June 6, 2022

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Regarding: Notice of Exempt Modification – AT&T Site CT2036 / FA# 10034996
Address: 751 Higgins Road, Cheshire, CT 06410

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC ("AT&T") currently maintains a wireless telecommunications facility on an existing +/- 249' self-support tower at the above-referenced address, latitude 41.4874639, longitude -72.9293319. Said self-support tower is operated by AT&T Towers.

AT&T desires to modify its existing telecommunications facility by swapping six (6) antennas, adding three (3) antennas, and swapping three (3) surge arrestors and installing accompanying feedlines as more particularly detailed and described on the enclosed Construction Drawings prepared by Hudson Design Group, last revised May 27, 2022. The centerline height of the existing antennas is and will remain at 255 feet. This modification may include B2, B5, B17, B14, B29, B30, B66, & n77 hardware that is 4G(LTE) and/or 5GNR capable through remote software configuration and either or both services may be turned off at various times.

Please accept this letter as notification pursuant to R.C.S.A §16-50j-73 for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the following individuals: The Honorable Sean M. Kimball, Town Manager of the Town of Cheshire, as elected official, Michael J. Strollo, Zoning Enforcement Officer of the Town of Cheshire, Michael Glidden, Town Planner of the Town of Cheshire, AT&T Towers, as tower operator/property owner. We have reached out to the Building and Zoning Departments for the Town of Cheshire who conducted a search and could not locate the original tower approval.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Specifically:

1. The proposed modifications will not result in an increase in the height of the existing structure.

2. The proposed modifications will not require an extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the modified facility will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. *Please see the RF emissions calculation for AT&T's modified facility enclosed herewith.*

5. The proposed modifications will not cause an ineligible change or alteration in the physical or environmental characteristics of the site.

6. The existing structure and its foundation can support the proposed loading. *Please see the structural analysis dated May 20, 2022, and prepared by GDP Engineering, enclosed herewith.*

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Evan Renwick

Evan Renwick
Site Acquisition Specialist
Centerline Communications, LLC
750 West Center Street, Suite 301
West Bridgewater, MA 02379
erenwick@clinellc.com

Enclosures: Exhibit 1 – Construction Drawings
Exhibit 2 – Property Card and GIS
Exhibit 3 – Structural Analysis
Exhibit 4 – Mount Analysis
Exhibit 5 – RF Emissions Analysis Report Evaluation
Exhibit 6 – Notice Delivery Confirmations

cc: The Honorable Sean M. Kimball, Town Manager, as elected official.
Michael J. Strollo, Zoning Enforcement Officer, Town of Cheshire
Michael Glidden, Town Planner, Town of Cheshire
AT&T Towers, as tower operator/property owner.

EXHIBIT 1

PROJECT INFORMATION

SCOPE OF WORK:

ITEMS TO BE MOUNTED ON THE EXISTING LATTICE TOWER:
- NEW AT&T ANTENNAS: TPA65R-BU8DA-K (ALPHA SECTOR, TOTAL OF 1).
- NEW AT&T ANTENNAS: TPA65R-BU6DA-K (TYP. OF 1 PER BETA & GAMMA SECTORS, TOTAL OF 2).
- NEW AT&T ANTENNAS: AIR 6419 B77G STACKED @ POS 3 (TYP. 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T ANTENNAS: AIR 6449 B77D STACKED @ POS 3 (TYP. 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T SURGE ARRESTOR: DC9-48-60-24-8C-EV (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- NEW AT&T (6) Y-CABLES
- NEW AT&T (3) 6AWG DC POWER CABLES & (3) 24 PAIRS OF FIBER RUNS.
- RELOCATED EXISTING ANTENNAS: DMP65R-BU8DA @ POS. 4 (TYP. OF 1 PER ALPHA SECTOR, TOTAL OF 1).
- RELOCATED EXISTING ANTENNAS: DMP65R-BU6DA @ POS. 4 (TYP. OF 1 PER BETA & GAMMA SECTORS, TOTAL OF 2).
- RELOCATED EXISTING RRUS: 4449 B5/B12 (700) @ POS. 4 (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- RELOCATED EXISTING RRUS: 4478 B14 (700) @ POS. 2 (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- RELOCATED EXISTING RRUS-32 B30 (WCS) @ POS. 4 (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- RELOCATED EXISTING RRUS-32 B2 (1900) @ POS. 2 (TYP. OF 1 PER SECTOR, TOTAL OF 3).

ITEMS TO BE MOUNTED IN EQUIPMENT LOCATION:
- INSTALL (1) NEW FRONTHAUL GATEWAY (FHG) 6648+IDLE XCEDE CABLE & (1) FINAL= 1x6601/1x5216/1xXMU03||xxxxx/1x6630 Mixed-Mode/xxxxx+IDLe//1x6648+IDLe Xcede.
- ADD (3) NEW -48V RECTIFIERS IN EXISTING POWER PLANT
- INSTALL (1) DC12.

ITEMS TO BE REMOVED:
- DECOMMISSION EXISTING AT&T ANTENNA: 800-10966 (ALPHA SECTOR, TOTAL OF 1).
- DECOMMISSION EXISTING AT&T ANTENNA: 800-10965 (TYP. OF 1 PER BETA & GAMMA SECTOR, TOTAL OF 2).
- DECOMMISSION EXISTING AT&T ANTENNA: HPA-65R-BUU-H8 (ALPHA SECTOR, TOTAL OF 1).
- DECOMMISSION EXISTING AT&T ANTENNA: HPA-65R-BUU-H6 (TYP. OF 1 PER BETA & GAMMA SECTOR, TOTAL OF 2).
- DECOMMISSION EXISTING AT&T SURGE ARRESTOR: DC6-48-60-18-8F (TYP. OF 1 PER SECTOR, TOTAL OF 3).
- DECOMMISSION EXISTING AT&T (6) 1-5/8" COAX CABLES & (3) FIBER CABLES.

ITEMS TO REMAIN:
- (3) ANTENNAS, (15) RRU'S, (6) DC POWER.

SITE ADDRESS:	751 HIGGINS ROAD CHESHIRE, CT 06410
LATITUDE:	41.4874722° N, 41° 29' 14.9" N
LONGITUDE:	-72.9293055° W, 72° 55' 45.5" W
TYPE OF SITE:	LATTICE TOWER / INDOOR EQUIPMENT
STRUCTURE HEIGHT:	249'-0"±
RAD CENTER:	255'-0"±
CURRENT USE:	TELECOMMUNICATIONS FACILITY
PROPOSED USE:	TELECOMMUNICATIONS FACILITY

DRAWING INDEX

SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	B
GN-1	GENERAL NOTES	B
A-1	COMPOUND & EQUIPMENT PLANS	B
A-2	EXISTING & PROPOSED ANTENNA PLANS	B
A-3	ELEVATION LAYOUT	B
A-4	DETAILS	B
G-1	GROUNDING DETAILS	B
RF-1	RF PLUMBING DIAGRAM	B

SITE NUMBER: CT2036

SITE NAME: CHESHIRE SW

FA CODE: 10034996

PACE ID: MRCTB055762, MRCTB055784, MRCTB053287, MRCTB053676

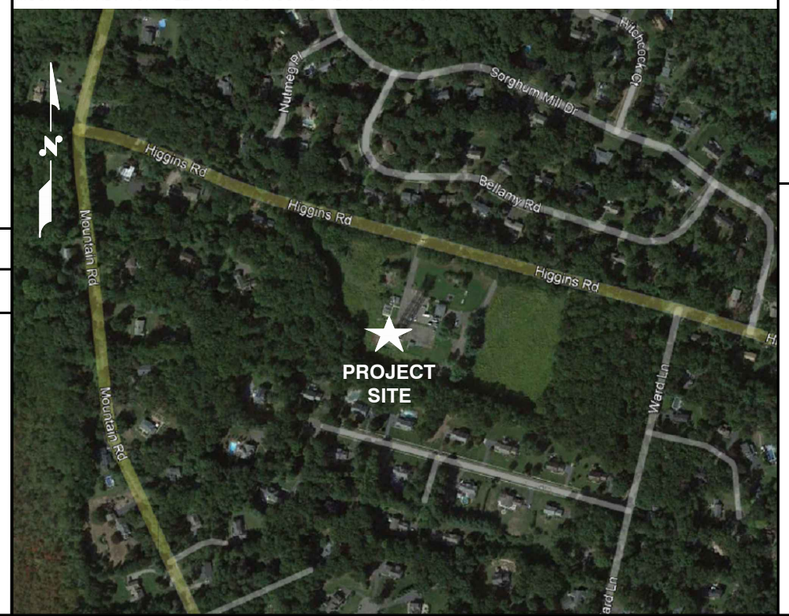
PROJECT: 5G NR RADIO || 5G NR 1SR CBAND, 2022 UPGRADE

ISSUED FOR PERMITTING

VICINITY MAP

DIRECTIONS TO SITE:

HEAD SOUTHEAST TOWARD CAPITAL BLVD. TURN LEFT ONTO CAPITAL BLVD. TURN LEFT ONTO STATE HWY 411, TURN LEFT TO MERGE ONTO I-91 S. MERGE ONTO I-91 S. KEEP RIGHT TO STAY ON I-91 S. TAKE EXIT 18 FOR I-691 W TOWARD MERIDEN/WATERBURY. CONTINUE ONTO I-691 W. TAKE EXIT 1 ON THE LEFT FOR I084 W TOWARD WATERBURY/DANBURY. MERGE ONTO I-84. TAKE EXIT 26 FOR CT-70 TOWARD CHESHIRE/PROSPECT. TURN LEFT ONTO CT-70 E/STATE HWY 801. TURN RIGHT ONTO MOUNTAIN RD. TURN LEFT ONTO HIGGINS RD. TURN RIGHT.



GENERAL NOTES

1. THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

72 HOURS

CALL
BEFORE YOU DIG
CALL TOLL FREE 1-800-922-4455
OR CALL 811

UNDERGROUND SERVICE ALERT

HUDSON Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

CENTERLINE COMMUNICATIONS
750 WEST CENTER STREET, SUITE #301
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT2036
SITE NAME: CHESHIRE SW

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at&t
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SCALE: AS SHOWN | DESIGNED BY: AT | DRAWN BY: GD

STATE OF CONNECTICUT · DANIEL P. HAMM · No. 24178 · LICENSED PROFESSIONAL ENGINEER

AT&T

TITLE SHEET
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	T-1	B

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.

2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.

3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81 STANDARDS) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.

4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.

5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, #6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS AND #2 AWG STRANDED COPPER FOR OUTDOOR BTS.

6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.

7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.

8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.

9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.

10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.

11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 AWG COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.

12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

   CONTRACTOR – CENTERLINE
   SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)
   OWNER – AT&T MOBILITY

2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.

3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.

4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.

5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.

6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.

7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.

8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.

9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.

10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.

11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.

12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.

13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.

15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCH UP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.

16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."

17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.

18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.

19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.

20. **APPLICABLE BUILDING CODES:**
    SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

    BUILDING CODE: IBC 2015 WITH 2018 CT STATE BUILDING CODE AMENDMENTS
    ELECTRICAL CODE: 2017 NATIONAL ELECTRICAL CODE (NFPA 70-2017)

    SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

    AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

    AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

    TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-H, STRUCTURAL STANDARDS FOR STEEL

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS

AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
BTCW	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	P	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD CL	RADIATION CENTER LINE (ANTENNAS)	VIF	VERIFY IN FIELD
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		

HUDSON Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

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WEST BRIDGEWATER, MA 02379

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SCALE: AS SHOWN | DESIGNED BY: AT | DRAWN BY: GD

STATE OF CONNECTICUT · DANIEL P. HAMM · No. 24178 · LICENSED PROFESSIONAL ENGINEER

AT&T

GENERAL NOTES
5G NR RADIO || 5G NR 1SR CBAND

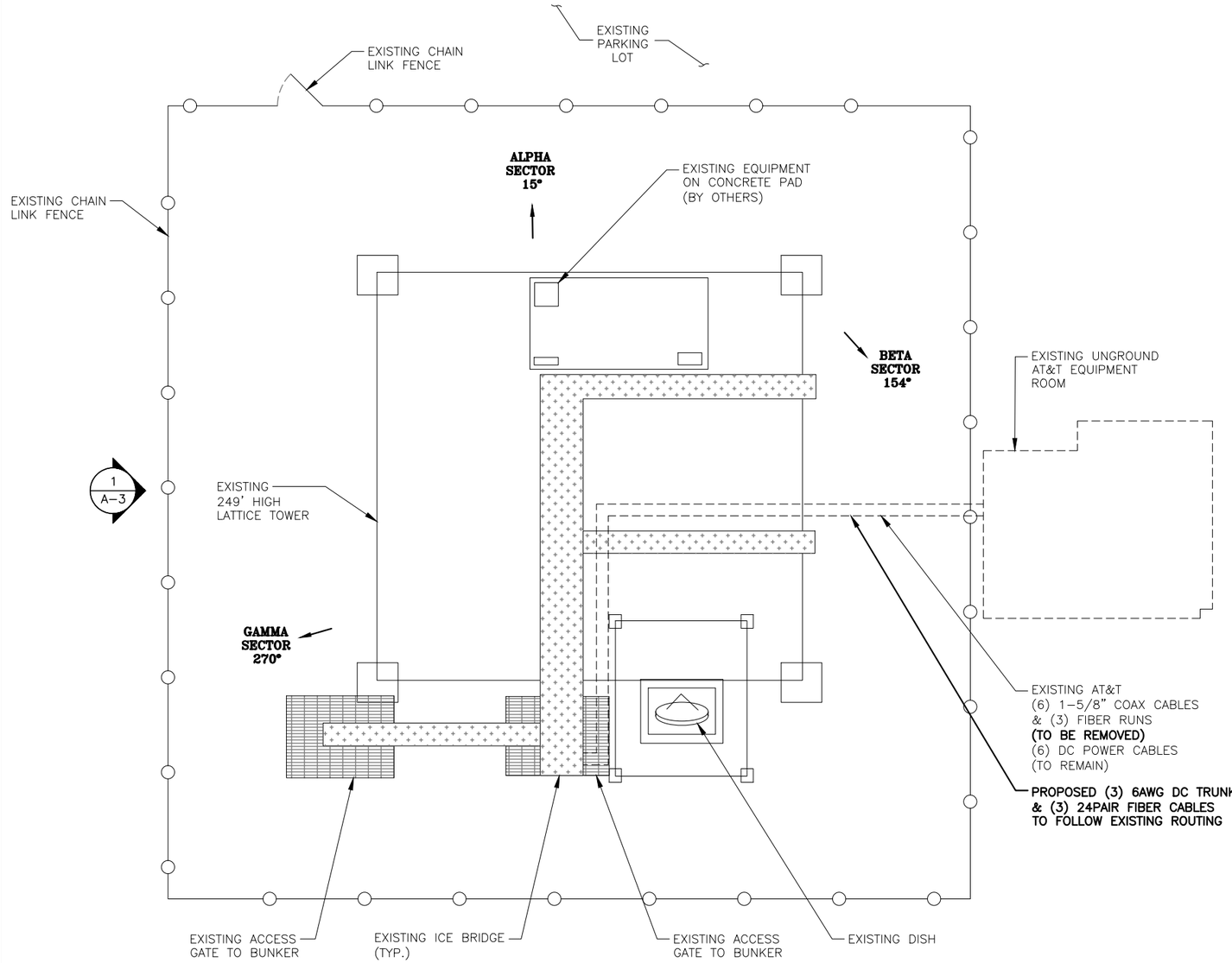
SITE NUMBER	DRAWING NUMBER	REV
CT2036	GN-1	B

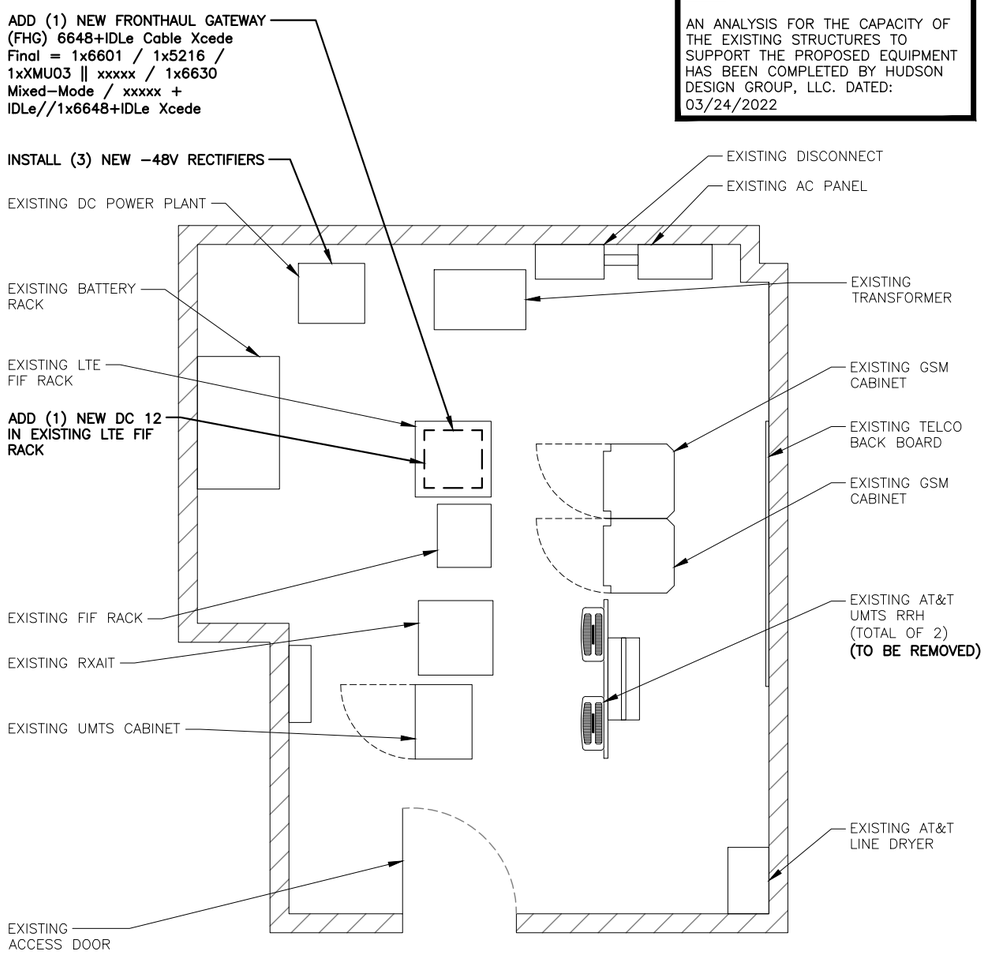
NOTE:

REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 10/25/2021 DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT HAS BEEN COMPLETED BY HUDSON DESIGN GROUP, LLC. DATED: 03/24/2022





COMPOUND PLAN (1 / A-1)
22x34 SCALE: 3/16"=1'-0"
11x17 SCALE: 3/32"=1'-0"

0 2'-8" 5'-4" 10'-8" 16'-0"

EQUIPMENT PLAN (2 / A-1)
22x34 SCALE: 1/2"=1'-0"
11x17 SCALE: 1/4"=1'-0"

0 1'-0" 2'-0" 4'-0" 6'-0"

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STATE OF CONNECTICUT · DANIEL P. HAMM · No. 24178 · LICENSED PROFESSIONAL ENGINEER

AT&T

COMPOUND & EQUIPMENT PLANS
5G NR RADIO || 5G NR 1SR CBAND

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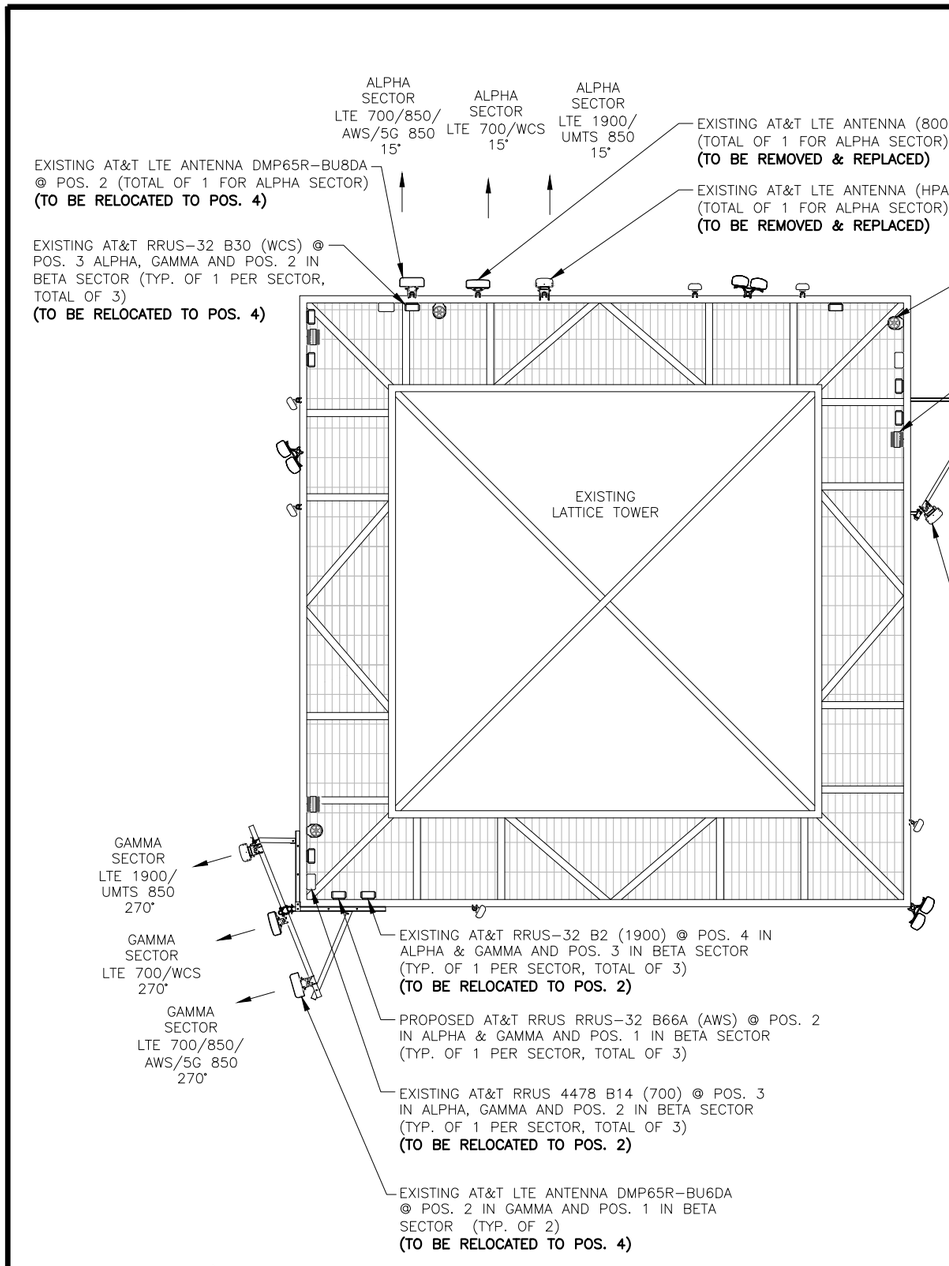
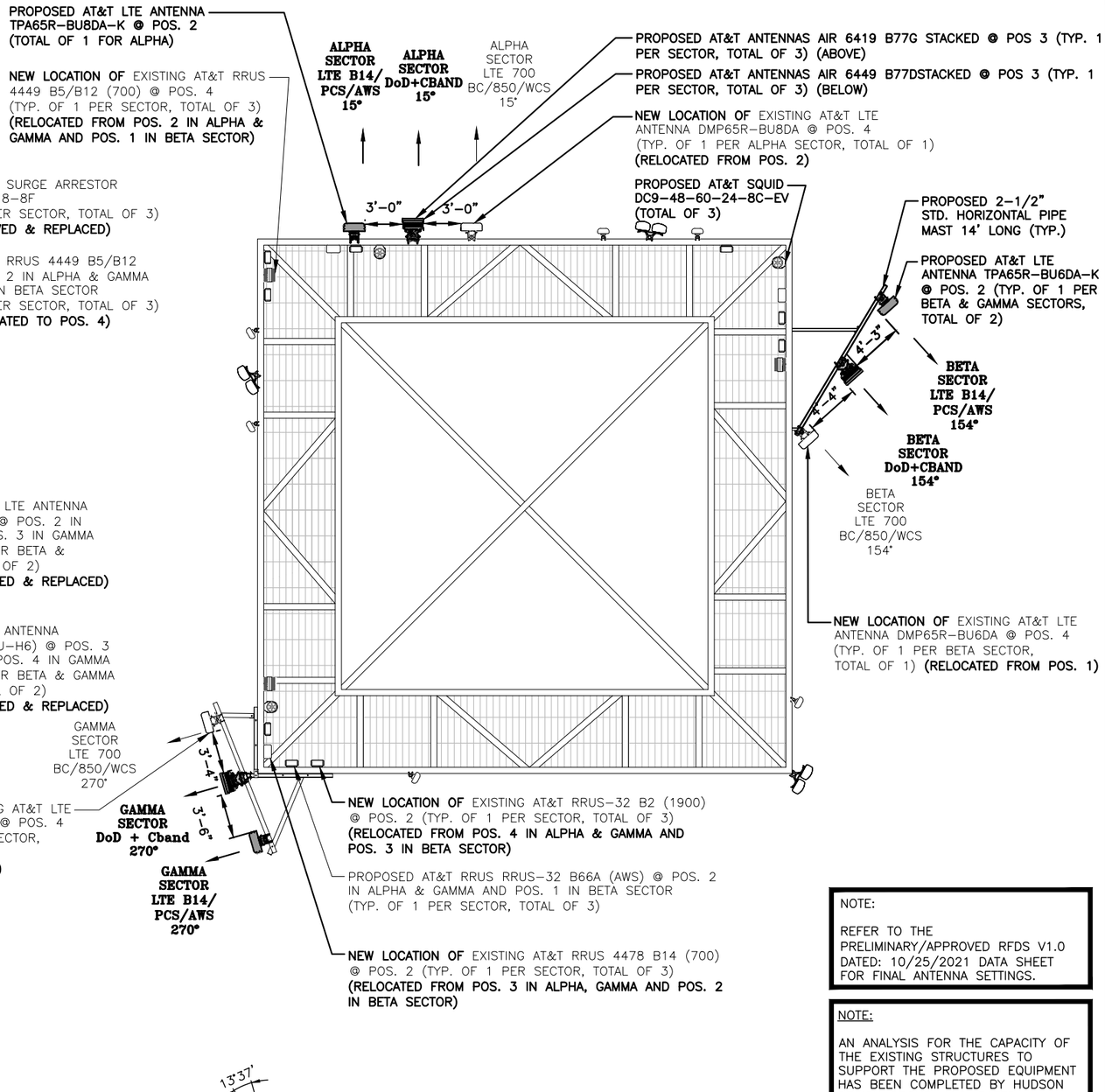


EXISTING ANTENNA LAYOUT

22x34 SCALE: 3/16"=1'-0" (1 A-2)
11x17 SCALE: 3/32"=1'-0" 0 2'-8" 5'-4" 10'-8" 16'-0"



PROPOSED ANTENNA LAYOUT

22x34 SCALE: 3/16"=1'-0" (2 A-2)
11x17 SCALE: 3/32"=1'-0" 0 2'-8" 5'-4" 10'-8" 16'-0"

NOTE:
REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 10/25/2021 DATA SHEET FOR FINAL ANTENNA SETTINGS.

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NOTE:
ANTENNAS AND MOUNTS TO BE ADJUSTED AS REQUIRED TO ACHIEVE A 3'-0" MINIMUM SEPARATION BETWEEN ANTENNAS

HUDSON Design Group LLC
45 BEECHWOOD DRIVE
NORTH ANDOVER, MA 01845
TEL: (978) 557-5553
FAX: (978) 336-5586

CENTERLINE COMMUNICATIONS
750 WEST CENTER STREET, SUITE #301
WEST BRIDGEWATER, MA 02379

SITE NUMBER: CT2036
SITE NAME: CHESHIRE SW

751 HIGGINS ROAD
CHESHIRE, CT 06410
NEW HAVEN COUNTY

at&t
550 COCHITUATE ROAD
FRAMINGHAM, MA 01701

NO.	DATE	REVISIONS	BY	CHK	APP'D
B	05/27/22	ISSUED FOR PERMITTING	MB	AT	DPH
A	03/14/22	ISSUED FOR REVIEW	GD	AT	DPH

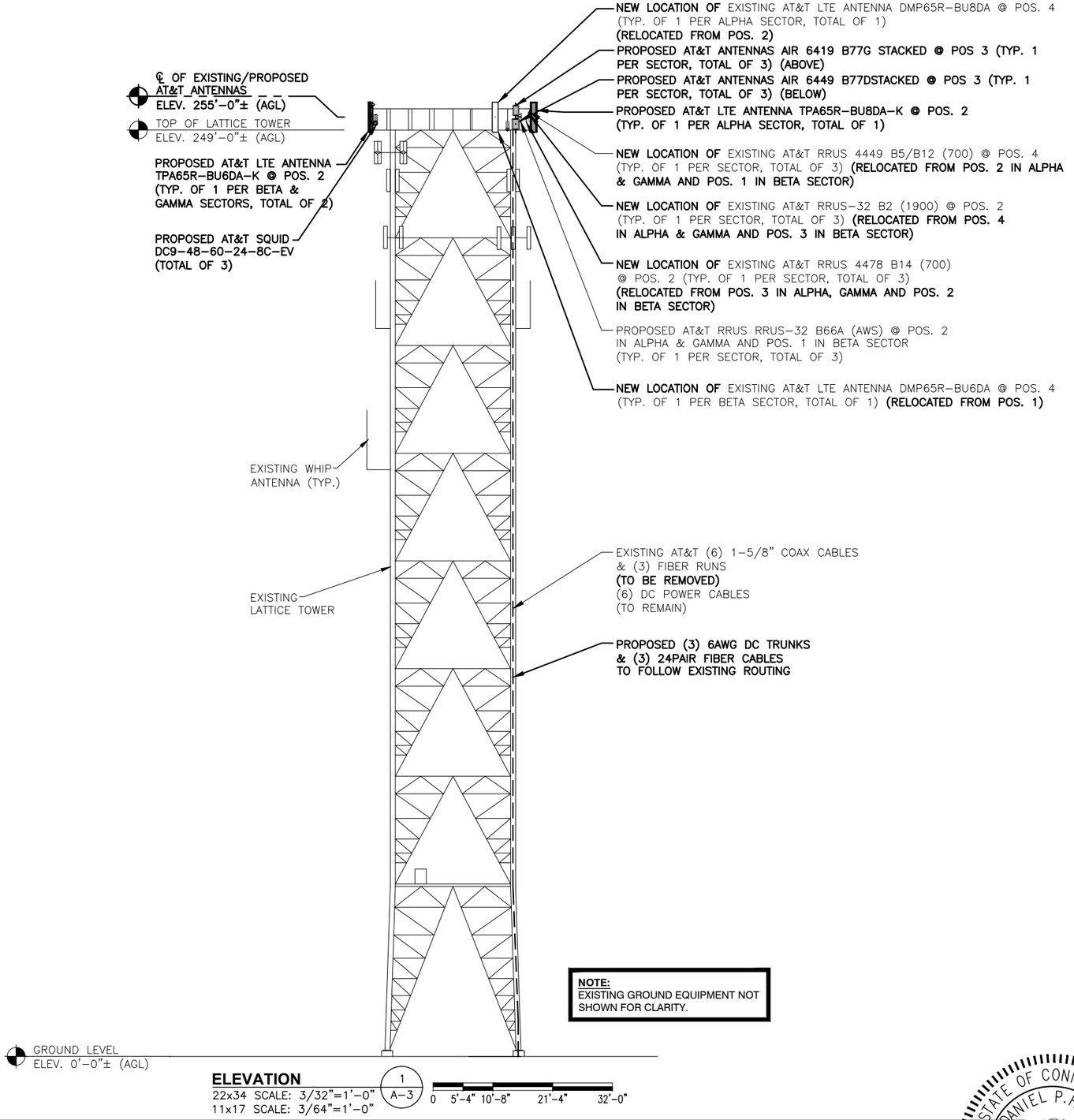
SCALE: AS SHOWN | DESIGNED BY: AT | DRAWN BY: GD

STATE OF CONNECTICUT · DANIEL P. HAMM · No. 24178 · LICENSED PROFESSIONAL ENGINEER

AT&T

ANTENNA LAYOUT PLANS & ELEVATION
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	A-2	B



ELEVATION 1 / A-3
22x34 SCALE: 3/32"=1'-0"
11x17 SCALE: 3/64"=1'-0"
0 5'-4" 10'-8" 21'-4" 32'-0"

NOTE:
REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 10/25/2021 DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT HAS BEEN COMPLETED BY HUDSON DESIGN GROUP, LLC. DATED: 03/24/2022

NOTE:
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ANTENNA LAYOUT PLANS & ELEVATION
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	A-3	B

ANTENNA SCHEDULE

SECTOR	EXISTING/ PROPOSED	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA ℄ HEIGHT	AZIMUTH	TMA/ DIPLEXER	RRU	SIZE (INCHES) (L x W x D)	FEEDER	RAYCAP
A1	–	–	–	–	–	–	–	–	–	–	(P) (1) RAYCAP DC9-48-60-24-8C-EV
A2	**PROPOSED**	**LTE B14/ PCS/AWS**	**TPA65R-BU8DA-K**	**96"X20.7"X7.7"**	**255'-0"±**	**15°**	–	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS)	– – – –	(E)(2) DC POWER **(P)(1) 6AWG DC POWER &** **(1) 24PAIR FIBER**	
A3	**PROPOSED**	**DOD CBAND**	**AIR6419 B77G AIR6449 B77D**	**31.1"X16.1"X7.3" 30.4"X15.9"X8.1"**	**255'-0"±**	**15°**	–	–	–	–	
A4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU8DA	96"X20.7"X7.7"	255'-0"±	15°	–	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	– –	**(P)(1)(Y-CABLE)**	
B1	–	–	–	–	–	–	–	–	–	–	(P) (1) RAYCAP DC9-48-60-24-8C-EV
B2	**PROPOSED**	**LTE B14/ PCS/AWS**	**TPA65R-BU6DA-K**	**71.2"X20.7"X7.7"**	**255'-0"±**	**154°**	–	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS)	– – – –	(E)(2) DC POWER **(P)(1) 6AWG DC POWER &** **(1) 24PAIR FIBER**	
B3	**PROPOSED**	**DOD CBAND**	**AIR6419 B77G AIR6449 B77D**	**31.1"X16.1"X7.3" 30.4"X15.9"X8.1"**	**255'-0"±**	**154°**	–	–	–	–	
B4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU6DA	71.2"X20.7"X7.7"	255'-0"±	154°	–	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	– –	**(P)(1)(Y-CABLE)**	
C1	–	–	–	–	–	–	–	–	–	–	(P) (1) RAYCAP DC9-48-60-24-8C-EV
C2	**PROPOSED**	**LTE B14/ PCS/AWS**	**TPA65R-BU6DA-K**	**71.2"X20.7"X7.7"**	**255'-0"±**	**270°**	–	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS)	– – – –	(E)(2) DC POWER **(P)(1) 6AWG DC POWER &** **(1) 24PAIR FIBER**	
C3	**PROPOSED**	**DOD CBAND**	**AIR6419 B77G AIR6449 B77D**	**31.1"X16.1"X7.3" 30.4"X15.9"X8.1"**	**255'-0"±**	**270°**	–	–	–	–	
C4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU6DA	71.2"X20.7"X7.7"	255'-0"±	270°	–	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	– –	**(P)(1)(Y-CABLE)**	

RRU CHART

QUANTITY	MODEL	SIZE (L x W x D)
E(3)	4478 B14 (700)	18.1"x13.4"x8.3"
E(3)	RRUS-32 B2 (1900)	27.2"x12.1"x7.0"
E(3)	RRUS-32 B66 (AWS)	27.2"x12.1"x7.0"
E(3)	4449 B5/B12 (700)	17.9"x13.2"x10.4"
E(3)	RRUS-32 B30 (WCS)	27.2"x12.1"x7.0"

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS

NOTE:

REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 10/25/2021 DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:

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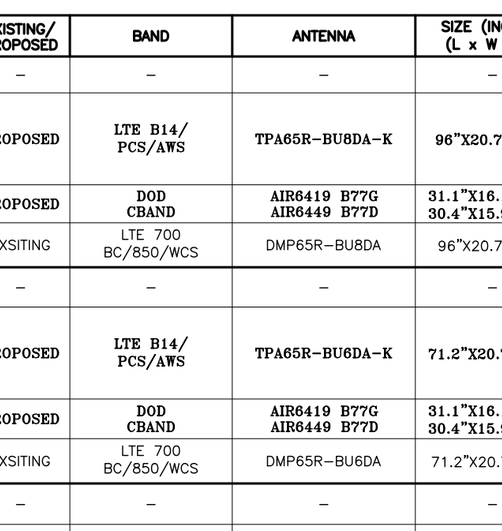
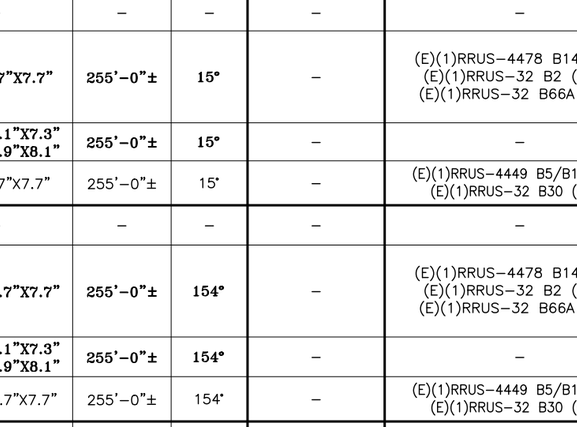
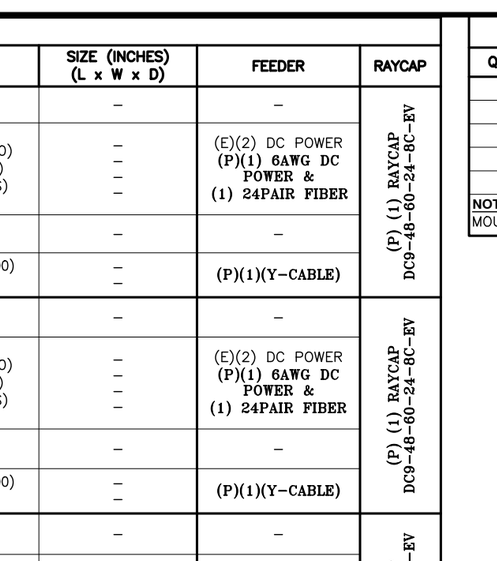
FINAL ANTENNA SCHEDULE (1 / A-4)
SCALE: N.T.S



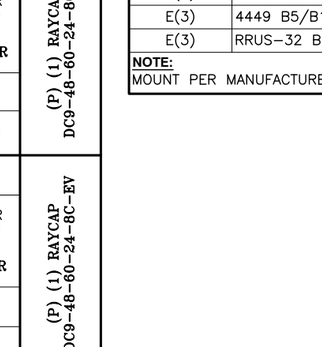
PROPOSED ANTENNA @ POS. 2 (ALPHA SECTOR) (2 / A-4)
22x34 SCALE: 3/4"=1'-0"
11x17 SCALE: 3/8"=1'-0"
0 8" 1'-4" 2'-8" 4'-0"

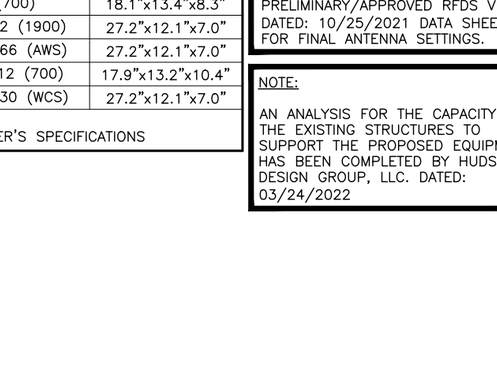


PROPOSED ANTENNA @ POS. 2 (BETA & GAMMA SECTOR) (3 / A-4)
22x34 SCALE: 3/4"=1'-0"
11x17 SCALE: 3/8"=1'-0"
0 8" 1'-4" 2'-8" 4'-0"



PROPOSED ANTENNA @ POS. 3 (4 / A-4)
22x34 SCALE: 1"=1'-0"
11x17 SCALE: 1/2"=1'-0"
0 0'-6" 1'-0" 2'-0" 3'-0"





NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS.

PROPOSED SURGE PROTECTOR MOUNTING DETAIL (5 / A-4)
SCALE: N.T.S

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at&t
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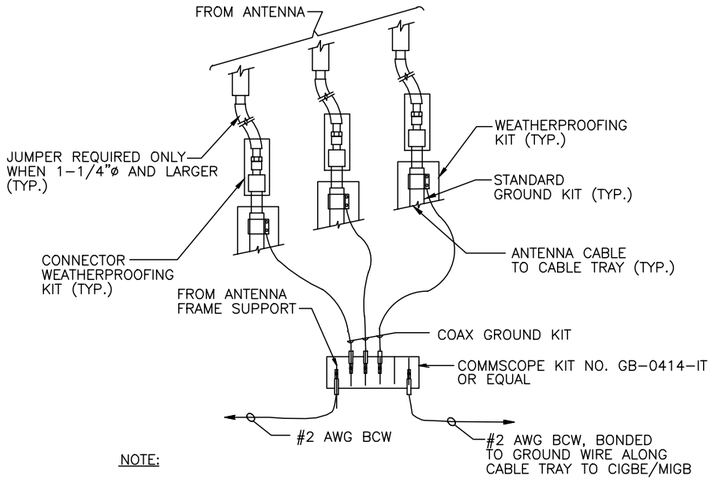
SCALE: AS SHOWN | DESIGNED BY: AT | DRAWN BY: GD

STATE OF CONNECTICUT
DANIEL P. HAMM
No. 24178
LICENSED PROFESSIONAL ENGINEER

AT&T

DETAILS
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	A-4	B

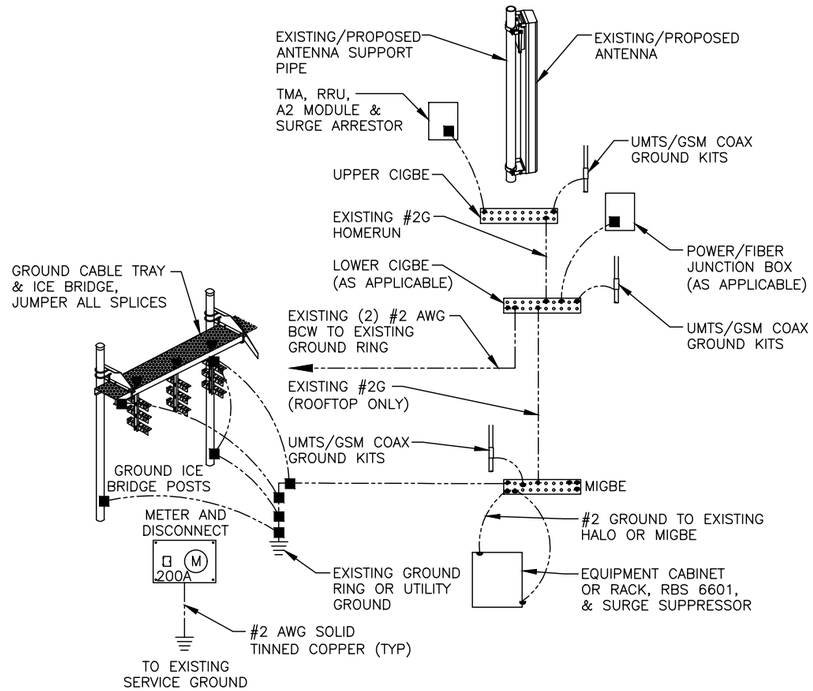


NOTE:

1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE.

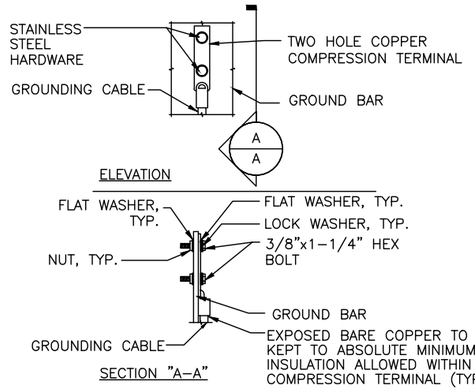
GROUND WIRE TO GROUND BAR CONNECTION DETAIL (1 / G-1)

SCALE: N.T.S



GROUNDING RISER DIAGRAM (2 / G-1)

SCALE: N.T.S



NOTES:

1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL (3 / G-1)

SCALE: N.T.S

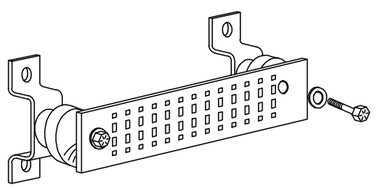
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" – SURGE PRODUCERS

CABLE ENTRY PORTS (HATCH PLATES) (#2 AWG)
GENERATOR FRAMEWORK (IF AVAILABLE) (#2 AWG)
TELCO GROUND BAR
COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2 AWG)
+24V POWER SUPPLY RETURN BAR (#2 AWG)
-48V POWER SUPPLY RETURN BAR (#2 AWG)
RECTIFIER FRAMES.

SECTION "A" – SURGE ABSORBERS

INTERIOR GROUND RING (#2 AWG)
EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2 AWG)
METALLIC COLD WATER PIPE (IF AVAILABLE) (#2 AWG)
BUILDING STEEL (IF AVAILABLE) (#2 AWG)



GROUND BAR - DETAIL (AS REQUIRED)

SCALE: N.T.S

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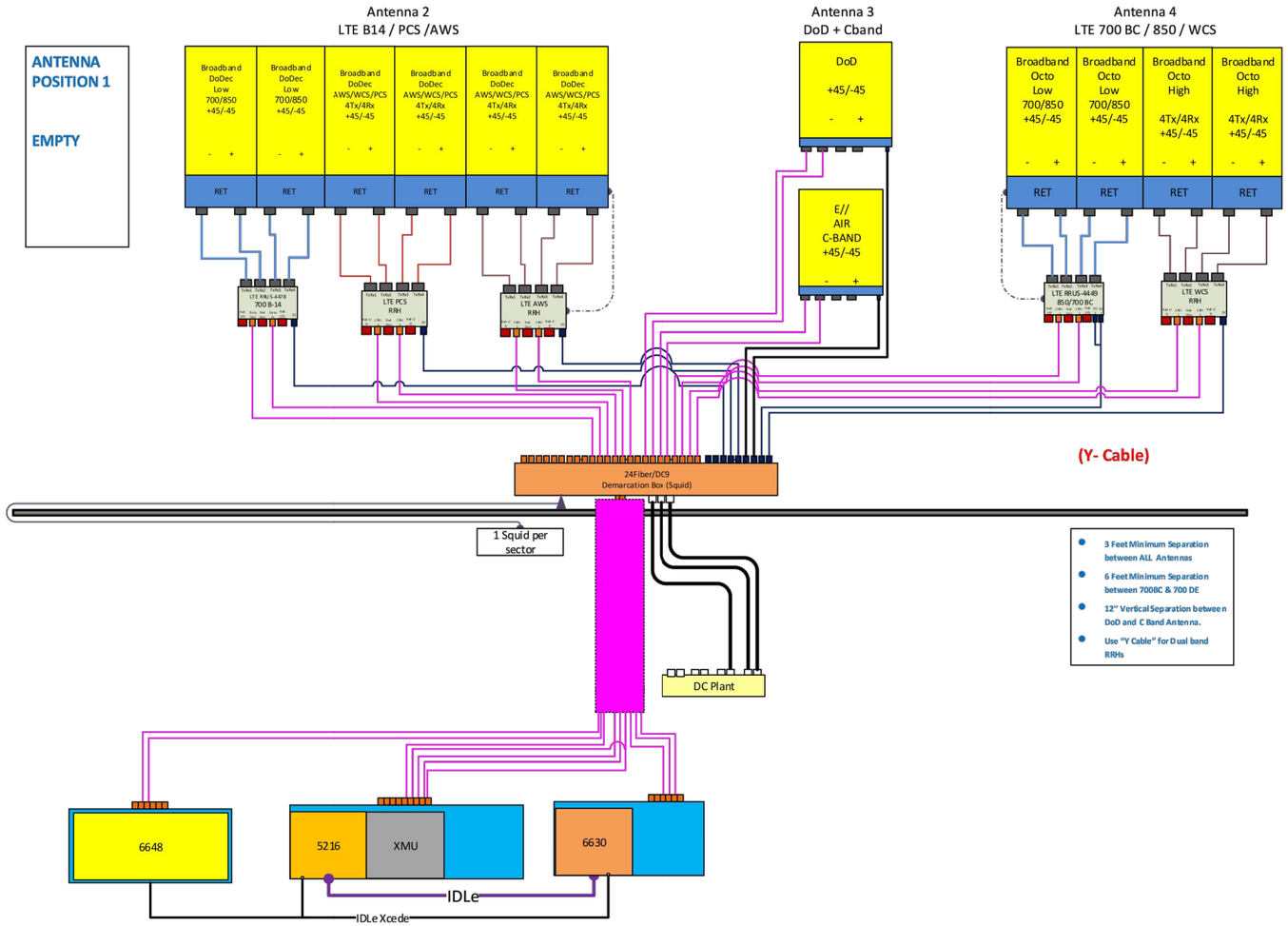
STATE OF CONNECTICUT · DANIEL P. HAMM · No. 24178 · LICENSED PROFESSIONAL ENGINEER

AT&T

GROUNDING DETAILS
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	G-1	B



RF PLUMBING DIAGRAM (1 / RF–1)
SCALE: N.T.S

NOTE:
1. CONTRACTOR TO CONFIRM ALL PARTS.
2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS

NOTE:

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AT&T

RF PLUMBING DIAGRAM
5G NR RADIO || 5G NR 1SR CBAND

SITE NUMBER	DRAWING NUMBER	REV
CT2036	RF–1	B

EXHIBIT 2

Town of Cheshire, CT

Property Listing Report

Map Block Lot	69 53	Building #	1	Unique Identifier	00712600

Property Information

Property Location	751 HIGGINS RD
Mailing Address	P O BOX 7207 BEDMINSTER NJ 07921
Land Use	Light Industrial
Zoning Code	R-40
Neighborhood	I-1C

Owner	AMER TEL & TEL CO
Co-Owner	AT&T PROPERTY TAX UNIT
Book / Page	0148/0566
Land Class	Industrial
Census Tract	3434
Acreage	19.8

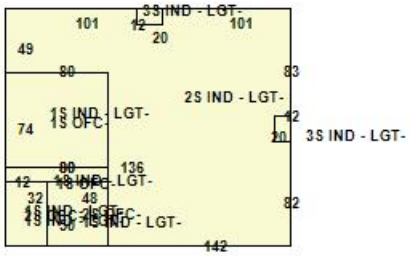
Valuation Summary

(Assessed value = 70% of Appraised Value)

Item	Appraised	Assessed
Buildings	2312630	1618840
Outbuildings	29640	20750
Land	429316	300520
Total	2771586	1940110

Utility Information

Electric	No
Gas	No
Sewer	No
Public Water	No
Well	No



Primary Construction Details

Year Built	1968
Building Desc.	Commercial
Building Style	
Stories	2.00
Exterior Walls	Pre-Cast Concrete
Exterior Walls 2	B. V. Solid
Interior Walls	
Interior Walls 2	
Interior Floors 1	Composite
Interior Floors 2	

Heating Fuel	
Heating Type	
AC Type	Central
Bedrooms	0
Full Bathrooms	0
Half Bathrooms	0
Extra Fixtures	0
Total Rooms	0
Bath Style	NA
Kitchen Style	
Occupancy	0

Building Use	Light Industrial
Building Condition	Average
Frame Type	Average
Fireplaces	0
Bsmt Gar	0
Fin Bsmt Area	
Fin Bsmt Quality	
Building Grade	-50
Roof Style	HIP
Roof Cover	Asphalt

Report Created On 3/23/2022

Town of Cheshire, CT

Property Listing Report | Map Block Lot **69 53** | Building # **1** | Unique Identifier **00712600**

Detached Outbuildings

Type	Description	Area (sq ft)	Condition	Year Built
Fencing	Fencing	2400	Average	1968
Paving	Paving	43000	Average	1968
Fencing	Fencing	1560	Average	1968
Fencing	Fencing	600	Average	1968

Attached Extra Features

Type	Description	Area (sq ft)	Condition	Year Built

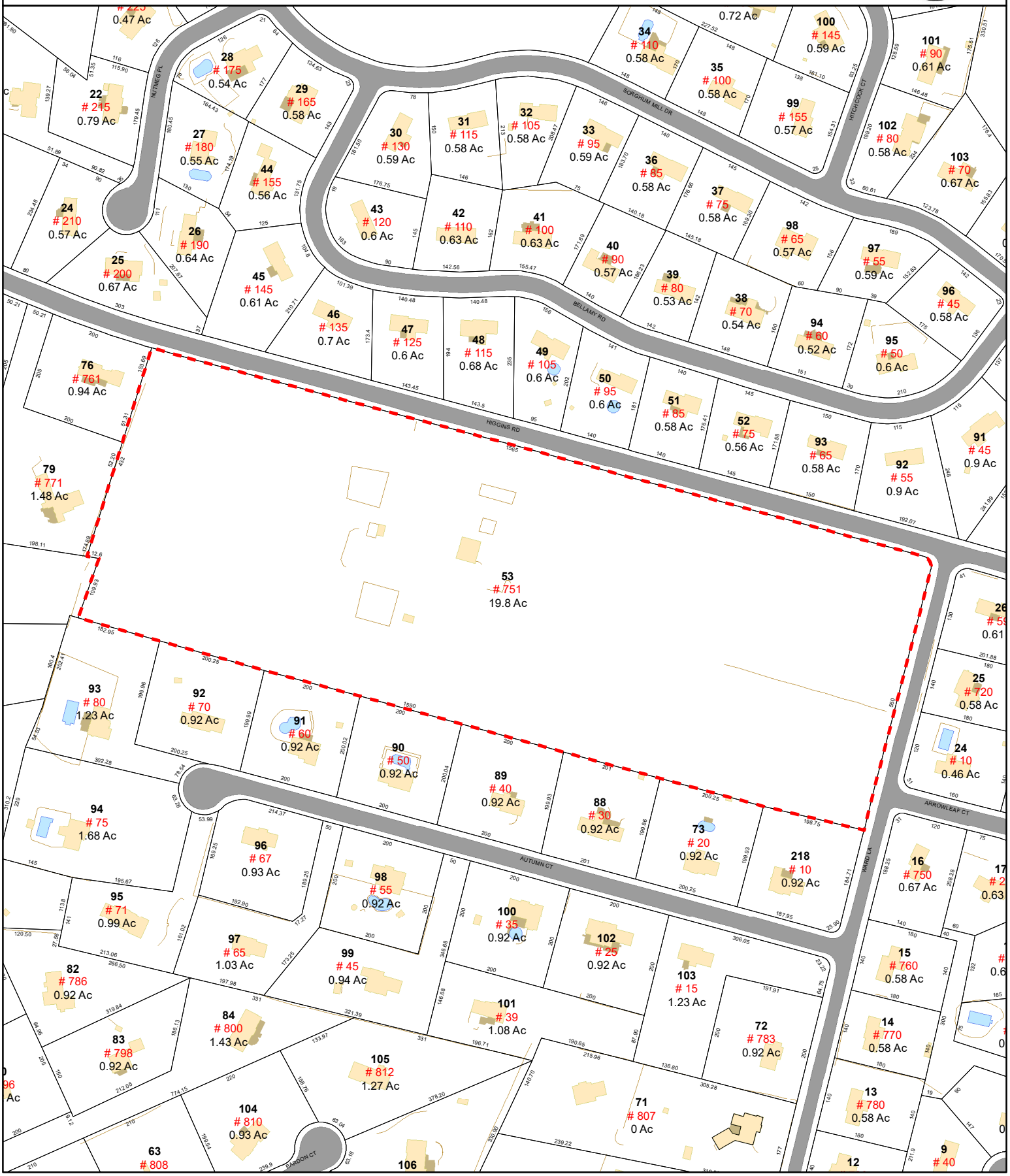
Sales History

Owner of Record	Book/ Page	Sale Date	Sale Price

Report Created On **3/23/2022**

Town of Cheshire, Connecticut - Assessment Parcel Map

Parcel: 00712600 **Location: 751 HIGGINS RD**



Approximate Scale: 1 inch = 242 feet

0 130 260 390 520

Feet

Map Produced: July 2021

Disclaimer: This map is for informational purposes only All information is subject to verification by any user. The Town of Cheshire and its mapping contractors assume no legal responsibility for the information contained herein.

EXHIBIT 3

Centerline Communications LLC
750 W Center St, Suite 301,
West Bridgewater, MA 02379

GPD Engineering and Architecture
Professional Corporation
Brian Daugherty
520 South Main Street, Suite 2531
Akron, OH 44311
(216) 927-8687
bdaugherty@gpdgroup.com

GPD# 2022702.66
May 20, 2022

STRUCTURAL ANALYSIS REPORT

AT&T DESIGNATION:	**USID #:**	**TAG0053**	**26014**
	Site FA #:	**10136365**	**10034996**
	Client #:	**CT2036**	
	Site Name:	**CHESHIRE**	
ANALYSIS CRITERIA:	**Codes:**	**TIA-222-H** **128 mph (3-second gust) w/ 0" ice** **50 mph (3-second gust) w/ 1" ice**	
SITE DATA:		**751 Higgins Road, Cheshire, CT 06410, New Haven County** **Latitude 41° 29' 14.87" N, Longitude 72° 55' 45.59" W** **Market: Connecticut** **250.0' Radio Relay Towers Wireline Self Support**	

To whom it may concern,

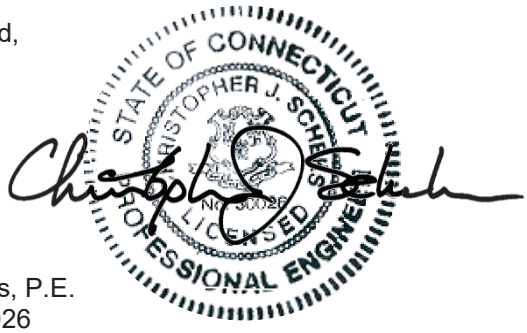
GPD is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

Analysis Results

Tower Stress Level with Proposed Equipment:	72.1%	Pass
Building Pedestal Ratio with Proposed Equipment:	22.7%	Pass

We at GPD appreciate the opportunity of providing our continuing professional services to you and Centerline Communications. If you have any questions or need further assistance on this or any other projects, please do not hesitate to call.

Respectfully submitted,



Christopher J. Scheks, P.E.
Connecticut #: 0030026

5/20/2022

SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT&T Mobility and commissioned by Centerline Communications.

The analysis has been performed in accordance with the TIA-222-H Standard based upon a 3-second gust wind speed of 128 mph. Applicable Standard references and design criteria are listed in report appendices.

Detailed foundation and geotechnical information for the building were not available or provided for this report. Therefore, the in-place capacities could not be verified. However, based on the reserve capacity of the supporting pedestals, it is our opinion that the supporting building and foundations will be adequate for the proposed loading configuration.

TOWER SUMMARY AND RESULTS

Member	Capacity	Results
Legs	72.1%	Pass
Leg Bolts	51.9%	Pass
Diagonals	41.3%	Pass
Horizontals	37.4%	Pass
Redundant Members	49.2%	Pass
Internal Bracing	42.0%	Pass
Member Bolts	58.3%	Pass
Anchor Rods	25.9%	Pass
Building Pedestals	22.7%	Pass
Foundation	Adequate	Pass

RECOMMENDATIONS

The tower and its foundation(s) have sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

ANALYSIS METHOD

RISA-3D (Version 17.0.4), tnxTower (Version 8.1.1.0), and EnerCalc (Build 12.20.8.24), commercially available software programs, were used to create a three-dimensional model of the tower and calculate primary member stresses for various load cases. Selected output from the analysis is included the report appendices. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information.

DOCUMENTS PROVIDED

Document	Remarks	Source
RF Data Sheet	RFDS Site ID CTL02036 Rev. 1, dated 11/10/2021	CLC
Tower Design	AT&T Co. Drawing #: NA4J03-902 Rev 3, dated 6/5/1967	AT&T
Building Drawings	AT&T Co. L-4 Junction Building, dated 12/1/1965	AT&T
Tower Mapping	GPD Project #: 2013723.01.TAG0053.03, dated 1/17/2014	AT&T
Ground Mapping	GPD Project #: 2013723.01.TAG0053.01, dated 6/14/2013	AT&T
Foundation Mapping	FDH Project #: 11-12049E-N1, dated 12/20/2011	AT&T
Geotechnical Report	Not Provided	N/A
Modification Drawings	GPD Project #: 2012856.05, dated 7/25/2012	AT&T
Post Modification Inspection	Centek Project #: 12033.OO40, dated 4/24/2013	AT&T
Mount Modification Drawing	GPD Project #: 2017723.13, dated 6/27/2017	GPD
Previous Tower Analysis	GPD Project #: 2021706.25, dated 12/13/2021	GPD
Mount Analysis	HDG Project #: CT2036, dated 3/24/2022	HDG

ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The appurtenance configuration is as supplied, determined from available photos, and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
4. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
5. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
6. All prior structural modifications, if applicable, are assumed to be as per data supplied/available and to have been properly installed.
7. Loading interpreted from photos is accurate to ±5' AGL, antenna size accurate to ±3.3 sf, and coax equal to the number of existing antennas without reserve.
8. All existing and proposed loading has been taken from the available site photos as well as documents supplied to GPD at the time of generating this report. All such documents are listed in the Documents Provided Table and are assumed to be accurate. GPD is not responsible for loading scenarios outside those conveyed in the supplied documentation.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD should be allowed to review any new information to determine its effect on the structural integrity of the tower.

DISCLAIMER OF WARRANTIES

GPD has not performed a recent site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD in connection with this Rigorous Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

This analysis is limited to the designated maximum wind and seismic conditions per the governing tower standards and code. Wind forces resulting in tower vibrations near the structure's resonant frequencies were not considered in this analysis and are outside the scope of this analysis. Lateral loading from any dynamic response was not evaluated under a time-domain based fatigue analysis.

GPD does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the capability of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the code specified amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

GPD makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD pursuant to this report will be limited to the total fee received for preparation of this report.

APPENDIX A

Tower Analysis Summary Form

Tower Analysis Summary Form

General Info

Site Name	CHESHIRE
Site Number	TAG0053
FA Number	10034996
Date of Analysis	5/20/2022
Company Performing Analysis	GPD

The information contained in this summary report is not to be used independently from the PE stamped tower analysis.

Tower Info	Description	Date
Tower Type (G, SST, MP)	SST	
Tower Height (top of steel AGL)	250'	
Tower Manufacturer	Radio Relay Towers	
Tower Model	Type "J"	
Tower Design	AT&T Co. Drawing #: NA4J03-902 Rev 3	6/5/1967
Building Drawings	AT&T Co. L-4 Junction Building	12/1/1965
Tower Mapping	TEP Project #: 111343	4/8/2011
Tower Mapping	Hudson Design Group	2/4/2013
Tower Mapping	GPD Project #: 2013724.01.TAG0053.03	1/17/2014
Ground Mapping	GPD Project #: 2013723.01.TAG0053.01	6/14/2013
Foundation Mapping	FDH Project #: 11-12049E-N1	12/20/2011
Modification Drawings	GPD Project #: 2012856.05	7/25/2012
Post Modification Inspection	Centek Project #: 12033.OO40	4/24/2013
Previous Structural Analysis	GPD Project #: 2021706.25	12/13/2021

Design Parameters

Design Code Used	TIA-222-H
Location of Tower (County, State)	New Haven, CT
Nominal Wind Speed (mph)	128 3-Second Gust
Ice Thickness (in)	1
Risk Category (I, II, III)	III
Exposure Category (B, C, D)	B
Topographic Category (1 to 5)	1

Analysis Results (% Maximum Usage)

Existing/Reserved + Future + Proposed Condition	
Tower (%)	72.1%
Anchor Rods (%)	25.9%
Building Pedestals (%)	22.7%
Foundation Adequate?	Yes

Existing / Reserved Loading

Antenna								Mount			Transmission Line			
Antenna Owner	Mount Height (ft)	Antenna CL (ft)	Quantity	Type	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Type	Quantity	Model	Size	Attachment Leg/Face
Unknown	252	265	1	Rod	Unknown	4' Lightning Rod		1	Unknown	Top Platform	1	Unknown	5/8"	Face A
Unknown	252	263	1	Beacon	Unknown	Flash Beacon				on the same mount				
AT&T Mobility	252	255	1	Panel	Kathrein	DMP65R-BU8DA	15/154/270	2	Unknown	Standoff Frames	6	Unknown	1-5/8"	Face D
AT&T Mobility	252	255	2	Panel	Kathrein	DMP65R-BU6DA	15/154/270	2	Unknown	Standoff Frames	6	DC Power	0.78"	Face D
AT&T Mobility	252	255	1*	Panel	Kathrein	800-10966	15			on the same mounts	3	Fiber	3/8"	Face D
AT&T Mobility	252	255	2*	Panel	Kathrein	800-10965	154/270			on the same mounts				
AT&T Mobility	252	255	2*	Panel	CCI	HPA-65R-BUU-H6	15/154/270			on the same mounts				
AT&T Mobility	252	255	1*	Panel	CCI	HPA-65R-BUU-H8	15/154/270			on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 32 B2				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 32 B30				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 4478 B14				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	4449 B5/B12				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS-32 B66A				on the same mounts				
AT&T Mobility	252	255	2	Surge	Raycap	DC6-48-60-18-8F				on the same mounts				
AT&T Mobility	252	255	2*	Surge	Raycap	DC6-48-60-18-8F				on the same mounts				
Verizon	252	255	3	Panel	Antel	BXA-70063-6CF	30/140/260	2	Unknown	7' P2 STD Mount Pipe	12	Unknown	1-5/8"	Face D
Verizon	252	254	3	Panel	Commscope	JAHHSS-65C-R3BT4	20/110/200	4	SitePro	VZWSMART-MSK7	3	Hybrid	1-5/8"	Face D
Verizon	252	254	3	RRU	Samsung	CBRS RT4401-48				on the same mounts				
Verizon	252	254	3	Panel	Samsung	MT6407-77A	30/110/200			on the same mounts				
Verizon	252	254	3	Panel	Andrew	JAHH-65C-R3B-V2	20/110/200	5	Unknown	9' P2.5 STD Mount Pipe				
Verizon	252	254	3	Diplexer	Commscope	CBC78T-DS-43-2X				on the same mounts				
Verizon	252	254	3	RRU	Samsung	B5/B13 RRH-BR04C (RFV01U-D2A)				on the same mounts				
Verizon	252	254	3	RRU	Samsung	B2/B66A RRH-BR049 (RFV01U-D1A)				on the same mounts				
Verizon	252	254	3	Surge	Raycap	RHSDC-3315-PF-48				on the same mounts				
Verizon	252	254	1	GPS	Lucen	GPS				on the same mounts				
Town of Cheshire	249	255	1	Dipole	RFI	0A20-41 DIN		1	Unknown	6' Sidearm	1	Unknown	7/8"	Face D
Town of Cheshire	249	252.5	1	Dipole	RFI	0A20-67 DIN		1	Unknown	6' Sidearm	1	Unknown	7/8"	Face D
Town of Cheshire	240	240	1	Dish	RFS	SC3-W100AC		1	Unknown	Mount Pipe	1	RFS	E105	Face D
Misc.	239.5							1	Unknown	Platform				
Sprint	225	225.5	3	Panel	Celwave	APXVTM14-ALU-120	30/130/210	8	Unknown	20' Pipe Mounts	4	Hybrid	1"	Face D
Sprint	225	225.5	3	Panel	Comscope	NNVV-65B-R4	30/130/210			on the same mounts				
Sprint	225	225.5	3	RRU	Alcatel Lucent	TD-RRH 8x25				on the same mounts				
Sprint	225	225.5	6	RRU	Alcatel Lucent	800 MHz 2x50W				on the same mounts				
Sprint	225	225.5	3	RRU	Alcatel Lucent	1900 MHz 4x45				on the same mounts				
Nextel	210	212	6	Panel	Decibel	DB844H90E-XY	30/255	2	Unknown	14' Sector Frames	6	Unknown	1-5/8"	Face D
T-Mobile	210	212	2	Panel	Ericsson	AIR21 B4A/B2P	60/140	2	Unknown	14' Sector Frames	2	Hybrid	7/8"	Face B
T-Mobile	210	212	2	Panel	Ericsson	KRC 118 048/1 B4A/B12P-B8P	60/140			on the same mounts				
T-Mobile	210	212	2	RRU	Ericsson	RRUS11 B12				on the same mounts				
T-Mobile	210	212	2	RRU	Ericsson	RRUS11 B2				on the same mounts				
Unknown	210	207	1	Panel	Unknown	26"x26"x2" Flat Panel	160			on the same mounts	1	Unknown	1/2"	Face A
Nextel	198	200	3	Panel	Decibel	DB844H90E-XY	135	1	Unknown	14' Sector Frame	3	Unknown	1-5/8"	Face D
SGI	190	196	2	Omni	Unknown	PG1-NOF-0091		2	Unknown	5' Standoffs	2	Unknown	7/8"	Face D
SGI	171	177	1	Omni	Unknown	PG1-DOF-0093		1	Unknown	5' Standoff	1	Unknown	7/8"	Face D
Misc.	139.5							1	Unknown	Platforms w/ Rails				
AT&T Internet Services	85	88	1	Yagi	Wade	WL 7-13/S		3	Unknown	Standoffs	7	Unknown	5/8"	Face D
AT&T Internet Services	85	85	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	84	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	83	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	81	1	Yagi	Wade	WL 14-69/S				on the same mounts				
Unknown	37	37	1	Camera	Vicon	Camera - V8300H		1	Unknown	2.5' Box Mount	1	Conduit	1"	Face A
Unknown	36.5	36.5	1	GPS	Lucent	407517689		1	Unknown	3' Side Arm	1	Unknown	1/2"	Face D
Unknown	21	21	2	Junction	Unknown	Junction Box		1	Unknown	Platform	1	Conduit	1"	Face A
Unknown	21	21	1	RRU	Unknown	28" x 15.5" x 10" RRU				on the same mount				

*Indicates equipment to be removed

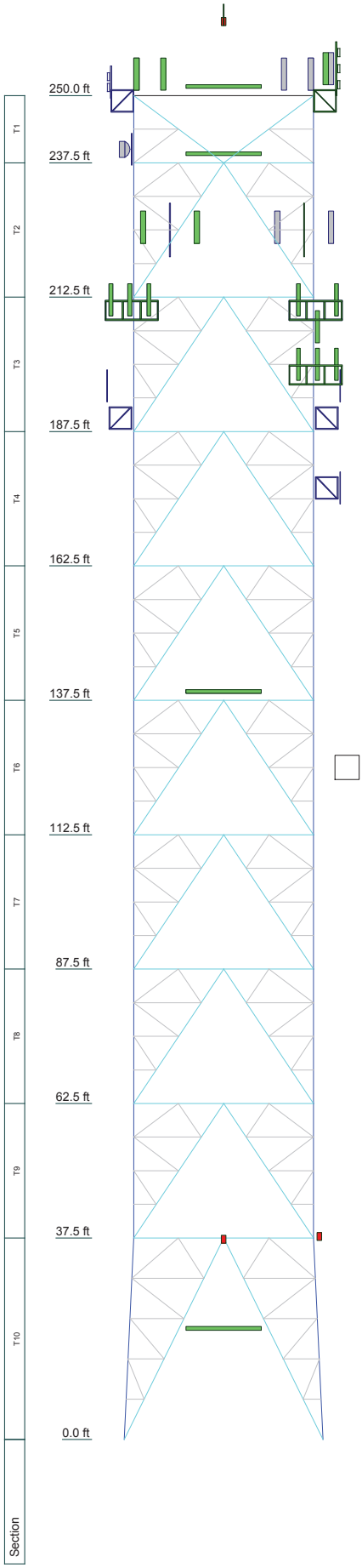
Proposed Loading

Antenna								Mount			Transmission Line			
Antenna Owner	Mount Height (ft)	Antenna CL (ft)	Quantity	Type	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Type	Quantity	Model	Size	Attachment Leg/Face
AT&T Mobility	252	255	2	Panel	CCI	TPA65R-BU6DA-K	15/154/270			on the existing mounts				
AT&T Mobility	252	255	1	Panel	CCI	TPA65R-BU8DA-K	15/154/270			on the existing mounts				
AT&T Mobility	252	255	3	Panel	Ericsson	AIR6449 B77D+AIR6419 B77G Stacked	15/154/270			on the existing mounts				
AT&T Mobility	252	254	1	Surge	Raycap	DC9-48-60-24-PC16-EV				on the proposed mounts				

Note: The proposed equipment shall be installed in addition to the existing/reserved loading at the same elevation.

APPENDIX B

Software Output Files and Calculations



MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A36	36 ksi	58 ksi			

TOWER DESIGN NOTES

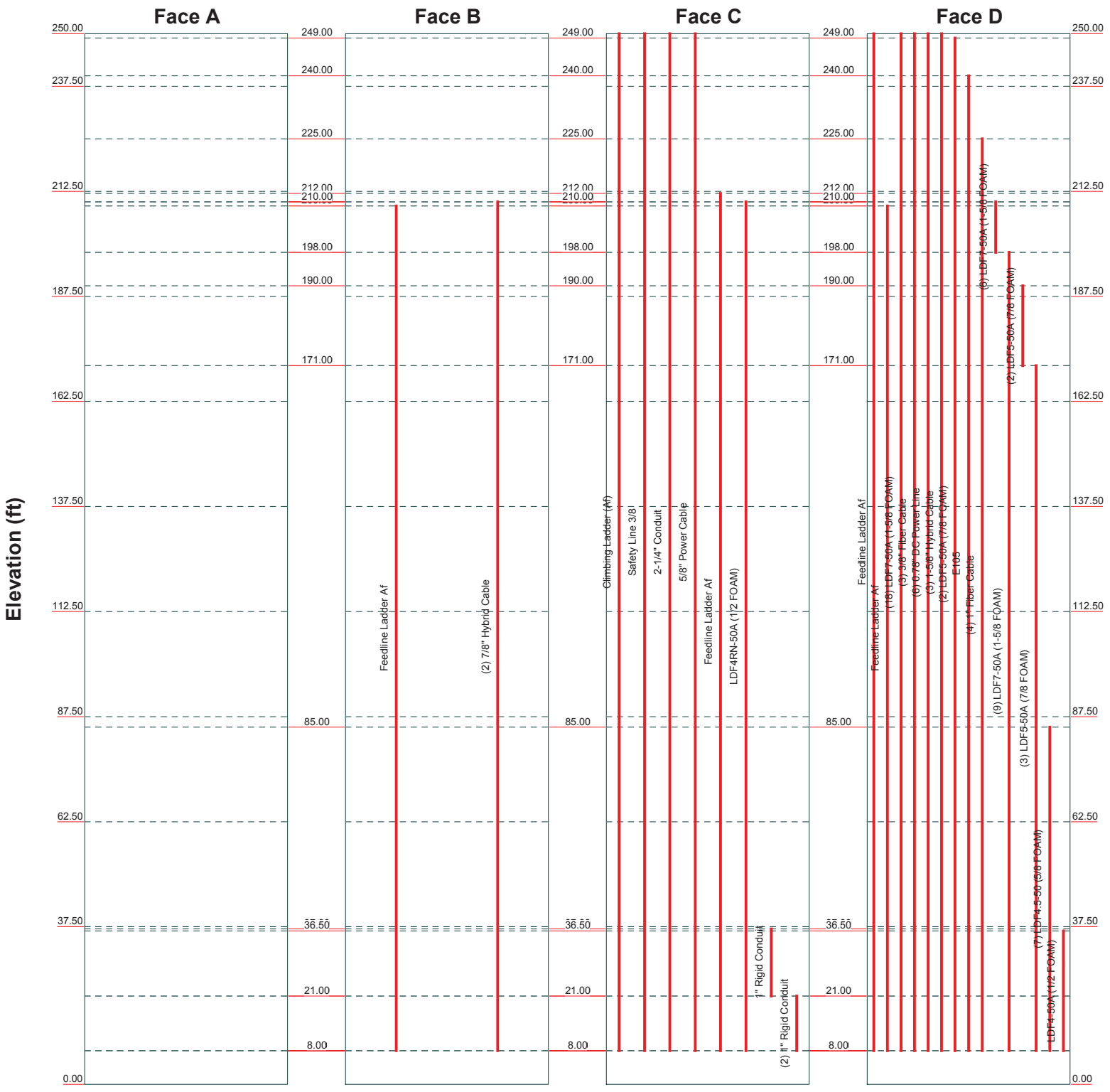
1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 128 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 1 with Crest Height of 0.00 ft

GPD
520 South Main Street Suite 2531
Akron, Ohio 44311
Phone: (330) 572-2100
FAX: (330) 572-2101

Job: ***TAG0053 - CHESHIRE***			
Project: ***2022702.66***			
Client: Centerline Communications	Drawn by: CKuhn	App'd:	
Code: TIA-222-H	Date: 05/19/22	Scale: NTS	
Path: T:\ATand\TAG0053 and 26014\24 2022702.66 Centerline Wireline SA\5_Structural\00_Structure\00_Rev 0\03_Modeling\TNX\TAG0053.eri		Dwg No. E-1	

Feed Line Distribution Chart
0' - 250'

Round | Flat | App In Face | App Out Face | Truss Leg



GPD
520 South Main Street Suite 2531
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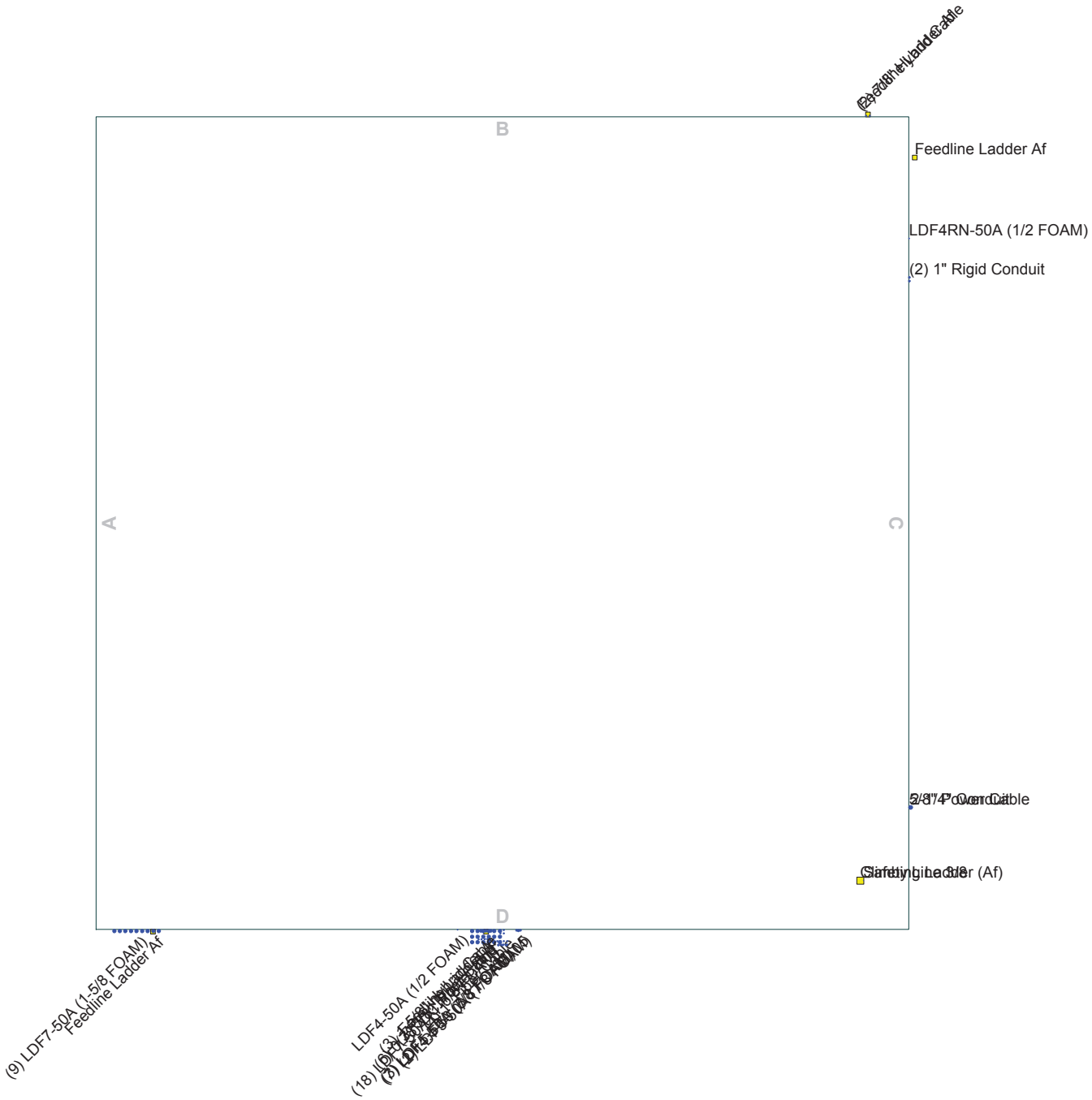
Phone: (330) 572-2100
FAX: (330) 572-2101

Job: ***TAG0053 - CHESHIRE***			
Project: ***2022702.66***			
Client: Centerline Communications		Drawn by: CKuhn	App'd:
Code: TIA-222-H		Date: 05/19/22	Scale: NTS
Path: T:\ATand\TAG0053 and 26014\24.2022702.66 Centerline Wireline SA\5_Structural\00_Structure\00_Rev.0\03_Modeling\TNX\TAG0053.eri			Dwg No. E-7

Feed Line Plan

Round Flat App In Face App Out Face



GPD 520 South Main Street Suite 2531 Akron, Ohio 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job: TAG0053 - CHESHIRE		
	Project: 2022702.66		
	Client: Centerline Communications	Drawn by: CKuhn	App'd:
	Code: TIA-222-H	Date: 05/19/22	Scale: NTS
	Path: T:\ATand\TAG0053 and 26014\24 2022702 66 Centerline Wireline SA\5_Structural\00_Structure\00_Rev 0\03_Modeling\TNX\TAG0053.eri		Dwg No. E-7

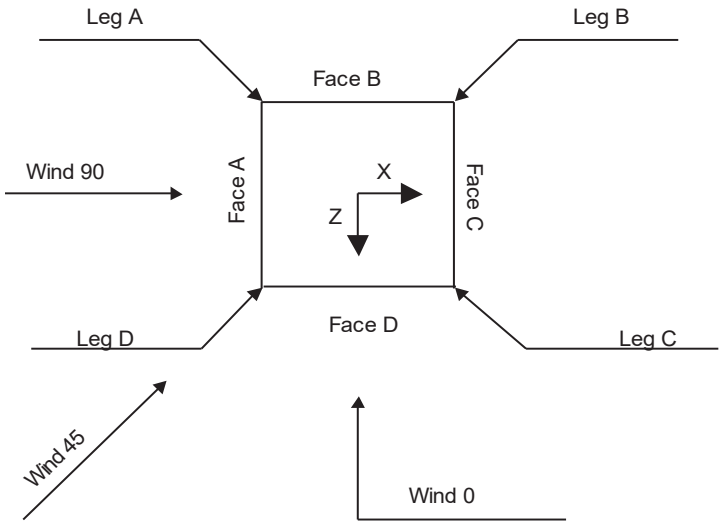
Tower Input Data

The main tower is a 4x free standing tower with an overall height of 250.00 ft above the ground line.
The base of the tower is set at an elevation of 0.00 ft above the ground line.
The face width of the tower is 33.50 ft at the top and 37.00 ft at the base.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

Tower is located in New Haven County, Connecticut.
Tower base elevation above sea level: 261.00 ft.
Basic wind speed of 128 mph.
Risk Category III.
Exposure Category B.
Simplified Topographic Factor Procedure for wind speed-up calculations is used.
Topographic Category: 1.
Crest Height: 0.00 ft.
Nominal ice thickness of 1.0000 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 50 mph is used in combination with ice.
Temperature drop of 50 °F.
Deflections calculated using a wind speed of 60 mph.
Pressures are calculated at each section.
Stress ratio used in tower member design is 1.
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

	Consider Moments - Legs		Distribute Leg Loads As Uniform		Use ASCE 10 X-Brace Ly Rules
	Consider Moments - Horizontals		Assume Legs Pinned	√	Calculate Redundant Bracing Forces
	Consider Moments - Diagonals		Assume Rigid Index Plate		Ignore Redundant Members in FEA
	Use Moment Magnification	√	Use Clear Spans For Wind Area		SR Leg Bolts Resist Compression
√	Use Code Stress Ratios	√	Use Clear Spans For KL/r		All Leg Panels Have Same Allowable
√	Use Code Safety Factors - Guys		Retension Guys To Initial Tension		Offset Girt At Foundation
	Escalate Ice	√	Bypass Mast Stability Checks	√	Consider Feed Line Torque
	Always Use Max Kz	√	Use Azimuth Dish Coefficients	√	Include Angle Block Shear Check
	Use Special Wind Profile	√	Project Wind Area of Appurt.		Use TIA-222-H Bracing Resist. Exemption
√	Include Bolts In Member Capacity		Autocalc Torque Arm Areas		Use TIA-222-H Tension Splice Exemption
	Leg Bolts Are At Top Of Section		Add IBC .6D+W Combination		Poles
√	Secondary Horizontal Braces Leg	√	Sort Capacity Reports By Component		Include Shear-Torsion Interaction
√	Use Diamond Inner Bracing (4 Sided)	√	Triangulate Diamond Inner Bracing		Always Use Sub-Critical Flow
	SR Members Have Cut Ends		Treat Feed Line Bundles As Cylinder		Use Top Mounted Sockets
	SR Members Are Concentric		Ignore KL/ry For 60 Deg. Angle Legs		Pole Without Linear Attachments
					Pole With Shroud Or No Appurtenances
					Outside and Inside Corner Radii Are Known



Square Tower

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	*Face or Leg*	*Allow Shield*	*Exclude From Torque Calculation*	*Component Type*	*Placement ft*	*Face Offset in*	*Lateral Offset (Frac FW)*	*#*	*# Per Row*	*Clear Spacing in*	*Width or Diameter in*	*Perimeter in*	*Weight plf*
***													
Climbing Ladder (Af)	C	No	No	Af (CaAa)	250.00 - 8.00	-24.0000	0.44	1	1	3.8400	3.8400		4.81
Safety Line 3/8	C	No	No	Ar (CaAa)	250.00 - 8.00	-24.0000	0.44	1	1	0.3750	0.3750		0.22
2-1/4" Conduit	C	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.35	1	1	2.2500	2.2500		0.32
5/8" Power Cable	C	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.35	1	1	0.6300	0.5000		0.15
***													
Feedline Ladder Af	D	No	No	Af (CaAa)	250.00 - 8.00	0.0000	0.02	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	C	No	No	Af (CaAa)	212.00 - 8.00	2.0000	-0.45	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	B	No	No	Af (CaAa)	209.00 - 8.00	0.0000	0.45	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	D	No	No	Af (CaAa)	209.00 - 8.00	0.0000	0.43	1	1	2.5000	2.5000		7.00
***													
LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.02	18	6	1.0000	1.9800		0.82
3/8" Fiber Cable	D	No	No	Ar (CaAa)	250.00 - 8.00	5.0000	0.02	3	3	0.3750	0.3750		0.10
0.78" DC Power Line	D	No	No	Ar (CaAa)	250.00 - 8.00	5.0000	0.02	6	6	0.7800	0.7800		0.33
1-5/8" Hybrid Cable	D	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.02	3	3	1.0000	1.6250		0.82
***													
LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	249.00 - 8.00	0.0000	-0.02	2	2	1.0000	1.0900		0.33

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
***													
E105	D	No	No	Ar (CaAa)	240.00 - 8.00	0.0000	-0.02	1	1	1.0000	1.3000		0.40
***													
1" Fiber Cable	D	No	No	Ar (CaAa)	225.00 - 8.00	0.0000	0	4	2	0.8800	0.8800		0.60
***													
LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	210.00 - 198.00	0.0000	0.45	6	6	1.0000	1.9800		0.82
LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	198.00 - 8.00	0.0000	0.45	9	9	1.0000	1.9800		0.82
***													
7/8" Hybrid Cable	B	No	No	Ar (CaAa)	210.00 - 8.00	0.0000	0.45	2	2	0.8750	0.8750		0.28
LDF4RN-50A (1/2 FOAM)	C	No	No	Ar (CaAa)	210.00 - 8.00	0.0000	-0.35	1	1	0.6300	0.6300		0.15
***													
LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	190.00 - 171.00	8.0000	0	2	2	1.0000	1.0900		0.33
LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	171.00 - 8.00	8.0000	0	3	3	1.0000	1.0900		0.33
***													
LDF4.5-50 (5/8 FOAM)	D	No	No	Ar (CaAa)	85.00 - 8.00	6.0000	0	7	4	0.8700	0.8700		0.15
***													
1" Rigid Conduit	C	No	No	Ar (CaAa)	37.00 - 21.00	0.0000	-0.3	1	1	1.0000	1.0000		0.50
1" Rigid Conduit	C	No	No	Ar (CaAa)	21.00 - 8.00	0.0000	-0.3	2	2	1.0000	1.0000		0.50
***													
LDF4-50A (1/2 FOAM)	D	No	No	Ar (CaAa)	36.50 - 8.00	0.0000	0.055	1	1	0.6300	0.6300		0.15
***													

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft Vert ft ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
***									
Lighting Rod 5/8" x 4'	B	None		0.0000	265.00	No Ice	0.25	0.25	31.00
						1/2" Ice	0.66	0.66	33.82
						1" Ice	0.97	0.97	39.29
Flash Beacon Lighting	B	None		0.0000	263.00	No Ice	2.70	2.70	50.00
						1/2" Ice	3.10	3.10	70.00
						1" Ice	3.50	3.50	90.00
13' I-Beam Mast Mount	B	None		0.0000	256.50	No Ice	13.00	13.00	300.00
						1/2" Ice	14.14	14.14	550.00
						1" Ice	15.08	15.08	800.00
***									
DMP65R-BU8DA w/ Mount Pipe	B	From Face	4.00 -10.00	-7.0000	252.00	No Ice	17.87	10.02	29.30
						1/2" Ice	18.50	11.44	147.98

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft / Vert ft / ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
			3.00			1" Ice	19.14	12.72	277.00
DMP65R-BU6DA w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	12.71	5.62	794.00
			-10.50			1/2" Ice	13.21	6.07	867.96
			3.00			1" Ice	13.71	6.53	948.56
DMP65R-BU6DA w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	12.71	5.62	794.00
			-20.75			1/2" Ice	13.21	6.07	867.96
			3.00			1" Ice	13.71	6.53	948.56
TPA-65R-BU8DA-K w/ Mount Pipe	B	From Face	4.00	-7.0000	252.00	No Ice	17.87	10.02	116.30
			-10.00			1/2" Ice	18.50	11.44	234.98
			3.00			1" Ice	19.14	12.72	364.01
TPA-65R-BU6DA-K w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	13.20	7.52	98.20
			-10.50			1/2" Ice	13.91	8.80	193.25
			3.00			1" Ice	14.59	9.93	297.04
TPA-65R-BU6DA-K w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	13.20	7.52	98.20
			-20.75			1/2" Ice	13.91	8.80	193.25
			3.00			1" Ice	14.59	9.93	297.04
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	B	From Face	4.00	-7.0000	252.00	No Ice	11.76	9.94	229.20
			-10.00			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	11.76	9.94	229.20
			-10.50			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	11.76	9.94	229.20
			-20.75			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
DC9-48-60-24-PC16-EV	B	From Face	4.00	-7.0000	252.00	No Ice	2.26	1.12	0.03
			-10.00			1/2" Ice	2.44	1.26	18.91
			2.00			1" Ice	2.64	1.40	40.64
RRUS 32 B2	B	From Face	4.00	-7.0000	252.00	No Ice	2.73	1.67	52.90
			-10.00			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B2	C	From Face	4.00	42.0000	252.00	No Ice	2.73	1.67	52.90
			-10.50			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B2	D	From Face	4.00	68.0000	252.00	No Ice	2.73	1.67	52.90
			-20.75			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B30	B	From Face	4.00	-7.0000	252.00	No Ice	2.69	1.57	60.00
			-10.00			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 32 B30	C	From Face	4.00	42.0000	252.00	No Ice	2.69	1.57	60.00
			-10.50			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 32 B30	D	From Face	4.00	68.0000	252.00	No Ice	2.69	1.57	60.00
			-20.75			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 4478 B14	B	From Face	4.00	-7.0000	252.00	No Ice	1.84	1.06	59.90
			-10.00			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
RRUS 4478 B14	C	From Face	4.00	42.0000	252.00	No Ice	1.84	1.06	59.90
			-10.50			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
RRUS 4478 B14	D	From Face	4.00	68.0000	252.00	No Ice	1.84	1.06	59.90
			-20.75			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
4449 B5/B12	B	From Face	4.00	-7.0000	252.00	No Ice	1.97	1.41	71.00
			-10.00			1/2" Ice	2.14	1.56	89.51

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft / Vert ft / ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
			3.00			1" Ice	2.33	1.73	110.84
4449 B5/B12	C	From Face	4.00	42.0000	252.00	No Ice	1.97	1.41	71.00
			-10.50			1/2" Ice	2.14	1.56	89.51
			3.00			1" Ice	2.33	1.73	110.84
4449 B5/B12	D	From Face	4.00	68.0000	252.00	No Ice	1.97	1.41	71.00
			-20.75			1/2" Ice	2.14	1.56	89.51
			3.00			1" Ice	2.33	1.73	110.84
RRUS-32 B66A	B	From Face	4.00	-7.0000	252.00	No Ice	2.86	1.78	55.12
			-10.00			1/2" Ice	3.09	1.97	77.44
			3.00			1" Ice	3.32	2.17	103.04
RRUS-32 B66A	C	From Face	4.00	42.0000	252.00	No Ice	2.86	1.78	55.12
			-10.50			1/2" Ice	3.09	1.97	77.44
			3.00			1" Ice	3.32	2.17	103.04
RRUS-32 B66A	D	From Face	4.00	68.0000	252.00	No Ice	2.86	1.78	55.12
			-20.75			1/2" Ice	3.09	1.97	77.44
			3.00			1" Ice	3.32	2.17	103.04
DC6-48-60-18-8F Surge Suppression Unit	C	From Face	4.00	42.0000	252.00	No Ice	0.92	0.92	18.90
			-10.50			1/2" Ice	1.46	1.46	36.62
			3.00			1" Ice	1.64	1.64	56.82
DC6-48-60-18-8F Surge Suppression Unit	D	From Face	4.00	68.0000	252.00	No Ice	0.92	0.92	18.90
			-20.75			1/2" Ice	1.46	1.46	36.62
			3.00			1" Ice	1.64	1.64	56.82
10' In-Face Frame	C	From Face	4.00	0.0000	252.00	No Ice	12.84	1.42	250.00
			-21.00			1/2" Ice	15.40	1.70	325.00
			3.00			1" Ice	17.96	1.98	400.00
10' In-Face Frame	D	From Face	4.00	0.0000	252.00	No Ice	12.84	1.42	250.00
			-21.00			1/2" Ice	15.40	1.70	325.00
			3.00			1" Ice	17.96	1.98	400.00
Tower Top Platform	B	None		0.0000	252.00	No Ice	85.00	85.00	4425.00
						1/2" Ice	97.00	97.00	5752.50
						1" Ice	110.00	110.00	7080.00
***									
JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	B	From Face	4.00	5.0000	252.00	No Ice	12.82	10.78	126.52
			16.25			1/2" Ice	13.42	12.20	227.13
			2.00			1" Ice	14.02	13.29	338.68
JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	C	From Face	4.00	5.0000	252.00	No Ice	12.82	10.78	126.52
			16.75			1/2" Ice	13.42	12.20	227.13
			2.00			1" Ice	14.02	13.29	338.68
JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	D	From Face	4.00	5.0000	252.00	No Ice	12.82	10.78	126.52
			16.25			1/2" Ice	13.42	12.20	227.13
			2.00			1" Ice	14.02	13.29	338.68
MT6407-77A w/ 7' P2.5 STD Mount Pipe & (2) VZWSMART-MSK7	B	From Face	4.00	15.0000	252.00	No Ice	5.42	3.27	103.40
			11.25			1/2" Ice	5.97	3.99	148.53
			2.00			1" Ice	6.45	4.59	199.20
MT6407-77A w/ 8' P2.5 STD Mount Pipe	C	From Face	4.00	5.0000	252.00	No Ice	5.42	3.27	103.40
			3.00			1/2" Ice	5.97	3.99	148.53
			2.00			1" Ice	6.45	4.59	199.20
MT6407-77A w/ 7' P2.5 STD Mount Pipe & (2) VZWSMART-MSK7	D	From Face	4.00	5.0000	252.00	No Ice	5.42	3.27	103.40
			11.25			1/2" Ice	5.97	3.99	148.53
			2.00			1" Ice	6.45	4.59	199.20
BXA-70063-6CF w/ 9' P2.5 STD Mount Pipe	A	From Face	4.00	-25.0000	252.00	No Ice	7.57	5.49	45.95
			1.00			1/2" Ice	8.02	6.23	104.10
			3.00			1" Ice	8.47	6.99	170.26
BXA-70063-6CF w/ 8' P2.5 STD Mount Pipe	B	From Face	4.00	15.0000	252.00	No Ice	7.57	5.49	45.95
			20.00			1/2" Ice	8.02	6.23	104.10
			3.00			1" Ice	8.47	6.99	170.26
BXA-70063-6CF w/ 9' P2.5	D	From Face	5.00	-55.0000	252.00	No Ice	7.57	5.49	45.95

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft Vert ft ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
STD Mount Pipe			-19.00			1/2" Ice	8.02	6.23	104.10
			3.00			1" Ice	8.47	6.99	170.26
JAHHSS-65C-R3BT4 w/	B	From Face	4.00	5.0000	252.00	No Ice	12.86	8.51	240.82
BSAMNT-SBS-2-3 & (3)			16.25			1/2" Ice	13.46	9.11	316.79
SCP10W Clamp			2.00			1" Ice	14.06	9.71	400.60
JAHHSS-65C-R3BT4 w/	C	From Face	4.00	5.0000	252.00	No Ice	12.86	8.51	240.82
BSAMNT-SBS-2-3 & (3)			16.75			1/2" Ice	13.46	9.11	316.79
SCP10W Clamp			2.00			1" Ice	14.06	9.71	400.60
JAHHSS-65C-R3BT4 w/	D	From Face	4.00	5.0000	252.00	No Ice	12.86	8.51	240.82
BSAMNT-SBS-2-3 & (3)			16.25			1/2" Ice	13.46	9.11	316.79
SCP10W Clamp			2.00			1" Ice	14.06	9.71	400.60
CBC78T-DS-43-2X	B	From Face	4.00	5.0000	252.00	No Ice	0.37	0.51	20.70
			16.25			1/2" Ice	0.45	0.60	27.04
			2.00			1" Ice	0.53	0.70	35.07
CBC78T-DS-43-2X	C	From Face	4.00	5.0000	252.00	No Ice	0.37	0.51	20.70
			16.75			1/2" Ice	0.45	0.60	27.04
			2.00			1" Ice	0.53	0.70	35.07
CBC78T-DS-43-2X	D	From Face	4.00	5.0000	252.00	No Ice	0.37	0.51	20.70
			16.25			1/2" Ice	0.45	0.60	27.04
			2.00			1" Ice	0.53	0.70	35.07
B5/B13 RRH-BR04C	B	From Face	4.00	0.0000	252.00	No Ice	1.88	1.01	70.30
(RFV01UD2A)			16.25			1/2" Ice	2.05	1.14	86.73
			2.00			1" Ice	2.22	1.28	105.83
B5/B13 RRH-BR04C	C	From Face	4.00	0.0000	252.00	No Ice	1.88	1.01	70.30
(RFV01UD2A)			16.75			1/2" Ice	2.05	1.14	86.73
			2.00			1" Ice	2.22	1.28	105.83
B5/B13 RRH-BR04C	D	From Face	4.00	0.0000	252.00	No Ice	1.88	1.01	70.30
(RFV01UD2A)			16.25			1/2" Ice	2.05	1.14	86.73
			2.00			1" Ice	2.22	1.28	105.83
B2/B66a RRH-BR049	B	From Face	4.00	0.0000	252.00	No Ice	1.88	1.25	84.40
(RFV01UD1A)			16.25			1/2" Ice	2.05	1.39	102.74
			2.00			1" Ice	2.22	1.54	123.87
B2/B66a RRH-BR049	C	From Face	4.00	0.0000	252.00	No Ice	1.88	1.25	84.40
(RFV01UD1A)			16.75			1/2" Ice	2.05	1.39	102.74
			2.00			1" Ice	2.22	1.54	123.87
B2/B66a RRH-BR049	D	From Face	4.00	0.0000	252.00	No Ice	1.88	1.25	84.40
(RFV01UD1A)			16.25			1/2" Ice	2.05	1.39	102.74
			2.00			1" Ice	2.22	1.54	123.87
CBRS RT4401-48	B	From Face	4.00	0.0000	252.00	No Ice	0.85	0.30	17.60
			16.25			1/2" Ice	0.97	0.37	24.53
			2.00			1" Ice	1.09	0.45	33.25
CBRS RT4401-48	C	From Face	4.00	0.0000	252.00	No Ice	0.85	0.30	17.60
			16.75			1/2" Ice	0.97	0.37	24.53
			2.00			1" Ice	1.09	0.45	33.25
CBRS RT4401-48	D	From Face	4.00	0.0000	252.00	No Ice	0.85	0.30	17.60
			16.25			1/2" Ice	0.97	0.37	24.53
			2.00			1" Ice	1.09	0.45	33.25
RHSDC-3315-PF-48	A	From Face	1.00	0.0000	252.00	No Ice	3.36	2.19	32.00
			5.00			1/2" Ice	3.60	2.39	60.54
			2.00			1" Ice	3.84	2.61	92.61
RHSDC-3315-PF-48	B	From Face	1.00	0.0000	252.00	No Ice	3.36	2.19	32.00
			-5.00			1/2" Ice	3.60	2.39	60.54
			2.00			1" Ice	3.84	2.61	92.61
RHSDC-3315-PF-48	D	From Face	1.00	0.0000	252.00	No Ice	3.36	2.19	32.00
			5.00			1/2" Ice	3.60	2.39	60.54
			2.00			1" Ice	3.84	2.61	92.61
GPS	B	From Face	4.00	0.0000	252.00	No Ice	0.11	0.11	0.87

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft / Vert ft / ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
			11.00			1/2" Ice	0.21	0.21	3.85
			2.00			1" Ice	0.28	0.28	7.85
Pipe Mount 7'x2.875"	B	From Face	4.00	0.0000	252.00	No Ice	2.01	2.01	45.00
			-2.00			1/2" Ice	2.59	2.59	59.81
			2.00			1" Ice	3.02	3.02	79.35
Pipe Mount 7'x2.875"	D	From Face	4.00	0.0000	252.00	No Ice	2.01	2.01	45.00
			11.00			1/2" Ice	2.59	2.59	59.81
			2.00			1" Ice	3.02	3.02	79.35
***									
OA20-67-DIN	A	From Leg	6.00	0.0000	249.00	No Ice	1.31	1.31	9.00
			0.00			1/2" Ice	2.03	2.03	19.35
			3.50			1" Ice	2.60	2.60	34.28
6' Standoff	A	From Leg	3.00	0.0000	249.00	No Ice	2.72	12.93	145.70
			0.00			1/2" Ice	4.11	17.82	223.26
			0.00			1" Ice	5.50	22.71	300.83
OA20-41-DIN	C	From Leg	6.00	0.0000	249.00	No Ice	3.73	3.73	28.00
			0.00			1/2" Ice	5.21	5.21	56.62
			6.00			1" Ice	6.42	6.42	92.76
6' Standoff	C	From Leg	3.00	0.0000	249.00	No Ice	2.72	12.93	145.70
			0.00			1/2" Ice	4.11	17.82	223.26
			0.00			1" Ice	5.50	22.71	300.83
***									
Pipe Mount 4'x4.5"	A	From Leg	0.50	0.0000	240.00	No Ice	0.00	0.00	43.20
			0.00			1/2" Ice	0.00	0.00	56.19
			0.00			1" Ice	0.00	0.00	72.23
***									
Platform	B	None		0.0000	239.50	No Ice	75.38	75.38	10500.00
						1/2" Ice	94.22	94.22	13000.00
						1" Ice	113.06	113.06	15500.00
***									
10' x 2.5" Mount Pipe	B	From Face	1.00	0.0000	225.00	No Ice	2.50	2.50	50.00
			-10.00			1/2" Ice	3.53	3.53	68.64
			0.00			1" Ice	4.58	4.58	93.79
10' x 2.5" Mount Pipe	D	From Face	1.00	0.0000	225.00	No Ice	2.50	2.50	50.00
			-15.00			1/2" Ice	3.53	3.53	68.64
			0.00			1" Ice	4.58	4.58	93.79
APXVTM14-ALU-I20 w/ 10' x 2" Mount Pipe	B	From Face	1.00	0.0000	225.00	No Ice	7.60	5.98	92.72
			15.00			1/2" Ice	8.52	7.37	158.56
			0.50			1" Ice	9.46	8.78	231.95
APXVTM14-ALU-I20 w/ 10' x 2" Mount Pipe	C	From Face	1.00	0.0000	225.00	No Ice	7.60	5.98	92.72
			-15.00			1/2" Ice	8.52	7.37	158.56
			0.50			1" Ice	9.46	8.78	231.95
APXVTM14-ALU-I20 w/ 10' x 2" Mount Pipe	D	From Face	1.00	0.0000	225.00	No Ice	7.60	5.98	92.72
			10.00			1/2" Ice	8.52	7.37	158.56
			0.50			1" Ice	9.46	8.78	231.95
NNVV-65B-R4 w/ Mount Pipe	B	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17	99.30
			15.00			1/2" Ice	12.77	8.13	187.33
			0.50			1" Ice	13.27	8.97	283.67
NNVV-65B-R4 w/ Mount Pipe	C	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17	99.30
			-15.00			1/2" Ice	12.77	8.13	187.33
			0.50			1" Ice	13.27	8.97	283.67
NNVV-65B-R4 w/ Mount Pipe	D	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17	99.30
			10.00			1/2" Ice	12.77	8.13	187.33
			0.50			1" Ice	13.27	8.97	283.67
TD-RRH8x20-25	B	From Face	1.00	0.0000	225.00	No Ice	3.70	1.29	66.00
			15.00			1/2" Ice	3.95	1.46	89.94
			0.50			1" Ice	4.20	1.64	117.22

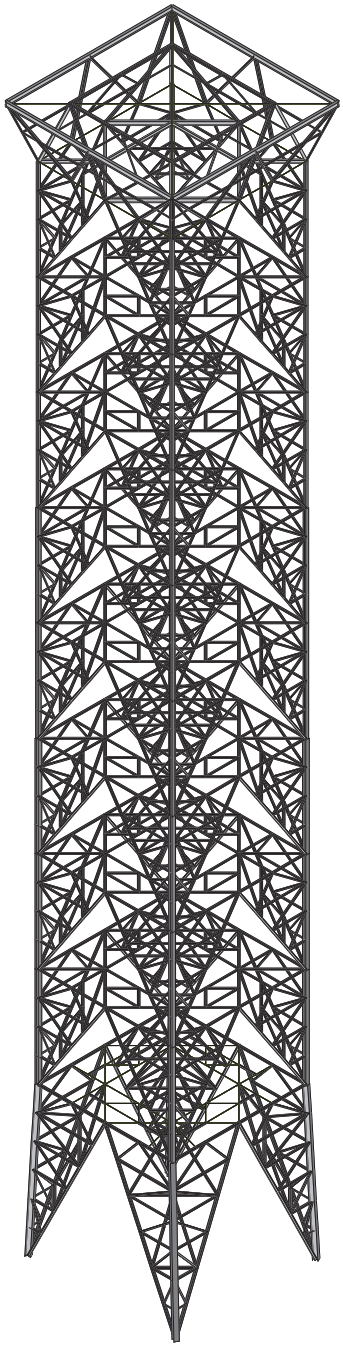
Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft Vert ft ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
TD-RRH8x20-25	C	From Face	1.00 -15.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	3.70 3.95 4.20	1.29 1.46 1.64	66.00 89.94 117.22
TD-RRH8x20-25	D	From Face	1.00 10.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	3.70 3.95 4.20	1.29 1.46 1.64	66.00 89.94 117.22
(2) 800 MHz 2x50W	B	From Face	1.00 15.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.09 2.27 2.46	1.73 1.90 2.08	53.00 73.74 97.45
(2) 800 MHz 2x50W	C	From Face	1.00 -15.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.09 2.27 2.46	1.73 1.90 2.08	53.00 73.74 97.45
(2) 800 MHz 2x50W	D	From Face	1.00 10.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.09 2.27 2.46	1.73 1.90 2.08	53.00 73.74 97.45
1900 4x45 65 MHz RRU	B	From Face	1.00 15.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.08 2.27 2.47	1.99 2.18 2.37	53.00 74.10 98.26
1900 4x45 65 MHz RRU	C	From Face	1.00 -15.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.08 2.27 2.47	1.99 2.18 2.37	53.00 74.10 98.26
1900 4x45 65 MHz RRU	D	From Face	1.00 10.00 0.50	0.0000	225.00	No Ice 1/2" Ice 1" Ice	2.08 2.27 2.47	1.99 2.18 2.37	53.00 74.10 98.26
***									
(3) DB844H90E-XY w/Mount Pipe	A	From Leg	1.00 0.00 2.00	60.0000	210.00	No Ice 1/2" Ice 1" Ice	2.24 2.61 2.99	3.34 3.73 4.13	43.38 78.61 121.53
(3) DB844H90E-XY w/Mount Pipe	D	From Leg	1.00 0.00 2.00	15.0000	210.00	No Ice 1/2" Ice 1" Ice	2.24 2.61 2.99	3.34 3.73 4.13	43.38 78.61 121.53
14' Sector Frame	A	From Leg	0.50 0.00 0.00	60.0000	210.00	No Ice 1/2" Ice 1" Ice	18.21 23.76 29.31	0.00 0.00 0.00	492.00 690.25 888.50
14' Sector Frame	D	From Leg	0.50 0.00 0.00	15.0000	210.00	No Ice 1/2" Ice 1" Ice	18.21 23.76 29.31	0.00 0.00 0.00	492.00 690.25 888.50
***									
AIR21 B4A/B2P w/ mount pipe	B	From Leg	1.00 0.00 2.00	0.0000	210.00	No Ice 1/2" Ice 1" Ice	6.13 6.52 6.92	5.54 6.20 6.87	101.25 156.43 218.21
AIR21 B4A/B2P w/ mount pipe	C	From Leg	1.00 0.00 2.00	-10.0000	210.00	No Ice 1/2" Ice 1" Ice	6.13 6.52 6.92	5.54 6.20 6.87	101.25 156.43 218.21
KRC 118 048/1 B4A/B12P-B8P w/ Mount Pipe	B	From Leg	1.00 0.00 2.00	0.0000	210.00	No Ice 1/2" Ice 1" Ice	11.54 12.16 12.79	10.68 12.09 13.33	154.59 246.84 348.90
KRC 118 048/1 B4A/B12P-B8P w/ Mount Pipe	C	From Leg	1.00 0.00 2.00	-10.0000	210.00	No Ice 1/2" Ice 1" Ice	11.54 12.16 12.79	10.68 12.09 13.33	154.59 246.84 348.90
RRUS 11 B12	B	From Leg	1.00 0.00 2.00	0.0000	210.00	No Ice 1/2" Ice 1" Ice	2.83 3.04 3.26	1.18 1.33 1.48	50.70 71.57 95.49
RRUS 11 B12	C	From Leg	1.00 0.00 2.00	-10.0000	210.00	No Ice 1/2" Ice 1" Ice	2.83 3.04 3.26	1.18 1.33 1.48	50.70 71.57 95.49
RRUS 11 B2	B	From Leg	1.00	0.0000	210.00	No Ice	2.83	1.18	50.70

Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft / Vert ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
			0.00			1/2" Ice	3.04	1.33	71.57
			2.00			1" Ice	3.26	1.48	95.49
RRUS 11 B2	C	From Leg	1.00	-10.0000	210.00	No Ice	2.83	1.18	50.70
			0.00			1/2" Ice	3.04	1.33	71.57
			2.00			1" Ice	3.26	1.48	95.49
26"x 26" Flat Panel	C	From Leg	1.00	0.0000	210.00	No Ice	5.60	0.52	15.00
			0.00			1/2" Ice	5.92	0.67	38.43
			-3.00			1" Ice	6.24	0.83	65.30
14' Sector Frame	B	From Leg	0.50	0.0000	210.00	No Ice	18.21	0.00	492.00
			0.00			1/2" Ice	23.76	0.00	690.25
			0.00			1" Ice	29.31	0.00	888.50
14' Sector Frame	C	From Leg	0.50	-10.0000	210.00	No Ice	18.21	0.00	492.00
			0.00			1/2" Ice	23.76	0.00	690.25
			0.00			1" Ice	29.31	0.00	888.50
***									
(3) DB844H90E-XY w/Mount Pipe	C	From Leg	1.00	-15.0000	198.00	No Ice	2.24	3.34	43.38
			0.00			1/2" Ice	2.61	3.73	78.61
			2.00			1" Ice	2.99	4.13	121.53
14' Sector Frame	C	From Leg	0.50	-15.0000	198.00	No Ice	18.21	0.00	492.00
			0.00			1/2" Ice	23.76	0.00	690.25
			0.00			1" Ice	29.31	0.00	888.50
***									
PG1-NOF-0091	A	From Leg	3.50	-45.0000	190.00	No Ice	1.40	1.40	7.50
			-3.50			1/2" Ice	2.23	2.23	18.71
			6.00			1" Ice	3.07	3.07	35.15
5' Standoff	A	From Leg	1.75	-45.0000	190.00	No Ice	2.72	12.93	145.70
			-1.75			1/2" Ice	4.11	17.82	223.26
			0.00			1" Ice	5.50	22.71	300.83
PG1-NOF-0091	B	From Leg	3.50	45.0000	190.00	No Ice	1.40	1.40	7.50
			3.50			1/2" Ice	2.23	2.23	18.71
			6.00			1" Ice	3.07	3.07	35.15
5' Standoff	B	From Leg	1.75	45.0000	190.00	No Ice	2.72	12.93	145.70
			1.75			1/2" Ice	4.11	17.82	223.26
			0.00			1" Ice	5.50	22.71	300.83
***									
PG1-DOF-0093	B	From Leg	3.50	45.0000	177.00	No Ice	1.40	1.40	7.50
			3.50			1/2" Ice	2.23	2.23	18.71
			0.00			1" Ice	3.07	3.07	35.15
5' Standoff	B	From Leg	1.75	45.0000	177.00	No Ice	2.72	12.93	145.70
			1.75			1/2" Ice	4.11	17.82	223.26
			0.00			1" Ice	5.50	22.71	300.83
***									
Catwalk	B	From Face	0.00	0.0000	139.50	No Ice	75.38	4.08	1250.00
			0.00			1/2" Ice	94.22	5.09	1600.00
			0.00			1" Ice	113.06	6.11	1950.00
Catwalk	C	From Face	0.00	0.0000	139.50	No Ice	75.38	4.08	1250.00
			0.00			1/2" Ice	94.22	5.09	1600.00
			0.00			1" Ice	113.06	6.11	1950.00
***									
WL14-69/S	B	From Leg	1.00	-28.0000	85.00	No Ice	2.88	2.88	5.00
			0.00			1/2" Ice	3.74	3.74	6.50
			0.00			1" Ice	4.61	4.61	8.45
WL14-69/S	C	From Leg	1.00	-39.0000	85.00	No Ice	2.88	2.88	5.00
			0.00			1/2" Ice	3.74	3.74	6.50
			-2.00			1" Ice	4.61	4.61	8.45
WL14-69/S	B	From Leg	1.00	-28.0000	85.00	No Ice	2.88	2.88	5.00
			0.00			1/2" Ice	3.74	3.74	6.50

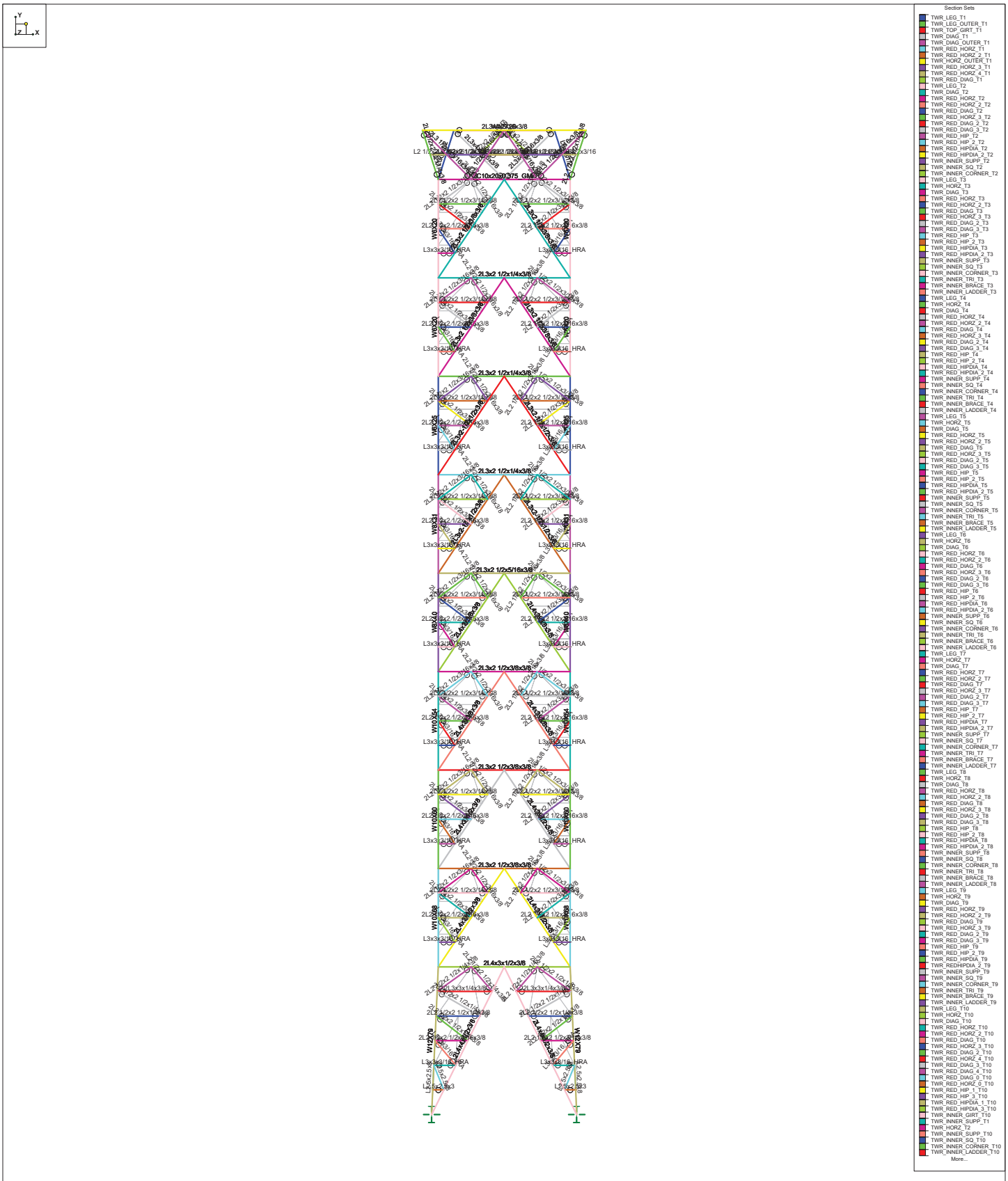
Description	Face or Leg	Offset Type	Offsets: Horz Lateral ft / Vert ft / ft	Azimuth Adjustment °	Placement ft		C_AA_A Front ft^2	C_AA_A Side ft^2	Weight lb
			-4.00			1" Ice	4.61	4.61	8.45
***									
Camera	B	From Leg	1.50	0.0000	37.00	No Ice	0.11	0.05	2.00
			0.00			1/2" Ice	0.16	0.08	3.30
			0.00			1" Ice	0.21	0.12	5.42
2.5' Box Mount	B	From Leg	0.75	0.0000	37.00	No Ice	1.36	1.36	20.00
			0.00			1/2" Ice	2.45	2.45	40.00
			0.00			1" Ice	3.50	3.50	64.00
***									
GPS	D	From Face	3.00	0.0000	36.50	No Ice	0.12	0.12	0.87
			0.00			1/2" Ice	0.21	0.21	3.85
			0.00			1" Ice	0.28	0.28	7.85
3' Side Arm	D	From Face	1.50	0.0000	36.50	No Ice	0.93	0.93	44.94
			0.00			1/2" Ice	1.13	1.13	54.87
			0.00			1" Ice	1.37	1.37	67.25
***									
Junction Box (40"x14"x9")	B	From Face	0.00	0.0000	21.00	No Ice	3.88	2.50	50.00
			10.00			1/2" Ice	3.88	2.50	50.00
			0.00			1" Ice	3.88	2.50	50.00
RRU (28" x 15.5" x 10")	B	From Face	0.00	0.0000	21.00	No Ice	3.62	2.36	65.00
			10.00			1/2" Ice	3.86	2.57	94.93
			0.00			1" Ice	4.11	2.78	128.52
Platform	B	From Face	0.00	0.0000	21.00	No Ice	0.00	0.00	0.00
			10.00			1/2" Ice	0.00	0.00	0.00
			0.00			1" Ice	0.00	0.00	0.00
***									

Dishes

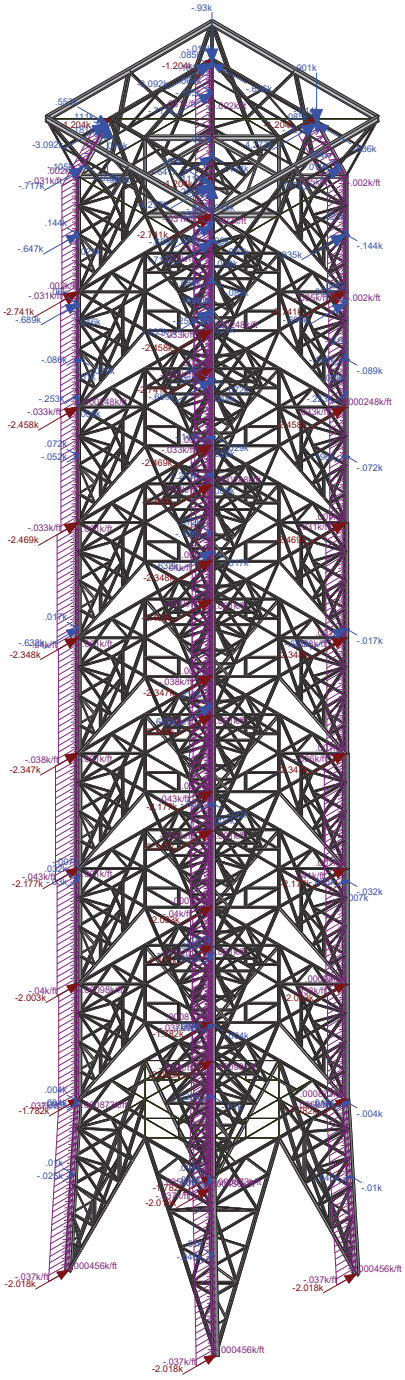
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral ft / Vert ft	Azimuth Adjustment °	3 dB Beam Width °	Elevation ft	Outside Diameter ft		Aperture Area ft^2	Weight lb
SC3-W100AC	A	Paraboloid w/Shroud (HP)	From Leg	1.00	74.0000		240.00	3.00	No Ice	7.07	400.00
				0.00					1/2" Ice	7.47	440.00
				0.00					1" Ice	7.86	480.00



GPD		SK - 1
C. Kuhn	TAG0053 - CHESHIRE	May 19, 2022 at 2:57 PM
2022702.66	Rendered Tower	TAG0053 - Non Angle Capacities.r...



