ 9 \end{gathered}$ | -13.25 | 896.04 | 0.015 |
| L8 | 95-90 (8) | TP20.528×19.2773x0.25 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 16.323 \\ 8 \end{gathered}$ | -13.91 | 954.94 | 0.015 |
| L9 | 90-89.75 (9) | TP20.5905x20.528×0.5 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 32.345 \\ 8 \end{gathered}$ | -13.98 | 1892.23 | 0.007 |
| L10 | $89.75-84.75$ (10) | TP21.8413×20.5905×0.48 13 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 33.100 \\ 0 \end{gathered}$ | -17.69 | 1936.35 | 0.009 |
| L11 | $84.75-84.58$ (11) | $\underset{5}{\mathrm{TP} 21.8838 \times 21.8413 \times 0.47}$ | 0.1700 | 0.0000 | 0.0 | $\begin{gathered} 32.744 \\ 8 \end{gathered}$ | -17.74 | 1915.57 | 0.009 |
| L12 | $84.58-84.33$ (12) | $\begin{gathered} \text { TP21.9464×21.8838×0.63 } \\ 75 \end{gathered}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 43.741 \\ 7 \end{gathered}$ | -17.81 | 2558.89 | 0.007 |
| L13 | $84.33-83.42$ (13) | TP22.174×21.9464x0.625 | 0.9100 | 0.0000 | 0.0 | $\begin{gathered} 43.367 \\ 3 \end{gathered}$ | -18.02 | 2536.99 | 0.007 |
| L14 | $83.42-83.17$ <br> (14) | TP22.2365x22.174×0.95 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 65.115 \\ 5 \end{gathered}$ | -18.11 | 3809.26 | 0.005 |
| L15 | $\begin{gathered} 83.17-83 \\ (15) \end{gathered}$ | TP22.2791 $\times 22.2365 \times 0.95$ | 0.1700 | 0.0000 | 0.0 | $\begin{gathered} 65.245 \\ 6 \end{gathered}$ | -18.17 | 3816.87 | 0.005 |
| L16 | $\begin{gathered} 83-82.75 \\ (16) \end{gathered}$ | TP22.3416x22.2791x0.7 | 0.2500 | 0.0000 | 0.0 | $48.780$ | -18.23 | 2853.64 | 0.006 |
| L17 | $82.75-77.75$ <br> (17) | TP23.5923 $\times 22.3416 \times 0.66$ 25 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 48.915 \\ 1 \end{gathered}$ | -19.52 | 2861.53 | 0.007 |
| L18 | $\begin{gathered} 77.75-70 \\ (18) \end{gathered}$ | TP25.531x23.5923x0.65 | 7.7500 | 0.0000 | 0.0 | $\begin{gathered} 49.981 \\ 7 \end{gathered}$ | -23.55 | 2923.93 | 0.008 |
| L19 | 70-69(19) | TP25.281×24.0304×0.7 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 55.405 \\ 5 \end{gathered}$ | -25.74 | 3241.22 | 0.008 |
| L20 | $\begin{gathered} 69-67.08 \\ (20) \end{gathered}$ | $\begin{gathered} \text { TP } 25.7612 \times 25.281 \times 0.687 \\ 5 \end{gathered}$ | 1.9200 | 0.0000 | 0.0 | $\begin{gathered} 55.506 \\ 9 \end{gathered}$ | -26.31 | 3247.15 | 0.008 |
| L21 | $67.08-66.83$ (21) | $\begin{gathered} \text { TP25.8237×25.7612x0.68 } \\ 75 \end{gathered}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 55.645 \\ 3 \end{gathered}$ | -26.42 | 3255.25 | 0.008 |
| L22 | 66.83-64.08 (22) | $\begin{gathered} \text { TP26.5115×25.8237×0.67 } \\ 5 \end{gathered}$ | 2.7500 | 0.0000 | 0.0 | $\begin{gathered} 56.155 \\ 7 \end{gathered}$ | -27.25 | 3285.11 | 0.008 |
| L23 | $\begin{gathered} 64.08-63.83 \\ \text { (23) } \end{gathered}$ | $\begin{gathered} \text { TP26.5741×26.5115×0.73 } \\ 75 \end{gathered}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 61.355 \\ 4 \end{gathered}$ | -27.35 | 3589.29 | 0.008 |
| L24 | $63.83-62.5$ | $\begin{gathered} \text { TP26.9067×26.5741×0.73 } \\ 75 \end{gathered}$ | 1.3300 | 0.0000 | 0.0 | $62.145$ | -27.80 | 3635.50 | 0.008 |
| L25 | 62.5-62.25 | TP26.9693x26.9067×0.86 | 0.2500 | 0.0000 | 0.0 | 72.505 | -27.91 | 4241.54 | 0.007 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation <br> ft | Size | $L$ $f t$ | $L_{u}$ ft | Kl/r | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (25) | 25 |  |  |  | 0 |  |  |  |
| L26 | $\begin{gathered} 62.25-57.25 \\ (26) \end{gathered}$ | $\begin{gathered} \text { TP28.2198×26.9693×0.83 } \\ 75 \end{gathered}$ | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 73.843 \\ 3 \end{gathered}$ | -29.71 | 4319.83 | 0.007 |
| L27 | $\begin{gathered} 57.25-53.5 \\ (27) \end{gathered}$ | $25$ | 3.7500 | 0.0000 | 0.0 | $\begin{gathered} 74.158 \\ 3 \end{gathered}$ | -31.10 | 4338.26 | 0.007 |
| L28 | $\begin{gathered} 53.5-53.25 \\ (28) \end{gathered}$ | $\begin{gathered} \text { TP29.2203×29.1578×0.83 } \\ 75 \end{gathered}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 76.541 \\ 3 \end{gathered}$ | -31.21 | 4477.67 | 0.007 |
| L29 | $\begin{gathered} 53.25-52.58 \\ (29) \end{gathered}$ | TP29.3879×29.2203×0.82 | 0.6700 | 0.0000 | 0.0 | $\begin{gathered} 75.877 \\ 3 \end{gathered}$ | -31.47 | 4438.82 | 0.007 |
| L30 | $\begin{gathered} 52.58-52.33 \\ (30) \end{gathered}$ | TP29.4504×29.3879×0.86 25 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 79.395 \\ 7 \end{gathered}$ | -31.57 | 4644.65 | 0.007 |
| L31 | $\begin{gathered} 52.33-47.33 \\ (31) \end{gathered}$ | TP30.701×29.4504×0.837 5 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 80.534 \\ 3 \end{gathered}$ | -33.52 | 4711.26 | 0.007 |
| L32 | $\begin{gathered} 47.33-44.58 \\ (32) \end{gathered}$ | TP31.3888×30.701×0.812 5 | 2.7500 | 0.0000 | 0.0 | $\begin{gathered} 79.995 \\ 2 \end{gathered}$ | -34.62 | 4679.72 | 0.007 |
| L33 | $\begin{gathered} 44.58-44.33 \\ (33) \end{gathered}$ | $\begin{aligned} & \text { TP31.4513×31.3888×0.81 } \\ & 25 \end{aligned}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 80.158 \\ 8 \end{gathered}$ | -34.74 | 4689.29 | 0.007 |
| L34 | $\begin{gathered} 44.33-41.92 \\ (34) \end{gathered}$ | TP32.0541x31.4513x0.8 | 2.4100 | 0.0000 | 0.0 | $\begin{gathered} 80.510 \\ 6 \end{gathered}$ | -35.70 | 4709.87 | 0.008 |
| L35 | $\begin{gathered} 41.92-41.67 \\ (35) \end{gathered}$ | $\begin{aligned} & \text { TP32.1166x32.0541×0.81 } \\ & 25 \end{aligned}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 81.899 \\ 4 \end{gathered}$ | -35.82 | 4791.12 | 0.007 |
| L36 | $\begin{gathered} 41.67-34.08 \\ (36) \end{gathered}$ | TP34.015x32.1166x0.787 <br> 5 | 7.5900 | 0.0000 | 0.0 | $\begin{gathered} 81.136 \\ 2 \end{gathered}$ | -36.90 | 4746.47 | 0.008 |
| L37 | $\begin{gathered} 34.08-34 \\ (37) \end{gathered}$ | $\begin{aligned} & \text { TP33.4082×32.1594×0.81 } \\ & 88 \end{aligned}$ | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 85.918 \\ 1 \end{gathered}$ | -40.57 | 5026.21 | 0.008 |
| L38 | 34-29(38) | $\begin{gathered} \text { TP34.657x33.4082x0.793 } \\ 8 \end{gathered}$ | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 86.550 \\ 3 \end{gathered}$ | -42.74 | 5063.19 | 0.008 |
| L39 | $\begin{gathered} 29-26.92 \\ (39) \end{gathered}$ | TP35.1765x34.657×0.793 8 | 2.0800 | 0.0000 | 0.0 | $\begin{gathered} 87.878 \\ 0 \end{gathered}$ | -43.66 | 5140.87 | 0.008 |
| L40 | $\begin{gathered} 26.92-26.67 \\ (40) \end{gathered}$ | TP35.239x35.1765x0.893 8 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 98.841 \\ 2 \end{gathered}$ | -43.79 | 5782.21 | 0.008 |
| L41 | $\begin{gathered} 26.67-21.67 \\ (41) \end{gathered}$ | TP36.4877x35.239×0.868 8 | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 99.639 \\ 7 \end{gathered}$ | -46.23 | 5828.92 | 0.008 |
| L42 | $\begin{gathered} 21.67-18 \\ (42) \end{gathered}$ | TP37.4044×36.4877×0.85 63 | 3.6700 | 0.0000 | 0.0 | $\begin{gathered} 100.76 \\ 80 \end{gathered}$ | -48.05 | 5894.91 | 0.008 |
| L43 | $18-17.75$ | TP37.4668×37.4044×0.99 $38$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 116.70 \\ 90 \end{gathered}$ | -48.21 | 6827.49 | 0.007 |
| L44 | $\begin{gathered} 17.75-17.5 \\ (44) \end{gathered}$ | TP37.5292×37.4668×0.99 38 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 116.90 \\ 90 \end{gathered}$ | -48.35 | 6839.18 | 0.007 |
| L45 | $\begin{gathered} 17.5-17.25 \\ (45) \end{gathered}$ | TP37.5917×37.5292x0.99 38 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 117.10 \\ 90 \end{gathered}$ | -48.48 | 6850.86 | 0.007 |
| L46 | $\begin{gathered} 17.25-17.08 \\ (46) \end{gathered}$ | $\begin{gathered} \text { TP37.6341×37.5917×0.99 } \\ 38 \end{gathered}$ | 0.1700 | 0.0000 | 0.0 | $\begin{gathered} 117.24 \\ 50 \end{gathered}$ | -48.58 | 6858.81 | 0.007 |
| L47 | $\begin{gathered} 17.08-16.83 \\ (47) \end{gathered}$ | TP37.6966x37.6341×0.89 38 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 105.91 \\ 40 \end{gathered}$ | -48.70 | 6195.96 | 0.008 |
| L48 | $\begin{gathered} 16.83-13 \\ (48) \end{gathered}$ | TP38.6531x37.6966x0.88 <br> 13 | 3.8300 | 0.0000 | 0.0 | $\begin{gathered} 107.18 \\ 20 \end{gathered}$ | -50.67 | 6270.17 | 0.008 |
| L49 | $\begin{aligned} & 13-12.75 \\ & (49) \end{aligned}$ | TP38.7156x38.6531×1.05 63 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 128.08 \\ 40 \end{gathered}$ | -50.83 | 7492.92 | 0.007 |
| L50 | $\begin{gathered} 12.75-11.92 \\ (50) \end{gathered}$ | $\begin{aligned} & \text { TP38.9229×38.7156x1.04 } \\ & 38 \end{aligned}$ | 0.8300 | 0.0000 | 0.0 | $\begin{gathered} 127.30 \\ 70 \end{gathered}$ | -51.31 | 7447.46 | 0.007 |
| L51 | $\begin{gathered} 11.92-11.67 \\ (51) \end{gathered}$ | TP38.9853×38.9229×0.81 88 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 100.62 \\ 10 \end{gathered}$ | -51.45 | 5886.35 | 0.009 |
| L52 | $\begin{gathered} 11.67-6.67 \\ (52) \end{gathered}$ | $\begin{gathered} \text { TP40.2341×38.9853×0.79 } \\ 38 \end{gathered}$ | 5.0000 | 0.0000 | 0.0 | $\begin{gathered} 99.527 \\ 9 \end{gathered}$ | -53.04 | 5822.38 | 0.009 |
| L53 | 6.67-6.5 (53) | $\begin{gathered} \text { TP40.2766×40.2341×0.79 } \\ 38 \end{gathered}$ | 0.1700 | 0.0000 | 0.0 | $\begin{gathered} 100.80 \\ 50 \end{gathered}$ | -54.08 | 5897.07 | 0.009 |
| L54 | 6.5-6.25 (54) | TP40.339x40.2766x0.918 8 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 116.43 \\ 50 \end{gathered}$ | -54.17 | 6811.46 | 0.008 |
| L55 | $6.25-3.75$ | TP40.9634×40.339×0.906 <br> 3 | 2.5000 | 0.0000 | 0.0 | $\begin{gathered} 115.07 \\ 00 \end{gathered}$ | -54.33 | 6731.58 | 0.008 |
| L56 | 3.75-3.5 (56) | TP41.0258×40.9634×1.00 63 | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 129.46 \\ 60 \end{gathered}$ | -55.72 | 7573.77 | 0.007 |
| L57 | 3.5-3 (57) | TP41.1507×41.0258×0.99 38 | 0.5000 | 0.0000 | 0.0 | $\begin{gathered} 128.09 \\ 80 \end{gathered}$ | -55.87 | 7493.72 | 0.007 |
| L58 | 3-2.75 (58) | $\begin{aligned} & \text { TP41.2132×41.1507×0.99 } \\ & 38 \end{aligned}$ | 0.2500 | 0.0000 | 0.0 | $\begin{gathered} 128.49 \\ 70 \end{gathered}$ | -56.16 | 7517.09 | 0.007 |
| L59 | 2.75-0 (59) | TP41.9x41.2132x1.0188 | 2.7500 | 0.0000 | 0.0 | $\begin{gathered} 131.85 \\ 30 \end{gathered}$ | -56.32 | 7713.39 | 0.007 |


| Section <br> No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio <br> $P_{u}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | $K$ | $K$ |  |

