



# STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

Internet: [ct.gov/csc](http://ct.gov/csc)

*Daniel F. Caruso*  
Chairman

August 30, 2010

Jennifer Young Gaudet  
Project Manager  
HPC Development LLC  
46 Mill Plain Road, 2<sup>nd</sup> floor  
Danbury, CT 06811

RE: **EM-T-MOBILE-034-100809** - Omnipoint Communications, as subsidiary of T-Mobile USA, Inc., notice of intent to modify an existing telecommunications facility located at 303 Boxwood Lane, Danbury, Connecticut.

Dear Mrs. Gaudet:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- a) the tower be reinforced and all coax cables be routed in accordance with the structural analysis prepared by Centek Engineering dated July 22, 2010 and stamped by Carlo Centore; and
- b) The tower shall not exceed 100 percent of its post-construction structural rating; and
- c) Not more than 45 days after completion of construction, a signed letter from a Professional Engineer duly licensed in the State of Connecticut shall be submitted to the Council to certify that the reinforcements have been properly completed and the tower does not exceed 100 percent of its post-construction structural rating.

The proposed modifications are to be implemented as specified here and in your notice dated August 6, 2010, including the placement of all necessary equipment and shelters within the tower compound. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any

deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,



Linda Roberts  
Executive Director

LR/CDM/laf

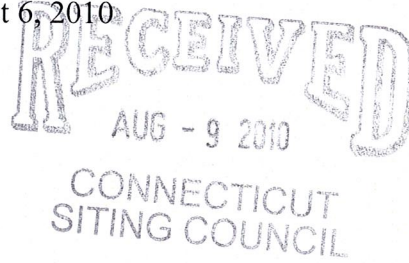
c: The Honorable Mark D. Boughton, Mayor, City of Danbury  
Dennis Elpern, City Planner, City of Danbury  
Western Connecticut State University



ORIGINAL

EM-T-MOBILE-034-100910

August 6, 2010



Connecticut Siting Council  
10 Franklin Square  
New Britain, Connecticut 06051  
Attn: Mr. S. Derek Phelps, Executive Director

Re: T-Mobile Northeast, LLC – exempt modification  
303 Boxwood Lane, Danbury, Connecticut

Dear Mr. Phelps:

This letter and attachments are submitted on behalf of T-Mobile Northeast, LLC (“T-Mobile”). T-Mobile plans to install antennas and related equipment at the Western Connecticut State University tower site at 303 Boxwood Lane in Danbury (coordinates 41°23’41.93” N, - 73°29’12.27” W). Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). It should be noted that this proposal was previously the subject of an exempt modification dated November 12, 2008 and acknowledged by the Council on December 10, 2008. In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the Mayor of Danbury.

T-Mobile will install three panel antennas at the 83’ level of the tower. The antennas will be installed flush to the legs of the tower; two twin TMAs will be mounted behind each antenna. Twelve coaxial cables will also be installed. T-Mobile’s equipment cabinets will be placed on a concrete pad near the base of the tower. Attached are a compound plan and elevation depicting the planned changes. Also attached are a structural analysis and associated reinforcement modification plan, which will be implemented at the time of construction to achieve structural sufficiency for T-Mobile’s installation. Consistent with T-Mobile’s lease rights, the elevation depicts a total of nine antennas; only three are proposed, in conformance with the structural analysis.

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes (“C.G.S.”) Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. The height of the overall structure will be unaffected. The top of the tower extends to approximately 100’; T-Mobile’s proposed antennas will be located with a center line of 83’ AGL.

Mr. S. Derek Phelps


August 6, 2010

Page 2

2. The addition of T-Mobile's equipment will not require any extension of the site boundaries. All equipment will be located within the existing fenced compound.
3. The proposed changes will not increase the noise level at the existing facility by six decibels or more. The incremental effect of the additional cabinets will be negligible.
4. The changes to the facility will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site. As indicated on the attached power density calculation, T-Mobile's operations at the site will result in a power density of 18.116%; the combined site operations will result in a total power density of 36.626%.

Please feel free to call me at (860) 798-7454 with questions concerning this matter. Thank you for your consideration.

Respectfully yours,



Jennifer Young Gaudet

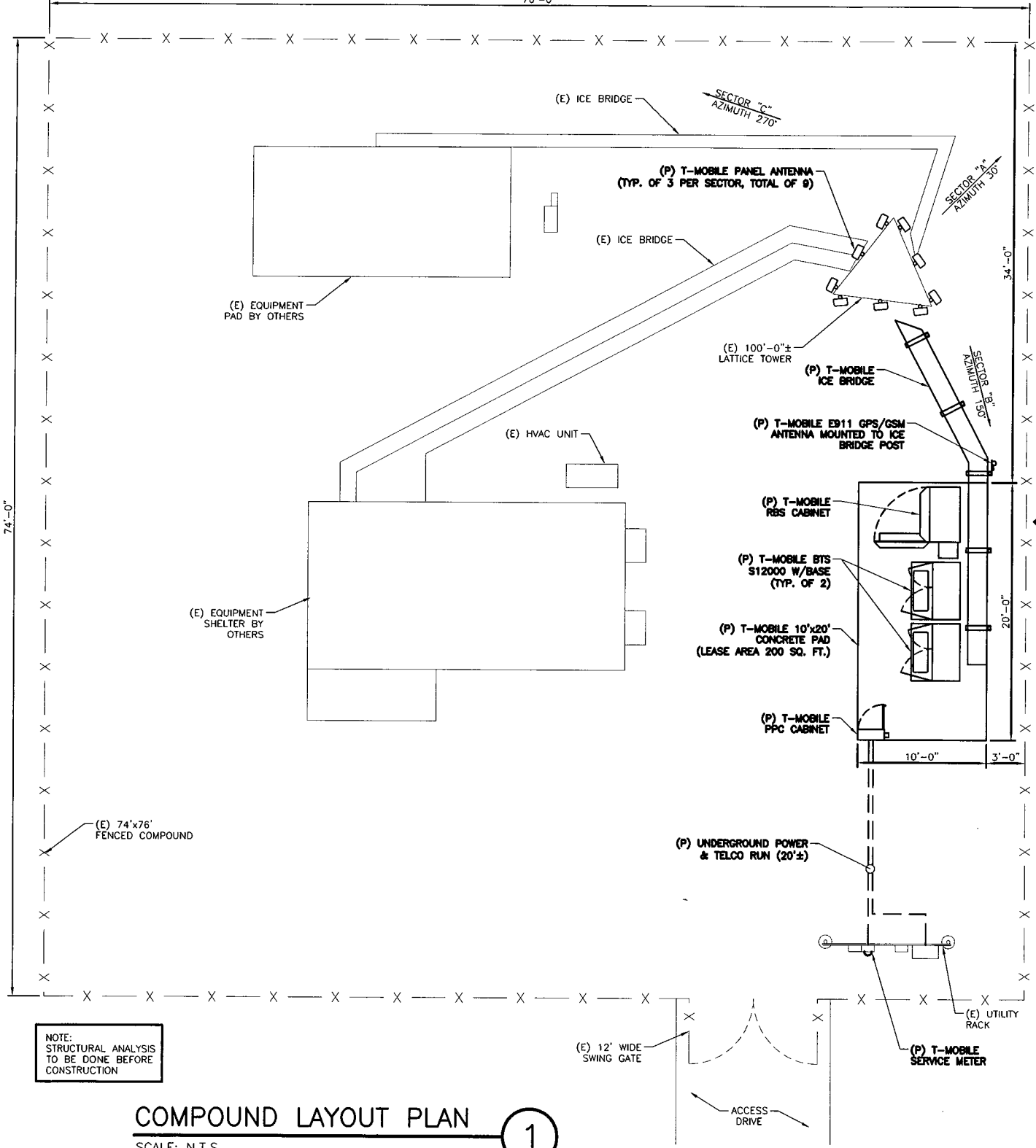
cc: Honorable Mark Boughton, Mayor, City of Danbury  
Western Connecticut State University (underlying property owner)

Attachments

NORTH



76'-0"



NOTE:  
STRUCTURAL ANALYSIS  
TO BE DONE BEFORE  
CONSTRUCTION

# COMPOUND LAYOUT PLAN

SCALE: N.T.S.