GPD		SK - 2
C. Kuhn	TAG0053 - CHESHIRE	May 20, 2022 at 6:44 AM
2022702.66	Members	TAG0053 - Non Angle Capacities.r...



Loads: BLC 2, No Ice Wind 0 deg

GPD		SK - 3
C. Kuhn	TAG0053 - CHESHIRE	May 20, 2022 at 6:46 AM
2022702.66	Example Forces	TAG0053 - Non Angle Capacities.r...

(Global) Model Settings

Chrok`x Rdbshmmr enqLdl adqB`kbr	4
L`whhsdqmkRdbshmmr enqLdl adqB`kbr	86
Hmbkt cd Rgd`qCdenq `shmm>	Xdr
Hmbcp`rd M`hkmf B`o`bhsx enqV hmc>	Xdr
Hmbkt cd V `cphmf >	Xdr
Sq`mr Kn`c Asvmhhsdqrdbshmf V nnc V `kk>	Xdr
@cp` Kn`c L drg 'hm}1(	033
Ldqfd Snkdqmbd 'hm(	-01
O,Cdks` @mkxrhr Snkdqmbd	/-4/$
Hmbkt cd O,Cdks` enqV `kk>	Xdr
@cshl `sh`kkx Hsdq`sd Rsheemdrr enqV `kk>	Mn
L`whsdq`shmm enqV `kkRsheemdrr	2
Fquhsx @bbdkdq`shmm'esrdb]1(	21-1
V `kkLdrg Rhyd 'hm(	01
Dhfdmrnkt shmmBnmudqfdmbd Snk'0-D,(	3
Udqshb`k@vhr	X
Fkna`kLdl adqNqhdms`shmmOk`md	WY
Rs`shb Rnkudq	Ro`qrd @bbdkdq`sdc
Cxm`l hb Rnkudq	@bbdkdq`sdc Rnkudq

GnsQnkkdc RsddkBncd	@HRB 04sg'25/,05(9KQEC
@citrsRsheemdrr>	Mn
QHR@Bnmmdbshmm Bncd	Mnmd
Bnkc Enql dc RsddkBncd	Mnmd
V nnc Bncd	Mnmd
V nnc Sdl odq`stqd	;0//E
Bnmbqdsd Bncd	Mnmd
L`rnmqx Bncd	Mnmd
@kl hmtl Bncd	Mnmd, Athchmf
Rs`hmkdrr RsddkBncd	Mnmd

Mtl adqneRgd`qQdf hmmr	3
Qdf hmm Ro`bhmf Hmbcpl dms'hm(	3
Ahwhk Bnkt l mL dsgnc	Dw`bshhsdfq`shmm
O`q d Ads` E`bsnq'OB@(	-54
Bnmbqdsd Rsqdrr Aknbj	Qdbs`mftk`q
Trd Bq`bjdc Rdbshmmr>	Xdr
Trd Bq`bjdc Rdbshmmr Rk`a>	Mn
A`c Eq`l hmf V `qmhmfr>	Mn
Tmtrdc Enqbd V `qmhmfr>	Xdr
L hm0 A`qCh`l -Ro`bhmf >	Mn
Bnmbqdsd Qda`qRds	QDA@Q^RDS^@RSL @504
L hm$ Rsddkenq Bnkt l m	0
L`w$ Rsddkenq Bnkt l m	7

(Global) Model Settings, Continued

Rdhrl hb Bncd	Mnmd
Rdhrl hb A`rd Dkdu`shmm'es(	MnsDmsdqdc
@cc A`rd V dhfigs>	Xdr
BsW	-/1
BsY	-/1
SW'rdb(	MnsDmsdqdc
SY'rdb(	MnsDmsdqdc
QW	2
QY	2

Hot Rolled Steel Properties

	K`adk	D@rh	F@rh	Mt	Sgdq '.0D--Cdmrhsx@.es--		Xhdkc@rh	Qx	Et@rh	Qs
0	@25	18///	001//	-184	-54	-38	25	0-4	47	0-1

Hot Rolled Steel Section Sets

	K`adk	Rg`od	Sxod	Cdrhfim K--	L`sdq`k	Cdrhfim--	@Zm1\	Hxx Zm3\	Hyy Zm3\	I Zm3\
0	SV Q^KDF^S0	K5w5w0.1	Bnkl m	Mnmd	@25	Sxohb`k	4-64	08-8/7	08-8/7	-368
1	SV Q^KDF^NTSDQ^S0	1K1 0.1w1 0.1w0.3w2.7	Bnkl m	Mnmd	@25	Sxohb`k	1-27	2-236	0-30	-/38
2	SV Q^SNO^FHQS^S0	1K2w8w4.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	3-07	04-4/7	2-18	-025
3	SV Q^CH@F^S0	1K2w8w4.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	3-07	04-4/7	2-18	-025
4	SV Q^CH@F^NTSDQ^S0	1K2 0.1w3w4.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	3-38	04-440	4-0	-035
5	SV Q^QDC^GNQY^S0	K1 0.1w1 0.1w2.05	Ad`l	Mnmd	@25	Sxohb`k	-8/1	-436	-436	-/00
6	SV Q^QDC^GNQY^1^S0	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
7	SV Q^GNQY^NTSDQ^S0	V 01W15	Ad`l	Mnmd	@25	Sxohb`k	6-54	06-2	1/3	-2
8	SV Q^QDC^GNQY^2^S0	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
9/	SV Q^QDC^GNQY^3^S0	K1 0.1w1 0.1w2.05	Ad`l	Mnmd	@25	Sxohb`k	-8/1	-436	-436	-/00
00	SV Q^QDC^CH@F^S0	K1 0.1w1 0.1w2.05	Bnkl m	Mnmd	@25	Sxohb`k	-8/1	-436	-436	-/00
01	SV Q^KDF^S1	V 5W1/	Bnkl m	Mnmd	@25	Sxohb`k	4-76	02-2	30-3	-13
02	SV Q^CH@F^S1	1K2w1 0.1w2.7w2.7	Bnkl m	Mnmd	@25	Sxohb`k	2-73	4-042	2-20	-07
03	SV Q^QDC^GNQY^S1	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
04	SV Q^QDC^GNQY^1^S1	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
05	SV Q^QDC^CH@F^S1	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
06	SV Q^QDC^GNQY^2^S1	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
07	SV Q^QDC^CH@F^1^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
08	SV Q^QDC^CH@F^2^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
1/	SV Q^QDC^GHO^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
10	SV Q^QDC^GHO^1^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
11	SV Q^QDC^GHOCH@^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
12	SV Q^QDC^GHOCH@^1^S1	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
13	SV Q^HMMDQ^RTOO^S1	V 0/W2/	Ad`l	Mnmd	@25	Sxohb`k	7-73	05-6	06/	-511
14	SV Q^HMMDQ^RP^S1	V 7W02	Ad`l	Mnmd	@25	Sxohb`k	2-73	1-62	28-5	-/76
15	SV Q^HMMDQ^BNQMDQ^--	V 7W02	Ad`l	Mnmd	@25	Sxohb`k	2-73	1-62	28-5	-/76
16	SV Q^KDF^S2	V 5W1/	Bnkl m	Mnmd	@25	Sxohb`k	4-76	02-2	30-3	-13
17	SV Q^GNQY^S2	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
18	SV Q^CH@F^S2	1K2w1 0.1w2.7w2.7	Bnkl m	Mnmd	@25	Sxohb`k	2-73	4-042	2-20	-07
2/	SV Q^QDC^GNQY^S2	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
20	SV Q^QDC^GNQY^1^S2	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
21	SV Q^QDC^CH@F^S2	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
22	SV Q^QDC^GNQY^2^S2	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
23	SV Q^QDC^CH@F^1^S2	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10

Hot Rolled Steel Section Sets (Continued)

	K`adk	Rg`od	Sxod	Cdr hfimK---	L`sdqhk	Cdr hfim---	@Zm1\	HxxZm3\	HyyZm3\	IZm3\
24	SV Q^QDC^CH@F^2^S2	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
25	SV Q^QDC^GHO^S2	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
26	SV Q^QDC^GHO^1^S2	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
27	SV Q^QDC^GHOCH@^S2	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
28	SV Q^QDC^GHOCH@^1^S2	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
3/	SV Q^HMMDQ^RTOO^S2	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
30	SV Q^HMMDQ^RP^S2	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
31	SV Q^HMMDQ^BNQMDQ^—	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
32	SV Q^HMMDQ^SQH^S2	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
33	SV Q^HMMDQ^AQ@BD^S2	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
34	SV Q^HMMDQ^K@CCDQ^—	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
35	SV Q^KDF^S3	V 5W14	Bnktl m	Mnmrd	@25	Sxohb`k	6-23	06-0	42-3	-350
36	SV Q^GNQY^S3	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
37	SV Q^CH@F^S3	1K2w1,0.1w0.1w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	4	5-888	3-056	-306
38	SV Q^QDC^GNQY^S3	K2w2w2.05^GQ@	Ad`l	Mnmrd	@25	Sxohb`k	0-/8	-85	-85	-/03
4/	SV Q^QDC^GNQY^1^S3	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
40	SV Q^QDC^CH@F^S3	K2w2w2.05^GQ@	Bnktl m	Mnmrd	@25	Sxohb`k	0-/8	-85	-85	-/03
41	SV Q^QDC^GNQY^2^S3	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
42	SV Q^QDC^CH@F^1^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
43	SV Q^QDC^CH@F^2^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
44	SV Q^QDC^GHO^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
45	SV Q^QDC^GHO^1^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
46	SV Q^QDC^GHOCH@^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
47	SV Q^QDC^GHOCH@^1^S3	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
48	SV Q^HMMDQ^RTOO^S3	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
5/	SV Q^HMMDQ^RP^S3	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
50	SV Q^HMMDQ^BNQMDQ^—	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
51	SV Q^HMMDQ^SQH^S3	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
52	SV Q^HMMDQ^AQ@BD^S3	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
53	SV Q^HMMDQ^K@CCDQ^—	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
54	SV Q^KDF^S4	V 7W20	Bnktl m	Mnmrd	@25	Sxohb`k	8-02	26-0	00/	-425
55	SV Q^GNQY^S4	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
56	SV Q^CH@F^S4	1K2w1,0.1w0.1w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	4	5-888	3-056	-306
57	SV Q^QDC^GNQY^S4	K2w2w2.05^GQ@	Ad`l	Mnmrd	@25	Sxohb`k	0-/8	-85	-85	-/03
58	SV Q^QDC^GNQY^1^S4	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
6/	SV Q^QDC^CH@F^S4	K2w2w2.05^GQ@	Bnktl m	Mnmrd	@25	Sxohb`k	0-/8	-85	-85	-/03
60	SV Q^QDC^GNQY^2^S4	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
61	SV Q^QDC^CH@F^1^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
62	SV Q^QDC^CH@F^2^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
63	SV Q^QDC^GHO^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
64	SV Q^QDC^GHO^1^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
65	SV Q^QDC^GHOCH@^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
66	SV Q^QDC^GHOCH@^1^S4	1K1 0.1w1 0.1w2.05w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
67	SV Q^HMMDQ^RTOO^S4	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
68	SV Q^HMMDQ^RP^S4	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
7/	SV Q^HMMDQ^BNQMDQ^—	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
70	SV Q^HMMDQ^SQH^S4	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
71	SV Q^HMMDQ^AQ@BD^S4	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
72	SV Q^HMMDQ^K@CCDQ^—	1K2w1 0.1w0.3w2.7	Ad`l	Mnmrd	@25	Sxohb`k	1-52	2-262	1-24	-/44
73	SV Q^KDF^S5	V 7W8/	Bnktl m	Mnmrd	@25	Sxohb`k	00-6	38-0	035	0-01
74	SV Q^GNQY^S5	1K2w1 0.1w4.05w2.7	Ad`l	Mnmrd	@25	Sxohb`k	2-131	3-144	1-734	-0/5
75	SV Q^CH@F^S5	1K3w2w2.7w2.7	Bnktl m	Mnmrd	@25	Sxohb`k	3-86	7-4/7	6-82	-122

Hot Rolled Steel Section Sets (Continued)

	K`adk	Rg`od	Sxod	Cdr hfimK---	L`sdqhk	Cdr hfim---	@Zm1\	hxxZm3\	hyyZm3\	l Zm3\
76	SV Q^QDC^GNQY^S5	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
77	SV Q^QDC^GNQY^1^S5	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
78	SV Q^QDC^CH@F^S5	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
8/	SV Q^QDC^GNQY^2^S5	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
80	SV Q^QDC^CH@F^1^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
81	SV Q^QDC^CH@F^2^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
82	SV Q^QDC^GHD^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
83	SV Q^QDC^GHD^1^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
84	SV Q^QDC^GHDCH@^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
85	SV Q^QDC^GHDCH@^1^S5	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
86	SV Q^HMMDQ^RTOO^S5	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
87	SV Q^HMMDQ^RP^S5	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
88	SV Q^HMMDQ^BNQMDQ^---	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
0//	SV Q^HMMDQ^SQH^S5	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
0/0	SV Q^HMMDQ^AQ@BD^S5	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
0/1	SV Q^HMMDQ^K@CCDQ^---	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
0/2	SV Q^KDF^S6	V 0/W43	Bnkl m	Mnmd	@25	Sxohb`k	04-7	0/2	2/2	0-71
0/3	SV Q^GNQY^S6	1K2w1 0.1w2.7w2.7	Ad`l	Mnmd	@25	Sxohb`k	2-73	4-042	2-20	-07
0/4	SV Q^CH@F^S6	1K3w2w2.7w2.7	Bnkl m	Mnmd	@25	Sxohb`k	3-86	7-4/7	6-82	-122
0/5	SV Q^QDC^GNQY^S6	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
0/6	SV Q^QDC^GNQY^1^S6	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
0/7	SV Q^QDC^CH@F^S6	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
0/8	SV Q^QDC^GNQY^2^S6	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
00/	SV Q^QDC^CH@F^1^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
000	SV Q^QDC^CH@F^2^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
001	SV Q^QDC^GHD^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
002	SV Q^QDC^GHD^1^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
003	SV Q^QDC^GHDCH@^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
004	SV Q^QDC^GHDCH@^1^S6	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
005	SV Q^HMMDQ^RTOO^S6	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
006	SV Q^HMMDQ^RP^S6	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
007	SV Q^HMMDQ^BNQMDQ^---	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
008	SV Q^HMMDQ^SQH^S6	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
01/	SV Q^HMMDQ^AQ@BD^S6	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
010	SV Q^HMMDQ^K@CCDQ^---	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
011	SV Q^KDF^S7	V 0/W5/	Bnkl m	Mnmd	@25	Sxohb`k	06-6	005	230	1-37
012	SV Q^GNQY^S7	1K2w1 0.1w2.7w2.7	Ad`l	Mnmd	@25	Sxohb`k	2-73	4-042	2-20	-07
013	SV Q^CH@F^S7	1K3w2w0.1w2.7	Bnkl m	Mnmd	@25	Sxohb`k	5-4	00-425	0/-0	-431
014	SV Q^QDC^GNQY^S7	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
015	SV Q^QDC^GNQY^1^S7	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
016	SV Q^QDC^CH@F^S7	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
017	SV Q^QDC^GNQY^2^S7	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
018	SV Q^QDC^CH@F^1^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
02/	SV Q^QDC^CH@F^2^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
020	SV Q^QDC^GHD^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
021	SV Q^QDC^GHD^1^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
022	SV Q^QDC^GHDCH@^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
023	SV Q^QDC^GHDCH@^1^S7	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
024	SV Q^HMMDQ^RTOO^S7	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
025	SV Q^HMMDQ^RP^S7	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
026	SV Q^HMMDQ^BNQMDQ^---	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
027	SV Q^HMMDQ^SQH^S7	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10

Hot Rolled Steel Section Sets (Continued)

	K`adk	Rg`od	Sxod	Cdr hfimK---	L`sdqhk	Cdr hfim---	@Zm1\	HxxZm3\	HyyZm3\	I Zm3\
028	SV Q^HMMDQ^AQ@BD^S7	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
03/	SV Q^HMMDQ^K@CCDQ^---	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
030	SV Q^KDF^S8	V 0/W57	Bnkl m	Mnmd	@25	Sxohb`k	08-8	023	283	2-45
031	SV Q^GNQY^S8	1K2w1 0.1w2.7w2.7	Ad`l	Mnmd	@25	Sxohb`k	2-73	4-042	2-20	-07
032	SV Q^CH@F^S8	1K3w2w0.1w2.7	Bnkl m	Mnmd	@25	Sxohb`k	5-4	00-425	0/-0	-431
033	SV Q^QDC^GNQY^S8	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
034	SV Q^QDC^GNQY^1^S8	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
035	SV Q^QDC^CH@F^S8	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
036	SV Q^QDC^GNQY^2^S8	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
037	SV Q^QDC^CH@F^1^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
038	SV Q^QDC^CH@F^2^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
04/	SV Q^QDC^GHO^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
040	SV Q^QDC^GHO^1^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
041	SV Q^QDC^GHOCH@^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
042	SV Q^QDCGHOCH@71^S8	1K1 0.1w1 0.1w2.05w2.7	Bnkl m	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
043	SV Q^HMMDQ^RTOO^S8	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
044	SV Q^HMMDQ^RP^S8	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
045	SV Q^HMMDQ^BNQMDQ^---	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
046	SV Q^HMMDQ^SQH^S8	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
047	SV Q^HMMDQ^AQ@BD^S8	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
048	SV Q^HMMDQ^K@CCDQ^---	1K2w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-52	2-262	1-24	-/44
05/	SV Q^KDF^S0/	V 01W68	Bnkl m	Mnmd	@25	Sxohb`k	12-1	105	551	2-73
050	SV Q^GNQY^S0/	1K3w2w0.1w2.7	Ad`l	Mnmd	@25	Sxohb`k	5-4	00-425	0/-0	-431
051	SV Q^CH@F^S0/	1K3w3w0.1w2.7	Bnkl m	Mnmd	@25	Sxohb`k	6-4	14-106	00-0	-514
052	SV Q^QDC^GNQY^S0/	K2w2w2.05^GQ@	Ad`l	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
053	SV Q^QDC^GNQY^1^S0/	1K1 0.1w1 0.1w2.05w2.7	Ad`l	Mnmd	@25	Sxohb`k	0-7	1-388	0-/8	-/10
054	SV Q^QDC^CH@F^S0/	K2w2w2.05^GQ@	Bnkl m	Mnmd	@25	Sxohb`k	0-/8	-85	-85	-/03
055	SV Q^QDC^GNQY^2^S0/	1K1 0.1w1 0.1w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-27	2-236	0-30	-/38
056	SV Q^QDC^CH@F^1^S0/	1K1 0.1w1 0.1w0.3w2.7	Bnkl m	Mnmd	@25	Sxohb`k	1-27	2-236	0-30	-/38
057	SV Q^QDC^GNQY^3^S0/	1K2w2w0.3w2.7	Ad`l	Mnmd	@25	Sxohb`k	1-77	4-424	1-38	-/5
058	SV Q^QDC^CH@F^2^S0/	1K1 0.1w1 0.1w0.3w2.7	Bnkl m	Mnmd	@25	Sxohb`k	1-27	2-236	0-30	-/38
06/	SV Q^QDC^CH@F^3^S0/	1K1 0.1w1 0.1w0.3w2.7	Bnkl m	Mnmd	@25	Sxohb`k	1-27	2-236	0-30	-/38
060	SV Q^QDC^CH@F^/^S0/	K1-4w1-4w7	Bnkl m	Mnmd	@25	Sxohb`k	1-15	0-11	0-11	-077
061	SV Q^QDC^GNQY^/^S0/	K1-4w1-4w2	Bnkl m	Mnmd	@25	Sxohb`k	-8/0	-424	-424	-/00
062	SV Q^QDC^GHO^0^S0/	KK3w3w7w2	Bnkl m	Mnmd	@25	Sxohb`k	6-4	14-0	00	-533
063	SV Q^QDC^GHO^2^S0/	KK2w2w2w2	Bnkl m	Mnmd	@25	Sxohb`k	1-07	3-/8	0-8	-/16
064	SV Q^QDC^GHOCH@^0^S---	KK2w2w2w2	Bnkl m	Mnmd	@25	Sxohb`k	1-07	3-/8	0-8	-/16
065	SV Q^QDC^GHOCH@^2^S---	KK2w2w2w2	Bnkl m	Mnmd	@25	Sxohb`k	1-07	3-/8	0-8	-/16
066	SV Q^HMMDQ^FHQS^S0/	B3w6-1	Bnkl m	Mnmd	@25	Sxohb`k	1-02	-314	3-47	-/71

Member Primary Data

	K`adk	Hnhms	Inhms	Jnhms	Qns`sd'c---	RdbshmmRg`od	Sxod	Cdr hfimKms	L`sdqhk	Cdr hfimQtk---
0	L0163	M57	M732			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
1	L0164	M732	M61			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
2	L0165	M50	M730			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
3	L0166	M730	M46			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
4	L0167	M4/	M73/			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
5	L0168	M73/	M35			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
6	L017/	M28	M731			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
7	L0170	M731	M65			SV Q^CH@F^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
8	L 0171	M65	M733			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
0/	L 0172	M733	M61			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
00	L 0173	M57	M734			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
01	L 0174	M734	M50			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
02	L 0175	M46	M735			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
03	L 0176	M735	M4/			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
04	L 0177	M35	M736			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
05	L 0178	M736	M28			SV Q^CHdF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
06	L 04	M02	M0			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
07	L 07	M02	M2			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
08	L 11	M07	M2			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
1/	L 14	M07	M4			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
10	L 18	M11	M4			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
11	L 21	M11	M6			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
12	L 25	M15	M6			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
13	L 28	M15	M0			SV Q^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
14	L 40	M18	M02			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
15	L 48	M2/	M02			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
16	L 56	M2/	M07			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
17	L 64	M20	M07			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
18	L 72	M20	M11			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
2/	L 80	M21	M11			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
20	L 88	M21	M15			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
21	L 0/6	M18	M15			SV Q^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
22	L 013	M66	M70			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
23	L 021	M67	M70			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
24	L 030	M67	M85			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
25	L 038	M68	M85			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
26	L 047	M68	M0/7			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
27	L 055	M7/	M0/7			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
28	L 064	M7/	M01/			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
3/	L 072	M66	M01/			SV Q^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
30	L 1/4	M018	M022			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
31	L 102	M02/	M022			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
32	L 111	M02/	M037			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
33	L 12/	M020	M037			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
34	L 128	M020	M05/			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
35	L 136	M021	M05/			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
36	L 145	M021	M061			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
37	L 153	M018	M061			SV Q^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
38	L 175	M070	M074			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
4/	L 183	M071	M074			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
40	L 2/2	M071	M1//			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
41	L 200	M072	M1//			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
42	L 21/	M072	M101			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
43	L 217	M073	M101			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
44	L 226	M073	M113			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
45	L 234	M070	M113			SV Q^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
46	L 256	M122	M126			SV Q^CHdF^S5	Bnkl m	Mnmd	@25	Sxohb`k
47	L 264	M123	M126			SV Q^CHdF^S5	Bnkl m	Mnmd	@25	Sxohb`k
48	L 273	M123	M141			SV Q^CHdF^S5	Bnkl m	Mnmd	@25	Sxohb`k
5/	L 281	M124	M141			SV Q^CHdF^S5	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	Hnhms	Inhms	Jnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
50	L 3/0	M124	M153			SV Q^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
51	L 3/8	M125	M153			SV Q^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
52	L 307	M125	M165			SV Q^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
53	L 315	M122	M165			SV Q^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
54	L 337	M174	M178			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
55	L 345	M175	M178			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
56	L 354	M175	M2/3			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
57	L 362	M176	M2/3			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
58	L 371	M176	M205			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
6/	L 38/	M177	M205			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
60	L 388	M177	M217			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
61	L 4/6	M174	M217			SV Q^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
62	L 418	M226	M230			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
63	L 426	M227	M230			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
64	L 435	M227	M245			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
65	L 443	M228	M245			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
66	L 452	M228	M257			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
67	L 460	M23/	M257			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
68	L 47/	M23/	M27/			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
7/	L 477	M226	M27/			SV Q^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
70	L 50/	M278	M282			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
71	L 507	M28/	M282			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
72	L 516	M28/	M3/7			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
73	L 524	M280	M3/7			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
74	L 533	M280	M31/			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
75	L 541	M281	M31/			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
76	L 550	M281	M321			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
77	L 558	M278	M321			SV Q^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
78	L 580	M330	M334		242-863	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/	L 6/0	M331	M334		5-/15	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
80	L 601	M331	M353		242-863	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
81	L 611	M332	M353		5-/15	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
82	L 622	M332	M368		242-863	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
83	L 632	M333	M368		5-/15	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
84	L 643	M333	M383		242-863	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
85	L 653	M330	M383		5-/15	SV Q^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
86	L 016/	M731	M732			SV Q^GNQY^NTSDQ^S0	Ad`l	Mnmd	@25	Sxohb`k
87	L 0160	M732	M730			SV Q^GNQY^NTSDQ^S0	Ad`l	Mnmd	@25	Sxohb`k
88	L 0161	M730	M73/			SV Q^GNQY^NTSDQ^S0	Ad`l	Mnmd	@25	Sxohb`k
0//	L 0162	M73/	M731			SV Q^GNQY^NTSDQ^S0	Ad`l	Mnmd	@25	Sxohb`k
0/0	L 03	M1	M3			SV Q^GNQY^S1	Ad`l	Mnmd	@25^Fdm	Sxohb`k
0/1	L 10	M3	M5			SV Q^GNQY^S1	Ad`l	Mnmd	@25^Fdm	Sxohb`k
0/2	L 17	M5	M7			SV Q^GNQY^S1	Ad`l	Mnmd	@25^Fdm	Sxohb`k
0/3	L 24	M7	M1			SV Q^GNQY^S1	Ad`l	Mnmd	@25^Fdm	Sxohb`k
0/4	L 012	M18	M2/			SV Q^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0/5	L 03/	M2/	M20			SV Q^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0/6	L 046	M20	M21			SV Q^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0/7	L 063	M21	M18			SV Q^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0/8	L 1/3	M66	M67			SV Q^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
00/	L 110	M67	M68			SV Q^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
000	L 127	M68	M7/			SV Q^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
001	L 144	M7/	M66			SV Q^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	RdbsmmRg`od	Sxod	Cdr hfimKhrs	L`sdqhk	Cdr hfimQtk--
002	L 174	M018	M02/			SV Q^GNQY^S4	Ad`l	Mnmd	@25	Sxohb`k
003	L 2/1	M02/	M020			SV Q^GNQY^S4	Ad`l	Mnmd	@25	Sxohb`k
004	L 208	M020	M021			SV Q^GNQY^S4	Ad`l	Mnmd	@25	Sxohb`k
005	L 225	M021	M018			SV Q^GNQY^S4	Ad`l	Mnmd	@25	Sxohb`k
006	L 255	M070	M071			SV Q^GNQY^S5	Ad`l	Mnmd	@25	Sxohb`k
007	L 272	M071	M072			SV Q^GNQY^S5	Ad`l	Mnmd	@25	Sxohb`k
008	L 3//	M072	M073			SV Q^GNQY^S5	Ad`l	Mnmd	@25	Sxohb`k
01/	L 306	M073	M070			SV Q^GNQY^S5	Ad`l	Mnmd	@25	Sxohb`k
010	L 336	M122	M123			SV Q^GNQY^S6	Ad`l	Mnmd	@25	Sxohb`k
011	L 353	M123	M124			SV Q^GNQY^S6	Ad`l	Mnmd	@25	Sxohb`k
012	L 370	M124	M125			SV Q^GNQY^S6	Ad`l	Mnmd	@25	Sxohb`k
013	L 387	M125	M122			SV Q^GNQY^S6	Ad`l	Mnmd	@25	Sxohb`k
014	L 417	M174	M175			SV Q^GNQY^S7	Ad`l	Mnmd	@25	Sxohb`k
015	L 434	M175	M176			SV Q^GNQY^S7	Ad`l	Mnmd	@25	Sxohb`k
016	L 451	M176	M177			SV Q^GNQY^S7	Ad`l	Mnmd	@25	Sxohb`k
017	L 468	M177	M174			SV Q^GNQY^S7	Ad`l	Mnmd	@25	Sxohb`k
018	L 5/8	M226	M227			SV Q^GNQY^S8	Ad`l	Mnmd	@25	Sxohb`k
02/	L 515	M227	M228			SV Q^GNQY^S8	Ad`l	Mnmd	@25	Sxohb`k
020	L 532	M228	M23/			SV Q^GNQY^S8	Ad`l	Mnmd	@25	Sxohb`k
021	L 55/	M23/	M226			SV Q^GNQY^S8	Ad`l	Mnmd	@25	Sxohb`k
022	L 58/	M278	M28/		246-217	SV Q^GNQY^S0/	Ad`l	Mnmd	@25	Sxohb`k
023	L 600	M28/	M280		246-217	SV Q^GNQY^S0/	Ad`l	Mnmd	@25	Sxohb`k
024	L 621	M280	M281		246-217	SV Q^GNQY^S0/	Ad`l	Mnmd	@25	Sxohb`k
025	L 642	M281	M278		246-217	SV Q^GNQY^S0/	Ad`l	Mnmd	@25	Sxohb`k
026	L 0110	M77	M687			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
027	L 0111	M687	M017			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
028	L 0112	M013	M7/0			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
03/	L 0113	M7/0	M008			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
030	L 0114	M001	M7//			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
031	L 0115	M7//	M0/6			SV Q^HMMDQ^AQ@BD^S2	Ad`l	Mnmd	@25	Sxohb`k
032	L 0058	M03/	M65/			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
033	L 006/	M65/	M07/			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
034	L 0060	M065	M650			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
035	L 0061	M650	M060			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
036	L 0062	M048	M651			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
037	L 0063	M651	M053			SV Q^HMMDQ^AQ@BD^S3	Ad`l	Mnmd	@25	Sxohb`k
038	L 0006	M081	M611			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
04/	L 0007	M611	M121			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
040	L 0008	M117	M613			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
041	L 001/	M613	M112			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
042	L 0010	M105	M614			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
043	L 0011	M614	M100			SV Q^HMMDQ^AQ@BD^S4	Ad`l	Mnmd	@25	Sxohb`k
044	L 0/54	M133	M576			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
045	L 0/55	M576	M173			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
046	L 0/56	M17/	M575			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
047	L 0/57	M575	M164			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
048	L 0/58	M157	M574			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
05/	L 0/6/	M574	M152			SV Q^HMMDQ^AQ@BD^S5	Ad`l	Mnmd	@25	Sxohb`k
050	L 0/02	M185	M535			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k
051	L 0/03	M535	M225			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k
052	L 0/04	M221	M538			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k
053	L 0/05	M538	M216			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
054	L 0/06	M21/	M537			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k
055	L 0/07	M537	M204			SV Q^HMMDQ^AQ@BD^S6	Ad`l	Mnmd	@25	Sxohb`k
056	L 850	M237	M5/7			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
057	L 851	M5/7	M277			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
058	L 852	M273	M500			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
06/	L 853	M500	M268			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
060	L 854	M261	M50/			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
061	L 855	M50/	M256			SV Q^HMMDQ^AQ@BD^S7	Ad`l	Mnmd	@25	Sxohb`k
062	L 8/8	M3//	M46/			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
063	L 80/	M46/	M33/			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
064	L 800	M325	M460			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
065	L 801	M460	M320			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
066	L 802	M313	M461			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
067	L 803	M461	M308			SV Q^HMMDQ^AQ@BD^S8	Ad`l	Mnmd	@25	Sxohb`k
068	L 742	M343	M411			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
07/	L 743	M411	M4/3			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
070	L 744	M388	M412			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
071	L 745	M412	M382			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
072	L 746	M373	M413			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
073	L 747	M413	M367			SV Q^HMMDQ^AQ@BD^S0/	Ad`l	Mnmd	@25^F dm	CQ0
074	L 0147	M1	M725			SV Q^HMMDQ^BNQMDQ^S1	Ad`l	Mnmd	@25	Sxohb`k
075	L 0148	M728	M7			SV Q^HMMDQ^BNQMDQ^S1	Ad`l	Mnmd	@25	Sxohb`k
076	L 015/	M727	M5			SV Q^HMMDQ^BNQMDQ^S1	Ad`l	Mnmd	@25	Sxohb`k
077	L 0150	M3	M726			SV Q^HMMDQ^BNQMDQ^S1	Ad`l	Mnmd	@25	Sxohb`k
078	L 01/5	M18	M687			SV Q^HMMDQ^BNQMDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
08/	L 01/6	M7/0	M21			SV Q^HMMDQ^BNQMDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
080	L 01/7	M7//	M20			SV Q^HMMDQ^BNQMDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
081	L 0043	M65/	M66			SV Q^HMMDQ^BNQMDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
082	L 0044	M650	M7/			SV Q^HMMDQ^BNQMDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
083	L 0045	M651	M68			SV Q^HMMDQ^BNQMDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
084	L 00/1	M018	M611			SV Q^HMMDQ^BNQMDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
085	L 00/2	M613	M021			SV Q^HMMDQ^BNQMDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
086	L 00/3	M614	M020			SV Q^HMMDQ^BNQMDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
087	L 0/4/	M070	M576			SV Q^HMMDQ^BNQMDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
088	L 0/40	M575	M073			SV Q^HMMDQ^BNQMDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
1//	L 0/41	M574	M072			SV Q^HMMDQ^BNQMDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
1/0	L 887	M535	M122			SV Q^HMMDQ^BNQMDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
1/1	L 888	M538	M125			SV Q^HMMDQ^BNQMDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
1/2	L 0///	M537	M124			SV Q^HMMDQ^BNQMDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
1/3	L 835	M174	M5/7			SV Q^HMMDQ^BNQMDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
1/4	L 836	M500	M177			SV Q^HMMDQ^BNQMDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
1/5	L 837	M50/	M176			SV Q^HMMDQ^BNQMDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
1/6	L 783	M461	M228			SV Q^HMMDQ^BNQMDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
1/7	L 784	M460	M23/			SV Q^HMMDQ^BNQMDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
1/8	L 785	M46/	M226			SV Q^HMMDQ^BNQMDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
10/	L 716	M411	M278			SV Q^HMMDQ^BNQMDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
100	L 717	M412	M281			SV Q^HMMDQ^BNQMDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
101	L 718	M413	M280			SV Q^HMMDQ^BNQMDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
102	L 734	M417	M438			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
103	L 735	M428	M437			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
104	L 736	M42/	M435			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
105	L 737	M43/	M434			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
106	L 738	M421	M433			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
107	L 74/	M430	M436			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
108	L 740	M423	M431			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
11/	L 741	M432	M416			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
110	L 748	M433	M430			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
111	L 75/	M434	M420			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
112	L 750	M435	M43/			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
113	L 751	M436	M422			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
114	L 752	M437	M418			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
115	L 753	M438	M428			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
116	L 754	M431	M432			SV Q^HMMDQ^FHQS^S0/	Bnkl m	Mnmd	@25	Sxohb`k
117	L 0116	M703	M704			SV Q^HMMDQ^K@CCDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
118	L 0117	M704	M688			SV Q^HMMDQ^K@CCDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
12/	L 0118	M688	M703			SV Q^HMMDQ^K@CCDQ^S2	Ad`l	Mnmd	@25	Sxohb`k
120	L 0064	M665	M652			SV Q^HMMDQ^K@CCDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
121	L 0065	M652	M666			SV Q^HMMDQ^K@CCDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
122	L 0066	M666	M665			SV Q^HMMDQ^K@CCDQ^S3	Ad`l	Mnmd	@25	Sxohb`k
123	L 0012	M627	M628			SV Q^HMMDQ^K@CCDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
124	L 0013	M628	M612			SV Q^HMMDQ^K@CCDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
125	L 0014	M612	M627			SV Q^HMMDQ^K@CCDQ^S4	Ad`l	Mnmd	@25	Sxohb`k
126	L 0/60	M6//	M573			SV Q^HMMDQ^K@CCDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
127	L 0/61	M573	M6/0			SV Q^HMMDQ^K@CCDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
128	L 0/62	M6/0	M6//			SV Q^HMMDQ^K@CCDQ^S5	Ad`l	Mnmd	@25	Sxohb`k
13/	L 0/08	M551	M552			SV Q^HMMDQ^K@CCDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
130	L 0/1/	M552	M536			SV Q^HMMDQ^K@CCDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
131	L 0/10	M536	M551			SV Q^HMMDQ^K@CCDQ^S6	Ad`l	Mnmd	@25	Sxohb`k
132	L 856	M513	M514			SV Q^HMMDQ^K@CCDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
133	L 857	M514	M5/8			SV Q^HMMDQ^K@CCDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
134	L 858	M5/8	M513			SV Q^HMMDQ^K@CCDQ^S7	Ad`l	Mnmd	@25	Sxohb`k
135	L 804	M475	M476			SV Q^HMMDQ^K@CCDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
136	L 805	M476	M462			SV Q^HMMDQ^K@CCDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
137	L 806	M462	M475			SV Q^HMMDQ^K@CCDQ^S8	Ad`l	Mnmd	@25	Sxohb`k
138	L 72/	M414	M410			SV Q^HMMDQ^K@CCDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
14/	L 720	M410	M415			SV Q^HMMDQ^K@CCDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
140	L 721	M415	M414			SV Q^HMMDQ^K@CCDQ^S0/	Ad`l	Mnmd	@25^F dm	CQ0
141	L 0143	M726	M725			SV Q^HMMDQ^RP^S1	Ad`l	Mnmd	@25	Sxohb`k
142	L 0144	M725	M728			SV Q^HMMDQ^RP^S1	Ad`l	Mnmd	@25	Sxohb`k
143	L 0145	M728	M727			SV Q^HMMDQ^RP^S1	Ad`l	Mnmd	@25	Sxohb`k
144	L 0146	M727	M726			SV Q^HMMDQ^RP^S1	Ad`l	Mnmd	@25	Sxohb`k
145	L 01/1	M687	M688			SV Q^HMMDQ^RP^S2	Ad`l	Mnmd	@25	Sxohb`k
146	L 01/2	M688	M7//			SV Q^HMMDQ^RP^S2	Ad`l	Mnmd	@25	Sxohb`k
147	L 01/3	M7//	M7/0			SV Q^HMMDQ^RP^S2	Ad`l	Mnmd	@25	Sxohb`k
148	L 01/4	M7/0	M687			SV Q^HMMDQ^RP^S2	Ad`l	Mnmd	@25	Sxohb`k
15/	L 004/	M65/	M650			SV Q^HMMDQ^RP^S3	Ad`l	Mnmd	@25	Sxohb`k
150	L 0040	M650	M651			SV Q^HMMDQ^RP^S3	Ad`l	Mnmd	@25	Sxohb`k
151	L 0041	M651	M652			SV Q^HMMDQ^RP^S3	Ad`l	Mnmd	@25	Sxohb`k
152	L 0042	M652	M65/			SV Q^HMMDQ^RP^S3	Ad`l	Mnmd	@25	Sxohb`k
153	L 0/87	M612	M611			SV Q^HMMDQ^RP^S4	Ad`l	Mnmd	@25	Sxohb`k
154	L 0/88	M611	M613			SV Q^HMMDQ^RP^S4	Ad`l	Mnmd	@25	Sxohb`k
155	L 00//	M613	M614			SV Q^HMMDQ^RP^S4	Ad`l	Mnmd	@25	Sxohb`k
156	L 00/0	M614	M612			SV Q^HMMDQ^RP^S4	Ad`l	Mnmd	@25	Sxohb`k
157	L 0/35	M576	M575			SV Q^HMMDQ^RP^S5	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	Hnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfimKms	L`sdqhk	Cdr hfimQtk--
158	L 0/36	M575	M574			SV Q^HMMDQ^RP^S5	Ad`l	Mnmd	@25	Sxohb`k
16/	L 0/37	M574	M573			SV Q^HMMDQ^RP^S5	Ad`l	Mnmd	@25	Sxohb`k
160	L 0/38	M573	M576			SV Q^HMMDQ^RP^S5	Ad`l	Mnmd	@25	Sxohb`k
161	L 883	M536	M535			SV Q^HMMDQ^RP^S6	Ad`l	Mnmd	@25	Sxohb`k
162	L 884	M535	M538			SV Q^HMMDQ^RP^S6	Ad`l	Mnmd	@25	Sxohb`k
163	L 885	M538	M537			SV Q^HMMDQ^RP^S6	Ad`l	Mnmd	@25	Sxohb`k
164	L 886	M537	M536			SV Q^HMMDQ^RP^S6	Ad`l	Mnmd	@25	Sxohb`k
165	L 831	M5/7	M500			SV Q^HMMDQ^RP^S7	Ad`l	Mnmd	@25	Sxohb`k
166	L 832	M500	M50/			SV Q^HMMDQ^RP^S7	Ad`l	Mnmd	@25	Sxohb`k
167	L 833	M50/	M5/8			SV Q^HMMDQ^RP^S7	Ad`l	Mnmd	@25	Sxohb`k
168	L 834	M5/8	M5/7			SV Q^HMMDQ^RP^S7	Ad`l	Mnmd	@25	Sxohb`k
17/	L 78/	M462	M461			SV Q^HMMDQ^RP^S8	Ad`l	Mnmd	@25	Sxohb`k
170	L 780	M461	M460			SV Q^HMMDQ^RP^S8	Ad`l	Mnmd	@25	Sxohb`k
171	L 781	M460	M46/			SV Q^HMMDQ^RP^S8	Ad`l	Mnmd	@25	Sxohb`k
172	L 782	M46/	M462			SV Q^HMMDQ^RP^S8	Ad`l	Mnmd	@25	Sxohb`k
173	L 712	M411	M412			SV Q^HMMDQ^RP^S0/	Ad`l	Mnmd	@25^F dm	CQ0
174	L 713	M412	M413			SV Q^HMMDQ^RP^S0/	Ad`l	Mnmd	@25^F dm	CQ0
175	L 714	M413	M410			SV Q^HMMDQ^RP^S0/	Ad`l	Mnmd	@25^F dm	CQ0
176	L 715	M410	M411			SV Q^HMMDQ^RP^S0/	Ad`l	Mnmd	@25^F dm	CQ0
177	L 8	M732	M73/			SV Q^HMMDQ^RTOO^S0	Ad`l	Mnmd	@25^F dm	Sxohb`k
178	L 0/	M0/	M00			SV Q^HMMDQ^RTOO^S0	Ad`l	Mnmd	@25^F dm	Sxohb`k
18/	L 00	M730	M731			SV Q^HMMDQ^RTOO^S0	Ad`l	Mnmd	@25^F dm	Sxohb`k
180	L 01	M01	M8			SV Q^HMMDQ^RTOO^S0	Ad`l	Mnmd	@25^F dm	Sxohb`k
181	L 02	M8	M00			SV Q^HMMDQ^RTOO^S0	Ad`l	Mnmd	@25^F dm	Sxohb`k
182	L 31	M02	M07			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
183	L 32	M07	M11			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
184	L 33	M11	M15			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
185	L 34	M15	M02			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
186	L 35	M02	M11			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
187	L 004	M35	M4/			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
188	L 005	M46	M50			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
2//	L 006	M57	M61			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
2/0	L 007	M65	M28			SV Q^HMMDQ^RTOO^S1	Ad`l	Mnmd	@25	Sxohb`k
2/1	L 080	M70	M85			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/2	L 081	M85	M0/7			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/3	L 082	M0/7	M01/			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/4	L 083	M01/	M70			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/5	L 084	M70	M0/7			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/6	L 085	M84	M0//			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/7	L 086	M0/6	M001			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
2/8	L 087	M008	M013			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
20/	L 088	M017	M77			SV Q^HMMDQ^RTOO^S2	Ad`l	Mnmd	@25	Sxohb`k
200	L 161	M022	M037			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
201	L 162	M037	M05/			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
202	L 163	M05/	M061			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
203	L 164	M061	M022			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
204	L 165	M022	M05/			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
205	L 166	M036	M041			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
206	L 167	M048	M053			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
207	L 168	M060	M065			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
208	L 17/	M07/	M03/			SV Q^HMMDQ^RTOO^S3	Ad`l	Mnmd	@25	Sxohb`k
21/	L 242	M074	M1//			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hnhms	Inhms	Jnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKms	L`sdqhk	Cdr hfimQtk--
210	L 243	M1//	M101			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
211	L 244	M101	M113			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
212	L 245	M113	M074			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
213	L 246	M074	M101			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
214	L 247	M088	M1/3			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
215	L 248	M100	M105			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
216	L 25/	M112	M117			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
217	L 250	M121	M081			SV Q^HMMDQ^RTOO^S4	Ad`l	Mnmd	@25	Sxohb`k
218	L 323	M126	M141			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
22/	L 324	M141	M153			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
220	L 325	M153	M165			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
221	L 326	M165	M126			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
222	L 327	M126	M153			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
223	L 328	M140	M145			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
224	L 33/	M152	M157			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
225	L 330	M164	M17/			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
226	L 331	M173	M133			SV Q^HMMDQ^RTOO^S5	Ad`l	Mnmd	@25	Sxohb`k
227	L 404	M178	M2/3			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
228	L 405	M2/3	M205			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
23/	L 406	M205	M217			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
230	L 407	M217	M178			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
231	L 408	M178	M205			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
232	L 41/	M2/2	M2/7			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
233	L 410	M204	M21/			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
234	L 411	M216	M221			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
235	L 412	M225	M185			SV Q^HMMDQ^RTOO^S6	Ad`l	Mnmd	@25	Sxohb`k
236	L 485	M230	M245			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
237	L 486	M245	M257			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
238	L 487	M257	M27/			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
24/	L 488	M27/	M230			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
240	L 5//	M230	M257			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
241	L 5/0	M244	M25/			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
242	L 5/1	M256	M261			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
243	L 5/2	M268	M273			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
244	L 5/3	M277	M237			SV Q^HMMDQ^RTOO^S7	Ad`l	Mnmd	@25	Sxohb`k
245	L 566	M282	M3/7			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
246	L 567	M3/7	M31/			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
247	L 568	M31/	M321			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
248	L 57/	M321	M282			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
25/	L 570	M282	M31/			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
250	L 571	M3/6	M301			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
251	L 572	M308	M313			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
252	L 573	M320	M325			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
253	L 574	M33/	M3//			SV Q^HMMDQ^RTOO^S8	Ad`l	Mnmd	@25	Sxohb`k
254	L 663	M334	M353			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
255	L 664	M353	M368			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
256	L 665	M368	M383			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
257	L 666	M383	M334			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
258	L 667	M334	M368			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
26/	L 668	M352	M358			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
260	L 67/	M367	M373			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
261	L 670	M382	M388			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhs	L`sdqhk	Cdr hfimQtk--
262	L 671	M4/3	M343			SV Q^HMMDQ^RTOO^S0/	Ad`l	Mnmd	@25^F dm	Sxohb`k
263	L 01/8	M7/1	M7/2			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
264	L 010/	M7/3	M7/4			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
265	L 0100	M7/5	M7/6			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
266	L 0101	M7/7	M7/8			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
267	L 0102	M7/8	M70/			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
268	L 0103	M70/	M7/7			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
27/	L 0104	M7/1	M700			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
270	L 0105	M700	M7/2			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
271	L 0106	M7/3	M701			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
272	L 0107	M701	M7/4			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
273	L 0108	M7/5	M702			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
274	L 011/	M702	M7/6			SV Q^HMMDQ^SQH^S2	Ad`l	Mnmd	@25	Sxohb`k
275	L 0046	M653	M654			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
276	L 0047	M655	M656			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
277	L 0048	M657	M658			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
278	L 005/	M66/	M660			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
28/	L 0050	M660	M661			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
280	L 0051	M661	M66/			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
281	L 0052	M653	M662			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
282	L 0053	M662	M654			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
283	L 0054	M655	M663			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
284	L 0055	M663	M656			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
285	L 0056	M657	M664			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
286	L 0057	M664	M658			SV Q^HMMDQ^SQH^S3	Ad`l	Mnmd	@25	Sxohb`k
287	L 00/4	M615	M616			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
288	L 00/5	M617	M618			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3//	L 00/6	M62/	M620			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/0	L 00/7	M621	M622			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/1	L 00/8	M622	M623			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/2	L 000/	M623	M621			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/3	L 0000	M620	M624			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/4	L 0001	M624	M62/			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/5	L 0002	M618	M625			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/6	L 0003	M625	M617			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/7	L 0004	M616	M626			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
3/8	L 0005	M626	M615			SV Q^HMMDQ^SQH^S4	Ad`l	Mnmd	@25	Sxohb`k
30/	L 0/42	M577	M578			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
300	L 0/43	M58/	M580			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
301	L 0/44	M581	M582			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
302	L 0/45	M583	M584			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
303	L 0/46	M584	M585			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
304	L 0/47	M585	M583			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
305	L 0/48	M577	M586			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
306	L 0/5/	M586	M578			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
307	L 0/50	M58/	M587			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
308	L 0/51	M587	M580			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
31/	L 0/52	M581	M588			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
310	L 0/53	M588	M582			SV Q^HMMDQ^SQH^S5	Ad`l	Mnmd	@25	Sxohb`k
311	L 0//0	M54/	M540			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
312	L 0//1	M541	M542			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
313	L 0//2	M543	M544			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
314	L 0//3	M545	M546			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
315	L 0//4	M546	M547			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
316	L 0//5	M547	M545			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
317	L 0//6	M54/	M548			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
318	L 0//7	M548	M540			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
32/	L 0//8	M541	M55/			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
320	L 0/0/	M55/	M542			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
321	L 0/00	M543	M550			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
322	L 0/01	M550	M544			SV Q^HMMDQ^SQH^S6	Ad`l	Mnmd	@25	Sxohb`k
323	L 838	M501	M502			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
324	L 84/	M503	M504			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
325	L 840	M505	M506			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
326	L 841	M507	M508			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
327	L 842	M508	M51/			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
328	L 843	M51/	M507			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
33/	L 844	M501	M510			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
330	L 845	M510	M502			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
331	L 846	M503	M511			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
332	L 847	M511	M504			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
333	L 848	M505	M512			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
334	L 85/	M512	M506			SV Q^HMMDQ^SQH^S7	Ad`l	Mnmd	@25	Sxohb`k
335	L 786	M463	M464			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
336	L 787	M465	M466			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
337	L 788	M467	M468			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
338	L 8//	M47/	M470			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
34/	L 8/0	M470	M471			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
340	L 8/1	M471	M47/			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
341	L 8/2	M468	M472			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
342	L 8/3	M472	M467			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
343	L 8/4	M466	M473			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
344	L 8/5	M473	M465			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
345	L 8/6	M464	M474			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
346	L 8/7	M474	M463			SV Q^HMMDQ^SQH^S8	Ad`l	Mnmd	@25	Sxohb`k
347	L 722	M416	M417			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
348	L 723	M418	M42/			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
35/	L 724	M420	M421			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
350	L 725	M422	M423			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
351	L 726	M423	M424			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
352	L 727	M424	M422			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
353	L 728	M416	M425			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
354	L 73/	M425	M417			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
355	L 730	M418	M426			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
356	L 731	M426	M42/			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
357	L 732	M420	M427			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
358	L 733	M427	M421			SV Q^HMMDQ^SQH^S0/	Ad`l	Mnmd	@25^F dm	CQ0
36/	L 0155	M1	M731			SV Q^KDF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
360	L 0156	M3	M73/			SV Q^KDF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
361	L 0157	M5	M730			SV Q^KDF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
362	L 0158	M7	M732			SV Q^KDF^NTSDQ^S0	Bnkl m	Mnmd	@25	Sxohb`k
363	L 0	M1	M0		07/	SV Q^KDF^S0	Bnkl m	Mnmd	@25	Sxohb`k
364	L 1	M3	M2		16/	SV Q^KDF^S0	Bnkl m	Mnmd	@25	Sxohb`k
365	L 2	M5	M4			SV Q^KDF^S0	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
366	L 3	M7	M6		8/	SV Q^KDF^S0	Bnkl m	Mnmd	@25	Sxohb`k
367	L 36	M18	M1			SV Q^KDF^S1	Bnkl m	Mnmd	@25	Sxohb`k
368	L 37	M2/	M3			SV Q^KDF^S1	Bnkl m	Mnmd	@25	Sxohb`k
37/	L 38	M20	M5			SV Q^KDF^S1	Bnkl m	Mnmd	@25	Sxohb`k
370	L 4/	M21	M7			SV Q^KDF^S1	Bnkl m	Mnmd	@25	Sxohb`k
371	L 008	M66	M18			SV Q^KDF^S2	Bnkl m	Mnmd	@25	Sxohb`k
372	L 01/	M67	M2/			SV Q^KDF^S2	Bnkl m	Mnmd	@25	Sxohb`k
373	L 010	M68	M20			SV Q^KDF^S2	Bnkl m	Mnmd	@25	Sxohb`k
374	L 011	M7/	M21			SV Q^KDF^S2	Bnkl m	Mnmd	@25	Sxohb`k
375	L 1//	M018	M66			SV Q^KDF^S3	Bnkl m	Mnmd	@25	Sxohb`k
376	L 1/0	M02/	M67			SV Q^KDF^S3	Bnkl m	Mnmd	@25	Sxohb`k
377	L 1/1	M020	M68			SV Q^KDF^S3	Bnkl m	Mnmd	@25	Sxohb`k
378	L 1/2	M021	M7/			SV Q^KDF^S3	Bnkl m	Mnmd	@25	Sxohb`k
38/	L 170	M070	M018			SV Q^KDF^S4	Bnkl m	Mnmd	@25	Sxohb`k
380	L 171	M071	M02/			SV Q^KDF^S4	Bnkl m	Mnmd	@25	Sxohb`k
381	L 172	M072	M020			SV Q^KDF^S4	Bnkl m	Mnmd	@25	Sxohb`k
382	L 173	M073	M021			SV Q^KDF^S4	Bnkl m	Mnmd	@25	Sxohb`k
383	L 251	M122	M070			SV Q^KDF^S5	Bnkl m	Mnmd	@25	Sxohb`k
384	L 252	M123	M071			SV Q^KDF^S5	Bnkl m	Mnmd	@25	Sxohb`k
385	L 253	M124	M072			SV Q^KDF^S5	Bnkl m	Mnmd	@25	Sxohb`k
386	L 254	M125	M073			SV Q^KDF^S5	Bnkl m	Mnmd	@25	Sxohb`k
387	L 332	M174	M122			SV Q^KDF^S6	Bnkl m	Mnmd	@25	Sxohb`k
388	L 333	M175	M123			SV Q^KDF^S6	Bnkl m	Mnmd	@25	Sxohb`k
4//	L 334	M176	M124			SV Q^KDF^S6	Bnkl m	Mnmd	@25	Sxohb`k
4/0	L 335	M177	M125			SV Q^KDF^S6	Bnkl m	Mnmd	@25	Sxohb`k
4/1	L 413	M226	M174			SV Q^KDF^S7	Bnkl m	Mnmd	@25	Sxohb`k
4/2	L 414	M227	M175			SV Q^KDF^S7	Bnkl m	Mnmd	@25	Sxohb`k
4/3	L 415	M228	M176			SV Q^KDF^S7	Bnkl m	Mnmd	@25	Sxohb`k
4/4	L 416	M23/	M177			SV Q^KDF^S7	Bnkl m	Mnmd	@25	Sxohb`k
4/5	L 5/4	M278	M226			SV Q^KDF^S8	Bnkl m	Mnmd	@25	Sxohb`k
4/6	L 5/5	M28/	M227			SV Q^KDF^S8	Bnkl m	Mnmd	@25	Sxohb`k
4/7	L 5/6	M280	M228			SV Q^KDF^S8	Bnkl m	Mnmd	@25	Sxohb`k
4/8	L 5/7	M281	M23/			SV Q^KDF^S8	Bnkl m	Mnmd	@25	Sxohb`k
40/	L 575	M330	M278			SV Q^KDF^S0/	Bnkl m	Mnmd	@25	Sxohb`k
400	L 576	M331	M28/			SV Q^KDF^S0/	Bnkl m	Mnmd	@25	Sxohb`k
401	L 577	M332	M280			SV Q^KDF^S0/	Bnkl m	Mnmd	@25	Sxohb`k
402	L 578	M333	M281			SV Q^KDF^S0/	Bnkl m	Mnmd	@25	Sxohb`k
403	L 771	M450	M46/			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
404	L 772	M46/	M45/			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
405	L 773	M454	M460			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
406	L 774	M460	M453			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
407	L 775	M452	M461			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
408	L 776	M461	M451			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
41/	L 777	M448	M462			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
410	L 778	M462	M447			SV Q^QDCGHOCH@1^S8	Bnkl m	Mnmd	@25	Sxohb`k
411	L 680	M4/4	M345			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
412	L 681	M345	M4/8			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
413	L 682	M4/5	M360			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
414	L 683	M360	M40/			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
415	L 684	M401	M375			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
416	L 685	M375	M4/7			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
417	L 686	M4/6	M335			SV Q^QDC^CH@F^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhrs	L`sdqhk	Cdr hfimQtk--
418	L 687	M335	M400			SV Q^QDC^CHdF^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
42/	L 45	M25	M26			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
420	L 53	M31	M34			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
421	L 61	M37	M34			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
422	L 7/	M42	M45			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
423	L 77	M48	M45			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
424	L 85	M53	M56			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
425	L 0/3	M6/	M56			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
426	L 001	M63	M26			SV Q^QDC^CHdF^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
427	L 018	M74	M75			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
428	L 026	M80	M83			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
43/	L 035	M87	M83			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
430	L 043	M0/2	M0/5			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
431	L 052	M00/	M0/5			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
432	L 060	M004	M007			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
433	L 07/	M011	M007			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
434	L 077	M015	M75			SV Q^QDC^CHdF^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
435	L 10/	M026	M027			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
436	L 107	M032	M035			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
437	L 116	M04/	M035			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
438	L 124	M044	M047			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
44/	L 133	M051	M047			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
440	L 141	M056	M06/			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
441	L 150	M063	M06/			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
442	L 158	M067	M027			SV Q^QDC^CHdF^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
443	L 180	M078	M08/			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
444	L 188	M084	M087			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
445	L 2/7	M1/1	M087			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
446	L 205	M1/6	M10/			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
447	L 214	M103	M10/			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
448	L 222	M108	M111			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
45/	L 231	M115	M111			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
450	L 24/	M12/	M08/			SV Q^QDC^CHdF^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
451	L 261	M130	M131			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
452	L 27/	M136	M14/			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
453	L 278	M143	M14/			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
454	L 286	M148	M151			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
455	L 3/5	M155	M151			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
456	L 303	M160	M163			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
457	L 312	M167	M163			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
458	L 320	M171	M131			SV Q^QDC^CHdF^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
46/	L 342	M182	M183			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
460	L 350	M188	M2/1			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
461	L 36/	M2/5	M2/1			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
462	L 367	M200	M203			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
463	L 376	M207	M203			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
464	L 384	M212	M215			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
465	L 4/3	M22/	M215			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
466	L 401	M223	M183			SV Q^QDC^CHdF^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
467	L 423	M234	M235			SV Q^QDC^CHdF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
468	L 431	M240	M243			SV Q^QDC^CHdF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
47/	L 440	M247	M243			SV Q^QDC^CHdF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	Hnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
470	L 448	M252	M255			SV Q^QDC^CHGF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
471	L 457	M26/	M255			SV Q^QDC^CHGF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
472	L 465	M264	M267			SV Q^QDC^CHGF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
473	L 474	M271	M267			SV Q^QDC^CHGF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
474	L 482	M275	M235			SV Q^QDC^CHGF^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
475	L 504	M286	M287			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
476	L 512	M3/2	M3/5			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
477	L 521	M30/	M3/5			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
478	L 53/	M304	M307			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
48/	L 538	M311	M307			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
480	L 546	M316	M32/			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
481	L 555	M323	M32/			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
482	L 563	M327	M287			SV Q^QDC^CHGF^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
483	L 585	M338	M34/		3-022	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
484	L 6/5	M346	M35/		244-756	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
485	L 606	M355	M35/		3-022	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
486	L 616	M361	M364		244-756	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
487	L 627	M370	M364		3-022	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
488	L 637	M376	M38/		244-756	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
5//	L 648	M385	M38/		3-022	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
5/0	L 658	M4/0	M34/		244-756	SV Q^QDC^CHGF^1^S0/	Bnkl m	Mnmd	@25	Sxohb`k
5/1	L 46	M26	M28			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/2	L 47	M27	M28			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/3	L 54	M34	M35			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/4	L 55	M33	M35			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/5	L 62	M34	M4/			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/6	L 63	M38	M4/			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/7	L 70	M45	M46			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
5/8	L 71	M44	M46			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
50/	L 78	M45	M50			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
500	L 8/	M5/	M50			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
501	L 86	M56	M57			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
502	L 87	M55	M57			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
503	L 0/4	M56	M61			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
504	L 0/5	M60	M61			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
505	L 002	M26	M65			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
506	L 003	M64	M65			SV Q^QDC^CHGF^2^S1	Bnkl m	Mnmd	@25	Sxohb`k
507	L 02/	M75	M77			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
508	L 020	M76	M77			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
51/	L 027	M83	M84			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
510	L 028	M82	M84			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
511	L 036	M83	M0//			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
512	L 037	M88	M0//			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
513	L 044	M0/5	M0/6			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
514	L 045	M0/4	M0/6			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
515	L 053	M0/5	M001			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
516	L 054	M000	M001			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
517	L 061	M007	M008			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
518	L 062	M006	M008			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
52/	L 070	M007	M013			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
520	L 071	M012	M013			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
521	L 078	M75	M017			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hnlmms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Kmrs	L`sdqhk	Cdr hfim Qtk--
522	L 08/	M016	M017			SV Q^QDC^CHGF^2^S2	Bnkl m	Mnmd	@25	Sxohb`k
523	L 100	M027	M03/			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
524	L 101	M028	M03/			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
525	L 108	M035	M036			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
526	L 11/	M034	M036			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
527	L 117	M035	M041			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
528	L 118	M040	M041			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
53/	L 125	M047	M048			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
530	L 126	M046	M048			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
531	L 134	M047	M053			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
532	L 135	M052	M053			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
533	L 142	M06/	M060			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
534	L 143	M058	M060			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
535	L 151	M06/	M065			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
536	L 152	M064	M065			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
537	L 16/	M027	M07/			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
538	L 160	M068	M07/			SV Q^QDC^CHGF^2^S3	Bnkl m	Mnmd	@25	Sxohb`k
54/	L 181	M08/	M081			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
540	L 182	M080	M081			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
541	L 2//	M087	M088			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
542	L 2/0	M086	M088			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
543	L 2/8	M087	M1/3			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
544	L 20/	M1/2	M1/3			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
545	L 206	M10/	M100			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
546	L 207	M1/8	M100			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
547	L 215	M10/	M105			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
548	L 216	M104	M105			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
55/	L 223	M111	M112			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
550	L 224	M110	M112			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
551	L 232	M111	M117			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
552	L 233	M116	M117			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
553	L 240	M08/	M121			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
554	L 241	M120	M121			SV Q^QDC^CHGF^2^S4	Bnkl m	Mnmd	@25	Sxohb`k
555	L 262	M131	M133			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
556	L 263	M132	M133			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
557	L 270	M14/	M140			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
558	L 271	M138	M140			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
56/	L 28/	M14/	M145			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
560	L 280	M144	M145			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
561	L 287	M151	M152			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
562	L 288	M150	M152			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
563	L 3/6	M151	M157			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
564	L 3/7	M156	M157			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
565	L 304	M163	M164			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
566	L 305	M162	M164			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
567	L 313	M163	M17/			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
568	L 314	M168	M17/			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
57/	L 321	M131	M173			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
570	L 322	M172	M173			SV Q^QDC^CHGF^2^S5	Bnkl m	Mnmd	@25	Sxohb`k
571	L 343	M183	M185			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
572	L 344	M184	M185			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
573	L 351	M2/1	M2/2			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hnhms	Inhms	Jnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
574	L 352	M2/0	M2/2			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
575	L 360	M2/1	M2/7			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
576	L 361	M2/6	M2/7			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
577	L 368	M203	M204			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
578	L 37/	M202	M204			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
58/	L 377	M203	M21/			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
580	L 378	M208	M21/			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
581	L 385	M215	M216			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
582	L 386	M214	M216			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
583	L 4/4	M215	M221			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
584	L 4/5	M220	M221			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
585	L 402	M183	M225			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
586	L 403	M224	M225			SV Q^QDC^CHGF^2^S6	Bnkl m	Mnmd	@25	Sxohb`k
587	L 424	M235	M237			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
588	L 425	M236	M237			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6//	L 432	M243	M244			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/0	L 433	M242	M244			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/1	L 441	M243	M25/			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/2	L 442	M248	M25/			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/3	L 45/	M255	M256			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/4	L 450	M254	M256			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/5	L 458	M255	M261			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/6	L 46/	M260	M261			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/7	L 466	M267	M268			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
6/8	L 467	M266	M268			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
60/	L 475	M267	M273			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
600	L 476	M272	M273			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
601	L 483	M235	M277			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
602	L 484	M276	M277			SV Q^QDC^CHGF^2^S7	Bnkl m	Mnmd	@25	Sxohb`k
603	L 505	M287	M3//			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
604	L 506	M288	M3//			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
605	L 513	M3/5	M3/6			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
606	L 514	M3/4	M3/6			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
607	L 522	M3/5	M301			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
608	L 523	M300	M301			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
61/	L 530	M307	M308			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
610	L 531	M306	M308			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
611	L 54/	M307	M313			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
612	L 540	M312	M313			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
613	L 547	M32/	M320			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
614	L 548	M318	M320			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
615	L 556	M32/	M325			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
616	L 557	M324	M325			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
617	L 564	M287	M33/			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
618	L 565	M328	M33/			SV Q^QDC^CHGF^2^S8	Bnkl m	Mnmd	@25	Sxohb`k
62/	L 587	M340	M341		2-266	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
620	L 6/7	M348	M351		245-512	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
621	L 608	M356	M351		2-266	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
622	L 618	M363	M366		245-512	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
623	L 63/	M371	M366		2-266	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
624	L 64/	M378	M381		245-512	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
625	L 650	M386	M381		2-266	SV Q^QDC^CHGF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhrs	L`sdqhk	Cdr hfimQtk--
626	L 660	M4/1	M341		245-512	SV Q^QDC^CHdF^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
627	L 588	M341	M343		245-366	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
628	L 6//	M342	M343		4-/35	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
63/	L 6/8	M351	M352		2-412	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
630	L 60/	M350	M352		243-843	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
631	L 61/	M351	M358		245-366	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
632	L 610	M357	M358		4-/35	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
633	L 62/	M366	M367		2-412	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
634	L 620	M365	M367		243-843	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
635	L 630	M366	M373		245-366	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
636	L 631	M372	M373		4-/35	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
637	L 640	M381	M382		2-412	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
638	L 641	M380	M382		243-843	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
64/	L 651	M381	M388		245-366	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
640	L 652	M387	M388		4-/35	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
641	L 661	M341	M4/3		2-412	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
642	L 662	M4/2	M4/3		243-843	SV Q^QDC^CHdF^3^S0/	Bnkl m	Mnmd	@25	Sxohb`k
643	L 06	M8	M04		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
644	L 1/	M8	M05		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
645	L 13	M0/	M08		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
646	L 16	M0/	M1/		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
647	L 20	M00	M12		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
648	L 23	M00	M13		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
65/	L 27	M01	M16		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
650	L 30	M01	M17		8/	SV Q^QDC^CHdF^S0	Bnkl m	Mnmd	@25	Sxohb`k
651	L 43	M23	M24			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
652	L 51	M3/	M32			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
653	L 6/	M36	M32			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
654	L 67	M40	M43			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
655	L 75	M47	M43			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
656	L 83	M51	M54			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
657	L 0/1	M58	M54			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
658	L 00/	M62	M24			SV Q^QDC^CHdF^S1	Bnkl m	Mnmd	@25	Sxohb`k
66/	L 016	M72	M73			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
660	L 024	M78	M81			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
661	L 033	M86	M81			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
662	L 041	M0/0	M0/3			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
663	L 050	M0/8	M0/3			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
664	L 058	M002	M005			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
665	L 067	M010	M005			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
666	L 075	M014	M73			SV Q^QDC^CHdF^S2	Bnkl m	Mnmd	@25	Sxohb`k
667	L 1/7	M024	M025			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
668	L 105	M030	M033			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
67/	L 114	M038	M033			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
670	L 122	M042	M045			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
671	L 131	M050	M045			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
672	L 14/	M054	M057			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
673	L 148	M062	M057			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
674	L 156	M066	M025			SV Q^QDC^CHdF^S3	Bnkl m	Mnmd	@25	Sxohb`k
675	L 178	M076	M077			SV Q^QDC^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
676	L 186	M082	M085			SV Q^QDC^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k
677	L 2/5	M1/0	M085			SV Q^QDC^CHdF^S4	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	Hnmms	I nhms	J nhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfimKms	L`sdqhk	Cdr hfimQtk--
678	L 203	M1/4	M1/7			SV Q^QDC^CH@F^S4	Bnkl m	Mnmd	@25	Sxohb`k
68/	L 212	M102	M1/7			SV Q^QDC^CH@F^S4	Bnkl m	Mnmd	@25	Sxohb`k
680	L 220	M106	M11/			SV Q^QDC^CH@F^S4	Bnkl m	Mnmd	@25	Sxohb`k
681	L 23/	M114	M11/			SV Q^QDC^CH@F^S4	Bnkl m	Mnmd	@25	Sxohb`k
682	L 237	M118	M077			SV Q^QDC^CH@F^S4	Bnkl m	Mnmd	@25	Sxohb`k
683	L 26/	M128	M13/			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
684	L 267	M134	M137			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
685	L 276	M142	M137			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
686	L 284	M146	M15/			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
687	L 3/3	M154	M15/			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
688	L 301	M158	M161			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
7//	L 310	M166	M161			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
7/0	L 318	M170	M13/			SV Q^QDC^CH@F^S5	Bnkl m	Mnmd	@25	Sxohb`k
7/1	L 340	M180	M181			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/2	L 348	M186	M2//			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/3	L 357	M2/4	M2//			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/4	L 365	M2/8	M201			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/5	L 374	M206	M201			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/6	L 382	M210	M213			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/7	L 4/1	M218	M213			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
7/8	L 40/	M222	M181			SV Q^QDC^CH@F^S6	Bnkl m	Mnmd	@25	Sxohb`k
70/	L 421	M232	M233			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
700	L 43/	M238	M241			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
701	L 438	M246	M241			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
702	L 446	M250	M253			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
703	L 455	M258	M253			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
704	L 463	M262	M265			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
705	L 472	M270	M265			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
706	L 480	M274	M233			SV Q^QDC^CH@F^S7	Bnkl m	Mnmd	@25	Sxohb`k
707	L 502	M284	M285			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
708	L 510	M3/0	M3/3			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
71/	L 52/	M3/8	M3/3			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
710	L 527	M302	M305			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
711	L 536	M310	M305			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
712	L 544	M314	M317			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
713	L 553	M322	M317			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
714	L 561	M326	M285			SV Q^QDC^CH@F^S8	Bnkl m	Mnmd	@25	Sxohb`k
715	L 583	M336	M337		6-058	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
716	L 6/3	M344	M347		241-720	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
717	L 604	M354	M347		6-058	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
718	L 614	M36/	M362		241-720	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
72/	L 625	M37/	M362		6-058	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
720	L 635	M374	M377		241-720	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
721	L 646	M384	M377		6-058	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
722	L 656	M4//	M337		241-720	SV Q^QDC^CH@F^S0/	Bnkl m	Mnmd	@25	Sxohb`k
723	L 7/6	M354	M406			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
724	L 7/7	M406	M344			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
725	L 7/8	M336	M407			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
726	L 70/	M407	M4//			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
727	L 700	M384	M408			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
728	L 701	M408	M374			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
73/	L 702	M37/	M41/			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	Hnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
730	L 703	M41/	M36/			SV Q^QDC^GHOCH@^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
731	L 0135	M713	M725			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
732	L 0136	M725	M714			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
733	L 0137	M715	M726			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
734	L 0138	M726	M716			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
735	L 014/	M717	M727			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
736	L 0140	M727	M718			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
737	L 0141	M720	M728			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
738	L 0142	M728	M72/			SV Q^QDC^GHOCH@^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
74/	L 0083	M675	M687			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
740	L 0084	M687	M676			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
741	L 0085	M677	M688			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
742	L 0086	M688	M678			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
743	L 0087	M681	M7//2			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
744	L 0088	M7//2	M682			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
745	L 01//2	M680	M7/0			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
746	L 01/0	M7/0	M68/			SV Q^QDC^GHOCH@^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
747	L 0031	M637	M65/			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
748	L 0032	M65/	M638			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
75/	L 0033	M64/	M650			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
750	L 0034	M650	M640			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
751	L 0035	M643	M651			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
752	L 0036	M651	M644			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
753	L 0037	M642	M652			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
754	L 0038	M652	M641			SV Q^QDC^GHOCH@^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
755	L 0/8/	M60/	M611			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
756	L 0/80	M611	M600			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
757	L 0/81	M601	M612			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
758	L 0/82	M612	M602			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
76/	L 0/83	M606	M613			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
760	L 0/84	M613	M605			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
761	L 0/85	M603	M614			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
762	L 0/86	M614	M604			SV Q^QDC^GHOCH@^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
763	L 0/27	M561	M573			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
764	L 0/28	M573	M562			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
765	L 0/3/	M565	M574			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
766	L 0/30	M574	M566			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
767	L 0/31	M567	M575			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
768	L 0/32	M575	M568			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
77/	L 0/33	M563	M576			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
770	L 0/34	M576	M564			SV Q^QDC^GHOCH@^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
771	L 875	M523	M535			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
772	L 876	M535	M524			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
773	L 877	M525	M536			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
774	L 878	M536	M526			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
775	L 88/	M527	M537			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
776	L 880	M537	M528			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
777	L 881	M53/	M538			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
778	L 882	M538	M530			SV Q^QDC^GHOCH@^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
78/	L 823	M485	M5/7			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
780	L 824	M5/7	M486			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
781	L 825	M5/2	M5/8			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhrs	L`sdqhk	Cdr hfimQtk--
782	L 826	M5/8	M5/1			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
783	L 827	M5//	M50/			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
784	L 828	M50/	M5/0			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
785	L 83/	M488	M500			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
786	L 830	M500	M487			SV Q^QDC^GHOCH@^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
787	L 704	M356	M410			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
788	L 705	M410	M348			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8//	L 706	M340	M411			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/0	L 707	M411	M4/1			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/1	L 708	M386	M412			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/2	L 71/	M412	M378			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/3	L 710	M371	M413			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/4	L 711	M413	M363			SV Q^QDC^GHOCH@^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
8/5	L 0127	M705	M721			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
8/6	L 0128	M721	M706			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
8/7	L 013/	M707	M722			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
8/8	L 0130	M722	M708			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
80/	L 0131	M71/	M723			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
800	L 0132	M723	M710			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
801	L 0133	M712	M724			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
802	L 0134	M724	M711			SV Q^QDC^GHOCH@^S1	Bnkl m	Mnmd	@25	Sxohb`k
803	L 0075	M67/	M683			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
804	L 0076	M683	M670			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
805	L 0077	M671	M684			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
806	L 0078	M684	M672			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
807	L 008/	M667	M685			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
808	L 0080	M685	M668			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
81/	L 0081	M673	M686			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
810	L 0082	M686	M674			SV Q^QDC^GHOCH@^S2	Bnkl m	Mnmd	@25	Sxohb`k
811	L 0023	M631	M645			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
812	L 0024	M645	M632			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
813	L 0025	M63/	M646			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
814	L 0026	M646	M630			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
815	L 0027	M635	M647			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
816	L 0028	M647	M636			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
817	L 003/	M633	M648			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
818	L 0030	M648	M634			SV Q^QDC^GHOCH@^S3	Bnkl m	Mnmd	@25	Sxohb`k
82/	L 0/71	M6/1	M607			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
820	L 0/72	M607	M6/2			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
821	L 0/73	M6/3	M608			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
822	L 0/74	M608	M6/4			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
823	L 0/75	M6/5	M61/			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
824	L 0/76	M61/	M6/6			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
825	L 0/77	M6/7	M610			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
826	L 0/78	M610	M6/8			SV Q^QDC^GHOCH@^S4	Bnkl m	Mnmd	@25	Sxohb`k
827	L 0/2/	M553	M57/			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
828	L 0/20	M57/	M554			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
83/	L 0/21	M555	M570			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
830	L 0/22	M570	M556			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
831	L 0/23	M557	M571			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
832	L 0/24	M571	M558			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
833	L 0/25	M560	M572			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
834	L 0/26	M572	M56/			SV Q^QDC^GHOCH@^S5	Bnkl m	Mnmd	@25	Sxohb`k
835	L 867	M515	M531			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
836	L 868	M531	M516			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
837	L 87/	M517	M532			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
838	L 870	M532	M518			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
84/	L 871	M521	M533			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
840	L 872	M533	M522			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
841	L 873	M52/	M534			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
842	L 874	M534	M520			SV Q^QDC^GHOCH@^S6	Bnkl m	Mnmd	@25	Sxohb`k
843	L 815	M477	M5/3			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
844	L 816	M5/3	M478			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
845	L 817	M48/	M5/4			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
846	L 818	M5/4	M480			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
847	L 82/	M481	M5/5			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
848	L 820	M5/5	M482			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
85/	L 821	M483	M5/6			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
850	L 822	M5/6	M484			SV Q^QDC^GHOCH@^S7	Bnkl m	Mnmd	@25	Sxohb`k
851	L 763	M44/	M455			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
852	L 764	M455	M440			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
853	L 765	M446	M456			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
854	L 766	M456	M445			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
855	L 767	M443	M457			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
856	L 768	M457	M444			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
857	L 77/	M441	M458			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
858	L 770	M458	M442			SV Q^QDC^GHOCH@^S8	Bnkl m	Mnmd	@25	Sxohb`k
86/	L 688	M37/	M36/			SV Q^QDC^GHO^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
860	L 7//	M354	M344			SV Q^QDC^GHO^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
861	L 7/0	M374	M384			SV Q^QDC^GHO^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
862	L 7/5	M336	M4//			SV Q^QDC^GHO^0^S0/	Bnkl m	Mnmd	@25	Sxohb`k
863	L 0123	M713	M714			SV Q^QDC^GHO^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
864	L 0124	M715	M716			SV Q^QDC^GHO^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
865	L 0125	M717	M718			SV Q^QDC^GHO^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
866	L 0126	M72/	M720			SV Q^QDC^GHO^1^S1	Bnkl m	Mnmd	@25	Sxohb`k
867	L 0071	M675	M676			SV Q^QDC^GHO^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
868	L 0072	M677	M678			SV Q^QDC^GHO^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
87/	L 0073	M68/	M680			SV Q^QDC^GHO^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
870	L 0074	M681	M682			SV Q^QDC^GHO^1^S2	Bnkl m	Mnmd	@25	Sxohb`k
871	L 002/	M637	M638			SV Q^QDC^GHO^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
872	L 0020	M64/	M640			SV Q^QDC^GHO^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
873	L 0021	M641	M642			SV Q^QDC^GHO^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
874	L 0022	M643	M644			SV Q^QDC^GHO^1^S3	Bnkl m	Mnmd	@25	Sxohb`k
875	L 0/67	M60/	M600			SV Q^QDC^GHO^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
876	L 0/68	M601	M602			SV Q^QDC^GHO^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
877	L 0/7/	M603	M604			SV Q^QDC^GHO^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
878	L 0/70	M605	M606			SV Q^QDC^GHO^1^S4	Bnkl m	Mnmd	@25	Sxohb`k
88/	L 0/15	M561	M562			SV Q^QDC^GHO^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
880	L 0/16	M563	M564			SV Q^QDC^GHO^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
881	L 0/17	M565	M566			SV Q^QDC^GHO^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
882	L 0/18	M567	M568			SV Q^QDC^GHO^1^S5	Bnkl m	Mnmd	@25	Sxohb`k
883	L 863	M523	M524			SV Q^QDC^GHO^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
884	L 864	M525	M526			SV Q^QDC^GHO^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
885	L 865	M527	M528			SV Q^QDC^GHO^1^S6	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
886	L 866	M53/	M530			SV Q^QDC^GHO^1^S6	Bnkl m	Mnmd	@25	Sxohb`k
887	L 811	M485	M486			SV Q^QDC^GHO^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
888	L 812	M487	M488			SV Q^QDC^GHO^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
0//1	L 813	M5//1	M5/0			SV Q^QDC^GHO^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/0	L 814	M5/1	M5/2			SV Q^QDC^GHO^1^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/1	L 76/	M447	M448			SV Q^QDC^GHO^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/2	L 760	M45/	M450			SV Q^QDC^GHO^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/3	L 761	M451	M452			SV Q^QDC^GHO^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/4	L 762	M453	M454			SV Q^QDC^GHO^1^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/5	L 7/1	M371	M363			SV Q^QDC^GHO^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/6	L 7/2	M356	M348			SV Q^QDC^GHO^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/7	L 7/3	M378	M386			SV Q^QDC^GHO^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/8	L 7/4	M4/1	M340			SV Q^QDC^GHO^2^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/0/	L 012/	M705	M706			SV Q^QDC^GHO^S1	Bnkl m	Mnmd	@25	Sxohb`k
0/00	L 0120	M707	M708			SV Q^QDC^GHO^S1	Bnkl m	Mnmd	@25	Sxohb`k
0/01	L 0121	M71/	M710			SV Q^QDC^GHO^S1	Bnkl m	Mnmd	@25	Sxohb`k
0/02	L 0122	M711	M712			SV Q^QDC^GHO^S1	Bnkl m	Mnmd	@25	Sxohb`k
0/03	L 0067	M667	M668			SV Q^QDC^GHO^S2	Bnkl m	Mnmd	@25	Sxohb`k
0/04	L 0068	M67/	M670			SV Q^QDC^GHO^S2	Bnkl m	Mnmd	@25	Sxohb`k
0/05	L 007/	M671	M672			SV Q^QDC^GHO^S2	Bnkl m	Mnmd	@25	Sxohb`k
0/06	L 0070	M673	M674			SV Q^QDC^GHO^S2	Bnkl m	Mnmd	@25	Sxohb`k
0/07	L 0015	M63/	M630			SV Q^QDC^GHO^S3	Bnkl m	Mnmd	@25	Sxohb`k
0/08	L 0016	M631	M632			SV Q^QDC^GHO^S3	Bnkl m	Mnmd	@25	Sxohb`k
0/1/	L 0017	M633	M634			SV Q^QDC^GHO^S3	Bnkl m	Mnmd	@25	Sxohb`k
0/10	L 0018	M635	M636			SV Q^QDC^GHO^S3	Bnkl m	Mnmd	@25	Sxohb`k
0/11	L 0/63	M6/1	M6/2			SV Q^QDC^GHO^S4	Bnkl m	Mnmd	@25	Sxohb`k
0/12	L 0/64	M6/3	M6/4			SV Q^QDC^GHO^S4	Bnkl m	Mnmd	@25	Sxohb`k
0/13	L 0/65	M6/5	M6/6			SV Q^QDC^GHO^S4	Bnkl m	Mnmd	@25	Sxohb`k
0/14	L 0/66	M6/7	M6/8			SV Q^QDC^GHO^S4	Bnkl m	Mnmd	@25	Sxohb`k
0/15	L 0/11	M553	M554			SV Q^QDC^GHO^S5	Bnkl m	Mnmd	@25	Sxohb`k
0/16	L 0/12	M555	M556			SV Q^QDC^GHO^S5	Bnkl m	Mnmd	@25	Sxohb`k
0/17	L 0/13	M557	M558			SV Q^QDC^GHO^S5	Bnkl m	Mnmd	@25	Sxohb`k
0/18	L 0/14	M56/	M560			SV Q^QDC^GHO^S5	Bnkl m	Mnmd	@25	Sxohb`k
0/2/	L 86/	M515	M516			SV Q^QDC^GHO^S6	Bnkl m	Mnmd	@25	Sxohb`k
0/20	L 860	M517	M518			SV Q^QDC^GHO^S6	Bnkl m	Mnmd	@25	Sxohb`k
0/21	L 861	M52/	M520			SV Q^QDC^GHO^S6	Bnkl m	Mnmd	@25	Sxohb`k
0/22	L 862	M521	M522			SV Q^QDC^GHO^S6	Bnkl m	Mnmd	@25	Sxohb`k
0/23	L 807	M477	M478			SV Q^QDC^GHO^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/24	L 808	M48/	M480			SV Q^QDC^GHO^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/25	L 81/	M481	M482			SV Q^QDC^GHO^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/26	L 810	M483	M484			SV Q^QDC^GHO^S7	Bnkl m	Mnmd	@25	Sxohb`k
0/27	L 755	M44/	M440			SV Q^QDC^GHO^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/28	L 756	M441	M442			SV Q^QDC^GHO^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/3/	L 757	M443	M444			SV Q^QDC^GHO^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/30	L 758	M445	M446			SV Q^QDC^GHO^S8	Bnkl m	Mnmd	@25	Sxohb`k
0/31	L 672	M40/	M403			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/32	L 673	M403	M4/5			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/33	L 674	M401	M405			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/34	L 675	M405	M4/7			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/35	L 676	M4/6	M404			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/36	L 677	M404	M400			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/37	L 678	M4/4	M402			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K`adk	Hlnhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhms	L`sdqhk	Cdr hfimQtk--
0/38	L 68/	M402	M4/8			SV Q^QDC^GNQY^/^S0/	Bnkl m	Mnmd	@25	Sxohb`k
0/4/	L 0151	M12	M13			SV Q^QDC^GNQY^1^S0	Ad`l	Mnmd	@25	Sxohb`k
0/40	L 0152	M08	M1/			SV Q^QDC^GNQY^1^S0	Ad`l	Mnmd	@25	Sxohb`k
0/41	L 0153	M04	M05			SV Q^QDC^GNQY^1^S0	Ad`l	Mnmd	@25	Sxohb`k
0/42	L 0154	M16	M17			SV Q^QDC^GNQY^1^S0	Ad`l	Mnmd	@25	Sxohb`k
0/43	L 42	M24	M25			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/44	L 50	M31	M32			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/45	L 58	M32	M37			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/46	L 66	M42	M43			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/47	L 74	M43	M48			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/48	L 82	M53	M54			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/5/	L 0/0	M54	M6/			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/50	L 0/8	M63	M24			SV Q^QDC^GNQY^1^S1	Ad`l	Mnmd	@25	Sxohb`k
0/51	L 015	M73	M74			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/52	L 023	M80	M81			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/53	L 032	M81	M87			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/54	L 040	M0/2	M0/3			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/55	L 05/	M0/3	M00/			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/56	L 057	M004	M005			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/57	L 066	M005	M011			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/58	L 074	M015	M73			SV Q^QDC^GNQY^1^S2	Ad`l	Mnmd	@25	Sxohb`k
0/6/	L 1/6	M025	M026			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/60	L 104	M032	M033			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/61	L 113	M033	M04/			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/62	L 121	M044	M045			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/63	L 130	M045	M051			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/64	L 138	M056	M057			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/65	L 147	M057	M063			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/66	L 155	M067	M025			SV Q^QDC^GNQY^1^S3	Ad`l	Mnmd	@25	Sxohb`k
0/67	L 177	M077	M078			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/68	L 185	M084	M085			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/7/	L 2/4	M085	M1/1			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/70	L 202	M1/6	M1/7			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/71	L 211	M1/7	M103			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/72	L 22/	M108	M11/			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/73	L 228	M11/	M115			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/74	L 236	M12/	M077			SV Q^QDC^GNQY^1^S4	Ad`l	Mnmd	@25	Sxohb`k
0/75	L 258	M13/	M130			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/76	L 266	M136	M137			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/77	L 275	M137	M143			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/78	L 283	M148	M15/			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/8/	L 3/2	M15/	M155			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/80	L 300	M160	M161			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/81	L 31/	M161	M167			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/82	L 317	M171	M13/			SV Q^QDC^GNQY^1^S5	Ad`l	Mnmd	@25	Sxohb`k
0/83	L 34/	M181	M182			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
0/84	L 347	M188	M2//			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
0/85	L 356	M2//	M2/5			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
0/86	L 364	M200	M201			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
0/87	L 373	M201	M207			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
0/88	L 381	M212	M213			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
00//	L 4/0	M213	M22/			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfim Khms	L`sdqhk	Cdr hfim Qtk--
00/0	L 4/8	M223	M181			SV Q^QDC^GNQY^1^S6	Ad`l	Mnmd	@25	Sxohb`k
00/1	L 420	M233	M234			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/2	L 428	M240	M241			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/3	L 437	M241	M247			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/4	L 445	M252	M253			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/5	L 454	M253	M26/			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/6	L 462	M264	M265			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/7	L 471	M265	M271			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
00/8	L 48/	M275	M233			SV Q^QDC^GNQY^1^S7	Ad`l	Mnmd	@25	Sxohb`k
000/	L 501	M285	M286			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0000	L 51/	M3/2	M3/3			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0001	L 518	M3/3	M30/			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0002	L 526	M304	M305			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0003	L 535	M305	M311			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0004	L 543	M316	M317			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0005	L 552	M317	M323			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0006	L 560	M327	M285			SV Q^QDC^GNQY^1^S8	Ad`l	Mnmd	@25	Sxohb`k
0007	L 582	M337	M338		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0008	L 6/2	M346	M347		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
001/	L 603	M347	M355		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0010	L 613	M361	M362		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0011	L 624	M362	M370		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0012	L 634	M376	M377		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0013	L 645	M377	M385		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0014	L 655	M4/0	M337		246-217	SV Q^QDC^GNQY^1^S0/	Ad`l	Mnmd	@25	Sxohb`k
0015	L 018/	M737	M738			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0016	L 0180	M74/	M740			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0017	L 0181	M741	M742			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0018	L 0182	M743	M744			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
002/	L 0183	M745	M746			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0020	L 0184	M747	M748			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0021	L 0185	M75/	M750			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0022	L 0186	M751	M752			SV Q^QDC^GNQY^2^S0	Ad`l	Mnmd	@25	Sxohb`k
0023	L 44	M26	M27			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0024	L 52	M33	M34			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0025	L 60	M34	M38			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0026	L 68	M44	M45			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0027	L 76	M45	M5/			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0028	L 84	M55	M56			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
003/	L 0/2	M56	M60			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0030	L 000	M64	M26			SV Q^QDC^GNQY^2^S1	Ad`l	Mnmd	@25	Sxohb`k
0031	L 017	M75	M76			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0032	L 025	M82	M83			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0033	L 034	M83	M88			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0034	L 042	M0/4	M0/5			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0035	L 051	M0/5	M000			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0036	L 06/	M006	M007			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0037	L 068	M007	M012			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
0038	L 076	M016	M75			SV Q^QDC^GNQY^2^S2	Ad`l	Mnmd	@25	Sxohb`k
004/	L 1/8	M027	M028			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0040	L 106	M034	M035			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0041	L 115	M035	M040			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I lnhms	J lnhms	Qns`sd'c--	Rdbshmm Rg`od	Sxod	Cdr hfimKhrs	L`sdqhk	Cdr hfimQtk--
0042	L 123	M046	M047			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0043	L 132	M047	M052			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0044	L 140	M058	M06/			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0045	L 15/	M06/	M064			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0046	L 157	M068	M027			SV Q^QDC^GNQY^2^S3	Ad`l	Mnmd	@25	Sxohb`k
0047	L 18/	M08/	M080			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0048	L 187	M086	M087			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
005/	L 2/6	M087	M1/2			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0050	L 204	M1/8	M10/			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0051	L 213	M10/	M104			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0052	L 221	M110	M111			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0053	L 230	M111	M116			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0054	L 238	M120	M08/			SV Q^QDC^GNQY^2^S4	Ad`l	Mnmd	@25	Sxohb`k
0055	L 260	M131	M132			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0056	L 268	M138	M14/			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0057	L 277	M14/	M144			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0058	L 285	M150	M151			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
006/	L 3/4	M151	M156			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0060	L 302	M162	M163			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0061	L 311	M163	M168			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0062	L 32/	M172	M131			SV Q^QDC^GNQY^2^S5	Ad`l	Mnmd	@25	Sxohb`k
0063	L 341	M183	M184			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0064	L 35/	M2/0	M2/1			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0065	L 358	M2/1	M2/6			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0066	L 366	M202	M203			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0067	L 375	M203	M208			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0068	L 383	M214	M215			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
007/	L 4/2	M215	M220			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0070	L 400	M224	M183			SV Q^QDC^GNQY^2^S6	Ad`l	Mnmd	@25	Sxohb`k
0071	L 422	M235	M236			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0072	L 430	M242	M243			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0073	L 44/	M243	M248			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0074	L 447	M254	M255			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0075	L 456	M255	M260			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0076	L 464	M266	M267			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0077	L 473	M267	M272			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
0078	L 481	M276	M235			SV Q^QDC^GNQY^2^S7	Ad`l	Mnmd	@25	Sxohb`k
008/	L 503	M287	M288			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0080	L 511	M3/4	M3/5			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0081	L 520	M3/5	M300			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0082	L 528	M306	M307			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0083	L 537	M307	M312			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0084	L 545	M318	M32/			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0085	L 554	M32/	M324			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0086	L 562	M328	M287			SV Q^QDC^GNQY^2^S8	Ad`l	Mnmd	@25	Sxohb`k
0087	L 584	M34/	M340		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
0088	L 6/4	M348	M35/		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01//	L 605	M35/	M356		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01/0	L 615	M363	M364		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01/1	L 626	M364	M371		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01/2	L 636	M378	M38/		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01/3	L 647	M38/	M386		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfimKms	L`sdqhk	Cdr hfimQtk--
01/4	L 657	M4/1	M34/		246-217	SV Q^QDC^GNQY^2^S0/	Ad`l	Mnmd	@25	Sxohb`k
01/5	L 0187	M740	M753			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
01/6	L 0188	M753	M752			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
01/7	L 02//	M75/	M754			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
01/8	L 02/0	M754	M748			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
010/	L 02/1	M737	M755			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0100	L 02/2	M755	M741			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0101	L 02/3	M744	M756			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0102	L 02/4	M756	M745			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0103	L 02/5	M742	M743			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0104	L 02/6	M738	M74/			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0105	L 02/7	M751	M750			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0106	L 02/8	M747	M746			SV Q^QDC^GNQY^3^S0	Ad`l	Mnmd	@25	Sxohb`k
0107	L 586	M341	M342		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0108	L 6/6	M350	M351		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
011/	L 607	M351	M357		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0110	L 617	M365	M366		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0111	L 628	M366	M372		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0112	L 638	M380	M381		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0113	L 65/	M381	M387		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0114	L 66/	M4/2	M341		246-217	SV Q^QDC^GNQY^3^S0/	Ad`l	Mnmd	@25	Sxohb`k
0115	L 05	M03	M04			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0116	L 08	M05	M06			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0117	L 12	M06	M08			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0118	L 15	M1/	M10			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
012/	L 2/	M10	M12			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0120	L 22	M13	M14			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0121	L 26	M14	M16			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0122	L 3/	M17	M03			SV Q^QDC^GNQY^S0	Ad`l	Mnmd	@25	Sxohb`k
0123	L 41	M22	M23			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0124	L 5/	M3/	M30			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0125	L 57	M30	M36			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0126	L 65	M40	M41			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0127	L 73	M41	M47			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0128	L 81	M51	M52			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
013/	L 0//	M52	M58			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0130	L 0/7	M62	M22			SV Q^QDC^GNQY^S1	Ad`l	Mnmd	@25	Sxohb`k
0131	L 014	M71	M72			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0132	L 022	M78	M8/			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0133	L 031	M8/	M86			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0134	L 04/	M0/0	M0/1			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0135	L 048	M0/1	M0/8			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0136	L 056	M002	M003			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0137	L 065	M003	M010			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
0138	L 073	M014	M71			SV Q^QDC^GNQY^S2	Ad`l	Mnmd	@25	Sxohb`k
014/	L 1/5	M023	M024			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0140	L 103	M030	M031			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0141	L 112	M031	M038			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0142	L 120	M042	M043			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0143	L 13/	M043	M050			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0144	L 137	M054	M055			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k
0145	L 146	M055	M062			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxohb`k

Member Primary Data (Continued)

	K adk	H nhms	I lnhms	J lnhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr lfim Khms	L`sdqhk	Cdr lfim Qtk--
0146	L 154	M066	M023			SV Q^QDC^GNQY^S3	Ad`l	Mnmd	@25	Sxolb`k
0147	L 176	M075	M076			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0148	L 184	M082	M083			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
015/	L 2/3	M083	M1/0			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0150	L 201	M1/4	M1/5			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0151	L 210	M1/5	M102			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0152	L 218	M106	M107			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0153	L 227	M107	M114			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0154	L 235	M118	M075			SV Q^QDC^GNQY^S4	Ad`l	Mnmd	@25	Sxolb`k
0155	L 257	M127	M128			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0156	L 265	M134	M135			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0157	L 274	M135	M142			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0158	L 282	M146	M147			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
016/	L 3/1	M147	M154			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0160	L 30/	M158	M16/			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0161	L 308	M16/	M166			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0162	L 316	M170	M127			SV Q^QDC^GNQY^S5	Ad`l	Mnmd	@25	Sxolb`k
0163	L 338	M18/	M180			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0164	L 346	M186	M187			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0165	L 355	M187	M2/4			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0166	L 363	M2/8	M20/			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0167	L 372	M20/	M206			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0168	L 380	M210	M211			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
017/	L 4//	M211	M218			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0170	L 4/7	M222	M18/			SV Q^QDC^GNQY^S6	Ad`l	Mnmd	@25	Sxolb`k
0171	L 42/	M231	M232			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0172	L 427	M238	M24/			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0173	L 436	M24/	M246			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0174	L 444	M250	M251			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0175	L 453	M251	M258			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0176	L 461	M262	M263			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0177	L 470	M263	M270			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
0178	L 478	M274	M231			SV Q^QDC^GNQY^S7	Ad`l	Mnmd	@25	Sxolb`k
018/	L 500	M283	M284			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0180	L 508	M3/0	M3/1			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0181	L 517	M3/1	M3/8			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0182	L 525	M302	M303			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0183	L 534	M303	M310			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0184	L 542	M314	M315			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0185	L 551	M315	M322			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0186	L 56/	M326	M283			SV Q^QDC^GNQY^S8	Ad`l	Mnmd	@25	Sxolb`k
0187	L 581	M335	M336		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
0188	L 6/1	M344	M345		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02//	L 602	M345	M354		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/0	L 612	M36/	M360		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/1	L 623	M360	M37/		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/2	L 633	M374	M375		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/3	L 644	M375	M384		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/4	L 654	M4//	M335		246-217	SV Q^QDC^GNQY^S0/	Ad`l	Mnmd	@25	Sxolb`k
02/5	L 4	M0	M2			SV Q^SNO^FHQS^S0	Ad`l	Mnmd	@25	Sxolb`k
02/6	L 5	M2	M4			SV Q^SNO^FHQS^S0	Ad`l	Mnmd	@25	Sxolb`k
02/7	L 6	M4	M6			SV Q^SNO^FHQS^S0	Ad`l	Mnmd	@25	Sxolb`k

Member Primary Data (Continued)

	K adk	H nhms	I nhms	J nhms	Qns`sd'c--	Rdbsmm Rg`od	Sxod	Cdr hfim Kms	L`sdqhk	Cdr hfim Qtk--
02/8	L 7	M6	M0			SV Q^SNO^FHQS^S0	Ad`l	Mnmd	@25	Sxohb`k

Hot Rolled Steel Design Parameters

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop--	J xx	J yy	Ba	Et mbs--
0	L 0163	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
1	L 0164	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
2	L 0165	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
3	L 0166	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
4	L 0167	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
5	L 0168	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
6	L 017/	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
7	L 0170	SV Q^CHdF^NTSDQ^S0	07-/28	07-/28	07-/28	07-/28	07-/28	07-/28	0-/3	0		K sdqhk
8	L 0171	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
9	L 0172	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
00	L 0173	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
01	L 0174	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
02	L 0175	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
03	L 0176	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
04	L 0177	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
05	L 0178	SV Q^CHdF^NTSDQ^S0	04-458	04-458	04-458	04-458	04-458	04-458	0-/4	0		K sdqhk
06	L 04	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
07	L 07	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
08	L 11	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
1/	L 14	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
10	L 18	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
11	L 21	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
12	L 25	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
13	L 28	SV Q^CHdF^S0	07-187	07-187	07-187	07-187	07-187	07-187	0-/4	0		K sdqhk
14	L 40	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
15	L 48	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
16	L 56	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
17	L 64	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
18	L 72	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
2/	L 80	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
20	L 88	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
21	L 0/6	SV Q^CHdF^S1	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
22	L 013	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
23	L 021	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
24	L 030	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
25	L 038	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
26	L 047	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
27	L 055	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
28	L 064	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
3/	L 072	SV Q^CHdF^S2	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/8	0		K sdqhk
30	L 1/4	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk
31	L 102	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk
32	L 111	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk
33	L 12/	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk
34	L 128	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk
35	L 136	SV Q^CHdF^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdqhk

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
36	L 145	SV Q^CHdF ^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
37	L 153	SV Q^CHdF ^S3	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
38	L 175	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
4/	L 183	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
40	L 2/2	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
41	L 200	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
42	L 21/	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
43	L 217	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
44	L 226	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
45	L 234	SV Q^CHdF ^S4	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-0	0		K sdq k
46	L 256	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
47	L 264	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
48	L 273	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
5/	L 281	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
50	L 3/0	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
51	L 3/8	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
52	L 307	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
53	L 315	SV Q^CHdF ^S5	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
54	L 337	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
55	L 345	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
56	L 354	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
57	L 362	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
58	L 371	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
6/	L 38/	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
60	L 388	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
61	L 4/6	SV Q^CHdF ^S6	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
62	L 418	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
63	L 426	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
64	L 435	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
65	L 443	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
66	L 452	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
67	L 460	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
68	L 47/	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
7/	L 477	SV Q^CHdF ^S7	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
70	L 50/	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
71	L 507	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
72	L 516	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
73	L 524	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
74	L 533	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
75	L 541	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
76	L 550	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
77	L 558	SV Q^CHdF ^S8	2/-/82	0/-/20	6-412	6-412	6-412	6-412	0-/7	0		K sdq k
78	L 580	SV Q^CHdF ^S0/	30-676	02-818	5-854	5-854	5-854	5-854	0-/1	0		K sdq k
8/	L 6/0	SV Q^CHdF ^S0/	30-676	02-818	5-854	5-854	5-854	5-854	0-/1	0		K sdq k
80	L 601	SV Q^CHdF ^S0/	30-340	02-706	5-8/8	5-8/8	5-8/8	5-8/8	0-/1	0		K sdq k
81	L 611	SV Q^CHdF ^S0/	30-340	02-706	5-8/8	5-8/8	5-8/8	5-8/8	0-/1	0		K sdq k
82	L 622	SV Q^CHdF ^S0/	30-676	02-818	5-854	5-854	5-854	5-854	0-/1	0		K sdq k
83	L 632	SV Q^CHdF ^S0/	30-676	02-818	5-854	5-854	5-854	5-854	0-/1	0		K sdq k
84	L 643	SV Q^CHdF ^S0/	30-340	02-706	5-8/8	5-8/8	5-8/8	5-8/8	0-/1	0		K sdq k
85	L 653	SV Q^CHdF ^S0/	30-340	02-706	5-8/8	5-8/8	5-8/8	5-8/8	0-/1	0		K sdq k
86	L 016/	SV Q^GNQY^NTSDQ^S0	30-4	7-64	1/-64	1/-64	1/-64	1/-64	0	0		K sdq k
87	L 0160	SV Q^GNQY^NTSDQ^S0	30-4	7-64	1/-64	1/-64	1/-64	1/-64	0	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
88	L 0161	SV Q^GNQY^NTSDQ^S0	30-4	7-64	1/-64	1/-64	1/-64	1/-64	0	0		K sdq k
0//	L 0162	SV Q^GNQY^NTSDQ^S0	30-4	7-64	1/-64	1/-64	1/-64	1/-64	0	0		K sdq k
0/0	L 012	SV Q^GNQY^S2	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/1	L 03/	SV Q^GNQY^S2	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/2	L 046	SV Q^GNQY^S2	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/3	L 063	SV Q^GNQY^S2	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/4	L 1/3	SV Q^GNQY^S3	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/5	L 110	SV Q^GNQY^S3	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/6	L 127	SV Q^GNQY^S3	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/7	L 144	SV Q^GNQY^S3	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
0/8	L 174	SV Q^GNQY^S4	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
00/	L 2/1	SV Q^GNQY^S4	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
000	L 208	SV Q^GNQY^S4	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
001	L 225	SV Q^GNQY^S4	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
002	L 255	SV Q^GNQY^S5	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
003	L 272	SV Q^GNQY^S5	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
004	L 3//	SV Q^GNQY^S5	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
005	L 306	SV Q^GNQY^S5	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
006	L 336	SV Q^GNQY^S6	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
007	L 353	SV Q^GNQY^S6	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
008	L 370	SV Q^GNQY^S6	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
01/	L 387	SV Q^GNQY^S6	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
010	L 417	SV Q^GNQY^S7	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
011	L 434	SV Q^GNQY^S7	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
012	L 451	SV Q^GNQY^S7	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
013	L 468	SV Q^GNQY^S7	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
014	L 5/8	SV Q^GNQY^S8	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
015	L 515	SV Q^GNQY^S8	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
016	L 532	SV Q^GNQY^S8	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
017	L 55/	SV Q^GNQY^S8	22-4	7-264	7-264	7-264	7-264	7-264	0-02	0		K sdq k
018	L 58/	SV Q^GNQY^S0/	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
02/	L 600	SV Q^GNQY^S0/	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
020	L 621	SV Q^GNQY^S0/	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
021	L 642	SV Q^GNQY^S0/	22-4	7-264	7-264	7-264	7-264	7-264	0-01	0		K sdq k
022	L 0110	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
023	L 0111	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
024	L 0112	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
025	L 0113	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
026	L 0114	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
027	L 0115	SV Q^HMMDQ^AQ@BD^S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
028	L 0058	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
03/	L 006/	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
030	L 0060	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
031	L 0061	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
032	L 0062	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
033	L 0063	SV Q^HMMDQ^AQ@BD^S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
034	L 0006	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
035	L 0007	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
036	L 0008	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
037	L 001/	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
038	L 0010	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
04/	L 0011	SV Q^HMMDQ^AQ@BD^S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfsg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
040	L0/54	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
041	L0/55	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
042	L0/56	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
043	L0/57	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
044	L0/58	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
045	L0/6/	SV Q^HMMDQ^AQ@BD^S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
046	L0/02	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
047	L0/03	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
048	L0/04	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
05/	L0/05	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
050	L0/06	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
051	L0/07	SV Q^HMMDQ^AQ@BD^S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
052	L850	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
053	L851	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
054	L852	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
055	L853	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
056	L854	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
057	L855	SV Q^HMMDQ^AQ@BD^S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
058	L8/8	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
06/	L80/	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
060	L800	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
061	L801	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
062	L802	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
063	L803	SV Q^HMMDQ^AQ@BD^S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
064	L0147	SV Q^HMMDQ^BNQMDQ^S1	00-733			Kaxx			0	0		K sdq k
065	L0148	SV Q^HMMDQ^BNQMDQ^S1	00-733			Kaxx			0	0		K sdq k
066	L015/	SV Q^HMMDQ^BNQMDQ^S1	00-733			Kaxx			0	0		K sdq k
067	L0150	SV Q^HMMDQ^BNQMDQ^S1	00-733			Kaxx			0	0		K sdq k
068	L01/5	SV Q^HMMDQ^BNQMDQ^S2	00-733			Kaxx			0-/2	0		K sdq k
07/	L01/6	SV Q^HMMDQ^BNQMDQ^S2	00-733			Kaxx			0-/2	0		K sdq k
070	L01/7	SV Q^HMMDQ^BNQMDQ^S2	00-733			Kaxx			0-/2	0		K sdq k
071	L0043	SV Q^HMMDQ^BNQMDQ^S3	00-733			Kaxx			0-/2	0		K sdq k
072	L0044	SV Q^HMMDQ^BNQMDQ^S3	00-733			Kaxx			0-/2	0		K sdq k
073	L0045	SV Q^HMMDQ^BNQMDQ^S3	00-733			Kaxx			0-/2	0		K sdq k
074	L00/1	SV Q^HMMDQ^BNQMDQ^S4	00-733			Kaxx			0-/2	0		K sdq k
075	L00/2	SV Q^HMMDQ^BNQMDQ^S4	00-733			Kaxx			0-/2	0		K sdq k
076	L00/3	SV Q^HMMDQ^BNQMDQ^S4	00-733			Kaxx			0-/2	0		K sdq k
077	L0/4/	SV Q^HMMDQ^BNQMDQ^S5	00-733			Kaxx			0-/2	0		K sdq k
078	L0/40	SV Q^HMMDQ^BNQMDQ^S5	00-733			Kaxx			0-/2	0		K sdq k
08/	L0/41	SV Q^HMMDQ^BNQMDQ^S5	00-733			Kaxx			0-/2	0		K sdq k
080	L887	SV Q^HMMDQ^BNQMDQ^S6	00-733			Kaxx			0-/2	0		K sdq k
081	L888	SV Q^HMMDQ^BNQMDQ^S6	00-733			Kaxx			0-/2	0		K sdq k
082	L0///	SV Q^HMMDQ^BNQMDQ^S6	00-733			Kaxx			0-/2	0		K sdq k
083	L835	SV Q^HMMDQ^BNQMDQ^S7	00-733			Kaxx			0-/2	0		K sdq k
084	L836	SV Q^HMMDQ^BNQMDQ^S7	00-733			Kaxx			0-/2	0		K sdq k
085	L837	SV Q^HMMDQ^BNQMDQ^S7	00-733			Kaxx			0-/2	0		K sdq k
086	L783	SV Q^HMMDQ^BNQMDQ^S8	00-733			Kaxx			0-/2	0		K sdq k
087	L784	SV Q^HMMDQ^BNQMDQ^S8	00-733			Kaxx			0-/2	0		K sdq k
088	L785	SV Q^HMMDQ^BNQMDQ^S8	00-733			Kaxx			0-/2	0		K sdq k
1//	L734	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdq k
1/0	L735	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdq k
1/1	L736	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl osno--	Kbnl oans--	K,snop---	Jxx	Jyy	Ba	Etmbs--
1/2	L737	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
1/3	L738	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
1/4	L74/	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
1/5	L740	SV Q^HMMDQ^FHQS^S0/	4-264	4-264	4-264	4-264	4-264	4-264	0	0		K sdqk
1/6	L741	SV Q^HMMDQ^FHQS^S0/	4-264	4-264	4-264	4-264	4-264	4-264	0	0		K sdqk
1/7	L748	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
1/8	L75/	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
10/	L750	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
100	L751	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
101	L752	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
102	L753	SV Q^HMMDQ^FHQS^S0/	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk
103	L754	SV Q^HMMDQ^FHQS^S0/	3-132	3-132	3-132	3-132	3-132	3-132	0	0		K sdqk
104	L0116	SV Q^HMMDQ^K@CCDQ^S2	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
105	L0117	SV Q^HMMDQ^K@CCDQ^S2	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
106	L0118	SV Q^HMMDQ^K@CCDQ^S2	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
107	L0064	SV Q^HMMDQ^K@CCDQ^S3	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
108	L0065	SV Q^HMMDQ^K@CCDQ^S3	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
11/	L0066	SV Q^HMMDQ^K@CCDQ^S3	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
110	L0012	SV Q^HMMDQ^K@CCDQ^S4	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
111	L0013	SV Q^HMMDQ^K@CCDQ^S4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
112	L0014	SV Q^HMMDQ^K@CCDQ^S4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
113	L0/60	SV Q^HMMDQ^K@CCDQ^S5	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
114	L0/61	SV Q^HMMDQ^K@CCDQ^S5	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
115	L0/62	SV Q^HMMDQ^K@CCDQ^S5	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
116	L0/08	SV Q^HMMDQ^K@CCDQ^S6	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
117	L0/1/	SV Q^HMMDQ^K@CCDQ^S6	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
118	L0/10	SV Q^HMMDQ^K@CCDQ^S6	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
12/	L856	SV Q^HMMDQ^K@CCDQ^S7	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
120	L857	SV Q^HMMDQ^K@CCDQ^S7	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
121	L858	SV Q^HMMDQ^K@CCDQ^S7	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
122	L804	SV Q^HMMDQ^K@CCDQ^S8	7-374	7-374	7-374	7-374	7-374	7-374	0-01	0		K sdqk
123	L805	SV Q^HMMDQ^K@CCDQ^S8	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
124	L806	SV Q^HMMDQ^K@CCDQ^S8	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	7-6/4	0-01	0		K sdqk
125	L0143	SV Q^HMMDQ^RP^S1	05-64	7-264	05-64	05-64	05-64	05-64	0	0		K sdqk
126	L0144	SV Q^HMMDQ^RP^S1	05-64	7-264	05-64	05-64	05-64	05-64	0	0		K sdqk
127	L0145	SV Q^HMMDQ^RP^S1	05-64	7-264	05-64	05-64	05-64	05-64	0	0		K sdqk
128	L0146	SV Q^HMMDQ^RP^S1	05-64	7-264	05-64	05-64	05-64	05-64	0	0		K sdqk
13/	L01/1	SV Q^HMMDQ^RP^S2	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
130	L01/2	SV Q^HMMDQ^RP^S2	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
131	L01/3	SV Q^HMMDQ^RP^S2	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
132	L01/4	SV Q^HMMDQ^RP^S2	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
133	L004/	SV Q^HMMDQ^RP^S3	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
134	L0040	SV Q^HMMDQ^RP^S3	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
135	L0041	SV Q^HMMDQ^RP^S3	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
136	L0042	SV Q^HMMDQ^RP^S3	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
137	L0/87	SV Q^HMMDQ^RP^S4	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
138	L0/88	SV Q^HMMDQ^RP^S4	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
14/	L00//	SV Q^HMMDQ^RP^S4	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
140	L00/0	SV Q^HMMDQ^RP^S4	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
141	L0/35	SV Q^HMMDQ^RP^S5	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
142	L0/36	SV Q^HMMDQ^RP^S5	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk
143	L0/37	SV Q^HMMDQ^RP^S5	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqk

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
144	L 0/38	SV Q^HMMDQ^RP^S5	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
145	L 883	SV Q^HMMDQ^RP^S6	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
146	L 884	SV Q^HMMDQ^RP^S6	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
147	L 885	SV Q^HMMDQ^RP^S6	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
148	L 886	SV Q^HMMDQ^RP^S6	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
15/	L 831	SV Q^HMMDQ^RP^S7	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
150	L 832	SV Q^HMMDQ^RP^S7	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
151	L 833	SV Q^HMMDQ^RP^S7	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
152	L 834	SV Q^HMMDQ^RP^S7	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
153	L 78/	SV Q^HMMDQ^RP^S8	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
154	L 780	SV Q^HMMDQ^RP^S8	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
155	L 781	SV Q^HMMDQ^RP^S8	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
156	L 782	SV Q^HMMDQ^RP^S8	05-64	7-264	05-64	05-64	05-64	05-64	0-/5	0		K sdqjk
157	L 31	SV Q^HMMDQ^RTOO^S1	12-577	4-811	00-733	00-733	00-733	00-733	0	0		K sdqjk
158	L 32	SV Q^HMMDQ^RTOO^S1	12-577	4-811	00-733	00-733	00-733	00-733	0	0		K sdqjk
16/	L 33	SV Q^HMMDQ^RTOO^S1	12-577	4-811	00-733	00-733	00-733	00-733	0	0		K sdqjk
160	L 34	SV Q^HMMDQ^RTOO^S1	12-577	4-811	00-733	00-733	00-733	00-733	0	0		K sdqjk
161	L 35	SV Q^HMMDQ^RTOO^S1	22-4	22-4	22-4	22-4	22-4	22-4	0	0		K sdqjk
162	L 004	SV Q^HMMDQ^RTOO^S1	00-733	00-733	00-733	00-733	00-733	00-733	0	0		K sdqjk
163	L 005	SV Q^HMMDQ^RTOO^S1	00-733	00-733	00-733	00-733	00-733	00-733	0	0		K sdqjk
164	L 006	SV Q^HMMDQ^RTOO^S1	00-733	00-733	00-733	00-733	00-733	00-733	0	0		K sdqjk
165	L 007	SV Q^HMMDQ^RTOO^S1	00-733	00-733	00-733	00-733	00-733	00-733	0	0		K sdqjk
166	L 080	SV Q^HMMDQ^RTOO^S2	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
167	L 081	SV Q^HMMDQ^RTOO^S2	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
168	L 082	SV Q^HMMDQ^RTOO^S2	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
17/	L 083	SV Q^HMMDQ^RTOO^S2	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
170	L 084	SV Q^HMMDQ^RTOO^S2	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdqjk
171	L 085	SV Q^HMMDQ^RTOO^S2	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
172	L 086	SV Q^HMMDQ^RTOO^S2	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
173	L 087	SV Q^HMMDQ^RTOO^S2	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
174	L 088	SV Q^HMMDQ^RTOO^S2	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
175	L 161	SV Q^HMMDQ^RTOO^S3	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
176	L 162	SV Q^HMMDQ^RTOO^S3	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
177	L 163	SV Q^HMMDQ^RTOO^S3	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
178	L 164	SV Q^HMMDQ^RTOO^S3	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
18/	L 165	SV Q^HMMDQ^RTOO^S3	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdqjk
180	L 166	SV Q^HMMDQ^RTOO^S3	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
181	L 167	SV Q^HMMDQ^RTOO^S3	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
182	L 168	SV Q^HMMDQ^RTOO^S3	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
183	L 17/	SV Q^HMMDQ^RTOO^S3	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
184	L 242	SV Q^HMMDQ^RTOO^S4	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
185	L 243	SV Q^HMMDQ^RTOO^S4	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
186	L 244	SV Q^HMMDQ^RTOO^S4	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
187	L 245	SV Q^HMMDQ^RTOO^S4	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
188	L 246	SV Q^HMMDQ^RTOO^S4	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdqjk
2//	L 247	SV Q^HMMDQ^RTOO^S4	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
2/0	L 248	SV Q^HMMDQ^RTOO^S4	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
2/1	L 25/	SV Q^HMMDQ^RTOO^S4	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
2/2	L 250	SV Q^HMMDQ^RTOO^S4	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdqjk
2/3	L 323	SV Q^HMMDQ^RTOO^S5	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
2/4	L 324	SV Q^HMMDQ^RTOO^S5	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk
2/5	L 325	SV Q^HMMDQ^RTOO^S5	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdqjk

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
2/6	L326	SV Q^HMMDQ^RTOO^S5	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
2/7	L327	SV Q^HMMDQ^RTOO^S5	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdq k
2/8	L328	SV Q^HMMDQ^RTOO^S5	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
20/	L33/	SV Q^HMMDQ^RTOO^S5	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
200	L330	SV Q^HMMDQ^RTOO^S5	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
201	L331	SV Q^HMMDQ^RTOO^S5	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
202	L404	SV Q^HMMDQ^RTOO^S6	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
203	L405	SV Q^HMMDQ^RTOO^S6	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
204	L406	SV Q^HMMDQ^RTOO^S6	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
205	L407	SV Q^HMMDQ^RTOO^S6	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
206	L408	SV Q^HMMDQ^RTOO^S6	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdq k
207	L41/	SV Q^HMMDQ^RTOO^S6	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
208	L410	SV Q^HMMDQ^RTOO^S6	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
21/	L411	SV Q^HMMDQ^RTOO^S6	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
210	L412	SV Q^HMMDQ^RTOO^S6	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
211	L485	SV Q^HMMDQ^RTOO^S7	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
212	L486	SV Q^HMMDQ^RTOO^S7	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
213	L487	SV Q^HMMDQ^RTOO^S7	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
214	L488	SV Q^HMMDQ^RTOO^S7	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
215	L5//	SV Q^HMMDQ^RTOO^S7	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdq k
216	L5/0	SV Q^HMMDQ^RTOO^S7	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
217	L5/1	SV Q^HMMDQ^RTOO^S7	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
218	L5/2	SV Q^HMMDQ^RTOO^S7	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
22/	L5/3	SV Q^HMMDQ^RTOO^S7	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
220	L566	SV Q^HMMDQ^RTOO^S8	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
221	L567	SV Q^HMMDQ^RTOO^S8	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
222	L568	SV Q^HMMDQ^RTOO^S8	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
223	L57/	SV Q^HMMDQ^RTOO^S8	12-577	4-811	00-733	00-733	00-733	00-733	0-13	0		K sdq k
224	L570	SV Q^HMMDQ^RTOO^S8	22-4	22-4	22-4	22-4	22-4	22-4	0-/0	0		K sdq k
225	L571	SV Q^HMMDQ^RTOO^S8	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
226	L572	SV Q^HMMDQ^RTOO^S8	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
227	L573	SV Q^HMMDQ^RTOO^S8	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
228	L574	SV Q^HMMDQ^RTOO^S8	00-733	00-733	00-733	00-733	00-733	00-733	0-/5	0		K sdq k
23/	L01/8	SV Q^HMMDQ^SQH-S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
230	L010/	SV Q^HMMDQ^SQH-S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
231	L0100	SV Q^HMMDQ^SQH-S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
232	L0101	SV Q^HMMDQ^SQH-S2	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
233	L0102	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
234	L0103	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
235	L0104	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
236	L0105	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
237	L0106	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
238	L0107	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
24/	L0108	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
240	L011/	SV Q^HMMDQ^SQH-S2	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
241	L0046	SV Q^HMMDQ^SQH-S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
242	L0047	SV Q^HMMDQ^SQH-S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
243	L0048	SV Q^HMMDQ^SQH-S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
244	L005/	SV Q^HMMDQ^SQH-S3	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
245	L0050	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
246	L0051	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
247	L0052	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---	
248	L 0053	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
25/	L 0054	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
250	L 0055	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
251	L 0056	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
252	L 0057	SV Q^HMMDQ^SQH-S3	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
253	L 00/4	SV Q^HMMDQ^SQH-S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
254	L 00/5	SV Q^HMMDQ^SQH-S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
255	L 00/6	SV Q^HMMDQ^SQH-S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
256	L 00/7	SV Q^HMMDQ^SQH-S4	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
257	L 00/8	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
258	L 000/	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
26/	L 0000	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
260	L 0001	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
261	L 0002	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
262	L 0003	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
263	L 0004	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
264	L 0005	SV Q^HMMDQ^SQH-S4	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
265	L 0/42	SV Q^HMMDQ^SQH-S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
266	L 0/43	SV Q^HMMDQ^SQH-S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
267	L 0/44	SV Q^HMMDQ^SQH-S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
268	L 0/45	SV Q^HMMDQ^SQH-S5	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
27/	L 0/46	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
270	L 0/47	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
271	L 0/48	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
272	L 0/5/	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
273	L 0/50	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
274	L 0/51	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
275	L 0/52	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
276	L 0/53	SV Q^HMMDQ^SQH-S5	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
277	L 0//0	SV Q^HMMDQ^SQH-S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
278	L 0//1	SV Q^HMMDQ^SQH-S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
28/	L 0//2	SV Q^HMMDQ^SQH-S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
280	L 0//3	SV Q^HMMDQ^SQH-S6	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
281	L 0//4	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
282	L 0//5	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
283	L 0//6	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
284	L 0//7	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
285	L 0//8	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
286	L 0/0/	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
287	L 0/00	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
288	L 0/01	SV Q^HMMDQ^SQH-S6	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3//	L 838	SV Q^HMMDQ^SQH-S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
3/0	L 84/	SV Q^HMMDQ^SQH-S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
3/1	L 840	SV Q^HMMDQ^SQH-S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
3/2	L 841	SV Q^HMMDQ^SQH-S7	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k	
3/3	L 842	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3/4	L 843	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3/5	L 844	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3/6	L 845	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3/7	L 846	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
3/8	L 847	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	
30/	L 848	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k	

