STATE OF CONNECTICUT<br>CONNECTICUT SITING COUNCIL<br>Ten Franklin Square, New Britain, CT 06051<br>Phone: (860) 827-2935 Fax: (860) 827-2950<br>E-Mail: siting.council@ct.gov<br>www.ct.gov/csc

## VIA ELECTRONIC MAIL

February 10, 2020

Kenneth C. Baldwin, Esq.
Robinson \& Cole LLP
280 Trumbull Street
Hartford, CT 06103
RE: EM-VER-036-200116 - Cello Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 220 Winthrop Road, Deep River, Connecticut.

## Dear Attorney Baldwin:

The Connecticut Siting Council (Council) is in receipt of your correspondence of January 22, 2020 and February 5, 2020 submitted in response to the Council's January 21, 2020 notification of an incomplete request for exempt modification with regard to the above-referenced matter.

The submission renders the request for exempt modification complete and the Council will process the request in accordance with the Federal Communications Commission 60-day timeframe.

Thank you for your attention and cooperation.
Sincerely,


Melanie A. Bachman
Executive Director

MAB/IN/emr

## Robidoux, Evan

| From: | Dandeneau, Kathleen [KDANDENEAU@RC.com](mailto:KDANDENEAU@RC.com) |
| :--- | :--- |
| Sent: | Wednesday, February 5, 2020 4:11 PM |
| To: | Bachman, Melanie; CSC-DL Siting Council |
| Cc: | Baldwin, Kenneth; Mayo, Rachel |
| Subject: | EM-VER-036-200116-220 Winthrop Road, Deep River, CT - Additional Information |
| Attachments: | Deep River_001.pdf |

The original has been mailed to the Siting Council.

Kathleen M. Dandeneau
Legal Administrative Assistant
Robinson \& Cole LLP
280 Trumbull Street
Hartford, CT 06103
Direct $860.541 .2689 \mid$ Fax 860.275.8299
kdandeneau@rc.com | www.rc.com

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Kenneth C. Baldwin

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Main (860) 275-8200
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Direct (860) 275-8345
Also admitted in Massachusetts

February 5, 2020

Melanie A. Bachman, Esq.
Executive Director/Staff Attorney
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051
Re: EM-VER-036-200116 - Cellco Partnership d/b/a Verizon Wireless Notice of Intent to Modify an Existing Telecommunications Facility Located at 220 Winthrop Road, Deep River, Connecticut

Dear Ms. Bachman:
In response to your January 21, 2020 letter regarding the above-referenced filing, attached is a full and complete copy of the Mounts Structural Replacement Report dated January 27, 2020, prepared by Paul J. Ford and Company.

If you have any questions or need any additional information, please do not hesitate to contact me.


Enclosures

## PF PAUL J. FORD \& COMPANY

Report Date:
Client:

January 27, 2020
On Air Engineering, LLC 88 Foundry Pond Road Cold Spring, NY 10516 Attn: David Weinpahl, P.E. (201) 456-4624

## Utility Name:

Structure:
Carrier:
Carrier Site Name:
Mount Type:
Site Address:
City, County, State:
Latitude, Longitude:

Existing 180-ft Monopole
Verizon Wireless Deep River West CT
(1) 12 ft Platform

220 Winthrop Rd Deep River, Middlesex County, CT 41.365772, -72.475314

PJF Project:
A42919-0016.003.7190
Paul J. Ford and Company is pleased to submit this "Mount Structural Replacement Report". The purpose of this analysis is to determine if the mount has sufficient capacity to support the equipment described herein. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point is not part of this document.

## Analysis Criteria:

Reference Standard: 2018 Connecticut State Building Code with the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception \#5 of Section 1609.1.1.

Ultimate Wind Speed: 130 mph 3 -second gust wind speed without ice
Nominal Wind Speed:
Ice Wind Speed:
IBC Site Criteria:

101 mph 3 -second gust wind speed without ice
50 mph 3 -second gust wind speed with $0.75^{\prime \prime}$ ice
Risk Category II, Topographic Category 1, Exposure Category C

## Summary of Analysis Results:

## SUFFICIENT*

*Sufficient upon completion of the changes listed in the 'Recommendations' section of this report.
We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and On Air Engineering, LLC. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully Submitted by:
Paul J. Ford and Company


Angela Sage, E.I.
Structural Designer
asage@pauljford.com


## Columbus

250 E Broad St. Suite 600
Columbus, OH 43215
Phone 614.221.6679


Orlando

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## 1) INTRODUCTION

The proposed mount under consideration is (1) 12 Platform installed at the $176^{\prime}$ elevation on a $180^{\prime}$ Monopole tower. The proposed mount considered in this analysis is a SitePro1 RMQP-496-HK.

## 2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the 2018 Connecticut State Building Code based upon an ultimate 3 -second gust wind speed of 130 mph converted to a nominal 3 -second gust wind speed of 101 mph per section 1609.3 .1 as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception \#5 of Section 1609.1.1. and 50 mph with 0.75 inch ice thickness. Risk Category II, Exposure Category C and Topographic Category 1 with a maximum Topographic Factor, Kzt, of 1 were used in this analysis.

In addition, the mount has been analyzed for various live loading conditions consisting of a 250 -pound maintenance load applied individually at the midpoint and cantilevered ends of horizontal members as well as a 250 -pound maintenance load applied individually at mount pipe locations using a 3-second wind speed of 30 mph .

Table 1 - Equipment Configuration

| Mounting Level (feet) | Center Line Elevation (feet) | Quantity | Manufacturer | Model | Status | Mount Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 176 | 178 | 6 | JMA WIRELESS | MX06FRO660-03 | Proposed | (1) SitePro1 RMQP-496-HK |
|  |  | 3 | SAMSUNG | B2/B66A RRH-BR049 |  |  |
|  |  | 3 | SAMSUNG | B5/B13 RRH-BR04C |  |  |
|  |  | 3 | JMA WIRELESS | 91900314 Dual Bracket |  |  |
|  |  | 1 | RFS | RRFDC-6627-PF-48 |  | Tower Mounted |
|  |  | 6 | ANTEL | BXA-70063-6CF-2 | To Be Removed | (1) $13.5^{\prime}$ Platform |
|  |  | 6 | ANTEL | BXA-171063-12CF-EDIN-2 |  |  |
|  |  | 3 | NOKIA | UHBB B13 RRH $2 \times 40$ |  |  |
|  |  | 2 | RFS | DB-B1-6C-8AB-0Z |  |  |

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Mount Manufacturer Drawings | SitePro1, $9 / 20 / 2018$ | RMQP-496-HK Rev. A | SitePro1 |
| Equipment Layout Drawing | OnAir, $12 / 04 / 2019$ | CT46130 Rev 1 | OnAir |
| Radio Frequency Data Sheet | Verizon, $10 / 15 / 2019$ | 1368979 | OnAir |

## 3.1) Analysis Method

RISA-3D (version 17.0.3), a commercially available analysis software package, was used to create a three-dimensional model of the mount and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix C. In addition, this analysis is in accordance with Verizon's NSTD-446 Antenna Mount Analysis and Modification Process (dated 03/29/19).

## 3.2) Assumptions

1) The analysis of the existing monopole tower or the effect of the mount attachment to the tower is not within the current scope of work.
2) The antenna mounting system was properly fabricated, installed and maintained in good condition, twist free and plumb in accordance with its original design and manufacturer's specifications and all bolts are tightened as specified by the manufacturer and AISC requirements.
3) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1.
4) All member connections have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report. All U-Bolt connections have been properly tightened. This analysis will be required to be revised if the existing conditions in the field differ from those shown in the above referenced documents or assumed in this analysis. No allowance was made for any damaged, missing, or rusted members.
5) Steel grades have been assumed as follows:
a) Channel, Solid Round, Angle, Plate, Unistrut
b) Pipe
c) HSS (Rectangular)

ASTM A36 (GR 36)
d) HSS (Round)

ASTM A53 (GR 35)
e) Connection Bolts

ASTM 500 (GR B-42)
f) Threaded Rods

ASTM A325
g) U-Bolts

ASTM F1554 (GR 36)
SAE 3429 (GR2)
6) Proposed equipment is to be installed in the locations specified in Appendix $A$. Any changes to the proposed equipment locations will render this report invalid.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 3 - Mount Component Capacity

| Notes | Component | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: |
| 1 | Mount Pipes | 81.7 | Pass |
| 1 | Face Horizontal | 28.1 | Pass |
| 1 | Standoff Members | 17.9 | Pass |
| 1 | Bracing Members | 15.6 | Pass |
| 1 | Support Rail | 27.2 | Pass |
| 1 | Corner Plates | 21.7 | Pass |
| 1 | Kick-Brace | 9.9 | Pass |
| 1 | Grating Support Members | 23.9 | Pass |
| 1 | Mount to Tower Connection |  |  |
| (bolts/welds) | 28.0 | Pass |  |

## Mount Rating (max from all components) =

Notes:

1. See additional documentation in "Appendix C - Software analysis Output" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The existing mount does not have sufficient capacity to support the existing and proposed loading. In order for the results of the analysis to be considered valid, the mount listed below shall be installed to support the proposed loading configuration.

- SitePro1 RMQP-496-HK with (12) 8-ft long, P2.0 X-STR (2.38" O.D. $\times 0.204^{\prime \prime}$ ) mount pipes

Verizon Mount Rating: M2050R(2500)-4[6]

## STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON EXISTING MOUNTS BY PAUL J. FORD AND COMPANY

1) It is the responsibility of the client to ensure that the information provided to Paul J. Ford and Company is accurate and complete. Paul J. Ford and Company will rely on the accuracy and completeness of such information in performing or furnishing services under this project.
2) If the existing conditions are not as represented on the referenced drawings and/or documents, Paul J. Ford and Company should be contacted immediately to evaluate the significance of the deviation.
3) The mount has been analyzed according to the minimum design loads recommended by the Reference Standard. If additional design loads are required, Paul J. Ford and Company should be made aware of this prior to the start of the project.
4) The standard of care for all Professional Engineering Services performed or furnished by Paul J. Ford and Company under this project will be the skill and care used by members of the Consultant's profession practicing under similar circumstances at the same time and in the same locality.
5) All Services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Paul J. Ford and Company is not responsible for the conclusions, opinions and/or recommendations made by others based on the information supplied herein.

## APPENDIX A

## WIRE FRAME AND RENDERED MODELS



Envelope Only Solution

| Paul J. Ford and Company |  | SK - 1 |
| :--- | :---: | :--- |
| AMS | Deep River West CT | Jan 27, 2020 at 9:20 AM |
| $42919-0016.003 .7190$ |  | $42919-0016.003 .7190 \_$Wind.r3d |



## APPENDIX B

## SOFTWARE INPUT CALCULATIONS

PF PAULJ. Ford
250 E Broad St, Ste $600 \cdot$ Columbus, OH 43215
Phone 614.221.6679 Www.pauljford.com

| Mount Loading per TIA-222-G-2 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure \& Wind Speed |  | Topo |  | Velocity Pressure | efficients |  | \|ce Loading |  |
|  |  | Exposure $\mathrm{Cat}=$ | C | $z_{\mathrm{g}}=$ | 900 ft |  | ij $=1.00$ |  |
| Structure Type = | Mount | Structure Class = | II | $\mathrm{a}=$ | 9.50 |  | $\mid \mathrm{w}=1$. |  |
| Mount Type = | 3 Sectors | Topographic Cat $=$ | 1 | $\mathrm{K}_{\text {zmin }}=$ | 0.85 |  | $\mathrm{q}_{2}={ }^{=} \quad 8.67$ | psf |
| Mount Centerline, $\mathrm{z}=$ | 176 ft | Crest Height = | 0 ft | $\mathrm{K}_{2}=$ | 1.43 | Calculated Value | $\mathrm{K}_{\mathrm{iz}}=1.18$ |  |
| Centerline Y Coordinate = | 0 in |  |  |  |  |  | $\mathrm{T}_{\text {Lz }}=1$ | in |
|  |  |  |  | $\mathrm{K}_{\mathrm{z}}=$ | 1.43 | Section 2.6.5.2 | $\mathrm{h}=1.00$ | in |
| Wind Speed = | 101 mph |  |  | $\mathrm{K}_{\text {It }}=$ | 1.00 | Section 2.6.6.4 | $\mathrm{W}_{1}=\quad 12.94$ | pst |
| Service Wind Speed = | 30 mph |  |  | $\mathrm{Gh}=$ | 1.00 | Section 2.6.7 |  |  |
| Const. Duration = |  |  |  | $K_{\text {d }}=$ | 0.95 | Table 2-2 | Wind Pressures |  |
| Non-Op Wind Speed = | \#N/A mph |  |  | $1=$ | 1.00 | Table 2-3 | Pressure $=$ | 35.367 |
| Op Wind Speed = | 30 mph |  |  | $\mathbf{a z}_{\mathbf{z}}=$ | $35.37 \mathrm{ps}!$ | Section 2.6.9.6 | Ice Pressure = | 8.667 |
| lce Wind Speed = | 50 mph |  |  |  |  |  |  |  |
| Ice Thickness = | 0.75 in |  |  |  |  |  |  |  |


| Antennas |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hem | Status | Manufacturer | Antenna | Helght (in) | Width (in) | Depth (in) | Flat or Round | Weight (lbs) | Sector I Face | Position | Top/Botto <br> m <br> Mounting Point Spacing | Override Spacing (in) | Max Antenna C/L (fit) | Min Antenna C/L (ft) | Antenna C/L (fi) | Antenna Top Mount Locatlon from Mount Pipe Bottom (in) | Antenna Bottom Mount Lacation from Mount Pipe Bottom (in) |
| 1 | P | JMA WIRELESS | (2) MX06FR0660-03 w/ dual bracket | 71.3 | 30.8 | 10.7 | Flat | 176 | A | 2 | 65.30 |  | 179.28 | 176.72 | 178 | 80.65 | 15.35 |
| 2 | P | JMA WIRELESS | (2) MX06FRO660-03 w/ dual bracket | 71.3 | 30.8 | 10.7 | Flat | 176 | B | 2 | 65.30 |  | 179.28 | $17 \overline{6} .72$ | 178 | 80.65 | 15.35 |
| 3 | P | JMA WIRELESS | (2) MX06FRO660-03 w/ dual bracket | 71.3 | 30.8 | 10.7 | Flat | 176 | C | 2 | 65.30 |  | 179.28 | 176.72 | 178 | 80.65 | 15.35 |
| 14 | P | SAMSUNG TELECOMMUNIGATIONS | B2/B6EA RRH-ERU49 | 15 | 15 | 8.1 | Flat | 70.3 | A | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| 15 | P | SAMSUNG TELECOMMUNIGATIONS | B2/B66A RRH-BR049 | 15 | 15 | 8.1 | Flat | 70.3 | B | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| 16 | P | SAMSUNG TELECOMMUNICATIONS | B2/B66A RRH-BR049 | 15 | 15 | 8.1 | Flat | 70.3 | C | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| 17 | P | SAMSUNG TELECOMMUNICATIONS | B5/B13 RRH-ERO4C | 15 | 15 | 8.1 | Flat | 70.3 | A | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| 18 | P | SAMSUNG TELECOMMUNICATIONS | BS/B13 RRH-BR04C | 15 | 15 | 8.1 | Flat | 70.3 | B | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| 19 | P | SAMSUNG TELECOMMUNICATIONS | B5/B13 RRH-ER04C | 15 | 15 | 8.1 | Flat | 70.3 | c | 2 | 9.00 |  | 181.63 | 174.38 | 178 | 52.50 | 43.50 |
| Dishes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Item | Status | Manufacturer | Microwave Dish | Dia (In) |  | Dish Type |  | Weight <br> (Ibs) | Sector $/$ Face | Position | Top/Botto m <br> Mounting Polnt Spacing | Override Spacing (in) | $\begin{array}{\|c\|} \hline \text { Max } \\ \text { Antenna } \\ \text { C/L (ft) } \end{array}$ |  | Antenna C/L (ft) | Antenna Top Mount Location fram Mount Plpe Bottom (in) | Antenna Bottom Mount Location from Mount Plpe Bottom (in) |

## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

| Paul J. Ford and Company |  | SK - 3 |
| :--- | :---: | :--- |
| AMS | Deep River West CT | Jan 27, 2020 at 9:20 AM |
| 42919-0016.003.7190 |  | $42919-0016.003 .7190 \_$Wind.r3d |



Member Shear Checks Displayed (Enveloped)
Envelope Only Solution
Paul J. Ford and Company
AMS
Deep River West CT
SK - 4

42919-0016.003.7190
Jan 27, 2020 at 9:20 AM





Loads: BLC 3, Wind 0
Envelope Only Solution

| Paul J. Ford and Company |  | SK - 8 |
| :--- | :---: | :--- |
| AMS | Deep River West CT | Jan 27, 2020 at 9:21 AM |
| $42919-0016.003 .7190$ |  | $42919-0016.003 .7190 \_$Wind.r3d |




## (Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :--- | :--- |
| Max Internal Sections for Member Calcs | 97 |
| Include Shear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include Warping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | .12 |
| P-Delta Analysis Tolerance | $0.50 \%$ |
| Include P-Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | Yes |
| Max Iterations for Wall Stiffness | 3 |
| Gravity Acceleration (in/sec^2) | 386.4 |
| Wall Mesh Size (in) | 24 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Y |
| Global Member Orientation Plane | XZ |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |
|  |  |
| Hot Rolled Steel Code | AlSC 14th(360-10): LRFD |
| Adjust Stiffness? | Yes(Iterative) |
| RISAConnection Code | None |
| Cold Formed Steel Code | None |
| Wood Code | None |
| Wood Temperature | < 100F |
| Concrete Code | None |
| Masonry Code | None |
| Aluminum Code | None - Building |
| Stainless Steel Code | None |


| Number of Shear Regions | 4 |
| :--- | :--- |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | .65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections Slab? | Yes |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| Concrete Rebar Set | REBAR SET ASTMA615 |
| Min \% Steel for Column | 1 |
| Max \% Steel for Column | 8 |

Company

## (Global) Model Settings, Continued

| Seismic Code | ASCE 7-10 |
| :--- | :--- |
| Seismic Base Elevation (in) | Not Entered |
| Add Base Weight? | Yes |
| Ct X | .02 |
| Ct Z | .02 |
| T X (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
| Ct Exp. X | .75 |
| Ct Exp. Z | .75 |
| SD1 | 1 |
| SDS | 1 |
| S1 | 1 |
| TL (sec) | 5 |
| Risk Cat | 1 or II |
| Drift Cat | Other |
| Om Z | 1 |
| Om X | 1 |
| Cd Z | 4 |
| Cd X | 4 |
| Rho Z | 1 |
| Rho X | 1 |
|  |  |

## Hot Rolled Steel Properties

| Label |  | E[ksi] | G [ksi] | Nu | Therm (/1E. Densitylk/t., |  | Yield[ksi] Ry |  | Fu[ksi] Rt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | . 3 | 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | . 3 | . 65 | . 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | . 3 | . 65 | 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 3 | . 65 | 49 | 50 | 1.4 | 65 | 1.3 |

## Member Primary Data

|  | Label | 1 Joint | $J$ Joint | K Joint | Rotate(deg) | Section/Shape | Type | Design List | Material | Design Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N1 | N2 |  |  | PIPE 3.0 | None | None | A53 Gr.B | Tvpical |
| 2 | M2 | N16 | N4 |  | 270 | L2x2x3 | None | None | A36 Gr. 36 | Typical |
| 3 | M3 | N16 | N6 |  |  | L2x2x3 | None | None | A36 Gr. 36 | Typical |
| 4 | M4 | N41 | N8 |  | 270 | L2x2x3 | None | None | A36 Gr. 36 | Typical |
| 5 | M5 | N41 | N10 |  |  | L2x2x3 | None | None | A36 Gr. 36 | Tvpical |
| 6 | M6 | N66 | N12 |  | 270 | L2x2x3 | None | None | A36 Gr. 36 | Typical |
| 7 | M7 | N66 | N14 |  |  | L2x2x3 | None | None | A36 Gr. 36 | Typical |
| 8 | M9 | N17 | N22 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 9 | M10 | N18 | N19 |  |  | RIGID | None | None | RIGID | Typical |
| 10 | M11 | N20 | N21 |  |  | PIPE 3.0 | None | None | A53 Gr.B | Typical |
| 11 | M12 | N24 | N22 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 12 | M13 | N23 | N24 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 13 | M14 | N25 | N26 |  |  | RIGID | Nane | None | RIGID | Typical |
| 14 | M15 | N29 | N27 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 15 | M16 | N28 | N29 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 16 | M17 | N30 | N35 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 17 | M18 | N33 | N31 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 18 | M19 | N32 | N33 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 19 | M20 | N34 | N35 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |

$\qquad$

Member Primary Data (Continued)

|  | Label | 1 Joint | $J$ Joint | $K$ Joint | Rotate(dea) | Section/Shape | Type | Design Lis | Material | Desian Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | M21 | N36 | N37 |  |  | RIGID | None | None | RIGID | Typical |
| 21 | M22 | N39 | N38 |  |  | RIGID | None | None | RIGID | Typical |
| 22 | M24 | N42 | N47 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 23 | M25 | N43 | N44 |  |  | RIGID | None | None | RIGID | Typical |
| 24 | M26 | N45 | N46 |  |  | PIPE 3.0 | None | None | A53 Gr.B | Typical |
| 25 | M27 | N49 | N47 |  |  | PL6" ${ }^{\text {x } 1 / 2^{\prime \prime}}$ | None | None | A36 Gr. 36 | Typical |
| 26 | M28 | N48 | N49 |  |  | PL6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 27 | M29 | N50 | N51 |  |  | RIGID | None | None | RIGID | Typical |
| 28 | M30 | N54 | N52 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 29 | M31 | N53 | N54 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 30 | M32 | N55 | N60 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 31 | M33 | N58 | N56 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 32 | M34 | N57 | N58 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 33 | M35 | N59 | N60 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Tvpical |
| 34 | M36 | N62 | N61 |  |  | RIGID | None | None | RIGID | Typical |
| 35 | M37 | N64 | N63 |  |  | RIGID | None | None | RIGID | Tvpical |
| 36 | M38 | N65 | N66 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 37 | M39 | N67 | N70 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 38. | M40 | N68 | N69 |  |  | RIGID | None | None | RIGID | Typical |
| 39 | M41 | N72 | N70 |  |  | PL 6" $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 40 | M42 | N71 | N72 |  |  | PL 6 " $\times 1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 41 | M43 | N73 | N74 |  |  | RIGID | None | None | RIGID | Typical |
| 42 | M44 | N77 | N75 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 43 | M45 | N76 | N77 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 44 | M46 | N78 | N83 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 45 | M47 | N81 | N79 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 46 | M48 | N80 | N81 |  |  | PL6x0.375 | None | None | A36 Gr. 36 | Typical |
| 47 | M49 | N82 | N83 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 48 | M50 | N85 | N84 |  |  | RIGID | None | None | RIGID | Typical |
| 49 | M51 | N86 | N87 |  |  | RIGID | None | None | RIGID | Tvpical |
| 50 | M52 | N89 | N88 |  |  | RIGID | None | None | RIGID | Typical |
| 51 | M70 | N124 | N125 |  |  | PIPE_2.0_HR.. | None | None | A53 Gr.B | Typical |
| 52 | M71 | N126 | N127 |  |  | PIPE_2.0_HR.. | None | None | A53 Gr.B | Typical |
| 53 | M72 | N128 | N129 |  |  | PIPE_2.0_HR.. | None | None | A53 Gr.B | Typical |
| 54 | M73 | N131 | N130 |  | 90 | L2.5x2.5×4 | None | None | A36 Gr. 36 | Typical |
| 55 | M74 | N133 | N132 |  | 90 | L2.5x2.5×4 | None | None | A36 Gr. 36 | Typical |
| 56 | M75 | N135 | N134 |  | 90 | L2.5×2.5×4 | None | None | A36 Gr. 36 | Typical |
| 57 | M76 | N137 | N136 |  |  | RIGID | None | None | RIGID | Typical |
| 58 | C4 | N111 | N112 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 59 | M64 | N114 | N113 |  |  | RIGID | None | None | RIGID | Tvpical |
| 60 | M65 | N116 | N115 |  |  | RIGID | None | None | RIGID | Typical |
| 61 | C3 | N117 | N118 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 62 | M67 | N120 | N119 |  |  | RIGID | None | None | RIGID | Typical |
| 63 | M68 | N122 | N121 |  |  | RIGID | None | None | RIGID | Typical |
| 64 | C2 | N123 | N124A |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 65 | M70A | N126A | N125A |  |  | RIGID | None | None | RIGID | Typical |
| 66 | M71A | N128A | N127A |  |  | RIGID | None | None | RIGID | Typical |
| 67 | C1 | N129A | N130A |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 68 | M73A | N132A | N131A |  |  | RIGID | None | None | RIGID | Typical |
| 69 | M74A | N134A | N133A |  |  | RIGID | None | None | RIGID | Typical |
| 70 | B4 | N135A | N136A |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 71 | M76A | N138 | N137A |  |  | RIGID | None | None | RIGID | Typical |
| 72 | M77 | N140 | N139 |  |  | RIGID | None | None | RIGID | Typical |
| 73 | B3 | N141 | N142 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 74 | M79 | N144 | N143 |  |  | RIGID | None | None | RIGID | Typical |
| 75 | M80 | N146 | N145 |  |  | RIGID | None | None | RIGID | Typical |
| 76 | B2 | N147 | N148 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |



## Member Primary Data (Continued)

|  | Label | 1 Joint | $J$ Joint | $K$ Joint | Rotate(deg) | Section/Shape | Type | Design Lis | Material | Design Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 77 | M82 | N150 | N149 |  |  | RIGID | None | None | RIGID | Typical |
| 78 | M83 | N152 | N151 |  |  | RIGID | None | None | RIGID | Typical |
| 79 | B1 | N153 | N154A |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 80 | M85A | N156A | N155A |  |  | RIGID | None | None | RIGID | Typical |
| 81 | M86A | N158A | N157 |  |  | RIGID | None | None | RIGID | Typical |
| 82 | A4 | N159B | N160A |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 83 | M88 | N162 | N161 |  |  | RIGID | None | None | RIGID | Typical |
| 84 | M89 | N164 | N163 |  |  | RIGID | None | None | RIGID | Typical |
| 85 | A3 | N165 | N166 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 86 | M91 | N168 | N167 |  |  | RIGID | None | None | RIGID | Typical |
| 87 | M92 | N170 | N169 |  |  | RIGID | None | None | RIGID | Typical |
| 88 | A2 | N171 | N172 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 89 | M94 | N174 | N173 |  |  | RIGID | None | None | RIGID | Typical |
| 90 | M95 | N176 | N175 |  |  | RIGID | None | None | RIGID | Typical |
| 91 | A1 | N177 | N178 |  |  | PIPE 2.0X | None | None | A53 Gr.B | Typical |
| 92 | M93 | N172A | N16 |  |  | HSS4X4X4 | None | None | A500 Gr.B Rect | Typical |
| 93 | M95A | N176A | N41 |  |  | HSS4X4X4 | None | None | A500 Gr. B Rect | Typical |
| 94 | M94A | N167A | N166A |  |  | LL2.5×2.5×3×3 | None | None | A36 Gr. 36 | Typical |
| 95 | M95B | N169A | N168A |  |  | LL2.5×2.5 $\times 3 \times 3$ | None | None | A36 Gr. 36 | Typical |
| 96 | M96 | N171A | N170A |  |  | LL2.5×2.5 $\times 3 \times 3$ | None | None | A36 Gr. 36 | Typical |

## Member Advanced Data

|  | Label | 1 Release | $J$ Release | 1 Offset[in] J Offset[in] | T/C Only | Physica | Defl Rat...A | Analysis. | Inactive | Seismic. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 2 | M2 | BenPIN | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 3 | M3 | BenPIN | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 4 | M4 | BenPIN | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 5 | M5 | BenPIN | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 6 | M6 | BenPIN | BenPIN |  |  | Yes' | ** NA ** |  |  | None |
| 7 | M7 | BenPIN | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 8 | M9 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 9 | M10 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 10 | M11 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 11 | M12 |  |  |  |  | Yes | **NA ** |  |  | None |
| 12 | M13 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 13 | M14 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 14 | M15 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 15 | M16 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 16 | M17 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 17 | M18 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 18 | M19 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 19 | M20 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 20 | M21 |  | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 21 | M22 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 22 | M24 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 23 | M25 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 24 | M26 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 25 | M27 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 26 | M28 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 27 | M29 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 28 | M30 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 29 | M31 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 30 | M32 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 31 | M33 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 32 | M34 |  |  |  |  | Yes | ** NA ** |  |  | None |



Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | 1 Offset[in] J Offset[in] | T/C Only | Physical | Defl Rat | Analysis ... | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 33 | M35 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 34 | M36 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 35 | M37 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 36 | M38 |  |  |  |  | Yes | **NA ** |  |  | None |
| 37 | M39 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 38 | M40 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 39 | M41 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 40 | M42 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 41 | M43 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 42 | M44 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 43 | M45 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 44 | M46 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 45 | M47 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 46 | M48 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 47 | M49 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 48 | M50 | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 49 | M51 |  | BenPIN |  |  | Yes | ** NA ** |  |  | None |
| 50 | M52 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 51 | M70 |  |  |  |  | Yes | **NA ** |  |  | None |
| 52 | M71 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 53 | M72 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 54 | M73 | 0000×0 | 0000×0 |  |  | Yes | ** NA ** |  |  | None |
| 55 | M74 | 0000 0 | 0000×0 |  |  | Yes | ** NA ** |  |  | None |
| 56 | M75 | OOOOXO | 0000×0 |  |  | Yes | ** NA ** |  |  | None |
| 57 | M76 |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 58 | C4 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 59 | M64 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 60 | M65 |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 61 | C3 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 62 | M67 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 63 | M68 |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 64 | C2 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 65 | M70A |  |  |  |  | Yes | **NA ** |  |  | None |
| 66 | M71A |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 67 | C1 |  |  |  |  | Yes | **NA ** |  |  | None |
| 68 | M73A |  |  |  |  | Yes | ** NA ** |  |  | None |
| 69 | M74A |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 70 | B4 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 71 | M76A |  |  |  |  | Yes | ** NA ** |  |  | None |
| 72 | M77 |  | $000 \times 00$ |  |  | Yes | **NA ** |  |  | None |
| 73 | B3 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 74 | M79 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 75 | M80 |  | $000 \times 00$ |  |  | Yes | **NA ** |  |  | None |
| 76 | B2 |  |  |  |  | Yes | **NA ** |  |  | None |
| 77 | M82 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 78 | M83 |  | $000 \times 00$ |  |  | Yes | **NA ** |  |  | None |
| 79 | B1 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 80 | M85A |  |  |  |  | Yes | ** NA ** |  |  | None |
| 81 | M86A |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 82 | A4 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 83 | M88 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 84 | M89 |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 85 | A3 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 86 | M91 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 87 | M92 |  | $000 \times 00$ |  |  | Yes | ** NA ** |  |  | None |
| 88 | A2 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 89 | M94 |  |  |  |  | Yes | ** NA ** |  |  | None |
|  | 3D Ver | on 17.0.3 | [G:\...... | .\...\003.7190_MAIR | SAl42919 | -0016.003 | 003.7190 | Wind.r3d |  | age 5 |

Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | 1 Offsetiin] | $J$ Offset[in] | T/C Only | Physic | Defl Rat | Analvsis. | Inactive | Seismic.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | M95 |  | O00X00 |  |  |  | Yes | ** NA ** |  |  | None |
| 91 | A1 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 92 | M93 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 93 | M95A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 94 | M94A | BenPIN |  |  |  |  | Yes | ** NA ** |  |  | None |
| 95 | M95B | BenPIN |  |  |  |  | Yes | ** NA ** |  |  | None |
| 96 | M96 | BenPIN |  |  |  |  | Yes | ** NA ** |  |  | None |

Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[in] | Lbyylin] | Lbzz[in] | Lcomp toplin | Lcomp bot[in] | L-torgu. | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | PIPE 3.0 | 150 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 2 | M2 | L2x2x3 | 51.837 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M3 | L2×2x3 | 51.837 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 4 | M4 | L2x2x3 | 51.837 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 5 | M5 | L2x2x3 | 51.837 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 6 | M6 | L2x2x3 | 51.837 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 7 | M7 | L2x2x | 51.837 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 8 | M9 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 9 | M11 | PIPE 3.0 | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 10 | M12 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 12.707 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 11 | M13 | PL 6" $\times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 12 | M15 | PL6x0.375 | 5.363 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 13 | M16 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 14 | M17 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 15 | M18 | PL6x0.375 | 5.363 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 16 | M19 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 17 | M20 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 18 | M24 | PL 6" $\times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 19 | M26 | PIPE 3.0 | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 20 | M27 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 12.707 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 21 | M28 | PL 6" $\times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 22 | M30 | PL6x0.375 | 5.363 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 23 | M31 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 24 | M32 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 25 | M33 | PL6x0.375 | 5.363 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 26 | M34 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 27 | M35 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 28 | M38 | HSS4X4X4 | 68.014 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 29 | M39 | PL 6" $\times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 30 | M41 | PL 6" $\times 1 / 2^{\prime \prime}$ | 12.707 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 31 | M42 | PL 6" $\times 1 / 2^{\prime \prime}$ | 3.184 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 32 | M44 | PL6x0.375 | 5.363 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 33 | M45 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 34 | M46 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 35 | M47 | PL6x0. 375 | 5.363 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 36 | M48 | PL6x0.375 | 3.499 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 37 | M49 | HSS4X4X4 | 30.71 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 38 | M70 | PIPE_2.0_... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 39 | M71 | PIPE_2.0_... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 40 | M72 | PIPE_2.0... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 41 | M73 | L2.5×2.5×4 | 19.173 |  |  |  |  |  |  |  |  | Lateral |
| 42 | M74 | L2.5×2.5×4 | 19.173 |  |  |  |  |  |  |  |  | Lateral |
| 43 | M75 | L2.5×2.5×4 | 19.173 |  |  |  |  |  |  |  |  | Lateral |
| 44 | C4 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 45 | C3 | PIPE_2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |

Company

## Hot Rolled Steel Design Parameters (Continued)

|  | Label | Shape | Lenathlin] | Lbvylin] | Lbzziin] | Lcomp toplin | Lcomo botlin | L-torau.. | Kw | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | C2 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 47 | C1 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 48 | B4 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 49 | B3 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 50 | B2 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 51 | B1 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 52 | A4 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 53 | A3 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 54 | A2 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 55 | A1 | PIPE 2.0X | 96 |  |  |  |  |  |  |  |  | Lateral |
| 56 | M93 | HSS4X4X4 | 68.014 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 57 | M95A | HSS4X4X4 | 68.014 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 58 | M94A | LL $2.5 \times 2.5 \times 3$. . | 52 |  |  |  |  |  |  |  |  | Lateral |
| 59 | M95B | LL2.5×2.5×3... | 52 |  |  |  |  |  |  |  |  | Lateral |
| 60 | M96 | LL $2.5 \times 2.5 \times 3$. | 52 |  |  |  |  |  |  |  |  | Lateral |

## Basic Load Cases

|  | BLC Description | Category | $X$ Gravity | Gravity | Z Gravity | Joint | Point | Distribut. | Area(Me. | Surface( |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dead | None |  | -1.1 |  |  | 12 |  | 3 |  |
| 2 | Live | None |  |  |  |  |  |  |  |  |
| 3 | Wind 0 | None |  |  |  |  | 24 | 120 |  |  |
| 4 | Wind 30 | None |  |  |  |  | 24 | 120 |  |  |
| 5 | Wind 60 | None |  |  |  |  | 24 | 120 |  |  |
| 6 | Wind 90 | None |  |  |  |  | 24 | 120 |  |  |
| 7 | Wind 120 | None |  |  |  |  | 24 | 120 |  |  |
| 8 | Wind 150 | None |  |  |  |  | 24 | 120 |  |  |
| 9 | Ice Load | None |  |  |  |  | 12 | 60 | 3 |  |
| 10 | Ice 0 | None |  |  |  |  | 24 | 120 |  |  |
| 11 | Ice 30 | None |  |  |  |  | 24 | 120 |  |  |
| 12 | Ice 60 | None |  |  |  |  | 24 | 120 |  |  |
| 13 | Ice 90 | None |  |  |  |  | 24 | 120 |  |  |
| 14 | Ice 120 | None |  |  |  |  | 24 | 120 |  |  |
| 15 | Ice 150 | None |  |  |  |  | 24 | 120 |  |  |
| 16 | Lm | None |  |  |  | 1 |  |  |  |  |
| 17 | Lv | None |  |  |  | 1 |  |  |  |  |
| 18 | BLC 1 Transient Area Loads | None |  | 1 |  |  |  | 75 |  |  |
| 19 | BLC 9 Transient Area Loads | None |  |  |  |  |  | 75 |  |  |

## Load Combinations

|  | Description | S... P. | B. | Fa. | B. | Fa. | B... | Fa... | B... | Fa... | B... $F$ | Fa... |  | Fa... | B...Fa... |  | Fa... B | B... Fa.. | B... Fa ... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4 D | Yes Y | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | $1.2 \mathrm{D}+1.6 \mathrm{~L}$ | Yes Y | 1 | 1.2 | 2 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | 1.2D+1.6 Wo @ 0 | Yes Y | 1 | 1.2 | 3 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | 1.2D+1.6 Wo @ 30 | Yes $Y$ | 1 | 1.2 | 4 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 1.2D+1.6Wo@60 | Yes Y | 1 | 1.2 | 5 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 1.2D+1.6Wo@90 | Yes Y | 1 | 1.2 | 6 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | 1.2D+1.6Wo@120 | Yes Y | 1 | 1.2 | 7 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | 1.2D+1.6Wo@150 | Yes $Y$ | 1 | 1.2 | 8 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | 1.2D+1.6Wo@180 | Yes Y | 1 | 1.2 | 3 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 1.2D+1.6Wo@210 | Yes Y | 1 | 1.2 | 4 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 1.2D+1.6Wo@240 | Yes Y | 1 | 1.2 | 5 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 1.2D+1.6Wo@270 | Yes Y | 1 | 1.2 | 6 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.2D+1.6Wo@300 | Yes Y | 1 | 1.2 | 7 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 | 1.2D+1.6 Wo @ 330 | Yes Y | 1 | 1.2 | 8 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |

Company
Designer
Job Number
Paul J. Ford and Company
Jan 27, 2020

AMS
42919-0016.003.7190
Deep River West CT

9:21 AM
Checked By:

## Load Combinations (Continued)

|  | Description S... |  |  |  |  |  |  |  |  |  |  | Fa... |  | Fa... |  |  |  | Fa.. |  |  | B... Fa... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 1.2D + 1.0 Di + 1.0 Wi@ 0 Yes | $Y$ | 1 | 1.2 | 9 | 1 | 10 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 1.2D+1.0 Di +1.0 Wi @ 30Yes | $Y$ | 1 | 1.2 | 9 | 1 | 11 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 17 | 1.2D+1.0 Di + 1.0 Wi@60Yes | $Y$ | 1 | 1.2 | 9 | 1 | 12 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18 | 1.2D+1.0 Di +1.0 Wi@ 90Yes | $Y$ | 1 | 1.2 | 9 | 1 | 13 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 19 | 1.2D + 1.0 Di +1.0 Wi @ ... Yes | $Y$ | 1 | 1.2 | 9 | 1 | 14 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 1.2D+1.0 Di +1.0Wi@...Yes | $Y$ | 1 | 1.2 | 9 | 1 | 15 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | 1.2D + 1.0 Di + 1.0 Wi@... Yes | $Y$ | 1 | 1.2 | 9 | 1 | 10 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | 1.2D+1.0 Di +1.0Wi@ ...Yes | $Y$ | 1 | 1.2 | 9 | 1 | 11 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 23 | 1.2D+1.0 Di +1.0 Wi@...Yes | $Y$ | 1 | 1.2 | 9 | 1 | 12 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | 1.2D+1.0 Di +1.0 Wi@...Yes | $Y$ | 1 | 1.2 | 9 | 1 | 13 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 25 | 1.2D+1.0 Di +1.0 Wi@ ... Yes | $Y$ | 1 | 1.2 | 9 | 1 | 14 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 | 1.2D+1.0 Di +1.0 Wi@ ... Yes | $Y$ | 1 | 1.2 | 9 | 1 | 15 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | 1.2D + 1.5 Lm + 1.0 Wm ... Yes | $Y$ | 1 | 1.2 | 3 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 28 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 4 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 29 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} \ldots$ Yes | $Y$ | 1 | 1.2 | 5 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 | 1.2D + $1.5 \mathrm{Lm}+1.0 \mathrm{Wm} \ldots$ Yes | $Y$ | 1 | 1.2 | 6 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 7 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 | 1.2D + 1.5 Lm + 1.0 Wm ... Yes | $Y$ | 1 | 1.2 | 8 | . 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 33 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 3 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 34 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} \ldots$ Yes | $Y$ | 1 | 1.2 | 4 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 5 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 36 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 6 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} \ldots$ Yes | $Y$ | 1 | 1.2 | 7 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}+1.0 \mathrm{Wm} . .$. Yes | $Y$ | 1 | 1.2 | 8 | -. 088 | 16 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 39 | 1.2D+1.5 Lv Yes | $Y$ | 1 | 1.2 | 17 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Envelope Joint Reactions

| Joint |  |  | $\times$ [lb] |  |  | Z [lb] |  | LC | MX[k-in] LC |  | $\begin{aligned} & \text { MY [k-in] } \\ & \hline 30.777 \\ & \hline \end{aligned}$ | $\begin{gathered} \text { LC } \\ \hline 9 \end{gathered}$ | $M Z[k-i n] \quad L C$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N65 | max | 4351.028 | 12 | 768.023 | 12 | 1637.864 | 3 | 1.105 | 13 |  |  | $9.657$ | 24 |
| 2 |  | min | -6569.516 | 6 | -317.691 | 6 | -1650.753 | 9 | -4.671 | 19 | -30.364 | 3 | -1.53 | 6 |
| 3 | N172A | max | 3147.09 | 14 | 767.983 | 8 | 5768.323 | 14 | 10.341 | 20 | 30.806 | 5 | 3.376 | 3 |
| 4 |  | min | -2041.851 | 8 | -317.66 | 14 | -3844.726 | 8 | -. 018 | 14 | -30.393 | 11 | -4.66 | 9 |
| 5 | N176A | max | 3421.906 | 10 | 768.083 | 4 | 3691.512 | 4 | 2.633 | 10 | 30.787 | 13 | -.842 | 9 |
| 6 |  | min | -2308.686 | 4 | -317.742 | 10 | -5610.508 | 10 | -7.237 | 4 | -30.373 | 7 | -8.485 | 15 |
| 7 | N166A | max | 3540.79 | 18 | 2562.336 | 18 | 53.264 | 14 | 0 | 39 | 0 | 39 | 0 | 39 |
| 8 |  | min | -1137.133 | 12 | -818.252 | 12 | -53.24 | 10 | 0 | 1 | 0 | 1 | 0 | 1 |
| 9 | N168A | max | 568.372 | 8 | 2562.247 | 26 | 984.477 | 8 | 0 | 39 | 0 | 39 | 0 | 39 |
| 10 |  | min | -1770.323 | 26 | -817.994 | 8 | -3066.31 | 26 | 0 | 1 | 0 | 1 | 0 | 1 |
| 11 | N170A | max | 568.623 | 4 | 2562.353 | 22 | 3066.43 | 22 | 0 | 39 | 0 | 39 | 0 | 39 |
| 12 |  | min | -1770.415 | 22 | -818.314 | 4 | -984.855 | 4 | 0 | 1 | 0 | 1 | 0 | 1 |
| 13 | Totals: | max | 6997.848 | 12 | 7955.754 | 23 | 6692.22 | 3 |  |  |  |  |  |  |
| 14 |  | min | -6997.889 | 6 | 3163.608 | 5 | -6692.211 | 9 |  |  |  |  |  |  |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

| Member |  |  | Code C... Loclin] LC Shear.,. |  |  |  | $\begin{gathered} \text { Loc[in] } \\ 66 \end{gathered}$ | $\begin{aligned} & \text { Dir LC phi*Pnc [lb] } \\ & \|11\| 19844.858 \end{aligned}$ |  | $\frac{\text { phi*Pnt [lb] phi*Mn y-... }}{44100} \frac{30.366}{}$ |  |  |  | $\begin{gathered} \text { Ean } \\ \hline \text { H3-6 } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | C1 | PIPE 2.0X |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | B1 | PIPE 2.0X | 817 | 24 | 6 | . 414 | 66 | 7 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 3 | A1 | PIPE 2.0X | . 817 | 24 | 14 | . 414 | 66 | 3 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 4 | A4 | PIPE 2.0X | . 808 | 24 | 6 | . 372 | 66 | 5 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 5 | B4 | PIPE 2.0X | . 808 | 24 | 10 | . 372 | 66 | 9 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 6 | C4 | PIPE 2.0X | . 808 | 24 | 14 | . 372 | 66 | 13 | 19844.858 | 44100 | 30.366 | 30.366 | $1 .$. | H3-6 |
| 7 | A3 | PIPE 2.0X | . 806 | 24 | 6 | . 335 | 24 | 5 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 8 | B3 | PIPE_2.0X | . 806 | 24 | 10 | . 335 | 24 | 9 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |
| 9 | C3 | PIPE_2.0X | . 806 | 24 | 14 | . 334 | 24 | 13 | 19844.858 | 44100 | 30.366 | 30.366 | 1... | H3-6 |



## Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

| Member |  | Shape | Code C... Loclin] LC Shear |  |  | Loclin | Dir LC <br> 5 |  | $\begin{gathered} \text { Cphi*Pnc [libl) } \\ 6295.422 \\ \hline \end{gathered}$ | phi*Pnt Ilbl phi*Mn v-...  <br> 32130 22.459 |  | $\frac{\text { phi'Mn z-... }}{22.459}$ | $\begin{aligned} & \mathrm{Cb} \\ & 3 \ldots \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Ean } \\ & \text { H3-6 } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | M72 | PIPE_2.0_H... | 772 | 6.25 5 | 460 | 14.062 |  |  |  |  |  |  |  |  |
| 11 | M70 | PIPE_2.0_H... | 772 | 6.2513 | 460 | 14.063 |  | 13 | 6295.422 | 32130 | 22.459 | 22.459 | 3... | H3-6 |
| 12 | M71 | PIPE_2.0_H... | 772 | 6.259 | 460 | 14.063 |  | 9 | 6295.422 | 32130 | 22.459 | 22.459 | 3... | H3-6 |
| 13 | C2 | PIPE 2.0X | 752 | 2410 | 254 | 66 |  | 10 | 19844.858 | 44100 | 30.366 | 30.366 | 1. | H3-6 |
| 14 | B2 | PIPE 2.0X | 751 | 246 | 254 | 66 |  | 6 | 19844.858 | 44100 | 30.366 | 30.366 | . | H3-6 |
| 15 | A2 | PIPE 2.0X | 751 | 2414 | 254 | 66 |  | 14 | 19844.85 | 44100 | 30.366 | 30.366 |  | H3-6 |
| 16 | M18 | PL6x0.375 | . 550 | 2.8495 | 124 | 2.849 | 1 | 10 | 63826.16 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 17 | M47 | PL6x0.375 | . 550 | 2.8499 | 124 | 2.849 | 1 | 14 | 63826.168 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 18 | M33 | PL6x0.375 | 550 | 2.84913 | 124 | 2.849 | 6 | 6 | 63826.168 | 72900 | 6.836 | 109.35 | 1. | H1-1b |
| 19 | M73 | L2.5x2.5x4 | 461 | 19.1735 | 323 | 0 | 1 | 13 | 35474.554 | 38556 | 13.363 | 30.449 | . 4 | H2-1 |
| 20 | M74 | L2.5x2.5×4 | 461 | 19.17313 | 323 | 0 | 9 | 9 | 35474.55 | 38556 | 13.363 | 30.449 | . 4 | H2-1 |
| 21 | M75 | L2.5×2.5×4 | 461 | 19.1739 | 323 | 0 | 5 | 5 | 35474.554 | 38556 | 13.363 | 30.449 |  | H2-1 |
| 22 | M15 | PL6x0. 375 | . 355 | 2.84911 | 213 | 2.849 | 1 | 19 | 63826.168 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 23 | M30 | PL6x0.375 | . 355 | 2.8497 | 213 | 2.849 | 1 | 15 | 63 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 24 | M44 | PL6x0. 375 | . 355 | 2.8493 | 213 | 2.849 | 2 | 23 | 63826.16 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 25 | M34 | PL6x0.375 | 346 | 1.4225 | 323 | 3.499 | $y 2$ | 21 | 68804 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 26 | M19 | PL6x0.375 | 346 | 1.4229 | 323 | 3.499 | 2 | 25 | 68804. | 72900 | 6.836 | 109.35 |  | H1-1b |
| 27 | M48 | PL6x0.375 | 346 | 1.42213 | 323 | 3.499 | 1 | 17 | 68804. | 72900 | 6.836 | 109.35 |  | H1-1b |
| 28 | M45 | PL6x0.375 | . 311 | 1.42212 | 281 | 3.499 | 1 | 19 | 68804.1 | 72900 | 6.836 | 109.35 | 1. | H1-1b |
| 29 | M31 | PL6x0.375 | 311 | 1.422 | 281 | 3.499 | 2 | 23 | 68804.199 | 72900 | . 836 | 109.35 |  | H1-1b |
| 30 | M16 | PL6x0.375 | 311 | 1.4228 | 281 | 3.499 | 1 | 15 | 68804.19 | 72900 | 6.836 | 109.35 |  | H1-1b |
| 31 | M1 | PIPE 3.0 | . 281 | 54.6886 | 261 | 50 |  | 5 | 28250.554 | 65205 | 68.985 | 68.985 | 3.. | H3-6 |
| 32 | M26 | PIPE_3.0 | 281 | 54.68710 | 261 | 50 |  | 9 | 28250.55 | 65205 | 68.985 | 68.985 | 3. | H3-6 |
| 33 | M11 | PIPE 3.0 | 281 | 4 | 261 | 50 |  | 13 | 28250.55 | 65205 | 68.985 | 68.985 | 3. | H3-6 |
| 34 | M5 | L2x2x | 239 | 25.91811 | 010 | 51.837 | y 1 | 17 | 9185.35 | 23392.8 | 6.693 | 13.031 |  | H2-1 |
| 35 | M3 | L2x2 | 239 | 25.9183 | . 010 | 51.837 | $v 2$ | 21 | 9185.35 | 23392.8 | 6.693 | 13.031 |  | H2-1 |
| 36 | M7 | $12 \times 2 \times 3$ | 239 | 25.9187 | . 010 | 51 | $y 2$ | 25 | 9185.35 | 23392.8 | 6.693 | 13.031 | 1. | H2-1 |
| 37 | M41 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 217 | 6.3546 | . 124 | 6.354 | 9 | 9 | 64843.035 | 97200 | 12.15 | 145.8 |  | H1-1b |
| 38 | M12 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 217 | 6.35414 | . 124 | 6.354 | y 5 | 5 | 64843.03 | 97200 | 12.15 | 145.8 |  | H1-1b |
| 39 | M27 | PL 6 " $\times 1 / 2^{\prime \prime}$ | 217 | 6.35410 | 124 | 6.354 | v 1 | 13 | 64843 | 97200 | 12.15 | 145.8 |  | H1-1b |
| 40 | M4 | L2 $\times 2 \times 3$ | 207 | 25.9189 | . 010 | 51.837 | z 1 | 15 | 9185.35 | 23392.8 | 6.693 | 13.03 |  | H2-1 |
| 41 | M2 | L2 $2 \times 2 \times 3$ | 207 | 25.91813 | . 010 | 51.837 | 1 | 19 | 9185.35 | 23392.8 | 6.693 | 13.03 |  | H2-1 |
| 42 | M6 | L2 $2 \times 2 \times 3$ | 207 | 25.9185 | . 010 | 51.837 | z 2 | 23 | 9185.35 | 23392.8 | 6.693 | 13.03 |  | H2-1 |
| 43 | M93 | HSS4X4X4 | 179 | 11 | 065 | 0 | 5 | 5 | 121966.8.. | 139518 | 194.166 | 194.166 | 2. | H1-1b |
| 44 | M95A | HSS4X4X4 | . 179 | 07 | 065 | 0 | 1 | 13 | 121966.8. | 139518 | 194.166 | 194.166 |  | H1-1b |
| 45 | M38 | HSS4X4X4 | . 179 | 3 | 065 | 0 | z 9 | 9 | 121966.8 | 139518 | 194.166 | 194.166 |  | H1-1b |
| 46 | M35 | HSS4X4X4 | . 156 | 30.7123 | . 057 | 3.519 | 1 | 11 | 135745.8 | 139518 | 194.166 | 194.166 | 1. | H1-1b |
| 47 | M49 | HSS4X4X4 | . 156 | 30.7119 | . 057 | 3.519 | 7 | 7 | 135745.8 | 139518 | 194.166 | 194.166 |  | H1-1b |
| 48 | M20 | HSS4X4X4 | 156 | 30.7115 | . 057 | 3.519 | 3 | 3 | 135745.8. | 139518 | 194.166 | 194.166 |  | H1-1b |
| 49 | M46 | HSS4X4X4 | . 141 | 30.7117 | 045 | 3.519 | 6 | 6 | 135745.8. | 139518 | 194.166 | 194.166 |  | H1-1b |
| 50 | M17 | HSS4X4X4 | . 141 | 30.7125 | . 045 | 3.519 | z 1 | 14 | 135745.8. | 139518 | 194.166 | 194.166 | 1 | H1-1b |
| 51 | M32 | HSS4X4X4 | 141 | 30.7121 | . 045 | 3.519 | 1 | 10 | 135745.8 | 139518 | 194.166 | 194.166 | 1. | H1-1b |
| 52 | M39 | PL ${ }^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 123 | 1.6596 | 144 | 3.184 | 5 | 5 | 94760.15 | 97200 | 12.15 | 145.8 | 2 | H1-1b |
| 53 | M24 | PL 6" $\times 1 / 2^{\prime \prime}$ | 123 | 1.65910 | 144 | 3.184 | v 9 | 9 | 94760.15 | 97200 | 12.15 | 145.8 | 2 | H1-1b |
| 54 | M9 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 123 | 1.65914 | . 144 | 3.184 | y 1 | 13 | 94760.15 | 97200 | 12.15 | 145.8 | 2 | H1-1b |
| 55 | M28 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 113 | 1.65910 | . 181 | 3.184 | v 1 | 11 | 94760.15 | 97200 | 12.15 | 145.8 | 2. | H1-1b |
| 56 | M42 | PL 6 " $\times 1 / 2^{\prime \prime}$ | 113 | 1.6596 | . 181 | 3.184 | 7 | 7 | 94760.158 | 97200 | 12.15 | 145.8 | 2. | H1-1b |
| 57 | M13 | PL $6^{\prime \prime} \times 1 / 2^{\prime \prime}$ | 113 | 1.65914 | 181 | 3.184 | 3 | 3 | 94760.15 | 97200 | 12.15 | 145.8 | 2. | H1-1b |
| 58 | M96 | LL2.5x2.5×3×3 | . 099 | 52.22 | . 003 | 52 | 1 | 12 | 43964.697 | 58320 | 47.452 | 30.595 | 1 | H1-1 ${ }^{\text {* }}$ |
| 59 | M94A | LL2 $2.5 \times 2.5 \times 3 \times 3$ | 099 | 5218 | 003 | 0 | z 1 | 14 | 43964.69 | 58320 | 47.452 | 30.595 | 1 | H1-1b* |
| 60 | M95B | LL2.5×2.5×3x3 | . 099 | 5226 | 003 | 52 | 1 | 12 | 43964.697 | 58320 | 47.452 | 30.595 | 1 | H1-1b* |


MOUNT TO TOWER CONNECTION CHECKS

$$
\begin{array}{cl}
\mathbf{4} & \\
9 & \text { in } \\
9 & \text { in } \\
\mathbf{1 . 5} & \text { in } \\
4.5 & \text { in } \\
4.5 & \text { in } \\
0 & \text { in } \\
0 & \text { in } \\
9.657 & \text { Kips-in } \\
30.777 & \text { Kips-in } \\
4.671 & \text { Kips-in }
\end{array}
$$

$$
\begin{array}{rll}
\text { REACTIONS } \\
\text { Px } & 1.651 & \text { Kip } \\
\text { Py } & 0.768 & \text { Kip } \\
\text { (Axial)Pz } & 6.57 & \text { Kip } \\
\text { Mx } & 9.657 & \text { Kip-in } \\
\text { My } & =30.777 & \text { Kip-in } \\
\text { (Torque)Mz } & 4.671 & \text { Kip-in } \\
\text { Number of Bolts }
\end{array}
$$

Plate Size b

> s7|og dof əכuełธ! p ospp

 Load eccentricity in $x$-direction, ex Load eccentricity in $y$-direction, ey Total Moment including load eccentricity $\Sigma M x=$ Total Moment including load eccentricity $5 \mathrm{My}=$ Total Moment including load eccentricity $5 \mathrm{Mz}=$ BOLT CHECKS

$$
\begin{aligned}
& 5.01 \\
& 0.72
\end{aligned}
$$

$$
\begin{array}{lll}
\text { Tension Reaction } & 5.01 & \text { kip }
\end{array}
$$

$$
\mathrm{A} 325 \mathrm{~N}
$$

$$
\begin{aligned}
& \text { kip } \\
& \text { kip }
\end{aligned}
$$

$$
0.625 \text { in }
$$

$$
\begin{array}{ll}
20.7 & \text { kips } \\
12.4 & \text { kips }
\end{array}
$$

[^0]
# ASCE 

## Address:

No Address at This Location

## ASCE 7 Hazards Report

Standard: $\quad$ ASCE/SEI 7-10 Elevation: 241.52 ft (NAVD 88)
Risk Category: II Latitude: 41.365772
Soil Class: D - Stiff Soil
Longitude: -72.475314


## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

130 Vmph
78 Vmph
88 Vmph
96 Vmph
106 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Thu Dec 122019
Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure $C$ Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

| Site Soil Class: | D - Stiff Soil |  |  |
| :---: | :---: | :---: | :---: |
| Results: |  |  |  |
| $\mathrm{S}_{\mathrm{s}}$ : | 0.17 | $S_{\text {DS }}$ | 0.182 |
| $\mathrm{S}_{1}$ | 0.06 | $\mathrm{S}_{\mathrm{D} 1}$ | 0.096 |
| $\mathrm{F}_{\mathrm{a}}$ | 1.6 | $\mathrm{T}_{\mathrm{L}}$ : | 6 |
| $F_{v}$ : | 2.4 | PGA : | 0.086 |
| $\mathrm{S}_{\text {MS }}$ : | 0.272 | $\mathrm{PGA}_{\mathrm{M}}$ : | 0.137 |
| $\mathrm{S}_{\mathrm{M1}}$ | 0.144 | $\mathrm{F}_{\mathrm{PGA}}$ | 1.6 |
|  |  | $l_{\text {e }}$ : | 1 |
| Seismic Design Category Data Accessed: | Thu Dec 122019 |  |  |
| Date Source: | USG <br> Supp Additi ASCE | Maps ba <br> ata of Ma <br> -specific <br> 1 are ava | $\begin{aligned} & \text { CE/SEI } \\ & 3, \text { and } \\ & \text { on pro } \\ & \text { JSGS. } \end{aligned}$ |

## Results:

| Ice Thickness: | 0.75 in. |
| :--- | :--- |
| Concurrent Temperature: | 15 F |
| Gust Speed: | 50 mph |
| Source: | Standard ASCE/SEl 7-10, Figs. 10-2 through 10-8 |
| Accessed: | Thu Dec 12 2019 |

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

## APPENDIX D

## SUPPLEMENTAL MODIFICATION INFORMATION



## APPENDIX E

## MANUFACTURER DRAWINGS (FOR REFERENCE ONLY)




## APPENDIX F

## POST MODIFICATION INSPECTION (PMI) REQUIREMENTS FOR DESKTOP REVIEW

# Post Modification Inspection (PMI) Report Requirements Documents \& Photos Required from Contractor 

Purpose - to provide PJF the proper documentation in order to complete the required Mount Desktop review of the Post Modification Inspection Report.

- Contractor is responsible for making certain the photos provided as noted below provide confirmation that the modification was completed in accordance with the modification drawings.
- Contractor shall relay any data that can impact the performance of the mount or the mount modification, this includes safety issues.


## Base Requirements:

- Provide "as built drawings" showing contractor's name, preparer's signature, and date. Any deviations from the drawing (proposed modification) must be shown.
- Notation that all hardware was properly installed, and the existing hardware was inspected for any issues.
- Verification that loading is as communicated in the modification drawings. NOTE if loading is different than what is conveyed in the modification drawing contact PJF immediately.
- Each photo should be time and date stamped.
- Photos should be high resolution and submitted in a Zip File and should be organized in the file structure as depicted in Schedule A attached.
- Any special photos outside of the standard requirements will be indicated on the drawings.
- Contractor shall ensure that the safety climb wire rope is supported and not adversely impacted by the install of the modification components. This may involve the install of wire rope guides, or other items to protect the wire rope.
- The photos in the file structure should be uploaded to pjfmount@pauljford.com as depicted on the drawings.


## Photo Requirements:

- Base and "During Installation Photos"
- Base pictures include
- Photo of Gate Signs showing the tower owner, site name, and number.
- Photo of carrier shelter showing the carrier site name and number if available.
- Photos of the galvanizing compound and/or paint used (if applicable), clearly showing the label and name.
- "During Installation" Photos if provided - must be placed only in this folder
- Photos taken at ground level
- Overall tower structure before and after installation of the modifications
- Photos of the appropriate mount before and after installation of the modifications; if the mounts are at different rad elevations, pictures must be provided for all elevations that the modifications were installed.
- Photos taken at Mount Elevation
- Photos showing each individual sector before and after installation of modifications. Each entire sector must be in one photo to show in the inter-connection of members.
- Close-up photos of each installed modification per the modification drawings; pictures should also include connection hardware (U-bolts, bolts, nuts, all-threaded rods, etc.)
- Photos showing the measurements of the installed modification member sizes (i.e. lengths, widths, depths, diameters, thicknesses).
- Photos showing the elevation or distances of the installed modifications from the appropriate reference locations shown in the modification drawings.
- Photos showing the installed modifications onto the tower with tape drop measurements (if applicable) (i.e. ring/collar mounts, tie-backs, V-bracing kits, etc.); if the existing mount elevations needs to be changed according to the modification drawings, a tape drop measurement shall be provided before the elevation change.
- Photos showing the safety climb wire rope above and below the mount prior to modification.
- Photos showing the safety climb wire rope above and below the mount post modification.


## Antenna and equipment placement and Geometry Certification:

- The contractor must certify that the antenna and equipment placement and geometry is in accordance with the antenna placement diagrams as included in this mount analysis.The contractor certifies per photos that the equipment on the mount is as depicted on the antenna placement diagrams as included in this mount analysis.
$\square \quad$ The contractor notes that the equipment on the mount is not in accordance with the antenna placement diagrams and has accordingly marked up the diagrams or provided a diagram outlining the differences.

Certifying Individual: Company

Name

Signature

## Schedule A - Photo \& Document File Structure

- VzW Site Number / Name
- Base \& "During Installation" Photos
- Pre-Installation Photos
- Alpha
- Beta
- Gamma
- Ground Level
- Tape Drop
- Post-Installation Photos
- Alpha
- Beta
- Gamma
- Ground Level
- Tape Drop
- Material Certification - Submission of this document including executed certification on Page 2
- Specific Required Additional Photos
- Required Additional Photos


## Special Instructions / Validation as required from the MA or any other information the contractor deems necessary to share that was identified:

## Issue:

## Response:

$\qquad$
$\qquad$
$\qquad$
$\qquad$

| From: | Dandeneau, Kathleen |
| :--- | :--- |
| To: | Bachman, Melanie; CSC-DL Siting Council |
| Cc: | Baldwin, Kenneth; Mayo, Rachel |
| Subject: | EM-VER-036-200116-220 Winthrop Road, Deep River, CT - Additional Information |
| Date: | Wednesday, January 22, 2020 3:20:11 PM |
| Attachments: | Deep River 001.pdf |

The original has been mailed to the Siting Council.

## Kathleen M. Dandeneau

Legal Administrative Assistant

Robinson \& Cole LLP
280 Trumbull Street
Hartford, CT 06103
Direct 860.541.2689 | Fax 860.275.8299
kdandeneau@rc.com | www.rc.com

## Robinson+Cole

Boston | Hartford | New York | Providence | Miami | Stamford Los Angeles | Wilmington | Philadelphia | Albany | New London

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Kenneth C. Baldwin

280 Trumbull Street
Hartford, CT 06103-3597
Main (860) 275-8200
Fax (860) 275-8299
kbaldwin@rc.com
Direct (860) 275-8345
Also admitted in Massachusetts

January 22, 2020

Melanie A. Bachman, Esq.
Executive Director/Staff Attorney
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051
Re: EM-VER-036-200116 - Cellco Partnership d/b/a Verizon Wireless Notice of Intent to Modify an Existing Telecommunications Facility Located at 220 Winthrop Road, Deep River, Connecticut

Dear Ms. Bachman:
In response to your January 21, 2020 letter regarding the above-referenced filing, attached is the following additional information.

1. A stamped and signed copy of the Structural Analysis Report prepared by Tower Engineering Solutions and dated December 5, 2019.
2. A stamped and signed full and complete copy of the Mounts Analysis dated December 13, 2019, prepared by Paul J. Ford and Company.

If you have any questions or need any additional information, please do not hesitate to contact me.


Enclosures


Tower Engineering Solutions
Phone (972) 483-0607, Fax (972) 975-9615
1320 Greenway Drive, Suite 600, Irving, Texas 75038

## Structural Analysis Report

Existing 180 ft. Valmont Monopole<br>Customer Name: SBA Communications Corp<br>Customer Site Number: CT46130-A<br>Customer Site Name: Deep River-winthrop Rd<br>Carrier Name: Verizon (App\#: 100842, V4)<br>Carrier Site ID / Name: 262760 / Deep River West CT<br>Site Location: 220 Winthrop Rd<br>Deep River, Connecticut<br>Middlesex County<br>Latitude: 41.365872<br>Longitude: -72.474849

Analysis Result:
Max Structural Usage: 86.5\% [Pass]
Max Foundation Usage: 77.0\% [Pass]


Additional Usage Caused by New Mount/Mount Modification: +0.3\%

Report Prepared By : Delu Zhou

Phone (972) 483-0607, Fax (972) 975-9615

## Structural Analysis Report

Existing 180 ft. Valmont Monopole<br>Customer Name: SBA Communications Corp<br>Customer Site Number: CT46130-A<br>Customer Site Name: Deep River-winthrop Rd<br>Carrier Name: Verizon (App\#: 100842, V4)<br>Carrier Site ID / Name: 262760 / Deep River West CT<br>Site Location: 220 Winthrop Rd<br>Deep River, Connecticut<br>Middlesex County<br>Latitude: 41.365872<br>Longitude: -72.474849

Analysis Result:<br>Max Structural Usage: 86.5\% [Pass]<br>Max Foundation Usage: 77.0\% [Pass]<br>Additional Usage Caused by New Mount/Mount Modification: +0.3\%

Report Prepared By: Delu Zhou

## Introduction

The purpose of this report is to summarize the analysis results on the 180 ft Valmont Monopole to support the proposed antennas and transmission lines in addition to those currently installed. Any modification listed under Sources of Information was assumed completed and was included in this analysis.

## Sources of Information

| Tower Drawings | Original structural design report \& permit drawings prepared by Valmont. Dated <br> 10-27-2000. Order No 17593-98. CT750 Deep River Site. Project No F082. Previous <br> structural report prepared by FDH Engineering, Inc. Dated 11-04-2013. Project No <br> 13SFRX1400. |
| :--- | :--- |
| Foundation Drawing | Original foundation drawings prepared by Valmont Industries, Inc. Dated 08-11- <br> 1998. Project No 2633. Order No 17593-98. Drawing No 2633-F. |
| Geotechnical Report | Geotechnical report prepared by TECTONIC Engineering Consultants, P.C. Dated 07- <br> 13-1998. Work Order No 1170.C750. |
| Modification Drawings | N/A |

## Analysis Criteria

The comprehensive analysis was performed in accordance with the requirements and stipulations of the ANSI/TIA/EIA 222-H. In accordance with this standard, the structure was analyzed using TESPoles, a proprietary analysis software. The program considers the structure as an elastic 3-D model with secondorder effects and temperature effects incorporated in the analysis. The analysis was performed using multiple wind directions.

| Wind Speed Used in the Analysis: | 123.0 mph (3-Sec. Gust) (Ultimate wind speed) |
| :--- | :--- |
| Wind Speed with Ice: | $50 \mathrm{mph}\left(3-S e c\right.$. Gust) with $3 / 4^{\prime \prime}$ radial ice concurrent |
| Service Load Wind Speed: | $60 \mathrm{mph}+0^{\prime \prime}$ Radial ice |
| Standard/Codes: | ANSI/TIA/EIA 222-H / 2018 IBC / 2018 Connecticut State |
|  | Building Code |
| Exposure Category: | C |
| Risk Category: | II |
| Topographic Category: | 1 |
| Crest Height: | 0 ft. |
| Seismic Parameters: | $\mathrm{S}_{5}=0.21, \mathrm{~S}_{1}=0.054$ |

This structural analysis is based upon the tower being classified as a Risk Category II; however, if a different classification is required subsequent to the date hereof, the tower classification will be changed to meet such requirement and a new structural analysis will be run.

## Existing Antennas, Mounts and Transmission Lines

The table below summarizes the antennas, mounts and transmission lines that were considered in the analysis as existing on the tower.

| Items | Elevation <br> ( ft ) | Qty. | Antenna Descriptions | Mount Type \& Qty. | Transmission $\qquad$ | Owner |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | 178.0 | 3 | JMA Wireless MX06FRO660-03- Panel | Platform w/ Handrails | (2) $15 / 8$ " Hybrid | Verizon |
| - |  | 3 | Amphenol BXA-70063-6CF-2- Panel |  |  |  |
| - |  | 6 | Amphenol BXA-171063-12CF-EDIN-2 Panel |  |  |  |
| - |  | 3 | Commscope CBC1923Q-43 Diplexer |  |  |  |
| - |  | 3 | Alcatel Lucent RRH2X40-07-U |  |  |  |
| - |  | 3 | Samsung B2/B66A RRH BR049 |  |  |  |
| - |  | 1 | Rfs Celwave DB-B1-6C-8AB-0Z COVP |  |  |  |
| 5 | 166.0 | 3 | RFS APXVTM14-C-120-Panel | Platform w/Handrails <br> + Sitepro PRK-1245L <br> + handrail kit + Sitepro PRK-SFS-H-L] | (4) 1-1/4" Hybrid | Sprint <br> Nextel |
| 6 |  | 3 | Commscope NNVV-65B-R4 - Panel |  |  |  |
| 7 |  | 3 | ALU 1900 Mhz |  |  |  |
| 8 |  | 6 | ALU 800 Mhz |  |  |  |
| 9 |  | 3 | ALU TD-RRH8x20-25 |  |  |  |
| 10 | 158.0 | 6 | EMS RR90-17-02DP - Panel | (3) T-Arms | (6) $15 / 8{ }^{\prime \prime}$ | T-Mobile |
| 11 |  | 6 | Airtech PCS 1900 G3 TMAs |  |  |  |
| 12 | 150.0 | 2 | Cci HPA-65R-BUU-H6- Panel | Low Profile Platform w/ Handrail kit HRK-12 | (12) $11 / 4^{\prime \prime} ;$ <br> [ (1) 10 mm \& (2) <br> 19.7 mm inside <br> (1) $3^{\prime \prime}$ Innerduct] | AT\&T |
| 13 |  | 1 | Commscope SBNHH-1D65A- Panel |  |  |  |
| 14 |  | 3 | Ericsson RRUS-32-RRU |  |  |  |
| 15 |  | 2 | KMW AM-X-CD-16-65-00T-RET Panel |  |  |  |
| 16 |  | 3 | Powerwave 7770 - Panel |  |  |  |
| 17 |  | 1 | KMW AM-X-CD-14-65-00T- Panel |  |  |  |
| 18 |  | 6 | Powerwave LGP21401 TMA |  |  |  |
| 19 |  | 3 | Ericsson RRUS-11-RRU |  |  |  |
| 20 |  | 1 | Raycap DC6-48-60-18-8F Surge |  |  |  |

## Proposed Carrier's Final Configuration of Antennas, Mounts and Transmission Lines

Information pertaining to the proposed carrier's final configuration of antennas and transmission lines was provided by SBA Communications Corp. The proposed antennas and lines are listed below.

| Items | Elevation (ft) | Qty. | Antenna Descriptions | Mount Type \& Qty. | Transmission Lines | Owner |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 178.0 | 6 | JMA MX06FRO660-03- Panel | Platform w/ Handrails <br> (3) 91900314 | (2) $15 / 8$ " Hybrid | Verizon |
| 2 |  | 3 | Samsung B5/B13 RRH BR04C |  |  |  |
| 3 |  | 3 | Samsung B2/B66A RRH BR049 |  |  |  |
| 4 |  | 1 | Raycap RRFDS-6627-PF48 |  |  |  |

See the attached coax layout for the line placement considered in the analysis.

## Analysis Results

The results of the structural analysis, performed for the wind and ice loading and antenna equipment as defined above, are summarized as the following:

|  | Pole shafts | Anchor <br> Bolts | Base Plate |
| :---: | :---: | :---: | :---: |
| Max. Usage: | $\mathbf{8 6 . 5 \%}$ | $\mathbf{7 8 . 0 \%}$ | $57.2 \%$ |
| Pass/Fail | Pass | Pass | Pass |

## Foundations

|  | Moment (Kip-Ft) | Shear (Kips) | Axial (Kips) |
| :---: | :---: | :---: | :---: |
| Analysis Reactions | 5490.3 | 45.8 | 69.8 |

The foundation has been investigated using the supplied documents and soils report and was found adequate. Therefore, no modification to the foundation will be required.

## Service Load Condition (Rigidity):

Operational characteristics of the tower are found to be within the limits prescribed by ANSI/TIA/EIA 222-H for the installed antennas. The maximum twist/sway at the elevation of the proposed equipment is 1.8668 degrees under the operational wind speed as specified in the Analysis Criteria.

## Conclusions

Based on the analysis results, the existing structure and its foundation were found to be adequate to safely support the existing and proposed equipment and meet the minimum requirements per the ANSI/TIA/EIA 222-H Standard under the design basic wind speed as specified in the Analysis Criteria.

## Standard Conditions

1. This analysis was performed based on the information supplied to (TES) Tower Engineering Solutions, LLC. Verification of the information provided was not included in the Scope of Work for TES. The accuracy of the analysis is dependent on the accuracy of the information provided.
2. The structural analysis was performance based upon the evidence available at the time of this report. All information provided by the client is considered to be accurate.
3. The analyses will be performed based on the codes as specified by the client or based on the best knowledge of the engineering staff of TES. In the absence of information to the contrary, all work will be performed in accordance with the latest relevant revision of ANSI/TIA-222. If wind speed and/or ice loads are different from the minimum values recommended by the ANSI/TIA-222 standard or other codes, TES should be notified in writing and the applicable minimum values provided by the client.
4. The configuration of the existing mounts, antennas, coax and other appurtenances were supplied by the customer for the current structural analysis. TES has not visited the tower site to verify the adequacy of the information provided. If there is any discrepancy found in the report regarding the existing conditions, TES should be notified immediately to evaluate the effect of the discrepancy on the analysis results.
5. The client will assume responsibility for rework associated with the differences in initially provided information, including tower and foundation information, existing and/or proposed equipment and transmission lines.
6. If a feasibility analysis was performed, final acceptance of changed conditions shall be based upon a rigorous structural analysis.

## Usage Diagram - Max Ratio $86.51 \%$ at 0.0 ft

| Structure: | CT46130-A-SBA | Code: | EIATIA-222-H | 12/5/2019 | ((1) 1 ) $)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Name: | Deep River-winthrop Rd | Exposure: | C |  | Ta |
| Height: | 180.00 (ft) | Gh: | 1.1 |  | EN |
| Base Elev: | 0.000 (t) |  |  | Page: 1 | Towt Engincerins Solutions |




| Type: | Tapered | Base Shape: 12 Sided | 12/5/2019 | ( (1H) ) |
| :---: | :---: | :---: | :---: | :---: |
| Site Name: | Deep River-winthrop Rd | Taper: 0.24800 |  |  |
| Height: | 180.00 (ft) |  |  | 1 |
| Base Elev: | 0.00 (ft) |  | Page: 2 | Tower Engincering Solutions |



## Structure: CT46130-A-SBA

| Type: | Tapered | Base Shape: | 12 Sided | 12/5/2019 |
| :--- | :--- | ---: | ---: | ---: |
| Site Name: | Deep River-winthrop Rd | Taper: | 0.24800 |  |
| Height: | $180.00(\mathrm{ft})$ |  |  |  |
| Base Elev: | $0.00(\mathrm{ft})$ |  | Page: 3 |  |


| Thickness <br> (in) | Specifications <br> (in) | Grade <br> (ksi) | Geometry |  |
| :--- | :---: | :---: | :---: | :---: |
| 2.7500 | 76.7 | 60.0 | Polygon |  |
| Reactions |  |  |  |  |
| Rement |  |  |  |  |
| Load Case | Shear | Axial |  |  |
| $1.2 \mathrm{D}+1.0 \mathrm{~W}$ 123 mph Wind | (FT-Kips) | (Kips) | (Kips) |  |
| $0.9 \mathrm{D}+1.0 \mathrm{~W}$ 123 mph Wind | 5490.3 | 45.8 | 56.5 |  |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind | 5425.5 | 45.8 | 42.3 |  |
| $1.2 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | 1165.4 | 9.6 | 69.8 |  |
| $0.9 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | 527.4 | 4.5 | 56.5 |  |
| $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind | 520.8 | 4.5 | 42.4 |  |

## Structure: CT46130-A-SBA - Coax Line Placement

Type:
Monopole
12/5/2019
Site Name: Deep River-winthrop Rd
Height: 180.00 (ft)
Page: 4


## Shaft Properties



| Sec. <br> No. | Shape | Length <br> (ft) | Thick <br> (in) | Fy <br> (ksi) | Joint <br> Type | Overlap <br> (in) | Weight <br> (lb) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 12 | 51.000 | 0.4375 | 65 |  | 0.00 | 13,505 |  |  |
| 2 | 12 | 52.083 | 0.4063 | 65 | Slip | 85.00 | 10,446 |  |  |
| 3 | 12 | 47.833 | 0.3438 | 65 | Slip | 70.00 | 6,281 |  |  |
| 4 | 12 | 46.667 | 0.2500 | 65 | Slip | 56.00 | 3,183 |  |  |
|  |  |  |  |  | Total Shaft Weight: |  |  |  | $\mathbf{3 3 , 4 1 4}$ |


|  | Bottom |  |  |  |  |  | Top |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sec. No. | Dia <br> (in) | Elev <br> (ft) | Area (sqin) | $\begin{gathered} l x \\ \left(i n^{\wedge} 4\right) \end{gathered}$ | W/t Ratio | D/t <br> Ratio | Dia <br> (in) | Elev <br> (ft) | Area (sqin) | $\begin{gathered} 1 \mathrm{x} \\ \left(\mathrm{in} n^{\wedge}\right) \\ \hline \end{gathered}$ | W/t Ratio | D/t Ratio | Taper |
| 1 | 62.00 | 0.00 | 86.73 | 41953.54 | 35.83 | 141.71 | 49.35 | 51.00 | 68.91 | 21044.2 | 28.08 | 112.8 | 0.248000 |
| 2 | 51.92 | 43.92 | 67.39 | 22826.23 | 32.10 | 127.81 | 39.00 | 96.00 | 50.49 | 9601.48 | 23.58 | 96.01 | 0.248000 |
| 3 | 41.14 | 90.17 | 45.15 | 9591.86 | 29.92 | 119.68 | 29.28 | 138.00 | 32.02 | 3421.62 | 20.68 | 85.17 | 0.248000 |
| 4 | 30.93 | 133.3 | 24.70 | 2968.17 | 31.01 | 123.73 | 19.36 | 180.00 | 15.38 | 717.07 | 18.61 | 77.44 | 0.248000 |

## Load Summary

| Structure: <br> Site Name: Height: <br> Base Elev: Gh: | CT46130-A |  |  | Code: | EIA/TIA-222-H | 12/5/2019 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Deep River | rop Rd |  | Exposure: | C |  |  |
|  | 180.00 (ft) |  |  | Crest Height: | 0.00 |  |  |
|  | 0.000 (ft) |  |  | Site Class: | D - Stiff Soil |  | -1 |
|  | 1.1 | Topography: | 1 | Struct Class: | II | Page: 6 | Tover Engincering Solutions |

## Discrete Appurtenances

| No. | Elev <br> (ft) |  |  | No lce |  |  | Ice |  |  | Hor. <br> Ecc. <br> (ft) | Vert Ecc <br> (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Description | Qty | Weight (lb) | $\begin{gathered} \text { CaAa } \\ (\mathrm{sf}) \end{gathered}$ | CaAa <br> Factor | Weight (lb) | CaAa (sf) | CaAa <br> Factor |  |  |
| 1 | 178.00 | JMA MX06FR0660-03 | 6 | 60.00 | 9.87 | 0.82 | 186.20 | 10.501 | 0.82 | 0.00 | 0.00 |
| 2 | 178.00 | Samsung B2/B66A RRH BR049 | 3 | 84.40 | 1.88 | 0.67 | 147.57 | 2.327 | 0.67 | 0.00 | 0.00 |
| 3 | 178.00 | Platform w/ Handrails w/ 91900314 | 1 | 2202.20 | 40.00 | 1.00 | 3375.10 | 50.652 | 1.00 | 0.00 | 0.00 |
| 4 | 178.00 | Sarnsung B5/B13 RRH BR04C | 3 | 70.30 | 2.22 | 0.67 | 99.75 | 2.535 | 0.67 | 0.00 | 0.00 |
| 5 | 178.00 | Raycap RRFDS-6627-PF48 | 1 | 32.00 | 2.61 | 1.00 | 69.76 | 2.937 | 1.00 | 0.00 | 0.00 |
| 6 | 166.00 | RFS APXVTM14-C-120 | 3 | 56.20 | 6.34 | 0.77 | 129.28 | 6.885 | 0.77 | 0.00 | 0.00 |
| 7 | 166.00 | Commscope NNVV-65B-R4 | 3 | 77.40 | 12.27 | 0.74 | 221.63 | 13.005 | 0.74 | 0.00 | 0.00 |
| 8 | 166.00 | ALU 1900 Mhz | 3 | 44.00 | 3.80 | 0.67 | 99.14 | 4.502 | 0.67 | 0.00 | 0.00 |
| 9 | 166.00 | ALU 800 Mhz | 6 | 53.00 | 2.49 | 0.50 | 90.36 | 3.068 | 0.50 | 0.00 | 0.00 |
| 10 | 166.00 | ALU TD-RRH8x20-25 | 3 | 70.00 | 4.05 | 0.67 | 120.20 | 4.444 | 0.67 | 0.00 | 0.00 |
| 11 | 166.00 | Sitepro | 1 | 230.00 | 6.70 | 1.00 | 392.20 | 10.244 | 1.00 | 0.00 | 0.00 |
| 12 | 166.00 | Sitepro | 1 | 406.61 | 7.00 | 1.00 | 650.34 | 10.456 | 1.00 | 0.00 | 0.00 |
| 13 | 166.00 | Platform w/ Hand Rails | 1 | 2000.00 | 40.00 | 1.00 | 3057.80 | 50.578 | 1.00 | 0.00 | 0.00 |
| 14 | 158.00 | T-Arms | 3 | 350.00 | 8.00 | 0.75 | 472.80 | 11.509 | 0.75 | 0.00 | 0.00 |
| 15 | 158.00 | EMS RR90-17-02DP | 6 | 13.50 | 7.34 | 0.68 | 84.72 | 7.931 | 0.68 | 0.00 | 0.00 |
| 16 | 158.00 | PCS1900 G3 TMA | 6 | 20.00 | 1.04 | 0.50 | 31.34 | 1.441 | 0.50 | 0.00 | 0.00 |
| 17 | 150.00 | Cci HPA-65R-BUU-H6 | 2 | 51.00 | 9.66 | 0.85 | 165.08 | 10.322 | 0.85 | 0.00 | 0.00 |
| 18 | 150.00 | SBNHH-1D65A | 1 | 33.50 | 5.88 | 1.00 | 104.86 | 6.402 | 1.00 | 0.00 | 0.00 |
| 19 | 150.00 | RRUS-32 | 3 | 77.00 | 3.87 | 0.67 | 128.08 | 3.695 | 0.67 | 0.00 | 0.00 |
| 20 | 150.00 | KMW AM-X-CD-16-65-00T | 2 | 48.50 | 8.02 | 0.75 | 129.64 | 9.417 | 0.75 | 0.00 | 0.00 |
| 21 | 150.00 | Powerwave 7770 | 3 | 35.00 | 5.51 | 0.73 | 95.06 | 6.017 | 0.73 | 0.00 | 0.00 |
| 22 | 150.00 | KMW AM-X-CD-14-65-00T | 1 | 36.40 | 7.05 | 1.00 | 92.16 | 8.371 | 1.00 | 0.00 | 0.00 |
| 23 | 150.00 | Powerwave LGP21401 TMA's | 6 | 14.10 | 1.22 | 0.50 | 26.60 | 1.615 | 0.50 | 0.00 | 0.00 |
| 24 | 150.00 | Ericsson RRUS-11 | 3 | 50.70 | 2.52 | 0.67 | 86.30 | 2.832 | 0.67 | 0.00 | 0.00 |
| 25 | 150.00 | Raycap DC6-48-60-18-8F | 1 | 31.80 | 1.81 | 0.67 | 62.71 | 2.241 | 0.67 | 0.00 | 0.00 |
| 26 | 150.00 | Platform w/ Hand Rail | 1 | 1600.00 | 35.00 | 1.00 | 2649.92 | 50.271 | 1.00 | 0.00 | 0.00 |
|  |  | Totals: | 73 | 10,480.11 |  |  | 18,359.04 |  |  |  |  |

## Linear Appurtenances

| Bottom <br> Elev. <br> (ft) | Top <br> Elev. <br> (ft) | Description | Exposed <br> Width | Exposed |
| :---: | :---: | :--- | :---: | :--- |
| 3.00 | 178.00 | $(2) 15 / 8^{\prime \prime}$ Hybrid | 0.00 | Inside |
| 3.00 | 166.00 | $(4) 1-1 / 4^{\prime \prime}$ Fiber | 0.00 | Inside |
| 3.00 | 158.00 | (6) $15 / 8^{\prime \prime}$ Coax | 0.00 | Inside |
| 3.00 | 150.00 | $(12) 11 / 4^{\prime \prime}$ Coax | 0.00 | Inside |
| 3.00 | 150.00 | $(1) 10$ mm Fiber | 0.00 | Inside |
| 3.00 | 150.00 | (2) 19.7 mm DC | 0.00 | Inside |
| 3.00 | 150.00 | (1) $3^{\prime \prime}$ Innerduct | 0.00 | Inside |

## Shaft Section Properties




## Increment Length: 2 (ft)

| Elev <br> (ft) | Description | Thick <br> (in) | Dia (in) | $\begin{gathered} \text { Area } \\ \left(i \eta^{\wedge} 2\right) \end{gathered}$ | $\begin{gathered} 1 x \\ \left(\operatorname{in}^{\wedge} 4\right) \end{gathered}$ | W/t Ratio | $\begin{gathered} \mathrm{D} / \mathrm{t} \\ \text { Ratio } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Fpy } \\ & \text { (ksi) } \end{aligned}$ | $\begin{gathered} \mathbf{5} \\ \left(\mathrm{in}^{\wedge} 3\right) \end{gathered}$ | Weight (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 94.00 |  | 0.4063 | 39.501 | 51.140 | 9976.4 | 23.91 | 97.23 | 78.6 | 487.9 | 652.3 |
| 96.00 | Top - Section 2 | 0.3438 | 39.692 | 43.554 | 8607.2 | 28.80 | 115.47 | 0.0 | 0.0 | 644.1 |
| 98.00 |  | 0.3438 | 39.196 | 43.005 | 8285.8 | 28.41 | 114.02 | 73.7 | 408.4 | 294.5 |
| 100.00 |  | 0.3438 | 38.700 | 42.456 | 7972.5 | 28.02 | 112.58 | 74.2 | 398.0 | 290.8 |
| 102.00 |  | 0.3438 | 38.204 | 41.907 | 7667.2 | 27.64 | 111.14 | 74.6 | 387.7 | 287.1 |
| 104.00 |  | 0.3438 | 37.708 | 41.358 | 7369.8 | 27.25 | 109.70 | 75.0 | 377.6 | 283.3 |
| 106.00 |  | 0.3438 | 37.212 | 40.809 | 7080.1 | 26.86 | 108.25 | 75.4 | 367.6 | 279.6 |
| 108.00 |  | 0.3438 | 36.716 | 40.260 | 6798.2 | 26.48 | 106.81 | 75.8 | 357.7 | 275.9 |
| 110.00 |  | 0.3438 | 36.220 | 39.711 | 6523.9 | 26.09 | 105.37 | 76.3 | 348.0 | 272.1 |
| 112.00 |  | 0.3438 | 35.724 | 39.162 | 6257.0 | 25.70 | 103.92 | 76.7 | 338.4 | 268.4 |
| 114.00 |  | 0.3438 | 35.228 | 38.613 | 5997.5 | 25.32 | 102.48 | 77.1 | 328.9 | 264.6 |
| 116.00 |  | 0.3438 | 34.732 | 38.063 | 5745.3 | 24.93 | 101.04 | 77.5 | 319.6 | 260.9 |
| 118.00 |  | 0.3438 | 34.236 | 37.514 | 5500.3 | 24.54 | 99.60 | 77.9 | 310.4 | 257.2 |
| 120.00 |  | 0.3438 | 33.740 | 36.965 | 5262.3 | 24.16 | 98.15 | 78.4 | 301.3 | 253.4 |
| 122.00 |  | 0.3438 | 33.244 | 36.416 | 5031.3 | 23.77 | 96.71 | 78.8 | 292.4 | 249.7 |
| 124.00 |  | 0.3438 | 32.748 | 35.867 | 4807.2 | 23.38 | 95.27 | 79.2 | 283.6 | 246.0 |
| 126.00 |  | 0.3438 | 32.252 | 35.318 | 4589.8 | 23.00 | 93.82 | 79.6 | 274.9 | 242.2 |
| 128.00 |  | 0.3438 | 31.756 | 34.769 | 4379.1 | 22.61 | 92.38 | 80.1 | 266.4 | 238.5 |
| 130.00 |  | 0.3438 | 31.260 | 34.220 | 4174.9 | 22.22 | 90.94 | 80.5 | 258.0 | 234.8 |
| 132.00 |  | 0.3438 | 30.764 | 33.671 | 3977.2 | 21.84 | 89.50 | 80.9 | 249.7 | 231.0 |
| 133.33 | Bot-Section 4 | 0.3438 | 30.433 | 33.305 | 3848.9 | 21.58 | 88.53 | 81.2 | 244.3 | 151.9 |
| 134.00 |  | 0.3438 | 30.268 | 33.122 | 3785.8 | 21.45 | 88.05 | 81.3 | 241.6 | 131.2 |
| 136.00 |  | 0.3438 | 29.772 | 32.573 | 3600.6 | 21.06 | 86.61 | 81.7 | 233.6 | 389.4 |
| 138.00 | Top - Section 3 | 0.2500 | 29.776 | 23.768 | 2644.8 | 29.77 | 119.10 | 0.0 | 0.0 | 382.9 |
| 140.00 |  | 0.2500 | 29.280 | 23.369 | 2513.8 | 29.24 | 117.12 | 72.8 | 165.9 | 160.4 |
| 142.00 |  | 0.2500 | 28.784 | 22.970 | 2387.1 | 28.71 | 115.14 | 73.4 | 160.2 | 157.7 |
| 144.00 |  | 0.2500 | 28.288 | 22.571 | 2264.8 | 28.18 | 113.15 | 74.0 | 154.7 | 155.0 |
| 146.00 |  | 0.2500 | 27.792 | 22.171 | 2146.7 | 27.64 | 111.17 | 74.6 | 149.2 | 152.2 |
| 148.00 |  | 0.2500 | 27.296 | 21.772 | 2032.8 | 27.11 | 109.18 | 75.1 | 143.9 | 149.5 |
| 150.00 |  | 0.2500 | 26.800 | 21.373 | 1923.0 | 26.58 | 107.20 | 75.7 | 138.6 | 146.8 |
| 152.00 |  | 0.2500 | 26.304 | 20.973 | 1817.2 | 26.05 | 105.22 | 76.3 | 133.5 | 144.1 |
| 154.00 |  | 0.2500 | 25.808 | 20.574 | 1715.4 | 25.52 | 103.23 | 76.9 | 128.4 | 141.4 |
| 156.00 |  | 0.2500 | 25.312 | 20.175 | 1617.4 | 24.99 | 101.25 | 77.5 | 123.4 | 138.7 |
| 158.00 |  | 0.2500 | 24.816 | 19.776 | 1523.3 | 24.45 | 99.26 | 78.0 | 118.6 | 135.9 |
| 160.00 |  | 0.2500 | 24.320 | 19.376 | 1432.9 | 23.92 | 97.28 | 78.6 | 113.8 | 133.2 |
| 162.00 |  | 0.2500 | 23.824 | 18.977 | 1346.1 | 23.39 | 95.30 | 79.2 | 109.2 | 130.5 |
| 164.00 |  | 0.2500 | 23.328 | 18.578 | 1262.9 | 22.86 | 93.31 | 79.8 | 104.6 | 127.8 |
| 166.00 |  | 0.2500 | 22.832 | 18.179 | 1183.2 | 22.33 | 91.33 | 80.4 | 100.1 | 125.1 |
| 168.00 |  | 0.2500 | 22.336 | 17.779 | 1107.0 | 21.80 | 89.34 | 80.9 | 95.7 | 122.4 |
| 170.00 |  | 0.2500 | 21.840 | 17.380 | 1034.0 | 21.26 | 87.36 | 81.5 | 91.5 | 119.6 |
| 172.00 |  | 0.2500 | 21.344 | 16.981 | 964.4 | 20.73 | 85.38 | 81.9 | 87.3 | 116.9 |
| 174.00 |  | 0.2500 | 20.848 | 16.581 | 898.0 | 20.20 | 83.39 | 81.9 | 83.2 | 114.2 |
| 176.00 |  | 0.2500 | 20.352 | 16.182 | 834.6 | 19.67 | 81.41 | 81.9 | 79.2 | 111.5 |
| 178.00 |  | 0.2500 | 19.856 | 15.783 | 774.4 | 19.14 | 79.42 | 81.9 | 75.3 | 108.8 |
| 180.00 |  | 0.2500 | 19.360 | 15.384 | 717.1 | 18.61 | 77.44 | 81.9 | 71.6 | 106.1 |

33413.9


| Elev (ft) | Kzt | Kz | $\begin{gathered} q z \\ \text { (psf) } \end{gathered}$ | $\begin{aligned} & \text { qzGh } \\ & \text { (psf) } \end{aligned}$ | $\begin{gathered} \text { C } \\ \text { (mph-ft) } \end{gathered}$ | Cf |  | Tributary (ft) | $\begin{aligned} & \mathrm{Aa} \\ & \text { (sf) } \end{aligned}$ | CfAa (sf) | Wind Force X <br> (lb) | Dead Load Ice (lb) | Tot Dead Load (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 1.00 | 0.85 | 31.009 | 34.11 | 603.99 | 0.950 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 2.00 | 1.00 | 0.85 | 31.009 | 34.11 | 599.16 | 0.950 | 0.000 | 2.00 | 10.655 | 10.12 | 345.3 | 0.0 | 705.4 |
| 4.00 | 1.00 | 0.85 | 31.009 | 34.11 | 594.33 | 0.950 | 0.000 | 2.00 | 10.569 | 10.04 | 342.5 | 0.0 | 699.7 |
| 6.00 | 1.00 | 0.85 | 31.009 | 34.11 | 589.49 | 0.950 | 0.000 | 2.00 | 10.484 | 9.96 | 339.7 | 0.0 | 694.0 |
| 8.00 | 1.00 | 0.85 | 31.009 | 34.11 | 584.66 | 0.950 | 0.000 | 2.00 | 10.398 | 9.88 | 337.0 | 0.0 | 688.3 |
| 10.00 | 1.00 | 0.85 | 31.009 | 34.11 | 579.83 | 0.950 | 0.000 | 2.00 | 10.313 | 9.80 | 334.2 | 0.0 | 682.6 |
| 12.00 | 1.00 | 0.85 | 31.009 | 34.11 | 575.00 | 0.950 | 0.000 | 2.00 | 10.227 | 9.72 | 331.4 | 0.0 | 676.9 |
| 14.00 | 1.00 | 0.85 | 31.009 | 34.11 | 570.17 | 0.950 | 0.000 | 2.00 | 10.142 | 9.63 | 328.6 | 0.0 | 671.2 |
| 16.00 | 1.00 | 0.86 | 31.392 | 34.53 | 568.81 | 0.950 | 0.000 | 2.00 | 10.056 | 9.55 | 329.9 | 0.0 | 665.5 |
| 18.00 | 1.00 | 0.88 | 32.180 | 35.40 | 570.99 | 0.950 | 0.000 | 2.00 | 9.970 | 9.47 | 335.3 | 0.0 | 659.8 |
| 20.00 | 1.00 | 0.90 | 32.902 | 36.19 | 572.38 | 0.950 | 0.000 | 2.00 | 9.885 | 9.39 | 339.9 | 0.0 | 654.1 |
| 22.00 | 1.00 | 0.92 | 33.569 | 36.93 | 573.12 | 0.950 | 0.000 | 2.00 | 9.799 | 9.31 | 343.8 | 0.0 | 648.3 |
| 24.00 | 1.00 | 0.94 | 34.189 | 37.61 | 573.32 | 0.950 | 0.000 | 2.00 | 9.714 | 9.23 | 347.0 | 0.0 | 642.6 |
| 26.00 | 1.00 | 0.95 | 34.770 | 38.25 | 573.06 | 0.950 | 0.000 | 2.00 | 9.628 | 9.15 | 349.8 | 0.0 | 636.9 |
| 28.00 | 1.00 | 0.97 | 35.317 | 38.85 | 572.39 | 0.950 | 0.000 | 2.00 | 9.542 | 9.07 | 352.2 | 0.0 | 631.2 |
| 30.00 | 1.00 | 0.98 | 35.834 | 39.42 | 571.37 | 0.950 | 0.000 | 2.00 | 9.457 | 8.98 | 354.1 | 0.0 | 625.5 |
| 32.00 | 1.00 | 1.00 | 36.324 | 39.96 | 570.03 | 0.950 | 0.000 | 2.00 | 9.371 | 8.90 | 355.7 | 0.0 | 619.8 |
| 34.00 | 1.00 | 1.01 | 36.791 | 40.47 | 568.42 | 0.950 | 0.000 | 2.00 | 9.286 | 8.82 | 357.0 | 0.0 | 614.1 |
| 36.00 | 1.00 | 1.02 | 37.236 | 40.96 | 566.55 | 0.950 | 0.000 | 2.00 | 9.200 | 8.74 | 358.0 | 0.0 | 608.4 |
| 38.00 | 1.00 | 1.03 | 37.662 | 41.43 | 564.46 | 0.950 | 0.000 | 2.00 | 9.115 | 8.66 | 358.7 | 0.0 | 602.7 |
| 40.00 | 1.00 | 1.04 | 38.071 | 41.88 | 562.16 | 0.950 | 0.000 | 2.00 | 9.029 | 8.58 | 359.2 | 0.0 | 597.0 |
| 42.00 | 1.00 | 1.05 | 38.464 | 42.31 | 559.68 | 0.950 | 0.000 | 2.00 | 8.943 | 8.50 | 359.5 | 0.0 | 591.3 |
| 43.92 Bot - Section 2 | 1.00 | 1.06 | 38.827 | 42.71 | 557.13 | 0.950 | 0.000 | 1.92 | 8.490 | 8.07 | 344.5 | 0.0 | 561.3 |
| 44.00 | 1.00 | 1.06 | 38.843 | 42.73 | 557.02 | 0.950 | 0.000 | 0.08 | 0.373 | 0.35 | 15.1 | 0.0 | 47.2 |
| 46.00 | 1.00 | 1.07 | 39.208 | 43.13 | 554.19 | 0.950 | 0.000 | 2.00 | 8.912 | 8.47 | 365.2 | 0.0 | 1127.3 |
| 48.00 | 1.00 | 1.08 | 39.561 | 43.52 | 551.23 | 0.950 | 0.000 | 2.00 | 8.827 | 8.39 | 364.9 | 0.0 | 1116.3 |
| 50.00 | 1.00 | 1.09 | 39.902 | 43.89 | 548.12 | 0.950 | 0.000 | 2.00 | 8.741 | 8.30 | 364.5 | 0.0 | 1105.3 |
| 51.00 Top - Section 1 | 1.00 | 1.10 | 40.069 | 44.08 | 546.52 | 0.950 | 0.000 | 1.00 | 4.339 | 4.12 | 181.7 | 0.0 | 548.5 |
| 52.00 | 1.00 | 1.10 | 40.233 | 44.26 | 553.90 | 0.950 | 0.000 | 1.00 | 4.317 | 4.10 | 181.5 | 0.0 | 265.1 |
| 54.00 | 1.00 | 1.11 | 40.554 | 44.61 | 550.58 | 0.950 | 0.000 | 2.00 | 8.570 | 8.14 | 363.2 | 0.0 | 526.3 |
| 56.00 | 1.00 | 1.12 | 40.866 | 44.95 | 547.14 | 0.950 | 0.000 | 2.00 | 8.485 | 8.06 | 362.3 | 0.0 | 521.0 |
| 58.00 | 1.00 | 1.13 | 41.169 | 45.29 | 543.60 | 0.950 | 0.000 | 2.00 | 8.399 | 7.98 | 361.3 | 0.0 | 515.7 |
| 60.00 | 1.00 | 1.14 | 41.464 | 45.61 | 539.95 | 0.950 | 0.000 | 2.00 | 8.313 | 7.90 | 360.2 | 0.0 | 510.4 |
| 62.00 | 1.00 | 1.14 | 41.751 | 45.93 | 536.21 | 0.950 | 0.000 | 2.00 | 8.228 | 7.82 | 359.0 | 0.0 | 505.1 |
| 64.00 | 1.00 | 1.15 | 42.031 | 46.23 | 532.38 | 0.950 | 0.000 | 2.00 | 8.142 | 7.74 | 357.6 | 0.0 | 499.8 |
| 66.00 | 1.00 | 1.16 | 42.304 | 46.53 | 528.47 | 0.950 | 0.000 | 2.00 | 8.057 | 7.65 | 356.2 | 0.0 | 494.5 |
| 68.00 | 1.00 | 1.17 | 42.571 | 46.83 | 524.47 | 0.950 | 0.000 | 2.00 | 7.971 | 7.57 | 354.6 | 0.0 | 489.2 |
| 70.00 | 1.00 | 1.17 | 42.831 | 47.11 | 520.39 | 0.950 | 0.000 | 2.00 | 7.885 | 7.49 | 352.9 | 0.0 | 483.9 |
| 72.00 | 1.00 | 1.18 | 43.086 | 47.39 | 516.24 | 0.950 | 0.000 | 2.00 | 7.800 | 7.41 | 351.2 | 0.0 | 478.6 |
| 74.00 | 1.00 | 1.19 | 43.335 | 47.67 | 512.02 | 0.950 | 0.000 | 2.00 | 7.714 | 7.33 | 349.3 | 0.0 | 473.3 |
| 76.00 | 1.00 | 1.19 | 43.579 | 47.94 | 507.73 | 0.950 | 0.000 | 2.00 | 7.629 | 7.25 | 347.4 | 0.0 | 468.0 |
| 78.00 | 1.00 | 1.20 | 43.818 | 48.20 | 503.38 | 0.950 | 0.000 | 2.00 | 7.543 | 7.17 | 345.4 | 0.0 | 462.7 |
| 80.00 | 1.00 | 1.21 | 44.053 | 48.46 | 498.96 | 0.950 | 0.000 | 2.00 | 7.458 | 7.08 | 343.3 | 0.0 | 457.4 |
| 82.00 | 1.00 | 1.21 | 44.282 | 48.71 | 494.49 | 0.950 | 0.000 | 2.00 | 7.372 | 7.00 | 341.1 | 0.0 | 452.1 |
| 84.00 | 1.00 | 1.22 | 44.507 | 48.96 | 489.96 | 0.950 | 0.000 | 2.00 | 7.286 | 6.92 | 338.9 | 0.0 | 446.8 |
| 86.00 | 1.00 | 1.23 | 44.728 | 49.20 | 485.37 | 0.950 | 0.000 | 2.00 | 7.201 | 6.84 | 336.6 | 0.0 | 441.5 |
| 88.00 | 1.00 | 1.23 | 44.945 | 49.44 | 480.73 | 0.950 | 0.000 | 2.00 | 7.115 | 6.76 | 334.2 | 0.0 | 436.2 |

## Wind Loading - Shaft



## Discrete Appurtenance Forces



## Total Applied Force Summary



| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{~W} 123 \mathrm{mph}$ Wind | 1 | Iterations | 29 |
| :---: | :---: | :---: | :---: |
| Dead Load Factor 1.20 |  |  |  |
| Wind Load Factor 1.00 |  |  |  |


| $\begin{gathered} \text { Elev } \\ \text { (ft) } \end{gathered}$ | Description | Lateral <br> FX (-) <br> (b) | Axial FY (-) <br> (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 |
| 2.00 |  | 345.27 | 705.41 | 0.00 | 0.00 |
| 4.00 |  | 342.50 | 724.29 | 0.00 | 0.00 |
| 6.00 |  | 339.73 | 743.16 | 0.00 | 0.00 |
| 8.00 |  | 336.95 | 737.46 | 0.00 | 0.00 |
| 10.00 |  | 334.18 | 731.75 | 0.00 | 0.00 |
| 12.00 |  | 331.41 | 726.05 | 0.00 | 0.00 |
| 14.00 |  | 328.63 | 720.34 | 0.00 | 0.00 |
| 16.00 |  | 329.88 | 714.63 | 0.00 | 0.00 |
| 18.00 |  | 335.29 | 708.93 | 0.00 | 0.00 |
| 20.00 |  | 339.86 | 703.22 | 0.00 | 0.00 |
| 22.00 |  | 343.75 | 697.51 | 0.00 | 0.00 |
| 24.00 |  | 347.05 | 691.81 | 0.00 | 0.00 |
| 26.00 |  | 349.84 | 686.10 | 0.00 | 0.00 |
| 28.00 |  | 352.18 | 680.39 | 0.00 | 0.00 |
| 30.00 |  | 354.13 | 674.69 | 0.00 | 0.00 |
| 32.00 |  | 355.72 | 668.98 | 0.00 | 0.00 |
| 34.00 |  | 357.00 | 663.27 | 0.00 | 0.00 |
| 36.00 |  | 357.99 | 657.57 | 0.00 | 0.00 |
| 38.00 |  | 358.72 | 651.86 | 0.00 | 0.00 |
| 40.00 |  | 359.21 | 646.16 | 0.00 | 0.00 |
| 42.00 |  | 359.48 | 640.45 | 0.00 | 0.00 |
| 43.92 |  | 344.50 | 608.41 | 0.00 | 0.00 |
| 44.00 |  | 15.15 | 49.26 | 0.00 | 0.00 |
| 46.00 |  | 365.16 | 1176.50 | 0.00 | 0.00 |
| 48.00 |  | 364.91 | 1165.50 | 0.00 | 0.00 |
| 50.00 |  | 364.49 | 1154.49 | 0.00 | 0.00 |
| 51.00 |  | 181.66 | 573.12 | 0.00 | 0.00 |
| 52.00 |  | 181.51 | 289.71 | 0.00 | 0.00 |
| 54.00 |  | 363.19 | 575.44 | 0.00 | 0.00 |
| 56.00 |  | 362.33 | 570.14 | 0.00 | 0.00 |
| 58.00 |  | 361.33 | 564.84 | 0.00 | 0.00 |
| 60.00 |  | 360.21 | 559.54 | 0.00 | 0.00 |
| 62.00 |  | 358.98 | 554.24 | 0.00 | 0.00 |
| 64.00 |  | 357.62 | 548.94 | 0.00 | 0.00 |
| 66.00 |  | 356.16 | 543.64 | 0.00 | 0.00 |
| 68.00 |  | 354.60 | 538.34 | 0.00 | 0.00 |
| 70.00 |  | 352.94 | 533.05 | 0.00 | 0.00 |
| 72.00 |  | 351.19 | 527.75 | 0.00 | 0.00 |
| 74.00 |  | 349.34 | 522.45 | 0.00 | 0.00 |
| 76.00 |  | 347.41 | 517.15 | 0.00 | 0.00 |
| 78.00 |  | 345.40 | 511.85 | 0.00 | 0.00 |
| 80.00 |  | 343.31 | 506.55 | 0.00 | 0.00 |
| 82.00 |  | 341.14 | 501.25 | 0.00 | 0.00 |
| 84.00 |  | 338.89 | 495.95 | 0.00 | 0.00 |
| 86.00 |  | 336.57 | 490.66 | 0.00 | 0.00 |
| 88.00 |  | 334.19 | 485.36 | 0.00 | 0.00 |

## Total Applied Force Summary



| Structure: | CT46130-A |  |  | Code: | EIA/TIA-222-H | 12/5/2019 | ((1) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Name: | Deep River | rop Rd |  | Exposure: | C |  | ((1) |
| Height: | 180.00 (ft) |  |  | Crest Height: | 0.00 |  | H |
| Base Elev: | 0.000 (ft) |  |  | Site Class: | D - Stiff Soil |  |  |
| Gh: | 1.1 | Topography: | 1 | Struct Class: | 11 | Page: 14 | Tower Engincering Solutions |


| Load Case: 1.2D + 1.0W 123 mph Wind |  | \% | Iterations | 29 |
| :---: | :---: | :---: | :---: | :---: |
| Dead Load Factor | 1.20 |  |  |  |
| Wind Load Factor | 1.00 |  |  |  |


| Seg <br> Elev <br> (ft) | Pu $\mathrm{FY}(-)$ <br> (kips) | $\underset{\substack{\text { FX } \\ \text { (kios) } \\ \text { ( } \\ \hline}}{ }$ | $\begin{gathered} \mathrm{Tu} \\ \text { MY (-) } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{aligned} & \mathbf{M u} \\ & \mathbf{M Z} \end{aligned}$ <br> (ft-kips) | $\begin{gathered} \text { Mu } \\ \text { MX } \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (dea) | $\begin{gathered} \text { Stress } \\ \text { Ratio } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -56.46 | -45.76 | 0.00 | -5490.3 | 0.00 | 5490.30 | 5123.29 | 1522.04 | 7808.40 | 6435.29 | 0.00 | 0.000 | 0.000 | 0.865 |
| 2.00 | -55.69 | -45.49 | 0.00 | -5398.7 | 0.00 | 5398.78 | 5107.67 | 1509.78 | 7683.09 | 6363.61 | 0.02 | -0.074 | 0.000 | 0.860 |
| 4.00 | -54.91 | -45.21 | 0.00 | -5307.8 | 0.00 | 5307.81 | 5091.62 | 1497.52 | 7558.79 | 6291.73 | 0.06 | -0.148 | 0.000 | 0.855 |
| 6.00 | -54.11 | -44.94 | 0.00 | -5217.3 | 0.00 | 5217.39 | 5075.16 | 1485.26 | 7435.50 | 6219.67 | 0.14 | -0.223 | 0.000 | 0.850 |
| 8.00 | -53.32 | -44.67 | 0.00 | -5127.5 | 0.00 | 5127.50 | 5058.29 | 1472.99 | 7313.22 | 6147.44 | 0.25 | -0.299 | 0.000 | 0.846 |
| 10.00 | -52.53 | -44.40 | 0.00 | -5038.1 | 0.00 | 5038.16 | 5041.00 | 1460.73 | 7191.96 | 6075.05 | 0.39 | -0.375 | 0.000 | 0.841 |
| 12.00 | -51.74 | -44.1 | 0.00 | -4949.3 | 0.00 | 4949.35 | 5023.29 | 1448.47 | 7071.72 | 6002.51 | 0.57 | -0.451 | 0.000 | . 836 |
| 14.00 | -50.97 | -43.87 | 0.00 | -4861.0 | 0.00 | 4861.08 | 5005.16 | 1436.20 | 6952.48 | 5929.84 | 0.77 | -0.529 | 0.000 | 0.831 |
| 16.00 | -50.20 | -43.60 | 0.00 | -4773.3 | 0.00 | 4773.33 | 4986.62 | 1423.94 | 6834.27 | 5857.05 | 1.01 | -0.606 | 0.000 | 0.826 |
| 18.00 | -49.43 | -43.33 | 0.00 | -4686.1 | 0.00 | 4686.13 | 4967.66 | 1411.68 | 6717.06 | 5784.16 | 1.28 | -0.685 | 0.000 | 0.821 |
| 20.00 | -48.67 | -43.05 | 0.00 | -4599.4 | 0.00 | 4599.47 | 4948.29 | 1399.42 | 6600.87 | 5711.17 | 1.59 | -0.764 | 0.000 | 0.816 |
| 22.00 | -47.92 | -42.76 | 0.00 | -4513.3 | 0.00 | 4513.38 | 4928.49 | 1387.15 | 6485.69 | 5638.10 | 1.93 | -0.843 | 0.000 | 11 |
| 24.00 | -47.18 | -42.47 | 0.00 | 4427.8 | 0.00 | 4427.86 | 4908.28 | 1374.89 | 6371.53 | 5564.95 | 2.30 | -0.923 | 0.000 | 0.806 |
| 26.00 | -46.44 | -42.17 | 0.00 | -4342.9 | 0.00 | 4342.93 | 4887.66 | 1362.63 | 6258.37 | 5491.76 | 2.70 | -1.004 | 0.000 | 0.801 |
| 28.00 | -45.70 | -41.87 | 0.00 | -4258.5 | 0.00 | 4258.59 | 4866.62 | 1350.36 | 6146.24 | 5418.52 | 3.14 | -1.085 | 0.000 | 0.796 |
| 30.00 | -44.98 | -41.57 | 0.00 | -4174.8 | 0.00 | 4174.84 | 4845.16 | 1338.10 | 6035.11 | 5345.24 | . 61 | -1.167 | . 000 | . 791 |
| 32.00 | -44.25 | -41.26 | 0.00 | -4091.7 | 0.00 | 4091.70 | 4823.28 | 1325.84 | 5925.00 | 5271.95 | 4.12 | -1.250 | 0.000 | 0.786 |
| 34 | -43.54 | -40.96 | 0.00 | -4009. | 0.00 | 4009.17 | 4800.99 | 1313.58 | 5815.91 | 5198.66 | 66 | -1.333 | 0.000 | 0.781 |
| 36.00 | -42.83 | -40.65 | 0.00 | -3927.2 | 0.00 | 3927.26 | 4778.28 | 1301.31 | 5707.83 | 5125.37 | 5.24 | -1.416 | 0.000 | 0.776 |
| 38.00 | -42.13 | -40.33 | 0.00 | -3845.9 | 0.00 | 3845.97 | 4755.15 | 1289.05 | 5600.76 | 5052.10 | 5.85 | -1.501 | 0.000 | 0.771 |
| 40.00 | -41.43 | -40.02 | 0.00 | -3765. | 0.00 | 3765.31 | 4731.61 | 1276.79 | 5494.70 | 4978.87 | 6.50 | -1.586 | 0.000 | 0.766 |
| 42.00 | -40.75 | -39.70 | 0.00 | -3685.2 | 0.00 | 3685.27 | 4707.65 | 1264.52 | 5389.66 | 4905.68 | 7.18 | -1.671 | 0.000 | 0.761 |
| 43.92 | -40.12 | -39.37 | 0.00 | -3609. | 0.00 | 3609.18 | 4684.30 | 1252.77 | 5289.95 | 4835.60 | 7.87 | -1.754 | 0.000 | 0.756 |
| 44.00 | -40.04 | -39.38 | 0.00 | -3605.9 | 0.00 | 3605.90 | 4683.27 | 1252.26 | 5285.64 | 4832.55 | 7.90 | -1.758 | 0.000 | 0.756 |
| 46.00 | -38.81 | -39.0 | 0.00 | 3527.1 | 0.00 | 3527.14 | 4658.48 | 1240.00 | 5182.62 | 4759.49 | 8.65 | -1.844 | 0.000 | 0.750 |
| 48.00 | -37.60 | -38.69 | 0.00 | -3449.0 | O | 3449.06 | 4633.27 | 1227.74 | 5080.62 | 4686.52 | 9.45 | -1.932 | 0.000 | 0.745 |
| 50.00 | -36.42 | -38.33 | 0.00 | -3371.6 | 0.00 | 3371.67 | 4607.64 | 1215.47 | 4979.64 | 4613.64 | 10.27 | -2.020 | 0.000 | 0.740 |
| 51.00 | -35.82 | -38.16 | 0.00 | -3333.3 | 0.00 | 3333.34 | 4157.28 | 1142.33 | 4736.69 | 4216.21 | 10.70 | -2.065 | 0.000 | 0.800 |
| 52.00 | -35.49 | -38.01 | 0.00 | -3295.1 | 0.00 | 3295.18 | 4146.96 | 1136.64 | 4689.60 | 4184.61 | 11.14 | -2.110 | 0.000 | 0.797 |
| 54.00 | -34.87 | -37.68 | 0.00 | -3219. | 0.00 | 3219.17 | 4126.01 | 1125.25 | 4596.10 | 4121.41 | 12.04 | -2.201 | 0.000 | 0.791 |
| 56.00 | -34.26 | -37.35 | 0.00 | -3143.8 | 0.00 | 3143.81 | 4104.64 | 1113.86 | 4503.55 | 4058.23 | 12.99 | -2.293 | 0.000 | 0.784 |
| 58.00 | -33.65 | -37.02 | 0.00 | -3069.1 | 0.00 | 3069.11 | 4082.85 | 1102.48 | 4411.95 | 3995.08 | 13.97 | -2.386 | 0.000 | 0.778 |
| 60.00 | -33.04 | -36.69 | 0.00 | -2995.0 | 00 | 2995.07 | 4060.64 | 1091.09 | 4321.28 | 3931.97 | 14.99 | -2.479 | 0.000 | 0.771 |
| 62.00 | -32.44 | -36.36 | 0.00 | -2921.6 | 0.00 | 2921.68 | 4038.02 | 1079.70 | 4231.55 | 3868.91 | 16.05 | -2.573 | 0.000 | 0.764 |
| 64.00 | -31.85 | -36.03 | 0.00 | -2848.9 | 0.00 | 2848.96 | 4014.98 | 1068.31 | 4142.77 | 3805.92 | 17.14 | -2.668 | 0.000 | 0.758 |
| 66.00 | -31.27 | -35.70 | 0.00 | -2776.8 | 0.00 | 2776.89 | 3991.52 | 1056.93 | 4054.92 | 3743.01 | 18.28 | -2.763 | 0.000 | 0.751 |
| 68.00 | -30.69 | -35.37 | 0.00 | -2705.4 | 0.00 | 2705.49 | 3967.65 | 1045.54 | 3968.02 | 3680.19 | 19.46 | -2.858 | 0.000 | 0.744 |
| 70.00 | -30.11 | -35.05 | 0.00 | -2634.7 | 0.00 | 2634 | 3943.36 | 1034.15 | 3882.06 | 3617.47 | 20.68 | -2.955 | 0.000 | 0.737 |
| 72.00 | -29.55 | -34.72 | 0.00 | -2564.6 | 0.00 | 2564.65 | 3918.66 | 1022.77 | 3797.04 | 3554.87 | 21.94 | -3.052 | 0.000 | 0.730 |
| 74.00 | -28.99 | -34.39 | 0.00 | -2495.2 | 0.00 | 2495.22 | 3893.54 | 1011.38 | 3712.96 | 3492.40 | 23.23 | -3.149 | 0.000 | 0.723 |
| 76.00 | -28.43 | -34.06 | 0.00 | -2426.4 | 0.00 | 2426.44 | 3868.00 | 999.99 | 3629.83 | 3430.07 | 24.57 | -3.247 | 0.000 | 0.716 |
| 78.00 | -27.88 | -33.74 | 0.00 | -2358.3 | 0.00 | 2358.32 | 3842.04 | 988.61 | 3547.63 | 3367.90 | 25.96 | -3.346 | 0.000 | 0.709 |
| 80.00 | -27.34 | -33.41 | 0.00 | -2290.8 | 0.00 | 2290.84 | 3815.67 | 977.22 | 3466.38 | 3305.90 | 27.38 | -3.445 | 0.000 | 0.701 |
| 82.00 | -26.80 | -33.09 | 0.00 | -2224.0 | 0.00 | 2224.02 | 3788.88 | 965.83 | 3386.07 | 3244.07 | 28.84 | -3.545 | 0.000 | 0.694 |
| 84.00 | -26.27 | -32.76 | 0.00 | -2157.8 | 0.00 | 2157.85 | 3761.67 | 954.44 | 3306.69 | 3182.44 | 30.35 | -3.645 | 0.000 | 0.686 |
| 86.00 | -25.74 | -32.44 | 0.00 | -2092.3 | 0.00 | 2092.32 | 3734.05 | 943.06 | 3228.26 | 3121.02 | 31.90 | -3.746 | 0.000 | 0.678 |
| 88.00 | -25.22 | -32.12 | 0.00 | -2027.4 | 0.00 | 2027.44 | 3706.01 | 931.67 | 3150.77 | 3059.82 | 33.49 | -3.847 | 0.000 | 0.671 |
| 90.00 | -24.74 | -31.78 | 0.00 | -1963.1 | 0.00 | 1963.19 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 35.12 | -3.949 | 0.000 | 0.663 |

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## Calculated Forces




## Wind Loading - Shaft

| Structure: CT46130-A <br> Site Name: Deep River- <br> Height: 180.00 (ft) <br> Base Elev: 0.000 (ft) <br> Gh: 1.1 |  | Topography | 1 | Code: Exposure: Crest Height: Site Class: Struct Class: |  |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | $12 / 5 / 2019$ <br> Page: 17 |  | Tower Enginecring Solutions |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.00 | 1.00 | 1.2445 .159 | 49.67 | 476.03 | 0.950 | 0.000 | 2.00 | 7.030 | 6.68 | 331.7 | 0.0 | 323.2 |
| 90.17 Bot - Section 3 | 1.00 | 1.2445 .176 | 49.69 | 475.64 | 0.950 | 0.000 | 0.17 | 0.582 | 0.55 | 27.5 | 0.0 | 26.8 |
| 92.00 | 1.00 | 1.2445 .368 | 49.90 | 471.29 | 0.950 | 0.000 | 1.83 | 6.471 | 6.15 | 306.8 | 0.0 | 544.6 |
| 94.00 | 1.00 | 1.2545 .574 | 50.13 | 466.50 | 0.950 | 0.000 | 2.00 | 6.977 | 6.63 | 332.3 | 0.0 | 587.0 |
| 96.00 Top - Section 2 | 1.00 | 1.2545 .776 | 50.35 | 461.67 | 0.950 | 0.000 | 2.00 | 6.891 | 6.55 | 329.7 | 0.0 | 579.7 |
| 98.00 | 1.00 | 1.2645 .975 | 50.57 | 464.94 | 0.950 | 0.000 | 2.00 | 6.806 | 6.47 | 327.0 | 0.0 | 265.1 |
| 100.00 | 1.00 | 1.2746 .171 | 50.79 | 460.03 | 0.950 | 0.000 | 2.00 | 6.720 | 6.38 | 324.2 | 0.0 | 261.7 |
| 102.00 | 1.00 | 1.2746 .364 | 51.00 | 455.09 | 0.950 | 0.000 | 2.00 | 6.635 | 6.30 | 321.5 | 0.0 | 258.4 |
| 104.00 | 1.00 | 1.2846 .554 | 51.21 | 450.10 | 0.950 | 0.000 | 2.00 | 6.549 | 6.22 | 318.6 | 0.0 | 255.0 |
| 106.00 | 1.00 | 1.2846 .741 | 51.42 | 445.07 | 0.950 | 0:000 | 2.00 | 6.464 | 6.14 | 315.7 | 0.0 | 251.6 |
| 108.00 | 1.00 | 1.2946 .926 | 51.62 | 440.00 | 0.950 | 0.000 | 2.00 | 6.378 | 6.06 | 312.8 | 0.0 | 248.3 |
| 110.00 | 1.00 | 1.2947 .107 | 51.82 | 434.90 | 0.950 | 0.000 | 2.00 | 6.292 | 5.98 | 309.8 | 0.0 | 244.9 |
| 112.00 | 1.00 | 1.3047 .286 | 52.01 | 429.75 | 0.950 | 0.000 | 2.00 | 6.207 | 5.90 | 306.7 | 0.0 | 241.5 |
| 114.00 | 1.00 | 1.3047 .463 | 52.21 | 424.58 | 0.950 | 0.000 | 2.00 | 6.121 | 5.82 | 303.6 | 0.0 | 238.2 |
| 116.00 | 1.00 | 1.3147 .637 | 52.40 | 419.37 | 0.950 | 0.000 | 2.00 | 6.036 | 5.73 | 300.5 | 0.0 | 234.8 |
| 118.00 | 1.00 | 1.3147 .809 | 52.59 | 414.12 | 0.950 | 0.000 | 2.00 | 5.950 | 5.65 | 297.3 | 0.0 | 231.5 |
| 120.00 | 1.00 | 1.3247 .978 | 52.78 | 408.85 | 0.950 | 0.000 | 2.00 | 5.864 | 5.57 | 294.0 | 0.0 | 228.1 |
| 122.00 | 1.00 | 1.3248 .145 | 52.96 | 403.54 | 0.950 | 0.000 | 2.00 | 5.779 | 5.49 | 290.7 | 0.0 | 224.7 |
| 124.00 | 1.00 | 1.3248 .310 | 53.14 | 398.20 | 0.950 | 0.000 | 2.00 | 5.693 | 5.41 | 287.4 | 0.0 | 221.4 |
| 126.00 | 1.00 | 1.3348 .473 | 53.32 | 392.83 | 0.950 | 0.000 | 2.00 | 5.608 | 5.33 | 284.1 | 0.0 | 218.0 |
| 128.00 | 1.00 | 1.3348 .634 | 53.50 | 387.43 | 0.950 | 0.000 | 2.00 | 5.522 | 5.25 | 280.7 | 0.0 | 214.6 |
| 130.00 | 1.00 | 1.3448 .793 | 53.67 | 382.00 | 0.950 | 0.000 | 2.00 | 5.437 | 5.16 | 277.2 | 0.0 | 211.3 |
| 132.00 | 1.00 | 1.3448 .950 | 53.85 | 376.54 | 0.950 | 0.000 | 2.00 | 5.351 | 5.08 | 273.7 | 0.0 | 207.9 |
| 133.33 Bot-Section 4 | 1.00 | 1.3449 .054 | 53.96 | 372.89 | 0.950 | 0.000 | 1.33 | 3.520 | 3.34 | 180.4 | 0.0 | 136.7 |
| 134.00 | 1.00 | 1.3549 .106 | 54.02 | 371.06 | 0.950 | 0.000 | 0.67 | 1.774 | 1.69 | 91.1 | 0.0 | 118.1 |
| 136.00 | 1.00 | 1.3549 .259 | 54.19 | 365.55 | 0.950 | 0.000 | 2.00 | 5.266 | 5.00 | 271.1 | 0.0 | 350.4 |
| 138.00 Top - Section 3 | 1.00 | 1.3549 .411 | 54.35 | 360.01 | 0.950 | 0.000 | 2.00 | 5.181 | 4.92 | 267.5 | 0.0 | 344.6 |
| 140.00 | 1.00 | 1.3649 .561 | 54.52 | 360.61 | 0.950 | 0.000 | 2.00 | 5.095 | 4.84 | 263.9 | 0.0 | 144.4 |
| 142.00 | 1.00 | 1.3649 .709 | 54.68 | 355.03 | 0.950 | 0.000 | 2.00 | 5.009 | 4.76 | 260.2 | 0.0 | 141.9 |
| 144.00 | 1.00 | 1.3749 .855 | 54.84 | 349.42 | 0.950 | 0.000 | 2.00 | 4.924 | 4.68 | 256.5 | 0.0 | 139.5 |
| 146.00 | 1.00 | 1.3750 .000 | 55.00 | 343.80 | 0.950 | 0.000 | 2.00 | 4.838 | 4.60 | 252.8 | 0.0 | 137.0 |
| 148.00 | 1.00 | 1.3750 .144 | 55.16 | 338.14 | 0.950 | 0.000 | 2.00 | 4.753 | 4.51 | 249.0 | 0.0 | 134.6 |
| 150.00 Appurtenance(s) | 1.00 | 1.3850 .286 | 55.31 | 332.47 | 0.950 | 0.000 | 2.00 | 4.667 | 4.43 | 245.2 | 0.0 | 132.1 |
| 152.00 | 1.00 | 1.3850 .426 | 55.47 | 326.77 | 0.950 | 0.000 | 2.00 | 4.581 | 4.35 | 241.4 | 0.0 | 129.7 |
| 154.00 | 1.00 | 1.3950 .565 | 55.62 | 321.05 | 0.950 | 0.000 | 2.00 | 4.496 | 4.27 | 237.6 | 0.0 | 127.2 |
| 156.00 | 1.00 | 1.3950 .703 | 55.77 | 315.31 | 0.950 | 0.000 | 2.00 | 4.410 | 4.19 | 233.7 | 0.0 | 124.8 |
| 158.00 Appurtenance(s) | 1.00 | 1.3950 .839 | 55.92 | 309.54 | 0.950 | 0.000 | 2.00 | 4.325 | 4.11 | 229.8 | 0.0 | 122.3 |
| 160.00 | 1.00 | 1.4050 .974 | 56.07 | 303.76 | 0.950 | 0.000 | 2.00 | 4.239 | 4.03 | 225.8 | 0.0 | 119.9 |
| 162.00 | 1.00 | 1.4051 .107 | 56.22 | 297.95 | 0.950 | 0.000 | 2.00 | 4.154 | 3.95 | 221.8 | 0.0 | 117.5 |
| 164.00 | 1.00 | 1.4051 .239 | 56.36 | 292.13 | 0.950 | 0.000 | 2.00 | 4.068 | 3.86 | 217.8 | 0.0 | 115.0 |
| 166.00 Appurtenance(s) | 1.00 | 1.4151 .370 | 56.51 | 286.28 | 0.950 | 0.000 | 2.00 | 3.982 | 3.78 | 213.8 | 0.0 | 112.6 |
| 168.00 | 1.00 | 1.4151 .500 | 56.65 | 280.42 | 0.950 | 0.000 | 2.00 | 3.897 | 3.70 | 209.7 | 0.0 | 110.1 |
| 170.00 | 1.00 | 1.4251 .628 | 56.79 | 274.53 | 0.950 | 0.000 | 2.00 | 3.811 | 3.62 | 205.6 | 0.0 | 107.7 |
| 172.00 | 1.00 | 1.4251 .756 | 56.93 | 268.63 | 0.950 | 0.000 | 2.00 | 3.726 | 3.54 | 201.5 | 0.0 | 105.2 |
| 174.00 | 1.00 | 1.4251 .882 | 57.07 | 262.70 | 0.950 | 0.000 | 2.00 | 3.640 | 3.46 | 197.3 | 0.0 | 102.8 |
| 176.00 | 1.00 | 1.4352 .007 | 57.21 | 256.76 | 0.950 | 0.000 | 2.00 | 3.554 | 3.38 | 193.2 | 0.0 | 100.3 |
| 178.00 Appurtenance(s) | 1.00 | 1.4352 .131 | 57.34 | 250.80 | 0.950 | 0.000 | 2.00 | 3.469 | 3.30 | 189.0 | 0.0 | 97.9 |
| 180.00 | 1.00 | 1.4352 .253 | 57.48 | 244.83 | 0.950 | 0.000 | 2.00 | 3.383 | 3.21 | 184.7 | 0.0 | 95.4 |
|  |  |  |  |  |  | Totals: | 80.00 |  |  | 27,684.8 |  | ,072.5 |

## Discrete Appurtenance Forces

| Structure: <br> Site Name: Height: <br> Base Elev: <br> Gh: |  | $\begin{array}{ll} : & \text { CT46130-A-SBA } \\ \text { e: } & \text { Deep River-winthr } \\ 180.00(\mathrm{ft}) \\ \mathrm{r}: & 0.000(\mathrm{ft}) \\ 1.1 \end{array}$ | rop RdTopography: |  | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | 12/5/2019 <br> Page: 18 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Case: $0.9 \mathrm{D}+1.0 \mathrm{~W} 123 \mathrm{mph}$ Wind $\begin{array}{ll}\text { Dead Load Factor } & 0.90 \\ \text { Wind Load Factor } & 1.00\end{array}$ |  |  |  |  | $\begin{aligned} & \text { qzGh } \\ & \text { (psf) } \end{aligned}$ | Orient <br> Factor <br> x Ka | Ka | Total CaAa (sf) | Dead <br> Load <br> ( b ) | Horiz <br> Ecc <br> (ft) |  |  | rations | 29 |
| No. $\begin{gathered}\text { Elev } \\ \text { (ft) }\end{gathered}$ |  | Description | Qty | $\begin{gathered} \text { qz } \\ \text { (psf) } \\ \hline \end{gathered}$ |  |  |  |  |  |  | $\begin{aligned} & \text { Vert } \\ & \text { Ecc } \\ & \text { (ft) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Wind } \\ & \text { FX } \\ & \text { (Ib) } \\ & \hline \end{aligned}$ | $\begin{gathered} \begin{array}{c} \text { Mom } \\ Y \\ (\mathrm{lb}-\mathrm{ft}) \end{array} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Mom } \\ & \mathbf{Z} \\ & (\mathrm{lb}-\mathrm{ft}) \end{aligned}$ |
| 1 | 178.00 S | Samsung B5/B13 RRH | 3 | 52.131 | 57.344 | 0.50 | 0.75 | 3.35 | 189.81 | 0.000 | 0.000 | 191.91 | 0.00 | 0.00 |
| 2 | 178.00 | Samsung B2/B66A RRH | 3 | 52.131 | 57.344 | 0.50 | 0.75 | 2.83 | 227.88 | 0.000 | 0.000 | 162.52 | 0.00 | 0.00 |
| 3 | 178.00 J | JMA MX06FRO660-03 | 6 | 52.131 | 57.344 | 0.61 | 0.75 | 36.42 | 324.00 | 0.000 | 0.000 | 2088.48 | 0.00 | 0.00 |
| 4 | 178.00 P | Platform w/ Handrails w/ | 1 | 52.131 | 57.344 | 1.00 | 1.00 | 40.00 | 1981.98 | 0.000 | 0.000 | 2293.75 | 0.00 | 0.00 |
| 5 | 178.00 | Raycap | 1 | 52.131 | 57.344 | 1.00 | 1.00 | 2.61 | 28.80 | 0.000 | 0.000 | 149.67 | 0.00 | 0.00 |
| 6 | 166.00 A | ALU 800 Mhz | 6 | 51.370 | 56.507 | 0.38 | 0.75 | 5.60 | 286.20 | 0.000 | 0.000 | 316.58 | 0.00 | 0.00 |
| 7 | 166.00 R | RFS APXVTM14-C-120 | 3 | 51.370 | 56.507 | 0.58 | 0.75 | 10.98 | 151.74 | 0.000 | 0.000 | 620.68 | 0.00 | 0.00 |
| 8 | 166.00 | Commscope | 3 | 51.370 | 56.507 | 0.55 | 0.75 | 20.43 | 208.98 | 0.000 | 0.000 | 1154.42 | 0.00 | 0.00 |
| 9 | 166.00 A | ALU 1900 Mhz | 3 | 51.370 | 56.507 | 0.50 | 0.75 | 5.73 | 118.80 | 0.000 | 0.000 | 323.70 | 0.00 | 0.00 |
| 10 | 166.00 | Sitepro | 1 | 51.370 | 56.507 | 1.00 | 1.00 | 7.00 | 365.95 | 0.000 | 0.000 | 395.55 | 0.00 | 0.00 |
| 11 | 166.00 A | ALU TD-RRH8x20-25 | 3 | 51.370 | 56.507 | 0.50 | 0.75 | 6.11 | 189.00 | 0.000 | 0.000 | 345.00 | 0.00 | 0.00 |
| 12 | 166.00 S | Sitepro | 1 | 51.370 | 56.507 | 1.00 | 1.00 | 6.70 | 207.00 | 0.000 | 0.000 | 378.60 | 0.00 | 0.00 |
| 13 | 166.00 P | Platform w/ Hand Rails | 1 | 51.370 | 56.507 | 1.00 | 1.00 | 40.00 | 1800.00 | 0.000 | 0.000 | 2260.29 | 0.00 | 0.00 |
| 14 | 158.00 P | PCS1900 G3 TMA | 6 | 50.839 | 55.923 | 0.40 | 0.80 | 2.50 | 108.00 | 0.000 | 0.000 | 139.58 | 0.00 | 0.00 |
| 15 | 158.00 T | T-Arms | 3 | 50.839 | 55.923 | 0.56 | 0.75 | 13.50 | 945.00 | 0.000 | 0.000 | 754.96 | 0.00 | 0.00 |
| 16 | 158.00 | EMS RR90-17-02DP | 6 | 50.839 | 55.923 | 0.54 | 0.80 | 23.96 | 72.90 | 0.000 | 0.000 | 1339.78 | 0.00 | 0.00 |
| 17 | 150.00 P | Powerwave 7770 | 3 | 50.286 | 55.314 | 0.55 | 0.75 | 9.05 | 94.50 | 0.000 | 0.000 | 500.60 | 0.00 | 0.00 |
| 18 | 150.00 | Cci HPA-65R-BUU-H6 | 2 | 50.286 | 55.314 | 0.77 | 0.90 | 14.78 | 91.80 | 0.000 | 0.000 | 817.53 | 0.00 | 0.00 |
| 19 | 150.00 | SBNHH-1D65A | 1 | 50.286 | 55.314 | 1.00 | 1.00 | 5.88 | 30.15 | 0.000 | 0.000 | 325.25 | 0.00 | 0.00 |
| 20 | 150.00 | RRUS-32 | 3 | 50.286 | 55.314 | 0.50 | 0.75 | 5.83 | 207.90 | 0.000 | 0.000 | 322.71 | 0.00 | 0.00 |
| 21 | 150.00 | KMW AM-X-CD-16-65-00T | 2 | 50.286 | 55.314 | 0.56 | 0.75 | 9.02 | 87.30 | 0.000 | 0.000 | 499.07 | 0.00 | 0.00 |
| 22 | 150.00 P | Powerwave LGP21401 | 6 | 50.286 | 55.314 | 0.38 | 0.75 | 2.75 | 76.14 | 0.000 | 0.000 | 151.84 | 0.00 | 0.00 |
| 23 | 150.00 | KMW AM-X-CD-14-65-00T | 1 | 50.286 | 55.314 | 0.75 | 0.75 | 5.29 | 32.76 | 0.000 | 0.000 | 292.47 | 0.00 | 0.00 |
| 24 | 150.00 | Ericsson RRUS-11 | 3 | 50.286 | 55.314 | 0.50 | 0.75 | 3.80 | 136.89 | 0.000 | 0.000 | 210.13 | 0.00 | 0.00 |
| 25 | 150.00 R | Raycap DC6-48-60-18-8F | 1 | 50.286 | 55.314 | 0.67 | 1.00 | 1.21 | 28.62 | 0.000 | 0.000 | 67.08 | 0.00 | 0.00 |
| 26 | 150.00 P | Platform w/ Hand Rail | 1 | 50.286 | 55.314 | 1.00 | 1.00 | 35.00 | 1440.00 | 0.000 | 0.000 | 1936.00 | 0.00 | 0.00 |


| Total Applied Force Summary |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure: <br> Site Name <br> Height: <br> Base Elev <br> Gh: | -SBATopography: 1 |  | Code: <br> Exposure: Crest Height: Site Class: Struct Class: |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ | $12 / 5 / 2019$ <br> Page: 19 | $\underbrace{((1) H \mid N)}_{\text {Tower Engincering Solulions }}$ |  |
| Load Case: $0.9 \mathrm{D}+1.0 \mathrm{~W} 123 \mathrm{mph}$ Wind <br> Dead Load Factor 0.90 <br> Wind Load Factor 1.00 |  |  |  |  |  |  | erations | 29 |
| Elev (ft) Description | Lateral FX (-) (lb) | Axial <br> FY (-) <br> (lb) | Torsion MY (lb-ft) | $\begin{gathered} \text { Momen } \\ \text { MZ } \\ (\mathrm{lb}-\mathrm{ft}) \\ \hline \end{gathered}$ |  |  |  |  |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  |  |  |  |
| 2.00 | 345.27 | 529.06 | 0.00 | 0.00 |  |  |  |  |
| 4.00 | 342.50 | 543.22 | 0.00 | 0.00 |  |  |  |  |
| 6.00 | 339.73 | 557.37 | 0.00 | 0.00 |  |  |  |  |
| 8.00 | 336.95 | 553.09 | 0.00 | 0.00 |  |  |  |  |
| 10.00 | 334.18 | 548.81 | 0.00 | 0.00 |  |  |  |  |
| 12.00 | 331.41 | 544.53 | 0.00 | 0.00 |  |  |  |  |
| 14.00 | 328.63 | 540.25 | 0.00 | 0.00 |  |  |  |  |
| 16.00 | 329.88 | 535.97 | 0.00 | 0.00 |  |  |  |  |
| 18.00 | 335.29 | 531.69 | 0.00 | 0.00 |  |  |  |  |
| 20.00 | 339.86 | 527.41 | 0.00 | 0.00 |  |  |  |  |
| 22.00 | 343.75 | 523.13 | 0.00 | 0.00 |  |  |  |  |
| 24.00 | 347.05 | 518.86 | 0.00 | 0.00 |  |  |  |  |
| 26.00 | 349.84 | 514.58 | 0.00 | 0.00 |  |  |  |  |
| 28.00 | 352.18 | 510.30 | 0.00 | 0.00 |  |  |  |  |
| 30.00 | 354.13 | 506.02 | 0.00 | 0.00 |  |  |  |  |
| 32.00 | 355.72 | 501.74 | 0.00 | 0.00 |  |  |  |  |
| 34.00 | 357.00 | 497.46 | 0.00 | 0.00 |  |  |  |  |
| 36.00 | 357.99 | 493.18 | 0.00 | 0.00 |  |  |  |  |
| 38.00 | 358.72 | 488.90 | 0.00 | 0.00 |  |  |  |  |
| 40.00 | 359.21 | 484.62 | 0.00 | 0.00 |  |  |  |  |
| 42.00 | 359.48 | 480.34 | 0.00 | 0.00 |  |  |  |  |
| 43.92 | 344.50 | 456.31 | 0.00 | 0.00 |  |  |  |  |
| 44.00 | 15.15 | 36.94 | 0.00 | 0.00 |  |  |  |  |
| 46.00 | 365.16 | 882.38 | 0.00 | 0.00 |  |  |  |  |
| 48.00 | 364.91 | 874.12 | 0.00 | 0.00 |  |  |  |  |
| 50.00 | 364.49 | 865.87 | 0.00 | 0.00 |  |  |  |  |
| 51.00 | 181.66 | 429.84 | 0.00 | 0.00 |  |  |  |  |
| 52.00 | 181.51 | 217.28 | 0.00 | 0.00 |  |  |  |  |
| 54.00 | 363.19 | 431.58 | 0.00 | 0.00 |  |  |  |  |
| 56.00 | 362.33 | 427.60 | 0.00 | 0.00 |  |  |  |  |
| 58.00 | 361.33 | 423.63 | 0.00 | 0.00 |  |  |  |  |
| 60.00 | 360.21 | 419.65 | 0.00 | 0.00 |  |  |  |  |
| 62.00 | 358.98 | 415.68 | 0.00 | 0.00 |  |  |  |  |
| 64.00 | 357.62 | 411.71 | 0.00 | 0.00 |  |  |  |  |
| 66.00 | 356.16 | 407.73 | 0.00 | 0.00 |  |  |  |  |
| 68.00 | 354.60 | 403.76 | 0.00 | 0.00 |  |  |  |  |
| 70.00 | 352.94 | 399.78 | 0.00 | 0.00 |  |  |  |  |
| 72.00 | 351.19 | 395.81 | 0.00 | 0.00 |  |  |  |  |
| 74.00 | 349.34 | 391.84 | 0.00 | 0.00 |  |  |  |  |
| 76.00 | 347.41 | 387.86 | 0.00 | 0.00 |  |  |  |  |
| 78.00 | 345.40 | 383.89 | 0.00 | 0.00 |  |  |  |  |
| 80.00 | 343.31 | 379.91 | 0.00 | 0.00 |  |  |  |  |
| 82.00 | 341.14 | 375.94 | 0.00 | 0.00 |  |  |  |  |
| 84.00 | 338.89 | 371.97 | 0.00 | 0.00 |  |  |  |  |
| 86.00 | 336.57 | 367.99 | 0.00 | 0.00 |  |  |  |  |
| 88.00 | 334.19 | 364.02 | 0.00 | 0.00 |  |  |  |  |

## Total Applied Force Summary



| Structure: | CT46130-A-SBA |  | Code: | EIA/TIA-222-H | 12/5/2019 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Site Name: | Deep River-winthrop Rd |  | Exposure: | C |  |
| Height: | 180.00 (ft) |  | Crest Height: | 0.00 |  |
| Base Elev: | 0.000 (ft) |  | Site Class: | D-Stiff Soil |  |
| Gh: | 1.1 | Topography: | 1 | Struct Class: | II |


| Load Case: 0.9D + 1.0W 123 mph Wind |  |  |  |  |  | Resultant Moment (ft-kips) |  |  |  |  |  |  |  | 29 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dead Load Factor Wind Load Factor |  |  | $\begin{array}{ll} \mathbf{r} & 0.90 \\ & 1.00 \end{array}$ |  |  |  |  |  |  |  |  |  |  |
| Seg Elev <br> (ft) | $\begin{aligned} & \mathrm{Pu} \\ & \text { FY (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \mathrm{Vu} \\ \text { FX (-) } \\ \text { (kios) } \end{gathered}$ | $\begin{gathered} \text { Tu } \\ \text { MY (-) } \\ \text { (ft-kips) } \end{gathered}$ |  | $\begin{gathered} \begin{array}{c} \text { Mu } \\ \text { MX } \\ \text { (ft-kips) } \end{array} \\ \hline \end{gathered}$ |  | phi Pn <br> (kips) | phi Vn (kips) |  | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \\ \hline \end{gathered}$ | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (dea) | $\begin{gathered} \text { Stress } \\ \text { Ratio } \\ \hline \end{gathered}$ |
| 0.00 | -42.34 | -45.75 | 0.00 | -5425.5 | 0.00 | 5425.51 | 5123.29 | 1522.04 | 7808.40 | 6435.29 | 0.00 | 0.000 | 0.000 | 0.852 |
| 2.00 | -41.75 | -45.46 | 0.00 | -5334.0 | 0.00 | 5334.01 | 5107.67 | 1509.78 | 7683.09 | 6363.61 | 0.02 | -0.073 | 0.000 | 0.847 |
| 4.00 | -41.15 | -45.17 | 0.00 | -5243.0 | 0.00 | 5243.09 | 5091.62 | 1497.52 | 7558.79 | 6291.73 | 0.06 | -0.146 | 0.000 | 0.842 |
| 6.00 | -40.53 | -44.88 | 0.00 | -5152.7 | 0.00 | 5152.76 | 5075.16 | 1485.26 | 7435.50 | 6219.67 | 0.14 | -0.220 | 0.000 | 0.837 |
| 8.00 | -39.92 | -44.59 | 0.00 | -5063.0 | 0.00 | 5063.00 | 5058.29 | 1472.99 | 7313.22 | 6147.44 | 0.25 | -0.295 | 0.000 | 0.832 |
| 10.00 | -39.32 | -44.31 | 0.00 | -4973.8 | 0.00 | 4973.82 | 5041.00 | 1460.73 | 7191.96 | 6075.05 | 0.39 | -0.370 | 0.000 | 0.827 |
| 12.00 | -38.72 | -44.02 | 0.00 | -4885.2 | 0.00 | 4885.21 | 5023.29 | 1448.47 | 7071.72 | 6002.51 | 0.56 | -0.446 | 0.000 | 0.822 |
| 14.00 | -38.12 | -43.74 | 0.00 | -4797.1 | 0.00 | 4797.17 | 5005.16 | 1436.20 | 6952.48 | 5929.84 | 0.77 | -0.522 | 0.000 | 0.818 |
| 16.00 | -37.53 | -43.45 | 0.00 | -4709.6 | 0.00 | 4709.69 | 4986.62 | 1423.94 | 6834.27 | 5857.05 | 1.00 | -0.599 | 0.000 | 0.813 |
| 18.00 | -36.95 | -43.16 | 0.00 | -4622.7 | 0.00 | 4622.78 | 4967.66 | 1411.68 | 6717.06 | 5784.16 | 1.27 | -0.676 | 0.000 | 0.808 |
| 20.00 | -36.36 | -42.87 | 0.00 | -4536.4 | 0.00 | 4536.46 | 4948.29 | 1399.42 | 6600.87 | 5711.17 | 1.57 | -0.754 | 0.000 | 0.803 |
| 22.00 | -35.79 | -42.57 | 0.00 | -4450.7 | 0.00 | 4450.72 | 4928.49 | 1387.15 | 6485.69 | 5638.10 | 1.90 | -0.832 | 0.000 | 0.798 |
| 24.00 | -35.22 | -42.26 | 0.00 | -4365.5 | 0.00 | 4365.59 | 4908.28 | 1374.89 | 6371.53 | 5564.95 | 2.27 | -0.911 | 0.000 | 0.793 |
| 26.00 | -34.65 | -41.95 | 0.00 | -4281.0 | 0.00 | 4281.08 | 4887.66 | 1362.63 | 6258.37 | 5491.76 | 2.67 | -0.991 | 0.000 | 0.788 |
| 28.00 | -34.09 | -41.64 | 0.00 | -4197.1 | 0.00 | 4197.18 | 4866.62 | 1350.36 | 6146.24 | 5418.52 | 3.10 | -1.071 | 0.000 | 0.783 |
| 30.00 | -33.53 | -41.32 | 0.00 | -4113.9 | 0.00 | 4113.91 | 4845.16 | 1338.10 | 6035.11 | 5345.24 | 3.57 | -1.152 | 0.000 | 0.778 |
| 32.00 | -32.98 | -41.00 | 0.00 | -4031.2 | 0.00 | 4031.27 | 4823.28 | 1325.84 | 5925.00 | 5271.95 | 4.07 | -1.233 | 0.000 | 0.772 |
| 34.00 | -32.43 | -40.68 | 0.00 | -3949.2 | 0.00 | 3949.27 | 4800.99 | 1313.58 | 5815.91 | 5198.66 | 4.60 | -1.315 | 0.000 | 0.767 |
| 36.00 | -31.89 | -40.36 | 0.00 | -3867.9 | 0.00 | 3867.92 | 4778.28 | 1301.31 | 5707.83 | 5125.37 | 5.17 | -1.397 | 0.000 | 0.762 |
| 38.00 | -31.35 | -40.03 | 0.00 | -3787.2 | 0.00 | 3787.21 | 4755.15 | 1289.05 | 5600.76 | 5052.10 | 5.77 | -1.480 | 0.000 | 0.757 |
| 40.00 | -30.81 | -39.70 | 0.00 | -3707.1 | 0.00 | 3707.15 | 4731.61 | 1276.79 | 5494.70 | 4978.87 | 6.41 | -1.564 | 0.000 | 0.752 |
| 42.00 | -30.29 | -39.37 | 0.00 | -3627.7 | 0.00 | 3627.75 | 4707.65 | 1264.52 | 5389.66 | 4905.68 | 7.09 | -1.648 | 0.000 | 0.747 |
| 43.92 | -29.81 | -39.04 | 0.00 | -3552.2 | 0.00 | 3552.28 | 4684.30 | 1252.77 | 5289.95 | 4835.60 | 7.76 | -1.730 | 0.000 | 0.742 |
| 44.00 | -29.75 | -39.05 | 0.00 | -3549.0 | 0.00 | 3549.03 | 4683.27 | 1252.26 | 5285.64 | 4832.55 | 7.80 | -1.733 | 0.000 | 0.742 |
| 46.00 | -28.82 | -38.70 | 0.00 | -3470.9 | 0.00 | 3470.94 | 4658.48 | 1240.00 | 5182.62 | 4759.49 | 8.54 | -1.819 | 0.000 | 0.736 |
| 48.00 | -27.90 | -38.35 | 0.00 | -3393.5 | 0.00 | 3393.55 | 4633.27 | 1227.74 | 5080.62 | 4686.52 | 9.32 | -1.905 | 0.000 | 0.731 |
| 50.00 | -27.00 | -37.98 | 0.00 | -3316.8 | 0.00 | 3316.86 | 4607.64 | 1215.47 | 4979.64 | 4613.64 | 10.14 | -1.991 | 0.000 | 0.726 |
| 51.00 | -26.55 | -37.81 | 0.00 | -3278.8 | 0.00 | 3278.87 | 4157.28 | 1142.33 | 4736.69 | 4216.21 | 10.56 | -2.035 | 0.000 | 0.785 |
| 52.00 | -26.29 | -37.65 | 0.00 | -3241.0 | 0.00 | 3241.07 | 4146.96 | 1136.64 | 4689.60 | 4184.61 | 10.99 | -2.079 | 0.000 | 0.782 |
| 54.00 | -25.82 | -37.31 | 0.00 | -3165.7 | 0.00 | 3165.77 | 4126.01 | 1125.25 | 4596.10 | 4121.41 | 11.88 | -2.169 | 0.000 | 0.775 |
| 56.00 | -25.35 | -36.97 | 0.00 | -3091.1 | 0.00 | 3091.16 | 4104.64 | 1113.86 | 4503.55 | 4058.23 | 12.81 | -2.260 | 0.000 | 0.769 |
| 58.00 | -24.88 | -36.63 | 0.00 | -3017.2 | 0.00 | 3017.22 | 4082.85 | 1102.48 | 4411.95 | 3995.08 | 13.78 | -2.351 | 0.000 | 0.762 |
| 60.00 | -24.42 | -36.29 | 0.00 | -2943.9 | 0.00 | 2943.95 | 4060.64 | 1091.09 | 4321.28 | 3931.97 | 14.78 | -2.443 | 0.000 | 0.756 |
| 62.00 | -23.96 | -35.96 | 0.00 | -2871.3 | 0.00 | 2871.36 | 4038.02 | 1079.70 | 4231.55 | 3868.91 | 15.82 | -2.535 | 0.000 | 0.749 |
| 64.00 | -23.51 | -35.62 | 0.00 | -2799.4 | 0.00 | 2799.45 | 4014.98 | 1068.31 | 4142.77 | 3805.92 | 16.91 | -2.628 | 0.000 | 0.743 |
| 66.00 | -23.06 | -35.28 | 0.00 | -2728.2 | 0.00 | 2728.22 | 3991.52 | 1056.93 | 4054.92 | 3743.01 | 18.03 | -2.721 | 0.000 | 0.736 |
| 68.00 | -22.61 | -34.95 | 0.00 | -2657.6 | 0.00 | 2657.65 | 3967.65 | 1045.54 | 3968.02 | 3680.19 | 19.19 | -2.815 | 0.000 | 0.729 |
| 70.00 | -22.18 | -34.61 | 0.00 | -2587.7 | 0.00 | 2587.76 | 3943.36 | 1034.15 | 3882.06 | 3617.47 | 20.39 | -2.910 | 0.000 | 0.722 |
| 72.00 | -21.74 | -34.27 | 0.00 | -2518.5 | 0.00 | 2518.54 | 3918.66 | 1022.77 | 3797.04 | 3554.87 | 21.63 | -3.005 | 0.000 | 0.715 |
| 74.00 | -21.31 | -33.94 | 0.00 | -2449.9 | 0.00 | 2449.99 | 3893.54 | 1011.38 | 3712.96 | 3492.40 | 22.91 | -3.101 | 0.000 | 0.708 |
| 76.00 | -20.89 | -33.61 | 0.00 | -2382.1 | 0.00 | 2382.11 | 3868.00 | 999.99 | 3629.83 | 3430.07 | 24.23 | -3.197 | 0.000 | 0.701 |
| 78.00 | -20.47 | -33.28 | 0.00 | -2314.9 | 0.00 | 2314.90 | 3842.04 | 988.61 | 3547.63 | 3367.90 | 25.59 | -3.294 | 0.000 | 0.694 |
| 80.00 | -20.05 | -32.95 | 0.00 | -2248.3 | 0.00 | 2248.35 | 3815.67 | 977.22 | 3466.38 | 3305.90 | 26.99 | -3.392 | 0.000 | 0.686 |
| 82.00 | -19.64 | -32.62 | 0.00 | -2182.4 | 0.00 | 2182.46 | 3788.88 | 965.83 | 3386.07 | 3244.07 | 28.43 | -3.489 | 0.000 | 0.679 |
| 84.00 | -19.23 | -32.29 | 0.00 | -2117.2 | 0.00 | 2117.23 | 3761.67 | 954.44 | 3306.69 | 3182.44 | 29.91 | -3.588 | 0.000 | 0.672 |
| 86.00 | -18.83 | -31.96 | 0.00 | -2052.6 | 0.00 | 2052.65 | 3734.05 | 943.06 | 3228.26 | 3121.02 | 31.43 | -3.687 | 0.000 | 0.664 |
| 88.00 | -18.44 | -31.64 | 0.00 | -1988.7 | 0.00 | 1988.73 | 3706.01 | 931.67 | 3150.77 | 3059.82 | 33.00 | -3.786 | 0.000 | 0.656 |
| 90.00 | -18.07 | -31.30 | 0.00 | -1925.4 | 0.00 | 1925.46 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 34.61 | -3.886 | 0.000 | 0.648 |

## Calculated Forces

| Structure: <br> Site Name: <br> Height: <br> Base Elev: <br> Gh: |  | CT46130-A <br> Deep Rive <br> 180.00 (ft) <br> 0.000 (ft) <br> 1.1 |  | Topography: |  |  | Code: <br> Exposure: <br> Crest Height <br> Site Class: <br> Struct Class | $\begin{aligned} & \hline \hline \text { EIA/TIA-222-H } \\ & C \\ & 0.00 \\ & \text { D-Stiff Soil } \\ & \text { II } \end{aligned}$ |  |  | 12/5/2019 <br> Page: 22 |  | $\underbrace{((1, W))}_{\text {Tower Enginering Solutions }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.17 | -18.02 | -31.28 | 0.00 | -1920.2 | 0.00 | 1920.24 | 3675.16 | 919.33 | 3067.89 | 2993.77 | 34.74 | -3.894 | 0.000 | 0.6 |
| 92.00 | -17.41 | -30.97 | 0.00 | -1862.8 | 0.00 | 1862.89 | 3648.68 | 908.90 | 2998.62 | 2938.12 | 36.25 | -3.986 | 0.000 | 0.640 |
| 94.00 | -16.75 | -30.62 | 0.00 | -1800.9 | 0.00 | 1800.95 | 3619.39 | 897.51 | 2923.96 | 2877.64 | 37.94 | -4.087 | 0.000 | 0.632 |
| 96.00 | -16.11 | -30.28 | 0.00 | -1739.7 | 0.00 | 1739.71 | 2873.56 | 764.37 | 2506.37 | 2303.28 | 39.68 | -4.188 | 0.000 | . 762 |
| 98.00 | -15.78 | -29.96 | 0.00 | -1679.1 | 0.00 | 1679.15 | 2853.66 | 754.73 | 2443.58 | 2258.25 | 41.45 | -4.289 | 0.000 | 0.751 |
| 100.00 | -15.44 | -29.64 | 0.00 | -1619.2 | 0.00 | 1619.23 | 2833.34 | 745.10 | 2381.59 | 2213.29 | 43.27 | 4.402 | 0.000 | 0.739 |
| 102.00 | -15.12 | -29.33 | 0.00 | -1559.9 | 0.00 | 1559.95 | 2812.61 | 735.46 | 2320.39 | 2168.43 | 45.14 | -4.516 | 0.000 | 0.726 |
| 104.00 | -14.79 | -29.02 | 0.00 | -1501.2 | 0.00 | 1501.29 | 2791.46 | 725.83 | 2259.99 | 2123.68 | 47.05 | -4.630 | 0.000 | 0.714 |
| 106.00 | -14.48 | -28.71 | 0.00 | -1443.2 | 0.00 | 1443.25 | 2769.89 | 716.19 | 2200.39 | 2079.04 | 49.02 | -4.743 | 0.000 | 0.701 |
| 108.00 | -14.16 | -28.40 | 0.00 | -1385.8 | 0.00 | 1385.83 | 2747.90 | 706.55 | 2141.58 | 2034.53 | 51.03 | -4.857 | 0.000 | 0.688 |
| 110.00 | -13.85 | -28.10 | 0.00 | -1329.0 | 0.00 | 1329.03 | 2725.50 | 696.92 | 2083.57 | 1990.17 | 53.08 | -4.970 | 0.000 | 0.675 |
| 112.00 | -13.55 | -27.79 | 0.00 | -1272.8 | 0.00 | 1272.84 | 2702.68 | 687.28 | 2026.36 | 1945.97 | 55.19 | -5.084 | 0.000 | 0.661 |
| 114.00 | -13.25 | -27.49 | 0.00 | -1217.2 | 0.00 | 1217.25 | 2679.45 | 677.65 | 1969.94 | 1901.93 | 57.34 | -5.197 | 0.000 | 0.647 |
| 116.00 | -12.95 | -27.19 | 0.00 | -1162.2 | 0.00 | 1162.27 | 2655.79 | 668.01 | 1914.32 | 1858.08 | 59.54 | -5.310 | 0.000 | 0.632 |
| 118.00 | -12.66 | -26.90 | 0.00 | -1107.8 | 0.00 | 1107.88 | 2631.73 | 658.38 | 1859.50 | 1814.42 | 61.78 | -5.422 | 0.000 | 0.617 |
| 120.00 | -12.37 | -26.60 | 0.00 | -1054.0 | 0.00 | 1054.09 | 2607.24 | 648.74 | 1805.47 | 1770.96 | 64.08 | -5.534 | 0.000 | 0.602 |
| 122.00 | -12.09 | -26.31 | 0.00 | -1000.8 | 0.00 | 1000.88 | 2582.34 | 639.11 | 1752.24 | 1727.73 | 66.41 | -5.645 | 0.000 | 0.586 |
| 124.00 | -11.81 | -26.02 | 0.00 | -948.25 | 0.00 | 948.25 | 2557.02 | 629.47 | 1699.80 | 1684.74 | 68.80 | -5.756 | 0.000 | 0.569 |
| 126.00 | -11.53 | -25.74 | 0.00 | -896.21 | 0.00 | 896.21 | 2531.28 | 619.84 | 1648.16 | 1641.98 | 71.23 | -5.865 | 0.000 | 0.552 |
| 128.00 | -11.27 | -25.45 | 0.00 | -844.74 | 0.00 | 844.74 | 2505.13 | 610.20 | 1597.32 | 1599.49 | 73.71 | -5.973 | 0.000 | 0.534 |
| 130.00 | -11.00 | -25.17 | 0.00 | -793.83 | 0.00 | 793.83 | 2478.56 | 600.57 | 1547.28 | 1557.27 | 76.23 | -6.079 | 0.000 | 0.516 |
| 132.00 | -10.75 | -24.89 | 0.00 | -743.49 | 0.00 | 743.49 | 2451.58 | 590.93 | 1498.03 | 1515.33 | 78.79 | -6.184 | 0.000 | 0.497 |
| 133.33 | -10.59 | -24.70 | 0.00 | -710.30 | 0.00 | 710.30 | 2433.35 | 584.51 | 1465.64 | 1487.53 | 80.53 | -6.253 | 0.000 | 0.484 |
| 134.00 | -10.44 | -24.61 | 0.00 | -693.83 | 0.00 | 693.83 | 2424.17 | 581.30 | 1449.58 | 1473.69 | 81.40 | -6.288 | 0.000 | 0.477 |
| 136.00 | -10.04 | -24.32 | 0.00 | -644.61 | 0.00 | 644.61 | 2396.35 | 571.66 | 1401.92 | 1432.35 | 84.05 | -6.388 | 0.000 | 0.456 |
| 138.00 | -9.65 | -24.02 | 0.00 | -595.98 | 0.00 | 595.98 | 1545.45 | 417.14 | 1026.36 | 929.77 | 86.74 | -6.486 | 0.000 | 0.651 |
| 140.00 | -9.46 | -23.76 | 0.00 | -547.94 | 0.00 | 547.94 | 1531.69 | 410.13 | 992.17 | 905.88 | 89.48 | -6.582 | 0.000 | 0.614 |
| 142.00 | -9.26 | -23.50 | 0.00 | -500.42 | 0.00 | 500.42 | 1517.50 | 403.12 | 958.56 | 882.03 | 92.25 | -6.700 | 0.000 | 0.577 |
| 144.00 | -9.07 | -23.24 | 0.00 | -453.43 | 0.00 | 453.43 | 1502.90 | 396.11 | 925.52 | 858.22 | 95.08 | -6.814 | 0.000 | 0.538 |
| 146.00 | -8.89 | -22.98 | 0.00 | -406.95 | 0.00 | 406.95 | 1487.88 | 389.11 | 893.06 | 834.49 | 97.95 | -6.922 | 0.000 | 0.497 |
| 148.00 | -8.71 | -22.73 | 0.00 | -360.98 | 0.00 | 360.98 | 1472.45 | 382.10 | 861.19 | 810.82 | 100.87 | -7.024 | 0.000 | 0.455 |
| 150.00 | -6.97 | -17.12 | 0.00 | -315.52 | 0.00 | 315.52 | 1456.60 | 375.09 | 829.89 | 787.25 | 103.82 | -7.118 | 0.000 | 0.408 |
| 152.00 | -6.82 | -16.87 | 0.00 | -281.28 | 0.00 | 281.28 | 1440.33 | 368.08 | 799.17 | 763.78 | 106.82 | -7.207 | 0.000 | 0.375 |
| 154.00 | -6.68 | -16.63 | 0.00 | -247.53 | 0.00 | 247.53 | 1423.65 | 361.08 | 769.03 | 740.42 | 109.85 | -7.290 | 0.000 | 0.341 |
| 156.00 | -6.54 | -16.39 | 0.00 | -214.28 | 0.00 | 214.28 | 1406.55 | 354.07 | 739.47 | 717.20 | 112.91 | -7.366 | 0.000 | 0.306 |
| 158.00 | -5.58 | -13.78 | 0.00 | -181.51 | 0.00 | 181.51 | 1389.03 | 347.06 | 710.49 | 694.11 | 116.00 | -7.436 | 0.000 | 0.267 |
| 160.00 | -5.47 | -13.55 | 0.00 | -153.94 | 0.00 | 153.94 | 1371.10 | 340.05 | 682.09 | 671.17 | 119.12 | -7.498 | 0.000 | 0.235 |
| 162.00 | -5.36 | -13.32 | 0.00 | -126.84 | 0.00 | 126.84 | 1352.75 | 333.05 | 654.27 | 648.41 | 122.27 | $-7.554$ | 0.000 | 0.201 |
| 164.00 | -5.25 | -13.09 | 0.00 | -100.21 | 0.00 | 100.21 | 1333.98 | 326.04 | 627.03 | 625.81 | 125.44 | -7.602 | 0.000 | 0.166 |
| 166.00 | -2.63 | -6.68 | 0.00 | -74.03 | 0.00 | 74.03 | 1314.79 | 319.03 | 600.37 | 603.42 | 128.62 | -7.641 | 0.000 | 0.125 |
| 168.00 | -2.54 | -6.46 | 0.00 | -60.68 | 0.00 | 60.68 | 1295.19 | 312.03 | 574.28 | 581.22 | 131.82 | -7.674 | 0.000 | 0.107 |
| 170.00 | -2.45 | -6.24 | 0.00 | -47.77 | 0.00 | 47.77 | 1275.17 | 305.02 | 548.78 | 559.24 | 135.03 | -7.702 | 0.000 | 0.088 |
| 172.00 | -2.37 | -6.02 | 0.00 | -35.29 | 0.00 | 35.29 | 1251.65 | 298.01 | 523.85 | 536.17 | 138.25 | -7.724 | 0.000 | 0.068 |
| 174.00 | -2.29 | -5.82 | 0.00 | -23.24 | 0.00 | 23.24 | 1222.21 | 291.00 | 499.51 | 511.11 | 141.48 | -7.742 | 0.000 | 0.048 |
| 176.00 | -2.21 | -5.61 | 0.00 | -11.61 | 0.00 | 11.61 | 1192.78 | 284.00 | 475.74 | 486.64 | 144.72 | -7.753 | 0.000 | 0.026 |
| 178.00 | -0.07 | -0.20 | 0.00 | -0.39 | 0.00 | 0.39 | 1163.35 | 276.99 | 452.55 | 462.78 | 147.96 | -7.757 | 0.000 | 0.001 |
| 180.00 | 0.00 | -0.18 | 0.00 | 0.00 | 0.00 | 0.00 | 1133.92 | 269.98 | 429.95 | 439.52 | 151.20 | -7.757 | 0.000 | 0.000 |

## Wind Loading - Shaft

| Structure <br> Site Name <br> Height: <br> Base Elev <br> Gh: | CT46130-A-SBA <br> Deep River-winth 180.00 (ft) 0.000 (ft) 1.1 | Topography: |  | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  |  | $\begin{aligned} & \text { EIATIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D- Stiff Soil } \\ & \text { II } \end{aligned}$ |  | $\begin{array}{c\|} \hline \hline \text { 12/5/2019 } \\ \text { Page: } 23 \\ \hline \end{array}$ |  |  | $\xrightarrow[\text { Tower Enginecing Solutions }]{((1) \mid(1))}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind <br> Dead Load Factor $\quad 1.20$ <br> Wind Load Factor $\quad 1.00$ |  |  |  |  |  |  |  |  |  |  |  | Iterati | ns 27 |
| Elev (ft) Description | Kzt | Kz | $\begin{gathered} \mathrm{qz} \\ \text { (psf) } \end{gathered}$ | $\begin{aligned} & \text { qzGh } \\ & \text { (psf) } \\ & \hline \end{aligned}$ | $\begin{gathered} C \\ \text { (mph-ft) } \end{gathered}$ | Cf | Ice <br> Thick <br> (in) | Tributary <br> (ft) | $\begin{aligned} & \text { Aa } \\ & \text { (sf) } \end{aligned}$ | $\begin{gathered} \text { CfAa } \\ \text { (sf) } \end{gathered}$ | Wind Force X (lb) | Dead Load Ice (Ib) | Tot Dead Load (lb) |
| 0.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 2.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.567 | 2.00 | 10.844 | 13.01 | 73.3 | 91.2 | 796.6 |
| 4.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.607 | 2.00 | 10.772 | 12.93 | 72.9 | 97.0 | 796.7 |
| 6.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.632 | 2.00 | 10.695 | 12.83 | 72.3 | 100.2 | 794.2 |
| 8.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.651 | 2.00 | 10.615 | 12.74 | 71.8 | 102.3 | 790.6 |
| 10.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.666 | 2.00 | 10.535 | 12.64 | 71.3 | 103.8 | 786.4 |
| 12.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.678 | 2.00 | 10.453 | 12.54 | 70.7 | 104.9 | 781.8 |
| 14.00 | 1.00 | 0.85 | 5.124 | 5.64 | 0.00 | 1.200 | 0.688 | 2.00 | 10.371 | 12.45 | 70.1 | 105.6 | 776.8 |
| 16.00 | 1.00 | 0.86 | 5.187 | 5.71 | 0.00 | 1.200 | 0.698 | 2.00 | 10.289 | 12.35 | 70.4 | 106.2 | 771.7 |
| 18.00 | 1.00 | 0.88 | 5.318 | 5.85 | 0.00 | 1.200 | 0.706 | 2.00 | 10.206 | 12.25 | 71.6 | 106.6 | 766.3 |
| 20.00 | 1.00 | 0.90 | 5.437 | 5.98 | 0.00 | 1.200 | 0.713 | 2.00 | 10.123 | 12.15 | 72.6 | 106.8 | 760.8 |
| 22.00 | 1.00 | 0.92 | 5.547 | 6.10 | 0.00 | 1.200 | 0.720 | 2.00 | 10.039 | 12.05 | 73.5 | 106.9 | 755.2 |
| 24.00 | 1.00 | 0.94 | 5.650 | 6.21 | 0.00 | 1.200 | 0.726 | 2.00 | 9.956 | 11.95 | 74.2 | 106.9 | 749.5 |
| 26.00 | 1.00 | 0.95 | 5.746 | 6.32 | 0.00 | 1.200 | 0.732 | 2.00 | 9.872 | 11.85 | 74.9 | 106.8 | 743.8 |
| 28.00 | 1.00 | 0.97 | 5.836 | 6.42 | 0.00 | 1.200 | 0.738 | 2.00 | 9.788 | 11.75 | 75.4 | 106.7 | 737.9 |
| 30.00 | 1.00 | 0.98 | 5.921 | 6.51 | 0.00 | 1.200 | 0.743 | 2.00 | 9.705 | 11.65 | 75.9 | 106.5 | 732.0 |
| 32.00 | 1.00 | 1.00 | 6.002 | 6.60 | 0.00 | 1.200 | 0.748 | 2.00 | 9.621 | 11.54 | 76.2 | 106.2 | 726.0 |
| 34.00 | 1.00 | 1.01 | 6.079 | 6.69 | 0.00 | 1.200 | 0.752 | 2.00 | 9.536 | 11.44 | 76.5 | 105.9 | 720.0 |
| 36.00 | 1.00 | 1.02 | 6.153 | 6.77 | 0.00 | 1.200 | 0.757 | 2.00 | 9.452 | 11.34 | 76.8 | 105.5 | 713.9 |
| 38.00 | 1.00 | 1.03 | 6.224 | 6.85 | 0.00 | 1.200 | 0.761 | 2.00 | 9.368 | 11.24 | 77.0 | 105.1 | 707.8 |
| 40.00 | 1.00 | 1.04 | 6.291 | 6.92 | 0.00 | 1.200 | 0.765 | 2.00 | 9.284 | 11.14 | 77.1 | 104.7 | 701.7 |
| 42.00 | 1.00 | 1.05 | 6.356 | 6.99 | 0.00 | 1.200 | 0.768 | 2.00 | 9.200 | 11.04 | 77.2 | 104.2 | 695.5 |
| 43.92 Bot - Section 2 | 1.00 | 1.06 | 6.416 | 7.06 | 0.00 | 1.200 | 0.772 | 1.92 | 8.737 | 10.48 | 74.0 | 99.4 | 660.7 |
| 44.00 | 1.00 | 1.06 | 6.419 | 7.06 | 0.00 | 1.200 | 0.772 | 0.08 | 0.384 | 0.46 | 3.3 | 4.4 | 51.6 |
| 46.00 | 1.00 | 1.07 | 6.479 | 7.13 | 0.00 | 1.200 | 0.775 | 2.00 | 9.171 | 11.01 | 78.4 | 104.8 | 1232.2 |
| 48.00 | 1.00 | 1.08 | 6.537 | 7.19 | 0.00 | 1.200 | 0.779 | 2.00 | 9.086 | 10.90 | 78.4 | 104.3 | 1220.6 |
| 50.00 | 1.00 | 1.09 | 6.594 | 7.25 | 0.00 | 1.200 | 0.782 | 2.00 | 9.002 | 10.80 | 78.3 | 103.7 | 1209.0 |
| 51.00 Top - Section 1 | 1.00 | 1.10 | 6.621 | 7.28 | 0.00 | 1.200 | 0.783 | 1.00 | 4.469 | 5.36 | 39.1 | 51.7 | 600.2 |
| 52.00 | 1.00 | 1.10 | 6.648 | 7.31 | 0.00 | 1.200 | 0.785 | 1.00 | 4.448 | 5.34 | 39.0 | 51.6 | 316.7 |
| 54.00 | 1.00 | 1.11 | 6.701 | 7.37 | 0.00 | 1.200 | 0.788 | 2.00 | 8.833 | 10.60 | 78.1 | 102.5 | 628.8 |
| 56.00 | 1.00 | 1.12 | 6.753 | 7.43 | 0.00 | 1.200 | 0.791 | 2.00 | 8.748 | 10.50 | 78.0 | 101.9 | 622.8 |
| 58.00 | 1.00 | 1.13 | 6.803 | 7.48 | 0.00 | 1.200 | 0.794 | 2.00 | 8.663 | 10.40 | 77.8 | 101.2 | 616.9 |
| 60.00 | 1.00 | 1.14 | 6.852 | 7.54 | 0.00 | 1.200 | 0.796 | 2.00 | 8.579 | 10.29 | 77.6 | 100.5 | 610.9 |
| 62.00 | 1.00 | 1.14 | 6.899 | 7.59 | 0.00 | 1.200 | 0.799 | 2.00 | 8.494 | 10.19 | 77.4 | 99.8 | 604.9 |
| 64.00 | 1.00 | 1.15 | 6.945 | 7.64 | 0.00 | 1.200 | 0.801 | 2.00 | 8.409 | 10.09 | 77.1 | 99.1 | 598.9 |
| 66.00 | 1.00 | 1.16 | 6.991 | 7.69 | 0.00 | 1.200 | 0.804 | 2.00 | 8.325 | 9.99 | 76.8 | 98.4 | 592.9 |
| 68.00 | 1.00 | 1.17 | 7.035 | 7.74 | 0.00 | 1.200 | 0.806 | 2.00 | 8.240 | 9.89 | 76.5 | 97.7 | 586.9 |
| 70.00 | 1.00 | 1.17 | 7.078 | 7.79 | 0.00 | 1.200 | 0.809 | 2.00 | 8.155 | 9.79 | 76.2 | 96.9 | 580.8 |
| 72.00 | 1.00 | 1.18 | 7.120 | 7.83 | 0.00 | 1.200 | 0.811 | 2.00 | 8.070 | 9.68 | 75.8 | 96.2 | 574.7 |
| 74.00 | 1.00 | 1.19 | 7.161 | 7.88 | 0.00 | 1.200 | 0.813 | 2.00 | 7.985 | 9.58 | 75.5 | 95.4 | 568.7 |
| 76.00 | 1.00 | 1.19 | 7.201 | 7.92 | 0.00 | 1.200 | 0.815 | 2.00 | 7.900 | 9.48 | 75.1 | 94.6 | 562.6 |
| 78.00 | 1.00 | 1.20 | 7.241 | 7.96 | 0.00 | 1.200 | 0.817 | 2.00 | 7.816 | 9.38 | 74.7 | 93.8 | 556.5 |
| 80.00 | 1.00 | 1.21 | 7.279 | 8.01 | 0.00 | 1.200 | 0.819 | 2.00 | 7.731 | 9.28 | 74.3 | 93.0 | 550.4 |
| 82.00 | 1.00 | 1.21 | 7.317 | 8.05 | 0.00 | 1.200 | 0.821 | 2.00 | 7.646 | 9.17 | 73.9 | 92.2 | 544.2 |
| 84.00 | 1.00 | 1.22 | 7.355 | 8.09 | 0.00 | 1.200 | 0.823 | 2.00 | 7.561 | 9.07 | 73.4 | 91.3 | 538.1 |
| 86.00 | 1.00 | 1.23 | 7.391 | 8.13 | 0.00 | 1.200 | 0.825 | 2.00 | 7.476 | 8.97 | 72.9 | 90.5 | 532.0 |
| 88.00 | 1.00 | 1.23 | 7.427 | 8.17 | 0.00 | 1.200 | 0.827 | 2.00 | 7.391 | 8.87 | 72.5 | 89.6 | 525.8 |

## Wind Loading - Shaft



## Discrete Appurtenance Forces

| Structure: <br> Site Name <br> Height: <br> Base Elev: <br> Gh: |  | CT46130-A-SBA Deep River-winthr $180.00(\mathrm{ft})$ $0.000(\mathrm{ft})$ 1.1 | op RdTopography: |  | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | 12/5/2019 <br> Page: 25 |  | Tower Enginering Solutions |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind $\begin{array}{ll}\text { Dead Load Factor } & 1.20 \\ \text { Wind Load Factor } & 1.00\end{array}$ |  |  |  |  |  | Orient <br> Factor <br> $\mathbf{x ~ K a ~}$ | Ka | Total CaAa (sf) |  |  |  |  | ations | 27 |
| No. $\begin{gathered}\text { Elev } \\ \text { (ft) }\end{gathered}$ |  | Description | Oty | $\begin{gathered} \mathbf{q z} \\ \text { (psf) } \end{gathered}$ | $\begin{aligned} & \text { qzGh } \\ & \text { (psf) } \end{aligned}$ |  |  |  | Dead <br> Load <br> (lb) | Horiz Ecc (ft) | Vert Ecc <br> (ft) | Wind FX <br> (lb) | $\begin{gathered} \text { Mom } \\ \text { Y } \\ \text { (lb-ft) } \end{gathered}$ | $\begin{gathered} \text { Mom } \\ Z \\ (\mathrm{lb}-\mathrm{ft}) \\ \hline \end{gathered}$ |
| 1 | 178.00 S | Samsung B5/B13 RRH | 3 | 8.614 | 9.476 | 0.50 | 0.75 | 3.82 | 289.84 | 0.000 | 0.000 | 36.22 | 0.00 | 0.00 |
| 2 | 178.00 S | Samsung B2/B66A RRH | 3 | 8.614 | 9.476 | 0.50 | 0.75 | 3.51 | 533.26 | 0.000 | 0.000 | 33.23 | 0.00 | 0.00 |
| 3 | 178.00 J | JMA MX06FRO660-03 | 6 | 8.614 | 9.476 | 0.61 | 0.75 | 38.75 | 1189.18 | 0.000 | 0.000 | 367.17 | 0.00 | 0.00 |
| 4 | 178.00 P | Platform w/ Handrails w/ | 1 | 8.614 | 9.476 | 1.00 | 1.00 | 50.65 | 3417.74 | 0.000 | 0.000 | 479.97 | 0.00 | 0.00 |
| 5 | 178.00 | Raycap | 1 | 8.614 | 9.476 | 1.00 | 1.00 | 2.94 | 57.76 | 0.000 | 0.000 | 27.83 | 0.00 | 0.00 |
| 6 | 166.00 A | ALU 800 Mhz | 6 | 8.489 | 9.338 | 0.38 | 0.75 | 6.90 | 479.14 | 0.000 | 0.000 | 64.45 | 0.00 | 0.00 |
| 7 | 166.00 R | RFS APXVTM14-C-120 | 3 | 8.489 | 9.338 | 0.58 | 0.75 | 11.93 | 421.57 | 0.000 | 0.000 | 111.37 | 0.00 | 0.00 |
| 8 | 166.00 | Commscope | 3 | 8.489 | 9.338 | 0.55 | 0.75 | 21.65 | 513.94 | 0.000 | 0.000 | 202.20 | 0.00 | 0.00 |
| 9 | 166.00 A | ALU 1900 Mhz | 3 | 8.489 | 9.338 | 0.50 | 0.75 | 6.79 | 230.21 | 0.000 | 0.000 | 63.37 | 0.00 | 0.00 |
| 10 | 166.00 S | Sitepro | 1 | 8.489 | 9.338 | 1.00 | 1.00 | 10.46 | 1138.27 | 0.000 | 0.000 | 97.63 | 0.00 | 0.00 |
| 11 | 166.00 A | ALU TD-RRH8x20-25 | 3 | 8.489 | 9.338 | 0.50 | 0.75 | 6.70 | 402.61 | 0.000 | 0.000 | 62.55 | 0.00 | 0.00 |
| 12 | 166.00 S | Sitepro | 1 | 8.489 | 9.338 | 1.00 | 1.00 | 10.24 | 337.20 | 0.000 | 0.000 | 95.65 | 0.00 | 0.00 |
| 13 | 166.00 P | Platform w/ Hand Rails | 1 | 8.489 | 9.338 | 1.00 | 1.00 | 50.58 | 2857.80 | 0.000 | 0.000 | 472.28 | 0.00 | 0.00 |
| 14 | 158.00 | PCS1900 G3 TMA | 6 | 8.401 | 9.241 | 0.40 | 0.80 | 3.46 | 173.64 | 0.000 | 0.000 | 31.95 | 0.00 | 0.00 |
| 15 | 158.00 T | T-Arms | 3 | 8.401 | 9.241 | 0.56 | 0.75 | 19.42 | 1418.40 | 0.000 | 0.000 | 179.47 | 0.00 | 0.00 |
| 16 | 158.00 E | EMS RR90-17-02DP | 6 | 8.401 | 9.241 | 0.54 | 0.80 | 25.89 | 524.52 | 0.000 | 0.000 | 239.22 | 0.00 | 0.00 |
| 17 | 150.00 P | Powerwave 7770 | 3 | 8.309 | 9.140 | 0.55 | 0.75 | 9.88 | 306.19 | 0.000 | 0.000 | 90.33 | 0.00 | 0.00 |
| 18 | 150.00 | Cci HPA-65R-BUU-H6 | 2 | 8.309 | 9.140 | 0.77 | 0.90 | 15.79 | 350.56 | 0.000 | 0.000 | 144.35 | 0.00 | 0.00 |
| 19 | 150.00 | SBNHH-1D65A | 1 | 8.309 | 9.140 | 1.00 | 1.00 | 6.40 | 111.56 | 0.000 | 0.000 | 58.52 | 0.00 | 0.00 |
| 20 | 150.00 R | Rrus-32 | 3 | 8.309 | 9.140 | 0.50 | 0.75 | 5.57 | 430.43 | 0.000 | 0.000 | 50.92 | 0.00 | 0.00 |
| 21 | 150.00 K | KMW AM-X-CD-16-65-00T | 2 | 8.309 | 9.140 | 0.56 | 0.75 | 10.59 | 185.68 | 0.000 | 0.000 | 96.83 | 0.00 | 0.00 |
| 22 | 150.00 P | Powerwave LGP21401 | 6 | 8.309 | 9.140 | 0.38 | 0.75 | 3.63 | 133.92 | 0.000 | 0.000 | 33.22 | 0.00 | 0.00 |
| 23 | 150.00 | KMW AM-X-CD-14-65-00T | 1 | 8.309 | 9.140 | 0.75 | 0.75 | 6.28 | 67.54 | 0.000 | 0.000 | 57.39 | 0.00 | 0.00 |
| 24 | 150.00 E | Ericsson RRUS-11 | 3 | 8.309 | 9.140 | 0.50 | 0.75 | 4.27 | 289.33 | 0.000 | 0.000 | 39.02 | 0.00 | 0.00 |
| 25 | 150.00 R | Raycap DC6-48-60-18-8F | 1 | 8.309 | 9.140 | 0.67 | 1.00 | 1.50 | 51.37 | 0.000 | 0.000 | 13.72 | 0.00 | 0.00 |
| 26 | 150.00 P | Platform w/ Hand Rail | 1 | 8.309 | 9.140 | 1.00 | 1.00 | 50.27 | 2369.92 | 0.000 | 0.000 | 459.50 | 0.00 | 0.00 |

## Total Applied Force Summary



| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Dead Load Factor | 1.20 |  |  |
| Wind Load Factor | 1.00 |  |  |


| Elev <br> (ft) | Description | Lateral <br> FX (-) <br> (lb) | Axial FY ( - ) <br> (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 |
| 2.00 |  | 73.35 | 796.58 | 0.00 | 0.00 |
| 4.00 |  | 72.86 | 821.28 | 0.00 | 0.00 |
| 6.00 |  | 72.34 | 843.39 | 0.00 | 0.00 |
| 8.00 |  | 71.80 | 839.81 | 0.00 | 0.00 |
| 10.00 |  | 71.25 | 835.58 | 0.00 | 0.00 |
| 12.00 |  | 70.70 | 830.93 | 0.00 | 0.00 |
| 14.00 |  | 70.15 | 825.99 | 0.00 | 0.00 |
| 16.00 |  | 70.45 | 820.82 | 0.00 | 0.00 |
| 18.00 |  | 71.64 | 815.48 | 0.00 | 0.00 |
| 20.00 |  | 72.65 | 810.00 | 0.00 | 0.00 |
| 22.00 |  | 73.51 | 804.40 | 0.00 | 0.00 |
| 24.00 |  | 74.25 | 798.70 | 0.00 | 0.00 |
| 26.00 |  | 74.87 | 792.92 | 0.00 | 0.00 |
| 28.00 |  | 75.41 | 787.07 | 0.00 | 0.00 |
| 30.00 |  | 75.85 | 781.16 | 0.00 | 0.00 |
| 32.00 |  | 76.23 | 775.19 | 0.00 | 0.00 |
| 34.00 |  | 76.53 | 769.17 | 0.00 | 0.00 |
| 36.00 |  | 76.77 | 763.11 | 0.00 | 0.00 |
| 38.00 |  | 76.96 | 757.00 | 0.00 | 0.00 |
| 40.00 |  | 77.10 | 750.86 | 0.00 | 0.00 |
| 42.00 |  | 77.18 | 744.69 | 0.00 | 0.00 |
| 43.92 |  | 74.00 | 707.84 | 0.00 | 0.00 |
| 44.00 |  | 3.25 | 53.65 | 0.00 | 0.00 |
| 46.00 |  | 78.43 | 1281.34 | 0.00 | 0.00 |
| 48.00 |  | 78.41 | 1269.79 | 0.00 | 0.00 |
| 50.00 |  | 78.35 | 1258.21 | 0.00 | 0.00 |
| 51.00 |  | 39.06 | 624.83 | 0.00 | 0.00 |
| 52.00 |  | 39.03 | 341.27 | 0.00 | 0.00 |
| 54.00 |  | 78.13 | 677.94 | 0.00 | 0.00 |
| 56.00 |  | 77.98 | 672.01 | 0.00 | 0.00 |
| 58.00 |  | 77.80 | 666.05 | 0.00 | 0.00 |
| 60.00 |  | 77.59 | 660.08 | 0.00 | 0.00 |
| 62.00 |  | 77.35 | 654.09 | 0.00 | 0.00 |
| 64.00 |  | 77.10 | 648.08 | 0.00 | 0.00 |
| 66.00 |  | 76.82 | 642.06 | 0.00 | 0.00 |
| 68.00 |  | 76.51 | 636.02 | 0.00 | 0.00 |
| 70.00 |  | 76.19 | 629.97 | 0.00 | 0.00 |
| 72.00 |  | 75.84 | 623.91 | 0.00 | 0.00 |
| 74.00 |  | 75.48 | 617.83 | 0.00 | 0.00 |
| 76.00 |  | 75.10 | 611.75 | 0.00 | 0.00 |
| 78.00 |  | 74.70 | 605.65 | 0.00 | 0.00 |
| 80.00 |  | 74.28 | 599.53 | 0.00 | 0.00 |
| 82.00 |  | 73.85 | 593.41 | 0.00 | 0.00 |
| 84.00 |  | 73.40 | 587.28 | 0.00 | 0.00 |
| 86.00 |  | 72.94 | 581.14 | 0.00 | 0.00 |
| 88.00 |  | 72.46 | 574.99 | 0.00 | 0.00 |

[^1]
## Total Applied Force Summary

| Structure: <br> Site Name: <br> Height: <br> Base Elev: <br> Gh: | Topography: |  | Cod Exp Cre Site Stru | ht: <br> s: | EIA/TIA-222-H C 0.00 D - Stiff Soil II | 12/5/2019 Page: 27 | $((1+1))$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.00 | 71.97 | 568.83 | 0.00 | 0.00 |  |  |  |
| 90.17 | 5.96 | 47.16 | 0.00 | 0.00 |  |  |  |
| 92.00 | 66.55 | 853.08 | 0.00 | 0.00 |  |  |  |
| 94.00 | 72.12 | 920.38 | 0.00 | 0.00 |  |  |  |
| 96.00 | 71.59 | 909.72 | 0.00 | 0.00 |  |  |  |
| 98.00 | 71.05 | 489.35 | 0.00 | 0.00 |  |  |  |
| 100.00 | 70.49 | 483.97 | 0.00 | 0.00 |  |  |  |
| 102.00 | 69.93 | 478.58 | 0.00 | 0.00 |  |  |  |
| 104.00 | 69.35 | 473.18 | 0.00 | 0.00 |  |  |  |
| 106.00 | 68.76 | 467.78 | 0.00 | 0.00 |  |  |  |
| 108.00 | 68.16 | 462.37 | 0.00 | 0.00 |  |  |  |
| 110.00 | 67.55 | 456.95 | 0.00 | 0.00 |  |  |  |
| 112.00 | 66.93 | 451.52 | 0.00 | 0.00 |  |  |  |
| 114.00 | 66.30 | 446.09 | 0.00 | 0.00 |  |  |  |
| 116.00 | 65.66 | 440.66 | 0.00 | 0.00 |  |  |  |
| 118.00 | 65.01 | 435.22 | 0.00 | 0.00 |  |  |  |
| 120.00 | 64.35 | 429.77 | 0.00 | 0.00 |  |  |  |
| 122.00 | 63.68 | 424.32 | 0.00 | 0.00 |  |  |  |
| 124.00 | 63.00 | 418.86 | 0.00 | 0.00 |  |  |  |
| 126.00 | 62.31 | 413.39 | 0.00 | 0.00 |  |  |  |
| 128.00 | 61.62 | 407.92 | 0.00 | 0.00 |  |  |  |
| 130.00 | 60.91 | 402.45 | 0.00 | 0.00 |  |  |  |
| 132.00 | 60.20 | 396.97 | 0.00 | 0.00 |  |  |  |
| 133.33 | 39.71 | 261.71 | 0.00 | 0.00 |  |  |  |
| 134.00 | 20.03 | 197.43 | 0.00 | 0.00 |  |  |  |
| 136.00 | 59.68 | 586.12 | 0.00 | 0.00 |  |  |  |
| 138.00 | 58.94 | 577.36 | 0.00 | 0.00 |  |  |  |
| 140.00 | 58.20 | 309.32 | 0.00 | 0.00 |  |  |  |
| 142.00 | 57.45 | 305.04 | 0.00 | 0.00 |  |  |  |
| 144.00 | 56.69 | 300.76 | 0.00 | 0.00 |  |  |  |
| 146.00 | 55.93 | 296.47 | 0.00 | 0.00 |  |  |  |
| 148.00 | 55.16 | 292.18 | 0.00 | 0.00 |  |  |  |
| 150.00 (23) attachments | 1098.17 | 4584.38 | 0.00 | 0.00 |  |  |  |
| 152.00 | 53.60 | 263.54 | 0.00 | 0.00 |  |  |  |
| 154.00 | 52.80 | 259.24 | 0.00 | 0.00 |  |  |  |
| 156.00 | 52.00 | 254.93 | 0.00 | 0.00 |  |  |  |
| 158.00 (15) attachments | 501.84 | 2367.19 | 0.00 | 0.00 |  |  |  |
| 160.00 (15) | 50.39 | 231.33 | 0.00 | 0.00 |  |  |  |
| 162.00 | 49.57 | 227.01 | 0.00 | 0.00 |  |  |  |
| 164.00 | 48.75 | 222.69 | 0.00 | 0.00 |  |  |  |
| 166.00 (21) attachments | 1217.42 | 6599.10 | 0.00 | 0.00 |  |  |  |
| 168.00 | 47.08 | 204.88 | 0.00 | 0.00 |  |  |  |
| 170.00 | 46.24 | 200.55 | 0.00 | 0.00 |  |  |  |
| 172.00 | 45.39 | 196.21 | 0.00 | 0.00 |  |  |  |
| 174.00 | 44.53 | 191.88 | 0.00 | 0.00 |  |  |  |
| 176.00 | 43.67 | 187.53 | 0.00 | 0.00 |  |  |  |
| 178.00 (14) attachments | 987.23 | 5670.96 | 0.00 | 0.00 |  |  |  |
| 180.00 (14) | 41.94 | 173.85 | 0.00 | 0.00 |  |  |  |
| Totals: | 9,621.76 | 69,823.03 | 0.00 | 0.00 |  |  |  |



| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind |  | ${ }^{1}$ | Iterations | 27 |
| :---: | :---: | :---: | :---: | :---: |
| Dead Load Factor | 1.20 |  |  |  |
| Wind Load Factor | 1.00 |  |  |  |


| Seg <br> Elev <br> (ft) | Pu FY ( - ) (kips) | $\begin{gathered} \text { VX } \\ \text { (kXips) } \\ \text { (kX) } \end{gathered}$ | Tu MY (-) (ft-kips) | Mu MZ (ft-kips |  | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { (kn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { (kn } \\ (\text { kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \mathrm{Tn} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | $\begin{gathered} \text { Stress } \\ \text { Ratio } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -69.82 | -9.63 | 0.00 | -1165.4 | 0.00 | 1165.43 | 5123.29 | 1522.04 | 7808.40 | 6435.29 | 0.00 | 0.000 | 0.000 | 0.195 |
| 2.00 | -69.02 | -9.58 | 0.00 | -1146.1 | 0.00 | 1146.17 | 5107.67 | 1509.78 | 7683.09 | 6363.61 | 0.00 | -0.016 | 0.000 | 0.194 |
| 4.00 | -68.20 | -9.52 | 0.00 | -1127.0 | 0.00 | 1127.02 | 5091.62 | 1497.52 | 7558.79 | 6291.73 | 0.01 | -0.031 | 0.000 | 0.193 |
| 6.00 | -67.35 | -9.47 | 0.00 | -1107.9 | 0.00 | 1107.98 | 5075.16 | 1485.26 | 7435.50 | 6219.67 | 0.03 | -0.047 | 0.000 | 0.191 |
| 8.00 | -66.51 | -9.41 | 0.00 | -1089.0 | 0.00 | 1089.05 | 5058.29 | 1472.99 | 7313.22 | 6147.44 | 0.05 | -0.063 | 0.000 | 0.190 |
| 10.00 | -65.67 | -9.36 | 0.00 | -1070.2 | 0.00 | 1070.22 | 5041.00 | 1460.73 | 7191.96 | 6075.05 | 0.08 | -0.080 | 0.000 | 0.189 |
| 12.00 | -64.84 | -9.31 | 0.00 | -1051.5 | 0.00 | 1051.51 | 5023.29 | 1448.47 | 7071.72 | 6002.51 | 0.12 | -0.096 | 0.000 | 0.188 |
| 14.00 | -64.01 | -9.25 | 0.00 | -1032.9 | 0.00 | 1032.90 | 5005.16 | 1436.20 | 6952.48 | 5929.84 | 0.16 | -0.112 | 0.000 | 0.187 |
| 16.00 | -63.19 | -9.20 | 0.00 | -1014.3 | 0.00 | 1014.39 | 4986.62 | 1423.94 | 6834.27 | 5857.05 | 0.22 | -0.129 | 0.000 | 0.186 |
| 18.00 | -62.37 | -9.14 | 0.00 | -996.00 | 0.00 | 996.00 | 4967.66 | 1411.68 | 6717.06 | 5784.16 | 0.27 | -0.145 | 0.000 | 0.185 |
| 20.00 | -61.56 | -9.09 | 0.00 | -977.71 | 0.00 | 977.71 | 4948.29 | 1399.42 | 6600.87 | 5711.17 | 0.34 | -0.162 | 0.000 | 0.184 |
| 22.00 | -60.75 | -9.03 | 0.00 | -959.54 | 0.00 | 959.54 | 4928.49 | 1387.15 | 6485.69 | 5638.10 | 0.41 | -0.179 | 0.000 | 0.183 |
| 24.00 | -59.95 | -8.97 | 0.00 | -941.48 | 0.00 | 941.48 | 4908.28 | 1374.89 | 6371.53 | 5564.95 | 0.49 | -0.196 | 0.000 | 0.181 |
| 26.00 | -59.15 | -8.91 | 0.00 | -923.54 | 0.00 | 923.54 | 4887.66 | 1362.63 | 6258.37 | 5491.76 | 0.57 | -0.213 | 0.000 | 0.180 |
| 28.00 | -58.36 | -8.85 | 0.00 | -905.73 | 0.00 | 905.73 | 4866.62 | 1350.36 | 6146.24 | 5418.52 | 0.67 | -0.231 | 0.000 | 0.179 |
| 30.00 | -57.58 | -8.79 | 0.00 | -888.03 | 0.00 | 888.03 | 4845.16 | 1338.10 | 6035.11 | 5345.24 | 0.77 | -0.248 | 0.000 | 0.178 |
| 32.00 | -56.80 | -8.72 | 0.00 | -870.46 | 0.00 | 870.46 | 4823.28 | 1325.84 | 5925.00 | 5271.95 | 0.88 | -0.266 | 0.000 | 0.177 |
| 34.00 | -56.03 | -8.66 | 0.00 | -853.01 | 0.00 | 853.01 | 4800.99 | 1313.58 | 5815.91 | 5198.66 | 0.99 | -0.283 | 0.000 | 0.176 |
| 36.00 | -55.27 | -8.60 | 0.00 | -835.68 | 0.00 | 835.68 | 4778.28 | 1301.31 | 5707.83 | 5125.37 | 1.11 | -0.301 | 0.000 | 0.175 |
| 38.00 | -54.51 | -8.53 | 0.00 | -818.49 | 0.00 | 818.49 | 4755.15 | 1289.05 | 5600.76 | 5052.10 | 1.24 | -0.319 | 0.000 | 0.174 |
| 40.00 | -53.75 | -8.47 | 0.00 | -801.42 | 0.00 | 801.42 | 4731.61 | 1276.79 | 5494.70 | 4978.87 | 1.38 | -0.337 | 0.000 | 0.172 |
| 42.00 | -53.01 | -8.41 | 0.00 | -784.48 | 0.00 | 784.48 | 4707.65 | 1264.52 | 5389.66 | 4905.68 | 1.53 | -0.355 | 0.000 | 0.171 |
| 43.92 | -52.30 | -8.34 | 0.00 | -768.37 | 0.00 | 768.37 | 4684.30 | 1252.77 | 5289.95 | 4835.60 | 1.67 | -0.373 | 0.000 | 0.170 |
| 44.00 | -52.24 | -8.34 | 0.00 | -767.67 | 0.00 | 767.67 | 4683.27 | 1252.26 | 5285.64 | 4832.55 | 1.68 | -0.374 | 0.000 | 0.170 |
| 46.00 | -50.96 | -8.27 | 0.00 | -750.99 | 0.00 | 750.99 | 4658.48 | 1240.00 | 5182.62 | 4759.49 | 1.84 | -0.392 | 0.000 | 0.169 |
| 48.00 | -49.69 | -8.20 | 0.00 | -734.46 | 0.00 | 734.46 | 4633.27 | 1227.74 | 5080.62 | 4686.52 | 2.01 | -0.411 | 0.000 | 0.167 |
| 50.00 | -48.43 | -8.12 | 0.00 | -718.06 | 0.00 | 718.06 | 4607.64 | 1215.47 | 4979.64 | 4613.64 | 2.18 | -0.430 | 0.000 | 0.166 |
| 51.00 | -47.80 | -8.09 | 0.00 | -709.94 | 0.00 | 709.94 | 4157.28 | 1142.33 | 4736.69 | 4216.21 | 2.27 | -0.439 | 0.000 | 0.180 |
| 52.00 | -47.46 | -8.06 | 0.00 | -701.85 | 0.00 | 701.85 | 4146.96 | 1136.64 | 4689.60 | 4184.61 | 2.37 | -0.449 | 0.000 | 0.179 |
| 54.00 | -46.78 | -7.99 | 0.00 | -685.73 | 0.00 | 685.73 | 4126.01 | 1125.25 | 4596.10 | 4121.41 | 2.56 | -0.468 | 0.000 | 0.178 |
| 56.00 | -46.10 | -7.92 | 0.00 | -669.75 | 0.00 | 669.75 | 4104.64 | 1113.86 | 4503.55 | 4058.23 | 2.76 | -0.488 | 0.000 | 0.176 |
| 58.00 | -45.44 | -7.85 | 0.00 | -653.91 | 0.00 | 653.91 | 4082.85 | 1102.48 | 4411.95 | 3995.08 | 2.97 | -0.507 | 0.000 | 0.175 |
| 60.00 | -44.77 | -7.79 | 0.00 | -638.20 | 0.00 | 638.20 | 4060.64 | 1091.09 | 4321.28 | 3931.97 | 3.19 | -0.527 | 0.000 | 0.173 |
| 62.00 | -44.12 | -7.72 | 0.00 | -622.63 | 0.00 | 622.63 | 4038.02 | 1079.70 | 4231.55 | 3868.91 | 3.41 | -0.547 | 0.000 | 0.172 |
| 64.00 | -43.47 | -7.65 | 0.00 | -607.19 | 0.00 | 607.19 | 4014.98 | 1068.31 | 4142.77 | 3805.92 | 3.65 | -0.567 | 0.000 | 0.170 |
| 66.00 | -42.82 | -7.58 | 0.00 | -591.89 | 0.00 | 591.89 | 3991.52 | 1056.93 | 4054.92 | 3743.01 | 3.89 | -0.588 | 0.000 | 0.169 |
| 68.00 | -42.19 | -7.51 | 0.00 | -576.73 | 0.00 | 576.73 | 3967.65 | 1045.54 | 3968.02 | 3680.19 | 4.14 | -0.608 | 0.000 | 0.167 |
| 70.00 | -41.56 | -7.45 | 0.00 | -561.70 | 0.00 | 561.70 | 3943.36 | 1034.15 | 3882.06 | 3617.47 | 4.40 | -0.629 | 0.000 | 0.166 |
| 72.00 | -40.93 | -7.38 | 0.00 | -546.81 | 0.00 | 546.81 | 3918.66 | 1022.77 | 3797.04 | 3554.87 | 4.67 | -0.649 | 0.000 | 0.164 |
| 74.00 | -40.31 | -7.31 | 0.00 | -532.05 | 0.00 | 532.05 | 3893.54 | 1011.38 | 3712.96 | 3492.40 | 4.94 | -0.670 | 0.000 | 0.163 |
| 76.00 | -39.70 | -7.24 | 0.00 | -517.43 | 0.00 | 517.43 | 3868.00 | 999.99 | 3629.83 | 3430.07 | 5.23 | -0.691 | 0.000 | 0.161 |
| 78.00 | -39.09 | -7.17 | 0.00 | -502.95 | 0.00 | 502.95 | 3842.04 | 988.61 | 3547.63 | 3367.90 | 5.52 | -0.712 | 0.000 | 0.160 |
| 80.00 | -38.49 | -7.11 | 0.00 | -488.60 | 0.00 | 488.60 | 3815.67 | 977.22 | 3466.38 | 3305.90 | 5.82 | -0.733 | 0.000 | 0.158 |
| 82.00 | -37.89 | -7.04 | 0.00 | -474.39 | 0.00 | 474.39 | 3788.88 | 965.83 | 3386.07 | 3244.07 | 6.14 | -0.755 | 0.000 | 0.156 |
| 84.00 | -37.30 | -6.97 | 0.00 | -460.31 | 0.00 | 460.31 | 3761.67 | 954.44 | 3306.69 | 3182.44 | 6.46 | -0.776 | 0.000 | 0.155 |
| 86.00 | -36.72 | -6.91 | 0.00 | -446.36 | 0.00 | 446.36 | 3734.05 | 943.06 | 3228.26 | 3121.02 | 6.79 | -0.797 | 0.000 | 0.153 |
| 88.00 | -36.14 | -6.84 | 0.00 | -432.55 | 0.00 | 432.55 | 3706.01 | 931.67 | 3150.77 | 3059.82 | 7.13 | -0.819 | 0.000 | 0.151 |
| 90.00 | -35.58 | -6.77 | 0.00 | -418.88 | 0.00 | 418.88 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 7.47 | -0.841 | 0.000 | 0.149 |


| Structure: <br> Site Name: Height: <br> Base Elev: Gh: |  | $\begin{aligned} & \text { CT46130-A } \\ & \text { Deep River } \\ & 180.00 \text { (ft) } \\ & 0.000 \text { (ft) } \\ & 1.1 \end{aligned}$ |  | Topography: |  |  | Code: Exposure: Crest Height Site Class: Struct Class | EIA/TIA-222-H <br> C <br> 0.00 <br> D - Stiff Soil <br> II |  |  | 12/5/2019 <br> Page: 29 |  | $\underbrace{((1+1)))}_{\text {Tower Enginering Solutions }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.17 | -35.53 | -6.77 | 0.00 | -417.75 | 0.00 | 417.75 | 3675.16 | 919.33 | 3067.89 | 2993.77 | 7.50 | -0.843 | 0.000 | 0.149 |
| 92.00 | -34.67 | -6.70 | 0.00 | -405.35 | 0.00 | 405.35 | 3648.68 | 908.90 | 2998.62 | 2938.12 | 7.83 | -0.863 | 0.000 | 0.148 |
| 94.00 | -33.75 | -6.63 | 0.00 | -391.95 | 0.00 | 391.95 | 3619.39 | 897.51 | 2923.96 | 2877.64 | 8.20 | -0.885 | 0.000 | 0.146 |
| 96.00 | -32.84 | -6.55 | 0.00 | -378.70 | 0.00 | 378.70 | 2873.56 | 764.37 | 2506.37 | 2303.28 | 8.57 | -0.906 | 0.000 | 0.176 |
| 98.00 | -32.35 | -6.49 | 0.00 | -365.59 | 0.00 | 365.59 | 2853.66 | 754.73 | 2443.58 | 2258.25 | 8.96 | -0.929 | 0.000 | . 173 |
| 100.00 | -31.86 | -6.42 | 0.00 | -352.62 | 0.00 | 352.62 | 2833.34 | 745.10 | 2381.59 | 2213.29 | 9.35 | -0.953 | 0.000 | 0.171 |
| 102.00 | -31.38 | -6.36 | 0.00 | -339.77 | 0.00 | 339.77 | 2812.61 | 735.46 | 2320.39 | 2168.43 | 9.76 | -0.978 | 0.000 | 0.168 |
| 104.00 | -30.91 | -6.29 | 0.00 | -327.06 | 0.00 | 327.06 | 2791.46 | 725.83 | 2259.99 | 2123.68 | 10.17 | -1.003 | 0.000 | 0.165 |
| 106.00 | -30.44 | -6.23 | 0.00 | -314.47 | 0.00 | 314.47 | 2769.89 | 716.19 | 2200.39 | 2079.04 | 10.60 | -1.027 | 0.000 | 0.162 |
| 108.00 | -29.98 | -6.17 | 0.00 | -302.01 | 0.00 | 302.01 | 2747.90 | 706.55 | 2141.58 | 2034.53 | 11.03 | -1.052 | 0.000 | 0.159 |
| 110.00 | -29.52 | -6.10 | 0.00 | -289.68 | 0.00 | 289.68 | 2725.50 | 696.92 | 2083.57 | 1990.17 | 11.48 | -1.077 | 0.000 | 0.156 |
| 112.00 | -29.07 | -6.04 | 0.00 | -277.47 | 0.00 | 277.47 | 2702.68 | 687.28 | 2026.36 | 1945.97 | 11.93 | -1.102 | 0.000 | 0.153 |
| 114.00 | -28.62 | -5.98 | 0.00 | -265.39 | 0.00 | 265.39 | 2679.45 | 677.65 | 1969.94 | 1901.93 | 12.40 | -1.126 | 0.000 | 0.150 |
| 116.00 | -28.18 | -5.92 | 0.00 | -253.43 | 0.00 | 253.43 | 2655.79 | 668.01 | 1914.32 | 1858.08 | 12.88 | -1.151 | 0.000 | 0.147 |
| 118.00 | -27.74 | -5.85 | 0.00 | -241.60 | 0.00 | 241.60 | 2631.73 | 658.38 | 1859.50 | 1814.42 | 13.37 | -1.175 | 0.000 | 0.144 |
| 120.00 | -27.31 | -5.79 | 0.00 | -229.90 | 0.00 | 229.90 | 2607.24 | 648.74 | 1805.47 | 1770.96 | 13.86 | -1.200 | 0.000 | 0.140 |
| 122.00 | -26.88 | -5.73 | 0.00 | -218.31 | 0.00 | 218.31 | 2582.34 | 639.11 | 1752.24 | 1727.73 | 14.37 | -1.224 | 0.000 | 0.137 |
| 124.00 | -26.46 | -5.67 | 0.00 | -206.85 | 0.00 | 206.85 | 2557.02 | 629.47 | 1699.80 | 1684.74 | 14.89 | -1.248 | 0.000 | 0.133 |
| 126.00 | -26.05 | -5.61 | 0.00 | -195.52 | 0.00 | 195.52 | 2531.28 | 619.84 | 1648.16 | 1641.98 | 15.42 | -1.272 | 0.000 | 0.129 |
| 128.00 | -25.64 | -5.55 | 0.00 | -184.30 | 0.00 | 184.30 | 2505.13 | 610.20 | 1597.32 | 1599.49 | 15.96 | -1.296 | 0.000 | 0.126 |
| 130.00 | -25.24 | -5.49 | 0.00 | -173.20 | 0.00 | 173.20 | 2478.56 | 600.57 | 1547.28 | 1557.27 | 16.50 | -1.319 | 0.000 | 0.121 |
| 132.00 | -24.84 | -5.43 | 0.00 | -162.22 | 0.00 | 162.22 | 2451.58 | 590.93 | 1498.03 | 1515.33 | 17.06 | -1.342 | 0.000 | 0.117 |
| 133.33 | -24.58 | -5.39 | 0.00 | -154.99 | 0.00 | 154.99 | 2433.35 | 584.51 | 1465.64 | 1487.53 | 17.44 | -1.357 | 0.000 | 0.114 |
| 134.00 | -24.38 | -5.37 | 0.00 | -151.40 | 0.00 | 151.40 | 2424.17 | 581.30 | 1449.58 | 1473.69 | 17.63 | -1.364 | 0.000 | 0.113 |
| 136.00 | -23.79 | -5.30 | 0.00 | -140.66 | 0.00 | 140.66 | 2396.35 | 571.66 | 1401.92 | 1432.35 | 18.20 | -1.386 | 0.000 | 0.108 |
| 138.00 | -23.22 | -5.24 | 0.00 | -130.05 | 0.00 | 130.05 | 1545.45 | 417.14 | 1026.36 | 929.77 | 18.79 | -1.408 | 0.000 | 0.155 |
| 140.00 | -22.91 | -5.18 | 0.00 | -119.57 | 0.00 | 119.57 | 1531.69 | 410.13 | 992.17 | 905.88 | 19.38 | -1.428 | 0.000 | 0.147 |
| 142.00 | -22.60 | -5.13 | 0.00 | -109.21 | 0.00 | 109.21 | 1517.50 | 403.12 | 958.56 | 882.03 | 19.99 | -1.454 | 0.000 | 0.139 |
| 144.00 | -22.30 | -5.07 | 0.00 | -98.95 | 0.00 | 98.95 | 1502.90 | 396.11 | 925.52 | 858.22 | 20.60 | -1.479 | 0.000 | 0.130 |
| 146.00 | -22.00 | -5.02 | 0.00 | -88.81 | 0.00 | 88.81 | 1487.88 | 389.11 | 893.06 | 834.49 | 21.23 | -1.503 | 0.000 | 0.121 |
| 148.00 | -21.71 | -4.96 | 0.00 | -78.77 | 0.00 | 78.77 | 1472.45 | 382.10 | 861.19 | 810.82 | 21.86 | -1.525 | 0.000 | 0.112 |
| 150.00 | -17.16 | -3.75 | 0.00 | -68.84 | 0.00 | 68.84 | 1456.60 | 375.09 | 829.89 | 787.25 | 22.51 | -1.546 | 0.000 | 0.099 |
| 152.00 | -16.89 | -3.69 | 0.00 | -61.35 | 0.00 | 61.35 | 1440.33 | 368.08 | 799.17 | 763.78 | 23.16 | -1.565 | 0.000 | 0.092 |
| 154.00 | -16.63 | -3.64 | 0.00 | -53.96 | 0.00 | 53.96 | 1423.65 | 361.08 | 769.03 | 740.42 | 23.82 | -1.583 | 0.000 | 0.085 |
| 156.00 | -16.38 | -3.58 | 0.00 | -46.68 | 0.00 | 46.68 | 1406.55 | 354.07 | 739.47 | 717.20 | 24.48 | -1.600 | 0.000 | 0.077 |
| 158.00 | -14.03 | -3.02 | 0.00 | -39.51 | 0.00 | 39.51 | 1389.03 | 347.06 | 710.49 | 694.11 | 25.16 | -1.615 | 0.000 | 0.067 |
| 160.00 | -13.80 | -2.97 | 0.00 | -33.48 | 0.00 | 33.48 | 1371.10 | 340.05 | 682.09 | 671.17 | 25.84 | -1.628 | 0.000 | 0.060 |
| 162.00 | -13.57 | -2.91 | 0.00 | -27.54 | 0.00 | 27.54 | 1352.75 | 333.05 | 654.27 | 648.41 | 26.52 | -1.640 | 0.000 | 0.053 |
| 164.00 | -13.35 | -2.86 | 0.00 | -21.72 | 0.00 | 21.72 | 1333.98 | 326.04 | 627.03 | 625.81 | 27.21 | -1.651 | 0.000 | 0.045 |
| 166.00 | -6.79 | -1.45 | 0.00 | -16.00 | 0.00 | 16.00 | 1314.79 | 319.03 | 600.37 | 603.42 | 27.90 | -1.659 | 0.000 | 0.032 |
| 168.00 | -6.58 | -1.40 | 0.00 | -13.09 | 0.00 | 13.09 | 1295.19 | 312.03 | 574.28 | 581.22 | 28.60 | -1.666 | 0.000 | 0.028 |
| 170.00 | -6.38 | -1.35 | 0.00 | -10.29 | 0.00 | 10.29 | 1275.17 | 305.02 | 548.78 | 559.24 | 29.30 | -1.672 | 0.000 | 0.023 |
| 172.00 | -6.19 | -1.30 | 0.00 | -7.59 | 0.00 | 7.59 | 1251.65 | 298.01 | 523.85 | 536.17 | 30.00 | -1.677 | 0.000 | 0.019 |
| 174.00 | -6.00 | -1.25 | 0.00 | -4.99 | 0.00 | 4.99 | 1222.21 | 291.00 | 499.51 | 511.11 | 30.71 | -1.681 | 0.000 | 0.015 |
| 176.00 | -5.81 | -1.20 | 0.00 | -2.49 | 0.00 | 2.49 | 1192.78 | 284.00 | 475.74 | 486.64 | 31.41 | -1.683 | 0.000 | 0.010 |
| 178.00 | -0.17 | -0.05 | 0.00 | -0.09 | 0.00 | 0.09 | 1163.35 | 276.99 | 452.55 | 462.78 | 32.12 | -1.684 | 0.000 | 0.000 |
| 180.00 | 0.00 | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 1133.92 | 269.98 | 429.95 | 439.52 | 32.82 | -1.684 | 0.000 | 0.000 |




[^2]
## Calculated Forces

| Structure: <br> Site Name: Height: <br> Base Elev: Gh: |  | CT46130 <br> Deep Riv <br> 180.00 (ft <br> 0.000 (ft) <br> 1.1 |  | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  |  |  | EIA/TIA-222-H $.00$ <br> D - Stiff Soil |  | 12/5/2019 <br> Page: 32 |  | $\xlongequal[\text { Tower Enginering Solutions }]{(((1) \mid N))}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Case: 1.2D + 1.0Ev Gust Response Factor Dead Load Factor Wind Load Factor |  |  |  | + 1.0Eh $1.10$ <br> 1.20 <br> 0.00 | Seis <br> Struc | Load Fac Frequen | (f1) | $\begin{aligned} & 1.00 \\ & 0.31 \\ & \hline \end{aligned}$ | ds 0.2 <br> Sd1 0.09 <br> SA 0. | Seis |  | $\rightarrow$ | erations Ss <br> S1 <br> Factor | $\begin{array}{r} 26 \\ 0.21 \\ 0.05 \\ 1.00 \\ \hline \end{array}$ |
| Seg <br> Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \end{gathered}$ (kios) | $\begin{aligned} & \begin{array}{l} \mathbf{V u} \\ \text { FX (-) } \\ \text { (kios) } \end{array} \end{aligned}$ | $\underset{\substack{\mathrm{MY}(-) \\ \text { (tt-kips) }}}{\substack{\text { an }}}$ | Mu MZ ft-kips) | $\begin{gathered} \text { Mu } \\ \text { MX } \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kios) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \mathbf{V n} \\ \text { (kips) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation Sway (dea) | Rotation Twist (dea) | $\begin{aligned} & \text { Stress } \\ & \text { Ratio } \\ & \hline \end{aligned}$ |
| 0.00 | -56.49 | -4.48 | 0.00 | -527.40 | 0.00 | 527.40 | 5123.29 | 1522.04 | 7808.40 | 6435.29 |  | 0.00 | 0.00 | 0.093 |
| 2.00 | -55.78 | -4.45 | 0.00 | -518.44 | 0.00 | 518.44 | 5107.67 | 1509.78 | 7683.09 | 6363.61 |  | 0.00 | -0.01 | 0.092 |
| 4.00 | -55.06 | -4.42 | 0.00 | -509.54 | 0.00 | 509.54 | 5091.62 | 1497.52 | 7558.79 | 6291.73 |  | 0.01 | -0.01 | 0.092 |
| 6.00 | -54.31 | -4.39 | 0.00 | -500.69 | 0.00 | 500.69 | 5075.16 | 1485.26 | 7435.50 | 6219.67 |  | 0.01 | -0.02 | 0.091 |
| 8.00 | -53.58 | -4.35 | 0.00 | -491.92 | 0.00 | 491.92 | 5058.29 | 1472.99 | 7313.22 | 6147.44 |  | 0.02 | -0.03 | 0.091 |
| 10.00 | -52.84 | -4.31 | 0.00 | -483.22 | 0.00 | 483.22 | 5041.00 | 1460.73 | 7191.96 | 6075.05 |  | 0.04 | -0.04 | 0.090 |
| 12.00 | -52.12 | -4.27 | 0.00 | -474.60 | 0.00 | 474.60 | 5023.29 | 1448.47 | 7071.72 | 6002.51 |  | 0.05 | -0.04 | 0.089 |
| 14.00 | -51.40 | -4.23 | 0.00 | -466.06 | 0.00 | 466.06 | 5005.16 | 1436.20 | 6952.48 | 5929.84 |  | 0.07 | -0.05 | 0.089 |
| 16.00 | -50.68 | -4.19 | 0.00 | -457.60 | 0.00 | 457.60 | 4986.62 | 1423.94 | 6834.27 | 5857.05 |  | 0.10 | -0.06 | 0.088 |
| 18.00 | -49.97 | -4.15 | 0.00 | -449.23 | 0.00 | 449.23 | 4967.66 | 1411.68 | 6717.06 | 5784.16 |  | 0.12 | -0.07 | 0.088 |
| 20.00 | -49.27 | -4.10 | 0.00 | -440.93 | 0.00 | 440.93 | 4948.29 | 1399.42 | 6600.87 | 5711.17 |  | 0.15 | -0.07 | 0.087 |
| 22.00 | -48.57 | -4.06 | 0.00 | -432.73 | 0.00 | 432.73 | 4928.49 | 1387.15 | 6485.69 | 5638.10 |  | 0.18 | -0.08 | 0.087 |
| 24.00 | -47.88 | -4.02 | 0.00 | -424.60 | 0.00 | 424.60 | 4908.28 | 1374.89 | 6371.53 | 5564.95 |  | 0.22 | -0.09 | 0.086 |
| 26.00 | -47.19 | -3.98 | 0.00 | -416.56 | 0.00 | 416.56 | 4887.66 | 1362.63 | 6258.37 | 5491.76 |  | 0.26 | -0.10 | 0.086 |
| 28.00 | -46.51 | -3.94 | 0.00 | -408.60 | 0.00 | 408.60 | 4866.62 | 1350.36 | 6146.24 | 5418.52 |  | 0.30 | -0.10 | 0.085 |
| 30.00 | -45.84 | -3.89 | 0.00 | -400.73 | 0.00 | 400.73 | 4845.16 | 1338.10 | 6035.11 | 5345.24 |  | 0.35 | -0.11 | 0.084 |
| 32.00 | -45.17 | -3.85 | 0.00 | -392.95 | 0.00 | 392.95 | 4823.28 | 1325.84 | 5925.00 | 5271.95 |  | 0.40 | -0.12 | 0.084 |
| 34.00 | -44.50 | -3.81 | 0.00 | -385.24 | 0.00 | 385.24 | 4800.99 | 1313.58 | 5815.91 | 5198.66 |  | 0.45 | -0.13 | 0.083 |
| 36.00 | -43.84 | -3.77 | 0.00 | -377.62 | 0.00 | 377.62 | 4778.28 | 1301.31 | 5707.83 | 5125.37 |  | 0.50 | -0.14 | 0.083 |
| 38.00 | -43.19 | -3.73 | 0.00 | -370.08 | 0.00 | 370.08 | 4755.15 | 1289.05 | 5600.76 | 5052.10 |  | 0.56 | -0.14 | 0.082 |
| 40.00 | -42.55 | -3.69 | 0.00 | -362.63 | 0.00 | 362.63 | 4731.61 | 1276.79 | 5494.70 | 4978.87 |  | 0.62 | -0.15 | 0.082 |
| 42.00 | -41.91 | -3.64 | 0.00 | -355.26 | 0.00 | 355.26 | 4707.65 | 1264.52 | 5389.66 | 4905.68 |  | 0.69 | -0.16 | 0.081 |
| 43.92 | -41.30 | -3.60 | 0.00 | -348.27 | 0.00 | 348.27 | 4684.30 | 1252.77 | 5289.95 | 4835.60 |  | 0.76 | -0.17 | 0.081 |
| 44.00 | -41.25 | -3.60 | 0.00 | -347.97 | 0.00 | 347.97 | 4683.27 | 1252.26 | 5285.64 | 4832.55 |  | 0.76 | -0.17 | 0.081 |
| 46.00 | -40.07 | -3.52 | 0.00 | -340.77 | 0.00 | 340.77 | 4658.48 | 1240.00 | 5182.62 | 4759.49 |  | 0.83 | -0.18 | 0.080 |
| 48.00 | -38.90 | -3.43 | 0.00 | -333.74 | 0.00 | 333.74 | 4633.27 | 1227.74 | 5080.62 | 4686.52 |  | 0.91 | -0.19 | 0.080 |
| 50.00 | -37.75 | -3.34 | 0.00 | -326.87 | 0.00 | 326.87 | 4607.64 | 1215.47 | 4979.64 | 4613.64 |  | 0.99 | -0.19 | 0.079 |
| 51.00 | -37.18 | -3.30 | 0.00 | -323.53 | 0.00 | 323.53 | 4157.28 | 1142.33 | 4736.69 | 4216.21 |  | 1.03 | -0.20 | 0.086 |
| 52.00 | -36.89 | -3.28 | 0.00 | -320.23 | 0.00 | 320.23 | 4146.96 | 1136.64 | 4689.60 | 4184.61 |  | 1.07 | -0.20 | 0.085 |
| 54.00 | -36.31 | -3.25 | 0.00 | -313.66 | 0.00 | 313.66 | 4126.01 | 1125.25 | 4596.10 | 4121.41 |  | 1.16 | -0.21 | 0.085 |
| 56.00 | -35.74 | -3.21 | 0.00 | -307.16 | 0.00 | 307.16 | 4104.64 | 1113.86 | 4503.55 | 4058.23 |  | 1.25 | -0.22 | 0.084 |
| 58.00 | -35.18 | -3.17 | 0.00 | -300.75 | 0.00 | 300.75 | 4082.85 | 1102.48 | 4411.95 | 3995.08 |  | 1.34 | -0.23 | 0.084 |
| 60.00 | -34.62 | -3.13 | 0.00 | -294.40 | 0.00 | 294.40 | 4060.64 | 1091.09 | 4321.28 | 3931.97 |  | 1.44 | -0.24 | 0.083 |
| 62.00 | -34.06 | -3.10 | 0.00 | -288.13 | 0.00 | 288.13 | 4038.02 | 1079.70 | 4231.55 | 3868.91 |  | 1.54 | -0.25 | 0.083 |
| 64.00 | -33.51 | -3.06 | 0.00 | -281.94 | 0.00 | 281.94 | 4014.98 | 1068.31 | 4142.77 | 3805.92 |  | 1.65 | -0.26 | 0.082 |
| 66.00 | -32.97 | -3.03 | 0.00 | -275.82 | 0.00 | 275.82 | 3991.52 | 1056.93 | 4054.92 | 3743.01 |  | 1.76 | -0.27 | 0.082 |
| 68.00 | -32.43 | -2.99 | 0.00 | -269.77 | 0.00 | 269.77 | 3967.65 | 1045.54 | 3968.02 | 3680.19 |  | 1.87 | -0.28 | 0.081 |
| 70.00 | -31.90 | -2.96 | 0.00 | -263.79 | 0.00 | 263.79 | 3943.36 | 1034.15 | 3882.06 | 3617.47 |  | 1.99 | -0.29 | 0.081 |
| 72.00 | -31.37 | -2.92 | 0.00 | -257.88 | 0.00 | 257.88 | 3918.66 | 1022.77 | 3797.04 | 3554.87 |  | 2.11 | -0.30 | 0.081 |
| 74.00 | -30.84 | -2.89 | 0.00 | -252.03 | 0.00 | 252.03 | 3893.54 | 1011.38 | 3712.96 | 3492.40 |  | 2.24 | -0.31 | 0.080 |
| 76.00 | -30.33 | -2.86 | 0.00 | -246.25 | 0.00 | 246.25 | 3868.00 | 999.99 | 3629.83 | 3430.07 |  | 2.37 | -0.32 | 0.080 |
| 78.00 | -29.82 | -2.83 | 0.00 | -240.53 | 0.00 | 240.53 | 3842.04 | 988.61 | 3547.63 | 3367.90 |  | 2.50 | -0.33 | 0.079 |
| 80.00 | -29.31 | -2.80 | 0.00 | -234.87 | 0.00 | 234.87 | 3815.67 | 977.22 | 3466.38 | 3305.90 |  | 2.64 | -0.34 | 0.079 |
| 82.00 | -28.81 | -2.78 | 0.00 | -229.26 | 0.00 | 229.26 | 3788.88 | 965.83 | 3386.07 | 3244.07 |  | 2.78 | -0.35 | 0.078 |
| 84.00 | -28.31 | -2.76 | 0.00 | -223.70 | 0.00 | 223.70 | 3761.67 | 954.44 | 3306.69 | 3182.44 |  | 2.93 | -0.36 | 0.078 |
| 86.00 | -27.82 | -2.74 | 0.00 | -218.18 | 0.00 | 218.18 | 3734.05 | 943.06 | 3228.26 | 3121.02 |  | 3.08 | -0.37 | 0.077 |
| 88.00 | -27.3 | -2.72 | 0.00 | -212.71 | 0.00 | 212.71 | 3706.01 | 931.67 | 3150.77 | 3059.82 |  | 3.24 | -0.38 | 0.077 |


| Structure: <br> Site Name: Height: <br> Base Elev: Gh: |  | CT46130-A <br> Deep River <br> 180.00 (ft) <br> 0.000 (ft) <br> 1.1 |  | Topography: |  | 1 | Code: Exposure: Crest Height: Site Class: Struct Class: | EIA/TIA-222-H <br> C $0.00$ <br> D - Stiff Soil <br> : II |  |  | 12/5/2019 Page: 33 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.00 | -26.85 | -2.70 | 0.00 | -207.27 | 0.00 | 207.27 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 3.40 | -0.39 | 0.076 |
| 90.17 | -26.81 | -2.70 | 0.00 | -206.82 | 0.00 | 206.82 | 3675.16 | 919.33 | 3067.89 | 2993.77 | 3.41 | -0.39 | 0.076 |
| 92.00 | -26.04 | -2.68 | 0.00 | -201.86 | 0.00 | 201.86 | 3648.68 | 908.90 | 2998.62 | 2938.12 | 3.56 | -0.40 | . 076 |
| 94.00 | -25.21 | -2.66 | 0.00 | -196.49 | 0.00 | 196.49 | 3619.39 | 897.51 | 2923.96 | 2877,64 | 3.73 | -0.41 | 0.075 |
| 96.00 | -24.39 | -2.64 | 0.00 | -191.17 | 0.00 | 191.17 | 2873.56 | 764.37 | 2506.37 | 2303.28 | 3.91 | -0.42 | 0.091 |
| 98.00 | -23.98 | -2.64 | 0.00 | -185.89 | 0.00 | 185.89 | 2853.66 | 754.73 | 2443.58 | 2258.25 | 4.09 | -0.43 | 0.091 |
| 100.00 | -23.59 | -2.64 | 0.00 | -180.60 | 0.00 | 180.60 | 2833.34 | 745.10 | 2381.59 | 2213.29 | 4.27 | -0.44 | 0.090 |
| 102.00 | -23.19 | -2.64 | 0.00 | -175.32 | 0.00 | 175.32 | 2812.61 | 735.46 | 2320.39 | 2168.43 | 4.46 | -0.46 | 0.089 |
| 104.00 | -22.80 | -2.64 | 0.00 | -170.04 | 0.00 | 170.04 | 2791.46 | 725.83 | 2259.99 | 2123.68 | 4.65 | -0.47 | 0.088 |
| 106.00 | -22.42 | -2.65 | 0.00 | -164.75 | 0.00 | 164.75 | 2769.89 | 716.19 | 2200.39 | 2079.04 | 4.85 | -0.48 | 0.087 |
| 108.00 | -22.04 | -2.65 | 0.00 | -159.46 | 0.00 | 159.46 | 2747.90 | 706.55 | 2141.58 | 2034.53 | 5.06 | -0.50 | 0.086 |
| 110.00 | -21.66 | -2.65 | 0.00 | -154.17 | 0.00 | 154.17 | 2725.50 | 696.92 | 2083.57 | 1990.17 | 5.27 | -0.51 | 0.085 |
| 112.00 | -21.29 | -2.65 | 0.00 | -148.87 | 0.00 | 148.87 | 2702.68 | 687.28 | 2026.36 | 1945.97 | 5.49 | -0.52 | 0.084 |
| 114.00 | -20.92 | -2.65 | 0.00 | -143.57 | 0.00 | 143.57 | 2679.45 | 677.65 | 1969.94 | 1901.93 | 5.71 | -0.54 | 0.083 |
| 116.00 | -20.56 | -2.65 | 0.00 | -138.27 | 0.00 | 138.27 | 2655.79 | 668.01 | 1914.32 | 1858.08 | 5.93 | -0.55 | 0.082 |
| 118.00 | -20.20 | -2.65 | 0.00 | -132.96 | 0.00 | 132.96 | 2631.73 | 658.38 | 1859.50 | 1814.42 | 6.17 | -0.56 | 0.081 |
| 120.00 | -19.85 | -2.66 | 0.00 | -127.66 | 0.00 | 127.66 | 2607.24 | 648.74 | 1805.47 | 1770.96 | 6.41 | -0.58 | 0.080 |
| 122.00 | -19.50 | -2.66 | 0.00 | -122.34 | 0.00 | 122.34 | 2582.34 | 639.11 | 1752.24 | 1727.73 | 6.65 | -0.59 | 0.078 |
| 124.00 | -19.15 | -2.66 | 0.00 | -117.03 | 0.00 | 117.03 | 2557.02 | 629.47 | 1699.80 | 1684.74 | 6.90 | -0.60 | 0.077 |
| 126.00 | -18.81 | -2.66 | 0.00 | -111.71 | 0.00 | 111.71 | 2531.28 | 619.84 | 1648.16 | 1641.98 | 7.16 | -0.62 | 0.075 |
| 128.00 | -18.47 | -2.66 | 0.00 | -106.40 | 0.00 | 106.40 | 2505.13 | 610.20 | 1597.32 | 1599.49 | 7.42 | -0.63 | 0.074 |
| 130.00 | -18.14 | -2.66 | 0.00 | -101.08 | 0.00 | 101.08 | 2478.56 | 600.57 | 1547.28 | 1557.27 | 7.68 | -0.64 | 0.072 |
| 132.00 | -17.82 | -2.66 | 0.00 | -95.76 | 0.00 | 95.76 | 2451.58 | 590.93 | 1498.03 | 1515.33 | 7.96 | -0.66 | 0.070 |
| 133.33 | -17.60 | -2.65 | 0.00 | -92.22 | 0.00 | 92.22 | 2433.35 | 584.51 | 1465.64 | 1487.53 | 8.14 | -0.67 | 0.069 |
| 134.00 | -17.43 | -2.65 | 0.00 | -90.45 | 0.00 | 90.45 | 2424.17 | 581.30 | 1449.58 | 1473.69 | 8.24 | -0.67 | 0.069 |
| 136.00 | -16.91 | -2.64 | 0.00 | -85.15 | 0.00 | 85.15 | 2396.35 | 571.66 | 1401.92 | 1432.35 | 8.52 | -0.68 | 0.067 |
| 138.00 | -16.40 | -2.63 | 0.00 | -79.87 | 0.00 | 79.87 | 1545.45 | 417.14 | 1026.36 | 929.77 | 8.81 | -0.70 | 0.097 |
| 140.00 | -16.16 | -2.62 | 0.00 | -74.61 | 0.00 | 74.61 | 1531.69 | 410.13 | 992.17 | 905.88 | 9.10 | -0.71 | 0.093 |
| 142.00 | -15.92 | -2.62 | 0.00 | -69.36 | 0.00 | 69.36 | 1517.50 | 403.12 | 958.56 | 882.03 | 9.40 | -0.73 | 0.089 |
| 144.00 | -15.68 | -2.61 | 0.00 | -64.13 | 0.00 | 64.13 | 1502.90 | 396.11 | 925.52 | 858.22 | 9.71 | -0.74 | 0.085 |
| 146.00 | -15.45 | -2.60 | 0.00 | -58.91 | 0.00 | 58.91 | 1487.88 | 389.11 | 893.06 | 834.49 | 10.03 | -0.76 | 0.081 |
| 148.00 | -15.22 | -2.59 | 0.00 | -53.71 | 0.00 | 53.71 | 1472.45 | 382.10 | 861.19 | 810.82 | 10.35 | -0.77 | 0.077 |
| 150.00 | -12.03 | -2.33 | 0.00 | -48.52 | 0.00 | 48.52 | 1456.60 | 375.09 | 829.89 | 787.25 | 10.67 | -0.79 | 0.070 |
| 152.00 | -11.83 | -2.32 | 0.00 | -43.86 | 0.00 | 43.86 | 1440.33 | 368.08 | 799.17 | 763.78 | 11.01 | -0.80 | 0.066 |
| 154.00 | -11.63 | -2.30 | 0.00 | -39.22 | 0.00 | 39.22 | 1423.65 | 361.08 | 769.03 | 740.42 | 11.34 | -0.81 | 0.061 |
| 156.00 | -11.43 | -2.29 | 0.00 | -34.62 | 0.00 | 34.62 | 1406.55 | 354.07 | 739.47 | 717.20 | 11.69 | -0.83 | 0.056 |
| 158.00 | -9.74 | -2.08 | 0.00 | -30.05 | 0.00 | 30.05 | 1389.03 | 347.06 | 710.49 | 694.11 | 12.04 | -0.84 | 0.050 |
| 160.00 | -9.57 | -2.06 | 0.00 | -25.89 | 0.00 | 25.89 | 1371.10 | 340.05 | 682.09 | 671.17 | 12.39 | -0.85 | 0.046 |
| 162.00 | -9.40 | -2.04 | 0.00 | -21.77 | 0.00 | 21.77 | 1352.75 | 333.05 | 654.27 | 648.41 | 12.75 | -0.86 | 0.041 |
| 164.00 | -9.23 | -2.01 | 0.00 | -17.70 | 0.00 | 17.70 | 1333.98 | 326.04 | 627.03 | 625.81 | 13.11 | -0.87 | 0.035 |
| 166.00 | -4.64 | -1.21 | 0.00 | -13.67 | 0.00 | 13.67 | 1314.79 | 319.03 | 600.37 | 603.42 | 13.47 | -0.87 | 0.026 |
| 168.00 | -4.49 | -1.18 | 0.00 | -11.26 | 0.00 | 11.26 | 1295.19 | 312.03 | 574.28 | 581.22 | 13.84 | -0.88 | 0.023 |
| 170.00 | -4.34 | -1.15 | 0.00 | -8.90 | 0.00 | 8.90 | 1275.17 | 305.02 | 548.78 | 559.24 | 14.21 | -0.88 | 0.019 |
| 172.00 | -4.20 | -1.12 | 0.00 | -6.60 | 0.00 | 6.60 | 1251.65 | 298.01 | 523.85 | 536.17 | 14.58 | -0.89 | 0.016 |
| 174.00 | -4.06 | -1.09 | 0.00 | -4.36 | 0.00 | 4.36 | 1222.21 | 291.00 | 499.51 | 511.11 | 14.95 | -0.89 | 0.012 |
| 176,00 | -3.92 | -1.05 | 0.00 | -2.18 | 0.00 | 2.18 | 1192.78 | 284.00 | 475.74 | 486.64 | 15.32 | -0.89 | 0.008 |
| 178.00 | -0.13 | -0.04 | 0.00 | -0.07 | 0.00 | 0.07 | 1163.35 | 276.99 | 452.55 | 462.78 | 15.70 | -0.89 | 0.000 |
| 180.00 | 0.00 | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 1133.92 | 269.98 | 429.95 | 439.52 | 16.07 | -0.89 | 0.000 |

Seismic Segment Forces (Factored)



## Seismic Segment Forces (Factored)




| Structure: <br> Site Name: <br> Height: <br> Base Elev: <br> Gh: |  | CT46130-A <br> Deep River- <br> 180.00 (ft) <br> 0.000 (ft) <br> 1.1 |  | Topography: |  |  | Code: Exposure: Crest Height: Site Class: Struct Class: | EIA/TIA-222-H <br> C $0.00$ <br> D - Stiff Soil <br> II |  |  | 12/5/2019 Page: 37 |  | olutions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.00 | -20.14 | -2.66 | 0.00 | -203.29 | 0.00 | 203.29 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 3.35 | -0.38 | 0.073 |
| 90.17 | -20.11 | -2.66 | 0.00 | -202.85 | 0.00 | 202.85 | 3675.16 | 919.33 | 3067.89 | 2993.77 | 3.36 | -0.38 | 0.073 |
| 92.00 | -19.53 | -2.63 | 0.00 | -197.98 | 0.00 | 197.98 | 3648.68 | 908.90 | 2998.62 | 2938.12 | 3.51 | -0.39 | 0.073 |
| 94.00 | -18.90 | -2.61 | 0.00 | -192.72 | 0.00 | 192.72 | 3619.39 | 897.51 | 2923.96 | 2877.64 | 3.68 | -0.40 | 0.072 |
| 96.00 | -18.29 | -2.60 | 0.00 | -187.49 | 0.00 | 187.49 | 2873.56 | 764.37 | 2506.37 | 2303.28 | 3.85 | -0.41 | 0.088 |
| 98.00 | -17.98 | -2.59 | 0.00 | -182.30 | 0.00 | 182.30 | 2853.66 | 754.73 | 2443.58 | 2258.25 | 4.02 | -0.42 | 0.087 |
| 100.00 | -17.68 | -2.59 | 0.00 | -177.11 | 0.00 | 177.11 | 2833.34 | 745.10 | 2381.59 | 2213.29 | 4.20 | -0.44 | 0.086 |
| 102.00 | -17.39 | -2.59 | 0.00 | -171.93 | 0.00 | 171.93 | 2812.61 | 735.46 | 2320.39 | 2168.43 | 4.39 | -0.45 | 0.085 |
| 104.00 | -17.10 | -2.59 | 0.00 | -166.75 | 0.00 | 166.75 | 2791.46 | 725.83 | 2259.99 | 2123.68 | 4.58 | -0.46 | 0.085 |
| 106.00 | -16.81 | -2.59 | 0.00 | -161.56 | 0.00 | 161.56 | 2769.89 | 716.19 | 2200.39 | 2079.04 | 4.78 | -0.47 | 0.084 |
| 108.00 | -16.52 | -2.60 | 0.00 | -156.37 | 0.00 | 156.37 | 2747.90 | 706.55 | 2141.58 | 2034.53 | 4.98 | -0.49 | 0.083 |
| 110.00 | -16.24 | -2.60 | 0.00 | -151.18 | 0.00 | 151.18 | 2725.50 | 696.92 | 2083.57 | 1990.17 | 5.18 | -0.50 | 0.082 |
| 112.00 | -15.96 | -2.60 | 0.00 | -145.98 | 0.00 | 145.98 | 2702.68 | 687.28 | 2026.36 | 1945.97 | 5.40 | -0.51 | 0.081 |
| 114.00 | -15.68 | -2.60 | 0.00 | -140.78 | 0.00 | 140.78 | 2679.45 | 677.65 | 1969.94 | 1901.93 | 5.62 | -0.53 | 0.080 |
| 116.00 | -15.41 | -2.60 | 0.00 | -135.59 | 0.00 | 135.59 | 2655.79 | 668.01 | 1914.32 | 1858.08 | 5.84 | -0.54 | 0.079 |
| 118.00 | -15.14 | -2.60 | 0.00 | -130.38 | 0.00 | 130.38 | 2631.73 | 658.38 | 1859.50 | 1814.42 | 6.07 | -0.55 | 0.078 |
| 120.00 | -14.88 | -2.60 | 0.00 | -125.18 | 0.00 | 125.18 | 2607.24 | 648.74 | 1805.47 | 1770.96 | 6.30 | -0.57 | 0.076 |
| 122.00 | -14.62 | -2.60 | 0.00 | -119.98 | 0.00 | 119.98 | 2582.34 | 639.11 | 1752.24 | 1727.73 | 6.54 | -0.58 | 0.075 |
| 124.00 | -14.36 | -2.60 | 0.00 | -114.77 | 0.00 | 114.77 | 2557.02 | 629.47 | 1699.80 | 1684.74 | 6.79 | -0.59 | 0.074 |
| 126.00 | -14.10 | -2.60 | 0.00 | -109.56 | 0.00 | 109.56 | 2531.28 | 619.84 | 1648.16 | 1641.98 | 7.04 | -0.61 | 0.072 |
| 128.00 | -13.85 | -2.61 | 0.00 | -104.35 | 0.00 | 104.35 | 2505.13 | 610.20 | 1597.32 | 1599.49 | 7.30 | -0.62 | 0.071 |
| 130.00 | -13.60 | -2.60 | 0.00 | -99.14 | 0.00 | 99.14 | 2478.56 | 600.57 | 1547.28 | 1557.27 | 7.56 | -0.63 | 0.069 |
| 132.00 | -13.36 | -2.60 | 0.00 | -93.93 | 0.00 | 93.93 | 2451.58 | 590.93 | 1498.03 | 1515.33 | 7.83 | -0.65 | 0.067 |
| 133.33 | -13.19 | -2.60 | 0.00 | -90.46 | 0.00 | 90.46 | 2433.35 | 584.51 | 1465.64 | 1487.53 | 8.01 | -0.65 | 0.066 |
| 134.00 | -13.06 | -2.60 | 0.00 | -88.73 | 0.00 | 88.73 | 2424.17 | 581.30 | 1449.58 | 1473.69 | 8.10 | -0.66 | 0.066 |
| 136.00 | -12.68 | -2.59 | 0.00 | -83.53 | 0.00 | 83.53 | 2396.35 | 571.66 | 1401.92 | 1432.35 | 8.38 | -0.67 | 0.064 |
| 138.00 | -12.29 | -2.57 | 0.00 | -78.36 | 0.00 | 78.36 | 1545.45 | 417.14 | 1026.36 | 929.77 | 8.66 | -0.68 | 0.092 |
| 140.00 | -12.11 | -2.57 | 0.00 | -73.21 | 0.00 | 73.21 | 1531.69 | 410.13 | 992.17 | 905.88 | 8.95 | -0.70 | 0.089 |
| 142.00 | -11.93 | -2.56 | 0.00 | -68.07 | 0.00 | 68.07 | 1517.50 | 403.12 | 958.56 | 882.03 | 9.25 | -0.71 | 0.085 |
| 144.00 | -11.76 | -2.56 | 0.00 | -62.94 | 0.00 | 62.94 | 1502.90 | 396.11 | 925.52 | 858.22 | 9.55 | -0.73 | 0.081 |
| 146.00 | -11.58 | -2.55 | 0.00 | -57.83 | 0.00 | 57.83 | 1487.88 | 389.11 | 893.06 | 834.49 | 9.86 | -0.74 | 0.077 |
| 148.00 | -11.41 | -2.54 | 0.00 | -52.74 | 0.00 | 52.74 | 1472.45 | 382.10 | 861.19 | 810.82 | 10.17 | -0.76 | 0.073 |
| 150.00 | -9.02 | -2.29 | 0.00 | -47.66 | 0.00 | 47.66 | 1456.60 | 375.09 | 829.89 | 787.25 | 10.49 | -0.77 | 0.067 |
| 152.00 | -8.86 | -2.27 | 0.00 | -43.09 | 0.00 | 43.09 | 1440.33 | 368.08 | 799.17 | 763.78 | 10.82 | -0.79 | 0.063 |
| 154.00 | -8.72 | -2.26 | 0.00 | -38.54 | 0.00 | 38.54 | 1423.65 | 361.08 | 769.03 | 740.42 | 11.15 | -0.80 | 0.058 |
| 156.00 | -8.57 | -2.24 | 0.00 | -34.02 | 0.00 | 34.02 | 1406.55 | 354.07 | 739.47 | 717.20 | 11.49 | -0.81 | 0.054 |
| 158.00 | -7.30 | -2.04 | 0.00 | -29.54 | 0.00 | 29.54 | 1389.03 | 347.06 | 710.49 | 694.11 | 11.83 | -0.82 | 0.048 |
| 160.00 | -7.17 | -2.02 | 0.00 | -25.45 | 0.00 | 25.45 | 1371.10 | 340.05 | 682.09 | 671.17 | 12.18 | -0.83 | 0.043 |
| 162.00 | -7.04 | -2.00 | 0.00 | -21.41 | 0.00 | 21.41 | 1352.75 | 333.05 | 654.27 | 648.41 | 12.53 | -0.84 | 0.038 |
| 164.00 | -6.92 | -1.98 | 0.00 | -17.41 | 0.00 | 17.41 | 1333.98 | 326.04 | 627.03 | 625.81 | 12.88 | -0.85 | 0.033 |
| 166.00 | -3.48 | -1.19 | 0.00 | -13.46 | 0.00 | 13.46 | 1314.79 | 319.03 | 600.37 | 603.42 | 13.24 | -0.86 | 0.025 |
| 168.00 | -3.36 | -1.16 | 0.00 | -11.09 | 0.00 | 11.09 | 1295.19 | 312.03 | 574.28 | 581.22 | 13.60 | -0.86 | 0.022 |
| 170.00 | -3.25 | -1.13 | 0.00 | -8.76 | 0.00 | 8.76 | 1275.17 | 305.02 | 548.78 | 559.24 | 13.96 | -0.87 | 0.018 |
| 172.00 | -3.14 | -1.10 | 0.00 | -6.50 | 0.00 | 6.50 | 1251.65 | 298.01 | 523.85 | 536.17 | 14.33 | -0.87 | 0.015 |
| 174.00 | -3.04 | -1.07 | 0.00 | -4.29 | 0.00 | 4.29 | 1222.21 | 291.00 | 499.51 | 511.11 | 14.69 | -0.88 | 0.011 |
| 176.00 | -2.93 | -1.04 | 0.00 | -2.15 | 0.00 | 2.15 | 1192.78 | 284.00 | 475.74 | 486.64 | 15.06 | -0.88 | 0.007 |
| 178.00 | -0.09 | -0.04 | 0.00 | -0.07 | 0.00 | 0.07 | 1163.35 | 276.99 | 452.55 | 462.78 | 15.43 | -0.88 | 0.000 |
| 180.00 | 0.00 | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 1133.92 | 269.98 | 429.95 | 439.52 | 15.80 | -0.88 | 0.000 |



## Wind Loading - Shaft

| Structure: <br> Site Name: Height: <br> Base Elev: <br> Gh: | $\begin{aligned} & \text { CT46130-A- } \\ & \text { Deep River- } \\ & 180.00(\mathrm{ft}) \\ & 0.000(\mathrm{ft}) \\ & 1.1 \end{aligned}$ | Topography |  | 1 | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | $12 / 5 / 2019$ <br> Page: 39 |  | $\underbrace{((1,1))}_{\text {Tower Enginecring Solutions }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.00 | 1.00 | 1.24 | 10.746 | 11.82 | 232.21 | 0.950 | 0.000 | 2.00 | 7.030 | 6.68 | 78.9 | 0.0 | 359.1 |
| 90.17 Bot - Section 3 | 1.00 | 1.24 | 10.750 | 11.82 | 232.02 | 0.950 | 0.000 | 0.17 | 0.582 | 0.55 | 6.5 | 0.0 | 29.7 |
| 92.00 | 1.00 | 1.24 | 10.795 | 11.88 | 229.90 | 0.950 | 0.000 | 1.83 | 6.471 | 6.15 | 73.0 | 0.0 | 605.1 |
| 94.00 | 1.00 | 1.25 | 10.844 | 11.93 | 227.56 | 0.950 | 0.000 | 2.00 | 6.977 | 6.63 | 79.1 | 0.0 | 652.3 |
| 96.00 Top - Section 2 | 1.00 | 1.25 | 10.893 | 11.98 | 225.20 | 0.950 | 0.000 | 2.00 | 6.891 | 6.55 | 78.4 | 0.0 | 644.1 |
| 98.00 | 1.00 | 1.26 | 10.940 | 12.03 | 226.80 | 0.950 | 0.000 | 2.00 | 6.806 | 6.47 | 77.8 | 0.0 | 294.5 |
| 100.00 | 1.00 | 1.27 | 10.987 | 12.09 | 224.41 | 0.950 | 0.000 | 2.00 | 6.720 | 6.38 | 77.2 | 0.0 | 290.8 |
| 102.00 | 1.00 | 1.27 | 11.033 | 12.14 | 221.99 | 0.950 | 0.000 | 2.00 | 6.635 | 6.30 | 76.5 | 0.0 | 287.1 |
| 104.00 | 1.00 | 1.28 | 11.078 | 12.19 | 219.56 | 0.950 | 0.000 | 2.00 | 6.549 | 6.22 | 75.8 | 0.0 | 283.3 |
| 106.00 | 1.00 | 1.28 | 11.122 | 12.23 | 217.11 | 0.950 | 0.000 | 2.00 | 6.464 | 6.14 | 75.1 | 0.0 | 279.6 |
| 108.00 | 1.00 | 1.29 | 11.166 | 12.28 | 214.63 | 0.950 | 0.000 | 2.00 | 6.378 | 6.06 | 74.4 | 0.0 | 275.9 |
| 110.00 | 1.00 | 1.29 | 11.209 | 12.33 | 212.14 | 0.950 | 0.000 | 2.00 | 6.292 | 5.98 | 73.7 | 0.0 | 272.1 |
| 112.00 | 1.00 | 1.30 | 11.252 | 12.38 | 209.64 | 0.950 | 0.000 | 2.00 | 6.207 | 5.90 | 73.0 | 0.0 | 268.4 |
| 114.00 | 1.00 | 1.30 | 11.294 | 12.42 | 207.11 | 0.950 | 0.000 | 2.00 | 6.121 | 5.82 | 72.2 | 0.0 | 264.6 |
| 116.00 | 1.00 | 1.31 | 11.335 | 12.47 | 204.57 | 0.950 | 0.000 | 2.00 | 6.036 | 5.73 | 71.5 | 0.0 | 260.9 |
| 118.00 | 1.00 | 1.31 | 11.376 | 12.51 | 202.01 | 0.950 | 0.000 | 2.00 | 5.950 | 5.65 | 70.7 | 0.0 | 257.2 |
| 120.00 | 1.00 | 1.32 | 11.417 | 12.56 | 199.44 | 0.950 | 0.000 | 2.00 | 5.864 | 5.57 | 70.0 | 0.0 | 253.4 |
| 122.00 | 1.00 | 1.32 | 11.456 | 12.60 | 196.85 | 0.950 | 0.000 | 2.00 | 5.779 | 5.49 | 69.2 | 0.0 | 249.7 |
| 124.00 | 1.00 | 1.32 | 11.496 | 12.65 | 194.24 | 0.950 | 0.000 | 2.00 | 5.693 | 5.41 | 68.4 | 0.0 | 246.0 |
| 126.00 | 1.00 | 1.33 | 11.534 | 12.69 | 191.62 | 0.950 | 0.000 | 2.00 | 5.608 | 5.33 | 67.6 | 0.0 | 242.2 |
| 128.00 | 1.00 | 1.33 | 11.573 | 12.73 | 188.99 | 0.950 | 0.000 | 2.00 | 5.522 | 5.25 | 66.8 | 0.0 | 238.5 |
| 130.00 | 1.00 | 1.34 | 11.611 | 12.77 | 186.34 | 0.950 | 0.000 | 2.00 | 5.437 | 5.16 | 66.0 | 0.0 | 234.8 |
| 132.00 | 1.00 | 1.34 | 11.648 | 12.81 | 183.68 | 0.950 | 0.000 | 2.00 | 5.351 | 5.08 | 65.1 | 0.0 | 231.0 |
| 133.33 Bot - Section 4 | 1.00 | 1.34 | 11.673 | 12.84 | 181.90 | 0.950 | 0.000 | 1.33 | 3.520 | 3.34 | 42.9 | 0.0 | 151.9 |
| 134.00 | 1.00 | 1.35 | 11.685 | 12.85 | 181.00 | 0.950 | 0.000 | 0.67 | 1.774 | 1.69 | 21.7 | 0.0 | 131.2 |
| 136.00 | 1.00 | 1.35 | 11.721 | 12.89 | 178.32 | 0.950 | 0.000 | 2.00 | 5.266 | 5.00 | 64.5 | 0.0 | 389.4 |
| 138.00 Top - Section 3 | 1.00 | 1.35 | 11.757 | 12.93 | 175.62 | 0.950 | 0.000 | 2.00 | 5.181 | 4.92 | 63.7 | 0.0 | 382.9 |
| 140.00 | 1.00 | 1.36 | 11.793 | 12.97 | 175.91 | 0.950 | 0.000 | 2.00 | 5.095 | 4.84 | 62.8 | 0.0 | 160.4 |
| 142.00 | 1.00 | 1.36 | 11.828 | 13.01 | 173.18 | 0.950 | 0.000 | 2.00 | 5.009 | 4.76 | 61.9 | 0.0 | 157.7 |
| 144.00 | 1.00 | 1.37 | 11.863 | 13.05 | 170.45 | 0.950 | 0.000 | 2.00 | 4.924 | 4.68 | 61.0 | 0.0 | 155.0 |
| 146.00 | 1.00 | 1.37 | 11.898 | 13.09 | 167.70 | 0.950 | 0.000 | 2.00 | 4.838 | 4.60 | 60.2 | 0.0 | 152.2 |
| 148.00 | 1.00 | 1.37 | 11.932 | 13.13 | 164.95 | 0.950 | 0.000 | 2.00 | 4.753 | 4.51 | 59.3 | 0.0 | 149.5 |
| 150.00 Appurtenance(s) | 1.00 | 1.38 | 11.966 | 13.16 | 162.18 | 0.950 | 0.000 | 2.00 | 4.667 | 4.43 | 58.4 | 0.0 | 146.8 |
| 152.00 | 1.00 | 1.38 | 11.999 | 13.20 | 159.40 | 0.950 | 0.000 | 2.00 | 4.581 | 4.35 | 57.4 | 0.0 | 144.1 |
| 154.00 | 1.00 | 1.39 | 12.032 | 13.24 | 156.61 | 0.950 | 0.000 | 2.00 | 4.496 | 4.27 | 56.5 | 0.0 | 141.4 |
| 156.00 | 1.00 | 1.39 | 12.065 | 13.27 | 153.81 | 0.950 | 0.000 | 2.00 | 4.410 | 4.19 | 55.6 | 0.0 | 138.7 |
| 158.00 Appurtenance(s) | 1.00 | 1.39 | 12.097 | 13.31 | 151.00 | 0.950 | 0.000 | 2.00 | 4.325 | 4.11 | 54.7 | 0.0 | 135.9 |
| 160.00 | 1.00 | 1.40 | 12.129 | 13.34 | 148.18 | 0.950 | 0.000 | 2.00 | 4.239 | 4.03 | 53.7 | 0.0 | 133.2 |
| 162.00 | 1.00 | 1.40 | 12.161 | 13.38 | 145.34 | 0.950 | 0.000 | 2.00 | 4.154 | 3.95 | 52.8 | 0.0 | 130.5 |
| 164.00 | 1.00 | 1.40 | 12.193 | 13.41 | 142.50 | 0.950 | 0.000 | 2.00 | 4.068 | 3.86 | 51.8 | 0.0 | 127.8 |
| 166.00 Appurtenance(s) | 1.00 | 1.41 | 12.224 | 13.45 | 139.65 | 0.950 | 0.000 | 2.00 | 3.982 | 3.78 | 50.9 | 0.0 | 125.1 |
| 168.00 | 1.00 | 1.41 | 12.255 | 13.48 | 136.79 | 0.950 | 0.000 | 2.00 | 3.897 | 3.70 | 49.9 | 0.0 | 122.4 |
| 170.00 | 1.00 | 1.42 | 12.285 | 13.51 | 133.92 | 0.950 | 0.000 | 2.00 | 3.811 | 3.62 | 48.9 | 0.0 | 119.6 |
| 172.00 | 1.00 | 1.42 | 12.315 | 13.55 | 131.04 | 0.950 | 0.000 | 2.00 | 3.726 | 3.54 | 47.9 | 0.0 | 116.9 |
| 174.00 | 1.00 | 1.42 | 12.345 | 13.58 | 128.15 | 0.950 | 0.000 | 2.00 | 3.640 | 3.46 | 47.0 | 0.0 | 114.2 |
| 176.00 | 1.00 | 1.43 | 12.375 | 13.61 | 125.25 | 0.950 | 0.000 | 2.00 | 3.554 | 3.38 | 46.0 | 0.0 | 111.5 |
| 178.00 Appurtenance(s) | 1.00 | 1.43 | 12.405 | 13.65 | 122.34 | 0.950 | 0.000 | 2.00 | 3.469 | 3.30 | 45.0 | 0.0 | 108.8 |
| 180.00 | 1.00 | 1.43 | 12.434 | 13.68 | 119.43 | 0.950 | 0.000 | 2.00 | 3.383 | 3.21 | 44.0 | 0.0 | 106.1 |
|  |  |  |  |  |  |  | Totals: | 180.00 |  |  | 6,587.7 |  | 3,413.9 |

## Discrete Appurtenance Forces

| Structure: <br> Site Name Height: <br> Base Elev: Gh: |  | CT46130-A-SBA <br> Deep River-winthrop 180.00 (ft) <br> 0.000 (ft) <br> 1.1 | op RdTopography: |  | Code: <br> Exposure: <br> Crest Height: <br> Site Class: <br> Struct Class: |  |  |  | $\begin{aligned} & \text { EIA/TIA-222-H } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | 12/5/2019 <br> Page: 40 |  | $\xrightarrow[\text { Tower Engincering Solutions }]{((1 \text { MHID) }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Case: $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind <br> Dead Load Factor 1.00 <br> Wind Load Factor $\quad 1.00$ |  |  |  |  |  | Orient <br> Factor <br> x Ka | Ka | Total CaAa (sf) |  |  |  | Iter | rations |  |
| No. $\begin{gathered}\text { Elev } \\ \text { (ft) }\end{gathered}$ |  | Description | Qty | $\begin{gathered} \text { qz } \\ \text { (psf) } \end{gathered}$ | qzGh <br> (psf) |  |  |  | Dead Load (lb) | Horiz Ecc <br> (ft) |  | Wind FX <br> (Ib) | $\begin{gathered} \text { Mom } \\ \mathbf{Y} \\ (\mathrm{lb-ft}) \\ \hline \end{gathered}$ |  |
| 1 | 178.00 | Samsung B5/B13 RRH | 3 | 12.405 | 13.645 | 0.50 | 0.75 | 3.35 | 210.90 | 0.000 | 0.000 | 45.67 | 0.00 | 0.00 |
| 2 | 178.00 | Samsung B2/B66A RRH | 3 | 12.405 | 13.645 | 0.50 | 0.75 | 2.83 | 253.20 | 0.000 | 0.000 | 38.67 | 0.00 | 0.00 |
| 3 | 178.00 | JMA MX06FRO660-03 | 6 | 12.405 | 13.645 | 0.61 | 0.75 | 36.42 | 360.00 | 0.000 | 0.000 | 496.96 | 0.00 | 0.00 |
| 4 | 178.00 P | Platform w/ Handrails w/ | 1 | 12.405 | 13.645 | 1.00 | 1.00 | 40.00 | 2202.20 | 0.000 | 0.000 | 545.81 | 0.00 | 0.00 |
| 5 | 178.00 | Raycap | 1 | 12.405 | 13.645 | 1.00 | 1.00 | 2.61 | 32.00 | 0.000 | 0.000 | 35.61 | 0.00 | 0.00 |
| 6 | 166.00 | ALU 800 Mhz | 6 | 12.224 | 13.446 | 0.38 | 0.75 | 5.60 | 318.00 | 0.000 | 0.000 | 75.33 | 0.00 | 0.00 |
| 7 | 166.00 | RFS APXVTM14-C-I20 | 3 | 12.224 | 13.446 | 0.58 | 0.75 | 10.98 | 168.60 | 0.000 | 0.000 | 147.69 | 0.00 | 0.00 |
| 8 | 166.00 | Commscope | 3 | 12.224 | 13.446 | 0.55 | 0.75 | 20.43 | 232.20 | 0.000 | 0.000 | 274.70 | 0.00 | 0.00 |
| 9 | 166.00 | ALU 1900 Mhz | 3 | 12.224 | 13.446 | 0.50 | 0.75 | 5.73 | 132.00 | 0.000 | 0.000 | 77.03 | 0.00 | 0.00 |
| 10 | 166.00 | Sitepro | 1 | 12.224 | 13.446 | 1.00 | 1.00 | 7.00 | 406.61 | 0.000 | 0.000 | 94.12 | 0.00 | 0.00 |
| 11 | 166.00 | ALU TD-RRH8x20-25 | 3 | 12.224 | 13.446 | 0.50 | 0.75 | 6.11 | 210.00 | 0.000 | 0.000 | 82.09 | 0.00 | 0.00 |
| 12 | 166.00 S | Sitepro | 1 | 12.224 | 13.446 | 1.00 | 1.00 | 6.70 | 230.00 | 0.000 | 0.000 | 90.09 | 0.00 | 0.00 |
| 13 | 166.00 P | Platform w/ Hand Rails | 1 | 12.224 | 13.446 | 1.00 | 1.00 | 40.00 | 2000.00 | 0.000 | 0.000 | 537.84 | 0.00 | 0.00 |
| 14 | 158.00 P | PCS1900 G3 TMA | 6 | 12.097 | 13.307 | 0.40 | 0.80 | 2.50 | 120.00 | 0.000 | 0.000 | 33.21 | 0.00 | 0.00 |
| 15 | 158.00 | T-Arms | 3 | 12.097 | 13.307 | 0.56 | 0.75 | 13.50 | 1050.00 | 0.000 | 0.000 | 179.64 | 0.00 | 0.00 |
| 16 | 158.00 | EMS RR90-17-02DP | 6 | 12.097 | 13.307 | 0.54 | 0.80 | 23.96 | 81.00 | 0.000 | 0.000 | 318.81 | 0.00 | 0.00 |
| 17 | 150.00 | Powerwave 7770 | 3 | 11.966 | 13.162 | 0.55 | 0.75 | 9.05 | 105.00 | 0.000 | 0.000 | 119.12 | 0.00 | 0.00 |
| 18 | 150.00 | Cci HPA-65R-BUU-H6 | 2 | 11.966 | 13.162 | 0.77 | 0.90 | 14.78 | 102.00 | 0.000 | 0.000 | 194.54 | 0.00 | 0.00 |
| 19 | 150.00 | SBNHH-1D65A | 1 | 11.966 | 13.162 | 1.00 | 1.00 | 5.88 | 33.50 | 0.000 | 0.000 | 77.39 | 0.00 | 0.00 |
| 20 | 150.00 | Rrus-32 | 3 | 11.966 | 13.162 | 0.50 | 0.75 | 5.83 | 231.00 | 0.000 | 0.000 | 76.79 | 0.00 | 0.00 |
| 21 | 150.00 | KMW AM-X-CD-16-65-00T | 2 | 11.966 | 13.162 | 0.56 | 0.75 | 9.02 | 97.00 | 0.000 | 0.000 | 118.76 | 0.00 | 0.00 |
| 22 | 150.00 | Powerwave LGP21401 | 6 | 11.966 | 13.162 | 0.38 | 0.75 | 2.75 | 84.60 | 0.000 | 0.000 | 36.13 | 0.00 | 0.00 |
| 23 | 150.00 | KMW AM-X-CD-14-65-00T | 1 | 11.966 | 13.162 | 0.75 | 0.75 | 5.29 | 36.40 | 0.000 | 0.000 | 69.60 | 0.00 | 0.00 |
| 24 | 150.00 | Ericsson RRUS-11 | 3 | 11.966 | 13.162 | 0.50 | 0.75 | 3.80 | 152.10 | 0.000 | 0.000 | 50.00 | 0.00 | 0.00 |
| 25 | 150.00 | Raycap DC6-48-60-18-8F | 1 | 11.966 | 13.162 | 0.67 | 1.00 | 1.21 | 31.80 | 0.000 | 0.000 | 15.96 | 0.00 | 0.00 |
| 26 | 150.00 | Platform w/ Hand Rail | 1 | 11.966 | 13.162 | 1.00 | 1.00 | 35.00 | 1600.00 | 0.000 | 0.000 | 460.68 | 0.00 | 0.00 |

Total Applied Force Summary


| Load Case: $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind |  |  | Iterations | 27 |
| :---: | :---: | :---: | :---: | :---: |
| Dead Load Factor | 1.00 |  |  |  |
| Wind Load Factor | 1.00 |  |  |  |


| Elev <br> (ft) | Doscription | Lateral FX (-) (lb) | Axial <br> FY(-) <br> (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 |  |
| 2.00 |  | 82.16 | 587.84 | 0.00 | 0.00 |  |
| 4.00 |  | 81.50 | 603.57 | 0.00 | 0.00 |  |
| 6.00 |  | 80.84 | 619.30 | 0.00 | 0.00 |  |
| 8.00 |  | 80.18 | 614.55 | 0.00 | 0.00 |  |
| 10.00 |  | 79.52 | 609.79 | 0.00 | 0.00 |  |
| 12.00 |  | 78.86 | 605.04 | 0.00 | 0.00 |  |
| 14.00 |  | 78.20 | 600.28 | 0.00 | 0.00 |  |
| 16.00 |  | 78.50 | 595.53 | 0.00 | 0.00 |  |
| 18.00 |  | 79.78 | 590.77 | 0.00 | 0.00 |  |
| 20.00 |  | 80.87 | 586.02 | 0.00 | 0.00 |  |
| 22.00 |  | 81.80 | 581.26 | 0.00 | 0.00 |  |
| 24.00 |  | 82.58 | 576.51 | 0.00 | 0.00 |  |
| 26.00 |  | 83.24 | 571.75 | 0.00 | 0.00 |  |
| 28.00 |  | 83.80 | 567.00 | 0.00 | 0.00 |  |
| 30.00 |  | 84.27 | 562.24 | 0.00 | 0.00 |  |
| 32.00 |  | 84.65 | 557.48 | 0.00 | 0.00 |  |
| 34.00 |  | 84.95 | 552.73 | 0.00 | 0.00 |  |
| 36.00 |  | 85.19 | 547.97 | 0.00 | 0.00 |  |
| 38.00 |  | 85.36 | 543.22 | 0.00 | 0.00 |  |
| 40.00 |  | 85.48 | 538.46 | 0.00 | 0.00 |  |
| 42.00 |  | 85.54 | 533.71 | 0.00 | 0.00 |  |
| 43.92 |  | 81.97 | 507.01 | 0.00 | 0.00 |  |
| 44.00 |  | 3.60 | 41.05 | 0.00 | 0.00 |  |
| 46.00 |  | 86.89 | 980.42 | 0.00 | 0.00 |  |
| 48.00 |  | 86.83 | 971.25 | 0.00 | 0.00 |  |
| 50.00 |  | 86.73 | 962.08 | 0.00 | 0.00 |  |
| 51.00 |  | 43.23 | 477.60 | 0.00 | 0.00 |  |
| 52.00 |  | 43.19 | 241.42 | 0.00 | 0.00 |  |
| 54.00 |  | 86.42 | 479.53 | 0.00 | 0.00 |  |
| 56.00 |  | 86.22 | 475.11 | 0.00 | 0.00 |  |
| 58.00 |  | 85.98 | 470.70 | 0.00 | 0.00 |  |
| 60.00 |  | 85.71 | 466.28 | 0.00 | 0.00 |  |
| 62.00 |  | 85.42 | 461.87 | 0.00 | 0.00 |  |
| 64.00 |  | 85.10 | 457.45 | 0.00 | 0.00 |  |
| 66.00 |  | 84.75 | 453.04 | 0.00 | 0.00 |  |
| 68.00 |  | 84.38 | 448.62 | 0.00 | 0.00 |  |
| 70.00 |  | 83.98 | 444.20 | 0.00 | 0.00 |  |
| 72.00 |  | 83.57 | 439.79 | 0.00 | 0.00 | - |
| 74.00 |  | 83.13 | 435.37 | 0.00 | 0.00 |  |
| 76.00 |  | 82.67 | 430.96 | 0.00 | 0.00 |  |
| 78.00 |  | 82.19 | 426.54 | 0.00 | 0.00 |  |
| 80.00 |  | 81.69 | 422.13 | 0.00 | 0.00 |  |
| 82.00 |  | 81.17 | 417.71 | 0.00 | 0.00 |  |
| 84.00 |  | 80.64 | 413.30 | 0.00 | 0.00 |  |
| 86.00 |  | 80.09 | 408.88 | 0.00 | 0.00 |  |
| 88.00 |  | 79.52 | 404.46 | 0.00 | 0.00 |  |

## Total Applied Force Summary



| Structure: | CT46130-A-SBA |  | Code: | EIA/TIA-222-H | 12/5/2019 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Site Name: | Deep River-winthrop Rd |  | Exposure: | C |  |
| Height: | 180.00 (ft) |  | Crest Height: | 0.00 |  |
| Base Elev: | 0.000 (ft) |  | Site Class: | D-Stiff Soil |  |
| Gh: | 1.1 | Topography: | 1 | Struct Class: | II |


| Load Case: $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind |  |  |  |  |  |  |  |  |  |  |  |  |  | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dead Wind |  | Factor <br> Factor | $\begin{array}{ll} \mathbf{r} & 1.00 \\ \mathbf{r} & 1.00 \end{array}$ |  |  |  |  |  |  |  |  |  |  |
| Seg Elev <br> (ft) | $\begin{aligned} & \mathrm{Pu} \\ & \text { FY (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ |  | Mu MZ <br> (ft-kips) |  | Resultant Moment (ft-kips) | phi Pn (kips) | $\begin{gathered} \text { phi } \\ \substack{\text { Vn } \\ \text { (kips) }} \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation Sway (deq) | Rotation Twist (deg) | $\begin{gathered} \text { Stress } \\ \text { Ratio } \\ \hline \end{gathered}$ |
| 0.00 | -47.07 | -10.89 | 0.00 | -1298.7 | 0.00 | 1298.75 | 5123.29 | 1522.04 | 7808.40 | 6435.29 | 0.00 | 0.000 | 0.000 | 0.211 |
| 2.00 | $-46.48$ | -10.82 | 0.00 | -1276.9 | 0.00 | 1276.97 | 5107.67 | 1509.78 | 7683.09 | 6363.61 | 0.00 | -0.017 | 0.000 | 0.210 |
| 4.00 | -45.87 | -10.75 | 0.00 | -1255.3 | 0.00 | 1255.34 | 5091.62 | 1497.52 | 7558.79 | 6291.73 | 0.02 | -0.035 | 0.000 | 0.209 |
| 6.00 | -45.25 | -10.68 | 0.00 | -1233.8 | 0.00 | 1233.84 | 5075.16 | 1485.26 | 7435.50 | 6219.67 | 0.03 | -0.053 | 0.000 | 0.207 |
| 8.00 | -44.63 | -10.62 | 0.00 | -1212.4 | 0.00 | 1212.48 | 5058.29 | 1472.99 | 7313.22 | 6147.44 | 0.06 | -0.071 | 0.000 | 0.206 |
| 10.00 | -44.02 | -10.55 | 0.00 | -1191.2 | 0.00 | 1191.25 | 5041.00 | 1460.73 | 7191.96 | 6075.05 | 0.09 | -0.089 | 0.000 | 0.205 |
| 12.00 | -43.41 | -10.48 | 0.00 | -1170.1 | 0.00 | 1170.15 | 5023.29 | 1448.47 | 7071.72 | 6002.51 | 0.13 | -0.107 | 0.000 | 0.204 |
| 14.00 | -42.81 | -10.42 | 0.00 | -1149.1 | 0.00 | 1149.18 | 5005.16 | 1436.20 | 6952.48 | 5929.84 | 0.18 | -0.125 | 0.000 | 0.202 |
| 16.00 | -42.21 | -10.35 | 0.00 | -1128.3 | 0.00 | 1128.35 | 4986.62 | 1423.94 | 6834.27 | 5857.05 | 0.24 | -0.143 | 0.000 | 0.201 |
| 18.00 | -41.62 | -10.28 | 0.00 | -1107.6 | 0.00 | 1107.65 | 4967.66 | 1411.68 | 6717.06 | 5784.16 | 0.30 | -0.162 | 0.000 | 0.200 |
| 20.00 | -41.03 | -10.21 | 0.00 | -1087.0 | 0.00 | 1087.08 | 4948.29 | 1399.42 | 6600.87 | 5711.17 | 0.38 | -0.181 | 0.000 | 0.199 |
| 22.00 | -40.44 | -10.14 | 0.00 | -1066.6 | 0.00 | 1066.65 | 4928.49 | 1387.15 | 6485.69 | 5638.10 | 0.46 | -0.199 | 0.000 | 0.197 |
| 24.00 | -39.86 | -10.07 | 0.00 | -1046.3 | 0.00 | 1046.37 | 4908.28 | 1374.89 | 6371.53 | 5564.95 | 0.54 | -0.218 | 0.000 | 0.196 |
| 26.00 | -39.29 | -10.00 | 0.00 | -1026.2 | 0.00 | 1026.22 | 4887.66 | 1362.63 | 6258.37 | 5491.76 | 0.64 | -0.237 | 0.000 | 0.195 |
| 28.00 | -38.72 | -9.93 | 0.00 | -1006.2 | 0.00 | 1006.22 | 4866.62 | 1350.36 | 6146.24 | 5418.52 | 0.74 | -0.257 | 0.000 | 0.194 |
| 30.00 | -38.15 | -9.85 | 0.00 | -986.37 | 0.00 | 986.37 | 4845.16 | 1338.10 | 6035.11 | 5345.24 | 0.85 | -0.276 | 0.000 | 0.192 |
| 32.00 | -37.59 | -9.78 | 0.00 | -966.67 | 0.00 | 966.67 | 4823.28 | 1325.84 | 5925.00 | 5271.95 | 0.97 | -0.295 | 0.000 | 0.191 |
| 34.00 | -37.04 | -9.70 | 0.00 | -947.11 | 0.00 | 947.11 | 4800.99 | 1313.58 | 5815.91 | 5198.66 | 1.10 | -0.315 | 0.000 | 0.190 |
| 36.00 | -36.49 | -9.63 | 0.00 | -927.71 | 0.00 | 927.71 | 4778.28 | 1301.31 | 5707.83 | 5125.37 | 1.24 | -0.335 | 0.000 | 0.189 |
| 38.00 | -35.94 | -9.55 | 0.00 | -908.45 | 0.00 | 908.45 | 4755.15 | 1289.05 | 5600.76 | 5052.10 | 1.38 | -0.355 | 0.000 | 0.187 |
| 40.00 | -35.40 | -9.47 | 0.00 | -889.35 | 0.00 | 889.35 | 4731.61 | 1276.79 | 5494.70 | 4978.87 | 1.54 | -0.375 | 0.000 | 0.186 |
| 42.00 | -34.86 | -9.40 | 0.00 | -870.40 | 0.00 | 870.40 | 4707.65 | 1264.52 | 5389.66 | 4905.68 | 1.70 | -0.395 | 0.000 | 0.185 |
| 43.92 | -34.36 | -9.32 | 0.00 | -852.39 | 0.00 | 852.39 | 4684.30 | 1252.77 | 5289.95 | 4835.60 | 1.86 | -0.415 | 0.000 | 0.184 |
| 44.00 | -34.31 | -9.32 | 0.00 | -851.62 | 0.00 | 851.62 | 4683.27 | 1252.26 | 5285.64 | 4832.55 | 1.87 | -0.415 | 0.000 | 0.184 |
| 46.00 | -33.33 | -9.24 | 0.00 | -832.97 | 0.00 | 832.97 | 4658.48 | 1240.00 | 5182.62 | 4759.49 | 2.05 | -0.436 | 0.000 | 0.182 |
| 48.00 | -32.36 | -9.16 | 0.00 | -814.50 | 0.00 | 814.50 | 4633.27 | 1227.74 | 5080.62 | 4686.52 | 2.23 | -0.457 | 0.000 | 0.181 |
| 50.00 | -31.39 | -9.07 | 0.00 | -796.19 | 0.00 | 796.19 | 4607.64 | 1215.47 | 4979.64 | 4613.64 | 2.43 | -0.477 | 0.000 | 0.179 |
| 51.00 | -30.91 | -9.03 | 0.00 | -787.12 | 0.00 | 787.12 | 4157.28 | 1142.33 | 4736.69 | 4216.21 | 2.53 | -0.488 | 0.000 | 0.194 |
| 52.00 | -30.67 | -8.99 | 0.00 | -778.09 | 0.00 | 778.09 | 4146.96 | 1136.64 | 4689.60 | 4184.61 | 2.63 | -0.498 | 0.000 | 0.193 |
| 54.00 | -30.19 | -8.91 | 0.00 | -760.11 | 0.00 | 760.11 | 4126.01 | 1125.25 | 4596.10 | 4121.41 | 2.85 | -0.520 | 0.000 | 0.192 |
| 56.00 | -29.71 | -8.83 | 0.00 | -742.28 | 0.00 | 742.28 | 4104.64 | 1113.86 | 4503.55 | 4058.23 | 3.07 | -0.542 | 0.000 | 0.190 |
| 58.00 | -29.24 | -8.75 | 0.00 | -724.62 | 0.00 | 724.62 | 4082.85 | 1102.48 | 4411.95 | 3995.08 | 3.30 | -0.564 | 0.000 | 0.189 |
| 60.00 | -28.77 | -8.67 | 0.00 | -707.11 | 0.00 | 707.11 | 4060.64 | 1091.09 | 4321.28 | 3931.97 | 3.54 | -0.586 | 0.000 | 0.187 |
| 62.00 | -28.30 | -8.60 | 0.00 | -689.76 | 0.00 | 689.76 | 4038.02 | 1079.70 | 4231.55 | 3868.91 | 3.79 | -0.608 | 0.000 | 0.185 |
| 64.00 | -27.84 | -8.52 | 0.00 | -672.57 | 0.00 | 672.57 | 4014.98 | 1068.31 | 4142.77 | 3805.92 | 4.05 | -0.630 | 0.000 | 0.184 |
| 66.00 | -27.39 | -8.44 | 0.00 | -655.54 | 0.00 | 655.54 | 3991.52 | 1056.93 | 4054.92 | 3743.01 | 4.32 | -0.653 | 0.000 | 0.182 |
| 68.00 | -26.94 | -8.36 | 0.00 | -638.67 | 0.00 | 638.67 | 3967.65 | 1045.54 | 3968.02 | 3680.19 | 4.60 | -0.675 | 0.000 | 0.180 |
| 70.00 | -26.49 | -8.28 | 0.00 | -621.95 | 0.00 | 621.95 | 3943.36 | 1034.15 | 3882.06 | 3617.47 | 4.89 | -0.698 | 0.000 | 0.179 |
| 72.00 | -26.05 | -8.20 | 0.00 | -605.39 | 0.00 | 605.39 | 3918.66 | 1022.77 | 3797.04 | 3554.87 | 5.19 | -0.721 | 0.000 | 0.177 |
| 74.00 | -25.61 | -8.12 | 0.00 | -588.99 | 0.00 | 588.99 | 3893.54 | 1011.38 | 3712.96 | 3492.40 | 5.49 | -0.744 | 0.000 | 0.175 |
| 76.00 | -25.18 | -8.04 | 0.00 | -572.75 | 0.00 | 572.75 | 3868.00 | 999.99 | 3629.83 | 3430.07 | 5.81 | -0.767 | 0.000 | 0.174 |
| 78.00 | -24.75 | -7.97 | 0.00 | -556.66 | 0.00 | 556.66 | 3842.04 | 988.61 | 3547.63 | 3367.90 | 6.14 | -0.790 | 0.000 | 0.172 |
| 80.00 | -24.33 | -7.89 | 0.00 | $-540.73$ | 0.00 | 540.73 | 3815.67 | 977.22 | 3466.38 | 3305.90 | 6.47 | -0.814 | 0.000 | 0.170 |
| 82.00 | -23.91 | -7.81 | 0.00 | -524.95 | 0.00 | 524.95 | 3788.88 | 965.83 | 3386.07 | 3244.07 | 6.82 | -0.837 | 0.000 | 0.168 |
| 84.00 | -23.49 | -7.73 | 0.00 | -509.33 | 0.00 | 509.33 | 3761.67 | 954.44 | 3306.69 | 3182.44 | 7.17 | -0.861 | 0.000 | 0.166 |
| 86.00 | -23.08 | -7.66 | 0.00 | -493.86 | 0.00 | 493.86 | 3734.05 | 943.06 | 3228.26 | 3121.02 | 7.54 | -0.885 | 0.000 | 0.164 |
| 88.00 | -22.67 | -7.58 | 0.00 | -478.54 | 0.00 | 478.54 | 3706.01 | 931.67 | 3150.77 | 3059.82 | 7.92 | -0.909 | 0.000 | 0.163 |
| 90.00 | -22.27 | -7.50 | 0.00 | -463.38 | 0.00 | 463.38 | 3677.55 | 920.28 | 3074.23 | 2998.84 | 8.30 | -0.933 | 0.000 | 0.161 |


| Structure: <br> Site Name: <br> Height: <br> Base Elev: <br> Gh: |  | CT46130-A-S <br> Deep River-w <br> 180.00 (ft) <br> 0.000 (ft) <br> 1.1 |  | Topography: |  | 1 | Code: <br> Exposure: <br> Crest Height <br> Site Class: <br> Struct Class | $\begin{aligned} & \text { EIA/TIA-222-1 } \\ & \text { C } \\ & 0.00 \\ & \text { D - Stiff Soil } \\ & \text { II } \end{aligned}$ |  | $2-\mathrm{H}$ | $12 / 5 / 2019$ <br> Page: 44 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90.17 | -22.24 | -7.50 | 0.00 | -462.13 | 0.00 | 462.13 | 3675.16 | 919.33 | 3067.89 | 2993.77 | 8.33 | -0.935 | 0.000 | 0.160 |
| 92.00 | -21.59 | -7.42 | 0.00 | -448.38 | 0.00 | 448.38 | 3648.68 | 908.90 | 2998.62 | 2938.12 | 8.70 | -0.957 | 0.000 | . 159 |
| 94.00 | -20.90 | -7.34 | 0.00 | -433.54 | 0.00 | 433.54 | 3619.39 | 897.51 | 2923.96 | 2877.64 | 9.10 | -0.981 | 0.000 | 0.156 |
| 96.00 | -20.21 | -7.26 | 0.00 | -418.85 | 0.00 | 418.85 | 2873.56 | 764.37 | 2506.37 | 2303.28 | 9.52 | -1.005 | 0.000 | 0.189 |
| 98.00 | -19.88 | -7.19 | 0.00 | -404.33 | 0.00 | 404.33 | 2853.66 | 754.73 | 2443.58 | 2258.25 | 9.95 | -1.030 | 0.000 | . 186 |
| 100.00 | -19.54 | -7.11 | 0.00 | -389.96 | 0.00 | 389.96 | 2833.34 | 745.10 | 2381.59 | 2213.29 | 10.38 | -1.057 | 0.000 | 0.183 |
| 102.00 | -19.21 | -7.04 | 0.00 | -375.74 | 0.00 | 375.74 | 2812.61 | 735.46 | 2320.39 | 2168.43 | 10.83 | -1.084 | 0.000 | 0.180 |
| 104.00 | -18.89 | -6.97 | 0.00 | -361.66 | 0.00 | 361.66 | 2791.46 | 725.83 | 2259.99 | 2123.68 | 11.29 | -1.112 | 0.000 | 0.177 |
| 106.00 | -18.56 | -6.89 | 0.00 | -347.73 | 0.00 | 347.73 | 2769.89 | 716.19 | 2200.39 | 2079.04 | 11.76 | -1.139 | 0.000 | 0.174 |
| 108.00 | -18.25 | -6.82 | 0.00 | -333.95 | 0.00 | 333.95 | 2747.90 | 706.55 | 2141.58 | 2034.53 | 12.25 | -1.167 | 0.000 | 0.171 |
| 110.00 | -17.93 | -6.75 | 0.00 | -320.31 | 0.00 | 320.31 | 2725.50 | 696.92 | 2083.57 | 1990.17 | 12.74 | -1.194 | 0.000 | 0.168 |
| 112.00 | -17.62 | -6.68 | 0.00 | -306.81 | 0.00 | 306.81 | 2702.68 | 687.28 | 2026.36 | 1945.97 | 13.25 | -1.221 | 0.000 | 0.164 |
| 114.00 | -17.31 | -6.61 | 0.00 | -293.45 | 0.00 | 293.45 | 2679.45 | 677.65 | 1969.94 | 1901.93 | 13.77 | -1.249 | 0.000 | 0.161 |
| 116.00 | -17.01 | -6.54 | 0.00 | -280.24 | 0.00 | 280.24 | 2655.79 | 668.01 | 1914.32 | 1858.08 | 14.29 | -1.276 | 0.000 | 0.157 |
| 118.00 | -16.71 | -6.47 | 0.00 | -267.16 | 0.00 | 267.16 | 2631.73 | 658.38 | 1859.50 | 1814.42 | 14.83 | -1.303 | 0.000 | 0.154 |
| 120.00 | -16.41 | -6.40 | 0.00 | -254.23 | 0.00 | 254.23 | 2607.24 | 648.74 | 1805.47 | 1770.96 | 15.39 | -1.330 | 0.000 | 0.150 |
| 122.00 | -16.12 | -6.33 | 0.00 | -241.43 | 0.00 | 241.43 | 2582.34 | 639.11 | 1752.24 | 1727.73 | 15.95 | -1.357 | 0.000 | 0.146 |
| 124.00 | -15.83 | -6.26 | 0.00 | -228.77 | 0.00 | 228.77 | 2557.02 | 629.47 | 1699.80 | 1684.74 | 16.52 | -1.383 | 0.000 | 0.142 |
| 126.00 | -15.55 | -6.20 | 0.00 | -216.25 | 0.00 | 216.25 | 2531.28 | 619.84 | 1648.16 | 1641.98 | 17.11 | -1.410 | 0.000 | 0.138 |
| 128.00 | -15.27 | -6.13 | 0.00 | -203.86 | 0.00 | 203.86 | 2505.13 | 610.20 | 1597.32 | 1599.49 | 17.71 | -1.436 | 0.000 | 0.134 |
| 130.00 | -14.99 | -6.06 | 0.00 | -191.60 | 0.00 | 191.60 | 2478.56 | 600.57 | 1547.28 | 1557.27 | 18.31 | -1.461 | 0.000 | 0.129 |
| 132.00 | -14.72 | -6.00 | 0.00 | -179.47 | 0.00 | 179.47 | 2451.58 | 590.93 | 1498.03 | 1515.33 | 18.93 | -1.487 | 0.000 | 0.125 |
| 133.33 | -14.54 | -5.95 | 0.00 | -171.48 | 0.00 | 171.48 | 2433.35 | 584.51 | 1465.64 | 1487.53 | 19.35 | -1.503 | 0.000 | 0.121 |
| 134.00 | -14.39 | -5.93 | 0.00 | -167.51 | 0.00 | 167.51 | 2424.17 | 581.30 | 1449.58 | 1473.69 | 19.56 | -1.512 | 0.000 | 0.120 |
| 136.00 | -13.96 | -5.86 | 0.00 | -155.65 | 0.00 | 155.65 | 2396.35 | 571.66 | 1401.92 | 1432.35 | 20.20 | -1.536 | 0.000 | 0.115 |
| 138.00 | -13.54 | -5.79 | 0.00 | -143.93 | 0.00 | 143.93 | 1545.45 | 417.14 | 1026.36 | 929.77 | 20.85 | -1.560 | 0.000 | 0.164 |
| 140.00 | -13.34 | -5.73 | 0.00 | -132.35 | 0.00 | 132.35 | 1531.69 | 410.13 | 992.17 | 905.88 | 21.50 | -1.583 | 0.000 | 0.155 |
| 142.00 | -13.14 | -5.67 | 0.00 | -120.90 | 0.00 | 120.90 | 1517.50 | 403.12 | 958.56 | 882.03 | 22.17 | -1.611 | 0.000 | 0.146 |
| 144.00 | -12.94 | -5.61 | 0.00 | -109.56 | 0.00 | 109.56 | 1502.90 | 396.11 | 925.52 | 858.22 | 22.85 | -1.639 | 0.000 | 0.136 |
| 146.00 | -12.75 | -5.55 | 0.00 | -98.35 | 0.00 | 98.35 | 1487.88 | 389.11 | 893.06 | 834.49 | 23.55 | -1.665 | 0.000 | 0.127 |
| 148.00 | -12.56 | -5.49 | 0.00 | -87.26 | 0.00 | 87.26 | 1472.45 | 382.10 | 861.19 | 810.82 | 24.25 | -1.689 | 0.000 | 0.116 |
| 150.00 | -9.93 | -4.14 | 0.00 | -76.28 | 0.00 | 76.28 | 1456.60 | 375.09 | 829.89 | 787.25 | 24.96 | -1.712 | 0.000 | 0.104 |
| 152.00 | -9.76 | -4.08 | 0.00 | -68.01 | 0.00 | 68.01 | 1440.33 | 368.08 | 799.17 | 763.78 | 25.68 | -1.734 | 0.000 | 0.096 |
| 154.00 | -9.60 | -4.02 | 0.00 | -59.86 | 0.00 | 59.86 | 1423.65 | 361.08 | 769.03 | 740.42 | 26.41 | -1.754 | 0.000 | 0.088 |
| 156.00 | -9.44 | -3.96 | 0.00 | -51.82 | 0.00 | 51.82 | 1406.55 | 354.07 | 739.47 | 717.20 | 27.15 | -1.772 | 0.000 | 0.079 |
| 158.00 | -8.04 | -3.33 | 0.00 | -43.90 | 0.00 | 43.90 | 1389.03 | 347.06 | 710.49 | 694.11 | 27.90 | -1.789 | 0.000 | 0.069 |
| 160.00 | -7.90 | -3.28 | 0.00 | -37.24 | 0.00 | 37.24 | 1371.10 | 340.05 | 682.09 | 671.17 | 28.65 | -1.804 | 0.000 | 0.061 |
| 162.00 | -7.76 | -3.22 | 0.00 | -30.69 | 0.00 | 30.69 | 1352.75 | 333.05 | 654.27 | 648.41 | 29.41 | $-1.818$ | 0.000 | 0.053 |
| 164.00 | -7.62 | -3.17 | 0.00 | -24.24 | 0.00 | 24.24 | 1333.98 | 326.04 | 627.03 | 625.81 | 30.18 | -1.829 | 0.000 | 0.045 |
| 166.00 | -3.83 | -1.62 | 0.00 | -17.91 | 0.00 | 17.91 | 1314.79 | 319.03 | 600.37 | 603.42 | 30.94 | -1.839 | 0.000 | 0.033 |
| 168.00 | -3.71 | -1.56 | 0.00 | -14.68 | 0.00 | 14.68 | 1295.19 | 312.03 | 574.28 | 581.22 | 31.72 | -1.847 | 0.000 | 0.028 |
| 170.00 | -3.59 | -1.51 | 0.00 | -11.56 | 0.00 | 11.56 | 1275.17 | 305.02 | 548.78 | 559.24 | 32.49 | -1.853 | 0.000 | 0.024 |
| 172.00 | -3.47 | -1.46 | 0.00 | -8.54 | 0.00 | 8.54 | 1251.65 | 298.01 | 523.85 | 536.17 | 33.27 | -1.859 | 0.000 | 0.019 |
| 174.00 | -3.35 | -1.41 | 0.00 | -5.62 | 0.00 | 5.62 | 1222.21 | 291.00 | 499.51 | 511.11 | 34.05 | -1.863 | 0.000 | 0.014 |
| 176.00 | -3.23 | -1.36 | 0.00 | -2.81 | 0.00 | 2.81 | 1192.78 | 284.00 | 475.74 | 486.64 | 34.83 | -1.866 | 0.000 | 0.009 |
| 178.00 | -0.10 | -0.05 | 0.00 | -0.09 | 0.00 | 0.09 | 1163.35 | 276.99 | 452.55 | 462.78 | 35.61 | -1.867 | 0.000 | 0.000 |
| 180.00 | 0.00 | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 1133.92 | 269.98 | 429.95 | 439.52 | 36.39 | -1.867 | 0.000 | 0.000 |

## Final Analysis Summary

| Structure: | CT46130-A-SBA |  |  | Code: | EIA/TIA-222-H | 12/5/2019 | ( (1010) ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Name: | Deep River-winthrop Rd |  |  | Exposure: | C |  |  |
| Height: | 180.00 (ft) |  |  | Crest Height: | 0.00 |  | ES |
| Base Elev: | 0.000 (ft) |  |  | Site Class: | D - Stiff Soil |  |  |
| Gh: | 1.1 | Topography: | 1 | Struct Class: | II | Page: 45 | Tower Enginecting Solutions |

## Reactions

| Load Case | Shear FX (kips) | Shear FZ <br> (kips) |  | Moment MX <br> (ft-kips) | Moment MY (ft-kips) | Moment MZ (ft-kips) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2D + 1.0W 123 mph Wind | 45.8 | 0.00 | 56.46 | 0.00 | 0.00 | 5490.30 |
| 0.9D + 1.0W 123 mph Wind | 45.8 | 0.00 | 42.34 | 0.00 | 0.00 | 5425.51 |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 50 \mathrm{mph}$ Wind | 9.6 | 0.00 | 69.82 | 0.00 | 0.00 | 1165.43 |
| $1.2 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | 4.5 | 0.00 | 56.49 | 0.00 | 0.00 | 527.40 |
| $0.9 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | 4.5 | 0.00 | 42.37 | 0.00 | 0.00 | 520.82 |
| $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind | 10.9 | 0.00 | 47.07 | 0.00 | 0.00 | 1298.75 |

## Max Stresses

| Load Case | $\begin{gathered} \text { Pu } \\ \text { FY (-) } \\ \text { (kips) } \end{gathered}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | Tu MY (-) (ft-kips) | $\begin{gathered} \text { Mu } \\ \text { MZ } \\ \text { (ft-kips) } \end{gathered}$ | Mu <br> MX <br> (ft-kips) | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Elev <br> (ft) | Stress <br> Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2D + 1.0W 123 mph Wind | -56.46 | -45.76 | 0.00 | -5490.3 | 0.00 | -5490.3 | 5123.29 | 1522.0 | 7808.40 | 6435.29 | 0.00 | 0.865 |
| $0.9 D+1.0 W 123 \mathrm{mph}$ Wind | -42.34 | -45.75 | 0.00 | -5425.5 | 0.00 | -5425.5 | 5123.29 | 1522.0 | 7808.40 | 6435.29 | 0.00 | 0.852 |
| 1.2D + 1.0Di + 1.0Wi 50 mph Wind | -69.82 | -9.63 | 0.00 | -1165.4 | 0.00 | -1165.4 | 5123.29 | 1522.0 | 7808.40 | 6435.29 | 0.00 | 0.195 |
| $1.2 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | -16.40 | -2.63 | 0.00 | -79.87 | 0.00 | -79.87 | 1545.45 | 417.14 | 1026.36 | 929.77 | 138.00 | 0.097 |
| $0.9 \mathrm{D}+1.0 \mathrm{Ev}+1.0 \mathrm{Eh}$ | -12.29 | -2.57 | 0.00 | -78.36 | 0.00 | -78.36 | 1545.45 | 417.14 | 1026.36 | 929.77 | 138.00 | 0.092 |
| $1.0 \mathrm{D}+1.0 \mathrm{~W} 60 \mathrm{mph}$ Wind | -47.07 | -10.89 | 0.00 | -1298.7 | 0.00 | -1298.7 | 5123.29 | 1522.0 | 7808.40 | 6435.29 | 0.00 | 0.211 |

## Base Plate Summary

| Structure: | CT46130-A-SB |  | Code: | EIA/TIA-222-H | 12/5/2019 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Site Name: | Deep River-winthrop Rd |  | Exposure: | C |  |
| Height: | $180.00(\mathrm{ft})$ |  | Crest Height: | 0.00 |  |
| Base Elev: | $0.000(\mathrm{ft})$ |  | Site Class: | D-Stiff Soil |  |
| Gh: | 1.1 | Topography: | 1 | Struct Class: | II |


| Reactions |  | Base Plate |  | Anchor Bolts |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Original Design |  | Yield (ksi): | 60.00 | Bolt Circle: | 70.69 |
| Moment (kip-ft): | 5076.00 | Width (in): | 76.69 | Number Bolts: | 20.00 |
| Axial (kip): | 59.10 | Style: | Polygon | Bolt Type: | $2.25{ }^{\prime \prime} 18 \mathrm{~J}$ |
| Shear (kip): | 41.70 | Polygon Sides: | 12.00 | Bolt Diameter (in): | 2.25 |
| Analysis |  | Clip Length (in): | 0.00 | Yield (ksi): | 75.00 |
| Moment (kip-ft): | 5490.30 | Effective Len (in): | 14.14 | Ultimate (ksi): | 100.00 |
| Axial (kip): | 69.82 | Moment (kip-in): | 825.08 | Arrangement: | Radial |
| Shear (kip): | 45.76 | Allow Stress (ksi): | 81.00 | Cluster Dist (in): | 0.00 |
|  |  | Applied Stress (ksi): | 0.00 | Start Angle (deg): | 0.00 |
| Moment Design \%: | 108.16 | Stress Ratio: | 0.57 | Compression |  |
|  |  |  |  | Force (kip): | 189.89 |
|  |  |  |  | Allowable (kip): | 243.75 |
|  |  |  |  | Ratio: | 0.78 |
|  |  |  |  | Tens |  |
|  |  |  |  | Force (kip): | 182.91 |
|  |  |  |  | Allowable (kip): | 243.75 |
|  |  |  |  | Ratio: | 0.75 |



## Check the capacities of Reinforceing Concrete:

Strength reduction factor (Flexure and axial tension):
5trength reduction factor (Axial compresion):

Concrete Pad:
One-Way Design Shear Capacity (L-Direction, Kips):
One-Way Design Shear Capacity (W-Direction, Kips):
One-Way Design Shear Capacity (Corner-Corner. Kips):
Lower Steel Pad Reinforcement Ratio (L-Direct. ):
Lower Steel Pad Moment Capacity (L-Direction. Kips-ft):
Lower Steel Pad Moment Capacity (W-Direction. Kips-ft):
Lower Steel Pad Moment Capacity (Corner-Corner, K-ft):
Upper Steel Pad Reinforcement Ratio (L-Direct. ):
Upper Steel Pad Moment Capacity (L-Direction. Kips-ft):
Upper Steel Pad Moment Capacity (W-Direction. Kips-ft):
Upper Steel Pad Moment Capacity (Corner-Corner, K-ft):

| 0.90 | Strength reduction factor (Shear): | 0.75 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.65 | Wind Load Factor on Concrete Design: | 1.00 |  |  |  |  |
|  |  |  |  |  |  |  |
| 1732.8 | $>$ | One-Way Factored Shear (L-D. Kips): | 341.2 | 0.20 | OK! |  |
| 1732.8 | $>$ | One-Way Factored Shear (W-D., Kips): | 341.2 | 0.20 | OK! |  |
| 2040.5 | $>$ | One-Way Factored Shear (C-C, Kips): | 740.1 | 0.36 | OK! |  |
| 0.0014 | OK! | Lower Steel Pad Reinf. Ratio (W-Direc | 0.0014 |  |  |  |
| 6364.6 | $>$ | Moment at Bottom (L-Direct. K-Ft); | 956.5 | 0.15 | OK! |  |
| 6364.6 | $>$ | Moment at Bottom (W-Direct. K-Ft): | 956.5 | 0.15 | OK! |  |
| 8978.4 | $>$ | Moment at Bottom (C-C Dir. K-Ft): | 1352.7 | 0.15 | OK! |  |
| 0.0019 | OK! | Upper Steel Reinf. Ratio (W-Direct. ): | 0.0019 |  |  |  |
| 8866.2 | $>$ | Moment at the top (L-Dir Kips-Ft): | 45.2 | 0.01 | OK! |  |
| 8866.2 | $>$ | Moment at the top (W-Dir Kips-Ft): | 45.2 | 0.01 | OK! |  |
| 12494.6 | $>$ | Moment at the top (C-C Direc. K-Ft): | 776.2 | 0.06 | OK! |  |

## PF PAUL J. FORD \& COMPANY

Report Date:
Client:

Structure:
Carrier:
Carrier Site Name:
Mount Type:
Site Address:
City, County, State:
Latitude, Longitude:

December 13, 2019
On Air Engineering, LLC 88 Foundry Pond Road Cold Spring, NY 10516
Attn: David Weinpahl, P.E.
(201) 456-4624

Existing 180-ft Monopole
Verizon Wireless
Deep River West CT
(1) 13.5 Foot Platform

220 Winthrop Rd
Deep River, Middlesex County, CT
41.365772, -72.475314

PJF Project:
A42919-0016.001.7190
Paul J. Ford and Company is pleased to submit this "Mount Structural Analysis Report". The purpose of this analysis is to determine if the mount has sufficient capacity to support the equipment described herein. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point is not part of this document.

## Analysis Criteria:

Reference Standard:
2018 Connecticut State Building Code with the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception \#5 of Section 1609.1.1.

Ultimate Wind Speed: 130 mph 3 -second gust wind speed without ice Nominal Wind Speed: 101 mph 3 -second gust wind speed without ice
Ice Wind Speed:

## Summary of Analysis Results:

Antenna Mount: $>\mathbf{2 0 0 \%} \quad$ INSUFFICIENT

We at Paul J. Ford and Company appreciate the opportunity of providing our continuing professional services to you and On Air Engineering, LLC. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully Submitted by: Paul J. Ford and Company

Gowtham Penumatsa
Structural Designer
gpenumatsa@pauljford.com AMS

## Columbus

250 E Broad St, Suite 600
Columbus, OH 43215
Phone 614.221.6679

www.PaulJFord.com
100\% Employee Owned

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## 1) INTRODUCTION

The existing mount under consideration is (1) 13.5 Platform installed at the $178^{\prime}$ elevation on a $180^{\prime}$ Monopole tower. The existing mount considered in this analysis is identified as a Valmont DCA152Z based on photos.

## 2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the 2018 Connecticut State Building Code based upon an ultimate 3 -second gust wind speed of 130 mph converted to a nominal 3 -second gust wind speed of 101 mph per section 1609.3 .1 as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception \#5 of Section 1609.1.1. and 50 mph with 0.75 inch ice thickness. Risk Category II, Exposure Category C and Topographic Category 1 with a maximum Topographic Factor, Kzt, of 1 were used in this analysis.

In addition, the mount has been analyzed for various live loading conditions consisting of a 250 -pound maintenance live load applied individually at the midpoint and cantilevered ends of horizontal members as well as a 250 pound maintenance live load applied individually at mount pipe locations using a 3-second wind speed of 30 mph .

Table 1 - Equipment Configuration

| Mounting Level (feet) | Center Line Elevation (feet) | Quantity | Manufacture r | : Model | Status | Mount Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 178 | 178 | 1 | Raycap | RRFDC-6627-PF-48 | Proposed | Tower Mounted |
|  |  | 3 | JMA | 9190314 Dual Bracket Mounts |  | (1)13.5' Platform |
|  |  | 6 | JMA Wireless | MX06FRO660-03 |  |  |
|  |  | 3 | Samsung Telecomm | B2/B66A RRH BR049 |  |  |
|  |  | 3 | Samsung <br> Telecomm | B15/B13 RRH BR04C |  |  |
|  |  | 6 | Antel | BXA-70063-6CF-2 | Equipment to be removed |  |
|  |  | 6 | Antel | BXA-171063-12CF-EDIN-2 |  |  |
|  |  | 3 | Nokia | B13 RRH 2X40 |  |  |
|  |  | 2 | RFS | DB-B1-6C-8AB-0Z |  |  |

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Mount Manufacturer Drawings | Valmont, $10 / 30 / 1997$ | DCA152Z | Valmont |
| Site Photos | Dated $12 / 9 / 2019$ | - | On Air Engineering |
| Radio Frequency Data Sheet | Verizon, $10 / 15 / 2019$ | 15284229 | On Air Engineering |

## 3.1) Analysis Method

RISA-3D (version 17.0.3), a commercially available analysis software package, was used to create a three-dimensional model of the mount and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix C. In addition, this analysis is in accordance with Verizon's NSTD-446 Antenna Mount Analysis and Modification Process (dated 03/29/19).

## 3.2) Assumptions

1) The analysis of the existing monopole tower or the effect of the mount attachment to the tower is not within the current scope of work.
2) The antenna mounting system was properly fabricated, installed and maintained in good condition, twist free and plumb in accordance with its original design and manufacturer's specifications and all bolts are tightened as specified by the manufacturer and AISC requirements.
3) The configuration of antennas, mounts, and other appurtenances are as specified in Table 1.
4) All member connections have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report. All U-Bolt connections have been properly tightened. This analysis will be required to be revised if the existing conditions in the field differ from those shown in the above referenced documents or assumed in this analysis. No allowance was made for any damaged, missing, or rusted members.
5) Steel grades have been assumed as follows:

| a) Channel, Solid Round, Angle, Plate, Unistrut | ASTM A36 (GR 36) |
| :--- | :--- |
| b) Pipe | ASTM A53 (GR 35) |
| c) HSS (Rectangular) | ASTM 500 (GR B-46) |
| d) HSS (Round) | ASTM 500 (GR B-42) |
| e) Connection Bolts | ASTM A325 |
| f) Threaded Rods | ASTM F1554 (GR 36) |
| g) U-Bolts | $S A E$ J429 (GR2) |

6) Proposed equipment is to be installed in the locations specified in Appendix A. Any changes to the proposed equipment locations will render this report invalid.
7) Mount has been modeled based on the photographs referenced in Table 2, indicating a match to the Valmont mount model \#DCA1522. Member information and dimensions not provided have been assumed to match those specified in the manufacturer drawings referenced in Table 2. No guarantee can be made as to the accuracy of these assumptions without a complete mount mapping.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 3 - Mount Component Capacity

| Notes | Component | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: |
| 1 | Mount Pipes | 157.4 | Fail |
| 1 | Face Horizontal | $>200$ | Fail |
| 1 | Standoff Members | 159.1 | Fail |
| 1 | Support Rail | 188.1 | Fail |
| 1 | Corner Plates | 171.4 | Fail |
| 1 | Grating Support Members | 12.2 | Pass |
| 1 | Mount to Tower Connection |  |  |
| (bolts/welds) | $>200$ | Fail |  |

Mount Rating (max from all components) =
Notes:

1. See additional documentation in "Appendix C - Software analysis Output" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The mount does not have sufficient capacity to carry the proposed loading configuration. Modifications will be required to bring the mount into compliance with the TIA-222-G Standard for the proposed loading configuration. Listed below is a brief description of the required modification:

- Provide kickers
- Provide hand rail kits
- Provide bracing kits
- Custom Modification reinforcement
- Estimated Cost: >\$10,000

Or

- Mount Replacement is recommended due to the severity of insufficiency.

Further engineering and detailing is required to design the necessary modifications. Connection from the mount to the tower and local stresses on the tower are insufficient.

## STANDARD CONDITIONS FOR FURNISHING OF PROFESSIONAL ENGINEERING SERVICES ON EXISTING MOUNTS BY PAUL J. FORD AND COMPANY

1) It is the responsibility of the client to ensure that the information provided to Paul J. Ford and Company is accurate and complete. Paul J. Ford and Company will rely on the accuracy and completeness of such information in performing or furnishing services under this project.
2) If the existing conditions are not as represented on the referenced drawings and/or documents, Paul J. Ford and Company should be contacted immediately to evaluate the significance of the deviation.
3) The mount has been analyzed according to the minimum design loads recommended by the Reference Standard. If additional design loads are required, Paul J. Ford and Company should be made aware of this prior to the start of the project.
4) The standard of care for all Professional Engineering Services performed or furnished by Paul J. Ford and Company under this project will be the skill and care used by members of the Consultant's profession practicing under similar circumstances at the same time and in the same locality.
5) All Services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Paul J. Ford and Company is not responsible for the conclusions, opinions and/or recommendations made by others based on the information supplied herein.

## APPENDIX A

## WIRE FRAME AND RENDERED MODELS

## APPENDIX B

## SOFTWARE INPUT CALCULATIONS



LEGEND EXISTING: BLUE PROPOSED: RED
(2) JMA WIRELESS MX06FRO660-3 ON JMA BRACKET \#91900314 (TYP, ALL SECTORS)
(1) SAMSUMG TELECOMM B15/B13 RRH BR04C (TYP, ALL SECTORS)


## NOTES:

1) A 6" VERTICAL TOLERANCE FOR PROPOSED EQUIPMENT IS ACCEPTABLE.
2) CONTRACTOR TO VERIFY LOCATION OF EXISTING EQUIPMENT PRIOR TO INSTALLATION OF PROPOSED EQUIPMENT. NOTIFY EOR FOR ANY DEVIATIONS.
3) INSTALL SHALL NOT CAUSE HARM TO THE STRUCTURE, CLIMBING FACILITY, SAFETY CLIMB OR ANY SYSTEM INSTALLED ON THE STRUCTURE.
Envelope Only Solution
Paul J. Ford and Company AZIMUTH $220^{\circ}$

SK-2
Dec 13, 2019 at 3:44 PM
42919-0016.001.7190_MA..r3d

## APPENDIX B

## SOFTWARE INPUT CALCULATIONS

PJF PaUl Jjard
250 E Broad St, Ste 600 - Columbus, OH 43215
Phone $614.221 .6679 \quad$ www.pauljford.com


## ASCE 7 Hazards Report

| Standard: | ASCE/SEI 7-10 | Elevation: |
| :--- | :--- | :--- |
| Risk Category: | II | Latit.52 ft (NAVD 88) |
| Soil Class: | D - Stiff Soil | Longitude: -72.4755314 |



## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

130 Vmph
78 Vmph
88 Vmph
96 Vmph
106 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Thu Dec 122019

Date Accessed:
Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure $C$ Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI $=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

| Site Soil Class: | D - Stiff Soil |  |  |
| :---: | :---: | :---: | :---: |
| Results: |  |  |  |
| $\mathrm{S}_{5}$ | 0.17 | $S_{\text {DS }}$ | 0.182 |
| $\mathrm{S}_{1}$ | 0.06 | $S_{\text {D1 }}$ | 0.096 |
| $\mathrm{F}_{\mathrm{a}}$ | 1.6 | $\mathrm{T}_{\mathrm{L}}$ : | 6 |
| $F_{v}$ | 2.4 | PGA | 0.086 |
| $\mathrm{S}_{\mathrm{MS}}$ : | 0.272 | PGA m: | 0.137 |
| $\mathrm{S}_{\mathrm{M} 1}$ | 0.144 | $\mathrm{F}_{\text {PGA }}$ | 1.6 |
|  |  | $l_{\text {e }}$ : | 1 |
| Seismic Design Category Data Accessed: | Brin Dec 122019 |  |  |
| Date Source: | USGS Supp Additi ASCE | Maps ata of Ma -specific are ava | CE/SEI |

## Results:

| Ice Thickness: | 0.75 in. |
| :--- | :--- |
| Concurrent Temperature: | 15 F |
| Gust Speed: | 50 mph |
| Source: | Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8 |
| Accessed: | Thu Dec 12 2019 |

Date Accessed: -Thu Dec 122019
Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

[^3]
## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT



Member Code Checks Displayed (Enveloped)
Envelope Only Solution
Paul J. Ford and Company
$\qquad$

| GP |
| :--- |
| $42919-0016.001 .7190$ |

DEEP RIVER WEST CT

SK - 3
Dec 13, 2019 at 3:44 PM
42919-0016.001.7190_MA..r3d


Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

| Paul J. Ford and Company | DEEP RIVER WEST CT | SK-4 |
| :---: | :---: | :---: |
| GP |  | Dec 13, 2019 at 3:45 PM |
| 42919-0016.001.7190 |  | 42919-0016.001.7190_MA.r3d |





Loads: BLC 1, Dead
Envelope Only Solution
Paul J. Ford and Company

SK-7
Dec 13, 2019 at 3:48 PM
42919-0016.001.7190_MA..r3d




## (Global) Model Settings

| Display Sections for Member Calcs | 5 |
| :--- | :--- |
| Max Internal Sections for Member Calcs | 97 |
| Include Shear Deformation? | Yes |
| Increase Nailing Capacity for Wind? | Yes |
| Include Warping? | Yes |
| Trans Load Btwn Intersecting Wood Wall? | Yes |
| Area Load Mesh (in^2) | 144 |
| Merge Tolerance (in) | .12 |
| P-Delta Analysis Tolerance | $0.50 \%$ |
| Include P-Delta for Walls? | Yes |
| Automatically Iterate Stiffness for Walls? | No |
| Max Iterations for Wall Stiffness | 3 |
| Gravity Acceleration (in/sec^2) | 386.4 |
| Wall Mesh Size (in) | 12 |
| Eigensolution Convergence Tol. (1.E-) | 4 |
| Vertical Axis | Y |
| Global Member Orientation Plane | XZ |
| Static Solver | Sparse Accelerated |
| Dynamic Solver | Accelerated Solver |


| Hot Rolled Steel Code | AISC 14th(360-10): LRFD |
| :--- | :--- |
| Adjust Stiffness? | Yes(Iterative) |
| RISAConnection Code | None |
| Cold Formed Steel Code | AISI S100-12: LRFD |
| Wood Code | None |
| Wood Temperature | $<100 F$ |
| Concrete Code | None |
| Masonry Code | None |
| Aluminum Code | None - Building |
| Stainless Steel Code | AlSC 14th(360-10): ASD |
| Adjust Stiffness? | Yes(Iterative) |


| Number of Shear Regions | 4 |
| :--- | :--- |
| Region Spacing Increment (in) | 4 |
| Biaxial Column Method | Exact Integration |
| Parme Beta Factor (PCA) | .65 |
| Concrete Stress Block | Rectangular |
| Use Cracked Sections? | Yes |
| Use Cracked Sections Slab? | Yes |
| Bad Framing Warnings? | No |
| Unused Force Warnings? | Yes |
| Min 1 Bar Diam. Spacing? | No |
| Concrete Rebar Set | REBAR SET ASTMA615 |
| Min \% Steel for Column | 1 |
| Max \% Steel for Column | 8 |



## (Global) Model Settings, Continued

| Seismic Code | ASCE 7-05 |
| :--- | :--- |
| Seismic Base Elevation (in) | Not Entered |
| Add Base Weight? | Yes |
| Ct X | .02 |
| Ct Z | .02 |
| TX (sec) | Not Entered |
| T Z (sec) | Not Entered |
| R X | 3 |
| R Z | 3 |
| Ct Exp. X | .75 |
| Ct Exp. Z | .75 |
| SD1 | 1 |
| SDS | 1 |
| S1 | 1 |
| TL (sec) | 5 |
| Occupancy Cat | 1 or II |
| Drift Cat | Other |
| Om Z | 1 |
| Om X | 1 |
| Cd Z | 4 |
| Cd X | 4 |
| Rho Z | 1 |
| Rho X | 1 |
|  |  |

## Hot Rolled Steel Properties

| Label |  | E [ksi] | G[ksi] | Nu | Therm (/1E. Densitylkft. |  | Yield[ksi] Ry |  | Fu[ksi] Rt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | 49 | 36 | 1.5 | 58 | 1.2 |
| 2 | A572 Gr. 50 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 3 | A992 | 29000 | 11154 | 3 | 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr. 42 | 29000 | 11154 | 3 | 65 | 49 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr. 46 | 29000 | 11154 | 3 | 65 | 49 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr. B ( 35 ksi ) | 29000 | 11154 | 3 | 65 | 49 | 35 | 1.5 | 60 | 1.2 |

Member Primary Data


## Member Primary Data (Continued)

|  | Label | 1 Joint | $J$ Joint | $K$ Joint Rotate(. | Section/Shape | Type | Design Lis | Material | Design Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | M29 | N74A | N73A |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 22 | M30 | N58 | N59 |  | RIGID | None | None | RIGID | Typical |
| 23 | M31 | N60 | N61 |  | RIGID | None | None | RIGID | Typical |
| 24 | M32 | N62 | N63 |  | RIGID | None | None | RIGID | Typical |
| 25 | M33 | N64 | N65 |  | RIGID | None | None | RIGID | Typical |
| 26 | M34 | N67 | N66 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 27 | BB3 | N69A | N68 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 28 | M25B | N71 | N70A |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 29 | M40 | N73B | N72 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 30 | M41 | N75 | N76 |  | RIGID | None | None | RIGID | Typical |
| 31 | M42 | N77 | N78 |  | RIGID | None | None | RIGID | Typical |
| 32 | M43 | N79 | N80 |  | RIGID | None | None | RIGID | Typical |
| 33 | M44 | N81 | N82 |  | RIGID | None | None | RIGID | Typical |
| 34 | M45 | N84 | N83 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 35 | AA3 | N86 | N85 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 36 | 25A | N88 | N87 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 37 | M51 | N90 | N89 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 38 | M52 | N89A | N90A | 180 | L2 $\times 2 \times 4$ | None | None | A36 Gr. 36 | Typical |
| 39 | M55 | N95 | N96 |  | RIGID | None | None | RIGID | Typical |
| 40 | M56 | N97 | N98 |  | RIGID | None | None | RIGID | Typical |
| 41 | M57 | N99 | N100 |  | RIGID | None | None | RIGID | Typical |
| 42 | M58 | N101 | N102 |  | RIGID | None | None | RIGID | Typical |
| 43 | M62 | N104 | N105 |  | RIGID | None | None | RIGID | Typical |
| 44 | M63 | N106 | N107 |  | RIGID | None | None | RIGID | Typical |
| 45 | M64 | N108 | N109 |  | RIGID | None | None | RIGID | Typical |
| 46 | M65 | N110A | N111 |  | RIGID | None | None | RIGID | Typical |
| 47 | M69 | N113 | N114 |  | RIGID | None | None | RIGID | Typical |
| 48 | M70 | N115 | N116 |  | RIGID | None | None | RIGID | Typical |
| 49 | M71 | N117 | N118 |  | RIGID | None | None | RIGID | Typical |
| 50 | M72 | N119 | N120 |  | RIGID | None | None | RIGID | Typical |
| 51 | C4 | N120A | N119A |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 52 | C3 | N122 | N121 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 53 | C2 | N124 | N123 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 54 | C1 | N126 | N125 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 55 | B4 | N145 | N144 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 56 | B3 | N147 | N146 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 57 | B2 | N149 | N148 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 58 | B1 | N151 | N150 |  | PIPE 2.0 | None | None | A53 Gr. B (35 ksi) | Typical |
| 59 | A4 | N170A | N169 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 60 | A3 | N172 | N171A |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 61 | A2 | N174 | N173 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 62 | A1 | N176 | N175 |  | PIPE 2.0 | None | None | A53 Gr. B ( 35 ksi ) | Typical |
| 63 | M90 | N191A | N192A | 180 | C5X6.7 | None | None | A36 Gr. 36 | Typical |
| 64 | M91 | N194 | N195 | 180 | L2x2x4 | None | None | A36 Gr. 36 | Typical |
| 65 | M92A | N196 | N197 | 180 | C5X6.7 | None | None | A36 Gr. 36 | Typical |
| 66 | M93A | N199 | N200 | 180 | L2x2x4 | None | None | A36 Gr. 36 | Typical |
| 67 | M94A | N199A | N200A | 90 | HSS4X4X3 | None | None | A500 Gr. 46 | Typical |
| 68 | M95A | N201 | N202 | 90 | HSS4X4X3 | None | None | A500 Gr. 46 | Typical |
| 69 | M96A | N203 | N204 | 90 | HSS4X4X3 | None | None | A500 Gr. 46 | Typical |
| 70 | M94B | N207 | N167 |  | RIGID | None | None | RIGID | Typical |
| 71 | M95B | N206 | N165 |  | RIGID | None | None | RIGID | Typical |
| 72 | M96B | N205 | N163 |  | RIGID | None | None | RIGID | Typical |
| 73 | M97A | N209 | N217 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 74 | M98A | N205A | N213 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 75 | M105A | N225 | N233 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 76 | M106A | N221 | N229 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 77 | M105B | N229 | N138 |  | RIGID | None | None | RIGID | Typical |

## Member Primary Data (Continued)

|  | Label | 1 Joint | $J$ Joint | K Joint Rotatel. | Section/Shape | Type | Desian Lis | Material | Desian Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 78 | M106B | N213 | N138 |  | RIGID | None | None | RIGID | Typical |
| 79 | M107B | N221 | N130 |  | RIGID | None | None | RIGID | Typical |
| 80 | M108B | N205A | N130 |  | RIGID | None | None | RIGID | Typical |
| 81 | M109B | N233 | N142 |  | RIGID | None | None | RIGID | Typical |
| 82 | M110B | N217 | N142 |  | RIGID | None | None | RIGID | Typical |
| 83 | M111B | N225 | N134 |  | RIGID | None | None | RIGID | Typical |
| 84 | M112A | N209 | N134 |  | RIGID | None | None | RIGID | Typical |
| 85 | M101 | N203A | N205B |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 86 | M102 | N202A | N204A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 87 | M103 | N207A | N209A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 88 | M104A | N206A | N208 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 89 | M105C | N208 | N200B |  | RIGID | None | None | RIGID | Typical |
| 90 | M106C | N204A | N200B |  | RIGID | None | Nonè | RIGID | Typical |
| 91 | M107A | N206A | N198 |  | RIGID | None | None | RIGID | Typical |
| 92 | M108A | N202A | N198 |  | RIGID | None | None | RIGID | Typical |
| 93 | M109A | N209A | N201A |  | RIGID | None | None | RIGID | Typical |
| 94 | M110A | N205B | N201A |  | RIGID | None | None | RIGID | Typical |
| 95 | M111A | N207A | N199B |  | RIGID | None | None | RIGID | Typical |
| 96 | M112 | N203A | N199B |  | RIGID | None | None | RIGID | Typical |
| 97 | M113 | N215 | N217A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 98 | M114 | N214 | N216 |  | $1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 99 | M115 | N219 | N221A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 100 | M116 | N218 | N220 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 101 | M117 | N220 | N212 |  | RIGID | None | None | RIGID | Typical |
| 102 | M118 | N216 | N212 |  | RIGID | None | None | RIGID | Typical |
| 103 | M119 | N218 | N210 |  | RIGID | None | None | RIGID | Typical |
| 104 | M120 | N214 | N210 |  | RIGID | None | None | RIGID | Typical |
| 105 | M121 | N221A | N213A |  | RIGID | None | None | RIGID | Typical |
| 106 | M122 | N217A | N213A |  | RIGID | None | None | RIGID | Typical |
| 107 | M123 | N219 | N211 |  | RIGID | None | None | RIGID | Typical |
| 108 | M124 | N215 | N211 |  | RIGID | None | None | RIGID | Typical |
| 109 | M125 | N227 | N229A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 110 | M126 | N226 | N228 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 111 | M127 | N231 | N233A |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 112 | M128 | N230 | N232 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 113 | M129 | N232 | N224 |  | RIGID | None | None | RIGID | Typical |
| 114 | M130 | N228 | N224 |  | RIGID | None | None | RIGID | Typical |
| 115 | M131 | N230 | N222 |  | RIGID | None | None | RIGID | Typical |
| 116 | M132 | N226 | N222 |  | RIGID | None | None | RIGID | Typical |
| 117 | M133 | N233A | N225A |  | RIGID | None | None | RIGID | Typical |
| 118 | M134 | N229A | N225A |  | RIGID | None | None | RIGID | Typical |
| 119 | M135 | N231 | N223 |  | RIGID | None | None | RIGID | Typical |
| 120 | M136 | N227 | N223 |  | RIGID | None | None | RIGID | Typical |
| 121 | M121A | N240 | N242 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 122 | M122A | N239 | N241 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 123 | M123A | N244 | N246 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 124 | M124A | N243 | N245 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 125 | M125A | N245 | N163A |  | RIGID | None | None | RIGID | Typical |
| 126 | M126A | N241 | N163A |  | RIGID | None | None | RIGID | Typical |
| 127 | M127A | N243 | N155 |  | RIGID | None | None | RIGID | Typical |
| 128 | M128A | N239 | N155 |  | RIGID | None | None | RIGID | Typical |
| 129 | M129A | N246 | N167B |  | RIGID | None | None | RIGID | Typical |
| 130 | M130A | N242 | N167B |  | RIGID | None | None | RIGID | Typical |
| 131 | M131A | N244 | N159 |  | RIGID | None | None | RIGID | Typical |
| 132 | M132A | N240 | N159 |  | RIGID | None | None | RIGID | Typical |
| 133 | M133A | N252 | N254 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 134 | M134A | N251 | N253 |  | 1/2" | None | None | A36 Gr. 36 | Typical |

## Member Primary Data (Continued)




## Member Primary Data (Continued)

|  | Label | 1 Joint | $J$ Joint | K Joint Rotate(. | Section/Shape | Type | Desian List | Material | Desian Rules |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 192 | M192 | N301 | N183 |  | RIGID | None | None | RIGID | Typical |
| 193 | M193 | N313 | N315 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 194 | M194 | N312 | N314 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 195 | M195 | N317 | N319 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 196 | M196 | N316 | N318 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 197 | M197 | N318 | N186 |  | RIGID | None | None | RIGID | Typical |
| 198 | M198 | N314 | N186 |  | RIGID | None | None | RIGID | Typical |
| 199 | M199 | N316 | N178 |  | RIGID | None | None | RIGID | Typical |
| 200 | M200 | N312 | N178 |  | RIGID | None | None | RIGID | Typical |
| 201 | M201 | N319 | N190 |  | RIGID | None | None | RIGID | Typical |
| 202 | M202 | N315 | N190 |  | RIGID | None | None | RIGID | Typical |
| 203 | M203 | N317 | N182 |  | RIGID | None | None | RIGID | Typical |
| 204 | M204 | N313 | N182 |  | RIGID | None | None | RIGID | Typical |
| 205 | M205 | N325 | N327 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 206 | M206 | N324 | N326 |  | $1 / 2^{\prime \prime}$ | None | None | A36 Gr. 36 | Typical |
| 207 | M207 | N329 | N331 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 208 | M208 | N328 | N330 |  | 1/2" | None | None | A36 Gr. 36 | Typical |
| 209 | M209 | N330 | N185 |  | RIGID | None | None | RIGID | Typical |
| 210 | M210 | N326 | N185 |  | RIGID | None | None | RIGID | Typical |
| 211 | M211 | N328 | N177 |  | RIGID | None | None | RIGID | Typical |
| 212 | M212 | N324 | N177 |  | RIGID | None | None | RIGID | Typical |
| 213 | M213 | N331 | N189 |  | RIGID | None | None | RIGID | Typical |
| 214 | M214 | N327 | N189 |  | RIGID | None | None | RIGID | Typical |
| 215 | M215 | N329 | N181 |  | RIGID | None | None | RIGID | Typical |
| 216 | M216 | N325 | N181 |  | RIGID | None | None | RIGID | Typical |
| 217 | CC1 | N298 | N299 |  | CF1 | Beam | None | A570 Gr. 33 | Typical |
| 218 | CC2 | N300A | N301A |  | CF1 | Beam | None | A570 Gr. 33 | Typical |
| 219 | BB1 | N303A | N304A |  | CF1 | Beam | None | A570 Gr. 33 | Typical |
| 220 | BB2 | N305A | N306A |  | CF1 | Beam | None | A570 Gr. 33 | Typical |
| 221 | AA1 | N308 | N309 |  | CF1 | Beam | None | A570 Gr. 33 | Typical |
| 222 | AA2 | N310 | N311 |  | CF1 | Beam | None | A570 Gr. 33 | Typical |

## Member Advanced Data

|  | Label | 1 Release | $J$ Release | 1 Offset[in] | $J$ Offset[in] | T/C Only | Physical | Defl Rat... | Analysis.. | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 2 | M5 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 3 | M6 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 4 | M7 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 5 | M8 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 6 | M10 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 7 | M12 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 8 | M13 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 9 | M14 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 10 | M15 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 11 | M16 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 12 | M17 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 13 | M18 |  | BenPIN |  |  |  | Yes | ** NA ** |  |  | None |
| 14 | M19 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 15 | M20 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 16 | M21 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 17 | M22 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 18 | M23 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 19 | CC3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 20 | M25 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 21 | M29 |  |  |  |  |  | Yes | \|** NA **| |  |  | None |

Company
Paul J. Ford and Company
Dec 13, 2019
Designer
Job Number
GP
42919-0016.001.7190
3:57 PM
Model Name
DEEP RIVER WEST CT
Checked By:

Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | 1 Offsetlinl | $J$ Offsetlin] | T/C. Only | Physical | Defl Rat... | Analvsis. | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | M30 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 23 | M31 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 24 | M32 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 25 | M33 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 26 | M34 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 27 | BB3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 28 | M25B |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 29 | M40 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 30 | M41 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 31 | M42 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 32 | M43 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 33 | M44 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 34 | M45 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 35 | AA3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 36 | 25A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 37 | M51 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 38 | M52 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 39 | M55 | O00X00 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 40 | M56 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 41 | M57 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 42 | M58 | OOOXOO |  |  |  |  | Yes | ** NA ** |  |  | None |
| 43 | M62 | OOOXOO |  |  |  |  | Yes | ** NA ** |  |  | None |
| 44 | M63 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 45 | M64 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 46 | M65 | $000 \times 00$ |  |  |  |  | Yes | **NA ** |  |  | None |
| 47 | M69 | 000×00 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 48 | M70 | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 49 | M71 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 50 | M72 | 000×00 |  |  |  |  | Yes | ** NA ** |  |  | None |
| 51 | C4 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 52 | C3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 53 | C2 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 54 | C1 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 55 | B4 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 56 | B3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 57 | B2 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 58 | B1 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 59 | A4 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 60 | A3 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 61 | A2 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 62 | A1 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 63 | M90 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 64 | M91 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 65 | M92A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 66 | M93A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 67 | M94A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 68 | M95A |  |  |  |  |  | Yes | ${ }^{* *}$ NA *** |  |  | None |
| 69 | M96A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 70 | M94B | BenPIN |  |  |  |  | Yes | ${ }^{* *} N A$ ** |  |  | None |
| 71 | M95B | BenPIN |  |  |  |  | Yes | ** NA ** |  |  | None |
| 72 | M96B | BenPin |  |  |  |  | Yes | ** NA ** |  |  | None |
| 73 | M97A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 74 | M98A | O00XOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 75 | M105A | OOOXOX |  |  |  |  | Yes | ${ }^{* *}$ NA ** |  |  | None |
| 76 | M106A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 77 | M105B |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 78 | M106B |  |  |  |  |  | Yes | ** $N$ A ** |  |  | None |

Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | 1 Offsetiin] | $J$ Offset[in] | T/C Only | Physic | Deff Rat...A | Analysis | Inactive | Seismic. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 79 | M107B | Release |  |  |  |  | Yes | **NA ** |  |  | None |
| 80 | M108B |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 81 | M109B |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 82 | M110B |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 83 | M111B |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 84 | M112A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 85 | M101 | OOOX0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 86 | M102 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 87 | M103 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None. |
| 88 | M104A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 89 | M105C |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 90 | M106C |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 91 | M107A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 92 | M108A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 93 | M109A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 94 | M110A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 95 | M111A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 96 | M112 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 97 | M113 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 98 | M114 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 99 | M115 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 100 | M116 | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 101 | M117 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 102 | M118 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 103 | M119 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 104 | M120 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 105 | M121 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 106 | M122 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 107 | M123 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 108 | M124 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 109 | M125 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 110 | M126 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 111 | M127 | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 112 | M128 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 113 | M129 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 114 | M130 |  |  |  |  |  | Yes | ${ }^{* *}$ NA ** |  |  | None |
| 115 | M131 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 116 | M132 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 117 | M133 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 118 | M134 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 119 | M135 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 120 | M136 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 121 | M121A | O00X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 122 | M122A | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 123 | M123A | O00X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 124 | M124A | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 125 | M125A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 126 | M126A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 127 | M127A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 128 | M128A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 129 | M129A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 130 | M130A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 131 | M131A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 132 | M132A |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 133 | M133A | 000X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 134 | M134A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 135 | M135A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |

$\qquad$
DEEP RIVER WEST CT

Member Advanced Data (Continued)

|  | Label | 1 Release | J Release | 10 ffset [in] | $J$ Offsetiin] | T/C Only | Physical | Defl Rat... | Analysis . | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 136 | M136A | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 137 | M137 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 138 | M138 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 139 | M139 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 140 | M140 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 141 | M141 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 142 | M142 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 143 | M143 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 144 | M144 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 145 | M145 | OOOX0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 146 | M146 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 147 | M147 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 148 | M148 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 149 | M149 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 150 | M150 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 151 | M151 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 152 | M152 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 153 | M153 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 154 | M154 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 155 | M155 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 156 | M156 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 157 | M157 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 158 | M158 | O00X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 159 | M159 | O00X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 160 | M160 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 161 | M161 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 162 | M162 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 163 | M163 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 164 | M164 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 165 | M165 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 166 | M166 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 167 | M167 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 168 | M168 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 169 | M169 | 000X0X |  |  |  |  | Yes | **NA ** |  |  | None |
| 170 | M170 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 171 | M171 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 172 | M172 | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 173 | M173 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 174 | M174 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 175 | M175 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 176 | M176 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 177 | M177 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 178 | M178 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| ¢179 | M179 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 180 | M180 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 181 | M181 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 182 | M182 | OOOXOX |  |  |  |  | Yes | **NA ** |  |  | None |
| 183 | M183 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 184 | M184 | 000X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 185 | M185 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 186 | M186 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 187 | M187 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 188 | M188 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 189 | M189 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 190 | M190 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 191 | M191 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 192 | M192 |  |  |  |  |  | Yes | ** NA ** |  |  | None |

## Member Advanced Data (Continued)

|  | Label | 1 Release | $J$ Release | $10 f f$ set[in] | $J$ Offset[in] | T/C Only | Physica | Defl Rat. | Analysis ... | Inactive | Seismic... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 193 | M193 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 194 | M194 | O00X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 195 | M195 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 196 | M196 | 000X0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 197 | M197 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 198 | M198 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 199 | M199 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 200 | M200 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 201 | M201 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 202 | M202 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 203 | M203 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 204 | M204 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 205 | M205 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 206 | M206 | 000x0X |  |  |  |  | Yes | ** NA ** |  |  | None |
| 207 | M207 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 208 | M208 | OOOXOX |  |  |  |  | Yes | ** NA ** |  |  | None |
| 209 | M209 |  |  |  |  |  | Yes | **NA ** |  |  | None |
| 210 | M210 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 211 | M211 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 212 | M212 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 213 | M213 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 214 | M214 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 215 | M215 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 216 | M216 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 217 | CC1 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 218 | CC2 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 219 | BB1 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 220 | BB2 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 221 | AA1 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 222 | AA2 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |

Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp top[. | Lcomp bot[... | L-tora... | Kyy | Kzz | Cb | Functi... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | C5X6.7 | 162.241 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 2 | M5 | L4X4X4 | 75.099 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M6 | PL $3 \times 0.38$ | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 4 | M7 | PL $3 \times 0.38$ | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 5 | M8 | PL 9"x $1 / 2^{\prime \prime}$ | 17.006 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 6 | M10 | PL 9'x $1 / 2^{\prime \prime}$ | 17.006 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 7 | M12 | PL 9"x 1/2" | 17.006 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 8 | M13 | L4X4X4 | 75.099 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 9 | M14 | PL $3 \times 0.38$ | 3 |  |  | Lbyv |  |  |  |  |  | Lateral |
| 10 | M15 | PL $3 \times 0.38$ | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 11 | M16 | L4X4X4 | 75.099 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 12 | M17 | PL $3 \times 0.38$ | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 13 | M18 | PL $3 \times 0.38$ | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 14 | M23 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 15 | CC3 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 16 | M25 | PIPE_2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 17 | M29 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 18 | M34 | PIPE_2.0 | 52 |  |  |  |  |  |  |  |  | Latera! |
| 19 | BB3 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 20 | M25B | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 21 | M40 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 22 | M45 | PIPE_2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |

## Hot Rolled Steel Design Parameters (Continued)

|  | Label | Shape | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp top[. | Lcomp bot[.. | L-tora... | Kyy | Kzz | Cb | Functi... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23 | AA3 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 24 | 25A | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 25 | M51 | PIPE 2.0 | 52 |  |  |  |  |  |  |  |  | Lateral |
| 26 | M52 | L2x2x4 | 162.241 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 27 | C4 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 28 | C3 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 29 | C2 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 30 | C1 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 31 | B4 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 32 | B3 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 33 | B2 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 34 | B1 | PIPE_2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 35 | A4 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 36 | A3 | PIPE 2.0 | 72 |  |  | 1 |  |  |  |  |  | Lateral |
| 37 | A2 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 38 | A1 | PIPE 2.0 | 72 |  |  |  |  |  |  |  |  | Lateral |
| 39 | M90 | C5X6.7 | 162.241 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 40 | M91 | L2x2x 4 | 162.241 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 41 | M92A | C5X6.7 | 162.241 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 42 | M93A | L2 $\times 2 \times 4$ | 162.241 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 43 | M94A | HSS4X4X3 | 77.844 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 44 | M95A | HSS4X4X3 | 78.514 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 45 | M96A | HSS4X4X3 | 77.844 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 46 | M97A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 47 | M98A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 48 | M105A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 49 | M106A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 50 | M101 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 51 | M102 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 52 | M103 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 53 | M104A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 54 | M113 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 55 | M114 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 56 | M115 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 57 | M116 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 58 | M125 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 59 | M126 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 60 | M127 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 61 | M128 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 62 | M121A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 63 | M122A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 64 | M123A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 65 | M124A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 66 | M133A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 67 | M134A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 68 | M135A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 69 | M136A | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 70 | M145 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 71 | M146 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 72 | M147 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 73 | M148 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 74 | M157 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 75 | M158 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 76 | M159 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 77 | M160 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 78 | M169 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 79 | M170 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |



## Hot Rolled Steel Design Parameters (Continued)

|  | Label | Shape | Lenathlin] | Lbyylin] | Lbzz[in] | Lcomp top[... | Lcomp botI...L | L-tora... | Kyy | Kzz | Cb | Functi... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | M171 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 81 | M172 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 82 | M181 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 83 | M182 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 84 | M183 | 1/2' | 4 |  |  |  |  |  |  |  |  | Lateral |
| 85 | M184 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 86 | M193 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 87 | M194 | $1 / 2^{\prime \prime}$ | 4 |  |  |  |  |  |  |  |  | Lateral |
| 88 | M195 | $1 / 2^{\prime \prime}$ | 4 |  |  |  |  |  |  |  |  | Lateral |
| 89 | M196 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 90 | M205 | $1 / 2^{\prime \prime}$ | 4 |  |  |  |  |  |  |  | , | Lateral |
| 91 | M206 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 92 | M207 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |
| 93 | M208 | 1/2" | 4 |  |  |  |  |  |  |  |  | Lateral |

## Basic Load Cases

|  | BLC Description | Category | $X$ Gravity | Gravity | Z Gravity | Joint | Point | Distribut. | Area(M... | Surface... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dead | None |  | -1.1 |  |  | 18 |  | 6 |  |
| 2 | Live | None |  |  |  |  |  |  | 6 |  |
| 3 | Wind 0 | None |  | . |  |  | 36 | 198 |  |  |
| 4 | Wind 30 | None |  |  |  |  | 36 | 198 |  |  |
| 5 | Wind 60 | None |  |  |  |  | 36 | 198 |  |  |
| 6 | Wind 90 | None |  | - |  |  | 36 | 198 |  |  |
| 7 | Wind 120 | None |  |  |  |  | 36 | 198 |  |  |
| 8 | Wind 150 | None |  |  |  |  | 36 | 198 |  |  |
| 9 | Ice Load | None |  |  |  |  | 18 | 99 | 6 |  |
| 10 | Ice 0 | None |  |  |  |  | 36 | 198 |  |  |
| 11 | Ice 30 | None |  |  |  |  | 36 | 198 |  |  |
| 12 | Ice 60 | None |  |  |  |  | 36 | 198 |  |  |
| 13 | Ice 90 | None |  |  |  |  | 36 | 198 |  |  |
| 14 | Ice 120 | None |  |  |  |  | 36 | 198 |  |  |
| 15 | Ice 150 | None |  |  |  |  | 36 | 198 |  |  |
| 16 | Lm | None |  |  |  | 1 |  |  |  |  |
| 17 | Lv | None |  |  |  | 1 |  |  |  |  |
| 18 | BLC 1 Transient Area Loads | None |  |  |  |  |  | 69 |  |  |
| 19 | BLC 2 Transient Area Loads | None |  |  |  |  |  | 69 |  |  |
| 20 | BLC 9 Transient Area Loads | None |  |  |  |  |  | 69 |  |  |

## Load Combinations

|  | Description | So..P... | S... BLC | Fac.. | BLC | Fac., | BLCF | ac.. | BLCF | Fac.. | BLCF | Fac.. | BLCF | Fac. | BLCF | Fac.. |  |  |  |  |  | Fac... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.4 D | Yes Y | 1 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | $1.2 \mathrm{D}+1.6 \mathrm{~L}$ | Yes Y | 1 | 1.2 | 2 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | 1.2D + 1.6 Wo @ 0 | Yes $Y$ | 1 | 1.2 | 3 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | $1.2 \mathrm{D}+1.6 \mathrm{Wo}$ @ 30 | Yes Y | 1 | 1.2 | 4 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | 1.2D+1.6Wo @ 60 | Yes, Y | 1 | 1.2 | 5 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | $1.2 \mathrm{D}+1.6 \mathrm{Wo}$ @ 90 | Yes Y | 1 | 1.2 | 6 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | $1.2 \mathrm{D}+1.6$ Wo @ 1... | Yes Y | 1 | 1.2 | 7 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | $1.2 \mathrm{D}+1.6 \mathrm{Wo}$ @ 1... | Yes Y | 1 | 1.2 | 8 | 1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | 1.2 D +1.6 Wo @ 1... | Yes Y | 1 | 1.2 | 3 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 1.2 D + 1.6 Wo @ 2... | Yes Y | 1 | 1.2 | 4 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | $1.2 \mathrm{D}+1.6 \mathrm{Wo}$ @ 2... | Yes Y | 1 | 1.2 | 5 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 1.2 D + 1.6 Wo @ 2... | Yes $Y$ | 1 | 1.2 | 6 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.2D+1.6 Wo @ 3... | Yes Y | 1 | 1.2 | 7 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 | $1.2 \mathrm{D}+1.6 \mathrm{Wo}$ @ 3... | Yes Y | 1 | 1.2 | 8 | -1.6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



## Load Combinations (Continued)

Description So..P... S...BLCFac., BLCFac.. BLCFFac...BLCFac...BLCFac..BLCFac., BLCFac..BLCFac.. BLCFac.. BLCFac..


Envelope Joint Reactions

| Joint |  |  | X [lb] |  |  | Z [16] |  |  | MX [k-ft] |  |  |  |  | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N200A | max | 5905.192 | 12 | 3389.032 | 18 | 730.046 | 3 | 0 | 39 | 1.929 | 9 | 19.528 |  |
| 2 |  | min | -5221.664 | 6 | -345.632 | 12 | -777.82 | 9 | 0 | 1 | -1.839 | 3 | -2.35 | 12 |
| 3 | N202 | max | 2487.555 | 14 | 3388.89 | 26 | 4490.578 | 14 | 17.138 | 26 | 1.919 | 5 | 1.16 | 8 |
| 4 |  | min | -2837.611 | 8 | -339.698 | 8 | -5091.615 | 8 | -2.028 | 8 | -1.829 | 11 | -9.782 | 26 |
| 5 | N204 | max | 2719.461 | 10 | 3389.661 | 22 | 5129.394 | 4 | 2.016 | 4 | 1.871 | 13 | 1.164 | 4 |
| 6 |  | min | -3064.005 | 4 | -341.847 | 4 | -4542.684 | 10 | -16.912 | 22 | -1.806 | 3 | -9.764 | 22 |
| 7 | Totals: | max | 8471.266 | 12 | 8844.35 | 18 | 8179.707 | 3 |  |  |  |  |  |  |
| 8 |  | min | -8471.752 | 6 | 3014.807 | 12 | -8179.873 | 9 |  |  |  |  |  |  |

Envelope AISC 14th(360-10): LRFD Steel Code Checks

|  | Member | Shape | Code Ch |  | LC | Shear Check | Loc[in] |  | phi*Pn, | phitPn..p | phi'M... | phi*M... | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | C5X6.7 | 2.093 | 13... | 6 | 6.103 | 13.52 | z 6 | 4033... | 63828 | 1.604 | 9.585 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 2 | M92A | C5X6.7 | 2.087 | 13... | 10 | 6.068 | 13.52 | z 10 | 4033... | 63828 | 1.604 | 9.585 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 3 | M90 | C5X6.7 | 2.062 | 13.... | 14 | 6.010 | 13.52 | z 14 | 4033.... | 63828 | 1.604 | 9.585 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 4 | M93A | L2x2x4 | 1.881 | 104.. | 10 | . 098 | 150.41 | z 11 | 1213... | 30585.6 | . 691 | 1.286 | 1. $\mathrm{H} 2-1$ |
| 5 | M52 | $L 2 \times 2 \times 4$ | 1.871 | 104.. | 6 | . 099 | 150.41 | z 7 | 1213.... | 30585.6 | . 691 | 1.283 | 1. $\mathrm{H} 2-1$ |
| 6 | M91 | L2x2x4 | 1.845 | 104.. | 14 | 097 | 150.41 | z 3 | 1213... | 30585.6 | 691 | 1.285 | 1. $\mathrm{H} 2-1$ |
| 7 | M12 | PL 9" $\times 1$. | 1.714 | 8.5... | 10 | 3.286 | 8.503 | y 7 | 68915.. | 145800 | 1.519 | 27.338 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 8 | M8 | PL9" $\times 1$. | 1.710 | 8.5... | 6 | 3.278 | 8.503 | y 3 | 68915.. | 145800 | 1.519 | 27.338 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 9 | M10 | PL 9" $\times 1 .$. | 1.709 | 8.5... | 14 | 3.311 | 8.503 | $\mathrm{v}^{11}$ | 68915.. | 145800 | 1.519 | 27.338 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 10 | M95A | HSS4X4... | 1.591 | 78.... | 25 | 115 | 78.514 | z 26 | 89908.. | 106812 | 12.662 | 12.662 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 11 | M94A | HSS4X4... | 1.577 | 77.... | 17 | . 115 | 77.844 | z 18 | 90171.. | 106812 | 12.662 | 12.662 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 12 | M96A | HSS4X4... | 1.576 | 77... | 21 | . 115 | 77.844 | z 22 | 90171.. | 106812 | 12.662 | 12.662 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 13 | M23 | PIPE_2.0 | 1.574 | 45.5 | 6 | . 659 | 45.5 | 6 | 25652.. | 32130 | 1.872 | 1.872 | 1.. H3-6 |
| 14 | M45 | PIPE_2.0 | 1.570 | 45.5 | 10 | . 661 | 45.5 |  | 25652. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 3-6$ |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

|  | Member | Shape | Code Che | Loc. | LC | Shear Check | Loc[in] | L. phi*Pn. phi*Pn..phi*M | phit | Eq |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | M34 | PIPE 2.0 | 1.547 | 45.5 | 14 | . 652 | 45.5 | $14 \mid 25652 . .321301 .872$ | 1.872 | 1. $\mathrm{H} 3-6$ |
| 16 | M135A | 1/2' | 1.435 | 4 | 18 | 098 | 0 | 126027...6361.74 . 053 | . 053 | 1.. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 17 | M.183 | 1/2" | 1.434 | 4 | 26 | . 098 | 0 | $126027 \ldots . .6361 .74$, 053 | . 053 | 1. $\mathrm{H} 1 \mathrm{H}-1 \mathrm{~b}$ |
| 18 | M103 | $1 / 2^{\prime \prime}$ | 1.434 | 4 | 22 | . 098 | 0 | $46027 \ldots 6361.74$. 053 | . 053 | 1. $\mathrm{H} 11-1 \mathrm{~b}$ |
| 19 | M184 | 1/2' | 1.330 | 4 | 21 | 104 | 0 | 6 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 20 | M136A | $1 / 2^{\prime \prime}$ | 1.330 | 4 | 25 | 104 | 0 | 106027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 21 | M104A | 1/2" | 1.330 | 4 | 17 | . 105 | 0 | $146027 \ldots 6361.74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 22 | M29 | PIPE 2.0 | 1.318 | 45.5 | 6 | 481 | 45.5 | 6 25652.. 321301.872 | 1.872 | 1. H3-6 |
| 23 | M181. | 1/2" | 1.313 | 4 | 18 | . 098 | 0 | 126027....6361.74 . 053 | . 053 | 1. $\mathrm{H}^{1}-1 \mathrm{~b}$ |
| 24 | M101 | 1/2" | 1.309 | 4 | 26 | . 098 | 0 | $86027 \ldots . .6361 .74 .053$ | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 25 | M133A | 1/2" | 1.309 | 4 | 22 | . 098 | 0 | 4 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 26 | M182 | $1 / 2^{\prime \prime}$ | 1.305 | 4 | 23 | . 104 | 0 | 146027...6361.74. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 27 | M134A | 1/2" | 1.302 | 4 | 15 | 104 | 0 | 6 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 28 | M102 | 1/2" | 1.301 | 4 | 19 | 104 | 0 | $146027 \ldots . .6361 .74 .053$ | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 29 | M51 | PIPE_2.0 | 1.295 | 45.5 | 10 | 466 | 45.5 | 10 25652.. 321301.872 | 1.872 | 1. $\mathrm{H} 3-6$ |
| 30 | M40 | PIPE_2.0 | 1.295 | 45.5 | 14 | 474 | 45.5 | $1425652 . .321301 .872$ | 1.872 | 1. $\mathrm{H} 3-6$ |
| 31 | AA3 | PIPE_2.0 | 1.073 | 45.5 | 5 | 739 | 45.5 | 11 25652.. 321301.872 | 1.872 | 2. $\mathrm{H} 3-6$ |
| 32 | CC3 | PIPE_2.0 | 1.067 | 45.5 | 13 | 741 | 6.5 | 6 25652.. 321301.872 | 1.872 | 2. $\mathrm{H} 3-6$ |
| 33 | BB3 | PIPE_2.0 | 1.056 | 45.5 | 9 | 729 | 45.5 | 3 25652... 321301.872 | 1.872 | 1. H3-6 |
| 34 | M25 | PIPE_2.0 | . 832 | 45.5 | 10 | 350 | 45.5 | $1125652 . .321301 .872$ | 1.872 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 35 | M25B | PIPE_2.0 | . 830 | 45.5 | 6 | . 347 | 45.5 |  | 1.872 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 36 | 25A | PIPE_2.0 | . 826 | 45.5 | 14 | . 352 | 45.5 | 3 25652... 321301.872 | 1.872 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 37 | M193 | $1 / 2^{\prime \prime}$ | 656 | 4 | 5 | . 027 | 0 | 5 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 38 | M113 | $1 / 2^{\prime \prime}$ | . 655 | 4 | 13 | . 027 | 0 | 136027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 39 | M145 | 1/2" | . 650 | 4 | 9 | . 027 | 0 | 9 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 40 | M205 | 1/2" | . 649 | 4 | 5 | . 031 | 0 | 5 6027....6361.74 $\quad 053$ | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 41 | M125 | 1/2" | 645 | 4 | 13 | . 031 | 0 | 136027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 42 | M157 | 1/2" | . 639 | 4 | 9 | 031 | 0 | $96027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 43 | M195 | 1/2" | . 553 | 4 | 5 | . 021 | 4 | 5 6027....6361.74. 053 | . 053 | 1. $\mathrm{H} 1 \mathrm{H}^{\text {- }}$ |
| 44 | M115 | 1/2" | . 553 | 4 | 13 | 021 | 4 | 136027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 45 | M147 | 1/2" | . 544 | 4 | 9 | 021 | 4 | 9 6027...6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 46 | M207 | 1/2" | . 527 | 4 | 5 | . 024 | 4 | 5 6027....6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 47 | M127 | 1/2" | . 527 | 4 | 13 | . 024 | 4 | 136027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 48 | M159 | 1/2" | 521 | 4 | 9 | . 024 | 4 | $96027 \ldots . .6361 .74$. 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 49 | M114 | 1/2" | . 507 | 4 | 5 | . 016 | 4 | 5 6027....6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 50 | M123A | 1/2" | 498 | 4 | 19 | . 027 | 0 | $196027 \ldots . .6361 .74 .053$ | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 51 | M194 | 1/2" | 498 | 4 | 9 | . 016 | 4 | $96027 \ldots . .6361 .74 .053$ | 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 52 | M105A | 1/2" | 498 | 4 | 23 | . 027 | 0 | 236027...6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 53 | M171 | 1/2" | 498 | 4 | 15 | . 027 | 0 | 156027...6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 54 | M146 | $1 / 2^{\prime \prime}$ | 493 | 4 | 13 | . 016 | 4 | 136027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 55 | M116 | 1/2" | 464 | 4 | 5 | . 015 | 0 | 5 6027....6361.74 . 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 56 | M196 | 1/2" | . 458 | 4 | 9 | . 015 | 0 | $96027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 57 | M148 | 1/2" | . 454 | 4 | 13 | . 015 | 0 | 136027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 58 | M97A | 1/2" | . 420 | 4 | 11 | . 021 | 4 | 116027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 59 | M121A | 1/2" | . 417 | 4 | 7 | . 021 | 4 | 7 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 60 | M169 | 1/2" | 412 | 4 | 3 | . 020 | 4 | 3 6027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 61 | M206 | 1/2" | . 383 | 4 | 9 | . 013 | 4 | $56027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 62 | M126 | 1/2" | . 380 | 4 | 5 | . 014 | 4 | ${ }^{13} 66027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 63 | M158 | 1/2" | 379 | 4 | 13 | 013 | 4 | $96027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 64 | M208 | $1 / 2^{\prime \prime}$ | 367 | 4 | 10 | . 017 | 0 | $176027 \ldots . .6361 .74 .053$ | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 65 | M128 | 1/2" | 365 | 4 | 6 | . 017 | 0 | $256027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{a}$ |
| 66 | M160 | $1 / 2^{\prime \prime}$ | 362 | 4 | 14 | 017 | 0 | 216027...6361.74 . 053 | . 053 | 1. H1-1a |
| 67 | M122A | 1/2" | . 320 | 4 | 19 | . 017 | 0 | 196027....6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 68 | M170 | 1/2" | 319 | 4 | 15 | . 017 | 0 | 156027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 69 | M98A | 1/2" | . 319 | 4 | 23 | . 017 | 0 | 23 6027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 70 | M106A | 1/2" | 273 | 4 | 11 | 013 | 4 | 1116027...6361.74 . 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 71 | M124A | 1/2" | 270 | 4 | 7 | . 013 | 4 | $76027 \ldots . .6361 .74$. 053 | . 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |



Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

|  | Member | Shape | Code Che |  | LC | Shear Check | Loclin] |  | ph | phi*Pn.. | phi'M.. |  | Ean |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72 | M172 | 1/2" | 268 | 4 | 3 | . 013 | 4 |  | 36027. | 6361.74 | 053 | 053 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 73 | C2 | PIPE_2.0 | 246 | 32. | 5 | . 092 | 32.25 |  | $520866 .$. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 74 | A2 | PIPE_2.0 | 246 | 32... | 9 | 095 | 32.25 |  | 9 20866.. | 32130 | 1.872 | 1.872 | 2. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 75 | B2 | PIPE_2.0 | 245 | 32. | 13 | . 090 | 32.25 |  | $1320866 .$. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 76 | C3 | PIPE_2.0 | 229 | 32. | 6 | 343 | 32.25 |  | 6 20866... | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 3-6$ |
| 77 | A3 | PIPE_2.0 | 226 | 32. | 10 | . 340 | 32.25 |  | $020866 .$. | 32130 | 1.872 | 1.872 | 1. H3-6 |
| 78 | B3 | PIPE_2.0 | 222 | 32. | 14 | . 336 | 32.25 |  | $420866 .$. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 3-6$ |
| 79 | A4 | PIPE_2.0 | 161 | 32. | 10 | 283 | 32.25 |  | $0.20866 .$. | 32130 | 1.872 | 1.872 | 1. H3-6 |
| 80 | C4 | PIPE_2.0 | .161 | 32. | 6 | . 282 | 32.25 |  | 6 20866.. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 3-6$ |
| 81 | B4 | PIPE_2.0 | . 157 | 32. | 14 | 279 | 32.25 |  | $420866 .$. | 32130 | 1.872 | 1.872 | 1. H3-6 |
| 82 | M18 | PL $3 \times 0 .$. | 125 | 0 | 4 | 849 | 3 | $y 7$ | $735509 .$. | 36936 | . 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 83 | M7 | PL $3 \times 0 \ldots$ | 125 | 0 | 12 | . 848 | 3 | v 9 | $935509 .$. | 36936 | . 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 84 | M17 | PL $3 \times 0 .$. | 125 | 0 | 4 | 849 | 3 | y 7 | $735510 .$. | 36936 | 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 85 | M6 | PL $3 \times 0 \ldots$ | 125 | 0 | 12 | 848 | 3 | $\checkmark 9$ | $935510 .$. | . 36936 | 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 86 | M15 | PL $3 \times 0 . \ldots$ | 124 | 0 | 8 | 854 | 3 | y 5 | $535509 .$. | 36936 | . 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 87 | M14 | PL $3 \times 0 \ldots$ | 124 | 0 | 8 | 854 | 3 | - 5 | 5 35510... | 36936 | 292 | 2.308 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 88 | M16 | L4X4X4 | . 122 | 37.... | 4 | . 536 | 75.099 |  | 7 36658... | 62532 | 3.138 | 5.841 | 1. $\mathrm{H} 2-1$ |
| 89 | M5 | L4X4X4 | . 122 | 37.... | 12 | 535 | 75.099 | z 9 | 9 36658.. | . 62532 | 3.138 | 5.841 | 1. $\mathrm{H} 2-1$ |
| 90 | M13 | L4X4X4 | . 121 | 37.... | 8 | . 539 | 75.099 | z 5 | 5 36658.. | 62532 | 3.138 | 5.841 | 1. $\mathrm{H} 2-1$ |
| 91 | C1 | PIPE_2.0 | . 078 | 32.... | 5 | 199 | 32.25 |  | 6 20866.. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 92 | B1 | PIPE_2.0 | . 077 | 32.... | 13 | 196 | 32.25 |  | $420866 .$. | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 93 | A1 | PIPE_2.0 | . 076 | 32.... | 9 | 191 | 32.25 |  | 0,20866... | 32130 | 1.872 | 1.872 | 1. $\mathrm{H} 1 \mathrm{H} 1-1 \mathrm{~b}$ |


$\begin{array}{rrl}\text { REACTIONS } & \\ \text { Px }= & 0.777 & \text { Kip } \\ \mathrm{Py}= & 3.389 & \mathrm{Kip} \\ \text { (Axial) } \mathrm{Pz}= & 5.905 & \text { Kip } \\ \mathrm{Mx}= & 234.33 & \text { Kip-in } \\ \mathrm{My}= & 23.148 & \text { Kip-in } \\ \text { (Torque) } \mathrm{Mz}= & 0 & \text { Kip-in } \\ \mathrm{Number} \text { of Bolts }\end{array}$
$=$
$\begin{array}{cl}\mathbf{4} & \\ \mathbf{8 . 5} & \text { in } \\ \mathbf{8 . 5} & \text { in } \\ \mathbf{1 . 2 5} & \text { in } \\ 4.25 & \text { in } \\ 4.25 & \text { in } \\ 0 & \text { in } \\ 0 & \text { in } \\ 234.33 & \text { Kips-in } \\ 23.148 & \text { Kips-in } \\ 0 & \text { Kips-in }\end{array}$

> BOLT CHECKS
> $\begin{aligned} & \text { Total Moment including load eccentricity } \Sigma \mathrm{Mx}= \\ & \text { Total Moment including load eccentricity } \Sigma \mathrm{My}=\end{aligned}$ Total Moment including load eccentricity $\Sigma \mathrm{Mz}=$

Load eccentricity in $x$-direction, ex | Tension Reaction | 22.93 | kip |
| :--- | :---: | :--- |
| Shear Reaction | 0.87 | kip |
| Bolt Type | A325N |  |
| Bolt Diameter | 0.625 | in |
| Tensile Strength | 20.7 | kips |
| Shear Strength | 12.4 | kips |
| Reduced Tensile Strength | - | kips | $\begin{array}{lcl}\text { Tension Reaction } & 22.93 & \text { kip } \\ \text { Shear Reaction } & 0.87 & \text { kip } \\ \text { Bolt Type } & \text { A325N } & \\ \text { Bolt Diameter } & 0.625 & \text { in } \\ \text { Tensile Strength } & 20.7 & \text { kip } \\ \text { Shear Strength } & 12.4 & \text { kip } \\ \text { Reduced Tensile Strength } & - & \text { kip }\end{array}$ $\begin{array}{lcl}\text { Tension Reaction } & 22.93 & \text { kip } \\ \text { Shear Reaction } & 0.87 & \text { kip } \\ \text { Bolt Type } & \text { A325N } & \\ \text { Bolt Diameter } & 0.625 & \text { in } \\ \text { Tensile Strength } & 20.7 & \text { kip } \\ \text { Shear Strength } & 12.4 & \text { kip } \\ \text { Reduced Tensile Strength } & - & \text { kip }\end{array}$ $\begin{array}{lcl}\text { Tension Reaction } & 22.93 & \text { kip } \\ \text { Shear Reaction } & 0.87 & \text { kip } \\ \text { Bolt Type } & \text { A325N } & \\ \text { Bolt Diameter } & 0.625 & \text { in } \\ \text { Tensile Strength } & 20.7 & \text { kip } \\ \text { Shear Strength } & 12.4 & \text { kip } \\ \text { Reduced Tensile Strength } & - & \text { kip }\end{array}$ $\begin{array}{lcl}\text { Tension Reaction } & 22.93 & \text { kip } \\ \text { Shear Reaction } & 0.87 & \text { kip } \\ \text { Bolt Type } & \text { A325N } & \\ \text { Bolt Diameter } & 0.625 & \text { in } \\ \text { Tensile Strength } & 20.7 & \text { kip } \\ \text { Shear Strength } & 12.4 & \text { kip } \\ \text { Reduced Tensile Strength } & - & \text { kip }\end{array}$ Tenșile Capacity Used Shear Capacity Used


[^0]:    | Tensile Capacity Used | $24.2 \%$ | Note: Tension reduction not required if tension or shear capacity $<\mathbf{3 0 \%}$ |
    | :--- | :--- | :--- |
    |  |  |  |

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[^2]:    Seismic Base Shear is Less Than 50\% of Wind Force - An Analysis is NOT Required

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