

■ ■ ■ ■ **T** ■ ■ **Mobile** ■ ■[®]

January 7, 2004

Via Facsimile

Pamela B. Katz, Chairman and
Members of the Siting Council
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

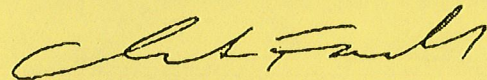
RE: Tower Sharing Request by T-Mobile
Future Verizon Facility at
Lot 54 Palmer Road, Chaplin
Doc. 211

Dear Ms. Katz and Members of the Siting Council:

At this time, T-Mobile would like to withdraw its Tower Share application for the Verizon Tower located at Palmer Road in Chaplin. T-mobile will be re-filing the application in the future at the 117' height.

I am sorry for any inconvenience this may have caused.

Respectfully submitted,



Christine Farrell
T-Mobile
100 Filley St.
Bloomfield, CT 06002
(860) 6794-6427

cc: Chaplin First Selectman Rusty Lanzit

T-Mobile

Omnipoint Holdings, Inc.
100 Filley Street, Bloomfield, CT. 06002
Telephone: (860) 692-7100 Fax: (860) 692-7159

Recipient (s):	Phone Number (s):	Fax Number (s):
CT SITING Council		
Mike Perone		

Date: 1/7/04

Pages: 2 (including cover sheet)

Sender: Christine Farnell Sender's Direct Dial: 860-7946427

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December 31, 2003

BY HAND

Pamela B. Katz, Chairman and
Members of the Siting Council
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

RECEIVED
JAN - 6 2004
CONNECTICUT
SITING COUNCIL

RE: Tower Sharing Request by T-Mobile
Future Verizon Facility at
Lot 54 Palmer Road, Chaplin
Doc. 211
Latitude: 41-47-04 / Longitude: 71-08-08

Dear Ms. Katz and Members of the Siting Council:

Pursuant to Connecticut General Statutes (C.G.S.) § 16-50aa, T-Mobile USA, Inc. acting through its wholly owned subsidiary Omnipoint Communications, Inc. ("T-Mobile") hereby requests an order from the Connecticut Siting Council ("Council") to approve the proposed shared use of a future communications tower, located at Lot 54 Palmer Road in the Town of Chaplin ("Verizon Facility"), owned by Cellco partnership d/b/a Verizon Wireless ("Verizon"). T-Mobile and Verizon have agreed to the shared use of the Verizon Facility, as detailed below. Verizon received approval to construct said Facility on November 4, 2003 and have already or will start construction shortly.

VERIZON FACILITY

The Verizon Facility consists of an approximately one hundred fifty (150) foot high monopole tower ("Tower") owned and operated by Verizon. T-Mobile will be at a mounting height of One Hundred Twenty Seven (127) feet. A chain link fence will surround the Verizon Facility. Verizon is approved to locate at the 147' level and Sprint is approved to locate at the 137' level. Sprint will be building the facility for Verizon, but Verizon will own the facility.

December 31, 2003

Page 2

T-MOBILE FACILITY

As shown on the enclosed plans prepared by All-Points Technology Corporation, P.C., including a site plan and tower elevation of the Verizon Facility, annexed hereto as Exhibit A, T-Mobile proposes a shared use of the Facility by placing antennas on the Tower and equipment needed to provide personal communications services ("PCS") within the existing fenced compound. T-Mobile will install up to nine (9) antennas at approximately the One Hundred Twenty Seven (127) foot level of the Tower. Associated unmanned equipment cabinets will be located on a concrete pad near the base of the tower within the existing compound.

Connecticut General Statutes § 16-50aa provides that, upon written request for shared use approval, an order approving such use shall be issued, "if the council finds that the proposed shared use of the facility is technically, legally, environmentally and economically feasible and meets public safety concerns." (C.G.S. § 16-50aa(c)(1).) Further, upon approval of such shared use, it is exclusive and no local zoning or land use approvals are required C.G.S. §16-50x. Shared use of the Verizon Facility satisfies the approval criteria set forth in C.G.S. § 16-50aa as follows:

- A. Technical Feasibility The existing Tower and compound were designed to accommodate multiple carriers. A structural analysis of the Tower with multiply carriers has been performed and is attached as Exhibit B. The structural analysis concludes that the existing tower can safely accommodate the proposed T-Mobile antennas. The proposed shared use of this Tower is technically feasible. Further there is sufficient room in the fenced compound for our facility, thus the site plan will not have to be altered.
- B. Legal Feasibility Pursuant to C.G.S. § 16-50aa, the Council has been authorized to issue an order approving shared use of the future Sprint Facility. (C.G.S. § 16-50aa (C)(1)). Under the authority vested in the Council by C.G.S. § 16-50aa, an order by the Council approving the shared use of a tower would permit the Applicant to obtain a building permit for the proposed installation.
- C. Environmental Feasibility The proposed shared use would have a minimal environmental effect, for the following reasons:

- 1.) The proposed installation would have a de minimis visual impact, and would not cause any significant change or alteration in the physical or environmental characteristics of the existing facility;
 - 2.) The proposed installation by T-Mobile would not increase the height of the tower or extend the boundaries of the Verizon Facility;
 - 3.) The proposed installation would not increase the noise levels at the existing facility boundaries by six decibels or more;
 - 4.) Operation of T-Mobile's antennas at this site would not exceed the total radio frequency electromagnetic radiation power density level adopted by the FCC and Connecticut Department of Health. The "worst case" exposure calculated for the operation of this facility for all carriers, would be approximately 11.77 % of the standard. See Cumulative Emissions Compliance Report dated December 31, 2003, prepared by Hassan Syed, T-Mobile Radio Frequency Engineer, annexed hereto as Exhibit C;
 - 5.) The proposed shared use of the Verizon Facility would not require any water or sanitary facilities, or generate any air emissions or discharges to water bodies. Further, the installation will not generate any traffic other than for periodic maintenance visits.
- D. Economic Feasibility The Applicant and the tower owner have agreed to share use of the Sprint Facility on terms agreeable to both parties. The proposed tower sharing is therefore economically feasible.
- E. Public Safety As stated above and evidenced in the Cumulative Emissions Compliance Report annexed hereto as Exhibit C, the operation of T-Mobile's antennas at this site would not exceed the total radio frequency electromagnetic radiation power density level adopted by the FCC and Connecticut Department of Health. Further, the addition of T-Mobile's telecommunications service in the Chaplin area through shared use of the Verizon Facility is expected to enhance the safety and welfare of local residents and travelers through the area resulting in an improvement to public safety in this area.

December 31, 2003

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Conclusion

As delineated above, the proposed shared use of the Verizon Facility satisfies the criteria set forth in C.G.S. § 16-50aa, and advances the General Assembly's and the Siting Council's goal of preventing the proliferation of tower in the State of Connecticut. T-Mobile therefore requests the Siting Council issue an order approving the proposed shared use of the Verizon Facility.

Respectfully submitted,

A handwritten signature in blue ink, appearing to read "Christine Farrell", written in a cursive style.

Christine Farrell
T-Mobile
100 Filley St.
Bloomfield, CT 06002
(860) 6794-6427

cc: Chaplin First Selectman Rusty Lanzit

Exhibit A

EMERSON COMMUNICATIONS, INC.
A WHOLLY OWNED SUBSIDIARY OF FORTRILE, USA
1000 MAIN STREET
MIDDLETOWN, CT 06457
OFFICE: (860) 467-7100
FAX: (860) 467-7170

ALL-POINTS TECHNOLOGY CORPORATION, P.C.
3 BULLOCK ROAD
MIDDLETOWN, CT 06457
OFFICE: (860) 467-7100
FAX: (860) 467-7170
www.allpointstech.com



APPROVALS

LANDLORD _____
LEASING _____
ZONING _____
CONSTRUCTION _____
A/E _____

PROJECT NO: CT-11-508-F
DRAWN BY: DWA
CHECKED BY: SMC

SUBMITTALS

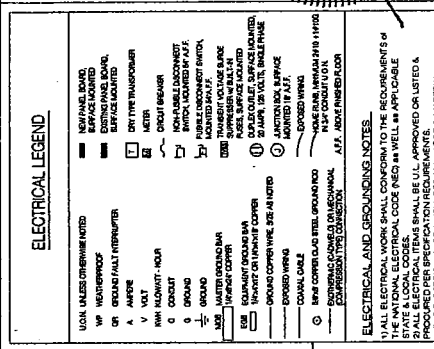
0 10/20/04 CONSTRUCTION DWA

THE DRAWING IS THE SOLE PROPERTY OF EMERSON COMMUNICATIONS, INC. AND IS NOT TO BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT THE WRITTEN PERMISSION OF EMERSON COMMUNICATIONS, INC.