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
300	L 85/	SV Q^HMMDQ^SQH-S7	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
301	L 786	SV Q^HMMDQ^SQH-S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
302	L 787	SV Q^HMMDQ^SQH-S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
303	L 788	SV Q^HMMDQ^SQH-S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
304	L 8//	SV Q^HMMDQ^SQH-S8	7-264	7-264	7-264	7-264	7-264	7-264	0-/5	0		K sdq k
305	L 8/0	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
306	L 8/1	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
307	L 8/2	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
308	L 8/3	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
31/	L 8/4	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
310	L 8/5	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
311	L 8/6	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
312	L 8/7	SV Q^HMMDQ^SQH-S8	4-811	4-811	4-811	4-811	4-811	4-811	0-01	0		K sdq k
313	L 0155	SV Q^KDF^NT SDQ^S0	02-61	02-61	02-61	02-61	02-61	02-61	0-/1	0		K sdq k
314	L 0156	SV Q^KDF^NT SDQ^S0	02-61	02-61	02-61	02-61	02-61	02-61	0-/1	0		K sdq k
315	L 0157	SV Q^KDF^NT SDQ^S0	02-61	02-61	02-61	02-61	02-61	02-61	0-/1	0		K sdq k
316	L 0158	SV Q^KDF^NT SDQ^S0	02-61	02-61	02-61	02-61	02-61	02-61	0-/1	0		K sdq k
317	L 0	SV Q^KDF^S0	02-61	02-61	02-61	02-61	02-61	02-61	0	0		K sdq k
318	L 1	SV Q^KDF^S0	02-61	02-61	02-61	02-61	02-61	02-61	0	0		K sdq k
32/	L 2	SV Q^KDF^S0	02-61	02-61	02-61	02-61	02-61	02-61	0	0		K sdq k
320	L 3	SV Q^KDF^S0	02-61	02-61	02-61	02-61	02-61	02-61	0	0		K sdq k
321	L 36	SV Q^KDF^S1	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
322	L 37	SV Q^KDF^S1	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
323	L 38	SV Q^KDF^S1	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
324	L 4/	SV Q^KDF^S1	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
325	L 008	SV Q^KDF^S2	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
326	L 01/	SV Q^KDF^S2	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
327	L 010	SV Q^KDF^S2	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
328	L 011	SV Q^KDF^S2	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
33/	L 1//	SV Q^KDF^S3	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
330	L 1/0	SV Q^KDF^S3	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
331	L 1/1	SV Q^KDF^S3	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
332	L 1/2	SV Q^KDF^S3	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
333	L 170	SV Q^KDF^S4	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
334	L 171	SV Q^KDF^S4	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
335	L 172	SV Q^KDF^S4	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
336	L 173	SV Q^KDF^S4	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
337	L 251	SV Q^KDF^S5	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
338	L 252	SV Q^KDF^S5	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
34/	L 253	SV Q^KDF^S5	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
340	L 254	SV Q^KDF^S5	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
341	L 332	SV Q^KDF^S6	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
342	L 333	SV Q^KDF^S6	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
343	L 334	SV Q^KDF^S6	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
344	L 335	SV Q^KDF^S6	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
345	L 413	SV Q^KDF^S7	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
346	L 414	SV Q^KDF^S7	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
347	L 415	SV Q^KDF^S7	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
348	L 416	SV Q^KDF^S7	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
35/	L 5/4	SV Q^KDF^S8	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
350	L 5/5	SV Q^KDF^S8	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
351	L 5/6	SV Q^KDF^S8	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfisgz--	Kaxxzes	Kayyzes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
352	L 5/7	SV Q^KDF^S8	14	5-14	5-14	5-14	5-14	5-14	0	0		K sdq k
353	L 575	SV Q^KDF^S0/	26-435	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl ---	0	0		K sdq k
354	L 576	SV Q^KDF^S0/	26-435	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl ---	0	0		K sdq k
355	L 577	SV Q^KDF^S0/	26-435	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl ---	0	0		K sdq k
356	L 578	SV Q^KDF^S0/	26-435	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl dms	Rdfl ---	0	0		K sdq k
357	L 771	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
358	L 772	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
36/	L 773	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
360	L 774	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
361	L 775	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
362	L 776	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
363	L 777	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
364	L 778	SV Q^QDCGHOCHG@1^S8	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
365	L 680	SV Q^QDC^CHGF^/^S0/	5-684	5-684	5-684	5-684	5-684	5-684	0	0		K sdq k
366	L 681	SV Q^QDC^CHGF^/^S0/	5-627	5-627	5-627	5-627	5-627	5-627	0	0		K sdq k
367	L 682	SV Q^QDC^CHGF^/^S0/	5-684	5-684	5-684	5-684	5-684	5-684	0	0		K sdq k
368	L 683	SV Q^QDC^CHGF^/^S0/	5-627	5-627	5-627	5-627	5-627	5-627	0	0		K sdq k
37/	L 684	SV Q^QDC^CHGF^/^S0/	5-627	5-627	5-627	5-627	5-627	5-627	0	0		K sdq k
370	L 685	SV Q^QDC^CHGF^/^S0/	5-684	5-684	5-684	5-684	5-684	5-684	0	0		K sdq k
371	L 686	SV Q^QDC^CHGF^/^S0/	5-684	5-684	5-684	5-684	5-684	5-684	0	0		K sdq k
372	L 687	SV Q^QDC^CHGF^/^S0/	5-627	5-627	5-627	5-627	5-627	5-627	0	0		K sdq k
373	L 45	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
374	L 53	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
375	L 61	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
376	L 7/	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
377	L 77	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
378	L 85	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
38/	L 0/3	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
380	L 001	SV Q^QDC^CHGF^1^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
381	L 018	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
382	L 026	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
383	L 035	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
384	L 043	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
385	L 052	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
386	L 060	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
387	L 07/	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
388	L 077	SV Q^QDC^CHGF^1^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
4//	L 10/	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/0	L 107	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/1	L 116	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/2	L 124	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/3	L 133	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/4	L 141	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/5	L 150	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/6	L 158	SV Q^QDC^CHGF^1^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
4/7	L 180	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
4/8	L 188	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
40/	L 2/7	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
400	L 205	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
401	L 214	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
402	L 222	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
403	L 231	SV Q^QDC^CHGF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
404	L 24/	SV Q^QDC^CHdF^1^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
405	L 261	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
406	L 27/	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
407	L 278	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
408	L 286	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
41/	L 3/5	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
410	L 303	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
411	L 312	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
412	L 320	SV Q^QDC^CHdF^1^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
413	L 342	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
414	L 350	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
415	L 36/	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
416	L 367	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
417	L 376	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
418	L 384	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
42/	L 4/3	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
420	L 401	SV Q^QDC^CHdF^1^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
421	L 423	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
422	L 431	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
423	L 440	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
424	L 448	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
425	L 457	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
426	L 465	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
427	L 474	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
428	L 482	SV Q^QDC^CHdF^1^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
43/	L 504	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
430	L 512	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
431	L 521	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
432	L 53/	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
433	L 538	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
434	L 546	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
435	L 555	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
436	L 563	SV Q^QDC^CHdF^1^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
437	L 585	SV Q^QDC^CHdF^1^S0/	0/-12	8-33	8-33	8-33	8-33	8-33	0-/4	0		K sdq k
438	L 6/5	SV Q^QDC^CHdF^1^S0/	0/-12	8-33	8-33	8-33	8-33	8-33	0-/4	0		K sdq k
44/	L 606	SV Q^QDC^CHdF^1^S0/	0/-232	8-442	8-442	8-442	8-442	8-442	0-/4	0		K sdq k
440	L 616	SV Q^QDC^CHdF^1^S0/	0/-232	8-442	8-442	8-442	8-442	8-442	0-/4	0		K sdq k
441	L 627	SV Q^QDC^CHdF^1^S0/	0/-12	8-33	8-33	8-33	8-33	8-33	0-/4	0		K sdq k
442	L 637	SV Q^QDC^CHdF^1^S0/	0/-12	8-33	8-33	8-33	8-33	8-33	0-/4	0		K sdq k
443	L 648	SV Q^QDC^CHdF^1^S0/	0/-232	8-442	8-442	8-442	8-442	8-442	0-/4	0		K sdq k
444	L 658	SV Q^QDC^CHdF^1^S0/	0/-232	8-442	8-442	8-442	8-442	8-442	0-/4	0		K sdq k
445	L 46	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
446	L 47	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
447	L 54	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
448	L 55	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
45/	L 62	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
450	L 63	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
451	L 70	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
452	L 71	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
453	L 78	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
454	L 8/	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
455	L 86	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
456	L 87	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
457	L 0/4	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
458	L 0/5	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
46/	L 002	SV Q^QDC^CHdF^2^S1	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
460	L 003	SV Q^QDC^CHdF^2^S1	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
461	L 02/	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
462	L 020	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
463	L 027	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
464	L 028	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
465	L 036	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
466	L 037	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
467	L 044	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
468	L 045	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
47/	L 053	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
470	L 054	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
471	L 061	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
472	L 062	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
473	L 070	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
474	L 071	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
475	L 078	SV Q^QDC^CHdF^2^S2	0/-34	0/-02	0/-02	0/-02	0/-02	0/-02	0-/3	0		K sdq k
476	L 08/	SV Q^QDC^CHdF^2^S2	6-412	6-1/2	6-1/2	6-1/2	6-1/2	6-1/2	0-/7	0		K sdq k
477	L 100	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
478	L 101	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
48/	L 108	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
480	L 11/	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
481	L 117	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
482	L 118	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
483	L 125	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
484	L 126	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
485	L 134	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
486	L 135	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
487	L 142	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
488	L 143	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
5//	L 151	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
5/0	L 152	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
5/1	L 16/	SV Q^QDC^CHdF^2^S3	0/-34	0/-01	0/-01	0/-01	0/-01	0/-01	0-/3	0		K sdq k
5/2	L 160	SV Q^QDC^CHdF^2^S3	6-412	6-082	6-082	6-082	6-082	6-082	0-/7	0		K sdq k
5/3	L 181	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
5/4	L 182	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
5/5	L 2//	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
5/6	L 2/0	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
5/7	L 2/8	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
5/8	L 20/	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
50/	L 206	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
500	L 207	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
501	L 215	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
502	L 216	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
503	L 223	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
504	L 224	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
505	L 232	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k
506	L 233	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
507	L 240	SV Q^QDC^CHdF^2^S4	0/-34	0/-/2	0/-/2	0/-/2	0/-/2	0/-/2	0-/3	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfsg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
508	L 241	SV Q^QDC^CHdF^2^S4	6-412	6-0/2	6-0/2	6-0/2	6-0/2	6-0/2	0-/8	0		K sdq k
51/	L 262	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
510	L 263	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
511	L 270	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
512	L 271	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
513	L 28/	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
514	L 280	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
515	L 287	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
516	L 288	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
517	L 3/6	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
518	L 3/7	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
52/	L 304	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
520	L 305	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
521	L 313	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
522	L 314	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
523	L 321	SV Q^QDC^CHdF^2^S5	0/-34	0/-/1	0/-/1	0/-/1	0/-/1	0/-/1	0-/3	0		K sdq k
524	L 322	SV Q^QDC^CHdF^2^S5	6-412	6-/82	6-/82	6-/82	6-/82	6-/82	0-/8	0		K sdq k
525	L 343	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
526	L 344	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
527	L 351	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
528	L 352	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
53/	L 360	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
530	L 361	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
531	L 368	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
532	L 37/	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
533	L 377	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
534	L 378	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
535	L 385	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
536	L 386	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
537	L 4/4	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
538	L 4/5	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
54/	L 402	SV Q^QDC^CHdF^2^S6	0/-34	8-82	8-82	8-82	8-82	8-82	0-/4	0		K sdq k
540	L 403	SV Q^QDC^CHdF^2^S6	6-412	6-//2	6-//2	6-//2	6-//2	6-//2	0-/8	0		K sdq k
541	L 424	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
542	L 425	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
543	L 432	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
544	L 433	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
545	L 441	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
546	L 442	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
547	L 45/	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
548	L 450	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
55/	L 458	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
550	L 46/	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
551	L 466	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
552	L 467	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
553	L 475	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
554	L 476	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
555	L 483	SV Q^QDC^CHdF^2^S7	0/-34	8-81	8-81	8-81	8-81	8-81	0-/4	0		K sdq k
556	L 484	SV Q^QDC^CHdF^2^S7	6-412	5-882	5-882	5-882	5-882	5-882	0-/8	0		K sdq k
557	L 505	SV Q^QDC^CHdF^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k
558	L 506	SV Q^QDC^CHdF^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/8	0		K sdq k
56/	L 513	SV Q^QDC^CHdF^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/4	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
560	L 514	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
561	L 522	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
562	L 523	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
563	L 530	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
564	L 531	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
565	L 54/	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
566	L 540	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
567	L 547	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
568	L 548	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
57/	L 556	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
570	L 557	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
571	L 564	SV Q^QDC^CH@F^2^S8	0/-34	8-80	8-80	8-80	8-80	8-80	0-/ 4	0		K sdq k
572	L 565	SV Q^QDC^CH@F^2^S8	6-412	5-872	5-872	5-872	5-872	5-872	0-/ 8	0		K sdq k
573	L 587	SV Q^QDC^CH@F^2^S0/	01-445	00-785	00-785	00-785	00-785	00-785	0-/ 2	0		K sdq k
574	L 6/7	SV Q^QDC^CH@F^2^S0/	01-445	00-785	00-785	00-785	00-785	00-785	0-/ 2	0		K sdq k
575	L 608	SV Q^QDC^CH@F^2^S0/	01-568	01-/08	01-/08	01-/08	01-/08	01-/08	0-/ 2	0		K sdq k
576	L 618	SV Q^QDC^CH@F^2^S0/	01-568	01-/08	01-/08	01-/08	01-/08	01-/08	0-/ 2	0		K sdq k
577	L 63/	SV Q^QDC^CH@F^2^S0/	01-445	00-785	00-785	00-785	00-785	00-785	0-/ 2	0		K sdq k
578	L 64/	SV Q^QDC^CH@F^2^S0/	01-445	00-785	00-785	00-785	00-785	00-785	0-/ 2	0		K sdq k
58/	L 650	SV Q^QDC^CH@F^2^S0/	01-568	01-155	01-155	01-155	01-155	01-155	0-/ 2	0		K sdq k
580	L 660	SV Q^QDC^CH@F^2^S0/	01-568	01-/08	01-/08	01-/08	01-/08	01-/08	0-/ 2	0		K sdq k
581	L 588	SV Q^QDC^CH@F^3^S0/	0/-564	8-884	8-884	8-884	8-884	8-884	0-/ 4	0		K sdq k
582	L 6//	SV Q^QDC^CH@F^3^S0/	7-088	6-408	6-408	6-408	6-408	6-408	0-/ 7	0		K sdq k
583	L 6/8	SV Q^QDC^CH@F^3^S0/	0/-564	8-884	8-884	8-884	8-884	8-884	0-/ 4	0		K sdq k
584	L 60/	SV Q^QDC^CH@F^3^S0/	7-088	6-408	6-408	6-408	6-408	6-408	0-/ 7	0		K sdq k
585	L 61/	SV Q^QDC^CH@F^3^S0/	0/-454	8-774	8-774	8-774	8-774	8-774	0-/ 4	0		K sdq k
586	L 610	SV Q^QDC^CH@F^3^S0/	7-182	6-502	6-502	6-502	6-502	6-502	0-/ 7	0		K sdq k
587	L 62/	SV Q^QDC^CH@F^3^S0/	0/-454	8-774	8-774	8-774	8-774	8-774	0-/ 4	0		K sdq k
588	L 620	SV Q^QDC^CH@F^3^S0/	7-182	6-502	6-502	6-502	6-502	6-502	0-/ 7	0		K sdq k
6//	L 630	SV Q^QDC^CH@F^3^S0/	0/-564	8-884	8-884	8-884	8-884	8-884	0-/ 4	0		K sdq k
6/0	L 631	SV Q^QDC^CH@F^3^S0/	7-088	6-408	6-408	6-408	6-408	6-408	0-/ 7	0		K sdq k
6/1	L 640	SV Q^QDC^CH@F^3^S0/	0/-564	8-884	8-884	8-884	8-884	8-884	0-/ 4	0		K sdq k
6/2	L 641	SV Q^QDC^CH@F^3^S0/	7-088	6-408	6-408	6-408	6-408	6-408	0-/ 7	0		K sdq k
6/3	L 651	SV Q^QDC^CH@F^3^S0/	0/-454	8-774	8-774	8-774	8-774	8-774	0-/ 4	0		K sdq k
6/4	L 652	SV Q^QDC^CH@F^3^S0/	7-182	6-502	6-502	6-502	6-502	6-502	0-/ 7	0		K sdq k
6/5	L 661	SV Q^QDC^CH@F^3^S0/	0/-454	8-774	8-774	8-774	8-774	8-774	0-/ 4	0		K sdq k
6/6	L 662	SV Q^QDC^CH@F^3^S0/	7-182	6-502	6-502	6-502	6-502	6-502	0-/ 7	0		K sdq k
6/7	L 06	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
6/8	L 1/	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
60/	L 13	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
600	L 16	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
601	L 20	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
602	L 23	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
603	L 27	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
604	L 30	SV Q^QDC^CH@F^S0	8-038	7-728	7-728	7-728	7-728	7-728	0	0		K sdq k
605	L 43	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
606	L 51	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
607	L 6/	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
608	L 67	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
61/	L 75	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
610	L 83	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k
611	L 0/1	SV Q^QDC^CH@F^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfsg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
612	L 00/	SV Q^QDC^CH@F ^S1	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
613	L 016	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
614	L 024	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
615	L 033	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
616	L 041	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
617	L 050	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
618	L 058	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
62/	L 067	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
620	L 075	SV Q^QDC^CH@F ^S2	6-412	6-/5	6-/5	6-/5	6-/5	6-/5	0	0		K sdqk
621	L 1/7	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
622	L 105	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
623	L 114	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
624	L 122	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
625	L 131	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
626	L 14/	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
627	L 148	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
628	L 156	SV Q^QDC^CH@F ^S3	6-412	6-/4	6-/4	6-/4	6-/4	6-/4	0	0		K sdqk
63/	L 178	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
630	L 186	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
631	L 2/5	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
632	L 203	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
633	L 212	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
634	L 220	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
635	L 23/	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
636	L 237	SV Q^QDC^CH@F ^S4	6-412	5-81	5-81	5-81	5-81	5-81	0	0		K sdqk
637	L 26/	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
638	L 267	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
64/	L 276	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
640	L 284	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
641	L 3/3	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
642	L 301	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
643	L 310	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
644	L 318	SV Q^QDC^CH@F ^S5	6-412	5-80	5-80	5-80	5-80	5-80	0	0		K sdqk
645	L 340	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
646	L 348	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
647	L 357	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
648	L 365	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
65/	L 374	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
650	L 382	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
651	L 4/1	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
652	L 40/	SV Q^QDC^CH@F ^S6	6-412	5-66	5-66	5-66	5-66	5-66	0	0		K sdqk
653	L 421	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
654	L 43/	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
655	L 438	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
656	L 446	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
657	L 455	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
658	L 463	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
66/	L 472	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
660	L 480	SV Q^QDC^CH@F ^S7	6-412	5-65	5-65	5-65	5-65	5-65	0	0		K sdqk
661	L 502	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
662	L 510	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
663	L 52/	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsg Z--	Kaxx Zes	Kayy Zes	Kbnl osno---	Kbnl oans---	K,snop---	Jxx	Jyy	Ba	Etmbs---
664	L 527	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
665	L 536	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
666	L 544	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
667	L 553	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
668	L 561	SV Q^QDC^CH@F ^S8	6-412	5-63	5-63	5-63	5-63	5-63	0	0		K sdqk
67/	L 583	SV Q^QDC^CH@F ^S0/	7-088	5-7/8	5-7/8	5-7/8	5-7/8	5-7/8	0	0		K sdqk
670	L 6/3	SV Q^QDC^CH@F ^S0/	7-088	5-7/8	5-7/8	5-7/8	5-7/8	5-7/8	0	0		K sdqk
671	L 604	SV Q^QDC^CH@F ^S0/	7-182	5-8/2	5-8/2	5-8/2	5-8/2	5-8/2	0	0		K sdqk
672	L 614	SV Q^QDC^CH@F ^S0/	7-182	5-8/2	5-8/2	5-8/2	5-8/2	5-8/2	0	0		K sdqk
673	L 625	SV Q^QDC^CH@F ^S0/	7-088	5-7/8	5-7/8	5-7/8	5-7/8	5-7/8	0	0		K sdqk
674	L 635	SV Q^QDC^CH@F ^S0/	7-088	5-7/8	5-7/8	5-7/8	5-7/8	5-7/8	0	0		K sdqk
675	L 646	SV Q^QDC^CH@F ^S0/	7-182	5-8/2	5-8/2	5-8/2	5-8/2	5-8/2	0	0		K sdqk
676	L 656	SV Q^QDC^CH@F ^S0/	7-182	5-8/2	5-8/2	5-8/2	5-8/2	5-8/2	0	0		K sdqk
677	L 7/6	SV Q^QDC^GHOCH@^0^S0/	02-818	02-818	02-818	02-818	02-818	02-818	0-/1	0		K sdqk
678	L 7/7	SV Q^QDC^GHOCH@^0^S0/	02-706	02-706	02-706	02-706	02-706	02-706	0-/1	0		K sdqk
68/	L 7/8	SV Q^QDC^GHOCH@^0^S0/	02-706	02-706	02-706	02-706	02-706	02-706	0-/1	0		K sdqk
680	L 70/	SV Q^QDC^GHOCH@^0^S0/	02-818	02-818	02-818	02-818	02-818	02-818	0-/1	0		K sdqk
681	L 700	SV Q^QDC^GHOCH@^0^S0/	02-818	02-818	02-818	02-818	02-818	02-818	0-/1	0		K sdqk
682	L 701	SV Q^QDC^GHOCH@^0^S0/	02-706	02-706	02-706	02-706	02-706	02-706	0-/1	0		K sdqk
683	L 702	SV Q^QDC^GHOCH@^0^S0/	02-706	02-706	02-706	02-706	02-706	02-706	0-/1	0		K sdqk
684	L 703	SV Q^QDC^GHOCH@^0^S0/	02-818	02-818	02-818	02-818	02-818	02-818	0-/1	0		K sdqk
685	L 0135	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
686	L 0136	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
687	L 0137	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
688	L 0138	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7//	L 014/	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/0	L 0140	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/1	L 0141	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/2	L 0142	SV Q^QDC^GHOCH@^1^S1	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/3	L 0083	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/4	L 0084	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/5	L 0085	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/6	L 0086	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/7	L 0087	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
7/8	L 0088	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
70/	L 01//	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
700	L 01/0	SV Q^QDC^GHOCH@^1^S2	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
701	L 0031	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
702	L 0032	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
703	L 0033	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
704	L 0034	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
705	L 0035	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
706	L 0036	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
707	L 0037	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
708	L 0038	SV Q^QDC^GHOCH@^1^S3	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
71/	L 0/8/	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
710	L 0/80	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
711	L 0/81	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
712	L 0/82	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
713	L 0/83	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
714	L 0/84	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk
715	L 0/85	SV Q^QDC^GHOCH@^1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
716	L 0/86	SV Q^QDC^GHOCH@1^S4	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
717	L 0/27	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
718	L 0/28	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
72/	L 0/3/	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
720	L 0/30	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
721	L 0/31	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
722	L 0/32	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
723	L 0/33	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
724	L 0/34	SV Q^QDC^GHOCH@1^S5	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
725	L 875	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
726	L 876	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
727	L 877	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
728	L 878	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
73/	L 88/	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
730	L 880	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
731	L 881	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
732	L 882	SV Q^QDC^GHOCH@1^S6	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
733	L 823	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
734	L 824	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
735	L 825	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
736	L 826	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
737	L 827	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
738	L 828	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
74/	L 83/	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
740	L 830	SV Q^QDC^GHOCH@1^S7	01-03	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
741	L 704	SV Q^QDC^GHOCH@2^S0/	04-456	04-456	04-456	04-456	04-456	04-456	0-/1	0		K sdq k
742	L 705	SV Q^QDC^GHOCH@2^S0/	04-255	04-255	04-255	04-255	04-255	04-255	0-/1	0		K sdq k
743	L 706	SV Q^QDC^GHOCH@2^S0/	04-255	04-255	04-255	04-255	04-255	04-255	0-/1	0		K sdq k
744	L 707	SV Q^QDC^GHOCH@2^S0/	04-456	04-456	04-456	04-456	04-456	04-456	0-/1	0		K sdq k
745	L 708	SV Q^QDC^GHOCH@2^S0/	04-456	04-456	04-456	04-456	04-456	04-456	0-/1	0		K sdq k
746	L 71/	SV Q^QDC^GHOCH@2^S0/	04-255	04-255	04-255	04-255	04-255	04-255	0-/1	0		K sdq k
747	L 710	SV Q^QDC^GHOCH@2^S0/	04-255	04-255	04-255	04-255	04-255	04-255	0-/1	0		K sdq k
748	L 711	SV Q^QDC^GHOCH@2^S0/	04-456	04-456	04-456	04-456	04-456	04-456	0-/1	0		K sdq k
75/	L 0127	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
750	L 0128	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
751	L 013/	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
752	L 0130	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
753	L 0131	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
754	L 0132	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
755	L 0133	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
756	L 0134	SV Q^QDC^GHOCH@^S1	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
757	L 0075	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
758	L 0076	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
76/	L 0077	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
760	L 0078	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
761	L 008/	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
762	L 0080	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
763	L 0081	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
764	L 0082	SV Q^QDC^GHOCH@^S2	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
765	L 0023	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
766	L 0024	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
767	L 0025	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfisgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
768	L 0026	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
77/	L 0027	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
770	L 0028	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
771	L 003/	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
772	L 0030	SV Q^QDC^GHOCH@^S3	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
773	L 0/71	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
774	L 0/72	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
775	L 0/73	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
776	L 0/74	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
777	L 0/75	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
778	L 0/76	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
78/	L 0/77	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
780	L 0/78	SV Q^QDC^GHOCH@^S4	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
781	L 0/2/	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
782	L 0/20	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
783	L 0/21	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
784	L 0/22	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
785	L 0/23	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
786	L 0/24	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
787	L 0/25	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
788	L 0/26	SV Q^QDC^GHOCH@^S5	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8//	L 867	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/0	L 868	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/1	L 87/	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/2	L 870	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/3	L 871	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/4	L 872	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/5	L 873	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/6	L 874	SV Q^QDC^GHOCH@^S6	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/7	L 815	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
8/8	L 816	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
80/	L 817	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
800	L 818	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
801	L 82/	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
802	L 820	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
803	L 821	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
804	L 822	SV Q^QDC^GHOCH@^S7	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
805	L 763	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
806	L 764	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
807	L 765	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
808	L 766	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
81/	L 767	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
810	L 768	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
811	L 77/	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
812	L 770	SV Q^QDC^GHOCH@^S8	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0/-/20	0-/3	0		K sdq k
813	L 688	SV Q^QDC^GHO^0^S0/	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
814	L 7//	SV Q^QDC^GHO^0^S0/	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
815	L 7/0	SV Q^QDC^GHO^0^S0/	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
816	L 7/5	SV Q^QDC^GHO^0^S0/	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
817	L 0123	SV Q^QDC^GHO^1^S1	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
818	L 0124	SV Q^QDC^GHO^1^S1	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
82/	L 0125	SV Q^QDC^GHO^1^S1	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
820	L 0126	SV Q^QDC^GH@^1^S1	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
821	L 0071	SV Q^QDC^GH@^1^S2	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
822	L 0072	SV Q^QDC^GH@^1^S2	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
823	L 0073	SV Q^QDC^GH@^1^S2	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
824	L 0074	SV Q^QDC^GH@^1^S2	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
825	L 002/	SV Q^QDC^GH@^1^S3	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
826	L 0020	SV Q^QDC^GH@^1^S3	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
827	L 0021	SV Q^QDC^GH@^1^S3	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
828	L 0022	SV Q^QDC^GH@^1^S3	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
83/	L 0/67	SV Q^QDC^GH@^1^S4	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
830	L 0/68	SV Q^QDC^GH@^1^S4	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
831	L 0/7/	SV Q^QDC^GH@^1^S4	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
832	L 0/70	SV Q^QDC^GH@^1^S4	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
833	L 0/15	SV Q^QDC^GH@^1^S5	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
834	L 0/16	SV Q^QDC^GH@^1^S5	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
835	L 0/17	SV Q^QDC^GH@^1^S5	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
836	L 0/18	SV Q^QDC^GH@^1^S5	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
837	L 863	SV Q^QDC^GH@^1^S6	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
838	L 864	SV Q^QDC^GH@^1^S6	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
84/	L 865	SV Q^QDC^GH@^1^S6	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
840	L 866	SV Q^QDC^GH@^1^S6	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
841	L 811	SV Q^QDC^GH@^1^S7	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
842	L 812	SV Q^QDC^GH@^1^S7	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
843	L 813	SV Q^QDC^GH@^1^S7	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
844	L 814	SV Q^QDC^GH@^1^S7	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
845	L 76/	SV Q^QDC^GH@^1^S8	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
846	L 760	SV Q^QDC^GH@^1^S8	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
847	L 761	SV Q^QDC^GH@^1^S8	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
848	L 762	SV Q^QDC^GH@^1^S8	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
85/	L 7/1	SV Q^QDC^GH@^2^S0/	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
850	L 7/2	SV Q^QDC^GH@^2^S0/	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
851	L 7/3	SV Q^QDC^GH@^2^S0/	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
852	L 7/4	SV Q^QDC^GH@^2^S0/	04-681	04-681	04-681	04-681	04-681	04-681	0-/1	0		K sdq k
853	L 012/	SV Q^QDC^GH@^S1	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
854	L 0120	SV Q^QDC^GH@^S1	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
855	L 0121	SV Q^QDC^GH@^S1	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
856	L 0122	SV Q^QDC^GH@^S1	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
857	L 0067	SV Q^QDC^GH@^S2	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
858	L 0068	SV Q^QDC^GH@^S2	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
86/	L 007/	SV Q^QDC^GH@^S2	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
860	L 0070	SV Q^QDC^GH@^S2	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
861	L 0015	SV Q^QDC^GH@^S3	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
862	L 0016	SV Q^QDC^GH@^S3	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
863	L 0017	SV Q^QDC^GH@^S3	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
864	L 0018	SV Q^QDC^GH@^S3	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
865	L 0/63	SV Q^QDC^GH@^S4	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
866	L 0/64	SV Q^QDC^GH@^S4	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
867	L 0/65	SV Q^QDC^GH@^S4	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
868	L 0/66	SV Q^QDC^GH@^S4	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
87/	L 0/11	SV Q^QDC^GH@^S5	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
870	L 0/12	SV Q^QDC^GH@^S5	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k
871	L 0/13	SV Q^QDC^GH@^S5	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl osno---	Kbnl oans---	K,snop---	Jxx	Jyy	Ba	Etmbs---	
872	L 0/14	SV Q^QDC^GK@D^S5	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
873	L 86/	SV Q^QDC^GK@D^S6	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
874	L 860	SV Q^QDC^GK@D^S6	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
875	L 861	SV Q^QDC^GK@D^S6	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
876	L 862	SV Q^QDC^GK@D^S6	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
877	L 807	SV Q^QDC^GK@D^S7	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
878	L 808	SV Q^QDC^GK@D^S7	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
88/	L 81/	SV Q^QDC^GK@D^S7	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
880	L 810	SV Q^QDC^GK@D^S7	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
881	L 755	SV Q^QDC^GK@D^S8	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
882	L 756	SV Q^QDC^GK@D^S8	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
883	L 757	SV Q^QDC^GK@D^S8	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
884	L 758	SV Q^QDC^GK@D^S8	6-785	6-785	6-785	6-785	6-785	6-785	0-/6	0		K sdqk	
885	L 672	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
886	L 673	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
887	L 674	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
888	L 675	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
0//1	L 676	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
0//0	L 677	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
0//1	L 678	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
0//2	L 68/	SV Q^QDC^GNQY^/^S0/	1-681	1-681	1-681	1-681	1-681	1-681	0	0		K sdqk	
0//3	L 0151	SV Q^QDC^GNQY^1^S0	01-64	01-64	01-64	01-64	01-64	01-64	0-/2	0		K sdqk	
0//4	L 0152	SV Q^QDC^GNQY^1^S0	01-64	01-64	01-64	01-64	01-64	01-64	0-/2	0		K sdqk	
0//5	L 0153	SV Q^QDC^GNQY^1^S0	01-64	01-64	01-64	01-64	01-64	01-64	0-/2	0		K sdqk	
0//6	L 0154	SV Q^QDC^GNQY^1^S0	01-64	01-64	01-64	01-64	01-64	01-64	0-/2	0		K sdqk	
0//7	L 42	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0//8	L 50	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/0/	L 58	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/00	L 66	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/01	L 74	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/02	L 82	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/03	L 0/0	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/04	L 0/8	SV Q^QDC^GNQY^1^S1	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/05	L 015	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/06	L 023	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/07	L 032	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/08	L 040	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/1/	L 05/	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/10	L 057	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/11	L 066	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/12	L 074	SV Q^QDC^GNQY^1^S2	7-264	7-01	7-01	7-01	7-01	7-01	0-/6	0		K sdqk	
0/13	L 1/6	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/14	L 104	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/15	L 113	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/16	L 121	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/17	L 130	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/18	L 138	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/2/	L 147	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/20	L 155	SV Q^QDC^GNQY^1^S3	7-264	7-00	7-00	7-00	7-00	7-00	0-/6	0		K sdqk	
0/21	L 177	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdqk	
0/22	L 185	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdqk	
0/23	L 2/4	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdqk	

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfisg Z--	Kaxx Zes	Kayy Zes	Kbnl o sno--	Kbnl o ans--	K,snop---	Jxx	Jyy	Ba	Et mbs--
0/24	L202	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdq k
0/25	L211	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdq k
0/26	L22/	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdq k
0/27	L228	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdq k
0/28	L236	SV Q^QDC^GNQY^1^S4	7-264	7-/3	7-/3	7-/3	7-/3	7-/3	0-/6	0		K sdq k
0/3/	L258	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/30	L266	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/31	L275	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/32	L283	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/33	L3/2	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/34	L300	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/35	L31/	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/36	L317	SV Q^QDC^GNQY^1^S5	7-264	7-/2	7-/2	7-/2	7-/2	7-/2	0-/6	0		K sdq k
0/37	L34/	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/38	L347	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/4/	L356	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/40	L364	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/41	L373	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/42	L381	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/43	L4/0	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/44	L4/8	SV Q^QDC^GNQY^1^S6	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/45	L420	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/46	L428	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/47	L437	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/48	L445	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/5/	L454	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/50	L462	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/51	L471	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/52	L48/	SV Q^QDC^GNQY^1^S7	7-264	6-84	6-84	6-84	6-84	6-84	0-/6	0		K sdq k
0/53	L501	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/54	L51/	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/55	L518	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/56	L526	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/57	L535	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/58	L543	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/6/	L552	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/60	L560	SV Q^QDC^GNQY^1^S8	7-264	6-83	6-83	6-83	6-83	6-83	0-/6	0		K sdq k
0/61	L582	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/62	L6/2	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/63	L603	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/64	L613	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/65	L624	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/66	L634	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/67	L645	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/68	L655	SV Q^QDC^GNQY^1^S0/	7-264	6-744	6-744	6-744	6-744	6-744	0-/6	0		K sdq k
0/7/	L018/	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/70	L0180	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/71	L0181	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/72	L0182	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/73	L0183	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/74	L0184	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/75	L0185	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---
0/76	L 0186	SV Q^QDC^GNQY^2^S0	0/-264	0/-264	0/-264	0/-264	0/-264	0/-264	0-/3	0		K sdq k
0/77	L 44	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/78	L 52	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/8/	L 60	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/80	L 68	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/81	L 76	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/82	L 84	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/83	L 0/2	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/84	L 000	SV Q^QDC^GNQY^2^S1	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/85	L 017	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/86	L 025	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/87	L 034	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0/88	L 042	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/ /	L 051	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/0	L 06/	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/1	L 068	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/2	L 076	SV Q^QDC^GNQY^2^S2	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/3	L 1/8	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/4	L 106	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/5	L 115	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/6	L 123	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/7	L 132	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
00/8	L 140	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
000/	L 15/	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0000	L 157	SV Q^QDC^GNQY^2^S3	01-452	01-2	01-2	01-2	01-2	01-2	0-/2	0		K sdq k
0001	L 18/	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0002	L 187	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0003	L 2/6	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0004	L 204	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0005	L 213	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0006	L 221	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0007	L 230	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
0008	L 238	SV Q^QDC^GNQY^2^S4	01-452	01-12	01-12	01-12	01-12	01-12	0-/2	0		K sdq k
001/	L 260	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0010	L 268	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0011	L 277	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0012	L 285	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0013	L 3/4	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0014	L 302	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0015	L 311	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0016	L 32/	SV Q^QDC^GNQY^2^S5	01-452	01-11	01-11	01-11	01-11	01-11	0-/2	0		K sdq k
0017	L 341	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0018	L 35/	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
002/	L 358	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0020	L 366	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0021	L 375	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0022	L 383	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0023	L 4/2	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0024	L 400	SV Q^QDC^GNQY^2^S6	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0025	L 422	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0026	L 430	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k
0027	L 44/	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdq k

Hot Rolled Steel Design Parameters (Continued)

	K adk	Rg`od	Kdmfsgz--	Kaxxzes	Kayyzes	Kbnl o sno---	Kbnl o ans---	K,snop---	Jxx	Jyy	Ba	Et mbs---	
0028	L 447	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk	
003/	L 456	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk	
0030	L 464	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk	
0031	L 473	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk	
0032	L 481	SV Q^QDC^GNQY^2^S7	01-452	01-03	01-03	01-03	01-03	01-03	0-/2	0		K sdqk	
0033	L 503	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0034	L 511	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0035	L 520	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0036	L 528	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0037	L 537	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0038	L 545	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
004/	L 554	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0040	L 562	SV Q^QDC^GNQY^2^S8	01-452	01-02	01-02	01-02	01-02	01-02	0-/2	0		K sdqk	
0041	L 584	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0042	L 6/4	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0043	L 605	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0044	L 615	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0045	L 626	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0046	L 636	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0047	L 647	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
0048	L 657	SV Q^QDC^GNQY^2^S0/	00-056	0/-536	0/-536	0/-536	0/-536	0/-536	0-/3	0		K sdqk	
005/	L 0187	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0050	L 0188	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0051	L 02//	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0052	L 02/0	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0053	L 02/1	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0054	L 02/2	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0055	L 02/3	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0056	L 02/4	SV Q^QDC^GNQY^3^S0	3-077	3-077	3-077	3-077	3-077	3-077	0	0		K sdqk	
0057	L 02/5	SV Q^QDC^GNQY^3^S0	7-264	7-264	7-264	7-264	7-264	7-264	0	0		K sdqk	
0058	L 02/6	SV Q^QDC^GNQY^3^S0	7-264	7-264	7-264	7-264	7-264	7-264	0	0		K sdqk	
006/	L 02/7	SV Q^QDC^GNQY^3^S0	7-264	7-264	7-264	7-264	7-264	7-264	0	0		K sdqk	
0060	L 02/8	SV Q^QDC^GNQY^3^S0	7-264	7-264	7-264	7-264	7-264	7-264	0	0		K sdqk	
0061	L 586	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0062	L 6/6	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0063	L 607	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0064	L 617	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0065	L 628	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0066	L 638	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0067	L 65/	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
0068	L 66/	SV Q^QDC^GNQY^3^S0/	02-847	02-327	02-327	02-327	02-327	02-327	0-/1	0		K sdqk	
007/	L 05	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0070	L 08	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0071	L 12	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0072	L 15	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0073	L 2/	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0074	L 22	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0075	L 26	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0076	L 3/	SV Q^QDC^GNQY^S0	7-264	7-02	7-02	7-02	7-02	7-02	0	0		K sdqk	
0077	L 41	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K sdqk	
0078	L 5/	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K sdqk	
008/	L 57	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K sdqk	

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmf sgZ--	KaxxZes\	KayyZes\	Kbnl o sno--	Kbnl o ans--	K,snqp---	Jxx	Jyy	Ba	Etmbs--
0080	L 65	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0081	L 73	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0082	L 81	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0083	L 0//	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0084	L 0/7	SV Q^QDC^GNQY^S1	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0085	L 014	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0086	L 022	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0087	L 031	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
0088	L 04/	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
01//	L 048	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
01/0	L 056	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
01/1	L 065	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
01/2	L 073	SV Q^QDC^GNQY^S2	3-077	2-82	2-82	2-82	2-82	2-82	0	0		K`sdqk
01/3	L 1/5	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
01/4	L 103	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
01/5	L 112	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
01/6	L 120	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
01/7	L 13/	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
01/8	L 137	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
010/	L 146	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
0100	L 154	SV Q^QDC^GNQY^S3	3-077	2-81	2-81	2-81	2-81	2-81	0	0		K`sdqk
0101	L 176	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0102	L 184	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0103	L 2/3	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0104	L 201	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0105	L 210	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0106	L 218	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0107	L 227	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
0108	L 235	SV Q^QDC^GNQY^S4	3-077	2-74	2-74	2-74	2-74	2-74	0	0		K`sdqk
011/	L 257	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0110	L 265	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0111	L 274	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0112	L 282	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0113	L 3/1	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0114	L 30/	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0115	L 308	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0116	L 316	SV Q^QDC^GNQY^S5	3-077	2-73	2-73	2-73	2-73	2-73	0	0		K`sdqk
0117	L 338	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0118	L 346	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
012/	L 355	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0120	L 363	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0121	L 372	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0122	L 380	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0123	L 4//	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0124	L 4/7	SV Q^QDC^GNQY^S6	3-077	2-66	2-66	2-66	2-66	2-66	0	0		K`sdqk
0125	L 42/	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
0126	L 427	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
0127	L 436	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
0128	L 444	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
013/	L 453	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
0130	L 461	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk
0131	L 470	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqk

Hot Rolled Steel Design Parameters (Continued)

	K`adk	Rg`od	Kdmfisgz--	Kaxxzes	Kayyzes	Kbnlosno--Kbnlo ans--K,snqp---			Jxx	Jyy	Ba	Etmbs--
0132	L478	SV Q^QDC^GNQY^S7	3-077	2-65	2-65	2-65	2-65	2-65	0	0		K`sdqjk
0133	L500	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0134	L508	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0135	L517	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0136	L525	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0137	L534	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0138	L542	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
014/	L551	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0140	L56/	SV Q^QDC^GNQY^S8	3-077	2-64	2-64	2-64	2-64	2-64	0	0		K`sdqjk
0141	L581	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0142	L6/1	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0143	L602	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0144	L612	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0145	L623	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0146	L633	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0147	L644	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
0148	L654	SV Q^QDC^GNQY^S0/	4-472	4-/52	4-/52	4-/52	4-/52	4-/52	0	0		K`sdqjk
015/	L4	SV Q^SNO^FHQS^S0	14-4	01-4	01-4	01-4	01-4	01-4	0-00	0		K`sdqjk
0150	L5	SV Q^SNO^FHQS^S0	14-4	01-4	01-4	01-4	01-4	01-4	0-00	0		K`sdqjk
0151	L6	SV Q^SNO^FHQS^S0	14-4	01-4	01-4	01-4	01-4	01-4	0-00	0		K`sdqjk
0152	L7	SV Q^SNO^FHQS^S0	14-4	01-4	01-4	01-4	01-4	01-4	0-00	0		K`sdqjk

Member Advanced Data

	K`adk	HQdkd`rd	IQdkd`rd	HNeerdszfm\	INeerdszfm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@m\kxrhr ---		Hm\bshudr	Rdhrlhb--
0	L0163	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
1	L0164	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
2	L0165	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
3	L0166	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
4	L0167	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
5	L0168	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
6	L017/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
7	L0170	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
8	L0171	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
0/	L0172	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
00	L0173	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
01	L0174	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
02	L0175	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
03	L0176	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
04	L0177	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
05	L0178	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
06	L04	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
07	L07	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
08	L11	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
1/	L14	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
10	L18	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
11	L21	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
12	L25	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
13	L28	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkrcd	Mnmd
14	L40						Xdr	))M@))		Dwbkrcd	Mnmd
15	L48						Xdr	))M@))		Dwbkrcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I Neerdsm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrl hb---
16	L 56						Xdr	))M@))	Dwbkcd	Mnmd
17	L 64						Xdr	))M@))	Dwbkcd	Mnmd
18	L 72						Xdr	))M@))	Dwbkcd	Mnmd
2/	L 80						Xdr	))M@))	Dwbkcd	Mnmd
20	L 88						Xdr	))M@))	Dwbkcd	Mnmd
21	L 0/6						Xdr	))M@))	Dwbkcd	Mnmd
22	L 013						Xdr	))M@))	Dwbkcd	Mnmd
23	L 021						Xdr	))M@))	Dwbkcd	Mnmd
24	L 030						Xdr	))M@))	Dwbkcd	Mnmd
25	L 038						Xdr	))M@))	Dwbkcd	Mnmd
26	L 047						Xdr	))M@))	Dwbkcd	Mnmd
27	L 055						Xdr	))M@))	Dwbkcd	Mnmd
28	L 064						Xdr	))M@))	Dwbkcd	Mnmd
3/	L 072						Xdr	))M@))	Dwbkcd	Mnmd
30	L 1/4						Xdr	))M@))	Dwbkcd	Mnmd
31	L 102						Xdr	))M@))	Dwbkcd	Mnmd
32	L 111						Xdr	))M@))	Dwbkcd	Mnmd
33	L 12/						Xdr	))M@))	Dwbkcd	Mnmd
34	L 128						Xdr	))M@))	Dwbkcd	Mnmd
35	L 136						Xdr	))M@))	Dwbkcd	Mnmd
36	L 145						Xdr	))M@))	Dwbkcd	Mnmd
37	L 153						Xdr	))M@))	Dwbkcd	Mnmd
38	L 175						Xdr	))M@))	Dwbkcd	Mnmd
4/	L 183						Xdr	))M@))	Dwbkcd	Mnmd
40	L 2/2						Xdr	))M@))	Dwbkcd	Mnmd
41	L 200						Xdr	))M@))	Dwbkcd	Mnmd
42	L 21/						Xdr	))M@))	Dwbkcd	Mnmd
43	L 217						Xdr	))M@))	Dwbkcd	Mnmd
44	L 226						Xdr	))M@))	Dwbkcd	Mnmd
45	L 234						Xdr	))M@))	Dwbkcd	Mnmd
46	L 256						Xdr	))M@))	Dwbkcd	Mnmd
47	L 264						Xdr	))M@))	Dwbkcd	Mnmd
48	L 273						Xdr	))M@))	Dwbkcd	Mnmd
5/	L 281						Xdr	))M@))	Dwbkcd	Mnmd
50	L 3/0						Xdr	))M@))	Dwbkcd	Mnmd
51	L 3/8						Xdr	))M@))	Dwbkcd	Mnmd
52	L 307						Xdr	))M@))	Dwbkcd	Mnmd
53	L 315						Xdr	))M@))	Dwbkcd	Mnmd
54	L 337						Xdr	))M@))	Dwbkcd	Mnmd
55	L 345						Xdr	))M@))	Dwbkcd	Mnmd
56	L 354						Xdr	))M@))	Dwbkcd	Mnmd
57	L 362						Xdr	))M@))	Dwbkcd	Mnmd
58	L 371						Xdr	))M@))	Dwbkcd	Mnmd
6/	L 38/						Xdr	))M@))	Dwbkcd	Mnmd
60	L 388						Xdr	))M@))	Dwbkcd	Mnmd
61	L 4/6						Xdr	))M@))	Dwbkcd	Mnmd
62	L 418						Xdr	))M@))	Dwbkcd	Mnmd
63	L 426						Xdr	))M@))	Dwbkcd	Mnmd
64	L 435						Xdr	))M@))	Dwbkcd	Mnmd
65	L 443						Xdr	))M@))	Dwbkcd	Mnmd
66	L 452						Xdr	))M@))	Dwbkcd	Mnmd
67	L 460						Xdr	))M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K`adk	HQdkd`rd	lQdkd`rd	HNeerdszm\	lNeerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmhbshud	Rdhrlhb---
68	L 47/						Xdr	)) M@))		Dwbkcd	Mnmd
7/	L 477						Xdr	)) M@))		Dwbkcd	Mnmd
70	L 50/						Xdr	)) M@))		Dwbkcd	Mnmd
71	L 507						Xdr	)) M@))		Dwbkcd	Mnmd
72	L 516						Xdr	)) M@))		Dwbkcd	Mnmd
73	L 524						Xdr	)) M@))		Dwbkcd	Mnmd
74	L 533						Xdr	)) M@))		Dwbkcd	Mnmd
75	L 541						Xdr	)) M@))		Dwbkcd	Mnmd
76	L 550						Xdr	)) M@))		Dwbkcd	Mnmd
77	L 558						Xdr	)) M@))		Dwbkcd	Mnmd
78	L 580						Xdr	)) M@))		Dwbkcd	Mnmd
8/	L 6/0						Xdr	)) M@))		Dwbkcd	Mnmd
80	L 601						Xdr	)) M@))		Dwbkcd	Mnmd
81	L 611						Xdr	)) M@))		Dwbkcd	Mnmd
82	L 622						Xdr	)) M@))		Dwbkcd	Mnmd
83	L 632						Xdr	)) M@))		Dwbkcd	Mnmd
84	L 643						Xdr	)) M@))		Dwbkcd	Mnmd
85	L 653						Xdr	)) M@))		Dwbkcd	Mnmd
86	L 016/						Xdr				Mnmd
87	L 0160						Xdr				Mnmd
88	L 0161						Xdr				Mnmd
0//	L 0162						Xdr				Mnmd
0/0	L 03						Xdr			Dwbkcd	Mnmd
0/1	L 10						Xdr			Dwbkcd	Mnmd
0/2	L 17						Xdr			Dwbkcd	Mnmd
0/3	L 24						Xdr			Dwbkcd	Mnmd
0/4	L 012						Xdr			Dwbkcd	Mnmd
0/5	L 03/						Xdr			Dwbkcd	Mnmd
0/6	L 046						Xdr			Dwbkcd	Mnmd
0/7	L 063						Xdr			Dwbkcd	Mnmd
0/8	L 1/3						Xdr			Dwbkcd	Mnmd
00/	L 110						Xdr			Dwbkcd	Mnmd
000	L 127						Xdr			Dwbkcd	Mnmd
001	L 144						Xdr			Dwbkcd	Mnmd
002	L 174						Xdr			Dwbkcd	Mnmd
003	L 2/1						Xdr			Dwbkcd	Mnmd
004	L 208						Xdr			Dwbkcd	Mnmd
005	L 225						Xdr			Dwbkcd	Mnmd
006	L 255						Xdr			Dwbkcd	Mnmd
007	L 272						Xdr			Dwbkcd	Mnmd
008	L 3//						Xdr			Dwbkcd	Mnmd
01/	L 306						Xdr			Dwbkcd	Mnmd
010	L 336						Xdr			Dwbkcd	Mnmd
011	L 353						Xdr			Dwbkcd	Mnmd
012	L 370						Xdr			Dwbkcd	Mnmd
013	L 387						Xdr			Dwbkcd	Mnmd
014	L 417						Xdr			Dwbkcd	Mnmd
015	L 434						Xdr			Dwbkcd	Mnmd
016	L 451						Xdr			Dwbkcd	Mnmd
017	L 468						Xdr			Dwbkcd	Mnmd
018	L 5/8						Xdr			Dwbkcd	Mnmd
02/	L 515						Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdszm\	I Neerdszm\	S.B Nmkx	Ogxrhb`k CdekQ`s--@mkxrhr ---			Hmbshud	Rdhrlhb---
020	L 532						Xdr			Dwbkcd	Mnmd
021	L 55/						Xdr			Dwbkcd	Mnmd
022	L 58/						Xdr			Dwbkcd	Mnmd
023	L 600						Xdr			Dwbkcd	Mnmd
024	L 621						Xdr			Dwbkcd	Mnmd
025	L 642						Xdr			Dwbkcd	Mnmd
026	L 0110	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
027	L 0111	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
028	L 0112	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
03/	L 0113	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
030	L 0114	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
031	L 0115	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
032	L 0058	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
033	L 006/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
034	L 0060	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
035	L 0061	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
036	L 0062	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
037	L 0063	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
038	L 0006	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
04/	L 0007	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
040	L 0008	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
041	L 001/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
042	L 0010	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
043	L 0011	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
044	L 0/54	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
045	L 0/55	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
046	L 0/56	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
047	L 0/57	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
048	L 0/58	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
05/	L 0/6/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
050	L 0/02	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
051	L 0/03	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
052	L 0/04	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
053	L 0/05	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
054	L 0/06	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
055	L 0/07	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
056	L 850	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
057	L 851	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
058	L 852	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
06/	L 853	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
060	L 854	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
061	L 855	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
062	L 8/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
063	L 80/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
064	L 800	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
065	L 801	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
066	L 802	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
067	L 803	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
068	L 742	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
07/	L 743	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
070	L 744	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
071	L 745	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K`adk	HQdkd`rd	lQdkd`rd	HNeerdsZm\	lNeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmhbshud	RdhrIhb---
072	L746	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
073	L747	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
074	L0147	AdmOHM	AdmOHM			Sdmrlmm---	Xdr			Mnmd
075	L0148	AdmOHM	AdmOHM			Sdmrlmm---	Xdr			Mnmd
076	L015/	AdmOHM	AdmOHM			Sdmrlmm---	Xdr			Mnmd
077	L0150	AdmOHM	AdmOHM			Sdmrlmm---	Xdr			Mnmd
078	L01/5	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
08/	L01/6	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
080	L01/7	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
081	L0043	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
082	L0044	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
083	L0045	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
084	L00/1	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
085	L00/2	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
086	L00/3	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
087	L0/4/	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
088	L0/40	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1//	L0/41	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/0	L887	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/1	L888	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/2	L0///	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/3	L835	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/4	L836	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/5	L837	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/6	L783	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/7	L784	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
1/8	L785	AdmOHM	AdmOHM			Sdmrlmm---	Xdr		Dwbkrcd	Mnmd
10/	L716	AdmOHM	AdmOHM				Xdr		Hmhbshud	Mnmd
100	L717	AdmOHM	AdmOHM				Xdr		Hmhbshud	Mnmd
101	L718	AdmOHM	AdmOHM				Xdr		Hmhbshud	Mnmd
102	L734	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
103	L735	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
104	L736	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
105	L737	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
106	L738	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
107	L74/	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
108	L740	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
11/	L741	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
110	L748	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
111	L75/	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
112	L750	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
113	L751	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
114	L752	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
115	L753	AdmOHM	AdmOHM				Xdr	))M@))	Hmhbshud	Mnmd
116	L754	AdmOHM	AdmOHM				Xdr	))M@))		Mnmd
117	L0116	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
118	L0117	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
12/	L0118	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
120	L0064	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
121	L0065	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
122	L0066	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd
123	L0012	AdmOHM	AdmOHM				Xdr		Dwbkrcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k CdekQ`s--@mkxrhr ---			Hmbshud	Rdhrl hb--
124	L 0013	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
125	L 0014	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
126	L 0/60	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
127	L 0/61	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
128	L 0/62	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
13/	L 0/08	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
130	L 0/1/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
131	L 0/10	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
132	L 856	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
133	L 857	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
134	L 858	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
135	L 804	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
136	L 805	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
137	L 806	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
138	L 72/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
14/	L 720	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
140	L 721	AdmOHM	AdmOHM				Xdr			Hmbshud	Mnmd
141	L 0143	AdmOHM	AdmOHM				Xdr				Mnmd
142	L 0144	AdmOHM	AdmOHM				Xdr				Mnmd
143	L 0145	AdmOHM	AdmOHM				Xdr				Mnmd
144	L 0146	AdmOHM	AdmOHM				Xdr				Mnmd
145	L 01/1	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
146	L 01/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
147	L 01/3	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
148	L 01/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
15/	L 004/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
150	L 0040	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
151	L 0041	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
152	L 0042	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
153	L 0/87	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
154	L 0/88	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
155	L 00//	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
156	L 00/0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
157	L 0/35	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
158	L 0/36	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
16/	L 0/37	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
160	L 0/38	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
161	L 883	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
162	L 884	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
163	L 885	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
164	L 886	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
165	L 831	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
166	L 832	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
167	L 833	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
168	L 834	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
17/	L 78/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
170	L 780	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
171	L 781	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
172	L 782	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
173	L 712	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
174	L 713	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
175	L 714	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I NeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmhbshud	Rdhrlhb---
176	L715	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
177	L8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
178	L0/	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
18/	L00	AdmOHM	AdmOHM				Xdr	Cde`tks		Dwbkcd	Mnmd
180	L01	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
181	L02	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
182	L31	AdmOHM	AdmOHM				Xdr				Mnmd
183	L32	AdmOHM	AdmOHM				Xdr				Mnmd
184	L33	AdmOHM	AdmOHM				Xdr				Mnmd
185	L34	AdmOHM	AdmOHM				Xdr				Mnmd
186	L35	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
187	L004	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
188	L005	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
2//	L006	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
2/0	L007	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
2/1	L080	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
2/2	L081	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
2/3	L082	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
2/4	L083	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
2/5	L084	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
2/6	L085	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
2/7	L086	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
2/8	L087	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
20/	L088	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
200	L161	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
201	L162	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
202	L163	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
203	L164	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
204	L165	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
205	L166	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
206	L167	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
207	L168	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
208	L17/	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
21/	L242	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
210	L243	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
211	L244	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
212	L245	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
213	L246	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
214	L247	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
215	L248	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
216	L25/	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
217	L250	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
218	L323	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
22/	L324	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
220	L325	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
221	L326	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
222	L327	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
223	L328	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
224	L33/	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
225	L330	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
226	L331	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
227	L404	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I Neerdsmz\	S.B Nmkx	Ogxrhb`k CdekQ`s--@mkxrhr ---			Hmhbshud	Rdhrl hb---
228	L 405	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
23/	L 406	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
230	L 407	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
231	L 408	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
232	L 41/	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
233	L 410	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
234	L 411	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
235	L 412	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
236	L 485	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
237	L 486	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
238	L 487	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
24/	L 488	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
240	L 5//	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
241	L 5/0	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
242	L 5/1	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
243	L 5/2	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
244	L 5/3	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
245	L 566	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
246	L 567	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
247	L 568	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
248	L 57/	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
25/	L 570	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
250	L 571	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
251	L 572	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
252	L 573	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
253	L 574	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
254	L 663	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
255	L 664	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
256	L 665	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
257	L 666	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
258	L 667	AdmOHM	AdmOHM				Xdr			Hmhbshud	Mnmd
26/	L 668	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
260	L 67/	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
261	L 670	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
262	L 671	WNNNWW	AdmOHM				Xdr			Hmhbshud	Mnmd
263	L 01/8	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
264	L 010/	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
265	L 0100	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
266	L 0101	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
267	L 0102	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
268	L 0103	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
27/	L 0104	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
270	L 0105	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
271	L 0106	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
272	L 0107	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
273	L 0108	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
274	L 011/	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
275	L 0046	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
276	L 0047	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
277	L 0048	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
278	L 005/	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd
28/	L 0050	AdmOHM	AdmOHM				Xdr			Dwbkt cd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrlhb---
280	L 0051	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
281	L 0052	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
282	L 0053	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
283	L 0054	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
284	L 0055	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
285	L 0056	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
286	L 0057	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
287	L 00/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
288	L 00/5	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3//	L 00/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/0	L 00/7	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/1	L 00/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/2	L 000/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/3	L 0000	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/4	L 0001	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/5	L 0002	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/6	L 0003	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/7	L 0004	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
3/8	L 0005	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
30/	L 0/42	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
300	L 0/43	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
301	L 0/44	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
302	L 0/45	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
303	L 0/46	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
304	L 0/47	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
305	L 0/48	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
306	L 0/5/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
307	L 0/50	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
308	L 0/51	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
31/	L 0/52	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
310	L 0/53	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
311	L 0//0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
312	L 0//1	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
313	L 0//2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
314	L 0//3	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
315	L 0//4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
316	L 0//5	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
317	L 0//6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
318	L 0//7	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
32/	L 0//8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
320	L 0/0/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
321	L 0/00	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
322	L 0/01	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
323	L 838	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
324	L 84/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
325	L 840	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
326	L 841	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
327	L 842	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
328	L 843	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
33/	L 844	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
330	L 845	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
331	L 846	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrlhb---
332	L 847	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
333	L 848	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
334	L 85/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
335	L 786	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
336	L 787	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
337	L 788	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
338	L 8//	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
34/	L 8/0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
340	L 8/1	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
341	L 8/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
342	L 8/3	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
343	L 8/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
344	L 8/5	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
345	L 8/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
346	L 8/7	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
347	L 722	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
348	L 723	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
35/	L 724	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
350	L 725	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
351	L 726	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
352	L 727	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
353	L 728	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
354	L 73/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
355	L 730	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
356	L 731	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
357	L 732	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
358	L 733	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
36/	L 0155	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
360	L 0156	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
361	L 0157	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
362	L 0158	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
363	L 0						Xdr	)) M@))		Dwbkcd	Mnmd
364	L 1						Xdr	)) M@))		Dwbkcd	Mnmd
365	L 2						Xdr	)) M@))		Dwbkcd	Mnmd
366	L 3						Xdr	)) M@))		Dwbkcd	Mnmd
367	L 36						Xdr	)) M@))			Mnmd
368	L 37						Xdr	)) M@))			Mnmd
37/	L 38						Xdr	)) M@))			Mnmd
370	L 4/						Xdr	)) M@))			Mnmd
371	L 008						Xdr	)) M@))			Mnmd
372	L 01/						Xdr	)) M@))			Mnmd
373	L 010						Xdr	)) M@))			Mnmd
374	L 011						Xdr	)) M@))			Mnmd
375	L 1//						Xdr	)) M@))			Mnmd
376	L 1/0						Xdr	)) M@))			Mnmd
377	L 1/1						Xdr	)) M@))			Mnmd
378	L 1/2						Xdr	)) M@))			Mnmd
38/	L 170						Xdr	)) M@))			Mnmd
380	L 171						Xdr	)) M@))			Mnmd
381	L 172						Xdr	)) M@))			Mnmd
382	L 173						Xdr	)) M@))			Mnmd
383	L 251						Xdr	)) M@))			Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I Neerdsm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrlhb---
384	L 252						Xdr	))M@))		Mnmd
385	L 253						Xdr	))M@))		Mnmd
386	L 254						Xdr	))M@))		Mnmd
387	L 332						Xdr	))M@))		Mnmd
388	L 333						Xdr	))M@))		Mnmd
4//	L 334						Xdr	))M@))		Mnmd
4/0	L 335						Xdr	))M@))		Mnmd
4/1	L 413						Xdr	))M@))		Mnmd
4/2	L 414						Xdr	))M@))		Mnmd
4/3	L 415						Xdr	))M@))		Mnmd
4/4	L 416						Xdr	))M@))		Mnmd
4/5	L 5/4						Xdr	))M@))		Mnmd
4/6	L 5/5						Xdr	))M@))		Mnmd
4/7	L 5/6						Xdr	))M@))		Mnmd
4/8	L 5/7						Xdr	))M@))		Mnmd
40/	L 575						Xdr	))M@))		Mnmd
400	L 576						Xdr	))M@))		Mnmd
401	L 577						Xdr	))M@))		Mnmd
402	L 578						Xdr	))M@))		Mnmd
403	L 771						Xdr	))M@))	Dwbkcd	Mnmd
404	L 772						Xdr	))M@))	Dwbkcd	Mnmd
405	L 773						Xdr	))M@))	Dwbkcd	Mnmd
406	L 774						Xdr	))M@))	Dwbkcd	Mnmd
407	L 775						Xdr	))M@))	Dwbkcd	Mnmd
408	L 776						Xdr	))M@))	Dwbkcd	Mnmd
41/	L 777						Xdr	))M@))	Dwbkcd	Mnmd
410	L 778						Xdr	))M@))	Dwbkcd	Mnmd
411	L 680						Xdr	))M@))	Dwbkcd	Mnmd
412	L 681						Xdr	))M@))	Dwbkcd	Mnmd
413	L 682						Xdr	))M@))	Dwbkcd	Mnmd
414	L 683						Xdr	))M@))	Dwbkcd	Mnmd
415	L 684						Xdr	))M@))	Dwbkcd	Mnmd
416	L 685						Xdr	))M@))	Dwbkcd	Mnmd
417	L 686						Xdr	))M@))	Dwbkcd	Mnmd
418	L 687						Xdr	))M@))	Dwbkcd	Mnmd
42/	L 45	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
420	L 53	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
421	L 61	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
422	L 7/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
423	L 77	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
424	L 85	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
425	L 0/3	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
426	L 001	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
427	L 018	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
428	L 026	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
43/	L 035	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
430	L 043	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
431	L 052	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
432	L 060	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
433	L 07/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
434	L 077	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
435	L 10/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I NeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrlhb---
436	L 107	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
437	L 116	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
438	L 124	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
44/	L 133	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
440	L 141	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
441	L 150	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
442	L 158	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
443	L 180	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
444	L 188	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
445	L 2/7	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
446	L 205	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
447	L 214	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
448	L 222	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
45/	L 231	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
450	L 24/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
451	L 261	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
452	L 27/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
453	L 278	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
454	L 286	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
455	L 3/5	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
456	L 303	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
457	L 312	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
458	L 320	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
46/	L 342	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
460	L 350	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
461	L 36/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
462	L 367	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
463	L 376	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
464	L 384	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
465	L 4/3	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
466	L 401	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
467	L 423	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
468	L 431	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
47/	L 440	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
470	L 448	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
471	L 457	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
472	L 465	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
473	L 474	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
474	L 482	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
475	L 504	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
476	L 512	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
477	L 521	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
478	L 53/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
48/	L 538	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
480	L 546	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
481	L 555	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
482	L 563	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
483	L 585	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
484	L 6/5	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
485	L 606	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
486	L 616	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
487	L 627	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K`adk	HQdkd`rd	lQdkd`rd	HNeerdsZm\	lNeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrlhb---
488	L 637	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5//	L 648	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/0	L 658	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/1	L 46	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/2	L 47	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/3	L 54	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/4	L 55	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/5	L 62	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/6	L 63	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/7	L 70	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
5/8	L 71	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
50/	L 78	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
500	L 8/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
501	L 86	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
502	L 87	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
503	L 0/4	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
504	L 0/5	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
505	L 002	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
506	L 003	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
507	L 02/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
508	L 020	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
51/	L 027	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
510	L 028	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
511	L 036	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
512	L 037	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
513	L 044	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
514	L 045	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
515	L 053	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
516	L 054	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
517	L 061	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
518	L 062	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
52/	L 070	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
520	L 071	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
521	L 078	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
522	L 08/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
523	L 100	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
524	L 101	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
525	L 108	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
526	L 11/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
527	L 117	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
528	L 118	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
53/	L 125	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
530	L 126	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
531	L 134	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
532	L 135	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
533	L 142	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
534	L 143	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
535	L 151	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
536	L 152	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
537	L 16/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
538	L 160	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
54/	L 181	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb--
540	L 182	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
541	L 2//	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
542	L 2/0	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
543	L 2/8	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
544	L 20/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
545	L 206	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
546	L 207	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
547	L 215	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
548	L 216	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
55/	L 223	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
550	L 224	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
551	L 232	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
552	L 233	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
553	L 240	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
554	L 241	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
555	L 262	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
556	L 263	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
557	L 270	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
558	L 271	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
56/	L 28/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
560	L 280	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
561	L 287	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
562	L 288	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
563	L 3/6	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
564	L 3/7	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
565	L 304	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
566	L 305	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
567	L 313	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
568	L 314	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
57/	L 321	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
570	L 322	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
571	L 343	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
572	L 344	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
573	L 351	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
574	L 352	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
575	L 360	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
576	L 361	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
577	L 368	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
578	L 37/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
58/	L 377	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
580	L 378	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
581	L 385	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
582	L 386	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
583	L 4/4	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
584	L 4/5	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
585	L 402	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
586	L 403	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
587	L 424	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
588	L 425	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
6//	L 432	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
6/0	L 433	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
6/1	L 441	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdszm\	I Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrl hb---
6/2	L 442	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/3	L 45/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/4	L 450	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/5	L 458	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/6	L 46/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/7	L 466	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
6/8	L 467	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
60/	L 475	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
600	L 476	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
601	L 483	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
602	L 484	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
603	L 505	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
604	L 506	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
605	L 513	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
606	L 514	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
607	L 522	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
608	L 523	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
61/	L 530	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
610	L 531	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
611	L 54/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
612	L 540	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
613	L 547	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
614	L 548	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
615	L 556	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
616	L 557	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
617	L 564	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
618	L 565	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
62/	L 587	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
620	L 6/7	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
621	L 608	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
622	L 618	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
623	L 63/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
624	L 64/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
625	L 650	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
626	L 660	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
627	L 588	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
628	L 6//	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
63/	L 6/8	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
630	L 60/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
631	L 61/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
632	L 610	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
633	L 62/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
634	L 620	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
635	L 630	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
636	L 631	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
637	L 640	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
638	L 641	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
64/	L 651	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
640	L 652	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
641	L 661	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
642	L 662	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
643	L 06	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdsZm\	l NeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
644	L 1/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
645	L 13	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
646	L 16	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
647	L 20	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
648	L 23	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
65/	L 27	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
650	L 30	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
651	L 43	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
652	L 51	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
653	L 6/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
654	L 67	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
655	L 75	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
656	L 83	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
657	L 0/1	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
658	L 00/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
66/	L 016	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
660	L 024	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
661	L 033	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
662	L 041	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
663	L 050	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
664	L 058	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
665	L 067	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
666	L 075	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
667	L 1/7	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
668	L 105	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
67/	L 114	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
670	L 122	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
671	L 131	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
672	L 14/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
673	L 148	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
674	L 156	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
675	L 178	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
676	L 186	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
677	L 2/5	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
678	L 203	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
68/	L 212	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
680	L 220	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
681	L 23/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
682	L 237	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
683	L 26/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
684	L 267	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
685	L 276	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
686	L 284	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
687	L 3/3	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
688	L 301	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7//	L 310	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/0	L 318	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/1	L 340	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/2	L 348	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/3	L 357	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/4	L 365	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
7/5	L 374	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
7/6	L 382	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
7/7	L 4/1	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
7/8	L 40/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
70/	L 421	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
700	L 43/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
701	L 438	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
702	L 446	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
703	L 455	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
704	L 463	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
705	L 472	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
706	L 480	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
707	L 502	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
708	L 510	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
71/	L 52/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
710	L 527	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
711	L 536	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
712	L 544	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
713	L 553	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
714	L 561	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
715	L 583	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
716	L 6/3	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
717	L 604	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
718	L 614	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
72/	L 625	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
720	L 635	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
721	L 646	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
722	L 656	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
723	L 7/6	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
724	L 7/7	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
725	L 7/8	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
726	L 70/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
727	L 700	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
728	L 701	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
73/	L 702	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
730	L 703	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
731	L 0135	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
732	L 0136	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
733	L 0137	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
734	L 0138	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
735	L 014/	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
736	L 0140	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
737	L 0141	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
738	L 0142	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
74/	L 0083	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
740	L 0084	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
741	L 0085	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
742	L 0086	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
743	L 0087	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
744	L 0088	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
745	L 01//	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
746	L 01/0	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd
747	L 0031	AdmOHM	AdmOHM				Xdr	))M@))		Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I NeerdsZm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrlhb---
748	L0032	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
75/	L0033	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
750	L0034	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
751	L0035	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
752	L0036	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
753	L0037	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
754	L0038	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
755	L0/8/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
756	L0/80	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
757	L0/81	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
758	L0/82	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
76/	L0/83	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
760	L0/84	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
761	L0/85	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
762	L0/86	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
763	L0/27	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
764	L0/28	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
765	L0/3/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
766	L0/30	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
767	L0/31	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
768	L0/32	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
77/	L0/33	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
770	L0/34	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
771	L875	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
772	L876	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
773	L877	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
774	L878	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
775	L88/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
776	L880	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
777	L881	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
778	L882	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
78/	L823	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
780	L824	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
781	L825	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
782	L826	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
783	L827	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
784	L828	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
785	L83/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
786	L830	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
787	L704	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
788	L705	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8//	L706	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/0	L707	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/1	L708	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/2	L71/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/3	L710	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/4	L711	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/5	L0127	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/6	L0128	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/7	L013/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
8/8	L0130	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
80/	L0131	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I Neerdsm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrl hb---
800	L 0132	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
801	L 0133	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
802	L 0134	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
803	L 0075	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
804	L 0076	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
805	L 0077	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
806	L 0078	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
807	L 008/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
808	L 0080	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
81/	L 0081	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
810	L 0082	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
811	L 0023	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
812	L 0024	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
813	L 0025	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
814	L 0026	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
815	L 0027	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
816	L 0028	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
817	L 003/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
818	L 0030	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
82/	L 0/71	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
820	L 0/72	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
821	L 0/73	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
822	L 0/74	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
823	L 0/75	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
824	L 0/76	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
825	L 0/77	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
826	L 0/78	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
827	L 0/2/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
828	L 0/20	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
83/	L 0/21	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
830	L 0/22	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
831	L 0/23	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
832	L 0/24	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
833	L 0/25	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
834	L 0/26	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
835	L 867	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
836	L 868	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
837	L 87/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
838	L 870	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
84/	L 871	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
840	L 872	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
841	L 873	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
842	L 874	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
843	L 815	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
844	L 816	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
845	L 817	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
846	L 818	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
847	L 82/	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
848	L 820	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
85/	L 821	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
850	L 822	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd
851	L 763	AdmOHM	AdmOHM				Xdr	)) M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	I Qdkd`rd	HNeerdsZm\	I Neerdsm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---	Hmbshud	Rdhrl hb---
852	L764	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
853	L765	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
854	L766	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
855	L767	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
856	L768	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
857	L77/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
858	L770	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
86/	L688	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
860	L7//	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
861	L7/0	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
862	L7/5	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
863	L0123	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
864	L0124	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
865	L0125	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
866	L0126	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
867	L0071	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
868	L0072	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
87/	L0073	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
870	L0074	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
871	L002/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
872	L0020	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
873	L0021	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
874	L0022	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
875	L0/67	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
876	L0/68	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
877	L0/7/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
878	L0/70	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
88/	L0/15	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
880	L0/16	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
881	L0/17	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
882	L0/18	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
883	L863	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
884	L864	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
885	L865	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
886	L866	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
887	L811	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
888	L812	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0///	L813	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//0	L814	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//1	L76/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//2	L760	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//3	L761	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//4	L762	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//5	L7/1	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//6	L7/2	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//7	L7/3	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0//8	L7/4	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0/0/	L012/	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0/00	L0120	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0/01	L0121	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0/02	L0122	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd
0/03	L0067	AdmOHM	AdmOHM				Xdr	))M@))	Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
0/04	L 0068	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/05	L 007/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/06	L 0070	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/07	L 0015	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/08	L 0016	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/1/	L 0017	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/10	L 0018	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/11	L 0/63	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/12	L 0/64	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/13	L 0/65	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/14	L 0/66	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/15	L 0/11	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/16	L 0/12	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/17	L 0/13	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/18	L 0/14	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/2/	L 86/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/20	L 860	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/21	L 861	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/22	L 862	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/23	L 807	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/24	L 808	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/25	L 81/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/26	L 810	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/27	L 755	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/28	L 756	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/3/	L 757	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/30	L 758	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/31	L 672	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/32	L 673	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/33	L 674	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/34	L 675	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/35	L 676	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/36	L 677	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/37	L 678	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/38	L 68/	AdmOHM	AdmOHM				Xdr	)) M@))		Dwbkcd	Mnmd
0/4/	L 0151	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/40	L 0152	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/41	L 0153	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/42	L 0154	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/43	L 42	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/44	L 50	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/45	L 58	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/46	L 66	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/47	L 74	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/48	L 82	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/5/	L 0/0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/50	L 0/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/51	L 015	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/52	L 023	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/53	L 032	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/54	L 040	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/55	L 05/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
0/56	L 057	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/57	L 066	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/58	L 074	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/6/	L 1/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/60	L 104	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/61	L 113	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/62	L 121	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/63	L 130	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/64	L 138	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/65	L 147	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/66	L 155	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/67	L 177	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/68	L 185	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/7/	L 2/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/70	L 202	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/71	L 211	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/72	L 22/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/73	L 228	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/74	L 236	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/75	L 258	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/76	L 266	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/77	L 275	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/78	L 283	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/8/	L 3/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/80	L 300	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/81	L 31/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/82	L 317	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/83	L 34/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/84	L 347	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/85	L 356	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/86	L 364	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/87	L 373	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0/88	L 381	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/ /	L 4/0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/0	L 4/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/1	L 420	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/2	L 428	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/3	L 437	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/4	L 445	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/5	L 454	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/6	L 462	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/7	L 471	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
00/8	L 48/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
000/	L 501	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0000	L 51/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0001	L 518	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0002	L 526	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0003	L 535	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0004	L 543	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0005	L 552	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0006	L 560	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0007	L 582	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
0008	L 6/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
001/	L 603	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0010	L 613	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0011	L 624	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0012	L 634	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0013	L 645	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0014	L 655	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0015	L 018/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0016	L 0180	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0017	L 0181	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0018	L 0182	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
002/	L 0183	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0020	L 0184	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0021	L 0185	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0022	L 0186	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0023	L 44	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0024	L 52	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0025	L 60	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0026	L 68	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0027	L 76	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0028	L 84	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
003/	L 0/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0030	L 000	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0031	L 017	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0032	L 025	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0033	L 034	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0034	L 042	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0035	L 051	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0036	L 06/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0037	L 068	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0038	L 076	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
004/	L 1/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0040	L 106	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0041	L 115	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0042	L 123	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0043	L 132	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0044	L 140	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0045	L 15/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0046	L 157	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0047	L 18/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0048	L 187	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
005/	L 2/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0050	L 204	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0051	L 213	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0052	L 221	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0053	L 230	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0054	L 238	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0055	L 260	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0056	L 268	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0057	L 277	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0058	L 285	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
006/	L 3/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
0060	L 302	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0061	L 311	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0062	L 32/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0063	L 341	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0064	L 35/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0065	L 358	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0066	L 366	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0067	L 375	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0068	L 383	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
007/	L 4/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0070	L 400	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0071	L 422	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0072	L 430	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0073	L 44/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0074	L 447	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0075	L 456	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0076	L 464	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0077	L 473	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0078	L 481	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
008/	L 503	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0080	L 511	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0081	L 520	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0082	L 528	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0083	L 537	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0084	L 545	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0085	L 554	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0086	L 562	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0087	L 584	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0088	L 6/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01//	L 605	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/0	L 615	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/1	L 626	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/2	L 636	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/3	L 647	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/4	L 657	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/5	L 0187	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/6	L 0188	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/7	L 02//	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
01/8	L 02/0	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
010/	L 02/1	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0100	L 02/2	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0101	L 02/3	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0102	L 02/4	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0103	L 02/5	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0104	L 02/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0105	L 02/7	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0106	L 02/8	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0107	L 586	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0108	L 6/6	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
011/	L 607	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0110	L 617	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0111	L 628	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdszm\	l Neerdszm\	S.B Nmkx	Ogxrhb`k	CdekQ`s--@mkxrhr ---		Hmbshud	Rdhrl hb---
0112	L 638	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0113	L 65/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0114	L 66/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0115	L 05	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0116	L 08	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0117	L 12	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0118	L 15	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
012/	L 2/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0120	L 22	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0121	L 26	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0122	L 3/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0123	L 41	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0124	L 5/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0125	L 57	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0126	L 65	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0127	L 73	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0128	L 81	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
013/	L 0//	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0130	L 0/7	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0131	L 014	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0132	L 022	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0133	L 031	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0134	L 04/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0135	L 048	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0136	L 056	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0137	L 065	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0138	L 073	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
014/	L 1/5	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0140	L 103	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0141	L 112	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0142	L 120	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0143	L 13/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0144	L 137	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0145	L 146	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0146	L 154	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0147	L 176	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0148	L 184	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
015/	L 2/3	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0150	L 201	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0151	L 210	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0152	L 218	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0153	L 227	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0154	L 235	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0155	L 257	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0156	L 265	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0157	L 274	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0158	L 282	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
016/	L 3/1	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0160	L 30/	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0161	L 308	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0162	L 316	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd
0163	L 338	AdmOHM	AdmOHM				Xdr			Dwbkcd	Mnmd

Member Advanced Data (Continued)

	K adk	HQdkd`rd	l Qdkd`rd	HNeerdsZm\	l NeerdsZm\	S.B Nmkx	Ogxrhb`k CdekQ`s--@m\kxrhr ---			Hm\bshud	Rdhrl hb---
0164	L 346	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0165	L 355	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0166	L 363	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0167	L 372	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0168	L 380	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
017/	L 4//	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0170	L 4/7	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0171	L 42/	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0172	L 427	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0173	L 436	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0174	L 444	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0175	L 453	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0176	L 461	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0177	L 470	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0178	L 478	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
018/	L 500	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0180	L 508	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0181	L 517	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0182	L 525	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0183	L 534	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0184	L 542	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0185	L 551	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0186	L 56/	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0187	L 581	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
0188	L 6/1	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02//	L 602	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/0	L 612	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/1	L 623	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/2	L 633	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/3	L 644	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/4	L 654	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/5	L 4	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/6	L 5	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/7	L 6	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd
02/8	L 7	AdmOHM	AdmOHM				Xdr			Dwbkl cd	Mnmd

Basic Load Cases

	AKB Cdr bqhosmm	B`sdfnqx	WFq`uhsx	X Fq`uhsx	Y Fq`uhsx	Inhms	Onhms	Chrsqhat sdc@qd`'Ld---Rtqèbd'---		
0	Cd`c	Mnmd		,0		3/	362	3/		
1	Mn Hbd V hmc / cdf	Mnmd				3/	020/	01/		
2	Mn Hbd V hmc 34 cdf	Mnmd				7/	0185	05/		
3	Mn Hbd V hmc 8/ cdf	Mnmd				3/	0203	01/		
4	Mn Hbd V hmc 024 cdf	Mnmd				7/	0163	05/		
5	Mn Hbd V hmc 07/ cdf	Mnmd				3/	020/	01/		
6	Mn Hbd V hmc 114 cdf	Mnmd				7/	0185	05/		
7	Mn Hbd V hmc 16/ cdf	Mnmd				3/	0203	01/		
8	Mn Hbd V hmc 204 cdf	Mnmd				7/	0163	05/		
0/	Hbd	Mnmd				3/	365	711		
00	Sdl odq`stqd Cqno	Mnmd						671		
01	Hbd V hmc / cdf	Mnmd				3/	02//	77		

Basic Load Cases (Continued)

	AKB Cdrbdqdshnm	B`sdfnqx	WFq`uhsx	X Fq`uhsx	Y Fq`uhsx	Inhms	Onhms	Chrsqhat sdc@qd`'Ld--Rtqè bd'--		
02	Hbd V hmc 34 cdf	Mnmd				7/	0125	05/		
03	Hbd V hmc 8/ cdf	Mnmd				3/	02/3	01/		
04	Hbd V hmc 024 cdf	Mnmd				7/	01/1	05/		
05	Hbd V hmc 07/ cdf	Mnmd				3/	02//	77		
06	Hbd V hmc 114 cdf	Mnmd				7/	0125	05/		
07	Hbd V hmc 16/ cdf	Mnmd				3/	02/3	01/		
08	Hbd V hmc 204 cdf	Mnmd				7/	01/1	05/		
1/	Rdquhbd V hmc / cdf	Mnmd				3/	0187	001		
10	Rdquhbd V hmc 34 cdf	Mnmd				7/	0125	05/		
11	Rdquhbd V hmc 8/ cdf	Mnmd				3/	0185	01/		
12	Rdquhbd V hmc 024 cdf	Mnmd				7/	0103	05/		
13	Rdquhbd V hmc 07/ cdf	Mnmd				3/	0187	001		
14	Rdquhbd V hmc 114 cdf	Mnmd				7/	0125	05/		
15	Rdquhbd V hmc 16/ cdf	Mnmd				3/	0185	01/		
16	Rdquhbd V hmc 204 cdf	Mnmd				7/	0103	05/		

Load Combinations

	Cdrbdqdshnm	Rn--O--	R--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--
0	Cd`c Nmkx	Xdr	X	0	0-3																		
1	0-1 Cd`c*0-/ V hmc / c--	Xdr	X	0	0-1	1	0																
2	/-8 Cd`c*0-/ V hmc / c--	Xdr	X	0	-8	1	0																
3	0-1 Cd`c*0-/ V hmc 34 --	Xdr	X	0	0-1	2	0																
4	/-8 Cd`c*0-/ V hmc 34 --	Xdr	X	0	-8	2	0																
5	0-1 Cd`c*0-/ V hmc 8/ --	Xdr	X	0	0-1	3	0																
6	/-8 Cd`c*0-/ V hmc 8/ --	Xdr	X	0	-8	3	0																
7	0-1 Cd`c*0-/ V hmc 02--	Xdr	X	0	0-1	4	0																
8	/-8 Cd`c*0-/ V hmc 02--	Xdr	X	0	-8	4	0																
0/	0-1 Cd`c*0-/ V hmc 07--	Xdr	X	0	0-1	5	0																
00	/-8 Cd`c*0-/ V hmc 07--	Xdr	X	0	-8	5	0																
01	0-1 Cd`c*0-/ V hmc 11--	Xdr	X	0	0-1	6	0																
02	/-8 Cd`c*0-/ V hmc 11--	Xdr	X	0	-8	6	0																
03	0-1 Cd`c*0-/ V hmc 16--	Xdr	X	0	0-1	7	0																
04	/-8 Cd`c*0-/ V hmc 16--	Xdr	X	0	-8	7	0																
05	0-1 Cd`c*0-/ V hmc 20--	Xdr	X	0	0-1	8	0																
06	/-8 Cd`c*0-/ V hmc 20--	Xdr	X	0	-8	8	0																
07	0-1 Cd`c*0-/ Hbd*0-/ S--	Xdr		0	0-1	0/	0	00	0														
08	0-1 Cd`c*0-/ V hmc / c--	Xdr		0	0-1	01	0	0/	0	00	0												
1/	0-1 Cd`c*0-/ V hmc 34 --	Xdr		0	0-1	02	0	0/	0	00	0												
10	0-1 Cd`c*0-/ V hmc 8/ --	Xdr		0	0-1	03	0	0/	0	00	0												
11	0-1 Cd`c*0-/ V hmc 02--	Xdr		0	0-1	04	0	0/	0	00	0												
12	0-1 Cd`c*0-/ V hmc 07--	Xdr		0	0-1	05	0	0/	0	00	0												
13	0-1 Cd`c*0-/ V hmc 11--	Xdr		0	0-1	06	0	0/	0	00	0												
14	0-1 Cd`c*0-/ V hmc 16--	Xdr		0	0-1	07	0	0/	0	00	0												
15	0-1 Cd`c*0-/ V hmc 20--	Xdr		0	0-1	08	0	0/	0	00	0												
16	Cd`c*V hmc / cdf, Rdq--	Xdr	X	0	0	1/	0																
17	Cd`c*V hmc 34 cdf, R--	Xdr	X	0	0	10	0																
18	Cd`c*V hmc 8/ cdf, R--	Xdr	X	0	0	11	0																
2/	Cd`c*V hmc 024 cdf, --	Xdr	X	0	0	12	0																
20	Cd`c*V hmc 07/ cdf, --	Xdr	X	0	0	13	0																
21	Cd`c*V hmc 114 cdf, --	Xdr	X	0	0	14	0																

Load Combinations (Continued)

	Cdr bdqosmm	Rn--O--	R--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--	AKB E`b--
22	Cd`c*V hmc 16/ cdf, ---	Xdr	X		0	0	15	0																
23	Cd`c*V hmc 204 cdf, ---	Xdr	X		0	0	16	0																
24	0-/ V hmc / cdf		X		1	0																		
25	0-/ V hmc 34 cdf		X		2	0																		
26	0-/ V hmc 8/ cdf		X		3	0																		
27	0-/ V hmc 024 cdf		X		4	0																		
28	0-/ V hmc 07/ cdf		X		5	0																		
3/	0-/ V hmc 114 cdf		X		6	0																		
30	0-/ V hmc 16/ cdf		X		7	0																		
31	0-/ V hmc 204 cdf		X		8	0																		

Joint Boundary Conditions

	Inhmns K`adk	W Z.hm\	X Z.hm\	Y Z.hm\	WQns-Z,esq`c\	X Qns-Z,esq`c\	Y Qns-Z,esq`c\
0	M330	Qd`bsnm	Qd`bsnm	Qd`bsnm		Qd`bsnm	
1	M331	Qd`bsnm	Qd`bsnm	Qd`bsnm		Qd`bsnm	
2	M332	Qd`bsnm	Qd`bsnm	Qd`bsnm		Qd`bsnm	
3	M333	Qd`bsnm	Qd`bsnm	Qd`bsnm		Qd`bsnm	

Envelope Joint Reactions

	Inhmns		W Z\	KB	X Z\	KB	Y Z\	KB	L W Z,es\	KB	L X Z,es\	KB	L Y Z,es\	KB
0	M330	l`w	33-/18	01	403-120	01	24-740	2	/	23	-322	05	/	23
1		lhm	,25-886	4	,276-032	4	,28-586	0/	/	0	,-276	8	/	0
2	M331	l`w	24-843	06	404-1/5	7	25-808	2	/	23	-311	02	/	23
3		lhm	,31-878	7	,270-/22	06	,3/-8/5	0/	/	0	,-36	3	/	0
4	M332	l`w	21-727	02	401-62	3	3/-840	1	/	23	-207	7	/	23
5		lhm	,28-433	3	,275-247	02	,25-868	00	/	0	,-163	06	/	0
6	M333	l`w	3/-163	05	4/5-063	05	28-512	1	/	23	-130	4	/	23
7		lhm	,22-426	8	,276-/48	8	,24-72	00	/	0	,-174	01	/	0
8	Sns`kr9	l`w	026-36	04	4/8-210	15	041-/64	2						
0/		lhm	,026-347	5	105-/21	2	,041-032	0/						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	L dl adq	Rg`od	Bncd Bgdbj	Knbzes\	KB	Rgd`q--Knbzes\	Clq	KB	ogh)Omb--ogh)Oms--ogh)L m--ogh)L m--Ba	Dpm
0	L 576	V 01W68	-610	5-147	7	-/45	5-147	x 7	617-/80 640-57 035-50 210-2	0--G0,0`
1	L 575	V 01W68	-608	5-147	01	-/44	5-147	x 01	617-/80 640-57 035-50 210-2	0--G0,0`
2	L 577	V 01W68	-600	5-147	3	-/46	5-147	x 3	617-/80 640-57 035-50 210-2	0--G0,0`
3	L 578	V 01W68	-6//	5-147	05	-/44	5-147	x 05	617-/80 640-57 035-50 210-2	0--G0,0`
4	L 5/5	V 0/W57	-577	/	7	-/42	5-14	x 0/	506-/1 533-65 0/7-16 12/-20	0 G0,0`
5	L 5/4	V 0/W57	-574	/	01	-/41	5-14	x 0/	506-/1 533-65 0/7-16 12/-20	0 G0,0`
6	L 5/6	V 0/W57	-572	/	3	-/41	5-14	x 1	506-/1 533-65 0/7-16 12/-20	0 G0,0`
7	L 5/7	V 0/W57	-558	/	05	-/40	5-14	x 1	506-/1 533-65 0/7-16 12/-20	0 G0,0`
8	L 414	V 0/W5/	-5/2	/	7	-/35	5-14	x 0/	437-033 462-37 83-4 1/0-31	0 G0,0`
0/	L 415	V 0/W5/	-484	/	3	-/34	5-14	x 1	437-033 462-37 83-4 1/0-31	0 G0,0`
00	L 413	V 0/W5/	-483	/	01	-/33	/	x 0/	437-033 462-37 83-4 1/0-31	0 G0,0`
01	L 416	V 0/W5/	-470	/	05	-/32	/	x 1	437-033 462-37 83-4 1/0-31	0 G0,0`
02	L 252	V 7W8/	-43/	/	7	-/28	5-14	x 0/	242-142 268-/7 38-84 0/6-35	0 G0,0`
03	L 253	V 7W8/	-422	/	3	-/27	5-14	x 1	242-142 268-/7 38-84 0/6-35	0 G0,0`

Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)

	L dl adq	Rg`od	Bncd Bgdbj	Knbzes\	KB	Rgd`q---	Knbzes\	Clq	KB	ogh)Omb---ogh)Oms---ogh)Lm---ogh)Lm---Ba					Dpm
04	L 251	V 7W3/	-416	/	01	-/25	/	x	0/	242-142	268-/7	38-84	0/6-35	0	G0,0`
05	L 254	V 7W3/	-402	/	05	-/24	/	x	1	242-142	268-/7	38-84	0/6-35	0	G0,0`
06	L 333	V 0/W43	-4/3	14	7	-/32	/	x	01	378-075	400-81	73-40	068-71	0	G0,0`
07	L 334	V 0/W43	-4//	5-14	3	-/30	5-14	x	1	378-075	400-81	73-40	068-71	0	G0,0`
08	L 332	V 0/W43	-387	5-14	01	-/30	/	x	7	378-075	400-81	73-40	068-71	0	G0,0`
1/	L 171	V 7W20	-380	5-14	7	-/30	/	x	01	164-/11	184-701	27-/6	71-/7	0	G0,0`
10	L 335	V 0/W43	-375	5-14	05	-/28	0-452	x	1	378-075	400-81	73-40	068-71	0	G0,0`
11	L 172	V 7W20	-375	5-14	3	-/27	/	x	05	164-/11	184-701	27-/6	71-/7	0	G0,0`
12	L 170	V 7W20	-37/	5-14	01	-/28	/	x	7	164-/11	184-701	27-/6	71-/7	0	G0,0`
13	L 173	V 7W20	-355	5-14	05	-/24	/	x	3	164-/11	184-701	27-/6	71-/7	0	G0,0`
14	L 1/0	V 5W14	-324	/	7	-/12	/	x	01	1/8-32	126-705	12-001	40-/2	0	G0,0`
15	L 1/1	V 5W14	-313	/	3	-/11	5-14	x	1	1/8-32	126-705	12-001	40-/2	0	G0,0`
16	L 1//	V 5W14	-305	/	01	-/10	/	x	7	1/8-32	126-705	12-001	40-/2	0	G0,0`
17	L 1/2	V 5W14	-288	/	05	-/08	/	x	1	1/8-32	126-705	12-001	40-/2	0	G0,0`
18	L 01/	V 5W1/	-26/	/	11	-/13	14	x	03	055-776	08/-077	07-033	3/-12	0	G0,0`
2/	L 010	V 5W1/	-223	/	1/	-/10	14	x	03	055-776	08/-077	07-033	3/-12	0	G0,0`
20	L 008	V 5W1/	-216	/	13	-/12	14	x	5	055-776	08/-077	07-033	3/-12	0	G0,0`
21	L 0160	V 01W15	-2/0	1/-64	13	-//6	/	x	0	08/-1/8	136-75	11-/48	41-487	0	G0,0`
22	L 0162	V 01W15	-2/0	1/-64	15	-//6	30-4	x	0	08/-1/8	136-75	11-/48	41-487	0	G0,0`
23	L 0161	V 01W15	-2//	1/-64	13	-//6	30-4	x	0	08/-1/8	136-75	11-/48	41-487	0	G0,0`
24	L 016/	V 01W15	-2//	1/-64	1/	-//6	/	x	0	08/-1/8	136-75	11-/48	41-487	0	G0,0`
25	L 011	V 5W1/	-175	/	15	-/10	14	x	5	055-776	08/-077	07-033	3/-12	0	G0,0`
26	L 37	V 5W1/	-043	/	11	-/03	/	x	03	055-776	08/-077	07-033	3/-12	0	G0,0a)
27	L 38	V 5W1/	-031	/	1/	-/02	/	x	03	055-776	08/-077	07-033	3/-12	0	G0,0a)
28	L 36	V 5W1/	-022	/	13	-/03	/	x	5	055-776	08/-077	07-033	3/-12	0	G0,0a)
3/	L 4/	V 5W1/	-01/	5-14	15	-/01	/	x	5	055-776	08/-077	07-033	3/-12	0	G0,0a)
30	L 31	V 0/W2/	-/5/	00-733	11	-/01	00-7---	x	11	137-705	175-305	12-757	72-588	0	G0,0a
31	L 32	V 0/W2/	-/5/	00-733	1/	-/01	00-7---	x	1/	137-705	175-305	12-757	72-588	0	G0,0a
32	L 34	V 0/W2/	-/48	00-733	13	-/01	00-7---	x	13	137-705	175-305	12-757	72-588	0	G0,0a
33	L 33	V 0/W2/	-/48	00-733	15	-/01	00-7---	x	15	137-705	175-305	12-757	72-588	0	G0,0a
34	L 0144	V 7W02	-/45	7-264	0	-//3	/	x	0	47-782	013-305	4-7/4	00-601	0	G0,0a
35	L 0145	V 7W02	-/45	7-264	0	-//3	/	x	0	47-782	013-305	4-7/4	00-601	0	G0,0a
36	L 0143	V 7W02	-/45	7-264	0	-//3	/	x	0	47-782	013-305	4-7/4	00-601	0	G0,0a
37	L 0146	V 7W02	-/44	7-264	0	-//3	/	x	0	47-782	013-305	4-7/4	00-601	0	G0,0a
38	L 740	B3w6-1	-/32	/	15	-//2	/	x	05	12-/68	58-/01	0-345	5-684	0	G0,0a)
4/	L 741	B3w6-1	-/31	/	15	-//2	4-264	x	05	12-/68	58-/01	0-345	5-684	0	G0,0a)
40	L 754	B3w6-1	-/18	/	15	-//1	/	x	01	23-712	58-/01	0-345	6-/65	0	G0,0a)
41	L 0150	V 7W02	-//5	/	7	-//2	/	x	0	2/-420	013-305	4-7/4	1/-757	0---	G0,0a)
42	L 015/	V 7W02	-//5	/	3	-//2	/	x	0	2/-420	013-305	4-7/4	1/-757	0---	G0,0a)
43	L 0147	V 7W02	-//4	/	01	-//2	/	x	0	2/-420	013-305	4-7/4	1/-757	0---	G0,0a)
44	L 0148	V 7W02	-//4	/	05	-//2	/	x	0	2/-420	013-305	4-7/4	1/-757	0---	G0,0a)
45	L 751	B3w6-1	-//3	1-/83	11	-//2	3-077	x	3	24-331	58-/01	0-345	6-/8	0	G0,0a
46	L 752	B3w6-1	-//3	1-/83	15	-//2	3-077	x	01	24-331	58-/01	0-345	6-/8	0	G0,0a
47	L 736	B3w6-1	-//3	1-/83	1/	-//2	/	x	7	24-331	58-/01	0-345	6-/8	0	G0,0a
48	L 734	B3w6-1	-//3	1-/83	12	-//2	/	x	01	24-331	58-/01	0-345	6-/8	0	G0,0a
5/	L 738	B3w6-1	-//3	1-/83	08	-//2	/	x	3	24-331	58-/01	0-345	6-/8	0	G0,0a
50	L 75/	B3w6-1	-//3	1-/83	12	-//2	3-077	x	7	24-331	58-/01	0-345	6-/8	0	G0,0a

TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2022702.66

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_DIAG_OUTER_T1	M1274	1.694	31.15	1.77	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1275	1.862	31.15	1.86	128.64	6.0%	Pass
TWR_DIAG_OUTER_T1	M1276	1.828	31.15	1.67	128.64	5.9%	Pass
TWR_DIAG_OUTER_T1	M1277	1.933	31.15	1.81	128.64	6.2%	Pass
TWR_DIAG_OUTER_T1	M1278	1.947	31.15	1.82	128.64	6.3%	Pass
TWR_DIAG_OUTER_T1	M1279	1.875	31.15	1.69	128.64	6.0%	Pass
TWR_DIAG_OUTER_T1	M1280	1.737	31.15	1.75	128.64	5.6%	Pass
TWR_DIAG_OUTER_T1	M1281	1.872	31.15	1.83	128.64	6.0%	Pass
TWR_DIAG_OUTER_T1	M1282	2.218	41.82	1.23	128.64	5.3%	Pass
TWR_DIAG_OUTER_T1	M1283	2.238	41.82	1.21	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1284	2.145	41.82	1.09	128.64	5.1%	Pass
TWR_DIAG_OUTER_T1	M1285	2.089	41.82	1.13	128.64	5.0%	Pass
TWR_DIAG_OUTER_T1	M1286	2.278	41.82	1.27	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1287	2.275	41.82	1.27	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1288	2.111	41.82	1.14	128.64	5.0%	Pass
TWR_DIAG_OUTER_T1	M1289	2.154	41.82	1.11	128.64	5.2%	Pass
TWR_DIAG_T1	M15	6.308	19.53	2.87	118.53	32.3%	Pass
TWR_DIAG_T1	M18	7.619	19.53	2.67	118.53	39.0%	Pass
TWR_DIAG_T1	M22	7.803	19.53	2.99	118.53	40.0%	Pass
TWR_DIAG_T1	M25	7.581	19.53	3.02	118.53	38.8%	Pass
TWR_DIAG_T1	M29	7.268	19.53	2.48	118.53	37.2%	Pass
TWR_DIAG_T1	M32	6.097	19.53	2.82	118.53	31.2%	Pass
TWR_DIAG_T1	M36	5.53	19.53	2.13	118.53	28.3%	Pass
TWR_DIAG_T1	M39	5.692	19.53	2.03	118.53	29.1%	Pass
TWR_DIAG_T2	M51	17.745	82.48	10.13	103.87	21.5%	Pass
TWR_DIAG_T2	M59	17.705	82.48	10.09	103.87	21.5%	Pass
TWR_DIAG_T2	M67	19.711	82.48	11.60	103.87	23.9%	Pass
TWR_DIAG_T2	M75	19.801	82.48	11.65	103.87	24.0%	Pass
TWR_DIAG_T2	M83	17.463	82.48	9.95	103.87	21.2%	Pass
TWR_DIAG_T2	M91	17.407	82.48	9.94	103.87	21.1%	Pass
TWR_DIAG_T2	M99	16.884	82.48	9.93	103.87	20.5%	Pass
TWR_DIAG_T2	M107	16.97	82.48	9.84	103.87	20.6%	Pass
TWR_DIAG_T3	M124	23.027	82.48	20.58	103.87	27.9%	Pass
TWR_DIAG_T3	M132	23.09	82.48	20.57	103.87	28.0%	Pass
TWR_DIAG_T3	M141	24.668	82.48	22.41	103.87	29.9%	Pass
TWR_DIAG_T3	M149	24.665	82.48	22.41	103.87	29.9%	Pass
TWR_DIAG_T3	M158	21.969	82.48	19.71	103.87	26.6%	Pass
TWR_DIAG_T3	M166	21.889	82.48	19.71	103.87	26.5%	Pass
TWR_DIAG_T3	M175	22.183	82.48	20.08	103.87	26.9%	Pass
TWR_DIAG_T3	M183	22.271	82.48	20.02	103.87	27.0%	Pass
TWR_DIAG_T4	M205	29.194	109.11	26.50	134.58	26.8%	Pass
TWR_DIAG_T4	M213	29.264	109.11	26.53	134.58	26.8%	Pass
TWR_DIAG_T4	M222	31.415	109.11	29.06	134.58	28.8%	Pass
TWR_DIAG_T4	M230	31.408	109.11	29.03	134.58	28.8%	Pass
TWR_DIAG_T4	M239	27.674	109.11	25.13	134.58	25.4%	Pass
TWR_DIAG_T4	M247	27.567	109.11	25.13	134.58	25.3%	Pass
TWR_DIAG_T4	M256	28.758	109.11	26.57	134.58	26.4%	Pass
TWR_DIAG_T4	M264	28.862	109.11	26.50	134.58	26.5%	Pass
TWR_DIAG_T5	M286	35.422	109.11	32.11	134.58	32.5%	Pass
TWR_DIAG_T5	M294	35.508	109.11	32.14	134.58	32.5%	Pass
TWR_DIAG_T5	M303	37.998	109.11	35.23	134.58	34.8%	Pass
TWR_DIAG_T5	M311	37.981	109.11	35.20	134.58	34.8%	Pass
TWR_DIAG_T5	M320	33.34	109.11	30.13	134.58	30.6%	Pass
TWR_DIAG_T5	M328	33.202	109.11	30.13	134.58	30.4%	Pass
TWR_DIAG_T5	M337	35.397	109.11	32.74	134.58	32.4%	Pass
TWR_DIAG_T5	M345	35.515	109.11	32.66	134.58	32.5%	Pass

TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2022702.66

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_DIAG_T6	M367	41.627	123.38	38.64	140.74	33.7%	Pass
TWR_DIAG_T6	M375	41.73	123.38	38.66	140.74	33.8%	Pass
TWR_DIAG_T6	M384	44.73	123.38	42.23	140.74	36.3%	Pass
TWR_DIAG_T6	M392	44.708	123.38	42.20	140.74	36.2%	Pass
TWR_DIAG_T6	M401	39.123	123.38	36.12	140.74	31.7%	Pass
TWR_DIAG_T6	M409	38.953	123.38	36.12	140.74	31.6%	Pass
TWR_DIAG_T6	M418	42.182	123.38	39.75	140.74	34.2%	Pass
TWR_DIAG_T6	M426	42.308	123.38	39.68	140.74	34.3%	Pass
TWR_DIAG_T7	M448	46.797	123.38	44.07	140.74	37.9%	Pass
TWR_DIAG_T7	M456	46.895	123.38	44.10	140.74	38.0%	Pass
TWR_DIAG_T7	M465	50.535	123.38	48.07	140.74	41.0%	Pass
TWR_DIAG_T7	M473	50.507	123.38	48.03	140.74	40.9%	Pass
TWR_DIAG_T7	M482	43.85	123.38	41.00	140.74	35.5%	Pass
TWR_DIAG_T7	M490	43.654	123.38	41.00	140.74	35.4%	Pass
TWR_DIAG_T7	M499	48.111	123.38	45.72	140.74	39.0%	Pass
TWR_DIAG_T7	M507	48.269	123.38	45.63	140.74	39.1%	Pass
TWR_DIAG_T8	M529	54.026	163.93	49.91	183.52	33.0%	Pass
TWR_DIAG_T8	M537	54.124	163.93	49.95	183.52	33.0%	Pass
TWR_DIAG_T8	M546	57.484	163.93	54.11	183.52	35.1%	Pass
TWR_DIAG_T8	M554	57.45	163.93	54.07	183.52	35.0%	Pass
TWR_DIAG_T8	M563	50.487	163.93	46.29	183.52	30.8%	Pass
TWR_DIAG_T8	M571	50.271	163.93	46.30	183.52	30.7%	Pass
TWR_DIAG_T8	M580	55.002	163.93	51.76	183.52	33.6%	Pass
TWR_DIAG_T8	M588	55.183	163.93	51.68	183.52	33.7%	Pass
TWR_DIAG_T9	M610	58.679	163.93	54.39	183.52	35.8%	Pass
TWR_DIAG_T9	M618	58.738	163.93	54.41	183.52	35.8%	Pass
TWR_DIAG_T9	M627	62.958	163.93	59.12	183.52	38.4%	Pass
TWR_DIAG_T9	M635	62.919	163.93	59.11	183.52	38.4%	Pass
TWR_DIAG_T9	M644	54.658	163.93	50.21	183.52	33.3%	Pass
TWR_DIAG_T9	M652	54.484	163.93	50.18	183.52	33.2%	Pass
TWR_DIAG_T9	M661	60.583	163.93	56.83	183.52	37.0%	Pass
TWR_DIAG_T9	M669	60.742	163.93	56.78	183.52	37.1%	Pass
TWR_DIAG_T10	M691	64.841	196.60	55.82	216.14	33.0%	Pass
TWR_DIAG_T10	M701	64.496	196.60	55.87	216.14	32.8%	Pass
TWR_DIAG_T10	M712	81.556	197.78	74.00	216.14	41.2%	Pass
TWR_DIAG_T10	M722	81.721	197.78	74.03	216.14	41.3%	Pass
TWR_DIAG_T10	M733	58.603	196.60	50.51	216.14	29.8%	Pass
TWR_DIAG_T10	M743	58.803	196.60	50.20	216.14	29.9%	Pass
TWR_DIAG_T10	M754	78.602	197.78	71.31	216.14	39.7%	Pass
TWR_DIAG_T10	M764	78.607	197.78	71.38	216.14	39.7%	Pass
TWR_HORZ_T3	M123	9.852	61.03	13.10	71.53	18.3%	Pass
TWR_HORZ_T3	M140	10.755	61.03	14.40	71.53	20.1%	Pass
TWR_HORZ_T3	M157	9.433	61.03	10.90	71.53	15.5%	Pass
TWR_HORZ_T3	M174	9.669	61.03	10.87	71.53	15.8%	Pass
TWR_HORZ_T4	M204	14.58	61.03	14.92	71.53	23.9%	Pass
TWR_HORZ_T4	M221	15.98	61.03	16.40	71.53	26.2%	Pass
TWR_HORZ_T4	M238	13.816	61.03	12.28	71.53	22.6%	Pass
TWR_HORZ_T4	M255	14.609	61.03	12.95	71.53	23.9%	Pass
TWR_HORZ_T5	M285	17.644	61.03	17.78	71.53	28.9%	Pass
TWR_HORZ_T5	M302	19.36	61.03	19.76	71.53	31.7%	Pass
TWR_HORZ_T5	M319	16.559	61.03	14.74	71.53	27.1%	Pass
TWR_HORZ_T5	M336	17.989	61.03	15.98	71.53	29.5%	Pass

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TWR_HORZ_T6	M366	21.282	74.47	21.56	87.93	28.6%	Pass
TWR_HORZ_T6	M383	23.259	74.47	23.77	87.93	31.2%	Pass
TWR_HORZ_T6	M400	19.9	74.47	18.03	87.93	26.7%	Pass
TWR_HORZ_T6	M417	21.905	74.47	19.84	87.93	29.4%	Pass
TWR_HORZ_T7	M447	24.449	87.31	24.66	103.87	28.0%	Pass
TWR_HORZ_T7	M464	26.522	87.31	26.96	103.87	30.4%	Pass
TWR_HORZ_T7	M481	22.722	87.31	20.76	103.87	26.0%	Pass
TWR_HORZ_T7	M498	25.223	87.31	23.17	103.87	28.9%	Pass
TWR_HORZ_T8	M528	27.841	87.31	27.91	103.87	31.9%	Pass
TWR_HORZ_T8	M545	29.945	87.31	30.32	103.87	34.3%	Pass
TWR_HORZ_T8	M562	25.766	87.31	23.36	103.87	29.5%	Pass
TWR_HORZ_T8	M579	28.655	87.31	26.14	103.87	32.8%	Pass
TWR_HORZ_T9	M609	30.059	87.31	30.06	103.87	34.4%	Pass
TWR_HORZ_T9	M626	32.635	87.31	32.88	103.87	37.4%	Pass
TWR_HORZ_T9	M643	27.737	87.31	25.45	103.87	31.8%	Pass
TWR_HORZ_T9	M660	31.415	87.31	28.84	103.87	36.0%	Pass
TWR_HORZ_T10	M690	33.162	181.47	27.81	183.52	18.3%	Pass
TWR_HORZ_T10	M711	31.937	181.47	29.18	183.52	17.6%	Pass
TWR_HORZ_T10	M732	29.195	181.47	24.27	183.52	16.1%	Pass
TWR_HORZ_T10	M753	30.571	181.47	28.02	183.52	16.8%	Pass
TWR_INNER_BRACE_T3	M1221	0.196	30.89	0.02	48.02	0.6%	Pass
TWR_INNER_BRACE_T3	M1222	0.198	30.89	0.01	48.02	0.6%	Pass
TWR_INNER_BRACE_T3	M1223	0.096	30.89	0.01	48.02	0.3%	Pass
TWR_INNER_BRACE_T3	M1224	0.095	30.89	0.02	48.02	0.3%	Pass
TWR_INNER_BRACE_T3	M1225	0.196	30.89	0.01	48.02	0.6%	Pass
TWR_INNER_BRACE_T3	M1226	0.196	30.89	0.01	48.02	0.6%	Pass
TWR_INNER_BRACE_T4	M1169	0.213	30.89	0.02	48.02	0.7%	Pass
TWR_INNER_BRACE_T4	M1170	0.215	30.89	0.01	48.02	0.7%	Pass
TWR_INNER_BRACE_T4	M1171	0.097	30.89	0.02	48.02	0.3%	Pass
TWR_INNER_BRACE_T4	M1172	0.095	30.89	0.02	48.02	0.3%	Pass
TWR_INNER_BRACE_T4	M1173	0.214	30.89	0.02	48.02	0.7%	Pass
TWR_INNER_BRACE_T4	M1174	0.213	30.89	0.02	48.02	0.7%	Pass
TWR_INNER_BRACE_T5	M1117	0.217	30.89	0.03	48.02	0.7%	Pass
TWR_INNER_BRACE_T5	M1118	0.217	30.89	0.02	48.02	0.7%	Pass
TWR_INNER_BRACE_T5	M1119	0.1	30.89	0.03	48.02	0.3%	Pass
TWR_INNER_BRACE_T5	M1120	0.099	30.89	0.03	48.02	0.3%	Pass
TWR_INNER_BRACE_T5	M1121	0.215	30.89	0.02	48.02	0.7%	Pass
TWR_INNER_BRACE_T5	M1122	0.217	30.89	0.03	48.02	0.7%	Pass
TWR_INNER_BRACE_T6	M1065	0.272	30.89	0.03	48.02	0.9%	Pass
TWR_INNER_BRACE_T6	M1066	0.273	30.89	0.02	48.02	0.9%	Pass
TWR_INNER_BRACE_T6	M1067	0.127	30.89	0.03	48.02	0.4%	Pass
TWR_INNER_BRACE_T6	M1068	0.125	30.89	0.03	48.02	0.4%	Pass
TWR_INNER_BRACE_T6	M1069	0.27	30.89	0.02	48.02	0.9%	Pass
TWR_INNER_BRACE_T6	M1070	0.273	30.89	0.03	48.02	0.9%	Pass

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TWR_INNER_BRACE_T7	M1013	0.327	30.89	0.04	48.02	1.1%	Pass
TWR_INNER_BRACE_T7	M1014	0.326	30.89	0.03	48.02	1.1%	Pass
TWR_INNER_BRACE_T7	M1015	0.155	30.89	0.04	48.02	0.5%	Pass
TWR_INNER_BRACE_T7	M1016	0.154	30.89	0.05	48.02	0.5%	Pass
TWR_INNER_BRACE_T7	M1017	0.324	30.89	0.04	48.02	1.0%	Pass
TWR_INNER_BRACE_T7	M1018	0.327	30.89	0.04	48.02	1.1%	Pass
TWR_INNER_BRACE_T8	M961	0.334	30.89	0.05	48.02	1.1%	Pass
TWR_INNER_BRACE_T8	M962	0.332	30.89	0.04	48.02	1.1%	Pass
TWR_INNER_BRACE_T8	M963	0.155	30.89	0.05	48.02	0.5%	Pass
TWR_INNER_BRACE_T8	M964	0.153	30.89	0.05	48.02	0.5%	Pass
TWR_INNER_BRACE_T8	M965	0.328	30.89	0.04	48.02	1.1%	Pass
TWR_INNER_BRACE_T8	M966	0.335	30.89	0.05	48.02	1.1%	Pass
TWR_INNER_BRACE_T9	M909	0.336	30.89	0.06	48.02	1.1%	Pass
TWR_INNER_BRACE_T9	M910	0.333	30.89	0.04	48.02	1.1%	Pass
TWR_INNER_BRACE_T9	M911	0.157	30.89	0.06	48.02	0.5%	Pass
TWR_INNER_BRACE_T9	M912	0.156	30.89	0.06	48.02	0.5%	Pass
TWR_INNER_BRACE_T9	M913	0.329	30.89	0.05	48.02	1.1%	Pass
TWR_INNER_BRACE_T9	M914	0.338	30.89	0.06	48.02	1.1%	Pass
TWR_INNER_CORNER_T3	M1206	0	15.44	3.97	48.02	8.3%	Pass
TWR_INNER_CORNER_T3	M1207	0	15.44	4.04	48.02	8.4%	Pass
TWR_INNER_CORNER_T3	M1208	0	15.44	4.01	48.02	8.3%	Pass
TWR_INNER_CORNER_T4	M1154	0	15.44	3.64	48.02	7.6%	Pass
TWR_INNER_CORNER_T4	M1155	0	15.44	3.85	48.02	8.0%	Pass
TWR_INNER_CORNER_T4	M1156	0	15.44	3.63	48.02	7.6%	Pass
TWR_INNER_CORNER_T5	M1102	0	15.44	4.37	48.02	9.1%	Pass
TWR_INNER_CORNER_T5	M1103	0	15.44	4.63	48.02	9.6%	Pass
TWR_INNER_CORNER_T5	M1104	0	15.44	4.36	48.02	9.1%	Pass
TWR_INNER_CORNER_T6	M1050	0	15.44	4.49	48.02	9.4%	Pass
TWR_INNER_CORNER_T6	M1051	0	15.44	4.72	48.02	9.8%	Pass
TWR_INNER_CORNER_T6	M1052	0	15.44	4.48	48.02	9.3%	Pass
TWR_INNER_CORNER_T7	M998	0	15.44	4.49	48.02	9.3%	Pass
TWR_INNER_CORNER_T7	M999	0	15.44	4.68	48.02	9.7%	Pass
TWR_INNER_CORNER_T7	M1000	0	15.44	4.47	48.02	9.3%	Pass
TWR_INNER_CORNER_T8	M946	0	15.44	5.03	48.02	10.5%	Pass
TWR_INNER_CORNER_T8	M947	0	15.44	5.25	48.02	10.9%	Pass
TWR_INNER_CORNER_T8	M948	0	15.44	5.00	48.02	10.4%	Pass
TWR_INNER_CORNER_T9	M894	0	15.44	5.46	48.02	11.4%	Pass
TWR_INNER_CORNER_T9	M895	0	15.44	5.73	48.02	11.9%	Pass
TWR_INNER_CORNER_T9	M896	0	15.44	5.48	48.02	11.4%	Pass
TWR_INNER_LADDER_T3	M1227	2.529	60.14	1.17	71.53	4.2%	Pass
TWR_INNER_LADDER_T3	M1228	0.875	58.32	1.88	71.53	2.6%	Pass
TWR_INNER_LADDER_T3	M1229	0.876	58.32	1.88	71.53	2.6%	Pass
TWR_INNER_LADDER_T4	M1175	1.61	58.32	1.74	71.53	2.8%	Pass
TWR_INNER_LADDER_T4	M1176	1.608	58.32	1.77	71.53	2.8%	Pass
TWR_INNER_LADDER_T4	M1177	2.361	60.14	2.16	71.53	3.9%	Pass
TWR_INNER_LADDER_T5	M1123	2.846	60.14	2.66	71.53	4.7%	Pass
TWR_INNER_LADDER_T5	M1124	1.978	58.32	2.09	71.53	3.4%	Pass
TWR_INNER_LADDER_T5	M1125	1.978	58.32	2.13	71.53	3.4%	Pass
TWR_INNER_LADDER_T6	M1071	2.025	58.32	2.12	71.53	3.5%	Pass

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TWR_INNER_LADDER_T6	M1072	2.025	58.32	2.18	71.53	3.5%	Pass
TWR_INNER_LADDER_T6	M1073	2.896	60.14	2.72	71.53	4.8%	Pass
TWR_INNER_LADDER_T7	M1019	2.865	60.14	2.70	71.53	4.8%	Pass
TWR_INNER_LADDER_T7	M1020	2.013	58.32	2.17	71.53	3.5%	Pass
TWR_INNER_LADDER_T7	M1021	2.011	58.32	2.09	71.53	3.4%	Pass
TWR_INNER_LADDER_T8	M967	3.202	60.14	3.08	71.53	5.3%	Pass
TWR_INNER_LADDER_T8	M968	2.3	58.32	2.42	71.53	3.9%	Pass
TWR_INNER_LADDER_T8	M969	2.298	58.32	2.33	71.53	3.9%	Pass
TWR_INNER_LADDER_T9	M915	3.5	60.14	3.37	71.53	5.8%	Pass
TWR_INNER_LADDER_T9	M916	2.514	58.32	2.65	71.53	4.3%	Pass
TWR_INNER_LADDER_T9	M917	2.508	58.32	2.54	71.53	4.3%	Pass
TWR_INNER_SQ_T3	M1202	1.482	7.72	3.16	48.02	19.2%	Pass
TWR_INNER_SQ_T3	M1203	1.424	7.72	3.08	48.02	18.4%	Pass
TWR_INNER_SQ_T3	M1204	1.325	7.72	3.45	48.02	17.2%	Pass
TWR_INNER_SQ_T3	M1205	1.297	7.72	3.30	48.02	16.8%	Pass
TWR_INNER_SQ_T4	M1150	1.23	7.72	3.14	48.02	15.9%	Pass
TWR_INNER_SQ_T4	M1151	1.299	7.72	3.36	48.02	16.8%	Pass
TWR_INNER_SQ_T4	M1152	2.101	7.72	2.84	48.02	27.2%	Pass
TWR_INNER_SQ_T4	M1153	2.156	7.72	3.04	48.02	27.9%	Pass
TWR_INNER_SQ_T5	M1098	2.613	7.72	3.70	48.02	33.8%	Pass
TWR_INNER_SQ_T5	M1099	1.423	7.72	3.76	48.02	18.4%	Pass
TWR_INNER_SQ_T5	M1100	1.525	7.72	4.08	48.02	19.7%	Pass
TWR_INNER_SQ_T5	M1101	2.549	7.72	3.41	48.02	33.0%	Pass
TWR_INNER_SQ_T6	M1046	1.45	7.72	3.85	48.02	18.8%	Pass
TWR_INNER_SQ_T6	M1047	1.555	7.72	4.18	48.02	20.1%	Pass
TWR_INNER_SQ_T6	M1048	2.626	7.72	3.47	48.02	34.0%	Pass
TWR_INNER_SQ_T6	M1049	2.663	7.72	3.78	48.02	34.5%	Pass
TWR_INNER_SQ_T7	M994	2.639	7.72	3.75	48.02	34.2%	Pass
TWR_INNER_SQ_T7	M995	1.44	7.72	3.81	48.02	18.6%	Pass
TWR_INNER_SQ_T7	M996	1.548	7.72	4.14	48.02	20.0%	Pass
TWR_INNER_SQ_T7	M997	2.623	7.72	3.44	48.02	34.0%	Pass
TWR_INNER_SQ_T8	M942	1.587	7.72	4.29	48.02	20.6%	Pass
TWR_INNER_SQ_T8	M943	1.706	7.72	4.65	48.02	22.1%	Pass
TWR_INNER_SQ_T8	M944	2.989	7.72	3.87	48.02	38.7%	Pass
TWR_INNER_SQ_T8	M945	2.984	7.72	4.21	48.02	38.6%	Pass
TWR_INNER_SQ_T9	M890	3.238	7.72	4.21	48.02	41.9%	Pass
TWR_INNER_SQ_T9	M891	1.843	7.72	5.09	48.02	23.9%	Pass
TWR_INNER_SQ_T9	M892	1.703	7.72	4.66	48.02	22.1%	Pass
TWR_INNER_SQ_T9	M893	3.244	7.72	4.61	48.02	42.0%	Pass

