



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

[www.ct.gov/csc](http://www.ct.gov/csc)

October 9, 2012

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **EM-VER-022-100119** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 53 Westminster Road, Canterbury, Connecticut. Extension of Time.

Dear Attorney Baldwin:

The Connecticut Siting Council (Council) considered your request for an additional extension of construction time for this exempt modification, dated September 25, 2012, and granted an additional twelve-month extension of time until February 10, 2014, to complete the construction of this project with the understanding that conditions contained in the original Council decision dated February 10, 2010 and additional conditions listed in the extension letter dated February 7, 2011 are satisfied. This extension is granted with the understanding that the Council will be notified should the applicant decide not to proceed with construction.

Sincerely,

Linda Roberts  
Executive Director

LR/CDM/laf

Enclosure: Decision Letter, dated February 10, 2010  
Extension Decision Letter, dated February 7, 2011

c: The Honorable Brian H. Sear, First Selectman, Town of Canterbury  
Steve Sadlowski, Zoning Enforcement Officer, Town of Canterbury  
Crown Castle USA, Inc.

280 Trumbull Street  
Hartford, CT 06103-3597  
Main (860) 275-8200  
Fax (860) 275-8299  
kbaldwin@rc.com  
Direct (860) 275-8345

Also admitted in Massachusetts

September 25, 2012

*Via Electronic Mail*

Linda Roberts  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

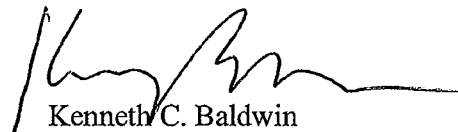
Re: **EM-VER-022-100119**  
**53 Westminster Road, Canterbury, Connecticut**

Dear Ms. Roberts:

By letter of February 10, 2010, Siting Council staff acknowledged receipt of the above-referenced exempt modification filing for Cellco's shared use of the existing tower at 53 Westminster Road in Canterbury, Connecticut. The Council's approval is due to expire on February 10, 2013. While Cellco intends to move forward with the construction, this cell site is not currently on the 2013 "build program". Cellco, therefore, requests that the Council extend the time period of this acknowledgement for an additional 12 months until February 10, 2014.

Thank you in advance for your cooperation.

Sincerely,



Kenneth C. Baldwin



Law Offices

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NEW YORK CITY

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SARASOTA

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KCB/kmd

Copy to:

Sandy M. Carter



# STATE OF CONNECTICUT

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December 8, 2011

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **EM-VER-022-100119** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 53 Westminster Road, Canterbury, Connecticut. Extension of Time.

Dear Attorney Baldwin:

The Connecticut Siting Council (Council) considered your request for an additional extension of construction time for this exempt modification, dated November 10, 2011, and granted an additional twelve-month extension of time until February 10, 2013, to complete the construction of this project with the understanding that conditions contained in the original Council decision dated February 10, 2010 and additional conditions listed in the extension letter dated February 7, 2011 are satisfied. This extension is granted with the understanding that the Council will be notified should the applicant decide not to proceed with construction.

Sincerely,

Linda Roberts  
Executive Director

LR/CDM/laf

Enclosure: Decision Letter, dated February 10, 2010  
Extension Decision Letter, dated February 7, 2011

c: The Honorable Brian H. Sear, First Selectman, Town of Canterbury  
Steve Sadlowski, Zoning Enforcement Officer, Town of Canterbury  
Crown Castle USA, Inc.

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Direct (860) 275-8345

November 10, 2011

*Via Electronic Mail*

Linda Roberts  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

Re: **EM-VER-022-100119**  
**53 Westminster Road, Canterbury, Connecticut**

Dear Ms. Roberts:

By letter of February 10, 2010, Siting Council staff acknowledged receipt of the above-referenced exempt modification filing for Cellco's shared use of the existing tower at 53 Westminster Road in Canterbury, Connecticut. The acknowledgement letter states that the validity of the staff's action will expire one year from the date of the acknowledgement letter. The Council granted Cellco a one year extension to February 10, 2012, to allow for the facility to be operational.

The purpose of this letter is to inform you that Cellco intends to move forward with the construction of this cell site, but will not do so in 2012. The construction of this facility is, however, on Cellco's construction schedule for 2013. We are, therefore, requesting that the Council staff extend the time period of its acknowledgement for an additional 12 months until February 10, 2013.

Thank you in advance for your cooperation.

Sincerely,



Kenneth C. Baldwin

KCB/kmd  
Copy to:  
Sandy M. Carter



*Law Offices*

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*Daniel F. Caruso*

*Chairman*

February 7, 2011

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **EM-VER-022-100119** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 53 Westminster Road, Canterbury, Connecticut. Extension of Time.

Dear Attorney Baldwin:

Pursuant to your request dated January 26, 2011, the Connecticut Siting Council (Council) hereby extends the time period of its acknowledgement dated February 10, 2010 (filing dated January 19, 2010) for an additional 12 months until February 10, 2012 with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated January 19, 2010. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

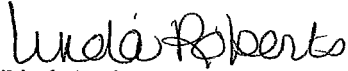


CONNECTICUT SITING COUNCIL  
*Affirmative Action / Equal Opportunity Employer*

This decision is under the exclusive jurisdiction of the Council. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,



Linda Roberts  
Executive Director

LR/CDM/laf

- c: The Honorable Brian H. Sear, First Selectman, Town of Canterbury  
Steve Sadlowski, Zoning Enforcement Officer, Town of Canterbury  
Crown Castle USA, Inc.

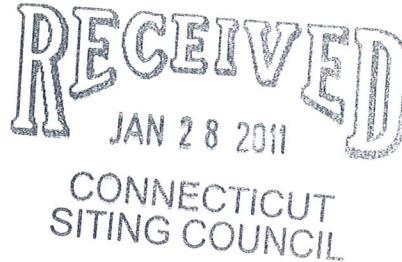
280 Trumbull Street  
Hartford, CT 06103-3597  
Main (860) 275-8200  
Fax (860) 275-8299  
kbaldwin@rc.com  
Direct (860) 275-8345

ORIGINAL

January 26, 2011

*Via Electronic Mail*

Linda Roberts  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051



Re: **EM-VER-022-100119**  
**53 Westminster Road, Canterbury, Connecticut**

Dear Ms. Roberts:

By letter of February 10, 2010, Siting Council staff acknowledged receipt of the above-referenced exempt modification filing for Cellco's shared use of the existing tower at 53 Westminster Road in Canterbury, Connecticut. The acknowledgement letter states that the validity of the staff's action will expire one year from the date of the acknowledgement letter.

The purpose of this letter is to inform you that, Cellco intends to move forward with the construction of this cell site, but will not do so in calendar year 2011. The construction of this facility is, however, on Cellco's construction schedule for 2012. We are, therefore, requesting that the Council staff extend the time period of its acknowledgement for an additional 12 months until February 10, 2012.



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*www.rc.com*

Thank you in advance for your cooperation.

Sincerely,

A handwritten signature in blue ink, appearing to read "Kenneth C. Baldwin".

Kenneth C. Baldwin

KCB/kmd  
Copy to:  
Sandy M. Carter



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Daniel F. Caruso  
Chairman

February 10, 2010

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

RE: **EM-VER-022-100119** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 53 Westminster Road, Canterbury, Connecticut.

Dear Attorney Baldwin:

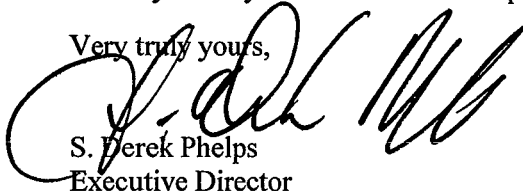
The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modifications are to be implemented as specified here and in your notice dated January 19, 2010, including the placement of all necessary equipment and shelters within the tower compound. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,

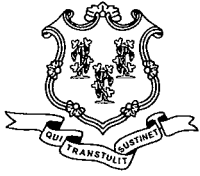


S. Derek Phelps  
Executive Director

SDP/MP/laf

c: The Honorable Brian H. Sear, First Selectman, Town of Canterbury  
Steve Sadlowski, Zoning Enforcement Officer, Town of Canterbury  
Crown Castle USA, Inc.





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January 20, 2010

The Honorable Brian H. Sear  
First Selectman  
Town of Canterbury  
P O Box 27  
Canterbury, CT 06331-0027

RE: **EM-VER-022-100119** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 53 Westminster Road, Canterbury, Connecticut.