CT-11-508-F
VERIZON CHAPLIN
LOT #4 PALMER ROAD
CHAPLIN, CT 06326

SHEET TITLE
ELECTRICAL & GROUNDING NOTES, RISERS & DETAILS

SHEET NUMBER
E-1



ELECTRICAL AND GROUNDING NOTES:

1. ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) AS WELL AS ANY APPLICABLE STATE & LOCAL CODES.

2. THE ELECTRICAL WORK SHALL BE APPROVED AS LISTED A PROCEDURE PER SPECIFICATION REQUIREMENTS.

3. THE ELECTRICAL WORK INCLUDES ALL LABOR & MATERIAL WORK TO PROVIDE COMPLETE OPERATING & APPROVED ELECTRICAL SYSTEM.

4. CONTRACTOR SHALL PROVIDE PERMITS & COORDINATION OF PERMITS FOR ALL WORK OUTSIDE A BUILDING AS EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUIT & SCHEDULE 40 PIPE PERMITTED BY CODES & WHERE APPLICABLE SHALL BE SCHEDULE 40 PIPE.

5. ELECTRICAL WIRING SHALL BE COPPER W/ THIN W/ MIN. #18 AWG.

6. ALL ELECTRICAL CONDUIT & CABLE BETWEEN ELECTRICAL UTILITY MANUFACTURER'S COAX CABLE SHELLS MINIMUM #18 AWG SHALL BE COOPERATED INSTALLATION W/ UTILITY COMPANY.

7. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

8. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

9. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

10. WHERE CONDUIT BETWEEN RISERS & LESSEES/LEASEE CELL SITE THE CONDUIT SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

11. THE CONDUIT POINT OF THESE CONDUITS SHALL BE PVC CONDUIT ABOVE GROUND & SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

12. POWER PRESENT SUPPLIED BY LESSEES/LEASEE.

13. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

14. GROUNDING CONDUIT SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

15. USE #12 COPPER STRANDED WIRE W/ GREEN COLOR INSULATION FOR ABOVE GROUND GROUNDING UNLESS OTHERWISE SPECIFIED & #10 COPPER STRANDED WIRE FOR BELOW GROUND GROUNDING AS INDICATED ON THE DRAWING.

16. ALL GROUND CONNECTIONS TO BE BURIED UNDERGROUND SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

17. DO NOT ALLOW BARE COPPER WIRE TO BE IN CONTACT W/ GALVANIZED STEEL.

18. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

19. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

20. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

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23. ALL ELECTRICAL CONDUIT & CABLE SHALL BE FULL LENGTH & SHALL BE INSTALLED IN A MANNER THAT PROVIDES FULL SUPPORT & PROTECTS FROM DAMAGE.

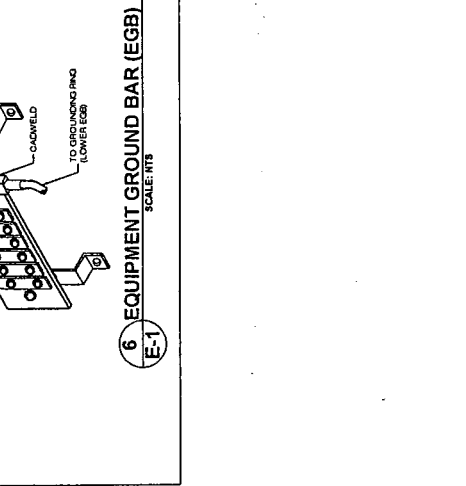
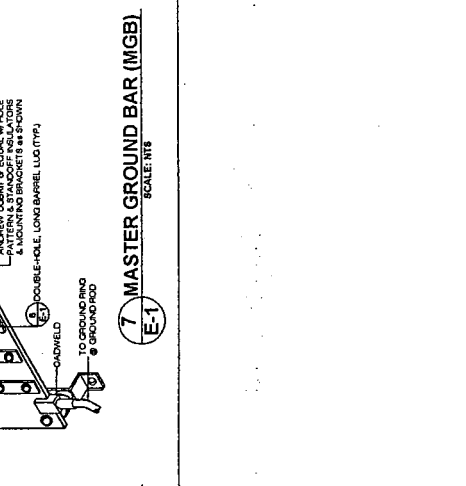
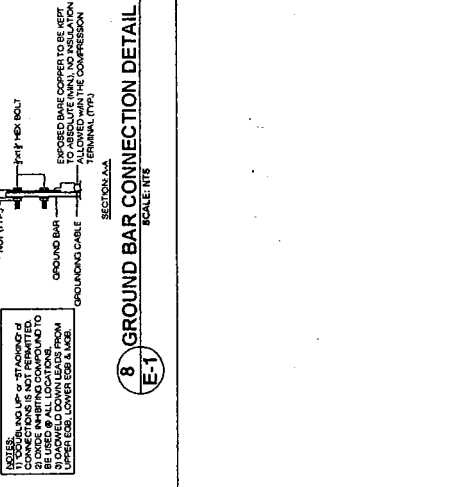
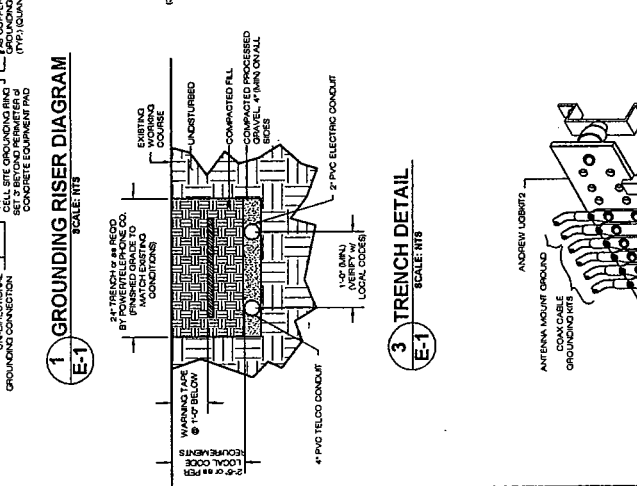
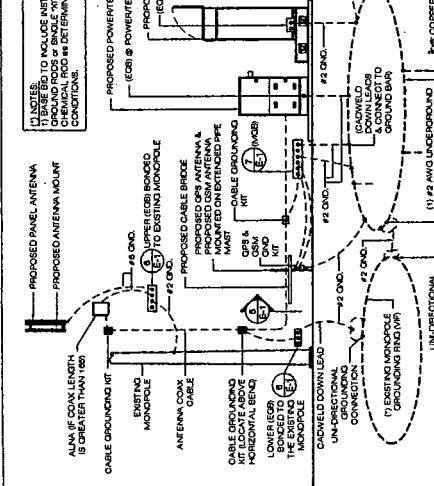
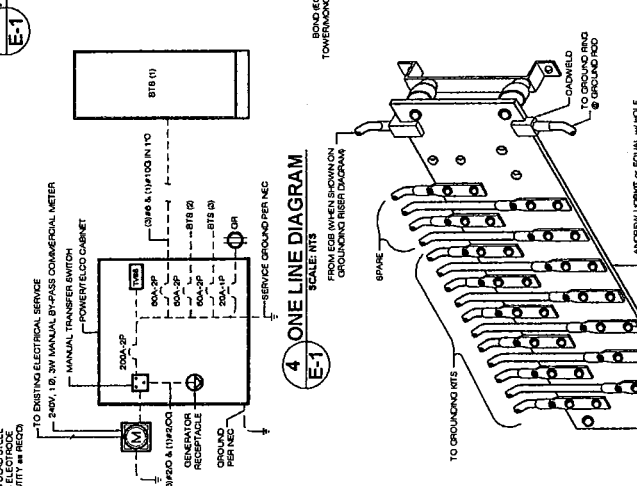
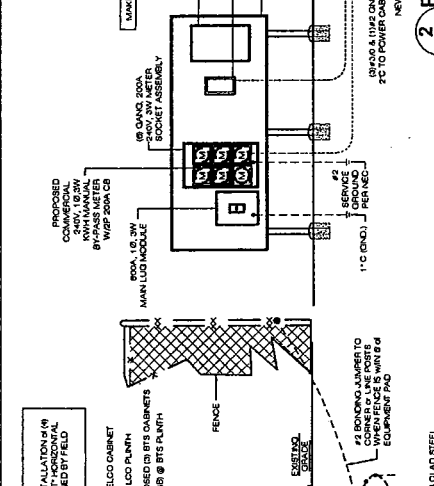
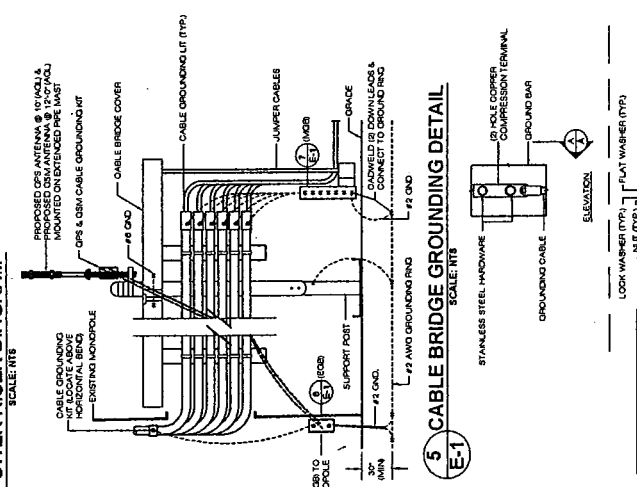
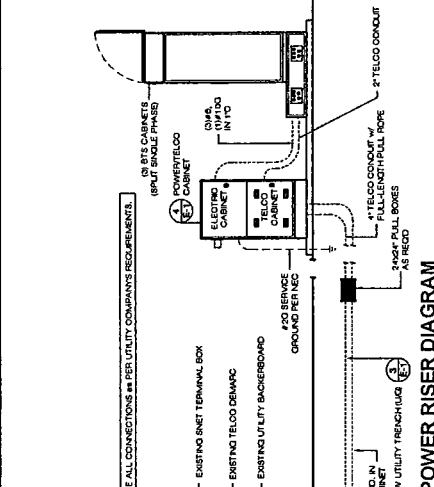