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TWR_INNER_SUPP_T3	M191	1.761	33.30	1.61	71.53	5.3%	Pass
TWR_INNER_SUPP_T3	M192	1.694	33.30	1.77	71.53	5.1%	Pass
TWR_INNER_SUPP_T3	M193	1.608	33.30	1.78	71.53	4.8%	Pass
TWR_INNER_SUPP_T3	M194	1.771	33.30	1.70	71.53	5.3%	Pass
TWR_INNER_SUPP_T3	M195	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M196	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M197	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M198	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M199	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M272	1.839	33.30	1.56	71.53	5.5%	Pass
TWR_INNER_SUPP_T4	M273	1.72	33.30	1.85	71.53	5.2%	Pass
TWR_INNER_SUPP_T4	M274	1.562	33.30	1.86	71.53	4.7%	Pass
TWR_INNER_SUPP_T4	M275	1.832	33.30	1.74	71.53	5.5%	Pass
TWR_INNER_SUPP_T4	M276	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M277	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M278	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M279	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M280	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M353	2.222	33.30	1.89	71.53	6.7%	Pass
TWR_INNER_SUPP_T5	M354	2.039	33.30	2.24	71.53	6.1%	Pass
TWR_INNER_SUPP_T5	M355	1.871	33.30	2.24	71.53	5.6%	Pass
TWR_INNER_SUPP_T5	M356	2.212	33.30	2.08	71.53	6.6%	Pass
TWR_INNER_SUPP_T5	M357	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M358	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M359	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M360	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M361	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M434	2.258	33.30	1.93	71.53	6.8%	Pass
TWR_INNER_SUPP_T6	M435	2.072	33.30	2.29	71.53	6.2%	Pass
TWR_INNER_SUPP_T6	M436	1.905	33.30	2.29	71.53	5.7%	Pass
TWR_INNER_SUPP_T6	M437	2.252	33.30	2.12	71.53	6.8%	Pass

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TWR_INNER_SUPP_T6	M438	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M439	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M440	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M441	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M442	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M515	2.238	33.30	1.90	71.53	6.7%	Pass
TWR_INNER_SUPP_T7	M516	2.067	33.30	2.27	71.53	6.2%	Pass
TWR_INNER_SUPP_T7	M517	1.907	33.30	2.29	71.53	5.7%	Pass
TWR_INNER_SUPP_T7	M518	2.242	33.30	2.11	71.53	6.7%	Pass
TWR_INNER_SUPP_T7	M519	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M520	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M521	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M522	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M523	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M596	2.502	33.30	2.13	71.53	7.5%	Pass
TWR_INNER_SUPP_T8	M597	2.364	33.30	2.55	71.53	7.1%	Pass
TWR_INNER_SUPP_T8	M598	2.123	33.30	2.57	71.53	6.4%	Pass
TWR_INNER_SUPP_T8	M599	2.508	33.30	2.38	71.53	7.5%	Pass
TWR_INNER_SUPP_T8	M600	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M601	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M602	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M603	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M604	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M677	2.721	33.30	2.36	71.53	8.2%	Pass
TWR_INNER_SUPP_T9	M678	2.533	33.30	2.78	71.53	7.6%	Pass
TWR_INNER_SUPP_T9	M679	2.261	33.30	2.78	71.53	6.8%	Pass
TWR_INNER_SUPP_T9	M680	2.71	33.30	2.57	71.53	8.1%	Pass
TWR_INNER_SUPP_T9	M681	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M682	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M683	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M684	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M685	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_TRI_T3	M1209	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1210	0.009	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1211	0.009	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1212	0.009	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1213	0.045	47.81	0.00	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1214	0.006	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1215	0.045	47.81	0.00	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1216	0.006	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1217	0.006	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1218	0.045	47.81	0.00	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1219	0.045	47.81	0.00	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1220	0.006	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1157	0.017	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1158	0.008	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1159	0.009	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1160	0.017	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1161	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1162	0.008	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1163	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1164	0.008	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1165	0.008	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1166	0.049	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1167	0.049	47.81	0.00	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1168	0.008	47.81	0.03	48.02	0.1%	Pass

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TWR_INNER_TRI_T5	M1105	0.021	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1106	0.02	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1107	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1108	0.009	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1109	0.009	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1110	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1111	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1112	0.009	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1113	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1114	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1115	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1116	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1053	0.021	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1054	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1055	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1056	0.021	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1057	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1058	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1059	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1060	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1061	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1062	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1063	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1064	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1001	0.021	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1002	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1003	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1004	0.021	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1005	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1006	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1007	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1008	0.01	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1009	0.009	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1010	0.049	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1011	0.049	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1012	0.009	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M949	0.024	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M950	0.01	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M951	0.011	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M952	0.024	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M953	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M954	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M955	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M956	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M957	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M958	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M959	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M960	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M897	0.026	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M898	0.011	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M899	0.012	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M900	0.026	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M901	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M902	0.012	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M903	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M904	0.05	47.81	0.01	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M905	0.05	47.81	0.01	48.02	0.1%	Pass

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TWR_INNER_TRI_T9	M906	0.011	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M907	0.012	47.81	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M908	0.051	47.81	0.01	48.02	0.1%	Pass
TWR_LEG_OUTER_T1	M1266	2.66	14.89	1.02	63.37	17.9%	Pass
TWR_LEG_OUTER_T1	M1267	2.651	14.89	1.05	63.37	17.8%	Pass
TWR_LEG_OUTER_T1	M1268	2.631	14.89	1.03	63.37	17.7%	Pass
TWR_LEG_OUTER_T1	M1269	2.647	14.89	0.99	63.37	17.8%	Pass
TWR_LEG_T1	M1	16.399	84.54	2.18	173.32	19.4%	Pass
TWR_LEG_T1	M2	19.245	84.54	1.49	173.32	22.8%	Pass
TWR_LEG_T1	M3	18.675	84.54	1.47	173.32	22.1%	Pass
TWR_LEG_T1	M4	15.786	84.54	2.32	173.32	18.7%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_REDHIPDIA_2_T9	M882	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_REDHIPDIA_2_T9	M883	0.589	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M884	0.592	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M885	0.588	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M886	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M887	0.593	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M888	0.58	14.70	0.00	48.02	3.9%	Pass
TWR_REDHIPDIA_2_T9	M889	0.579	14.70	0.00	48.02	3.9%	Pass
TWR_RED_DIAG_0_T10	M791	8.276	22.51	6.28	59.46	36.8%	Pass
TWR_RED_DIAG_0_T10	M792	11.072	22.89	8.00	59.46	48.4%	Pass
TWR_RED_DIAG_0_T10	M793	8.06	22.51	6.23	59.46	35.8%	Pass
TWR_RED_DIAG_0_T10	M794	11.266	22.89	8.48	59.46	49.2%	Pass
TWR_RED_DIAG_0_T10	M795	10.943	22.89	8.44	59.46	47.8%	Pass
TWR_RED_DIAG_0_T10	M796	7.972	22.51	6.34	59.46	35.4%	Pass
TWR_RED_DIAG_0_T10	M797	8.297	22.51	6.52	59.46	36.9%	Pass
TWR_RED_DIAG_0_T10	M798	10.901	22.89	8.11	59.46	47.6%	Pass
TWR_RED_DIAG_2_T2	M56	0.596	21.11	0.90	48.02	2.8%	Pass
TWR_RED_DIAG_2_T2	M64	0.603	21.11	0.90	48.02	2.9%	Pass
TWR_RED_DIAG_2_T2	M72	0.886	21.11	1.22	48.02	4.2%	Pass
TWR_RED_DIAG_2_T2	M80	0.884	21.11	1.22	48.02	4.2%	Pass
TWR_RED_DIAG_2_T2	M88	0.69	21.11	0.99	48.02	3.3%	Pass
TWR_RED_DIAG_2_T2	M96	0.686	21.11	1.00	48.02	3.2%	Pass
TWR_RED_DIAG_2_T2	M104	0.618	21.11	0.96	48.02	2.9%	Pass
TWR_RED_DIAG_2_T2	M112	0.619	21.11	0.96	48.02	2.9%	Pass
TWR_RED_DIAG_2_T3	M129	0.289	21.11	0.54	48.02	1.4%	Pass
TWR_RED_DIAG_2_T3	M137	0.282	21.11	0.54	48.02	1.3%	Pass
TWR_RED_DIAG_2_T3	M146	0.211	21.11	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T3	M154	0.216	21.11	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T3	M163	0.097	21.11	0.35	48.02	0.7%	Pass
TWR_RED_DIAG_2_T3	M171	0.098	21.11	0.38	48.02	0.8%	Pass
TWR_RED_DIAG_2_T3	M180	0.239	21.11	0.56	48.02	1.2%	Pass
TWR_RED_DIAG_2_T3	M188	0.23	21.11	0.55	48.02	1.2%	Pass
TWR_RED_DIAG_2_T4	M210	0.204	21.15	0.48	48.02	1.0%	Pass
TWR_RED_DIAG_2_T4	M218	0.156	21.15	0.44	48.02	0.9%	Pass
TWR_RED_DIAG_2_T4	M227	0.209	21.15	0.57	48.02	1.2%	Pass
TWR_RED_DIAG_2_T4	M235	0.213	21.15	0.57	48.02	1.2%	Pass
TWR_RED_DIAG_2_T4	M244	0.066	21.15	0.32	48.02	0.7%	Pass
TWR_RED_DIAG_2_T4	M252	0.083	21.15	0.37	48.02	0.8%	Pass
TWR_RED_DIAG_2_T4	M261	0.143	21.15	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T4	M269	0.144	21.15	0.51	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M291	0.299	21.54	0.45	48.02	1.4%	Pass
TWR_RED_DIAG_2_T5	M299	0.312	21.54	0.48	48.02	1.4%	Pass
TWR_RED_DIAG_2_T5	M308	0.115	21.54	0.46	48.02	1.0%	Pass
TWR_RED_DIAG_2_T5	M316	0.156	21.54	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M325	0.295	21.54	0.44	48.02	1.4%	Pass
TWR_RED_DIAG_2_T5	M333	0.245	21.54	0.41	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M342	0.17	21.54	0.55	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M350	0.148	21.54	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T6	M372	0.467	21.58	0.54	48.02	2.2%	Pass
TWR_RED_DIAG_2_T6	M380	0.518	21.58	0.59	48.02	2.4%	Pass
TWR_RED_DIAG_2_T6	M389	0.039	21.58	0.38	48.02	0.8%	Pass
TWR_RED_DIAG_2_T6	M397	0.117	21.58	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T6	M406	0.529	21.58	0.60	48.02	2.5%	Pass

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TWR_RED_DIAG_2_T6	M414	0.463	21.58	0.56	48.02	2.1%	Pass
TWR_RED_DIAG_2_T6	M423	0.14	21.58	0.52	48.02	1.1%	Pass
TWR_RED_DIAG_2_T6	M431	0.074	21.58	0.41	48.02	0.9%	Pass
TWR_RED_DIAG_2_T7	M453	1.11	21.97	0.91	48.02	5.1%	Pass
TWR_RED_DIAG_2_T7	M461	1.191	21.97	0.98	48.02	5.4%	Pass
TWR_RED_DIAG_2_T7	M470	0.106	21.97	0.42	48.02	0.9%	Pass
TWR_RED_DIAG_2_T7	M478	0.175	21.97	0.47	48.02	1.0%	Pass
TWR_RED_DIAG_2_T7	M487	1.152	21.97	1.00	48.02	5.2%	Pass
TWR_RED_DIAG_2_T7	M495	1.075	21.97	0.93	48.02	4.9%	Pass
TWR_RED_DIAG_2_T7	M504	0.174	21.97	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T7	M512	0.114	21.97	0.43	48.02	0.9%	Pass
TWR_RED_DIAG_2_T8	M534	1.427	22.02	1.26	48.02	6.5%	Pass
TWR_RED_DIAG_2_T8	M542	1.503	22.02	1.32	48.02	6.8%	Pass
TWR_RED_DIAG_2_T8	M551	0.156	22.02	0.60	48.02	1.3%	Pass
TWR_RED_DIAG_2_T8	M559	0.233	22.02	0.67	48.02	1.4%	Pass
TWR_RED_DIAG_2_T8	M568	1.499	22.02	1.35	48.02	6.8%	Pass
TWR_RED_DIAG_2_T8	M576	1.399	22.02	1.29	48.02	6.4%	Pass
TWR_RED_DIAG_2_T8	M585	0.244	22.02	0.71	48.02	1.5%	Pass
TWR_RED_DIAG_2_T8	M593	0.169	22.02	0.64	48.02	1.3%	Pass
TWR_RED_DIAG_2_T9	M615	2.103	22.06	1.65	48.02	9.5%	Pass
TWR_RED_DIAG_2_T9	M623	2.163	22.06	1.72	48.02	9.8%	Pass
TWR_RED_DIAG_2_T9	M632	0.506	22.06	0.73	48.02	2.3%	Pass
TWR_RED_DIAG_2_T9	M640	0.556	22.06	0.75	48.02	2.5%	Pass
TWR_RED_DIAG_2_T9	M649	2.177	22.06	1.75	48.02	9.9%	Pass
TWR_RED_DIAG_2_T9	M657	2.079	22.06	1.68	48.02	9.4%	Pass
TWR_RED_DIAG_2_T9	M666	0.557	22.06	0.77	48.02	2.5%	Pass
TWR_RED_DIAG_2_T9	M674	0.525	22.06	0.74	48.02	2.4%	Pass
TWR_RED_DIAG_2_T10	M696	0.455	31.45	1.43	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M706	0.457	31.45	1.41	63.37	2.2%	Pass
TWR_RED_DIAG_2_T10	M717	0.359	30.71	1.17	63.37	1.8%	Pass
TWR_RED_DIAG_2_T10	M727	0.362	30.71	1.24	63.37	2.0%	Pass
TWR_RED_DIAG_2_T10	M738	0.435	31.45	1.43	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M748	0.426	31.45	1.42	63.37	2.2%	Pass
TWR_RED_DIAG_2_T10	M759	0.359	30.71	1.27	63.37	2.0%	Pass
TWR_RED_DIAG_2_T10	M769	0.358	30.71	1.21	63.37	1.9%	Pass
TWR_RED_DIAG_3_T2	M57	2.369	21.11	0.00	48.02	11.2%	Pass
TWR_RED_DIAG_3_T2	M58	1.355	39.66	0.10	48.02	3.4%	Pass
TWR_RED_DIAG_3_T2	M65	2.421	21.11	0.00	48.02	11.5%	Pass
TWR_RED_DIAG_3_T2	M66	1.378	39.66	0.09	48.02	3.5%	Pass
TWR_RED_DIAG_3_T2	M73	2.644	21.11	0.00	48.02	12.5%	Pass
TWR_RED_DIAG_3_T2	M74	1.481	39.66	0.21	48.02	3.7%	Pass
TWR_RED_DIAG_3_T2	M81	2.628	21.11	0.00	48.02	12.4%	Pass
TWR_RED_DIAG_3_T2	M82	1.477	39.66	0.21	48.02	3.7%	Pass
TWR_RED_DIAG_3_T2	M89	2.385	21.11	0.00	48.02	11.3%	Pass
TWR_RED_DIAG_3_T2	M90	1.344	39.66	0.08	48.02	3.4%	Pass
TWR_RED_DIAG_3_T2	M97	2.329	21.11	0.00	48.02	11.0%	Pass
TWR_RED_DIAG_3_T2	M98	1.32	39.66	0.09	48.02	3.3%	Pass
TWR_RED_DIAG_3_T2	M105	2.541	21.11	0.00	48.02	12.0%	Pass
TWR_RED_DIAG_3_T2	M106	1.393	39.66	0.06	48.02	3.5%	Pass
TWR_RED_DIAG_3_T2	M113	2.56	21.11	0.00	48.02	12.1%	Pass
TWR_RED_DIAG_3_T2	M114	1.4	39.66	0.07	48.02	3.5%	Pass
TWR_RED_DIAG_3_T3	M130	0.758	21.11	0.30	48.02	3.6%	Pass
TWR_RED_DIAG_3_T3	M131	0.417	39.66	0.33	48.02	1.1%	Pass
TWR_RED_DIAG_3_T3	M138	0.777	21.11	0.30	48.02	3.7%	Pass

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TWR_RED_DIAG_3_T3	M139	0.465	39.66	0.30	48.02	1.2%	Pass
TWR_RED_DIAG_3_T3	M147	0.807	21.11	0.19	48.02	3.8%	Pass
TWR_RED_DIAG_3_T3	M148	0.383	39.66	0.31	48.02	1.0%	Pass
TWR_RED_DIAG_3_T3	M155	0.777	21.11	0.21	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M156	0.349	39.66	0.34	48.02	0.9%	Pass
TWR_RED_DIAG_3_T3	M164	0.601	21.11	0.15	48.02	2.8%	Pass
TWR_RED_DIAG_3_T3	M165	0.311	39.66	0.22	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M172	0.632	21.11	0.14	48.02	3.0%	Pass
TWR_RED_DIAG_3_T3	M173	0.3	39.66	0.22	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M181	0.788	21.11	0.19	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M182	0.334	39.66	0.34	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M189	0.773	21.11	0.19	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M190	0.337	39.66	0.34	48.02	0.8%	Pass
TWR_RED_DIAG_3_T4	M211	0.578	21.15	0.17	48.02	2.7%	Pass
TWR_RED_DIAG_3_T4	M212	0.345	39.73	0.21	48.02	0.9%	Pass
TWR_RED_DIAG_3_T4	M219	0.554	21.15	0.16	48.02	2.6%	Pass
TWR_RED_DIAG_3_T4	M220	0.38	39.73	0.15	48.02	1.0%	Pass
TWR_RED_DIAG_3_T4	M228	0.739	21.15	0.04	48.02	3.5%	Pass
TWR_RED_DIAG_3_T4	M229	0.269	39.73	0.17	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M236	0.72	21.15	0.10	48.02	3.4%	Pass
TWR_RED_DIAG_3_T4	M237	0.269	39.73	0.25	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M245	0.471	21.15	0.02	48.02	2.2%	Pass
TWR_RED_DIAG_3_T4	M246	0.301	39.73	0.10	48.02	0.8%	Pass
TWR_RED_DIAG_3_T4	M253	0.542	21.15	0.04	48.02	2.6%	Pass
TWR_RED_DIAG_3_T4	M254	0.272	39.73	0.12	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M262	0.734	21.15	0.05	48.02	3.5%	Pass
TWR_RED_DIAG_3_T4	M263	0.231	39.73	0.23	48.02	0.6%	Pass
TWR_RED_DIAG_3_T4	M270	0.687	21.15	0.00	48.02	3.2%	Pass
TWR_RED_DIAG_3_T4	M271	0.19	39.73	0.17	48.02	0.5%	Pass
TWR_RED_DIAG_3_T5	M292	0.753	21.54	0.45	48.02	3.5%	Pass
TWR_RED_DIAG_3_T5	M293	0.564	40.35	0.35	48.02	1.4%	Pass
TWR_RED_DIAG_3_T5	M300	0.768	21.54	0.50	48.02	3.6%	Pass
TWR_RED_DIAG_3_T5	M301	0.655	40.35	0.33	48.02	1.6%	Pass
TWR_RED_DIAG_3_T5	M309	0.631	21.54	0.11	48.02	2.9%	Pass
TWR_RED_DIAG_3_T5	M310	0.342	40.35	0.19	48.02	0.8%	Pass
TWR_RED_DIAG_3_T5	M317	0.733	21.54	0.22	48.02	3.4%	Pass
TWR_RED_DIAG_3_T5	M318	0.38	40.35	0.31	48.02	0.9%	Pass
TWR_RED_DIAG_3_T5	M326	0.65	21.54	0.35	48.02	3.0%	Pass
TWR_RED_DIAG_3_T5	M327	0.494	40.35	0.29	48.02	1.2%	Pass
TWR_RED_DIAG_3_T5	M334	0.644	21.54	0.30	48.02	3.0%	Pass
TWR_RED_DIAG_3_T5	M335	0.457	40.35	0.28	48.02	1.1%	Pass
TWR_RED_DIAG_3_T5	M343	0.759	21.54	0.22	48.02	3.5%	Pass
TWR_RED_DIAG_3_T5	M344	0.376	40.35	0.33	48.02	0.9%	Pass
TWR_RED_DIAG_3_T5	M351	0.635	21.54	0.13	48.02	2.9%	Pass
TWR_RED_DIAG_3_T5	M352	0.31	40.35	0.24	48.02	0.8%	Pass
TWR_RED_DIAG_3_T6	M373	0.786	21.58	0.61	48.02	3.6%	Pass
TWR_RED_DIAG_3_T6	M374	0.725	40.42	0.39	48.02	1.8%	Pass
TWR_RED_DIAG_3_T6	M381	0.842	21.58	0.70	48.02	3.9%	Pass
TWR_RED_DIAG_3_T6	M382	0.844	40.42	0.39	48.02	2.1%	Pass
TWR_RED_DIAG_3_T6	M390	0.606	21.58	0.14	48.02	2.8%	Pass
TWR_RED_DIAG_3_T6	M391	0.416	40.42	0.18	48.02	1.0%	Pass
TWR_RED_DIAG_3_T6	M398	0.697	21.58	0.25	48.02	3.2%	Pass
TWR_RED_DIAG_3_T6	M399	0.448	40.42	0.28	48.02	1.1%	Pass
TWR_RED_DIAG_3_T6	M407	0.837	21.58	0.67	48.02	3.9%	Pass
TWR_RED_DIAG_3_T6	M408	0.771	40.42	0.43	48.02	1.9%	Pass
TWR_RED_DIAG_3_T6	M415	0.807	21.58	0.58	48.02	3.7%	Pass
TWR_RED_DIAG_3_T6	M416	0.7	40.42	0.40	48.02	1.7%	Pass
TWR_RED_DIAG_3_T6	M424	0.744	21.58	0.26	48.02	3.4%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_DIAG_3_T6	M425	0.452	40.42	0.32	48.02	1.1%	Pass
TWR_RED_DIAG_3_T6	M432	0.633	21.58	0.16	48.02	2.9%	Pass
TWR_RED_DIAG_3_T6	M433	0.381	40.42	0.24	48.02	0.9%	Pass
TWR_RED_DIAG_3_T7	M454	1.083	21.97	0.97	48.02	4.9%	Pass
TWR_RED_DIAG_3_T7	M455	1.02	41.04	0.60	48.02	2.5%	Pass
TWR_RED_DIAG_3_T7	M462	1.149	21.97	1.10	48.02	5.2%	Pass
TWR_RED_DIAG_3_T7	M463	1.163	41.04	0.61	48.02	2.8%	Pass
TWR_RED_DIAG_3_T7	M471	0.782	21.97	0.40	48.02	3.6%	Pass
TWR_RED_DIAG_3_T7	M472	0.626	41.04	0.31	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M479	0.816	21.97	0.44	48.02	3.7%	Pass
TWR_RED_DIAG_3_T7	M480	0.613	41.04	0.37	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M488	1.148	21.97	1.06	48.02	5.2%	Pass
TWR_RED_DIAG_3_T7	M489	1.079	41.04	0.65	48.02	2.6%	Pass
TWR_RED_DIAG_3_T7	M496	1.107	21.97	0.94	48.02	5.0%	Pass
TWR_RED_DIAG_3_T7	M497	0.991	41.04	0.61	48.02	2.4%	Pass
TWR_RED_DIAG_3_T7	M505	0.843	21.97	0.42	48.02	3.8%	Pass
TWR_RED_DIAG_3_T7	M506	0.609	41.04	0.39	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M513	0.78	21.97	0.38	48.02	3.6%	Pass
TWR_RED_DIAG_3_T7	M514	0.563	41.04	0.35	48.02	1.4%	Pass
TWR_RED_DIAG_3_T8	M535	1.476	22.02	1.39	48.02	6.7%	Pass
TWR_RED_DIAG_3_T8	M536	1.326	41.11	0.89	48.02	3.2%	Pass
TWR_RED_DIAG_3_T8	M543	1.53	22.02	1.52	48.02	6.9%	Pass
TWR_RED_DIAG_3_T8	M544	1.472	41.11	0.89	48.02	3.6%	Pass
TWR_RED_DIAG_3_T8	M552	1.038	22.02	0.66	48.02	4.7%	Pass
TWR_RED_DIAG_3_T8	M553	0.828	41.11	0.50	48.02	2.0%	Pass
TWR_RED_DIAG_3_T8	M560	1.054	22.02	0.67	48.02	4.8%	Pass
TWR_RED_DIAG_3_T8	M561	0.787	41.11	0.55	48.02	1.9%	Pass
TWR_RED_DIAG_3_T8	M569	1.537	22.02	1.45	48.02	7.0%	Pass
TWR_RED_DIAG_3_T8	M570	1.371	41.11	0.94	48.02	3.3%	Pass
TWR_RED_DIAG_3_T8	M577	1.506	22.02	1.34	48.02	6.8%	Pass
TWR_RED_DIAG_3_T8	M578	1.287	41.11	0.91	48.02	3.1%	Pass
TWR_RED_DIAG_3_T8	M586	1.082	22.02	0.65	48.02	4.9%	Pass
TWR_RED_DIAG_3_T8	M587	0.76	41.11	0.57	48.02	1.8%	Pass
TWR_RED_DIAG_3_T8	M594	1.038	22.02	0.63	48.02	4.7%	Pass
TWR_RED_DIAG_3_T8	M595	0.755	41.11	0.54	48.02	1.8%	Pass
TWR_RED_DIAG_3_T9	M616	1.888	22.06	2.01	48.02	8.6%	Pass
TWR_RED_DIAG_3_T9	M617	1.775	41.17	1.19	48.02	4.3%	Pass
TWR_RED_DIAG_3_T9	M624	1.942	22.06	2.14	48.02	8.8%	Pass
TWR_RED_DIAG_3_T9	M625	1.922	41.17	1.19	48.02	4.7%	Pass
TWR_RED_DIAG_3_T9	M633	1.273	22.06	1.05	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M634	1.129	41.17	0.70	48.02	2.7%	Pass
TWR_RED_DIAG_3_T9	M641	1.284	22.06	1.05	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M642	1.079	41.17	0.74	48.02	2.6%	Pass
TWR_RED_DIAG_3_T9	M650	1.958	22.06	2.06	48.02	8.9%	Pass
TWR_RED_DIAG_3_T9	M651	1.811	41.17	1.24	48.02	4.4%	Pass

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TWR_RED_DIAG_3_T9	M658	1.92	22.06	1.94	48.02	8.7%	Pass
TWR_RED_DIAG_3_T9	M659	1.726	41.17	1.22	48.02	4.2%	Pass
TWR_RED_DIAG_3_T9	M667	1.315	22.06	1.01	48.02	6.0%	Pass
TWR_RED_DIAG_3_T9	M668	1.046	41.17	0.76	48.02	2.5%	Pass
TWR_RED_DIAG_3_T9	M675	1.278	22.06	1.01	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M676	1.051	41.17	0.74	48.02	2.6%	Pass
TWR_RED_DIAG_3_T10	M698	0.577	19.80	1.56	63.37	2.9%	Pass
TWR_RED_DIAG_3_T10	M708	0.594	19.80	1.55	63.37	3.0%	Pass
TWR_RED_DIAG_3_T10	M719	0.537	19.40	1.24	63.37	2.8%	Pass
TWR_RED_DIAG_3_T10	M729	0.535	19.40	1.33	63.37	2.8%	Pass
TWR_RED_DIAG_3_T10	M740	0.543	19.80	1.55	63.37	2.7%	Pass
TWR_RED_DIAG_3_T10	M750	0.529	19.80	1.54	63.37	2.7%	Pass
TWR_RED_DIAG_3_T10	M761	0.53	18.63	1.35	63.37	2.8%	Pass
TWR_RED_DIAG_3_T10	M771	0.531	19.40	1.27	63.37	2.7%	Pass
TWR_RED_DIAG_4_T10	M699	2.063	28.05	1.46	63.37	7.4%	Pass
TWR_RED_DIAG_4_T10	M700	1.708	48.66	1.25	63.37	3.5%	Pass
TWR_RED_DIAG_4_T10	M709	2.086	28.05	1.53	63.37	7.4%	Pass
TWR_RED_DIAG_4_T10	M710	1.764	48.66	1.28	63.37	3.6%	Pass
TWR_RED_DIAG_4_T10	M720	1.628	28.68	0.90	63.37	5.7%	Pass
TWR_RED_DIAG_4_T10	M721	1.27	47.73	0.93	63.37	2.7%	Pass
TWR_RED_DIAG_4_T10	M730	1.646	28.68	0.88	63.37	5.7%	Pass
TWR_RED_DIAG_4_T10	M731	1.258	47.73	0.93	63.37	2.6%	Pass
TWR_RED_DIAG_4_T10	M741	2.125	28.05	1.50	63.37	7.6%	Pass
TWR_RED_DIAG_4_T10	M742	1.742	48.66	1.30	63.37	3.6%	Pass
TWR_RED_DIAG_4_T10	M751	2.088	28.05	1.45	63.37	7.4%	Pass
TWR_RED_DIAG_4_T10	M752	1.691	48.66	1.27	63.37	3.5%	Pass
TWR_RED_DIAG_4_T10	M762	1.671	28.68	0.87	63.37	5.8%	Pass
TWR_RED_DIAG_4_T10	M763	1.239	47.73	0.94	63.37	2.6%	Pass
TWR_RED_DIAG_4_T10	M772	1.67	28.68	0.87	63.37	5.8%	Pass
TWR_RED_DIAG_4_T10	M773	1.248	47.73	0.95	63.37	2.6%	Pass
TWR_RED_DIAG_T1	M17	1.105	5.33	0.73	24.08	20.7%	Pass
TWR_RED_DIAG_T1	M20	1.125	5.33	0.72	24.08	21.1%	Pass
TWR_RED_DIAG_T1	M24	0.947	5.33	0.55	24.08	17.8%	Pass
TWR_RED_DIAG_T1	M27	0.931	5.33	0.56	24.08	17.5%	Pass
TWR_RED_DIAG_T1	M31	1.067	5.33	0.66	24.08	20.0%	Pass
TWR_RED_DIAG_T1	M34	1.044	5.33	0.68	24.08	19.6%	Pass
TWR_RED_DIAG_T1	M38	0.789	5.33	0.41	24.08	14.8%	Pass
TWR_RED_DIAG_T1	M41	0.798	5.33	0.40	24.08	15.0%	Pass
TWR_RED_DIAG_T2	M54	0.249	14.93	0.02	30.21	1.7%	Pass
TWR_RED_DIAG_T2	M62	0.304	14.93	0.01	30.21	2.0%	Pass
TWR_RED_DIAG_T2	M70	0.038	14.93	0.08	30.21	0.3%	Pass
TWR_RED_DIAG_T2	M78	0.053	14.93	0.10	30.21	0.4%	Pass
TWR_RED_DIAG_T2	M86	0.288	14.93	0.07	30.21	1.9%	Pass
TWR_RED_DIAG_T2	M94	0.231	14.93	0.08	30.21	1.5%	Pass
TWR_RED_DIAG_T2	M102	0.052	14.93	0.13	30.21	0.4%	Pass
TWR_RED_DIAG_T2	M110	0.028	14.93	0.11	30.21	0.4%	Pass
TWR_RED_DIAG_T3	M127	0.678	14.93	0.07	30.21	4.5%	Pass
TWR_RED_DIAG_T3	M135	0.793	14.93	0.10	30.21	5.3%	Pass
TWR_RED_DIAG_T3	M144	0.34	14.93	0.18	30.21	2.3%	Pass
TWR_RED_DIAG_T3	M152	0.386	14.93	0.25	30.21	2.6%	Pass
TWR_RED_DIAG_T3	M161	0.681	14.93	0.08	30.21	4.6%	Pass
TWR_RED_DIAG_T3	M169	0.588	14.93	0.12	30.21	3.9%	Pass
TWR_RED_DIAG_T3	M178	0.384	14.93	0.30	30.21	2.6%	Pass
TWR_RED_DIAG_T3	M186	0.318	14.93	0.20	30.21	2.1%	Pass
TWR_RED_DIAG_T4	M208	1.067	14.97	0.39	30.21	7.1%	Pass

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TWR_RED_DIAG_T4	M216	1.213	14.97	0.41	30.21	8.1%	Pass
TWR_RED_DIAG_T4	M225	0.453	14.97	0.21	30.21	3.0%	Pass
TWR_RED_DIAG_T4	M233	0.494	14.97	0.31	30.21	3.3%	Pass
TWR_RED_DIAG_T4	M242	1.165	14.97	0.45	30.21	7.8%	Pass
TWR_RED_DIAG_T4	M250	1.02	14.97	0.41	30.21	6.8%	Pass
TWR_RED_DIAG_T4	M259	0.492	14.97	0.37	30.21	3.3%	Pass
TWR_RED_DIAG_T4	M267	0.427	14.97	0.28	30.21	2.9%	Pass
TWR_RED_DIAG_T5	M289	1.937	15.54	0.92	30.21	12.5%	Pass
TWR_RED_DIAG_T5	M297	2.099	15.54	0.93	30.21	13.5%	Pass
TWR_RED_DIAG_T5	M306	1.048	15.54	0.61	30.21	6.7%	Pass
TWR_RED_DIAG_T5	M314	1.059	15.54	0.68	30.21	6.8%	Pass
TWR_RED_DIAG_T5	M323	2.037	15.54	0.98	30.21	13.1%	Pass
TWR_RED_DIAG_T5	M331	1.871	15.54	0.95	30.21	12.0%	Pass
TWR_RED_DIAG_T5	M340	1.034	15.54	0.74	30.21	6.7%	Pass
TWR_RED_DIAG_T5	M348	1.023	15.54	0.69	30.21	6.6%	Pass
TWR_RED_DIAG_T6	M370	2.738	15.58	1.51	30.21	17.6%	Pass
TWR_RED_DIAG_T6	M378	2.948	15.58	1.54	30.21	18.9%	Pass
TWR_RED_DIAG_T6	M387	1.527	15.58	0.84	30.21	9.8%	Pass
TWR_RED_DIAG_T6	M395	1.487	15.58	0.87	30.21	9.5%	Pass
TWR_RED_DIAG_T6	M404	2.887	15.58	1.59	30.21	18.5%	Pass
TWR_RED_DIAG_T6	M412	2.671	15.58	1.54	30.21	17.1%	Pass
TWR_RED_DIAG_T6	M421	1.423	15.58	0.90	30.21	9.1%	Pass
TWR_RED_DIAG_T6	M429	1.466	15.58	0.90	30.21	9.4%	Pass
TWR_RED_DIAG_T7	M451	3.543	16.23	2.15	30.21	21.8%	Pass
TWR_RED_DIAG_T7	M459	3.781	16.23	2.21	30.21	23.3%	Pass
TWR_RED_DIAG_T7	M468	2.272	16.23	1.37	30.21	14.0%	Pass
TWR_RED_DIAG_T7	M476	2.167	16.23	1.34	30.21	13.3%	Pass
TWR_RED_DIAG_T7	M485	3.706	16.23	2.27	30.21	22.8%	Pass
TWR_RED_DIAG_T7	M493	3.462	16.23	2.19	30.21	21.3%	Pass
TWR_RED_DIAG_T7	M502	2.093	16.23	1.38	30.21	12.9%	Pass
TWR_RED_DIAG_T7	M510	2.199	16.23	1.43	30.21	13.5%	Pass
TWR_RED_DIAG_T8	M532	4.466	16.28	2.92	30.21	27.4%	Pass
TWR_RED_DIAG_T8	M540	4.67	16.28	2.94	30.21	28.7%	Pass
TWR_RED_DIAG_T8	M549	2.827	16.28	1.85	30.21	17.4%	Pass
TWR_RED_DIAG_T8	M557	2.724	16.28	1.85	30.21	16.7%	Pass
TWR_RED_DIAG_T8	M566	4.579	16.28	3.02	30.21	28.1%	Pass
TWR_RED_DIAG_T8	M574	4.358	16.28	2.96	30.21	26.8%	Pass
TWR_RED_DIAG_T8	M583	2.637	16.28	1.93	30.21	16.2%	Pass
TWR_RED_DIAG_T8	M591	2.75	16.28	2.00	30.21	16.9%	Pass
TWR_RED_DIAG_T9	M613	5.71	16.38	3.67	30.21	34.9%	Pass
TWR_RED_DIAG_T9	M621	5.885	16.38	3.71	30.21	35.9%	Pass
TWR_RED_DIAG_T9	M630	4.088	16.38	2.53	30.21	25.0%	Pass
TWR_RED_DIAG_T9	M638	3.95	16.38	2.49	30.21	24.1%	Pass
TWR_RED_DIAG_T9	M647	5.817	16.38	3.80	30.21	35.5%	Pass
TWR_RED_DIAG_T9	M655	5.603	16.38	3.73	30.21	34.2%	Pass
TWR_RED_DIAG_T9	M664	3.861	16.38	2.53	30.21	23.6%	Pass
TWR_RED_DIAG_T9	M672	4.023	16.38	2.61	30.21	24.6%	Pass
TWR_RED_DIAG_T10	M694	1.238	16.05	1.67	30.21	7.7%	Pass
TWR_RED_DIAG_T10	M704	1.27	16.05	1.65	30.21	7.9%	Pass
TWR_RED_DIAG_T10	M715	0.422	15.61	1.16	30.21	3.8%	Pass
TWR_RED_DIAG_T10	M725	0.474	15.61	1.20	30.21	4.0%	Pass
TWR_RED_DIAG_T10	M736	1.287	16.05	1.73	30.21	8.0%	Pass
TWR_RED_DIAG_T10	M746	1.233	16.05	1.71	30.21	7.7%	Pass
TWR_RED_DIAG_T10	M757	0.484	15.61	1.23	30.21	4.1%	Pass
TWR_RED_DIAG_T10	M767	0.443	15.61	1.21	30.21	4.0%	Pass
TWR_RED_HIPDIA_1_T10	M807	0.353	19.46	0.13	60.42	1.8%	Pass
TWR_RED_HIPDIA_1_T10	M808	0.349	19.78	0.12	60.42	1.8%	Pass
TWR_RED_HIPDIA_1_T10	M809	0.346	19.78	0.10	60.42	1.7%	Pass
TWR_RED_HIPDIA_1_T10	M810	0.33	19.46	0.13	60.42	1.7%	Pass
TWR_RED_HIPDIA_1_T10	M811	0.329	19.46	0.08	60.42	1.7%	Pass

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TAG0053 - CHESHIRE

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_1_T10	M812	0.298	19.78	0.10	60.42	1.5%	Pass
TWR_RED_HIPDIA_1_T10	M813	0.299	19.78	0.12	60.42	1.5%	Pass
TWR_RED_HIPDIA_1_T10	M814	0.351	19.46	0.08	60.42	1.8%	Pass
TWR_RED_HIPDIA_2_T2	M1246	1.534	14.70	0.00	48.02	10.4%	Pass
TWR_RED_HIPDIA_2_T2	M1247	1.533	14.70	0.00	48.02	10.4%	Pass
TWR_RED_HIPDIA_2_T2	M1248	1.539	14.70	0.00	48.02	10.5%	Pass
TWR_RED_HIPDIA_2_T2	M1249	1.537	14.70	0.00	48.02	10.5%	Pass
TWR_RED_HIPDIA_2_T2	M1250	1.537	14.70	0.00	48.02	10.5%	Pass
TWR_RED_HIPDIA_2_T2	M1251	1.538	14.70	0.00	48.02	10.5%	Pass
TWR_RED_HIPDIA_2_T2	M1252	1.532	14.70	0.00	48.02	10.4%	Pass
TWR_RED_HIPDIA_2_T2	M1253	1.531	14.70	0.00	48.02	10.4%	Pass
TWR_RED_HIPDIA_2_T3	M1194	0.609	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1195	0.61	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1196	0.597	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1197	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1198	0.609	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1199	0.61	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1200	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1201	0.604	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1142	0.609	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1143	0.61	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1144	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1145	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1146	0.609	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1147	0.611	14.70	0.00	48.02	4.2%	Pass
TWR_RED_HIPDIA_2_T4	M1148	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1149	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1090	0.61	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1091	0.61	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1092	0.597	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1093	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1094	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1095	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1096	0.609	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1097	0.611	14.70	0.00	48.02	4.2%	Pass
TWR_RED_HIPDIA_2_T6	M1038	0.587	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1039	0.586	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1040	0.599	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T6	M1041	0.602	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T6	M1042	0.595	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1043	0.595	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1044	0.599	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T6	M1045	0.601	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M986	0.599	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M987	0.602	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M988	0.587	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M989	0.586	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M990	0.599	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M991	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M992	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T7	M993	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T8	M934	0.599	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T8	M935	0.602	14.70	0.00	48.02	4.1%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_2_T8	M936	0.587	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M937	0.586	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M938	0.598	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T8	M939	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T8	M940	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T8	M941	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_3_T10	M815	0.966	15.58	0.00	60.42	6.2%	Pass
TWR_RED_HIPDIA_3_T10	M816	0.888	15.99	0.00	60.42	5.6%	Pass
TWR_RED_HIPDIA_3_T10	M817	0.87	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M818	0.944	15.58	0.00	60.42	6.1%	Pass
TWR_RED_HIPDIA_3_T10	M819	0.952	15.58	0.00	60.42	6.1%	Pass
TWR_RED_HIPDIA_3_T10	M820	0.867	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M821	0.865	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M822	0.952	15.58	0.00	60.42	6.1%	Pass
TWR_RED_HIPDIA_T2	M1238	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1239	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1240	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1241	0.128	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1242	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1243	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1244	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1245	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1186	0.134	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1187	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1188	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1189	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1190	0.132	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1191	0.127	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1192	0.13	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1193	0.134	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T4	M1134	0.153	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1135	0.148	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1136	0.15	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1137	0.143	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1138	0.147	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1139	0.151	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1140	0.147	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1141	0.147	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1082	0.157	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1083	0.148	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1084	0.16	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1085	0.153	21.53	0.02	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1086	0.152	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1087	0.154	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1088	0.157	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1089	0.152	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T6	M1030	0.195	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1031	0.183	21.53	0.05	48.02	0.8%	Pass
TWR_RED_HIPDIA_T6	M1032	0.202	21.53	0.05	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1033	0.193	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1034	0.188	21.53	0.05	48.02	0.9%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_T6	M1035	0.191	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1036	0.194	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1037	0.187	21.53	0.05	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M978	0.211	21.53	0.05	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M979	0.196	21.53	0.07	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M980	0.219	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M981	0.207	21.53	0.07	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M982	0.199	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M983	0.208	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M984	0.201	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M985	0.205	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M926	0.237	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M927	0.217	21.53	0.09	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M928	0.248	21.53	0.09	48.02	1.2%	Pass
TWR_RED_HIPDIA_T8	M929	0.232	21.53	0.10	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M930	0.222	21.53	0.08	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M931	0.228	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M932	0.232	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M933	0.22	21.53	0.09	48.02	1.0%	Pass
TWR_RED_HIPDIA_T9	M874	0.324	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M875	0.314	21.53	0.18	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M876	0.326	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M877	0.318	21.53	0.18	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M878	0.313	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M879	0.315	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M880	0.311	21.53	0.17	48.02	1.4%	Pass
TWR_RED_HIPDIA_T9	M881	0.316	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIP_1_T10	M799	0.061	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M800	0.054	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M801	0.061	218.03	0.05	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M806	0.06	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_2_T2	M1234	0	8.69	1.40	48.02	2.9%	Pass
TWR_RED_HIP_2_T2	M1235	0	8.69	1.40	48.02	2.9%	Pass
TWR_RED_HIP_2_T2	M1236	0	8.69	1.40	48.02	2.9%	Pass
TWR_RED_HIP_2_T2	M1237	0	8.69	1.40	48.02	2.9%	Pass
TWR_RED_HIP_2_T3	M1182	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T3	M1183	0	8.69	0.46	48.02	0.9%	Pass
TWR_RED_HIP_2_T3	M1184	0	8.69	0.47	48.02	1.0%	Pass
TWR_RED_HIP_2_T3	M1185	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T4	M1130	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T4	M1131	0	8.69	0.46	48.02	1.0%	Pass
TWR_RED_HIP_2_T4	M1132	0	8.69	0.44	48.02	0.9%	Pass
TWR_RED_HIP_2_T4	M1133	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1078	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1079	0	8.69	0.44	48.02	0.9%	Pass
TWR_RED_HIP_2_T5	M1080	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1081	0	8.69	0.46	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1026	0	8.69	0.43	48.02	0.9%	Pass
TWR_RED_HIP_2_T6	M1027	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1028	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1029	0	8.69	0.44	48.02	0.9%	Pass
TWR_RED_HIP_2_T7	M974	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T7	M975	0	8.69	0.44	48.02	0.9%	Pass
TWR_RED_HIP_2_T7	M976	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T7	M977	0	8.69	0.45	48.02	0.9%	Pass
TWR_RED_HIP_2_T8	M922	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T8	M923	0	8.69	0.47	48.02	1.0%	Pass
TWR_RED_HIP_2_T8	M924	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T8	M925	0	8.69	0.45	48.02	0.9%	Pass
TWR_RED_HIP_2_T9	M870	0	8.69	0.48	48.02	1.0%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIP_2_T9	M871	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T9	M872	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T9	M873	0	8.69	0.49	48.02	1.0%	Pass
TWR_RED_HIP_3_T10	M802	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M803	0	15.14	0.56	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M804	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M805	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_T2	M1230	0	34.59	0.10	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1231	0	34.59	0.10	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1232	0	34.59	0.10	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1233	0	34.59	0.10	48.02	0.2%	Pass
TWR_RED_HIP_T3	M1178	0	34.59	0.12	48.02	0.3%	Pass
TWR_RED_HIP_T3	M1179	0	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T3	M1180	0	34.59	0.12	48.02	0.3%	Pass
TWR_RED_HIP_T3	M1181	0	34.59	0.12	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1126	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1127	0	34.59	0.17	48.02	0.4%	Pass
TWR_RED_HIP_T4	M1128	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1129	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1074	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1075	0	34.59	0.16	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1076	0	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1077	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1022	0.01	34.59	0.16	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1023	0	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T6	M1024	0.007	34.59	0.16	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1025	0.01	34.59	0.17	48.02	0.3%	Pass
TWR_RED_HIP_T7	M970	0.007	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T7	M971	0	34.59	0.16	48.02	0.3%	Pass
TWR_RED_HIP_T7	M972	0.005	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T7	M973	0.007	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T8	M918	0.071	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T8	M919	0.059	34.59	0.20	48.02	0.4%	Pass
TWR_RED_HIP_T8	M920	0.069	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T8	M921	0.071	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T9	M866	0.086	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HIP_T9	M867	0.086	34.59	0.20	48.02	0.4%	Pass
TWR_RED_HIP_T9	M868	0.084	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HIP_T9	M869	0.075	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HORZ_0_T10	M783	6.605	27.51	9.15	24.04	38.0%	Pass
TWR_RED_HORZ_0_T10	M784	4.712	27.51	6.48	24.04	26.9%	Pass
TWR_RED_HORZ_0_T10	M785	6.573	27.51	8.89	24.04	37.0%	Pass
TWR_RED_HORZ_0_T10	M786	4.804	27.51	6.40	24.04	26.6%	Pass
TWR_RED_HORZ_0_T10	M787	4.943	27.51	6.65	24.04	27.7%	Pass
TWR_RED_HORZ_0_T10	M788	6.309	27.51	8.87	24.04	36.9%	Pass
TWR_RED_HORZ_0_T10	M789	4.754	27.51	6.64	24.04	27.6%	Pass
TWR_RED_HORZ_0_T10	M790	6.217	27.51	9.00	24.04	37.4%	Pass
TWR_RED_HORZ_2_T1	M1262	0.435	13.33	0.89	48.02	3.3%	Pass
TWR_RED_HORZ_2_T1	M1263	0.026	13.33	0.44	48.02	0.9%	Pass
TWR_RED_HORZ_2_T1	M1264	0.451	13.33	0.87	48.02	3.4%	Pass
TWR_RED_HORZ_2_T1	M1265	0	13.33	0.49	48.02	1.0%	Pass
TWR_RED_HORZ_2_T2	M53	0.874	32.85	0.83	48.02	2.7%	Pass
TWR_RED_HORZ_2_T2	M61	0.873	32.85	0.84	48.02	2.7%	Pass
TWR_RED_HORZ_2_T2	M69	1.254	32.85	1.18	48.02	3.8%	Pass
TWR_RED_HORZ_2_T2	M77	1.252	32.85	1.17	48.02	3.8%	Pass
TWR_RED_HORZ_2_T2	M85	0.983	32.85	0.94	48.02	3.0%	Pass
TWR_RED_HORZ_2_T2	M93	0.987	32.85	0.94	48.02	3.0%	Pass
TWR_RED_HORZ_2_T2	M101	0.94	32.85	0.85	48.02	2.9%	Pass
TWR_RED_HORZ_2_T2	M109	0.939	32.85	0.86	48.02	2.9%	Pass
TWR_RED_HORZ_2_T3	M126	0.431	32.85	0.45	48.02	1.3%	Pass

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TWR_RED_HORZ_2_T3	M134	0.427	32.85	0.45	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M143	0.42	32.85	0.36	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M151	0.416	32.85	0.37	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M160	0.198	32.85	0.23	48.02	0.6%	Pass
TWR_RED_HORZ_2_T3	M168	0.226	32.85	0.24	48.02	0.7%	Pass
TWR_RED_HORZ_2_T3	M177	0.469	32.85	0.41	48.02	1.4%	Pass
TWR_RED_HORZ_2_T3	M185	0.438	32.85	0.38	48.02	1.3%	Pass
TWR_RED_HORZ_2_T4	M207	0.358	32.93	0.40	48.02	1.1%	Pass
TWR_RED_HORZ_2_T4	M215	0.305	32.93	0.34	48.02	0.9%	Pass
TWR_RED_HORZ_2_T4	M224	0.438	32.93	0.38	48.02	1.3%	Pass
TWR_RED_HORZ_2_T4	M232	0.457	32.93	0.38	48.02	1.4%	Pass
TWR_RED_HORZ_2_T4	M241	0.172	32.93	0.21	48.02	0.5%	Pass
TWR_RED_HORZ_2_T4	M249	0.226	32.93	0.25	48.02	0.7%	Pass
TWR_RED_HORZ_2_T4	M258	0.403	32.93	0.32	48.02	1.2%	Pass
TWR_RED_HORZ_2_T4	M266	0.361	32.93	0.30	48.02	1.1%	Pass
TWR_RED_HORZ_2_T5	M288	0.349	33.48	0.53	48.02	1.1%	Pass
TWR_RED_HORZ_2_T5	M296	0.38	33.48	0.55	48.02	1.2%	Pass
TWR_RED_HORZ_2_T5	M305	0.301	33.48	0.27	48.02	0.9%	Pass
TWR_RED_HORZ_2_T5	M313	0.412	33.48	0.34	48.02	1.2%	Pass
TWR_RED_HORZ_2_T5	M322	0.354	33.48	0.55	48.02	1.1%	Pass
TWR_RED_HORZ_2_T5	M330	0.308	33.48	0.48	48.02	1.0%	Pass
TWR_RED_HORZ_2_T5	M339	0.437	33.48	0.36	48.02	1.3%	Pass
TWR_RED_HORZ_2_T5	M347	0.335	33.48	0.31	48.02	1.0%	Pass
TWR_RED_HORZ_2_T6	M369	0.518	33.56	0.81	48.02	1.7%	Pass
TWR_RED_HORZ_2_T6	M377	0.574	33.56	0.88	48.02	1.8%	Pass
TWR_RED_HORZ_2_T6	M386	0.246	33.56	0.17	48.02	0.7%	Pass
TWR_RED_HORZ_2_T6	M394	0.373	33.56	0.32	48.02	1.1%	Pass
TWR_RED_HORZ_2_T6	M403	0.585	33.56	0.89	48.02	1.9%	Pass
TWR_RED_HORZ_2_T6	M411	0.529	33.56	0.80	48.02	1.7%	Pass
TWR_RED_HORZ_2_T6	M420	0.415	33.56	0.35	48.02	1.2%	Pass
TWR_RED_HORZ_2_T6	M428	0.289	33.56	0.22	48.02	0.9%	Pass
TWR_RED_HORZ_2_T7	M450	0.967	34.18	1.58	48.02	3.3%	Pass
TWR_RED_HORZ_2_T7	M458	1.052	34.18	1.68	48.02	3.5%	Pass
TWR_RED_HORZ_2_T7	M467	0.341	34.18	0.34	48.02	1.0%	Pass
TWR_RED_HORZ_2_T7	M475	0.403	34.18	0.42	48.02	1.2%	Pass
TWR_RED_HORZ_2_T7	M484	1.073	34.18	1.63	48.02	3.4%	Pass
TWR_RED_HORZ_2_T7	M492	0.987	34.18	1.53	48.02	3.2%	Pass
TWR_RED_HORZ_2_T7	M501	0.414	34.18	0.42	48.02	1.2%	Pass
TWR_RED_HORZ_2_T7	M509	0.352	34.18	0.35	48.02	1.0%	Pass
TWR_RED_HORZ_2_T8	M531	1.384	34.18	2.02	48.02	4.2%	Pass
TWR_RED_HORZ_2_T8	M539	1.45	34.18	2.12	48.02	4.4%	Pass
TWR_RED_HORZ_2_T8	M548	0.507	34.18	0.45	48.02	1.5%	Pass
TWR_RED_HORZ_2_T8	M556	0.584	34.18	0.54	48.02	1.7%	Pass
TWR_RED_HORZ_2_T8	M565	1.483	34.18	2.11	48.02	4.4%	Pass
TWR_RED_HORZ_2_T8	M573	1.408	34.18	1.99	48.02	4.1%	Pass
TWR_RED_HORZ_2_T8	M582	0.625	34.18	0.53	48.02	1.8%	Pass
TWR_RED_HORZ_2_T8	M590	0.558	34.18	0.46	48.02	1.6%	Pass
TWR_RED_HORZ_2_T9	M612	1.864	34.25	2.85	48.02	5.9%	Pass
TWR_RED_HORZ_2_T9	M620	1.95	34.25	2.93	48.02	6.1%	Pass
TWR_RED_HORZ_2_T9	M629	0.753	34.25	0.93	48.02	2.2%	Pass
TWR_RED_HORZ_2_T9	M637	0.777	34.25	0.99	48.02	2.3%	Pass
TWR_RED_HORZ_2_T9	M646	1.98	34.25	2.94	48.02	6.1%	Pass
TWR_RED_HORZ_2_T9	M654	1.897	34.25	2.83	48.02	5.9%	Pass
TWR_RED_HORZ_2_T9	M663	0.791	34.25	0.98	48.02	2.3%	Pass
TWR_RED_HORZ_2_T9	M671	0.769	34.25	0.95	48.02	2.2%	Pass
TWR_RED_HORZ_2_T10	M693	1.365	34.90	0.58	48.02	3.9%	Pass
TWR_RED_HORZ_2_T10	M703	1.358	34.90	0.58	48.02	3.9%	Pass
TWR_RED_HORZ_2_T10	M714	1.074	34.90	0.46	48.02	3.1%	Pass
TWR_RED_HORZ_2_T10	M724	1.148	34.90	0.46	48.02	3.3%	Pass
TWR_RED_HORZ_2_T10	M735	1.369	34.90	0.56	48.02	3.9%	Pass

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_2_T10	M745	1.352	34.90	0.55	48.02	3.9%	Pass
TWR_RED_HORZ_2_T10	M756	1.172	34.90	0.46	48.02	3.4%	Pass
TWR_RED_HORZ_2_T10	M766	1.117	34.90	0.46	48.02	3.2%	Pass
TWR_RED_HORZ_3_T1	M1290	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1291	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1292	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1293	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1294	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1295	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1296	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1297	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T2	M55	0	14.32	1.79	48.02	3.7%	Pass
TWR_RED_HORZ_3_T2	M63	0	14.32	1.82	48.02	3.8%	Pass
TWR_RED_HORZ_3_T2	M71	0.065	14.32	1.93	48.02	4.0%	Pass
TWR_RED_HORZ_3_T2	M79	0.065	14.32	1.93	48.02	4.0%	Pass
TWR_RED_HORZ_3_T2	M87	0	14.32	1.78	48.02	3.7%	Pass
TWR_RED_HORZ_3_T2	M95	0	14.32	1.75	48.02	3.7%	Pass
TWR_RED_HORZ_3_T2	M103	0	14.32	1.83	48.02	3.8%	Pass
TWR_RED_HORZ_3_T2	M111	0	14.32	1.84	48.02	3.8%	Pass
TWR_RED_HORZ_3_T3	M128	0.225	14.32	0.65	48.02	1.6%	Pass
TWR_RED_HORZ_3_T3	M136	0.194	14.32	0.70	48.02	1.5%	Pass
TWR_RED_HORZ_3_T3	M145	0.207	14.32	0.61	48.02	1.4%	Pass
TWR_RED_HORZ_3_T3	M153	0.23	14.32	0.57	48.02	1.6%	Pass
TWR_RED_HORZ_3_T3	M162	0.1	14.32	0.56	48.02	1.2%	Pass
TWR_RED_HORZ_3_T3	M170	0.105	14.32	0.55	48.02	1.1%	Pass
TWR_RED_HORZ_3_T3	M179	0.227	14.32	0.55	48.02	1.6%	Pass
TWR_RED_HORZ_3_T3	M187	0.227	14.32	0.56	48.02	1.6%	Pass
TWR_RED_HORZ_3_T4	M209	0.08	14.32	0.69	48.02	1.4%	Pass
TWR_RED_HORZ_3_T4	M217	0.003	14.32	0.75	48.02	1.6%	Pass
TWR_RED_HORZ_3_T4	M226	0.069	14.32	0.57	48.02	1.2%	Pass
TWR_RED_HORZ_3_T4	M234	0.13	14.32	0.52	48.02	1.1%	Pass
TWR_RED_HORZ_3_T4	M243	0	14.32	0.64	48.02	1.3%	Pass
TWR_RED_HORZ_3_T4	M251	0	14.32	0.63	48.02	1.3%	Pass
TWR_RED_HORZ_3_T4	M260	0.105	14.32	0.49	48.02	1.0%	Pass
TWR_RED_HORZ_3_T4	M268	0.061	14.32	0.48	48.02	1.0%	Pass
TWR_RED_HORZ_3_T5	M290	0.258	14.48	0.85	48.02	1.8%	Pass
TWR_RED_HORZ_3_T5	M298	0.21	14.48	0.93	48.02	1.9%	Pass
TWR_RED_HORZ_3_T5	M307	0.09	14.48	0.65	48.02	1.3%	Pass
TWR_RED_HORZ_3_T5	M315	0.214	14.48	0.62	48.02	1.5%	Pass
TWR_RED_HORZ_3_T5	M324	0.171	14.48	0.81	48.02	1.7%	Pass
TWR_RED_HORZ_3_T5	M332	0.165	14.48	0.77	48.02	1.6%	Pass
TWR_RED_HORZ_3_T5	M341	0.232	14.48	0.61	48.02	1.6%	Pass
TWR_RED_HORZ_3_T5	M349	0.149	14.48	0.58	48.02	1.2%	Pass
TWR_RED_HORZ_3_T6	M371	0.262	14.51	1.01	48.02	2.1%	Pass
TWR_RED_HORZ_3_T6	M379	0.224	14.51	1.10	48.02	2.3%	Pass
TWR_RED_HORZ_3_T6	M388	0.057	14.51	0.75	48.02	1.6%	Pass
TWR_RED_HORZ_3_T6	M396	0.199	14.51	0.69	48.02	1.4%	Pass
TWR_RED_HORZ_3_T6	M405	0.251	14.51	0.99	48.02	2.1%	Pass
TWR_RED_HORZ_3_T6	M413	0.226	14.51	0.93	48.02	1.9%	Pass
TWR_RED_HORZ_3_T6	M422	0.232	14.51	0.69	48.02	1.6%	Pass
TWR_RED_HORZ_3_T6	M430	0.138	14.51	0.68	48.02	1.4%	Pass
TWR_RED_HORZ_3_T7	M452	0.441	14.70	1.27	48.02	3.0%	Pass
TWR_RED_HORZ_3_T7	M460	0.442	14.70	1.42	48.02	3.0%	Pass
TWR_RED_HORZ_3_T7	M469	0.158	14.70	0.88	48.02	1.8%	Pass
TWR_RED_HORZ_3_T7	M477	0.275	14.70	0.86	48.02	1.9%	Pass
TWR_RED_HORZ_3_T7	M486	0.491	14.70	1.33	48.02	3.3%	Pass
TWR_RED_HORZ_3_T7	M494	0.455	14.70	1.23	48.02	3.1%	Pass
TWR_RED_HORZ_3_T7	M503	0.308	14.70	0.86	48.02	2.1%	Pass
TWR_RED_HORZ_3_T7	M511	0.244	14.70	0.80	48.02	1.7%	Pass
TWR_RED_HORZ_3_T8	M533	0.735	14.70	1.61	48.02	5.0%	Pass

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TWR_RED_HORZ_3_T8	M541	0.72	14.70	1.76	48.02	4.9%	Pass
TWR_RED_HORZ_3_T8	M550	0.308	14.70	1.06	48.02	2.2%	Pass
TWR_RED_HORZ_3_T8	M558	0.409	14.70	1.03	48.02	2.8%	Pass
TWR_RED_HORZ_3_T8	M567	0.778	14.70	1.66	48.02	5.3%	Pass
TWR_RED_HORZ_3_T8	M575	0.752	14.70	1.57	48.02	5.1%	Pass
TWR_RED_HORZ_3_T8	M584	0.435	14.70	0.99	48.02	3.0%	Pass
TWR_RED_HORZ_3_T8	M592	0.399	14.70	0.98	48.02	2.7%	Pass
TWR_RED_HORZ_3_T9	M614	1.049	14.72	2.08	48.02	7.1%	Pass
TWR_RED_HORZ_3_T9	M622	1.035	14.72	2.24	48.02	7.0%	Pass
TWR_RED_HORZ_3_T9	M631	0.583	14.72	1.40	48.02	4.0%	Pass
TWR_RED_HORZ_3_T9	M639	0.687	14.72	1.35	48.02	4.7%	Pass
TWR_RED_HORZ_3_T9	M648	1.099	14.72	2.12	48.02	7.5%	Pass
TWR_RED_HORZ_3_T9	M656	1.071	14.72	2.03	48.02	7.3%	Pass
TWR_RED_HORZ_3_T9	M665	0.718	14.72	1.34	48.02	4.9%	Pass
TWR_RED_HORZ_3_T9	M673	0.686	14.72	1.32	48.02	4.7%	Pass
TWR_RED_HORZ_3_T10	M695	1.425	24.72	0.87	63.37	5.8%	Pass
TWR_RED_HORZ_3_T10	M705	1.418	24.72	0.89	63.37	5.7%	Pass
TWR_RED_HORZ_3_T10	M716	1.026	24.72	0.75	63.37	4.1%	Pass
TWR_RED_HORZ_3_T10	M726	1.122	24.72	0.75	63.37	4.5%	Pass
TWR_RED_HORZ_3_T10	M737	1.421	24.72	0.82	63.37	5.7%	Pass
TWR_RED_HORZ_3_T10	M747	1.405	24.72	0.79	63.37	5.7%	Pass
TWR_RED_HORZ_3_T10	M758	1.14	24.72	0.74	63.37	4.6%	Pass
TWR_RED_HORZ_3_T10	M768	1.06	24.72	0.74	63.37	4.3%	Pass
TWR_RED_HORZ_4_T1	M1298	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1299	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1300	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1301	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1302	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1303	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1304	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1305	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1306	0.002	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1307	0.002	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1308	0.002	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1309	0.002	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T10	M697	0.97	27.41	1.63	79.69	3.5%	Pass
TWR_RED_HORZ_4_T10	M707	1.001	27.41	1.68	79.69	3.7%	Pass
TWR_RED_HORZ_4_T10	M718	0.675	27.41	1.19	79.69	2.5%	Pass
TWR_RED_HORZ_4_T10	M728	0.685	27.41	1.19	79.69	2.5%	Pass
TWR_RED_HORZ_4_T10	M739	1.018	27.41	1.66	79.69	3.7%	Pass
TWR_RED_HORZ_4_T10	M749	0.986	27.41	1.61	79.69	3.6%	Pass
TWR_RED_HORZ_4_T10	M760	0.722	27.41	1.17	79.69	2.6%	Pass
TWR_RED_HORZ_4_T10	M770	0.724	27.41	1.17	79.69	2.6%	Pass
TWR_RED_HORZ_T1	M16	1.566	6.30	0.97	24.08	24.9%	Pass
TWR_RED_HORZ_T1	M19	1.91	6.30	1.26	24.08	30.3%	Pass
TWR_RED_HORZ_T1	M23	1.369	6.30	0.72	24.08	21.7%	Pass
TWR_RED_HORZ_T1	M26	1.34	6.30	0.73	24.08	21.3%	Pass
TWR_RED_HORZ_T1	M30	1.733	6.30	1.11	24.08	27.5%	Pass
TWR_RED_HORZ_T1	M33	1.485	6.30	0.93	24.08	23.6%	Pass
TWR_RED_HORZ_T1	M37	1.096	6.30	0.56	24.08	17.4%	Pass
TWR_RED_HORZ_T1	M40	1.103	6.30	0.55	24.08	17.5%	Pass
TWR_RED_HORZ_T2	M52	0	31.25	0.40	30.21	1.3%	Pass
TWR_RED_HORZ_T2	M60	0	31.25	0.46	30.21	1.5%	Pass
TWR_RED_HORZ_T2	M68	0.014	31.25	0.16	30.21	0.5%	Pass
TWR_RED_HORZ_T2	M76	0.045	31.25	0.17	30.21	0.6%	Pass
TWR_RED_HORZ_T2	M84	0	31.25	0.44	30.21	1.4%	Pass
TWR_RED_HORZ_T2	M92	0	31.25	0.38	30.21	1.3%	Pass
TWR_RED_HORZ_T2	M100	0.061	31.25	0.16	30.21	0.5%	Pass
TWR_RED_HORZ_T2	M108	0.025	31.25	0.15	30.21	0.5%	Pass
TWR_RED_HORZ_T3	M125	0	31.25	0.84	30.21	2.8%	Pass

TIA-222-H Code Angle Bracing Member Checks
TAG0053 - CHESHIRE
GPD Project #: 2022702.66

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_T3	M133	0.022	31.25	0.95	30.21	3.1%	Pass
TWR_RED_HORZ_T3	M142	0.147	31.25	0.44	30.21	1.5%	Pass
TWR_RED_HORZ_T3	M150	0.208	31.25	0.48	30.21	1.6%	Pass
TWR_RED_HORZ_T3	M159	0.002	31.25	0.84	30.21	2.8%	Pass
TWR_RED_HORZ_T3	M167	0.041	31.25	0.74	30.21	2.5%	Pass
TWR_RED_HORZ_T3	M176	0.25	31.25	0.49	30.21	1.6%	Pass
TWR_RED_HORZ_T3	M184	0.162	31.25	0.42	30.21	1.4%	Pass
TWR_RED_HORZ_T4	M206	0.296	31.29	1.21	30.21	4.0%	Pass
TWR_RED_HORZ_T4	M214	0.327	31.29	1.35	30.21	4.5%	Pass
TWR_RED_HORZ_T4	M223	0.094	31.29	0.53	30.21	1.7%	Pass
TWR_RED_HORZ_T4	M231	0.206	31.29	0.57	30.21	1.9%	Pass
TWR_RED_HORZ_T4	M240	0.36	31.29	1.30	30.21	4.3%	Pass
TWR_RED_HORZ_T4	M248	0.319	31.29	1.15	30.21	3.8%	Pass
TWR_RED_HORZ_T4	M257	0.257	31.29	0.57	30.21	1.9%	Pass
TWR_RED_HORZ_T4	M265	0.158	31.29	0.48	30.21	1.6%	Pass
TWR_RED_HORZ_T5	M287	0.867	31.57	2.17	30.21	7.2%	Pass
TWR_RED_HORZ_T5	M295	0.889	31.57	2.34	30.21	7.7%	Pass
TWR_RED_HORZ_T5	M304	0.498	31.57	1.17	30.21	3.9%	Pass
TWR_RED_HORZ_T5	M312	0.576	31.57	1.19	30.21	3.9%	Pass
TWR_RED_HORZ_T5	M321	0.938	31.57	2.27	30.21	7.5%	Pass
TWR_RED_HORZ_T5	M329	0.9	31.57	2.10	30.21	6.9%	Pass
TWR_RED_HORZ_T5	M338	0.629	31.57	1.17	30.21	3.9%	Pass
TWR_RED_HORZ_T5	M346	0.574	31.57	1.14	30.21	3.8%	Pass
TWR_RED_HORZ_T6	M368	1.468	31.61	2.95	30.21	9.8%	Pass
TWR_RED_HORZ_T6	M376	1.514	31.61	3.17	30.21	10.5%	Pass
TWR_RED_HORZ_T6	M385	0.728	31.61	1.55	30.21	5.1%	Pass
TWR_RED_HORZ_T6	M393	0.749	31.61	1.52	30.21	5.0%	Pass
TWR_RED_HORZ_T6	M402	1.564	31.61	3.11	30.21	10.3%	Pass
TWR_RED_HORZ_T6	M410	1.5	31.61	2.88	30.21	9.5%	Pass
TWR_RED_HORZ_T6	M419	0.785	31.61	1.47	30.21	4.8%	Pass
TWR_RED_HORZ_T6	M427	0.777	31.61	1.49	30.21	4.9%	Pass
TWR_RED_HORZ_T7	M449	2.195	31.89	3.90	30.21	12.9%	Pass
TWR_RED_HORZ_T7	M457	2.27	31.89	4.16	30.21	13.8%	Pass
TWR_RED_HORZ_T7	M466	1.318	31.89	2.44	30.21	8.1%	Pass
TWR_RED_HORZ_T7	M474	1.29	31.89	2.34	30.21	7.7%	Pass
TWR_RED_HORZ_T7	M483	2.333	31.89	4.08	30.21	13.5%	Pass
TWR_RED_HORZ_T7	M491	2.237	31.89	3.82	30.21	12.6%	Pass
TWR_RED_HORZ_T7	M500	1.332	31.89	2.27	30.21	7.5%	Pass
TWR_RED_HORZ_T7	M508	1.377	31.89	2.37	30.21	7.8%	Pass
TWR_RED_HORZ_T8	M530	2.963	31.92	4.87	30.21	16.1%	Pass
TWR_RED_HORZ_T8	M538	2.996	31.92	5.08	30.21	16.8%	Pass
TWR_RED_HORZ_T8	M547	1.749	31.92	2.98	30.21	9.9%	Pass
TWR_RED_HORZ_T8	M555	1.742	31.92	2.88	30.21	9.5%	Pass
TWR_RED_HORZ_T8	M564	3.079	31.92	4.99	30.21	16.5%	Pass
TWR_RED_HORZ_T8	M572	3.01	31.92	4.75	30.21	15.7%	Pass
TWR_RED_HORZ_T8	M581	1.781	31.92	2.80	30.21	9.3%	Pass
TWR_RED_HORZ_T8	M589	1.817	31.92	2.90	30.21	9.6%	Pass
TWR_RED_HORZ_T9	M611	3.805	31.96	6.22	30.21	20.6%	Pass
TWR_RED_HORZ_T9	M619	3.861	31.96	6.41	30.21	21.2%	Pass
TWR_RED_HORZ_T9	M628	2.51	31.96	4.32	30.21	14.3%	Pass
TWR_RED_HORZ_T9	M636	2.456	31.96	4.19	30.21	13.9%	Pass
TWR_RED_HORZ_T9	M645	3.945	31.96	6.34	30.21	21.0%	Pass
TWR_RED_HORZ_T9	M653	3.865	31.96	6.11	30.21	20.2%	Pass
TWR_RED_HORZ_T9	M662	2.502	31.96	4.10	30.21	13.6%	Pass
TWR_RED_HORZ_T9	M670	2.58	31.96	4.26	30.21	14.1%	Pass
TWR_RED_HORZ_T10	M692	1.569	25.98	1.69	30.21	6.0%	Pass
TWR_RED_HORZ_T10	M702	1.557	25.98	1.72	30.21	6.0%	Pass
TWR_RED_HORZ_T10	M713	1.005	25.98	0.79	30.21	3.9%	Pass
TWR_RED_HORZ_T10	M723	1.046	25.98	0.85	30.21	4.0%	Pass
TWR_RED_HORZ_T10	M734	1.632	25.98	1.70	30.21	6.3%	Pass

TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2022702.66

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_T10	M744	1.612	25.98	1.64	30.21	6.2%	Pass
TWR_RED_HORZ_T10	M755	1.079	25.98	0.85	30.21	4.2%	Pass
TWR_RED_HORZ_T10	M765	1.059	25.98	0.80	30.21	4.1%	Pass
TWR_TOP_GIRT_T1	M5	0.636	41.85	13.46	118.53	11.4%	Pass
TWR_TOP_GIRT_T1	M6	0.607	41.85	13.28	118.53	11.2%	Pass
TWR_TOP_GIRT_T1	M7	0.567	41.85	13.30	118.53	11.2%	Pass
TWR_TOP_GIRT_T1	M8	0.414	41.85	13.36	118.53	11.3%	Pass

TIA-222-H Code Bolt Checks
TAG0053 - CHESHIRE
GPD Project #: 2022702.66

Section #	Elevation (Ft.)	Section Set	Member	Bolt Grade	Bolt Size (in)	# of Bolts	Comp. (K)	Ten. (K)	Maximum Load (K)	Allowable Load (K)	% Capacity
T1	#N/A	TWR_LEG_T1	L6x6x1/2	A307	0.75	2	19.245	2.317	19.245	90.300	21.3%
T1	#N/A	TWR_TOP_GIRT_T1	2L3x4x5/16x3/8	A307	0.75	2	0.636	13.462	13.462	49.701	27.1%
T1	#N/A	TWR_DIAG_T1	2L3x4x5/16x3/8	A307	0.75	2	7.803	3.02	7.803	49.701	15.7%
T1	#N/A	TWR_DIAG_OUTER_T1	2L3 1/2x4x5/16x3/8	A307	0.75	2	2.278	1.859	2.278	49.701	4.6%
T1	#N/A	TWR_RED_HORZ_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	1.91	1.256	1.910	15.701	12.2%
T1	#N/A	TWR_RED_HORZ_2_T1	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.451	0.892	0.892	31.402	2.8%
T1	#N/A	TWR_RED_HORZ_3_T1	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.336	0.336	31.402	1.1%
T1	#N/A	TWR_RED_HORZ_4_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	0.002	0.136	0.136	15.701	0.9%
T1	#N/A	TWR_RED_DIAG_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	1.125	0.734	1.125	15.701	7.2%
T2	#N/A	TWR_LEG_T2	W6X20	A307	0.75	16	25.73	0	25.730	168.800	15.2%
T2	#N/A	TWR_DIAG_T2	2L3x2 1/2x3/8x3/8	A307	0.75	4	19.801	11.649	19.801	49.701	39.8%
T2	#N/A	TWR_RED_HORZ_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.254	1.175	1.254	31.402	4.0%
T2	#N/A	TWR_RED_HORZ_3_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.065	1.934	1.934	31.402	6.2%
T2	#N/A	TWR_RED_DIAG_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.886	1.221	1.221	31.402	3.9%
T2	#N/A	TWR_RED_DIAG_3_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.644	0.205	2.644	31.402	8.4%
T2	#N/A	TWR_RED_HIP_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.101	0.101	31.402	0.3%
T2	#N/A	TWR_RED_HIP_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	1.403	1.403	31.402	4.5%
T2	#N/A	TWR_RED_HIPDIA_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.131	0	0.131	31.402	0.4%
T2	#N/A	TWR_RED_HIPDIA_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.539	0	1.539	31.402	4.9%
T3	#N/A	TWR_LEG_T3	W6X20	A307	0.75	24	48.703	7.632	48.703	168.800	28.9%
T3	#N/A	TWR_HORZ_T3	2L3x2 1/2x1/4x3/8	A307	0.75	3	10.755	14.403	14.403	62.531	23.0%
T3	#N/A	TWR_DIAG_T3	2L3x2 1/2x3/8x3/8	A307	0.75	2	24.668	22.409	24.668	49.701	49.6%
T3	#N/A	TWR_RED_HORZ_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.469	0.454	0.469	31.402	1.5%
T3	#N/A	TWR_RED_HORZ_3_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.23	0.701	0.701	31.402	2.2%
T3	#N/A	TWR_RED_DIAG_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.289	0.563	0.563	31.402	1.8%
T3	#N/A	TWR_RED_DIAG_3_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.807	0.338	0.807	31.402	2.6%
T3	#N/A	TWR_RED_HIP_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.135	0.135	31.402	0.4%
T3	#N/A	TWR_RED_HIP_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.51	0.510	31.402	1.6%
T3	#N/A	TWR_RED_HIPDIA_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.134	0	0.134	31.402	0.4%
T3	#N/A	TWR_RED_HIPDIA_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.61	0	0.610	31.402	1.9%
T3	#N/A	TWR_INNER_SUPP_T3	2L3x2 1/2x1/4x3/8	A307	0.75	2	1.771	1.783	1.783	44.588	4.0%
T3	#N/A	TWR_INNER_SQ_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.482	3.446	3.446	31.402	11.0%
T3	#N/A	TWR_INNER_CORNER_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.043	4.043	31.402	12.9%
T3	#N/A	TWR_INNER_TRI_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.045	0.054	0.054	31.402	0.2%
T3	#N/A	TWR_INNER_BRACE_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.198	0.015	0.198	31.402	0.6%
T3	#N/A	TWR_INNER_LADDER_T3	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.529	1.883	2.529	44.588	5.7%
T4	#N/A	TWR_LEG_T4	W6X25	A307	0.75	32	74.091	29.126	74.091	273.400	27.1%
T4	#N/A	TWR_HORZ_T4	2L3x2 1/2x1/4x3/8	A307	0.75	3	15.98	16.395	16.395	62.531	26.2%
T4	#N/A	TWR_DIAG_T4	2L3x2-1/2x1/2x3/8	A307	0.75	4	31.415	29.063	31.415	99.402	31.6%
T4	#N/A	TWR_RED_HORZ_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.457	0.397	0.457	31.402	1.5%
T4	#N/A	TWR_RED_HORZ_3_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.13	0.746	0.746	31.402	2.4%
T4	#N/A	TWR_RED_DIAG_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.213	0.574	0.574	31.402	1.8%
T4	#N/A	TWR_RED_DIAG_3_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.739	0.251	0.739	31.402	2.4%
T4	#N/A	TWR_RED_HIP_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.171	0.171	31.402	0.5%
T4	#N/A	TWR_RED_HIP_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.506	0.506	31.402	1.6%
T4	#N/A	TWR_RED_HIPDIA_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.153	0.008	0.153	31.402	0.5%
T4	#N/A	TWR_RED_HIPDIA_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.611	0	0.611	31.402	1.9%
T4	#N/A	TWR_INNER_SUPP_T4	2L3x2 1/2x1/4x3/8	A307	0.75	2	1.839	1.855	1.855	44.588	4.2%
T4	#N/A	TWR_INNER_SQ_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.156	3.358	3.358	31.402	10.7%
T4	#N/A	TWR_INNER_CORNER_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	3.847	3.847	31.402	12.3%
T4	#N/A	TWR_INNER_TRI_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.05	0.054	0.054	31.402	0.2%
T4	#N/A	TWR_INNER_BRACE_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.215	0.02	0.215	31.402	0.7%
T4	#N/A	TWR_INNER_LADDER_T4	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.361	2.164	2.361	44.588	5.3%
T5	#N/A	TWR_LEG_T5	W8X31	A307	0.75	32	111.925	58.602	111.925	340.600	32.9%
T5	#N/A	TWR_HORZ_T5	2L3x2 1/2x1/4x3/8	A307	0.75	3	19.36	19.759	19.759	62.531	31.6%
T5	#N/A	TWR_DIAG_T5	2L3x2-1/2x1/2x3/8	A307	0.75	4	37.998	35.234	37.998	99.402	38.2%

Section #	Elevation (Ft.)	Section Set	Member	Bolt Grade	Bolt Size (in)	# of Bolts	Comp. (K)	Ten. (K)	Maximum Load (K)	Allowable Load (K)	% Capacity
T5	#N/A	TWR_RED_HORZ_2_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.437	0.554	0.554	31.402	1.8%
T5	#N/A	TWR_RED_HORZ_3_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.258	0.929	0.929	31.402	3.0%
T5	#N/A	TWR_RED_DIAG_2_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.312	0.552	0.552	31.402	1.8%
T5	#N/A	TWR_RED_DIAG_3_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.768	0.504	0.768	31.402	2.4%
T5	#N/A	TWR_RED_HIP_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.161	0.161	31.402	0.5%
T5	#N/A	TWR_RED_HIP_2_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.513	0.513	31.402	1.6%
T5	#N/A	TWR_RED_HIPDIA_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.16	0.015	0.160	31.402	0.5%
T5	#N/A	TWR_RED_HIPDIA_2_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.611	0	0.611	31.402	1.9%
T5	#N/A	TWR_INNER_SUPP_T5	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.222	2.244	2.244	44.588	5.0%
T5	#N/A	TWR_INNER_SQ_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.613	4.082	4.082	31.402	13.0%
T5	#N/A	TWR_INNER_CORNER_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.63	4.630	31.402	14.7%
T5	#N/A	TWR_INNER_TRI_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.051	0.054	0.054	31.402	0.2%
T5	#N/A	TWR_INNER_BRACE_T5	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.217	0.026	0.217	31.402	0.7%
T5	#N/A	TWR_INNER_LADDER_T5	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.846	2.663	2.846	44.588	6.4%
T6	#N/A	TWR_LEG_T6	W8X40	A307	0.75	32	158.322	94.752	158.322	471.700	33.6%
T6	#N/A	TWR_HORZ_T6	2L3x2 1/2x5/16x3/8	A307	0.75	3	23.259	23.771	23.771	74.551	31.9%
T6	#N/A	TWR_DIAG_T6	2L4x3x3/8x3/8	A307	0.75	4	44.73	42.229	44.730	99.402	45.0%
T6	#N/A	TWR_RED_HORZ_2_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.585	0.89	0.890	31.402	2.8%
T6	#N/A	TWR_RED_HORZ_3_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.262	1.099	1.099	31.402	3.5%
T6	#N/A	TWR_RED_DIAG_2_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.529	0.595	0.595	31.402	1.9%
T6	#N/A	TWR_RED_DIAG_3_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.844	0.703	0.844	31.402	2.7%
T6	#N/A	TWR_RED_HIP_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.01	0.183	0.183	31.402	0.6%
T6	#N/A	TWR_RED_HIP_2_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.5	0.500	31.402	1.6%
T6	#N/A	TWR_RED_HIPDIA_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.202	0.057	0.202	31.402	0.6%
T6	#N/A	TWR_RED_HIPDIA_2_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.602	0	0.602	31.402	1.9%
T6	#N/A	TWR_INNER_SUPP_T6	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.258	2.294	2.294	44.588	5.1%
T6	#N/A	TWR_INNER_SQ_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.663	4.175	4.175	31.402	13.3%
T6	#N/A	TWR_INNER_CORNER_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.72	4.720	31.402	15.0%
T6	#N/A	TWR_INNER_TRI_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.05	0.054	0.054	31.402	0.2%
T6	#N/A	TWR_INNER_BRACE_T6	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.273	0.032	0.273	31.402	0.9%
T6	#N/A	TWR_INNER_LADDER_T6	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.896	2.721	2.896	44.588	6.5%
T7	#N/A	TWR_LEG_T7	W10X54	A307	0.75	32	212.794	139.531	212.794	484.800	43.9%
T7	#N/A	TWR_HORZ_T7	2L3x2 1/2x3/8x3/8	A307	0.75	4	26.522	26.959	26.959	99.402	27.1%
T7	#N/A	TWR_DIAG_T7	2L4x3x3/8x3/8	A307	0.75	4	50.535	48.071	50.535	99.402	50.8%
T7	#N/A	TWR_RED_HORZ_2_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.073	1.679	1.679	31.402	5.3%
T7	#N/A	TWR_RED_HORZ_3_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.491	1.416	1.416	31.402	4.5%
T7	#N/A	TWR_RED_DIAG_2_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.191	0.997	1.191	31.402	3.8%
T7	#N/A	TWR_RED_DIAG_3_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.163	1.102	1.163	31.402	3.7%
T7	#N/A	TWR_RED_HIP_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.007	0.158	0.158	31.402	0.5%
T7	#N/A	TWR_RED_HIP_2_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.511	0.511	31.402	1.6%
T7	#N/A	TWR_RED_HIPDIA_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.219	0.073	0.219	31.402	0.7%
T7	#N/A	TWR_RED_HIPDIA_2_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.603	0	0.603	31.402	1.9%
T7	#N/A	TWR_INNER_SUPP_T7	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.242	2.289	2.289	44.588	5.1%
T7	#N/A	TWR_INNER_SQ_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.639	4.143	4.143	31.402	13.2%
T7	#N/A	TWR_INNER_CORNER_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.68	4.680	31.402	14.9%
T7	#N/A	TWR_INNER_TRI_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.05	0.053	0.053	31.402	0.2%
T7	#N/A	TWR_INNER_BRACE_T7	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.327	0.045	0.327	31.402	1.0%
T7	#N/A	TWR_INNER_LADDER_T7	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.865	2.696	2.865	44.588	6.4%
T8	#N/A	TWR_LEG_T8	W10X60	A307	0.75	32	274.945	191.151	274.945	530.100	51.9%
T8	#N/A	TWR_HORZ_T8	2L3x2 1/2x3/8x3/8	A307	0.75	4	29.945	30.319	30.319	99.402	30.5%
T8	#N/A	TWR_DIAG_T8	2L4x3x1/2x3/8	A307	0.75	5	57.484	54.111	57.484	124.252	46.3%
T8	#N/A	TWR_RED_HORZ_2_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.483	2.116	2.116	31.402	6.7%
T8	#N/A	TWR_RED_HORZ_3_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.778	1.764	1.764	31.402	5.6%
T8	#N/A	TWR_RED_DIAG_2_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.503	1.345	1.503	31.402	4.8%
T8	#N/A	TWR_RED_DIAG_3_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.537	1.523	1.537	31.402	4.9%
T8	#N/A	TWR_RED_HIP_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.071	0.198	0.198	31.402	0.6%
T8	#N/A	TWR_RED_HIP_2_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.504	0.504	31.402	1.6%
T8	#N/A	TWR_RED_HIPDIA_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.248	0.102	0.248	31.402	0.8%
T8	#N/A	TWR_RED_HIPDIA_2_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.603	0	0.603	31.402	1.9%
T8	#N/A	TWR_INNER_SUPP_T8	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.508	2.567	2.567	44.588	5.8%
T8	#N/A	TWR_INNER_SQ_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.989	4.654	4.654	31.402	14.8%
T8	#N/A	TWR_INNER_CORNER_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	5.251	5.251	31.402	16.7%
T8	#N/A	TWR_INNER_TRI_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.051	0.053	0.053	31.402	0.2%
T8	#N/A	TWR_INNER_BRACE_T8	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.335	0.051	0.335	31.402	1.1%
T8	#N/A	TWR_INNER_LADDER_T8	2L3x2 1/2x1/4x3/8	A307	0.75	2	3.202	3.084	3.202	44.588	7.2%
T9	#N/A	TWR_LEG_T9	W10X68	A307	0.75	40	345.22	249.835	345.220	706.800	48.8%
T9	#N/A	TWR_HORZ_T9	2L3x2 1/2x3/8x3/8	A307	0.75	4	32.635	32.875	32.875	99.402	33.1%
T9	#N/A	TWR_DIAG_T9	2L4x3x1/2x3/8	A307	0.75	6	62.958	59.122	62.958	149.103	42.2%
T9	#N/A	TWR_RED_HORZ_2_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.98	2.944	2.944	31.402	9.4%
T9	#N/A	TWR_RED_HORZ_3_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.099	2.237	2.237	31.402	7.1%
T9	#N/A	TWR_RED_DIAG_2_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.177	1.747	2.177	31.402	6.9%
T9	#N/A	TWR_RED_DIAG_3_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.958	2.142	2.142	31.402	6.8%
T9	#N/A	TWR_RED_HIP_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.086	0.212	0.212	31.402	0.7%
T9	#N/A	TWR_RED_HIP_2_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.499	0.499	31.402	1.6%
T9	#N/A	TWR_RED_HIPDIA_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.326	0.181	0.326	31.402	1.0%
T9	#N/A	TWR_REDHIPDIA_2_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.596	0	0.596	31.402	1.9%
T9	#N/A	TWR_INNER_SUPP_T9	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.721	2.776	2.776	44.588	6.2%
T9	#N/A	TWR_INNER_SQ_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	3.244	5.085	5.085	31.402	16.2%
T9	#N/A	TWR_INNER_CORNER_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	5.726	5.726	31.402	18.2%
T9	#N/A	TWR_INNER_TRI_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.051	0.054	0.054	31.402	0.2%
T9	#N/A	TWR_INNER_BRACE_T9	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.338	0.058	0.338	31.402	1.1%
T9	#N/A	TWR_INNER_LADDER_T9	2L3x2 1/2x1/4x3/8	A307	0.75	2	3.5	3.37	3.500	44.588	7.8%
T10	#N/A	TWR_LEG_T10	W12X79	A307	0.75	56	423.243	314.483	423.243	883.600	47.9%
T10	#N/A	TWR_HORZ_T10	2L4x3x1/2x3/8	A307	0.75	4	33.162	29.18	33.162	99.402	33.4%
T10	#N/A	TWR_DIAG_T10	2L4x4x1/2x3/8	A307	0.75	8	81.721	74.026	81.721	198.804	41.1%
T10	#N/A	TWR_RED_HORZ_2_T10	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.369	0.579	1.369	31.402	4.4%
T10	#N/A	TWR_RED_HORZ_3_T10	2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	1.425	0.886	1.425	41.869	3.4%
T10	#N/A	TWR_RED_DIAG_2_T10	2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	0.457	1.428	1.428	41.869	3.4%
T10	#N/A	TWR_RED_HORZ_4_T10	2L3x3x1/4x3/8	A307	0.75	2	1.018	1.678	1.678	44.588	3.8%
T10	#N/A	TWR_RED_DIAG_3_T10	2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	0.594	1.562	1.562	41.869	3.7%
T10	#N/A	TWR_RED_DIAG_4_T10	2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	2.125	1.531	2.125	41.869	5.1%
T10	#N/A	TWR_RED_DIAG_0_T10	L2.5x2.5x8	A307	0.75	2	11.266	8.477	11.266	24.850	45.3%
T10	#N/A	TWR_RED_HORZ_0_T10	L2.5x2.5x3	A307	0.75	2	6.605	9.146	9.146	15.701	58.3%
T10	#N/A	TWR_RED_HIP_1_T10	LL4x4x8x3	A307	0.75	2	0.061	0.056	0.061	49.701	0.1%
T10	#N/A	TWR_RED_HIP_3_T10	LL3x3x3x3	A307	0.75	2	0	0.557	0.557	33.441	1.7%
T10	#N/A	TWR_RED_HIPDIA_1_T10	LL3x3x3x3	A307	0.75	2	0.353	0.129	0.353	33.441	1.1%
T10	#N/A	TWR_RED_HIPDIA_3_T10	LL3x3x3x3	A307	0.75	2	0.966	0	0.966	33.441	2.9%

APPENDIX C

Additional Calculations

Self-Support Anchor Rod Analysis - TIA-222-H-1
TAG0053 - CHESHIRE
GPD Project #: 2022702.66

General Info	
Apply TIA-222-H Section 15.5	No
Modified Anchor Rods	No
Leg Eccentricity	No
Overstrength	No
Max Capacity	105%

Tower Reactions		
Compression, P_u =	515.21	kips
Compression Shear, V_u =	54.65	kips
Uplift, P_u =	387.14	kips
Uplift Shear, V_u =	46.96	kips
Number of Tower Legs =	4	
Tower Axial Force =	152.14	kips

Anchor Rods		
Number of Anchor Rods, n =	12	
Anchor Rod Grade =	C-1015	
Anchor Rod Diameter, d =	2.25	in
Bolt Circle Diameter, BC =	34	in
Rod Clear Span, l_{ar} =	0	in
Is grout present?	No	
Yield Strength, F_y =	47	ksi
Tensile Strength, F_u =	56	ksi
Rod Compression, P_{uc} =	42.93	kips
Rod Shear, V_u =	4.55	kips
Rod Moment, M_u =	0.00	k-in
Rod Tension, P_{ut} =	32.26	kips
Rod Shear, V_u =	3.91	kips
Rod Moment, M_u =	0.00	k-in

Anchor Rod Results		
$\phi_t R_{nt}$ =	136.50	kips
$\phi_c R_{nc}$ =	168.19	kips
$\phi_c R_{nb}$ =	168.19	kips
$\phi_v R_{nv}$ =	83.50	kips
$\phi_c R_{nvc}$ =	75.68	kips
$\phi_f M_n$ =	80.30	k-in
Tension Interaction	5.8%	OK
Compression Interaction	25.9%	OK

Title Block Line 1
You can change this area
using the "Settings" menu item
and then using the "Printing &
Title Block" selection.
Title Block Line 6

Project Title: TAG0053 (10136365) CHESHIRE
Engineer: C Kuhn
Project ID: 2022702.66
Project Descr: Pedestal Analysis

Printed: 20 MAY 2022, 7:06AM

Concrete Column

File: 4 Pedestal Checks.ec6

Lic. # : KW-06004426

GPD ASSOCIATES

DESCRIPTION: Pedestal Analysis

Code References

Calculations per ACI 318-11, IBC 2012, CBC 2013, ASCE 7-10
Load Combinations Used : IBC 2015

General Information

f'c : Concrete 28 day strength	=	3.0 ksi
E =	=	3,122.0 ksi
Density	=	150.0 pcf
β	=	0.850
fy - Main Rebar	=	40.0 ksi
E - Main Rebar	=	29,000.0 ksi
Allow. Reinforcing Limits		*ASTM A615 Bars Used*
Min. Reinf.	=	1.0 %
Max. Reinf.	=	8.0 %

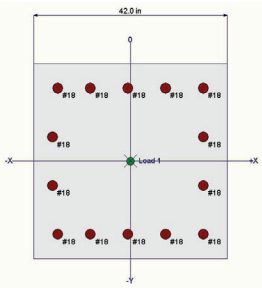
Overall Column Height = 6.20 ft
End Fixity: Top Free, Bottom Fixed

Brace condition for deflection (buckling) along columns :
X-X (width) axis :
Unbraced Length for buckling ABOUT Y-Y Axis = 6.20 ft, K = 2.10
Y-Y (depth) axis :
Unbraced Length for buckling ABOUT X-X Axis = 6.20 ft, K = 2.10

Column Cross Section

Column Dimensions : 42.0in Square Column, Column Edge to Rebar Edge Cover = 4.125in

Column Reinforcing : 4 - #18 bars @ corners,, 3.0 - #18 bars top & bottom between corner bars, 2.0 - #18 bars left & right between corner bars



Applied Loads

Entered loads are factored per load combinations specified by user.

Column self weight included : 11,392.5 lbs * Dead Load Factor
AXIAL LOADS . . .
LC40 - Node 44: Axial Load at 6.20 ft above base, D = 89.072, W = 440.559 k
BENDING LOADS . . .
LC36 - Node 441: Lat. Point Load at 6.20 ft creating Mx-x, W = 50.538 k
Lat. Point Load at 6.20 ft creating My-y, W = 50.431 k

DESIGN SUMMARY

Load Combination +1.20D+0.50Lr+0.50L+W+1.60H
Location of max.above base 6.158 ft

Maximum Stress Ratio **0.227 : 1**
Ratio = (Pu^2+Mu^2)^.5 / (PhiPn^2+PhiMn^2)^.5

Pu =	561.12 k	φ * Pn =	2,476.44 k
Mu-x =	-313.336 k-ft	φ * Mn-x =	-1,402.99 k-ft
Mu-y =	-312.672 k-ft	φ * Mn-y =	1,339.74 k-ft
Mu Angle =	45.0 deg		
Mu at Angle =	442.655 k-ft	φMn at Angle =	1,946.42 k-ft

Pn & Mn values located at Pu-Mu vector intersection with capacity curve

Column Capacities . . .

Pnmax : Nominal Max. Compressive Axial Capacity	6,595.40 k
Pnmin : Nominal Min. Tension Axial Capacity	k
φ Pn, max : Usable Compressive Axial Capacity	3,429.61 k
φ Pn, min : Usable Tension Axial Capacity	k

Maximum SERVICE Load Reactions . .

Top along Y-Y	0.0 k	Bottom along Y-Y	50.431 k
Top along X-X	0.0 k	Bottom along X-X	50.538 k

Maximum SERVICE Load Deflections . . .

Along Y-Y 0.008529 in at 6.20 ft above base
for load combination : W Only

Along X-X 0.008511 in at 6.20 ft above base
for load combination : W Only

General Section Information . φ = 0.650 β = 0.850 θ = 0.80

ρ : % Reinforcing	3.175 %	Rebar % Ok
Reinforcing Area	56.0 in^2	
Concrete Area	1,764.0 in^2	

Concrete Column

DESCRIPTION: Pedestal Analysis

Governing Load Combination Results

Governing Factored Load Combination	Moment X-X	Moment Y-Y	Dist. from base ft	Axial Load k Pu	φ * Pn	Bending Analysis k-ft δx	δx * Mux	δy	δy * Muy	Alpha (deg)	δ Mu	φ Mn	Utilization Ratio
+1.40D+1.60H			6.16	140.65	3,429.61					0.000			**0.041**
+1.20D+0.50Lr+1.60L+1.60H			6.16	120.56	3,429.61					0.000			**0.035**
+1.20D+1.60L+0.50S+1.60H			6.16	120.56	3,429.61					0.000			**0.035**
+1.20D+1.60Lr+0.50L+1.60H			6.16	120.56	3,429.61					0.000			**0.035**
+1.20D+1.60Lr+0.50W+1.60H	Actual	Actual	6.16	340.84	2,752.82	1.000	-156.67	1.000	-156.34	45.000	221.33	1,775.09	**0.125**
+1.20D+0.50L+1.60S+1.60H			6.16	120.56	3,429.61					0.000			**0.035**
+1.20D+1.60S+0.50W+1.60H	Actual	Actual	6.16	340.84	2,752.82	1.000	-156.67	1.000	-156.34	45.000	221.33	1,775.09	**0.125**
+1.20D+0.50Lr+0.50L+W+1.60H	Actual	Actual	6.16	561.12	2,476.44	1.000	-313.34	1.000	-312.67	45.000	442.65	1,946.42	**0.227**
+1.20D+0.50L+0.50S+W+1.60H	Actual	Actual	6.16	561.12	2,476.44	1.000	-313.34	1.000	-312.67	45.000	442.65	1,946.42	**0.227**
+1.20D+0.50L+0.70S+E+1.60H			6.16	120.56	3,429.61					0.000			**0.035**
+0.90D+W+0.90H	Actual	Actual	6.16	530.98	2,383.84	1.000	-313.34	1.000	-312.67	45.000	442.65	1,995.93	**0.222**
+0.90D+E+0.90H			6.16	90.42	3,429.61					0.000			**0.026**

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction @ Base	@ Top	k	Y-Y Axis Reaction @ Base	@ Top	Axial Reaction @ Base	My - End Moments @ Base	@ Top	k-ft	Mx - End Moments @ Base	@ Top
+D+H						100.465					
+D+L+H						100.465					
+D+Lr+H						100.465					
+D+S+H						100.465					
+D+0.750Lr+0.750L+H						100.465					
+D+0.750L+0.750S+H						100.465					
+D+0.60W+H	30.259			30.323		364.800	188.001			187.603	
+D+0.70E+H						100.465					
+D+0.750Lr+0.750L+0.450W+H	22.694			22.742		298.716	141.001			140.702	
+D+0.750L+0.750S+0.450W+H	22.694			22.742		298.716	141.001			140.702	
+D+0.750L+0.750S+0.5250E+H						100.465					
+0.60D+0.60W+0.60H	30.259			30.323		324.614	188.001			187.603	
+0.60D+0.70E+0.60H						60.279					
D Only						100.465					
Lr Only											
L Only											
S Only											
W Only	50.431			50.538		440.559	313.336			312.672	
E Only											
H Only											

Maximum Moment Reactions

Note: Only non-zero reactions are listed.

Load Combination	Moment About X-X Axis @ Base	@ Top		Moment About Y-Y Axis @ Base	@ Top	
+D+H			k-ft			k-ft
+D+L+H			k-ft			k-ft
+D+Lr+H			k-ft			k-ft
+D+S+H			k-ft			k-ft
+D+0.750Lr+0.750L+H			k-ft			k-ft
+D+0.750L+0.750S+H			k-ft			k-ft
+D+0.60W+H	188.001		k-ft	187.603		k-ft
+D+0.70E+H			k-ft			k-ft
+D+0.750Lr+0.750L+0.450W+H	141.001		k-ft	140.702		k-ft
+D+0.750L+0.750S+0.450W+H	141.001		k-ft	140.702		k-ft
+D+0.750L+0.750S+0.5250E+H			k-ft			k-ft
+0.60D+0.60W+0.60H	188.001		k-ft	187.603		k-ft
+0.60D+0.70E+0.60H			k-ft			k-ft
D Only			k-ft			k-ft
Lr Only			k-ft			k-ft
L Only			k-ft			k-ft
S Only			k-ft			k-ft
W Only	313.336		k-ft	312.672		k-ft

Concrete Column

DESCRIPTION: Pedestal Analysis

Maximum Moment Reactions

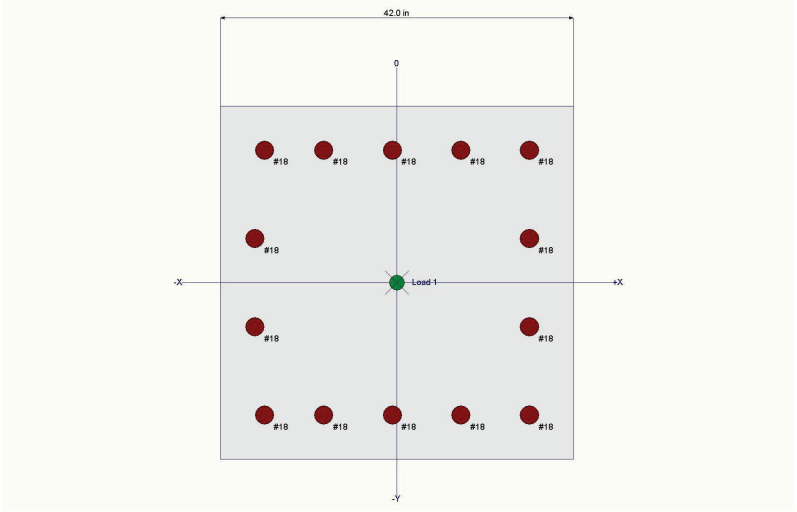
Note: Only non-zero reactions are listed.

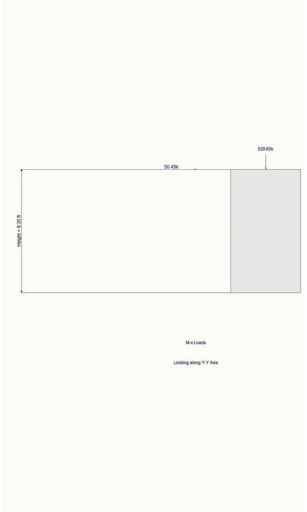
Load Combination	Moment About X-X Axis @ Base	Moment About X-X Axis @ Top	Moment About Y-Y Axis @ Base	Moment About Y-Y Axis @ Top
E Only	k-ft			k-ft
H Only	k-ft			k-ft

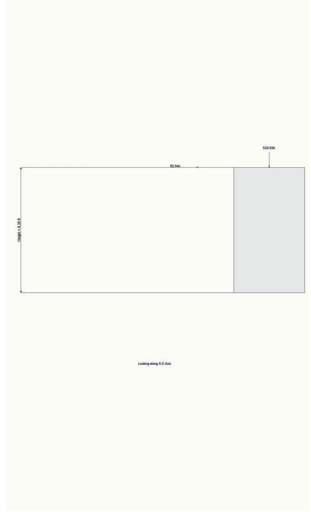
Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection		Distance		Max. Y-Y Deflection		Distance	
+D+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+L+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+Lr+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+S+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+0.750Lr+0.750L+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+0.750L+0.750S+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+0.60W+H	0.0051	in	6.200	ft	0.005	in	6.200	ft
+D+0.70E+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+D+0.750Lr+0.750L+0.450W+H	0.0038	in	6.200	ft	0.004	in	6.200	ft
+D+0.750L+0.750S+0.450W+H	0.0038	in	6.200	ft	0.004	in	6.200	ft
+D+0.750L+0.750S+0.5250E+H	0.0000	in	0.000	ft	0.000	in	0.000	ft
+0.60D+0.60W+0.60H	0.0051	in	6.200	ft	0.005	in	6.200	ft
+0.60D+0.70E+0.60H	0.0000	in	0.000	ft	0.000	in	0.000	ft
D Only	0.0000	in	0.000	ft	0.000	in	0.000	ft
Lr Only	0.0000	in	0.000	ft	0.000	in	0.000	ft
L Only	0.0000	in	0.000	ft	0.000	in	0.000	ft
S Only	0.0000	in	0.000	ft	0.000	in	0.000	ft
W Only	0.0085	in	6.200	ft	0.009	in	6.200	ft
E Only	0.0000	in	0.000	ft	0.000	in	0.000	ft
H Only	0.0000	in	0.000	ft	0.000	in	0.000	ft

Sketches

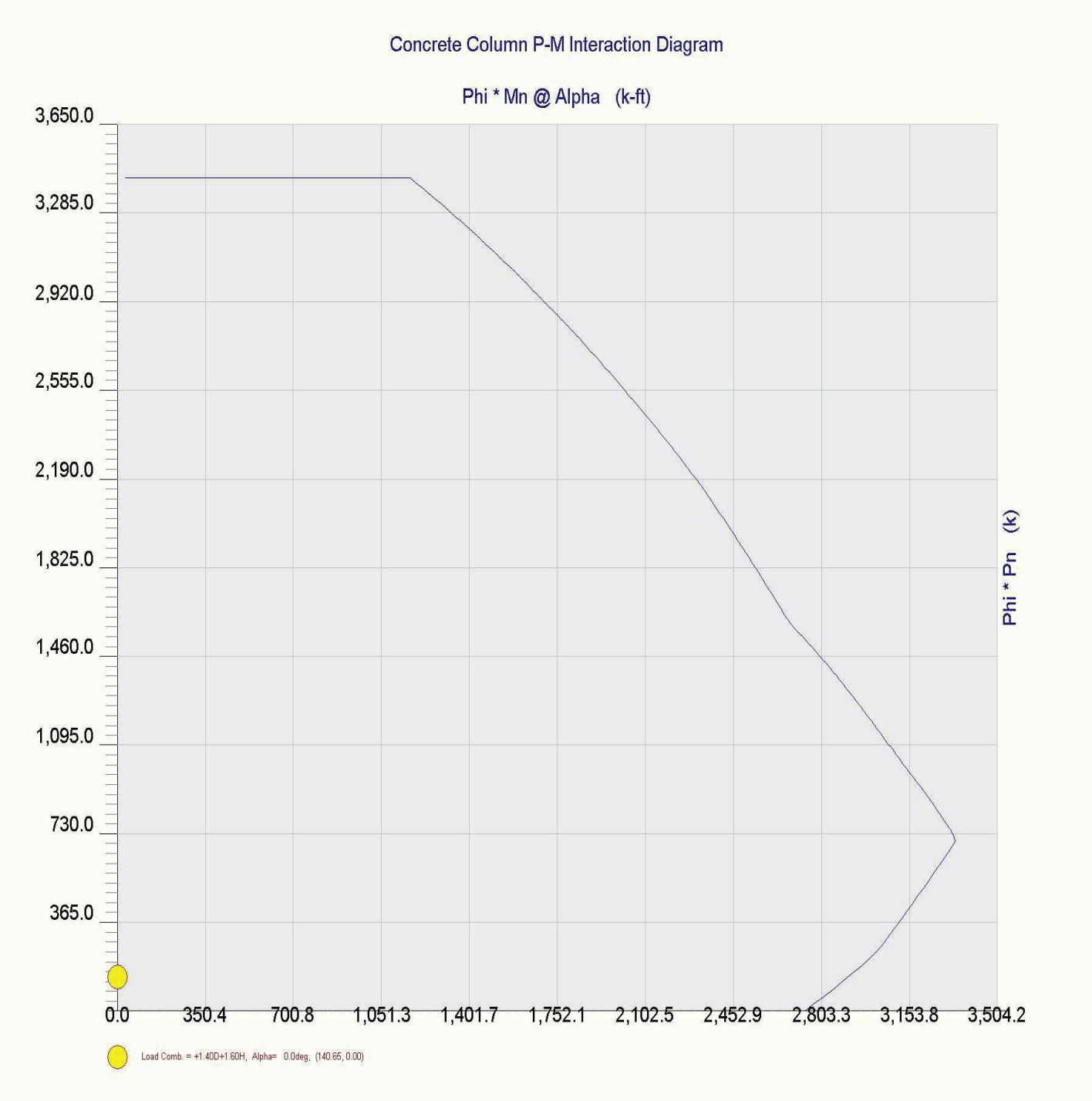






Interaction Diagrams

DESCRIPTION: Pedestal Analysis



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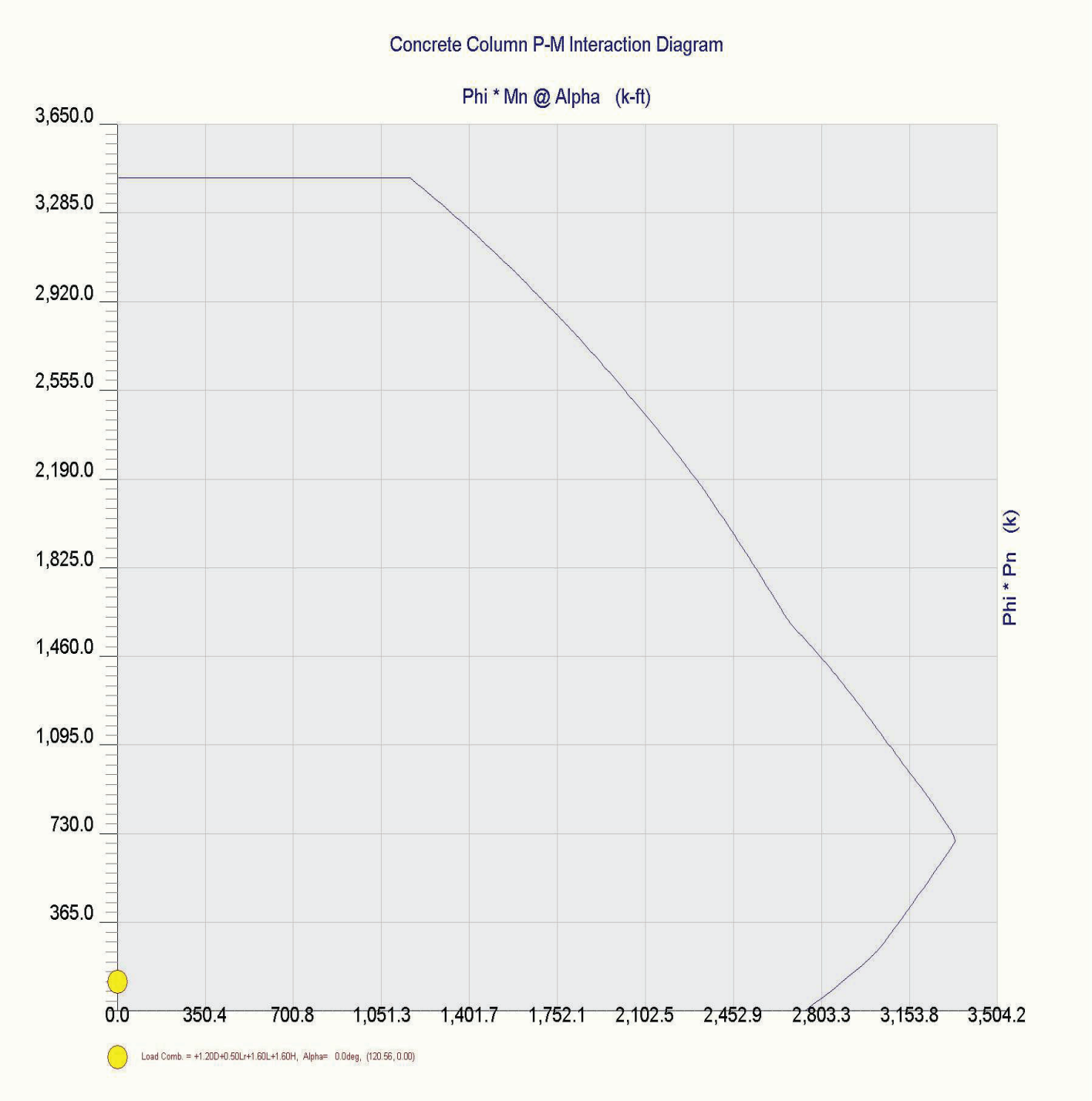

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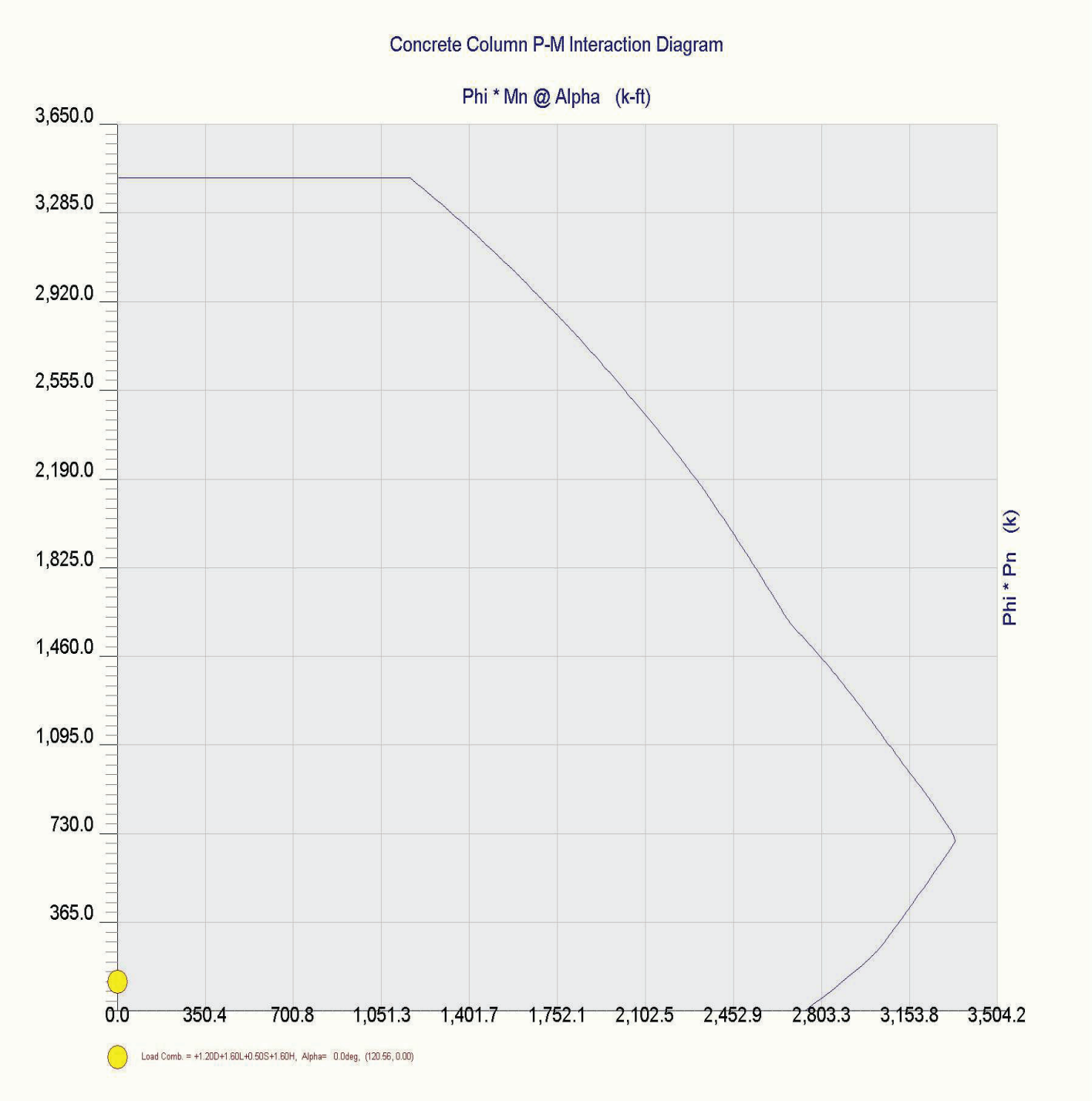

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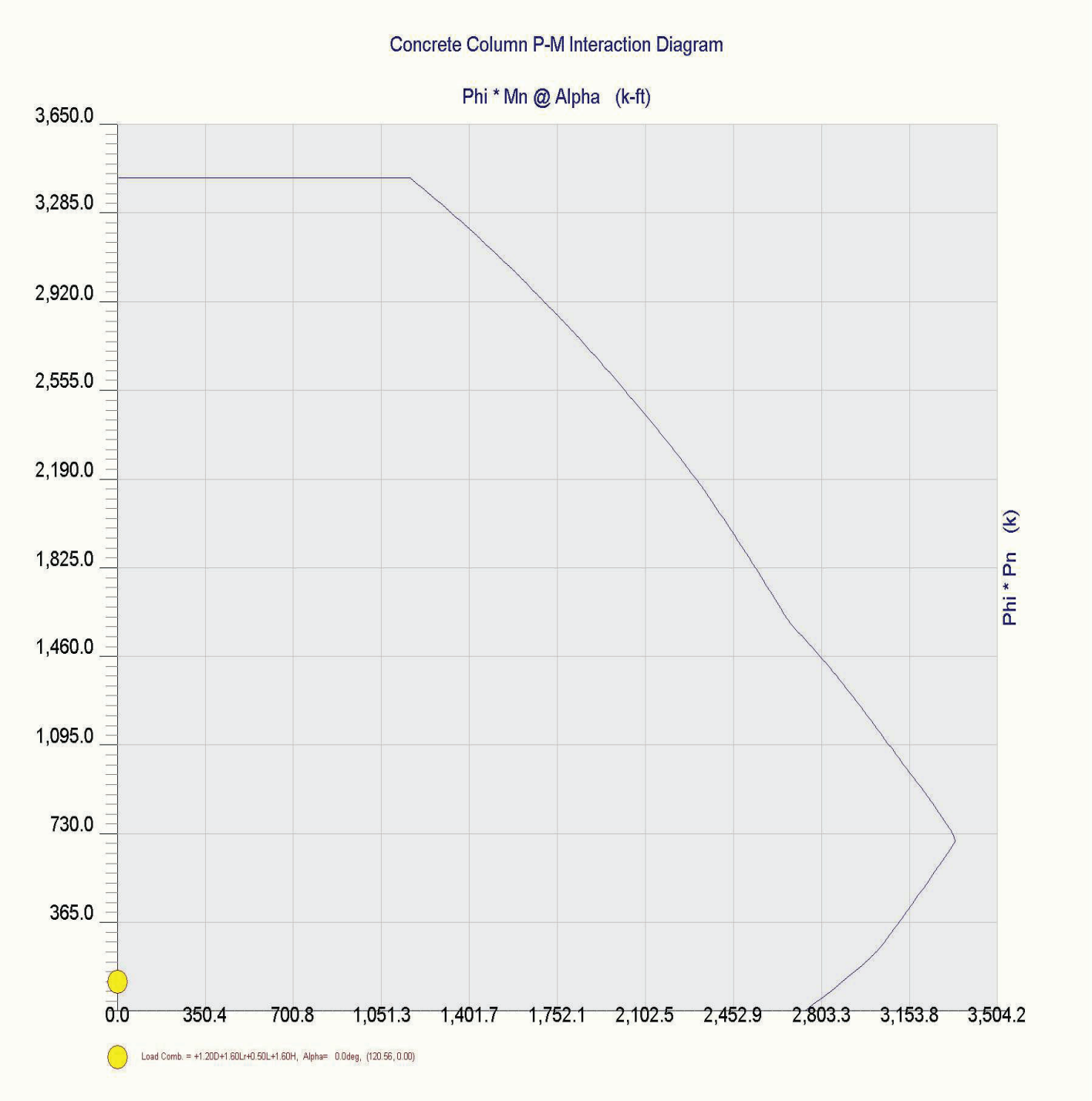

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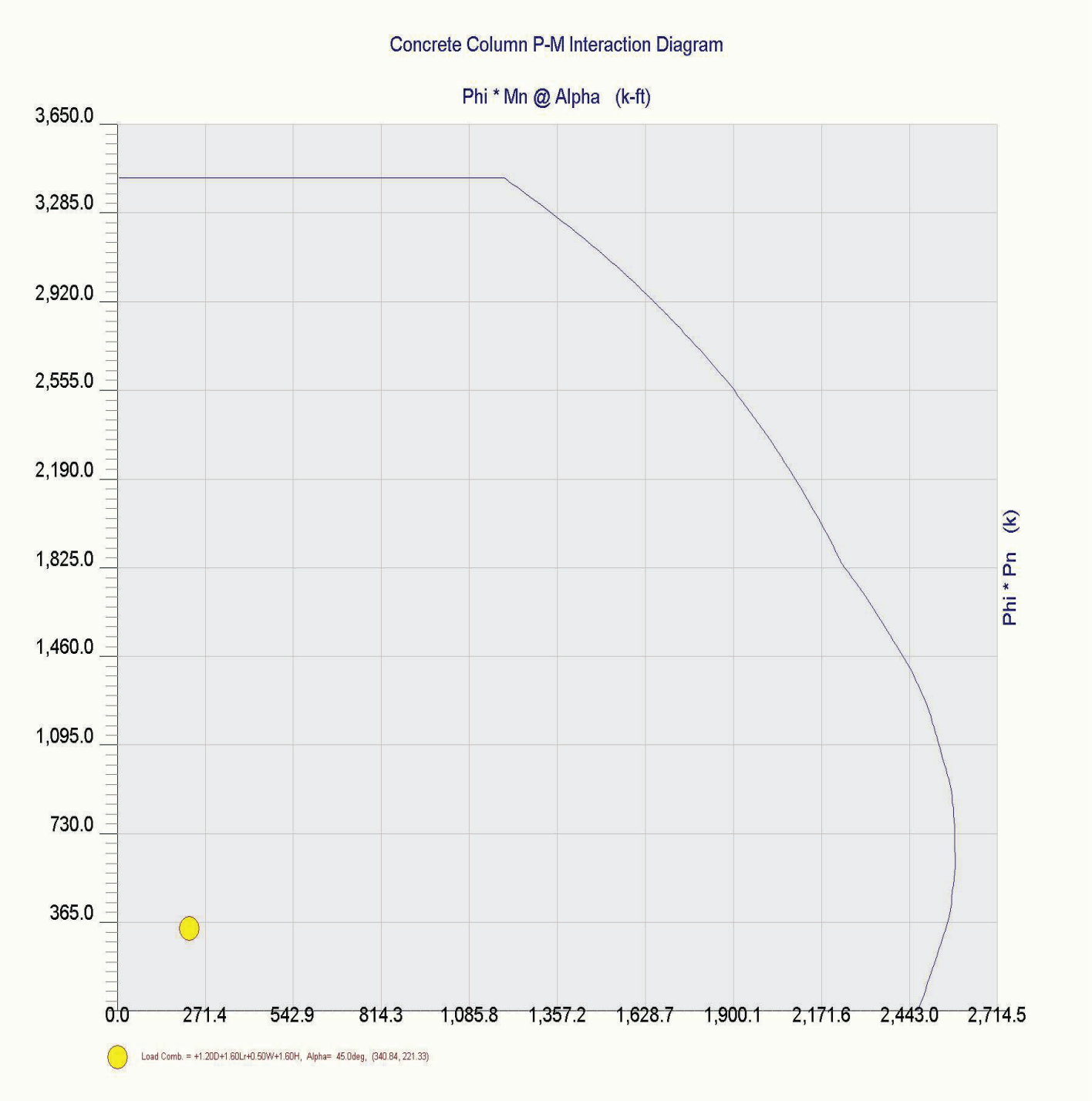

