

Filed by:

Kri Pelletier, Property Specialist - SBA Communications
134 Flanders Rd., Suite 125, Westborough, MA 01581
508.251.0720 x 3804 - kpelletier@sbasite.com

June 20, 2018

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

Notice of Exempt Modification
100 Tatnic Hill Road, Brooklyn, CT
41 46 1.78 N
-71 58 19.02 W
Sprint #: CT33XC566

Dear Ms. Bachman:

Sprint currently maintains antennas at the 157-foot level of the existing 175-foot Monopole Tower at 100 Tatnic Hill Road in Brooklyn, CT. The tower is owned by SBA Towers, LLC. The property is owned by the Sophie and Benjamin Davidson. Sprint now intends to replace (6) existing cell antennas with (6) newer technology cell antennas at the 157-foot level of the tower. The proposed full scope of work is as follows:

Remove:

- (6) 1-5/8" lines

Remove and Replace:

- Remove:
 - (6) Decibel - DB908h90e-m – Panel Antennas
- Replace with:
 - (3) RFS - APXVTM14-C-I20 – Panel Antennas
 - (3) Commscope - NNVV-65B-R4 – Panel Antennas
 - (3) ALU - 1900 MHz - RRUs
 - (6) ALU - 800 MHz - RRUs
 - (3) ALU - TD-RRH8x20-25 – RRU

Install:

- (1) Handrail Kit & V-Brace Kit:
 - Site Pro PRK-1245L; Site Pro HRK-14-U; Site Pro PRK-SFS-H-L
- (4) 1-1/4" Fiber

Existing Equipment to Remain (Including entitlements):

- (1) Low Profile Platform

At 75':

- (1) GPS
- (1) ½" line

This facility was originally approved by the Town of Brooklyn on August 4, 1999, ahead of Council's jurisdiction. August 8, 1999 publication was made to the Norwich Bulletin confirming Site Plan Approval by the Town's Planning and Zoning Commission. The Town does not have any further documentation of original approval on file and this modification complies with all known conditions.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16.50j-72(b)(2). In accordance with R.C.S.A. § 16.50j-73, a copy of this letter is being sent to the Town of Brooklyn's First Selectman, Richard Ives, and Zoning Enforcement Officer, Martha Fraenkel, as well as to the property owner. (Separate notice is not being sent to tower owner, as it belongs to SBA.)

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. §16.50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modification will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modification will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above-referenced telecommunication facility constitute an exempt modifications under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Kri Pelletier
Property Specialist
SBA COMMUNICATIONS CORPORATION
134 Flanders Rd., Suite 125
Westborough, MA 01581
508.251.0720 x3804 + T
508.366.2610 + F
203.446.7700 + C
kpelletier@sbasite.com
Attachments

cc: Richard Ives, First Selectman / with attachments

Town of Brooklyn, 4 Wolf Den Road, Brooklyn, CT 06234

Martha Fraenkel, Zoning Enforcement Officer / with attachments

Town of Brooklyn, Clifford Green Memorial Center, 69 South Main Street, Brooklyn, CT 06234

Sophie & Benjamin Davidson

18 Nicks Close, St Helens, Tasmania 7216 Australia

POWER DENSITY

SPRINT Site Inventory and Power Data by Antenna

| Sector: | A | Sector: | B | Sector: | C |
|--------------------|--------------------------|--------------------|--------------------------|--------------------|--------------------------|
| Antenna #: | 1 | Antenna #: | 1 | Antenna #: | 1 |
| Make / Model: | Commscope NNVV-65B-R4 | Make / Model: | Commscope NNVV-65B-R4 | Make / Model: | Commscope NNVV-65B-R4 |
| Gain: | 12.75 / 15.05 dBd | Gain: | 12.75 / 15.05 dBd | Gain: | 12.75 / 15.05 dBd |
| Height (AGL): | 157 feet | Height (AGL): | 157 feet | Height (AGL): | 157 feet |
| Frequency Bands | 850 MHz / 1900 MHz (PCS) | Frequency Bands | 850 MHz / 1900 MHz (PCS) | Frequency Bands | 850 MHz / 1900 MHz (PCS) |
| Channel Count | 10 | Channel Count | 10 | Channel Count | 10 |
| Total TX Power(W): | 280 Watts | Total TX Power(W): | 280 Watts | Total TX Power(W): | 280 Watts |
| ERP (W): | 7,378.61 | ERP (W): | 7,378.61 | ERP (W): | 7,378.61 |
| Antenna A1 MPE% | 1.44 % | Antenna B1 MPE% | 1.44 % | Antenna C1 MPE% | 1.44 % |
| Antenna #: | 2 | Antenna #: | 2 | Antenna #: | 2 |
| Make / Model: | RFS APXVTM14-ALU- I20 | Make / Model: | RFS APXVTM14-ALU- I20 | Make / Model: | RFS APXVTM14-ALU- I20 |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 157 feet | Height (AGL): | 157 feet | Height (AGL): | 157 feet |
| Frequency Bands | 2500 MHz (BRS) | Frequency Bands | 2500 MHz (BRS) | Frequency Bands | 2500 MHz (BRS) |
| Channel Count | 8 | Channel Count | 8 | Channel Count | 8 |
| Total TX Power(W): | 160 Watts | Total TX Power(W): | 160 Watts | Total TX Power(W): | 160 Watts |
| ERP (W): | 6,224.72 | ERP (W): | 6,224.72 | ERP (W): | 6,224.72 |
| Antenna A2 MPE% | 0.98 % | Antenna B2 MPE% | 0.98 % | Antenna C2 MPE% | 0.98 % |

| Site Composite MPE% | |
|-------------------------|--------|
| Carrier | MPE% |
| SPRINT – Max per sector | 2.42 % |
| Nextel | 0.26 % |
| Verizon Wireless | 1.72 % |
| T-Mobile | 1.66 % |
| Site Total MPE %: | 6.06 % |

| | |
|------------------------|--------|
| SPRINT Sector A Total: | 2.42 % |
| SPRINT Sector B Total: | 2.42 % |
| SPRINT Sector C Total: | 2.42 % |
| Site Total: | 6.06 % |

| SPRINT Frequency Band / Technology (Per Sector) | # Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ($\mu\text{W}/\text{cm}^2$) | Frequency (MHz) | Allowable MPE ($\mu\text{W}/\text{cm}^2$) | Calculated % MPE |
|---|------------|-------------------------|---------------|---|-----------------|---|------------------|
| Sprint 850 MHz CDMA | 1 | 376.73 | 157 | 0.59 | 850 MHz | 567 | 0.10% |
| Sprint 850 MHz LTE | 2 | 941.82 | 157 | 2.97 | 850 MHz | 567 | 0.52% |
| Sprint 1900 MHz (PCS) CDMA | 5 | 511.82 | 157 | 4.03 | 1900 MHz (PCS) | 1000 | 0.41% |
| Sprint 1900 MHz (PCS) LTE | 2 | 1,279.56 | 157 | 4.03 | 1900 MHz (PCS) | 1000 | 0.41% |
| Sprint 2500 MHz (BRS) LTE | 8 | 778.09 | 157 | 9.81 | 2500 MHz (BRS) | 1000 | 0.98% |
| | | | | | | Total: | 2.42% |

ORIGIN ID:BBFA
RICK WOODS
SBA NETWORK SERVICES INC
134 FLANDERS ROAD
SUITE 125
WESTBOROUGH, MA 01581
UNITED STATES US

(508) 614-0389

SHIP DATE: 19JUN18
ACT WT: 1.001LB
CAD: 105843304/NET3980

BILL SENDER

TO RICHARD IVES, FIRST SELECTMAN

TOWN OF BROOKLYN
4 WOLF DEN ROAD

BROOKLYN CT 06234

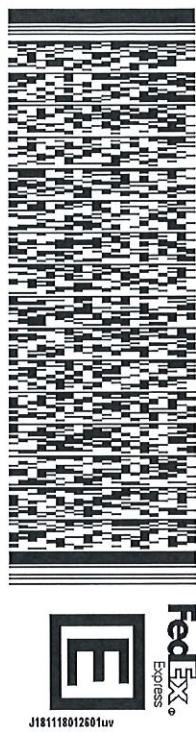
(508) 251-0720 X-3804

INV#

PO#

REF: 1056-92009669

DEPT:



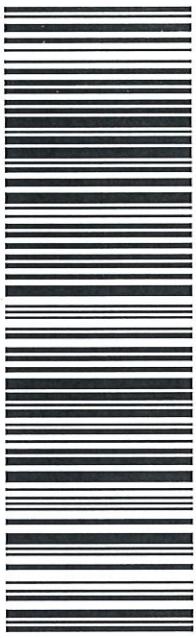
552J293DFDC45

WED - 20 JUN 12:00P
PRIORITY OVERNIGHT

TRK# 7725 1388 3397
0201

EB GONA

06234
CT-US
BDL



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 SBA NETWORK SERVICES INC CAD:105843304/NET3980
 134 FLANDERS ROAD SUITE 125
 WESTBOROUGH, MA 01581
 UNITED STATES US

SHIP DATE: 19 JUN 18
 ACTWGT:100 LB
 CAD:105843304/NET3980
 BILL SENDER

To MARTHA FRAENKEL, ZONING OFFICER

TOWN OF BROOKLYN

CLIFFORD GREEN MEMORIAL CENTER

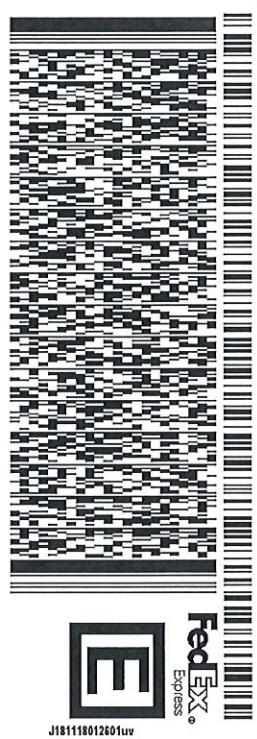
69 SOUTH MAIN STREET

BROOKLYN CT 06234

(508) 251-0720 X-3804

REF: 105843304/NET3980
 PO: DEPT:

552J293DF/DCA5



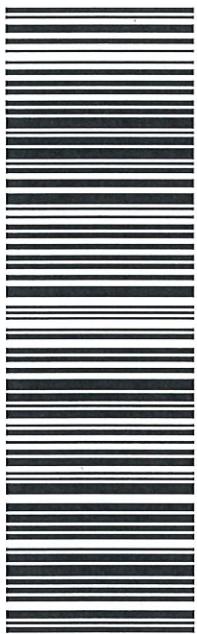
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 PRIORITY OVERNIGHT

TRK#
 0201

7725 1392 4850

EB GONA

06234
 CT-US
 BDL



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 KRI PELLETIER
 SB COMMUNICATIONS CORPORATION
 134 FLANDERS RD
 SUITE 25
 WESTBOROUGH, MA 01581 US
 SIGN: KRI PELLETIER

SHIP DATE: 20JUN18
 ACTWTG: 1.00 LB
 CAD: 105843304/NET:3980
 BILL SENDER
 NO EEE 30.37(a)

TO SOPHIE & BENJAMIN DAVIDSON

18 NICKS CLOSE

ST HELENS 7216

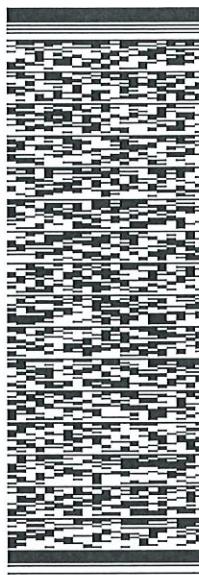
5082510720
 INV:
 PO:

REF: 1056920096089
 DEPT:



(AU)

552J293DFDC45



PM

INTL ECONOMY

TRK# 7725 2030 8172
 0430

7216
 SYD
 -AU



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 SBA COMMUNICATIONS CORPORATION
 134 Flanders Rd
 Suite 125
 Westborough, MA 01581
 UNITED STATES, US

Ship Date: 20JUN18
 AcWgt: 1.00LB
 CAD: 105843304/NET-3980
 BILL SENDER
 ENVAT:

To Sophie & Benjamin Davidson

18 Nicks Close

ST HELENS, 7216

(AU)



5082510720

S6 LSTX

AWB

J181118012620uv



Form
0430

PKG TYPE: ENV

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DISC1:Proposals

DISC2:

DISC3:

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EEI: NO EEE 30.37(a)

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 Suite 125
 Westborough, MA 01581
 UNITED STATES, US

Ship Date: 20 JUN 18
 ActWgt: 1.00 LB
 CAD: 105843304/NET13980
 BILL-SENDER
 EIN/VAT:

To Sophie & Benjamin Davidson

18 Nicks Close

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DESC2:

DESC3:

DESC4:

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SIGN: Kit Pelleter
 T/C: S 500575468
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100 TATNIC HILL RD**Location** 100 TATNIC HILL RD**Mblu** 15/ / 16-5/ /**Acct#** 00116805**Owner** DAVIDSON BENJAMIN & SOPHIE**Assessment** \$193,800**Appraisal** \$276,900**PID** 1241**Building Count** 1**Current Value**

| Appraisal | | | |
|----------------|--------------|-----------|-----------|
| Valuation Year | Improvements | Land | Total |
| 2016 | \$0 | \$276,900 | \$276,900 |
| Assessment | | | |
| Valuation Year | Improvements | Land | Total |
| 2016 | \$0 | \$193,800 | \$193,800 |

Owner of Record

Owner DAVIDSON BENJAMIN & SOPHIE
Co-Owner C/O SBA TOWERS
Care Of
Address ATTN: TAX DEPT CT01915-S
 8051 CONGRESS AVE
 BOCA RATON, FL 33487-1307

Sale Price \$0
Certificate
Book & Page 216/ 6
Sale Date 09/09/1999
Qualified U

3+ this is
 SBA's
 address

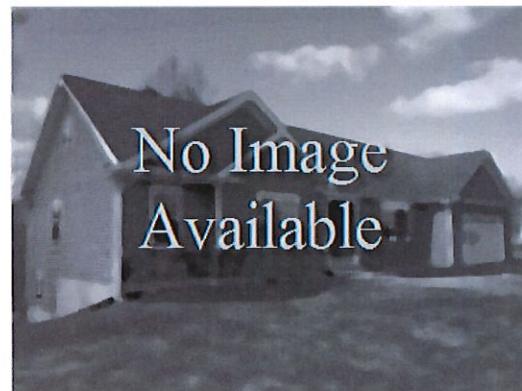
Ownership History

| Ownership History | | | | |
|----------------------------|------------|-------------|-------------|------------|
| Owner | Sale Price | Certificate | Book & Page | Sale Date |
| DAVIDSON BENJAMIN & SOPHIE | \$0 | | 216/ 6 | 09/09/1999 |
| HALE NEWELL D | \$0 | | 112/ 259 | 04/29/1991 |

Building Information**Building 1 : Section 1****Year Built:****Living Area:** 0**Building Photo****Replacement Cost:** \$0**Building Percent****Good:****Replacement Cost****Less Depreciation:** \$0**Building Attributes**

| Field | Description |
|-------|-------------|
| | |

| | |
|--------------------|-------------|
| Style | Vacant Land |
| Model | |
| Grade: | |
| Stories: | |
| Occupancy | |
| Exterior Wall 1 | |
| Exterior Wall 2 | |
| Roof Structure: | |
| Roof Cover | |
| Interior Wall 1 | |
| Interior Wall 2 | |
| Interior Flr 1 | |
| Interior Flr 2 | |
| Heat Fuel | |
| Heat Type: | |
| AC Type: | |
| Total Bedrooms: | |
| Total Bthrms: | |
| Total Half Baths: | |
| Total Xtra Fixtrs: | |
| Total Rooms: | |
| Bath Style: | |
| Kitchen Style: | |



(http://images.vgsi.com/photos/BrooklynCTPhotos//default.jpg)

Building Layout

(http://images.vgsi.com/photos/BrooklynCTPhotos//Sketches/12-

| Building Sub-Areas (sq ft) | Legend |
|--------------------------------|--------|
| No Data for Building Sub-Areas | |



Extra Features

| Extra Features | Legend |
|----------------------------|--------|
| No Data for Extra Features | |

Land

Land Use

| | |
|---------------|--------|
| Use Code | 1300 |
| Description | VACANT |
| Zone | RA |
| Neighborhood | 0050 |
| Alt Land Appr | No |
| Category | |

Land Line Valuation

| | |
|-----------------|-----------|
| Size (Acres) | 1.67 |
| Frontage | |
| Depth | |
| Assessed Value | \$193,800 |
| Appraised Value | \$276,900 |

Outbuildings

| Outbuildings | Legend |
|--------------------------|--------|
| No Data for Outbuildings | |

Valuation History

| Appraisal | | | |
|-----------------------|---------------------|-------------|--------------|
| Valuation Year | Improvements | Land | Total |
| 2017 | \$0 | \$276,900 | \$276,900 |
| 2016 | \$0 | \$276,900 | \$276,900 |
| 2015 | \$0 | \$276,900 | \$276,900 |

| Assessment | | | |
|-----------------------|---------------------|-------------|--------------|
| Valuation Year | Improvements | Land | Total |
| 2017 | \$0 | \$193,800 | \$193,800 |
| 2016 | \$0 | \$193,800 | \$193,800 |
| 2015 | \$0 | \$193,800 | \$193,800 |

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RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

SPRINT Existing Facility

Site ID: CT33XC566

Brooklyn
100 Old Tatnic Hill Road
Brooklyn, CT 06234

June 15, 2018

EBI Project Number: 6218004397

| Site Compliance Summary | |
|---|------------------|
| Compliance Status: | COMPLIANT |
| Site total MPE% of FCC general population allowable limit: | 6.06 % |



June 15, 2018

SPRINT
Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495

Emissions Analysis for Site: **CT33XC566 – Brooklyn**

EBI Consulting was directed to analyze the proposed SPRINT facility located at **100 Old Tatnic Hill Road, Brooklyn, CT**, for the purpose of determining whether the emissions from the Proposed SPRINT Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

General population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 850 MHz Band is approximately $567 \mu\text{W}/\text{cm}^2$. The general population exposure limit for the 1900 MHz (PCS) and 2500 MHz (BRS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed SPRINT Wireless antenna facility located at **100 Old Tatnic Hill Road, Brooklyn, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since SPRINT is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 1 CDMA channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.
- 2) 2 LTE channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 50 Watts per Channel.
- 3) 5 CDMA channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 16 Watts per Channel.
- 4) 2 LTE channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 5) 8 LTE channels (2500 MHz (BRS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.



- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the **Commscope NNVV-65B-R4** and the **RFS APXVTM14-ALU-I20** for transmission in the 850 MHz, 1900 MHz (PCS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerlines of the proposed antennas are **157 feet** above ground level (AGL) for **Sector A**, **157 feet** above ground level (AGL) for **Sector B** and **157 feet** above ground level (AGL) for Sector C.
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general population threshold limits.



SPRINT Site Inventory and Power Data by Antenna

| Sector: | A | Sector: | B | Sector: | C |
|--------------------|--------------------------|--------------------|--------------------------|--------------------|--------------------------|
| Antenna #: | 1 | Antenna #: | 1 | Antenna #: | 1 |
| Make / Model: | Commscope NNVV-65B-R4 | Make / Model: | Commscope NNVV-65B-R4 | Make / Model: | Commscope NNVV-65B-R4 |
| Gain: | 12.75 / 15.05 dBd | Gain: | 12.75 / 15.05 dBd | Gain: | 12.75 / 15.05 dBd |
| Height (AGL): | 157 feet | Height (AGL): | 157 feet | Height (AGL): | 157 feet |
| Frequency Bands | 850 MHz / 1900 MHz (PCS) | Frequency Bands | 850 MHz / 1900 MHz (PCS) | Frequency Bands | 850 MHz / 1900 MHz (PCS) |
| Channel Count | 10 | Channel Count | 10 | Channel Count | 10 |
| Total TX Power(W): | 280 Watts | Total TX Power(W): | 280 Watts | Total TX Power(W): | 280 Watts |
| ERP (W): | 7,378.61 | ERP (W): | 7,378.61 | ERP (W): | 7,378.61 |
| Antenna A1 MPE% | 1.44 % | Antenna B1 MPE% | 1.44 % | Antenna C1 MPE% | 1.44 % |
| Antenna #: | 2 | Antenna #: | 2 | Antenna #: | 2 |
| Make / Model: | RFS APXVTM14-ALU-I20 | Make / Model: | RFS APXVTM14-ALU-I20 | Make / Model: | RFS APXVTM14-ALU-I20 |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 157 feet | Height (AGL): | 157 feet | Height (AGL): | 157 feet |
| Frequency Bands | 2500 MHz (BRS) | Frequency Bands | 2500 MHz (BRS) | Frequency Bands | 2500 MHz (BRS) |
| Channel Count | 8 | Channel Count | 8 | Channel Count | 8 |
| Total TX Power(W): | 160 Watts | Total TX Power(W): | 160 Watts | Total TX Power(W): | 160 Watts |
| ERP (W): | 6,224.72 | ERP (W): | 6,224.72 | ERP (W): | 6,224.72 |
| Antenna A2 MPE% | 0.98 % | Antenna B2 MPE% | 0.98 % | Antenna C2 MPE% | 0.98 % |

| Site Composite MPE% | |
|--------------------------|---------------|
| Carrier | MPE% |
| SPRINT – Max per sector | 2.42 % |
| Nextel | 0.26 % |
| Verizon Wireless | 1.72 % |
| T-Mobile | 1.66 % |
| Site Total MPE %: | 6.06 % |

| | |
|------------------------|---------------|
| SPRINT Sector A Total: | 2.42 % |
| SPRINT Sector B Total: | 2.42 % |
| SPRINT Sector C Total: | 2.42 % |
| Site Total: | 6.06 % |

| SPRINT – Frequency Band / Technology (Per Sector) | # Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ($\mu\text{W}/\text{cm}^2$) | Frequency (MHz) | Allowable MPE ($\mu\text{W}/\text{cm}^2$) | Calculated % MPE |
|---|------------|-------------------------|---------------|---|-----------------|---|------------------|
| Sprint 850 MHz CDMA | 1 | 376.73 | 157 | 0.59 | 850 MHz | 567 | 0.10% |
| Sprint 850 MHz LTE | 2 | 941.82 | 157 | 2.97 | 850 MHz | 567 | 0.52% |
| Sprint 1900 MHz (PCS) CDMA | 5 | 511.82 | 157 | 4.03 | 1900 MHz (PCS) | 1000 | 0.41% |
| Sprint 1900 MHz (PCS) LTE | 2 | 1,279.56 | 157 | 4.03 | 1900 MHz (PCS) | 1000 | 0.41% |
| Sprint 2500 MHz (BRS) LTE | 8 | 778.09 | 157 | 9.81 | 2500 MHz (BRS) | 1000 | 0.98% |
| | | | | | | Total: | 2.42% |



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the SPRINT facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| SPRINT Sector | Power Density Value (%) |
|------------------------------------|-------------------------|
| Sector A: | 2.42 % |
| Sector B: | 2.42 % |
| Sector C: | 2.42 % |
| SPRINT Maximum Total (per sector): | 2.42 % |
| Site Total: | 6.06 % |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is **6.06 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



Tower Engineering Solutions

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8445 Freeport Parkway, Suite 375, Irving, Texas 75063

Structural Analysis Report

Existing 175 ft. SUMMIT Monopole

Customer Name: SBA Communications Corp

Customer Site Number: CT01915-S

Customer Site Name: South Brooklyn

Carrier Name: Sprint Nextel

Carrier Site ID / Name: CT33XC566 / Brooklyn

Site Location: 100 Old Tatnic Hill Road

Brooklyn, Connecticut

Windham County

Latitude: 41.767160

Longitude: -71.971949

Analysis Result:

Max Structural Usage: 80.8% [Pass]

Max Foundation Usage: 49.0% [Pass]

Additional Usage Caused by Mount Modification: 5.0%



Report Prepared By : Delu Zhou

Introduction

The purpose of this report is to summarize the analysis results on the 175 ft. SUMMIT Monopole to support the proposed antennas and transmission lines in addition to those currently installed. Any modification listed under Sources of Information was assumed completed and was included in this analysis.

Sources of Information

| | |
|------------------------------|--|
| Tower Drawings | Tower Drawings prepared by Paul J. Ford and Company, Job # 29200-401 Dated 04/05/2000 |
| Foundation Drawing | Foundation Drawings prepared by Paul J. Ford and Company, Job # 29200-401 Dated 04/05/2000 |
| Geotechnical Report | Geotechnical Report prepared by FDH Engineering, Project # 1201186EG1 Dated 08/16/2012 |
| Modification Drawings | N/A |

Analysis Criteria

The rigorous analysis was performed in accordance with the requirements and stipulations of the ANSI/TIA/EIA 222-G. In accordance with this standard, the structure was analyzed using **TESPoles**, a proprietary analysis software. The program considers the structure as an elastic 3-D model with second-order effects and temperature effects incorporated in the analysis. The analysis was performed using multiple wind directions.

| | |
|---|--|
| Wind Speed Used in the Analysis: | Ultimate Design Wind Speed V_{ult} = 130.0 mph (3-Sec. Gust)/ Nominal Design Wind Speed V_{asd} = 101.0 mph (3-Sec. Gust) |
| Wind Speed with Ice: | 50 mph (3-Sec. Gust) with 1" radial ice concurrent |
| Operational Wind Speed: | 60 mph + 0" Radial ice |
| Standard/Codes: | ANSI/TIA/EIA 222-G / 2012 IBC / 2016 Connecticut State Building Code |
| Exposure Category: | B |
| Structure Class: | II |
| Topographic Category: | 1 |
| Crest Height: | 0 ft. |
| Seismic Parameters: | $S_S = 0.171$, $S_1 = 0.062$ |

This structural analysis is based upon the tower being classified as a Structure Class II; however, if a different classification is required subsequent to the date hereof, the tower classification will be changed to meet such requirement and a new structural analysis will be run.

Existing Antennas, Mounts and Transmission Lines

The table below summarizes the antennas, mounts and transmission lines that were considered in the analysis as existing on the tower.

| Items | Elevation (ft.) | Qty. | Antenna Descriptions | Mount Type & Qty. | Transmission Lines | Owner |
|-------|-----------------|------|--|---|---------------------------------|---------------|
| 1 | 175.0 | 3 | Antel - BXA-70063/6CF - Panel | (1) Low Profile Platform | (12) 1 5/8" (1) 1 5/8" Fiber | Verizon |
| 2 | | 3 | Antel - BXA-171085/12CF - Panel | | | |
| 3 | | 3 | Antel - BXA-70080/6CF - Panel | | | |
| 4 | | 3 | Antel - WBX065X19R050 - Panel | | | |
| 5 | | 3 | Alcatel - RRH2x40-AWS - RRH | | | |
| 6 | | 6 | RFS - FD9R6004/2C-3L - Diplexer | | | |
| 7 | | 1 | RFS - DB-T1-6Z-8AB-0Z - Distribution Box | | | |
| - | 157.0 | 6 | Decibel - DB908h90e-m - Panel | (1) Low Profile Platform | (6) 1 5/8" | Sprint Nextel |
| 12 | 140.0 | 3 | RFS - APXV18-206516S-C-A20 - Panel | (1) Platform w/Handrails (HRK CommScope P/N MT-195-12) | (12) 1 5/8" | T-Mobile |
| 13 | | 3 | Commscope - LNX-6515DS-VTM - Panel | | | |
| 14 | | 3 | Ericsson - KRY 112 144/1 - TMA | | | |
| 15 | | 3 | Kathrein - 782 11056 - Bias T | | | |
| - | 75.0 | 1 | GPS | Direct | (1) 1/2" | Sprint Nextel |

Proposed Carrier's Final Configuration of Antennas, Mounts and Transmission Lines

Information pertaining to the proposed carrier's final configuration of antennas and transmission lines was provided by SBA Communications Corp. The proposed antennas and lines are listed below.

| Items | Elevation (ft) | Qty. | Antenna Descriptions | Mount Type & Qty. | Transmission Lines | Owner |
|-------|----------------|------|---------------------------------|--|--------------------|------------------|
| 8 | 157.0 | 3 | RFS - APXVTM14-C-I20 - Panel | (1) LP Platform w/ handrail kit & v-brace kit [(1) SitePro PRK-1245L (1) SitePro HRK-14-U & (1) SitePro PRK-SFS-H-L] | (4) 1 1/4" Fiber | Sprint Nextel |
| 9 | | 3 | Commscope - NNVV-65B-R4 - Panel | | | |
| 10 | | 3 | ALU - 1900 MHz - RRU | | | |
| 11 | | 6 | ALU - 800 MHz - RRU | | | |
| 12 | | 3 | ALU - TD-RRH8x20-25 - RRU | | | |
| 17 | 75.0 | 1 | GPS | Dircect | (1) 1/2" | |

See the attached coax layout for the line placement considered in the analysis.

