

March 21, 2023

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Regarding: Notice of Exempt Modification – AT&T Site CT2036 / FA# 10034996
Address: 751 Higgins Road, Cheshire, CT 06410

Dear Ms. Bachman:

New Cingular Wireless, PCS, LLC (“AT&T”) currently maintains a wireless telecommunications facility on an existing +/- 249’ self-support tower at the above-referenced address, latitude 41.4874639, longitude -72.9293319. Said self-support tower is operated by AT&T Towers.

AT&T desires to modify its existing telecommunications facility by installing three (3) Radio Units as more particularly detailed and described on the enclosed Construction Drawings prepared by TEP Northeast, last revised February 1, 2023. The centerline height of the existing antennas is and will remain at 255 feet.

Please accept this letter as notification pursuant to R.C.S.A §16-50j-73 for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to the following individuals: The Honorable Sean M. Kimball, Town Manager of the Town of Cheshire, as elected official, Michael J. Strollo, Zoning Enforcement Officer of the Town of Cheshire, Michael Glidden, Town Planner of the Town of Cheshire, AT&T Towers, as tower operator/property owner. We have reached out to the Building and Zoning Departments for the Town of Cheshire who conducted a search and could not locate the original tower approval.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Specifically:

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require an extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the modified facility will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard. *Please see the RF emissions calculation for AT&T's modified facility enclosed herewith.*
5. The proposed modifications will not cause an ineligible change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading. *Please see the structural analysis dated March 3, 2023, and prepared by GDP Engineering, enclosed herewith.*

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



William Hurley
Site Acquisition Specialist
Centerline Communications, LLC
750 West Center Street, Suite 301
West Bridgewater, MA 02379
whurley@clinellc.com

Enclosures: Exhibit 1 – Construction Drawings
Exhibit 2 – Property Card and GIS
Exhibit 3 – Structural Analysis
Exhibit 4 – Mount Analysis
Exhibit 5 – RF Emissions Analysis Report Evaluation
Exhibit 6 – Notice Delivery Confirmations

cc: The Honorable Sean M. Kimball, Town Manager, as elected official.
Michael J. Strollo, Zoning Enforcement Officer, Town of Cheshire
Michael Glidden, Town Planner, Town of Cheshire
AT&T Towers, as tower operator/property owner.

Exhibit 1

PROJECT INFORMATION

SCOPE OF WORK: ITEMS TO BE MOUNTED ON THE EXISTING LATTICE TOWER:
 • NEW AT&T RADIOS: 2012 B29 (TYP. OF 1 PER SECTOR, TOTAL OF 3).

ITEMS TO BE MOUNTED IN EQUIPMENT LOCATION:
 • FINAL=5216-XMU-6630-IDLE/6648-XCEDE

ITEMS TO BE REMOVED:
 N/A

ITEMS TO REMAIN:
 • (9) ANTENNAS, (15) RRU'S, (3) SURGE ARRESTORS, (9) DC TRUNKS, (3) FIBER CABLES & (3) Y-CABLES.

RFDS: FINAL APPROVED V1 9/13/22

SITE ADDRESS: 751 HIGGINS ROAD
 CHESHIRE, CT 06410

LATITUDE: 41.487472° N, 41° 29' 14.9" N

LONGITUDE: 72.929305° W, 72° 55' 45.5" W

TYPE OF SITE: LATTICE TOWER / INDOOR EQUIPMENT

STRUCTURE HEIGHT: 249'-0"±

RAD CENTER: 255'-0"±

CURRENT USE: TELECOMMUNICATIONS FACILITY

PROPOSED USE: TELECOMMUNICATIONS FACILITY



SITE NUMBER: CTL02036

SITE NAME: CHESHIRE SW

FA CODE: 10034996

PACE ID: MRCTB062236

PROJECT: LTE 6C 2023 UPGRADE

VICINITY MAP

GENERAL NOTES

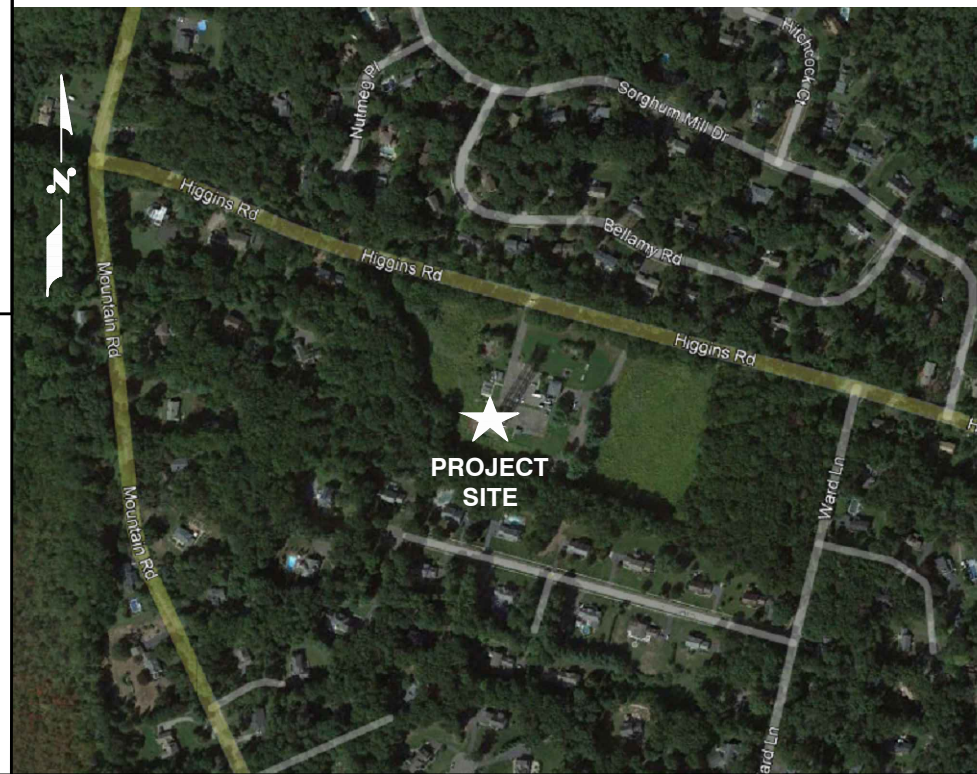
DIRECTIONS TO SITE:

HEAD SOUTHEAST TOWARD CAPITAL BLVD. TURN LEFT ONTO CAPITAL BLVD. TURN LEFT ONTO STATE HWY 411, TURN LEFT TO MERGE ONTO I-91 S. MERGE ONTO I-91 S. KEEP RIGHT TO STAY ON I-91 S. TAKE EXIT 18 FOR I-691 W TOWARD MERIDEN/WATERBURY. CONTINUE ONTO I-691 W. TAKE EXIT 1 ON THE LEFT FOR I084 W TOWARD WATERBURY/DANBURY. MERGE ONTO I-84. TAKE EXIT 26 FOR CT-70 TOWARD CHESHIRE/PROSPECT. TURN LEFT ONTO CT-70 E/STATE HWY 801. TURN RIGHT ONTO MOUNTAIN RD. TURN LEFT ONTO HIGGINS RD. TURN RIGHT.

1. THIS DOCUMENT IS THE CREATION, DESIGN, PROPERTY AND COPYRIGHTED WORK OF AT&T. ANY DUPLICATION OR USE WITHOUT EXPRESS WRITTEN CONSENT IS STRICTLY PROHIBITED. DUPLICATION AND USE BY GOVERNMENT AGENCIES FOR THE PURPOSES OF CONDUCTING THEIR LAWFULLY AUTHORIZED REGULATORY AND ADMINISTRATIVE FUNCTIONS IS SPECIFICALLY ALLOWED.
2. THE FACILITY IS AN UNMANNED PRIVATE AND SECURED EQUIPMENT INSTALLATION. IT IS ONLY ACCESSED BY TRAINED TECHNICIANS FOR PERIODIC ROUTINE MAINTENANCE AND THEREFORE DOES NOT REQUIRE ANY WATER OR SANITARY SEWER SERVICE. THE FACILITY IS NOT GOVERNED BY REGULATIONS REQUIRING PUBLIC ACCESS PER ADA REQUIREMENTS.
3. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE AT&T MOBILITY REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.
4. CONSTRUCTION DRAWINGS ARE VALID FOR SIX MONTHS AFTER ENGINEER OF RECORD'S STAMPED AND SIGNED SUBMITTAL DATE LISTED HEREIN.

DRAWING INDEX

SHEET NO.	DESCRIPTION	REV.
T-1	TITLE SHEET	0
GN-1	GENERAL NOTES	0
A-1	COMPOUND & EQUIPMENT PLANS	0
A-2	EXISTING & PROPOSED ANTENNA LAYOUTS	0
A-3	ELEVATION	0
A-4	DETAILS	0
G-1	GROUNDING DETAILS	0
RF-1	RF PLUMBING DIAGRAM	0



72 HOURS



CALL BEFORE YOU DIG



CALL TOLL FREE 1-800-922-4455

OR CALL 811

UNDERGROUND SERVICE ALERT



750 WEST CENTER STREET, SUITE #301
 WEST BRIDGEWATER, MA 02379

SITE NUMBER: CTL02036
SITE NAME: CHESHIRE SW

751 HIGGINS ROAD
 CHESHIRE, CT 06410
 NEW HAVEN COUNTY



550 COCHITUATE ROAD
 FRAMINGHAM, MA 01701

NO.	DATE	REVISIONS	BY	CHK	APP'D
0	02/01/23	ISSUED FOR REVIEW	DO	AT	DPH
A	01/11/23	ISSUED FOR REVIEW	VD	AT	DPH

SCALE: AS SHOWN DESIGNED BY: AT DRAWN BY: VD

AT&T

TITLE SHEET
 LTE 6C 2023 UPGRADE

SITE NUMBER	DRAWING NUMBER	REV
CTL02036	T-1	0

GROUNDING NOTES

1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
2. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION, AND AC POWER GES'S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81 STANDARDS) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, #6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS AND #2 AWG STRANDED COPPER FOR OUTDOOR BTS.
6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
7. APPROVED ANTIOXIDANT COATINGS (I.E., CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO GROUND BAR.
9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.
11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 AWG COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.
12. ALL NEW STRUCTURES WITH A FOUNDATION AND/OR FOOTING HAVING 20 FT. OR MORE OF 1/2 IN. OR GREATER ELECTRICALLY CONDUCTIVE REINFORCING STEEL MUST HAVE IT BONDED TO THE GROUND RING USING AN EXOTHERMIC WELD CONNECTION USING #2 AWG SOLID BARE TINNED COPPER GROUND WIRE, PER NEC 250.50

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:
 CONTRACTOR – CENTERLINE
 SUBCONTRACTOR – GENERAL CONTRACTOR (CONSTRUCTION)
 OWNER – AT&T MOBILITY
2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.
7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.
9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND T1 CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.
10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.
11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.
12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION.
13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000 PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE DONE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.
15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLESS OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE E (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCH UP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED USING A COMPATIBLE ZINC RICH PAINT.
16. CONSTRUCTION SHALL COMPLY WITH SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF AT&T SITES."
17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.
20. **APPLICABLE BUILDING CODES:**
 SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF CONTRACT AWARD SHALL GOVERN THE DESIGN.

**BUILDING CODE: IBC 2021 WITH 2022 CT STATE BUILDING CODE AMENDMENTS
 ELECTRICAL CODE: 2020 NATIONAL ELECTRICAL CODE (NFPA 70-2020)**

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318; BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE;

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) MANUAL OF STEEL CONSTRUCTION, ASD, FOURTEENTH EDITION;

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222-H, STRUCTURAL STANDARDS FOR STEEL

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHODS OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MOST RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

ABBREVIATIONS					
AGL	ABOVE GRADE LEVEL	EQ	EQUAL	REQ	REQUIRED
AWG	AMERICAN WIRE GAUGE	GC	GENERAL CONTRACTOR	RF	RADIO FREQUENCY
BBU	BATTERY BACKUP UNIT	GRC	GALVANIZED RIGID CONDUIT	TBD	TO BE DETERMINED
BTCW	BARE TINNED SOLID COPPER WIRE	MGB	MASTER GROUND BAR	TBR	TO BE REMOVED
BGR	BURIED GROUND RING	MIN	MINIMUM	TBRR	TO BE REMOVED AND REPLACED
BTS	BASE TRANSCEIVER STATION	P	PROPOSED	TYP	TYPICAL
E	EXISTING	NTS	NOT TO SCALE	UG	UNDER GROUND
EGB	EQUIPMENT GROUND BAR	RAD	RADIATION CENTER LINE (ANTENNA)	VIF	VERIFY IN FIELD
EGR	EQUIPMENT GROUND RING	REF	REFERENCE		



750 WEST CENTER STREET, SUITE #301
 WEST BRIDGEWATER, MA 02379

SITE NUMBER: CTL02036
 SITE NAME: CHESHIRE SW

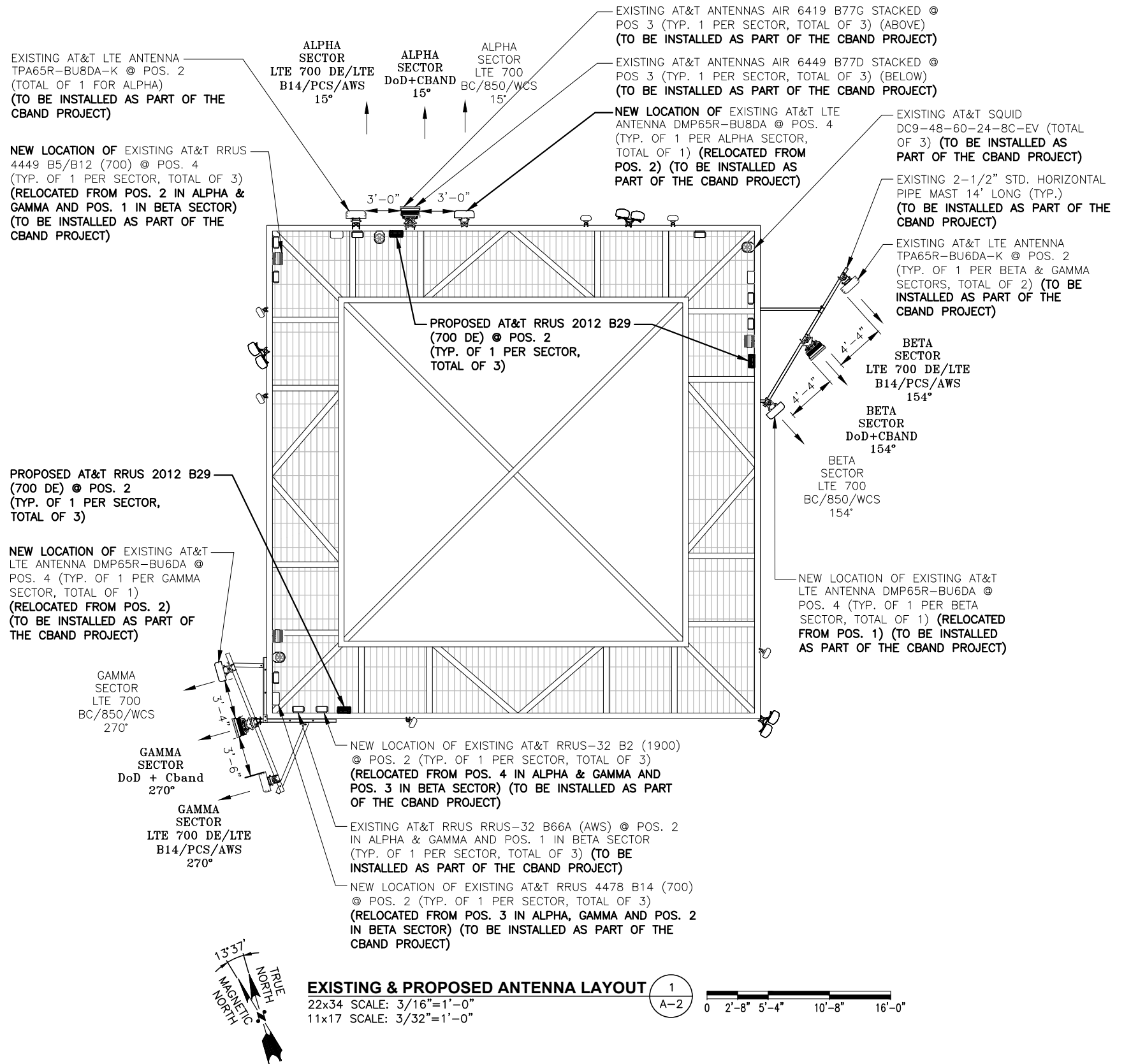
751 HIGGINS ROAD
 CHESHIRE, CT 06410
 NEW HAVEN COUNTY



550 COCHITUATE ROAD
 FRAMINGHAM, MA 01701

0	02/01/23	ISSUED FOR REVIEW	DO	AT	DPH
A	01/11/23	ISSUED FOR REVIEW	VD	AT	DPH
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: VD		

AT&T		
GENERAL NOTES LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	GN-1	0



EXISTING & PROPOSED ANTENNA LAYOUT 1
 22x34 SCALE: 3/16"=1'-0"
 11x17 SCALE: 3/32"=1'-0"

NOTE:
 REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 09/13/2022 DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
 ALL EQUIPMENT INSTALLATIONS ARE PENDING THE COMPLETION OF A STRUCTURAL ANALYSIS OF THE EXISTING STRUCTURE.

NOTE:
 ANTENNAS AND MOUNTS TO BE ADJUSTED AS REQUIRED TO ACHIEVE A 3'-0" MINIMUM SEPARATION BETWEEN ANTENNAS



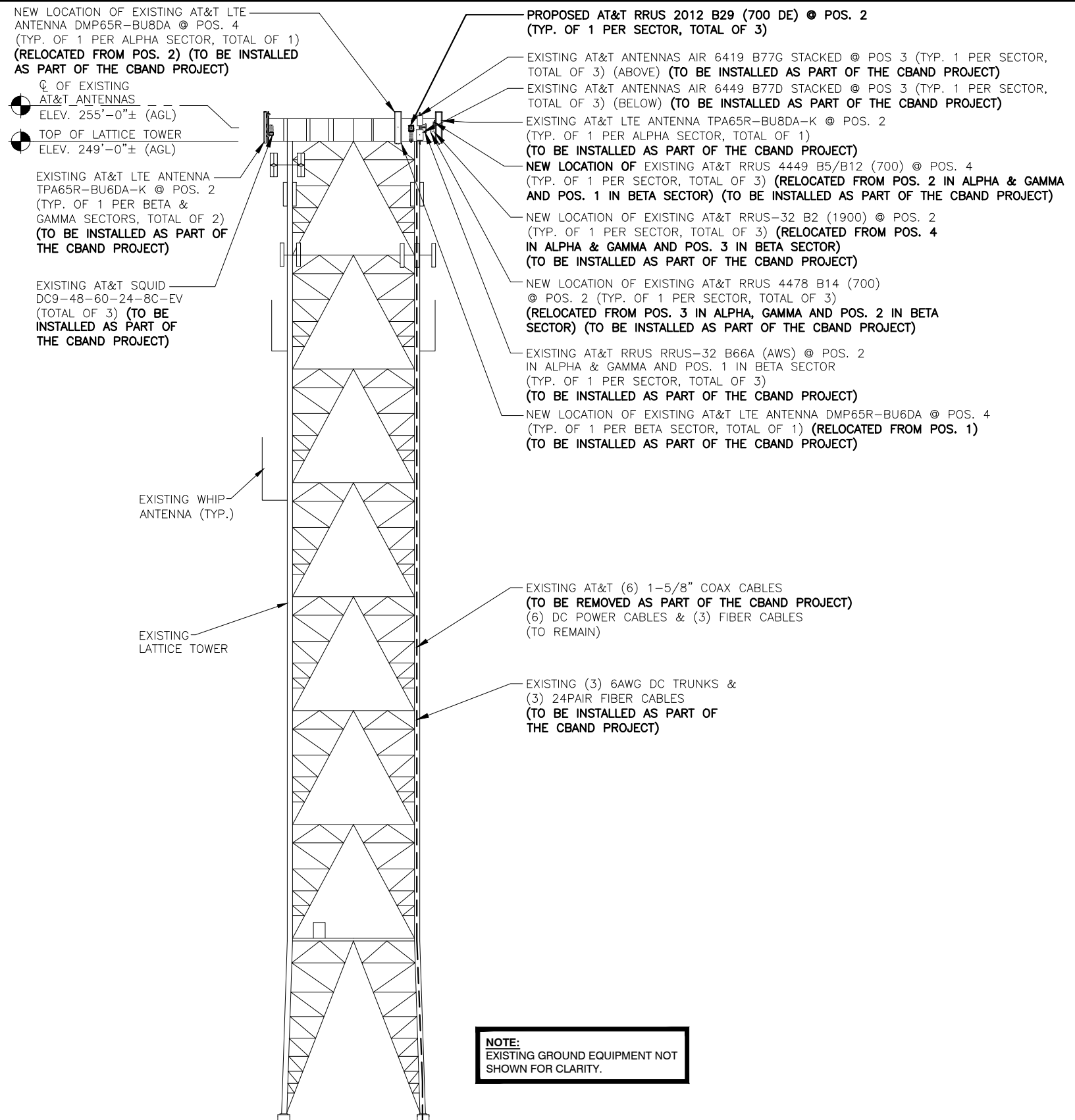
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AT&T		
EXISTING & PROPOSED ANTENNA LAYOUTS LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	A-2	0

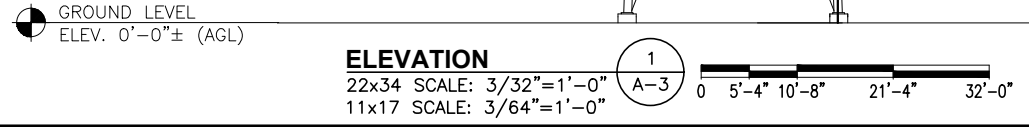


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NOTE:
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NOTE:
ANTENNAS AND MOUNTS TO BE ADJUSTED AS REQUIRED TO ACHIEVE A 3'-0" MINIMUM SEPARATION BETWEEN ANTENNAS

NOTE:
EXISTING GROUND EQUIPMENT NOT SHOWN FOR CLARITY.



TEP OPCO, LLC.
45 BEECHWOOD DRIVE, NORTH ANDOVER, MA 01845
TEL: (978) 557-5553

750 WEST CENTER STREET, SUITE #301
WEST BRIDGEWATER, MA 02379

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AT&T		
ELEVATION LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	A-3	0

ANTENNA SCHEDULE

SECTOR	EXISTING/ PROPOSED	BAND	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA Ø HEIGHT	AZIMUTH	TMA/ DIPLEXER	RRU	SIZE (INCHES) (L x W x D)	FEEDER	RAYCAP
A1	-	-	-	-	-	-	-	-	-	-	(E) (1) RAYCAP DC9-48-60-24-8C-EV
A2	EXSITING	LTE 700 DE/LTE B14/PCS/AWS	TPA65R-BU8DA-K	96"X20.7"X7.7"	255'-0"±	15°	-	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS) (P)(1) RRUS-2012 B29 (700 DE)	18.1"x13.4"x8.3"	(E)(2) DC POWER (E)(1) 6AWG DC POWER & (1) 24PAIR FIBER	
A3	EXSITING	DOD CBAND	AIR6419 B77G AIR6449 B77D	31.1"X16.1"X7.3" 30.4"X15.9"X8.1"	255'-0"±	15°	-	-	-	-	
A4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU8DA	96"X20.7"X7.7"	255'-0"±	15°	-	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	-	(E)(1)(Y-CABLE)	
B1	-	-	-	-	-	-	-	-	-	-	(E) (1) RAYCAP DC9-48-60-24-8C-EV
B2	EXSITING	LTE 700 DE/LTE B14/PCS/AWS	TPA65R-BU8DA-K	96"X20.7"X7.7"	255'-0"±	154°	-	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS) (P)(1) RRUS-2012 B29 (700 DE)	18.1"x13.4"x8.3"	(E)(2) DC POWER (E)(1) 6AWG DC POWER & (1) 24PAIR FIBER	
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B4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU8DA	96"X20.7"X7.7"	255'-0"±	154°	-	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	-	(E)(1)(Y-CABLE)	
C1	-	-	-	-	-	-	-	-	-	-	(E) (1) RAYCAP DC9-48-60-24-8C-EV
C2	EXSITING	LTE 700 DE/LTE B14/PCS/AWS	TPA65R-BU8DA-K	96"X20.7"X7.7"	255'-0"±	270°	-	(E)(1)RRUS-4478 B14 (700) (E)(1)RRUS-32 B2 (1900) (E)(1)RRUS-32 B66A (AWS) (P)(1) RRUS-2012 B29 (700 DE)	18.1"x13.4"x8.3"	(E)(2) DC POWER (E)(1) 6AWG DC POWER & (1) 24PAIR FIBER	
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C4	EXSITING	LTE 700 BC/850/WCS	DMP65R-BU8DA	96"X20.7"X7.7"	255'-0"±	270°	-	(E)(1)RRUS-4449 B5/B12 (700) (E)(1)RRUS-32 B30 (WCS)	-	(E)(1)(Y-CABLE)	

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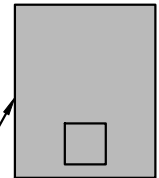
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RRU CHART		
QUANTITY	MODEL	SIZE (L x W x D)
P(3)	2012 B29 (700 DE)	18.1"x13.4"x8.3"
E(3)	4478 B14 (700)	18.1"x13.4"x8.3"
E(3)	RRUS-32 B2 (1900)	27.2"x12.1"x7.0"
E(3)	RRUS-32 B66 (AWS)	27.2"x12.1"x7.0"
E(3)	4449 B5/B12 (700)	17.9"x13.2"x10.4"
E(3)	RRUS-32 B30 (WCS)	27.2"x12.1"x7.0"

NOTE:
MOUNT PER MANUFACTURER'S SPECIFICATIONS

FINAL ANTENNA SCHEDULE 1
SCALE: N.T.S

NOTE:
SEE RFDS FOR RRH
FREQUENCY AND
MODEL NUMBER



PROPOSED RRU REFER TO THE
FINAL RFDS AND CHART FOR
QUANTITY, MODEL AND DIMENSIONS

NOTE:
MOUNT PER MANUFACTURER'S
SPECIFICATIONS.

PROPOSED RRUS DETAIL 2
SCALE: N.T.S



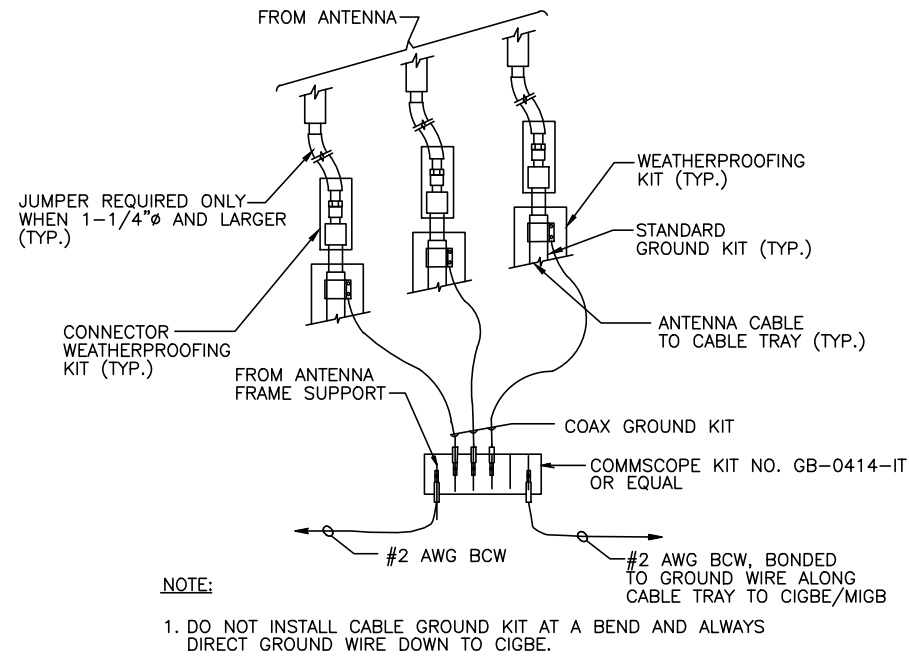
SITE NUMBER: CTL02036
SITE NAME: CHESHIRE SW

751 HIGGINS ROAD
CHESHIRE, CT 06410
NEW HAVEN COUNTY

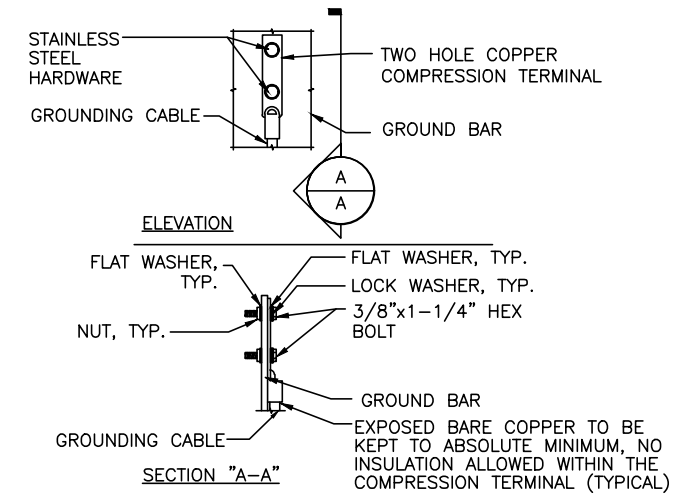


0	02/01/23	ISSUED FOR REVIEW	DO	AT	DPH
A	01/11/23	ISSUED FOR REVIEW	VD	AT	DPH
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: VD		

AT&T		
DETAILS LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	A-4	0

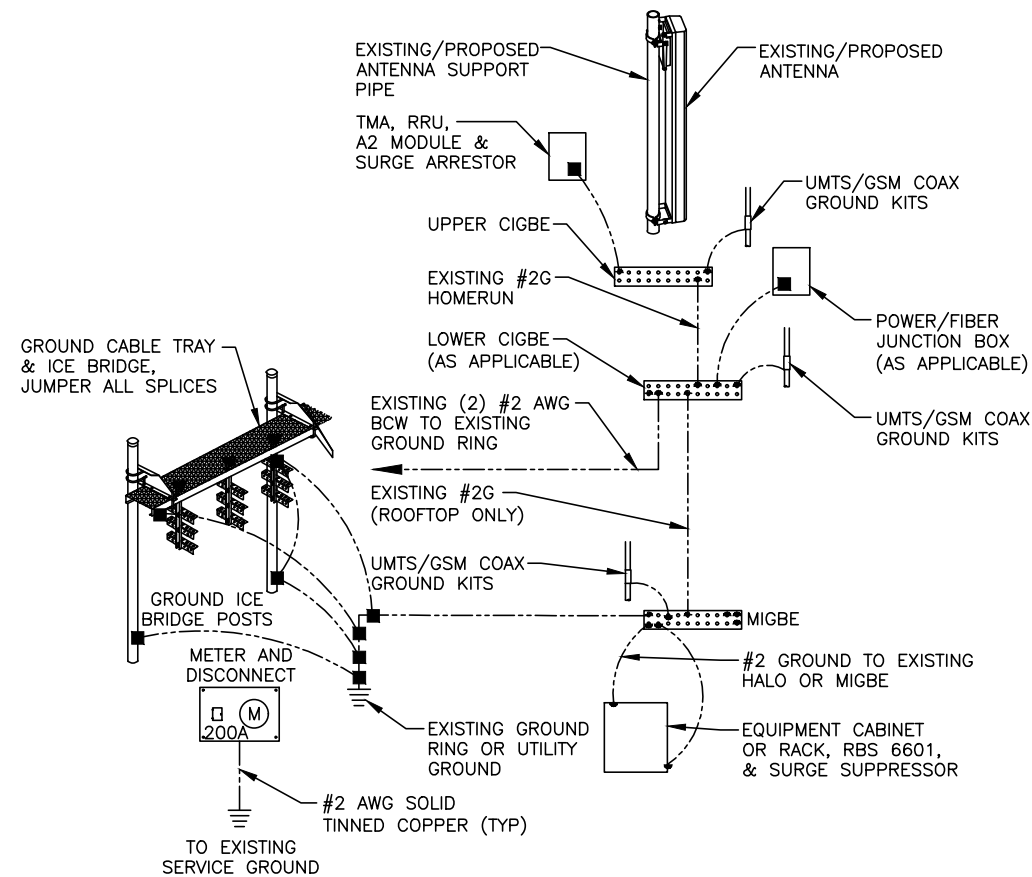


GROUND WIRE TO GROUND BAR CONNECTION DETAIL 1
SCALE: N.T.S. G-1



- NOTES:**
1. "DOUBLING UP" OR "STACKING" OF CONNECTION IS NOT PERMITTED.
2. OXIDE INHIBITING COMPOUND TO BE USED AT ALL LOCATION.
3. CADWELD DOWNLEADS FROM UPPER EGB, LOWER EGB, AND MGB

TYPICAL GROUND BAR CONNECTION DETAIL 3
SCALE: N.T.S. G-1



GROUNDING RISER DIAGRAM 2
SCALE: N.T.S. G-1

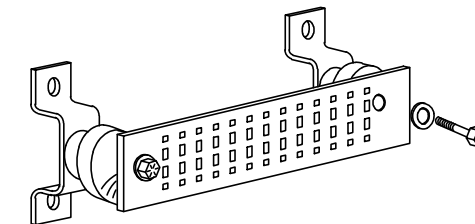
EACH GROUND CONDUCTOR TERMINATING ON ANY GROUND BAR SHALL HAVE AN IDENTIFICATION TAG ATTACHED AT EACH END THAT WILL IDENTIFY ITS ORIGIN AND DESTINATION.

SECTION "P" - SURGE PRODUCERS

- CABLE ENTRY PORTS (HATCH PLATES) (#2 AWG)
- GENERATOR FRAMEWORK (IF AVAILABLE) (#2 AWG)
- TELCO GROUND BAR
- COMMERCIAL POWER COMMON NEUTRAL/GROUND BOND (#2 AWG)
- +24V POWER SUPPLY RETURN BAR (#2 AWG)
- 48V POWER SUPPLY RETURN BAR (#2 AWG)
- RECTIFIER FRAMES.

SECTION "A" - SURGE ABSORBERS

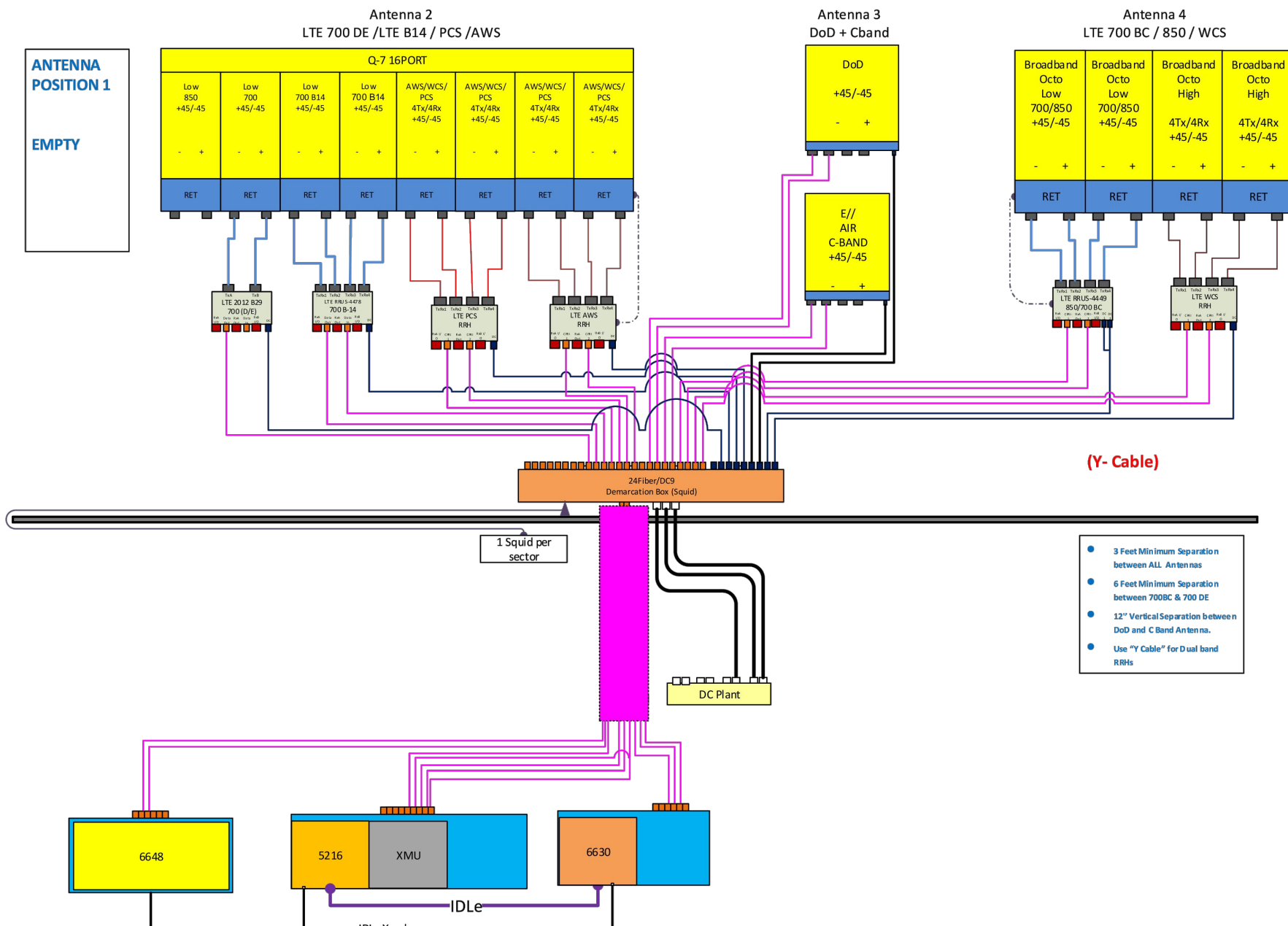
- INTERIOR GROUND RING (#2 AWG)
- EXTERNAL EARTH GROUND FIELD (BURIED GROUND RING) (#2 AWG)
- METALLIC COLD WATER PIPE (IF AVAILABLE) (#2 AWG)
- BUILDING STEEL (IF AVAILABLE) (#2 AWG)



GROUND BAR - DETAIL (AS REQUIRED) 4
SCALE: N.T.S. G-1

0	02/01/23	ISSUED FOR REVIEW	DO	AT	DPH
A	01/11/23	ISSUED FOR REVIEW	VD	AT	DPH
NO.	DATE	REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: VD		

AT&T		
GROUNDING DETAILS LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	G-1	0



NOTE:
 1. CONTRACTOR TO CONFIRM ALL PARTS.
 2. INSTALL ALL EQUIPMENT TO MANUFACTURER'S RECOMMENDATIONS

NOTE:
 REFER TO THE PRELIMINARY/APPROVED RFDS V1.0 DATED: 10/25/2021 DATA SHEET FOR FINAL ANTENNA SETTINGS.

RF PLUMBING DIAGRAM
 SCALE: N.T.S

1
RF-1

NO.	DATE	ISSUED FOR REVIEW	DO	AT	DPH
0	02/01/23	ISSUED FOR REVIEW	DO	AT	DPH
A	01/11/23	ISSUED FOR REVIEW	VD	AT	DPH
		REVISIONS	BY	CHK	APP'D
SCALE: AS SHOWN		DESIGNED BY: AT	DRAWN BY: VD		

AT&T		
RF PLUMBING DIAGRAM LTE 6C 2023 UPGRADE		
SITE NUMBER	DRAWING NUMBER	REV
CTL02036	RF-1	0

Exhibit 2



Town of Cheshire, CT

Property Listing Report

Map Block Lot **69 53**

Building # **1** Unique Identifier **00712600**

Property Information

Property Location	751 HIGGINS RD
Mailing Address	P O BOX 7207 BEDMINSTER NJ 07921
Land Use	Light Industrial
Zoning Code	R-40
Neighborhood	I-1C

Owner	AMER TEL & TEL CO
Co-Owner	AT&T PROPERTY TAX UNIT
Book / Page	0148/0566
Land Class	Industrial
Census Tract	3434
Acreage	19.8

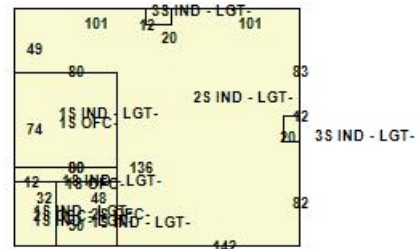
Valuation Summary

(Assessed value = 70% of Appraised Value)

Item	Appraised	Assessed
Buildings	2312630	1618840
Outbuildings	29640	20750
Land	429316	300520
Total	2771586	1940110

Utility Information

Electric	No
Gas	No
Sewer	No
Public Water	No
Well	No



Primary Construction Details

Year Built	1968
Building Desc.	Commercial
Building Style	
Stories	2.00
Exterior Walls	Pre-Cast Concrete
Exterior Walls 2	B. V. Solid
Interior Walls	
Interior Walls 2	
Interior Floors 1	Composite
Interior Floors 2	

Heating Fuel	
Heating Type	
AC Type	Central
Bedrooms	0
Full Bathrooms	0
Half Bathrooms	0
Extra Fixtures	0
Total Rooms	0
Bath Style	NA
Kitchen Style	
Occupancy	0

Building Use	Light Industrial
Building Condition	Average
Frame Type	Average
Fireplaces	0
Bsmt Gar	0
Fin Bsmt Area	
Fin Bsmt Quality	
Building Grade	-50
Roof Style	HIP
Roof Cover	Asphalt

Report Created On

3/23/2022



Town of Cheshire, CT

Property Listing Report

Map Block Lot **69 53**

Building # **1**

Unique Identifier

00712600

Detached Outbuildings

Type	Description	Area (sq ft)	Condition	Year Built
Fencing	Fencing	2400	Average	1968
Paving	Paving	43000	Average	1968
Fencing	Fencing	1560	Average	1968
Fencing	Fencing	600	Average	1968

Attached Extra Features

Type	Description	Area (sq ft)	Condition	Year Built

Sales History

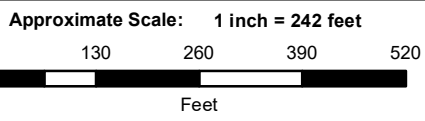
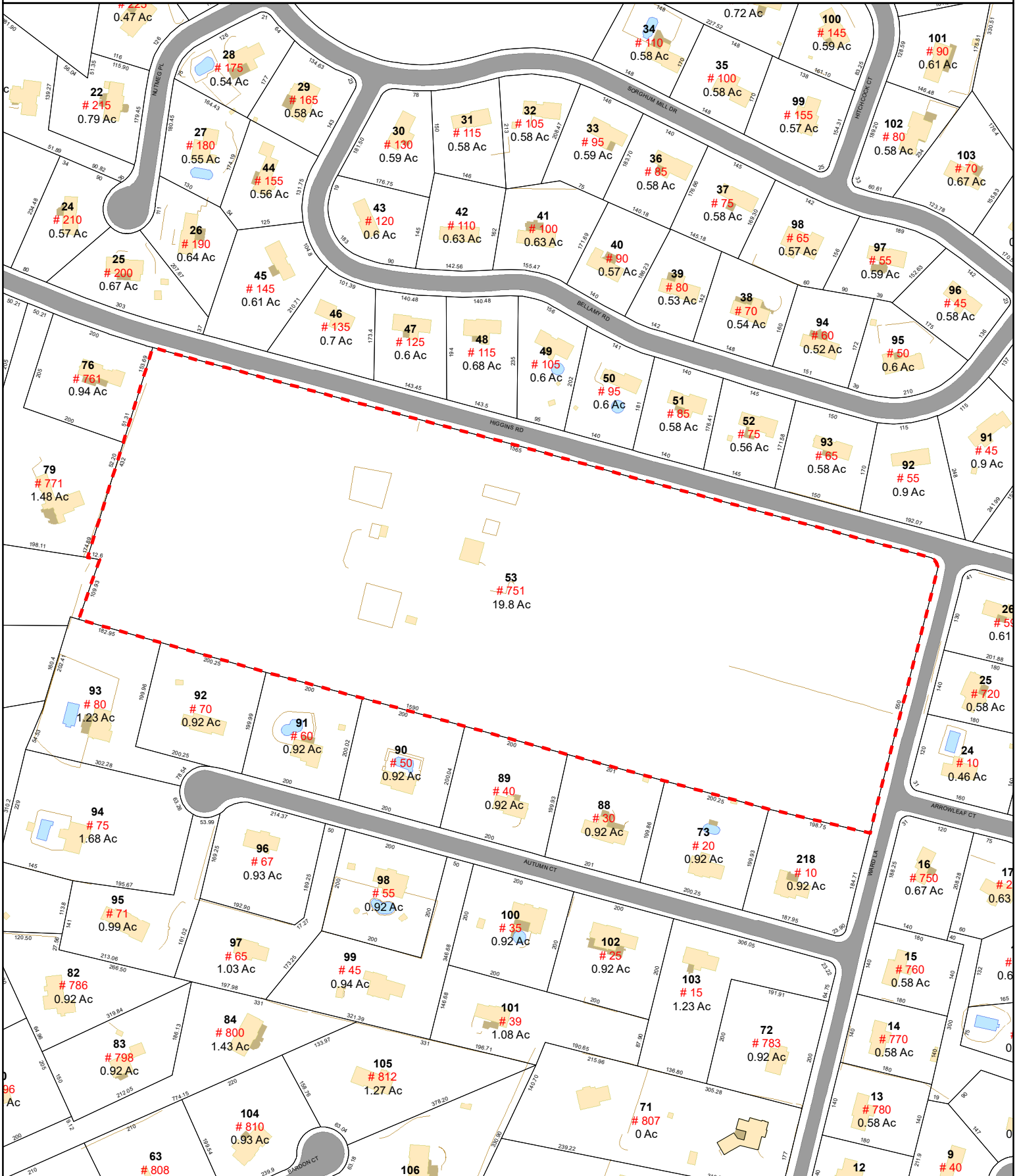
Owner of Record	Book/ Page	Sale Date	Sale Price

Town of Cheshire, Connecticut - Assessment Parcel Map



Parcel: 00712600

Location: 751 HIGGINS RD



Map Produced: July 2021

Disclaimer: This map is for informational purposes only. All information is subject to verification by any user. The Town of Cheshire and its mapping contractors assume no legal responsibility for the information contained herein.

Exhibit 3



Centerline Communications LLC
 750 W Center St, Suite 301,
 West Bridgewater, MA 02379



GPD Engineering and Architecture
 Professional Corporation

Mac Risley
 520 South Main Street, Suite 2531
 Akron, OH 44311
 (678) 781-5067
 mrisley@gpdgroup.com

GPD# 2023701.51
 March 7, 2023

STRUCTURAL ANALYSIS REPORT

AT&T DESIGNATION: **USID #:** **TAG0053** **26014**
 Site FA #: **10136365** **10034996**
 Client #: **CT2036**
 Site Name: **CHESHIRE**

ANALYSIS CRITERIA: **Codes:** **TIA-222-H & 2022 CBC**
 128 mph (3-second gust) w/ 0" ice
 50 mph (3-second gust) w/ 1" ice

SITE DATA: **751 Higgins Road, Cheshire, CT 06410, New Haven County**
 Latitude 41° 29' 14.87" N, Longitude 72° 55' 45.59" W
 Market: Connecticut
 250.0' Radio Relay Towers Wireline Self Support

To whom it may concern,

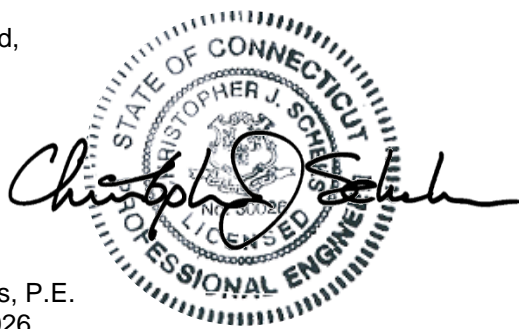
GPD is pleased to submit this Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

Analysis Results

Tower Stress Level with Proposed Equipment: 72.4% Pass
 Building Pedestal Ratio with Proposed Equipment: 22.7% Pass

We at GPD appreciate the opportunity of providing our continuing professional services to you and Centerline Communications. If you have any questions or need further assistance on this or any other projects, please do not hesitate to call.

Respectfully submitted,



Christopher J. Scheks, P.E.
 Connecticut #: 0030026

3/7/2023

SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT&T Mobility and commissioned by Centerline Communications.

The analysis has been performed in accordance with the 2022 Connecticut State Building Code based upon a 3-second gust wind speed of 128 mph. Applicable Standard references and design criteria are listed in report appendices.

Detailed foundation and geotechnical information for the building were not available or provided for this report. Therefore, the in-place capacities could not be verified. However, based on the reserve capacity of the supporting pedestals, it is our opinion that the supporting building and foundations will be adequate for the proposed loading configuration.

TOWER SUMMARY AND RESULTS

Member	Capacity	Results
Legs	72.4%	Pass
Leg Bolts	52.2%	Pass
Diagonals	41.6%	Pass
Horizontals	37.6%	Pass
Redundant Members	49.5%	Pass
Internal Bracing	42.0%	Pass
Member Bolts	58.6%	Pass
Anchor Rods	26.0%	Pass
Building Pedestals	22.7%	Pass
Foundation	Adequate	Pass

RECOMMENDATIONS

The tower and its foundation(s) have sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

ANALYSIS METHOD

RISA-3D (Version 17.0.4), tnxTower (Version 8.1.1.0), and EnerCalc (Build 12.20.8.24), commercially available software programs, were used to create a three-dimensional model of the tower and calculate primary member stresses for various load cases. Selected output from the analysis is included in the report appendices. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information.

DOCUMENTS PROVIDED

Document	Remarks	Source
RF Data Sheet	RFDS Name CTL02036 Rev preliminary, dated 1/13/2023	CLC
Construction Drawings	CLC Site #: CTL02036, Rev 0, dated: 2/1/2023	CLC
Tower Design	AT&T Co. Drawing #: NA4J03-902 Rev 3, dated 6/5/1967	AT&T
Building Drawings	AT&T Co. L-4 Junction Building, dated 12/1/1965	AT&T
Tower Mapping	GPD Project #: 2013723.01.TAG0053.03, dated 1/17/2014	AT&T
Ground Mapping	GPD Project #: 2013723.01.TAG0053.01, dated 6/14/2013	AT&T
Foundation Mapping	FDH Project #: 11-12049E-N1, dated 12/20/2011	AT&T
Geotechnical Report	Not Provided	N/A
Modification Drawings	GPD Project #: 2012856.05, dated 7/25/2012	AT&T
Post Modification Inspection	Centek Project #: 12033.OO40, dated 4/24/2013	AT&T
Previous Tower Analysis	GPD Project #: 2022702.66, dated 5/20/2022	GPD
Mount Analysis	TEP Project #: CT2036 Rev 1, dated 2/17/2023	GPD

ASSUMPTIONS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The appurtenance configuration is as supplied, determined from available photos, and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
4. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
5. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
6. All prior structural modifications, if applicable, are assumed to be as per data supplied/available and to have been properly installed.
7. Loading interpreted from photos is accurate to $\pm 5'$ AGL, antenna size accurate to ± 3.3 sf, and coax equal to the number of existing antennas without reserve.
8. All existing and proposed loading has been taken from the available site photos as well as documents supplied to GPD at the time of generating this report. All such documents are listed in the Documents Provided Table and are assumed to be accurate. GPD is not responsible for loading scenarios outside those conveyed in the supplied documentation.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD should be allowed to review any new information to determine its effect on the structural integrity of the tower.

DISCLAIMER OF WARRANTIES

GPD has not performed a recent site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD in connection with this Rigorous Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

This analysis is limited to the designated maximum wind and seismic conditions per the governing tower standards and code. Wind forces resulting in tower vibrations near the structure's resonant frequencies were not considered in this analysis and are outside the scope of this analysis. Lateral loading from any dynamic response was not evaluated under a time-domain based fatigue analysis.

GPD does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the capability of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the code specified amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

GPD makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD pursuant to this report will be limited to the total fee received for preparation of this report.

APPENDIX A

Tower Analysis Summary Form

Tower Analysis Summary Form

General Info

Site Name	CHESHIRE
Site Number	TAG0053
FA Number	10034996
Date of Analysis	3/7/2023
Company Performing Analysis	GPD

The information contained in this summary report is not to be used independently from the PE stamped tower analysis.

Tower Info	Description	Date
Tower Type (G, SST, MP)	SST	
Tower Height (top of steel AGL)	250'	
Tower Manufacturer	Radio Relay Towers	
Tower Model	Type "J"	
Tower Design	AT&T Co. Drawing #: NA4J03-902 Rev 3	6/5/1967
Building Drawings	AT&T Co. L-4 Junction Building	12/1/1965
Tower Mapping	TEP Project #: 111343	4/8/2011
Tower Mapping	Hudson Design Group	2/4/2013
Tower Mapping	GPD Project #: 2013724.01.TAG0053.03	1/17/2014
Ground Mapping	GPD Project #: 2013723.01.TAG0053.01	6/14/2013
Foundation Mapping	FDH Project #: 11-12049E-N1	12/20/2011
Modification Drawings	GPD Project #: 2012856.05	7/25/2012
Post Modification Inspection	Centek Project #: 12033.OO40	4/24/2013
Previous Structural Analysis	GPD Project #: 2022702.66	5/20/2022
Mount Analysis	TEP Project #: CT2036 Rev 1	2/17/2023

Design Parameters	
Design Code Used	TIA-222-H & 2022 CBC
Location of Tower (County, State)	New Haven, CT
Nominal Wind Speed (mph)	128 3-Second Gust
Ice Thickness (in)	1
Risk Category (I, II, III)	III
Exposure Category (B, C, D)	B
Topographic Category (1 to 5)	1

Analysis Results (% Maximum Usage)	
Existing/Reserved + Future + Proposed Condition	
Tower (%)	72.4%
Anchor Rods (%)	26.0%
Building Pedestals (%)	22.7%
Foundation Adequate?	Yes

Existing / Reserved Loading

Antenna Owner	Mount Height (ft)	Antenna						Mount			Transmission Line			
		Antenna CL (ft)	Quantity	Type	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Type	Quantity	Model	Size	Attachment Leg/Face
Unknown	252	265	1	Rod	Unknown	4' Lightning Rod		1	Unknown	Top Platform	1	Unknown	5/8"	Face A
Unknown	252	263	1	Beacon	Unknown	Flash Beacon				on the same mount				
AT&T Mobility	252	255	1	Panel	Kathrein	DMP65R-BU8DA	15/154/270	2	Unknown	Standoff Frames	6*	Unknown	1-5/8"	Face D
AT&T Mobility	252	255	2	Panel	Kathrein	DMP65R-BU6DA	15/154/270	2	Unknown	Standoff Frames	6	DC Power	0.78"	Face D
AT&T Mobility	252	255	2	Panel	CCI	TPA65R-BU6DA-K	15/154/270			on the existing mounts	3	Fiber	3/8"	Face D
AT&T Mobility	252	255	1	Panel	CCI	TPA65R-BU8DA-K	15/154/270			on the existing mounts				
AT&T Mobility	252	255	3	Panel	Ericsson	AIR6449 B77D+AIR6419 B77G Stacked	15/154/270			on the existing mounts				
AT&T Mobility	252	254	3	Surge	Raycap	DC9-48-60-24-8C-EV				on the proposed mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 32 B2				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 32 B30				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS 4478 B14				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	4449 B5/B12				on the same mounts				
AT&T Mobility	252	255	3	RRU	Ericsson	RRUS-32 B66A				on the same mounts				
AT&T Mobility	252	254	3	Surge	Raycap	DC9-48-60-24-8C-EV				on the same mounts				
Verizon	252	255	3	Panel	Antel	BXA-70063-6CF	30/140/260	2	Unknown	7' P2 STD Mount Pipe	12	Unknown	1-5/8"	Face D
Verizon	252	254	3	Panel	Commscope	JAHSS-65C-R3BT4	20/110/200	4	SitePro	VZSMART-MSK7	3	Hybrid	1-5/8"	Face D
Verizon	252	254	3	RRU	Samsung	CBRS RT4401-48				on the same mounts				
Verizon	252	254	3	Panel	Samsung	MT6407-77A	30/110/200			on the same mounts				
Verizon	252	254	3	Panel	Andrew	JAHH-65C-R3B-V2	20/110/200	5	Unknown	9' P2.5 STD Mount Pipe				
Verizon	252	254	3	Diplexer	Commscope	CBC78T-DS-43-2X				on the same mounts				
Verizon	252	254	3	RRU	Samsung	B5/B13 RRH-BR04C (RFV01U-D2A)				on the same mounts				
Verizon	252	254	3	RRU	Samsung	B2/B66A RRH-BR049 (RFV01U-D1A)				on the same mounts				
Verizon	252	254	3	Surge	Raycap	RHSDC-3315-PF-48				on the same mounts				
Verizon	252	254	1	GPS	Lucent	GPS				on the same mounts				
Town of Cheshire	249	255	1	Dipole	RFI	0A20-41 DIN		1	Unknown	6' Sidearm	1	Unknown	7/8"	Face D
Town of Cheshire	249	252.5	1	Dipole	RFI	0A20-67 DIN		1	Unknown	6' Sidearm	1	Unknown	7/8"	Face D
Town of Cheshire	240	240	1	Dish	RFS	SC3-W100AC		1	Unknown	Mount Pipe	1	RFS	E105	Face D
Misc.	239.5							1	Unknown	Platform				
Sprint	225	225.5	3	Panel	Celwave	APXVTM14-ALU-120	30/130/210	8	Unknown	20' Pipe Mounts	4	Hybrid	1"	Face D
Sprint	225	225.5	3	Panel	Comscope	NNVV-65B-R4	30/130/210			on the same mounts				
Sprint	225	225.5	3	RRU	Alcatel Lucent	TD-RRH 8x25				on the same mounts				
Sprint	225	225.5	6	RRU	Alcatel Lucent	800 MHz 2x50W				on the same mounts				
Sprint	225	225.5	3	RRU	Alcatel Lucent	1900 MHz 4x45				on the same mounts				
Nextel	210	212	6	Panel	Decibel	DB844H90E-XY	30/255	2	Unknown	14' Sector Frames	6	Unknown	1-5/8"	Face D
T-Mobile	210	212	2	Panel	Ericsson	AIR21 B4A/B2P	60/140	2	Unknown	14' Sector Frames	2	Hybrid	7/8"	Face B
T-Mobile	210	212	2	Panel	Ericsson	KRC 118 048/1 B4A/B12P-B8P	60/140			on the same mounts				
T-Mobile	210	212	2	RRU	Ericsson	RRUS11 B12				on the same mounts				
T-Mobile	210	212	2	RRU	Ericsson	RRUS11 B2				on the same mounts				
Unknown	210	207	1	Panel	Unknown	26"x26"x2" Flat Panel	160			on the same mounts	1	Unknown	1/2"	Face A
Nextel	198	200	3	Panel	Decibel	DB844H90E-XY	135	1	Unknown	14' Sector Frame	3	Unknown	1-5/8"	Face D
SGI	190	196	2	Omni	Unknown	PG1-NOF-0091		2	Unknown	5' Standoffs	2	Unknown	7/8"	Face D
SGI	171	177	1	Omni	Unknown	PG1-DOF-0093		1	Unknown	5' Standoff	1	Unknown	7/8"	Face D
Misc.	139.5							1	Unknown	Platforms w/ Rails				
AT&T Internet Services	85	88	1	Yagi	Wade	WL 7-13/S		3	Unknown	Standoffs	7	Unknown	5/8"	Face D
AT&T Internet Services	85	85	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	84	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	83	1	Yagi	Wade	WL 14-69/S				on the same mounts				
AT&T Internet Services	85	81	1	Yagi	Wade	WL 14-69/S				on the same mounts				
Unknown	37	37	1	Camera	Vicon	Camera - V8300H		1	Unknown	2.5' Box Mount	1	Conduit	1"	Face A
Unknown	36.5	36.5	1	GPS	Lucent	407517689		1	Unknown	3' Side Arm	1	Unknown	1/2"	Face D
Unknown	21	21	2	Junction	Unknown	Junction Box		1	Unknown	Platform	1	Conduit	1"	Face A
Unknown	21	21	1	RRU	Unknown	28" x 15.5" x 10" RRU				on the same mount				

*Indicates equipment to be removed

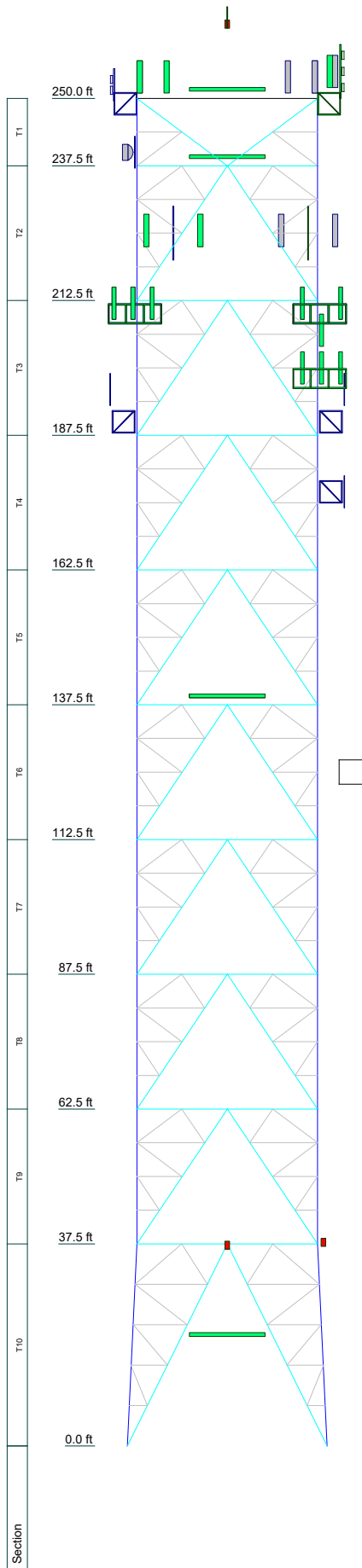
Proposed Loading

Antenna Owner	Mount Height (ft)	Antenna						Mount			Transmission Line			
		Antenna CL (ft)	Quantity	Type	Manufacturer	Model	Azimuth	Quantity	Manufacturer	Type	Quantity	Model	Size	Attachment Leg/Face
AT&T Mobility	252	255	3	RRH	Ericsson	RRUS-2012 B29	15/154/270			on the existing mounts	3	DC Power	6AWG	Face D
AT&T Mobility											3	Fiber	24Pair	Face D

Note: The proposed equipment shall be installed in addition to the existing/reserved loading at the same elevation.

APPENDIX B

Software Output Files and Calculations




MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A36	36 ksi	58 ksi			

TOWER DESIGN NOTES

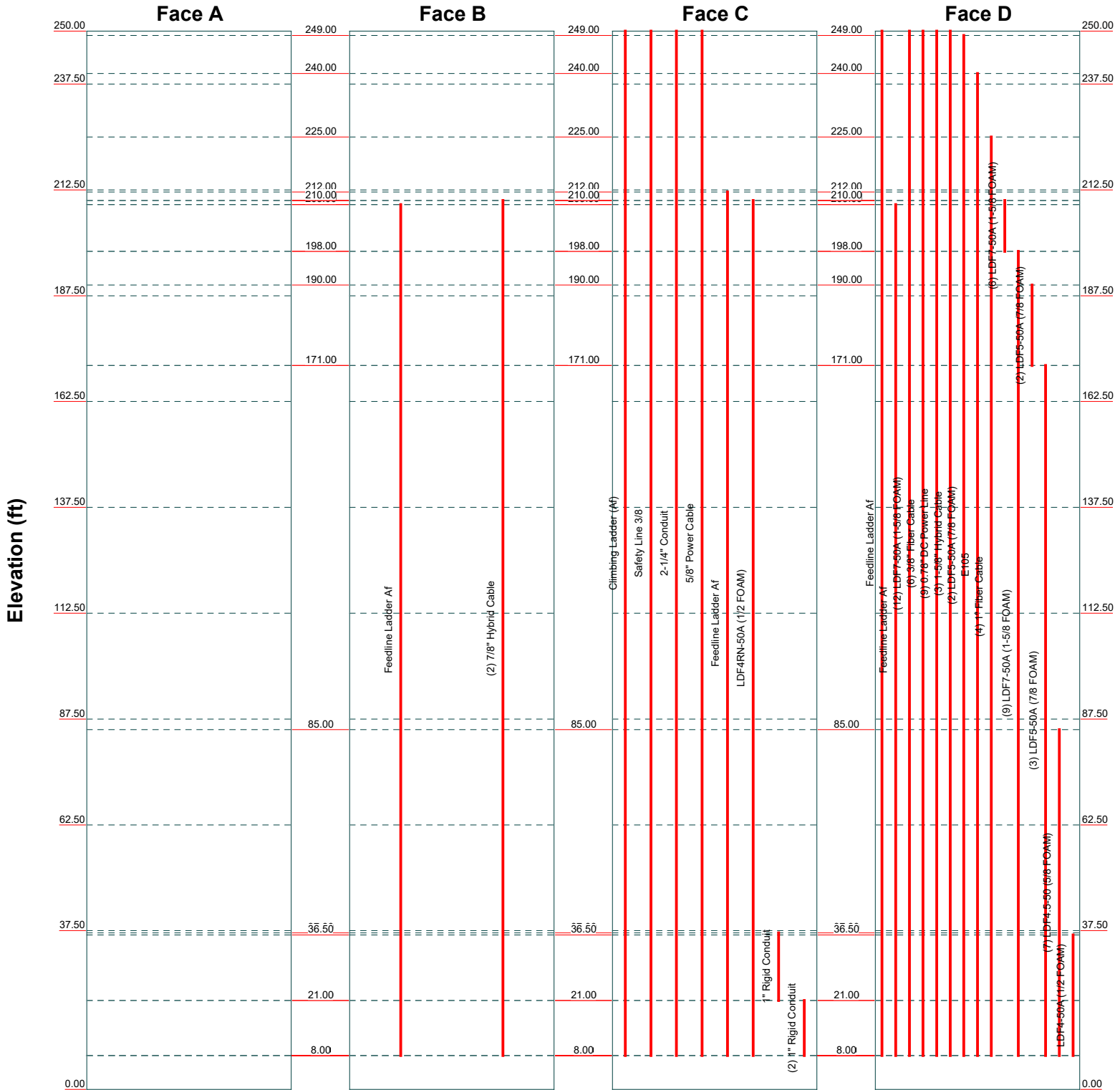
1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-H Standard.
3. Tower designed for a 128 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 1 with Crest Height of 0.00 ft

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	Project: 2023701.51		
	Client: Centerline Communications	Drawn by: ckuhn	App'd:
	Code: TIA-222-H	Date: 03/01/23	Scale: NTS
	Path:		Dwg No. E-1

Feed Line Distribution Chart

0' - 250'

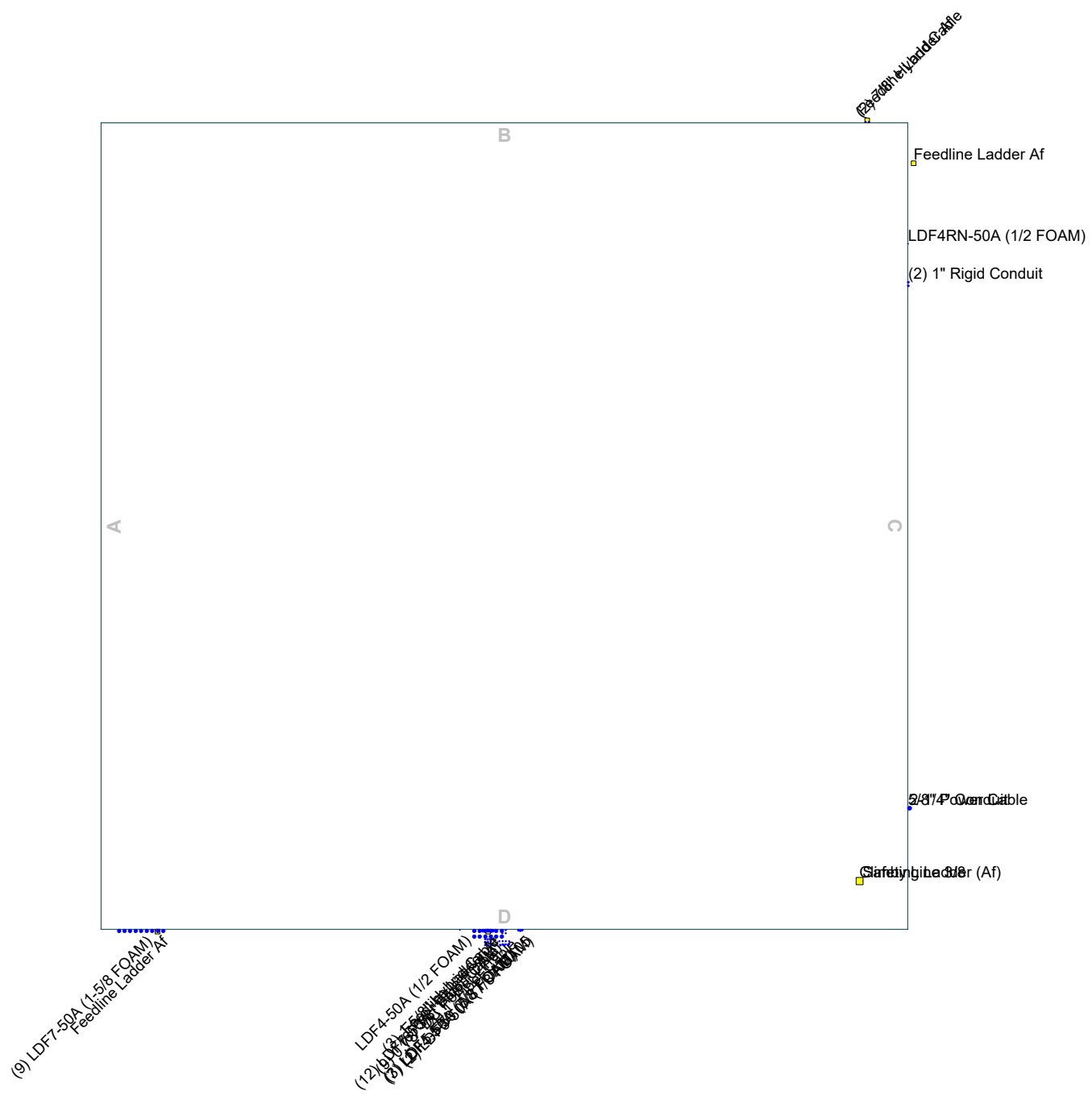
— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



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	Project: 2023701.51		
	Client: Centerline Communications	Drawn by: ckuhn	App'd:
	Code: TIA-222-H	Date: 03/01/23	Scale: NTS
	Path:		Dwg No. E-7

Feed Line Plan

— Round
 — Flat
 — App In Face
 — App Out Face



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	Project: 2023701.51		
	Client: Centerline Communications	Drawn by: ckuhn	App'd:
	Code: TIA-222-H	Date: 03/01/23	Scale: NTS
	Path:	Dwg No. E-7	

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Tower Input Data

The main tower is a 4x free standing tower with an overall height of 250.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 33.50 ft at the top and 37.00 ft at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in New Haven County, Connecticut.

Tower base elevation above sea level: 261.00 ft.

Basic wind speed of 128 mph.

Risk Category III.

Exposure Category B.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 1.

Crest Height: 0.00 ft.

Nominal ice thickness of 1.0000 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

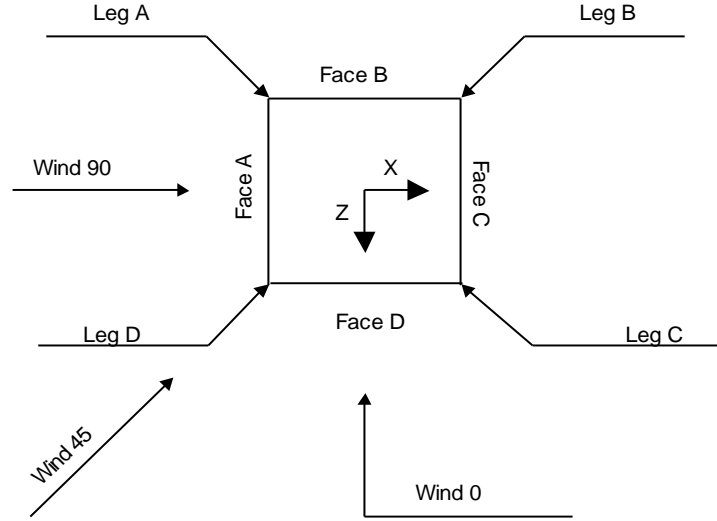
Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg √ Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r Retension Guys To Initial Tension √ Bypass Mast Stability Checks √ Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination √ Sort Capacity Reports By Component √ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs 	<ul style="list-style-type: none"> Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feed Line Torque √ Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
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Square Tower

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf

Climbing Ladder (Af)	C	No	No	Af (CaAa)	250.00 - 8.00	-24.000	0.44	1	1	3.8400	3.8400		4.81
Safety Line 3/8"	C	No	No	Ar (CaAa)	250.00 - 8.00	-24.000	0.44	1	1	0.3750	0.3750		0.22
2-1/4" Conduit	C	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.35	1	1	2.2500	2.2500		0.32
5/8" Power Cable	C	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.35	1	1	0.6300	0.5000		0.15

Feedline Ladder Af	D	No	No	Af (CaAa)	250.00 - 8.00	0.0000	0.02	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	C	No	No	Af (CaAa)	212.00 - 8.00	2.0000	-0.45	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	B	No	No	Af (CaAa)	209.00 - 8.00	0.0000	0.45	1	1	2.5000	2.5000		7.00
Feedline Ladder Af	D	No	No	Af (CaAa)	209.00 - 8.00	0.0000	0.43	1	1	2.5000	2.5000		7.00

LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.02	12	6	1.0000	1.9800		0.82
3/8" Fiber Cable	D	No	No	Ar (CaAa)	250.00 - 8.00	5.0000	0.02	6	3	0.3750	0.3750		0.10
0.78" DC Power Line	D	No	No	Ar (CaAa)	250.00 - 8.00	5.0000	0.02	9	3	0.7800	0.7800		0.33
1-5/8" Hybrid Cable	D	No	No	Ar (CaAa)	250.00 - 8.00	0.0000	0.02	3	3	1.0000	1.6250		0.82

LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	249.00 - 8.00	0.0000	-0.02	2	2	1.0000	1.0900		0.33

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Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
*** E105	D	No	No	Ar (CaAa)	240.00 - 8.00	0.0000	-0.02	1	1	1.0000	1.3000		0.40
*** 1" Fiber Cable	D	No	No	Ar (CaAa)	225.00 - 8.00	0.0000	0	4	2	0.8800	0.8800		0.60
*** LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	210.00 - 198.00	0.0000	0.45	6	6	1.0000	1.9800		0.82
*** LDF7-50A (1-5/8 FOAM)	D	No	No	Ar (CaAa)	198.00 - 8.00	0.0000	0.45	9	9	1.0000	1.9800		0.82
*** 7/8" Hybrid Cable	B	No	No	Ar (CaAa)	210.00 - 8.00	0.0000	0.45	2	2	0.8750	0.8750		0.28
*** LDF4RN-50A (1/2 FOAM)	C	No	No	Ar (CaAa)	210.00 - 8.00	0.0000	-0.35	1	1	0.6300	0.6300		0.15
*** LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	190.00 - 171.00	8.0000	0	2	2	1.0000	1.0900		0.33
*** LDF5-50A (7/8 FOAM)	D	No	No	Ar (CaAa)	171.00 - 8.00	8.0000	0	3	3	1.0000	1.0900		0.33
*** LDF4.5-50 (5/8 FOAM)	D	No	No	Ar (CaAa)	85.00 - 8.00	6.0000	0	7	4	0.8700	0.8700		0.15
*** 1" Rigid Conduit	C	No	No	Ar (CaAa)	37.00 - 21.00	0.0000	-0.3	1	1	1.0000	1.0000		0.50
*** 1" Rigid Conduit	C	No	No	Ar (CaAa)	21.00 - 8.00	0.0000	-0.3	2	2	1.0000	1.0000		0.50
*** LDF4-50A (1/2 FOAM)	D	No	No	Ar (CaAa)	36.50 - 8.00	0.0000	0.055	1	1	0.6300	0.6300		0.15

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAAA Front ft ²	CAAA Side ft ²	Weight lb
*** Lighting Rod 5/8" x 4'	B	None		0.0000	265.00	No Ice 0.25 1/2" Ice 0.66 1" Ice 0.97	0.25 0.66 0.97	31.00 33.82 39.29
Flash Beacon Lighting	B	None		0.0000	263.00	No Ice 2.70 1/2" Ice 3.10 1" Ice 3.50	2.70 3.10 3.50	50.00 70.00 90.00
13' I-Beam Mast Mount	B	None		0.0000	256.50	No Ice 13.00 1/2" Ice 14.14 1" Ice 15.08	13.00 14.14 15.08	300.00 550.00 800.00
*** DMP65R-BU8DA w/ Mount Pipe	B	From Face	4.00 -10.00 3.00	-7.0000	252.00	No Ice 17.87 1/2" Ice 18.50 1" Ice 19.14	10.02 11.44 12.72	29.30 147.98 277.00

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight
			Horz	Vert					
DMP65R-BU6DA w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	12.71	5.62	794.00
			-10.50			1/2" Ice	13.21	6.07	867.96
			3.00			1" Ice	13.71	6.53	948.56
DMP65R-BU6DA w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	12.71	5.62	794.00
			-20.75			1/2" Ice	13.21	6.07	867.96
			3.00			1" Ice	13.71	6.53	948.56
TPA-65R-BU8DA-K w/ Mount Pipe	B	From Face	4.00	-7.0000	252.00	No Ice	17.87	10.02	116.30
			-10.00			1/2" Ice	18.50	11.44	234.98
			3.00			1" Ice	19.14	12.72	364.01
TPA-65R-BU6DA-K w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	13.20	7.52	98.20
			-10.50			1/2" Ice	13.91	8.80	193.25
			3.00			1" Ice	14.59	9.93	297.04
TPA-65R-BU6DA-K w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	13.20	7.52	98.20
			-20.75			1/2" Ice	13.91	8.80	193.25
			3.00			1" Ice	14.59	9.93	297.04
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	B	From Face	4.00	-7.0000	252.00	No Ice	11.76	9.94	229.20
			-10.00			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	C	From Face	4.00	42.0000	252.00	No Ice	11.76	9.94	229.20
			-10.50			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
AIR6449 B77D+AIR6419 B77G STACKED w/ Mount Pipe	D	From Face	4.00	68.0000	252.00	No Ice	11.76	9.94	229.20
			-20.75			1/2" Ice	12.47	11.21	331.21
			3.00			1" Ice	13.14	12.34	441.99
RRUS 32 B2	B	From Face	4.00	-7.0000	252.00	No Ice	2.73	1.67	52.90
			-10.00			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B2	C	From Face	4.00	42.0000	252.00	No Ice	2.73	1.67	52.90
			-10.50			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B2	D	From Face	4.00	68.0000	252.00	No Ice	2.73	1.67	52.90
			-20.75			1/2" Ice	2.95	1.86	73.96
			3.00			1" Ice	3.18	2.05	98.21
RRUS 32 B30	B	From Face	4.00	-7.0000	252.00	No Ice	2.69	1.57	60.00
			-10.00			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 32 B30	C	From Face	4.00	42.0000	252.00	No Ice	2.69	1.57	60.00
			-10.50			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 32 B30	D	From Face	4.00	68.0000	252.00	No Ice	2.69	1.57	60.00
			-20.75			1/2" Ice	2.91	1.76	80.40
			3.00			1" Ice	3.14	1.95	103.95
RRUS 4478 B14	B	From Face	4.00	-7.0000	252.00	No Ice	1.84	1.06	59.90
			-10.00			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
RRUS 4478 B14	C	From Face	4.00	42.0000	252.00	No Ice	1.84	1.06	59.90
			-10.50			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
RRUS 4478 B14	D	From Face	4.00	68.0000	252.00	No Ice	1.84	1.06	59.90
			-20.75			1/2" Ice	2.01	1.20	75.78
			3.00			1" Ice	2.19	1.34	94.29
4449 B5/B12	B	From Face	4.00	-7.0000	252.00	No Ice	1.97	1.41	71.00
			-10.00			1/2" Ice	2.14	1.56	89.51
			3.00			1" Ice	2.33	1.73	110.84
4449 B5/B12	C	From Face	4.00	42.0000	252.00	No Ice	1.97	1.41	71.00
			-10.50			1/2" Ice	2.14	1.56	89.51
			3.00			1" Ice	2.33	1.73	110.84

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft ²	ft ²	lb
4449 B5/B12	D	From Face	4.00	4.00	68.0000	252.00	No Ice 1.97	1.41	71.00
			-20.75				1/2" Ice 2.14	1.56	89.51
			3.00				1" Ice 2.33	1.73	110.84
RRUS-32 B66A	B	From Face	4.00	4.00	-7.0000	252.00	No Ice 2.86	1.78	55.12
			-10.00				1/2" Ice 3.09	1.97	77.44
			3.00				1" Ice 3.32	2.17	103.04
RRUS-32 B66A	C	From Face	4.00	4.00	42.0000	252.00	No Ice 2.86	1.78	55.12
			-10.50				1/2" Ice 3.09	1.97	77.44
			3.00				1" Ice 3.32	2.17	103.04
RRUS-32 B66A	D	From Face	4.00	4.00	68.0000	252.00	No Ice 2.86	1.78	55.12
			-20.75				1/2" Ice 3.09	1.97	77.44
			3.00				1" Ice 3.32	2.17	103.04
2012 B29	B	From Face	4.00	4.00	-7.0000	252.00	No Ice 1.86	0.70	43.10
			-10.00				1/2" Ice 2.03	0.81	56.25
			3.00				1" Ice 2.20	0.94	71.85
2012 B29	C	From Face	4.00	4.00	42.0000	252.00	No Ice 1.86	0.70	43.10
			-10.50				1/2" Ice 2.03	0.81	56.25
			3.00				1" Ice 2.20	0.94	71.85
2012 B29	D	From Face	4.00	4.00	68.0000	252.00	No Ice 1.86	0.70	43.10
			-20.75				1/2" Ice 2.03	0.81	56.25
			3.00				1" Ice 2.20	0.94	71.85
DC9-48-60-24-8C-EV	B	From Face	4.00	4.00	-7.0000	252.00	No Ice 2.74	4.78	26.20
			-10.00				1/2" Ice 2.96	5.06	63.27
			2.00				1" Ice 3.20	5.35	104.42
DC9-48-60-24-8C-EV	C	From Face	4.00	4.00	42.0000	252.00	No Ice 2.74	4.78	26.20
			-10.50				1/2" Ice 2.96	5.06	63.27
			3.00				1" Ice 3.20	5.35	104.42
DC9-48-60-24-8C-EV	D	From Face	4.00	4.00	68.0000	252.00	No Ice 2.74	4.78	26.20
			-20.75				1/2" Ice 2.96	5.06	63.27
			3.00				1" Ice 3.20	5.35	104.42
10' In-Face Frame	C	From Face	4.00	4.00	0.0000	252.00	No Ice 12.84	1.42	250.00
			-21.00				1/2" Ice 15.40	1.70	325.00
			3.00				1" Ice 17.96	1.98	400.00
10' In-Face Frame	D	From Face	4.00	4.00	0.0000	252.00	No Ice 12.84	1.42	250.00
			-21.00				1/2" Ice 15.40	1.70	325.00
			3.00				1" Ice 17.96	1.98	400.00
Tower Top Platform	B	None			0.0000	252.00	No Ice 85.00	85.00	4425.00
							1/2" Ice 97.00	97.00	5752.50
							1" Ice 110.00	110.00	7080.00
L2 1/2x2 1/2x1/4 Mount Reinforcement	B	From Face	2.00	2.00	0.0000	252.00	No Ice 4.38	4.38	32.23
			-10.00				1/2" Ice 6.17	6.17	51.14
			3.00				1" Ice 7.97	7.97	70.05
(2) Pipe Mount 8'x2.875"	B	From Face	2.00	2.00	0.0000	252.00	No Ice 3.02	3.02	67.00
			-10.00				1/2" Ice 4.10	4.10	89.03
			3.00				1" Ice 5.20	5.20	117.92
P3 STD x 12.5' Horizontal	C	From Face	2.00	2.00	0.0000	252.00	No Ice 4.38	0.10	94.75
			-20.75				1/2" Ice 5.23	0.14	134.30
			3.00				1" Ice 6.10	0.19	184.21

JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	B	From Face	4.00	4.00	5.0000	252.00	No Ice 12.82	10.78	126.52
			16.25				1/2" Ice 13.42	12.20	227.13
			2.00				1" Ice 14.02	13.29	338.68
JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	C	From Face	4.00	4.00	5.0000	252.00	No Ice 12.82	10.78	126.52
			16.75				1/2" Ice 13.42	12.20	227.13
			2.00				1" Ice 14.02	13.29	338.68
JAHH-65C-R3B-V2 w/ 9' P2.5 STD Mount Pipe	D	From Face	4.00	4.00	5.0000	252.00	No Ice 12.82	10.78	126.52
			16.25				1/2" Ice 13.42	12.20	227.13

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight	
			Horz	Vert						
			ft	ft	°	ft	ft ²	ft ²	lb	
MT6407-77A w/ 7' P2.5 STD Mount Pipe & (2) VZWSMART-MSK7	B	From Face	2.00				1" Ice	14.02	13.29	338.68
			4.00		15.0000	252.00	No Ice	5.42	3.27	103.40
			11.25				1/2" Ice	5.97	3.99	148.53
MT6407-77A w/ 8' P2.5 STD Mount Pipe	C	From Face	2.00				1" Ice	6.45	4.59	199.20
			4.00		5.0000	252.00	No Ice	5.42	3.27	103.40
			3.00				1/2" Ice	5.97	3.99	148.53
MT6407-77A w/ 7' P2.5 STD Mount Pipe & (2) VZWSMART-MSK7	D	From Face	2.00				1" Ice	6.45	4.59	199.20
			4.00		5.0000	252.00	No Ice	5.42	3.27	103.40
			11.25				1/2" Ice	5.97	3.99	148.53
BXA-70063-6CF w/ 9' P2.5 STD Mount Pipe	A	From Face	2.00				1" Ice	6.45	4.59	199.20
			4.00		-25.0000	252.00	No Ice	7.57	5.49	45.95
			1.00				1/2" Ice	8.02	6.23	104.10
BXA-70063-6CF w/ 8' P2.5 STD Mount Pipe	B	From Face	3.00				1" Ice	8.47	6.99	170.26
			4.00		15.0000	252.00	No Ice	7.57	5.49	45.95
			20.00				1/2" Ice	8.02	6.23	104.10
BXA-70063-6CF w/ 9' P2.5 STD Mount Pipe	D	From Face	3.00				1" Ice	8.47	6.99	170.26
			5.00		-55.0000	252.00	No Ice	7.57	5.49	45.95
			-19.00				1/2" Ice	8.02	6.23	104.10
JAHSS-65C-R3BT4 w/ BSAMNT-SBS-2-3 & (3) SCP10W Clamp	B	From Face	3.00				1" Ice	8.47	6.99	170.26
			4.00		5.0000	252.00	No Ice	12.86	8.51	240.82
			16.25				1/2" Ice	13.46	9.11	316.79
JAHSS-65C-R3BT4 w/ BSAMNT-SBS-2-3 & (3) SCP10W Clamp	C	From Face	2.00				1" Ice	14.06	9.71	400.60
			4.00		5.0000	252.00	No Ice	12.86	8.51	240.82
			16.75				1/2" Ice	13.46	9.11	316.79
JAHSS-65C-R3BT4 w/ BSAMNT-SBS-2-3 & (3) SCP10W Clamp	D	From Face	2.00				1" Ice	14.06	9.71	400.60
			4.00		5.0000	252.00	No Ice	12.86	8.51	240.82
			16.25				1/2" Ice	13.46	9.11	316.79
CBC78T-DS-43-2X	B	From Face	2.00				1" Ice	14.06	9.71	400.60
			4.00		5.0000	252.00	No Ice	0.37	0.51	20.70
			16.25				1/2" Ice	0.45	0.60	27.04
CBC78T-DS-43-2X	C	From Face	2.00				1" Ice	0.53	0.70	35.07
			4.00		5.0000	252.00	No Ice	0.37	0.51	20.70
			16.75				1/2" Ice	0.45	0.60	27.04
CBC78T-DS-43-2X	D	From Face	2.00				1" Ice	0.53	0.70	35.07
			4.00		5.0000	252.00	No Ice	0.37	0.51	20.70
			16.25				1/2" Ice	0.45	0.60	27.04
B5/B13 RRH-BR04C (RFV01UD2A)	B	From Face	2.00				1" Ice	0.53	0.70	35.07
			4.00		0.0000	252.00	No Ice	1.88	1.01	70.30
			16.25				1/2" Ice	2.05	1.14	86.73
B5/B13 RRH-BR04C (RFV01UD2A)	C	From Face	2.00				1" Ice	2.22	1.28	105.83
			4.00		0.0000	252.00	No Ice	1.88	1.01	70.30
			16.75				1/2" Ice	2.05	1.14	86.73
B5/B13 RRH-BR04C (RFV01UD2A)	D	From Face	2.00				1" Ice	2.22	1.28	105.83
			4.00		0.0000	252.00	No Ice	1.88	1.01	70.30
			16.25				1/2" Ice	2.05	1.14	86.73
B2/B66a RRH-BR049 (RFV01UD1A)	B	From Face	2.00				1" Ice	2.22	1.28	105.83
			4.00		0.0000	252.00	No Ice	1.88	1.25	84.40
			16.25				1/2" Ice	2.05	1.39	102.74
B2/B66a RRH-BR049 (RFV01UD1A)	C	From Face	2.00				1" Ice	2.22	1.54	123.87
			4.00		0.0000	252.00	No Ice	1.88	1.25	84.40
			16.75				1/2" Ice	2.05	1.39	102.74
B2/B66a RRH-BR049 (RFV01UD1A)	D	From Face	2.00				1" Ice	2.22	1.54	123.87
			4.00		0.0000	252.00	No Ice	1.88	1.25	84.40
			16.25				1/2" Ice	2.05	1.39	102.74
CBRS RT4401-48	B	From Face	2.00				1" Ice	2.22	1.54	123.87
			4.00		0.0000	252.00	No Ice	0.85	0.30	17.60
			16.25				1/2" Ice	0.97	0.37	24.53

<p>tnxTower</p> <p>GPD 520 South Main Street Suite 2531 Akron, Ohio 44311 Phone: (330) 572-2100 FAX: (330) 572-2101</p>	Job		TAG0053 - CHESHIRE					Page	
	Project		2023701.51					Date	
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							ckuhn		

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight
			ft ft ft	°	ft	ft ²	ft ²	lb
x 2" Mount Pipe			-15.00			1/2" Ice	8.52	7.37
			0.50			1" Ice	9.46	8.78
APXVTM14-ALU-I20 w/ 10' x 2" Mount Pipe	D	From Face	1.00	0.0000	225.00	No Ice	7.60	5.98
			10.00			1/2" Ice	8.52	7.37
			0.50			1" Ice	9.46	8.78
NNVV-65B-R4 w/ Mount Pipe	B	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17
			15.00			1/2" Ice	12.77	8.13
			0.50			1" Ice	13.27	8.97
NNVV-65B-R4 w/ Mount Pipe	C	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17
			-15.00			1/2" Ice	12.77	8.13
			0.50			1" Ice	13.27	8.97
NNVV-65B-R4 w/ Mount Pipe	D	From Face	1.00	0.0000	225.00	No Ice	12.27	7.17
			10.00			1/2" Ice	12.77	8.13
			0.50			1" Ice	13.27	8.97
TD-RRH8x20-25	B	From Face	1.00	0.0000	225.00	No Ice	3.70	1.29
			15.00			1/2" Ice	3.95	1.46
			0.50			1" Ice	4.20	1.64
TD-RRH8x20-25	C	From Face	1.00	0.0000	225.00	No Ice	3.70	1.29
			-15.00			1/2" Ice	3.95	1.46
			0.50			1" Ice	4.20	1.64
TD-RRH8x20-25	D	From Face	1.00	0.0000	225.00	No Ice	3.70	1.29
			10.00			1/2" Ice	3.95	1.46
			0.50			1" Ice	4.20	1.64
(2) 800 MHz 2x50W	B	From Face	1.00	0.0000	225.00	No Ice	2.09	1.73
			15.00			1/2" Ice	2.27	1.90
			0.50			1" Ice	2.46	2.08
(2) 800 MHz 2x50W	C	From Face	1.00	0.0000	225.00	No Ice	2.09	1.73
			-15.00			1/2" Ice	2.27	1.90
			0.50			1" Ice	2.46	2.08
(2) 800 MHz 2x50W	D	From Face	1.00	0.0000	225.00	No Ice	2.09	1.73
			10.00			1/2" Ice	2.27	1.90
			0.50			1" Ice	2.46	2.08
1900 4x45 65 MHz RRU	B	From Face	1.00	0.0000	225.00	No Ice	2.08	1.99
			15.00			1/2" Ice	2.27	2.18
			0.50			1" Ice	2.47	2.37
1900 4x45 65 MHz RRU	C	From Face	1.00	0.0000	225.00	No Ice	2.08	1.99
			-15.00			1/2" Ice	2.27	2.18
			0.50			1" Ice	2.47	2.37
1900 4x45 65 MHz RRU	D	From Face	1.00	0.0000	225.00	No Ice	2.08	1.99
			10.00			1/2" Ice	2.27	2.18
			0.50			1" Ice	2.47	2.37