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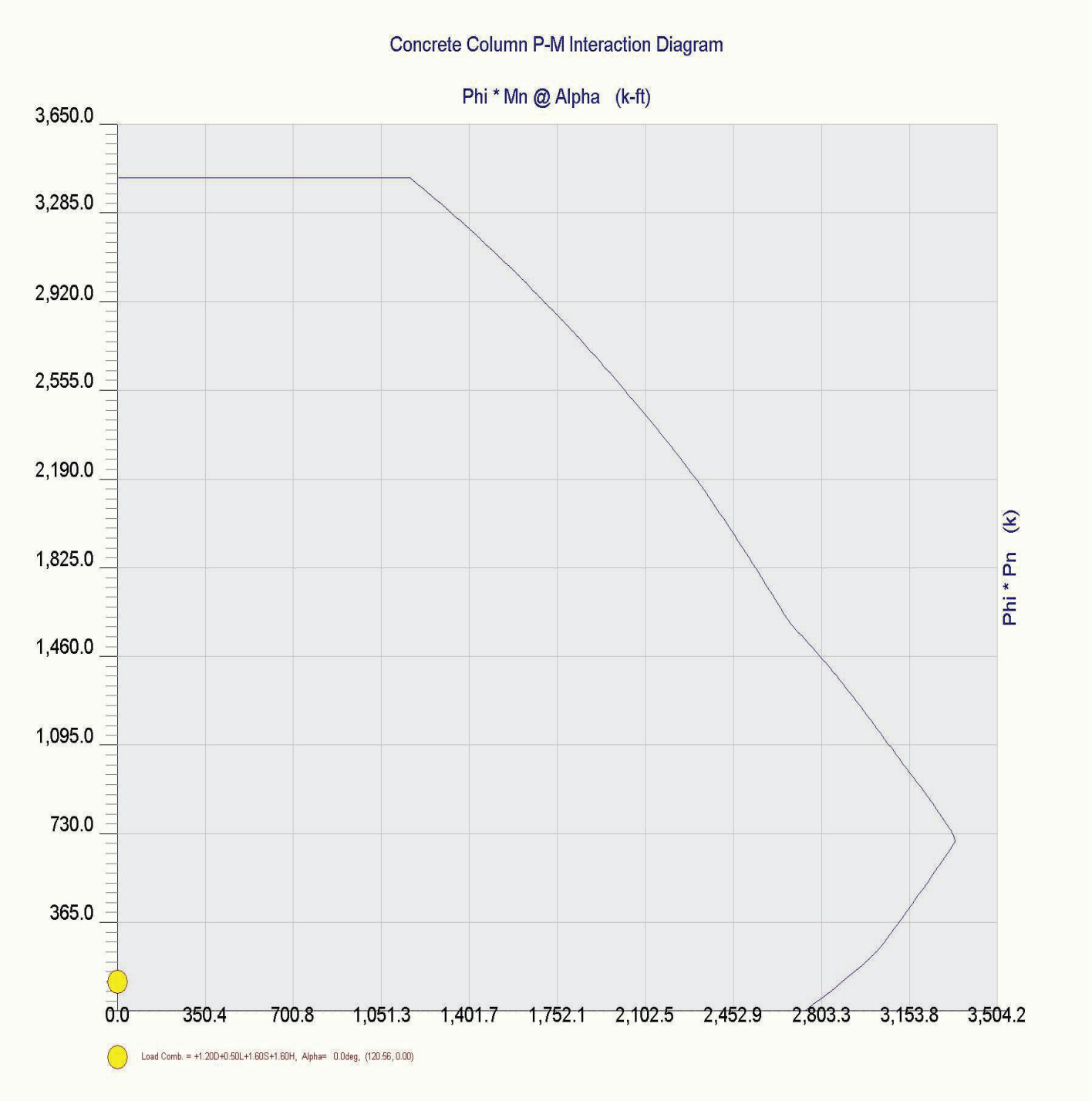

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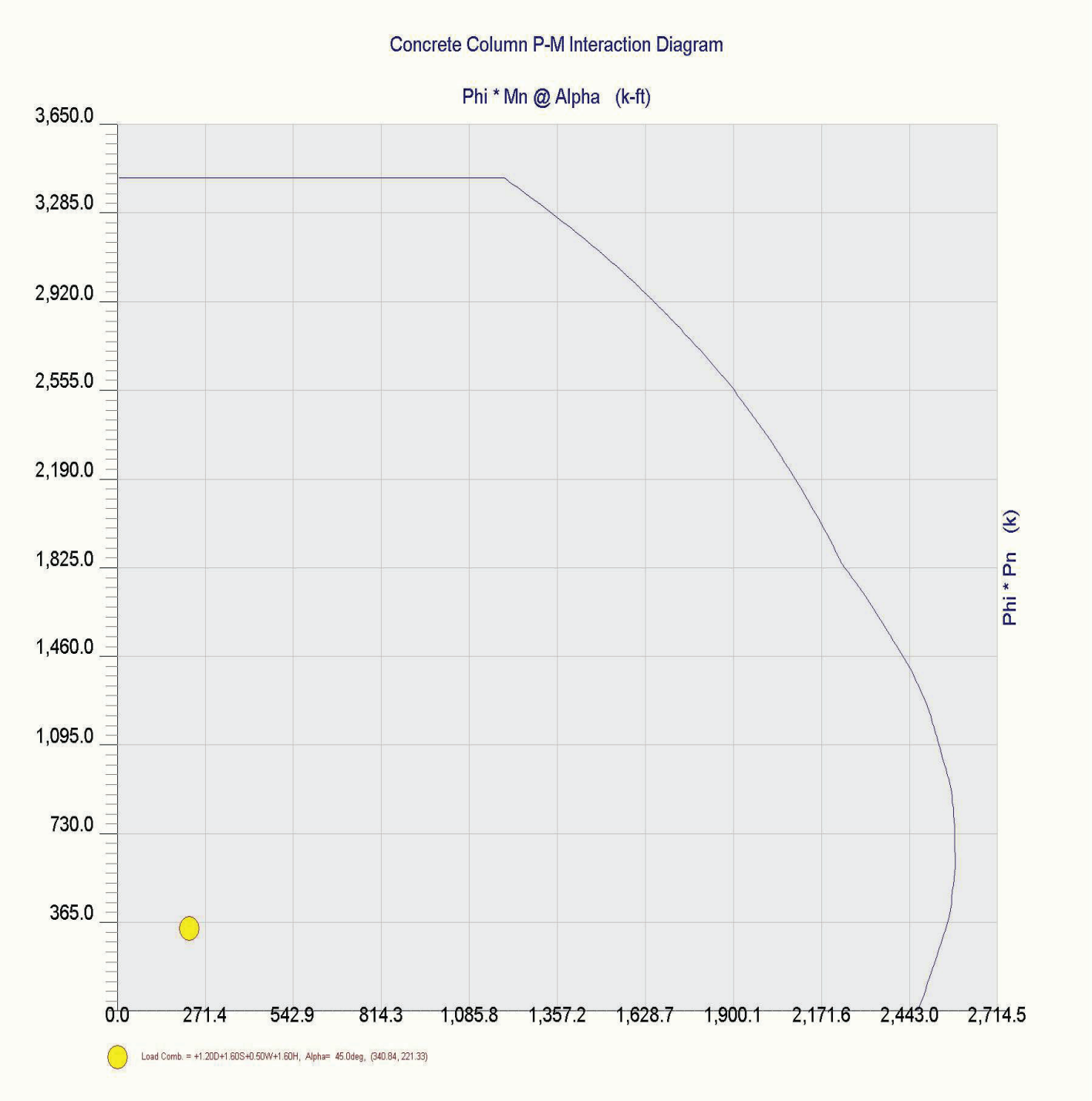

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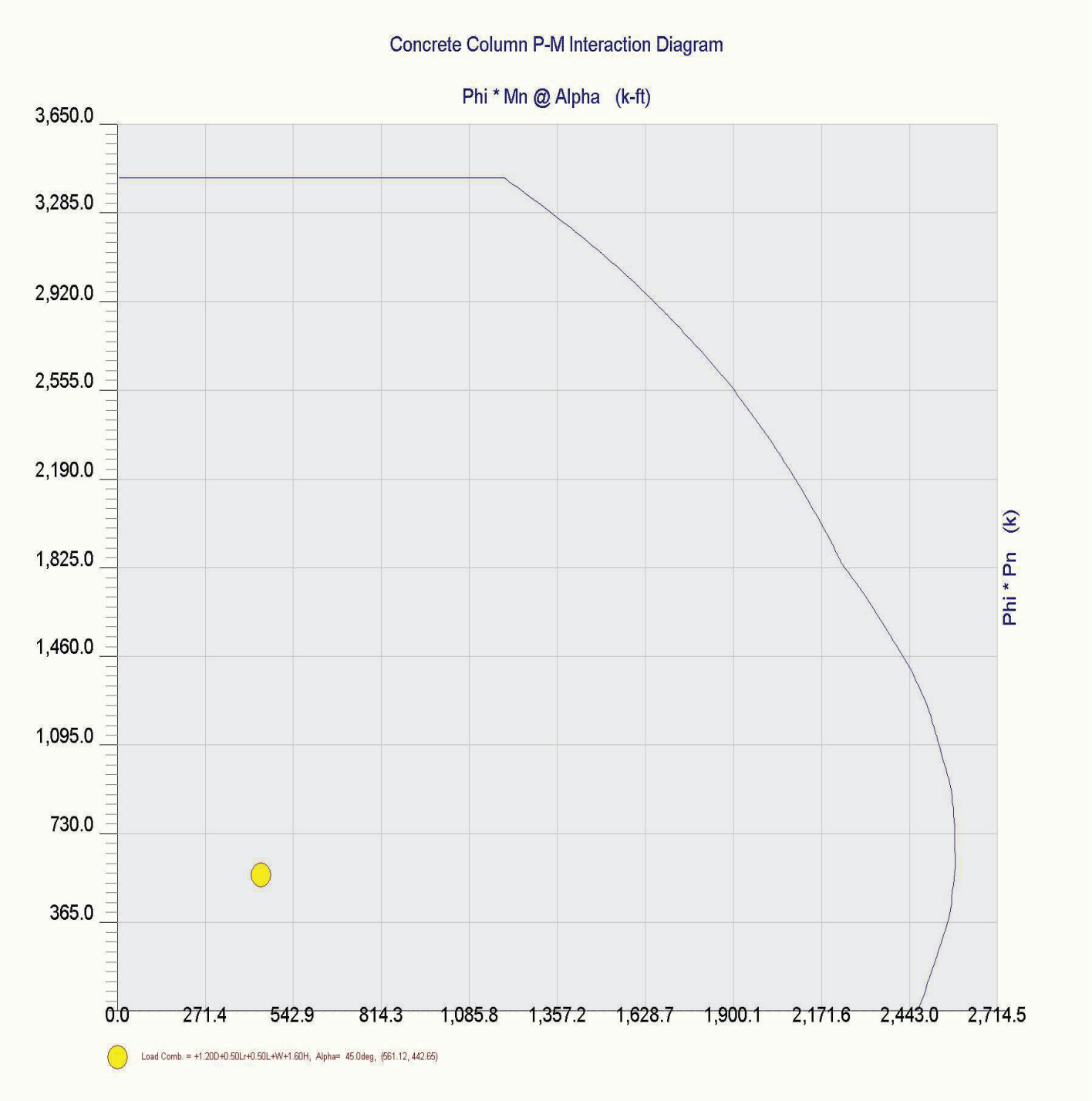

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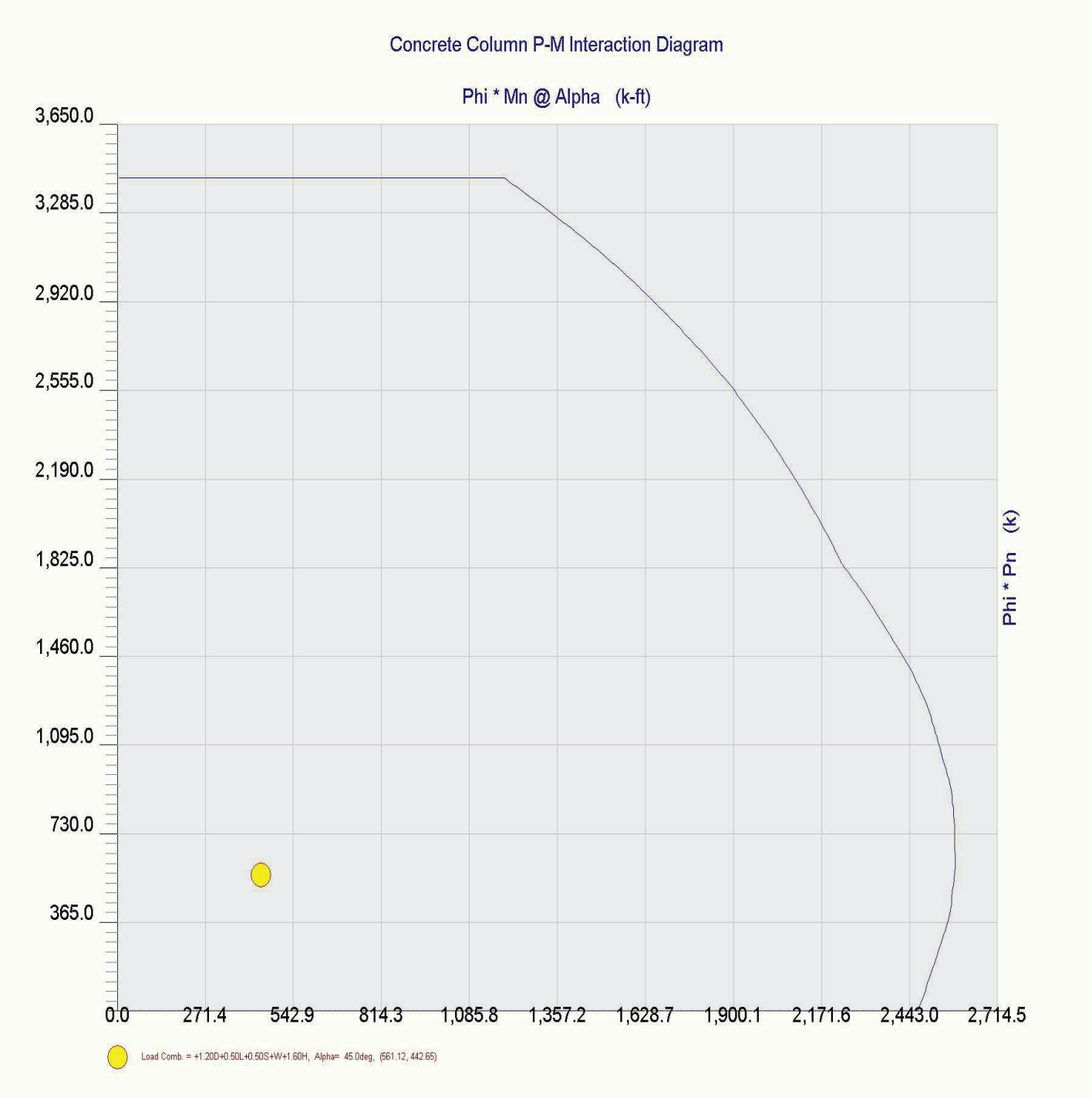

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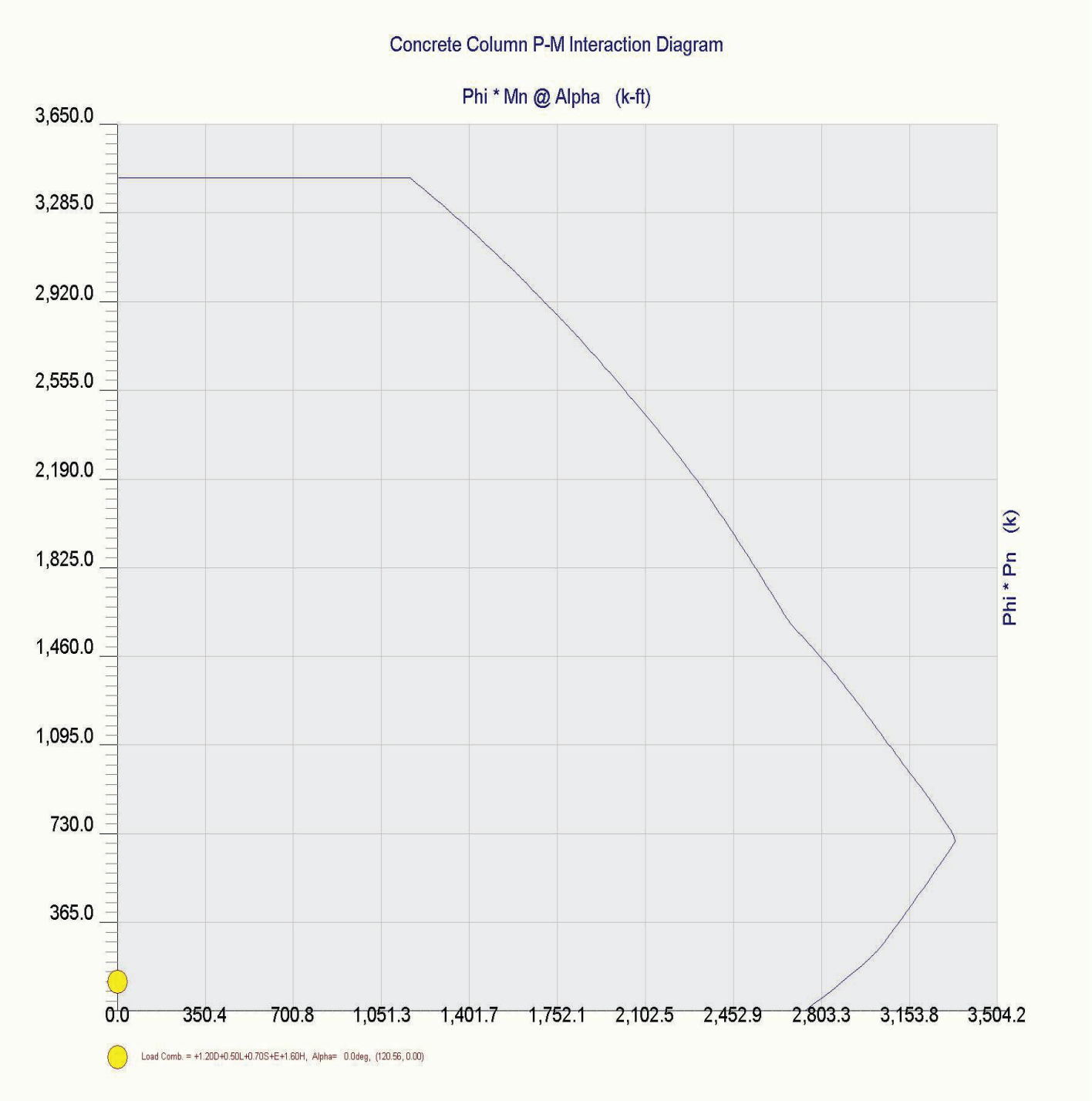
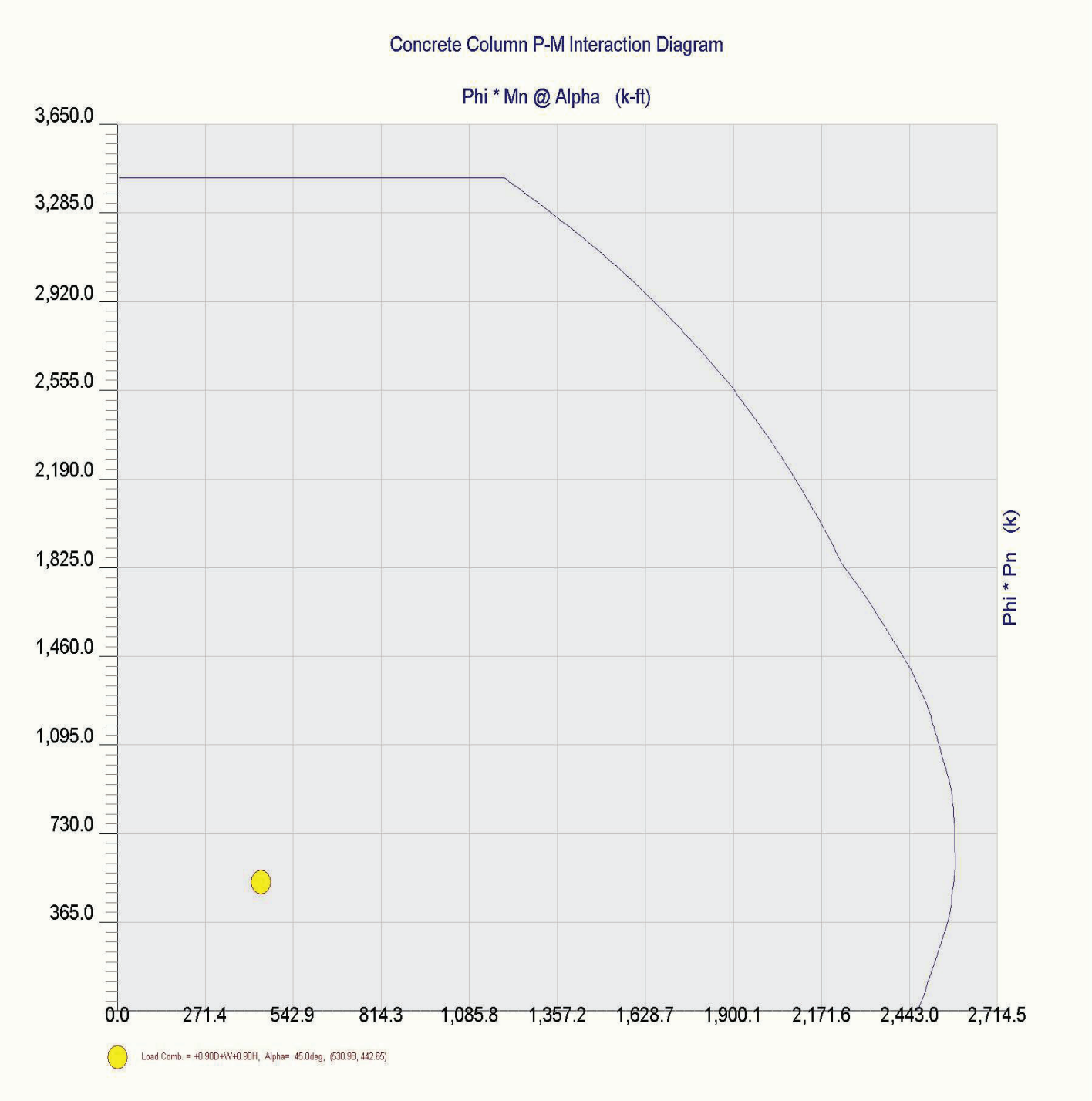


Concrete Column

DESCRIPTION: Pedestal Analysis



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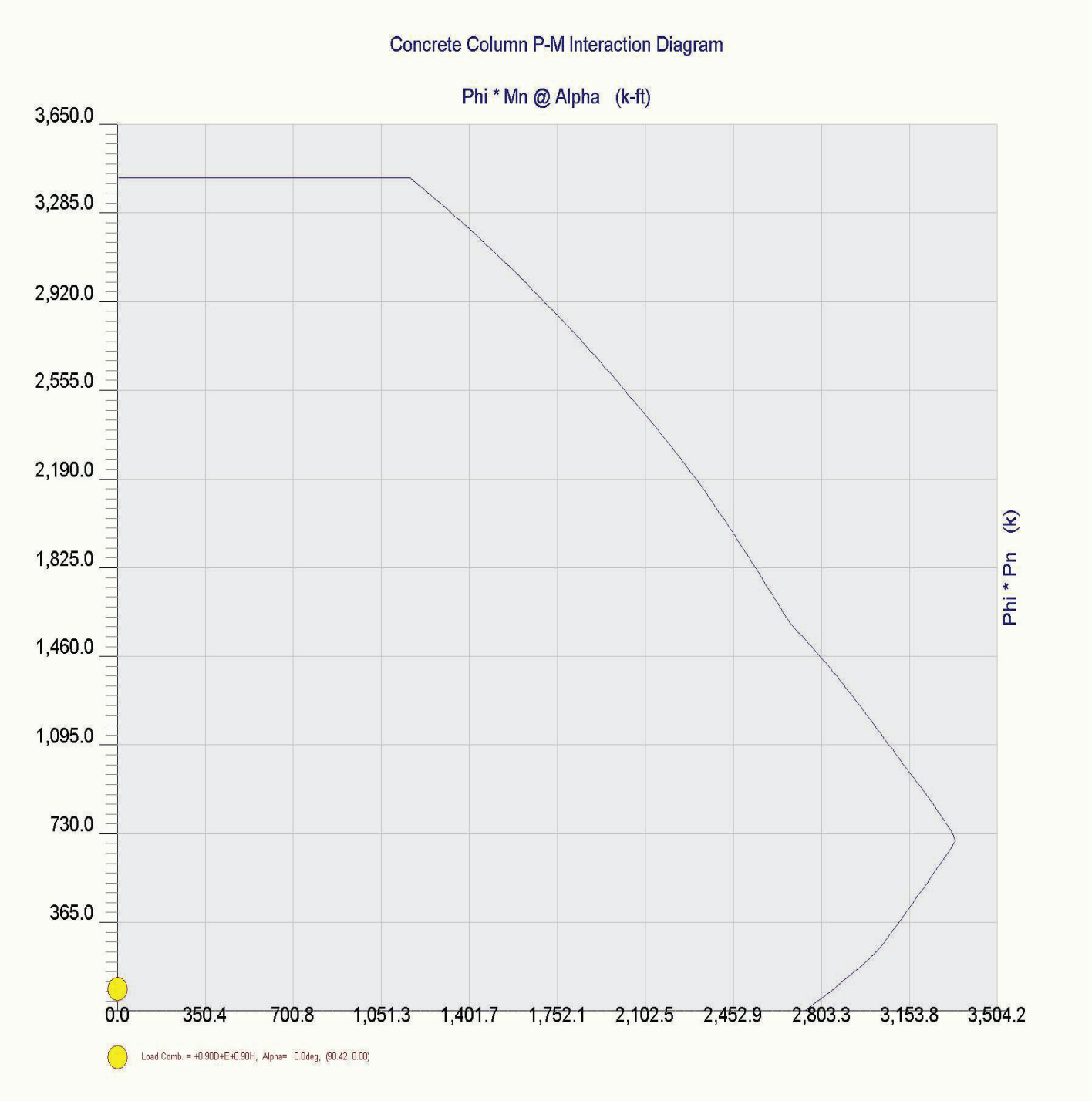


EXHIBIT 4

March 24, 2022

Centerline Communications
750 West Center Street, Suite #301
West Bridgewater, MA 02379

RE:		
	Site Number:	CT2036
	FA Number:	10034996
	PACE Number:	MRCTB055784
	PT Number:	2051A11L77
	Site Name:	CHESHIRE SW
	Site Address:	751 Higgins Road Cheshire, CT 06410

To Whom It May Concern:

Hudson Design Group LLC (HDG) has been authorized by Centerline Communications to perform a mount analysis on the existing AT&T antenna/RRH mounts to determine their capability of supporting the following additional loading:

- (1) DMP65R-BU8DA Antennas (96.0"x20.7"x7.7" – Wt. = 119 lbs. /each)
- (2) DMP65R-BU6DA Antennas (71.2"x20.7"x7.7" – Wt. = 80 lbs. /each)
- (3) B14 4478 RRH's (18.1"x13.4"x8.3" – Wt. = 60 lbs. /each)
- (3) RRUS-32 B2 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)
- (3) RRUS-32 B66A RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)
- (3) B5/B12 4449 RRH's (17.9"x13.2"x9.4" – Wt. = 73 lbs. /each)
- (3) RRUS-32 B30 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each)
- **(1) TPA65R-BU8DA-K Antennas (96.0"x20.7"x7.7" – Wt. = 87 lbs. /each)**
- **(2) TPA65R-BU6DA-K Antennas (71.2"x20.7"x7.7" – Wt. = 69 lbs. /each)**
- **(3) AIR6449 Antennas (30.6"x15.9"x10.6" – Wt. 82 lbs. /each)**
- **(3) AIR6419 Antennas (31.1"x16.1"x7.3" – Wt. = 66 lbs. /each)**
- **(3) DC9-48-60-24-8C-EV Surge Arrestor (24.0"x9.7" Ø – Wt. = 33 lbs.)**

**Proposed equipment shown in bold.*

No original structural design documents or fabrication drawings were available for the existing mounts. Previous HDG Mount Analysis dated June 21, 2021, was used to perform this analysis. HDG obtained visual inspection photos of the existing AT&T antenna mounts on December 30, 2021.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-H, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2015 with 2018 Connecticut State Building Code, and AT&T Mount Technical Directive – R16.
- HDG considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all around the mount. Per TIA-222-H and Appendix N of the Connecticut State Building Code, the max basic wind speed for this site is equal to 125 mph with a max basic wind speed with ice of 50 mph and a max ice thickness of 1.0 in. An escalated ice thickness of 1.23 in was used for this analysis.
- HDG considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.
- HDG considers this site to be topographic category 1; tower is located on flat terrain or the bottom of a hill or ridge.
- HDG considers this site to have a spectral response acceleration parameter at short periods, S_S, of 0.186 and a spectral response acceleration parameter at a period of 1 second, S_1, of 0.063.
- The existing mount is secured to the existing self-supporting tower with threaded rods and steel plates tightened to the existing catwalk handrail system. HDG considers the threaded rods as the governing connection.

Based on our evaluation, we have determined that the existing mounts **ARE CAPABLE** of supporting the proposed installation.

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Existing Alpha Sector Mount Rating	25	LC7	79%	**PASS**
Existing Beta Sector Mount Rating	93	LC7	97%	**PASS**
Existing Gamma Sector Mount Rating	153	LC7	51%	**PASS**

This determination was based on the following limitations and assumptions:

1. HDG is not responsible for any modifications completed prior to and hereafter which HDG was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mount has been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. HDG performed a localized analysis on the mount itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,
Hudson Design Group LLC

Michael Cabral
Vice President

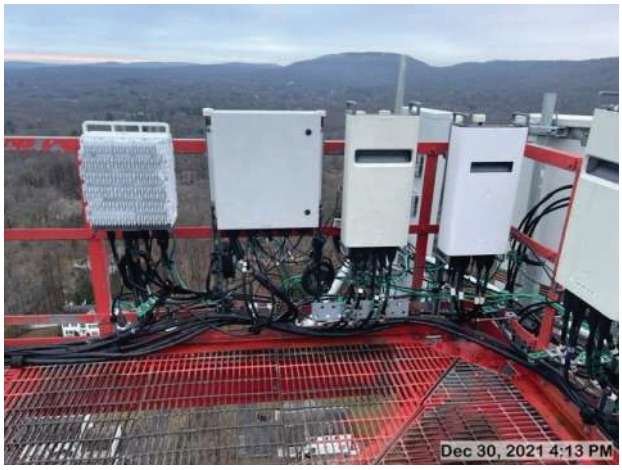
Daniel P. Hamm, PE
Principal

FIELD PHOTOS:


Dec 30, 2021 4:12 PM


Dec 30, 2021 4:12 PM


Dec 30, 2021 4:13 PM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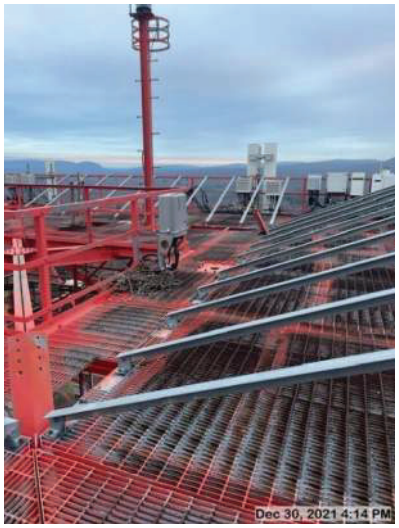
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HUDSON
Design Group LLC

Wind & Ice
Calculations

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

2.6.5.2 Velocity Pressure Coeff:

$K_z = 2.01\ (z/z_g)^{2/\alpha}$

z=	255	(ft)
z_g=	1200	(ft)
α=	7.0	

K_z= 1.291

$K_{zmin} \le K_z \le 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_c
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.2 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$K_{zt} = [1+(K_c K_t/K_h)]^2$ $\quad K_h = e^{(f*z/H)}$

K_{zt}= 1

(If Category 1 then K_{zt}=1.0)

Category= **1**

K_h=	1	
K_c=	0.9	(from Table 2-4)
K_t=	0	(from Table 2-5)
f=	0	(from Table 2-5)
z=	255	
z_s=	280	(Mean elevation of base of structure above sea level)
H=	0	(Ht. of the crest above surrounding terrain)
K_{zt}=	1.00	(from 2.6.6.2.1)
K_e=	0.99	(from 2.6.8)

2.6.10 Design Ice Thickness

Max Ice Thickness = t_i = 1.00 in
Importance Factor = I= 1.0 (from Table 2-3)
K_{iz} = 1.23 (from Sec. 2.6.10)

$t_{iz} = t_i * I * K_{iz} * (K_{zt})^{0.35}$ $\quad t_{iz}$ = 1.23 in

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2.6.9 Gust Effect Factor

2.6.9.1 Self Supporting Lattice Structures

G_h = 1.0 Latticed Structures > 600 ft

G_h = 0.85 Latticed Structures 450 ft or less

G_h = 0.85 + 0.15 [h/150 - 3.0] h= ht. of structure

h=	250	G_h=	0.85
2.6.9.2 Guyed Masts		G_h=	0.85
2.6.9.3 Pole Structures		G_h=	1.1
2.6.9 Appurtenances		G_h=	1.0

2.6.9.4 Structures Supported on Other Structures
(Cantilivered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5)

G_h=	1.35	**Gh=**	**1.00**

2.6.11.2 Design Wind Force on Appurtenances

$F = q_z * G_h * (EPA)_A$

q_z= $0.00256 * K_z * K_{zt} * K_s * K_e * K_d * V_{max}^2$

		K_z=	1.291	(from 2.6.5.2)
		K_{zt}=	1.0	(from 2.6.6.2.1)
		K_s=	1.0	(from 2.6.7)
q_z=	**43.46**	K_e=	0.99	(from 2.6.8)
$q_{z\ (ice)}$=	**6.95**	K_d=	0.85	(from Table 2-2)
$q_{z\ (30)}$=	**2.50**	V_{max}=	125	mph (Ultimate Wind Speed)
		$V_{max\ (ice)}$=	50	mph
		V_{30}=	30	mph

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95
Tubular pole structures supporting antennas enclosed within a cylindrical shroud	1.00

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Determine Ca:

Table 2-9

Force Coefficients (Ca) for Appurtenances				
Member Type		Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
		Ca	Ca	Ca
Flat		1.2	1.4	2.0
Square/Rectangular HSS		1.2 - 2.8(r_s) ≥ 0.85	1.4 - 4.0(r_s) ≥ 0.90	2.0 - 6.0(r_s) ≥ 1.25
Round	C < 39 (Subcritical)	0.7	0.8	1.2
	39 ≤ C ≤ 78 (Transitional)	$4.14/(C^{0.485})$	$3.66/(C^{0.415})$	$46.8/(C^{1.0})$
	C > 78 (Supercritical)	0.5	0.6	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
(Aspect ratio is independent of the spacing between support points of a linear appurtenance,

Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = 1.23 in | **Angle =** 0 (deg) | **Equivalent Angle =** 180 (deg)

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	4.64	1.30	777	143	45
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.44	1.24	552	102	32
AIR6449 Antenna	30.6	15.9	10.6	3.38	1.92	1.20	176	35	10
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.93	1.20	181	36	10
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	4.64	1.30	777	143	45
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.44	1.24	552	102	32
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.36	1.20	86	18	5
B5/B12 4449 RRH (Side)	17.9	9.4	13.2	1.17	1.90	1.20	61	14	4
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	2.25	1.20	119	25	7
RRUS-32 B66A RRH (Side)	27.2	7.0	12.1	1.32	3.89	1.26	72	17	4
B14 4478 RRH	18.1	13.4	8.3	1.68	1.35	1.20	88	19	5
B14 4478 RRH (Side)	18.1	8.3	13.4	1.04	2.18	1.20	54	13	3
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	2.25	1.20	119	25	7
RRUS-32 B30 RRH (Side)	27.2	7.0	12.1	1.32	3.89	1.26	72	17	4
RRUS-32 B30 RRH (Shielded)	27.2	0.0	7.0	0.00	0.00	1.20	0	4	0
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	2.25	1.20	119	25	7
RRUS-32 B2 RRH (Side)	27.2	7.0	12.1	1.32	3.89	1.26	72	17	4
Surge Arrestor	24.0	9.7	9.7	1.62	2.47	0.70	49	11	3
5x2-3/4 Angle	2.8	12.0	-	0.23	0.23	1.25	12		
3x3 Angle	3.0	12.0	-	0.25	0.25	1.25	14		
2-1/2x2-1/2 Angle	2.5	12.0	-	0.21	0.21	1.25	11		
PL 2x1/2	2.0	12.0	-	0.17	0.17	1.25	9		
HSS 3x3	3.0	12.0	-	0.25	0.25	1.25	14		
3-1/2" Pipe	4.0	12.0	-	0.33	0.33	0.70	10		
2-1/2" Pipe	2.9	12.0	-	0.24	0.24	0.70	7		
2" Pipe	2.4	12.0	-	0.20	0.20	0.70	6		

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Angle =	30	(deg)	Ice Thickness =	1.23	in.	Equivalent Angle =	210	(deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	671
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	475
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	176	119	162
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	181	88	158
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	671
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	475
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	86	61	79
B5/B12 4449 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	43	86	54
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B66A RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	88	54	79
B14 4478 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	44	88	55
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B30 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78
RRUS-32 B30 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	36	72	45
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B2 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
TPA65R-BU6DA-K Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	33
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	32
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
B5/B12 4449 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	17
B5/B12 4449 RRH (Side)	20.4	7.8	15.7	1.11	2.21	2.60	1.30	1.20	1.20	9	18	12
RRUS-32 B66A RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B66A RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16
B14 4478 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	17
B14 4478 RRH (Side)	20.6	7.9	15.9	1.13	2.26	2.59	1.30	1.20	1.20	9	19	12
RRUS-32 B30 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B30 RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16
RRUS-32 B30 RRH (Shielded)	29.7	3.6	9.5	0.75	1.95	8.15	3.14	1.44	1.23	7	17	10
RRUS-32 B2 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B2 RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	9
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	9
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	5
B5/B12 4449 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	2	5	3
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B66A RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	5
B14 4478 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	3	5	3
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B30 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4
RRUS-32 B30 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	2	4	3
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B2 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4

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WIND LOADS

Angle = 60 (deg) | Ice Thickness = 1.23 in. | Equivalent Angle = 240 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	459
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	321
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	176	119	133
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	181	88	111
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	459
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	321
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	86	61	67
B5/B12 4449 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	64	86	80
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B66A RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	88	54	63
B14 4478 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	66	88	82
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B30 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112
RRUS-32 B30 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	71	72	72
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B2 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112

WIND LOADS WITH ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
TPA65R-BU6DA-K Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	28
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	24
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
B5/B12 4449 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	15
B5/B12 4449 RRH (Side)	20.4	11.7	15.7	1.66	2.21	1.73	1.30	1.20	1.20	14	18	17
RRUS-32 B66A RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B66A RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23
B14 4478 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	14
B14 4478 RRH (Side)	20.6	11.9	15.9	1.70	2.26	1.73	1.30	1.20	1.20	14	19	18
RRUS-32 B30 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B30 RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23
RRUS-32 B30 RRH (Shielded)	29.7	8.2	9.5	1.69	1.95	3.62	3.14	1.25	1.23	15	17	16
RRUS-32 B2 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B2 RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23

WIND LOADS AT 30 MPH:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	8
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	6
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
B5/B12 4449 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	4	5	5
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B66A RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	4
B14 4478 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	4	5	5
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B30 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6
RRUS-32 B30 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	4	4	4
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B2 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM Checked By: MSC

HUDSON Design Group LLC

WIND LOADS

Angle =	90	(deg)	Ice Thickness =	1.23	in.	Equivalent Angle =	270	(deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	353
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	244
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	176	119	119
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	181	88	88
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	353
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	244
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	86	61	61
B5/B12 4449 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	61	86	86
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	72
RRUS-32 B66A RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	72	119	119
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	88	54	54
B14 4478 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	54	88	88
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	72
RRUS-32 B30 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	72	119	119
RRUS-32 B30 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	72	72
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	72
RRUS-32 B2 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	72	119	119

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	72
TPA65R-BU6DA-K Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	51
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	25
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	20
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	72
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	51
B5/B12 4449 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	14
B5/B12 4449 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	18
RRUS-32 B66A RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	17
RRUS-32 B66A RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	25
B14 4478 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	13
B14 4478 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	19
RRUS-32 B30 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	17
RRUS-32 B30 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	25
RRUS-32 B30 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	17
RRUS-32 B2 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	17
RRUS-32 B2 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	25

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	20
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	14
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	7
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	5
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	20
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	14
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
B5/B12 4449 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	5
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	4
RRUS-32 B66A RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	7
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	3
B14 4478 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	5
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	4
RRUS-32 B30 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	7
RRUS-32 B30 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	4
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	4
RRUS-32 B2 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	7

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM Checked By: MSC

HUDSON Design Group LLC

WIND LOADS

Angle =	120	(deg)	Ice Thickness =	1.23	in.	Equivalent Angle =	300	(deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	459
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	321
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	176	119	133
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	181	88	111
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	459
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	321
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	86	61	67
B5/B12 4449 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	64	86	80
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B66A RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	88	54	63
B14 4478 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	66	88	82
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B30 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112
RRUS-32 B30 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	71	72	72
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	84
RRUS-32 B2 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	91	119	112

WIND LOADS WITH ICE:

TPA65R-BU8DA-K Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
TPA65R-BU6DA-K Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	28
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	24
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
B5/B12 4449 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	15
B5/B12 4449 RRH (Side)	20.4	11.7	15.7	1.66	2.21	1.73	1.30	1.20	1.20	14	18	17
RRUS-32 B66A RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B66A RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23
B14 4478 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	14
B14 4478 RRH (Side)	20.6	11.9	15.9	1.70	2.26	1.73	1.30	1.20	1.20	14	19	18
RRUS-32 B30 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B30 RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23
RRUS-32 B30 RRH (Shielded)	29.7	8.2	9.5	1.69	1.95	3.62	3.14	1.25	1.23	15	17	16
RRUS-32 B2 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 B2 RRH (Side)	29.7	10.9	14.6	2.25	3.00	2.72	2.04	1.21	1.20	19	25	23

WIND LOADS AT 30 MPH:

TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	8
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	6
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
B5/B12 4449 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	4	5	5
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B66A RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	4
B14 4478 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	4	5	5
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B30 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6
RRUS-32 B30 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	4	4	4
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 B2 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	5	7	6

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM Checked By: MSC

HUDSON Design Group LLC

WIND LOADS

Angle = 150 (deg) | Ice Thickness = 1.23 in. | Equivalent Angle = 330 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	671
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	475
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	176	119	162
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	181	88	158
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	777	353	671
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	552	244	475
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	86	61	79
B5/B12 4449 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	43	86	54
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B66A RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	88	54	79
B14 4478 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	44	88	55
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B30 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78
RRUS-32 B30 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	36	72	45
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	119	72	108
RRUS-32 B2 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	64	119	78

WIND LOADS WITH ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
TPA65R-BU6DA-K Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	33
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	32
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
B5/B12 4449 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	17
B5/B12 4449 RRH (Side)	20.4	7.8	15.7	1.11	2.21	2.60	1.30	1.20	1.20	9	18	12
RRUS-32 B66A RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B66A RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16
B14 4478 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	17
B14 4478 RRH (Side)	20.6	7.9	15.9	1.13	2.26	2.59	1.30	1.20	1.20	9	19	12
RRUS-32 B30 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B30 RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16
RRUS-32 B30 RRH (Shielded)	29.7	3.6	9.5	0.75	1.95	8.15	3.14	1.44	1.23	7	17	10
RRUS-32 B2 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 B2 RRH (Side)	29.7	7.3	14.6	1.50	3.00	4.08	2.04	1.27	1.20	13	25	16

WIND LOADS AT 30 MPH:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs) (normal)	Force (lbs) (side)	Force (lbs) (angle)
TPA65R-BU8DA-K Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
TPA65R-BU6DA-K Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	9
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	9
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
B5/B12 4449 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	5
B5/B12 4449 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	2	5	3
RRUS-32 B66A RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B66A RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4
B14 4478 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	5
B14 4478 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	3	5	3
RRUS-32 B30 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B30 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4
RRUS-32 B30 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	2	4	3
RRUS-32 B2 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 B2 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	4	7	4

Date: 3/23/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

ICE WEIGHT CALCULATIONS

Thickness of ice: 1.23 in.
Density of ice: 56 pcf

TPA65R-BU8DA-K Antenna

Weight of ice based on total radial SF area:

Height (in):	96.0	
Width (in):	20.7	
Depth (in):	7.7	
Total weight of ice on object:		280 lbs
Weight of object:	87.0	lbs
Combined weight of ice and object:		367 lbs

TPA65R-BU6DA-K Antenna

Weight of ice based on total radial SF area:

Height (in):	71.2	
Width (in):	20.7	
Depth (in):	7.7	
Total weight of ice on object:		208 lbs
Weight of object:	69.0	lbs
Combined weight of ice and object:		277 lbs

AIR6449 Antenna

Weight of ice based on total radial SF area:

Height (in):	30.6	
Width (in):	15.9	
Depth (in):	10.6	
Total weight of ice on object:		78 lbs
Weight of object:	82.0	lbs
Combined weight of ice and object:		160 lbs

AIR6419 Antenna

Weight of ice based on total radial SF area:

Height (in):	31.1	
Width (in):	16.1	
Depth (in):	7.3	
Total weight of ice on object:		74 lbs
Weight of object:	66.0	lbs
Combined weight of ice and object:		140 lbs

DMP65R-BU8DA Antenna

Weight of ice based on total radial SF area:

Height (in):	96.0	
Width (in):	20.7	
Depth (in):	7.7	
Total weight of ice on object:		280 lbs
Weight of object:	119.0	lbs
Combined weight of ice and object:		399 lbs

DMP65R-BU6DA Antenna

Weight of ice based on total radial SF area:

Height (in):	71.2	
Width (in):	20.7	
Depth (in):	7.7	
Total weight of ice on object:		208 lbs
Weight of object:	80.0	lbs
Combined weight of ice and object:		288 lbs

B5/B12 4449 RRH

Weight of ice based on total radial SF area:

Height (in):	17.9	
Width (in):	13.2	
Depth (in):	9.4	
Total weight of ice on object:		39 lbs
Weight of object:	73.0	lbs
Combined weight of ice and object:		112 lbs

RRUS-32 B66A RRH

Weight of ice based on total radial SF area:

Height (in):	27.2	
Width (in):	12.1	
Depth (in):	7.0	
Total weight of ice on object:		52 lbs
Weight of object:	60.0	lbs
Combined weight of ice and object:		112 lbs

B14 4478 RRH

Weight of ice based on total radial SF area:

Height (in):	18.1	
Width (in):	13.4	
Depth (in):	8.3	
Total weight of ice on object:		39 lbs
Weight of object:	60.0	lbs
Combined weight of ice and object:		99 lbs

RRUS-32 B30 RRH

Weight of ice based on total radial SF area:

Height (in):	27.2	
Width (in):	12.1	
Depth (in):	7.0	
Total weight of ice on object:		52 lbs
Weight of object:	60.0	lbs
Combined weight of ice and object:		112 lbs

Date: 3/23/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

RRUS-32 B2 RRH

Weight of ice based on total radial SF area:

Height (in):	27.2	
Width (in):	12.1	
Depth (in):	7.0	
Total weight of ice on object:		52 lbs
Weight of object:	60.0	lbs
Combined weight of ice and object:		112 lbs

Squid Surge Arrestor

Weight of ice based on total radial SF area:

Depth (in):	24.0	
Diameter(in):	9.7	
Total weight of ice on object:		33 lbs
Weight of object:	33	lbs
Combined weight of ice and object:		66 lbs

L 5x2-3/4 Angles

Weight of ice based on total radial SF area:

Height (in):	2.75	
Width (in):	5	
Per foot weight of ice on object:		10 plf

L 2-1/2x2-1/2 Angles

Weight of ice based on total radial SF area:

Height (in):	2.5	
Width (in):	2.5	
Per foot weight of ice on object:		7 plf

L 3x3 Angles

Weight of ice based on total radial SF area:

Height (in):	3	
Width (in):	3	
Per foot weight of ice on object:		8 plf

HSS 3x3

Weight of ice based on total radial SF area:

Height (in):	3	
Width (in):	3	
Per foot weight of ice on object:		8 plf

PL 2x1/2

Weight of ice based on total radial SF area:

Height (in):	2	
Width (in):	0.25	
Per foot weight of ice on object:		5 plf

3-1/2" Pipe

Per foot weight of ice:

diameter (in):	4	
Per foot weight of ice on object:		8 plf

2-1/2" pipe

Per foot weight of ice:

diameter (in):	2.88	
Per foot weight of ice on object:		6 plf

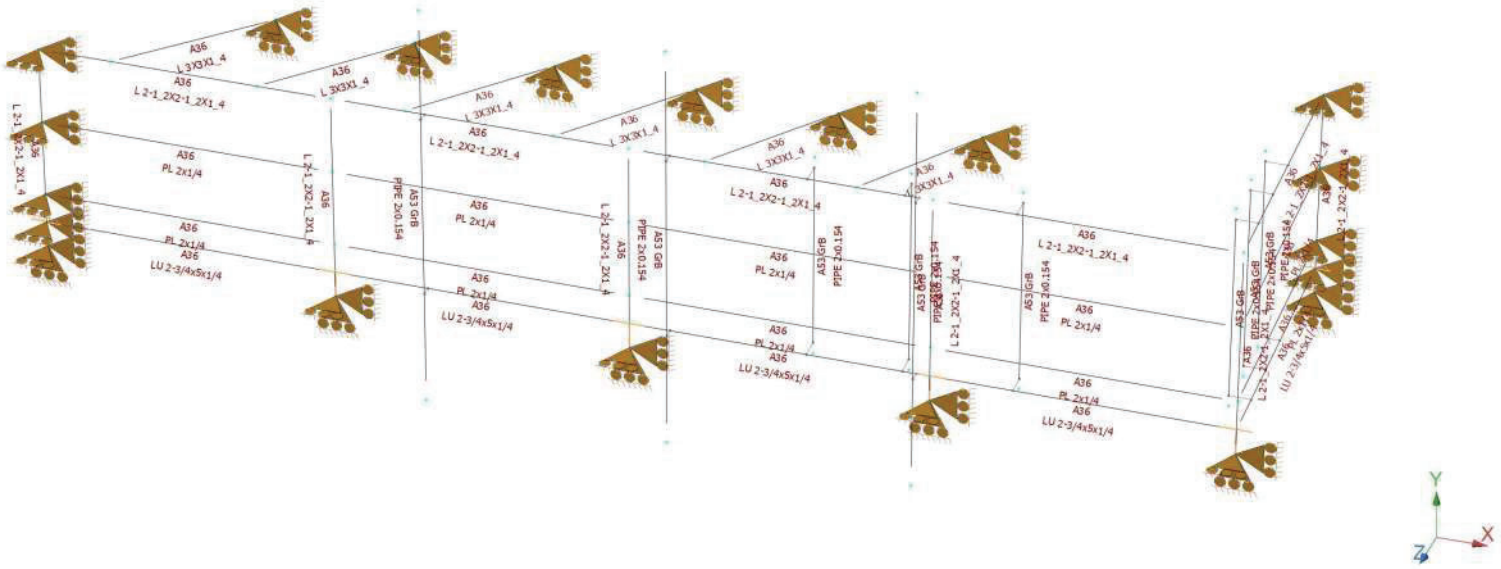
2" pipe

Per foot weight of ice:

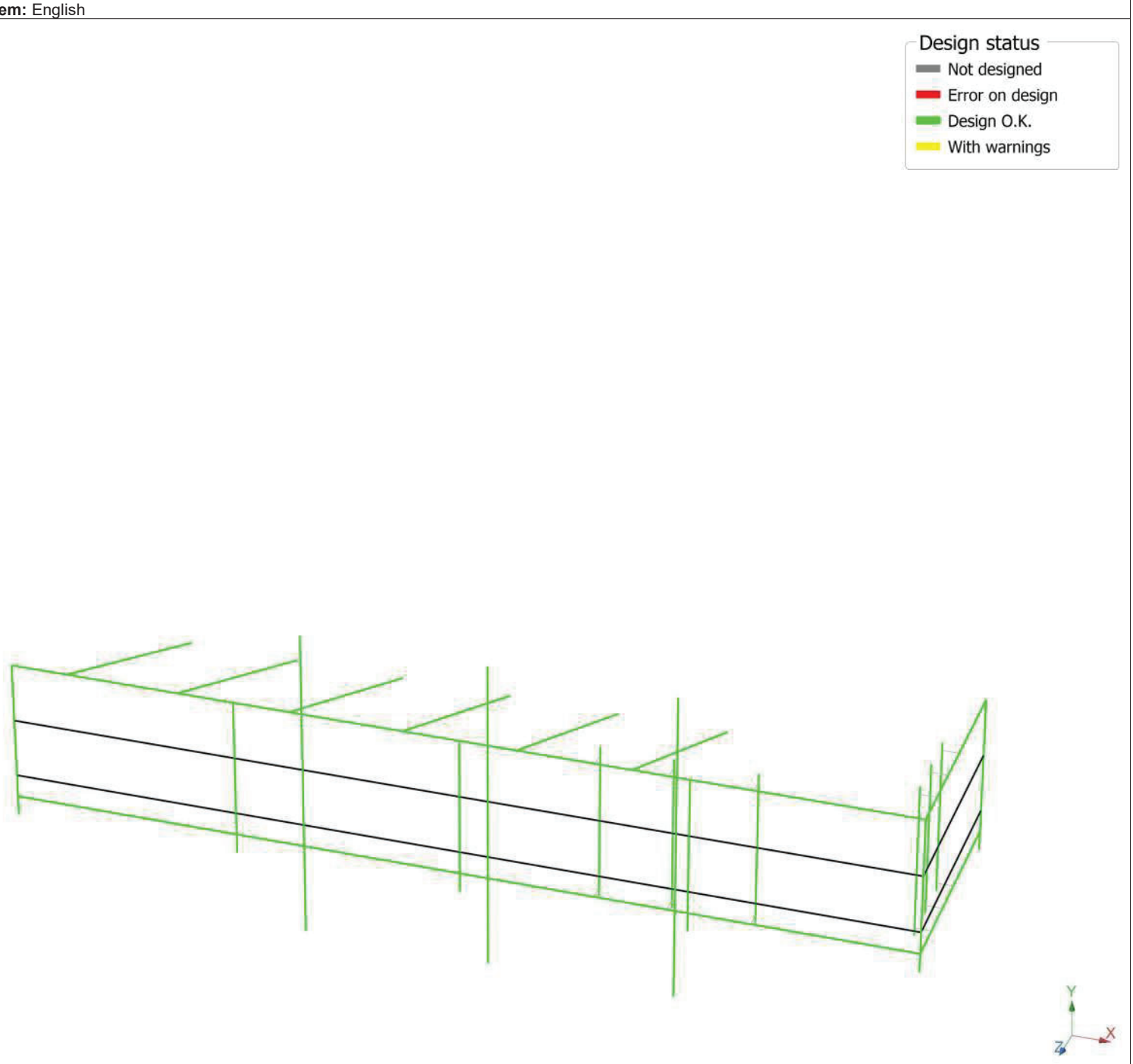
diameter (in):	2.38	
Per foot weight of ice on object:		5 plf

Alpha Sector
Calculations


Y
X
Z


A36
L 3X3X1_4
A36
L 2-1_2X2-1_2X1_4
A36
PL 2x1/4
A36
LU 2-3/4x5x1/4
A53 GrB
PIPE 2x0.154
Y
X
Z

Current Date: 3/24/2022 2:35 PM
Units system: English



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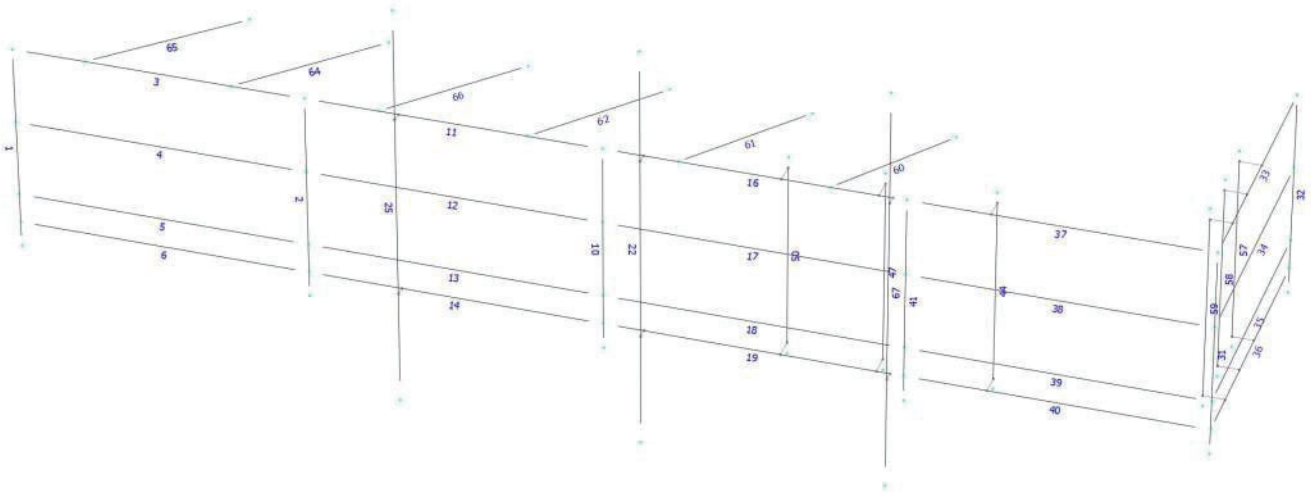
Units system: English



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Units system: English

Load data

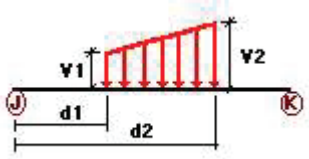
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	1	z	-0.011	-0.011	0.00	No	100.00	Yes
	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	3	z	-0.011	-0.011	0.00	No	100.00	Yes
	4	z	-0.009	-0.009	0.00	No	100.00	Yes
	5	z	-0.009	-0.009	0.00	No	100.00	Yes
	6	z	-0.012	-0.012	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes

	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes
	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	50	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	59	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes
	62	z	-0.014	-0.014	0.00	No	100.00	Yes
	64	z	-0.014	-0.014	0.00	No	100.00	Yes
	65	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
W30	1	z	-0.011	-0.011	0.00	No	100.00	Yes
	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	3	z	-0.011	-0.011	0.00	No	100.00	Yes
	4	z	-0.009	-0.009	0.00	No	100.00	Yes
	5	z	-0.009	-0.009	0.00	No	100.00	Yes
	6	z	-0.012	-0.012	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes
	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes
	22	z	-0.006	-0.006	0.00	No	100.00	Yes
	25	z	-0.006	-0.006	0.00	No	100.00	Yes
	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	32	z	-0.011	-0.011	0.00	No	100.00	Yes
	33	z	-0.011	-0.011	0.00	No	100.00	Yes
	34	z	-0.009	-0.009	0.00	No	100.00	Yes
	35	z	-0.009	-0.009	0.00	No	100.00	Yes
	36	z	-0.012	-0.012	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	50	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	59	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes
	62	z	-0.014	-0.014	0.00	No	100.00	Yes

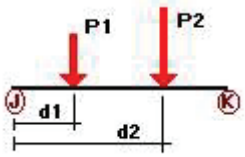
	64	z	-0.014	-0.014	0.00	No	100.00	Yes
	65	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
	67	z	-0.006	-0.006	0.00	No	100.00	Yes
W60	1	x	-0.011	-0.011	0.00	No	100.00	Yes
	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	3	x	-0.011	-0.011	0.00	No	100.00	Yes
	4	x	-0.009	-0.009	0.00	No	100.00	Yes
	5	x	-0.009	-0.009	0.00	No	100.00	Yes
	6	x	-0.012	-0.012	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	22	x	-0.006	-0.006	0.00	No	100.00	Yes
	25	x	-0.006	-0.006	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	59	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	67	x	-0.006	-0.006	0.00	No	100.00	Yes
W90	22	x	-0.006	-0.006	0.00	No	100.00	Yes
	25	x	-0.006	-0.006	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	59	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes

	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	67	x	-0.006	-0.006	0.00	No	100.00	Yes
W120	1	x	-0.011	-0.011	0.00	No	100.00	Yes
	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	3	x	-0.011	-0.011	0.00	No	100.00	Yes
	4	x	-0.009	-0.009	0.00	No	100.00	Yes
	5	x	-0.009	-0.009	0.00	No	100.00	Yes
	6	x	-0.012	-0.012	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	22	x	-0.006	-0.006	0.00	No	100.00	Yes
	25	x	-0.006	-0.006	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	59	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	67	x	-0.006	-0.006	0.00	No	100.00	Yes
W150	1	z	0.011	0.011	0.00	No	100.00	Yes
	2	z	0.011	0.011	0.00	No	100.00	Yes
	3	z	0.011	0.011	0.00	No	100.00	Yes
	4	z	0.009	0.009	0.00	No	100.00	Yes
	5	z	0.009	0.009	0.00	No	100.00	Yes
	6	z	0.012	0.012	0.00	No	100.00	Yes
	10	z	0.011	0.011	0.00	No	100.00	Yes
	11	z	0.011	0.011	0.00	No	100.00	Yes
	12	z	0.009	0.009	0.00	No	100.00	Yes
	13	z	0.009	0.009	0.00	No	100.00	Yes
	14	z	0.012	0.012	0.00	No	100.00	Yes
	16	z	0.011	0.011	0.00	No	100.00	Yes
	17	z	0.009	0.009	0.00	No	100.00	Yes

	18	z	0.009	0.009	0.00	No	100.00	Yes
	19	z	0.012	0.012	0.00	No	100.00	Yes
	22	z	0.006	0.006	0.00	No	100.00	Yes
	25	z	0.006	0.006	0.00	No	100.00	Yes
	31	z	0.011	0.011	0.00	No	100.00	Yes
	32	z	0.011	0.011	0.00	No	100.00	Yes
	33	z	0.011	0.011	0.00	No	100.00	Yes
	34	z	0.009	0.009	0.00	No	100.00	Yes
	35	z	0.009	0.009	0.00	No	100.00	Yes
	36	z	0.012	0.012	0.00	No	100.00	Yes
	37	z	0.011	0.011	0.00	No	100.00	Yes
	38	z	0.009	0.009	0.00	No	100.00	Yes
	39	z	0.009	0.009	0.00	No	100.00	Yes
	40	z	0.012	0.012	0.00	No	100.00	Yes
	41	z	0.011	0.011	0.00	No	100.00	Yes
	44	z	0.006	0.006	0.00	No	100.00	Yes
	47	z	0.006	0.006	0.00	No	100.00	Yes
	50	z	0.006	0.006	0.00	No	100.00	Yes
	57	z	0.006	0.006	0.00	No	100.00	Yes
	58	z	0.006	0.006	0.00	No	100.00	Yes
	59	z	0.006	0.006	0.00	No	100.00	Yes
	60	z	0.014	0.014	0.00	No	100.00	Yes
	61	z	0.014	0.014	0.00	No	100.00	Yes
	62	z	0.014	0.014	0.00	No	100.00	Yes
	64	z	0.014	0.014	0.00	No	100.00	Yes
	65	z	0.014	0.014	0.00	No	100.00	Yes
	66	z	0.014	0.014	0.00	No	100.00	Yes
	67	z	0.006	0.006	0.00	No	100.00	Yes
Di	1	y	-0.007	-0.007	0.00	No	100.00	Yes
	2	y	-0.007	-0.007	0.00	No	100.00	Yes
	3	y	-0.007	-0.007	0.00	No	100.00	Yes
	4	y	-0.005	-0.005	0.00	No	100.00	Yes
	5	y	-0.005	-0.005	0.00	No	100.00	Yes
	6	y	-0.01	-0.01	0.00	No	100.00	Yes
	10	y	-0.007	-0.007	0.00	No	100.00	Yes
	11	y	-0.007	-0.007	0.00	No	100.00	Yes
	12	y	-0.005	-0.005	0.00	No	100.00	Yes
	13	y	-0.005	-0.005	0.00	No	100.00	Yes
	14	y	-0.01	-0.01	0.00	No	100.00	Yes
	16	y	-0.007	-0.007	0.00	No	100.00	Yes
	17	y	-0.005	-0.005	0.00	No	100.00	Yes
	18	y	-0.005	-0.005	0.00	No	100.00	Yes
	19	y	-0.01	-0.01	0.00	No	100.00	Yes
	22	y	-0.005	-0.005	0.00	No	100.00	Yes
	25	y	-0.005	-0.005	0.00	No	100.00	Yes
	31	y	-0.007	-0.007	0.00	No	100.00	Yes
	32	y	-0.007	-0.007	0.00	No	100.00	Yes
	33	y	-0.007	-0.007	0.00	No	100.00	Yes
	34	y	-0.005	-0.005	0.00	No	100.00	Yes
	35	y	-0.005	-0.005	0.00	No	100.00	Yes
	36	y	-0.01	-0.01	0.00	No	100.00	Yes
	37	y	-0.007	-0.007	0.00	No	100.00	Yes
	38	y	-0.005	-0.005	0.00	No	100.00	Yes
	39	y	-0.005	-0.005	0.00	No	100.00	Yes
	40	y	-0.01	-0.01	0.00	No	100.00	Yes
	41	y	-0.007	-0.007	0.00	No	100.00	Yes
	44	y	-0.005	-0.005	0.00	No	100.00	Yes
	47	y	-0.005	-0.005	0.00	No	100.00	Yes
	50	y	-0.005	-0.005	0.00	No	100.00	Yes
	57	y	-0.005	-0.005	0.00	No	100.00	Yes

58	y	-0.005	-0.005	0.00	No	100.00	Yes
59	y	-0.005	-0.005	0.00	No	100.00	Yes
60	y	-0.008	-0.008	0.00	No	100.00	Yes
61	y	-0.008	-0.008	0.00	No	100.00	Yes
62	y	-0.008	-0.008	0.00	No	100.00	Yes
64	y	-0.008	-0.008	0.00	No	100.00	Yes
65	y	-0.008	-0.008	0.00	No	100.00	Yes
66	y	-0.008	-0.008	0.00	No	100.00	Yes
67	y	-0.005	-0.005	0.00	No	100.00	Yes

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	22	y	-0.041	1.00	No
		y	-0.041	3.00	No
		y	-0.033	5.00	No
		y	-0.033	7.00	No
	25	y	-0.048	0.50	No
		y	-0.048	7.50	No
	44	y	-0.06	2.00	No
	47	y	-0.06	2.00	No
	50	y	-0.033	2.00	No
	57	y	-0.06	2.00	No
	58	y	-0.073	2.00	No
	59	y	-0.06	2.00	No
	67	y	-0.044	0.50	No
		y	-0.044	7.50	No
Wo	22	z	-0.088	1.00	No
		z	-0.088	3.00	No
		z	-0.091	5.00	No
		z	-0.091	7.00	No
	25	z	-0.389	0.50	No
		z	-0.389	7.50	No
	44	z	-0.088	2.00	No
	50	z	-0.049	2.00	No
	57	z	-0.072	2.00	No
	58	z	-0.061	2.00	No
	59	z	-0.072	2.00	No
	67	z	-0.389	0.50	No
		z	-0.389	7.50	No
W30	22	3	-0.081	1.00	No
		3	-0.081	3.00	No
		3	-0.079	5.00	No
		3	-0.079	7.00	No
	25	3	-0.336	0.50	No
		3	-0.336	7.50	No
	44	3	-0.079	2.00	No
	47	3	-0.045	2.00	No
	50	3	-0.049	2.00	No

	57	3	-0.078	2.00	No
	58	3	-0.054	2.00	No
	59	3	-0.078	2.00	No
	67	3	-0.336	0.50	No
		3	-0.336	7.50	No
W60	22	3	-0.067	1.00	No
		3	-0.067	3.00	No
		3	-0.056	5.00	No
		3	-0.056	7.00	No
	25	3	-0.23	0.50	No
		3	-0.23	7.50	No
	44	3	-0.063	2.00	No
	47	3	-0.072	2.00	No
	50	3	-0.049	2.00	No
	57	3	-0.112	2.00	No
	58	3	-0.08	2.00	No
	59	3	-0.112	2.00	No
	67	3	-0.23	0.50	No
		3	-0.23	7.50	No
W90	22	x	-0.06	1.00	No
		x	-0.06	3.00	No
		x	-0.044	5.00	No
		x	-0.044	7.00	No
	25	x	-0.177	0.50	No
		x	-0.177	7.50	No
	44	x	-0.054	2.00	No
	47	x	-0.072	2.00	No
	50	x	-0.049	2.00	No
	57	x	-0.119	2.00	No
	58	x	-0.086	2.00	No
	59	x	-0.119	2.00	No
	67	x	-0.177	0.50	No
		x	-0.177	7.50	No
W120	22	2	-0.067	1.00	No
		2	-0.067	3.00	No
		2	-0.056	5.00	No
		2	-0.056	7.00	No
	25	2	-0.23	0.50	No
		2	-0.23	7.50	No
	44	2	-0.063	2.00	No
	47	2	-0.072	2.00	No
	50	2	-0.049	2.00	No
	57	2	-0.112	2.00	No
	58	2	-0.08	2.00	No
	59	2	-0.112	2.00	No
	67	2	-0.23	0.50	No
		2	-0.23	7.50	No
W150	22	2	-0.081	1.00	No
		2	-0.081	3.00	No
		2	-0.079	5.00	No
		2	-0.079	7.00	No
	25	2	-0.336	0.50	No
		2	-0.336	7.50	No
	44	2	-0.079	2.00	No
	47	2	-0.045	2.00	No
	50	2	-0.049	2.00	No
	57	2	-0.078	2.00	No
	58	2	-0.054	2.00	No
	59	2	-0.078	2.00	No
	67	2	-0.336	0.50	No

		2	-0.336	7.50	No
Di	22	y	-0.039	1.00	No
		y	-0.039	3.00	No
		y	-0.037	5.00	No
		y	-0.037	7.00	No
	25	y	-0.14	0.50	No
		y	-0.14	7.50	No
	44	y	-0.052	2.00	No
	47	y	-0.052	2.00	No
	50	y	-0.033	2.00	No
	57	y	-0.052	2.00	No
	58	y	-0.039	2.00	No
	59	y	-0.052	2.00	No
	67	y	-0.14	0.50	No
		y	-0.14	7.50	No
WI0	22	z	-0.018	1.00	No
		z	-0.018	3.00	No
		z	-0.018	5.00	No
		z	-0.018	7.00	No
	25	z	-0.072	0.50	No
		z	-0.072	7.50	No
	44	z	-0.019	2.00	No
	47	z	-0.004	2.00	No
	50	z	-0.011	2.00	No
	57	z	-0.017	2.00	No
	58	z	-0.014	2.00	No
	59	z	-0.017	2.00	No
	67	z	-0.072	0.50	No
		z	-0.072	7.50	No
WI30	22	3	-0.017	1.00	No
		3	-0.017	3.00	No
		3	-0.016	5.00	No
		3	-0.016	7.00	No
	25	3	-0.062	0.50	No
		3	-0.062	7.50	No
	44	3	-0.017	2.00	No
	47	3	-0.01	2.00	No
	50	3	-0.011	2.00	No
	57	3	-0.016	2.00	No
	58	3	-0.012	2.00	No
	59	3	-0.016	2.00	No
	67	3	-0.062	0.50	No
		3	-0.062	7.50	No
WI60	22	3	-0.014	1.00	No
		3	-0.014	3.00	No
		3	-0.012	5.00	No
		3	-0.012	7.00	No
	25	3	-0.045	0.50	No
		3	-0.045	7.50	No
	44	3	-0.014	2.00	No
	47	3	-0.016	2.00	No
	50	3	-0.011	2.00	No
	57	3	-0.023	2.00	No
	58	3	-0.017	2.00	No
	59	3	-0.023	2.00	No
	67	3	-0.045	0.50	No
		3	-0.045	7.50	No
WI90	22	x	-0.013	1.00	No
		x	-0.013	3.00	No
		x	-0.01	5.00	No

		x	-0.01	7.00	No
	25	x	-0.036	0.50	No
		x	-0.036	7.50	No
	44	x	-0.013	2.00	No
	47	x	-0.017	2.00	No
	50	x	-0.011	2.00	No
	57	x	-0.025	2.00	No
	58	x	-0.018	2.00	No
	59	x	-0.025	2.00	No
	67	x	-0.036	0.50	No
		x	-0.036	7.50	No
WI120	22	2	-0.014	1.00	No
		2	-0.014	3.00	No
		2	-0.012	5.00	No
		2	-0.012	7.00	No
	25	2	-0.045	0.50	No
		2	-0.045	7.50	No
	44	2	-0.014	2.00	No
	47	2	-0.016	2.00	No
	50	2	-0.011	2.00	No
	57	2	-0.023	2.00	No
	58	2	-0.017	2.00	No
	59	2	-0.023	2.00	No
	67	2	-0.045	0.50	No
		2	-0.045	7.50	No
WI150	22	2	-0.017	1.00	No
		2	-0.017	3.00	No
		2	-0.016	5.00	No
		2	-0.016	7.00	No
	25	2	-0.062	0.50	No
		2	-0.062	7.50	No
	44	2	-0.017	2.00	No
	47	2	-0.01	2.00	No
	50	2	-0.011	2.00	No
	57	2	-0.016	2.00	No
	58	2	-0.012	2.00	No
	59	2	-0.016	2.00	No
	67	2	-0.062	0.50	No
		2	-0.062	7.50	No
WL0	22	z	-0.005	1.00	No
		z	-0.005	3.00	No
		z	-0.005	5.00	No
		z	-0.005	7.00	No
	25	z	-0.023	0.50	No
		z	-0.023	7.50	No
	44	z	-0.005	2.00	No
	50	z	-0.003	2.00	No
	57	z	-0.004	2.00	No
	58	z	-0.004	2.00	No
	59	z	-0.004	2.00	No
	67	z	-0.023	0.50	No
		z	-0.023	7.50	No
WL30	22	3	-0.005	1.00	No
		3	-0.005	3.00	No
		3	-0.005	5.00	No
		3	-0.005	7.00	No
	25	3	-0.02	0.50	No
		3	-0.02	7.50	No
	44	3	-0.005	2.00	No
	47	3	-0.003	2.00	No

	50	3	-0.003	2.00	No
	57	3	-0.004	2.00	No
	58	3	-0.003	2.00	No
	59	3	-0.004	2.00	No
	67	3	-0.02	0.50	No
		3	-0.02	7.50	No
WL60	22	3	-0.004	1.00	No
		3	-0.004	3.00	No
		3	-0.003	5.00	No
		3	-0.003	7.00	No
	25	3	-0.013	0.50	No
		3	-0.013	7.50	No
	44	3	-0.004	2.00	No
	47	3	-0.004	2.00	No
	50	3	-0.003	2.00	No
	57	3	-0.006	2.00	No
	58	3	-0.005	2.00	No
	59	3	-0.006	2.00	No
	67	3	-0.013	0.50	No
		3	-0.013	7.50	No
WL90	22	x	-0.004	1.00	No
		x	-0.004	3.00	No
		x	-0.003	5.00	No
		x	-0.003	7.00	No
	25	x	-0.01	0.50	No
		x	-0.01	7.50	No
	44	x	-0.003	2.00	No
	47	x	-0.004	2.00	No
	50	x	-0.003	2.00	No
	57	x	-0.007	2.00	No
	58	x	-0.005	2.00	No
	59	x	-0.007	2.00	No
	67	x	-0.01	0.50	No
		x	-0.01	7.50	No
WL120	22	2	-0.004	1.00	No
		2	-0.004	3.00	No
		2	-0.003	5.00	No
		2	-0.003	7.00	No
	25	2	-0.013	0.50	No
		2	-0.013	7.50	No
	44	2	-0.004	2.00	No
	47	2	-0.004	2.00	No
	50	2	-0.003	2.00	No
	57	2	-0.006	2.00	No
	58	2	-0.005	2.00	No
	59	2	-0.006	2.00	No
	67	2	-0.013	0.50	No
		2	-0.013	7.50	No
WL150	22	2	-0.005	1.00	No
		2	-0.005	3.00	No
		2	-0.005	5.00	No
		2	-0.005	7.00	No
	25	2	-0.02	0.50	No
		2	-0.02	7.50	No
	44	2	-0.005	2.00	No
	47	2	-0.003	2.00	No
	50	2	-0.003	2.00	No
	57	2	-0.004	2.00	No
	58	2	-0.003	2.00	No
	59	2	-0.004	2.00	No

67	2	-0.02	0.50	No
	2	-0.02	7.50	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00

WL150	0.00	0.00	0.00

Current Date: 3/24/2022 2:36 PM
Units system: English

Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150
LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	L 2-1_2X2-1_2X1_4	**1**	LC7 at 0.00%	0.05	OK	
		2	LC7 at 10.94%	0.32	OK	
		3	LC3 at 22.92%	0.23	OK	
		10	LC1 at 26.56%	0.28	OK	
		11	LC2 at 68.75%	0.35	OK	
		16	LC1 at 24.11%	**0.50**	**OK**	
		31	LC12 at 10.94%	0.13	OK	
		32	LC4 at 100.00%	0.09	OK	
		33	LC4 at 45.31%	0.24	OK	
		37	LC1 at 100.00%	0.28	OK	
		41	LC8 at 10.94%	0.33	OK	
	L 3X3X1_4	**60**	LC1 at 0.00%	**0.15**	**OK**	
		61	LC9 at 0.00%	0.14	OK	
		62	LC9 at 0.00%	0.10	OK	
		64	LC9 at 0.00%	0.12	OK	
		65	LC11 at 0.00%	0.12	OK	
		66	LC11 at 0.00%	0.15	OK	
	LU 2-3/4x5x1/4	**6**	LC7 at 100.00%	0.13	OK	
		14	LC7 at 0.00%	0.51	OK	
		19	LC8 at 100.00%	**0.52**	**OK**	
		36	LC8 at 0.00%	0.18	OK	
		40	LC7 at 0.00%	0.24	OK	
	PIPE 2x0.154	**22**	LC7 at 72.92%	0.13	OK	
		25	LC7 at 27.08%	**0.79**	**OK**	
		44	LC1 at 50.00%	0.09	OK	
		47	LC6 at 6.25%	0.11	OK	
		50	LC6 at 93.75%	0.06	OK	
		57	LC4 at 50.00%	0.15	OK	
		58	LC4 at 50.00%	0.13	OK	
		59	LC4 at 50.00%	0.12	OK	
		67	LC7 at 27.08%	0.79	OK	
	PL 2x1/4	**4**	LC8 at 100.00%	**0.47**	**With warnings**	
		5	LC1 at 100.00%	0.46	With warnings	
		12	LC2 at 0.00%	0.46	With warnings	
		13	LC1 at 100.00%	0.45	With warnings	
		17	LC7 at 100.00%	0.45	With warnings	
		18	LC2 at 100.00%	0.45	With warnings	
		34	LC9 at 0.00%	0.42	With warnings	
		35	LC9 at 0.00%	0.41	With warnings	
		38	LC2 at 0.00%	0.46	With warnings	
		39	LC7 at 0.00%	0.47	With warnings	

Current Date: 3/24/2022 2:35 PM
Units system: English

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	0.00	0.00	0.00	0
2	0.00	0.50	0.00	0
3	0.00	1.08	0.00	0
4	0.00	2.58	0.00	0
5	0.00	4.08	0.00	0
6	5.50	0.00	0.00	0
7	5.50	0.50	0.00	0
8	5.50	1.08	0.00	0
9	5.50	2.58	0.00	0
10	5.50	4.08	0.00	0
17	11.00	0.00	0.00	0
18	11.00	0.50	0.00	0
19	11.00	1.08	0.00	0
20	11.00	2.58	0.00	0
21	11.00	4.08	0.00	0
23	16.50	0.50	0.00	0
24	16.50	1.08	0.00	0
25	16.50	2.58	0.00	0
26	16.50	4.08	0.00	0
32	11.75	6.29	0.20	0
33	11.75	-1.71	0.20	0
38	7.25	6.29	0.20	0
39	7.25	-1.71	0.20	0

45	22.00	0.00	0.00	0
46	22.00	0.50	0.00	0
47	22.00	1.08	0.00	0
48	22.00	2.58	0.00	0
49	22.00	4.08	0.00	0
50	22.00	0.00	-5.50	0
51	22.00	0.50	-5.50	0
52	22.00	1.08	-5.50	0
53	22.00	2.58	-5.50	0
54	22.00	4.08	-5.50	0
55	16.50	0.00	0.00	0
62	18.00	4.29	-0.40	0
68	16.00	4.29	-0.40	0
74	14.25	4.29	-0.40	0
102	21.60	0.29	-3.00	0
103	21.60	0.29	-2.00	0
109	15.125	4.08	0.00	0
113	12.375	4.08	0.00	0
115	12.375	0.50	-8.00	0
116	15.125	0.50	-8.00	0
118	9.625	4.08	0.00	0
125	4.125	4.08	0.00	0
129	1.375	4.08	0.00	0
131	4.125	0.50	-8.00	0
132	1.375	0.50	-8.00	0
133	6.875	0.50	-8.00	0
134	9.625	0.50	-8.00	0
138	6.875	4.08	0.00	0
139	16.25	6.29	0.20	0
140	16.25	-1.71	0.20	0
73	14.25	0.29	-0.40	0
67	16.00	0.29	-0.40	0
61	18.00	0.29	-0.40	0
107	21.60	4.29	-1.00	0
106	21.60	4.29	-2.00	0
105	21.60	4.29	-3.00	0
104	21.60	0.29	-1.00	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
1	1	1	1	0	1	0
2	1	0	1	0	0	0
3	1	0	1	0	0	0
4	1	0	1	0	0	0
5	1	0	1	0	0	0
6	1	1	1	0	1	0
17	1	1	1	0	1	0
45	1	1	1	0	1	0
50	1	1	1	0	1	0
51	1	0	1	0	0	0
52	1	0	1	0	0	0
53	1	0	1	0	0	0
54	1	0	1	0	0	0
55	1	1	1	0	1	0

115	1	1	1	0	0	0
116	1	1	1	0	0	0
131	1	1	1	0	0	0
132	1	1	1	0	0	0
133	1	1	1	0	0	0
134	1	1	1	0	0	0

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	lg factor
1	5	1		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
2	6	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
3	10	5		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
4	4	9		PL 2x1/4	A36	0.00	0.00	0.00
5	3	8		PL 2x1/4	A36	0.00	0.00	0.00
6	2	7		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
10	17	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
11	21	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
12	9	20		PL 2x1/4	A36	0.00	0.00	0.00
13	8	19		PL 2x1/4	A36	0.00	0.00	0.00
14	7	18		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
16	26	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
17	20	25		PL 2x1/4	A36	0.00	0.00	0.00
18	19	24		PL 2x1/4	A36	0.00	0.00	0.00
19	18	23		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
22	32	33		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
25	38	39		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
31	45	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
32	50	54		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
33	54	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
34	48	53		PL 2x1/4	A36	0.00	0.00	0.00
35	47	52		PL 2x1/4	A36	0.00	0.00	0.00
36	46	51		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
37	49	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
38	25	48		PL 2x1/4	A36	0.00	0.00	0.00
39	24	47		PL 2x1/4	A36	0.00	0.00	0.00
40	23	46		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
41	55	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
44	62	61		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
47	68	67		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
50	74	73		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	105	102		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
58	106	103		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
59	107	104		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	109	116		L 3X3X1_4	A36	0.00	0.00	0.00
61	113	115		L 3X3X1_4	A36	0.00	0.00	0.00
62	118	134		L 3X3X1_4	A36	0.00	0.00	0.00
64	125	131		L 3X3X1_4	A36	0.00	0.00	0.00
65	129	132		L 3X3X1_4	A36	0.00	0.00	0.00
66	138	133		L 3X3X1_4	A36	0.00	0.00	0.00
67	139	140		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00

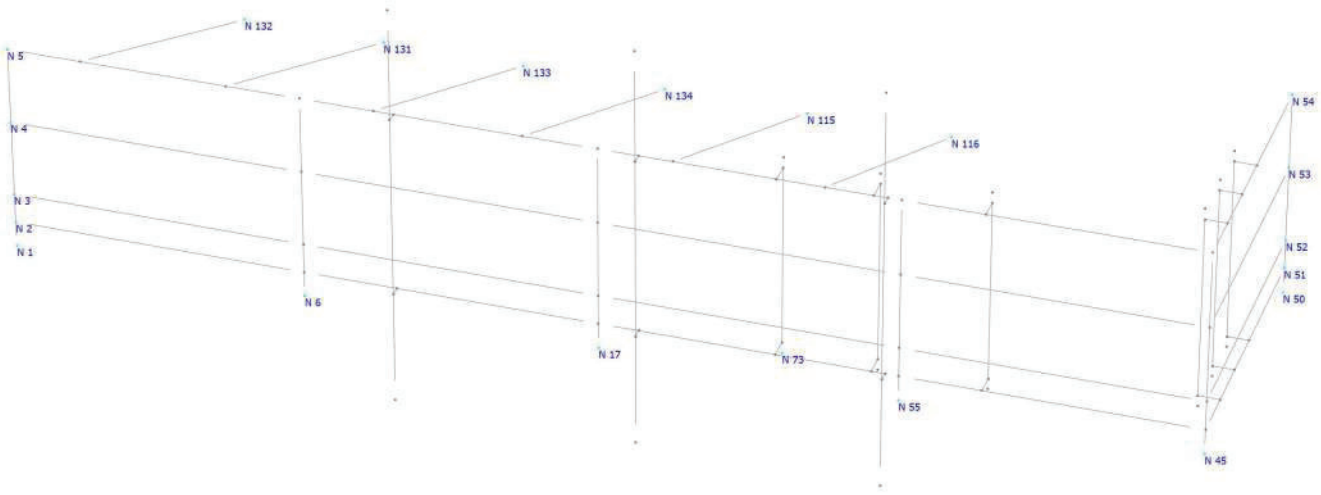
Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
1	270.00	0	0.00	0.00	0.00
2	180.00	0	0.00	0.00	0.00
3	90.00	0	0.00	0.00	0.00
6	270.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	90.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
16	90.00	0	0.00	0.00	0.00
19	270.00	0	0.00	0.00	0.00
22	315.00	0	0.00	0.00	0.00
25	315.00	0	0.00	0.00	0.00
31	270.00	0	0.00	0.00	0.00
32	270.00	0	0.00	0.00	0.00
33	90.00	0	0.00	0.00	0.00
36	270.00	0	0.00	0.00	0.00
37	90.00	0	0.00	0.00	0.00
40	270.00	0	0.00	0.00	0.00
41	180.00	0	0.00	0.00	0.00
44	315.00	0	0.00	0.00	0.00
47	315.00	0	0.00	0.00	0.00
50	315.00	0	0.00	0.00	0.00
57	315.00	0	0.00	0.00	0.00
58	315.00	0	0.00	0.00	0.00
59	315.00	0	0.00	0.00	0.00
60	90.00	0	0.00	0.00	0.00
61	90.00	0	0.00	0.00	0.00
62	90.00	0	0.00	0.00	0.00
64	90.00	0	0.00	0.00	0.00
65	90.00	0	0.00	0.00	0.00
66	90.00	0	0.00	0.00	0.00
67	315.00	0	0.00	0.00	0.00

Hinges

	Node-J				Node-K						
Member	M33	M22	V3	V2	M33	M22	V3	V2	TOR	AXL	Axial rigidity
4	0	0	0	0	0	0	0	0	0	0	Tension only
5	0	0	0	0	0	0	0	0	0	0	Tension only
12	0	0	0	0	0	0	0	0	0	0	Tension only
13	0	0	0	0	0	0	0	0	0	0	Tension only
17	0	0	0	0	0	0	0	0	0	0	Tension only
18	0	0	0	0	0	0	0	0	0	0	Tension only
34	0	0	0	0	0	0	0	0	0	0	Tension only
35	0	0	0	0	0	0	0	0	0	0	Tension only
38	0	0	0	0	0	0	0	0	0	0	Tension only
39	0	0	0	0	0	0	0	0	0	0	Tension only

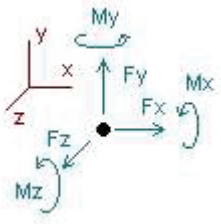
Current Date: 3/24/2022 2:37 PM
Units system: English



Current Date: 3/24/2022 2:36 PM
Units system: English

Analysis result

Reactions



Direction of positive forces and moments

	Forces [Kip]			Moments [Kip*ft]		
Node	**FX**	**FY**	**FZ**	**MX**	**MY**	**MZ**
Condition **LC1=1.2D+1.6Wo**						
1	0.01832	0.03266	0.00261	0.00000	-0.00119	0.00000
2	-0.66120	0.00000	0.00904	0.00000	0.00000	0.00000
3	-0.13306	0.00000	0.06083	0.00000	0.00000	0.00000
4	-0.14246	0.00000	0.06837	0.00000	0.00000	0.00000
5	0.18245	0.00000	0.00580	0.00000	0.00000	0.00000
6	-0.22887	-0.12348	0.62255	0.00000	-0.00291	0.00000
17	0.40659	0.16336	0.74550	0.00000	0.00037	0.00000
45	-0.20101	0.29854	-0.18301	0.00000	0.00219	0.00000
50	-0.00082	0.16018	0.10519	0.00000	-0.00134	0.00000
51	-0.05824	0.00000	0.59249	0.00000	0.00000	0.00000
52	-0.00608	0.00000	-0.12518	0.00000	0.00000	0.00000
53	0.00041	0.00000	0.04096	0.00000	0.00000	0.00000
54	-0.03852	0.00000	0.44178	0.00000	0.00000	0.00000
55	0.83353	0.02438	0.76996	0.00000	0.00138	0.00000
115	-0.00573	0.14482	0.30732	0.00000	0.00000	0.00000
116	0.02177	0.54711	1.20295	0.00000	0.00000	0.00000
131	0.00021	0.06290	0.12405	0.00000	0.00000	0.00000
132	0.00084	0.07440	0.14880	0.00000	0.00000	0.00000
133	0.01079	0.41104	0.88556	0.00000	0.00000	0.00000
134	0.00106	0.14177	0.29783	0.00000	0.00000	0.00000
SUM	0.00000	1.93769	6.12339	0.00000	-0.00149	0.00000
Condition **LC2=1.2D+1.6W30**						
1	0.01629	0.03695	0.00275	0.00000	-0.00130	0.00000
2	0.03490	0.00000	0.02199	0.00000	0.00000	0.00000
3	-0.00812	0.00000	0.06062	0.00000	0.00000	0.00000
4	-0.01701	0.00000	0.06845	0.00000	0.00000	0.00000
5	1.22161	0.00000	0.00534	0.00000	0.00000	0.00000
6	-0.11830	-0.05840	0.50718	0.00000	-0.00213	0.00000
17	0.35487	0.23095	0.58891	0.00000	0.00000	0.00000
45	-0.09793	0.28899	-0.17468	0.00000	0.00117	0.00000
50	-0.00226	0.15495	0.09538	0.00000	-0.00032	0.00000
51	-0.00505	0.00000	0.51693	0.00000	0.00000	0.00000
52	-0.00464	0.00000	-0.09728	0.00000	0.00000	0.00000
53	0.00052	0.00000	0.08836	0.00000	0.00000	0.00000
54	0.00258	0.00000	0.38328	0.00000	0.00000	0.00000
55	0.91726	0.13486	0.60848	0.00000	0.00149	0.00000
115	-0.00544	0.13712	0.29015	0.00000	0.00000	0.00000

116	0.01648	0.43393	0.95143	0.00000	0.00000	0.00000
131	0.00053	0.06410	0.12659	0.00000	0.00000	0.00000
132	0.00083	0.07367	0.14717	0.00000	0.00000	0.00000
133	0.00409	0.33498	0.72321	0.00000	0.00000	0.00000
134	0.00472	0.10558	0.21765	0.00000	0.00000	0.00000
SUM	2.31592	1.93769	5.13192	0.00000	-0.00109	0.00000

Condition **LC3=1.2D+1.6W60**

1	0.03928	0.04585	0.00007	0.00000	0.00020	0.00000
2	0.70989	0.00000	-0.01826	0.00000	0.00000	0.00000
3	-0.01512	0.00000	0.00143	0.00000	0.00000	0.00000
4	0.02154	0.00000	-0.00067	0.00000	0.00000	0.00000
5	2.05254	0.00000	-0.06795	0.00000	0.00000	0.00000
6	-0.11472	0.16919	0.18492	0.00000	-0.00135	0.00000
17	0.23076	0.37710	0.22122	0.00000	-0.00013	0.00000
45	-0.08945	0.28571	-0.09279	0.00000	-0.00106	0.00000
50	-0.00020	0.14882	0.07183	0.00000	0.00182	0.00000
51	0.10778	0.00000	0.25165	0.00000	0.00000	0.00000
52	0.05763	0.00000	-0.10678	0.00000	0.00000	0.00000
53	0.07181	0.00000	0.08740	0.00000	0.00000	0.00000
54	0.09292	0.00000	0.24967	0.00000	0.00000	0.00000
55	0.64504	0.37166	0.23605	0.00000	0.00083	0.00000
115	0.07822	0.06128	0.07990	0.00000	0.00000	0.00000
116	0.08768	0.22254	0.43979	0.00000	0.00000	0.00000
131	0.07880	-0.00291	-0.06381	0.00000	0.00000	0.00000
132	0.08105	0.04463	0.04211	0.00000	0.00000	0.00000
133	0.08403	0.18360	0.34639	0.00000	0.00000	0.00000
134	0.08218	0.03025	0.00910	0.00000	0.00000	0.00000
SUM	4.30168	1.93769	1.87129	0.00000	0.00030	0.00000

Condition **LC4=1.2D+1.6W90**

1	0.02273	0.04951	0.00035	0.00000	0.00006	0.00000
2	0.89907	0.00000	-0.00178	0.00000	0.00000	0.00000
3	-0.02480	0.00000	0.00109	0.00000	0.00000	0.00000
4	-0.00283	0.00000	-0.00058	0.00000	0.00000	0.00000
5	2.10207	0.00000	-0.06694	0.00000	0.00000	0.00000
6	0.07581	0.28082	0.02066	0.00000	-0.00014	0.00000
17	0.13126	0.45853	-0.00113	0.00000	-0.00016	0.00000
45	-0.03348	0.29489	-0.09918	0.00000	-0.00197	0.00000
50	-0.00165	0.14196	0.05286	0.00000	0.00271	0.00000
51	0.16032	0.00000	0.06193	0.00000	0.00000	0.00000
52	0.05879	0.00000	-0.09593	0.00000	0.00000	0.00000
53	0.07191	0.00000	0.10603	0.00000	0.00000	0.00000
54	0.13448	0.00000	0.04370	0.00000	0.00000	0.00000
55	0.33075	0.55001	-0.03958	0.00000	0.00032	0.00000
115	0.08085	0.02126	-0.00976	0.00000	0.00000	0.00000
116	0.07942	0.03438	0.01992	0.00000	0.00000	0.00000
131	0.07948	0.00792	-0.03977	0.00000	0.00000	0.00000
132	0.08101	0.04081	0.03358	0.00000	0.00000	0.00000
133	0.07952	0.05561	0.06764	0.00000	0.00000	0.00000
134	0.08246	0.00199	-0.05310	0.00000	0.00000	0.00000
SUM	4.40716	1.93769	0.00000	0.00000	0.00082	0.00000

Condition **LC5=1.2D+1.6W120**

1	0.01239	0.05143	0.00036	0.00000	-0.00007	0.00000
2	1.04592	0.00000	0.01549	0.00000	0.00000	0.00000
3	0.00898	0.00000	0.00036	0.00000	0.00000	0.00000
4	0.03214	0.00000	-0.00047	0.00000	0.00000	0.00000
5	1.99343	0.00000	-0.06679	0.00000	0.00000	0.00000
6	0.29590	0.39390	-0.14668	0.00000	0.00112	0.00000
17	0.01482	0.53688	-0.22093	0.00000	-0.00024	0.00000
45	0.06500	0.30417	-0.15580	0.00000	-0.00215	0.00000
50	-0.00116	0.13970	0.05051	0.00000	0.00270	0.00000
51	0.15823	0.00000	-0.07759	0.00000	0.00000	0.00000
52	0.05858	0.00000	-0.09275	0.00000	0.00000	0.00000
53	0.07174	0.00000	0.08931	0.00000	0.00000	0.00000
54	0.13114	0.00000	-0.16828	0.00000	0.00000	0.00000
55	-0.05916	0.71854	-0.30013	0.00000	-0.00046	0.00000
115	0.08361	-0.01538	-0.09196	0.00000	0.00000	0.00000
116	0.07157	-0.14528	-0.38132	0.00000	0.00000	0.00000
131	0.08015	0.01888	-0.01546	0.00000	0.00000	0.00000
132	0.08094	0.03744	0.02605	0.00000	0.00000	0.00000
133	0.07534	-0.07371	-0.21411	0.00000	0.00000	0.00000
134	0.08214	-0.02888	-0.12111	0.00000	0.00000	0.00000
SUM	4.30168	1.93769	-1.87129	0.00000	0.00090	0.00000

Condition **LC6=1.2D+1.6W150**

1	0.02394	0.12569	-0.00193	0.00000	0.00141	0.00000
2	1.17912	0.00000	-0.02536	0.00000	0.00000	0.00000
3	-0.04415	0.00000	-0.05742	0.00000	0.00000	0.00000
4	0.04640	0.00000	-0.07124	0.00000	0.00000	0.00000
5	1.01542	0.00000	-0.00785	0.00000	0.00000	0.00000
6	0.25186	0.59330	-0.46310	0.00000	0.00199	0.00000
17	-0.19325	0.70544	-0.59965	0.00000	-0.00027	0.00000
45	0.19854	0.31795	-0.17642	0.00000	-0.00240	0.00000
50	-0.00383	0.14244	0.06820	0.00000	0.00186	0.00000
51	0.10044	0.00000	-0.20549	0.00000	0.00000	0.00000
52	-0.00107	0.00000	-0.12829	0.00000	0.00000	0.00000
53	0.00299	0.00000	-0.12335	0.00000	0.00000	0.00000
54	0.07279	0.00000	-0.25602	0.00000	0.00000	0.00000
55	-0.34031	0.89903	-0.62302	0.00000	-0.00101	0.00000
115	0.01136	-0.09226	-0.30365	0.00000	0.00000	0.00000
116	-0.01559	-0.38033	-0.94479	0.00000	0.00000	0.00000
131	0.00230	-0.04870	-0.20688	0.00000	0.00000	0.00000
132	0.00573	-0.00001	-0.09752	0.00000	0.00000	0.00000
133	-0.00166	-0.21478	-0.56574	0.00000	0.00000	0.00000
134	0.00489	-0.11010	-0.34238	0.00000	0.00000	0.00000
SUM	2.31592	1.93769	-5.13192	0.00000	0.00158	0.00000

Condition **LC7=1.2D-1.6Wo**

1	0.00433	0.12939	-0.00179	0.00000	0.00129	0.00000
2	0.74858	0.00000	-0.01283	0.00000	0.00000	0.00000
3	-0.20316	0.00000	-0.05780	0.00000	0.00000	0.00000
4	0.03146	0.00000	-0.07115	0.00000	0.00000	0.00000
5	-0.11862	0.00000	-0.00725	0.00000	0.00000	0.00000
6	0.45762	0.70188	-0.61307	0.00000	0.00315	0.00000
17	-0.29918	0.70170	-0.73260	0.00000	-0.00032	0.00000
45	0.11836	0.33597	-0.17606	0.00000	-0.00210	0.00000
50	-0.00254	0.14475	0.08244	0.00000	0.00135	0.00000
51	0.07095	0.00000	-0.28163	0.00000	0.00000	0.00000
52	-0.00180	0.00000	-0.10697	0.00000	0.00000	0.00000

53	0.00278	0.00000	-0.07331	0.00000	0.00000	0.00000
54	0.04792	0.00000	-0.33291	0.00000	0.00000	0.00000
55	-0.85794	0.99912	-0.77140	0.00000	-0.00179	0.00000
115	0.01348	-0.09931	-0.31984	0.00000	0.00000	0.00000
116	-0.02048	-0.48867	-1.18755	0.00000	0.00000	0.00000
131	0.00340	-0.02652	-0.15746	0.00000	0.00000	0.00000
132	0.00560	-0.00654	-0.11211	0.00000	0.00000	0.00000
133	-0.00285	-0.35028	-0.86278	0.00000	0.00000	0.00000
134	0.00208	-0.10380	-0.32733	0.00000	0.00000	0.00000
SUM	0.00000	1.93769	-6.12339	0.00000	0.00158	0.00000

Condition **LC8=1.2D-1.6W30**

1	0.00782	0.12585	-0.00186	0.00000	0.00139	0.00000
2	-0.00114	0.00000	-0.02687	0.00000	0.00000	0.00000
3	-0.25410	0.00000	-0.05741	0.00000	0.00000	0.00000
4	-0.00693	0.00000	-0.07118	0.00000	0.00000	0.00000
5	-1.22122	0.00000	-0.00768	0.00000	0.00000	0.00000
6	0.30007	0.63521	-0.49651	0.00000	0.00231	0.00000
17	-0.20599	0.63224	-0.57721	0.00000	0.00017	0.00000
45	-0.03021	0.34755	-0.15450	0.00000	-0.00110	0.00000
50	-0.00106	0.15027	0.09323	0.00000	0.00032	0.00000
51	0.01739	0.00000	-0.26021	0.00000	0.00000	0.00000
52	-0.00319	0.00000	-0.13502	0.00000	0.00000	0.00000
53	0.00260	0.00000	-0.07405	0.00000	0.00000	0.00000
54	0.00648	0.00000	-0.29781	0.00000	0.00000	0.00000
55	-0.93633	0.88894	-0.60883	0.00000	-0.00183	0.00000
115	0.01318	-0.09252	-0.30464	0.00000	0.00000	0.00000
116	-0.01444	-0.37587	-0.93609	0.00000	0.00000	0.00000
131	0.00316	-0.02685	-0.15805	0.00000	0.00000	0.00000
132	0.00557	-0.00556	-0.10991	0.00000	0.00000	0.00000
133	0.00393	-0.27571	-0.70399	0.00000	0.00000	0.00000
134	-0.00149	-0.06586	-0.24332	0.00000	0.00000	0.00000
SUM	-2.31592	1.93769	-5.13192	0.00000	0.00127	0.00000

Condition **LC9=1.2D-1.6W60**

1	-0.00945	0.11892	0.00106	0.00000	-0.00007	0.00000
2	-0.44899	0.00000	0.01289	0.00000	0.00000	0.00000
3	-0.32073	0.00000	0.00205	0.00000	0.00000	0.00000
4	-0.25921	0.00000	-0.00222	0.00000	0.00000	0.00000
5	-1.92993	0.00000	0.06592	0.00000	0.00000	0.00000
6	0.22690	0.40760	-0.17383	0.00000	0.00139	0.00000
17	-0.09452	0.48451	-0.20976	0.00000	0.00025	0.00000
45	-0.06802	0.35166	-0.19226	0.00000	0.00107	0.00000
50	-0.00305	0.15674	0.11849	0.00000	-0.00180	0.00000
51	-0.09537	0.00000	-0.08623	0.00000	0.00000	0.00000
52	-0.06524	0.00000	-0.12485	0.00000	0.00000	0.00000
53	-0.06869	0.00000	0.01859	0.00000	0.00000	0.00000
54	-0.08395	0.00000	-0.21196	0.00000	0.00000	0.00000
55	-0.62097	0.65071	-0.23617	0.00000	-0.00113	0.00000
115	-0.07060	-0.01409	-0.08856	0.00000	0.00000	0.00000
116	-0.08497	-0.16561	-0.42644	0.00000	0.00000	0.00000
131	-0.07509	0.03753	0.02648	0.00000	0.00000	0.00000
132	-0.07462	0.02427	-0.00307	0.00000	0.00000	0.00000
133	-0.07636	-0.12128	-0.32062	0.00000	0.00000	0.00000
134	-0.07884	0.00674	-0.04083	0.00000	0.00000	0.00000
SUM	-4.30168	1.93769	-1.87129	0.00000	-0.00030	0.00000

Condition **LC10=1.2D-1.6W90**

1	0.00558	0.11453	0.00071	0.00000	0.00006	0.00000
2	-0.67785	0.00000	-0.00332	0.00000	0.00000	0.00000
3	-0.28299	0.00000	0.00230	0.00000	0.00000	0.00000
4	-0.21239	0.00000	-0.00225	0.00000	0.00000	0.00000
5	-1.99688	0.00000	0.06503	0.00000	0.00000	0.00000
6	0.06098	0.29728	-0.00956	0.00000	0.00022	0.00000
17	-0.01620	0.40349	0.01247	0.00000	0.00026	0.00000
45	-0.12364	0.34459	-0.18340	0.00000	0.00198	0.00000
50	-0.00161	0.16311	0.13708	0.00000	-0.00269	0.00000
51	-0.14801	0.00000	0.10065	0.00000	0.00000	0.00000
52	-0.06638	0.00000	-0.13533	0.00000	0.00000	0.00000
53	-0.06879	0.00000	-0.00142	0.00000	0.00000	0.00000
54	-0.12481	0.00000	-0.00480	0.00000	0.00000	0.00000
55	-0.30396	0.46949	0.03932	0.00000	-0.00061	0.00000
115	-0.07310	0.02585	0.00092	0.00000	0.00000	0.00000
116	-0.07616	0.02240	-0.00674	0.00000	0.00000	0.00000
131	-0.07577	0.02719	0.00355	0.00000	0.00000	0.00000
132	-0.07456	0.02789	0.00500	0.00000	0.00000	0.00000
133	-0.07156	0.00636	-0.04274	0.00000	0.00000	0.00000
134	-0.07905	0.03552	0.02255	0.00000	0.00000	0.00000
SUM	-4.40716	1.93769	0.00000	0.00000	-0.00079	0.00000

Condition **LC11=1.2D-1.6W120**

1	0.01298	0.11131	0.00056	0.00000	0.00018	0.00000
2	-0.86123	0.00000	-0.02004	0.00000	0.00000	0.00000
3	-0.31817	0.00000	0.00284	0.00000	0.00000	0.00000
4	-0.28902	0.00000	-0.00229	0.00000	0.00000	0.00000
5	-1.85950	0.00000	0.06500	0.00000	0.00000	0.00000
6	-0.10381	0.18424	0.15740	0.00000	-0.00096	0.00000
17	0.08605	0.32860	0.23261	0.00000	0.00029	0.00000
45	-0.16552	0.33368	-0.14495	0.00000	0.00218	0.00000
50	-0.00206	0.16497	0.13900	0.00000	-0.00270	0.00000
51	-0.14647	0.00000	0.26611	0.00000	0.00000	0.00000
52	-0.06615	0.00000	-0.13726	0.00000	0.00000	0.00000
53	-0.06865	0.00000	0.00106	0.00000	0.00000	0.00000
54	-0.12114	0.00000	0.21359	0.00000	0.00000	0.00000
55	0.04175	0.30095	0.29911	0.00000	0.00008	0.00000
115	-0.07574	0.06383	0.08608	0.00000	0.00000	0.00000
116	-0.06827	0.20130	0.39260	0.00000	0.00000	0.00000
131	-0.07646	0.01671	-0.01968	0.00000	0.00000	0.00000
132	-0.07448	0.03095	0.01185	0.00000	0.00000	0.00000
133	-0.06708	0.13611	0.24009	0.00000	0.00000	0.00000
134	-0.07872	0.06504	0.08759	0.00000	0.00000	0.00000
SUM	-4.30168	1.93769	1.87129	0.00000	-0.00093	0.00000

Condition **LC12=1.2D-1.6W150**

1	0.00162	0.03624	0.00289	0.00000	-0.00128	0.00000
2	-1.04551	0.00000	0.02176	0.00000	0.00000	0.00000
3	-0.27989	0.00000	0.06053	0.00000	0.00000	0.00000
4	-0.22870	0.00000	0.06836	0.00000	0.00000	0.00000
5	-0.91204	0.00000	0.00711	0.00000	0.00000	0.00000
6	-0.06451	-0.01537	0.47282	0.00000	-0.00182	0.00000
17	0.26714	0.16015	0.61248	0.00000	0.00029	0.00000
45	-0.22100	0.31935	-0.20856	0.00000	0.00253	0.00000
50	0.00050	0.16167	0.11892	0.00000	-0.00190	0.00000
51	-0.08927	0.00000	0.56496	0.00000	0.00000	0.00000

52	-0.00678	0.00000	-0.10908	0.00000	0.00000	0.00000
53	0.00024	0.00000	0.05755	0.00000	0.00000	0.00000
54	-0.06351	0.00000	0.38268	0.00000	0.00000	0.00000
55	0.30207	0.12272	0.61984	0.00000	0.00064	0.00000
115	-0.00360	0.14000	0.29610	0.00000	0.00000	0.00000
116	0.01752	0.43752	0.95759	0.00000	0.00000	0.00000
131	0.00122	0.08232	0.16728	0.00000	0.00000	0.00000
132	0.00072	0.06843	0.13548	0.00000	0.00000	0.00000
133	0.00953	0.27890	0.59549	0.00000	0.00000	0.00000
134	-0.00166	0.14576	0.30772	0.00000	0.00000	0.00000
SUM	-2.31592	1.93769	5.13192	0.00000	-0.00153	0.00000

Condition **LC13=0.9D+1.6Wo**

1	0.01511	0.01219	0.00249	0.00000	-0.00120	0.00000
2	-0.65381	0.00000	0.00963	0.00000	0.00000	0.00000
3	-0.11721	0.00000	0.06042	0.00000	0.00000	0.00000
4	-0.15026	0.00000	0.06872	0.00000	0.00000	0.00000
5	0.19094	0.00000	0.00601	0.00000	0.00000	0.00000
6	-0.24631	-0.19543	0.62138	0.00000	-0.00292	0.00000
17	0.39459	0.05592	0.74409	0.00000	0.00035	0.00000
45	-0.19320	0.21830	-0.14406	0.00000	0.00218	0.00000
50	-0.00043	0.12202	0.08112	0.00000	-0.00132	0.00000
51	-0.05906	0.00000	0.56782	0.00000	0.00000	0.00000
52	-0.00513	0.00000	-0.09648	0.00000	0.00000	0.00000
53	0.00003	0.00000	0.02756	0.00000	0.00000	0.00000
54	-0.03939	0.00000	0.43728	0.00000	0.00000	0.00000
55	0.83933	-0.10341	0.77113	0.00000	0.00140	0.00000
115	-0.00671	0.13889	0.30830	0.00000	0.00000	0.00000
116	0.02133	0.54023	1.20173	0.00000	0.00000	0.00000
131	-0.00025	0.05826	0.12802	0.00000	0.00000	0.00000
132	0.00003	0.06590	0.14418	0.00000	0.00000	0.00000
133	0.00976	0.40347	0.88281	0.00000	0.00000	0.00000
134	0.00064	0.13691	0.30125	0.00000	0.00000	0.00000
SUM	0.00000	1.45327	6.12339	0.00000	-0.00152	0.00000

Condition **LC14=0.9D+1.6W30**

1	0.01322	0.01659	0.00264	0.00000	-0.00131	0.00000
2	0.04981	0.00000	0.02257	0.00000	0.00000	0.00000
3	-0.00265	0.00000	0.06021	0.00000	0.00000	0.00000
4	-0.02182	0.00000	0.06880	0.00000	0.00000	0.00000
5	1.22937	0.00000	0.00555	0.00000	0.00000	0.00000
6	-0.13712	-0.13036	0.50594	0.00000	-0.00215	0.00000
17	0.34315	0.12341	0.58745	0.00000	-0.00002	0.00000
45	-0.08940	0.20871	-0.13596	0.00000	0.00115	0.00000
50	-0.00188	0.11679	0.07133	0.00000	-0.00030	0.00000
51	-0.00585	0.00000	0.49248	0.00000	0.00000	0.00000
52	-0.00369	0.00000	-0.06857	0.00000	0.00000	0.00000
53	0.00014	0.00000	0.07495	0.00000	0.00000	0.00000
54	0.00171	0.00000	0.37875	0.00000	0.00000	0.00000
55	0.92383	0.00703	0.60959	0.00000	0.00151	0.00000
115	-0.00641	0.13117	0.29110	0.00000	0.00000	0.00000
116	0.01605	0.42708	0.95030	0.00000	0.00000	0.00000
131	0.00007	0.05951	0.13065	0.00000	0.00000	0.00000
132	0.00002	0.06516	0.14252	0.00000	0.00000	0.00000
133	0.00306	0.32742	0.72047	0.00000	0.00000	0.00000
134	0.00430	0.10075	0.22115	0.00000	0.00000	0.00000

SUM	2.31592	1.45327	5.13192	0.00000	-0.00112	0.00000
Condition	**LC15=0.9D+1.6W60**					
1	0.03622	0.02551	-0.00005	0.00000	0.00018	0.00000
2	0.72446	0.00000	-0.01767	0.00000	0.00000	0.00000
3	-0.00964	0.00000	0.00103	0.00000	0.00000	0.00000
4	0.01672	0.00000	-0.00032	0.00000	0.00000	0.00000
5	2.06033	0.00000	-0.06773	0.00000	0.00000	0.00000
6	-0.13351	0.09720	0.18362	0.00000	-0.00137	0.00000
17	0.21920	0.26956	0.21972	0.00000	-0.00016	0.00000
45	-0.08094	0.20545	-0.05411	0.00000	-0.00108	0.00000
50	0.00018	0.11065	0.04780	0.00000	0.00184	0.00000
51	0.10698	0.00000	0.22725	0.00000	0.00000	0.00000
52	0.05857	0.00000	-0.07810	0.00000	0.00000	0.00000
53	0.07143	0.00000	0.07400	0.00000	0.00000	0.00000
54	0.09205	0.00000	0.24515	0.00000	0.00000	0.00000
55	0.65172	0.24376	0.23705	0.00000	0.00085	0.00000
115	0.07724	0.05534	0.08088	0.00000	0.00000	0.00000
116	0.08728	0.21572	0.43874	0.00000	0.00000	0.00000
131	0.07835	-0.00750	-0.05973	0.00000	0.00000	0.00000
132	0.08025	0.03612	0.03745	0.00000	0.00000	0.00000
133	0.08301	0.17605	0.34370	0.00000	0.00000	0.00000
134	0.08177	0.02542	0.01261	0.00000	0.00000	0.00000
SUM	4.30168	1.45327	1.87129	0.00000	0.00027	0.00000
Condition	**LC16=0.9D+1.6W90**					
1	0.01974	0.02924	0.00024	0.00000	0.00005	0.00000
2	0.91536	0.00000	-0.00119	0.00000	0.00000	0.00000
3	-0.01942	0.00000	0.00069	0.00000	0.00000	0.00000
4	-0.00763	0.00000	-0.00024	0.00000	0.00000	0.00000
5	2.10960	0.00000	-0.06672	0.00000	0.00000	0.00000
6	0.05599	0.20885	0.01928	0.00000	-0.00016	0.00000
17	0.11865	0.35082	-0.00268	0.00000	-0.00019	0.00000
45	-0.02574	0.21473	-0.05998	0.00000	-0.00199	0.00000
50	-0.00126	0.10380	0.02887	0.00000	0.00273	0.00000
51	0.15949	0.00000	0.03651	0.00000	0.00000	0.00000
52	0.05974	0.00000	-0.06727	0.00000	0.00000	0.00000
53	0.07154	0.00000	0.09371	0.00000	0.00000	0.00000
54	0.13359	0.00000	0.03863	0.00000	0.00000	0.00000
55	0.33883	0.42204	-0.03874	0.00000	0.00034	0.00000
115	0.07988	0.01533	-0.00874	0.00000	0.00000	0.00000
116	0.07904	0.02757	0.01891	0.00000	0.00000	0.00000
131	0.07902	0.00336	-0.03563	0.00000	0.00000	0.00000
132	0.08020	0.03228	0.02890	0.00000	0.00000	0.00000
133	0.07850	0.04807	0.06498	0.00000	0.00000	0.00000
134	0.08206	-0.00281	-0.04954	0.00000	0.00000	0.00000
SUM	4.40716	1.45327	0.00000	0.00000	0.00078	0.00000
Condition	**LC17=0.9D+1.6W120**					
1	0.00939	0.03115	0.00025	0.00000	-0.00008	0.00000
2	1.06239	0.00000	0.01609	0.00000	0.00000	0.00000
3	0.01436	0.00000	-0.00003	0.00000	0.00000	0.00000
4	0.02733	0.00000	-0.00012	0.00000	0.00000	0.00000
5	2.00092	0.00000	-0.06657	0.00000	0.00000	0.00000
6	0.27609	0.32191	-0.14812	0.00000	0.00110	0.00000
17	0.00249	0.42913	-0.22252	0.00000	-0.00026	0.00000
45	0.07234	0.22392	-0.11497	0.00000	-0.00217	0.00000
50	-0.00076	0.10158	0.02667	0.00000	0.00272	0.00000

51	0.15734	0.00000	-0.10687	0.00000	0.00000	0.00000
52	0.05953	0.00000	-0.06407	0.00000	0.00000	0.00000
53	0.07136	0.00000	0.08167	0.00000	0.00000	0.00000
54	0.13020	0.00000	-0.17586	0.00000	0.00000	0.00000
55	-0.05103	0.59060	-0.29944	0.00000	-0.00044	0.00000
115	0.08264	-0.02129	-0.09091	0.00000	0.00000	0.00000
116	0.07120	-0.15210	-0.38234	0.00000	0.00000	0.00000
131	0.07970	0.01433	-0.01131	0.00000	0.00000	0.00000
132	0.08013	0.02891	0.02137	0.00000	0.00000	0.00000
133	0.07433	-0.08122	-0.21669	0.00000	0.00000	0.00000
134	0.08174	-0.03366	-0.11751	0.00000	0.00000	0.00000
SUM	4.30168	1.45327	-1.87129	0.00000	0.00087	0.00000

Condition **LC18=0.9D+1.6W150**

1	0.02094	0.10541	-0.00204	0.00000	0.00140	0.00000
2	1.19513	0.00000	-0.02475	0.00000	0.00000	0.00000
3	-0.03878	0.00000	-0.05782	0.00000	0.00000	0.00000
4	0.04163	0.00000	-0.07090	0.00000	0.00000	0.00000
5	1.02259	0.00000	-0.00763	0.00000	0.00000	0.00000
6	0.23215	0.52130	-0.46460	0.00000	0.00197	0.00000
17	-0.20567	0.59761	-0.60136	0.00000	-0.00030	0.00000
45	0.20503	0.23704	-0.14117	0.00000	-0.00241	0.00000
50	-0.00345	0.10473	0.04469	0.00000	0.00188	0.00000
51	0.09982	0.00000	-0.21264	0.00000	0.00000	0.00000
52	-0.00013	0.00000	-0.12109	0.00000	0.00000	0.00000
53	0.00261	0.00000	-0.12576	0.00000	0.00000	0.00000
54	0.07183	0.00000	-0.26450	0.00000	0.00000	0.00000
55	-0.33085	0.77137	-0.62212	0.00000	-0.00099	0.00000
115	0.01040	-0.09817	-0.30259	0.00000	0.00000	0.00000
116	-0.01593	-0.38712	-0.94572	0.00000	0.00000	0.00000
131	0.00185	-0.05325	-0.20271	0.00000	0.00000	0.00000
132	0.00493	-0.00852	-0.10218	0.00000	0.00000	0.00000
133	-0.00267	-0.22227	-0.56827	0.00000	0.00000	0.00000
134	0.00450	-0.11488	-0.33876	0.00000	0.00000	0.00000
SUM	2.31592	1.45327	-5.13192	0.00000	0.00155	0.00000

Condition **LC19=0.9D-1.6Wo**

1	0.00114	0.10893	-0.00191	0.00000	0.00128	0.00000
2	0.75641	0.00000	-0.01219	0.00000	0.00000	0.00000
3	-0.18745	0.00000	-0.05821	0.00000	0.00000	0.00000
4	0.02355	0.00000	-0.07080	0.00000	0.00000	0.00000
5	-0.11034	0.00000	-0.00704	0.00000	0.00000	0.00000
6	0.44038	0.62990	-0.61465	0.00000	0.00313	0.00000
17	-0.31227	0.59400	-0.73429	0.00000	-0.00035	0.00000
45	0.12318	0.25562	-0.13503	0.00000	-0.00212	0.00000
50	-0.00215	0.10668	0.05867	0.00000	0.00138	0.00000
51	0.07012	0.00000	-0.31092	0.00000	0.00000	0.00000
52	-0.00085	0.00000	-0.07867	0.00000	0.00000	0.00000
53	0.00240	0.00000	-0.08084	0.00000	0.00000	0.00000
54	0.04697	0.00000	-0.34052	0.00000	0.00000	0.00000
55	-0.84837	0.87124	-0.77082	0.00000	-0.00177	0.00000
115	0.01252	-0.10522	-0.31878	0.00000	0.00000	0.00000
116	-0.02082	-0.49544	-1.18843	0.00000	0.00000	0.00000
131	0.00294	-0.03115	-0.15346	0.00000	0.00000	0.00000
132	0.00480	-0.01502	-0.11671	0.00000	0.00000	0.00000
133	-0.00384	-0.35768	-0.86509	0.00000	0.00000	0.00000
134	0.00169	-0.10859	-0.32372	0.00000	0.00000	0.00000