## Pole Bending Design Data

| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio Mux | $M_{u y}$ | $\phi M_{n y}$ | Ratio Muy |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | kip-ft | kip-ft | $\phi M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| L1 | 130-125 (1) | TP11.775x10.525x0.1875 | 0.63 | 120.74 | 0.005 | 0.00 | 120.74 | 0.000 |
| L2 | 125-120 (2) | TP13.025x11.775x0.1875 | 2.28 | 148.43 | 0.015 | 0.00 | 148.43 | 0.000 |
| L3 | 120-115 (3) | TP14.275x13.025x0.1875 | 46.78 | 178.97 | 0.261 | 0.00 | 178.97 | 0.000 |
| L4 | 115-110 (4) | TP15.525x14.275x0.1875 | 91.06 | 212.37 | 0.429 | 0.00 | 212.37 | 0.000 |
| L5 | 110-105 (5) | TP16.7758x15.525x0.25 | 161.84 | 327.79 | 0.494 | 0.00 | 327.79 | 0.000 |
| L6 | 105-100 (6) | TP18.0265x16.7758x0.25 | 236.53 | 379.69 | 0.623 | 0.00 | 379.69 | 0.000 |
| L7 | 100-95 (7) | TP19.2773x18.0265x0.25 | 327.43 | 435.39 | 0.752 | 0.00 | 435.39 | 0.000 |
| L8 | 95-90 (8) | TP20.528x19.2773x0.25 | 431.90 | 494.91 | 0.873 | 0.00 | 494.91 | 0.000 |
| L9 | 90-89.75 (9) | TP20.5905x20.528x0.5 | 437.20 | 959.70 | 0.456 | 0.00 | 959.70 | 0.000 |
| L10 | $\begin{gathered} 89.75-84.75 \\ (10) \end{gathered}$ | TP21.8413×20.5905x0.48 13 | 551.23 | 1046.54 | 0.527 | 0.00 | 1046.54 | 0.000 |
| L11 | $84.75-84.58$ <br> (11) | $\begin{gathered} \text { TP21.8838×21.8413×0.47 } \\ 5 \end{gathered}$ | 555.47 | 1038.02 | 0.535 | 0.00 | 1038.02 | 0.000 |
| L12 | $84.58-84.33$ <br> (12) | TP21.9464×21.8838×0.63 75 | 561.71 | 1369.79 | 0.410 | 0.00 | 1369.79 | 0.000 |
| L13 | $84.33-83.42$ <br> (13) | TP22.174x21.9464x0.625 | 584.50 | 1374.59 | 0.425 | 0.00 | 1374.59 | 0.000 |
| L14 | $83.42-83.17$ <br> (14) | TP22.2365x22.174×0.95 | 590.79 | 2008.30 | 0.294 | 0.00 | 2008.30 | 0.000 |
| L15 | $\begin{gathered} 83.17-83 \\ (15) \end{gathered}$ | TP22.2791x22.2365x0.95 | 595.07 | 2016.50 | 0.295 | 0.00 | 2016.50 | 0.000 |
| L16 | $\begin{gathered} 83-82.75 \\ (16) \end{gathered}$ | TP22.3416x22.2791x0.7 | 601.37 | 1547.78 | 0.389 | 0.00 | 1547.78 | 0.000 |
| L17 | $\begin{gathered} 82.75-77.75 \\ (17) \end{gathered}$ | $\begin{aligned} & \text { TP23.5923×22.3416x0.66 } \\ & 25 \end{aligned}$ | 729.73 839.17 | 1649.97 | 0.442 | 0.00 | 1649.97 1758.70 | 0.000 |
| L18 | $\begin{gathered} 77.75-70 \\ (18) \end{gathered}$ | TP25.531x23.5923x0.65 | 839.17 | 1758.70 | 0.477 | 0.00 | 1758.70 | 0.000 |
| L19 | 70-69 (19) | TP25.281x24.0304x0.7 | 992.27 | 2004.28 | 0.495 | 0.00 | 2004.28 | 0.000 |
| L20 | $\begin{gathered} 69-67.08 \\ (20) \end{gathered}$ | TP25.7612×25.281×0.687 5 | 1052.27 | 2050.31 | 0.513 | 0.00 | 2050.31 | 0.000 |
| L21 | $\begin{gathered} 67.08-66.83 \\ (21) \end{gathered}$ | $\begin{gathered} \text { TP25.8237×25.7612×0.68 } \\ 75 \end{gathered}$ | 1060.13 | 2060.68 | 0.514 | 0.00 | 2060.68 | 0.000 |
| L22 | $\begin{gathered} 66.83-64.08 \\ (22) \end{gathered}$ | TP26.5115×25.8237×0.67 | 1147.24 | 2140.07 | 0.536 | 0.00 | 2140.07 | 0.000 |
| L23 | $\begin{gathered} 64.08-63.83 \\ (23) \end{gathered}$ | $\begin{gathered} \text { TP26.5741×26.5115×0.73 } \\ 75 \end{gathered}$ | 1155.22 | 2332.73 | 0.495 | 0.00 | 2332.73 | 0.000 |
| L24 | $\begin{gathered} 63.83-62.5 \\ (24) \end{gathered}$ | $\begin{gathered} \text { TP26.9067×26.5741×0.73 } \\ 75 \end{gathered}$ | 1197.88 | 2394.04 | 0.500 | 0.00 | 2394.04 | 0.000 |
| L25 | $\begin{gathered} 62.5-62.25 \\ (25) \end{gathered}$ | TP26.9693x26.9067x0.86 25 | 1205.93 | 2773.36 | 0.435 | 0.00 | 2773.36 | 0.000 |
| L26 | $\begin{gathered} 62.25-57.25 \\ (26) \end{gathered}$ | TP28.2198×26.9693x0.83 75 | 1369.28 | 2969.61 | 0.461 | 0.00 | 2969.61 | 0.000 |
| L27 | $\begin{gathered} 57.25-53.5 \\ (27) \end{gathered}$ | TP29.1578×28.2198×0.81 25 | 1494.67 | 3092.92 | 0.483 | 0.00 | 3092.92 | 0.000 |
| L28 | $\begin{gathered} 53.5-53.25 \\ (28) \end{gathered}$ | $\begin{gathered} \text { TP29.2203×29.1578×0.83 } \\ 75 \end{gathered}$ | 1503.12 | 3193.91 | 0.471 | 0.00 | 3193.91 | 0.000 |
| L29 | $\begin{gathered} 53.25-52.58 \\ (29) \end{gathered}$ | $\begin{gathered} \text { TP29.3879×29.2203×0.82 } \\ 5 \end{gathered}$ | 1525.81 | 3188.22 | 0.479 | 0.00 | 3188.22 | 0.000 |
| L30 | $\begin{gathered} 52.58-52.33 \\ (30) \end{gathered}$ | TP29.4504×29.3879×0.86 $25$ | 1534.30 | 3334.82 | 0.460 | 0.00 | 3334.82 | 0.000 |
| L31 | $\begin{gathered} 52.33-47.33 \\ (31) \end{gathered}$ | $\begin{gathered} \mathrm{TP} 30.701 \times 29.4504 \times 0.837 \\ 5 \end{gathered}$ | 1706.34 | 3540.88 | 0.482 | 0.00 | 3540.88 | 0.000 |
| L32 | $\begin{gathered} 47.33-44.58 \\ (32) \end{gathered}$ | TP31.3888x30.701×0.812 5 | 1802.83 | 3606.29 | 0.500 | 0.00 | 3606.29 | 0.000 |
| L33 | $\begin{gathered} 44.58-44.33 \\ (33) \end{gathered}$ | $\begin{aligned} & \text { TP31.4513×31.3888×0.81 } \\ & 25 \end{aligned}$ | 1811.66 | 3621.24 | 0.500 | 0.00 | 3621.24 | 0.000 |
| L34 | $\begin{gathered} 44.33-41.92 \\ (34) \end{gathered}$ | TP32.0541x31.4513x0.8 | 1897.38 | 3713.51 | 0.511 | 0.00 | 3713.51 | 0.000 |
| L35 | 41.92-41.67 | TP32.1166x32.0541x0.81 | 1906.33 | 3782.29 | 0.504 | 0.00 | 3782.29 | 0.000 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation <br> ft | Size | $M_{u x}$ <br> kip-ft | $\phi M_{n x}$ | Ratio Mux $\phi M_{n x}$ | Muy <br> kip-ft | $\phi M_{n y}$ | Ratio Muy $\phi M_{n y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\phi M$ |  |  | $\phi M_{n y}$ |
|  | (35) | 25 |  |  |  |  |  |  |
| L36 | $\begin{gathered} 41.67-34.08 \\ (36) \end{gathered}$ | TP34.015×32.1166x0.787 | 2002.53 | 3835.00 | 0.522 | 0.00 | 3835.00 | 0.000 |
| L37 | $\begin{gathered} 34.08-34 \\ (37) \end{gathered}$ | $\begin{aligned} & \text { TP33.4082×32.1594×0.81 } \\ & 88 \end{aligned}$ | 2186.20 | 4134.16 | 0.529 | 0.00 | 4134.16 | 0.000 |
| L38 | 34-29(38) | TP34.657×33.4082×0.793 8 | 2374.21 | 4334.48 | 0.548 | 0.00 | 4334.48 | 0.000 |
| L39 | $\begin{gathered} 29-26.92 \\ (39) \end{gathered}$ | TP35.1765 $34.657 \times 0.793$ 8 | 2453.58 | 4470.03 | 0.549 | 0.00 | 4470.03 | 0.000 |
| L40 | $\begin{gathered} 26.92-26.67 \\ (40) \end{gathered}$ | TP35.239×35.1765×0.893 8 | 2463.17 | 5007.82 | 0.492 | 0.00 | 5007.82 | 0.000 |
| L41 | $\begin{gathered} 26.67-21.67 \\ (41) \end{gathered}$ | TP36.4877×35.239×0.868 8 | 2656.96 | 5243.85 | 0.507 | 0.00 | 5243.85 | 0.000 |
| L42 | $\begin{gathered} 21.67-18 \\ (42) \end{gathered}$ | TP37.4044×36.4877×0.85 63 | 2801.68 | 5446.66 | 0.514 | 0.00 | 5446.66 | 0.000 |
| L43 | $\begin{gathered} 18-17.75 \\ (43) \end{gathered}$ | TP37.4668×37.4044x0.99 38 | 2811.62 | 6271.97 | 0.448 | 0.00 | 6271.97 | 0.000 |
| L44 | $\begin{gathered} 17.75-17.5 \\ (44) \end{gathered}$ | TP37.5292×37.4668×0.99 38 | 2821.56 | 6293.75 | 0.448 | 0.00 | 6293.75 | 0.000 |
| L45 | $17.5-17.25$ <br> (45) | $\begin{gathered} \text { TP37.5917×37.5292×0.99 } \\ 38 \end{gathered}$ | 2831.51 | 6315.56 | 0.448 | 0.00 | 6315.56 | 0.000 |
| L46 | $\begin{gathered} 17.25-17.08 \\ (46) \end{gathered}$ | TP37.6341×37.5917×0.99 38 | 2838.28 | 6330.42 | 0.448 | 0.00 | 6330.42 | 0.000 |
| L47 | $\begin{gathered} 17.08-16.83 \\ (47) \end{gathered}$ | $\begin{gathered} \text { TP37.6966×37.6341×0.89 } \\ 38 \end{gathered}$ | 2848.25 | 5759.90 | 0.494 | 0.00 | 5759.90 | 0.000 |
| L48 | $\begin{gathered} 16.83-13 \\ (48) \end{gathered}$ | TP38.6531×37.6966x0.88 13 | 3002.09 | 5987.94 | 0.501 | 0.00 | 5987.94 | 0.000 |
| L49 | $\begin{gathered} 13-12.75 \\ (49) \end{gathered}$ | TP38.7156x38.6531×1.05 63 | 3012.21 | 7101.60 | 0.424 | 0.00 | 7101.60 | 0.000 |
| L50 | $\begin{gathered} 12.75-11.92 \\ (50) \end{gathered}$ | TP38.9229×38.7156×1.04 38 | 3045.86 | 7103.12 | 0.429 | 0.00 | 7103.12 | 0.000 |
| L51 | $\begin{gathered} 11.92-11.67 \\ (51) \end{gathered}$ | $\begin{aligned} & \text { TP38.9853×38.9229×0.81 } \\ & 88 \end{aligned}$ | 3056.02 | 5690.58 | 0.537 | 0.00 | 5690.58 | 0.000 |
| L52 | $\begin{gathered} 11.67-6.67 \\ (52) \end{gathered}$ | $\begin{gathered} \text { TP40.2341×38.9853×0.79 } \\ 38 \end{gathered}$ | 3178.57 | 5748.95 | 0.553 | 0.00 | 5748.95 | 0.000 |
| L53 | 6.67-6.5 (53) | $\begin{gathered} \text { TP40.2766x40.2341×0.79 } \\ 38 \end{gathered}$ | 3260.98 | 5898.87 | 0.553 | 0.00 | 5898.87 | 0.000 |
| L54 | 6.5-6.25 (54) | TP40.339×40.2766x0.918 8 | 3268.01 | 6777.90 | 0.482 | 0.00 | 6777.90 | 0.000 |
| L55 | $\begin{aligned} & 6.25-3.75 \\ & (55) \end{aligned}$ | TP40.9634×40.339×0.906 3 | 3278.36 | 6713.54 | 0.488 | 0.00 | 6713.54 | 0.000 |
| L56 | 3.75-3.5 (56) | TP41.0258×40.9634×1.00 63 | 3382.32 | 7637.49 | 0.443 | 0.00 | 7637.49 | 0.000 |
| L57 | 3.5-3 (57) | TP41.1507×41.0258×0.99 38 | 3392.77 | 7573.59 | 0.448 | 0.00 | 7573.59 | 0.000 |
| L58 | 3-2.75 (58) | TP41.2132x41.1507x0.99 38 | 3413.68 | 7621.49 | 0.448 | 0.00 | 7621.49 | 0.000 |
| L59 | 2.75-0 (59) | TP41.9x41.2132×1.0188 | 3424.16 | 7823.22 | 0.438 | 0.00 | 7823.22 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | Ratio $T_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  |  | $K$ | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L1 | 130-125 (1) | TP11.775x10.525x0.1875 | 0.26 | 122.78 | 0.002 | 0.00 | 125.15 | 0.000 |
| L2 | 125-120 (2) | TP13.025x11.775x0.1875 | 2.24 | 136.02 | 0.016 | 0.00 | 153.60 | 0.000 |
| L3 | 120-115 (3) | TP14.275x13.025x0.1875 | 8.57 | 149.27 | 0.057 | 0.14 | 184.97 | 0.001 |
| L4 | 115-110 (4) | TP15.525x14.275x0.1875 | 9.14 | 162.51 | 0.056 | 0.06 | 219.25 | 0.000 |
| L5 | 110-105 (5) | TP16.7758x15.525x0.25 | 14.31 | 233.47 | 0.061 | 0.77 | 339.39 | 0.002 |
| L6 | 105-100 (6) | TP18.0265x16.7758x0.25 | 15.39 | 251.14 | 0.061 | 0.68 | 392.70 | 0.002 |
| L7 | 100-95 (7) | TP19.2773x18.0265x0.25 | 20.65 | 268.81 | 0.077 | 0.73 | 449.91 | 0.002 |
| L8 | 95-90 (8) | TP20.528x19.2773x0.25 | 21.17 | 286.48 | 0.074 | 0.79 | 511.00 | 0.002 |
| L9 | 90-89.75 (9) | TP20.5905x20.528x0.5 | 21.18 | 567.67 | 0.037 | 0.79 | 1003.20 | 0.001 |
| L10 | 89.75-84.75 | TP21.8413x20.5905x0.48 | 24.94 | 580.91 | 0.043 | 0.92 | 1091.46 | 0.001 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | Ratio $T_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | K | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L11 | 84.75-84.58 <br> (11) | $\begin{gathered} \text { TP21.8838x21.8413x0.47 } \\ 5 \end{gathered}$ | 24.95 | 574.67 | 0.043 | 0.93 | 1082.21 | 0.001 |
| L12 | $\begin{gathered} 84.58-84.33 \\ (12) \end{gathered}$ | $\begin{gathered} \text { TP21.9464×21.8838×0.63 } \\ 75 \end{gathered}$ | 24.99 | 767.67 | 0.033 | 0.93 | 1438.91 | 0.001 |
| L13 | $\begin{gathered} 84.33-83.42 \\ (13) \end{gathered}$ | TP22.174x21.9464x0.625 | 25.12 | 761.10 | 0.033 | 0.93 | 1442.67 | 0.001 |
| L14 | $83.42-83.17$ <br> (14) | TP22.2365x22.174×0.95 | 25.16 | 1142.78 | 0.022 | 0.94 | 2139.77 | 0.000 |
| L15 | $\begin{gathered} 83.17-83 \\ (15) \end{gathered}$ | TP22.2791x22.2365×0.95 | 25.19 | 1145.06 | 0.022 | 0.94 | 2148.32 | 0.000 |
| L16 | $\begin{gathered} 83-82.75 \\ (16) \end{gathered}$ | TP22.3416x22.2791x0.7 | 25.22 | 856.09 | 0.029 | 0.94 | 1629.71 | 0.001 |
| L17 | $82.75-77.75$ | TP23.5923x22.3416x0.66 25 | 26.11 | 858.46 | 0.030 | 0.82 | 1731.49 | 0.000 |
| L18 | $\begin{gathered} 77.75-70 \\ (18) \end{gathered}$ | TP25.531x23.5923x0.65 | 30.13 | 877.18 | 0.034 | 0.90 | 1842.59 | 0.000 |
| L19 | 70-69 (19) | TP25.281x24.0304x0.7 | 31.07 | 972.37 | 0.032 | 1.02 | 2102.47 | 0.000 |
| L20 | $\begin{gathered} 69-67.08 \\ (20) \end{gathered}$ | TP25.7612×25.281×0.687 5 | 31.41 | 974.15 | 0.032 | 1.05 | 2148.53 | 0.000 |
| L21 | $\begin{gathered} 67.08-66.83 \\ (21) \end{gathered}$ | $\begin{gathered} \text { TP25.8237×25.7612×0.68 } \\ 75 \end{gathered}$ | 31.43 | 976.58 | 0.032 | 1.06 | 2159.27 | 0.000 |
| L22 | $\begin{gathered} 66.83-64.08 \\ (22) \end{gathered}$ | $\begin{aligned} & \text { TP26.5115×25.8237×0.67 } \\ & 5 \end{aligned}$ | 31.90 | 985.53 | 0.032 | 1.12 | 2239.78 | 0.001 |
| L23 | $\begin{gathered} 64.08-63.83 \\ (23) \end{gathered}$ | $\begin{gathered} \text { TP26.5741×26.5115×0.73 } \\ 75 \end{gathered}$ | 31.93 | 1076.79 | 0.030 | 1.13 | 2447.18 | 0.000 |
| L24 | $\begin{gathered} 63.83-62.5 \\ (24) \end{gathered}$ | $\begin{gathered} \text { TP26.9067×26.5741×0.73 } \\ 75 \end{gathered}$ | 32.17 | 1090.65 | 0.030 | 1.15 | 2510.59 | 0.000 |
| L25 | $\begin{gathered} 62.5-62.25 \\ (25) \end{gathered}$ | TP26.9693x26.9067x0.86 $25$ | 32.20 | 1272.46 | 0.025 | 1.16 | 2922.12 | 0.000 |
| L26 | $\begin{gathered} 62.25-57.25 \\ (26) \end{gathered}$ | TP28.2198×26.9693×0.83 75 | 33.09 | 1295.95 | 0.026 | 1.25 | 3121.47 | 0.000 |
| L27 | $\begin{gathered} 57.25-53.5 \\ (27) \end{gathered}$ | $\begin{gathered} \text { TP29.1578×28.2198×0.81 } \\ 25 \end{gathered}$ | 33.75 | 1301.48 | 0.026 | 1.32 | 3245.02 | 0.000 |
| L28 | $53.5-53.25$ <br> (28) | $\begin{gathered} \text { TP29.2203 } \times 29.1578 \times 0.83 \\ 75 \end{gathered}$ | 33.78 | 1343.30 | 0.025 | 1.33 | 3353.72 | 0.000 |
| L29 | $\begin{gathered} 53.25-52.58 \\ (29) \end{gathered}$ | $\begin{gathered} \text { TP29.3879×29.2203×0.82 } \\ 5 \end{gathered}$ | 33.91 | 1331.65 | 0.025 | 1.34 | 3345.72 | 0.000 |
| L30 | $52.58-52.33$ <br> (30) | $\begin{gathered} \text { TP29.4504×29.3879×0.86 } \\ 25 \end{gathered}$ | 33.95 | 1393.40 | 0.024 | 1.34 | 3503.94 | 0.000 |
| L31 | $\begin{gathered} 52.33-47.33 \\ (31) \end{gathered}$ | $\begin{gathered} \mathrm{TP} 30.701 \times 29.4504 \times 0.837 \\ 5 \end{gathered}$ | 34.83 | 1413.38 | 0.025 | 1.44 | 3712.78 | 0.000 |
| L32 | $\begin{gathered} 47.33-44.58 \\ (32) \end{gathered}$ | TP31.3888×30.701×0.812 | 35.31 | 1403.92 | 0.025 | 1.49 | 3775.95 | 0.000 |
| L33 | $\begin{gathered} 44.58-44.33 \\ (33) \end{gathered}$ | TP31.4513x31.3888×0.81 25 | 35.34 | 1406.79 | 0.025 | 1.49 | 3791.41 | 0.000 |
| L34 | 44.33-41.92 <br> (34) | TP32.0541x31.4513x0.8 | 35.76 | 1412.96 | 0.025 | 1.53 | 3884.52 | 0.000 |
| L35 | $\begin{gathered} 41.92-41.67 \\ (35) \end{gathered}$ | TP32.1166x32.0541×0.81 25 | 35.78 | 1437.33 | 0.025 | 1.53 | 3957.85 | 0.000 |
| L36 | $\begin{gathered} 41.67-34.08 \\ (36) \end{gathered}$ | TP34.015×32.1166×0.787 | 36.24 | 1423.94 | 0.025 | 1.57 | 4007.74 | 0.000 |
| L37 | $\begin{gathered} 34.08-34 \\ (37) \end{gathered}$ | $\begin{aligned} & \text { TP33.4082×32.1594×0.81 } \\ & 88 \end{aligned}$ | 37.18 | 1507.86 | 0.025 | 1.65 | 4322.54 | 0.000 |
| L38 | 34-29 (38) | TP34.657×33.4082×0.793 8 | 37.98 | 1518.96 | 0.025 | 1.73 | 4524.54 | 0.000 |
| L39 | $\begin{gathered} 29-26.92 \\ (39) \end{gathered}$ | TP35.1765x34.657x0.793 <br> 8 | 38.31 | 1542.26 | 0.025 | 1.76 | 4664.43 | 0.000 |
| L40 | $\begin{gathered} 26.92-26.67 \\ (40) \end{gathered}$ | $\begin{gathered} \text { TP35.239×35.1765×0.893 } \\ 8 \end{gathered}$ | 38.33 | 1734.66 | 0.022 | 1.77 | 5240.60 | 0.000 |
| L41 | $\begin{gathered} 26.67-21.67 \\ (41) \end{gathered}$ | TP36.4877×35.239×0.868 8 | 39.13 | 1748.68 | 0.022 | 1.84 | 5478.87 | 0.000 |
| L42 | $\begin{gathered} 21.67-18 \\ (42) \end{gathered}$ | TP37.4044×36.4877×0.85 63 | 39.70 | 1768.47 | 0.022 | 1.89 | 5685.42 | 0.000 |
| L43 | $\begin{gathered} 18-17.75 \\ (43) \end{gathered}$ | $\begin{aligned} & \text { TP37.4668×37.4044×0.99 } \\ & 38 \end{aligned}$ | 39.71 | 2048.25 | 0.019 | 1.89 | 6571.34 | 0.000 |
| L44 | $\begin{gathered} 17.75-17.5 \\ (44) \end{gathered}$ | TP37.5292×37.4668×0.99 38 | 39.75 | 2051.75 | 0.019 | 1.90 | 6593.86 | 0.000 |
| L45 | $\begin{gathered} 17.5-17.25 \\ (45) \end{gathered}$ | TP37.5917×37.5292×0.99 38 | 39.79 | 2055.26 | 0.019 | 1.90 | 6616.42 | 0.000 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation | Size | Actual $V_{u}$ | $\phi V_{n}$ | Ratio $V_{u}$ | Actual $T_{u}$ | $\phi T_{n}$ | Ratio $T_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  |  | K | K | $\phi V_{n}$ | kip-ft | kip-ft | $\phi T_{n}$ |
| L46 | 17.25-17.08 <br> (46) | $\begin{gathered} \text { TP37.6341×37.5917×0.99 } \\ 38 \end{gathered}$ | 39.82 | 2057.64 | 0.019 | 1.90 | 6631.77 | 0.000 |
| L47 | $17.08-16.83$ <br> (47) | $\begin{gathered} \text { TP37.6966x37.6341×0.89 } \\ 38 \end{gathered}$ | 39.85 | 1858.79 | 0.021 | 1.90 | 6017.43 | 0.000 |
| L48 | $\begin{gathered} 16.83-13 \\ (48) \end{gathered}$ | TP38.6531x37.6966x0.88 13 | 40.43 | 1881.05 | 0.021 | 1.96 | 6249.85 | 0.000 |
| L49 | $13-12.75$ <br> (49) | TP38.7156x38.6531x1.05 63 | 40.44 | 2247.88 | 0.018 | 1.96 | 7446.37 | 0.000 |
| L50 | $12.75-11.92$ <br> (50) | $\begin{gathered} \text { TP38.9229×38.7156×1.04 } \\ 38 \end{gathered}$ | 40.58 | 2234.24 | 0.018 | 1.97 | 7444.39 | 0.000 |
| L51 | $\begin{gathered} 11.92-11.67 \\ (51) \end{gathered}$ | $\begin{aligned} & \mathrm{TP} 38.9853 \times 38.9229 \times 0.81 \\ & 88 \end{aligned}$ | 40.61 | 1765.91 | 0.023 | 1.97 | 5928.57 | 0.000 |
| L52 | $\begin{gathered} 11.67-6.67 \\ (52) \end{gathered}$ | TP40.2341×38.9853x0.79 38 | 41.18 | 1757.92 | 0.023 | 2.05 | 5983.12 | 0.000 |
| L53 | 6.67-6.5 (53) | $\begin{gathered} \text { TP40.2766x40.2341×0.79 } \\ 38 \end{gathered}$ | 41.33 | 1771.03 | 0.023 | 2.07 | 6137.60 | 0.000 |
| L54 | 6.5-6.25 (54) | $\begin{gathered} \text { TP40.339×40.2766x0.918 } \\ 8 \end{gathered}$ | 41.37 | 2046.68 | 0.020 | 2.08 | 7074.44 | 0.000 |
| L55 | $6.25-3.75$ <br> (55) | TP40.9634×40.339x0.906 3 | 41.56 | 2035.46 | 0.020 | 2.11 | 7004.79 | 0.000 |
| L56 | 3.75-3.5 (56) | TP41.0258×40.9634×1.00 63 | 41.76 | 2275.68 | 0.018 | 2.14 | 7985.97 | 0.000 |
| L57 | 3.5-3 (57) | TP41.1507x41.0258x0.99 38 | 41.84 | 2255.13 | 0.019 | 2.16 | 7916.38 | 0.000 |
| L58 | 3-2.75 (58) | TP41.2132×41.1507×0.99 38 | 41.87 | 2258.63 | 0.019 | 2.16 | 7965.85 | 0.000 |
| L59 | 2.75-0 (59) | TP41.9x41.2132x1.0188 | 42.10 | 2333.79 | 0.018 | 2.20 | 8181.48 | 0.000 |

Pole Interaction Design Data

| Section No. | Elevation | Ratio $P_{u}$ | Ratio Mux | Ratio Muy | Ratio $V_{u}$ | Ratio $T_{u}$ | Comb. Stress | Allow. <br> Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L1 | 130-125 (1) | 0.000 | 0.005 | 0.000 | 0.002 | 0.000 | 0.005 | 1.050 | 4.8.2 |
| L2 | 125-120 (2) | 0.033 | 0.015 | 0.000 | 0.016 | 0.000 | 0.049 | 1.050 | 4.8.2 |
| L3 | 120-115 (3) | 0.009 | 0.261 | 0.000 | 0.057 | 0.001 | 0.273 | 1.050 | 4.8.2 |
| L4 | 115-110 (4) | 0.008 | 0.429 | 0.000 | 0.056 | 0.000 | 0.440 | 1.050 | 4.8.2 |
| L5 | 110-105 (5) | 0.011 | 0.494 | 0.000 | 0.061 | 0.002 | 0.509 | 1.050 | 4.8.2 |
| L6 | 105-100 (6) | 0.011 | 0.623 | 0.000 | 0.061 | 0.002 | 0.638 | 1.050 | 4.8.2 |
| L7 | 100-95 (7) | 0.015 | 0.752 | 0.000 | 0.077 | 0.002 | 0.773 | 1.050 | 4.8.2 |
| L8 | 95-90 (8) | 0.015 | 0.873 | 0.000 | 0.074 | 0.002 | 0.893 | 1.050 | 4.8.2 |
| L9 | 90-89.75 (9) | 0.007 | 0.456 | 0.000 | 0.037 | 0.001 | 0.464 | 1.050 | 4.8.2 |
| L10 | $\begin{gathered} 89.75-84.75 \\ (10) \end{gathered}$ | 0.009 | 0.527 | 0.000 | 0.043 | 0.001 | 0.538 | 1.050 | 4.8.2 |
| L11 | $84.75-84.58$ <br> (11) | 0.009 | 0.535 | 0.000 | 0.043 | 0.001 | 0.546 | 1.050 | 4.8.2 |
| L12 | $\begin{gathered} 84.58-84.33 \\ (12) \end{gathered}$ | 0.007 | 0.410 | 0.000 | 0.033 | 0.001 | 0.418 | 1.050 | 4.8.2 |
| L13 | $\begin{gathered} 84.33-83.42 \\ (13) \end{gathered}$ | 0.007 | 0.425 | 0.000 | 0.033 | 0.001 | 0.433 | 1.050 | 4.8.2 |
| L14 | $83.42-83.17$ <br> (14) | 0.005 | 0.294 | 0.000 | 0.022 | 0.000 | 0.299 | 1.050 | 4.8.2 |
| L15 | $83.17-83$ <br> (15) | 0.005 | 0.295 | 0.000 | 0.022 | 0.000 | 0.300 | 1.050 | 4.8.2 |
| L16 | $\begin{gathered} 83-82.75 \\ (16) \end{gathered}$ | 0.006 | 0.389 | 0.000 | 0.029 | 0.001 | 0.396 | 1.050 | 4.8.2 |
| L17 | $82.75-77.75$ <br> (17) | 0.007 | 0.442 | 0.000 | 0.030 | 0.000 | 0.450 | 1.050 | 4.8.2 |
| L18 | $\begin{gathered} 77.75-70 \\ (18) \end{gathered}$ | 0.008 | 0.477 | 0.000 | 0.034 | 0.000 | 0.486 | 1.050 | 4.8.2 |
| L19 | 70-69 (19) | 0.008 | 0.495 | 0.000 | 0.032 | 0.000 | 0.504 | 1.050 | 4.8.2 |
| L20 | $\begin{gathered} 69-67.08 \\ (20) \end{gathered}$ | 0.008 | 0.513 | 0.000 | 0.032 | 0.000 | 0.522 | 1.050 | 4.8.2 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation | Ratio $P_{u}$ | Ratio Mux | Ratio Muy | Ratio $V_{u}$ | Ratio $T_{u}$ | Comb. Stress | Allow. <br> Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L21 | $\begin{gathered} 67.08-66.83 \\ (21) \end{gathered}$ | 0.008 | 0.514 | 0.000 | 0.032 | 0.000 | 0.524 | 1.050 | 4.8.2 |
| L22 | $\begin{gathered} 66.83-64.08 \\ (22) \end{gathered}$ | 0.008 | 0.536 | 0.000 | 0.032 | 0.001 | 0.545 | 1.050 | 4.8.2 |
| L23 | $\begin{aligned} & 64.08-63.83 \\ & (23) \end{aligned}$ | 0.008 | 0.495 | 0.000 | 0.030 | 0.000 | 0.504 | 1.050 | 4.8.2 |
| L24 | $\begin{gathered} 63.83-62.5 \\ (24) \end{gathered}$ | 0.008 | 0.500 | 0.000 | 0.030 | 0.000 | 0.509 | 1.050 | 4.8.2 |
| L25 | $\begin{gathered} 62.5-62.25 \\ (25) \end{gathered}$ | 0.007 | 0.435 | 0.000 | 0.025 | 0.000 | 0.442 | 1.050 | 4.8.2 |
| L26 | $\begin{gathered} 62.25-57.25 \\ (26) \end{gathered}$ | 0.007 | 0.461 | 0.000 | 0.026 | 0.000 | 0.469 | 1.050 | 4.8.2 |
| L27 | $\begin{gathered} 57.25-53.5 \\ (27) \end{gathered}$ | 0.007 | 0.483 | 0.000 | 0.026 | 0.000 | 0.491 | 1.050 | 4.8.2 |
| L28 | $\begin{gathered} 53.5-53.25 \\ (28) \end{gathered}$ | 0.007 | 0.471 | 0.000 | 0.025 | 0.000 | 0.478 | 1.050 | 4.8.2 |
| L29 | $\begin{gathered} 53.25-52.58 \\ (29) \end{gathered}$ | 0.007 | 0.479 | 0.000 | 0.025 | 0.000 | 0.486 | 1.050 | 4.8.2 |
| L30 | $\begin{gathered} 52.58-52.33 \\ (30) \end{gathered}$ | 0.007 | 0.460 | 0.000 | 0.024 | 0.000 | 0.467 | 1.050 | 4.8.2 |
| L31 | $\begin{gathered} 52.33-47.33 \\ (31) \end{gathered}$ | 0.007 | 0.482 | 0.000 | 0.025 | 0.000 | 0.490 | 1.050 | 4.8.2 |
| L32 | $\begin{gathered} 47.33-44.58 \\ (32) \end{gathered}$ | 0.007 | 0.500 | 0.000 | 0.025 | 0.000 | 0.508 | 1.050 | 4.8.2 |
| L33 | 44.58-44.33 <br> (33) | 0.007 | 0.500 | 0.000 | 0.025 | 0.000 | 0.508 | 1.050 | 4.8.2 |
| L34 | $\begin{gathered} 44.33-41.92 \\ (34) \end{gathered}$ | 0.008 | 0.511 | 0.000 | 0.025 | 0.000 | 0.519 | 1.050 | 4.8.2 |
| L35 | $\begin{gathered} 41.92-41.67 \\ \text { (35) } \end{gathered}$ | 0.007 | 0.504 | 0.000 | 0.025 | 0.000 | 0.512 | 1.050 | 4.8.2 |
| L36 | $\begin{gathered} 41.67-34.08 \\ (36) \end{gathered}$ | 0.008 | 0.522 | 0.000 | 0.025 | 0.000 | 0.531 | 1.050 | 4.8.2 |
| L37 | $\begin{gathered} 34.08-34 \\ (37) \end{gathered}$ | 0.008 | 0.529 | 0.000 | 0.025 | 0.000 | 0.538 | 1.050 | 4.8.2 |
| L38 | 34-29 (38) | 0.008 | 0.548 | 0.000 | 0.025 | 0.000 | 0.557 | 1.050 | 4.8 .2 |
| L39 | $\begin{gathered} 29-26.92 \\ (39) \end{gathered}$ | 0.008 | 0.549 | 0.000 | 0.025 | 0.000 | 0.558 | 1.050 | 4.8.2 |
| L40 | $\begin{gathered} 26.92-26.67 \\ (40) \end{gathered}$ | 0.008 | 0.492 | 0.000 | 0.022 | 0.000 | 0.500 | 1.050 | 4.8.2 |
| L41 | $\begin{gathered} 26.67-21.67 \\ (41) \end{gathered}$ | 0.008 | 0.507 | 0.000 | 0.022 | 0.000 | 0.515 | 1.050 | 4.8.2 |
| L42 | $\begin{gathered} 21.67-18 \\ (42) \end{gathered}$ | 0.008 | 0.514 | 0.000 | 0.022 | 0.000 | 0.523 | 1.050 | 4.8.2 |
| L43 | $\begin{gathered} 18-17.75 \\ (43) \end{gathered}$ | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8.2 |
| L44 | $17.75-17.5$ <br> (44) | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8.2 |
| L45 | $\begin{gathered} 17.5-17.25 \\ (45) \end{gathered}$ | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8.2 |
| L46 | 17.25-17.08 <br> (46) | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8.2 |
| L47 | $\begin{gathered} 17.08-16.83 \\ (47) \end{gathered}$ | 0.008 | 0.494 | 0.000 | 0.021 | 0.000 | 0.503 | 1.050 | 4.8.2 |
| L48 | $\begin{gathered} 16.83-13 \\ (48) \end{gathered}$ | 0.008 | 0.501 | 0.000 | 0.021 | 0.000 | 0.510 | 1.050 | 4.8.2 |
| L49 | $\begin{gathered} 13-12.75 \\ (49) \end{gathered}$ | 0.007 | 0.424 | 0.000 | 0.018 | 0.000 | 0.431 | 1.050 | 4.8.2 |
| L50 | $\begin{gathered} 12.75-11.92 \\ (50) \end{gathered}$ | 0.007 | 0.429 | 0.000 | 0.018 | 0.000 | 0.436 | 1.050 | 4.8.2 |
| L51 | $\begin{gathered} 11.92-11.67 \\ (51) \end{gathered}$ | 0.009 | 0.537 | 0.000 | 0.023 | 0.000 | 0.546 | 1.050 | 4.8.2 |
| L52 | $\begin{gathered} 11.67-6.67 \\ (52) \end{gathered}$ | 0.009 | 0.553 | 0.000 | 0.023 | 0.000 | 0.563 | 1.050 | 4.8.2 |
| L53 | $6.67-6.5$ (53) | 0.009 | 0.553 | 0.000 | 0.023 | 0.000 | 0.563 | 1.050 | 4.8 .2 |
| L54 | 6.5-6.25 (54) | 0.008 | 0.482 | 0.000 | 0.020 | 0.000 | 0.491 | 1.050 | 4.8 .2 |
| L55 | $6.25-3.75$ <br> (55) | 0.008 | 0.488 | 0.000 | 0.020 | 0.000 | 0.497 | 1.050 | 4.8.2 |
| L56 | 3.75-3.5 (56) | 0.007 | 0.443 | 0.000 | 0.018 | 0.000 | 0.451 | 1.050 | 4.8 .2 |
| L57 | 3.5-3 (57) | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8 .2 |

tnxTower Report - version 8.1.1.0

| Section No. | Elevation | Ratio $P_{u}$ | Ratio $M_{u x}$ | Ratio Muy | Ratio $V_{u}$ | Ratio $T_{u}$ | Comb. Stress | Allow. Stress | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  | $\phi P_{n}$ | $\phi M_{n x}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L58 | 3-2.75 (58) | 0.007 | 0.448 | 0.000 | 0.019 | 0.000 | 0.456 | 1.050 | 4.8.2 |
| L59 | 2.75-0 (59) | 0.007 | 0.438 | 0.000 | 0.018 | 0.000 | 0.445 | 1.050 | 4.8.2 |