1



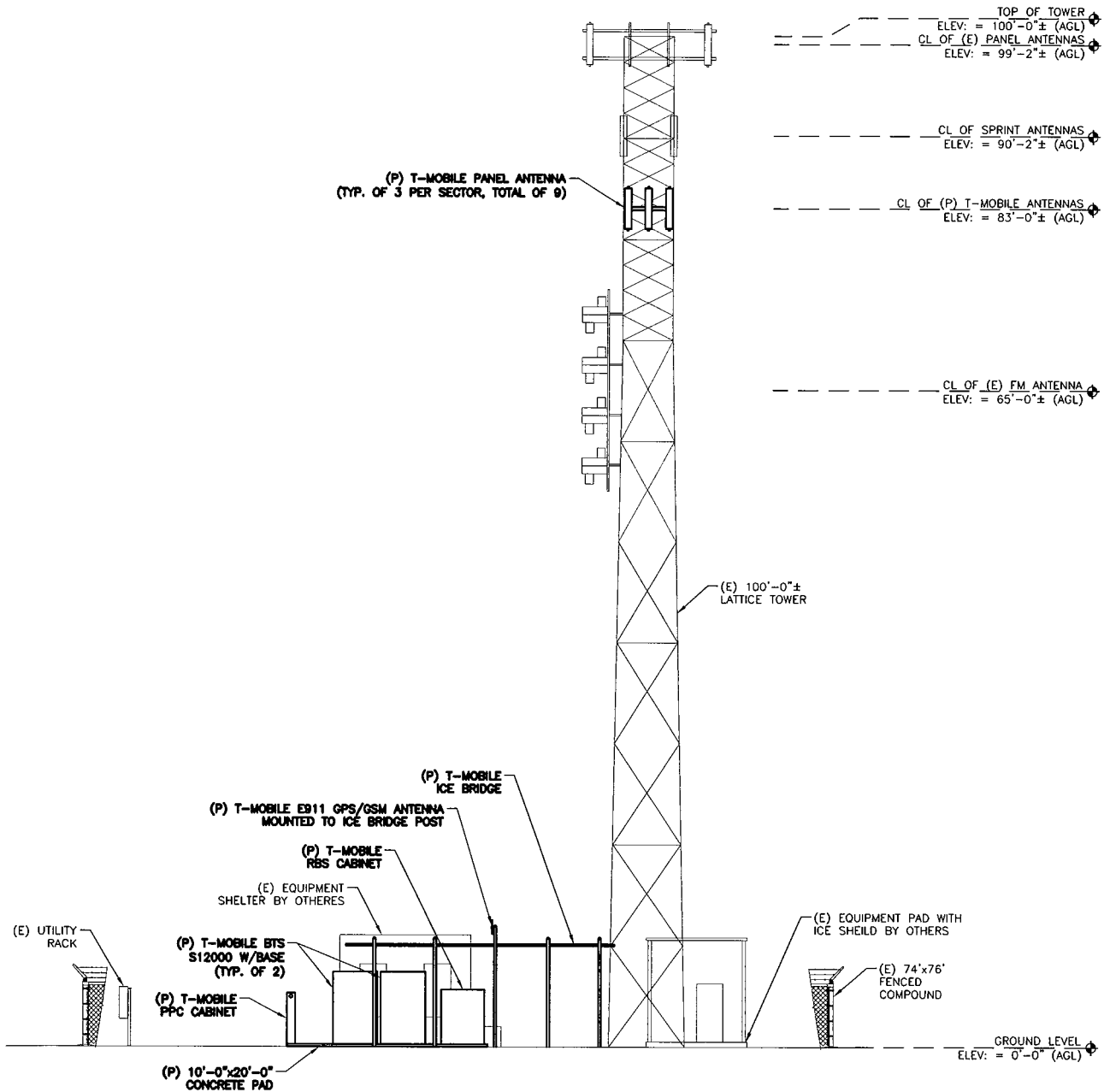
50 Eastman St.  
South Easton, MA 02375  
Phone: (508) 936-6393  
Fax: (508) 936-6395

OMNIPONT COMMUNICATIONS INC.  
A WHOLLY-OWNED SUBSIDIARY  
OF T-MOBILE USA, INC.  
35 GRIFFIN ROAD SOUTH  
BLOOMFIELD, CT 06002  
OFFICE: (860)-692-7100  
FAX: (860)-692-7159

PROJECT LOCATION:  
WCSU  
**CTFF703A**  
303 BOXWOOD LN  
DANBURY, CT. 06810  
APPROVED BY:

SITE TYPE:  
LATTICE TOWER  
PROJECT MANAGER:  
JT  
DATE:  
11/03/08  
DRAWN BY:  
PN  
REVISION:  
3

BSDA PROJ. #:  
2806.122  
SHEET:  
**LE-1**



# ELEVATION

SCALE: N.T.S.

1



50 Eastman St.  
 South Easton, MA 02375  
 Phone: (508) 936-6393  
 Fax: (508) 936-6395

OMNIPPOINT COMMUNICATIONS INC.

A WHOLLY-OWNED SUBSIDIARY  
 OF T-MOBILE USA, INC.  
 35 GRIFFIN ROAD SOUTH  
 BLOOMFIELD, CT 06002  
 OFFICE: (860)-692-7100  
 FAX: (860)-692-7159

PROJECT LOCATION:  
 WCSJ  
**CTFF703A**  
 303 BOXWOOD LN  
 DANBURY, CT. 06810

APPROVED BY:

SITE TYPE:  
 LATTICE TOWER

PROJECT MANAGER:  
 JT

DRAWN BY:  
 PN

DATE:  
 11/03/08

REVISION:  
 3

BSDA PROJ. #:  
 2806.122

SHEET:

LE-2

**Structural Analysis Report**

*100' Existing Self Support Lattice Tower*

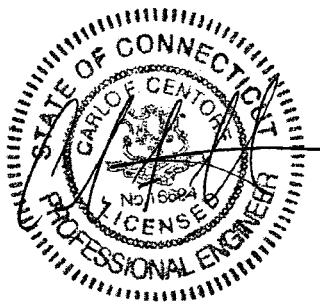
*Proposed T-Mobile Antenna Installation*

*T-Mobile Site Ref: CTFF703*

*303 Boxwood Lane,  
Danbury, CT*

*CEN TEK Project No. 10106*

*Date: July 22, 2010*



**Prepared for:**  
*T-Mobile Towers  
4 Sylvan Way  
Parsippany, NJ 07054*

## Introduction

The purpose of this report is to summarize the results of the non-linear, P- $\Delta$  structural analysis of the antenna installation proposed by T-Mobile on the existing self supporting lattice tower located in Danbury, Connecticut.

The host tower is a 100-ft, three-legged self-support lattice tower originally designed and manufactured by Fred A. Nudd Corporation; file no: 96-4992 signed and sealed January 21, 1997. Subsequent reinforcement and partial member replacement was designed by Centek (formerly Natcomm LLC); job no. 361A and is depicted in design drawing S-1, Revision #4, dated November 28, 2001. The tower geometry, structure member sizes and the foundation system information were taken from the aforementioned design documents. Antenna and appurtenance information were obtained from a comparison of the design documents and field documentation conducted by Centek during June 2010.

The tower is made up of five (5) steel sections consisting of A500-42, A500-50, and A500-61ksi pipe legs. Diagonal lateral support bracing consists of A36 single angle and steel rod construction. The vertical tower sections are connected by bolted flange plates while the pipe legs and bracing are connected by welded (0'-40'), bolted and welded gusset connections (40'-100'). The tower face width is 7.5-ft at the bottom tapering to 3.5-ft at the top.

The aforementioned design report prepared by Fred A. Nudd Corporation and subsequent reinforcement by Natcomm LLC; together with an RF data sheet provided by T-Mobile is available for reference in Section 4 of this report.

T-Mobile proposes the installation of three (3) RFS APX16DWV-16DWV panel antennas and six (6) TMA's mounted to the existing tower. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna configuration

## Antenna and Appurtenance Summary

The existing tower was designed to support several communication antennas. The existing, proposed and future loads considered in this analysis consist of the following:

- **Sprint/Nextel (Existing):**  
Antennas: (8) DB844H90, (2) 5' Unknown Panels, and (2) 6' Unknown Panel antennas mounted to (3) 12' Nudd Starmount Sector Frames with a RAD center elevation of 98-ft above the existing tower base.  
Coax Cables: Sixteen (16) 7/8"  $\varnothing$  coax cables and six (6) 1 5/8"  $\varnothing$  coax cables.
- **Unknown (Existing):**  
Antennas: (1) 3' parabolic grid antenna with a RAD center elevation of 96-ft above the existing tower base.  
Coax Cables: One (1) 1/2"  $\varnothing$  coax cable.



- **Sprint/Nextel (Existing):**  
Antennas: (2) 4' Unknown Panels and (1) 6' Panel antennas flush mounted to the tower legs with a RAD center elevation of 89-ft above the existing tower base.  
Coax Cables: Six (6) 1 5/8" Ø coax cables.
- **WCSU FM (Existing):**  
Antennas: (1) 4-Bay Shively Labs 6810 FM Antenna w/Radomes with a RAD center elevation of 65-ft above the existing tower base.  
Coax Cables: One (1) 1 5/8" Ø coax cable.
- **Sprint/Nextel (Existing):**  
Antennas: (1) GPS antenna mounted to a 2' standoff mount with a RAD center elevation of 30-ft above the existing tower base.  
Coax Cables: One (1) 1/2" Ø coax cable.
- **T-Mobile: (Proposed):**  
Antennas: **Three (3) RFS APX16DWV-16DWVS panel antennas and six (6) RFS Twin TMA's flush mounted to the tower legs with a RAD center elevation of 83-ft above the existing tower base.**  
Coax Cables: **Twelve (12) 1 5/8" Ø coax cables.**

### Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- **All coax cables shall be routed as specified on in Section 3 of this report.**

## A n a l y s i s

The existing tower was analyzed using a comprehensive computer program entitled RISATower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower legs, and the model assumes that the leg members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for 85 mph basic wind speed (fastest mile) with no ice and 74mph with ½ inch accumulative ice to determine stresses in members as per guidelines of the TIA/EIA-222-F-96 entitled "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures", the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

## T o w e r L o a d i n g

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of ½" radial ice tower structure and its components.