(3) DB844H90E-XY w/ Mount Pipe	A	From Leg	1.00	60.0000	210.00	No Ice	2.24	3.34
			0.00			1/2" Ice	2.61	3.73
			2.00			1" Ice	2.99	4.13
(3) DB844H90E-XY w/ Mount Pipe	D	From Leg	1.00	15.0000	210.00	No Ice	2.24	3.34
			0.00			1/2" Ice	2.61	3.73
			2.00			1" Ice	2.99	4.13
14' Sector Frame	A	From Leg	0.50	60.0000	210.00	No Ice	18.21	0.00
			0.00			1/2" Ice	23.76	0.00
			0.00			1" Ice	29.31	0.00
14' Sector Frame	D	From Leg	0.50	15.0000	210.00	No Ice	18.21	0.00
			0.00			1/2" Ice	23.76	0.00
			0.00			1" Ice	29.31	0.00

AIR21 B4A/B2P w/ mount pipe	B	From Leg	1.00	0.0000	210.00	No Ice	6.13	5.54
			0.00			1/2" Ice	6.52	6.20

tnxTower GPD 520 South Main Street Suite 2531 Akron, Ohio 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	TAG0053 - CHESHIRE	Page	9 of 11
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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft ²	ft ²	lb
AIR21 B4A/B2P w/ mount pipe	C	From Leg	2.00				1" Ice 6.92	6.87	218.21
			1.00		-10.0000	210.00	No Ice 6.13	5.54	101.25
			0.00				1/2" Ice 6.52	6.20	156.43
			2.00				1" Ice 6.92	6.87	218.21
KRC 118 048/1 B4A/B12P-B8P w/ Mount Pipe	B	From Leg	1.00		0.0000	210.00	No Ice 11.54	10.68	154.59
			0.00				1/2" Ice 12.16	12.09	246.84
			2.00				1" Ice 12.79	13.33	348.90
KRC 118 048/1 B4A/B12P-B8P w/ Mount Pipe	C	From Leg	1.00		-10.0000	210.00	No Ice 11.54	10.68	154.59
			0.00				1/2" Ice 12.16	12.09	246.84
			2.00				1" Ice 12.79	13.33	348.90
RRUS 11 B12	B	From Leg	1.00		0.0000	210.00	No Ice 2.83	1.18	50.70
			0.00				1/2" Ice 3.04	1.33	71.57
			2.00				1" Ice 3.26	1.48	95.49
RRUS 11 B12	C	From Leg	1.00		-10.0000	210.00	No Ice 2.83	1.18	50.70
			0.00				1/2" Ice 3.04	1.33	71.57
			2.00				1" Ice 3.26	1.48	95.49
RRUS 11 B2	B	From Leg	1.00		0.0000	210.00	No Ice 2.83	1.18	50.70
			0.00				1/2" Ice 3.04	1.33	71.57
			2.00				1" Ice 3.26	1.48	95.49
RRUS 11 B2	C	From Leg	1.00		-10.0000	210.00	No Ice 2.83	1.18	50.70
			0.00				1/2" Ice 3.04	1.33	71.57
			2.00				1" Ice 3.26	1.48	95.49
26"x 26" Flat Panel	C	From Leg	1.00		0.0000	210.00	No Ice 5.60	0.52	15.00
			0.00				1/2" Ice 5.92	0.67	38.43
			-3.00				1" Ice 6.24	0.83	65.30
14' Sector Frame	B	From Leg	0.50		0.0000	210.00	No Ice 18.21	0.00	492.00
			0.00				1/2" Ice 23.76	0.00	690.25
			0.00				1" Ice 29.31	0.00	888.50
14' Sector Frame	C	From Leg	0.50		-10.0000	210.00	No Ice 18.21	0.00	492.00
			0.00				1/2" Ice 23.76	0.00	690.25
			0.00				1" Ice 29.31	0.00	888.50

(3) DB844H90E-XY w/Mount Pipe	C	From Leg	1.00		-15.0000	198.00	No Ice 2.24	3.34	43.38
			0.00				1/2" Ice 2.61	3.73	78.61
			2.00				1" Ice 2.99	4.13	121.53
14' Sector Frame	C	From Leg	0.50		-15.0000	198.00	No Ice 18.21	0.00	492.00
			0.00				1/2" Ice 23.76	0.00	690.25
			0.00				1" Ice 29.31	0.00	888.50

PG1-NOF-0091	A	From Leg	3.50		-45.0000	190.00	No Ice 1.40	1.40	7.50
			-3.50				1/2" Ice 2.23	2.23	18.71
			6.00				1" Ice 3.07	3.07	35.15
5' Standoff	A	From Leg	1.75		-45.0000	190.00	No Ice 2.72	12.93	145.70
			-1.75				1/2" Ice 4.11	17.82	223.26
			0.00				1" Ice 5.50	22.71	300.83
PG1-NOF-0091	B	From Leg	3.50		45.0000	190.00	No Ice 1.40	1.40	7.50
			3.50				1/2" Ice 2.23	2.23	18.71
			6.00				1" Ice 3.07	3.07	35.15
5' Standoff	B	From Leg	1.75		45.0000	190.00	No Ice 2.72	12.93	145.70
			1.75				1/2" Ice 4.11	17.82	223.26
			0.00				1" Ice 5.50	22.71	300.83

PG1-DOF-0093	B	From Leg	3.50		45.0000	177.00	No Ice 1.40	1.40	7.50
			3.50				1/2" Ice 2.23	2.23	18.71
			0.00				1" Ice 3.07	3.07	35.15
5' Standoff	B	From Leg	1.75		45.0000	177.00	No Ice 2.72	12.93	145.70
			1.75				1/2" Ice 4.11	17.82	223.26

tnxTower GPD 520 South Main Street Suite 2531 Akron, Ohio 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	TAG0053 - CHESHIRE	Page	10 of 11
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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	CAAA Front	CAAA Side	Weight	
			Horz Lateral	Vert						ft
***			0.00				1" Ice	5.50	22.71	300.83
Catwalk	B	From Face	0.00		0.0000	139.50	No Ice	75.38	4.08	1250.00
			0.00				1/2" Ice	94.22	5.09	1600.00
			0.00				1" Ice	113.06	6.11	1950.00
Catwalk	C	From Face	0.00		0.0000	139.50	No Ice	75.38	4.08	1250.00
			0.00				1/2" Ice	94.22	5.09	1600.00
			0.00				1" Ice	113.06	6.11	1950.00

WL14-69/S	B	From Leg	1.00		-28.0000	85.00	No Ice	2.88	2.88	5.00
			0.00				1/2" Ice	3.74	3.74	6.50
			0.00				1" Ice	4.61	4.61	8.45
WL14-69/S	C	From Leg	1.00		-39.0000	85.00	No Ice	2.88	2.88	5.00
			0.00				1/2" Ice	3.74	3.74	6.50
			-2.00				1" Ice	4.61	4.61	8.45
WL14-69/S	B	From Leg	1.00		-28.0000	85.00	No Ice	2.88	2.88	5.00
			0.00				1/2" Ice	3.74	3.74	6.50
			-4.00				1" Ice	4.61	4.61	8.45

Camera	B	From Leg	1.50		0.0000	37.00	No Ice	0.11	0.05	2.00
			0.00				1/2" Ice	0.16	0.08	3.30
			0.00				1" Ice	0.21	0.12	5.42
2.5' Box Mount	B	From Leg	0.75		0.0000	37.00	No Ice	1.36	1.36	20.00
			0.00				1/2" Ice	2.45	2.45	40.00
			0.00				1" Ice	3.50	3.50	64.00

GPS	D	From Face	3.00		0.0000	36.50	No Ice	0.12	0.12	0.87
			0.00				1/2" Ice	0.21	0.21	3.85
			0.00				1" Ice	0.28	0.28	7.85
3' Side Arm	D	From Face	1.50		0.0000	36.50	No Ice	0.93	0.93	44.94
			0.00				1/2" Ice	1.13	1.13	54.87
			0.00				1" Ice	1.37	1.37	67.25

Junction Box (40"x14"x9")	B	From Face	0.00		0.0000	21.00	No Ice	3.88	2.50	50.00
			10.00				1/2" Ice	3.88	2.50	50.00
			0.00				1" Ice	3.88	2.50	50.00
RRU (28" x 15.5" x 10")	B	From Face	0.00		0.0000	21.00	No Ice	3.62	2.36	65.00
			10.00				1/2" Ice	3.86	2.57	94.93
			0.00				1" Ice	4.11	2.78	128.52
Platform	B	From Face	0.00		0.0000	21.00	No Ice	0.00	0.00	0.00
			10.00				1/2" Ice	0.00	0.00	0.00
			0.00				1" Ice	0.00	0.00	0.00

Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight
				Horz Lateral	Vert						

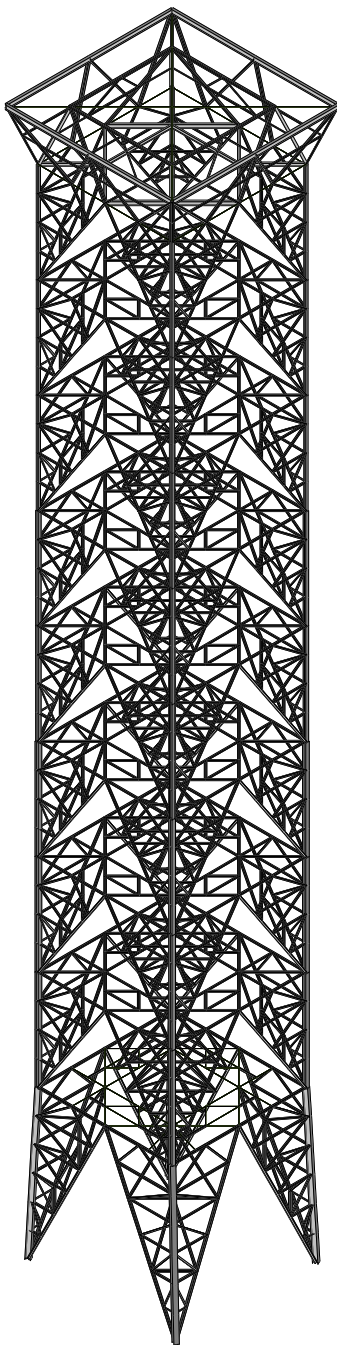
tnxTower

GPD

520 South Main Street Suite 2531
Akron, Ohio 44311
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Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight	
				Horz Lateral ft	Vert ft							
SC3-W100AC	A	Paraboloid w/Shroud (HP)	From Leg	1.00	74.0000			240.00	3.00	No Ice	7.07	400.00
				0.00					1/2" Ice	7.47	440.00	
				0.00					1" Ice	7.86	480.00	



Envelope Only Solution

GPD
C. Kuhn
2023701.51

TAG0053 / CHESHIRE
Rendered Tower

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Mar 7, 2023 at 6:50 AM
TAG0053 Final.r3d

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HÍ	VY Ü`ÜÖÖ`ÖÖÖ`HË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
HÏ	VY Ü`ÜÖÖ`PÖ`VH	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
HÏ	VY Ü`ÜÖÖ`PÖ`G`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
HÏ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
HJ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
I€	VY Ü`ÖPÖÜ`ÜWÜË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IF	VY Ü`ÖPÖÜ`Ü`VH	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IG	VY Ü`ÖPÖÜ`ÖUÜË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IH	VY Ü`ÖPÖÜ`VÜQË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
II	VY Ü`ÖPÖÜ`ÖÜÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÍ	VY Ü`ÖPÖÜ`SÖËË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IÏ	VY Ü`SÖÖ`VI	Y I`Y G	P[]^	P[]^	ÖHÍ	V]`ææ	I`ËH	F I`Ë	I`ËH	Ë I F
IÏ	VY Ü`PUUZ`VI	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IÏ	VY Ü`ÖÖÖ`VI	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	I`	I`Ë JJ	I`Ë I	Ë F I
IJ	VY Ü`ÜÖÖ`PUUZ`Ë	Shc`H`HFÏ`PUCE	P[]^	P[]^	ÖHÍ	V]`ææ	FËJ	Ë I	Ë I	Ë F I
I€	VY Ü`ÜÖÖ`PUUZ`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IF	VY Ü`ÜÖÖ`ÖÖÖ`VI	Shc`H`HFÏ`PUCE	P[]^	P[]^	ÖHÍ	V]`ææ	FËJ	Ë I	Ë I	Ë F I
IG	VY Ü`ÜÖÖ`PUUZ`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IH	VY Ü`ÜÖÖ`ÖÖÖ`GË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`ÖÖÖ`HË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`VI	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`G`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IJ	VY Ü`ÖPÖÜ`ÜWÜË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
I€	VY Ü`ÖPÖÜ`Ü`VI	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IF	VY Ü`ÖPÖÜ`ÖUÜË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IG	VY Ü`ÖPÖÜ`VÜQË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IH	VY Ü`ÖPÖÜ`ÖÜÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
II	VY Ü`ÖPÖÜ`SÖËË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IÏ	VY Ü`SÖÖ`VI	Y I`Y H	P[]^	P[]^	ÖHÍ	V]`ææ	JË H	H I`Ë	F FË	Ë H I
IÏ	VY Ü`PUUZ`VI	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IÏ	VY Ü`ÖÖÖ`VI	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	I`	I`Ë JJ	I`Ë I	Ë F I
IÏ	VY Ü`ÜÖÖ`PUUZ`Ë	Shc`H`HFÏ`PUCE	P[]^	P[]^	ÖHÍ	V]`ææ	FËJ	Ë I	Ë I	Ë F I
IJ	VY Ü`ÜÖÖ`PUUZ`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
I€	VY Ü`ÜÖÖ`ÖÖÖ`VI	Shc`H`HFÏ`PUCE	P[]^	P[]^	ÖHÍ	V]`ææ	FËJ	Ë I	Ë I	Ë F I
IF	VY Ü`ÜÖÖ`PUUZ`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IG	VY Ü`ÜÖÖ`ÖÖÖ`GË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IH	VY Ü`ÜÖÖ`ÖÖÖ`HË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`VI	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`G`Ë	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IÏ	VY Ü`ÜÖÖ`PÖ`ÖÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IJ	VY Ü`ÖPÖÜ`ÜWÜË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
IJ	VY Ü`ÖPÖÜ`Ü`VI	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
I€	VY Ü`ÖPÖÜ`ÖUÜË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IF	VY Ü`ÖPÖÜ`VÜQË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IG	VY Ü`ÖPÖÜ`ÖÜÖË	GSGÄFDc`GFBDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	FË	GË JJ	FËJ	ËGF
IH	VY Ü`ÖPÖÜ`SÖËË	GShc`GÄFDc`FD`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	GË H	HËH H	GËH	ËH I
II	VY Ü`SÖÖ`VI	Y I`Y I`€	P[]^	P[]^	ÖHÍ	V]`ææ	F FË	I`Ë	F I`	FË G
IÏ	VY Ü`PUUZ`VI	GShc`GÄFDc`HFÏ`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	HË G	I`Ë I	GË I`	Ë I`
IÏ	VY Ü`ÖÖÖ`VI	GShc`H`H`çHD	P[]^	P[]^	ÖHÍ	V]`ææ	I`Ë I	I`Ë I	I`Ë H	Ë H

<chFc`YX'GhY'8 YgJ| b'DU'Ua Yhfg'f' cbh|bi YXL

	Sää^	Ü@^	Š^)* oZca	Sà`Zca	Sà::Zca	Š&{ } A	ZHŠ&{ } A	ZHŠ&{ } H	S`	S::	Òa	Ø`&caH
FFUJ	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI €	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI F	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI G	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI H	TÍJG	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI I	TÍFI	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI Í	TÍGG	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI Î	TÍHF	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI Ì	TÍHU	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI Ì	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI J	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI €	TÍÍÍ	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI F	TÍÍH	VY Ü'ÜÖÖ' PUÜZ#FGHÎH	FGH	FGH	FGH	FGH	FGH	FGH	FÆH	F		Sää^ ð
FFI G	TÍJÍ	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI H	TÍ€	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI I	TÍFI	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI Í	TÍG	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI Î	TÍH	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI Ì	TÍÍ	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI Ì	TÍÍ	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI J	TÍÍ	VY Ü'ÜÖÖ' PUÜZ#FFHÎÍ	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	FÆH	F		Sää^ ð
FFI €	TFGÍ	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI F	TFGJ	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI G	TFH€	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI H	TFHEF	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI I	TFHEG	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Í	TFHEH	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Î	TFHEI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Ì	TFHEI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Ì	TFHEI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI J	TFHEI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI €	TFHEI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI F	TFHEJ	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI G	TÍJÍ	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI H	TÍ€	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI I	TÍFI	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI Í	TÍG	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI Î	TÍHU	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI Ì	TÍIJ	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI Ì	TÍÍ€	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI J	TÍÍ€	VY Ü'ÜÖÖ' PUÜZ#FHËÍ	FHËH	FHËH	FHËH	FHËH	FHËH	FHËH	FÆG	F		Sää^ ð
FFI €	TFI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI F	TFJ	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI G	TGH	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI H	TG	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI I	THE	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Í	THH	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Î	THI	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Ì	TÍ€	VY Ü'ÜÖÖ' PUÜZ#IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	IÆH	F	F		Sää^ ð
FFI Í	TÍG	VY Ü'ÜÖÖ' PUÜZ#IÆH	HËH	HËH	HËH	HËH	HËH	HËH	F	F		Sää^ ð
FFI J	TÍ€	VY Ü'ÜÖÖ' PUÜZ#IÆH	HËH	HËH	HËH	HËH	HËH	HËH	F	F		Sää^ ð
FFI €	TÍ	VY Ü'ÜÖÖ' PUÜZ#IÆH	HËH	HËH	HËH	HËH	HËH	HËH	F	F		Sää^ ð



TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2023701.51

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_DIAG_OUTER_T1	M1274	1.394	31.15	1.84	128.64	4.5%	Pass
TWR_DIAG_OUTER_T1	M1275	1.47	31.15	1.89	128.64	4.7%	Pass
TWR_DIAG_OUTER_T1	M1276	1.475	31.15	1.72	128.64	4.7%	Pass
TWR_DIAG_OUTER_T1	M1277	1.495	31.15	1.81	128.64	4.8%	Pass
TWR_DIAG_OUTER_T1	M1278	1.527	31.15	1.85	128.64	4.9%	Pass
TWR_DIAG_OUTER_T1	M1279	1.497	31.15	1.77	128.64	4.8%	Pass
TWR_DIAG_OUTER_T1	M1280	1.397	31.15	1.81	128.64	4.5%	Pass
TWR_DIAG_OUTER_T1	M1281	1.495	31.15	1.86	128.64	4.8%	Pass
TWR_DIAG_OUTER_T1	M1282	2.252	41.82	1.26	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1283	2.27	41.82	1.25	128.64	5.4%	Pass
TWR_DIAG_OUTER_T1	M1284	2.233	41.82	1.17	128.64	5.3%	Pass
TWR_DIAG_OUTER_T1	M1285	2.169	41.82	1.22	128.64	5.2%	Pass
TWR_DIAG_OUTER_T1	M1286	2.305	41.82	1.30	128.64	5.5%	Pass
TWR_DIAG_OUTER_T1	M1287	2.307	41.82	1.30	128.64	5.5%	Pass
TWR_DIAG_OUTER_T1	M1288	2.194	41.82	1.23	128.64	5.2%	Pass
TWR_DIAG_OUTER_T1	M1289	2.239	41.82	1.19	128.64	5.4%	Pass
TWR_DIAG_T1	M15	6.215	19.53	2.82	118.53	31.8%	Pass
TWR_DIAG_T1	M18	7.624	19.53	2.65	118.53	39.0%	Pass
TWR_DIAG_T1	M22	8.133	19.53	3.29	118.53	41.6%	Pass
TWR_DIAG_T1	M25	7.963	19.53	3.28	118.53	40.8%	Pass
TWR_DIAG_T1	M29	7.503	19.53	2.60	118.53	38.4%	Pass
TWR_DIAG_T1	M32	6.312	19.53	2.94	118.53	32.3%	Pass
TWR_DIAG_T1	M36	5.839	19.53	2.28	118.53	29.9%	Pass
TWR_DIAG_T1	M39	5.869	19.53	2.23	118.53	30.0%	Pass
TWR_DIAG_T2	M51	17.916	82.48	10.30	103.87	21.7%	Pass
TWR_DIAG_T2	M59	17.871	82.48	10.26	103.87	21.7%	Pass
TWR_DIAG_T2	M67	20.089	82.48	11.92	103.87	24.4%	Pass
TWR_DIAG_T2	M75	20.193	82.48	11.99	103.87	24.5%	Pass
TWR_DIAG_T2	M83	18.061	82.48	10.42	103.87	21.9%	Pass
TWR_DIAG_T2	M91	17.998	82.48	10.42	103.87	21.8%	Pass
TWR_DIAG_T2	M99	17.206	82.48	10.20	103.87	20.9%	Pass
TWR_DIAG_T2	M107	17.286	82.48	10.11	103.87	21.0%	Pass
TWR_DIAG_T3	M124	23.062	82.48	20.62	103.87	28.0%	Pass
TWR_DIAG_T3	M132	23.126	82.48	20.61	103.87	28.0%	Pass
TWR_DIAG_T3	M141	25.024	82.48	22.76	103.87	30.3%	Pass
TWR_DIAG_T3	M149	25.023	82.48	22.76	103.87	30.3%	Pass
TWR_DIAG_T3	M158	22.465	82.48	20.19	103.87	27.2%	Pass
TWR_DIAG_T3	M166	22.384	82.48	20.19	103.87	27.1%	Pass
TWR_DIAG_T3	M175	22.49	82.48	20.39	103.87	27.3%	Pass
TWR_DIAG_T3	M183	22.576	82.48	20.32	103.87	27.4%	Pass
TWR_DIAG_T4	M205	29.099	109.11	26.41	134.58	26.7%	Pass
TWR_DIAG_T4	M213	29.171	109.11	26.44	134.58	26.7%	Pass
TWR_DIAG_T4	M222	31.773	109.11	29.42	134.58	29.1%	Pass
TWR_DIAG_T4	M230	31.77	109.11	29.39	134.58	29.1%	Pass
TWR_DIAG_T4	M239	28.132	109.11	25.56	134.58	25.8%	Pass
TWR_DIAG_T4	M247	28.022	109.11	25.57	134.58	25.7%	Pass
TWR_DIAG_T4	M256	29.068	109.11	26.88	134.58	26.6%	Pass
TWR_DIAG_T4	M264	29.169	109.11	26.80	134.58	26.7%	Pass
TWR_DIAG_T5	M286	35.207	109.11	31.89	134.58	32.3%	Pass
TWR_DIAG_T5	M294	35.295	109.11	31.91	134.58	32.3%	Pass
TWR_DIAG_T5	M303	38.357	109.11	35.59	134.58	35.2%	Pass
TWR_DIAG_T5	M311	38.345	109.11	35.56	134.58	35.1%	Pass
TWR_DIAG_T5	M320	33.757	109.11	30.52	134.58	30.9%	Pass
TWR_DIAG_T5	M328	33.614	109.11	30.52	134.58	30.8%	Pass
TWR_DIAG_T5	M337	35.709	109.11	33.04	134.58	32.7%	Pass
TWR_DIAG_T5	M345	35.823	109.11	32.97	134.58	32.8%	Pass



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TWR_DIAG_T6	M367	41.295	123.38	38.29	140.74	33.5%	Pass
TWR_DIAG_T6	M375	41.401	123.38	38.31	140.74	33.6%	Pass
TWR_DIAG_T6	M384	45.089	123.38	42.59	140.74	36.5%	Pass
TWR_DIAG_T6	M392	45.073	123.38	42.56	140.74	36.5%	Pass
TWR_DIAG_T6	M401	39.499	123.38	36.47	140.74	32.0%	Pass
TWR_DIAG_T6	M409	39.323	123.38	36.47	140.74	31.9%	Pass
TWR_DIAG_T6	M418	42.495	123.38	40.06	140.74	34.4%	Pass
TWR_DIAG_T6	M426	42.616	123.38	39.98	140.74	34.5%	Pass
TWR_DIAG_T7	M448	46.358	123.38	43.58	140.74	37.6%	Pass
TWR_DIAG_T7	M456	46.459	123.38	43.62	140.74	37.7%	Pass
TWR_DIAG_T7	M465	50.893	123.38	48.43	140.74	41.3%	Pass
TWR_DIAG_T7	M473	50.873	123.38	48.39	140.74	41.2%	Pass
TWR_DIAG_T7	M482	44.188	123.38	41.32	140.74	35.8%	Pass
TWR_DIAG_T7	M490	43.985	123.38	41.32	140.74	35.7%	Pass
TWR_DIAG_T7	M499	48.425	123.38	46.02	140.74	39.2%	Pass
TWR_DIAG_T7	M507	48.577	123.38	45.94	140.74	39.4%	Pass
TWR_DIAG_T8	M529	53.458	163.93	49.31	183.52	32.6%	Pass
TWR_DIAG_T8	M537	53.558	163.93	49.34	183.52	32.7%	Pass
TWR_DIAG_T8	M546	57.848	163.93	54.47	183.52	35.3%	Pass
TWR_DIAG_T8	M554	57.822	163.93	54.42	183.52	35.3%	Pass
TWR_DIAG_T8	M563	50.808	163.93	46.59	183.52	31.0%	Pass
TWR_DIAG_T8	M571	50.584	163.93	46.60	183.52	30.9%	Pass
TWR_DIAG_T8	M580	55.322	163.93	52.07	183.52	33.7%	Pass
TWR_DIAG_T8	M588	55.497	163.93	51.98	183.52	33.9%	Pass
TWR_DIAG_T9	M610	58.007	163.93	53.67	183.52	35.4%	Pass
TWR_DIAG_T9	M618	58.067	163.93	53.68	183.52	35.4%	Pass
TWR_DIAG_T9	M627	63.323	163.93	59.48	183.52	38.6%	Pass
TWR_DIAG_T9	M635	63.295	163.93	59.47	183.52	38.6%	Pass
TWR_DIAG_T9	M644	54.957	163.93	50.49	183.52	33.5%	Pass
TWR_DIAG_T9	M652	54.775	163.93	50.46	183.52	33.4%	Pass
TWR_DIAG_T9	M661	60.906	163.93	57.14	183.52	37.2%	Pass
TWR_DIAG_T9	M669	61.058	163.93	57.09	183.52	37.2%	Pass
TWR_DIAG_T10	M691	63.83	196.60	54.85	216.14	32.5%	Pass
TWR_DIAG_T10	M701	63.467	196.60	54.90	216.14	32.3%	Pass
TWR_DIAG_T10	M712	81.952	197.78	74.39	216.14	41.4%	Pass
TWR_DIAG_T10	M722	82.105	197.78	74.43	216.14	41.5%	Pass
TWR_DIAG_T10	M733	58.875	196.60	50.77	216.14	29.9%	Pass
TWR_DIAG_T10	M743	59.084	196.60	50.45	216.14	30.1%	Pass
TWR_DIAG_T10	M754	78.914	197.78	71.66	216.14	39.9%	Pass
TWR_DIAG_T10	M764	78.935	197.78	71.72	216.14	39.9%	Pass
TWR_HORZ_T3	M123	9.878	61.03	13.13	71.53	18.4%	Pass
TWR_HORZ_T3	M140	10.944	61.03	14.62	71.53	20.4%	Pass
TWR_HORZ_T3	M157	9.674	61.03	11.18	71.53	15.9%	Pass
TWR_HORZ_T3	M174	9.832	61.03	11.02	71.53	16.1%	Pass
TWR_HORZ_T4	M204	14.531	61.03	14.88	71.53	23.8%	Pass
TWR_HORZ_T4	M221	16.178	61.03	16.59	71.53	26.5%	Pass
TWR_HORZ_T4	M238	14.057	61.03	12.51	71.53	23.0%	Pass
TWR_HORZ_T4	M255	14.779	61.03	13.10	71.53	24.2%	Pass
TWR_HORZ_T5	M285	17.521	61.03	17.66	71.53	28.7%	Pass
TWR_HORZ_T5	M302	19.557	61.03	19.96	71.53	32.0%	Pass
TWR_HORZ_T5	M319	16.776	61.03	14.95	71.53	27.5%	Pass
TWR_HORZ_T5	M336	18.158	61.03	16.12	71.53	29.8%	Pass



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TWR_HORZ_T6	M366	21.088	74.47	21.37	87.93	28.3%	Pass
TWR_HORZ_T6	M383	23.456	74.47	23.97	87.93	31.5%	Pass
TWR_HORZ_T6	M400	20.095	74.47	18.22	87.93	27.0%	Pass
TWR_HORZ_T6	M417	22.075	74.47	19.99	87.93	29.6%	Pass
TWR_HORZ_T7	M447	24.173	87.31	24.38	103.87	27.7%	Pass
TWR_HORZ_T7	M464	26.719	87.31	27.16	103.87	30.6%	Pass
TWR_HORZ_T7	M481	22.896	87.31	20.94	103.87	26.2%	Pass
TWR_HORZ_T7	M498	25.393	87.31	23.32	103.87	29.1%	Pass
TWR_HORZ_T8	M528	27.491	87.31	27.57	103.87	31.5%	Pass
TWR_HORZ_T8	M545	30.144	87.31	30.52	103.87	34.5%	Pass
TWR_HORZ_T8	M562	25.928	87.31	23.53	103.87	29.7%	Pass
TWR_HORZ_T8	M579	28.827	87.31	26.29	103.87	33.0%	Pass
TWR_HORZ_T9	M609	29.647	87.31	29.65	103.87	34.0%	Pass
TWR_HORZ_T9	M626	32.833	87.31	33.07	103.87	37.6%	Pass
TWR_HORZ_T9	M643	27.889	87.31	25.61	103.87	31.9%	Pass
TWR_HORZ_T9	M660	31.587	87.31	29.00	103.87	36.2%	Pass
TWR_HORZ_T10	M690	33.005	181.47	27.68	183.52	18.2%	Pass
TWR_HORZ_T10	M711	32.079	181.47	29.31	183.52	17.7%	Pass
TWR_HORZ_T10	M732	29.359	181.47	24.40	183.52	16.2%	Pass
TWR_HORZ_T10	M753	30.68	181.47	28.13	183.52	16.9%	Pass
TWR_INNER_BRACE_T3	M1221	0.021	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T3	M1222	0.02	30.89	0.01	48.02	0.1%	Pass
TWR_INNER_BRACE_T3	M1223	0.019	30.89	0.01	48.02	0.1%	Pass
TWR_INNER_BRACE_T3	M1224	0.02	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T3	M1225	0.021	30.89	0.01	48.02	0.1%	Pass
TWR_INNER_BRACE_T3	M1226	0.019	30.89	0.01	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1169	0.032	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1170	0.034	30.89	0.01	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1171	0.033	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1172	0.032	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1173	0.033	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T4	M1174	0.032	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1117	0.043	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1118	0.039	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1119	0.039	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1120	0.038	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1121	0.041	30.89	0.02	48.02	0.1%	Pass
TWR_INNER_BRACE_T5	M1122	0.04	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_BRACE_T6	M1065	0.051	30.89	0.03	48.02	0.2%	Pass
TWR_INNER_BRACE_T6	M1066	0.047	30.89	0.02	48.02	0.2%	Pass
TWR_INNER_BRACE_T6	M1067	0.047	30.89	0.03	48.02	0.2%	Pass
TWR_INNER_BRACE_T6	M1068	0.047	30.89	0.03	48.02	0.2%	Pass
TWR_INNER_BRACE_T6	M1069	0.048	30.89	0.02	48.02	0.2%	Pass
TWR_INNER_BRACE_T6	M1070	0.047	30.89	0.03	48.02	0.2%	Pass



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TWR_INNER_BRACE_T7	M1013	0.064	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T7	M1014	0.056	30.89	0.03	48.02	0.2%	Pass
TWR_INNER_BRACE_T7	M1015	0.054	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T7	M1016	0.055	30.89	0.05	48.02	0.2%	Pass
TWR_INNER_BRACE_T7	M1017	0.062	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T7	M1018	0.058	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M961	0.074	30.89	0.05	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M962	0.063	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M963	0.06	30.89	0.05	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M964	0.061	30.89	0.05	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M965	0.07	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T8	M966	0.066	30.89	0.05	48.02	0.2%	Pass
TWR_INNER_BRACE_T9	M909	0.082	30.89	0.06	48.02	0.3%	Pass
TWR_INNER_BRACE_T9	M910	0.068	30.89	0.04	48.02	0.2%	Pass
TWR_INNER_BRACE_T9	M911	0.062	30.89	0.06	48.02	0.2%	Pass
TWR_INNER_BRACE_T9	M912	0.066	30.89	0.06	48.02	0.2%	Pass
TWR_INNER_BRACE_T9	M913	0.078	30.89	0.05	48.02	0.3%	Pass
TWR_INNER_BRACE_T9	M914	0.072	30.89	0.06	48.02	0.2%	Pass
TWR_INNER_CORNER_T3	M1206	0	15.44	4.02	48.02	8.4%	Pass
TWR_INNER_CORNER_T3	M1207	0	15.44	4.10	48.02	8.5%	Pass
TWR_INNER_CORNER_T3	M1208	0	15.44	4.06	48.02	8.5%	Pass
TWR_INNER_CORNER_T4	M1154	0	15.44	3.67	48.02	7.6%	Pass
TWR_INNER_CORNER_T4	M1155	0	15.44	3.88	48.02	8.1%	Pass
TWR_INNER_CORNER_T4	M1156	0	15.44	3.66	48.02	7.6%	Pass
TWR_INNER_CORNER_T5	M1102	0	15.44	4.39	48.02	9.1%	Pass
TWR_INNER_CORNER_T5	M1103	0	15.44	4.66	48.02	9.7%	Pass
TWR_INNER_CORNER_T5	M1104	0	15.44	4.39	48.02	9.1%	Pass
TWR_INNER_CORNER_T6	M1050	0	15.44	4.51	48.02	9.4%	Pass
TWR_INNER_CORNER_T6	M1051	0	15.44	4.74	48.02	9.9%	Pass
TWR_INNER_CORNER_T6	M1052	0	15.44	4.50	48.02	9.4%	Pass
TWR_INNER_CORNER_T7	M998	0	15.44	4.50	48.02	9.4%	Pass
TWR_INNER_CORNER_T7	M999	0	15.44	4.69	48.02	9.8%	Pass
TWR_INNER_CORNER_T7	M1000	0	15.44	4.48	48.02	9.3%	Pass
TWR_INNER_CORNER_T8	M946	0	15.44	5.04	48.02	10.5%	Pass
TWR_INNER_CORNER_T8	M947	0	15.44	5.26	48.02	10.9%	Pass
TWR_INNER_CORNER_T8	M948	0	15.44	5.01	48.02	10.4%	Pass
TWR_INNER_CORNER_T9	M894	0	15.44	5.46	48.02	11.4%	Pass
TWR_INNER_CORNER_T9	M895	0	15.44	5.73	48.02	11.9%	Pass
TWR_INNER_CORNER_T9	M896	0	15.44	5.49	48.02	11.4%	Pass
TWR_INNER_LADDER_T3	M1227	2.557	60.14	1.20	71.53	4.3%	Pass
TWR_INNER_LADDER_T3	M1228	0.893	58.32	1.90	71.53	2.7%	Pass
TWR_INNER_LADDER_T3	M1229	0.894	58.32	1.90	71.53	2.7%	Pass
TWR_INNER_LADDER_T4	M1175	1.625	58.32	1.75	71.53	2.8%	Pass
TWR_INNER_LADDER_T4	M1176	1.623	58.32	1.79	71.53	2.8%	Pass
TWR_INNER_LADDER_T4	M1177	2.387	60.14	2.19	71.53	4.0%	Pass
TWR_INNER_LADDER_T5	M1123	2.872	60.14	2.68	71.53	4.8%	Pass
TWR_INNER_LADDER_T5	M1124	1.99	58.32	2.11	71.53	3.4%	Pass
TWR_INNER_LADDER_T5	M1125	1.99	58.32	2.15	71.53	3.4%	Pass
TWR_INNER_LADDER_T6	M1071	2.033	58.32	2.14	71.53	3.5%	Pass



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TWR_INNER_LADDER_T6	M1072	2.033	58.32	2.19	71.53	3.5%	Pass
TWR_INNER_LADDER_T6	M1073	2.918	60.14	2.73	71.53	4.9%	Pass
TWR_INNER_LADDER_T7	M1019	2.884	60.14	2.70	71.53	4.8%	Pass
TWR_INNER_LADDER_T7	M1020	2.018	58.32	2.18	71.53	3.5%	Pass
TWR_INNER_LADDER_T7	M1021	2.016	58.32	2.10	71.53	3.5%	Pass
TWR_INNER_LADDER_T8	M967	3.221	60.14	3.09	71.53	5.4%	Pass
TWR_INNER_LADDER_T8	M968	2.304	58.32	2.44	71.53	4.0%	Pass
TWR_INNER_LADDER_T8	M969	2.301	58.32	2.35	71.53	3.9%	Pass
TWR_INNER_LADDER_T9	M915	3.519	60.14	3.37	71.53	5.9%	Pass
TWR_INNER_LADDER_T9	M916	2.516	58.32	2.67	71.53	4.3%	Pass
TWR_INNER_LADDER_T9	M917	2.51	58.32	2.56	71.53	4.3%	Pass
TWR_INNER_SQ_T3	M1202	1.505	7.72	3.21	48.02	19.5%	Pass
TWR_INNER_SQ_T3	M1203	1.442	7.72	3.12	48.02	18.7%	Pass
TWR_INNER_SQ_T3	M1204	1.341	7.72	3.50	48.02	17.4%	Pass
TWR_INNER_SQ_T3	M1205	1.311	7.72	3.34	48.02	17.0%	Pass
TWR_INNER_SQ_T4	M1150	1.236	7.72	3.16	48.02	16.0%	Pass
TWR_INNER_SQ_T4	M1151	1.312	7.72	3.40	48.02	17.0%	Pass
TWR_INNER_SQ_T4	M1152	2.124	7.72	2.86	48.02	27.5%	Pass
TWR_INNER_SQ_T4	M1153	2.171	7.72	3.08	48.02	28.1%	Pass
TWR_INNER_SQ_T5	M1098	2.625	7.72	3.74	48.02	34.0%	Pass
TWR_INNER_SQ_T5	M1099	1.426	7.72	3.77	48.02	18.5%	Pass
TWR_INNER_SQ_T5	M1100	1.537	7.72	4.12	48.02	19.9%	Pass
TWR_INNER_SQ_T5	M1101	2.568	7.72	3.42	48.02	33.3%	Pass
TWR_INNER_SQ_T6	M1046	1.449	7.72	3.85	48.02	18.8%	Pass
TWR_INNER_SQ_T6	M1047	1.566	7.72	4.21	48.02	20.3%	Pass
TWR_INNER_SQ_T6	M1048	2.639	7.72	3.47	48.02	34.2%	Pass
TWR_INNER_SQ_T6	M1049	2.67	7.72	3.81	48.02	34.6%	Pass
TWR_INNER_SQ_T7	M994	2.643	7.72	3.78	48.02	34.2%	Pass
TWR_INNER_SQ_T7	M995	1.437	7.72	3.81	48.02	18.6%	Pass
TWR_INNER_SQ_T7	M996	1.557	7.72	4.17	48.02	20.2%	Pass
TWR_INNER_SQ_T7	M997	2.633	7.72	3.43	48.02	34.1%	Pass
TWR_INNER_SQ_T8	M942	1.582	7.72	4.28	48.02	20.5%	Pass
TWR_INNER_SQ_T8	M943	1.714	7.72	4.68	48.02	22.2%	Pass
TWR_INNER_SQ_T8	M944	2.996	7.72	3.85	48.02	38.8%	Pass
TWR_INNER_SQ_T8	M945	2.985	7.72	4.24	48.02	38.7%	Pass
TWR_INNER_SQ_T9	M890	3.243	7.72	4.19	48.02	42.0%	Pass
TWR_INNER_SQ_T9	M891	1.852	7.72	5.11	48.02	24.0%	Pass
TWR_INNER_SQ_T9	M892	1.697	7.72	4.64	48.02	22.0%	Pass
TWR_INNER_SQ_T9	M893	3.244	7.72	4.64	48.02	42.0%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_INNER_SUPP_T3	M191	1.79	33.30	1.64	71.53	5.4%	Pass
TWR_INNER_SUPP_T3	M192	1.716	33.30	1.80	71.53	5.2%	Pass
TWR_INNER_SUPP_T3	M193	1.631	33.30	1.81	71.53	4.9%	Pass
TWR_INNER_SUPP_T3	M194	1.799	33.30	1.72	71.53	5.4%	Pass
TWR_INNER_SUPP_T3	M195	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M196	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M197	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M198	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T3	M199	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M272	1.859	33.30	1.58	71.53	5.6%	Pass
TWR_INNER_SUPP_T4	M273	1.731	33.30	1.88	71.53	5.2%	Pass
TWR_INNER_SUPP_T4	M274	1.579	33.30	1.88	71.53	4.7%	Pass
TWR_INNER_SUPP_T4	M275	1.853	33.30	1.75	71.53	5.6%	Pass
TWR_INNER_SUPP_T4	M276	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M277	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M278	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M279	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T4	M280	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M353	2.242	33.30	1.91	71.53	6.7%	Pass
TWR_INNER_SUPP_T5	M354	2.045	33.30	2.27	71.53	6.1%	Pass
TWR_INNER_SUPP_T5	M355	1.888	33.30	2.26	71.53	5.7%	Pass
TWR_INNER_SUPP_T5	M356	2.232	33.30	2.08	71.53	6.7%	Pass
TWR_INNER_SUPP_T5	M357	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M358	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M359	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M360	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T5	M361	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M434	2.275	33.30	1.94	71.53	6.8%	Pass
TWR_INNER_SUPP_T6	M435	2.073	33.30	2.31	71.53	6.2%	Pass
TWR_INNER_SUPP_T6	M436	1.919	33.30	2.31	71.53	5.8%	Pass
TWR_INNER_SUPP_T6	M437	2.269	33.30	2.12	71.53	6.8%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_INNER_SUPP_T6	M438	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M439	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M440	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M441	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T6	M442	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M515	2.252	33.30	1.92	71.53	6.8%	Pass
TWR_INNER_SUPP_T7	M516	2.076	33.30	2.29	71.53	6.2%	Pass
TWR_INNER_SUPP_T7	M517	1.919	33.30	2.30	71.53	5.8%	Pass
TWR_INNER_SUPP_T7	M518	2.257	33.30	2.10	71.53	6.8%	Pass
TWR_INNER_SUPP_T7	M519	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M520	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M521	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M522	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T7	M523	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M596	2.517	33.30	2.15	71.53	7.6%	Pass
TWR_INNER_SUPP_T8	M597	2.372	33.30	2.57	71.53	7.1%	Pass
TWR_INNER_SUPP_T8	M598	2.136	33.30	2.58	71.53	6.4%	Pass
TWR_INNER_SUPP_T8	M599	2.522	33.30	2.36	71.53	7.6%	Pass
TWR_INNER_SUPP_T8	M600	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M601	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M602	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M603	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T8	M604	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M677	2.735	33.30	2.37	71.53	8.2%	Pass
TWR_INNER_SUPP_T9	M678	2.54	33.30	2.79	71.53	7.6%	Pass
TWR_INNER_SUPP_T9	M679	2.274	33.30	2.79	71.53	6.8%	Pass
TWR_INNER_SUPP_T9	M680	2.724	33.30	2.56	71.53	8.2%	Pass
TWR_INNER_SUPP_T9	M681	0	4.16	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M682	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M683	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M684	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_SUPP_T9	M685	0	33.30	0.00	71.53	0.0%	Pass
TWR_INNER_TRI_T3	M1209	0.01	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1210	0.009	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1211	0.009	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1212	0.01	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T3	M1213	0.008	47.81	0.00	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1214	0.006	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1215	0.008	47.81	0.00	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1216	0.006	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1217	0.007	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1218	0.008	47.81	0.00	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1219	0.008	47.81	0.00	48.02	0.0%	Pass
TWR_INNER_TRI_T3	M1220	0.006	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1157	0.017	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1158	0.008	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1159	0.009	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1160	0.017	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T4	M1161	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1162	0.008	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1163	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1164	0.008	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1165	0.008	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1166	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1167	0.011	47.81	0.00	48.02	0.0%	Pass
TWR_INNER_TRI_T4	M1168	0.008	47.81	0.01	48.02	0.0%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_INNER_TRI_T5	M1105	0.021	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1106	0.02	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1107	0.01	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1108	0.009	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T5	M1109	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1110	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1111	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1112	0.009	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1113	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1114	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1115	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T5	M1116	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1053	0.021	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1054	0.01	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1055	0.01	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1056	0.021	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T6	M1057	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1058	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1059	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1060	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1061	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1062	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1063	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T6	M1064	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1001	0.021	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1002	0.009	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1003	0.01	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1004	0.021	30.89	0.03	48.02	0.1%	Pass
TWR_INNER_TRI_T7	M1005	0.012	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1006	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1007	0.012	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1008	0.01	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1009	0.009	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1010	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1011	0.013	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T7	M1012	0.009	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M949	0.024	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M950	0.01	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M951	0.011	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M952	0.024	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T8	M953	0.014	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M954	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M955	0.014	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M956	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M957	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M958	0.014	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M959	0.014	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T8	M960	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M897	0.026	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M898	0.011	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M899	0.012	30.89	0.05	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M900	0.026	30.89	0.04	48.02	0.1%	Pass
TWR_INNER_TRI_T9	M901	0.016	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M902	0.012	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M903	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M904	0.016	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M905	0.015	47.81	0.01	48.02	0.0%	Pass



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TWR_INNER_TRI_T9	M906	0.011	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M907	0.012	47.81	0.01	48.02	0.0%	Pass
TWR_INNER_TRI_T9	M908	0.015	47.81	0.01	48.02	0.0%	Pass
TWR_LEG_OUTER_T1	M1266	2.7	14.89	0.00	63.37	18.1%	Pass
TWR_LEG_OUTER_T1	M1267	2.709	14.89	0.00	63.37	18.2%	Pass
TWR_LEG_OUTER_T1	M1268	2.685	14.89	0.00	63.37	18.0%	Pass
TWR_LEG_OUTER_T1	M1269	2.686	14.89	0.00	63.37	18.0%	Pass
TWR_LEG_T1	M1	12.119	84.54	2.35	173.32	14.3%	Pass
TWR_LEG_T1	M2	15.196	84.54	1.53	173.32	18.0%	Pass
TWR_LEG_T1	M3	14.874	84.54	1.56	173.32	17.6%	Pass
TWR_LEG_T1	M4	11.902	84.54	2.38	173.32	14.1%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_REDHIPDIA_2_T9	M882	0.585	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M883	0.584	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M884	0.588	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M885	0.584	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M886	0.583	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M887	0.587	14.70	0.00	48.02	4.0%	Pass
TWR_REDHIPDIA_2_T9	M888	0.575	14.70	0.00	48.02	3.9%	Pass
TWR_REDHIPDIA_2_T9	M889	0.574	14.70	0.00	48.02	3.9%	Pass
TWR_RED_DIAG_0_T10	M791	8.309	22.51	6.33	59.46	36.9%	Pass
TWR_RED_DIAG_0_T10	M792	11.14	22.89	8.09	59.46	48.7%	Pass
TWR_RED_DIAG_0_T10	M793	8.128	22.51	6.29	59.46	36.1%	Pass
TWR_RED_DIAG_0_T10	M794	11.332	22.89	8.53	59.46	49.5%	Pass
TWR_RED_DIAG_0_T10	M795	10.998	22.89	8.50	59.46	48.0%	Pass
TWR_RED_DIAG_0_T10	M796	8.03	22.51	6.41	59.46	35.7%	Pass
TWR_RED_DIAG_0_T10	M797	8.327	22.51	6.58	59.46	37.0%	Pass
TWR_RED_DIAG_0_T10	M798	10.967	22.89	8.21	59.46	47.9%	Pass
TWR_RED_DIAG_2_T2	M56	0.587	21.11	0.89	48.02	2.8%	Pass
TWR_RED_DIAG_2_T2	M64	0.595	21.11	0.90	48.02	2.8%	Pass
TWR_RED_DIAG_2_T2	M72	0.886	21.11	1.22	48.02	4.2%	Pass
TWR_RED_DIAG_2_T2	M80	0.884	21.11	1.22	48.02	4.2%	Pass
TWR_RED_DIAG_2_T2	M88	0.696	21.11	1.00	48.02	3.3%	Pass
TWR_RED_DIAG_2_T2	M96	0.691	21.11	1.00	48.02	3.3%	Pass
TWR_RED_DIAG_2_T2	M104	0.617	21.11	0.96	48.02	2.9%	Pass
TWR_RED_DIAG_2_T2	M112	0.619	21.11	0.96	48.02	2.9%	Pass
TWR_RED_DIAG_2_T3	M129	0.282	21.11	0.53	48.02	1.3%	Pass
TWR_RED_DIAG_2_T3	M137	0.275	21.11	0.53	48.02	1.3%	Pass
TWR_RED_DIAG_2_T3	M146	0.211	21.11	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T3	M154	0.216	21.11	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T3	M163	0.103	21.11	0.35	48.02	0.7%	Pass
TWR_RED_DIAG_2_T3	M171	0.105	21.11	0.38	48.02	0.8%	Pass
TWR_RED_DIAG_2_T3	M180	0.231	21.11	0.56	48.02	1.2%	Pass
TWR_RED_DIAG_2_T3	M188	0.222	21.11	0.55	48.02	1.1%	Pass
TWR_RED_DIAG_2_T4	M210	0.198	21.15	0.48	48.02	1.0%	Pass
TWR_RED_DIAG_2_T4	M218	0.158	21.15	0.44	48.02	0.9%	Pass
TWR_RED_DIAG_2_T4	M227	0.209	21.15	0.58	48.02	1.2%	Pass
TWR_RED_DIAG_2_T4	M235	0.213	21.15	0.57	48.02	1.2%	Pass
TWR_RED_DIAG_2_T4	M244	0.073	21.15	0.33	48.02	0.7%	Pass
TWR_RED_DIAG_2_T4	M252	0.083	21.15	0.37	48.02	0.8%	Pass
TWR_RED_DIAG_2_T4	M261	0.143	21.15	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T4	M269	0.144	21.15	0.51	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M291	0.296	21.54	0.45	48.02	1.4%	Pass
TWR_RED_DIAG_2_T5	M299	0.317	21.54	0.48	48.02	1.5%	Pass
TWR_RED_DIAG_2_T5	M308	0.114	21.54	0.46	48.02	1.0%	Pass
TWR_RED_DIAG_2_T5	M316	0.149	21.54	0.53	48.02	1.1%	Pass
TWR_RED_DIAG_2_T5	M325	0.301	21.54	0.45	48.02	1.4%	Pass
TWR_RED_DIAG_2_T5	M333	0.25	21.54	0.41	48.02	1.2%	Pass
TWR_RED_DIAG_2_T5	M342	0.171	21.54	0.56	48.02	1.2%	Pass
TWR_RED_DIAG_2_T5	M350	0.147	21.54	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T6	M372	0.472	21.58	0.55	48.02	2.2%	Pass
TWR_RED_DIAG_2_T6	M380	0.525	21.58	0.59	48.02	2.4%	Pass
TWR_RED_DIAG_2_T6	M389	0.038	21.58	0.39	48.02	0.8%	Pass
TWR_RED_DIAG_2_T6	M397	0.118	21.58	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T6	M406	0.537	21.58	0.60	48.02	2.5%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_DIAG_2_T6	M414	0.47	21.58	0.56	48.02	2.2%	Pass
TWR_RED_DIAG_2_T6	M423	0.133	21.58	0.52	48.02	1.1%	Pass
TWR_RED_DIAG_2_T6	M431	0.073	21.58	0.42	48.02	0.9%	Pass
TWR_RED_DIAG_2_T7	M453	1.104	21.97	0.93	48.02	5.0%	Pass
TWR_RED_DIAG_2_T7	M461	1.193	21.97	1.00	48.02	5.4%	Pass
TWR_RED_DIAG_2_T7	M470	0.11	21.97	0.42	48.02	0.9%	Pass
TWR_RED_DIAG_2_T7	M478	0.173	21.97	0.47	48.02	1.0%	Pass
TWR_RED_DIAG_2_T7	M487	1.166	21.97	1.01	48.02	5.3%	Pass
TWR_RED_DIAG_2_T7	M495	1.08	21.97	0.94	48.02	4.9%	Pass
TWR_RED_DIAG_2_T7	M504	0.172	21.97	0.49	48.02	1.0%	Pass
TWR_RED_DIAG_2_T7	M512	0.119	21.97	0.44	48.02	0.9%	Pass
TWR_RED_DIAG_2_T8	M534	1.437	22.02	1.28	48.02	6.5%	Pass
TWR_RED_DIAG_2_T8	M542	1.516	22.02	1.34	48.02	6.9%	Pass
TWR_RED_DIAG_2_T8	M551	0.161	22.02	0.61	48.02	1.3%	Pass
TWR_RED_DIAG_2_T8	M559	0.23	22.02	0.68	48.02	1.4%	Pass
TWR_RED_DIAG_2_T8	M568	1.516	22.02	1.36	48.02	6.9%	Pass
TWR_RED_DIAG_2_T8	M576	1.413	22.02	1.30	48.02	6.4%	Pass
TWR_RED_DIAG_2_T8	M585	0.247	22.02	0.71	48.02	1.5%	Pass
TWR_RED_DIAG_2_T8	M593	0.172	22.02	0.65	48.02	1.3%	Pass
TWR_RED_DIAG_2_T9	M615	2.117	22.06	1.68	48.02	9.6%	Pass
TWR_RED_DIAG_2_T9	M623	2.18	22.06	1.75	48.02	9.9%	Pass
TWR_RED_DIAG_2_T9	M632	0.509	22.06	0.73	48.02	2.3%	Pass
TWR_RED_DIAG_2_T9	M640	0.557	22.06	0.76	48.02	2.5%	Pass
TWR_RED_DIAG_2_T9	M649	2.198	22.06	1.77	48.02	10.0%	Pass
TWR_RED_DIAG_2_T9	M657	2.098	22.06	1.70	48.02	9.5%	Pass
TWR_RED_DIAG_2_T9	M666	0.557	22.06	0.77	48.02	2.5%	Pass
TWR_RED_DIAG_2_T9	M674	0.528	22.06	0.75	48.02	2.4%	Pass
TWR_RED_DIAG_2_T10	M696	0.462	31.45	1.44	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M706	0.464	31.45	1.43	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M717	0.359	30.71	1.18	63.37	1.9%	Pass
TWR_RED_DIAG_2_T10	M727	0.361	30.71	1.25	63.37	2.0%	Pass
TWR_RED_DIAG_2_T10	M738	0.435	31.45	1.44	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M748	0.425	31.45	1.43	63.37	2.3%	Pass
TWR_RED_DIAG_2_T10	M759	0.359	30.71	1.28	63.37	2.0%	Pass
TWR_RED_DIAG_2_T10	M769	0.358	30.71	1.22	63.37	1.9%	Pass
TWR_RED_DIAG_3_T2	M57	1.867	21.11	0.00	48.02	8.8%	Pass
TWR_RED_DIAG_3_T2	M58	1.177	39.66	0.11	48.02	3.0%	Pass
TWR_RED_DIAG_3_T2	M65	1.924	21.11	0.00	48.02	9.1%	Pass
TWR_RED_DIAG_3_T2	M66	1.176	39.66	0.08	48.02	3.0%	Pass
TWR_RED_DIAG_3_T2	M73	2.041	21.11	0.00	48.02	9.7%	Pass
TWR_RED_DIAG_3_T2	M74	1.305	39.66	0.22	48.02	3.3%	Pass
TWR_RED_DIAG_3_T2	M81	2.017	21.11	0.00	48.02	9.6%	Pass
TWR_RED_DIAG_3_T2	M82	1.323	39.66	0.23	48.02	3.3%	Pass
TWR_RED_DIAG_3_T2	M89	1.894	21.11	0.00	48.02	9.0%	Pass
TWR_RED_DIAG_3_T2	M90	1.181	39.66	0.10	48.02	3.0%	Pass
TWR_RED_DIAG_3_T2	M97	1.855	21.11	0.00	48.02	8.8%	Pass
TWR_RED_DIAG_3_T2	M98	1.175	39.66	0.09	48.02	3.0%	Pass
TWR_RED_DIAG_3_T2	M105	1.934	21.11	0.00	48.02	9.2%	Pass
TWR_RED_DIAG_3_T2	M106	1.138	39.66	0.08	48.02	2.9%	Pass
TWR_RED_DIAG_3_T2	M113	1.939	21.11	0.00	48.02	9.2%	Pass
TWR_RED_DIAG_3_T2	M114	1.117	39.66	0.09	48.02	2.8%	Pass
TWR_RED_DIAG_3_T3	M130	0.75	21.11	0.29	48.02	3.6%	Pass
TWR_RED_DIAG_3_T3	M131	0.411	39.66	0.32	48.02	1.0%	Pass
TWR_RED_DIAG_3_T3	M138	0.769	21.11	0.29	48.02	3.6%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_DIAG_3_T3	M139	0.459	39.66	0.29	48.02	1.2%	Pass
TWR_RED_DIAG_3_T3	M147	0.806	21.11	0.19	48.02	3.8%	Pass
TWR_RED_DIAG_3_T3	M148	0.382	39.66	0.31	48.02	1.0%	Pass
TWR_RED_DIAG_3_T3	M155	0.776	21.11	0.21	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M156	0.349	39.66	0.34	48.02	0.9%	Pass
TWR_RED_DIAG_3_T3	M164	0.622	21.11	0.15	48.02	2.9%	Pass
TWR_RED_DIAG_3_T3	M165	0.315	39.66	0.22	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M172	0.639	21.11	0.14	48.02	3.0%	Pass
TWR_RED_DIAG_3_T3	M173	0.304	39.66	0.22	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M181	0.784	21.11	0.19	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M182	0.334	39.66	0.34	48.02	0.8%	Pass
TWR_RED_DIAG_3_T3	M189	0.777	21.11	0.19	48.02	3.7%	Pass
TWR_RED_DIAG_3_T3	M190	0.336	39.66	0.34	48.02	0.8%	Pass
TWR_RED_DIAG_3_T4	M211	0.576	21.15	0.17	48.02	2.7%	Pass
TWR_RED_DIAG_3_T4	M212	0.34	39.73	0.20	48.02	0.9%	Pass
TWR_RED_DIAG_3_T4	M219	0.559	21.15	0.16	48.02	2.6%	Pass
TWR_RED_DIAG_3_T4	M220	0.383	39.73	0.15	48.02	1.0%	Pass
TWR_RED_DIAG_3_T4	M228	0.721	21.15	0.04	48.02	3.4%	Pass
TWR_RED_DIAG_3_T4	M229	0.269	39.73	0.17	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M236	0.712	21.15	0.09	48.02	3.4%	Pass
TWR_RED_DIAG_3_T4	M237	0.265	39.73	0.25	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M245	0.47	21.15	0.03	48.02	2.2%	Pass
TWR_RED_DIAG_3_T4	M246	0.296	39.73	0.10	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M253	0.522	21.15	0.04	48.02	2.5%	Pass
TWR_RED_DIAG_3_T4	M254	0.282	39.73	0.13	48.02	0.7%	Pass
TWR_RED_DIAG_3_T4	M262	0.715	21.15	0.05	48.02	3.4%	Pass
TWR_RED_DIAG_3_T4	M263	0.233	39.73	0.24	48.02	0.6%	Pass
TWR_RED_DIAG_3_T4	M270	0.689	21.15	0.00	48.02	3.3%	Pass
TWR_RED_DIAG_3_T4	M271	0.19	39.73	0.17	48.02	0.5%	Pass
TWR_RED_DIAG_3_T5	M292	0.756	21.54	0.44	48.02	3.5%	Pass
TWR_RED_DIAG_3_T5	M293	0.563	40.35	0.36	48.02	1.4%	Pass
TWR_RED_DIAG_3_T5	M300	0.777	21.54	0.51	48.02	3.6%	Pass
TWR_RED_DIAG_3_T5	M301	0.66	40.35	0.33	48.02	1.6%	Pass
TWR_RED_DIAG_3_T5	M309	0.623	21.54	0.11	48.02	2.9%	Pass
TWR_RED_DIAG_3_T5	M310	0.342	40.35	0.19	48.02	0.8%	Pass
TWR_RED_DIAG_3_T5	M317	0.729	21.54	0.22	48.02	3.4%	Pass
TWR_RED_DIAG_3_T5	M318	0.378	40.35	0.31	48.02	0.9%	Pass
TWR_RED_DIAG_3_T5	M326	0.661	21.54	0.36	48.02	3.1%	Pass
TWR_RED_DIAG_3_T5	M327	0.504	40.35	0.29	48.02	1.2%	Pass
TWR_RED_DIAG_3_T5	M334	0.647	21.54	0.31	48.02	3.0%	Pass
TWR_RED_DIAG_3_T5	M335	0.461	40.35	0.28	48.02	1.1%	Pass
TWR_RED_DIAG_3_T5	M343	0.764	21.54	0.23	48.02	3.5%	Pass
TWR_RED_DIAG_3_T5	M344	0.379	40.35	0.34	48.02	0.9%	Pass
TWR_RED_DIAG_3_T5	M351	0.637	21.54	0.13	48.02	3.0%	Pass
TWR_RED_DIAG_3_T5	M352	0.31	40.35	0.25	48.02	0.8%	Pass
TWR_RED_DIAG_3_T6	M373	0.8	21.58	0.62	48.02	3.7%	Pass
TWR_RED_DIAG_3_T6	M374	0.732	40.42	0.40	48.02	1.8%	Pass
TWR_RED_DIAG_3_T6	M381	0.856	21.58	0.71	48.02	4.0%	Pass
TWR_RED_DIAG_3_T6	M382	0.852	40.42	0.40	48.02	2.1%	Pass
TWR_RED_DIAG_3_T6	M390	0.619	21.58	0.15	48.02	2.9%	Pass
TWR_RED_DIAG_3_T6	M391	0.424	40.42	0.19	48.02	1.0%	Pass
TWR_RED_DIAG_3_T6	M398	0.704	21.58	0.26	48.02	3.3%	Pass
TWR_RED_DIAG_3_T6	M399	0.455	40.42	0.29	48.02	1.1%	Pass
TWR_RED_DIAG_3_T6	M407	0.847	21.58	0.69	48.02	3.9%	Pass
TWR_RED_DIAG_3_T6	M408	0.781	40.42	0.44	48.02	1.9%	Pass
TWR_RED_DIAG_3_T6	M415	0.817	21.58	0.59	48.02	3.8%	Pass
TWR_RED_DIAG_3_T6	M416	0.709	40.42	0.41	48.02	1.8%	Pass
TWR_RED_DIAG_3_T6	M424	0.744	21.58	0.26	48.02	3.4%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_DIAG_3_T6	M425	0.452	40.42	0.32	48.02	1.1%	Pass
TWR_RED_DIAG_3_T6	M432	0.638	21.58	0.16	48.02	3.0%	Pass
TWR_RED_DIAG_3_T6	M433	0.383	40.42	0.24	48.02	0.9%	Pass
TWR_RED_DIAG_3_T7	M454	1.1	21.97	0.99	48.02	5.0%	Pass
TWR_RED_DIAG_3_T7	M455	1.028	41.04	0.61	48.02	2.5%	Pass
TWR_RED_DIAG_3_T7	M462	1.166	21.97	1.12	48.02	5.3%	Pass
TWR_RED_DIAG_3_T7	M463	1.173	41.04	0.62	48.02	2.9%	Pass
TWR_RED_DIAG_3_T7	M471	0.791	21.97	0.41	48.02	3.6%	Pass
TWR_RED_DIAG_3_T7	M472	0.632	41.04	0.31	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M479	0.818	21.97	0.45	48.02	3.7%	Pass
TWR_RED_DIAG_3_T7	M480	0.616	41.04	0.37	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M488	1.161	21.97	1.07	48.02	5.3%	Pass
TWR_RED_DIAG_3_T7	M489	1.092	41.04	0.66	48.02	2.7%	Pass
TWR_RED_DIAG_3_T7	M496	1.12	21.97	0.95	48.02	5.1%	Pass
TWR_RED_DIAG_3_T7	M497	1.002	41.04	0.62	48.02	2.4%	Pass
TWR_RED_DIAG_3_T7	M505	0.853	21.97	0.43	48.02	3.9%	Pass
TWR_RED_DIAG_3_T7	M506	0.617	41.04	0.39	48.02	1.5%	Pass
TWR_RED_DIAG_3_T7	M513	0.79	21.97	0.39	48.02	3.6%	Pass
TWR_RED_DIAG_3_T7	M514	0.571	41.04	0.35	48.02	1.4%	Pass
TWR_RED_DIAG_3_T8	M535	1.497	22.02	1.41	48.02	6.8%	Pass
TWR_RED_DIAG_3_T8	M536	1.336	41.11	0.91	48.02	3.3%	Pass
TWR_RED_DIAG_3_T8	M543	1.55	22.02	1.54	48.02	7.0%	Pass
TWR_RED_DIAG_3_T8	M544	1.484	41.11	0.91	48.02	3.6%	Pass
TWR_RED_DIAG_3_T8	M552	1.045	22.02	0.67	48.02	4.7%	Pass
TWR_RED_DIAG_3_T8	M553	0.833	41.11	0.51	48.02	2.0%	Pass
TWR_RED_DIAG_3_T8	M560	1.057	22.02	0.68	48.02	4.8%	Pass
TWR_RED_DIAG_3_T8	M561	0.792	41.11	0.56	48.02	1.9%	Pass
TWR_RED_DIAG_3_T8	M569	1.554	22.02	1.47	48.02	7.1%	Pass
TWR_RED_DIAG_3_T8	M570	1.386	41.11	0.95	48.02	3.4%	Pass
TWR_RED_DIAG_3_T8	M577	1.523	22.02	1.36	48.02	6.9%	Pass
TWR_RED_DIAG_3_T8	M578	1.3	41.11	0.92	48.02	3.2%	Pass
TWR_RED_DIAG_3_T8	M586	1.086	22.02	0.65	48.02	4.9%	Pass
TWR_RED_DIAG_3_T8	M587	0.763	41.11	0.58	48.02	1.9%	Pass
TWR_RED_DIAG_3_T8	M594	1.047	22.02	0.64	48.02	4.8%	Pass
TWR_RED_DIAG_3_T8	M595	0.758	41.11	0.55	48.02	1.8%	Pass
TWR_RED_DIAG_3_T9	M616	1.912	22.06	2.03	48.02	8.7%	Pass
TWR_RED_DIAG_3_T9	M617	1.787	41.17	1.21	48.02	4.3%	Pass
TWR_RED_DIAG_3_T9	M624	1.967	22.06	2.16	48.02	8.9%	Pass
TWR_RED_DIAG_3_T9	M625	1.936	41.17	1.21	48.02	4.7%	Pass
TWR_RED_DIAG_3_T9	M633	1.281	22.06	1.06	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M634	1.133	41.17	0.70	48.02	2.8%	Pass
TWR_RED_DIAG_3_T9	M641	1.287	22.06	1.05	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M642	1.083	41.17	0.75	48.02	2.6%	Pass
TWR_RED_DIAG_3_T9	M650	1.979	22.06	2.08	48.02	9.0%	Pass
TWR_RED_DIAG_3_T9	M651	1.829	41.17	1.26	48.02	4.4%	Pass



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TWR_RED_DIAG_3_T9	M658	1.94	22.06	1.96	48.02	8.8%	Pass
TWR_RED_DIAG_3_T9	M659	1.741	41.17	1.23	48.02	4.2%	Pass
TWR_RED_DIAG_3_T9	M667	1.319	22.06	1.02	48.02	6.0%	Pass
TWR_RED_DIAG_3_T9	M668	1.049	41.17	0.76	48.02	2.5%	Pass
TWR_RED_DIAG_3_T9	M675	1.288	22.06	1.02	48.02	5.8%	Pass
TWR_RED_DIAG_3_T9	M676	1.055	41.17	0.75	48.02	2.6%	Pass
TWR_RED_DIAG_3_T10	M698	0.583	19.80	1.58	63.37	2.9%	Pass
TWR_RED_DIAG_3_T10	M708	0.599	19.80	1.56	63.37	3.0%	Pass
TWR_RED_DIAG_3_T10	M719	0.539	19.40	1.25	63.37	2.8%	Pass
TWR_RED_DIAG_3_T10	M729	0.538	19.40	1.34	63.37	2.8%	Pass
TWR_RED_DIAG_3_T10	M740	0.544	19.80	1.56	63.37	2.7%	Pass
TWR_RED_DIAG_3_T10	M750	0.53	19.80	1.55	63.37	2.7%	Pass
TWR_RED_DIAG_3_T10	M761	0.533	18.63	1.36	63.37	2.9%	Pass
TWR_RED_DIAG_3_T10	M771	0.534	19.40	1.28	63.37	2.8%	Pass
TWR_RED_DIAG_4_T10	M699	2.084	28.05	1.47	63.37	7.4%	Pass
TWR_RED_DIAG_4_T10	M700	1.719	48.66	1.27	63.37	3.5%	Pass
TWR_RED_DIAG_4_T10	M709	2.108	28.05	1.55	63.37	7.5%	Pass
TWR_RED_DIAG_4_T10	M710	1.776	48.66	1.30	63.37	3.6%	Pass
TWR_RED_DIAG_4_T10	M720	1.625	28.68	0.89	63.37	5.7%	Pass
TWR_RED_DIAG_4_T10	M721	1.266	47.73	0.92	63.37	2.7%	Pass
TWR_RED_DIAG_4_T10	M730	1.658	28.68	0.89	63.37	5.8%	Pass
TWR_RED_DIAG_4_T10	M731	1.268	47.73	0.94	63.37	2.7%	Pass
TWR_RED_DIAG_4_T10	M741	2.143	28.05	1.52	63.37	7.6%	Pass
TWR_RED_DIAG_4_T10	M742	1.756	48.66	1.31	63.37	3.6%	Pass
TWR_RED_DIAG_4_T10	M751	2.105	28.05	1.46	63.37	7.5%	Pass
TWR_RED_DIAG_4_T10	M752	1.705	48.66	1.28	63.37	3.5%	Pass
TWR_RED_DIAG_4_T10	M762	1.683	28.68	0.88	63.37	5.9%	Pass
TWR_RED_DIAG_4_T10	M763	1.248	47.73	0.95	63.37	2.6%	Pass
TWR_RED_DIAG_4_T10	M772	1.668	28.68	0.86	63.37	5.8%	Pass
TWR_RED_DIAG_4_T10	M773	1.243	47.73	0.95	63.37	2.6%	Pass
TWR_RED_DIAG_T1	M17	0.973	5.33	0.64	24.08	18.3%	Pass
TWR_RED_DIAG_T1	M20	1.035	5.33	0.59	24.08	19.4%	Pass
TWR_RED_DIAG_T1	M24	1.165	5.33	0.74	24.08	21.9%	Pass
TWR_RED_DIAG_T1	M27	1.118	5.33	0.77	24.08	21.0%	Pass
TWR_RED_DIAG_T1	M31	0.997	5.33	0.61	24.08	18.7%	Pass
TWR_RED_DIAG_T1	M34	0.996	5.33	0.61	24.08	18.7%	Pass
TWR_RED_DIAG_T1	M38	0.919	5.33	0.50	24.08	17.2%	Pass
TWR_RED_DIAG_T1	M41	0.888	5.33	0.53	24.08	16.7%	Pass
TWR_RED_DIAG_T2	M54	0.161	14.93	0.02	30.21	1.1%	Pass
TWR_RED_DIAG_T2	M62	0.221	14.93	0.02	30.21	1.5%	Pass
TWR_RED_DIAG_T2	M70	0.025	14.93	0.13	30.21	0.4%	Pass
TWR_RED_DIAG_T2	M78	0.055	14.93	0.14	30.21	0.5%	Pass
TWR_RED_DIAG_T2	M86	0.216	14.93	0.07	30.21	1.4%	Pass
TWR_RED_DIAG_T2	M94	0.189	14.93	0.09	30.21	1.3%	Pass
TWR_RED_DIAG_T2	M102	0.048	14.93	0.17	30.21	0.6%	Pass
TWR_RED_DIAG_T2	M110	0.021	14.93	0.16	30.21	0.5%	Pass
TWR_RED_DIAG_T3	M127	0.639	14.93	0.08	30.21	4.3%	Pass
TWR_RED_DIAG_T3	M135	0.754	14.93	0.11	30.21	5.1%	Pass
TWR_RED_DIAG_T3	M144	0.339	14.93	0.19	30.21	2.3%	Pass
TWR_RED_DIAG_T3	M152	0.387	14.93	0.25	30.21	2.6%	Pass
TWR_RED_DIAG_T3	M161	0.661	14.93	0.09	30.21	4.4%	Pass
TWR_RED_DIAG_T3	M169	0.583	14.93	0.12	30.21	3.9%	Pass
TWR_RED_DIAG_T3	M178	0.384	14.93	0.30	30.21	2.6%	Pass
TWR_RED_DIAG_T3	M186	0.318	14.93	0.20	30.21	2.1%	Pass
TWR_RED_DIAG_T4	M208	1.079	14.97	0.41	30.21	7.2%	Pass



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TAG0053 - CHESHIRE

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_DIAG_T4	M216	1.227	14.97	0.43	30.21	8.2%	Pass
TWR_RED_DIAG_T4	M225	0.437	14.97	0.22	30.21	2.9%	Pass
TWR_RED_DIAG_T4	M233	0.499	14.97	0.32	30.21	3.3%	Pass
TWR_RED_DIAG_T4	M242	1.185	14.97	0.46	30.21	7.9%	Pass
TWR_RED_DIAG_T4	M250	1.038	14.97	0.42	30.21	6.9%	Pass
TWR_RED_DIAG_T4	M259	0.501	14.97	0.38	30.21	3.3%	Pass
TWR_RED_DIAG_T4	M267	0.436	14.97	0.30	30.21	2.9%	Pass
TWR_RED_DIAG_T5	M289	1.956	15.54	0.95	30.21	12.6%	Pass
TWR_RED_DIAG_T5	M297	2.121	15.54	0.96	30.21	13.7%	Pass
TWR_RED_DIAG_T5	M306	1.055	15.54	0.62	30.21	6.8%	Pass
TWR_RED_DIAG_T5	M314	1.071	15.54	0.69	30.21	6.9%	Pass
TWR_RED_DIAG_T5	M323	2.068	15.54	1.00	30.21	13.3%	Pass
TWR_RED_DIAG_T5	M331	1.897	15.54	0.97	30.21	12.2%	Pass
TWR_RED_DIAG_T5	M340	1.05	15.54	0.75	30.21	6.8%	Pass
TWR_RED_DIAG_T5	M348	1.035	15.54	0.71	30.21	6.7%	Pass
TWR_RED_DIAG_T6	M370	2.762	15.58	1.54	30.21	17.7%	Pass
TWR_RED_DIAG_T6	M378	2.977	15.58	1.57	30.21	19.1%	Pass
TWR_RED_DIAG_T6	M387	1.534	15.58	0.85	30.21	9.8%	Pass
TWR_RED_DIAG_T6	M395	1.507	15.58	0.88	30.21	9.7%	Pass
TWR_RED_DIAG_T6	M404	2.925	15.58	1.62	30.21	18.8%	Pass
TWR_RED_DIAG_T6	M412	2.703	15.58	1.56	30.21	17.3%	Pass
TWR_RED_DIAG_T6	M421	1.44	15.58	0.92	30.21	9.2%	Pass
TWR_RED_DIAG_T6	M429	1.471	15.58	0.91	30.21	9.4%	Pass
TWR_RED_DIAG_T7	M451	3.57	16.23	2.19	30.21	22.0%	Pass
TWR_RED_DIAG_T7	M459	3.814	16.23	2.25	30.21	23.5%	Pass
TWR_RED_DIAG_T7	M468	2.274	16.23	1.37	30.21	14.0%	Pass
TWR_RED_DIAG_T7	M476	2.194	16.23	1.37	30.21	13.5%	Pass
TWR_RED_DIAG_T7	M485	3.749	16.23	2.31	30.21	23.1%	Pass
TWR_RED_DIAG_T7	M493	3.498	16.23	2.22	30.21	21.5%	Pass
TWR_RED_DIAG_T7	M502	2.116	16.23	1.41	30.21	13.0%	Pass
TWR_RED_DIAG_T7	M510	2.198	16.23	1.44	30.21	13.5%	Pass
TWR_RED_DIAG_T8	M532	4.498	16.28	2.97	30.21	27.6%	Pass
TWR_RED_DIAG_T8	M540	4.707	16.28	2.98	30.21	28.9%	Pass
TWR_RED_DIAG_T8	M549	2.828	16.28	1.87	30.21	17.4%	Pass
TWR_RED_DIAG_T8	M557	2.748	16.28	1.88	30.21	16.9%	Pass
TWR_RED_DIAG_T8	M566	4.627	16.28	3.06	30.21	28.4%	Pass
TWR_RED_DIAG_T8	M574	4.399	16.28	3.00	30.21	27.0%	Pass
TWR_RED_DIAG_T8	M583	2.658	16.28	1.96	30.21	16.3%	Pass
TWR_RED_DIAG_T8	M591	2.749	16.28	2.02	30.21	16.9%	Pass
TWR_RED_DIAG_T9	M613	5.747	16.38	3.73	30.21	35.1%	Pass
TWR_RED_DIAG_T9	M621	5.927	16.38	3.77	30.21	36.2%	Pass
TWR_RED_DIAG_T9	M630	4.084	16.38	2.54	30.21	24.9%	Pass
TWR_RED_DIAG_T9	M638	3.979	16.38	2.51	30.21	24.3%	Pass
TWR_RED_DIAG_T9	M647	5.871	16.38	3.84	30.21	35.8%	Pass
TWR_RED_DIAG_T9	M655	5.651	16.38	3.77	30.21	34.5%	Pass
TWR_RED_DIAG_T9	M664	3.886	16.38	2.56	30.21	23.7%	Pass
TWR_RED_DIAG_T9	M672	4.016	16.38	2.61	30.21	24.5%	Pass
TWR_RED_DIAG_T10	M694	1.25	16.05	1.69	30.21	7.8%	Pass
TWR_RED_DIAG_T10	M704	1.281	16.05	1.67	30.21	8.0%	Pass
TWR_RED_DIAG_T10	M715	0.424	15.61	1.17	30.21	3.9%	Pass
TWR_RED_DIAG_T10	M725	0.478	15.61	1.21	30.21	4.0%	Pass
TWR_RED_DIAG_T10	M736	1.294	16.05	1.74	30.21	8.1%	Pass
TWR_RED_DIAG_T10	M746	1.239	16.05	1.73	30.21	7.7%	Pass
TWR_RED_DIAG_T10	M757	0.487	15.61	1.24	30.21	4.1%	Pass
TWR_RED_DIAG_T10	M767	0.445	15.61	1.23	30.21	4.1%	Pass
TWR_RED_HIPDIA_1 T10	M807	0.355	19.46	0.12	60.42	1.8%	Pass
TWR_RED_HIPDIA_1 T10	M808	0.344	19.78	0.12	60.42	1.7%	Pass
TWR_RED_HIPDIA_1 T10	M809	0.341	19.78	0.10	60.42	1.7%	Pass
TWR_RED_HIPDIA_1 T10	M810	0.331	19.46	0.12	60.42	1.7%	Pass
TWR_RED_HIPDIA_1 T10	M811	0.33	19.46	0.08	60.42	1.7%	Pass



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TAG0053 - CHESHIRE

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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_1_T10	M812	0.302	19.78	0.10	60.42	1.5%	Pass
TWR_RED_HIPDIA_1_T10	M813	0.304	19.78	0.12	60.42	1.5%	Pass
TWR_RED_HIPDIA_1_T10	M814	0.353	19.46	0.09	60.42	1.8%	Pass
TWR_RED_HIPDIA_2_T2	M1246	1.227	14.70	0.00	48.02	8.3%	Pass
TWR_RED_HIPDIA_2_T2	M1247	1.227	14.70	0.00	48.02	8.3%	Pass
TWR_RED_HIPDIA_2_T2	M1248	1.233	14.70	0.00	48.02	8.4%	Pass
TWR_RED_HIPDIA_2_T2	M1249	1.232	14.70	0.00	48.02	8.4%	Pass
TWR_RED_HIPDIA_2_T2	M1250	1.232	14.70	0.00	48.02	8.4%	Pass
TWR_RED_HIPDIA_2_T2	M1251	1.233	14.70	0.00	48.02	8.4%	Pass
TWR_RED_HIPDIA_2_T2	M1252	1.226	14.70	0.00	48.02	8.3%	Pass
TWR_RED_HIPDIA_2_T2	M1253	1.225	14.70	0.00	48.02	8.3%	Pass
TWR_RED_HIPDIA_2_T3	M1194	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1195	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1196	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1197	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1198	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1199	0.604	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1200	0.604	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T3	M1201	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1142	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1143	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1144	0.602	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1145	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1146	0.604	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1147	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T4	M1148	0.595	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T4	M1149	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1090	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1091	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1092	0.597	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1093	0.596	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1094	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1095	0.603	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1096	0.605	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T5	M1097	0.604	14.70	0.00	48.02	4.1%	Pass
TWR_RED_HIPDIA_2_T6	M1038	0.584	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1039	0.584	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1040	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1041	0.591	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1042	0.592	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1043	0.592	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1044	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T6	M1045	0.591	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M986	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M987	0.591	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M988	0.585	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M989	0.583	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M990	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M991	0.592	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M992	0.593	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T7	M993	0.593	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M934	0.595	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M935	0.591	14.70	0.00	48.02	4.0%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_2_T8	M936	0.585	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M937	0.583	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M938	0.594	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M939	0.592	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M940	0.593	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_2_T8	M941	0.593	14.70	0.00	48.02	4.0%	Pass
TWR_RED_HIPDIA_3_T10	M815	0.954	15.58	0.00	60.42	6.1%	Pass
TWR_RED_HIPDIA_3_T10	M816	0.885	15.99	0.00	60.42	5.5%	Pass
TWR_RED_HIPDIA_3_T10	M817	0.861	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M818	0.926	15.58	0.00	60.42	5.9%	Pass
TWR_RED_HIPDIA_3_T10	M819	0.927	15.58	0.00	60.42	5.9%	Pass
TWR_RED_HIPDIA_3_T10	M820	0.86	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M821	0.858	15.99	0.00	60.42	5.4%	Pass
TWR_RED_HIPDIA_3_T10	M822	0.929	15.58	0.00	60.42	6.0%	Pass
TWR_RED_HIPDIA_T2	M1238	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1239	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1240	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1241	0.128	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1242	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1243	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1244	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T2	M1245	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1186	0.134	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1187	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1188	0.129	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1189	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1190	0.132	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1191	0.127	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1192	0.131	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T3	M1193	0.134	21.53	0.00	48.02	0.6%	Pass
TWR_RED_HIPDIA_T4	M1134	0.153	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1135	0.148	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1136	0.15	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1137	0.143	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1138	0.147	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1139	0.151	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1140	0.147	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T4	M1141	0.148	21.53	0.00	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1082	0.157	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1083	0.148	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1084	0.161	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1085	0.154	21.53	0.02	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1086	0.152	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1087	0.155	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1088	0.158	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T5	M1089	0.152	21.53	0.01	48.02	0.7%	Pass
TWR_RED_HIPDIA_T6	M1030	0.196	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1031	0.183	21.53	0.05	48.02	0.8%	Pass
TWR_RED_HIPDIA_T6	M1032	0.202	21.53	0.05	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1033	0.193	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1034	0.188	21.53	0.05	48.02	0.9%	Pass



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TAG0053 - CHESHIRE

GPD Project #: 2023701.51

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIPDIA_T6	M1035	0.191	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1036	0.194	21.53	0.04	48.02	0.9%	Pass
TWR_RED_HIPDIA_T6	M1037	0.187	21.53	0.05	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M978	0.211	21.53	0.05	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M979	0.196	21.53	0.07	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M980	0.219	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M981	0.208	21.53	0.07	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M982	0.2	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M983	0.209	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T7	M984	0.201	21.53	0.06	48.02	0.9%	Pass
TWR_RED_HIPDIA_T7	M985	0.206	21.53	0.06	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M926	0.237	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M927	0.217	21.53	0.09	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M928	0.248	21.53	0.09	48.02	1.2%	Pass
TWR_RED_HIPDIA_T8	M929	0.232	21.53	0.10	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M930	0.223	21.53	0.08	48.02	1.0%	Pass
TWR_RED_HIPDIA_T8	M931	0.229	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M932	0.233	21.53	0.08	48.02	1.1%	Pass
TWR_RED_HIPDIA_T8	M933	0.221	21.53	0.09	48.02	1.0%	Pass
TWR_RED_HIPDIA_T9	M874	0.324	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M875	0.314	21.53	0.18	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M876	0.327	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M877	0.318	21.53	0.18	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M878	0.313	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M879	0.316	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIPDIA_T9	M880	0.311	21.53	0.17	48.02	1.4%	Pass
TWR_RED_HIPDIA_T9	M881	0.317	21.53	0.17	48.02	1.5%	Pass
TWR_RED_HIP_1_T10	M799	0.062	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M800	0.055	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M801	0.062	218.03	0.05	216.14	0.0%	Pass
TWR_RED_HIP_1_T10	M806	0.061	218.03	0.06	216.14	0.0%	Pass
TWR_RED_HIP_2_T2	M1234	0	8.69	1.13	48.02	2.4%	Pass
TWR_RED_HIP_2_T2	M1235	0	8.69	1.13	48.02	2.4%	Pass
TWR_RED_HIP_2_T2	M1236	0	8.69	1.13	48.02	2.4%	Pass
TWR_RED_HIP_2_T2	M1237	0	8.69	1.13	48.02	2.4%	Pass
TWR_RED_HIP_2_T3	M1182	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T3	M1183	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T3	M1184	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T3	M1185	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T4	M1130	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T4	M1131	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T4	M1132	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T4	M1133	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1078	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1079	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T5	M1080	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T5	M1081	0	8.69	0.52	48.02	1.1%	Pass
TWR_RED_HIP_2_T6	M1026	0	8.69	0.49	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1027	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1028	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T6	M1029	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T7	M974	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T7	M975	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T7	M976	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T7	M977	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T8	M922	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T8	M923	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T8	M924	0	8.69	0.51	48.02	1.1%	Pass
TWR_RED_HIP_2_T8	M925	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T9	M870	0	8.69	0.49	48.02	1.0%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HIP_2_T9	M871	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T9	M872	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_2_T9	M873	0	8.69	0.50	48.02	1.0%	Pass
TWR_RED_HIP_3_T10	M802	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M803	0	15.14	0.56	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M804	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_3_T10	M805	0	15.14	0.54	60.42	0.9%	Pass
TWR_RED_HIP_T2	M1230	0	34.59	0.09	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1231	0	34.59	0.09	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1232	0	34.59	0.09	48.02	0.2%	Pass
TWR_RED_HIP_T2	M1233	0	34.59	0.09	48.02	0.2%	Pass
TWR_RED_HIP_T3	M1178	0	34.59	0.11	48.02	0.2%	Pass
TWR_RED_HIP_T3	M1179	0	34.59	0.12	48.02	0.2%	Pass
TWR_RED_HIP_T3	M1180	0	34.59	0.11	48.02	0.2%	Pass
TWR_RED_HIP_T3	M1181	0	34.59	0.11	48.02	0.2%	Pass
TWR_RED_HIP_T4	M1126	0	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1127	0	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1128	0	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T4	M1129	0	34.59	0.13	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1074	0	34.59	0.13	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1075	0	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1076	0	34.59	0.13	48.02	0.3%	Pass
TWR_RED_HIP_T5	M1077	0	34.59	0.13	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1022	0.012	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1023	0.002	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1024	0.009	34.59	0.15	48.02	0.3%	Pass
TWR_RED_HIP_T6	M1025	0.012	34.59	0.14	48.02	0.3%	Pass
TWR_RED_HIP_T7	M970	0.009	34.59	0.12	48.02	0.3%	Pass
TWR_RED_HIP_T7	M971	0	34.59	0.13	48.02	0.3%	Pass
TWR_RED_HIP_T7	M972	0.006	34.59	0.12	48.02	0.3%	Pass
TWR_RED_HIP_T7	M973	0.008	34.59	0.12	48.02	0.2%	Pass
TWR_RED_HIP_T8	M918	0.073	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T8	M919	0.061	34.59	0.19	48.02	0.4%	Pass
TWR_RED_HIP_T8	M920	0.071	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T8	M921	0.073	34.59	0.18	48.02	0.4%	Pass
TWR_RED_HIP_T9	M866	0.088	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HIP_T9	M867	0.088	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HIP_T9	M868	0.085	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HIP_T9	M869	0.076	34.59	0.21	48.02	0.4%	Pass
TWR_RED_HORZ_0_T10	M783	6.647	27.51	9.20	24.04	38.3%	Pass
TWR_RED_HORZ_0_T10	M784	4.762	27.51	6.53	24.04	27.2%	Pass
TWR_RED_HORZ_0_T10	M785	6.618	27.51	8.93	24.04	37.2%	Pass
TWR_RED_HORZ_0_T10	M786	4.854	27.51	6.45	24.04	26.8%	Pass
TWR_RED_HORZ_0_T10	M787	4.989	27.51	6.67	24.04	27.8%	Pass
TWR_RED_HORZ_0_T10	M788	6.39	27.51	8.92	24.04	37.1%	Pass
TWR_RED_HORZ_0_T10	M789	4.794	27.51	6.66	24.04	27.7%	Pass
TWR_RED_HORZ_0_T10	M790	6.288	27.51	9.05	24.04	37.6%	Pass
TWR_RED_HORZ_2_T1	M1262	0.255	13.33	0.74	48.02	1.9%	Pass
TWR_RED_HORZ_2_T1	M1263	0.255	13.33	0.68	48.02	1.9%	Pass
TWR_RED_HORZ_2_T1	M1264	0.241	13.33	0.70	48.02	1.8%	Pass
TWR_RED_HORZ_2_T1	M1265	0.22	13.33	0.73	48.02	1.7%	Pass
TWR_RED_HORZ_2_T2	M53	0.863	32.85	0.82	48.02	2.6%	Pass
TWR_RED_HORZ_2_T2	M61	0.864	32.85	0.83	48.02	2.6%	Pass
TWR_RED_HORZ_2_T2	M69	1.254	32.85	1.18	48.02	3.8%	Pass
TWR_RED_HORZ_2_T2	M77	1.25	32.85	1.17	48.02	3.8%	Pass
TWR_RED_HORZ_2_T2	M85	0.988	32.85	0.95	48.02	3.0%	Pass
TWR_RED_HORZ_2_T2	M93	0.994	32.85	0.94	48.02	3.0%	Pass
TWR_RED_HORZ_2_T2	M101	0.939	32.85	0.85	48.02	2.9%	Pass
TWR_RED_HORZ_2_T2	M109	0.938	32.85	0.86	48.02	2.9%	Pass
TWR_RED_HORZ_2_T3	M126	0.424	32.85	0.45	48.02	1.3%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_2_T3	M134	0.419	32.85	0.44	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M143	0.42	32.85	0.36	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M151	0.416	32.85	0.37	48.02	1.3%	Pass
TWR_RED_HORZ_2_T3	M160	0.205	32.85	0.23	48.02	0.6%	Pass
TWR_RED_HORZ_2_T3	M168	0.234	32.85	0.25	48.02	0.7%	Pass
TWR_RED_HORZ_2_T3	M177	0.461	32.85	0.40	48.02	1.4%	Pass
TWR_RED_HORZ_2_T3	M185	0.429	32.85	0.37	48.02	1.3%	Pass
TWR_RED_HORZ_2_T4	M207	0.354	32.93	0.39	48.02	1.1%	Pass
TWR_RED_HORZ_2_T4	M215	0.309	32.93	0.35	48.02	0.9%	Pass
TWR_RED_HORZ_2_T4	M224	0.438	32.93	0.38	48.02	1.3%	Pass
TWR_RED_HORZ_2_T4	M232	0.449	32.93	0.38	48.02	1.4%	Pass
TWR_RED_HORZ_2_T4	M241	0.182	32.93	0.22	48.02	0.6%	Pass
TWR_RED_HORZ_2_T4	M249	0.227	32.93	0.25	48.02	0.7%	Pass
TWR_RED_HORZ_2_T4	M258	0.405	32.93	0.32	48.02	1.2%	Pass
TWR_RED_HORZ_2_T4	M266	0.361	32.93	0.30	48.02	1.1%	Pass
TWR_RED_HORZ_2_T5	M288	0.35	33.48	0.53	48.02	1.1%	Pass
TWR_RED_HORZ_2_T5	M296	0.39	33.48	0.56	48.02	1.2%	Pass
TWR_RED_HORZ_2_T5	M305	0.3	33.48	0.27	48.02	0.9%	Pass
TWR_RED_HORZ_2_T5	M313	0.407	33.48	0.34	48.02	1.2%	Pass
TWR_RED_HORZ_2_T5	M322	0.36	33.48	0.56	48.02	1.2%	Pass
TWR_RED_HORZ_2_T5	M330	0.314	33.48	0.49	48.02	1.0%	Pass
TWR_RED_HORZ_2_T5	M339	0.441	33.48	0.36	48.02	1.3%	Pass
TWR_RED_HORZ_2_T5	M347	0.336	33.48	0.31	48.02	1.0%	Pass
TWR_RED_HORZ_2_T6	M369	0.53	33.56	0.82	48.02	1.7%	Pass
TWR_RED_HORZ_2_T6	M377	0.586	33.56	0.89	48.02	1.9%	Pass
TWR_RED_HORZ_2_T6	M386	0.258	33.56	0.18	48.02	0.8%	Pass
TWR_RED_HORZ_2_T6	M394	0.379	33.56	0.33	48.02	1.1%	Pass
TWR_RED_HORZ_2_T6	M403	0.595	33.56	0.90	48.02	1.9%	Pass
TWR_RED_HORZ_2_T6	M411	0.538	33.56	0.81	48.02	1.7%	Pass
TWR_RED_HORZ_2_T6	M420	0.412	33.56	0.35	48.02	1.2%	Pass
TWR_RED_HORZ_2_T6	M428	0.292	33.56	0.21	48.02	0.9%	Pass
TWR_RED_HORZ_2_T7	M450	0.985	34.18	1.57	48.02	3.3%	Pass
TWR_RED_HORZ_2_T7	M458	1.071	34.18	1.68	48.02	3.5%	Pass
TWR_RED_HORZ_2_T7	M467	0.347	34.18	0.35	48.02	1.0%	Pass
TWR_RED_HORZ_2_T7	M475	0.404	34.18	0.42	48.02	1.2%	Pass
TWR_RED_HORZ_2_T7	M484	1.088	34.18	1.65	48.02	3.4%	Pass
TWR_RED_HORZ_2_T7	M492	1.002	34.18	1.54	48.02	3.2%	Pass
TWR_RED_HORZ_2_T7	M501	0.415	34.18	0.41	48.02	1.2%	Pass
TWR_RED_HORZ_2_T7	M509	0.359	34.18	0.35	48.02	1.1%	Pass
TWR_RED_HORZ_2_T8	M531	1.407	34.18	2.03	48.02	4.2%	Pass
TWR_RED_HORZ_2_T8	M539	1.473	34.18	2.13	48.02	4.4%	Pass
TWR_RED_HORZ_2_T8	M548	0.512	34.18	0.46	48.02	1.5%	Pass
TWR_RED_HORZ_2_T8	M556	0.594	34.18	0.54	48.02	1.7%	Pass
TWR_RED_HORZ_2_T8	M565	1.502	34.18	2.13	48.02	4.4%	Pass
TWR_RED_HORZ_2_T8	M573	1.427	34.18	2.00	48.02	4.2%	Pass
TWR_RED_HORZ_2_T8	M582	0.636	34.18	0.53	48.02	1.9%	Pass
TWR_RED_HORZ_2_T8	M590	0.564	34.18	0.47	48.02	1.7%	Pass
TWR_RED_HORZ_2_T9	M612	1.892	34.25	2.87	48.02	6.0%	Pass
TWR_RED_HORZ_2_T9	M620	1.978	34.25	2.95	48.02	6.1%	Pass
TWR_RED_HORZ_2_T9	M629	0.758	34.25	0.93	48.02	2.2%	Pass
TWR_RED_HORZ_2_T9	M637	0.78	34.25	0.99	48.02	2.3%	Pass
TWR_RED_HORZ_2_T9	M646	2.005	34.25	2.97	48.02	6.2%	Pass
TWR_RED_HORZ_2_T9	M654	1.92	34.25	2.85	48.02	5.9%	Pass
TWR_RED_HORZ_2_T9	M663	0.795	34.25	0.98	48.02	2.3%	Pass
TWR_RED_HORZ_2_T9	M671	0.774	34.25	0.95	48.02	2.3%	Pass
TWR_RED_HORZ_2_T10	M693	1.383	34.90	0.59	48.02	4.0%	Pass
TWR_RED_HORZ_2_T10	M703	1.374	34.90	0.59	48.02	3.9%	Pass
TWR_RED_HORZ_2_T10	M714	1.082	34.90	0.46	48.02	3.1%	Pass
TWR_RED_HORZ_2_T10	M724	1.159	34.90	0.46	48.02	3.3%	Pass
TWR_RED_HORZ_2_T10	M735	1.377	34.90	0.56	48.02	3.9%	Pass



