# STATE OF CONNECTICUT 

CONNECTICUT SITING COUNCIL
Ten Franklin Square, New Britain, CT 06051
Phone: (860) 827-2935 Fax: (860) 827-2950
E-Mail: siting.council@ct.gov
Web Site: portal.ct.gov/csc

## VIA ELECTRONIC MAIL

January 15, 2021
Duncan J. Forsyth, Esq.
Halloran \& Sage LLP
1 Godwin Square, 225 Asylum Street
Hartford, CT 06103
forsyth@halloransage.com
RE: EM-VER-020-201224 - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 719 George Washington Turnpike, Burlington, Connecticut.

Dear Attorney Forsyth:
The Connecticut Siting Council (Council) is in receipt of your correspondence of January 11, 2021 submitted in response to a request for an exempt modification filed with the Council by Verizon Wireless (Verizon) on December 24, 2020 for an exempt modification to the telecommunications facility located at 719 George Washington Turnpike in Burlington. Thank you for taking the time to submit comments.

Before making a final decision on any request for an exempt modification, the Council carefully considers the proposal in accordance with the required feasibility criteria under 16-50j-72 of the Regulations of Connecticut State Agencies. Entities requesting an exempt modification for an existing telecommunications facility must demonstrate that the proposal is consistent with the exempt modification criteria, including, but not limited to, changes on an existing site that do not increase the tower height; extend the boundaries of the site by any dimension; increase noise levels at the site boundary by 6 decibels or more, or to levels that exceed state criteria; increase radio frequency power density at the site boundary to or above standards adopted by the Federal Communications Commission; cause a significant adverse change or alteration in the physical or environmental characteristics of the site; or impair the structural integrity of the facility. (Emphasis added).

The January 11, 2021 correspondence submitted on behalf of the Town of Burlington expresses valid concerns regarding the May 8, 2020 Structural Analysis (SA) submitted with the December 24, 2020 Verizon exempt modification request and conducted by Nexius on behalf of Verizon indicating a tower stress level at $115.2 \%$ of its acceptable capacity if Verizon's proposed equipment is installed on the facility. The Nexius SA accounts for similar T-Mobile and AT\&T equipment installations that were approved by the Council in 2019.

The Council did not receive written notification of T-Mobile and AT\&T's completion of their approved equipment installations prior to the submission of Verizon's December 24, 2020 exempt modification request. ${ }^{1}$ A condition of the Council's approval for the equipment installations of both T-Mobile and AT\&T is to provide written notification of completion of the installations prior to the expiration of the approval,

[^0]or to submit a written request for an extension of time to complete the installation at least 60 days prior to the expiration of the approval.

On July 8, 2019 and November 18, 2019, the Council approved exempt modification requests for equipment installations from T-Mobile and AT\&T, respectively, each of which included SAs indicating tower stress levels below $100 \%$. These requests, including, but not limited to, the SAs and the Council's decision letters, are available on the Council's "Decisions by Town" web page for the Town of Burlington under the filing numbers EM-T-Mobile-020-190614 and EM-CING-020-191015 or by following the links below:
https://portal.ct.gov/-/media/CSC/2_EMS-
medialibrary/Burlington/GeorgeWashingtonTpke/T_Mobile/emtmobile020190614dcltrGeorgeWashingto nTpkepdf.pdf
https://portal.ct.gov/-/media/CSC/2 EMS-
medialibrary/Burlington/GeorgeWashingtonTpke/ATT_CING/emcing020191015decisiongeorgewashingt ontpkepdf.pdf

Please be advised that the Council's approval of T-Mobile's above-referenced equipment installation expired on July 8, 2020 and the Council's approval of AT\&T's above-referenced equipment installation expired on November 18, 2020 per Condition No. 7 of each respective Council decision letter. Neither carrier submitted written notification of completion of construction per Condition 5 nor a written request for an extension to complete construction per Condition 8.

On April 23, 2020, the Council received a request for an exempt modification at the subject facility from Verizon. The Council issued written notice of an incomplete request for exempt modification on April 30, 2020 due to the absence of the previously approved T-Mobile and AT\&T equipment installations from the SA submitted with the request. Please note that the April 17, 2020 SA provided with Verizon's request indicated a tower stress level of $97.7 \%$ without accounting for the approved AT\&T and T-Mobile equipment loading. Verizon withdrew the request on June 17, 2020.

On December 24, 2020, the Council received another request for an exempt modification at the subject facility from Verizon with a statement indicating the Council's deadline for construction and notice of equipment installation completion has expired for both the AT\&T and T-Mobile requests referenced above and therefore, the equipment approved in those requests did not need to be included in its SA. Please note that the structural analysis dated May 8,2020 and attached to the Town's correspondence was not submitted to the Council with either of the Verizon requests for exempt modification.

The December 24, 2020 Verizon request for an exempt modification, EM-VER-020-201224, is currently under review. Unfortunately, it is not evident at this time whether T-Mobile and AT\&T completed their approved equipment installations at the facility within the Council's deadline for completion of construction. In an effort to elicit a confirmation from AT\&T and T-Mobile as to the status of their approved, but now expired without extension, equipment installations, and to ensure the Town's concerns about its emergency communications equipment are addressed, a copy of the January 11, 2021 correspondence and this correspondence is being provided to representatives for AT\&T, T-Mobile and Verizon.

A response, that is copied to all of the recipients of this correspondence, from the representatives of AT\&T, T-Mobile and Verizon by close of business on January 22, 2021 would be appreciated. If a response is not received by that date and the SA issues associated with the respective carrier equipment installations on the facility remain unresolved, the Council may initiate a feasibility proceeding pursuant to the Tower Sharing Policy under Connecticut General Statutes §16-50aa.

Thank you for your attention to this matter.
Sincerely,

## s/Melanie Bachman

Melanie Bachman
Executive Director
MAB/IN/emr
C: The Honorable Theodore C. Shafer, First Selectman, Town of Burlington
Michael Boucher, Fire Chief, Town of Burlington
Kenneth C. Baldwin, Esq., Robinson \& Cole LLP
Lucia Chiocchio, Esq., Cuddy + Feder LLP
Mark Richard, Site Development Manager, T-Mobile

January 11, 2021

Via Email: siting.council@ct.gov
Melanie A. Bachman, Esq.
Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051
Re: EM-VER-020-201224 - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 719 George Washington Turnpike, Burlington, CT

## Dear Ms Bachman:

This office represents the Town of Burlington and we have been asked to respond to the above referenced application by Cellco Partnership d/b/a Verizon Wireless concerning proposed modifications of the telecommunications facility located at 719 George Washington Turnpike which is owned by the Town of Burlington and located at the Town's Main Fire Station.

It is important to note that, on two occasions, the Town has been advised by Verizon representatives that the subject communications facility is currently overstressed, including a prior report by Nexius that stated that the "Tower Stress Level" was at $115.2 \%$ of its acceptable capacity. Thus, the current Nexius report can only be viewed as highly suspect. It is important to note that, over the past several years, the only modifications to equipment on the communications tower was done by the three carriers leasing space on the tower, which modifications were allowed based on representations made by those carrier's consultants. The Town is in the process of retaining its own consultant to examine these reports and the current structural integrity of the tower. Thus, the Town requests that no approvals, or work, be allowed on the tower until a total review and analysis can take place. Since Town emergency communications equipment is also located on the tower, any further work impacting the structural integrity of the tower could put public safety in jeopardy.

The report and another advisement from Verizon establishing the overstressed condition of the tower are attached for your review. If you have any questions, or would like to discuss the matter further, please do not hesitate to contact me at 860-944-9910.

Very truly yours,
HALLORAN \& SAGE, LLP

## By: Duncan J. Farsyth

Duncan J. Forsyth
cc: Kenneth C. Baldwin, Esq.(via email)
Theodore C. Shafer, First Selectman (via email)
Michael Boucher, Fire Chief (via email)
Kenneth R. Slater, Jr., Esq. (via email)

June $25^{\text {th }}, 2020$
Town of Burlington
200 Spielman Highway
Burlington, CT 06013
Attn: Selectman Shafer
Via Certified Mail: 7019-1120-0001-4276-3709
Re: Proposed Modifications to Existing Verizon Wireless Equipment
Site Name: Burlington, CT
Site Address: 719 George Washington Turnpike

Dear Selectman Shafer:

Pursuant to my email dated May 27, 2020, it has come to Verizon's attention that the Tower located at the above-captioned address is structurally failing in its existing condition, the tower fails with a stress ratio above $105 \%$. The failing status of the tower is not only a hazard, but it is also putting Verizon's assets at risk.