Analysis Results

The results of the structural analysis, performed for the wind and ice loading and antenna equipment as defined above, are summarized as the following:

| | Pole shafts | Anchor Bolts | Base Plate | Flange Plate |
|-------------|--------------|--------------|--------------|--------------|
| Max. Usage: | 64.9% | 32.7% | 63.7% | 80.8% |
| Pass/Fail | Pass | Pass | Pass | Pass |

Foundations

| | Moment (Kip-Ft) | Shear (Kips) |
|---------------------------|-----------------|--------------|
| Original Design Reactions | 3710.0 | 29.7 |
| Analysis Reactions | 3437.1 | 27.6 |
| Factored Reactions* | 5008.5 | 40.1 |
| % of Design Reactions | 68.7% | 68.8% |

* Per section 15.5.1 of the TIA-222-G standard, factored reactions were obtained by multiplying a 1.35 factor to the original design reactions.

The foundation has been investigated using the supplied documents and soils report and was found adequate. Therefore, no modification to the foundation will be required.

Operational Condition (Rigidity):

Operational characteristics of the tower are found to be within the limits prescribed by ANSI/TIA/EIA 222-G for the installed antennas. The maximum twist/sway at the elevation of the proposed equipment is 1.3471 degrees under the operational wind speed as specified in the Analysis Criteria.

Conclusions

Based on the analysis results, the existing structure and its foundation were found to be adequate to safely support the existing and proposed equipment and meet the minimum requirements per the ANSI/TIA/EIA 222-G Standard under the design basic wind speed as specified in the Analysis Criteria.

Standard Conditions

1. This analysis was performed based on the information supplied to **(TES) Tower Engineering Solutions, LLC**. Verification of the information provided was not included in the Scope of Work for **TES**. The accuracy of the analysis is dependent on the accuracy of the information provided.
2. The analysis is based on the presumption that the tower members and components along with any existing reinforcement items have been correctly and properly designed, manufactured, installed and maintained.
3. All the existing structural members were assumed to be in good condition with no physical damage or deterioration associated with corrosion.
4. An initial tension of 10% of the break strength on all the existing guy wires was assumed in all the structural analyses of guyed towers unless different values were provided by the client. **TES** cannot take responsibility for the deviations in the analysis results because of differences in the initial tension forces of the existing guy wires.
5. Secondary component or connection secondary components, welds and bolts are assumed to be able to carry their intended original design loads. **TES** cannot take responsibility for verification of the adequacy on the connections, bolts and welds present in the structure.
6. The analyses will be performed based on the codes as specified by the client or based on the best knowledge of the engineering staff of **TES**. In the absence of information to the contrary, all work will be performed in accordance with the latest relevant revision of ANSI/TIA-222. If wind speed and/or ice loads are different from the minimum values recommended by the EIA/TIA-222 standard or other codes, **TES** should be notified in writing and the applicable minimum values provided by the client.
7. The configuration of the existing mounts, antennas, coax and other appurtenances were supplied by the customer for the current structural analysis. **TES** has not visited the tower site to verify the adequacy of the information provided. If there is any discrepancy found in the report regarding the existing conditions, **TES** should be notified immediately to evaluate the effect of the discrepancy on the analysis results.
8. The client will assume responsibility for rework associated with the differences in initially provided information, including tower and foundation information, existing and/or proposed equipment and transmission lines.
9. If a feasibility analysis was performed, final acceptance of changed conditions shall be based upon a rigorous structural analysis.

Usage Diagram - Max Ratio 64.91% at 83.8ft

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)

Code: EIA/TIA-222-G
Exposure: B
G_h: 1.1

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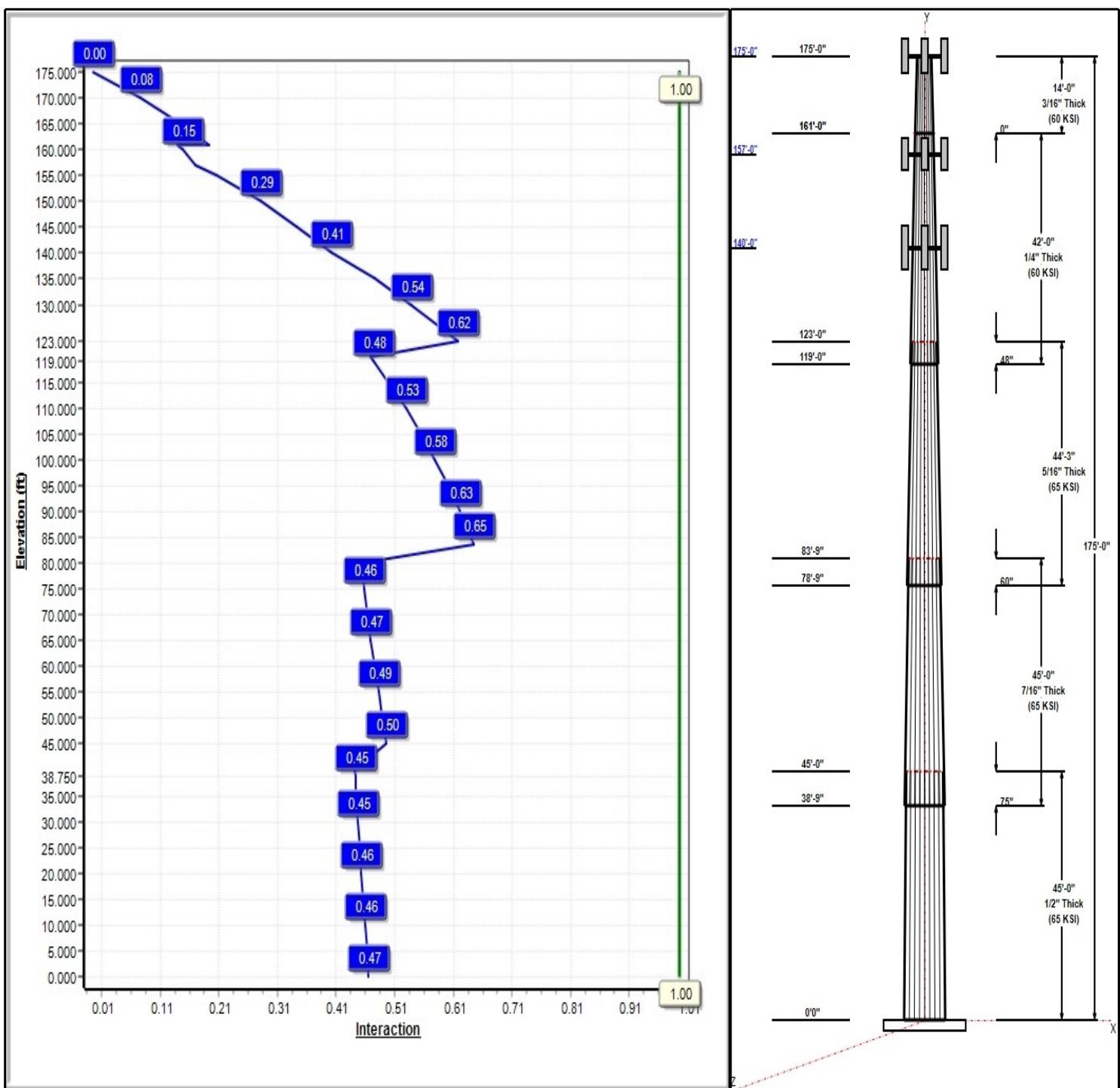
Dead Load Factor: 1.20
Wind Load Factor: 1.60

Load Case : 1.2D + 1.6W 101 mph Wind



Iterations: 25

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Structure: CT01915-S-SBA

Type: Tapered
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.00 (ft)

Base Shape: 18 Sided
Taper: 0.23000

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| Shaft Properties | | | | | | | |
|------------------|-------------|----------|-------------|------------|------------|---------|-------------|
| Seq | Length (ft) | Top (in) | Bottom (in) | Thick (in) | Joint Type | Taper | Grade (ksi) |
| 1 | 45.00 | 46.68 | 57.03 | 0.500 | | 0.23000 | 65 |
| 2 | 45.00 | 38.64 | 48.99 | 0.438 | Slip | 0.23000 | 65 |
| 3 | 44.25 | 30.24 | 40.42 | 0.313 | Slip | 0.23000 | 65 |
| 4 | 42.00 | 22.00 | 31.66 | 0.250 | Slip | 0.23000 | 60 |
| 5 | 14.00 | 18.78 | 22.00 | 0.188 | Butt | 0.23000 | 60 |

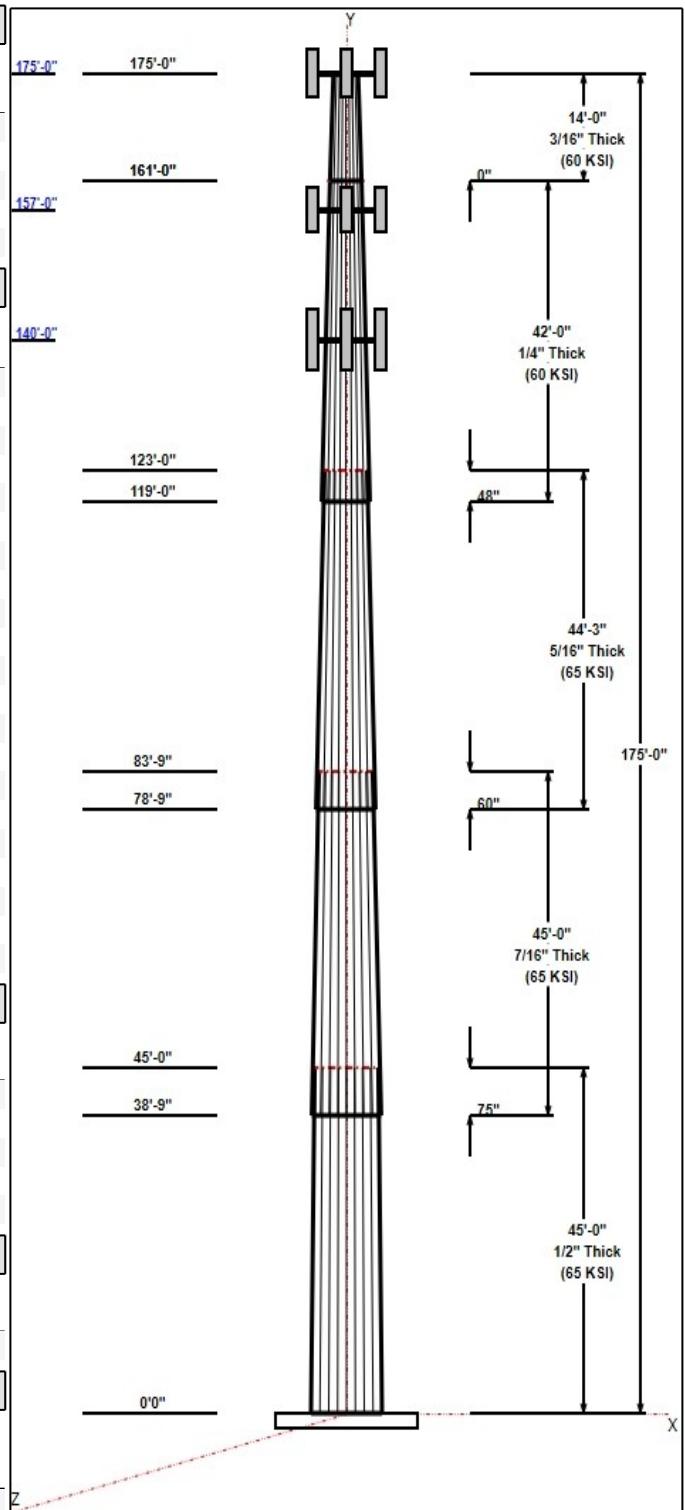
| Discrete Appurtenances | | | | |
|------------------------|-----------------|-----|---------------------------|---------------|
| Attach Elev (ft) | Force Elev (ft) | Qty | Description | Carrier |
| 175.00 | 175.00 | 1 | 6' Lightning rod | |
| 175.00 | 175.00 | 3 | BXA-70063/6CF | Verizon |
| 175.00 | 175.00 | 3 | BXA-171085/12CF | Verizon |
| 175.00 | 175.00 | 3 | WBX065X19R050 | Verizon |
| 175.00 | 175.00 | 3 | BXA-70080/6CF | Verizon |
| 175.00 | 175.00 | 3 | RRH2x40-AWS | Verizon |
| 175.00 | 175.00 | 6 | FD9R6004/2C-3L (3.1 lbs) | Verizon |
| 175.00 | 175.00 | 1 | DB-T1-6Z-8AB-0Z | Verizon |
| 175.00 | 175.00 | 1 | Low Profile Platform-flat | Verizon |
| 157.00 | 157.00 | 1 | Platform w/ Handrail + | Sprint Nextel |
| 157.00 | 157.00 | 3 | APXVTM14-C-I20 | Sprint Nextel |
| 157.00 | 157.00 | 3 | NNVV-65B-R4 | Sprint Nextel |
| 157.00 | 157.00 | 3 | ALU - 1900 MHz - RRU | Sprint Nextel |
| 157.00 | 157.00 | 6 | ALU - 800 MHz - RRU | Sprint Nextel |
| 157.00 | 157.00 | 3 | ALU - TD-RRH8x20-25 - | Sprint Nextel |
| 140.00 | 140.00 | 3 | APXV18-206516S-C-A20 | T-Mobile |
| 140.00 | 140.00 | 3 | LNX-6515DS-VTM | T-Mobile |
| 140.00 | 140.00 | 3 | KRY 112 144/1 | T-Mobile |
| 140.00 | 140.00 | 3 | 782 11056 | T-Mobile |
| 140.00 | 140.00 | 1 | Platform w/ Hand Rails | T-Mobile |
| 75.00 | 75.00 | 1 | GPS | Sprint Nextel |

| Linear Appurtenances | | | | |
|----------------------|--------------|-----------|---------------|---------------|
| Elev From (ft) | Elev To (ft) | Placement | Description | Carrier |
| 0.00 | 175.00 | Inside | 1 5/8" Coax | Verizon |
| 0.00 | 175.00 | Inside | 1 5/8" Hybrid | Verizon |
| 0.00 | 157.00 | Inside | 1 1/4" Fiber | Sprint Nextel |
| 0.00 | 140.00 | Inside | 1 5/8" Coax | T-Mobile |
| 0.00 | 75.00 | Inside | 1/2" Coax | Sprint Nextel |

| Anchor Bolts | | | |
|--------------|----------------|-------------|-------------|
| Qty | Specifications | Grade (ksi) | Arrangement |
| 32 | 2.25" 18J | 75.0 | Cluster |

| Base Plate | | | |
|----------------|---------------------|-------------|----------|
| Thickness (in) | Specifications (in) | Grade (ksi) | Geometry |
| 2.5000 | 68.0 | 50.0 | Clipped |

| Reactions | | | |
|--------------------------|------------------|--------------|--------------|
| Load Case | Moment (FT-Kips) | Shear (Kips) | Axial (Kips) |
| 1.2D + 1.6W 101 mph Wind | 3439.1 | 27.6 | 51.4 |



Structure: CT01915-S-SBA

Type: Tapered
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.00 (ft)

Base Shape: 18 Sided
Taper: 0.23000

5/23/2018

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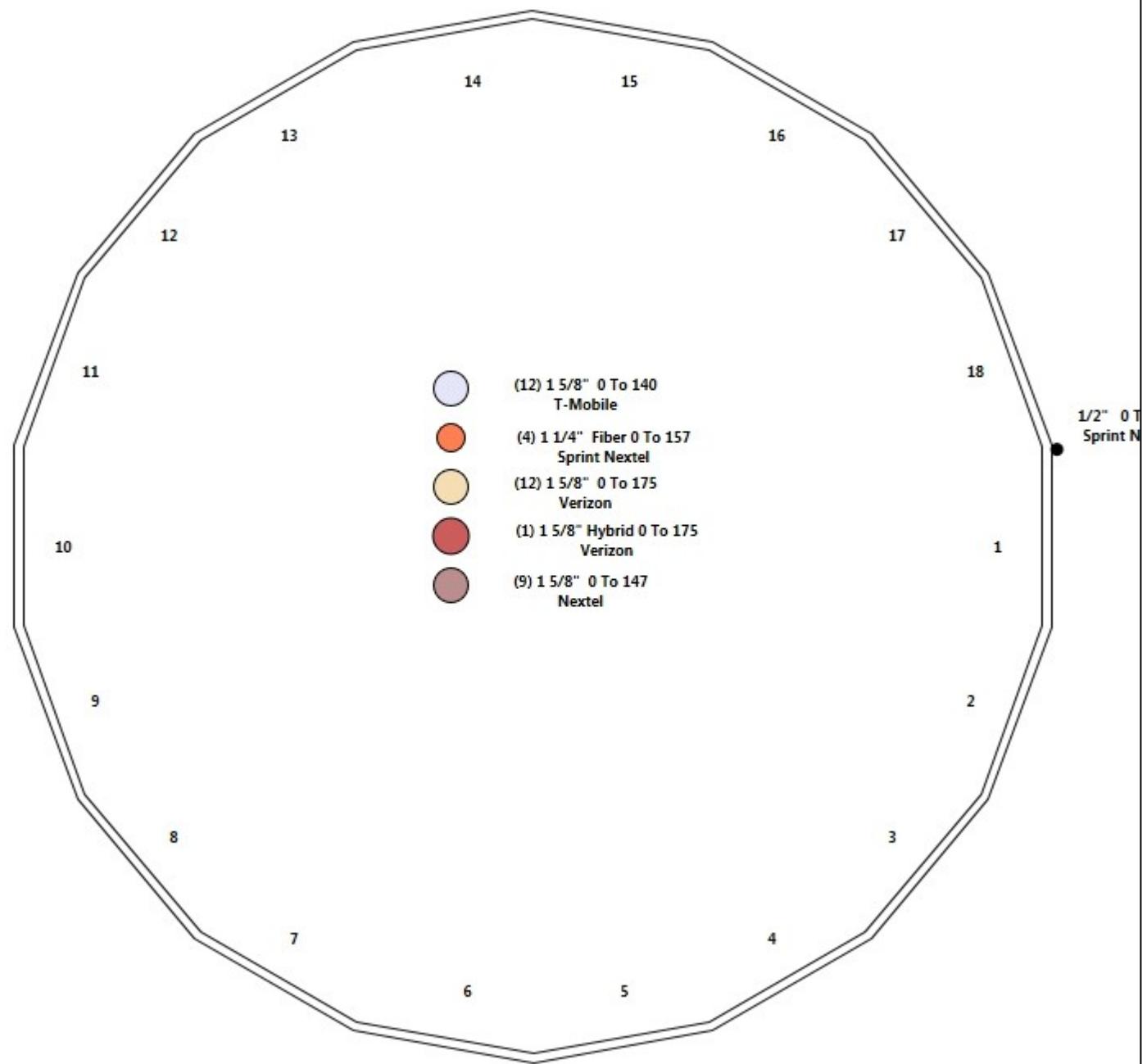
| | | | |
|----------------------------------|--------|------|------|
| 0.9D + 1.6W 101 mph Wind | 3401.6 | 27.6 | 38.5 |
| 1.2D + 1.0Di + 1.0Wi 50 mph Wind | 1026.1 | 8.0 | 83.6 |
| 1.2D + 1.0E | 196.4 | 1.6 | 51.4 |
| 0.9D + 1.0E | 194.1 | 1.6 | 38.6 |
| 1.0D + 1.0W 60 mph Wind | 754.0 | 6.1 | 42.8 |

Structure: CT01915-S-SBA - Coax Line Placement

Type: Monopole
Site Name: South Brooklyn
Height: 175.00 (ft)

5/23/2018

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Shaft Properties

Structure: CT01915-S-SBA

Code: EIA/TIA-222-G

5/23/2018

Site Name: South Brooklyn

Exposure: B

Height: 175.00 (ft)

Crest Height: 0.00

Base Elev: 0.000 (ft)

Site Class: D - Stiff Soil

Gh: 1.1

Topography: 1

Struct Class: II

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| Sec. No. | Shape | Length (ft) | Thick (in) | Fy (ksi) | Joint Type | Overlap (in) | Weight (lb) |
|----------------------------|-------|-------------|------------|----------|------------|--------------|---------------|
| 1 | 18 | 45.000 | 0.5000 | 65 | | 0.00 | 12,479 |
| 2 | 18 | 45.000 | 0.4375 | 65 | Slip | 75.00 | 9,224 |
| 3 | 18 | 44.250 | 0.3125 | 65 | Slip | 60.00 | 5,229 |
| 4 | 18 | 42.000 | 0.2500 | 60 | Slip | 48.00 | 3,014 |
| 5 | 18 | 14.000 | 0.1875 | 60 | Flange | 0.00 | 573 |
| Total Shaft Weight: | | | | | | | 30,519 |

Bottom

| Sec. No. | Dia (in) | Elev (ft) | Area (sqin) | Ix (in^4) | W/t Ratio | D/t Ratio | Dia (in) | Elev (ft) | Area (sqin) | Ix (in^4) | W/t Ratio | D/t Ratio | Taper |
|----------|----------|-----------|-------------|-----------|-----------|-----------|----------|-----------|-------------|-----------|-----------|-----------|----------|
| 1 | 57.03 | 0.00 | 89.71 | 36220.24 | 18.70 | 114.06 | 46.68 | 45.00 | 73.29 | 19745.8 | 15.05 | 93.36 | 0.230000 |
| 2 | 48.99 | 38.75 | 67.42 | 20082.80 | 18.33 | 111.98 | 38.64 | 83.75 | 53.05 | 9783.25 | 14.16 | 88.33 | 0.230000 |
| 3 | 40.42 | 78.75 | 39.78 | 8083.32 | 21.39 | 129.34 | 30.24 | 123.00 | 29.68 | 3358.97 | 15.65 | 96.77 | 0.230000 |
| 4 | 31.66 | 119.0 | 24.92 | 3106.62 | 20.92 | 126.64 | 22.00 | 161.00 | 17.26 | 1031.48 | 14.11 | 88.00 | 0.230000 |
| 5 | 22.00 | 161.0 | 12.98 | 780.30 | 19.28 | 117.33 | 18.78 | 175.00 | 11.06 | 483.24 | 16.25 | 100.1 | 0.230000 |

Top

Load Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Topography: 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Discrete Appurtenances

| No. | Elev (ft) | Description | Qty | No Ice | | | Ice | | | Hor. Ecc. (ft) | Vert Ecc (ft) |
|----------------|--------------|-------------------------------|-----------|-----------------|--------------|----------------|------------------|--------------|----------------|----------------------|---------------------|
| | | | | Weight (lb) | CaAa (sf) | CaAa Factor | Weight (lb) | CaAa (sf) | CaAa Factor | | |
| 1 | 175.00 | 6' Lightning rod | 1 | 6.50 | 0.38 | 1.00 | 55.65 | 1.853 | 1.00 | 0.00 | 0.00 |
| 2 | 175.00 | BXA-70063/6CF | 3 | 17.00 | 7.57 | 0.70 | 208.88 | 11.312 | 0.70 | 0.00 | 0.00 |
| 3 | 175.00 | BXA-171085/12CF | 3 | 15.00 | 4.78 | 0.84 | 144.86 | 7.988 | 0.84 | 0.00 | 0.00 |
| 4 | 175.00 | WBX065X19R050 | 3 | 20.90 | 5.22 | 0.72 | 141.43 | 8.605 | 0.72 | 0.00 | 0.00 |
| 5 | 175.00 | BXA-70080/6CF | 3 | 18.00 | 5.84 | 0.88 | 188.52 | 9.069 | 0.88 | 0.00 | 0.00 |
| 6 | 175.00 | RRH2x40-AWS | 3 | 44.00 | 2.52 | 0.82 | 126.22 | 4.176 | 0.82 | 0.00 | 0.00 |
| 7 | 175.00 | FD9R6004/2C-3L (3.1 lbs) | 6 | 3.10 | 0.36 | 0.67 | 13.97 | 0.960 | 0.67 | 0.00 | 0.00 |
| 8 | 175.00 | DB-T1-6Z-8AB-0Z | 1 | 18.90 | 4.80 | 0.71 | 226.05 | 6.011 | 0.71 | 0.00 | 0.00 |
| 9 | 175.00 | Low Profile Platform-flat | 1 | 1200.00 | 25.00 | 1.00 | 2617.86 | 53.357 | 1.00 | 0.00 | 0.00 |
| 10 | 157.00 | Platform w/ Handrail + | 1 | 2800.00 | 54.00 | 1.00 | 6072.63 | 14.590 | 1.00 | 0.00 | 0.00 |
| 11 | 157.00 | APXVTM14-C-I20 | 3 | 56.20 | 6.34 | 0.77 | 286.02 | 7.864 | 0.77 | 0.00 | 0.00 |
| 12 | 157.00 | NNVV-65B-R4 | 3 | 84.70 | 12.27 | 0.74 | 503.26 | 14.220 | 0.74 | 0.00 | 0.00 |
| 13 | 157.00 | ALU - 1900 MHz - RRU | 3 | 60.00 | 2.77 | 0.75 | 171.76 | 4.469 | 0.75 | 0.00 | 0.00 |
| 14 | 157.00 | ALU - 800 MHz - RRU | 6 | 53.00 | 2.49 | 0.75 | 152.06 | 4.022 | 0.75 | 0.00 | 0.00 |
| 15 | 157.00 | ALU - TD-RRH8x20-25 - RRU | 3 | 70.00 | 4.05 | 0.75 | 228.65 | 5.168 | 0.75 | 0.00 | 0.00 |
| 16 | 140.00 | APXV18-206516S-C-A20 | 3 | 18.70 | 3.61 | 0.73 | 111.49 | 6.069 | 0.73 | 0.00 | 0.00 |
| 17 | 140.00 | LNX-6515DS-VTM | 3 | 50.30 | 11.47 | 0.80 | 357.78 | 15.775 | 0.80 | 0.00 | 0.00 |
| 18 | 140.00 | KRY 112 144/1 | 3 | 11.00 | 0.41 | 0.73 | 25.28 | 1.039 | 0.73 | 0.00 | 0.00 |
| 19 | 140.00 | 782 11056 | 3 | 1.80 | 0.13 | 0.78 | 5.08 | 0.517 | 0.78 | 0.00 | 0.00 |
| 20 | 140.00 | Platform w/ Hand Rails (flat) | 1 | 2000.00 | 40.00 | 1.00 | 4773.15 | 67.731 | 1.00 | 0.00 | 0.00 |
| 21 | 75.00 | GPS | 1 | 10.00 | 1.00 | 1.00 | 46.47 | 1.886 | 1.00 | 0.00 | 0.00 |
| Totals: | | | 57 | 7,774.80 | | | 22,285.70 | | | | |