Dear First Selectman Sear:

The Connecticut Siting Council (Council) received this request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72.

If you have any questions or comments regarding this proposal, please call me or inform the Council by February 3, 2010.

Thank you for your cooperation and consideration.

Very truly yours,

A handwritten signature in black ink, appearing to read "S. Derek Phelps".

S. Derek Phelps  
Executive Director

SDP/jbw

Enclosure: Notice of Intent

c: Steve Sadlowski, Zoning Enforcement Officer, Town of Canterbury

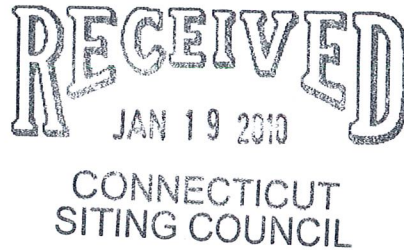
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Main (860) 275-8200  
Fax (860) 275-8299  
kbaldwin@rc.com  
Direct (860) 275-8345

ORIGINAL

January 19, 2010

*Via Hand Delivery*

S. Derek Phelps  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051



Re: **Notice of Exempt Modification  
53 Westminster Road, Canterbury, Connecticut**

Dear Mr. Phelps:

On November 7, 2001, Cellco Partnership d/b/a Verizon Wireless ("Cellco") received Connecticut Siting Council ("Council") approval to share the Crown Castle USA, Inc. ("Crown") tower (TS-VER-022-011018) at 53 Westminster Road in Canterbury, Connecticut. Cellco never installed its equipment at this facility. Cellco is now prepared to install its antennas and associated equipment at this site and submits this notice accordingly.

Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Canterbury's First Selectman, Brian H. Sear. A copy of this letter is also being sent to John R. Lemire, the owner of the property on which the tower is located.

The existing facility consists of a 180-foot self-supporting monopole tower capable of supporting multiple carriers within a fenced compound. The tower is shared by Sprint with antennas at the 180-foot level and AT&T with antennas at the 160-foot level on the tower. Cellco intends to install twelve (12) panel-type antennas at the 170-foot level on the tower and place a 12' x 30' equipment shelter on the ground within the existing fenced compound. Attached behind Tab 1 are Project Plans for the proposed Cellco facility.

The planned modifications to the Canterbury facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).



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S. Derek Phelps  
January 19, 2010  
Page 2

1. The proposed modification will not increase the overall height of the existing tower. Cellco's antennas will be mounted with their centerline at the 170-foot level on the 180-foot tower.
2. The proposed installation of a 12' x 30' equipment shelter will not require an extension of the fenced compound or lease area.
3. The proposed installation will not increase the noise levels at the facility by six decibels or more.
4. The operation of the antennas will not increase radio frequency (RF) power density levels at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. The cumulative worst-case RF power density calculations for all existing and proposed Cellco antennas would be 16.35% of the FCC standard. A copy of the cumulative power density calculations table is attached behind Tab 2.

Also attached, behind Tab 3, is a Structural Analysis confirming that the tower and foundation can support the existing and Cellco antennas and associated equipment.

For the foregoing reasons, Cellco respectfully submits that the proposed antenna installation at the facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Kenneth C. Baldwin

Attachments

Copy to:

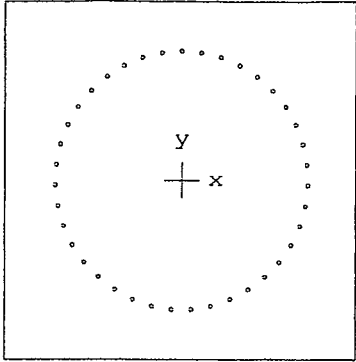
Brian H. Sear, Canterbury First Selectman  
John R. Lemire  
Sandy M. Carter





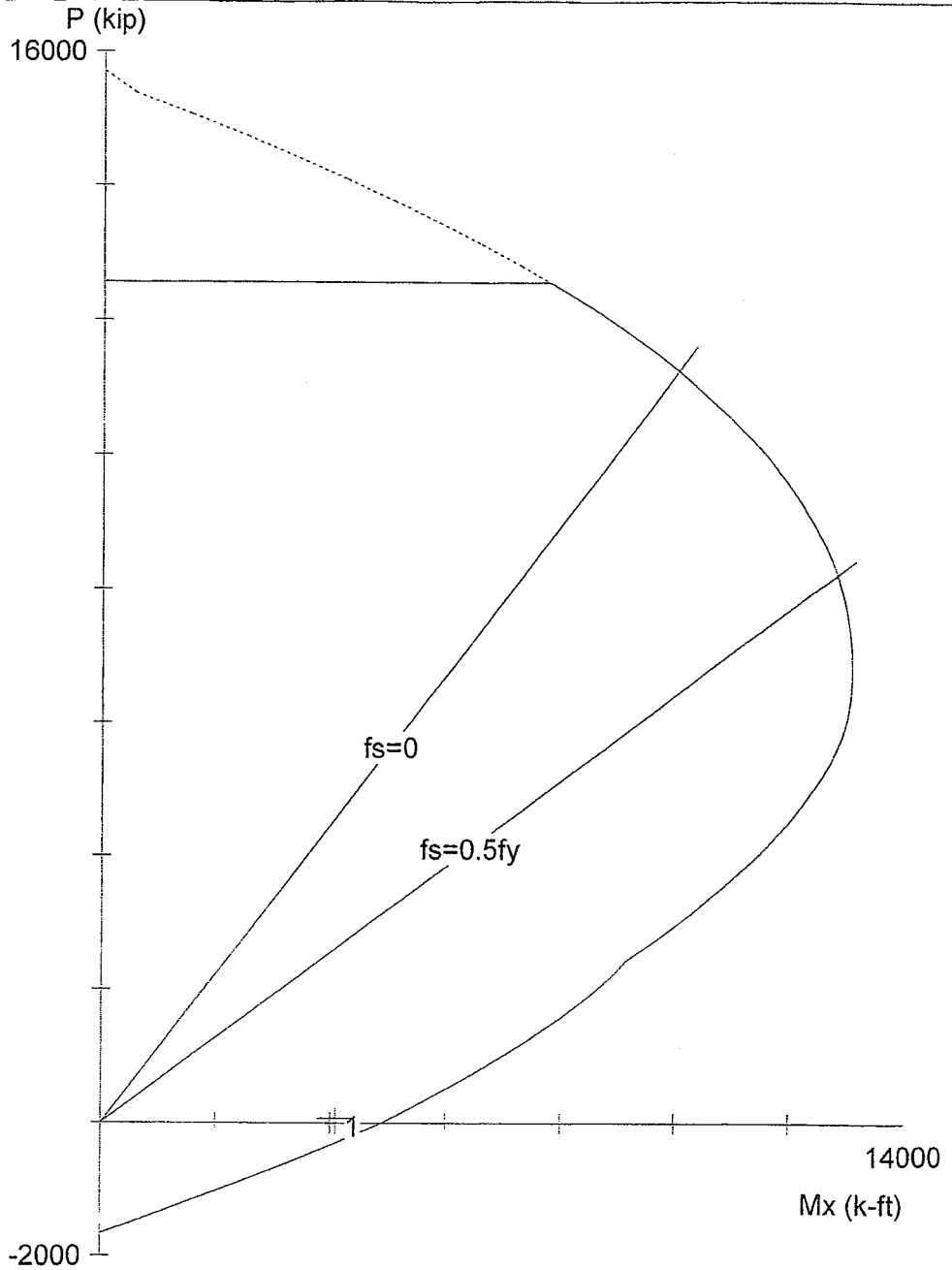






78 x 78 in

Code: ACI 318-95  
 Units: English  
 Run axis: About X-axis  
 Run option: Investigation  
 Slenderness: Not considered  
 Column type: Structural  
 Bars: ASTM A615  
 Date: 09/04/09  
 Time: 10:18:18



PCACOL V3.00 (PCA 1999) - Licensed to: Paul J. Ford and Company, Columbus, OH

File: untitled.col

Project: 37509-0930Rev1

Column:

Engineer:

$f_c = 4$  ksi

$f_y = 60$  ksi

$A_g = 6084$  in<sup>2</sup>

39 #8 bars

$E_c = 3605$  ksi

$E_s = 29000$  ksi

$A_s = 30.81$  in<sup>2</sup>

Rho = 0.51%

$f_c = 3.4$  ksi

$e_{rup} = \text{Infinity}$

$X_o = 0.00$  in

$I_x = 3.08459e+006$  in<sup>4</sup>

$e_u = 0.003$  in/in

$Y_o = 0.00$  in

$I_y = 3.08459e+006$  in<sup>4</sup>

Beta1 = 0.85

Clear spacing = 3.53 in

Clear cover = 10.38 in

General Information:

=====

File Name: untitled.col  
 Project: 37509-0930Rev1  
 Column: Engineer:  
 Code: ACI 318-95 Units: English  
  
 Run Option: Investigation Slenderness: Not considered  
 Run Axis: X-axis Column Type: Structural

Material Properties:

=====

f'c = 4 ksi fy = 60 ksi  
 Ec = 3605 ksi Es = 29000 ksi  
 fc = 3.4 ksi Rupture strain = Infinity  
 Ultimate strain = 0.003 in/in  
 Betal = 0.85

Section:

=====

Rectangular: Width = 78 in Depth = 78 in  
  
 Gross section area, Ag = 6084 in^2  
 Ix = 3.08459e+006 in^4 Iy = 3.08459e+006 in^4  
 Xo = 0 in Yo = 0 in

Reinforcement:

=====

Rebar Database: ASTM A615

Size	Diam (in)	Area (in^2)	Size	Diam (in)	Area (in^2)	Size	Diam (in)	Area (in^2)
# 3	0.38	0.11	# 4	0.50	0.20	# 5	0.63	0.31
# 6	0.75	0.44	# 7	0.88	0.60	# 8	1.00	0.79
# 9	1.13	1.00	# 10	1.27	1.27	# 11	1.41	1.56
# 14	1.69	2.25	# 18	2.26	4.00			

Confinement: Tied; #3 ties with #10 bars, #4 with larger bars.  
 phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.7

Layout: Circular  
 Pattern: All Sides Equal (Cover to transverse reinforcement)  
 Total steel area, As = 30.81 in^2 at 0.51%  
 39 #8 Cover = 10 in

Factored Loads and Moments with Corresponding Capacities: (see user's manual for notation)

=====

No.	Pu kip	Mux k-ft	fMnx k-ft	fMn/Mu
1	69.0	4096.0	5052.8	1.234

\*\*\* Program completed as requested! \*\*\*



Foundation Loads:

Tower leg compression = 34 (kips)  
 Horizontal load at top of pier = 24 (kips)  
 Overturning moment at top of pier = 3088 (ft-kips)

Design criteria:

Safety factor against overturning = 1.5

Soil Properties:

Soil density = 125 (pcf)  
 Allowable soil bearing = 6 (ksf)  
 Depth to water table = 99 (ft)

Dimensions:

Pier shape (round or square) S ("R" or "S")  
 Pier width = 6.5 (ft)  
 Pier height above grade = 0.5 (ft)  
 depth to bottom of footing = 5.5 (ft)  
 Footing thickness = 3 (ft)  
 Footing width = 24.5 (ft)  
 Footing length = 24.5 (ft)

Concrete:

Concrete strength = 4 (ksi)  
 Rebar strength = 60 (ksi)  
 ultimate load factor = 1.3

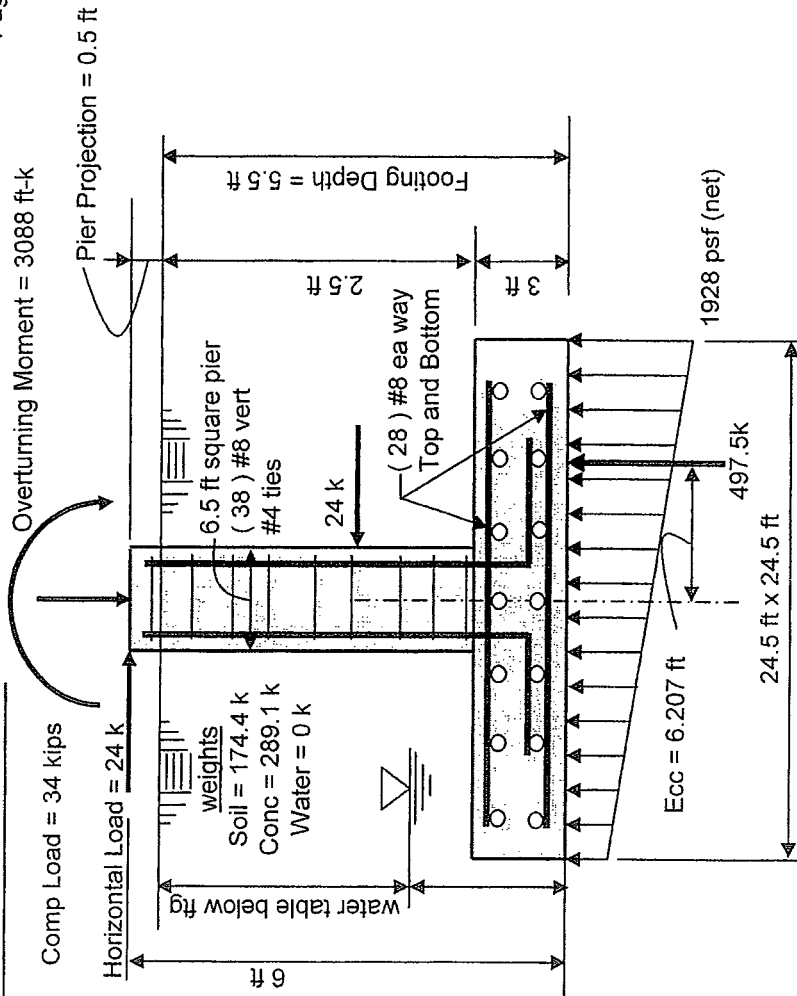
Reinforcing Steel:

Pad  
 minimum cover over rebar = 3 inches  
 size of pad rebar = #8 bar  
 quantity of pad rebar = 28 (ea direction)

Reinforcing Steel:

Pier  
 size of vert rebar in pier = #8 bar  
 vertical rebar quantity = 38  
 size of pier ties = #4 bar  
 minimum cover over rebar = 3 inches

Total volume of concrete = 71.4 cu yd



**Summary of analysis results**

Maximum Net Soil Bearing = 1.928 ksf  
 Allowable Net Soil Bearing = 6 ksf  
**Soil Bearing Stress Ratio = 0.32 Okay**

Ult Bending Shear Capacity = 126 psi  
 Ult Bending Shear Stress = 31 psi  
**Bending Shear Stress Ratio = 0.25 Okay**

Fig Overturning Resistance = 6094 ft-kips  
 Overturning Moment = 3088 ft-kips  
 Required Overturning Safety Factor = 1.5  
 Overturning Safety Factor = 1.974  
**Ratio = 0.76 Okay**

Pad Bending Moment Capacity = 3069 ft-k  
 Pad Bending Moment = 1428 ft-k  
**Bending Moment Stress Ratio = 0.47 OK**

# Stiffened or Unstiffened, UngROUTED, Circular Base Plate - Any Rod Material

## TIA Rev F

### Site Data

BU#:	
Site Name:	
App #:	
Connection Type:	Butt

Reactions		
Moment:	3088	ft-kips
Axial:	34	kips
Shear:	24	kips

### Anchor Rod Data

Qty:	16	
Diam:	2.25	in
Rod Material:	A615-J	
Strength (Fu):	100	ksi
Yield (Fy):	75	ksi
Bolt Circle:	60	in

If No stiffeners, Criteria: **AISC ASD** <-Only Applicable to Unstiffened Cases

### Anchor Rod Results

Maximum Rod Tension: 152.3 Kips  
 Allowable Tension: 195.0 Kips  
 Anchor Rod Stress Ratio: 78.1% Pass

Stiffened
Service, ASD
Fty*ASIF

### Plate Data

Diam:	65	in
Thick:	2	in
Grade:	50	ksi
Single-Rod B-eff:	9.92	in

### Base Plate Results

Base Plate Stress: 39.8 ksi  
 Allowable Plate Stress: 50.0 ksi  
 Base Plate Stress Ratio: 79.7% Pass

### Flexural Check

Stiffened
Service, ASD
0.75*Fy*ASIF
Y.L. Length:
N/A, Roark

### Stiffener Data (Welding at both sides)

Config:	1	*
Weld Type:	Both	
Groove Depth:	0.5	in **
Groove Angle:	45	degrees
Fillet H. Weld:	0.5	in
Fillet V. Weld:	0.3125	in
Width:	6	in
Height:	18	in
Thick:	1	in
Notch:	0.75	in
Grade:	50	ksi
Weld str.:	70	ksi