Basic Wind Speed:	Fairfield County; v = 85 mph (fastest mile)	[Section 16 of TIA/EIA-222-F-96]
	Danbury; v = 95 mph (3 second gust) equivalent to v = 77.5 mph (fastest mile) <i>TIA/EIA-222-F wind speed controls</i>	[Appendix K of the 2005 CT Building Code Supplement]
Load Cases:	<u>Load Case 1</u> ; 85 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation. This load case typically controls the design of monopole towers.	[Section 2.3.16 of TIA/EIA-222-F-96]
	<u>Load Case 2</u> ; 74 mph wind speed w/ ½" radial ice plus gravity load – used in calculation of tower stresses. This load case typically controls the design of lattice towers.	[Section 2.3.16 of TIA/EIA-222-F-96]
	<u>Load Case 3</u> ; Seismic – not checked	[Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type

## Tower Capacity

Tower stresses were calculated utilizing the structural analysis software RISATower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

- With the reinforcements outlined in section 3 of this report the calculated stresses **were found** to be within allowable limits. In Load Case 2, per RISATower "Section Capacity Table", this tower was found to be at **97.7%** of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Leg (T4)	40'-53.33'	96.7%	PASS
Diagonal (T2)	60'-80'	94.5%	PASS
Horizontal (T1)	80'-100'	97.7%	PASS

## Foundation and Anchors

The existing foundation consists of three (3) 2.0-ft  $\varnothing$  x 4.25-ft long reinforced concrete piers on a 14.5-ft square x 3-ft thick reinforced concrete pad bearing directly on existing sub grade. The existing foundation dimensions and sub-grade conditions used in the analysis of the existing foundation were obtained from the aforementioned manufacturers original design documents; Fred A. Nudd Corporation; file no: 96-4992. Tower legs are connected to the foundation by means of (4) 1.5"  $\varnothing$ , ASTM A36 anchor bolts per leg, embedded into the concrete foundation structure.

Review of the foundation and anchor design consisted of verification of applied loads obtained from the tower design calculations and code checks of allowable stresses:

- The tower leg reactions developed from the governing Load Case 2 of the proposed reinforced tower condition were used in the verification of the foundation and anchor bolts:

Leg Reactions	Vector	Proposed Load (kips/ft-kips)
Leg	Shear	12.1
	Compression	171.2
	Uplift	141.3
Tower Base	Overturning Moment	1058.3

- The anchor bolts were found to be within allowable limits.

Tower Section	Component	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Tension	77.0%	PASS

- The foundation was **NOT** found to be within allowable limits.

Foundation	Design Limit	IBC 2003/2005 CT State Building Code Section 3108.4.2 (FS) <sup>(2)</sup>	Proposed Loading (FS) <sup>(2)</sup>	Result
Reinf. Conc. Pad and Pier	OM <sup>(1)</sup>	2.00	1.76	FAIL

Note 1: OM denotes Overturning Moment

Note 2: FS denotes Factor of Safety

- The foundation resists over one and a half times the calculated wind load, but not two times per the requirements of Section 3108.4.2 of the 2009 CT State Building Code Supplement to the 2003 International Building Code (IBC).

### Conclusion

This analysis indicates that the subject self support steel tower **is adequate** to support the proposed antenna installation, with the proposed reinforcements outlined on drawings S-1 thru S-2, within section 3 of this report, with the exception of the existing foundation (see below).

#### Exceptions: - Existing Foundation:

- It is recommended that T-Mobile apply for a code modification from the office of the Connecticut State Building Inspector requesting a modification to the factor of safety to resist overturning from 2.0x as stipulated by Section 3108.4.2 of the 2009 CT State Building Code Supplement to the 2003 International Building Code (IBC) to 1.5x; as applicable at the time of the original design of the tower structure. Should a modification not be approved by the local official, foundation reinforcements involving a geo-technical study and anchorage design for the existing foundation will be necessary in addition to the tower reinforcements proposed herein.

The analysis is based, in part, on the information provided to this office by T-Mobile. If the existing conditions are different than the information in this report, CENTEK Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

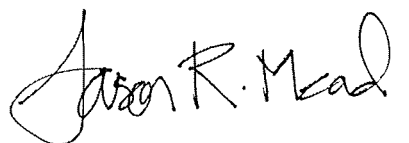
Respectfully Submitted by:



Carlo F. Centore, PE  
 Principal ~ Structural Engineer



Prepared by:



Jason R. Mead  
 Structural Engineer

CENTEK Engineering, Inc.  
Structural Analysis – 100' Self Support Lattice Tower  
T-Mobile Antenna Installation – CTFF703  
Danbury, CT  
July 22, 2010

Standard Conditions for Furnishing of  
Professional Engineering Services on  
Existing Structures

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of CENTEK engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provide to CENTEK engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. CENTEK engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

CENTEK Engineering, Inc.  
Structural Analysis – 100' Self Support Lattice Tower  
T-Mobile Antenna Installation – CTFF703  
Danbury, CT  
July 22, 2010

## General Description of Structural Analysis Program

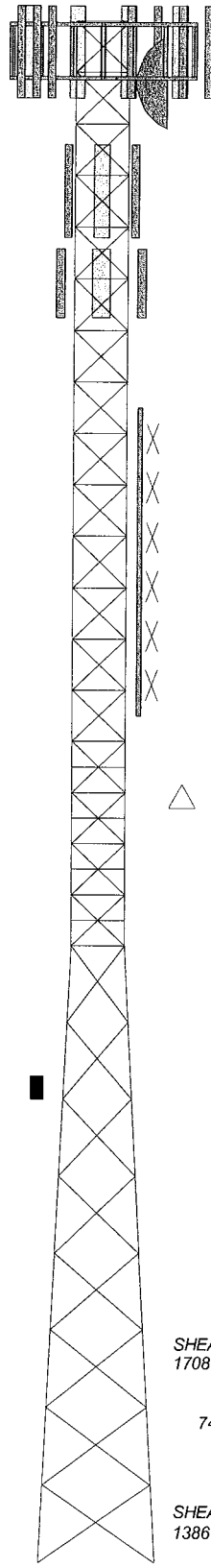
RISATower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, RISATower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

### RISATower Features:

- RISATower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- RISATower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.

Section	T1	T2	T3	T4	T5	T6
Legs	P2.5x276	P2.5x276 (GR)	P3x3 (GF)	P5x375 (GR)	P5x375 (GR)	P5x375 (GR)
Leg Grade	A500-50	A500-50	A500M-61	A500-42	A500-42	A500-42
Diagonals	SR 5/8	SR 5/8	SR 3/4	SR 3/4	L2x2x3/16	L2 1/2x2 1/2x3/16
Diagonal Grade			A36	A36		
Top Girts	L1 1/2x1 1/2x3/16		2L1 1/2x1 1/2x3/16	2L1 1/2x1 1/2x3/16	N.A.	N.A.
Bottom Girts	L1 1/2x1 1/2x3/16		2L1 1/2x1 1/2x3/16	2L1 1/2x1 1/2x3/16	N.A.	N.A.
Horizontals					N.A.	N.A.
Sec. Horizontals					N.A.	N.A.
Face Width (ft)					5.5	5.5
# Panels @ (ft)			2 @ 3.335	4 @ 3.325	8 @ 5	8 @ 5
Weight (lb)	754.8	1132.7	566.6	1357.0	2762.6	2993.6

100.0 ft  
80.0 ft  
60.0 ft  
53.3 ft  
40.0 ft  
20.0 ft  
0.0 ft



### DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
12' Boom Stairmount (Sprint Nextel)	98	APX16PV-16PVL-X w/mount pipe (T-Mobile - proposed)	83
12' Boom Stairmount (Sprint Nextel)	98	APX16PV-16PVL-X w/mount pipe (T-Mobile - proposed)	83
12' Boom Stairmount (Sprint Nextel)	98	APX16PV-16PVL-X w/mount pipe (T-Mobile - proposed)	83
(4) DB844H90 (Sprint Nextel)	98	(2) ATMAA1412D-1A20 Twin TMA (T-Mobile - proposed)	80
(2) 60"x12"x4" Panel (Sprint Nextel)	98	(2) ATMAA1412D-1A20 Twin TMA (T-Mobile - proposed)	80
72" x 10" x 5" Panel (Sprint Nextel)	98	(2) ATMAA1412D-1A20 Twin TMA (T-Mobile - proposed)	80
72" x 10" x 5" Panel (Sprint Nextel)	98	(2) ATMAA1412D-1A20 Twin TMA (T-Mobile - proposed)	80
Parabolic Grid	96	4-Bay 6810 w/Radome	65
72" x 10" x 5" Panel w/mount pipe (Sprint)	89	2.5" Tube x 2' Standoff (Sprint)	30
48"x6.5"x3" Panel w/mount pipe (Sprint)	89	GPS (Sprint)	30
48"x6.5"x3" Panel w/mount pipe (Sprint)	89		
APX16PV-16PVL-X w/mount pipe (T-Mobile - proposed)	83		