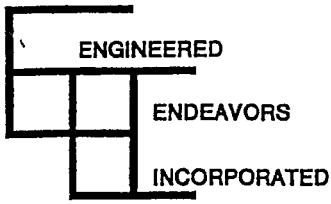
Exhibit B



RECEIVED
SEP 24 2003
CONNECTICUT
SITING COUNCIL

ENGINEERED ENDEAVORS INCORPORATED

**Sprint PCS
Structure & Foundation
Design Calculations
150' Monopole
Site: Chaplin/CT33XC583
EEI Job #: 11855-E01 Rev. 1**

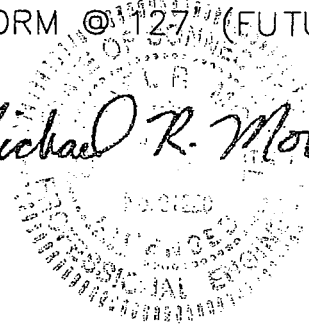
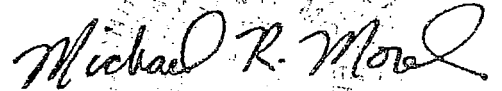


Customer SPRINT PCS/NJ By L. PADGETT 9/8/03
Date
Structure 147' MONOPOLE Checked _____ 11855
Job/Quote No.

SITE LOCATION - WINDHAM COUNTY, CT
SITE NAME - CHAPLIN, CT33XC583

ANTENNA LOADING:

- (12) DAPA 48000 DIRECTIONAL ANTENNAS
LOW PROFILE PLATFORM @ 147' (SPRINT)
- (12) DAPA 48000 DIRECTIONAL ANTENNAS
LOW PROFILE PLATFORM @ 137' (VERIZON)
- (12) DAPA 48000 DIRECTIONAL ANTENNAS
LOW PROFILE PLATFORM @ 127' (FUTURE)



DESIGN NOTES:

DESIGNED IN ACCORDANCE WITH TIA/EIA 222 F
90 MPH FASTEST MILE WIND SPEED AND
2000 IBC 110 MPH 3-SECOND GUST WIND.
1/2" RADIAL ICE.

NOTE: DESIGN IS IN COMPLIANCE WITH SPRINT
SPECIFICATION SSEO 3.001.06.001, Rev 2

NOTE: IT IS THE RESPONSIBILITY
OF THE PURCHASER TO VERIFY
THAT THE WIND LOADS AND DESIGN
CRITERIA SPECIFIED MEET THE REQUIREMENTS
OF ALL LOCAL BUILDING CODES

Engineered Endeavors Inc.

7610 Jenther Drive
Mentor, Ohio 44060
Tel (440) 918-1101 Fax (440) 918-1108

Communications Structure Nonlinear Analysis and Design Program

16:37:50 09-08-2003
Revision 1.3 - 2/07/00
Engineer: L. PADGETT

Customer SPRINT PCS/NJ
Job Name 11855, REV. 1
Structure 147' MONOPOLE
Location WINDHAM COUNTY, CT
Site CHAPLIN

OD BOT	OD TOP	NUM. SIDES	THICK INCH	TAPER IN/FT	LENGTH FT	JOINT INCH	JOINT TYPE	YIELD KSI	WEIGHT LBS	JOINT HEIGHT
31.96	21.00	18	0.1875	0.210	52.25	54.00	SLIP	65.0	2748.	96.00
41.23	30.52	18	0.2500	0.210	51.08	68.00	SLIP	65.0	4854.	50.00
50.50	39.42	18	0.3125	0.210	52.83	0.00	BASEPL	65.0	7864.	0.00
TOTAL TUBE WEIGHT								15466.	POUNDS	
POLE SHAFT LENGTH								146.00	FEET	

E = 29600.0 KSI
UNIT WGT = 0.283 LBS/CU IN
AISC constants are used for stress reductions.
TUBE SECTIONS HAVE 18 SIDES AND ARE TREATED AS ROUND
Internal bend radius = 3 X T
Tube diameters are measured flat to flat.
Tube diameters are increased by 1.020 for wind across points.
Drag coefficients are increase by 1.300 for steps on the pole.
AISC Tube Shape Coefficient of 1.000 is applied.
ORIGINAL DATA FILE NAME T:\ENG4\JOBS11\11855172
REVISED DATA FILE NAME T:\ENG4\JOBS11\11855147

APPURTENANCES

DESCRIPTION	NUM.	ELEV.	Kz	< WITHOUT ICE >			< WITH ICE >			Ca FACTOR
				AREA	WGT	Ca	AREA	WGT	Ca	
48000	12	146.	1.529	3.20	18.	1.4000	3.65	41.	1.4000	0.85
12' LOW PROFILE PLAT	1	146.	1.529	7.50	1500.	2.0000	9.20	1750.	2.0000	1.00
48000	12	136.	1.499	3.20	18.	1.4000	3.65	41.	1.4000	0.85
12' LOW PROFILE PLAT	1	136.	1.499	7.50	1500.	2.0000	9.20	1750.	2.0000	1.00
48000	12	126.	1.466	3.20	18.	1.4000	3.65	41.	1.4000	0.85
12' LOW PROFILE PLAT	1	126.	1.466	7.50	1500.	2.0000	9.20	1750.	2.0000	1.00

LOAD CASE 1

OPERATIONAL LOADING

DEAD LOAD FACTOR 1.00 WIND PSF REDUCTION 1.00 RADIAL ICE 0.00 IN.