I would like to work with you on behalf of Verizon to rectify the existing condition of the tower, however there has been a lack of communication from you on this matter. Please reach out so we can work together to plan and execute steps to get the tower to a passing status. If I do not hear back from you by the end of business day on July 3, 2020, Verizon will be notifying the Connecticut Siting Council of the failing structural and corresponding issues.

Thank you for your attention to this matter, I may be reached by phone at 603-475-0347, or via email at rrafferty@saigrp.com.


Enclosure:
Email dated 5/27/2020
cc: Chief John Haviland

| From: | Rebecca Rafferty |
| :--- | :--- |
| Sent: | Wednesday, May 27, 2020 8:44 AM |
| To: | 'selectmensoffice@burlingtonct.us'; John Haviland |
| Subject: | VZW \& Other Carriers-Burlington_CT Fuze\#2559312 |
| Importance: | High |
| Follow Up Flag: | Follow up |
| Flag Status: | Completed |

Hi Selectman Shafer \& Fire Chief Haviland,
As you may know this site required CSC approval prior to any modifications. At the request of the CSC we updated our Structural Analysis to reflect the current equipment of AT\&T and T-Mobile on the tower, please note we did not have prior knowledge of AT\&T/T-MOs 2019 modifications when I provided the Structural Analysis dated February 26,2020 to the both of you. After A\&E review, it has come to my attention that even without VZW's current proposed loading and mount structural modifications, just existing condition, the tower fails with stress ratio above $105 \%$ ". The SAs by ATT and T-MO have some inaccurate data or settings, AT\&T ran it under the wrong Structure class and TMO mapping has small discrepancies.

Based on this information, Structural Modification Design will be required in the amount of $\$ 3,500.00$, this does not include the mod construction cost. Verizon is looking for feedback so that the carriers can share the costs of the modification design as well as the modification construction costs.
Respectfully,
Rebecca Rafferty
Site Acquisition Specialist
rrafferty@saigrp.com | C 603-475-0347
$5, \mathrm{Al}$

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## Structural Analysis Report

| Property Owner Structural Type <br> Site Address <br> Site ID Site Name Latitude Longitude | Town of Burlington <br> 179 ft Monopole Tower <br> 719 George Washington Tpke <br> Burlington, CT 06103 <br> N/A <br> N/A <br> 41.766825 <br> $-72.961511$ |
| :---: | :---: |
| Client Site Type Site ID Site Name Location Code | Verizon Wireless <br> 20 Alexander Drive, $2^{\text {nd }}$ Floor <br> Wallingford, CT 06492 <br> MACRO <br> N/A <br> BURLINGTON_CT <br> 46857 |
| Prepared by <br> Job/Task Number <br> Rev <br> Email <br> Phone <br> Date <br> Result | Nexius Solutions, Inc. 300 Apollo Drive, Suite 7 Chelmsford, MA 01824 VZW46857A01-NX062 2 <br> structurals@nexius.com 972-581-9888 05/08/2020 <br> Inadequate (115.2\%) |

## 

## Dear Sir / Madam:

Nexius Solutions is pleased to submit this Report to determine the structural integrity of the referred tower.

Referenced documents used for this analysis are listed in the section DOCUMENTS \& REFERENCES. This analysis has been performed in compliance with

- 2018 Connecticut State Building Code (IBC 2015 w/ State Amendments)
- ANSI/TIA-222-G w/ Addendums, Structural Standard for Antenna Supporting Structures and Antennas.

Detailed design parameters are listed in Table 1. Analysis loading is detailed in Table 2 and Table 3.
Based on our analysis we have determined the following result:

| Tower Stress Level | Inadequate (115.2\%) |
| :--- | :--- |
| Base Plate | Adequate (99.9\%) |
| Foundation | Adequate (90.3\%) |

Nexius Solutions appreciates the opportunity of providing continued engineering services. Should you have any questions, comments or require additional information, please do not hesitate to contact us.

Sincerely,
Analysis Prepared by: Approved by:
Akshay Doddamani
Structural Engineer
Jiazhu Hu, P.E.
Engineering Manager
License \#: 31530


## 

DOCUMENTS \& REFERENCES
> RFDS, Location Code: 46857, Site Name: BURLINGTON_CT , by Verizon Wireless, dated 01/08/2020.
> Construction Drawings (FOR CONSTRUCTION), Location Code: 46857, Verizon Site Name: BURLINGTON_CT, by Nexius dated 02/26/2020.
> Structural Analysis, Centek Project No: 19027.15, T-Mobile Site Ref: CTHA539A, by CENTEK Engineering, Inc. dated 04/24/2019.
> Construction Drawings, Site ID: CTHA539A, T-Mobile Site Name: BURLINGTON FIRE DEPARTMENT FLAGPOLE, T-Mobile Site Ref: CTHA539A, by CENTEK Engineering, Inc. dated 05/29/2019.
> Structural Analysis, Job Number: CT1123, AT\&T Site Name: BURLINGTON-GEORGE WASH, by HUDSON Design Group, dated 10/01/2019.
> Construction Drawings, Site Number: CT1123, AT\&T Site Name: BURLINGTON-GEORGE WASH, by HUDSON Design Group, dated 07/03/2019.
> Structural Analysis, Rev 1, Location Code: 46857, Verizon Site Name: BURLINGTON_CT, by Nexius dated 04/17/2020.

DESIGN STANDARDS \& PARAMETERS
TAble 1 STANDARDS \& DESIGN PARAMETERS

| Codes and Standards |  |
| :---: | :---: |
| Building Code | 2018 Connecticut State Building Code (IBC 2015 w/ State Amendments) |
| TIA Standard | ANSI/TIA-222-G w/ Addendums |
| Wind Parameters |  |
| Ultimate Wind Speed | 120 mph |
| Nominal Wind Speed | 93 mph |
| Nominal Wind Speed with Ice | 50 mph |
| Radial Ice Thickness | 1 in |
| Exposure Category | C |
| Structure Class | III |
| Topographic Category | 1 |
| Seismic Design Parameters* |  |
| $\mathrm{S}_{\text {s }}$ | 0.182 |
| $\mathrm{S}_{1}$ | 0.064 |

## RESULTS \& RECOMMENDATIONS

The existing structural modification details are not available. It is assumed that the installed tower reinforcement was originally designed, installed and maintained properly and the equivalent thickness(es) for section(s) with tower modifications used in the above referred previous structural analyses are correct. It is further assumed that the proposed mount and tower modifications detailed in the referred construction drawings for other co-located carriers are installed. Based on our analysis, it is determined that the existing tower structure to be inadequate to support the existing and proposed loading.

All structural components and connections should be checked for tightness and good condition prior to installing any proposed loading. The analysis is performed based on structural information obtained from provided drawings, site visit and some measurements. The analysis assumes that the provided information is accurate. If the site conditions are different from assumptions or do not meet requirements, the analysis result would not be valid and Nexius should be notified for re-evaluation.