## Section Capacity Table

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} ø P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | $\begin{aligned} & \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 130-125 | Pole | TP11.775x10.525x0.1875 | 1 | -0.10 | 429.73 | 0.5 | Pass |
| L2 | 125-120 | Pole | TP13.025x11.775x0.1875 | 2 | -15.07 | 476.08 | 5.8 | Pass |
| L3 | 120-115 | Pole | TP14.275×13.025x0.1875 | 3 | -4.27 | 522.44 | 26.0 | Pass |
| L4 | 115-110 | Pole | TP15.525x14.275x0.1875 | 4 | -4.50 | 568.80 | 41.9 | Pass |
| L5 | 110-105 | Pole | TP16.7758x15.525x0.25 | 5 | -8.84 | 817.15 | 48.5 | Pass |
| L6 | 105-100 | Pole | TP18.0265x16.7758x0.25 | 6 | -9.33 | 879.00 | 60.8 | Pass |
| L7 | 100-95 | Pole | TP19.2773x18.0265x0.25 | 7 | -13.25 | 940.84 | 73.6 | Pass |
| L8 | 95-90 | Pole | TP20.528x19.2773x0.25 | 8 | -13.91 | 1002.69 | 85.0 | Pass |
| L9 | 90-89.75 | Pole | TP20.5905x20.528x0.5 | 9 | -13.98 | 1986.84 | 44.2 | Pass |
| L10 | 89.75-84.75 | Pole | TP21.8413x20.5905x0.4813 | 10 | -17.69 | 2033.17 | 51.2 | Pass |
| L11 | 84.75-84.58 | Pole | TP21.8838x21.8413x0.475 | 11 | -17.74 | 2011.35 | 52.0 | Pass |
| L12 | 84.58-84.33 | Pole | TP21.9464x21.8838x0.6375 | 12 | -17.81 | 2686.83 | 39.8 | Pass |
| L13 | 84.33-83.42 | Pole | TP22.174x21.9464x0.625 | 13 | -18.02 | 2663.84 | 41.3 | Pass |
| L14 | 83.42-83.17 | Pole | TP22.2365x22.174x0.95 | 14 | -18.11 | 3999.72 | 28.5 | Pass |
| L15 | 83.17-83 | Pole | TP22.2791x22.2365x0.95 | 15 | -18.17 | 4007.71 | 28.6 | Pass |
| L16 | 83-82.75 | Pole | TP22.3416x22.2791x0.7 | 16 | -18.23 | 2996.32 | 37.7 | Pass |
| L17 | 82.75-77.75 | Pole | TP23.5923x22.3416x0.6625 | 17 | -19.52 | 3004.61 | 42.9 | Pass |
| L18 | 77.75-70 | Pole | TP25.531x23.5923x0.65 | 18 | -23.55 | 3070.13 | 46.3 | Pass |
| L19 | 70-69 | Pole | TP25.281x24.0304x0.7 | 19 | -25.74 | 3403.28 | 48.0 | Pass |
| L20 | 69-67.08 | Pole | TP25.7612x25.281x0.6875 | 20 | -26.31 | 3409.51 | 49.8 | Pass |
| L21 | 67.08-66.83 | Pole | TP25.8237x25.7612x0.6875 | 21 | -26.42 | 3418.01 | 49.9 | Pass |
| L22 | 66.83-64.08 | Pole | TP26.5115x25.8237x0.675 | 22 | -27.25 | 3449.37 | 51.9 | Pass |
| L23 | 64.08-63.83 | Pole | TP26.5741x26.5115x0.7375 | 23 | -27.35 | 3768.75 | 48.0 | Pass |
| L24 | 63.83-62.5 | Pole | TP26.9067x26.5741x0.7375 | 24 | -27.80 | 3817.27 | 48.5 | Pass |
| L25 | 62.5-62.25 | Pole | TP26.9693x26.9067x0.8625 | 25 | -27.91 | 4453.62 | 42.1 | Pass |
| L26 | 62.25-57.25 | Pole | TP28.2198x26.9693x0.8375 | 26 | -29.71 | 4535.82 | 44.6 | Pass |
| L27 | 57.25-53.5 | Pole | TP29.1578x28.2198x0.8125 | 27 | -31.10 | 4555.17 | 46.8 | Pass |
| L28 | 53.5-53.25 | Pole | TP29.2203x29.1578x0.8375 | 28 | -31.21 | 4701.55 | 45.5 | Pass |
| L29 | 53.25-52.58 | Pole | TP29.3879x29.2203x0.825 | 29 | -31.47 | 4660.76 | 46.3 | Pass |
| L30 | 52.58-52.33 | Pole | TP29.4504x29.3879x0.8625 | 30 | -31.57 | 4876.88 | 44.5 | Pass |
| L31 | 52.33-47.33 | Pole | TP30.701x29.4504x0.8375 | 31 | -33.52 | 4946.82 | 46.6 | Pass |
| L32 | 47.33-44.58 | Pole | TP31.3888x30.701x0.8125 | 32 | -34.62 | 4913.71 | 48.4 | Pass |
| L33 | 44.58-44.33 | Pole | TP31.4513x31.3888x0.8125 | 33 | -34.74 | 4923.75 | 48.4 | Pass |
| L34 | 44.33-41.92 | Pole | TP32.0541×31.4513x0.8 | 34 | -35.70 | 4945.36 | 49.4 | Pass |
| L35 | 41.92-41.67 | Pole | TP32.1166x32.0541x0.8125 | 35 | -35.82 | 5030.68 | 48.8 | Pass |
| L36 | 41.67-34.08 | Pole | TP34.015x32.1166x0.7875 | 36 | -36.90 | 4983.79 | 50.5 | Pass |
| L37 | 34.08-34 | Pole | TP33.4082x32.1594x0.8188 | 37 | -40.57 | 5277.52 | 51.2 | Pass |
| L38 | 34-29 | Pole | TP34.657x33.4082x0.7938 | 38 | -42.74 | 5316.35 | 53.0 | Pass |
| L39 | 29-26.92 | Pole | TP35.1765x34.657x0.7938 | 39 | -43.66 | 5397.91 | 53.1 | Pass |
| L40 | 26.92-26.67 | Pole | TP35.239x35.1765x0.8938 | 40 | -43.79 | 6071.32 | 47.6 | Pass |
| L41 | 26.67-21.67 | Pole | TP36.4877x35.239x0.8688 | 41 | -46.23 | 6120.37 | 49.1 | Pass |
| L42 | 21.67-18 | Pole | TP37.4044x36.4877x0.8563 | 42 | -48.05 | 6189.66 | 49.8 | Pass |
| L43 | 18-17.75 | Pole | TP37.4668x37.4044×0.9938 | 43 | -48.21 | 7168.86 | 43.4 | Pass |
| L44 | 17.75-17.5 | Pole | TP37.5292x37.4668x0.9938 | 44 | -48.35 | 7181.14 | 43.4 | Pass |
| L45 | 17.5-17.25 | Pole | TP37.5917x37.5292x0.9938 | 45 | -48.48 | 7193.40 | 43.4 | Pass |
| L46 | 17.25-17.08 | Pole | TP37.6341x37.5917x0.9938 | 46 | -48.58 | 7201.75 | 43.4 | Pass |
| L47 | 17.08-16.83 | Pole | TP37.6966x37.6341x0.8938 | 47 | -48.70 | 6505.76 | 47.9 | Pass |
| L48 | 16.83-13 | Pole | TP38.6531x37.6966x0.8813 | 48 | -50.67 | 6583.68 | 48.6 | Pass |
| L49 | 13-12.75 | Pole | TP38.7156x38.6531x1.0563 | 49 | -50.83 | 7867.57 | 41.1 | Pass |
| L50 | 12.75-11.92 | Pole | TP38.9229x38.7156x1.0438 | 50 | -51.31 | 7819.83 | 41.5 | Pass |
| L51 | 11.92-11.67 | Pole | TP38.9853x38.9229x0.8188 | 51 | -51.45 | 6180.67 | 52.0 | Pass |
| L52 | 11.67-6.67 | Pole | TP40.2341x38.9853x0.7938 | 52 | -53.04 | 6113.50 | 53.6 | Pass |
| L53 | 6.67-6.5 | Pole | TP40.2766x40.2341x0.7938 | 53 | -54.08 | 6191.92 | 53.6 | Pass |
| L54 | 6.5-6.25 | Pole | TP40.339x40.2766x0.9188 | 54 | -54.17 | 7152.03 | 46.7 | Pass |
| L55 | 6.25-3.75 | Pole | TP40.9634x40.339x0.9063 | 55 | -54.33 | 7068.16 | 47.3 | Pass |

tnxTower Report - version 8.1.1.0

130 Ft Monopole Tower Structural Analysis

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\emptyset P_{\text {allow }}$ K | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L56 | 3.75-3.5 | Pole | TP41.0258x40.9634x1.0063 | 56 | -55.72 | 7952.46 | 42.9 | Pass |
| L57 | 3.5-3 | Pole | TP41.1507x41.0258x0.9938 | 57 | -55.87 | 7868.41 | 43.4 | Pass |
| L58 | 3-2.75 | Pole | TP41.2132x41.1507x0.9938 | 58 | -56.16 | 7892.94 | 43.4 | Pass |
| L59 | 2.75-0 | Pole | TP41.9x41.2132x1.0188 | 59 | -56.32 | 8099.06 | 42.4 | Pass |
|  |  |  |  |  |  | Pole (L8) RATING = | $\begin{gathered} \text { Summary } \\ 85.0 \\ \mathbf{8 5 . 0} \\ \hline \end{gathered}$ | Pass Pass |

*NOTE: Above stress ratios for reinforced sections are approximate. More exact calculations are presented in Appendix C.

## APPENDIX B

## BASE LEVEL DRAWING


!

## APPENDIX C

## ADDITIONAL CALCULATIONS

$$
\begin{aligned}
& \text { Site BU: } 806376 \\
& \text { Work Order: } 1963271 \\
& \hline \text { CAROWN } \\
& \text { CASTLE }
\end{aligned}
$$

Pole Geometry
Copyright © 2019 Crown Castle

|  | Pole Height Above Base (ft) | Section Length (ft) | Lap Splice Length <br> (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Bend Radius <br> (in) | Pole Material |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 130 | 20 | 0 | 12 | 10.525 | 15.525 | 0.1875 | Auto | A572-65 |
| 2 | 110 | 40 | 4 | 12 | 15.53 | 25.531 | 0.25 | Auto | A572-65 |
| 3 | 74 | 39.92 | 4.92 | 12 | 24.03 | 34.015 | 0.3125 | Auto | A572-65 |
| 4 | 39 | 39 | 0 | 12 | 32.16 | 41.9 | 0.34375 | Auto | A572-65 |
|  |  |  |  |  |  |  |  |  |  |

Reinforcement Configuration

|  | Bottom Effective <br> Elevation (ft) | Top Effective <br> Elevation (ft) | Type | Model | Number | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 17.08 | 44.58 | plate | PL $0.75 \times 4.00$ (100ksi) | 3 | $\times$ |  |  |  | $\times$ |  |  |  | $\times$ |  |  |  |
| 2 | 44.58 | 67.08 | plate | PL $0.75 \times 4.00$ ( 100 ksi ) | 3 |  |  |  | $x$ |  |  |  | $x$ |  |  |  | $\times$ |
| 3 | 67.08 | 84.58 | plate | PL $0.75 \times 4.00$ ( 100 ksi ) | 3 | $\times$ |  |  |  | $\times$ |  |  |  | $\times$ |  |  |  |
| 4 | 0 | 3.75 | plate | S) $1.25 \times 7.00$ ( 65 ksi ) P. | 2 |  |  |  |  |  |  |  | c |  |  |  | c |
| 5 | 3 | 13 | plate | CCI-AFP-060100 | 2 | $\times$ |  |  |  |  |  |  |  | $\times$ |  |  |  |
| 6 | 0 | 13 | plate | CCI-AFP-060100 | 1 |  |  |  |  | $\times$ |  |  |  |  |  |  |  |
| 7 | 11.92 | 41.92 | plate | CCI-AFP-060100 | 1 |  |  | $x$ |  |  |  |  |  |  |  |  |  |
| 8 | 11.92 | 26.92 | plate | CCI-AFP-060100 | 2 |  |  |  |  |  |  |  | $\times$ |  |  |  | $\times$ |
| 9 | 18 | 53.5 | plate | CCI-AFP-060100 | 2 |  |  |  |  |  |  | $\times$ |  |  |  | $x$ |  |
| 10 | 41.92 | 62.5 | plate | CCI-AFP-045100 | 1 |  |  | $\times$ |  |  |  |  |  |  |  |  |  |
| 11 | 53.5 | 64.08 | plate | CCI-AFP-045100 | 2 |  |  |  |  |  |  | x |  |  |  | $x$ |  |
| 12 | 83 | 90 | plate | CCI-SFP-045100 | 3 |  |  | x |  |  |  | x |  |  |  | x |  |
| 13 | 0 | 6.5 | plate | CCI-WCFP-065125 | 1 |  |  |  |  |  |  |  | 1.5 |  |  |  |  |
| 14 | 0 | 18 | plate | CCI-WCFP-065125 | 3 |  |  |  | $\times$ |  |  | x |  |  |  | x |  |
| 15 | 0 | 17.5 | plate | CCI-WCFP-060100 | 3 |  | -2 |  |  |  | $x$ |  |  |  | $x$ |  |  |
| 16 | 17.5 | 52.58 | plate | CCI-CFP-060100 | 3 |  | -2 |  |  |  | $x$ |  |  |  | $x$ |  |  |
| 17 | 52.58 | 83.42 | plate | CCI-CFP-045125 | 3 |  | x |  |  |  | x |  |  |  | x |  |  |
| 18 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Reinforcement Details

|  | B (in) | H (in) | Gross <br> Area <br> (in ${ }^{2}$ ) | Pole Face to Centroid (in) | Bottom Termination Type | Bottom Termination Length (in) | Top Termination Type | Top Termination Length (in) | Lu (in) | Net Area (in2) | Bolt Hole Size (in) | Reinforcement Material |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4 | 0.75 | 3 | 0.375 | PC 8.8 - M20 (100) | 15 | PC 8.8 - M20 (100) | 15.000 | 15.000 | 2.063 | 1.1875 | A514-GR100 |
| 2 | 4 | 0.75 | 3 | 0.375 | PC 8.8 - M20 (100) | 15 | PC 8.8 - M20 (100) | 15.000 | 15.000 | 2.063 | 1.1875 | A514-GR100 |
| 3 | 4 | 0.75 | 3 | 0.375 | PC 8.8 - M20 (100) | 15 | PC 8.8 - M20 (100) | 15.000 | 15.000 | 2.063 | 1.1875 | A514-GR100 |
| 4 | 1.25 | 6.25 | 7.8125 | 3.125 | Welded | n/a | Capacity Input | n/a | 0.750 | 7.813 | 0.0000 | A572-65 |
| 5 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 6 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 7 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 8 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 9 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 10 | 4.5 | 1 | 4.5 | 0.5 | PC 8.8 - M20 (100) | 24 | PC 8.8 - M20 (100) | 24.000 | 20.000 | 3.250 | 1.1875 | A572-65 |
| 11 | 4.5 | 1 | 4.5 | 0.5 | PC 8.8 - M20 (100) | 24 | PC 8.8 - M20 (100) | 24.000 | 20.000 | 3.250 | 1.1875 | A572-65 |
| 12 | 4.5 | 1 | 4.5 | 0.5 | PC 8.8 - M20 (100) | 18 | PC 8.8 - M20 (100) | 18.000 | 20.000 | 3.250 | 1.1875 | A572-65 |
| 13 | 6.5 | 1.25 | 8.125 | 0.625 | Welded | n/a | PC 8.8 - M20 (100) | 33.000 | 19.000 | 6.563 | 1.1875 | A572-65 |
| 14 | 6.5 | 1.25 | 8.125 | 0.625 | Welded | n/a | PC 8.8 - M20 (100) | 33.000 | 19.000 | 6.563 | 1.1875 | A572-65 |
| 15 | 6 | 1 | 6 | 0.5 | Welded | n/a | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 16 | 6 | 1 | 6 | 0.5 | PC 8.8 - M20 (100) | 30 | PC 8.8 - M20 (100) | 30.000 | 16.000 | 4.750 | 1.1875 | A572-65 |
| 17 | 4.5 | 1.25 | 5.625 | 0.625 | PC 8.8 - M20 (100) | 21 | PC 8.8 - M20 (100) | 21.000 | 24.000 | 4.063 | 1.1875 | A572-65 |

Connection Details for Custom Reinforcements

| Reinforcement | End | \# Bolts | N or X | Bolt Spacing (in) | Edge Dist (in) | Weld Grade (ksi) | Transverse (Horiz.) Weld Type | Horiz. Weld Length (in) | Horiz. Groove Depth (in) | Horiz. Groove Angle (deg) |  | Vertical Weld Length (in) | Vertical Fillet Size (in) | Rev H Connection Capacity (kip) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { PL } 0.75 \times 4.00 \\ (100 \mathrm{ksi}) \\ \hline \end{gathered}$ | Top Bottom | 55 | N | 3 | 3 | - | - | - | - | - | - | - | - | - |
|  |  |  | N | 3 | 3 | - | - | - | - | - | - | - | - | - |
| $\begin{gathered} \text { (TS) } 1.25 \times 7.00 \\ (65 \mathrm{ksi}) \mathrm{PJP} \end{gathered}$ | Top | 0 | N | 0 | 0 | - | - | - | - | - | - | - | - | 1000 |
|  | Bottom | - | - | - | - | 80 | PJP Groove | 12.5 | 0.5 | 45 | 0.625 | - | - | - |
| CCI-WCFP-065125 | Top Bottom | 11 | N | 3 | 3 | - | - | - | - | - | - | - | - | - |
|  |  | - | - | - | - | 80 | CJP Groove | 6.5 | 1.25 | 45 | 0.5 | - | - |  |
| CCI-WCFP-060100 | Top 10 |  | N | 3 | 3 | - | - ${ }^{-}$ | 6 | - | - | - | - | - | - |
|  | Bottom | - |  | - | - | 80 | CJP Groove |  | 1 | 45 | 0.375 | - | - |  |
| CCI-CFP-060100 | TopBottom | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ | NN | 3 | 3 | - | -- | - | - | - | - | - | - | - |
|  |  |  |  | 3 | 3 | - |  | - | - | - | - | - | - |  |
| CCI-CFP-045125 | Top Bottom | 7 | NN | 33 | 33 | - | - | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  | - |  | - | - | - |

TNX Geometry Input

| Increment (ft): |  |  | 5 | Export to TNX |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Section Height (ft) |  |  | Section Length (ft) | Lap Splice Length <br> (ft) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Tapered Pole Grade | Weight Multiplier |
| 1 | 130 | - | 125 | 5 |  | 12 | 10.525 | 11.775 | 0.1875 | A572-65 | 1.000 |
| 2 | 125 | - | 120 | 5 |  | 12 | 11.775 | 13.025 | 0.1875 | A572-65 | 1.000 |
| 3 | 120 | - |  | 5 |  | 12 | 13.025 | 14.275 | 0.1875 | A572-65 | 1.000 |
| 4 | 115 | - | 110 | 5 | 0 | 12 | 14.275 | 15.525 | 0.1875 | A572-65 | 1.000 |
| 5 | 110 | - | 105 | 5 |  | 12 | 15.525 | 16.776 | 0.25 | A572-65 | 1.000 |
| 6 | 105 | - | 100 | 5 |  | 12 | 16.776 | 18.027 | 0.25 | A572-65 | 1.000 |
| 7 | 100 | - | 95 | 5 |  | 12 | 18.027 | 19.277 | 0.25 | A572-65 | 1.000 |
| 8 | 95 | - | 90 | 5 |  | 12 | 19.277 | 20.528 | 0.25 | A572-65 | 1.000 |
| 9 | 90 | - | 89.75 | 0.25 |  | 12 | 20.528 | 20.591 | 0.5 | A572-65 | 0.924 |
| 10 | 89.75 | - | 84.75 | 5 |  | 12 | 20.591 | 21.841 | 0.48125 | A572-65 | 0.934 |
| 11 | 84.75 | - | 84.58 | 0.17 |  | 12 | 21.841 | 21.884 | 0.475 | A572-65 | 0.945 |
| 12 | 84.58 | - | 84.33 | 0.25 |  | 12 | 21.884 | 21.946 | 0.6375 | A572-65 | 0.914 |
| 13 | 84.33 | - | 83.42 | 0.91 |  | 12 | 21.946 | 22.174 | 0.625 | A572-65 | 0.927 |
| 14 | 83.42 | - | 83.17 | 0.25 |  | 12 | 22.174 | 22.237 | 0.95 | A572-65 | 0.877 |
| 15 | 83.17 | - | 83 | 0.17 |  | 12 | 22.237 | 22.279 | 0.95 | A572-65 | 0.876 |
| 16 | 83 | - | 82.75 | 0.25 |  | 12 | 22.279 | 22.342 | 0.7 | A572-65 | 0.896 |
| 17 | 82.75 | - | 77.75 | 5 |  | 12 | 22.342 | 23.592 | 0.6625 | A572-65 | 0.914 |
| 18 | 77.75 | - | 74 | 7.75 | 4 | 12 | 23.592 | 25.531 | 0.65 | A572-65 | 0.909 |
| 19 | 74 | - | 69 | 5 |  | 12 | 24.030 | 25.281 | 0.7 | A572-65 | 0.921 |
| 20 | 69 | - | 67.08 | 1.92 |  | 12 | 25.281 | 25.761 | 0.6875 | A572-65 | 0.928 |
| 21 | 67.08 | - | 66.83 | 0.25 |  | 12 | 25.761 | 25.824 | 0.6875 | A572-65 | 0.927 |
| 22 | 66.83 | - | 64.08 | 2.75 |  | 12 | 25.824 | 26.512 | 0.675 | A572-65 | 0.931 |
| 23 | 64.08 | - | 63.83 | 0.25 |  | 12 | 26.512 | 26.574 | 0.7375 | A572-65 | 1.000 |
| 24 | 63.83 | - | 62.5 | 1.33 |  | 12 | 26.574 | 26.907 | 0.7375 | A572-65 | 0.993 |
| 25 | 62.5 | - | 62.25 | 0.25 |  | 12 | 26.907 | 26.969 | 0.8625 | A572-65 | 0.914 |
| 26 | 62.25 | - | 57.25 | 5 |  | 12 | 26.969 | 28.220 | 0.8375 | A572-65 | 0.914 |
| 27 | 57.25 | - | 53.5 | 3.75 |  | 12 | 28.220 | 29.158 | 0.8125 | A572-65 | 0.923 |
| 28 | 53.5 | - | 53.25 | 0.25 |  | 12 | 29.158 | 29.220 | 0.8375 | A572-65 | 0.934 |
| 29 | 53.25 | - | 52.58 | 0.67 |  | 12 | 29.220 | 29.388 | 0.825 | A572-65 | 0.945 |
| 30 | 52.58 | - | 52.33 | 0.25 |  | 12 | 29.388 | 29.450 | 0.8625 | A572-65 | 0.918 |
| 31 | 52.33 | - | 47.33 | 5 |  | 12 | 29.450 | 30.701 | 0.8375 | A572-65 | 0.921 |
| 32 | 47.33 | - | 44.58 | 2.75 |  | 12 | 30.701 | 31.389 | 0.8125 | A572-65 | 0.935 |
| 33 | 44.58 | - | 44.33 | 0.25 |  | 12 | 31.389 | 31.451 | 0.8125 | A572-65 | 0.934 |
| 34 | 44.33 | - | 41.92 | 2.41 |  | 12 | 31.451 | 32.054 | 0.8 | A572-65 | 0.938 |
| 35 | 41.92 | - | 41.67 | 0.25 |  | 12 | 32.054 | 32.117 | 0.8125 | A572-65 | 0.941 |
| 36 | 41.67 | - | 39 | 7.59 | 4.92 | 12 | 32.117 | 34.015 | 0.7875 | A572-65 | 0.958 |
| 37 | 39 | - | 34 | 5 |  | 12 | 32.159 | 33.408 | 0.81875 | A572-65 | 0.950 |
| 38 | 34 | - | 29 | 5 |  | 12 | 33.408 | 34.657 | 0.79375 | A572-65 | 0.960 |
| 39 | 29 | - | 26.92 | 2.08 |  | 12 | 34.657 | 35.177 | 0.79375 | A572-65 | 0.952 |
| 40 | 26.92 | - | 26.67 | 0.25 |  | 12 | 35.177 | 35.239 | 0.89375 | A572-65 | 0.968 |
| 41 | 26.67 | - | 21.67 | 5 |  | 12 | 35.239 | 36.488 | 0.86875 | A572-65 | 0.974 |
| 42 | 21.67 | - | 18 | 3.67 |  | 12 | 36.488 | 37.404 | 0.85625 | A572-65 | 0.974 |
| 43 | 18 | - | 17.75 | 0.25 |  | 12 | 37.404 | 37.467 | 0.99375 | A572-65 | 0.947 |
| 44 | 17.75 | - | 17.5 | 0.25 |  | 12 | 37.467 | 37.529 | 0.99375 | A572-65 | 0.946 |
| 45 | 17.5 | - | 17.25 | 0.25 |  | 12 | 37.529 | 37.592 | 0.99375 | A572-65 | 0.945 |
| 46 | 17.25 | - | 17.08 | 0.17 |  | 12 | 37.592 | 37.634 | 0.99375 | A572-65 | 0.945 |
| 47 | 17.08 | - | 16.83 | 0.25 |  | 12 | 37.634 | 37.697 | 0.89375 | A572-65 | 0.961 |
| 48 | 16.83 | - | 13 | 3.83 |  | 12 | 37.697 | 38.653 | 0.88125 | A572-65 | 0.960 |
| 49 | 13 | - | 12.75 | 0.25 |  | 12 | 38.653 | 38.716 | 1.05625 | A572-65 | 0.944 |
| 50 | 12.75 | - | 11.92 | 0.83 |  | 12 | 38.716 | 38.923 | 1.04375 | A572-65 | 0.952 |
| 51 | 11.92 | - | 11.67 | 0.25 |  | 12 | 38.923 | 38.985 | 0.81875 | A572-65 | 1.026 |
| 52 | 11.67 | - | 6.67 | 5 |  | 12 | 38.985 | 40.234 | 0.79375 | A572-65 | 1.038 |
| 53 | 6.67 | - |  | 0.17 |  | 12 | 40.234 | 40.277 | 0.79375 | A572-65 | 1.037 |
| 54 | 6.5 | - | 6.25 | 0.25 |  | 12 | 40.277 | 40.339 | 0.91875 | A572-65 | 0.968 |
| 55 | 6.25 | - | 3.75 | 2.5 |  | 12 | 40.339 | 40.963 | 0.90625 | A572-65 | 0.971 |
| 56 | 3.75 | - |  | 0.25 |  | 12 | 40.963 | 41.026 | 1.00625 | A572-65 | 0.934 |
| 57 | 3.5 | - |  | 0.5 |  | 12 | 41.026 | 41.151 | 0.99375 | A572-65 | 0.944 |
| 58 | 3 | - | 2.75 | 0.25 |  | 12 | 41.151 | 41.213 | 0.99375 | A572-65 | 0.913 |
| 59 | 2.75 | - | 0 | 2.75 |  | 12 | 41.213 | 41.900 | 1.01875 | A572-65 | 0.882 |

