



ORIGINAL

October 26, 2012

**RECEIVED**  
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**CONNECTICUT  
 SITING COUNCIL**
**VIA OVERNIGHT COURIER**

Connecticut Siting Council  
 10 Franklin Square  
 New Britain, Connecticut 06051  
 Attn: Ms. Linda Roberts, Executive Director

Re: New Cingular Wireless PCS, LLC – Exempt Modification  
161 Pinney Street, Colebrook, Connecticut

Dear Ms. Roberts:

This letter and attachments are submitted on behalf of New Cingular Wireless PCS, LLC (“AT&T”). AT&T is making modifications to certain existing sites in its Connecticut system in order to implement LTE technology. Please accept this letter and attachments as notification, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies (“R.S.C.A.”), of construction that constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and attachments is being sent to the First Selectman of the Town of Colebrook.

AT&T plans to modify the existing wireless communications facility owned by Crown Castle and located at 161 Pinney Street, Colebrook (coordinates 41° -57’-58.83” N, 73°-07’-17.98” W). Attached are a compound plan and elevation depicting the planned changes, and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration. Also included is a power density report reflecting the modification to AT&T’s operations at the site.

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes (“C.G.S.”) Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2).

1. AT&T will add three (3) LTE panel antennas, and a Surge Arrestor on new pipe mounts at a centerline height of approximately 140’. Six (6) RRUSs (remote radio units) will be attached to the pole behind the LTE antennas at a centerline height of approximately 138’. AT&T will also place a DC power and fiber run from the equipment

to the antennas along the existing coaxial cable run. These changes will not extend the height of the approximately 148' structure.

2. AT&T will place related equipment in the existing Shelter, and mount a new GPS antenna on the existing Ice Bridge Post. These changes will be within the existing compound and will have no effect on the site boundaries.

3. The proposed changes will not increase the noise level at the existing facility by six (6) decibels or more. The incremental effect of the proposed changes will be negligible.

4. The changes to the facility will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site. As indicated on the attached report prepared by C Squared Systems, LLC, AT&T's operations at the site will result in a power density of approximately 1.64%; the combined site operations will result in a total power density of approximately 27.797%.

Please feel free to contact me by phone at (860) 798-7454 or by e-mail at [jgaudet@hpcwireless.com](mailto:jgaudet@hpcwireless.com) with questions concerning this matter. Thank you for your consideration.

Respectfully yours,

  
Jennifer Young Gaudet (by )

Attachments

cc: Honorable Thomas D. Mckee, First Selectman, Town of Colebrook  
Ellen Fredsall (underlying property owner)







C Squared Systems, LLC  
65 Dartmouth Drive, Unit A3  
Auburn, NH 03032  
(603) 644-2800  
support@csquaredsystems.com

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Calculated Radio Frequency Emissions



CT1012

(Pinney Street)

161 Pinney Street, Colebrook, CT 06098

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October 2, 2012

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## 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed modifications to the existing AT&T antenna arrays mounted on the monopole tower located at 161 Pinney Street in Colebrook, CT. The coordinates of the tower are 41° 57' 58.89" N, 73° 07' 18.06" W.

AT&T is proposing the following modifications:

- 1) Install three multi-band (700/850/1900/2100 MHz) antennas for their LTE network (one per sector).

## 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz. The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter ( $\text{mW}/\text{cm}^2$ ). The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

#### 4. Calculation Results

Table 1 below outlines the power density information for the site. Because the proposed AT&T antennas are directional in nature, the majority of the RF power is focused out towards the horizon. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the tower. Please refer to Attachment C for the vertical patterns of the proposed AT&T antennas. The calculated results for AT&T in Table 1 include a nominal 10 dB off-beam pattern loss to account for the lower relative gain below the antennas.

Carrier	Antenna Height (Feet)	Operating Frequency (MHz)	Number of Trans.	ERP Per Transmitter (Watts)	Power Density (mw/cm <sup>2</sup> )	Limit	%MPE
<i>Cingular GSM</i>	137	880	4	296	0.0227	0.5867	3.87%
<i>Cingular GSM</i>	137	1900	2	427	0.0164	1.0000	1.64%
<i>Cingular UMTS</i>	137	880	1	500	0.0096	0.5867	1.63%
Sprint	147	1962.5	11	250	0.0458	1.0000	4.58%
Verizon PCS	130	1970	7	281	0.0419	1.0000	4.19%
Verizon cellular	130	869	9	305	0.0584	0.5793	10.08%
Verizon AWS	130	2145	1	702	0.0149	1.0000	1.49%
Verizon LTE	130	698	2	636	0.0271	0.4653	5.82%
AT&T UMTS	140	880	2	565	0.0021	0.5867	0.35%
AT&T UMTS	140	1900	2	875	0.0032	1.0000	0.32%
AT&T LTE	140	734	1	1313	0.0024	0.4893	0.49%
AT&T GSM	140	880	1	283	0.0005	0.5867	0.09%
AT&T GSM	140	1900	4	525	0.0039	1.0000	0.39%
						<b>Total</b>	<b>27.79%</b>

**Table 1: Carrier Information**<sup>1 2 3</sup>

<sup>1</sup> The existing CSC filing for Cingular should be removed and replaced with the updated AT&T technologies and values provided in Table 1. The power density information for carriers other than AT&T was taken directly from the CSC database dated 7/26/2012. Please note that %MPE values listed are rounded to two decimal points. The total %MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not reflect the total value listed in the table.

<sup>2</sup> In the case where antenna models are not uniform across all 3 sectors for the same frequency band, the antenna model with the highest gain was used for the calculations to present a worse-case scenario.

<sup>3</sup> Antenna height listed for AT&T is in reference to the Paul J Ford & Company Structural Analysis dated August 14, 2012.

## 5. Conclusion

The above analysis verifies that emissions from the existing site will be below the maximum power density levels as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Even when using conservative methods, the cumulative power density from the proposed transmit antennas at the existing facility is well below the limits for the general public. The highest expected percent of Maximum Permissible Exposure at ground level is **27.79% of the FCC limit**.

As noted previously, obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. As a result, the predicted signal levels are more conservative (higher) than the actual signal levels will be from the finished modifications.

## 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in ANSI/IEEE Std. C95.3, ANSI/IEEE Std. C95.1 and FCC OET Bulletin 65 Edition 97-01.

A handwritten signature in black ink, appearing to read 'Daniel L. Goulet'.

Daniel L. Goulet  
C Squared Systems, LLC

October 2, 2012

Date

### **Attachment A: References**

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering & Technology

ANSI C95.1-1982, American National Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 300 kHz to 100 GHz. IEEE-SA Standards Board

IEEE Std C95.3-1991 (Reaff 1997), IEEE Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave. IEEE-SA Standards Board

**Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)**

**(A) Limits for Occupational/Controlled Exposure<sup>4</sup>**

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm <sup>2</sup> )	Averaging Time  E  <sup>2</sup> ,  H  <sup>2</sup> or S (minutes)
0.3-3.0	614	1.63	(100)*	6
3.0-30	1842/f	4.89/f	(900/f <sup>2</sup> )*	6
30-300	61.4	0.163	1.0	6
300-1500	-	-	f/300	6
1500-100,000	-	-	5	6

**(B) Limits for General Population/Uncontrolled Exposure<sup>5</sup>**

Frequency Range (MHz)	Electric Field Strength (E) (V/m)	Magnetic Field Strength (E) (A/m)	Power Density (S) (mW/cm <sup>2</sup> )	Averaging Time  E  <sup>2</sup> ,  H  <sup>2</sup> or S (minutes)
0.3-1.34	614	1.63	(100)*	30
1.34-30	824/f	2.19/f	(180/f <sup>2</sup> )*	30
30-300	27.5	0.073	0.2	30
300-1500	-	-	f/1500	30
1500-100,000	-	-	1.0	30

f = frequency in MHz \* Plane-wave equivalent power density

**Table 2: FCC Limits for Maximum Permissible Exposure (MPE)**

<sup>4</sup> Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure.

<sup>5</sup> General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

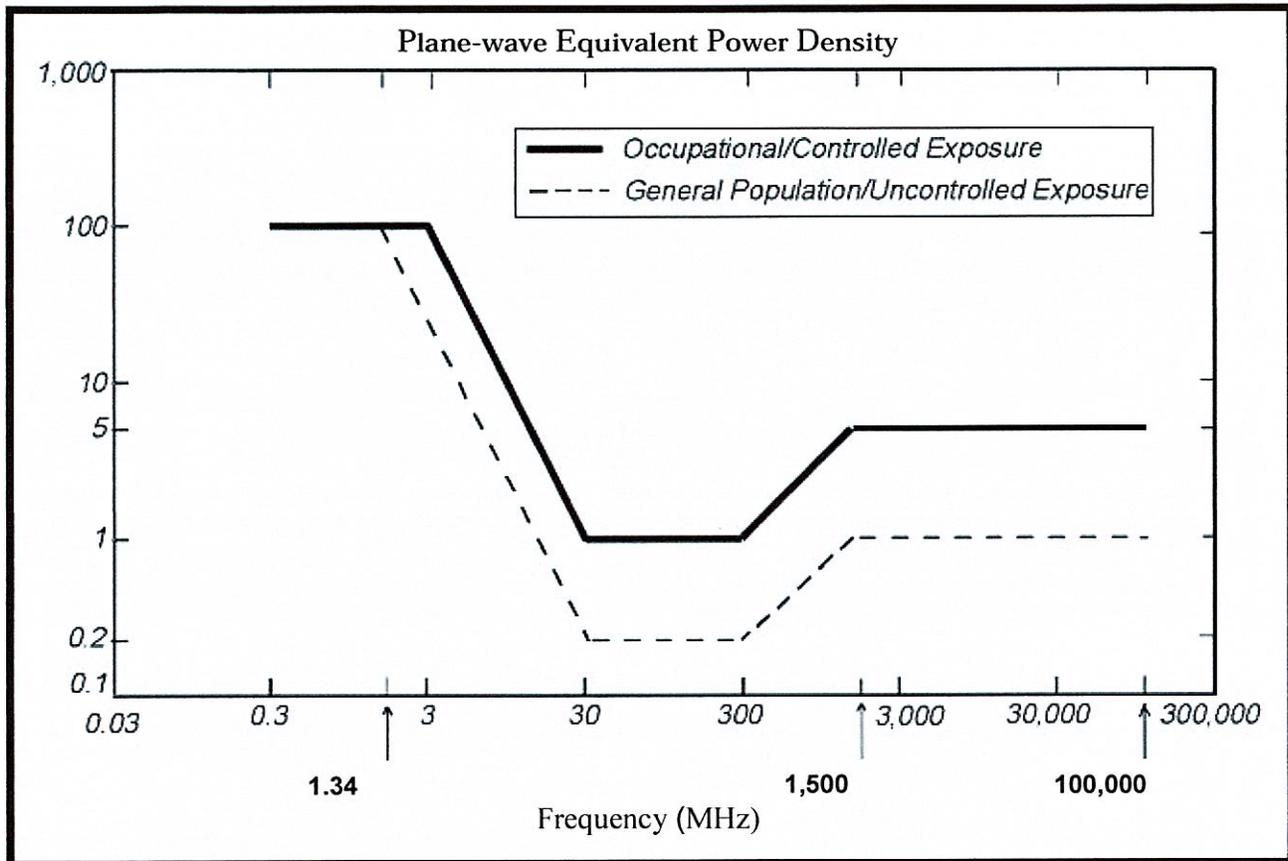
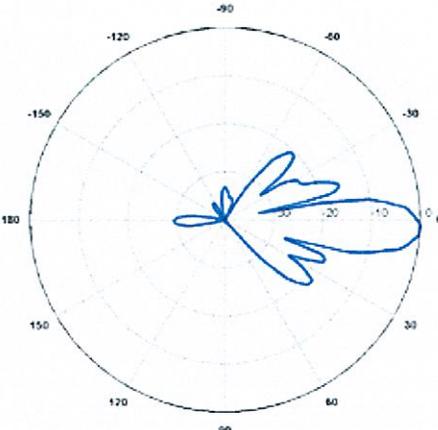
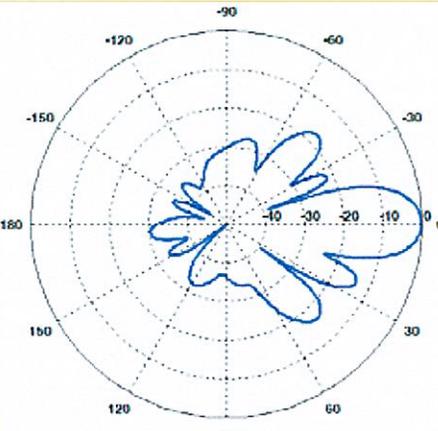
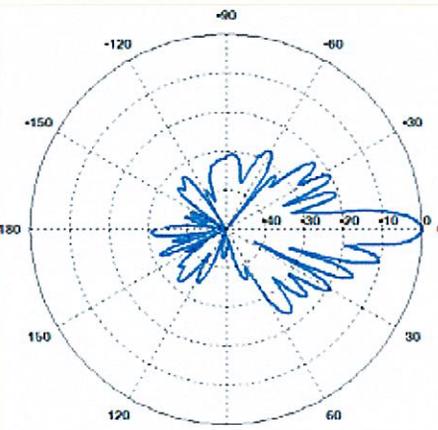