## 

## LOADING

Table 2 - Proposed Antenna and Cable Information

| Mount Elev. ft | Ant. Ctr. Elev. ft | Qty | Antenna Manufacturer | Antenna Model | No. of Feed <br> Lines | Feed Line Size in | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 160.0 | 160.0 | 6 | CommScope | NHH-65B-R2B | 1 | 12x24 <br> Hybrid Cable | - |
|  |  | 3 | Samsung | B2/B66A RRH-BR049 |  |  |  |
|  |  | 3 | Samsung | B5/B13 RRH-BR04C |  |  |  |
|  |  | 1 | Raycap | RVZDC-6627-PF-48 |  |  |  |

Table 3 - Existing and Reserved Antenna and Cable Information

| Mount Elev. ft | Ant. Ctr. Elev. ft | Qty | Antenna Manufacturer | Antenna Model | No. of Feed <br> Lines | Feed Line Size in | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 179.0 | 191.0 | 3 | - | 20-ft Omni Antenna | 3 | 1-5/8 | 1 |
| 179.0 | 179.0 | 3 | RFS | APXVAARR24_43 | 4 | $\begin{gathered} 1-5 / 8 \\ \text { Hybriflex } \\ 1-1 / 4 \end{gathered}$ | 1 |
|  |  | 3 | Ericsson | AIR21 B2A/B4P |  |  |  |
|  |  | 3 | Ericsson | AIR32 |  |  |  |
|  |  | 3 | Ericsson | 4449 B71 B12 RRH |  |  |  |
|  |  | 1 | - | 14-ft Low Profile Platform w/ Site Pro 1 handrail kit ( $\mathrm{p} / \mathrm{n}$ HRK14) |  |  |  |
| 168.0 | 170.0 | 3 | Powerwave | 7770.0 | $\begin{gathered} 12 \\ 2 \\ 6 \end{gathered}$ | 1-5/8 <br> Fiber <br> DC | 1 |
|  |  | 3 | CCI | HPA65R-BU8A |  |  |  |
|  |  | 6 | Kathrein | 80010966 |  |  |  |
|  |  | 6 | Powerwave | LGP21401 |  |  |  |
|  |  | 3 | Ericsson | B25 4415 |  |  |  |
|  |  | 3 | Ericsson | B2/B66A 8843 |  |  |  |
|  |  | 3 | Ericsson | B5/B12 4449 |  |  |  |
|  |  | 3 | Raycap | DC6-48-60-18-8F |  |  |  |
|  |  | 1 | - | 14-ft Low Profile Platform Reinforced w/ Handrail Kit and Kicker Reinforcement Kit |  |  |  |
|  |  | 1 | Valmont | Light duty Tri-bracket |  |  |  |
| 158.0 | 160.0 | 6 | Celwave | APL866513 | 12 | 1-5/8 | 1 |
|  |  | 1 | - | 14-ft Low Profile Platform Reinforced w/ Proposed Handrail kit and Kicker Reinforcement Kit |  |  |  |
|  |  | 3 | Amphenol | BXA-70063-6CF | - | - | 2 |
|  |  | 3 | Amphenol | BXA-171063-8BF |  |  |  |
|  |  | 6 | RFS | FD9R6004/2C-3L |  |  |  |
| 138.5 | 138.5 | 1 | - | 3-ft Standoff Mount | 1 | 1-5/8 | 1 |
|  |  | 1 | - | 20-ft 4-Bay Dipole |  |  |  |
| 132.5 | 132.5 | 1 | - | 3-ft Yagi | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{gathered} 1-5 / 8 \\ 1 / 2 \end{gathered}$ | 1 |
|  |  | 1 | - | 8-ft Omni Directional Whip |  |  |  |
|  |  | 1 | - | 3-ft Standoff Mount |  |  |  |
| 112.5 | 112.5 | 1 | - | 10-ft Dipole Antenna | 1 | 1-5/8 | 1 |

[^1](1) Existing Equipment, (2) Equipment to be removed; Not considered in this analysis

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## ANALYSIS

tnxTower, a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for required loading cases. Selected output from the analysis is included in APPENDICES.

RESULTS - MEMBER CAPACITIES

| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \phi P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 179-139.5 | Pole | TP28.0455x19.5x0.1875 | 1 | -11.15 | 1062.10 | 115.2 | Fail |
| L2 | 139.5-93.4 | Pole | TP37.5377x26.8051x0.37 5 | 2 | -21.63 | 3187.78 | 85.3 | Pass |
| L3 | 93.4-46.31 | Pole | TP47.123x35.6737x0.375 | 3 | -35.48 | 3800.33 | 101.7 | Fail |
| L4 | 46.31-0 | Pole | TP56.25x44.9739x0.375 | 4 | -54.44 | 4334.66 | 113.7 | Fail |
|  |  |  |  |  |  | Pole (L1) Base Plate RATING | $\begin{gathered} \text { Summary } \\ 115.2 \\ 99.9 \\ \mathbf{1 1 5 . 2} \end{gathered}$ | Fail <br> Pass <br> Fail |

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## Standard Conditions for Providing Structural Consulting Services on Existing Structures

1. The structure is analyzed to the best of our ability using all information that is provided or can be obtained during fieldwork (if authorized by client). If the existing conditions are not as we have represented in this analysis, the analysis would not be valid, and we should be contacted to evaluate the significance of the deviation and revise the assessment accordingly.
2. The structural analysis has been performed assuming that the structural members, parts and component were originally designed properly and are all in "like new" condition. No allowance was made for excessive corrosion, damaged or missing structural members, loose bolts, misaligned parts, or any reduction in strength due to the age or fatigue of the product.
3. The structural analysis provided is an assessment of the primary load carrying capacity of the structural members, components and parts. We provided a limited scope of service. In some cases, we cannot verify the capacity of every weld, plate, connection detail, etc. In some cases, structural fabrication details are unknown at the time of our analysis, and the detailed field measurement of some of the required details may not be possible. In instances where we cannot perform connection capacity calculations, it is assumed that the existing manufactured connections develop the full capacity of the primary members being connected.
4. We cannot be held responsible for structural members, components and parts that are installed improperly, are loose or have a tendency of working loose over the lifetime. Our analysis has been performed assuming fully tightened connections, and proper installation per manufacturer's instructions.
5. The structural analysis has been performed using information currently provided by the client and potentially field verified. We have been provided with a loading arrangement for all telecommunications equipment on the structure. Our analysis has been based upon a particular loading arrangement provided. We are not responsible for deviations in the loading arrangements that may occur over time. If deviations in loading arrangements are proposed, then the analysis would not be valid and we should be contacted to revise the analysis.
6. We cannot be held responsible for temporary and unbalanced loads on structure. Our analysis is based on a particular loading arrangement or as-build field condition. We are not responsible for the methods and means of how the loading arrangement is accomplished by the contractor. These methods and means may include rigging of equipment or hardware to lift and locate, temporary hanging of equipment in locations other than the final arrangement, movement and tie off of tower riggers, personnel, and their equipment, etc.
7. It is assumed that all welded connections are performed in the shop under the latest American Welding Society Code. No field welds are permitted or assumed for the existing pre-manufactured equipment.
8. Steel grade and strength are unknown and cannot be field tested. We cannot be held responsible for equipment manufactured from inferior steel or bolts. Our analysis assumes that standard structural grade steel has been used by the equipment manufacturer for all assembled parts of the mounting apparatus. Acceptable steels and connection components are specified by the American Institute of Steel Construction. In case no accurate info available, following material assumptions were used:

| Pipe | ASTM A572-65 |
| :--- | :--- |
| Anchor Bolts | ASTM A615-75 |
| Base Plate | ASTM A572-60 |

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## Appendix \#1: Loading Parameters and Calculations

## Address:

No Address at This Location

## ASCE 7 Hazards Report



## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

119 Vmph
76 Vmph
85 Vmph
91 Vmph
97 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Mon Feb 242020

## Date Accessed:

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

## Seismic

Site Soil Class: D-Stiff Soil

Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.182 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.064 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.292 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.155 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.194 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.103 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.092 |
| $\mathrm{PGA}_{\mathrm{M}}:$ | 0.147 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category <br> B




Mon Feb 242020
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CIVIL ENGINEERS
Ice

Results:
Ice Thickness: $\quad 1.00 \mathrm{in}$.