## TNX Section Forces

| Increment (ft): |  | ) 5 | TNX Output |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Section | Height (ft) | $\mathrm{P}_{\mathrm{u}} \quad$ (K) | $\mathrm{M}_{\mathrm{ux}} \quad \text { (kip- }$ <br> ft) | $\mathrm{V}_{\mathrm{u}} \quad$ (K) |
| 1 | 130 | 125 | 0.10 | 0.63 | 0.26 |
| 2 | 125 | 120 | 4.16 | 5.23 | 8.02 |
| 3 | 120 | - 115 | 4.27 | 46.78 | 8.57 |
| 4 | 115 | - 110 | 4.50 | 91.06 | 9.14 |
| 5 | 110 | 105 | 8.84 | 161.84 | 14.31 |
| 6 | 105 | - 100 | 9.33 | 236.53 | 15.39 |
| 7 | 100 | - 95 | 13.25 | 327.43 | 20.65 |
| 8 | 95 | - 90 | 13.91 | 431.90 | 21.17 |
| 9 | 90 | - 89.75 | 13.98 | 437.20 | 21.18 |
| 10 | 89.75 | - 84.75 | 17.69 | 551.23 | 24.94 |
| 11 | 84.75 | 84.58 | 17.74 | 555.47 | 24.95 |
| 12 | 84.58 | - 84.33 | 17.81 | 561.71 | 24.99 |
| 13 | 84.33 | - 83.42 | 18.02 | 584.50 | 25.12 |
| 14 | 83.42 | - 83.17 | 18.11 | 590.79 | 25.16 |
| 15 | 83.17 | - 83 | 18.17 | 595.07 | 25.19 |
| 16 | 83 | - 82.75 | 18.23 | 601.37 | 25.22 |
| 17 | 82.75 | - 77.75 | 19.52 | 729.73 | 26.11 |
| 18 | 77.75 | 74 | 23.55 | 839.17 | 30.13 |
| 19 | 74 | - 69 | 25.74 | 992.28 | 31.07 |
| 20 | 69 | - 67.08 | 26.31 | 1052.27 | 31.41 |
| 21 | 67.08 | - 66.83 | 26.42 | 1060.12 | 31.43 |
| 22 | 66.83 | - 64.08 | 27.25 | 1147.24 | 31.90 |
| 23 | 64.08 | - 63.83 | 27.35 | 1155.23 | 31.93 |
| 24 | 63.83 | 62.5 | 27.80 | 1197.88 | 32.17 |
| 25 | 62.5 | - 62.25 | 27.91 | 1205.93 | 32.20 |
| 26 | 62.25 | - 57.25 | 29.71 | 1369.27 | 33.09 |
| 27 | 57.25 | - 53.5 | 31.10 | 1494.67 | 33.75 |
| 28 | 53.5 | - 53.25 | 31.21 | 1503.12 | 33.78 |
| 29 | 53.25 | - 52.58 | 31.47 | 1525.81 | 33.91 |
| 30 | 52.58 | - 52.33 | 31.57 | 1534.30 | 33.95 |
| 31 | 52.33 | - 47.33 | 33.52 | 1706.34 | 34.83 |
| 32 | 47.33 | - 44.58 | 34.62 | 1802.82 | 35.31 |
| 33 | 44.58 | - 44.33 | 34.74 | 1811.66 | 35.34 |
| 34 | 44.33 | - 41.92 | 35.70 | 1897.38 | 35.76 |
| 35 | 41.92 | - 41.67 | 35.82 | 1906.33 | 35.78 |
| 36 | 41.67 | - 39 | 36.90 | 2002.54 | 36.24 |
| 37 | 39 | - 34 | 40.57 | 2186.20 | 37.18 |
| 38 | 34 | - 29 | 42.74 | 2374.21 | 37.98 |
| 39 | 29 | - 26.92 | 43.66 | 2453.58 | 38.31 |
| 40 | 26.92 | - 26.67 | 43.79 | 2463.17 | 38.33 |
| 41 | 26.67 | - 21.67 | 46.23 | 2656.96 | 39.13 |
| 42 | 21.67 | - 18 | 48.05 | 2801.68 | 39.70 |
| 43 | 18 | - 17.75 | 48.21 | 2811.62 | 39.71 |
| 44 | 17.75 | - 17.5 | 48.35 | 2821.56 | 39.75 |
| 45 | 17.5 | - 17.25 | 48.48 | 2831.51 | 39.79 |
| 46 | 17.25 | - 17.08 | 48.58 | 2838.28 | 39.82 |
| 47 | 17.08 | - 16.83 | 48.70 | 2848.25 | 39.85 |
| 48 | 16.83 | - 13 | 50.67 | 3002.09 | 40.43 |
| 49 | 13 | - 12.75 | 50.83 | 3012.21 | 40.44 |
| 50 | 12.75 | - 11.92 | 51.31 | 3045.86 | 40.58 |
| 51 | 11.92 | - 11.67 | 51.45 | 3056.02 | 40.61 |
| 52 | 11.67 | - 6.67 | 54.06 | 3260.98 | 41.32 |
| 53 | 6.67 | - 6.5 | 54.17 | 3268.01 | 41.33 |
| 54 | 6.5 | - 6.25 | 54.31 | 3278.36 | 41.37 |
| 55 | 6.25 | - 3.75 | 55.69 | 3382.32 | 41.75 |
| 56 | 3.75 | - 3.5 | 55.86 | 3392.77 | 41.76 |
| 57 | 3.5 | - 3 | 56.15 | 3413.69 | 41.84 |
| 58 | 3 | - 2.75 | 56.30 | 3424.16 | 41.87 |
| 59 | 2.75 | - 0 | 57.87 | 3539.99 | 42.31 |

Analysis Results

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 130-125 | Pole | TP11.775×10.525×0.1875 | Pole | 0.5\% | Pass |
| 125-120 | Pole | TP13.025×11.775×0.1875 | Pole | 4.6\% | Pass |
| 120-115 | Pole | TP14.275x13.025×0.1875 | Pole | 26.0\% | Pass |
| 115-110 | Pole | TP15.525x14.275×0.1875 | Pole | 41.8\% | Pass |
| 110-105 | Pole | TP16.776x15.525×0.25 | Pole | 48.3\% | Pass |
| 105-100 | Pole | TP18.027×16.776×0.25 | Pole | 60.6\% | Pass |
| 100-95 | Pole | TP19.277x18.027×0.25 | Pole | 73.4\% | Pass |
| 95-90 | Pole | TP20.528x19.277×0.25 | Pole | 84.8\% | Pass |
| 90-89.75 | Pole + Reinf. | TP20.591×20.528×0.5 | Reinf. 12 Tension Rupture | 75.7\% | Pass |
| 89.75-84.75 | Pole + Reinf. | TP21.841×20.591×0.4813 | Reinf. 12 Tension Rupture | 87.3\% | Pass |
| 84.75-84.58 | Pole + Reinf. | TP21.884×21.841×0.475 | Reinf. 12 Tension Rupture | 87.7\% | Pass |
| 84.58-84.33 | Pole + Reinf. | TP21.946x21.884×0.6375 | Reinf. 12 Tension Rupture | 67.8\% | Pass |
| 84.33-83.42 | Pole + Reinf. | TP22.174x21.946x0.625 | Reinf. 12 Tension Rupture | 69.6\% | Pass |
| 83.42-83.17 | Pole + Reinf. | TP22.237x22.174×0.95 | Reinf. 17 Tension Rupture | 48.8\% | Pass |
| 83.17-83 | Pole + Reinf. | TP22.279x22.237×0.95 | Reinf. 17 Tension Rupture | 49.1\% | Pass |
| 83-82.75 | Pole + Reinf. | TP22.342×22.279x0.7 | Reinf. 17 Tension Rupture | 65.2\% | Pass |
| 82.75-77.75 | Pole + Reinf. | TP23.592×22.342×0.6625 | Reinf. 17 Tension Rupture | 73.3\% | Pass |
| 77.75-74 | Pole + Reinf. | TP25.531×23.592×0.65 | Reinf. 17 Tension Rupture | 79.9\% | Pass |
| 74-69 | Pole + Reinf. | TP25.281×24.03x0.7 | Reinf. 17 Tension Rupture | 82.2\% | Pass |
| 69-67.08 | Pole + Reinf. | TP25.761×25.281×0.6875 | Reinf. 17 Tension Rupture | 84.8\% | Pass |
| 67.08-66.83 | Pole + Reinf. | TP25.824×25.761×0.6875 | Reinf. 17 Tension Rupture | 85.1\% | Pass |
| 66.83-64.08 | Pole + Reinf. | TP26.512x25.824×0.675 | Reinf. 17 Tension Rupture | 88.5\% | Pass |
| 64.08-63.83 | Pole + Reinf. | TP26.574×26.512×0.7375 | Reinf. 17 Tension Rupture | 85.0\% | Pass |
| 63.83-62.5 | Pole + Reinf. | TP26.907×26.574×0.7375 | Reinf. 17 Tension Rupture | 86.5\% | Pass |
| 62.5-62.25 | Pole + Reinf. | TP26.969×26.907×0.8625 | Reinf. 17 Tension Rupture | 71.7\% | Pass |
| 62.25-57.25 | Pole + Reinf. | TP28.22x26.969x0.8375 | Reinf. 17 Tension Rupture | 76.4\% | Pass |
| 57.25-53.5 | Pole + Reinf. | TP29.158×28.22×0.8125 | Reinf. 17 Tension Rupture | 79.6\% | Pass |
| 53.5-53.25 | Pole + Reinf. | TP29.22x29.158x0.8375 | Reinf. 10 Tension Rupture | 78.9\% | Pass |
| 53.25-52.58 | Pole + Reinf. | TP29.388x29.22x0.825 | Reinf. 10 Tension Rupture | 79.5\% | Pass |
| 52.58-52.33 | Pole + Reinf. | TP29.45×29.388x0.8625 | Reinf. 10 Tension Rupture | 76.6\% | Pass |
| 52.33-47.33 | Pole + Reinf. | TP30.701×29.45x0.8375 | Reinf. 10 Tension Rupture | 80.5\% | Pass |
| 47.33-44.58 | Pole + Reinf. | TP31.389×30.701×0.8125 | Reinf. 10 Tension Rupture | 82.4\% | Pass |
| 44.58-44.33 | Pole + Reinf. | TP31.451×31.389×0.8125 | Reinf. 10 Tension Rupture | 82.6\% | Pass |
| 44.33-41.92 | Pole + Reinf. | TP32.054×31.451×0.8 | Reinf. 10 Tension Rupture | 84.3\% | Pass |
| 41.92-41.67 | Pole + Reinf. | TP32.117×32.054×0.8125 | Reinf. 9 Tension Rupture | 75.1\% | Pass |
| 41.67-39 | Pole + Reinf. | TP34.015 $32.117 \times 0.7875$ | Reinf. 9 Tension Rupture | 76.6\% | Pass |
| 39-34 | Pole + Reinf. | TP33.408×32.159×0.8188 | Reinf. 9 Tension Rupture | 78.3\% | Pass |
| 34-29 | Pole + Reinf. | TP34.657×33.408×0.7938 | Reinf. 9 Tension Rupture | 80.6\% | Pass |
| 29-26.92 | Pole + Reinf. | TP35.177×34.657×0.7938 | Reinf. 9 Tension Rupture | 81.5\% | Pass |
| 26.92-26.67 | Pole + Reinf. | TP35.239×35.177×0.8938 | Reinf. 7 Tension Rupture | 76.3\% | Pass |
| 26.67-21.67 | Pole + Reinf. | TP36.488×35.239×0.8688 | Reinf. 7 Tension Rupture | 78.4\% | Pass |
| 21.67-18 | Pole + Reinf. | TP37.404×36.488×0.8563 | Reinf. 7 Tension Rupture | 79.8\% | Pass |
| 18-17.75 | Pole + Reinf. | TP37.467×37.404×0.9938 | Reinf. 16 Tension Rupture | 67.1\% | Pass |
| 17.75-17.5 | Pole + Reinf. | TP37.529x37.467×0.9938 | Reinf. 16 Tension Rupture | 67.2\% | Pass |
| 17.5-17.25 | Pole + Reinf. | TP37.592×37.529x0.9938 | Reinf. 15 Tension Rupture | 67.3\% | Pass |
| 17.25-17.08 | Pole + Reinf. | TP37.634×37.592×0.9938 | Reinf. 15 Tension Rupture | 67.3\% | Pass |
| 17.08-16.83 | Pole + Reinf. | TP37.697×37.634×0.8938 | Reinf. 15 Tension Rupture | 73.5\% | Pass |
| 16.83-13 | Pole + Reinf. | TP38.653×37.697×0.8813 | Reinf. 15 Tension Rupture | 74.8\% | Pass |
| 13-12.75 | Pole + Reinf. | TP38.716×38.653×1.0563 | Reinf. 5 Tension Rupture | 63.5\% | Pass |
| 12.75-11.92 | Pole + Reinf. | TP38.923×38.716×1.0438 | Reinf. 5 Tension Rupture | 63.8\% | Pass |
| 11.92-11.67 | Pole + Reinf. | TP38.985×38.923×0.8188 | Reinf. 15 Tension Rupture | 81.7\% | Pass |
| 11.67-6.67 | Pole + Reinf. | TP40.234×38.985×0.7938 | Reinf. 15 Tension Rupture | 83.3\% | Pass |
| $6.67-6.5$ | Pole + Reinf. | TP40.277×40.234×0.7938 | Reinf. 15 Tension Rupture | 83.4\% | Pass |
| 6.5-6.25 | Pole + Reinf. | TP40.339x40.277×0.9188 | Reinf. 5 Tension Rupture | 77.9\% | Pass |
| 6.25-3.75 | Pole + Reinf. | TP40.963x40.339x0.9063 | Reinf. 5 Tension Rupture | 78.6\% | Pass |
| 3.75-3.5 | Pole + Reinf. | TP41.026x40.963×1.0063 | Reinf. 14 Tension Rupture | 68.1\% | Pass |
| 3.5-3 | Pole + Reinf. | TP41.151×41.026×0.9938 | Reinf. 14 Tension Rupture | 68.3\% | Pass |
| 3-2.75 | Pole + Reinf. | TP41.213x41.151×0.9938 | Reinf. 15 Tension Rupture | 73.2\% | Pass |
| 2.75-0 | Pole + Reinf. | TP41.9x41.213x1.0188 | Reinf. 4 Weldment | 86.8\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 84.8\% | Pass |
|  |  |  | Reinforcement | 88.5\% | Pass |
|  |  |  | Overall | 88.5\% | Pass |

## Additional Calculations

| Section | Moment of Inertia (in ${ }^{4}$ ) |  |  | Area (in ${ }^{2}$ ) |  |  | \% Capacity* |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pole | Reinf. | Total | Pole | Reinf. | Total | Pole | R1 | R2 | R3 | R4 | R5 | R6 | R7 | R8 | R9 | R10 | R11 | R12 | R13 | R14 | R15 | R16 | R17 |
| 130-125 | 120 | n/a | 120 | 6.99 | n/a | 6.99 | 0.5\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 125-120 | 163 | n/a | 163 | 7.74 | n/a | 7.74 | 4.6\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 120-115 | 216 | n/a | 216 | 8.49 | n/a | 8.49 | 26.0\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 115-110 | 278 | n/a | 278 | 9.25 | n/a | 9.25 | 41.8\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 110-105 | 464 | n/a | 464 | 13.28 | n/a | 13.28 | 48.3\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 105-100 | 578 | n/a | 578 | 14.29 | n/a | 14.29 | 60.6\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100-95 | 709 | n/a | 709 | 15.30 | n/a | 15.30 | 73.4\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 95-90 | 858 | n/a | 858 | 16.30 | n/a | 16.30 | 84.8\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 90-89.75 | 866 | 799 | 1664 | 16.35 | 13.50 | 29.85 | 42.9\% |  |  |  |  |  |  |  |  |  |  |  | 75.7\% |  |  |  |  |  |
| 89.75-84.75 | 1036 | 892 | 1928 | 17.36 | 13.50 | 30.86 | 50.3\% |  |  |  |  |  |  |  |  |  |  |  | 87.3\% |  |  |  |  |  |
| 84.75-84.58 | 1042 | 896 | 1937 | 17.39 | 13.50 | 30.89 | 50.6\% |  |  |  |  |  |  |  |  |  |  |  | 87.7\% |  |  |  |  |  |
| 84.58-84.33 | 1051 | 1486 | 2537 | 17.44 | 22.50 | 39.94 | 39.2\% |  |  | 51.5\% |  |  |  |  |  |  |  |  | 67.8\% |  |  |  |  |  |
| 84.33-83.42 | 1084 | 1516 | 2600 | 17.62 | 22.50 | 40.12 | 40.3\% |  |  | 52.8\% |  |  |  |  |  |  |  |  | 69.6\% |  |  |  |  |  |
| 83.42-83.17 | 1094 | 2703 | 3796 | 17.67 | 39.38 | 57.05 | 28.0\% |  |  | 36.7\% |  |  |  |  |  |  |  |  | 48.3\% |  |  |  |  | 48.8\% |
| 83.17-83 | 1100 | 2712 | 3812 | 17.71 | 39.38 | 57.08 | 28.2\% |  |  | 36.8\% |  |  |  |  |  |  |  |  | 48.5\% |  |  |  |  | 49.1\% |
| 83-82.75 | 1109 | 1795 | 2905 | 17.76 | 25.88 | 43.63 | 37.5\% |  |  | 49.0\% |  |  |  |  |  |  |  |  |  |  |  |  |  | 65.2\% |
| 82.75-77.75 | 1309 | 1990 | 3299 | 18.76 | 25.88 | 44.64 | 43.0\% |  |  | 55.1\% |  |  |  |  |  |  |  |  |  |  |  |  |  | 73.3\% |
| 77.75-74 | 1473 | 2142 | 3615 | 19.52 | 25.88 | 45.39 | 47.6\% |  |  | 60.1\% |  |  |  |  |  |  |  |  |  |  |  |  |  | 79.9\% |
| 74-69 | 2002 | 2269 | 4271 | 25.09 | 25.88 | 50.96 | 46.5\% |  |  | 61.9\% |  |  |  |  |  |  |  |  |  |  |  |  |  | 82.2\% |
| 69-67.08 | 2120 | 2351 | 4471 | 25.57 | 25.88 | 51.45 | 48.0\% |  |  | 63.8\% |  |  |  |  |  |  |  |  |  |  |  |  |  | 84.8\% |
| 67.08-66.83 | 2135 | 2362 | 4498 | 25.63 | 25.88 | 51.51 | 48.1\% |  | 64.1\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 85.1\% |
| 66.83-64.08 | 2313 | 2483 | 4796 | 26.33 | 25.88 | 52.20 | 50.4\% |  | 66.7\% |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 88.5\% |
| 64.08-63.83 | 2353 | 2954 | 5307 | 26.39 | 34.88 | 61.26 | 50.6\% |  | 64.0\% |  |  |  |  |  |  |  |  | 69.8\% |  |  |  |  |  | 85.0\% |
| 63.83-62.5 | 2444 | 3025 | 5468 | 26.72 | 34.88 | 61.60 | 51.8\% |  | 65.2\% |  |  |  |  |  |  |  |  | 71.1\% |  |  |  |  |  | 86.5\% |
| 62.5-62.25 | 2436 | 3898 | 6334 | 26.78 | 39.38 | 66.16 | 41.1\% |  | 54.0\% |  |  |  |  |  |  |  | 71.0\% | 71.0\% |  |  |  |  |  | 71.7\% |
| 62.25-57.25 | 2795 | 4250 | 7046 | 28.04 | 39.38 | 67.42 | 44.5\% |  | 57.6\% |  |  |  |  |  |  |  | 75.7\% | 75.7\% |  |  |  |  |  | 76.4\% |
| 57.25-53.5 | 3087 | 4525 | 7612 | 28.98 | 39.38 | 68.36 | 46.9\% |  | 60.0\% |  |  |  |  |  |  |  | 79.0\% | 79.0\% |  |  |  |  |  | 79.6\% |
| 53.5-53.25 | 3110 | 4720 | 7830 | 29.05 | 42.38 | 71.42 | 47.0\% |  | 59.2\% |  |  |  |  |  |  | 67.7\% | 78.9\% |  |  |  |  |  |  | 78.5\% |
| 53.25-52.58 | 3164 | 4772 | 7936 | 29.22 | 42.38 | 71.59 | 47.4\% |  | 59.6\% |  |  |  |  |  |  | 68.2\% | 79.5\% |  |  |  |  |  |  | 79.1\% |
| 52.58-52.33 | 3183 | 5071 | 8254 | 29.28 | 43.50 | 72.78 | 45.7\% |  | 57.6\% |  |  |  |  |  |  | 68.3\% | 76.6\% |  |  |  |  |  | 71.2\% |  |
| 52.33-47.33 | 3611 | 5485 | 9095 | 30.53 | 43.50 | 74.03 | 48.8\% |  | 60.5\% |  |  |  |  |  |  | 71.7\% | 80.5\% |  |  |  |  |  | 74.7\% |  |
| 47.33-44.58 | 3862 | 5719 | 9581 | 31.23 | 43.50 | 74.73 | 50.4\% |  | 61.9\% |  |  |  |  |  |  | 73.5\% | 82.4\% |  |  |  |  |  | 76.5\% |  |
| 44.58-44.33 | 3885 | 5740 | 9625 | 31.29 | 43.50 | 74.79 | 50.6\% | 63.2\% |  |  |  |  |  |  |  | 73.6\% | 82.6\% |  |  |  |  |  | 76.7\% |  |
| 44.33-41.92 | 4115 | 5950 | 10065 | 31.89 | 43.50 | 75.39 | 52.0\% | 64.4\% |  |  |  |  |  |  |  | 75.0\% | 84.3\% |  |  |  |  |  | 78.2\% |  |
| 41.92-41.67 | 4138 | 6045 | 10183 | 31.96 | 45.00 | 76.96 | 51.2\% | 63.1\% |  |  |  |  |  | 72.7\% |  | 75.1\% |  |  |  |  |  |  | 74.7\% |  |
| 41.67-39 | 4404 | 6293 | 10697 | 32.63 | 45.00 | 77.63 | 52.7\% | 64.4\% |  |  |  |  |  | 74.2\% |  | 76.6\% |  |  |  |  |  |  | 76.3\% |  |
| 39-34 | 5114 | 6529 | 11643 | 36.55 | 45.00 | 81.55 | 52.3\% | 65.8\% |  |  |  |  |  | 76.0\% |  | 78.3\% |  |  |  |  |  |  | 78.0\% |  |
| 34-29 | 5716 | 7014 | 12729 | 37.93 | 45.00 | 82.93 | 54.7\% | 67.7\% |  |  |  |  |  | 78.4\% |  | 80.6\% |  |  |  |  |  |  | 80.3\% |  |
| 29-26.92 | 5979 | 7220 | 13200 | 38.50 | 45.00 | 83.50 | 55.6\% | 68.5\% |  |  |  |  |  | 79.3\% |  | 81.5\% |  |  |  |  |  |  | 81.2\% |  |
| 26.92-26.67 | 6047 | 8878 | 14925 | 38.57 | 57.00 | 95.57 | 52.9\% | 64.1\% |  |  |  |  |  | 76.3\% | 67.4\% | 69.6\% |  |  |  |  |  |  | 72.8\% |  |
| 26.67-21.67 | 6718 | 9488 | 16206 | 39.95 | 57.00 | 96.95 | 55.1\% | 65.8\% |  |  |  |  |  | 78.4\% | 69.3\% | 71.5\% |  |  |  |  |  |  | 74.7\% |  |
| 21.67-18 | 7242 | 9949 | 17190 | 40.96 | 57.00 | 97.96 | 56.7\% | 67.0\% |  |  |  |  |  | 79.8\% | 70.6\% | 72.8\% |  |  |  |  |  |  | 76.0\% |  |
| 18-17.75 | 7238 | 12612 | 19850 | 41.03 | 69.38 | 110.41 | 47.3\% | 56.1\% |  |  |  |  |  | 65.3\% | 66.1\% |  |  |  |  |  | 64.8\% |  | 67.1\% |  |
| 17.75-17.5 | 7275 | 12652 | 19927 | 41.10 | 69.38 | 110.48 | 47.4\% | 56.2\% |  |  |  |  |  | 65.3\% | 66.2\% |  |  |  |  |  | 64.9\% |  | 67.2\% |  |
| 17.5-17.25 | 7312 | 12693 | 20005 | 41.17 | 69.38 | 110.54 | 47.5\% | 56.3\% |  |  |  |  |  | 65.4\% | 66.3\% |  |  |  |  |  | 64.9\% | 67.3\% |  |  |
| 17.25-17.08 | 7337 | 12721 | 20057 | 41.22 | 69.38 | 110.59 | 47.6\% | 56.3\% |  |  |  |  |  | 65.5\% | 66.3\% |  |  |  |  |  | 65.0\% | 67.3\% |  |  |
| 17.08-16.83 | 7374 | 11092 | 18466 | 41.29 | 60.38 | 101.66 | 52.0\% |  |  |  |  |  |  | 71.4\% | 72.4\% |  |  |  |  |  | 70.9\% | 73.5\% |  |  |
| 16.83-13 | 7955 | 11640 | 19595 | 42.34 | 60.38 | 102.72 | 53.5\% |  |  |  |  |  |  | 72.7\% | 73.7\% |  |  |  |  |  | 72.2\% | 74.8\% |  |  |
| 13-12.75 | 7995 | 15215 | 23210 | 42.41 | 78.38 | 120.79 | 44.8\% |  |  |  |  | 63.5\% | 59.8\% | 61.8\% | 62.4\% |  |  |  |  |  | 61.2\% | 63.3\% |  |  |
| 12.75-11.92 | 8125 | 15374 | 23499 | 42.64 | 78.38 | 121.02 | 45.1\% |  |  |  |  | 63.8\% | 60.1\% | 62.0\% | 62.7\% |  |  |  |  |  | 61.5\% | 63.6\% |  |  |
| 11.92-11.67 | 8177 | 10548 | 18725 | 42.71 | 60.38 | 103.09 | 57.9\% |  |  |  |  | 80.8\% | 65.4\% |  |  |  |  |  |  |  | 73.5\% | 81.7\% |  |  |
| 11.67-6.67 | 8995 | 11209 | 20204 | 44.09 | 60.38 | 104.47 | 59.9\% |  |  |  |  | 82.3\% | 66.9\% |  |  |  |  |  |  |  | 75.0\% | 83.3\% |  |  |
| 6.67-6.5 | 9024 | 11232 | 20256 | 44.14 | 60.38 | 104.51 | 60.0\% |  |  |  |  | 82.4\% | 67.0\% |  |  |  |  |  |  |  | 75.0\% | 83.4\% |  |  |
| 6.5-6.25 | 9256 | 14118 | 23374 | 44.21 | 68.50 | 112.71 | 56.2\% |  |  |  |  | 77.9\% | 67.0\% |  |  |  |  |  |  | 62.9\% | 71.2\% | 77.4\% |  |  |
| 6.25-3.75 | 9693 | 14546 | 24240 | 44.90 | 68.50 | 113.40 | 57.2\% |  |  |  |  | 78.6\% | 67.7\% |  |  |  |  |  |  | 63.5\% | 71.9\% | 78.2\% |  |  |
| 3.75-3.5 | 9595 | 17018 | 26613 | 44.97 | 76.00 | 120.97 | 50.2\% |  |  |  | 57.4\% | 62.1\% | 66.6\% |  |  |  |  |  |  |  | 68.1\% | 66.6\% |  |  |
| 3.5-3 | 9683 | 17117 | 26800 | 45.10 | 76.00 | 121.10 | 50.4\% |  |  |  | 57.5\% | 62.3\% | 66.7\% |  |  |  |  |  |  |  | 68.3\% | 66.8\% |  |  |
| 3-2.75 | 9907 | 16832 | 26739 | 45.17 | 72.13 | 117.30 | 54.8\% |  |  |  | 64.1\% |  | 67.0\% |  |  |  |  |  |  | 56.8\% | 71.2\% | 73.2\% |  |  |
| 2.75-0 | 10321 | 18654 | 28974 | 45.93 | 72.13 | 118.06 | 52.8\% |  |  |  | 86.8\% |  | 67.8\% |  |  |  |  |  |  | 57.5\% | 72.0\% | 74.0\% |  |  |