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Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_2_T10	M745	1.361	34.90	0.55	48.02	3.9%	Pass
TWR_RED_HORZ_2_T10	M756	1.183	34.90	0.46	48.02	3.4%	Pass
TWR_RED_HORZ_2_T10	M766	1.126	34.90	0.46	48.02	3.2%	Pass
TWR_RED_HORZ_3_T1	M1290	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1291	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1292	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1293	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1294	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1295	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1296	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T1	M1297	0	20.13	0.34	48.02	0.7%	Pass
TWR_RED_HORZ_3_T2	M55	0	14.32	1.48	48.02	3.1%	Pass
TWR_RED_HORZ_3_T2	M63	0	14.32	1.49	48.02	3.1%	Pass
TWR_RED_HORZ_3_T2	M71	0.076	14.32	1.63	48.02	3.4%	Pass
TWR_RED_HORZ_3_T2	M79	0.096	14.32	1.65	48.02	3.4%	Pass
TWR_RED_HORZ_3_T2	M87	0	14.32	1.49	48.02	3.1%	Pass
TWR_RED_HORZ_3_T2	M95	0	14.32	1.48	48.02	3.1%	Pass
TWR_RED_HORZ_3_T2	M103	0	14.32	1.44	48.02	3.0%	Pass
TWR_RED_HORZ_3_T2	M111	0	14.32	1.42	48.02	3.0%	Pass
TWR_RED_HORZ_3_T3	M128	0.218	14.32	0.64	48.02	1.5%	Pass
TWR_RED_HORZ_3_T3	M136	0.188	14.32	0.69	48.02	1.4%	Pass
TWR_RED_HORZ_3_T3	M145	0.207	14.32	0.61	48.02	1.4%	Pass
TWR_RED_HORZ_3_T3	M153	0.23	14.32	0.57	48.02	1.6%	Pass
TWR_RED_HORZ_3_T3	M162	0.102	14.32	0.53	48.02	1.1%	Pass
TWR_RED_HORZ_3_T3	M170	0.108	14.32	0.52	48.02	1.1%	Pass
TWR_RED_HORZ_3_T3	M179	0.226	14.32	0.55	48.02	1.6%	Pass
TWR_RED_HORZ_3_T3	M187	0.227	14.32	0.56	48.02	1.6%	Pass
TWR_RED_HORZ_3_T4	M209	0.079	14.32	0.66	48.02	1.4%	Pass
TWR_RED_HORZ_3_T4	M217	0.008	14.32	0.71	48.02	1.5%	Pass
TWR_RED_HORZ_3_T4	M226	0.069	14.32	0.54	48.02	1.1%	Pass
TWR_RED_HORZ_3_T4	M234	0.126	14.32	0.50	48.02	1.0%	Pass
TWR_RED_HORZ_3_T4	M243	0	14.32	0.62	48.02	1.3%	Pass
TWR_RED_HORZ_3_T4	M251	0	14.32	0.60	48.02	1.3%	Pass
TWR_RED_HORZ_3_T4	M260	0.107	14.32	0.47	48.02	1.0%	Pass
TWR_RED_HORZ_3_T4	M268	0.062	14.32	0.47	48.02	1.0%	Pass
TWR_RED_HORZ_3_T5	M290	0.26	14.48	0.83	48.02	1.8%	Pass
TWR_RED_HORZ_3_T5	M298	0.217	14.48	0.93	48.02	1.9%	Pass
TWR_RED_HORZ_3_T5	M307	0.092	14.48	0.61	48.02	1.3%	Pass
TWR_RED_HORZ_3_T5	M315	0.212	14.48	0.62	48.02	1.5%	Pass
TWR_RED_HORZ_3_T5	M324	0.181	14.48	0.78	48.02	1.6%	Pass
TWR_RED_HORZ_3_T5	M332	0.169	14.48	0.74	48.02	1.5%	Pass
TWR_RED_HORZ_3_T5	M341	0.236	14.48	0.62	48.02	1.6%	Pass
TWR_RED_HORZ_3_T5	M349	0.151	14.48	0.56	48.02	1.2%	Pass
TWR_RED_HORZ_3_T6	M371	0.274	14.51	0.97	48.02	2.0%	Pass
TWR_RED_HORZ_3_T6	M379	0.229	14.51	1.08	48.02	2.2%	Pass
TWR_RED_HORZ_3_T6	M388	0.068	14.51	0.71	48.02	1.5%	Pass
TWR_RED_HORZ_3_T6	M396	0.205	14.51	0.69	48.02	1.4%	Pass
TWR_RED_HORZ_3_T6	M405	0.26	14.51	1.00	48.02	2.1%	Pass
TWR_RED_HORZ_3_T6	M413	0.234	14.51	0.92	48.02	1.9%	Pass
TWR_RED_HORZ_3_T6	M422	0.231	14.51	0.68	48.02	1.6%	Pass
TWR_RED_HORZ_3_T6	M430	0.143	14.51	0.65	48.02	1.3%	Pass
TWR_RED_HORZ_3_T7	M452	0.455	14.70	1.27	48.02	3.1%	Pass
TWR_RED_HORZ_3_T7	M460	0.455	14.70	1.43	48.02	3.1%	Pass
TWR_RED_HORZ_3_T7	M469	0.162	14.70	0.86	48.02	1.8%	Pass
TWR_RED_HORZ_3_T7	M477	0.277	14.70	0.87	48.02	1.9%	Pass
TWR_RED_HORZ_3_T7	M486	0.502	14.70	1.34	48.02	3.4%	Pass
TWR_RED_HORZ_3_T7	M494	0.466	14.70	1.24	48.02	3.2%	Pass
TWR_RED_HORZ_3_T7	M503	0.317	14.70	0.86	48.02	2.2%	Pass
TWR_RED_HORZ_3_T7	M511	0.256	14.70	0.81	48.02	1.7%	Pass
TWR_RED_HORZ_3_T8	M533	0.751	14.70	1.62	48.02	5.1%	Pass



TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2023701.51

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_3_T8	M541	0.736	14.70	1.78	48.02	5.0%	Pass
TWR_RED_HORZ_3_T8	M550	0.313	14.70	1.07	48.02	2.2%	Pass
TWR_RED_HORZ_3_T8	M558	0.419	14.70	1.03	48.02	2.9%	Pass
TWR_RED_HORZ_3_T8	M567	0.792	14.70	1.67	48.02	5.4%	Pass
TWR_RED_HORZ_3_T8	M575	0.765	14.70	1.58	48.02	5.2%	Pass
TWR_RED_HORZ_3_T8	M584	0.445	14.70	1.00	48.02	3.0%	Pass
TWR_RED_HORZ_3_T8	M592	0.406	14.70	0.99	48.02	2.8%	Pass
TWR_RED_HORZ_3_T9	M614	1.069	14.72	2.10	48.02	7.3%	Pass
TWR_RED_HORZ_3_T9	M622	1.054	14.72	2.25	48.02	7.2%	Pass
TWR_RED_HORZ_3_T9	M631	0.591	14.72	1.40	48.02	4.0%	Pass
TWR_RED_HORZ_3_T9	M639	0.698	14.72	1.36	48.02	4.7%	Pass
TWR_RED_HORZ_3_T9	M648	1.115	14.72	2.14	48.02	7.6%	Pass
TWR_RED_HORZ_3_T9	M656	1.087	14.72	2.04	48.02	7.4%	Pass
TWR_RED_HORZ_3_T9	M665	0.73	14.72	1.35	48.02	5.0%	Pass
TWR_RED_HORZ_3_T9	M673	0.696	14.72	1.33	48.02	4.7%	Pass
TWR_RED_HORZ_3_T10	M695	1.444	24.72	0.87	63.37	5.8%	Pass
TWR_RED_HORZ_3_T10	M705	1.436	24.72	0.89	63.37	5.8%	Pass
TWR_RED_HORZ_3_T10	M716	1.034	24.72	0.75	63.37	4.2%	Pass
TWR_RED_HORZ_3_T10	M726	1.132	24.72	0.75	63.37	4.6%	Pass
TWR_RED_HORZ_3_T10	M737	1.43	24.72	0.82	63.37	5.8%	Pass
TWR_RED_HORZ_3_T10	M747	1.415	24.72	0.79	63.37	5.7%	Pass
TWR_RED_HORZ_3_T10	M758	1.15	24.72	0.74	63.37	4.7%	Pass
TWR_RED_HORZ_3_T10	M768	1.069	24.72	0.74	63.37	4.3%	Pass
TWR_RED_HORZ_4_T1	M1298	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1299	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1300	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1301	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1302	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1303	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1304	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1305	0	21.37	0.04	24.08	0.1%	Pass
TWR_RED_HORZ_4_T1	M1306	0	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1307	0	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1308	0	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T1	M1309	0	5.94	0.14	24.08	0.6%	Pass
TWR_RED_HORZ_4_T10	M697	0.985	27.41	1.64	79.69	3.6%	Pass
TWR_RED_HORZ_4_T10	M707	1.017	27.41	1.69	79.69	3.7%	Pass
TWR_RED_HORZ_4_T10	M718	0.682	27.41	1.19	79.69	2.5%	Pass
TWR_RED_HORZ_4_T10	M728	0.698	27.41	1.20	79.69	2.5%	Pass
TWR_RED_HORZ_4_T10	M739	1.032	27.41	1.67	79.69	3.8%	Pass
TWR_RED_HORZ_4_T10	M749	0.999	27.41	1.62	79.69	3.6%	Pass
TWR_RED_HORZ_4_T10	M760	0.734	27.41	1.18	79.69	2.7%	Pass
TWR_RED_HORZ_4_T10	M770	0.731	27.41	1.17	79.69	2.7%	Pass
TWR_RED_HORZ_T1	M16	1.376	6.30	0.87	24.08	21.8%	Pass
TWR_RED_HORZ_T1	M19	1.599	6.30	0.93	24.08	25.4%	Pass
TWR_RED_HORZ_T1	M23	1.651	6.30	0.97	24.08	26.2%	Pass
TWR_RED_HORZ_T1	M26	1.614	6.30	1.05	24.08	25.6%	Pass
TWR_RED_HORZ_T1	M30	1.522	6.30	0.96	24.08	24.2%	Pass
TWR_RED_HORZ_T1	M33	1.389	6.30	0.83	24.08	22.0%	Pass
TWR_RED_HORZ_T1	M37	1.3	6.30	0.71	24.08	20.6%	Pass
TWR_RED_HORZ_T1	M40	1.315	6.30	0.80	24.08	20.9%	Pass
TWR_RED_HORZ_T2	M52	0	31.25	0.32	30.21	1.0%	Pass
TWR_RED_HORZ_T2	M60	0	31.25	0.38	30.21	1.3%	Pass
TWR_RED_HORZ_T2	M68	0.012	31.25	0.13	30.21	0.4%	Pass
TWR_RED_HORZ_T2	M76	0.045	31.25	0.16	30.21	0.5%	Pass
TWR_RED_HORZ_T2	M84	0	31.25	0.37	30.21	1.2%	Pass
TWR_RED_HORZ_T2	M92	0.007	31.25	0.31	30.21	1.0%	Pass
TWR_RED_HORZ_T2	M100	0.055	31.25	0.15	30.21	0.5%	Pass
TWR_RED_HORZ_T2	M108	0.018	31.25	0.12	30.21	0.4%	Pass
TWR_RED_HORZ_T3	M125	0.005	31.25	0.80	30.21	2.7%	Pass



TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2023701.51

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_T3	M133	0.032	31.25	0.91	30.21	3.0%	Pass
TWR_RED_HORZ_T3	M142	0.146	31.25	0.44	30.21	1.5%	Pass
TWR_RED_HORZ_T3	M150	0.205	31.25	0.48	30.21	1.6%	Pass
TWR_RED_HORZ_T3	M159	0.008	31.25	0.82	30.21	2.7%	Pass
TWR_RED_HORZ_T3	M167	0.047	31.25	0.73	30.21	2.4%	Pass
TWR_RED_HORZ_T3	M176	0.247	31.25	0.48	30.21	1.6%	Pass
TWR_RED_HORZ_T3	M184	0.162	31.25	0.42	30.21	1.4%	Pass
TWR_RED_HORZ_T4	M206	0.314	31.29	1.21	30.21	4.0%	Pass
TWR_RED_HORZ_T4	M214	0.344	31.29	1.36	30.21	4.5%	Pass
TWR_RED_HORZ_T4	M223	0.099	31.29	0.49	30.21	1.6%	Pass
TWR_RED_HORZ_T4	M231	0.207	31.29	0.57	30.21	1.9%	Pass
TWR_RED_HORZ_T4	M240	0.373	31.29	1.32	30.21	4.4%	Pass
TWR_RED_HORZ_T4	M248	0.332	31.29	1.17	30.21	3.9%	Pass
TWR_RED_HORZ_T4	M257	0.265	31.29	0.58	30.21	1.9%	Pass
TWR_RED_HORZ_T4	M265	0.171	31.29	0.49	30.21	1.6%	Pass
TWR_RED_HORZ_T5	M287	0.896	31.57	2.19	30.21	7.2%	Pass
TWR_RED_HORZ_T5	M295	0.917	31.57	2.36	30.21	7.8%	Pass
TWR_RED_HORZ_T5	M304	0.508	31.57	1.18	30.21	3.9%	Pass
TWR_RED_HORZ_T5	M312	0.586	31.57	1.21	30.21	4.0%	Pass
TWR_RED_HORZ_T5	M321	0.961	31.57	2.30	30.21	7.6%	Pass
TWR_RED_HORZ_T5	M329	0.923	31.57	2.13	30.21	7.0%	Pass
TWR_RED_HORZ_T5	M338	0.645	31.57	1.19	30.21	3.9%	Pass
TWR_RED_HORZ_T5	M346	0.592	31.57	1.16	30.21	3.8%	Pass
TWR_RED_HORZ_T6	M368	1.504	31.61	2.98	30.21	9.8%	Pass
TWR_RED_HORZ_T6	M376	1.549	31.61	3.20	30.21	10.6%	Pass
TWR_RED_HORZ_T6	M385	0.737	31.61	1.56	30.21	5.2%	Pass
TWR_RED_HORZ_T6	M393	0.763	31.61	1.54	30.21	5.1%	Pass
TWR_RED_HORZ_T6	M402	1.593	31.61	3.14	30.21	10.4%	Pass
TWR_RED_HORZ_T6	M410	1.529	31.61	2.92	30.21	9.6%	Pass
TWR_RED_HORZ_T6	M419	0.801	31.61	1.48	30.21	4.9%	Pass
TWR_RED_HORZ_T6	M427	0.788	31.61	1.50	30.21	5.0%	Pass
TWR_RED_HORZ_T7	M449	2.238	31.89	3.93	30.21	13.0%	Pass
TWR_RED_HORZ_T7	M457	2.313	31.89	4.19	30.21	13.9%	Pass
TWR_RED_HORZ_T7	M466	1.323	31.89	2.44	30.21	8.1%	Pass
TWR_RED_HORZ_T7	M474	1.312	31.89	2.37	30.21	7.8%	Pass
TWR_RED_HORZ_T7	M483	2.369	31.89	4.12	30.21	13.6%	Pass
TWR_RED_HORZ_T7	M491	2.272	31.89	3.86	30.21	12.8%	Pass
TWR_RED_HORZ_T7	M500	1.356	31.89	2.29	30.21	7.6%	Pass
TWR_RED_HORZ_T7	M508	1.384	31.89	2.37	30.21	7.8%	Pass
TWR_RED_HORZ_T8	M530	3.012	31.92	4.90	30.21	16.2%	Pass
TWR_RED_HORZ_T8	M538	3.044	31.92	5.12	30.21	17.0%	Pass
TWR_RED_HORZ_T8	M547	1.754	31.92	2.98	30.21	9.9%	Pass
TWR_RED_HORZ_T8	M555	1.761	31.92	2.91	30.21	9.6%	Pass
TWR_RED_HORZ_T8	M564	3.12	31.92	5.04	30.21	16.7%	Pass
TWR_RED_HORZ_T8	M572	3.05	31.92	4.80	30.21	15.9%	Pass
TWR_RED_HORZ_T8	M581	1.802	31.92	2.82	30.21	9.3%	Pass
TWR_RED_HORZ_T8	M589	1.84	31.92	2.90	30.21	9.6%	Pass
TWR_RED_HORZ_T9	M611	3.862	31.96	6.26	30.21	20.7%	Pass
TWR_RED_HORZ_T9	M619	3.918	31.96	6.45	30.21	21.4%	Pass
TWR_RED_HORZ_T9	M628	2.511	31.96	4.32	30.21	14.3%	Pass
TWR_RED_HORZ_T9	M636	2.479	31.96	4.21	30.21	13.9%	Pass
TWR_RED_HORZ_T9	M645	3.992	31.96	6.40	30.21	21.2%	Pass
TWR_RED_HORZ_T9	M653	3.912	31.96	6.16	30.21	20.4%	Pass
TWR_RED_HORZ_T9	M662	2.527	31.96	4.12	30.21	13.6%	Pass
TWR_RED_HORZ_T9	M670	2.585	31.96	4.25	30.21	14.1%	Pass
TWR_RED_HORZ_T10	M692	1.594	25.98	1.70	30.21	6.1%	Pass
TWR_RED_HORZ_T10	M702	1.579	25.98	1.73	30.21	6.1%	Pass
TWR_RED_HORZ_T10	M713	1.015	25.98	0.80	30.21	3.9%	Pass
TWR_RED_HORZ_T10	M723	1.059	25.98	0.86	30.21	4.1%	Pass
TWR_RED_HORZ_T10	M734	1.643	25.98	1.71	30.21	6.3%	Pass



TIA-222-H Code Angle Bracing Member Checks

TAG0053 - CHESHIRE

GPD Project #: 2023701.51

Section Set	Member	Comp. (K)	$\Phi P_{n,Comp}$ (K)	Ten (K)	$\Phi P_{n,Ten}$ (K)	Capacity	Pass/Fail
TWR_RED_HORZ_T10	M744	1.625	25.98	1.65	30.21	6.3%	Pass
TWR_RED_HORZ_T10	M755	1.092	25.98	0.86	30.21	4.2%	Pass
TWR_RED_HORZ_T10	M765	1.071	25.98	0.80	30.21	4.1%	Pass
TWR_TOP_GIRT_T1	M5	0.613	41.85	0.58	118.53	1.5%	Pass
TWR_TOP_GIRT_T1	M6	0.684	41.85	0.62	118.53	1.6%	Pass
TWR_TOP_GIRT_T1	M7	0.533	41.85	0.61	118.53	1.3%	Pass
TWR_TOP_GIRT_T1	M8	0.404	41.85	0.58	118.53	1.0%	Pass



TIA-222-H Code Bolt Checks
TAG0053 - CHESHIRE
GPD Project #: 2023701.51

Section #	Elevation (Ft.)	Section Set	Member	Bolt Grade	Bolt Size (in)	# of Bolts	Comp. (K)	Ten. (K)	Maximum Load (K)	Allowable Load (K)	% Capacity
T1	250	TWR_LEG_T1	L6x6x1/2	A307	0.75	12	15.196	2.383	15.196	90.300	16.8%
T1	250	TWR_TOP_GIRT_T1	2L3x4x5/16x3/8	A307	0.75	2	0.684	0.62	0.684	49.701	1.4%
T1	250	TWR_DIAG_T1	2L3x4x5/16x3/8	A307	0.75	2	8.133	3.288	8.133	49.701	16.4%
T1	250	TWR_DIAG_OUTER_T1	2L3 1/2x4x5/16x3/8	A307	0.75	2	2.307	1.892	2.307	49.701	4.6%
T1	250	TWR_RED_HORZ_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	1.651	1.046	1.651	15.701	10.5%
T1	250	TWR_RED_HORZ_2_T1	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.255	0.74	0.740	31.402	2.4%
T1	250	TWR_RED_HORZ_3_T1	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.336	0.336	31.402	1.1%
T1	250	TWR_RED_HORZ_4_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	0	0.136	0.136	15.701	0.9%
T1	250	TWR_RED_DIAG_T1	L2 1/2x2 1/2x3/16	A307	0.75	2	1.165	0.77	1.165	15.701	7.4%
T2	237.5	TWR_LEG_T2	W6X20	A307	0.75	16	23.305	0	23.305	168.800	13.8%
T2	237.5	TWR_DIAG_T2	2L3x2 1/2x3/8x3/8	A307	0.75	4	20.193	11.987	20.193	49.701	40.6%
T2	237.5	TWR_RED_HORZ_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.254	1.175	1.254	31.402	4.0%
T2	237.5	TWR_RED_HORZ_3_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.096	1.648	1.648	31.402	5.2%
T2	237.5	TWR_RED_DIAG_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.886	1.221	1.221	31.402	3.9%
T2	237.5	TWR_RED_DIAG_3_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.041	0.233	2.041	31.402	6.5%
T2	237.5	TWR_RED_HIP_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.088	0.088	31.402	0.3%
T2	237.5	TWR_RED_HIP_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	1.134	1.134	31.402	3.6%
T2	237.5	TWR_RED_HIPDIA_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.131	0	0.131	31.402	0.4%
T2	237.5	TWR_RED_HIPDIA_2_T2	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.233	0	1.233	31.402	3.9%
T3	212.5	TWR_LEG_T3	W6X20	A307	0.75	24	48.813	8.306	48.813	168.800	28.9%
T3	212.5	TWR_HORZ_T3	2L3x2 1/2x1/4x3/8	A307	0.75	3	10.944	14.616	14.616	62.531	23.4%
T3	212.5	TWR_DIAG_T3	2L3x2 1/2x3/8x3/8	A307	0.75	2	25.024	22.764	25.024	49.701	50.3%
T3	212.5	TWR_RED_HORZ_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.461	0.446	0.461	31.402	1.5%
T3	212.5	TWR_RED_HORZ_3_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.23	0.694	0.694	31.402	2.2%
T3	212.5	TWR_RED_DIAG_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.282	0.555	0.555	31.402	1.8%
T3	212.5	TWR_RED_DIAG_3_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.806	0.337	0.806	31.402	2.6%
T3	212.5	TWR_RED_HIP_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.116	0.116	31.402	0.4%
T3	212.5	TWR_RED_HIP_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.511	0.511	31.402	1.6%
T3	212.5	TWR_RED_HIPDIA_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.134	0	0.134	31.402	0.4%
T3	212.5	TWR_RED_HIPDIA_2_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.605	0	0.605	31.402	1.9%
T3	212.5	TWR_INNER_SUPP_T3	2L3x2 1/2x1/4x3/8	A307	0.75	2	1.799	1.812	1.812	44.588	4.1%
T3	212.5	TWR_INNER_SQ_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.505	3.503	3.503	31.402	11.2%
T3	212.5	TWR_INNER_CORNER_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.096	4.096	31.402	13.0%
T3	212.5	TWR_INNER_TRI_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.01	0.031	0.031	31.402	0.1%
T3	212.5	TWR_INNER_BRACE_T3	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.021	0.015	0.021	31.402	0.1%
T3	212.5	TWR_INNER_LADDER_T3	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.557	1.904	2.557	44.588	5.7%
T4	187.5	TWR_LEG_T4	W6X25	A307	0.75	32	75.027	30.027	75.027	273.400	27.4%
T4	187.5	TWR_HORZ_T4	2L3x2 1/2x1/4x3/8	A307	0.75	3	16.178	16.593	16.593	62.531	26.5%
T4	187.5	TWR_DIAG_T4	2L3x2-1/2x1/2x3/8	A307	0.75	4	31.773	29.42	31.773	99.402	32.0%
T4	187.5	TWR_RED_HORZ_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.449	0.39	0.449	31.402	1.4%
T4	187.5	TWR_RED_HORZ_3_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.126	0.714	0.714	31.402	2.3%
T4	187.5	TWR_RED_DIAG_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.213	0.575	0.575	31.402	1.8%
T4	187.5	TWR_RED_DIAG_3_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.721	0.247	0.721	31.402	2.3%
T4	187.5	TWR_RED_HIP_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.147	0.147	31.402	0.5%
T4	187.5	TWR_RED_HIP_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.509	0.509	31.402	1.6%
T4	187.5	TWR_RED_HIPDIA_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.153	0.008	0.153	31.402	0.5%
T4	187.5	TWR_RED_HIPDIA_2_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.605	0	0.605	31.402	1.9%
T4	187.5	TWR_INNER_SUPP_T4	2L3x2 1/2x1/4x3/8	A307	0.75	2	1.859	1.877	1.877	44.588	4.2%
T4	187.5	TWR_INNER_SQ_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.171	3.397	3.397	31.402	10.8%
T4	187.5	TWR_INNER_CORNER_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	3.878	3.878	31.402	12.3%
T4	187.5	TWR_INNER_TRI_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.017	0.03	0.030	31.402	0.1%
T4	187.5	TWR_INNER_BRACE_T4	2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.034	0.02	0.034	31.402	0.1%
T4	187.5	TWR_INNER_LADDER_T4	2L3x2 1/2x1/4x3/8	A307	0.75	2	2.387	2.185	2.387	44.588	5.4%
T5	162.5	TWR_LEG_T5	W8X31	A307	1	32	113.119	59.767	113.119	340.600	33.2%
T5	162.5	TWR_HORZ_T5	2L3x2 1/2x1/4x3/8	A307	0.75	3	19.557	19.956	19.956	62.531	31.9%
T5	162.5	TWR_DIAG_T5	2L3x2-1/2x1/2x3/8	A307	0.75	4	38.357	35.59	38.357	99.402	38.6%

Section #	Elevation (Ft.)	Section Set	Member	Bolt Grade	Bolt Size (in)	# of Bolts	Comp. (K)	Ten. (K)	Maximum Load (K)	Allowable Load (K)	% Capacity
T5	162.5	TWR_RED_HORZ_2	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.441	0.56	0.560	31.402	1.8%
T5	162.5	TWR_RED_HORZ_3	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.26	0.93	0.930	31.402	3.0%
T5	162.5	TWR_RED_DIAG_2	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.317	0.555	0.555	31.402	1.8%
T5	162.5	TWR_RED_DIAG_3	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.777	0.51	0.777	31.402	2.5%
T5	162.5	TWR_RED_HIP	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.136	0.136	31.402	0.4%
T5	162.5	TWR_RED_HIP_2	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.515	0.515	31.402	1.6%
T5	162.5	TWR_RED_HIPDIA	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.161	0.015	0.161	31.402	0.5%
T5	162.5	TWR_RED_HIPDIA_2	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.605	0	0.605	31.402	1.9%
T5	162.5	TWR_INNER_SUPP	T5 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.242	2.265	2.265	44.588	5.1%
T5	162.5	TWR_INNER_SQ	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.625	4.121	4.121	31.402	13.1%
T5	162.5	TWR_INNER_CORNER	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.655	4.655	31.402	14.8%
T5	162.5	TWR_INNER_TRI	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.021	0.037	0.037	31.402	0.1%
T5	162.5	TWR_INNER_BRACE	T5 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.043	0.027	0.043	31.402	0.1%
T5	162.5	TWR_INNER_LADDER	T5 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.872	2.679	2.872	44.588	6.4%
T6	137.5	TWR_LEG	T6 W8x40	A307	1	32	159.73	96.521	159.730	471.700	33.9%
T6	137.5	TWR_HORZ	T6 2L3x2 1/2x5/16x3/8	A307	0.75	3	23.456	23.968	23.968	74.551	32.1%
T6	137.5	TWR_DIAG	T6 2L4x3x3/8x3/8	A307	0.75	4	45.089	42.585	45.089	99.402	45.4%
T6	137.5	TWR_RED_HORZ_2	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.595	0.901	0.901	31.402	2.9%
T6	137.5	TWR_RED_HORZ_3	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.274	1.078	1.078	31.402	3.4%
T6	137.5	TWR_RED_DIAG_2	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.537	0.602	0.602	31.402	1.9%
T6	137.5	TWR_RED_DIAG_3	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.856	0.714	0.856	31.402	2.7%
T6	137.5	TWR_RED_HIP	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.012	0.152	0.152	31.402	0.5%
T6	137.5	TWR_RED_HIP_2	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.503	0.503	31.402	1.6%
T6	137.5	TWR_RED_HIPDIA	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.202	0.057	0.202	31.402	0.6%
T6	137.5	TWR_RED_HIPDIA_2	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.594	0	0.594	31.402	1.9%
T6	137.5	TWR_INNER_SUPP	T6 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.275	2.312	2.312	44.588	5.2%
T6	137.5	TWR_INNER_SQ	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.67	4.208	4.208	31.402	13.4%
T6	137.5	TWR_INNER_CORNER	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.736	4.736	31.402	15.1%
T6	137.5	TWR_INNER_TRI	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.021	0.038	0.038	31.402	0.1%
T6	137.5	TWR_INNER_BRACE	T6 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.051	0.032	0.051	31.402	0.2%
T6	137.5	TWR_INNER_LADDER	T6 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.918	2.732	2.918	44.588	6.5%
T7	112.5	TWR_LEG	T7 W10x54	A307	1	32	214.364	141.458	214.364	484.800	44.2%
T7	112.5	TWR_HORZ	T7 2L3x2 1/2x3/8x3/8	A307	0.75	4	26.719	27.155	27.155	99.402	27.3%
T7	112.5	TWR_DIAG	T7 2L4x3x3/8x3/8	A307	0.75	4	50.893	48.426	50.893	99.402	51.2%
T7	112.5	TWR_RED_HORZ_2	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.088	1.681	1.681	31.402	5.4%
T7	112.5	TWR_RED_HORZ_3	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.502	1.426	1.426	31.402	4.5%
T7	112.5	TWR_RED_DIAG_2	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.193	1.009	1.193	31.402	3.8%
T7	112.5	TWR_RED_DIAG_3	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.173	1.116	1.173	31.402	3.7%
T7	112.5	TWR_RED_HIP	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.009	0.128	0.128	31.402	0.4%
T7	112.5	TWR_RED_HIP_2	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.51	0.510	31.402	1.6%
T7	112.5	TWR_RED_HIPDIA	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.219	0.074	0.219	31.402	0.7%
T7	112.5	TWR_RED_HIPDIA_2	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.594	0	0.594	31.402	1.9%
T7	112.5	TWR_INNER_SUPP	T7 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.257	2.304	2.304	44.588	5.2%
T7	112.5	TWR_INNER_SQ	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.643	4.172	4.172	31.402	13.3%
T7	112.5	TWR_INNER_CORNER	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	4.69	4.690	31.402	14.9%
T7	112.5	TWR_INNER_TRI	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.021	0.037	0.037	31.402	0.1%
T7	112.5	TWR_INNER_BRACE	T7 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.064	0.045	0.064	31.402	0.2%
T7	112.5	TWR_INNER_LADDER	T7 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.884	2.703	2.884	44.588	6.5%
T8	87.5	TWR_LEG	T8 W10x60	A307	1	32	276.616	193.166	276.616	530.100	52.2%
T8	87.5	TWR_HORZ	T8 2L3x2 1/2x3/8x3/8	A307	0.75	4	30.144	30.515	30.515	99.402	30.7%
T8	87.5	TWR_DIAG	T8 2L4x3x1/2x3/8	A307	0.75	5	57.848	54.467	57.848	124.252	46.6%
T8	87.5	TWR_RED_HORZ_2	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.502	2.132	2.132	31.402	6.8%
T8	87.5	TWR_RED_HORZ_3	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.792	1.777	1.777	31.402	5.7%
T8	87.5	TWR_RED_DIAG_2	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.516	1.36	1.516	31.402	4.8%
T8	87.5	TWR_RED_DIAG_3	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.554	1.539	1.554	31.402	4.9%
T8	87.5	TWR_RED_HIP	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.073	0.186	0.186	31.402	0.6%
T8	87.5	TWR_RED_HIP_2	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.51	0.510	31.402	1.6%
T8	87.5	TWR_RED_HIPDIA	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.248	0.102	0.248	31.402	0.8%
T8	87.5	TWR_RED_HIPDIA_2	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.595	0	0.595	31.402	1.9%
T8	87.5	TWR_INNER_SUPP	T8 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.522	2.582	2.582	44.588	5.8%
T8	87.5	TWR_INNER_SQ	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.996	4.682	4.682	31.402	14.9%
T8	87.5	TWR_INNER_CORNER	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	5.258	5.258	31.402	16.7%
T8	87.5	TWR_INNER_TRI	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.024	0.042	0.042	31.402	0.1%
T8	87.5	TWR_INNER_BRACE	T8 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.074	0.051	0.074	31.402	0.2%
T8	87.5	TWR_INNER_LADDER	T8 2L3x2 1/2x1/4x3/8	A307	0.75	2	3.221	3.089	3.221	44.588	7.2%
T9	62.5	TWR_LEG	T9 W10x68	A307	1	40	346.921	251.95	346.921	706.800	49.1%
T9	62.5	TWR_HORZ	T9 2L3x2 1/2x3/8x3/8	A307	0.75	4	32.833	33.068	33.068	99.402	33.3%
T9	62.5	TWR_DIAG	T9 2L4x3x1/2x3/8	A307	0.75	6	63.323	59.476	63.323	149.103	42.5%
T9	62.5	TWR_RED_HORZ_2	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.005	2.971	2.971	31.402	9.5%
T9	62.5	TWR_RED_HORZ_3	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.115	2.251	2.251	31.402	7.2%
T9	62.5	TWR_RED_DIAG_2	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	2.198	1.767	2.198	31.402	7.0%
T9	62.5	TWR_RED_DIAG_3	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.979	2.16	2.160	31.402	6.9%
T9	62.5	TWR_RED_HIP	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.088	0.213	0.213	31.402	0.7%
T9	62.5	TWR_RED_HIP_2	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	0.502	0.502	31.402	1.6%
T9	62.5	TWR_RED_HIPDIA	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.327	0.182	0.327	31.402	1.0%
T9	62.5	TWR_RED_HIPDIA_2	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.588	0	0.588	31.402	1.9%
T9	62.5	TWR_INNER_SUPP	T9 2L3x2 1/2x1/4x3/8	A307	0.75	2	2.735	2.791	2.791	44.588	6.3%
T9	62.5	TWR_INNER_SQ	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	3.244	5.112	5.112	31.402	16.3%
T9	62.5	TWR_INNER_CORNER	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0	5.728	5.728	31.402	18.2%
T9	62.5	TWR_INNER_TRI	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.026	0.046	0.046	31.402	0.1%
T9	62.5	TWR_INNER_BRACE	T9 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	0.082	0.058	0.082	31.402	0.3%
T9	62.5	TWR_INNER_LADDER	T9 2L3x2 1/2x1/4x3/8	A307	0.75	2	3.519	3.373	3.519	44.588	7.9%
T10	37.5	TWR_LEG	T10 W12x79	A307	1	56	424.926	316.876	424.926	883.600	48.1%
T10	37.5	TWR_HORZ	T10 2L4x3x1/2x3/8	A307	0.75	4	33.005	29.313	33.005	99.402	33.2%
T10	37.5	TWR_DIAG	T10 2L4x4x1/2x3/8	A307	0.75	8	82.105	74.432	82.105	198.804	41.3%
T10	37.5	TWR_RED_HORZ_2	T10 2L2 1/2x2 1/2x3/16x3/8	A307	0.75	2	1.383	0.586	1.383	31.402	4.4%
T10	37.5	TWR_RED_HORZ_3	T10 2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	1.444	0.892	1.444	41.869	3.4%
T10	37.5	TWR_RED_DIAG_2	T10 2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	0.464	1.444	1.444	41.869	3.4%
T10	37.5	TWR_RED_HORZ_4	T10 2L3x3x1/4x3/8	A307	0.75	2	1.032	1.688	1.688	44.588	3.8%
T10	37.5	TWR_RED_DIAG_3	T10 2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	0.599	1.58	1.580	41.869	3.8%
T10	37.5	TWR_RED_DIAG_4	T10 2L2 1/2x2 1/2x1/4x3/8	A307	0.75	2	2.143	1.545	2.143	41.869	5.1%
T10	37.5	TWR_RED_DIAG_5	T10 L2.5x2.5x8	A307	0.75	2	11.332	8.53	11.332	24.850	45.6%
T10	37.5	TWR_RED_HORZ_6	T10 L2.5x2.5x3	A307	0.75	2	6.647	9.2	9.200	15.701	58.6%
T10	37.5	TWR_RED_HIP	T10 LL4x4x8x3	A307	0.75	2	0.062	0.056	0.062	49.701	0.1%
T10	37.5	TWR_RED_HIP_3	T10 LL3x3x3x3	A307	0.75	2	0	0.557	0.557	33.441	

APPENDIX C

Additional Calculations



Self-Support Anchor Rod Analysis - TIA-222-H-1
TAG0053 - CHESHIRE
GPD Project #: 2023701.51

General Info	
Apply TIA-222-H Section 15.5	No
Modified Anchor Rods	No
Leg Eccentricity	No
Overstrength	No
Max Capacity	105%

Tower Reactions		
Compression, P_u =	516.74	kips
Compression Shear, V_u =	54.65	kips
Uplift, P_u =	389.52	kips
Uplift Shear, V_u =	46.99	kips
Number of Tower Legs =	4	
Tower Axial Force =	215.63	kips

Anchor Rods		
Number of Anchor Rods, n =	12	
Anchor Rod Grade =	C-1015	
Anchor Rod Diameter, d =	2.25	in
Bolt Circle Diameter, BC =	34	in
Rod Clear Span, l_{ar} =	0	in
Is grout present?	No	
Yield Strength, F_y =	47	ksi
Tensile Strength, F_u =	56	ksi
Rod Compression, P_{uc} =	43.06	kips
Rod Shear, V_u =	4.55	kips
Rod Moment, M_u =	0.00	k-in
Rod Tension, P_{ut} =	32.46	kips
Rod Shear, V_u =	3.92	kips
Rod Moment, M_u =	0.00	k-in

Anchor Rod Results		
$\phi_t R_{nt}$ =	136.50	kips
$\phi_c R_{nc}$ =	168.19	kips
$\phi_c R_{nb}$ =	168.19	kips
$\phi_v R_{nv}$ =	83.50	kips
$\phi_c R_{nvc}$ =	75.68	kips
$\phi_f M_n$ =	80.30	k-in
Tension Interaction	5.9%	OK
Compression Interaction	26.0%	OK

Concrete Column

Project File: 4 Pedestal Checks.ec6

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : IBC 2018

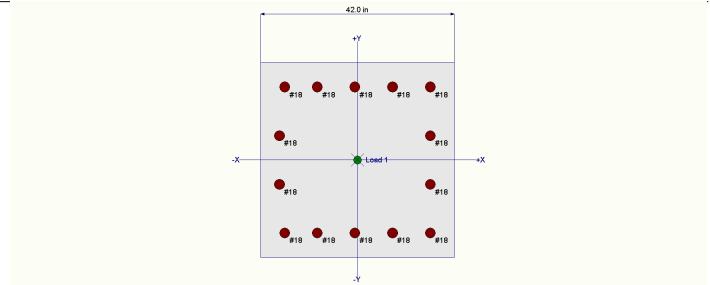
General Information

f'c : Concrete 28 day strength =	3.0 ksi	Overall Column Height =	6.20 ft
E =	3,122.0 ksi	End Fixity	Top Free, Bottom Fixed
Density =	150.0 pcf	Brace condition for deflection (buckling) along column	
β =	0.850	X-X (width) axis :	
fy - Main Rebar =	40.0 ksi	Unbraced Length for buckling ABOUT Y-Y Axis =	6.20 ft, K = 2.10
E - Main Rebar =	29,000.0 ksi	Y-Y (depth) axis :	
Allow. Reinforcing Limits	ASTM A615 Bars Used	Unbraced Length for buckling ABOUT X-X Axis =	6.20 ft, K = 2.10
Min. Reinf. =	1.0 %		
Max. Reinf. =	8.0 %		

Column Cross Section

Column Dimensions : 42.0in Square Column, Column
 Edge to Rebar Edge Cover = 4.125in

Column Reinforcing : 4 - #18 bars @ corners,, 3.0 - #18
 bars top & bottom between corner
 bars, 2.0 - #18 bars left & right



Entered loads are factored per load combinations specified by user.

Applied Loads

Column self weight included : 11,392.5 lbs * Dead Load Factor

AXIAL LOADS . . .

LC40 - Node 44: Axial Load at 6.20 ft above base, D = 89.072, W = 442.545 k

BENDING LOADS . . .

LC36 - Node 441: Lat. Point Load at 6.20 ft creating Mx-x, W = 50.538 k

Lat. Point Load at 6.20 ft creating My-y, W = 50.431 k

DESIGN SUMMARY

Load Combination	+1.20D+W	Maximum SERVICE Load Reactions .
Location of max.above base	6.158 ft	Top along Y-Y 0.0 k Bottom along Y-Y 50.431 k
Maximum Stress Ratio	0.227 : 1	Top along X-X 0.0 k Bottom along X-X 50.538 k
Ratio = (Pu ² +Mu ²) ^{0.5} / (PhiPn ² +PhiMn ²) ^{0.5}		Maximum SERVICE Load Deflections . .
Pu = 563.10 k ϕ * Pn = 2,476.44 k		Along Y-Y 0.008529 in at 6.20 ft above base
Mu-x = -313.336 k-ft ϕ * Mn-x = 1,402.99 k-ft		for load combination : W Only
Mu-y = -312.672 k-ft ϕ * Mn-y = 1,339.74 k-ft		Along X-X 0.008511 in at 6.20 ft above base
Mu Angle = 45.0 deg		for load combination : W Only
Mu at Angle = 442.655 k-ft ϕ Mn at Angle = 1,946.42 k-ft		General Section Information ϕ = 0.650 β = 0.850 θ = 0.80
<i>Pn & Mn values located at Pu-Mu vector intersection with capacity curve</i>		ρ : % Reinforcing 3.175 % Rebar % Ok
Column Capacities . .		Reinforcing Area 56.0 in ²
Pnmax : Nominal Max. Compressive Axial Capacity 6,595.40 k		Concrete Area 1,764.0 in ²
Pnmin : Nominal Min. Tension Axial Capacity k		
ϕ Pn, max : Usable Compressive Axial Capacity 3,429.61 k		
ϕ Pn, min : Usable Tension Axial Capacity k		

Concrete Column

Project File: 4 Pedestal Checks.ec6

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Governing Load Combination Results

Governing Factored Load Combination	Moment		Dist. from base ft	Axial Load k		Bending Analysis k-ft						Utilization Ratio	
	X-X	Y-Y		Pu	$\phi * Pn$	δx	$\delta x * Mux$	δy	$\delta y * Muy$	Alpha (deg)	δMu		ϕMn
+1.40D			6.16	140.65	3,429.61					0.000			0.041
+1.20D			6.16	120.56	3,429.61					0.000			0.035
+1.20D+0.50W	Actual	Actual	6.16	341.83	2,752.82	1.000	-156.67	1.000	-156.34	45.000	221.33	1,775.09	0.125
+1.20D+W	Actual	Actual	6.16	563.10	2,476.44	1.000	-313.34	1.000	-312.67	45.000	442.65	1,946.42	0.227
+0.90D+W	Actual	Actual	6.16	532.96	2,407.08	1.000	-313.34	1.000	-312.67	45.000	442.65	1,983.76	0.223
+0.90D			6.16	90.42	3,429.61					0.000			0.026

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction k		Y-Y Axis Reaction k		Axial Reaction @ Base	Mx - End Moments k-ft		My - End Moments k-ft	
	@ Base	@ Top	@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
D Only					100.465				
+D+0.60W	30.259		30.323		365.992	-188.001		-187.603	
+D+0.450W	22.694		22.742		299.610	-141.001		-140.702	
+0.60D+0.60W	30.259		30.323		325.806	-188.001		-187.603	
+0.60D					60.279				
W Only	50.431		50.538		442.545	-313.336		-312.672	

Maximum Moment Reactions

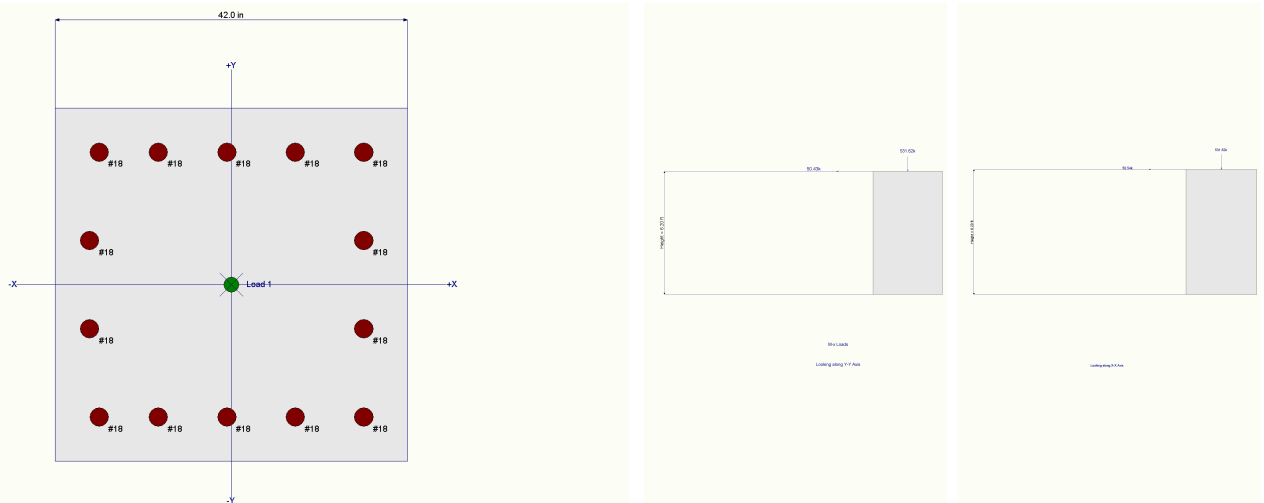
Note: Only non-zero reactions are listed.

Load Combination	Moment About X-X Axis @ Base		k-ft	Moment About Y-Y Axis @ Base		k-ft
	@ Base	@ Top		@ Base	@ Top	
D Only						
+D+0.60W	-188.001		k-ft	-187.603		k-ft
+D+0.450W	-141.001		k-ft	-140.702		k-ft
+0.60D+0.60W	-188.001		k-ft	-187.603		k-ft
+0.60D			k-ft			k-ft
W Only	-313.336		k-ft	-312.672		k-ft

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection		Distance	Max. Y-Y Deflection		Distance
	in	ft		in	ft	
D Only	0.0000	0.000	0.000	0.000	0.000	0.000
+D+0.60W	-0.0051	6.200	6.200	0.005	6.200	6.200
+D+0.450W	-0.0038	6.200	6.200	0.004	6.200	6.200
+0.60D+0.60W	-0.0051	6.200	6.200	0.005	6.200	6.200
+0.60D	0.0000	0.000	0.000	0.000	0.000	0.000
W Only	-0.0084	6.158	6.158	0.008	6.158	6.158

Sketches



Interaction Diagrams

Concrete Column

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Concrete Column

Project File: 4 Pedestal Checks.ec6

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Concrete Column

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Concrete Column

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

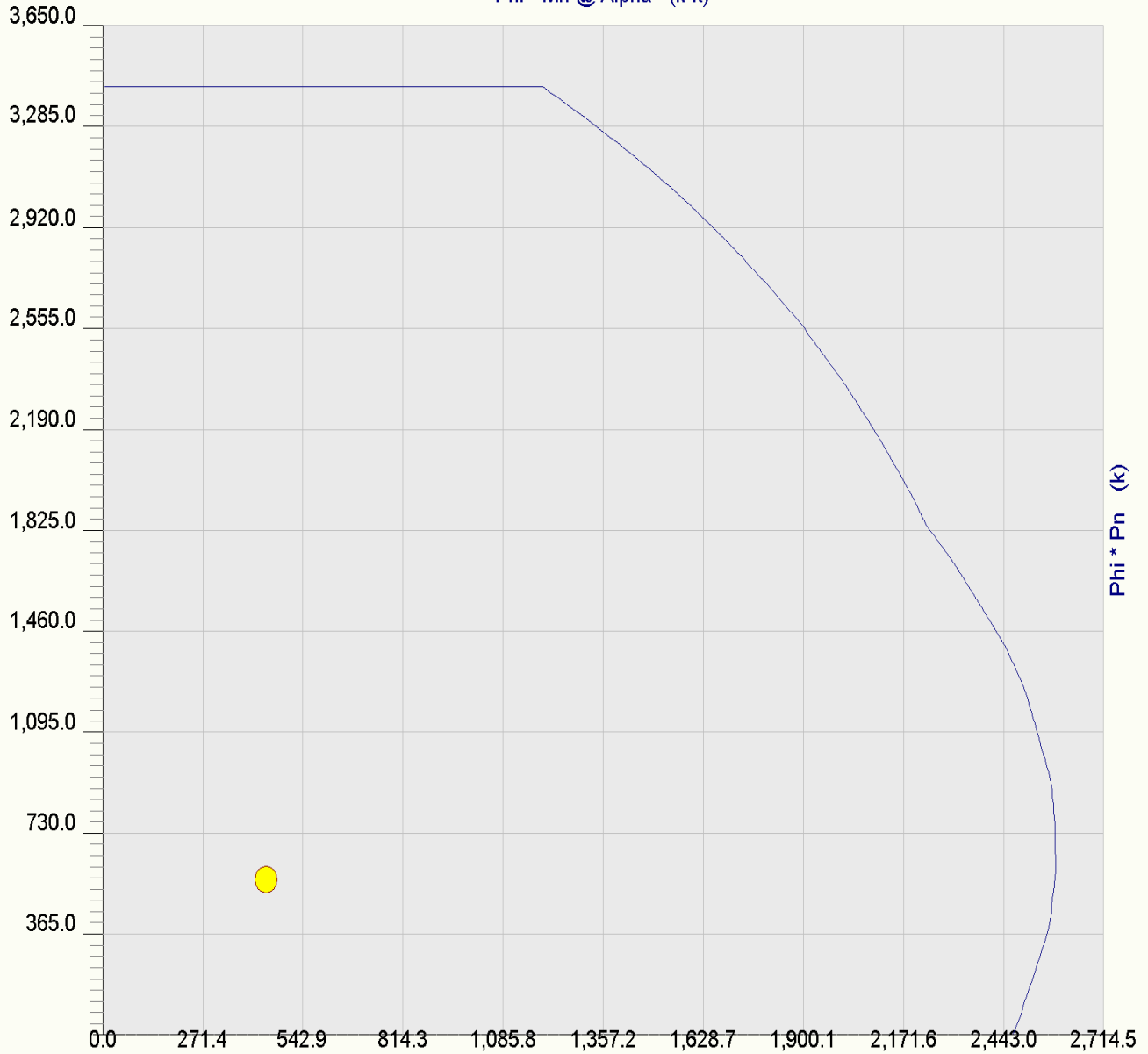
(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Load Comb. = +1.20D+W, Alpha= 45.0deg, (563.10, 442.65)

Concrete Column

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

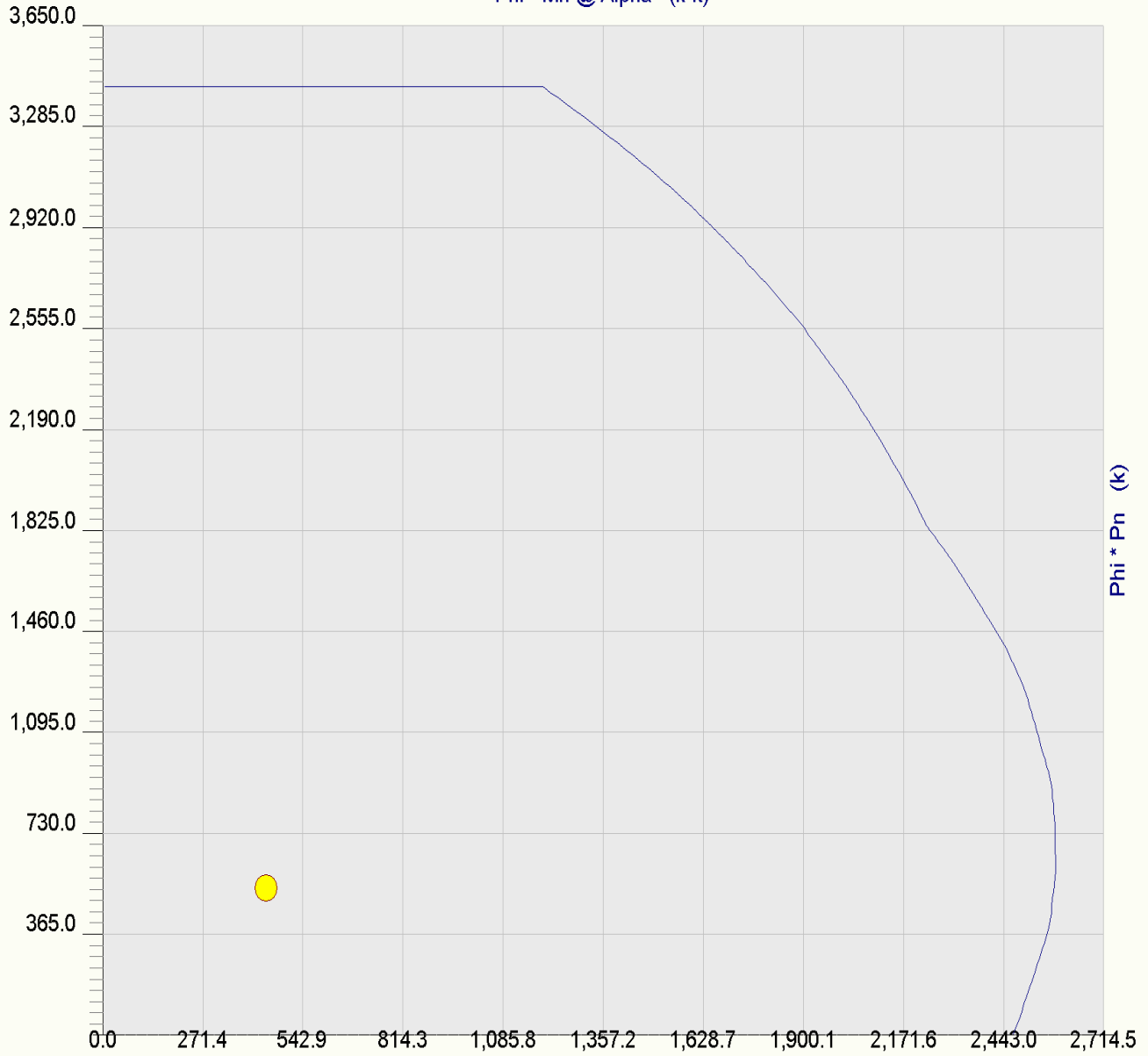
(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Load Comb. = +0.90D+W, Alpha= 45.0deg, (532.96, 442.65)

Concrete Column

Project File: 4 Pedestal Checks.ec6

LIC# : KW-06016111, Build:20.23.2.14

GPD ASSOCIATES

(c) ENERCALC INC 1983-2022

DESCRIPTION: Pedestal Analysis

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)

Phi * Pn (k)



Exhibit 4

February 17, 2023 (Rev.1)

February 16, 2023



Centerline Communications
750 West Center Street, Suite #301
West Bridgewater, MA 02379

RE: AT&T Site Number: CT2036 (LTE 6C)
FA Number: 10034996
PACE Number: MRCTB062236
PT Number: 2051A1479J
TEP Project Number: 359206
AT&T Site Name: CHESHIRE SW
Site Address: 751 Higgins Road
Cheshire, CT 06410

To Whom It May Concern:

TEP Northeast (TEP NE) has been authorized by Centerline Communications to perform a mount analysis on the existing AT&T antenna/RRH mounts to determine their capability of supporting the following additional loading (based on RFDS V2.00 dated 1/13/2023):

- (1) QD8616-7 Antennas (96.0"x22.0"x9.6" – Wt. = 150 lbs. /each)
- (2) QD6616-7 Antennas (72.0"x22.0"x9.6" – Wt. = 130 lbs. /each)
- (3) AIR6449 Antennas (30.6"x15.9"x10.6" – Wt. 82 lbs. /each)
- (3) AIR6419 Antennas (31.1"x16.1"x7.3" – Wt. = 66 lbs. /each)
- (1) DMP65R-BU8DA Antennas (96.0"x20.7"x7.7" – Wt. = 119 lbs. /each)
- (2) DMP65R-BU6DA Antennas (71.2"x20.7"x7.7" – Wt. = 96 lbs. /each)
- (3) 4478 B14 RRH's (18.1"x13.4"x8.3" – Wt. = 60 lbs. /each) (Pos. 2)
- (3) RRUS-32 B2 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each) (Pos. 2)
- (3) RRUS-32 B66A RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each) (Pos. 2)
- (3) 4449 B5/B12 RRH's (17.9"x13.2"x9.4" – Wt. = 73 lbs. /each) (Pos. 4)
- (3) RRUS-32 B30 RRH's (27.2"x12.1"x7.0" – Wt. = 60 lbs. /each) (Pos. 4)
- (3) DC9-48-60-24-8C-EV Surge Arrestors (31.4"x10.2" Ø – Wt. = 29 lbs.) (Pos. 4)
- **(3) 2012 B29 RRH's (16.5"x13.5"x5.9" – Wt. = 43 lbs. /each) (Pos. 2)**

**Proposed equipment shown in bold.*

No original structural design documents or fabrication drawings were available for the existing mounts. Previous Mount Mapping Report prepared by Provertic, LLC dated July 20, 2022, was used to perform this analysis.

Mount Analysis Methods:

- This analysis was conducted in accordance with EIA/TIA-222-H, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures, the International Building Code 2021 with 2022 Connecticut State Building Code, and AT&T Mount Technical Directive – R22.
- TEP NE considers this mount to be asymmetrical and has applied wind loads in 30 degree increments all around the mount. Per TIA-222-H and Appendix P of the Connecticut State Building Code, the max basic wind speed for this site is equal to 120 mph with a max basic wind speed with ice of 50 mph and a max ice thickness of 1.0 in. An escalated ice thickness of 1.23 in was used for this analysis.
- TEP NE considers this site to be exposure category B; tower is located in an urban/suburban or wooded area with numerous closely spaced obstructions.
- TEP NE considers this site to be topographic category 1; tower is located on flat terrain or the bottom of a hill or ridge.
- TEP NE considers this site to have a spectral response acceleration parameter at short periods, S_s , of 0.200 and a spectral response acceleration parameter at a period of 1 second, S_1 , of 0.054.
- The existing mounts are secured to the existing self supporting tower with threaded rods and steel plates plate clamps ubolts tightened around the existing catwalk handrail system. TEP NE considers the threaded rods as the governing connection members.

Based on the mapping data from the Mount Mapping Rerpot prepared by Provertic, LLC dated July 20, 2022, TEP NE discovered some discrepancies from the previous Hudson Design Group Mount Analysis Report. Based on our evaluation, we have determined that the existing mounts **ARE CAPABLE** of supporting the proposed installation with the following modifications:

- **Reinforce existing handrail steel angle with proposed L2-1/2x2-1/2x1/4 steel angle (total of 1 per Alpha sector).**
- **Install proposed 2-1/2" x-strong (2.88" O.D.) pipe mast behind existing DMP65R-BU6DA antenna and TPA65R-BU8DA-K antenna secured to the existing mount (total of 2 per Alpha sector).**
- **Replace existing 2-1/2" (2.88" O.D.) horizontal face pipe with proposed 3" std. (3.5" O.D.) horizontal face pipe secured to the existing mount (total of 1 per Beta sector).**

	Component	Controlling Load Case	Stress Ratio	Pass/Fail
Modified Alpha Sector Mount Rating	16	LC7	88%	PASS
Modified Beta Sector Mount Rating	104	LC7	91%	PASS
Existing Gamma Sector Mount Rating	12	LC6	67%	PASS

Reference Documents:

- Mount Mapping Report prepared by Provertic, LLC dated July 20, 2022.

This determination was based on the following limitations and assumptions:

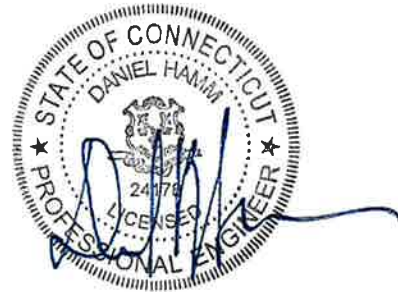
1. TEP NE is not responsible for any modifications completed prior to and hereafter which TEP NE was not directly involved.
2. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
3. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer's requirements.
4. The existing mounts have been adequately secured to the tower structure per the mount manufacturer's specifications.
5. All components pertaining to AT&T's mounts must be tightened and re-plumbed prior to the installation of new appurtenances.
6. TEP NE performed a localized analysis on the mounts itself and not on the supporting tower structure.

Please feel free to contact our office should you have any questions.

Respectfully Submitted,
TEP Northeast



Michael Cabral
Director



Daniel P. Hamm, PE
Vice President

FIELD PHOTOS:





**Wind & Ice
Calculations**

Date: 1/6/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: JC Checked By: MSC



2.6.5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$z = 255$ (ft)
 $z_g = 1200$ (ft)
 $\alpha = 7.0$

$K_z = 1.291$

$K_{zmin} \leq K_z \leq 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_c
B	1200 ft	7.0	0.70	0.9
C	900 ft	9.5	0.85	1.0
D	700 ft	11.5	1.03	1.1

2.6.6.2 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2.0
4	0.72	1.5

$$K_{zt} = [1 + (K_c K_t / K_h)]^2$$

$$K_h = e^{(fz/H)}$$

$K_{zt} = 1$

(If Category 1 then $K_{zt} = 1.0$)

Category = 1

$K_h = 1$

$K_c = 0.9$ (from Table 2-4)

$K_t = 0$ (from Table 2-5)

$f = 0$ (from Table 2-5)

$z = 255$

$z_s = 280$ (Mean elevation of base of structure above sea level)

$H = 0$ (Ht. of the crest above surrounding terrain)

$K_{zt} = 1.00$ (from 2.6.6.2.1)

$K_e = 0.99$ (from 2.6.8)

2.6.10 Design Ice Thickness

Max Ice Thickness =
 Importance Factor =

$t_i = 1.00$ in

$I = 1.00$ (from Table 2-3)

$K_{iz} = 1.23$ (from Sec. 2.6.10)

$$t_{iz} = t_i * I * K_{iz} * (K_{zt})^{0.35}$$

$t_{iz} = 1.23$ in

Date: 1/6/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: JC Checked By: MSC



2.6.9 Gust Effect Factor

2.6.9.1 Self Supporting Lattice Structures

$G_h = 1.0$ Latticed Structures > 600 ft

$G_h = 0.85$ Latticed Structures 450 ft or less

$G_h = 0.85 + 0.15 [h/150 - 3.0]$

$h =$ ht. of structure

$h =$ 250

$G_h =$ 0.85

2.6.9.2 Guyed Masts

$G_h =$ 0.85

2.6.9.3 Pole Structures

$G_h =$ 1.1

2.6.9 Appurtenances

$G_h =$ 1.0

2.6.9.4 Structures Supported on Other Structures

(Cantilevered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5)

$G_h =$ 1.35

$G_h =$ 1.00

2.6.11.2 Design Wind Force on Appurtenances

$F = q_z * G_h * (EPA)_A$

$q_z = 0.00256 * K_z * K_{zt} * K_s * K_e * K_d * V_{max}^2$

$q_z =$	40.05
$q_z (ice) =$	6.95
$q_z (30) =$	2.50

$K_z =$	1.291 (from 2.6.5.2)
$K_{zt} =$	1.0 (from 2.6.6.2.1)
$K_s =$	1.0 (from 2.6.7)
$K_e =$	0.99 (from 2.6.8)
$K_d =$	0.85 (from Table 2-2)
$V_{max} =$	120 mph (Ultimate Wind Speed)
$V_{max (ice)} =$	50 mph
$V_{30} =$	30 mph

Table 2-2

Structure Type	Wind Direction Probability Factor, K_d
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances	0.95
Tubular pole structures supporting antennas enclosed within a cylindrical shroud	1.00

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Determine Ca:

Table 2-9

Force Coefficients (Ca) for Appurtenances			
Member Type	Aspect Ratio ≤ 2.5	Aspect Ratio = 7	Aspect Ratio ≥ 25
	Ca	Ca	Ca
Flat	1.2	1.4	2.0
Square/Rectangular HSS	1.2 - 2.8(r _s) ≥ 0.85	1.4 - 4.0(r _s) ≥ 0.90	2.0 - 6.0(r _s) ≥ 1.25
Round	C < 39 (Subcritical)	0.7	0.8
	39 ≤ C ≤ 78 (Transitional)	4.14/(C ^{0.485})	3.66/(C ^{0.415})
	C > 78 (Supercritical)	0.5	0.6

Aspect Ratio is the overall length/width ratio in the plane normal to the wind direction.
 (Aspect ratio is independent of the spacing between support points of a linear appurtenance,
 Note: Linear interpolation may be used for aspect ratios other than those shown.

Ice Thickness = **1.23 in** **Angle = 0 (deg)** **Equivalent Angle = 180 (deg)**

Appurtenances	Height	Width	Depth	Flat Area	Aspect Ratio	Ca	Force (lbs)	Force (lbs) (w/ Ice)	Force (lbs) (30 mph)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	4.36	1.28	754	149	47
QD6616-7 Antenna	72.0	22.0	9.6	11.00	3.27	1.23	544	109	34
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.93	1.20	167	36	10
AIR6449 Antenna	30.6	15.9	10.6	3.38	1.92	1.20	162	35	10
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	4.64	1.30	716	143	45
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.44	1.24	509	102	32
4478 B14 RRH	18.1	13.4	8.3	1.68	1.35	1.20	81	19	5
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	2.18	1.20	50	13	3
RRUS-32 RRH	27.2	12.1	7.0	2.29	2.25	1.20	110	25	7
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	3.89	1.26	67	17	4
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	0.00	1.20	0	4	0
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.36	1.20	79	18	5
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.90	1.20	56	14	4
2012 B29 RRH	16.5	13.5	5.9	1.55	1.22	1.20	74	18	5
Surge Arrestor	31.4	10.2	10.2	2.22	3.08	0.70	62	14	4
5x2-3/4 Angle	2.8	12.0		0.23	0.23	2.00		18	
3x3 Angle	3.0	12.0		0.25	0.25	2.00		20	
2-1/2x2-1/2 Angle	2.5	12.0		0.21	0.21	2.00		17	
PL 2x1/2	2.0	12.0		0.17	0.17	2.00		13	
HSS 3x3	3.0	12.0		0.25	0.25	1.25		13	
3" Pipe	3.5	12.0		0.29	0.29	1.20		14	
2-1/2" Pipe	2.9	12.0		0.24	0.24	1.20		12	
2" Pipe	2.4	12.0		0.20	0.20	1.20		10	

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WIND LOADS

Angle = 30 (deg) Ice Thickness = 1.23 in. Equivalent Angle = 210 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Aspect Ratio	Aspect Ratio	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	754	385	661
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	544	272	476
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	167	81	146
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	162	110	149
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	716	325	618
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	509	225	438
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	81	50	73
4478 B14 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	41	81	51
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	110	67	99
RRUS-32 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	59	110	72
RRUS-32 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	34	67	42
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	79	56	73
4449 B5/B12 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	40	79	50
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	74	33	64

WIND LOADS WITH ICE:

QD8616-7 Antenna	98.5	24.5	12.1	16.72	8.24	4.03	8.17	1.27	1.44	147	82	131
QD6616-7 Antenna	74.5	24.5	12.1	12.64	6.23	3.04	6.18	1.22	1.36	108	59	95
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	32
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	33
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
4478 B14 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	17
4478 B14 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	14
RRUS-32 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	19
RRUS-32 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	8
4449 B5/B12 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	17
4449 B5/B12 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	15
2012 B29 RRH	19.0	16.0	8.4	2.10	1.10	1.19	2.27	1.20	1.20	18	9	15

WIND LOADS AT 30 MPH:

QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	47	24	41
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	34	17	30
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	9
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	9
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	5
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	4
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	5
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	1
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	5
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	4
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	5	2	4

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 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 60 (deg) Ice Thickness = 1.23 in. Equivalent Angle = 240 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	754	385	477
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	544	272	340
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	167	81	102
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	162	110	123
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	716	325	423
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	509	225	296
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	81	50	58
4478 B14 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	61	81	76
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	110	67	78
RRUS-32 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	84	110	103
RRUS-32 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	65	67	66
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	79	56	62
4449 B5/B12 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	59	79	74
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	74	33	43

WIND LOADS WITH ICE:

QD8616-7 Antenna	98.5	24.5	12.1	16.72	8.24	4.03	8.17	1.27	1.44	147	82	99
QD6616-7 Antenna	74.5	24.5	12.1	12.64	6.23	3.04	6.18	1.22	1.36	108	59	71
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	24
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	28
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
4478 B14 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	14
4478 B14 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	17
RRUS-32 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	23
RRUS-32 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	14
4449 B5/B12 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	15
4449 B5/B12 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	17
2012 B29 RRH	19.0	16.0	8.4	2.10	1.10	1.19	2.27	1.20	1.20	18	9	11

WIND LOADS AT 30 MPH:

QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	47	24	30
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	34	17	21
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	6
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	8
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	4
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	5
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	6
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	3
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	5
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	5	2	3

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 Project No.: CT2036
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = **90** (deg) Ice Thickness = **1.23** in. Equivalent Angle = **270** (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	754	385	385
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	544	272	272
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	167	81	81
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	162	110	110
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	716	325	325
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	509	225	225
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	81	50	50
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	50	81	81
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	110	67	67
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	67	110	110
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	67	67
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	79	56	56
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	56	79	79
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	74	33	33

WIND LOADS WITH ICE:

QD8616-7 Antenna	98.5	24.5	12.1	16.72	8.24	4.03	8.17	1.27	1.44	147	82	82
QD6616-7 Antenna	74.5	24.5	12.1	12.64	6.23	3.04	6.18	1.22	1.36	108	59	59
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	20
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	25
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	72
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	51
4478 B14 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	13
4478 B14 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	19
RRUS-32 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	17
RRUS-32 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	25
RRUS-32 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	17
4449 B5/B12 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	14
4449 B5/B12 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	18
2012 B29 RRH	19.0	16.0	8.4	2.10	1.10	1.19	2.27	1.20	1.20	18	9	9

WIND LOADS AT 30 MPH:

QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	47	24	24
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	34	17	17
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	5
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	7
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	20
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	14
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	3
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	5
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	4
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	7
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	4
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	5
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	5	2	2

Date: 1/6/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 120 (deg) Ice Thickness = 1.23 in. Equivalent Angle = 300 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	754	385	477
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	544	272	340
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	167	81	102
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	162	110	123
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	716	325	423
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	509	225	296
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	81	50	58
4478 B14 RRH (Side)	18.1	10.1	13.4	1.26	1.68	1.80	1.35	1.20	1.20	61	81	76
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	110	67	78
RRUS-32 RRH (Side)	27.2	9.1	12.1	1.71	2.29	3.00	2.25	1.22	1.20	84	110	103
RRUS-32 RRH (Shielded)	27.2	6.8	7.0	1.29	1.32	4.00	3.89	1.27	1.26	65	67	66
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	79	56	62
4449 B5/B12 RRH (Side)	17.9	9.9	13.2	1.23	1.64	1.81	1.36	1.20	1.20	59	79	74
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	74	33	43

WIND LOADS WITH ICE:

QD8616-7 Antenna	98.5	24.5	12.1	16.72	8.24	4.03	8.17	1.27	1.44	147	82	99
QD6616-7 Antenna	74.5	24.5	12.1	12.64	6.23	3.04	6.18	1.22	1.36	108	59	71
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	24
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	28
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	89
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	63
4478 B14 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	14
4478 B14 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	17
RRUS-32 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	19
RRUS-32 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	23
RRUS-32 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	14
4449 B5/B12 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	15
4449 B5/B12 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	17
2012 B29 RRH	19.0	16.0	8.4	2.10	1.10	1.19	2.27	1.20	1.20	18	9	11

WIND LOADS AT 30 MPH:

QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	47	24	30
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	34	17	21
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	6
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	8
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	26
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	18
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	4
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	5
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	5
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	6
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	3
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	4
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	5
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	5	2	3

Date: 1/6/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: JC Checked By: MSC



WIND LOADS

Angle = 150 (deg) Ice Thickness = 1.23 in. Equivalent Angle = 330 (deg)

WIND LOADS WITH NO ICE:

Appurtenances	Height	Width	Depth	Flat Area (normal)	Flat Area (side)	Ratio (normal)	Ratio (side)	Ca (normal)	Ca (side)	Force (lbs)	Force (lbs)	Force (lbs)
QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	754	385	661
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	544	272	476
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	167	81	146
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	162	110	149
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	716	325	618
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	509	225	438
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	81	50	73
4478 B14 RRH (Side)	18.1	6.7	13.4	0.84	1.68	2.70	1.35	1.21	1.20	41	81	51
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	110	67	99
RRUS-32 RRH (Side)	27.2	6.1	12.1	1.14	2.29	4.50	2.25	1.29	1.20	59	110	72
RRUS-32 RRH (Shielded)	27.2	3.0	7.0	0.57	1.32	8.99	3.89	1.47	1.26	34	67	42
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	79	56	73
4449 B5/B12 RRH (Side)	17.9	6.6	13.2	0.82	1.64	2.71	1.36	1.21	1.20	40	79	50
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	74	33	64

WIND LOADS WITH ICE:

QD8616-7 Antenna	98.5	24.5	12.1	16.72	8.24	4.03	8.17	1.27	1.44	147	82	131
QD6616-7 Antenna	74.5	24.5	12.1	12.64	6.23	3.04	6.18	1.22	1.36	108	59	95
AIR6419 Antenna	33.6	18.6	9.8	4.32	2.27	1.81	3.44	1.20	1.24	36	20	32
AIR6449 Antenna	33.1	18.4	13.1	4.21	3.00	1.80	2.53	1.20	1.20	35	25	33
DMP65R-BU8DA Antenna	98.5	23.2	10.2	15.83	6.94	4.25	9.70	1.28	1.49	141	72	123
DMP65R-BU6DA Antenna	73.7	23.2	10.2	11.84	5.19	3.18	7.25	1.23	1.41	101	51	89
4478 B14 RRH	20.6	15.9	10.8	2.26	1.53	1.30	1.91	1.20	1.20	19	13	17
4478 B14 RRH (Side)	20.6	10.8	15.9	1.53	2.26	1.91	1.30	1.20	1.20	13	19	14
RRUS-32 RRH	29.7	14.6	9.5	3.00	1.95	2.04	3.14	1.20	1.23	25	17	23
RRUS-32 RRH (Side)	29.7	9.5	14.6	1.95	3.00	3.14	2.04	1.23	1.20	17	25	19
RRUS-32 RRH (Shielded)	29.7	2.5	9.5	0.51	1.95	12.09	3.14	1.57	1.23	6	17	8
4449 B5/B12 RRH	20.4	15.7	11.9	2.21	1.68	1.30	1.72	1.20	1.20	18	14	17
4449 B5/B12 RRH (Side)	20.4	11.9	15.7	1.68	2.21	1.72	1.30	1.20	1.20	14	18	15
2012 B29 RRH	19.0	16.0	8.4	2.10	1.10	1.19	2.27	1.20	1.20	18	9	15

WIND LOADS AT 30 MPH:

QD8616-7 Antenna	96.0	22.0	9.6	14.67	6.40	4.36	10.00	1.28	1.50	47	24	41
QD6616-7 Antenna	72.0	22.0	9.6	11.00	4.80	3.27	7.50	1.23	1.42	34	17	30
AIR6419 Antenna	31.1	16.1	7.3	3.48	1.58	1.93	4.26	1.20	1.28	10	5	9
AIR6449 Antenna	30.6	15.9	10.6	3.38	2.25	1.92	2.89	1.20	1.22	10	7	9
DMP65R-BU8DA Antenna	96.0	20.7	7.7	13.80	5.13	4.64	12.47	1.30	1.58	45	20	39
DMP65R-BU6DA Antenna	71.2	20.7	7.7	10.24	3.81	3.44	9.25	1.24	1.47	32	14	27
4478 B14 RRH	18.1	13.4	8.3	1.68	1.04	1.35	2.18	1.20	1.20	5	3	5
4478 B14 RRH (Side)	18.1	8.3	13.4	1.04	1.68	2.18	1.35	1.20	1.20	3	5	4
RRUS-32 RRH	27.2	12.1	7.0	2.29	1.32	2.25	3.89	1.20	1.26	7	4	6
RRUS-32 RRH (Side)	27.2	7.0	12.1	1.32	2.29	3.89	2.25	1.26	1.20	4	7	5
RRUS-32 RRH (Shielded)	27.2	0.0	7.0	0.00	1.32	0.00	3.89	1.20	1.26	0	4	1
4449 B5/B12 RRH	17.9	13.2	9.4	1.64	1.17	1.36	1.90	1.20	1.20	5	4	5
4449 B5/B12 RRH (Side)	17.9	9.4	13.2	1.17	1.64	1.90	1.36	1.20	1.20	4	5	4
2012 B29 RRH	16.5	13.5	5.9	1.55	0.68	1.22	2.80	1.20	1.21	5	2	4

Date: 1/6/2023

Project Name: CHESHIRE SW

Project No.: CT2036

Designed By: JC Checked By: MSC



ICE WEIGHT CALCULATIONS

Thickness of ice: 1.23 in.
Density of ice: 56 pcf

QD8616-7 Antenna

Weight of ice based on total radial SF area:
Height (in): 96.0
Width (in): 22.0
Depth (in): 9.6
Total weight of ice on object: 303 lbs
Weight of object: 150.0 lbs
Combined weight of ice and object: 453 lbs

QD6616-7 Antenna

Weight of ice based on total radial SF area:
Height (in): 72.0
Width (in): 22.0
Depth (in): 9.6
Total weight of ice on object: 228 lbs
Weight of object: 130.0 lbs
Combined weight of ice and object: 358 lbs

AIR6419 Antenna

Weight of ice based on total radial SF area:
Height (in): 31.1
Width (in): 16.1
Depth (in): 7.3
Total weight of ice on object: 74 lbs
Weight of object: 66.0 lbs
Combined weight of ice and object: 140 lbs

AIR6449 Antenna

Weight of ice based on total radial SF area:
Height (in): 30.6
Width (in): 15.9
Depth (in): 10.6
Total weight of ice on object: 78 lbs
Weight of object: 82.0 lbs
Combined weight of ice and object: 160 lbs

DMP65R-BU8DA Antenna

Weight of ice based on total radial SF area:
Height (in): 96.0
Width (in): 20.7
Depth (in): 7.7
Total weight of ice on object: 280 lbs
Weight of object: 119.0 lbs
Combined weight of ice and object: 399 lbs

DMP65R-BU6DA Antenna

Weight of ice based on total radial SF area:
Height (in): 71.2
Width (in): 20.7
Depth (in): 7.7
Total weight of ice on object: 208 lbs
Weight of object: 80.0 lbs
Combined weight of ice and object: 288 lbs

4478 B14 RRH

Weight of ice based on total radial SF area:
Height (in): 18.1
Width (in): 13.4
Depth (in): 8.3
Total weight of ice on object: 39 lbs
Weight of object: 60.0 lbs
Combined weight of ice and object: 99 lbs

RRUS-32 RRH

Weight of ice based on total radial SF area:
Height (in): 27.2
Width (in): 12.1
Depth (in): 7.0
Total weight of ice on object: 52 lbs
Weight of object: 60.0 lbs
Combined weight of ice and object: 112 lbs

4449 B5/B12 RRH

Weight of ice based on total radial SF area:
Height (in): 17.9
Width (in): 13.2
Depth (in): 9.4
Total weight of ice on object: 39 lbs
Weight of object: 73.0 lbs
Combined weight of ice and object: 112 lbs

2012 B29 RRH

Weight of ice based on total radial SF area:
Height (in): 16.5
Width (in): 13.5
Depth (in): 5.9
Total weight of ice on object: 33 lbs
Weight of object: 43.0 lbs
Combined weight of ice and object: 76 lbs

Date: 1/6/2023

Project Name: CHESHIRE SW

Project No.: CT2036

Designed By: JC Checked By: MSC



Squid Surge Arrestor

Weight of ice based on total radial SF area:

Depth (in): 31.4

Diameter(in): 10.2

Total weight of ice on object: 45 lbs

Weight of object: 29 lbs

Combined weight of ice and object: 74 lbs

L 5x2-3/4 Angles

Weight of ice based on total radial SF area:

Height (in): 2.75

Width (in): 5

Per foot weight of ice on object: 10 plf

L 3x3 Angles

Weight of ice based on total radial SF area:

Height (in): 3

Width (in): 3

Per foot weight of ice on object: 8 plf

PL 2x1/2

Weight of ice based on total radial SF area:

Height (in): 2

Width (in): 0.25

Per foot weight of ice on object: 5 plf

L 2-1/2x2-1/2 Angles

Weight of ice based on total radial SF area:

Height (in): 2.5

Width (in): 2.5

Per foot weight of ice on object: 7 plf

HSS 3x3

Weight of ice based on total radial SF area:

Height (in): 3

Width (in): 3

Per foot weight of ice on object: 8 plf

2" pipe

Per foot weight of ice:

diameter (in): 2.38

Per foot weight of ice on object: 5 plf

2-1/2" pipe

Per foot weight of ice:

diameter (in): 2.88

Per foot weight of ice on object: 6 plf

3" Pipe

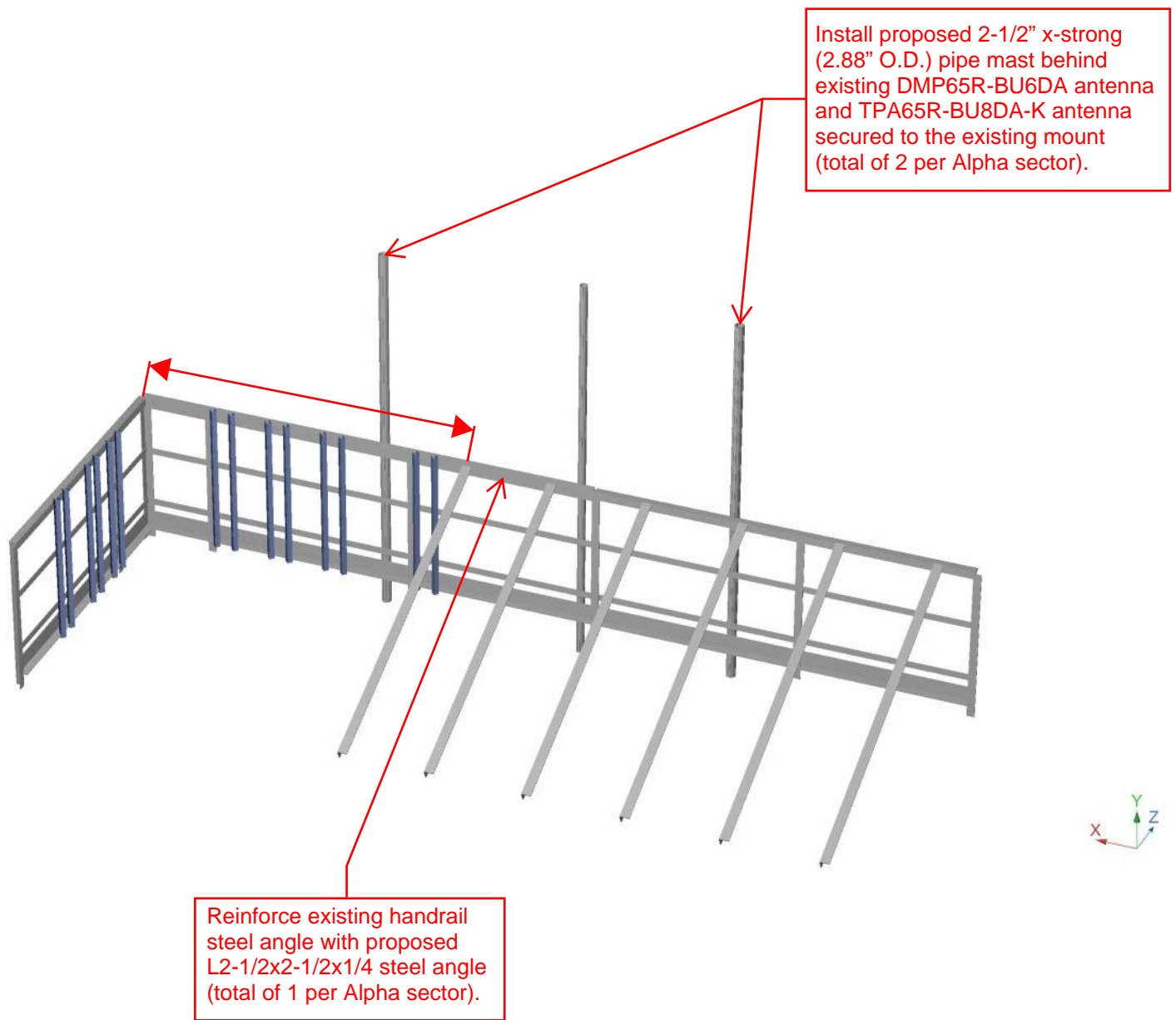
Per foot weight of ice:

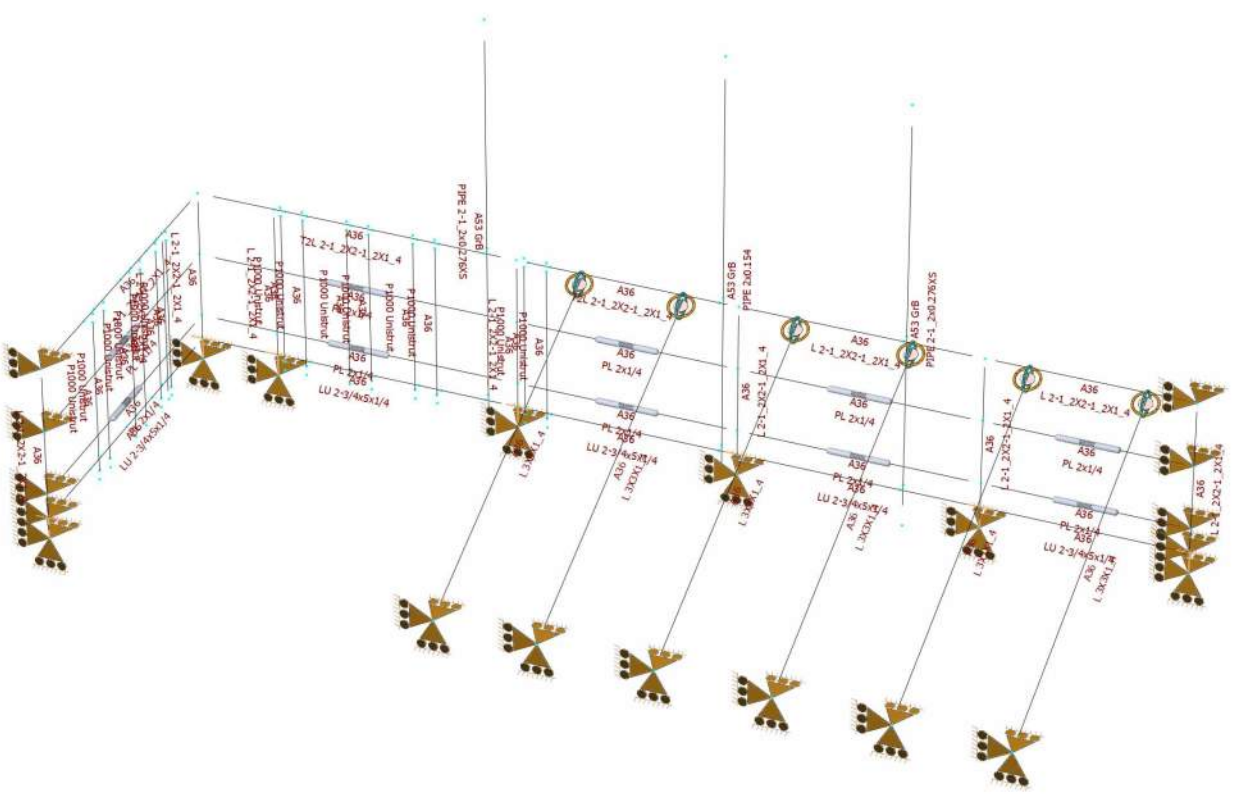
diameter (in): 3.5

Per foot weight of ice on object: 7 plf



Modified Alpha Sector Calculations

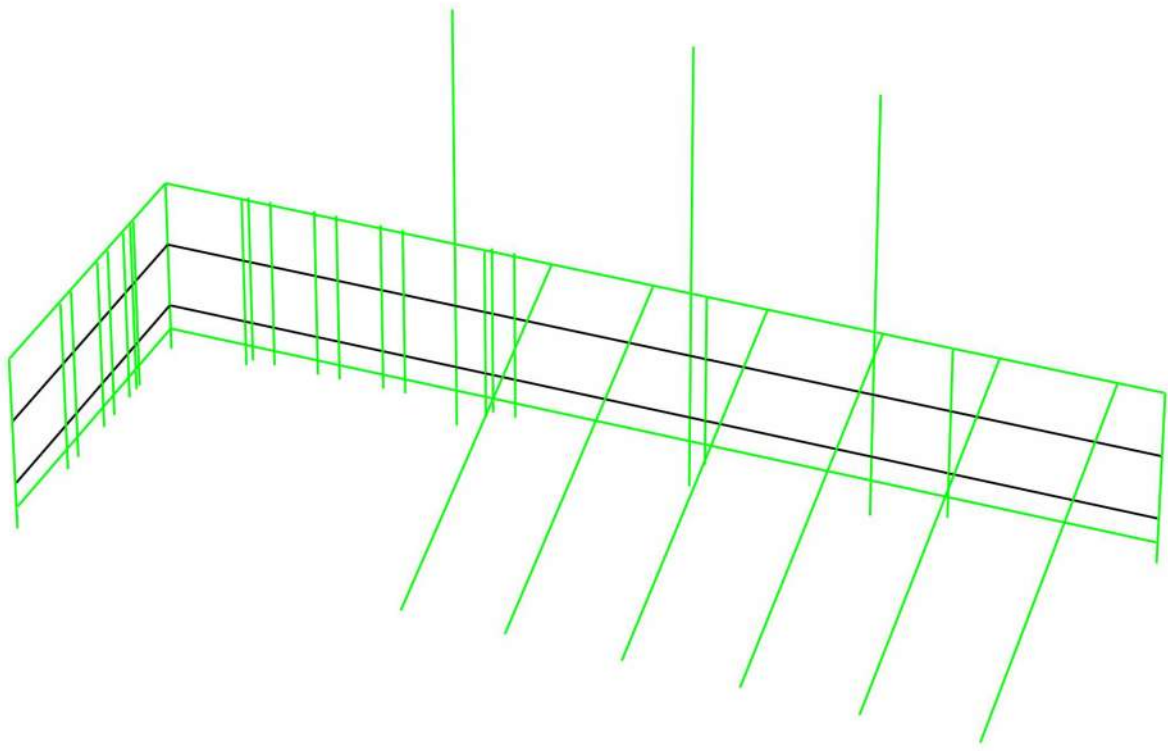


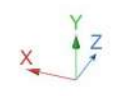
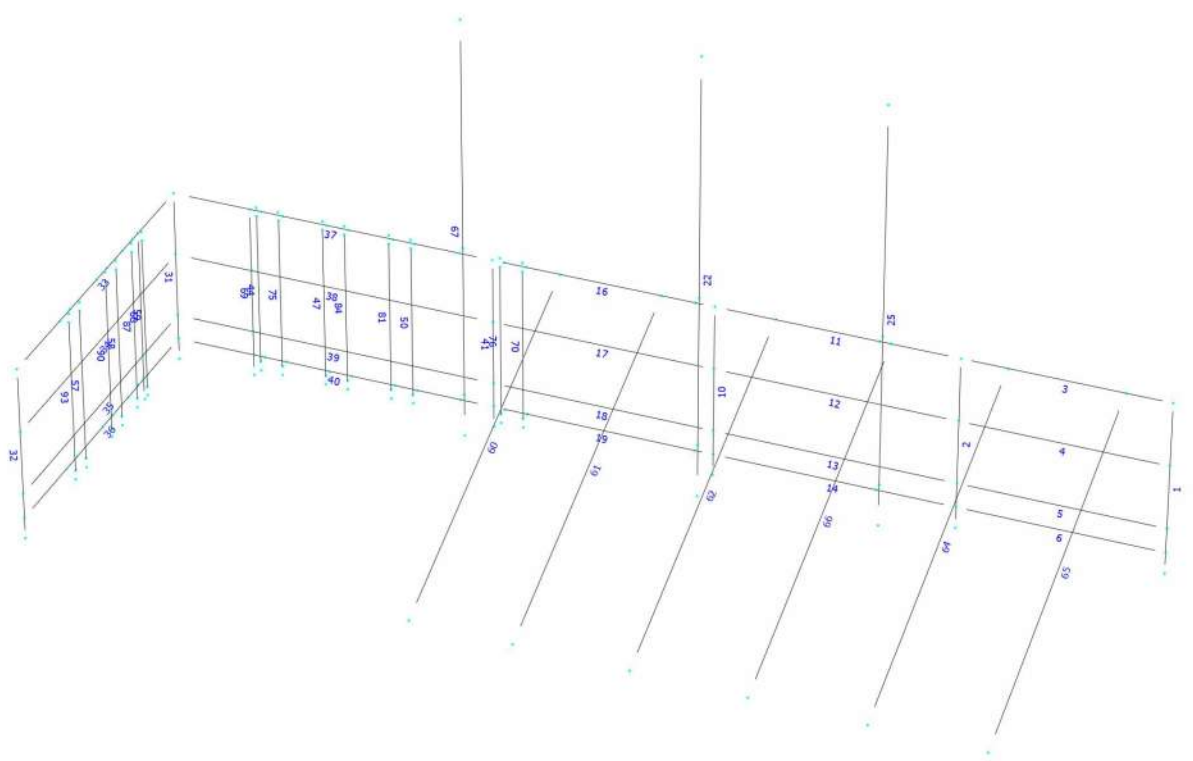