Concurrent Temperature: 5 F
Gust Speed: $\quad 50 \mathrm{mph}$
Data Source:
Date Accessed:
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Mon Feb 242020
Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

חexivs

Appendix \#2: tnxTower Output

179.0tt

ALL REACTIONS
ARE FACTORED
$A X I A L$
$114 K$
SHEAR
13 K ,$\substack{\text { MOMENT } \\ 2115 \mathrm{kip}-\mathrm{tt}}$ TORQUE 5 kip-ft
50 mph WIND - 1.0000 in ICE


| TYPE | elevation | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| $20^{\prime} \times 2^{\prime \prime}$ Dia Ommi Antennaw M Mg Pipe (Town) | 179 | B2B66A 8843 RRH (ATI) | 170 |
|  | 179 | ${ }^{\text {B2B66A }} 8843$ RRH (ATI) | 170 |
| $20^{20} \times 2$ " Dia Ommi Antennaw M Mg Pipe (Tow) | 179 | B2B66A 8843 RRH (ATI) | 170 |
| APVVAARR24.43 W M Mig pipe (T-Molie) | 179 | B5IB12 4499 RRH (ATI) | 170 |
| APVVAARR24.43 W M Mg pipe (T-Moile) | 179 | B5182 4499 RRH (ATI) | 170 |
| APVVAARR24.43 W M Mg pipe (T-Motie) | 179 | B5112 24499 RRH (ATIT) | 170 |
| AR21 122AB4P w/ Mg Pipe (T-Mobile) | 179 | DC6-48.60-18.8F (ATI) | 170 |
| AR21 1224 A4P w/ M Mg Pipe ( 7 -Mobile) | 179 | DC6-48-6.6-18.8F (ATI) | 170 |
| AIR21 B2A/B4P w/ Mtg Pipe (T-Mobile) | ${ }^{179}$ |  | ${ }^{170}$ |
| AR32 W M Ms Pipe ( $T$-Mobile) | 179 | 14.4 Platatom reinforceed w H Hantaia and Kicker kit (ATI) | 168 |
| AR32w M Mg Pipe (TMobile) | 179 | Nas10-1 (Added Handrial) Neirion) | 158 |
| $4499871 / 1212$ RRH (T-Mobile) | 179 | (2) NHH-656-R28 w M Mg pipe (Verizon) | ${ }^{158}$ |
| 44998711812 RRH ( 7 -Mobile) | 179 | (2) NHH-658-R28 w M M Mg pipe (Verizon) | ${ }^{158}$ |
|  | 179 <br> 177 |  | 158 <br> 158 <br> 1 |
| 7770.0 w Mig Pipe (ATI) | 170 | AP.666513 wMount Pipe (Nerizon) | 158 |
| 7770.0 w M Mg Pipe (ATI) | 170 | APL666513 WMount Pipe (Verizon) | ${ }^{158}$ |
| 7770.0 w M Mg Pipe (ATI) | 170 | APL666513 WMount Pipe (Verizon) | ${ }^{158}$ |
| HPAGSR-BUBA W M MIt Pipe (ATI) | 170 | APL665513 WMount Pipe Verizon) | $\begin{array}{r}158 \\ 158 \\ \hline\end{array}$ |
| HPAGSR.BUBA W M M M Pipe (ATI) | 1170 | ${ }^{\text {APL }} 866513$ w Mount Pipe (Verizon) | 158 <br> ${ }_{158} 1$ |
| $800-1096 \mathrm{~W} / \mathrm{mg}$ plpe (ATI) | 170 | ${ }^{\text {B2B66A R R H Bro49 }}$ (evizon) | ${ }^{158}$ |
| 800-10966 W/ mg ppipe (ATI) | 170 | ${ }^{\text {B2B66A RRH Bro49 ( Nerizon) }}$ | 158 |
| ${ }^{800-10966 \mathrm{~W} \text { / } \mathrm{mg} \text { pipe (ATI) }}$ | 170 170 |  | 158 <br> 158 <br> 1 |
| $800-10966 \mathrm{~W} / \mathrm{mg}$ pipe (ATI) | 170 | Samsung 856B13 RRHH-BRO4C (verizon) | 158 |
| $800-10966 \mathrm{~W} / \mathrm{mgg} \mathrm{pipe}$ (ATI) | ${ }^{170}$ | RVVZC.6627.-F.48 V Verizon) | 158 <br> ${ }_{158}$ <br> 188 |
| ${ }^{\text {LGPP2 } 2001(\text { ATI) }}$ | ${ }^{170}$ |  | ${ }^{1588}$ |
| LGP21401 (ATI) | 170 | ${ }^{20} 4$-bay Dipole (Toun) | 133.5 |
|  | 170 170 |  | 138.5 132.5 |
| LGP21401 (ATI) | 170 | $3^{\text {² ragi }}$ | 1325 |
| 4415 B25 RRH (ATI) | 170 | So 701 (3tt pipe mount side am) | 132.5 |
|  | ${ }_{170}^{170}$ |  | ${ }^{112.5} 112.5$ |



TOWER DESIGN NOTES

1. Tower designed for Exposure C to the $\mathrm{T} A$-222-G Standard

Standard.
Tower designed for a a3 mph basic wind in accordance with the TIA-222-G Standard.
4. Deflections are based upon a 60 mph wind.
5. Tower Structure Class III.
5. Tower Structure Class 111 .
6. Topographic Category 1 with Crest Height of 0.00 ft
Weld together tover
8. Weod togetern tower sections have flange connections.
9. Tower members are" "hot dipped" galvanized in ac
0. Welds are fabricated with

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## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Basic wind speed of 93 mph .
Structure Class III.
Exposure Category C.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 1.0000 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf.
A wind speed of 50 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
Weld together tower sections have flange connections..
Connections use galvanized A325 bolts, nuts and locking devices. Installation per TIA/EIA-222 and AISC
Specifications..
Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards..
Welds are fabricated with ER-70S-6 electrodes..
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Tapered Pole Section Geometry

| Section | Elevation <br> $f t$ | Section <br> Length <br> ft | Splice Length $f t$ | Number of Sides | Top Diameter in | Bottom Diameter in | Wall <br> Thickness in | Bend <br> Radius <br> in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 179.00-139.50 | 39.50 | 4.00 | 18 | 19.5000 | 28.0455 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | 139.50-93.40 | 50.10 | 5.20 | 18 | 26.8051 | 37.5377 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | 93.40-46.31 | 52.29 | 6.39 | 18 | 35.6737 | 47.1230 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 46.31-0.00 | 52.70 |  | 18 | 44.9739 | 56.2500 | 0.3750 | 1.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

Tapered Pole Properties

| Section | Tip Dia. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in |


| tnxTOWer | Job | Page |  |
| :---: | :--- | :---: | :--- |
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| Section | Tip Dia. <br> in | Area <br> in $^{2}$ | $I$ <br> in $^{4}$ | $r$ <br> in | $C$ <br> in | $I / C$ <br> in $^{3}$ | $J$ <br> in $^{4}$ | $I t / Q$ <br> in $^{2}$ | $w$ <br> in |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 37.3224 | 42.0143 | 6613.8340 | 12.5311 | 18.1223 | 364.9563 | 13236.3706 | 21.0112 | 5.6186 | 14.983 |
|  | 47.7921 | 55.6418 | 15362.6008 | 16.5955 | 23.9385 | 641.7533 | 30745.4162 | 27.8262 | 7.6336 | 20.356 |
| L4 | 46.9982 | 53.0838 | 13339.7306 | 15.8326 | 22.8467 | 583.8794 | 26697.0140 | 26.5469 | 7.2554 | 19.348 |
|  | 57.0599 | 66.5052 | 26231.8094 | 19.8356 | 28.5750 | 917.9986 | 52498.1354 | 33.2589 | 9.2400 | 24.64 |


| Tower Elevation <br> ft | Gusset <br> Area (perface) <br> $f t^{2}$ | Gusset Thickness <br> in | Gusset Grade | Adjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle <br> Stitch Bolt Spacing <br> Horizontals <br> in | Double Angle <br> Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 |  |  |  | 1 | 1 | 1 |  |  |  |
| 179.00-139.50 |  |  |  |  |  |  |  |  |  |
| L2 |  |  |  | 1 | 1 | 1 |  |  |  |
| 139.50-93.40 |  |  |  |  |  |  |  |  |  |
| L3 93.40-46.31 |  |  |  | 1 | 1 | 1 |  |  |  |
| L4 46.31-0.00 |  |  |  | 1 | 1 | 1 |  |  |  |

## Monopole Base Plate Data

| Base Plate Data |  |
| :---: | :---: |
| Base plate is square |  |
| Base plate is sgouted | A615-75 |
| Anchor bolt grade | 2.2500 in |
| Anchor bolt size | 18 |
| Number of bolts | 48.0000 in |
| Embedment length | 3 ks |
| fic | 3.2500 in |
| Grout space | A572-60 |
| Base plate grade | 2.0000 in |
| Base plate thickness | 65.0000 in |
| Bolt circle diameter | 71.0000 in |
| Outer diameter | 56.2500 in |
| Inner diameter | Stiffened Plate |
| Base plate type | 1 |
| Bolts per stiffener | 0.7500 in |
| Stiffener thickness | 12.0000 in |
| Stiffener height |  |

Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From <br> Torque Calculation | Component Type | Placement <br> $f t$ | Total Number |  | $\begin{aligned} & C_{A} A_{A} \\ & f t^{2} / f t \end{aligned}$ | Weight <br> $k l f$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LDF7-50A (1-5/8 | B | No | Yes | Inside Pole | 179.00-3.00 | 3 | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Town) |  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 | B | No | Yes | Inside Pole | 138.50-3.00 | 1 | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Town) |  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 | B | No | Yes | Inside Pole | 132.50-3.00 | 1 | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Town) |  |  |  |  |  |  | $1{ }^{1 /}$ Ice | 0.00 | 0.00 |
| LDF4-50A (1/2 | B | No | Yes | Inside Pole | 128.50-3.00 | 1 | No Ice | 0.00 | 0.00 |


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|  | Project | BURLINGTON_CT | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:12:39 05/08/20 } \end{array}$ |
|  | Client | Verizon Wireless | Designed by Akshay Doddamani |


| Description | Face or Leg | Allow Shield | Exclude <br> From <br> Torque Calculation | Component Type | Placement | Total Number |  | $C_{A} A_{A}$ $f t^{2} / f t$ | Weight klf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FOAM) | B | No | Yes | Inside Pole | 113.00-3.00 | 1 | 1/2" Ice | 0.00 | 0.00 |
| (Town) |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Town) | B | No | Yes | Inside Pole | 160.00-3.00 | 12 | 1 " Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Verizon) | B | No | Yes | Inside Pole | 160.00-3.00 | 1 | 1 " Ice | 0.00 | 0.00 |
| HYbrid Cable |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| 12X24 |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Verizon) | C | No | Yes | Inside Pole | 179.00-3.00 | 4 | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.00 |
| HYBRIFLEX 1-1/4" |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| (T-Mobile) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
|  | C | No | Yes | Inside Pole | 179.00-3.00 | 6 | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (T-Mobile) | C | No | Yes | Inside Pole | 170.00-3.00 | 2 | 1 " Ice | 0.00 | 0.00 |
| FB-L98B-002 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| (Fiber) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (AT\&T) | C | No | Yes | Inside Pole | 170.00-3.00 | 6 | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.00 |
| WR-VG122ST-BRD |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| A (DC Cable) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (AT\&T) | C | No | Yes | Inside Pole | 170.00-3.00 | 12 | 1 " Ice | 0.00 | 0.00 |
| LDF7-50A (1-5/8 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (AT\&T) | B | No | Yes | Inside Pole | 132.50-3.00 | 1 | 1 " Ice | 0.00 | 0.00 |
| LDF4P-50A (1/2 |  |  |  |  |  |  | No Ice | 0.00 | 0.00 |
| FOAM) |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.00 |
| (Town) |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.00 | 0.00 |

Feed Line/Linear Appurtenances Section Areas

| Tower <br> Section | Tower <br> Elevation <br> $f t$ | Face | $A_{R}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face | $C_{A} A_{A}$ <br> Out Face | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $f t^{2}$ | $f t^{2}$ | $f t^{2}$ | $f t^{2}$ | K |
| L1 | $179.00-139.50$ | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.33 |
| L2 | $139.50-93.40$ | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.91 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.74 |
| L3 | $93.40-46.31$ | C | 0.000 | 0.000 | 0.000 | 0.000 | 1.23 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.79 |
| L4 | $46.31-0.00$ | C | 0.000 | 0.000 | 0.000 | 0.000 | 1.26 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.73 |
|  |  | C | 0.000 | 0.000 | 0.000 | 0.000 | 1.16 |

Feed Line/Linear Appurtenances Section Areas - With Ice

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| :---: | :---: | :---: | :---: |
|  | Project | BURLINGTON_CT | Date 14:12:39 05/08/20 |
|  | Client | Verizon Wireless | Designed by <br> Akshay Doddamani |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Tower Section \& Tower Elevation ft \& Face or Leg \& \begin{tabular}{l}
Ice \\
Thickness in
\end{tabular} \& \(A_{R}\)

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& $C_{A} A_{A}$ In Face $\mathrm{ft}^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
\text { ft }^{2}
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& \multirow[t]{3}{*}{179.00-139.50} \& A \& \multirow[t]{3}{*}{2.924} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.33 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.91 <br>
\hline \multirow[t]{3}{*}{L2} \& \multirow[t]{3}{*}{139.50-93.40} \& A \& \multirow[t]{3}{*}{2.834} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.74 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1.23 <br>
\hline \multirow[t]{3}{*}{L3} \& \multirow[t]{3}{*}{93.40-46.31} \& A \& \multirow[t]{3}{*}{2.693} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.79 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1.26 <br>
\hline \multirow[t]{3}{*}{L4} \& \multirow[t]{3}{*}{46.31-0.00} \& A \& \multirow[t]{3}{*}{2.416} \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.73 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 1.16 <br>
\hline
\end{tabular}

## Shielding Factor Ka

| Tower |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | | Feed Line |
| :---: |
| Record No. |$\quad$ Description | Feed Line |
| :---: |
| Segment Elev. | | $K_{a}$ |
| :---: |
| No Ice |$\quad$| $K_{a}$ |
| :---: |
| Ice |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
O
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$

Side \& Weight <br>
\hline \multicolumn{10}{|l|}{***** 191 ft *****} <br>
\hline 20' X 2" Dia Omni Antenna \& A \& From Face \& 3.00 \& 0.0000 \& 179.00 \& No Ice \& 4.00 \& 4.00 \& 0.02 <br>
\hline w/ Mtg Pipe \& \& \& -6.00 \& \& \& 1/2' Ice \& 6.03 \& 6.03 \& 0.05 <br>
\hline (Town) \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.07 \& 8.07 \& 0.09 <br>
\hline 20' X 2" Dia Omni Antenna \& B \& From Face \& 3.00 \& 0.0000 \& 179.00 \& No Ice \& 4.00 \& 4.00 \& 0.02 <br>
\hline w/ Mtg Pipe \& \& \& -6.00 \& \& \& 1/2' Ice \& 6.03 \& 6.03 \& 0.05 <br>
\hline (Town) \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.07 \& 8.07 \& 0.09 <br>
\hline 20' X 2" Dia Omni Antenna \& C \& From Face \& 3.00 \& 0.0000 \& 179.00 \& No Ice \& 4.00 \& 4.00 \& 0.02 <br>
\hline w/ Mtg Pipe \& \& \& -6.00 \& \& \& 1/2' Ice \& 6.03 \& 6.03 \& 0.05 <br>
\hline (Town) \& \& \& 10.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 8.07 \& 8.07 \& 0.09 <br>
\hline \multicolumn{10}{|l|}{***** 160 ft *****} <br>
\hline (2) NHH-65B-R2B w/ Mtg \& A \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 8.62 \& 7.35 \& 0.08 <br>
\hline pipe \& \& \& -2.00 \& \& \& 1/2' Ice \& 9.25 \& 8.38 \& 0.16 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.87 \& 9.27 \& 0.24 <br>
\hline (2) NHH-65B-R2B w/ Mtg \& B \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 8.62 \& 7.35 \& 0.08 <br>
\hline pipe \& \& \& -2.00 \& \& \& 1/2' Ice \& 9.25 \& 8.38 \& 0.16 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 9.87 \& 9.27 \& 0.24 <br>
\hline (2) NHH-65B-R2B w/ Mtg \& C \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 8.62 \& 7.35 \& 0.08 <br>
\hline pipe \& \& \& -2.00 \& \& \& 1/2' Ice \& 9.25 \& 8.38 \& 0.16 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& 1 " Ice \& 9.87 \& 9.27 \& 0.24 <br>
\hline APL866513 w/Mount Pipe \& A \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline (Verizon) \& \& \& -5.00 \& \& \& 1/2' Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 5.89 \& 7.06 \& 0.15 <br>
\hline APL866513 w/Mount Pipe \& B \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline (Verizon) \& \& \& -5.00 \& \& \& 1/2" Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 5.89 \& 7.06 \& 0.15 <br>
\hline APL866513 w/Mount Pipe \& C \& From Face \& 2.75 \& 0.0000 \& 158.00 \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline
\end{tabular}

| tnxTower | Job | VZW468547A01 | Page 5 of 9 |
| :---: | :---: | :---: | :---: |
| Nexius <br> 300 Apollo Drive, Suite 7 | Project | BURLINGTON_CT | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:12:39 05/08/20 } \end{array}$ |
| Chelmsford, MA 01824 <br> Phone: 1 (978) 923-7965 <br> FAX: | Client | Verizon Wireless | Designed by Akshay Doddamani |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight <br>