Rating per TIA-222-H Section 15.5.

| BU \# | 806376 |
| ---: | :---: |
| Site Name | HRT 100 943239 |
| Order \# | 556638 Rev 1 |


| TIA-222 Revision | H |
| ---: | :---: |


| Applied Loads |  |
| ---: | :---: |
| Moment (kip-ft) | 91.06 |
| Axial Force (kips) | 4.50 |
| Shear Force (kips) | 9.14 |


| Site Info |  |
| ---: | :---: |
| BU \# | 806376 |
| Site Name | HRT 100 943239 |
| Order \# | 556638 Rev 1 |


| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | $H$ |
| Grout Considered: | See Custom Sheet |
| $\mathrm{l}_{\mathrm{ar}}$ (in) | See Custom Sheet |


| Applied Loads |  |
| ---: | :---: |
| Moment (kip-ft) | 3539.99 |
| Axial Force (kips) | 57.87 |
| Shear Force (kips) |  |

*TIA-222-H Section 15.5 Applied


Connection Properties
Analysis Results

Anchor Rod Data
GROUP 1: (12) 2-1/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 49.88" BC GROUP 2: (3) 2-1/4" $\varnothing$ bolts (A193 Gr. B7 N; Fy=105 ksi, Fu=125 ksi) on $53.38^{\prime \prime}$ BC

Base Plate Data
55.88" OD x 2.5" Plate (A572-60; Fy=60 ksi, Fu=75 ksi)

Stiffener Data
N/A

Pole Data
41.9 " x 1.01875" 12-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)

Anchor Rod Summary
(units of kips, kip-in) GROUP 1:

| Pu_c = 225.34 | $\phi P n \_c=268.39$ | Stress Rating |
| :--- | :--- | :---: |
| $V u=3.53$ | $\phi V n=120.77$ | $\mathbf{8 4 . 7 \%}$ |
| $\mathrm{Mu}=6.3$ | $\phi \mathrm{Mn}=128.14$ | Pass |

GROUP 2:

| Pu_t = 235.99 | $\phi P n \_t=304.69$ | Stress Rating |
| :--- | :--- | :---: |
| $\mathrm{Vu=0}$ | $\phi V n=186.38$ | $\mathbf{7 3 . 8 \%}$ |
| $\mathrm{Mu}=0$ | $\phi \mathrm{Mn}=179.4$ | Pass |


| Base Plate Summary |  |  |
| :--- | :--- | :---: |
| Max Stress (ksi): | 32.35 | (Flexural) |
| Allowable Stress (ksi): | 54 |  |
| Stress Rating: | $\mathbf{5 7 . 1 \%}$ | Pass |

## $\mathbb{C C}$ plalate

| Elevation (ft) | 0 |
| :--- | :--- |

note: Bending interaction not considered when Grout Considered = "Yes"

| Bolt <br> Group | Resist <br> Axial | Resist Shear | Induce Plate <br> Bending | Grout <br> Considered | Apply at BARB <br> Elevation | BARB CL Elevation <br> (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | Yes | Yes | No | No |  |
| 2 | No | No | No | No | No |  |


| usto | Bolt Con | ection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bolt | Bolt Group ID | Location (deg.) | Diameter (in) | Material | Bolt Circle (in) | Eta Factor, n : | $\mathrm{l}_{\text {ar }}$ (in): | Thread Type | Area Override, in^2 $^{\wedge}$ | Tension Only |
| 1 | 1 | 0 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N -Included |  | No |
| 2 | 1 | 30 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N -Included |  | No |
| 3 | 1 | 60 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 4 | 1 | 90 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N -Included |  | No |
| 5 | 1 | 120 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N -Included |  | No |
| 6 | 1 | 150 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 7 | 1 | 180 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 8 | 1 | 210 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N -Included |  | No |
| 9 | 1 | 240 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 10 | 1 | 270 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 11 | 1 | 300 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 12 | 1 | 330 | 2.25 | A615-75 | 49.88 | 0.5 | 2.75 | N-Included |  | No |
| 13 | 2 | 15 | 2.25 | A193 Gr. B7 | 53.38 | 0.5 | 8.5 | N -Included |  | No |
| 14 | 2 | 135 | 2.25 | A193 Gr. B7 | 53.38 | 0.5 | 8.5 | N-Included |  | No |
| 15 | 2 | 255 | 2.25 | A193 Gr. B7 | 53.38 | 0.5 | 8.5 | N -Included |  | No |
|  |  |  |  |  |  |  |  |  |  |  |

## Plot Graphic



BU \# : 806376
Site Name: HRT 100943239
App. Number: 556638 Rev 1

\section*{| TIA-222 Revision: | H |
| ---: | :---: |
| Tower Type: | Monopole |}


| Top \& Bot. Pad Rein. Different?: | $\square$ |
| ---: | :---: |
| Block Foundation?: | $\square$ |
| Rectangular Pad?: | $\square$ |


| Superstructure Analysis Reactions |  |  |  |
| ---: | :---: | :--- | :---: |
| Compression, $\mathbf{P}_{\text {comp }}:$ |  | 58 |  |
| kase Shear, Vu_comp: | 42 | kips |  |
| Base |  |  |  |
|  |  |  |  |
| Moment, $\mathbf{M}_{\mathbf{u}}:$ | 3540 | ft -kips |  |
| Tower Height, $\mathbf{H}:$ | 130 | ft |  |
|  |  |  |  |
| BP Dist. Above Fdn, $\mathbf{b p}_{\text {dist: }}:$ | 5 | in |  |


| Pier Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Pier Shape: | Circular |  |  |
| Pier Diameter, dpier: | 6 | ft |  |
| Ext. Above Grade, E: | 0.5 | ft |  |
| Pier Rebar Size, Sc: | 10 |  |  |
| Pier Rebar Quantity, mc: | 36 |  |  |
| Pier Tie/Spiral Size, St: | 4 |  |  |
| Pier Tie/Spiral Quantity, mt: | 3 |  |  |
| Pier Reinforcement Type: | Tie |  |  |
| Pier Clear Cover, $\mathbf{c c}$ pier: | 3 | in |  |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating $^{*}$ | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 289.96 | 42.00 | $\mathbf{1 3 . 8 \%}$ | Pass |
| Bearing Pressure (ksf) | 7.50 | 3.40 | $\mathbf{4 5 . 3} \%$ | Pass |
| Overturning (kip*ft) | 5386.50 | 3914.50 | $\mathbf{7 2 . 7} \%$ | Pass |
| Pier Flexure (Comp.) (kip*ft) | 5778.60 | 3771.00 | $\mathbf{6 2 . 2 \%}$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 13497.04 | 85.99 | $\mathbf{0 . 6 \%}$ | Pass |
| Pad Flexure (kip*ft) | 2927.56 | 1780.57 | $\mathbf{5 7 . 9 \%}$ | Pass |
| Pad Shear - 1-way (kips) | 674.44 | 298.64 | $\mathbf{4 2 . 2 \%}$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.164 | 0.000 | $\mathbf{0 . 0 \%}$ | Pass |
| Flexural 2-way (Comp) (kip*f) | 3867.66 | 2262.60 | $\mathbf{5 5 . 7} \%$ | Pass |

*Rating per TIA-222-H Section 15.5

| Structural Rating*: | $62.2 \%$ |
| ---: | :--- |
| Soil Rating*: | $\mathbf{7 2 . 7 \%}$ |


| Pad Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Depth, D: | 8 | ft |  |
| Pad Width, $\mathbf{W}_{1}:$ | 22 | ft |  |
| Pad Thickness, T: | 3 | ft |  |
| Pad Rebar Size (Bottom dir. 2), $\mathbf{S p}_{\mathbf{2}}:$ | 10 |  |  |
| Pad Rebar Quantity (Bottom dir. 2), $\mathbf{m p}_{\mathbf{2}}:$ | 17 |  |  |
| Pad Clear Cover, $\mathbf{c c}_{\text {pad }}:$ | 3 | in |  |

Material Properties

| Rebar Grade, Fy: | 60 | ksi |
| ---: | :---: | :--- |
| Concrete Compressive Strength, F'c: | 3 | ksi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |

## Soil Properties

| Soil Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Total Soil Unit Weight, $\gamma:$ | 115 | pcf |  |
| Ultimate Gross Bearing, Qult: | 10.000 | ksf |  |
| Cohesion, $\mathbf{C u}:$ | 0.000 | ksf |  |
| Friction Angle, $\varphi:$ | 33 | degrees |  |
| SPT Blow Count, $\mathbf{N}_{\text {blows: }}:$ | 33 |  |  |
| Base Friction, $\mu:$ |  |  |  |
| Neglected Depth, $\mathbf{N}:$ | 3.00 | ft |  |
| Foundation Bearing on Rock? | No |  |  |
| Groundwater Depth, $\mathbf{g w}:$ | 15 | ft |  |

Address:
No Address at This Location

## ASCE 7 Hazards Report

| Standard: | ASCE/SEl 7-10 | Elevation: |
| :--- | :--- | :--- |
| Risk Category: | II | ft (NAVD 88) |
| Soil Class: | D - Stiff Soil | Latitude: 41.731472 |
|  |  | Longitude: -72.607778 |



## Seismic

## Site Soil Class:

D - Stiff Soil
Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.18 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.064 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.288 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.152 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.192 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.102 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.091 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.145 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category <br> B




## Data Accessed:

Date Source:

Wed Apr 212021
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2.
Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CIMIL ENGINEERS
Ice

## Results:

Ice Thickness:
Concurrent Temperature: 1.00 in .

Gust Speed:
Data Source:
Date Accessed:

5 F
50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed Apr 212021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

## Exhibit E

## Mount Analysis

Date: July 30, 2021

Darcy Tarr
Crown Castle
3530 Toringdon Way, Suite 300

Charlotte, NC 28277
(704) 405-6589

## Subject:

Carrier Designation:

## Crown Castle Designation:

Engineering Firm Designation:
Site Data:

Structure Information:

Trylon
1825 W. Walnut Hill Lane,
Suite 302
Irving, TX 75038
214-930-1730

Tower Height \& Type:
Mount Elevation:
Mount Type:
Trylon

Mount Replacement Analysis Report

| Dish Network Dish 5G |  |
| :--- | :--- |
| Carrier Site Number: | BOBDL00047A |
| Carrier Site Name: | CT-CCI-T-806376 |

Crown Castle BU Number: 806376
Crown Castle Site Name: HRT 100943239
Crown Castle JDE Job Number: 650042
Crown Castle Order Number: 556638 Rev. 1
Trylon Report Designation: 189056
1455 Forbes Street, East Hartford, Hartford County, CT, 06118
Latitude $41^{\circ} 43^{\prime} 53.30^{\prime \prime}$ Longitude $-72^{\circ} 36^{\prime} 28.00^{\prime \prime}$
130.0 ft Monopole
77.0 ft
8.0 ft Platform

Dear Darcy Tarr,
Trylon is pleased to submit this "Mount Replacement Analysis Report" to determine the structural integrity of Dish Network's antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

Platform
Sufficient*
*Sufficient upon completion of the changes listed in the 'Recommendations' section of this report.

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: Aura Baltoiu
Respectfully Submitted by:
Cliff Abernathy, P.E.

## TABLE OF CONTENTS

## 1) INTRODUCTION

## 2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided
3.1) Analysis Method
3.2) Assumptions
4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity
4.1) Recommendations
5) APPENDIX A

Wire Frame and Rendered Models
6) APPENDIX B

Software Input Calculations
7) APPENDIX C

Software Analysis Output
8) APPENDIX D

Additional Calculations
9) APPENDIX E

Supplemental Drawings

## 1) INTRODUCTION

This is a proposed 3 sector 8.0 ft Platform, designed by Commscope.

## 2) ANALYSIS CRITERIA

| Building Code: | 2015 IBC |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| Ultimate Wind Speed: | 125 mph |
| Exposure Category: | C |
| Topographic Factor at Base: | 1.00 |
| Topographic Factor at Mount: | 1.00 |
| Ice Thickness: | 2.0 in |
| Wind Speed with Ice: | 50 mph |
| Seismic S: | 0.180 |
| Seismic S: | 0.064 |
| Live Loading Wind Speed: | 30 mph |
| Man Live Load at Mid/End-Points: 250 lb |  |
| Man Live Load at Mount Pipes: | 500 lb |

Table 1 - Proposed Equipment Configuration

| Mount Centerline (ft) | Antenna Centerline (ft) | $\qquad$ | Antenna Manufacturer | Antenna Model | Mount / Modification Details |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 77.0 | 77.0 | 3 | JMA WIRELESS | MX08FRO665-21 | 8.0 ft Platform [Commscope, MC-PK8-C] |
|  |  | 3 | FUJITSU | TA08025-B604 |  |
|  |  | 3 | FUJITSU | TA08025-B605 |  |
|  |  | 1 | RAYCAP | RDIDC-9181-PF-48 |  |

3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Crown Application | Dish Network <br> Application | 556638, Rev.1 | CCI Sites |
| Mount Manufacturer Drawings | Commscope | MC-PK8-C | Trylon |

## 3.1) Analysis Method

RISA-3D (Version 17.0.4), a commercially available analysis software package, was used to create a threedimensional model of the antenna mounting system and calculate member stresses for various loading cases.

A tool internally developed, using Microsoft Excel, by Trylon was used to calculate wind loading on all appurtenances, dishes, and mount members for various load cases. Selected output from the analysis is included in Appendix B.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 Tower Mount Analysis (Revision B).

## 3.2) Assumptions

1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
2) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1 and the referenced drawings.
3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
4) The analysis will be required to be revised if the existing conditions in the field differ from those shown in the above-referenced documents or assumed in this analysis. No allowance was made for any damaged, missing, or rusted members.
5) Prior structural modifications to the tower mounting system are assumed to be installed as shown per available data.
6) Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate
HSS (Rectangular)
Pipe
Connection Bolts

ASTM A36 (GR 36)
ASTM A500 (GR B-46)
ASTM A53 (GR 35)
ASTM A325

This analysis may be affected if any assumptions are not valid or have been made in error. Trylon should be notified to determine the effect on the structural integrity of the antenna mounting system.

## 4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity (Platform, All Sectors)

| Notes | Component | Critical Member | Centerline (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1,2 | Mount Pipe(s) | MP9 | 77.0 | 36.1 | Pass |
|  | Horizontal(s) | H1 |  | 10.1 | Pass |
|  | Standoff(s) | SA3 |  | 57.4 | Pass |
|  | Bracing(s) | PB3 |  | 43.6 | Pass |
|  | Handrail(s) | M19 |  | 14.7 | Pass |
|  | Corner Angle(s) | CP2 |  | 5.6 | Pass |
|  | Plate(s) | CP6 |  | 24.1 | Pass |
|  | Mount Connection(s) | - |  | 23.0 | Pass |


| Structure Rating (max from all components) $=$ | $\mathbf{5 7 . 4 \%}$ |
| :--- | :---: | :---: |
| Notes: <br> 1) | See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the \% capacity <br> consumed. <br> Rating per TIA-222-H, Section 15.5 |
| 2) |  |

## 4.1) Recommendations

The mount has sufficient capacity to carry the proposed loading configuration. In order for the results of the analysis to be considered valid, the proposed mount listed below must be installed.

1. Commscope, MC-PK8-C.

No structural modifications are required at this time, provided that the above-listed changes are implemented.

## APPENDIX A

## WIRE FRAME AND RENDERED MODELS



Envelope Only Solution

| Trylon | 806376 | SK-1 |
| :---: | :---: | :---: |
| AB |  | July 28, 2021 at 8:21 AM |
| 189056 |  | 806376.r3d |



| Trylon | 806376 | SK - 2 |
| :---: | :---: | :---: |
| AB |  | July 28, 2021 at 8:21 AM |
| 189056 |  | 806376.r3d |

## APPENDIX B

## SOFTWARE INPUT CALCULATIONS

Address:
No Address at This Location

## ASCE 7 Hazards Report

| Standard: | ASCE/SEI 7-10 | Elevation: 41.23 ft (NAVD 88) |
| :--- | :--- | :--- |
| Risk Category: | II | Latitude: 41.731472 |
| Soil Class: | D - Stiff Soil | Longitude: -72.607778 |



## Seismic

Site Soil Class:
D - Stiff Soil
Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.18 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.064 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.288 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.152 |



## Seismic Design Category <br> B

| $\mathrm{S}_{\mathrm{DS}}:$ | 0.192 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.102 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.091 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.145 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |



## Data Accessed:

Date Source:

Wed Jul 282021
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2.
Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CIMIL ENGINEERS
Ice

## Results:

Ice Thickness:
Concurrent Temperature: 1.00 in .

Gust Speed:

## Data Source:

Date Accessed:

5 F
50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed Jul 282021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

TIA LOAD CALCULATOR 2.0

| PROJECT DATA |  |
| ---: | :---: |
| Job Code: | 189056 |
| Carrier Site ID: | BOBDL00047A |
| Carrier Site Name: | CT-CCI-T-806376 |


| WIND PARAMETERS | mph |  |
| ---: | :---: | :--- |
| Design Wind Speed: | 125 | -- |
| Wind Escalation Factor $\left(\mathrm{K}_{\mathrm{s}}\right):$ | 1.00 | -- |
| Velocity Coefficient $\left(\mathrm{K}_{\mathrm{z}}\right):$ | 1.20 | -- |
| Directionality Factor $\left(\mathrm{K}_{\mathrm{d}}\right):$ | 0.95 | -- |
| Gust Effect Factor $(\mathrm{Gh}):$ | 1.00 | -- |
| Shielding Factor $\left(\mathrm{K}_{\mathrm{a}}\right):$ | 0.90 | psf |
| Velocity Pressure $\left(\mathrm{a}_{\mathrm{z}}\right):$ | 45.45 |  |


| STRUCTURE DETAlLS |  |  |
| ---: | :---: | :--- |
| Mount Type: | Platform | -- |
| Mount Elevation: | 77.0 | ft. |
| Number of Sectors: | 3 | -- |
| Structure Type: | Monopole | -- |
| Structure Height: | 130.0 | ft. |


| ICE PARAMETERS |  |  |
| ---: | :---: | :--- |
| Design Ice Wind Speed: | 50 | mph |
| Design Ice Thickness $\left(\mathrm{t}_{\mathrm{i}}\right):$ | 2.00 | in |
| Importance Factor $\left(\mathrm{l}_{\mathrm{i}}\right):$ | 1.00 | -- |
| Ice Velocity Pressure $\left(\mathrm{q}_{\mathrm{z}}\right):$ | 45.45 | psf |
| Mount Ice Thickness $\left(\mathrm{t}_{\mathrm{i}}\right):$ | 2.18 | in |


| ANALYSIS CRITERIA |  |  |
| ---: | :---: | :--- |
| Structure Risk Category: | II | -- |
| Exposure Category: | C | -- |
| Site Class: | D - Stiff Soil | -- |
| Ground Elevation: | 41.23 | ft. |


| WIND STRUCTURE CALCULATIONS |  |  |
| ---: | :---: | :--- |
| Flat Member Pressure: | 81.81 | psf |
| Round Member Pressure: | 49.09 | psf |
| Ice Wind Pressure: | 7.14 | psf |


| TOPOGRAPHIC DATA |  |  |
| ---: | :---: | :--- |
| Topographic Category: | 1.00 | -- |
| Topographic Feature: | N/A | -- |
| Crest Point Elevation: | 0.00 | ft. |
| Base Point Elevation: | 0.00 | ft. |
| Crest to Mid-Height (L/2): | 0.00 | ft. |
| Distance from Crest $(\mathrm{x}):$ | 0.00 | ft |
| Base Topo Factor $\left(\mathrm{K}_{\mathrm{zt}}\right):$ | 1.00 | -- |
| Mount Topo Factor $\left(\mathrm{K}_{\mathrm{zt}}\right):$ | 1.00 | -- |


| SEISMIC PARAMETERS |  |  |
| ---: | :---: | :--- |
| Importance Factor $\left(\mathrm{I}_{\mathrm{e}}\right):$ | 1.00 | - |
| Short Period Accel $\left(\mathrm{S}_{\mathrm{s}}\right):$ | 0.180 | g |
| 1 Second Accel $\left(\mathrm{S}_{1}\right):$ | 0.064 | g |
| Short Period Des. $\left(\mathrm{S}_{\mathrm{DS}}\right):$ | 0.19 | g |
| 1 Second Des. $\left(\mathrm{S}_{\mathrm{D} 1}\right):$ | 0.10 | g |
| Short Period Coeff. $\left(\mathrm{F}_{\mathrm{a}}\right):$ | 1.60 | -- |
| 1 Second Coeff. $\left(\mathrm{F}_{\mathrm{v}}\right):$ | 2.40 | -- |
| Response Coefficient $(\mathrm{Cs}):$ | 0.10 | -- |
| Amplification Factor $\left(\mathrm{A}_{\mathrm{S}}\right):$ | 1.20 | -- |