WIND VELOCITY 50 BOTTOM 6.45 PSF TOP 9.77 PSF
 MAX BASE ROTATION 0.00 DEG

APPLIED APPURTENANCE FORCES

	ELEVATION FT	WEIGHT KIPS	WIND KIPS
48000	146.00	0.220	0.756
12' LOW PROFILE PLAT	146.00	1.500	0.248
48000	136.00	0.220	0.741
12' LOW PROFILE PLAT	136.00	1.500	0.243
48000	126.00	0.220	0.725
12' LOW PROFILE PLAT	126.00	1.500	0.238

TUBE ELEV FT	PROPERTIES		MEMBER FORCES			STRESSES		ALLOW RATIOS	TOTAL		
	DIAM IN	WALL IN	SHEAR K	BENDING K-FT	AXIAL K	AXIAL KSI	BEND. KSI		DEFL IN	TILT DEG	
146.00	21.00	0.1875	1.16	0.00	1.90	0.16	0.00	49.24	0.00	30.5	1.87
136.00	23.10	0.1875	1.16	11.56	1.90	0.14	1.81	48.08	0.04	26.6	1.85
126.00	25.20	0.1875	2.39	35.48	4.05	0.27	4.66	47.10	0.10	22.8	1.78
116.00	27.29	0.1875	3.62	71.64	6.35	0.40	8.00	46.28	0.18	19.1	1.67
106.00	29.39	0.1875	3.83	109.90	6.89	0.40	10.57	45.58	0.24	15.8	1.52
96.00	31.49	0.1875	4.04	150.32	7.48	0.41	12.58	44.96	0.29	12.8	1.34
TYPE OF JOINT: SLIP JOINT											
96.00	30.99	0.2500	4.31	150.32	8.71	0.36	9.80	48.01	0.21	12.8	1.34
83.00	33.71	0.2500	4.31	206.32	8.71	0.33	11.34	47.07	0.25	9.4	1.15
72.00	36.02	0.2500	4.58	256.72	9.78	0.35	12.35	46.38	0.27	6.9	0.97
61.00	38.33	0.2500	4.83	309.90	10.84	0.36	13.15	45.78	0.29	4.9	0.80
50.00	40.64	0.2500	5.09	365.84	11.97	0.38	13.79	45.25	0.31	3.2	0.63
TYPE OF JOINT: SLIP JOINT											
50.00	40.01	0.3125	5.33	365.84	13.97	0.36	11.44	47.63	0.25	3.2	0.63
40.00	42.11	0.3125	5.33	419.13	13.97	0.34	11.82	47.07	0.26	2.0	0.49
30.00	44.21	0.3125	5.55	474.60	15.38	0.36	12.13	46.57	0.27	1.1	0.37
20.00	46.30	0.3125	5.76	532.20	16.85	0.37	12.38	46.11	0.28	0.5	0.24
10.00	48.40	0.3125	5.98	591.98	18.39	0.39	12.60	45.69	0.28	0.1	0.12
0.00	50.50	0.3125	6.33	654.00	20.83	0.42	12.77	45.30	0.29	0.0	0.00

REACTION COMPONENTS (KIPS AND FT-KIPS)

TRANSVERSE SHEAR	VERTICAL FORCE	WIND SHEAR	MOMENT ABOUT TRANSVERSE	MOMENT ABOUT VERTICAL	MOMENT ABOUT WIND AXIS
0.000	20.833	-6.335	654.000	0.000	0.000

LOAD CASE 2

90 MPH FASTEST MILE & 110 MPH 3-SEC GUST WIND

DEAD LOAD FACTOR 1.00 WIND PSF REDUCTION 1.00 RADIAL ICE 0.00 IN.

WIND VELOCITY 90 BOTTOM 20.91 PSF TOP 31.66 PSF
 MAX BASE ROTATION 0.00 DEG

APPLIED APPURTENANCE FORCES

	ELEVATION FT	WEIGHT KIPS	WIND KIPS
48000	146.00	0.220	2.449
12' LOW PROFILE PLAT	146.00	1.500	0.804
48000	136.00	0.220	2.400
12' LOW PROFILE PLAT	136.00	1.500	0.788
48000	126.00	0.220	2.348
12' LOW PROFILE PLAT	126.00	1.500	0.771

TUBE ELEV FT	TUBE PROPERTIES		MEMBER FORCES			STRESSES			STRESS RATIOS	TOTAL	
	DIAM IN	WALL IN	SHEAR K	BENDING K-FT	AXIAL K	AXIAL KSI	BEND. KSI	ALLOW KSI		DEFL IN	TILT DEG
146.00	21.00	0.1875	3.73	0.00	1.56	0.13	0.00	49.24	0.00	97.5	6.01
136.00	23.10	0.1875	3.73	37.06	1.56	0.12	5.80	48.08	0.12	85.1	5.94
126.00	25.20	0.1875	7.72	113.82	3.36	0.23	14.94	47.10	0.32	73.0	5.74
116.00	27.29	0.1875	11.66	229.86	5.24	0.33	25.67	46.28	0.56	61.4	5.38
106.00	29.39	0.1875	12.35	352.83	5.81	0.34	33.93	45.58	0.75	50.7	4.89
96.00	31.49	0.1875	13.05	482.93	6.45	0.35	40.41	44.96	0.91	41.1	4.32
TYPE OF JOINT: SLIP JOINT											
96.00	30.99	0.2500	13.92	482.93	7.76	0.32	31.49	48.01	0.66	41.1	4.32
83.00	33.71	0.2500	13.92	663.49	7.76	0.30	36.48	47.07	0.78	30.2	3.69
72.00	36.02	0.2500	14.82	826.15	8.92	0.32	39.73	46.38	0.86	22.3	3.14
61.00	38.33	0.2500	15.64	998.03	10.07	0.34	42.34	45.78	0.93	15.7	2.58
50.00	40.64	0.2500	16.46	1178.96	11.31	0.36	44.45	45.25	0.99	10.4	2.02
TYPE OF JOINT: SLIP JOINT											
50.00	40.01	0.3125	17.26	1178.96	13.44	0.34	36.86	47.63	0.78	10.4	2.02
40.00	42.11	0.3125	17.26	1351.45	13.44	0.33	38.10	47.07	0.82	6.6	1.60
30.00	44.21	0.3125	17.97	1531.10	15.38	0.36	39.13	46.57	0.85	3.7	1.18
20.00	46.30	0.3125	18.66	1717.71	16.86	0.37	39.97	46.11	0.87	1.6	0.78
10.00	48.40	0.3125	19.37	1911.38	18.40	0.39	40.67	45.69	0.90	0.4	0.38
0.00	50.50	0.3125	20.52	2112.29	20.83	0.42	41.26	45.30	0.92	0.0	0.00

REACTION COMPONENTS (KIPS AND FT-KIPS)						
TRANSVERSE SHEAR	VERTICAL FORCE	WIND SHEAR	MOMENT ABOUT TRANSVERSE	MOMENT ABOUT VERTICAL	MOMENT ABOUT WIND AXIS	
0.000	20.835	-20.523	2112.294	0.000	0.000	

LOAD CASE 3

BASIC LOADING PLUS ICE

DEAD LOAD FACTOR 1.00 WIND PSF REDUCTION 0.75 RADIAL ICE 0.50 IN.