Linear Appurtenances

| Bottom Elev. (ft) | Top Elev. (ft) | Description | Exposed Width | Exposed |
|-------------------------|----------------------|-------------------|------------------|---------|
| 0.00 | 175.00 | (12) 1 5/8" Coax | 0.00 | Inside |
| 0.00 | 175.00 | (1) 1 5/8" Hybrid | 0.00 | Inside |
| 0.00 | 157.00 | (4) 1 1/4" Fiber | 0.00 | Inside |
| 0.00 | 140.00 | (12) 1 5/8" Coax | 0.00 | Inside |
| 0.00 | 75.00 | (1) 1/2" Coax | 0.00 | Inside |

Shaft Section Properties

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Increment Length: 5 (ft)

| Elev (ft) | Description | Thick (in) | Dia (in) | Area (in^2) | Ix (in^4) | W/t Ratio | D/t Ratio | Fpy (ksi) | S (in^3) | Weight (lb) |
|--------------|-----------------|---------------|-------------|----------------|--------------|--------------|--------------|--------------|-------------|----------------|
| 0.00 | | 0.5000 | 57.030 | 89.710 | 36220.2 | 18.70 | 114.06 | 79.4 | 1250. | 0.0 |
| 5.00 | | 0.5000 | 55.880 | 87.885 | 34054.4 | 18.30 | 111.76 | 79.9 | 1200. | 1510.8 |
| 10.00 | | 0.5000 | 54.730 | 86.060 | 31976.7 | 17.89 | 109.46 | 80.4 | 1150. | 1479.7 |
| 15.00 | | 0.5000 | 53.580 | 84.235 | 29985.2 | 17.48 | 107.16 | 80.8 | 1102. | 1448.7 |
| 20.00 | | 0.5000 | 52.430 | 82.410 | 28078.2 | 17.08 | 104.86 | 81.3 | 1054. | 1417.6 |
| 25.00 | | 0.5000 | 51.280 | 80.585 | 26253.8 | 16.67 | 102.56 | 81.8 | 1008. | 1386.6 |
| 30.00 | | 0.5000 | 50.130 | 78.760 | 24510.2 | 16.27 | 100.26 | 82.3 | 963.0 | 1355.5 |
| 35.00 | | 0.5000 | 48.980 | 76.935 | 22845.6 | 15.86 | 97.96 | 82.5 | 918.7 | 1324.5 |
| 38.75 | Bot - Section 2 | 0.5000 | 48.117 | 75.566 | 21647.8 | 15.56 | 96.23 | 82.5 | 886.1 | 973.0 |
| 40.00 | | 0.5000 | 47.830 | 75.110 | 21258.1 | 15.46 | 95.66 | 82.5 | 875.4 | 606.4 |
| 45.00 | Top - Section 1 | 0.4375 | 47.555 | 65.426 | 18351.4 | 17.76 | 108.70 | 0.0 | 0.0 | 2389.1 |
| 50.00 | | 0.4375 | 46.405 | 63.829 | 17040.2 | 17.29 | 106.07 | 81.1 | 723.3 | 1099.6 |
| 55.00 | | 0.4375 | 45.255 | 62.232 | 15793.0 | 16.83 | 103.44 | 81.6 | 687.4 | 1072.4 |
| 60.00 | | 0.4375 | 44.105 | 60.636 | 14608.2 | 16.37 | 100.81 | 82.2 | 652.4 | 1045.2 |
| 65.00 | | 0.4375 | 42.955 | 59.039 | 13484.2 | 15.90 | 98.18 | 82.5 | 618.3 | 1018.1 |
| 70.00 | | 0.4375 | 41.805 | 57.442 | 12419.4 | 15.44 | 95.55 | 82.5 | 585.1 | 990.9 |
| 75.00 | | 0.4375 | 40.655 | 55.845 | 11412.2 | 14.97 | 92.93 | 82.5 | 552.9 | 963.7 |
| 78.75 | Bot - Section 3 | 0.4375 | 39.792 | 54.647 | 10693.6 | 14.63 | 90.95 | 82.5 | 529.3 | 705.0 |
| 80.00 | | 0.4375 | 39.505 | 54.248 | 10460.9 | 14.51 | 90.30 | 82.5 | 521.6 | 400.2 |
| 83.75 | Top - Section 2 | 0.3125 | 39.267 | 38.637 | 7407.7 | 20.75 | 125.66 | 0.0 | 0.0 | 1183.1 |
| 85.00 | | 0.3125 | 38.980 | 38.352 | 7244.9 | 20.58 | 124.74 | 77.2 | 366.1 | 163.7 |
| 90.00 | | 0.3125 | 37.830 | 37.211 | 6617.5 | 19.93 | 121.06 | 78.0 | 344.5 | 642.8 |
| 95.00 | | 0.3125 | 36.680 | 36.071 | 6027.5 | 19.29 | 117.38 | 78.7 | 323.7 | 623.4 |
| 100.00 | | 0.3125 | 35.530 | 34.930 | 5473.6 | 18.64 | 113.70 | 79.5 | 303.4 | 604.0 |
| 105.00 | | 0.3125 | 34.380 | 33.789 | 4954.7 | 17.99 | 110.02 | 80.2 | 283.9 | 584.6 |
| 110.00 | | 0.3125 | 33.230 | 32.649 | 4469.7 | 17.34 | 106.34 | 81.0 | 264.9 | 565.2 |
| 115.00 | | 0.3125 | 32.080 | 31.508 | 4017.4 | 16.69 | 102.66 | 81.8 | 246.7 | 545.8 |
| 119.00 | Bot - Section 4 | 0.3125 | 31.160 | 30.596 | 3678.4 | 16.17 | 99.71 | 82.4 | 232.5 | 422.7 |
| 120.00 | | 0.3125 | 30.930 | 30.368 | 3596.7 | 16.04 | 98.98 | 82.5 | 229.0 | 188.2 |
| 123.00 | Top - Section 3 | 0.2500 | 30.740 | 24.193 | 2841.6 | 20.27 | 122.96 | 0.0 | 0.0 | 556.3 |
| 125.00 | | 0.2500 | 30.280 | 23.828 | 2714.9 | 19.95 | 121.12 | 72.8 | 176.6 | 163.4 |
| 130.00 | | 0.2500 | 29.130 | 22.915 | 2414.8 | 19.14 | 116.52 | 73.6 | 163.3 | 397.6 |
| 135.00 | | 0.2500 | 27.980 | 22.003 | 2137.6 | 18.32 | 111.92 | 74.5 | 150.5 | 382.1 |
| 140.00 | | 0.2500 | 26.830 | 21.090 | 1882.6 | 17.51 | 107.32 | 75.3 | 138.2 | 366.6 |
| 145.00 | | 0.2500 | 25.680 | 20.178 | 1648.6 | 16.70 | 102.72 | 76.2 | 126.4 | 351.1 |
| 150.00 | | 0.2500 | 24.530 | 19.265 | 1434.9 | 15.89 | 98.12 | 76.2 | 115.2 | 335.5 |
| 155.00 | | 0.2500 | 23.380 | 18.353 | 1240.5 | 15.08 | 93.52 | 76.2 | 104.5 | 320.0 |
| 157.00 | | 0.2500 | 22.920 | 17.988 | 1168.0 | 14.76 | 91.68 | 76.2 | 100.4 | 123.7 |
| 160.00 | | 0.2500 | 22.230 | 17.441 | 1064.6 | 14.27 | 88.92 | 76.2 | 94.3 | 180.8 |
| 161.00 | Top - Section 4 | 0.2500 | 22.000 | 17.258 | 1031.5 | 14.11 | 88.00 | 76.2 | 92.3 | 59.0 |
| 161.00 | Bot - Section 5 | 0.1875 | 22.000 | 12.981 | 780.3 | 18.81 | 117.33 | 73.5 | 69.9 | |
| 165.00 | | 0.1875 | 21.080 | 12.433 | 685.7 | 18.41 | 112.43 | 74.4 | 64.1 | 173.0 |
| 170.00 | | 0.1875 | 19.930 | 11.749 | 578.6 | 17.33 | 106.29 | 75.5 | 57.2 | 205.7 |
| 175.00 | | 0.1875 | 18.780 | 11.064 | 483.2 | 16.25 | 100.16 | 76.2 | 50.7 | 194.1 |

30519.4

Wind Loading - Shaft

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1 **Topography:** 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.6W 101 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.60



Iterations

25

| Elev (ft) | Description | Kzt | Kz | qz (psf) | qzGh (psf) | C (mph-ft) | Cf | Ice Thick (in) | Tributary (ft) | Aa (sf) | CfAa (sf) | Wind Force X (lb) | Dead Load Ice (lb) | Tot Dead Load (lb) |
|------------------------|-------------|------|------|----------|------------|------------|-------|----------------|----------------|---------|-----------|-------------------|--------------------|--------------------|
| 0.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 407.79 | 0.650 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 5.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 399.57 | 0.650 | 0.000 | 5.00 | 23.886 | 15.53 | 474.5 | 0.0 | 1812.9 |
| 10.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 391.35 | 0.650 | 0.000 | 5.00 | 23.399 | 15.21 | 464.9 | 0.0 | 1775.7 |
| 15.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 383.12 | 0.650 | 0.000 | 5.00 | 22.913 | 14.89 | 455.2 | 0.0 | 1738.4 |
| 20.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 374.90 | 0.650 | 0.000 | 5.00 | 22.426 | 14.58 | 445.5 | 0.0 | 1701.2 |
| 25.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 366.68 | 0.650 | 0.000 | 5.00 | 21.940 | 14.26 | 435.9 | 0.0 | 1663.9 |
| 30.00 | | 1.00 | 0.70 | 17.381 | 19.12 | 358.61 | 0.650 | 0.000 | 5.00 | 21.453 | 13.94 | 426.6 | 0.0 | 1626.6 |
| 35.00 | | 1.00 | 0.73 | 18.163 | 19.98 | 358.18 | 0.650 | 0.000 | 5.00 | 20.966 | 13.63 | 435.7 | 0.0 | 1589.4 |
| 38.75 Bot - Section 2 | | 1.00 | 0.75 | 18.699 | 20.57 | 357.03 | 0.650 | 0.000 | 3.75 | 15.406 | 10.01 | 329.6 | 0.0 | 1167.6 |
| 40.00 | | 1.00 | 0.76 | 18.870 | 20.76 | 356.51 | 0.650 | 0.000 | 1.25 | 5.167 | 3.36 | 111.5 | 0.0 | 727.7 |
| 45.00 Top - Section 1 | | 1.00 | 0.79 | 19.516 | 21.47 | 353.84 | 0.650 | 0.000 | 5.00 | 20.364 | 13.24 | 454.6 | 0.0 | 2867.0 |
| 50.00 | | 1.00 | 0.81 | 20.112 | 22.12 | 357.09 | 0.650 | 0.000 | 5.00 | 19.877 | 12.92 | 457.3 | 0.0 | 1319.5 |
| 55.00 | | 1.00 | 0.83 | 20.667 | 22.73 | 353.02 | 0.650 | 0.000 | 5.00 | 19.390 | 12.60 | 458.5 | 0.0 | 1286.9 |
| 60.00 | | 1.00 | 0.85 | 21.187 | 23.31 | 348.35 | 0.650 | 0.000 | 5.00 | 18.904 | 12.29 | 458.2 | 0.0 | 1254.3 |
| 65.00 | | 1.00 | 0.87 | 21.678 | 23.85 | 343.17 | 0.650 | 0.000 | 5.00 | 18.417 | 11.97 | 456.7 | 0.0 | 1221.7 |
| 70.00 | | 1.00 | 0.89 | 22.142 | 24.36 | 337.53 | 0.650 | 0.000 | 5.00 | 17.931 | 11.65 | 454.2 | 0.0 | 1189.1 |
| 75.00 Appurtenance(s) | | 1.00 | 0.91 | 22.582 | 24.84 | 331.50 | 0.650 | 0.000 | 5.00 | 17.444 | 11.34 | 450.7 | 0.0 | 1156.5 |
| 78.75 Bot - Section 3 | | 1.00 | 0.92 | 22.899 | 25.19 | 326.74 | 0.650 | 0.000 | 3.75 | 12.764 | 8.30 | 334.4 | 0.0 | 846.0 |
| 80.00 | | 1.00 | 0.93 | 23.003 | 25.30 | 325.11 | 0.650 | 0.000 | 1.25 | 4.260 | 2.77 | 112.1 | 0.0 | 480.2 |
| 83.75 Top - Section 2 | | 1.00 | 0.94 | 23.306 | 25.64 | 320.10 | 0.650 | 0.000 | 3.75 | 12.597 | 8.19 | 335.9 | 0.0 | 1419.7 |
| 85.00 | | 1.00 | 0.94 | 23.404 | 25.74 | 323.58 | 0.650 | 0.000 | 1.25 | 4.138 | 2.69 | 110.8 | 0.0 | 196.5 |
| 90.00 | | 1.00 | 0.96 | 23.790 | 26.17 | 316.60 | 0.650 | 0.000 | 5.00 | 16.249 | 10.56 | 442.2 | 0.0 | 771.4 |
| 95.00 | | 1.00 | 0.97 | 24.160 | 26.58 | 309.36 | 0.650 | 0.000 | 5.00 | 15.762 | 10.25 | 435.7 | 0.0 | 748.1 |
| 100.00 | | 1.00 | 0.99 | 24.517 | 26.97 | 301.87 | 0.650 | 0.000 | 5.00 | 15.276 | 9.93 | 428.4 | 0.0 | 724.8 |
| 105.00 | | 1.00 | 1.00 | 24.861 | 27.35 | 294.14 | 0.650 | 0.000 | 5.00 | 14.789 | 9.61 | 420.6 | 0.0 | 701.5 |
| 110.00 | | 1.00 | 1.02 | 25.194 | 27.71 | 286.19 | 0.650 | 0.000 | 5.00 | 14.303 | 9.30 | 412.2 | 0.0 | 678.2 |
| 115.00 | | 1.00 | 1.03 | 25.516 | 28.07 | 278.05 | 0.650 | 0.000 | 5.00 | 13.816 | 8.98 | 403.3 | 0.0 | 654.9 |
| 119.00 Bot - Section 4 | | 1.00 | 1.04 | 25.766 | 28.34 | 271.40 | 0.650 | 0.000 | 4.00 | 10.703 | 6.96 | 315.5 | 0.0 | 507.2 |
| 120.00 | | 1.00 | 1.04 | 25.828 | 28.41 | 269.72 | 0.650 | 0.000 | 1.00 | 2.669 | 1.74 | 78.9 | 0.0 | 225.9 |
| 123.00 Top - Section 3 | | 1.00 | 1.05 | 26.011 | 28.61 | 264.63 | 0.650 | 0.000 | 3.00 | 7.891 | 5.13 | 234.8 | 0.0 | 667.5 |
| 125.00 | | 1.00 | 1.05 | 26.131 | 28.74 | 265.59 | 0.650 | 0.000 | 2.00 | 5.163 | 3.36 | 154.4 | 0.0 | 196.1 |
| 130.00 | | 1.00 | 1.07 | 26.425 | 29.07 | 256.94 | 0.650 | 0.000 | 5.00 | 12.568 | 8.17 | 379.9 | 0.0 | 477.2 |
| 135.00 | | 1.00 | 1.08 | 26.712 | 29.38 | 248.13 | 0.650 | 0.000 | 5.00 | 12.081 | 7.85 | 369.2 | 0.0 | 458.5 |
| 140.00 Appurtenance(s) | | 1.00 | 1.09 | 26.991 | 29.69 | 239.17 | 0.650 | 0.000 | 5.00 | 11.595 | 7.54 | 358.0 | 0.0 | 439.9 |
| 145.00 | | 1.00 | 1.10 | 27.263 | 29.99 | 230.07 | 0.650 | 0.000 | 5.00 | 11.108 | 7.22 | 346.5 | 0.0 | 421.3 |
| 150.00 | | 1.00 | 1.11 | 27.528 | 30.28 | 220.84 | 0.650 | 0.000 | 5.00 | 10.622 | 6.90 | 334.5 | 0.0 | 402.7 |
| 155.00 | | 1.00 | 1.12 | 27.787 | 30.57 | 211.47 | 0.650 | 0.000 | 5.00 | 10.135 | 6.59 | 322.2 | 0.0 | 384.0 |
| 157.00 Appurtenance(s) | | 1.00 | 1.12 | 27.889 | 30.68 | 207.69 | 0.650 | 0.000 | 2.00 | 3.918 | 2.55 | 125.0 | 0.0 | 148.4 |
| 160.00 | | 1.00 | 1.13 | 28.040 | 30.84 | 201.98 | 0.650 | 0.000 | 3.00 | 5.731 | 3.73 | 183.8 | 0.0 | 217.0 |
| 161.00 Top - Section 4 | | 1.00 | 1.13 | 28.090 | 30.90 | 200.07 | 0.650 | 0.000 | 1.00 | 1.871 | 1.22 | 60.1 | 0.0 | 70.8 |
| 165.00 | | 1.00 | 1.14 | 28.288 | 31.12 | 192.38 | 0.650 | 0.000 | 4.00 | 7.291 | 4.74 | 235.9 | 0.0 | 207.5 |
| 170.00 | | 1.00 | 1.15 | 28.530 | 31.38 | 182.66 | 0.650 | 0.000 | 5.00 | 8.676 | 5.64 | 283.2 | 0.0 | 246.9 |
| 175.00 Appurtenance(s) | | 1.00 | 1.16 | 28.768 | 31.64 | 172.84 | 0.650 | 0.000 | 5.00 | 8.189 | 5.32 | 269.5 | 0.0 | 232.9 |

Totals: 175.00 14,256.5 36,623.3

Discrete Appurtenance Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.6W 101 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.60



| No. | Elev (ft) | Description | Qty | qz (psf) | qzGh (psf) | CaAa x Ka | Ka | Total CaAa (sf) | Dead Load (lb) | Horiz Ecc (ft) | Vert Ecc (ft) | Wind FX (lb) | Mom Y (lb-ft) | Mom Z (lb-ft) |
|-----|-----------|---------------------------|-----|----------|------------|-----------|------|-----------------|----------------|----------------|---------------|--------------|---------------|---------------|
| 1 | 175.00 | Low Profile Platform-flat | 1 | 28.768 | 31.644 | 1.00 | 1.00 | 25.00 | 1440.00 | 0.000 | 0.000 | 1265.78 | 0.00 | 0.00 |
| 2 | 175.00 | DB-T1-6Z-8AB-0Z | 1 | 28.768 | 31.644 | 0.71 | 1.00 | 3.41 | 22.68 | 0.000 | 0.000 | 172.55 | 0.00 | 0.00 |
| 3 | 175.00 | FD9R6004/2C-3L (3.1 lbs) | 6 | 28.768 | 31.644 | 0.67 | 1.00 | 1.45 | 22.32 | 0.000 | 0.000 | 73.27 | 0.00 | 0.00 |
| 4 | 175.00 | RRH2x40-AWS | 3 | 28.768 | 31.644 | 0.82 | 1.00 | 6.20 | 158.40 | 0.000 | 0.000 | 313.87 | 0.00 | 0.00 |
| 5 | 175.00 | BXA-70080/6CF | 3 | 28.768 | 31.644 | 0.88 | 1.00 | 15.42 | 64.80 | 0.000 | 0.000 | 780.61 | 0.00 | 0.00 |
| 6 | 175.00 | WBX065X19R050 | 3 | 28.768 | 31.644 | 0.72 | 1.00 | 11.28 | 75.24 | 0.000 | 0.000 | 570.88 | 0.00 | 0.00 |
| 7 | 175.00 | BXA-171085/12CF | 3 | 28.768 | 31.644 | 0.84 | 1.00 | 12.05 | 54.00 | 0.000 | 0.000 | 609.88 | 0.00 | 0.00 |
| 8 | 175.00 | BXA-70063/6CF | 3 | 28.768 | 31.644 | 0.70 | 1.00 | 15.90 | 61.20 | 0.000 | 0.000 | 804.88 | 0.00 | 0.00 |
| 9 | 175.00 | 6' Lightning rod | 1 | 28.768 | 31.644 | 1.00 | 1.00 | 0.38 | 7.80 | 0.000 | 0.000 | 19.24 | 0.00 | 0.00 |
| 10 | 157.00 | ALU - TD-RRH8x20-25 - | 3 | 27.889 | 30.678 | 0.60 | 0.80 | 7.29 | 252.00 | 0.000 | 0.000 | 357.83 | 0.00 | 0.00 |
| 11 | 157.00 | ALU - 800 MHz - RRU | 6 | 27.889 | 30.678 | 0.60 | 0.80 | 8.96 | 381.60 | 0.000 | 0.000 | 440.00 | 0.00 | 0.00 |
| 12 | 157.00 | ALU - 1900 MHz - RRU | 3 | 27.889 | 30.678 | 0.60 | 0.80 | 4.99 | 216.00 | 0.000 | 0.000 | 244.74 | 0.00 | 0.00 |
| 13 | 157.00 | NNVV-65B-R4 | 3 | 27.889 | 30.678 | 0.59 | 0.80 | 21.79 | 304.92 | 0.000 | 0.000 | 1069.64 | 0.00 | 0.00 |
| 14 | 157.00 | APXVTM14-C-I20 | 3 | 27.889 | 30.678 | 0.62 | 0.80 | 11.72 | 202.32 | 0.000 | 0.000 | 575.10 | 0.00 | 0.00 |
| 15 | 157.00 | Platform w/ Handrail + | 1 | 27.889 | 30.678 | 1.00 | 1.00 | 54.00 | 3360.00 | 0.000 | 0.000 | 2650.59 | 0.00 | 0.00 |
| 16 | 140.00 | Platform w/ Hand Rails | 1 | 26.991 | 29.690 | 1.00 | 1.00 | 40.00 | 2400.00 | 0.000 | 0.000 | 1900.15 | 0.00 | 0.00 |
| 17 | 140.00 | 782 11056 | 3 | 26.991 | 29.690 | 0.62 | 0.80 | 0.24 | 6.48 | 0.000 | 0.000 | 11.56 | 0.00 | 0.00 |
| 18 | 140.00 | KRY 112 144/1 | 3 | 26.991 | 29.690 | 0.58 | 0.80 | 0.72 | 39.60 | 0.000 | 0.000 | 34.12 | 0.00 | 0.00 |
| 19 | 140.00 | LNX-6515DS-VTM | 3 | 26.991 | 29.690 | 0.64 | 0.80 | 22.02 | 181.08 | 0.000 | 0.000 | 1046.15 | 0.00 | 0.00 |
| 20 | 140.00 | APXV18-206516S-C-A20 | 3 | 26.991 | 29.690 | 0.58 | 0.80 | 6.32 | 67.32 | 0.000 | 0.000 | 300.45 | 0.00 | 0.00 |
| 21 | 75.00 | GPS | 1 | 22.582 | 24.841 | 1.00 | 1.00 | 1.00 | 12.00 | 0.000 | 0.000 | 39.74 | 0.00 | 0.00 |

Totals: 9,329.76 13,281.03

Total Applied Force Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.6W 101 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.60



| Elev (ft) | Description | Lateral FX (-) (lb) | Axial FY (-) (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
|-----------|------------------|---------------------|-------------------|--------------------|-------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | | 474.54 | 1986.11 | 0.00 | 0.00 |
| 10.00 | | 464.87 | 1948.85 | 0.00 | 0.00 |
| 15.00 | | 455.20 | 1911.59 | 0.00 | 0.00 |
| 20.00 | | 445.54 | 1874.33 | 0.00 | 0.00 |
| 25.00 | | 435.87 | 1837.07 | 0.00 | 0.00 |
| 30.00 | | 426.56 | 1799.81 | 0.00 | 0.00 |
| 35.00 | | 435.66 | 1762.55 | 0.00 | 0.00 |
| 38.75 | | 329.56 | 1297.46 | 0.00 | 0.00 |
| 40.00 | | 111.54 | 770.94 | 0.00 | 0.00 |
| 45.00 | | 454.63 | 3040.11 | 0.00 | 0.00 |
| 50.00 | | 457.33 | 1492.64 | 0.00 | 0.00 |
| 55.00 | | 458.45 | 1460.04 | 0.00 | 0.00 |
| 60.00 | | 458.20 | 1427.44 | 0.00 | 0.00 |
| 65.00 | | 456.73 | 1394.84 | 0.00 | 0.00 |
| 70.00 | | 454.18 | 1362.23 | 0.00 | 0.00 |
| 75.00 | (1) attachments | 490.40 | 1341.63 | 0.00 | 0.00 |
| 78.75 | | 334.37 | 975.11 | 0.00 | 0.00 |
| 80.00 | | 112.10 | 523.26 | 0.00 | 0.00 |
| 83.75 | | 335.86 | 1548.84 | 0.00 | 0.00 |
| 85.00 | | 110.80 | 239.53 | 0.00 | 0.00 |
| 90.00 | | 442.22 | 943.58 | 0.00 | 0.00 |
| 95.00 | | 435.66 | 920.29 | 0.00 | 0.00 |
| 100.00 | | 428.45 | 897.00 | 0.00 | 0.00 |
| 105.00 | | 420.62 | 873.71 | 0.00 | 0.00 |
| 110.00 | | 412.23 | 850.42 | 0.00 | 0.00 |
| 115.00 | | 403.29 | 827.14 | 0.00 | 0.00 |
| 119.00 | | 315.47 | 644.94 | 0.00 | 0.00 |
| 120.00 | | 78.87 | 260.30 | 0.00 | 0.00 |
| 123.00 | | 234.81 | 770.85 | 0.00 | 0.00 |
| 125.00 | | 154.35 | 264.97 | 0.00 | 0.00 |
| 130.00 | | 379.94 | 649.37 | 0.00 | 0.00 |
| 135.00 | | 369.19 | 630.74 | 0.00 | 0.00 |
| 140.00 | (13) attachments | 3650.45 | 3306.59 | 0.00 | 0.00 |
| 145.00 | | 346.45 | 518.60 | 0.00 | 0.00 |
| 150.00 | | 334.50 | 499.97 | 0.00 | 0.00 |
| 155.00 | | 322.18 | 481.34 | 0.00 | 0.00 |
| 157.00 | (19) attachments | 5462.89 | 4904.16 | 0.00 | 0.00 |
| 160.00 | | 183.83 | 265.89 | 0.00 | 0.00 |
| 161.00 | | 60.14 | 87.14 | 0.00 | 0.00 |
| 165.00 | | 235.94 | 272.73 | 0.00 | 0.00 |
| 170.00 | | 283.16 | 328.34 | 0.00 | 0.00 |
| 175.00 | (24) attachments | 4880.46 | 2220.81 | 0.00 | 0.00 |
| | Totals: | 27,537.54 | 51,413.24 | 0.00 | 0.00 |

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

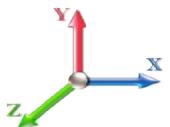
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Load Case: 1.2D + 1.6W 101 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.60