Figure 1: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

**Attachment C: AT&T Antenna Data Sheets and Electrical Patterns**

<p><b>700 MHz</b></p> <p>Manufacturer: KMW            Model #: AM-X-CD-16-65-00T-RET            Frequency Band: 698-806 MHz            Gain: 13.4 dBd            Vertical Beamwidth: 12.3°            Horizontal Beamwidth: 65°            Polarization: Dual Slant <math>\pm 45^\circ</math>            Size L x W x D: 72.0" x 11.8" x 5.9"</p>	
<p><b>850 MHz</b></p> <p>Manufacturer: Powerwave            Model #: 7770.00            Frequency Band: 824-896 MHz            Gain: 11.5 dBd            Vertical Beamwidth: 15°            Horizontal Beamwidth: 82°            Polarization: Dual Linear <math>\pm 45^\circ</math>            Size L x W x D: 55.0" x 11.0" x 5.0"</p>	
<p><b>1900 MHz</b></p> <p>Manufacturer: Powerwave            Model #: 7770.00            Frequency Band: 1850-1990 MHz            Gain: 13.4 dBd            Vertical Beamwidth: 7°            Horizontal Beamwidth: 86°            Polarization: Dual Linear <math>\pm 45^\circ</math>            Size L x W x D: 55.0" x 11.0" x 5.0"</p>	

### 3. RF Exposure Prediction Methods

The emission field calculation results displayed in the following figures were generated using the following formula as outlined in FCC bulletin OET 65:

$$\text{Power Density} = \left( \frac{1.6^2 \times EIRP}{4\pi \times R^2} \right) \times \text{Off Beam Loss}$$

Where:

EIRP = Effective Isotropic Radiated Power

R = Radial Distance =  $\sqrt{(H^2 + V^2)}$

H = Horizontal Distance from antenna in meters

V = Vertical Distance from radiation center of antenna in meters

Ground reflection factor of 1.6

Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and power, and that all channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not take into account actual terrain elevations which could attenuate the signal. As a result, the predicted signal levels reported below are much higher than the actual signal levels will be from the finished modifications.



PAUL J. FORD AND COMPANY  
 STRUCTURAL ENGINEERS  
 250 East Broad Street • Suite 1500 • Columbus, Ohio 43215-3708

Date: August 14, 2012

Eva Morales  
 Crown Castle USA Inc.  
 3530 Toringdon Way, Suite 300  
 Charlotte, NC 28277  
 704.405.6612

Paul J. Ford and Company  
 250 East Broad Street, Suite 1500  
 Columbus, Ohio 43215  
 614.221.6679  
 kmahlum@pjfweb.com

Subject: Structural Analysis Report

**Carrier Designation:** AT&T Mobility Co-Locate  
 Carrier Site Number: CT1012  
 Carrier Site Name: PINNEY STREET

**Crown Castle Designation:** Crown Castle BU Number: 876377  
 Crown Castle Site Name: HORTON 2 / FREDSELL

PROPERTY  
 Crown Castle JDE Job Number: 199136  
 Crown Castle Work Order Number: 519445  
 Crown Castle Application Number: 157742 Rev. 1

**Engineering Firm Designation:** Paul J. Ford Project Number: 37512-1619 R1

**Site Data:** 161 Pinney Street, COLEBROOK, Litchfield County, CT  
 Latitude 41° 57' 58.57", Longitude -73° 7' 19.65"  
 148 Foot - Monopole Tower

Dear Eva Morales,

Paul J. Ford is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 481671, in accordance with application 157742, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Existing + Reserved + Proposed Equipment **Sufficient Capacity**  
 Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and 2005 CT State Building Code using a fastest mile wind speed of 80 mph with no ice, 28.1 mph with 1 inch ice thickness and 50 mph under service loads.

We at Paul J. Ford appreciate the opportunity of providing our continuing professional services to you and Crown Castle USA Inc. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

  
 Kevin Mahlum, E.I.  
 Structural Engineer

tnxTower Report - version 6.0.3.0





PAUL J. FORD AND COMPANY  
STRUCTURAL ENGINEERS  
250 East Broad Street • Suite 1500 • Columbus, Ohio 43215-3708

Date: **August 14, 2012**

Eva Morales  
Crown Castle USA Inc.  
3530 Toringdon Way, Suite 300  
Charlotte, NC 28277  
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**Carrier Site Number:** CT1012  
**Carrier Site Name:** PINNEY STREET

**Crown Castle Designation:** **Crown Castle BU Number:** 876377  
**Crown Castle Site Name:** HORTON 2 /  
FREDSALL

PROPERTY

**Crown Castle JDE Job Number:** 199136  
**Crown Castle Work Order Number:** 519445  
**Crown Castle Application Number:** 157742 Rev. 1

**Engineering Firm Designation:** **Paul J. Ford Project Number:** 37512-1619 R1

**Site Data:** **161 Pinney Street, COLEBROOK, Litchfield County, CT**  
**Latitude 41° 57' 58.57", Longitude -73° 7' 19.65"**  
**148 Foot - Monopole Tower**

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Paul J. Ford is pleased to submit this "**Structural Analysis Report**" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 481671, in accordance with application 157742, revision 1.

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LC7: Existing + Reserved + Proposed Equipment

**Sufficient Capacity**

Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and 2005 CT State Building Code using a fastest mile wind speed of 80 mph with no ice, 28.1 mph with 1 inch ice thickness and 50 mph under service loads.

We at Paul J. Ford appreciate the opportunity of providing our continuing professional services to you and Crown Castle USA Inc. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:

Kevin Mahlum, E.I.  
Structural Engineer

tnxTower Report - version 6.0.3.0

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**1) INTRODUCTION**

This tower is a 148 ft Monopole tower designed by SUMMIT in September of 2000. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

**2) ANALYSIS CRITERIA**

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures and 2005 CT State Building Code using a fastest mile wind speed of 80 mph with no ice, 28.1 mph with 1 inch ice thickness and 50 mph under service loads.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
140.0	140.0	1	kmw communications	AM-X-CD-14-65-00T-RET w/ Pipe	3	3/8	-
		2		AM-X-CD-16-65-00T-RET w/ Pipe			
		1	raycap	DC6-48-60-18-8F			
138.0	138.0	6	ericsson	RRUS-11			
		1	tower mounts	Side Arm Mount [SO 102-3]			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note			
150.0	148.0	3	alcatel lucent	1900MHz RRH (65MHz)	3	1-1/4	2			
		3		800 EXTERNAL NOTCH FILTER						
		3		800MHZ RRH						
		9	rfs celwave	ACU-A20-N						
		3		APXVSP18-C-A20 w/ Pipe						
		1	tower mounts	Miscellaneous (NA507-1)						
		6	decibel	DB980H90E-M w/ Pipe				6	1-5/8	3
		1	tower mounts	Platform Mount [LP 401-1]	-	-	1			
140.0	140.0	6	powerwave technologies	7770.00 w/ Pipe	12	1-5/8	1			
		6		LGP 17201						
		6		LGP21901						
		1	tower mounts	T-Arm Mount [TA 602-3]						
130.0	130.0	3	antel	BXA-171085-12BF-EDIN-2 w/ Pipe	-	-	2			
		1		BXA-70080-6CF-EDIN-6 w/ Pipe						
		2		BXA-70080/6CF w/ Pipe						
		2		LPA-80080-6CF-EDIN-6 w/ Pipe						
		6	rfs celwave	FD9R6004/2C-3L						
		2	antel	LPA-80080/6CF w/ Pipe				-	-	3
		6		LPA-185080/12CFx2 w/ Pipe						
		4		LPA-80080/6CF w/ Pipe						
		1	tower mounts	Platform Mount [LP 305-1]	12	1-5/8	1			
100.0	102.0	1	lucent	KS24019-L112A	1	1/2	1			
	100.0	1	tower mounts	Side Arm Mount [SO 701-1]						

- Notes:  
 1) Existing Equipment  
 2) Reserved Equipment  
 3) Equipment to be Removed

### 3) ANALYSIS PROCEDURE

**Table 3 - Documents Provided**

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	SEA Cpmconsultants, 99674.03-A, 09/05/2000	1532992	CCISITES
4-POST-MODIFICATION INSPECTION	PJF, 41708-0177_Record, 02/11/2009	2385953	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	PJF/Summit, 29200-1364/11163, 09/11/2000	1629428	CCISITES
4-TOWER MANUFACTURER DRAWINGS	PJF/Summit, 29200-1364/11163, 09/11/2000	1883532	CCISITES

#### 3.1) Analysis Method

tnxTower (version 6.0.3.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole was reinforced in conformance with the referenced modification drawings

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford should be notified to determine the effect on the structural integrity of the tower.

**4) ANALYSIS RESULTS**

**Table 4 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P <sub>allow</sub> (K)	% Capacity	Pass / Fail
L1	148 - 117.25	Pole	TP27.227x22x0.1875	1	-6.75	755.23	55.9	Pass
L2	117.25 - 97.25	Pole	TP30.2515x26.2571x0.25	2	-9.45	1142.41	79.1	Pass
L3	97.25 - 80.75	Pole	TP33.056x30.2515x0.443	3	-11.60	2049.74	55.7	Pass
L4	80.75 - 40	Pole	TP39.483x31.4476x0.4385	4	-20.07	2447.21	75.2	Pass
L5	40 - 13.25	Pole	TP43.4677x37.7133x0.4502	5	-28.31	2845.69	82.5	Pass
L6	13.25 - 12.75	Pole	TP43.5527x43.4677x0.4516	6	-28.44	2827.21	83.3	Pass
L7	12.75 - 5.3333	Pole	TP44.8134x43.5527x0.4254	7	-30.21	2838.90	86.6	Pass
L8	5.3333 - 4.75	Pole	TP44.9126x44.8134x0.4467	8	-30.36	2888.05	85.5	Pass
L9	4.75 - 0	Pole	TP45.72x44.9126x0.4425	9	-31.56	2947.77	85.9	Pass
							Summary	
						Pole (L7)	86.6	Pass
						Rating =	86.6	Pass

**Table 5 - Tower Component Stresses vs. Capacity – LC7**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	90.4	Pass
1	Base Plate	0	78.4	Pass
1	Base Foundation Steel Interaction	0	91.4	Pass
1, 2	Base Foundation Soil Interaction	0	92.3	Pass

<b>Structure Rating (max from all components) =</b>	<b>92.3%</b>
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Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.
- 2) According to the procedures prescribed and agreed to by the Crown Castle Engineering Foundation Committee, held in January 2010, the existing caisson foundation was analyzed using the methodology in the software 'PLS-Caisson' (Version 8.10, or newer, by Power Line Systems, Inc.). Per the methods in PLS-Caisson, the soil reactions of cohesive soils are calculated using 8CD independent of the depth of the soil layer. The depth of soil to be ignored at the top of the caisson is the greater of the geotechnical report's recommendation, the frost depth of the site or half of the caisson diameter.