### MATERIAL STRENGTH

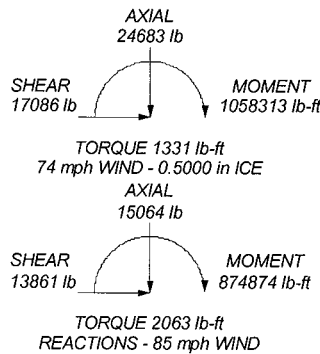
GRADE	Fy	Fu	GRADE	Fy	Fu
A500-50	50 ksi	62 ksi	A500M-61	61 ksi	75 ksi
A36	36 ksi	58 ksi	A500-42	42 ksi	58 ksi

### TOWER DESIGN NOTES

1. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
2. Tower is also designed for a 74 mph basic wind with 0.50 in ice.
3. Deflections are based upon a 50 mph wind.
4. Grouted pipe fc is 8 ksi
5. TOWER RATING: 97.7%

#### MAX. CORNER REACTIONS AT BASE:

DOWN: 171165 lb  
UPLIFT: -141345 lb  
SHEAR: 12062 lb



**CEN TEK Engineering, Inc.**

63-2 N Branford Rd  
Branford, CT 06405  
Phone: (203) 488-0580  
FAX: (203) 488-8587

Job: **100' Nudd Self-Support Lattice ~ w/ Reinf.**

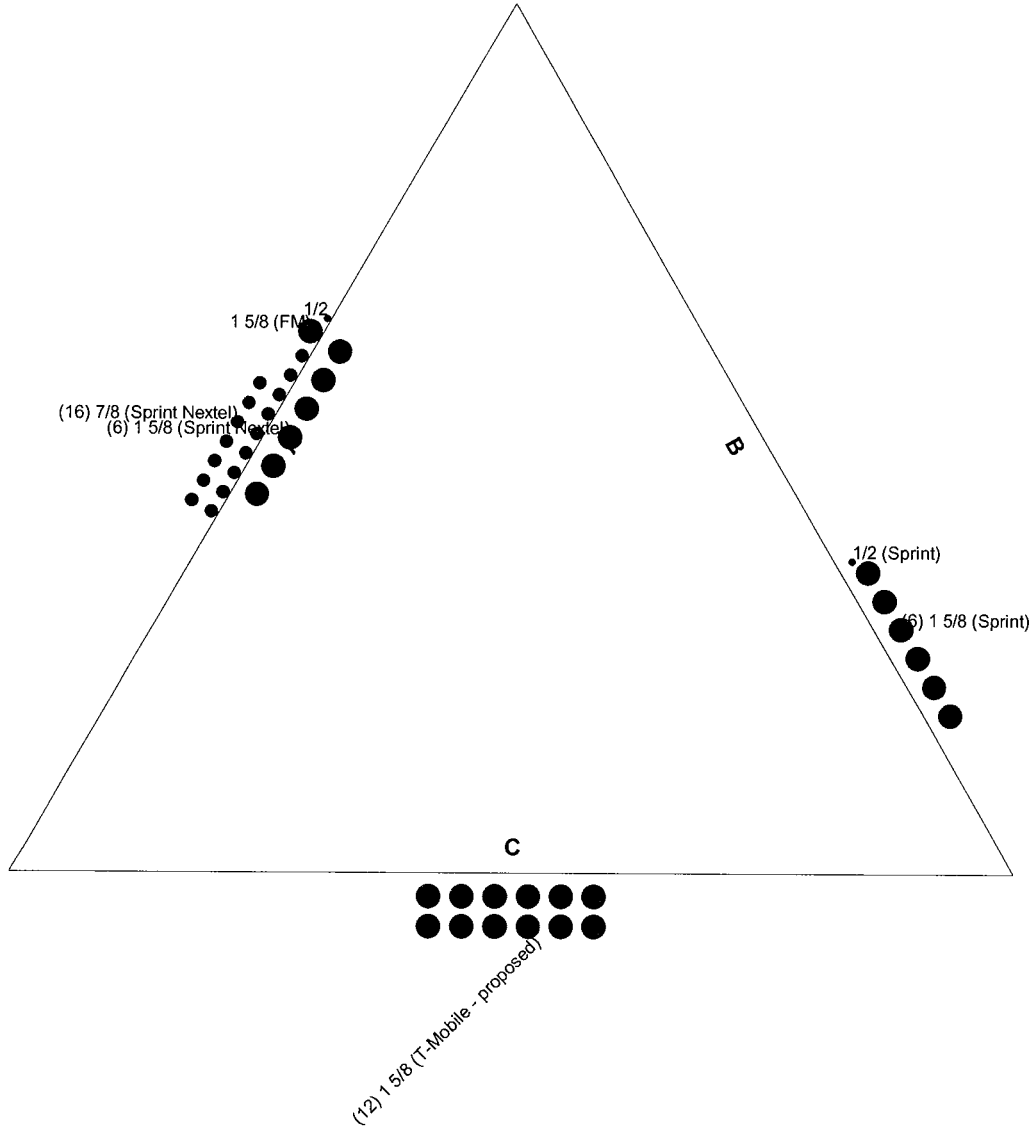
Project: **303 Boxwood Lane, Danbury, CT**

Client: **T-Mobile - CTF703A** Drawn by: **Staff** App'd:

Code: **TIA/EIA-222-F** Date: **07/22/10** Scale: **NTS**

Path:  Dwg No. **E-1**

# Feedline Plan



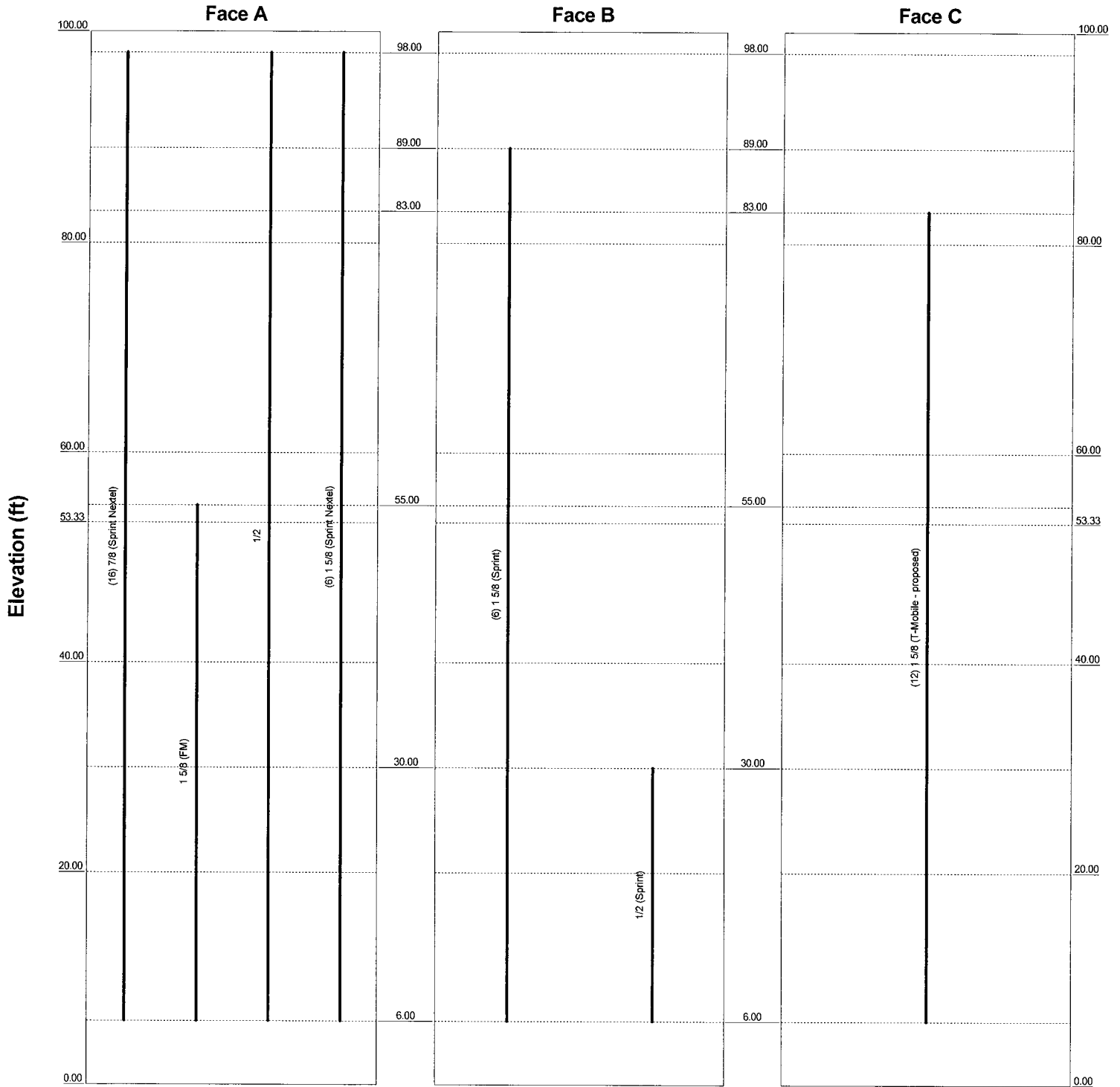
<b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job: <b>100' Nudd Self-Support Lattice ~ w/ Reinf.</b>		
	Project: <b>303 Boxwood Lane, Danbury, CT</b>		
	Client: <b>T-Mobile - CTFF703A</b>	Drawn by: <b>Staff</b>	App'd:
	Code: <b>TIA/EIA-222-F</b>	Date: <b>07/22/10</b>	Scale: <b>NTS</b>
	Path:		Dwg No. <b>E-7</b>