Iterations

25

| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -51.38 | -27.60 | 0.00 | -3439.1 | 0.00 | 3439.14 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.000 | 0.000 | 0.470 |
| 5.00 | -49.33 | -27.24 | 0.00 | -3301.1 | 0.00 | 3301.15 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.07 | -0.132 | 0.000 | 0.467 |
| 10.00 | -47.32 | -26.88 | 0.00 | -3164.9 | 0.00 | 3164.98 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.28 | -0.267 | 0.000 | 0.464 |
| 15.00 | -45.35 | -26.52 | 0.00 | -3030.6 | 0.00 | 3030.60 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.64 | -0.405 | 0.000 | 0.461 |
| 20.00 | -43.41 | -26.17 | 0.00 | -2898.0 | 0.00 | 2898.00 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 1.14 | -0.546 | 0.000 | 0.458 |
| 25.00 | -41.51 | -25.82 | 0.00 | -2767.1 | 0.00 | 2767.17 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 1.78 | -0.689 | 0.000 | 0.454 |
| 30.00 | -39.65 | -25.47 | 0.00 | -2638.0 | 0.00 | 2638.09 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 2.59 | -0.836 | 0.000 | 0.451 |
| 35.00 | -37.84 | -25.09 | 0.00 | -2510.7 | 0.00 | 2510.75 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 3.54 | -0.985 | 0.000 | 0.448 |
| 38.75 | -36.52 | -24.79 | 0.00 | -2416.6 | 0.00 | 2416.65 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 4.36 | -1.100 | 0.000 | 0.447 |
| 40.00 | -35.71 | -24.72 | 0.00 | -2385.6 | 0.00 | 2385.67 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 4.65 | -1.140 | 0.000 | 0.447 |
| 45.00 | -32.61 | -24.29 | 0.00 | -2262.0 | 0.00 | 2262.06 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 5.93 | -1.295 | 0.000 | 0.500 |
| 50.00 | -31.06 | -23.89 | 0.00 | -2140.5 | 0.00 | 2140.59 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 7.37 | -1.454 | 0.000 | 0.494 |
| 55.00 | -29.54 | -23.48 | 0.00 | -2021.1 | 0.00 | 2021.15 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 8.99 | -1.628 | 0.000 | 0.487 |
| 60.00 | -28.06 | -23.07 | 0.00 | -1903.7 | 0.00 | 1903.73 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 10.79 | -1.804 | 0.000 | 0.480 |
| 65.00 | -26.61 | -22.65 | 0.00 | -1788.3 | 0.00 | 1788.39 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 12.77 | -1.984 | 0.000 | 0.473 |
| 70.00 | -25.19 | -22.23 | 0.00 | -1675.1 | 0.00 | 1675.13 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 14.95 | -2.167 | 0.000 | 0.468 |
| 75.00 | -23.81 | -21.75 | 0.00 | -1563.9 | 0.00 | 1563.99 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 17.32 | -2.352 | 0.000 | 0.463 |
| 78.75 | -22.81 | -21.42 | 0.00 | -1482.4 | 0.00 | 1482.41 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 19.22 | -2.495 | 0.000 | 0.458 |
| 80.00 | -22.26 | -21.32 | 0.00 | -1455.6 | 0.00 | 1455.64 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 19.88 | -2.543 | 0.000 | 0.456 |
| 83.75 | -20.69 | -20.95 | 0.00 | -1375.6 | 0.00 | 1375.69 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 21.94 | -2.688 | 0.000 | 0.649 |
| 85.00 | -20.40 | -20.88 | 0.00 | -1349.5 | 0.00 | 1349.51 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 22.65 | -2.737 | 0.000 | 0.645 |
| 90.00 | -19.39 | -20.48 | 0.00 | -1245.1 | 0.00 | 1245.11 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 25.65 | -2.992 | 0.000 | 0.626 |
| 95.00 | -18.40 | -20.08 | 0.00 | -1142.7 | 0.00 | 1142.71 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 28.92 | -3.249 | 0.000 | 0.605 |
| 100.00 | -17.44 | -19.68 | 0.00 | -1042.3 | 0.00 | 1042.33 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 32.46 | -3.507 | 0.000 | 0.584 |
| 105.00 | -16.51 | -19.27 | 0.00 | -943.96 | 0.00 | 943.96 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 36.27 | -3.765 | 0.000 | 0.560 |
| 110.00 | -15.61 | -18.88 | 0.00 | -847.59 | 0.00 | 847.59 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 40.35 | -4.022 | 0.000 | 0.533 |
| 115.00 | -14.74 | -18.47 | 0.00 | -753.21 | 0.00 | 753.21 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 44.69 | -4.277 | 0.000 | 0.505 |
| 119.00 | -14.08 | -18.14 | 0.00 | -679.33 | 0.00 | 679.33 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 48.36 | -4.480 | 0.000 | 0.479 |
| 120.00 | -13.79 | -18.06 | 0.00 | -661.19 | 0.00 | 661.19 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 49.30 | -4.531 | 0.000 | 0.473 |
| 123.00 | -13.01 | -17.80 | 0.00 | -606.99 | 0.00 | 606.99 | 1577.63 | 788.82 | 1975.86 | 989.40 | 52.20 | -4.682 | 0.000 | 0.622 |
| 125.00 | -12.70 | -17.66 | 0.00 | -571.40 | 0.00 | 571.40 | 1561.09 | 780.55 | 1925.40 | 964.13 | 54.18 | -4.782 | 0.000 | 0.601 |
| 130.00 | -12.00 | -17.29 | 0.00 | -483.08 | 0.00 | 483.08 | 1518.76 | 759.38 | 1800.86 | 901.77 | 59.33 | -5.058 | 0.000 | 0.544 |
| 135.00 | -11.33 | -16.91 | 0.00 | -396.65 | 0.00 | 396.65 | 1475.03 | 737.52 | 1678.77 | 840.64 | 64.76 | -5.317 | 0.000 | 0.480 |
| 140.00 | -8.34 | -13.00 | 0.00 | -312.10 | 0.00 | 312.10 | 1429.92 | 714.96 | 1559.34 | 780.83 | 70.45 | -5.553 | 0.000 | 0.406 |
| 145.00 | -7.81 | -12.63 | 0.00 | -247.13 | 0.00 | 247.13 | 1383.42 | 691.71 | 1442.75 | 722.45 | 76.38 | -5.764 | 0.000 | 0.348 |
| 150.00 | -7.31 | -12.26 | 0.00 | -183.99 | 0.00 | 183.99 | 1321.23 | 660.61 | 1314.97 | 658.46 | 82.51 | -5.950 | 0.000 | 0.285 |
| 155.00 | -6.85 | -11.91 | 0.00 | -122.67 | 0.00 | 122.67 | 1258.65 | 629.32 | 1192.75 | 597.26 | 88.81 | -6.102 | 0.000 | 0.211 |
| 157.00 | -2.55 | -5.95 | 0.00 | -98.86 | 0.00 | 98.86 | 1233.62 | 616.81 | 1145.53 | 573.62 | 91.38 | -6.153 | 0.000 | 0.175 |
| 160.00 | -2.30 | -5.74 | 0.00 | -81.00 | 0.00 | 81.00 | 1196.07 | 598.03 | 1076.49 | 539.05 | 95.26 | -6.219 | 0.000 | 0.152 |
| 161.00 | -2.21 | -5.68 | 0.00 | -75.26 | 0.00 | 75.26 | 1183.55 | 591.78 | 1053.96 | 527.76 | 96.56 | -6.240 | 0.000 | 0.145 |
| 161.00 | -2.21 | -5.68 | 0.00 | -75.26 | 0.00 | 75.26 | 858.57 | 429.28 | 768.96 | 385.05 | 96.56 | -6.240 | 0.000 | 0.198 |
| 165.00 | -1.96 | -5.41 | 0.00 | -52.56 | 0.00 | 52.56 | 832.45 | 416.23 | 713.85 | 357.46 | 101.81 | -6.310 | 0.000 | 0.150 |
| 170.00 | -1.66 | -5.10 | 0.00 | -25.49 | 0.00 | 25.49 | 798.56 | 399.28 | 646.76 | 323.86 | 108.45 | -6.391 | 0.000 | 0.081 |
| 175.00 | 0.00 | -4.88 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 115.15 | -6.422 | 0.000 | 0.000 |

Wind Loading - Shaft

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1 **Topography:** 1

Code: EIA/TIA-222-G **Exposure:** B
Crest Height: 0.00 **Site Class:** D - Stiff Soil
Struct Class: II

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Load Case: 0.9D + 1.6W 101 mph Wind

Dead Load Factor 0.90
Wind Load Factor 1.60



Iterations

25

| Elev (ft) | Description | Kzt | Kz | qz (psf) | qzGh (psf) | C (mph-ft) | Cf | Ice Thick (in) | Tributary (ft) | Aa (sf) | CfAa (sf) | Wind Force X (lb) | Dead Load Ice (lb) | Tot Dead Load (lb) |
|------------------------|-------------|------|------|----------|------------|------------|-------|----------------|----------------|---------|-----------|-------------------|--------------------|--------------------|
| 0.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 407.79 | 0.650 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 5.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 399.57 | 0.650 | 0.000 | 5.00 | 23.886 | 15.53 | 474.5 | 0.0 | 1359.7 |
| 10.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 391.35 | 0.650 | 0.000 | 5.00 | 23.399 | 15.21 | 464.9 | 0.0 | 1331.8 |
| 15.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 383.12 | 0.650 | 0.000 | 5.00 | 22.913 | 14.89 | 455.2 | 0.0 | 1303.8 |
| 20.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 374.90 | 0.650 | 0.000 | 5.00 | 22.426 | 14.58 | 445.5 | 0.0 | 1275.9 |
| 25.00 | | 1.00 | 0.70 | 17.366 | 19.10 | 366.68 | 0.650 | 0.000 | 5.00 | 21.940 | 14.26 | 435.9 | 0.0 | 1247.9 |
| 30.00 | | 1.00 | 0.70 | 17.381 | 19.12 | 358.61 | 0.650 | 0.000 | 5.00 | 21.453 | 13.94 | 426.6 | 0.0 | 1220.0 |
| 35.00 | | 1.00 | 0.73 | 18.163 | 19.98 | 358.18 | 0.650 | 0.000 | 5.00 | 20.966 | 13.63 | 435.7 | 0.0 | 1192.0 |
| 38.75 Bot - Section 2 | | 1.00 | 0.75 | 18.699 | 20.57 | 357.03 | 0.650 | 0.000 | 3.75 | 15.406 | 10.01 | 329.6 | 0.0 | 875.7 |
| 40.00 | | 1.00 | 0.76 | 18.870 | 20.76 | 356.51 | 0.650 | 0.000 | 1.25 | 5.167 | 3.36 | 111.5 | 0.0 | 545.7 |
| 45.00 Top - Section 1 | | 1.00 | 0.79 | 19.516 | 21.47 | 353.84 | 0.650 | 0.000 | 5.00 | 20.364 | 13.24 | 454.6 | 0.0 | 2150.2 |
| 50.00 | | 1.00 | 0.81 | 20.112 | 22.12 | 357.09 | 0.650 | 0.000 | 5.00 | 19.877 | 12.92 | 457.3 | 0.0 | 989.6 |
| 55.00 | | 1.00 | 0.83 | 20.667 | 22.73 | 353.02 | 0.650 | 0.000 | 5.00 | 19.390 | 12.60 | 458.5 | 0.0 | 965.2 |
| 60.00 | | 1.00 | 0.85 | 21.187 | 23.31 | 348.35 | 0.650 | 0.000 | 5.00 | 18.904 | 12.29 | 458.2 | 0.0 | 940.7 |
| 65.00 | | 1.00 | 0.87 | 21.678 | 23.85 | 343.17 | 0.650 | 0.000 | 5.00 | 18.417 | 11.97 | 456.7 | 0.0 | 916.3 |
| 70.00 | | 1.00 | 0.89 | 22.142 | 24.36 | 337.53 | 0.650 | 0.000 | 5.00 | 17.931 | 11.65 | 454.2 | 0.0 | 891.8 |
| 75.00 Appurtenance(s) | | 1.00 | 0.91 | 22.582 | 24.84 | 331.50 | 0.650 | 0.000 | 5.00 | 17.444 | 11.34 | 450.7 | 0.0 | 867.4 |
| 78.75 Bot - Section 3 | | 1.00 | 0.92 | 22.899 | 25.19 | 326.74 | 0.650 | 0.000 | 3.75 | 12.764 | 8.30 | 334.4 | 0.0 | 634.5 |
| 80.00 | | 1.00 | 0.93 | 23.003 | 25.30 | 325.11 | 0.650 | 0.000 | 1.25 | 4.260 | 2.77 | 112.1 | 0.0 | 360.2 |
| 83.75 Top - Section 2 | | 1.00 | 0.94 | 23.306 | 25.64 | 320.10 | 0.650 | 0.000 | 3.75 | 12.597 | 8.19 | 335.9 | 0.0 | 1064.8 |
| 85.00 | | 1.00 | 0.94 | 23.404 | 25.74 | 323.58 | 0.650 | 0.000 | 1.25 | 4.138 | 2.69 | 110.8 | 0.0 | 147.4 |
| 90.00 | | 1.00 | 0.96 | 23.790 | 26.17 | 316.60 | 0.650 | 0.000 | 5.00 | 16.249 | 10.56 | 442.2 | 0.0 | 578.5 |
| 95.00 | | 1.00 | 0.97 | 24.160 | 26.58 | 309.36 | 0.650 | 0.000 | 5.00 | 15.762 | 10.25 | 435.7 | 0.0 | 561.1 |
| 100.00 | | 1.00 | 0.99 | 24.517 | 26.97 | 301.87 | 0.650 | 0.000 | 5.00 | 15.276 | 9.93 | 428.4 | 0.0 | 543.6 |
| 105.00 | | 1.00 | 1.00 | 24.861 | 27.35 | 294.14 | 0.650 | 0.000 | 5.00 | 14.789 | 9.61 | 420.6 | 0.0 | 526.1 |
| 110.00 | | 1.00 | 1.02 | 25.194 | 27.71 | 286.19 | 0.650 | 0.000 | 5.00 | 14.303 | 9.30 | 412.2 | 0.0 | 508.7 |
| 115.00 | | 1.00 | 1.03 | 25.516 | 28.07 | 278.05 | 0.650 | 0.000 | 5.00 | 13.816 | 8.98 | 403.3 | 0.0 | 491.2 |
| 119.00 Bot - Section 4 | | 1.00 | 1.04 | 25.766 | 28.34 | 271.40 | 0.650 | 0.000 | 4.00 | 10.703 | 6.96 | 315.5 | 0.0 | 380.4 |
| 120.00 | | 1.00 | 1.04 | 25.828 | 28.41 | 269.72 | 0.650 | 0.000 | 1.00 | 2.669 | 1.74 | 78.9 | 0.0 | 169.4 |
| 123.00 Top - Section 3 | | 1.00 | 1.05 | 26.011 | 28.61 | 264.63 | 0.650 | 0.000 | 3.00 | 7.891 | 5.13 | 234.8 | 0.0 | 500.6 |
| 125.00 | | 1.00 | 1.05 | 26.131 | 28.74 | 265.59 | 0.650 | 0.000 | 2.00 | 5.163 | 3.36 | 154.4 | 0.0 | 147.1 |
| 130.00 | | 1.00 | 1.07 | 26.425 | 29.07 | 256.94 | 0.650 | 0.000 | 5.00 | 12.568 | 8.17 | 379.9 | 0.0 | 357.9 |
| 135.00 | | 1.00 | 1.08 | 26.712 | 29.38 | 248.13 | 0.650 | 0.000 | 5.00 | 12.081 | 7.85 | 369.2 | 0.0 | 343.9 |
| 140.00 Appurtenance(s) | | 1.00 | 1.09 | 26.991 | 29.69 | 239.17 | 0.650 | 0.000 | 5.00 | 11.595 | 7.54 | 358.0 | 0.0 | 329.9 |
| 145.00 | | 1.00 | 1.10 | 27.263 | 29.99 | 230.07 | 0.650 | 0.000 | 5.00 | 11.108 | 7.22 | 346.5 | 0.0 | 316.0 |
| 150.00 | | 1.00 | 1.11 | 27.528 | 30.28 | 220.84 | 0.650 | 0.000 | 5.00 | 10.622 | 6.90 | 334.5 | 0.0 | 302.0 |
| 155.00 | | 1.00 | 1.12 | 27.787 | 30.57 | 211.47 | 0.650 | 0.000 | 5.00 | 10.135 | 6.59 | 322.2 | 0.0 | 288.0 |
| 157.00 Appurtenance(s) | | 1.00 | 1.12 | 27.889 | 30.68 | 207.69 | 0.650 | 0.000 | 2.00 | 3.918 | 2.55 | 125.0 | 0.0 | 111.3 |
| 160.00 | | 1.00 | 1.13 | 28.040 | 30.84 | 201.98 | 0.650 | 0.000 | 3.00 | 5.731 | 3.73 | 183.8 | 0.0 | 162.7 |
| 161.00 Top - Section 4 | | 1.00 | 1.13 | 28.090 | 30.90 | 200.07 | 0.650 | 0.000 | 1.00 | 1.871 | 1.22 | 60.1 | 0.0 | 53.1 |
| 165.00 | | 1.00 | 1.14 | 28.288 | 31.12 | 192.38 | 0.650 | 0.000 | 4.00 | 7.291 | 4.74 | 235.9 | 0.0 | 155.7 |
| 170.00 | | 1.00 | 1.15 | 28.530 | 31.38 | 182.66 | 0.650 | 0.000 | 5.00 | 8.676 | 5.64 | 283.2 | 0.0 | 185.1 |
| 175.00 Appurtenance(s) | | 1.00 | 1.16 | 28.768 | 31.64 | 172.84 | 0.650 | 0.000 | 5.00 | 8.189 | 5.32 | 269.5 | 0.0 | 174.7 |

Totals: 175.00 14,256.5 27,467.4

Discrete Appurtenance Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



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Load Case: 0.9D + 1.6W 101 mph Wind

Dead Load Factor 0.90
Wind Load Factor 1.60



| No. | Elev (ft) | Description | Qty | qz (psf) | qzGh (psf) | CaAa x Ka | Ka | Total CaAa (sf) | Dead Load (lb) | Horiz Ecc (ft) | Vert Ecc (ft) | Wind FX (lb) | Mom Y (lb-ft) | Mom Z (lb-ft) |
|-----|-----------|---------------------------|-----|----------|------------|-----------|------|-----------------|----------------|----------------|---------------|--------------|---------------|---------------|
| 1 | 175.00 | Low Profile Platform-flat | 1 | 28.768 | 31.644 | 1.00 | 1.00 | 25.00 | 1080.00 | 0.000 | 0.000 | 1265.78 | 0.00 | 0.00 |
| 2 | 175.00 | DB-T1-6Z-8AB-0Z | 1 | 28.768 | 31.644 | 0.71 | 1.00 | 3.41 | 17.01 | 0.000 | 0.000 | 172.55 | 0.00 | 0.00 |
| 3 | 175.00 | FD9R6004/2C-3L (3.1 lbs) | 6 | 28.768 | 31.644 | 0.67 | 1.00 | 1.45 | 16.74 | 0.000 | 0.000 | 73.27 | 0.00 | 0.00 |
| 4 | 175.00 | RRH2x40-AWS | 3 | 28.768 | 31.644 | 0.82 | 1.00 | 6.20 | 118.80 | 0.000 | 0.000 | 313.87 | 0.00 | 0.00 |
| 5 | 175.00 | BXA-70080/6CF | 3 | 28.768 | 31.644 | 0.88 | 1.00 | 15.42 | 48.60 | 0.000 | 0.000 | 780.61 | 0.00 | 0.00 |
| 6 | 175.00 | WBX065X19R050 | 3 | 28.768 | 31.644 | 0.72 | 1.00 | 11.28 | 56.43 | 0.000 | 0.000 | 570.88 | 0.00 | 0.00 |
| 7 | 175.00 | BXA-171085/12CF | 3 | 28.768 | 31.644 | 0.84 | 1.00 | 12.05 | 40.50 | 0.000 | 0.000 | 609.88 | 0.00 | 0.00 |
| 8 | 175.00 | BXA-70063/6CF | 3 | 28.768 | 31.644 | 0.70 | 1.00 | 15.90 | 45.90 | 0.000 | 0.000 | 804.88 | 0.00 | 0.00 |
| 9 | 175.00 | 6' Lightning rod | 1 | 28.768 | 31.644 | 1.00 | 1.00 | 0.38 | 5.85 | 0.000 | 0.000 | 19.24 | 0.00 | 0.00 |
| 10 | 157.00 | ALU - TD-RRH8x20-25 - | 3 | 27.889 | 30.678 | 0.60 | 0.80 | 7.29 | 189.00 | 0.000 | 0.000 | 357.83 | 0.00 | 0.00 |
| 11 | 157.00 | ALU - 800 MHz - RRU | 6 | 27.889 | 30.678 | 0.60 | 0.80 | 8.96 | 286.20 | 0.000 | 0.000 | 440.00 | 0.00 | 0.00 |
| 12 | 157.00 | ALU - 1900 MHz - RRU | 3 | 27.889 | 30.678 | 0.60 | 0.80 | 4.99 | 162.00 | 0.000 | 0.000 | 244.74 | 0.00 | 0.00 |
| 13 | 157.00 | NNVV-65B-R4 | 3 | 27.889 | 30.678 | 0.59 | 0.80 | 21.79 | 228.69 | 0.000 | 0.000 | 1069.64 | 0.00 | 0.00 |
| 14 | 157.00 | APXVTM14-C-I20 | 3 | 27.889 | 30.678 | 0.62 | 0.80 | 11.72 | 151.74 | 0.000 | 0.000 | 575.10 | 0.00 | 0.00 |
| 15 | 157.00 | Platform w/ Handrail + | 1 | 27.889 | 30.678 | 1.00 | 1.00 | 54.00 | 2520.00 | 0.000 | 0.000 | 2650.59 | 0.00 | 0.00 |
| 16 | 140.00 | Platform w/ Hand Rails | 1 | 26.991 | 29.690 | 1.00 | 1.00 | 40.00 | 1800.00 | 0.000 | 0.000 | 1900.15 | 0.00 | 0.00 |
| 17 | 140.00 | 782 11056 | 3 | 26.991 | 29.690 | 0.62 | 0.80 | 0.24 | 4.86 | 0.000 | 0.000 | 11.56 | 0.00 | 0.00 |
| 18 | 140.00 | KRY 112 144/1 | 3 | 26.991 | 29.690 | 0.58 | 0.80 | 0.72 | 29.70 | 0.000 | 0.000 | 34.12 | 0.00 | 0.00 |
| 19 | 140.00 | LNX-6515DS-VTM | 3 | 26.991 | 29.690 | 0.64 | 0.80 | 22.02 | 135.81 | 0.000 | 0.000 | 1046.15 | 0.00 | 0.00 |
| 20 | 140.00 | APXV18-206516S-C-A20 | 3 | 26.991 | 29.690 | 0.58 | 0.80 | 6.32 | 50.49 | 0.000 | 0.000 | 300.45 | 0.00 | 0.00 |
| 21 | 75.00 | GPS | 1 | 22.582 | 24.841 | 1.00 | 1.00 | 1.00 | 9.00 | 0.000 | 0.000 | 39.74 | 0.00 | 0.00 |

Totals: 6,997.32 13,281.03

Total Applied Force Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



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Load Case: 0.9D + 1.6W 101 mph Wind

Dead Load Factor 0.90
Wind Load Factor 1.60



Iterations

25

| Elev (ft) | Description | Lateral FX (-) (lb) | Axial FY (-) (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
|-----------|------------------|---------------------|-------------------|--------------------|-------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | | 474.54 | 1489.58 | 0.00 | 0.00 |
| 10.00 | | 464.87 | 1461.63 | 0.00 | 0.00 |
| 15.00 | | 455.20 | 1433.69 | 0.00 | 0.00 |
| 20.00 | | 445.54 | 1405.74 | 0.00 | 0.00 |
| 25.00 | | 435.87 | 1377.80 | 0.00 | 0.00 |
| 30.00 | | 426.56 | 1349.85 | 0.00 | 0.00 |
| 35.00 | | 435.66 | 1321.91 | 0.00 | 0.00 |
| 38.75 | | 329.56 | 973.09 | 0.00 | 0.00 |
| 40.00 | | 111.54 | 578.21 | 0.00 | 0.00 |
| 45.00 | | 454.63 | 2280.08 | 0.00 | 0.00 |
| 50.00 | | 457.33 | 1119.48 | 0.00 | 0.00 |
| 55.00 | | 458.45 | 1095.03 | 0.00 | 0.00 |
| 60.00 | | 458.20 | 1070.58 | 0.00 | 0.00 |
| 65.00 | | 456.73 | 1046.13 | 0.00 | 0.00 |
| 70.00 | | 454.18 | 1021.67 | 0.00 | 0.00 |
| 75.00 | (1) attachments | 490.40 | 1006.22 | 0.00 | 0.00 |
| 78.75 | | 334.37 | 731.33 | 0.00 | 0.00 |
| 80.00 | | 112.10 | 392.45 | 0.00 | 0.00 |
| 83.75 | | 335.86 | 1161.63 | 0.00 | 0.00 |
| 85.00 | | 110.80 | 179.65 | 0.00 | 0.00 |
| 90.00 | | 442.22 | 707.68 | 0.00 | 0.00 |
| 95.00 | | 435.66 | 690.22 | 0.00 | 0.00 |
| 100.00 | | 428.45 | 672.75 | 0.00 | 0.00 |
| 105.00 | | 420.62 | 655.28 | 0.00 | 0.00 |
| 110.00 | | 412.23 | 637.82 | 0.00 | 0.00 |
| 115.00 | | 403.29 | 620.35 | 0.00 | 0.00 |
| 119.00 | | 315.47 | 483.71 | 0.00 | 0.00 |
| 120.00 | | 78.87 | 195.23 | 0.00 | 0.00 |
| 123.00 | | 234.81 | 578.14 | 0.00 | 0.00 |
| 125.00 | | 154.35 | 198.72 | 0.00 | 0.00 |
| 130.00 | | 379.94 | 487.03 | 0.00 | 0.00 |
| 135.00 | | 369.19 | 473.06 | 0.00 | 0.00 |
| 140.00 | (13) attachments | 3650.45 | 2479.94 | 0.00 | 0.00 |
| 145.00 | | 346.45 | 388.95 | 0.00 | 0.00 |
| 150.00 | | 334.50 | 374.98 | 0.00 | 0.00 |
| 155.00 | | 322.18 | 361.01 | 0.00 | 0.00 |
| 157.00 | (19) attachments | 5462.89 | 3678.12 | 0.00 | 0.00 |
| 160.00 | | 183.83 | 199.42 | 0.00 | 0.00 |
| 161.00 | | 60.14 | 65.35 | 0.00 | 0.00 |
| 165.00 | | 235.94 | 204.55 | 0.00 | 0.00 |
| 170.00 | | 283.16 | 246.25 | 0.00 | 0.00 |
| 175.00 | (24) attachments | 4880.46 | 1665.60 | 0.00 | 0.00 |
| | Totals: | 27,537.54 | 38,559.93 | 0.00 | 0.00 |

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

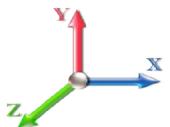
5/23/2018



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Load Case: 0.9D + 1.6W 101 mph Wind