## APPENDIX A

### TNXTOWER OUTPUT

#### Tower Input Data

There is a pole section.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Litchfield County, Connecticut.

Basic wind speed of 80 mph.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 28 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

#### Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification ✓ Use Code Stress Ratios ✓ Use Code Safety Factors - Guys ✓ Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination	Distribute Leg Loads As Uniform Assume Legs Pinned ✓ Assume Rigid Index Plate ✓ Use Clear Spans For Wind Area ✓ Use Clear Spans For KL/r Retension Guys To Initial Tension ✓ Bypass Mast Stability Checks ✓ Use Azimuth Dish Coefficients ✓ Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing	Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation ✓ Consider Feedline Torque Include Angle Block Shear Check Poles ✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets
--	--	---

#### Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	148.0000- 117.2500	30.7500	3.50	18	22.0000	27.2270	0.1875	0.7500	A572-60 (60 ksi)
L2	117.2500- 97.2500	23.5000	0.00	18	26.2571	30.2514	0.2500	1.0000	A572-60 (60 ksi)
L3	97.2500- 80.7500	16.5000	4.25	18	30.2514	33.0560	0.4430	1.7721	Reinf 57.15 ksi (57 ksi)
L4	80.7500- 40.0000	45.0000	5.00	18	31.4476	39.4830	0.4385	1.7538	Reinf 57.63 ksi (58 ksi)
L5	40.0000- 13.2500	31.7500	0.00	18	37.7133	43.4677	0.4502	1.8009	Reinf 57.88 ksi (58 ksi)
L6	13.2500- 12.7500	0.5000	0.00	18	43.4677	43.5527	0.4516	1.8063	Reinf 57.22 ksi (57 ksi)
L7	12.7500-	7.4167	0.00	18	43.5527	44.8134	0.4254	1.7017	Reinf 59.22 ksi

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L8	5.3333-4.7500	0.5833	0.00	18	44.8134	44.9126	0.4467	1.7867	(59 ksi) Reinf 57.28 ksi (57 ksi)
L9	4.7500-0.0000	4.7500		18	44.9126	45.7200	0.4425	1.7699	Reinf 57.96 ksi (58 ksi)

### Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I/Q in <sup>2</sup>	w in	w/t
L1	22.3394	12.9812	780.3007	7.7434	11.1760	69.8193	1561.6281	6.4918	3.5420	18.891
L2	27.6470	16.0919	1486.4203	9.5990	13.8313	107.4677	2974.7964	8.0475	4.4620	23.797
L3	30.7181	23.8062	2707.1425	10.6505	15.3677	176.1575	5417.8471	11.9053	4.8843	19.537
L4	32.7033	43.1535	5242.4244	11.0082	15.9754	328.1569	10491.747	21.5809	4.7631	10.863
L5	39.2152	53.2488	9341.2384	13.2284	19.1583	487.5807	18694.768	26.6295	5.8451	12.983
L6	44.1382	61.4719	14371.544	15.2712	22.0816	650.8386	28761.999	30.7418	6.8579	15.232
L7	44.2245	61.7774	14499.193	15.3009	22.1248	655.3380	29017.464	30.8946	6.8705	15.214
L8	45.5047	62.9001	15642.411	15.7502	22.7652	687.1191	31305.406	31.4560	7.1010	15.898
L9	46.4253	63.5892	16469.708	16.0735	23.2258	709.1139	32961.088	31.8006	7.2680	16.425

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>r</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
L1 148.0000- 117.2500				1	1	1		
L2 117.2500- 97.2500				1	1	1		
L3 97.2500- 80.7500				1	1	1		
L4 80.7500- 40.0000				1	1	1		
L5 40.0000- 13.2500				1	1	1		
L6 13.2500- 12.7500				1	1	1		
L7 12.7500- 5.3333				1	1	1		
L8 5.3333- 4.7500				1	1	1		
L9 4.7500-				1	1	1		

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_r$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft <sup>2</sup>	in					in	in
0.0000								

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement	Total Number	Number Per Row	Clear Spacing	Width or Diameter	Perimeter	Weight
				ft			in	r	r	plf
*****										

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement	Total Number		$C_d A_A$	Weight	
				ft			ft <sup>2</sup> /ft	plf	
HB114-1-0813U4-M5J(1 1/4")	C	No	Inside Pole	148.0000 - 0.0000	3	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	1.20 1.20 1.20 1.20 1.20	
***									
LCF158-50A(1-5/8")	C	No	Inside Pole	140.0000 - 0.0000	12	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.80 0.80 0.80 0.80 0.80	
FB-L98B-002-75000(3/8")	C	No	Inside Pole	140.0000 - 0.0000	1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.06 0.06 0.06 0.06 0.06	
WR-VG122ST-BRDA(3/8)	C	No	CaAa (Out Of Face)	140.0000 - 0.0000	1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.20 0.74 1.89 6.03 21.63	
WR-VG122ST-BRDA(3/8)	C	No	CaAa (Out Of Face)	140.0000 - 0.0000	1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0385 0.1385 0.2385 0.4385 0.8385	0.20 0.74 1.89 6.03 21.63	
***									
LDF7-50A(1-5/8")	C	No	Inside Pole	130.0000 - 0.0000	12	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.82 0.82 0.82 0.82 0.82	
***									
LDF4-50A(1/2")	C	No	Inside Pole	100.0000 - 0.0000	1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.15 0.15 0.15 0.15 0.15	
***									
LDF4-50A(1/2")	C	No	Inside Pole	8.2500 - 0.0000	1	No Ice 1/2" Ice 1" Ice 2" Ice 4" Ice	0.0000 0.0000 0.0000 0.0000 0.0000	0.15 0.15 0.15 0.15 0.15	
***									
Aero MP3-05	C	No	CaAa (Out Of	99.5000 - 0.0000	1	No Ice	0.3478	0.00	

Description	Face or Shield Leg	Allow Shield	Component Type	Placement ft	Total Number	C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight plf
			Face)		1/2" Ice	0.4001	0.00
					1" Ice	0.6566	0.00
					2" Ice	0.8788	0.00
					4" Ice	1.3232	0.00
*****							

**Feed Line/Linear Appurtenances Section Areas**

Tower Section n	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
L1	148.0000-117.2500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.876	0.46
L2	117.2500-97.2500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	1.553	0.47
L3	97.2500-80.7500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	6.374	0.39
L4	80.7500-40.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	15.742	0.96
L5	40.0000-13.2500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	10.333	0.63
L6	13.2500-12.7500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.193	0.01
L7	12.7500-5.3333	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	2.865	0.18
L8	5.3333-4.7500	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.225	0.01
L9	4.7500-0.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	1.835	0.11

**Feed Line/Linear Appurtenances Section Areas - With Ice**

Tower Section n	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
L1	148.0000-117.2500	A	1.181	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	6.250	0.58
L2	117.2500-97.2500	A	1.152	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	7.063	0.57
L3	97.2500-80.7500	A	1.126	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	15.648	0.46
L4	80.7500-40.0000	A	1.075	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	38.646	1.14
L5	40.0000-13.2500	A	1.000	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	24.787	0.74
L6	13.2500-12.7500	A	1.000	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.448	0.01
L7	12.7500-5.3333	A	1.000	0.000	0.000	0.000	0.000	0.00

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
L8	5.3333-4.7500	B	1.000	0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	6.638	0.20
		A		0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
L9	4.7500-0.0000	C	1.000	0.000	0.000	0.000	0.522	0.02
		A		0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	4.252	0.13

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>X</sub> in	CP <sub>Z</sub> in	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
L1	148.0000-117.2500	-0.0375	0.0217	-0.2271	0.1311
L2	117.2500-97.2500	-0.1003	0.0579	-0.3770	0.2176
L3	97.2500-80.7500	-0.4377	0.2527	-0.8611	0.4972
L4	80.7500-40.0000	-0.4443	0.2565	-0.8925	0.5153
L5	40.0000-13.2500	-0.4509	0.2603	-0.9096	0.5252
L6	13.2500-12.7500	-0.4535	0.2618	-0.8994	0.5192
L7	12.7500-5.3333	-0.4542	0.2622	-0.9025	0.5210
L8	5.3333-4.7500	-0.4548	0.2626	-0.9055	0.5228
L9	4.7500-0.0000	-0.4552	0.2628	-0.9076	0.5240

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft	Azimuth Adjustmen t °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K	
Platform Mount [LP 401-1]	C	None			148.0000	No Ice	24.3300	24.3300	1.65
						1/2" Ice	30.2200	30.2200	2.03
						1" Ice	36.1100	36.1100	2.41
						2" Ice	47.8900	47.8900	3.18
						4" Ice	71.4500	71.4500	4.72
*** APXVSPP18-C-A20 w/ Mount Pipe	A	From Face	4.0000 0.00 -2.00	0.0000	150.0000	No Ice	8.4975	6.9458	0.08
						1/2" Ice	9.1490	8.1266	0.15
						1" Ice	9.7672	9.0212	0.22
						2" Ice	11.0311	10.8440	0.41
						4" Ice	13.6786	14.8507	0.91
APXVSPP18-C-A20 w/ Mount Pipe	B	From Face	4.0000 0.00 -2.00	0.0000	150.0000	No Ice	8.4975	6.9458	0.08
						1/2" Ice	9.1490	8.1266	0.15
						1" Ice	9.7672	9.0212	0.22
						2" Ice	11.0311	10.8440	0.41
						4" Ice	13.6786	14.8507	0.91
APXVSPP18-C-A20 w/ Mount Pipe	C	From Face	4.0000 0.00 -2.00	0.0000	150.0000	No Ice	8.4975	6.9458	0.08
						1/2" Ice	9.1490	8.1266	0.15
						1" Ice	9.7672	9.0212	0.22
						2" Ice	11.0311	10.8440	0.41
						4" Ice	13.6786	14.8507	0.91
1900MHz RRH (65MHz)	A	From Face	4.0000 0.00	0.0000	150.0000	No Ice	2.6979	2.7708	0.06
						1/2" Ice	2.9362	3.0111	0.08

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K	
			-2.00			Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
						4" Ice			
1900MHz RRH (65MHz)	B	From Face	4.0000	0.0000	150.0000	No Ice	2.6979	2.7708	0.06
			0.00			1/2"	2.9362	3.0111	0.08
			-2.00			Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
						4" Ice			
1900MHz RRH (65MHz)	C	From Face	4.0000	0.0000	150.0000	No Ice	2.6979	2.7708	0.06
			0.00			1/2"	2.9362	3.0111	0.08
			-2.00			Ice	3.1832	3.2600	0.11
						1" Ice	3.7030	3.7837	0.18
						2" Ice	4.8463	4.9348	0.35
						4" Ice			
(3) ACU-A20-N	A	From Face	4.0000	0.0000	150.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2"	0.1210	0.1890	0.00
			-2.00			Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
						4" Ice			
(3) ACU-A20-N	B	From Face	4.0000	0.0000	150.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2"	0.1210	0.1890	0.00
			-2.00			Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
						4" Ice			
(3) ACU-A20-N	C	From Face	4.0000	0.0000	150.0000	No Ice	0.0778	0.1361	0.00
			0.00			1/2"	0.1210	0.1890	0.00
			-2.00			Ice	0.1728	0.2506	0.00
						1" Ice	0.3025	0.3997	0.01
						2" Ice	0.6654	0.8015	0.04
						4" Ice			
800MHZ RRH	A	From Face	4.0000	0.0000	150.0000	No Ice	2.4899	2.0685	0.05
			0.00			1/2"	2.7061	2.2705	0.07
			-2.00			Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
						4" Ice			
800MHZ RRH	B	From Face	4.0000	0.0000	150.0000	No Ice	2.4899	2.0685	0.05
			0.00			1/2"	2.7061	2.2705	0.07
			-2.00			Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
						4" Ice			
800MHZ RRH	C	From Face	4.0000	0.0000	150.0000	No Ice	2.4899	2.0685	0.05
			0.00			1/2"	2.7061	2.2705	0.07
			-2.00			Ice	2.9310	2.4812	0.10
						1" Ice	3.4068	2.9284	0.16
						2" Ice	4.4620	3.9265	0.32
						4" Ice			
800 EXTERNAL NOTCH FILTER	A	From Face	4.0000	0.0000	150.0000	No Ice	0.7701	0.3747	0.01
			0.00			1/2"	0.8898	0.4647	0.02
			-2.00			Ice	1.0181	0.5634	0.02
						1" Ice	1.3007	0.7868	0.04
						2" Ice	1.9696	1.3372	0.11
						4" Ice			
800 EXTERNAL NOTCH FILTER	B	From Face	4.0000	0.0000	150.0000	No Ice	0.7701	0.3747	0.01
			0.00			1/2"	0.8898	0.4647	0.02
			-2.00			Ice	1.0181	0.5634	0.02
						1" Ice	1.3007	0.7868	0.04
						2" Ice	1.9696	1.3372	0.11
						4" Ice			
800 EXTERNAL NOTCH	C	From Face	4.0000	0.0000	150.0000	No Ice	0.7701	0.3747	0.01