### Stiffener Results

Horizontal Weld : 55.0% Pass  
 Vertical Weld: 56.9% Pass  
 Plate Flex+Shear, fb/Fb+(fv/Fv)^2: 13.7% Pass  
 Plate Tension+Shear, ft/Ft+(fv/Fv)^2: 55.5% Pass  
 Plate Comp. (AISC Bracket): 56.5% Pass

### Pole Results

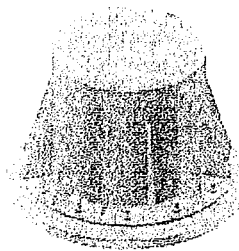
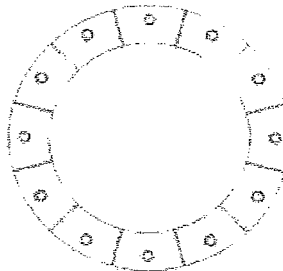
Pole Punching Shear Check: 12.8% Pass

### Pole Data

Diam:	50	in
Thick:	0.375	in
Grade:	65	ksi
# of Sides:	18	"0" IF Round
Fu	80	ksi
Reinf. Fillet Weld	0	"0" if None

### Stress Increase Factor

ASIF:	1.333
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\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes



APPENDIX C

Table C1 - List of Attached Documents

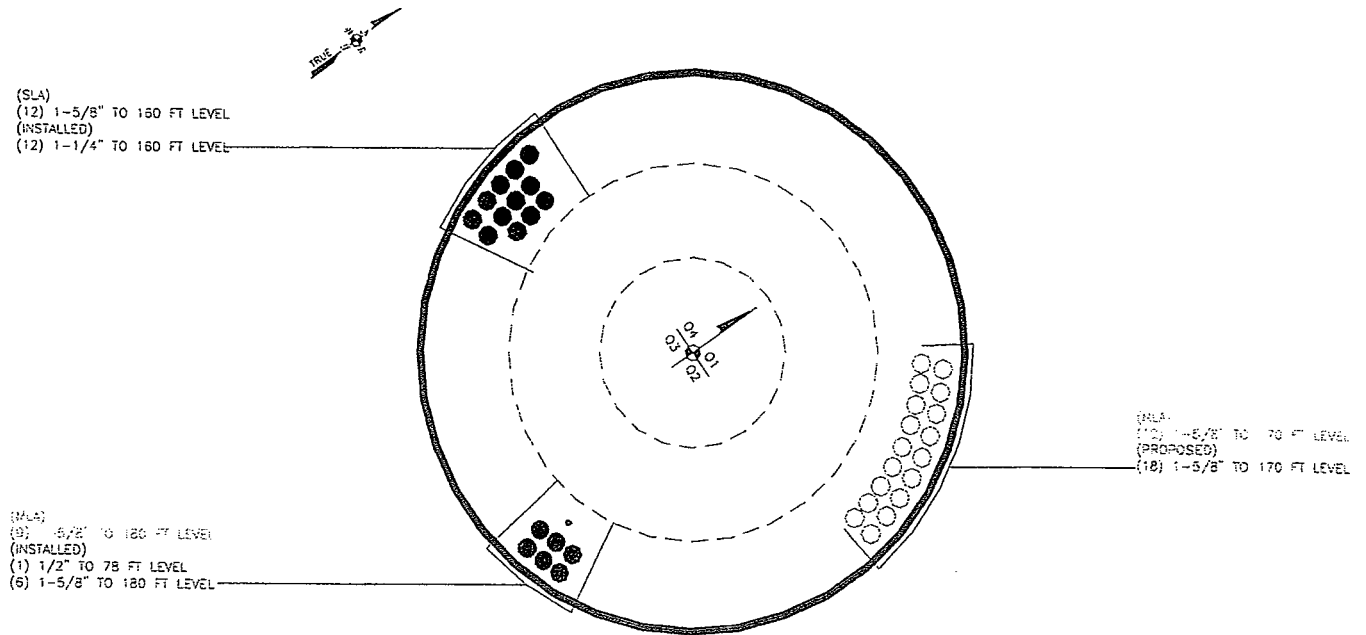
Attachment
ERI Monopole Profile
Base Plate Calculations
Foundation Calculations

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Program Version 5.3.1.0 - 10/3/2008 File:T:/375\_Crown\_Castle/2009/37509-0930 BU 876375/37509-0930Rev1 WO 292648/37509-0930Rev1.eri

APPENDIX B

Cable Routing Drawing



### Pole Interaction Design Data

Section No.	Elevation ft	Ratio	Ratio	Ratio	Ratio	Ratio	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		$P$	$f_{bx}$	$f_{by}$	$f_v$	$f_t$			
		$P_a$	$F_{bx}$	$F_{by}$	$F_v$	$F_t$			
L1	180 - 134 (1)	0.008	1.087	0.000	0.054	0.000	1.096	1.333	H1-3+VT ✓
L2	134 - 88.497 (2)	0.010	1.303	0.000	0.041	0.000	1.314	1.333	H1-3+VT ✓
L3	88.497 - 43.294 (3)	0.012	1.243	0.000	0.033	0.000	1.255	1.333	H1-3+VT ✓
L4	43.294 - 0 (4)	0.015	1.313	0.000	0.031	0.000	1.328	1.333	H1-3+VT ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
L1	180 - 134	Pole	TP26.374x17.62x0.25	1	-6.35	1051.52	82.2	Pass
L2	134 - 88.497	Pole	TP34.533x25.2403x0.3125	2	-12.86	1722.08	98.6	Pass
L3	88.497 - 43.294	Pole	TP42.51x33.084x0.375	3	-22.07	2545.39	94.2	Pass
L4	43.294 - 0	Pole	TP50x40.7609x0.375	4	-34.00	3043.84	99.6	Pass
Summary								
Pole (L4)							99.6	Pass
RATING =							99.6	Pass

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
180.00	Pipe 12' Low Profile Platform (LP 717-1)	8	187.622	9.7807	0.0003	6664
170.00	Antel BXA-70063/6CF w/ Mount Pipe	8	167.507	9.4060	0.0003	3330
161.00	(2) 7770.00 w/ Mount Pipe	8	149.714	9.0501	0.0003	1749
160.00	12' Low Profile Platform (LP 303-1)	8	147.768	9.0087	0.0003	1661
79.00	Spectracom 8225	8	33.126	3.9787	0.0003	956
78.00	3' Side Arm Mount	8	32.258	3.9183	0.0003	954

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P/P <sub>a</sub>
L1	180 - 134 (1)	TP26.374x17.62x0.25	46.00	0.00	0.0	39.000	20.2265	-6.35	788.84	0.008
L2	134 - 88.497 (2)	TP34.533x25.2403x0.3125	48.83	0.00	0.0	39.000	33.1252	-12.86	1291.88	0.010
L3	88.497 - 43.294 (3)	TP42.51x33.084x0.375	49.53	0.00	0.0	39.000	48.9621	-22.07	1909.52	0.012
L4	43.294 - 0 (4)	TP50x40.7609x0.375	48.54	0.00	0.0	39.000	58.5500	-34.00	2283.45	0.015

### Pole Bending Design Data

Section No.	Elevation ft	Size	Actual M <sub>x</sub> kip-ft	Actual f <sub>bx</sub> ksi	Allow. F <sub>bx</sub> ksi	Ratio f <sub>bx</sub> /F <sub>bx</sub>	Actual M <sub>y</sub> kip-ft	Actual f <sub>by</sub> ksi	Allow. F <sub>by</sub> ksi	Ratio f <sub>by</sub> /F <sub>by</sub>
L1	180 - 134 (1)	TP26.374x17.62x0.25	448.55	42.389	39.000	1.087	0.00	0.000	39.000	0.000
L2	134 - 88.497 (2)	TP34.533x25.2403x0.3125	1154.6	50.832	39.000	1.303	0.00	0.000	39.000	0.000
L3	88.497 - 43.294 (3)	TP42.51x33.084x0.375	2005.9	48.493	39.000	1.243	0.00	0.000	39.000	0.000
L4	43.294 - 0 (4)	TP50x40.7609x0.375	3033.8	51.214	39.000	1.313	0.00	0.000	39.000	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V K	Actual f <sub>v</sub> ksi	Allow. F <sub>v</sub> ksi	Ratio f <sub>v</sub> /F <sub>v</sub>	Actual T kip-ft	Actual f <sub>t</sub> ksi	Allow. F <sub>t</sub> ksi	Ratio f <sub>t</sub> /F <sub>t</sub>
L1	180 - 134 (1)	TP26.374x17.62x0.25	14.21	0.702	26.000	0.054	0.00	0.000	26.000	0.000
L2	134 - 88.497 (2)	TP34.533x25.2403x0.3125	17.52	0.529	26.000	0.041	0.00	0.000	26.000	0.000
L3	88.497 - 43.294 (3)	TP42.51x33.084x0.375	20.82	0.425	26.000	0.033	0.00	0.000	26.000	0.000
L4	43.294 - 0 (4)	TP50x40.7609x0.375	23.67	0.404	26.000	0.031	0.00	0.000	26.000	0.000