\hline \multirow[t]{2}{*}{(Verizon)} \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Face} \& -5.00 \& \multirow{5}{*}{0.0000} \& \multirow{4}{*}{158.00} \& 1/2" Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 5.89 \& 7.06 \& 0.15 <br>
\hline APL866513 w/Mount Pipe \& \& \& 2.75 \& \& \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline (Verizon) \& \& \& 5.00 \& \& \& 1/2" Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \multirow{4}{*}{APL866513 w/Mount Pipe (Verizon)} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Face} \& 2.00 \& \& \multirow{4}{*}{158.00} \& $1{ }^{\prime \prime}$ Ice \& 5.89 \& 7.06 \& 0.15 <br>
\hline \& \& \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline \& \& \& 5.00 \& \& \& 1/2" Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 5.89 \& 7.06 \& 0.15 <br>
\hline \multirow[t]{3}{*}{APL866513 w/Mount Pipe (Verizon)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 4.76 \& 5.28 \& 0.04 <br>
\hline \& \& \& 5.00 \& \& \& 1/2" Ice \& 5.39 \& 6.31 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 5.89 \& 7.06 \& 0.15 <br>

\hline \multirow[t]{3}{*}{| B2/B66A RRH BR049 |
| :--- |
| (Verizon) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>

\hline \& \& \& -1.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 2.22 \& 1.28 \& 0.12 <br>
\hline \multirow[t]{3}{*}{B2/B66A RRH BR049 (Verizon)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>
\hline \& \& \& -1.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.22 \& 1.28 \& 0.12 <br>

\hline \multirow[t]{3}{*}{| B2/B66A RRH BR049 |
| :--- |
| (Verizon) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>

\hline \& \& \& -1.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.22 \& 1.28 \& 0.12 <br>
\hline Samsung B5/B13 \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>
\hline RRH-BR04C \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.22 \& 1.28 \& 0.12 <br>
\hline Samsung B5/B13 \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>
\hline RRH-BR04C \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& 1" Ice \& 2.22 \& 1.28 \& 0.12 <br>
\hline Samsung B5/B13 \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 1.88 \& 1.01 \& 0.08 <br>
\hline RRH-BR04C \& \& \& 2.00 \& \& \& 1/2" Ice \& 2.05 \& 1.14 \& 0.10 <br>
\hline (Verizon) \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.22 \& 1.28 \& 0.12 <br>

\hline \multirow[t]{3}{*}{| RVZDC-6627-PF-48 |
| :--- |
| (Verizon) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 3.77 \& 3.06 \& 0.05 <br>

\hline \& \& \& -1.00 \& \& \& 1/2" Ice \& 4.11 \& 3.51 \& 0.09 <br>
\hline \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 4.47 \& 3.97 \& 0.13 <br>
\hline \multirow[t]{3}{*}{14' Low Profile Platform (Verizon)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 0.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 17.46 \& 17.46 \& 1.35 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 22.44 \& 22.44 \& 1.62 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 27.42 \& 27.42 \& 1.89 <br>
\hline \multirow[t]{2}{*}{NA 509-3 (Site Pro 1 Kicker Kit, P/N PRK-1245L)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 11.84 \& 11.84 \& 0.28 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 16.96 \& 16.96 \& 0.30 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 22.08 \& 22.08 \& 0.32 <br>
\hline \multicolumn{8}{|l|}{***** 138.5 ft *****} \& \& <br>
\hline \multirow[t]{3}{*}{20' 4-bay Dipole (Town)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{138.50} \& No Ice \& 4.00 \& 4.00 \& 0.06 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 6.00 \& 6.00 \& 0.10 <br>
\hline \& \& \& 4.00 \& \& \& 1" Ice \& 8.00 \& 8.00 \& 0.14 <br>
\hline \multirow[t]{3}{*}{SO 701 (3ft pipe mount side arm)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 0.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{138.50} \& No Ice \& 0.30 \& 0.30 \& 0.01 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 0.61 \& 0.61 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 0.81 \& 0.81 \& 0.09 <br>
\hline \multicolumn{10}{|l|}{***** 112.5-ft *****} <br>
\hline \multirow[t]{3}{*}{10' 2-bay Dipole (Town)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{112.50} \& No Ice \& 3.38 \& 3.38 \& 0.05 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 4.97 \& 4.97 \& 0.08 <br>
\hline \& \& \& 5.00 \& \& \& 1" Ice \& 5.57 \& 5.57 \& 0.11 <br>
\hline \multirow[t]{2}{*}{SO 701 (3ft pipe mount side arm)} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{4}{*}{112.50} \& No Ice \& 0.30 \& 0.30 \& 0.01 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 0.61 \& 0.61 \& 0.05 <br>
\hline (Town) \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.81 \& 0.81 \& 0.09 <br>
\hline ***** 160 ft ***** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{NA510-1 (Added Handrail) (Verizon)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 2.75 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{158.00} \& No Ice \& 6.00 \& 6.00 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 8.50 \& 8.50 \& 0.34 <br>
\hline \& \& \& 5.00 \& \& \& 1" Ice \& 11.00 \& 11.00 \& 0.42 <br>
\hline
\end{tabular}

| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | VZW468547A01 | 6 of 9 |
| Nexius 300 Apollo Drive, Suite 7 | Project | BURLINGTON_CT | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:12:39 05/08/20 } \end{array}$ |
| Chelmsford, MA 01824 <br> Phone: 1 (978) 923-7965 <br> FAX: | Client | Verizon Wireless | Designed by Akshay Doddamani |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\)
Side

$f t^{2}$ \& Weight <br>

\hline APXVAARR24-43 w/ Mtg pipe (T-Mobile) \& A \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 17.13 \\
& 17.75 \\
& 18.39
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 10.79 \\
& 12.21 \\
& 13.49
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.14 \\
& 0.26 \\
& 0.39
\end{aligned}
$$
\] <br>

\hline APXVAARR24-43 w/ Mtg pipe (T-Mobile) \& B \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 17.13 \\
& 17.75 \\
& 18.39
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 10.79 \\
& 12.21 \\
& 13.49
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.14 \\
& 0.26 \\
& 0.39
\end{aligned}
$$
\] <br>

\hline APXVAARR24-43 w/ Mtg pipe (T-Mobile) \& C \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 17.13 \\
& 17.75 \\
& 18.39
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 10.79 \\
& 12.21 \\
& 13.49
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.14 \\
& 0.26 \\
& 0.39
\end{aligned}
$$
\] <br>

\hline AIR21 B2A/B4P w/ Mtg Pipe (T-Mobile) \& A \& From Face \& $$
\begin{gathered}
3.00 \\
-5.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.90 \\
& 7.62 \\
& 8.27
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.22 \\
& 7.40 \\
& 8.43
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.18 \\
& 0.24 \\
& 0.31
\end{aligned}
$$
\] <br>

\hline AIR21 B2A/B4P w/ Mtg Pipe (T-Mobile) \& B \& From Face \& $$
\begin{gathered}
3.00 \\
-5.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.90 \\
& 7.62 \\
& 8.27
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.22 \\
& 7.40 \\
& 8.43
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.18 \\
& 0.24 \\
& 0.31
\end{aligned}
$$
\] <br>

\hline AIR21 B2A/B4P w/ Mtg Pipe (T-Mobile) \& C \& From Face \& $$
\begin{gathered}
3.00 \\
-5.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.90 \\
& 7.62 \\
& 8.27
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.22 \\
& 7.40 \\
& 8.43
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.18 \\
& 0.24 \\
& 0.31
\end{aligned}
$$
\] <br>

\hline AIR32 w/ Mtg Pipe (T-Mobile) \& A \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 7.29 \\
& 8.01 \\
& 8.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.61 \\
& 7.80 \\
& 8.83
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.16 \\
& 0.23 \\
& 0.30
\end{aligned}
$$
\] <br>