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Load data

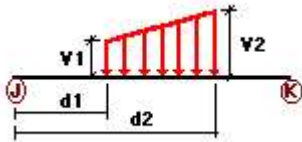
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	1	z	-0.017	0.00	0.00	No	0.00	No
	2	z	-0.017	0.00	0.00	No	0.00	No
	3	z	-0.017	0.00	0.00	No	0.00	No
	4	z	-0.013	0.00	0.00	No	0.00	No
	5	z	-0.013	0.00	0.00	No	0.00	No
	6	z	-0.018	0.00	0.00	No	0.00	No
	10	z	-0.017	0.00	0.00	No	0.00	No
	11	z	-0.017	0.00	0.00	No	0.00	No
	12	z	-0.013	0.00	0.00	No	0.00	No
	13	z	-0.013	0.00	0.00	No	0.00	No

W30

14	z	-0.018	0.00	0.00	No	0.00	No
16	z	-0.017	0.00	0.00	No	0.00	No
17	z	-0.013	0.00	0.00	No	0.00	No
18	z	-0.013	0.00	0.00	No	0.00	No
19	z	-0.018	0.00	0.00	No	0.00	No
31	z	-0.017	0.00	0.00	No	0.00	No
37	z	-0.017	0.00	0.00	No	0.00	No
38	z	-0.013	0.00	0.00	No	0.00	No
39	z	-0.013	0.00	0.00	No	0.00	No
40	z	-0.018	0.00	0.00	No	0.00	No
41	z	-0.017	0.00	0.00	No	0.00	No
44	z	-0.007	0.00	0.00	No	0.00	No
47	z	-0.007	0.00	0.00	No	0.00	No
50	z	-0.007	0.00	0.00	No	0.00	No
57	z	-0.007	0.00	0.00	No	0.00	No
58	z	-0.007	0.00	0.00	No	0.00	No
59	z	-0.007	0.00	0.00	No	0.00	No
60	z	-0.02	0.00	0.00	No	0.00	No
61	z	-0.02	0.00	0.00	No	0.00	No
62	z	-0.02	0.00	0.00	No	0.00	No
64	z	-0.02	0.00	0.00	No	0.00	No
65	z	-0.02	0.00	0.00	No	0.00	No
66	z	-0.02	0.00	0.00	No	0.00	No
69	z	-0.017	0.00	0.00	No	0.00	No
70	z	-0.007	0.00	0.00	No	0.00	No
75	z	-0.007	0.00	0.00	No	0.00	No
76	z	-0.007	0.00	0.00	No	0.00	No
81	z	-0.007	0.00	0.00	No	0.00	No
84	z	-0.007	0.00	0.00	No	0.00	No
87	z	-0.007	0.00	0.00	No	0.00	No
90	z	-0.007	0.00	0.00	No	0.00	No
93	z	-0.007	0.00	0.00	No	0.00	No
1	z	-0.017	0.00	0.00	No	0.00	No
2	z	-0.017	0.00	0.00	No	0.00	No
3	z	-0.017	0.00	0.00	No	0.00	No
4	z	-0.013	0.00	0.00	No	0.00	No
5	z	-0.013	0.00	0.00	No	0.00	No
6	z	-0.018	0.00	0.00	No	0.00	No
10	z	-0.017	0.00	0.00	No	0.00	No
11	z	-0.017	0.00	0.00	No	0.00	No
12	z	-0.013	0.00	0.00	No	0.00	No
13	z	-0.013	0.00	0.00	No	0.00	No
14	z	-0.018	0.00	0.00	No	0.00	No
16	z	-0.017	0.00	0.00	No	0.00	No
17	z	-0.013	0.00	0.00	No	0.00	No
18	z	-0.013	0.00	0.00	No	0.00	No
19	z	-0.018	0.00	0.00	No	0.00	No
22	z	-0.01	0.00	0.00	No	0.00	No
25	z	-0.012	0.00	0.00	No	0.00	No
31	z	-0.017	0.00	0.00	No	0.00	No
32	z	-0.017	0.00	0.00	No	0.00	No
33	z	-0.017	0.00	0.00	No	0.00	No
34	z	-0.013	0.00	0.00	No	0.00	No
35	z	-0.013	0.00	0.00	No	0.00	No
36	z	-0.018	0.00	0.00	No	0.00	No
37	z	-0.017	0.00	0.00	No	0.00	No
38	z	-0.013	0.00	0.00	No	0.00	No
39	z	-0.013	0.00	0.00	No	0.00	No
40	z	-0.018	0.00	0.00	No	0.00	No
41	z	-0.017	0.00	0.00	No	0.00	No

	44	z	-0.007	0.00	0.00	No	0.00	No
	47	z	-0.007	0.00	0.00	No	0.00	No
	50	z	-0.007	0.00	0.00	No	0.00	No
	57	z	-0.007	0.00	0.00	No	0.00	No
	58	z	-0.007	0.00	0.00	No	0.00	No
	59	z	-0.007	0.00	0.00	No	0.00	No
	60	z	-0.02	0.00	0.00	No	0.00	No
	61	z	-0.02	0.00	0.00	No	0.00	No
	62	z	-0.02	0.00	0.00	No	0.00	No
	64	z	-0.02	0.00	0.00	No	0.00	No
	65	z	-0.02	0.00	0.00	No	0.00	No
	66	z	-0.02	0.00	0.00	No	0.00	No
	67	z	-0.012	0.00	0.00	No	0.00	No
	68	z	-0.017	0.00	0.00	No	0.00	No
	69	z	-0.017	0.00	0.00	No	0.00	No
	70	z	-0.007	0.00	0.00	No	0.00	No
	75	z	-0.007	0.00	0.00	No	0.00	No
	76	z	-0.007	0.00	0.00	No	0.00	No
	81	z	-0.007	0.00	0.00	No	0.00	No
	84	z	-0.007	0.00	0.00	No	0.00	No
	87	z	-0.007	0.00	0.00	No	0.00	No
	90	z	-0.007	0.00	0.00	No	0.00	No
	93	z	-0.007	0.00	0.00	No	0.00	No
W60	1	x	-0.017	0.00	0.00	No	0.00	No
	2	x	-0.017	0.00	0.00	No	0.00	No
	3	x	-0.017	0.00	0.00	No	0.00	No
	4	x	-0.013	0.00	0.00	No	0.00	No
	5	x	-0.013	0.00	0.00	No	0.00	No
	6	x	-0.018	0.00	0.00	No	0.00	No
	10	x	-0.017	0.00	0.00	No	0.00	No
	11	x	-0.017	0.00	0.00	No	0.00	No
	12	x	-0.013	0.00	0.00	No	0.00	No
	13	x	-0.013	0.00	0.00	No	0.00	No
	14	x	-0.018	0.00	0.00	No	0.00	No
	16	x	-0.017	0.00	0.00	No	0.00	No
	17	x	-0.013	0.00	0.00	No	0.00	No
	18	x	-0.013	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	22	x	-0.01	0.00	0.00	No	0.00	No
	25	x	-0.012	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	37	x	-0.017	0.00	0.00	No	0.00	No
	38	x	-0.013	0.00	0.00	No	0.00	No
	39	x	-0.013	0.00	0.00	No	0.00	No
	40	x	-0.018	0.00	0.00	No	0.00	No
	41	x	-0.017	0.00	0.00	No	0.00	No
	44	x	-0.007	0.00	0.00	No	0.00	No
	47	x	-0.007	0.00	0.00	No	0.00	No
	50	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	59	x	-0.007	0.00	0.00	No	0.00	No
	60	x	-0.02	0.00	0.00	No	0.00	No
	61	x	-0.02	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No

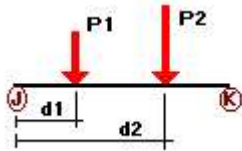
	64	x	-0.02	0.00	0.00	No	0.00	No
	65	x	-0.02	0.00	0.00	No	0.00	No
	66	x	-0.02	0.00	0.00	No	0.00	No
	67	x	-0.012	0.00	0.00	No	0.00	No
	68	x	-0.017	0.00	0.00	No	0.00	No
	69	x	-0.017	0.00	0.00	No	0.00	No
	70	x	-0.007	0.00	0.00	No	0.00	No
	75	x	-0.007	0.00	0.00	No	0.00	No
	76	x	-0.007	0.00	0.00	No	0.00	No
	81	x	-0.007	0.00	0.00	No	0.00	No
	84	x	-0.007	0.00	0.00	No	0.00	No
	87	x	-0.007	0.00	0.00	No	0.00	No
	90	x	-0.007	0.00	0.00	No	0.00	No
	93	x	-0.007	0.00	0.00	No	0.00	No
W90	22	x	-0.01	0.00	0.00	No	0.00	No
	25	x	-0.012	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	44	x	-0.007	0.00	0.00	No	0.00	No
	47	x	-0.007	0.00	0.00	No	0.00	No
	50	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	59	x	-0.007	0.00	0.00	No	0.00	No
	60	x	-0.02	0.00	0.00	No	0.00	No
	61	x	-0.02	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	64	x	-0.02	0.00	0.00	No	0.00	No
	65	x	-0.02	0.00	0.00	No	0.00	No
	66	x	-0.02	0.00	0.00	No	0.00	No
	67	x	-0.012	0.00	0.00	No	0.00	No
	68	x	-0.017	0.00	0.00	No	0.00	No
	70	x	-0.007	0.00	0.00	No	0.00	No
	75	x	-0.007	0.00	0.00	No	0.00	No
	76	x	-0.007	0.00	0.00	No	0.00	No
	81	x	-0.007	0.00	0.00	No	0.00	No
	84	x	-0.007	0.00	0.00	No	0.00	No
	87	x	-0.007	0.00	0.00	No	0.00	No
	90	x	-0.007	0.00	0.00	No	0.00	No
	93	x	-0.007	0.00	0.00	No	0.00	No
W120	1	x	-0.017	0.00	0.00	No	0.00	No
	2	x	-0.017	0.00	0.00	No	0.00	No
	3	x	-0.017	0.00	0.00	No	0.00	No
	4	x	-0.013	0.00	0.00	No	0.00	No
	5	x	-0.013	0.00	0.00	No	0.00	No
	6	x	-0.018	0.00	0.00	No	0.00	No
	10	x	-0.017	0.00	0.00	No	0.00	No
	11	x	-0.017	0.00	0.00	No	0.00	No
	12	x	-0.013	0.00	0.00	No	0.00	No
	13	x	-0.013	0.00	0.00	No	0.00	No
	14	x	-0.018	0.00	0.00	No	0.00	No
	16	x	-0.017	0.00	0.00	No	0.00	No
	17	x	-0.013	0.00	0.00	No	0.00	No
	18	x	-0.013	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	22	x	-0.01	0.00	0.00	No	0.00	No

	25	x	-0.012	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	37	x	-0.017	0.00	0.00	No	0.00	No
	38	x	-0.013	0.00	0.00	No	0.00	No
	39	x	-0.013	0.00	0.00	No	0.00	No
	40	x	-0.018	0.00	0.00	No	0.00	No
	41	x	-0.017	0.00	0.00	No	0.00	No
	44	x	-0.007	0.00	0.00	No	0.00	No
	47	x	-0.007	0.00	0.00	No	0.00	No
	50	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	59	x	-0.007	0.00	0.00	No	0.00	No
	60	x	-0.02	0.00	0.00	No	0.00	No
	61	x	-0.02	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	64	x	-0.02	0.00	0.00	No	0.00	No
	65	x	-0.02	0.00	0.00	No	0.00	No
	66	x	-0.02	0.00	0.00	No	0.00	No
	67	x	-0.012	0.00	0.00	No	0.00	No
	68	x	-0.017	0.00	0.00	No	0.00	No
	69	x	-0.017	0.00	0.00	No	0.00	No
	70	x	-0.007	0.00	0.00	No	0.00	No
	75	x	-0.007	0.00	0.00	No	0.00	No
	76	x	-0.007	0.00	0.00	No	0.00	No
	81	x	-0.007	0.00	0.00	No	0.00	No
	84	x	-0.007	0.00	0.00	No	0.00	No
	87	x	-0.007	0.00	0.00	No	0.00	No
	90	x	-0.007	0.00	0.00	No	0.00	No
	93	x	-0.007	0.00	0.00	No	0.00	No
W150	1	z	0.017	0.00	0.00	No	0.00	No
	2	z	0.017	0.00	0.00	No	0.00	No
	3	z	0.017	0.00	0.00	No	0.00	No
	4	z	0.013	0.00	0.00	No	0.00	No
	5	z	0.013	0.00	0.00	No	0.00	No
	6	z	0.018	0.00	0.00	No	0.00	No
	10	z	0.017	0.00	0.00	No	0.00	No
	11	z	0.017	0.00	0.00	No	0.00	No
	12	z	0.013	0.00	0.00	No	0.00	No
	13	z	0.013	0.00	0.00	No	0.00	No
	14	z	0.018	0.00	0.00	No	0.00	No
	16	z	0.017	0.00	0.00	No	0.00	No
	17	z	0.013	0.00	0.00	No	0.00	No
	18	z	0.013	0.00	0.00	No	0.00	No
	19	z	0.018	0.00	0.00	No	0.00	No
	22	z	0.01	0.00	0.00	No	0.00	No
	25	z	0.012	0.00	0.00	No	0.00	No
	31	z	0.017	0.00	0.00	No	0.00	No
	32	z	0.017	0.00	0.00	No	0.00	No
	33	z	0.017	0.00	0.00	No	0.00	No
	34	z	0.013	0.00	0.00	No	0.00	No
	35	z	0.013	0.00	0.00	No	0.00	No
	36	z	0.018	0.00	0.00	No	0.00	No
	37	z	0.017	0.00	0.00	No	0.00	No
	38	z	0.013	0.00	0.00	No	0.00	No

	39	z	0.013	0.00	0.00	No	0.00	No
	40	z	0.018	0.00	0.00	No	0.00	No
	41	z	0.017	0.00	0.00	No	0.00	No
	44	z	0.007	0.00	0.00	No	0.00	No
	47	z	0.007	0.00	0.00	No	0.00	No
	50	z	0.007	0.00	0.00	No	0.00	No
	57	z	0.007	0.00	0.00	No	0.00	No
	58	z	0.007	0.00	0.00	No	0.00	No
	59	z	0.007	0.00	0.00	No	0.00	No
	60	z	0.02	0.00	0.00	No	0.00	No
	61	z	0.02	0.00	0.00	No	0.00	No
	62	z	0.02	0.00	0.00	No	0.00	No
	64	z	0.02	0.00	0.00	No	0.00	No
	65	z	0.02	0.00	0.00	No	0.00	No
	66	z	0.02	0.00	0.00	No	0.00	No
	67	z	0.012	0.00	0.00	No	0.00	No
	68	z	0.017	0.00	0.00	No	0.00	No
	69	z	0.017	0.00	0.00	No	0.00	No
	70	z	0.007	0.00	0.00	No	0.00	No
	75	z	0.007	0.00	0.00	No	0.00	No
	76	z	0.007	0.00	0.00	No	0.00	No
	81	z	0.007	0.00	0.00	No	0.00	No
	84	z	0.007	0.00	0.00	No	0.00	No
	87	z	0.007	0.00	0.00	No	0.00	No
	90	z	0.007	0.00	0.00	No	0.00	No
	93	z	0.007	0.00	0.00	No	0.00	No
Di	1	y	-0.007	0.00	0.00	No	0.00	No
	2	y	-0.007	0.00	0.00	No	0.00	No
	3	y	-0.007	0.00	0.00	No	0.00	No
	4	y	-0.005	0.00	0.00	No	0.00	No
	5	y	-0.005	0.00	0.00	No	0.00	No
	6	y	-0.01	0.00	0.00	No	0.00	No
	10	y	-0.007	0.00	0.00	No	0.00	No
	11	y	-0.007	0.00	0.00	No	0.00	No
	12	y	-0.005	0.00	0.00	No	0.00	No
	13	y	-0.005	0.00	0.00	No	0.00	No
	14	y	-0.01	0.00	0.00	No	0.00	No
	16	y	-0.007	0.00	0.00	No	0.00	No
	17	y	-0.005	0.00	0.00	No	0.00	No
	18	y	-0.005	0.00	0.00	No	0.00	No
	19	y	-0.01	0.00	0.00	No	0.00	No
	22	y	-0.005	0.00	0.00	No	0.00	No
	25	y	-0.006	0.00	0.00	No	0.00	No
	31	y	-0.007	0.00	0.00	No	0.00	No
	32	y	-0.007	0.00	0.00	No	0.00	No
	33	y	-0.007	0.00	0.00	No	0.00	No
	34	y	-0.005	0.00	0.00	No	0.00	No
	35	y	-0.005	0.00	0.00	No	0.00	No
	36	y	-0.01	0.00	0.00	No	0.00	No
	37	y	-0.007	0.00	0.00	No	0.00	No
	38	y	-0.005	0.00	0.00	No	0.00	No
	39	y	-0.005	0.00	0.00	No	0.00	No
	40	y	-0.01	0.00	0.00	No	0.00	No
	41	y	-0.007	0.00	0.00	No	0.00	No
	44	y	-0.004	0.00	0.00	No	0.00	No
	47	y	-0.004	0.00	0.00	No	0.00	No
	50	y	-0.004	0.00	0.00	No	0.00	No
	57	y	-0.004	0.00	0.00	No	0.00	No
	58	y	-0.004	0.00	0.00	No	0.00	No
	59	y	-0.004	0.00	0.00	No	0.00	No

60	y	-0.008	0.00	0.00	No	0.00	No
61	y	-0.008	0.00	0.00	No	0.00	No
62	y	-0.008	0.00	0.00	No	0.00	No
64	y	-0.008	0.00	0.00	No	0.00	No
65	y	-0.008	0.00	0.00	No	0.00	No
66	y	-0.008	0.00	0.00	No	0.00	No
67	y	-0.006	0.00	0.00	No	0.00	No
68	y	-0.007	0.00	0.00	No	0.00	No
69	y	-0.007	0.00	0.00	No	0.00	No
70	y	-0.004	0.00	0.00	No	0.00	No
75	y	-0.004	0.00	0.00	No	0.00	No
76	y	-0.004	0.00	0.00	No	0.00	No
81	y	-0.004	0.00	0.00	No	0.00	No
84	y	-0.004	0.00	0.00	No	0.00	No
87	y	-0.004	0.00	0.00	No	0.00	No
90	y	-0.004	0.00	0.00	No	0.00	No
93	y	-0.004	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	22	y	-0.033	2.00	No
		y	-0.033	4.00	No
		y	-0.041	6.00	No
		y	-0.041	8.00	No
	25	y	-0.06	1.50	No
		y	-0.06	8.50	No
	44	y	-0.037	2.00	No
	47	y	-0.03	2.00	No
	50	y	-0.03	2.00	No
	57	y	-0.015	2.00	No
	58	y	-0.03	2.00	No
	59	y	-0.03	2.00	No
	67	y	-0.044	1.50	No
		y	-0.044	8.50	No
	70	y	-0.022	2.00	No
	75	y	-0.037	2.00	No
	76	y	-0.022	2.00	No
	81	y	-0.03	2.00	No
	84	y	-0.03	2.00	No
	87	y	-0.03	2.00	No
90	y	-0.03	2.00	No	
93	y	-0.015	2.00	No	
Wo	22	z	-0.084	2.00	No
		z	-0.084	4.00	No
		z	-0.082	6.00	No
		z	-0.082	8.00	No
	25	z	-0.358	1.50	No
		z	-0.358	8.50	No

	44	z	-0.04	2.00	No
	47	z	-0.056	2.00	No
	50	z	-0.041	2.00	No
	57	z	-0.031	2.00	No
	58	z	-0.034	2.00	No
	59	z	-0.034	2.00	No
	67	z	-0.377	1.50	No
		z	-0.377	8.50	No
	70	z	-0.037	2.00	No
	75	z	-0.04	2.00	No
	76	z	-0.037	2.00	No
	81	z	-0.041	2.00	No
	84	z	-0.056	2.00	No
	87	z	-0.034	2.00	No
	90	z	-0.034	2.00	No
W30	93	z	-0.031	2.00	No
	22	3	-0.073	2.00	No
		3	-0.073	4.00	No
		3	-0.075	6.00	No
		3	-0.075	8.00	No
	25	3	-0.31	1.50	No
		3	-0.31	8.50	No
	44	3	-0.037	2.00	No
	47	3	-0.05	2.00	No
	50	3	-0.037	2.00	No
	57	3	-0.031	2.00	No
	58	3	-0.036	2.00	No
	59	3	-0.036	2.00	No
	67	3	-0.331	1.50	No
		3	-0.331	8.50	No
	70	3	-0.032	2.00	No
	75	3	-0.037	2.00	No
	76	3	-0.032	2.00	No
	81	3	-0.037	2.00	No
	84	3	-0.05	2.00	No
	87	3	-0.036	2.00	No
	90	3	-0.036	2.00	No
W60	93	3	-0.031	2.00	No
	22	3	-0.052	2.00	No
		3	-0.052	4.00	No
		3	-0.062	6.00	No
		3	-0.062	8.00	No
	25	3	-0.212	1.50	No
		3	-0.212	8.50	No
	44	3	-0.031	2.00	No
	47	3	-0.039	2.00	No
	50	3	-0.029	2.00	No
	57	3	-0.031	2.00	No
	58	3	-0.052	2.00	No
	59	3	-0.052	2.00	No
	67	3	-0.239	1.50	No
		3	-0.239	8.50	No
	70	3	-0.022	2.00	No
	75	3	-0.031	2.00	No
	76	3	-0.022	2.00	No
	81	3	-0.026	2.00	No
	84	3	-0.039	2.00	No
	87	3	-0.052	2.00	No
	90	3	-0.052	2.00	No
	93	3	-0.031	2.00	No

W90	22	x	-0.041	2.00	No
		x	-0.041	4.00	No
		x	-0.055	6.00	No
		x	-0.055	8.00	No
	25	x	-0.163	1.50	No
		x	-0.163	8.50	No
	44	x	-0.028	2.00	No
	47	x	-0.034	2.00	No
	50	x	-0.025	2.00	No
	57	x	-0.031	2.00	No
	58	x	-0.056	2.00	No
	59	x	-0.056	2.00	No
	67	x	-0.193	1.50	No
		x	-0.193	8.50	No
	70	x	-0.017	2.00	No
	75	x	-0.028	2.00	No
	76	x	-0.017	2.00	No
	81	x	-0.025	2.00	No
	84	x	-0.034	2.00	No
	87	x	-0.056	2.00	No
90	x	-0.056	2.00	No	
93	x	-0.031	2.00	No	
W120	22	2	-0.052	2.00	No
		2	-0.052	4.00	No
		2	-0.062	6.00	No
		2	-0.062	8.00	No
	25	2	-0.212	1.50	No
		2	-0.212	8.50	No
	44	2	-0.031	2.00	No
	47	2	-0.039	2.00	No
	50	2	-0.029	2.00	No
	57	2	-0.031	2.00	No
	58	2	-0.052	2.00	No
	59	2	-0.052	2.00	No
	67	2	-0.239	1.50	No
		2	-0.239	8.50	No
	70	2	-0.022	2.00	No
	75	2	-0.031	2.00	No
	76	2	-0.022	2.00	No
	81	2	-0.026	2.00	No
	84	2	-0.039	2.00	No
	87	2	-0.052	2.00	No
90	2	-0.052	2.00	No	
93	2	-0.031	2.00	No	
W150	22	2	-0.073	2.00	No
		2	-0.073	4.00	No
		2	-0.075	6.00	No
		2	-0.075	8.00	No
	25	2	-0.31	1.50	No
		2	-0.31	8.50	No
	44	2	-0.037	2.00	No
	47	2	-0.05	2.00	No
	50	2	-0.037	2.00	No
	57	2	-0.031	2.00	No
	58	2	-0.036	2.00	No
	59	2	-0.036	2.00	No
67	2	-0.331	1.50	No	
	2	-0.331	8.50	No	
70	2	-0.032	2.00	No	
75	2	-0.037	2.00	No	

	76	2	-0.032	2.00	No
	81	2	-0.037	2.00	No
	84	2	-0.05	2.00	No
	87	2	-0.036	2.00	No
	90	2	-0.036	2.00	No
	93	2	-0.031	2.00	No
Di	22	y	-0.037	2.00	No
		y	-0.037	4.00	No
		y	-0.039	6.00	No
		y	-0.039	8.00	No
	25	y	-0.14	1.50	No
		y	-0.14	8.50	No
	44	y	-0.02	2.00	No
	47	y	-0.026	2.00	No
	50	y	-0.02	2.00	No
	57	y	-0.023	2.00	No
	58	y	-0.026	2.00	No
	59	y	-0.026	2.00	No
	67	y	-0.14	1.50	No
		y	-0.14	8.50	No
	70	y	-0.017	2.00	No
	75	y	-0.02	2.00	No
	76	y	-0.017	2.00	No
	81	y	-0.02	2.00	No
	84	y	-0.026	2.00	No
	87	y	-0.026	2.00	No
	90	y	-0.026	2.00	No
W10	93	y	-0.023	2.00	No
	22	z	-0.019	2.00	No
		z	-0.019	4.00	No
		z	-0.018	6.00	No
		z	-0.018	8.00	No
	25	z	-0.072	1.50	No
		z	-0.072	8.50	No
	44	z	-0.009	2.00	No
	47	z	-0.013	2.00	No
	50	z	-0.01	2.00	No
	57	z	-0.007	2.00	No
	58	z	-0.009	2.00	No
	59	z	-0.009	2.00	No
	67	z	-0.075	1.50	No
		z	-0.075	8.50	No
	70	z	-0.009	2.00	No
	75	z	-0.009	2.00	No
	76	z	-0.009	2.00	No
	81	z	-0.01	2.00	No
	84	z	-0.013	2.00	No
	87	z	-0.009	2.00	No
	90	z	-0.009	2.00	No
W130	93	z	-0.007	2.00	No
	22	3	-0.016	2.00	No
		3	-0.016	4.00	No
		3	-0.017	6.00	No
		3	-0.017	8.00	No
	25	3	-0.062	1.50	No
		3	-0.062	8.50	No
	44	3	-0.009	2.00	No
	47	3	-0.012	2.00	No
	50	3	-0.009	2.00	No
	57	3	-0.007	2.00	No

	58	3	-0.01	2.00	No
	59	3	-0.01	2.00	No
	67	3	-0.066	1.50	No
		3	-0.066	8.50	No
	70	3	-0.008	2.00	No
	75	3	-0.009	2.00	No
	76	3	-0.008	2.00	No
	81	3	-0.009	2.00	No
	84	3	-0.012	2.00	No
	87	3	-0.01	2.00	No
	90	3	-0.01	2.00	No
WI60	93	3	-0.007	2.00	No
	22	3	-0.012	2.00	No
		3	-0.012	4.00	No
		3	-0.014	6.00	No
		3	-0.014	8.00	No
	25	3	-0.045	1.50	No
		3	-0.045	8.50	No
	44	3	-0.008	2.00	No
	47	3	-0.01	2.00	No
	50	3	-0.007	2.00	No
	57	3	-0.007	2.00	No
	58	3	-0.012	2.00	No
	59	3	-0.012	2.00	No
	67	3	-0.05	1.50	No
		3	-0.05	8.50	No
	70	3	-0.006	2.00	No
	75	3	-0.008	2.00	No
	76	3	-0.006	2.00	No
	81	3	-0.007	2.00	No
	84	3	-0.01	2.00	No
	87	3	-0.012	2.00	No
	90	3	-0.012	2.00	No
WI90	93	3	-0.007	2.00	No
	22	x	-0.01	2.00	No
		x	-0.01	4.00	No
		x	-0.013	6.00	No
		x	-0.013	8.00	No
	25	x	-0.036	1.50	No
		x	-0.036	8.50	No
	44	x	-0.007	2.00	No
	47	x	-0.009	2.00	No
	50	x	-0.007	2.00	No
	57	x	-0.007	2.00	No
	58	x	-0.013	2.00	No
	59	x	-0.013	2.00	No
	67	x	-0.042	1.50	No
		x	-0.042	8.50	No
	70	x	-0.005	2.00	No
	75	x	-0.007	2.00	No
	76	x	-0.005	2.00	No
	81	x	-0.007	2.00	No
	84	x	-0.009	2.00	No
	87	x	-0.013	2.00	No
	90	x	-0.013	2.00	No
	93	x	-0.007	2.00	No
WI120	22	2	-0.012	2.00	No
		2	-0.012	4.00	No
		2	-0.014	6.00	No
		2	-0.014	8.00	No

	25	2	-0.045	1.50	No
		2	-0.045	8.50	No
	44	2	-0.008	2.00	No
	47	2	-0.01	2.00	No
	50	2	-0.007	2.00	No
	57	2	-0.007	2.00	No
	58	2	-0.012	2.00	No
	59	2	-0.012	2.00	No
	67	2	-0.05	1.50	No
		2	-0.05	8.50	No
	70	2	-0.006	2.00	No
	75	2	-0.008	2.00	No
	76	2	-0.006	2.00	No
	81	2	-0.007	2.00	No
	84	2	-0.01	2.00	No
	87	2	-0.012	2.00	No
	90	2	-0.012	2.00	No
	93	2	-0.007	2.00	No
WI150	22	2	-0.016	2.00	No
		2	-0.016	4.00	No
		2	-0.017	6.00	No
		2	-0.017	8.00	No
	25	2	-0.062	1.50	No
		2	-0.062	8.50	No
	44	2	-0.009	2.00	No
	47	2	-0.012	2.00	No
	50	2	-0.009	2.00	No
	57	2	-0.007	2.00	No
	58	2	-0.01	2.00	No
	59	2	-0.01	2.00	No
	67	2	-0.066	1.50	No
		2	-0.066	8.50	No
	70	2	-0.008	2.00	No
	75	2	-0.009	2.00	No
	76	2	-0.008	2.00	No
	81	2	-0.009	2.00	No
	84	2	-0.012	2.00	No
	87	2	-0.01	2.00	No
	90	2	-0.01	2.00	No
	93	2	-0.007	2.00	No
WLO	22	z	-0.006	2.00	No
		z	-0.006	4.00	No
		z	-0.006	6.00	No
		z	-0.006	8.00	No
	25	z	-0.023	1.50	No
		z	-0.023	8.50	No
	44	z	-0.003	2.00	No
	47	z	-0.004	2.00	No
	50	z	-0.003	2.00	No
	57	z	-0.002	2.00	No
	58	z	-0.002	2.00	No
	59	z	-0.002	2.00	No
	67	z	-0.024	1.50	No
		z	-0.024	8.50	No
	70	z	-0.003	2.00	No
	75	z	-0.003	2.00	No
	76	z	-0.003	2.00	No
	81	z	-0.003	2.00	No
	84	z	-0.004	2.00	No
	87	z	-0.002	2.00	No

	90	z	-0.002	2.00	No
	93	z	-0.002	2.00	No
WL30	22	3	-0.005	2.00	No
		3	-0.005	4.00	No
		3	-0.005	6.00	No
		3	-0.005	8.00	No
	25	3	-0.02	1.50	No
		3	-0.02	8.50	No
	44	3	-0.003	2.00	No
	47	3	-0.003	2.00	No
	50	3	-0.003	2.00	No
	57	3	-0.002	2.00	No
	58	3	-0.003	2.00	No
	59	3	-0.003	2.00	No
	67	3	-0.021	1.50	No
		3	-0.021	8.50	No
	70	3	-0.002	2.00	No
	75	3	-0.003	2.00	No
	76	3	-0.002	2.00	No
	81	3	-0.003	2.00	No
	84	3	-0.003	2.00	No
	87	3	-0.003	2.00	No
	90	3	-0.003	2.00	No
WL60	93	3	-0.002	2.00	No
	22	3	-0.004	2.00	No
		3	-0.004	4.00	No
		3	-0.004	6.00	No
		3	-0.004	8.00	No
	25	3	-0.014	1.50	No
		3	-0.014	8.50	No
	44	3	-0.002	2.00	No
	47	3	-0.003	2.00	No
	50	3	-0.002	2.00	No
	57	3	-0.002	2.00	No
	58	3	-0.003	2.00	No
	59	3	-0.003	2.00	No
	67	3	-0.015	1.50	No
		3	-0.015	8.50	No
	70	3	-0.002	2.00	No
	75	3	-0.002	2.00	No
	76	3	-0.002	2.00	No
	81	3	-0.002	2.00	No
	84	3	-0.003	2.00	No
	87	3	-0.003	2.00	No
	90	3	-0.003	2.00	No
	93	3	-0.002	2.00	No
WL90	22	x	-0.003	2.00	No
		x	-0.003	4.00	No
		x	-0.004	6.00	No
		x	-0.004	8.00	No
	25	x	-0.011	1.50	No
		x	-0.011	8.50	No
	44	x	-0.002	2.00	No
	47	x	-0.002	2.00	No
	50	x	-0.002	2.00	No
	57	x	-0.002	2.00	No
	58	x	-0.004	2.00	No
	59	x	-0.004	2.00	No
	67	x	-0.013	1.50	No
		x	-0.013	8.50	No

	70	x	-0.001	2.00	No
	75	x	-0.002	2.00	No
	76	x	-0.001	2.00	No
	81	x	-0.002	2.00	No
	84	x	-0.002	2.00	No
	87	x	-0.004	2.00	No
	90	x	-0.004	2.00	No
WL120	93	x	-0.002	2.00	No
	22	2	-0.004	2.00	No
		2	-0.004	4.00	No
		2	-0.004	6.00	No
		2	-0.004	8.00	No
	25	2	-0.014	1.50	No
		2	-0.014	8.50	No
	44	2	-0.002	2.00	No
	47	2	-0.003	2.00	No
	50	2	-0.002	2.00	No
	57	2	-0.002	2.00	No
	58	2	-0.003	2.00	No
	59	2	-0.003	2.00	No
	67	2	-0.015	1.50	No
		2	-0.015	8.50	No
	70	2	-0.002	2.00	No
	75	2	-0.002	2.00	No
	76	2	-0.002	2.00	No
	81	2	-0.002	2.00	No
	84	2	-0.003	2.00	No
	87	2	-0.003	2.00	No
	90	2	-0.003	2.00	No
WL150	93	2	-0.002	2.00	No
	22	2	-0.005	2.00	No
		2	-0.005	4.00	No
		2	-0.005	6.00	No
		2	-0.005	8.00	No
	25	2	-0.02	1.50	No
		2	-0.02	8.50	No
	44	2	-0.003	2.00	No
	47	2	-0.003	2.00	No
	50	2	-0.003	2.00	No
	57	2	-0.002	2.00	No
	58	2	-0.003	2.00	No
	59	2	-0.003	2.00	No
	67	2	-0.021	1.50	No
		2	-0.021	8.50	No
	70	2	-0.002	2.00	No
	75	2	-0.003	2.00	No
	76	2	-0.002	2.00	No
	81	2	-0.003	2.00	No
	84	2	-0.003	2.00	No
	87	2	-0.003	2.00	No
	90	2	-0.003	2.00	No
	93	2	-0.002	2.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00

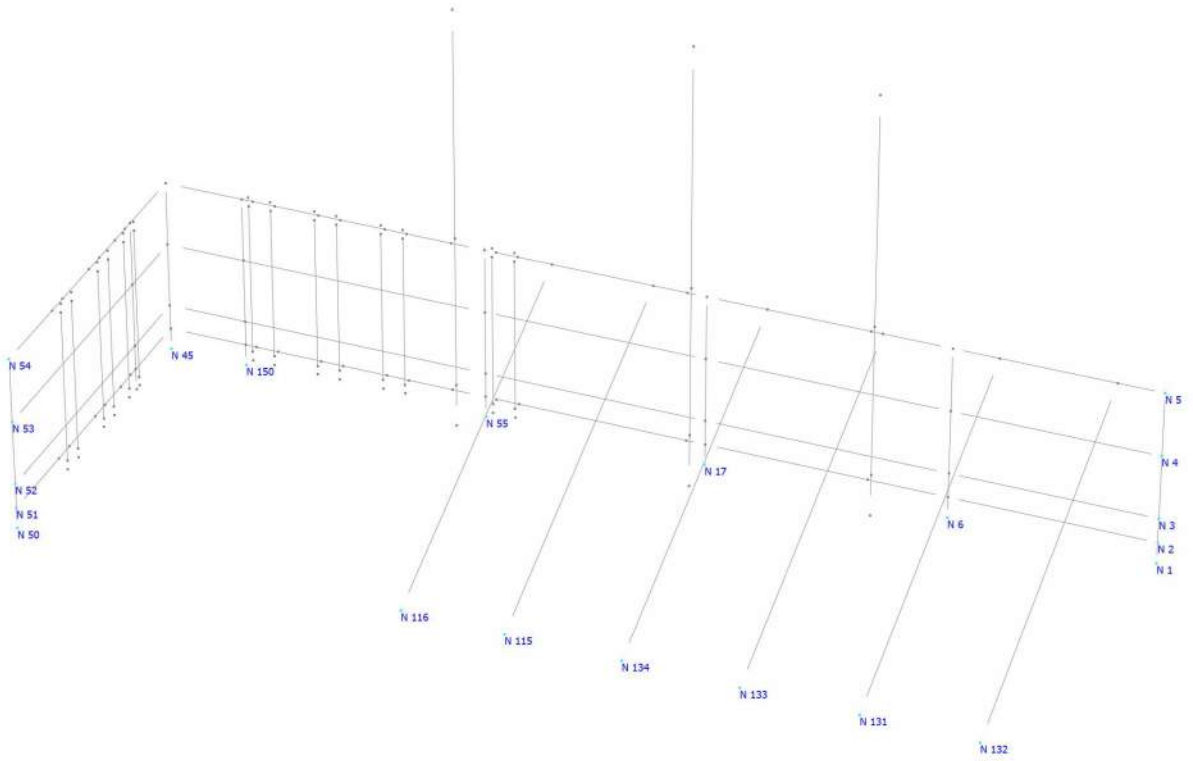
Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

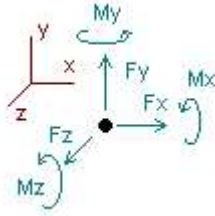
LC1=1.2D+1.6W_o
LC2=1.2D+1.6W₃₀
LC3=1.2D+1.6W₆₀
LC4=1.2D+1.6W₉₀
LC5=1.2D+1.6W₁₂₀
LC6=1.2D+1.6W₁₅₀
LC7=1.2D-1.6W_o
LC8=1.2D-1.6W₃₀
LC9=1.2D-1.6W₆₀
LC10=1.2D-1.6W₉₀
LC11=1.2D-1.6W₁₂₀
LC12=1.2D-1.6W₁₅₀
LC13=0.9D+1.6W_o
LC14=0.9D+1.6W₃₀
LC15=0.9D+1.6W₆₀
LC16=0.9D+1.6W₉₀
LC17=0.9D+1.6W₁₂₀
LC18=0.9D+1.6W₁₅₀
LC19=0.9D-1.6W_o
LC20=0.9D-1.6W₃₀
LC21=0.9D-1.6W₆₀
LC22=0.9D-1.6W₉₀
LC23=0.9D-1.6W₁₂₀
LC24=0.9D-1.6W₁₅₀
LC25=1.2D+Di+W_{I0}
LC26=1.2D+Di+W_{I30}
LC27=1.2D+Di+W_{I60}
LC28=1.2D+Di+W_{I90}
LC29=1.2D+Di+W_{I120}
LC30=1.2D+Di+W_{I150}
LC31=1.2D+Di-W_{I0}
LC32=1.2D+Di-W_{I30}
LC33=1.2D+Di-W_{I60}
LC34=1.2D+Di-W_{I90}
LC35=1.2D+Di-W_{I120}
LC36=1.2D+Di-W_{I150}
LC37=0.9D
LC38=1.2D
LC41=1.2D+W_{L0}
LC42=1.2D+W_{L30}
LC43=1.2D+W_{L60}
LC44=1.2D+W_{L90}
LC45=1.2D+W_{L120}
LC46=1.2D+W_{L150}
LC47=1.2D-W_{L0}
LC48=1.2D-W_{L30}
LC49=1.2D-W_{L60}
LC50=1.2D-W_{L90}
LC51=1.2D-W_{L120}
LC52=1.2D-W_{L150}

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
<i>L 2-1_2X2-1_2X1_4</i>		1	LC7 at 0.00%	0.05	OK	
		2	LC2 at 50.00%	0.17	OK	
		3	LC5 at 0.00%	0.19	OK	
		10	LC2 at 53.13%	0.17	OK	
		11	LC3 at 67.19%	0.39	OK	
		31	LC1 at 100.00%	0.19	OK	
		32	LC10 at 12.50%	0.25	OK	
		33	LC9 at 100.00%	0.54	OK	
		41	LC1 at 100.00%	0.21	OK	
		68	LC10 at 12.50%	0.20	OK	
		69	LC1 at 25.00%	0.20	OK	
		<i>L 3X3X1_4</i>		60	LC1 at 100.00%	0.33
61	LC3 at 50.00%			0.20	OK	
62	LC23 at 50.00%			0.21	OK	
64	LC3 at 50.00%			0.20	OK	
65	LC5 at 50.00%			0.20	OK	
66	LC23 at 50.00%			0.24	OK	
<i>LU 2-3/4x5x1/4</i>		6	LC7 at 0.00%	0.10	OK	
		14	LC7 at 100.00%	0.21	OK	
		19	LC7 at 0.00%	0.25	OK	
		36	LC10 at 100.00%	0.50	OK	
		40	LC10 at 0.00%	0.49	OK	
<i>P1000 Unistrut</i>		44	LC7 at 50.00%	0.16	OK	Eq. H1.2-1
		47	LC1 at 50.00%	0.26	OK	Eq. H1.2-1
		50	LC1 at 50.00%	0.33	OK	Eq. H1.2-1
		57	LC4 at 50.00%	0.17	OK	Eq. H1.2-1
		58	LC4 at 50.00%	0.24	OK	Eq. H1.2-1
		59	LC9 at 93.75%	0.21	OK	Eq. H1.2-1
		70	LC7 at 93.75%	0.26	OK	Eq. H1.2-1
		75	LC7 at 50.00%	0.16	OK	Eq. H1.2-1
		76	LC7 at 93.75%	0.18	OK	Eq. H1.2-1
		81	LC1 at 50.00%	0.31	OK	Eq. H1.2-1
		84	LC1 at 50.00%	0.29	OK	Eq. H1.2-1
		87	LC10 at 50.00%	0.21	OK	Eq. H1.2-1
		90	LC4 at 50.00%	0.24	OK	Eq. H1.2-1
		93	LC4 at 50.00%	0.15	OK	Eq. H1.2-1
<i>PIPE 2-1_2x0.276XS</i>		25	LC1 at 54.17%	0.69	OK	
		67	LC1 at 54.17%	0.72	OK	
<i>PIPE 2x0.154</i>		22	LC7 at 52.08%	0.51	OK	
<i>PL 2x1/4</i>		4	LC8 at 100.00%	0.49	With warnings	
		5	LC12 at 100.00%	0.47	With warnings	
		12	LC8 at 100.00%	0.60	With warnings	
		13	LC12 at 100.00%	0.59	With warnings	
		17	LC8 at 100.00%	0.57	With warnings	
		18	LC12 at 100.00%	0.53	With warnings	
		34	LC11 at 100.00%	0.62	With warnings	
		35	LC10 at 100.00%	0.66	With warnings	
		38	LC2 at 0.00%	0.64	With warnings	
39	LC6 at 0.00%	0.64	With warnings			
<i>T2L 2-1_2X2-1_2X1_4</i>		16	LC7 at 30.21%	0.88	OK	
		37	LC1 at 90.28%	0.60	OK	



Analysis result

Reactions



Direction of positive forces and moments

Node	Forces [Kip]			Moments [Kip*ft]		
	FX	FY	FZ	MX	MY	MZ
Condition LC1=1.2D+1.6Wo						
1	-0.02871	0.03825	0.00475	0.00000	-0.00376	0.00000
2	-0.13998	0.00000	0.06440	0.00000	0.00000	0.00000
3	-0.00791	0.00000	0.07578	0.00000	0.00000	0.00000
4	-0.07771	0.00000	0.09297	0.00000	0.00000	0.00000
5	0.11783	0.00000	0.00533	0.00000	0.00000	0.00000
6	-0.03543	-0.26391	0.23392	0.00000	0.00021	0.00000
17	0.03473	-0.17856	0.15783	0.00000	0.00021	0.00000
45	-0.08987	0.19114	-0.25563	0.00000	0.00635	0.00000
50	0.00399	0.14614	0.20481	0.00000	-0.00398	0.00000
51	-0.03148	0.00000	0.48449	0.00000	0.00000	0.00000
52	0.00356	0.00000	-0.21446	0.00000	0.00000	0.00000
53	-0.00092	0.00000	0.04105	0.00000	0.00000	0.00000
54	-0.06925	0.00000	1.09449	0.00000	0.00000	0.00000
55	-0.00143	-0.37774	0.41530	0.00000	-0.00755	0.00000
115	0.00000	-0.23711	-0.53025	0.00000	0.00000	0.00000
116	-0.00001	1.33986	2.99228	0.00000	0.00000	0.00000
131	0.00000	0.12235	0.27300	0.00000	0.00000	0.00000
132	0.00000	0.07494	0.16706	0.00000	0.00000	0.00000
133	0.00000	0.60890	1.36065	0.00000	0.00000	0.00000
134	0.00000	0.34799	0.77733	0.00000	0.00000	0.00000
150	0.32259	0.48025	0.43932	0.00000	0.01052	0.00000
SUM	0.00000	2.29248	7.88442	0.00000	0.00201	0.00000
Condition LC2=1.2D+1.6W30						
1	-0.03180	0.03444	0.00463	0.00000	-0.00371	0.00000
2	-0.02524	0.00000	0.06183	0.00000	0.00000	0.00000
3	0.04202	0.00000	0.07579	0.00000	0.00000	0.00000
4	-0.03215	0.00000	0.09306	0.00000	0.00000	0.00000
5	1.99351	0.00000	0.00902	0.00000	0.00000	0.00000
6	0.01058	-0.11495	0.25382	0.00000	-0.00009	0.00000
17	0.05663	-0.11841	0.19487	0.00000	0.00010	0.00000
45	-0.07146	0.12209	-0.21357	0.00000	0.00342	0.00000
50	0.00140	0.14682	0.10346	0.00000	0.00118	0.00000
51	0.01785	0.00000	0.57100	0.00000	0.00000	0.00000
52	0.00221	0.00000	-0.07689	0.00000	0.00000	0.00000
53	0.00027	0.00000	0.07485	0.00000	0.00000	0.00000
54	-0.01405	0.00000	1.01188	0.00000	0.00000	0.00000
55	0.06775	-0.18812	0.38910	0.00000	-0.00599	0.00000

115	0.00002	-0.13810	-0.30898	0.00000	0.00000	0.00000
116	-0.00016	1.08574	2.42494	0.00000	0.00000	0.00000
131	-0.00001	0.14219	0.31734	0.00000	0.00000	0.00000
132	0.00000	0.06973	0.15542	0.00000	0.00000	0.00000
133	-0.00005	0.49942	1.11591	0.00000	0.00000	0.00000
134	-0.00003	0.30187	0.67418	0.00000	0.00000	0.00000
150	0.35406	0.44976	0.34126	0.00000	0.00886	0.00000

SUM	2.37135	2.29248	7.27292	0.00000	0.00378	0.00000
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Condition **LC3=1.2D+1.6W60**

1	0.02846	0.09310	0.00038	0.00000	-0.00003	0.00000
2	0.72039	0.00000	0.00244	0.00000	0.00000	0.00000
3	0.00159	0.00000	0.00116	0.00000	0.00000	0.00000
4	0.05289	0.00000	-0.00067	0.00000	0.00000	0.00000
5	3.40232	0.00000	0.00704	0.00000	0.00000	0.00000
6	0.02065	0.22615	-0.03014	0.00000	0.00009	0.00000
17	0.11442	0.27503	-0.03211	0.00000	-0.00075	0.00000
45	0.02637	-0.06282	-0.08863	0.00000	-0.00988	0.00000
50	0.00272	0.15613	-0.27303	0.00000	0.02309	0.00000
51	0.21662	0.00000	0.76542	0.00000	0.00000	0.00000
52	0.08486	0.00000	0.09275	0.00000	0.00000	0.00000
53	0.11049	0.00000	-0.16239	0.00000	0.00000	0.00000
54	0.19588	0.00000	0.47896	0.00000	0.00000	0.00000
55	0.14793	0.26823	-0.00910	0.00000	-0.00154	0.00000
115	0.14024	-0.02674	-0.11743	0.00000	0.00000	0.00000
116	0.14015	0.36712	0.76260	0.00000	0.00000	0.00000
131	0.14023	0.03742	0.02594	0.00000	0.00000	0.00000
132	0.14023	0.01857	-0.01617	0.00000	0.00000	0.00000
133	0.14020	0.23580	0.46938	0.00000	0.00000	0.00000
134	0.14022	0.10700	0.18145	0.00000	0.00000	0.00000
150	0.36924	0.59749	-0.20352	0.00000	0.00211	0.00000

SUM	6.33611	2.29248	1.85432	0.00000	0.01308	0.00000
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Condition **LC4=1.2D+1.6W90**

1	-0.00035	0.07244	0.00027	0.00000	0.00002	0.00000
2	0.48555	0.00000	-0.00201	0.00000	0.00000	0.00000
3	-0.00759	0.00000	0.00089	0.00000	0.00000	0.00000
4	0.01414	0.00000	-0.00035	0.00000	0.00000	0.00000
5	3.42448	0.00000	0.00739	0.00000	0.00000	0.00000
6	0.12684	0.40613	0.00807	0.00000	0.00006	0.00000
17	0.11611	0.47579	0.02409	0.00000	-0.00040	0.00000
45	-0.01717	-0.04836	-0.03790	0.00000	-0.01251	0.00000
50	0.00077	0.16536	-0.34405	0.00000	0.02681	0.00000
51	0.25113	0.00000	0.69354	0.00000	0.00000	0.00000
52	0.08486	0.00000	0.09836	0.00000	0.00000	0.00000
53	0.11100	0.00000	-0.17102	0.00000	0.00000	0.00000
54	0.24539	0.00000	0.16310	0.00000	0.00000	0.00000
55	0.22844	0.57707	-0.01393	0.00000	0.00105	0.00000
115	0.14022	0.07615	0.11249	0.00000	0.00000	0.00000
116	0.14026	-0.07487	-0.22499	0.00000	0.00000	0.00000
131	0.14023	0.04401	0.04068	0.00000	0.00000	0.00000
132	0.14023	0.01814	-0.01714	0.00000	0.00000	0.00000
133	0.14023	0.02543	-0.00084	0.00000	0.00000	0.00000
134	0.14024	0.01105	-0.03298	0.00000	0.00000	0.00000
150	0.25870	0.54413	-0.30365	0.00000	-0.00028	0.00000

SUM	6.16371	2.29248	0.00000	0.00000	0.01474	0.00000
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Condition **LC5=1.2D+1.6W120**

1	-0.01331	0.05297	-0.00003	0.00000	0.00011	0.00000
2	0.42656	0.00000	-0.00605	0.00000	0.00000	0.00000
3	0.04031	0.00000	0.00043	0.00000	0.00000	0.00000
4	0.06239	0.00000	-0.00011	0.00000	0.00000	0.00000
5	3.39486	0.00000	0.00795	0.00000	0.00000	0.00000
6	0.24342	0.58361	0.04606	0.00000	-0.00009	0.00000
17	0.12847	0.66969	0.07780	0.00000	-0.00018	0.00000
45	0.05026	-0.04788	-0.04465	0.00000	-0.01245	0.00000
50	0.00062	0.17429	-0.30784	0.00000	0.02474	0.00000
51	0.23262	0.00000	0.48515	0.00000	0.00000	0.00000
52	0.08662	0.00000	0.08869	0.00000	0.00000	0.00000
53	0.10984	0.00000	-0.14320	0.00000	0.00000	0.00000
54	0.24558	0.00000	-0.17786	0.00000	0.00000	0.00000
55	0.33781	0.87372	-0.01490	0.00000	0.00328	0.00000
115	0.14020	0.16652	0.31442	0.00000	0.00000	0.00000
116	0.14036	-0.49272	-1.15897	0.00000	0.00000	0.00000
131	0.14023	0.04982	0.05367	0.00000	0.00000	0.00000
132	0.14023	0.01761	-0.01832	0.00000	0.00000	0.00000
133	0.14027	-0.18651	-0.47447	0.00000	0.00000	0.00000
134	0.14025	-0.08374	-0.24480	0.00000	0.00000	0.00000
150	0.14851	0.51510	-0.33728	0.00000	-0.00286	0.00000

SUM 6.33611 2.29248 -1.85432 0.00000 0.01255 0.00000

Condition **LC6=1.2D+1.6W150**

1	0.02509	0.10187	-0.00416	0.00000	0.00372	0.00000
2	0.24556	0.00000	-0.06555	0.00000	0.00000	0.00000
3	-0.04989	0.00000	-0.07436	0.00000	0.00000	0.00000
4	0.05878	0.00000	-0.09364	0.00000	0.00000	0.00000
5	1.74035	0.00000	0.00542	0.00000	0.00000	0.00000
6	0.15422	0.91351	-0.23799	0.00000	0.00037	0.00000
17	-0.04080	1.02727	-0.15918	0.00000	-0.00050	0.00000
45	0.23344	0.02208	-0.09810	0.00000	-0.00722	0.00000
50	-0.00383	0.19981	-0.00556	0.00000	0.00671	0.00000
51	0.05959	0.00000	-0.20705	0.00000	0.00000	0.00000
52	0.00646	0.00000	-0.07122	0.00000	0.00000	0.00000
53	-0.00154	0.00000	-0.12486	0.00000	0.00000	0.00000
54	0.11359	0.00000	-0.85576	0.00000	0.00000	0.00000
55	0.08447	1.30114	-0.39444	0.00000	0.00683	0.00000
115	-0.00002	0.19923	0.33024	0.00000	0.00000	0.00000
116	0.00015	-1.07085	-2.50894	0.00000	0.00000	0.00000
131	0.00000	-0.05385	-0.23530	0.00000	0.00000	0.00000
132	0.00000	-0.03334	-0.18948	0.00000	0.00000	0.00000
133	0.00004	-0.45059	-1.12190	0.00000	0.00000	0.00000
134	0.00003	-0.27440	-0.72810	0.00000	0.00000	0.00000
150	-0.25434	0.41060	-0.43296	0.00000	-0.00976	0.00000

SUM 2.37135 2.29248 -7.27292 0.00000 0.00014 0.00000

Condition **LC7=1.2D-1.6Wo**

1	0.00740	0.08701	-0.00421	0.00000	0.00373	0.00000
2	0.06790	0.00000	-0.06801	0.00000	0.00000	0.00000
3	-0.15229	0.00000	-0.07453	0.00000	0.00000	0.00000
4	0.06660	0.00000	-0.09344	0.00000	0.00000	0.00000
5	-0.15986	0.00000	0.00100	0.00000	0.00000	0.00000
6	0.22956	0.95881	-0.21733	0.00000	0.00051	0.00000
17	-0.10505	1.07119	-0.13005	0.00000	-0.00042	0.00000
45	0.23377	0.09327	-0.11020	0.00000	-0.00580	0.00000

50	-0.00278	0.20950	0.09049	0.00000	0.00247	0.00000
51	0.01755	0.00000	-0.27028	0.00000	0.00000	0.00000
52	0.00826	0.00000	-0.10320	0.00000	0.00000	0.00000
53	-0.00328	0.00000	-0.02583	0.00000	0.00000	0.00000
54	0.08174	0.00000	-0.95174	0.00000	0.00000	0.00000
55	0.12011	1.43628	-0.40952	0.00000	0.00812	0.00000
115	0.00000	0.28437	0.52054	0.00000	0.00000	0.00000
116	-0.00001	-1.28681	-2.99205	0.00000	0.00000	0.00000
131	0.00000	-0.06634	-0.26324	0.00000	0.00000	0.00000
132	0.00000	-0.02812	-0.17780	0.00000	0.00000	0.00000
133	0.00000	-0.56860	-1.38549	0.00000	0.00000	0.00000
134	0.00000	-0.30257	-0.79109	0.00000	0.00000	0.00000
150	-0.40961	0.40450	-0.42845	0.00000	-0.01114	0.00000

SUM	0.00000	2.29248	-7.88442	0.00000	-0.00255	0.00000
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Condition **LC8=1.2D-1.6W30**

1	0.01101	0.09046	-0.00407	0.00000	0.00366	0.00000
2	-0.03029	0.00000	-0.06584	0.00000	0.00000	0.00000
3	-0.15242	0.00000	-0.07454	0.00000	0.00000	0.00000
4	-0.10337	0.00000	-0.09338	0.00000	0.00000	0.00000
5	-1.96882	0.00000	-0.00434	0.00000	0.00000	0.00000
6	0.18037	0.80987	-0.23665	0.00000	0.00077	0.00000
17	-0.12616	1.01072	-0.16738	0.00000	-0.00029	0.00000
45	0.20857	0.16121	-0.15385	0.00000	-0.00290	0.00000
50	-0.00028	0.20831	0.18790	0.00000	-0.00259	0.00000
51	-0.03186	0.00000	-0.34613	0.00000	0.00000	0.00000
52	0.00955	0.00000	-0.23649	0.00000	0.00000	0.00000
53	-0.00451	0.00000	-0.08536	0.00000	0.00000	0.00000
54	0.02465	0.00000	-0.85153	0.00000	0.00000	0.00000
55	0.04719	1.24691	-0.38568	0.00000	0.00647	0.00000
115	0.00002	0.18223	0.29230	0.00000	0.00000	0.00000
116	-0.00015	-1.03116	-2.42021	0.00000	0.00000	0.00000
131	-0.00001	-0.08574	-0.30659	0.00000	0.00000	0.00000
132	0.00000	-0.02230	-0.16481	0.00000	0.00000	0.00000
133	-0.00005	-0.45989	-1.14261	0.00000	0.00000	0.00000
134	-0.00003	-0.25558	-0.68618	0.00000	0.00000	0.00000
150	-0.43477	0.43744	-0.32748	0.00000	-0.00941	0.00000

SUM	-2.37135	2.29248	-7.27292	0.00000	-0.00429	0.00000
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Condition **LC9=1.2D-1.6W60**

1	-0.04252	0.03629	0.00039	0.00000	0.00005	0.00000
2	-0.57858	0.00000	-0.00675	0.00000	0.00000	0.00000
3	-0.30998	0.00000	0.00047	0.00000	0.00000	0.00000
4	-0.57317	0.00000	0.00014	0.00000	0.00000	0.00000
5	-3.14349	0.00000	-0.00070	0.00000	0.00000	0.00000
6	0.16761	0.47052	0.04696	0.00000	0.00040	0.00000
17	-0.15858	0.61501	0.06076	0.00000	0.00044	0.00000
45	0.16174	0.30359	-0.30689	0.00000	0.01021	0.00000
50	-0.00164	0.20370	0.56409	0.00000	-0.02414	0.00000
51	-0.23051	0.00000	-0.33943	0.00000	0.00000	0.00000
52	-0.07278	0.00000	-0.59067	0.00000	0.00000	0.00000
53	-0.11469	0.00000	0.13144	0.00000	0.00000	0.00000
54	-0.18748	0.00000	-0.29003	0.00000	0.00000	0.00000
55	-0.00795	0.79144	0.00767	0.00000	0.00190	0.00000
115	-0.14022	0.07531	0.11062	0.00000	0.00000	0.00000
116	-0.14031	-0.31479	-0.76125	0.00000	0.00000	0.00000
131	-0.14023	0.02008	-0.01279	0.00000	0.00000	0.00000

132	-0.14023	0.02778	0.00442	0.00000	0.00000	0.00000
133	-0.14026	-0.19720	-0.49834	0.00000	0.00000	0.00000
134	-0.14025	-0.06186	-0.19592	0.00000	0.00000	0.00000
150	-0.40260	0.32260	0.22148	0.00000	-0.00284	0.00000

SUM	-6.33611	2.29248	-1.85432	0.00000	-0.01398	0.00000
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Condition **LC10=1.2D-1.6W90**

1	-0.01870	0.05344	0.00035	0.00000	-0.00003	0.00000
2	-0.46294	0.00000	-0.00192	0.00000	0.00000	0.00000
3	-0.19421	0.00000	0.00045	0.00000	0.00000	0.00000
4	-0.39185	0.00000	-0.00012	0.00000	0.00000	0.00000
5	-3.25732	0.00000	-0.00092	0.00000	0.00000	0.00000
6	0.07126	0.29041	0.00888	0.00000	0.00057	0.00000
17	-0.17213	0.41543	0.00515	0.00000	0.00012	0.00000
45	0.18495	0.29019	-0.35051	0.00000	0.01282	0.00000
50	0.00042	0.19716	0.64047	0.00000	-0.02788	0.00000
51	-0.26447	0.00000	-0.21746	0.00000	0.00000	0.00000
52	-0.07242	0.00000	-0.66662	0.00000	0.00000	0.00000
53	-0.11515	0.00000	0.14085	0.00000	0.00000	0.00000
54	-0.23540	0.00000	0.03140	0.00000	0.00000	0.00000
55	-0.09423	0.48290	0.01173	0.00000	-0.00055	0.00000
115	-0.14024	-0.02503	-0.11361	0.00000	0.00000	0.00000
116	-0.14021	0.12560	0.22301	0.00000	0.00000	0.00000
131	-0.14023	0.01286	-0.02893	0.00000	0.00000	0.00000
132	-0.14023	0.02832	0.00562	0.00000	0.00000	0.00000
133	-0.14023	0.01393	-0.02655	0.00000	0.00000	0.00000
134	-0.14023	0.03360	0.01743	0.00000	0.00000	0.00000
150	-0.30015	0.37366	0.32131	0.00000	-0.00047	0.00000

SUM	-6.16371	2.29248	0.00000	0.00000	-0.01542	0.00000
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Condition **LC11=1.2D-1.6W120**

1	-0.00692	0.07167	0.00064	0.00000	-0.00013	0.00000
2	-0.41924	0.00000	0.00219	0.00000	0.00000	0.00000
3	-0.21705	0.00000	0.00085	0.00000	0.00000	0.00000
4	-0.46115	0.00000	-0.00036	0.00000	0.00000	0.00000
5	-3.22117	0.00000	-0.00125	0.00000	0.00000	0.00000
6	-0.04129	0.11431	-0.02928	0.00000	0.00076	0.00000
17	-0.19322	0.21990	-0.04814	0.00000	-0.00015	0.00000
45	0.13511	0.29007	-0.34506	0.00000	0.01284	0.00000
50	0.00062	0.18694	0.60666	0.00000	-0.02599	0.00000
51	-0.24560	0.00000	-0.04069	0.00000	0.00000	0.00000
52	-0.07418	0.00000	-0.63167	0.00000	0.00000	0.00000
53	-0.11401	0.00000	0.13347	0.00000	0.00000	0.00000
54	-0.23335	0.00000	0.35726	0.00000	0.00000	0.00000
55	-0.19529	0.18845	0.01356	0.00000	-0.00269	0.00000
115	-0.14026	-0.11268	-0.30950	0.00000	0.00000	0.00000
116	-0.14011	0.54175	1.15276	0.00000	0.00000	0.00000
131	-0.14023	0.00706	-0.04189	0.00000	0.00000	0.00000
132	-0.14023	0.02871	0.00649	0.00000	0.00000	0.00000
133	-0.14020	0.22606	0.44757	0.00000	0.00000	0.00000
134	-0.14021	0.12782	0.22801	0.00000	0.00000	0.00000
150	-0.20811	0.40242	0.35269	0.00000	0.00199	0.00000

SUM	-6.33611	2.29248	1.85432	0.00000	-0.01338	0.00000
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Condition **LC12=1.2D-1.6W150**

1	-0.04555	0.02263	0.00477	0.00000	-0.00370	0.00000
2	-0.28749	0.00000	0.06222	0.00000	0.00000	0.00000
3	-0.06878	0.00000	0.07561	0.00000	0.00000	0.00000
4	-0.30039	0.00000	0.09300	0.00000	0.00000	0.00000
5	-1.65792	0.00000	0.00294	0.00000	0.00000	0.00000
6	0.04485	-0.21672	0.25418	0.00000	0.00034	0.00000
17	-0.03115	-0.13559	0.18827	0.00000	0.00019	0.00000
45	-0.06705	0.25860	-0.26696	0.00000	0.00778	0.00000
50	0.00510	0.15744	0.30315	0.00000	-0.00827	0.00000
51	-0.07347	0.00000	0.46442	0.00000	0.00000	0.00000
52	0.00558	0.00000	-0.27566	0.00000	0.00000	0.00000
53	-0.00264	0.00000	0.09788	0.00000	0.00000	0.00000
54	-0.10053	0.00000	1.02261	0.00000	0.00000	0.00000
55	0.04126	-0.23965	0.39734	0.00000	-0.00624	0.00000
115	-0.00002	-0.14689	-0.32866	0.00000	0.00000	0.00000
116	0.00014	1.12150	2.50481	0.00000	0.00000	0.00000
131	0.00000	0.11058	0.24670	0.00000	0.00000	0.00000
132	0.00000	0.07899	0.17613	0.00000	0.00000	0.00000
133	0.00004	0.49042	1.09572	0.00000	0.00000	0.00000
134	0.00003	0.31876	0.71204	0.00000	0.00000	0.00000
150	0.16664	0.47239	0.44240	0.00000	0.00900	0.00000

 SUM -2.37135 2.29248 7.27292 0.00000 -0.00090 0.00000

Condition **LC13=0.9D+1.6Wo**

1	-0.02634	0.02234	0.00468	0.00000	-0.00376	0.00000
2	-0.13102	0.00000	0.06482	0.00000	0.00000	0.00000
3	0.00343	0.00000	0.07563	0.00000	0.00000	0.00000
4	-0.08389	0.00000	0.09302	0.00000	0.00000	0.00000
5	0.12815	0.00000	0.00454	0.00000	0.00000	0.00000
6	-0.05849	-0.35045	0.23209	0.00000	0.00012	0.00000
17	0.04391	-0.28978	0.15456	0.00000	0.00024	0.00000
45	-0.10671	0.15074	-0.21202	0.00000	0.00626	0.00000
50	0.00386	0.10182	0.16835	0.00000	-0.00378	0.00000
51	-0.02964	0.00000	0.46257	0.00000	0.00000	0.00000
52	0.00207	0.00000	-0.17516	0.00000	0.00000	0.00000
53	-0.00038	0.00000	0.03201	0.00000	0.00000	0.00000
54	-0.07048	0.00000	1.07994	0.00000	0.00000	0.00000
55	-0.01350	-0.51007	0.41621	0.00000	-0.00762	0.00000
115	0.00000	-0.24302	-0.52902	0.00000	0.00000	0.00000
116	-0.00001	1.33276	2.99082	0.00000	0.00000	0.00000
131	0.00000	0.11534	0.27174	0.00000	0.00000	0.00000
132	0.00000	0.06909	0.16841	0.00000	0.00000	0.00000
133	0.00000	0.60377	1.36356	0.00000	0.00000	0.00000
134	0.00000	0.34228	0.77898	0.00000	0.00000	0.00000
150	0.33904	0.37454	0.43868	0.00000	0.01060	0.00000

 SUM 0.00000 1.71936 7.88442 0.00000 0.00207 0.00000

Condition **LC14=0.9D+1.6W30**

1	-0.02916	0.01876	0.00457	0.00000	-0.00370	0.00000
2	-0.01005	0.00000	0.06227	0.00000	0.00000	0.00000
3	0.04187	0.00000	0.07564	0.00000	0.00000	0.00000
4	-0.03681	0.00000	0.09312	0.00000	0.00000	0.00000
5	2.00359	0.00000	0.00817	0.00000	0.00000	0.00000
6	-0.01284	-0.20160	0.25191	0.00000	-0.00018	0.00000
17	0.06689	-0.22972	0.19157	0.00000	0.00012	0.00000
45	-0.08696	0.08113	-0.17039	0.00000	0.00333	0.00000
50	0.00127	0.10248	0.06704	0.00000	0.00138	0.00000

51	0.01970	0.00000	0.54955	0.00000	0.00000	0.00000
52	0.00072	0.00000	-0.03763	0.00000	0.00000	0.00000
53	0.00082	0.00000	0.06583	0.00000	0.00000	0.00000
54	-0.01528	0.00000	0.99735	0.00000	0.00000	0.00000
55	0.05631	-0.32052	0.38983	0.00000	-0.00606	0.00000
115	0.00002	-0.14407	-0.30790	0.00000	0.00000	0.00000
116	-0.00016	1.07879	2.42380	0.00000	0.00000	0.00000
131	-0.00001	0.13515	0.31600	0.00000	0.00000	0.00000
132	0.00000	0.06392	0.15686	0.00000	0.00000	0.00000
133	-0.00005	0.49435	1.11895	0.00000	0.00000	0.00000
134	-0.00003	0.29618	0.67586	0.00000	0.00000	0.00000
150	0.37150	0.34452	0.34052	0.00000	0.00893	0.00000
SUM	2.37135	1.71936	7.27292	0.00000	0.00383	0.00000

Condition **LC15=0.9D+1.6W60**

1	0.03160	0.07784	0.00032	0.00000	-0.00003	0.00000
2	0.73850	0.00000	0.00286	0.00000	0.00000	0.00000
3	0.00079	0.00000	0.00103	0.00000	0.00000	0.00000
4	0.04812	0.00000	-0.00063	0.00000	0.00000	0.00000
5	3.41232	0.00000	0.00614	0.00000	0.00000	0.00000
6	-0.00494	0.13895	-0.03215	0.00000	-0.00001	0.00000
17	0.12625	0.16337	-0.03556	0.00000	-0.00072	0.00000
45	0.00971	-0.10478	-0.04318	0.00000	-0.00996	0.00000
50	0.00261	0.11295	-0.30755	0.00000	0.02326	0.00000
51	0.21843	0.00000	0.76569	0.00000	0.00000	0.00000
52	0.08349	0.00000	0.10165	0.00000	0.00000	0.00000
53	0.11101	0.00000	-0.16881	0.00000	0.00000	0.00000
54	0.19468	0.00000	0.46619	0.00000	0.00000	0.00000
55	0.13570	0.13603	-0.00873	0.00000	-0.00162	0.00000
115	0.14024	-0.03285	-0.11665	0.00000	0.00000	0.00000
116	0.14015	0.36049	0.76219	0.00000	0.00000	0.00000
131	0.14023	0.03036	0.02459	0.00000	0.00000	0.00000
132	0.14023	0.01279	-0.01468	0.00000	0.00000	0.00000
133	0.14020	0.23077	0.47254	0.00000	0.00000	0.00000
134	0.14022	0.10136	0.18327	0.00000	0.00000	0.00000
150	0.38658	0.49207	-0.20422	0.00000	0.00218	0.00000
SUM	6.33611	1.71936	1.85432	0.00000	0.01311	0.00000

Condition **LC16=0.9D+1.6W90**

1	0.00279	0.05721	0.00021	0.00000	0.00002	0.00000
2	0.50475	0.00000	-0.00157	0.00000	0.00000	0.00000
3	-0.00840	0.00000	0.00076	0.00000	0.00000	0.00000
4	0.00937	0.00000	-0.00030	0.00000	0.00000	0.00000
5	3.43444	0.00000	0.00650	0.00000	0.00000	0.00000
6	0.10130	0.31887	0.00594	0.00000	-0.00004	0.00000
17	0.12829	0.36440	0.02051	0.00000	-0.00037	0.00000
45	-0.03478	-0.08881	0.00778	0.00000	-0.01259	0.00000
50	0.00067	0.12217	-0.37850	0.00000	0.02698	0.00000
51	0.25294	0.00000	0.69355	0.00000	0.00000	0.00000
52	0.08350	0.00000	0.10720	0.00000	0.00000	0.00000
53	0.11151	0.00000	-0.17741	0.00000	0.00000	0.00000
54	0.24419	0.00000	0.15044	0.00000	0.00000	0.00000
55	0.21514	0.44449	-0.01384	0.00000	0.00097	0.00000
115	0.14022	0.06998	0.11311	0.00000	0.00000	0.00000
116	0.14026	-0.08129	-0.22491	0.00000	0.00000	0.00000
131	0.14023	0.03695	0.03931	0.00000	0.00000	0.00000
132	0.14023	0.01236	-0.01564	0.00000	0.00000	0.00000

133	0.14023	0.02046	0.00247	0.00000	0.00000	0.00000
134	0.14023	0.00544	-0.03109	0.00000	0.00000	0.00000
150	0.27659	0.43714	-0.30451	0.00000	-0.00020	0.00000

SUM	6.16371	1.71936	0.00000	0.00000	0.01478	0.00000
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Condition **LC17=0.9D+1.6W120**

1	-0.01021	0.03772	-0.00009	0.00000	0.00012	0.00000
2	0.44690	0.00000	-0.00560	0.00000	0.00000	0.00000
3	0.03955	0.00000	0.00029	0.00000	0.00000	0.00000
4	0.05760	0.00000	-0.00006	0.00000	0.00000	0.00000
5	3.40469	0.00000	0.00706	0.00000	0.00000	0.00000
6	0.21817	0.49656	0.04379	0.00000	-0.00019	0.00000
17	0.13935	0.55799	0.07412	0.00000	-0.00016	0.00000
45	0.03235	-0.08829	0.00108	0.00000	-0.01253	0.00000
50	0.00052	0.13109	-0.34225	0.00000	0.02491	0.00000
51	0.23444	0.00000	0.48512	0.00000	0.00000	0.00000
52	0.08526	0.00000	0.09751	0.00000	0.00000	0.00000
53	0.11036	0.00000	-0.14958	0.00000	0.00000	0.00000
54	0.24437	0.00000	-0.19042	0.00000	0.00000	0.00000
55	0.32523	0.74085	-0.01509	0.00000	0.00321	0.00000
115	0.14020	0.16031	0.31497	0.00000	0.00000	0.00000
116	0.14036	-0.49896	-1.15848	0.00000	0.00000	0.00000
131	0.14023	0.04276	0.05231	0.00000	0.00000	0.00000
132	0.14023	0.01182	-0.01684	0.00000	0.00000	0.00000
133	0.14026	-0.19142	-0.47102	0.00000	0.00000	0.00000
134	0.14025	-0.08934	-0.24288	0.00000	0.00000	0.00000
150	0.16599	0.40826	-0.33827	0.00000	-0.00278	0.00000

SUM	6.33611	1.71936	-1.85432	0.00000	0.01259	0.00000
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Condition **LC18=0.9D+1.6W150**

1	0.02812	0.08661	-0.00422	0.00000	0.00372	0.00000
2	0.26575	0.00000	-0.06507	0.00000	0.00000	0.00000
3	-0.05056	0.00000	-0.07449	0.00000	0.00000	0.00000
4	0.05413	0.00000	-0.09360	0.00000	0.00000	0.00000
5	1.74997	0.00000	0.00458	0.00000	0.00000	0.00000
6	0.12947	0.82658	-0.24036	0.00000	0.00027	0.00000
17	-0.03052	0.91535	-0.16299	0.00000	-0.00048	0.00000
45	0.21624	-0.01824	-0.05310	0.00000	-0.00730	0.00000
50	-0.00394	0.15651	-0.04030	0.00000	0.00690	0.00000
51	0.06142	0.00000	-0.20496	0.00000	0.00000	0.00000
52	0.00506	0.00000	-0.06403	0.00000	0.00000	0.00000
53	-0.00102	0.00000	-0.13008	0.00000	0.00000	0.00000
54	0.11236	0.00000	-0.86860	0.00000	0.00000	0.00000
55	0.07242	1.16822	-0.39493	0.00000	0.00676	0.00000
115	-0.00002	0.19302	0.33079	0.00000	0.00000	0.00000
116	0.00015	-1.07692	-2.50809	0.00000	0.00000	0.00000
131	0.00000	-0.06090	-0.23665	0.00000	0.00000	0.00000
132	0.00000	-0.03916	-0.18805	0.00000	0.00000	0.00000
133	0.00004	-0.45547	-1.11836	0.00000	0.00000	0.00000
134	0.00003	-0.27998	-0.72615	0.00000	0.00000	0.00000
150	-0.23775	0.30374	-0.43424	0.00000	-0.00969	0.00000

SUM	2.37135	1.71936	-7.27292	0.00000	0.00020	0.00000
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Condition **LC19=0.9D-1.6W0**

1	0.00991	0.07126	-0.00428	0.00000	0.00373	0.00000
2	0.07767	0.00000	-0.06748	0.00000	0.00000	0.00000
3	-0.13857	0.00000	-0.07470	0.00000	0.00000	0.00000
4	0.05991	0.00000	-0.09338	0.00000	0.00000	0.00000
5	-0.14971	0.00000	0.00022	0.00000	0.00000	0.00000
6	0.20616	0.87199	-0.21979	0.00000	0.00043	0.00000
17	-0.09605	0.95972	-0.13389	0.00000	-0.00040	0.00000
45	0.21578	0.05465	-0.06546	0.00000	-0.00588	0.00000
50	-0.00290	0.16520	0.05449	0.00000	0.00266	0.00000
51	0.01938	0.00000	-0.29288	0.00000	0.00000	0.00000
52	0.00678	0.00000	-0.06449	0.00000	0.00000	0.00000
53	-0.00274	0.00000	-0.03500	0.00000	0.00000	0.00000
54	0.08051	0.00000	-0.96552	0.00000	0.00000	0.00000
55	0.10737	1.30324	-0.41011	0.00000	0.00805	0.00000
115	0.00000	0.27812	0.52098	0.00000	0.00000	0.00000
116	-0.00001	-1.29279	-2.99099	0.00000	0.00000	0.00000
131	0.00000	-0.07337	-0.26451	0.00000	0.00000	0.00000
132	0.00000	-0.03398	-0.17648	0.00000	0.00000	0.00000
133	0.00000	-0.57347	-1.38190	0.00000	0.00000	0.00000
134	0.00000	-0.30814	-0.78910	0.00000	0.00000	0.00000
150	-0.39348	0.29692	-0.43017	0.00000	-0.01106	0.00000

 SUM 0.00000 1.71936 -7.88442 0.00000 -0.00248 0.00000

Condition **LC20=0.9D-1.6W30**

1	0.01351	0.07472	-0.00414	0.00000	0.00366	0.00000
2	-0.02084	0.00000	-0.06532	0.00000	0.00000	0.00000
3	-0.13871	0.00000	-0.07470	0.00000	0.00000	0.00000
4	-0.10925	0.00000	-0.09332	0.00000	0.00000	0.00000
5	-1.95867	0.00000	-0.00505	0.00000	0.00000	0.00000
6	0.15700	0.72312	-0.23904	0.00000	0.00069	0.00000
17	-0.11727	0.89926	-0.17118	0.00000	-0.00027	0.00000
45	0.19047	0.12260	-0.10909	0.00000	-0.00298	0.00000
50	-0.00040	0.16402	0.15184	0.00000	-0.00240	0.00000
51	-0.03003	0.00000	-0.36876	0.00000	0.00000	0.00000
52	0.00807	0.00000	-0.19771	0.00000	0.00000	0.00000
53	-0.00397	0.00000	-0.09456	0.00000	0.00000	0.00000
54	0.02341	0.00000	-0.86537	0.00000	0.00000	0.00000
55	0.03435	1.11396	-0.38609	0.00000	0.00640	0.00000
115	0.00002	0.17605	0.29291	0.00000	0.00000	0.00000
116	-0.00015	-1.03729	-2.41948	0.00000	0.00000	0.00000
131	-0.00001	-0.09273	-0.30780	0.00000	0.00000	0.00000
132	0.00000	-0.02820	-0.16356	0.00000	0.00000	0.00000
133	-0.00004	-0.46481	-1.13914	0.00000	0.00000	0.00000
134	-0.00003	-0.26118	-0.68425	0.00000	0.00000	0.00000
150	-0.41882	0.32985	-0.32910	0.00000	-0.00933	0.00000

 SUM -2.37135 1.71936 -7.27292 0.00000 -0.00422 0.00000

Condition **LC21=0.9D-1.6W60**

1	-0.04014	0.02046	0.00032	0.00000	0.00005	0.00000
2	-0.56931	0.00000	-0.00626	0.00000	0.00000	0.00000
3	-0.29865	0.00000	0.00031	0.00000	0.00000	0.00000
4	-0.57893	0.00000	0.00020	0.00000	0.00000	0.00000
5	-3.13313	0.00000	-0.00138	0.00000	0.00000	0.00000
6	0.14460	0.38388	0.04468	0.00000	0.00032	0.00000
17	-0.14972	0.50360	0.05710	0.00000	0.00046	0.00000
45	0.14444	0.26348	-0.26215	0.00000	0.01012	0.00000
50	-0.00176	0.15943	0.52778	0.00000	-0.02394	0.00000

51	-0.22869	0.00000	-0.36208	0.00000	0.00000	0.00000
52	-0.07426	0.00000	-0.55163	0.00000	0.00000	0.00000
53	-0.11414	0.00000	0.12242	0.00000	0.00000	0.00000
54	-0.18874	0.00000	-0.30425	0.00000	0.00000	0.00000
55	-0.02004	0.65867	0.00760	0.00000	0.00183	0.00000
115	-0.14022	0.06922	0.11144	0.00000	0.00000	0.00000
116	-0.14031	-0.32121	-0.76118	0.00000	0.00000	0.00000
131	-0.14023	0.01310	-0.01398	0.00000	0.00000	0.00000
132	-0.14023	0.02187	0.00563	0.00000	0.00000	0.00000
133	-0.14026	-0.20216	-0.49498	0.00000	0.00000	0.00000
134	-0.14025	-0.06749	-0.19408	0.00000	0.00000	0.00000
150	-0.38611	0.21650	0.22017	0.00000	-0.00276	0.00000
SUM	-6.33611	1.71936	-1.85432	0.00000	-0.01391	0.00000

Condition **LC22=0.9D-1.6W90**

1	-0.01632	0.03760	0.00028	0.00000	-0.00003	0.00000
2	-0.45382	0.00000	-0.00144	0.00000	0.00000	0.00000
3	-0.18292	0.00000	0.00029	0.00000	0.00000	0.00000
4	-0.39767	0.00000	-0.00007	0.00000	0.00000	0.00000
5	-3.24683	0.00000	-0.00160	0.00000	0.00000	0.00000
6	0.04828	0.20381	0.00673	0.00000	0.00050	0.00000
17	-0.16315	0.30410	0.00161	0.00000	0.00014	0.00000
45	0.16760	0.25006	-0.30571	0.00000	0.01273	0.00000
50	0.00029	0.15290	0.60408	0.00000	-0.02767	0.00000
51	-0.26266	0.00000	-0.24018	0.00000	0.00000	0.00000
52	-0.07391	0.00000	-0.62749	0.00000	0.00000	0.00000
53	-0.11460	0.00000	0.13181	0.00000	0.00000	0.00000
54	-0.23667	0.00000	0.01708	0.00000	0.00000	0.00000
55	-0.10626	0.35025	0.01195	0.00000	-0.00062	0.00000
115	-0.14024	-0.03105	-0.11265	0.00000	0.00000	0.00000
116	-0.14021	0.11897	0.22260	0.00000	0.00000	0.00000
131	-0.14023	0.00588	-0.03011	0.00000	0.00000	0.00000
132	-0.14023	0.02241	0.00683	0.00000	0.00000	0.00000
133	-0.14023	0.00891	-0.02334	0.00000	0.00000	0.00000
134	-0.14023	0.02795	0.01921	0.00000	0.00000	0.00000
150	-0.28370	0.26757	0.32015	0.00000	-0.00039	0.00000
SUM	-6.16371	1.71936	0.00000	0.00000	-0.01535	0.00000

Condition **LC23=0.9D-1.6W120**

1	-0.00454	0.05582	0.00057	0.00000	-0.00013	0.00000
2	-0.41027	0.00000	0.00265	0.00000	0.00000	0.00000
3	-0.20580	0.00000	0.00070	0.00000	0.00000	0.00000
4	-0.46703	0.00000	-0.00031	0.00000	0.00000	0.00000
5	-3.21060	0.00000	-0.00193	0.00000	0.00000	0.00000
6	-0.06424	0.02774	-0.03131	0.00000	0.00068	0.00000
17	-0.18411	0.10864	-0.05156	0.00000	-0.00013	0.00000
45	0.11773	0.24992	-0.30020	0.00000	0.01275	0.00000
50	0.00049	0.14269	0.57024	0.00000	-0.02578	0.00000
51	-0.24379	0.00000	-0.06351	0.00000	0.00000	0.00000
52	-0.07567	0.00000	-0.59252	0.00000	0.00000	0.00000
53	-0.11347	0.00000	0.12443	0.00000	0.00000	0.00000
54	-0.23462	0.00000	0.34285	0.00000	0.00000	0.00000
55	-0.20726	0.05592	0.01405	0.00000	-0.00276	0.00000
115	-0.14026	-0.11865	-0.30842	0.00000	0.00000	0.00000
116	-0.14011	0.53493	1.15192	0.00000	0.00000	0.00000
131	-0.14023	0.00008	-0.04307	0.00000	0.00000	0.00000
132	-0.14023	0.02280	0.00770	0.00000	0.00000	0.00000

133	-0.14020	0.22098	0.45063	0.00000	0.00000	0.00000
134	-0.14021	0.12214	0.22973	0.00000	0.00000	0.00000
150	-0.19168	0.29632	0.35167	0.00000	0.00207	0.00000

SUM	-6.33611	1.71936	1.85432	0.00000	-0.01331	0.00000
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Condition **LC24=0.9D-1.6W150**

1	-0.04318	0.00674	0.00470	0.00000	-0.00370	0.00000
2	-0.27859	0.00000	0.06266	0.00000	0.00000	0.00000
3	-0.05745	0.00000	0.07546	0.00000	0.00000	0.00000
4	-0.30605	0.00000	0.09305	0.00000	0.00000	0.00000
5	-1.64741	0.00000	0.00221	0.00000	0.00000	0.00000
6	0.02178	-0.30325	0.25226	0.00000	0.00026	0.00000
17	-0.02201	-0.24679	0.18498	0.00000	0.00021	0.00000
45	-0.08442	0.21843	-0.22203	0.00000	0.00769	0.00000
50	0.00497	0.11326	0.26684	0.00000	-0.00807	0.00000
51	-0.07166	0.00000	0.44146	0.00000	0.00000	0.00000
52	0.00409	0.00000	-0.23660	0.00000	0.00000	0.00000
53	-0.00210	0.00000	0.08888	0.00000	0.00000	0.00000
54	-0.10177	0.00000	1.00802	0.00000	0.00000	0.00000
55	0.02915	-0.37203	0.39812	0.00000	-0.00631	0.00000
115	-0.00002	-0.15283	-0.32752	0.00000	0.00000	0.00000
116	0.00014	1.11449	2.50356	0.00000	0.00000	0.00000
131	0.00000	0.10359	0.24549	0.00000	0.00000	0.00000
132	0.00000	0.07311	0.17740	0.00000	0.00000	0.00000
133	0.00004	0.48532	1.09871	0.00000	0.00000	0.00000
134	0.00003	0.31305	0.71370	0.00000	0.00000	0.00000
150	0.18310	0.36628	0.44158	0.00000	0.00908	0.00000

SUM	-2.37135	1.71936	7.27292	0.00000	-0.00084	0.00000
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Condition **LC25=1.2D+Di+W10**

1	-0.01681	0.13640	0.00087	0.00000	-0.00006	0.00000
2	-0.03987	0.00000	-0.00332	0.00000	0.00000	0.00000
3	-0.10474	0.00000	0.00177	0.00000	0.00000	0.00000
4	0.03980	0.00000	-0.00060	0.00000	0.00000	0.00000
5	-0.07949	0.00000	0.00705	0.00000	0.00000	0.00000
6	0.18103	0.72715	0.00749	0.00000	0.00080	0.00000
17	-0.10153	0.81063	0.00605	0.00000	-0.00032	0.00000
45	0.12217	0.28628	-0.32799	0.00000	0.00091	0.00000
50	0.00162	0.33076	0.26475	0.00000	-0.00154	0.00000
51	-0.01513	0.00000	0.19675	0.00000	0.00000	0.00000
52	0.01101	0.00000	-0.28959	0.00000	0.00000	0.00000
53	-0.00383	0.00000	0.06248	0.00000	0.00000	0.00000
54	0.00235	0.00000	0.17070	0.00000	0.00000	0.00000
55	0.08041	0.96795	0.00981	0.00000	-0.00020	0.00000
115	0.00000	0.03397	-0.05326	0.00000	0.00000	0.00000
116	0.00000	0.17327	0.25801	0.00000	0.00000	0.00000
131	0.00000	0.06098	0.00708	0.00000	0.00000	0.00000
132	0.00000	0.05248	-0.01191	0.00000	0.00000	0.00000
133	0.00000	0.10855	0.11342	0.00000	0.00000	0.00000
134	0.00000	0.07931	0.04806	0.00000	0.00000	0.00000
150	-0.07699	0.73327	0.03239	0.00000	0.00017	0.00000

SUM	0.00000	4.50098	0.50000	0.00000	-0.00023	0.00000
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Condition **LC26=1.2D+Di+W130**

1	-0.01809	0.13497	0.00085	0.00000	-0.00004	0.00000
2	-0.02984	0.00000	-0.00386	0.00000	0.00000	0.00000
3	-0.10165	0.00000	0.00176	0.00000	0.00000	0.00000
4	0.03964	0.00000	-0.00058	0.00000	0.00000	0.00000
5	0.17131	0.00000	0.00765	0.00000	0.00000	0.00000
6	0.19220	0.75468	0.01197	0.00000	0.00075	0.00000
17	-0.09093	0.83547	0.01517	0.00000	-0.00031	0.00000
45	0.12418	0.27679	-0.32021	0.00000	0.00042	0.00000
50	0.00124	0.33111	0.24800	0.00000	-0.00072	0.00000
51	-0.00744	0.00000	0.19878	0.00000	0.00000	0.00000
52	0.01083	0.00000	-0.27295	0.00000	0.00000	0.00000
53	-0.00365	0.00000	0.06046	0.00000	0.00000	0.00000
54	0.01139	0.00000	0.14689	0.00000	0.00000	0.00000
55	0.09367	1.00321	0.00855	0.00000	0.00007	0.00000
115	0.00000	0.04373	-0.03146	0.00000	0.00000	0.00000
116	0.00000	0.12500	0.15015	0.00000	0.00000	0.00000
131	0.00000	0.06377	0.01332	0.00000	0.00000	0.00000
132	0.00000	0.05174	-0.01356	0.00000	0.00000	0.00000
133	0.00000	0.08413	0.05884	0.00000	0.00000	0.00000
134	0.00000	0.06770	0.02212	0.00000	0.00000	0.00000
150	-0.07327	0.72867	0.01772	0.00000	-0.00009	0.00000

 SUM 0.31961 4.50098 0.31961 0.00000 0.00009 0.00000

Condition **LC27=1.2D+Di+W160**

1	-0.01917	0.13396	0.00084	0.00000	-0.00004	0.00000
2	-0.03593	0.00000	-0.00409	0.00000	0.00000	0.00000
3	-0.10660	0.00000	0.00174	0.00000	0.00000	0.00000
4	0.04002	0.00000	-0.00057	0.00000	0.00000	0.00000
5	0.11579	0.00000	0.00752	0.00000	0.00000	0.00000
6	0.19816	0.76187	0.01395	0.00000	0.00075	0.00000
17	-0.09002	0.84425	0.01846	0.00000	-0.00029	0.00000
45	0.12201	0.27890	-0.31754	0.00000	0.00033	0.00000
50	0.00119	0.33161	0.24630	0.00000	-0.00060	0.00000
51	-0.00661	0.00000	0.20160	0.00000	0.00000	0.00000
52	0.01082	0.00000	-0.27116	0.00000	0.00000	0.00000
53	-0.00365	0.00000	0.06003	0.00000	0.00000	0.00000
54	0.01278	0.00000	0.14378	0.00000	0.00000	0.00000
55	0.09800	1.01560	0.00847	0.00000	0.00017	0.00000
115	0.00000	0.04795	-0.02204	0.00000	0.00000	0.00000
116	0.00000	0.10675	0.10937	0.00000	0.00000	0.00000
131	0.00000	0.06354	0.01282	0.00000	0.00000	0.00000
132	0.00000	0.05190	-0.01321	0.00000	0.00000	0.00000
133	0.00000	0.07327	0.03457	0.00000	0.00000	0.00000
134	0.00000	0.06379	0.01337	0.00000	0.00000	0.00000
150	-0.07798	0.72757	0.01456	0.00000	-0.00018	0.00000