Dead Load Factor 0.90
Wind Load Factor 1.60



Iterations 25

| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -38.53 | -27.58 | 0.00 | -3401.6 | 0.00 | 3401.64 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.000 | 0.000 | 0.463 |
| 5.00 | -36.98 | -27.19 | 0.00 | -3263.7 | 0.00 | 3263.74 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.07 | -0.131 | 0.000 | 0.460 |
| 10.00 | -35.45 | -26.80 | 0.00 | -3127.7 | 0.00 | 3127.79 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.28 | -0.264 | 0.000 | 0.457 |
| 15.00 | -33.96 | -26.42 | 0.00 | -2993.7 | 0.00 | 2993.77 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.63 | -0.401 | 0.000 | 0.454 |
| 20.00 | -32.49 | -26.04 | 0.00 | -2861.6 | 0.00 | 2861.66 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 1.12 | -0.539 | 0.000 | 0.450 |
| 25.00 | -31.06 | -25.67 | 0.00 | -2731.4 | 0.00 | 2731.43 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 1.76 | -0.681 | 0.000 | 0.447 |
| 30.00 | -29.65 | -25.30 | 0.00 | -2603.0 | 0.00 | 2603.07 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 2.55 | -0.826 | 0.000 | 0.443 |
| 35.00 | -28.28 | -24.91 | 0.00 | -2476.5 | 0.00 | 2476.56 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 3.50 | -0.973 | 0.000 | 0.440 |
| 38.75 | -27.28 | -24.60 | 0.00 | -2383.1 | 0.00 | 2383.14 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 4.31 | -1.087 | 0.000 | 0.439 |
| 40.00 | -26.66 | -24.52 | 0.00 | -2352.3 | 0.00 | 2352.39 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 4.60 | -1.125 | 0.000 | 0.439 |
| 45.00 | -24.32 | -24.09 | 0.00 | -2229.7 | 0.00 | 2229.78 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 5.86 | -1.279 | 0.000 | 0.491 |
| 50.00 | -23.15 | -23.67 | 0.00 | -2109.3 | 0.00 | 2109.35 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 7.28 | -1.435 | 0.000 | 0.485 |
| 55.00 | -22.00 | -23.25 | 0.00 | -1991.0 | 0.00 | 1991.01 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 8.88 | -1.606 | 0.000 | 0.478 |
| 60.00 | -20.87 | -22.82 | 0.00 | -1874.7 | 0.00 | 1874.77 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 10.65 | -1.780 | 0.000 | 0.471 |
| 65.00 | -19.77 | -22.39 | 0.00 | -1760.6 | 0.00 | 1760.66 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 12.61 | -1.957 | 0.000 | 0.465 |
| 70.00 | -18.69 | -21.96 | 0.00 | -1648.7 | 0.00 | 1648.70 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 14.76 | -2.137 | 0.000 | 0.460 |
| 75.00 | -17.65 | -21.48 | 0.00 | -1538.8 | 0.00 | 1538.89 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 17.09 | -2.320 | 0.000 | 0.454 |
| 78.75 | -16.90 | -21.15 | 0.00 | -1458.3 | 0.00 | 1458.33 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 18.97 | -2.460 | 0.000 | 0.449 |
| 80.00 | -16.47 | -21.04 | 0.00 | -1431.9 | 0.00 | 1431.90 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 19.62 | -2.508 | 0.000 | 0.448 |
| 83.75 | -15.29 | -20.68 | 0.00 | -1352.9 | 0.00 | 1352.98 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 21.65 | -2.650 | 0.000 | 0.636 |
| 85.00 | -15.07 | -20.60 | 0.00 | -1327.1 | 0.00 | 1327.13 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 22.35 | -2.699 | 0.000 | 0.632 |
| 90.00 | -14.29 | -20.19 | 0.00 | -1224.1 | 0.00 | 1224.12 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 25.31 | -2.949 | 0.000 | 0.613 |
| 95.00 | -13.54 | -19.78 | 0.00 | -1123.1 | 0.00 | 1123.18 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 28.53 | -3.201 | 0.000 | 0.593 |
| 100.00 | -12.81 | -19.37 | 0.00 | -1024.3 | 0.00 | 1024.30 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 32.02 | -3.455 | 0.000 | 0.572 |
| 105.00 | -12.10 | -18.96 | 0.00 | -927.46 | 0.00 | 927.46 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 35.77 | -3.708 | 0.000 | 0.548 |
| 110.00 | -11.41 | -18.56 | 0.00 | -832.67 | 0.00 | 832.67 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 39.79 | -3.961 | 0.000 | 0.522 |
| 115.00 | -10.74 | -18.15 | 0.00 | -739.89 | 0.00 | 739.89 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 44.07 | -4.211 | 0.000 | 0.494 |
| 119.00 | -10.25 | -17.82 | 0.00 | -667.28 | 0.00 | 667.28 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 47.68 | -4.411 | 0.000 | 0.469 |
| 120.00 | -10.03 | -17.75 | 0.00 | -649.46 | 0.00 | 649.46 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 48.61 | -4.461 | 0.000 | 0.463 |
| 123.00 | -9.43 | -17.49 | 0.00 | -596.22 | 0.00 | 596.22 | 1577.63 | 788.82 | 1975.86 | 989.40 | 51.46 | -4.609 | 0.000 | 0.609 |
| 125.00 | -9.19 | -17.35 | 0.00 | -561.24 | 0.00 | 561.24 | 1561.09 | 780.55 | 1925.40 | 964.13 | 53.41 | -4.707 | 0.000 | 0.589 |
| 130.00 | -8.66 | -16.97 | 0.00 | -474.51 | 0.00 | 474.51 | 1518.76 | 759.38 | 1800.86 | 901.77 | 58.48 | -4.979 | 0.000 | 0.532 |
| 135.00 | -8.15 | -16.59 | 0.00 | -389.67 | 0.00 | 389.67 | 1475.03 | 737.52 | 1678.77 | 840.64 | 63.83 | -5.233 | 0.000 | 0.470 |
| 140.00 | -5.97 | -12.75 | 0.00 | -306.71 | 0.00 | 306.71 | 1429.92 | 714.96 | 1559.34 | 780.83 | 69.43 | -5.465 | 0.000 | 0.397 |
| 145.00 | -5.58 | -12.39 | 0.00 | -242.96 | 0.00 | 242.96 | 1383.42 | 691.71 | 1442.75 | 722.45 | 75.26 | -5.673 | 0.000 | 0.341 |
| 150.00 | -5.20 | -12.03 | 0.00 | -181.03 | 0.00 | 181.03 | 1321.23 | 660.61 | 1314.97 | 658.46 | 81.29 | -5.855 | 0.000 | 0.279 |
| 155.00 | -4.86 | -11.68 | 0.00 | -120.87 | 0.00 | 120.87 | 1258.65 | 629.32 | 1192.75 | 597.26 | 87.50 | -6.005 | 0.000 | 0.207 |
| 157.00 | -1.77 | -5.86 | 0.00 | -97.51 | 0.00 | 97.51 | 1233.62 | 616.81 | 1145.53 | 573.62 | 90.02 | -6.055 | 0.000 | 0.172 |
| 160.00 | -1.59 | -5.66 | 0.00 | -79.92 | 0.00 | 79.92 | 1196.07 | 598.03 | 1076.49 | 539.05 | 93.84 | -6.120 | 0.000 | 0.150 |
| 161.00 | -1.52 | -5.60 | 0.00 | -74.26 | 0.00 | 74.26 | 1183.55 | 591.78 | 1053.96 | 527.76 | 95.12 | -6.141 | 0.000 | 0.142 |
| 161.00 | -1.52 | -5.60 | 0.00 | -74.26 | 0.00 | 74.26 | 858.57 | 429.28 | 768.96 | 385.05 | 95.12 | -6.141 | 0.000 | 0.195 |
| 165.00 | -1.34 | -5.34 | 0.00 | -51.87 | 0.00 | 51.87 | 832.45 | 416.23 | 713.85 | 357.46 | 100.29 | -6.210 | 0.000 | 0.147 |
| 170.00 | -1.12 | -5.03 | 0.00 | -25.17 | 0.00 | 25.17 | 798.56 | 399.28 | 646.76 | 323.86 | 106.83 | -6.290 | 0.000 | 0.079 |
| 175.00 | 0.00 | -4.88 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 113.42 | -6.321 | 0.000 | 0.000 |

Wind Loading - Shaft

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1 **Topography:** 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



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Load Case: 1.2D + 1.0Di + 1.0Wi 50 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.00



| Elev (ft) | Description | Kzt | Kz | qz (psf) | qzGh (psf) | C (mph-ft) | Cf | Ice Thick (in) | Tributary (ft) | Aa (sf) | CfAa (sf) | Wind Force X (lb) | Dead Load Ice (lb) | Tot Dead Load (lb) |
|------------------------|-------------|------|------|----------|------------|------------|-------|----------------|----------------|---------|-----------|-------------------|--------------------|--------------------|
| 0.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 5.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 1.656 | 5.00 | 25.266 | 30.32 | 141.9 | 596.8 | 2409.8 |
| 10.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 1.775 | 5.00 | 24.878 | 29.85 | 139.8 | 628.2 | 2403.9 |
| 15.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 1.848 | 5.00 | 24.453 | 29.34 | 137.4 | 641.7 | 2380.1 |
| 20.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 1.902 | 5.00 | 24.011 | 28.81 | 134.9 | 647.4 | 2348.5 |
| 25.00 | | 1.00 | 0.70 | 4.256 | 4.68 | 0.00 | 1.200 | 1.945 | 5.00 | 23.561 | 28.27 | 132.4 | 648.5 | 2312.4 |
| 30.00 | | 1.00 | 0.70 | 4.260 | 4.69 | 0.00 | 1.200 | 1.981 | 5.00 | 23.104 | 27.72 | 129.9 | 646.6 | 2273.2 |
| 35.00 | | 1.00 | 0.73 | 4.451 | 4.90 | 0.00 | 1.200 | 2.012 | 5.00 | 22.643 | 27.17 | 133.0 | 642.5 | 2231.9 |
| 38.75 Bot - Section 2 | | 1.00 | 0.75 | 4.583 | 5.04 | 0.00 | 1.200 | 2.032 | 3.75 | 16.676 | 20.01 | 100.9 | 478.7 | 1646.3 |
| 40.00 | | 1.00 | 0.76 | 4.625 | 5.09 | 0.00 | 1.200 | 2.039 | 1.25 | 5.592 | 6.71 | 34.1 | 162.0 | 889.6 |
| 45.00 Top - Section 1 | | 1.00 | 0.79 | 4.783 | 5.26 | 0.00 | 1.200 | 2.063 | 5.00 | 22.083 | 26.50 | 139.4 | 641.1 | 3508.0 |
| 50.00 | | 1.00 | 0.81 | 4.929 | 5.42 | 0.00 | 1.200 | 2.085 | 5.00 | 21.614 | 25.94 | 140.6 | 633.1 | 1952.6 |
| 55.00 | | 1.00 | 0.83 | 5.065 | 5.57 | 0.00 | 1.200 | 2.105 | 5.00 | 21.144 | 25.37 | 141.4 | 624.3 | 1911.1 |
| 60.00 | | 1.00 | 0.85 | 5.193 | 5.71 | 0.00 | 1.200 | 2.123 | 5.00 | 20.673 | 24.81 | 141.7 | 614.7 | 1868.9 |
| 65.00 | | 1.00 | 0.87 | 5.313 | 5.84 | 0.00 | 1.200 | 2.140 | 5.00 | 20.201 | 24.24 | 141.7 | 604.4 | 1826.1 |
| 70.00 | | 1.00 | 0.89 | 5.426 | 5.97 | 0.00 | 1.200 | 2.156 | 5.00 | 19.728 | 23.67 | 141.3 | 593.6 | 1782.6 |
| 75.00 Appurtenance(s) | | 1.00 | 0.91 | 5.534 | 6.09 | 0.00 | 1.200 | 2.171 | 5.00 | 19.253 | 23.10 | 140.7 | 582.2 | 1738.7 |
| 78.75 Bot - Section 3 | | 1.00 | 0.92 | 5.612 | 6.17 | 0.00 | 1.200 | 2.182 | 3.75 | 14.127 | 16.95 | 104.7 | 430.1 | 1276.0 |
| 80.00 | | 1.00 | 0.93 | 5.637 | 6.20 | 0.00 | 1.200 | 2.185 | 1.25 | 4.715 | 5.66 | 35.1 | 144.7 | 625.0 |
| 83.75 Top - Section 2 | | 1.00 | 0.94 | 5.712 | 6.28 | 0.00 | 1.200 | 2.195 | 3.75 | 13.969 | 16.76 | 105.3 | 427.4 | 1847.1 |
| 85.00 | | 1.00 | 0.94 | 5.736 | 6.31 | 0.00 | 1.200 | 2.198 | 1.25 | 4.596 | 5.52 | 34.8 | 141.7 | 338.2 |
| 90.00 | | 1.00 | 0.96 | 5.830 | 6.41 | 0.00 | 1.200 | 2.211 | 5.00 | 18.092 | 21.71 | 139.2 | 554.3 | 1325.7 |
| 95.00 | | 1.00 | 0.97 | 5.921 | 6.51 | 0.00 | 1.200 | 2.223 | 5.00 | 17.615 | 21.14 | 137.7 | 541.5 | 1289.6 |
| 100.00 | | 1.00 | 0.99 | 6.008 | 6.61 | 0.00 | 1.200 | 2.234 | 5.00 | 17.138 | 20.57 | 135.9 | 528.3 | 1253.1 |
| 105.00 | | 1.00 | 1.00 | 6.093 | 6.70 | 0.00 | 1.200 | 2.245 | 5.00 | 16.660 | 19.99 | 134.0 | 514.9 | 1216.4 |
| 110.00 | | 1.00 | 1.02 | 6.174 | 6.79 | 0.00 | 1.200 | 2.256 | 5.00 | 16.183 | 19.42 | 131.9 | 501.2 | 1179.4 |
| 115.00 | | 1.00 | 1.03 | 6.253 | 6.88 | 0.00 | 1.200 | 2.266 | 5.00 | 15.704 | 18.85 | 129.6 | 487.2 | 1142.2 |
| 119.00 Bot - Section 4 | | 1.00 | 1.04 | 6.315 | 6.95 | 0.00 | 1.200 | 2.274 | 4.00 | 12.218 | 14.66 | 101.8 | 380.7 | 887.9 |
| 120.00 | | 1.00 | 1.04 | 6.330 | 6.96 | 0.00 | 1.200 | 2.276 | 1.00 | 3.049 | 3.66 | 25.5 | 96.0 | 321.9 |
| 123.00 Top - Section 3 | | 1.00 | 1.05 | 6.375 | 7.01 | 0.00 | 1.200 | 2.281 | 3.00 | 9.032 | 10.84 | 76.0 | 282.9 | 950.5 |
| 125.00 | | 1.00 | 1.05 | 6.404 | 7.04 | 0.00 | 1.200 | 2.285 | 2.00 | 5.925 | 7.11 | 50.1 | 186.3 | 382.4 |
| 130.00 | | 1.00 | 1.07 | 6.476 | 7.12 | 0.00 | 1.200 | 2.294 | 5.00 | 14.480 | 17.38 | 123.8 | 451.2 | 928.4 |
| 135.00 | | 1.00 | 1.08 | 6.546 | 7.20 | 0.00 | 1.200 | 2.303 | 5.00 | 14.000 | 16.80 | 121.0 | 436.5 | 895.0 |
| 140.00 Appurtenance(s) | | 1.00 | 1.09 | 6.615 | 7.28 | 0.00 | 1.200 | 2.311 | 5.00 | 13.521 | 16.22 | 118.1 | 421.5 | 861.4 |
| 145.00 | | 1.00 | 1.10 | 6.681 | 7.35 | 0.00 | 1.200 | 2.319 | 5.00 | 13.041 | 15.65 | 115.0 | 406.4 | 827.7 |
| 150.00 | | 1.00 | 1.11 | 6.746 | 7.42 | 0.00 | 1.200 | 2.327 | 5.00 | 12.561 | 15.07 | 111.9 | 391.1 | 793.8 |
| 155.00 | | 1.00 | 1.12 | 6.810 | 7.49 | 0.00 | 1.200 | 2.335 | 5.00 | 12.081 | 14.50 | 108.6 | 375.7 | 759.7 |
| 157.00 Appurtenance(s) | | 1.00 | 1.12 | 6.835 | 7.52 | 0.00 | 1.200 | 2.338 | 2.00 | 4.697 | 5.64 | 42.4 | 147.8 | 296.2 |
| 160.00 | | 1.00 | 1.13 | 6.872 | 7.56 | 0.00 | 1.200 | 2.342 | 3.00 | 6.902 | 8.28 | 62.6 | 216.1 | 433.1 |
| 161.00 Top - Section 4 | | 1.00 | 1.13 | 6.884 | 7.57 | 0.00 | 1.200 | 2.343 | 1.00 | 2.262 | 2.71 | 20.6 | 71.4 | 142.2 |
| 165.00 | | 1.00 | 1.14 | 6.933 | 7.63 | 0.00 | 1.200 | 2.349 | 4.00 | 8.857 | 10.63 | 81.1 | 275.5 | 483.1 |
| 170.00 | | 1.00 | 1.15 | 6.992 | 7.69 | 0.00 | 1.200 | 2.356 | 5.00 | 10.639 | 12.77 | 98.2 | 328.5 | 575.4 |
| 175.00 Appurtenance(s) | | 1.00 | 1.16 | 7.050 | 7.76 | 0.00 | 1.200 | 2.363 | 5.00 | 10.158 | 12.19 | 94.5 | 312.6 | 545.5 |

Totals: 175.00 4,510.2 55,060.6

Discrete Appurtenance Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.0Di + 1.0Wi 50 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.00



| No. | Elev (ft) | Description | Qty | qz (psf) | qzGh (psf) | CaAa x Ka | Ka | Total CaAa (sf) | Dead Load (lb) | Horiz Ecc (ft) | Vert Ecc (ft) | Wind FX (lb) | Mom Y (lb-ft) | Mom Z (lb-ft) |
|-----|-----------|---------------------------|-----|----------|------------|-----------|------|-----------------|----------------|----------------|---------------|--------------|---------------|---------------|
| 1 | 175.00 | Low Profile Platform-flat | 1 | 7.050 | 7.755 | 1.00 | 1.00 | 53.36 | 2557.86 | 0.000 | 0.000 | 413.80 | 0.00 | 0.00 |
| 2 | 175.00 | DB-T1-6Z-8AB-0Z | 1 | 7.050 | 7.755 | 0.71 | 1.00 | 4.27 | 229.83 | 0.000 | 0.000 | 33.10 | 0.00 | 0.00 |
| 3 | 175.00 | FD9R6004/2C-3L (3.1 lbs) | 6 | 7.050 | 7.755 | 0.67 | 1.00 | 3.86 | 73.73 | 0.000 | 0.000 | 29.94 | 0.00 | 0.00 |
| 4 | 175.00 | RRH2x40-AWS | 3 | 7.050 | 7.755 | 0.82 | 1.00 | 10.27 | 352.87 | 0.000 | 0.000 | 79.66 | 0.00 | 0.00 |
| 5 | 175.00 | BXA-70080/6CF | 3 | 7.050 | 7.755 | 0.88 | 1.00 | 23.94 | 468.35 | 0.000 | 0.000 | 185.68 | 0.00 | 0.00 |
| 6 | 175.00 | WBX065X19R050 | 3 | 7.050 | 7.755 | 0.72 | 1.00 | 18.59 | 360.33 | 0.000 | 0.000 | 144.14 | 0.00 | 0.00 |
| 7 | 175.00 | BXA-171085/12CF | 3 | 7.050 | 7.755 | 0.84 | 1.00 | 20.13 | 361.39 | 0.000 | 0.000 | 156.11 | 0.00 | 0.00 |
| 8 | 175.00 | BXA-70063/6CF | 3 | 7.050 | 7.755 | 0.70 | 1.00 | 23.76 | 515.04 | 0.000 | 0.000 | 184.23 | 0.00 | 0.00 |
| 9 | 175.00 | 6' Lightning rod | 1 | 7.050 | 7.755 | 1.00 | 1.00 | 1.85 | 51.65 | 0.000 | 0.000 | 14.37 | 0.00 | 0.00 |
| 10 | 157.00 | ALU - TD-RRH8x20-25 - | 3 | 6.835 | 7.518 | 0.60 | 0.80 | 9.30 | 727.95 | 0.000 | 0.000 | 69.93 | 0.00 | 0.00 |
| 11 | 157.00 | ALU - 800 MHz - RRU | 6 | 6.835 | 7.518 | 0.60 | 0.80 | 14.48 | 849.39 | 0.000 | 0.000 | 108.86 | 0.00 | 0.00 |
| 12 | 157.00 | ALU - 1900 MHz - RRU | 3 | 6.835 | 7.518 | 0.60 | 0.80 | 8.04 | 479.57 | 0.000 | 0.000 | 60.48 | 0.00 | 0.00 |
| 13 | 157.00 | NNVV-65B-R4 | 3 | 6.835 | 7.518 | 0.59 | 0.80 | 25.26 | 1385.10 | 0.000 | 0.000 | 189.88 | 0.00 | 0.00 |
| 14 | 157.00 | APXVTM14-C-I20 | 3 | 6.835 | 7.518 | 0.62 | 0.80 | 14.53 | 891.79 | 0.000 | 0.000 | 109.26 | 0.00 | 0.00 |
| 15 | 157.00 | Platform w/ Handrail + | 1 | 6.835 | 7.518 | 1.00 | 1.00 | 114.59 | 7932.63 | 0.000 | 0.000 | 861.54 | 0.00 | 0.00 |
| 16 | 140.00 | Platform w/ Hand Rails | 1 | 6.615 | 7.276 | 1.00 | 1.00 | 67.73 | 4573.15 | 0.000 | 0.000 | 492.83 | 0.00 | 0.00 |
| 17 | 140.00 | 782 11056 | 3 | 6.615 | 7.276 | 0.62 | 0.80 | 0.97 | 9.73 | 0.000 | 0.000 | 7.04 | 0.00 | 0.00 |
| 18 | 140.00 | KRY 112 144/1 | 3 | 6.615 | 7.276 | 0.58 | 0.80 | 1.82 | 73.13 | 0.000 | 0.000 | 13.25 | 0.00 | 0.00 |
| 19 | 140.00 | LNX-6515DS-VTM | 3 | 6.615 | 7.276 | 0.64 | 0.80 | 30.29 | 907.32 | 0.000 | 0.000 | 220.38 | 0.00 | 0.00 |
| 20 | 140.00 | APXV18-206516S-C-A20 | 3 | 6.615 | 7.276 | 0.58 | 0.80 | 10.63 | 285.69 | 0.000 | 0.000 | 77.37 | 0.00 | 0.00 |
| 21 | 75.00 | GPS | 1 | 5.534 | 6.088 | 1.00 | 1.00 | 1.89 | 40.47 | 0.000 | 0.000 | 11.48 | 0.00 | 0.00 |

Totals: 23,126.96

3,463.32

Total Applied Force Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.0Di + 1.0Wi 50 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.00



| Elev (ft) | Description | Lateral FX (-) (lb) | Axial FY (-) (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
|----------------|------------------|---------------------|-------------------|--------------------|-------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | | 141.94 | 2582.95 | 0.00 | 0.00 |
| 10.00 | | 139.76 | 2577.04 | 0.00 | 0.00 |
| 15.00 | | 137.37 | 2553.29 | 0.00 | 0.00 |
| 20.00 | | 134.89 | 2521.68 | 0.00 | 0.00 |
| 25.00 | | 132.36 | 2485.53 | 0.00 | 0.00 |
| 30.00 | | 129.91 | 2446.36 | 0.00 | 0.00 |
| 35.00 | | 133.05 | 2405.03 | 0.00 | 0.00 |
| 38.75 | | 100.88 | 1776.20 | 0.00 | 0.00 |
| 40.00 | | 34.13 | 932.93 | 0.00 | 0.00 |
| 45.00 | | 139.41 | 3681.17 | 0.00 | 0.00 |
| 50.00 | | 140.63 | 2125.75 | 0.00 | 0.00 |
| 55.00 | | 141.37 | 2084.30 | 0.00 | 0.00 |
| 60.00 | | 141.70 | 2042.10 | 0.00 | 0.00 |
| 65.00 | | 141.66 | 1999.23 | 0.00 | 0.00 |
| 70.00 | | 141.30 | 1955.80 | 0.00 | 0.00 |
| 75.00 | (1) attachments | 152.13 | 1952.33 | 0.00 | 0.00 |
| 78.75 | | 104.65 | 1405.18 | 0.00 | 0.00 |
| 80.00 | | 35.09 | 668.01 | 0.00 | 0.00 |
| 83.75 | | 105.32 | 1976.28 | 0.00 | 0.00 |
| 85.00 | | 34.80 | 381.25 | 0.00 | 0.00 |
| 90.00 | | 139.23 | 1497.92 | 0.00 | 0.00 |
| 95.00 | | 137.67 | 1461.78 | 0.00 | 0.00 |
| 100.00 | | 135.92 | 1425.33 | 0.00 | 0.00 |
| 105.00 | | 133.99 | 1388.60 | 0.00 | 0.00 |
| 110.00 | | 131.89 | 1351.60 | 0.00 | 0.00 |
| 115.00 | | 129.63 | 1314.36 | 0.00 | 0.00 |
| 119.00 | | 101.84 | 1025.65 | 0.00 | 0.00 |
| 120.00 | | 25.47 | 356.34 | 0.00 | 0.00 |
| 123.00 | | 76.00 | 1053.79 | 0.00 | 0.00 |
| 125.00 | | 50.09 | 451.28 | 0.00 | 0.00 |
| 130.00 | | 123.78 | 1100.59 | 0.00 | 0.00 |
| 135.00 | | 120.98 | 1067.20 | 0.00 | 0.00 |
| 140.00 | (13) attachments | 928.92 | 6882.64 | 0.00 | 0.00 |
| 145.00 | | 115.01 | 925.00 | 0.00 | 0.00 |
| 150.00 | | 111.86 | 891.09 | 0.00 | 0.00 |
| 155.00 | | 108.59 | 857.03 | 0.00 | 0.00 |
| 157.00 | (19) attachments | 1442.33 | 12601.52 | 0.00 | 0.00 |
| 160.00 | | 62.61 | 481.95 | 0.00 | 0.00 |
| 161.00 | | 20.55 | 158.53 | 0.00 | 0.00 |
| 165.00 | | 81.05 | 548.25 | 0.00 | 0.00 |
| 170.00 | | 98.19 | 656.89 | 0.00 | 0.00 |
| 175.00 | (24) attachments | 1335.56 | 5597.99 | 0.00 | 0.00 |
| Totals: | | 7,973.54 | 83,647.75 | 0.00 | 0.00 |

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.2D + 1.0Di + 1.0Wi 50 mph Wind