## LOAD COMBINATIONS [LRFD]

| \# | Description |
| :---: | :---: |
| 1 | 1.4DL |
| 2 | 1.2DL + 1WL 0 AZI |
| 3 | 1.2DL + 1WL 30 AZI |
| 4 | 1.2DL + 1WL 45 AZI |
| 5 | 1.2DL + 1WL 60 AZI |
| 6 | 1.2DL + 1WL 90 AZI |
| 7 | 1.2DL + 1WL 120 AZI |
| 8 | 1.2DL + 1WL 135 AZI |
| 9 | 1.2DL + 1WL 150 AZI |
| 10 | 1.2DL + 1WL 180 AZI |
| 11 | 1.2DL + 1WL 210 AZI |
| 12 | 1.2DL + 1WL 225 AZI |
| 13 | 1.2DL + 1WL 240 AZI |
| 14 | 1.2DL + 1WL 270 AZI |
| 15 | 1.2DL + 1WL 300 AZI |
| 16 | 1.2DL + 1WL 315 AZI |
| 17 | 1.2DL + 1WL 330 AZI |
| 18 | 0.9DL + 1WL 0 AZI |
| 19 | 0.9DL + 1WL 30 AZI |
| 20 | 0.9DL + 1WL 45 AZI |
| 21 | 0.9DL + 1WL 60 AZI |
| 22 | 0.9DL + 1WL 90 AZI |
| 23 | $0.9 \mathrm{DL}+1 \mathrm{WL} 120 \mathrm{AZI}$ |
| 24 | 0.9DL + 1WL 135 AZI |
| 25 | $0.9 \mathrm{DL}+1 \mathrm{WL} 150 \mathrm{AZI}$ |
| 26 | $0.9 \mathrm{DL}+1 \mathrm{WL} 180 \mathrm{AZI}$ |
| 27 | 0.9DL + 1WL 210 AZI |
| 28 | 0.9DL + 1WL 225 AZI |
| 29 | $0.9 \mathrm{DL}+1 \mathrm{WL} 240 \mathrm{AZI}$ |
| 30 | $0.9 \mathrm{DL}+1 \mathrm{WL} 270 \mathrm{AZI}$ |
| 31 | $0.9 \mathrm{DL}+1 \mathrm{WL} 300 \mathrm{AZI}$ |
| 32 | $0.9 \mathrm{DL}+1 \mathrm{WL} 315 \mathrm{AZI}$ |
| 33 | 0.9DL + 1WL 330 AZI |
| 34 | 1.2DL + 1DLi + 1WLi 0 AZI |
| 35 | 1.2DL + 1DLi + 1WLi 30 AZI |
| 36 | 1.2DL + 1DLi + 1WLi 45 AZI |
| 37 | 1.2DL + 1DLi + 1WLi 60 AZI |
| 38 | 1.2DL + 1DLi + 1WLi 90 AZI |
| 39 | 1.2DL + 1DLi + 1WLi 120 AZI |
| 40 | 1.2DL + 1DLi + 1WLi 135 AZI |
| 41 | 1.2DL + 1DLi + 1WLi 150 AZI |


| \# | Description |
| :---: | :---: |
| 42 | 1.2DL + 1DLi + 1WLi 180 AZI |
| 43 | 1.2DL + 1DLi + 1WLi 210 AZI |
| 44 | 1.2DL + 1DLi + 1WLi 225 AZI |
| 45 | 1.2DL + 1DLi + 1WLi 240 AZI |
| 46 | 1.2DL + 1DLi + 1WLi 270 AZI |
| 47 | 1.2DL + 1DLi + 1WLi 300 AZI |
| 48 | 1.2DL + 1DLi + 1WLi 315 AZI |
| 49 | 1.2DL + 1DLi + 1WLi 330 AZI |
| 50 | (1.2+0.2Sds) +1.0 E 0 AZI |
| 51 | (1.2+0.2Sds) + 1.0E 30 AZI |
| 52 | (1.2+0.2Sds) + 1.0E 45 AZI |
| 53 | (1.2+0.2Sds) + 1.0E 60 AZI |
| 54 | (1.2+0.2Sds) + 1.0E 90 AZI |
| 55 | (1.2+0.2Sds) +1.0 E 120 AZI |
| 56 | (1.2+0.2Sds) + 1.0E 135 AZI |
| 57 | (1.2+0.2Sds) + 1.0E 150 AZI |
| 58 | (1.2+0.2Sds) + 1.0E 180 AZI |
| 59 | (1.2+0.2Sds) + 1.0E 210 AZI |
| 60 | (1.2+0.2Sds) + 1.0E 225 AZI |
| 61 | (1.2+0.2Sds) + 1.0E 240 AZI |
| 62 | (1.2+0.2Sds) + 1.0E 270 AZI |
| 63 | (1.2+0.2Sds) + 1.0E 300 AZI |
| 64 | (1.2+0.2Sds) +1.0 E 315 AZI |
| 65 | (1.2+0.2Sds) + 1.0E 330 AZI |
| 66 | (0.9-0.2Sds) +1.0 E 0 AZI |
| 67 | (0.9-0.2Sds) + 1.0E 30 AZI |
| 68 | (0.9-0.2Sds) +1.0 E 45 AZI |
| 69 | (0.9-0.2Sds) +1.0 E 60 AZI |
| 70 | (0.9-0.2Sds) +1.0 E 90 AZI |
| 71 | (0.9-0.2Sds) + 1.0E 120 AZI |
| 72 | (0.9-0.2Sds) + 1.0E 135 AZI |
| 73 | (0.9-0.2Sds) + 1.0E 150 AZI |
| 74 | (0.9-0.2Sds) + 1.0E 180 AZI |
| 75 | (0.9-0.2Sds) + 1.0E 210 AZI |
| 76 | (0.9-0.2Sds) + 1.0E 225 AZI |
| 77 | (0.9-0.2Sds) + 1.0E 240 AZI |
| 78 | (0.9-0.2Sds) + 1.0E 270 AZI |
| 79 | (0.9-0.2Sds) + 1.0E 300 AZI |
| 80 | (0.9-0.2Sds) + 1.0E 315 AZI |
| 81 | (0.9-0.2Sds) + 1.0E 330 AZI |
| 82-88 | 1.2D + 1.5 Lv1 |


| \# | Description | \# | Description |
| :---: | :---: | :---: | :---: |
| 89 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 0$ AZI - MP1 | 121 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 0$ AZI - MP3 |
| 90 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 30 \mathrm{AZI}-\mathrm{MP} 1$ | 122 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 30 \mathrm{AZI}-\mathrm{MP} 3$ |
| 91 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 45 \mathrm{AZI}-\mathrm{MP} 1$ | 123 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 45 \mathrm{AZI}-\mathrm{MP} 3$ |
| 92 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 60 \mathrm{AZI}-\mathrm{MP} 1$ | 124 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 60 \mathrm{AZI}-\mathrm{MP} 3$ |
| 93 | 1.2D + 1.5Lm + 1.0Wm 90 AZI - MP1 | 125 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 90$ AZI - MP3 |
| 94 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 120 \mathrm{AZI}-\mathrm{MP} 1$ | 126 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 120 \mathrm{AZI}-\mathrm{MP} 3$ |
| 95 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 135 \mathrm{AZI}-\mathrm{MP} 1$ | 127 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 135 \mathrm{AZI}-\mathrm{MP} 3$ |
| 96 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 150 \mathrm{AZI}-\mathrm{MP} 1$ | 128 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 150 \mathrm{AZI}-\mathrm{MP} 3$ |
| 97 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 180 \mathrm{AZI}-\mathrm{MP} 1$ | 129 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 180 \mathrm{AZI}-\mathrm{MP} 3$ |
| 98 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 210 \mathrm{AZI}-\mathrm{MP} 1$ | 130 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 210 \mathrm{AZI}-\mathrm{MP} 3$ |
| 99 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 225 \mathrm{AZI}-\mathrm{MP} 1$ | 131 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 225 \mathrm{AZI}-\mathrm{MP} 3$ |
| 100 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 240 \mathrm{AZI}-\mathrm{MP} 1$ | 132 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 240 \mathrm{AZI}-\mathrm{MP} 3$ |
| 101 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 270 \mathrm{AZI}-\mathrm{MP} 1$ | 133 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 270 \mathrm{AZI}-\mathrm{MP} 3$ |
| 102 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 300 \mathrm{AZI}-\mathrm{MP} 1$ | 134 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 300 \mathrm{AZI}-\mathrm{MP} 3$ |
| 103 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 315 \mathrm{AZI}-\mathrm{MP} 1$ | 135 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 315 \mathrm{AZI}-\mathrm{MP} 3$ |
| 104 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 330 \mathrm{AZI}-\mathrm{MP} 1$ | 136 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 330 \mathrm{AZI}-\mathrm{MP} 3$ |
| 105 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 0 \mathrm{AZI}-\mathrm{MP} 2$ | 137 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 0$ AZI - MP4 |
| 106 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 30 \mathrm{AZI}-\mathrm{MP} 2$ | 138 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 30 \mathrm{AZI}-\mathrm{MP} 4$ |
| 107 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 45 \mathrm{AZI}-\mathrm{MP} 2$ | 139 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 45 \mathrm{AZI}-\mathrm{MP} 4$ |
| 108 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 60 \mathrm{AZI}-\mathrm{MP} 2$ | 140 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 60 \mathrm{AZI}-\mathrm{MP} 4$ |
| 109 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 90 \mathrm{AZI}-\mathrm{MP} 2$ | 141 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 90 \mathrm{AZI}-\mathrm{MP} 4$ |
| 110 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 120 \mathrm{AZI}-\mathrm{MP} 2$ | 142 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 120 \mathrm{AZI}-\mathrm{MP} 4$ |
| 111 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 135 \mathrm{AZI}-\mathrm{MP} 2$ | 143 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 135 \mathrm{AZI}-\mathrm{MP} 4$ |
| 112 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 150 \mathrm{AZI}-\mathrm{MP} 2$ | 144 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 150 \mathrm{AZI}-\mathrm{MP} 4$ |
| 113 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 180 \mathrm{AZI}-\mathrm{MP} 2$ | 145 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 180 \mathrm{AZI}-\mathrm{MP} 4$ |
| 114 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 210 \mathrm{AZI}-\mathrm{MP} 2$ | 146 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 210 \mathrm{AZI}-\mathrm{MP} 4$ |
| 115 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 225 \mathrm{AZI}-\mathrm{MP} 2$ | 147 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 225 \mathrm{AZI}-\mathrm{MP} 4$ |
| 116 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 240 \mathrm{AZI}-\mathrm{MP} 2$ | 148 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 240 \mathrm{AZI}-\mathrm{MP} 4$ |
| 117 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 270 \mathrm{AZI}-\mathrm{MP} 2$ | 149 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 270 \mathrm{AZI}-\mathrm{MP} 4$ |
| 118 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 300 \mathrm{AZI}-\mathrm{MP} 2$ | 150 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 300 \mathrm{AZI}-\mathrm{MP} 4$ |
| 119 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 315 \mathrm{AZI}-\mathrm{MP} 2$ | 151 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 315 \mathrm{AZI}-\mathrm{MP} 4$ |
| 120 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 330 \mathrm{AZI}-\mathrm{MP} 2$ | 152 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} 330 \mathrm{AZI}-\mathrm{MP4}$ |

[^2]EQUIPMENT LOADING

| Appurtenance Name/Location | Qty. | Elevation [ft] | -- | $E P A_{N}(f t 2)$ | $E P A_{T}(f t 2)$ | Weight (los) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MX08FRO665-21 | 3 | 77 | No Ice | 8.01 | 3.21 | 82.50 |
| MP2/MP5/MP8, 0/100/220 | -- | -- | w/ Ice | 10.18 | 5.12 | 371.12 |
| TA08025-B604 | 3 | 77 | No Ice | 1.96 | 0.98 | 63.90 |
| MP2/MP5/MP8, 0/120/240 | -- | -- | w/ Ice | 2.51 | 1.41 | 93.72 |
| TA08025-B605 | 3 | 77 | No Ice | 1.96 | 1.13 | 75.00 |
| MP2/MP5/MP8, 0/120/240 | -- | -- | w/ Ice | 2.51 | 1.58 | 99.60 |
| RDIDC-9181-PF-48 | 1 | 77 | No Ice | 2.01 | 1.17 | 21.85 |
| MP2, 0 | -- | -- | w/ Ice | 2.57 | 1.63 | 98.23 |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No lce |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No lce |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No lce |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No lce |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |

## EQUIPMENT LOADING [CONT.]

| Appurtenance Name/Location | Qty | Elevation [ft] | -- | $E P A_{N}(f t 2)$ | $E P A_{T}(f t 2)$ | Weight (Ibs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |
|  |  |  | No Ice |  |  |  |
| -- | -- | -- | w/ Ice |  |  |  |

## EQUIPMENT WIND CALCULATIONS

| Appurtenance Name | Qty. | Elevation [ft] | $K_{z t}$ | $K_{z}$ | $K_{d}$ | $t_{d}$ | $\begin{gathered} \mathbf{q}_{z} \\ {[p s f]} \end{gathered}$ | $\begin{gathered} q_{z i} \\ {[p s f]} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MX08FRO665-21 | 3 | 77 | 1.00 | 1.20 | 0.95 | 2.18 | 45.45 | 7.27 |
| TA08025-B604 | 3 | 77 | 1.00 | 1.20 | 0.95 | 2.18 | 45.45 | 7.27 |
| TA08025-B605 | 3 | 77 | 1.00 | 1.20 | 0.95 | 2.18 | 45.45 | 7.27 |
| RDIDC-9181-PF-48 | 1 | 77 | 1.00 | 1.20 | 0.95 | 2.18 | 45.45 | 7.27 |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

EQUIPMENT LATERAL WIND FORCE CALCULATIONS

| Appurtenance Name | Qty. | -- | $\begin{gathered} 0^{\circ} \\ 180^{\circ} \end{gathered}$ | $\begin{gathered} 30^{\circ} \\ 210^{\circ} \end{gathered}$ | $\begin{gathered} 60^{\circ} \\ 240^{\circ} \end{gathered}$ | $\begin{gathered} 90^{\circ} \\ 270^{\circ} \end{gathered}$ | $\begin{aligned} & 120^{\circ} \\ & 300^{\circ} \end{aligned}$ | $\begin{aligned} & 150^{\circ} \\ & 330^{\circ} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MX08FRO665-21 | 3 | No Ice | 327.65 | 180.39 | 278.57 | 131.31 | 278.57 | 180.39 |
| MP2/MP5/MP8, 0/100/220 | -- | w/ Ice | 66.65 | 41.79 | 58.36 | 33.50 | 58.36 | 41.79 |
| TA08025-B604 | 3 | No Ice | 80.32 | 50.18 | 70.27 | 40.13 | 70.27 | 50.18 |
| MP2/MP5/MP8, 0/120/240 | -- | w/ Ice | 16.43 | 11.03 | 14.63 | 9.23 | 14.63 | 11.03 |
| TA08025-B605 | 3 | No Ice | 80.32 | 54.73 | 71.79 | 46.20 | 71.79 | 54.73 |
| MP2/MP5/MP8, 0/120/240 | -- | w/ Ice | 16.43 | 11.84 | 14.90 | 10.31 | 14.90 | 11.84 |
| RDIDC-9181-PF-48 | 1 | No Ice | 82.30 | 56.41 | 73.67 | 47.79 | 73.67 | 56.41 |
| MP2, 0 | -- | w/ Ice | 16.80 | 12.21 | 15.27 | 10.68 | 15.27 | 12.21 |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No lce |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |

## EQUIPMENT LATERAL WIND FORCE CALCULATIONS [CONT.]

| Appurtenance Name | Qty. | -- | $\begin{gathered} 0^{\circ} \\ 180^{\circ} \end{gathered}$ | $\begin{gathered} 30^{\circ} \\ 210^{\circ} \end{gathered}$ | $\begin{gathered} 60^{\circ} \\ 240^{\circ} \end{gathered}$ | $\begin{gathered} 90^{\circ} \\ 270^{\circ} \end{gathered}$ | $\begin{aligned} & 120^{\circ} \\ & 300^{\circ} \end{aligned}$ | $\begin{aligned} & 150^{\circ} \\ & 330^{\circ} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No lce |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No lce |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No lce |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No lce |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |
|  |  | No Ice |  |  |  |  |  |  |
| -- | -- | w/ Ice |  |  |  |  |  |  |

## EQUIPMENT SEISMIC FORCE CALCULATIONS

| Appurtenance Name | Qty. | Elevation [ft] | Weight [lbs] | $\begin{gathered} F_{p} \\ {[\mathrm{lbs}]} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| MX08FRO665-21 | 3 | 77 | 82.5 | 9.50 |
| TA08025-B604 | 3 | 77 | 63.9 | 7.36 |
| TA08025-B605 | 3 | 77 | 75 | 8.64 |
| RDIDC-9181-PF-48 | 1 | 77 | 21.85 | 2.52 |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT

## (Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :---: | :---: |
| Max Internal S ections for Member Calcs | 97 |
| Include S hear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include W arping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | . 12 |
| P-Delta Analysis Tolerance | 0.50\% |
| Include P -Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | Yes |
| Max Iterations for Wall Stiffness | 3 |
| G ravity Acceleration (in/sec ${ }^{\text {2 } 2) ~}$ | 386.4 |
| Wall Mesh Size (in) | 24 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Z |
| G lobal Member Orientation Plane | XY |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |
| Hot Rolled Steel Code | AISC 15th(360-16): LRFD |
| Adjust Stiffness? | Yes(Iterative) |
| R ISAC onnection Code | AISC 15th(360-16): LRFD |
| C old F ormed S teel C ode | AIS I S 100-12: LRFD |
| Wood Code | AWC NDS-15: ASD |
| Wood Temperature | < 100F |
| C oncrete Code | AC I 318-14 |
| Masonry Code | AC I 530-13: S trength |
| Aluminum Code | AA ADM 1-10: LRFD - Building |
| Stainless Steel Code | AISC 14th(360-10): LRFD |
| Adjust Stiffness? | Yes(Iterative) |
| Number of Shear Regions | 4 |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | . 65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections S lab? | Yes |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| C oncrete Rebar Set | REBAR_SET_ASTMA615 |
| Min \% S teel for Column | 1 |
| Max \% S teel for Column | 8 |

(Global) Model Settings, Continued

| Seismic Code | ASCE 7-10 |
| :--- | :--- |
| Seismic Base Elevation (in) | Not Entered |
| Add Base W eight? | Yes |
| Ct X | .02 |
| Ct Z | .02 |
| T X (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
| Ct Exp. X | .75 |
| Ct Exp. Z | .75 |
| SD1 | 1 |
| SDS | 1 |
| S1 | 1 |
| TL (sec) | 5 |
| Risk Cat | I or II |
| Drift Cat | Other |
| Om Z | 1 |
| Om X | 1 |
| Cd Z | 1 |
| Cd X | 1 |
| Rho Z | 1 |
| Rho X | 1 |
|  |  |

## Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (/1E5 F) | Density[k/ft^3] | Y ield[psi] | Ry | Fu[psi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50000 | 1.1 | 65000 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | . 49 | 36000 | 1.5 | 58000 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | . 49 | 50000 | 1.1 | 65000 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | . 3 | . 65 | . 527 | 42000 | 1.4 | 58000 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46000 | 1.4 | 58000 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | . 3 | . 65 | . 49 | 35000 | 1.6 | 60000 | 1.2 |
| 7 | A1085 | 29000 | 11154 | . 3 | . 65 | . 49 | 50000 | 1.4 | 65000 | 1.3 |

## Cold Formed Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (/1E5 F) | Density[k/ft^3] | Y ield[psi] | Fu[psi] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A653 S S Gr33 | 29500 | 11346 | . 3 | . 65 | 49 | 33000 | 45000 |
| 2 | A653 S S Gr50/1 | 29500 | 11346 | . 3 | . 65 | . 49 | 50000 | 65000 |

Hot Rolled Steel Section Sets

| Label |  | Shape Type |  | Design List | Material | Design ... A [in2] |  | lyy [in4] Izz [in4] |  | [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Plates | 6.5 "x0.37" Plate | Beam | RECT | A53 Gr.B | Typical | 2.405 | . 027 | 8.468 | . 106 |
| 2 | G rating Bracing | L $2 \times 2 \times 3$ | Beam | Single Angle | A36 Gr. 36 | Typical | . 722 | . 271 | . 271 | . 009 |
| 3 | Standoffs | PIPE 3.5 | Beam | Pipe | A53 Gr.B | Typical | 2.5 | 4.52 | 4.52 | 9.04 |
| 4 | Standoff Bracing | C3X5 | Beam | Channel | A36 Gr. 36 | Typical | 1.47 | . 241 | 1.85 | . 043 |
| 5 | Handrails | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 6 | Handrail Corners | $6.6 \times 4.46 \times 0.25$ | Beam | Single Angle | A36 Gr. 36 | Typical | 2.702 | 4.759 | 12.473 | . 055 |
| 7 | Horizontals | PIPE 3.5 | Beam | Pipe | A53 Gr.B | Typical | 2.5 | 4.52 | 4.52 | 9.04 |

Hot Rolled Steel Section Sets (Continued)

| Label |  | Shape | Type | Des ign List | Material | Design ... A [in2] |  | lyy [in4] Izz [in4] J [in4] |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | Mount Pipes | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |

Cold Formed Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design R... A [in2] |  | lyy [in4] | Izz [in4] | $J$ [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | CF1A | 8CU1.25X057 | Beam | None | A653 S S Gr33 | Typical | . 581 | . 057 | 4.41 | . 00063 |

## Joint Boundary Conditions

| Joint Label |  | X [k/in] | $Y$ [k/in] | Z [k/in] | X Rot.[k-ft/rad] | Y Rot.[k-ft/rad] | Z Rot.[k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N25 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 2 | N1 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 3 | N13 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |

## Basic Load Cases

| BLC Description |  | Category | X Gravity | Y Gravity Z Gravity |  | Joint | $\begin{gathered} \text { Point } \\ \hline 13 \\ \hline \end{gathered}$ | Distribu...Area(M... Surface... |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Self Weight |  |  |  | -1 |  |  |  | 3 |  |
| 2 | Structure Wind X | WLX |  |  |  |  |  | 33 |  |  |
| 3 | Structure Wind Y | WLY |  |  |  |  |  | 33 |  |  |
| 4 | Wind Load 0 AZI | WLX |  |  |  |  | 13 |  |  |  |
| 5 | Wind Load 30 AZI | None |  |  |  |  | 26 |  |  |  |
| 6 | Wind Load 45 AZI | None |  |  |  |  | 26 |  |  |  |
| 7 | Wind Load 60 AZI | None |  |  |  |  | 26 |  |  |  |
| 8 | Wind Load 90 AZI | WLY |  |  |  |  | 13 |  |  |  |
| 9 | Wind Load 120 AZI | None |  |  |  |  | 26 |  |  |  |
| 10 | Wind Load 135 AZI | None |  |  |  |  | 26 |  |  |  |
| 11 | Wind Load 150 AZI | None |  |  |  |  | 26 |  |  |  |
| 12 | Ice Weight | OL1 |  |  |  |  | 13 | 33 | 3 |  |
| 13 | Structure Ice Wind $X$ | OL2 |  |  |  |  |  | 33 |  |  |
| 14 | Structure Ice Wind $Y$ | OL3 |  |  |  |  |  | 33 |  |  |
| 15 | Ice Wind Load 0 AZI | OL2 |  |  |  |  | 13 |  |  |  |
| 16 | Ice Wind Load 30 AZI | None |  |  |  |  | 26 |  |  |  |
| 17 | Ice Wind Load 45 AZI | None |  |  |  |  | 26 |  |  |  |
| 18 | Ice Wind Load 60 AZI | None |  |  |  |  | 26 |  |  |  |
| 19 | Ice Wind Load 90 AZI | OL3 |  |  |  |  | 13 |  |  |  |
| 20 | Ice Wind Load 120 AZI | None |  |  |  |  | 26 |  |  |  |
| 21 | Ice Wind Load 135 AZI | None |  |  |  |  | 26 |  |  |  |
| 22 | Ice Wind Load 150 AZI | None |  |  |  |  | 26 |  |  |  |
| 23 | Seismic Load X | ELX | -. 115 |  |  |  | 13 |  |  |  |
| 24 | Seismic Load Y | ELY |  | -. 115 |  |  | 13 |  |  |  |
| 25 | Live Load 1 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 26 | Live Load 2 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 27 | Live Load 3 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 28 | Live Load 4 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 29 | Live Load 5 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 30 | Live Load 6 (Lv) | LL |  |  |  |  | 1 |  |  |  |
| 31 | Maintenance Load 1 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 32 | Maintenance Load 2 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 33 | Maintenance Load 3 (Lm) | None |  |  |  |  | 1 |  |  |  |

## Basic Load Cases (Continued)

| BLC Description |  | Category | X Gravity | Y Gravity Z G ravity |  | Joint | Point | Distribu...Area(M... Surface... |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | Maintenance Load 4 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 35 | Maintenance Load 5 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 36 | Maintenance Load 6 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 37 | Maintenance Load 7 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 38 | Maintenance Load 8 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 39 | Maintenance Load 9 (Lm) | None |  |  |  |  | 1 |  |  |  |
| 40 | Maintenance Load 7 (Lm) | None |  |  |  |  |  |  |  |  |
| 41 | Maintenance Load 8 (Lm) | None |  |  |  |  |  |  |  |  |
| 42 | Maintenance Load 9 (Lm) | None |  |  |  |  |  |  |  |  |
| 43 | BLC 1 Transient Area Loads | None |  |  |  |  |  | 9 |  |  |
| 44 | BLC 12 Trans ient Area Loads | None |  |  |  |  |  | 9 |  |  |