 SUM 0.25880 4.50098 0.25880 0.00000 0.00013 0.00000

Condition **LC28=1.2D+Di+W190**

1	-0.02140	0.13177	0.00082	0.00000	-0.00002	0.00000
2	-0.04013	0.00000	-0.00469	0.00000	0.00000	0.00000
3	-0.11251	0.00000	0.00172	0.00000	0.00000	0.00000
4	0.04051	0.00000	-0.00054	0.00000	0.00000	0.00000
5	0.15667	0.00000	0.00762	0.00000	0.00000	0.00000
6	0.21241	0.78610	0.01906	0.00000	0.00072	0.00000
17	-0.08414	0.87217	0.02660	0.00000	-0.00025	0.00000
45	0.12315	0.27698	-0.31212	0.00000	-0.00006	0.00000
50	0.00090	0.33254	0.23537	0.00000	-0.00006	0.00000

51	-0.00166	0.00000	0.18551	0.00000	0.00000	0.00000
52	0.01077	0.00000	-0.26030	0.00000	0.00000	0.00000
53	-0.00358	0.00000	0.05869	0.00000	0.00000	0.00000
54	0.01974	0.00000	0.09739	0.00000	0.00000	0.00000
55	0.11249	1.05765	0.00611	0.00000	0.00053	0.00000
115	0.00000	0.06106	0.00726	0.00000	0.00000	0.00000
116	0.00000	0.04665	-0.02492	0.00000	0.00000	0.00000
131	0.00000	0.06455	0.01508	0.00000	0.00000	0.00000
132	0.00000	0.05178	-0.01347	0.00000	0.00000	0.00000
133	0.00000	0.04535	-0.02784	0.00000	0.00000	0.00000
134	0.00000	0.05058	-0.01616	0.00000	0.00000	0.00000
150	-0.08921	0.72379	-0.00119	0.00000	-0.00055	0.00000

SUM	0.32400	4.50098	0.00000	0.00000	0.00030	0.00000

Condition **LC29=1.2D+Di+W1120**

1	-0.02378	0.12946	0.00081	0.00000	-0.00001	0.00000
2	-0.05895	0.00000	-0.00529	0.00000	0.00000	0.00000
3	-0.12254	0.00000	0.00170	0.00000	0.00000	0.00000
4	0.04114	0.00000	-0.00051	0.00000	0.00000	0.00000
5	0.11684	0.00000	0.00760	0.00000	0.00000	0.00000
6	0.22509	0.80864	0.02417	0.00000	0.00070	0.00000
17	-0.08235	0.89922	0.03435	0.00000	-0.00020	0.00000
45	0.12755	0.27950	-0.31250	0.00000	-0.00005	0.00000
50	0.00088	0.33402	0.24072	0.00000	-0.00035	0.00000
51	-0.00437	0.00000	0.15992	0.00000	0.00000	0.00000
52	0.01103	0.00000	-0.26584	0.00000	0.00000	0.00000
53	-0.00374	0.00000	0.05989	0.00000	0.00000	0.00000
54	0.01951	0.00000	0.05050	0.00000	0.00000	0.00000
55	0.12152	1.09763	0.00431	0.00000	0.00085	0.00000
115	0.00000	0.07231	0.03241	0.00000	0.00000	0.00000
116	0.00000	-0.00982	-0.15112	0.00000	0.00000	0.00000
131	0.00000	0.06517	0.01645	0.00000	0.00000	0.00000
132	0.00000	0.05180	-0.01343	0.00000	0.00000	0.00000
133	0.00000	0.01733	-0.09047	0.00000	0.00000	0.00000
134	0.00000	0.03754	-0.04529	0.00000	0.00000	0.00000
150	-0.10899	0.71819	-0.00716	0.00000	-0.00091	0.00000

SUM	0.25880	4.50098	-0.25880	0.00000	0.00002	0.00000

Condition **LC30=1.2D+Di+W1150**

1	-0.02445	0.12875	0.00080	0.00000	-0.00001	0.00000
2	-0.06179	0.00000	-0.00552	0.00000	0.00000	0.00000
3	-0.12364	0.00000	0.00169	0.00000	0.00000	0.00000
4	0.04118	0.00000	-0.00050	0.00000	0.00000	0.00000
5	0.17380	0.00000	0.00777	0.00000	0.00000	0.00000
6	0.22939	0.81930	0.02612	0.00000	0.00068	0.00000
17	-0.08051	0.90846	0.03766	0.00000	-0.00019	0.00000
45	0.12944	0.27797	-0.31162	0.00000	-0.00005	0.00000
50	0.00086	0.33449	0.24214	0.00000	-0.00043	0.00000
51	-0.00509	0.00000	0.16071	0.00000	0.00000	0.00000
52	0.01111	0.00000	-0.26733	0.00000	0.00000	0.00000
53	-0.00379	0.00000	0.06029	0.00000	0.00000	0.00000
54	0.01953	0.00000	0.04653	0.00000	0.00000	0.00000
55	0.12434	1.11057	0.00416	0.00000	0.00093	0.00000
115	0.00000	0.07563	0.03983	0.00000	0.00000	0.00000
116	0.00000	-0.02717	-0.18991	0.00000	0.00000	0.00000
131	0.00000	0.06606	0.01845	0.00000	0.00000	0.00000
132	0.00000	0.05158	-0.01391	0.00000	0.00000	0.00000

133	0.00000	0.00674	-0.11414	0.00000	0.00000	0.00000
134	0.00000	0.03316	-0.05510	0.00000	0.00000	0.00000
150	-0.11076	0.71543	-0.00773	0.00000	-0.00101	0.00000

SUM	0.31961	4.50098	-0.31961	0.00000	-0.00007	0.00000
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Condition **LC31=1.2D+Di-WI0**

1	-0.02728	0.12614	0.00079	0.00000	0.00000	0.00000
2	-0.09278	0.00000	-0.00606	0.00000	0.00000	0.00000
3	-0.13940	0.00000	0.00166	0.00000	0.00000	0.00000
4	0.03100	0.00000	-0.00047	0.00000	0.00000	0.00000
5	-0.06814	0.00000	0.00725	0.00000	0.00000	0.00000
6	0.24208	0.83329	0.03072	0.00000	0.00068	0.00000
17	-0.08196	0.93025	0.04575	0.00000	-0.00014	0.00000
45	0.12899	0.28817	-0.31313	0.00000	0.00017	0.00000
50	0.00103	0.33625	0.25623	0.00000	-0.00111	0.00000
51	-0.01172	0.00000	0.14524	0.00000	0.00000	0.00000
52	0.01146	0.00000	-0.28141	0.00000	0.00000	0.00000
53	-0.00406	0.00000	0.06221	0.00000	0.00000	0.00000
54	0.01488	0.00000	0.02389	0.00000	0.00000	0.00000
55	0.12967	1.13926	0.00431	0.00000	0.00116	0.00000
115	0.00000	0.08319	0.05672	0.00000	0.00000	0.00000
116	0.00000	-0.06914	-0.28370	0.00000	0.00000	0.00000
131	0.00000	0.06479	0.01560	0.00000	0.00000	0.00000
132	0.00000	0.05221	-0.01251	0.00000	0.00000	0.00000
133	0.00000	-0.01872	-0.17104	0.00000	0.00000	0.00000
134	0.00000	0.02353	-0.07661	0.00000	0.00000	0.00000
150	-0.13378	0.71176	-0.00544	0.00000	-0.00124	0.00000

SUM	0.00000	4.50098	-0.50000	0.00000	-0.00047	0.00000
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Condition **LC32=1.2D+Di-WI30**

1	-0.02604	0.12743	0.00082	0.00000	-0.00001	0.00000
2	-0.10090	0.00000	-0.00552	0.00000	0.00000	0.00000
3	-0.13755	0.00000	0.00167	0.00000	0.00000	0.00000
4	0.01012	0.00000	-0.00048	0.00000	0.00000	0.00000
5	-0.30757	0.00000	0.00666	0.00000	0.00000	0.00000
6	0.23136	0.80594	0.02623	0.00000	0.00073	0.00000
17	-0.09271	0.90543	0.03665	0.00000	-0.00016	0.00000
45	0.12780	0.29664	-0.32104	0.00000	0.00065	0.00000
50	0.00141	0.33590	0.27293	0.00000	-0.00193	0.00000
51	-0.01940	0.00000	0.14334	0.00000	0.00000	0.00000
52	0.01164	0.00000	-0.29800	0.00000	0.00000	0.00000
53	-0.00423	0.00000	0.06421	0.00000	0.00000	0.00000
54	0.00582	0.00000	0.04770	0.00000	0.00000	0.00000
55	0.11698	1.10394	0.00552	0.00000	0.00089	0.00000
115	0.00000	0.07345	0.03495	0.00000	0.00000	0.00000
116	0.00000	-0.02088	-0.17584	0.00000	0.00000	0.00000
131	0.00000	0.06205	0.00947	0.00000	0.00000	0.00000
132	0.00000	0.05293	-0.01091	0.00000	0.00000	0.00000
133	0.00000	0.00565	-0.11658	0.00000	0.00000	0.00000
134	0.00000	0.03513	-0.05068	0.00000	0.00000	0.00000
150	-0.13635	0.71738	0.00928	0.00000	-0.00097	0.00000

SUM	-0.31961	4.50098	-0.31961	0.00000	-0.00081	0.00000
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Condition **LC33=1.2D+Di-WI60**

1	-0.02493	0.12850	0.00082	0.00000	-0.00001	0.00000
2	-0.09557	0.00000	-0.00529	0.00000	0.00000	0.00000
3	-0.13491	0.00000	0.00168	0.00000	0.00000	0.00000
4	0.01901	0.00000	-0.00050	0.00000	0.00000	0.00000
5	-0.25703	0.00000	0.00679	0.00000	0.00000	0.00000
6	0.22521	0.79868	0.02426	0.00000	0.00073	0.00000
17	-0.09355	0.89664	0.03336	0.00000	-0.00018	0.00000
45	0.12961	0.29492	-0.32365	0.00000	0.00075	0.00000
50	0.00147	0.33540	0.27463	0.00000	-0.00204	0.00000
51	-0.02024	0.00000	0.14046	0.00000	0.00000	0.00000
52	0.01165	0.00000	-0.29978	0.00000	0.00000	0.00000
53	-0.00423	0.00000	0.06464	0.00000	0.00000	0.00000
54	0.00443	0.00000	0.05082	0.00000	0.00000	0.00000
55	0.11242	1.09154	0.00559	0.00000	0.00079	0.00000
115	0.00000	0.06922	0.02550	0.00000	0.00000	0.00000
116	0.00000	-0.00262	-0.13504	0.00000	0.00000	0.00000
131	0.00000	0.06225	0.00992	0.00000	0.00000	0.00000
132	0.00000	0.05278	-0.01124	0.00000	0.00000	0.00000
133	0.00000	0.01653	-0.09226	0.00000	0.00000	0.00000
134	0.00000	0.03905	-0.04193	0.00000	0.00000	0.00000
150	-0.13213	0.71811	0.01242	0.00000	-0.00088	0.00000
SUM	-0.25880	4.50098	-0.25880	0.00000	-0.00085	0.00000

Condition **LC34=1.2D+Di-WI90**

1	-0.02269	0.13072	0.00084	0.00000	-0.00003	0.00000
2	-0.09164	0.00000	-0.00469	0.00000	0.00000	0.00000
3	-0.13005	0.00000	0.00170	0.00000	0.00000	0.00000
4	0.02230	0.00000	-0.00053	0.00000	0.00000	0.00000
5	-0.29995	0.00000	0.00669	0.00000	0.00000	0.00000
6	0.21089	0.77442	0.01915	0.00000	0.00076	0.00000
17	-0.09939	0.86870	0.02522	0.00000	-0.00021	0.00000
45	0.12833	0.29700	-0.32904	0.00000	0.00114	0.00000
50	0.00176	0.33447	0.28557	0.00000	-0.00259	0.00000
51	-0.02519	0.00000	0.15653	0.00000	0.00000	0.00000
52	0.01170	0.00000	-0.31065	0.00000	0.00000	0.00000
53	-0.00430	0.00000	0.06599	0.00000	0.00000	0.00000
54	-0.00252	0.00000	0.09719	0.00000	0.00000	0.00000
55	0.09785	1.04948	0.00795	0.00000	0.00044	0.00000
115	0.00000	0.05612	-0.00377	0.00000	0.00000	0.00000
116	0.00000	0.05747	-0.00075	0.00000	0.00000	0.00000
131	0.00000	0.06123	0.00764	0.00000	0.00000	0.00000
132	0.00000	0.05290	-0.01097	0.00000	0.00000	0.00000
133	0.00000	0.04446	-0.02983	0.00000	0.00000	0.00000
134	0.00000	0.05226	-0.01240	0.00000	0.00000	0.00000
150	-0.12110	0.72175	0.02816	0.00000	-0.00052	0.00000
SUM	-0.32400	4.50098	0.00000	0.00000	-0.00101	0.00000

Condition **LC35=1.2D+Di-WI120**

1	-0.02029	0.13312	0.00085	0.00000	-0.00004	0.00000
2	-0.07412	0.00000	-0.00409	0.00000	0.00000	0.00000
3	-0.12324	0.00000	0.00173	0.00000	0.00000	0.00000
4	0.03572	0.00000	-0.00056	0.00000	0.00000	0.00000
5	-0.26772	0.00000	0.00670	0.00000	0.00000	0.00000
6	0.19791	0.75176	0.01404	0.00000	0.00078	0.00000
17	-0.10110	0.84164	0.01746	0.00000	-0.00026	0.00000
45	0.12338	0.29514	-0.32859	0.00000	0.00113	0.00000
50	0.00178	0.33299	0.28026	0.00000	-0.00230	0.00000

51	-0.02248	0.00000	0.18205	0.00000	0.00000	0.00000
52	0.01144	0.00000	-0.30515	0.00000	0.00000	0.00000
53	-0.00414	0.00000	0.06480	0.00000	0.00000	0.00000
54	-0.00227	0.00000	0.14408	0.00000	0.00000	0.00000
55	0.08841	1.00953	0.00977	0.00000	0.00012	0.00000
115	0.00000	0.04486	-0.02894	0.00000	0.00000	0.00000
116	0.00000	0.11395	0.12546	0.00000	0.00000	0.00000
131	0.00000	0.06058	0.00620	0.00000	0.00000	0.00000
132	0.00000	0.05289	-0.01098	0.00000	0.00000	0.00000
133	0.00000	0.07251	0.03287	0.00000	0.00000	0.00000
134	0.00000	0.06530	0.01674	0.00000	0.00000	0.00000
150	-0.10209	0.72670	0.03410	0.00000	-0.00015	0.00000
SUM	-0.25880	4.50098	0.25880	0.00000	-0.00072	0.00000

Condition **LC36=1.2D+Di-WI150**

1	-0.01962	0.13381	0.00086	0.00000	-0.00005	0.00000
2	-0.07100	0.00000	-0.00385	0.00000	0.00000	0.00000
3	-0.12145	0.00000	0.00174	0.00000	0.00000	0.00000
4	0.03258	0.00000	-0.00057	0.00000	0.00000	0.00000
5	-0.32301	0.00000	0.00653	0.00000	0.00000	0.00000
6	0.19367	0.74112	0.01209	0.00000	0.00080	0.00000
17	-0.10294	0.83240	0.01415	0.00000	-0.00027	0.00000
45	0.12161	0.29654	-0.32948	0.00000	0.00113	0.00000
50	0.00179	0.33253	0.27885	0.00000	-0.00222	0.00000
51	-0.02176	0.00000	0.18127	0.00000	0.00000	0.00000
52	0.01136	0.00000	-0.30366	0.00000	0.00000	0.00000
53	-0.00410	0.00000	0.06440	0.00000	0.00000	0.00000
54	-0.00229	0.00000	0.14803	0.00000	0.00000	0.00000
55	0.08570	0.99659	0.00992	0.00000	0.00003	0.00000
115	0.00000	0.04156	-0.03631	0.00000	0.00000	0.00000
116	0.00000	0.13129	0.16421	0.00000	0.00000	0.00000
131	0.00000	0.05969	0.00421	0.00000	0.00000	0.00000
132	0.00000	0.05310	-0.01051	0.00000	0.00000	0.00000
133	0.00000	0.08310	0.05653	0.00000	0.00000	0.00000
134	0.00000	0.06968	0.02653	0.00000	0.00000	0.00000
150	-0.10016	0.72957	0.03466	0.00000	-0.00006	0.00000
SUM	-0.31961	4.50098	0.31961	0.00000	-0.00063	0.00000

Condition **LC37=0.9D**

1	-0.00744	0.04737	0.00021	0.00000	-0.00001	0.00000
2	-0.02840	0.00000	-0.00143	0.00000	0.00000	0.00000
3	-0.04081	0.00000	0.00048	0.00000	0.00000	0.00000
4	0.01383	0.00000	-0.00017	0.00000	0.00000	0.00000
5	-0.02734	0.00000	0.00235	0.00000	0.00000	0.00000
6	0.07029	0.26014	0.00645	0.00000	0.00025	0.00000
17	-0.02727	0.33403	0.01067	0.00000	-0.00007	0.00000
45	0.05442	0.11614	-0.13462	0.00000	0.00025	0.00000
50	0.00037	0.13279	0.10844	0.00000	-0.00058	0.00000
51	-0.00545	0.00000	0.06881	0.00000	0.00000	0.00000
52	0.00444	0.00000	-0.11662	0.00000	0.00000	0.00000
53	-0.00163	0.00000	0.02691	0.00000	0.00000	0.00000
54	0.00368	0.00000	0.04266	0.00000	0.00000	0.00000
55	0.03877	0.39813	-0.00051	0.00000	0.00022	0.00000
115	0.00000	0.01824	-0.00249	0.00000	0.00000	0.00000
116	0.00000	0.01961	0.00057	0.00000	0.00000	0.00000
131	0.00000	0.02106	0.00381	0.00000	0.00000	0.00000
132	0.00000	0.01755	-0.00403	0.00000	0.00000	0.00000

133	0.00000	0.01499	-0.00976	0.00000	0.00000	0.00000
134	0.00000	0.01692	-0.00545	0.00000	0.00000	0.00000
150	-0.04747	0.32238	0.00373	0.00000	-0.00025	0.00000

SUM	0.00000	1.71936	0.00000	0.00000	-0.00020	0.00000
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Condition **LC38=1.2D**

1	-0.00992	0.06316	0.00028	0.00000	-0.00001	0.00000
2	-0.03788	0.00000	-0.00190	0.00000	0.00000	0.00000
3	-0.05442	0.00000	0.00064	0.00000	0.00000	0.00000
4	0.01844	0.00000	-0.00022	0.00000	0.00000	0.00000
5	-0.03645	0.00000	0.00313	0.00000	0.00000	0.00000
6	0.09372	0.34686	0.00860	0.00000	0.00033	0.00000
17	-0.03635	0.44537	0.01423	0.00000	-0.00009	0.00000
45	0.07257	0.15485	-0.17950	0.00000	0.00033	0.00000
50	0.00049	0.17706	0.14461	0.00000	-0.00077	0.00000
51	-0.00726	0.00000	0.09174	0.00000	0.00000	0.00000
52	0.00592	0.00000	-0.15551	0.00000	0.00000	0.00000
53	-0.00217	0.00000	0.03588	0.00000	0.00000	0.00000
54	0.00491	0.00000	0.05689	0.00000	0.00000	0.00000
55	0.05169	0.53084	-0.00069	0.00000	0.00029	0.00000
115	0.00000	0.02432	-0.00332	0.00000	0.00000	0.00000
116	0.00000	0.02615	0.00076	0.00000	0.00000	0.00000
131	0.00000	0.02808	0.00508	0.00000	0.00000	0.00000
132	0.00000	0.02340	-0.00537	0.00000	0.00000	0.00000
133	0.00000	0.01998	-0.01301	0.00000	0.00000	0.00000
134	0.00000	0.02256	-0.00727	0.00000	0.00000	0.00000
150	-0.06330	0.42985	0.00498	0.00000	-0.00034	0.00000

SUM	0.00000	2.29248	0.00000	0.00000	-0.00027	0.00000
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Condition **LC41=1.2D+WLO**

1	-0.00825	0.06478	0.00029	0.00000	-0.00002	0.00000
2	-0.02956	0.00000	-0.00147	0.00000	0.00000	0.00000
3	-0.04842	0.00000	0.00066	0.00000	0.00000	0.00000
4	0.01803	0.00000	-0.00024	0.00000	0.00000	0.00000
5	-0.03729	0.00000	0.00310	0.00000	0.00000	0.00000
6	0.08397	0.32991	0.00494	0.00000	0.00035	0.00000
17	-0.03926	0.42628	0.00821	0.00000	-0.00012	0.00000
45	0.07158	0.15453	-0.18206	0.00000	0.00045	0.00000
50	0.00058	0.17616	0.14582	0.00000	-0.00084	0.00000
51	-0.00775	0.00000	0.09827	0.00000	0.00000	0.00000
52	0.00584	0.00000	-0.15667	0.00000	0.00000	0.00000
53	-0.00213	0.00000	0.03591	0.00000	0.00000	0.00000
54	0.00297	0.00000	0.07828	0.00000	0.00000	0.00000
55	0.04403	0.50354	0.00028	0.00000	0.00008	0.00000
115	0.00000	0.01656	-0.02066	0.00000	0.00000	0.00000
116	0.00000	0.06474	0.08700	0.00000	0.00000	0.00000
131	0.00000	0.02748	0.00373	0.00000	0.00000	0.00000
132	0.00000	0.02345	-0.00528	0.00000	0.00000	0.00000
133	0.00000	0.04027	0.03233	0.00000	0.00000	0.00000
134	0.00000	0.03147	0.01266	0.00000	0.00000	0.00000
150	-0.05435	0.43331	0.01093	0.00000	-0.00012	0.00000

SUM	0.00000	2.29248	0.15600	0.00000	-0.00022	0.00000
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Condition **LC42=1.2D+WL30**

1	-0.00864	0.06433	0.00029	0.00000	-0.00002	0.00000
2	-0.02651	0.00000	-0.00164	0.00000	0.00000	0.00000
3	-0.04709	0.00000	0.00065	0.00000	0.00000	0.00000
4	0.01794	0.00000	-0.00024	0.00000	0.00000	0.00000
5	0.04128	0.00000	0.00327	0.00000	0.00000	0.00000
6	0.08741	0.33858	0.00633	0.00000	0.00033	0.00000
17	-0.03610	0.43440	0.01074	0.00000	-0.00011	0.00000
45	0.07239	0.15159	-0.17949	0.00000	0.00030	0.00000
50	0.00047	0.17633	0.14096	0.00000	-0.00060	0.00000
51	-0.00552	0.00000	0.10012	0.00000	0.00000	0.00000
52	0.00580	0.00000	-0.15185	0.00000	0.00000	0.00000
53	-0.00208	0.00000	0.03532	0.00000	0.00000	0.00000
54	0.00567	0.00000	0.07193	0.00000	0.00000	0.00000
55	0.04760	0.51522	-0.00056	0.00000	0.00016	0.00000
115	0.00000	0.01958	-0.01391	0.00000	0.00000	0.00000
116	0.00000	0.04893	0.05167	0.00000	0.00000	0.00000
131	0.00000	0.02836	0.00570	0.00000	0.00000	0.00000
132	0.00000	0.02322	-0.00579	0.00000	0.00000	0.00000
133	0.00000	0.03265	0.01528	0.00000	0.00000	0.00000
134	0.00000	0.02761	0.00402	0.00000	0.00000	0.00000
150	-0.05363	0.43170	0.00618	0.00000	-0.00021	0.00000
SUM	0.09899	2.29248	0.09899	0.00000	-0.00014	0.00000

Condition **LC43=1.2D+WL60**

1	-0.00903	0.06397	0.00028	0.00000	-0.00001	0.00000
2	-0.02900	0.00000	-0.00172	0.00000	0.00000	0.00000
3	-0.04903	0.00000	0.00065	0.00000	0.00000	0.00000
4	0.01808	0.00000	-0.00023	0.00000	0.00000	0.00000
5	0.02164	0.00000	0.00323	0.00000	0.00000	0.00000
6	0.08950	0.34117	0.00702	0.00000	0.00033	0.00000
17	-0.03645	0.43709	0.01157	0.00000	-0.00011	0.00000
45	0.07189	0.15230	-0.17896	0.00000	0.00028	0.00000
50	0.00046	0.17649	0.14087	0.00000	-0.00059	0.00000
51	-0.00547	0.00000	0.09974	0.00000	0.00000	0.00000
52	0.00581	0.00000	-0.15176	0.00000	0.00000	0.00000
53	-0.00209	0.00000	0.03530	0.00000	0.00000	0.00000
54	0.00594	0.00000	0.06960	0.00000	0.00000	0.00000
55	0.04958	0.51933	-0.00018	0.00000	0.00019	0.00000
115	0.00000	0.02138	-0.00988	0.00000	0.00000	0.00000
116	0.00000	0.04257	0.03747	0.00000	0.00000	0.00000
131	0.00000	0.02829	0.00555	0.00000	0.00000	0.00000
132	0.00000	0.02327	-0.00567	0.00000	0.00000	0.00000
133	0.00000	0.02878	0.00665	0.00000	0.00000	0.00000
134	0.00000	0.02640	0.00133	0.00000	0.00000	0.00000
150	-0.05546	0.43141	0.00550	0.00000	-0.00024	0.00000
SUM	0.07637	2.29248	0.07637	0.00000	-0.00014	0.00000

Condition **LC44=1.2D+WL90**

1	-0.00972	0.06329	0.00028	0.00000	-0.00001	0.00000
2	-0.03030	0.00000	-0.00190	0.00000	0.00000	0.00000
3	-0.05088	0.00000	0.00064	0.00000	0.00000	0.00000
4	0.01824	0.00000	-0.00022	0.00000	0.00000	0.00000
5	0.03354	0.00000	0.00326	0.00000	0.00000	0.00000
6	0.09391	0.34864	0.00858	0.00000	0.00032	0.00000
17	-0.03420	0.44586	0.01446	0.00000	-0.00010	0.00000
45	0.07164	0.15186	-0.17685	0.00000	0.00015	0.00000
50	0.00036	0.17678	0.13711	0.00000	-0.00039	0.00000

51	-0.00374	0.00000	0.09605	0.00000	0.00000	0.00000
52	0.00578	0.00000	-0.14797	0.00000	0.00000	0.00000
53	-0.00206	0.00000	0.03475	0.00000	0.00000	0.00000
54	0.00825	0.00000	0.05690	0.00000	0.00000	0.00000
55	0.05380	0.53215	-0.00095	0.00000	0.00030	0.00000
115	0.00000	0.02510	-0.00159	0.00000	0.00000	0.00000
116	0.00000	0.02451	-0.00290	0.00000	0.00000	0.00000
131	0.00000	0.02859	0.00622	0.00000	0.00000	0.00000
132	0.00000	0.02324	-0.00575	0.00000	0.00000	0.00000
133	0.00000	0.02011	-0.01272	0.00000	0.00000	0.00000
134	0.00000	0.02229	-0.00786	0.00000	0.00000	0.00000
150	-0.05860	0.43006	0.00047	0.00000	-0.00034	0.00000
SUM	0.09600	2.29248	0.00000	0.00000	-0.00007	0.00000

Condition **LC45=1.2D+WL120**

1	-0.01046	0.06259	0.00027	0.00000	-0.00001	0.00000
2	-0.03632	0.00000	-0.00209	0.00000	0.00000	0.00000
3	-0.05428	0.00000	0.00063	0.00000	0.00000	0.00000
4	0.01844	0.00000	-0.00021	0.00000	0.00000	0.00000
5	0.02216	0.00000	0.00326	0.00000	0.00000	0.00000
6	0.09780	0.35566	0.01014	0.00000	0.00032	0.00000
17	-0.03324	0.45457	0.01714	0.00000	-0.00008	0.00000
45	0.07325	0.15258	-0.17727	0.00000	0.00017	0.00000
50	0.00037	0.17723	0.13936	0.00000	-0.00052	0.00000
51	-0.00485	0.00000	0.08889	0.00000	0.00000	0.00000
52	0.00587	0.00000	-0.15032	0.00000	0.00000	0.00000
53	-0.00212	0.00000	0.03517	0.00000	0.00000	0.00000
54	0.00787	0.00000	0.04406	0.00000	0.00000	0.00000
55	0.05620	0.54384	-0.00153	0.00000	0.00039	0.00000
115	0.00000	0.02792	0.00472	0.00000	0.00000	0.00000
116	0.00000	0.00790	-0.04002	0.00000	0.00000	0.00000
131	0.00000	0.02879	0.00666	0.00000	0.00000	0.00000
132	0.00000	0.02324	-0.00574	0.00000	0.00000	0.00000
133	0.00000	0.01141	-0.03218	0.00000	0.00000	0.00000
134	0.00000	0.01832	-0.01674	0.00000	0.00000	0.00000
150	-0.06432	0.42845	-0.00056	0.00000	-0.00045	0.00000
SUM	0.07637	2.29248	-0.07637	0.00000	-0.00017	0.00000

Condition **LC46=1.2D+WL150**

1	-0.01070	0.06233	0.00027	0.00000	-0.00001	0.00000
2	-0.03700	0.00000	-0.00217	0.00000	0.00000	0.00000
3	-0.05452	0.00000	0.00063	0.00000	0.00000	0.00000
4	0.01845	0.00000	-0.00021	0.00000	0.00000	0.00000
5	0.04218	0.00000	0.00332	0.00000	0.00000	0.00000
6	0.09938	0.35944	0.01081	0.00000	0.00031	0.00000
17	-0.03309	0.45721	0.01806	0.00000	-0.00008	0.00000
45	0.07363	0.15200	-0.17672	0.00000	0.00015	0.00000
50	0.00035	0.17738	0.13920	0.00000	-0.00051	0.00000
51	-0.00480	0.00000	0.08868	0.00000	0.00000	0.00000
52	0.00589	0.00000	-0.15015	0.00000	0.00000	0.00000
53	-0.00213	0.00000	0.03493	0.00000	0.00000	0.00000
54	0.00818	0.00000	0.04162	0.00000	0.00000	0.00000
55	0.05804	0.54863	-0.00122	0.00000	0.00043	0.00000
115	0.00000	0.02975	0.00881	0.00000	0.00000	0.00000
116	0.00000	0.00149	-0.05434	0.00000	0.00000	0.00000
131	0.00000	0.02911	0.00738	0.00000	0.00000	0.00000
132	0.00000	0.02316	-0.00591	0.00000	0.00000	0.00000

133	0.00000	0.00766	-0.04056	0.00000	0.00000	0.00000
134	0.00000	0.01681	-0.02010	0.00000	0.00000	0.00000
150	-0.06486	0.42750	-0.00133	0.00000	-0.00048	0.00000

SUM	0.09899	2.29248	-0.09899	0.00000	-0.00018	0.00000
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Condition **LC47=1.2D-WL0**

1	-0.01159	0.06152	0.00027	0.00000	0.00000	0.00000
2	-0.04604	0.00000	-0.00233	0.00000	0.00000	0.00000
3	-0.05975	0.00000	0.00062	0.00000	0.00000	0.00000
4	0.01650	0.00000	-0.00020	0.00000	0.00000	0.00000
5	-0.03435	0.00000	0.00316	0.00000	0.00000	0.00000
6	0.10350	0.36381	0.01225	0.00000	0.00031	0.00000
17	-0.03347	0.46446	0.02025	0.00000	-0.00006	0.00000
45	0.07365	0.15507	-0.17696	0.00000	0.00021	0.00000
50	0.00040	0.17796	0.14340	0.00000	-0.00071	0.00000
51	-0.00677	0.00000	0.08531	0.00000	0.00000	0.00000
52	0.00600	0.00000	-0.15436	0.00000	0.00000	0.00000
53	-0.00221	0.00000	0.03568	0.00000	0.00000	0.00000
54	0.00685	0.00000	0.03559	0.00000	0.00000	0.00000
55	0.05941	0.55816	-0.00165	0.00000	0.00050	0.00000
115	0.00000	0.03209	0.01403	0.00000	0.00000	0.00000
116	0.00000	-0.01245	-0.08549	0.00000	0.00000	0.00000
131	0.00000	0.02869	0.00644	0.00000	0.00000	0.00000
132	0.00000	0.02336	-0.00547	0.00000	0.00000	0.00000
133	0.00000	-0.00031	-0.05837	0.00000	0.00000	0.00000
134	0.00000	0.01364	-0.02719	0.00000	0.00000	0.00000
150	-0.07213	0.42647	-0.00098	0.00000	-0.00056	0.00000

SUM	0.00000	2.29248	-0.15600	0.00000	-0.00031	0.00000
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Condition **LC48=1.2D-WL30**

1	-0.01121	0.06193	0.00027	0.00000	-0.00001	0.00000
2	-0.04863	0.00000	-0.00217	0.00000	0.00000	0.00000
3	-0.05920	0.00000	0.00062	0.00000	0.00000	0.00000
4	0.00991	0.00000	-0.00021	0.00000	0.00000	0.00000
5	-0.10933	0.00000	0.00299	0.00000	0.00000	0.00000
6	0.10018	0.35519	0.01086	0.00000	0.00033	0.00000
17	-0.03669	0.45635	0.01773	0.00000	-0.00007	0.00000
45	0.07309	0.15775	-0.17958	0.00000	0.00036	0.00000
50	0.00051	0.17779	0.14825	0.00000	-0.00095	0.00000
51	-0.00900	0.00000	0.08343	0.00000	0.00000	0.00000
52	0.00604	0.00000	-0.15918	0.00000	0.00000	0.00000
53	-0.00226	0.00000	0.03644	0.00000	0.00000	0.00000
54	0.00414	0.00000	0.04184	0.00000	0.00000	0.00000
55	0.05597	0.54652	-0.00082	0.00000	0.00041	0.00000
115	0.00000	0.02909	0.00733	0.00000	0.00000	0.00000
116	0.00000	0.00335	-0.05018	0.00000	0.00000	0.00000
131	0.00000	0.02782	0.00450	0.00000	0.00000	0.00000
132	0.00000	0.02358	-0.00497	0.00000	0.00000	0.00000
133	0.00000	0.00730	-0.04137	0.00000	0.00000	0.00000
134	0.00000	0.01750	-0.01857	0.00000	0.00000	0.00000
150	-0.07251	0.42830	0.00378	0.00000	-0.00047	0.00000

SUM	-0.09899	2.29248	-0.09899	0.00000	-0.00039	0.00000
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Condition **LC49=1.2D-WL60**

1	-0.01081	0.06231	0.00028	0.00000	-0.00001	0.00000
2	-0.04637	0.00000	-0.00209	0.00000	0.00000	0.00000
3	-0.05820	0.00000	0.00063	0.00000	0.00000	0.00000
4	0.01311	0.00000	-0.00021	0.00000	0.00000	0.00000
5	-0.09149	0.00000	0.00302	0.00000	0.00000	0.00000
6	0.09804	0.35258	0.01017	0.00000	0.00033	0.00000
17	-0.03631	0.45365	0.01689	0.00000	-0.00007	0.00000
45	0.07346	0.15717	-0.18009	0.00000	0.00038	0.00000
50	0.00053	0.17762	0.14834	0.00000	-0.00096	0.00000
51	-0.00905	0.00000	0.08379	0.00000	0.00000	0.00000
52	0.00603	0.00000	-0.15927	0.00000	0.00000	0.00000
53	-0.00225	0.00000	0.03645	0.00000	0.00000	0.00000
54	0.00388	0.00000	0.04417	0.00000	0.00000	0.00000
55	0.05392	0.54239	-0.00120	0.00000	0.00038	0.00000
115	0.00000	0.02728	0.00328	0.00000	0.00000	0.00000
116	0.00000	0.00971	-0.03597	0.00000	0.00000	0.00000
131	0.00000	0.02788	0.00464	0.00000	0.00000	0.00000
132	0.00000	0.02353	-0.00508	0.00000	0.00000	0.00000
133	0.00000	0.01117	-0.03272	0.00000	0.00000	0.00000
134	0.00000	0.01871	-0.01587	0.00000	0.00000	0.00000
150	-0.07085	0.42848	0.00446	0.00000	-0.00044	0.00000
SUM	-0.07637	2.29248	-0.07637	0.00000	-0.00040	0.00000

Condition **LC50=1.2D-WL90**

1	-0.01012	0.06300	0.00028	0.00000	-0.00001	0.00000
2	-0.04516	0.00000	-0.00190	0.00000	0.00000	0.00000
3	-0.05669	0.00000	0.00064	0.00000	0.00000	0.00000
4	0.01419	0.00000	-0.00022	0.00000	0.00000	0.00000
5	-0.10405	0.00000	0.00300	0.00000	0.00000	0.00000
6	0.09360	0.34511	0.00861	0.00000	0.00033	0.00000
17	-0.03854	0.44488	0.01400	0.00000	-0.00008	0.00000
45	0.07367	0.15766	-0.18218	0.00000	0.00051	0.00000
50	0.00062	0.17733	0.15211	0.00000	-0.00115	0.00000
51	-0.01078	0.00000	0.08747	0.00000	0.00000	0.00000
52	0.00606	0.00000	-0.16305	0.00000	0.00000	0.00000
53	-0.00228	0.00000	0.03701	0.00000	0.00000	0.00000
54	0.00157	0.00000	0.05688	0.00000	0.00000	0.00000
55	0.04968	0.52956	-0.00043	0.00000	0.00027	0.00000
115	0.00000	0.02356	-0.00502	0.00000	0.00000	0.00000
116	0.00000	0.02777	0.00440	0.00000	0.00000	0.00000
131	0.00000	0.02758	0.00396	0.00000	0.00000	0.00000
132	0.00000	0.02357	-0.00501	0.00000	0.00000	0.00000
133	0.00000	0.01984	-0.01333	0.00000	0.00000	0.00000
134	0.00000	0.02282	-0.00668	0.00000	0.00000	0.00000
150	-0.06777	0.42979	0.00948	0.00000	-0.00033	0.00000
SUM	-0.09600	2.29248	0.00000	0.00000	-0.00046	0.00000

Condition **LC51=1.2D-WL120**

1	-0.00937	0.06374	0.00029	0.00000	-0.00002	0.00000
2	-0.03943	0.00000	-0.00172	0.00000	0.00000	0.00000
3	-0.05453	0.00000	0.00064	0.00000	0.00000	0.00000
4	0.01838	0.00000	-0.00023	0.00000	0.00000	0.00000
5	-0.09503	0.00000	0.00300	0.00000	0.00000	0.00000
6	0.08964	0.33806	0.00705	0.00000	0.00034	0.00000
17	-0.03946	0.43617	0.01132	0.00000	-0.00010	0.00000
45	0.07189	0.15710	-0.18174	0.00000	0.00049	0.00000
50	0.00061	0.17689	0.14986	0.00000	-0.00103	0.00000

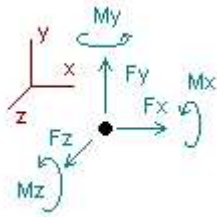
51	-0.00967	0.00000	0.09465	0.00000	0.00000	0.00000
52	0.00597	0.00000	-0.16071	0.00000	0.00000	0.00000
53	-0.00222	0.00000	0.03648	0.00000	0.00000	0.00000
54	0.00195	0.00000	0.06979	0.00000	0.00000	0.00000
55	0.04719	0.51785	0.00016	0.00000	0.00018	0.00000
115	0.00000	0.02073	-0.01136	0.00000	0.00000	0.00000
116	0.00000	0.04440	0.04154	0.00000	0.00000	0.00000
131	0.00000	0.02737	0.00349	0.00000	0.00000	0.00000
132	0.00000	0.02357	-0.00500	0.00000	0.00000	0.00000
133	0.00000	0.02856	0.00615	0.00000	0.00000	0.00000
134	0.00000	0.02680	0.00221	0.00000	0.00000	0.00000
150	-0.06227	0.43125	0.01051	0.00000	-0.00023	0.00000
SUM	-0.07637	2.29248	0.07637	0.00000	-0.00036	0.00000

Condition **LC52=1.2D-WL150**

1	-0.00914	0.06398	0.00029	0.00000	-0.00002	0.00000
2	-0.03868	0.00000	-0.00164	0.00000	0.00000	0.00000
3	-0.05395	0.00000	0.00065	0.00000	0.00000	0.00000
4	0.01716	0.00000	-0.00023	0.00000	0.00000	0.00000
5	-0.11439	0.00000	0.00294	0.00000	0.00000	0.00000
6	0.08808	0.33428	0.00638	0.00000	0.00035	0.00000
17	-0.03962	0.43353	0.01040	0.00000	-0.00010	0.00000
45	0.07156	0.15764	-0.18231	0.00000	0.00051	0.00000
50	0.00063	0.17673	0.15002	0.00000	-0.00104	0.00000
51	-0.00972	0.00000	0.09497	0.00000	0.00000	0.00000
52	0.00595	0.00000	-0.16088	0.00000	0.00000	0.00000
53	-0.00221	0.00000	0.03651	0.00000	0.00000	0.00000
54	0.00164	0.00000	0.07233	0.00000	0.00000	0.00000
55	0.04537	0.51306	-0.00016	0.00000	0.00014	0.00000
115	0.00000	0.01890	-0.01544	0.00000	0.00000	0.00000
116	0.00000	0.05080	0.05586	0.00000	0.00000	0.00000
131	0.00000	0.02705	0.00278	0.00000	0.00000	0.00000
132	0.00000	0.02364	-0.00484	0.00000	0.00000	0.00000
133	0.00000	0.03231	0.01453	0.00000	0.00000	0.00000
134	0.00000	0.02830	0.00556	0.00000	0.00000	0.00000
150	-0.06167	0.43225	0.01129	0.00000	-0.00019	0.00000
SUM	-0.09899	2.29248	0.09899	0.00000	-0.00035	0.00000

Envelope for nodal reactions

Note.- **Ic** is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

- LC1=1.2D+1.6Wo
- LC2=1.2D+1.6W30
- LC3=1.2D+1.6W60
- LC4=1.2D+1.6W90
- LC5=1.2D+1.6W120
- LC6=1.2D+1.6W150
- LC7=1.2D-1.6Wo
- LC8=1.2D-1.6W30
- LC9=1.2D-1.6W60
- LC10=1.2D-1.6W90
- LC11=1.2D-1.6W120
- LC12=1.2D-1.6W150
- LC13=0.9D+1.6Wo
- LC14=0.9D+1.6W30
- LC15=0.9D+1.6W60
- LC16=0.9D+1.6W90
- LC17=0.9D+1.6W120
- LC18=0.9D+1.6W150
- LC19=0.9D-1.6Wo
- LC20=0.9D-1.6W30
- LC21=0.9D-1.6W60
- LC22=0.9D-1.6W90
- LC23=0.9D-1.6W120
- LC24=0.9D-1.6W150
- LC25=1.2D+Di+Wl0
- LC26=1.2D+Di+Wl30
- LC27=1.2D+Di+Wl60
- LC28=1.2D+Di+Wl90
- LC29=1.2D+Di+Wl120
- LC30=1.2D+Di+Wl150
- LC31=1.2D+Di-Wl0
- LC32=1.2D+Di-Wl30
- LC33=1.2D+Di-Wl60
- LC34=1.2D+Di-Wl90
- LC35=1.2D+Di-Wl120
- LC36=1.2D+Di-Wl150
- LC37=0.9D
- LC38=1.2D
- LC41=1.2D+Wl0
- LC42=1.2D+Wl30
- LC43=1.2D+Wl60
- LC44=1.2D+Wl90
- LC45=1.2D+Wl120
- LC46=1.2D+Wl150
- LC47=1.2D-Wl0
- LC48=1.2D-Wl30
- LC49=1.2D-Wl60
- LC50=1.2D-Wl90
- LC51=1.2D-Wl120
- LC52=1.2D-Wl150

Node		Forces						Moments					
		Fx	lc	Fy	lc	Fz	lc	Mx	lc	My	lc	Mz	lc
		[Kip]		[Kip]		[Kip]		[Kip*ft]		[Kip*ft]		[Kip*ft]	
1	Max	0.032	LC15	0.136	LC25	0.005	LC12	0.00000	LC1	0.00373	LC19	0.00000	LC1
	Min	-0.046	LC12	0.007	LC24	-0.004	LC19	0.00000	LC1	-0.00376	LC1	0.00000	LC1
2	Max	0.738	LC15	0.000	LC1	0.065	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.579	LC9	0.000	LC1	-0.068	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
3	Max	0.042	LC2	0.000	LC1	0.076	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.310	LC9	0.000	LC1	-0.075	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1

4	Max	0.067	LC7	0.000	LC1	0.093	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.579	LC21	0.000	LC1	-0.094	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
5	Max	3.434	LC16	0.000	LC1	0.009	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-3.257	LC10	0.000	LC1	-0.005	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
6	Max	0.243	LC5	0.959	LC7	0.254	LC12	0.00000	LC1	0.00080	LC25	0.00000	LC1
	Min	-0.064	LC23	-0.350	LC13	-0.240	LC18	0.00000	LC1	-0.00019	LC17	0.00000	LC1
17	Max	0.139	LC17	1.071	LC7	0.195	LC2	0.00000	LC1	0.00046	LC21	0.00000	LC1
	Min	-0.193	LC11	-0.290	LC13	-0.171	LC20	0.00000	LC1	-0.00075	LC3	0.00000	LC1
45	Max	0.234	LC7	0.304	LC9	0.008	LC16	0.00000	LC1	0.01284	LC11	0.00000	LC1
	Min	-0.107	LC13	-0.105	LC15	-0.351	LC10	0.00000	LC1	-0.01259	LC16	0.00000	LC1
50	Max	0.005	LC12	0.336	LC31	0.640	LC10	0.00000	LC1	0.02698	LC16	0.00000	LC1
	Min	-0.004	LC18	0.102	LC13	-0.379	LC16	0.00000	LC1	-0.02788	LC10	0.00000	LC1
51	Max	0.253	LC16	0.000	LC1	0.766	LC15	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.264	LC10	0.000	LC1	-0.369	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
52	Max	0.087	LC5	0.000	LC1	0.107	LC16	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.076	LC23	0.000	LC1	-0.667	LC10	0.00000	LC1	0.00000	LC1	0.00000	LC1
53	Max	0.112	LC16	0.000	LC1	0.141	LC10	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.115	LC10	0.000	LC1	-0.177	LC16	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.246	LC5	0.000	LC1	1.094	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.237	LC22	0.000	LC1	-0.966	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
55	Max	0.338	LC5	1.436	LC7	0.416	LC13	0.00000	LC1	0.00812	LC7	0.00000	LC1
	Min	-0.207	LC23	-0.510	LC13	-0.410	LC19	0.00000	LC1	-0.00762	LC13	0.00000	LC1
115	Max	0.140	LC3	0.284	LC7	0.521	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC11	-0.243	LC13	-0.530	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
116	Max	0.140	LC17	1.340	LC1	2.992	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC9	-1.293	LC19	-2.992	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
131	Max	0.140	LC15	0.142	LC2	0.317	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC23	-0.093	LC20	-0.308	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
132	Max	0.140	LC5	0.079	LC12	0.177	LC24	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC9	-0.039	LC18	-0.189	LC6	0.00000	LC1	0.00000	LC1	0.00000	LC1
133	Max	0.140	LC5	0.609	LC1	1.364	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC9	-0.573	LC19	-1.385	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.140	LC5	0.348	LC1	0.779	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.140	LC9	-0.308	LC19	-0.791	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
150	Max	0.387	LC15	0.733	LC25	0.442	LC12	0.00000	LC1	0.01060	LC13	0.00000	LC1
	Min	-0.435	LC8	0.216	LC21	-0.434	LC18	0.00000	LC1	-0.01114	LC7	0.00000	LC1

Date: 2/16/2023
Project Name: CHESHIRE SW
Project No.: CT2036
Designed By: KM Checked By: MSC



CHECK CONNECTION CAPACITY (Worst Case) → ALPHA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A36 3/8" Bolt (Assumed)

Allowable Tensile Load =

$F_{Tall} =$ 2402 lbs.

Allowable Shear Load =

$F_{vall} =$ 1441 lbs.

TENSILE FORCES

Reaction $F =$ 1340 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 140 lbs. (See Bentley Output)

Reactions in Z direction: 2992 lbs. (See Bentley Output)

Resultant: 2995 lbs.

No. of Supports = 1

No. of Bolts / Support = 4

Tension Design Load / Bolts =

$f_t =$ 335.00 lbs. $<$ 2402 lbs. **Therefore, OK !**

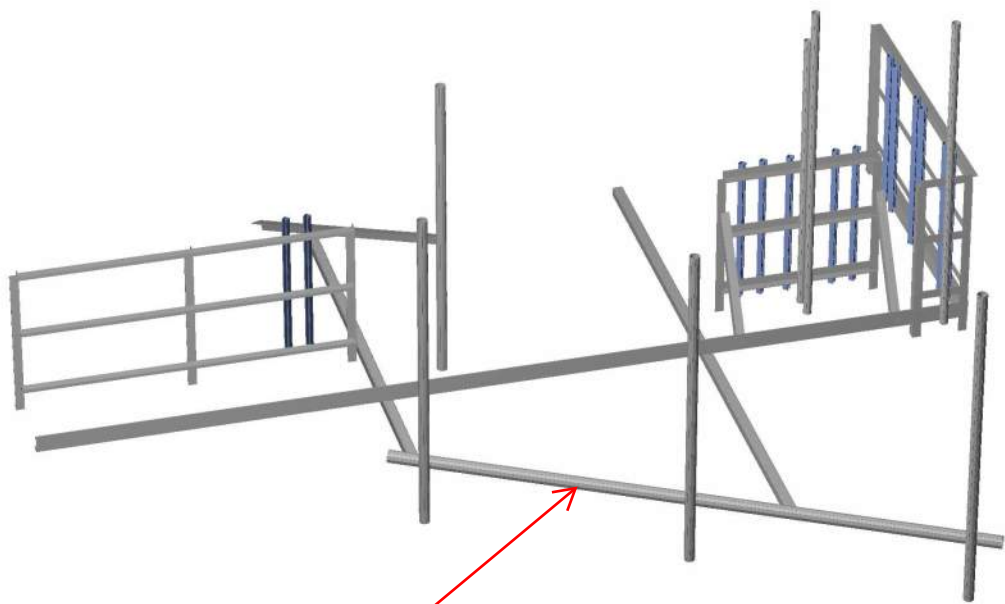
Shear Design Load / Bolts =

$f_v =$ 748.82 lbs. $<$ 1441 lbs. **Therefore, OK !**

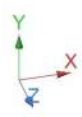
CHECK COMBINED TENSION AND SHEAR

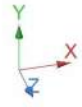
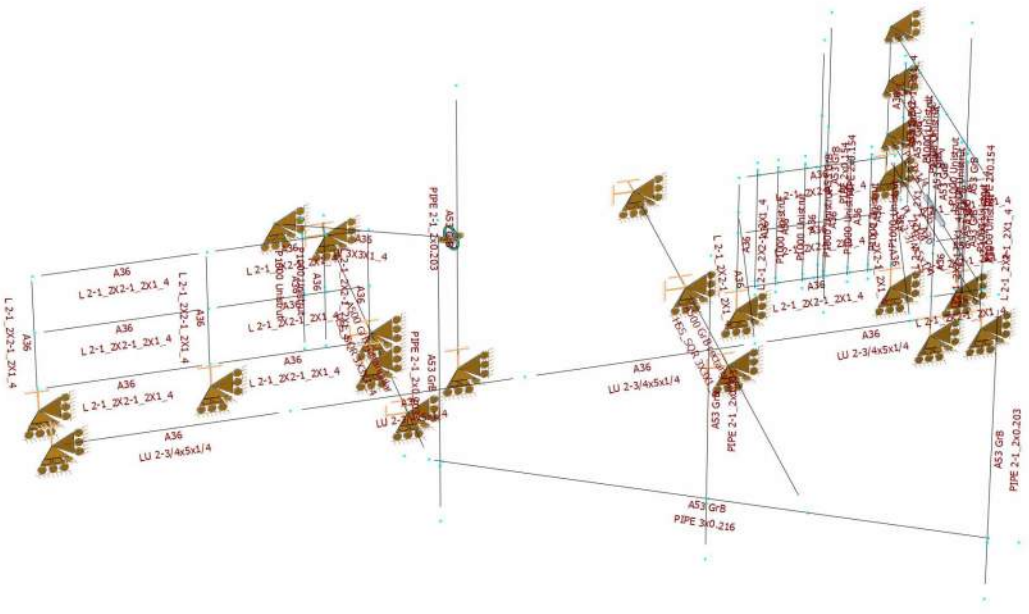
f_t / F_T	+	f_v / F_v	\leq	1.0
0.139	+	0.520	=	0.659 $<$ 1.0 Therefore, OK !

Modified Beta Sector Calculations



Replace existing 2-1/2" (2.88" O.D.) horizontal face pipe with proposed 3" std. (3.5" O.D.) horizontal face pipe secured to the existing mount (total of 1 per Beta sector).

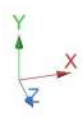
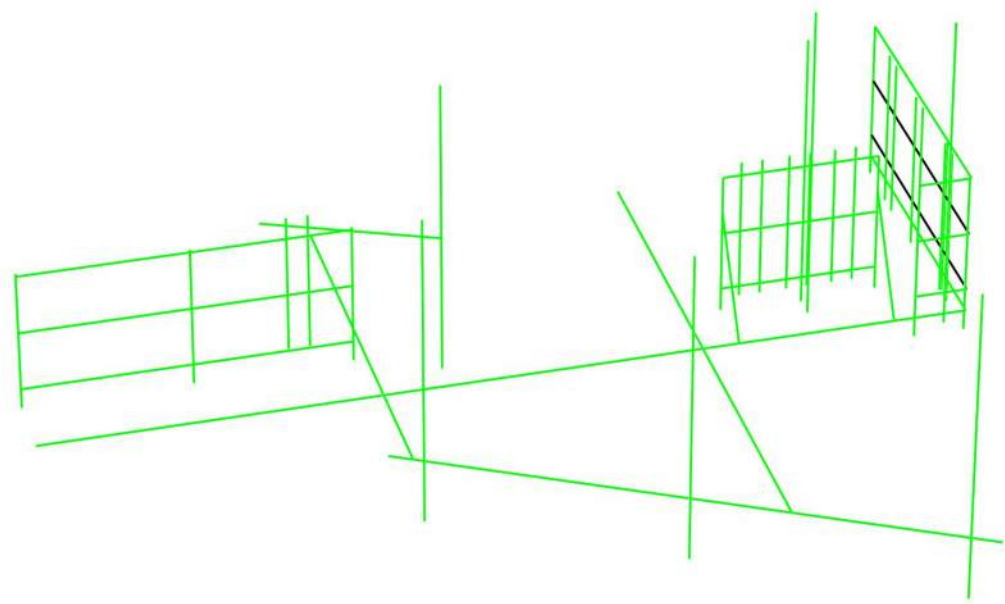


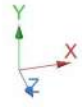
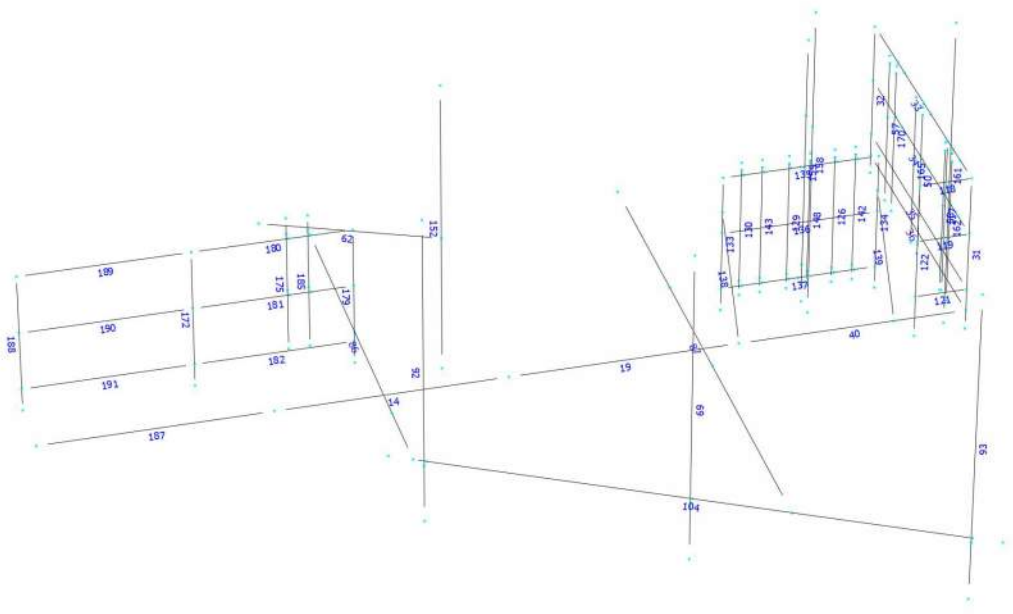




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Load data

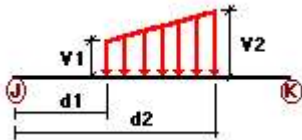
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category
D	Dead Load	No	DL
Wo	Wind Load (NO ICE)	No	WIND
W30	WL 30deg	No	WIND
W60	WL 60deg	No	WIND
W90	WL 90deg	No	WIND
W120	WL 120deg	No	WIND
W150	WL 150deg	No	WIND
Di	Ice Load	No	LL
WI0	WL ICE 0deg	No	WIND
WI30	WL ICE 30deg	No	WIND
WI60	WL ICE 60deg	No	WIND
WI90	WL ICE 90deg	No	WIND
WI120	WL ICE 120deg	No	WIND
WI150	WL ICE 150deg	No	WIND
WL0	WL 30 mph 0deg	No	WIND
WL30	WL 30 mph 30deg	No	WIND
WL60	WL 30 mph 60deg	No	WIND
WL90	WL 30 mph 90deg	No	WIND
WL120	WL 30 mph 120deg	No	WIND
WL150	WL 30 mph 150deg	No	WIND

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	14	z	-0.018	0.00	0.00	No	0.00	No
	19	z	-0.018	0.00	0.00	No	0.00	No
	31	z	-0.017	0.00	0.00	No	0.00	No
	40	z	-0.018	0.00	0.00	No	0.00	No
	50	z	-0.007	0.00	0.00	No	0.00	No
	57	z	-0.007	0.00	0.00	No	0.00	No
	58	z	-0.007	0.00	0.00	No	0.00	No
	62	z	-0.02	0.00	0.00	No	0.00	No
	104	z	-0.014	0.00	0.00	No	0.00	No
	117	z	-0.017	0.00	0.00	No	0.00	No

118	z	-0.017	0.00	0.00	No	0.00	No
119	z	-0.017	0.00	0.00	No	0.00	No
121	z	-0.017	0.00	0.00	No	0.00	No
122	z	-0.017	0.00	0.00	No	0.00	No
126	z	-0.007	0.00	0.00	No	0.00	No
129	z	-0.007	0.00	0.00	No	0.00	No
130	z	-0.007	0.00	0.00	No	0.00	No
133	z	-0.017	0.00	0.00	No	0.00	No
134	z	-0.017	0.00	0.00	No	0.00	No
135	z	-0.017	0.00	0.00	No	0.00	No
136	z	-0.017	0.00	0.00	No	0.00	No
137	z	-0.017	0.00	0.00	No	0.00	No
138	z	-0.017	0.00	0.00	No	0.00	No
139	z	-0.017	0.00	0.00	No	0.00	No
142	z	-0.007	0.00	0.00	No	0.00	No
143	z	-0.007	0.00	0.00	No	0.00	No
148	z	-0.007	0.00	0.00	No	0.00	No
152	z	-0.012	0.00	0.00	No	0.00	No
155	z	-0.01	0.00	0.00	No	0.00	No
158	z	-0.01	0.00	0.00	No	0.00	No
161	z	-0.01	0.00	0.00	No	0.00	No
162	z	-0.007	0.00	0.00	No	0.00	No
165	z	-0.007	0.00	0.00	No	0.00	No
170	z	-0.007	0.00	0.00	No	0.00	No
172	z	-0.017	0.00	0.00	No	0.00	No
175	z	-0.007	0.00	0.00	No	0.00	No
179	z	-0.017	0.00	0.00	No	0.00	No
180	z	-0.017	0.00	0.00	No	0.00	No
181	z	-0.017	0.00	0.00	No	0.00	No
182	z	-0.017	0.00	0.00	No	0.00	No
185	z	-0.007	0.00	0.00	No	0.00	No
187	z	-0.018	0.00	0.00	No	0.00	No
188	z	-0.017	0.00	0.00	No	0.00	No
189	z	-0.017	0.00	0.00	No	0.00	No
190	z	-0.017	0.00	0.00	No	0.00	No
191	z	-0.017	0.00	0.00	No	0.00	No
W30	14	z	-0.018	0.00	0.00	No	No
	19	z	-0.018	0.00	0.00	No	No
	31	z	-0.017	0.00	0.00	No	No
	32	z	-0.017	0.00	0.00	No	No
	33	z	-0.017	0.00	0.00	No	No
	34	z	-0.013	0.00	0.00	No	No
	35	z	-0.013	0.00	0.00	No	No
	36	z	-0.018	0.00	0.00	No	No
	40	z	-0.018	0.00	0.00	No	No
	50	z	-0.007	0.00	0.00	No	No
	57	z	-0.007	0.00	0.00	No	No
	58	z	-0.007	0.00	0.00	No	No
	62	z	-0.02	0.00	0.00	No	No
	69	z	-0.012	0.00	0.00	No	No
	86	z	-0.013	0.00	0.00	No	No
	87	z	-0.013	0.00	0.00	No	No
	92	z	-0.012	0.00	0.00	No	No
	93	z	-0.012	0.00	0.00	No	No
	104	z	-0.014	0.00	0.00	No	No
	117	z	-0.017	0.00	0.00	No	No
	118	z	-0.017	0.00	0.00	No	No
	119	z	-0.017	0.00	0.00	No	No
	121	z	-0.017	0.00	0.00	No	No
	122	z	-0.017	0.00	0.00	No	No

	126	z	-0.007	0.00	0.00	No	0.00	No
	129	z	-0.007	0.00	0.00	No	0.00	No
	130	z	-0.007	0.00	0.00	No	0.00	No
	133	z	-0.017	0.00	0.00	No	0.00	No
	134	z	-0.017	0.00	0.00	No	0.00	No
	135	z	-0.017	0.00	0.00	No	0.00	No
	136	z	-0.017	0.00	0.00	No	0.00	No
	137	z	-0.017	0.00	0.00	No	0.00	No
	138	z	-0.017	0.00	0.00	No	0.00	No
	139	z	-0.017	0.00	0.00	No	0.00	No
	142	z	-0.007	0.00	0.00	No	0.00	No
	143	z	-0.007	0.00	0.00	No	0.00	No
	148	z	-0.007	0.00	0.00	No	0.00	No
	152	z	-0.012	0.00	0.00	No	0.00	No
	155	z	-0.01	0.00	0.00	No	0.00	No
	158	z	-0.01	0.00	0.00	No	0.00	No
	161	z	-0.01	0.00	0.00	No	0.00	No
	162	z	-0.007	0.00	0.00	No	0.00	No
	165	z	-0.007	0.00	0.00	No	0.00	No
	170	z	-0.007	0.00	0.00	No	0.00	No
	172	z	-0.017	0.00	0.00	No	0.00	No
	175	z	-0.007	0.00	0.00	No	0.00	No
	179	z	-0.017	0.00	0.00	No	0.00	No
	180	z	-0.017	0.00	0.00	No	0.00	No
	181	z	-0.017	0.00	0.00	No	0.00	No
	182	z	-0.017	0.00	0.00	No	0.00	No
	185	z	-0.007	0.00	0.00	No	0.00	No
	187	z	-0.018	0.00	0.00	No	0.00	No
	188	z	-0.017	0.00	0.00	No	0.00	No
	189	z	-0.017	0.00	0.00	No	0.00	No
	190	z	-0.017	0.00	0.00	No	0.00	No
	191	z	-0.017	0.00	0.00	No	0.00	No
W60	14	x	-0.018	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	40	x	-0.018	0.00	0.00	No	0.00	No
	50	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	69	x	-0.012	0.00	0.00	No	0.00	No
	86	x	-0.013	0.00	0.00	No	0.00	No
	87	x	-0.013	0.00	0.00	No	0.00	No
	92	x	-0.012	0.00	0.00	No	0.00	No
	93	x	-0.012	0.00	0.00	No	0.00	No
	104	x	-0.014	0.00	0.00	No	0.00	No
	117	x	-0.017	0.00	0.00	No	0.00	No
	118	x	-0.017	0.00	0.00	No	0.00	No
	119	x	-0.017	0.00	0.00	No	0.00	No
	121	x	-0.017	0.00	0.00	No	0.00	No
	122	x	-0.017	0.00	0.00	No	0.00	No
	126	x	-0.007	0.00	0.00	No	0.00	No
	129	x	-0.007	0.00	0.00	No	0.00	No
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	133	x	-0.017	0.00	0.00	No	0.00	No

W90

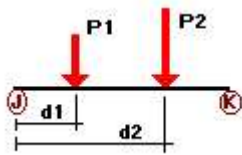
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137	x	-0.017	0.00	0.00	No	0.00	No
138	x	-0.017	0.00	0.00	No	0.00	No
139	x	-0.017	0.00	0.00	No	0.00	No
142	x	-0.007	0.00	0.00	No	0.00	No
143	x	-0.007	0.00	0.00	No	0.00	No
148	x	-0.007	0.00	0.00	No	0.00	No
152	x	-0.012	0.00	0.00	No	0.00	No
155	x	-0.01	0.00	0.00	No	0.00	No
158	x	-0.01	0.00	0.00	No	0.00	No
161	x	-0.01	0.00	0.00	No	0.00	No
162	x	-0.007	0.00	0.00	No	0.00	No
165	x	-0.007	0.00	0.00	No	0.00	No
170	x	-0.007	0.00	0.00	No	0.00	No
172	x	-0.017	0.00	0.00	No	0.00	No
175	x	-0.007	0.00	0.00	No	0.00	No
179	x	-0.017	0.00	0.00	No	0.00	No
180	x	-0.017	0.00	0.00	No	0.00	No
181	x	-0.017	0.00	0.00	No	0.00	No
182	x	-0.017	0.00	0.00	No	0.00	No
185	x	-0.007	0.00	0.00	No	0.00	No
187	x	-0.018	0.00	0.00	No	0.00	No
188	x	-0.017	0.00	0.00	No	0.00	No
189	x	-0.017	0.00	0.00	No	0.00	No
190	x	-0.017	0.00	0.00	No	0.00	No
191	x	-0.017	0.00	0.00	No	0.00	No
14	x	-0.018	0.00	0.00	No	0.00	No
19	x	-0.018	0.00	0.00	No	0.00	No
31	x	-0.017	0.00	0.00	No	0.00	No
32	x	-0.017	0.00	0.00	No	0.00	No
33	x	-0.017	0.00	0.00	No	0.00	No
34	x	-0.013	0.00	0.00	No	0.00	No
35	x	-0.013	0.00	0.00	No	0.00	No
36	x	-0.018	0.00	0.00	No	0.00	No
50	x	-0.007	0.00	0.00	No	0.00	No
57	x	-0.007	0.00	0.00	No	0.00	No
58	x	-0.007	0.00	0.00	No	0.00	No
62	x	-0.02	0.00	0.00	No	0.00	No
69	x	-0.012	0.00	0.00	No	0.00	No
86	x	-0.013	0.00	0.00	No	0.00	No
87	x	-0.013	0.00	0.00	No	0.00	No
92	x	-0.012	0.00	0.00	No	0.00	No
93	x	-0.012	0.00	0.00	No	0.00	No
117	x	-0.017	0.00	0.00	No	0.00	No
122	x	-0.017	0.00	0.00	No	0.00	No
126	x	-0.007	0.00	0.00	No	0.00	No
129	x	-0.007	0.00	0.00	No	0.00	No
130	x	-0.007	0.00	0.00	No	0.00	No
138	x	-0.017	0.00	0.00	No	0.00	No
139	x	-0.017	0.00	0.00	No	0.00	No
142	x	-0.007	0.00	0.00	No	0.00	No
143	x	-0.007	0.00	0.00	No	0.00	No
148	x	-0.007	0.00	0.00	No	0.00	No
152	x	-0.012	0.00	0.00	No	0.00	No
155	x	-0.01	0.00	0.00	No	0.00	No
158	x	-0.01	0.00	0.00	No	0.00	No
161	x	-0.01	0.00	0.00	No	0.00	No
162	x	-0.007	0.00	0.00	No	0.00	No

	165	x	-0.007	0.00	0.00	No	0.00	No
	170	x	-0.007	0.00	0.00	No	0.00	No
	175	x	-0.007	0.00	0.00	No	0.00	No
	185	x	-0.007	0.00	0.00	No	0.00	No
	187	x	-0.018	0.00	0.00	No	0.00	No
W120	14	x	-0.018	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	40	x	-0.018	0.00	0.00	No	0.00	No
	50	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	69	x	-0.012	0.00	0.00	No	0.00	No
	86	x	-0.013	0.00	0.00	No	0.00	No
	87	x	-0.013	0.00	0.00	No	0.00	No
	92	x	-0.012	0.00	0.00	No	0.00	No
	93	x	-0.012	0.00	0.00	No	0.00	No
	104	x	-0.014	0.00	0.00	No	0.00	No
	117	x	-0.017	0.00	0.00	No	0.00	No
	122	x	-0.017	0.00	0.00	No	0.00	No
	126	x	-0.007	0.00	0.00	No	0.00	No
	129	x	-0.007	0.00	0.00	No	0.00	No
	130	x	-0.007	0.00	0.00	No	0.00	No
	133	x	-0.017	0.00	0.00	No	0.00	No
	134	x	-0.017	0.00	0.00	No	0.00	No
	135	x	-0.017	0.00	0.00	No	0.00	No
	136	x	-0.017	0.00	0.00	No	0.00	No
	137	x	-0.017	0.00	0.00	No	0.00	No
	138	x	-0.017	0.00	0.00	No	0.00	No
	139	x	-0.017	0.00	0.00	No	0.00	No
	142	x	-0.007	0.00	0.00	No	0.00	No
	143	x	-0.007	0.00	0.00	No	0.00	No
	148	x	-0.007	0.00	0.00	No	0.00	No
	152	x	-0.012	0.00	0.00	No	0.00	No
	155	x	-0.01	0.00	0.00	No	0.00	No
	158	x	-0.01	0.00	0.00	No	0.00	No
	161	x	-0.01	0.00	0.00	No	0.00	No
	162	x	-0.007	0.00	0.00	No	0.00	No
	165	x	-0.007	0.00	0.00	No	0.00	No
	170	x	-0.007	0.00	0.00	No	0.00	No
	172	x	-0.017	0.00	0.00	No	0.00	No
	175	x	-0.007	0.00	0.00	No	0.00	No
	179	x	-0.017	0.00	0.00	No	0.00	No
	180	x	-0.017	0.00	0.00	No	0.00	No
	181	x	-0.017	0.00	0.00	No	0.00	No
	182	x	-0.017	0.00	0.00	No	0.00	No
	185	x	-0.007	0.00	0.00	No	0.00	No
	187	x	-0.018	0.00	0.00	No	0.00	No
	188	x	-0.017	0.00	0.00	No	0.00	No
	189	x	-0.017	0.00	0.00	No	0.00	No
	190	x	-0.017	0.00	0.00	No	0.00	No
	191	x	-0.017	0.00	0.00	No	0.00	No
W150	14	z	0.018	0.00	0.00	No	0.00	No
	19	z	0.018	0.00	0.00	No	0.00	No

31	z	0.017	0.00	0.00	No	0.00	No
32	z	0.017	0.00	0.00	No	0.00	No
33	z	0.017	0.00	0.00	No	0.00	No
34	z	0.013	0.00	0.00	No	0.00	No
35	z	0.013	0.00	0.00	No	0.00	No
36	z	0.018	0.00	0.00	No	0.00	No
40	z	0.018	0.00	0.00	No	0.00	No
50	z	0.007	0.00	0.00	No	0.00	No
57	z	0.007	0.00	0.00	No	0.00	No
58	z	0.007	0.00	0.00	No	0.00	No
62	z	0.02	0.00	0.00	No	0.00	No
69	z	0.012	0.00	0.00	No	0.00	No
86	z	0.013	0.00	0.00	No	0.00	No
87	z	0.013	0.00	0.00	No	0.00	No
92	z	0.012	0.00	0.00	No	0.00	No
93	z	0.012	0.00	0.00	No	0.00	No
104	z	0.014	0.00	0.00	No	0.00	No
117	z	0.017	0.00	0.00	No	0.00	No
122	z	0.017	0.00	0.00	No	0.00	No
126	z	0.007	0.00	0.00	No	0.00	No
129	z	0.007	0.00	0.00	No	0.00	No
130	z	0.007	0.00	0.00	No	0.00	No
133	z	0.017	0.00	0.00	No	0.00	No
134	z	0.017	0.00	0.00	No	0.00	No
135	z	0.017	0.00	0.00	No	0.00	No
136	z	0.017	0.00	0.00	No	0.00	No
137	z	0.017	0.00	0.00	No	0.00	No
138	z	0.017	0.00	0.00	No	0.00	No
139	z	0.017	0.00	0.00	No	0.00	No
142	z	0.007	0.00	0.00	No	0.00	No
143	z	0.007	0.00	0.00	No	0.00	No
148	z	0.007	0.00	0.00	No	0.00	No
152	z	0.012	0.00	0.00	No	0.00	No
155	z	0.01	0.00	0.00	No	0.00	No
158	z	0.01	0.00	0.00	No	0.00	No
161	z	0.01	0.00	0.00	No	0.00	No
162	z	0.007	0.00	0.00	No	0.00	No
165	z	0.007	0.00	0.00	No	0.00	No
170	z	0.007	0.00	0.00	No	0.00	No
172	z	0.017	0.00	0.00	No	0.00	No
175	z	0.007	0.00	0.00	No	0.00	No
179	z	0.017	0.00	0.00	No	0.00	No
180	z	0.017	0.00	0.00	No	0.00	No
181	z	0.017	0.00	0.00	No	0.00	No
182	z	0.017	0.00	0.00	No	0.00	No
185	z	0.007	0.00	0.00	No	0.00	No
187	z	0.018	0.00	0.00	No	0.00	No
188	z	0.017	0.00	0.00	No	0.00	No
189	z	0.017	0.00	0.00	No	0.00	No
190	z	0.017	0.00	0.00	No	0.00	No
191	z	0.017	0.00	0.00	No	0.00	No
Di	14	y	-0.01	0.00	0.00	No	No
	19	y	-0.01	0.00	0.00	No	No
	31	y	-0.007	0.00	0.00	No	No
	32	y	-0.007	0.00	0.00	No	No
	33	y	-0.007	0.00	0.00	No	No
	34	y	-0.005	0.00	0.00	No	No
	35	y	-0.005	0.00	0.00	No	No
	36	y	-0.01	0.00	0.00	No	No
	40	y	-0.01	0.00	0.00	No	No

50	y	-0.004	0.00	0.00	No	0.00	No
57	y	-0.004	0.00	0.00	No	0.00	No
58	y	-0.004	0.00	0.00	No	0.00	No
62	y	-0.008	0.00	0.00	No	0.00	No
69	y	-0.006	0.00	0.00	No	0.00	No
86	y	-0.008	0.00	0.00	No	0.00	No
87	y	-0.008	0.00	0.00	No	0.00	No
92	y	-0.006	0.00	0.00	No	0.00	No
93	y	-0.006	0.00	0.00	No	0.00	No
104	y	-0.007	0.00	0.00	No	0.00	No
117	y	-0.007	0.00	0.00	No	0.00	No
122	y	-0.007	0.00	0.00	No	0.00	No
126	y	-0.004	0.00	0.00	No	0.00	No
129	y	-0.004	0.00	0.00	No	0.00	No
130	y	-0.004	0.00	0.00	No	0.00	No
142	y	-0.004	0.00	0.00	No	0.00	No
143	y	-0.004	0.00	0.00	No	0.00	No
148	y	-0.004	0.00	0.00	No	0.00	No
152	y	-0.006	0.00	0.00	No	0.00	No
155	y	-0.005	0.00	0.00	No	0.00	No
158	y	-0.005	0.00	0.00	No	0.00	No
161	y	-0.005	0.00	0.00	No	0.00	No
162	y	-0.004	0.00	0.00	No	0.00	No
165	y	-0.004	0.00	0.00	No	0.00	No
170	y	-0.004	0.00	0.00	No	0.00	No
172	y	-0.007	0.00	0.00	No	0.00	No
175	y	-0.004	0.00	0.00	No	0.00	No
179	y	-0.007	0.00	0.00	No	0.00	No
180	y	-0.007	0.00	0.00	No	0.00	No
181	y	-0.007	0.00	0.00	No	0.00	No
182	y	-0.007	0.00	0.00	No	0.00	No
185	y	-0.004	0.00	0.00	No	0.00	No
187	y	-0.01	0.00	0.00	No	0.00	No
188	y	-0.007	0.00	0.00	No	0.00	No
189	y	-0.007	0.00	0.00	No	0.00	No
190	y	-0.007	0.00	0.00	No	0.00	No
191	y	-0.007	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	50	y	-0.015	2.00	No
	57	y	-0.03	2.00	No
	58	y	-0.037	2.00	No
	69	y	-0.033	1.00	No
		y	-0.033	3.00	No
		y	-0.041	5.00	No
		y	-0.041	7.00	No
	92	y	-0.04	1.25	No

		y	-0.04	6.25	No
	93	y	-0.065	1.25	No
		y	-0.065	6.25	No
	126	y	-0.03	2.00	No
	129	y	-0.03	2.00	No
	130	y	-0.03	2.00	No
	142	y	-0.03	2.00	No
	143	y	-0.03	2.00	No
	148	y	-0.03	2.00	No
	162	y	-0.037	2.00	No
	165	y	-0.015	2.00	No
	170	y	-0.03	2.00	No
	175	y	-0.022	2.00	No
	185	y	-0.022	2.00	No
Wo	50	z	-0.031	2.00	No
	57	z	-0.034	2.00	No
	58	z	-0.028	2.00	No
	69	z	-0.084	1.00	No
		z	-0.084	3.00	No
		z	-0.082	5.00	No
		z	-0.082	7.00	No
	92	z	-0.255	1.25	No
		z	-0.255	6.25	No
	93	z	-0.272	1.25	No
		z	-0.272	6.25	No
	126	z	-0.056	2.00	No
	129	z	-0.056	2.00	No
	130	z	-0.041	2.00	No
	142	z	-0.056	2.00	No
	143	z	-0.041	2.00	No
	148	z	-0.056	2.00	No
	162	z	-0.028	2.00	No
	165	z	-0.031	2.00	No
	170	z	-0.034	2.00	No
	175	z	-0.037	2.00	No
	185	z	-0.037	2.00	No
W30	50	3	-0.031	2.00	No
	57	3	-0.036	2.00	No
	58	3	-0.025	2.00	No
	69	3	-0.073	1.00	No
		3	-0.073	3.00	No
		3	-0.075	5.00	No
		3	-0.075	7.00	No
	92	3	-0.22	1.25	No
		3	-0.22	6.25	No
	93	3	-0.238	1.25	No
		3	-0.238	6.25	No
	126	3	-0.05	2.00	No
	129	3	-0.05	2.00	No
	130	3	-0.037	2.00	No
	142	3	-0.05	2.00	No
	143	3	-0.037	2.00	No
	148	3	-0.05	2.00	No
	162	3	-0.025	2.00	No
	165	3	-0.031	2.00	No
	170	3	-0.036	2.00	No
	175	3	-0.032	2.00	No
	185	3	-0.032	2.00	No
W60	50	3	-0.031	2.00	No
	57	3	-0.052	2.00	No

	58	3	-0.037	2.00	No
	69	3	-0.052	1.00	No
		3	-0.052	3.00	No
		3	-0.062	5.00	No
		3	-0.062	7.00	No
	92	3	-0.148	1.25	No
		3	-0.148	6.25	No
	93	3	-0.171	1.25	No
		3	-0.171	6.25	No
	126	3	-0.039	2.00	No
	129	3	-0.039	2.00	No
	130	3	-0.029	2.00	No
	142	3	-0.039	2.00	No
	143	3	-0.029	2.00	No
	148	3	-0.039	2.00	No
	162	3	-0.037	2.00	No
	165	3	-0.031	2.00	No
	170	3	-0.052	2.00	No
	175	3	-0.022	2.00	No
	185	3	-0.022	2.00	No
W90	50	x	-0.031	2.00	No
	57	x	-0.056	2.00	No
	58	x	-0.04	2.00	No
	69	x	-0.041	1.00	No
		x	-0.041	3.00	No
		x	-0.055	5.00	No
		x	-0.055	7.00	No
	92	x	-0.113	1.25	No
		x	-0.113	6.25	No
	93	x	-0.137	1.25	No
		x	-0.137	6.25	No
	126	x	-0.034	2.00	No
	129	x	-0.034	2.00	No
	130	x	-0.025	2.00	No
	142	x	-0.034	2.00	No
	143	x	-0.025	2.00	No
	148	x	-0.034	2.00	No
	162	x	-0.04	2.00	No
	165	x	-0.031	2.00	No
	170	x	-0.056	2.00	No
	175	x	-0.017	2.00	No
	185	x	-0.017	2.00	No
W120	50	2	-0.031	2.00	No
	57	2	-0.052	2.00	No
	58	2	-0.037	2.00	No
	69	2	-0.052	1.00	No
		2	-0.052	3.00	No
		2	-0.062	5.00	No
		2	-0.062	7.00	No
	92	2	-0.148	1.25	No
		2	-0.148	6.25	No
	93	2	-0.171	1.25	No
		2	-0.171	6.25	No
	126	2	-0.039	2.00	No
	129	2	-0.039	2.00	No
	130	2	-0.029	2.00	No
	142	2	-0.039	2.00	No
	143	2	-0.029	2.00	No
	148	2	-0.039	2.00	No
	162	2	-0.037	2.00	No

	165	2	-0.031	2.00	No
	170	2	-0.052	2.00	No
	175	2	-0.022	2.00	No
	185	2	-0.022	2.00	No
W150	50	2	-0.031	2.00	No
	57	2	-0.036	2.00	No
	58	2	-0.025	2.00	No
	69	2	-0.073	1.00	No
		2	-0.073	3.00	No
		2	-0.075	5.00	No
		2	-0.075	7.00	No
	92	2	-0.22	1.25	No
		2	-0.22	6.25	No
	93	2	-0.238	1.25	No
		2	-0.238	6.25	No
	126	2	-0.05	2.00	No
	129	2	-0.05	2.00	No
	130	2	-0.037	2.00	No
	142	2	-0.05	2.00	No
	143	2	-0.037	2.00	No
	148	2	-0.05	2.00	No
	162	2	-0.025	2.00	No
	165	2	-0.031	2.00	No
	170	2	-0.036	2.00	No
	175	2	-0.032	2.00	No
	185	2	-0.032	2.00	No
Di	50	y	-0.023	2.00	No
	57	y	-0.026	2.00	No
	58	y	-0.02	2.00	No
	69	y	-0.037	1.00	No
		y	-0.037	3.00	No
		y	-0.039	5.00	No
		y	-0.039	7.00	No
	92	y	-0.104	1.25	No
		y	-0.104	6.25	No
	93	y	-0.114	1.25	No
		y	-0.114	6.25	No
	126	y	-0.026	2.00	No
	129	y	-0.026	2.00	No
	130	y	-0.02	2.00	No
	142	y	-0.026	2.00	No
	143	y	-0.02	2.00	No
	148	y	-0.026	2.00	No
	162	y	-0.02	2.00	No
	165	y	-0.023	2.00	No
	170	y	-0.026	2.00	No
	175	y	-0.017	2.00	No
	185	y	-0.017	2.00	No
W10	50	z	-0.007	2.00	No
	57	z	-0.008	2.00	No
	58	z	-0.007	2.00	No
	69	z	-0.019	1.00	No
		z	-0.019	3.00	No
		z	-0.018	5.00	No
		z	-0.018	7.00	No
	92	z	-0.052	1.25	No
		z	-0.052	6.25	No
	93	z	-0.055	1.25	No
		z	-0.055	6.25	No
	126	z	-0.013	2.00	No

	129	z	-0.013	2.00	No
	130	z	-0.01	2.00	No
	142	z	-0.013	2.00	No
	143	z	-0.01	2.00	No
	148	z	-0.013	2.00	No
	162	z	-0.007	2.00	No
	165	z	-0.007	2.00	No
	170	z	-0.009	2.00	No
	175	z	-0.009	2.00	No
	185	z	-0.009	2.00	No
WI30	50	3	-0.007	2.00	No
	57	3	-0.01	2.00	No
	58	3	-0.008	2.00	No
	69	3	-0.016	1.00	No
		3	-0.016	3.00	No
		3	-0.017	5.00	No
		3	-0.017	7.00	No
	92	3	-0.045	1.25	No
		3	-0.045	6.25	No
	93	3	-0.048	1.25	No
		3	-0.048	6.25	No
	126	3	-0.012	2.00	No
	129	3	-0.012	2.00	No
	130	3	-0.009	2.00	No
	142	3	-0.012	2.00	No
	143	3	-0.009	2.00	No
	148	3	-0.012	2.00	No
	162	3	-0.008	2.00	No
	165	3	-0.007	2.00	No
	170	3	-0.01	2.00	No
	175	3	-0.008	2.00	No
WI60	185	3	-0.008	2.00	No
	50	3	-0.007	2.00	No
	57	3	-0.012	2.00	No
	58	3	-0.009	2.00	No
	69	3	-0.012	1.00	No
		3	-0.012	3.00	No
		3	-0.014	5.00	No
		3	-0.014	7.00	No
	92	3	-0.032	1.25	No
		3	-0.032	6.25	No
	93	3	-0.036	1.25	No
		3	-0.036	6.25	No
	126	3	-0.01	2.00	No
	129	3	-0.01	2.00	No
	130	3	-0.007	2.00	No
	142	3	-0.01	2.00	No
	143	3	-0.007	2.00	No
	148	3	-0.01	2.00	No
	162	3	-0.009	2.00	No
	165	3	-0.007	2.00	No
	170	3	-0.012	2.00	No
	175	3	-0.006	2.00	No
	185	3	-0.006	2.00	No
WI90	50	x	-0.007	2.00	No
	57	x	-0.013	2.00	No
	58	x	-0.009	2.00	No
	69	x	-0.01	1.00	No
		x	-0.01	3.00	No
		x	-0.013	5.00	No

		x	-0.013	7.00	No
	92	x	-0.026	1.25	No
		x	-0.026	6.25	No
	93	x	-0.03	1.25	No
		x	-0.03	6.25	No
	126	x	-0.009	2.00	No
	129	x	-0.009	2.00	No
	130	x	-0.007	2.00	No
	142	x	-0.009	2.00	No
	143	x	-0.007	2.00	No
	148	x	-0.009	2.00	No
	162	x	-0.009	2.00	No
	165	x	-0.007	2.00	No
	170	x	-0.013	2.00	No
	175	x	-0.005	2.00	No
	185	x	-0.005	2.00	No
WI120	50	2	-0.007	2.00	No
	57	2	-0.012	2.00	No
	58	2	-0.009	2.00	No
	69	2	-0.012	1.00	No
		2	-0.012	3.00	No
		2	-0.014	5.00	No
		2	-0.014	7.00	No
	92	2	-0.032	1.25	No
		2	-0.032	6.25	No
	93	2	-0.036	1.25	No
		2	-0.036	6.25	No
	126	2	-0.01	2.00	No
	129	2	-0.01	2.00	No
	130	2	-0.007	2.00	No
	142	2	-0.01	2.00	No
	143	2	-0.007	2.00	No
	148	2	-0.01	2.00	No
	162	2	-0.009	2.00	No
	165	2	-0.007	2.00	No
	170	2	-0.012	2.00	No
	175	2	-0.006	2.00	No
	185	2	-0.006	2.00	No
WI150	50	2	-0.007	2.00	No
	57	2	-0.01	2.00	No
	58	2	-0.008	2.00	No
	69	2	-0.016	1.00	No
		2	-0.016	3.00	No
		2	-0.017	5.00	No
		2	-0.017	6.00	No
	92	2	-0.045	1.25	No
		2	-0.045	6.25	No
	93	2	-0.048	1.25	No
		2	-0.048	6.25	No
	126	2	-0.012	2.00	No
	129	2	-0.012	2.00	No
	130	2	-0.009	2.00	No
	142	2	-0.012	2.00	No
	143	2	-0.009	2.00	No
	148	2	-0.012	2.00	No
	162	2	-0.008	2.00	No
	165	2	-0.007	2.00	No
	170	2	-0.01	2.00	No
	175	2	-0.008	2.00	No
	185	2	-0.008	2.00	No

WLO	50	z	-0.002	2.00	No
	57	z	-0.002	2.00	No
	58	z	-0.002	2.00	No
	69	z	-0.006	1.00	No
		z	-0.006	3.00	No
		z	-0.006	5.00	No
	92	z	-0.006	7.00	No
		z	-0.016	1.25	No
		z	-0.016	6.25	No
	93	z	-0.017	1.25	No
		z	-0.017	6.25	No
	126	z	-0.004	2.00	No
	129	z	-0.004	2.00	No
	130	z	-0.003	2.00	No
	142	z	-0.004	2.00	No
	143	z	-0.003	2.00	No
	148	z	-0.004	2.00	No
	162	z	-0.002	2.00	No
165	z	-0.002	2.00	No	
170	z	-0.002	2.00	No	
175	z	-0.003	2.00	No	
185	z	-0.003	2.00	No	
WL30	50	3	-0.002	2.00	No
	57	3	-0.003	2.00	No
	58	3	-0.002	2.00	No
		3	-0.005	1.00	No
		3	-0.005	3.00	No
	69	3	-0.005	5.00	No
		3	-0.005	7.00	No
		3	-0.005	7.00	No
	92	3	-0.014	1.25	No
		3	-0.014	6.25	No
	93	3	-0.015	1.25	No
		3	-0.015	6.25	No
	126	3	-0.003	2.00	No
	129	3	-0.003	2.00	No
	130	3	-0.003	2.00	No
	142	3	-0.003	2.00	No
	143	3	-0.003	2.00	No
	148	3	-0.003	2.00	No
162	3	-0.002	2.00	No	
165	3	-0.002	2.00	No	
170	3	-0.003	2.00	No	
175	3	-0.002	2.00	No	
185	3	-0.002	2.00	No	
WL60	50	3	-0.002	2.00	No
	57	3	-0.003	2.00	No
	58	3	-0.003	2.00	No
		3	-0.004	1.00	No
		3	-0.004	3.00	No
	69	3	-0.004	5.00	No
		3	-0.004	7.00	No
		3	-0.004	7.00	No
	92	3	-0.01	1.25	No
		3	-0.01	6.25	No
	93	3	-0.011	1.25	No
		3	-0.011	6.25	No
	126	3	-0.003	2.00	No
	129	3	-0.003	2.00	No
	130	3	-0.002	2.00	No
	142	3	-0.003	2.00	No
	143	3	-0.002	2.00	No

	148	3	-0.003	2.00	No
	162	3	-0.003	2.00	No
	165	3	-0.002	2.00	No
	170	3	-0.003	2.00	No
	175	3	-0.002	2.00	No
WL90	185	3	-0.002	2.00	No
	50	x	-0.002	2.00	No
	57	x	-0.004	2.00	No
	58	x	-0.003	2.00	No
	69	x	-0.003	1.00	No
		x	-0.003	3.00	No
		x	-0.004	5.00	No
		x	-0.004	7.00	No
	92	x	-0.008	1.25	No
		x	-0.008	6.25	No
	93	x	-0.009	1.25	No
		x	-0.009	6.25	No
	126	x	-0.002	2.00	No
	129	x	-0.002	2.00	No
	130	x	-0.002	2.00	No
	142	x	-0.002	2.00	No
	143	x	-0.002	2.00	No
	148	x	-0.002	2.00	No
	162	x	-0.003	2.00	No
	165	x	-0.002	2.00	No
	170	x	-0.004	2.00	No
	175	x	-0.001	2.00	No
WL120	185	x	-0.001	2.00	No
	50	2	-0.002	2.00	No
	57	2	-0.003	2.00	No
	58	2	-0.003	2.00	No
	69	2	-0.004	1.00	No
		2	-0.004	3.00	No
		2	-0.004	5.00	No
		2	-0.004	7.00	No
	92	2	-0.01	1.25	No
		2	-0.01	6.25	No
	93	2	-0.011	1.25	No
		2	-0.011	6.25	No
	126	2	-0.003	2.00	No
	129	2	-0.003	2.00	No
	130	2	-0.002	2.00	No
	142	2	-0.003	2.00	No
	143	2	-0.002	2.00	No
	148	2	-0.003	2.00	No
	162	2	-0.003	2.00	No
	165	2	-0.002	2.00	No
	170	2	-0.003	2.00	No
	175	2	-0.002	2.00	No
WL150	185	2	-0.002	2.00	No
	50	2	-0.002	2.00	No
	57	2	-0.003	2.00	No
	58	2	-0.002	2.00	No
	69	2	-0.005	1.00	No
		2	-0.005	3.00	No
		2	-0.005	5.00	No
		2	-0.005	7.00	No
	92	2	-0.014	1.25	No
		2	-0.014	6.25	No
	93	2	-0.015	1.25	No

	2	-0.015	6.25	No
126	2	-0.003	2.00	No
129	2	-0.003	2.00	No
130	2	-0.003	2.00	No
142	2	-0.003	2.00	No
143	2	-0.003	2.00	No
148	2	-0.003	2.00	No
162	2	-0.002	2.00	No
165	2	-0.002	2.00	No
170	2	-0.003	2.00	No
175	2	-0.002	2.00	No
185	2	-0.002	2.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00

WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00

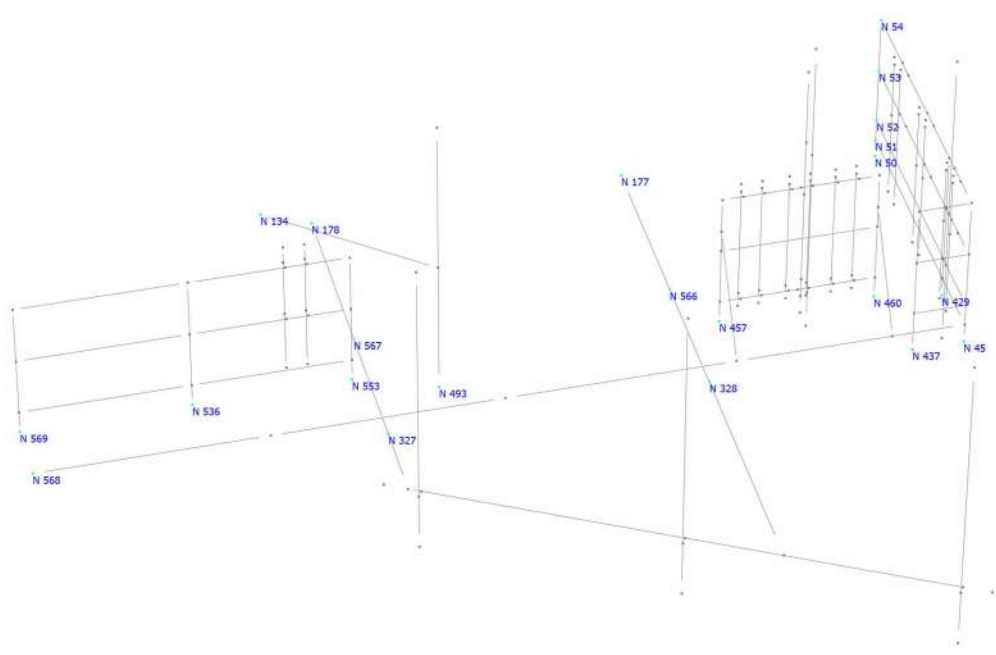
Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

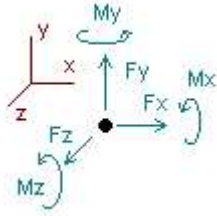
LC1=1.2D+1.6W_o
LC2=1.2D+1.6W₃₀
LC3=1.2D+1.6W₆₀
LC4=1.2D+1.6W₉₀
LC5=1.2D+1.6W₁₂₀
LC6=1.2D+1.6W₁₅₀
LC7=1.2D-1.6W_o
LC8=1.2D-1.6W₃₀
LC9=1.2D-1.6W₆₀
LC10=1.2D-1.6W₉₀
LC11=1.2D-1.6W₁₂₀
LC12=1.2D-1.6W₁₅₀
LC13=0.9D+1.6W_o
LC14=0.9D+1.6W₃₀
LC15=0.9D+1.6W₆₀
LC16=0.9D+1.6W₉₀
LC17=0.9D+1.6W₁₂₀
LC18=0.9D+1.6W₁₅₀
LC19=0.9D-1.6W_o
LC20=0.9D-1.6W₃₀
LC21=0.9D-1.6W₆₀
LC22=0.9D-1.6W₉₀
LC23=0.9D-1.6W₁₂₀
LC24=0.9D-1.6W₁₅₀
LC25=1.2D+Di+W_{I0}
LC26=1.2D+Di+W_{I30}
LC27=1.2D+Di+W_{I60}
LC28=1.2D+Di+W_{I90}
LC29=1.2D+Di+W_{I120}
LC30=1.2D+Di+W_{I150}
LC31=1.2D+Di-W_{I0}
LC32=1.2D+Di-W_{I30}
LC33=1.2D+Di-W_{I60}
LC34=1.2D+Di-W_{I90}
LC35=1.2D+Di-W_{I120}
LC36=1.2D+Di-W_{I150}
LC37=0.9D
LC38=1.2D
LC41=1.2D+W_{L0}
LC42=1.2D+W_{L30}
LC43=1.2D+W_{L60}
LC44=1.2D+W_{L90}
LC45=1.2D+W_{L120}
LC46=1.2D+W_{L150}
LC47=1.2D-W_{L0}
LC48=1.2D-W_{L30}
LC49=1.2D-W_{L60}
LC50=1.2D-W_{L90}
LC51=1.2D-W_{L120}
LC52=1.2D-W_{L150}

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
<i>HSS_SQR 3X3X1_4</i>		86	LC6 at 18.75%	0.76	OK	
		87	LC8 at 56.25%	0.79	OK	
<i>L 2-1_2X2-1_2X1_4</i>		31	LC22 at 26.56%	0.20	OK	
		32	LC10 at 12.50%	0.05	OK	
		33	LC4 at 44.53%	0.35	OK	
		117	LC4 at 12.50%	0.38	OK	
		118	LC4 at 0.00%	0.15	OK	
		119	LC4 at 100.00%	0.26	OK	
		121	LC4 at 0.00%	0.20	OK	
		122	LC7 at 89.06%	0.44	OK	
		133	LC3 at 84.38%	0.28	OK	
		134	LC1 at 25.00%	0.32	OK	
		135	LC7 at 50.00%	0.46	OK	
		136	LC11 at 100.00%	0.13	OK	
		137	LC11 at 100.00%	0.34	OK	
		138	LC7 at 0.00%	0.35	OK	
		139	LC8 at 0.00%	0.19	OK	
		172	LC1 at 100.00%	0.75	OK	
		179	LC7 at 100.00%	0.87	OK	
		180	LC7 at 64.58%	0.10	OK	
		181	LC7 at 39.58%	0.13	OK	
		182	LC2 at 0.00%	0.16	OK	
		188	LC1 at 100.00%	0.52	OK	
189	LC8 at 31.25%	0.09	OK			
190	LC6 at 0.00%	0.07	OK			
191	LC8 at 100.00%	0.18	OK			
<i>L 3X3X1_4</i>		62	LC5 at 50.00%	0.16	OK	
<i>LU 2-3/4x5x1/4</i>		14	LC7 at 100.00%	0.44	OK	
		19	LC7 at 15.63%	0.15	OK	
		36	LC13 at 100.00%	0.06	OK	
		40	LC13 at 22.92%	0.80	OK	
		187	LC7 at 0.00%	0.44	OK	
<i>P1000 Unistrut</i>		50	LC10 at 93.75%	0.14	OK	Eq. H1.2-1
		57	LC10 at 50.00%	0.26	OK	Eq. H1.2-1
		58	LC15 at 42.19%	0.15	OK	Eq. H1.2-1
		126	LC11 at 87.50%	0.30	OK	Eq. H1.2-1
		129	LC5 at 87.50%	0.26	OK	Eq. H1.2-1
		130	LC5 at 87.50%	0.23	OK	Eq. H1.2-1
		142	LC12 at 87.50%	0.27	OK	Eq. H1.2-1
		143	LC3 at 87.50%	0.28	OK	Eq. H1.2-1
		148	LC11 at 87.50%	0.26	OK	Eq. H1.2-1
		162	LC10 at 50.00%	0.14	OK	Eq. H1.1-1
		165	LC10 at 50.00%	0.15	OK	Eq. H1.2-1
		170	LC10 at 50.00%	0.25	OK	Eq. H1.2-1
		175	LC6 at 45.83%	0.07	OK	Sec. G5
		185	LC6 at 45.83%	0.08	OK	Sec. G5
		<i>PIPE 2-1_2x0.203</i>		69	LC7 at 78.13%	0.53
92	LC7 at 78.13%			0.81	OK	
93	LC7 at 78.13%			0.88	OK	
152	LC7 at 100.00%			0.34	OK	
<i>PIPE 2x0.154</i>		155	LC3 at 50.00%	0.12	OK	
		158	LC11 at 60.42%	0.05	OK	
		161	LC10 at 45.83%	0.08	OK	
<i>PIPE 3x0.216</i>		104	LC7 at 33.33%	0.91	OK	
<i>PL 2x1/4</i>		34	LC10 at 23.44%	0.23	With warnings	



Analysis result

Reactions



Direction of positive forces and moments

Node	Forces [Kip]			Moments [Kip*ft]		
	FX	FY	FZ	MX	MY	MZ
Condition LC1=1.2D+1.6Wo						
45	-0.37980	2.11213	0.06706	0.00000	0.00302	0.00000
50	0.00582	0.12373	0.05539	0.00000	0.00000	0.00000
52	0.04538	0.00000	0.00523	0.00000	0.00000	0.00000
53	-0.00663	0.00000	0.02199	0.00000	0.00000	0.00000
54	-0.00317	0.00000	0.60822	0.00000	0.00000	0.00000
134	0.14970	0.21675	0.46522	0.00000	0.00000	0.00000
177	0.01878	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.01461	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.38676	0.29941	0.60320	2.10039	0.00000	0.48756
328	0.41735	0.53214	1.88959	-0.18419	0.00000	0.41236
429	0.09752	0.39190	0.09349	0.00000	-0.00001	0.00000
437	0.85659	-4.27008	-0.22899	0.00000	-0.00039	0.00000
457	-0.00350	1.00258	1.18929	0.00000	-0.13607	0.00000
460	-0.63806	1.74695	1.28687	0.00000	0.00363	0.00000
493	-0.19244	-0.51650	-0.20089	0.00000	-0.03724	0.00000
536	-0.14580	0.57548	0.67548	0.00000	0.01458	0.00000
553	0.37190	0.46050	0.53516	0.00000	0.02327	0.00000
566	-0.15631	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.12154	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00627	-0.85105	-0.08364	0.00000	-0.01357	0.00000
569	-0.15125	0.50655	0.29414	0.00000	0.01278	0.00000
SUM	0.00000	2.45424	7.27680	1.89598	-0.13001	0.89992
Condition LC2=1.2D+1.6W30						
45	-0.34551	1.83025	0.06966	0.00000	0.00309	0.00000
50	0.00507	0.13318	0.04160	0.00000	0.00000	0.00000
52	0.05114	0.00000	0.05855	0.00000	0.00000	0.00000
53	-0.00627	0.00000	0.07140	0.00000	0.00000	0.00000
54	0.03533	0.00000	0.57912	0.00000	0.00000	0.00000
134	0.14457	0.21042	0.45223	0.00000	0.00000	0.00000
177	0.02649	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.06506	0.02228	0.00000	-0.01671	0.00000	0.00000
327	1.59367	0.63976	1.25333	0.26715	0.00000	-0.12562
328	0.44789	0.19179	0.85388	0.47604	0.00000	-0.14166
429	-0.05022	0.31567	0.01988	0.00000	-0.00001	0.00000
437	0.78764	-3.73688	-0.17188	0.00000	-0.00036	0.00000
457	0.25022	1.05912	1.08193	0.00000	-0.12758	0.00000
460	-0.26659	1.49465	1.20119	0.00000	0.00133	0.00000

493	-0.17816	-0.47029	-0.18474	0.00000	-0.03979	0.00000
536	-0.15058	0.53658	0.65318	0.00000	0.01666	0.00000
553	0.31132	0.46378	0.49710	0.00000	0.03317	0.00000
566	-0.22046	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.54143	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00538	-0.81718	-0.07861	0.00000	-0.01378	0.00000
569	-0.13683	0.47965	0.28936	0.00000	0.01336	0.00000

SUM	1.81698	2.45425	6.68718	0.72297	-0.11391	-0.26728
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Condition **LC3=1.2D+1.6W60**

45	0.00878	-1.01341	0.07739	0.00000	0.00311	0.00000
50	0.02680	0.16357	-0.00794	0.00000	0.00001	0.00000
52	0.13061	0.00000	0.04221	0.00000	0.00000	0.00000
53	0.05427	0.00000	0.00859	0.00000	0.00000	0.00000
54	0.22917	0.00000	0.20484	0.00000	0.00000	0.00000
134	0.13286	0.03079	0.01225	0.00000	0.00000	0.00000
177	0.06533	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.12604	0.02228	0.00000	-0.01671	0.00000	0.00000
327	2.17239	0.63005	1.09411	-1.00366	0.00000	-0.15203
328	0.49790	0.20149	-0.11435	-0.57276	0.00000	-0.21239
429	-0.96819	-0.17591	-0.51032	0.00000	-0.00003	0.00000
437	0.07279	1.32355	0.22266	0.00000	-0.00005	0.00000
457	1.31290	0.99739	0.34703	0.00000	-0.00927	0.00000
460	1.79549	-0.19745	0.25910	0.00000	0.00556	0.00000
493	0.34664	-0.21749	-0.05597	0.00000	-0.10706	0.00000
536	0.13579	0.17045	-0.00046	0.00000	-0.01327	0.00000
553	0.33057	0.23952	-0.01568	0.00000	-0.00743	0.00000
566	-0.12901	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.63421	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00648	0.09265	0.01619	0.00000	-0.00039	0.00000
569	0.01101	0.08526	-0.03646	0.00000	0.00311	0.00000

SUM	5.72441	2.45425	1.54319	-1.59663	-0.12570	-0.36442
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Condition **LC4=1.2D+1.6W90**

45	0.05419	-1.31161	0.06975	0.00000	0.00277	0.00000
50	0.02531	0.17805	-0.02055	0.00000	0.00001	0.00000
52	0.13233	0.00000	0.02423	0.00000	0.00000	0.00000
53	0.05643	0.00000	-0.06368	0.00000	0.00000	0.00000
54	0.25679	0.00000	0.08998	0.00000	0.00000	0.00000
134	0.12804	0.02382	-0.00233	0.00000	0.00000	0.00000
177	0.05627	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.13004	0.02228	0.00000	-0.01671	0.00000	0.00000
327	2.30479	0.63654	0.88219	-2.47683	0.00000	-0.23800
328	0.30237	0.19501	-0.88219	-1.70522	0.00000	-0.32409
429	-1.05812	-0.20974	-0.55755	0.00000	-0.00003	0.00000
437	-0.01962	1.90837	0.25883	0.00000	-0.00002	0.00000
457	1.29899	0.84262	0.20630	0.00000	0.01723	0.00000
460	1.89568	-0.32097	0.12329	0.00000	0.00573	0.00000
493	0.35794	-0.16744	-0.03244	0.00000	-0.10476	0.00000
536	0.08054	0.13156	-0.02540	0.00000	-0.00537	0.00000
553	0.22230	0.24891	-0.05276	0.00000	0.00304	0.00000
566	-0.05358	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.66750	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00697	0.12932	0.02220	0.00000	-0.00048	0.00000
569	-0.00414	0.04604	-0.03988	0.00000	0.00719	0.00000

SUM	5.50602	2.45425	0.00000	-4.20226	-0.07469	-0.56209
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Condition **LC5=1.2D+1.6W120**

45	0.10576	-1.52701	0.05375	0.00000	0.00209	0.00000
50	0.02464	0.18129	-0.00752	0.00000	0.00001	0.00000
52	0.12211	0.00000	-0.00391	0.00000	0.00000	0.00000
53	0.05890	0.00000	-0.19519	0.00000	0.00000	0.00000
54	0.23368	0.00000	0.00523	0.00000	0.00000	0.00000
134	0.12286	0.01631	-0.01805	0.00000	0.00000	0.00000
177	0.04930	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.13702	0.02228	0.00000	-0.01671	0.00000	0.00000
327	2.48830	0.58311	0.66323	-3.73240	0.00000	-0.27802
328	0.14495	0.24843	-1.64300	-2.99419	0.00000	-0.33622
429	-0.96942	-0.16730	-0.52332	0.00000	-0.00002	0.00000
437	-0.15823	2.35735	0.21759	0.00000	0.00003	0.00000
457	1.32966	0.80638	0.05481	0.00000	0.02122	0.00000
460	1.91855	-0.57675	-0.01456	0.00000	0.00281	0.00000
493	0.36708	-0.11721	0.00721	0.00000	-0.09421	0.00000
536	0.18589	0.11335	-0.04316	0.00000	-0.01637	0.00000
553	0.20620	0.18190	-0.08971	0.00000	-0.00372	0.00000
566	0.00439	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.72553	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00632	0.16427	0.02942	0.00000	-0.00022	0.00000
569	0.07197	0.06634	-0.03602	0.00000	-0.00094	0.00000

SUM 5.72441 2.45425 -1.54319 -6.74681 -0.08934 -0.61424

Condition **LC6=1.2D+1.6W150**

45	0.39832	-2.17485	-0.08508	0.00000	-0.00374	0.00000
50	0.00085	0.13891	0.01281	0.00000	0.00000	0.00000
52	-0.02505	0.00000	-0.12543	0.00000	0.00000	0.00000
53	0.00412	0.00000	-0.26952	0.00000	0.00000	0.00000
54	0.04772	0.00000	-0.38502	0.00000	0.00000	0.00000
134	-0.14033	-0.17030	-0.47664	0.00000	0.00000	0.00000
177	-0.00124	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.08927	0.02228	0.00000	-0.01671	0.00000	0.00000
327	2.19000	0.54971	0.20672	-4.87580	0.00000	-0.39427
328	-0.17427	0.28184	-2.31393	-3.99539	0.00000	-0.38928
429	-0.25405	0.09618	-0.20160	0.00000	0.00001	0.00000
437	-0.89642	4.56381	0.23828	0.00000	0.00039	0.00000
457	0.39606	-0.29272	-1.04927	0.00000	0.14927	0.00000
460	0.83266	-1.29974	-0.91720	0.00000	-0.00050	0.00000
493	0.18111	0.70545	0.17584	0.00000	0.02278	0.00000
536	0.10777	-0.34769	-0.66634	0.00000	-0.00850	0.00000
553	-0.34610	-0.19042	-0.51121	0.00000	-0.01148	0.00000
566	0.01035	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.74289	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00813	0.88943	0.08960	0.00000	0.01596	0.00000
569	0.13097	-0.41911	-0.30718	0.00000	-0.00843	0.00000

SUM 1.81698 2.45425 -6.58518 -8.89141 0.15575 -0.78354

Condition **LC7=1.2D-1.6Wo**

45	0.42453	-2.25078	-0.09255	0.00000	-0.00406	0.00000
50	0.00018	0.13420	0.03817	0.00000	0.00000	0.00000
52	-0.03674	0.00000	-0.11997	0.00000	0.00000	0.00000
53	0.00463	0.00000	-0.27073	0.00000	0.00000	0.00000
54	0.01171	0.00000	-0.44835	0.00000	0.00000	0.00000
134	-0.14437	-0.17617	-0.48892	0.00000	0.00000	0.00000
177	-0.01811	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.01444	0.02228	0.00000	-0.01671	0.00000	0.00000

327	0.37923	0.21477	-0.61171	-4.35121	0.00000	0.16883
328	-0.40609	0.61678	-1.88107	-5.60023	0.00000	0.08564
429	-0.13235	0.15360	-0.15363	0.00000	0.00001	0.00000
437	-0.96536	4.80771	0.23979	0.00000	0.00043	0.00000
457	0.15245	-0.48532	-1.15575	0.00000	0.16596	0.00000
460	0.56084	-1.33076	-1.10846	0.00000	-0.00062	0.00000
493	0.18376	0.74297	0.20689	0.00000	0.03376	0.00000
536	0.15554	-0.36106	-0.68331	0.00000	-0.01334	0.00000
553	-0.39189	-0.24699	-0.54116	0.00000	-0.01456	0.00000
566	0.15069	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.12016	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00716	0.92462	0.09703	0.00000	0.01626	0.00000
569	0.16988	-0.41307	-0.30306	0.00000	-0.01271	0.00000
SUM	0.00000	2.45425	-7.27680	-9.97165	0.17111	0.25447

Condition **LC8=1.2D-1.6W30**

45	0.38455	-1.95760	-0.08898	0.00000	-0.00388	0.00000
50	0.00013	0.12557	0.05110	0.00000	0.00000	0.00000
52	-0.04347	0.00000	-0.16658	0.00000	0.00000	0.00000
53	0.00398	0.00000	-0.26822	0.00000	0.00000	0.00000
54	-0.02698	0.00000	-0.44966	0.00000	0.00000	0.00000
134	-0.13973	-0.16942	-0.47477	0.00000	0.00000	0.00000
177	-0.02594	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.06447	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-1.59299	-0.09566	-1.25632	-2.60235	0.00000	0.79599
328	-0.44014	0.92721	-0.85089	-6.23568	0.00000	0.60831
429	0.01406	0.22611	-0.08222	0.00000	0.00001	0.00000
437	-0.89124	4.26065	0.18349	0.00000	0.00039	0.00000
457	-0.09880	-0.53931	-1.05136	0.00000	0.15555	0.00000
460	0.19155	-1.07538	-1.05656	0.00000	0.00176	0.00000
493	0.17171	0.69401	0.19277	0.00000	0.03782	0.00000
536	0.15492	-0.32033	-0.65880	0.00000	-0.01539	0.00000
553	-0.32120	-0.24816	-0.50326	0.00000	-0.02743	0.00000
566	0.21585	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.53647	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00619	0.89366	0.09204	0.00000	0.01647	0.00000
569	0.14856	-0.39087	-0.29895	0.00000	-0.01305	0.00000
SUM	-1.81698	2.45424	-6.68718	-8.85825	0.15226	1.40430

Condition **LC9=1.2D-1.6W60**

45	0.02457	0.90847	-0.09148	0.00000	-0.00369	0.00000
50	-0.02275	0.09919	0.10040	0.00000	-0.00001	0.00000
52	-0.12463	0.00000	-0.13430	0.00000	0.00000	0.00000
53	-0.05735	0.00000	-0.12014	0.00000	0.00000	0.00000
54	-0.22117	0.00000	-0.13087	0.00000	0.00000	0.00000
134	-0.14027	0.01072	-0.02915	0.00000	0.00000	0.00000
177	-0.06506	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.12531	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-2.16974	-0.08711	-1.09407	-1.38271	0.00000	0.83935
328	-0.49320	0.91865	0.11430	-5.33336	0.00000	0.69688
429	0.93083	0.70650	0.44544	0.00000	0.00002	0.00000
437	-0.16731	-0.82479	-0.20616	0.00000	0.00009	0.00000
457	-1.16132	-0.47350	-0.32341	0.00000	0.03612	0.00000
460	-1.86754	0.62292	-0.16705	0.00000	-0.00237	0.00000
493	-0.33869	0.43766	0.06283	0.00000	0.10761	0.00000
536	-0.13379	0.04249	-0.00950	0.00000	0.01432	0.00000
553	-0.32595	-0.01866	0.01104	0.00000	0.00893	0.00000

566	0.12677	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.62810	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00581	-0.01547	-0.00293	0.00000	0.00310	0.00000
569	-0.01481	0.00340	0.03186	0.00000	-0.00164	0.00000

SUM	-5.72441	2.45424	-1.54319	-6.73629	0.16247	1.53623

Condition **LC10=1.2D-1.6W90**

45	-0.01469	1.19309	-0.09112	0.00000	-0.00364	0.00000
50	-0.02045	0.08613	0.11465	0.00000	-0.00001	0.00000
52	-0.12559	0.00000	-0.14255	0.00000	0.00000	0.00000
53	-0.05905	0.00000	-0.03778	0.00000	0.00000	0.00000
54	-0.24842	0.00000	-0.02621	0.00000	0.00000	0.00000
134	-0.13467	0.01767	-0.01489	0.00000	0.00000	0.00000
177	-0.05621	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.12945	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-2.30245	-0.10332	-0.88116	0.08803	0.00000	0.93027
328	-0.29997	0.93486	0.88116	-4.27420	0.00000	0.82270
429	1.02316	0.75102	0.49531	0.00000	0.00002	0.00000
437	-0.07648	-1.40700	-0.24068	0.00000	0.00005	0.00000
457	-1.15117	-0.31960	-0.18118	0.00000	0.01150	0.00000
460	-1.97376	0.74595	-0.00085	0.00000	-0.00286	0.00000
493	-0.35257	0.38769	0.03648	0.00000	0.10412	0.00000
536	-0.07795	0.08153	0.01511	0.00000	0.00639	0.00000
553	-0.21625	-0.02788	0.04789	0.00000	-0.00077	0.00000
566	0.05311	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.66257	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00621	-0.05219	-0.00906	0.00000	0.00317	0.00000
569	0.00047	0.04254	0.03487	0.00000	-0.00567	0.00000

SUM	-5.50603	2.45424	0.00000	-4.20639	0.11229	1.75297

Condition **LC11=1.2D-1.6W120**

45	-0.06380	1.40490	-0.07808	0.00000	-0.00308	0.00000
50	-0.01904	0.08083	0.10181	0.00000	-0.00001	0.00000
52	-0.11440	0.00000	-0.11850	0.00000	0.00000	0.00000
53	-0.06061	0.00000	0.03006	0.00000	0.00000	0.00000
54	-0.22503	0.00000	0.09850	0.00000	0.00000	0.00000
134	-0.12855	0.02525	0.00065	0.00000	0.00000	0.00000
177	-0.04919	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.13660	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-2.48942	-0.06498	-0.66469	1.38623	0.00000	0.96293
328	-0.13998	0.89653	1.64446	-2.98396	0.00000	0.84619
429	0.93658	0.71244	0.46294	0.00000	0.00002	0.00000
437	0.05939	-1.85254	-0.20125	0.00000	0.00000	0.00000
457	-1.18519	-0.28474	-0.02597	0.00000	0.00907	0.00000
460	-1.99858	1.00101	0.16793	0.00000	0.00003	0.00000
493	-0.36424	0.33715	-0.00623	0.00000	0.09201	0.00000
536	-0.18355	0.10014	0.03276	0.00000	0.01739	0.00000
553	-0.19680	0.03986	0.08489	0.00000	0.00685	0.00000
566	-0.00536	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.72211	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00548	-0.08696	-0.01643	0.00000	0.00288	0.00000
569	-0.07665	0.02160	0.03034	0.00000	0.00255	0.00000

SUM	-5.72441	2.45424	1.54319	-1.61795	0.12771	1.80912

Condition **LC12=1.2D-1.6W150**

45	-0.35224	2.03303	0.05790	0.00000	0.00263	0.00000
50	0.00473	0.11983	0.08054	0.00000	0.00000	0.00000
52	0.03291	0.00000	0.00944	0.00000	0.00000	0.00000
53	-0.00593	0.00000	0.06497	0.00000	0.00000	0.00000
54	-0.03893	0.00000	0.51736	0.00000	0.00000	0.00000
134	0.14490	0.21081	0.45304	0.00000	0.00000	0.00000
177	0.00158	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.08927	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-2.19632	-0.04421	-0.21242	2.60189	0.00000	1.06264
328	0.18310	0.87575	2.31963	-1.89857	0.00000	0.90158
429	0.22219	0.45030	0.14449	0.00000	-0.00001	0.00000
437	0.78703	-4.02514	-0.22761	0.00000	-0.00036	0.00000
457	-0.24828	0.80902	1.07982	0.00000	-0.11993	0.00000
460	-0.91041	1.71716	1.07964	0.00000	0.00353	0.00000
493	-0.18849	-0.47856	-0.16815	0.00000	-0.02532	0.00000
536	-0.09578	0.56225	0.65839	0.00000	0.00978	0.00000
553	0.32056	0.40343	0.50524	0.00000	0.02033	0.00000
566	-0.01317	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.74285	0.03960	0.00000	0.00660	0.00000	0.00000
568	-0.00731	-0.81970	-0.07638	0.00000	-0.01323	0.00000
569	-0.11070	0.51651	0.29929	0.00000	0.00856	0.00000

 SUM -1.81698 2.45424 6.58518 0.68311 -0.11402 1.96423

Condition **LC13=0.9D+1.6Wo**

45	-0.38182	2.12080	0.06683	0.00000	0.00301	0.00000
50	0.00564	0.09080	0.04411	0.00000	0.00000	0.00000
52	0.04492	0.00000	0.01623	0.00000	0.00000	0.00000
53	-0.00635	0.00000	0.01644	0.00000	0.00000	0.00000
54	-0.00432	0.00000	0.61012	0.00000	0.00000	0.00000
134	0.15010	0.21103	0.46628	0.00000	0.00000	0.00000
177	0.01878	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.01461	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-0.38676	0.23331	0.60320	2.39761	0.00000	0.39885
328	0.41735	0.39035	1.88959	0.58271	0.00000	0.34478
429	0.10120	0.32525	0.10140	0.00000	-0.00001	0.00000
437	0.86623	-4.32556	-0.23031	0.00000	-0.00039	0.00000
457	-0.02315	0.93680	1.18746	0.00000	-0.13817	0.00000
460	-0.62810	1.69264	1.28609	0.00000	0.00318	0.00000
493	-0.19336	-0.54178	-0.20153	0.00000	-0.03796	0.00000
536	-0.14475	0.54602	0.67599	0.00000	0.01430	0.00000
553	0.36956	0.43077	0.53513	0.00000	0.02359	0.00000
566	-0.15631	0.02970	0.00000	0.00495	0.00000	0.00000
567	0.12154	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00630	-0.85541	-0.08456	0.00000	-0.01393	0.00000
569	-0.14949	0.49284	0.29433	0.00000	0.01247	0.00000

 SUM 0.00000 1.84068 7.27680 2.96516 -0.13392 0.74363

Condition **LC14=0.9D+1.6W30**

45	-0.34760	1.83928	0.06944	0.00000	0.00308	0.00000
50	0.00489	0.10025	0.03032	0.00000	0.00000	0.00000
52	0.05069	0.00000	0.06955	0.00000	0.00000	0.00000
53	-0.00600	0.00000	0.06586	0.00000	0.00000	0.00000
54	0.03418	0.00000	0.58102	0.00000	0.00000	0.00000
134	0.14499	0.20473	0.45335	0.00000	0.00000	0.00000
177	0.02649	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.06506	0.01671	0.00000	-0.01253	0.00000	0.00000
327	1.59367	0.57538	1.25333	0.56291	0.00000	-0.21287

328	0.44789	0.04828	0.85388	1.24274	0.00000	-0.20914
429	-0.04651	0.24905	0.02781	0.00000	-0.00001	0.00000
437	0.79743	-3.79291	-0.17321	0.00000	-0.00036	0.00000
457	0.23054	0.99338	1.08010	0.00000	-0.12972	0.00000
460	-0.25671	1.44043	1.20038	0.00000	0.00088	0.00000
493	-0.17911	-0.49572	-0.18545	0.00000	-0.04050	0.00000
536	-0.14964	0.50727	0.65371	0.00000	0.01639	0.00000
553	0.30921	0.43419	0.49709	0.00000	0.03346	0.00000
566	-0.22046	0.02970	0.00000	0.00495	0.00000	0.00000
567	-0.54143	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00541	-0.82178	-0.07957	0.00000	-0.01415	0.00000
569	-0.13520	0.46603	0.28956	0.00000	0.01307	0.00000

SUM	1.81698	1.84069	6.68718	1.79050	-0.11785	-0.42201
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Condition **LC15=0.9D+1.6W60**

45	0.00575	-0.99931	0.07726	0.00000	0.00310	0.00000
50	0.02655	0.13070	-0.01923	0.00000	0.00001	0.00000
52	0.13035	0.00000	0.05122	0.00000	0.00000	0.00000
53	0.05453	0.00000	0.00309	0.00000	0.00000	0.00000
54	0.22805	0.00000	0.20693	0.00000	0.00000	0.00000
134	0.13372	0.02578	0.01482	0.00000	0.00000	0.00000
177	0.06533	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.12604	0.01671	0.00000	-0.01253	0.00000	0.00000
327	2.17239	0.56635	1.09411	-0.70938	0.00000	-0.23795
328	0.49790	0.05731	-0.11435	0.18804	0.00000	-0.27888
429	-0.96430	-0.24191	-0.50210	0.00000	-0.00003	0.00000
437	0.08491	1.25963	0.22134	0.00000	-0.00006	0.00000
457	1.29261	0.93182	0.34516	0.00000	-0.01201	0.00000
460	1.80420	-0.25034	0.25976	0.00000	0.00504	0.00000
493	0.34502	-0.24399	-0.05867	0.00000	-0.10746	0.00000
536	0.13602	0.14382	0.00052	0.00000	-0.01344	0.00000
553	0.33029	0.21111	-0.01498	0.00000	-0.00713	0.00000
566	-0.12901	0.02970	0.00000	0.00495	0.00000	0.00000
567	-0.63421	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00644	0.08259	0.01438	0.00000	-0.00074	0.00000
569	0.01182	0.07430	-0.03607	0.00000	0.00291	0.00000

SUM	5.72441	1.84069	1.54319	-0.53651	-0.12979	-0.51682
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Condition **LC16=0.9D+1.6W90**

45	0.05106	-1.29715	0.06968	0.00000	0.00276	0.00000
50	0.02506	0.14522	-0.03183	0.00000	0.00001	0.00000
52	0.13206	0.00000	0.03276	0.00000	0.00000	0.00000
53	0.05668	0.00000	-0.06771	0.00000	0.00000	0.00000
54	0.25568	0.00000	0.09126	0.00000	0.00000	0.00000
134	0.12891	0.01885	0.00031	0.00000	0.00000	0.00000
177	0.05627	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.13004	0.01671	0.00000	-0.01253	0.00000	0.00000
327	2.30479	0.57308	0.88219	-2.18232	0.00000	-0.32279
328	0.30237	0.05058	-0.88219	-0.94916	0.00000	-0.38940
429	-1.05415	-0.27577	-0.54929	0.00000	-0.00002	0.00000
437	-0.00733	1.84389	0.25750	0.00000	-0.00002	0.00000
457	1.27868	0.77711	0.20439	0.00000	0.01443	0.00000
460	1.90430	-0.37378	0.12367	0.00000	0.00521	0.00000
493	0.35631	-0.19411	-0.03521	0.00000	-0.10514	0.00000
536	0.08063	0.10510	-0.02438	0.00000	-0.00553	0.00000
553	0.22232	0.22065	-0.05202	0.00000	0.00329	0.00000
566	-0.05358	0.02970	0.00000	0.00495	0.00000	0.00000

567	-0.66750	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00692	0.11903	0.02035	0.00000	-0.00083	0.00000
569	-0.00350	0.03516	-0.03948	0.00000	0.00700	0.00000

SUM	5.50602	1.84069	0.00000	-3.14664	-0.07885	-0.71220
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Condition **LC17=0.9D+1.6W120**

45	0.10256	-1.51216	0.05369	0.00000	0.00209	0.00000
50	0.02439	0.14846	-0.01880	0.00000	0.00001	0.00000
52	0.12185	0.00000	0.00463	0.00000	0.00000	0.00000
53	0.05915	0.00000	-0.19923	0.00000	0.00000	0.00000
54	0.23257	0.00000	0.00652	0.00000	0.00000	0.00000
134	0.12375	0.01138	-0.01533	0.00000	0.00000	0.00000
177	0.04930	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.13702	0.01671	0.00000	-0.01253	0.00000	0.00000
327	2.48831	0.51998	0.66324	-3.43803	0.00000	-0.36173
328	0.14495	0.10368	-1.64300	-2.24268	0.00000	-0.40051
429	-0.96549	-0.23333	-0.51507	0.00000	-0.00002	0.00000
437	-0.14576	2.29229	0.21628	0.00000	0.00002	0.00000
457	1.30932	0.74093	0.05290	0.00000	0.01838	0.00000
460	1.92711	-0.62945	-0.01422	0.00000	0.00229	0.00000
493	0.36543	-0.14406	0.00434	0.00000	-0.09459	0.00000
536	0.18584	0.08706	-0.04210	0.00000	-0.01653	0.00000
553	0.20654	0.15381	-0.08894	0.00000	-0.00351	0.00000
566	0.00439	0.02970	0.00000	0.00495	0.00000	0.00000
567	-0.72553	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00627	0.15374	0.02753	0.00000	-0.00057	0.00000
569	0.07243	0.05552	-0.03561	0.00000	-0.00112	0.00000

SUM	5.72441	1.84069	-1.54319	-5.69587	-0.09355	-0.76225
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Condition **LC18=0.9D+1.6W150**

45	0.39450	-2.15689	-0.08501	0.00000	-0.00374	0.00000
50	0.00057	0.10614	0.00152	0.00000	0.00000	0.00000
52	-0.02528	0.00000	-0.11686	0.00000	0.00000	0.00000
53	0.00437	0.00000	-0.27356	0.00000	0.00000	0.00000
54	0.04665	0.00000	-0.38372	0.00000	0.00000	0.00000
134	-0.13929	-0.17497	-0.47334	0.00000	0.00000	0.00000
177	-0.00124	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.08927	0.01671	0.00000	-0.01253	0.00000	0.00000
327	2.19000	0.48644	0.20672	-4.58142	0.00000	-0.47679
328	-0.17427	0.13723	-2.31393	-3.25015	0.00000	-0.45239
429	-0.25034	0.03011	-0.19342	0.00000	0.00001	0.00000
437	-0.88242	4.49415	0.23712	0.00000	0.00039	0.00000
457	0.37546	-0.35786	-1.05127	0.00000	0.14605	0.00000
460	0.84073	-1.35171	-0.91712	0.00000	-0.00106	0.00000
493	0.17927	0.67576	0.17205	0.00000	0.02222	0.00000
536	0.10680	-0.37159	-0.66483	0.00000	-0.00852	0.00000
553	-0.34356	-0.21596	-0.51008	0.00000	-0.01139	0.00000
566	0.01035	0.02970	0.00000	0.00495	0.00000	0.00000
567	-0.74289	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00806	0.87477	0.08715	0.00000	0.01562	0.00000
569	0.13023	-0.42775	-0.30659	0.00000	-0.00845	0.00000

SUM	1.81698	1.84069	-6.58518	-7.84673	0.15114	-0.92917
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Condition **LC19=0.9D-1.6W0**

45	0.42066	-2.23258	-0.09246	0.00000	-0.00406	0.00000
50	-0.00010	0.10143	0.02688	0.00000	0.00000	0.00000
52	-0.03696	0.00000	-0.11138	0.00000	0.00000	0.00000
53	0.00488	0.00000	-0.27478	0.00000	0.00000	0.00000
54	0.01064	0.00000	-0.44705	0.00000	0.00000	0.00000
134	-0.14330	-0.18081	-0.48556	0.00000	0.00000	0.00000
177	-0.01811	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.01444	0.01671	0.00000	-0.01253	0.00000	0.00000
327	0.37923	0.15011	-0.61171	-4.05505	0.00000	0.08564
328	-0.40609	0.47355	-1.88107	-4.85784	0.00000	0.02334
429	-0.12867	0.08753	-0.14547	0.00000	0.00001	0.00000
437	-0.95123	4.73769	0.23865	0.00000	0.00042	0.00000
457	0.13183	-0.55045	-1.15777	0.00000	0.16272	0.00000
460	0.56887	-1.38266	-1.10840	0.00000	-0.00119	0.00000
493	0.18191	0.71313	0.20301	0.00000	0.03320	0.00000
536	0.15446	-0.38480	-0.68177	0.00000	-0.01335	0.00000
553	-0.38909	-0.27238	-0.53999	0.00000	-0.01449	0.00000
566	0.15069	0.02970	0.00000	0.00495	0.00000	0.00000
567	-0.12016	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00710	0.90973	0.09454	0.00000	0.01592	0.00000
569	0.16899	-0.42163	-0.30247	0.00000	-0.01271	0.00000
SUM	0.00000	1.84068	-7.27680	-8.92805	0.16647	0.10898

Condition **LC20=0.9D-1.6W30**

45	0.38076	-1.93981	-0.08891	0.00000	-0.00388	0.00000
50	-0.00014	0.09280	0.03980	0.00000	0.00000	0.00000
52	-0.04369	0.00000	-0.15799	0.00000	0.00000	0.00000
53	0.00423	0.00000	-0.27228	0.00000	0.00000	0.00000
54	-0.02805	0.00000	-0.44836	0.00000	0.00000	0.00000
134	-0.13868	-0.17409	-0.47149	0.00000	0.00000	0.00000
177	-0.02594	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.06447	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-1.59299	-0.16196	-1.25632	-2.30488	0.00000	0.71138
328	-0.44014	0.78562	-0.85089	-5.49313	0.00000	0.54589
429	0.01770	0.16000	-0.07408	0.00000	0.00001	0.00000
437	-0.87728	4.19127	0.18237	0.00000	0.00039	0.00000
457	-0.11937	-0.60450	-1.05338	0.00000	0.15235	0.00000
460	0.19967	-1.12738	-1.05646	0.00000	0.00121	0.00000
493	0.16988	0.66435	0.18899	0.00000	0.03726	0.00000
536	0.15400	-0.34424	-0.65731	0.00000	-0.01540	0.00000
553	-0.31876	-0.27371	-0.50212	0.00000	-0.02732	0.00000
566	0.21585	0.02970	0.00000	0.00495	0.00000	0.00000
567	0.53647	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00612	0.87897	0.08959	0.00000	0.01613	0.00000
569	0.14787	-0.39946	-0.29836	0.00000	-0.01307	0.00000
SUM	-1.81698	1.84068	-6.68718	-7.81316	0.14768	1.25728

Condition **LC21=0.9D-1.6W60**

45	0.02176	0.92109	-0.09155	0.00000	-0.00369	0.00000
50	-0.02296	0.06632	0.08911	0.00000	-0.00001	0.00000
52	-0.12504	0.00000	-0.12326	0.00000	0.00000	0.00000
53	-0.05708	0.00000	-0.12526	0.00000	0.00000	0.00000
54	-0.22227	0.00000	-0.12920	0.00000	0.00000	0.00000
134	-0.13957	0.00536	-0.02737	0.00000	0.00000	0.00000
177	-0.06506	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.12531	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-2.16974	-0.15409	-1.09407	-1.08377	0.00000	0.75347

328	-0.49320	0.77774	0.11430	-4.58520	0.00000	0.63352
429	0.93426	0.63982	0.45331	0.00000	0.00002	0.00000
437	-0.15572	-0.88613	-0.20729	0.00000	0.00009	0.00000
457	-1.18129	-0.53886	-0.32538	0.00000	0.03351	0.00000
460	-1.85824	0.56956	-0.16837	0.00000	-0.00286	0.00000
493	-0.33994	0.40912	0.06109	0.00000	0.10674	0.00000
536	-0.13393	0.01592	-0.00841	0.00000	0.01421	0.00000
553	-0.32566	-0.04546	0.01146	0.00000	0.00908	0.00000
566	0.12677	0.02970	0.00000	0.00495	0.00000	0.00000
567	0.62810	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00586	-0.02475	-0.00453	0.00000	0.00275	0.00000
569	-0.01444	-0.00780	0.03223	0.00000	-0.00177	0.00000
SUM	-5.72441	1.84068	-1.54319	-5.68414	0.15807	1.38699

Condition **LC22=0.9D-1.6W90**

45	-0.01744	1.20534	-0.09119	0.00000	-0.00364	0.00000
50	-0.02066	0.05326	0.10336	0.00000	-0.00001	0.00000
52	-0.12600	0.00000	-0.13150	0.00000	0.00000	0.00000
53	-0.05878	0.00000	-0.04289	0.00000	0.00000	0.00000
54	-0.24952	0.00000	-0.02455	0.00000	0.00000	0.00000
134	-0.13400	0.01228	-0.01317	0.00000	0.00000	0.00000
177	-0.05621	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.12945	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-2.30245	-0.17056	-0.88116	0.38676	0.00000	0.84328
328	-0.29997	0.79422	0.88116	-3.52140	0.00000	0.75818
429	1.02657	0.68432	0.50316	0.00000	0.00002	0.00000
437	-0.06504	-1.46780	-0.24180	0.00000	0.00005	0.00000
457	-1.17111	-0.38502	-0.18315	0.00000	0.00894	0.00000
460	-1.96439	0.69251	-0.00214	0.00000	-0.00335	0.00000
493	-0.35378	0.35931	0.03483	0.00000	0.10324	0.00000
536	-0.07796	0.05478	0.01616	0.00000	0.00627	0.00000
553	-0.21626	-0.05484	0.04827	0.00000	-0.00058	0.00000
566	0.05311	0.02970	0.00000	0.00495	0.00000	0.00000
567	0.66257	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00626	-0.06123	-0.01062	0.00000	0.00282	0.00000
569	0.00100	0.03127	0.03523	0.00000	-0.00582	0.00000
SUM	-5.50602	1.84068	0.00000	-3.14979	0.10793	1.60146

Condition **LC23=0.9D-1.6W120**

45	-0.06645	1.41679	-0.07820	0.00000	-0.00309	0.00000
50	-0.01923	0.04797	0.09050	0.00000	-0.00001	0.00000
52	-0.11482	0.00000	-0.10744	0.00000	0.00000	0.00000
53	-0.06036	0.00000	0.02455	0.00000	0.00000	0.00000
54	-0.22613	0.00000	0.10037	0.00000	0.00000	0.00000
134	-0.12790	0.01982	0.00230	0.00000	0.00000	0.00000
177	-0.04919	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.13660	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-2.48942	-0.13258	-0.66469	1.68515	0.00000	0.87484
328	-0.13998	0.75624	1.64446	-2.22658	0.00000	0.78066
429	0.94000	0.64572	0.47079	0.00000	0.00002	0.00000
437	0.07062	-1.91277	-0.20240	0.00000	0.00000	0.00000
457	-1.20511	-0.35021	-0.02793	0.00000	0.00656	0.00000
460	-1.98915	0.94746	0.16693	0.00000	-0.00046	0.00000
493	-0.36543	0.30896	-0.00779	0.00000	0.09113	0.00000
536	-0.18341	0.07322	0.03376	0.00000	0.01726	0.00000
553	-0.19715	0.01273	0.08523	0.00000	0.00709	0.00000
566	-0.00536	0.02970	0.00000	0.00495	0.00000	0.00000

567	0.72211	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00552	-0.09576	-0.01795	0.00000	0.00253	0.00000
569	-0.07592	0.01026	0.03069	0.00000	0.00240	0.00000

SUM	-5.72441	1.84068	1.54319	-0.55659	0.12343	1.65550
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Condition **LC24=0.9D-1.6W150**

45	-0.35432	2.04194	0.05769	0.00000	0.00262	0.00000
50	0.00455	0.08691	0.06925	0.00000	0.00000	0.00000
52	0.03246	0.00000	0.02045	0.00000	0.00000	0.00000
53	-0.00566	0.00000	0.05943	0.00000	0.00000	0.00000
54	-0.04007	0.00000	0.51927	0.00000	0.00000	0.00000
134	0.14532	0.20512	0.45416	0.00000	0.00000	0.00000
177	0.00158	0.01671	0.00000	-0.01253	0.00000	0.00000
178	-0.08927	0.01671	0.00000	-0.01253	0.00000	0.00000
327	-2.19632	-0.11173	-0.21242	2.90095	0.00000	0.97329
328	0.18310	0.73539	2.31963	-1.13471	0.00000	0.83486
429	0.22583	0.38364	0.15238	0.00000	-0.00001	0.00000
437	0.79681	-4.08098	-0.22889	0.00000	-0.00036	0.00000
457	-0.26794	0.74326	1.07797	0.00000	-0.12207	0.00000
460	-0.90049	1.66291	1.07884	0.00000	0.00308	0.00000
493	-0.18944	-0.50399	-0.16886	0.00000	-0.02603	0.00000
536	-0.09486	0.53293	0.65892	0.00000	0.00951	0.00000
553	0.31851	0.37386	0.50524	0.00000	0.02062	0.00000
566	-0.01317	0.02970	0.00000	0.00495	0.00000	0.00000
567	0.74285	0.02970	0.00000	0.00495	0.00000	0.00000
568	-0.00734	-0.82426	-0.07734	0.00000	-0.01359	0.00000
569	-0.10911	0.50285	0.29948	0.00000	0.00827	0.00000

SUM	-1.81698	1.84068	6.58518	1.75108	-0.11797	1.80815
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Condition **LC25=1.2D+Di+W10**

45	0.02029	-0.10632	0.00136	0.00000	0.00005	0.00000
50	0.00357	0.24047	0.08645	0.00000	0.00000	0.00000
52	0.00529	0.00000	-0.09189	0.00000	0.00000	0.00000
53	-0.00241	0.00000	0.03686	0.00000	0.00000	0.00000
54	0.00642	0.00000	0.01870	0.00000	0.00000	0.00000
134	-0.00576	0.04808	-0.01594	0.00000	0.00000	0.00000
177	0.00225	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.00161	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.04523	0.53567	0.06999	-1.89807	0.00000	0.64261
328	0.04993	1.07634	0.21801	-5.44265	0.00000	0.56698
429	-0.02197	0.47733	-0.05740	0.00000	0.00000	0.00000
437	-0.07128	0.31454	0.00877	0.00000	0.00003	0.00000
457	0.10934	0.40206	0.06434	0.00000	0.02091	0.00000
460	-0.04970	0.32747	0.06117	0.00000	0.00388	0.00000
493	0.00783	0.17476	0.00752	0.00000	0.00273	0.00000
536	-0.00678	0.21753	-0.00311	0.00000	0.00168	0.00000
553	0.01738	0.19437	0.00785	0.00000	-0.00125	0.00000
566	-0.01875	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.01341	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00053	0.08236	0.01426	0.00000	0.00317	0.00000
569	-0.01273	0.08246	-0.00393	0.00000	0.00197	0.00000

SUM	0.00000	4.29090	0.42300	-7.37727	0.03318	1.20959
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Condition **LC26=1.2D+Di+W130**

45	0.02528	-0.14995	0.00198	0.00000	0.00007	0.00000
50	0.00341	0.24199	0.08315	0.00000	0.00000	0.00000
52	0.00630	0.00000	-0.08857	0.00000	0.00000	0.00000
53	-0.00236	0.00000	0.03754	0.00000	0.00000	0.00000
54	0.01278	0.00000	0.01400	0.00000	0.00000	0.00000
134	-0.00648	0.04712	-0.01794	0.00000	0.00000	0.00000
177	0.00305	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.00900	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.21742	0.57596	0.13760	-2.21074	0.00000	0.55722
328	0.04899	1.03606	0.04060	-5.43004	0.00000	0.49250
429	-0.04614	0.46435	-0.06949	0.00000	0.00000	0.00000
437	-0.08106	0.39577	0.01801	0.00000	0.00004	0.00000
457	0.14917	0.41086	0.04890	0.00000	0.02221	0.00000
460	0.00894	0.29090	0.04971	0.00000	0.00358	0.00000
493	0.01005	0.18176	0.01006	0.00000	0.00226	0.00000
536	-0.00730	0.21155	-0.00653	0.00000	0.00202	0.00000
553	0.00763	0.19493	0.00216	0.00000	0.00039	0.00000
566	-0.02535	0.07160	0.00000	0.01193	0.00000	0.00000
567	-0.07492	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00068	0.08716	0.01499	0.00000	0.00314	0.00000
569	-0.01018	0.07868	-0.00464	0.00000	0.00206	0.00000

 SUM 0.24890 4.29090 0.27153 -7.67733 0.03575 1.04972

Condition **LC27=1.2D+Di+W160**

45	0.02677	-0.15972	0.00182	0.00000	0.00006	0.00000
50	0.00342	0.24187	0.08266	0.00000	0.00000	0.00000
52	0.00647	0.00000	-0.08804	0.00000	0.00000	0.00000
53	-0.00238	0.00000	0.03758	0.00000	0.00000	0.00000
54	0.01361	0.00000	0.01663	0.00000	0.00000	0.00000
134	-0.00674	0.04677	-0.01867	0.00000	0.00000	0.00000
177	0.00226	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.00670	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.16224	0.56390	0.10194	-2.24143	0.00000	0.57599
328	0.03633	1.04811	0.03100	-5.52362	0.00000	0.50487
429	-0.04863	0.46282	-0.07079	0.00000	0.00000	0.00000
437	-0.08464	0.41692	0.01897	0.00000	0.00004	0.00000
457	0.14647	0.40417	0.04505	0.00000	0.02339	0.00000
460	0.01039	0.28773	0.04763	0.00000	0.00364	0.00000
493	0.01040	0.18410	0.01083	0.00000	0.00213	0.00000
536	-0.00430	0.21040	-0.00798	0.00000	0.00176	0.00000
553	0.00548	0.19205	0.00000	0.00000	0.00079	0.00000
566	-0.01881	0.07160	0.00000	0.01193	0.00000	0.00000
567	-0.05579	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00070	0.08923	0.01534	0.00000	0.00313	0.00000
569	-0.00773	0.07880	-0.00479	0.00000	0.00188	0.00000

 SUM 0.20223 4.29090 0.21920 -7.80159 0.03681 1.08086

Condition **LC28=1.2D+Di+W190**

45	0.03392	-0.20727	0.00120	0.00000	0.00003	0.00000
50	0.00308	0.24385	0.08065	0.00000	0.00000	0.00000
52	0.00653	0.00000	-0.08703	0.00000	0.00000	0.00000
53	-0.00209	0.00000	0.02826	0.00000	0.00000	0.00000
54	0.01756	0.00000	-0.00106	0.00000	0.00000	0.00000
134	-0.00766	0.04554	-0.02121	0.00000	0.00000	0.00000
177	0.00150	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.00885	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.21692	0.56681	0.08552	-2.44782	0.00000	0.55894

328	0.01686	1.04520	-0.08552	-5.66425	0.00000	0.48577
429	-0.06065	0.45745	-0.07754	0.00000	0.00000	0.00000
437	-0.10062	0.50990	0.02368	0.00000	0.00005	0.00000
457	0.16129	0.39426	0.02215	0.00000	0.02577	0.00000
460	0.04030	0.25370	0.02250	0.00000	0.00340	0.00000
493	0.01274	0.19236	0.01562	0.00000	0.00278	0.00000
536	0.00933	0.20886	-0.01225	0.00000	0.00037	0.00000
553	0.00209	0.17962	-0.00626	0.00000	0.00058	0.00000
566	-0.01250	0.07160	0.00000	0.01193	0.00000	0.00000
567	-0.07363	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00076	0.09560	0.01642	0.00000	0.00313	0.00000
569	0.00140	0.08125	-0.00512	0.00000	0.00105	0.00000
SUM	0.27600	4.29090	0.00000	-8.14861	0.03716	1.04471

Condition **LC29=1.2D+Di+W1120**

45	0.04136	-0.24022	-0.00082	0.00000	-0.00005	0.00000
50	0.00299	0.24436	0.08252	0.00000	0.00000	0.00000
52	0.00501	0.00000	-0.09032	0.00000	0.00000	0.00000
53	-0.00182	0.00000	0.00906	0.00000	0.00000	0.00000
54	0.01421	0.00000	-0.01347	0.00000	0.00000	0.00000
134	-0.00856	0.04433	-0.02371	0.00000	0.00000	0.00000
177	0.00024	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.00820	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.20334	0.55864	0.04116	-2.61513	0.00000	0.55696
328	-0.00865	1.05337	-0.17410	-5.84299	0.00000	0.48484
429	-0.04902	0.46327	-0.07339	0.00000	0.00000	0.00000
437	-0.12098	0.58094	0.01821	0.00000	0.00005	0.00000
457	0.14963	0.37471	-0.00060	0.00000	0.02808	0.00000
460	0.03063	0.22732	-0.00033	0.00000	0.00326	0.00000
493	0.01414	0.20081	0.02159	0.00000	0.00430	0.00000
536	0.00436	0.20045	-0.01530	0.00000	0.00123	0.00000
553	-0.01630	0.18190	-0.01269	0.00000	0.00155	0.00000
566	-0.00196	0.07160	0.00000	0.01193	0.00000	0.00000
567	-0.06823	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00067	0.10166	0.01767	0.00000	0.00316	0.00000
569	0.00296	0.07558	-0.00467	0.00000	0.00116	0.00000
SUM	0.20223	4.29090	-0.21920	-8.49467	0.04274	1.04180

Condition **LC30=1.2D+Di+W1150**

45	0.04335	-0.24943	-0.00129	0.00000	-0.00007	0.00000
50	0.00306	0.24398	0.08300	0.00000	0.00000	0.00000
52	0.00469	0.00000	-0.09092	0.00000	0.00000	0.00000
53	-0.00185	0.00000	0.01106	0.00000	0.00000	0.00000
54	0.01321	0.00000	-0.01218	0.00000	0.00000	0.00000
134	-0.00884	0.04395	-0.02450	0.00000	0.00000	0.00000
177	0.00029	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.01099	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.27287	0.56980	0.05155	-2.73276	0.00000	0.52981
328	-0.01204	1.04221	-0.22974	-5.86079	0.00000	0.46277
429	-0.04649	0.46406	-0.07243	0.00000	0.00000	0.00000
437	-0.12648	0.59954	0.01701	0.00000	0.00006	0.00000
457	0.15309	0.37458	-0.00591	0.00000	0.02845	0.00000
460	0.03422	0.21727	-0.00239	0.00000	0.00320	0.00000
493	0.01448	0.20345	0.02307	0.00000	0.00446	0.00000
536	0.00441	0.19826	-0.01648	0.00000	0.00131	0.00000
553	-0.02099	0.18132	-0.01482	0.00000	0.00202	0.00000
566	-0.00245	0.07160	0.00000	0.01193	0.00000	0.00000

567	-0.09148	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00066	0.10370	0.01807	0.00000	0.00317	0.00000
569	0.00418	0.07443	-0.00463	0.00000	0.00112	0.00000

SUM	0.24890	4.29090	-0.27153	-8.63010	0.04371	0.99257
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Condition **LC31=1.2D+Di-WI0**

45	0.04800	-0.25963	-0.00342	0.00000	-0.00016	0.00000
50	0.00309	0.24282	0.08622	0.00000	0.00000	0.00000
52	0.00285	0.00000	-0.09533	0.00000	0.00000	0.00000
53	-0.00178	0.00000	0.00679	0.00000	0.00000	0.00000
54	0.00685	0.00000	-0.01638	0.00000	0.00000	0.00000
134	-0.00949	0.04309	-0.02629	0.00000	0.00000	0.00000
177	-0.00224	0.04028	0.00000	-0.03021	0.00000	0.00000
178	0.00161	0.04028	0.00000	-0.03021	0.00000	0.00000
327	0.04512	0.52382	-0.07011	-2.73622	0.00000	0.59760
328	-0.04977	1.08820	-0.21789	-6.14244	0.00000	0.52126
429	-0.02236	0.47560	-0.06170	0.00000	0.00000	0.00000
437	-0.14193	0.63089	0.00708	0.00000	0.00006	0.00000
457	0.11558	0.34594	-0.01970	0.00000	0.03072	0.00000
460	-0.01009	0.21401	-0.01692	0.00000	0.00335	0.00000
493	0.01465	0.20895	0.02764	0.00000	0.00592	0.00000
536	0.01191	0.19640	-0.01899	0.00000	0.00057	0.00000
553	-0.02798	0.17267	-0.01919	0.00000	0.00166	0.00000
566	0.01867	0.07160	0.00000	0.01193	0.00000	0.00000
567	-0.01339	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00052	0.10866	0.01915	0.00000	0.00321	0.00000
569	0.01016	0.07573	-0.00395	0.00000	0.00047	0.00000

SUM	0.00000	4.29090	-0.42300	-8.91521	0.04581	1.11886
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Condition **LC32=1.2D+Di-WI30**

45	0.04280	-0.21589	-0.00381	0.00000	-0.00017	0.00000
50	0.00319	0.24132	0.08944	0.00000	0.00000	0.00000
52	0.00174	0.00000	-0.09872	0.00000	0.00000	0.00000
53	-0.00182	0.00000	0.01167	0.00000	0.00000	0.00000
54	0.00048	0.00000	-0.01489	0.00000	0.00000	0.00000
134	-0.00877	0.04405	-0.02430	0.00000	0.00000	0.00000
177	-0.00304	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.00899	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.21740	0.48399	-0.13761	-2.42531	0.00000	0.68335
328	-0.04891	1.12802	-0.04058	-6.15596	0.00000	0.59539
429	0.00191	0.48847	-0.04949	0.00000	0.00000	0.00000
437	-0.13208	0.54961	-0.00219	0.00000	0.00006	0.00000
457	0.07589	0.33714	-0.00460	0.00000	0.02926	0.00000
460	-0.06857	0.25059	-0.00806	0.00000	0.00366	0.00000
493	0.01257	0.20194	0.02540	0.00000	0.00653	0.00000
536	0.01236	0.20239	-0.01551	0.00000	0.00024	0.00000
553	-0.01833	0.17212	-0.01351	0.00000	-0.00009	0.00000
566	0.02531	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.07485	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00036	0.10386	0.01843	0.00000	0.00325	0.00000
569	0.00757	0.07950	-0.00320	0.00000	0.00038	0.00000

SUM	-0.24890	4.29090	-0.27153	-8.61782	0.04312	1.27875
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Condition **LC33=1.2D+Di-WI60**

45	0.04136	-0.20612	-0.00372	0.00000	-0.00017	0.00000
50	0.00320	0.24140	0.08994	0.00000	0.00000	0.00000
52	0.00160	0.00000	-0.09922	0.00000	0.00000	0.00000
53	-0.00181	0.00000	0.00949	0.00000	0.00000	0.00000
54	-0.00035	0.00000	-0.01622	0.00000	0.00000	0.00000
134	-0.00851	0.04440	-0.02356	0.00000	0.00000	0.00000
177	-0.00226	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.00670	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.16223	0.49591	-0.10195	-2.39463	0.00000	0.66462
328	-0.03628	1.11610	-0.03099	-6.06351	0.00000	0.58330
429	0.00435	0.49006	-0.04821	0.00000	0.00000	0.00000
437	-0.12853	0.52846	-0.00316	0.00000	0.00005	0.00000
457	0.07853	0.34384	-0.00063	0.00000	0.02813	0.00000
460	-0.07002	0.25377	-0.00508	0.00000	0.00360	0.00000
493	0.01217	0.19961	0.02452	0.00000	0.00661	0.00000
536	0.00937	0.20353	-0.01408	0.00000	0.00050	0.00000
553	-0.01614	0.17500	-0.01135	0.00000	-0.00045	0.00000
566	0.01879	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.05575	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00033	0.10179	0.01807	0.00000	0.00325	0.00000
569	0.00512	0.07938	-0.00307	0.00000	0.00057	0.00000
SUM	-0.20223	4.29090	-0.21920	-8.49469	0.04210	1.24792

Condition **LC34=1.2D+Di-WI90**

45	0.03417	-0.15900	-0.00297	0.00000	-0.00013	0.00000
50	0.00348	0.23956	0.09193	0.00000	0.00000	0.00000
52	0.00145	0.00000	-0.10033	0.00000	0.00000	0.00000
53	-0.00210	0.00000	0.02518	0.00000	0.00000	0.00000
54	-0.00427	0.00000	-0.00255	0.00000	0.00000	0.00000
134	-0.00759	0.04563	-0.02103	0.00000	0.00000	0.00000
177	-0.00150	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.00884	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.21690	0.49292	-0.08551	-2.18846	0.00000	0.68178
328	-0.01684	1.11909	0.08551	-5.92397	0.00000	0.60256
429	0.01666	0.49561	-0.04135	0.00000	0.00000	0.00000
437	-0.11246	0.43557	-0.00780	0.00000	0.00005	0.00000
457	0.06379	0.35374	0.02191	0.00000	0.02561	0.00000
460	-0.10011	0.28780	0.01750	0.00000	0.00384	0.00000
493	0.00995	0.19134	0.02003	0.00000	0.00609	0.00000
536	-0.00433	0.20508	-0.00977	0.00000	0.00189	0.00000
553	-0.01288	0.18743	-0.00508	0.00000	-0.00035	0.00000
566	0.01250	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.07359	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00027	0.09542	0.01700	0.00000	0.00326	0.00000
569	-0.00404	0.07693	-0.00269	0.00000	0.00139	0.00000
SUM	-0.27600	4.29090	0.00000	-8.14897	0.04165	1.28434

Condition **LC35=1.2D+Di-WI120**

45	0.02696	-0.12571	-0.00125	0.00000	-0.00006	0.00000
50	0.00366	0.23904	0.09020	0.00000	0.00000	0.00000
52	0.00311	0.00000	-0.09694	0.00000	0.00000	0.00000
53	-0.00237	0.00000	0.03611	0.00000	0.00000	0.00000
54	-0.00094	0.00000	0.01474	0.00000	0.00000	0.00000
134	-0.00669	0.04684	-0.01852	0.00000	0.00000	0.00000
177	-0.00023	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.00820	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.20337	0.50089	-0.04119	-2.02048	0.00000	0.68363

328	0.00870	1.11112	0.17413	-5.74501	0.00000	0.60364
429	0.00474	0.48952	-0.04575	0.00000	0.00000	0.00000
437	-0.09219	0.36448	-0.00233	0.00000	0.00004	0.00000
457	0.07533	0.37329	0.04516	0.00000	0.02353	0.00000
460	-0.09053	0.31417	0.04412	0.00000	0.00397	0.00000
493	0.00837	0.18289	0.01363	0.00000	0.00438	0.00000
536	0.00075	0.21349	-0.00679	0.00000	0.00103	0.00000
553	0.00569	0.18515	0.00134	0.00000	-0.00117	0.00000
566	0.00195	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.06821	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00037	0.08937	0.01574	0.00000	0.00322	0.00000
569	-0.00554	0.08260	-0.00321	0.00000	0.00129	0.00000
SUM	-0.20223	4.29090	0.21920	-7.80204	0.03624	1.28726

Condition **LC36=1.2D+Di-WI150**

45	0.02491	-0.11651	-0.00070	0.00000	-0.00003	0.00000
50	0.00357	0.23945	0.08969	0.00000	0.00000	0.00000
52	0.00339	0.00000	-0.09637	0.00000	0.00000	0.00000
53	-0.00234	0.00000	0.03632	0.00000	0.00000	0.00000
54	0.00008	0.00000	0.01214	0.00000	0.00000	0.00000
134	-0.00641	0.04721	-0.01774	0.00000	0.00000	0.00000
177	-0.00029	0.04028	0.00000	-0.03021	0.00000	0.00000
178	-0.01099	0.04028	0.00000	-0.03021	0.00000	0.00000
327	-0.27292	0.48966	-0.05159	-1.90248	0.00000	0.71072
328	0.01212	1.12236	0.22978	-5.72671	0.00000	0.62568
429	0.00225	0.48869	-0.04667	0.00000	0.00000	0.00000
437	-0.08667	0.34591	-0.00113	0.00000	0.00004	0.00000
457	0.07192	0.37341	0.05034	0.00000	0.02311	0.00000
460	-0.09409	0.32422	0.04519	0.00000	0.00404	0.00000
493	0.00808	0.18026	0.01227	0.00000	0.00427	0.00000
536	0.00068	0.21566	-0.00560	0.00000	0.00094	0.00000
553	0.01032	0.18573	0.00347	0.00000	-0.00168	0.00000
566	0.00242	0.07160	0.00000	0.01193	0.00000	0.00000
567	0.09146	0.07160	0.00000	0.01193	0.00000	0.00000
568	0.00038	0.08732	0.01535	0.00000	0.00322	0.00000
569	-0.00677	0.08375	-0.00324	0.00000	0.00133	0.00000
SUM	-0.24890	4.29090	0.27153	-7.66575	0.03523	1.33640

Condition **LC37=0.9D**

45	0.00893	-0.04023	0.00003	0.00000	0.00000	0.00000
50	0.00080	0.09860	0.03403	0.00000	0.00000	0.00000
52	0.00118	0.00000	-0.03318	0.00000	0.00000	0.00000
53	-0.00080	0.00000	0.01226	0.00000	0.00000	0.00000
54	0.00333	0.00000	-0.00328	0.00000	0.00000	0.00000
134	-0.00235	0.01557	-0.00649	0.00000	0.00000	0.00000
177	0.00000	0.01671	0.00000	-0.01253	0.00000	0.00000
178	0.00000	0.01671	0.00000	-0.01253	0.00000	0.00000
327	0.00000	0.19653	0.00000	-0.88626	0.00000	0.25754
328	0.00000	0.42713	0.00000	-2.25456	0.00000	0.19392
429	-0.01111	0.19954	-0.02419	0.00000	0.00000	0.00000
437	-0.03554	0.18736	0.00373	0.00000	0.00002	0.00000
457	0.06010	0.19654	0.00633	0.00000	0.00826	0.00000
460	-0.02726	0.15942	0.00564	0.00000	0.00149	0.00000
493	0.00409	0.08254	0.00611	0.00000	0.00169	0.00000
536	-0.00004	0.07985	-0.00318	0.00000	0.00042	0.00000
553	0.00024	0.08282	-0.00167	0.00000	-0.00052	0.00000
566	0.00000	0.02970	0.00000	0.00495	0.00000	0.00000

567	0.00000	0.02970	0.00000	0.00495	0.00000	0.00000
568	0.00015	0.02894	0.00508	0.00000	0.00105	0.00000
569	-0.00173	0.03325	-0.00121	0.00000	0.00050	0.00000

SUM	0.00000	1.84068	0.00000	-3.15598	0.01290	0.45146
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Condition **LC38=1.2D**

45	0.01193	-0.05375	0.00004	0.00000	0.00000	0.00000
50	0.00107	0.13146	0.04537	0.00000	0.00000	0.00000
52	0.00157	0.00000	-0.04424	0.00000	0.00000	0.00000
53	-0.00107	0.00000	0.01635	0.00000	0.00000	0.00000
54	0.00444	0.00000	-0.00437	0.00000	0.00000	0.00000
134	-0.00313	0.02075	-0.00866	0.00000	0.00000	0.00000
177	0.00000	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00000	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.00000	0.26188	0.00000	-1.18289	0.00000	0.34344
328	0.00000	0.56966	0.00000	-3.00902	0.00000	0.25884
429	-0.01481	0.26605	-0.03226	0.00000	0.00000	0.00000
437	-0.04743	0.24998	0.00497	0.00000	0.00002	0.00000
457	0.08014	0.26201	0.00843	0.00000	0.01103	0.00000
460	-0.03633	0.21255	0.00753	0.00000	0.00198	0.00000
493	0.00546	0.11007	0.00816	0.00000	0.00225	0.00000
536	-0.00004	0.10645	-0.00424	0.00000	0.00056	0.00000
553	0.00031	0.11042	-0.00223	0.00000	-0.00069	0.00000
566	0.00000	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.00000	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00020	0.03860	0.00677	0.00000	0.00139	0.00000
569	-0.00230	0.04433	-0.00162	0.00000	0.00067	0.00000

SUM	0.00000	2.45425	0.00000	-4.21213	0.01721	0.60228
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Condition **LC41=1.2D+WLO**

45	0.00763	-0.02987	0.00080	0.00000	0.00003	0.00000
50	0.00113	0.13122	0.04543	0.00000	0.00000	0.00000
52	0.00194	0.00000	-0.04376	0.00000	0.00000	0.00000
53	-0.00116	0.00000	0.02015	0.00000	0.00000	0.00000
54	0.00440	0.00000	0.00049	0.00000	0.00000	0.00000
134	-0.00253	0.02155	-0.00701	0.00000	0.00000	0.00000
177	0.00068	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00050	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.01382	0.26363	0.02186	-1.05320	0.00000	0.35004
328	0.01513	0.56792	0.06814	-2.89851	0.00000	0.26556
429	-0.01480	0.26603	-0.03165	0.00000	0.00000	0.00000
437	-0.03656	0.20128	0.00519	0.00000	0.00002	0.00000
457	0.07925	0.27048	0.02110	0.00000	0.00948	0.00000
460	-0.04242	0.23000	0.01917	0.00000	0.00206	0.00000
493	0.00440	0.10461	0.00502	0.00000	0.00179	0.00000
536	-0.00312	0.10992	-0.00158	0.00000	0.00074	0.00000
553	0.00772	0.11399	0.00227	0.00000	-0.00123	0.00000
566	-0.00567	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.00418	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00020	0.03432	0.00597	0.00000	0.00139	0.00000
569	-0.00608	0.04541	-0.00160	0.00000	0.00091	0.00000

SUM	0.00000	2.45425	0.13000	-3.97193	0.01519	0.61560
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Condition **LC42=1.2D+WL30**

45	0.00945	-0.04421	0.00085	0.00000	0.00003	0.00000
50	0.00109	0.13155	0.04443	0.00000	0.00000	0.00000
52	0.00222	0.00000	-0.04276	0.00000	0.00000	0.00000
53	-0.00115	0.00000	0.02005	0.00000	0.00000	0.00000
54	0.00624	0.00000	-0.00030	0.00000	0.00000	0.00000
134	-0.00284	0.02115	-0.00784	0.00000	0.00000	0.00000
177	0.00095	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00279	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.06724	0.27638	0.04254	-1.14986	0.00000	0.32380
328	0.01524	0.55516	0.01261	-2.89470	0.00000	0.24245
429	-0.02164	0.26252	-0.03506	0.00000	0.00000	0.00000
437	-0.04033	0.22883	0.00781	0.00000	0.00002	0.00000
457	0.09013	0.27240	0.01609	0.00000	0.01006	0.00000
460	-0.02548	0.21769	0.01506	0.00000	0.00196	0.00000
493	0.00514	0.10744	0.00610	0.00000	0.00165	0.00000
536	-0.00243	0.10757	-0.00315	0.00000	0.00078	0.00000
553	0.00361	0.11323	-0.00031	0.00000	-0.00058	0.00000
566	-0.00788	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.02319	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00025	0.03655	0.00634	0.00000	0.00138	0.00000
569	-0.00447	0.04422	-0.00183	0.00000	0.00088	0.00000
SUM	0.07495	2.45425	0.08061	-4.06477	0.01618	0.56624

Condition **LC43=1.2D+WL60**

45	0.00971	-0.04668	0.00094	0.00000	0.00003	0.00000
50	0.00111	0.13160	0.04446	0.00000	0.00000	0.00000
52	0.00223	0.00000	-0.04276	0.00000	0.00000	0.00000
53	-0.00115	0.00000	0.02012	0.00000	0.00000	0.00000
54	0.00628	0.00000	0.00058	0.00000	0.00000	0.00000
134	-0.00285	0.02113	-0.00789	0.00000	0.00000	0.00000
177	0.00070	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00207	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.05008	0.27273	0.03156	-1.15919	0.00000	0.32967
328	0.01117	0.55882	0.00946	-2.92338	0.00000	0.24652
429	-0.02245	0.26174	-0.03559	0.00000	0.00000	0.00000
437	-0.04101	0.23345	0.00801	0.00000	0.00002	0.00000
457	0.09016	0.27086	0.01516	0.00000	0.01029	0.00000
460	-0.02450	0.21765	0.01526	0.00000	0.00200	0.00000
493	0.00520	0.10761	0.00616	0.00000	0.00162	0.00000
536	-0.00239	0.10757	-0.00316	0.00000	0.00077	0.00000
553	0.00367	0.11325	-0.00031	0.00000	-0.00057	0.00000
566	-0.00579	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.01722	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00025	0.03656	0.00634	0.00000	0.00138	0.00000
569	-0.00446	0.04421	-0.00185	0.00000	0.00088	0.00000
SUM	0.06081	2.45425	0.06647	-4.10279	0.01642	0.57619

Condition **LC44=1.2D+WL90**

45	0.01184	-0.06122	0.00071	0.00000	0.00002	0.00000
50	0.00100	0.13214	0.04367	0.00000	0.00000	0.00000
52	0.00235	0.00000	-0.04223	0.00000	0.00000	0.00000
53	-0.00107	0.00000	0.01690	0.00000	0.00000	0.00000
54	0.00777	0.00000	-0.00425	0.00000	0.00000	0.00000
134	-0.00314	0.02074	-0.00868	0.00000	0.00000	0.00000
177	0.00046	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00269	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.06583	0.27325	0.02579	-1.22228	0.00000	0.32461

328	0.00522	0.55830	-0.02579	-2.96956	0.00000	0.24129
429	-0.02669	0.26031	-0.03787	0.00000	0.00000	0.00000
437	-0.04547	0.26140	0.00981	0.00000	0.00002	0.00000
457	0.09339	0.26691	0.00872	0.00000	0.01116	0.00000
460	-0.01626	0.20861	0.00810	0.00000	0.00195	0.00000
493	0.00588	0.11019	0.00746	0.00000	0.00174	0.00000
536	0.00155	0.10683	-0.00460	0.00000	0.00039	0.00000
553	0.00223	0.10964	-0.00243	0.00000	-0.00050	0.00000
566	-0.00384	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.02236	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00028	0.03862	0.00668	0.00000	0.00137	0.00000
569	-0.00167	0.04477	-0.00199	0.00000	0.00064	0.00000
SUM	0.08000	2.45425	0.00000	-4.21206	0.01680	0.56589

Condition **LC45=1.2D+WL120**

45	0.01415	-0.07128	0.00008	0.00000	0.00000	0.00000
50	0.00100	0.13220	0.04441	0.00000	0.00000	0.00000
52	0.00183	0.00000	-0.04339	0.00000	0.00000	0.00000
53	-0.00101	0.00000	0.01127	0.00000	0.00000	0.00000
54	0.00644	0.00000	-0.00774	0.00000	0.00000	0.00000
134	-0.00343	0.02036	-0.00948	0.00000	0.00000	0.00000
177	0.00008	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00253	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.06263	0.27115	0.01232	-1.27627	0.00000	0.32382
328	-0.00252	0.56040	-0.05333	-3.02478	0.00000	0.24045
429	-0.02268	0.26247	-0.03642	0.00000	0.00000	0.00000
437	-0.05184	0.28245	0.00789	0.00000	0.00002	0.00000
457	0.09102	0.26229	0.00192	0.00000	0.01177	0.00000
460	-0.01841	0.19958	0.00155	0.00000	0.00189	0.00000
493	0.00632	0.11288	0.00938	0.00000	0.00221	0.00000
536	0.00048	0.10430	-0.00564	0.00000	0.00060	0.00000
553	-0.00340	0.10990	-0.00454	0.00000	-0.00021	0.00000
566	-0.00066	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.02104	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00025	0.04060	0.00709	0.00000	0.00139	0.00000
569	-0.00093	0.04319	-0.00184	0.00000	0.00065	0.00000
SUM	0.06081	2.45425	-0.06647	-4.32127	0.01831	0.56427

Condition **LC46=1.2D+WL150**

45	0.01451	-0.07196	-0.00012	0.00000	-0.00001	0.00000
50	0.00100	0.13212	0.04439	0.00000	0.00000	0.00000
52	0.00179	0.00000	-0.04342	0.00000	0.00000	0.00000
53	-0.00100	0.00000	0.01221	0.00000	0.00000	0.00000
54	0.00637	0.00000	-0.00748	0.00000	0.00000	0.00000
134	-0.00345	0.02033	-0.00953	0.00000	0.00000	0.00000
177	0.00008	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00340	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.08469	0.27424	0.01612	-1.30903	0.00000	0.31584
328	-0.00406	0.55730	-0.07127	-3.02992	0.00000	0.23431
429	-0.02153	0.26263	-0.03579	0.00000	0.00000	0.00000
437	-0.05287	0.28450	0.00756	0.00000	0.00002	0.00000
457	0.09139	0.26184	0.00038	0.00000	0.01178	0.00000
460	-0.01897	0.19836	0.00170	0.00000	0.00188	0.00000
493	0.00628	0.11309	0.00949	0.00000	0.00225	0.00000
536	0.00046	0.10431	-0.00562	0.00000	0.00060	0.00000
553	-0.00347	0.10992	-0.00452	0.00000	-0.00022	0.00000
566	-0.00063	0.03960	0.00000	0.00660	0.00000	0.00000

567	-0.02833	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00024	0.04062	0.00710	0.00000	0.00139	0.00000
569	-0.00095	0.04317	-0.00182	0.00000	0.00065	0.00000

SUM	0.07495	2.45425	-0.08061	-4.35917	0.01833	0.55015
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Condition **LC47=1.2D-WL0**

45	0.01625	-0.07744	-0.00076	0.00000	-0.00004	0.00000
50	0.00102	0.13173	0.04535	0.00000	0.00000	0.00000
52	0.00123	0.00000	-0.04471	0.00000	0.00000	0.00000
53	-0.00099	0.00000	0.01119	0.00000	0.00000	0.00000
54	0.00448	0.00000	-0.00840	0.00000	0.00000	0.00000
134	-0.00373	0.01995	-0.01032	0.00000	0.00000	0.00000
177	-0.00068	0.02228	0.00000	-0.01671	0.00000	0.00000
178	0.00050	0.02228	0.00000	-0.01671	0.00000	0.00000
327	0.01381	0.26012	-0.02188	-1.31241	0.00000	0.33679
328	-0.01512	0.57143	-0.06812	-3.11918	0.00000	0.25209
429	-0.01491	0.26589	-0.03294	0.00000	0.00000	0.00000
437	-0.05832	0.29866	0.00474	0.00000	0.00002	0.00000
457	0.08104	0.25353	-0.00415	0.00000	0.01262	0.00000
460	-0.03023	0.19511	-0.00349	0.00000	0.00191	0.00000
493	0.00649	0.11553	0.01122	0.00000	0.00267	0.00000
536	0.00306	0.10299	-0.00691	0.00000	0.00038	0.00000
553	-0.00708	0.10685	-0.00673	0.00000	-0.00012	0.00000
566	0.00566	0.03960	0.00000	0.00660	0.00000	0.00000
567	-0.00418	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00021	0.04288	0.00757	0.00000	0.00140	0.00000
569	0.00148	0.04326	-0.00164	0.00000	0.00042	0.00000

SUM	0.00000	2.45425	-0.13000	-4.45181	0.01926	0.58888
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Condition **LC48=1.2D-WL30**

45	0.01438	-0.06313	-0.00076	0.00000	-0.00004	0.00000
50	0.00104	0.13138	0.04631	0.00000	0.00000	0.00000
52	0.00093	0.00000	-0.04571	0.00000	0.00000	0.00000
53	-0.00100	0.00000	0.01228	0.00000	0.00000	0.00000
54	0.00264	0.00000	-0.00816	0.00000	0.00000	0.00000
134	-0.00343	0.02036	-0.00948	0.00000	0.00000	0.00000
177	-0.00095	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00279	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.06724	0.24741	-0.04255	-1.21593	0.00000	0.36307
328	-0.01524	0.58414	-0.01261	-3.12308	0.00000	0.27517
429	-0.00804	0.26945	-0.02948	0.00000	0.00000	0.00000
437	-0.05454	0.27111	0.00211	0.00000	0.00002	0.00000
457	0.07017	0.25161	0.00080	0.00000	0.01200	0.00000
460	-0.04712	0.20742	0.00012	0.00000	0.00201	0.00000
493	0.00578	0.11269	0.01020	0.00000	0.00284	0.00000
536	0.00236	0.10534	-0.00533	0.00000	0.00034	0.00000
553	-0.00299	0.10761	-0.00416	0.00000	-0.00079	0.00000
566	0.00787	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.02318	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00016	0.04066	0.00720	0.00000	0.00141	0.00000
569	-0.00014	0.04444	-0.00141	0.00000	0.00046	0.00000

SUM	-0.07495	2.45425	-0.08061	-4.35922	0.01825	0.63824
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Condition **LC49=1.2D-WL60**

45	0.01414	-0.06059	-0.00087	0.00000	-0.00004	0.00000
50	0.00104	0.13135	0.04630	0.00000	0.00000	0.00000
52	0.00093	0.00000	-0.04571	0.00000	0.00000	0.00000
53	-0.00099	0.00000	0.01159	0.00000	0.00000	0.00000
54	0.00260	0.00000	-0.00868	0.00000	0.00000	0.00000
134	-0.00341	0.02038	-0.00944	0.00000	0.00000	0.00000
177	-0.00070	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00207	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.05008	0.25105	-0.03156	-1.20660	0.00000	0.35720
328	-0.01117	0.58049	-0.00945	-3.09451	0.00000	0.27113
429	-0.00727	0.27017	-0.02898	0.00000	0.00000	0.00000
437	-0.05387	0.26648	0.00191	0.00000	0.00002	0.00000
457	0.07014	0.25315	0.00176	0.00000	0.01179	0.00000
460	-0.04811	0.20745	0.00021	0.00000	0.00197	0.00000
493	0.00570	0.11252	0.01011	0.00000	0.00285	0.00000
536	0.00232	0.10533	-0.00532	0.00000	0.00035	0.00000
553	-0.00303	0.10760	-0.00416	0.00000	-0.00079	0.00000
566	0.00579	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.01721	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00016	0.04065	0.00721	0.00000	0.00141	0.00000
569	-0.00014	0.04446	-0.00139	0.00000	0.00046	0.00000
SUM	-0.06081	2.45425	-0.06647	-4.32132	0.01802	0.62832

Condition **LC50=1.2D-WL90**

45	0.01202	-0.04625	-0.00064	0.00000	-0.00003	0.00000
50	0.00113	0.13080	0.04708	0.00000	0.00000	0.00000
52	0.00080	0.00000	-0.04625	0.00000	0.00000	0.00000
53	-0.00107	0.00000	0.01556	0.00000	0.00000	0.00000
54	0.00111	0.00000	-0.00435	0.00000	0.00000	0.00000
134	-0.00313	0.02076	-0.00864	0.00000	0.00000	0.00000
177	-0.00046	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00269	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.06583	0.25053	-0.02579	-1.14352	0.00000	0.36227
328	-0.00522	0.58102	0.02579	-3.04843	0.00000	0.27637
429	-0.00295	0.27177	-0.02667	0.00000	0.00000	0.00000
437	-0.04940	0.23856	0.00013	0.00000	0.00002	0.00000
457	0.06690	0.25710	0.00817	0.00000	0.01090	0.00000
460	-0.05640	0.21649	0.00708	0.00000	0.00202	0.00000
493	0.00503	0.10994	0.00884	0.00000	0.00275	0.00000
536	-0.00163	0.10607	-0.00388	0.00000	0.00073	0.00000
553	-0.00161	0.11120	-0.00203	0.00000	-0.00087	0.00000
566	0.00384	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.02236	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00013	0.03859	0.00686	0.00000	0.00142	0.00000
569	-0.00293	0.04390	-0.00125	0.00000	0.00069	0.00000
SUM	-0.08000	2.45425	0.00000	-4.21217	0.01763	0.63865

Condition **LC51=1.2D-WL120**

45	0.00976	-0.03604	-0.00007	0.00000	-0.00001	0.00000
50	0.00115	0.13076	0.04638	0.00000	0.00000	0.00000
52	0.00135	0.00000	-0.04508	0.00000	0.00000	0.00000
53	-0.00114	0.00000	0.01945	0.00000	0.00000	0.00000
54	0.00244	0.00000	0.00016	0.00000	0.00000	0.00000
134	-0.00284	0.02115	-0.00784	0.00000	0.00000	0.00000
177	-0.00008	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00253	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.06263	0.25260	-0.01232	-1.08947	0.00000	0.36304

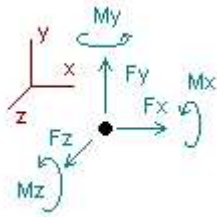
328	0.00252	0.57894	0.05333	-2.99320	0.00000	0.27723
429	-0.00705	0.26944	-0.02820	0.00000	0.00000	0.00000
437	-0.04304	0.21749	0.00206	0.00000	0.00002	0.00000
457	0.06926	0.26172	0.01507	0.00000	0.01035	0.00000
460	-0.05428	0.22553	0.01446	0.00000	0.00208	0.00000
493	0.00456	0.10725	0.00683	0.00000	0.00224	0.00000
536	-0.00054	0.10860	-0.00286	0.00000	0.00052	0.00000
553	0.00406	0.11095	0.00007	0.00000	-0.00114	0.00000
566	0.00066	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.02104	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00016	0.03661	0.00645	0.00000	0.00140	0.00000
569	-0.00367	0.04548	-0.00142	0.00000	0.00069	0.00000
SUM	-0.06081	2.45425	0.06647	-4.10288	0.01616	0.64027

Condition **LC52=1.2D-WL150**

45	0.00937	-0.03541	0.00015	0.00000	0.00000	0.00000
50	0.00115	0.13083	0.04638	0.00000	0.00000	0.00000
52	0.00138	0.00000	-0.04506	0.00000	0.00000	0.00000
53	-0.00115	0.00000	0.01927	0.00000	0.00000	0.00000
54	0.00252	0.00000	-0.00054	0.00000	0.00000	0.00000
134	-0.00282	0.02117	-0.00779	0.00000	0.00000	0.00000
177	-0.00008	0.02228	0.00000	-0.01671	0.00000	0.00000
178	-0.00340	0.02228	0.00000	-0.01671	0.00000	0.00000
327	-0.08469	0.24950	-0.01612	-1.05668	0.00000	0.37102
328	0.00406	0.58204	0.07128	-2.98801	0.00000	0.28336
429	-0.00816	0.26934	-0.02880	0.00000	0.00000	0.00000
437	-0.04200	0.21544	0.00238	0.00000	0.00002	0.00000
457	0.06889	0.26217	0.01657	0.00000	0.01031	0.00000
460	-0.05369	0.22674	0.01394	0.00000	0.00209	0.00000
493	0.00461	0.10704	0.00676	0.00000	0.00222	0.00000
536	-0.00052	0.10859	-0.00287	0.00000	0.00052	0.00000
553	0.00411	0.11093	0.00005	0.00000	-0.00113	0.00000
566	0.00063	0.03960	0.00000	0.00660	0.00000	0.00000
567	0.02833	0.03960	0.00000	0.00660	0.00000	0.00000
568	0.00017	0.03659	0.00645	0.00000	0.00140	0.00000
569	-0.00365	0.04549	-0.00143	0.00000	0.00069	0.00000
SUM	-0.07495	2.45425	0.08061	-4.06490	0.01612	0.65439

Envelope for nodal reactions

Note.- **Ic** is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

- LC1=1.2D+1.6Wo
- LC2=1.2D+1.6W30
- LC3=1.2D+1.6W60
- LC4=1.2D+1.6W90
- LC5=1.2D+1.6W120
- LC6=1.2D+1.6W150
- LC7=1.2D-1.6Wo
- LC8=1.2D-1.6W30
- LC9=1.2D-1.6W60
- LC10=1.2D-1.6W90
- LC11=1.2D-1.6W120
- LC12=1.2D-1.6W150
- LC13=0.9D+1.6Wo
- LC14=0.9D+1.6W30
- LC15=0.9D+1.6W60
- LC16=0.9D+1.6W90
- LC17=0.9D+1.6W120
- LC18=0.9D+1.6W150
- LC19=0.9D-1.6Wo
- LC20=0.9D-1.6W30
- LC21=0.9D-1.6W60
- LC22=0.9D-1.6W90
- LC23=0.9D-1.6W120
- LC24=0.9D-1.6W150
- LC25=1.2D+Di+Wl0
- LC26=1.2D+Di+Wl30
- LC27=1.2D+Di+Wl60
- LC28=1.2D+Di+Wl90
- LC29=1.2D+Di+Wl120
- LC30=1.2D+Di+Wl150
- LC31=1.2D+Di-Wl0
- LC32=1.2D+Di-Wl30
- LC33=1.2D+Di-Wl60
- LC34=1.2D+Di-Wl90
- LC35=1.2D+Di-Wl120
- LC36=1.2D+Di-Wl150
- LC37=0.9D
- LC38=1.2D
- LC41=1.2D+Wl0
- LC42=1.2D+Wl30
- LC43=1.2D+Wl60
- LC44=1.2D+Wl90
- LC45=1.2D+Wl120
- LC46=1.2D+Wl150
- LC47=1.2D-Wl0
- LC48=1.2D-Wl30
- LC49=1.2D-Wl60
- LC50=1.2D-Wl90
- LC51=1.2D-Wl120
- LC52=1.2D-Wl150

Node		Forces						Moments					
		Fx	lc	Fy	lc	Fz	lc	Mx	lc	My	lc	Mz	lc
		[Kip]		[Kip]		[Kip]		[Kip*ft]		[Kip*ft]		[Kip*ft]	
45	Max	0.425	LC7	2.121	LC13	0.077	LC3	0.00000	LC1	0.00311	LC3	0.00000	LC1
	Min	-0.382	LC13	-2.251	LC7	-0.093	LC7	0.00000	LC1	-0.00406	LC7	0.00000	LC1
50	Max	0.027	LC3	0.244	LC29	0.115	LC10	0.00000	LC1	0.00001	LC5	0.00000	LC1
	Min	-0.023	LC21	0.048	LC23	-0.032	LC16	0.00000	LC1	-0.00001	LC23	0.00000	LC1
52	Max	0.132	LC4	0.000	LC1	0.070	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.126	LC22	0.000	LC1	-0.167	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1

53	Max	0.059	LC17	0.000	LC1	0.071	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.061	LC11	0.000	LC1	-0.275	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.257	LC4	0.000	LC1	0.610	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.250	LC22	0.000	LC1	-0.450	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.150	LC13	0.217	LC1	0.466	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.144	LC7	-0.181	LC19	-0.489	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
177	Max	0.065	LC15	0.040	LC25	0.000	LC1	-0.01253	LC13	0.00000	LC1	0.00000	LC1
	Min	-0.065	LC9	0.017	LC13	0.000	LC1	-0.03021	LC25	0.00000	LC1	0.00000	LC1
178	Max	0.137	LC17	0.040	LC25	0.000	LC1	-0.01253	LC13	0.00000	LC1	0.00000	LC1
	Min	-0.137	LC11	0.017	LC13	0.000	LC1	-0.03021	LC25	0.00000	LC1	0.00000	LC1
327	Max	2.488	LC17	0.640	LC2	1.253	LC14	2.90095	LC24	0.00000	LC1	1.06264	LC12
	Min	-2.489	LC11	-0.171	LC22	-1.256	LC8	-4.87580	LC6	0.00000	LC1	-0.47679	LC18
328	Max	0.498	LC15	1.128	LC32	2.320	LC12	1.24274	LC14	0.00000	LC1	0.90158	LC12
	Min	-0.493	LC9	0.048	LC14	-2.314	LC18	-6.23568	LC8	0.00000	LC1	-0.45239	LC18
429	Max	1.027	LC22	0.751	LC10	0.503	LC22	0.00000	LC1	0.00002	LC21	0.00000	LC1
	Min	-1.058	LC4	-0.276	LC16	-0.558	LC4	0.00000	LC1	-0.00003	LC3	0.00000	LC1
437	Max	0.866	LC13	4.808	LC7	0.259	LC4	0.00000	LC1	0.00043	LC7	0.00000	LC1
	Min	-0.965	LC7	-4.326	LC13	-0.242	LC22	0.00000	LC1	-0.00039	LC13	0.00000	LC1
457	Max	1.330	LC5	1.059	LC2	1.189	LC1	0.00000	LC1	0.16596	LC7	0.00000	LC1
	Min	-1.205	LC23	-0.604	LC20	-1.158	LC19	0.00000	LC1	-0.13817	LC13	0.00000	LC1
460	Max	1.927	LC17	1.747	LC1	1.287	LC1	0.00000	LC1	0.00573	LC4	0.00000	LC1
	Min	-1.999	LC11	-1.383	LC19	-1.108	LC7	0.00000	LC1	-0.00335	LC22	0.00000	LC1
493	Max	0.367	LC5	0.743	LC7	0.207	LC7	0.00000	LC1	0.10761	LC9	0.00000	LC1
	Min	-0.365	LC23	-0.542	LC13	-0.202	LC13	0.00000	LC1	-0.10746	LC15	0.00000	LC1
536	Max	0.186	LC5	0.575	LC1	0.676	LC13	0.00000	LC1	0.01739	LC11	0.00000	LC1
	Min	-0.184	LC11	-0.385	LC19	-0.683	LC7	0.00000	LC1	-0.01653	LC17	0.00000	LC1
553	Max	0.372	LC1	0.464	LC2	0.535	LC1	0.00000	LC1	0.03346	LC14	0.00000	LC1
	Min	-0.392	LC7	-0.274	LC20	-0.541	LC7	0.00000	LC1	-0.02743	LC8	0.00000	LC1
566	Max	0.216	LC8	0.072	LC25	0.000	LC1	0.01193	LC25	0.00000	LC1	0.00000	LC1
	Min	-0.220	LC14	0.030	LC13	0.000	LC1	0.00495	LC13	0.00000	LC1	0.00000	LC1
567	Max	0.743	LC12	0.072	LC25	0.000	LC1	0.01193	LC25	0.00000	LC1	0.00000	LC1
	Min	-0.743	LC18	0.030	LC13	0.000	LC1	0.00495	LC13	0.00000	LC1	0.00000	LC1
568	Max	0.008	LC6	0.925	LC7	0.097	LC7	0.00000	LC1	0.01647	LC8	0.00000	LC1
	Min	-0.007	LC24	-0.855	LC13	-0.085	LC13	0.00000	LC1	-0.01415	LC14	0.00000	LC1
569	Max	0.170	LC7	0.517	LC12	0.299	LC24	0.00000	LC1	0.01336	LC2	0.00000	LC1
	Min	-0.151	LC1	-0.428	LC18	-0.307	LC6	0.00000	LC1	-0.01307	LC20	0.00000	LC1

Date: 2/16/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: KM Checked By: MSC



CHECK CONNECTION CAPACITY (Worst Case) → BETA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A325 1/2" U-Bolt

Allowable Tensile Load =

$F_{Tall} =$ 12061 lbs.