Dead Load Factor 1.20
Wind Load Factor 1.00



| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -83.64 | -8.00 | 0.00 | -1026.1 | 0.00 | 1026.11 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.000 | 0.000 | 0.151 |
| 5.00 | -81.06 | -7.92 | 0.00 | -986.10 | 0.00 | 986.10 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.02 | -0.040 | 0.000 | 0.150 |
| 10.00 | -78.47 | -7.83 | 0.00 | -946.52 | 0.00 | 946.52 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.08 | -0.080 | 0.000 | 0.149 |
| 15.00 | -75.92 | -7.74 | 0.00 | -907.37 | 0.00 | 907.37 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.19 | -0.121 | 0.000 | 0.148 |
| 20.00 | -73.39 | -7.66 | 0.00 | -868.66 | 0.00 | 868.66 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 0.34 | -0.163 | 0.000 | 0.147 |
| 25.00 | -70.90 | -7.57 | 0.00 | -830.38 | 0.00 | 830.38 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 0.53 | -0.206 | 0.000 | 0.146 |
| 30.00 | -68.45 | -7.48 | 0.00 | -792.53 | 0.00 | 792.53 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 0.77 | -0.250 | 0.000 | 0.145 |
| 35.00 | -66.04 | -7.38 | 0.00 | -755.11 | 0.00 | 755.11 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 1.06 | -0.295 | 0.000 | 0.144 |
| 38.75 | -64.26 | -7.30 | 0.00 | -727.42 | 0.00 | 727.42 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 1.30 | -0.330 | 0.000 | 0.144 |
| 40.00 | -63.32 | -7.29 | 0.00 | -718.30 | 0.00 | 718.30 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 1.39 | -0.342 | 0.000 | 0.144 |
| 45.00 | -59.64 | -7.18 | 0.00 | -681.83 | 0.00 | 681.83 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 1.78 | -0.388 | 0.000 | 0.161 |
| 50.00 | -57.50 | -7.07 | 0.00 | -645.94 | 0.00 | 645.94 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 2.21 | -0.436 | 0.000 | 0.159 |
| 55.00 | -55.41 | -6.97 | 0.00 | -610.57 | 0.00 | 610.57 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 2.69 | -0.489 | 0.000 | 0.157 |
| 60.00 | -53.37 | -6.86 | 0.00 | -575.74 | 0.00 | 575.74 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 3.23 | -0.542 | 0.000 | 0.155 |
| 65.00 | -51.36 | -6.74 | 0.00 | -541.45 | 0.00 | 541.45 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 3.83 | -0.597 | 0.000 | 0.153 |
| 70.00 | -49.40 | -6.63 | 0.00 | -507.73 | 0.00 | 507.73 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 4.49 | -0.652 | 0.000 | 0.152 |
| 75.00 | -47.45 | -6.50 | 0.00 | -474.58 | 0.00 | 474.58 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 5.20 | -0.708 | 0.000 | 0.150 |
| 78.75 | -46.04 | -6.40 | 0.00 | -450.22 | 0.00 | 450.22 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 5.77 | -0.751 | 0.000 | 0.149 |
| 80.00 | -45.37 | -6.38 | 0.00 | -442.22 | 0.00 | 442.22 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 5.97 | -0.766 | 0.000 | 0.148 |
| 83.75 | -43.39 | -6.27 | 0.00 | -418.31 | 0.00 | 418.31 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 6.59 | -0.810 | 0.000 | 0.211 |
| 85.00 | -43.01 | -6.26 | 0.00 | -410.48 | 0.00 | 410.48 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 6.80 | -0.825 | 0.000 | 0.210 |
| 90.00 | -41.50 | -6.16 | 0.00 | -379.18 | 0.00 | 379.18 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 7.71 | -0.903 | 0.000 | 0.204 |
| 95.00 | -40.03 | -6.05 | 0.00 | -348.40 | 0.00 | 348.40 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 8.70 | -0.981 | 0.000 | 0.198 |
| 100.00 | -38.60 | -5.94 | 0.00 | -318.16 | 0.00 | 318.16 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 9.77 | -1.060 | 0.000 | 0.191 |
| 105.00 | -37.21 | -5.83 | 0.00 | -288.46 | 0.00 | 288.46 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 10.92 | -1.138 | 0.000 | 0.184 |
| 110.00 | -35.85 | -5.72 | 0.00 | -259.31 | 0.00 | 259.31 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 12.15 | -1.217 | 0.000 | 0.176 |
| 115.00 | -34.54 | -5.60 | 0.00 | -230.71 | 0.00 | 230.71 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 13.47 | -1.295 | 0.000 | 0.167 |
| 119.00 | -33.51 | -5.50 | 0.00 | -208.29 | 0.00 | 208.29 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 14.58 | -1.357 | 0.000 | 0.160 |
| 120.00 | -33.15 | -5.49 | 0.00 | -202.79 | 0.00 | 202.79 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 14.87 | -1.373 | 0.000 | 0.158 |
| 123.00 | -32.09 | -5.40 | 0.00 | -186.34 | 0.00 | 186.34 | 1577.63 | 788.82 | 1975.86 | 989.40 | 15.75 | -1.419 | 0.000 | 0.209 |
| 125.00 | -31.64 | -5.38 | 0.00 | -175.53 | 0.00 | 175.53 | 1561.09 | 780.55 | 1925.40 | 964.13 | 16.35 | -1.450 | 0.000 | 0.202 |
| 130.00 | -30.53 | -5.27 | 0.00 | -148.65 | 0.00 | 148.65 | 1518.76 | 759.38 | 1800.86 | 901.77 | 17.91 | -1.535 | 0.000 | 0.185 |
| 135.00 | -29.46 | -5.16 | 0.00 | -122.31 | 0.00 | 122.31 | 1475.03 | 737.52 | 1678.77 | 840.64 | 19.56 | -1.615 | 0.000 | 0.166 |
| 140.00 | -22.61 | -4.06 | 0.00 | -96.53 | 0.00 | 96.53 | 1429.92 | 714.96 | 1559.34 | 780.83 | 21.29 | -1.687 | 0.000 | 0.139 |
| 145.00 | -21.68 | -3.94 | 0.00 | -76.25 | 0.00 | 76.25 | 1383.42 | 691.71 | 1442.75 | 722.45 | 23.10 | -1.753 | 0.000 | 0.121 |
| 150.00 | -20.79 | -3.82 | 0.00 | -56.56 | 0.00 | 56.56 | 1321.23 | 660.61 | 1314.97 | 658.46 | 24.97 | -1.810 | 0.000 | 0.102 |
| 155.00 | -19.94 | -3.69 | 0.00 | -37.48 | 0.00 | 37.48 | 1258.65 | 629.32 | 1192.75 | 597.26 | 26.89 | -1.857 | 0.000 | 0.079 |
| 157.00 | -7.39 | -1.84 | 0.00 | -30.10 | 0.00 | 30.10 | 1233.62 | 616.81 | 1145.53 | 573.62 | 27.67 | -1.872 | 0.000 | 0.058 |
| 160.00 | -6.91 | -1.76 | 0.00 | -24.57 | 0.00 | 24.57 | 1196.07 | 598.03 | 1076.49 | 539.05 | 28.85 | -1.892 | 0.000 | 0.051 |
| 161.00 | -6.75 | -1.74 | 0.00 | -22.81 | 0.00 | 22.81 | 1183.55 | 591.78 | 1053.96 | 527.76 | 29.25 | -1.898 | 0.000 | 0.049 |
| 161.00 | -6.75 | -1.74 | 0.00 | -22.81 | 0.00 | 22.81 | 858.57 | 429.28 | 768.96 | 385.05 | 29.25 | -1.898 | 0.000 | 0.067 |
| 165.00 | -6.20 | -1.64 | 0.00 | -15.85 | 0.00 | 15.85 | 832.45 | 416.23 | 713.85 | 357.46 | 30.85 | -1.920 | 0.000 | 0.052 |
| 170.00 | -5.55 | -1.53 | 0.00 | -7.63 | 0.00 | 7.63 | 798.56 | 399.28 | 646.76 | 323.86 | 32.87 | -1.944 | 0.000 | 0.031 |
| 175.00 | 0.00 | -1.34 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 34.92 | -1.954 | 0.000 | 0.000 |

Seismic Segment Forces (Factored)

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



Topography: 1

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Load Case: 1.2D + 1.0E



| | | | | | |
|-----------------------------|------|----------------------------|------|-------------------|------|
| Gust Response Factor | 1.10 | Sds | 0.18 | Iterations | 23 |
| Dead Load Factor | 1.20 | Seismic Load Factor | 1.00 | Sd1 | 0.10 |
| Wind Load Factor | 0.00 | Structure Frequency | 0.33 | SA | 0.03 |

Ss 0.17
S1 0.06
Seismic Importance Factor 1.00

| Top Elev (ft) | Description | Wz (lb) | a | b | c | Lateral Fs (lb) | R: 1.50 |
|----------------------|--------------------|-----------------|----------|----------|----------------|------------------------|-----------------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5.00 | | 1510.7 | 0.00 | 0.03 | 0.02 | 23.97 | |
| 10.00 | | 1479.7 | 0.01 | 0.05 | 0.03 | 35.12 | |
| 15.00 | | 1448.6 | 0.01 | 0.06 | 0.03 | 40.52 | |
| 20.00 | | 1417.6 | 0.02 | 0.07 | 0.04 | 42.99 | |
| 25.00 | | 1386.5 | 0.04 | 0.07 | 0.04 | 43.95 | |
| 30.00 | | 1355.5 | 0.06 | 0.07 | 0.04 | 44.19 | |
| 35.00 | | 1324.4 | 0.08 | 0.07 | 0.04 | 44.14 | |
| 38.75 | Bot - Section 2 | 972.99 | 0.09 | 0.07 | 0.04 | 32.94 | |
| 40.00 | | 606.38 | 0.10 | 0.07 | 0.04 | 20.63 | |
| 45.00 | Top - Section 1 | 2389.1 | 0.12 | 0.07 | 0.03 | 82.94 | |
| 50.00 | | 1099.5 | 0.15 | 0.07 | 0.03 | 38.81 | |
| 55.00 | | 1072.4 | 0.19 | 0.06 | 0.02 | 38.16 | |
| 60.00 | | 1045.2 | 0.22 | 0.06 | 0.02 | 36.89 | |
| 65.00 | | 1018.0 | 0.26 | 0.05 | 0.02 | 34.64 | |
| 70.00 | | 990.89 | 0.30 | 0.04 | 0.01 | 31.05 | |
| 75.00 | Appurtenance(s) | 973.73 | 0.35 | 0.03 | 0.01 | 26.05 | |
| 78.75 | Bot - Section 3 | 704.96 | 0.38 | 0.02 | 0.01 | 15.42 | |
| 80.00 | | 400.18 | 0.39 | 0.02 | 0.01 | 7.99 | |
| 83.75 | Top - Section 2 | 1183.0 | 0.43 | 0.01 | 0.01 | 15.84 | |
| 85.00 | | 163.74 | 0.45 | 0.00 | 0.01 | 1.79 | |
| 90.00 | | 642.81 | 0.50 | -0.02 | 0.01 | 0.18 | |
| 95.00 | | 623.41 | 0.56 | -0.04 | 0.01 | -6.78 | |
| 100.00 | | 604.00 | 0.62 | -0.06 | 0.02 | -12.74 | |
| 105.00 | | 584.59 | 0.68 | -0.08 | 0.03 | -16.98 | |
| 110.00 | | 565.19 | 0.75 | -0.10 | 0.04 | -19.15 | |
| 115.00 | | 545.78 | 0.82 | -0.11 | 0.06 | -19.21 | |
| 119.00 | Bot - Section 4 | 422.65 | 0.87 | -0.12 | 0.08 | -14.21 | |
| 120.00 | | 188.22 | 0.89 | -0.12 | 0.08 | -6.19 | |
| 123.00 | Top - Section 3 | 556.27 | 0.93 | -0.12 | 0.10 | -16.55 | |
| 125.00 | | 163.40 | 0.96 | -0.12 | 0.11 | -4.40 | |
| 130.00 | | 397.64 | 1.04 | -0.10 | 0.15 | -6.93 | |
| 135.00 | | 382.12 | 1.12 | -0.05 | 0.20 | -1.69 | |
| 140.00 | Appurtenance(s) | 2611.9 | 1.21 | 0.01 | 0.26 | 31.59 | |
| 145.00 | | 351.07 | 1.30 | 0.12 | 0.33 | 11.28 | |
| 150.00 | | 335.54 | 1.39 | 0.26 | 0.42 | 18.70 | |
| 155.00 | | 320.02 | 1.48 | 0.46 | 0.52 | 26.55 | |
| 157.00 | Appurtenance(s) | 4054.3 | 1.52 | 0.55 | 0.57 | 384.62 | |
| 160.00 | | 180.83 | 1.58 | 0.72 | 0.64 | 20.59 | |
| 161.00 | Top - Section 4 | 59.04 | 1.60 | 0.78 | 0.67 | 7.11 | |
| 165.00 | | 172.96 | 1.68 | 1.05 | 0.78 | 25.68 | |
| 170.00 | | 205.72 | 1.78 | 1.46 | 0.95 | 38.46 | |
| 175.00 | Appurtenance(s) | 1782.7 | 1.89 | 1.98 | 1.14 | 408.83 | |
| Totals: | | 38,294.2 | | | 1,506.8 | | Total Wind: 27,537.5 |

Seismic Base Shear is Less Than 50% of Wind Force - An Analysis is NOT Required

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018

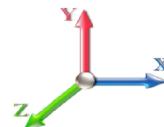


Topography: 1

Page: 21

Load Case: 1.2D + 1.0E

| | | | | | |
|-----------------------------|------|----------------------------|------|----------------------------------|------|
| Gust Response Factor | 1.10 | Sds | 0.18 | Iterations | 23 |
| Dead Load Factor | 1.20 | Sd1 | 0.10 | Ss | 0.17 |
| Wind Load Factor | 0.00 | Structure Frequency | 0.33 | S1 | 0.06 |
| | | SA | 0.03 | Seismic Importance Factor | 1.00 |



| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -51.41 | -1.63 | 0.00 | -196.36 | 0.00 | 196.36 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.00 | 0.00 | 0.034 |
| 5.00 | -49.43 | -1.62 | 0.00 | -188.18 | 0.00 | 188.18 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.00 | -0.01 | -0.02 | 0.034 |
| 10.00 | -47.48 | -1.59 | 0.00 | -180.10 | 0.00 | 180.10 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.02 | -0.02 | -0.03 | 0.034 |
| 15.00 | -45.57 | -1.55 | 0.00 | -172.16 | 0.00 | 172.16 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.04 | -0.02 | -0.03 | 0.033 |
| 20.00 | -43.69 | -1.52 | 0.00 | -164.40 | 0.00 | 164.40 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 0.06 | -0.03 | -0.03 | 0.033 |
| 25.00 | -41.85 | -1.48 | 0.00 | -156.82 | 0.00 | 156.82 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 0.10 | -0.04 | -0.04 | 0.032 |
| 30.00 | -40.05 | -1.44 | 0.00 | -149.44 | 0.00 | 149.44 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 0.15 | -0.05 | -0.05 | 0.032 |
| 35.00 | -38.29 | -1.40 | 0.00 | -142.26 | 0.00 | 142.26 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 0.20 | -0.06 | -0.06 | 0.032 |
| 38.75 | -36.99 | -1.36 | 0.00 | -137.02 | 0.00 | 137.02 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 0.25 | -0.06 | -0.06 | 0.032 |
| 40.00 | -36.22 | -1.35 | 0.00 | -135.32 | 0.00 | 135.32 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 0.26 | -0.06 | -0.06 | 0.031 |
| 45.00 | -33.18 | -1.26 | 0.00 | -128.59 | 0.00 | 128.59 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 0.34 | -0.07 | -0.07 | 0.035 |
| 50.00 | -31.69 | -1.23 | 0.00 | -122.26 | 0.00 | 122.26 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 0.42 | -0.08 | -0.08 | 0.035 |
| 55.00 | -30.23 | -1.19 | 0.00 | -116.12 | 0.00 | 116.12 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 0.51 | -0.09 | -0.09 | 0.034 |
| 60.00 | -28.80 | -1.16 | 0.00 | -110.15 | 0.00 | 110.15 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 0.61 | -0.10 | -0.10 | 0.034 |
| 65.00 | -27.41 | -1.13 | 0.00 | -104.35 | 0.00 | 104.35 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 0.73 | -0.11 | -0.11 | 0.034 |
| 70.00 | -26.04 | -1.10 | 0.00 | -98.71 | 0.00 | 98.71 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 0.85 | -0.12 | -0.12 | 0.033 |
| 75.00 | -24.70 | -1.07 | 0.00 | -93.21 | 0.00 | 93.21 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 0.99 | -0.13 | -0.13 | 0.033 |
| 78.75 | -23.73 | -1.06 | 0.00 | -89.18 | 0.00 | 89.18 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 1.10 | -0.14 | -0.14 | 0.033 |
| 80.00 | -23.20 | -1.05 | 0.00 | -87.86 | 0.00 | 87.86 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 1.13 | -0.15 | -0.15 | 0.033 |
| 83.75 | -21.66 | -1.03 | 0.00 | -83.92 | 0.00 | 83.92 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 1.25 | -0.16 | -0.16 | 0.047 |
| 85.00 | -21.42 | -1.04 | 0.00 | -82.62 | 0.00 | 82.62 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 1.29 | -0.16 | -0.16 | 0.047 |
| 90.00 | -20.47 | -1.04 | 0.00 | -77.45 | 0.00 | 77.45 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 1.47 | -0.17 | -0.17 | 0.046 |
| 95.00 | -19.55 | -1.04 | 0.00 | -72.26 | 0.00 | 72.26 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 1.66 | -0.19 | -0.19 | 0.045 |
| 100.00 | -18.65 | -1.04 | 0.00 | -67.06 | 0.00 | 67.06 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 1.87 | -0.21 | -0.21 | 0.045 |
| 105.00 | -17.78 | -1.04 | 0.00 | -61.84 | 0.00 | 61.84 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 2.09 | -0.22 | -0.22 | 0.043 |
| 110.00 | -16.93 | -1.05 | 0.00 | -56.62 | 0.00 | 56.62 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 2.33 | -0.24 | -0.24 | 0.042 |
| 115.00 | -16.10 | -1.05 | 0.00 | -51.39 | 0.00 | 51.39 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 2.59 | -0.26 | -0.26 | 0.041 |
| 119.00 | -15.46 | -1.05 | 0.00 | -47.20 | 0.00 | 47.20 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 2.82 | -0.27 | -0.27 | 0.040 |
| 120.00 | -15.20 | -1.05 | 0.00 | -46.15 | 0.00 | 46.15 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 2.87 | -0.27 | -0.27 | 0.039 |
| 123.00 | -14.43 | -1.05 | 0.00 | -43.01 | 0.00 | 43.01 | 1577.63 | 788.82 | 1975.86 | 989.40 | 3.05 | -0.29 | -0.29 | 0.053 |
| 125.00 | -14.16 | -1.05 | 0.00 | -40.92 | 0.00 | 40.92 | 1561.09 | 780.55 | 1925.40 | 964.13 | 3.17 | -0.29 | -0.29 | 0.052 |
| 130.00 | -13.51 | -1.05 | 0.00 | -35.68 | 0.00 | 35.68 | 1518.76 | 759.38 | 1800.86 | 901.77 | 3.49 | -0.31 | -0.31 | 0.048 |
| 135.00 | -12.88 | -1.05 | 0.00 | -30.43 | 0.00 | 30.43 | 1475.03 | 737.52 | 1678.77 | 840.64 | 3.83 | -0.33 | -0.33 | 0.045 |
| 140.00 | -9.57 | -1.00 | 0.00 | -25.18 | 0.00 | 25.18 | 1429.92 | 714.96 | 1559.34 | 780.83 | 4.18 | -0.35 | -0.35 | 0.039 |
| 145.00 | -9.05 | -0.99 | 0.00 | -20.18 | 0.00 | 20.18 | 1383.42 | 691.71 | 1442.75 | 722.45 | 4.56 | -0.37 | -0.37 | 0.034 |
| 150.00 | -8.55 | -0.97 | 0.00 | -15.23 | 0.00 | 15.23 | 1321.23 | 660.61 | 1314.97 | 658.46 | 4.95 | -0.38 | -0.38 | 0.030 |
| 155.00 | -8.07 | -0.94 | 0.00 | -10.38 | 0.00 | 10.38 | 1258.65 | 629.32 | 1192.75 | 597.26 | 5.36 | -0.40 | -0.40 | 0.024 |
| 157.00 | -3.17 | -0.52 | 0.00 | -8.50 | 0.00 | 8.50 | 1233.62 | 616.81 | 1145.53 | 573.62 | 5.53 | -0.40 | -0.40 | 0.017 |
| 160.00 | -2.91 | -0.50 | 0.00 | -6.93 | 0.00 | 6.93 | 1196.07 | 598.03 | 1076.49 | 539.05 | 5.78 | -0.41 | -0.41 | 0.015 |
| 161.00 | -2.82 | -0.49 | 0.00 | -6.43 | 0.00 | 6.43 | 1183.55 | 591.78 | 1053.96 | 527.76 | 5.87 | -0.41 | -0.41 | 0.015 |
| 161.00 | -2.82 | -0.49 | 0.00 | -6.43 | 0.00 | 6.43 | 858.57 | 429.28 | 768.96 | 385.05 | 5.87 | -0.41 | -0.41 | 0.020 |
| 165.00 | -2.55 | -0.47 | 0.00 | -4.45 | 0.00 | 4.45 | 832.45 | 416.23 | 713.85 | 357.46 | 6.21 | -0.41 | -0.41 | 0.016 |
| 170.00 | -2.22 | -0.43 | 0.00 | -2.13 | 0.00 | 2.13 | 798.56 | 399.28 | 646.76 | 323.86 | 6.65 | -0.42 | -0.42 | 0.009 |
| 175.00 | 0.00 | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 7.09 | -0.42 | -0.42 | 0.000 |

Seismic Segment Forces (Factored)

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



Topography: 1

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Load Case: 0.9D + 1.0E



| | | | | | |
|-----------------------------|------|----------------------------|------|-------------------|------|
| Gust Response Factor | 1.10 | Sds | 0.18 | Iterations | 23 |
| Dead Load Factor | 0.90 | Seismic Load Factor | 1.00 | Sd1 | 0.10 |
| Wind Load Factor | 0.00 | Structure Frequency | 0.33 | SA | 0.03 |

Ss 0.17
S1 0.06
Seismic Importance Factor 1.00

| Top Elev (ft) | Description | Wz (lb) | a | b | c | Lateral Fs (lb) | R: 1.50 |
|----------------------|--------------------|-----------------|----------|----------|----------------|------------------------|-----------------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 5.00 | | 1510.7 | 0.00 | 0.03 | 0.02 | 23.97 | |
| 10.00 | | 1479.7 | 0.01 | 0.05 | 0.03 | 35.12 | |
| 15.00 | | 1448.6 | 0.01 | 0.06 | 0.03 | 40.52 | |
| 20.00 | | 1417.6 | 0.02 | 0.07 | 0.04 | 42.99 | |
| 25.00 | | 1386.5 | 0.04 | 0.07 | 0.04 | 43.95 | |
| 30.00 | | 1355.5 | 0.06 | 0.07 | 0.04 | 44.19 | |
| 35.00 | | 1324.4 | 0.08 | 0.07 | 0.04 | 44.14 | |
| 38.75 | Bot - Section 2 | 972.99 | 0.09 | 0.07 | 0.04 | 32.94 | |
| 40.00 | | 606.38 | 0.10 | 0.07 | 0.04 | 20.63 | |
| 45.00 | Top - Section 1 | 2389.1 | 0.12 | 0.07 | 0.03 | 82.94 | |
| 50.00 | | 1099.5 | 0.15 | 0.07 | 0.03 | 38.81 | |
| 55.00 | | 1072.4 | 0.19 | 0.06 | 0.02 | 38.16 | |
| 60.00 | | 1045.2 | 0.22 | 0.06 | 0.02 | 36.89 | |
| 65.00 | | 1018.0 | 0.26 | 0.05 | 0.02 | 34.64 | |
| 70.00 | | 990.89 | 0.30 | 0.04 | 0.01 | 31.05 | |
| 75.00 | Appurtenance(s) | 973.73 | 0.35 | 0.03 | 0.01 | 26.05 | |
| 78.75 | Bot - Section 3 | 704.96 | 0.38 | 0.02 | 0.01 | 15.42 | |
| 80.00 | | 400.18 | 0.39 | 0.02 | 0.01 | 7.99 | |
| 83.75 | Top - Section 2 | 1183.0 | 0.43 | 0.01 | 0.01 | 15.84 | |
| 85.00 | | 163.74 | 0.45 | 0.00 | 0.01 | 1.79 | |
| 90.00 | | 642.81 | 0.50 | -0.02 | 0.01 | 0.18 | |
| 95.00 | | 623.41 | 0.56 | -0.04 | 0.01 | -6.78 | |
| 100.00 | | 604.00 | 0.62 | -0.06 | 0.02 | -12.74 | |
| 105.00 | | 584.59 | 0.68 | -0.08 | 0.03 | -16.98 | |
| 110.00 | | 565.19 | 0.75 | -0.10 | 0.04 | -19.15 | |
| 115.00 | | 545.78 | 0.82 | -0.11 | 0.06 | -19.21 | |
| 119.00 | Bot - Section 4 | 422.65 | 0.87 | -0.12 | 0.08 | -14.21 | |
| 120.00 | | 188.22 | 0.89 | -0.12 | 0.08 | -6.19 | |
| 123.00 | Top - Section 3 | 556.27 | 0.93 | -0.12 | 0.10 | -16.55 | |
| 125.00 | | 163.40 | 0.96 | -0.12 | 0.11 | -4.40 | |
| 130.00 | | 397.64 | 1.04 | -0.10 | 0.15 | -6.93 | |
| 135.00 | | 382.12 | 1.12 | -0.05 | 0.20 | -1.69 | |
| 140.00 | Appurtenance(s) | 2611.9 | 1.21 | 0.01 | 0.26 | 31.59 | |
| 145.00 | | 351.07 | 1.30 | 0.12 | 0.33 | 11.28 | |
| 150.00 | | 335.54 | 1.39 | 0.26 | 0.42 | 18.70 | |
| 155.00 | | 320.02 | 1.48 | 0.46 | 0.52 | 26.55 | |
| 157.00 | Appurtenance(s) | 4054.3 | 1.52 | 0.55 | 0.57 | 384.62 | |
| 160.00 | | 180.83 | 1.58 | 0.72 | 0.64 | 20.59 | |
| 161.00 | Top - Section 4 | 59.04 | 1.60 | 0.78 | 0.67 | 7.11 | |
| 165.00 | | 172.96 | 1.68 | 1.05 | 0.78 | 25.68 | |
| 170.00 | | 205.72 | 1.78 | 1.46 | 0.95 | 38.46 | |
| 175.00 | Appurtenance(s) | 1782.7 | 1.89 | 1.98 | 1.14 | 408.83 | |
| Totals: | | 38,294.2 | | | 1,506.8 | | Total Wind: 27,537.5 |