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K
FILTER			0.00 -2.00			1/2" 0.8898 Ice 1.0181 1" Ice 1.3007 2" Ice 1.9696 4" Ice	0.4647 0.5634 0.7868 1.3372	0.02 0.02 0.04 0.11
Miscellaneous (NA507-1)	C	From Face	4.0000 0.00 -2.00	0.0000	150.0000	No Ice 4.8000 1/2" 6.7000 Ice 8.6000 1" Ice 12.4000 2" Ice 20.0000 4" Ice	4.8000 6.7000 8.6000 12.4000 20.0000	0.25 0.29 0.34 0.44 0.64
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**								
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(2) 7770.00 w/ Mount Pipe	A	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 6.1194 1/2" 6.6258 Ice 7.1283 1" Ice 8.1643 2" Ice 10.3599 4" Ice	4.2543 5.0137 5.7109 7.1553 10.4117	0.06 0.10 0.16 0.29 0.66
(2) 7770.00 w/ Mount Pipe	B	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 6.1194 1/2" 6.6258 Ice 7.1283 1" Ice 8.1643 2" Ice 10.3599 4" Ice	4.2543 5.0137 5.7109 7.1553 10.4117	0.06 0.10 0.16 0.29 0.66
(2) 7770.00 w/ Mount Pipe	C	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 6.1194 1/2" 6.6258 Ice 7.1283 1" Ice 8.1643 2" Ice 10.3599 4" Ice	4.2543 5.0137 5.7109 7.1553 10.4117	0.06 0.10 0.16 0.29 0.66
(2) LGP 17201	A	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 1.9460 1/2" 2.1337 Ice 2.3301 1" Ice 2.7488 2" Ice 3.6900 4" Ice	0.5180 0.6396 0.7699 1.0564 1.7331	0.03 0.04 0.06 0.09 0.19
(2) LGP 17201	B	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 1.9460 1/2" 2.1337 Ice 2.3301 1" Ice 2.7488 2" Ice 3.6900 4" Ice	0.5180 0.6396 0.7699 1.0564 1.7331	0.03 0.04 0.06 0.09 0.19
(2) LGP 17201	C	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 1.9460 1/2" 2.1337 Ice 2.3301 1" Ice 2.7488 2" Ice 3.6900 4" Ice	0.5180 0.6396 0.7699 1.0564 1.7331	0.03 0.04 0.06 0.09 0.19
(2) LGP21901	A	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 0.2695 1/2" 0.3432 Ice 0.4255 1" Ice 0.6160 2" Ice 1.1009 4" Ice	0.1838 0.2483 0.3216 0.4940 0.9425	0.01 0.01 0.01 0.02 0.07
(2) LGP21901	B	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 0.2695 1/2" 0.3432 Ice 0.4255 1" Ice 0.6160 2" Ice 1.1009 4" Ice	0.1838 0.2483 0.3216 0.4940 0.9425	0.01 0.01 0.01 0.02 0.07
(2) LGP21901	C	From Face	4.0000 0.00 0.00	0.0000	140.0000	No Ice 0.2695 1/2" 0.3432 Ice 0.4255	0.1838 0.2483 0.3216	0.01 0.01 0.01

Description	Face or Leg	Offset Type	Offsets:			Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight	
			Horz	Lateral	Vert						ft
T-Arm Mount [TA 602-3]	C	None				0.0000	140.0000	1" Ice	0.6160	0.4940	0.02
								2" Ice	1.1009	0.9425	0.07
								4" Ice			
								No Ice	11.5900	11.5900	0.77
								1/2"	15.4400	15.4400	0.99
								Ice	19.2900	19.2900	1.21
AM-X-CD-16-65-00T-RET w/ Mount Pipe	A	From Leg	4.0000	0.00	0.00	0.0000	140.0000	1" Ice	26.9900	26.9900	1.64
								2" Ice	42.3900	42.3900	2.50
								4" Ice			
								No Ice	8.4975	6.3042	0.07
								1/2"	9.1490	7.4790	0.14
								Ice	9.7672	8.3676	0.21
AM-X-CD-14-65-00T-RET w/ Mount Pipe	B	From Leg	4.0000	0.00	0.00	0.0000	140.0000	1" Ice	11.0311	10.1785	0.38
								2" Ice	13.6786	14.0237	0.87
								4" Ice			
								No Ice	5.7442	4.0153	0.03
								1/2"	6.1977	4.6330	0.08
								Ice	6.6606	5.2765	0.13
AM-X-CD-16-65-00T-RET w/ Mount Pipe	C	From Leg	4.0000	0.00	0.00	0.0000	140.0000	1" Ice	11.0311	10.1785	0.38
								2" Ice	13.6786	14.0237	0.87
								4" Ice			
								No Ice	8.4975	6.3042	0.07
								1/2"	9.1490	7.4790	0.14
								Ice	9.7672	8.3676	0.21
DC6-48-60-18-8F	B	From Leg	4.0000	0.00	0.00	0.0000	140.0000	1" Ice	3.5432	3.5432	0.13
								2" Ice	4.6580	4.6580	0.30
								4" Ice			
								No Ice	2.5667	2.5667	0.02
								1/2"	2.7978	2.7978	0.04
								Ice	3.0377	3.0377	0.07
*** (2) RRUS-11	A	From Leg	2.0000	0.00	0.00	0.0000	138.0000	1" Ice	5.6127	1.9002	0.17
								2" Ice	6.9402	2.7532	0.36
								4" Ice			
								No Ice	4.4236	1.1855	0.05
								1/2"	4.7079	1.3512	0.07
								Ice	5.0009	1.5256	0.10
(2) RRUS-11	B	From Leg	2.0000	0.00	0.00	0.0000	138.0000	1" Ice	5.6127	1.9002	0.17
								2" Ice	6.9402	2.7532	0.36
								4" Ice			
								No Ice	4.4236	1.1855	0.05
								1/2"	4.7079	1.3512	0.07
								Ice	5.0009	1.5256	0.10
(2) RRUS-11	C	From Leg	2.0000	0.00	0.00	0.0000	138.0000	1" Ice	5.6127	1.9002	0.17
								2" Ice	6.9402	2.7532	0.36
								4" Ice			
								No Ice	4.4236	1.1855	0.05
								1/2"	4.7079	1.3512	0.07
								Ice	5.0009	1.5256	0.10
Side Arm Mount [SO 102-3]	C	None				0.0000	138.0000	1" Ice	4.9200	4.9200	0.20
								2" Ice	6.8400	6.8400	0.32
								4" Ice			
								No Ice	3.0000	3.0000	0.08
								1/2"	3.4800	3.4800	0.11
								Ice	3.9600	3.9600	0.14
*** (2) LPA-80080/6CF w/ Mount Pipe	A	From Face	4.0000	0.00	0.00	0.0000	130.0000	1" Ice	6.6508	14.9795	0.36
								2" Ice	8.8342	19.2168	0.86
								4" Ice			
								No Ice	4.5639	10.7282	0.05
								1/2"	5.1051	11.9896	0.11
								Ice	5.6116	12.9683	0.19

Description	Face or Leg	Offset Type	Offsets:			Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub>		Weight
			Horz	Lateral	Vert			Front	Side	
			ft	ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
(2) LPA-80080/6CF w/ Mount Pipe	B	From Face	4.0000	0.0000	130.0000	No Ice	4.5639	10.7282	0.05	
			0.00	0.0000	130.0000	1/2"	5.1051	11.9896	0.11	
			0.00	0.0000	130.0000	Ice	5.6116	12.9683	0.19	
				0.0000	130.0000	1" Ice	6.6508	14.9795	0.36	
				0.0000	130.0000	2" Ice	8.8342	19.2168	0.86	
BXA-171085-12BF-EDIN-2 w/ Mount Pipe	A	From Face	4.0000	0.0000	130.0000	No Ice	4.9710	5.2283	0.04	
			0.00	0.0000	130.0000	1/2"	5.5211	6.3892	0.08	
			0.00	0.0000	130.0000	Ice	6.0361	7.2610	0.14	
				0.0000	130.0000	1" Ice	7.0911	9.0462	0.27	
				0.0000	130.0000	2" Ice	9.3593	12.8165	0.67	
BXA-171085-12BF-EDIN-2 w/ Mount Pipe	B	From Face	4.0000	0.0000	130.0000	No Ice	4.9710	5.2283	0.04	
			0.00	0.0000	130.0000	1/2"	5.5211	6.3892	0.08	
			0.00	0.0000	130.0000	Ice	6.0361	7.2610	0.14	
				0.0000	130.0000	1" Ice	7.0911	9.0462	0.27	
				0.0000	130.0000	2" Ice	9.3593	12.8165	0.67	
BXA-171085-12BF-EDIN-2 w/ Mount Pipe	C	From Face	4.0000	0.0000	130.0000	No Ice	4.9710	5.2283	0.04	
			0.00	0.0000	130.0000	1/2"	5.5211	6.3892	0.08	
			0.00	0.0000	130.0000	Ice	6.0361	7.2610	0.14	
				0.0000	130.0000	1" Ice	7.0911	9.0462	0.27	
				0.0000	130.0000	2" Ice	9.3593	12.8165	0.67	
BXA-70080/6CF w/ Mount Pipe	A	From Face	4.0000	0.0000	130.0000	No Ice	6.0736	6.0983	0.04	
			0.00	0.0000	130.0000	1/2"	6.6306	7.2558	0.09	
			0.00	0.0000	130.0000	Ice	7.1524	8.1258	0.16	
				0.0000	130.0000	1" Ice	8.2495	9.9156	0.31	
				0.0000	130.0000	2" Ice	10.7781	13.7095	0.75	
BXA-70080/6CF w/ Mount Pipe	B	From Face	4.0000	0.0000	130.0000	No Ice	6.0736	6.0983	0.04	
			0.00	0.0000	130.0000	1/2"	6.6306	7.2558	0.09	
			0.00	0.0000	130.0000	Ice	7.1524	8.1258	0.16	
				0.0000	130.0000	1" Ice	8.2495	9.9156	0.31	
				0.0000	130.0000	2" Ice	10.7781	13.7095	0.75	
BXA-70080-6CF-EDIN-6 w/ Mount Pipe	C	From Face	4.0000	0.0000	130.0000	No Ice	6.0062	6.2035	0.04	
			0.00	0.0000	130.0000	1/2"	6.5619	7.3594	0.10	
			0.00	0.0000	130.0000	Ice	7.0826	8.2293	0.16	
				0.0000	130.0000	1" Ice	8.1672	10.0193	0.31	
				0.0000	130.0000	2" Ice	10.6907	13.8398	0.75	
(2) LPA-80080-6CF-EDIN-6 w/ Mount Pipe	C	From Face	4.0000	0.0000	130.0000	No Ice	4.5604	10.7396	0.05	
			0.00	0.0000	130.0000	1/2"	5.1019	12.0018	0.11	
			0.00	0.0000	130.0000	Ice	5.6085	12.9809	0.19	
				0.0000	130.0000	1" Ice	6.6479	14.9930	0.36	
				0.0000	130.0000	2" Ice	8.8318	19.2318	0.86	
(2) FD9R6004/2C-3L	A	From Face	4.0000	0.0000	130.0000	No Ice	0.3665	0.0846	0.00	
			0.00	0.0000	130.0000	1/2"	0.4506	0.1362	0.01	
			0.00	0.0000	130.0000	Ice	0.5433	0.1965	0.01	
				0.0000	130.0000	1" Ice	0.7546	0.3430	0.02	
				0.0000	130.0000	2" Ice	1.2808	0.7396	0.06	
(2) FD9R6004/2C-3L	B	From Face	4.0000	0.0000	130.0000	No Ice	0.3665	0.0846	0.00	
			0.00	0.0000	130.0000	1/2"	0.4506	0.1362	0.01	
			0.00	0.0000	130.0000	Ice	0.5433	0.1965	0.01	
				0.0000	130.0000	1" Ice	0.7546	0.3430	0.02	
				0.0000	130.0000	2" Ice	1.2808	0.7396	0.06	
(2) FD9R6004/2C-3L	C	From Face	4.0000	0.0000	130.0000	No Ice	0.3665	0.0846	0.00	
			0.00	0.0000	130.0000	1/2"	0.4506	0.1362	0.01	
			0.00	0.0000	130.0000	Ice	0.5433	0.1965	0.01	
				0.0000	130.0000	1" Ice	0.7546	0.3430	0.02	
				0.0000	130.0000	2" Ice	1.2808	0.7396	0.06	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight	
			Horz	Lateral Vert						
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
Platform Mount [LP 305-1]	C	None			0.0000	130.0000	4" Ice			
							No Ice	18.0100	18.0100	1.12
							1/2" Ice	23.3300	23.3300	1.35
							Ice	28.6500	28.6500	1.58
							1" Ice	39.2900	39.2900	2.05
							2" Ice	60.5700	60.5700	2.97
							4" Ice			
***										
Side Arm Mount [SO 701-1]	A	None			0.0000	100.0000	No Ice	0.8500	1.6700	0.07
							1/2" Ice	1.1400	2.3400	0.08
							Ice	1.4300	3.0100	0.09
							1" Ice	2.0100	4.3500	0.12
							2" Ice	3.1700	7.0300	0.18
							4" Ice			
KS24019-L112A	A	From Face	2.0000	0.00	0.0000	100.0000	No Ice	0.1556	0.1556	0.01
							1/2" Ice	0.2247	0.2247	0.01
							Ice	0.3025	0.3025	0.01
							1" Ice	0.4840	0.4840	0.02
							2" Ice	0.9506	0.9506	0.06
							4" Ice			
*****										