WIND VELOCITY 90 BOTTOM 15.68 PSF TOP 23.75 PSF
 MAX BASE ROTATION 0.00 DEG

APPLIED APPURTENANCE FORCES

	ELEVATION FT	WEIGHT KIPS	WIND KIPS
48000	146.00	0.491	2.095
12' LOW PROFILE PLAT	146.00	1.750	0.740
48000	136.00	0.491	2.053
12' LOW PROFILE PLAT	136.00	1.750	0.725
48000	126.00	0.491	2.009
12' LOW PROFILE PLAT	126.00	1.750	0.709

TUBE PROPERTIES			MEMBER FORCES			STRESSES			STRESS	TOTAL	
ELEV FT	DIAM IN	WALL IN	SHEAR K	BENDING K-FT	AXIAL K	AXIAL KSI	BEND. KSI	ALLOW KSI	RATIOS	DEFL IN	TILT DEG
146.00	21.00	0.1875	3.27	0.01	2.18	0.18	0.00	49.24	0.00	83.5	5.17
136.00	23.10	0.1875	3.27	32.58	2.18	0.16	5.10	48.08	0.11	72.8	5.11
126.00	25.20	0.1875	6.74	99.72	4.59	0.31	13.09	47.10	0.28	62.4	4.93
116.00	27.29	0.1875	10.16	200.95	7.09	0.44	22.44	46.28	0.49	52.4	4.61
106.00	29.39	0.1875	10.68	307.45	7.66	0.45	29.56	45.58	0.66	43.2	4.19
96.00	31.49	0.1875	11.22	419.32	8.29	0.45	35.08	44.96	0.79	35.0	3.70
TYPE OF JOINT: SLIP JOINT											
96.00	30.99	0.2500	11.87	419.32	9.58	0.40	27.34	48.01	0.58	35.0	3.70
83.00	33.71	0.2500	11.87	573.36	9.58	0.36	31.52	47.07	0.68	25.6	3.15
72.00	36.02	0.2500	12.54	711.17	10.72	0.38	34.20	46.38	0.74	18.9	2.67
61.00	38.33	0.2500	13.16	855.81	11.86	0.40	36.30	45.78	0.80	13.3	2.19
50.00	40.64	0.2500	13.77	1007.22	13.07	0.41	37.97	45.25	0.85	8.8	1.71
TYPE OF JOINT: SLIP JOINT											
50.00	40.01	0.3125	14.37	1007.22	15.54	0.40	31.49	47.63	0.67	8.8	1.71
40.00	42.11	0.3125	14.37	1150.90	15.54	0.38	32.45	47.07	0.70	5.6	1.35
30.00	44.21	0.3125	14.90	1299.86	16.95	0.39	33.22	46.57	0.72	3.1	1.00
20.00	46.30	0.3125	15.41	1453.99	18.42	0.41	33.83	46.11	0.74	1.4	0.66
10.00	48.40	0.3125	15.94	1613.35	19.96	0.42	34.33	45.69	0.76	0.3	0.32
0.00	50.50	0.3125	16.80	1778.06	22.40	0.45	34.73	45.30	0.77	0.0	0.00

REACTION COMPONENTS (KIPS AND FT-KIPS)

TRANSVERSE SHEAR	VERTICAL FORCE	WIND SHEAR	MOMENT ABOUT TRANSVERSE	MOMENT ABOUT VERTICAL	MOMENT ABOUT WIND AXIS
0.000	22.398	-16.801	1778.060	0.000	0.000

SUMMARY TABLE

ELEV	STRESS RATIO	AXIAL	BENDING	LOADING
146.00	0.01	1.56	0.0	2 90 MPH FASTEST MILE & 110 MPH
136.00	0.12	1.56	37.1	2 90 MPH FASTEST MILE & 110 MPH
126.00	0.32	3.36	113.8	2 90 MPH FASTEST MILE & 110 MPH
116.00	0.56	5.24	229.9	2 90 MPH FASTEST MILE & 110 MPH
106.00	0.75	5.81	352.8	2 90 MPH FASTEST MILE & 110 MPH
96.00	0.91	6.45	482.9	2 90 MPH FASTEST MILE & 110 MPH
83.00	0.78	7.76	663.5	2 90 MPH FASTEST MILE & 110 MPH
72.00	0.86	8.92	826.2	2 90 MPH FASTEST MILE & 110 MPH
61.00	0.93	10.07	998.0	2 90 MPH FASTEST MILE & 110 MPH
50.00	0.99	11.31	1179.0	2 90 MPH FASTEST MILE & 110 MPH
40.00	0.82	13.44	1351.4	2 90 MPH FASTEST MILE & 110 MPH
30.00	0.85	15.38	1531.1	2 90 MPH FASTEST MILE & 110 MPH
20.00	0.87	16.86	1717.7	2 90 MPH FASTEST MILE & 110 MPH
10.00	0.90	18.40	1911.4	2 90 MPH FASTEST MILE & 110 MPH
0.00	0.92	20.83	2112.3	2 90 MPH FASTEST MILE & 110 MPH

MAXIMUM SUPPORT MOMENT K-FT 2112.29
 CORRESPONDING AXIAL FORCE KIPS 20.83
 CORRESPONDING SHEAR FORCE KIPS 20.52

BASE PLATE AT ELEVATION 0.00 FEET

TUBE DIAMETER 50.50 INCHES
 DESIGN MOMENT 2112.3 KIP FT
 DESIGN MOMENT IS 0. DEGREES FROM THE WIND DIRECTION
 BOLTS ARE ON THE KNUCKLES OF THE TUBE

APPLIED AXIAL FORCE 20.8 KIPS
 APPLIED SHEAR 20.52 KIPS

BOLT DATA

BOLT TYPE A615 GR75
 BOLTS ARE EVENLY SPACED
 DIAMETER 2.250 INCHES
 EFFECTIVE AREA 3.250 SQ IN
 TOTAL LENGTH 6.0 FEET
 End plates are required.
 MINIMUM EMBEDMENT 7.5 FEET
 NUMBER OF BOLTS 12
 BOLT CIRCLE DIAMETER 59.00 INCHES
 ALLOWABLE STRESS 60.0 KSI
 APPLIED AXIAL STRESS 44.6 KSI
 MAX BOLT FORCE 144.9 KIPS
 BOLT BENDING STRESS 2.5 KSI
 COMBINED BOLT STRESS 47.1 KSI
 CLEARANCE UNDER PLATE 3.25 INCHES
 BOLT WEIGHT 1353.6 POUNDS

PLATE DATA

DIAMETER OF PLATE 65.00 INCHES
 MATERIAL A572 GR60
 PROVIDED THICKNESS 1.500 INCHES
 REQUIRED THICKNESS 1.389 INCHES
 BOLT HOLE DIAMETER 2.625 INCHES
 CENTER HOLE SIZE 40.00 INCHES
 NET WEIGHT 847.6 POUNDS
 RAW STOCK WEIGHT 1793.5 POUNDS
 SURFACE AREA 27.73 SQ FT
 ALLOWABLE STRESS 59.99 KSI
 MAX APPLIED STRESS 51.44 KSI

CONCRETE STRENGTH 3000. PSI

Base Plate - use 65.00 inch ROUND x 1.500 inch A572 GR60
 with (12) 2.250 diameter x 8.00 foot caged A615 GR75 bolts
 on a 59.00 inch bolt circle. End plates are required.