Seismic Base Shear is Less Than 50% of Wind Force - An Analysis is NOT Required

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



Topography: 1

Page: 23

Load Case: 0.9D + 1.0E



| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -38.56 | -1.63 | 0.00 | -194.12 | 0.00 | 194.12 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.00 | 0.00 | 0.032 |
| 5.00 | -37.07 | -1.61 | 0.00 | -185.95 | 0.00 | 185.95 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.00 | -0.01 | -0.02 | 0.032 |
| 10.00 | -35.61 | -1.58 | 0.00 | -177.88 | 0.00 | 177.88 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.02 | -0.02 | -0.02 | 0.031 |
| 15.00 | -34.17 | -1.55 | 0.00 | -169.96 | 0.00 | 169.96 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.04 | -0.02 | -0.02 | 0.031 |
| 20.00 | -32.77 | -1.51 | 0.00 | -162.22 | 0.00 | 162.22 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 0.06 | -0.03 | -0.03 | 0.031 |
| 25.00 | -31.39 | -1.47 | 0.00 | -154.68 | 0.00 | 154.68 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 0.10 | -0.04 | -0.04 | 0.030 |
| 30.00 | -30.04 | -1.43 | 0.00 | -147.34 | 0.00 | 147.34 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 0.15 | -0.05 | -0.05 | 0.030 |
| 35.00 | -28.72 | -1.39 | 0.00 | -140.21 | 0.00 | 140.21 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 0.20 | -0.06 | -0.06 | 0.030 |
| 38.75 | -27.75 | -1.35 | 0.00 | -135.01 | 0.00 | 135.01 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 0.24 | -0.06 | -0.06 | 0.030 |
| 40.00 | -27.17 | -1.33 | 0.00 | -133.32 | 0.00 | 133.32 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 0.26 | -0.06 | -0.06 | 0.029 |
| 45.00 | -24.89 | -1.25 | 0.00 | -126.64 | 0.00 | 126.64 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 0.33 | -0.07 | -0.07 | 0.033 |
| 50.00 | -23.77 | -1.22 | 0.00 | -120.38 | 0.00 | 120.38 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 0.41 | -0.08 | -0.08 | 0.032 |
| 55.00 | -22.67 | -1.18 | 0.00 | -114.29 | 0.00 | 114.29 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 0.50 | -0.09 | -0.09 | 0.032 |
| 60.00 | -21.60 | -1.15 | 0.00 | -108.39 | 0.00 | 108.39 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 0.61 | -0.10 | -0.10 | 0.032 |
| 65.00 | -20.55 | -1.11 | 0.00 | -102.66 | 0.00 | 102.66 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 0.72 | -0.11 | -0.11 | 0.032 |
| 70.00 | -19.53 | -1.08 | 0.00 | -97.10 | 0.00 | 97.10 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 0.84 | -0.12 | -0.12 | 0.031 |
| 75.00 | -18.53 | -1.06 | 0.00 | -91.68 | 0.00 | 91.68 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 0.97 | -0.13 | -0.13 | 0.031 |
| 78.75 | -17.80 | -1.04 | 0.00 | -87.71 | 0.00 | 87.71 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 1.08 | -0.14 | -0.14 | 0.031 |
| 80.00 | -17.40 | -1.04 | 0.00 | -86.40 | 0.00 | 86.40 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 1.12 | -0.14 | -0.14 | 0.031 |
| 83.75 | -16.24 | -1.02 | 0.00 | -82.52 | 0.00 | 82.52 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 1.23 | -0.15 | -0.15 | 0.045 |
| 85.00 | -16.06 | -1.02 | 0.00 | -81.25 | 0.00 | 81.25 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 1.28 | -0.16 | -0.16 | 0.044 |
| 90.00 | -15.35 | -1.02 | 0.00 | -76.15 | 0.00 | 76.15 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 1.45 | -0.17 | -0.17 | 0.044 |
| 95.00 | -14.66 | -1.02 | 0.00 | -71.05 | 0.00 | 71.05 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 1.63 | -0.19 | -0.19 | 0.043 |
| 100.00 | -13.99 | -1.02 | 0.00 | -65.93 | 0.00 | 65.93 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 1.84 | -0.20 | -0.20 | 0.042 |
| 105.00 | -13.33 | -1.03 | 0.00 | -60.81 | 0.00 | 60.81 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 2.06 | -0.22 | -0.22 | 0.041 |
| 110.00 | -12.70 | -1.03 | 0.00 | -55.68 | 0.00 | 55.68 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 2.30 | -0.24 | -0.24 | 0.040 |
| 115.00 | -12.08 | -1.03 | 0.00 | -50.54 | 0.00 | 50.54 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 2.56 | -0.25 | -0.25 | 0.039 |
| 119.00 | -11.59 | -1.03 | 0.00 | -46.43 | 0.00 | 46.43 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 2.77 | -0.27 | -0.27 | 0.037 |
| 120.00 | -11.40 | -1.03 | 0.00 | -45.41 | 0.00 | 45.41 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 2.83 | -0.27 | -0.27 | 0.037 |
| 123.00 | -10.82 | -1.03 | 0.00 | -42.32 | 0.00 | 42.32 | 1577.63 | 788.82 | 1975.86 | 989.40 | 3.00 | -0.28 | -0.28 | 0.050 |
| 125.00 | -10.62 | -1.03 | 0.00 | -40.27 | 0.00 | 40.27 | 1561.09 | 780.55 | 1925.40 | 964.13 | 3.12 | -0.29 | -0.29 | 0.049 |
| 130.00 | -10.13 | -1.03 | 0.00 | -35.13 | 0.00 | 35.13 | 1518.76 | 759.38 | 1800.86 | 901.77 | 3.44 | -0.31 | -0.31 | 0.046 |
| 135.00 | -9.66 | -1.03 | 0.00 | -29.98 | 0.00 | 29.98 | 1475.03 | 737.52 | 1678.77 | 840.64 | 3.77 | -0.33 | -0.33 | 0.042 |
| 140.00 | -7.18 | -0.99 | 0.00 | -24.83 | 0.00 | 24.83 | 1429.92 | 714.96 | 1559.34 | 780.83 | 4.12 | -0.35 | -0.35 | 0.037 |
| 145.00 | -6.79 | -0.97 | 0.00 | -19.90 | 0.00 | 19.90 | 1383.42 | 691.71 | 1442.75 | 722.45 | 4.49 | -0.36 | -0.36 | 0.032 |
| 150.00 | -6.41 | -0.95 | 0.00 | -15.03 | 0.00 | 15.03 | 1321.23 | 660.61 | 1314.97 | 658.46 | 4.88 | -0.38 | -0.38 | 0.028 |
| 155.00 | -6.05 | -0.93 | 0.00 | -10.26 | 0.00 | 10.26 | 1258.65 | 629.32 | 1192.75 | 597.26 | 5.28 | -0.39 | -0.39 | 0.022 |
| 157.00 | -2.38 | -0.52 | 0.00 | -8.41 | 0.00 | 8.41 | 1233.62 | 616.81 | 1145.53 | 573.62 | 5.45 | -0.39 | -0.39 | 0.017 |
| 160.00 | -2.18 | -0.50 | 0.00 | -6.86 | 0.00 | 6.86 | 1196.07 | 598.03 | 1076.49 | 539.05 | 5.70 | -0.40 | -0.40 | 0.015 |
| 161.00 | -2.11 | -0.49 | 0.00 | -6.36 | 0.00 | 6.36 | 1183.55 | 591.78 | 1053.96 | 527.76 | 5.78 | -0.40 | -0.40 | 0.014 |
| 161.00 | -2.11 | -0.49 | 0.00 | -6.36 | 0.00 | 6.36 | 858.57 | 429.28 | 768.96 | 385.05 | 5.78 | -0.40 | -0.40 | 0.019 |
| 165.00 | -1.91 | -0.46 | 0.00 | -4.41 | 0.00 | 4.41 | 832.45 | 416.23 | 713.85 | 357.46 | 6.12 | -0.41 | -0.41 | 0.015 |
| 170.00 | -1.66 | -0.42 | 0.00 | -2.10 | 0.00 | 2.10 | 798.56 | 399.28 | 646.76 | 323.86 | 6.55 | -0.41 | -0.41 | 0.009 |
| 175.00 | 0.00 | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 6.98 | -0.42 | -0.42 | 0.000 |

Wind Loading - Shaft

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1
Topography: 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.0D + 1.0W 60 mph Wind

Dead Load Factor 1.00
Wind Load Factor 1.00



| Elev (ft) | Description | Kzt | Kz | qz (psf) | qzGh (psf) | C (mph-ft) | Cf | Ice Thick (in) | Tributary (ft) | Aa (sf) | CfAa (sf) | Wind Force X (lb) | Dead Load Ice (lb) | Tot Dead Load (lb) |
|------------------------|-------------|------|------|----------|------------|------------|-------|----------------|----------------|---------|-----------|-------------------|--------------------|--------------------|
| 0.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 242.25 | 0.650 | 0.000 | 0.00 | 0.000 | 0.00 | 0.0 | 0.0 | 0.0 |
| 5.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 237.37 | 0.650 | 0.000 | 5.00 | 23.886 | 15.53 | 104.7 | 0.0 | 1510.8 |
| 10.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 232.48 | 0.650 | 0.000 | 5.00 | 23.399 | 15.21 | 102.5 | 0.0 | 1479.7 |
| 15.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 227.60 | 0.650 | 0.000 | 5.00 | 22.913 | 14.89 | 100.4 | 0.0 | 1448.7 |
| 20.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 222.71 | 0.650 | 0.000 | 5.00 | 22.426 | 14.58 | 98.3 | 0.0 | 1417.6 |
| 25.00 | | 1.00 | 0.70 | 6.129 | 6.74 | 217.83 | 0.650 | 0.000 | 5.00 | 21.940 | 14.26 | 96.1 | 0.0 | 1386.6 |
| 30.00 | | 1.00 | 0.70 | 6.134 | 6.75 | 213.03 | 0.650 | 0.000 | 5.00 | 21.453 | 13.94 | 94.1 | 0.0 | 1355.5 |
| 35.00 | | 1.00 | 0.73 | 6.410 | 7.05 | 212.78 | 0.650 | 0.000 | 5.00 | 20.966 | 13.63 | 96.1 | 0.0 | 1324.5 |
| 38.75 Bot - Section 2 | | 1.00 | 0.75 | 6.599 | 7.26 | 212.10 | 0.650 | 0.000 | 3.75 | 15.406 | 10.01 | 72.7 | 0.0 | 973.0 |
| 40.00 | | 1.00 | 0.76 | 6.659 | 7.33 | 211.79 | 0.650 | 0.000 | 1.25 | 5.167 | 3.36 | 24.6 | 0.0 | 606.4 |
| 45.00 Top - Section 1 | | 1.00 | 0.79 | 6.887 | 7.58 | 210.20 | 0.650 | 0.000 | 5.00 | 20.364 | 13.24 | 100.3 | 0.0 | 2389.1 |
| 50.00 | | 1.00 | 0.81 | 7.098 | 7.81 | 212.13 | 0.650 | 0.000 | 5.00 | 19.877 | 12.92 | 100.9 | 0.0 | 1099.6 |
| 55.00 | | 1.00 | 0.83 | 7.294 | 8.02 | 209.71 | 0.650 | 0.000 | 5.00 | 19.390 | 12.60 | 101.1 | 0.0 | 1072.4 |
| 60.00 | | 1.00 | 0.85 | 7.477 | 8.22 | 206.94 | 0.650 | 0.000 | 5.00 | 18.904 | 12.29 | 101.1 | 0.0 | 1045.2 |
| 65.00 | | 1.00 | 0.87 | 7.650 | 8.42 | 203.86 | 0.650 | 0.000 | 5.00 | 18.417 | 11.97 | 100.7 | 0.0 | 1018.1 |
| 70.00 | | 1.00 | 0.89 | 7.814 | 8.60 | 200.52 | 0.650 | 0.000 | 5.00 | 17.931 | 11.65 | 100.2 | 0.0 | 990.9 |
| 75.00 Appurtenance(s) | | 1.00 | 0.91 | 7.969 | 8.77 | 196.93 | 0.650 | 0.000 | 5.00 | 17.444 | 11.34 | 99.4 | 0.0 | 963.7 |
| 78.75 Bot - Section 3 | | 1.00 | 0.92 | 8.081 | 8.89 | 194.10 | 0.650 | 0.000 | 3.75 | 12.764 | 8.30 | 73.8 | 0.0 | 705.0 |
| 80.00 | | 1.00 | 0.93 | 8.118 | 8.93 | 193.13 | 0.650 | 0.000 | 1.25 | 4.260 | 2.77 | 24.7 | 0.0 | 400.2 |
| 83.75 Top - Section 2 | | 1.00 | 0.94 | 8.225 | 9.05 | 190.16 | 0.650 | 0.000 | 3.75 | 12.597 | 8.19 | 74.1 | 0.0 | 1183.1 |
| 85.00 | | 1.00 | 0.94 | 8.260 | 9.09 | 192.22 | 0.650 | 0.000 | 1.25 | 4.138 | 2.69 | 24.4 | 0.0 | 163.7 |
| 90.00 | | 1.00 | 0.96 | 8.396 | 9.24 | 188.08 | 0.650 | 0.000 | 5.00 | 16.249 | 10.56 | 97.5 | 0.0 | 642.8 |
| 95.00 | | 1.00 | 0.97 | 8.526 | 9.38 | 183.78 | 0.650 | 0.000 | 5.00 | 15.762 | 10.25 | 96.1 | 0.0 | 623.4 |
| 100.00 | | 1.00 | 0.99 | 8.652 | 9.52 | 179.33 | 0.650 | 0.000 | 5.00 | 15.276 | 9.93 | 94.5 | 0.0 | 604.0 |
| 105.00 | | 1.00 | 1.00 | 8.774 | 9.65 | 174.74 | 0.650 | 0.000 | 5.00 | 14.789 | 9.61 | 92.8 | 0.0 | 584.6 |
| 110.00 | | 1.00 | 1.02 | 8.891 | 9.78 | 170.02 | 0.650 | 0.000 | 5.00 | 14.303 | 9.30 | 90.9 | 0.0 | 565.2 |
| 115.00 | | 1.00 | 1.03 | 9.005 | 9.91 | 165.18 | 0.650 | 0.000 | 5.00 | 13.816 | 8.98 | 89.0 | 0.0 | 545.8 |
| 119.00 Bot - Section 4 | | 1.00 | 1.04 | 9.093 | 10.00 | 161.23 | 0.650 | 0.000 | 4.00 | 10.703 | 6.96 | 69.6 | 0.0 | 422.7 |
| 120.00 | | 1.00 | 1.04 | 9.115 | 10.03 | 160.23 | 0.650 | 0.000 | 1.00 | 2.669 | 1.74 | 17.4 | 0.0 | 188.2 |
| 123.00 Top - Section 3 | | 1.00 | 1.05 | 9.179 | 10.10 | 157.21 | 0.650 | 0.000 | 3.00 | 7.891 | 5.13 | 51.8 | 0.0 | 556.3 |
| 125.00 | | 1.00 | 1.05 | 9.222 | 10.14 | 157.78 | 0.650 | 0.000 | 2.00 | 5.163 | 3.36 | 34.0 | 0.0 | 163.4 |
| 130.00 | | 1.00 | 1.07 | 9.326 | 10.26 | 152.64 | 0.650 | 0.000 | 5.00 | 12.568 | 8.17 | 83.8 | 0.0 | 397.6 |
| 135.00 | | 1.00 | 1.08 | 9.427 | 10.37 | 147.41 | 0.650 | 0.000 | 5.00 | 12.081 | 7.85 | 81.4 | 0.0 | 382.1 |
| 140.00 Appurtenance(s) | | 1.00 | 1.09 | 9.525 | 10.48 | 142.08 | 0.650 | 0.000 | 5.00 | 11.595 | 7.54 | 79.0 | 0.0 | 366.6 |
| 145.00 | | 1.00 | 1.10 | 9.621 | 10.58 | 136.68 | 0.650 | 0.000 | 5.00 | 11.108 | 7.22 | 76.4 | 0.0 | 351.1 |
| 150.00 | | 1.00 | 1.11 | 9.715 | 10.69 | 131.19 | 0.650 | 0.000 | 5.00 | 10.622 | 6.90 | 73.8 | 0.0 | 335.5 |
| 155.00 | | 1.00 | 1.12 | 9.806 | 10.79 | 125.63 | 0.650 | 0.000 | 5.00 | 10.135 | 6.59 | 71.1 | 0.0 | 320.0 |
| 157.00 Appurtenance(s) | | 1.00 | 1.12 | 9.842 | 10.83 | 123.38 | 0.650 | 0.000 | 2.00 | 3.918 | 2.55 | 27.6 | 0.0 | 123.7 |
| 160.00 | | 1.00 | 1.13 | 9.896 | 10.89 | 119.99 | 0.650 | 0.000 | 3.00 | 5.731 | 3.73 | 40.5 | 0.0 | 180.8 |
| 161.00 Top - Section 4 | | 1.00 | 1.13 | 9.913 | 10.90 | 118.85 | 0.650 | 0.000 | 1.00 | 1.871 | 1.22 | 13.3 | 0.0 | 59.0 |
| 165.00 | | 1.00 | 1.14 | 9.983 | 10.98 | 114.28 | 0.650 | 0.000 | 4.00 | 7.291 | 4.74 | 52.0 | 0.0 | 173.0 |
| 170.00 | | 1.00 | 1.15 | 10.069 | 11.08 | 108.51 | 0.650 | 0.000 | 5.00 | 8.676 | 5.64 | 62.5 | 0.0 | 205.7 |
| 175.00 Appurtenance(s) | | 1.00 | 1.16 | 10.152 | 11.17 | 102.67 | 0.650 | 0.000 | 5.00 | 8.189 | 5.32 | 59.4 | 0.0 | 194.1 |

Totals: 175.00 3,144.5 30,519.4

Discrete Appurtenance Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.0D + 1.0W 60 mph Wind

Dead Load Factor 1.00
Wind Load Factor 1.00



Iterations

24

| No. | Elev (ft) | Description | Qty | qz (psf) | qzGh (psf) | CaAa x Ka | Ka | Total CaAa (sf) | Dead Load (lb) | Horiz Ecc (ft) | Vert Ecc (ft) | Wind FX (lb) | Mom Y (lb-ft) | Mom Z (lb-ft) |
|-----|-----------|---------------------------|-----|----------|------------|-----------|------|-----------------|----------------|----------------|---------------|--------------|---------------|---------------|
| 1 | 175.00 | Low Profile Platform-flat | 1 | 10.152 | 11.168 | 1.00 | 1.00 | 25.00 | 1200.00 | 0.000 | 0.000 | 279.19 | 0.00 | 0.00 |
| 2 | 175.00 | DB-T1-6Z-8AB-0Z | 1 | 10.152 | 11.168 | 0.71 | 1.00 | 3.41 | 18.90 | 0.000 | 0.000 | 38.06 | 0.00 | 0.00 |
| 3 | 175.00 | FD9R6004/2C-3L (3.1 lbs) | 6 | 10.152 | 11.168 | 0.67 | 1.00 | 1.45 | 18.60 | 0.000 | 0.000 | 16.16 | 0.00 | 0.00 |
| 4 | 175.00 | RRH2x40-AWS | 3 | 10.152 | 11.168 | 0.82 | 1.00 | 6.20 | 132.00 | 0.000 | 0.000 | 69.23 | 0.00 | 0.00 |
| 5 | 175.00 | BXA-70080/6CF | 3 | 10.152 | 11.168 | 0.88 | 1.00 | 15.42 | 54.00 | 0.000 | 0.000 | 172.18 | 0.00 | 0.00 |
| 6 | 175.00 | WBX065X19R050 | 3 | 10.152 | 11.168 | 0.72 | 1.00 | 11.28 | 62.70 | 0.000 | 0.000 | 125.92 | 0.00 | 0.00 |
| 7 | 175.00 | BXA-171085/12CF | 3 | 10.152 | 11.168 | 0.84 | 1.00 | 12.05 | 45.00 | 0.000 | 0.000 | 134.52 | 0.00 | 0.00 |
| 8 | 175.00 | BXA-70063/6CF | 3 | 10.152 | 11.168 | 0.70 | 1.00 | 15.90 | 51.00 | 0.000 | 0.000 | 177.53 | 0.00 | 0.00 |
| 9 | 175.00 | 6' Lightning rod | 1 | 10.152 | 11.168 | 1.00 | 1.00 | 0.38 | 6.50 | 0.000 | 0.000 | 4.24 | 0.00 | 0.00 |
| 10 | 157.00 | ALU - TD-RRH8x20-25 - | 3 | 9.842 | 10.827 | 0.60 | 0.80 | 7.29 | 210.00 | 0.000 | 0.000 | 78.93 | 0.00 | 0.00 |
| 11 | 157.00 | ALU - 800 MHz - RRU | 6 | 9.842 | 10.827 | 0.60 | 0.80 | 8.96 | 318.00 | 0.000 | 0.000 | 97.05 | 0.00 | 0.00 |
| 12 | 157.00 | ALU - 1900 MHz - RRU | 3 | 9.842 | 10.827 | 0.60 | 0.80 | 4.99 | 180.00 | 0.000 | 0.000 | 53.98 | 0.00 | 0.00 |
| 13 | 157.00 | NNVV-65B-R4 | 3 | 9.842 | 10.827 | 0.59 | 0.80 | 21.79 | 254.10 | 0.000 | 0.000 | 235.93 | 0.00 | 0.00 |
| 14 | 157.00 | APXVTM14-C-I20 | 3 | 9.842 | 10.827 | 0.62 | 0.80 | 11.72 | 168.60 | 0.000 | 0.000 | 126.85 | 0.00 | 0.00 |
| 15 | 157.00 | Platform w/ Handrail + | 1 | 9.842 | 10.827 | 1.00 | 1.00 | 54.00 | 2800.00 | 0.000 | 0.000 | 584.63 | 0.00 | 0.00 |
| 16 | 140.00 | Platform w/ Hand Rails | 1 | 9.525 | 10.478 | 1.00 | 1.00 | 40.00 | 2000.00 | 0.000 | 0.000 | 419.11 | 0.00 | 0.00 |
| 17 | 140.00 | 782 11056 | 3 | 9.525 | 10.478 | 0.62 | 0.80 | 0.24 | 5.40 | 0.000 | 0.000 | 2.55 | 0.00 | 0.00 |
| 18 | 140.00 | KRY 112 144/1 | 3 | 9.525 | 10.478 | 0.58 | 0.80 | 0.72 | 33.00 | 0.000 | 0.000 | 7.53 | 0.00 | 0.00 |
| 19 | 140.00 | LNX-6515DS-VTM | 3 | 9.525 | 10.478 | 0.64 | 0.80 | 22.02 | 150.90 | 0.000 | 0.000 | 230.75 | 0.00 | 0.00 |
| 20 | 140.00 | APXV18-206516S-C-A20 | 3 | 9.525 | 10.478 | 0.58 | 0.80 | 6.32 | 56.10 | 0.000 | 0.000 | 66.27 | 0.00 | 0.00 |
| 21 | 75.00 | GPS | 1 | 7.969 | 8.766 | 1.00 | 1.00 | 1.00 | 10.00 | 0.000 | 0.000 | 8.77 | 0.00 | 0.00 |

Totals: 7,774.80

2,929.35

Total Applied Force Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

5/23/2018



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Load Case: 1.0D + 1.0W 60 mph Wind

Dead Load Factor 1.00
Wind Load Factor 1.00



| Elev (ft) | Description | Lateral FX (-) (lb) | Axial FY (-) (lb) | Torsion MY (lb-ft) | Moment MZ (lb-ft) |
|-----------|------------------|---------------------|-------------------|--------------------|-------------------|
| 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | | 104.67 | 1655.09 | 0.00 | 0.00 |
| 10.00 | | 102.53 | 1624.04 | 0.00 | 0.00 |
| 15.00 | | 100.40 | 1592.99 | 0.00 | 0.00 |
| 20.00 | | 98.27 | 1561.94 | 0.00 | 0.00 |
| 25.00 | | 96.14 | 1530.89 | 0.00 | 0.00 |
| 30.00 | | 94.09 | 1499.84 | 0.00 | 0.00 |
| 35.00 | | 96.09 | 1468.79 | 0.00 | 0.00 |
| 38.75 | | 72.69 | 1081.21 | 0.00 | 0.00 |
| 40.00 | | 24.60 | 642.45 | 0.00 | 0.00 |
| 45.00 | | 100.28 | 2533.43 | 0.00 | 0.00 |
| 50.00 | | 100.87 | 1243.87 | 0.00 | 0.00 |
| 55.00 | | 101.12 | 1216.70 | 0.00 | 0.00 |
| 60.00 | | 101.06 | 1189.53 | 0.00 | 0.00 |
| 65.00 | | 100.74 | 1162.36 | 0.00 | 0.00 |
| 70.00 | | 100.18 | 1135.19 | 0.00 | 0.00 |
| 75.00 | (1) attachments | 108.17 | 1118.03 | 0.00 | 0.00 |
| 78.75 | | 73.75 | 812.59 | 0.00 | 0.00 |
| 80.00 | | 24.73 | 436.05 | 0.00 | 0.00 |
| 83.75 | | 74.08 | 1290.70 | 0.00 | 0.00 |
| 85.00 | | 24.44 | 199.61 | 0.00 | 0.00 |
| 90.00 | | 97.54 | 786.31 | 0.00 | 0.00 |
| 95.00 | | 96.09 | 766.91 | 0.00 | 0.00 |
| 100.00 | | 94.50 | 747.50 | 0.00 | 0.00 |
| 105.00 | | 92.78 | 728.09 | 0.00 | 0.00 |
| 110.00 | | 90.92 | 708.69 | 0.00 | 0.00 |
| 115.00 | | 88.95 | 689.28 | 0.00 | 0.00 |
| 119.00 | | 69.58 | 537.45 | 0.00 | 0.00 |
| 120.00 | | 17.40 | 216.92 | 0.00 | 0.00 |
| 123.00 | | 51.79 | 642.37 | 0.00 | 0.00 |
| 125.00 | | 34.05 | 220.80 | 0.00 | 0.00 |
| 130.00 | | 83.80 | 541.14 | 0.00 | 0.00 |
| 135.00 | | 81.43 | 525.62 | 0.00 | 0.00 |
| 140.00 | (13) attachments | 805.17 | 2755.49 | 0.00 | 0.00 |
| 145.00 | | 76.42 | 432.17 | 0.00 | 0.00 |
| 150.00 | | 73.78 | 416.64 | 0.00 | 0.00 |
| 155.00 | | 71.06 | 401.12 | 0.00 | 0.00 |
| 157.00 | (19) attachments | 1204.93 | 4086.80 | 0.00 | 0.00 |
| 160.00 | | 40.55 | 221.57 | 0.00 | 0.00 |
| 161.00 | | 13.26 | 72.62 | 0.00 | 0.00 |
| 165.00 | | 52.04 | 227.28 | 0.00 | 0.00 |
| 170.00 | | 62.46 | 273.62 | 0.00 | 0.00 |
| 175.00 | (24) attachments | 1076.47 | 1850.67 | 0.00 | 0.00 |
| | Totals: | 6,073.86 | 42,844.37 | 0.00 | 0.00 |

Calculated Forces

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Load Case: 1.0D + 1.0W 60 mph Wind