\hline AIR32 w/ Mtg Pipe (T-Mobile) \& B \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 7.29 \\
& 8.01 \\
& 8.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.61 \\
& 7.80 \\
& 8.83
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.16 \\
& 0.23 \\
& 0.30
\end{aligned}
$$
\] <br>

\hline AIR32 w/ Mtg Pipe (T-Mobile) \& C \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 7.29 \\
& 8.01 \\
& 8.67
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.61 \\
& 7.80 \\
& 8.83
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.16 \\
& 0.23 \\
& 0.30
\end{aligned}
$$
\] <br>

\hline | 4449 B71/B12 RRH |
| :--- |
| (T-Mobile) | \& A \& From Face \& \[

$$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.16 \\
& 1.29 \\
& 1.44
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.10 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline | 4449 B71/B12 RRH |
| :--- |
| (T-Mobile) | \& B \& From Face \& \[

$$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.16 \\
& 1.29 \\
& 1.44
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.10 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline | 4449 B71/B12 RRH |
| :--- |
| (T-Mobile) | \& C \& From Face \& \[

$$
\begin{aligned}
& 3.00 \\
& 5.00 \\
& 0.00
\end{aligned}
$$

\] \& 0.0000 \& 179.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 1.65 \\
& 1.81 \\
& 1.98
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.16 \\
& 1.29 \\
& 1.44
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.10 \\
& 0.11
\end{aligned}
$$
\] <br>

\hline 14-ft Platform w/ Site Pro 1 Handrail kit (T-Mobile) ***** 170 ft ***** \& C \& From Face \& $$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 177.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 23.46 \\
& 30.94 \\
& 38.42
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 23.46 \\
& 30.94 \\
& 38.42
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.58 \\
& 1.96 \\
& 2.34
\end{aligned}
$$
\] <br>

\hline | 7770.0 w/ Mtg Pipe |
| :--- |
| (AT\&T) | \& A \& From Face \& \[

$$
\begin{gathered}
3.00 \\
-6.00 \\
0.00
\end{gathered}
$$

\] \& 0.0000 \& 170.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.08 \\
& 6.69 \\
& 7.21
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.59 \\
& 5.66 \\
& 6.45
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.11 \\
& 0.17
\end{aligned}
$$
\] <br>

\hline 7770.0 w/ Mtg Pipe (AT\&T) \& B \& From Face \& $$
\begin{gathered}
3.00 \\
-6.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 170.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.08 \\
& 6.69 \\
& 7.21
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.59 \\
& 5.66 \\
& 6.45
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.11 \\
& 0.17
\end{aligned}
$$
\] <br>

\hline | 7770.0 w/ Mtg Pipe |
| :--- |
| (AT\&T) | \& C \& From Face \& \[

$$
\begin{gathered}
3.00 \\
-6.00 \\
0.00
\end{gathered}
$$

\] \& 0.0000 \& 170.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 6.08 \\
& 6.69 \\
& 7.21
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.59 \\
& 5.66 \\
& 6.45
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.06 \\
& 0.11 \\
& 0.17
\end{aligned}
$$
\] <br>

\hline HPA65R-BU8A w/ Mtg Pipe (AT\&T) \& A \& From Face \& $$
\begin{gathered}
3.00 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 170.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 11.23 \\
& 11.85 \\
& 12.47
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
9.94 \\
11.37 \\
12.64
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.17 \\
& 0.27
\end{aligned}
$$
\] <br>

\hline HPA65R-BU8A w/ Mtg Pipe (AT\&T) \& B \& From Face \& $$
\begin{gathered}
3.00 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 170.00 \& No Ice 1/2" Ice 1" Ice \& \[

$$
\begin{aligned}
& 11.23 \\
& 11.85 \\
& 12.47
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
9.94 \\
11.37 \\
12.64
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.17 \\
& 0.27
\end{aligned}
$$
\] <br>

\hline HPA65R-BU8A w/ Mtg Pipe (AT\&T) \& C \& From Face \& $$
\begin{gathered}
3.00 \\
-2.00
\end{gathered}
$$ \& 0.0000 \& 170.00 \& No Ice $1 / 2^{\text {" }}$ Ice \& \[

$$
\begin{aligned}
& 11.23 \\
& 11.85
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
9.94 \\
11.37
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.17
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

| tnxTower | Job | VZW468547A01 | Page 7 of 9 |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| Nexius 300 Apollo Drive, Suite 7 | Project | BURLINGTON_CT | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:12:39 05/08/20 } \end{array}$ |
| Chelmsford, MA 01824 <br> Phone: 1 (978) 923-7965 <br> FAX: | Client | Verizon Wireless | Designed by Akshay Doddamani |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& $C_{A} A_{A}$ Front

\[
f t^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight <br>

\hline \multirow{4}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Face} \& 0.00 \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{170.00} \& 1" Ice \& 12.47 \& 12.64 \& 0.27 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2" Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& 1 " Ice \& 18.63 \& 12.09 \& 0.38 <br>
\hline \multirow[t]{3}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2' Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 18.63 \& 12.09 \& 0.38 <br>
\hline \multirow[t]{3}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2' Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 18.63 \& 12.09 \& 0.38 <br>
\hline \multirow[t]{3}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2' Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 18.63 \& 12.09 \& 0.38 <br>
\hline \multirow[t]{3}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2' Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 18.63 \& 12.09 \& 0.38 <br>
\hline \multirow[t]{3}{*}{800-10966 W/ mtg pipe (AT\&T)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 17.36 \& 9.40 \& 0.14 <br>
\hline \& \& \& 4.00 \& \& \& 1/2' Ice \& 17.99 \& 10.82 \& 0.26 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 18.63 \& 12.09 \& 0.38 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2' Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2' Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2' Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2' Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{| LGP21401 |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.10 \& 0.35 \& 0.01 <br>

\hline \& \& \& -6.00 \& \& \& 1/2' Ice \& 1.24 \& 0.44 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.38 \& 0.54 \& 0.03 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& 4415 \text { B25 RRH } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.84 \& 0.82 \& 0.05 <br>

\hline \& \& \& -2.00 \& \& \& 1/2' Ice \& 2.01 \& 0.94 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.19 \& 1.07 \& 0.08 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& 4415 \text { B25 RRH } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.84 \& 0.82 \& 0.05 <br>

\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 2.01 \& 0.94 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 2.19 \& 1.07 \& 0.08 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& 4415 \text { B25 RRH } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.84 \& 0.82 \& 0.05 <br>

\hline \& \& \& -2.00 \& \& \& 1/2" Ice \& 2.01 \& 0.94 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.19 \& 1.07 \& 0.08 <br>

\hline \multirow[t]{3}{*}{| B2/B66A 8843 RRH |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.64 \& 1.35 \& 0.07 <br>

\hline \& \& \& 2.00 \& \& \& 1/2' Ice \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.97 \& 1.65 \& 0.11 <br>

\hline \multirow[t]{3}{*}{| B2/B66A 8843 RRH |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.64 \& 1.35 \& 0.07 <br>

\hline \& \& \& 2.00 \& \& \& 1/2" Ice \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& $1^{\prime \prime}$ Ice \& 1.97 \& 1.65 \& 0.11 <br>

\hline \multirow[t]{3}{*}{| B2/B66A 8843 RRH |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{170.00} \& No Ice \& 1.64 \& 1.35 \& 0.07 <br>

\hline \& \& \& 2.00 \& \& \& 1/2' Ice \& 1.80 \& 1.50 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 1.97 \& 1.65 \& 0.11 <br>

\hline \multirow[t]{2}{*}{| B5/B12 4449 RRH |
| :--- |
| (AT\&T) |} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{From Face} \& 3.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{170.00} \& No Ice \& 1.64 \& 1.29 \& 0.07 <br>