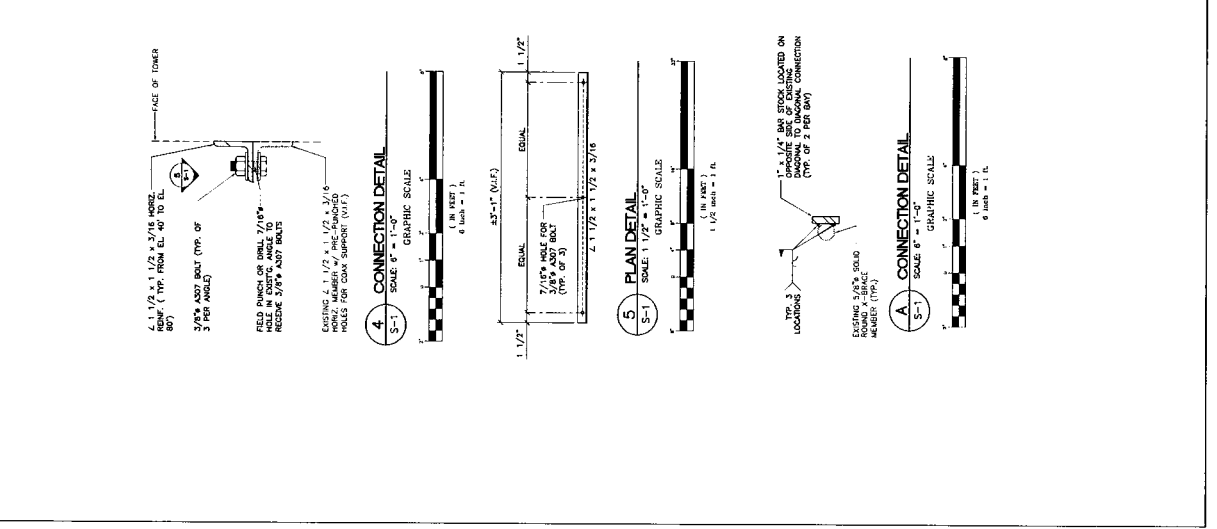
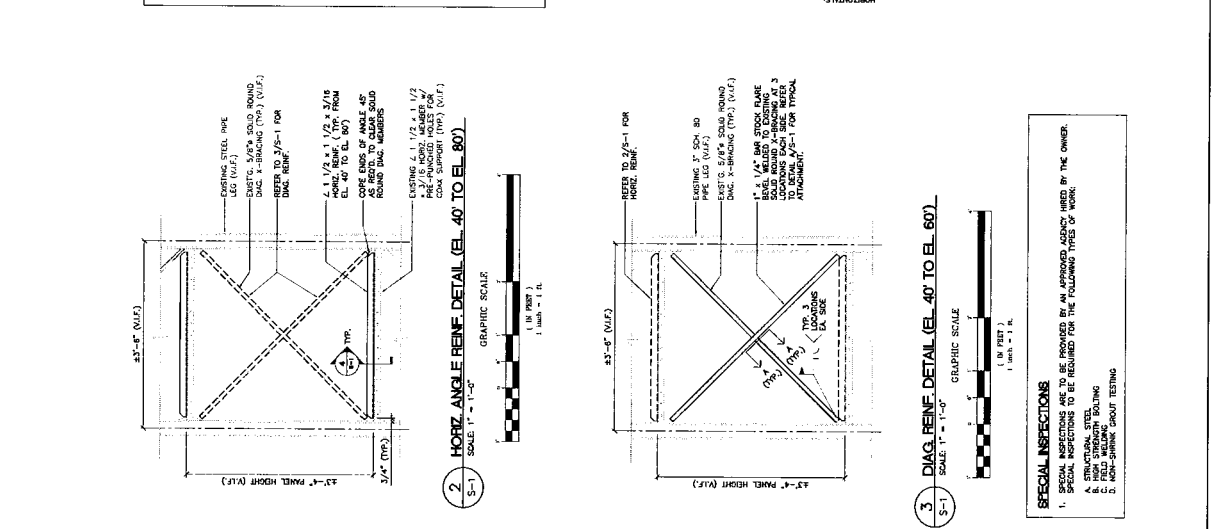
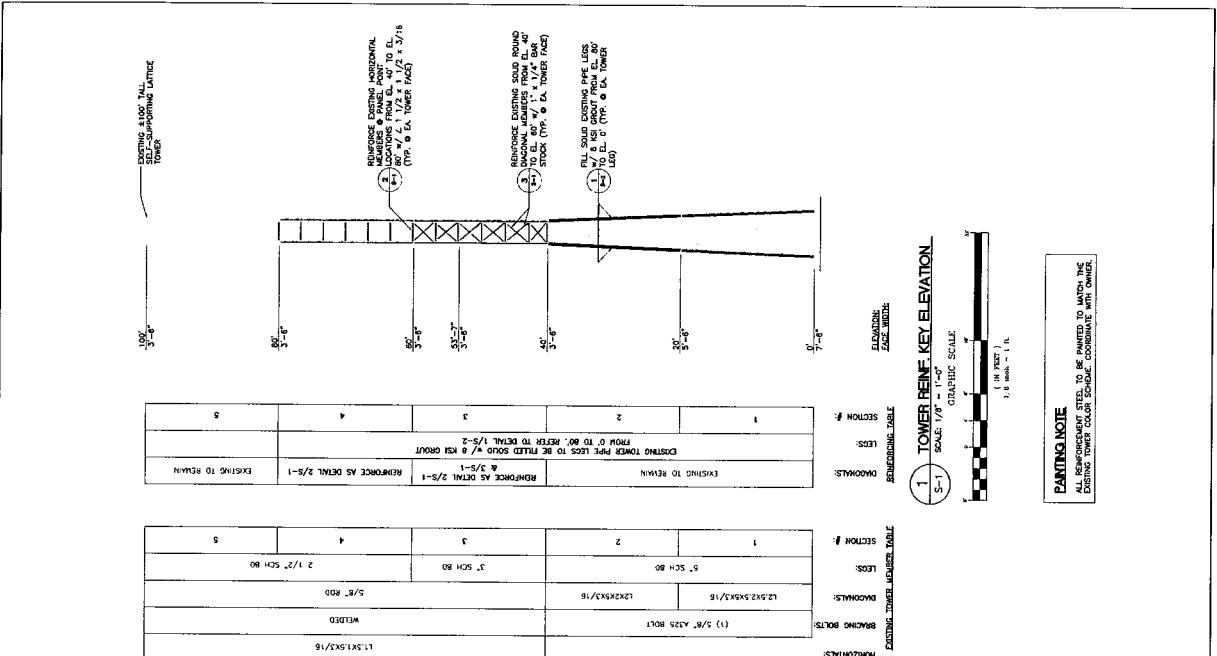
# Feedline Distribution Chart

## 0' - 100'

Round   
  Flat   
  App In Face   
  App Out Face   
  Truss Leg



<b>CEN TEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Job: 100' Nudd Self-Support Lattice ~ w/ Reinf.</b>		
	Project: 303 Boxwood Lane, Danbury, CT		
	Client: T-Mobile - CTFF703A	Drawn by: Staff	App'd:
	Code: TIA/EIA-222-F	Date: 07/22/10	Scale: NTS
	Path:	Dwg No. E-7	



**PAINTING NOTE**  
 ALL REINFORCEMENT STEEL TO BE PAINTED TO MATCH THE EXISTING TOWER COLOR SCHEME. COORDINATE WITH OWNER.

**SPECIAL INSPECTIONS**  
 SPECIAL INSPECTIONS ARE TO BE PROVIDED BY AN APPROVED AGENCY HIRED BY THE OWNER.  
 1. SPECIAL INSPECTIONS TO BE REQUIRED FOR THE FOLLOWING TYPES OF WORK:  
 A. REINFORCING BAR PLACEMENT  
 B. WELDING  
 C. JOINT-BRANDING JOINT TESTING



**Tower Loading Conditions**

Antenna	Elevation	Windload	Deadload
1 642 Starburst	100	1076	513
2 12' Boom	100	411	142
1 2' Shively 6B10	87	187	433
1 without radon	87	425	433

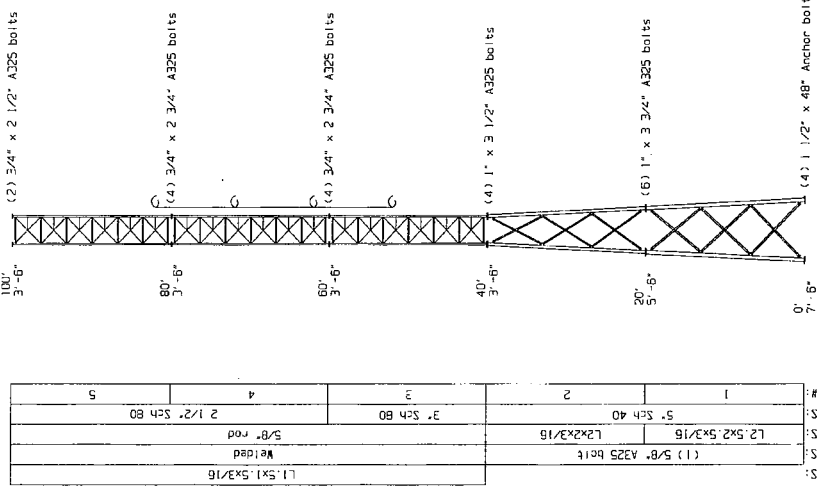
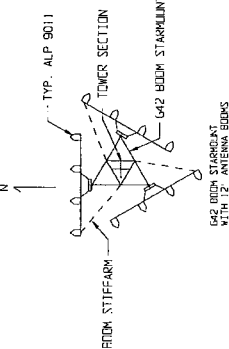
DTY	Type	Elevation	Start	Stop	Windload	Deadload
1	1-5/8" Helix	10	10	87	4.20	2.400
1	1-5/8" Helix	10	87	87	4.20	2.400

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

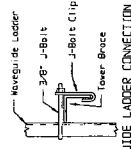
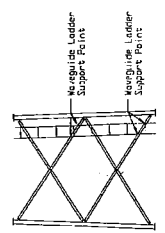
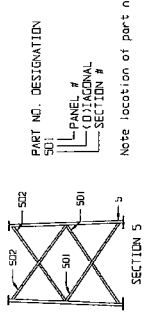
**TOWER DESIGN CONDITIONS**  
 This tower was designed to resist .85 mph wind speed with 1/2" radius ice per ANSI/EIA/TIA 222-F recommended standard. Maximum wind speed is 110 mph. Maximum ice thickness is 1/2".  
 Allowable steel stresses per AISI ASD 9th Edition  
 Allowable concrete stresses per ACI 318-88

**MATERIAL SPECIFICATIONS**  
 Tower Legs: ASTM A500, Section 3, Fy = 50 ksi  
 All other steel: ASTM A36, Fy = 36 ksi  
 Hardware: A325 Hex Dipped Galvanized Bolts with Acro Nuts  
 Galvanizing: ASTM A535, Fy > 36 ksi  
 Anchor Bolts: ASTM A36, Fy > 36 ksi

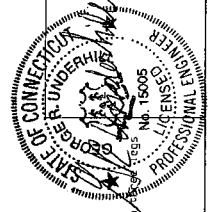
**ANTENNA INSTALLATION NOTES:**  
 1. Azimuth locations per Heros/Mucione  
 2. Initial antenna installation: (G) ALP 9011 (I) Shively 6B10



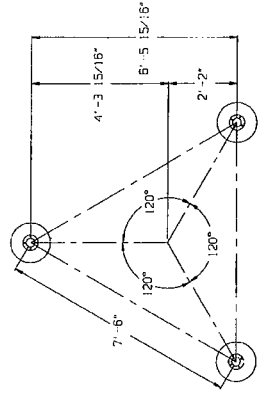
SECTION #	HEIGHT	FLANGE BOLTS
1	5'-5 3/4"	2 L2x2x3/16
2	5'-5 3/4"	2 L2x2x3/16
3	3'-5 3/4"	2 L2x2x3/16
4	2'-1 1/2"	2 L2x2x3/16
5	3'-6"	2 L2x2x3/16



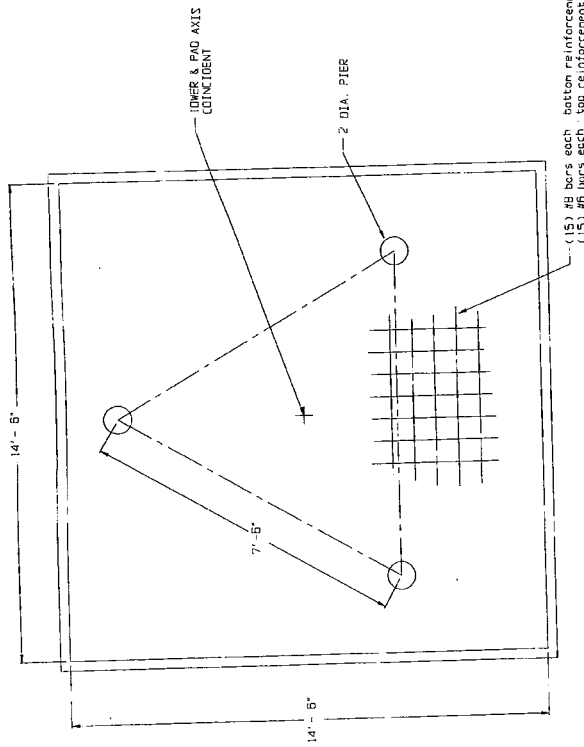
**WAVEGUIDE LADDER CONNECTION**  
 APPROX. TOWER SECTION WEIGHTS (lb):  
 Section 5 : 802 +/-  
 Section 4 : 802 +/-  
 Section 3 : 802 +/-  
 Section 2 : 1251 +/-  
 Section 1 : 1411 +/-  
 Total Tower Weight: 5256 +/-



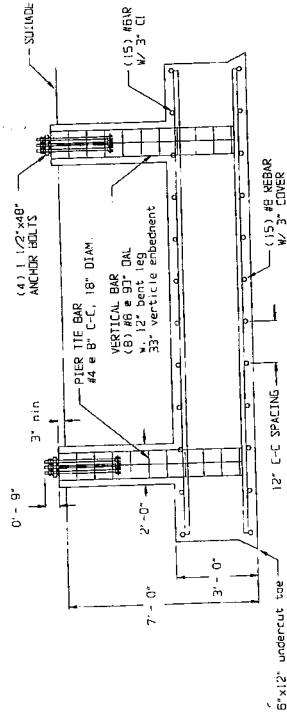
CT43XC836  
 FOUNDATION LAYOUT



FRED A. NUDD CORPORATION  
 Route 104-Ontario, New York 14519-2515/2524-2531  
 SCALE: N/S  
 DATE: 1/21/97  
 DRAWN BY: PEB  
 CHECKED BY: PEB  
 PROJECT: 100' S128PA CELLULAR TOWER  
 NEXTEL  
 WEST CONNECTICUT STATE UNIV.  
 DRAWING NUMBER: 90-4952-1



(15) #8 bars each bottom reinforcement  
 (15) #8 bars each top reinforcement



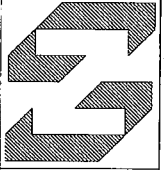
**CONCRETE SPECIFICATIONS**

- Concrete shall have a minimum compressive strength of at least 4000 psi at 28 days. It is our recommendation that 4000 psi concrete be used. If any other concrete is used, the contractor shall submit test results to the Engineer's Office for approval. Certified compression test results must be submitted to the Engineer's Office prior to site acceptance.
- Concrete installation shall meet ACT 318-B9 concrete requirements for reinforced concrete.
- All concrete shall be placed against undisturbed soil free of free standing water and all foreign objects and materials. If this is not required, special pouring procedures will be required.
- Minimum concrete cover shall be 3" over all reinforcing bars.
- Reinforcing bars shall be ASTM A-615 Grade 60.
- Assemble bars with tie wires.
- Proportion pouring: 80% 1's and 2's, 20% 1's only for finishing.

**SOIL SPECIFICATIONS**

- Soil is assumed to be per Vector Eng. boring logs dated 9/3/94.
- Per observation of the boring logs, undisturbed samples at below grade shall be taken to a minimum 10,000 psf (local fill layer) with subgrade reaction of 2,000 kips/cu. ft at bottom of concrete pad.
  - Reinforcing bars shall be free of free standing water and shall be kept prior to pouring concrete and shall be kept until backfill is in place. If not possible, special pouring procedures must be followed.
  - Soils are not to be disturbed or submerged.
  - See EIA 7.2.2.
  - Backfill shall be compacted to 100 pcf.
  - Soil fill shall be placed in layers to prevent accumulation of water around foundation and anchors.