SUM	0.00000	1.45327	-6.12339	0.00000	0.00155	0.00000
Condition **LC20=0.9D-1.6W30**						
1	0.00462	0.10538	-0.00198	0.00000	0.00138	0.00000
2	0.00690	0.00000	-0.02624	0.00000	0.00000	0.00000
3	-0.23847	0.00000	-0.05782	0.00000	0.00000	0.00000
4	-0.01524	0.00000	-0.07083	0.00000	0.00000	0.00000
5	-1.21256	0.00000	-0.00746	0.00000	0.00000	0.00000
6	0.28297	0.56329	-0.49802	0.00000	0.00229	0.00000
17	-0.21922	0.52453	-0.57886	0.00000	0.00015	0.00000
45	-0.02538	0.26720	-0.11341	0.00000	-0.00112	0.00000
50	-0.00068	0.11219	0.06946	0.00000	0.00034	0.00000
51	0.01656	0.00000	-0.28974	0.00000	0.00000	0.00000
52	-0.00224	0.00000	-0.10647	0.00000	0.00000	0.00000
53	0.00222	0.00000	-0.08166	0.00000	0.00000	0.00000
54	0.00553	0.00000	-0.30541	0.00000	0.00000	0.00000
55	-0.92688	0.76109	-0.60817	0.00000	-0.00180	0.00000
115	0.01222	-0.09842	-0.30356	0.00000	0.00000	0.00000
116	-0.01479	-0.38268	-0.93706	0.00000	0.00000	0.00000
131	0.00270	-0.03147	-0.15405	0.00000	0.00000	0.00000
132	0.00477	-0.01404	-0.11450	0.00000	0.00000	0.00000
133	0.00293	-0.28315	-0.70639	0.00000	0.00000	0.00000
134	-0.00189	-0.07066	-0.23975	0.00000	0.00000	0.00000
SUM	-2.31592	1.45327	-5.13192	0.00000	0.00124	0.00000
Condition **LC21=0.9D-1.6W60**						
1	-0.01265	0.09845	0.00094	0.00000	-0.00009	0.00000
2	-0.44236	0.00000	0.01351	0.00000	0.00000	0.00000
3	-0.30389	0.00000	0.00165	0.00000	0.00000	0.00000
4	-0.26622	0.00000	-0.00187	0.00000	0.00000	0.00000
5	-1.92205	0.00000	0.06614	0.00000	0.00000	0.00000
6	0.20913	0.33565	-0.17528	0.00000	0.00137	0.00000
17	-0.10776	0.37679	-0.21137	0.00000	0.00023	0.00000
45	-0.06203	0.27139	-0.15343	0.00000	0.00105	0.00000
50	-0.00267	0.11861	0.09457	0.00000	-0.00177	0.00000
51	-0.09616	0.00000	-0.11070	0.00000	0.00000	0.00000
52	-0.06429	0.00000	-0.09632	0.00000	0.00000	0.00000
53	-0.06906	0.00000	0.00527	0.00000	0.00000	0.00000
54	-0.08488	0.00000	-0.21653	0.00000	0.00000	0.00000
55	-0.61228	0.52293	-0.23537	0.00000	-0.00111	0.00000
115	-0.07157	-0.01998	-0.08747	0.00000	0.00000	0.00000
116	-0.08533	-0.17243	-0.42744	0.00000	0.00000	0.00000
131	-0.07556	0.03290	0.03046	0.00000	0.00000	0.00000
132	-0.07542	0.01579	-0.00766	0.00000	0.00000	0.00000
133	-0.07737	-0.12873	-0.32306	0.00000	0.00000	0.00000
134	-0.07925	0.00191	-0.03732	0.00000	0.00000	0.00000
SUM	-4.30168	1.45327	-1.87129	0.00000	-0.00032	0.00000
Condition **LC22=0.9D-1.6W90**						
1	0.00236	0.09404	0.00059	0.00000	0.00004	0.00000
2	-0.67143	0.00000	-0.00271	0.00000	0.00000	0.00000
3	-0.26799	0.00000	0.00190	0.00000	0.00000	0.00000
4	-0.21916	0.00000	-0.00190	0.00000	0.00000	0.00000
5	-1.98867	0.00000	0.06524	0.00000	0.00000	0.00000
6	0.04372	0.22527	-0.01093	0.00000	0.00020	0.00000
17	-0.02766	0.29589	0.01089	0.00000	0.00024	0.00000
45	-0.11763	0.26410	-0.14471	0.00000	0.00196	0.00000

50	-0.00123	0.12502	0.11315	0.00000	-0.00267	0.00000
51	-0.14875	0.00000	0.07630	0.00000	0.00000	0.00000
52	-0.06544	0.00000	-0.10681	0.00000	0.00000	0.00000
53	-0.06917	0.00000	-0.01474	0.00000	0.00000	0.00000
54	-0.12574	0.00000	-0.00942	0.00000	0.00000	0.00000
55	-0.29614	0.34193	0.04030	0.00000	-0.00059	0.00000
115	-0.07407	0.01996	0.00202	0.00000	0.00000	0.00000
116	-0.07655	0.01555	-0.00783	0.00000	0.00000	0.00000
131	-0.07623	0.02255	0.00753	0.00000	0.00000	0.00000
132	-0.07537	0.01940	0.00041	0.00000	0.00000	0.00000
133	-0.07257	-0.00111	-0.04525	0.00000	0.00000	0.00000
134	-0.07945	0.03066	0.02598	0.00000	0.00000	0.00000
SUM	-4.40716	1.45327	0.00000	0.00000	-0.00082	0.00000

Condition **LC23=0.9D-1.6W120**

1	0.00976	0.09081	0.00044	0.00000	0.00017	0.00000
2	-0.85476	0.00000	-0.01943	0.00000	0.00000	0.00000
3	-0.30314	0.00000	0.00243	0.00000	0.00000	0.00000
4	-0.29577	0.00000	-0.00194	0.00000	0.00000	0.00000
5	-1.85129	0.00000	0.06521	0.00000	0.00000	0.00000
6	-0.12106	0.11226	0.15611	0.00000	-0.00098	0.00000
17	0.07456	0.22102	0.23109	0.00000	0.00027	0.00000
45	-0.15949	0.25317	-0.10623	0.00000	0.00216	0.00000
50	-0.00168	0.12690	0.11505	0.00000	-0.00267	0.00000
51	-0.14721	0.00000	0.24173	0.00000	0.00000	0.00000
52	-0.06520	0.00000	-0.10872	0.00000	0.00000	0.00000
53	-0.06902	0.00000	-0.01227	0.00000	0.00000	0.00000
54	-0.12206	0.00000	0.20897	0.00000	0.00000	0.00000
55	0.04953	0.17342	0.30019	0.00000	0.00010	0.00000
115	-0.07672	0.05794	0.08717	0.00000	0.00000	0.00000
116	-0.06867	0.19443	0.39144	0.00000	0.00000	0.00000
131	-0.07693	0.01207	-0.01570	0.00000	0.00000	0.00000
132	-0.07528	0.02247	0.00726	0.00000	0.00000	0.00000
133	-0.06810	0.12860	0.23748	0.00000	0.00000	0.00000
134	-0.07914	0.06017	0.09101	0.00000	0.00000	0.00000
SUM	-4.30168	1.45327	1.87129	0.00000	-0.00096	0.00000

Condition **LC24=0.9D-1.6W150**

1	-0.00160	0.01576	0.00277	0.00000	-0.00129	0.00000
2	-1.03875	0.00000	0.02235	0.00000	0.00000	0.00000
3	-0.26406	0.00000	0.06013	0.00000	0.00000	0.00000
4	-0.23558	0.00000	0.06871	0.00000	0.00000	0.00000
5	-0.90389	0.00000	0.00732	0.00000	0.00000	0.00000
6	-0.08201	-0.08731	0.47159	0.00000	-0.00184	0.00000
17	0.25493	0.05266	0.61102	0.00000	0.00027	0.00000
45	-0.21232	0.23909	-0.16993	0.00000	0.00251	0.00000
50	0.00088	0.12351	0.09489	0.00000	-0.00188	0.00000
51	-0.09012	0.00000	0.54064	0.00000	0.00000	0.00000
52	-0.00583	0.00000	-0.08038	0.00000	0.00000	0.00000
53	-0.00014	0.00000	0.04417	0.00000	0.00000	0.00000
54	-0.06441	0.00000	0.37815	0.00000	0.00000	0.00000
55	0.30738	-0.00505	0.62092	0.00000	0.00066	0.00000
115	-0.00458	0.13409	0.29714	0.00000	0.00000	0.00000
116	0.01709	0.43063	0.95636	0.00000	0.00000	0.00000
131	0.00075	0.07768	0.17123	0.00000	0.00000	0.00000
132	-0.00009	0.05994	0.13087	0.00000	0.00000	0.00000
133	0.00850	0.27137	0.59283	0.00000	0.00000	0.00000

134	-0.00208	0.14089	0.31113	0.00000	0.00000	0.00000
SUM	-2.31592	1.45327	5.13192	0.00000	-0.00156	0.00000

Condition **LC25=1.2D+Di+WI0**

1	0.02987	0.17103	0.00128	0.00000	0.00016	0.00000
2	-0.09428	0.00000	-0.01102	0.00000	0.00000	0.00000
3	-0.14062	0.00000	0.00404	0.00000	0.00000	0.00000
4	0.03814	0.00000	-0.00313	0.00000	0.00000	0.00000
5	-0.06108	0.00000	-0.00271	0.00000	0.00000	0.00000
6	0.15631	0.70505	0.06167	0.00000	-0.00014	0.00000
17	0.08518	0.85706	0.07413	0.00000	0.00014	0.00000
45	-0.07310	0.56496	-0.25425	0.00000	0.00022	0.00000
50	-0.00287	0.26843	0.15613	0.00000	-0.00020	0.00000
51	0.00328	0.00000	0.21454	0.00000	0.00000	0.00000
52	-0.00689	0.00000	-0.19225	0.00000	0.00000	0.00000
53	0.00252	0.00000	0.05545	0.00000	0.00000	0.00000
54	0.00192	0.00000	0.07506	0.00000	0.00000	0.00000
55	0.02268	1.05888	0.07000	0.00000	-0.00001	0.00000
115	0.00795	0.05981	0.00601	0.00000	0.00000	0.00000
116	0.00568	0.10049	0.09728	0.00000	0.00000	0.00000
131	0.00364	0.03432	-0.05168	0.00000	0.00000	0.00000
132	0.00728	0.07876	0.04728	0.00000	0.00000	0.00000
133	0.01082	0.10455	0.10440	0.00000	0.00000	0.00000
134	0.00356	0.05284	-0.01023	0.00000	0.00000	0.00000
SUM	0.00000	4.05619	0.44200	0.00000	0.00017	0.00000

Condition **LC26=1.2D+Di+WI30**

1	0.02943	0.17127	0.00130	0.00000	0.00015	0.00000
2	-0.00602	0.00000	-0.00917	0.00000	0.00000	0.00000
3	-0.12431	0.00000	0.00399	0.00000	0.00000	0.00000
4	0.03798	0.00000	-0.00312	0.00000	0.00000	0.00000
5	0.07324	0.00000	-0.00270	0.00000	0.00000	0.00000
6	0.17352	0.71473	0.04555	0.00000	-0.00003	0.00000
17	0.07743	0.86812	0.05023	0.00000	0.00010	0.00000
45	-0.05709	0.56378	-0.25561	0.00000	0.00009	0.00000
50	-0.00308	0.26768	0.15403	0.00000	-0.00006	0.00000
51	0.01056	0.00000	0.20607	0.00000	0.00000	0.00000
52	-0.00672	0.00000	-0.19120	0.00000	0.00000	0.00000
53	0.00254	0.00000	0.05352	0.00000	0.00000	0.00000
54	0.00755	0.00000	0.06545	0.00000	0.00000	0.00000
55	0.02718	1.07486	0.04574	0.00000	-0.00002	0.00000
115	0.00806	0.05702	-0.00024	0.00000	0.00000	0.00000
116	0.00485	0.08403	0.06063	0.00000	0.00000	0.00000
131	0.00366	0.03411	-0.05217	0.00000	0.00000	0.00000
132	0.00728	0.07876	0.04728	0.00000	0.00000	0.00000
133	0.01000	0.09409	0.08193	0.00000	0.00000	0.00000
134	0.00396	0.04775	-0.02152	0.00000	0.00000	0.00000
SUM	0.28001	4.05619	0.28001	0.00000	0.00023	0.00000

Condition **LC27=1.2D+Di+WI60**

1	0.02867	0.17144	0.00131	0.00000	0.00014	0.00000
2	-0.00766	0.00000	-0.00841	0.00000	0.00000	0.00000
3	-0.13021	0.00000	0.00397	0.00000	0.00000	0.00000
4	0.03828	0.00000	-0.00312	0.00000	0.00000	0.00000
5	0.05007	0.00000	-0.00266	0.00000	0.00000	0.00000
6	0.18325	0.72061	0.03723	0.00000	0.00003	0.00000
17	0.07303	0.86951	0.04137	0.00000	0.00009	0.00000
45	-0.05672	0.56413	-0.25383	0.00000	0.00005	0.00000
50	-0.00315	0.26759	0.15381	0.00000	-0.00003	0.00000
51	0.01245	0.00000	0.21115	0.00000	0.00000	0.00000
52	-0.00668	0.00000	-0.19120	0.00000	0.00000	0.00000
53	0.00254	0.00000	0.05286	0.00000	0.00000	0.00000
54	0.00906	0.00000	0.07252	0.00000	0.00000	0.00000
55	0.00719	1.08083	0.03691	0.00000	-0.00005	0.00000
115	0.00818	0.05626	-0.00195	0.00000	0.00000	0.00000
116	0.00454	0.07782	0.04674	0.00000	0.00000	0.00000
131	0.00371	0.03488	-0.05044	0.00000	0.00000	0.00000
132	0.00727	0.07852	0.04676	0.00000	0.00000	0.00000
133	0.00988	0.08719	0.06680	0.00000	0.00000	0.00000
134	0.00388	0.04742	-0.02222	0.00000	0.00000	0.00000
SUM	0.23759	4.05619	0.23759	0.00000	0.00024	0.00000

Condition **LC28=1.2D+Di+WI90**

1	0.02728	0.17177	0.00134	0.00000	0.00013	0.00000
2	0.03418	0.00000	-0.00637	0.00000	0.00000	0.00000
3	-0.13334	0.00000	0.00392	0.00000	0.00000	0.00000
4	0.03865	0.00000	-0.00311	0.00000	0.00000	0.00000
5	0.07602	0.00000	-0.00261	0.00000	0.00000	0.00000
6	0.20733	0.73429	0.01734	0.00000	0.00018	0.00000
17	0.06330	0.88065	0.01276	0.00000	0.00009	0.00000
45	-0.04583	0.56487	-0.25662	0.00000	-0.00007	0.00000
50	-0.00334	0.26665	0.15118	0.00000	0.00010	0.00000
51	0.01951	0.00000	0.19018	0.00000	0.00000	0.00000
52	-0.00653	0.00000	-0.18975	0.00000	0.00000	0.00000
53	0.00256	0.00000	0.05207	0.00000	0.00000	0.00000
54	0.01455	0.00000	0.04755	0.00000	0.00000	0.00000
55	-0.03156	1.10353	0.00195	0.00000	-0.00013	0.00000
115	0.00850	0.05087	-0.01402	0.00000	0.00000	0.00000
116	0.00346	0.05399	-0.00645	0.00000	0.00000	0.00000
131	0.00379	0.03594	-0.04811	0.00000	0.00000	0.00000
132	0.00727	0.07818	0.04599	0.00000	0.00000	0.00000
133	0.00929	0.07186	0.03345	0.00000	0.00000	0.00000
134	0.00391	0.04358	-0.03069	0.00000	0.00000	0.00000
SUM	0.29900	4.05619	0.00000	0.00000	0.00029	0.00000

Condition **LC29=1.2D+Di+WI120**

1	0.02570	0.17212	0.00137	0.00000	0.00011	0.00000
2	0.04819	0.00000	-0.00433	0.00000	0.00000	0.00000
3	-0.14351	0.00000	0.00386	0.00000	0.00000	0.00000
4	0.03915	0.00000	-0.00310	0.00000	0.00000	0.00000
5	0.04513	0.00000	-0.00255	0.00000	0.00000	0.00000
6	0.22934	0.74819	-0.00305	0.00000	0.00033	0.00000
17	0.04984	0.89058	-0.01538	0.00000	0.00010	0.00000
45	-0.03556	0.56636	-0.26336	0.00000	-0.00009	0.00000
50	-0.00328	0.26637	0.15095	0.00000	0.00009	0.00000
51	0.01903	0.00000	0.17136	0.00000	0.00000	0.00000
52	-0.00656	0.00000	-0.18939	0.00000	0.00000	0.00000

53	0.00253	0.00000	0.05010	0.00000	0.00000	0.00000
54	0.01395	0.00000	0.02004	0.00000	0.00000	0.00000
55	-0.08144	1.12472	-0.03115	0.00000	-0.00022	0.00000
115	0.00885	0.04571	-0.02559	0.00000	0.00000	0.00000
116	0.00246	0.03135	-0.05701	0.00000	0.00000	0.00000
131	0.00387	0.03727	-0.04516	0.00000	0.00000	0.00000
132	0.00726	0.07775	0.04504	0.00000	0.00000	0.00000
133	0.00876	0.05588	-0.00140	0.00000	0.00000	0.00000
134	0.00385	0.03989	-0.03882	0.00000	0.00000	0.00000
SUM	0.23759	4.05619	-0.23759	0.00000	0.00031	0.00000

Condition **LC30=1.2D+Di+WI150**

1	0.02535	0.17221	0.00138	0.00000	0.00010	0.00000
2	0.06851	0.00000	-0.00352	0.00000	0.00000	0.00000
3	-0.14286	0.00000	0.00384	0.00000	0.00000	0.00000
4	0.03917	0.00000	-0.00310	0.00000	0.00000	0.00000
5	0.06796	0.00000	-0.00254	0.00000	0.00000	0.00000
6	0.23629	0.75260	-0.01038	0.00000	0.00038	0.00000
17	0.04337	0.89409	-0.02482	0.00000	0.00008	0.00000
45	-0.02952	0.56605	-0.26480	0.00000	-0.00008	0.00000
50	-0.00320	0.26663	0.15207	0.00000	0.00006	0.00000
51	0.01698	0.00000	0.17799	0.00000	0.00000	0.00000
52	-0.00661	0.00000	-0.18999	0.00000	0.00000	0.00000
53	0.00252	0.00000	0.04816	0.00000	0.00000	0.00000
54	0.01220	0.00000	0.02533	0.00000	0.00000	0.00000
55	-0.08481	1.12949	-0.03867	0.00000	-0.00024	0.00000
115	0.00891	0.04486	-0.02750	0.00000	0.00000	0.00000
116	0.00218	0.02622	-0.06843	0.00000	0.00000	0.00000
131	0.00389	0.03736	-0.04495	0.00000	0.00000	0.00000
132	0.00726	0.07770	0.04492	0.00000	0.00000	0.00000
133	0.00846	0.05088	-0.01221	0.00000	0.00000	0.00000
134	0.00396	0.03809	-0.04280	0.00000	0.00000	0.00000
SUM	0.28001	4.05619	-0.28001	0.00000	0.00031	0.00000

Condition **LC31=1.2D+Di-WI0**

1	0.02322	0.17268	0.00141	0.00000	0.00009	0.00000
2	0.02475	0.00000	-0.00176	0.00000	0.00000	0.00000
3	-0.16862	0.00000	0.00379	0.00000	0.00000	0.00000
4	0.04021	0.00000	-0.00309	0.00000	0.00000	0.00000
5	-0.07038	0.00000	-0.00244	0.00000	0.00000	0.00000
6	0.25731	0.76701	-0.03050	0.00000	0.00053	0.00000
17	0.02996	0.89644	-0.04596	0.00000	0.00008	0.00000
45	-0.03292	0.56860	-0.26678	0.00000	-0.00005	0.00000
50	-0.00305	0.26679	0.15313	0.00000	0.00000	0.00000
51	0.01338	0.00000	0.16784	0.00000	0.00000	0.00000
52	-0.00671	0.00000	-0.19042	0.00000	0.00000	0.00000
53	0.00249	0.00000	0.04933	0.00000	0.00000	0.00000
54	0.00923	0.00000	0.01167	0.00000	0.00000	0.00000
55	-0.15275	1.14389	-0.06112	0.00000	-0.00034	0.00000
115	0.00924	0.04241	-0.03302	0.00000	0.00000	0.00000
116	0.00148	0.01043	-0.10377	0.00000	0.00000	0.00000
131	0.00401	0.03975	-0.03964	0.00000	0.00000	0.00000
132	0.00724	0.07699	0.04334	0.00000	0.00000	0.00000
133	0.00828	0.03340	-0.05064	0.00000	0.00000	0.00000
134	0.00361	0.03779	-0.04335	0.00000	0.00000	0.00000
SUM	0.00000	4.05619	-0.44200	0.00000	0.00031	0.00000

Condition **LC32=1.2D+Di-WI30**

1	0.02372	0.17252	0.00139	0.00000	0.00011	0.00000
2	-0.06433	0.00000	-0.00363	0.00000	0.00000	0.00000
3	-0.18192	0.00000	0.00384	0.00000	0.00000	0.00000
4	0.04045	0.00000	-0.00310	0.00000	0.00000	0.00000
5	-0.20537	0.00000	-0.00245	0.00000	0.00000	0.00000
6	0.23865	0.75722	-0.01437	0.00000	0.00041	0.00000
17	0.04033	0.88532	-0.02209	0.00000	0.00012	0.00000
45	-0.05201	0.56986	-0.26371	0.00000	0.00008	0.00000
50	-0.00283	0.26753	0.15523	0.00000	-0.00014	0.00000
51	0.00614	0.00000	0.17349	0.00000	0.00000	0.00000
52	-0.00688	0.00000	-0.19150	0.00000	0.00000	0.00000
53	0.00248	0.00000	0.05326	0.00000	0.00000	0.00000
54	0.00365	0.00000	0.02031	0.00000	0.00000	0.00000
55	-0.15709	1.12792	-0.03680	0.00000	-0.00033	0.00000
115	0.00913	0.04520	-0.02680	0.00000	0.00000	0.00000
116	0.00232	0.02692	-0.06706	0.00000	0.00000	0.00000
131	0.00399	0.04005	-0.03894	0.00000	0.00000	0.00000
132	0.00724	0.07697	0.04328	0.00000	0.00000	0.00000
133	0.00910	0.04376	-0.02839	0.00000	0.00000	0.00000
134	0.00322	0.04292	-0.03197	0.00000	0.00000	0.00000
SUM	-0.28001	4.05619	-0.28001	0.00000	0.00026	0.00000

Condition **LC33=1.2D+Di-WI60**

1	0.02449	0.17236	0.00138	0.00000	0.00011	0.00000
2	-0.06272	0.00000	-0.00439	0.00000	0.00000	0.00000
3	-0.17601	0.00000	0.00386	0.00000	0.00000	0.00000
4	0.04014	0.00000	-0.00310	0.00000	0.00000	0.00000
5	-0.18220	0.00000	-0.00249	0.00000	0.00000	0.00000
6	0.22891	0.75133	-0.00604	0.00000	0.00035	0.00000
17	0.04472	0.88393	-0.01323	0.00000	0.00013	0.00000
45	-0.05236	0.56951	-0.26551	0.00000	0.00012	0.00000
50	-0.00277	0.26763	0.15545	0.00000	-0.00017	0.00000
51	0.00425	0.00000	0.16844	0.00000	0.00000	0.00000
52	-0.00692	0.00000	-0.19150	0.00000	0.00000	0.00000
53	0.00247	0.00000	0.05389	0.00000	0.00000	0.00000
54	0.00214	0.00000	0.01326	0.00000	0.00000	0.00000
55	-0.13709	1.12195	-0.02796	0.00000	-0.00030	0.00000
115	0.00901	0.04595	-0.02509	0.00000	0.00000	0.00000
116	0.00263	0.03313	-0.05317	0.00000	0.00000	0.00000
131	0.00395	0.03928	-0.04067	0.00000	0.00000	0.00000
132	0.00724	0.07720	0.04380	0.00000	0.00000	0.00000
133	0.00923	0.05066	-0.01326	0.00000	0.00000	0.00000
134	0.00330	0.04326	-0.03127	0.00000	0.00000	0.00000
SUM	-0.23759	4.05619	-0.23759	0.00000	0.00024	0.00000

Condition **LC34=1.2D+Di-WI90**

1	0.02587	0.17204	0.00135	0.00000	0.00013	0.00000
2	-0.10412	0.00000	-0.00643	0.00000	0.00000	0.00000
3	-0.17319	0.00000	0.00392	0.00000	0.00000	0.00000
4	0.03979	0.00000	-0.00311	0.00000	0.00000	0.00000
5	-0.20820	0.00000	-0.00254	0.00000	0.00000	0.00000
6	0.20491	0.73766	0.01385	0.00000	0.00021	0.00000
17	0.05473	0.87278	0.01537	0.00000	0.00013	0.00000
45	-0.06417	0.56878	-0.26216	0.00000	0.00024	0.00000
50	-0.00257	0.26856	0.15808	0.00000	-0.00029	0.00000
51	-0.00278	0.00000	0.18844	0.00000	0.00000	0.00000

52	-0.00707	0.00000	-0.19295	0.00000	0.00000	0.00000
53	0.00246	0.00000	0.05540	0.00000	0.00000	0.00000
54	-0.00334	0.00000	0.03786	0.00000	0.00000	0.00000
55	-0.09793	1.09921	0.00702	0.00000	-0.00022	0.00000
115	0.00869	0.05132	-0.01306	0.00000	0.00000	0.00000
116	0.00371	0.05697	0.00007	0.00000	0.00000	0.00000
131	0.00387	0.03824	-0.04297	0.00000	0.00000	0.00000
132	0.00725	0.07754	0.04456	0.00000	0.00000	0.00000
133	0.00982	0.06596	0.02004	0.00000	0.00000	0.00000
134	0.00326	0.04712	-0.02275	0.00000	0.00000	0.00000
SUM	-0.29900	4.05619	0.00000	0.00000	0.00019	0.00000

Condition **LC35=1.2D+Di-WI120**

1	0.02743	0.17164	0.00132	0.00000	0.00014	0.00000
2	-0.11829	0.00000	-0.00847	0.00000	0.00000	0.00000
3	-0.16397	0.00000	0.00397	0.00000	0.00000	0.00000
4	0.03924	0.00000	-0.00312	0.00000	0.00000	0.00000
5	-0.17696	0.00000	-0.00260	0.00000	0.00000	0.00000
6	0.18340	0.72380	0.03423	0.00000	0.00006	0.00000
17	0.06675	0.86289	0.04353	0.00000	0.00013	0.00000
45	-0.07208	0.56725	-0.25677	0.00000	0.00026	0.00000
50	-0.00264	0.26885	0.15831	0.00000	-0.00029	0.00000
51	-0.00234	0.00000	0.20955	0.00000	0.00000	0.00000
52	-0.00704	0.00000	-0.19329	0.00000	0.00000	0.00000
53	0.00248	0.00000	0.05570	0.00000	0.00000	0.00000
54	-0.00277	0.00000	0.06619	0.00000	0.00000	0.00000
55	-0.04854	1.07806	0.04007	0.00000	-0.00013	0.00000
115	0.00834	0.05651	-0.00142	0.00000	0.00000	0.00000
116	0.00471	0.07958	0.05054	0.00000	0.00000	0.00000
131	0.00378	0.03685	-0.04604	0.00000	0.00000	0.00000
132	0.00726	0.07798	0.04555	0.00000	0.00000	0.00000
133	0.01035	0.08201	0.05505	0.00000	0.00000	0.00000
134	0.00332	0.05076	-0.01472	0.00000	0.00000	0.00000
SUM	-0.23759	4.05619	0.23759	0.00000	0.00017	0.00000

Condition **LC36=1.2D+Di-WI150**

1	0.02774	0.17149	0.00131	0.00000	0.00015	0.00000
2	-0.13748	0.00000	-0.00926	0.00000	0.00000	0.00000
3	-0.16710	0.00000	0.00399	0.00000	0.00000	0.00000
4	0.03918	0.00000	-0.00312	0.00000	0.00000	0.00000
5	-0.19939	0.00000	-0.00261	0.00000	0.00000	0.00000
6	0.17757	0.71949	0.04155	0.00000	0.00001	0.00000
17	0.07174	0.85943	0.05299	0.00000	0.00014	0.00000
45	-0.07712	0.56753	-0.25582	0.00000	0.00026	0.00000
50	-0.00272	0.26859	0.15719	0.00000	-0.00026	0.00000
51	-0.00029	0.00000	0.20366	0.00000	0.00000	0.00000
52	-0.00699	0.00000	-0.19269	0.00000	0.00000	0.00000
53	0.00250	0.00000	0.05716	0.00000	0.00000	0.00000
54	-0.00102	0.00000	0.06112	0.00000	0.00000	0.00000
55	-0.04478	1.07323	0.04758	0.00000	-0.00012	0.00000
115	0.00828	0.05735	0.00046	0.00000	0.00000	0.00000
116	0.00499	0.08471	0.06197	0.00000	0.00000	0.00000
131	0.00376	0.03671	-0.04635	0.00000	0.00000	0.00000
132	0.00726	0.07805	0.04570	0.00000	0.00000	0.00000
133	0.01065	0.08705	0.06595	0.00000	0.00000	0.00000
134	0.00321	0.05256	-0.01075	0.00000	0.00000	0.00000

SUM	-0.28001	4.05619	0.28001	0.00000	0.00018	0.00000
Condition	**LC37=0.9D**					
1	0.00957	0.06129	0.00036	0.00000	0.00004	0.00000
2	-0.02103	0.00000	-0.00184	0.00000	0.00000	0.00000
3	-0.04733	0.00000	0.00122	0.00000	0.00000	0.00000
4	0.01429	0.00000	-0.00104	0.00000	0.00000	0.00000
5	-0.01964	0.00000	-0.00066	0.00000	0.00000	0.00000
6	0.05296	0.21586	0.00412	0.00000	0.00005	0.00000
17	0.03859	0.32288	0.00459	0.00000	0.00007	0.00000
45	-0.02082	0.24066	-0.12253	0.00000	0.00005	0.00000
50	-0.00117	0.11435	0.07149	0.00000	-0.00006	0.00000
51	0.00273	0.00000	0.08759	0.00000	0.00000	0.00000
52	-0.00286	0.00000	-0.08600	0.00000	0.00000	0.00000
53	0.00113	0.00000	0.02359	0.00000	0.00000	0.00000
54	0.00283	0.00000	0.02230	0.00000	0.00000	0.00000
55	-0.02136	0.38361	-0.00235	0.00000	-0.00007	0.00000
115	0.00291	0.01778	-0.00303	0.00000	0.00000	0.00000
116	0.00116	0.02056	0.00333	0.00000	0.00000	0.00000
131	0.00138	0.01377	-0.01223	0.00000	0.00000	0.00000
132	0.00241	0.02552	0.01392	0.00000	0.00000	0.00000
133	0.00304	0.02259	0.00790	0.00000	0.00000	0.00000
134	0.00122	0.01439	-0.01074	0.00000	0.00000	0.00000
SUM	0.00000	1.45327	0.00000	0.00000	0.00009	0.00000
Condition	**LC38=1.2D**					
1	0.01276	0.08173	0.00048	0.00000	0.00005	0.00000
2	-0.02804	0.00000	-0.00245	0.00000	0.00000	0.00000
3	-0.06311	0.00000	0.00163	0.00000	0.00000	0.00000
4	0.01905	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.02618	0.00000	-0.00087	0.00000	0.00000	0.00000
6	0.07062	0.28781	0.00550	0.00000	0.00007	0.00000
17	0.05145	0.43051	0.00613	0.00000	0.00009	0.00000
45	-0.02775	0.32089	-0.16340	0.00000	0.00007	0.00000
50	-0.00157	0.15246	0.09533	0.00000	-0.00008	0.00000
51	0.00364	0.00000	0.11680	0.00000	0.00000	0.00000
52	-0.00381	0.00000	-0.11468	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.03146	0.00000	0.00000	0.00000
54	0.00377	0.00000	0.02974	0.00000	0.00000	0.00000
55	-0.02849	0.51148	-0.00313	0.00000	-0.00009	0.00000
115	0.00388	0.02371	-0.00405	0.00000	0.00000	0.00000
116	0.00154	0.02742	0.00444	0.00000	0.00000	0.00000
131	0.00184	0.01836	-0.01631	0.00000	0.00000	0.00000
132	0.00322	0.03402	0.01856	0.00000	0.00000	0.00000
133	0.00406	0.03012	0.01053	0.00000	0.00000	0.00000
134	0.00163	0.01918	-0.01432	0.00000	0.00000	0.00000
SUM	0.00000	1.93769	0.00000	0.00000	0.00012	0.00000
Condition	**LC41=1.2D+WL0**					
1	0.01377	0.08141	0.00046	0.00000	0.00006	0.00000
2	-0.04498	0.00000	-0.00391	0.00000	0.00000	0.00000
3	-0.06197	0.00000	0.00166	0.00000	0.00000	0.00000
4	0.01870	0.00000	-0.00140	0.00000	0.00000	0.00000
5	-0.02435	0.00000	-0.00092	0.00000	0.00000	0.00000
6	0.05607	0.27810	0.02030	0.00000	-0.00004	0.00000
17	0.05888	0.42498	0.02408	0.00000	0.00010	0.00000
45	-0.03353	0.32036	-0.16174	0.00000	0.00011	0.00000
50	-0.00154	0.15269	0.09569	0.00000	-0.00011	0.00000

51	0.00223	0.00000	0.12283	0.00000	0.00000	0.00000
52	-0.00384	0.00000	-0.11490	0.00000	0.00000	0.00000
53	0.00151	0.00000	0.03241	0.00000	0.00000	0.00000
54	0.00275	0.00000	0.03798	0.00000	0.00000	0.00000
55	-0.00063	0.49843	0.01669	0.00000	-0.00004	0.00000
115	0.00369	0.02586	0.00079	0.00000	0.00000	0.00000
116	0.00218	0.04116	0.03512	0.00000	0.00000	0.00000
131	0.00178	0.01746	-0.01829	0.00000	0.00000	0.00000
132	0.00322	0.03431	0.01922	0.00000	0.00000	0.00000
133	0.00446	0.04149	0.03530	0.00000	0.00000	0.00000
134	0.00161	0.02144	-0.00936	0.00000	0.00000	0.00000
SUM	0.00000	1.93769	0.13200	0.00000	0.00009	0.00000

Condition **LC42=1.2D+WL30**

1	0.01366	0.08151	0.00047	0.00000	0.00006	0.00000
2	-0.01917	0.00000	-0.00334	0.00000	0.00000	0.00000
3	-0.05473	0.00000	0.00165	0.00000	0.00000	0.00000
4	0.01864	0.00000	-0.00140	0.00000	0.00000	0.00000
5	0.01691	0.00000	-0.00091	0.00000	0.00000	0.00000
6	0.06032	0.28098	0.01520	0.00000	0.00000	0.00000
17	0.05693	0.42805	0.01760	0.00000	0.00009	0.00000
45	-0.02810	0.31995	-0.16264	0.00000	0.00008	0.00000
50	-0.00160	0.15249	0.09518	0.00000	-0.00007	0.00000
51	0.00410	0.00000	0.12147	0.00000	0.00000	0.00000
52	-0.00379	0.00000	-0.11463	0.00000	0.00000	0.00000
53	0.00151	0.00000	0.03125	0.00000	0.00000	0.00000
54	0.00418	0.00000	0.03579	0.00000	0.00000	0.00000
55	0.00079	0.50305	0.00999	0.00000	-0.00004	0.00000
115	0.00371	0.02534	-0.00037	0.00000	0.00000	0.00000
116	0.00195	0.03650	0.02473	0.00000	0.00000	0.00000
131	0.00179	0.01739	-0.01846	0.00000	0.00000	0.00000
132	0.00322	0.03431	0.01921	0.00000	0.00000	0.00000
133	0.00420	0.03824	0.02833	0.00000	0.00000	0.00000
134	0.00174	0.01986	-0.01285	0.00000	0.00000	0.00000
SUM	0.08627	1.93769	0.08627	0.00000	0.00011	0.00000

Condition **LC43=1.2D+WL60**

1	0.01336	0.08159	0.00047	0.00000	0.00006	0.00000
2	-0.02055	0.00000	-0.00302	0.00000	0.00000	0.00000
3	-0.05673	0.00000	0.00164	0.00000	0.00000	0.00000
4	0.01877	0.00000	-0.00140	0.00000	0.00000	0.00000
5	0.00669	0.00000	-0.00090	0.00000	0.00000	0.00000
6	0.06402	0.28338	0.01177	0.00000	0.00002	0.00000
17	0.05506	0.42852	0.01346	0.00000	0.00009	0.00000
45	-0.02801	0.32013	-0.16204	0.00000	0.00006	0.00000
50	-0.00162	0.15246	0.09512	0.00000	-0.00006	0.00000
51	0.00472	0.00000	0.12298	0.00000	0.00000	0.00000
52	-0.00378	0.00000	-0.11464	0.00000	0.00000	0.00000
53	0.00151	0.00000	0.03105	0.00000	0.00000	0.00000
54	0.00468	0.00000	0.03793	0.00000	0.00000	0.00000
55	-0.00812	0.50563	0.00597	0.00000	-0.00006	0.00000
115	0.00376	0.02517	-0.00076	0.00000	0.00000	0.00000
116	0.00181	0.03373	0.01855	0.00000	0.00000	0.00000
131	0.00181	0.01772	-0.01774	0.00000	0.00000	0.00000
132	0.00322	0.03421	0.01899	0.00000	0.00000	0.00000
133	0.00415	0.03540	0.02209	0.00000	0.00000	0.00000
134	0.00171	0.01976	-0.01306	0.00000	0.00000	0.00000

SUM	0.06647	1.93769	0.06647	0.00000	0.00012	0.00000
Condition	**LC44=1.2D+WL90**					
1	0.01298	0.08172	0.00048	0.00000	0.00005	0.00000
2	-0.00989	0.00000	-0.00245	0.00000	0.00000	0.00000
3	-0.05585	0.00000	0.00163	0.00000	0.00000	0.00000
4	0.01890	0.00000	-0.00139	0.00000	0.00000	0.00000
5	0.01319	0.00000	-0.00088	0.00000	0.00000	0.00000
6	0.07017	0.28726	0.00599	0.00000	0.00006	0.00000
17	0.05333	0.43158	0.00580	0.00000	0.00009	0.00000
45	-0.02526	0.32037	-0.16269	0.00000	0.00003	0.00000
50	-0.00167	0.15219	0.09437	0.00000	-0.00003	0.00000
51	0.00675	0.00000	0.11720	0.00000	0.00000	0.00000
52	-0.00374	0.00000	-0.11423	0.00000	0.00000	0.00000
53	0.00152	0.00000	0.03075	0.00000	0.00000	0.00000
54	0.00627	0.00000	0.03120	0.00000	0.00000	0.00000
55	-0.01979	0.51213	-0.00386	0.00000	-0.00008	0.00000
115	0.00385	0.02365	-0.00416	0.00000	0.00000	0.00000
116	0.00151	0.02699	0.00351	0.00000	0.00000	0.00000
131	0.00183	0.01805	-0.01700	0.00000	0.00000	0.00000
132	0.00322	0.03410	0.01875	0.00000	0.00000	0.00000
133	0.00398	0.03094	0.01238	0.00000	0.00000	0.00000
134	0.00172	0.01870	-0.01539	0.00000	0.00000	0.00000
SUM	0.08300	1.93769	0.00000	0.00000	0.00013	0.00000
Condition	**LC45=1.2D+WL120**					
1	0.01255	0.08184	0.00049	0.00000	0.00005	0.00000
2	-0.00625	0.00000	-0.00186	0.00000	0.00000	0.00000
3	-0.05771	0.00000	0.00161	0.00000	0.00000	0.00000
4	0.01906	0.00000	-0.00139	0.00000	0.00000	0.00000
5	0.00494	0.00000	-0.00087	0.00000	0.00000	0.00000
6	0.07595	0.29120	0.00008	0.00000	0.00011	0.00000
17	0.05006	0.43441	-0.00183	0.00000	0.00009	0.00000
45	-0.02282	0.32077	-0.16433	0.00000	0.00002	0.00000
50	-0.00165	0.15212	0.09436	0.00000	-0.00003	0.00000
51	0.00654	0.00000	0.11168	0.00000	0.00000	0.00000
52	-0.00375	0.00000	-0.11417	0.00000	0.00000	0.00000
53	0.00151	0.00000	0.03049	0.00000	0.00000	0.00000
54	0.00604	0.00000	0.02356	0.00000	0.00000	0.00000
55	-0.03375	0.51814	-0.01309	0.00000	-0.00010	0.00000
115	0.00395	0.02221	-0.00739	0.00000	0.00000	0.00000
116	0.00123	0.02061	-0.01073	0.00000	0.00000	0.00000
131	0.00186	0.01844	-0.01613	0.00000	0.00000	0.00000
132	0.00322	0.03398	0.01847	0.00000	0.00000	0.00000
133	0.00383	0.02634	0.00237	0.00000	0.00000	0.00000
134	0.00170	0.01761	-0.01780	0.00000	0.00000	0.00000
SUM	0.06647	1.93769	-0.06647	0.00000	0.00014	0.00000
Condition	**LC46=1.2D+WL150**					
1	0.01242	0.08190	0.00049	0.00000	0.00005	0.00000
2	0.00274	0.00000	-0.00153	0.00000	0.00000	0.00000
3	-0.05627	0.00000	0.00161	0.00000	0.00000	0.00000
4	0.01907	0.00000	-0.00139	0.00000	0.00000	0.00000
5	0.01467	0.00000	-0.00086	0.00000	0.00000	0.00000
6	0.07855	0.29298	-0.00292	0.00000	0.00013	0.00000
17	0.04803	0.43571	-0.00622	0.00000	0.00008	0.00000
45	-0.02053	0.32066	-0.16477	0.00000	0.00002	0.00000

50	-0.00163	0.15220	0.09470	0.00000	-0.00003	0.00000
51	0.00595	0.00000	0.11365	0.00000	0.00000	0.00000
52	-0.00376	0.00000	-0.11435	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.02991	0.00000	0.00000	0.00000
54	0.00552	0.00000	0.02507	0.00000	0.00000	0.00000
55	-0.03561	0.52038	-0.01669	0.00000	-0.00011	0.00000
115	0.00397	0.02203	-0.00779	0.00000	0.00000	0.00000
116	0.00110	0.01822	-0.01607	0.00000	0.00000	0.00000
131	0.00186	0.01849	-0.01602	0.00000	0.00000	0.00000
132	0.00322	0.03395	0.01841	0.00000	0.00000	0.00000
133	0.00370	0.02428	-0.00209	0.00000	0.00000	0.00000
134	0.00175	0.01688	-0.01942	0.00000	0.00000	0.00000
SUM	0.08627	1.93769	-0.08627	0.00000	0.00014	0.00000

Condition **LC47=1.2D-WL0**

1	0.01174	0.08205	0.00050	0.00000	0.00004	0.00000
2	-0.01102	0.00000	-0.00099	0.00000	0.00000	0.00000
3	-0.06438	0.00000	0.00159	0.00000	0.00000	0.00000
4	0.01941	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.02799	0.00000	-0.00083	0.00000	0.00000	0.00000
6	0.08522	0.29753	-0.00930	0.00000	0.00017	0.00000
17	0.04396	0.43604	-0.01182	0.00000	0.00008	0.00000
45	-0.02195	0.32141	-0.16506	0.00000	0.00003	0.00000
50	-0.00159	0.15224	0.09497	0.00000	-0.00005	0.00000
51	0.00505	0.00000	0.11077	0.00000	0.00000	0.00000
52	-0.00379	0.00000	-0.11447	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.03051	0.00000	0.00000	0.00000
54	0.00478	0.00000	0.02150	0.00000	0.00000	0.00000
55	-0.05632	0.52453	-0.02295	0.00000	-0.00014	0.00000
115	0.00407	0.02155	-0.00889	0.00000	0.00000	0.00000
116	0.00091	0.01367	-0.02624	0.00000	0.00000	0.00000
131	0.00190	0.01925	-0.01433	0.00000	0.00000	0.00000
132	0.00321	0.03373	0.01791	0.00000	0.00000	0.00000
133	0.00365	0.01876	-0.01423	0.00000	0.00000	0.00000
134	0.00164	0.01692	-0.01927	0.00000	0.00000	0.00000
SUM	0.00000	1.93769	-0.13200	0.00000	0.00014	0.00000

Condition **LC48=1.2D-WL30**

1	0.01185	0.08195	0.00050	0.00000	0.00005	0.00000
2	-0.03690	0.00000	-0.00156	0.00000	0.00000	0.00000
3	-0.07150	0.00000	0.00160	0.00000	0.00000	0.00000
4	0.01947	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.06927	0.00000	-0.00083	0.00000	0.00000	0.00000
6	0.08092	0.29464	-0.00420	0.00000	0.00014	0.00000
17	0.04597	0.43297	-0.00534	0.00000	0.00009	0.00000
45	-0.02740	0.32182	-0.16416	0.00000	0.00007	0.00000
50	-0.00154	0.15243	0.09549	0.00000	-0.00009	0.00000
51	0.00319	0.00000	0.11212	0.00000	0.00000	0.00000
52	-0.00383	0.00000	-0.11473	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.03166	0.00000	0.00000	0.00000
54	0.00335	0.00000	0.02369	0.00000	0.00000	0.00000
55	-0.05777	0.51992	-0.01625	0.00000	-0.00014	0.00000
115	0.00404	0.02207	-0.00772	0.00000	0.00000	0.00000
116	0.00114	0.01834	-0.01586	0.00000	0.00000	0.00000
131	0.00189	0.01933	-0.01416	0.00000	0.00000	0.00000
132	0.00321	0.03373	0.01791	0.00000	0.00000	0.00000
133	0.00391	0.02200	-0.00726	0.00000	0.00000	0.00000

134	0.00151	0.01850	-0.01578	0.00000	0.00000	0.00000
SUM	-0.08627	1.93769	-0.08627	0.00000	0.00012	0.00000

Condition **LC49=1.2D-WL60**

1	0.01216	0.08186	0.00049	0.00000	0.00005	0.00000
2	-0.03552	0.00000	-0.00187	0.00000	0.00000	0.00000
3	-0.06949	0.00000	0.00161	0.00000	0.00000	0.00000
4	0.01933	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.05905	0.00000	-0.00085	0.00000	0.00000	0.00000
6	0.07721	0.29224	-0.00077	0.00000	0.00012	0.00000
17	0.04784	0.43250	-0.00121	0.00000	0.00010	0.00000
45	-0.02749	0.32164	-0.16476	0.00000	0.00008	0.00000
50	-0.00152	0.15246	0.09554	0.00000	-0.00010	0.00000
51	0.00256	0.00000	0.11061	0.00000	0.00000	0.00000
52	-0.00384	0.00000	-0.11472	0.00000	0.00000	0.00000
53	0.00149	0.00000	0.03187	0.00000	0.00000	0.00000
54	0.00285	0.00000	0.02156	0.00000	0.00000	0.00000
55	-0.04886	0.51734	-0.01223	0.00000	-0.00012	0.00000
115	0.00400	0.02224	-0.00733	0.00000	0.00000	0.00000
116	0.00127	0.02110	-0.00968	0.00000	0.00000	0.00000
131	0.00187	0.01900	-0.01489	0.00000	0.00000	0.00000
132	0.00321	0.03383	0.01813	0.00000	0.00000	0.00000
133	0.00396	0.02485	-0.00102	0.00000	0.00000	0.00000
134	0.00154	0.01860	-0.01557	0.00000	0.00000	0.00000
SUM	-0.06647	1.93769	-0.06647	0.00000	0.00012	0.00000

Condition **LC50=1.2D-WL90**

1	0.01253	0.08174	0.00048	0.00000	0.00005	0.00000
2	-0.04609	0.00000	-0.00245	0.00000	0.00000	0.00000
3	-0.07045	0.00000	0.00162	0.00000	0.00000	0.00000
4	0.01921	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.06556	0.00000	-0.00086	0.00000	0.00000	0.00000
6	0.07109	0.28837	0.00501	0.00000	0.00007	0.00000
17	0.04962	0.42944	0.00646	0.00000	0.00010	0.00000
45	-0.03044	0.32141	-0.16399	0.00000	0.00011	0.00000
50	-0.00146	0.15273	0.09630	0.00000	-0.00013	0.00000
51	0.00054	0.00000	0.11620	0.00000	0.00000	0.00000
52	-0.00389	0.00000	-0.11513	0.00000	0.00000	0.00000
53	0.00149	0.00000	0.03231	0.00000	0.00000	0.00000
54	0.00127	0.00000	0.02821	0.00000	0.00000	0.00000
55	-0.03710	0.51083	-0.00239	0.00000	-0.00010	0.00000
115	0.00391	0.02376	-0.00394	0.00000	0.00000	0.00000
116	0.00158	0.02784	0.00537	0.00000	0.00000	0.00000
131	0.00185	0.01867	-0.01562	0.00000	0.00000	0.00000
132	0.00321	0.03394	0.01837	0.00000	0.00000	0.00000
133	0.00413	0.02931	0.00868	0.00000	0.00000	0.00000
134	0.00153	0.01966	-0.01323	0.00000	0.00000	0.00000
SUM	-0.08300	1.93769	0.00000	0.00000	0.00010	0.00000

Condition **LC51=1.2D-WL120**

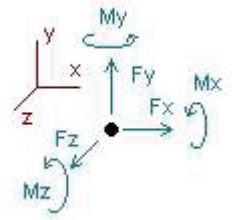
1	0.01297	0.08161	0.00047	0.00000	0.00006	0.00000
2	-0.04982	0.00000	-0.00304	0.00000	0.00000	0.00000
3	-0.06851	0.00000	0.00164	0.00000	0.00000	0.00000
4	0.01905	0.00000	-0.00139	0.00000	0.00000	0.00000
5	-0.05730	0.00000	-0.00088	0.00000	0.00000	0.00000
6	0.06529	0.28442	0.01092	0.00000	0.00003	0.00000
17	0.05284	0.42661	0.01408	0.00000	0.00010	0.00000
45	-0.03268	0.32100	-0.16247	0.00000	0.00012	0.00000
50	-0.00148	0.15280	0.09631	0.00000	-0.00013	0.00000
51	0.00075	0.00000	0.12191	0.00000	0.00000	0.00000
52	-0.00388	0.00000	-0.11519	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.03243	0.00000	0.00000	0.00000
54	0.00149	0.00000	0.03592	0.00000	0.00000	0.00000
55	-0.02322	0.50482	0.00683	0.00000	-0.00008	0.00000
115	0.00381	0.02520	-0.00070	0.00000	0.00000	0.00000
116	0.00186	0.03422	0.01960	0.00000	0.00000	0.00000
131	0.00183	0.01827	-0.01649	0.00000	0.00000	0.00000
132	0.00322	0.03406	0.01866	0.00000	0.00000	0.00000
133	0.00429	0.03390	0.01870	0.00000	0.00000	0.00000
134	0.00155	0.02075	-0.01083	0.00000	0.00000	0.00000
SUM	-0.06647	1.93769	0.06647	0.00000	0.00009	0.00000

Condition **LC52=1.2D-WL150**

1	0.01309	0.08155	0.00047	0.00000	0.00006	0.00000
2	-0.05871	0.00000	-0.00337	0.00000	0.00000	0.00000
3	-0.07014	0.00000	0.00165	0.00000	0.00000	0.00000
4	0.01903	0.00000	-0.00140	0.00000	0.00000	0.00000
5	-0.06700	0.00000	-0.00089	0.00000	0.00000	0.00000
6	0.06277	0.28265	0.01392	0.00000	0.00001	0.00000
17	0.05477	0.42531	0.01848	0.00000	0.00010	0.00000
45	-0.03495	0.32111	-0.16204	0.00000	0.00012	0.00000
50	-0.00150	0.15272	0.09597	0.00000	-0.00012	0.00000
51	0.00133	0.00000	0.11996	0.00000	0.00000	0.00000
52	-0.00386	0.00000	-0.11502	0.00000	0.00000	0.00000
53	0.00150	0.00000	0.03300	0.00000	0.00000	0.00000
54	0.00201	0.00000	0.03441	0.00000	0.00000	0.00000
55	-0.02132	0.50258	0.01043	0.00000	-0.00007	0.00000
115	0.00379	0.02538	-0.00031	0.00000	0.00000	0.00000
116	0.00198	0.03662	0.02495	0.00000	0.00000	0.00000
131	0.00182	0.01822	-0.01661	0.00000	0.00000	0.00000
132	0.00322	0.03409	0.01872	0.00000	0.00000	0.00000
133	0.00441	0.03597	0.02316	0.00000	0.00000	0.00000
134	0.00150	0.02149	-0.00921	0.00000	0.00000	0.00000
SUM	-0.08627	1.93769	0.08627	0.00000	0.00009	0.00000

Envelope for nodal reactions

Note.- **Ic** is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150
LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

Node		Forces						Moments					
		Fx [Kip]	lc	Fy [Kip]	lc	Fz [Kip]	lc	Mx [Kip*ft]	lc	My [Kip*ft]	lc	Mz [Kip*ft]	lc
1	Max	0.039	LC3	0.173	LC31	0.003	LC12	0.00000	LC1	0.00141	LC6	0.00000	LC1
	Min	-0.013	LC21	0.012	LC13	-0.002	LC18	0.00000	LC1	-0.00131	LC14	0.00000	LC1
2	Max	1.195	LC18	0.000	LC1	0.023	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-1.046	LC12	0.000	LC1	-0.027	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
3	Max	0.014	LC17	0.000	LC1	0.061	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.321	LC9	0.000	LC1	-0.058	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
4	Max	0.046	LC6	0.000	LC1	0.069	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.296	LC23	0.000	LC1	-0.071	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
5	Max	2.110	LC16	0.000	LC1	0.066	LC21	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-1.997	LC10	0.000	LC1	-0.068	LC3	0.00000	LC1	0.00000	LC1	0.00000	LC1
6	Max	0.458	LC7	0.767	LC31	0.623	LC1	0.00000	LC1	0.00315	LC7	0.00000	LC1
	Min	-0.246	LC13	-0.195	LC13	-0.615	LC19	0.00000	LC1	-0.00292	LC13	0.00000	LC1
17	Max	0.407	LC1	0.896	LC31	0.746	LC1	0.00000	LC1	0.00037	LC1	0.00000	LC1
	Min	-0.312	LC19	0.053	LC24	-0.734	LC19	0.00000	LC1	-0.00035	LC19	0.00000	LC1
45	Max	0.205	LC18	0.570	LC32	-0.054	LC15	0.00000	LC1	0.00253	LC12	0.00000	LC1
	Min	-0.221	LC12	0.205	LC15	-0.267	LC31	0.00000	LC1	-0.00241	LC18	0.00000	LC1
50	Max	0.001	LC24	0.269	LC35	0.158	LC35	0.00000	LC1	0.00273	LC16	0.00000	LC1
	Min	-0.004	LC6	0.102	LC17	0.027	LC17	0.00000	LC1	-0.00270	LC11	0.00000	LC1
51	Max	0.160	LC4	0.000	LC1	0.592	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.149	LC22	0.000	LC1	-0.311	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
52	Max	0.060	LC16	0.000	LC1	-0.064	LC17	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.066	LC10	0.000	LC1	-0.193	LC35	0.00000	LC1	0.00000	LC1	0.00000	LC1
53	Max	0.072	LC4	0.000	LC1	0.106	LC4	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.069	LC22	0.000	LC1	-0.126	LC18	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.134	LC4	0.000	LC1	0.442	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.126	LC22	0.000	LC1	-0.341	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
55	Max	0.924	LC14	1.144	LC31	0.771	LC13	0.00000	LC1	0.00151	LC14	0.00000	LC1
	Min	-0.936	LC8	-0.103	LC13	-0.771	LC7	0.00000	LC1	-0.00183	LC8	0.00000	LC1
115	Max	0.084	LC5	0.145	LC1	0.308	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.077	LC23	-0.105	LC19	-0.320	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
116	Max	0.088	LC3	0.547	LC1	1.203	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.085	LC21	-0.495	LC19	-1.188	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
131	Max	0.080	LC5	0.082	LC12	0.171	LC24	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.077	LC23	-0.053	LC18	-0.207	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
132	Max	0.081	LC3	0.079	LC25	0.149	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.075	LC21	-0.015	LC19	-0.117	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
133	Max	0.084	LC3	0.411	LC1	0.886	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.077	LC21	-0.358	LC19	-0.865	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.082	LC4	0.146	LC12	0.311	LC24	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.079	LC22	-0.115	LC18	-0.342	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

CHECK CONNECTION CAPACITY (Worst Case) → ALPHA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A36 3/8" Bolt (Assumed)

Allowable Tensile Load =

F_{Tall} = 2402 lbs.

Allowable Shear Load =

F_{Vall} = 1441 lbs.

TENSILE FORCES

Reaction **F =** 547 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 88 lbs. (See Bentley Output)
Reactions in Z direction: 1203 lbs. (See Bentley Output)

Resultant: 1206 lbs.

No. of Supports = 1
No. of Bolts / Support = 4

Tension Design Load /Bolts =

f_t = 136.75 lbs. < 2402 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

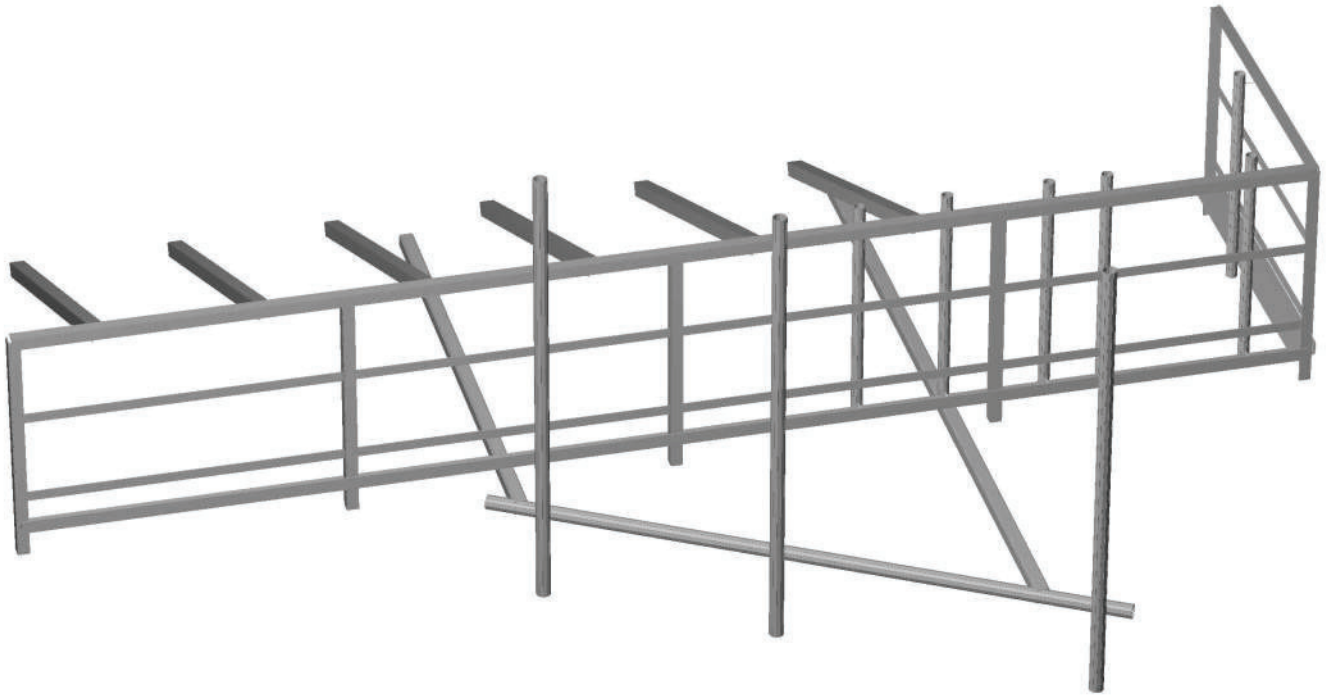
f_v = 301.55 lbs. < 1441 lbs. **Therefore, OK !**

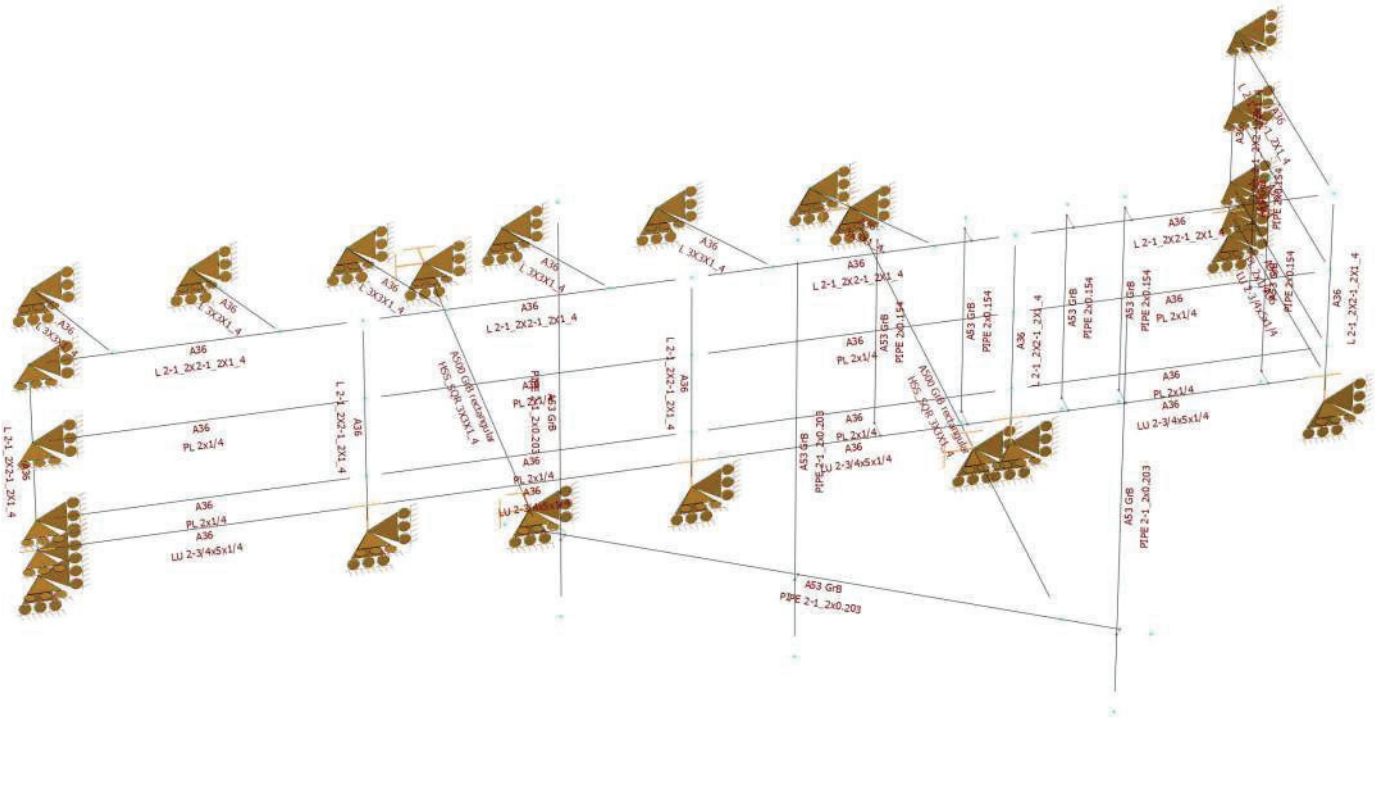
CHECK COMBINED TENSION AND SHEAR

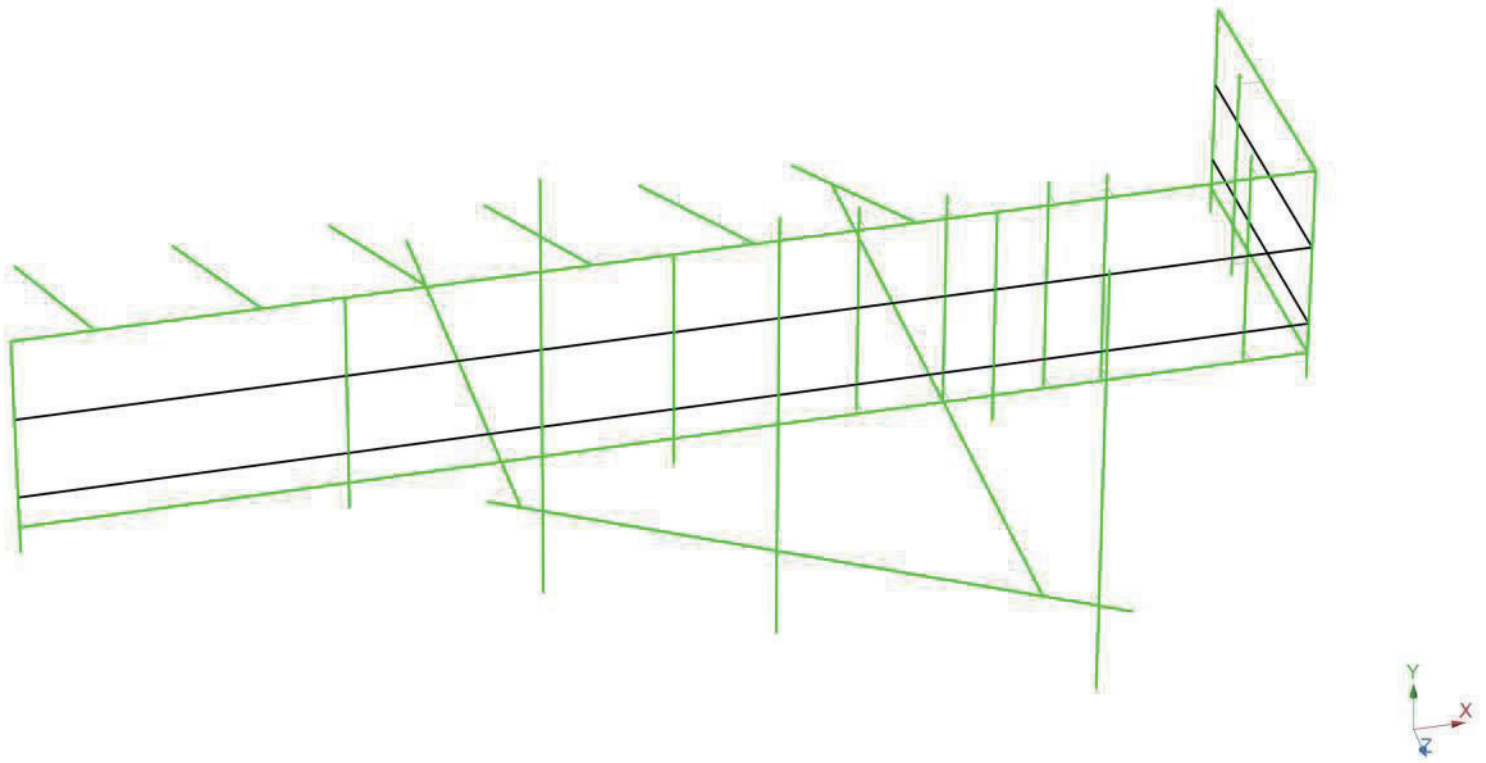
f_t / F_T	+	f_v / F_V	≤	1.0			
0.057	+	0.209	=	0.266	<	1.0	**Therefore, OK !**

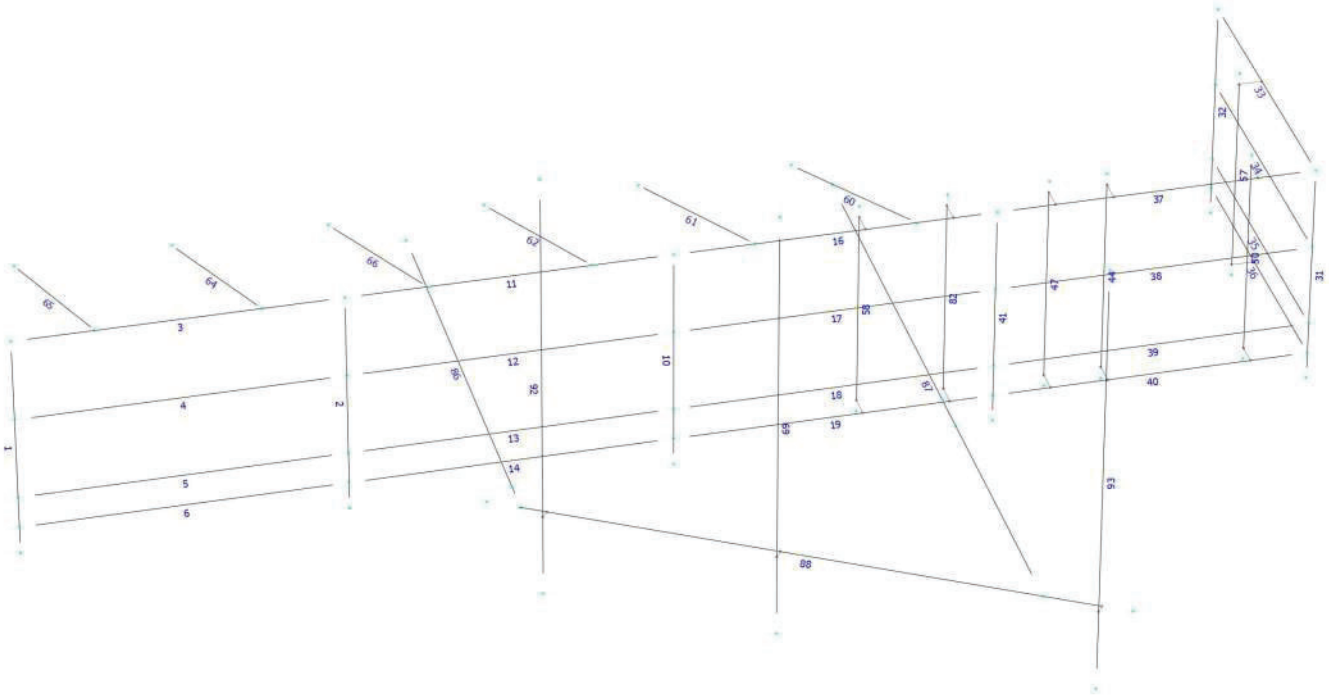
HUDSON
Design Group LLC

Beta Sector
Calculations


Y
X
Z


A36
L 3X3X1_4
A36
L 2-1_2X2-1_2X1_4
A36
PL 2x1/4
A36
LU 2-3/4x5x1/4
A53 GrB
PIPE 2-1_2x0.203
A53 GrB
PIPE 2x0.154
A500 GrB rectangular
HSS_SQR-3X3X1_4
Y
X
Z


Design status
Not designed
Error on design
Design O.K.
With warnings
Y
X
Z


Y
X
Z

Current Date: 3/24/2022 2:10 PM
Units system: English

Load data

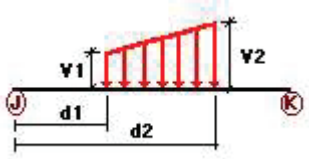
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	1	z	-0.011	-0.011	0.00	No	100.00	Yes
	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	3	z	-0.011	-0.011	0.00	No	100.00	Yes
	4	z	-0.009	-0.009	0.00	No	100.00	Yes
	5	z	-0.009	-0.009	0.00	No	100.00	Yes
	6	z	-0.012	-0.012	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes

	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes
	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	50	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes
	62	z	-0.014	-0.014	0.00	No	100.00	Yes
	64	z	-0.014	-0.014	0.00	No	100.00	Yes
	65	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
	69	z	-0.007	-0.007	0.00	No	100.00	Yes
	82	z	-0.006	-0.006	0.00	No	100.00	Yes
	88	z	-0.007	-0.007	0.00	No	100.00	Yes
	92	z	-0.007	-0.007	0.00	No	100.00	Yes
	93	z	-0.007	-0.007	0.00	No	100.00	Yes
W30	1	z	-0.011	-0.011	0.00	No	100.00	Yes
	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	3	z	-0.011	-0.011	0.00	No	100.00	Yes
	4	z	-0.009	-0.009	0.00	No	100.00	Yes
	5	z	-0.009	-0.009	0.00	No	100.00	Yes
	6	z	-0.012	-0.012	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes
	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes
	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	32	z	-0.011	-0.011	0.00	No	100.00	Yes
	33	z	-0.011	-0.011	0.00	No	100.00	Yes
	34	z	-0.009	-0.009	0.00	No	100.00	Yes
	35	z	-0.009	-0.009	0.00	No	100.00	Yes
	36	z	-0.012	-0.012	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	50	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes

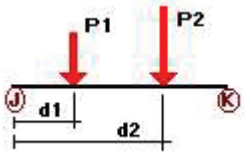
	62	z	-0.014	-0.014	0.00	No	100.00	Yes
	64	z	-0.014	-0.014	0.00	No	100.00	Yes
	65	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
	69	z	-0.007	-0.007	0.00	No	100.00	Yes
	82	z	-0.006	-0.006	0.00	No	100.00	Yes
	86	z	-0.014	-0.014	0.00	No	100.00	Yes
	87	z	-0.014	-0.014	0.00	No	100.00	Yes
	88	z	-0.007	-0.007	0.00	No	100.00	Yes
	92	z	-0.007	-0.007	0.00	No	100.00	Yes
	93	z	-0.007	-0.007	0.00	No	100.00	Yes
W60	1	x	-0.011	-0.011	0.00	No	100.00	Yes
	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	3	x	-0.011	-0.011	0.00	No	100.00	Yes
	4	x	-0.009	-0.009	0.00	No	100.00	Yes
	5	x	-0.009	-0.009	0.00	No	100.00	Yes
	6	x	-0.012	-0.012	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	69	x	-0.007	-0.007	0.00	No	100.00	Yes
	82	x	-0.006	-0.006	0.00	No	100.00	Yes
	86	x	-0.014	-0.014	0.00	No	100.00	Yes
	87	x	-0.014	-0.014	0.00	No	100.00	Yes
	88	x	-0.007	-0.007	0.00	No	100.00	Yes
	92	x	-0.007	-0.007	0.00	No	100.00	Yes
	93	x	-0.007	-0.007	0.00	No	100.00	Yes
W90	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes

	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	69	x	-0.007	-0.007	0.00	No	100.00	Yes
	82	x	-0.006	-0.006	0.00	No	100.00	Yes
	86	x	-0.014	-0.014	0.00	No	100.00	Yes
	87	x	-0.014	-0.014	0.00	No	100.00	Yes
	88	x	-0.007	-0.007	0.00	No	100.00	Yes
	92	x	-0.007	-0.007	0.00	No	100.00	Yes
	93	x	-0.007	-0.007	0.00	No	100.00	Yes
W120	1	x	-0.011	-0.011	0.00	No	100.00	Yes
	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	3	x	-0.011	-0.011	0.00	No	100.00	Yes
	4	x	-0.009	-0.009	0.00	No	100.00	Yes
	5	x	-0.009	-0.009	0.00	No	100.00	Yes
	6	x	-0.012	-0.012	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	50	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	64	x	-0.014	-0.014	0.00	No	100.00	Yes
	65	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	69	x	-0.007	-0.007	0.00	No	100.00	Yes
	82	x	-0.006	-0.006	0.00	No	100.00	Yes
	86	x	-0.014	-0.014	0.00	No	100.00	Yes
	87	x	-0.014	-0.014	0.00	No	100.00	Yes

	88	x	-0.007	-0.007	0.00	No	100.00	Yes
	92	x	-0.007	-0.007	0.00	No	100.00	Yes
	93	x	-0.007	-0.007	0.00	No	100.00	Yes
W150	1	z	0.011	0.011	0.00	No	100.00	Yes
	2	z	0.011	0.011	0.00	No	100.00	Yes
	3	z	0.011	0.011	0.00	No	100.00	Yes
	4	z	0.009	0.009	0.00	No	100.00	Yes
	5	z	0.009	0.009	0.00	No	100.00	Yes
	6	z	0.012	0.012	0.00	No	100.00	Yes
	10	z	0.011	0.011	0.00	No	100.00	Yes
	11	z	0.011	0.011	0.00	No	100.00	Yes
	12	z	0.009	0.009	0.00	No	100.00	Yes
	13	z	0.009	0.009	0.00	No	100.00	Yes
	14	z	0.012	0.012	0.00	No	100.00	Yes
	16	z	0.011	0.011	0.00	No	100.00	Yes
	17	z	0.009	0.009	0.00	No	100.00	Yes
	18	z	0.009	0.009	0.00	No	100.00	Yes
	19	z	0.012	0.012	0.00	No	100.00	Yes
	31	z	0.011	0.011	0.00	No	100.00	Yes
	32	z	0.011	0.011	0.00	No	100.00	Yes
	33	z	0.011	0.011	0.00	No	100.00	Yes
	34	z	0.009	0.009	0.00	No	100.00	Yes
	35	z	0.009	0.009	0.00	No	100.00	Yes
	36	z	0.012	0.012	0.00	No	100.00	Yes
	37	z	0.011	0.011	0.00	No	100.00	Yes
	38	z	0.009	0.009	0.00	No	100.00	Yes
	39	z	0.009	0.009	0.00	No	100.00	Yes
	40	z	0.012	0.012	0.00	No	100.00	Yes
	41	z	0.011	0.011	0.00	No	100.00	Yes
	44	z	0.006	0.006	0.00	No	100.00	Yes
	47	z	0.006	0.006	0.00	No	100.00	Yes
	50	z	0.006	0.006	0.00	No	100.00	Yes
	57	z	0.006	0.006	0.00	No	100.00	Yes
	58	z	0.006	0.006	0.00	No	100.00	Yes
	60	z	0.014	0.014	0.00	No	100.00	Yes
	61	z	0.014	0.014	0.00	No	100.00	Yes
	62	z	0.014	0.014	0.00	No	100.00	Yes
	64	z	0.014	0.014	0.00	No	100.00	Yes
	65	z	0.014	0.014	0.00	No	100.00	Yes
	66	z	0.014	0.014	0.00	No	100.00	Yes
	69	z	0.007	0.007	0.00	No	100.00	Yes
	82	z	0.006	0.006	0.00	No	100.00	Yes
	86	z	0.014	0.014	0.00	No	100.00	Yes
	87	z	0.014	0.014	0.00	No	100.00	Yes
	88	z	0.007	0.007	0.00	No	100.00	Yes
	92	z	0.007	0.007	0.00	No	100.00	Yes
	93	z	0.007	0.007	0.00	No	100.00	Yes
Di	1	y	-0.007	-0.007	0.00	No	100.00	Yes
	2	y	-0.007	-0.007	0.00	No	100.00	Yes
	3	y	-0.007	-0.007	0.00	No	100.00	Yes
	4	y	-0.005	-0.005	0.00	No	100.00	Yes
	5	y	-0.005	-0.005	0.00	No	100.00	Yes
	6	y	-0.01	-0.01	0.00	No	100.00	Yes
	10	y	-0.007	-0.007	0.00	No	100.00	Yes
	11	y	-0.007	-0.007	0.00	No	100.00	Yes
	12	y	-0.005	-0.005	0.00	No	100.00	Yes
	13	y	-0.005	-0.005	0.00	No	100.00	Yes
	14	y	-0.01	-0.01	0.00	No	100.00	Yes
	16	y	-0.007	-0.007	0.00	No	100.00	Yes
	17	y	-0.005	-0.005	0.00	No	100.00	Yes

18	y	-0.005	-0.005	0.00	No	100.00	Yes
19	y	-0.01	-0.01	0.00	No	100.00	Yes
31	y	-0.007	-0.007	0.00	No	100.00	Yes
32	y	-0.007	-0.007	0.00	No	100.00	Yes
33	y	-0.007	-0.007	0.00	No	100.00	Yes
34	y	-0.005	-0.005	0.00	No	100.00	Yes
35	y	-0.005	-0.005	0.00	No	100.00	Yes
36	y	-0.01	-0.01	0.00	No	100.00	Yes
37	y	-0.007	-0.007	0.00	No	100.00	Yes
38	y	-0.005	-0.005	0.00	No	100.00	Yes
39	y	-0.005	-0.005	0.00	No	100.00	Yes
40	y	-0.01	-0.01	0.00	No	100.00	Yes
41	y	-0.007	-0.007	0.00	No	100.00	Yes
44	y	-0.005	-0.005	0.00	No	100.00	Yes
47	y	-0.005	-0.005	0.00	No	100.00	Yes
50	y	-0.005	-0.005	0.00	No	100.00	Yes
57	y	-0.005	-0.005	0.00	No	100.00	Yes
58	y	-0.005	-0.005	0.00	No	100.00	Yes
60	y	-0.008	-0.008	0.00	No	100.00	Yes
61	y	-0.008	-0.008	0.00	No	100.00	Yes
62	y	-0.008	-0.008	0.00	No	100.00	Yes
64	y	-0.008	-0.008	0.00	No	100.00	Yes
65	y	-0.008	-0.008	0.00	No	100.00	Yes
66	y	-0.008	-0.008	0.00	No	100.00	Yes
69	y	-0.006	-0.006	0.00	No	100.00	Yes
82	y	-0.005	-0.005	0.00	No	100.00	Yes
86	y	-0.008	-0.008	0.00	Yes	10.00	Yes
87	y	-0.008	-0.008	60.00	Yes	100.00	Yes
88	y	-0.006	-0.006	0.00	No	100.00	Yes
92	y	-0.006	-0.006	0.00	No	100.00	Yes
93	y	-0.006	-0.006	0.00	No	100.00	Yes

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	44	y	-0.06	2.00	No
	47	y	-0.06	2.00	No
	50	y	-0.033	2.00	No
	57	y	-0.06	2.00	No
	58	y	-0.073	2.00	No
	69	y	-0.041	1.00	No
		y	-0.041	3.00	No
		y	-0.033	4.00	No
		y	-0.033	6.00	No
	82	y	-0.06	2.00	No
	92	y	-0.04	1.25	No
		y	-0.04	6.25	No
	93	y	-0.035	1.25	No
		y	-0.035	6.25	No

Wo	44	z	-0.088	2.00	No
	47	z	-0.119	2.00	No
	50	z	-0.049	2.00	No
	57	z	-0.072	2.00	No
	58	z	-0.086	2.00	No
	69	z	-0.088	1.00	No
		z	-0.088	3.00	No
		z	-0.091	4.00	No
		z	-0.091	6.00	No
	82	z	-0.119	2.00	No
	92	z	-0.276	1.25	No
		z	-0.276	6.25	No
	93	z	-0.276	1.25	No
		z	-0.276	6.25	No
W30	44	3	-0.079	2.00	No
	47	3	-0.108	2.00	No
	50	3	-0.049	2.00	No
	57	3	-0.078	2.00	No
	58	3	-0.079	2.00	No
	69	3	-0.081	1.00	No
		3	-0.081	3.00	No
		3	-0.079	4.00	No
		3	-0.079	6.00	No
	82	3	-0.108	2.00	No
	92	3	-0.238	1.25	No
		3	-0.238	6.25	No
	93	3	-0.238	1.25	No
		3	-0.238	6.25	No
W60	44	3	-0.063	2.00	No
	47	3	-0.084	2.00	No
	50	3	-0.049	2.00	No
	57	3	-0.112	2.00	No
	58	3	-0.067	2.00	No
	69	3	-0.067	1.00	No
		3	-0.067	3.00	No
		3	-0.056	4.00	No
		3	-0.056	6.00	No
	82	3	-0.084	2.00	No
	92	3	-0.161	1.25	No
		3	-0.161	6.25	No
	93	3	-0.161	1.25	No
		3	-0.161	6.25	No
W90	44	x	-0.054	2.00	No
	47	x	-0.072	2.00	No
	50	x	-0.049	2.00	No
	57	x	-0.119	2.00	No
	58	x	-0.061	2.00	No
	69	x	-0.06	1.00	No
		x	-0.06	3.00	No
		x	-0.044	4.00	No
		x	-0.044	6.00	No
	82	x	-0.072	2.00	No
	92	x	-0.122	1.25	No
		x	-0.122	6.25	No
	93	x	-0.122	1.25	No
		x	-0.122	6.25	No
W120	44	2	-0.063	2.00	No
	47	2	-0.084	2.00	No
	50	2	-0.049	2.00	No
	57	2	-0.112	2.00	No

	58	2	-0.067	2.00	No
	69	2	-0.067	1.00	No
		2	-0.067	3.00	No
		2	-0.056	4.00	No
		2	-0.056	6.00	No
	82	2	-0.084	2.00	No
	92	2	-0.161	1.25	No
		2	-0.161	6.25	No
	93	2	-0.161	1.25	No
		2	-0.161	6.25	No
W150	44	2	-0.079	2.00	No
	47	2	-0.108	2.00	No
	50	2	-0.049	2.00	No
	57	2	-0.078	2.00	No
	58	2	-0.079	2.00	No
	69	2	-0.081	1.00	No
		2	-0.081	3.00	No
		2	-0.079	4.00	No
		2	-0.079	6.00	No
	82	2	-0.108	2.00	No
	92	2	-0.238	1.25	No
		2	-0.238	6.25	No
	93	2	-0.238	1.25	No
		2	-0.238	6.25	No
Di	44	y	-0.039	2.00	No
	47	y	-0.052	2.00	No
	50	y	-0.033	2.00	No
	57	y	-0.052	2.00	No
	58	y	-0.039	2.00	No
	69	y	-0.039	1.00	No
		y	-0.039	3.00	No
		y	-0.037	4.00	No
		y	-0.037	6.00	No
	82	y	-0.052	2.00	No
	92	y	-0.104	1.25	No
		y	-0.104	6.25	No
	93	y	-0.104	1.25	No
		y	-0.104	6.25	No
WI0	44	z	-0.019	2.00	No
	47	z	-0.025	2.00	No
	50	z	-0.011	2.00	No
	57	z	-0.017	2.00	No
	58	z	-0.018	2.00	No
	69	z	-0.018	1.00	No
		z	-0.018	3.00	No
		z	-0.018	4.00	No
		z	-0.018	6.00	No
	82	z	-0.025	2.00	No
	92	z	-0.051	1.25	No
		z	-0.051	6.25	No
	93	z	-0.051	1.25	No
		z	-0.051	6.25	No
WI30	44	3	-0.017	2.00	No
	47	3	-0.023	2.00	No
	50	3	-0.011	2.00	No
	57	3	-0.016	2.00	No
	58	3	-0.017	2.00	No
	69	3	-0.017	1.00	No
		3	-0.017	3.00	No
		3	-0.016	4.00	No

		3	-0.016	6.00	No
	82	3	-0.023	2.00	No
	92	3	-0.045	1.25	No
		3	-0.045	6.25	No
	93	3	-0.045	1.25	No
		3	-0.045	6.25	No
WI60	44	3	-0.014	2.00	No
	47	3	-0.019	2.00	No
	50	3	-0.011	2.00	No
	57	3	-0.023	2.00	No
	58	3	-0.015	2.00	No
	69	3	-0.014	1.00	No
		3	-0.014	3.00	No
		3	-0.012	4.00	No
		3	-0.012	6.00	No
	82	3	-0.019	2.00	No
	92	3	-0.032	1.25	No
		3	-0.032	6.25	No
	93	3	-0.032	1.25	No
		3	-0.032	6.25	No
WI90	44	x	-0.013	2.00	No
	47	x	-0.017	2.00	No
	50	x	-0.011	2.00	No
	57	x	-0.025	2.00	No
	58	x	-0.014	2.00	No
	69	x	-0.013	1.00	No
		x	-0.013	3.00	No
		x	-0.01	4.00	No
		x	-0.01	6.00	No
	82	x	-0.017	2.00	No
	92	x	-0.026	1.25	No
		x	-0.026	6.25	No
	93	x	-0.026	1.25	No
		x	-0.026	6.25	No
WI120	44	2	-0.014	2.00	No
	47	2	-0.019	2.00	No
	50	2	-0.011	2.00	No
	57	2	-0.023	2.00	No
	58	2	-0.015	2.00	No
	69	2	-0.014	1.00	No
		2	-0.014	3.00	No
		2	-0.012	4.00	No
		2	-0.012	6.00	No
	82	2	-0.019	2.00	No
	92	2	-0.032	1.25	No
		2	-0.032	6.25	No
	93	2	-0.032	1.25	No
		2	-0.032	6.25	No
WI150	44	2	-0.017	2.00	No
	47	2	-0.023	2.00	No
	50	2	-0.011	2.00	No
	57	2	-0.016	2.00	No
	58	2	-0.017	2.00	No
	69	2	-0.017	1.00	No
		2	-0.017	3.00	No
		2	-0.016	4.00	No
		2	-0.016	6.00	No
	82	2	-0.023	2.00	No
	92	2	-0.045	1.25	No
		2	-0.045	6.25	No

	93	2	-0.045	1.25	No
		2	-0.045	6.25	No
WL0	44	z	-0.005	2.00	No
	47	z	-0.007	2.00	No
	50	z	-0.003	2.00	No
	57	z	-0.004	2.00	No
	58	z	-0.005	2.00	No
	69	z	-0.005	1.00	No
		z	-0.005	3.00	No
		z	-0.005	4.00	No
		z	-0.005	6.00	No
	82	z	-0.007	2.00	No
	92	z	-0.016	1.25	No
		z	-0.016	6.25	No
	93	z	-0.016	1.25	No
		z	-0.016	6.25	No
WL30	44	3	-0.005	2.00	No
	47	3	-0.006	2.00	No
	50	3	-0.003	2.00	No
	57	3	-0.004	2.00	No
	58	3	-0.005	2.00	No
	69	3	-0.005	1.00	No
		3	-0.005	3.00	No
		3	-0.005	4.00	No
		3	-0.005	6.00	No
	82	3	-0.006	2.00	No
	92	3	-0.014	1.25	No
		3	-0.014	6.25	No
	93	3	-0.014	1.25	No
		3	-0.014	6.25	No
WL60	44	3	-0.004	2.00	No
	47	3	-0.005	2.00	No
	50	3	-0.003	2.00	No
	57	3	-0.006	2.00	No
	58	3	-0.004	2.00	No
	69	3	-0.004	1.00	No
		3	-0.004	3.00	No
		3	-0.003	4.00	No
		3	-0.003	6.00	No
	82	3	-0.005	2.00	No
	92	3	-0.009	1.25	No
		3	-0.009	6.25	No
	93	3	-0.009	1.25	No
		3	-0.009	6.25	No
WL90	44	x	-0.003	2.00	No
	47	x	-0.004	2.00	No
	50	x	-0.003	2.00	No
	57	x	-0.007	2.00	No
	58	x	-0.004	2.00	No
	69	3	-0.004	1.00	No
		3	-0.004	3.00	No
		3	-0.003	4.00	No
		3	-0.003	6.00	No
	82	x	-0.004	2.00	No
	92	x	-0.007	1.25	No
		x	-0.007	6.25	No
	93	x	-0.007	1.25	No
		x	-0.007	6.25	No
WL120	44	2	-0.004	2.00	No
	47	2	-0.005	2.00	No

	50	2	-0.003	2.00	No
	57	2	-0.006	2.00	No
	58	2	-0.004	2.00	No
	69	2	-0.004	1.00	No
		2	-0.004	3.00	No
		2	-0.003	4.00	No
		2	-0.003	6.00	No
	82	2	-0.005	2.00	No
	92	2	-0.009	1.25	No
		2	-0.009	6.25	No
	93	2	-0.009	1.25	No
		2	-0.009	6.25	No
WL150	44	2	-0.005	2.00	No
	47	2	-0.006	2.00	No
	50	2	-0.003	2.00	No
	57	2	-0.004	2.00	No
	58	2	-0.005	2.00	No
	69	2	-0.005	1.00	No
		2	-0.005	3.00	No
		2	-0.005	4.00	No
		2	-0.005	6.00	No
	82	2	-0.006	2.00	No
	92	2	-0.014	1.25	No
		2	-0.014	6.25	No
	93	2	-0.014	1.25	No
		2	-0.014	6.25	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00

Current Date: 3/24/2022 2:10 PM
Units system: English

Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150
LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS_SQR 3X3X1_4	**86**	LC7 at 6.25%	**0.58**	**OK**	
		87	LC7 at 62.50%	0.56	OK	
	L 2-1_2X2-1_2X1_4	**1**	LC26 at 0.00%	0.05	OK	
		2	LC8 at 45.31%	0.13	OK	
		3	LC5 at 22.92%	0.14	OK	
		10	LC7 at 28.13%	0.15	OK	
		11	LC15 at 22.92%	0.13	OK	
		16	LC1 at 23.75%	**0.28**	**OK**	
		31	LC36 at 10.94%	0.08	OK	
		32	LC4 at 100.00%	0.08	OK	
		33	LC4 at 43.75%	0.17	OK	
		37	LC1 at 82.81%	0.22	OK	
		41	LC7 at 26.56%	0.20	OK	
	L 3X3X1_4	**60**	LC11 at 0.00%	0.11	OK	
		61	LC10 at 0.00%	**0.13**	**OK**	
		62	LC9 at 0.00%	0.11	OK	
		64	LC9 at 0.00%	0.12	OK	
		65	LC11 at 0.00%	0.12	OK	
		66	LC9 at 0.00%	0.12	OK	
	LU 2-3/4x5x1/4	**6**	LC6 at 50.00%	0.05	OK	
		14	LC7 at 100.00%	0.06	OK	
		19	LC7 at 100.00%	**0.21**	**OK**	
		36	LC7 at 0.00%	0.11	OK	
		40	LC7 at 0.00%	0.17	OK	
	PIPE 2-1_2x0.203	**69**	LC7 at 78.13%	0.72	OK	
		88	LC7 at 93.75%	0.72	OK	
		92	LC7 at 78.13%	0.96	OK	
		93	LC7 at 78.13%	**0.97**	**OK**	
	PIPE 2x0.154	**44**	LC1 at 50.00%	0.12	OK	
		47	LC1 at 50.00%	0.12	OK	
		50	LC19 at 50.00%	0.06	OK	
		57	LC4 at 50.00%	**0.15**	**OK**	
		58	LC1 at 50.00%	0.08	OK	
		82	LC1 at 6.25%	0.09	OK	
	PL 2x1/4	**4**	LC6 at 100.00%	**0.47**	**With warnings**	
		5	LC2 at 100.00%	0.46	With warnings	
		12	LC2 at 0.00%	0.45	With warnings	
		13	LC6 at 0.00%	0.45	With warnings	
		17	LC7 at 100.00%	0.46	With warnings	
		18	LC12 at 100.00%	0.44	With warnings	
		34	LC10 at 0.00%	0.41	With warnings	
		35	LC9 at 0.00%	0.42	With warnings	
		38	LC2 at 0.00%	0.47	With warnings	
		39	LC6 at 0.00%	0.46	With warnings	

Current Date: 3/24/2022 2:11 PM
Units system: English

Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
1	0.00	0.00	0.00	0
2	0.00	0.50	0.00	0
3	0.00	1.08	0.00	0
4	0.00	2.58	0.00	0
5	0.00	4.08	0.00	0
6	5.50	0.00	0.00	0
7	5.50	0.50	0.00	0
8	5.50	1.08	0.00	0
9	5.50	2.58	0.00	0
10	5.50	4.08	0.00	0
17	11.00	0.00	0.00	0
18	11.00	0.50	0.00	0
19	11.00	1.08	0.00	0
20	11.00	2.58	0.00	0
21	11.00	4.08	0.00	0
23	16.50	0.50	0.00	0
24	16.50	1.08	0.00	0
25	16.50	2.58	0.00	0
26	16.50	4.08	0.00	0
45	22.00	0.00	0.00	0
46	22.00	0.50	0.00	0
47	22.00	1.08	0.00	0
48	22.00	2.58	0.00	0

49	22.00	4.08	0.00	0
50	22.00	0.00	-5.50	0
51	22.00	0.50	-5.50	0
52	22.00	1.08	-5.50	0
53	22.00	2.58	-5.50	0
54	22.00	4.08	-5.50	0
55	16.50	0.00	0.00	0
61	18.50	0.29	-0.40	0
62	18.50	4.29	-0.40	0
68	17.50	4.29	-0.40	0
73	21.00	0.29	-0.40	0
74	21.00	4.29	-0.40	0
102	21.60	0.29	-3.00	0
105	21.60	4.29	-3.00	0
107	14.25	4.29	-0.40	0
109	15.125	4.08	0.00	0
113	12.375	4.08	0.00	0
115	12.375	0.50	-8.00	0
116	15.125	0.50	-8.00	0
118	9.625	4.08	0.00	0
125	4.125	4.08	0.00	0
129	1.375	4.08	0.00	0
131	4.125	0.50	-8.00	0
132	1.375	0.50	-8.00	0
133	6.875	0.50	-8.00	0
134	9.625	0.50	-8.00	0
138	6.875	4.08	0.00	0
143	11.9591	6.50	3.1181	0
144	11.9591	-1.50	3.1181	0
169	15.75	0.29	-0.40	0
170	15.75	4.29	-0.40	0
177	15.8606	0.00	-8.00	0
178	8.2401	0.00	-8.00	0
179	8.2401	0.00	0.664	0
180	15.8606	0.00	5.2618	0
282	17.151	0.00	6.0403	0
302	7.736	0.00	0.3599	0
327	8.2401	0.00	0.00	0
328	15.8606	0.00	0.00	0
329	8.522	6.50	1.0444	0
330	8.522	-1.50	1.0444	0
331	16.6054	6.50	5.9215	0
332	16.6054	-1.50	5.9215	0
104	14.25	0.29	-0.40	0
67	17.50	0.29	-0.40	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
1	1	1	1	0	1	0
2	1	0	1	0	0	0
3	1	0	1	0	0	0
4	1	0	1	0	0	0
5	1	0	1	0	0	0
6	1	1	1	0	1	0

17	1	1	1	0	1	0
45	1	1	1	0	1	0
50	1	1	1	0	1	0
51	1	0	1	0	0	0
52	1	0	1	0	0	0
53	1	0	1	0	0	0
54	1	0	1	0	0	0
55	1	1	1	0	1	0
115	1	1	1	0	0	0
116	1	1	1	0	0	0
131	1	1	1	0	0	0
132	1	1	1	0	0	0
133	1	1	1	0	0	0
134	1	1	1	0	0	0
177	1	1	1	1	0	1
178	1	1	1	1	0	1
327	1	1	1	1	0	1
328	1	1	1	1	0	1

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	lg factor
1	5	1		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
2	6	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
3	10	5		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
4	4	9		PL 2x1/4	A36	0.00	0.00	0.00
5	3	8		PL 2x1/4	A36	0.00	0.00	0.00
6	2	7		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
10	17	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
11	21	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
12	9	20		PL 2x1/4	A36	0.00	0.00	0.00
13	8	19		PL 2x1/4	A36	0.00	0.00	0.00
14	7	18		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
16	26	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
17	20	25		PL 2x1/4	A36	0.00	0.00	0.00
18	19	24		PL 2x1/4	A36	0.00	0.00	0.00
19	18	23		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
31	45	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
32	50	54		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
33	54	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
34	48	53		PL 2x1/4	A36	0.00	0.00	0.00
35	47	52		PL 2x1/4	A36	0.00	0.00	0.00
36	46	51		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
37	49	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
38	25	48		PL 2x1/4	A36	0.00	0.00	0.00
39	24	47		PL 2x1/4	A36	0.00	0.00	0.00
40	23	46		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
41	55	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
44	62	61		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
47	68	67		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
50	74	73		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	105	102		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
58	107	104		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	109	116		L 3X3X1_4	A36	0.00	0.00	0.00
61	113	115		L 3X3X1_4	A36	0.00	0.00	0.00

62	118	134	L 3X3X1_4	A36	0.00	0.00	0.00
64	125	131	L 3X3X1_4	A36	0.00	0.00	0.00
65	129	132	L 3X3X1_4	A36	0.00	0.00	0.00
66	138	133	L 3X3X1_4	A36	0.00	0.00	0.00
69	143	144	PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
82	170	169	PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
86	179	178	HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
87	177	180	HSS_SQR 3X3X1_4	A500 GrB rectangular	0.00	0.00	0.00
88	282	302	PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
92	329	330	PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
93	331	332	PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00

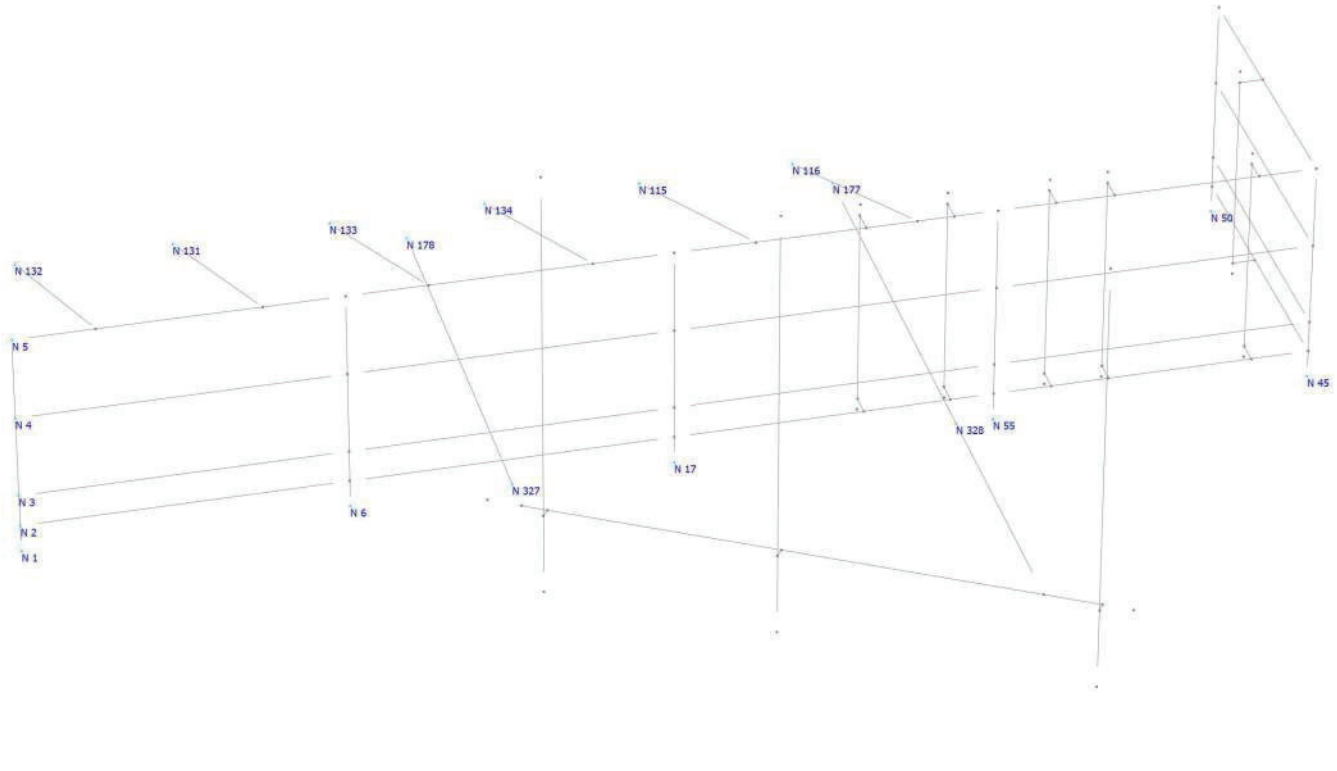
Orientation of local axes

Member	Rotation [Deg]	Axes23	NX	NY	NZ
1	270.00	0	0.00	0.00	0.00
2	180.00	0	0.00	0.00	0.00
3	90.00	0	0.00	0.00	0.00
6	270.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	90.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
16	90.00	0	0.00	0.00	0.00
19	270.00	0	0.00	0.00	0.00
31	270.00	0	0.00	0.00	0.00
32	270.00	0	0.00	0.00	0.00
33	90.00	0	0.00	0.00	0.00
36	270.00	0	0.00	0.00	0.00
37	90.00	0	0.00	0.00	0.00
40	270.00	0	0.00	0.00	0.00
41	180.00	0	0.00	0.00	0.00
44	315.00	0	0.00	0.00	0.00
47	315.00	0	0.00	0.00	0.00
50	315.00	0	0.00	0.00	0.00
57	315.00	0	0.00	0.00	0.00
58	315.00	0	0.00	0.00	0.00
60	90.00	0	0.00	0.00	0.00
61	90.00	0	0.00	0.00	0.00
62	90.00	0	0.00	0.00	0.00
64	90.00	0	0.00	0.00	0.00
65	90.00	0	0.00	0.00	0.00
66	90.00	0	0.00	0.00	0.00
69	315.00	0	0.00	0.00	0.00
82	315.00	0	0.00	0.00	0.00
92	315.00	0	0.00	0.00	0.00
93	315.00	0	0.00	0.00	0.00

Hinges

	Node-J				Node-K						
Member	**M33**	**M22**	**V3**	**V2**	**M33**	**M22**	**V3**	**V2**	**TOR**	**AXL**	**Axial rigidity**
4	0	0	0	0	0	0	0	0	0	0	Tension only
5	0	0	0	0	0	0	0	0	0	0	Tension only
12	0	0	0	0	0	0	0	0	0	0	Tension only
13	0	0	0	0	0	0	0	0	0	0	Tension only
17	0	0	0	0	0	0	0	0	0	0	Tension only
18	0	0	0	0	0	0	0	0	0	0	Tension only
34	0	0	0	0	0	0	0	0	0	0	Tension only
35	0	0	0	0	0	0	0	0	0	0	Tension only
38	0	0	0	0	0	0	0	0	0	0	Tension only
39	0	0	0	0	0	0	0	0	0	0	Tension only

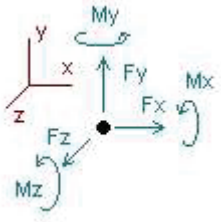
Current Date: 3/24/2022 2:13 PM
Units system: English



Current Date: 3/24/2022 2:11 PM
Units system: English

Analysis result

Reactions



Direction of positive forces and moments

	Forces [Kip]			Moments [Kip*ft]		
Node	**FX**	**FY**	**FZ**	**MX**	**MY**	**MZ**
Condition **LC1=1.2D+1.6Wo**						
1	-0.00700	0.04911	0.00329	0.00000	-0.00153	0.00000
2	-0.25253	0.00000	0.05033	0.00000	0.00000	0.00000
3	-0.12080	0.00000	0.06014	0.00000	0.00000	0.00000
4	-0.09917	0.00000	0.06841	0.00000	0.00000	0.00000
5	0.10021	0.00000	0.00744	0.00000	0.00000	0.00000
6	0.10301	0.01965	0.20444	0.00000	-0.00004	0.00000
17	0.08119	0.08548	0.27843	0.00000	-0.00059	0.00000
45	-0.09267	0.21530	-0.18201	0.00000	0.00200	0.00000
50	-0.00069	0.12889	0.07093	0.00000	-0.00101	0.00000
51	-0.04470	0.00000	0.54168	0.00000	0.00000	0.00000
52	-0.00476	0.00000	-0.08766	0.00000	0.00000	0.00000
53	-0.00009	0.00000	0.02625	0.00000	0.00000	0.00000
54	-0.03185	0.00000	0.31117	0.00000	0.00000	0.00000
55	0.35584	0.18275	0.43663	0.00000	0.00021	0.00000
115	-0.00128	0.06983	0.13958	0.00000	0.00000	0.00000
116	0.01082	0.33877	0.73825	0.00000	0.00000	0.00000
131	0.00248	0.09821	0.20246	0.00000	0.00000	0.00000
132	0.00061	0.06288	0.12309	0.00000	0.00000	0.00000
133	-0.00116	0.09244	0.18982	0.00000	0.00000	0.00000
134	0.00253	0.08990	0.18390	0.00000	0.00000	0.00000
177	0.00945	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.06745	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.02635	0.47579	1.30746	3.25721	0.00000	0.81910
328	-0.05054	0.25242	1.40599	2.17322	0.00000	0.32395
SUM	0.00000	2.24066	6.08004	5.32482	-0.00096	1.14305
Condition **LC2=1.2D+1.6W30**						
1	-0.00645	0.04948	0.00328	0.00000	-0.00153	0.00000
2	-0.11956	0.00000	0.04973	0.00000	0.00000	0.00000
3	-0.08446	0.00000	0.06018	0.00000	0.00000	0.00000
4	-0.07771	0.00000	0.06842	0.00000	0.00000	0.00000
5	0.34267	0.00000	0.00737	0.00000	0.00000	0.00000
6	0.12029	0.02228	0.20970	0.00000	-0.00008	0.00000
17	0.12776	0.09094	0.25467	0.00000	-0.00034	0.00000
45	-0.06435	0.20783	-0.17275	0.00000	0.00155	0.00000
50	-0.00180	0.12904	0.06393	0.00000	-0.00054	0.00000
51	-0.01660	0.00000	0.51259	0.00000	0.00000	0.00000
52	-0.00390	0.00000	-0.06342	0.00000	0.00000	0.00000

53	0.00022	0.00000	0.07450	0.00000	0.00000	0.00000
54	-0.00691	0.00000	0.27830	0.00000	0.00000	0.00000
55	0.34511	0.23765	0.35408	0.00000	0.00015	0.00000
115	-0.00120	0.06864	0.13679	0.00000	0.00000	0.00000
116	0.00910	0.28299	0.61371	0.00000	0.00000	0.00000
131	0.00251	0.09873	0.20361	0.00000	0.00000	0.00000
132	0.00062	0.06284	0.12299	0.00000	0.00000	0.00000
133	-0.00112	0.09185	0.18849	0.00000	0.00000	0.00000
134	0.00261	0.09097	0.18625	0.00000	0.00000	0.00000
177	-0.00551	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.05189	0.03960	0.00000	-0.05281	0.00000	0.00000
327	1.47793	0.78276	1.40250	0.96622	0.00000	-0.21227
328	0.01857	-0.05454	0.41085	1.87433	0.00000	-0.42157
SUM	2.00592	2.24066	4.96577	2.73493	-0.00079	-0.63384

Condition **LC3=1.2D+1.6W60**

1	0.02394	0.05386	0.00030	0.00000	0.00005	0.00000
2	0.41407	0.00000	-0.00057	0.00000	0.00000	0.00000
3	-0.00421	0.00000	0.00101	0.00000	0.00000	0.00000
4	0.03329	0.00000	-0.00062	0.00000	0.00000	0.00000
5	1.24055	0.00000	-0.06689	0.00000	0.00000	0.00000
6	0.01894	0.16939	-0.00421	0.00000	-0.00002	0.00000
17	0.06834	0.20651	0.01093	0.00000	-0.00028	0.00000
45	-0.03854	0.18701	-0.07242	0.00000	-0.00048	0.00000
50	0.00018	0.13170	0.04794	0.00000	0.00124	0.00000
51	0.07752	0.00000	0.21758	0.00000	0.00000	0.00000
52	0.05801	0.00000	-0.08144	0.00000	0.00000	0.00000
53	0.07183	0.00000	0.07885	0.00000	0.00000	0.00000
54	0.07516	0.00000	0.11083	0.00000	0.00000	0.00000
55	0.19354	0.43338	0.06181	0.00000	-0.00018	0.00000
115	0.08150	0.01770	-0.01798	0.00000	0.00000	0.00000
116	0.08281	0.12594	0.22358	0.00000	0.00000	0.00000
131	0.07998	0.01967	-0.01353	0.00000	0.00000	0.00000
132	0.08093	0.03753	0.02627	0.00000	0.00000	0.00000
133	0.08155	0.02992	0.00927	0.00000	0.00000	0.00000
134	0.07991	0.02062	-0.01140	0.00000	0.00000	0.00000
177	0.06428	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.01245	0.03960	0.00000	-0.05281	0.00000	0.00000
327	1.52094	0.72242	0.98406	0.07208	0.00000	-0.16722
328	0.23281	0.00579	0.02286	0.87362	0.00000	-0.40062
SUM	4.54977	2.24066	1.52622	0.84010	0.00033	-0.56783

Condition **LC4=1.2D+1.6W90**

1	0.01896	0.05415	0.00035	0.00000	0.00005	0.00000
2	0.37009	0.00000	-0.00142	0.00000	0.00000	0.00000
3	-0.02298	0.00000	0.00111	0.00000	0.00000	0.00000
4	0.00510	0.00000	-0.00061	0.00000	0.00000	0.00000
5	1.20234	0.00000	-0.06638	0.00000	0.00000	0.00000
6	0.03465	0.17134	0.00212	0.00000	-0.00004	0.00000
17	0.10698	0.20647	-0.01376	0.00000	0.00008	0.00000
45	-0.05045	0.18890	-0.05857	0.00000	-0.00105	0.00000
50	-0.00084	0.12989	0.03339	0.00000	0.00170	0.00000
51	0.10823	0.00000	0.09355	0.00000	0.00000	0.00000
52	0.05862	0.00000	-0.07487	0.00000	0.00000	0.00000
53	0.07201	0.00000	0.09807	0.00000	0.00000	0.00000
54	0.10205	0.00000	-0.01357	0.00000	0.00000	0.00000
55	0.10681	0.50442	-0.05184	0.00000	-0.00011	0.00000

115	0.08173	0.02007	-0.01284	0.00000	0.00000	0.00000
116	0.08017	0.04908	0.05201	0.00000	0.00000	0.00000
131	0.08001	0.02140	-0.00965	0.00000	0.00000	0.00000
132	0.08094	0.03681	0.02464	0.00000	0.00000	0.00000
133	0.08159	0.02772	0.00437	0.00000	0.00000	0.00000
134	0.07996	0.02300	-0.00611	0.00000	0.00000	0.00000
177	0.05887	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.02158	0.03960	0.00000	-0.05281	0.00000	0.00000
327	1.63442	0.70895	0.53112	-1.53771	0.00000	-0.41295
328	0.26546	0.01927	-0.53112	-0.42717	0.00000	-0.58703
SUM	4.53312	2.24066	0.00000	-2.07049	0.00063	-0.99998

Condition **LC5=1.2D+1.6W120**

1	0.02454	0.05342	0.00028	0.00000	0.00006	0.00000
2	0.48054	0.00000	-0.00195	0.00000	0.00000	0.00000
3	-0.00474	0.00000	0.00105	0.00000	0.00000	0.00000
4	0.03281	0.00000	-0.00063	0.00000	0.00000	0.00000
5	1.24092	0.00000	-0.06687	0.00000	0.00000	0.00000
6	0.02702	0.17280	0.00802	0.00000	-0.00011	0.00000
17	0.12469	0.20612	-0.03612	0.00000	0.00033	0.00000
45	-0.04232	0.19422	-0.05957	0.00000	-0.00136	0.00000
50	-0.00023	0.12675	0.03339	0.00000	0.00175	0.00000
51	0.10892	0.00000	-0.02989	0.00000	0.00000	0.00000
52	0.05843	0.00000	-0.07252	0.00000	0.00000	0.00000
53	0.07170	0.00000	0.09313	0.00000	0.00000	0.00000
54	0.10036	0.00000	-0.13103	0.00000	0.00000	0.00000
55	0.01455	0.56969	-0.15729	0.00000	-0.00014	0.00000
115	0.08190	0.02681	0.00208	0.00000	0.00000	0.00000
116	0.07784	-0.02477	-0.11294	0.00000	0.00000	0.00000
131	0.07998	0.01978	-0.01328	0.00000	0.00000	0.00000
132	0.08092	0.03763	0.02649	0.00000	0.00000	0.00000
133	0.08154	0.03000	0.00944	0.00000	0.00000	0.00000
134	0.07992	0.02077	-0.01110	0.00000	0.00000	0.00000
177	0.05654	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.03937	0.03960	0.00000	-0.05281	0.00000	0.00000
327	1.53558	0.62371	0.00560	-2.93813	0.00000	-0.57078
328	0.27772	0.10450	-1.01252	-1.90104	0.00000	-0.71072
SUM	4.54977	2.24066	-1.52622	-4.94478	0.00053	-1.28149

Condition **LC6=1.2D+1.6W150**

1	0.04378	0.12611	-0.00211	0.00000	0.00164	0.00000
2	0.54321	0.00000	-0.05391	0.00000	0.00000	0.00000
3	-0.06472	0.00000	-0.05643	0.00000	0.00000	0.00000
4	0.04472	0.00000	-0.07146	0.00000	0.00000	0.00000
5	0.18787	0.00000	-0.00821	0.00000	0.00000	0.00000
6	-0.12392	0.31116	-0.20556	0.00000	-0.00001	0.00000
17	0.02034	0.31952	-0.28580	0.00000	0.00061	0.00000
45	0.03332	0.21199	-0.04876	0.00000	-0.00189	0.00000
50	-0.00308	0.12429	0.04769	0.00000	0.00120	0.00000
51	0.06772	0.00000	-0.18235	0.00000	0.00000	0.00000
52	-0.00077	0.00000	-0.13393	0.00000	0.00000	0.00000
53	0.00277	0.00000	-0.10619	0.00000	0.00000	0.00000
54	0.05110	0.00000	-0.21942	0.00000	0.00000	0.00000
55	-0.25578	0.71102	-0.41213	0.00000	-0.00060	0.00000
115	0.00897	-0.02593	-0.15617	0.00000	0.00000	0.00000
116	-0.00613	-0.21378	-0.57333	0.00000	0.00000	0.00000
131	0.00176	-0.05249	-0.21506	0.00000	0.00000	0.00000

132	0.00576	0.00199	-0.09305	0.00000	0.00000	0.00000
133	0.00847	-0.03768	-0.18243	0.00000	0.00000	0.00000
134	0.00141	-0.04298	-0.19381	0.00000	0.00000	0.00000
177	-0.02007	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.14478	0.03960	0.00000	-0.05281	0.00000	0.00000
327	1.49745	0.62917	-0.35554	-4.00126	0.00000	-0.83226
328	0.10650	0.09904	-1.45781	-2.66354	0.00000	-0.90325
SUM	2.00592	2.24066	-4.96577	-6.77042	0.00095	-1.73551

Condition **LC7=1.2D-1.6Wo**

1	0.04256	0.12539	-0.00216	0.00000	0.00164	0.00000
2	0.41006	0.00000	-0.05423	0.00000	0.00000	0.00000
3	-0.06292	0.00000	-0.05649	0.00000	0.00000	0.00000
4	0.04515	0.00000	-0.07144	0.00000	0.00000	0.00000
5	-0.06573	0.00000	-0.00821	0.00000	0.00000	0.00000
6	-0.12270	0.31147	-0.20247	0.00000	-0.00001	0.00000
17	0.00308	0.31224	-0.29349	0.00000	0.00077	0.00000
45	-0.00303	0.22336	-0.04039	0.00000	-0.00202	0.00000
50	-0.00199	0.12247	0.06148	0.00000	0.00102	0.00000
51	0.05451	0.00000	-0.24377	0.00000	0.00000	0.00000
52	-0.00109	0.00000	-0.11787	0.00000	0.00000	0.00000
53	0.00241	0.00000	-0.09860	0.00000	0.00000	0.00000
54	0.03819	0.00000	-0.25024	0.00000	0.00000	0.00000
55	-0.35698	0.75071	-0.48214	0.00000	-0.00048	0.00000
115	0.00921	-0.01823	-0.13902	0.00000	0.00000	0.00000
116	-0.00806	-0.26276	-0.68267	0.00000	0.00000	0.00000
131	0.00176	-0.05190	-0.21373	0.00000	0.00000	0.00000
132	0.00575	0.00182	-0.09344	0.00000	0.00000	0.00000
133	0.00845	-0.03833	-0.18388	0.00000	0.00000	0.00000
134	0.00136	-0.04300	-0.19385	0.00000	0.00000	0.00000
177	-0.00935	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.06683	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.02506	0.26342	-1.30954	-4.38126	0.00000	-0.09219
328	0.05113	0.46479	-1.40391	-4.73245	0.00000	-0.40302
SUM	0.00000	2.24066	-6.08004	-9.21932	0.00093	-0.49522

Condition **LC8=1.2D-1.6W30**

1	0.04126	0.12496	-0.00217	0.00000	0.00163	0.00000
2	0.24157	0.00000	-0.05366	0.00000	0.00000	0.00000
3	-0.06129	0.00000	-0.05656	0.00000	0.00000	0.00000
4	0.04551	0.00000	-0.07143	0.00000	0.00000	0.00000
5	-0.32662	0.00000	-0.00823	0.00000	0.00000	0.00000
6	-0.13226	0.30921	-0.20769	0.00000	0.00005	0.00000
17	-0.04729	0.30663	-0.26966	0.00000	0.00053	0.00000
45	-0.05065	0.23186	-0.03135	0.00000	-0.00158	0.00000
50	-0.00087	0.12240	0.06894	0.00000	0.00055	0.00000
51	0.02602	0.00000	-0.25024	0.00000	0.00000	0.00000
52	-0.00191	0.00000	-0.13554	0.00000	0.00000	0.00000
53	0.00207	0.00000	-0.12466	0.00000	0.00000	0.00000
54	0.01311	0.00000	-0.22872	0.00000	0.00000	0.00000
55	-0.33568	0.69459	-0.40025	0.00000	-0.00038	0.00000
115	0.00914	-0.01768	-0.13766	0.00000	0.00000	0.00000
116	-0.00614	-0.20687	-0.55767	0.00000	0.00000	0.00000
131	0.00176	-0.05172	-0.21334	0.00000	0.00000	0.00000
132	0.00574	0.00169	-0.09373	0.00000	0.00000	0.00000
133	0.00842	-0.03867	-0.18463	0.00000	0.00000	0.00000
134	0.00131	-0.04316	-0.19417	0.00000	0.00000	0.00000

177	0.00548	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.05143	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-1.47716	-0.02954	-1.40235	-2.13445	0.00000	0.95535
328	-0.01886	0.75775	-0.41100	-4.51704	0.00000	0.33248
SUM	-2.00592	2.24066	-4.96577	-6.75710	0.00079	1.28783

Condition **LC9=1.2D-1.6W60**

1	0.01080	0.12064	0.00080	0.00000	0.00005	0.00000
2	-0.21152	0.00000	-0.00353	0.00000	0.00000	0.00000
3	-0.16091	0.00000	0.00265	0.00000	0.00000	0.00000
4	-0.18519	0.00000	-0.00234	0.00000	0.00000	0.00000
5	-1.15772	0.00000	0.06562	0.00000	0.00000	0.00000
6	-0.01761	0.16268	0.00625	0.00000	0.00000	0.00000
17	0.00467	0.19160	-0.02573	0.00000	0.00041	0.00000
45	-0.10772	0.25094	-0.05652	0.00000	0.00037	0.00000
50	-0.00279	0.12052	0.08725	0.00000	-0.00122	0.00000
51	-0.06881	0.00000	-0.11579	0.00000	0.00000	0.00000
52	-0.06356	0.00000	-0.08528	0.00000	0.00000	0.00000
53	-0.06957	0.00000	-0.01702	0.00000	0.00000	0.00000
54	-0.06949	0.00000	-0.12135	0.00000	0.00000	0.00000
55	-0.16640	0.49890	-0.10876	0.00000	-0.00007	0.00000
115	-0.07355	0.03490	0.02080	0.00000	0.00000	0.00000
116	-0.07961	-0.05111	-0.17009	0.00000	0.00000	0.00000
131	-0.07563	0.02744	0.00411	0.00000	0.00000	0.00000
132	-0.07455	0.02721	0.00349	0.00000	0.00000	0.00000
133	-0.07421	0.02346	-0.00488	0.00000	0.00000	0.00000
134	-0.07594	0.02606	0.00101	0.00000	0.00000	0.00000
177	-0.06438	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.01304	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-1.52086	0.02705	-0.98397	-1.24874	0.00000	0.91379
328	-0.23220	0.70117	-0.02295	-3.58018	0.00000	0.31783
SUM	-4.54977	2.24066	-1.52622	-4.93453	-0.00046	1.23162

Condition **LC10=1.2D-1.6W90**

1	0.01485	0.12031	0.00071	0.00000	0.00004	0.00000
2	-0.21965	0.00000	-0.00260	0.00000	0.00000	0.00000
3	-0.12352	0.00000	0.00250	0.00000	0.00000	0.00000
4	-0.09479	0.00000	-0.00233	0.00000	0.00000	0.00000
5	-1.15726	0.00000	0.06515	0.00000	0.00000	0.00000
6	-0.02282	0.16057	-0.00001	0.00000	0.00003	0.00000
17	-0.01702	0.19184	-0.00114	0.00000	0.00010	0.00000
45	-0.11236	0.24912	-0.05878	0.00000	0.00092	0.00000
50	-0.00178	0.12243	0.10201	0.00000	-0.00168	0.00000
51	-0.09937	0.00000	-0.01125	0.00000	0.00000	0.00000
52	-0.06415	0.00000	-0.09201	0.00000	0.00000	0.00000
53	-0.06973	0.00000	-0.02166	0.00000	0.00000	0.00000
54	-0.09604	0.00000	-0.00434	0.00000	0.00000	0.00000
55	-0.08135	0.42753	0.00505	0.00000	-0.00013	0.00000
115	-0.07373	0.03149	0.01332	0.00000	0.00000	0.00000
116	-0.07684	0.02630	0.00280	0.00000	0.00000	0.00000
131	-0.07565	0.02672	0.00248	0.00000	0.00000	0.00000
132	-0.07455	0.02763	0.00442	0.00000	0.00000	0.00000
133	-0.07423	0.02426	-0.00310	0.00000	0.00000	0.00000
134	-0.07598	0.02505	-0.00122	0.00000	0.00000	0.00000
177	-0.05909	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.02059	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-1.63544	0.03530	-0.53151	0.36038	0.00000	1.16127

328	-0.26322	0.69291	0.53151	-2.31491	0.00000	0.50737
SUM	-4.53312	2.24066	0.00000	-2.06014	-0.00070	1.66863

Condition **LC11=1.2D-1.6W120**

1	0.01041	0.12101	0.00083	0.00000	0.00003	0.00000
2	-0.27647	0.00000	-0.00221	0.00000	0.00000	0.00000
3	-0.17685	0.00000	0.00263	0.00000	0.00000	0.00000
4	-0.16539	0.00000	-0.00234	0.00000	0.00000	0.00000
5	-1.16698	0.00000	0.06559	0.00000	0.00000	0.00000
6	-0.02996	0.15857	-0.00582	0.00000	0.00008	0.00000
17	-0.03306	0.19304	0.02117	0.00000	-0.00017	0.00000
45	-0.10623	0.24315	-0.06038	0.00000	0.00123	0.00000
50	-0.00237	0.12544	0.10184	0.00000	-0.00172	0.00000
51	-0.10007	0.00000	0.11473	0.00000	0.00000	0.00000
52	-0.06394	0.00000	-0.09384	0.00000	0.00000	0.00000
53	-0.06942	0.00000	-0.01691	0.00000	0.00000	0.00000
54	-0.09421	0.00000	0.11294	0.00000	0.00000	0.00000
55	0.00395	0.36270	0.11061	0.00000	-0.00012	0.00000
115	-0.07392	0.02580	0.00076	0.00000	0.00000	0.00000
116	-0.07441	0.09972	0.16679	0.00000	0.00000	0.00000
131	-0.07564	0.02705	0.00323	0.00000	0.00000	0.00000
132	-0.07454	0.02721	0.00349	0.00000	0.00000	0.00000
133	-0.07422	0.02370	-0.00436	0.00000	0.00000	0.00000
134	-0.07596	0.02583	0.00056	0.00000	0.00000	0.00000
177	-0.05680	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.03847	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-1.53770	0.11380	-0.00702	1.77612	0.00000	1.31440
328	-0.27444	0.61442	1.01394	-0.82225	0.00000	0.63395
SUM	-4.54977	2.24066	1.52622	0.84826	-0.00066	1.94836

Condition **LC12=1.2D-1.6W150**

1	-0.00734	0.04844	0.00328	0.00000	-0.00153	0.00000
2	-0.34523	0.00000	0.05000	0.00000	0.00000	0.00000
3	-0.14903	0.00000	0.06012	0.00000	0.00000	0.00000
4	-0.12251	0.00000	0.06840	0.00000	0.00000	0.00000
5	-0.13599	0.00000	0.00754	0.00000	0.00000	0.00000
6	0.09434	0.01951	0.20752	0.00000	-0.00005	0.00000
17	0.06345	0.07891	0.27076	0.00000	-0.00044	0.00000
45	-0.11791	0.22613	-0.17144	0.00000	0.00185	0.00000
50	0.00042	0.12701	0.08486	0.00000	-0.00119	0.00000
51	-0.05805	0.00000	0.47341	0.00000	0.00000	0.00000
52	-0.00505	0.00000	-0.07040	0.00000	0.00000	0.00000
53	-0.00046	0.00000	0.04138	0.00000	0.00000	0.00000
54	-0.04479	0.00000	0.27618	0.00000	0.00000	0.00000
55	0.24901	0.22282	0.36647	0.00000	0.00032	0.00000
115	-0.00104	0.07861	0.15914	0.00000	0.00000	0.00000
116	0.00904	0.28926	0.62791	0.00000	0.00000	0.00000
131	0.00245	0.09791	0.20179	0.00000	0.00000	0.00000
132	0.00061	0.06294	0.12321	0.00000	0.00000	0.00000
133	-0.00119	0.09304	0.19117	0.00000	0.00000	0.00000
134	0.00244	0.08865	0.18110	0.00000	0.00000	0.00000
177	0.01979	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.14385	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-1.50108	0.10338	0.35252	2.85893	0.00000	1.56991
328	-0.10166	0.62483	1.46083	-0.01191	0.00000	0.82691
SUM	-2.00592	2.24066	4.96577	2.74141	-0.00103	2.39682

Condition **LC13=0.9D+1.6Wo**

1	-0.01114	0.02739	0.00316	0.00000	-0.00154	0.00000
2	-0.25606	0.00000	0.05083	0.00000	0.00000	0.00000
3	-0.11343	0.00000	0.05969	0.00000	0.00000	0.00000
4	-0.10660	0.00000	0.06878	0.00000	0.00000	0.00000
5	0.10604	0.00000	0.00760	0.00000	0.00000	0.00000
6	0.10297	-0.02177	0.20421	0.00000	-0.00004	0.00000
17	0.07257	0.03585	0.28020	0.00000	-0.00062	0.00000
45	-0.07691	0.16028	-0.16592	0.00000	0.00200	0.00000
50	-0.00037	0.09731	0.05379	0.00000	-0.00100	0.00000
51	-0.04544	0.00000	0.52966	0.00000	0.00000	0.00000
52	-0.00407	0.00000	-0.06693	0.00000	0.00000	0.00000
53	-0.00037	0.00000	0.01656	0.00000	0.00000	0.00000
54	-0.03240	0.00000	0.31356	0.00000	0.00000	0.00000
55	0.35541	0.06620	0.44309	0.00000	0.00023	0.00000
115	-0.00228	0.06339	0.13954	0.00000	0.00000	0.00000
116	0.01039	0.32946	0.73161	0.00000	0.00000	0.00000
131	0.00193	0.09225	0.20346	0.00000	0.00000	0.00000
132	-0.00018	0.05481	0.11941	0.00000	0.00000	0.00000
133	-0.00208	0.08592	0.18960	0.00000	0.00000	0.00000
134	0.00203	0.08384	0.18469	0.00000	0.00000	0.00000
177	0.00945	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.06745	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-0.02635	0.38280	1.30746	3.39735	0.00000	0.72356
328	-0.05054	0.16337	1.40599	2.51498	0.00000	0.33170
SUM	0.00000	1.68049	6.08004	5.83313	-0.00097	1.05525

Condition **LC14=0.9D+1.6W30**

1	-0.01060	0.02776	0.00315	0.00000	-0.00154	0.00000
2	-0.12311	0.00000	0.05023	0.00000	0.00000	0.00000
3	-0.07710	0.00000	0.05973	0.00000	0.00000	0.00000
4	-0.08515	0.00000	0.06879	0.00000	0.00000	0.00000
5	0.34850	0.00000	0.00752	0.00000	0.00000	0.00000
6	0.12025	-0.01915	0.20946	0.00000	-0.00008	0.00000
17	0.11914	0.04132	0.25644	0.00000	-0.00037	0.00000
45	-0.04859	0.15281	-0.15668	0.00000	0.00156	0.00000
50	-0.00149	0.09745	0.04679	0.00000	-0.00053	0.00000
51	-0.01734	0.00000	0.50058	0.00000	0.00000	0.00000
52	-0.00322	0.00000	-0.04270	0.00000	0.00000	0.00000
53	-0.00006	0.00000	0.06481	0.00000	0.00000	0.00000
54	-0.00746	0.00000	0.28069	0.00000	0.00000	0.00000
55	0.34472	0.12108	0.36053	0.00000	0.00017	0.00000
115	-0.00220	0.06221	0.13676	0.00000	0.00000	0.00000
116	0.00867	0.27369	0.60708	0.00000	0.00000	0.00000
131	0.00196	0.09276	0.20461	0.00000	0.00000	0.00000
132	-0.00018	0.05476	0.11931	0.00000	0.00000	0.00000
133	-0.00205	0.08532	0.18828	0.00000	0.00000	0.00000
134	0.00211	0.08491	0.18705	0.00000	0.00000	0.00000
177	-0.00551	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.05189	0.02970	0.00000	-0.03960	0.00000	0.00000
327	1.47793	0.68986	1.40250	1.11084	0.00000	-0.30616
328	0.01857	-0.14370	0.41085	2.21615	0.00000	-0.41205
SUM	2.00592	1.68049	4.96577	3.24778	-0.00079	-0.71821

Condition **LC15=0.9D+1.6W60**

1	0.01975	0.03210	0.00016	0.00000	0.00004	0.00000
2	0.40972	0.00000	-0.00007	0.00000	0.00000	0.00000
3	0.00273	0.00000	0.00056	0.00000	0.00000	0.00000
4	0.02773	0.00000	-0.00026	0.00000	0.00000	0.00000
5	1.24530	0.00000	-0.06674	0.00000	0.00000	0.00000
6	0.01965	0.12804	-0.00448	0.00000	-0.00002	0.00000
17	0.05862	0.15691	0.01272	0.00000	-0.00030	0.00000
45	-0.02299	0.13206	-0.05635	0.00000	-0.00048	0.00000
50	0.00049	0.10011	0.03082	0.00000	0.00125	0.00000
51	0.07677	0.00000	0.20560	0.00000	0.00000	0.00000
52	0.05870	0.00000	-0.06075	0.00000	0.00000	0.00000
53	0.07155	0.00000	0.06918	0.00000	0.00000	0.00000
54	0.07461	0.00000	0.11322	0.00000	0.00000	0.00000
55	0.19415	0.31664	0.06814	0.00000	-0.00016	0.00000
115	0.08051	0.01122	-0.01813	0.00000	0.00000	0.00000
116	0.08240	0.11666	0.21704	0.00000	0.00000	0.00000
131	0.07944	0.01371	-0.01253	0.00000	0.00000	0.00000
132	0.08013	0.02947	0.02261	0.00000	0.00000	0.00000
133	0.08063	0.02338	0.00901	0.00000	0.00000	0.00000
134	0.07941	0.01463	-0.01046	0.00000	0.00000	0.00000
177	0.06428	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.01245	0.02970	0.00000	-0.03960	0.00000	0.00000
327	1.52093	0.62960	0.98406	0.21824	0.00000	-0.26064
328	0.23281	-0.08343	0.02286	1.21579	0.00000	-0.39085
SUM	4.54977	1.68049	1.52622	1.35482	0.00033	-0.65149

Condition **LC16=0.9D+1.6W90**

1	0.01477	0.03239	0.00021	0.00000	0.00004	0.00000
2	0.36573	0.00000	-0.00091	0.00000	0.00000	0.00000
3	-0.01605	0.00000	0.00066	0.00000	0.00000	0.00000
4	-0.00046	0.00000	-0.00024	0.00000	0.00000	0.00000
5	1.20708	0.00000	-0.06623	0.00000	0.00000	0.00000
6	0.03535	0.12999	0.00185	0.00000	-0.00004	0.00000
17	0.09726	0.15688	-0.01196	0.00000	0.00005	0.00000
45	-0.03492	0.13395	-0.04252	0.00000	-0.00104	0.00000
50	-0.00053	0.09830	0.01628	0.00000	0.00171	0.00000
51	0.10748	0.00000	0.08158	0.00000	0.00000	0.00000
52	0.05931	0.00000	-0.05419	0.00000	0.00000	0.00000
53	0.07173	0.00000	0.08840	0.00000	0.00000	0.00000
54	0.10149	0.00000	-0.01119	0.00000	0.00000	0.00000
55	0.10746	0.38766	-0.04554	0.00000	-0.00009	0.00000
115	0.08073	0.01359	-0.01297	0.00000	0.00000	0.00000
116	0.07977	0.03980	0.04549	0.00000	0.00000	0.00000
131	0.07947	0.01544	-0.00864	0.00000	0.00000	0.00000
132	0.08014	0.02874	0.02098	0.00000	0.00000	0.00000
133	0.08068	0.02118	0.00411	0.00000	0.00000	0.00000
134	0.07947	0.01700	-0.00518	0.00000	0.00000	0.00000
177	0.05887	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.02158	0.02970	0.00000	-0.03960	0.00000	0.00000
327	1.63442	0.61619	0.53112	-1.38837	0.00000	-0.50531
328	0.26546	-0.07002	-0.53112	-0.08401	0.00000	-0.57648
SUM	4.53312	1.68049	0.00000	-1.55158	0.00063	-1.08179

Condition **LC17=0.9D+1.6W120**

1	0.02035	0.03167	0.00014	0.00000	0.00005	0.00000
2	0.47614	0.00000	-0.00144	0.00000	0.00000	0.00000
3	0.00219	0.00000	0.00060	0.00000	0.00000	0.00000
4	0.02725	0.00000	-0.00026	0.00000	0.00000	0.00000
5	1.24566	0.00000	-0.06672	0.00000	0.00000	0.00000
6	0.02772	0.13145	0.00775	0.00000	-0.00011	0.00000
17	0.11498	0.15653	-0.03432	0.00000	0.00031	0.00000
45	-0.02680	0.13927	-0.04353	0.00000	-0.00135	0.00000
50	0.00009	0.09516	0.01630	0.00000	0.00175	0.00000
51	0.10817	0.00000	-0.04184	0.00000	0.00000	0.00000
52	0.05911	0.00000	-0.05185	0.00000	0.00000	0.00000
53	0.07142	0.00000	0.08347	0.00000	0.00000	0.00000
54	0.09980	0.00000	-0.12866	0.00000	0.00000	0.00000
55	0.01524	0.45293	-0.15102	0.00000	-0.00013	0.00000
115	0.08090	0.02034	0.00195	0.00000	0.00000	0.00000
116	0.07745	-0.03404	-0.11945	0.00000	0.00000	0.00000
131	0.07944	0.01382	-0.01227	0.00000	0.00000	0.00000
132	0.08013	0.02957	0.02283	0.00000	0.00000	0.00000
133	0.08062	0.02346	0.00918	0.00000	0.00000	0.00000
134	0.07942	0.01478	-0.01017	0.00000	0.00000	0.00000
177	0.05654	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.03937	0.02970	0.00000	-0.03960	0.00000	0.00000
327	1.53558	0.53106	0.00560	-2.78615	0.00000	-0.66216
328	0.27772	0.01510	-1.01252	-1.55670	0.00000	-0.69957
SUM	4.54977	1.68049	-1.52622	-4.42206	0.00053	-1.36173

Condition **LC18=0.9D+1.6W150**

1	0.03963	0.10441	-0.00224	0.00000	0.00163	0.00000
2	0.53904	0.00000	-0.05340	0.00000	0.00000	0.00000
3	-0.05785	0.00000	-0.05688	0.00000	0.00000	0.00000
4	0.03924	0.00000	-0.07110	0.00000	0.00000	0.00000
5	0.19240	0.00000	-0.00806	0.00000	0.00000	0.00000
6	-0.12383	0.26978	-0.20585	0.00000	-0.00001	0.00000
17	0.01143	0.26976	-0.28404	0.00000	0.00058	0.00000
45	0.04659	0.15654	-0.03423	0.00000	-0.00188	0.00000
50	-0.00277	0.09303	0.03092	0.00000	0.00121	0.00000
51	0.06711	0.00000	-0.18568	0.00000	0.00000	0.00000
52	-0.00009	0.00000	-0.12429	0.00000	0.00000	0.00000
53	0.00250	0.00000	-0.11023	0.00000	0.00000	0.00000
54	0.05050	0.00000	-0.21914	0.00000	0.00000	0.00000
55	-0.25322	0.59457	-0.40578	0.00000	-0.00058	0.00000
115	0.00798	-0.03238	-0.15625	0.00000	0.00000	0.00000
116	-0.00651	-0.22306	-0.57985	0.00000	0.00000	0.00000
131	0.00123	-0.05841	-0.21394	0.00000	0.00000	0.00000
132	0.00496	-0.00608	-0.09673	0.00000	0.00000	0.00000
133	0.00756	-0.04427	-0.18280	0.00000	0.00000	0.00000
134	0.00092	-0.04897	-0.19285	0.00000	0.00000	0.00000
177	-0.02007	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.14478	0.02970	0.00000	-0.03960	0.00000	0.00000
327	1.49745	0.53656	-0.35554	-3.84748	0.00000	-0.92284
328	0.10650	0.00961	-1.45781	-2.31911	0.00000	-0.89153
SUM	2.00592	1.68049	-4.96577	-6.24579	0.00095	-1.81436

Condition **LC19=0.9D-1.6Wo**

1	0.03842	0.10369	-0.00229	0.00000	0.00163	0.00000
2	0.40591	0.00000	-0.05373	0.00000	0.00000	0.00000
3	-0.05606	0.00000	-0.05694	0.00000	0.00000	0.00000
4	0.03966	0.00000	-0.07108	0.00000	0.00000	0.00000
5	-0.06112	0.00000	-0.00805	0.00000	0.00000	0.00000
6	-0.12279	0.27008	-0.20275	0.00000	-0.00001	0.00000
17	-0.00608	0.26245	-0.29172	0.00000	0.00075	0.00000
45	0.01045	0.16789	-0.02619	0.00000	-0.00202	0.00000
50	-0.00168	0.09121	0.04471	0.00000	0.00104	0.00000
51	0.05389	0.00000	-0.24675	0.00000	0.00000	0.00000
52	-0.00042	0.00000	-0.10784	0.00000	0.00000	0.00000
53	0.00214	0.00000	-0.10334	0.00000	0.00000	0.00000
54	0.03758	0.00000	-0.24966	0.00000	0.00000	0.00000
55	-0.35427	0.63431	-0.47582	0.00000	-0.00046	0.00000
115	0.00822	-0.02465	-0.13904	0.00000	0.00000	0.00000
116	-0.00844	-0.27206	-0.68922	0.00000	0.00000	0.00000
131	0.00123	-0.05783	-0.21265	0.00000	0.00000	0.00000
132	0.00495	-0.00625	-0.09711	0.00000	0.00000	0.00000
133	0.00754	-0.04490	-0.18419	0.00000	0.00000	0.00000
134	0.00088	-0.04901	-0.19294	0.00000	0.00000	0.00000
177	-0.00935	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.06683	0.02970	0.00000	-0.03960	0.00000	0.00000
327	0.02506	0.17084	-1.30954	-4.22715	0.00000	-0.18283
328	0.05113	0.37532	-1.40391	-4.38655	0.00000	-0.39196
SUM	0.00000	1.68049	-6.08004	-8.69291	0.00093	-0.57479

Condition **LC20=0.9D-1.6W30**

1	0.03712	0.10325	-0.00230	0.00000	0.00162	0.00000
2	0.23746	0.00000	-0.05315	0.00000	0.00000	0.00000
3	-0.05446	0.00000	-0.05701	0.00000	0.00000	0.00000
4	0.04002	0.00000	-0.07106	0.00000	0.00000	0.00000
5	-0.32195	0.00000	-0.00808	0.00000	0.00000	0.00000
6	-0.13249	0.26782	-0.20798	0.00000	0.00005	0.00000
17	-0.05663	0.25681	-0.26789	0.00000	0.00050	0.00000
45	-0.03700	0.17638	-0.01740	0.00000	-0.00158	0.00000
50	-0.00057	0.09115	0.05217	0.00000	0.00056	0.00000
51	0.02540	0.00000	-0.25296	0.00000	0.00000	0.00000
52	-0.00124	0.00000	-0.12521	0.00000	0.00000	0.00000
53	0.00180	0.00000	-0.12994	0.00000	0.00000	0.00000
54	0.01249	0.00000	-0.22791	0.00000	0.00000	0.00000
55	-0.33290	0.57825	-0.39391	0.00000	-0.00036	0.00000
115	0.00814	-0.02409	-0.13764	0.00000	0.00000	0.00000
116	-0.00653	-0.21618	-0.56426	0.00000	0.00000	0.00000
131	0.00122	-0.05767	-0.21229	0.00000	0.00000	0.00000
132	0.00495	-0.00638	-0.09739	0.00000	0.00000	0.00000
133	0.00751	-0.04522	-0.18491	0.00000	0.00000	0.00000
134	0.00082	-0.04919	-0.19330	0.00000	0.00000	0.00000
177	0.00548	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.05143	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-1.47716	-0.12223	-1.40235	-1.98469	0.00000	0.86305
328	-0.01886	0.66839	-0.41100	-4.17103	0.00000	0.34180
SUM	-2.00592	1.68049	-4.96577	-6.23493	0.00079	1.20485

Condition **LC21=0.9D-1.6W60**

1	0.00664	0.09890	0.00067	0.00000	0.00003	0.00000
2	-0.21575	0.00000	-0.00303	0.00000	0.00000	0.00000
3	-0.15441	0.00000	0.00220	0.00000	0.00000	0.00000
4	-0.19181	0.00000	-0.00197	0.00000	0.00000	0.00000
5	-1.15205	0.00000	0.06577	0.00000	0.00000	0.00000
6	-0.01751	0.12123	0.00598	0.00000	0.00000	0.00000
17	-0.00329	0.14185	-0.02395	0.00000	0.00039	0.00000
45	-0.09462	0.19559	-0.03969	0.00000	0.00038	0.00000
50	-0.00248	0.08909	0.07032	0.00000	-0.00120	0.00000
51	-0.06947	0.00000	-0.12932	0.00000	0.00000	0.00000
52	-0.06287	0.00000	-0.06476	0.00000	0.00000	0.00000
53	-0.06984	0.00000	-0.02487	0.00000	0.00000	0.00000
54	-0.07010	0.00000	-0.12005	0.00000	0.00000	0.00000
55	-0.16411	0.38265	-0.10238	0.00000	-0.00005	0.00000
115	-0.07454	0.02851	0.02085	0.00000	0.00000	0.00000
116	-0.08001	-0.06044	-0.17674	0.00000	0.00000	0.00000
131	-0.07617	0.02147	0.00510	0.00000	0.00000	0.00000
132	-0.07534	0.01915	-0.00015	0.00000	0.00000	0.00000
133	-0.07513	0.01694	-0.00509	0.00000	0.00000	0.00000
134	-0.07644	0.01999	0.00179	0.00000	0.00000	0.00000
177	-0.06438	0.02970	0.00000	-0.03960	0.00000	0.00000
178	-0.01304	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-1.52086	-0.06571	-0.98397	-1.10049	0.00000	0.82102
328	-0.23220	0.61187	-0.02295	-3.23442	0.00000	0.32690
SUM	-4.54977	1.68049	-1.52622	-4.41412	-0.00046	1.14792

Condition **LC22=0.9D-1.6W90**

1	0.01069	0.09856	0.00058	0.00000	0.00003	0.00000
2	-0.22413	0.00000	-0.00210	0.00000	0.00000	0.00000
3	-0.11704	0.00000	0.00205	0.00000	0.00000	0.00000
4	-0.10114	0.00000	-0.00197	0.00000	0.00000	0.00000
5	-1.15171	0.00000	0.06530	0.00000	0.00000	0.00000
6	-0.02275	0.11912	-0.00027	0.00000	0.00003	0.00000
17	-0.02508	0.14208	0.00062	0.00000	0.00007	0.00000
45	-0.09886	0.19380	-0.04287	0.00000	0.00093	0.00000
50	-0.00146	0.09097	0.08501	0.00000	-0.00166	0.00000
51	-0.10002	0.00000	-0.02299	0.00000	0.00000	0.00000
52	-0.06347	0.00000	-0.07148	0.00000	0.00000	0.00000
53	-0.07000	0.00000	-0.03126	0.00000	0.00000	0.00000
54	-0.09663	0.00000	-0.00212	0.00000	0.00000	0.00000
55	-0.07923	0.31129	0.01147	0.00000	-0.00011	0.00000
115	-0.07473	0.02509	0.01336	0.00000	0.00000	0.00000
116	-0.07725	0.01698	-0.00384	0.00000	0.00000	0.00000
131	-0.07619	0.02074	0.00347	0.00000	0.00000	0.00000
132	-0.07535	0.01957	0.00077	0.00000	0.00000	0.00000
133	-0.07514	0.01775	-0.00330	0.00000	0.00000	0.00000
134	-0.07648	0.01898	-0.00045	0.00000	0.00000	0.00000
177	-0.05909	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.02059	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-1.63544	-0.05751	-0.53151	0.50545	0.00000	1.06743
328	-0.26322	0.60367	0.53151	-1.97009	0.00000	0.51566
SUM	-4.53312	1.68049	0.00000	-1.54385	-0.00070	1.58309

Condition **LC23=0.9D-1.6W120**

1	0.00625	0.09926	0.00070	0.00000	0.00002	0.00000
2	-0.28094	0.00000	-0.00170	0.00000	0.00000	0.00000
3	-0.17036	0.00000	0.00218	0.00000	0.00000	0.00000
4	-0.17174	0.00000	-0.00197	0.00000	0.00000	0.00000
5	-1.16143	0.00000	0.06574	0.00000	0.00000	0.00000
6	-0.02989	0.11712	-0.00608	0.00000	0.00008	0.00000
17	-0.04112	0.14329	0.02293	0.00000	-0.00019	0.00000
45	-0.09272	0.18783	-0.04445	0.00000	0.00123	0.00000
50	-0.00206	0.09399	0.08483	0.00000	-0.00170	0.00000
51	-0.10071	0.00000	0.10297	0.00000	0.00000	0.00000
52	-0.06326	0.00000	-0.07330	0.00000	0.00000	0.00000
53	-0.06970	0.00000	-0.02651	0.00000	0.00000	0.00000
54	-0.09480	0.00000	0.11516	0.00000	0.00000	0.00000
55	0.00604	0.24647	0.11706	0.00000	-0.00010	0.00000
115	-0.07492	0.01940	0.00079	0.00000	0.00000	0.00000
116	-0.07483	0.09039	0.16013	0.00000	0.00000	0.00000
131	-0.07619	0.02108	0.00422	0.00000	0.00000	0.00000
132	-0.07534	0.01915	-0.00016	0.00000	0.00000	0.00000
133	-0.07513	0.01719	-0.00455	0.00000	0.00000	0.00000
134	-0.07646	0.01976	0.00133	0.00000	0.00000	0.00000
177	-0.05680	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.03847	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-1.53770	0.02089	-0.00702	1.91851	0.00000	1.21960
328	-0.27444	0.52528	1.01394	-0.47865	0.00000	0.64164
SUM	-4.54977	1.68049	1.52622	1.36065	-0.00066	1.86123

Condition **LC24=0.9D-1.6W150**

1	-0.01148	0.02671	0.00315	0.00000	-0.00154	0.00000
2	-0.34887	0.00000	0.05050	0.00000	0.00000	0.00000
3	-0.14153	0.00000	0.05967	0.00000	0.00000	0.00000
4	-0.12987	0.00000	0.06877	0.00000	0.00000	0.00000
5	-0.13019	0.00000	0.00769	0.00000	0.00000	0.00000
6	0.09423	-0.02190	0.20728	0.00000	-0.00006	0.00000
17	0.05462	0.02924	0.27254	0.00000	-0.00046	0.00000
45	-0.10170	0.17110	-0.15553	0.00000	0.00186	0.00000
50	0.00073	0.09544	0.06774	0.00000	-0.00118	0.00000
51	-0.05880	0.00000	0.46158	0.00000	0.00000	0.00000
52	-0.00436	0.00000	-0.04967	0.00000	0.00000	0.00000
53	-0.00074	0.00000	0.03171	0.00000	0.00000	0.00000
54	-0.04536	0.00000	0.27855	0.00000	0.00000	0.00000
55	0.24837	0.10629	0.37289	0.00000	0.00034	0.00000
115	-0.00204	0.07219	0.15912	0.00000	0.00000	0.00000
116	0.00861	0.27993	0.62124	0.00000	0.00000	0.00000
131	0.00190	0.09194	0.20278	0.00000	0.00000	0.00000
132	-0.00019	0.05487	0.11954	0.00000	0.00000	0.00000
133	-0.00211	0.08652	0.19095	0.00000	0.00000	0.00000
134	0.00194	0.08259	0.18189	0.00000	0.00000	0.00000
177	0.01979	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.14385	0.02970	0.00000	-0.03960	0.00000	0.00000
327	-1.50108	0.01043	0.35252	2.99946	0.00000	1.47430
328	-0.10167	0.53573	1.46083	0.33150	0.00000	0.83401
SUM	-2.00592	1.68049	4.96577	3.25174	-0.00103	2.30831

Condition **LC25=1.2D+Di+WI0**

1	0.03717	0.18704	0.00149	0.00000	0.00010	0.00000
2	0.03588	0.00000	-0.00497	0.00000	0.00000	0.00000
3	-0.06847	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04826	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.04888	0.00000	-0.00179	0.00000	0.00000	0.00000
6	-0.00103	0.38391	0.00007	0.00000	0.00002	0.00000
17	0.04979	0.42224	-0.00538	0.00000	0.00007	0.00000
45	-0.10919	0.41908	-0.12281	0.00000	0.00006	0.00000
50	-0.00254	0.23577	0.12130	0.00000	-0.00011	0.00000
51	0.00385	0.00000	0.12490	0.00000	0.00000	0.00000
52	-0.00551	0.00000	-0.15167	0.00000	0.00000	0.00000
53	0.00204	0.00000	0.05937	0.00000	0.00000	0.00000
54	0.00126	0.00000	0.00644	0.00000	0.00000	0.00000
55	0.01934	0.79152	-0.00850	0.00000	-0.00015	0.00000
115	0.00845	0.05534	-0.00468	0.00000	0.00000	0.00000
116	0.00482	0.09184	0.07815	0.00000	0.00000	0.00000
131	0.00479	0.05323	-0.00950	0.00000	0.00000	0.00000
132	0.00717	0.07263	0.03360	0.00000	0.00000	0.00000
133	0.00826	0.05751	-0.00018	0.00000	0.00000	0.00000
134	0.00455	0.05661	-0.00192	0.00000	0.00000	0.00000
177	0.00091	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00683	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.00304	0.72136	0.13323	-0.80186	0.00000	0.73519
328	-0.00469	0.69020	0.14277	-2.63719	0.00000	0.03015
SUM	0.00000	4.31750	0.39100	-3.54466	0.00000	0.76534

Condition **LC26=1.2D+Di+WI30**

1	0.03728	0.18710	0.00149	0.00000	0.00010	0.00000
2	0.05504	0.00000	-0.00504	0.00000	0.00000	0.00000
3	-0.06525	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04826	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.01444	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00096	0.38417	0.00075	0.00000	0.00002	0.00000
17	0.05660	0.42299	-0.00843	0.00000	0.00010	0.00000
45	-0.10303	0.41801	-0.12382	0.00000	0.00000	0.00000
50	-0.00270	0.23575	0.11964	0.00000	-0.00005	0.00000
51	0.00765	0.00000	0.12282	0.00000	0.00000	0.00000
52	-0.00542	0.00000	-0.15106	0.00000	0.00000	0.00000
53	0.00207	0.00000	0.05889	0.00000	0.00000	0.00000
54	0.00458	0.00000	0.00094	0.00000	0.00000	0.00000
55	0.01624	0.79878	-0.01909	0.00000	-0.00016	0.00000
115	0.00845	0.05529	-0.00480	0.00000	0.00000	0.00000
116	0.00458	0.08461	0.06200	0.00000	0.00000	0.00000
131	0.00479	0.05326	-0.00944	0.00000	0.00000	0.00000
132	0.00717	0.07263	0.03360	0.00000	0.00000	0.00000
133	0.00827	0.05751	-0.00019	0.00000	0.00000	0.00000
134	0.00455	0.05664	-0.00186	0.00000	0.00000	0.00000
177	-0.00098	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00755	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.17782	0.75850	0.14728	-1.07062	0.00000	0.61114
328	0.00466	0.65306	0.02667	-2.65810	0.00000	-0.05848
SUM	0.24961	4.31750	0.24961	-3.83433	0.00002	0.55266

Condition **LC27=1.2D+Di+WI60**

1	0.03727	0.18708	0.00148	0.00000	0.00010	0.00000
2	0.05430	0.00000	-0.00506	0.00000	0.00000	0.00000
3	-0.06523	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04826	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.01727	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00108	0.38422	0.00088	0.00000	0.00002	0.00000
17	0.05688	0.42274	-0.00876	0.00000	0.00011	0.00000
45	-0.10330	0.41796	-0.12277	0.00000	-0.00002	0.00000
50	-0.00277	0.23586	0.11943	0.00000	-0.00003	0.00000
51	0.00887	0.00000	0.12395	0.00000	0.00000	0.00000
52	-0.00539	0.00000	-0.15115	0.00000	0.00000	0.00000
53	0.00209	0.00000	0.05853	0.00000	0.00000	0.00000
54	0.00572	0.00000	0.00270	0.00000	0.00000	0.00000
55	0.01318	0.80081	-0.02226	0.00000	-0.00015	0.00000
115	0.00847	0.05563	-0.00405	0.00000	0.00000	0.00000
116	0.00448	0.08240	0.05708	0.00000	0.00000	0.00000
131	0.00479	0.05326	-0.00944	0.00000	0.00000	0.00000
132	0.00717	0.07263	0.03360	0.00000	0.00000	0.00000
133	0.00827	0.05750	-0.00020	0.00000	0.00000	0.00000
134	0.00455	0.05664	-0.00187	0.00000	0.00000	0.00000
177	-0.00069	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00543	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.13025	0.74667	0.10797	-1.11099	0.00000	0.63466
328	0.00315	0.66489	0.01931	-2.74775	0.00000	-0.04292
SUM	0.19870	4.31750	0.19870	-3.96435	0.00003	0.59174

Condition **LC28=1.2D+Di+WI90**

1	0.03734	0.18707	0.00148	0.00000	0.00010	0.00000
2	0.06479	0.00000	-0.00516	0.00000	0.00000	0.00000
3	-0.06529	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04823	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.00663	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00230	0.38451	0.00178	0.00000	0.00001	0.00000
17	0.06182	0.42286	-0.01229	0.00000	0.00015	0.00000
45	-0.10087	0.41795	-0.12345	0.00000	-0.00010	0.00000
50	-0.00291	0.23559	0.11742	0.00000	0.00004	0.00000
51	0.01312	0.00000	0.11184	0.00000	0.00000	0.00000
52	-0.00531	0.00000	-0.15027	0.00000	0.00000	0.00000
53	0.00211	0.00000	0.05748	0.00000	0.00000	0.00000
54	0.00937	0.00000	-0.01205	0.00000	0.00000	0.00000
55	0.00154	0.81100	-0.03814	0.00000	-0.00015	0.00000
115	0.00849	0.05620	-0.00279	0.00000	0.00000	0.00000
116	0.00410	0.07147	0.03267	0.00000	0.00000	0.00000
131	0.00479	0.05328	-0.00940	0.00000	0.00000	0.00000
132	0.00717	0.07264	0.03361	0.00000	0.00000	0.00000
133	0.00827	0.05751	-0.00019	0.00000	0.00000	0.00000
134	0.00455	0.05665	-0.00184	0.00000	0.00000	0.00000
177	-0.00150	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.01044	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.15389	0.74720	0.05383	-1.32164	0.00000	0.59651
328	0.00805	0.66436	-0.05383	-2.90515	0.00000	-0.07154
SUM	0.24700	4.31750	0.00000	-4.33241	0.00006	0.52497

Condition **LC29=1.2D+Di+WI120**

1	0.03730	0.18700	0.00148	0.00000	0.00010	0.00000
2	0.06233	0.00000	-0.00525	0.00000	0.00000	0.00000
3	-0.06521	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04821	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.01693	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00313	0.38473	0.00259	0.00000	0.00000	0.00000
17	0.06383	0.42267	-0.01537	0.00000	0.00019	0.00000
45	-0.10124	0.41899	-0.12414	0.00000	-0.00014	0.00000
50	-0.00282	0.23514	0.11746	0.00000	0.00004	0.00000
51	0.01316	0.00000	0.09693	0.00000	0.00000	0.00000
52	-0.00534	0.00000	-0.15003	0.00000	0.00000	0.00000
53	0.00207	0.00000	0.05446	0.00000	0.00000	0.00000
54	0.00913	0.00000	-0.02653	0.00000	0.00000	0.00000
55	-0.01325	0.82000	-0.05304	0.00000	-0.00015	0.00000
115	0.00852	0.05691	-0.00123	0.00000	0.00000	0.00000
116	0.00375	0.06120	0.00972	0.00000	0.00000	0.00000
131	0.00479	0.05330	-0.00936	0.00000	0.00000	0.00000
132	0.00717	0.07264	0.03362	0.00000	0.00000	0.00000
133	0.00827	0.05749	-0.00022	0.00000	0.00000	0.00000
134	0.00455	0.05667	-0.00181	0.00000	0.00000	0.00000
177	-0.00176	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.01216	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.13158	0.73449	-0.01619	-1.49452	0.00000	0.58138
328	0.00962	0.67706	-0.11109	-3.09941	0.00000	-0.08410
SUM	0.19870	4.31750	-0.19870	-4.69955	0.00006	0.49728

Condition **LC30=1.2D+Di+WI150**

1	0.03731	0.18700	0.00148	0.00000	0.00010	0.00000
2	0.06450	0.00000	-0.00526	0.00000	0.00000	0.00000
3	-0.06523	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04821	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.01328	0.00000	-0.00178	0.00000	0.00000	0.00000
6	0.00341	0.38479	0.00276	0.00000	0.00000	0.00000
17	0.06481	0.42280	-0.01612	0.00000	0.00020	0.00000
45	-0.09993	0.41895	-0.12402	0.00000	-0.00014	0.00000
50	-0.00276	0.23515	0.11839	0.00000	0.00003	0.00000
51	0.01195	0.00000	0.09847	0.00000	0.00000	0.00000
52	-0.00536	0.00000	-0.15044	0.00000	0.00000	0.00000
53	0.00205	0.00000	0.05285	0.00000	0.00000	0.00000
54	0.00799	0.00000	-0.02387	0.00000	0.00000	0.00000
55	-0.01502	0.82168	-0.05579	0.00000	-0.00015	0.00000
115	0.00853	0.05694	-0.00116	0.00000	0.00000	0.00000
116	0.00369	0.05932	0.00551	0.00000	0.00000	0.00000
131	0.00479	0.05330	-0.00935	0.00000	0.00000	0.00000
132	0.00717	0.07264	0.03362	0.00000	0.00000	0.00000
133	0.00827	0.05749	-0.00022	0.00000	0.00000	0.00000
134	0.00455	0.05667	-0.00180	0.00000	0.00000	0.00000
177	-0.00222	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.01631	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.18110	0.74298	-0.02114	-1.59224	0.00000	0.54389
328	0.01137	0.66858	-0.15281	-3.13169	0.00000	-0.11123
SUM	0.24961	4.31750	-0.24961	-4.82955	0.00005	0.43266

Condition **LC31=1.2D+Di-WI0**

1	0.03721	0.18688	0.00148	0.00000	0.00010	0.00000
2	0.04967	0.00000	-0.00531	0.00000	0.00000	0.00000
3	-0.06825	0.00000	0.00441	0.00000	0.00000	0.00000
4	0.04817	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.04693	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00276	0.38487	0.00315	0.00000	0.00000	0.00000
17	0.06225	0.42186	-0.01701	0.00000	0.00022	0.00000
45	-0.10395	0.42052	-0.12310	0.00000	-0.00016	0.00000
50	-0.00264	0.23488	0.11944	0.00000	0.00001	0.00000
51	0.01041	0.00000	0.08843	0.00000	0.00000	0.00000
52	-0.00542	0.00000	-0.15076	0.00000	0.00000	0.00000
53	0.00200	0.00000	0.05012	0.00000	0.00000	0.00000
54	0.00645	0.00000	-0.03072	0.00000	0.00000	0.00000
55	-0.02850	0.82665	-0.06481	0.00000	-0.00013	0.00000
115	0.00856	0.05797	0.00112	0.00000	0.00000	0.00000
116	0.00344	0.05302	-0.00854	0.00000	0.00000	0.00000
131	0.00479	0.05329	-0.00936	0.00000	0.00000	0.00000
132	0.00717	0.07265	0.03364	0.00000	0.00000	0.00000
133	0.00826	0.05748	-0.00024	0.00000	0.00000	0.00000
134	0.00455	0.05666	-0.00182	0.00000	0.00000	0.00000
177	-0.00091	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00682	0.03961	0.00000	-0.05281	0.00000	0.00000
327	0.00303	0.69772	-0.13325	-1.62715	0.00000	0.63226
328	0.00470	0.71384	-0.14275	-3.38288	0.00000	-0.05133
SUM	0.00000	4.31750	-0.39100	-5.11565	0.00005	0.58093

Condition **LC32=1.2D+Di-WI30**

1	0.03713	0.18684	0.00148	0.00000	0.00010	0.00000
2	0.03209	0.00000	-0.00524	0.00000	0.00000	0.00000
3	-0.07319	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04815	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.08119	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00046	0.38463	0.00248	0.00000	0.00001	0.00000
17	0.05537	0.42111	-0.01396	0.00000	0.00019	0.00000
45	-0.10998	0.42158	-0.12212	0.00000	-0.00010	0.00000
50	-0.00248	0.23491	0.12111	0.00000	-0.00005	0.00000
51	0.00662	0.00000	0.09053	0.00000	0.00000	0.00000
52	-0.00551	0.00000	-0.15138	0.00000	0.00000	0.00000
53	0.00196	0.00000	0.05061	0.00000	0.00000	0.00000
54	0.00314	0.00000	-0.02522	0.00000	0.00000	0.00000
55	-0.02523	0.81937	-0.05421	0.00000	-0.00012	0.00000
115	0.00855	0.05802	0.00125	0.00000	0.00000	0.00000
116	0.00369	0.06024	0.00760	0.00000	0.00000	0.00000
131	0.00479	0.05326	-0.00945	0.00000	0.00000	0.00000
132	0.00717	0.07265	0.03364	0.00000	0.00000	0.00000
133	0.00826	0.05750	-0.00021	0.00000	0.00000	0.00000
134	0.00454	0.05663	-0.00189	0.00000	0.00000	0.00000
177	0.00098	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00754	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.17782	0.66076	-0.14728	-1.35894	0.00000	0.75651
328	-0.00465	0.75079	-0.02667	-3.36294	0.00000	0.03717
SUM	-0.24961	4.31750	-0.24961	-4.82749	0.00002	0.79368

Condition **LC33=1.2D+Di-WI60**

1	0.03714	0.18686	0.00148	0.00000	0.00010	0.00000
2	0.03252	0.00000	-0.00522	0.00000	0.00000	0.00000
3	-0.07288	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04816	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.07839	0.00000	-0.00179	0.00000	0.00000	0.00000
6	0.00040	0.38458	0.00234	0.00000	0.00001	0.00000
17	0.05511	0.42136	-0.01363	0.00000	0.00018	0.00000
45	-0.10974	0.42163	-0.12316	0.00000	-0.00008	0.00000
50	-0.00241	0.23480	0.12131	0.00000	-0.00007	0.00000
51	0.00540	0.00000	0.08939	0.00000	0.00000	0.00000
52	-0.00555	0.00000	-0.15129	0.00000	0.00000	0.00000
53	0.00195	0.00000	0.05097	0.00000	0.00000	0.00000
54	0.00200	0.00000	-0.02698	0.00000	0.00000	0.00000
55	-0.02220	0.81735	-0.05105	0.00000	-0.00013	0.00000
115	0.00854	0.05768	0.00050	0.00000	0.00000	0.00000
116	0.00379	0.06245	0.01253	0.00000	0.00000	0.00000
131	0.00479	0.05326	-0.00945	0.00000	0.00000	0.00000
132	0.00717	0.07265	0.03364	0.00000	0.00000	0.00000
133	0.00826	0.05750	-0.00021	0.00000	0.00000	0.00000
134	0.00454	0.05664	-0.00188	0.00000	0.00000	0.00000
177	0.00069	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00543	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.13025	0.67252	-0.10797	-1.31858	0.00000	0.73298
328	-0.00314	0.73904	-0.01931	-3.27380	0.00000	0.02170
SUM	-0.19870	4.31750	-0.19870	-4.69799	0.00001	0.75468

Condition **LC34=1.2D+Di-WI90**

1	0.03710	0.18688	0.00148	0.00000	0.00010	0.00000
2	0.02371	0.00000	-0.00513	0.00000	0.00000	0.00000
3	-0.07461	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04813	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.08882	0.00000	-0.00180	0.00000	0.00000	0.00000
6	-0.00116	0.38429	0.00145	0.00000	0.00001	0.00000
17	0.05011	0.42123	-0.01010	0.00000	0.00014	0.00000
45	-0.11203	0.42163	-0.12252	0.00000	0.00000	0.00000
50	-0.00227	0.23506	0.12332	0.00000	-0.00014	0.00000
51	0.00115	0.00000	0.10154	0.00000	0.00000	0.00000
52	-0.00563	0.00000	-0.15217	0.00000	0.00000	0.00000
53	0.00192	0.00000	0.05202	0.00000	0.00000	0.00000
54	-0.00165	0.00000	-0.01224	0.00000	0.00000	0.00000
55	-0.01038	0.80714	-0.03515	0.00000	-0.00013	0.00000
115	0.00852	0.05711	-0.00075	0.00000	0.00000	0.00000
116	0.00417	0.07338	0.03694	0.00000	0.00000	0.00000
131	0.00479	0.05323	-0.00951	0.00000	0.00000	0.00000
132	0.00717	0.07265	0.03364	0.00000	0.00000	0.00000
133	0.00826	0.05751	-0.00019	0.00000	0.00000	0.00000
134	0.00454	0.05662	-0.00192	0.00000	0.00000	0.00000
177	0.00150	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.01043	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.15390	0.67194	-0.05383	-1.10797	0.00000	0.77117
328	-0.00803	0.73962	0.05383	-3.11694	0.00000	0.05036
SUM	-0.24700	4.31750	0.00000	-4.33052	-0.00002	0.82153

Condition **LC35=1.2D+Di-WI120**

1	0.03711	0.18694	0.00148	0.00000	0.00010	0.00000
2	0.02470	0.00000	-0.00504	0.00000	0.00000	0.00000
3	-0.07312	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04821	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.07871	0.00000	-0.00180	0.00000	0.00000	0.00000
6	-0.00170	0.38406	0.00063	0.00000	0.00002	0.00000
17	0.04816	0.42142	-0.00702	0.00000	0.00010	0.00000
45	-0.11178	0.42060	-0.12179	0.00000	0.00004	0.00000
50	-0.00235	0.23551	0.12328	0.00000	-0.00014	0.00000
51	0.00111	0.00000	0.11642	0.00000	0.00000	0.00000
52	-0.00559	0.00000	-0.15240	0.00000	0.00000	0.00000
53	0.00197	0.00000	0.05503	0.00000	0.00000	0.00000
54	-0.00141	0.00000	0.00224	0.00000	0.00000	0.00000
55	0.00425	0.79816	-0.02026	0.00000	-0.00013	0.00000
115	0.00849	0.05640	-0.00231	0.00000	0.00000	0.00000
116	0.00451	0.08365	0.05988	0.00000	0.00000	0.00000
131	0.00479	0.05322	-0.00953	0.00000	0.00000	0.00000
132	0.00717	0.07264	0.03362	0.00000	0.00000	0.00000
133	0.00826	0.05751	-0.00018	0.00000	0.00000	0.00000
134	0.00454	0.05661	-0.00193	0.00000	0.00000	0.00000
177	0.00176	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.01215	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.13160	0.68456	0.01617	-0.93487	0.00000	0.78623
328	-0.00958	0.72700	0.11111	-2.92234	0.00000	0.06296
SUM	-0.19870	4.31750	0.19870	-3.96282	-0.00002	0.84919

Condition **LC36=1.2D+Di-WI150**

1	0.03711	0.18695	0.00148	0.00000	0.00010	0.00000
2	0.02283	0.00000	-0.00502	0.00000	0.00000	0.00000
3	-0.07344	0.00000	0.00440	0.00000	0.00000	0.00000
4	0.04821	0.00000	-0.00332	0.00000	0.00000	0.00000
5	-0.08233	0.00000	-0.00180	0.00000	0.00000	0.00000
6	-0.00204	0.38401	0.00046	0.00000	0.00002	0.00000
17	0.04717	0.42130	-0.00627	0.00000	0.00009	0.00000
45	-0.11306	0.42064	-0.12192	0.00000	0.00004	0.00000
50	-0.00242	0.23550	0.12236	0.00000	-0.00013	0.00000
51	0.00231	0.00000	0.11489	0.00000	0.00000	0.00000
52	-0.00557	0.00000	-0.15200	0.00000	0.00000	0.00000
53	0.00199	0.00000	0.05665	0.00000	0.00000	0.00000
54	-0.00027	0.00000	-0.00042	0.00000	0.00000	0.00000
55	0.00605	0.79647	-0.01751	0.00000	-0.00013	0.00000
115	0.00848	0.05637	-0.00238	0.00000	0.00000	0.00000
116	0.00457	0.08553	0.06409	0.00000	0.00000	0.00000
131	0.00479	0.05322	-0.00954	0.00000	0.00000	0.00000
132	0.00717	0.07264	0.03362	0.00000	0.00000	0.00000
133	0.00826	0.05751	-0.00018	0.00000	0.00000	0.00000
134	0.00454	0.05660	-0.00195	0.00000	0.00000	0.00000
177	0.00221	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.01629	0.03961	0.00000	-0.05281	0.00000	0.00000
327	-0.18114	0.67602	0.02111	-0.83699	0.00000	0.82369
328	-0.01131	0.73554	0.15284	-2.88972	0.00000	0.09008
SUM	-0.24961	4.31750	0.24961	-3.83232	-0.00001	0.91376

Condition **LC37=0.9D**

1	0.01243	0.06520	0.00039	0.00000	0.00003	0.00000
2	0.01286	0.00000	-0.00150	0.00000	0.00000	0.00000
3	-0.02306	0.00000	0.00134	0.00000	0.00000	0.00000
4	0.01648	0.00000	-0.00110	0.00000	0.00000	0.00000
5	-0.01398	0.00000	-0.00045	0.00000	0.00000	0.00000
6	0.00060	0.12419	0.00079	0.00000	0.00000	0.00000
17	0.02770	0.14899	-0.00540	0.00000	0.00008	0.00000
45	-0.04716	0.16507	-0.05031	0.00000	-0.00002	0.00000
50	-0.00094	0.09463	0.05105	0.00000	-0.00002	0.00000
51	0.00239	0.00000	0.04059	0.00000	0.00000	0.00000
52	-0.00207	0.00000	-0.06207	0.00000	0.00000	0.00000
53	0.00083	0.00000	0.02359	0.00000	0.00000	0.00000
54	0.00179	0.00000	-0.00427	0.00000	0.00000	0.00000
55	-0.00033	0.34980	-0.01875	0.00000	-0.00006	0.00000
115	0.00299	0.01930	0.00011	0.00000	0.00000	0.00000
116	0.00122	0.02796	0.01989	0.00000	0.00000	0.00000
131	0.00162	0.01794	-0.00293	0.00000	0.00000	0.00000
132	0.00239	0.02418	0.01094	0.00000	0.00000	0.00000
133	0.00275	0.01956	0.00062	0.00000	0.00000	0.00000
134	0.00149	0.01811	-0.00254	0.00000	0.00000	0.00000
177	0.00000	0.02970	0.00000	-0.03960	0.00000	0.00000
178	0.00000	0.02970	0.00000	-0.03960	0.00000	0.00000
327	0.00000	0.27849	0.00000	-0.44012	0.00000	0.27937
328	0.00000	0.26767	0.00000	-1.02944	0.00000	-0.02789
SUM	0.00000	1.68049	0.00000	-1.54877	0.00001	0.25148

Condition **LC38=1.2D**

1	0.01658	0.08694	0.00053	0.00000	0.00004	0.00000
2	0.01715	0.00000	-0.00201	0.00000	0.00000	0.00000
3	-0.03075	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02198	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.01864	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00080	0.16559	0.00105	0.00000	0.00000	0.00000
17	0.03693	0.19865	-0.00720	0.00000	0.00010	0.00000
45	-0.06288	0.22009	-0.06708	0.00000	-0.00003	0.00000
50	-0.00126	0.12618	0.06807	0.00000	-0.00003	0.00000
51	0.00319	0.00000	0.05412	0.00000	0.00000	0.00000
52	-0.00276	0.00000	-0.08276	0.00000	0.00000	0.00000
53	0.00110	0.00000	0.03146	0.00000	0.00000	0.00000
54	0.00239	0.00000	-0.00570	0.00000	0.00000	0.00000
55	-0.00045	0.46640	-0.02499	0.00000	-0.00008	0.00000
115	0.00398	0.02574	0.00015	0.00000	0.00000	0.00000
116	0.00163	0.03728	0.02651	0.00000	0.00000	0.00000
131	0.00217	0.02391	-0.00391	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01459	0.00000	0.00000	0.00000
133	0.00367	0.02608	0.00083	0.00000	0.00000	0.00000
134	0.00198	0.02414	-0.00339	0.00000	0.00000	0.00000
177	0.00000	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00000	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.00000	0.37127	0.00000	-0.58732	0.00000	0.37246
328	0.00000	0.35694	0.00000	-1.37344	0.00000	-0.03730
SUM	0.00000	2.24066	0.00000	-2.06638	0.00001	0.33516

Condition **LC41=1.2D+WL0**

1	0.01657	0.08696	0.00053	0.00000	0.00004	0.00000
2	0.01521	0.00000	-0.00196	0.00000	0.00000	0.00000
3	-0.03079	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02199	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.01893	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00028	0.16546	0.00063	0.00000	0.00001	0.00000
17	0.03520	0.19869	-0.00557	0.00000	0.00008	0.00000
45	-0.06362	0.21990	-0.06710	0.00000	0.00000	0.00000
50	-0.00125	0.12629	0.06827	0.00000	-0.00005	0.00000
51	0.00233	0.00000	0.05881	0.00000	0.00000	0.00000
52	-0.00277	0.00000	-0.08286	0.00000	0.00000	0.00000
53	0.00111	0.00000	0.03277	0.00000	0.00000	0.00000
54	0.00171	0.00000	-0.00099	0.00000	0.00000	0.00000
55	0.00618	0.46154	-0.01720	0.00000	-0.00008	0.00000
115	0.00397	0.02538	-0.00064	0.00000	0.00000	0.00000
116	0.00182	0.04264	0.03849	0.00000	0.00000	0.00000
131	0.00216	0.02391	-0.00393	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02609	0.00084	0.00000	0.00000	0.00000
134	0.00198	0.02414	-0.00340	0.00000	0.00000	0.00000
177	0.00021	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00196	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.00132	0.37462	0.04021	-0.46243	0.00000	0.38677
328	-0.00086	0.35359	0.04379	-1.26101	0.00000	-0.02578
SUM	0.00000	2.24066	0.11500	-1.82906	0.00000	0.36100

Condition **LC42=1.2D+WL30**

1	0.01659	0.08698	0.00053	0.00000	0.00004	0.00000
2	0.02003	0.00000	-0.00198	0.00000	0.00000	0.00000
3	-0.02954	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02216	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.00966	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00092	0.16552	0.00081	0.00000	0.00001	0.00000
17	0.03709	0.19889	-0.00642	0.00000	0.00009	0.00000
45	-0.06192	0.21961	-0.06735	0.00000	-0.00002	0.00000
50	-0.00129	0.12629	0.06788	0.00000	-0.00003	0.00000
51	0.00328	0.00000	0.05843	0.00000	0.00000	0.00000
52	-0.00275	0.00000	-0.08272	0.00000	0.00000	0.00000
53	0.00111	0.00000	0.03258	0.00000	0.00000	0.00000
54	0.00254	0.00000	-0.00224	0.00000	0.00000	0.00000
55	0.00521	0.46357	-0.02018	0.00000	-0.00008	0.00000
115	0.00397	0.02537	-0.00065	0.00000	0.00000	0.00000
116	0.00175	0.04062	0.03397	0.00000	0.00000	0.00000
131	0.00217	0.02392	-0.00389	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02608	0.00082	0.00000	0.00000	0.00000
134	0.00198	0.02415	-0.00338	0.00000	0.00000	0.00000
177	-0.00031	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00234	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.05492	0.38617	0.04548	-0.54300	0.00000	0.34954
328	0.00147	0.34205	0.00826	-1.26578	0.00000	-0.05232
SUM	0.07425	2.24066	0.07425	-1.91439	0.00001	0.29722

Condition **LC43=1.2D+WL60**

1	0.01659	0.08697	0.00053	0.00000	0.00004	0.00000
2	0.01990	0.00000	-0.00198	0.00000	0.00000	0.00000
3	-0.02964	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02216	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.01056	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00094	0.16554	0.00086	0.00000	0.00001	0.00000
17	0.03718	0.19883	-0.00655	0.00000	0.00009	0.00000
45	-0.06200	0.21960	-0.06705	0.00000	-0.00002	0.00000
50	-0.00130	0.12632	0.06782	0.00000	-0.00003	0.00000
51	0.00363	0.00000	0.05876	0.00000	0.00000	0.00000
52	-0.00274	0.00000	-0.08274	0.00000	0.00000	0.00000
53	0.00112	0.00000	0.03248	0.00000	0.00000	0.00000
54	0.00286	0.00000	-0.00174	0.00000	0.00000	0.00000
55	0.00425	0.46419	-0.02113	0.00000	-0.00008	0.00000
115	0.00397	0.02546	-0.00047	0.00000	0.00000	0.00000
116	0.00172	0.03995	0.03248	0.00000	0.00000	0.00000
131	0.00217	0.02392	-0.00389	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02608	0.00082	0.00000	0.00000	0.00000
134	0.00198	0.02415	-0.00338	0.00000	0.00000	0.00000
177	-0.00019	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00152	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.03617	0.38163	0.02997	-0.55840	0.00000	0.35857
328	0.00091	0.34658	0.00539	-1.30007	0.00000	-0.04639
SUM	0.05445	2.24066	0.05445	-1.96409	0.00001	0.31218

Condition **LC44=1.2D+WL90**

1	0.01660	0.08697	0.00053	0.00000	0.00004	0.00000
2	0.02202	0.00000	-0.00201	0.00000	0.00000	0.00000
3	-0.02925	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02215	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.00831	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00133	0.16561	0.00109	0.00000	0.00000	0.00000
17	0.03847	0.19885	-0.00747	0.00000	0.00010	0.00000
45	-0.06154	0.21961	-0.06714	0.00000	-0.00004	0.00000
50	-0.00135	0.12625	0.06724	0.00000	-0.00001	0.00000
51	0.00487	0.00000	0.05543	0.00000	0.00000	0.00000
52	-0.00271	0.00000	-0.08250	0.00000	0.00000	0.00000
53	0.00113	0.00000	0.03222	0.00000	0.00000	0.00000
54	0.00394	0.00000	-0.00572	0.00000	0.00000	0.00000
55	0.00103	0.46690	-0.02538	0.00000	-0.00008	0.00000
115	0.00398	0.02561	-0.00013	0.00000	0.00000	0.00000
116	0.00162	0.03704	0.02597	0.00000	0.00000	0.00000
131	0.00217	0.02393	-0.00387	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02607	0.00081	0.00000	0.00000	0.00000
134	0.00198	0.02416	-0.00336	0.00000	0.00000	0.00000
177	-0.00007	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00191	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.04053	0.38179	0.01984	-0.59835	0.00000	0.35560
328	-0.00066	0.34643	-0.00994	-1.33039	0.00000	-0.04923
SUM	0.06290	2.24066	0.00990	-2.03435	0.00002	0.30637

Condition **LC45=1.2D+WL120**

1	0.01660	0.08695	0.00052	0.00000	0.00004	0.00000
2	0.02197	0.00000	-0.00203	0.00000	0.00000	0.00000
3	-0.02958	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02215	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.01046	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00150	0.16568	0.00131	0.00000	0.00000	0.00000
17	0.03905	0.19881	-0.00830	0.00000	0.00011	0.00000
45	-0.06149	0.21988	-0.06738	0.00000	-0.00005	0.00000
50	-0.00132	0.12613	0.06731	0.00000	-0.00001	0.00000
51	0.00478	0.00000	0.05151	0.00000	0.00000	0.00000
52	-0.00272	0.00000	-0.08246	0.00000	0.00000	0.00000
53	0.00111	0.00000	0.03133	0.00000	0.00000	0.00000
54	0.00378	0.00000	-0.00951	0.00000	0.00000	0.00000
55	-0.00279	0.46932	-0.02939	0.00000	-0.00008	0.00000
115	0.00399	0.02581	0.00031	0.00000	0.00000	0.00000
116	0.00153	0.03427	0.01979	0.00000	0.00000	0.00000
131	0.00217	0.02393	-0.00387	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02607	0.00081	0.00000	0.00000	0.00000
134	0.00198	0.02416	-0.00336	0.00000	0.00000	0.00000
177	-0.00047	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00335	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.03667	0.37827	-0.00441	-0.66506	0.00000	0.34398
328	0.00251	0.34995	-0.03095	-1.39820	0.00000	-0.05768
SUM	0.05445	2.24066	-0.05445	-2.16888	0.00002	0.28629

Condition **LC46=1.2D+WL150**

1	0.01660	0.08695	0.00052	0.00000	0.00004	0.00000
2	0.02256	0.00000	-0.00204	0.00000	0.00000	0.00000
3	-0.02949	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02215	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.00934	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00161	0.16569	0.00137	0.00000	0.00000	0.00000
17	0.03939	0.19888	-0.00857	0.00000	0.00012	0.00000
45	-0.06111	0.21987	-0.06735	0.00000	-0.00005	0.00000
50	-0.00130	0.12613	0.06757	0.00000	-0.00001	0.00000
51	0.00444	0.00000	0.05195	0.00000	0.00000	0.00000
52	-0.00273	0.00000	-0.08257	0.00000	0.00000	0.00000
53	0.00111	0.00000	0.03087	0.00000	0.00000	0.00000
54	0.00345	0.00000	-0.00875	0.00000	0.00000	0.00000
55	-0.00333	0.46982	-0.03021	0.00000	-0.00008	0.00000
115	0.00399	0.02578	0.00024	0.00000	0.00000	0.00000
116	0.00151	0.03372	0.01856	0.00000	0.00000	0.00000
131	0.00217	0.02393	-0.00386	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01458	0.00000	0.00000	0.00000
133	0.00367	0.02607	0.00080	0.00000	0.00000	0.00000
134	0.00199	0.02416	-0.00335	0.00000	0.00000	0.00000
177	-0.00067	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00501	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.05605	0.38155	-0.00645	-0.70238	0.00000	0.32968
328	0.00337	0.34667	-0.04729	-1.41064	0.00000	-0.06800
SUM	0.07425	2.24066	-0.07425	-2.21863	0.00002	0.26168

Condition **LC47=1.2D-WL0**

1	0.01658	0.08692	0.00052	0.00000	0.00004	0.00000
2	0.01909	0.00000	-0.00205	0.00000	0.00000	0.00000
3	-0.03071	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02197	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.01835	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00133	0.16572	0.00148	0.00000	0.00000	0.00000
17	0.03866	0.19860	-0.00882	0.00000	0.00012	0.00000
45	-0.06215	0.22027	-0.06707	0.00000	-0.00006	0.00000
50	-0.00127	0.12606	0.06786	0.00000	-0.00002	0.00000
51	0.00406	0.00000	0.04944	0.00000	0.00000	0.00000
52	-0.00275	0.00000	-0.08267	0.00000	0.00000	0.00000
53	0.00110	0.00000	0.03014	0.00000	0.00000	0.00000
54	0.00307	0.00000	-0.01040	0.00000	0.00000	0.00000
55	-0.00708	0.47126	-0.03278	0.00000	-0.00008	0.00000
115	0.00400	0.02609	0.00094	0.00000	0.00000	0.00000
116	0.00144	0.03191	0.01452	0.00000	0.00000	0.00000
131	0.00217	0.02392	-0.00389	0.00000	0.00000	0.00000
132	0.00319	0.03224	0.01459	0.00000	0.00000	0.00000
133	0.00367	0.02608	0.00082	0.00000	0.00000	0.00000
134	0.00198	0.02415	-0.00338	0.00000	0.00000	0.00000
177	-0.00021	0.03960	0.00000	-0.05281	0.00000	0.00000
178	-0.00196	0.03960	0.00000	-0.05281	0.00000	0.00000
327	0.00132	0.36792	-0.04021	-0.71216	0.00000	0.35813
328	0.00086	0.36030	-0.04379	-1.48568	0.00000	-0.04884
SUM	0.00000	2.24066	-0.11500	-2.30345	0.00002	0.30929

Condition **LC48=1.2D-WL30**

1	0.01656	0.08690	0.00052	0.00000	0.00004	0.00000
2	0.01427	0.00000	-0.00203	0.00000	0.00000	0.00000
3	-0.03186	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02164	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.02755	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00068	0.16565	0.00129	0.00000	0.00000	0.00000
17	0.03676	0.19841	-0.00797	0.00000	0.00011	0.00000
45	-0.06384	0.22057	-0.06681	0.00000	-0.00004	0.00000
50	-0.00123	0.12607	0.06825	0.00000	-0.00003	0.00000
51	0.00310	0.00000	0.04982	0.00000	0.00000	0.00000
52	-0.00277	0.00000	-0.08281	0.00000	0.00000	0.00000
53	0.00109	0.00000	0.03033	0.00000	0.00000	0.00000
54	0.00225	0.00000	-0.00915	0.00000	0.00000	0.00000
55	-0.00610	0.46922	-0.02981	0.00000	-0.00007	0.00000
115	0.00400	0.02610	0.00096	0.00000	0.00000	0.00000
116	0.00151	0.03393	0.01905	0.00000	0.00000	0.00000
131	0.00216	0.02390	-0.00394	0.00000	0.00000	0.00000
132	0.00319	0.03225	0.01461	0.00000	0.00000	0.00000
133	0.00367	0.02609	0.00086	0.00000	0.00000	0.00000
134	0.00198	0.02414	-0.00340	0.00000	0.00000	0.00000
177	0.00031	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00234	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.05492	0.35639	-0.04548	-0.63165	0.00000	0.39538
328	-0.00146	0.37182	-0.00826	-1.48100	0.00000	-0.02231
SUM	-0.07425	2.24066	-0.07425	-2.21826	0.00001	0.37308

Condition **LC49=1.2D-WL60**

1	0.01656	0.08690	0.00052	0.00000	0.00004	0.00000
2	0.01440	0.00000	-0.00203	0.00000	0.00000	0.00000
3	-0.03178	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02167	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.02666	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00066	0.16564	0.00125	0.00000	0.00000	0.00000
17	0.03667	0.19847	-0.00784	0.00000	0.00011	0.00000
45	-0.06377	0.22058	-0.06711	0.00000	-0.00004	0.00000
50	-0.00121	0.12604	0.06831	0.00000	-0.00004	0.00000
51	0.00276	0.00000	0.04949	0.00000	0.00000	0.00000
52	-0.00278	0.00000	-0.08279	0.00000	0.00000	0.00000
53	0.00108	0.00000	0.03043	0.00000	0.00000	0.00000
54	0.00192	0.00000	-0.00965	0.00000	0.00000	0.00000
55	-0.00515	0.46861	-0.02885	0.00000	-0.00008	0.00000
115	0.00399	0.02601	0.00077	0.00000	0.00000	0.00000
116	0.00154	0.03460	0.02054	0.00000	0.00000	0.00000
131	0.00216	0.02390	-0.00393	0.00000	0.00000	0.00000
132	0.00319	0.03225	0.01460	0.00000	0.00000	0.00000
133	0.00367	0.02609	0.00086	0.00000	0.00000	0.00000
134	0.00198	0.02414	-0.00340	0.00000	0.00000	0.00000
177	0.00019	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00152	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.03616	0.36092	-0.02997	-0.61624	0.00000	0.38635
328	-0.00090	0.36729	-0.00539	-1.44676	0.00000	-0.02823
SUM	-0.05445	2.24066	-0.05445	-2.16862	0.00001	0.35812

Condition **LC50=1.2D-WL90**

1	0.01655	0.08691	0.00053	0.00000	0.00004	0.00000
2	0.01227	0.00000	-0.00200	0.00000	0.00000	0.00000
3	-0.03213	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02159	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.02886	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00026	0.16556	0.00101	0.00000	0.00000	0.00000
17	0.03538	0.19845	-0.00692	0.00000	0.00010	0.00000
45	-0.06422	0.22056	-0.06702	0.00000	-0.00002	0.00000
50	-0.00117	0.12610	0.06889	0.00000	-0.00006	0.00000
51	0.00151	0.00000	0.05282	0.00000	0.00000	0.00000
52	-0.00280	0.00000	-0.08303	0.00000	0.00000	0.00000
53	0.00107	0.00000	0.03069	0.00000	0.00000	0.00000
54	0.00084	0.00000	-0.00568	0.00000	0.00000	0.00000
55	-0.00193	0.46589	-0.02460	0.00000	-0.00008	0.00000
115	0.00399	0.02586	0.00043	0.00000	0.00000	0.00000
116	0.00164	0.03752	0.02705	0.00000	0.00000	0.00000
131	0.00216	0.02389	-0.00396	0.00000	0.00000	0.00000
132	0.00319	0.03225	0.01460	0.00000	0.00000	0.00000
133	0.00367	0.02610	0.00087	0.00000	0.00000	0.00000
134	0.00198	0.02413	-0.00342	0.00000	0.00000	0.00000
177	0.00007	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00191	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.04053	0.36076	-0.01984	-0.57630	0.00000	0.38933
328	0.00066	0.36745	0.00994	-1.41648	0.00000	-0.02539
SUM	-0.06290	2.24066	-0.00990	-2.09840	0.00000	0.36394

Condition **LC51=1.2D-WL120**

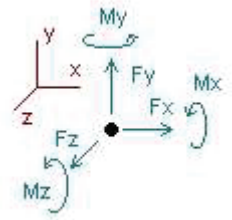
1	0.01656	0.08693	0.00053	0.00000	0.00004	0.00000
2	0.01232	0.00000	-0.00198	0.00000	0.00000	0.00000
3	-0.03184	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02168	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.02675	0.00000	-0.00060	0.00000	0.00000	0.00000
6	0.00010	0.16550	0.00079	0.00000	0.00001	0.00000
17	0.03481	0.19849	-0.00609	0.00000	0.00009	0.00000
45	-0.06427	0.22030	-0.06678	0.00000	-0.00001	0.00000
50	-0.00120	0.12623	0.06882	0.00000	-0.00006	0.00000
51	0.00160	0.00000	0.05674	0.00000	0.00000	0.00000
52	-0.00279	0.00000	-0.08307	0.00000	0.00000	0.00000
53	0.00109	0.00000	0.03158	0.00000	0.00000	0.00000
54	0.00100	0.00000	-0.00189	0.00000	0.00000	0.00000
55	0.00189	0.46347	-0.02059	0.00000	-0.00008	0.00000
115	0.00398	0.02566	-0.00001	0.00000	0.00000	0.00000
116	0.00173	0.04028	0.03323	0.00000	0.00000	0.00000
131	0.00216	0.02389	-0.00395	0.00000	0.00000	0.00000
132	0.00319	0.03225	0.01460	0.00000	0.00000	0.00000
133	0.00367	0.02610	0.00086	0.00000	0.00000	0.00000
134	0.00198	0.02413	-0.00341	0.00000	0.00000	0.00000
177	0.00047	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00335	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.03667	0.36427	0.00441	-0.50957	0.00000	0.40094
328	-0.00251	0.36394	0.03095	-1.34865	0.00000	-0.01693
SUM	-0.05445	2.24066	0.05445	-1.96383	0.00000	0.38401

Condition **LC52=1.2D-WL150**

1	0.01655	0.08693	0.00053	0.00000	0.00004	0.00000
2	0.01174	0.00000	-0.00197	0.00000	0.00000	0.00000
3	-0.03192	0.00000	0.00179	0.00000	0.00000	0.00000
4	0.02165	0.00000	-0.00147	0.00000	0.00000	0.00000
5	-0.02786	0.00000	-0.00060	0.00000	0.00000	0.00000
6	-0.00001	0.16548	0.00074	0.00000	0.00001	0.00000
17	0.03446	0.19842	-0.00582	0.00000	0.00009	0.00000
45	-0.06465	0.22031	-0.06682	0.00000	-0.00001	0.00000
50	-0.00121	0.12623	0.06856	0.00000	-0.00005	0.00000
51	0.00195	0.00000	0.05630	0.00000	0.00000	0.00000
52	-0.00278	0.00000	-0.08296	0.00000	0.00000	0.00000
53	0.00109	0.00000	0.03204	0.00000	0.00000	0.00000
54	0.00133	0.00000	-0.00264	0.00000	0.00000	0.00000
55	0.00243	0.46298	-0.01977	0.00000	-0.00008	0.00000
115	0.00398	0.02569	0.00006	0.00000	0.00000	0.00000
116	0.00174	0.04083	0.03446	0.00000	0.00000	0.00000
131	0.00216	0.02389	-0.00396	0.00000	0.00000	0.00000
132	0.00319	0.03225	0.01460	0.00000	0.00000	0.00000
133	0.00367	0.02610	0.00087	0.00000	0.00000	0.00000
134	0.00198	0.02412	-0.00343	0.00000	0.00000	0.00000
177	0.00067	0.03960	0.00000	-0.05281	0.00000	0.00000
178	0.00501	0.03960	0.00000	-0.05281	0.00000	0.00000
327	-0.05605	0.36099	0.00645	-0.47223	0.00000	0.41523
328	-0.00336	0.36723	0.04729	-1.33618	0.00000	-0.00661
SUM	-0.07425	2.24066	0.07425	-1.91402	0.00000	0.40862

Envelope for nodal reactions

Note.- **Ic** is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150
LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

Node		Forces						Moments					
		Fx [Kip]	lc	Fy [Kip]	lc	Fz [Kip]	lc	Mx [Kip*ft]	lc	My [Kip*ft]	lc	Mz [Kip*ft]	lc
1	Max	0.044	LC6	0.187	LC26	0.003	LC1	0.00000	LC1	0.00164	LC6	0.00000	LC1
	Min	-0.011	LC24	0.027	LC24	-0.002	LC20	0.00000	LC1	-0.00154	LC13	0.00000	LC1
2	Max	0.543	LC6	0.000	LC1	0.051	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.349	LC24	0.000	LC1	-0.054	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
3	Max	0.003	LC15	0.000	LC1	0.060	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.177	LC11	0.000	LC1	-0.057	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
4	Max	0.048	LC26	0.000	LC1	0.069	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.192	LC21	0.000	LC1	-0.071	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
5	Max	1.246	LC17	0.000	LC1	0.066	LC21	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-1.167	LC11	0.000	LC1	-0.067	LC3	0.00000	LC1	0.00000	LC1	0.00000	LC1
6	Max	0.120	LC2	0.385	LC31	0.210	LC2	0.00000	LC1	0.00008	LC11	0.00000	LC1
	Min	-0.132	LC20	-0.022	LC24	-0.208	LC20	0.00000	LC1	-0.00011	LC5	0.00000	LC1
17	Max	0.128	LC2	0.423	LC26	0.280	LC13	0.00000	LC1	0.00077	LC7	0.00000	LC1
	Min	-0.057	LC20	0.029	LC24	-0.293	LC7	0.00000	LC1	-0.00062	LC13	0.00000	LC1
45	Max	0.047	LC18	0.422	LC34	-0.017	LC20	0.00000	LC1	0.00200	LC13	0.00000	LC1
	Min	-0.118	LC12	0.132	LC15	-0.182	LC1	0.00000	LC1	-0.00202	LC7	0.00000	LC1
50	Max	0.001	LC24	0.236	LC27	0.123	LC34	0.00000	LC1	0.00175	LC17	0.00000	LC1
	Min	-0.003	LC6	0.089	LC21	0.016	LC16	0.00000	LC1	-0.00172	LC11	0.00000	LC1
51	Max	0.109	LC5	0.000	LC1	0.542	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.101	LC23	0.000	LC1	-0.253	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
52	Max	0.059	LC16	0.000	LC1	-0.043	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.064	LC10	0.000	LC1	-0.152	LC35	0.00000	LC1	0.00000	LC1	0.00000	LC1
53	Max	0.072	LC4	0.000	LC1	0.098	LC4	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.070	LC22	0.000	LC1	-0.130	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.102	LC4	0.000	LC1	0.314	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.097	LC22	0.000	LC1	-0.250	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
55	Max	0.356	LC1	0.827	LC31	0.443	LC13	0.00000	LC1	0.00034	LC24	0.00000	LC1
	Min	-0.357	LC7	0.066	LC13	-0.482	LC7	0.00000	LC1	-0.00060	LC6	0.00000	LC1
115	Max	0.082	LC5	0.079	LC12	0.159	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.075	LC23	-0.032	LC18	-0.156	LC18	0.00000	LC1	0.00000	LC1	0.00000	LC1
116	Max	0.083	LC3	0.339	LC1	0.738	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.080	LC21	-0.272	LC19	-0.689	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
131	Max	0.080	LC4	0.099	LC2	0.205	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.076	LC22	-0.058	LC18	-0.215	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
132	Max	0.081	LC4	0.073	LC32	0.123	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.075	LC22	-0.006	LC20	-0.097	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
133	Max	0.082	LC4	0.093	LC12	0.191	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.075	LC22	-0.045	LC20	-0.185	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.080	LC4	0.091	LC2	0.187	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.076	LC22	-0.049	LC20	-0.194	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1

177	Max	0.064	LC15	0.040	LC25	0.000	LC1	-0.03960	LC13	0.00000	LC1	0.00000	LC1
	Min	-0.064	LC9	0.030	LC13	0.000	LC1	-0.05281	LC25	0.00000	LC1	0.00000	LC1
178	Max	0.144	LC24	0.040	LC25	0.000	LC1	-0.03960	LC13	0.00000	LC1	0.00000	LC1
	Min	-0.145	LC6	0.030	LC13	0.000	LC1	-0.05281	LC25	0.00000	LC1	0.00000	LC1
327	Max	1.634	LC4	0.783	LC2	1.403	LC14	3.39735	LC13	0.00000	LC1	1.56991	LC12
	Min	-1.635	LC22	-0.122	LC20	-1.402	LC8	-4.38126	LC7	0.00000	LC1	-0.92284	LC18
328	Max	0.278	LC5	0.758	LC8	1.461	LC12	2.51498	LC13	0.00000	LC1	0.83401	LC24
	Min	-0.274	LC23	-0.144	LC14	-1.458	LC18	-4.73245	LC7	0.00000	LC1	-0.90325	LC6

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

CHECK CONNECTION CAPACITY (Worst Case) → BETA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = 1/2" U-Bolt

Allowable Tensile Load =

F_{Tall} = 12061 lbs.

Allowable Shear Load =

F_{Vall}= 9048 lbs.

TENSILE FORCES

Reaction **F =** 783 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 1635 lbs. (See Bentley Output)
Reactions in Z direction: 1403 lbs. (See Bentley Output)

Resultant: 2154 lbs.

No. of Supports = 1
No. of Bolts / Support = 1

Tension Design Load /Bolts =

f_t= 783.00 lbs. < 12061 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

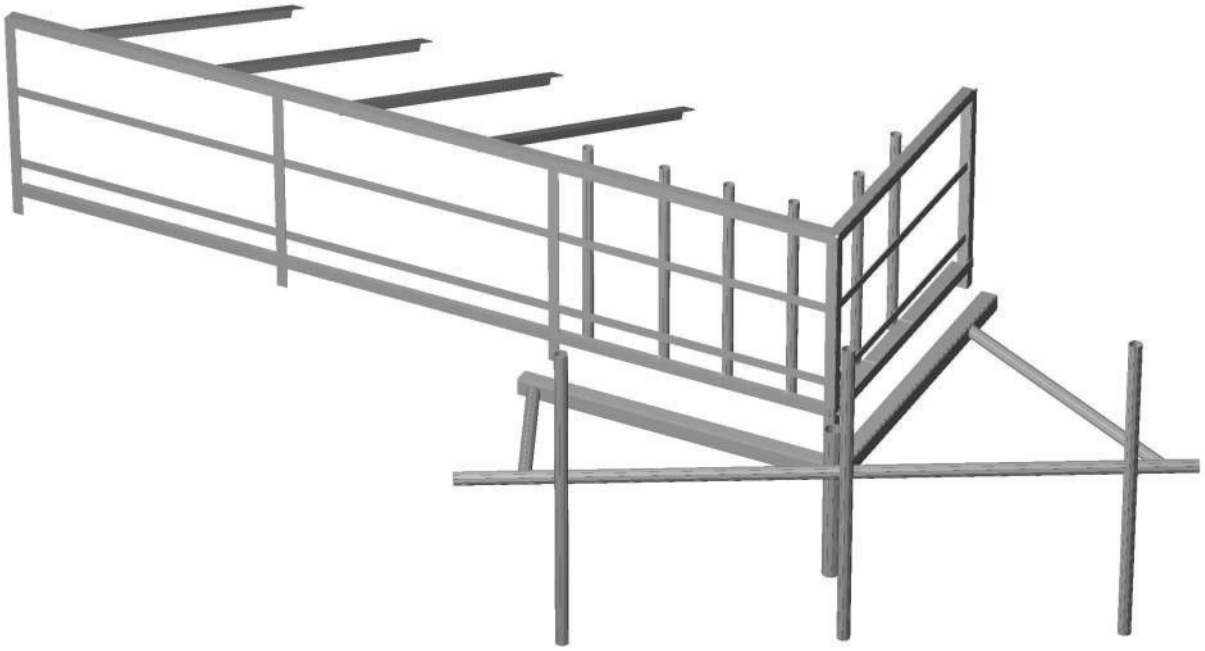
f_v= 2154.45 lbs. < 9048 lbs. **Therefore, OK !**

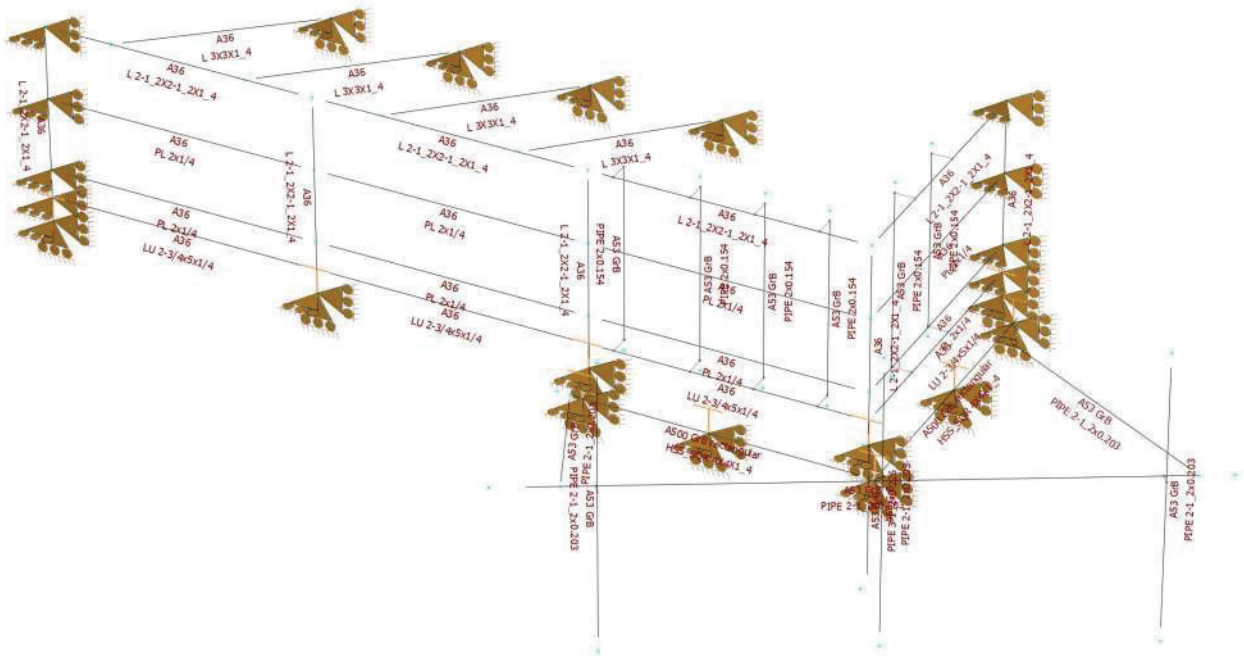
CHECK COMBINED TENSION AND SHEAR

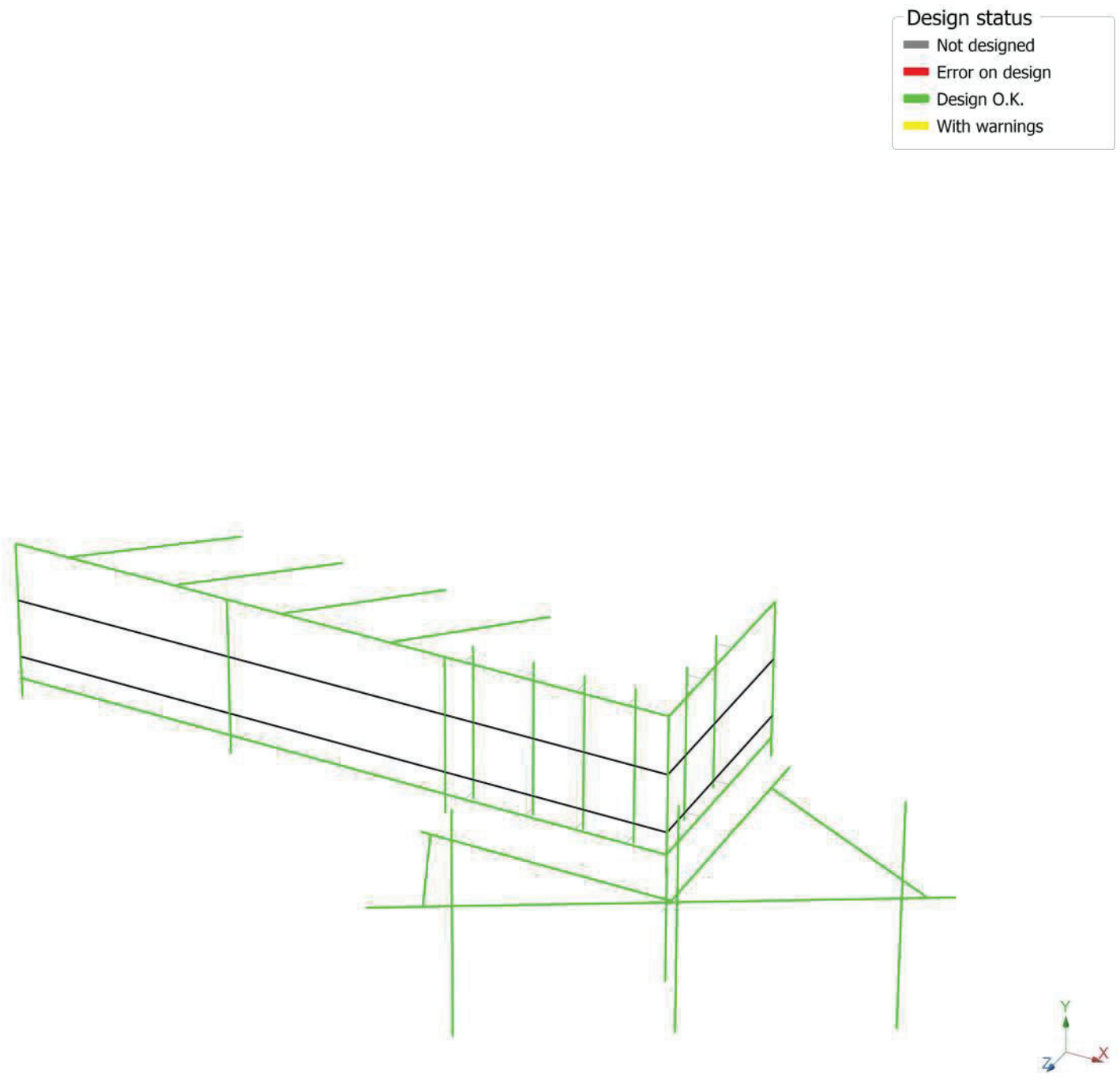
f_t / F_T	+	f_v / F_V	≤	1.0			
0.065	+	0.238	=	0.303	<	1.0	**Therefore, OK !**

HUDSON
Design Group LLC

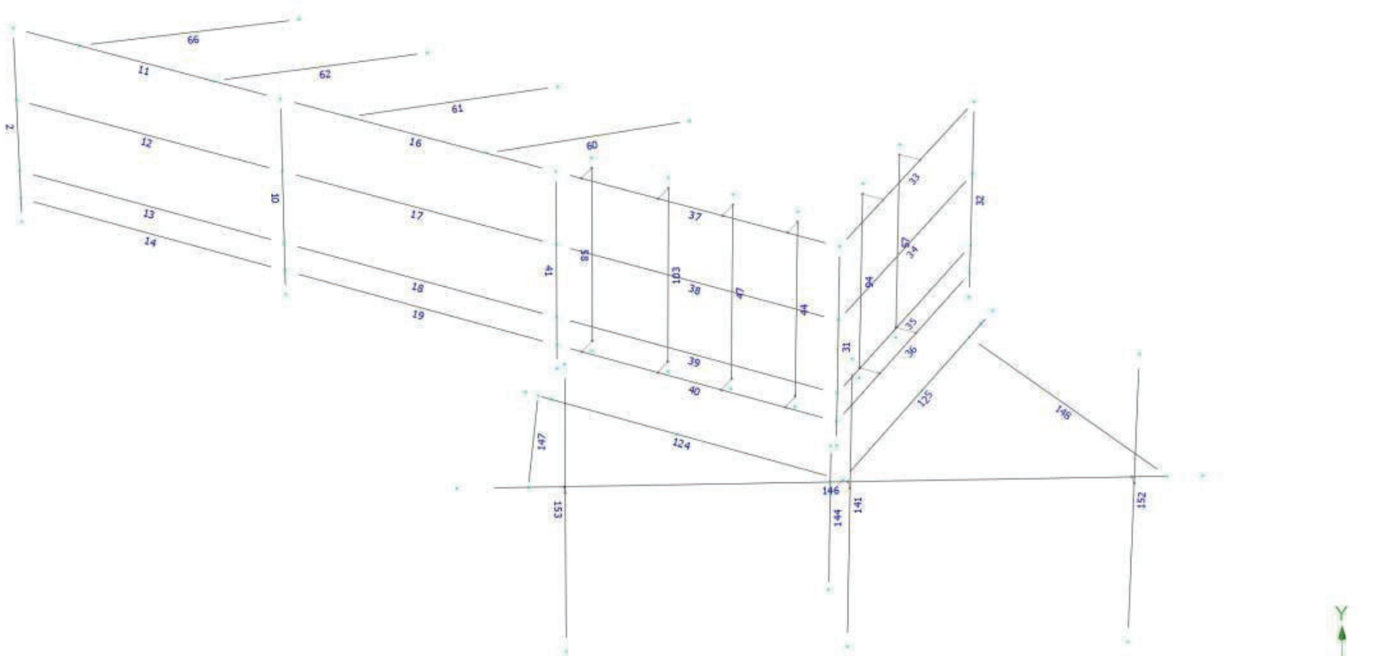
Gamma Sector
Calculations


Y
X
Z


A36
L 3X3X1_4
A36
L 2-1_2X2-1_2X1_4
A36
PL 2x1/4
A36
LU 2-3/4x5x1/4
A53 GrB
PIPE 2-1_2x0.203
A53 GrB
PIPE 2x0.154
Y
X
Z


Design status
Not designed
Error on design
Design O.K.
With warnings
Y
X
Z

Current Date: 3/24/2022 2:22 PM
Units system: English



Current Date: 3/24/2022 2:22 PM
Units system: English

Load data

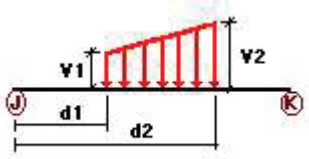
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes
	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes

	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes
	62	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
	94	z	-0.006	-0.006	0.00	No	100.00	Yes
	103	z	-0.006	-0.006	0.00	No	100.00	Yes
	124	z	-0.014	-0.014	0.00	No	100.00	Yes
	141	z	-0.013	-0.013	0.00	No	100.00	Yes
	144	z	-0.01	-0.01	0.00	No	100.00	Yes
	146	z	-0.007	-0.007	0.00	No	100.00	Yes
	147	z	-0.007	-0.007	0.00	No	100.00	Yes
	148	z	-0.007	-0.007	0.00	No	100.00	Yes
	152	z	-0.013	-0.013	0.00	No	100.00	Yes
	153	z	-0.013	-0.013	0.00	No	100.00	Yes
W30	2	z	-0.011	-0.011	0.00	No	100.00	Yes
	10	z	-0.011	-0.011	0.00	No	100.00	Yes
	11	z	-0.011	-0.011	0.00	No	100.00	Yes
	12	z	-0.009	-0.009	0.00	No	100.00	Yes
	13	z	-0.009	-0.009	0.00	No	100.00	Yes
	14	z	-0.012	-0.012	0.00	No	100.00	Yes
	16	z	-0.011	-0.011	0.00	No	100.00	Yes
	17	z	-0.009	-0.009	0.00	No	100.00	Yes
	18	z	-0.009	-0.009	0.00	No	100.00	Yes
	19	z	-0.012	-0.012	0.00	No	100.00	Yes
	31	z	-0.011	-0.011	0.00	No	100.00	Yes
	32	z	-0.011	-0.011	0.00	No	100.00	Yes
	33	z	-0.011	-0.011	0.00	No	100.00	Yes
	34	z	-0.009	-0.009	0.00	No	100.00	Yes
	35	z	-0.009	-0.009	0.00	No	100.00	Yes
	36	z	-0.012	-0.012	0.00	No	100.00	Yes
	37	z	-0.011	-0.011	0.00	No	100.00	Yes
	38	z	-0.009	-0.009	0.00	No	100.00	Yes
	39	z	-0.009	-0.009	0.00	No	100.00	Yes
	40	z	-0.012	-0.012	0.00	No	100.00	Yes
	41	z	-0.011	-0.011	0.00	No	100.00	Yes
	44	z	-0.006	-0.006	0.00	No	100.00	Yes
	47	z	-0.006	-0.006	0.00	No	100.00	Yes
	57	z	-0.006	-0.006	0.00	No	100.00	Yes
	58	z	-0.006	-0.006	0.00	No	100.00	Yes
	60	z	-0.014	-0.014	0.00	No	100.00	Yes
	61	z	-0.014	-0.014	0.00	No	100.00	Yes
	62	z	-0.014	-0.014	0.00	No	100.00	Yes
	66	z	-0.014	-0.014	0.00	No	100.00	Yes
	94	z	-0.006	-0.006	0.00	No	100.00	Yes
	103	z	-0.006	-0.006	0.00	No	100.00	Yes
	124	z	-0.014	-0.014	0.00	No	100.00	Yes
	125	z	-0.014	-0.014	0.00	No	100.00	Yes
	141	z	-0.013	-0.013	0.00	No	100.00	Yes
	144	z	-0.01	-0.01	0.00	No	100.00	Yes
	146	z	-0.007	-0.007	0.00	No	100.00	Yes

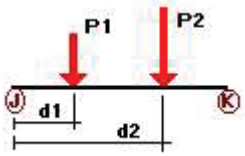
	147	z	-0.007	-0.007	0.00	No	100.00	Yes
	148	z	-0.007	-0.007	0.00	No	100.00	Yes
	152	z	-0.013	-0.013	0.00	No	100.00	Yes
	153	z	-0.013	-0.013	0.00	No	100.00	Yes
W60	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	94	x	-0.006	-0.006	0.00	No	100.00	Yes
	103	x	-0.006	-0.006	0.00	No	100.00	Yes
	124	x	-0.014	-0.014	0.00	No	100.00	Yes
	125	x	-0.014	-0.014	0.00	No	100.00	Yes
	141	x	-0.013	-0.013	0.00	No	100.00	Yes
	144	x	-0.01	-0.01	0.00	No	100.00	Yes
	146	x	-0.007	-0.007	0.00	No	100.00	Yes
	147	x	-0.007	-0.007	0.00	No	100.00	Yes
	148	x	-0.007	-0.007	0.00	No	100.00	Yes
	152	x	-0.013	-0.013	0.00	No	100.00	Yes
	153	x	-0.013	-0.013	0.00	No	100.00	Yes
W90	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	94	x	-0.006	-0.006	0.00	No	100.00	Yes
	103	x	-0.006	-0.006	0.00	No	100.00	Yes

	125	x	-0.014	-0.014	0.00	No	100.00	Yes
	141	x	-0.013	-0.013	0.00	No	100.00	Yes
	144	x	-0.01	-0.01	0.00	No	100.00	Yes
	146	x	-0.007	-0.007	0.00	No	100.00	Yes
	147	x	-0.007	-0.007	0.00	No	100.00	Yes
	148	x	-0.007	-0.007	0.00	No	100.00	Yes
	152	x	-0.013	-0.013	0.00	No	100.00	Yes
	153	x	-0.013	-0.013	0.00	No	100.00	Yes
W120	2	x	-0.011	-0.011	0.00	No	100.00	Yes
	10	x	-0.011	-0.011	0.00	No	100.00	Yes
	11	x	-0.011	-0.011	0.00	No	100.00	Yes
	12	x	-0.009	-0.009	0.00	No	100.00	Yes
	13	x	-0.009	-0.009	0.00	No	100.00	Yes
	14	x	-0.012	-0.012	0.00	No	100.00	Yes
	16	x	-0.011	-0.011	0.00	No	100.00	Yes
	17	x	-0.009	-0.009	0.00	No	100.00	Yes
	18	x	-0.009	-0.009	0.00	No	100.00	Yes
	19	x	-0.012	-0.012	0.00	No	100.00	Yes
	31	x	-0.011	-0.011	0.00	No	100.00	Yes
	32	x	-0.011	-0.011	0.00	No	100.00	Yes
	33	x	-0.011	-0.011	0.00	No	100.00	Yes
	34	x	-0.009	-0.009	0.00	No	100.00	Yes
	35	x	-0.009	-0.009	0.00	No	100.00	Yes
	36	x	-0.012	-0.012	0.00	No	100.00	Yes
	37	x	-0.011	-0.011	0.00	No	100.00	Yes
	38	x	-0.009	-0.009	0.00	No	100.00	Yes
	39	x	-0.009	-0.009	0.00	No	100.00	Yes
	40	x	-0.012	-0.012	0.00	No	100.00	Yes
	41	x	-0.011	-0.011	0.00	No	100.00	Yes
	44	x	-0.006	-0.006	0.00	No	100.00	Yes
	47	x	-0.006	-0.006	0.00	No	100.00	Yes
	57	x	-0.006	-0.006	0.00	No	100.00	Yes
	58	x	-0.006	-0.006	0.00	No	100.00	Yes
	60	x	-0.014	-0.014	0.00	No	100.00	Yes
	61	x	-0.014	-0.014	0.00	No	100.00	Yes
	62	x	-0.014	-0.014	0.00	No	100.00	Yes
	66	x	-0.014	-0.014	0.00	No	100.00	Yes
	94	x	-0.006	-0.006	0.00	No	100.00	Yes
	103	x	-0.006	-0.006	0.00	No	100.00	Yes
	124	x	-0.014	-0.014	0.00	No	100.00	Yes
	125	x	-0.014	-0.014	0.00	No	100.00	Yes
	141	x	-0.013	-0.013	0.00	No	100.00	Yes
	144	x	-0.01	-0.01	0.00	No	100.00	Yes
	146	x	-0.007	-0.007	0.00	No	100.00	Yes
	147	x	-0.007	-0.007	0.00	No	100.00	Yes
	148	x	-0.007	-0.007	0.00	No	100.00	Yes
	152	x	-0.013	-0.013	0.00	No	100.00	Yes
	153	x	-0.013	-0.013	0.00	No	100.00	Yes
W150	2	z	0.011	0.011	0.00	No	100.00	Yes
	10	z	0.011	0.011	0.00	No	100.00	Yes
	11	z	0.011	0.011	0.00	No	100.00	Yes
	12	z	0.009	0.009	0.00	No	100.00	Yes
	13	z	0.009	0.009	0.00	No	100.00	Yes
	14	z	0.012	0.012	0.00	No	100.00	Yes
	16	z	0.011	0.011	0.00	No	100.00	Yes
	17	z	0.009	0.009	0.00	No	100.00	Yes
	18	z	0.009	0.009	0.00	No	100.00	Yes
	19	z	0.012	0.012	0.00	No	100.00	Yes
	31	z	0.011	0.011	0.00	No	100.00	Yes
	32	z	0.011	0.011	0.00	No	100.00	Yes

	33	z	0.011	0.011	0.00	No	100.00	Yes
	34	z	0.009	0.009	0.00	No	100.00	Yes
	35	z	0.009	0.009	0.00	No	100.00	Yes
	36	z	0.012	0.012	0.00	No	100.00	Yes
	37	z	0.011	0.011	0.00	No	100.00	Yes
	38	z	0.009	0.009	0.00	No	100.00	Yes
	39	z	0.009	0.009	0.00	No	100.00	Yes
	40	z	0.012	0.012	0.00	No	100.00	Yes
	41	z	0.011	0.011	0.00	No	100.00	Yes
	44	z	0.006	0.006	0.00	No	100.00	Yes
	47	z	0.006	0.006	0.00	No	100.00	Yes
	57	z	0.006	0.006	0.00	No	100.00	Yes
	58	z	0.006	0.006	0.00	No	100.00	Yes
	60	z	0.014	0.014	0.00	No	100.00	Yes
	61	z	0.014	0.014	0.00	No	100.00	Yes
	62	z	0.014	0.014	0.00	No	100.00	Yes
	66	z	0.014	0.014	0.00	No	100.00	Yes
	94	z	0.006	0.006	0.00	No	100.00	Yes
	103	z	0.006	0.006	0.00	No	100.00	Yes
	124	z	0.014	0.014	0.00	No	100.00	Yes
	125	z	0.014	0.014	0.00	No	100.00	Yes
	141	z	0.013	0.013	0.00	No	100.00	Yes
	144	z	0.01	0.01	0.00	No	100.00	Yes
	146	z	0.007	0.007	0.00	No	100.00	Yes
	147	z	0.007	0.007	0.00	No	100.00	Yes
	148	z	0.007	0.007	0.00	No	100.00	Yes
	152	z	0.013	0.013	0.00	No	100.00	Yes
	153	z	0.013	0.013	0.00	No	100.00	Yes
Di	2	y	-0.007	-0.007	0.00	No	100.00	Yes
	10	y	-0.007	-0.007	0.00	No	100.00	Yes
	11	y	-0.007	-0.007	0.00	No	100.00	Yes
	12	y	-0.005	-0.005	0.00	No	100.00	Yes
	13	y	-0.005	-0.005	0.00	No	100.00	Yes
	14	y	-0.01	-0.01	0.00	No	100.00	Yes
	16	y	-0.007	-0.007	0.00	No	100.00	Yes
	17	y	-0.005	-0.005	0.00	No	100.00	Yes
	18	y	-0.005	-0.005	0.00	No	100.00	Yes
	19	y	-0.01	-0.01	0.00	No	100.00	Yes
	31	y	-0.007	-0.007	0.00	No	100.00	Yes
	32	y	-0.007	-0.007	0.00	No	100.00	Yes
	33	y	-0.007	-0.007	0.00	No	100.00	Yes
	34	y	-0.005	-0.005	0.00	No	100.00	Yes
	35	y	-0.005	-0.005	0.00	No	100.00	Yes
	36	y	-0.01	-0.01	0.00	No	100.00	Yes
	37	y	-0.007	-0.007	0.00	No	100.00	Yes
	38	y	-0.005	-0.005	0.00	No	100.00	Yes
	39	y	-0.005	-0.005	0.00	No	100.00	Yes
	40	y	-0.01	-0.01	0.00	No	100.00	Yes
	41	y	-0.007	-0.007	0.00	No	100.00	Yes
	44	y	-0.005	-0.005	0.00	No	100.00	Yes
	47	y	-0.005	-0.005	0.00	No	100.00	Yes
	57	y	-0.005	-0.005	0.00	No	100.00	Yes
	58	y	-0.005	-0.005	0.00	No	100.00	Yes
	60	y	-0.008	-0.008	0.00	No	100.00	Yes
	61	y	-0.008	-0.008	0.00	No	100.00	Yes
	62	y	-0.008	-0.008	0.00	No	100.00	Yes
	66	y	-0.008	-0.008	0.00	No	100.00	Yes
	94	y	-0.005	-0.005	0.00	No	100.00	Yes
	103	y	-0.005	-0.005	0.00	No	100.00	Yes
	141	y	-0.006	-0.006	0.00	No	100.00	Yes

144	y	-0.008	-0.008	0.00	No	100.00	Yes
146	y	-0.006	-0.006	0.00	No	100.00	Yes
147	y	-0.008	-0.008	0.00	No	100.00	Yes
148	y	-0.008	-0.008	0.00	No	100.00	Yes
152	y	-0.006	-0.006	0.00	No	100.00	Yes
153	y	-0.006	-0.006	0.00	No	100.00	Yes

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	44	y	-0.06	2.00	No
	47	y	-0.06	2.00	No
	57	y	-0.06	2.00	No
	58	y	-0.073	2.00	No
	94	y	-0.06	2.00	No
	103	y	-0.033	2.00	No
	141	y	-0.041	0.50	No
		y	-0.041	2.50	No
		y	-0.033	3.50	No
		y	-0.033	5.50	No
	152	y	-0.035	0.50	No
		y	-0.035	5.50	No
	153	y	-0.04	0.50	No
		y	-0.04	5.50	No
Wo	44	z	-0.088	2.00	No
	47	z	-0.119	2.00	No
	57	z	-0.072	2.00	No
	58	z	-0.086	2.00	No
	94	z	-0.072	2.00	No
	103	z	-0.049	2.00	No
	141	z	-0.088	0.50	No
		z	-0.088	2.50	No
		z	-0.091	3.50	No
		z	-0.091	5.50	No
	152	z	-0.276	0.50	No
		z	-0.276	5.50	No
	153	z	-0.276	0.50	No
		z	-0.276	5.50	No
W30	44	3	-0.079	2.00	No
	47	3	-0.108	2.00	No
	57	3	-0.078	2.00	No
	58	3	-0.079	2.00	No
	94	3	-0.078	2.00	No
	103	3	-0.049	2.00	No
	141	3	-0.081	0.50	No
		3	-0.081	2.50	No
		3	-0.079	3.50	No
		3	-0.079	5.50	No
	152	3	-0.238	0.50	No

		3	-0.238	5.50	No
	153	3	-0.238	0.50	No
		3	-0.238	5.50	No
W60	44	3	-0.063	2.00	No
	47	3	-0.084	2.00	No
	57	3	-0.112	2.00	No
	58	3	-0.067	2.00	No
	94	3	-0.112	2.00	No
	103	3	-0.049	2.00	No
	141	3	-0.067	0.50	No
		3	-0.067	2.50	No
		3	-0.056	3.50	No
		3	-0.056	5.50	No
	152	3	-0.161	0.50	No
		3	-0.161	5.50	No
	153	3	-0.161	0.50	No
		3	-0.161	5.50	No
W90	44	x	-0.054	2.00	No
	47	x	-0.072	2.00	No
	57	x	-0.119	2.00	No
	58	x	-0.061	2.00	No
	94	x	-0.119	2.00	No
	103	x	-0.049	2.00	No
	141	x	-0.06	0.50	No
		x	-0.06	2.50	No
		x	-0.044	3.50	No
		x	-0.044	5.50	No
	152	x	-0.122	0.50	No
		x	-0.122	5.50	No
	153	x	-0.122	0.50	No
		x	-0.122	5.50	No
W120	44	2	-0.063	2.00	No
	47	2	-0.084	2.00	No
	57	2	-0.112	2.00	No
	58	2	-0.067	2.00	No
	94	2	-0.112	2.00	No
	103	2	-0.049	2.00	No
	141	2	-0.067	0.50	No
		2	-0.067	2.50	No
		2	-0.056	3.50	No
		2	-0.056	5.50	No
	152	2	-0.161	0.50	No
		2	-0.161	5.50	No
	153	2	-0.161	0.50	No
		2	-0.161	5.50	No
W150	44	2	-0.079	2.00	No
	47	2	-0.108	2.00	No
	57	2	-0.078	2.00	No
	58	2	-0.079	2.00	No
	94	2	-0.078	2.00	No
	103	2	-0.049	2.00	No
	141	2	-0.081	0.50	No
		2	-0.081	2.50	No
		2	-0.079	3.50	No
		2	-0.079	5.50	No
	152	2	-0.238	0.50	No
		2	-0.238	5.50	No
	153	2	-0.238	0.50	No
		2	-0.238	5.50	No
Di	44	y	-0.039	2.00	No

	47	y	-0.052	2.00	No
	57	y	-0.052	2.00	No
	58	y	-0.039	2.00	No
	94	y	-0.052	2.00	No
	103	y	-0.033	2.00	No
	141	y	-0.039	0.50	No
		y	-0.039	2.50	No
		y	-0.037	3.50	No
		y	-0.037	5.50	No
	152	y	-0.104	0.50	No
		y	-0.104	5.50	No
	153	y	-0.104	0.50	No
		y	-0.104	5.50	No
WI0	44	z	-0.019	2.00	No
	47	z	-0.025	2.00	No
	57	z	-0.017	2.00	No
	58	z	-0.018	2.00	No
	94	z	-0.017	2.00	No
	103	z	-0.011	2.00	No
	141	z	-0.018	0.50	No
		z	-0.018	2.50	No
		z	-0.018	3.50	No
		z	-0.018	5.50	No
	152	z	-0.051	0.50	No
		z	-0.051	5.50	No
	153	z	-0.051	0.50	No
		z	-0.051	5.50	No
WI30	44	3	-0.017	2.00	No
	47	3	-0.023	2.00	No
	57	3	-0.016	2.00	No
	58	3	-0.017	2.00	No
	94	3	-0.016	2.00	No
	103	3	-0.011	2.00	No
	141	3	-0.017	0.50	No
		3	-0.017	2.50	No
		3	-0.016	3.50	No
		3	-0.016	5.50	No
	152	3	-0.045	0.50	No
		3	-0.045	5.50	No
	153	3	-0.045	0.50	No
		3	-0.045	5.50	No
WI60	44	3	-0.014	2.00	No
	47	3	-0.019	2.00	No
	57	3	-0.023	2.00	No
	58	3	-0.015	2.00	No
	94	3	-0.023	2.00	No
	103	3	-0.011	2.00	No
	141	3	-0.014	0.50	No
		3	-0.014	2.50	No
		3	-0.012	3.50	No
		3	-0.012	5.50	No
	152	3	-0.032	0.50	No
		3	-0.032	5.50	No
	153	3	-0.032	0.50	No
		3	-0.032	5.50	No
WI90	44	x	-0.013	2.00	No
	47	x	-0.017	2.00	No
	57	x	-0.025	2.00	No
	58	x	-0.014	2.00	No
	94	x	-0.025	2.00	No

	103	x	-0.011	2.00	No
	141	x	-0.013	0.50	No
		x	-0.013	2.50	No
		x	-0.01	3.50	No
		x	-0.01	5.50	No
	152	x	-0.026	0.50	No
		x	-0.026	5.50	No
	153	x	-0.026	0.50	No
		x	-0.026	5.50	No
WI120	44	2	-0.014	2.00	No
	47	2	-0.019	2.00	No
	57	2	-0.023	2.00	No
	58	2	-0.015	2.00	No
	94	2	-0.023	2.00	No
	103	2	-0.011	2.00	No
	141	2	-0.014	0.50	No
		2	-0.014	2.50	No
		2	-0.012	3.50	No
		2	-0.012	5.50	No
	152	2	-0.032	0.50	No
		2	-0.032	5.50	No
	153	2	-0.032	0.50	No
		2	-0.032	5.50	No
WI150	44	2	-0.017	2.00	No
	47	2	-0.023	2.00	No
	57	2	-0.016	2.00	No
	58	2	-0.017	2.00	No
	94	2	-0.016	2.00	No
	103	2	-0.011	2.00	No
	141	2	-0.017	0.50	No
		2	-0.017	2.50	No
		2	-0.016	3.50	No
		2	-0.016	5.50	No
	152	2	-0.045	0.50	No
		2	-0.045	5.50	No
	153	2	-0.045	0.50	No
		2	-0.045	5.50	No
WL0	44	z	-0.005	2.00	No
	47	z	-0.007	2.00	No
	57	z	-0.004	2.00	No
	58	z	-0.005	2.00	No
	94	z	-0.004	2.00	No
	103	z	-0.003	2.00	No
	141	z	-0.005	0.50	No
		z	-0.005	2.50	No
		z	-0.005	3.50	No
		z	-0.005	5.50	No
	152	z	-0.016	0.50	No
		z	-0.016	5.50	No
	153	z	-0.016	0.50	No
		z	-0.016	5.50	No
WL30	44	3	-0.005	2.00	No
	47	3	-0.006	2.00	No
	57	3	-0.004	2.00	No
	58	3	-0.005	2.00	No
	94	3	-0.004	2.00	No
	103	3	-0.003	2.00	No
	141	3	-0.005	0.50	No
		3	-0.005	2.50	No
		3	-0.005	3.50	No

		3	-0.005	5.50	No
	152	3	-0.014	0.50	No
		3	-0.014	5.50	No
	153	3	-0.014	0.50	No
		3	-0.014	5.50	No
WL60	44	3	-0.004	2.00	No
	47	3	-0.005	2.00	No
	57	3	-0.006	2.00	No
	58	3	-0.004	2.00	No
	94	3	-0.006	2.00	No
	103	3	-0.003	2.00	No
	141	3	-0.004	0.50	No
		3	-0.004	2.50	No
		3	-0.003	3.50	No
		3	-0.003	5.50	No
	152	3	-0.009	0.50	No
		3	-0.009	5.50	No
	153	3	-0.009	0.50	No
		3	-0.009	5.50	No
WL90	44	x	-0.003	2.00	No
	47	x	-0.004	2.00	No
	57	x	-0.007	2.00	No
	58	x	-0.004	2.00	No
	94	x	-0.007	2.00	No
	103	x	-0.003	2.00	No
	141	x	-0.004	0.50	No
		x	-0.004	2.50	No
		x	-0.003	3.50	No
		x	-0.003	5.50	No
	152	x	-0.007	0.50	No
		x	-0.007	5.50	No
	153	x	-0.007	0.50	No
		x	-0.007	5.50	No
WL120	44	2	-0.004	2.00	No
	47	2	-0.005	2.00	No
	57	2	-0.006	2.00	No
	58	2	-0.004	2.00	No
	94	2	-0.006	2.00	No
	103	2	-0.003	2.00	No
	141	2	-0.004	0.50	No
		2	-0.004	2.50	No
		2	-0.003	3.50	No
		2	-0.003	5.50	No
	152	2	-0.009	0.50	No
		2	-0.009	5.50	No
	153	2	-0.009	0.50	No
		2	-0.009	5.50	No
WL150	44	2	-0.005	2.00	No
	47	2	-0.006	2.00	No
	57	2	-0.004	2.00	No
	58	2	-0.005	2.00	No
	94	2	-0.004	2.00	No
	103	2	-0.003	2.00	No
	141	2	-0.005	0.50	No
		2	-0.005	2.50	No
		2	-0.005	3.50	No
		2	-0.005	5.50	No
	152	2	-0.014	0.50	No
		2	-0.014	5.50	No
	153	2	-0.014	0.50	No

	2	-0.014	5.50	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00

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Units system: English

Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150
LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	HSS_SQR 4X4X1_4	**124**	LC34 at 0.00%	**0.08**	**OK**	
		125	LC25 at 0.00%	0.07	OK	
	L 2-1_2X2-1_2X1_4	**2**	LC25 at 100.00%	0.04	OK	
		10	LC7 at 39.06%	0.14	OK	
		11	LC6 at 0.00%	0.13	OK	
		16	LC1 at 22.92%	**0.25**	**OK**	
		31	LC32 at 10.94%	0.13	OK	
		32	LC4 at 100.00%	0.09	OK	
		33	LC4 at 39.58%	0.21	OK	
		37	LC1 at 40.00%	0.20	OK	
		41	LC1 at 100.00%	0.17	OK	
	L 3X3X1_4	**60**	LC11 at 0.00%	0.12	OK	
		61	LC9 at 0.00%	**0.13**	**OK**	
		62	LC11 at 0.00%	0.12	OK	
		66	LC9 at 0.00%	0.12	OK	
	LU 2-3/4x5x1/4	**14**	LC6 at 100.00%	0.04	OK	
		19	LC6 at 0.00%	0.05	OK	
		36	LC8 at 0.00%	0.15	OK	
		40	LC7 at 100.00%	**0.16**	**OK**	
	PIPE 2-1_2x0.203	**141**	LC7 at 46.88%	0.24	OK	
		146	LC31 at 50.00%	0.43	OK	
		147	LC32 at 100.00%	0.16	OK	
		148	LC31 at 0.00%	0.25	OK	
		152	LC7 at 46.88%	0.51	OK	
		153	LC7 at 46.88%	**0.51**	**OK**	
	PIPE 2x0.154	**44**	LC1 at 50.00%	0.09	OK	
		47	LC1 at 50.00%	0.14	OK	
		57	LC4 at 50.00%	**0.16**	**OK**	
		58	LC1 at 50.00%	0.09	OK	
		94	LC4 at 50.00%	0.14	OK	
		103	LC1 at 50.00%	0.09	OK	
	PIPE 3-1_2x0.226	**144**	LC26 at 72.92%	**0.12**	**OK**	
	PL 2x1/4	**12**	LC6 at 100.00%	**0.47**	**With warnings**	
		13	LC2 at 100.00%	0.46	With warnings	
		17	LC7 at 100.00%	0.45	With warnings	
		18	LC6 at 0.00%	0.44	With warnings	
		34	LC10 at 0.00%	0.41	With warnings	
		35	LC9 at 0.00%	0.42	With warnings	
		38	LC2 at 0.00%	0.46	With warnings	
		39	LC2 at 0.00%	0.46	With warnings	

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Geometry data

GLOSSARY

Cb22, Cb33	: Moment gradient coefficients
Cm22, Cm33	: Coefficients applied to bending term in interaction formula
d0	: Tapered member section depth at J end of member
DJX	: Rigid end offset distance measured from J node in axis X
DJY	: Rigid end offset distance measured from J node in axis Y
DJZ	: Rigid end offset distance measured from J node in axis Z
DKX	: Rigid end offset distance measured from K node in axis X
DKY	: Rigid end offset distance measured from K node in axis Y
DKZ	: Rigid end offset distance measured from K node in axis Z
dL	: Tapered member section depth at K end of member
Ig factor	: Inertia reduction factor (Effective Inertia/Gross Inertia) for reinforced concrete members
K22	: Effective length factor about axis 2
K33	: Effective length factor about axis 3
L22	: Member length for calculation of axial capacity
L33	: Member length for calculation of axial capacity
LB pos	: Lateral unbraced length of the compression flange in the positive side of local axis 2
LB neg	: Lateral unbraced length of the compression flange in the negative side of local axis 2
RX	: Rotation about X
RY	: Rotation about Y
RZ	: Rotation about Z
TO	: 1 = Tension only member 0 = Normal member
TX	: Translation in X
TY	: Translation in Y
TZ	: Translation in Z

Nodes

Node	X [ft]	Y [ft]	Z [ft]	Rigid Floor
6	5.50	0.00	0.00	0
7	5.50	0.50	0.00	0
8	5.50	1.08	0.00	0
9	5.50	2.58	0.00	0
10	5.50	4.08	0.00	0
17	11.00	0.00	0.00	0
18	11.00	0.50	0.00	0
19	11.00	1.08	0.00	0
20	11.00	2.58	0.00	0
21	11.00	4.08	0.00	0
23	16.50	0.50	0.00	0
24	16.50	1.08	0.00	0
25	16.50	2.58	0.00	0
26	16.50	4.08	0.00	0
45	22.00	0.00	0.00	0
46	22.00	0.50	0.00	0
47	22.00	1.08	0.00	0
48	22.00	2.58	0.00	0
49	22.00	4.08	0.00	0
50	22.00	0.00	-5.50	0
51	22.00	0.50	-5.50	0
52	22.00	1.08	-5.50	0
53	22.00	2.58	-5.50	0

54	22.00	4.08	-5.50	0
55	16.50	0.00	0.00	0
62	21.00	4.29	-0.40	0
68	19.75	4.29	-0.40	0
102	21.60	0.29	-3.25	0
105	21.60	4.29	-3.25	0
107	17.00	4.29	-0.40	0
109	15.125	4.08	0.00	0
113	12.375	4.08	0.00	0
115	12.375	0.50	-8.00	0
116	15.125	0.50	-8.00	0
118	9.625	4.08	0.00	0
133	6.875	0.50	-8.00	0
134	9.625	0.50	-8.00	0
138	6.875	4.08	0.00	0
331	21.60	0.29	-1.75	0
332	21.60	4.29	-1.75	0
350	18.50	4.29	-0.40	0
406	16.50	-0.50	0.25	0
407	16.00	-0.50	0.25	0
409	19.00	-0.50	0.25	0
410	22.25	-0.50	0.25	0
411	22.25	-0.50	-6.00	0
414	22.25	-0.50	-3.00	0
442	22.6412	2.4167	0.7759	0
443	22.6412	-3.5833	0.7759	0
450	22.25	-0.50	0.75	0
451	22.25	0.50	0.75	0
452	22.25	-2.50	0.75	0
453	22.25	-0.25	0.75	0
458	27.946	-0.25	-2.3814	0
483	16.554	-0.25	3.8814	0
497	16.25	-0.50	0.25	0
499	17.639	-0.25	3.2849	0
517	27.4035	-0.25	-2.0832	0
518	22.25	-0.50	-5.50	0
519	22.25	-0.50	-5.00	0
523	26.981	2.4167	-1.6099	0
524	26.981	-3.5833	-1.6099	0
525	18.3014	2.4167	3.1617	0
526	18.3014	-3.5833	3.1617	0
61	21.00	0.29	-0.40	0
67	19.75	0.29	-0.40	0
349	18.50	0.29	-0.40	0
104	17.00	0.29	-0.40	0

Restraints

Node	TX	TY	TZ	RX	RY	RZ
6	1	1	1	0	1	0
7	1	0	1	0	0	0
8	1	0	1	0	0	0
9	1	0	1	0	0	0
10	1	0	1	0	0	0
17	1	1	1	0	1	0

45	1	1	1	0	1	0
50	1	1	1	0	1	0
51	1	0	1	0	0	0
52	1	0	1	0	0	0
53	1	0	1	0	0	0
54	1	0	1	0	0	0
55	1	1	1	0	1	0
115	1	1	1	0	0	0
116	1	1	1	0	0	0
133	1	1	1	0	0	0
134	1	1	1	0	0	0
406	1	1	1	0	1	0
409	1	1	1	0	1	0
410	1	1	1	0	1	0
414	1	1	1	0	1	0
518	1	1	1	0	1	0