**ENGINEERED
ENDEAVORS
INCORPORATED**

The Experienced Point of View

7610 Jenther Drive * Mentor, OH 44060-4872
Ph: (440) 918-1101 * Ph: (888) 270-3855
Fx: (440) 918-1108 * www.engend.com

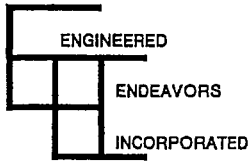
**DESIGN CALCULATIONS
FOR A
SPREAD FOOTER FOUNDATION**

**Sprint PCS
147 ft Monopole**

**Chaplin
CT33XC583
Windham County, CT**

**EEL Project Number 11855, Revision 1
September 9, 2003**

FOUNDATION DESIGN CALCULATIONS FOR A SPREAD FOOTER FOUNDATION



ENGINEERED ENDEAVORS INCORPORATED
7610 Jenther Drive * Mentor, Ohio 44060
Tel: (440) 918-1101 * Fax: (440) 918-1108

CUSTOMER: SPRINT PCS
STRUCTURE: 147' MONOPOLE
JOB NUMBER: 11855, Revision 1
LOCATION: WINDHAM COUNTY, CT
SITE NAME: CHAPLIN

SERVICE LOADS AT BASE OF THE MONOPOLE

DESIGN LOADING	
MOMENT	2112.3 ft-kips
SHEAR	20.5 kips
AXIAL	20.8 kips

ANCHOR BOLTS	QUANTITY	12.0
	LENGTH	6.0 ft
	BOLT CIRCLE	59.0 in
	PROJECTION	12.0 in

FOUNDATION PARAMETERS

MINIMUM PEDESTAL WIDTH	79.0 in
PEDESTAL PROJECTION	12.0 in
MINIMUM FOUNDATION HEIGHT	5.5 ft

	HEIGHT	WIDTH	SOIL UNIT WEIGHT	100 pcf
FOOTING	4.50 ft	24.00 ft	CONCRETE WEIGHT	150 pcf
PEDESTAL	1.00 ft	7.00 ft	ANGLE OF FRICTION	10 degrees

FOUNDATION WEIGHT	396.15 kips		
CONCRETE VOLUME	97.81 yds ³		
SOIL WEIGHT	0.00 kips	H= 0.00	
TOTAL VERTICAL LOAD	416.95 kips	B= 24.00	
KERN OF ECCENTRICITY	4.00 ft		
ACTUAL ECCENTRICITY	5.34 ft		
OVERTURNING MOMENT	2225.2 ft-kips		
RESISTING MOMENT	5003.4 ft-kips		
ALLOWABLE GROSS SOIL PRESSURE	0.0 ksf		
ALLOWABLE NET SOIL PRESSURE	6.0 ksf		

		GROSS	NET
SOIL PRESSURE	MAXIMUM q=	1.74 ksf	1.05 ksf
	MINIMUM q=	0.00 ksf	

SAFETY FACTOR **Sf = 2.25**

ULTIMATE STRENGTH DESIGN OF FOOTING

CONCRETE, psi	3000
STEEL, KSI	60

SHEAR IN FOOTING

1. CASE I - DEAD LOAD, TWO-WAY SHEAR

$$U = 1.4 * D$$

Ultimate Vertical Load, kips	583.73		
Ultimate Pressure, ksf	1.01		
Ultimate shear V, kips	461.11		
Design shear Vn, kips	4719.70		O.K.

2. CASE II - WIND LOAD, ONE-WAY SHEAR

$$U = 0.9 * D + 1.3 * W$$

Ultimate Moment, kip-ft	2892.71		
Ultimate Vertical Load, kips	375.26		
Eccentricity, ft	7.71		
Ultimate Pressure, ksf	qult= 2.43		
Dist. from edge to critical sect., ft	4.50		
Pressure distance ft	c= 12.87		
Pressure @ critical section, ksf	1.58		
Ultimate Shear, kips	216.49		
Design Shear, kips	1287.19		O.K.

FLEXURE STRENGTH DESIGN

Ultimate Moment, kip-ft	Case I	878.64		
	Case II	2569.43	ql=	0.83
Coefficient of Resistance	Rn=	51.6		
Reinforcement Ratio	r=	0.00087		
Min. Reinforcement Ratio	r min	0.00180		
Min. Steel Area, sq.in.	A1	24.88		
Type of Bars	#	8		
	Ab, in^2=	0.79		
BOTTOM	Min. Number of Bars	31.50		
	Actual Number of Bars	36.00		
	Actual Steel Area, sq.in.	28.44		
	Steel Ratio Actual	ra= 0.00206		
	Revised Coef. of Resist	Rn= 123.43		
	Design Moment, kip-ft	6142.67		
	Horizontal Spacing, in	shor= 8.06		
TOP	Min. Steel Area, sq.in	24.88		
	Min. Number of Bars	31.50		
	Actual Number of Bars	36.00		
	Top Steel Area, sq.in	28.44		
	Horizontal Spacing, in	shor= 8.06		

PEDESTAL DESIGN

Pedestal Width, in	84	Ultim. Momen	2772.7
Concrete, ksi	3		
Reinforcement, ksi	60		
Rebars , #8	44	Area, sq.in	0.79
Design Rebars	12	Area, sq.in	2.90
Minimum reinforcement ratio	0.0050	Rebar space, i	5.35
Actual reinforcement ratio	0.0049		
Concrete cover , in	4		
Rebar layout radius, in	37.50		

Bending about the major axis

No.	Angle, deg	Coord., in	Edge Dist., in	No.	Angle, deg	Coord., in	dge Dist., in
1	0	37.50	4.50	7	180	-37.50	79.50
2	30	32.48	9.52	8	210	-32.48	74.48
3	60	18.75	23.25	9	240	-18.75	60.75
4	90	0.00	42.00	10	270	0.00	42.00
5	120	-18.75	60.75	11	300	18.75	23.25
6	150	-32.48	74.48	12	330	32.48	9.52

Location of neutral axis $e=$ **8.4**
 Compression zone, $a=$ **7.14**

Compression zone			Tension zone		
No.	e	Force kips	No.	e	Force kips
1	0.0014	109.62	2	0.0004	33.72
eu= 0.003			3	0.0053	173.80
			4	0.0120	173.80
			5	0.0187	173.80
			6	0.0236	173.80
			7	0.0254	173.80
			8	0.0236	173.80
			9	0.0187	173.80
			10	0.0120	173.80
			11	0.0053	173.80
			12	0.0004	33.72
Concrete, kips		1529.39			
Total compression		1639.01	Total tension, kips		1631.65

Moment due to compression

Rebars	Force kips	Mom. Arm. in	Moment k-ft
1	109.62	37.50	342.56
Concrete	1529.39	38.43	4897.87
Total in compressio			5240.42

Moment due to tension

Rebars	Force kips	Mom. Arm. in	Moment k-ft
2	33.72	32.48	-91.26
3	173.80	18.75	-271.56
4	173.80	0.00	0.00
5	173.80	-18.75	271.56
6	173.80	-32.48	470.36
7	173.80	-37.50	543.13
8	173.80	-32.48	470.36
9	173.80	-18.75	271.56
10	173.80	0.00	0.00
11	173.80	18.75	-271.56
12	33.72	32.48	-91.26
Total in tension			1301.32

Design moment about the major axis, kip **5887.56**

Bending about the diagonal

No.	Angle, deg phi	Coord., in c1	Edge Dist., in di	No.	Angle, deg phi	Coord., in c1	dge Dist., in di
1	0	37.50	21.90	7	180	-37.50	96.90
2	30	32.48	26.92	8	210	-32.48	91.87
3	60	18.75	40.65	9	240	-18.75	78.15
4	90	0.00	59.40	10	270	0.00	59.40
5	120	-18.75	78.15	11	300	18.75	40.65
6	150	-32.48	91.87	12	330	32.48	26.92

Location of neutral axis $c=$, 27.55
 Compression zone, $a=$ 23.42

No.	c	Force kips	Tension zone	No.	e	Force kips
1	0.000615575	44.32		2		
2	6.84918E-05	5.75		3	0.0014	119.80
12	6.84918E-05	5.75	$e_y=$ 0.00207	4	0.0035	173.80
				5	0.0055	173.80
				6	0.0070	173.80
				7	0.0076	173.80
				8	0.0070	173.80
				9	0.0055	173.80
				10	0.0035	173.80
				11	0.0014	119.80
				12		
Concrete, kips		1398.37				
Total compression		1454.20	Total tension, kips			1456.2

Moment due to compression

Rebars	Force kips	Mom. Arm. in	Moment k-ft
1	44.32	37.50	138.51
2	5.75	32.48	15.57
12	5.75	32.48	15.57
Concrete	1398.37	51.59	6011.95

Total in compressio 6181.60

Design Moment, kip-ft 6383.04

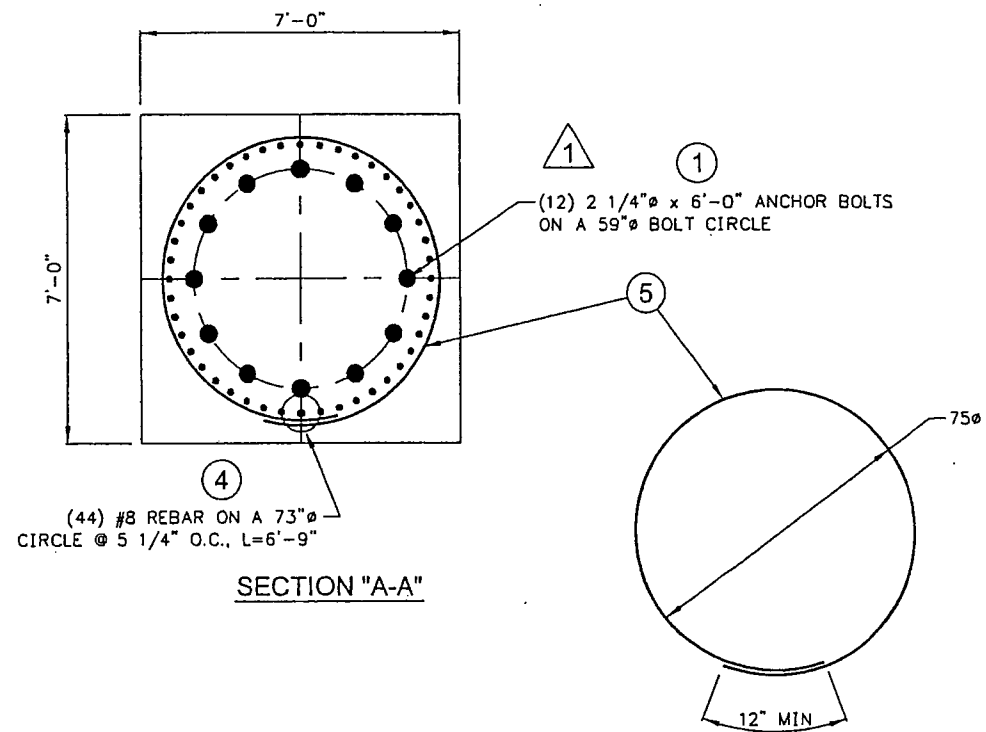
Pedestal Design Moment, kip-ft

Moment due to tension

Rebars	Force kips	Mom. Arm in	Moment k-ft
3	119.80	18.75	-187.19
4	173.80	18.75	-271.56
5	173.80	0.00	0.00
6	173.80	-18.75	271.56
7	173.80	-37.50	543.13
8	173.80	-32.48	470.36
9	173.80	-18.75	271.56
10	173.80	0.00	0.00
11	119.80	18.75	-187.19

Total in tension 910.66

5887.56



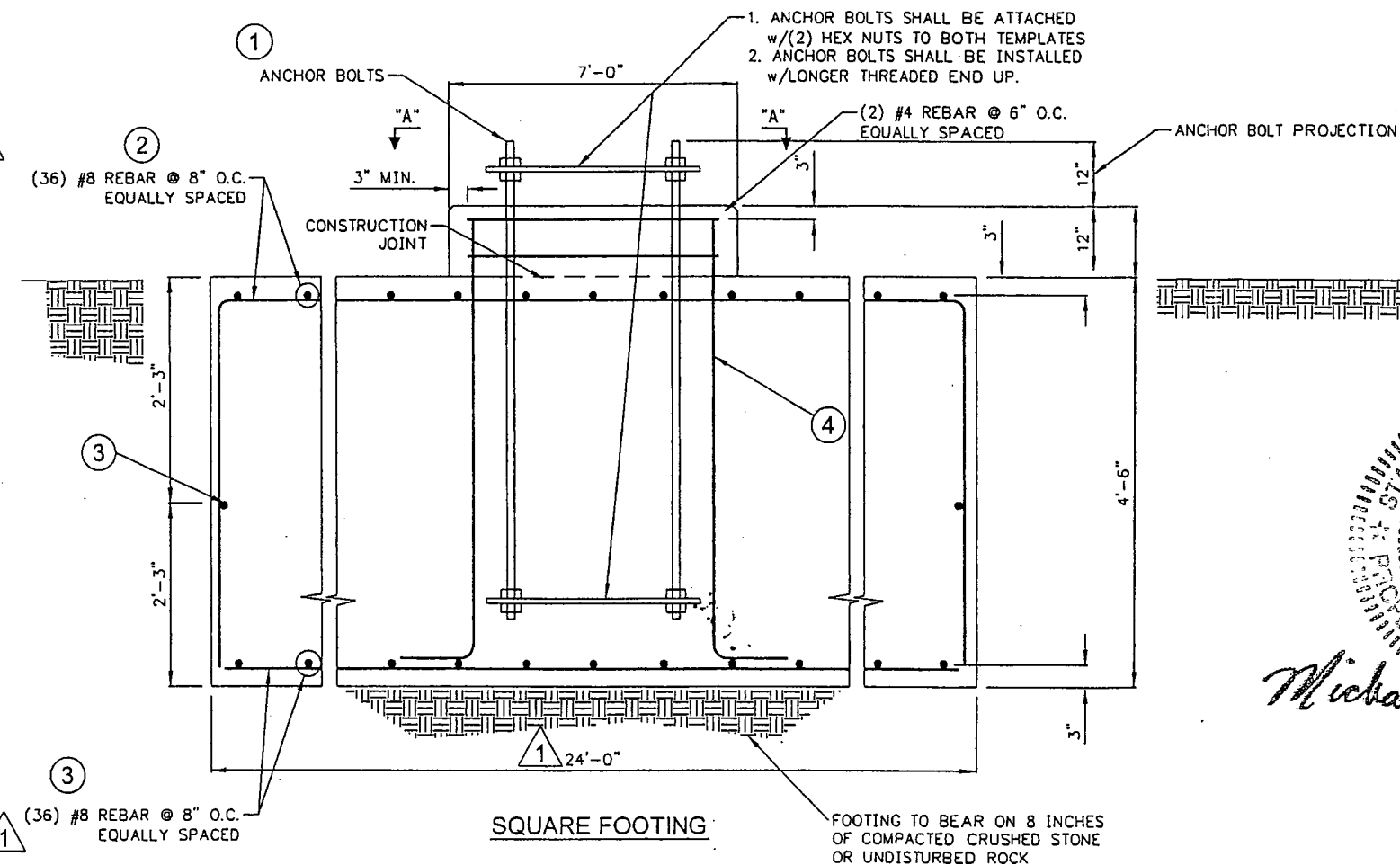
FOUNDATION LOADING	
MOMENT	2112.3 kip-ft
SHEAR	20.5 kips
AXIAL	20.8 kips

MATERIAL LIST		
ITEM	QTY.	DESCRIPTION
1	12	2 1/4" x 6'-0" (A615-GR.75) ANCHOR BOLTS
2	72	#8 REBAR x 31'-6" (ASTM A615-GR.60)
3	76	#8 REBAR x 23'-6" (ASTM A615-GR.60)
4	44	#8 REBAR x 6'-9" (ASTM A615-GR.60)
5	2	#4 REBAR x 21'-9" (ASTM A615-GR.60)

VOL. CONCRETE @ 4000 psi (TYPE II CEMENT)	99.0 yd ³
STEEL (ASTM A615-GR.60)	11650.0 lbs

GENERAL NOTES:

- FOUNDATION DESIGN IS BASE ON THE FOLLOWING: EEI JOB# 11855, DRAWING# GS54762 SOIL REPORT BY CLARENCE WELTI GEOTECHNICAL, REPORT NO. N/A - JULY 24, 2003
- FOUNDATION EMBEDMENT IS SHOWN FROM THE GROUND LEVEL AT THE TIME OF SOIL INVESTIGATION AS DEPICTED IN THE SOIL REPORT. SHOULD THE ACTUAL SOIL CONDITIONS DIFFER FROM THOSE IN THE REPORT, THE GEOTECHNICAL ENGINEER AND FOUNDATION DESIGNER SHOULD BE NOTIFIED IN ORDER TO RE-EVALUATE THE FOUNDATION DESIGN.
- SOIL REPORT SHOULD BE CONSULTED PRIOR TO CONSTRUCTION. STEEL CAISSON OR SLURRY METHOD MAY BE REQUIRED TO PREVENT SOIL FROM CAVING DURING CONSTRUCTION. THE CAISSON SHOULD BE REMOVED AFTER COMPLETION OF CONCRETING OR, IF LEFT IN THE GROUND, ALL VOIDS AROUND THE CAISSON SHALL BE FILLED WITH PRESSURIZED GROUT. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES.
- FOUNDATION EXCAVATION SHALL BE INSPECTED PRIOR TO PLACEMENT OF REINFORCEMENT AND ANCHOR BOLTS.
- SPECIAL INSPECTION OF REINFORCEMENT, ANCHOR BOLT INSTALLATION, AND CONCRETE IS REQUIRED PER 2000 IBC. FOUNDATION REINFORCEMENT AND ANCHOR BOLTS SHALL BE INSPECTED PRIOR TO PLACEMENT.
- REINFORCING STEEL SHALL COMFORM TO ASTM A615-87, F_y=60 ksi. REINFORCEMENT SHALL BE ASSEMBLED USING STEEL WIRE. WELDING IS NOT PERMITTED. MINIMUM SPLICE LENGTH: FOR NO. 6 BARS AND SMALLER - 44 x ϕ bar; FOR NO. 7 BARS AND LARGER - 55 x ϕ bar. HORIZONTAL TIES SHALL BE STAGGERED WITH NO MORE THAN 50% OF SPLICES IN ONE PLACE.
- CONCRETE MIX DESIGN AND CONSTRUCTION PROCEDURE SHALL BE IN COMPLIANCE WITH ACI 318-02, ACI 336.3R-93, AND ALL APPLICABLE STATE AND LOCAL CODES.
 - MINIMUM COMPRESSIVE STRENGTH - 4000 psi AT 28 DAYS. USE TYPE II CEMENT UNLESS STATED OTHERWISE.
 - CONCRETE MIX SHOULD HAVE A SLUMP OF 7" (± 1 ") FOR DRILLED PIER AND 3" (± 1 ") FOR MAT FOUNDATIONS.
 - FOR DRILLED PIERS ONLY THE CONCRETE OVER THE ENTIRE LENGTH OF ANCHOR BOLTS SHALL BE VIBRATED. FOR MAT FOUNDATIONS ALL CONCRETE SHALL BE VIBRATED.
- ANCHOR BOLT ORIENTATION REQUIRED PRIOR TO CONCRETE PLACEMENT. THE CONTRACTOR SHOULD CONSULT THE SITE PLAN AND MONOPOLE DRAWING FOR PROPER ACCESS PORT ORIENTATION.



STATE OF CONNECTICUT
MICHAEL R. MCKEEL
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LICENSED PROFESSIONAL ENGINEER

Michael R. McKee

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SPRINT PCS
147'-0" MONOPOLE
CHAPLIN, CT33XC583
WINDHAM COUNTY, CT

1	REVISED POLE HGT/AB'S/REACT	9/9/03	L.A.P.	
0	COMPLETED DRAWING (172' POLE)	8/9/03	L.A.P.	
REV	DESCRIPTION	DATE	DWN	CHK

SCALE: N.T.S.	PROJECT NO. 11855
SHEET 1 of 1	DRAWING NO. 11855S-147.1

Exhibit C



T-Mobile USA Inc.
100 Filley St, Bloomfield, CT 06002-1853
Phone: (860) 692-7100
Fax: (860) 692-7159

Technical Memo

To: Farrell, Christine
From: Hassan Syed - Radio Frequency Engineer
cc: Overbey Jason
Subject: Power Density Report for CT11508F
Date: December 31, 2003

1. Introduction:

This report is the result of an Electromagnetic Field Intensities (EMF - Power Densities) study for the T-Mobile PCS antenna installation on a New Monopole at 54 Paimer Road, Chaplin, CT. This study incorporates the most conservative consideration for determining the practical combined worst case power density levels that would be theoretically encountered from locations surrounding the transmitting location.

2. Discussion:

The following assumptions were used in the calculations:

- 1) The emissions from T-Mobile transmitters are in the 1935-1945 MHz frequency band.
- 2) The antenna array consists of three sectors, with 3 antennas per sector.
- 3) The model number for each antenna is EMS RR90-17-02DP.
- 4) The antenna center line height is 127 ft.
- 5) The maximum transmit power from any sector is 1744.7 Watts Effective Radiated Power (EIRP) assuming 8 channels per sector.
- 6) All the antennas are simultaneously transmitting and receiving, 24 hours a day.
- 7) Power levels emitting from the antennas are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 8) The average ground level of the studied area does not change significantly with respect to the transmitting location

Equations given in "FCC OET Bulletin 65, Edition 97-01" were then used with the above information to perform the calculations.

3. Conclusion:

Based on the above worst case assumptions, the power density calculation from the T-Mobile PCS antenna installation on a New Monopole at 54 Paimer Road, Chaplin, CT, is 0.02614 mW/cm². This value represents 2.614% of the Maximum Permissible Emission (MPE) standard of 1 milliwatt per square centimeter (mW/cm²) set forth in the FCC/ANSI/IEEE C95.1-1991. Furthermore, the proposed antenna location for T-Mobile will not interfere with existing public safety communications, AM or FM radio broadcasts, TV, Police Communications, HAM Radio communications or any other signals in the area.

The combined Power Density from other carriers is 9.16%. The combined Power Density for the site is 11.774% of the M.P.E. standard.

New England Market



Connecticut

Worst Case Power Density

Site:	CT11508F
Site Address:	54 Paimer Road
Town:	Chaplin
Tower Height:	150 ft.
Tower Style:	New Monopole
Base Station TX output	20 W
Number of channels	8
Antenna Model	EMS RR90-17-02DP
Cable Size	1 5/8 in.
Cable Length	140 ft.
Antenna Height	127.0 ft.
Ground Reflection	1.6
Frequency	1935.0 MHz
Jumper & Connector loss	4.50 dB
Antenna Gain	16.5 dBi
Cable Loss per foot	0.0116 dB
Total Cable Loss	1.6240 dB
Total Attenuation	6.1240 dB
Total EIRP per Channel	53.39 dBm
(In Watts)	218.09 W
Total EIRP per Sector	62.42 dBm
(In Watts)	1744.70 W
nsg	10.3760
Power Density (S) =	0.026144 mW/cm²
Voicestream Worst Case % MPE =	2.6144%
Equation Used :	$S = \frac{(1000)(grf)^2 (Power) 10^{(nsg/10)}}{4\pi (R)^2}$
	Office of Engineering and Technology (OET) Bulletin 65, Edition 97-01, August 1997

Co-Location Total	
Carrier	% of Standard
Verizon	5.2000 %
Cingular	
Sprint PCS	3.9600 %
AT&T Wireless	
Nextel	
Total Excluding T-Mobile	9.1600 %
T-Mobile	2.6144
Total % MPE for Site	11.7744%



100 Filley Street, Bloomfield, CT 06002
860-794-6427 fax 860-692-7159

First Selectman Rusty Lanzit
Town of Chaplin
495 Phoenixville Road
Chaplin, CT 06235

**RE: Tower Share– Existing Wireless Telecommunications Facility
Lot 54 Palmer Road, Chaplin, Connecticut**

Dear First Selectman Rusty Lanzit:

Omnipoint Communications, Inc. a.k.a. T-Mobile (formerly Voicestream Wireless Corp.) intends to co-locate antennas on the existing monopole located at Lot 54 Palmer Road, Chaplin. Attached, please find a copy of our application to the CT Siting Council.

If you have any questions or concerns, please feel free to call me at 860-794-6427, or the CT Siting Council.

Very Truly Yours

Christine Farrell
T-Mobile Real Estate and Zoning

Attachments-Application

Cc: CSC