Total Concrete: 25 Cuyd  
 Template Flange: 50C1

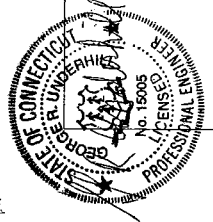


**FRED A. NUDD CORPORATION**  
 Route 104-Danbar, New York 14519-315/924-2531

SCALE: N/A	DATE: 1/21/97	DESIGNER: PEB
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FOUNDATION DETAILS

NEXTEL  
 WEST CONNECTICUT ST., CT  
 96-4992-2



**TOWER STRUCTURAL NOTES**

TOWER DESIGN CRITERIA  
 THIS TOWER IS DESIGNED AND REINFORCED TO RESIST 85 MPH WIND SPEED AND 1/2" ALLOWABLE STEEL STRESS PER AISC AND WITH 100% WIND LOADS.  
 MATERIAL SPECIFICATIONS (FOR EXISTING TOWER) PER ORIGINAL DRAWING  
 TOWER LEGS:  
 ASTM A36; ALL OTHER SECTIONS 91 92  
 ANCHOR BOLTS:  
 ANCHOR BOLTS: 7/8" x 35 1/2"  
 ALL OTHER STEEL:  
 ANCHOR BOLTS: 7/8" x 35 1/2"  
 GALVANIZING:  
 GALVANIZING: ZINC RICH

TOWER LEGS:  
 ANCHOR BOLTS: 7/8" x 35 1/2"  
 MATERIAL SPECIFICATIONS (FOR IMPROVED REINFORCEMENT UP TOWER)  
 TOWER LEGS:  
 ANCHOR BOLTS: 7/8" x 35 1/2"  
 ANCHOR BOLTS: 7/8" x 35 1/2"  
 ANCHOR BOLTS: 7/8" x 35 1/2"

1. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS WHICH MAY BE REQUIRED FOR THE WORK BY THE STATE, COUNTY OR LOCAL GOVERNMENT AGENCIES.  
 2. CONTRACTOR SHALL MAKE SURE TO OBTAIN ALL NECESSARY PERMITS AND INSPECTIONS FOR THE EXISTING AND NEW CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND INSPECTIONS FOR THE EXISTING AND NEW CONSTRUCTION.  
 3. EXISTING TOWER STRUCTURE SHALL BE REINFORCED PER CONTRACT DRAWINGS.

4. ALL NEW ANTENAS AND COAX LINES SHALL BE INSTALLED PER CONTRACT DRAWINGS.  
 5. STRUCTURAL STEEL SHALL CONFORM TO THE CURRENT TOWER SPECIFICATION FOR THE DESIGN, FABRICATION AND SECTION OF STRUCTURAL STEEL FOR WILLOWDALE, AND THE "AISC CODE OF STANDARDS PRACTICE FOR STEEL."  
 6. ALL WELDING SHALL BE DONE BY A CERTIFIED WELDER IN ACCORDANCE WITH A.A.I.S. STANDARDS.  
 7. CONTRACTOR SHALL SUBMIT TO ALL INSPECTIONS BY THE "AISC INSPECTOR" FOR THE DESIGN, FABRICATION AND SECTION OF STRUCTURAL STEEL FOR WILLOWDALE, AND THE "AISC CODE OF STANDARDS PRACTICE FOR STEEL."  
 8. ALL WELDING SHALL BE DONE BY A CERTIFIED WELDER IN ACCORDANCE WITH A.A.I.S. STANDARDS.  
 9. CONTRACTOR SHALL VERIFY THE SITE PRIOR TO THE START OF WORK WITH SURVEYING RECORDS TO BE RECORDED ON TOWER LEGS USING ASTM A332 OR A333 AND QUALITY CHECK AND INSPECTION RECORDS SHALL BE SUBMITTED FOR ALL STRUCTURAL STEEL WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. SUBMIT 5 SETS OF PRINTS TO THE ENGINEER FOR REVIEW.  
 10. THE STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER THE WORK IS FULLY COMPLETED.  
 11. ALL BEARING ENDS OF COLUMNS, RIFTERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE DURATION.  
 12. EXISTING TOWER STRUCTURE DIMENSIONS WERE TAKEN FROM DRAWING NO. 89-492-1 DATED 08/10/89. CONTRACTOR SHALL VERIFY ALL DIMENSIONS AND MAKE SURE THEY ARE CORRECT BEFORE STARTING WORK. THE FIELD MEASUREMENT SHALL BE SUBMITTED FOR REFERENCE TO THE ENGINEER.  
 13. TOWER REINFORCING SHALL BE CONDUCTED BY CERTIFIED WELDERS AND FIELD CREWS SHALL BE TRAINED AND EXPERIENCED IN ALL ASPECTS OF TOWER REINFORCEMENT. ALL SAFETY PROCEDURES, WORKING AND ERECTION METHODS SHALL BE STANDARD TO THE INDUSTRY AND IN COMPLIANCE WITH OSHA.  
 14. CONTRACTOR SHALL SUBMIT THE METHOD OF CONSTRUCTION AND SECTION FOR REVIEW BY THE ENGINEER PRIOR TO FABRICATION.  
 15. THE CONTRACTOR SHALL CONDUCT AND MAINTAIN AN INDEPENDENT LOGBOOK THROUGHOUT THE PROJECT.  
 16. ALL PROPOSED HORIZONTAL, DIAGONAL BRACING AND GUSSET PLATES MAY BE FIELD REPAIRED AND WELD REPAIRED, EXCEPT AS NOTED.  
 17. ALL REINFORCEMENT SHALL BE TIGHTENED TO SHAP TIGHT CONDITION AS DENIED BY AISC SPECIFICATION UNLESS OTHERWISE NOTED.  
 18. ALL 3/4" BOLTS ARE TO BE TIGHTENED TO SHAP TIGHT CONDITION AS DENIED BY AISC SPECIFICATION UNLESS OTHERWISE NOTED.  
 19. WAREHOLDING DATA SHALL BE 7/8" THICK UNLESS SPECIFICALLY NOTED.  
 20. BOLT HOLES SHALL BE FINISHED OR DRILLED OR MILLER FLAME CUT HOLES ARE NOT ACCEPTABLE.  
 21. ALL REINFORCEMENT SHALL BE APPROVED BY THE ENGINEER AND PAID FOR BY THE CONTRACTOR.  
 22. ALL WELDING SHALL BE DONE USING E70XX ELECTRODES, WHERE FLEET WELD SECS ARE TO BE WELDED TO THE TOWER LEGS. ALL WELDING SHALL BE DONE IN ACCORDANCE WITH AISC SPECIFICATION, 3RD EDITION. AT THE COMPLETION ALL WELDING, ALL DAMAGE TO GALVANIZING SHALL BE REPAIRED.  
 23. TOUCH-UP ALL DAMAGED GALVANIZING WITH ZINC RICH "DOWNEY" TERTIARY ZINC TOUCH-UP GALVANIZING NON GALVANIZED STEEL WITH SAME PAINT APPLIED IN SHOP OR FIELD.  
 24. A SMALL PORTION OF THE GALVANIZING MAY BE OMITTED TO FACILITATE THE WELDING OF THE TOWER LEGS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND INSPECTIONS FOR THE EXISTING AND NEW CONSTRUCTION. REFER TO PARTING NOTES.

25. USE PRECAUTIONS & PROCEDURES PER AISC D11 WHEN WELDING GALVANIZED METALS.  
 26. ALL STEEL WORK SHALL BE GALVANIZED IN ACCORDANCE WITH THE SPECIFICATION ASTM A133 UNLESS OTHERWISE NOTED.  
 27. EXISTING CORRAL CABLES AND WATERSHEDS TO REMAIN WITH TOWER REINFORCEMENT INTERFERENCE IN SERVICE.  
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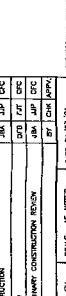
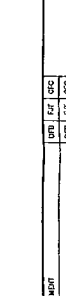
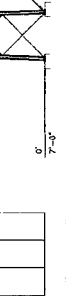
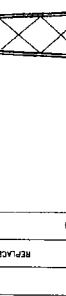
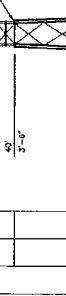
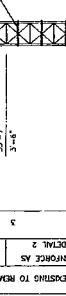
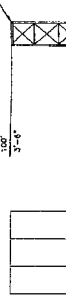
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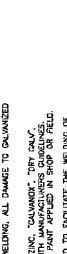
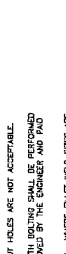
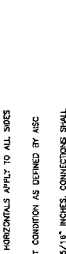
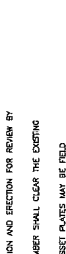
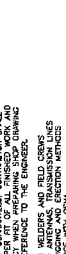
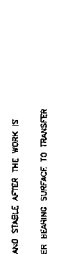
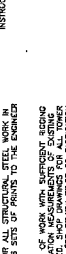
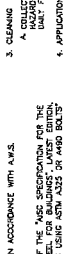
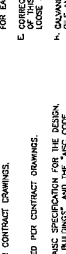
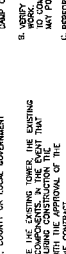
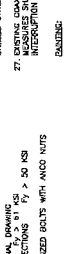
**EXISTING TOWER ELEVATION**



**SECTION #**

SECTION #	DESCRIPTION	DATE
1	REPLACE WITH 5\"/>	
2		
3		
4		
5		

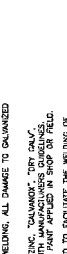
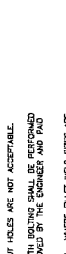
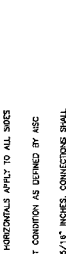
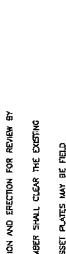
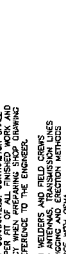
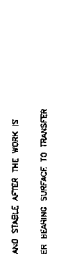
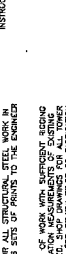
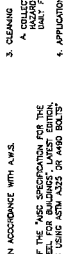
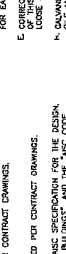
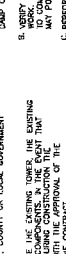
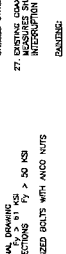
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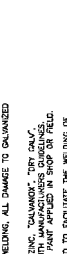
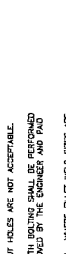
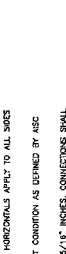
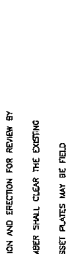
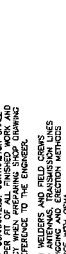
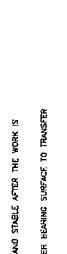
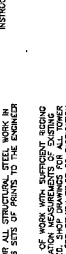
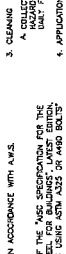
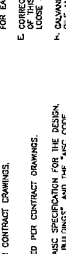
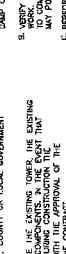
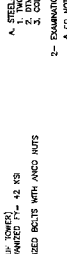
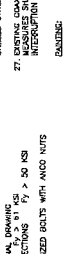
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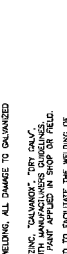
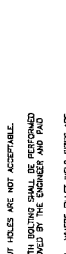
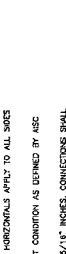
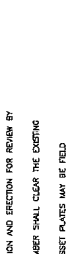
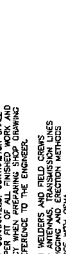
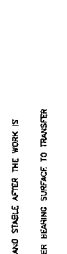
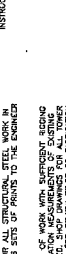
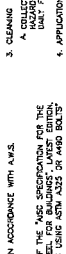
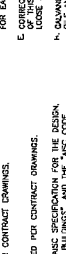
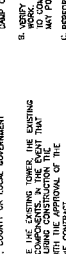
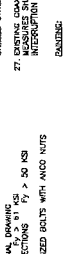
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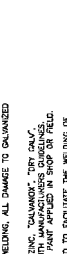
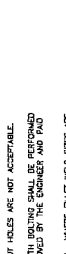
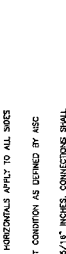
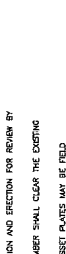
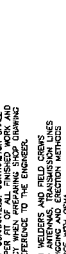
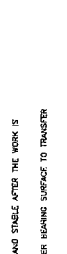
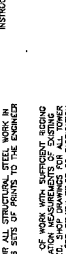
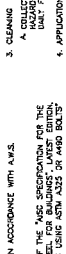
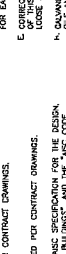
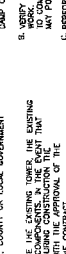
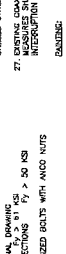
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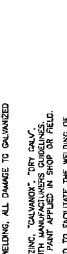
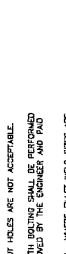
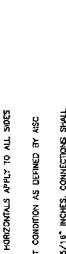
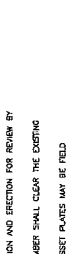
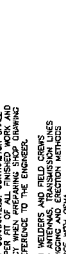
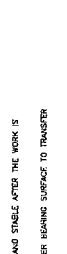
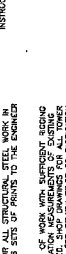
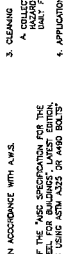
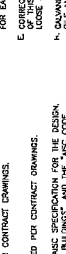
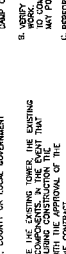
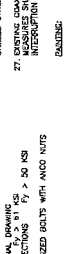
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## Technical Memo

To: Transcend  
From: Amir Uzzaman - Radio Frequency Engineer  
cc: Jason Overbey  
Subject: Power Density Report for CTF703A  
Date: June 11, 2010

### 1. Introduction:

This report is the result of an Electromagnetic Field Intensities (EMF - Power Densities) study for the T-Mobile antenna installation on a Self Support Tower at 303 Boxwood Lane, Danbury, CT. This study incorporates the most conservative consideration for determining the practical combined worst case power density levels that would be theoretically encountered from locations surrounding the transmitting location.

### 2. Discussion:

The following assumptions were used in the calculations:

- 1) The emissions from T-Mobile transmitters are in the (1940-1949.8), (2140-2145), (2110-2120)MHz frequency Band.
- 2) The antenna array consists of three sectors, with 1 antenna per sector.
- 3) The model number of the antennas are APX16DWV-16DWV, APXV18-209014-C, APXV18-209014-C
- 3) The model number for UMTS antenna is APX16DWV-16DWV.
- 4) GSM antenna center line height is 83 ft.
- 4) UMTS antenna center line height is 83 ft.
- 5) The maximum transmit power from any GSM sector is 2565.19 Watts Effective Radiated Power (EIRP) assuming 8 channels per sector.
- 5) The maximum transmit power from any UMTS sector is 2330.72 Watts Effective Radiated Power (EIRP) assuming 2 channels per sector.
- 6) All the antennas are simultaneously transmitting and receiving, 24 hours a day.
- 7) Power levels emitting from the antennas are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 8) The average ground level of the studied area does not change significantly with respect to the transmitting location.

Equations given in "FCC OET Bulletin 65, Edition 97-01" were then used with the above information to perform the calculations.

### 3. Conclusion:

Based on the above worst case assumptions, the power density calculation from the T-Mobile antenna installation on a Self Support Tower at 303 Boxwood Lane, Danbury, CT, is 0.18116 mW/cm<sup>2</sup>. This value represents 18.116% of the Maximum Permissible Exposure (MPE) standard of 1 milliwatt per square centimeter (mW/cm<sup>2</sup>) set forth in the FCC/ANSI/IEEE C95.1-1991. Furthermore, the proposed antenna location for T-Mobile will not interfere with existing public safety communications, AM or FM radio broadcasts, TV, Police Communications, HAM Radio communications or any other signals in the area. The combined Power Density from other carriers is 18.51%. The combined Power Density for the site is 36.626% of the M.P.E. standard.

**Connecticut Market**



**Worst Case Power Density**

Site: **CTFF703A**  
 Site Address: **303 Boxwood Lane**  
 Town: **Danbury**  
 Tower Height: **100 ft.**  
 Tower Style: **Self Support Tower**

GSM Data		UMTS Data	
Base Station TX output	20 W	Base Station TX output	40 W
Number of channels	8	Number of channels	2
Antenna Model	APX16DWV-16DWV	Antenna Model	APX16DWV-16DWV
Cable Size	1 5/8	Cable Size	1 5/8
Cable Length	17.5 ft.	Cable Length	16.0 ft.
Antenna Height	86.0 ft.	Antenna Height	88.0 ft.
Ground Reflection	1.6	Ground Reflection	1.6
Frequency	1945.0 MHz	Frequency	2.1 GHz
Jumper & Connector loss	4.50 dB	Jumper & Connector loss	1.50 dB
Antenna Gain	18.0 dBi	Antenna Gain	18.0 dBi
Cable Loss per foot	0.0116 dB	Cable Loss per foot	0.0116 dB
Total Cable Loss	1.4500 dB	Total Cable Loss	1.8560 dB
Total Attenuation	5.9500 dB	Total Attenuation	3.3560 dB
Total EIRP per Channel (In Watts)	55.06 dBm 320.65 W	Total EIRP per Channel (In Watts)	60.66 dBm 1165.36 W
Total EIRP per Sector (In Watts)	64.09 dBm 2565.19 W	Total EIRP per Sector (In Watts)	63.67 dBm 2330.72 W
nsg	12.0500	nsg	14.6440
Power Density (S) = 0.094920 mW/cm <sup>2</sup>		Power Density (S) = 0.086244 mW/cm <sup>2</sup>	
T-Mobile Worst Case % MPE =		18.1164%	
Equation Used : $S = \frac{(1000)(grf)^2 (Power)^{10}}{4\pi (R)^2}$			
Office of Engineering and Technology (OET) Bulletin 65, Edition 97-01, August 1997			

Co-Location Total	
Carrier	% of Standard
Sprint/Nextel WiMax	6.1900 %
Cingular	
Sprint CDMA	0.0300 %
AT&T Wireless	
Pocket	
MetroPCS	
Nextel iDen	12.2900 %
Other Antenna Systems	
<b>Total Excluding T-Mobile</b>	<b>18.5100 %</b>
T-Mobile	18.1164
<b>Total % MPE for Site</b>	<b>36.6264%</b>