### Tower Pressures - No Ice

$G_H = 1.690$

Section Elevation	z	K <sub>z</sub>	q <sub>z</sub>	A <sub>G</sub>	F a c e	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face	C <sub>A</sub> A <sub>A</sub> Out Face
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 148.0000-117.2500	132.2079	1.487	24	63.072	A	0.000	63.072	63.072	100.00	0.000	0.000
					B	0.000	63.072	100.00	0.000	0.000	
					C	0.000	63.072	100.00	0.000	0.876	
L2 117.2500-97.2500	107.0516	1.4	23	47.586	A	0.000	47.586	47.586	100.00	0.000	0.000
					B	0.000	47.586	100.00	0.000	0.000	
					C	0.000	47.586	100.00	0.000	1.553	
L3 97.2500-80.7500	88.8782	1.327	22	43.524	A	0.000	43.524	43.524	100.00	0.000	0.000
					B	0.000	43.524	100.00	0.000	0.000	
					C	0.000	43.524	100.00	0.000	6.374	
L4 80.7500-40.0000	60.1817	1.187	19	121.723	A	0.000	121.723	121.723	100.00	0.000	0.000
					B	0.000	121.723	100.00	0.000	0.000	
					C	0.000	121.723	100.00	0.000	15.742	
L5 40.0000-13.2500	26.3617	1	16	91.493	A	0.000	91.493	91.493	100.00	0.000	0.000
					B	0.000	91.493	100.00	0.000	0.000	
					C	0.000	91.493	100.00	0.000	10.333	
L6 13.2500-12.7500	12.9999	1	16	1.813	A	0.000	1.813	1.813	100.00	0.000	0.000
					B	0.000	1.813	100.00	0.000	0.000	
					C	0.000	1.813	100.00	0.000	0.193	
L7 12.7500-5.3333	9.0240	1	16	27.308	A	0.000	27.308	27.308	100.00	0.000	0.000
					B	0.000	27.308	100.00	0.000	0.000	
					C	0.000	27.308	100.00	0.000	2.865	
L8 5.3333-4.7500	5.0415	1	16	2.181	A	0.000	2.181	2.181	100.00	0.000	0.000
					B	0.000	2.181	100.00	0.000	0.000	
					C	0.000	2.181	100.00	0.000	0.225	
L9 4.7500-0.0000	2.3679	1	16	17.938	A	0.000	17.938	17.938	100.00	0.000	0.000
					B	0.000	17.938	100.00	0.000	0.000	
					C	0.000	17.938	100.00	0.000	1.835	

### Tower Pressure - With Ice

$G_H = 1.690$

Section Elevation ft	z ft	$K_z$	$q_z$ psf	$t_z$ in	$A_G$ ft <sup>2</sup>	F a c e	$A_F$ ft <sup>2</sup>	$A_R$ ft <sup>2</sup>	$A_{leg}$ ft <sup>2</sup>	Leg %	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>
L1 148.0000-117.2500	132.2079	1.487	3	1.1812	69.126	A	0.000	69.126	69.126	100.00	0.000	0.000
						B	0.000	69.126		100.00	0.000	0.000
						C	0.000	69.126		100.00	0.000	6.250
L2 117.2500-97.2500	107.0516	1.4	3	1.1517	51.524	A	0.000	51.524	51.524	100.00	0.000	0.000
						B	0.000	51.524		100.00	0.000	0.000
						C	0.000	51.524		100.00	0.000	7.063
L3 97.2500-80.7500	88.8782	1.327	3	1.1262	46.621	A	0.000	46.621	46.621	100.00	0.000	0.000
						B	0.000	46.621		100.00	0.000	0.000
						C	0.000	46.621		100.00	0.000	15.648
L4 80.7500-40.0000	60.1817	1.187	2	1.0748	129.372	A	0.000	129.372	129.372	100.00	0.000	0.000
						B	0.000	129.372		100.00	0.000	0.000
						C	0.000	129.372		100.00	0.000	38.646
L5 40.0000-13.2500	26.3617	1	2	1.0000	96.285	A	0.000	96.285	96.285	100.00	0.000	0.000
						B	0.000	96.285		100.00	0.000	0.000
						C	0.000	96.285		100.00	0.000	24.787
L6 13.2500-12.7500	12.9999	1	2	1.0000	1.896	A	0.000	1.896	1.896	100.00	0.000	0.000
						B	0.000	1.896		100.00	0.000	0.000
						C	0.000	1.896		100.00	0.000	0.448
L7 12.7500-5.3333	9.0240	1	2	1.0000	28.544	A	0.000	28.544	28.544	100.00	0.000	0.000
						B	0.000	28.544		100.00	0.000	0.000
						C	0.000	28.544		100.00	0.000	6.638
L8 5.3333-4.7500	5.0415	1	2	1.0000	2.278	A	0.000	2.278	2.278	100.00	0.000	0.000
						B	0.000	2.278		100.00	0.000	0.000
						C	0.000	2.278		100.00	0.000	0.522
L9 4.7500-0.0000	2.3679	1	2	1.0000	18.729	A	0.000	18.729	18.729	100.00	0.000	0.000
						B	0.000	18.729		100.00	0.000	0.000
						C	0.000	18.729		100.00	0.000	4.252

### Tower Pressure - Service

$G_H = 1.690$

Section Elevation ft	z ft	$K_z$	$q_z$ psf	$A_G$ ft <sup>2</sup>	F a c e	$A_F$ ft <sup>2</sup>	$A_R$ ft <sup>2</sup>	$A_{leg}$ ft <sup>2</sup>	Leg %	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>
L1 148.0000-117.2500	132.2079	1.487	10	63.072	A	0.000	63.072	63.072	100.00	0.000	0.000
					B	0.000	63.072		100.00	0.000	0.000
					C	0.000	63.072		100.00	0.000	0.876
L2 117.2500-97.2500	107.0516	1.4	9	47.586	A	0.000	47.586	47.586	100.00	0.000	0.000
					B	0.000	47.586		100.00	0.000	0.000
					C	0.000	47.586		100.00	0.000	1.553
L3 97.2500-80.7500	88.8782	1.327	8	43.524	A	0.000	43.524	43.524	100.00	0.000	0.000
					B	0.000	43.524		100.00	0.000	0.000
					C	0.000	43.524		100.00	0.000	6.374
L4 80.7500-40.0000	60.1817	1.187	8	121.72	A	0.000	121.723	121.723	100.00	0.000	0.000
					B	0.000	121.723		100.00	0.000	0.000
					C	0.000	121.723		100.00	0.000	15.742
L5 40.0000-13.2500	26.3617	1	6	91.493	A	0.000	91.493	91.493	100.00	0.000	0.000
					B	0.000	91.493		100.00	0.000	0.000
					C	0.000	91.493		100.00	0.000	10.333
L6 13.2500-12.7500	12.9999	1	6	1.813	A	0.000	1.813	1.813	100.00	0.000	0.000
					B	0.000	1.813		100.00	0.000	0.000
					C	0.000	1.813		100.00	0.000	0.193
L7 12.7500-5.3333	9.0240	1	6	27.308	A	0.000	27.308	27.308	100.00	0.000	0.000
					B	0.000	27.308		100.00	0.000	0.000
					C	0.000	27.308		100.00	0.000	2.865

Section Elevation ft	z ft	K <sub>z</sub>	q <sub>z</sub> psf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L8 5.3333-4.7500	5.0415	1	6	2.181	A	0.000	2.181	2.181	100.00	0.000	0.000
					B	0.000	2.181		100.00	0.000	0.000
					C	0.000	2.181		100.00	0.000	0.225
L9 4.7500-0.0000	2.3679	1	6	17.938	A	0.000	17.938	17.938	100.00	0.000	0.000
					B	0.000	17.938		100.00	0.000	0.000
					C	0.000	17.938		100.00	0.000	1.835

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	148 - 117.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-15.88	0.16	-1.88
			Max. Mx	11	-6.75	224.35	-1.29
			Max. My	8	-6.75	0.27	-225.52
			Max. Vy	11	-13.07	224.35	-1.29
			Max. Vx	8	13.07	0.27	-225.52
			Max. Torque	11			1.17

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L2	117.25 - 97.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-19.71	0.32	-1.98
			Max. Mx	11	-9.45	549.36	-1.55
			Max. My	8	-9.45	0.50	-550.49
			Max. Vy	11	-14.64	549.36	-1.55
			Max. Vx	8	14.64	0.50	-550.49
			Max. Torque	11			1.17
L3	97.25 - 80.75	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-22.42	0.38	-2.01
			Max. Mx	11	-11.60	734.66	-1.68
			Max. My	8	-11.60	0.62	-735.78
			Max. Vy	11	-15.63	734.66	-1.68
			Max. Vx	8	15.63	0.62	-735.78
			Max. Torque	11			1.18
L4	80.75 - 40	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-32.90	0.62	-2.09
			Max. Mx	11	-20.07	1421.34	-2.08
			Max. My	8	-20.07	0.99	-1422.37
			Max. Vy	11	-18.62	1421.34	-2.08
			Max. Vx	8	18.61	0.99	-1422.37
			Max. Torque	11			1.25
L5	40 - 13.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-42.79	0.81	-2.15
			Max. Mx	11	-28.31	2044.64	-2.38
			Max. My	8	-28.31	1.28	-2045.59
			Max. Vy	11	-20.58	2044.64	-2.38
			Max. Vx	8	20.58	1.28	-2045.59
			Max. Torque	11			1.30
L6	13.25 - 12.75	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-42.93	0.82	-2.15
			Max. Mx	11	-28.44	2054.93	-2.38
			Max. My	8	-28.44	1.29	-2055.88
			Max. Vy	11	-20.60	2054.93	-2.38
			Max. Vx	8	20.60	1.29	-2055.88
			Max. Torque	11			1.30
L7	12.75 - 5.3333	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-45.04	0.86	-2.17
			Max. Mx	11	-30.21	2209.24	-2.45
			Max. My	8	-30.21	1.36	-2210.17
			Max. Vy	11	-21.03	2209.24	-2.45
			Max. Vx	8	21.03	1.36	-2210.17
			Max. Torque	11			1.31
L8	5.3333 - 4.75	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-45.21	0.86	-2.17
			Max. Mx	11	-30.36	2221.51	-2.45
			Max. My	8	-30.36	1.36	-2222.44
			Max. Vy	11	-21.06	2221.51	-2.45
			Max. Vx	8	21.05	1.36	-2222.44
			Max. Torque	11			1.31
L9	4.75 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-46.63	0.89	-2.17
			Max. Mx	11	-31.56	2322.14	-2.49
			Max. My	8	-31.56	1.40	-2323.06
			Max. Vy	11	-21.33	2322.14	-2.49
			Max. Vx	8	21.33	1.40	-2323.06
			Max. Torque	11			1.32