Allowable Shear Load =

$F_{vall} =$ 9048 lbs.

TENSILE FORCES

Reaction $F =$ 640 lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 2489 lbs. (See Bentley Output)

Reactions in Z direction: 1256 lbs. (See Bentley Output)

Resultant: 2788 lbs.

No. of Supports = 1

No. of Bolts / Support = 2

Tension Design Load /Bolts =

$f_t =$ 320.00 lbs. < 12061 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

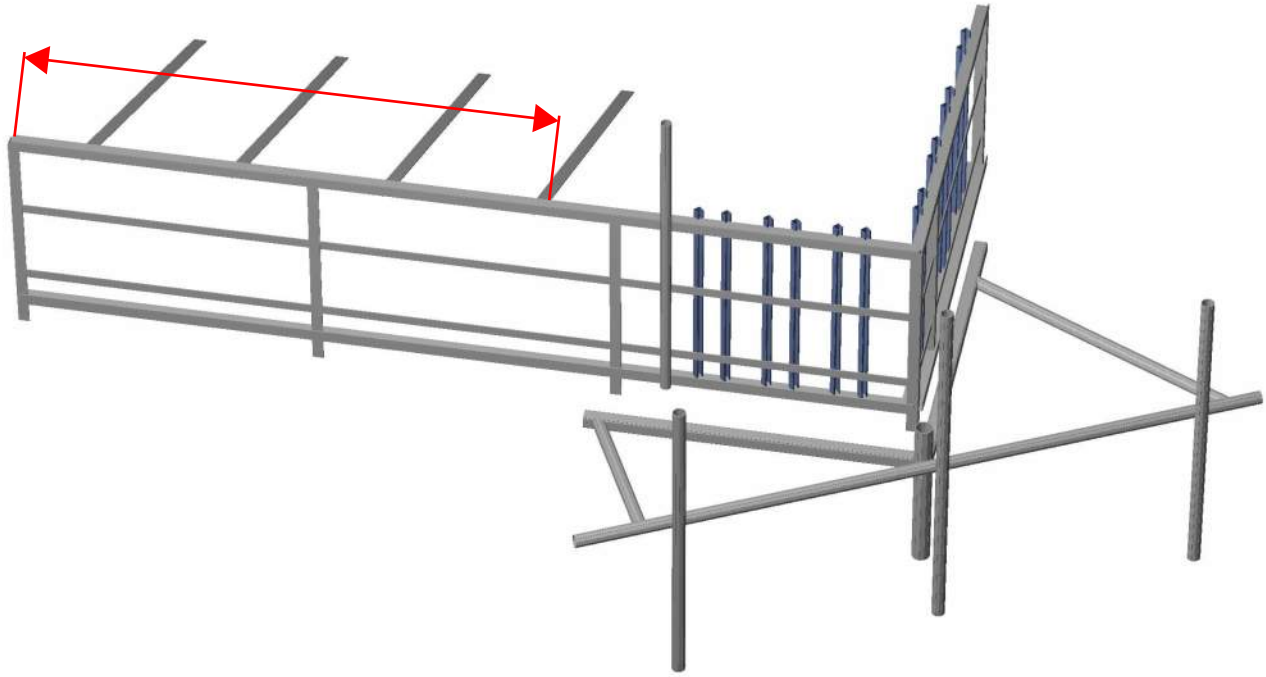
$f_v =$ 1393.97 lbs. < 9048 lbs. **Therefore, OK !**

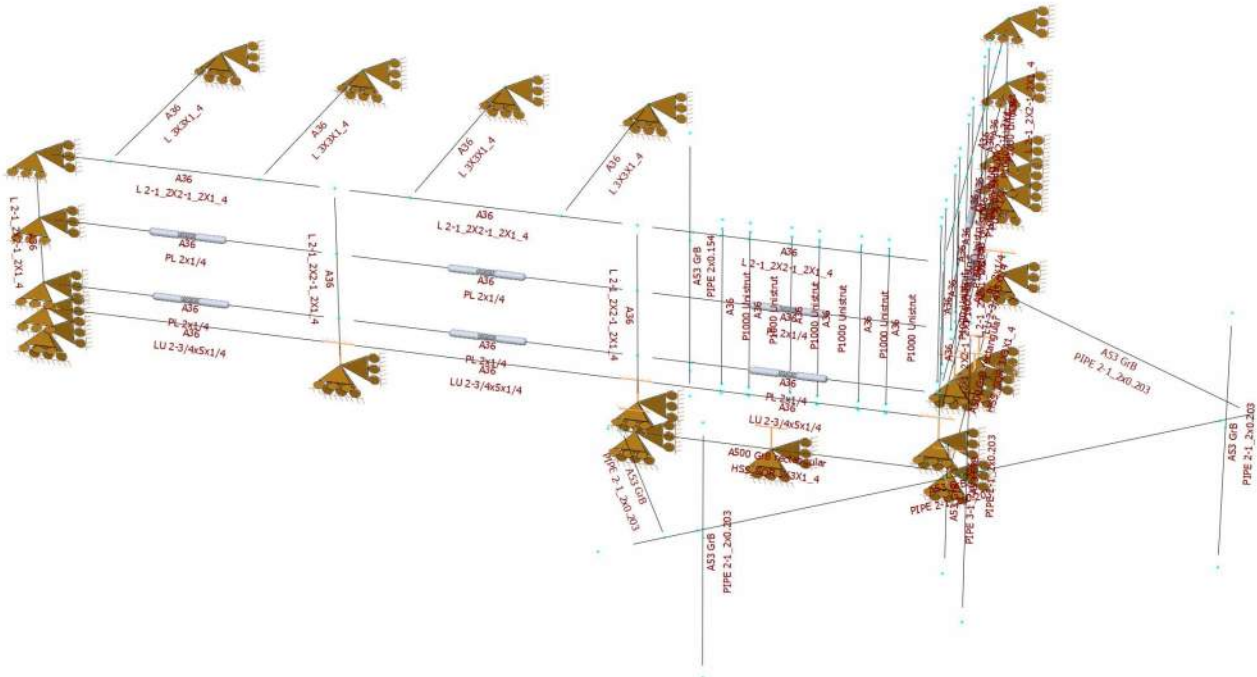
CHECK COMBINED TENSION AND SHEAR

$$\begin{array}{rclclcl}
 f_t / F_T & + & f_v / F_v & \leq & 1.0 & \\
 0.027 & + & 0.154 & = & 0.181 & < & 1.0 & \text{Therefore, OK !}
 \end{array}$$



Existing Gamma Sector Calculations

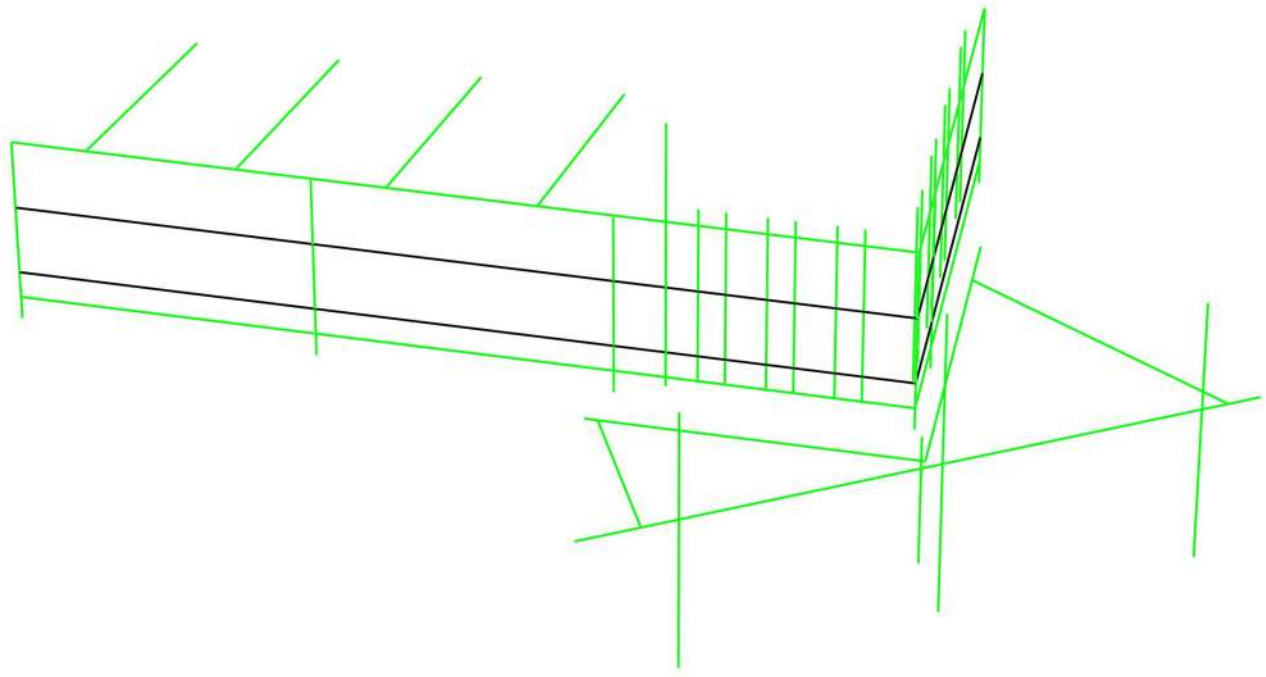


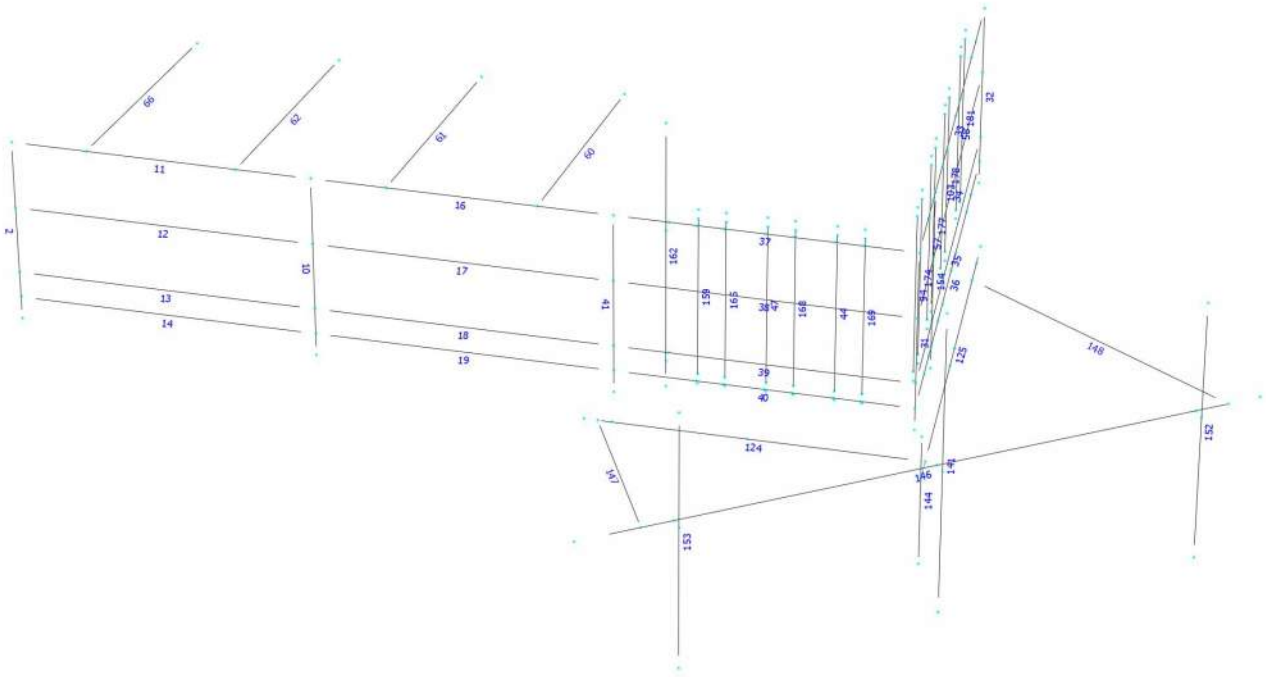




Design status

- Not designed
- Error on design
- Design O.K.
- With warnings





Load data

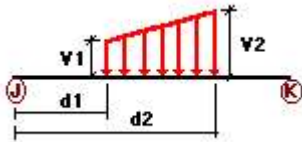
GLOSSARY

Comb : Indicates if load condition is a load combination

Load Conditions

Condition	Description	Comb.	Category																																																											
D	Dead Load	No	DL																																																											
Wo	Wind Load (NO ICE)	No	WIND																																																											
W30	WL 30deg	No	WIND																																																											
W60	WL 60deg	No	WIND																																																											
W90	WL 90deg	No </tr <tr> <td>W120</td> <td>WL 120deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>W150</td> <td>WL 150deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>Di</td> <td>Ice Load</td> <td>No</td> <td>LL</td> </tr> <tr> <td>WI0</td> <td>WL ICE 0deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WI30</td> <td>WL ICE 30deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WI60</td> <td>WL ICE 60deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WI90</td> <td>WL ICE 90deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WI120</td> <td>WL ICE 120deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WI150</td> <td>WL ICE 150deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL0</td> <td>WL 30 mph 0deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL30</td> <td>WL 30 mph 30deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL60</td> <td>WL 30 mph 60deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL90</td> <td>WL 30 mph 90deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL120</td> <td>WL 30 mph 120deg</td> <td>No</td> <td>WIND</td> </tr> <tr> <td>WL150</td> <td>WL 30 mph 150deg</td> <td>No</td> <td>WIND</td> </tr>	W120	WL 120deg	No	WIND	W150	WL 150deg	No	WIND	Di	Ice Load	No	LL	WI0	WL ICE 0deg	No	WIND	WI30	WL ICE 30deg	No	WIND	WI60	WL ICE 60deg	No	WIND	WI90	WL ICE 90deg	No	WIND	WI120	WL ICE 120deg	No	WIND	WI150	WL ICE 150deg	No	WIND	WL0	WL 30 mph 0deg	No	WIND	WL30	WL 30 mph 30deg	No	WIND	WL60	WL 30 mph 60deg	No	WIND	WL90	WL 30 mph 90deg	No	WIND	WL120	WL 30 mph 120deg	No	WIND	WL150	WL 30 mph 150deg	No	WIND
W120	WL 120deg	No	WIND																																																											
W150	WL 150deg	No	WIND																																																											
Di	Ice Load	No	LL																																																											
WI0	WL ICE 0deg	No	WIND																																																											
WI30	WL ICE 30deg	No	WIND																																																											
WI60	WL ICE 60deg	No	WIND																																																											
WI90	WL ICE 90deg	No	WIND																																																											
WI120	WL ICE 120deg	No	WIND																																																											
WI150	WL ICE 150deg	No	WIND																																																											
WL0	WL 30 mph 0deg	No	WIND																																																											
WL30	WL 30 mph 30deg	No	WIND																																																											
WL60	WL 30 mph 60deg	No	WIND																																																											
WL90	WL 30 mph 90deg	No	WIND																																																											
WL120	WL 30 mph 120deg	No	WIND																																																											
WL150	WL 30 mph 150deg	No	WIND																																																											

Distributed force on members



Condition	Member	Dir1	Val1 [Kip/ft]	Val2 [Kip/ft]	Dist1 [ft]	%	Dist2 [ft]	%
Wo	2	z	-0.017	0.00	0.00	No	0.00	No
	10	z	-0.017	0.00	0.00	No	0.00	No
	11	z	-0.017	0.00	0.00	No	0.00	No
	12	z	-0.013	0.00	0.00	No	0.00	No
	13	z	-0.013	0.00	0.00	No	0.00	No
	14	z	-0.018	0.00	0.00	No	0.00	No
	16	z	-0.017	0.00	0.00	No	0.00	No
	17	z	-0.013	0.00	0.00	No	0.00	No
	18	z	-0.013	0.00	0.00	No	0.00	No
	19	z	-0.018	0.00	0.00	No	0.00	No

	31	z	-0.017	0.00	0.00	No	0.00	No
	37	z	-0.017	0.00	0.00	No	0.00	No
	38	z	-0.013	0.00	0.00	No	0.00	No
	39	z	-0.013	0.00	0.00	No	0.00	No
	40	z	-0.018	0.00	0.00	No	0.00	No
	41	z	-0.017	0.00	0.00	No	0.00	No
	44	z	-0.007	0.00	0.00	No	0.00	No
	47	z	-0.007	0.00	0.00	No	0.00	No
	57	z	-0.007	0.00	0.00	No	0.00	No
	58	z	-0.007	0.00	0.00	No	0.00	No
	60	z	-0.02	0.00	0.00	No	0.00	No
	61	z	-0.02	0.00	0.00	No	0.00	No
	62	z	-0.02	0.00	0.00	No	0.00	No
	66	z	-0.02	0.00	0.00	No	0.00	No
	94	z	-0.007	0.00	0.00	No	0.00	No
	103	z	-0.007	0.00	0.00	No	0.00	No
	124	z	-0.013	0.00	0.00	No	0.00	No
	141	z	-0.012	0.00	0.00	No	0.00	No
	144	z	-0.016	0.00	0.00	No	0.00	No
	146	z	-0.012	0.00	0.00	No	0.00	No
	147	z	-0.012	0.00	0.00	No	0.00	No
	148	z	-0.012	0.00	0.00	No	0.00	No
	152	z	-0.012	0.00	0.00	No	0.00	No
	153	z	-0.012	0.00	0.00	No	0.00	No
	154	z	-0.017	0.00	0.00	No	0.00	No
	159	z	-0.007	0.00	0.00	No	0.00	No
	162	z	-0.01	0.00	0.00	No	0.00	No
	165	z	-0.007	0.00	0.00	No	0.00	No
	168	z	-0.007	0.00	0.00	No	0.00	No
	169	z	-0.007	0.00	0.00	No	0.00	No
	174	z	-0.007	0.00	0.00	No	0.00	No
	177	z	-0.007	0.00	0.00	No	0.00	No
	178	z	-0.007	0.00	0.00	No	0.00	No
	181	z	-0.007	0.00	0.00	No	0.00	No
W30	2	z	-0.017	0.00	0.00	No	0.00	No
	10	z	-0.017	0.00	0.00	No	0.00	No
	11	z	-0.017	0.00	0.00	No	0.00	No
	12	z	-0.013	0.00	0.00	No	0.00	No
	13	z	-0.013	0.00	0.00	No	0.00	No
	14	z	-0.018	0.00	0.00	No	0.00	No
	16	z	-0.017	0.00	0.00	No	0.00	No
	17	z	-0.013	0.00	0.00	No	0.00	No
	18	z	-0.013	0.00	0.00	No	0.00	No
	19	z	-0.018	0.00	0.00	No	0.00	No
	31	z	-0.017	0.00	0.00	No	0.00	No
	32	z	-0.017	0.00	0.00	No	0.00	No
	33	z	-0.017	0.00	0.00	No	0.00	No
	34	z	-0.013	0.00	0.00	No	0.00	No
	35	z	-0.013	0.00	0.00	No	0.00	No
	36	z	-0.018	0.00	0.00	No	0.00	No
	37	z	-0.017	0.00	0.00	No	0.00	No
	38	z	-0.013	0.00	0.00	No	0.00	No
	39	z	-0.013	0.00	0.00	No	0.00	No
	40	z	-0.018	0.00	0.00	No	0.00	No
	41	z	-0.017	0.00	0.00	No	0.00	No
	44	z	-0.007	0.00	0.00	No	0.00	No
	47	z	-0.007	0.00	0.00	No	0.00	No
	57	z	-0.007	0.00	0.00	No	0.00	No
	58	z	-0.007	0.00	0.00	No	0.00	No
	60	z	-0.02	0.00	0.00	No	0.00	No

	61	z	-0.02	0.00	0.00	No	0.00	No
	62	z	-0.02	0.00	0.00	No	0.00	No
	66	z	-0.02	0.00	0.00	No	0.00	No
	94	z	-0.007	0.00	0.00	No	0.00	No
	103	z	-0.007	0.00	0.00	No	0.00	No
	124	z	-0.013	0.00	0.00	No	0.00	No
	125	z	-0.013	0.00	0.00	No	0.00	No
	141	z	-0.012	0.00	0.00	No	0.00	No
	144	z	-0.016	0.00	0.00	No	0.00	No
	146	z	-0.012	0.00	0.00	No	0.00	No
	147	z	-0.012	0.00	0.00	No	0.00	No
	148	z	-0.012	0.00	0.00	No	0.00	No
	152	z	-0.012	0.00	0.00	No	0.00	No
	153	z	-0.012	0.00	0.00	No	0.00	No
	154	z	-0.017	0.00	0.00	No	0.00	No
	159	z	-0.007	0.00	0.00	No	0.00	No
	162	z	-0.01	0.00	0.00	No	0.00	No
	165	z	-0.007	0.00	0.00	No	0.00	No
	168	z	-0.007	0.00	0.00	No	0.00	No
	169	z	-0.007	0.00	0.00	No	0.00	No
	174	z	-0.007	0.00	0.00	No	0.00	No
	177	z	-0.007	0.00	0.00	No	0.00	No
	178	z	-0.007	0.00	0.00	No	0.00	No
	181	z	-0.007	0.00	0.00	No	0.00	No
W60	2	x	-0.017	0.00	0.00	No	0.00	No
	10	x	-0.017	0.00	0.00	No	0.00	No
	11	x	-0.017	0.00	0.00	No	0.00	No
	12	x	-0.013	0.00	0.00	No	0.00	No
	13	x	-0.013	0.00	0.00	No	0.00	No
	14	x	-0.018	0.00	0.00	No	0.00	No
	16	x	-0.017	0.00	0.00	No	0.00	No
	17	x	-0.013	0.00	0.00	No	0.00	No
	18	x	-0.013	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	37	x	-0.017	0.00	0.00	No	0.00	No
	38	x	-0.013	0.00	0.00	No	0.00	No
	39	x	-0.013	0.00	0.00	No	0.00	No
	40	x	-0.018	0.00	0.00	No	0.00	No
	41	x	-0.017	0.00	0.00	No	0.00	No
	44	x	-0.007	0.00	0.00	No	0.00	No
	47	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	60	x	-0.02	0.00	0.00	No	0.00	No
	61	x	-0.02	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	66	x	-0.02	0.00	0.00	No	0.00	No
	94	x	-0.007	0.00	0.00	No	0.00	No
	103	x	-0.007	0.00	0.00	No	0.00	No
	124	x	-0.013	0.00	0.00	No	0.00	No
	125	x	-0.013	0.00	0.00	No	0.00	No
	141	x	-0.012	0.00	0.00	No	0.00	No
	144	x	-0.016	0.00	0.00	No	0.00	No
	146	x	-0.012	0.00	0.00	No	0.00	No

	147	x	-0.012	0.00	0.00	No	0.00	No
	148	x	-0.012	0.00	0.00	No	0.00	No
	152	x	-0.012	0.00	0.00	No	0.00	No
	153	x	-0.012	0.00	0.00	No	0.00	No
	154	x	-0.017	0.00	0.00	No	0.00	No
	159	x	-0.007	0.00	0.00	No	0.00	No
	162	x	-0.01	0.00	0.00	No	0.00	No
	165	x	-0.007	0.00	0.00	No	0.00	No
	168	x	-0.007	0.00	0.00	No	0.00	No
	169	x	-0.007	0.00	0.00	No	0.00	No
	174	x	-0.007	0.00	0.00	No	0.00	No
	177	x	-0.007	0.00	0.00	No	0.00	No
	178	x	-0.007	0.00	0.00	No	0.00	No
	181	x	-0.007	0.00	0.00	No	0.00	No
W90	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No
	33	x	-0.017	0.00	0.00	No	0.00	No
	34	x	-0.013	0.00	0.00	No	0.00	No
	35	x	-0.013	0.00	0.00	No	0.00	No
	36	x	-0.018	0.00	0.00	No	0.00	No
	44	x	-0.007	0.00	0.00	No	0.00	No
	47	x	-0.007	0.00	0.00	No	0.00	No
	57	x	-0.007	0.00	0.00	No	0.00	No
	58	x	-0.007	0.00	0.00	No	0.00	No
	60	x	-0.02	0.00	0.00	No	0.00	No
	61	x	-0.02	0.00	0.00	No	0.00	No
	62	x	-0.02	0.00	0.00	No	0.00	No
	66	x	-0.02	0.00	0.00	No	0.00	No
	94	x	-0.007	0.00	0.00	No	0.00	No
	103	x	-0.007	0.00	0.00	No	0.00	No
	125	x	-0.013	0.00	0.00	No	0.00	No
	141	x	-0.012	0.00	0.00	No	0.00	No
	144	x	-0.016	0.00	0.00	No	0.00	No
	146	x	-0.012	0.00	0.00	No	0.00	No
	147	x	-0.012	0.00	0.00	No	0.00	No
	148	x	-0.012	0.00	0.00	No	0.00	No
	152	x	-0.012	0.00	0.00	No	0.00	No
	153	x	-0.012	0.00	0.00	No	0.00	No
	154	x	-0.017	0.00	0.00	No	0.00	No
	159	x	-0.007	0.00	0.00	No	0.00	No
	162	x	-0.01	0.00	0.00	No	0.00	No
	165	x	-0.007	0.00	0.00	No	0.00	No
	168	x	-0.007	0.00	0.00	No	0.00	No
	169	x	-0.007	0.00	0.00	No	0.00	No
	174	x	-0.007	0.00	0.00	No	0.00	No
	177	x	-0.007	0.00	0.00	No	0.00	No
	178	x	-0.007	0.00	0.00	No	0.00	No
	181	x	-0.007	0.00	0.00	No	0.00	No
W120	2	x	-0.017	0.00	0.00	No	0.00	No
	10	x	-0.017	0.00	0.00	No	0.00	No
	11	x	-0.017	0.00	0.00	No	0.00	No
	12	x	-0.013	0.00	0.00	No	0.00	No
	13	x	-0.013	0.00	0.00	No	0.00	No
	14	x	-0.018	0.00	0.00	No	0.00	No
	16	x	-0.017	0.00	0.00	No	0.00	No
	17	x	-0.013	0.00	0.00	No	0.00	No
	18	x	-0.013	0.00	0.00	No	0.00	No
	19	x	-0.018	0.00	0.00	No	0.00	No
	31	x	-0.017	0.00	0.00	No	0.00	No
	32	x	-0.017	0.00	0.00	No	0.00	No

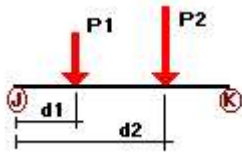
33	x	-0.017	0.00	0.00	No	0.00	No
34	x	-0.013	0.00	0.00	No	0.00	No
35	x	-0.013	0.00	0.00	No	0.00	No
36	x	-0.018	0.00	0.00	No	0.00	No
37	x	-0.017	0.00	0.00	No	0.00	No
38	x	-0.013	0.00	0.00	No	0.00	No
39	x	-0.013	0.00	0.00	No	0.00	No
40	x	-0.018	0.00	0.00	No	0.00	No
41	x	-0.017	0.00	0.00	No	0.00	No
44	x	-0.007	0.00	0.00	No	0.00	No
47	x	-0.007	0.00	0.00	No	0.00	No
57	x	-0.007	0.00	0.00	No	0.00	No
58	x	-0.007	0.00	0.00	No	0.00	No
60	x	-0.02	0.00	0.00	No	0.00	No
61	x	-0.02	0.00	0.00	No	0.00	No
62	x	-0.02	0.00	0.00	No	0.00	No
66	x	-0.02	0.00	0.00	No	0.00	No
94	x	-0.007	0.00	0.00	No	0.00	No
103	x	-0.007	0.00	0.00	No	0.00	No
124	x	-0.013	0.00	0.00	No	0.00	No
125	x	-0.013	0.00	0.00	No	0.00	No
141	x	-0.012	0.00	0.00	No	0.00	No
144	x	-0.016	0.00	0.00	No	0.00	No
146	x	-0.012	0.00	0.00	No	0.00	No
147	x	-0.012	0.00	0.00	No	0.00	No
148	x	-0.012	0.00	0.00	No	0.00	No
152	x	-0.012	0.00	0.00	No	0.00	No
153	x	-0.012	0.00	0.00	No	0.00	No
154	x	-0.017	0.00	0.00	No	0.00	No
159	x	-0.007	0.00	0.00	No	0.00	No
162	x	-0.01	0.00	0.00	No	0.00	No
165	x	-0.007	0.00	0.00	No	0.00	No
168	x	-0.007	0.00	0.00	No	0.00	No
169	x	-0.007	0.00	0.00	No	0.00	No
174	x	-0.007	0.00	0.00	No	0.00	No
177	x	-0.007	0.00	0.00	No	0.00	No
178	x	-0.007	0.00	0.00	No	0.00	No
181	x	-0.007	0.00	0.00	No	0.00	No
W150	2	z	0.017	0.00	No	0.00	No
	10	z	0.017	0.00	No	0.00	No
	11	z	0.017	0.00	No	0.00	No
	12	z	0.013	0.00	No	0.00	No
	13	z	0.013	0.00	No	0.00	No
	14	z	-0.018	0.00	No	0.00	No
	16	z	0.017	0.00	No	0.00	No
	17	z	0.013	0.00	No	0.00	No
	18	z	0.013	0.00	No	0.00	No
	19	z	-0.018	0.00	No	0.00	No
	31	z	0.017	0.00	No	0.00	No
	32	z	0.017	0.00	No	0.00	No
	33	z	0.017	0.00	No	0.00	No
	34	z	0.013	0.00	No	0.00	No
	35	z	0.013	0.00	No	0.00	No
	36	z	-0.018	0.00	No	0.00	No
	37	z	0.017	0.00	No	0.00	No
	38	z	0.013	0.00	No	0.00	No
	39	z	0.013	0.00	No	0.00	No
	40	z	-0.018	0.00	No	0.00	No
	41	z	0.017	0.00	No	0.00	No
	44	z	0.007	0.00	No	0.00	No

Di

47	z	0.007	0.00	0.00	No	0.00	No
57	z	0.007	0.00	0.00	No	0.00	No
58	z	0.007	0.00	0.00	No	0.00	No
60	z	0.02	0.00	0.00	No	0.00	No
61	z	0.02	0.00	0.00	No	0.00	No
62	z	0.02	0.00	0.00	No	0.00	No
66	z	0.02	0.00	0.00	No	0.00	No
94	z	0.007	0.00	0.00	No	0.00	No
103	z	0.007	0.00	0.00	No	0.00	No
124	z	0.013	0.00	0.00	No	0.00	No
125	z	0.013	0.00	0.00	No	0.00	No
141	z	-0.012	0.00	0.00	No	0.00	No
144	z	-0.016	0.00	0.00	No	0.00	No
146	z	-0.012	0.00	0.00	No	0.00	No
147	z	-0.012	0.00	0.00	No	0.00	No
148	z	-0.012	0.00	0.00	No	0.00	No
152	z	-0.012	0.00	0.00	No	0.00	No
153	z	-0.012	0.00	0.00	No	0.00	No
154	z	0.017	0.00	0.00	No	0.00	No
159	z	0.007	0.00	0.00	No	0.00	No
162	z	0.01	0.00	0.00	No	0.00	No
165	z	0.007	0.00	0.00	No	0.00	No
168	z	0.007	0.00	0.00	No	0.00	No
169	z	0.007	0.00	0.00	No	0.00	No
174	z	0.007	0.00	0.00	No	0.00	No
177	z	0.007	0.00	0.00	No	0.00	No
178	z	0.007	0.00	0.00	No	0.00	No
181	z	0.007	0.00	0.00	No	0.00	No
2	y	-0.007	0.00	0.00	No	0.00	No
10	y	-0.007	0.00	0.00	No	0.00	No
11	y	-0.007	0.00	0.00	No	0.00	No
12	y	-0.005	0.00	0.00	No	0.00	No
13	y	-0.005	0.00	0.00	No	0.00	No
14	y	-0.01	0.00	0.00	No	0.00	No
16	y	-0.007	0.00	0.00	No	0.00	No
17	y	-0.005	0.00	0.00	No	0.00	No
18	y	-0.005	0.00	0.00	No	0.00	No
19	y	-0.01	0.00	0.00	No	0.00	No
31	y	-0.007	0.00	0.00	No	0.00	No
32	y	-0.007	0.00	0.00	No	0.00	No
33	y	-0.007	0.00	0.00	No	0.00	No
34	y	-0.005	0.00	0.00	No	0.00	No
35	y	-0.005	0.00	0.00	No	0.00	No
36	y	-0.01	0.00	0.00	No	0.00	No
37	y	-0.007	0.00	0.00	No	0.00	No
38	y	-0.005	0.00	0.00	No	0.00	No
39	y	-0.005	0.00	0.00	No	0.00	No
40	y	-0.01	0.00	0.00	No	0.00	No
41	y	-0.007	0.00	0.00	No	0.00	No
44	y	-0.004	0.00	0.00	No	0.00	No
47	y	-0.004	0.00	0.00	No	0.00	No
57	y	-0.004	0.00	0.00	No	0.00	No
58	y	-0.004	0.00	0.00	No	0.00	No
60	y	-0.008	0.00	0.00	No	0.00	No
61	y	-0.008	0.00	0.00	No	0.00	No
62	y	-0.008	0.00	0.00	No	0.00	No
66	y	-0.008	0.00	0.00	No	0.00	No
94	y	-0.004	0.00	0.00	No	0.00	No
103	y	-0.004	0.00	0.00	No	0.00	No
124	y	-0.008	0.00	0.00	No	0.00	No

125	y	-0.008	0.00	0.00	No	0.00	No
141	y	-0.006	0.00	0.00	No	0.00	No
144	y	-0.008	0.00	0.00	No	0.00	No
146	y	-0.006	0.00	0.00	No	0.00	No
147	y	-0.008	0.00	0.00	No	0.00	No
148	y	-0.008	0.00	0.00	No	0.00	No
152	y	-0.006	0.00	0.00	No	0.00	No
153	y	-0.006	0.00	0.00	No	0.00	No
154	y	-0.007	0.00	0.00	No	0.00	No
159	y	-0.004	0.00	0.00	No	0.00	No
162	y	-0.005	0.00	0.00	No	0.00	No
165	y	-0.004	0.00	0.00	No	0.00	No
168	y	-0.004	0.00	0.00	No	0.00	No
169	y	-0.004	0.00	0.00	No	0.00	No
174	y	-0.004	0.00	0.00	No	0.00	No
177	y	-0.004	0.00	0.00	No	0.00	No
178	y	-0.004	0.00	0.00	No	0.00	No
181	y	-0.004	0.00	0.00	No	0.00	No

Concentrated forces on members



Condition	Member	Dir1	Value1 [Kip]	Dist1 [ft]	%
D	44	y	-0.03	2.00	No
	47	y	-0.03	2.00	No
	57	y	-0.03	2.00	No
	58	y	-0.037	2.00	No
	94	y	-0.03	2.00	No
	103	y	-0.015	2.00	No
	141	y	-0.033	0.50	No
		y	-0.033	2.50	No
		y	-0.041	4.50	No
		y	-0.041	6.50	No
	152	y	-0.065	0.50	No
		y	-0.065	5.50	No
	153	y	-0.04	0.50	No
		y	-0.04	5.50	No
	159	y	-0.022	2.00	No
	165	y	-0.022	2.00	No
	168	y	-0.03	2.00	No
	169	y	-0.03	2.00	No
	174	y	-0.03	2.00	No
	177	y	-0.03	2.00	No
178	y	-0.015	2.00	No	
181	y	-0.037	2.00	No	
Wo	44	z	-0.056	2.00	No
	47	z	-0.041	2.00	No
	57	z	-0.034	2.00	No
	58	z	-0.028	2.00	No
	94	z	-0.034	2.00	No

	103	z	-0.031	2.00	No
	141	z	-0.084	0.50	No
		z	-0.084	2.50	No
		z	-0.082	4.50	No
		z	-0.082	6.50	No
	152	z	-0.272	0.50	No
		z	-0.272	5.50	No
	153	z	-0.255	0.50	No
		z	-0.255	5.50	No
	159	z	-0.037	2.00	No
	165	z	-0.037	2.00	No
	168	z	-0.041	2.00	No
	169	z	-0.056	2.00	No
	174	z	-0.034	2.00	No
	177	z	-0.034	2.00	No
	178	z	-0.031	2.00	No
	181	z	-0.028	2.00	No
W30	44	3	-0.05	2.00	No
	47	3	-0.037	2.00	No
	57	3	-0.036	2.00	No
	58	3	-0.025	2.00	No
	94	3	-0.036	2.00	No
	103	3	-0.031	2.00	No
	141	3	-0.073	0.50	No
		3	-0.073	2.50	No
		3	-0.075	4.50	No
		3	-0.075	6.50	No
	152	3	-0.238	0.50	No
		3	-0.238	5.50	No
	153	3	-0.22	0.50	No
		3	-0.22	5.50	No
	159	3	-0.032	2.00	No
	165	3	-0.032	2.00	No
	168	3	-0.037	2.00	No
	169	3	-0.025	2.00	No
	174	3	-0.036	2.00	No
	177	3	-0.036	2.00	No
	178	3	-0.031	2.00	No
	181	3	-0.025	2.00	No
W60	44	3	-0.039	2.00	No
	47	3	-0.028	2.00	No
	57	3	-0.052	2.00	No
	58	3	-0.037	2.00	No
	94	3	-0.052	2.00	No
	103	3	-0.031	2.00	No
	141	3	-0.052	0.50	No
		3	-0.052	2.50	No
		3	-0.062	4.50	No
		3	-0.062	6.50	No
	152	3	-0.171	0.50	No
		3	-0.171	5.50	No
	153	3	-0.148	0.50	No
		3	-0.148	5.50	No
	159	3	-0.022	2.00	No
	165	3	-0.022	2.00	No
	168	3	-0.028	2.00	No
	169	3	-0.039	2.00	No
	174	3	-0.052	2.00	No
	177	3	-0.052	2.00	No
	178	3	-0.031	2.00	No

W90	181	3	-0.037	2.00	No
	44	x	-0.034	2.00	No
	47	x	-0.025	2.00	No
	57	x	-0.056	2.00	No
	58	x	-0.04	2.00	No
	94	x	-0.056	2.00	No
	103	x	-0.031	2.00	No
	141	x	-0.041	0.50	No
		x	-0.041	2.50	No
		x	-0.055	4.50	No
		x	-0.055	6.50	No
	152	x	-0.137	0.50	No
		x	-0.137	5.50	No
	153	x	-0.113	0.50	No
		x	-0.113	5.50	No
	159	x	-0.017	2.00	No
	165	x	-0.017	2.00	No
	168	x	-0.025	2.00	No
169	x	-0.034	2.00	No	
174	x	-0.056	2.00	No	
177	x	-0.056	2.00	No	
178	x	-0.031	2.00	No	
181	x	-0.04	2.00	No	
W120	44	2	-0.039	2.00	No
	47	2	-0.028	2.00	No
	57	2	-0.052	2.00	No
	58	2	-0.037	2.00	No
	94	2	-0.052	2.00	No
	103	2	-0.031	2.00	No
	141	2	-0.052	0.50	No
		2	-0.052	2.50	No
		2	-0.062	4.50	No
		2	-0.062	6.50	No
	152	2	-0.171	0.50	No
		2	-0.171	5.50	No
	153	2	-0.148	0.50	No
		2	-0.148	5.50	No
	159	2	-0.022	2.00	No
	165	2	-0.022	2.00	No
	168	2	-0.028	2.00	No
	169	2	-0.039	2.00	No
174	2	-0.052	2.00	No	
177	2	-0.052	2.00	No	
178	2	-0.031	2.00	No	
181	2	-0.037	2.00	No	
W150	44	2	-0.05	2.00	No
	47	2	-0.037	2.00	No
	57	2	-0.036	2.00	No
	58	2	-0.025	2.00	No
	94	2	-0.036	2.00	No
	103	2	-0.031	2.00	No
	141	2	-0.073	0.50	No
		2	-0.073	2.50	No
		2	-0.075	4.50	No
		2	-0.075	6.50	No
	152	2	-0.238	0.50	No
		2	-0.238	5.50	No
	153	2	-0.22	0.50	No
		2	-0.22	5.50	No
	159	2	-0.032	2.00	No

	165	2	-0.032	2.00	No
	168	2	-0.037	2.00	No
	169	2	-0.025	2.00	No
	174	2	-0.036	2.00	No
	177	2	-0.036	2.00	No
	178	2	-0.031	2.00	No
	181	2	-0.025	2.00	No
Di	44	y	-0.052	2.00	No
	47	y	-0.039	2.00	No
	57	y	-0.052	2.00	No
	58	y	-0.039	2.00	No
	94	y	-0.052	2.00	No
	103	y	-0.045	2.00	No
	141	y	-0.037	0.50	No
		y	-0.037	2.50	No
		y	-0.039	4.50	No
		y	-0.039	6.50	No
	152	y	-0.114	0.50	No
		y	-0.114	5.50	No
	153	y	-0.104	0.50	No
		y	-0.104	5.50	No
	159	y	-0.033	2.00	No
	165	y	-0.033	2.00	No
	168	y	-0.039	2.00	No
	169	y	-0.052	2.00	No
	174	y	-0.052	2.00	No
	177	y	-0.052	2.00	No
	178	y	-0.045	2.00	No
WI0	181	y	-0.039	2.00	No
	44	z	-0.013	2.00	No
	47	z	-0.01	2.00	No
	57	z	-0.009	2.00	No
	58	z	-0.007	2.00	No
	94	z	-0.009	2.00	No
	103	z	-0.007	2.00	No
	141	z	-0.019	0.50	No
		z	-0.019	2.50	No
		z	-0.018	4.50	No
		z	-0.018	6.50	No
	152	z	-0.055	0.50	No
		z	-0.055	5.50	No
	153	z	-0.052	0.50	No
		z	-0.052	5.50	No
	159	z	-0.009	2.00	No
	165	z	-0.009	2.00	No
	168	z	-0.01	2.00	No
	169	z	-0.013	2.00	No
	174	z	-0.009	2.00	No
	177	z	-0.009	2.00	No
	178	z	-0.007	2.00	No
	181	z	-0.007	2.00	No
WI30	44	3	-0.012	2.00	No
	47	3	-0.009	2.00	No
	57	3	-0.01	2.00	No
	58	3	-0.008	2.00	No
	94	3	-0.01	2.00	No
	103	3	-0.007	2.00	No
	141	3	-0.016	0.50	No
		3	-0.016	2.50	No
		3	-0.017	4.50	No

		3	-0.017	6.50	No
	152	3	-0.048	0.50	No
		3	-0.048	5.50	No
	153	3	-0.045	0.50	No
		3	-0.045	5.50	No
	159	3	-0.008	2.00	No
	165	3	-0.008	2.00	No
	168	3	-0.009	2.00	No
	169	3	-0.012	2.00	No
	174	3	-0.01	2.00	No
	177	3	-0.01	2.00	No
	178	3	-0.007	2.00	No
WI60	181	3	-0.008	2.00	No
	44	3	-0.01	2.00	No
	47	3	-0.007	2.00	No
	57	3	-0.012	2.00	No
	58	3	-0.009	2.00	No
	94	3	-0.012	2.00	No
	103	3	-0.007	2.00	No
	141	3	-0.012	0.50	No
		3	-0.012	2.50	No
		3	-0.014	4.50	No
		3	-0.014	6.50	No
	152	3	-0.036	0.50	No
		3	-0.036	5.50	No
	153	3	-0.032	0.50	No
		3	-0.032	5.50	No
	159	3	-0.006	2.00	No
	165	3	-0.006	2.00	No
	168	3	-0.007	2.00	No
	169	3	-0.01	2.00	No
	174	3	-0.012	2.00	No
	177	3	-0.012	2.00	No
	178	3	-0.007	2.00	No
WI90	181	3	-0.009	2.00	No
	44	x	-0.009	2.00	No
	47	x	-0.007	2.00	No
	57	x	-0.013	2.00	No
	58	x	-0.009	2.00	No
	94	x	-0.013	2.00	No
	103	x	-0.007	2.00	No
	141	x	-0.01	0.50	No
		x	-0.01	2.50	No
		x	-0.013	4.50	No
		x	-0.013	6.50	No
	152	x	-0.03	0.50	No
		x	-0.03	5.50	No
	153	x	-0.026	0.50	No
		x	-0.026	5.50	No
	159	x	-0.005	2.00	No
	165	x	-0.005	2.00	No
	168	x	-0.007	2.00	No
	169	x	-0.009	2.00	No
	174	x	-0.013	2.00	No
	177	x	-0.013	2.00	No
	178	x	-0.007	2.00	No
WI120	181	x	-0.009	2.00	No
	44	2	-0.01	2.00	No
	47	2	-0.007	2.00	No
	57	2	-0.012	2.00	No

	58	2	-0.009	2.00	No
	94	2	-0.012	2.00	No
	103	2	-0.007	2.00	No
	141	2	-0.012	0.50	No
		2	-0.012	2.50	No
		2	-0.014	4.50	No
		2	-0.014	6.50	No
	152	2	-0.036	0.50	No
		2	-0.036	5.50	No
	153	2	-0.032	0.50	No
		2	-0.032	5.50	No
	159	2	-0.006	2.00	No
	165	2	-0.006	2.00	No
	168	2	-0.007	2.00	No
	169	2	-0.01	2.00	No
	174	2	-0.012	2.00	No
	177	2	-0.012	2.00	No
	178	2	-0.007	2.00	No
W1150	181	2	-0.009	2.00	No
	44	2	-0.012	2.00	No
	47	2	-0.009	2.00	No
	57	2	-0.01	2.00	No
	58	2	-0.008	2.00	No
	94	2	-0.01	2.00	No
	103	2	-0.007	2.00	No
	141	2	-0.016	0.50	No
		2	-0.016	2.50	No
		2	-0.017	4.50	No
		2	-0.017	6.50	No
	152	2	-0.048	0.50	No
		2	-0.048	5.50	No
	153	2	-0.045	0.50	No
		2	-0.045	5.50	No
	159	2	-0.008	2.00	No
	165	2	-0.008	2.00	No
	168	2	-0.009	2.00	No
	169	2	-0.012	2.00	No
	174	2	-0.01	2.00	No
	177	2	-0.01	2.00	No
	178	2	-0.007	2.00	No
WLO	181	2	-0.008	2.00	No
	44	z	-0.004	2.00	No
	47	z	-0.003	2.00	No
	57	z	-0.002	2.00	No
	58	z	-0.002	2.00	No
	94	z	-0.002	2.00	No
	103	z	-0.002	2.00	No
	141	z	-0.006	0.50	No
		z	-0.006	2.50	No
		z	-0.006	4.50	No
		z	-0.006	6.50	No
	152	z	-0.017	0.50	No
		z	-0.017	5.50	No
	153	z	-0.016	0.50	No
		z	-0.016	5.50	No
	159	z	-0.003	2.00	No
	165	z	-0.003	2.00	No
	168	z	-0.003	2.00	No
	169	z	-0.004	2.00	No
	174	z	-0.002	2.00	No

	177	z	-0.002	2.00	No
	178	z	-0.002	2.00	No
	181	z	-0.002	2.00	No
WL30	44	3	-0.003	2.00	No
	47	3	-0.003	2.00	No
	57	3	-0.003	2.00	No
	58	3	-0.002	2.00	No
	94	3	-0.003	2.00	No
	103	3	-0.002	2.00	No
	141	3	-0.005	0.50	No
		3	-0.005	2.50	No
		3	-0.005	4.50	No
		3	-0.005	6.50	No
	152	3	-0.015	0.50	No
		3	-0.015	5.50	No
	153	3	-0.014	0.50	No
		3	-0.014	5.50	No
	159	3	-0.002	2.00	No
	165	3	-0.002	2.00	No
	168	3	-0.003	2.00	No
	169	3	-0.003	2.00	No
	174	3	-0.003	2.00	No
	177	3	-0.003	2.00	No
	178	3	-0.002	2.00	No
	181	3	-0.002	2.00	No
WL60	44	3	-0.003	2.00	No
	47	3	-0.002	2.00	No
	57	3	-0.003	2.00	No
	58	3	-0.003	2.00	No
	94	3	-0.003	2.00	No
	103	3	-0.002	2.00	No
	141	3	-0.004	0.50	No
		3	-0.004	2.50	No
		3	-0.004	4.50	No
		3	-0.004	6.50	No
	152	3	-0.011	0.50	No
		3	-0.011	5.50	No
	153	3	-0.01	0.50	No
		3	-0.01	5.50	No
	159	3	-0.002	2.00	No
	165	3	-0.002	2.00	No
	168	3	-0.002	2.00	No
	169	3	-0.003	2.00	No
	174	3	-0.003	2.00	No
	177	3	-0.003	2.00	No
	178	3	-0.002	2.00	No
	181	3	-0.003	2.00	No
WL90	44	x	-0.002	2.00	No
	47	x	-0.002	2.00	No
	57	x	-0.004	2.00	No
	58	x	-0.003	2.00	No
	94	x	-0.004	2.00	No
	103	x	-0.002	2.00	No
	141	x	-0.003	0.50	No
		x	-0.003	2.50	No
		x	-0.004	4.50	No
		x	-0.004	6.50	No
	152	x	-0.009	0.50	No
		x	-0.009	5.50	No
	153	x	-0.008	0.50	No

		x	-0.008	5.50	No
	159	x	-0.001	2.00	No
	165	x	-0.001	2.00	No
	168	x	-0.002	2.00	No
	169	x	-0.002	2.00	No
	174	x	-0.004	2.00	No
	177	x	-0.004	2.00	No
	178	x	-0.002	2.00	No
	181	x	-0.003	2.00	No
WL120	44	2	-0.003	2.00	No
	47	2	-0.002	2.00	No
	57	2	-0.003	2.00	No
	58	2	-0.003	2.00	No
	94	2	-0.003	2.00	No
	103	2	-0.002	2.00	No
	141	2	-0.004	0.50	No
		2	-0.004	2.50	No
		2	-0.004	4.50	No
		2	-0.004	6.50	No
	152	2	-0.011	0.50	No
		2	-0.011	5.50	No
	153	2	-0.01	0.50	No
		2	-0.01	5.50	No
	159	2	-0.002	2.00	No
	165	2	-0.002	2.00	No
	168	2	-0.002	2.00	No
	169	2	-0.003	2.00	No
	174	2	-0.003	2.00	No
	177	2	-0.003	2.00	No
	178	2	-0.002	2.00	No
	181	2	-0.003	2.00	No
WL150	44	2	-0.003	2.00	No
	47	2	-0.003	2.00	No
	57	2	-0.003	2.00	No
	58	2	-0.002	2.00	No
	94	2	-0.003	2.00	No
	103	2	-0.002	2.00	No
	141	2	-0.005	0.50	No
		2	-0.005	2.50	No
		2	-0.005	4.50	No
		2	-0.005	6.50	No
	152	2	-0.015	0.50	No
		2	-0.015	5.50	No
	153	2	-0.014	0.50	No
		2	-0.014	5.50	No
	159	2	-0.002	2.00	No
	165	2	-0.002	2.00	No
	168	2	-0.003	2.00	No
	169	2	-0.003	2.00	No
	174	2	-0.003	2.00	No
	177	2	-0.003	2.00	No
	178	2	-0.002	2.00	No
	181	2	-0.002	2.00	No

Self weight multipliers for load conditions

Condition	Description	Self weight multiplier			
		Comb.	MultX	MultY	MultZ
D	Dead Load	No	0.00	-1.00	0.00
Wo	Wind Load (NO ICE)	No	0.00	0.00	0.00
W30	WL 30deg	No	0.00	0.00	0.00
W60	WL 60deg	No	0.00	0.00	0.00
W90	WL 90deg	No	0.00	0.00	0.00
W120	WL 120deg	No	0.00	0.00	0.00
W150	WL 150deg	No	0.00	0.00	0.00
Di	Ice Load	No	0.00	0.00	0.00
WI0	WL ICE 0deg	No	0.00	0.00	0.00
WI30	WL ICE 30deg	No	0.00	0.00	0.00
WI60	WL ICE 60deg	No	0.00	0.00	0.00
WI90	WL ICE 90deg	No	0.00	0.00	0.00
WI120	WL ICE 120deg	No	0.00	0.00	0.00
WI150	WL ICE 150deg	No	0.00	0.00	0.00
WL0	WL 30 mph 0deg	No	0.00	0.00	0.00
WL30	WL 30 mph 30deg	No	0.00	0.00	0.00
WL60	WL 30 mph 60deg	No	0.00	0.00	0.00
WL90	WL 30 mph 90deg	No	0.00	0.00	0.00
WL120	WL 30 mph 120deg	No	0.00	0.00	0.00
WL150	WL 30 mph 150deg	No	0.00	0.00	0.00

Earthquake (Dynamic analysis only)

Condition	a/g	Ang. [Deg]	Damp. [%]
D	0.00	0.00	0.00
Wo	0.00	0.00	0.00
W30	0.00	0.00	0.00
W60	0.00	0.00	0.00
W90	0.00	0.00	0.00
W120	0.00	0.00	0.00
W150	0.00	0.00	0.00
Di	0.00	0.00	0.00
WI0	0.00	0.00	0.00
WI30	0.00	0.00	0.00
WI60	0.00	0.00	0.00
WI90	0.00	0.00	0.00
WI120	0.00	0.00	0.00
WI150	0.00	0.00	0.00
WL0	0.00	0.00	0.00
WL30	0.00	0.00	0.00
WL60	0.00	0.00	0.00
WL90	0.00	0.00	0.00
WL120	0.00	0.00	0.00
WL150	0.00	0.00	0.00

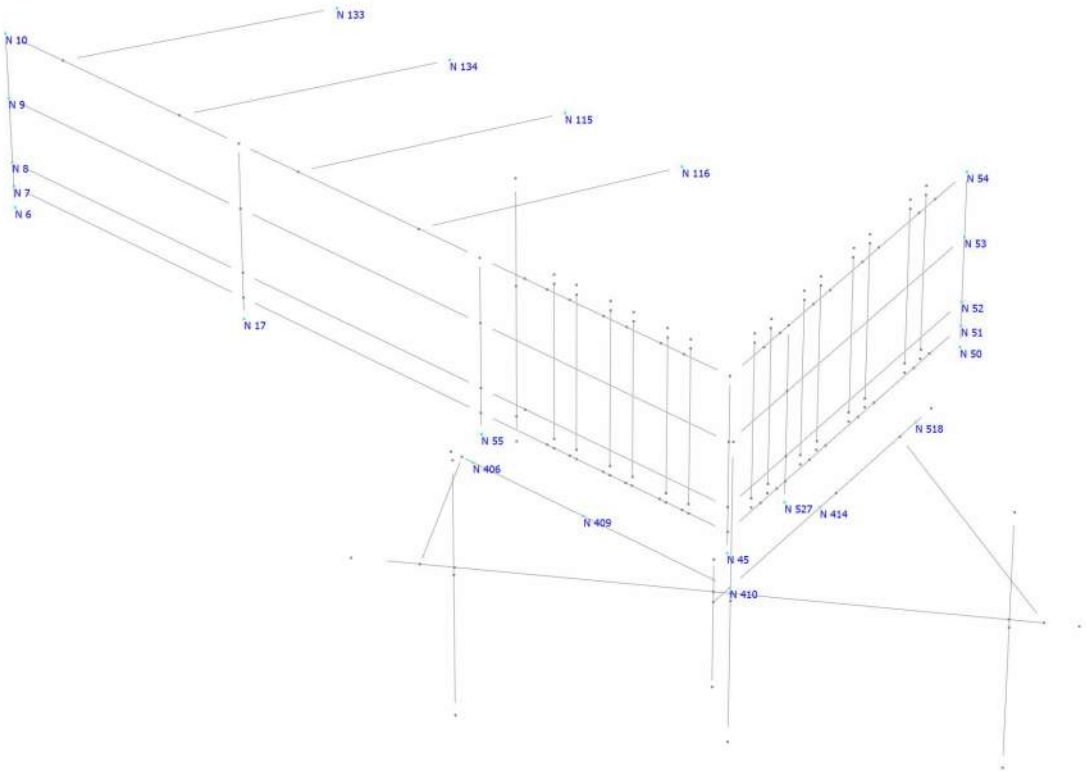
Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

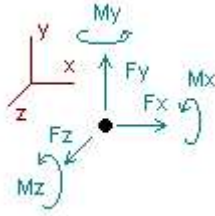
LC1=1.2D+1.6W_o
LC2=1.2D+1.6W₃₀
LC3=1.2D+1.6W₆₀
LC4=1.2D+1.6W₉₀
LC5=1.2D+1.6W₁₂₀
LC6=1.2D+1.6W₁₅₀
LC7=1.2D-1.6W_o
LC8=1.2D-1.6W₃₀
LC9=1.2D-1.6W₆₀
LC10=1.2D-1.6W₉₀
LC11=1.2D-1.6W₁₂₀
LC12=1.2D-1.6W₁₅₀
LC13=0.9D+1.6W_o
LC14=0.9D+1.6W₃₀
LC15=0.9D+1.6W₆₀
LC16=0.9D+1.6W₉₀
LC17=0.9D+1.6W₁₂₀
LC18=0.9D+1.6W₁₅₀
LC19=0.9D-1.6W_o
LC20=0.9D-1.6W₃₀
LC21=0.9D-1.6W₆₀
LC22=0.9D-1.6W₉₀
LC23=0.9D-1.6W₁₂₀
LC24=0.9D-1.6W₁₅₀
LC25=1.2D+D_i+W_{I0}
LC26=1.2D+D_i+W_{I30}
LC27=1.2D+D_i+W_{I60}
LC28=1.2D+D_i+W_{I90}
LC29=1.2D+D_i+W_{I120}
LC30=1.2D+D_i+W_{I150}
LC31=1.2D+D_i-W_{I0}
LC32=1.2D+D_i-W_{I30}
LC33=1.2D+D_i-W_{I60}
LC34=1.2D+D_i-W_{I90}
LC35=1.2D+D_i-W_{I120}
LC36=1.2D+D_i-W_{I150}
LC37=0.9D
LC38=1.2D
LC41=1.2D+W_{L0}
LC42=1.2D+W_{L30}
LC43=1.2D+W_{L60}
LC44=1.2D+W_{L90}
LC45=1.2D+W_{L120}
LC46=1.2D+W_{L150}
LC47=1.2D-W_{L0}
LC48=1.2D-W_{L30}
LC49=1.2D-W_{L60}
LC50=1.2D-W_{L90}
LC51=1.2D-W_{L120}
LC52=1.2D-W_{L150}

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
<i>HSS_SQR 3X3X1_4</i>		124	LC36 at 0.00%	0.16	OK	
		125	LC31 at 0.00%	0.11	OK	
<i>L 2-1_2X2-1_2X1_4</i>		2	LC8 at 100.00%	0.04	OK	
		10	LC7 at 37.50%	0.21	OK	
		11	LC17 at 22.92%	0.19	OK	
		16	LC1 at 22.92%	0.38	OK	
		31	LC10 at 100.00%	0.16	OK	
		32	LC4 at 100.00%	0.09	OK	
		33	LC4 at 45.00%	0.47	OK	
		37	LC4 at 0.00%	0.35	OK	
		41	LC19 at 100.00%	0.24	OK	
		154	LC4 at 62.50%	0.11	OK	
		<i>L 3X3X1_4</i>		60	LC11 at 0.00%	0.17
61	LC9 at 0.00%			0.17	OK	
62	LC11 at 0.00%			0.16	OK	
66	LC9 at 0.00%			0.17	OK	
<i>LU 2-3/4x5x1/4</i>		14	LC7 at 100.00%	0.05	OK	
		19	LC12 at 100.00%	0.06	OK	
		36	LC10 at 24.38%	0.22	OK	
		40	LC9 at 100.00%	0.24	OK	
<i>P1000 Unistrut</i>		44	LC1 at 50.00%	0.24	OK	Eq. H1.2-1
		47	LC1 at 50.00%	0.24	OK	Eq. H1.2-1
		57	LC10 at 50.00%	0.21	OK	Eq. H1.2-1
		58	LC4 at 50.00%	0.21	OK	Eq. H1.2-1
		94	LC10 at 50.00%	0.17	OK	Eq. H1.2-1
		103	LC4 at 50.00%	0.21	OK	Eq. H1.2-1
		159	LC1 at 50.00%	0.21	OK	Eq. H1.2-1
		165	LC1 at 50.00%	0.22	OK	Eq. H1.2-1
		168	LC1 at 50.00%	0.24	OK	Eq. H1.2-1
		169	LC19 at 50.00%	0.21	OK	Eq. H1.2-1
		174	LC10 at 50.00%	0.18	OK	Eq. H1.2-1
		177	LC4 at 50.00%	0.23	OK	Eq. H1.2-1
		178	LC4 at 50.00%	0.20	OK	Eq. H1.2-1
181	LC4 at 50.00%	0.18	OK	Eq. H1.2-1		
<i>PIPE 2-1_2x0.203</i>		141	LC7 at 50.00%	0.26	OK	
		146	LC31 at 50.00%	0.59	OK	
		147	LC8 at 0.00%	0.13	OK	
		148	LC31 at 0.00%	0.22	OK	
		152	LC1 at 46.88%	0.50	OK	
		153	LC7 at 46.88%	0.47	OK	
<i>PIPE 2x0.154</i>		162	LC1 at 58.33%	0.09	OK	
<i>PIPE 3-1_2x0.226</i>		144	LC27 at 72.92%	0.13	OK	
<i>PL 2x1/4</i>		12	LC6 at 100.00%	0.67	With warnings	
		13	LC12 at 100.00%	0.66	With warnings	
		17	LC7 at 100.00%	0.65	With warnings	
		18	LC6 at 0.00%	0.65	With warnings	
		34	LC3 at 25.00%	0.56	With warnings	
		35	LC11 at 100.00%	0.58	With warnings	
		38	LC2 at 0.00%	0.66	With warnings	
39	LC1 at 0.00%	0.63	With warnings			



Analysis result

Reactions



Direction of positive forces and moments

Node	Forces [Kip]			Moments [Kip*ft]		
	FX	FY	FZ	MX	MY	MZ
Condition LC1=1.2D+1.6Wo						
6	-0.01711	0.02841	0.00474	0.00000	-0.00206	0.00000
7	-0.16160	0.00000	0.06095	0.00000	0.00000	0.00000
8	-0.10850	0.00000	0.08833	0.00000	0.00000	0.00000
9	-0.11401	0.00000	0.10256	0.00000	0.00000	0.00000
10	0.11907	0.00000	0.01393	0.00000	0.00000	0.00000
17	0.20806	-0.00494	0.36512	0.00000	-0.00087	0.00000
45	-0.15236	0.15535	-0.02728	0.00000	0.00306	0.00000
50	0.00031	0.20645	0.09712	0.00000	-0.00151	0.00000
51	-0.04814	0.00000	0.88384	0.00000	0.00000	0.00000
52	-0.00549	0.00000	-0.10961	0.00000	0.00000	0.00000
53	0.00264	0.00000	0.03804	0.00000	0.00000	0.00000
54	-0.04285	0.00000	0.83909	0.00000	0.00000	0.00000
55	0.33841	0.00701	0.41327	0.00000	-0.00009	0.00000
115	-0.00672	0.06992	0.15750	0.00000	0.00000	0.00000
116	0.02046	0.32003	0.71281	0.00000	0.00000	0.00000
133	-0.00058	0.07581	0.16914	0.00000	0.00000	0.00000
134	0.00317	0.14109	0.31556	0.00000	0.00000	0.00000
406	0.33552	0.16385	0.69680	0.00000	0.11515	0.00000
409	0.00000	-0.37382	0.05980	0.00000	-0.00747	0.00000
410	-1.21233	1.06936	1.75488	0.00000	-0.48530	0.00000
414	0.00000	-0.37234	0.00000	0.00000	0.00000	0.00000
518	0.84157	0.00899	0.49809	0.00000	0.21219	0.00000
527	-0.03475	0.37384	0.05681	0.00000	0.00112	0.00000
578	0.03524	0.36877	0.12452	0.00000	-0.03479	0.00000
SUM	0.00000	2.23777	7.31601	0.00000	-0.20058	0.00000
Condition LC2=1.2D+1.6W30						
6	-0.01667	0.02943	0.00474	0.00000	-0.00209	0.00000
7	-0.03925	0.00000	0.06255	0.00000	0.00000	0.00000
8	-0.07903	0.00000	0.08836	0.00000	0.00000	0.00000
9	-0.10767	0.00000	0.10256	0.00000	0.00000	0.00000
10	0.31895	0.00000	0.01383	0.00000	0.00000	0.00000
17	0.22222	-0.01261	0.36474	0.00000	-0.00080	0.00000
45	-0.15602	0.14615	-0.02926	0.00000	0.00198	0.00000
50	-0.00277	0.20192	0.08825	0.00000	-0.00025	0.00000
51	0.01213	0.00000	0.80805	0.00000	0.00000	0.00000
52	-0.00234	0.00000	-0.07081	0.00000	0.00000	0.00000
53	0.00249	0.00000	0.10290	0.00000	0.00000	0.00000

54	0.01898	0.00000	0.74229	0.00000	0.00000	0.00000
55	0.36113	0.04643	0.36950	0.00000	0.00026	0.00000
115	-0.00614	0.08014	0.18027	0.00000	0.00000	0.00000
116	0.01745	0.28533	0.63572	0.00000	0.00000	0.00000
133	-0.00057	0.07588	0.16930	0.00000	0.00000	0.00000
134	0.00314	0.14077	0.31485	0.00000	0.00000	0.00000
406	0.36367	0.12962	0.70820	0.00000	0.17140	0.00000
409	0.00000	-0.30562	0.05980	0.00000	-0.00747	0.00000
410	0.20088	1.06686	0.94210	0.00000	0.01470	0.00000
414	0.00000	-0.43056	0.00000	0.00000	0.00000	0.00000
518	0.77024	0.02233	0.46209	0.00000	0.19918	0.00000
527	-0.01542	0.37954	0.04048	0.00000	0.00027	0.00000
578	0.03643	0.38219	0.11552	0.00000	-0.03478	0.00000

SUM	1.90183	2.23777	6.27602	0.00000	0.34239	0.00000
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Condition **LC3=1.2D+1.6W60**

6	0.02867	0.04132	0.00018	0.00000	0.00006	0.00000
7	0.78202	0.00000	-0.00121	0.00000	0.00000	0.00000
8	0.00619	0.00000	0.00078	0.00000	0.00000	0.00000
9	0.04326	0.00000	-0.00030	0.00000	0.00000	0.00000
10	1.58068	0.00000	-0.09531	0.00000	0.00000	0.00000
17	0.05179	0.15792	0.00836	0.00000	-0.00013	0.00000
45	-0.04434	0.10816	-0.04882	0.00000	-0.00326	0.00000
50	-0.00532	0.18989	0.05124	0.00000	0.00548	0.00000
51	0.25553	0.00000	0.46350	0.00000	0.00000	0.00000
52	0.09378	0.00000	-0.09318	0.00000	0.00000	0.00000
53	0.10372	0.00000	0.10267	0.00000	0.00000	0.00000
54	0.25808	0.00000	0.26857	0.00000	0.00000	0.00000
55	0.16532	0.36898	-0.05704	0.00000	0.00038	0.00000
115	0.11474	0.03632	0.02352	0.00000	0.00000	0.00000
116	0.11313	0.02553	-0.00056	0.00000	0.00000	0.00000
133	0.11424	0.03908	0.02967	0.00000	0.00000	0.00000
134	0.11341	0.01933	-0.01433	0.00000	0.00000	0.00000
406	0.27302	0.12546	0.43431	0.00000	0.13384	0.00000
409	0.00000	-0.29837	0.00000	0.00000	0.00000	0.00000
410	0.85462	1.11046	0.21013	0.00000	0.23598	0.00000
414	0.03380	-0.54057	0.00000	0.00000	0.01268	0.00000
518	0.54121	0.02246	0.26826	0.00000	0.17279	0.00000
527	0.03419	0.38642	-0.04717	0.00000	-0.00360	0.00000
578	0.08364	0.44537	0.06706	0.00000	-0.05325	0.00000

SUM	5.59538	2.23777	1.57034	0.00000	0.50098	0.00000
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Condition **LC4=1.2D+1.6W90**

6	0.02069	0.04273	0.00028	0.00000	0.00003	0.00000
7	0.70503	0.00000	0.00016	0.00000	0.00000	0.00000
8	-0.02266	0.00000	0.00090	0.00000	0.00000	0.00000
9	0.00033	0.00000	-0.00027	0.00000	0.00000	0.00000
10	1.54524	0.00000	-0.09458	0.00000	0.00000	0.00000
17	0.07422	0.15017	0.00816	0.00000	-0.00001	0.00000
45	-0.07377	0.11375	-0.05832	0.00000	-0.00415	0.00000
50	-0.00769	0.18525	0.03479	0.00000	0.00641	0.00000
51	0.30205	0.00000	0.24473	0.00000	0.00000	0.00000
52	0.09594	0.00000	-0.08391	0.00000	0.00000	0.00000
53	0.10363	0.00000	0.11886	0.00000	0.00000	0.00000
54	0.30638	0.00000	0.01029	0.00000	0.00000	0.00000
55	0.16552	0.39958	-0.09842	0.00000	0.00077	0.00000
115	0.11534	0.04314	0.03872	0.00000	0.00000	0.00000

116	0.11015	-0.00486	-0.06816	0.00000	0.00000	0.00000
133	0.11426	0.03800	0.02724	0.00000	0.00000	0.00000
134	0.11342	0.02132	-0.00987	0.00000	0.00000	0.00000
406	0.15996	0.11815	0.23777	0.00000	0.07667	0.00000
409	0.00000	-0.29525	0.00000	0.00000	0.00000	0.00000
410	1.38613	1.12015	-0.38148	0.00000	0.45770	0.00000
414	0.03380	-0.56210	0.00000	0.00000	0.01268	0.00000
518	0.26262	0.03079	0.11497	0.00000	0.10164	0.00000
527	0.04633	0.38388	-0.07061	0.00000	-0.00426	0.00000
578	0.07121	0.45307	0.02874	0.00000	-0.04120	0.00000

SUM	5.62811	2.23777	0.00000	0.00000	0.60627	0.00000
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Condition **LC5=1.2D+1.6W120**

6	0.02876	0.04183	0.00019	0.00000	0.00002	0.00000
7	0.78915	0.00000	0.00116	0.00000	0.00000	0.00000
8	0.00611	0.00000	0.00077	0.00000	0.00000	0.00000
9	0.04327	0.00000	-0.00029	0.00000	0.00000	0.00000
10	1.57144	0.00000	-0.09540	0.00000	0.00000	0.00000
17	0.05099	0.14732	0.00759	0.00000	-0.00002	0.00000
45	-0.08184	0.13195	-0.06867	0.00000	-0.00414	0.00000
50	-0.00604	0.18380	0.04037	0.00000	0.00594	0.00000
51	0.27621	0.00000	0.00304	0.00000	0.00000	0.00000
52	0.09472	0.00000	-0.08521	0.00000	0.00000	0.00000
53	0.10337	0.00000	0.10851	0.00000	0.00000	0.00000
54	0.28223	0.00000	-0.25051	0.00000	0.00000	0.00000
55	0.15061	0.41153	-0.11896	0.00000	0.00089	0.00000
115	0.11548	0.05030	0.05465	0.00000	0.00000	0.00000
116	0.10883	-0.02154	-0.10535	0.00000	0.00000	0.00000
133	0.11425	0.03937	0.03030	0.00000	0.00000	0.00000
134	0.11333	0.01828	-0.01668	0.00000	0.00000	0.00000
406	0.03175	0.11156	0.01776	0.00000	0.00833	0.00000
409	0.00000	-0.27320	0.00000	0.00000	0.00000	0.00000
410	1.71492	1.10927	-0.92503	0.00000	0.61083	0.00000
414	0.03380	-0.57758	0.00000	0.00000	0.01268	0.00000
518	-0.05047	0.03953	-0.05800	0.00000	0.02054	0.00000
527	0.04823	0.37014	-0.09608	0.00000	-0.00394	0.00000
578	0.05628	0.45523	-0.01450	0.00000	-0.02698	0.00000

SUM	5.59538	2.23777	-1.57034	0.00000	0.62413	0.00000
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Condition **LC6=1.2D+1.6W150**

6	0.01527	0.14012	-0.00433	0.00000	0.00053	0.00000
7	0.25599	0.00000	0.06706	0.00000	0.00000	0.00000
8	-0.04068	0.00000	-0.08498	0.00000	0.00000	0.00000
9	0.05481	0.00000	-0.10520	0.00000	0.00000	0.00000
10	0.16089	0.00000	-0.01388	0.00000	0.00000	0.00000
17	-0.05533	0.32544	-0.06021	0.00000	0.00082	0.00000
45	-0.04085	0.18586	-0.01928	0.00000	-0.00267	0.00000
50	-0.00629	0.18035	0.05411	0.00000	0.00203	0.00000
51	0.08910	0.00000	-0.37619	0.00000	0.00000	0.00000
52	0.00138	0.00000	-0.20283	0.00000	0.00000	0.00000
53	0.00020	0.00000	-0.17369	0.00000	0.00000	0.00000
54	0.10464	0.00000	-0.64682	0.00000	0.00000	0.00000
55	-0.01308	0.55449	-0.12517	0.00000	0.00028	0.00000
115	0.01300	-0.01357	-0.14613	0.00000	0.00000	0.00000
116	-0.01532	-0.24885	-0.66971	0.00000	0.00000	0.00000
133	0.00683	-0.01341	-0.14465	0.00000	0.00000	0.00000
134	0.00161	-0.08206	-0.29821	0.00000	0.00000	0.00000

406	-0.00067	0.10753	0.01323	0.00000	-0.00427	0.00000
409	0.00000	-0.26575	-0.05980	0.00000	0.00747	0.00000
410	1.42590	1.09984	-0.67898	0.00000	0.49677	0.00000
414	0.00000	-0.56240	0.00000	0.00000	0.00000	0.00000
518	-0.05242	0.04406	0.00865	0.00000	-0.01250	0.00000
527	-0.00154	0.34460	-0.08781	0.00000	-0.00143	0.00000
578	-0.00160	0.44153	0.00216	0.00000	0.00175	0.00000

SUM	1.90183	2.23777	-3.75264	0.00000	0.48877	0.00000
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Condition **LC7=1.2D-1.6Wo**

6	0.05268	0.14726	-0.00363	0.00000	0.00218	0.00000
7	0.35591	0.00000	-0.06457	0.00000	0.00000	0.00000
8	-0.07658	0.00000	-0.08473	0.00000	0.00000	0.00000
9	0.05861	0.00000	-0.10560	0.00000	0.00000	0.00000
10	-0.07930	0.00000	-0.01437	0.00000	0.00000	0.00000
17	-0.21831	0.33429	-0.36715	0.00000	0.00084	0.00000
45	-0.06270	0.19562	-0.00699	0.00000	-0.00308	0.00000
50	-0.00354	0.18075	0.07288	0.00000	0.00132	0.00000
51	0.04496	0.00000	-0.57465	0.00000	0.00000	0.00000
52	-0.00037	0.00000	-0.21961	0.00000	0.00000	0.00000
53	-0.00003	0.00000	-0.16826	0.00000	0.00000	0.00000
54	0.05875	0.00000	-0.74998	0.00000	0.00000	0.00000
55	-0.17682	0.56786	-0.40475	0.00000	0.00008	0.00000
115	0.01392	-0.01973	-0.16030	0.00000	0.00000	0.00000
116	-0.01726	-0.27226	-0.72226	0.00000	0.00000	0.00000
133	0.00693	-0.01188	-0.14125	0.00000	0.00000	0.00000
134	0.00105	-0.09302	-0.32302	0.00000	0.00000	0.00000
406	-0.39799	0.11633	-0.67859	0.00000	-0.25270	0.00000
409	0.00000	-0.28734	-0.05980	0.00000	0.00747	0.00000
410	1.25542	1.18327	-1.76433	0.00000	0.54095	0.00000
414	0.00000	-0.73993	0.00000	0.00000	0.00000	0.00000
518	-0.85227	0.03959	-0.50509	0.00000	-0.17852	0.00000
527	0.04208	0.34408	-0.14369	0.00000	-0.00092	0.00000
578	-0.00517	0.55290	-0.12627	0.00000	0.01380	0.00000

SUM	0.00000	2.23777	-7.31601	0.00000	0.13144	0.00000
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Condition **LC8=1.2D-1.6W30**

6	0.05165	0.14630	-0.00366	0.00000	0.00221	0.00000
7	0.20355	0.00000	-0.06628	0.00000	0.00000	0.00000
8	-0.07521	0.00000	-0.08477	0.00000	0.00000	0.00000
9	0.05871	0.00000	-0.10559	0.00000	0.00000	0.00000
10	-0.28576	0.00000	-0.01432	0.00000	0.00000	0.00000
17	-0.22699	0.34204	-0.36653	0.00000	0.00079	0.00000
45	-0.07909	0.20742	0.00586	0.00000	-0.00203	0.00000
50	-0.00053	0.18529	0.08241	0.00000	0.00008	0.00000
51	-0.01505	0.00000	-0.52887	0.00000	0.00000	0.00000
52	-0.00347	0.00000	-0.24450	0.00000	0.00000	0.00000
53	-0.00001	0.00000	-0.21507	0.00000	0.00000	0.00000
54	-0.00394	0.00000	-0.66362	0.00000	0.00000	0.00000
55	-0.18285	0.52728	-0.36175	0.00000	-0.00024	0.00000
115	0.01337	-0.03067	-0.18468	0.00000	0.00000	0.00000
116	-0.01396	-0.23747	-0.64465	0.00000	0.00000	0.00000
133	0.00692	-0.01215	-0.14184	0.00000	0.00000	0.00000
134	0.00110	-0.09203	-0.32080	0.00000	0.00000	0.00000
406	-0.42666	0.15071	-0.69009	0.00000	-0.30918	0.00000
409	0.00000	-0.35602	-0.05980	0.00000	0.00747	0.00000
410	-0.15704	1.18705	-0.95191	0.00000	0.04122	0.00000

414	0.00000	-0.67913	0.00000	0.00000	0.00000	0.00000
518	-0.78091	0.02481	-0.46873	0.00000	-0.16581	0.00000
527	0.02094	0.33694	-0.12966	0.00000	-0.00008	0.00000
578	-0.00661	0.53739	-0.11718	0.00000	0.01396	0.00000

SUM	-1.90183	2.23777	-6.27602	0.00000	-0.41161	0.00000

Condition **LC9=1.2D-1.6W60**

6	0.00735	0.13371	0.00095	0.00000	0.00004	0.00000
7	-0.43494	0.00000	-0.00273	0.00000	0.00000	0.00000
8	-0.25659	0.00000	0.00292	0.00000	0.00000	0.00000
9	-0.25533	0.00000	-0.00269	0.00000	0.00000	0.00000
10	-1.44533	0.00000	0.09401	0.00000	0.00000	0.00000
17	-0.04972	0.17349	-0.01045	0.00000	0.00010	0.00000
45	-0.22606	0.24981	0.10348	0.00000	0.00310	0.00000
50	0.00178	0.19660	0.11910	0.00000	-0.00560	0.00000
51	-0.25883	0.00000	-0.31706	0.00000	0.00000	0.00000
52	-0.09955	0.00000	-0.16646	0.00000	0.00000	0.00000
53	-0.10148	0.00000	-0.11638	0.00000	0.00000	0.00000
54	-0.24365	0.00000	-0.24622	0.00000	0.00000	0.00000
55	0.01355	0.20532	0.06406	0.00000	-0.00043	0.00000
115	-0.10743	0.01626	-0.02096	0.00000	0.00000	0.00000
116	-0.10899	0.02034	-0.01164	0.00000	0.00000	0.00000
133	-0.10785	0.02583	0.00046	0.00000	0.00000	0.00000
134	-0.10907	0.02735	0.00394	0.00000	0.00000	0.00000
406	-0.33618	0.15489	-0.41609	0.00000	-0.27191	0.00000
409	0.00000	-0.36376	0.00000	0.00000	0.00000	0.00000
410	-0.81061	1.14433	-0.22031	0.00000	-0.18008	0.00000
414	-0.03380	-0.56947	0.00000	0.00000	-0.01268	0.00000
518	-0.55202	0.02435	-0.27470	0.00000	-0.13929	0.00000
527	-0.02694	0.32428	-0.08491	0.00000	0.00382	0.00000
578	-0.05368	0.47447	-0.06867	0.00000	0.03234	0.00000

SUM	-5.59538	2.23777	-1.57034	0.00000	-0.57059	0.00000

Condition **LC10=1.2D-1.6W90**

6	0.01368	0.13227	0.00077	0.00000	0.00007	0.00000
7	-0.42121	0.00000	-0.00383	0.00000	0.00000	0.00000
8	-0.20344	0.00000	0.00268	0.00000	0.00000	0.00000
9	-0.15165	0.00000	-0.00268	0.00000	0.00000	0.00000
10	-1.44676	0.00000	0.09337	0.00000	0.00000	0.00000
17	-0.04779	0.18161	-0.01049	0.00000	0.00003	0.00000
45	-0.22264	0.24800	0.12767	0.00000	0.00398	0.00000
50	0.00423	0.20087	0.13499	0.00000	-0.00653	0.00000
51	-0.30532	0.00000	-0.14701	0.00000	0.00000	0.00000
52	-0.10170	0.00000	-0.14883	0.00000	0.00000	0.00000
53	-0.10139	0.00000	-0.10863	0.00000	0.00000	0.00000
54	-0.29049	0.00000	-0.00353	0.00000	0.00000	0.00000
55	0.02982	0.17262	0.10590	0.00000	-0.00079	0.00000
115	-0.10795	0.00730	-0.04090	0.00000	0.00000	0.00000
116	-0.10606	0.05205	0.05895	0.00000	0.00000	0.00000
133	-0.10787	0.02636	0.00166	0.00000	0.00000	0.00000
134	-0.10904	0.02714	0.00346	0.00000	0.00000	0.00000
406	-0.22320	0.16257	-0.21946	0.00000	-0.21498	0.00000
409	0.00000	-0.36827	0.00000	0.00000	0.00000	0.00000
410	-1.34208	1.13515	0.37115	0.00000	-0.40177	0.00000
414	-0.03380	-0.54702	0.00000	0.00000	-0.01268	0.00000
518	-0.27351	0.01590	-0.12135	0.00000	-0.06802	0.00000
527	-0.03881	0.32476	-0.06356	0.00000	0.00448	0.00000

578	-0.04113	0.46647	-0.03034	0.00000	0.02021	0.00000
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SUM	-5.62811	2.23777	0.00000	0.00000	-0.67600	0.00000
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Condition LC11=1.2D-1.6W120						
6	0.00719	0.13299	0.00094	0.00000	0.00009	0.00000
7	-0.43963	0.00000	-0.00502	0.00000	0.00000	0.00000
8	-0.26346	0.00000	0.00291	0.00000	0.00000	0.00000
9	-0.25037	0.00000	-0.00269	0.00000	0.00000	0.00000
10	-1.43949	0.00000	0.09408	0.00000	0.00000	0.00000
17	-0.04722	0.18447	-0.00981	0.00000	0.00000	0.00000
45	-0.20207	0.23234	0.14039	0.00000	0.00399	0.00000
50	0.00268	0.20199	0.12846	0.00000	-0.00610	0.00000
51	-0.28011	0.00000	0.06364	0.00000	0.00000	0.00000
52	-0.10052	0.00000	-0.12058	0.00000	0.00000	0.00000
53	-0.10107	0.00000	-0.08259	0.00000	0.00000	0.00000
54	-0.26520	0.00000	0.24558	0.00000	0.00000	0.00000
55	0.03764	0.16159	0.12672	0.00000	-0.00093	0.00000
115	-0.10817	0.00233	-0.05197	0.00000	0.00000	0.00000
116	-0.10471	0.06801	0.09451	0.00000	0.00000	0.00000
133	-0.10786	0.02563	0.00004	0.00000	0.00000	0.00000
134	-0.10900	0.02822	0.00590	0.00000	0.00000	0.00000
406	-0.09485	0.16927	0.00063	0.00000	-0.14665	0.00000
409	0.00000	-0.39043	0.00000	0.00000	0.00000	0.00000
410	-1.67108	1.14567	0.91475	0.00000	-0.55501	0.00000
414	-0.03380	-0.53249	0.00000	0.00000	-0.01268	0.00000
518	0.03954	0.00766	0.05151	0.00000	0.01320	0.00000
527	-0.03773	0.33539	-0.03993	0.00000	0.00418	0.00000
578	-0.02610	0.46513	0.01288	0.00000	0.00591	0.00000
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SUM	-5.59538	2.23777	1.57034	0.00000	-0.69400	0.00000
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Condition LC12=1.2D-1.6W150						
6	0.02006	0.03485	0.00544	0.00000	-0.00041	0.00000
7	-0.06878	0.00000	-0.07070	0.00000	0.00000	0.00000
8	-0.12863	0.00000	0.08856	0.00000	0.00000	0.00000
9	-0.11694	0.00000	0.10212	0.00000	0.00000	0.00000
10	-0.11925	0.00000	0.01341	0.00000	0.00000	0.00000
17	0.04722	0.00419	0.05828	0.00000	-0.00084	0.00000
45	-0.17154	0.17138	0.00170	0.00000	0.00263	0.00000
50	0.00307	0.20656	0.11528	0.00000	-0.00223	0.00000
51	-0.09254	0.00000	0.62830	0.00000	0.00000	0.00000
52	-0.00726	0.00000	-0.08242	0.00000	0.00000	0.00000
53	0.00244	0.00000	0.06649	0.00000	0.00000	0.00000
54	-0.08852	0.00000	0.71993	0.00000	0.00000	0.00000
55	0.16744	0.02088	0.13241	0.00000	-0.00028	0.00000
115	-0.00574	0.06490	0.14590	0.00000	0.00000	0.00000
116	0.01854	0.29602	0.65921	0.00000	0.00000	0.00000
133	-0.00048	0.07766	0.17326	0.00000	0.00000	0.00000
134	0.00259	0.12930	0.28895	0.00000	0.00000	0.00000
406	-0.06245	0.17331	0.00513	0.00000	-0.13406	0.00000
409	0.00000	-0.39772	0.05980	0.00000	-0.00747	0.00000
410	-1.38203	1.15515	0.66869	0.00000	-0.44092	0.00000
414	0.00000	-0.54786	0.00000	0.00000	0.00000	0.00000
518	0.04150	0.00304	-0.01510	0.00000	0.04622	0.00000
527	0.00771	0.36722	-0.00821	0.00000	0.00164	0.00000
578	0.03176	0.47889	-0.00378	0.00000	-0.02280	0.00000
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SUM	-1.90183	2.23777	3.75264	0.00000	-0.55853	0.00000

Condition **LC13=0.9D+1.6Wo**

6	-0.02124	0.00671	0.00461	0.00000	-0.00207	0.00000
7	-0.16994	0.00000	0.06142	0.00000	0.00000	0.00000
8	-0.09829	0.00000	0.08789	0.00000	0.00000	0.00000
9	-0.11912	0.00000	0.10292	0.00000	0.00000	0.00000
10	0.12249	0.00000	0.01407	0.00000	0.00000	0.00000
17	0.20681	-0.04627	0.36530	0.00000	-0.00087	0.00000
45	-0.12284	0.10901	-0.03314	0.00000	0.00307	0.00000
50	0.00072	0.15813	0.07579	0.00000	-0.00149	0.00000
51	-0.04765	0.00000	0.87755	0.00000	0.00000	0.00000
52	-0.00476	0.00000	-0.08467	0.00000	0.00000	0.00000
53	0.00233	0.00000	0.02724	0.00000	0.00000	0.00000
54	-0.04456	0.00000	0.84409	0.00000	0.00000	0.00000
55	0.31726	-0.06482	0.41314	0.00000	-0.00010	0.00000
115	-0.00764	0.06348	0.15749	0.00000	0.00000	0.00000
116	0.01994	0.31427	0.71424	0.00000	0.00000	0.00000
133	-0.00138	0.06772	0.16544	0.00000	0.00000	0.00000
134	0.00262	0.13515	0.31662	0.00000	0.00000	0.00000
406	0.34341	0.12895	0.69451	0.00000	0.13252	0.00000
409	0.00000	-0.29106	0.05980	0.00000	-0.00747	0.00000
410	-1.21780	0.78470	1.75620	0.00000	-0.49227	0.00000
414	0.00000	-0.23212	0.00000	0.00000	0.00000	0.00000
518	0.84290	0.00439	0.49886	0.00000	0.20799	0.00000
527	-0.03474	0.28635	0.07192	0.00000	0.00110	0.00000
578	0.03149	0.25374	0.12471	0.00000	-0.03217	0.00000
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SUM	0.00000	1.67833	7.31601	0.00000	-0.19178	0.00000

Condition **LC14=0.9D+1.6W30**

6	-0.02080	0.00773	0.00461	0.00000	-0.00210	0.00000
7	-0.04750	0.00000	0.06302	0.00000	0.00000	0.00000
8	-0.06901	0.00000	0.08791	0.00000	0.00000	0.00000
9	-0.11280	0.00000	0.10292	0.00000	0.00000	0.00000
10	0.32239	0.00000	0.01397	0.00000	0.00000	0.00000
17	0.22104	-0.05392	0.36492	0.00000	-0.00081	0.00000
45	-0.12672	0.09981	-0.03503	0.00000	0.00199	0.00000
50	-0.00236	0.15359	0.06694	0.00000	-0.00022	0.00000
51	0.01262	0.00000	0.80165	0.00000	0.00000	0.00000
52	-0.00161	0.00000	-0.04588	0.00000	0.00000	0.00000
53	0.00218	0.00000	0.09210	0.00000	0.00000	0.00000
54	0.01727	0.00000	0.74729	0.00000	0.00000	0.00000
55	0.34015	-0.02544	0.36937	0.00000	0.00025	0.00000
115	-0.00706	0.07370	0.18024	0.00000	0.00000	0.00000
116	0.01693	0.27958	0.63720	0.00000	0.00000	0.00000
133	-0.00137	0.06779	0.16560	0.00000	0.00000	0.00000
134	0.00259	0.13482	0.31591	0.00000	0.00000	0.00000
406	0.37166	0.09464	0.70590	0.00000	0.18894	0.00000
409	0.00000	-0.22121	0.05980	0.00000	-0.00747	0.00000
410	0.19531	0.78177	0.94341	0.00000	0.00755	0.00000
414	0.00000	-0.29171	0.00000	0.00000	0.00000	0.00000
518	0.77162	0.01760	0.46288	0.00000	0.19492	0.00000
527	-0.01532	0.29205	0.05557	0.00000	0.00024	0.00000
578	0.03263	0.26751	0.11572	0.00000	-0.03212	0.00000
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SUM	1.90183	1.67833	6.27602	0.00000	0.35117	0.00000

Condition **LC15=0.9D+1.6W60**

6	0.02441	0.01957	0.00004	0.00000	0.00005	0.00000
7	0.77481	0.00000	-0.00073	0.00000	0.00000	0.00000
8	0.01320	0.00000	0.00032	0.00000	0.00000	0.00000
9	0.03775	0.00000	0.00007	0.00000	0.00000	0.00000
10	1.58455	0.00000	-0.09516	0.00000	0.00000	0.00000
17	0.05351	0.11674	0.00851	0.00000	-0.00013	0.00000
45	-0.01386	0.06165	-0.05486	0.00000	-0.00324	0.00000
50	-0.00491	0.14155	0.02996	0.00000	0.00551	0.00000
51	0.25598	0.00000	0.45743	0.00000	0.00000	0.00000
52	0.09451	0.00000	-0.06828	0.00000	0.00000	0.00000
53	0.10342	0.00000	0.09189	0.00000	0.00000	0.00000
54	0.25634	0.00000	0.27350	0.00000	0.00000	0.00000
55	0.14178	0.29716	-0.05721	0.00000	0.00036	0.00000
115	0.11382	0.02985	0.02345	0.00000	0.00000	0.00000
116	0.11264	0.01984	0.00105	0.00000	0.00000	0.00000
133	0.11344	0.03099	0.02594	0.00000	0.00000	0.00000
134	0.11288	0.01343	-0.01319	0.00000	0.00000	0.00000
406	0.28101	0.09043	0.43201	0.00000	0.15135	0.00000
409	0.00000	-0.21384	0.00000	0.00000	0.00000	0.00000
410	0.84905	0.82630	0.21143	0.00000	0.22881	0.00000
414	0.03380	-0.40239	0.00000	0.00000	0.01268	0.00000
518	0.54259	0.01731	0.26906	0.00000	0.16853	0.00000
527	0.03482	0.29893	-0.03216	0.00000	-0.00362	0.00000
578	0.07983	0.33080	0.06726	0.00000	-0.05059	0.00000