Members

Member	NJ	NK	Description	Section	Material	d0 [in]	dL [in]	lg factor
2	6	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
10	17	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
11	21	10		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
12	9	20		PL 2x1/4	A36	0.00	0.00	0.00
13	8	19		PL 2x1/4	A36	0.00	0.00	0.00
14	7	18		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
16	26	21		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
17	20	25		PL 2x1/4	A36	0.00	0.00	0.00
18	19	24		PL 2x1/4	A36	0.00	0.00	0.00
19	18	23		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
31	45	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
32	50	54		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
33	54	49		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
34	48	53		PL 2x1/4	A36	0.00	0.00	0.00
35	47	52		PL 2x1/4	A36	0.00	0.00	0.00
36	46	51		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
37	49	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
38	25	48		PL 2x1/4	A36	0.00	0.00	0.00
39	24	47		PL 2x1/4	A36	0.00	0.00	0.00
40	23	46		LU 2-3/4x5x1/4	A36	0.00	0.00	0.00
41	55	26		L 2-1_2X2-1_2X1_4	A36	0.00	0.00	0.00
44	62	61		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
47	68	67		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
57	105	102		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
58	107	104		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
60	109	116		L 3X3X1_4	A36	0.00	0.00	0.00
61	113	115		L 3X3X1_4	A36	0.00	0.00	0.00
62	118	134		L 3X3X1_4	A36	0.00	0.00	0.00
66	138	133		L 3X3X1_4	A36	0.00	0.00	0.00
94	332	331		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
103	350	349		PIPE 2x0.154	A53 GrB	0.00	0.00	0.00
124	410	407		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
125	410	411		HSS_SQR 4X4X1_4	A500 GrB rectangular	0.00	0.00	0.00
141	442	443		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
144	452	451		PIPE 3-1_2x0.226	A53 GrB	0.00	0.00	0.00

146	483	458		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
147	499	497		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
148	519	517		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
152	523	524		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00
153	525	526		PIPE 2-1_2x0.203	A53 GrB	0.00	0.00	0.00

Orientation of local axes

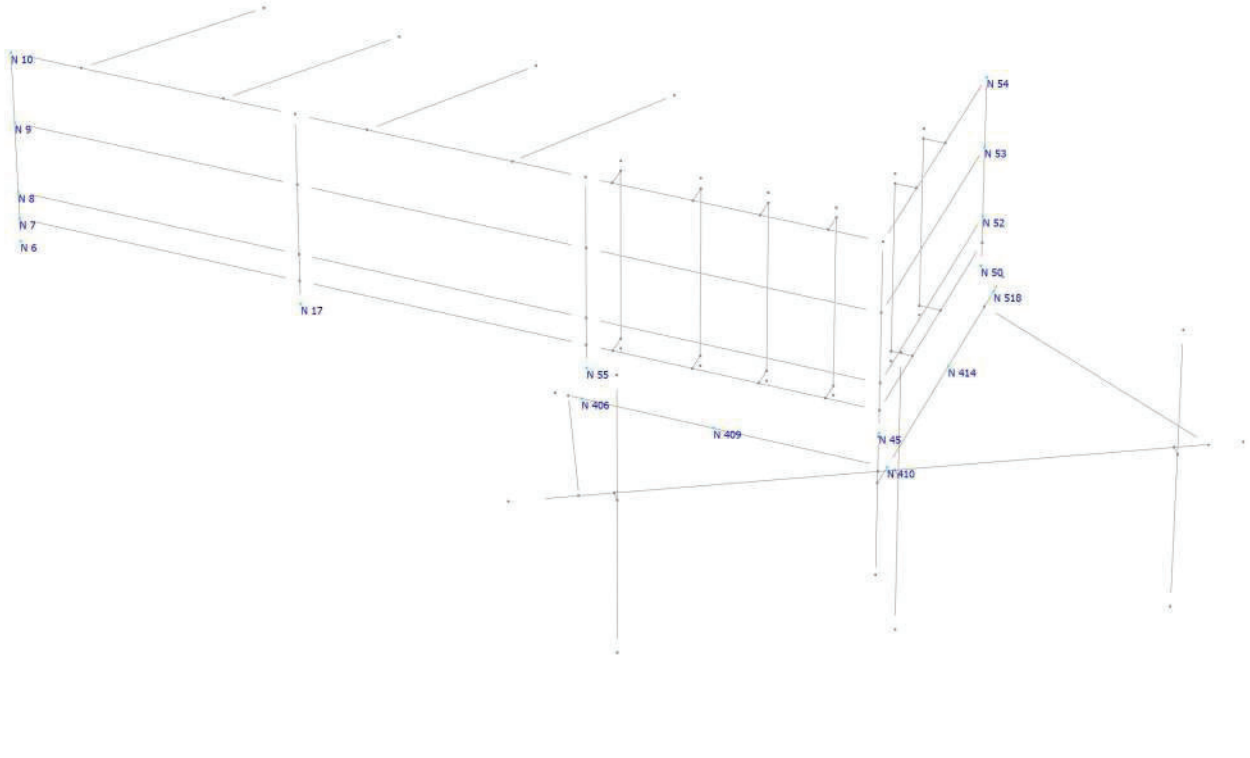
Member	Rotation [Deg]	Axes23	NX	NY	NZ
2	180.00	0	0.00	0.00	0.00
10	180.00	0	0.00	0.00	0.00
11	90.00	0	0.00	0.00	0.00
14	270.00	0	0.00	0.00	0.00
16	90.00	0	0.00	0.00	0.00
19	270.00	0	0.00	0.00	0.00
31	270.00	0	0.00	0.00	0.00
32	270.00	0	0.00	0.00	0.00
33	90.00	0	0.00	0.00	0.00
36	270.00	0	0.00	0.00	0.00
37	90.00	0	0.00	0.00	0.00
40	270.00	0	0.00	0.00	0.00
41	180.00	0	0.00	0.00	0.00
44	315.00	0	0.00	0.00	0.00
47	315.00	0	0.00	0.00	0.00
57	315.00	0	0.00	0.00	0.00
58	315.00	0	0.00	0.00	0.00
60	90.00	0	0.00	0.00	0.00
61	90.00	0	0.00	0.00	0.00
62	90.00	0	0.00	0.00	0.00
66	90.00	0	0.00	0.00	0.00
94	315.00	0	0.00	0.00	0.00
103	315.00	0	0.00	0.00	0.00
141	315.00	0	0.00	0.00	0.00
147	90.00	0	0.00	0.00	0.00
148	90.00	0	0.00	0.00	0.00
152	315.00	0	0.00	0.00	0.00
153	315.00	0	0.00	0.00	0.00

Rigid end offsets

Member	DJX [in]	DJY [in]	DJZ [in]	DKX [in]	DKY [in]	DKZ [in]
144	0.00	0.00	-3.00	0.00	0.00	-3.00

Hinges

	Node-J				Node-K						
Member	**M33**	**M22**	**V3**	**V2**	**M33**	**M22**	**V3**	**V2**	**TOR**	**AXL**	**Axial rigidity**
12	0	0	0	0	0	0	0	0	0	0	Tension only
13	0	0	0	0	0	0	0	0	0	0	Tension only
17	0	0	0	0	0	0	0	0	0	0	Tension only
18	0	0	0	0	0	0	0	0	0	0	Tension only
34	0	0	0	0	0	0	0	0	0	0	Tension only
35	0	0	0	0	0	0	0	0	0	0	Tension only
38	0	0	0	0	0	0	0	0	0	0	Tension only
39	0	0	0	0	0	0	0	0	0	0	Tension only


N 10
N 9
N 8
N 7
N 6
N 17
N 55
N 406
N 409
N 45
N 410
N 414
N 54
N 53
N 52
N 50
N 518
Y
X
Z

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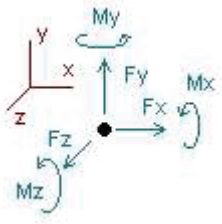
Analysis result

Reactions



Direction of positive forces and moments

	Forces [Kip]			Moments [Kip*ft]		
Node	**FX**	**FY**	**FZ**	**MX**	**MY**	**MZ**
Condition **LC1=1.2D+1.6Wo**						
6	-0.00618	0.04966	0.00324	0.00000	-0.00140	0.00000
7	-0.11373	0.00000	0.04033	0.00000	0.00000	0.00000
8	-0.05840	0.00000	0.06039	0.00000	0.00000	0.00000
9	-0.07124	0.00000	0.06839	0.00000	0.00000	0.00000
10	0.11027	0.00000	0.00765	0.00000	0.00000	0.00000
17	0.12723	0.03689	0.23694	0.00000	-0.00054	0.00000
45	-0.11387	0.37012	-0.21728	0.00000	0.00237	0.00000
50	-0.00069	0.16090	0.09561	0.00000	-0.00121	0.00000
51	-0.05643	0.00000	0.70375	0.00000	0.00000	0.00000
52	-0.00598	0.00000	-0.11603	0.00000	0.00000	0.00000
53	0.00048	0.00000	0.03702	0.00000	0.00000	0.00000
54	-0.04464	0.00000	0.48645	0.00000	0.00000	0.00000
55	0.21824	0.14173	0.33488	0.00000	-0.00051	0.00000
115	-0.00364	0.05659	0.11010	0.00000	0.00000	0.00000
116	0.01515	0.23797	0.51301	0.00000	0.00000	0.00000
133	0.00056	0.06102	0.11893	0.00000	0.00000	0.00000
134	0.00287	0.10385	0.21505	0.00000	0.00000	0.00000
406	0.37235	0.16738	0.71411	0.00000	0.16691	0.00000
409	0.00000	-0.25147	0.06440	0.00000	-0.00805	0.00000
410	-1.23031	1.03649	1.73516	0.00000	-0.49960	0.00000
414	0.04604	-0.19275	0.11782	0.00000	-0.04664	0.00000
518	0.81192	0.07389	0.47129	0.00000	0.20058	0.00000
SUM	0.00000	2.05224	5.80118	0.00000	-0.18809	0.00000
Condition **LC2=1.2D+1.6W30**						
6	-0.00577	0.05021	0.00324	0.00000	-0.00143	0.00000
7	0.02768	0.00000	0.04219	0.00000	0.00000	0.00000
8	-0.03444	0.00000	0.06038	0.00000	0.00000	0.00000
9	-0.06409	0.00000	0.06840	0.00000	0.00000	0.00000
10	0.32892	0.00000	0.00756	0.00000	0.00000	0.00000
17	0.14638	0.03384	0.23523	0.00000	-0.00046	0.00000
45	-0.09454	0.36212	-0.20008	0.00000	0.00158	0.00000
50	-0.00225	0.15905	0.08714	0.00000	-0.00045	0.00000
51	-0.01070	0.00000	0.62978	0.00000	0.00000	0.00000
52	-0.00469	0.00000	-0.09076	0.00000	0.00000	0.00000
53	0.00071	0.00000	0.08803	0.00000	0.00000	0.00000
54	-0.00469	0.00000	0.42095	0.00000	0.00000	0.00000
55	0.23772	0.18251	0.27963	0.00000	-0.00020	0.00000

115	-0.00305	0.06505	0.12892	0.00000	0.00000	0.00000
116	0.01229	0.20145	0.43178	0.00000	0.00000	0.00000
133	0.00058	0.06128	0.11950	0.00000	0.00000	0.00000
134	0.00282	0.10319	0.21359	0.00000	0.00000	0.00000
406	0.39757	0.13485	0.72683	0.00000	0.21827	0.00000
409	0.00000	-0.23270	0.06440	0.00000	-0.00805	0.00000
410	0.26496	1.02249	0.87393	0.00000	0.03322	0.00000
414	0.04479	-0.16938	0.10751	0.00000	-0.04425	0.00000
518	0.73179	0.07828	0.43002	0.00000	0.18508	0.00000
SUM	1.97198	2.05225	4.72817	0.00000	0.38331	0.00000

Condition **LC3=1.2D+1.6W60**

6	0.02431	0.05511	0.00028	0.00000	0.00009	0.00000
7	0.51134	0.00000	-0.00314	0.00000	0.00000	0.00000
8	-0.00525	0.00000	0.00109	0.00000	0.00000	0.00000
9	0.03531	0.00000	-0.00066	0.00000	0.00000	0.00000
10	0.99926	0.00000	-0.06676	0.00000	0.00000	0.00000
17	0.03510	0.16592	0.00387	0.00000	-0.00015	0.00000
45	-0.09052	0.34326	-0.10797	0.00000	-0.00069	0.00000
50	-0.00044	0.15781	0.06891	0.00000	0.00155	0.00000
51	0.09753	0.00000	0.32665	0.00000	0.00000	0.00000
52	0.05757	0.00000	-0.10618	0.00000	0.00000	0.00000
53	0.07206	0.00000	0.09149	0.00000	0.00000	0.00000
54	0.08917	0.00000	0.23266	0.00000	0.00000	0.00000
55	0.13550	0.34907	0.01156	0.00000	-0.00026	0.00000
115	0.08066	0.02050	-0.01166	0.00000	0.00000	0.00000
116	0.08387	0.06846	0.09501	0.00000	0.00000	0.00000
133	0.08091	0.03645	0.02385	0.00000	0.00000	0.00000
134	0.08013	0.02213	-0.00804	0.00000	0.00000	0.00000
406	0.28963	0.13032	0.45534	0.00000	0.16886	0.00000
409	0.00000	-0.21297	0.00000	0.00000	0.00000	0.00000
410	0.80659	0.97787	0.23674	0.00000	0.20248	0.00000
414	0.10889	-0.13799	0.06297	0.00000	-0.03080	0.00000
518	0.50125	0.07630	0.25188	0.00000	0.14694	0.00000
SUM	3.99287	2.05225	1.55790	0.00000	0.48802	0.00000

Condition **LC4=1.2D+1.6W90**

6	0.01949	0.05549	0.00036	0.00000	0.00005	0.00000
7	0.47345	0.00000	-0.00088	0.00000	0.00000	0.00000
8	-0.02397	0.00000	0.00115	0.00000	0.00000	0.00000
9	0.00633	0.00000	-0.00063	0.00000	0.00000	0.00000
10	0.99176	0.00000	-0.06636	0.00000	0.00000	0.00000
17	0.04468	0.16169	0.00230	0.00000	-0.00002	0.00000
45	-0.11762	0.34305	-0.08986	0.00000	-0.00156	0.00000
50	-0.00198	0.15338	0.05131	0.00000	0.00229	0.00000
51	0.14595	0.00000	0.10592	0.00000	0.00000	0.00000
52	0.05866	0.00000	-0.09774	0.00000	0.00000	0.00000
53	0.07221	0.00000	0.11360	0.00000	0.00000	0.00000
54	0.13163	0.00000	0.01799	0.00000	0.00000	0.00000
55	0.15551	0.39271	-0.05807	0.00000	0.00026	0.00000
115	0.08147	0.02982	0.00906	0.00000	0.00000	0.00000
116	0.07996	0.02415	-0.00360	0.00000	0.00000	0.00000
133	0.08093	0.03634	0.02360	0.00000	0.00000	0.00000
134	0.08005	0.02209	-0.00812	0.00000	0.00000	0.00000
406	0.16516	0.12038	0.23995	0.00000	0.10418	0.00000
409	0.00000	-0.18592	0.00000	0.00000	0.00000	0.00000
410	1.32081	0.94727	-0.36851	0.00000	0.41753	0.00000

414	0.09357	-0.12953	0.02571	0.00000	-0.01532	0.00000
518	0.23350	0.08133	0.10284	0.00000	0.08062	0.00000
SUM	4.09155	2.05225	0.00000	0.00000	0.58801	0.00000

Condition **LC5=1.2D+1.6W120**

6	0.02473	0.05443	0.00030	0.00000	0.00002	0.00000
7	0.49201	0.00000	0.00109	0.00000	0.00000	0.00000
8	-0.00513	0.00000	0.00104	0.00000	0.00000	0.00000
9	0.03324	0.00000	-0.00064	0.00000	0.00000	0.00000
10	0.97357	0.00000	-0.06695	0.00000	0.00000	0.00000
17	0.02159	0.15856	0.00083	0.00000	0.00003	0.00000
45	-0.13000	0.34725	-0.09407	0.00000	-0.00189	0.00000
50	-0.00135	0.14960	0.05058	0.00000	0.00227	0.00000
51	0.14434	0.00000	-0.10876	0.00000	0.00000	0.00000
52	0.05846	0.00000	-0.09475	0.00000	0.00000	0.00000
53	0.07191	0.00000	0.10644	0.00000	0.00000	0.00000
54	0.12891	0.00000	-0.19555	0.00000	0.00000	0.00000
55	0.15441	0.42344	-0.11138	0.00000	0.00061	0.00000
115	0.08197	0.03999	0.03170	0.00000	0.00000	0.00000
116	0.07702	-0.01125	-0.08244	0.00000	0.00000	0.00000
133	0.08092	0.03769	0.02662	0.00000	0.00000	0.00000
134	0.07991	0.01900	-0.01502	0.00000	0.00000	0.00000
406	0.02150	0.11503	0.00177	0.00000	0.02116	0.00000
409	0.00000	-0.18548	0.00000	0.00000	0.00000	0.00000
410	1.65909	0.93763	-0.93932	0.00000	0.57312	0.00000
414	0.07640	-0.11881	-0.01387	0.00000	0.00171	0.00000
518	-0.05064	0.08516	-0.05550	0.00000	0.00904	0.00000
SUM	3.99287	2.05225	-1.55790	0.00000	0.60606	0.00000

Condition **LC6=1.2D+1.6W150**

6	0.04224	0.12709	-0.00211	0.00000	0.00152	0.00000
7	0.39400	0.00000	-0.04460	0.00000	0.00000	0.00000
8	-0.06158	0.00000	-0.05667	0.00000	0.00000	0.00000
9	0.04553	0.00000	-0.07142	0.00000	0.00000	0.00000
10	0.15436	0.00000	-0.00843	0.00000	0.00000	0.00000
17	-0.13716	0.29117	-0.24009	0.00000	0.00048	0.00000
45	-0.05754	0.35530	-0.08158	0.00000	-0.00239	0.00000
50	-0.00398	0.14752	0.06580	0.00000	0.00157	0.00000
51	0.09320	0.00000	-0.28732	0.00000	0.00000	0.00000
52	-0.00097	0.00000	-0.14093	0.00000	0.00000	0.00000
53	0.00298	0.00000	-0.11628	0.00000	0.00000	0.00000
54	0.07450	0.00000	-0.30890	0.00000	0.00000	0.00000
55	-0.02115	0.52696	-0.32977	0.00000	0.00033	0.00000
115	0.01054	-0.01067	-0.12238	0.00000	0.00000	0.00000
116	-0.00937	-0.16643	-0.46880	0.00000	0.00000	0.00000
133	0.00580	0.00278	-0.09130	0.00000	0.00000	0.00000
134	0.00149	-0.05502	-0.22072	0.00000	0.00000	0.00000
406	-0.12223	0.10436	-0.25859	0.00000	-0.04996	0.00000
409	0.00000	-0.17800	-0.06440	0.00000	0.00805	0.00000
410	1.93899	0.91093	-1.59467	0.00000	0.71922	0.00000
414	0.00007	-0.08681	-0.05701	0.00000	0.00724	0.00000
518	-0.37773	0.08305	-0.22803	0.00000	-0.06519	0.00000
SUM	1.97198	2.05225	-4.72817	0.00000	0.62086	0.00000

Condition **LC7=1.2D-1.6Wo**

6	0.04078	0.12636	-0.00215	0.00000	0.00150	0.00000
7	0.21989	0.00000	-0.04395	0.00000	0.00000	0.00000
8	-0.05939	0.00000	-0.05676	0.00000	0.00000	0.00000
9	0.04451	0.00000	-0.07139	0.00000	0.00000	0.00000
10	-0.08131	0.00000	-0.00846	0.00000	0.00000	0.00000
17	-0.14040	0.28927	-0.23987	0.00000	0.00054	0.00000
45	-0.10174	0.36394	-0.07933	0.00000	-0.00236	0.00000
50	-0.00257	0.14605	0.08028	0.00000	0.00119	0.00000
51	0.06785	0.00000	-0.38048	0.00000	0.00000	0.00000
52	-0.00153	0.00000	-0.12999	0.00000	0.00000	0.00000
53	0.00262	0.00000	-0.10833	0.00000	0.00000	0.00000
54	0.05187	0.00000	-0.38294	0.00000	0.00000	0.00000
55	-0.04804	0.53231	-0.34984	0.00000	0.00053	0.00000
115	0.01073	-0.00832	-0.11715	0.00000	0.00000	0.00000
116	-0.01054	-0.17880	-0.49639	0.00000	0.00000	0.00000
133	0.00580	0.00273	-0.09140	0.00000	0.00000	0.00000
134	0.00146	-0.05482	-0.22026	0.00000	0.00000	0.00000
406	-0.40426	0.12169	-0.70189	0.00000	-0.24487	0.00000
409	0.00000	-0.16934	-0.06440	0.00000	0.00805	0.00000
410	1.25131	0.85028	-1.74275	0.00000	0.52248	0.00000
414	-0.03066	-0.04806	-0.11875	0.00000	0.03638	0.00000
518	-0.81639	0.07896	-0.47500	0.00000	-0.18121	0.00000
SUM	0.00000	2.05224	-5.80118	0.00000	0.14222	0.00000

Condition **LC8=1.2D-1.6W30**

6	0.03972	0.12540	-0.00217	0.00000	0.00152	0.00000
7	0.05877	0.00000	-0.04587	0.00000	0.00000	0.00000
8	-0.05838	0.00000	-0.05677	0.00000	0.00000	0.00000
9	0.03260	0.00000	-0.07138	0.00000	0.00000	0.00000
10	-0.29969	0.00000	-0.00847	0.00000	0.00000	0.00000
17	-0.15103	0.29235	-0.23796	0.00000	0.00047	0.00000
45	-0.12421	0.37161	-0.08151	0.00000	-0.00157	0.00000
50	-0.00097	0.14810	0.08963	0.00000	0.00042	0.00000
51	0.02150	0.00000	-0.34603	0.00000	0.00000	0.00000
52	-0.00277	0.00000	-0.14172	0.00000	0.00000	0.00000
53	0.00234	0.00000	-0.13324	0.00000	0.00000	0.00000
54	0.01124	0.00000	-0.33227	0.00000	0.00000	0.00000
55	-0.07195	0.49227	-0.29545	0.00000	0.00023	0.00000
115	0.01012	-0.01654	-0.13544	0.00000	0.00000	0.00000
116	-0.00748	-0.14279	-0.41607	0.00000	0.00000	0.00000
133	0.00578	0.00250	-0.09193	0.00000	0.00000	0.00000
134	0.00152	-0.05418	-0.21884	0.00000	0.00000	0.00000
406	-0.43007	0.15446	-0.71473	0.00000	-0.29660	0.00000
409	0.00000	-0.18945	-0.06440	0.00000	0.00805	0.00000
410	-0.24324	0.86581	-0.88186	0.00000	-0.00999	0.00000
414	-0.02960	-0.06982	-0.10834	0.00000	0.03412	0.00000
518	-0.73619	0.07252	-0.43336	0.00000	-0.16597	0.00000
SUM	-1.97198	2.05224	-4.72817	0.00000	-0.42931	0.00000

Condition **LC9=1.2D-1.6W60**

6	0.01072	0.12061	0.00082	0.00000	0.00001	0.00000
7	-0.27127	0.00000	-0.00067	0.00000	0.00000	0.00000
8	-0.17652	0.00000	0.00258	0.00000	0.00000	0.00000
9	-0.17622	0.00000	-0.00232	0.00000	0.00000	0.00000
10	-0.90152	0.00000	0.06555	0.00000	0.00000	0.00000
17	-0.03418	0.16176	-0.00663	0.00000	0.00014	0.00000
45	-0.15524	0.38691	-0.11023	0.00000	0.00062	0.00000

50	-0.00266	0.15061	0.11078	0.00000	-0.00154	0.00000
51	-0.08690	0.00000	-0.18176	0.00000	0.00000	0.00000
52	-0.06482	0.00000	-0.11221	0.00000	0.00000	0.00000
53	-0.06911	0.00000	-0.00985	0.00000	0.00000	0.00000
54	-0.08321	0.00000	-0.21205	0.00000	0.00000	0.00000
55	0.02704	0.32659	-0.02754	0.00000	0.00022	0.00000
115	-0.07356	0.02936	0.00821	0.00000	0.00000	0.00000
116	-0.07882	-0.01094	-0.08136	0.00000	0.00000	0.00000
133	-0.07453	0.02780	0.00480	0.00000	0.00000	0.00000
134	-0.07573	0.02601	0.00090	0.00000	0.00000	0.00000
406	-0.32224	0.15930	-0.44315	0.00000	-0.24738	0.00000
409	0.00000	-0.20962	0.00000	0.00000	0.00000	0.00000
410	-0.78478	0.90974	-0.24498	0.00000	-0.17927	0.00000
414	-0.09360	-0.10014	-0.06376	0.00000	0.02060	0.00000
518	-0.50573	0.07424	-0.25503	0.00000	-0.12771	0.00000
SUM	-3.99287	2.05224	-1.55790	0.00000	-0.53431	0.00000

Condition **LC10=1.2D-1.6W90**

6	0.01473	0.11990	0.00071	0.00000	0.00005	0.00000
7	-0.28235	0.00000	-0.00271	0.00000	0.00000	0.00000
8	-0.14006	0.00000	0.00246	0.00000	0.00000	0.00000
9	-0.08752	0.00000	-0.00232	0.00000	0.00000	0.00000
10	-0.93087	0.00000	0.06518	0.00000	0.00000	0.00000
17	-0.03526	0.16674	-0.00538	0.00000	0.00004	0.00000
45	-0.15229	0.38716	-0.11372	0.00000	0.00147	0.00000
50	-0.00112	0.15524	0.12870	0.00000	-0.00227	0.00000
51	-0.13505	0.00000	0.01424	0.00000	0.00000	0.00000
52	-0.06589	0.00000	-0.12092	0.00000	0.00000	0.00000
53	-0.06924	0.00000	-0.01303	0.00000	0.00000	0.00000
54	-0.12508	0.00000	-0.00736	0.00000	0.00000	0.00000
55	0.03094	0.28194	0.04248	0.00000	-0.00025	0.00000
115	-0.07429	0.01891	-0.01505	0.00000	0.00000	0.00000
116	-0.07496	0.03437	0.01958	0.00000	0.00000	0.00000
133	-0.07455	0.02780	0.00480	0.00000	0.00000	0.00000
134	-0.07565	0.02665	0.00233	0.00000	0.00000	0.00000
406	-0.19779	0.16956	-0.22767	0.00000	-0.18282	0.00000
409	0.00000	-0.23724	0.00000	0.00000	0.00000	0.00000
410	-1.29902	0.94001	0.36010	0.00000	-0.39439	0.00000
414	-0.07819	-0.10802	-0.02649	0.00000	0.00507	0.00000
518	-0.23804	0.06923	-0.10595	0.00000	-0.06128	0.00000
SUM	-4.09155	2.05224	0.00000	0.00000	-0.63439	0.00000

Condition **LC11=1.2D-1.6W120**

6	0.01058	0.12058	0.00082	0.00000	0.00008	0.00000
7	-0.28027	0.00000	-0.00476	0.00000	0.00000	0.00000
8	-0.16857	0.00000	0.00264	0.00000	0.00000	0.00000
9	-0.12347	0.00000	-0.00233	0.00000	0.00000	0.00000
10	-0.90656	0.00000	0.06569	0.00000	0.00000	0.00000
17	-0.03312	0.16991	-0.00394	0.00000	-0.00004	0.00000
45	-0.13447	0.38296	-0.11078	0.00000	0.00180	0.00000
50	-0.00172	0.15892	0.12914	0.00000	-0.00226	0.00000
51	-0.13355	0.00000	0.23118	0.00000	0.00000	0.00000
52	-0.06568	0.00000	-0.12340	0.00000	0.00000	0.00000
53	-0.06895	0.00000	-0.00815	0.00000	0.00000	0.00000
54	-0.12193	0.00000	0.20719	0.00000	0.00000	0.00000
55	0.03819	0.25156	0.09575	0.00000	-0.00059	0.00000
115	-0.07482	0.01038	-0.03405	0.00000	0.00000	0.00000

116	-0.07206	0.06930	0.09736	0.00000	0.00000	0.00000
133	-0.07455	0.02702	0.00307	0.00000	0.00000	0.00000
134	-0.07556	0.02810	0.00556	0.00000	0.00000	0.00000
406	-0.05399	0.17509	0.01059	0.00000	-0.09979	0.00000
409	0.00000	-0.23806	0.00000	0.00000	0.00000	0.00000
410	-1.63751	0.94936	0.93095	0.00000	-0.55010	0.00000
414	-0.06093	-0.11874	0.01308	0.00000	-0.01203	0.00000
518	0.04607	0.06587	0.05231	0.00000	0.01041	0.00000
SUM	-3.99287	2.05224	1.55790	0.00000	-0.65252	0.00000

Condition **LC12=1.2D-1.6W150**

6	-0.00669	0.04874	0.00324	0.00000	-0.00141	0.00000
7	-0.24214	0.00000	0.04106	0.00000	0.00000	0.00000
8	-0.09899	0.00000	0.06033	0.00000	0.00000	0.00000
9	-0.08004	0.00000	0.06840	0.00000	0.00000	0.00000
10	-0.11609	0.00000	0.00765	0.00000	0.00000	0.00000
17	0.11360	0.03534	0.23696	0.00000	-0.00050	0.00000
45	-0.15158	0.37792	-0.21227	0.00000	0.00239	0.00000
50	0.00074	0.15939	0.11018	0.00000	-0.00158	0.00000
51	-0.08171	0.00000	0.59958	0.00000	0.00000	0.00000
52	-0.00651	0.00000	-0.09857	0.00000	0.00000	0.00000
53	0.00010	0.00000	0.04991	0.00000	0.00000	0.00000
54	-0.06721	0.00000	0.40889	0.00000	0.00000	0.00000
55	0.18976	0.14772	0.31484	0.00000	-0.00032	0.00000
115	-0.00344	0.06026	0.11827	0.00000	0.00000	0.00000
116	0.01395	0.22509	0.48440	0.00000	0.00000	0.00000
133	0.00056	0.06134	0.11966	0.00000	0.00000	0.00000
134	0.00280	0.10291	0.21295	0.00000	0.00000	0.00000
406	0.08998	0.18592	0.27103	0.00000	-0.02858	0.00000
409	0.00000	-0.24606	0.06440	0.00000	-0.00805	0.00000
410	-1.91769	0.97584	1.58649	0.00000	-0.69635	0.00000
414	0.01549	-0.15113	0.05615	0.00000	-0.01762	0.00000
518	0.37312	0.06896	0.22462	0.00000	0.08475	0.00000
SUM	-1.97198	2.05224	4.72817	0.00000	-0.66726	0.00000

Condition **LC13=0.9D+1.6Wo**

6	-0.01032	0.02787	0.00311	0.00000	-0.00141	0.00000
7	-0.11963	0.00000	0.04077	0.00000	0.00000	0.00000
8	-0.04847	0.00000	0.05994	0.00000	0.00000	0.00000
9	-0.07626	0.00000	0.06876	0.00000	0.00000	0.00000
10	0.11199	0.00000	0.00779	0.00000	0.00000	0.00000
17	0.12689	-0.00402	0.23730	0.00000	-0.00054	0.00000
45	-0.08387	0.27883	-0.19032	0.00000	0.00238	0.00000
50	-0.00032	0.12227	0.07289	0.00000	-0.00120	0.00000
51	-0.05754	0.00000	0.68695	0.00000	0.00000	0.00000
52	-0.00507	0.00000	-0.08875	0.00000	0.00000	0.00000
53	0.00011	0.00000	0.02431	0.00000	0.00000	0.00000
54	-0.04530	0.00000	0.48533	0.00000	0.00000	0.00000
55	0.19573	0.05714	0.33723	0.00000	-0.00052	0.00000
115	-0.00454	0.05039	0.11061	0.00000	0.00000	0.00000
116	0.01452	0.23075	0.51121	0.00000	0.00000	0.00000
133	-0.00023	0.05297	0.11531	0.00000	0.00000	0.00000
134	0.00232	0.09784	0.21596	0.00000	0.00000	0.00000
406	0.37641	0.13133	0.71258	0.00000	0.17677	0.00000
409	0.00000	-0.19886	0.06440	0.00000	-0.00805	0.00000
410	-1.23301	0.79901	1.73623	0.00000	-0.50248	0.00000
414	0.04412	-0.16188	0.11792	0.00000	-0.04536	0.00000

518	0.81247	0.05555	0.47166	0.00000	0.19815	0.00000
SUM	0.00000	1.53918	5.80118	0.00000	-0.18225	0.00000

Condition **LC14=0.9D+1.6W30**

6	-0.00997	0.02839	0.00310	0.00000	-0.00144	0.00000
7	0.02473	0.00000	0.04264	0.00000	0.00000	0.00000
8	-0.02843	0.00000	0.05993	0.00000	0.00000	0.00000
9	-0.06990	0.00000	0.06877	0.00000	0.00000	0.00000
10	0.33156	0.00000	0.00770	0.00000	0.00000	0.00000
17	0.14799	-0.00695	0.23558	0.00000	-0.00046	0.00000
45	-0.06371	0.27068	-0.17331	0.00000	0.00158	0.00000
50	-0.00187	0.12042	0.06442	0.00000	-0.00044	0.00000
51	-0.01179	0.00000	0.61315	0.00000	0.00000	0.00000
52	-0.00378	0.00000	-0.06348	0.00000	0.00000	0.00000
53	0.00034	0.00000	0.07532	0.00000	0.00000	0.00000
54	-0.00534	0.00000	0.41981	0.00000	0.00000	0.00000
55	0.21328	0.09799	0.28202	0.00000	-0.00022	0.00000
115	-0.00395	0.05886	0.12944	0.00000	0.00000	0.00000
116	0.01167	0.19424	0.43001	0.00000	0.00000	0.00000
133	-0.00022	0.05323	0.11588	0.00000	0.00000	0.00000
134	0.00227	0.09718	0.21450	0.00000	0.00000	0.00000
406	0.40167	0.09875	0.72529	0.00000	0.22821	0.00000
409	0.00000	-0.17910	0.06440	0.00000	-0.00805	0.00000
410	0.26222	0.78472	0.87499	0.00000	0.03026	0.00000
414	0.04285	-0.13919	0.10760	0.00000	-0.04296	0.00000
518	0.73236	0.05997	0.43040	0.00000	0.18264	0.00000
SUM	1.97198	1.53919	4.72817	0.00000	0.38914	0.00000

Condition **LC15=0.9D+1.6W60**

6	0.02008	0.03327	0.00015	0.00000	0.00008	0.00000
7	0.50722	0.00000	-0.00269	0.00000	0.00000	0.00000
8	0.00176	0.00000	0.00064	0.00000	0.00000	0.00000
9	0.02969	0.00000	-0.00029	0.00000	0.00000	0.00000
10	1.00158	0.00000	-0.06661	0.00000	0.00000	0.00000
17	0.03706	0.12519	0.00420	0.00000	-0.00015	0.00000
45	-0.06113	0.25187	-0.08074	0.00000	-0.00069	0.00000
50	-0.00007	0.11915	0.04618	0.00000	0.00156	0.00000
51	0.09649	0.00000	0.30949	0.00000	0.00000	0.00000
52	0.05847	0.00000	-0.07896	0.00000	0.00000	0.00000
53	0.07170	0.00000	0.07876	0.00000	0.00000	0.00000
54	0.08856	0.00000	0.23159	0.00000	0.00000	0.00000
55	0.11238	0.26442	0.01392	0.00000	-0.00027	0.00000
115	0.07977	0.01427	-0.01122	0.00000	0.00000	0.00000
116	0.08326	0.06133	0.09343	0.00000	0.00000	0.00000
133	0.08011	0.02841	0.02024	0.00000	0.00000	0.00000
134	0.07958	0.01612	-0.00712	0.00000	0.00000	0.00000
406	0.29373	0.09418	0.45380	0.00000	0.17878	0.00000
409	0.00000	-0.15935	0.00000	0.00000	0.00000	0.00000
410	0.80385	0.74069	0.23779	0.00000	0.19952	0.00000
414	0.10695	-0.10818	0.06307	0.00000	-0.02950	0.00000
518	0.50182	0.05781	0.25226	0.00000	0.14450	0.00000
SUM	3.99287	1.53919	1.55790	0.00000	0.49382	0.00000

Condition **LC16=0.9D+1.6W90**

6	0.01526	0.03364	0.00022	0.00000	0.00003	0.00000
7	0.46932	0.00000	-0.00043	0.00000	0.00000	0.00000
8	-0.01697	0.00000	0.00069	0.00000	0.00000	0.00000
9	0.00072	0.00000	-0.00027	0.00000	0.00000	0.00000
10	0.99408	0.00000	-0.06622	0.00000	0.00000	0.00000
17	0.04665	0.12097	0.00263	0.00000	-0.00002	0.00000
45	-0.08823	0.25166	-0.06266	0.00000	-0.00156	0.00000
50	-0.00161	0.11471	0.02860	0.00000	0.00230	0.00000
51	0.14490	0.00000	0.08879	0.00000	0.00000	0.00000
52	0.05956	0.00000	-0.07055	0.00000	0.00000	0.00000
53	0.07185	0.00000	0.10089	0.00000	0.00000	0.00000
54	0.13102	0.00000	0.01691	0.00000	0.00000	0.00000
55	0.13240	0.30805	-0.05574	0.00000	0.00024	0.00000
115	0.08057	0.02359	0.00950	0.00000	0.00000	0.00000
116	0.07935	0.01703	-0.00516	0.00000	0.00000	0.00000
133	0.08013	0.02830	0.01999	0.00000	0.00000	0.00000
134	0.07950	0.01608	-0.00720	0.00000	0.00000	0.00000
406	0.16927	0.08419	0.23841	0.00000	0.11408	0.00000
409	0.00000	-0.13224	0.00000	0.00000	0.00000	0.00000
410	1.31807	0.71063	-0.36746	0.00000	0.41457	0.00000
414	0.09162	-0.10011	0.02581	0.00000	-0.01403	0.00000
518	0.23408	0.06268	0.10324	0.00000	0.07817	0.00000
SUM	4.09155	1.53919	0.00000	0.00000	0.59379	0.00000

Condition **LC17=0.9D+1.6W120**

6	0.02051	0.03258	0.00017	0.00000	0.00001	0.00000
7	0.48810	0.00000	0.00154	0.00000	0.00000	0.00000
8	0.00187	0.00000	0.00058	0.00000	0.00000	0.00000
9	0.02763	0.00000	-0.00027	0.00000	0.00000	0.00000
10	0.97587	0.00000	-0.06680	0.00000	0.00000	0.00000
17	0.02359	0.11784	0.00117	0.00000	0.00003	0.00000
45	-0.10087	0.25583	-0.06609	0.00000	-0.00189	0.00000
50	-0.00098	0.11095	0.02795	0.00000	0.00228	0.00000
51	0.14328	0.00000	-0.12763	0.00000	0.00000	0.00000
52	0.05937	0.00000	-0.06757	0.00000	0.00000	0.00000
53	0.07155	0.00000	0.09572	0.00000	0.00000	0.00000
54	0.12827	0.00000	-0.19769	0.00000	0.00000	0.00000
55	0.13136	0.33880	-0.10909	0.00000	0.00059	0.00000
115	0.08108	0.03377	0.03215	0.00000	0.00000	0.00000
116	0.07641	-0.01838	-0.08402	0.00000	0.00000	0.00000
133	0.08013	0.02965	0.02301	0.00000	0.00000	0.00000
134	0.07937	0.01299	-0.01410	0.00000	0.00000	0.00000
406	0.02560	0.07880	0.00023	0.00000	0.03104	0.00000
409	0.00000	-0.13182	0.00000	0.00000	0.00000	0.00000
410	1.65636	0.70160	-0.93828	0.00000	0.57015	0.00000
414	0.07446	-0.08975	-0.01377	0.00000	0.00301	0.00000
518	-0.05005	0.06632	-0.05510	0.00000	0.00660	0.00000
SUM	3.99287	1.53919	-1.55790	0.00000	0.61182	0.00000

Condition **LC18=0.9D+1.6W150**

6	0.03802	0.10529	-0.00224	0.00000	0.00151	0.00000
7	0.38987	0.00000	-0.04415	0.00000	0.00000	0.00000
8	-0.05459	0.00000	-0.05713	0.00000	0.00000	0.00000
9	0.04002	0.00000	-0.07105	0.00000	0.00000	0.00000
10	0.15632	0.00000	-0.00828	0.00000	0.00000	0.00000
17	-0.13514	0.25038	-0.23980	0.00000	0.00048	0.00000
45	-0.02857	0.26322	-0.05824	0.00000	-0.00238	0.00000

50	-0.00362	0.10934	0.04360	0.00000	0.00158	0.00000
51	0.09232	0.00000	-0.28696	0.00000	0.00000	0.00000
52	-0.00008	0.00000	-0.13408	0.00000	0.00000	0.00000
53	0.00262	0.00000	-0.11959	0.00000	0.00000	0.00000
54	0.07381	0.00000	-0.31329	0.00000	0.00000	0.00000
55	-0.04376	0.44253	-0.32730	0.00000	0.00031	0.00000
115	0.00965	-0.01695	-0.12203	0.00000	0.00000	0.00000
116	-0.00997	-0.17354	-0.47034	0.00000	0.00000	0.00000
133	0.00501	-0.00528	-0.09494	0.00000	0.00000	0.00000
134	0.00095	-0.06096	-0.21965	0.00000	0.00000	0.00000
406	-0.11813	0.06807	-0.26012	0.00000	-0.04010	0.00000
409	0.00000	-0.12429	-0.06440	0.00000	0.00805	0.00000
410	1.93625	0.67547	-1.59364	0.00000	0.71625	0.00000
414	-0.00187	-0.05813	-0.05690	0.00000	0.00854	0.00000
518	-0.37714	0.06404	-0.22762	0.00000	-0.06763	0.00000
SUM	1.97198	1.53919	-4.72817	0.00000	0.62660	0.00000

Condition **LC19=0.9D-1.6Wo**

6	0.03668	0.10462	-0.00228	0.00000	0.00149	0.00000
7	0.21841	0.00000	-0.04351	0.00000	0.00000	0.00000
8	-0.05262	0.00000	-0.05720	0.00000	0.00000	0.00000
9	0.03660	0.00000	-0.07102	0.00000	0.00000	0.00000
10	-0.07802	0.00000	-0.00832	0.00000	0.00000	0.00000
17	-0.14080	0.24838	-0.23956	0.00000	0.00053	0.00000
45	-0.07312	0.27195	-0.05593	0.00000	-0.00235	0.00000
50	-0.00220	0.10787	0.05809	0.00000	0.00120	0.00000
51	0.06697	0.00000	-0.38023	0.00000	0.00000	0.00000
52	-0.00064	0.00000	-0.12312	0.00000	0.00000	0.00000
53	0.00226	0.00000	-0.11161	0.00000	0.00000	0.00000
54	0.05117	0.00000	-0.38733	0.00000	0.00000	0.00000
55	-0.06931	0.44781	-0.34741	0.00000	0.00052	0.00000
115	0.00983	-0.01454	-0.11668	0.00000	0.00000	0.00000
116	-0.01113	-0.18595	-0.49801	0.00000	0.00000	0.00000
133	0.00500	-0.00531	-0.09501	0.00000	0.00000	0.00000
134	0.00093	-0.06080	-0.21928	0.00000	0.00000	0.00000
406	-0.40021	0.08537	-0.70341	0.00000	-0.23512	0.00000
409	0.00000	-0.11656	-0.06440	0.00000	0.00805	0.00000
410	1.24861	0.61615	-1.74174	0.00000	0.51958	0.00000
414	-0.03258	-0.01941	-0.11865	0.00000	0.03766	0.00000
518	-0.81582	0.05960	-0.47459	0.00000	-0.18363	0.00000
SUM	0.00000	1.53918	-5.80118	0.00000	0.14793	0.00000

Condition **LC20=0.9D-1.6W30**

6	0.03562	0.10367	-0.00230	0.00000	0.00151	0.00000
7	0.05610	0.00000	-0.04543	0.00000	0.00000	0.00000
8	-0.05162	0.00000	-0.05722	0.00000	0.00000	0.00000
9	0.02665	0.00000	-0.07101	0.00000	0.00000	0.00000
10	-0.29743	0.00000	-0.00832	0.00000	0.00000	0.00000
17	-0.15167	0.25143	-0.23766	0.00000	0.00046	0.00000
45	-0.09460	0.27963	-0.05884	0.00000	-0.00157	0.00000
50	-0.00061	0.10992	0.06744	0.00000	0.00043	0.00000
51	0.02060	0.00000	-0.34461	0.00000	0.00000	0.00000
52	-0.00188	0.00000	-0.13463	0.00000	0.00000	0.00000
53	0.00198	0.00000	-0.13771	0.00000	0.00000	0.00000
54	0.01053	0.00000	-0.33608	0.00000	0.00000	0.00000
55	-0.09368	0.40782	-0.29302	0.00000	0.00022	0.00000
115	0.00923	-0.02274	-0.13493	0.00000	0.00000	0.00000

116	-0.00807	-0.14997	-0.41776	0.00000	0.00000	0.00000
133	0.00498	-0.00554	-0.09553	0.00000	0.00000	0.00000
134	0.00098	-0.06017	-0.21789	0.00000	0.00000	0.00000
406	-0.42606	0.11819	-0.71625	0.00000	-0.28692	0.00000
409	0.00000	-0.13762	-0.06440	0.00000	0.00805	0.00000
410	-0.24590	0.63193	-0.88084	0.00000	-0.01281	0.00000
414	-0.03151	-0.04050	-0.10824	0.00000	0.03539	0.00000
518	-0.73563	0.05314	-0.43296	0.00000	-0.16837	0.00000
SUM	-1.97198	1.53918	-4.72817	0.00000	-0.42360	0.00000

Condition **LC21=0.9D-1.6W60**

6	0.00654	0.09880	0.00069	0.00000	0.00000	0.00000
7	-0.27524	0.00000	-0.00023	0.00000	0.00000	0.00000
8	-0.16998	0.00000	0.00214	0.00000	0.00000	0.00000
9	-0.18174	0.00000	-0.00195	0.00000	0.00000	0.00000
10	-0.89888	0.00000	0.06570	0.00000	0.00000	0.00000
17	-0.03322	0.12067	-0.00631	0.00000	0.00014	0.00000
45	-0.13081	0.29513	-0.08190	0.00000	0.00062	0.00000
50	-0.00229	0.11221	0.08837	0.00000	-0.00152	0.00000
51	-0.08782	0.00000	-0.20130	0.00000	0.00000	0.00000
52	-0.06392	0.00000	-0.08530	0.00000	0.00000	0.00000
53	-0.06946	0.00000	-0.01949	0.00000	0.00000	0.00000
54	-0.08392	0.00000	-0.21497	0.00000	0.00000	0.00000
55	0.00970	0.24244	-0.02507	0.00000	0.00021	0.00000
115	-0.07445	0.02319	0.00876	0.00000	0.00000	0.00000
116	-0.07942	-0.01815	-0.08313	0.00000	0.00000	0.00000
133	-0.07533	0.01975	0.00119	0.00000	0.00000	0.00000
134	-0.07628	0.02000	0.00182	0.00000	0.00000	0.00000
406	-0.31823	0.12307	-0.44467	0.00000	-0.23769	0.00000
409	0.00000	-0.15781	0.00000	0.00000	0.00000	0.00000
410	-0.78744	0.67530	-0.24396	0.00000	-0.18209	0.00000
414	-0.09550	-0.07045	-0.06366	0.00000	0.02187	0.00000
518	-0.50518	0.05504	-0.25464	0.00000	-0.13010	0.00000
SUM	-3.99287	1.53918	-1.55790	0.00000	-0.52857	0.00000

Condition **LC22=0.9D-1.6W90**

6	0.01054	0.09808	0.00057	0.00000	0.00004	0.00000
7	-0.28686	0.00000	-0.00226	0.00000	0.00000	0.00000
8	-0.13392	0.00000	0.00201	0.00000	0.00000	0.00000
9	-0.09231	0.00000	-0.00195	0.00000	0.00000	0.00000
10	-0.92851	0.00000	0.06533	0.00000	0.00000	0.00000
17	-0.03428	0.12562	-0.00507	0.00000	0.00003	0.00000
45	-0.12767	0.29538	-0.08667	0.00000	0.00147	0.00000
50	-0.00075	0.11683	0.10619	0.00000	-0.00226	0.00000
51	-0.13592	0.00000	-0.00255	0.00000	0.00000	0.00000
52	-0.06500	0.00000	-0.09403	0.00000	0.00000	0.00000
53	-0.06960	0.00000	-0.02561	0.00000	0.00000	0.00000
54	-0.12578	0.00000	-0.00873	0.00000	0.00000	0.00000
55	0.01383	0.19783	0.04501	0.00000	-0.00026	0.00000
115	-0.07519	0.01274	-0.01449	0.00000	0.00000	0.00000
116	-0.07557	0.02716	0.01780	0.00000	0.00000	0.00000
133	-0.07535	0.01976	0.00120	0.00000	0.00000	0.00000
134	-0.07620	0.02064	0.00324	0.00000	0.00000	0.00000
406	-0.19378	0.13337	-0.22918	0.00000	-0.17311	0.00000
409	0.00000	-0.18551	0.00000	0.00000	0.00000	0.00000
410	-1.30168	0.70504	0.36113	0.00000	-0.39721	0.00000
414	-0.08010	-0.07795	-0.02639	0.00000	0.00634	0.00000

518	-0.23749	0.05019	-0.10556	0.00000	-0.06368	0.00000
SUM	-4.09155	1.53918	0.00000	0.00000	-0.62863	0.00000

Condition **LC23=0.9D-1.6W120**

6	0.00639	0.09876	0.00069	0.00000	0.00007	0.00000
7	-0.28477	0.00000	-0.00432	0.00000	0.00000	0.00000
8	-0.16243	0.00000	0.00219	0.00000	0.00000	0.00000
9	-0.12826	0.00000	-0.00196	0.00000	0.00000	0.00000
10	-0.90420	0.00000	0.06583	0.00000	0.00000	0.00000
17	-0.03215	0.12879	-0.00363	0.00000	-0.00004	0.00000
45	-0.10983	0.29117	-0.08370	0.00000	0.00180	0.00000
50	-0.00136	0.12051	0.10661	0.00000	-0.00225	0.00000
51	-0.13443	0.00000	0.21436	0.00000	0.00000	0.00000
52	-0.06479	0.00000	-0.09649	0.00000	0.00000	0.00000
53	-0.06930	0.00000	-0.02075	0.00000	0.00000	0.00000
54	-0.12262	0.00000	0.20582	0.00000	0.00000	0.00000
55	0.02107	0.16746	0.09830	0.00000	-0.00059	0.00000
115	-0.07572	0.00420	-0.03348	0.00000	0.00000	0.00000
116	-0.07267	0.06208	0.09557	0.00000	0.00000	0.00000
133	-0.07535	0.01898	-0.00054	0.00000	0.00000	0.00000
134	-0.07611	0.02209	0.00648	0.00000	0.00000	0.00000
406	-0.04997	0.13895	0.00907	0.00000	-0.09006	0.00000
409	0.00000	-0.18630	0.00000	0.00000	0.00000	0.00000
410	-1.64017	0.71379	0.93199	0.00000	-0.55292	0.00000
414	-0.06284	-0.08831	0.01317	0.00000	-0.01076	0.00000
518	0.04662	0.04702	0.05269	0.00000	0.00801	0.00000
SUM	-3.99287	1.53918	1.55790	0.00000	-0.64674	0.00000

Condition **LC24=0.9D-1.6W150**

6	-0.01084	0.02696	0.00311	0.00000	-0.00142	0.00000
7	-0.24803	0.00000	0.04149	0.00000	0.00000	0.00000
8	-0.08906	0.00000	0.05989	0.00000	0.00000	0.00000
9	-0.08506	0.00000	0.06877	0.00000	0.00000	0.00000
10	-0.11437	0.00000	0.00779	0.00000	0.00000	0.00000
17	0.11325	-0.00557	0.23733	0.00000	-0.00050	0.00000
45	-0.12162	0.28663	-0.18533	0.00000	0.00240	0.00000
50	0.00111	0.12076	0.08748	0.00000	-0.00157	0.00000
51	-0.08283	0.00000	0.58280	0.00000	0.00000	0.00000
52	-0.00560	0.00000	-0.07132	0.00000	0.00000	0.00000
53	-0.00026	0.00000	0.03722	0.00000	0.00000	0.00000
54	-0.06787	0.00000	0.40777	0.00000	0.00000	0.00000
55	0.16728	0.06312	0.31718	0.00000	-0.00033	0.00000
115	-0.00434	0.05407	0.11879	0.00000	0.00000	0.00000
116	0.01333	0.21787	0.48261	0.00000	0.00000	0.00000
133	-0.00024	0.05330	0.11604	0.00000	0.00000	0.00000
134	0.00225	0.09690	0.21386	0.00000	0.00000	0.00000
406	0.09400	0.14983	0.26951	0.00000	-0.01882	0.00000
409	0.00000	-0.19435	0.06440	0.00000	-0.00805	0.00000
410	-1.92035	0.73970	1.58753	0.00000	-0.69917	0.00000
414	0.01358	-0.12030	0.05625	0.00000	-0.01635	0.00000
518	0.37367	0.05026	0.22499	0.00000	0.08235	0.00000
SUM	-1.97198	1.53918	4.72817	0.00000	-0.66146	0.00000

Condition **LC25=1.2D+Di+WI0**

6	0.03718	0.18714	0.00148	0.00000	0.00011	0.00000
7	0.04918	0.00000	-0.00502	0.00000	0.00000	0.00000
8	-0.08070	0.00000	0.00439	0.00000	0.00000	0.00000
9	0.04796	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.02486	0.00000	-0.00177	0.00000	0.00000	0.00000
17	0.00039	0.38341	-0.00285	0.00000	0.00002	0.00000
45	-0.18523	0.63830	-0.19427	0.00000	0.00011	0.00000
50	-0.00288	0.27866	0.15483	0.00000	-0.00012	0.00000
51	0.00472	0.00000	0.17916	0.00000	0.00000	0.00000
52	-0.00684	0.00000	-0.19088	0.00000	0.00000	0.00000
53	0.00255	0.00000	0.06993	0.00000	0.00000	0.00000
54	0.00078	0.00000	0.04907	0.00000	0.00000	0.00000
55	0.13199	0.59899	0.00374	0.00000	-0.00007	0.00000
115	0.00807	0.05369	-0.00870	0.00000	0.00000	0.00000
116	0.00570	0.06947	0.02670	0.00000	0.00000	0.00000
133	0.00717	0.07253	0.03338	0.00000	0.00000	0.00000
134	0.00481	0.05352	-0.00886	0.00000	0.00000	0.00000
406	-0.00100	0.32301	0.07866	0.00000	-0.07365	0.00000
409	0.00000	-0.58862	0.00000	0.00000	0.00000	0.00000
410	-0.09458	1.98402	0.14799	0.00000	-0.02231	0.00000
414	0.02364	-0.30669	0.00987	0.00000	-0.01729	0.00000
518	0.07194	0.14187	0.03948	0.00000	0.04337	0.00000
SUM	0.00000	3.88932	0.38300	0.00000	-0.06983	0.00000

Condition **LC26=1.2D+Di+WI30**

6	0.03726	0.18722	0.00148	0.00000	0.00010	0.00000
7	0.06641	0.00000	-0.00477	0.00000	0.00000	0.00000
8	-0.07587	0.00000	0.00439	0.00000	0.00000	0.00000
9	0.04842	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00434	0.00000	-0.00178	0.00000	0.00000	0.00000
17	0.00216	0.38296	-0.00308	0.00000	0.00003	0.00000
45	-0.18191	0.63740	-0.19426	0.00000	0.00001	0.00000
50	-0.00310	0.27835	0.15288	0.00000	-0.00002	0.00000
51	0.01086	0.00000	0.17092	0.00000	0.00000	0.00000
52	-0.00669	0.00000	-0.19015	0.00000	0.00000	0.00000
53	0.00258	0.00000	0.06835	0.00000	0.00000	0.00000
54	0.00613	0.00000	0.03912	0.00000	0.00000	0.00000
55	0.13469	0.60426	-0.00339	0.00000	-0.00003	0.00000
115	0.00815	0.05480	-0.00623	0.00000	0.00000	0.00000
116	0.00532	0.06475	0.01618	0.00000	0.00000	0.00000
133	0.00717	0.07257	0.03346	0.00000	0.00000	0.00000
134	0.00480	0.05341	-0.00910	0.00000	0.00000	0.00000
406	0.00306	0.31924	0.08173	0.00000	-0.06688	0.00000
409	0.00000	-0.58676	0.00000	0.00000	0.00000	0.00000
410	0.08310	1.98247	0.04785	0.00000	0.04115	0.00000
414	0.02365	-0.30383	0.00887	0.00000	-0.01715	0.00000
518	0.06414	0.14249	0.03549	0.00000	0.04203	0.00000
SUM	0.24466	3.88932	0.24466	0.00000	-0.00074	0.00000

Condition **LC27=1.2D+Di+WI60**

6	0.03727	0.18723	0.00148	0.00000	0.00010	0.00000
7	0.06755	0.00000	-0.00474	0.00000	0.00000	0.00000
8	-0.07546	0.00000	0.00439	0.00000	0.00000	0.00000
9	0.04842	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00431	0.00000	-0.00178	0.00000	0.00000	0.00000
17	0.00227	0.38278	-0.00302	0.00000	0.00004	0.00000
45	-0.18332	0.63726	-0.19266	0.00000	-0.00003	0.00000

50	-0.00318	0.27837	0.15261	0.00000	0.00001	0.00000
51	0.01266	0.00000	0.17299	0.00000	0.00000	0.00000
52	-0.00664	0.00000	-0.19020	0.00000	0.00000	0.00000
53	0.00259	0.00000	0.06771	0.00000	0.00000	0.00000
54	0.00778	0.00000	0.04275	0.00000	0.00000	0.00000
55	0.13463	0.60523	-0.00478	0.00000	-0.00001	0.00000
115	0.00816	0.05506	-0.00564	0.00000	0.00000	0.00000
116	0.00524	0.06382	0.01411	0.00000	0.00000	0.00000
133	0.00717	0.07258	0.03347	0.00000	0.00000	0.00000
134	0.00480	0.05340	-0.00914	0.00000	0.00000	0.00000
406	-0.00893	0.31965	0.06247	0.00000	-0.07474	0.00000
409	0.00000	-0.58530	0.00000	0.00000	0.00000	0.00000
410	0.06973	1.97834	0.03443	0.00000	0.03826	0.00000
414	0.02230	-0.30149	0.00608	0.00000	-0.01585	0.00000
518	0.04418	0.14240	0.02430	0.00000	0.03682	0.00000
SUM	0.20152	3.88932	0.20153	0.00000	-0.01541	0.00000

Condition **LC28=1.2D+Di+WI90**

6	0.03730	0.18723	0.00148	0.00000	0.00010	0.00000
7	0.07366	0.00000	-0.00442	0.00000	0.00000	0.00000
8	-0.07429	0.00000	0.00439	0.00000	0.00000	0.00000
9	0.04834	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.01455	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00288	0.38210	-0.00321	0.00000	0.00005	0.00000
45	-0.18282	0.63709	-0.19332	0.00000	-0.00014	0.00000
50	-0.00339	0.27774	0.15018	0.00000	0.00012	0.00000
51	0.01929	0.00000	0.14956	0.00000	0.00000	0.00000
52	-0.00650	0.00000	-0.18908	0.00000	0.00000	0.00000
53	0.00261	0.00000	0.06523	0.00000	0.00000	0.00000
54	0.01353	0.00000	0.01712	0.00000	0.00000	0.00000
55	0.13493	0.61167	-0.01457	0.00000	0.00005	0.00000
115	0.00826	0.05664	-0.00214	0.00000	0.00000	0.00000
116	0.00470	0.05740	-0.00019	0.00000	0.00000	0.00000
133	0.00717	0.07265	0.03363	0.00000	0.00000	0.00000
134	0.00479	0.05321	-0.00956	0.00000	0.00000	0.00000
406	-0.02333	0.31828	0.03723	0.00000	-0.08190	0.00000
409	0.00000	-0.58204	0.00000	0.00000	0.00000	0.00000
410	0.14079	1.97423	-0.04525	0.00000	0.06772	0.00000
414	0.02050	-0.30000	0.00160	0.00000	-0.01402	0.00000
518	0.01203	0.14314	0.00641	0.00000	0.02890	0.00000
SUM	0.25500	3.88932	0.00000	0.00000	0.00087	0.00000

Condition **LC29=1.2D+Di+WI120**

6	0.03726	0.18716	0.00148	0.00000	0.00009	0.00000
7	0.06529	0.00000	-0.00415	0.00000	0.00000	0.00000
8	-0.07796	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04823	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00148	0.00000	-0.00180	0.00000	0.00000	0.00000
17	0.00200	0.38168	-0.00342	0.00000	0.00006	0.00000
45	-0.18405	0.63775	-0.19507	0.00000	-0.00019	0.00000
50	-0.00331	0.27720	0.15012	0.00000	0.00011	0.00000
51	0.01899	0.00000	0.12357	0.00000	0.00000	0.00000
52	-0.00653	0.00000	-0.18874	0.00000	0.00000	0.00000
53	0.00257	0.00000	0.06117	0.00000	0.00000	0.00000
54	0.01308	0.00000	-0.00972	0.00000	0.00000	0.00000
55	0.13263	0.61584	-0.02204	0.00000	0.00010	0.00000
115	0.00834	0.05779	0.00042	0.00000	0.00000	0.00000

116	0.00428	0.05256	-0.01096	0.00000	0.00000	0.00000
133	0.00717	0.07271	0.03378	0.00000	0.00000	0.00000
134	0.00477	0.05303	-0.00995	0.00000	0.00000	0.00000
406	-0.04211	0.31780	0.00619	0.00000	-0.09292	0.00000
409	0.00000	-0.58189	0.00000	0.00000	0.00000	0.00000
410	0.17559	1.97217	-0.11602	0.00000	0.08496	0.00000
414	0.01827	-0.29814	-0.00349	0.00000	-0.01182	0.00000
518	-0.02448	0.14366	-0.01396	0.00000	0.01968	0.00000
SUM	0.20152	3.88932	-0.20153	0.00000	0.00007	0.00000

Condition **LC30=1.2D+Di+WI150**

6	0.03725	0.18715	0.00148	0.00000	0.00009	0.00000
7	0.06530	0.00000	-0.00412	0.00000	0.00000	0.00000
8	-0.07813	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04821	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00181	0.00000	-0.00180	0.00000	0.00000	0.00000
17	0.00200	0.38167	-0.00350	0.00000	0.00006	0.00000
45	-0.18374	0.63768	-0.19469	0.00000	-0.00018	0.00000
50	-0.00322	0.27729	0.15121	0.00000	0.00009	0.00000
51	0.01695	0.00000	0.12595	0.00000	0.00000	0.00000
52	-0.00658	0.00000	-0.18923	0.00000	0.00000	0.00000
53	0.00255	0.00000	0.05937	0.00000	0.00000	0.00000
54	0.01124	0.00000	-0.00591	0.00000	0.00000	0.00000
55	0.13254	0.61626	-0.02283	0.00000	0.00010	0.00000
115	0.00835	0.05789	0.00065	0.00000	0.00000	0.00000
116	0.00424	0.05204	-0.01213	0.00000	0.00000	0.00000
133	0.00717	0.07272	0.03380	0.00000	0.00000	0.00000
134	0.00477	0.05301	-0.01000	0.00000	0.00000	0.00000
406	-0.04388	0.31663	0.00246	0.00000	-0.09280	0.00000
409	0.00000	-0.58195	0.00000	0.00000	0.00000	0.00000
410	0.23205	1.97131	-0.15379	0.00000	0.10538	0.00000
414	0.01791	-0.29617	-0.00452	0.00000	-0.01143	0.00000
518	-0.03213	0.14379	-0.01809	0.00000	0.01788	0.00000
SUM	0.24466	3.88932	-0.24466	0.00000	0.01919	0.00000

Condition **LC31=1.2D+Di-WI0**

6	0.03719	0.18708	0.00148	0.00000	0.00009	0.00000
7	0.04903	0.00000	-0.00405	0.00000	0.00000	0.00000
8	-0.08350	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04555	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.02774	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00021	0.38144	-0.00345	0.00000	0.00007	0.00000
45	-0.18915	0.63879	-0.19439	0.00000	-0.00018	0.00000
50	-0.00306	0.27707	0.15231	0.00000	0.00004	0.00000
51	0.01395	0.00000	0.10988	0.00000	0.00000	0.00000
52	-0.00667	0.00000	-0.18950	0.00000	0.00000	0.00000
53	0.00250	0.00000	0.05682	0.00000	0.00000	0.00000
54	0.00853	0.00000	-0.01959	0.00000	0.00000	0.00000
55	0.12876	0.61691	-0.02535	0.00000	0.00013	0.00000
115	0.00837	0.05830	0.00156	0.00000	0.00000	0.00000
116	0.00409	0.05044	-0.01570	0.00000	0.00000	0.00000
133	0.00717	0.07274	0.03385	0.00000	0.00000	0.00000
134	0.00477	0.05295	-0.01013	0.00000	0.00000	0.00000
406	-0.07640	0.31882	-0.04846	0.00000	-0.11542	0.00000
409	0.00000	-0.58089	0.00000	0.00000	0.00000	0.00000
410	0.14420	1.96386	-0.16971	0.00000	0.07984	0.00000
414	0.01437	-0.29169	-0.01157	0.00000	-0.00809	0.00000

518	-0.08217	0.14350	-0.04627	0.00000	0.00461	0.00000
SUM	0.00000	3.88932	-0.38300	0.00000	-0.03890	0.00000

Condition **LC32=1.2D+Di-WI30**

6	0.03711	0.18700	0.00148	0.00000	0.00009	0.00000
7	0.03241	0.00000	-0.00429	0.00000	0.00000	0.00000
8	-0.08757	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04286	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.05577	0.00000	-0.00180	0.00000	0.00000	0.00000
17	-0.00161	0.38188	-0.00322	0.00000	0.00006	0.00000
45	-0.19275	0.63970	-0.19418	0.00000	-0.00008	0.00000
50	-0.00283	0.27739	0.15427	0.00000	-0.00006	0.00000
51	0.00782	0.00000	0.11774	0.00000	0.00000	0.00000
52	-0.00681	0.00000	-0.19024	0.00000	0.00000	0.00000
53	0.00247	0.00000	0.05872	0.00000	0.00000	0.00000
54	0.00318	0.00000	-0.00978	0.00000	0.00000	0.00000
55	0.12606	0.61164	-0.01822	0.00000	0.00009	0.00000
115	0.00829	0.05721	-0.00087	0.00000	0.00000	0.00000
116	0.00448	0.05514	-0.00521	0.00000	0.00000	0.00000
133	0.00717	0.07271	0.03377	0.00000	0.00000	0.00000
134	0.00477	0.05305	-0.00992	0.00000	0.00000	0.00000
406	-0.08047	0.32261	-0.05153	0.00000	-0.12220	0.00000
409	0.00000	-0.58276	0.00000	0.00000	0.00000	0.00000
410	-0.03348	1.96543	-0.06957	0.00000	0.01639	0.00000
414	0.01436	-0.29453	-0.01057	0.00000	-0.00823	0.00000
518	-0.07437	0.14286	-0.04228	0.00000	0.00594	0.00000
SUM	-0.24466	3.88932	-0.24466	0.00000	-0.10799	0.00000

Condition **LC33=1.2D+Di-WI60**

6	0.03711	0.18700	0.00148	0.00000	0.00009	0.00000
7	0.03143	0.00000	-0.00433	0.00000	0.00000	0.00000
8	-0.08788	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04247	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.05555	0.00000	-0.00180	0.00000	0.00000	0.00000
17	-0.00172	0.38205	-0.00328	0.00000	0.00006	0.00000
45	-0.19141	0.63984	-0.19573	0.00000	-0.00005	0.00000
50	-0.00276	0.27737	0.15453	0.00000	-0.00009	0.00000
51	0.00602	0.00000	0.11557	0.00000	0.00000	0.00000
52	-0.00686	0.00000	-0.19020	0.00000	0.00000	0.00000
53	0.00246	0.00000	0.05944	0.00000	0.00000	0.00000
54	0.00153	0.00000	-0.01346	0.00000	0.00000	0.00000
55	0.12613	0.61068	-0.01682	0.00000	0.00007	0.00000
115	0.00828	0.05694	-0.00146	0.00000	0.00000	0.00000
116	0.00456	0.05608	-0.00313	0.00000	0.00000	0.00000
133	0.00717	0.07270	0.03376	0.00000	0.00000	0.00000
134	0.00478	0.05307	-0.00988	0.00000	0.00000	0.00000
406	-0.06847	0.32219	-0.03227	0.00000	-0.11433	0.00000
409	0.00000	-0.58422	0.00000	0.00000	0.00000	0.00000
410	-0.02010	1.96955	-0.05615	0.00000	0.01927	0.00000
414	0.01571	-0.29686	-0.00777	0.00000	-0.00952	0.00000
518	-0.05441	0.14294	-0.03109	0.00000	0.01116	0.00000
SUM	-0.20153	3.88932	-0.20153	0.00000	-0.09333	0.00000

Condition **LC34=1.2D+Di-WI90**

6	0.03707	0.18696	0.00148	0.00000	0.00010	0.00000
7	0.02464	0.00000	-0.00465	0.00000	0.00000	0.00000
8	-0.08907	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04360	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.06633	0.00000	-0.00179	0.00000	0.00000	0.00000
17	-0.00236	0.38274	-0.00309	0.00000	0.00004	0.00000
45	-0.19158	0.64000	-0.19530	0.00000	0.00007	0.00000
50	-0.00254	0.27800	0.15696	0.00000	-0.00019	0.00000
51	-0.00061	0.00000	0.13940	0.00000	0.00000	0.00000
52	-0.00700	0.00000	-0.19131	0.00000	0.00000	0.00000
53	0.00244	0.00000	0.06158	0.00000	0.00000	0.00000
54	-0.00422	0.00000	0.01234	0.00000	0.00000	0.00000
55	0.12574	0.60427	-0.00703	0.00000	0.00001	0.00000
115	0.00818	0.05540	-0.00489	0.00000	0.00000	0.00000
116	0.00510	0.06249	0.01115	0.00000	0.00000	0.00000
133	0.00717	0.07264	0.03363	0.00000	0.00000	0.00000
134	0.00479	0.05322	-0.00953	0.00000	0.00000	0.00000
406	-0.05408	0.32357	-0.00703	0.00000	-0.10717	0.00000
409	0.00000	-0.58749	0.00000	0.00000	0.00000	0.00000
410	-0.09117	1.97366	0.02352	0.00000	-0.01019	0.00000
414	0.01751	-0.29835	-0.00330	0.00000	-0.01135	0.00000
518	-0.02227	0.14221	-0.01319	0.00000	0.01907	0.00000
SUM	-0.25500	3.88932	0.00000	0.00000	-0.10961	0.00000

Condition **LC35=1.2D+Di-WI120**

6	0.03710	0.18702	0.00148	0.00000	0.00010	0.00000
7	0.03187	0.00000	-0.00491	0.00000	0.00000	0.00000
8	-0.08621	0.00000	0.00438	0.00000	0.00000	0.00000
9	0.04680	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.05488	0.00000	-0.00178	0.00000	0.00000	0.00000
17	-0.00146	0.38320	-0.00289	0.00000	0.00003	0.00000
45	-0.18982	0.63931	-0.19394	0.00000	0.00012	0.00000
50	-0.00263	0.27853	0.15702	0.00000	-0.00019	0.00000
51	-0.00032	0.00000	0.16609	0.00000	0.00000	0.00000
52	-0.00697	0.00000	-0.19164	0.00000	0.00000	0.00000
53	0.00248	0.00000	0.06506	0.00000	0.00000	0.00000
54	-0.00378	0.00000	0.03946	0.00000	0.00000	0.00000
55	0.12797	0.60011	0.00043	0.00000	-0.00004	0.00000
115	0.00810	0.05425	-0.00746	0.00000	0.00000	0.00000
116	0.00551	0.06733	0.02194	0.00000	0.00000	0.00000
133	0.00717	0.07258	0.03349	0.00000	0.00000	0.00000
134	0.00480	0.05338	-0.00917	0.00000	0.00000	0.00000
406	-0.03530	0.32405	0.02401	0.00000	-0.09615	0.00000
409	0.00000	-0.58764	0.00000	0.00000	0.00000	0.00000
410	-0.12597	1.97571	0.09429	0.00000	-0.02742	0.00000
414	0.01974	-0.30021	0.00179	0.00000	-0.01356	0.00000
518	0.01424	0.14169	0.00718	0.00000	0.02829	0.00000
SUM	-0.20153	3.88932	0.20153	0.00000	-0.10881	0.00000

Condition **LC36=1.2D+Di-WI150**

6	0.03710	0.18702	0.00148	0.00000	0.00010	0.00000
7	0.03187	0.00000	-0.00494	0.00000	0.00000	0.00000
8	-0.08601	0.00000	0.00439	0.00000	0.00000	0.00000
9	0.04678	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.05518	0.00000	-0.00178	0.00000	0.00000	0.00000
17	-0.00146	0.38320	-0.00281	0.00000	0.00003	0.00000
45	-0.19012	0.63938	-0.19432	0.00000	0.00011	0.00000

50	-0.00271	0.27843	0.15593	0.00000	-0.00016	0.00000
51	0.00172	0.00000	0.16372	0.00000	0.00000	0.00000
52	-0.00692	0.00000	-0.19115	0.00000	0.00000	0.00000
53	0.00250	0.00000	0.06687	0.00000	0.00000	0.00000
54	-0.00194	0.00000	0.03565	0.00000	0.00000	0.00000
55	0.12807	0.59969	0.00122	0.00000	-0.00004	0.00000
115	0.00809	0.05415	-0.00768	0.00000	0.00000	0.00000
116	0.00555	0.06786	0.02311	0.00000	0.00000	0.00000
133	0.00717	0.07257	0.03347	0.00000	0.00000	0.00000
134	0.00480	0.05341	-0.00911	0.00000	0.00000	0.00000
406	-0.03352	0.32523	0.02775	0.00000	-0.09627	0.00000
409	0.00000	-0.58760	0.00000	0.00000	0.00000	0.00000
410	-0.18243	1.97658	0.13206	0.00000	-0.04784	0.00000
414	0.02010	-0.30217	0.00283	0.00000	-0.01395	0.00000
518	0.02190	0.14157	0.01131	0.00000	0.03010	0.00000
SUM	-0.24466	3.88932	0.24466	0.00000	-0.12793	0.00000

Condition **LC37=0.9D**

6	0.01243	0.06536	0.00039	0.00000	0.00003	0.00000
7	0.01668	0.00000	-0.00131	0.00000	0.00000	0.00000
8	-0.02934	0.00000	0.00134	0.00000	0.00000	0.00000
9	0.01518	0.00000	-0.00110	0.00000	0.00000	0.00000
10	-0.00510	0.00000	-0.00045	0.00000	0.00000	0.00000
17	0.00054	0.12269	-0.00110	0.00000	0.00001	0.00000
45	-0.08808	0.27405	-0.08446	0.00000	-0.00001	0.00000
50	-0.00113	0.11579	0.06766	0.00000	-0.00002	0.00000
51	0.00341	0.00000	0.05839	0.00000	0.00000	0.00000
52	-0.00272	0.00000	-0.08159	0.00000	0.00000	0.00000
53	0.00108	0.00000	0.02897	0.00000	0.00000	0.00000
54	0.00206	0.00000	0.00818	0.00000	0.00000	0.00000
55	0.06643	0.25382	-0.00666	0.00000	0.00003	0.00000
115	0.00269	0.01856	-0.00160	0.00000	0.00000	0.00000
116	0.00183	0.02162	0.00526	0.00000	0.00000	0.00000
133	0.00239	0.02413	0.01082	0.00000	0.00000	0.00000
134	0.00163	0.01802	-0.00273	0.00000	0.00000	0.00000
406	-0.01218	0.10858	0.00459	0.00000	-0.02943	0.00000
409	0.00000	-0.15814	0.00000	0.00000	0.00000	0.00000
410	0.00810	0.70742	-0.00312	0.00000	0.00867	0.00000
414	0.00577	-0.08927	-0.00029	0.00000	-0.00385	0.00000
518	-0.00169	0.05656	-0.00117	0.00000	0.00726	0.00000
SUM	0.00000	1.53918	0.00000	0.00000	-0.01730	0.00000

Condition **LC38=1.2D**

6	0.01657	0.08714	0.00053	0.00000	0.00004	0.00000
7	0.02224	0.00000	-0.00175	0.00000	0.00000	0.00000
8	-0.03912	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.02024	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.00679	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00073	0.16358	-0.00147	0.00000	0.00002	0.00000
45	-0.11745	0.36539	-0.11262	0.00000	-0.00002	0.00000
50	-0.00151	0.15439	0.09022	0.00000	-0.00003	0.00000
51	0.00455	0.00000	0.07787	0.00000	0.00000	0.00000
52	-0.00362	0.00000	-0.10880	0.00000	0.00000	0.00000
53	0.00145	0.00000	0.03863	0.00000	0.00000	0.00000
54	0.00275	0.00000	0.01090	0.00000	0.00000	0.00000
55	0.08858	0.33843	-0.00888	0.00000	0.00004	0.00000
115	0.00359	0.02475	-0.00213	0.00000	0.00000	0.00000

116	0.00244	0.02882	0.00701	0.00000	0.00000	0.00000
133	0.00319	0.03217	0.01443	0.00000	0.00000	0.00000
134	0.00218	0.02403	-0.00365	0.00000	0.00000	0.00000
406	-0.01623	0.14476	0.00612	0.00000	-0.03924	0.00000
409	0.00000	-0.21084	0.00000	0.00000	0.00000	0.00000
410	0.01079	0.94321	-0.00416	0.00000	0.01156	0.00000
414	0.00770	-0.11902	-0.00039	0.00000	-0.00513	0.00000
518	-0.00226	0.07541	-0.00156	0.00000	0.00968	0.00000
SUM	0.00000	2.05224	0.00000	0.00000	-0.02307	0.00000

Condition **LC41=1.2D+WL0**

6	0.01657	0.08715	0.00053	0.00000	0.00005	0.00000
7	0.02240	0.00000	-0.00189	0.00000	0.00000	0.00000
8	-0.03866	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.02024	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.00628	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00075	0.16385	-0.00138	0.00000	0.00001	0.00000
45	-0.11702	0.36535	-0.11264	0.00000	0.00002	0.00000
50	-0.00149	0.15460	0.09051	0.00000	-0.00005	0.00000
51	0.00334	0.00000	0.08666	0.00000	0.00000	0.00000
52	-0.00364	0.00000	-0.10895	0.00000	0.00000	0.00000
53	0.00145	0.00000	0.04056	0.00000	0.00000	0.00000
54	0.00173	0.00000	0.01953	0.00000	0.00000	0.00000
55	0.08902	0.33595	-0.00486	0.00000	0.00001	0.00000
115	0.00355	0.02411	-0.00355	0.00000	0.00000	0.00000
116	0.00266	0.03145	0.01286	0.00000	0.00000	0.00000
133	0.00319	0.03214	0.01436	0.00000	0.00000	0.00000
134	0.00218	0.02411	-0.00347	0.00000	0.00000	0.00000
406	-0.00433	0.14545	0.02610	0.00000	-0.03259	0.00000
409	0.00000	-0.21207	0.00000	0.00000	0.00000	0.00000
410	-0.02669	0.94602	0.04311	0.00000	-0.00409	0.00000
414	0.00916	-0.12110	0.00296	0.00000	-0.00659	0.00000
518	0.02185	0.07523	0.01184	0.00000	0.01577	0.00000
SUM	0.00000	2.05224	0.11200	0.00000	-0.02745	0.00000

Condition **LC42=1.2D+WL30**

6	0.01659	0.08718	0.00053	0.00000	0.00004	0.00000
7	0.02708	0.00000	-0.00182	0.00000	0.00000	0.00000
8	-0.03747	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.02056	0.00000	-0.00147	0.00000	0.00000	0.00000
10	0.00161	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00125	0.16373	-0.00144	0.00000	0.00002	0.00000
45	-0.11602	0.36509	-0.11262	0.00000	-0.00001	0.00000
50	-0.00154	0.15452	0.09004	0.00000	-0.00002	0.00000
51	0.00488	0.00000	0.08482	0.00000	0.00000	0.00000
52	-0.00361	0.00000	-0.10879	0.00000	0.00000	0.00000
53	0.00146	0.00000	0.04008	0.00000	0.00000	0.00000
54	0.00307	0.00000	0.01730	0.00000	0.00000	0.00000
55	0.08973	0.33736	-0.00676	0.00000	0.00002	0.00000
115	0.00357	0.02440	-0.00291	0.00000	0.00000	0.00000
116	0.00256	0.03019	0.01006	0.00000	0.00000	0.00000
133	0.00319	0.03215	0.01438	0.00000	0.00000	0.00000
134	0.00218	0.02409	-0.00351	0.00000	0.00000	0.00000
406	-0.00325	0.14427	0.02684	0.00000	-0.03064	0.00000
409	0.00000	-0.21148	0.00000	0.00000	0.00000	0.00000
410	0.02857	0.94594	0.01374	0.00000	0.01534	0.00000
414	0.00914	-0.12068	0.00263	0.00000	-0.00652	0.00000

518	0.01928	0.07548	0.01053	0.00000	0.01529	0.00000
SUM	0.07283	2.05224	0.07283	0.00000	-0.00647	0.00000

Condition **LC43=1.2D+WL60**

6	0.01660	0.08718	0.00053	0.00000	0.00004	0.00000
7	0.02728	0.00000	-0.00181	0.00000	0.00000	0.00000
8	-0.03742	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.02056	0.00000	-0.00147	0.00000	0.00000	0.00000
10	0.00147	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00126	0.16368	-0.00144	0.00000	0.00002	0.00000
45	-0.11642	0.36505	-0.11216	0.00000	-0.00002	0.00000
50	-0.00157	0.15452	0.08997	0.00000	-0.00001	0.00000
51	0.00541	0.00000	0.08539	0.00000	0.00000	0.00000
52	-0.00359	0.00000	-0.10880	0.00000	0.00000	0.00000
53	0.00146	0.00000	0.03987	0.00000	0.00000	0.00000
54	0.00355	0.00000	0.01830	0.00000	0.00000	0.00000
55	0.08974	0.33769	-0.00725	0.00000	0.00003	0.00000
115	0.00357	0.02449	-0.00271	0.00000	0.00000	0.00000
116	0.00253	0.02987	0.00934	0.00000	0.00000	0.00000
133	0.00319	0.03215	0.01438	0.00000	0.00000	0.00000
134	0.00218	0.02409	-0.00353	0.00000	0.00000	0.00000
406	-0.00782	0.14438	0.01944	0.00000	-0.03360	0.00000
409	0.00000	-0.21051	0.00000	0.00000	0.00000	0.00000
410	0.02294	0.94357	0.00813	0.00000	0.01410	0.00000
414	0.00862	-0.11926	0.00156	0.00000	-0.00602	0.00000
518	0.01161	0.07534	0.00623	0.00000	0.01329	0.00000
SUM	0.05515	2.05224	0.05515	0.00000	-0.01218	0.00000

Condition **LC44=1.2D+WL90**

6	0.01660	0.08719	0.00053	0.00000	0.00004	0.00000
7	0.02896	0.00000	-0.00172	0.00000	0.00000	0.00000
8	-0.03715	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.02068	0.00000	-0.00147	0.00000	0.00000	0.00000
10	0.00396	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00143	0.16349	-0.00149	0.00000	0.00002	0.00000
45	-0.11647	0.36502	-0.11225	0.00000	-0.00005	0.00000
50	-0.00163	0.15435	0.08927	0.00000	0.00002	0.00000
51	0.00733	0.00000	0.07909	0.00000	0.00000	0.00000
52	-0.00355	0.00000	-0.10849	0.00000	0.00000	0.00000
53	0.00147	0.00000	0.03925	0.00000	0.00000	0.00000
54	0.00523	0.00000	0.01148	0.00000	0.00000	0.00000
55	0.08979	0.33941	-0.00989	0.00000	0.00005	0.00000
115	0.00360	0.02491	-0.00178	0.00000	0.00000	0.00000
116	0.00239	0.02814	0.00549	0.00000	0.00000	0.00000
133	0.00319	0.03217	0.01442	0.00000	0.00000	0.00000
134	0.00218	0.02404	-0.00363	0.00000	0.00000	0.00000
406	-0.01203	0.14404	0.01209	0.00000	-0.03574	0.00000
409	0.00000	-0.20980	0.00000	0.00000	0.00000	0.00000
410	0.04358	0.94303	-0.01341	0.00000	0.02260	0.00000
414	0.00810	-0.11930	0.00026	0.00000	-0.00550	0.00000
518	0.00234	0.07556	0.00106	0.00000	0.01101	0.00000
SUM	0.07000	2.05224	0.00000	0.00000	-0.00755	0.00000

Condition **LC45=1.2D+WL120**

6	0.01659	0.08716	0.00053	0.00000	0.00004	0.00000
7	0.02673	0.00000	-0.00165	0.00000	0.00000	0.00000
8	-0.03808	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.02055	0.00000	-0.00147	0.00000	0.00000	0.00000
10	0.00069	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00120	0.16338	-0.00154	0.00000	0.00002	0.00000
45	-0.11670	0.36519	-0.11276	0.00000	-0.00006	0.00000
50	-0.00160	0.15421	0.08932	0.00000	0.00001	0.00000
51	0.00709	0.00000	0.07220	0.00000	0.00000	0.00000
52	-0.00356	0.00000	-0.10842	0.00000	0.00000	0.00000
53	0.00146	0.00000	0.03807	0.00000	0.00000	0.00000
54	0.00496	0.00000	0.00438	0.00000	0.00000	0.00000
55	0.08922	0.34053	-0.01189	0.00000	0.00006	0.00000
115	0.00362	0.02522	-0.00108	0.00000	0.00000	0.00000
116	0.00228	0.02685	0.00261	0.00000	0.00000	0.00000
133	0.00319	0.03219	0.01446	0.00000	0.00000	0.00000
134	0.00217	0.02399	-0.00374	0.00000	0.00000	0.00000
406	-0.01718	0.14383	0.00359	0.00000	-0.03874	0.00000
409	0.00000	-0.20952	0.00000	0.00000	0.00000	0.00000
410	0.05273	0.94275	-0.03329	0.00000	0.02710	0.00000
414	0.00749	-0.11929	-0.00113	0.00000	-0.00489	0.00000
518	-0.00769	0.07576	-0.00453	0.00000	0.00847	0.00000
SUM	0.05515	2.05224	-0.05515	0.00000	-0.00798	0.00000

Condition **LC46=1.2D+WL150**

6	0.01659	0.08716	0.00053	0.00000	0.00004	0.00000
7	0.02682	0.00000	-0.00164	0.00000	0.00000	0.00000
8	-0.03813	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.02057	0.00000	-0.00147	0.00000	0.00000	0.00000
10	0.00092	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00120	0.16338	-0.00158	0.00000	0.00002	0.00000
45	-0.11659	0.36516	-0.11266	0.00000	-0.00006	0.00000
50	-0.00157	0.15424	0.08963	0.00000	0.00001	0.00000
51	0.00652	0.00000	0.07287	0.00000	0.00000	0.00000
52	-0.00358	0.00000	-0.10856	0.00000	0.00000	0.00000
53	0.00145	0.00000	0.03752	0.00000	0.00000	0.00000
54	0.00444	0.00000	0.00545	0.00000	0.00000	0.00000
55	0.08921	0.34071	-0.01222	0.00000	0.00006	0.00000
115	0.00362	0.02526	-0.00100	0.00000	0.00000	0.00000
116	0.00226	0.02663	0.00213	0.00000	0.00000	0.00000
133	0.00319	0.03219	0.01447	0.00000	0.00000	0.00000
134	0.00217	0.02398	-0.00376	0.00000	0.00000	0.00000
406	-0.01788	0.14343	0.00217	0.00000	-0.03874	0.00000
409	0.00000	-0.20998	0.00000	0.00000	0.00000	0.00000
410	0.07491	0.94237	-0.04826	0.00000	0.03521	0.00000
414	0.00734	-0.11798	-0.00153	0.00000	-0.00474	0.00000
518	-0.01064	0.07568	-0.00612	0.00000	0.00777	0.00000
SUM	0.07283	2.05224	-0.07283	0.00000	-0.00042	0.00000

Condition **LC47=1.2D-WL0**

6	0.01657	0.08713	0.00053	0.00000	0.00004	0.00000
7	0.02209	0.00000	-0.00162	0.00000	0.00000	0.00000
8	-0.03958	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.02024	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.00731	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00070	0.16332	-0.00156	0.00000	0.00002	0.00000
45	-0.11788	0.36544	-0.11260	0.00000	-0.00006	0.00000

50	-0.00153	0.15418	0.08993	0.00000	0.00000	0.00000
51	0.00576	0.00000	0.06909	0.00000	0.00000	0.00000
52	-0.00360	0.00000	-0.10865	0.00000	0.00000	0.00000
53	0.00144	0.00000	0.03670	0.00000	0.00000	0.00000
54	0.00376	0.00000	0.00226	0.00000	0.00000	0.00000
55	0.08813	0.34091	-0.01291	0.00000	0.00007	0.00000
115	0.00363	0.02539	-0.00071	0.00000	0.00000	0.00000
116	0.00222	0.02619	0.00115	0.00000	0.00000	0.00000
133	0.00319	0.03220	0.01449	0.00000	0.00000	0.00000
134	0.00217	0.02395	-0.00383	0.00000	0.00000	0.00000
406	-0.02814	0.14408	-0.01387	0.00000	-0.04588	0.00000
409	0.00000	-0.20960	0.00000	0.00000	0.00000	0.00000
410	0.04828	0.94041	-0.05143	0.00000	0.02721	0.00000
414	0.00623	-0.11694	-0.00374	0.00000	-0.00368	0.00000
518	-0.02637	0.07558	-0.01496	0.00000	0.00360	0.00000
SUM	0.00000	2.05224	-0.11200	0.00000	-0.01869	0.00000

Condition **LC48=1.2D-WL30**

6	0.01655	0.08710	0.00053	0.00000	0.00004	0.00000
7	0.01741	0.00000	-0.00168	0.00000	0.00000	0.00000
8	-0.04077	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01992	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.01520	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00020	0.16344	-0.00150	0.00000	0.00002	0.00000
45	-0.11888	0.36569	-0.11263	0.00000	-0.00003	0.00000
50	-0.00148	0.15426	0.09040	0.00000	-0.00003	0.00000
51	0.00422	0.00000	0.07092	0.00000	0.00000	0.00000
52	-0.00364	0.00000	-0.10882	0.00000	0.00000	0.00000
53	0.00143	0.00000	0.03718	0.00000	0.00000	0.00000
54	0.00242	0.00000	0.00450	0.00000	0.00000	0.00000
55	0.08742	0.33951	-0.01100	0.00000	0.00006	0.00000
115	0.00361	0.02510	-0.00135	0.00000	0.00000	0.00000
116	0.00232	0.02745	0.00395	0.00000	0.00000	0.00000
133	0.00319	0.03219	0.01448	0.00000	0.00000	0.00000
134	0.00217	0.02397	-0.00378	0.00000	0.00000	0.00000
406	-0.02922	0.14526	-0.01461	0.00000	-0.04784	0.00000
409	0.00000	-0.21019	0.00000	0.00000	0.00000	0.00000
410	-0.00698	0.94048	-0.02206	0.00000	0.00779	0.00000
414	0.00625	-0.11736	-0.00341	0.00000	-0.00375	0.00000
518	-0.02380	0.07533	-0.01365	0.00000	0.00407	0.00000
SUM	-0.07283	2.05224	-0.07283	0.00000	-0.03967	0.00000

Condition **LC49=1.2D-WL60**

6	0.01655	0.08710	0.00053	0.00000	0.00004	0.00000
7	0.01721	0.00000	-0.00170	0.00000	0.00000	0.00000
8	-0.04082	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01992	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.01506	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00019	0.16349	-0.00150	0.00000	0.00002	0.00000
45	-0.11848	0.36573	-0.11308	0.00000	-0.00002	0.00000
50	-0.00145	0.15425	0.09047	0.00000	-0.00004	0.00000
51	0.00370	0.00000	0.07035	0.00000	0.00000	0.00000
52	-0.00365	0.00000	-0.10880	0.00000	0.00000	0.00000
53	0.00143	0.00000	0.03739	0.00000	0.00000	0.00000
54	0.00194	0.00000	0.00350	0.00000	0.00000	0.00000
55	0.08742	0.33918	-0.01051	0.00000	0.00005	0.00000
115	0.00360	0.02501	-0.00155	0.00000	0.00000	0.00000

116	0.00235	0.02777	0.00468	0.00000	0.00000	0.00000
133	0.00319	0.03219	0.01447	0.00000	0.00000	0.00000
134	0.00217	0.02398	-0.00377	0.00000	0.00000	0.00000
406	-0.02465	0.14515	-0.00721	0.00000	-0.04487	0.00000
409	0.00000	-0.21116	0.00000	0.00000	0.00000	0.00000
410	-0.00136	0.94286	-0.01645	0.00000	0.00902	0.00000
414	0.00677	-0.11878	-0.00234	0.00000	-0.00425	0.00000
518	-0.01613	0.07547	-0.00936	0.00000	0.00608	0.00000
SUM	-0.05516	2.05224	-0.05515	0.00000	-0.03396	0.00000

Condition **LC50=1.2D-WL90**

6	0.01654	0.08710	0.00053	0.00000	0.00004	0.00000
7	0.01553	0.00000	-0.00178	0.00000	0.00000	0.00000
8	-0.04109	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01980	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.01755	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00002	0.16367	-0.00145	0.00000	0.00002	0.00000
45	-0.11843	0.36577	-0.11299	0.00000	0.00001	0.00000
50	-0.00139	0.15443	0.09117	0.00000	-0.00007	0.00000
51	0.00178	0.00000	0.07665	0.00000	0.00000	0.00000
52	-0.00369	0.00000	-0.10911	0.00000	0.00000	0.00000
53	0.00142	0.00000	0.03801	0.00000	0.00000	0.00000
54	0.00027	0.00000	0.01032	0.00000	0.00000	0.00000
55	0.08736	0.33745	-0.00787	0.00000	0.00004	0.00000
115	0.00358	0.02459	-0.00248	0.00000	0.00000	0.00000
116	0.00249	0.02950	0.00853	0.00000	0.00000	0.00000
133	0.00319	0.03217	0.01443	0.00000	0.00000	0.00000
134	0.00218	0.02402	-0.00367	0.00000	0.00000	0.00000
406	-0.02044	0.14549	0.00014	0.00000	-0.04273	0.00000
409	0.00000	-0.21187	0.00000	0.00000	0.00000	0.00000
410	-0.02200	0.94340	0.00509	0.00000	0.00052	0.00000
414	0.00729	-0.11874	-0.00105	0.00000	-0.00477	0.00000
518	-0.00685	0.07525	-0.00419	0.00000	0.00835	0.00000
SUM	-0.07000	2.05224	0.00000	0.00000	-0.03859	0.00000

Condition **LC51=1.2D-WL120**

6	0.01655	0.08712	0.00053	0.00000	0.00004	0.00000
7	0.01775	0.00000	-0.00185	0.00000	0.00000	0.00000
8	-0.04016	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.01993	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.01428	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00025	0.16379	-0.00140	0.00000	0.00001	0.00000
45	-0.11820	0.36560	-0.11248	0.00000	0.00002	0.00000
50	-0.00142	0.15457	0.09112	0.00000	-0.00007	0.00000
51	0.00201	0.00000	0.08354	0.00000	0.00000	0.00000
52	-0.00368	0.00000	-0.10918	0.00000	0.00000	0.00000
53	0.00144	0.00000	0.03919	0.00000	0.00000	0.00000
54	0.00053	0.00000	0.01741	0.00000	0.00000	0.00000
55	0.08794	0.33634	-0.00587	0.00000	0.00002	0.00000
115	0.00356	0.02428	-0.00318	0.00000	0.00000	0.00000
116	0.00260	0.03080	0.01141	0.00000	0.00000	0.00000
133	0.00319	0.03215	0.01439	0.00000	0.00000	0.00000
134	0.00218	0.02407	-0.00355	0.00000	0.00000	0.00000
406	-0.01528	0.14569	0.00864	0.00000	-0.03973	0.00000
409	0.00000	-0.21215	0.00000	0.00000	0.00000	0.00000
410	-0.03115	0.94367	0.02497	0.00000	-0.00398	0.00000
414	0.00790	-0.11875	0.00035	0.00000	-0.00538	0.00000

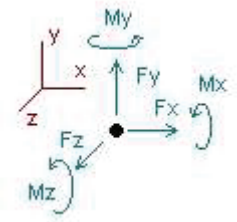
518	0.00317	0.07506	0.00140	0.00000	0.01089	0.00000
SUM	-0.05516	2.05224	0.05515	0.00000	-0.03816	0.00000

Condition **LC52=1.2D-WL150**

6	0.01655	0.08712	0.00053	0.00000	0.00004	0.00000
7	0.01767	0.00000	-0.00187	0.00000	0.00000	0.00000
8	-0.04011	0.00000	0.00179	0.00000	0.00000	0.00000
9	0.01991	0.00000	-0.00147	0.00000	0.00000	0.00000
10	-0.01451	0.00000	-0.00059	0.00000	0.00000	0.00000
17	0.00025	0.16379	-0.00136	0.00000	0.00001	0.00000
45	-0.11831	0.36563	-0.11258	0.00000	0.00002	0.00000
50	-0.00145	0.15454	0.09081	0.00000	-0.00006	0.00000
51	0.00259	0.00000	0.08287	0.00000	0.00000	0.00000
52	-0.00367	0.00000	-0.10904	0.00000	0.00000	0.00000
53	0.00144	0.00000	0.03974	0.00000	0.00000	0.00000
54	0.00105	0.00000	0.01635	0.00000	0.00000	0.00000
55	0.08795	0.33615	-0.00555	0.00000	0.00002	0.00000
115	0.00355	0.02424	-0.00326	0.00000	0.00000	0.00000
116	0.00262	0.03101	0.01189	0.00000	0.00000	0.00000
133	0.00318	0.03215	0.01438	0.00000	0.00000	0.00000
134	0.00218	0.02408	-0.00353	0.00000	0.00000	0.00000
406	-0.01459	0.14610	0.01006	0.00000	-0.03973	0.00000
409	0.00000	-0.21170	0.00000	0.00000	0.00000	0.00000
410	-0.05332	0.94405	0.03994	0.00000	-0.01209	0.00000
414	0.00805	-0.12006	0.00075	0.00000	-0.00553	0.00000
518	0.00613	0.07513	0.00299	0.00000	0.01159	0.00000
SUM	-0.07283	2.05224	0.07283	0.00000	-0.04572	0.00000

Envelope for nodal reactions

Note.- **Ic** is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

LC1=1.2D+1.6Wo
LC2=1.2D+1.6W30
LC3=1.2D+1.6W60
LC4=1.2D+1.6W90
LC5=1.2D+1.6W120
LC6=1.2D+1.6W150
LC7=1.2D-1.6Wo
LC8=1.2D-1.6W30
LC9=1.2D-1.6W60
LC10=1.2D-1.6W90
LC11=1.2D-1.6W120
LC12=1.2D-1.6W150

LC13=0.9D+1.6Wo
LC14=0.9D+1.6W30
LC15=0.9D+1.6W60
LC16=0.9D+1.6W90
LC17=0.9D+1.6W120
LC18=0.9D+1.6W150
LC19=0.9D-1.6Wo
LC20=0.9D-1.6W30
LC21=0.9D-1.6W60
LC22=0.9D-1.6W90
LC23=0.9D-1.6W120
LC24=0.9D-1.6W150
LC25=1.2D+Di+WI0
LC26=1.2D+Di+WI30
LC27=1.2D+Di+WI60
LC28=1.2D+Di+WI90
LC29=1.2D+Di+WI120
LC30=1.2D+Di+WI150
LC31=1.2D+Di-WI0
LC32=1.2D+Di-WI30
LC33=1.2D+Di-WI60
LC34=1.2D+Di-WI90
LC35=1.2D+Di-WI120
LC36=1.2D+Di-WI150
LC37=0.9D
LC38=1.2D
LC41=1.2D+WL0
LC42=1.2D+WL30
LC43=1.2D+WL60
LC44=1.2D+WL90
LC45=1.2D+WL120
LC46=1.2D+WL150
LC47=1.2D-WL0
LC48=1.2D-WL30
LC49=1.2D-WL60
LC50=1.2D-WL90
LC51=1.2D-WL120
LC52=1.2D-WL150

		Forces						Moments					
Node		**Fx** [Kip]	**lc**	**Fy** [Kip]	**lc**	**Fz** [Kip]	**lc**	**Mx** [Kip*ft]	**lc**	**My** [Kip*ft]	**lc**	**Mz** [Kip*ft]	**lc**
6	Max	0.042	LC6	0.187	LC28	0.003	LC1	0.00000	LC1	0.00152	LC8	0.00000	LC1
	Min	-0.011	LC24	0.027	LC24	-0.002	LC20	0.00000	LC1	-0.00144	LC14	0.00000	LC1
7	Max	0.511	LC3	0.000	LC1	0.043	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.287	LC22	0.000	LC1	-0.046	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
8	Max	0.002	LC17	0.000	LC1	0.060	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.177	LC9	0.000	LC1	-0.057	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
9	Max	0.048	LC27	0.000	LC1	0.069	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.182	LC21	0.000	LC1	-0.071	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
10	Max	1.002	LC15	0.000	LC1	0.066	LC23	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.931	LC10	0.000	LC1	-0.067	LC5	0.00000	LC1	0.00000	LC1	0.00000	LC1
17	Max	0.148	LC14	0.383	LC25	0.237	LC24	0.00000	LC1	0.00054	LC7	0.00000	LC1
	Min	-0.152	LC20	-0.007	LC14	-0.240	LC6	0.00000	LC1	-0.00054	LC13	0.00000	LC1
45	Max	-0.029	LC18	0.640	LC34	-0.056	LC19	0.00000	LC1	0.00240	LC24	0.00000	LC1
	Min	-0.193	LC32	0.252	LC16	-0.217	LC1	0.00000	LC1	-0.00239	LC6	0.00000	LC1

50	Max	0.001	LC24	0.279	LC25	0.157	LC35	0.00000	LC1	0.00230	LC16	0.00000	LC1
	Min	-0.004	LC6	0.108	LC19	0.028	LC17	0.00000	LC1	-0.00227	LC10	0.00000	LC1
51	Max	0.146	LC4	0.000	LC1	0.704	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.136	LC22	0.000	LC1	-0.380	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
52	Max	0.060	LC16	0.000	LC1	-0.063	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.066	LC10	0.000	LC1	-0.192	LC35	0.00000	LC1	0.00000	LC1	0.00000	LC1
53	Max	0.072	LC4	0.000	LC1	0.114	LC4	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.070	LC22	0.000	LC1	-0.138	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.132	LC4	0.000	LC1	0.486	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.126	LC22	0.000	LC1	-0.387	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
55	Max	0.238	LC2	0.617	LC31	0.337	LC13	0.00000	LC1	0.00061	LC5	0.00000	LC1
	Min	-0.094	LC20	0.057	LC13	-0.350	LC7	0.00000	LC1	-0.00059	LC23	0.00000	LC1
115	Max	0.082	LC5	0.065	LC2	0.129	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.076	LC23	-0.023	LC20	-0.135	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
116	Max	0.084	LC3	0.238	LC1	0.513	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.079	LC21	-0.186	LC19	-0.498	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
133	Max	0.081	LC4	0.073	LC31	0.120	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.075	LC23	-0.006	LC20	-0.096	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.080	LC3	0.104	LC1	0.216	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.076	LC21	-0.061	LC18	-0.221	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
406	Max	0.402	LC14	0.325	LC36	0.727	LC2	0.00000	LC1	0.22821	LC14	0.00000	LC1
	Min	-0.430	LC8	0.068	LC18	-0.716	LC20	0.00000	LC1	-0.29660	LC8	0.00000	LC1
409	Max	0.000	LC1	-0.117	LC19	0.064	LC1	0.00000	LC1	0.00805	LC6	0.00000	LC1
	Min	0.000	LC1	-0.589	LC25	-0.064	LC6	0.00000	LC1	-0.00805	LC1	0.00000	LC1
410	Max	1.939	LC6	1.984	LC25	1.736	LC13	0.00000	LC1	0.71922	LC6	0.00000	LC1
	Min	-1.920	LC24	0.616	LC19	-1.743	LC7	0.00000	LC1	-0.69917	LC24	0.00000	LC1
414	Max	0.109	LC3	-0.019	LC19	0.118	LC13	0.00000	LC1	0.03766	LC19	0.00000	LC1
	Min	-0.096	LC21	-0.307	LC25	-0.119	LC7	0.00000	LC1	-0.04664	LC1	0.00000	LC1
518	Max	0.812	LC13	0.144	LC30	0.472	LC13	0.00000	LC1	0.20058	LC1	0.00000	LC1
	Min	-0.816	LC7	0.047	LC23	-0.475	LC7	0.00000	LC1	-0.18363	LC19	0.00000	LC1

Date: 3/24/2022
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM **Checked By:** MSC

HUDSON Design Group LLC

CHECK CONNECTION CAPACITY (Worst Case) → GAMMA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A325 1/2" Bolt

Allowable Tensile Load =

F_{Tall} = 8836 lbs.

Allowable Shear Load =

F_{Vall}= 5301 lbs.

TENSILE FORCES

Reaction **F =** 1743 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 1939 lbs. (See Bentley Output)
Reactions in Y direction: 1984 lbs. (See Bentley Output)

Resultant: 2774 lbs.

No. of Supports = 1
No. of Bolts / Support = 2

Tension Design Load /Bolts =

f_t= 871.50 lbs. < 8836 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

f_v= 1387.08 lbs. < 5301 lbs. **Therefore, OK !**

CHECK COMBINED TENSION AND SHEAR

f_t / F_T	+	f_v / F_V	≤	1.0			
0.099	+	0.262	=	0.360	<	1.0	**Therefore, OK !**

EXHIBIT 5

Radio Frequency Exposure Analysis Report

April 7, 2022

Centerline on behalf of AT&T
Centerline Communications Project Number: 566599

AT&T Site Name: Cheshire SW
Site Number: CT2036
FA#: 10034996
USID: 26014

Site Address: 751 Higgins Road, Cheshire, CT 06410

Site Compliance Summary

AT&T Compliance Status:	Compliant
Cumulative Calculated Power Density (Ground Level):	1.66451 µW/cm^2
Cumulative General Population % MPE (Ground Level):	0.18052%

April 7, 2022

Centerline
Attn: Jennifer Iliades, Project Manager
750 W Center St, Suite 301
West Bridgewater, MA 02379

RF Exposure Analysis for Site: **Cheshire SW**

Centerline Communications, LLC ("Centerline") was contracted to analyze the proposed AT&T facility at **751 Higgins Road, Cheshire, CT 06410** for the purpose of determining whether the predictive exposure from the proposed facility is within specified federal limits.

All information used in this report was analyzed as a percentage of the Maximum Permissible Exposure (% MPE) limits as detailed in 47 CFR § 1.1310 as well as Federal Communications Commission (FCC) OET Bulletin 65 Edition 97-01. The FCC MPE limits are typically expressed in units of milliwatts per square centimeter (mW/cm^2) or microwatts per square centimeter ($\mu W/cm^2$). The exposure limits vary depending upon the frequencies being utilized. The General Population/Uncontrolled MPE limit (in mW/cm^2) for frequencies between 300 and 1500 is defined as frequency (in MHz) divided by 1500 ($f_{MHz}/1500$). Frequencies between 1500 and 100,000 MHz have a General Population/Uncontrolled MPE limit of 1 mW/cm^2 (1000 $\mu W/cm^2$). The calculated power density at each sample point divided by the limit at each calculated frequency provides a result in % MPE. Summing the calculated % MPE from all contributors provides a cumulative % MPE at a particular sample point. Wireless carriers use different frequency bands with varying MPE limits; therefore, it is useful to report results in terms of % MPE as opposed to power density.

All results were compared to the FCC radio frequency exposure rules as detailed in 47 CFR § 1.1307(b) to determine compliance with the MPE limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/ controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits, as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means. Additional details can be found in FCC OET 65.

Calculation Methodology

Centerline Communications, LLC has performed theoretical modeling of the site using a software tool, RoofMaster®, which incorporates calculation methodologies detailed in FCC OET 65. RoofMaster® uses a cylindrical model for conservative power density predictions within the near field of the antenna where the antenna pattern has not truly formed yet. Within this area power density values tend to decrease based upon an inverse distance function. At the point where it is appropriate for modeling to change from near-field calculations to far-field calculations, the power decreases inversely with the square of the distance. The modeling is based on worst-case assumptions in terms of transmitter power and duty cycle. No losses were included in the power calculations unless they were specifically provided for the project.

In OET 65, a far field model is presented to calculate the spatial peak power density. The RoofMaster® implementation of this model incorporates antenna manufacturer's horizontal and vertical pattern data to determine the power density in all directions. This model yields the power density at a single point in space. In order to determine the spatial power density for comparison to the FCC limits, the average of several points calculated within the human profile (0-6') must be conducted. RoofMaster® calculates seven power density values between 0-6' above the specified study plane and performs a linear spatial average.

Data & Results

The following table details the antennas and operating parameters for the AT&T antenna system as well as any other antenna systems at the site. This is based on antenna information provided by the client and data compiled from other sources where necessary. The data below was input into Roofmaster® to perform the theoretical exposure calculations at the ground.

The theoretical calculations performed in Roofmaster® determine the cumulative exposure at all sample points at ground level (0-6' spatial average). The results from highest cumulative sample point at ground level surrounding the site are displayed in the table below. The contribution from directional antennas to the maximum cumulative totals varies greatly depending on location; therefore, the contribution from one antenna sector at the highest calculated exposure point may be greater or less than other sectors since sectorized directional antennas are pointed in different directions and there is not much overlapping exposure.

The contribution to the cumulative power density and % MPE for each antenna/frequency band is listed in the table. The cumulative power density and cumulative % MPE are displayed at the bottom of the table.

Maximum Calculated Cumulative Power Density (Location: approximately of site)

Antenna ID	Make / Model	Frequency Band (MHz)	Antenna Gain (dBd)	Antenna Centerline (ft)	Channel Count	TX Power/ Channel (watts)	ERP (watts)	Calculated Power Density (μW/cm²)	General Population MPE Limit (μW/cm²)	General Population % MPE
AT&T A 1	CCI TPA65R-BU8D	700	12.95	255.00	4.00	40.00	3155.88	0.00936	466.67	0.00201
AT&T A 1	CCI TPA65R-BU8D	1900	15.15	255.00	2.00	40.00	2618.73	0.00560	1000.00	0.00056
AT&T A 1	CCI TPA65R-BU8D	1900	15.35	255.00	2.00	40.00	2742.14	0.00559	1000.00	0.00056
AT&T A 1	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00620	1000.00	0.00062
AT&T A 1	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00620	1000.00	0.00062
AT&T A 2	AIR6449	3700	23.55	257.00	1.00	108.40	24548.74	0.13503	1000.00	0.01350
AT&T A 3	AIR6419 LTE	3400	22.85	253.00	1.00	54.20	10447.19	0.56468	1000.00	0.05647
AT&T A 3	AIR6419 NR	3400	22.85	253.00	1.00	54.00	10408.63	0.25192	1000.00	0.02519
AT&T A 4	CCI DMP65R-BU8D	700	12.25	255.00	2.00	40.00	1343.04	0.00746	466.67	0.00160
AT&T A 4	CCI DMP65R-BU8D	850	12.55	255.00	2.00	40.00	1439.10	0.00719	566.67	0.00127
AT&T A 4	CCI DMP65R-BU8D	2300	15.15	255.00	4.00	25.00	3273.41	0.01263	1000.00	0.00126
AT&T B 5	CCI TPA65R-BU8D	700	12.95	255.00	4.00	40.00	3155.88	0.00001	466.67	0.00000
AT&T B 5	CCI TPA65R-BU8D	1900	15.15	255.00	2.00	40.00	2618.73	0.00000	1000.00	0.00000
AT&T B 5	CCI TPA65R-BU8D	1900	15.35	255.00	2.00	40.00	2742.14	0.00000	1000.00	0.00000
AT&T B 5	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00000	1000.00	0.00000
AT&T B 5	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00000	1000.00	0.00000
AT&T B 6	AIR6449	3700	23.55	257.00	1.00	108.40	24548.74	0.00004	1000.00	0.00000
AT&T B 7	AIR6419 LTE	3400	22.85	253.00	1.00	54.20	10447.19	0.00029	1000.00	0.00003
AT&T B 7	AIR6419 NR	3400	22.85	253.00	1.00	54.00	10408.63	0.00003	1000.00	0.00000
AT&T B 8	CCI DMP65R-BU8D	700	12.25	255.00	2.00	40.00	1343.04	0.00000	466.67	0.00000
AT&T B 8	CCI DMP65R-BU8D	850	12.55	255.00	2.00	40.00	1439.10	0.00000	566.67	0.00000
AT&T B 8	CCI DMP65R-BU8D	2300	15.15	255.00	4.00	25.00	3273.41	0.00000	1000.00	0.00000
AT&T C 9	CCI TPA65R-BU8D	700	12.95	255.00	4.00	40.00	3155.88	0.00001	466.67	0.00000
AT&T C 9	CCI TPA65R-BU8D	1900	15.15	255.00	2.00	40.00	2618.73	0.00000	1000.00	0.00000
AT&T C 9	CCI TPA65R-BU8D	1900	15.35	255.00	2.00	40.00	2742.14	0.00000	1000.00	0.00000
AT&T C 9	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00000	1000.00	0.00000
AT&T C 9	CCI TPA65R-BU8D	2100	15.85	255.00	2.00	40.00	3076.73	0.00000	1000.00	0.00000
AT&T C 10	AIR6449	3700	23.55	257.00	1.00	108.40	24548.74	0.00016	1000.00	0.00002
AT&T C 11	AIR6419 LTE	3400	22.85	253.00	1.00	54.20	10447.19	0.00010	1000.00	0.00001
AT&T C 11	AIR6419 NR	3400	22.85	253.00	1.00	54.00	10408.63	0.00008	1000.00	0.00001
AT&T C 12	CCI DMP65R-BU8D	700	12.25	255.00	2.00	40.00	1343.04	0.00000	466.67	0.00000
AT&T C 12	CCI DMP65R-BU8D	850	12.55	255.00	2.00	40.00	1439.10	0.00000	566.67	0.00000
AT&T C 12	CCI DMP65R-BU8D	2300	15.15	255.00	4.00	25.00	3273.41	0.00000	1000.00	0.00000
Unknown A 13	GENERIC PANEL 6FT	1900	15.84	245.00	2.00	60.00	4604.49	0.00745	1000.00	0.00075

Antenna ID	Make / Model	Frequency Band (MHz)	Antenna Gain (dBd)	Antenna Centerline (ft)	Channel Count	TX Power/ Channel (watts)	ERP (watts)	Calculated Power Density (μW/cm²)	General Population MPE Limit (μW/cm²)	General Population % MPE
Unknown A 14	GENERIC PANEL 6FT	600	12.33	245.00	2.00	60.00	2052.02	0.02165	400.00	0.00541
Unknown A 15	GENERIC PANEL 6FT	700	12.33	245.00	2.00	60.00	2052.02	0.01922	466.67	0.00412
Unknown A 15	GENERIC PANEL 6FT	2100	15.84	245.00	2.00	60.00	4604.49	0.02054	1000.00	0.00205
Unknown A 16	GENERIC PANEL	3700	23.55	245.00	4.00	80.00	72468.62	0.26529	1000.00	0.02653
Unknown B 17	GENERIC PANEL 6FT	1900	15.84	245.00	2.00	60.00	4604.49	0.00001	1000.00	0.00000
Unknown B 18	GENERIC PANEL 6FT	600	12.33	245.00	2.00	60.00	2052.02	0.00001	400.00	0.00000
Unknown B 19	GENERIC PANEL 6FT	700	12.33	245.00	2.00	60.00	2052.02	0.00001	466.67	0.00000
Unknown B 19	GENERIC PANEL 6FT	2100	15.84	245.00	2.00	60.00	4604.49	0.00000	1000.00	0.00000
Unknown B 20	GENERIC PANEL	3700	23.55	245.00	4.00	80.00	72468.62	0.00033	1000.00	0.00003
Unknown C 21	GENERIC PANEL 6FT	1900	15.84	245.00	2.00	60.00	4604.49	0.00001	1000.00	0.00000
Unknown C 22	GENERIC PANEL 6FT	600	12.33	245.00	2.00	60.00	2052.02	0.00001	400.00	0.00000
Unknown C 23	GENERIC PANEL 6FT	700	12.33	245.00	2.00	60.00	2052.02	0.00001	466.67	0.00000
Unknown C 23	GENERIC PANEL 6FT	2100	15.84	245.00	2.00	60.00	4604.49	0.00002	1000.00	0.00000
Unknown C 24	GENERIC PANEL	3700	23.55	245.00	4.00	80.00	72468.62	0.00033	1000.00	0.00003
Unknown A 25	GENERIC PANEL 6FT	850	12.62	238.00	4.00	40.00	2924.96	0.02467	566.67	0.00435
Unknown A 25	GENERIC PANEL 6FT	1900	15.84	238.00	4.00	40.00	6139.32	0.02630	1000.00	0.00263
Unknown A 26	GENERIC PANEL 6FT	2100	16.39	238.00	4.00	40.00	6968.19	0.02583	1000.00	0.00258
Unknown A 26	GENERIC PANEL 6FT	700	12.33	238.00	4.00	40.00	2736.02	0.02198	466.67	0.00471
Unknown A 27	GENERIC PANEL	3700	23.34	238.00	4.00	50.00	43154.89	0.19419	1000.00	0.01942
Unknown B 28	GENERIC PANEL 6FT	850	12.62	238.00	4.00	40.00	2924.96	0.00000	566.67	0.00000
Unknown B 28	GENERIC PANEL 6FT	1900	15.84	238.00	4.00	40.00	6139.32	0.00000	1000.00	0.00000
Unknown B 29	GENERIC PANEL 6FT	2100	16.39	238.00	4.00	40.00	6968.19	0.00000	1000.00	0.00000
Unknown B 29	GENERIC PANEL 6FT	700	12.33	238.00	4.00	40.00	2736.02	0.00002	466.67	0.00000
Unknown B 30	GENERIC PANEL	3700	23.34	238.00	4.00	50.00	43154.89	0.00092	1000.00	0.00009
Unknown C 31	GENERIC PANEL 6FT	850	12.62	238.00	4.00	40.00	2924.96	0.00001	566.67	0.00000
Unknown C 31	GENERIC PANEL 6FT	1900	15.84	238.00	4.00	40.00	6139.32	0.00004	1000.00	0.00000
Unknown C 32	GENERIC PANEL 6FT	2100	16.39	238.00	4.00	40.00	6968.19	0.00001	1000.00	0.00000
Unknown C 32	GENERIC PANEL 6FT	700	12.33	238.00	4.00	40.00	2736.02	0.00003	466.67	0.00001

Antenna ID	Make / Model	Frequency Band (MHz)	Antenna Gain (dBd)	Antenna Centerline (ft)	Channel Count	TX Power/ Channel (watts)	ERP (watts)	Calculated Power Density (µW/cm²)	General Population MPE Limit (µW/cm²)	General Population % MPE
Unknown C 33	GENERIC PANEL	3700	23.34	238.00	4.00	50.00	43154.89	0.00026	1000.00	0.00003
Unknown A 34	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00357	566.67	0.00063
Unknown A 35	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.01339	566.67	0.00236
Unknown A 36	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00457	566.67	0.00081
Unknown B 37	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown B 38	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown B 39	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown C 40	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown C 41	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown C 42	GENERIC PANEL 6FT	850	12.62	222.00	1.00	60.00	1096.86	0.00000	566.67	0.00000
Unknown A 43	GENERIC OMNI	850	8.96	203.00	1.00	25.25	198.73	0.00037	566.67	0.00007
Unknown B 44	GENERIC OMNI	850	8.96	203.00	1.00	25.25	198.73	0.00027	566.67	0.00005
Unknown C 45	GENERIC OMNI	850	8.96	167.00	1.00	25.25	198.73	0.00060	566.67	0.00011
							Cumulative Power Density:	**1.66451 µW/cm²**	**Cumulative % MPE:**	**0.18052%**

Summary

The theoretical calculations performed for this analysis yielded cumulative power density totals in all areas at ground that are within the allowable federal limits for public exposure to RF energy. Therefore, the site is **Compliant** with FCC rules and regulations.

Michelle Stone

Michelle Stone
RF EME Technical Writer II
Centerline Communications, LLC

EXHIBIT 6

Proof of Delivery

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

Tracking Number

1Z9Y45030304804227

Weight

1.00 LBS

Service

UPS Ground

Shipped / Billed On

04/22/2022

Delivered On

06/07/2022 11:46 A.M.

Delivered To

84 S MAIN ST
CHESHIRE, CT, 06410, US

Received By

SHARPERD

Left At

Receiver

Reference Number(s)

CT2036-CSC TOWN MANAGER

Thank you for giving us this opportunity to serve you. Details are only available for shipments delivered within the last 120 days. Please print for your records if you require this information after 120 days.

Sincerely,

UPS

Tracking results provided by UPS: 06/08/2022 10:22 A.M. EST

Proof of Delivery

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

Tracking Number

1Z9Y45030305651239

Weight

1.00 LBS

Service

UPS Ground

Shipped / Billed On

04/22/2022

Delivered On

06/07/2022 11:45 A.M.

Delivered To

84 S MAIN ST
CHESHIRE, CT, 06410, US

Received By

DONNA

Left At

Receiver

Reference Number(s)

CT2036-CSC TOWN PLANNER

Thank you for giving us this opportunity to serve you. Details are only available for shipments delivered within the last 120 days. Please print for your records if you require this information after 120 days.

Sincerely,

UPS

Tracking results provided by UPS: 06/08/2022 10:24 A.M. EST

Proof of Delivery

Dear Customer,

This notice serves as proof of delivery for the shipment listed below.

Tracking Number

1Z9Y45030330206691

Weight

1.00 LBS

Service

UPS Ground

Shipped / Billed On

04/22/2022

Delivered On

06/07/2022 11:45 A.M.

Delivered To

84 S MAIN ST
CHESHIRE, CT, 06410, US

Received By

DONNA

Left At

Receiver

Reference Number(s)

CT2036-CSC ZEO

Thank you for giving us this opportunity to serve you. Details are only available for shipments delivered within the last 120 days. Please print for your records if you require this information after 120 days.

Sincerely,

UPS

Tracking results provided by UPS: 06/08/2022 10:25 A.M. EST

(https://www.
loc=en_US&re

Your shipment
1Z9Y45030315900245

Estimated delivery
Tomorrow, June 09 by 7:00 P.M.

Label Created

On the Way

Out for Delivery

Delivery

Ship To
BROOKHAVEN, GA US

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View Details

Get updates for your package

Enroll in UPS My Choice and take the worry out of missed deliveries, or having packages sit outside while you're away.

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