**Maximum Reactions**

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	14	46.63	-0.00	0.00
	Max. H <sub>x</sub>	11	31.57	21.32	-0.01
	Max. H <sub>z</sub>	2	31.57	-0.01	21.32
	Max. M <sub>x</sub>	2	2320.52	-0.01	21.32
	Max. M <sub>z</sub>	5	2321.78	-21.32	0.01
	Max. Torsion	11	1.32	21.32	-0.01
	Min. Vert	8	31.57	0.01	-21.32
	Min. H <sub>x</sub>	5	31.57	-21.32	0.01
	Min. H <sub>z</sub>	8	31.57	0.01	-21.32
	Min. M <sub>x</sub>	8	-2323.06	0.01	-21.32
	Min. M <sub>z</sub>	11	-2322.14	21.32	-0.01
	Min. Torsion	5	-1.32	-21.32	0.01

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturing Moment, M <sub>x</sub> kip-ft	Overturing Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	31.57	0.00	-0.00	1.18	0.17	-0.00
Dead+Wind 0 deg - No Ice	31.57	0.01	-21.32	-2320.52	-1.05	-0.25
Dead+Wind 30 deg - No Ice	31.57	10.67	-18.47	-2010.60	-1161.93	0.44
Dead+Wind 60 deg - No Ice	31.57	18.47	-10.67	-1161.00	-2011.43	1.02
Dead+Wind 90 deg - No Ice	31.57	21.32	-0.01	0.04	-2321.78	1.32
Dead+Wind 120 deg - No Ice	31.57	18.46	10.65	1161.41	-2010.21	1.27
Dead+Wind 150 deg - No Ice	31.57	10.65	18.46	2011.92	-1159.81	0.88
Dead+Wind 180 deg - No Ice	31.57	-0.01	21.32	2323.06	1.40	0.25
Dead+Wind 210 deg - No Ice	31.57	-10.67	18.47	2013.14	1162.29	-0.44
Dead+Wind 240 deg - No Ice	31.57	-18.47	10.67	1163.53	2011.79	-1.02
Dead+Wind 270 deg - No Ice	31.57	-21.32	0.01	2.49	2322.14	-1.32
Dead+Wind 300 deg - No Ice	31.57	-18.46	-10.65	-1158.87	2010.57	-1.27
Dead+Wind 330 deg - No Ice	31.57	-10.65	-18.46	-2009.38	1160.17	-0.88
Dead+Ice+Temp	46.63	0.00	-0.00	2.17	0.89	-0.00
Dead+Wind 0 deg+Ice+Temp	46.63	-0.00	-3.48	-393.69	0.97	-0.10
Dead+Wind 30 deg+Ice+Temp	46.63	1.74	-3.01	-340.61	-197.20	0.08
Dead+Wind 60 deg+Ice+Temp	46.63	3.01	-1.74	-195.59	-342.28	0.23
Dead+Wind 90 deg+Ice+Temp	46.63	3.48	0.00	2.51	-395.38	0.33
Dead+Wind 120 deg+Ice+Temp	46.63	3.01	1.74	200.60	-342.28	0.33
Dead+Wind 150 deg+Ice+Temp	46.63	1.74	3.01	345.62	-197.21	0.25
Dead+Wind 180 deg+Ice+Temp	46.63	0.00	3.48	398.70	0.97	0.10
Dead+Wind 210 deg+Ice+Temp	46.63	-1.74	3.01	345.62	199.14	-0.08
Dead+Wind 240 deg+Ice+Temp	46.63	-3.01	1.74	200.60	344.21	-0.23
Dead+Wind 270 deg+Ice+Temp	46.63	-3.48	-0.00	2.50	397.31	-0.33
Dead+Wind 300 deg+Ice+Temp	46.63	-3.01	-1.74	-195.60	344.21	-0.33
Dead+Wind 330 deg+Ice+Temp	46.63	-1.74	-3.01	-340.61	199.14	-0.25
Dead+Wind 0 deg - Service	31.57	0.00	-8.33	-906.71	-0.30	-0.10
Dead+Wind 30 deg - Service	31.57	4.17	-7.21	-785.47	-454.27	0.17
Dead+Wind 60 deg - Service	31.57	7.21	-4.17	-453.23	-786.46	0.40
Dead+Wind 90 deg - Service	31.57	8.33	-0.00	0.79	-907.69	0.52
Dead+Wind 120 deg - Service	31.57	7.21	4.16	454.95	-785.98	0.50
Dead+Wind 150 deg - Service	31.57	4.16	7.21	787.54	-453.43	0.34
Dead+Wind 180 deg - Service	31.57	-0.00	8.33	909.26	0.66	0.10

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturing Moment, M <sub>x</sub>	Overturing Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Service						
Dead+Wind 210 deg - Service	31.57	-4.17	7.21	788.02	454.62	-0.17
Dead+Wind 240 deg - Service	31.57	-7.21	4.17	455.78	786.82	-0.40
Dead+Wind 270 deg - Service	31.57	-8.33	0.00	1.75	908.05	-0.52
Dead+Wind 300 deg - Service	31.57	-7.21	-4.16	-452.40	786.34	-0.50
Dead+Wind 330 deg - Service	31.57	-4.16	-7.21	-784.99	453.79	-0.34

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-31.57	0.00	-0.00	31.57	0.00	0.001%
2	0.01	-31.57	-21.32	-0.01	31.57	21.32	0.013%
3	10.67	-31.57	-18.47	-10.67	31.57	18.47	0.000%
4	18.47	-31.57	-10.67	-18.47	31.57	10.67	0.000%
5	21.32	-31.57	-0.01	-21.32	31.57	0.01	0.003%
6	18.46	-31.57	10.65	-18.46	31.57	-10.65	0.000%
7	10.65	-31.57	18.46	-10.65	31.57	-18.46	0.000%
8	-0.01	-31.57	21.32	0.01	31.57	-21.32	0.013%
9	-10.67	-31.57	18.47	10.67	31.57	-18.47	0.000%
10	-18.47	-31.57	10.67	-18.47	31.57	-10.67	0.000%
11	-21.32	-31.57	0.01	21.32	31.57	-0.01	0.003%
12	-18.46	-31.57	-10.65	18.46	31.57	10.65	0.000%
13	-10.65	-31.57	-18.46	10.65	31.57	18.46	0.000%
14	0.00	-46.63	0.00	-0.00	46.63	0.00	0.004%
15	-0.00	-46.63	-3.48	0.00	46.63	3.48	0.001%
16	1.74	-46.63	-3.01	-1.74	46.63	3.01	0.001%
17	3.01	-46.63	-1.74	-3.01	46.63	1.74	0.001%
18	3.48	-46.63	0.00	-3.48	46.63	-0.00	0.001%
19	3.01	-46.63	1.74	-3.01	46.63	-1.74	0.001%
20	1.74	-46.63	3.01	-1.74	46.63	-3.01	0.001%
21	0.00	-46.63	3.48	-0.00	46.63	-3.48	0.001%
22	-1.74	-46.63	3.01	1.74	46.63	-3.01	0.001%
23	-3.01	-46.63	1.74	3.01	46.63	-1.74	0.001%
24	-3.48	-46.63	-0.00	3.48	46.63	0.00	0.001%
25	-3.01	-46.63	-1.74	3.01	46.63	1.74	0.001%
26	-1.74	-46.63	-3.01	1.74	46.63	3.01	0.001%
27	0.00	-31.57	-8.33	-0.00	31.57	8.33	0.006%
28	4.17	-31.57	-7.22	-4.17	31.57	7.21	0.002%
29	7.21	-31.57	-4.17	-7.21	31.57	4.17	0.002%
30	8.33	-31.57	-0.00	-8.33	31.57	0.00	0.006%
31	7.21	-31.57	4.16	-7.21	31.57	-4.16	0.002%
32	4.16	-31.57	7.21	-4.16	31.57	-7.21	0.002%
33	-0.00	-31.57	8.33	0.00	31.57	-8.33	0.006%
34	-4.17	-31.57	7.22	4.17	31.57	-7.21	0.002%
35	-7.21	-31.57	4.17	7.21	31.57	-4.17	0.002%
36	-8.33	-31.57	0.00	8.33	31.57	-0.00	0.006%
37	-7.21	-31.57	-4.16	7.21	31.57	4.16	0.002%
38	-4.16	-31.57	-7.21	4.16	31.57	7.21	0.002%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	15	0.00013072	0.00014622

3	Yes	21	0.00000001	0.00009754
4	Yes	21	0.00000001	0.00009438
5	Yes	17	0.00003244	0.00008861
6	Yes	21	0.00000001	0.00009888
7	Yes	21	0.00000001	0.00009522
8	Yes	15	0.00013075	0.00014840
9	Yes	21	0.00000001	0.00009583
10	Yes	21	0.00000001	0.00009907
11	Yes	17	0.00003244	0.00009255
12	Yes	21	0.00000001	0.00009397
13	Yes	21	0.00000001	0.00009755
14	Yes	6	0.00000001	0.00004794
15	Yes	17	0.00000001	0.00010104
16	Yes	17	0.00000001	0.00011333
17	Yes	17	0.00000001	0.00011309
18	Yes	17	0.00000001	0.00010231
19	Yes	17	0.00000001	0.00011617
20	Yes	17	0.00000001	0.00011560
21	Yes	17	0.00000001	0.00010360
22	Yes	17	0.00000001	0.00011620
23	Yes	17	0.00000001	0.00011667
24	Yes	17	0.00000001	0.00010288
25	Yes	17	0.00000001	0.00011366
26	Yes	17	0.00000001	0.00011401
27	Yes	15	0.00013627	0.00007319
28	Yes	17	0.00000001	0.00012325
29	Yes	17	0.00000001	0.00011284
30	Yes	15	0.00013632	0.00009341
31	Yes	17	0.00000001	0.00012855
32	Yes	17	0.00000001	0.00011609
33	Yes	15	0.00013637	0.00007370
34	Yes	17	0.00000001	0.00011752
35	Yes	17	0.00000001	0.00012862
36	Yes	15	0.00013632	0.00009420
37	Yes	17	0.00000001	0.00011213
38	Yes	17	0.00000001	0.00012390

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	148 - 117.25	35.723	34	2.1278	0.0076
L2	120.75 - 97.25	23.983	34	1.9043	0.0035
L3	97.25 - 80.75	15.536	34	1.4767	0.0019
L4	85 - 40	11.961	34	1.3086	0.0015
L5	45 - 13.25	3.423	34	0.6949	0.0006
L6	13.25 - 12.75	0.295	34	0.2154	0.0002
L7	12.75 - 5.3333	0.273	34	0.2075	0.0002
L8	5.3333 - 4.75	0.047	34	0.0842	0.0001
L9	4.75 - 0	0.037	34	0.0750	0.0001

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
150.0000	APXVSPP18-C-A20 w/ Mount Pipe	34	35.723	2.1278	0.0076	20042
148.0000	Platform Mount [LP 401-1]	34	35.723	2.1278	0.0076	20042
140.0000	(2) 7770.00 w/ Mount Pipe	34	32.168	2.0866	0.0063	12526
138.0000	(2) RRUS-11	34	31.287	2.0747	0.0059	10020
130.0000	(2) LPA-80080/6CF w/ Mount Pipe	34	27.818	2.0143	0.0047	5566