31	Yes	5	0.00000001	0.00040313
32	Yes	5	0.00000001	0.00040236
33	Yes	4	0.00000001	0.00056461
34	Yes	5	0.00000001	0.00040236
35	Yes	5	0.00000001	0.00040313
36	Yes	4	0.00000001	0.00056489
37	Yes	5	0.00000001	0.00040208
38	Yes	5	0.00000001	0.00040285

**Maximum Tower Deflections - Service Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 134	65.493	33	3.4104	0.0001
L2	137.33 - 88.497	37.067	33	2.7542	0.0001
L3	92.827 - 43.294	16.147	33	1.6938	0.0001
L4	48.544 - 0	4.339	33	0.8335	0.0001

**Critical Deflections and Radius of Curvature - Service Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
183.00	(2) FV65-14-00NA2 w/Mount Pipe	33	65.493	3.4104	0.0001	18204
180.00	12' Low Profile Platform (LP 717-1)	33	65.493	3.4104	0.0001	18204
170.00	Antel BXA-70063/6CF w/ Mount Pipe	33	58.451	3.2774	0.0001	9101
161.00	(2) 7770.00 w/ Mount Pipe	33	52.223	3.1518	0.0001	4789
160.00	12' Low Profile Platform (LP 303-1)	33	51.542	3.1372	0.0001	4549
79.00	Spectracom 8225	33	11.519	1.3602	0.0001	2720
78.00	3' Side Arm Mount	33	11.217	1.3375	0.0001	2714

**Maximum Tower Deflections - Design Wind**

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 134	187.622	8	9.7807	0.0003
L2	137.33 - 88.497	106.386	8	7.9053	0.0003
L3	92.827 - 43.294	46.418	8	4.8686	0.0003
L4	48.544 - 0	12.487	8	2.3983	0.0002

**Critical Deflections and Radius of Curvature - Design Wind**

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
183.00	(2) FV65-14-00NA2 w/Mount	8	187.622	9.7807	0.0003	6664



Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
13	-11.82	-34.29	-20.47	11.82	34.29	20.47	0.000%
14	0.00	-41.30	0.00	0.00	41.30	0.00	0.000%
15	0.00	-41.30	-19.13	0.00	41.30	19.13	0.000%
16	9.56	-41.30	-16.56	-9.56	41.30	16.56	0.000%
17	16.56	-41.30	-9.56	-16.56	41.30	9.56	0.000%
18	19.13	-41.30	0.00	-19.13	41.30	-0.00	0.000%
19	16.56	-41.30	9.56	-16.56	41.30	-9.56	0.000%
20	9.56	-41.30	16.56	-9.56	41.30	-16.56	0.000%
21	0.00	-41.30	19.13	0.00	41.30	-19.13	0.000%
22	-9.56	-41.30	16.56	9.56	41.30	-16.56	0.000%
23	-16.56	-41.30	9.56	16.56	41.30	-9.56	0.000%
24	-19.13	-41.30	0.00	19.13	41.30	-0.00	0.000%
25	-16.56	-41.30	-9.56	16.56	41.30	9.56	0.000%
26	-9.56	-41.30	-16.56	9.56	41.30	16.56	0.000%
27	0.00	-34.29	-8.18	0.00	34.29	8.18	0.000%
28	4.09	-34.29	-7.08	-4.09	34.29	7.08	0.000%
29	7.08	-34.29	-4.09	-7.08	34.29	4.09	0.000%
30	8.18	-34.29	0.00	-8.18	34.29	-0.00	0.000%
31	7.08	-34.29	4.09	-7.08	34.29	-4.09	0.000%
32	4.09	-34.29	7.08	-4.09	34.29	-7.08	0.000%
33	0.00	-34.29	8.18	0.00	34.29	-8.18	0.000%
34	-4.09	-34.29	7.08	4.09	34.29	-7.08	0.000%
35	-7.08	-34.29	4.09	7.08	34.29	-4.09	0.000%
36	-8.18	-34.29	0.00	8.18	34.29	-0.00	0.000%
37	-7.08	-34.29	-4.09	7.08	34.29	4.09	0.000%
38	-4.09	-34.29	-7.08	4.09	34.29	7.08	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00001142
3	Yes	6	0.00000001	0.00022767
4	Yes	6	0.00000001	0.00022740
5	Yes	5	0.00000001	0.00001288
6	Yes	6	0.00000001	0.00022775
7	Yes	6	0.00000001	0.00022748
8	Yes	5	0.00000001	0.00001142
9	Yes	6	0.00000001	0.00022748
10	Yes	6	0.00000001	0.00022775
11	Yes	5	0.00000001	0.00001288
12	Yes	6	0.00000001	0.00022740
13	Yes	6	0.00000001	0.00022767
14	Yes	4	0.00000001	0.00000001
15	Yes	5	0.00000001	0.00005234
16	Yes	6	0.00000001	0.00078503
17	Yes	6	0.00000001	0.00078415
18	Yes	5	0.00000001	0.00005442
19	Yes	6	0.00000001	0.00078535
20	Yes	6	0.00000001	0.00078447
21	Yes	5	0.00000001	0.00005234
22	Yes	6	0.00000001	0.00078447
23	Yes	6	0.00000001	0.00078535
24	Yes	5	0.00000001	0.00005442
25	Yes	6	0.00000001	0.00078415
26	Yes	6	0.00000001	0.00078503
27	Yes	4	0.00000001	0.00056450
28	Yes	5	0.00000001	0.00040285
29	Yes	5	0.00000001	0.00040208
30	Yes	4	0.00000001	0.00056489

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overtuning Moment, M <sub>x</sub>	Overtuning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 0 deg - No Ice	34.29	0.00	-23.64	-3087.46	0.00	0.00
Dead+Wind 30 deg - No Ice	34.29	11.82	-20.47	-2673.81	-1543.76	0.06
Dead+Wind 60 deg - No Ice	34.29	20.47	-11.82	-1543.70	-2673.87	0.11
Dead+Wind 90 deg - No Ice	34.29	23.64	0.00	0.06	-3087.52	0.12
Dead+Wind 120 deg - No Ice	34.29	20.47	11.82	1543.82	-2673.87	0.11
Dead+Wind 150 deg - No Ice	34.29	11.82	20.47	2673.93	-1543.76	0.06
Dead+Wind 180 deg - No Ice	34.29	0.00	23.64	3087.57	0.00	0.00
Dead+Wind 210 deg - No Ice	34.29	-11.82	20.47	2673.93	1543.76	-0.06
Dead+Wind 240 deg - No Ice	34.29	-20.47	11.82	1543.82	2673.87	-0.11
Dead+Wind 270 deg - No Ice	34.29	-23.64	0.00	0.06	3087.52	-0.12
Dead+Wind 300 deg - No Ice	34.29	-20.47	-11.82	-1543.70	2673.87	-0.11
Dead+Wind 330 deg - No Ice	34.29	-11.82	-20.47	-2673.81	1543.76	-0.06
Dead+Ice	41.30	0.00	0.00	0.09	0.00	0.00
Dead+Wind 0 deg+Ice	41.30	0.00	-19.13	-2601.30	0.00	0.00
Dead+Wind 30 deg+Ice	41.30	9.56	-16.56	-2252.79	-1300.70	0.06
Dead+Wind 60 deg+Ice	41.30	16.56	-9.56	-1300.61	-2252.88	0.11
Dead+Wind 90 deg+Ice	41.30	19.13	0.00	0.09	-2601.40	0.12
Dead+Wind 120 deg+Ice	41.30	16.56	9.56	1300.80	-2252.88	0.11
Dead+Wind 150 deg+Ice	41.30	9.56	16.56	2252.98	-1300.70	0.06
Dead+Wind 180 deg+Ice	41.30	0.00	19.13	2601.49	0.00	0.00
Dead+Wind 210 deg+Ice	41.30	-9.56	16.56	2252.98	1300.70	-0.06
Dead+Wind 240 deg+Ice	41.30	-16.56	9.56	1300.80	2252.88	-0.11
Dead+Wind 270 deg+Ice	41.30	-19.13	0.00	0.09	2601.40	-0.12
Dead+Wind 300 deg+Ice	41.30	-16.56	-9.56	-1300.61	2252.88	-0.11
Dead+Wind 330 deg+Ice	41.30	-9.56	-16.56	-2252.79	1300.70	-0.06
Dead+Wind 0 deg - Service	34.29	0.00	-8.18	-1072.09	0.00	0.00
Dead+Wind 30 deg - Service	34.29	4.09	-7.08	-928.47	-536.08	0.02
Dead+Wind 60 deg - Service	34.29	7.08	-4.09	-536.03	-928.52	0.04
Dead+Wind 90 deg - Service	34.29	8.18	0.00	0.06	-1072.15	0.04
Dead+Wind 120 deg - Service	34.29	7.08	4.09	536.14	-928.52	0.04
Dead+Wind 150 deg - Service	34.29	4.09	7.08	928.58	-536.08	0.02
Dead+Wind 180 deg - Service	34.29	0.00	8.18	1072.21	0.00	0.00
Dead+Wind 210 deg - Service	34.29	-4.09	7.08	928.58	536.08	-0.02
Dead+Wind 240 deg - Service	34.29	-7.08	4.09	536.14	928.52	-0.04
Dead+Wind 270 deg - Service	34.29	-8.18	0.00	0.06	1072.15	-0.04
Dead+Wind 300 deg - Service	34.29	-7.08	-4.09	-536.03	928.52	-0.04
Dead+Wind 330 deg - Service	34.29	-4.09	-7.08	-928.47	536.08	-0.02

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-34.29	0.00	0.00	34.29	0.00	0.000%
2	0.00	-34.29	-23.64	0.00	34.29	23.64	0.000%
3	11.82	-34.29	-20.47	-11.82	34.29	20.47	0.000%
4	20.47	-34.29	-11.82	-20.47	34.29	11.82	0.000%
5	23.64	-34.29	0.00	-23.64	34.29	0.00	0.000%
6	20.47	-34.29	11.82	-20.47	34.29	-11.82	0.000%
7	11.82	-34.29	20.47	-11.82	34.29	-20.47	0.000%
8	0.00	-34.29	23.64	0.00	34.29	-23.64	0.000%
9	-11.82	-34.29	20.47	11.82	34.29	-20.47	0.000%
10	-20.47	-34.29	11.82	20.47	34.29	-11.82	0.000%
11	-23.64	-34.29	0.00	23.64	34.29	0.00	0.000%
12	-20.47	-34.29	-11.82	20.47	34.29	11.82	0.000%

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	180 - 134	Pole	Max Tension	33	0.00	0.00	0.00
			Max. Compression	14	-12.02	0.00	0.00
			Max. Mx	5	-6.35	-448.55	-0.00
			Max. My	8	-6.35	0.00	-448.55
			Max. Vy	5	14.21	-448.55	-0.00
			Max. Vx	8	14.21	0.00	-448.55
			Max. Torque	17			0.00
L2	134 - 88.497	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-18.91	0.00	0.00
			Max. Mx	5	-12.86	-1154.64	-0.01
			Max. My	8	-12.86	0.00	-1154.64
			Max. Vy	5	17.52	-1154.64	-0.01
			Max. Vx	8	17.52	0.00	-1154.64
			Max. Torque	5			0.00
L3	88.497 - 43.294	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-28.57	0.00	-0.09
			Max. Mx	5	-22.07	-2005.85	-0.06
			Max. My	8	-22.07	0.00	-2005.91
			Max. Vy	5	20.82	-2005.85	-0.06
			Max. Vx	8	20.82	0.00	-2005.91
			Max. Torque	5			-0.13
L4	43.294 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	14	-41.30	0.00	-0.09
			Max. Mx	5	-34.27	-3087.52	-0.06
			Max. My	8	-34.27	0.00	-3087.57
			Max. Vy	5	23.67	-3087.52	-0.06
			Max. Vx	8	23.67	0.00	-3087.57
			Max. Torque	5			-0.13

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	21	41.30	0.00	-19.13
	Max. H <sub>x</sub>	11	34.29	23.64	0.00
	Max. H <sub>z</sub>	2	34.29	0.00	23.64
	Max. M <sub>x</sub>	2	3087.46	0.00	23.64
	Max. M <sub>z</sub>	5	3087.52	-23.64	0.00
	Max. Torsion	11	0.12	23.64	0.00
	Min. Vert	1	34.29	0.00	0.00
	Min. H <sub>x</sub>	5	34.29	-23.64	0.00
	Min. H <sub>z</sub>	8	34.29	0.00	-23.64
	Min. M <sub>x</sub>	8	-3087.57	0.00	-23.64
	Min. M <sub>z</sub>	11	-3087.52	23.64	0.00
	Min. Torsion	5	-0.12	-23.64	0.00

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	34.29	0.00	0.00	0.05	0.00	0.00

### Tower Pressure - Service

$G_H = 1.690$

Section Elevation	z	$K_z$	$q_z$	$A_G$	F a c e	$A_F$	$A_R$	$A_{leg}$	Leg %	$C_A A_A$ In Face	$C_A A_A$ Out Face
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>
L1 180.00-134.00	155.71	1.558	10	84.322	A	0.000	84.322	84.322	100.00	0.000	0.000
					B	0.000	84.322	100.00	0.000	0.000	
					C	0.000	84.322	100.00	0.000	0.000	
L2 134.00-88.50	110.49	1.412	9	114.52	A	0.000	114.529	114.529	100.00	0.000	0.000
					B	0.000	114.529	100.00	0.000	0.000	
					C	0.000	114.529	100.00	0.000	0.000	
L3 88.50-43.29	65.61	1.217	8	143.93	A	0.000	143.930	143.930	100.00	0.000	0.000
					B	0.000	143.930	100.00	0.000	0.000	
					C	0.000	143.930	100.00	0.000	0.000	
L4 43.29-0.00	21.00	1	6	165.52	A	0.000	165.528	165.528	100.00	0.000	0.000
					B	0.000	165.528	100.00	0.000	0.000	
					C	0.000	165.528	100.00	0.000	0.000	

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice
15	Dead+Wind 0 deg+Ice
16	Dead+Wind 30 deg+Ice
17	Dead+Wind 60 deg+Ice
18	Dead+Wind 90 deg+Ice
19	Dead+Wind 120 deg+Ice
20	Dead+Wind 150 deg+Ice
21	Dead+Wind 180 deg+Ice
22	Dead+Wind 210 deg+Ice
23	Dead+Wind 240 deg+Ice
24	Dead+Wind 270 deg+Ice
25	Dead+Wind 300 deg+Ice
26	Dead+Wind 330 deg+Ice
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K	
3' Side Arm Mount	C	From Face	0.00	0.0000	78.00	1/2"	0.60	0.60	0.01
			0.00			Ice			
			0.00			No Ice	0.76	0.76	0.03
			0.00			1/2"	0.96	0.96	0.04
			0.00						
			0.00						

\*\*

### Tower Pressures - No Ice

$G_H = 1.690$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L1 180.00-134.00	155.71	1.558	29	84.322	A	0.000	84.322	84.322	100.00	0.000	0.000
					B	0.000	84.322	100.00	0.000	0.000	
					C	0.000	84.322	100.00	0.000	0.000	
L2 134.00-88.50	110.49	1.412	26	114.529	A	0.000	114.529	114.529	100.00	0.000	0.000
					B	0.000	114.529	100.00	0.000	0.000	
					C	0.000	114.529	100.00	0.000	0.000	
L3 88.50-43.29	65.61	1.217	22	143.930	A	0.000	143.930	143.930	100.00	0.000	0.000
					B	0.000	143.930	100.00	0.000	0.000	
					C	0.000	143.930	100.00	0.000	0.000	
L4 43.29-0.00	21.00	1	18	165.528	A	0.000	165.528	165.528	100.00	0.000	0.000
					B	0.000	165.528	100.00	0.000	0.000	
					C	0.000	165.528	100.00	0.000	0.000	

### Tower Pressure - With Ice

$G_H = 1.690$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	t <sub>z</sub> in	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
L1 180.00-134.00	155.71	1.558	22	0.5000	88.155	A	0.000	88.155	88.155	100.00	0.000	0.000
						B	0.000	88.155	100.00	0.000	0.000	
						C	0.000	88.155	100.00	0.000	0.000	
L2 134.00-88.50	110.49	1.412	20	0.5000	118.321	A	0.000	118.321	118.321	100.00	0.000	0.000
						B	0.000	118.321	100.00	0.000	0.000	
						C	0.000	118.321	100.00	0.000	0.000	
L3 88.50-43.29	65.61	1.217	17	0.5000	147.697	A	0.000	147.697	147.697	100.00	0.000	0.000
						B	0.000	147.697	100.00	0.000	0.000	
						C	0.000	147.697	100.00	0.000	0.000	
L4 43.29-0.00	21.00	1	14	0.5000	169.135	A	0.000	169.135	169.135	100.00	0.000	0.000
						B	0.000	169.135	100.00	0.000	0.000	
						C	0.000	169.135	100.00	0.000	0.000	

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K
Mount Pipe			0.00 0.00			1/2" Ice	8.57 7.13	0.13
Antel BXA-70063/6CF w/ Mount Pipe	B	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	7.99 8.57 7.13	0.06 0.13
Antel BXA-70063/6CF w/ Mount Pipe	C	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	7.99 8.57 7.13	0.06 0.13
Antel BXA-185063/12CF w/Mount Pipe	A	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.77 5.22 4.23	0.02 0.05
Antel BXA-185063/12CF w/Mount Pipe	B	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.77 5.22 4.23	0.02 0.05
Antel BXA-185063/12CF w/Mount Pipe	C	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.77 5.22 4.23	0.02 0.05
(2) Antel LPA-80080/6CF w/mount pipe	A	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.47 4.95 11.93	0.06 0.12
(2) Antel LPA-80080/6CF w/mount pipe	B	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.47 4.95 11.93	0.06 0.12
(2) Antel LPA-80080/6CF w/mount pipe	C	From Face	4.00 0.00 0.00	0.0000	170.00	No Ice 1/2" Ice	4.47 4.95 11.93	0.06 0.12
12' Low Profile Platform (LP 303-1)	C	None		0.0000	170.00	No Ice 1/2" Ice	14.66 18.87 18.87	1.10 1.70
***								
(2) 7770.00 w/ Mount Pipe	A	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	6.12 6.63 5.01	0.06 0.10
(2) 7770.00 w/ Mount Pipe	B	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	6.12 6.63 5.01	0.06 0.10
(2) 7770.00 w/ Mount Pipe	C	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	6.12 6.63 5.01	0.06 0.10
(2) LGP21401	A	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	1.29 1.45 0.31	0.01 0.02
(2) LGP21401	B	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	1.29 1.45 0.31	0.01 0.02
(2) LGP21401	C	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	1.29 1.45 0.31	0.01 0.02
(2) Powerwave LGP21901	A	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	0.28 0.36 0.18	0.01 0.01
(2) Powerwave LGP21901	B	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	0.28 0.36 0.18	0.01 0.01
(2) Powerwave LGP21901	C	From Face	4.00 0.00 0.00	0.0000	161.00	No Ice 1/2" Ice	0.28 0.36 0.18	0.01 0.01
12' Low Profile Platform (LP 303-1)	C	None		0.0000	160.00	No Ice 1/2" Ice	14.66 18.87 18.87	1.10 1.70
**								
Spectracom 8225	C	From Face	3.00	0.0000	79.00	No Ice	0.45 0.45	0.00

Tower Sectio n	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	1.44

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Sectio n	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.00-134.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	1.14
L2	134.00-88.50	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	1.51
L3	88.50-43.29	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	1.50
L4	43.29-0.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	1.44

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
L1	180.00-134.00	0.0000	0.0000	0.0000	0.0000
L2	134.00-88.50	0.0000	0.0000	0.0000	0.0000
L3	88.50-43.29	0.0000	0.0000	0.0000	0.0000
L4	43.29-0.00	0.0000	0.0000	0.0000	0.0000

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustmen t	Placement ft	C <sub>A</sub> A <sub>A</sub> Front ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Side ft <sup>2</sup>	Weight K	
(2) FV65-14-00NA2 w/Mount Pipe	A	From Face	4.00	0.0000	183.00	No Ice	8.64	6.95	0.06
			0.00			1/2"	9.29	8.13	0.12
			0.00			Ice			
(2) FV65-14-00NA2 w/Mount Pipe	B	From Face	4.00	0.0000	183.00	No Ice	8.64	6.95	0.06
			0.00			1/2"	9.29	8.13	0.12
			0.00			Ice			
(2) FV65-14-00NA2 w/Mount Pipe	C	From Face	4.00	0.0000	183.00	No Ice	8.64	6.95	0.06
			0.00			1/2"	9.29	8.13	0.12
			0.00			Ice			
12' Low Profile Platform (LP 717-1)	C	None		0.0000	180.00	No Ice	21.24	21.24	1.10
						1/2"	23.56	23.56	1.70
***									
Antel BXA-70063/6CF w/	A	From Face	4.00	0.0000	170.00	No Ice	7.99	6.29	0.06

### Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	I/Q in <sup>2</sup>	w in	w/t
L1	17.8918	13.7831	525.3925	6.1664	8.9510	58.6968	1051.4762	6.8929	2.6611	10.644
	26.7809	20.7294	1787.3245	9.2740	13.3980	133.4024	3577.0008	10.3667	4.2018	16.807
L2	26.2731	24.7252	1941.0895	8.8494	12.8221	151.3866	3884.7332	12.3650	3.8923	12.455
	35.0657	33.9425	5021.7310	12.1483	17.5428	286.2565	10050.069	16.9745	5.5278	17.689
L3	34.4311	38.9319	5262.3314	11.6117	16.8067	313.1095	10531.587	19.4697	5.1628	13.767
	43.1658	50.1512	11248.759	14.9579	21.5951	520.8946	22512.320	25.0804	6.8218	18.191
L4	42.4044	48.0694	9905.2687	14.3370	20.7066	478.3638	19823.570	24.0393	6.5139	17.37
	50.7713	59.0662	18377.109	17.6169	25.4000	723.5082	36778.399	29.5387	8.1400	21.707

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>r</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontal
ft	ft <sup>2</sup>	in					in	in
L1 180.00-134.00				1	1	1		
L2 134.00-88.50				1	1	1		
L3 88.50-43.29				1	1	1		
L4 43.29-0.00				1	1	1		

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Shield Leg	Allow Shield	Component Type	Placement ft	Total Number	C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight plf
1-5/8"	C	No	Inside Pole	180.00 - 0.00	6	No Ice	0.00
						1/2" Ice	0.00
1-5/8"	C	No	Inside Pole	170.00 - 0.00	18	No Ice	0.00
						1/2" Ice	0.00
1-5/8"	C	No	Inside Pole	160.00 - 0.00	12	No Ice	0.00
						1/2" Ice	0.00
1/2"	C	No	Inside Pole	78.00 - 0.00	1	No Ice	0.00
						1/2" Ice	0.00

### Feed Line/Linear Appurtenances Section Areas

Tower Section n	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.00-134.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	1.14
L2	134.00-88.50	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	1.51
L3	88.50-43.29	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	1.50
L4	43.29-0.00	A	0.000	0.000	0.000	0.000	0.00



APPENDIX A

Output From Computer Programs

**Tower Input Data**

There is a pole section.  
 This tower is designed using the TIA/EIA-222-F standard.  
 The following design criteria apply:  
 Tower is located in Windham County, Connecticut.  
 Basic wind speed of 85 mph.  
 Nominal ice thickness of 0.5000 in.  
 Ice density of 56 pcf.  
 A wind speed of 74 mph is used in combination with ice.  
 Deflections calculated using a wind speed of 50 mph.  
 A non-linear (P-delta) analysis was used.  
 Pressures are calculated at each section.  
 Stress ratio used in pole design is 1.333.  
 Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

**Options**

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>Add IBC .6D+W Combination</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>√ Use Clear Spans For KL/r</li> <li>Retension Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>SR Members Have Cut Ends</li> <li>Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> </ul> | <ul style="list-style-type: none"> <li>√ Treat Feedline Bundles As Cylinder</li> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feedline Torque</li> <li>Include Angle Block Shear Check</li> <li style="text-align: center;"><del>Poles</del></li> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|

**Tapered Pole Section Geometry**

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L1	180.00-134.00	46.00	3.33	18	17.6200	26.3740	0.2500	1.0000	A572-65 (65 ksi)
L2	134.00-88.50	48.83	4.33	18	25.2403	34.5330	0.3125	1.2500	A572-65 (65 ksi)
L3	88.50-43.29	49.53	5.25	18	33.0840	42.5100	0.3750	1.5000	A572-65 (65 ksi)
L4	43.29-0.00	48.54		18	40.7609	50.0000	0.3750	1.5000	A572-65 (65 ksi)

**ANALYSIS RESULTS**

Our structural analysis indicates that the existing monopole structure and foundation have sufficient capacity to adequately support the existing, reserved, and proposed loading.

**Table 4 - Component Stresses vs. Capacity**

Notes	Component	Elevation ft	% Capacity	Pass / Fail
<b>Risa Tower Analysis Summary:</b>				
	L1	180 - 134	82.2	Pass
	L2	134 - 88.497	98.6	Pass
	L3	88.497 - 43.294	94.2	Pass
	L4	43.294 - 0	99.6	Pass
<b>Additional Components:</b>				
	Base Plate	0 - 0	79.7	Pass
	Anchor Rods	0 - 0	78.1	Pass
	Foundation (Soil)	0 - 0	76	Pass
	Foundation (Structural)	0 - 0	81	Pass
<b>Structural Rating (maximum capacity of all components) =</b>				<b>99.6</b>

As summarized in Table 4 above, our analysis indicates that the existing monopole structure and foundation have sufficient capacity to adequately support the existing, reserved, and proposed loading. Modifications are not required at this time.

Information for the existing monopole and foundation is based on the available drawings, documents, and/or information listed in Table 3 below.

**Table 3 - Reference Documents Provided**

Document	Source	Reference	Remarks
Proposed Antenna Loading	Crown Castle	876375	
Existing Antenna Loading	Crown Castle	876375	
Geotechnical Reports	CCISITES	1615348	Dr. Clarence Welti, 01/24/2000
Foundation Mapping	CCISITES	1615408	FDH, 09-04033E N1, 4/15/2009
Tower Mapping	CCISITES	2428368	FDH, 09-04023T T1, 05/04/2009
Tower Structural Analysis Reports	CCISITES	2431086	CCI, 271546, 05/11/2009
Tower Reinforcement Drawing	CCISITES		PJF, 37509-930, 08/31/2009

## ANALYSIS PROCEDURE

### ANALYSIS METHODS

RISA Tower (Version 5.3.1.0), a commercially available software program, was used to create a three-dimensional model of the monopole and calculate member stresses for various dead, live, wind, and ice load cases. The analysis was performed in accordance with the TIA/EIA-222-F Standard. Selected output from the analysis is included in Appendix A.

### ASSUMPTIONS

1. Monopole was fabricated and installed in accordance with the manufacturer's specifications.
2. Monopole has been properly maintained in accordance with manufacturer's specifications.
3. The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4. Taper lengths were assumed per the minimum design standard per ASCE 48-05
5. Shaft steel assumed to be 65ksi. Base plate assumed to be 50ksi steel.

If any of the above assumptions are not valid or have been made in error, then the results of this analysis may be affected. In that case, please notify Paul J. Ford and Company immediately so that we can review any new and/or modified information and determine its affect on the analysis results regarding the structural adequacy of the monopole and foundation.

## INTRODUCTION

At the request of Crown Castle International, Paul J. Ford and Company has analyzed the monopole at the CANTERBURY / LEMIRE site located in CANTERBURY, Windham County, CT. This structural analysis has been performed in accordance with the TIA/EIA-222-F-1996 Standard, "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures" to determine if the monopole structure has adequate capacity to support the existing, reserved, and proposed antenna loading.

## ANALYSIS CRITERIA

The existing monopole has been analyzed for the antenna and coax loading listed in Tables 1 and 2 below. The monopole has been analyzed in accordance with the TIA/EIA-222-F-1996 Standard for the following fastest-mile Basic Wind Speeds: 85 mph without ice, 74 with 0.5" radial ice, and 50 mph without ice as recommended for Windham County, CT.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level ft.	Center Line Elevation ft.	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
170*	170	3	Antel	BXA-70063/6CF w/ Mount Pipe	18	1-5/8" (I)	Proposed
		3	Antel	BXA-185063/12CF w/Mount Pipe			
		6	Antel	LPA-80080/6CF w/mount pipe			
		1	-	12' Low Profile Platform (LP 303-1)			

\*MLA loading consists of: (12) DB844H90 with (12) 1 5/8" coax, but does not control over the proposed loading and coax.

(E) Coax to be mounted externally and exposed to the wind. See coax layout in Appendix B.

(I) Coax to be mounted internally and shielded from the wind. See coax layout in Appendix B.

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level ft.	Center Line Elevation ft.	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
180	183	6*	EMS	FV65-14-00NA2 w/Mount Pipe	6	1-5/8" (I)	MLA
	180	1	-	12' Low Profile Platform (LP 717-1)			Existing
160	161	6	Powerwave	7770.00 w/ Mount Pipe	12**	1-5/8" (I)	Existing
		6	Powerwave	LGP21401			
		6	Powerwave	LGP21901			
	160	1	-	12' Low Profile Platform (LP 303-1)			Existing
78	79	1	Spectracom	8225	1	1/2" (I)	Existing
	78	1	-	3' Side Arm Mount			Existing

\*MLA loading controls. Existing loading consists of: (6) DB980H90E-M with (6) 1 5/8" coax.

\*\*SLA coax loading controls. Existing coax consists of (12) 1 1/4"

(E) Coax to be mounted externally and exposed to the wind. See coax layout in Appendix B.

(I) Coax to be mounted internally and shielded from the wind. See coax layout in Appendix B.

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**PAUL J. FORD AND COMPANY**  
**STRUCTURAL ENGINEERS**  
 250 East Broad Street • Suite 1500 • Columbus, Ohio 43215-3708

September 4, 2009

Eva Morales  
 Crown Castle International  
 46 Broadway  
 Albany, NY 12204  
 518-433-6250

**Structure is Adequate**  
**Monopole is Adequate**  
**Foundation is Adequate**

**Subject: Structural Analysis Report of Existing 180-Ft Monopole**

<b>Carrier Designation</b>	<b>Verizon Wireless Co-Locate</b>	
	Carrier Site Number:	118601
	Carrier Site Name:	Canterbury CT
<b>Crown Castle Designation</b>	<b>Crown Castle BU Number:</b>	876375
	<b>Crown Castle Site Name:</b>	CANTERBURY / LEMIRE
	<b>Crown Castle JDE Job Number:</b>	124367
	<b>Crown Castle Application Number:</b>	87690Rev1
	<b>Crown Castle PO Number:</b>	344053
	<b>Crown Castle WO Number:</b>	292648
<b>Engineering Firm Designation</b>	<b>Paul J. Ford and Company</b>	37509-0930Rev1
<b>Site Data</b>	53 Westminster Rd., CANTERBURY, Windham County, CT	
	Latitude 41° 42' 7.1", Longitude -71° 58' 50.1"	

Dear Eva Morales,

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural adequacy of the above monopole. This analysis has been performed in accordance with the Crown Castle Structural "Statement of Work", the terms of the Purchase Order, and the TIA/EIA-222-F Standard for the following Basic Wind Speeds: 85 mph without ice, 74 mph with 0.5" radial ice, and 50 mph (Operational) without ice.

The monopole was analyzed with the addition of the proposed antenna loading shown in the table below combined with the existing and reserved loading on the structure:

Elevation - ft	Count	Antenna Description
170	3	Antel BXA-70063/6CF w/ Mount Pipe
	3	Antel BXA-185063/12CF w/Mount Pipe
	6	Antel LPA-80080/6CF w/mount pipe
	1	12' Low Profile Platform (LP 303-1)

Based on our analysis, we have determined that the existing monopole structure and foundation have sufficient capacity to adequately support the existing, reserved, and proposed loading. Modifications are not required at this time.

Respectfully submitted,

Christina Hedges, EIT  
 Structural Engineer  
 chedges@pjfweb.com