\hline \& \& \& 6.00 \& \& \& $1 / 2$ ' Ice \& 1.80 \& 1.44 \& 0.09 <br>
\hline
\end{tabular}

| tnxTower <br> Nexius <br> 300 Apollo Drive, Suite 7 <br> Chelmsford, MA 01824 <br> Phone: 1 (978) 923-7965 <br> FAX: | Job | VZW468547A01 | $\begin{aligned} & \text { Page } \\ & 8 \text { of } 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | BURLINGTON_CT | $\begin{aligned} & \text { Date } \\ & \text { 14:12:39 05/08/20 } \end{aligned}$ |
|  | Client | Verizon Wireless | Designed by <br> Akshay Doddamani |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \begin{tabular}{l}
Face \\
or \\
Leg
\end{tabular} \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& $C_{A} A_{A}$ Side

$$
f t^{2}
$$ \& Weight <br>

\hline \multirow{4}{*}{| B5/B12 4449 RRH |
| :--- |
| (AT\&T) |} \& \multirow{4}{*}{B} \& \multirow{4}{*}{From Face} \& 0.00 \& \& \& 1" Ice \& 1.97 \& 1.59 \& 0.11 <br>

\hline \& \& \& 3.00 \& 0.0000 \& 170.00 \& No Ice \& 1.64 \& 1.29 \& 0.07 <br>
\hline \& \& \& 6.00 \& \& \& 1/2" Ice \& 1.80 \& 1.44 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 1.97 \& 1.59 \& 0.11 <br>

\hline \multirow[t]{3}{*}{| B5/B12 4449 RRH |
| :--- |
| (AT\&T) |} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.00 \& 0.0000 \& 170.00 \& No Ice \& 1.64 \& 1.29 \& 0.07 <br>

\hline \& \& \& 6.00 \& \& \& 1/2" Ice \& 1.80 \& 1.44 \& 0.09 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 1.97 \& 1.59 \& 0.11 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { DC6-48-60-18-8F } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 170.00 \& No Ice \& 2.74 \& 4.78 \& 0.03 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.96 \& 5.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.20 \& 5.35 \& 0.10 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { DC6-48-60-18-8F } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 170.00 \& No Ice \& 2.74 \& 4.78 \& 0.03 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.96 \& 5.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 3.20 \& 5.35 \& 0.10 <br>

\hline \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { DC6-48-60-18-8F } \\
& \text { (AT\&T) }
\end{aligned}
$$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 170.00 \& No Ice \& 2.74 \& 4.78 \& 0.03 <br>

\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.96 \& 5.06 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 3.20 \& 5.35 \& 0.10 <br>
\hline \multirow[t]{3}{*}{14-ft Platform reinforced w/ Handrail and Kicker kit (AT\&T)} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 0.00 \& 0.0000 \& 168.00 \& No Ice \& 35.30 \& 35.30 \& 1.85 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 47.90 \& 47.90 \& 2.25 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 60.50 \& 60.50 \& 2.66 <br>
\hline Valmont Light duty \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.00 \& 0.0000 \& 170.00 \& No Ice \& 1.76 \& 1.76 \& 0.05 <br>
\hline Tri-bracket (1) \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.08 \& 2.08 \& 0.07 <br>
\hline (AT\&T) \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 2.40 \& 2.40 \& 0.09 <br>
\hline ***** 132.5 ft ***** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{8' x 2 " Omni} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& 0.0000 \& 132.50 \& No Ice \& 1.60 \& 1.60 \& 0.02 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 2.42 \& 2.42 \& 0.03 <br>
\hline \& \& \& 4.00 \& \& \& 1" Ice \& 3.24 \& 3.24 \& 0.05 <br>
\hline \multirow[t]{3}{*}{3' Yagi} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 4.00 \& 0.0000 \& 132.50 \& No Ice \& 2.08 \& 2.08 \& 0.03 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 3.79 \& 3.79 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 5.50 \& 5.50 \& 0.07 <br>
\hline \multirow[t]{3}{*}{SO 701 (3ft pipe mount side arm)} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 0.00 \& 0.0000 \& 132.50 \& No Ice \& 0.30 \& 0.30 \& 0.01 <br>
\hline \& \& \& -6.00 \& \& \& 1/2" Ice \& 0.61 \& 0.61 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 0.81 \& 0.81 \& 0.09 <br>
\hline
\end{tabular}

## Section Capacity Table

| Section No. | Elevation $f t$ | Component Type | Size | Critical <br> Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \phi P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 179-139.5 | Pole | TP28.0455x19.5x0.1875 | 1 | -11.15 | 1062.10 | 115.2 | Fail ${ }^{\mathbf{3}}$ |
| L2 | 139.5-93.4 | Pole | TP37.5377x26.8051x0.375 | 2 | -21.63 | 3187.78 | 85.3 | Pass |
| L3 | 93.4-46.31 | Pole | TP47.123x35.6737x0.375 | 3 | -35.48 | 3800.33 | 101.7 | Fail $\mathbf{X}$ |
| L4 | 46.31-0 | Pole | TP56.25x44.9739x0.375 | 4 | -54.44 | 4334.66 | 113.7 | Fail $\mathbf{X}$ |
|  |  |  |  |  |  | Pole (L1) | $\begin{gathered} \text { Summary } \\ 115.2 \end{gathered}$ | Fail $\mathbf{X}$ |
|  |  |  |  |  |  | Base Plate RATING = | $\begin{gathered} 99.9 \\ \mathbf{1 1 5 . 2} \end{gathered}$ | Pass <br> Fail |

## nexius

Appendix \#3: Foundation Capacity Check

Drilled Pier Foundation
BU \#
Site Name $\qquad$ CROWN Order Number: VZW468547A01

| TIA-222 Revison: | G |
| ---: | :--- |
| Tower Type: | Monopole |


| Analysis Results |  |  |
| :---: | :---: | :---: |
| Soil Lateral Capacity | Compression | Uplift |
| $\mathrm{D}_{\mathrm{v}=0}(\mathrm{ft} \mathrm{from} \mathrm{TOC)}$ | 6.78 | - |
| Soil Safety Factor | 2.88 | - |
| Max Moment (kip-ft) | 5970.20 | - |
| Rating | 46.1\% | - |
| Soil Vertical Capacity | Compression | Uplift |
| Skin Friction (kips) | 803.42 | - |
| End Bearing (kips) | 99.40 | - |
| Weight of Concrete (kips) | 222.66 | - |
| Total Capacity (kips) | 902.82 | - |
| Axial (kips) | 276.66 | - |
| Rating | 30.6\% | - |
| Reinforced Concrete Capacity | Compression | Uplift |
| Critical Depth (ft from TOC) | 7.25 | - |
| Critical Moment (kip-ft) | 5967.79 | - |
| Critical Moment Capacity | 6608.48 | - |
| Rating | 90.3\% | - |
| Soil Interaction Rating |  |  |
| Structural Foundation Rating |  |  |

## Soil Proffle

| Soil Profile |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Groundwa | Depth | n/a | ft |  |  | \# of Layers | 2 |  |  |  |  |  |  |  |
| Layer | Top <br> (ft) | Bottom <br> (ft) | Thickness <br> (ft) | $\begin{aligned} & \gamma_{\text {soil }} \\ & \text { (pcf) } \end{aligned}$ | $Y_{\text {concrete }}$ (pcf) | Cohesion (ksf) | Angle of Friction (degrees) | Calculated Ultimate Skin Friction Comp (ksf) | Calculated Ultimate Skin Friction Uplift (ksf) | Ultimate Skin Friction Comp Override (ksf) | Ultimate Skin Friction Uplift Override (ksf) | Ult. Gross <br> Bearing <br> Capacity <br> (ksf) | SPT Blow Count | Soil Type |
| 1 | 0 | 3.33 | 3.33 | 130 | 150 |  | 0 | 0.000 | 0.000 |  |  | 0 | n/a | Cohesionless |
| 2 | 3.33 | 27 | 23.67 | 130 | 150 |  | 34 | 1.921 | 1.921 |  |  |  | n/a | Cohesionless |


[^0]:    ${ }^{1}$ Verizon submitted an exempt modification request to the Council in April 2020 that was rendered incomplete due to the absence of the previously approved T-Mobile and AT\&T equipment installations from the SA submitted with the request. On June 19, 2020, Verizon provided the Council with written notification of withdrawal of the request. S: \EMS_TS $\backslash 1 \_B Y T O W N \backslash O r a n g e \backslash O v e r l a n d D r i v e \backslash A T \& T \_C I N G \backslash e m-a t \& t-107-200124 \_2 n d-i n c o m p l e t t r \_\_O v e r l a n d D r i v e . d o c x ~$

[^1]:    Notes:

