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Hartford, CT 06103-3597
Main (860) 275-8200
Fax (860) 275-8299
kbaldwin@rc.com
Direct (860) 275-8345

Also admitted in Massachusetts

July 24, 2014

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re: **Notice of Exempt Modification – Facility Modification
144 Old Boston Post Road, Danbury, Connecticut**

Dear Ms. Bachman:

Cellco Partnership d/b/a Verizon Wireless (“Cellco”) currently maintains ten (10) wireless telecommunications antennas at the top of the existing 65-foot tower at 144 Old Boston Post Road in Danbury, Connecticut (the “Property”). The tower and Property are owned by AT&T. The Council approved Cellco’s use of this tower in 2000. Cellco now intends to modify its facility by replacing four (4) of existing antennas with two (2) BXA-171063-12BF, 1900 MHz antennas and two (2) model BXA-171063-12BF, 2100 MHz antennas, all at the same level on the tower. Cellco also intends to install two (2) remote radio heads (“RRHs”) behind its 2100 MHz antennas and one (1) HYBRIFLEX™ antenna cable. Included in Attachment 1 are specifications for Cellco’s replacement antennas, RRHs and HYBRIFLEX™ cable.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Mark D. Boughton, Mayor for the City of Danbury.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

13046502-v1

Robinson+Cole

Melanie A. Bachman

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1. The proposed modifications will not result in an increase in the height of the existing tower. Cellco's new antennas and RRHs will be installed at the top of the existing 65-foot tower.

2. The proposed modifications will not involve any change to ground-mounted equipment and, therefore, will not require the extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the replacement antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) safety standard. Far Field Approximation tables for each of Cellco's operating frequencies are included behind Attachment 2. The Far Field calculations demonstrate that Cellco's modified facility will operate well within the RF emissions safety limits established by the FCC.

5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.

6. The tower and its foundation can support Cellco's proposed modifications. (See Structural Analysis included in Attachment 3).

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Kenneth C. Baldwin

Enclosures

Copy to:

Mark D. Boughton, Danbury Mayor
Sandy M. Carter

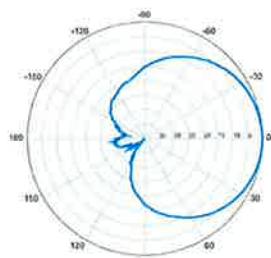
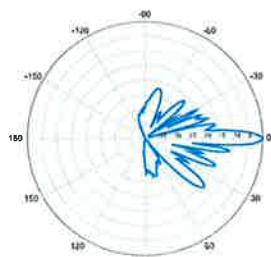
ATTACHMENT 1

BXA-171063-12BF-EDIN-X

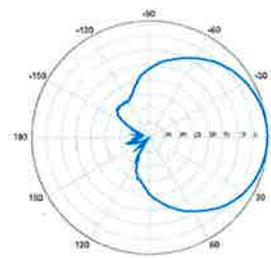
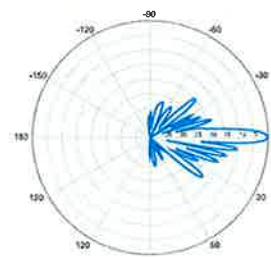
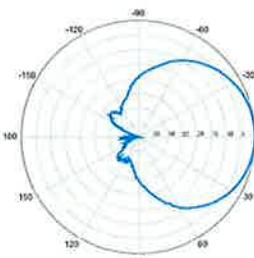
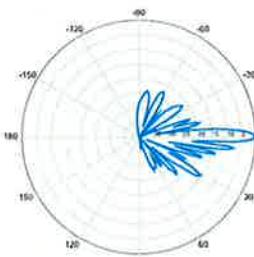
Replace "X" with desired electrical downtilt

X-Pol | FET Panel | 63° | 19.0 dBi

Electrical Characteristics		1710-2170 MHz		
Frequency bands	1710-1880 MHz	1850-1990 MHz	1920-2170 MHz	
Polarization	±45°	±45°	±45°	
Horizontal beamwidth	68°	65°	60°	
Vertical beamwidth	4.5°	4.5°	4.5°	
Gain	16.1 dBd / 18.2 dBi	16.5 dBd / 18.6 dBi	16.9 dBd / 19.0 dBi	
Electrical downtilt (X)		0, 2, 4, 5		
Impedance		50Ω		
VSWR		≤1.5:1		
First upper sidelobe		< -17 dB		
Front-to-back ratio		> 30 dB		
In-band isolation		< -25 dB		
IM3 (20W carrier)		< -150 dBc		
Input power		300 W		
Lightning protection		Direct Ground		
Connector(s)		2 Ports / EDIN / Female / Bottom		
Operating temperature		-40° to +60° C / -40° to +140° F		
Mechanical Characteristics				
Dimensions Length x Width x Depth		1842 x 154 x 105 mm	72.5 x 6.1 x 4.1 in	
Depth with z-brackets		133 mm	5.2 in	
Weight without mounting brackets		5.8 kg	12.8 lbs	
Survival wind speed		> 201 km/hr	> 125 mph	
Wind area	Front: 0.28 m ² Wind load @ 161 km/hr (100 mph)	Side: 0.19 m ² Front: 460 N Side: 304 N	Front: 3.1 ft ² Side: 2.1 ft ² Front: 103 lbf Side: 68 lbf	
Mounting Options		Part Number	Fits Pipe Diameter	Weight
2-Point Mounting Bracket Kit	26799997	50-102 mm	2.0-4.0 in	2.3 kg 5 lbs
2-Point Mounting & Downtilt Bracket Kit	26799999	50-102 mm	2.0-4.0 in	3.6 kg 8 lbs
Concealment Configurations	For concealment configurations, order BXA-171063-12BF-EDIN-X-FP			

**BXA-171063-12BF-EDIN-X**Horizontal | 1710-1880 MHz
BXA-171063-12BF-EDIN-0

0° | Vertical | 1710-1880 MHz

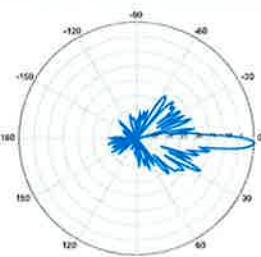
BXA-171063-12BF-EDIN-XHorizontal | 1850-1990 MHz
BXA-171063-12BF-EDIN-0**BXA-171063-12BF-EDIN-X**Horizontal | 1920-2170 MHz
BXA-171063-12BF-EDIN-0

0° | Vertical | 1920-2170 MHz

Quoted performance parameters are provided to offer typical or range values only and may vary as a result of normal manufacturing and operational conditions. Extreme operational conditions and/or stress on structural supports is beyond our control. Such conditions may result in damage to this product. Improvements to product may be made without notice.

BXA-171063-12BF-EDIN-X

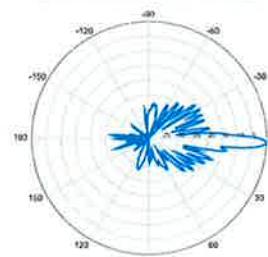
X-Pol | FET Panel | 63° | 19.0 dBi

BXA-171063-12BF-EDIN-2

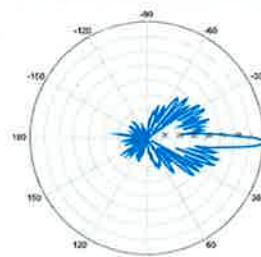
2° | Vertical | 1710-1880 MHz

BXA-171063-12BF-EDIN-4

2° | Vertical | 1850-1990 MHz

BXA-171063-12BF-EDIN-2

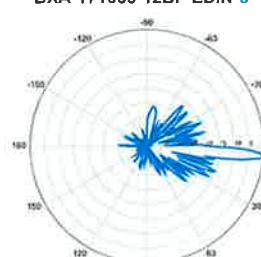
2° | Vertical | 1920-2170 MHz

BXA-171063-12BF-EDIN-2

4° | Vertical | 1710-1880 MHz

BXA-171063-12BF-EDIN-4

4° | Vertical | 1850-1990 MHz

BXA-171063-12BF-EDIN-5

4° | Vertical | 1920-2170 MHz

4° | Vertical | 1710-1880 MHz

BXA-171063-12BF-EDIN-5

5° | Vertical | 1850-1990 MHz

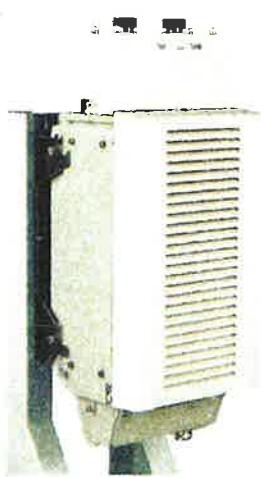
BXA-171063-12BF-EDIN-5

5° | Vertical | 1920-2170 MHz

Quoted performance parameters are provided to offer typical or range values only and may vary as a result of normal manufacturing and operational conditions. Extreme operational conditions and/or stress on structural supports is beyond our control. Such conditions may result in damage to this product. Improvements to product may be made without notice.

Alcatel-Lucent RRH2x40-AWS REMOTE RADIO HEAD

The Alcatel-Lucent RRH2x40-AWS is a high-power, small form-factor Remote Radio Head (RRH) operating in the AWS frequency band (1700/2100MHz - 3GPP Band 4). The Alcatel-Lucent RRH2x40-AWS is designed with an eco-efficient approach, providing operators with the means to achieve high quality and capacity coverage with minimum site requirements.



A distributed eNodeB expands deployment options by using two components, a Base Band Unit (BBU) containing the digital assets and a separate RRH containing the radio-frequency (RF) elements. This modular design optimizes available space and allows the main components of an eNodeB to be installed separately, within the same site or several kilometres apart.

The Alcatel-Lucent RRH2x40-AWS is linked to the BBU by an optical-fiber connection carrying downlink and uplink digital radio signals along with operations, administration and maintenance (OA&M) information. The Alcatel-Lucent RRH2x40-AWS has two transmit RF paths, 40 W RF output power per transmit path, and is designed to manage up to four-way receive diversity. The device is ideally suited to support macro coverage, with multiple-input multiple-output (MIMO) 2x2 operation in up to 20 MHz of bandwidth.

The Alcatel-Lucent RRH2x40-AWS is designed to make available all the benefits of a distributed eNodeB, with excellent RF characteristics, with low

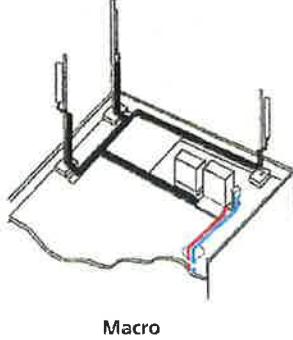
capital expenditures (CAPEX) and low operating expenditures (OPEX). The limited space available in some sites may prevent the installation of traditional single-cabinet BTS equipment or require costly cranes to be employed, leaving coverage holes. However, many of these sites can host an Alcatel-Lucent RRH2x40-AWS installation, providing more flexible site selection and improved network quality along with greatly reduced installation time and costs.

Fast, low-cost installation and deployment

The Alcatel-Lucent RRH2x40-AWS is a zero-footprint solution and operates noise-free, simplifying negotiations with site property owners and minimizing environmental impacts. Installation can easily be done by a single person because the Alcatel-Lucent RRH2x40-AWS is compact and weighs less than 20 kg (44 lb), eliminating the need for a crane to hoist the BTS cabinet to the rooftop. A site can be in operation in less than one day — a fraction of the time required for a traditional BTS.

Excellent RF performance

Because of its small size and weight, the Alcatel-Lucent RRH2x40-AWS can be installed close to the antenna. Operators can therefore locate the Alcatel-Lucent RRH2x40-AWS where RF engineering is deemed ideal, minimizing trade-offs between available sites and RF optimum sites. The RF feeder cost and installation costs are reduced or eliminated, and there is no need for a Tower Mounted Amplifier (TMA) because losses introduced by the RF feeder are greatly reduced. The Alcatel-Lucent RRH2x40-AWS provides more RF power while at the same time consuming less electricity.



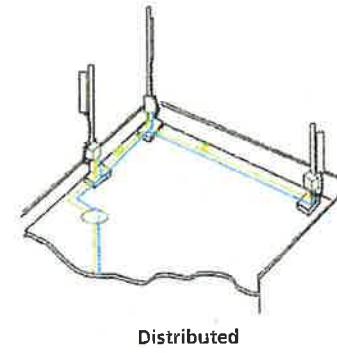
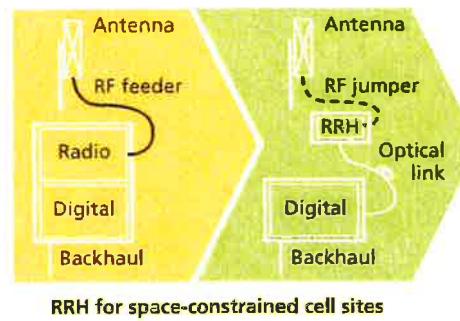
Macro

Features

- Zero-footprint deployment
- Easy installation, with a lightweight unit can be carried and set up by one person
- Optimized RF power, with flexible site selection and elimination of a TMA
- Convection-cooled (fanless)
- Noise-free
- Best-in-class power efficiency, with significantly reduced energy consumption

Benefits

- Leverages existing real estate with lower site costs
- Reduces installation costs, with fewer installation materials and simplified logistics
- Decreases power costs and minimizes environmental impacts, with the potential for eco-sustainable power options
- Improves RF performance and adds flexibility to network planning



Distributed

Technical specifications

Physical dimensions

- Height: 620 mm (24.4 in.)
- Width: 270 mm (10.63 in.)
- Depth: 170m (6.7 in.)
- Weight (without mounting kit): less than 20 kg (44 lb)

Power

- Power supply: -48VDC

Operating environment

- Outdoor temperature range:
 - With solar load: -40°C to +50°C (-40°F to +122°F)
 - Without solar load: -40°C to +55°C (-40°F to +131°F)
- Rx diversity: 2-way or 4-way with optional Rx Diversity module
- Noise figure: below 2.0 dB typical
- Antenna Line Device features
 - TMA and Remote electrical tilt (RET) support via AISG v2.0

- Passive convection cooling (no fans)
- Enclosure protection
 - IP65 (International Protection rating)

RF characteristics

- Frequency band: 1700/2100 MHz (AWS); 3GPP Band 4
- Bandwidth: up to 20 MHz
- RF output power at antenna port: 40 W nominal RF power for each Tx port
- Rx diversity: 2-way or 4-way with optional Rx Diversity module
- Noise figure: below 2.0 dB typical
- Antenna Line Device features
 - TMA and Remote electrical tilt (RET) support via AISG v2.0

Optical characteristics

Type/number of fibers

- Single-mode variant
 - One Single Mode Single Fiber per RRH2x, carrying UL and DL using CWDM
 - Single mode dual fiber (SM/DF)
- Multi-mode variant
 - Two Multi-mode fibers per RRH2x: one carrying UL, the other carrying DL

Optical fiber length

- Up to 500 m (0.31 mi), using MM fiber
- Up to 20 km (12.43 mi), using SM fiber

Digital Ports and Alarms

- Two optical ports to support daisy-chaining
- Six external alarms

Product Data Sheet HB158-1-08UB-S8J18



HYBRIFLEX™ RRH Hybrid Feeder Cabling Solution, 1-5/8", Single-Mode Fiber

Product Description

RFS' HYBRIFLEX Remote Radio Head (RRH) hybrid feeder cabling solution combines optical fiber and DC power for RRHs in a single lightweight aluminum corrugated cable, making it the world's most innovative solution for RRH deployments.

It was developed to reduce installation complexity and costs at Cellular sites. HYBRIFLEX allows mobile operators deploying an RRH architecture to standardize the RRH installation process and eliminate the need for and cost of cable grounding. HYBRIFLEX combines optical fiber (multi-mode or single-mode) and power in a single corrugated cable. It eliminates the need for junction boxes and can connect multiple RRHs with a single feeder. Standard RFS CELLFLEX® accessories can be used with HYBRIFLEX cable. Both pre-connectorized and on-site options are available.

Features/Benefits

- » Aluminum corrugated armor with outstanding bending characteristics – minimizes installation time and enables mechanical protection and shielding
- » Same accessories as 1 5/8" coaxial cable
- » Outer conductor grounding – Eliminates typical grounding requirements and saves on installation costs
- » Lightweight solution and compact design – Decreases tower loading
- » Robust cabling – Eliminates need for expensive cable trays and ducts
- » Installation of tight bundled fiber optic cable pairs directly to the RRH – Reduces CAPEX and wind load by eliminating need for interconnection
- » Optical fiber and power cables housed in single corrugated cable – Saves CAPEX by standardizing RRH cable installation and reducing installation requirements
- » Outdoor polyethylene jacket – Ensures long-lasting cable protection

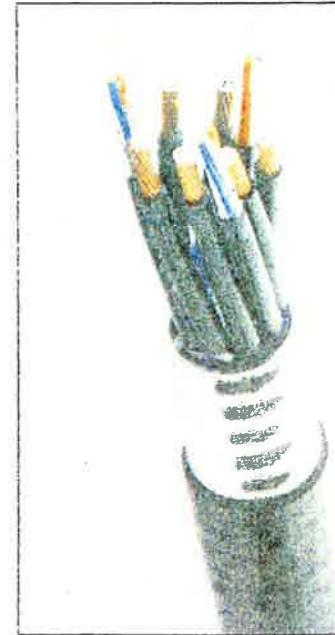


Figure 1: HYBRIFLEX Series

Technical Specifications

Outer Conductor Armor	Corrugated Aluminum	[mm (in)]	46.5 (1.83)
Jacket	Polyethylene, PE	[mm (in)]	50.3 (1.98)
UV-Protection	Individual and External Jacket		Yes
Weight, Approximate	[kg/m (lb/ft)]	1.9 (1.30)	
Minimum Bending Radius, Single Bending	[mm (in)]	200 (8)	
Minimum Bending Radius, Repeated Bending	[mm (in)]	500 (20)	
Recommended/Maximum Clamp Spacing	[m (ft)]	1.0 / 1.2 (3.25 / 4.0)	
Electrical Properties			
DC-Resistance Outer Conductor Armor	[Ω/km (Ω/1000ft)]	0.68 (0.205)	
DC-Resistance Power Cable, 8 mm² (8AWG)	[Ω/km (Ω/1000ft)]	2.1 (0.307)	
Optical Properties			
Version		Single-mode OM3	
Quantity, Fiber Count		16 (8 pairs)	
Core/Clad	[μm]	50/125	
Primary Coating (Acrylate)	[μm]	245	
Buffer Diameter, Nominal	[μm]	900	
Secondary Protection, Jacket, Nominal	[mm (in)]	2.0 (0.08)	
Minimum Bending Radius	[mm (in)]	104 (4.1)	
Insertion Loss @ wavelength 850nm	[dB/km]	3.0	
Insertion Loss @ wavelength 1310nm	[dB/km]	1.0	
Standards (Meets or exceeds)		UL34-V0, UL1666 RoHS Compliant	
Power Properties			
Size (Power)	[mm (AWG)]	8.4 (8)	
Quantity, Wire Count (Power)		16 (8 pairs)	
Size (Alarm)	[mm (AWG)]	0.8 (18)	
Quantity, Wire Count (Alarm)		4 (2 pairs)	
Type		UV protected	
Strands		19	
Primary Jacket Diameter, Nominal	[mm (in)]	6.8 (0.27)	
Standards (Meets or exceeds)		NFPA 130, IEC 60332-2-19 UL Type X-HHV-2, UL 44 UL-L5 Limited Smoke, UL VW-1 IEEE-383 (1974), IEEE1202/FT4 RoHS Compliant	
Environmental Properties			
Installation Temperature	[°C (°F)]	-40 to +65 (-40 to 149)	
Operation Temperature	[°C (°F)]	-40 to +65 (-40 to 149)	

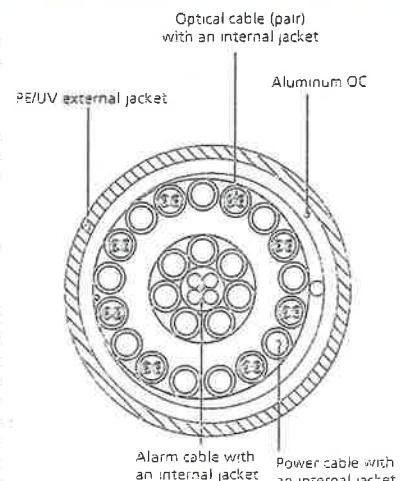


Figure 2: Construction Detail

ATTACHMENT 2

Far Field Approximation
with downtilt variation

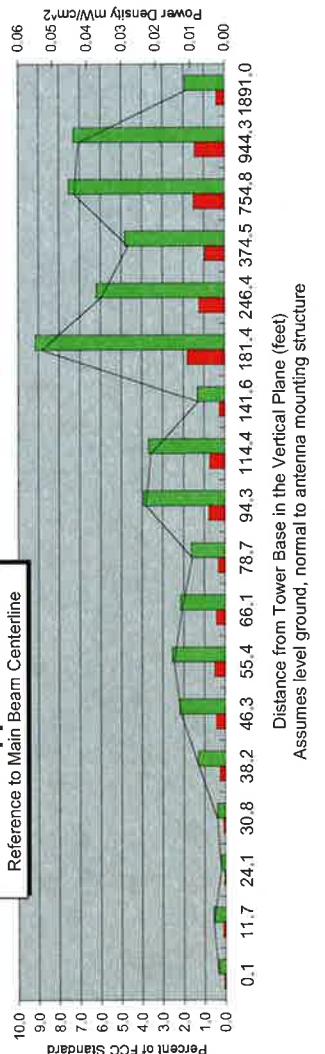
Estimated Radiated Emission

Single Emitter Far Field Model Dipole / Wire/ Yagi Antenna Types

Location:	Danbury South, CT
Site #:	5-0169
Date:	07/15/14
Name:	Ryan Ulanday
File Name:	Danbury South, CT - FF Power
Operating Freq. (MHz)	869.0
Antenna Height (ft):	69.0
Antenna Gain (dB):	16.7
Antenna Size (in.):	72.0
Downtilt (degrees):	0.0
Feedline Loss (dB):	0.0
Power @ J4 (w):	3915.0

Far Field Approximation

Reference to Main Beam Centerline



This approximation is only valid in the far field, which begins at: **64.4 Feet**

Enter Main Beam
Distance in feet below:

Calc Angle	90.0	80.0	70.0	65.0	60.0	55.0	50.0	45.0	40.0	35.0	30.0	25.0	20.0	15.0	10.0	5.0	4.0	2.0
Solve for r_dx to antenna	66.0	67.0	70.3	72.8	76.2	80.6	86.2	93.4	102.7	115.1	132.1	156.2	193.1	255.1	380.3	757.6	946.6	1892.1
Distance from Antenna Structure Base in Horizontal plane	0.1	11.7	24.1	30.8	38.2	46.3	55.4	66.1	78.7	94.3	114.4	141.6	181.4	246.4	374.5	754.8	944.3	1891.0
Angle from Main Beam (reference to horizontal plane)	90	80	70	65	60	55	50	45	40	35	30	25	20	15	10	5	4	0
dB down from centerline (referenced to centerline)	36.76	34.35	38.52	35.34	29.54	26.8	25.59	25.63	25.99	21.21	20.29	23.24	13.03	12.3	9.92	2	0.2	0
Reflection Coefficient (1 to 4.2.56 typical)	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56
Power Density (mW/cm^2)	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.01	0.05	0.04	0.03	0.04	0.04	#NUM!
Percent of Occupational Standard	0.1	0.1	0.0	0.1	0.3	0.4	0.5	0.4	0.3	0.8	0.7	0.3	1.8	1.2	1.0	1.5	1.5	#NUM!
Percent of General Population Standard	0.3	0.6	0.2	0.4	1.3	2.2	2.5	2.2	1.6	3.9	3.7	1.3	9.2	6.2	4.8	7.5	7.3	#NUM!
Antenna Type	DB846F65ZAXY																	
Max%	9.15%																	

Instructions:

- Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to be saved as.
- References to J4 refer to a point where the transmission line exits the equipment shelter and proceeds to the antenna(s). There is typically a connector located here where power measurements are made.
- Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dB, and 2.17 to dB to obtain dB), Antenna Size (vertical size in inches), Downtilt (in Degrees, enter zero if none), Feedline loss from J4 to Antenna, and J4 P.
- From manufacturer's plots, or data sheet, input Angle from mainbeam and dB below mainbeam centerline.
- Enter Reflection coefficient (2.56 would be typical, 1 for free space)
- Spreadsheets calculates actual power density, then relates to Occupational or General Population percentage of FCC Standard.
- An odd distance may be entered in the rightmost column of the lower table.

Far Field Approximation
with downtilt variation

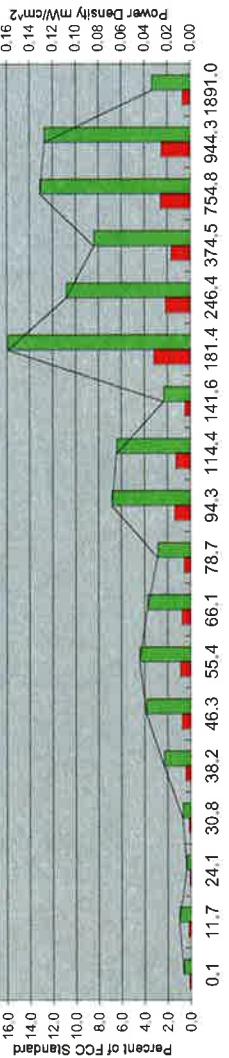
Estimated Radiated Emission

Single Emitter Far Field Model

Dipole / Wire / Yagi Antenna Types

Location:	Danbury South, CT
Site #:	5-0169
Date:	07/15/14
Name:	Ryan Ulanday
File Name:	Danbury South, CT - FF Power
Operating Freq. (MHz)	1971.0
Antenna Height (ft):	69.0
Antenna Gain (dBi):	18.7
Antenna Size (in.):	72.4
Downtilt (degrees):	0.0
Feedline Loss (dB):	0.0
Power @ J4 (w):	7440.0

Far Field Approximation



This approximation is only valid in the far field, which begins at: 65.2 Feet

**Enter Main Beam
Distance in feet below:**

Calc Angle	90.0	80.0	70.0	65.0	60.0	55.0	50.0	45.0	40.0	35.0	30.0	25.0	20.0	15.0	10.0	5.0	4.0	2.0	
Solve for r_dx to antenna	66.0	67.0	70.3	72.8	76.2	80.6	86.2	93.4	102.7	115.1	132.1	156.2	193.1	255.1	380.3	757.6	946.6	1892.1	
Distance from Antenna Structure Base in Horizontal plane	0.1	11.7	24.1	30.8	38.2	46.3	55.4	66.1	78.7	94.3	114.4	141.6	181.4	246.4	374.5	754.8	944.3	1891.0	#NUM!
Angle from Main Beam (reference to horizontal plane)	90	80	70	65	60	55	50	45	40	35	30	25	20	15	10	5	4	2	0
dB down from centerline (referenced to centerline)	35.76	34.35	33.52	35.34	29.54	26.8	25.59	25.63	25.99	21.21	20.29	23.24	13.03	12.3	9.92	2	0.2	0	0
Reflection Coefficient (1 to 4.256 typical)	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56
Power Density (mW/cm²)	0.01	0.01	0.01	0.01	0.02	0.04	0.04	0.04	0.04	0.03	0.07	0.06	0.02	0.16	0.11	0.08	0.13	0.03	#NUM!
Percent of Occupational Standard	0.1	0.2	0.1	0.5	0.8	0.9	0.7	0.6	1.4	1.3	0.5	3.2	2.2	1.7	2.6	2.5	0.7	#NUM!	#NUM!
Percent of General Population Standard	0.6	1.0	0.3	0.7	2.3	3.8	4.4	3.7	2.8	6.8	6.4	2.3	15.9	10.8	8.4	13.1	12.7	3.3	#NUM!

Antenna Type: BX4-171063-12CF
Max%: 15.91%

Instructions:

- 1) Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to be saved as.
- 2) References to J4 refer to a point where the transmission line exits the equipment shelter and proceeds to the antenna(s). There is typically a connector located here where power measurements are made.
- 3) Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dB, add 2.17 to dBd to obtain dB), Antenna Size (vertical size in inches), Downtilt (in Degrees, enter zero if none), Feedline loss from J4 to Antenna, and J4 Port.
- 4) From manufacturer's plots, or data sheet, input Angle from mainbeam and dB below mainbeam centerline.
- 5) Enter Reflection coefficient (2.56 would be typical, 1 for free space)
- 6) Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
- 7) An odd distance may be entered in the rightmost column of the lower table.

Far Field Approximation
with downtilt variation

Estimated Radiated Emission

Single Emitter Far Field Model

Dipole / Wire / Yagi Antenna Types

Location:	Danbury South, CT
Site #:	5-0169
Date:	07/15/14
Name:	Ryan Ulanday
File Name:	Danbury South, CT - FF Power
Operating Freq (MHz):	746.0
Antenna Height (ft):	69.0
Antenna Gain (dBi):	16.7
Antenna Size (in.):	71.0
Downtilt (degrees):	0.0
Feedline Loss (dB):	0.0
Power @ J4 (w):	892.0

Far Field Approximation

Reference to Main Beam Centerline

0.01

0.01

0.01

0.01

0.01

0.01

0.01

0.01

0.01

0.01

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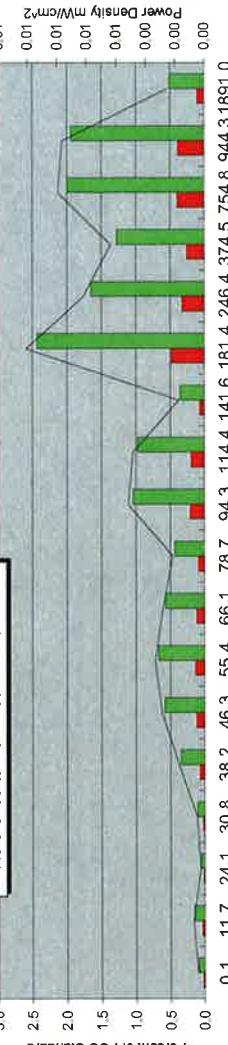
0.01

0.01

0.01

0.01

0.01



Distance from Tower Base in the Vertical Plane (feet)
Assumes level ground, normal to antenna mounting structure

% Occupational % General Public —— Power Density

This approximation is only valid in the far field, which begins at: 62.6 Feet

Enter Main Beam
Distance in feet below:

Calc Angle	90.0	80.0	70.0	65.0	60.0	55.0	50.0	45.0	40.0	35.0	30.0	25.0	20.0	15.0	10.0	5.0	4.0	2.0
Solve for r_dx to antenna	66.0	67.0	70.3	72.8	76.2	80.6	86.2	93.4	102.7	115.1	132.1	156.2	193.1	255.1	380.3	757.6	946.6	1892.1
Distance from Antenna Structure Base in Horizontal plane	0.1	11.7	24.1	30.8	38.2	46.3	55.4	66.1	78.7	94.3	114.4	141.6	181.4	246.4	374.5	754.8	944.3	1891.0
Angle from Main Beam (reference to horizontal plane)	90	80	70	65	60	55	50	45	40	35	30	25	20	15	10	5	4	0
dB down from centerline (referenced to centerline)	36.76	34.35	38.52	35.34	29.54	26.8	25.59	25.63	25.99	21.21	20.29	23.24	13.03	12.3	9.92	2	0.2	0
Reflection Coefficient (1 to 4.256 typical)	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56
Power Density (mW/cm^2)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01	#NUM!
Percent of Occupational Standard	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.5	0.3	0.3	0.4	0.4	0.1	#NUM!
Percent of General Population Standard	0.1	0.1	0.1	0.3	0.6	0.7	0.6	0.4	1.0	1.0	0.4	2.4	1.6	1.3	2.0	1.9	0.5	#NUM!
Antenna Type	BX4-70063-6CF																	
Max%	2.43%																	

Instructions:

- 1) Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to be saved as.
- 2) References to J4 refer to a point where the transmission line exits the equipment shelter and proceeds to the antenna(s). There is typically a connector located here where power measurements are made.
- 3) Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dBi, add 2.17 to dBd to obtain dB), Antenna Size (vertical size in inches), Downtilt (in Degrees, enter zero if none), Feedline loss from J4 to Antenna, and J4 centerline.
- 4) From manufacturer's plots, or data sheet, input Angle from mainbeam and dB below mainbeam centerline.
- 5) Enter Reflection coefficient (2.56 would be typical).
- 6) Spreadsheets calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
- 7) An odd distance may be entered in the rightmost column of the lower table.

Far Field Approximation
with downtilt variation

Estimated Radiated Emission

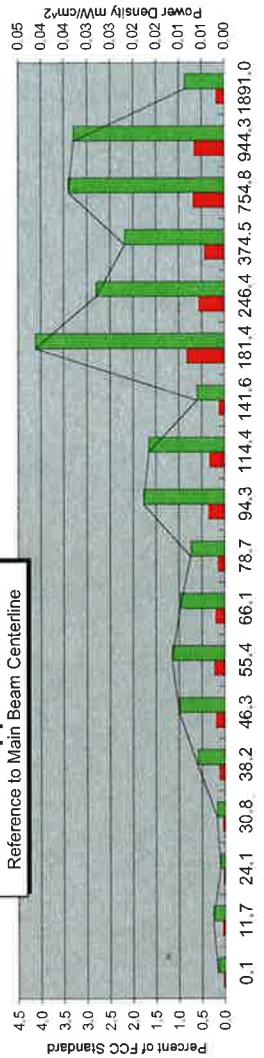
Single Emitter Far Field Model

Dipole / Wire/ Yagi Antenna Types

Location:	Danbury South, CT
Site #:	5-0169
Date:	07/15/14
Name:	Ryan Ulanday
File Name:	Danbury South, CT - FF Power
Operating Freq. (MHz)	2110.0
Antenna Height (ft):	69.0
Antenna Gain (dBi):	19.1
Antenna Size (in.):	72.4
Downtilt (degrees):	0.0
Feedline Loss (dB):	0.0
Power @ J4 (w):	1750.0

Far Field Approximation

Reference to Main Beam Centerline



Assumes level ground, normal to antenna mounting structure

— % Occupational ■ % General Public - - - Power Density

This approximation is only valid in the far field, which begins at: 65.2 Feet

Enter Main Beam
Distance in feet below:

Calc Angle	90.0	80.0	70.0	65.0	60.0	55.0	50.0	45.0	40.0	35.0	30.0	25.0	20.0	15.0	10.0	5.0	4.0	2.0
Solve for r, dB to antenna	66.0	67.0	70.3	72.8	76.2	80.6	86.2	93.4	102.7	115.1	132.1	156.2	193.1	255.1	380.3	757.6	946.6	1892.1
Distance from Antenna Structure Base in Horizontal plane	0.1	11.7	24.1	30.8	38.2	46.3	55.4	66.1	78.7	94.3	114.4	141.6	181.4	246.4	374.5	754.8	944.3	1891.0 #NUM!
Angle from Main Beam (reference to horizontal plane)	90	80	70	65	60	55	50	45	40	35	30	25	20	15	10	5	4	0
dB down from centerline (referenced to centerline)	36.76	34.35	38.52	35.34	29.54	26.8	25.59	25.63	25.99	21.21	20.29	23.24	13.03	12.3	9.92	2	0.2	0
Reflection Coefficient (1 to 4.256 typical)	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56	2.56
Power Density (mW/cm ²)	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.01	0.04	0.03	0.02	0.03	0.01	#NUM!	
Percent of Occupational Standard	0.0	0.1	0.0	0.1	0.2	0.2	0.1	0.4	0.3	0.1	0.8	0.6	0.4	0.7	0.7	0.2	#NUM!	
Percent of General Population Standard	0.1	0.3	0.1	0.2	0.6	1.0	1.1	1.0	0.7	1.8	1.7	0.6	4.1	2.8	2.2	3.4	3.3	0.9
Antenna Type	BXA-171063-12CF																	
Max%	4.12%																	

Instructions:

- Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to be saved as.
- References to J4 refer to a point where the transmission line exits the equipment shelter and proceeds to the antenna(s). There is typically a connector located here where power measurements are made.
- Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dBi, add 2.17 to dBd to obtain dBi), Antenna Size (vertical size in inches), Downtilt (in Degrees, enter zero if none), Feedline loss from J4 to Antenna, and J4 P.
- From manufacturer's plots, or data sheet; input Angle from mainbeam and dB below mainbeam centerline.
- Enter Reflection coefficient (2.56 would be typical 1 for free space)
- Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
- An odd distance may be entered in the rightmost column of the lower table.

ATTACHMENT 3

**AT&T Towers**

2300 Northlake Center Dr., Ste 40
Tucker GA 30084
404-532-5800

Wednesday, June 04, 2014



FDH Engineering, Inc.
6521 Meridien Dr.
Raleigh, NC 27616
919-755-1012

**STRUCTURAL ANALYSIS
65' SST**

AT&T DESIGNATION:	Site USID: SNET005-A
	Site FA: 10137472
	Site Name: Danbury
	Project Number: 1466U11400
	Carrier Project: 3_Wireline Verizon Modification 12-13-13
ANALYSIS CRITERIA:	TIA/EIA-222-F
	Codes: 2005 Connecticut Building Code

SITE DATA: 144 Old Boston Post Road, Danbury, CT 6810, Fairfield County
Latitude 41° 21' 34.22" N, Longitude 73° 27' 55.68" W
Market: NYC/NNJ
65' SST

Mr. Marty Jelleme

FDH Engineering Inc. is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

Analysis Results

Tower Stress Level with Proposed Equipment:	89.30%	Pass
Foundation Ratio with Proposed Equipment:	93.80%	Pass

We at FDH Engineering Inc. appreciate the opportunity of providing our continuing professional services to you and AT&T Towers. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully Submitted by: Mark S. Grgis, EI

Analysis Prepared by: Mark S. Grgis, EI

Analysis Reviewed by: Bradley R. Newman, PE



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Not for use or disclosure outside the AT&T companies
except under written agreement

FDH Engineering, Inc., 6521 Meridien Drive, Raleigh, NC 27616, Ph. 919.755.1012, Fax 919.755.1031

**Structural Analysis for
AT&T Towers**

65' Self-Support Tower

**Site Name: Danbury
Site USID: SNET005-A
Site FA#: 10137472**

Carrier Project: 3_Wireline Verizon Modification 12-13-13

FDH Project Number 1466U11400

Analysis Results

Tower Components	89.3%	Sufficient
Foundation	93.8%	Sufficient

Prepared By:



Mark S. Girgis, EI
Project Engineer

Reviewed By:



Bradley R. Newman, PE
Senior Project Engineer
CT PE License No. 29630

FDH Engineering, Inc.
6521 Meridien Drive
Raleigh, NC 27616
(919) 755-1012
info@fdh-inc.com



June 4, 2014

Prepared pursuant to TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and the 2005 Connecticut Building Code

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Conclusions	3
Recommendation.....	3
RESULTS.....	4
GENERAL COMMENTS	5
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EXECUTIVE SUMMARY

At the request of AT&T Towers, FDH Engineering, Inc. performed a structural analysis of the existing self-supported tower located in Danbury, CT to determine whether the tower is structurally adequate to support both the existing and proposed loads pursuant to the *Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, TIA/EIA-222-F* and the *2005 Connecticut Building Code (CBC)*. Information pertaining to the existing/proposed antenna loading, current tower geometry, the member sizes, soil parameters and foundation dimensions was obtained from:

- FDH, Inc. (Job No. 11-07130T T1) Self-Support Tower Mapping Report dated August 23, 2011
- FDH Engineering, Inc. (Project No. 11-07110E N1) Dispersive Wave Propagation Testing of an Existing Tower Foundation dated August 23, 2011
- FDH Engineering, Inc. (Project No. 11-07110E G1) Geotechnical Evaluation of Subsurface Conditions dated August 24, 2011
- FDH Engineering, Inc. (Project No. 12-03174E S1) Modification Drawings for a 65' Self-Support Tower dated March 16, 2012
- Hudson Design Group, LLC (Project No. CT2133) Final Report of Special Inspection dated January 11, 2013
- All documents and photos acquired from AT&T Siterra
- AT&T Towers

The *basic design wind speed* per the *TIA/EIA-222-F* standards is 85 mph without ice and 38 mph with 1/2" radial ice. Ice is considered to increase in thickness with height.

Conclusions

With the existing and proposed antennas from Verizon in place at 69 ft, the tower meets the requirements of the *TIA/EIA-222-F* standards and the *2005 CBC* provided the **Recommendations** listed below are satisfied. Furthermore, given the existing foundation dimensions (see FDH Project No. 11-07110E N1), and given soil parameters (see FDH Project No. 11-07110E G1), the foundation should have the necessary capacity to support the existing and proposed loading. For a more detailed description of the analysis of the tower, see the **Results** section of this report.

Our structural analysis has been performed assuming all information provided to FDH Engineering, Inc. is accurate (i.e., the steel data, tower layout, existing antenna loading, and proposed antenna loading) and that the tower has been properly erected and maintained per the original design drawings.

Recommendations

To ensure the requirements of the *TIA/EIA-222-F* standards and the *2005 CBC* are met with the existing and proposed loading in place, we have the following recommendations:

1. The proposed feed line must be installed adjacent to Verizon's existing feed lines.
2. RRU/RRH Stipulation: The equipment may be installed in any arrangement as determined by the client.

RESULTS

The following yield strength of steel for individual members was used for analysis:

Table 1 - Material Strength

Member Type	Yield Strength
Legs	36 ksi (Assumed)
Bracing	36 ksi (Assumed)

Table 2 displays the summary of the ratio (as a percentage) of force in the member to their capacities. Values greater than 100% indicate locations where the maximum force in the member exceeds its capacity. **Table 3** displays the maximum foundation reactions. **Table 4** displays the maximum antenna rotations at service wind speed (dishes only).

If the assumptions outlined in this report differ from actual field conditions, FDH Engineering, Inc. should be contacted to perform a revised analysis. Furthermore, as no information pertaining to the allowable twist and sway requirements for the existing or proposed appurtenances was provided, deflection and rotation were not taken into consideration when performing this analysis.

See the **Appendix** for detailed modeling information.

Table 2 - Summary of Working Percentage of Structural Components

Section No.	Elevation (ft)	Component Type	Size	% Capacity*	Pass Fail
T1	65 - 50.1042	Leg	15.5"Ø x 0.260 8-Sided Polygon	36.1	Pass
		Top Girt	12.45"Ø x 0.265 8-Sided Polygon	39.9	Pass
T2	50.1042 - 48.1042	Leg	15.5"Ø x 0.260 8-Sided Polygon	52.3	Pass
		Horizontal	12.45"Ø x 0.265 8-Sided Polygon	76.3	Pass
T3	48.1042 - 25.1667	Leg	15.5"Ø x 0.260 8-Sided Polygon	75.0	Pass
		Horizontal	W10x26	89.3	Pass
T4	25.1667 - 0	Leg	15.5"Ø x 0.260 8-Sided Polygon	18.4	Pass
		Diagonal	W6x25	23.6 38.1 (b)	Pass
		Horizontal	12.45"Ø x 0.265 8-Sided Polygon	0.7 1.1 (b)	Pass

*Capacities include 1/3 allowable increase for wind per *TIA/EIA-222-F* standards.

Table 3 - Maximum Base Reactions

Load Type	Direction	Current Analysis* (TIA/EIA-222-F)
Individual Foundation	Horizontal	21 k
	Uplift	80 k
	Compression	101 k
Overturning Moment	---	1,180 k-ft

*Foundation adequate per independent analysis.

Table 4 - Maximum Antenna Rotations at Service Wind Speeds (Dishes Only)

Centerline Elevation (ft)	Antenna	Tilt* (deg)	Twist* (deg)
60.5	(1) 6' Dish	0.0134	0.1060
57.5	(1) Radiowaves SPD2-5.8	0.0134	0.1011
57	(1) 6' Dish	0.0133	0.1002
46.5	(1) Gabriel PRFTV-48/75	0.0125	0.0780

*Allowable tilt and twist values to be determined by the carrier

GENERAL COMMENTS

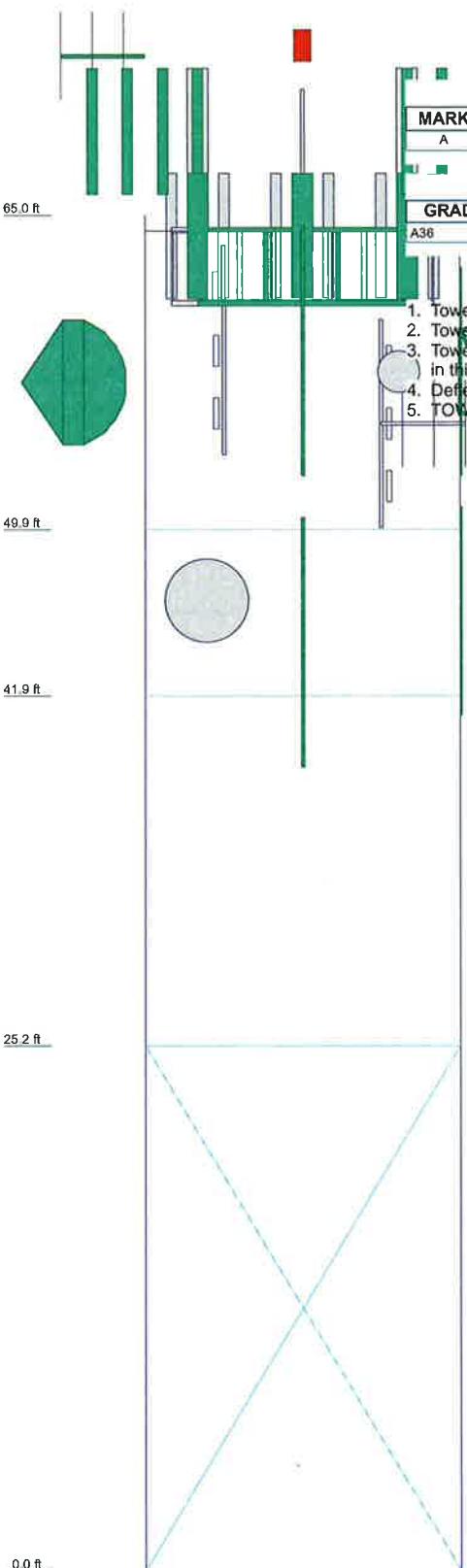
This engineering analysis is based upon the theoretical capacity of the structure. It is not a condition assessment of the tower and its foundation. It is the responsibility of AT&T Towers to verify that the tower modeled and analyzed is the correct structure (with accurate antenna loading information) modeled. If there are substantial modifications to be made or the assumptions made in this analysis are not accurate, FDH Engineering, Inc. should be notified immediately to perform a revised analysis.

LIMITATIONS

All opinions and conclusions are considered accurate to a reasonable degree of engineering certainty based upon the evidence available at the time of this report. All opinions and conclusions are subject to revision based upon receipt of new or additional/updated information. All services are provided exercising a level of care and diligence equivalent to the standard and care of our profession. No other warranty or guarantee, expressed or implied, is offered. Our services are confidential in nature and we will not release this report to any other party without the client's consent. The use of this engineering work is limited to the express purpose for which it was commissioned and it may not be reused, copied, or distributed for any other purpose without the written consent of FDH Engineering, Inc.

APPENDIX

Section	T4	T3	T2	T1
Legs		15.5 \varnothing x 0.260 8-Sided Polygon		
Leg Grade	A36			
Diagonals	W6x25			N.A.
Diagonal Grade	A36			N.A.
Top Girts		12.45 \varnothing x 0.265 8-Sided Polygon		
Horizontal			A	
Face Width (ft)		W10x30		N.A.
# Panels @ (ft)		15.0313		
Weight (K)	19.4	1 @ 25.1667	1 @ 8	1 @ 14.2812
	9.4	36	27	37



SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	12.45 \varnothing x 0.265 8-Sided Polygon		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A36	36 ksi	58 ksi			

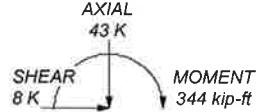
TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 38 mph basic wind with 0.50 in ice. Ice is considered to increase in thickness with height.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 89.3%

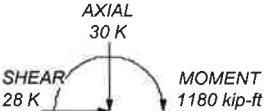
MAX. CORNER REACTIONS AT BASE:

DOWN: 101 K
SHEAR: 21 K

UPLIFT: -80 K
SHEAR: 17 K



TORQUE 11 kip-ft
38 mph WIND - 0.5000 in ICE

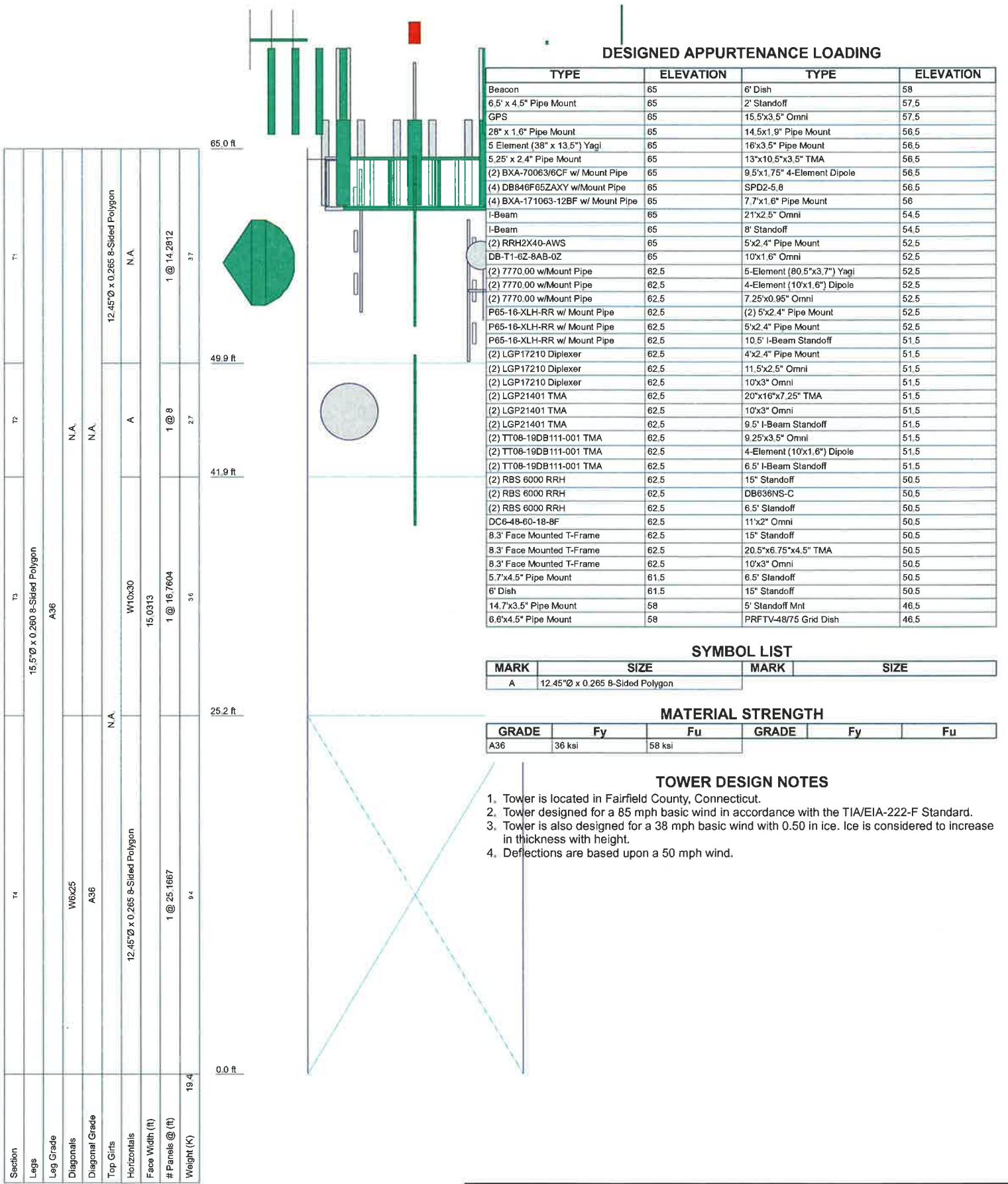


TORQUE 44 kip-ft
REACTIONS - 85 mph WIND



FDH Engineering, Inc.
6521 Meridian Drive
Raleigh, NC 27616
Phone: (919) 755-1012
FAX: (919) 755-1031

Job: Danbury, SNET005-A/FA# 10137472			
Project: 1466U11400	Drawn by: Mark S. Grgis	App'd:	
Client: AT&T Towers	Date: 06/04/14	Scale: NTS	
Code: TIA/EIA-222-F			
Path: Dwg No. E-1			

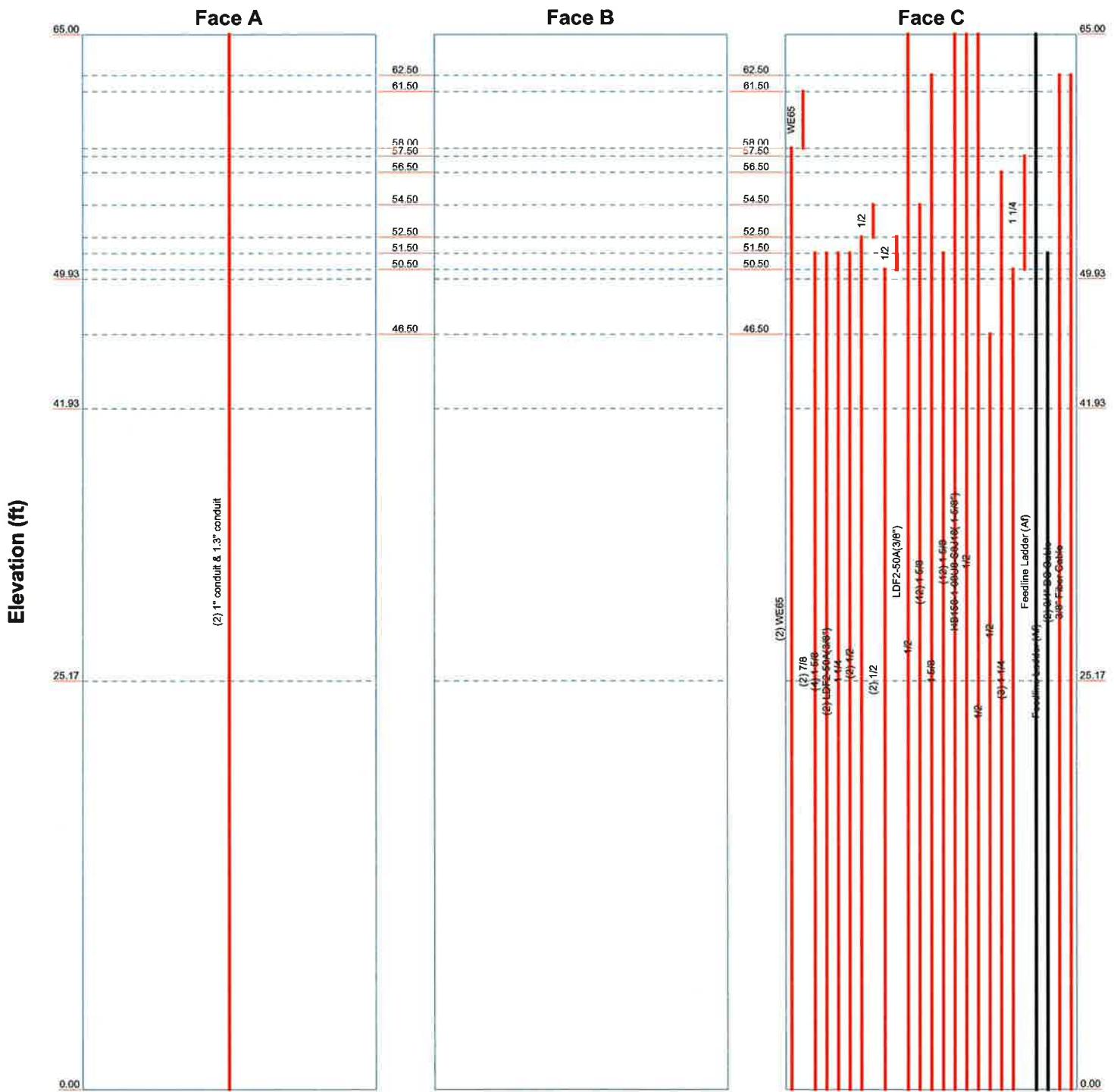


- TOWER DESIGN NOTES**
1. Tower is located in Fairfield County, Connecticut.
 2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
 3. Tower is also designed for a 38 mph basic wind with 0.50 in ice. Ice is considered to increase in thickness with height.
 4. Deflections are based upon a 50 mph wind.

Feed Line Distribution Chart

0' - 65'

Round Flat App In Face App Out Face Truss Leg

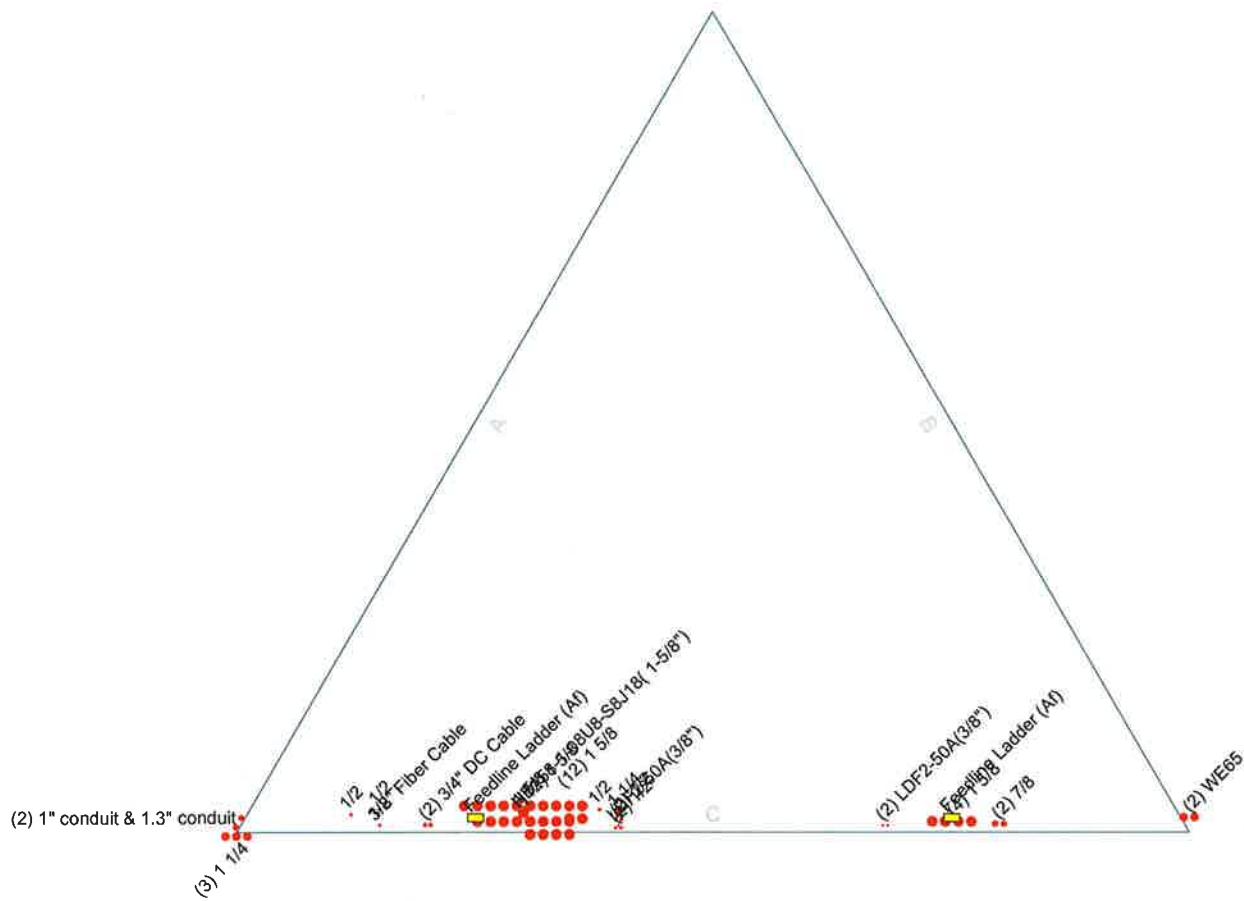


FDH Engineering, Inc.
6521 Meridien Drive
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Job: Danbury, SNET005-A/FA# 10137472			
Project: 1466U11400	Drawn by: Mark S. Grgis	App'd:	
Client: AT&T Towers			
Code: TIA/EIA-222-F	Date: 06/04/14	Scale: NTS	
Path:			Dwg No. E-7

Feed Line Plan

Round ————— Flat ————— App In Face ————— App Out Face



FDH Engineering, Inc.		
6521 Meridien Drive		
Raleigh, NC 27616		
Phone: (919) 755-1012		
FAX: (919) 755-1031		
Job: Danbury, SNET005-A/FA# 10137472		
Project: 1466U11400		
Client: AT&T Towers	Drawn by: Mark S. Girgis	App'd:
Code: TIA/EIA-222-F	Date: 06/04/14	Scale: NTS
Path:		Dwg No. E-7

<p>tnxTower</p> <p>FDH Engineering, Inc. 6521 Meridien Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1031</p>	Job Danbury, SNET005-A/FA# 10137472	Page 1 of 32
	Project 1466U11400	Date 14:44:06 06/04/14
	Client AT&T Towers	Designed by Mark S. Girgis

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 65.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 15.03 ft at the top and 15.03 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

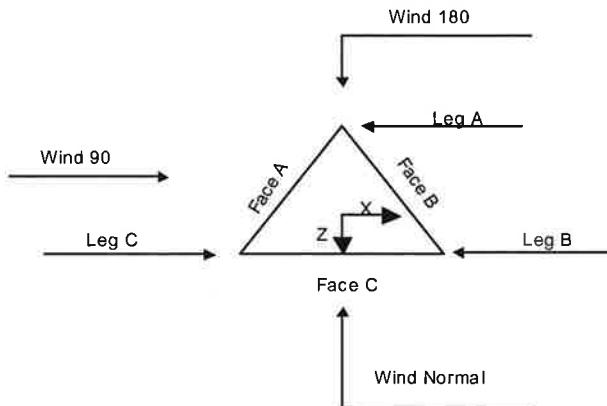
The following design criteria apply:

- Tower is located in Fairfield County, Connecticut.
- Basic wind speed of 85 mph.
- Nominal ice thickness of 0.5000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56 pcf.
- A wind speed of 38 mph is used in combination with ice.
- Temperature drop of 50 °F.
- Deflections calculated using a wind speed of 50 mph.
- Pressures are calculated at each section.
- Stress ratio used in tower member design is 1.333.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs	Distribute Leg Loads As Uniform	Treat Feedline Bundles As Cylinder
Consider Moments - Horizontals	Assume Legs Pinned	Use ASCE 10 X-Brace Ly Rules
Consider Moments - Diagonals	✓ Assume Rigid Index Plate	✓ Calculate Redundant Bracing Forces
Use Moment Magnification	✓ Use Clear Spans For Wind Area	Ignore Redundant Members in FEA
✓ Use Code Stress Ratios	✓ Use Clear Spans For KL/r	✓ SR Leg Bolts Resist Compression
✓ Use Code Safety Factors - Guys	Retension Guys To Initial Tension	✓ All Leg Panels Have Same Allowable
✓ Escalate Ice	Bypass Mast Stability Checks	Offset Girt At Foundation
Always Use Max Kz	✓ Use Azimuth Dish Coefficients	✓ Consider Feedline Torque
Use Special Wind Profile	✓ Project Wind Area of Appurt.	✓ Include Angle Block Shear Check
✓ Include Bolts In Member Capacity	Autocalc Torque Arm Areas	Poles
Leg Bolts Are At Top Of Section	SR Members Have Cut Ends	Include Shear-Torsion Interaction
✓ Secondary Horizontal Braces Leg	Sort Capacity Reports By Component	Always Use Sub-Critical Flow
Use Diamond Inner Bracing (4 Sided)	Triangulate Diamond Inner Bracing	Use Top Mounted Sockets
Add IBC .6D+W Combination	Use TIA-222-G Tension Splice Capacity	
	Exemption	

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Triangular Tower

Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
				ft		ft
T1	65.00-49.93			15.03	1	15.07
T2	49.93-41.93			15.03	1	8.00
T3	41.93-25.17			15.03	1	16.76
T4	25.17-0.00			15.03	1	25.17

Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	65.00-49.93	14.28	X Brace	No	Yes	9.5000	0.0000
T2	49.93-41.93	8.00	X Brace	No	Yes	0.0000	0.0000
T3	41.93-25.17	16.76	X Brace	No	Yes	0.0000	0.0000
T4	25.17-0.00	25.17	X Brace	No	Yes	0.0000	0.0000

Tower Section Geometry (cont'd)

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Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 65.00-49.93	Arbitrary Shape	15.5"Ø x 0.260 8-Sided Polygon	A36 (36 ksi)	Equal Angle		A36 (36 ksi)
T2 49.93-41.93	Arbitrary Shape	15.5"Ø x 0.260 8-Sided Polygon	A36 (36 ksi)	Equal Angle		A36 (36 ksi)
T3 41.93-25.17	Arbitrary Shape	15.5"Ø x 0.260 8-Sided Polygon	A36 (36 ksi)	Wide Flange		A36 (36 ksi)
T4 25.17-0.00	Arbitrary Shape	15.5"Ø x 0.260 8-Sided Polygon	A36 (36 ksi)	Wide Flange	W6x25	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T1 65.00-49.93	None	Flat Bar		A36 (36 ksi)	Arbitrary Shape	12.45"Ø x 0.265 8-Sided Polygon	A36 (36 ksi)
T2 49.93-41.93	None	Flat Bar		A36 (36 ksi)	Arbitrary Shape	12.45"Ø x 0.265 8-Sided Polygon	A36 (36 ksi)
T3 41.93-25.17	None	Flat Bar		A36 (36 ksi)	Wide Flange	W10x30	A572-50 (50 ksi)
T4 25.17-0.00	None	Flat Bar		A36 (36 ksi)	Arbitrary Shape	12.45"Ø x 0.265 8-Sided Polygon	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A_r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
T1 65.00-49.93	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000
T2 49.93-41.93	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000
T3 41.93-25.17	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000
T4 25.17-0.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000

Tower Section Geometry (cont'd)

Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
				X Y	X Y	X Y	X Y	X Y	X Y	X Y

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		K Factors ¹									
Tower Elevation	Calc K Single Angles	Calc K Solid Rounds	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
ft				X Y	X Y	X Y	X Y	X Y	X Y	X Y	
65.00-49.93	Yes	Yes	I	1	1	1	1	1	1	1	
49.93-41.93	Yes	Yes	I	1	1	1	1	1	1	1	
41.93-25.17	Yes	Yes	I	1	1	1	1	1	1	1	
T4 25.17-0.00	Yes	Yes	I	1	1	1	1	1	1	1	

¹Note: K-factors are applied to member segment lengths. K-braces without inner supporting members will have the K-factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

Tower Section Geometry (cont'd)

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Shield	Allow Component Type	Placement	Face Offset	Lateral Offset	# Per Row	# Spacing in	Clear in	Width or Diameter in	Perimeter in	Weight plf
	Leg		ft	in	(Frac FW)						

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Section	Elevation	CP _X	CP _Z	CP _X Ice	CP _Z Ice
	ft	in	in	in	in
T1	65.00-49.93	-8.5238	12.9131	-9.1469	12.9126
T2	49.93-41.93	-6.0560	14.6200	-6.7993	13.2003
T3	41.93-25.17	-7.8040	18.6951	-8.7445	17.1123
T4	25.17-0.00	-6.2306	14.9259	-6.9289	13.3030

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K
Beacon	A	From Leg	0.00 0.00 7.30	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.00 2.50 3.00 4.00 6.00	0.02 0.03 0.04 0.06 0.10
6.5" x 4.5" Pipe Mount	A	From Leg	0.00 0.00 3.00	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.60 3.01 3.42 4.28 6.12	0.07 0.09 0.12 0.19 0.38
*** GPS	C	From Leg	0.00 11.00 1.50	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.62 0.75 0.89 1.20 1.96	0.01 0.02 0.03 0.05 0.13
28" x 1.6" Pipe Mount	C	From Leg	0.00 7.00 0.00	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.36 0.49 0.65 1.01 1.87	0.03 0.03 0.04 0.05 0.11
*** 5 Element (38" x 13.5") Yagi	C	From Leg	0.00 0.00 7.60	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.50 1.90 2.30 3.10 4.70	0.02 0.02 0.03 0.04 0.05
5.25" x 2.4" Pipe Mount	C	From Leg	0.00 0.00 3.00	0.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.33 1.63 1.95 2.60 4.11	0.03 0.04 0.05 0.09 0.22
*** (2) BXA-70063/6CF w/ Mount Pipe	A	From Leg	0.00 0.00 4.00	-40.0000	65.00	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	7.98 8.62 9.23 10.47 13.08	0.04 0.10 0.17 0.33 0.79
(4) DB846F65ZAXY w/Mount Pipe	B	From Leg	0.00 0.00 4.00	75.0000	65.00	No Ice 1/2" Ice 1" Ice	7.27 7.88 8.48	0.05 0.11 0.19

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	Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K
(4)	BXA-171063-12BF w/ Mount Pipe	C	From Leg	0.00 0.00 4.00	40.0000	65.00	2" Ice 9.72 4" Ice 12.33 No Ice 4.97 1/2" Ice 5.52 1" Ice 6.04 2" Ice 7.09 4" Ice 9.36	11.81 15.98 5.23 6.39 7.26 9.05 12.82	0.37 0.87 0.04 0.09 0.14 0.27 0.67
I-Beam		A	From Leg	0.00 0.00 1.50	0.0000	65.00	No Ice 8.76 1/2" Ice 12.74 1" Ice 16.72 2" Ice 24.68 4" Ice 40.60	0.78 0.95 1.13 1.49 2.21	0.34 0.50 0.66 0.97 1.59
I-Beam		C	From Leg	0.00 0.00 1.50	0.0000	65.00	No Ice 8.76 1/2" Ice 12.74 1" Ice 16.72 2" Ice 24.68 4" Ice 40.60	0.78 0.95 1.13 1.49 2.21	0.34 0.50 0.66 0.97 1.59
(2)	RRH2X40-AWS	A	From Leg	0.00 0.00 4.00	-40.0000	65.00	No Ice 2.52 1/2" Ice 2.75 1" Ice 2.99 2" Ice 3.50 4" Ice 4.61	1.59 1.80 2.01 2.46 3.48	0.04 0.06 0.08 0.13 0.28
DB-T1-6Z-8AB-0Z		C	From Leg	0.00 0.00 4.00	40.0000	65.00	No Ice 5.60 1/2" Ice 5.92 1" Ice 6.24 2" Ice 6.91 4" Ice 8.37	2.33 2.56 2.79 3.28 4.37	0.04 0.08 0.12 0.21 0.45

(2)	7770.00 w/Mount Pipe	A	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 6.46 1/2" Ice 7.14 1" Ice 7.73 2" Ice 8.94 4" Ice 11.51	4.59 5.66 6.45 8.06 11.64	0.05 0.10 0.16 0.30 0.71
(2)	7770.00 w/Mount Pipe	B	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 6.46 1/2" Ice 7.14 1" Ice 7.73 2" Ice 8.94 4" Ice 11.51	4.59 5.66 6.45 8.06 11.64	0.05 0.10 0.16 0.30 0.71
(2)	7770.00 w/Mount Pipe	C	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 6.46 1/2" Ice 7.14 1" Ice 7.73 2" Ice 8.94 4" Ice 11.51	4.59 5.66 6.45 8.06 11.64	0.05 0.10 0.16 0.30 0.71
P65-16-XLH-RR w/ Mount Pipe		A	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 8.64 1/2" Ice 9.29 1" Ice 9.91 2" Ice 11.18 4" Ice 13.83	6.36 7.54 8.43 10.24 14.10	0.08 0.14 0.22 0.39 0.89
P65-16-XLH-RR w/ Mount Pipe		B	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 8.64 1/2" Ice 9.29 1" Ice 9.91 2" Ice 11.18 4" Ice 13.83	6.36 7.54 8.43 10.24 14.10	0.08 0.14 0.22 0.39 0.89
P65-16-XLH-RR w/ Mount Pipe		C	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 8.64 1/2" Ice 9.29 1" Ice 9.91 2" Ice 11.18 4" Ice 13.83	6.36 7.54 8.43 10.24 14.10	0.08 0.14 0.22 0.39 0.89

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<i>Description</i>	<i>Face or Leg</i>	<i>Offset Type</i>	<i>Offsets:</i> <i>Horz Lateral Vert</i> <i>ft ft ft</i>	<i>Azimuth Adjustment</i> <i>°</i>	<i>Placement</i> <i>ft</i>	<i>C_{AA}</i> <i>Front</i>	<i>C_{AA}</i> <i>Side</i>	<i>Weight</i> <i>K</i>	
(2) LGP17210 Diplexer	A	From Face	0.00 0.00 1.50	50.0000	62.50	4" Ice No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	13.83 1.95 2.13 2.33 2.75 3.69	14.10 0.50 0.62 0.75 1.03 1.69	0.89 0.01 0.02 0.03 0.07 0.17
(2) LGP17210 Diplexer	B	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.95 2.13 2.33 2.75 3.69	0.50 0.62 0.75 1.03 1.69	0.01 0.02 0.03 0.07 0.17
(2) LGP17210 Diplexer	C	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	1.95 2.13 2.33 2.75 3.69	0.50 0.62 0.75 1.03 1.69	0.01 0.02 0.03 0.07 0.17
(2) LGP21401 TMA	A	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.95 1.09 1.24 1.57 2.32	0.37 0.48 0.60 0.87 1.51	0.02 0.02 0.03 0.05 0.12
(2) LGP21401 TMA	B	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.95 1.09 1.24 1.57 2.32	0.37 0.48 0.60 0.87 1.51	0.02 0.02 0.03 0.05 0.12
(2) LGP21401 TMA	C	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.95 1.09 1.24 1.57 2.32	0.37 0.48 0.60 0.87 1.51	0.02 0.02 0.03 0.05 0.12
(2) TT08-19DB111-001 TMA	A	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.92 1.06 1.21 1.54 2.29	0.75 0.88 1.02 1.32 2.04	0.02 0.03 0.04 0.06 0.15
(2) TT08-19DB111-001 TMA	B	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.92 1.06 1.21 1.54 2.29	0.75 0.88 1.02 1.32 2.04	0.02 0.03 0.04 0.06 0.15
(2) TT08-19DB111-001 TMA	C	From Face	0.00 0.00 1.50	30.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.92 1.06 1.21 1.54 2.29	0.75 0.88 1.02 1.32 2.04	0.02 0.03 0.04 0.06 0.15
(2) RBS 6000 RRH	A	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.94 3.17 3.41 3.91 5.02	1.19 1.35 1.52 1.89 2.72	0.06 0.07 0.10 0.15 0.30
(2) RBS 6000 RRH	B	From Face	0.00 0.00 1.50	50.0000	62.50	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	2.94 3.17 3.41 3.91 5.02	1.19 1.35 1.52 1.89 2.72	0.06 0.07 0.10 0.15 0.30
(2) RBS 6000 RRH	C	From Face	0.00	30.0000	62.50	No Ice	2.94	1.19	0.06

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
<hr/>										

Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L	L _u	Kl/r	F _a	A	Actual P K	Allow. P _a K	Ratio P P _a
T1	65 - 49.9271	15.5"Ø x 0.260 8-Sided Polygon	15.07	14.28	30.9 K=1.00	19.875	13.1302	-8.46	260.97	0.032
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	8.00	8.00	17.3 K=1.00	20.758	13.1302	-21.22	272.56	0.078
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	16.76	16.76	36.3 K=1.00	19.478	13.1302	-33.36	255.76	0.130
T4	25.1667 - 0	15.5"Ø x 0.260 8-Sided Polygon	25.17	25.17	54.5 K=1.00	17.946	13.1302	-57.80	235.63	0.245

Leg Bending Design Data (Compression)

Section No.	Elevation ft	Size	Actual M _x kip-ft	Actual f _{bx} ksi	Allow. F _{bx} ksi	Ratio f _{bx} / F _{bx}	Actual M _y kip-ft	Actual f _{by} ksi	Allow. F _{by} ksi	Ratio f _{by} / F _{by}
T1	65 - 49.9271	15.5"Ø x 0.260 8-Sided Polygon	-31.18	-7.192	21.600	0.333	-10.81	-2.495	21.600	0.116
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	-41.43	-9.557	21.600	0.442	16.60	-3.830	21.600	0.177
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	-50.78	-11.714	21.600	0.542	-30.61	-7.061	21.600	0.327
T4	25.1667 - 0	15.5"Ø x 0.260 8-Sided Polygon	0.00	0.000	21.600	0.000	0.00	0.000	21.600	0.000

Leg Interaction Design Data (Compression)

Section No.	Elevation ft	Size	Ratio P P _a	Ratio f _{bx} F _{bx}	Ratio f _{by} F _{by}	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
T1	65 - 49.9271	15.5"Ø x 0.260 8-Sided Polygon	0.032	0.333	0.116	0.481 ✓	1.333	H1-3 ✓
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	0.078	0.442	0.177	0.698 ✓	1.333	H1-3 ✓
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	0.130	0.542	0.327	1.000 ✓	1.333	H1-3 ✓

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Section No.	Elevation	Size	L	L _u	Kl/r	F _a	A	Actual P K	Allow. P _a K	Ratio P / P _a
	ft		ft	ft		ksi	in ²			
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	8.00	8.00	17.3	21.600	13.1302	10.48	283.61	0.037
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	16.76	16.76	36.3	21.600	13.1302	20.73	283.61	0.073
T4	25.1667 - 0	15.5"Ø x 0.260 8-Sided Polygon	25.17	25.17	54.5	21.600	13.1302	47.55	283.61	0.168

Leg Bending Design Data (Tension)

Section No.	Elevation	Size	Actual M _x kip-ft	Actual f _{bx} ksi	Allow. F _{bx} ksi	Ratio f _{bx} / F _{bx}	Actual M _y kip-ft	Actual f _{by} ksi	Allow. F _{by} ksi	Ratio f _{by} / F _{by}
	ft									
T1	65 - 49.9271	15.5"Ø x 0.260 8-Sided Polygon	29.52	6.810	21.600	0.315	-10.74	2.477	21.600	0.115
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	40.37	9.314	21.600	0.431	-16.66	3.844	21.600	0.178
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	50.34	11.613	21.600	0.538	-30.67	7.075	21.600	0.328
T4	25.1667 - 0	15.5"Ø x 0.260 8-Sided Polygon	0.00	0.000	21.600	0.000	0.00	0.000	21.600	0.000

Leg Interaction Design Data (Tension)

Section No.	Elevation	Size	Ratio P / P _a	Ratio f _{bx} / F _{bx}	Ratio f _{by} / F _{by}	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
	ft							
T1	65 - 49.9271	15.5"Ø x 0.260 8-Sided Polygon	0.017	0.315	0.115	0.447 ✓	1.333	H2-1 ✓
T2	49.9271 - 41.9271	15.5"Ø x 0.260 8-Sided Polygon	0.037	0.431	0.178	0.646 ✓	1.333	H2-1 ✓
T3	41.9271 - 25.1667	15.5"Ø x 0.260 8-Sided Polygon	0.073	0.538	0.328	0.938 ✓	1.333	H2-1 ✓
T4	25.1667 - 0	15.5"Ø x 0.260 8-Sided Polygon	0.168	0.000	0.000	0.168 ✓	1.333	H2-1 ✓

Diagonal Design Data (Tension)

Section No.	Elevation	Size	L	L _u	Kl/r	F _a	A	Actual P K	Allow. P _a K	Ratio P / P _a
	ft		ft	ft		ksi	in ²			
T4	25.1667 - 0	W6x25	29.31	13.40	105.8	29.000	5.2950	23.21	153.56	0.151 ✓

<p><i>tnxTower</i></p> <p>FDH Engineering, Inc. 6521 Meridian Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1031</p>	Job	Danbury, SNET005-A/FA# 10137472	Page	30 of 32
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	Client	AT&T Towers	Designed by	Mark S. Grgis

Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	KL/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T2	49.9271 - 41.9271	12.45"Ø x 0.265 8-Sided Polygon	15.03	13.74	37.2	21.600	10.7000	1.68	231.12	0.007
T3	41.9271 - 25.1667	W10x30	15.03	13.74	120.3	32.500	6.3769	0.09	207.25	0.000
T4	25.1667 - 0	12.45"Ø x 0.265 8-Sided Polygon	15.03	13.74	37.2	21.600	10.7000	1.04	231.12	0.005*

* DL controls

Horizontal Bending Design Data

Section No.	Elevation ft	Size	Actual M _x kip-ft	Actual f _{bx} ksi	Allow. F _{bx} ksi	Ratio f _{bx} F _{bx}	Actual M _y kip-ft	Actual f _{by} ksi	Allow. F _{by} ksi	Ratio f _{by} F _{by}
T2	49.9271 - 41.9271	12.45"Ø x 0.265 8-Sided Polygon	-49.82	19.180	21.600	0.888	-0.07	0.027	21.600	0.001
T3	41.9271 - 25.1667	W10x30	-66.10	24.481	20.618	1.187	0.04	0.074	37.500	0.002
T4	25.1667 - 0	12.45"Ø x 0.265 8-Sided Polygon	0.00	0.000	21.600	0.000	0.00	0.000	21.600	0.000

Horizontal Interaction Design Data

Section No.	Elevation ft	Size	Ratio P P _a	Ratio f _{bx} F _{bx}	Ratio f _{by} F _{by}	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
T2	49.9271 - 41.9271	12.45"Ø x 0.265 8-Sided Polygon	0.007	0.888	0.001	0.896 ✓	1.333	H2-1 ✓
T3	41.9271 - 25.1667	W10x30	0.000	1.187	0.002	1.190 ✓	1.333	H2-1 ✓
T4	25.1667 - 0	12.45"Ø x 0.265 8-Sided Polygon	0.005	0.000	0.000	0.005* ✓	1.000	H2-1 ✓

* DL controls

Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	KL/r	F _a ksi	A in ²	Actual P K	Allow. P _a K	Ratio P P _a
T1	65 - 49.9271	12.45"Ø x 0.265 8-Sided Polygon	15.03	13.74	37.2	21.600	10.7000	0.74	231.12	0.003

tnxTower FDH Engineering, Inc. 6521 Meridian Drive Raleigh, NC 27616 Phone: (919) 755-1012 FAX: (919) 755-1031	Job	Danbury, SNET005-A/FA# 10137472	Page	31 of 32
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	Client	AT&T Towers	Designed by	Mark S. Grgis

Top Girt Bending Design Data

Section No.	Elevation ft	Size	Actual M_x kip-ft	Actual f_{bx} ksi	Allow. F_{bx} ksi	Ratio $\frac{f_{bx}}{F_{bx}}$	Actual M_y kip-ft	Actual f_{by} ksi	Allow. F_{by} ksi	Ratio $\frac{f_{by}}{F_{by}}$
T1	65 - 49.9271	12.45"Ø x 0.265 8-Sided Polygon	-26.65	10.259	21.600	0.475	-0.06	0.022	21.600	0.001

Top Girt Interaction Design Data

Section No.	Elevation ft	Size	Ratio P	Ratio f_{bx}	Ratio f_{by}	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
			$\frac{P}{P_a}$	$\frac{f_{bx}}{F_{bx}}$	$\frac{f_{by}}{F_{by}}$			
T1	65 - 49.9271	12.45"Ø x 0.265 8-Sided Polygon	0.003	0.475	0.001	0.479 ✓	1.333 ✓	H2-1 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P _{allow} K	% Capacity	Pass Fail
T1	65 - 49.9271	Leg Top Girt	15.5"Ø x 0.260 8-Sided Polygon	1	-8.46	347.87	36.1	Pass
			12.45"Ø x 0.265 8-Sided Polygon	4	0.74	308.08	39.9	Pass
T2	49.9271 - 41.9271	Leg	15.5"Ø x 0.260 8-Sided Polygon	8	-21.22	363.33	52.3	Pass
			Horizontal 12.45"Ø x 0.265 8-Sided Polygon	10	1.68	308.08	76.3	Pass
T3	41.9271 - 25.1667	Leg	15.5"Ø x 0.260 8-Sided Polygon	13	-33.36	340.92	75.0	Pass
T4	25.1667 - 0	Horizontal Leg	W10x30	16	0.09	276.26	89.3	Pass
			15.5"Ø x 0.260 8-Sided Polygon	20	-57.80	314.10	18.4	Pass
		Diagonal	W6x25	25	-28.29	119.70	23.6	Pass
		Horizontal	12.45"Ø x 0.265 8-Sided Polygon	23	-1.47	207.67	38.1 (b) 0.7 1.1 (b) Summary	Pass
						Leg (T3)	75.0	Pass
						Diagonal (T4)	38.1	Pass
						Horizontal (T3)	89.3	Pass
						Top Girt (T1)	39.9	Pass
						Bolt Checks	38.1	Pass
						RATING =	89.3	Pass

Project: Danbury, S NET DOG-A

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Date:

By: NSH

FDH Project #:

Checked By:

Drawing #:

Overturining:

$$FS = \frac{(P + W_L + W_C)(I/2)}{M_s + V(d)} = \frac{(43 K + 140 K)(21.6 \text{ ft}/2)}{1,180 \text{ k-ft} + 28 K(2.5 \text{ ft})}$$

$$= 1.6 > 1.5 \quad \text{OK} \quad 1.5/1.6 = \boxed{93.8\%}$$

Toe Pressure:

$$g_u H = 25 \text{ ksf}$$

$$\frac{M}{S} + \frac{P}{A} \Rightarrow S = \frac{I}{q} = \frac{11,197.4 \text{ in}^4}{13} = 861.3 \text{ ft}^3$$

$$\sigma = \frac{1,180 \text{ k-ft}}{861.3 \text{ ft}^3} + \frac{43 \text{ k}}{357.2 \text{ ft}^2} = 1.49 \text{ ksf}$$

$$\frac{1.49 \text{ ksf}}{0.5(28 \text{ ksf})} = \boxed{11.9\%}$$