SUM	5.59538	1.67833	1.57034	0.00000	0.50971	0.00000

Condition **LC16=0.9D+1.6W90**

6	0.01644	0.02099	0.00015	0.00000	0.00002	0.00000
7	0.69781	0.00000	0.00064	0.00000	0.00000	0.00000
8	-0.01565	0.00000	0.00045	0.00000	0.00000	0.00000
9	-0.00518	0.00000	0.00010	0.00000	0.00000	0.00000
10	1.54908	0.00000	-0.09443	0.00000	0.00000	0.00000
17	0.07594	0.10899	0.00831	0.00000	-0.00001	0.00000
45	-0.04329	0.06723	-0.06435	0.00000	-0.00414	0.00000
50	-0.00728	0.13691	0.01353	0.00000	0.00643	0.00000
51	0.30249	0.00000	0.23866	0.00000	0.00000	0.00000
52	0.09667	0.00000	-0.05904	0.00000	0.00000	0.00000
53	0.10332	0.00000	0.10809	0.00000	0.00000	0.00000
54	0.30463	0.00000	0.01521	0.00000	0.00000	0.00000
55	0.14198	0.32775	-0.09861	0.00000	0.00076	0.00000
115	0.11441	0.03668	0.03864	0.00000	0.00000	0.00000
116	0.10966	-0.01054	-0.06653	0.00000	0.00000	0.00000
133	0.11347	0.02990	0.02351	0.00000	0.00000	0.00000
134	0.11288	0.01542	-0.00873	0.00000	0.00000	0.00000
406	0.16797	0.08307	0.23548	0.00000	0.09416	0.00000
409	0.00000	-0.21061	0.00000	0.00000	0.00000	0.00000
410	1.38055	0.83688	-0.38020	0.00000	0.45052	0.00000
414	0.03380	-0.42443	0.00000	0.00000	0.01268	0.00000
518	0.26401	0.02522	0.11578	0.00000	0.09738	0.00000
527	0.04702	0.29639	-0.05562	0.00000	-0.00428	0.00000
578	0.06739	0.33847	0.02895	0.00000	-0.03853	0.00000

SUM	5.62811	1.67833	0.00000	0.00000	0.61496	0.00000

Condition **LC17=0.9D+1.6W120**

6	0.02451	0.02009	0.00005	0.00000	0.00001	0.00000
7	0.78193	0.00000	0.00164	0.00000	0.00000	0.00000
8	0.01312	0.00000	0.00032	0.00000	0.00000	0.00000
9	0.03776	0.00000	0.00007	0.00000	0.00000	0.00000
10	1.57529	0.00000	-0.09524	0.00000	0.00000	0.00000
17	0.05271	0.10614	0.00774	0.00000	-0.00002	0.00000
45	-0.05137	0.08543	-0.07471	0.00000	-0.00413	0.00000
50	-0.00563	0.13546	0.01913	0.00000	0.00597	0.00000
51	0.27666	0.00000	-0.00302	0.00000	0.00000	0.00000
52	0.09545	0.00000	-0.06036	0.00000	0.00000	0.00000
53	0.10307	0.00000	0.09775	0.00000	0.00000	0.00000
54	0.28047	0.00000	-0.24559	0.00000	0.00000	0.00000
55	0.12709	0.33969	-0.11916	0.00000	0.00087	0.00000
115	0.11456	0.04384	0.05458	0.00000	0.00000	0.00000
116	0.10834	-0.02723	-0.10372	0.00000	0.00000	0.00000
133	0.11345	0.03128	0.02658	0.00000	0.00000	0.00000
134	0.11279	0.01238	-0.01554	0.00000	0.00000	0.00000
406	0.03974	0.07645	0.01547	0.00000	0.02576	0.00000
409	0.00000	-0.18877	0.00000	0.00000	0.00000	0.00000
410	1.70935	0.82712	-0.92377	0.00000	0.60366	0.00000
414	0.03380	-0.44023	0.00000	0.00000	0.01268	0.00000
518	-0.04907	0.03348	-0.05717	0.00000	0.01628	0.00000
527	0.04888	0.28266	-0.08110	0.00000	-0.00396	0.00000
578	0.05247	0.34055	-0.01429	0.00000	-0.02432	0.00000
SUM	5.59538	1.67833	-1.57034	0.00000	0.63279	0.00000

Condition **LC18=0.9D+1.6W150**

6	0.01104	0.11838	-0.00446	0.00000	0.00052	0.00000
7	0.24798	0.00000	0.06753	0.00000	0.00000	0.00000
8	-0.03371	0.00000	-0.08543	0.00000	0.00000	0.00000
9	0.04934	0.00000	-0.10483	0.00000	0.00000	0.00000
10	0.16523	0.00000	-0.01372	0.00000	0.00000	0.00000
17	-0.05417	0.28405	-0.06010	0.00000	0.00082	0.00000
45	-0.01682	0.13797	-0.02249	0.00000	-0.00266	0.00000
50	-0.00588	0.13209	0.03299	0.00000	0.00205	0.00000
51	0.08957	0.00000	-0.37929	0.00000	0.00000	0.00000
52	0.00211	0.00000	-0.18415	0.00000	0.00000	0.00000
53	-0.00011	0.00000	-0.18141	0.00000	0.00000	0.00000
54	0.10291	0.00000	-0.64329	0.00000	0.00000	0.00000
55	-0.02970	0.48276	-0.12519	0.00000	0.00026	0.00000
115	0.01208	-0.02003	-0.14621	0.00000	0.00000	0.00000
116	-0.01579	-0.25452	-0.66804	0.00000	0.00000	0.00000
133	0.00604	-0.02150	-0.14834	0.00000	0.00000	0.00000
134	0.00108	-0.08797	-0.29707	0.00000	0.00000	0.00000
406	0.00731	0.07243	0.01094	0.00000	0.01316	0.00000
409	0.00000	-0.18145	-0.05980	0.00000	0.00747	0.00000
410	1.42033	0.81759	-0.67772	0.00000	0.48962	0.00000
414	0.00000	-0.42483	0.00000	0.00000	0.00000	0.00000
518	-0.05102	0.03809	0.00947	0.00000	-0.01676	0.00000
527	-0.00057	0.25849	-0.07441	0.00000	-0.00145	0.00000
578	-0.00541	0.32677	0.00237	0.00000	0.00441	0.00000
SUM	1.90183	1.67833	-3.75264	0.00000	0.49745	0.00000

Condition **LC19=0.9D-1.6W_o**

6	0.04845	0.12552	-0.00376	0.00000	0.00217	0.00000
7	0.34784	0.00000	-0.06409	0.00000	0.00000	0.00000
8	-0.06961	0.00000	-0.08518	0.00000	0.00000	0.00000
9	0.05315	0.00000	-0.10524	0.00000	0.00000	0.00000
10	-0.07494	0.00000	-0.01422	0.00000	0.00000	0.00000
17	-0.21712	0.29290	-0.36704	0.00000	0.00084	0.00000
45	-0.03869	0.14772	-0.01020	0.00000	-0.00307	0.00000
50	-0.00314	0.13250	0.05178	0.00000	0.00135	0.00000
51	0.04543	0.00000	-0.57774	0.00000	0.00000	0.00000
52	0.00036	0.00000	-0.20095	0.00000	0.00000	0.00000
53	-0.00033	0.00000	-0.17597	0.00000	0.00000	0.00000
54	0.05702	0.00000	-0.74644	0.00000	0.00000	0.00000
55	-0.19339	0.49612	-0.40480	0.00000	0.00007	0.00000
115	0.01301	-0.02619	-0.16038	0.00000	0.00000	0.00000
116	-0.01772	-0.27793	-0.72057	0.00000	0.00000	0.00000
133	0.00614	-0.01996	-0.14494	0.00000	0.00000	0.00000
134	0.00052	-0.09893	-0.32188	0.00000	0.00000	0.00000
406	-0.39012	0.08119	-0.68087	0.00000	-0.23556	0.00000
409	0.00000	-0.20473	-0.05980	0.00000	0.00747	0.00000
410	1.24994	0.90432	-1.76310	0.00000	0.53396	0.00000
414	0.00000	-0.60256	0.00000	0.00000	0.00000	0.00000
518	-0.85089	0.03249	-0.50426	0.00000	-0.18272	0.00000
527	0.04301	0.25798	-0.13030	0.00000	-0.00094	0.00000
578	-0.00893	0.43790	-0.12606	0.00000	0.01643	0.00000
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SUM	0.00000	1.67833	-7.31601	0.00000	0.14001	0.00000

Condition **LC20=0.9D-1.6W₃₀**

6	0.04747	0.12455	-0.00379	0.00000	0.00220	0.00000
7	0.19561	0.00000	-0.06581	0.00000	0.00000	0.00000
8	-0.06834	0.00000	-0.08522	0.00000	0.00000	0.00000
9	0.05318	0.00000	-0.10522	0.00000	0.00000	0.00000
10	-0.28117	0.00000	-0.01417	0.00000	0.00000	0.00000
17	-0.22690	0.30053	-0.36642	0.00000	0.00079	0.00000
45	-0.05455	0.15939	0.00197	0.00000	-0.00202	0.00000
50	-0.00012	0.13706	0.06131	0.00000	0.00010	0.00000
51	-0.01459	0.00000	-0.53093	0.00000	0.00000	0.00000
52	-0.00275	0.00000	-0.22526	0.00000	0.00000	0.00000
53	-0.00032	0.00000	-0.22452	0.00000	0.00000	0.00000
54	-0.00568	0.00000	-0.65928	0.00000	0.00000	0.00000
55	-0.19899	0.45575	-0.36178	0.00000	-0.00025	0.00000
115	0.01245	-0.03702	-0.18451	0.00000	0.00000	0.00000
116	-0.01442	-0.24323	-0.64315	0.00000	0.00000	0.00000
133	0.00612	-0.02020	-0.14548	0.00000	0.00000	0.00000
134	0.00057	-0.09801	-0.31983	0.00000	0.00000	0.00000
406	-0.41890	0.11564	-0.69235	0.00000	-0.29220	0.00000
409	0.00000	-0.27497	-0.05980	0.00000	0.00747	0.00000
410	-0.16243	0.90845	-0.95066	0.00000	0.03440	0.00000
414	0.00000	-0.54051	0.00000	0.00000	0.00000	0.00000
518	-0.77958	0.01788	-0.46792	0.00000	-0.16996	0.00000
527	0.02182	0.25091	-0.11622	0.00000	-0.00010	0.00000
578	-0.01032	0.42212	-0.11698	0.00000	0.01655	0.00000
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SUM	-1.90183	1.67833	-6.27602	0.00000	-0.40301	0.00000

Condition **LC21=0.9D-1.6W60**

6	0.00317	0.11197	0.00082	0.00000	0.00003	0.00000
7	-0.44320	0.00000	-0.00225	0.00000	0.00000	0.00000
8	-0.25033	0.00000	0.00247	0.00000	0.00000	0.00000
9	-0.25853	0.00000	-0.00232	0.00000	0.00000	0.00000
10	-1.44184	0.00000	0.09415	0.00000	0.00000	0.00000
17	-0.04981	0.13197	-0.01033	0.00000	0.00009	0.00000
45	-0.20139	0.20180	0.09945	0.00000	0.00311	0.00000
50	0.00218	0.14836	0.09797	0.00000	-0.00557	0.00000
51	-0.25833	0.00000	-0.31891	0.00000	0.00000	0.00000
52	-0.09883	0.00000	-0.14713	0.00000	0.00000	0.00000
53	-0.10179	0.00000	-0.12601	0.00000	0.00000	0.00000
54	-0.24536	0.00000	-0.24181	0.00000	0.00000	0.00000
55	-0.00252	0.13380	0.06408	0.00000	-0.00044	0.00000
115	-0.10835	0.00986	-0.02088	0.00000	0.00000	0.00000
116	-0.10949	0.01457	-0.01020	0.00000	0.00000	0.00000
133	-0.10865	0.01775	-0.00321	0.00000	0.00000	0.00000
134	-0.10961	0.02139	0.00497	0.00000	0.00000	0.00000
406	-0.32842	0.11987	-0.41835	0.00000	-0.25491	0.00000
409	0.00000	-0.28282	0.00000	0.00000	0.00000	0.00000
410	-0.81600	0.86483	-0.21904	0.00000	-0.18688	0.00000
414	-0.03380	-0.43021	0.00000	0.00000	-0.01268	0.00000
518	-0.55070	0.01783	-0.27390	0.00000	-0.14343	0.00000
527	-0.02642	0.23824	-0.07143	0.00000	0.00380	0.00000
578	-0.05738	0.35910	-0.06847	0.00000	0.03493	0.00000
SUM	-5.59538	1.67833	-1.57034	0.00000	-0.56194	0.00000

Condition **LC22=0.9D-1.6W90**

6	0.00950	0.11053	0.00064	0.00000	0.00006	0.00000
7	-0.42944	0.00000	-0.00335	0.00000	0.00000	0.00000
8	-0.19718	0.00000	0.00224	0.00000	0.00000	0.00000
9	-0.15485	0.00000	-0.00231	0.00000	0.00000	0.00000
10	-1.44324	0.00000	0.09351	0.00000	0.00000	0.00000
17	-0.04788	0.14008	-0.01037	0.00000	0.00002	0.00000
45	-0.19796	0.19999	0.12363	0.00000	0.00399	0.00000
50	0.00463	0.15263	0.11385	0.00000	-0.00650	0.00000
51	-0.30482	0.00000	-0.14886	0.00000	0.00000	0.00000
52	-0.10098	0.00000	-0.12948	0.00000	0.00000	0.00000
53	-0.10169	0.00000	-0.11827	0.00000	0.00000	0.00000
54	-0.29219	0.00000	0.00088	0.00000	0.00000	0.00000
55	0.01374	0.10111	0.10594	0.00000	-0.00080	0.00000
115	-0.10887	0.00091	-0.04083	0.00000	0.00000	0.00000
116	-0.10656	0.04627	0.06037	0.00000	0.00000	0.00000
133	-0.10867	0.01829	-0.00201	0.00000	0.00000	0.00000
134	-0.10958	0.02118	0.00449	0.00000	0.00000	0.00000
406	-0.21544	0.12760	-0.22173	0.00000	-0.19796	0.00000
409	0.00000	-0.28743	0.00000	0.00000	0.00000	0.00000
410	-1.34746	0.85479	0.37243	0.00000	-0.40855	0.00000
414	-0.03380	-0.40723	0.00000	0.00000	-0.01268	0.00000
518	-0.27219	0.00978	-0.12057	0.00000	-0.07216	0.00000
527	-0.03834	0.23872	-0.05008	0.00000	0.00446	0.00000
578	-0.04483	0.35110	-0.03014	0.00000	0.02279	0.00000
SUM	-5.62811	1.67833	0.00000	0.00000	-0.66732	0.00000

Condition **LC23=0.9D-1.6W120**

6	0.00302	0.11125	0.00081	0.00000	0.00007	0.00000
7	-0.44795	0.00000	-0.00455	0.00000	0.00000	0.00000
8	-0.25712	0.00000	0.00247	0.00000	0.00000	0.00000
9	-0.25363	0.00000	-0.00232	0.00000	0.00000	0.00000
10	-1.43599	0.00000	0.09423	0.00000	0.00000	0.00000
17	-0.04736	0.14294	-0.00970	0.00000	0.00000	0.00000
45	-0.17719	0.18408	0.13551	0.00000	0.00400	0.00000
50	0.00308	0.15373	0.10728	0.00000	-0.00607	0.00000
51	-0.27962	0.00000	0.06312	0.00000	0.00000	0.00000
52	-0.09979	0.00000	-0.10279	0.00000	0.00000	0.00000
53	-0.10137	0.00000	-0.09188	0.00000	0.00000	0.00000
54	-0.26690	0.00000	0.24995	0.00000	0.00000	0.00000
55	0.02143	0.09011	0.12679	0.00000	-0.00094	0.00000
115	-0.10909	-0.00406	-0.05190	0.00000	0.00000	0.00000
116	-0.10521	0.06223	0.09593	0.00000	0.00000	0.00000
133	-0.10866	0.01756	-0.00363	0.00000	0.00000	0.00000
134	-0.10954	0.02227	0.00693	0.00000	0.00000	0.00000
406	-0.08708	0.13432	-0.00164	0.00000	-0.12957	0.00000
409	0.00000	-0.30941	0.00000	0.00000	0.00000	0.00000
410	-1.67646	0.86423	0.91605	0.00000	-0.56180	0.00000
414	-0.03380	-0.39236	0.00000	0.00000	-0.01268	0.00000
518	0.04085	0.00199	0.05229	0.00000	0.00906	0.00000
527	-0.03720	0.24961	-0.02567	0.00000	0.00416	0.00000
578	-0.02980	0.34982	0.01307	0.00000	0.00849	0.00000
SUM	-5.59538	1.67833	1.57034	0.00000	-0.68528	0.00000

Condition **LC24=0.9D-1.6W150**

6	0.01592	0.01315	0.00531	0.00000	-0.00043	0.00000
7	-0.07715	0.00000	-0.07024	0.00000	0.00000	0.00000
8	-0.11844	0.00000	0.08812	0.00000	0.00000	0.00000
9	-0.12205	0.00000	0.10249	0.00000	0.00000	0.00000
10	-0.11580	0.00000	0.01355	0.00000	0.00000	0.00000
17	0.04600	-0.03714	0.05846	0.00000	-0.00084	0.00000
45	-0.14205	0.12503	-0.00417	0.00000	0.00264	0.00000
50	0.00348	0.15823	0.09398	0.00000	-0.00220	0.00000
51	-0.09204	0.00000	0.62202	0.00000	0.00000	0.00000
52	-0.00653	0.00000	-0.05751	0.00000	0.00000	0.00000
53	0.00213	0.00000	0.05571	0.00000	0.00000	0.00000
54	-0.09023	0.00000	0.72492	0.00000	0.00000	0.00000
55	0.14636	-0.05097	0.13226	0.00000	-0.00029	0.00000
115	-0.00667	0.05847	0.14588	0.00000	0.00000	0.00000
116	0.01801	0.29026	0.66064	0.00000	0.00000	0.00000
133	-0.00128	0.06958	0.16957	0.00000	0.00000	0.00000
134	0.00204	0.12336	0.29001	0.00000	0.00000	0.00000
406	-0.05467	0.13836	0.00286	0.00000	-0.11697	0.00000
409	0.00000	-0.31658	0.05980	0.00000	-0.00747	0.00000
410	-1.38741	0.87380	0.66998	0.00000	-0.44773	0.00000
414	0.00000	-0.40794	0.00000	0.00000	0.00000	0.00000
518	0.04281	-0.00270	-0.01432	0.00000	0.04207	0.00000
527	0.00768	0.27974	0.00690	0.00000	0.00162	0.00000
578	0.02805	0.36366	-0.00358	0.00000	-0.02021	0.00000
SUM	-1.90183	1.67833	3.75264	0.00000	-0.54982	0.00000

Condition **LC25=1.2D+Di+W10**

6	0.03714	0.18665	0.00147	0.00000	0.00011	0.00000
7	0.07843	0.00000	-0.00513	0.00000	0.00000	0.00000
8	-0.08569	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04356	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.02798	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00813	0.38499	-0.00164	0.00000	0.00002	0.00000
45	-0.23046	0.37215	0.04747	0.00000	0.00003	0.00000
50	-0.00346	0.38218	0.17275	0.00000	-0.00028	0.00000
51	-0.00495	0.00000	0.11846	0.00000	0.00000	0.00000
52	-0.00661	0.00000	-0.20596	0.00000	0.00000	0.00000
53	0.00261	0.00000	0.07078	0.00000	0.00000	0.00000
54	0.01102	0.00000	0.02242	0.00000	0.00000	0.00000
55	0.15798	0.57268	0.01181	0.00000	0.00000	0.00000
115	0.00821	0.05499	-0.00580	0.00000	0.00000	0.00000
116	0.00506	0.05980	0.00518	0.00000	0.00000	0.00000
133	0.00717	0.07272	0.03379	0.00000	0.00000	0.00000
134	0.00478	0.05316	-0.00967	0.00000	0.00000	0.00000
406	-0.02708	0.31483	0.08605	0.00000	-0.12795	0.00000
409	0.00000	-0.68360	0.00000	0.00000	0.00000	0.00000
410	-0.08207	2.26652	0.15240	0.00000	-0.00084	0.00000
414	0.00000	-1.24216	0.00000	0.00000	0.00000	0.00000
518	0.07273	0.04432	0.03964	0.00000	0.05808	0.00000
527	-0.00495	0.75489	-0.12721	0.00000	0.00025	0.00000
578	0.03642	1.00496	0.00991	0.00000	-0.02644	0.00000
SUM	0.00000	4.59910	0.41600	0.00000	-0.09702	0.00000

Condition **LC26=1.2D+Di+W130**

6	0.03723	0.18682	0.00147	0.00000	0.00010	0.00000
7	0.09570	0.00000	-0.00487	0.00000	0.00000	0.00000
8	-0.08073	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04767	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00448	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00990	0.38376	-0.00171	0.00000	0.00003	0.00000
45	-0.22656	0.37003	0.04518	0.00000	-0.00014	0.00000
50	-0.00402	0.38153	0.16964	0.00000	-0.00008	0.00000
51	0.00531	0.00000	0.11203	0.00000	0.00000	0.00000
52	-0.00613	0.00000	-0.20443	0.00000	0.00000	0.00000
53	0.00262	0.00000	0.07266	0.00000	0.00000	0.00000
54	0.02146	0.00000	0.00948	0.00000	0.00000	0.00000
55	0.16080	0.57900	0.00525	0.00000	0.00005	0.00000
115	0.00830	0.05655	-0.00234	0.00000	0.00000	0.00000
116	0.00458	0.05457	-0.00647	0.00000	0.00000	0.00000
133	0.00717	0.07273	0.03381	0.00000	0.00000	0.00000
134	0.00478	0.05310	-0.00979	0.00000	0.00000	0.00000
406	-0.02323	0.31048	0.08779	0.00000	-0.12057	0.00000
409	0.00000	-0.67575	0.00000	0.00000	0.00000	0.00000
410	0.10144	2.26854	0.04688	0.00000	0.06455	0.00000
414	0.00000	-1.25396	0.00000	0.00000	0.00000	0.00000
518	0.06332	0.04605	0.03482	0.00000	0.05647	0.00000
527	-0.00205	0.75613	-0.12867	0.00000	0.00011	0.00000
578	0.03666	1.00952	0.00870	0.00000	-0.02650	0.00000
SUM	0.26870	4.59910	0.26870	0.00000	-0.02597	0.00000

Condition **LC27=1.2D+Di+W160**

6	0.03723	0.18684	0.00147	0.00000	0.00010	0.00000
7	0.09561	0.00000	-0.00481	0.00000	0.00000	0.00000
8	-0.08058	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04743	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00288	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00982	0.38342	-0.00171	0.00000	0.00003	0.00000
45	-0.22793	0.36977	0.04618	0.00000	-0.00017	0.00000
50	-0.00409	0.38141	0.16932	0.00000	-0.00005	0.00000
51	0.00652	0.00000	0.11221	0.00000	0.00000	0.00000
52	-0.00606	0.00000	-0.20424	0.00000	0.00000	0.00000
53	0.00261	0.00000	0.07284	0.00000	0.00000	0.00000
54	0.02271	0.00000	0.01060	0.00000	0.00000	0.00000
55	0.15989	0.58025	0.00356	0.00000	0.00006	0.00000
115	0.00832	0.05694	-0.00146	0.00000	0.00000	0.00000
116	0.00446	0.05327	-0.00937	0.00000	0.00000	0.00000
133	0.00717	0.07273	0.03382	0.00000	0.00000	0.00000
134	0.00477	0.05308	-0.00984	0.00000	0.00000	0.00000
406	-0.03552	0.31112	0.06845	0.00000	-0.12869	0.00000
409	0.00000	-0.67764	0.00000	0.00000	0.00000	0.00000
410	0.08817	2.27140	0.03396	0.00000	0.06163	0.00000
414	0.00000	-1.25891	0.00000	0.00000	0.00000	0.00000
518	0.04465	0.04614	0.02442	0.00000	0.05147	0.00000
527	-0.00168	0.75650	-0.12874	0.00000	0.00009	0.00000
578	0.03564	1.01277	0.00610	0.00000	-0.02556	0.00000
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SUM	0.22203	4.59910	0.22203	0.00000	-0.04107	0.00000

Condition **LC28=1.2D+Di+W190**

6	0.03727	0.18696	0.00147	0.00000	0.00010	0.00000
7	0.10380	0.00000	-0.00457	0.00000	0.00000	0.00000
8	-0.07814	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04742	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.01545	0.00000	-0.00180	0.00000	0.00000	0.00000
17	0.01057	0.38220	-0.00174	0.00000	0.00004	0.00000
45	-0.22927	0.37015	0.04364	0.00000	-0.00030	0.00000
50	-0.00441	0.38070	0.16722	0.00000	0.00009	0.00000
51	0.01285	0.00000	0.08139	0.00000	0.00000	0.00000
52	-0.00576	0.00000	-0.20308	0.00000	0.00000	0.00000
53	0.00258	0.00000	0.07285	0.00000	0.00000	0.00000
54	0.02928	0.00000	-0.02654	0.00000	0.00000	0.00000
55	0.15954	0.58555	-0.00294	0.00000	0.00012	0.00000
115	0.00840	0.05845	0.00191	0.00000	0.00000	0.00000
116	0.00400	0.04821	-0.02065	0.00000	0.00000	0.00000
133	0.00717	0.07274	0.03385	0.00000	0.00000	0.00000
134	0.00477	0.05301	-0.00999	0.00000	0.00000	0.00000
406	-0.04986	0.30996	0.04322	0.00000	-0.13564	0.00000
409	0.00000	-0.67686	0.00000	0.00000	0.00000	0.00000
410	0.16511	2.27255	-0.04898	0.00000	0.09354	0.00000
414	0.00000	-1.26268	0.00000	0.00000	0.00000	0.00000
518	0.00867	0.04749	0.00461	0.00000	0.04235	0.00000
527	0.00048	0.75625	-0.13207	0.00000	0.00000	0.00000
578	0.03409	1.01442	0.00115	0.00000	-0.02404	0.00000
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SUM	0.28400	4.59910	0.00000	0.00000	-0.02375	0.00000

Condition **LC29=1.2D+Di+W1120**

6	0.03726	0.18696	0.00147	0.00000	0.00010	0.00000
7	0.09742	0.00000	-0.00443	0.00000	0.00000	0.00000
8	-0.07959	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04470	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00307	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00960	0.38163	-0.00184	0.00000	0.00005	0.00000
45	-0.23293	0.37307	0.04182	0.00000	-0.00031	0.00000
50	-0.00421	0.38043	0.16769	0.00000	0.00003	0.00000
51	0.00972	0.00000	0.04508	0.00000	0.00000	0.00000
52	-0.00591	0.00000	-0.20307	0.00000	0.00000	0.00000
53	0.00255	0.00000	0.07074	0.00000	0.00000	0.00000
54	0.02623	0.00000	-0.06506	0.00000	0.00000	0.00000
55	0.15666	0.58736	-0.00656	0.00000	0.00015	0.00000
115	0.00844	0.05921	0.00359	0.00000	0.00000	0.00000
116	0.00376	0.04553	-0.02662	0.00000	0.00000	0.00000
133	0.00717	0.07276	0.03389	0.00000	0.00000	0.00000
134	0.00476	0.05294	-0.01015	0.00000	0.00000	0.00000
406	-0.06811	0.30927	0.01215	0.00000	-0.14558	0.00000
409	0.00000	-0.67410	0.00000	0.00000	0.00000	0.00000
410	0.20233	2.27115	-0.12180	0.00000	0.11194	0.00000
414	0.00000	-1.26575	0.00000	0.00000	0.00000	0.00000
518	-0.03336	0.04881	-0.01863	0.00000	0.03145	0.00000
527	0.00038	0.75432	-0.13490	0.00000	0.00004	0.00000
578	0.03207	1.01551	-0.00466	0.00000	-0.02212	0.00000

SUM	0.22203	4.59910	-0.22203	0.00000	-0.02427	0.00000

Condition **LC30=1.2D+Di+W1150**

6	0.03726	0.18697	0.00147	0.00000	0.00010	0.00000
7	0.09816	0.00000	-0.00438	0.00000	0.00000	0.00000
8	-0.07944	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.04421	0.00000	-0.00332	0.00000	0.00000	0.00000
10	0.00537	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00960	0.38148	-0.00191	0.00000	0.00005	0.00000
45	-0.23265	0.37311	0.04229	0.00000	-0.00031	0.00000
50	-0.00416	0.38043	0.16807	0.00000	0.00001	0.00000
51	0.00877	0.00000	0.04499	0.00000	0.00000	0.00000
52	-0.00594	0.00000	-0.20323	0.00000	0.00000	0.00000
53	0.00254	0.00000	0.07040	0.00000	0.00000	0.00000
54	0.02531	0.00000	-0.06405	0.00000	0.00000	0.00000
55	0.15698	0.58818	-0.00775	0.00000	0.00015	0.00000
115	0.00845	0.05944	0.00411	0.00000	0.00000	0.00000
116	0.00368	0.04462	-0.02864	0.00000	0.00000	0.00000
133	0.00717	0.07277	0.03390	0.00000	0.00000	0.00000
134	0.00476	0.05292	-0.01019	0.00000	0.00000	0.00000
406	-0.06964	0.30774	0.00833	0.00000	-0.14491	0.00000
409	0.00000	-0.67057	0.00000	0.00000	0.00000	0.00000
410	0.25652	2.27101	-0.15836	0.00000	0.13137	0.00000
414	0.00000	-1.26969	0.00000	0.00000	0.00000	0.00000
518	-0.04059	0.04946	-0.02253	0.00000	0.02978	0.00000
527	0.00042	0.75429	-0.13484	0.00000	0.00005	0.00000
578	0.03190	1.01692	-0.00563	0.00000	-0.02192	0.00000

SUM	0.26870	4.59910	-0.26870	0.00000	-0.00563	0.00000

Condition **LC31=1.2D+Di-WI0**

6	0.03720	0.18690	0.00147	0.00000	0.00009	0.00000
7	0.08225	0.00000	-0.00435	0.00000	0.00000	0.00000
8	-0.08365	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03844	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.02636	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00763	0.38141	-0.00197	0.00000	0.00005	0.00000
45	-0.23974	0.37633	0.04435	0.00000	-0.00025	0.00000
50	-0.00367	0.38056	0.17064	0.00000	-0.00014	0.00000
51	0.00011	0.00000	0.02475	0.00000	0.00000	0.00000
52	-0.00633	0.00000	-0.20431	0.00000	0.00000	0.00000
53	0.00250	0.00000	0.06741	0.00000	0.00000	0.00000
54	0.01665	0.00000	-0.07900	0.00000	0.00000	0.00000
55	0.15211	0.58714	-0.00862	0.00000	0.00016	0.00000
115	0.00845	0.05954	0.00434	0.00000	0.00000	0.00000
116	0.00365	0.04415	-0.02969	0.00000	0.00000	0.00000
133	0.00717	0.07279	0.03394	0.00000	0.00000	0.00000
134	0.00476	0.05287	-0.01030	0.00000	0.00000	0.00000
406	-0.10317	0.31027	-0.04396	0.00000	-0.16789	0.00000
409	0.00000	-0.67497	0.00000	0.00000	0.00000	0.00000
410	0.17010	2.27737	-0.17739	0.00000	0.10700	0.00000
414	0.00000	-1.28314	0.00000	0.00000	0.00000	0.00000
518	-0.09568	0.04951	-0.05332	0.00000	0.01488	0.00000
527	-0.00116	0.75252	-0.13588	0.00000	0.00015	0.00000
578	0.02874	1.02586	-0.01333	0.00000	-0.01904	0.00000
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SUM	0.00000	4.59910	-0.41600	0.00000	-0.06499	0.00000

Condition **LC32=1.2D+Di-WI30**

6	0.03712	0.18674	0.00147	0.00000	0.00010	0.00000
7	0.06498	0.00000	-0.00460	0.00000	0.00000	0.00000
8	-0.08861	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03433	0.00000	-0.00332	0.00000	0.00000	0.00000
10	-0.05882	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00585	0.38264	-0.00190	0.00000	0.00004	0.00000
45	-0.24364	0.37844	0.04663	0.00000	-0.00009	0.00000
50	-0.00310	0.38122	0.17375	0.00000	-0.00035	0.00000
51	-0.01015	0.00000	0.03119	0.00000	0.00000	0.00000
52	-0.00682	0.00000	-0.20585	0.00000	0.00000	0.00000
53	0.00249	0.00000	0.06553	0.00000	0.00000	0.00000
54	0.00620	0.00000	-0.06605	0.00000	0.00000	0.00000
55	0.14929	0.58083	-0.00207	0.00000	0.00011	0.00000
115	0.00836	0.05799	0.00088	0.00000	0.00000	0.00000
116	0.00413	0.04937	-0.01806	0.00000	0.00000	0.00000
133	0.00717	0.07278	0.03392	0.00000	0.00000	0.00000
134	0.00476	0.05293	-0.01018	0.00000	0.00000	0.00000
406	-0.10702	0.31462	-0.04570	0.00000	-0.17527	0.00000
409	0.00000	-0.68284	0.00000	0.00000	0.00000	0.00000
410	-0.01340	2.27538	-0.07187	0.00000	0.04162	0.00000
414	0.00000	-1.27130	0.00000	0.00000	0.00000	0.00000
518	-0.08627	0.04776	-0.04850	0.00000	0.01649	0.00000
527	-0.00407	0.75128	-0.13442	0.00000	0.00029	0.00000
578	0.02850	1.02127	-0.01212	0.00000	-0.01898	0.00000
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SUM	-0.26870	4.59910	-0.26870	0.00000	-0.13605	0.00000

Condition **LC33=1.2D+Di-WI60**

6	0.03712	0.18672	0.00147	0.00000	0.00010	0.00000
7	0.06508	0.00000	-0.00466	0.00000	0.00000	0.00000
8	-0.08875	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03457	0.00000	-0.00331	0.00000	0.00000	0.00000
10	-0.05721	0.00000	-0.00181	0.00000	0.00000	0.00000
17	0.00593	0.38298	-0.00190	0.00000	0.00004	0.00000
45	-0.24227	0.37870	0.04563	0.00000	-0.00006	0.00000
50	-0.00303	0.38134	0.17408	0.00000	-0.00038	0.00000
51	-0.01136	0.00000	0.03100	0.00000	0.00000	0.00000
52	-0.00688	0.00000	-0.20603	0.00000	0.00000	0.00000
53	0.00250	0.00000	0.06535	0.00000	0.00000	0.00000
54	0.00495	0.00000	-0.06718	0.00000	0.00000	0.00000
55	0.15019	0.57958	-0.00037	0.00000	0.00009	0.00000
115	0.00835	0.05760	-0.00001	0.00000	0.00000	0.00000
116	0.00424	0.05067	-0.01516	0.00000	0.00000	0.00000
133	0.00717	0.07277	0.03391	0.00000	0.00000	0.00000
134	0.00476	0.05295	-0.01013	0.00000	0.00000	0.00000
406	-0.09474	0.31398	-0.02636	0.00000	-0.16715	0.00000
409	0.00000	-0.68095	0.00000	0.00000	0.00000	0.00000
410	-0.00012	2.27252	-0.05895	0.00000	0.04453	0.00000
414	0.00000	-1.26635	0.00000	0.00000	0.00000	0.00000
518	-0.06760	0.04766	-0.03810	0.00000	0.02149	0.00000
527	-0.00445	0.75091	-0.13435	0.00000	0.00031	0.00000
578	0.02952	1.01802	-0.00952	0.00000	-0.01992	0.00000
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SUM	-0.22203	4.59910	-0.22203	0.00000	-0.12095	0.00000

Condition **LC34=1.2D+Di-WI90**

6	0.03707	0.18660	0.00147	0.00000	0.00010	0.00000
7	0.05764	0.00000	-0.00490	0.00000	0.00000	0.00000
8	-0.09125	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03321	0.00000	-0.00331	0.00000	0.00000	0.00000
10	-0.06900	0.00000	-0.00180	0.00000	0.00000	0.00000
17	0.00532	0.38421	-0.00187	0.00000	0.00003	0.00000
45	-0.24154	0.37836	0.04860	0.00000	0.00008	0.00000
50	-0.00271	0.38205	0.17618	0.00000	-0.00051	0.00000
51	-0.01768	0.00000	0.06153	0.00000	0.00000	0.00000
52	-0.00718	0.00000	-0.20719	0.00000	0.00000	0.00000
53	0.00253	0.00000	0.06539	0.00000	0.00000	0.00000
54	-0.00160	0.00000	-0.03005	0.00000	0.00000	0.00000
55	0.15085	0.57423	0.00615	0.00000	0.00004	0.00000
115	0.00827	0.05607	-0.00340	0.00000	0.00000	0.00000
116	0.00471	0.05576	-0.00384	0.00000	0.00000	0.00000
133	0.00717	0.07276	0.03388	0.00000	0.00000	0.00000
134	0.00477	0.05303	-0.00997	0.00000	0.00000	0.00000
406	-0.08039	0.31514	-0.00113	0.00000	-0.16021	0.00000
409	0.00000	-0.68175	0.00000	0.00000	0.00000	0.00000
410	-0.07707	2.27137	0.02398	0.00000	0.01263	0.00000
414	0.00000	-1.26256	0.00000	0.00000	0.00000	0.00000
518	-0.03161	0.04632	-0.01828	0.00000	0.03061	0.00000
527	-0.00657	0.75115	-0.13123	0.00000	0.00040	0.00000
578	0.03107	1.01636	-0.00457	0.00000	-0.02144	0.00000
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SUM	-0.28400	4.59910	0.00000	0.00000	-0.13827	0.00000

Condition **LC35=1.2D+Di-WI120**

6	0.03709	0.18660	0.00147	0.00000	0.00011	0.00000
7	0.06356	0.00000	-0.00504	0.00000	0.00000	0.00000
8	-0.08977	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03674	0.00000	-0.00331	0.00000	0.00000	0.00000
10	-0.05709	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00621	0.38477	-0.00177	0.00000	0.00003	0.00000
45	-0.23752	0.37542	0.05018	0.00000	0.00009	0.00000
50	-0.00291	0.38232	0.17569	0.00000	-0.00045	0.00000
51	-0.01456	0.00000	0.09801	0.00000	0.00000	0.00000
52	-0.00704	0.00000	-0.20719	0.00000	0.00000	0.00000
53	0.00256	0.00000	0.06747	0.00000	0.00000	0.00000
54	0.00145	0.00000	0.00847	0.00000	0.00000	0.00000
55	0.15355	0.57244	0.00975	0.00000	0.00001	0.00000
115	0.00823	0.05532	-0.00506	0.00000	0.00000	0.00000
116	0.00494	0.05843	0.00211	0.00000	0.00000	0.00000
133	0.00717	0.07274	0.03384	0.00000	0.00000	0.00000
134	0.00478	0.05309	-0.00982	0.00000	0.00000	0.00000
406	-0.06215	0.31584	0.02994	0.00000	-0.15027	0.00000
409	0.00000	-0.68450	0.00000	0.00000	0.00000	0.00000
410	-0.11429	2.27276	0.09681	0.00000	-0.00578	0.00000
414	0.00000	-1.25951	0.00000	0.00000	0.00000	0.00000
518	0.01041	0.04500	0.00495	0.00000	0.04152	0.00000
527	-0.00647	0.75308	-0.12827	0.00000	0.00036	0.00000
578	0.03309	1.01529	0.00124	0.00000	-0.02336	0.00000
SUM	-0.22203	4.59910	0.22203	0.00000	-0.13775	0.00000

Condition **LC36=1.2D+Di-WI150**

6	0.03708	0.18658	0.00147	0.00000	0.00011	0.00000
7	0.06268	0.00000	-0.00510	0.00000	0.00000	0.00000
8	-0.08990	0.00000	0.00437	0.00000	0.00000	0.00000
9	0.03748	0.00000	-0.00331	0.00000	0.00000	0.00000
10	-0.05953	0.00000	-0.00179	0.00000	0.00000	0.00000
17	0.00618	0.38492	-0.00170	0.00000	0.00002	0.00000
45	-0.23769	0.37537	0.04963	0.00000	0.00009	0.00000
50	-0.00296	0.38231	0.17532	0.00000	-0.00044	0.00000
51	-0.01361	0.00000	0.09815	0.00000	0.00000	0.00000
52	-0.00700	0.00000	-0.20703	0.00000	0.00000	0.00000
53	0.00257	0.00000	0.06780	0.00000	0.00000	0.00000
54	0.00237	0.00000	0.00747	0.00000	0.00000	0.00000
55	0.15318	0.57163	0.01094	0.00000	0.00000	0.00000
115	0.00821	0.05509	-0.00558	0.00000	0.00000	0.00000
116	0.00502	0.05934	0.00413	0.00000	0.00000	0.00000
133	0.00717	0.07274	0.03383	0.00000	0.00000	0.00000
134	0.00478	0.05311	-0.00978	0.00000	0.00000	0.00000
406	-0.06061	0.31737	0.03376	0.00000	-0.15094	0.00000
409	0.00000	-0.68805	0.00000	0.00000	0.00000	0.00000
410	-0.16848	2.27291	0.13337	0.00000	-0.02521	0.00000
414	0.00000	-1.25558	0.00000	0.00000	0.00000	0.00000
518	0.01764	0.04436	0.00885	0.00000	0.04318	0.00000
527	-0.00653	0.75312	-0.12829	0.00000	0.00035	0.00000
578	0.03326	1.01388	0.00221	0.00000	-0.02357	0.00000
SUM	-0.26870	4.59910	0.26870	0.00000	-0.15640	0.00000

Condition **LC37=0.9D**

6	0.01240	0.06509	0.00039	0.00000	0.00003	0.00000
7	0.02622	0.00000	-0.00139	0.00000	0.00000	0.00000
8	-0.02993	0.00000	0.00133	0.00000	0.00000	0.00000
9	0.01325	0.00000	-0.00110	0.00000	0.00000	0.00000
10	-0.00905	0.00000	-0.00045	0.00000	0.00000	0.00000
17	0.00354	0.12393	-0.00054	0.00000	0.00001	0.00000
45	-0.08869	0.13889	0.01752	0.00000	-0.00004	0.00000
50	-0.00123	0.14494	0.06364	0.00000	-0.00008	0.00000
51	-0.00146	0.00000	0.02140	0.00000	0.00000	0.00000
52	-0.00219	0.00000	-0.07456	0.00000	0.00000	0.00000
53	0.00092	0.00000	0.02672	0.00000	0.00000	0.00000
54	0.00521	0.00000	-0.01171	0.00000	0.00000	0.00000
55	0.06297	0.21572	0.00083	0.00000	0.00004	0.00000
115	0.00276	0.01926	-0.00006	0.00000	0.00000	0.00000
116	0.00149	0.01721	-0.00454	0.00000	0.00000	0.00000
133	0.00239	0.02423	0.01104	0.00000	0.00000	0.00000
134	0.00162	0.01784	-0.00316	0.00000	0.00000	0.00000
406	-0.02364	0.10511	0.00685	0.00000	-0.05178	0.00000
409	0.00000	-0.24819	0.00000	0.00000	0.00000	0.00000
410	0.01642	0.84540	-0.00384	0.00000	0.02095	0.00000
414	0.00000	-0.41632	0.00000	0.00000	0.00000	0.00000
518	-0.00407	0.01759	-0.00240	0.00000	0.01261	0.00000
527	-0.00022	0.26261	-0.04537	0.00000	0.00007	0.00000
578	0.01128	0.34502	-0.00060	0.00000	-0.00787	0.00000
SUM	0.00000	1.67833	0.00000	0.00000	-0.02606	0.00000

Condition **LC38=1.2D**

6	0.01653	0.08679	0.00052	0.00000	0.00005	0.00000
7	0.03497	0.00000	-0.00186	0.00000	0.00000	0.00000
8	-0.03991	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01767	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.01206	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00471	0.16524	-0.00072	0.00000	0.00002	0.00000
45	-0.11826	0.18519	0.02336	0.00000	-0.00005	0.00000
50	-0.00164	0.19325	0.08485	0.00000	-0.00011	0.00000
51	-0.00194	0.00000	0.02853	0.00000	0.00000	0.00000
52	-0.00293	0.00000	-0.09941	0.00000	0.00000	0.00000
53	0.00122	0.00000	0.03563	0.00000	0.00000	0.00000
54	0.00695	0.00000	-0.01562	0.00000	0.00000	0.00000
55	0.08397	0.28763	0.00111	0.00000	0.00005	0.00000
115	0.00368	0.02568	-0.00008	0.00000	0.00000	0.00000
116	0.00199	0.02295	-0.00606	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01472	0.00000	0.00000	0.00000
134	0.00216	0.02378	-0.00421	0.00000	0.00000	0.00000
406	-0.03151	0.14013	0.00913	0.00000	-0.06904	0.00000
409	0.00000	-0.33088	0.00000	0.00000	0.00000	0.00000
410	0.02190	1.12718	-0.00512	0.00000	0.02793	0.00000
414	0.00000	-0.55507	0.00000	0.00000	0.00000	0.00000
518	-0.00542	0.02344	-0.00320	0.00000	0.01682	0.00000
527	-0.00030	0.35015	-0.06050	0.00000	0.00010	0.00000
578	0.01504	0.46001	-0.00080	0.00000	-0.01050	0.00000
SUM	0.00000	2.23777	0.00000	0.00000	-0.03475	0.00000

Condition **LC41=1.2D+WL0**

6	0.01652	0.08675	0.00052	0.00000	0.00005	0.00000
7	0.03436	0.00000	-0.00198	0.00000	0.00000	0.00000
8	-0.04022	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01853	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.01242	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00480	0.16579	-0.00066	0.00000	0.00001	0.00000
45	-0.11680	0.18465	0.02355	0.00000	-0.00001	0.00000
50	-0.00161	0.19350	0.08516	0.00000	-0.00013	0.00000
51	-0.00268	0.00000	0.04162	0.00000	0.00000	0.00000
52	-0.00297	0.00000	-0.09965	0.00000	0.00000	0.00000
53	0.00124	0.00000	0.03609	0.00000	0.00000	0.00000
54	0.00612	0.00000	-0.00178	0.00000	0.00000	0.00000
55	0.08479	0.28535	0.00435	0.00000	0.00002	0.00000
115	0.00365	0.02496	-0.00167	0.00000	0.00000	0.00000
116	0.00221	0.02542	-0.00055	0.00000	0.00000	0.00000
133	0.00319	0.03229	0.01470	0.00000	0.00000	0.00000
134	0.00216	0.02383	-0.00411	0.00000	0.00000	0.00000
406	-0.01985	0.14085	0.02910	0.00000	-0.06292	0.00000
409	0.00000	-0.33220	0.00000	0.00000	0.00000	0.00000
410	-0.01700	1.12541	0.04693	0.00000	0.01111	0.00000
414	0.00000	-0.54920	0.00000	0.00000	0.00000	0.00000
518	0.02062	0.02279	0.01117	0.00000	0.02349	0.00000
527	-0.00088	0.35042	-0.05930	0.00000	0.00011	0.00000
578	0.01622	0.45715	0.00279	0.00000	-0.01164	0.00000
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SUM	0.00000	2.23777	0.12600	0.00000	-0.03990	0.00000

Condition **LC42=1.2D+WL30**

6	0.01655	0.08680	0.00052	0.00000	0.00005	0.00000
7	0.03939	0.00000	-0.00189	0.00000	0.00000	0.00000
8	-0.03877	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01961	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.00313	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00529	0.16539	-0.00069	0.00000	0.00001	0.00000
45	-0.11605	0.18400	0.02326	0.00000	-0.00006	0.00000
50	-0.00176	0.19329	0.08436	0.00000	-0.00007	0.00000
51	0.00015	0.00000	0.03978	0.00000	0.00000	0.00000
52	-0.00283	0.00000	-0.09926	0.00000	0.00000	0.00000
53	0.00124	0.00000	0.03654	0.00000	0.00000	0.00000
54	0.00902	0.00000	-0.00487	0.00000	0.00000	0.00000
55	0.08566	0.28740	0.00211	0.00000	0.00004	0.00000
115	0.00368	0.02548	-0.00052	0.00000	0.00000	0.00000
116	0.00205	0.02365	-0.00448	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01471	0.00000	0.00000	0.00000
134	0.00216	0.02380	-0.00415	0.00000	0.00000	0.00000
406	-0.01843	0.13949	0.02989	0.00000	-0.06045	0.00000
409	0.00000	-0.32926	0.00000	0.00000	0.00000	0.00000
410	0.03933	1.12509	0.01299	0.00000	0.03135	0.00000
414	0.00000	-0.55157	0.00000	0.00000	0.00000	0.00000
518	0.01796	0.02335	0.00982	0.00000	0.02305	0.00000
527	0.00001	0.35085	-0.05967	0.00000	0.00007	0.00000
578	0.01630	0.45771	0.00245	0.00000	-0.01166	0.00000
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SUM	0.08061	2.23777	0.08061	0.00000	-0.01767	0.00000

Condition **LC43=1.2D+WL60**

6	0.01655	0.08681	0.00052	0.00000	0.00005	0.00000
7	0.03921	0.00000	-0.00189	0.00000	0.00000	0.00000
8	-0.03879	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01950	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.00360	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00526	0.16533	-0.00069	0.00000	0.00001	0.00000
45	-0.11613	0.18399	0.02328	0.00000	-0.00006	0.00000
50	-0.00181	0.19328	0.08402	0.00000	-0.00006	0.00000
51	0.00073	0.00000	0.04022	0.00000	0.00000	0.00000
52	-0.00280	0.00000	-0.09907	0.00000	0.00000	0.00000
53	0.00125	0.00000	0.03686	0.00000	0.00000	0.00000
54	0.00958	0.00000	-0.00482	0.00000	0.00000	0.00000
55	0.08536	0.28760	0.00183	0.00000	0.00004	0.00000
115	0.00368	0.02555	-0.00036	0.00000	0.00000	0.00000
116	0.00203	0.02344	-0.00496	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01471	0.00000	0.00000	0.00000
134	0.00216	0.02380	-0.00416	0.00000	0.00000	0.00000
406	-0.02217	0.13966	0.02395	0.00000	-0.06289	0.00000
409	0.00000	-0.32956	0.00000	0.00000	0.00000	0.00000
410	0.03548	1.12532	0.00912	0.00000	0.03055	0.00000
414	0.00000	-0.55204	0.00000	0.00000	0.00000	0.00000
518	0.01174	0.02339	0.00636	0.00000	0.02139	0.00000
527	0.00008	0.35088	-0.05975	0.00000	0.00007	0.00000
578	0.01596	0.45803	0.00159	0.00000	-0.01135	0.00000

SUM	0.06647	2.23777	0.06647	0.00000	-0.02226	0.00000

Condition **LC44=1.2D+WL90**

6	0.01656	0.08684	0.00052	0.00000	0.00004	0.00000
7	0.04133	0.00000	-0.00181	0.00000	0.00000	0.00000
8	-0.03803	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01996	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.00061	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00543	0.16492	-0.00069	0.00000	0.00002	0.00000
45	-0.11662	0.18398	0.02264	0.00000	-0.00011	0.00000
50	-0.00191	0.19304	0.08334	0.00000	-0.00002	0.00000
51	0.00286	0.00000	0.03152	0.00000	0.00000	0.00000
52	-0.00270	0.00000	-0.09870	0.00000	0.00000	0.00000
53	0.00124	0.00000	0.03689	0.00000	0.00000	0.00000
54	0.01179	0.00000	-0.01521	0.00000	0.00000	0.00000
55	0.08500	0.28931	-0.00025	0.00000	0.00006	0.00000
115	0.00370	0.02604	0.00073	0.00000	0.00000	0.00000
116	0.00188	0.02182	-0.00857	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01472	0.00000	0.00000	0.00000
134	0.00216	0.02378	-0.00422	0.00000	0.00000	0.00000
406	-0.02682	0.13934	0.01595	0.00000	-0.06525	0.00000
409	0.00000	-0.33000	0.00000	0.00000	0.00000	0.00000
410	0.05872	1.12727	-0.01623	0.00000	0.04023	0.00000
414	0.00000	-0.55523	0.00000	0.00000	0.00000	0.00000
518	0.00062	0.02364	0.00023	0.00000	0.01857	0.00000
527	0.00077	0.35092	-0.06062	0.00000	0.00003	0.00000
578	0.01549	0.45979	0.00006	0.00000	-0.01088	0.00000

SUM	0.08400	2.23777	0.00000	0.00000	-0.01731	0.00000

Condition **LC45=1.2D+WL120**

6	0.01656	0.08684	0.00052	0.00000	0.00004	0.00000
7	0.03966	0.00000	-0.00177	0.00000	0.00000	0.00000
8	-0.03850	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01876	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.00353	0.00000	-0.00061	0.00000	0.00000	0.00000
17	0.00517	0.16479	-0.00073	0.00000	0.00002	0.00000
45	-0.11759	0.18487	0.02223	0.00000	-0.00011	0.00000
50	-0.00184	0.19298	0.08351	0.00000	-0.00004	0.00000
51	0.00167	0.00000	0.02102	0.00000	0.00000	0.00000
52	-0.00276	0.00000	-0.09871	0.00000	0.00000	0.00000
53	0.00123	0.00000	0.03632	0.00000	0.00000	0.00000
54	0.01061	0.00000	-0.02621	0.00000	0.00000	0.00000
55	0.08446	0.28980	-0.00130	0.00000	0.00007	0.00000
115	0.00372	0.02624	0.00118	0.00000	0.00000	0.00000
116	0.00182	0.02105	-0.01027	0.00000	0.00000	0.00000
133	0.00319	0.03231	0.01473	0.00000	0.00000	0.00000
134	0.00215	0.02376	-0.00426	0.00000	0.00000	0.00000
406	-0.03240	0.13904	0.00633	0.00000	-0.06821	0.00000
409	0.00000	-0.32842	0.00000	0.00000	0.00000	0.00000
410	0.07064	1.12714	-0.03882	0.00000	0.04596	0.00000
414	0.00000	-0.55781	0.00000	0.00000	0.00000	0.00000
518	-0.01212	0.02397	-0.00682	0.00000	0.01528	0.00000
527	0.00068	0.35033	-0.06143	0.00000	0.00005	0.00000
578	0.01489	0.46089	-0.00170	0.00000	-0.01031	0.00000

SUM	0.06647	2.23777	-0.06647	0.00000	-0.01724	0.00000

Condition **LC46=1.2D+WL150**

6	0.01656	0.08685	0.00052	0.00000	0.00004	0.00000
7	0.03995	0.00000	-0.00176	0.00000	0.00000	0.00000
8	-0.03843	0.00000	0.00178	0.00000	0.00000	0.00000
9	0.01866	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.00290	0.00000	-0.00061	0.00000	0.00000	0.00000
17	0.00520	0.16474	-0.00074	0.00000	0.00002	0.00000
45	-0.11740	0.18485	0.02226	0.00000	-0.00011	0.00000
50	-0.00180	0.19299	0.08395	0.00000	-0.00004	0.00000
51	0.00112	0.00000	0.02111	0.00000	0.00000	0.00000
52	-0.00278	0.00000	-0.09895	0.00000	0.00000	0.00000
53	0.00122	0.00000	0.03587	0.00000	0.00000	0.00000
54	0.01010	0.00000	-0.02559	0.00000	0.00000	0.00000
55	0.08440	0.28998	-0.00153	0.00000	0.00007	0.00000
115	0.00372	0.02630	0.00130	0.00000	0.00000	0.00000
116	0.00180	0.02087	-0.01067	0.00000	0.00000	0.00000
133	0.00319	0.03231	0.01473	0.00000	0.00000	0.00000
134	0.00215	0.02376	-0.00426	0.00000	0.00000	0.00000
406	-0.03289	0.13860	0.00516	0.00000	-0.06805	0.00000
409	0.00000	-0.32763	0.00000	0.00000	0.00000	0.00000
410	0.08773	1.12701	-0.05020	0.00000	0.05208	0.00000
414	0.00000	-0.55823	0.00000	0.00000	0.00000	0.00000
518	-0.01450	0.02417	-0.00809	0.00000	0.01471	0.00000
527	0.00070	0.35033	-0.06141	0.00000	0.00005	0.00000
578	0.01482	0.46089	-0.00202	0.00000	-0.01023	0.00000

SUM	0.08061	2.23777	-0.08061	0.00000	-0.01146	0.00000

Condition **LC47=1.2D-WL0**

6	0.01654	0.08683	0.00052	0.00000	0.00004	0.00000
7	0.03557	0.00000	-0.00173	0.00000	0.00000	0.00000
8	-0.03961	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01681	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.01170	0.00000	-0.00061	0.00000	0.00000	0.00000
17	0.00463	0.16468	-0.00077	0.00000	0.00002	0.00000
45	-0.11972	0.18573	0.02318	0.00000	-0.00009	0.00000
50	-0.00167	0.19301	0.08455	0.00000	-0.00009	0.00000
51	-0.00120	0.00000	0.01545	0.00000	0.00000	0.00000
52	-0.00288	0.00000	-0.09917	0.00000	0.00000	0.00000
53	0.00121	0.00000	0.03517	0.00000	0.00000	0.00000
54	0.00777	0.00000	-0.02946	0.00000	0.00000	0.00000
55	0.08315	0.28991	-0.00213	0.00000	0.00007	0.00000
115	0.00372	0.02639	0.00152	0.00000	0.00000	0.00000
116	0.00177	0.02047	-0.01156	0.00000	0.00000	0.00000
133	0.00319	0.03231	0.01475	0.00000	0.00000	0.00000
134	0.00215	0.02373	-0.00431	0.00000	0.00000	0.00000
406	-0.04318	0.13941	-0.01085	0.00000	-0.07516	0.00000
409	0.00000	-0.32956	0.00000	0.00000	0.00000	0.00000
410	0.06079	1.12896	-0.05717	0.00000	0.04475	0.00000
414	0.00000	-0.56096	0.00000	0.00000	0.00000	0.00000
518	-0.03147	0.02409	-0.01758	0.00000	0.01014	0.00000
527	0.00029	0.34988	-0.06170	0.00000	0.00008	0.00000
578	0.01386	0.46288	-0.00440	0.00000	-0.00936	0.00000

SUM	0.00000	2.23777	-0.12600	0.00000	-0.02959	0.00000

Condition **LC48=1.2D-WL30**

6	0.01652	0.08678	0.00052	0.00000	0.00004	0.00000
7	0.03055	0.00000	-0.00182	0.00000	0.00000	0.00000
8	-0.04106	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01572	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.02099	0.00000	-0.00061	0.00000	0.00000	0.00000
17	0.00414	0.16508	-0.00074	0.00000	0.00002	0.00000
45	-0.12048	0.18638	0.02347	0.00000	-0.00004	0.00000
50	-0.00152	0.19321	0.08535	0.00000	-0.00015	0.00000
51	-0.00403	0.00000	0.01728	0.00000	0.00000	0.00000
52	-0.00302	0.00000	-0.09957	0.00000	0.00000	0.00000
53	0.00121	0.00000	0.03473	0.00000	0.00000	0.00000
54	0.00487	0.00000	-0.02637	0.00000	0.00000	0.00000
55	0.08228	0.28787	0.00011	0.00000	0.00005	0.00000
115	0.00369	0.02587	0.00036	0.00000	0.00000	0.00000
116	0.00193	0.02224	-0.00763	0.00000	0.00000	0.00000
133	0.00319	0.03231	0.01474	0.00000	0.00000	0.00000
134	0.00215	0.02376	-0.00426	0.00000	0.00000	0.00000
406	-0.04459	0.14077	-0.01164	0.00000	-0.07763	0.00000
409	0.00000	-0.33251	0.00000	0.00000	0.00000	0.00000
410	0.00447	1.12928	-0.02324	0.00000	0.02451	0.00000
414	0.00000	-0.55858	0.00000	0.00000	0.00000	0.00000
518	-0.02881	0.02353	-0.01622	0.00000	0.01058	0.00000
527	-0.00061	0.34945	-0.06133	0.00000	0.00012	0.00000
578	0.01378	0.46232	-0.00406	0.00000	-0.00933	0.00000

SUM	-0.08061	2.23777	-0.08061	0.00000	-0.05183	0.00000

Condition **LC49=1.2D-WL60**

6	0.01652	0.08678	0.00052	0.00000	0.00004	0.00000
7	0.03073	0.00000	-0.00183	0.00000	0.00000	0.00000
8	-0.04104	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01584	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.02052	0.00000	-0.00061	0.00000	0.00000	0.00000
17	0.00417	0.16514	-0.00075	0.00000	0.00002	0.00000
45	-0.12040	0.18639	0.02345	0.00000	-0.00004	0.00000
50	-0.00148	0.19323	0.08569	0.00000	-0.00015	0.00000
51	-0.00462	0.00000	0.01685	0.00000	0.00000	0.00000
52	-0.00305	0.00000	-0.09976	0.00000	0.00000	0.00000
53	0.00120	0.00000	0.03440	0.00000	0.00000	0.00000
54	0.00431	0.00000	-0.02641	0.00000	0.00000	0.00000
55	0.08258	0.28766	0.00039	0.00000	0.00005	0.00000
115	0.00369	0.02581	0.00021	0.00000	0.00000	0.00000
116	0.00195	0.02245	-0.00716	0.00000	0.00000	0.00000
133	0.00319	0.03231	0.01474	0.00000	0.00000	0.00000
134	0.00215	0.02376	-0.00426	0.00000	0.00000	0.00000
406	-0.04086	0.14060	-0.00569	0.00000	-0.07519	0.00000
409	0.00000	-0.33221	0.00000	0.00000	0.00000	0.00000
410	0.00832	1.12905	-0.01936	0.00000	0.02531	0.00000
414	0.00000	-0.55811	0.00000	0.00000	0.00000	0.00000
518	-0.02259	0.02349	-0.01277	0.00000	0.01225	0.00000
527	-0.00068	0.34943	-0.06125	0.00000	0.00012	0.00000
578	0.01412	0.46199	-0.00319	0.00000	-0.00964	0.00000

SUM	-0.06647	2.23777	-0.06647	0.00000	-0.04723	0.00000

Condition **LC50=1.2D-WL90**

6	0.01650	0.08674	0.00052	0.00000	0.00005	0.00000
7	0.02861	0.00000	-0.00191	0.00000	0.00000	0.00000
8	-0.04180	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01538	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.02350	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00400	0.16555	-0.00074	0.00000	0.00001	0.00000
45	-0.11990	0.18639	0.02409	0.00000	0.00001	0.00000
50	-0.00137	0.19346	0.08636	0.00000	-0.00020	0.00000
51	-0.00675	0.00000	0.02555	0.00000	0.00000	0.00000
52	-0.00315	0.00000	-0.10012	0.00000	0.00000	0.00000
53	0.00121	0.00000	0.03437	0.00000	0.00000	0.00000
54	0.00210	0.00000	-0.01602	0.00000	0.00000	0.00000
55	0.08293	0.28596	0.00248	0.00000	0.00003	0.00000
115	0.00367	0.02531	-0.00089	0.00000	0.00000	0.00000
116	0.00209	0.02408	-0.00354	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01473	0.00000	0.00000	0.00000
134	0.00216	0.02378	-0.00420	0.00000	0.00000	0.00000
406	-0.03621	0.14092	0.00231	0.00000	-0.07282	0.00000
409	0.00000	-0.33177	0.00000	0.00000	0.00000	0.00000
410	-0.01492	1.12710	0.00598	0.00000	0.01562	0.00000
414	0.00000	-0.55492	0.00000	0.00000	0.00000	0.00000
518	-0.01146	0.02323	-0.00663	0.00000	0.01506	0.00000
527	-0.00137	0.34938	-0.06038	0.00000	0.00016	0.00000
578	0.01459	0.46024	-0.00166	0.00000	-0.01011	0.00000

SUM	-0.08400	2.23777	0.00000	0.00000	-0.05219	0.00000

Condition **LC51=1.2D-WL120**

6	0.01651	0.08674	0.00052	0.00000	0.00005	0.00000
7	0.03027	0.00000	-0.00195	0.00000	0.00000	0.00000
8	-0.04133	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01658	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.02059	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00426	0.16569	-0.00070	0.00000	0.00001	0.00000
45	-0.11893	0.18551	0.02450	0.00000	0.00000	0.00000
50	-0.00144	0.19352	0.08620	0.00000	-0.00018	0.00000
51	-0.00556	0.00000	0.03605	0.00000	0.00000	0.00000
52	-0.00309	0.00000	-0.10012	0.00000	0.00000	0.00000
53	0.00122	0.00000	0.03494	0.00000	0.00000	0.00000
54	0.00328	0.00000	-0.00503	0.00000	0.00000	0.00000
55	0.08348	0.28547	0.00352	0.00000	0.00003	0.00000
115	0.00365	0.02511	-0.00134	0.00000	0.00000	0.00000
116	0.00216	0.02484	-0.00184	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01471	0.00000	0.00000	0.00000
134	0.00216	0.02380	-0.00416	0.00000	0.00000	0.00000
406	-0.03063	0.14123	0.01193	0.00000	-0.06987	0.00000
409	0.00000	-0.33335	0.00000	0.00000	0.00000	0.00000
410	-0.02685	1.12723	0.02857	0.00000	0.00989	0.00000
414	0.00000	-0.55234	0.00000	0.00000	0.00000	0.00000
518	0.00127	0.02290	0.00041	0.00000	0.01835	0.00000
527	-0.00128	0.34997	-0.05956	0.00000	0.00014	0.00000
578	0.01519	0.45914	0.00010	0.00000	-0.01069	0.00000

SUM	-0.06647	2.23777	0.06647	0.00000	-0.05225	0.00000

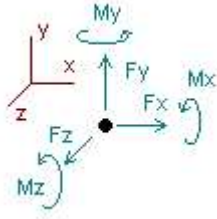
Condition **LC52=1.2D-WL150**

6	0.01651	0.08674	0.00052	0.00000	0.00005	0.00000
7	0.02999	0.00000	-0.00196	0.00000	0.00000	0.00000
8	-0.04140	0.00000	0.00177	0.00000	0.00000	0.00000
9	0.01667	0.00000	-0.00146	0.00000	0.00000	0.00000
10	-0.02122	0.00000	-0.00060	0.00000	0.00000	0.00000
17	0.00423	0.16573	-0.00069	0.00000	0.00001	0.00000
45	-0.11913	0.18553	0.02447	0.00000	0.00001	0.00000
50	-0.00148	0.19352	0.08575	0.00000	-0.00017	0.00000
51	-0.00500	0.00000	0.03596	0.00000	0.00000	0.00000
52	-0.00307	0.00000	-0.09988	0.00000	0.00000	0.00000
53	0.00123	0.00000	0.03539	0.00000	0.00000	0.00000
54	0.00380	0.00000	-0.00565	0.00000	0.00000	0.00000
55	0.08354	0.28529	0.00375	0.00000	0.00003	0.00000
115	0.00365	0.02506	-0.00145	0.00000	0.00000	0.00000
116	0.00218	0.02502	-0.00144	0.00000	0.00000	0.00000
133	0.00319	0.03230	0.01471	0.00000	0.00000	0.00000
134	0.00216	0.02381	-0.00415	0.00000	0.00000	0.00000
406	-0.03013	0.14167	0.01310	0.00000	-0.07002	0.00000
409	0.00000	-0.33414	0.00000	0.00000	0.00000	0.00000
410	-0.04394	1.12736	0.03995	0.00000	0.00378	0.00000
414	0.00000	-0.55192	0.00000	0.00000	0.00000	0.00000
518	0.00365	0.02270	0.00168	0.00000	0.01892	0.00000
527	-0.00130	0.34998	-0.05959	0.00000	0.00014	0.00000
578	0.01526	0.45914	0.00042	0.00000	-0.01076	0.00000

SUM	-0.08061	2.23777	0.08061	0.00000	-0.05803	0.00000

Envelope for nodal reactions

Note.- I_c is the controlling load condition



Direction of positive forces and moments

Envelope of nodal reactions for :

- LC1=1.2D+1.6W_o
- LC2=1.2D+1.6W₃₀
- LC3=1.2D+1.6W₆₀
- LC4=1.2D+1.6W₉₀
- LC5=1.2D+1.6W₁₂₀
- LC6=1.2D+1.6W₁₅₀
- LC7=1.2D-1.6W_o
- LC8=1.2D-1.6W₃₀
- LC9=1.2D-1.6W₆₀
- LC10=1.2D-1.6W₉₀
- LC11=1.2D-1.6W₁₂₀
- LC12=1.2D-1.6W₁₅₀
- LC13=0.9D+1.6W_o
- LC14=0.9D+1.6W₃₀
- LC15=0.9D+1.6W₆₀
- LC16=0.9D+1.6W₉₀
- LC17=0.9D+1.6W₁₂₀
- LC18=0.9D+1.6W₁₅₀
- LC19=0.9D-1.6W_o
- LC20=0.9D-1.6W₃₀
- LC21=0.9D-1.6W₆₀
- LC22=0.9D-1.6W₉₀
- LC23=0.9D-1.6W₁₂₀
- LC24=0.9D-1.6W₁₅₀
- LC25=1.2D+D_i+W_{I0}
- LC26=1.2D+D_i+W_{I30}
- LC27=1.2D+D_i+W_{I60}
- LC28=1.2D+D_i+W_{I90}
- LC29=1.2D+D_i+W_{I120}
- LC30=1.2D+D_i+W_{I150}
- LC31=1.2D+D_i-W_{I0}
- LC32=1.2D+D_i-W_{I30}
- LC33=1.2D+D_i-W_{I60}
- LC34=1.2D+D_i-W_{I90}
- LC35=1.2D+D_i-W_{I120}
- LC36=1.2D+D_i-W_{I150}
- LC37=0.9D
- LC38=1.2D
- LC41=1.2D+W_{L0}
- LC42=1.2D+W_{L30}
- LC43=1.2D+W_{L60}
- LC44=1.2D+W_{L90}
- LC45=1.2D+W_{L120}
- LC46=1.2D+W_{L150}
- LC47=1.2D-W_{L0}
- LC48=1.2D-W_{L30}
- LC49=1.2D-W_{L60}
- LC50=1.2D-W_{L90}
- LC51=1.2D-W_{L120}
- LC52=1.2D-W_{L150}

Node		Forces						Moments					
		Fx	lc	Fy	lc	Fz	lc	Mx	lc	My	lc	Mz	lc
		[Kip]		[Kip]		[Kip]		[Kip*ft]		[Kip*ft]		[Kip*ft]	
6	Max	0.053	LC7	0.187	LC30	0.005	LC12	0.00000	LC1	0.00221	LC8	0.00000	LC1
	Min	-0.021	LC13	0.007	LC13	-0.004	LC18	0.00000	LC1	-0.00210	LC14	0.00000	LC1
7	Max	0.789	LC5	0.000	LC1	0.068	LC18	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.448	LC23	0.000	LC1	-0.071	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
8	Max	0.013	LC15	0.000	LC1	0.089	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.263	LC11	0.000	LC1	-0.085	LC18	0.00000	LC1	0.00000	LC1	0.00000	LC1
9	Max	0.059	LC8	0.000	LC1	0.103	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.259	LC21	0.000	LC1	-0.106	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
10	Max	1.585	LC15	0.000	LC1	0.094	LC23	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-1.447	LC10	0.000	LC1	-0.095	LC5	0.00000	LC1	0.00000	LC1	0.00000	LC1
17	Max	0.222	LC2	0.385	LC25	0.365	LC13	0.00000	LC1	0.00084	LC7	0.00000	LC1
	Min	-0.227	LC8	-0.054	LC14	-0.367	LC7	0.00000	LC1	-0.00087	LC13	0.00000	LC1
45	Max	-0.014	LC15	0.379	LC33	0.140	LC11	0.00000	LC1	0.00400	LC23	0.00000	LC1
	Min	-0.244	LC32	0.062	LC15	-0.075	LC17	0.00000	LC1	-0.00415	LC4	0.00000	LC1
50	Max	0.005	LC22	0.382	LC35	0.176	LC34	0.00000	LC1	0.00643	LC16	0.00000	LC1
	Min	-0.008	LC4	0.132	LC18	0.014	LC16	0.00000	LC1	-0.00653	LC10	0.00000	LC1
51	Max	0.302	LC16	0.000	LC1	0.884	LC1	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.305	LC10	0.000	LC1	-0.578	LC19	0.00000	LC1	0.00000	LC1	0.00000	LC1
52	Max	0.097	LC16	0.000	LC1	-0.046	LC14	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.102	LC10	0.000	LC1	-0.244	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
53	Max	0.104	LC3	0.000	LC1	0.119	LC4	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.102	LC21	0.000	LC1	-0.225	LC20	0.00000	LC1	0.00000	LC1	0.00000	LC1
54	Max	0.306	LC4	0.000	LC1	0.844	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.292	LC22	0.000	LC1	-0.750	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
55	Max	0.361	LC2	0.588	LC30	0.413	LC1	0.00000	LC1	0.00089	LC5	0.00000	LC1
	Min	-0.199	LC20	-0.065	LC13	-0.405	LC19	0.00000	LC1	-0.00094	LC23	0.00000	LC1
115	Max	0.115	LC5	0.080	LC2	0.180	LC2	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.109	LC23	-0.037	LC20	-0.185	LC8	0.00000	LC1	0.00000	LC1	0.00000	LC1
116	Max	0.113	LC3	0.320	LC1	0.714	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.109	LC21	-0.278	LC19	-0.722	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
133	Max	0.114	LC4	0.078	LC12	0.173	LC12	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.109	LC22	-0.021	LC18	-0.148	LC18	0.00000	LC1	0.00000	LC1	0.00000	LC1
134	Max	0.113	LC4	0.141	LC1	0.317	LC13	0.00000	LC1	0.00000	LC1	0.00000	LC1
	Min	-0.110	LC21	-0.099	LC19	-0.323	LC7	0.00000	LC1	0.00000	LC1	0.00000	LC1
406	Max	0.372	LC14	0.317	LC36	0.708	LC2	0.00000	LC1	0.18894	LC14	0.00000	LC1
	Min	-0.427	LC8	0.072	LC18	-0.692	LC20	0.00000	LC1	-0.30918	LC8	0.00000	LC1
409	Max	0.000	LC1	-0.181	LC18	0.060	LC1	0.00000	LC1	0.00747	LC6	0.00000	LC1
	Min	0.000	LC1	-0.688	LC36	-0.060	LC6	0.00000	LC1	-0.00747	LC1	0.00000	LC1
410	Max	1.715	LC5	2.277	LC31	1.756	LC13	0.00000	LC1	0.61083	LC5	0.00000	LC1
	Min	-1.676	LC23	0.782	LC14	-1.764	LC7	0.00000	LC1	-0.56180	LC23	0.00000	LC1

414	Max	0.034	LC3	-0.232	LC13	0.000	LC1	0.00000	LC1	0.01268	LC3	0.00000	LC1
	Min	-0.034	LC9	-1.283	LC31	0.000	LC1	0.00000	LC1	-0.01268	LC9	0.00000	LC1
518	Max	0.843	LC13	0.050	LC31	0.499	LC13	0.00000	LC1	0.21219	LC1	0.00000	LC1
	Min	-0.852	LC7	-0.003	LC24	-0.505	LC7	0.00000	LC1	-0.18272	LC19	0.00000	LC1
527	Max	0.049	LC17	0.756	LC27	0.072	LC13	0.00000	LC1	0.00448	LC10	0.00000	LC1
	Min	-0.039	LC10	0.238	LC21	-0.144	LC7	0.00000	LC1	-0.00428	LC16	0.00000	LC1
578	Max	0.084	LC3	1.026	LC31	0.125	LC13	0.00000	LC1	0.03493	LC21	0.00000	LC1
	Min	-0.057	LC21	0.254	LC13	-0.126	LC7	0.00000	LC1	-0.05325	LC3	0.00000	LC1

Date: 2/16/2023
 Project Name: CHESHIRE SW
 Project No.: CT2036
 Designed By: KM Checked By: MSC



CHECK CONNECTION CAPACITY (Worst Case) → GAMMA SECTOR

Reference: AISC Steel Construction Manual 14th Edition (ASD)

Bolt Type = A325 1/2" Bolt

Allowable Tensile Load =

$F_{Tall} = 8836$ lbs.

Allowable Shear Load =

$F_{vall} = 5301$ lbs.

TENSILE FORCES

Reaction $F = 1764$ lbs. (See Bentley Output)

SHEAR FORCES

Reactions in X direction: 1715 lbs. (See Bentley Output)

Reactions in Y direction: 2277 lbs. (See Bentley Output)

Resultant: 2851 lbs.

No. of Supports = 1

No. of Bolts / Support = 2

Tension Design Load /Bolts =

$f_t = 882.00$ lbs. < 8836 lbs. **Therefore, OK !**

Shear Design Load / Bolts=

$f_v = 1425.30$ lbs. < 5301 lbs. **Therefore, OK !**

CHECK COMBINED TENSION AND SHEAR

$$\begin{array}{rclcl}
 f_t / F_T & + & f_v / F_v & \leq & 1.0 \\
 0.100 & + & 0.269 & = & 0.369 < 1.0 \text{ Therefore, OK !}
 \end{array}$$

Exhibit 5

Radio Frequency Exposure Analysis Report

March 14, 2023

AT&T

Site Name: CHESHIRE SW

Site Number: CT2036

FA#: 10034996

USID: 26014

Site Address: 751 Higgins Road, Cheshire, CT 06410



Michael Fischer, P.E.
Registered Professional Engineer (Electrical)
Connecticut License Number 33928
Expires January 31, 2024

Signed 14 March 2023

Site Compliance Summary

AT&T Compliance Status:	Compliant
Cumulative Calculated Power Density (Ground Level):	6.52314 $\mu\text{W}/\text{cm}^2$
Cumulative General Population % MPE (Ground Level):	0.66930%



March 14, 2023

Centerline
Attn: Ryan Burgdorfer, Project Manager
750 W Center St, Suite 301
West Bridgewater, MA 02379

RF Exposure Analysis for Site: **CHESHIRE SW**

Centerline Communications, LLC ("Centerline") was contracted to analyze the proposed AT&T facility at **751 Higgins Road, Cheshire, CT 06410** for the purpose of determining whether the predictive exposure from the proposed facility is within specified federal limits.

All information used in this report was analyzed as a percentage of the Maximum Permissible Exposure (% MPE) limits as detailed in 47 CFR § 1.1310 as well as Federal Communications Commission (FCC) OET Bulletin 65 Edition 97-01. The FCC MPE limits are typically expressed in units of milliwatts per square centimeter (mW/cm^2) or microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The exposure limits vary depending upon the frequencies being utilized. The General Population/Uncontrolled MPE limit (in mW/cm^2) for frequencies between 300 and 1500 is defined as frequency (in MHz) divided by 1500 ($f_{\text{MHz}}/1500$). Frequencies between 1500 and 100,000 MHz have a General Population/Uncontrolled MPE limit of $1 \text{ mW}/\text{cm}^2$ ($1000 \mu\text{W}/\text{cm}^2$). The calculated power density at each sample point divided by the limit at each calculated frequency provides a result in % MPE. Summing the calculated % MPE from all contributors provides a cumulative % MPE at a particular sample point. Wireless carriers use different frequency bands with varying MPE limits; therefore, it is useful to report results in terms of % MPE as opposed to power density.

All results were compared to the FCC radio frequency exposure rules as detailed in 47 CFR § 1.1307(b) to determine compliance with the MPE limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits, as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means. Additional details can be found in FCC OET 65.



Calculation Methodology

IXUS electromagnetic energy (EME) calculation software was used to assess all RF field levels presented in this study. IXUS software uses a fast and accurate EME calculation tool that allows for the determination of RF field strength in the vicinity of radio communication base stations and transmitters. At its core, the IXUS EME calculation module implements evaluation techniques detailed in the ITU-TK.61, CENELEC EN 50383, and IEC 62232 specifications and referenced in C95.3 IEEE Recommended Practice for Measurements and Computations of Electric, Magnetic, and Electromagnetic Fields with Respect to Human Exposure to Such Fields, 0 Hz to 300 GHz. The EME calculation result at any point in 3D space is achieved via a synthetic ray tracing technique, a conservative cylindrical envelope method, or through full-wave electromagnetic simulation. The ray tracing method is an advanced computation method described in IEC 622322 where the power is summed from elemental sources representing the individual components of the antenna which are selected by an analysis of published manufacturer datasheets and antenna pattern information. The selection of the solution method is determined by the particular antenna being considered.

In order to determine the spatial power density for comparison to the FCC limits, IXUS performs a spatial average of power density values between 0-6' above the specified study plane (e.g., ground level).



Data & Results

The following table details the antennas and operating parameters for the AT&T antenna system as well as any other antenna systems at the site. This is based on antenna information provided by the client and data compiled from other sources where necessary. The data below was input into IXUS to perform the theoretical exposure calculations at ground level.

The theoretical calculations performed in IXUS determine the cumulative exposure at all sample points at ground level (0-6' spatial average). The results from highest cumulative sample point at ground level surrounding the site are displayed in the table below. The contribution from directional antennas to the maximum cumulative totals varies greatly depending on location; therefore, the contribution from one antenna sector at the highest calculated exposure point may be greater or less than other sectors since sectorized directional antennas are pointed in different directions and there is not much overlapping exposure.

The contribution to the cumulative power density and % MPE for each antenna/frequency band is listed in the table(s) below. The cumulative power density and cumulative % MPE are displayed at the bottom of the table(s) below.



Maximum Calculated Cumulative Power Density @ Ground Level (Location: approximately 170' north of site)

Antenna ID	Make / Model	Frequency Band (MHz)	Antenna Gain (dBd)	Antenna Centerline (ft)	Channel Count	TX Power/Channel (watts)	ERP (watts)	Calculated Power Density ($\mu\text{W}/\text{cm}^2$)	General Population MPE Limit ($\mu\text{W}/\text{cm}^2$)	General Population % MPE
AT&T A	Quintel QD8616-7	700	13.05	255.00	6.00	40.00	3633.06	0.00528	466.67	0.00113
AT&T A	Quintel QD8616-7	1900	15.05	255.00	4.00	30.00	3838.67	0.00154	1000.00	0.00015
AT&T A	Quintel QD8616-7	2100	15.35	255.00	4.00	30.00	4113.21	0.00104	1000.00	0.00010
AT&T A	Ericsson AIR 6419	3450	23.05	257.00	1.00	54.22	10943.58	0.77780	1000.00	0.07778
AT&T A	Ericsson AIR 6449	3700	23.55	253.00	1.00	86.75	19645.79	0.61290	1000.00	0.06129
AT&T A	CCI DMP65R-BU8D	700	12.95	255.00	4.00	30.00	2366.91	0.00472	466.67	0.00101
AT&T A	CCI DMP65R-BU8D	850	13.85	255.00	4.00	30.00	2911.93	0.00047	566.67	0.00008
AT&T A	CCI DMP65R-BU8D	2300	15.95	255.00	4.00	18.75	2951.23	0.00017	1000.00	0.00002
AT&T B	Quintel QD6616-7	700	12.55	255.00	6.00	40.00	3237.97	0.00025	466.67	0.00005
AT&T B	Quintel QD6616-7	1900	15.05	255.00	4.00	30.00	3838.67	0.00011	1000.00	0.00001
AT&T B	Quintel QD6616-7	2100	15.55	255.00	4.00	30.00	4307.06	0.00062	1000.00	0.00006
AT&T B	Ericsson AIR 6419	3450	23.05	257.00	1.00	54.22	10943.58	0.01459	1000.00	0.00146
AT&T B	Ericsson AIR 6449	3700	23.55	253.00	1.00	86.75	19645.79	0.01532	1000.00	0.00153
AT&T B	CCI DMP65R-BU6D	700	11.85	255.00	4.00	30.00	1837.30	0.00005	466.67	0.00001
AT&T B	CCI DMP65R-BU6D	850	12.45	255.00	4.00	30.00	2109.51	0.00023	566.67	0.00004
AT&T B	CCI DMP65R-BU6D	2300	16.25	255.00	4.00	18.75	3162.30	0.00005	1000.00	0.00000
AT&T C	Quintel QD6616-7	700	12.55	255.00	6.00	40.00	3237.97	0.00016	466.67	0.00003
AT&T C	Quintel QD6616-7	1900	15.05	255.00	4.00	30.00	3838.67	0.00005	1000.00	0.00000
AT&T C	Quintel QD6616-7	2100	15.55	255.00	4.00	30.00	4307.06	0.00008	1000.00	0.00001
AT&T C	Ericsson AIR 6419	3450	23.05	257.00	1.00	54.22	10943.58	0.03379	1000.00	0.00338
AT&T C	Ericsson AIR 6449	3700	23.55	253.00	1.00	86.75	19645.79	0.09414	1000.00	0.00941
AT&T C	CCI DMP65R-BU6D	700	11.85	255.00	4.00	30.00	1837.30	0.00007	466.67	0.00002
AT&T C	CCI DMP65R-BU6D	850	12.45	255.00	4.00	30.00	2109.51	0.00022	566.67	0.00004
AT&T C	CCI DMP65R-BU6D	2300	16.25	255.00	4.00	18.75	3162.30	0.00004	1000.00	0.00000
Unknown A	Generic Panel 6ft	600	11.95	245.00	2.00	60.00	1880.10	0.00223	400.00	0.00056
Unknown A	Generic Panel 6ft	700	12.35	245.00	2.00	60.00	2061.49	0.00180	466.67	0.00039
Unknown A	Generic Panel 6ft	1900	15.55	245.00	2.00	60.00	4307.06	0.00109	1000.00	0.00011
Unknown A	Generic Panel 6ft	2100	15.55	245.00	2.00	60.00	4307.06	0.00109	1000.00	0.00011
Unknown A	Generic Panel 3ft	2500	22.35	245.00	4.00	60.00	41229.80	1.77500	1000.00	0.17750
Unknown B	Generic Panel 6ft	600	11.95	245.00	2.00	60.00	1880.10	0.00008	400.00	0.00002
Unknown B	Generic Panel 6ft	700	12.35	245.00	2.00	60.00	2061.49	0.00008	466.67	0.00002
Unknown B	Generic Panel 6ft	1900	15.55	245.00	2.00	60.00	4307.06	0.00010	1000.00	0.00001
Unknown B	Generic Panel 6ft	2100	15.55	245.00	2.00	60.00	4307.06	0.00010	1000.00	0.00001
Unknown B	Generic Panel 3ft	2500	22.35	245.00	4.00	60.00	41229.80	0.07034	1000.00	0.00703
Unknown C	Generic Panel 6ft	600	11.95	245.00	2.00	60.00	1880.10	0.00008	400.00	0.00002



Antenna ID	Make / Model	Frequency Band (MHz)	Antenna Gain (dBd)	Antenna Centerline (ft)	Channel Count	TX Power/ Channel (watts)	ERP (watts)	Calculated Power Density ($\mu\text{W}/\text{cm}^2$)	General Population MPE Limit ($\mu\text{W}/\text{cm}^2$)	General Population % MPE
Unknown C	Generic Panel 6ft	700	12.35	245.00	2.00	60.00	2061.49	0.00008	466.67	0.00002
Unknown C	Generic Panel 6ft	1900	15.55	245.00	2.00	60.00	4307.06	0.00010	1000.00	0.00001
Unknown C	Generic Panel 6ft	2100	15.55	245.00	2.00	60.00	4307.06	0.00010	1000.00	0.00001
Unknown C	Generic Panel 3ft	2600	22.35	245.00	4.00	60.00	41229.80	0.06566	1000.00	0.00657
Unknown A	Generic Panel 6ft	700	12.75	238.00	4.00	40.00	3013.84	0.00022	466.67	0.00005
Unknown A	Generic Panel 6ft	850	12.55	238.00	4.00	40.00	2878.19	0.04303	566.67	0.00759
Unknown A	Generic Panel 6ft	1900	15.55	238.00	4.00	40.00	5742.75	0.02156	1000.00	0.00216
Unknown A	Generic Panel 6ft	2100	16.45	238.00	4.00	40.00	7065.13	0.00146	1000.00	0.00015
Unknown A	Generic Panel 3ft	3700	23.55	238.00	4.00	50.00	45292.89	2.58700	1000.00	0.25870
Unknown B	Generic Panel 6ft	700	12.75	238.00	4.00	40.00	3013.84	0.00001	466.67	0.00000
Unknown B	Generic Panel 6ft	850	12.55	238.00	4.00	40.00	2878.19	0.00051	566.67	0.00009
Unknown B	Generic Panel 6ft	1900	15.55	238.00	4.00	40.00	5742.75	0.00045	1000.00	0.00005
Unknown B	Generic Panel 6ft	2100	16.45	238.00	4.00	40.00	7065.13	0.00001	1000.00	0.00000
Unknown B	Generic Panel 3ft	3700	23.55	238.00	4.00	50.00	45292.89	0.12970	1000.00	0.01297
Unknown C	Generic Panel 6ft	700	12.75	238.00	4.00	40.00	3013.84	0.00001	466.67	0.00000
Unknown C	Generic Panel 6ft	850	12.55	238.00	4.00	40.00	2878.19	0.00047	566.67	0.00008
Unknown C	Generic Panel 6ft	1900	15.55	238.00	4.00	40.00	5742.75	0.00030	1000.00	0.00003
Unknown C	Generic Panel 6ft	2100	16.45	238.00	4.00	40.00	7065.13	0.00001	1000.00	0.00000
Unknown C	Generic Panel 3ft	3700	23.55	238.00	4.00	50.00	45292.89	0.10100	1000.00	0.01010
Unknown A	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.05027	566.67	0.00887
Unknown A	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.05027	566.67	0.00887
Unknown A	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.05027	566.67	0.00887
Unknown B	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00048	566.67	0.00009
Unknown B	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00048	566.67	0.00009
Unknown B	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00048	566.67	0.00009
Unknown C	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00045	566.67	0.00008
Unknown C	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00045	566.67	0.00008
Unknown C	Generic Panel 6ft	850	12.55	222.00	4.00	40.00	2878.19	0.00045	566.67	0.00008
Unknown	Generic Omni 1900	1900	11.95	203.00	4.00	37.50	391.69	0.00023	1000.00	0.00002
Unknown	Generic Omni 1900	1900	11.95	203.00	4.00	37.50	391.69	0.00023	1000.00	0.00002
Unknown	Generic Omni 1900	1900	11.95	137.00	4.00	37.50	391.69	0.00172	1000.00	0.00017
							Cumulative Power Density:	6.52314 $\mu\text{W}/\text{cm}^2$	Cumulative % MPE:	0.66930%



Summary

The theoretical calculations performed for this analysis yielded cumulative power density totals in all areas at ground level that are within the allowable federal limits for public exposure to RF energy. Therefore, the site is **compliant** with FCC rules and regulations.

A handwritten signature in black ink, appearing to read "Katrina Styx", with a long, sweeping horizontal stroke extending to the right.

Katrina Styx
RF EME Technical Writer
Centerline Communications, LLC

Exhibit 6

William Hurley

From: UPS <pkginfo@ups.com>
Sent: Friday, March 24, 2023 11:22 AM
To: William Hurley
Subject: UPS Delivery Notification, Tracking Number 1Z9Y45030330812777



Hello, your package has been delivered.

Delivery Date: Friday, 03/24/2023

Delivery Time: 11:19 AM

Signed by: SHEPARD

CENTERLINE SITE ACQUISITION

Tracking Number:	1Z9Y45030330812777
Ship To:	OFFICE OF THE TOWN MANAGER 84 SOUTH MAIN STREET CHESHIRE, CT 06410 US
Number of Packages:	1
UPS Service:	UPS Ground
Package Weight:	1.0 LBS
Reference Number:	CT2036 TOWN MANAGER

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William Hurley

From: UPS <pkginfo@ups.com>
Sent: Friday, March 24, 2023 11:22 AM
To: William Hurley
Subject: UPS Delivery Notification, Tracking Number 1Z9Y45030320085162



Hello, your package has been delivered.

Delivery Date: Friday, 03/24/2023

Delivery Time: 11:20 AM

Signed by: DONNA

CENTERLINE SITE ACQUISITION

Tracking Number:	1Z9Y45030320085162
Ship To:	PLANNING AND ZONING DEPARTMENT 84 SOUTH MAIN STREET CHESHIRE, CT 064103108 US
Number of Packages:	1
UPS Service:	UPS Ground
Package Weight:	1.0 LBS
Reference Number:	CT2036 ZEO

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William Hurley

From: UPS <pkginfo@ups.com>
Sent: Friday, March 24, 2023 11:22 AM
To: William Hurley
Subject: UPS Delivery Notification, Tracking Number 1Z9Y45030310780821



Hello, your package has been delivered.

Delivery Date: Friday, 03/24/2023

Delivery Time: 11:20 AM

Signed by: DONNA

CENTERLINE SITE ACQUISITION

Tracking Number:	1Z9Y45030310780821
Ship To:	PLANNING AND ZONING DEPARTMENT 84 SOUTH MAIN STREET CHESHIRE, CT 06410 US
Number of Packages:	1
UPS Service:	UPS Ground
Package Weight:	1.0 LBS
Reference Number:	CT2036 TOWN PLANNER

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William Hurley

From: UPS <pkginfo@ups.com>
Sent: Monday, March 27, 2023 3:20 PM
To: William Hurley
Subject: UPS Delivery Notification, Tracking Number 1Z9Y45030306947838



Hello, your package has been delivered.

Delivery Date: Monday, 03/27/2023

Delivery Time: 3:19 PM

Signed by: MAILROOM

CENTERLINE SITE ACQUISITION

Tracking Number:	1Z9Y45030306947838
Ship To:	AT&T TOWERS 1025 LENOX PARK BLVD NE 3RD FLOOR BROOKHAVEN, GA 30319 US
Number of Packages:	1
UPS Service:	UPS Ground
Package Weight:	1.0 LBS
Reference Number:	CT2036 AT&T TOWERS

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