## Load Combinations

|  | Des cription | Solve | PD. | SR...B... | Factor | BLC | Factor | B... | ...Fa... ${ }^{\text {B }}$ | B ...F | Fa... | BLC | Fa... | B... | Fa... ${ }^{\text {B }}$ | ...Fa.. | ..B... | ..Fa... ${ }^{\text {B }}$ | ...Fa. | B. | Fa.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4DL | Yes | Y | DL | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 1.2DL + 1WL 0 AZI | Yes | Y | DL | 1.2 | 2 | 1 | 3 |  | 4 | 1 |  |  |  |  |  |  |  |  |  |  |
| 3 | 1.2DL + 1WL 30 AZI | Yes | Y | DL | 1.2 | 2 | . 866 | 3 | . 5 | 5 | 1 |  |  |  |  |  |  |  |  |  |  |
| 4 | 1.2DL + 1WL 45 AZI | Yes | Y | DL | 1.2 | 2 | . 707 | 3 | . 7076 | 6 | 1 |  |  |  |  |  |  |  |  |  |  |
| 5 | 1.2DL + 1WL 60 AZI | Yes | Y | DL | 1.2 | 2 | . 5 | 3 | 8667 | 7 | 1 |  |  |  |  |  |  |  |  |  |  |
| 6 | 1.2DL + 1WL 90 AZI | Yes | Y | DL | 1.2 | 2 |  | 3 | 1 | 8 | 1 |  |  |  |  |  |  |  |  |  |  |
| 7 | 1.2DL + 1WL 120 AZI | Yes | Y | DL | 1.2 | 2 | -. 5 | 3 | 8669 | 9 | 1 |  |  |  |  |  |  |  |  |  |  |
| 8 | 1.2DL + 1WL 135 AZI | Yes | Y | DL | 1.2 | 2 | -. 707 | 3 | 7071 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |
| 9 | 1.2DL + 1WL 150 AZI | Yes | Y | DL | 1.2 | 2 | -. 866 | 3 | . 51 | 11 | 1 |  |  |  |  |  |  |  |  |  |  |
| 10 | 1.2DL + 1WL 180 AZI | Yes | Y | DL | 1.2 | 2 | -1 | 3 |  | 4 | -1 |  |  |  |  |  |  |  |  |  |  |
| 11 | 1.2DL + 1WL 210 AZI | Yes | Y | DL | 1.2 | 2 | -. 866 | 3 | -. 5 | 5 | -1 |  |  |  |  |  |  |  |  |  |  |
| 12 | 1.2DL + 1WL 225 AZI | Yes | Y | DL | 1.2 | 2 | -. 707 | 3 | -.7... 6 | 6 | -1 |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.2DL + 1WL 240 AZI | Yes | Y | DL | 1.2 | 2 | -. 5 | 3 | -.8... 7 | 7 | -1 |  |  |  |  |  |  |  |  |  |  |
| 14 | 1.2DL + 1WL 270 AZI | Yes | Y | DL | 1.2 | 2 |  | 3 | -1 | 8 | -1 |  |  |  |  |  |  |  |  |  |  |
| 15 | 1.2DL + 1WL 300 AZI | Yes | Y | DL | 1.2 | 2 | . 5 | 3 | -.8. | 9 | -1 |  |  |  |  |  |  |  |  |  |  |
| 16 | 1.2DL + 1WL 315 AZI | Yes | Y | DL | 1.2 | 2 | . 707 | 3 | -.7... 1 | $10-1$ | -1 |  |  |  |  |  |  |  |  |  |  |
| 17 | 1.2DL + 1WL 330 AZI | Yes | Y | DL | 1.2 | 2 | . 866 | 3 | -. 51 | 11 | -1 |  |  |  |  |  |  |  |  |  |  |
| 18 | 0.9DL + 1WL 0 AZI | Yes | Y | DL | . 9 | 2 | 1 | 3 |  | 4 | 1 |  |  |  |  |  |  |  |  |  |  |
| 19 | 0.9DL + 1WL 30 AZI | Yes | Y | DL | . 9 | 2 | . 866 | 3 | . 5 | 5 | 1 |  |  |  |  |  |  |  |  |  |  |
| 20 | 0.9DL + 1WL 45 AZI | Yes | Y | DL | . 9 | 2 | . 707 | 3 | . 7076 | 6 | 1 |  |  |  |  |  |  |  |  |  |  |
| 21 | 0.9DL + 1WL 60 AZI | Yes | Y | DL | . 9 | 2 | . 5 | 3 | . 8667 | 7 | 1 |  |  |  |  |  |  |  |  |  |  |
| 22 | 0.9DL + 1WL 90 AZI | Yes | Y | DL | . 9 | 2 |  | 3 | 1 | 8 | 1 |  |  |  |  |  |  |  |  |  |  |
| 23 | 0.9DL + 1WL 120 AZI | Yes | Y | DL | . 9 | 2 | -. 5 | 3 | 8669 | 9 | 1 |  |  |  |  |  |  |  |  |  |  |
| 24 | 0.9DL + 1WL 135 AZI | Yes | Y | DL | . 9 | 2 | -. 707 | 3 | . 7071 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |
| 25 | 0.9DL + 1WL 150 AZI | Yes | Y | DL | . 9 | 2 | -. 866 | 3 | . 51 | 11 | 1 |  |  |  |  |  |  |  |  |  |  |
| 26 | 0.9DL + 1WL 180 AZI | Yes | Y | DL | . 9 | 2 | -1 | 3 |  | 4 | -1 |  |  |  |  |  |  |  |  |  |  |
| 27 | 0.9DL + 1WL 210 AZI | Yes | Y | DL | . 9 | 2 | -. 866 | 3 | -. 5 | 5 | -1 |  |  |  |  |  |  |  |  |  |  |
| 28 | 0.9DL + 1WL 225 AZI | Yes | Y | DL | . 9 | 2 | -. 707 | 3 | -.7... 6 | 6 | -1 |  |  |  |  |  |  |  |  |  |  |
| 29 | 0.9DL + 1WL 240 AZI | Yes | Y | DL | . 9 | 2 | -. 5 | 3 | -.8. | 7 | -1 |  |  |  |  |  |  |  |  |  |  |
| 30 | 0.9DL + 1WL 270 AZI | Yes | Y | DL | . 9 | 2 |  | 3 | -1 | 8 | -1 |  |  |  |  |  |  |  |  |  |  |
| 31 | 0.9DL + 1WL 300 AZI | Yes | Y | DL | . 9 | 2 | . 5 | 3 | -.8... 9 | 9 | -1 |  |  |  |  |  |  |  |  |  |  |
| 32 | 0.9DL + 1WL 315 AZI | Yes | Y | DL | . 9 | 2 | . 707 | 3 | -.7... 1 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |
| 33 | 0.9DL + 1WL 330 AZI | Yes | Y | DL | . 9 | 2 | . 866 | 3 | -. 51 | 11 - | -1 |  |  |  |  |  |  |  |  |  |  |
| 34 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 | 13 | 11 | 14 |  | 15 | 1 |  |  |  |  |  |  |  |  |
| 35 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 | 13. | . 8661 | 14 | . 5 | 16 | 1 |  |  |  |  |  |  |  |  |
| 36 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 | 13. | . 7071 | 14.7 | 707 | 17 | 1 |  |  |  |  |  |  |  |  |

Job Number : 189056
8:22 AM

Model Name : 806376

## Load Combinations (Continued)

| Des cription |  | Solve | PD.. | R...B. ${ }_{\text {DL }}$ | .. Factor BLC |  | $\begin{gathered} \text { Factor } \\ \hline 1 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { B...Fa...B } \\ & \hline 12: 5] 1 \end{aligned}$ |  | $\frac{B . . . F a . . . E ~}{14.866}$ | BLC | 1 | B...Fa. | . ${ }^{\text {B...F }}$ | ${ }^{\text {a...B. }}$ | ...Fa...В...Fa... ...Fa... |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 37 | 1.2DL + 1DLi + 1WL... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 |  | 1 | 13 |  |  | 141 | 19 | 1 |  |  |  |  |  |  |
| 39 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-.514 | 14.866 | 20 | 1 |  |  |  |  |  |  |
| 40 | 1.2DL + 1 DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-7. 7.1 | 14.707 | 21 | 1 |  |  |  |  |  |  |
| 41 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-8.8. 14 | 14.5 | 22 | 1 |  |  |  |  |  |  |
| 42 | $1.2 \mathrm{LL}+1 \mathrm{DLi}+1 \mathrm{WL}$... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-114 | 14 | 15 | -1 |  |  |  |  |  |  |
| 43 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-8...14 | 14-. 5 | 16 | -1 |  |  |  |  |  |  |
| 44 | 1.2DL + 1 DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3-7. 71 | 14-7... | 17 | -1 |  |  |  |  |  |  |
| 45 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | --. 51 | 14-8... | 18 | -1 |  |  |  |  |  |  |
| 46 | 1.2DL + 1 DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 |  | 13 |  | 14-1 | 19 | -1 |  |  |  |  |  |  |
| 47 | 1.2DL + 1DLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3.51 | 14-8... | 20 | -1 |  |  |  |  |  |  |
| 48 | $1.2 \mathrm{DL}+1 \mathrm{DLi}+1 \mathrm{WL}$. | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3.7071 | 14-7. | 21 | -1 |  |  |  |  |  |  |
| 49 | 1.2DL + 1 LLi + 1WL... | Yes | Y | DL | 1.2 | OL1 | 1 |  | 3.8661 | 14-. 5 | 22 | -1 |  |  |  |  |  |  |
| 50 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | 1 | E. |  |  |  |  |  |  |  |  |  |  |
| 51 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | . 866 | E. | . 5 |  |  |  |  |  |  |  |  |  |
| 52 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | . 707 | E. | ...707 |  |  |  |  |  |  |  |  |  |
| 53 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | . 5 |  | ... 866 |  |  |  |  |  |  |  |  |  |
| 54 | (1.2+0.2Sds) +1.0 E . | Yes | Y | DL | 1.238 | ELX |  | E. | 1 |  |  |  |  |  |  |  |  |  |
| 55 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 5 |  | . 866 |  |  |  |  |  |  |  |  |  |
| 56 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 707 | E. | ... 707 |  |  |  |  |  |  |  |  |  |
| 57 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 866 | E. |  |  |  |  |  |  |  |  |  |  |
| 58 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -1 | E. |  |  |  |  |  |  |  |  |  |  |
| 59 | (1.2+0.2sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 866 | E. | ..-. 5 |  |  |  |  |  |  |  |  |  |
| 60 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 707 |  | ...-7... |  |  |  |  |  |  |  |  |  |
| 61 | (1.2+0.2Sds) +1.0 E | Yes | Y | DL | 1.238 | ELX | -. 5 | E. | ...8. |  |  |  |  |  |  |  |  |  |
| 62 | (1.2+0.2Sds) +1.0 E . | Yes | Y | DL | 1.238 | ELX |  |  | ..-1 |  |  |  |  |  |  |  |  |  |
| 63 | (1.2+0.2Sds) +1.0 E . | Yes | Y | DL | 1.238 | ELX | . 5 |  | ..-8... |  |  |  |  |  |  |  |  |  |
| 64 | ( $1.2+0.2 \mathrm{dss}$ ) +1.0 E . | Yes | Y | DL | 1.238 | ELX | . 707 |  | ...-7... |  |  |  |  |  |  |  |  |  |
| 65 | (1.2+0.2Sds) +1.0 E . | Yes | Y | DL | 1.238 | ELX | . 866 | E.. |  |  |  |  |  |  |  |  |  |  |
| 66 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | 1 | E.. |  |  |  |  |  |  |  |  |  |  |
| 67 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 866 | E.. | . 5 |  |  |  |  |  |  |  |  |  |
| 68 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 707 | E. | . 707 |  |  |  |  |  |  |  |  |  |
| 69 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 5 | E. | . 866 |  |  |  |  |  |  |  |  |  |
| 70 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX |  |  | 1 |  |  |  |  |  |  |  |  |  |
| 71 | (0.9-0.2Sds) + 1.0 E | Yes | Y | DL | . 862 | ELX | -. 5 | E. | . 866 |  |  |  |  |  |  |  |  |  |
| 72 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | -. 707 | E. | ...707 |  |  |  |  |  |  |  |  |  |
| 73 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | -. 866 | E.. | . 5 |  |  |  |  |  |  |  |  |  |
| 74 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | -1 | E. |  |  |  |  |  |  |  |  |  |  |
| 75 | (0.9-0.2Sds) + 1.0 E | Yes | Y | DL | . 862 | ELX | -. 866 | E.. | ... .5 |  |  |  |  |  |  |  |  |  |
| 76 | (0.9-0.2sds) +1.0 E | Yes | Y | DL | . 862 | ELX | -. 707 | E.. | ... 7 |  |  |  |  |  |  |  |  |  |
| 77 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | -. 5 |  | .-.8... |  |  |  |  |  |  |  |  |  |
| 78 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX |  | E.. | -1 |  |  |  |  |  |  |  |  |  |
| 79 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 5 |  | ...8... |  |  |  |  |  |  |  |  |  |
| 80 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 707 | E. | ... 7. |  |  |  |  |  |  |  |  |  |
| 81 | (0.9-0.2Sds) +1.0 E | Yes | Y | DL | . 862 | ELX | . 866 | E.. | ... -5 |  |  |  |  |  |  |  |  |  |
| 82 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 1$ | Yes | Y | DL | 1.2 | 25 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 83 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 2$ | Yes | Y | DL | 1.2 | 26 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 84 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 3$ | Yes | Y | DL | 1.2 | 27 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 85 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 4$ | Yes | Y | DL | 1.2 | 28 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 86 | $1.2 \mathrm{D}+1.5$ Lv5 | Yes | Y | DL | 1.2 | 29 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 87 | $1.2 \mathrm{D}+1.5 \mathrm{Lv} 6$ | Yes | Y | DL | 1.2 | 30 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 88 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 4 | . 0582 | 2.058 | 3 |  |  |  |  |  |  |  |

Job Number : 189056
8:22 AM

Model Name : 806376

## Load Combinations (Continued)

|  | Des cription | Solve |  | ...B. | Fac |  | Factor |  | Fa...B. | Fa... | BLC | Fa...B | Fa. | ..B...F | Fa...B. | Fa | ...Fa.. | . .B...Fa |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 89 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 . .$. | Yes | Y | DL | 1.2 | 31 | 1.5 | 5. | . 0582 | . 05 | 3 | 029 |  |  |  |  |  |  |
| 90 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 6 | . 0582 | . 041 | 3 | . 041 |  |  |  |  |  |  |
| 91 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |
| 92 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 31 | 1.5 | 8 | . 0582 |  | 3 | 058 |  |  |  |  |  |  |
| 93 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 9.0 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |
| 94 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 31 | 1.5 | 10.0 | . 0582 | -0. | 3 | . 041 |  |  |  |  |  |  |
| 95 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 |  | . 0582 | -. 05 | 3 | . 029 |  |  |  |  |  |  |
| 96 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 31 | 1.5 | 4.0 | . 0582 | -0. | 3 |  |  |  |  |  |  |  |
| 97 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 5 | . 0582 | -. 05 | 3 | $-0$. |  |  |  |  |  |  |
| 98 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 31 | 1.5 | 6 | . 0582 | -0. | 3 | -0. |  |  |  |  |  |  |
| 99 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 7 | . 0582 | -0. | 3 | -05 |  |  |  |  |  |  |
| 100 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 31 | 1.5 | 8 | . 0582 |  | 3 | -0... |  |  |  |  |  |  |
| 101 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 | 9.0 | . 0582 | . 029 | 3 | -05 |  |  |  |  |  |  |
| 102 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 31 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -0... |  |  |  |  |  |  |
| 103 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 31 | 1.5 |  | . 0582 | 05 | - | -0... |  |  |  |  |  |  |
| 104 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 4.0 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |
| 105 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 5. | . 0582 | . 05 | 3 | 029 |  |  |  |  |  |  |
| 106 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 6 | . 0582 | . 041 | 3 | . 041 |  |  |  |  |  |  |
| 107 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |
| 108 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 32 | 1.5 | 8 | . 0582 |  | 3 | 058 |  |  |  |  |  |  |
| 109 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 9.0 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |
| 110 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 32 | 1.5 | 10. | . 0582 | -0. | 3 | . 041 |  |  |  |  |  |  |
| 111 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 11. | . 0582 | -. 05 | 3 | 029 |  |  |  |  |  |  |
| 112 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 32 | 1.5 | 4. | . 0582 | -0. | 3 |  |  |  |  |  |  |  |
| 113 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 5. | . 0582 | -. 05 | 3 | -0.. |  |  |  |  |  |  |
| 114 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 6.0 | . 0582 | -0. |  | -0... |  |  |  |  |  |  |
| 115 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 7 | . 0582 | -0. | 3 | -.05 |  |  |  |  |  |  |
| 116 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 8 | . 0582 |  | 3 | -0... |  |  |  |  |  |  |
| 117 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 9.0 | . 0582 | . 029 | 3 | -05 |  |  |  |  |  |  |
| 118 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -0... |  |  |  |  |  |  |
| 119 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 32 | 1.5 | 11. | . 0582 | . 05 | 3 | -0... |  |  |  |  |  |  |
| 120 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 33 | 1.5 | 4.0 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |
| 121 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 5. | . 0582 | . 05 | 3 | 029 |  |  |  |  |  |  |
| 122 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 6 | . 0582 | . 041 | , | 041 |  |  |  |  |  |  |
| 123 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 33 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |
| 124 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 8. | . 0582 |  | 3 | 058 |  |  |  |  |  |  |
| 125 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 33 | 1.5 | 9. | . 0582 | $-0$. | 3 | . 05 |  |  |  |  |  |  |
| 126 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 10.0 | . 0582 | -0. | 3 | . 041 |  |  |  |  |  |  |
| 127 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 33 | 1.5 | 11. | . 0582 | -05 | 3 | 029 |  |  |  |  |  |  |
| 128 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 4. | . 0582 | -0. | 3 |  |  |  |  |  |  |  |
| 129 | 1.2D + 1.5Lm + 1.0. | Yes | Y | DL | 1.2 | 33 | 1.5 | 5. | . 0582 | -. 05 | 3 | -0. |  |  |  |  |  |  |
| 130 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 6.0 | . 0582 | -0. |  | -0... |  |  |  |  |  |  |
| 131 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 33 | 1.5 | 7.0 | . 0582 | -0. | 3 | -05 |  |  |  |  |  |  |
| 132 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 8. | . 0582 |  | 3 | -0... |  |  |  |  |  |  |
| 133 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 9.0 | . 0582 | . 029 | 3 | -05 |  |  |  |  |  |  |
| 134 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 33 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -0... |  |  |  |  |  |  |
| 135 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 33 | 1.5 | 11. | . 0582 | . 05 | 3 | -0.. |  |  |  |  |  |  |
| 136 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 4. | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |
| 137 | 1.2D + 1.5Lm + 1.0. | Yes | Y | DL | 1.2 | 34 | 1.5 | 5. | . 0582 | . 05 | 3 | 029 |  |  |  |  |  |  |
| 138 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 6. | . 0582 | . 041 | - | . 041 |  |  |  |  |  |  |
| 139 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 7.0 | . 0582 | 029 | 3 | . 05 |  |  |  |  |  |  |
| 140 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 8. | . 0582 |  | 3 | 058 |  |  |  |  |  |  |

Job Number : 189056
8:22 AM

Model Name : 806376

## Load Combinations (Continued)

|  | Des cription | Solve |  |  | Factor |  | Factor | B... | Fa...B... | Fa. | BLC | Fa... ${ }^{\text {B }}$ | .Fa | .B...F | a... | Fa... | B...Fa | Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 141 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$... | Yes | Y | DL | 1.2 | 34 | 1.5 | 9.0 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |
| 142 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$. | Yes | Y | DL | 1.2 | 34 | 1.5 | 10.0 | . 0582 | -0. | , | 041 |  |  |  |  |  |  |
| 143 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 11.0 | . 0582 | -05 | 3 | 029 |  |  |  |  |  |  |
| 144 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 4 | . 0582 | -0. | 3 |  |  |  |  |  |  |  |
| 145 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 5 | . 0582 | -. 05 | 3 | -.0... |  |  |  |  |  |  |
| 146 | 1.2D $+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 6 | . 0582 | -0. | 3 | -0.. |  |  |  |  |  |  |
| 147 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 34 | 1.5 | 7 | . 0582 | -0.. | 3 | -. 05 |  |  |  |  |  |  |
| 148 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 8 | . 0582 |  | - | -.0. |  |  |  |  |  |  |
| 149 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 34 | 1.5 | 9 | . 0582 | . 029 | 3 | -. 05 |  |  |  |  |  |  |
| 150 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -.0. |  |  |  |  |  |  |
| 151 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 34 | 1.5 | 11.0 | . 0582 | . 05 | 3 | -0.. |  |  |  |  |  |  |
| 152 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 4 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |
| 153 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 5 | . 0582 | . 05 | , | 029 |  |  |  |  |  |  |
| 154 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 6 | . 0582 | . 041 | 3 | 041 |  |  |  |  |  |  |
| 155 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 35 | 1.5 | 7 | . 0582 | . 029 | 3 | 05 |  |  |  |  |  |  |
| 156 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 8 | . 0582 |  | 3 | 058 |  |  |  |  |  |  |
| 157 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 9 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |
| 158 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 10.0 | . 0582 | -0. | 3 | 041 |  |  |  |  |  |  |
| 159 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 35 | 1.5 |  | . 0582 | -05 | 3 | 029 |  |  |  |  |  |  |
| 160 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 4 | . 0582 | -0. | 3 |  |  |  |  |  |  |  |
| 161 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 5 | . 0582 | -. 05 | - | -.0... |  |  |  |  |  |  |
| 162 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 6 | . 0582 | -0. | 3 | -0. |  |  |  |  |  |  |
| 163 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 35 | 1.5 | 7 | . 0582 | -0. | 3 | -. 05 |  |  |  |  |  |  |
| 164 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 8 | . 0582 |  | 3 | -0.. |  |  |  |  |  |  |
| 165 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 9 | . 0582 | . 029 | - | -. 05 |  |  |  |  |  |  |
| 166 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 35 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -0.1. |  |  |  |  |  |  |
| 167 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$. | Yes | Y | DL | 1.2 | 35 | 1.5 | 11.0 | . 0582. | . 05 | 3 | -0. |  |  |  |  |  |  |
| 168 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 36 | 1.5 | 4 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |
| 169 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 36 | 1.5 | 5 | . 0582. | 05 | 3 | 029 |  |  |  |  |  |  |
| 170 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 6 | . 0582 | . 041 | 3 | 041 |  |  |  |  |  |  |
| 171 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |
| 172 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$. | Yes | Y | DL | 1.2 | 36 | 1.5 | 8 | . 0582 |  | 3 | . 058 |  |  |  |  |  |  |
| 173 | 1.2D + 1.5Lm + 1.0. | Yes | Y | DL | 1.2 | 36 | 1.5 | 9 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |
| 174 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 10.0 | . 0582 | -0. | , | 041 |  |  |  |  |  |  |
| 175 | 1.2D + 1.5Lm + 1.0.. | Yes | Y | DL | 1.2 | 36 | 1.5 | 11.0 | . 0582 | -05 | 3 | 029 |  |  |  |  |  |  |
| 176 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 4.0 | . 0582 | -0... | 3 |  |  |  |  |  |  |  |
| 177 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 5 | . 0582 | -. 05 |  | -0. |  |  |  |  |  |  |
| 178 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 6 | . 0582 | -0.. | 3 | -0... |  |  |  |  |  |  |
| 179 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 7 | . 0582 | -0. | 3 | -05 |  |  |  |  |  |  |
| 180 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 8 | . 0582 |  | 3 | -0... |  |  |  |  |  |  |
| 181 | 1.2D + $1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 9 | . 0582 | . 029 | 3 | -05 |  |  |  |  |  |  |
| 182 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 10.0 | . 0582 | . 041 | 3 | -0. |  |  |  |  |  |  |
| 183 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 36 | 1.5 | 11.0 | . 0582. | . 05 |  | -0. |  |  |  |  |  |  |
| 184 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 4 | . 0582 | . 058 | - |  |  |  |  |  |  |  |
| 185 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$. | Yes | Y | DL | 1.2 | 37 | 1.5 | 5 | . 0582 | . 05 | , | . 029 |  |  |  |  |  |  |
| 186 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 6 | . 0582 | . 041 | 3 | 041 |  |  |  |  |  |  |
| 187 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0$. | Yes | Y | DL | 1.2 | 37 | 1.5 | 7 | . 0582 | . 029 |  | . 05 |  |  |  |  |  |  |
| 188 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 .$. | Yes | Y | DL | 1.2 | 37 | 1.5 | 8 | . 0582 |  | 3 | 058 |  |  |  |  |  |  |
| 189 | 1.2D + $1.5 \mathrm{Lm}+1.0$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 9 | . 0582 | -0. |  | . 05 |  |  |  |  |  |  |
| 190 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 10.0 | . 0582 | -0. | 3 | 041 |  |  |  |  |  |  |
| 191 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 11.0 | . 0582 | -05 | 3 | 029 |  |  |  |  |  |  |
| 192 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 4 | . 0582 | -0.. | 3 |  |  |  |  |  |  |  |