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
100.0000	Side Arm Mount [SO 701-1]	34	16.416	1.5229	0.0020	2994

### Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
L1	148 - 117.25	91.002	8	5.4112	0.0193
L2	120.75 - 97.25	61.153	9	4.8544	0.0090
L3	97.25 - 80.75	39.642	9	3.7679	0.0049
L4	85 - 40	30.527	9	3.3397	0.0039
L5	45 - 13.25	8.743	9	1.7747	0.0016
L6	13.25 - 12.75	0.755	9	0.5502	0.0004
L7	12.75 - 5.3333	0.698	9	0.5301	0.0004
L8	5.3333 - 4.75	0.120	9	0.2150	0.0002
L9	4.75 - 0	0.095	9	0.1917	0.0001

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
ft			in	°	°	ft
150.0000	APXVSPP18-C-A20 w/ Mount Pipe	8	91.002	5.4112	0.0193	8071
148.0000	Platform Mount [LP 401-1]	8	91.002	5.4112	0.0193	8071
140.0000	(2) 7770.00 w/ Mount Pipe	8	81.965	5.3111	0.0159	5044
138.0000	(2) RRUS-11	8	79.724	5.2819	0.0151	4035
130.0000	(2) LPA-80080/6CF w/ Mount Pipe	8	70.904	5.1314	0.0120	2240
100.0000	Side Arm Mount [SO 701-1]	9	41.885	3.8856	0.0052	1186

### Compression Checks

### Pole Design Data

Section No.	Elevation	Size	L	L <sub>v</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P/P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
L1	148 - 117.25	TP27.227x22x0.1875	30.7500	0.0000	0.0	36.000	15.7378	-6.75	566.56	0.012
	(1)									
L2	117.25 - 97.25	TP30.2515x26.2571x0.25	23.5000	0.0000	0.0	36.000	23.8062	-9.45	857.02	0.011
	(2)									
L3	97.25 - 80.75	TP33.056x30.2515x0.443	16.5000	0.0000	0.0	34.290	44.8438	-11.60	1537.69	0.008
	(3)									
L4	80.75 - 40	TP39.483x31.4476x0.4385	45.0000	0.0000	0.0	34.578	53.0935	-20.07	1835.87	0.011
L5	40 - 13.25	TP43.4677x37.7133x0.450	31.7500	0.0000	0.0	34.728	61.4719	-28.31	2134.80	0.013
	(5)									
L6	13.25 - 12.75	TP43.5527x43.4677x0.451	0.5000	0.0000	0.0	34.332	61.7774	-28.44	2120.94	0.013
	(6)									
L7	12.75 - 5.3333	TP44.8134x43.5527x0.425	7.4167	0.0000	0.0	35.532	59.9377	-30.21	2129.71	0.014
	(7)									
L8	5.3333 - 4.75	TP44.9126x44.8134x0.446	0.5833	0.0000	0.0	34.368	63.0407	-30.36	2166.58	0.014
	(8)									
L9	4.75 - 0	TP45.72x44.9126x0.4425	4.7500	0.0000	0.0	34.776	63.5892	-31.56	2211.38	0.014
	(9)									

Section No.	Elevation ft	Size	L ft	$L_u$ ft	$Kl/r$	$F_a$ ksi	A $in^2$	Actual P K	Allow. $P_a$ K	Ratio $\frac{P}{P_a}$
-------------	-----------------	------	---------	-------------	--------	--------------	-------------	---------------	-------------------	-----------------------

### Pole Bending Design Data

Section No.	Elevation ft	Size	Actual $M_x$ kip-ft	Actual $f_{bx}$ ksi	Allow. $F_{bx}$ ksi	Ratio $\frac{f_{bx}}{F_{bx}}$	Actual $M_y$ kip-ft	Actual $f_{by}$ ksi	Allow. $F_{by}$ ksi	Ratio $\frac{f_{by}}{F_{by}}$
L1	148 - 117.25 (1)	TP27.227x22x0.1875	225.57	26.338	36.000	0.732	0.00	0.000	36.000	0.000
L2	117.25 - 97.25 (2)	TP30.2515x26.2571x0.25	550.80	37.521	36.000	1.042	0.00	0.000	36.000	0.000
L3	97.25 - 80.75 (3)	TP33.056x30.2515x0.443	736.23	25.185	34.290	0.734	0.00	0.000	34.290	0.000
L4	80.75 - 40 (4)	TP39.483x31.4476x0.438	1423.3	34.294	34.578	0.992	0.00	0.000	34.578	0.000
L5	40 - 13.25 (5)	TP43.4677x37.7133x0.45	2046.9	37.741	34.728	1.087	0.00	0.000	34.728	0.000
L6	13.25 - 12.75 (6)	TP43.5527x43.4677x0.45	2057.2	37.670	34.332	1.097	0.00	0.000	34.332	0.000
L7	12.75 - 5.3333 (7)	TP44.8134x43.5527x0.42	2211.6	40.494	35.532	1.140	0.00	0.000	35.532	0.000
L8	5.3333 - 4.75 (8)	TP44.9126x44.8134x0.44	2223.9	38.665	34.368	1.125	0.00	0.000	34.368	0.000
L9	4.75 - 0 (9)	TP45.72x44.9126x0.4425	2324.5	39.338	34.776	1.131	0.00	0.000	34.776	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual $f_v$ ksi	Allow. $F_v$ ksi	Ratio $\frac{f_v}{F_v}$	Actual T kip-ft	Actual $f_{vt}$ ksi	Allow. $F_{vt}$ ksi	Ratio $\frac{f_{vt}}{F_{vt}}$
L1	148 - 117.25 (1)	TP27.227x22x0.1875	13.08	0.831	24.000	0.069	0.63	0.036	24.000	0.001
L2	117.25 - 97.25 (2)	TP30.2515x26.2571x0.25	14.65	0.616	24.000	0.051	0.60	0.020	24.000	0.001
L3	97.25 - 80.75 (3)	TP33.056x30.2515x0.443	15.64	0.349	22.860	0.031	0.58	0.010	22.860	0.000
L4	80.75 - 40 (4)	TP39.483x31.4476x0.438	18.63	0.351	23.052	0.030	0.52	0.006	23.052	0.000
L5	40 - 13.25 (5)	TP43.4677x37.7133x0.45	20.59	0.335	23.152	0.029	0.47	0.004	23.152	0.000
L6	13.25 - 12.75 (6)	TP43.5527x43.4677x0.45	20.61	0.334	22.888	0.029	0.46	0.004	22.888	0.000
L7	12.75 - 5.3333 (7)	TP44.8134x43.5527x0.42	21.04	0.351	23.688	0.030	0.45	0.004	23.688	0.000
L8	5.3333 - 4.75 (8)	TP44.9126x44.8134x0.44	21.06	0.334	22.912	0.029	0.45	0.004	22.912	0.000
L9	4.75 - 0 (9)	TP45.72x44.9126x0.4425	21.34	0.336	23.184	0.029	0.44	0.004	23.184	0.000

### Pole Interaction Design Data

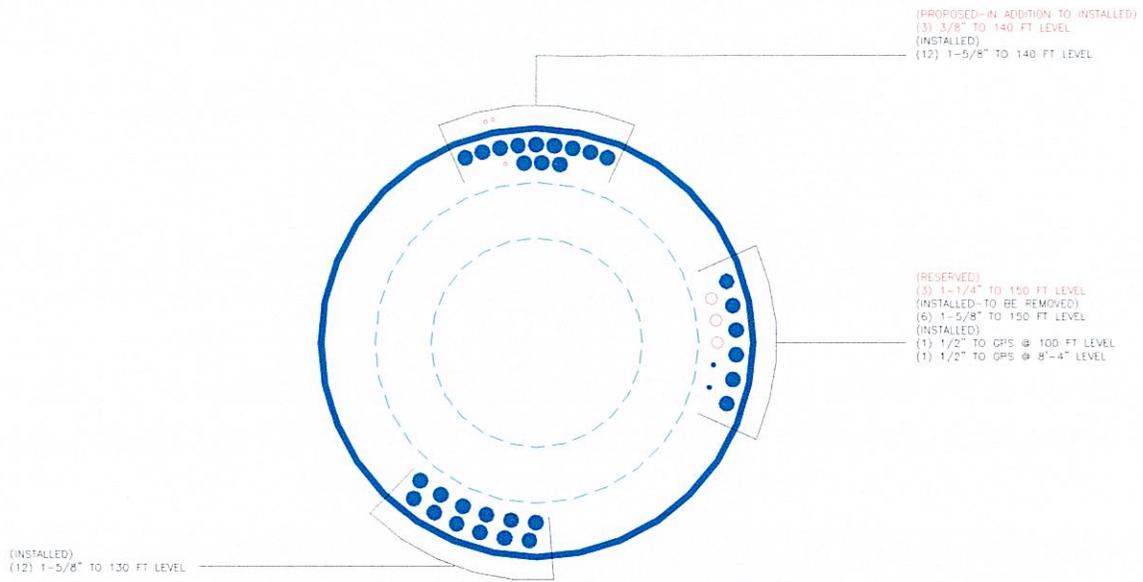
Section No.	Elevation ft	Ratio $\frac{P}{P_a}$	Ratio $\frac{f_{bx}}{F_{bx}}$	Ratio $\frac{f_{by}}{F_{by}}$	Ratio $\frac{f_v}{F_v}$	Ratio $\frac{f_{vt}}{F_{vt}}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	148 - 117.25 (1)	0.012	0.732	0.000	0.069	0.001	0.745	1.333	H1-3+VT ✓

Section No.	Elevation ft	Ratio	Ratio	Ratio	Ratio	Ratio	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		$P$	$f_{bx}$	$f_{by}$	$f_v$	$f_{vt}$			
		$P_a$	$F_{bx}$	$F_{by}$	$F_v$	$F_{vt}$			
L2	117.25 - 97.25 (2)	0.011	1.042	0.000	0.051	0.001	1.054	1.333	H1-3+VT ✓
L3	97.25 - 80.75 (3)	0.008	0.734	0.000	0.031	0.000	0.742	1.333	H1-3+VT ✓
L4	80.75 - 40 (4)	0.011	0.992	0.000	0.030	0.000	1.003	1.333	H1-3+VT ✓
L5	40 - 13.25 (5)	0.013	1.087	0.000	0.029	0.000	1.100	1.333	H1-3+VT ✓
L6	13.25 - 12.75 (6)	0.013	1.097	0.000	0.029	0.000	1.111	1.333	H1-3+VT ✓
L7	12.75 - 5.3333 (7)	0.014	1.140	0.000	0.030	0.000	1.154	1.333	H1-3+VT ✓
L8	5.3333 - 4.75 (8)	0.014	1.125	0.000	0.029	0.000	1.139	1.333	H1-3+VT ✓
L9	4.75 - 0 (9)	0.014	1.131	0.000	0.029	0.000	1.146	1.333	H1-3+VT ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail	
L1	148 - 117.25	Pole	TP27.227x22x0.1875	1	-6.75	755.23	55.9	Pass	
L2	117.25 - 97.25	Pole	TP30.2515x26.2571x0.25	2	-9.45	1142.41	79.1	Pass	
L3	97.25 - 80.75	Pole	TP33.056x30.2515x0.443	3	-11.60	2049.74	55.7	Pass	
L4	80.75 - 40	Pole	TP39.483x31.4476x0.4385	4	-20.07	2447.21	75.2	Pass	
L5	40 - 13.25	Pole	TP43.4677x37.7133x0.4502	5	-28.31	2845.69	82.5	Pass	
L6	13.25 - 12.75	Pole	TP43.5527x43.4677x0.4516	6	-28.44	2827.21	83.3	Pass	
L7	12.75 - 5.3333	Pole	TP44.8134x43.5527x0.4254	7	-30.21	2838.90	86.6	Pass	
L8	5.3333 - 4.75	Pole	TP44.9126x44.8134x0.4467	8	-30.36	2888.05	85.5	Pass	
L9	4.75 - 0	Pole	TP45.72x44.9126x0.4425	9	-31.56	2947.77	85.9	Pass	
							Summary		
							Pole (L7)	86.6	Pass
							<b>RATING =</b>	<b>86.6</b>	<b>Pass</b>

### APPENDIX B BASE LEVEL DRAWING



**APPENDIX C**  
**ADDITIONAL CALCULATIONS**



## Square, Stiffened / Unstiffened Base Plate, Any Rod Material - Rev. F /G

- Assumptions: 1) Rod groups at corners. Total # rods divisible by 4. Maximum total # of rods = 48 (12 per Corner).  
 2) Rod Spacing = Straight Center-to-Center distance between any (2) adjacent rods (same corner)  
 3) Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)\*(Rod Diameter)

### Site Data

BU#: \_\_\_\_\_  
 Site Name: \_\_\_\_\_  
 App #: \_\_\_\_\_

### Anchor Rod Data

Qty:	12	
Diam:	2.25	in
Rod Material:	A615-J	
Yield, Fy:	75	ksi
Strength, Fu:	100	ksi
Bolt Circle:	52	in
Anchor Spacing:	6	in

### Plate Data

W=Side:	51	in
Thick:	2.75	in
Grade:	55	ksi
Clip Distance:	8	in

### Stiffener Data (Welding at both sides)

Configuration:	Unstiffened	
Weld Type:		**
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		←- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

### Pole Data

Diam:	45.72	in
Thick:	0.3125	in
Grade:	65	ksi
# of Sides:	18	"0" IF Round

### Stress Increase Factor

ASD ASIF:	1.333
-----------	-------

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

### Base Reactions

TIA Revision:	F	
Unfactored Moment, M:	2325	ft-kips
Unfactored Axial, P:	32	kips
Unfactored Shear, V:	21	kips

### Anchor Rod Results

TIA F --> Maximum Rod Tension: 176.2 Kips  
 Allowable Tension: 195.0 Kips  
 Anchor Rod Stress Ratio: 90.4% **Pass**

### Base Plate Results

Base Plate Stress: 43.1 ksi  
 Allowable PL Bending Stress: 55.0 ksi  
 Base Plate Stress Ratio: 78.4% **Pass**

### Flexural Check

### PL Ref. Data

Yield Line (in):	26.40
Max PL Length:	26.40

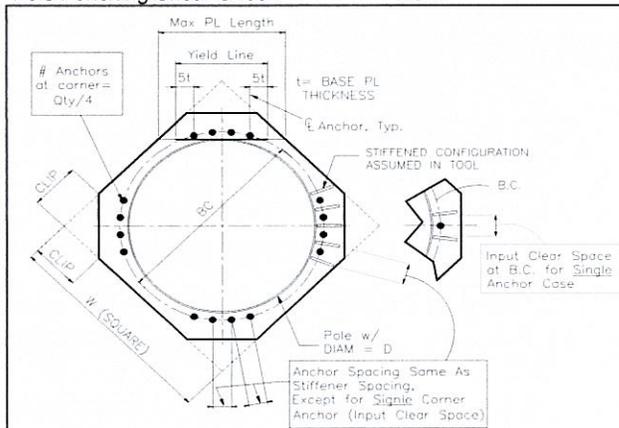
### N/A - Unstiffened

### Stiffener Results

Horizontal Weld: N/A  
 Vertical Weld: N/A  
 Plate Flex+Shear,  $f_b/F_b + (f_v/F_v)^2$ : N/A  
 Plate Tension+Shear,  $f_t/F_t + (f_v/F_v)^2$ : N/A  
 Plate Comp. (AISC Bracket): N/A

### Pole Results

Pole Punching Shear Check: N/A





**DRILLED PIER SOIL AND STEEL ANALYSIS - TIA/EIA-222-F**

**Unfactored Base Reactions from RISA**

	Comp. (+)	Tension (-)	
Moment, M =	2325.0		k-ft
Shear, V =	21.0		kips
Axial Load, P =	32.0		kips
OTM =	2335.5	0.0	k-ft @ Ground

**Safety Factors / Load Factors /  $\Phi$  Factors**

Tower Type =	Monopole DP
ACI Code =	ACI 318-02
Seismic Design Category =	D
Reference Standard =	TIA/EIA-222-F
Use 1.3 Load Factor?	Yes
Load Factor =	1.30

**Drilled Pier Parameters**

Diameter =	6	ft
Height Above Grade =	0.5	ft
Depth Below Grade =	18.5	ft
fc' =	3	ksi
cc =	0.003	in/in
Mat Ftdn. Cap Width =	10	ft
Mat Ftdn. Cap Length =	10	ft
Depth Below Grade =	5.5	ft

**Safety Factor  $\Phi$  Factor**

Soil Lateral Resistance =	2.00	0.75
Skin Friction =	2.00	0.75
End Bearing =	2.00	0.75
Concrete Wt. Resist Uplift =	1.25	

**Load Combinations Checked per TIA/EIA-222-F**

- Ult. Skin Friction/2.00 + Ult. End Bearing/2.00 + Effective Soil Wt. - Buoyant Conc. Wt.  $\geq$  Compression
- Ult. Skin Friction/2.00 + Buoyant Conc. Wt./1.25  $\geq$  Uplift
- Ult. Skin Friction/1.50 + Buoyant Conc. Wt./1.50  $\geq$  Uplift

**Steel Parameters**

Number of Bars =	16	
Rebar Size =	#11	
Rebar Fy =	60	ksi
Rebar MOE =	29000	ksi
Tie Size =	#5	
Side Clear Cover to Ties =	3	in

**Soil Parameters**

Water Table Depth =	11.00	ft
Depth to Ignore Soil =	3.33	ft
Depth to Full Cohesion =	0	ft
Full Cohesion Starts at?	Ground	

Above Full Cohesion Lateral Resistance =  $4(\text{Cohesion})(\text{Dia})(H)$   
 Below Full Cohesion Lateral Resistance =  $8(\text{Cohesion})(\text{Dia})(H)$

**Direct Embed Pole Shaft Parameters**

Dia @ Grade =		in
Dia @ Depth Below Grade =		in
Number of Sides =		
Thickness =		in
Fy =		ksi
Backfill Condition =		

**Maximum Capacity Ratios**

Maximum Soil Ratio =	100.0%
Maximum Steel Ratio =	100.0%

**Define Soil Layers**

Note: Cohesion = Undrained Shear Strength = Unconfined Compressive Strength / 2

Layer	Thickness ft	Unit Weight pcf	Cohesion psf	Friction Angle degrees	Soil Type	Ultimate End Bearing psf	Comp. Ult. Skin Friction psf	Tension Ult. Skin Friction psf	Depth ft
1	3	100	0	0	Sand				3
2	8	140	0	38	Sand	8000			11
3	3	139	0	38	Sand	8000			14
4	4	160	0	40	Sand	12000			18
5	6	160	0	40	Sand	12000			24
6									
7									
8									
9									
10									
11									
12									

**Soil Results: Overturning**

Depth to COR =	13.29	ft, from Grade
Bending Moment, M =	2614.67	k-ft, from COR
Resisting Moment, Ma =	2832.28	k-ft, from COR

**MOMENT RATIO = 92.3% OK**

Shear, V =	21.00	kips
Resisting Shear, Va =	22.75	kips

**SHEAR RATIO = 92.3% OK**

**Soil Results: Uplift**

Uplift, T =	0.00	kips
Allowable Uplift Cap., Ta =	105.52	kips

**UPLIFT RATIO = 0.0% OK**

**Soil Results: Compression**

Compression, C =	32.00	kips
Allowable Comp. Cap., Ca =	430.33	kips

**COMPRESSION RATIO = 7.4% OK**

**Steel Results (ACI 318-02):**

Minimum Steel Area =	13.57	sq in
Actual Steel Area =	24.96	sq in

Allowable Min Axial, Pa =	-1036.80	kips, Where Ma = 0 k-ft
Allowable Max Axial, Pa =	4726.51	kips, Where Ma = 0 k-ft

Axial Load, P =	38.79	kips @ 5.50 ft Below Grade
Moment, M =	2389.82	k-ft @ 5.50 ft Below Grade
Allowable Moment, Ma =	2613.61	k-ft

**MOMENT RATIO = 91.4% OK**

## Moment Capacity of Drilled Concrete Shaft (Caisson) for TIA Rev F or G

**Note:** Shaft assumed to have ties, not spiral, transverse reinforcing

### Site Data

BU#: 876377  
 Site Name: Horton 2 / Fredsall Property  
 App #:

Enter Load Factors Below:

For M (WL)	1.3	<--- Enter Factor
For P (DL)	1.3	<--- Enter Factor

### Pier Properties

#### Concrete:

Pier Diameter = 6.0 ft  
 Concrete Area = 4071.5 in<sup>2</sup>

#### Reinforcement:

Clear Cover to Tie = 3.00 in  
 Horiz. Tie Bar Size = 5  
 Vert. Cage Diameter = 5.28 ft  
 Vert. Cage Diameter = 63.34 in  
**Vertical Bar Size = 11**  
 Bar Diameter = 1.41 in  
 Bar Area = 1.56 in<sup>2</sup>  
 Number of Bars = 16  
 As Total = 24.96 in<sup>2</sup>  
 A s/ Aconc, Rho: 0.0061 0.61%

### Maximum Shaft Superimposed Forces

TIA Revision:	F	
Max. Service Shaft M:	2389.82	ft-kips (* Note)
Max. Service Shaft P:	38.79	kips
Max Axial Force Type:	Comp.	

(\* Note: Max Shaft Superimposed Moment does not necessarily equal to the shaft top reaction moment

Load Factor	Shaft Factored Loads	
1.30	Mu:	3106.766 ft-kips
1.30	Pu:	50.427 kips

### Material Properties

Concrete Comp. strength, f'c =	3000	psi
Reinforcement yield strength, Fy =	60	ksi
Reinforcing Modulus of Elasticity, E =	29000	ksi
Reinforcement yield strain =	0.00207	
Limiting compressive strain =	0.003	

### ACI 318 Code

Select Analysis ACI Code = 2002

### Seismic Properties

Seismic Design Category = D

Seismic Risk = High

Solve  
(Run)

<-- Press Upon Completing All Input

ACI 10.5 , ACI 21.10.4, and IBC 1810.

Min As for Flexural, Tension Controlled, Shafts:

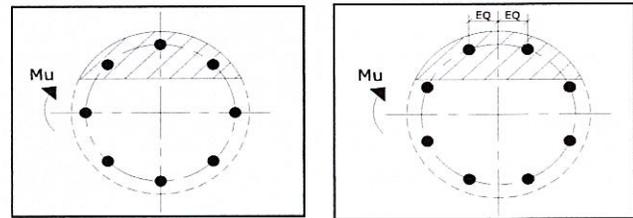
(3)\*(Sqrt(f'c)/Fy: 0.0027  
 200 / Fy: 0.0033

### Minimum Rho Check:

Actual Req'd Min. Rho:	0.33%	Flexural
Provided Rho:	0.61%	OK

### Results:

Governing Orientation Case: 2



Case 1

Case 2

Dist. From Edge to Neutral Axis: 12.24 in

Extreme Steel Strain,  $\epsilon_t$ : 0.0134

$\epsilon_t > 0.0050$ , Tension Controlled

Reduction Factor,  $\phi$ : 0.900

Ref. Shaft Max Axial Capacities, $\phi$ Max(Pn or Tn):		
Max Pu = ( $\phi=0.65$ ) Pn.		
Pn per ACI 318 (10-2)	6144.47	kips
at Mu=( $\phi=0.65$ )Mn=	3192.16	ft-kips
Max Tu, ( $\phi=0.9$ ) Tn =	1347.84	kips
at Mu= $\phi=(0.90)$ Mn=	0.00	ft-kips

Output Note: Negative Pu=Tension

For Axial Compression, $\phi$ Pn = Pu:	50.43	kips
Drilled Shaft Moment Capacity, $\phi$ Mn:	3397.68	ft-kips
Drilled Shaft Superimposed Mu:	3106.77	ft-kips

(Mu/ $\phi$ Mn, Drilled Shaft Flexure CSR: 91.4%