## Load Combinations (Continued)

|  | Des cription | Solve |  | . B .. |  |  | Fac |  | a...B. |  |  |  | . Fa |  | a. | ....Fa. | B. | a. | .Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 193 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 37 | 1.5 | 5 | . 0582 | -05 | 3 | -.0... |  |  |  |  |  |  |  |
| 194 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 6 | . 0582 | -0. | 3 | -.0... |  |  |  |  |  |  |  |
| 195 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 37 | 1.5 | 7 | . 0582 | -0. | 3 | -. 05 |  |  |  |  |  |  |  |
| 196 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 8 | . 0582 |  | 3 | -.0... |  |  |  |  |  |  |  |
| 197 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 37 | 1.5 | 9 | . 0582 | . 029 | 3 | -. 05 |  |  |  |  |  |  |  |
| 198 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 10 | . 0582 | . 041 | 3 | -.0... |  |  |  |  |  |  |  |
| 199 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 37 | 1.5 | 11 | . 0582 | . 05 | 3 | -.0... |  |  |  |  |  |  |  |
| 200 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 4 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |  |
| 201 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 5 | . 0582 | . 05 | 3 | . 029 |  |  |  |  |  |  |  |
| 202 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 6 | . 0582 | . 041 | 3 | . 041 |  |  |  |  |  |  |  |
| 203 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |  |
| 204 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 8 | . 0582 |  | 3 | . 058 |  |  |  |  |  |  |  |
| 205 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 9 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |  |
| 206 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 10 | . 0582 | -0. | 3 | . 041 |  |  |  |  |  |  |  |
| 207 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 11 | . 0582 | -. 05 | 3 | . 029 |  |  |  |  |  |  |  |
| 208 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 4 | . 0582 | -.0. | 3 |  |  |  |  |  |  |  |  |
| 209 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 5 | . 0582 | -. 05 | 3 | -.0... |  |  |  |  |  |  |  |
| 210 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 6 | . 0582 | -0. | 3 | -.0... |  |  |  |  |  |  |  |
| 211 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 7 | . 0582 | -0. | 3 | -. 05 |  |  |  |  |  |  |  |
| 212 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 8 | . 0582 |  | 3 | -.0... |  |  |  |  |  |  |  |
| 213 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 9 | . 0582 | . 029 | 3 | -. 05 |  |  |  |  |  |  |  |
| 214 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 38 | 1.5 | 10 | . 0582 | . 041 | 3 | -.0... |  |  |  |  |  |  |  |
| 215 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 38 | 1.5 | 11 | . 0582 | . 05 | 3 | -.0... |  |  |  |  |  |  |  |
| 216 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 4 | . 0582 | . 058 | 3 |  |  |  |  |  |  |  |  |
| 217 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 5 | . 0582 | . 05 | 3 | . 029 |  |  |  |  |  |  |  |
| 218 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 6 | . 0582 | . 041 | 3 | . 041 |  |  |  |  |  |  |  |
| 219 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 7 | . 0582 | . 029 | 3 | . 05 |  |  |  |  |  |  |  |
| 220 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 8 | . 0582 |  | 3 | . 058 |  |  |  |  |  |  |  |
| 221 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 9 | . 0582 | -0. | 3 | . 05 |  |  |  |  |  |  |  |
| 222 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 10 | . 0582 | -0. | 3 | . 041 |  |  |  |  |  |  |  |
| 223 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 39 | 1.5 | 11. | . 0582 | -. 05 | 3 | . 029 |  |  |  |  |  |  |  |
| 224 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 4 | . 0582 | -0. | 3 |  |  |  |  |  |  |  |  |
| 225 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 5 | . 0582 | -. 05 | 3 | -.0... |  |  |  |  |  |  |  |
| 226 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 6 | . 0582 | -0. | 3 | -.0... |  |  |  |  |  |  |  |
| 227 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 7 | . 0582 | -0. | 3 | -. 05 |  |  |  |  |  |  |  |
| 228 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 39 | 1.5 | 8 | . 0582 |  | 3 | -.0... |  |  |  |  |  |  |  |
| 229 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 9 | . 0582 | . 029 | 3 | -. 05 |  |  |  |  |  |  |  |
| 230 | 1.2D + 1.5Lm + 1.0... | Yes | Y | DL | 1.2 | 39 | 1.5 | 10 | . 0582 | . 041 | 3 | -.0... |  |  |  |  |  |  |  |
| 231 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \ldots$ | Yes | Y | DL | 1.2 | 39 | 1.5 | 11. | . 0582 | . 05 | 3 | -.0... |  |  |  |  |  |  |  |

Envelope Joint Reactions

| Joint |  |  | X [b] | LC | Y [b] | LC | Z [lb] | LC | MX [lb-ft] LC |  | MY [lb-ft] | LC | MZ [lb-ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N25 | max | 1580.52 | 3 | 961.27 | 20 | 2328.63 | 39 | 507.26 | 31 | 546.48 | 33 | 1827.37 | 3 |
| 2 |  | min | -1576.74 | 27 | -967.5 | 12 | -104.71 | 31 | -4106.44 | 39 | -2527.12 | 41 | -1826.91 | 27 |
| 3 | N1 | max | 1665.75 | 17 | 991.51 | 8 | 2324.86 | 45 | 4102.48 | 46 | 511.67 | 19 | 1920.9 | 25 |
| 4 |  | min | -1661.94 | 25 | -985.24 | 32 | -82.5 | 21 | -471.17 | 22 | -2521.15 | 43 | -1921.35 | 17 |
| 5 | N13 | max | 352.14 | 18 | 1610.85 | 22 | 2235.66 | 34 | 732.02 | 14 | 4593.49 | 34 | 1551.54 | 14 |
| 6 |  | min | -360.03 | 10 | -1610.87 | 30 | -135.37 | 26 | -731.55 | 6 | -657.99 | 26 | -1551.56 | 6 |
| 7 | Totals: | max | 3188.37 | 18 | 2933.42 | 6 | 6594.78 | 36 |  |  |  |  |  |  |
| 8 |  | min | -3188.37 | 10 | -2933.42 | 14 | 1367.67 | 76 |  |  |  |  |  |  |

Company

## Envelope A ISC 15th(360-16): LRFD Steel Code Checks

| Member Shape |  |  | $\begin{gathered} \text { Code Check } \\ \hline .603 \\ \hline \end{gathered}$ | Loc[in] | $\begin{array}{r} \text { LC } \\ \hline 39 \end{array}$ | She...Lo. |  |  | phi*P ... phi*P |  | phi*M...phi*M. |  | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SA3 | PIPE_3.5 |  |  |  | . 190 | 40 | 116 | 64491.. | 78750 | 7953.. | 7953.. | ...H1-1b |
| 2 | SA2 | PIPE 3.5 | . 602 | 40 | 45 | . 199 | 40 | 9 | 64491.. | 78750 | 7953. | 7953 | $\ldots \mathrm{H}$-1-1b |
| 3 | SA1 | PIPE 3.5 | . 578 | 40 | 34 | . 176 | 40 | 146 | 64491.. | 78750 | 7953... | 7953.. | .. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 4 | PB3 | C $3 \times 5$ | . 458 | 34.86 | 39 | . 169 | 63. | y 353 | 32858.. | 47628 | 981.26 | 4104 | .. H 1 -1 b |
| 5 | PB2 | C 3X5 | . 456 | 34.86 | 45 | . 169 | 6.54 | y 493 | 32858. | 47628 | 981.26 | 4104 | ... $\mathrm{H} 1-1 \mathrm{~b}$ |
| 6 | PB1 | C3X5 | . 433 | 34.86 | 49 | . 158 | 6.54 | y 38 | 32858.. | 47628 | 981.26 | 4104 | $\ldots \mathrm{H}$.-1b |
| 7 | MP9 | PIPE 2.0 | . 380 | 57 | 10 | . 045 | 57 | 15 | 20866.. | 32130 | 1871... | 1871... | $\ldots \mathrm{H}$-1-1b |
| 8 | MP1 | PIPE 2.0 | . 365 | 57 | 16 | . 046 | 57 | 10 | 20866.. | 32130 | 1871... | 1871... | .H1-1b |
| 9 | MP3 | PIPE 2.0 | . 359 | 57 | 5 | . 053 | 57 | 10 | 20866.. | 32130 | 1871... | 1871... | $1 \mathrm{H1-1b}$ |
| 10 | MP6 | PIPE_2.0 | . 354 | 57 | 15 | . 048 | 57 | 5 | 20866.. | 32130 | 1871... | 1871.. | $\ldots \mathrm{H} 1-1 \mathrm{~b}$ |
| 11 | MP4 | PIPE_2.0 | . 351 | 57 | 10 | . 043 | 57 | 6 | 20866.. | 32130 | 1871.... | 1871... | $1 \mathrm{H} 1-1 \mathrm{~b}$ |
| 12 | MP2 | PIPE 2.0 | . 333 | 57 | 6 | . 049 | 57 | 5 | 20866.. | 32130 | 1871... | 1871.. | $1 \mathrm{H} 1-1 \mathrm{~b}$ |
| 13 | MP8 | PIPE_2.0 | . 331 | 57 | 10 | . 044 | 57 | 10 | 20866.. | 32130 | 1871... | 1871... | ...H1-1b |
| 14 | MP7 | PIPE 2.0 | . 328 | 57 | 3 | . 048 | 57 | 16 | 20866.. | 32130 | 1871.... | 1871... | $1 \mathrm{H1-1b}$ |
| 15 | MP5 | PIPE 2.0 | . 323 | 57 | 9 | . 042 | 57 | 10 | 20866.. | 32130 | 1871. | 1871. | $1 \mathrm{H} 1-1 \mathrm{~b}$ |
| 16 | CP6 | 6.5 "x0.37" Plate | . 254 | 21 | 8 | . 109 | 21 | y 372 | 27548. | 75757. | . 583.96 | 6395. | $\ldots$... ${ }^{\text {1-1b }}$ |
| 17 | CP4 | 6.5 "x0.37" Plate | . 249 | 21 | 2 | . 101 | 21 | y 472 | 27548...7 | 75757.. | . 583.96 | 6186... | ... $\mathrm{H} 1-1 \mathrm{~b}$ |
| 18 | CP5 | 6.5"x0.37" Plate | . 244 | 21 | 13 | . 109 | 21 | y 47 | 27548. | 75757. | . 583.96 | 6219. | $\ldots \mathrm{H} 1-1 \mathrm{~b}$ |
| 19 | M19 | PIPE 2.0 | . 147 | 72 | 10 | . 155 | 72 | 2 | 14916.. | 32130 | 1871. | 1871. | ...H1-1b |
| 20 | M20 | PIPE_2.0 | . 145 | 24 | 16 | . 154 | 72 | 8 | 14916.. | 32130 | 1871.. | 1871. | $\ldots \mathrm{H}$.-1b |
| 21 | M21 | PIPE 2.0 | . 140 | 72 | 5 | . 143 | 72 | 13 | 14916.. | 32130 | 1871.. | 1871... | . $\mathrm{H} 1-1 \mathrm{~b}$ |
| 22 | IFH21 | L2x2x3 | . 123 | 0 | 30 | . 035 | 0 | z 43 | 18084. | 23392. | . 557.72 | 1182. | $1 \mathrm{H} 2-1$ |
| 23 | IFH32 | L2x2x3 | . 119 | 0 | 14 | . 035 | 0 | y 41 | 18084. | 23392. | . 557.72 | 1182. | $1 \mathrm{H} 2-1$ |
| 24 | IFH12 | L2x2x3 | . 114 | 0 | 25 | . 034 | 0 | y 351 | 18084..2 | 23392. | . 557.72 | 1179.. | $1 \mathrm{H} 2-1$ |
| 25 | IFH11 | L2x2x 3 | . 113 | 0 | 3 | . 035 | 0 | z 49 | 18084..2 | 23392. | . 557.72 | 1179.. | $1 \mathrm{H} 2-1$ |
| 26 | H1 | PIPE 3.5 | . 107 | 48 | 105 | . 102 | 72 | 10 | 60666... | 78750 | 7953... | 7953.. | $1 \mathrm{H} 1-1 \mathrm{~b}$ |
| 27 | H3 | PIPE 3.5 | . 104 | 48 | 207 | . 098 | 24 | 15 | 60666... | 78750 | 7953. | 7953 | $1 \mathrm{H} 1-1 \mathrm{~b}$ |
| 28 | IFH 31 | L2x2x ${ }^{\text {2 }}$ | . 104 | 0 | 26 | . 034 | 0 | z 38 | $18084 . .2$ | 23392. | . 557.72 | 1182. | $1 \mathrm{H} 2-1$ |
| 29 | H2 | PIPE 3.5 | . 102 | 48 | 159 | . 095 | 72 | 5 | 60666... | 78750 | 7953.. | 7953... | 1 H1-1b |
| 30 | IFH22 | L2x $2 \times 3$ | . 101 | 0 | 2 | . 034 | 0 | y 46 | 18084..2 | 23392. | . 557.72 | 1182. | $1 \mathrm{H} 2-1$ |
| 31 | CP2 | $6.6 \times 4.46 \times 0.25$ | . 059 | 0 | 26 | . 045 | 42 | y 175 | $51170 .$. | 87561 | 2464. | 7125.. | $1 \mathrm{H} 2-1$ |
| 32 | CP3 | $6.6 \times 4.46 \times 0.25$ | . 058 | 0 | 22 | . 042 | 0 | y 3 | $51170 .$. | 87561 | 2464... | 7125... | $1 \mathrm{H} 2-1$ |
| 33 | CP1 | $6.6 \times 4.46 \times 0.25$ | . 054 | 18.81 | 18 | . 041 | 0 | y 145 | $51170 .$. | 87561 | 2464.... | 7125... | $1 \mathrm{H} 2-1$ |

## Envelope A IS IS 100-12: LRFD Cold Formed S teel Code Checks

Member Shape Code Check Loc[in]LC Shea...Loc[i..DirLC phi*Pn[..phi*Tn[...phi*Mn...phi*Mn... Cb Cmyy Cmzz Eqn No Data to Print ...

## APPENDIX D

## ADDITIONAL CALCUATIONS

BOLT TOOL 1.5.2

| Project Data |  |
| ---: | :---: |
| Job Code: | 189056 |
| Carrier Site ID: | BOBDL00047A |
| Carrier Site Name: | CT-CCI-T-806376 |


| Connection Description |
| :---: |
| Standoff to Monopole |


| Code |  |
| ---: | :---: |
| Design Standard: | TIA-222-H |
| Slip Check: | No |
| Pretension Standard: | AISC |


| Bolt Properties |  |  |
| ---: | :---: | :--- |
| Connection Type: | Bolt |  |
| Diameter: | 0.625 | in |
| Grade: | A325 | -- |
| Yield Strength (Fy): | 92 | ksi |
| Ultimate Strength (Fu): | 120 | ksi |
| Number of Bolts: | 4 | -- |
| Threads Included: | No | -- |
| Double Shear: | No | -- |
| Connection Pipe Size: | - | in |


| Bolt Check* |  |  |
| ---: | :---: | :--- |
| Tensile Capacity $\left(\phi \mathrm{T}_{\mathrm{n}}\right):$ | 20340.1 | lbs |
| Shear Capacity $\left(\phi \mathrm{V}_{\mathrm{n}}\right):$ | 17257.3 | lbs |
| Tension Force $\left(\mathrm{T}_{\mathrm{u}}\right):$ | 4914.3 | lbs |
| Shear Force $\left(\mathrm{V}_{\mathrm{u}}\right):$ | 698.8 | lbs |
| Tension Usage: | $23.0 \%$ | -- |
| Shear Usage: | $3.9 \%$ | -- |
| Interaction: | $23.0 \%$ | Pass |
| Controlling Member: | SA2 | -- |
| Controlling LC: | 42 | -- |

*Rating per TIA-222-H Section 15.5


## APPENDIX E

SUPPLEMENTAL DRAWINGS




## Exhibit F

## Power Density/RF Emissions Report

# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

Dish Wireless Existing Facility

Site ID: BOBDL00047A
806376
1455 Forbes Street
East Hartford, Connecticut 06II8
September 28, 202 I
EBI Project Number: 6221005703

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general <br> population <br> allowable limit: | $\mathbf{5 9 . 2 4 \%}$ |

environmental | engineering | due diligence
September 28, 202 I
Dish Wireless

Emissions Analysis for Site: BOBDL00047A - 806376

EBI Consulting was directed to analyze the proposed Dish Wireless facility located at 1455 Forbes Street in East Hartford, Connecticut for the purpose of determining whether the emissions from the Proposed Dish Wireless Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-0 land ANSI/IEEE Std C95.I. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR I.I307(b)(I) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, respectively. The general population exposure limit for the $1900 \mathrm{MHz}(\mathrm{PCS}), 2100 \mathrm{MHz}(\mathrm{AWS})$ and II GHz frequency bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure.
environmental | engineering | due diligence

Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed Dish Wireless Wireless antenna facility located at 1455 Forbes Street in East Hartford, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since Dish Wireless is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6 -foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 4 n 7 I channels ( 600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
2) 4 n 70 channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
3) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-0I recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
4) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
environmental | engineering | due diligence
5) The antennas used in this modeling are the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900$ MHz channel(s) in Sector A, the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900 \mathrm{MHz}$ channel(s) in Sector B, the JMA MX08FRO665-2I for the $600 \mathrm{MHz} / 1900 \mathrm{MHz}$ channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 20 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
6) The antenna mounting height centerline of the proposed antennas is 77 feet above ground level (AGL).
7) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
8) All calculations were done with respect to uncontrolled / general population threshold limits.
environmental | engineering | due diligence

## Dish Wireless Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | I | Antenna \#: | I | Antenna \#: | I |
| Make / Model: | $\begin{gathered} \text { JMA MX08FRO665- } \\ 21 \end{gathered}$ | Make / Model: | $\begin{gathered} \text { JMA MX08FRO665- } \\ 21 \end{gathered}$ | Make / Model: | $\begin{gathered} \text { JMA MX08FRO665- } \\ 21 \end{gathered}$ |
| Frequency Bands: | $\begin{gathered} 600 \mathrm{MHz} / \mathrm{I} 900 \\ \mathrm{MHz} \end{gathered}$ | Frequency Bands: | $\begin{gathered} 600 \mathrm{MHz} / \mathrm{I} 900 \\ \mathrm{MHz} \end{gathered}$ | Frequency Bands: | $\begin{gathered} 600 \mathrm{MHz} / \mathrm{I} 900 \\ \mathrm{MHz} \end{gathered}$ |
| Gain: | $\begin{gathered} 17.45 \mathrm{dBd} / 22.65 \\ \mathrm{dBd} \end{gathered}$ | Gain: | $\begin{gathered} 17.45 \mathrm{dBd} / 22.65 \\ \mathrm{dBd} \end{gathered}$ | Gain: | $\begin{gathered} 17.45 \mathrm{dBd} / 22.65 \\ \mathrm{dBd} \end{gathered}$ |
| Height (AGL): | 77 feet | Height (AGL): | 77 feet | Height (AGL): | 77 feet |
| Channel Count: | 8 | Channel Count: | 8 | Channel Count: | 8 |
| Total TX Power (W): | 280 Watts | Total TX Power (W): | 280 Watts | Total TX Power (W): | 280 Watts |
| ERP (W): | 3,065.5 I | ERP (W): | 3,065.5 I | ERP (W): | 3,065.5 I |
| Antenna AI MPE \%: | 3.14\% | Antenna BI MPE \%: | 3.14\% | Antenna CI MPE \%: | 3.14\% |

environmental | engineering | due diligence

| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| Dish Wireless (Max at Sector A): | $3.14 \%$ |
| Sprint | $6.41 \%$ |
| Clearwire | $0.22 \%$ |
| AT\&T | $9.72 \%$ |
| Verizon | $9.8 \%$ |
| T-Mobile | $29.95 \%$ |
| Site Total MPE \% : | $59.24 \%$ |


| Dish Wireless MPE \% Per Sector |  |  |
| :---: | :---: | :---: |
| Dish Wireless Sector A Total: | $3.14 \%$ |  |
| Dish Wireless Sector B Total: | $3.14 \%$ |  |
| Dish Wireless Sector C Total: | $3.14 \%$ |  |
| Site Total MPE \% : |  |  |
| $59.24 \%$ |  |  |

## Dish Wireless Maximum MPE Power Values (Sector A)

| Dish Wireless Frequency Band / Technology (Sector A) | \# Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dish Wireless $600 \mathrm{MHz} \mathrm{n7I}$ | 4 | 223.68 | 77.0 | 6.38 | $600 \mathrm{MHz} \mathrm{n7I}$ | 400 | 1.60\% |
| Dish Wireless $1900 \mathrm{MHz} \mathrm{n70}$ | 4 | 542.70 | 77.0 | 15.48 | $1900 \mathrm{MHz} \mathrm{n70}$ | 1000 | 1.55\% |
|  |  |  |  |  |  | Total: | 3.14\% |

- NOTE: Totals may vary by approximately $0.01 \%$ due to summation of remainders in calculations.
environmental | engineering | due diligence


## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the Dish Wireless facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| Dish Wireless Sector | Power Density Value (\%) |
| :---: | :---: |
| Sector A: | $3.14 \%$ |
| Sector B: | $3.14 \%$ |
| Sector C: | $3.14 \%$ |
| Dish Wireless <br> Maximum MPE \% <br> (Sector A): | $3.14 \%$ |
| Site Total: |  |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{5 9 . 2 4 \%}$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.

## Exhibit G

## Letter of Authorization

4545 E River Rd, Suite 320
West Henrietta, NY 14586

## Crown Castle Letter of Authorization

## CT - CONNECTICUT SITING COUNCIL

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## Re: Tower Share Application

Crown Castle telecommunications site at:
1455 FORBES STREET, EAST HARTFORD, CT 06118
CROWN ATLANTIC COMPANY LLC ("Crown Castle") hereby authorizes DISH Wireless, LLC, including their Agent, to act as our Agent in the processing of all zoning applications, building permits and approvals through the CT - CONNECTICUT SITING COUNCIL for the existing wireless communications site described below:

Crown Site ID/Name: 806376/HRT 100943239
Customer Site ID: BOBDLooo47A/CT-CCI-T-806376
Site Address: 1455 FORBES STREET, EAST HARTFORD, CT 06118

Crown Castle


## Exhibit H

## Recipient Mailings



## Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage $®$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {TM }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

## Click-N-Ship ${ }^{\circledR}$ Label Record

| USPS TRACKING \# : <br> 9405503699300026154793 |  |  |  |
| :---: | :---: | :---: | :---: |
| Trans. \#: 545423559 |  | Priority Mail® Postage: | \$8.70 |
| Print Date: 10/07/2021 <br> Ship Date: $10 / 07 / 2021$ |  |  |  |
|  |  |  |  |
| ExpectedDelivery Date:10/12/2021 |  |  |  |
| From: | DEBORAH CHASE Ref\#: DS-806376NORTHEAST SITE SOLUTIONS |  |  |
|  |  |  |  |
|  | 420 MAIN ST |  |  |
|  | STE 1 |  |  |
|  | STURBRIDGE MA 01566-1359 |  |  |
| To: | RICH ZAJAC |  |  |
|  | CROWN CASTLE |  |  |
|  | 4545 E RIVER RD |  |  |
|  | STE 320 |  |  |
|  | W HENRIETTA NY 14586-9024 |  |  |
| * Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date. |  |  |  |



## Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage $®$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {TM }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

## Click-N-Ship ${ }^{\circledR}$ Label Record

| USPS TRACKING \# : <br> 9405503699300026154809 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 545423559 | Priority Mail® Postage: | \$9.00 |
| Print Date: |  | 10/07/2021 |  |  |
| Ship Date: <br> Expected |  | 10/07/2021 |  |  |
| Delivery Date: |  | 10/12/2021 |  |  |
| From: | DEBORAH CHASE Reff: DS-806376NORTHEAST SITE SOLUTIONS |  |  |  |
|  |  |  |  |  |
|  | 420 MAIN ST |  |  |  |
|  | STE 1 |  |  |  |
|  | STURBRIDGE MA 01566-1359 |  |  |  |
| то: | MARCIA A LECLERC |  |  |  |
|  | EATS HARTFORD TOWN HALL |  |  |  |
|  | 740 MAIN ST |  |  |  |
|  | EAST HARTFORD CT 06108-3140 |  |  |  |



## Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage $®$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {TM }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

## Click-N-Ship ${ }^{\circledR}$ Label Record

| USPS TRACKING \# : <br> 9405503699300026154823 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 545423559 | Priority Mail® Postage: | \$9.00 |
| Print Date: |  | 10/07/2021 |  |  |
| Ship Date: <br> Expected |  | 10/07/2021 |  |  |
| Delivery Date: |  | 10/12/2021 |  |  |
| From: | DEBORAH CHASE Reff: DS-806376NORTHEAST SITE SOLUTIONS |  |  |  |
|  |  |  |  |  |
|  | 420 MAIN ST |  |  |  |
|  | STE 1 |  |  |  |
|  | STURBRIDGE MA 01566-1359 |  |  |  |
|  | EILEEN BUCKHEIT |  |  |  |
|  | DEVELOPMENT DIRECTOR |  |  |  |
|  | 740 MAIN ST |  |  |  |
|  | EAST HARTFORD CT 06108-3140 |  |  |  |



## Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage $®$, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office ${ }^{\text {TM }}$, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

## Click-N-Ship® Label Record

| USPS TRACKING \# : <br> 9405503699300026154847 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Trans. \#: |  | 545423559 | Priority Mail® Postage: | \$22.65 |
| Srint Date: |  | 10/07/2021 |  |  |
|  |  | 10/07/2021 |  |  |
| Expected Delivery Date: |  | 10/12/2021 |  |  |
| From: | DEBORAH CHASE Reff: DS-806376NORTHEAST SITE SOLUTIONS |  |  |  |
|  |  |  |  |  |
|  | 420 MAIN ST |  |  |  |
|  | STE 1 |  |  |  |
|  | STURBRIDGE MA 01566-1359 |  |  |  |
|  | JACK-REBECCA HANDEL |  |  |  |
|  | 1455 FORBES ST |  |  |  |
|  | EAST HARTFORD CT 06118-3300 |  |  |  |

## 806376



UNIONVILLE
24 MILL ST
UNIONVILLE, CT 06085-9998 (800)275-8777


Prepaid Mail
1
$\$ 0.00$
West Henrietta, NY 14586
Weight: 01 b 2.10 oz
Acceptance Date:
Fri 10/08/2021
Tracking \#:
9405503699300026154793
$\begin{array}{ll}\text { Prepaid Mail } \\ \text { East Hartford, CT } \\ & 106108\end{array} \$ 0.00$
Weight: 1 ib 2.40 oz
Acceptance Date:
Fri 10/08/2021
Tracking \#:
9405503699300026154809
Prepaid Mall
East Hartford, CT $^{1} 06118$
Weight: 1 lb 2.50 oz
Acceptance Date:
Fri 10/08/2021
Tracking \#:
9405503699300026154847

| Prepaid Mail 1 <br> East Hartford, CT 06108 <br> Weight: 1 lb 2.40 oz <br> Acceptance Date: <br> Fri 10/08/2021 <br> Tracking \#: <br> 9405503699300026154823 | \$0.00 |
| :---: | :---: |
| Grand Total: | \$0.00 |


[^0]:    DISH Wiriless LLC. TEMPAATE VERSION $38-07 / 23 / 2021$

[^1]:    tnxTower Report - version 8.1.1.0

[^2]:    *This page shows an example of maintenance loads for (4) pipes, the number of mount pipe LCs may vary per site