Dead Load Factor 1.00
Wind Load Factor 1.00



Iterations 24

| Seg Elev (ft) | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Total Deflect (in) | Rotation Sway (deg) | Rotation Twist (deg) | Stress Ratio |
|---------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|--------------------|---------------------|----------------------|--------------|
| 0.00 | -42.84 | -6.08 | 0.00 | -754.03 | 0.00 | 754.03 | 6411.04 | 3205.52 | 14877.2 | 7449.66 | 0.00 | 0.000 | 0.000 | 0.108 |
| 5.00 | -41.18 | -6.00 | 0.00 | -723.61 | 0.00 | 723.61 | 6318.35 | 3159.17 | 14361.2 | 7191.28 | 0.02 | -0.029 | 0.000 | 0.107 |
| 10.00 | -39.56 | -5.92 | 0.00 | -693.61 | 0.00 | 693.61 | 6224.09 | 3112.04 | 13850.5 | 6935.58 | 0.06 | -0.059 | 0.000 | 0.106 |
| 15.00 | -37.96 | -5.83 | 0.00 | -664.02 | 0.00 | 664.02 | 6128.26 | 3064.13 | 13345.4 | 6682.66 | 0.14 | -0.089 | 0.000 | 0.106 |
| 20.00 | -36.40 | -5.75 | 0.00 | -634.85 | 0.00 | 634.85 | 6030.87 | 3015.43 | 12846.2 | 6432.65 | 0.25 | -0.120 | 0.000 | 0.105 |
| 25.00 | -34.86 | -5.67 | 0.00 | -606.08 | 0.00 | 606.08 | 5931.91 | 2965.95 | 12352.9 | 6185.64 | 0.39 | -0.151 | 0.000 | 0.104 |
| 30.00 | -33.36 | -5.59 | 0.00 | -577.71 | 0.00 | 577.71 | 5831.38 | 2915.69 | 11865.8 | 5941.76 | 0.57 | -0.183 | 0.000 | 0.103 |
| 35.00 | -31.89 | -5.51 | 0.00 | -549.75 | 0.00 | 549.75 | 5715.88 | 2857.94 | 11358.6 | 5687.79 | 0.78 | -0.216 | 0.000 | 0.102 |
| 38.75 | -30.81 | -5.44 | 0.00 | -529.09 | 0.00 | 529.09 | 5614.19 | 2807.10 | 10956.1 | 5486.19 | 0.96 | -0.241 | 0.000 | 0.102 |
| 40.00 | -30.16 | -5.42 | 0.00 | -522.29 | 0.00 | 522.29 | 5580.30 | 2790.15 | 10823.5 | 5419.80 | 1.02 | -0.250 | 0.000 | 0.102 |
| 45.00 | -27.63 | -5.33 | 0.00 | -495.17 | 0.00 | 495.17 | 4741.11 | 2370.56 | 9166.15 | 4589.89 | 1.30 | -0.284 | 0.000 | 0.114 |
| 50.00 | -26.38 | -5.24 | 0.00 | -468.53 | 0.00 | 468.53 | 4656.71 | 2328.36 | 8781.22 | 4397.14 | 1.62 | -0.318 | 0.000 | 0.112 |
| 55.00 | -25.16 | -5.15 | 0.00 | -442.34 | 0.00 | 442.34 | 4570.75 | 2285.37 | 8401.44 | 4206.97 | 1.97 | -0.356 | 0.000 | 0.111 |
| 60.00 | -23.97 | -5.05 | 0.00 | -416.60 | 0.00 | 416.60 | 4483.21 | 2241.61 | 8027.05 | 4019.49 | 2.36 | -0.395 | 0.000 | 0.109 |
| 65.00 | -22.80 | -4.96 | 0.00 | -391.33 | 0.00 | 391.33 | 4386.28 | 2193.14 | 7644.63 | 3828.00 | 2.80 | -0.434 | 0.000 | 0.107 |
| 70.00 | -21.66 | -4.87 | 0.00 | -366.53 | 0.00 | 366.53 | 4267.64 | 2133.82 | 7234.64 | 3622.70 | 3.27 | -0.474 | 0.000 | 0.106 |
| 75.00 | -20.54 | -4.76 | 0.00 | -342.19 | 0.00 | 342.19 | 4149.01 | 2074.50 | 6835.94 | 3423.05 | 3.79 | -0.515 | 0.000 | 0.105 |
| 78.75 | -19.73 | -4.69 | 0.00 | -324.34 | 0.00 | 324.34 | 4060.03 | 2030.01 | 6544.34 | 3277.03 | 4.21 | -0.546 | 0.000 | 0.104 |
| 80.00 | -19.29 | -4.67 | 0.00 | -318.48 | 0.00 | 318.48 | 4030.37 | 2015.18 | 6448.55 | 3229.07 | 4.35 | -0.557 | 0.000 | 0.103 |
| 83.75 | -18.00 | -4.59 | 0.00 | -300.98 | 0.00 | 300.98 | 2677.54 | 1338.77 | 4285.17 | 2145.77 | 4.81 | -0.588 | 0.000 | 0.147 |
| 85.00 | -17.80 | -4.57 | 0.00 | -295.25 | 0.00 | 295.25 | 2664.37 | 1332.18 | 4232.36 | 2119.33 | 4.96 | -0.599 | 0.000 | 0.146 |
| 90.00 | -17.01 | -4.48 | 0.00 | -272.40 | 0.00 | 272.40 | 2610.69 | 1305.34 | 4022.76 | 2014.37 | 5.62 | -0.655 | 0.000 | 0.142 |
| 95.00 | -16.24 | -4.39 | 0.00 | -250.00 | 0.00 | 250.00 | 2555.44 | 1277.72 | 3815.94 | 1910.80 | 6.33 | -0.711 | 0.000 | 0.137 |
| 100.00 | -15.49 | -4.30 | 0.00 | -228.04 | 0.00 | 228.04 | 2498.62 | 1249.31 | 3612.11 | 1808.74 | 7.11 | -0.768 | 0.000 | 0.132 |
| 105.00 | -14.76 | -4.21 | 0.00 | -206.53 | 0.00 | 206.53 | 2440.24 | 1220.12 | 3411.50 | 1708.29 | 7.94 | -0.824 | 0.000 | 0.127 |
| 110.00 | -14.05 | -4.13 | 0.00 | -185.47 | 0.00 | 185.47 | 2380.29 | 1190.15 | 3214.34 | 1609.56 | 8.84 | -0.880 | 0.000 | 0.121 |
| 115.00 | -13.36 | -4.04 | 0.00 | -164.84 | 0.00 | 164.84 | 2318.78 | 1159.39 | 3020.85 | 1512.67 | 9.79 | -0.936 | 0.000 | 0.115 |
| 119.00 | -12.82 | -3.97 | 0.00 | -148.69 | 0.00 | 148.69 | 2268.44 | 1134.22 | 2868.85 | 1436.56 | 10.59 | -0.980 | 0.000 | 0.109 |
| 120.00 | -12.60 | -3.95 | 0.00 | -144.72 | 0.00 | 144.72 | 2255.69 | 1127.85 | 2831.25 | 1417.73 | 10.80 | -0.992 | 0.000 | 0.108 |
| 123.00 | -11.96 | -3.89 | 0.00 | -132.87 | 0.00 | 132.87 | 1577.63 | 788.82 | 1975.86 | 989.40 | 11.43 | -1.025 | 0.000 | 0.142 |
| 125.00 | -11.73 | -3.86 | 0.00 | -125.09 | 0.00 | 125.09 | 1561.09 | 780.55 | 1925.40 | 964.13 | 11.87 | -1.047 | 0.000 | 0.137 |
| 130.00 | -11.19 | -3.78 | 0.00 | -105.78 | 0.00 | 105.78 | 1518.76 | 759.38 | 1800.86 | 901.77 | 13.00 | -1.107 | 0.000 | 0.125 |
| 135.00 | -10.66 | -3.70 | 0.00 | -86.88 | 0.00 | 86.88 | 1475.03 | 737.52 | 1678.77 | 840.64 | 14.19 | -1.164 | 0.000 | 0.111 |
| 140.00 | -7.92 | -2.84 | 0.00 | -68.39 | 0.00 | 68.39 | 1429.92 | 714.96 | 1559.34 | 780.83 | 15.44 | -1.216 | 0.000 | 0.093 |
| 145.00 | -7.49 | -2.76 | 0.00 | -54.17 | 0.00 | 54.17 | 1383.42 | 691.71 | 1442.75 | 722.45 | 16.73 | -1.262 | 0.000 | 0.080 |
| 150.00 | -7.07 | -2.68 | 0.00 | -40.36 | 0.00 | 40.36 | 1321.23 | 660.61 | 1314.97 | 658.46 | 18.08 | -1.303 | 0.000 | 0.067 |
| 155.00 | -6.67 | -2.61 | 0.00 | -26.94 | 0.00 | 26.94 | 1258.65 | 629.32 | 1192.75 | 597.26 | 19.46 | -1.336 | 0.000 | 0.050 |
| 157.00 | -2.62 | -1.31 | 0.00 | -21.73 | 0.00 | 21.73 | 1233.62 | 616.81 | 1145.53 | 573.62 | 20.02 | -1.347 | 0.000 | 0.040 |
| 160.00 | -2.39 | -1.26 | 0.00 | -17.81 | 0.00 | 17.81 | 1196.07 | 598.03 | 1076.49 | 539.05 | 20.87 | -1.362 | 0.000 | 0.035 |
| 161.00 | -2.32 | -1.25 | 0.00 | -16.55 | 0.00 | 16.55 | 1183.55 | 591.78 | 1053.96 | 527.76 | 21.16 | -1.366 | 0.000 | 0.033 |
| 161.00 | -2.32 | -1.25 | 0.00 | -16.55 | 0.00 | 16.55 | 858.57 | 429.28 | 768.96 | 385.05 | 21.16 | -1.366 | 0.000 | 0.046 |
| 165.00 | -2.10 | -1.19 | 0.00 | -11.56 | 0.00 | 11.56 | 832.45 | 416.23 | 713.85 | 357.46 | 22.31 | -1.382 | 0.000 | 0.035 |
| 170.00 | -1.82 | -1.12 | 0.00 | -5.61 | 0.00 | 5.61 | 798.56 | 399.28 | 646.76 | 323.86 | 23.77 | -1.399 | 0.000 | 0.020 |
| 175.00 | 0.00 | -1.08 | 0.00 | 0.00 | 0.00 | 0.00 | 758.80 | 379.40 | 578.42 | 289.64 | 25.24 | -1.406 | 0.000 | 0.000 |

Final Analysis Summary

Structure: CT01915-S-SBA
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Topography: 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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Reactions

| Load Case | Shear FX (kips) | Shear FZ (kips) | Axial FY (kips) | Moment MX (ft-kips) | Moment MY (ft-kips) | Moment MZ (ft-kips) |
|----------------------------------|-----------------|-----------------|-----------------|---------------------|---------------------|---------------------|
| 1.2D + 1.6W 101 mph Wind | 27.6 | 0.00 | 51.38 | 0.00 | 0.00 | 3439.14 |
| 0.9D + 1.6W 101 mph Wind | 27.6 | 0.00 | 38.53 | 0.00 | 0.00 | 3401.64 |
| 1.2D + 1.0Di + 1.0Wi 50 mph Wind | 8.0 | 0.00 | 83.64 | 0.00 | 0.00 | 1026.11 |
| 1.2D + 1.0E | 1.6 | 0.00 | 51.41 | 0.00 | 0.00 | 196.36 |
| 0.9D + 1.0E | 1.6 | 0.00 | 38.56 | 0.00 | 0.00 | 194.12 |
| 1.0D + 1.0W 60 mph Wind | 6.1 | 0.00 | 42.84 | 0.00 | 0.00 | 754.03 |

Max Stresses

| Load Case | Pu FY (-) (kips) | Vu FX (-) (kips) | Tu MY (-) (ft-kips) | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | phi Mn (ft-kips) | Elev (ft) | Stress Ratio |
|----------------------------------|------------------|------------------|---------------------|-----------------|-----------------|----------------------------|---------------|---------------|------------------|------------------|-----------|--------------|
| 1.2D + 1.6W 101 mph Wind | -20.69 | -20.95 | 0.00 | -1375.6 | 0.00 | -1375.6 | 2677.54 | 1338.7 | 4285.17 | 2145.77 | 83.75 | 0.649 |
| 0.9D + 1.6W 101 mph Wind | -15.29 | -20.68 | 0.00 | -1352.9 | 0.00 | -1352.9 | 2677.54 | 1338.7 | 4285.17 | 2145.77 | 83.75 | 0.636 |
| 1.2D + 1.0Di + 1.0Wi 50 mph Wind | -43.39 | -6.27 | 0.00 | -418.31 | 0.00 | -418.31 | 2677.54 | 1338.7 | 4285.17 | 2145.77 | 83.75 | 0.211 |
| 1.2D + 1.0E | -14.43 | -1.05 | 0.00 | -43.01 | 0.00 | -43.01 | 1577.63 | 788.82 | 1975.86 | 989.40 | 123.00 | 0.053 |
| 0.9D + 1.0E | -10.82 | -1.03 | 0.00 | -42.32 | 0.00 | -42.32 | 1577.63 | 788.82 | 1975.86 | 989.40 | 123.00 | 0.050 |
| 1.0D + 1.0W 60 mph Wind | -18.00 | -4.59 | 0.00 | -300.98 | 0.00 | -300.98 | 2677.54 | 1338.7 | 4285.17 | 2145.77 | 83.75 | 0.147 |

Base Plate Summary

Structure: CT01915-S-SB
Site Name: South Brooklyn
Height: 175.00 (ft)
Base Elev: 0.000 (ft)
Gh: 1.1

Topography: 1

Code: EIA/TIA-222-G
Exposure: B
Crest Height: 0.00
Site Class: D - Stiff Soil
Struct Class: II

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| Reactions | | Base Plate | | Anchor Bolts | |
|-------------------------|---------|-----------------------|---------|----------------------------|-----------|
| Original Design | | Yield (ksi): | 50.00 | Bolt Circle: | 64.00 |
| Moment (kip-ft): | 3710.00 | Width (in): | 68.00 | Number Bolts: | 32.00 |
| Axial (kip): | 38.30 | Style: | Clipped | Bolt Type: | 2.25" 18J |
| Shear (kip): | 29.70 | Polygon Sides: | 8.00 | Bolt Diameter (in): | 2.25 |
| Analysis | | Clip Length (in): | 18.50 | Yield (ksi): | 75.00 |
| Moment (kip-ft): | 3439.14 | Effective Len (in): | 6.47 | Ultimate (ksi): | 100.00 |
| Axial (kip): | 83.64 | Moment (kip-in): | 290.02 | Arrangement: | Clustered |
| Shear (kip): | 27.60 | Allow Stress (ksi): | 67.50 | Cluster Dist (in): | 6.00 |
| | | Applied Stress (ksi): | 0.00 | Start Angle (deg): | 45.00 |
| Moment Design %: | 92.70 | Stress Ratio: | 0.64 | Compression | |
| | | | | Force (kip): | 83.22 |
| | | | | Allowable (kip): | 260.00 |
| | | | | Ratio: | 0.33 |
| | | | | Tension | |
| | | | | Force (kip): | 77.99 |
| | | | | Allowable (kip): | 260.00 |
| | | | | Ratio: | 0.31 |



Monopole Mat Foundation Design

Date

5/23/2018

| | | | |
|----------------|---------------|-------------------------|-----------|
| Customer Name: | Sprint Nextel | EIA/TIA Standard: | EIA-222-G |
| Site Name: | | Structure Height (Ft.): | 175 |
| Site Number: | CT01915-S-SBA | Engineer Name: | D. Zhou |
| Engr. Number: | 53618 | Engineer Login ID: | |

Foundation Info Obtained from:

Structure Type:

Monopole

Analysis or Design?

Analysis

Base Reactions (Factored):

Axial Load (Kips):

51.4

Shear Force (Kips):

27.6

Uplift Force (Kips):

0.0

Moment (Kips-ft):

3439.1

Allowable overstress %: 5.0%

Foundation Geometries:

Diameter of Pier (ft.):

8.0

Mods required -Yes/No ?: No

Pier Height A. G. (ft.):

0.50

Depth of Base BG (ft.):

7.0

Length of Pad (ft.):

25

Thickness of Pad (ft.):

3.50

Width of Pad (ft.):

25

Final Length of pad (ft)

25.0

Final width of pad (ft):

25.0

Control Value for Cell D18:

0

Control Value for Cell F18: 0

Material Properties and Rebar Info:

Concrete Strength (psi):

3000

Steel Elastic Modulus:

29000 ksi

Vertical bar yield (ksi)

60

Tie steel yield (ksi):

40

Vertical Rebar Size #:

11

Tie / Stirrup Size #:

5

Qty. of Vertical Rebars:

36

Tie Spacing (in):

6.0

Pad Rebar Yield (Ksi):

60

Pad Steel Rebar Size (#):

9

Concrete Cover (in.):

3

Unit Weight of Concrete:

150.0 pcf

Rebar at the bottom of the concrete pad:

42

Qty. of Rebar in Pad (L):

42

Rebar at the top of the concrete pad:

42

Qty. of Rebar in Pad (W):

42

Apply 1.35 factor for e/w Per G: 1.35

Soil Design Parameters:

Soil Unit Weight (pcf):

125.0

Soil Buoyant Weight:

50.0

Pcf

Water Table B.G.S. (ft.):

7.0

Unit Weight of Water:

62.4

pcf

Angle from Top of Pad:

30

Ultimate Bearing Pressure (psf):

15000

Ultimate Skin Friction:

0

Psf

Angle from Bottom of Pad:

25

Consider Friction for O.T.M. (Y/N):

No

Consider Friction for bearing (Y/N):

No

Angle from Bottom of Pad:

25

Consider soil hori. force for O.T.M.:

No

Reduction factor on the maximum soil bearing pressure:

1.00

Foundation Analysis and Design:

Uplift Strength Reduction Factor:

0.75

Compression Strength Reduction Factor:

0.75

Total Dry Soil Volume (cu. Ft.):

2011.57

Total Dry Soil Weight (Kips):

251.45

Total Buoyant Soil Volume (cu. Ft.):

0.00

Total Buoyant Soil Weight (Kips):

0.00

Total Effective Soil Weight (Kips):

251.45

Weight from the Concrete Block at Top (K):

0.00

Total Dry Concrete Volume (cu. Ft.):

2388.56

Total Dry Concrete Weight (Kips):

358.28

Total Buoyant Concrete Volume (cu. Ft.):

0.00

Total Buoyant Concrete Weight (Kips):

0.00

Total Effective Concrete Weight (Kips):

358.28

Total Vertical Load on Base (Kips):

661.11

Check Soil Capacities:

Calculated Maximum Net Soil Pressure under the base (psf):

3091

<

Allowable Factored Soil Bearing (psf):

11250

0.27

OK!

Allowable Foundation Overturning Resistance (kips-ft.):

7501.7

>

Design Factored Moment (kips-ft.):

3646

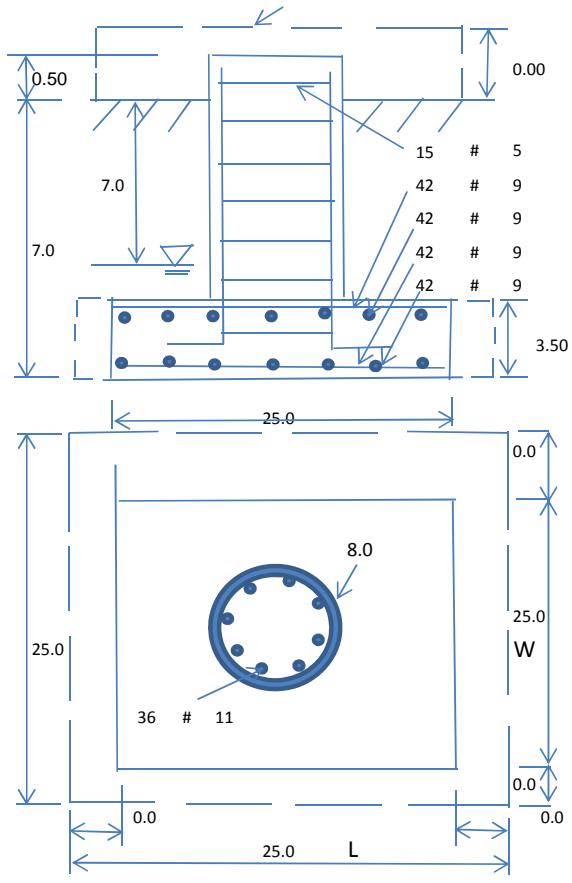
0.49

OK!

Factor of Safety Against Overturning (O. R. Moment/Design Moment):

2.06

OK!



Check the capacities of Reinforcing Concrete:

| | | | | | |
|--|---------|--|--------|------|-----|
| Strength reduction factor (Flexure and axial tension): | 0.90 | Strength reduction factor (Shear): | 0.75 | | |
| Strength reduction factor (Axial compression): | 0.65 | Wind Load Factor on Concrete Design: | 1.00 | | |
| (1) Concrete Pier: | | | | | |
| Vertical Steel Rebar Area (sq. in./each): | 1.56 | Tie / Stirrup Area (sq. in./each): | 0.31 | | |
| Calculated Moment Capacity (Mn,Kips-Ft): | 10388.7 | > Design Factored Moment (Mu, Kips-Ft): | 3549.5 | 0.34 | OK! |
| Calculated Shear Capacity (Kips): | 912.1 | > Design Factored Shear (Kips): | 27.6 | 0.03 | OK! |
| Calculated Tension Capacity (Tn, Kips): | 3032.6 | > Design Factored Tension (Tu Kips): | 0.0 | 0.00 | OK! |
| Calculated Compression Capacity (Pn, Kips): | 9523.4 | > Design Factored Axial Load (Pu Kips): | 51.4 | 0.01 | OK! |
| Moment & Axial Strength Combination: | 0.34 | OK! Check Tie Spacing (Design/Required): | | 0.5 | OK! |
| Pier Reinforcement Ratio: | 0.008 | Reinforcement Ratio is satisfied per ACI | | | |

(2) Concrete Pad:

| | | | | | |
|---|--------|--|--------|------|-----|
| One-Way Design Shear Capacity (L-Direction, Kips): | 947.4 | > One-Way Factored Shear (L-D. Kips): | 272.3 | 0.29 | OK! |
| One-Way Design Shear Capacity (W-Direction, Kips): | 947.4 | > One-Way Factored Shear (W-D., Kips) | 272.3 | 0.29 | OK! |
| One-Way Design Shear Capacity (Corner-Corner, Kips): | 1036.6 | > One-Way Factored Shear (C-C, Kips): | 471.5 | 0.45 | OK! |
| Lower Steel Pad Reinforcement Ratio (L-Direct.): | 0.0036 | OK! Lower Steel Pad Reinf. Ratio (W-Direc | 0.0036 | | |
| Lower Steel Pad Moment Capacity (L-Direction. Kips-ft): | 6953.4 | > Moment at Bottom (L-Direct. K-Ft): | 721.3 | 0.10 | OK! |
| Lower Steel Pad Moment Capacity (W-Direction. Kips-ft): | 6953.4 | > Moment at Bottom (W-Direct. K-Ft): | 721.3 | 0.10 | OK! |
| Lower Steel Pad Moment Capacity (Corner-Corner,K-ft): | 9704.8 | > Moment at Bottom (C-C Dir. K-Ft): | 1020.0 | 0.11 | OK! |
| Upper Steel Pad Reinforcement Ratio (L-Direct.): | 0.0036 | OK! Upper Steel Reinf. Ratio (W-Direct.): | 0.0036 | | |
| Upper Steel Pad Moment Capacity (L-Direction. Kips-ft): | 6953.4 | > Moment at the top (L-Dir Kips-Ft): | 238.9 | 0.03 | OK! |
| Upper Steel Pad Moment Capacity (W-Direction. Kips-ft): | 6953.4 | > Moment at the top (W-Dir Kips-Ft): | 238.9 | 0.03 | OK! |
| Upper Steel Pad Moment Capacity (Corner-Corner. K-ft): | 9704.8 | > Moment at the top (C-C Direc. K-Ft): | 399.0 | 0.04 | OK! |

Antenna Mount Structural Analysis



SBA Site: CT01915-S South Brooklyn
Sprint Site Number: CT33XC566
Project: Sprint DO Macro Upgrade

Prepared For: Sprint

Mount Description: (1) Platform

Site Location: 100 Old Tatnic Hill Rd, Brooklyn, CT
Windham County
41.76716°, -71.971949°

Design Codes: ANSI/TIA-222-G
IBC 2012 w/ 2016 CT Building Code

Analysis Load Case: Sprint Final Configuration

Analysis Result: Adequate @ 80% - Once Augmented
See Conclusion



Revision 0
March 19, 2018

CT33XC566-PASSING-MOUNT-STRUCTURAL-ANALYSIS-03-19-18



GeoStructural • P.O. Box 2621, Boise, ID 83701 • Office: (530) 539-4787
Professional Engineers | Tower Technicians | Climbers | sUAS Mapping

1.0 Introduction

An antenna mount structural analysis has been performed on Sprint's existing mount assembly located at the CT01915-S South Brooklyn communications site in Windham County, CT considering the final equipment loading configuration listed in Section 3.0.

2.0 Analysis Criteria

An elastic three-dimensional model of the mount structure has been analyzed pursuant to the following criteria:

- IBC 2012 – International Building Code.
- ANSI/TIA-222-G – Structural Standard for Antenna Supporting Structures and Antennas.
- AISC – Steel Construction Manual.
- ANSI/AWS D1.1 – Structural Welding Code.

| | |
|---|--|
| Wind w/o ice = 130 mph (3-sec gust Ultimate Wind Speed) | |
| Wind w/o ice = 101 mph (3-sec gust Equivalent per TIA-222-G Tower Code) | |
| Wind with ice = 50 mph (3-sec gust, 1" Ice) Exposure Category B | Topographic Category 1 Structure Class II |

The following documents were provided:

- Mount and Tower Record Documents
SBA
- Tower Structural Analysis
TES, 1/9/18.
- RF Design
Sprint DOMU Project

The results of the analysis are illustrated in Section 4.0. If any of the existing or proposed conditions reported in this analysis are not properly represented, please contact our office immediately to request an amended report.

3.0 Appurtenance Information

Table 3.1 – Sprint Final Configuration¹

| COR | (Quantity) Appurtenance Make/Model | Mount Description |
|---------|------------------------------------|-------------------|
| 157.0'± | (3) RFS APXVTM14-ALU-I20 | (1) Platform |
| | (3) COMMSCOPE NNVV-65B-R4 | |
| | (6) ALU 800MHz RRH | |
| | (3) ALU 1900MHz RRH | |
| | (3) ALU 2500MHz RRH | |

1. Refer to antenna installation Construction Drawings (by others, when applicable) for additional information regarding final antenna and equipment orientations.
2. Panel antennas to be installed in Positions 1 and 3 (as close to the center of face near existing standoff as possible. RRH units to be installed on dual swivel brackets behind panel antennas in Positions 1 and 3.

4.0 Analysis Results

Table 4.1 – Existing Mount Capacity

| Load Case | Governing Mount Component ¹ | % Capacity ² | Result |
|----------------------------|--|-------------------------|-------------------------|
| Final Sprint Configuration | Angle Rail | 165% | Inadequate ³ |

1. Refer to the Calculations & Software Output portion of this report for mount component and structural information.
2. Listed results are expressed as a percentage of available mount member capacity based upon the assumed material strengths listed in Table 4.3. 105% is an acceptable allowable stress percentage for mount components.
3. Structural augments to the existing mount structure are required to obtain a mount structure capable of supporting the currently proposed final loading configuration in Table 3.1.

Table 4.2 – Augmented Mount Capacity

| Load Case | Governing Mount Component ¹ | % Capacity ² | Result |
|----------------------------|--|-------------------------|--------------------------------------|
| Final Sprint Configuration | Angle Rail | 80% | Adequate Once Augmented ³ |

1. Refer to the Calculations & Software Output portion of this report for mount component and structural information.
2. Listed results are expressed as a percentage of available mount member capacity based upon the assumed material strengths listed in Table 4.3. 105% is an acceptable allowable stress percentage for mount components.
3. Refer to [GeoStructural Mount Augmentation Drawings](#) and Section 5.0 for information regarding required mount augments.

Table 4.3 – Structural Component Material Strengths

| Structural Component | Nominal Strength/Material ¹ |
|--|---|
| Pipe | $F_y = 35$ ksi (A53, Gr. B) |
| Tube | $F_y = 46$ ksi (A500, Gr. B) |
| Structural Shapes (L, C, W, etc.), Plate / Bar | $F_y = 36$ ksi (A36) |
| Uni-Strut | $F_y = 33$ ksi (A570, Gr. 33) |
| Connection Bolts | A325 |
| Stainless Steel Bolts | 18-8 Stainless, Grade 316/304 $F_y = 74$ ksi (Yield) & $F_u = 29$ ksi (Tension) |
| U-Bolts / Threaded Rod | SAE J429 Grade 2 (Substitution: ASTM A449) $F_y = 57$ ksi (Yield) & $F_u = 74$ ksi (Tension) |
| Welds | E70XX Electrodes |

1. Strengths listed were assumed for this analysis and are based upon ASTM, AISC, RCSC, AWS and ACI preferred specification values. Values and materials are consistent with industry standards. Material strengths were taken from original design documents when available.

5.0 Conclusion & Recommendations

Based on Sprint's final equipment loading configuration, the existing mount assembly does not have sufficient capacity to support the loading considered in this analysis pursuant to the listed standards. Structural augments (reinforcements) will be required and are briefly summarized below:

- Install Platform Reinforcement Kit; located 4' below the existing collar mount and attaching to the middle of the existing back-to-back angle platform member at the platform corners.
 - Sitepro1 PRK-1245L, (1) total.
- Remove and properly dispose of existing single angle handrail.
- Install Handrail Kit; located 3.0' above the existing platform rail and attaching to the mount pipes.
 - Sitepro1 HRK14-U, (1) total. Attach all mount pipes to new handrail with kit-provided cross-over plates. (6) new Pipe2.0STD x 9' tall mount pipes will be required to span between the existing rail and new top and bottom rails.
- Install V-Brace Kit; located 2.5' below the existing platform rail and attaching to the new bottom handrail kit.
 - Sitepro1 PRK-SFS-H-L, (1) total. Attach kit ring mount in kit to monopole shaft.
 - If the PRK-SFS-H-L kit is not available, provide (6) total L2-1/2x2-1/2x3/16 x ~8' long replacement angles, field-cut and drill to suit.
 - Pipe2.0STD x 14.0' Horizontal Rail, (3) total. Attach SFS-H-L kit angles to new horizontal bottom rail.
 - Pipe2.0STD x ~4' long corner braces, (3) total. Attach to new horizontal bottom rail w/ Sitepro1 PUCK brackets, (6) total.
 - Sitepro1 SCX1-K, (6) total. Attach all mount pipes to new horizontal bottom rail.
- Panel antennas to be installed in Positions 1 and 3 (as close to the center of face near existing standoff as possible. RRH units to be installed on dual swivel brackets behind panel antennas in Positions 1 and 3.
- Lower the panel antenna installation centerline approximately 1.5'.

Once the recommended augments are successfully implemented, the **augmented** mount assembly has sufficient capacity to support the loading considered in this analysis pursuant to the listed standards.

Augmentation Requirements:

- In order to obtain a mount structure capable of supporting the currently proposed final loading configuration, upgrade augments must be installed in accordance with GeoStructural's Mount Augmentation Drawings.
- Antennas and equipment shall be installed centered vertically on the mount front face rails. If this assumption is incorrect, the results of this analysis will be affected.

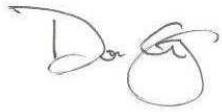
This analysis only encompasses the antenna mount assembly. The tower, overall mount support structure, foundation, etc. are beyond the scope of this analysis. If any of the existing or proposed conditions (appurtenance loading, member sizes, etc.) reported in this analysis are not properly represented, please contact our office immediately to request an amended report.

Prepared by:



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jesse.drennen@geostructural.com

Reviewed and Approved by:



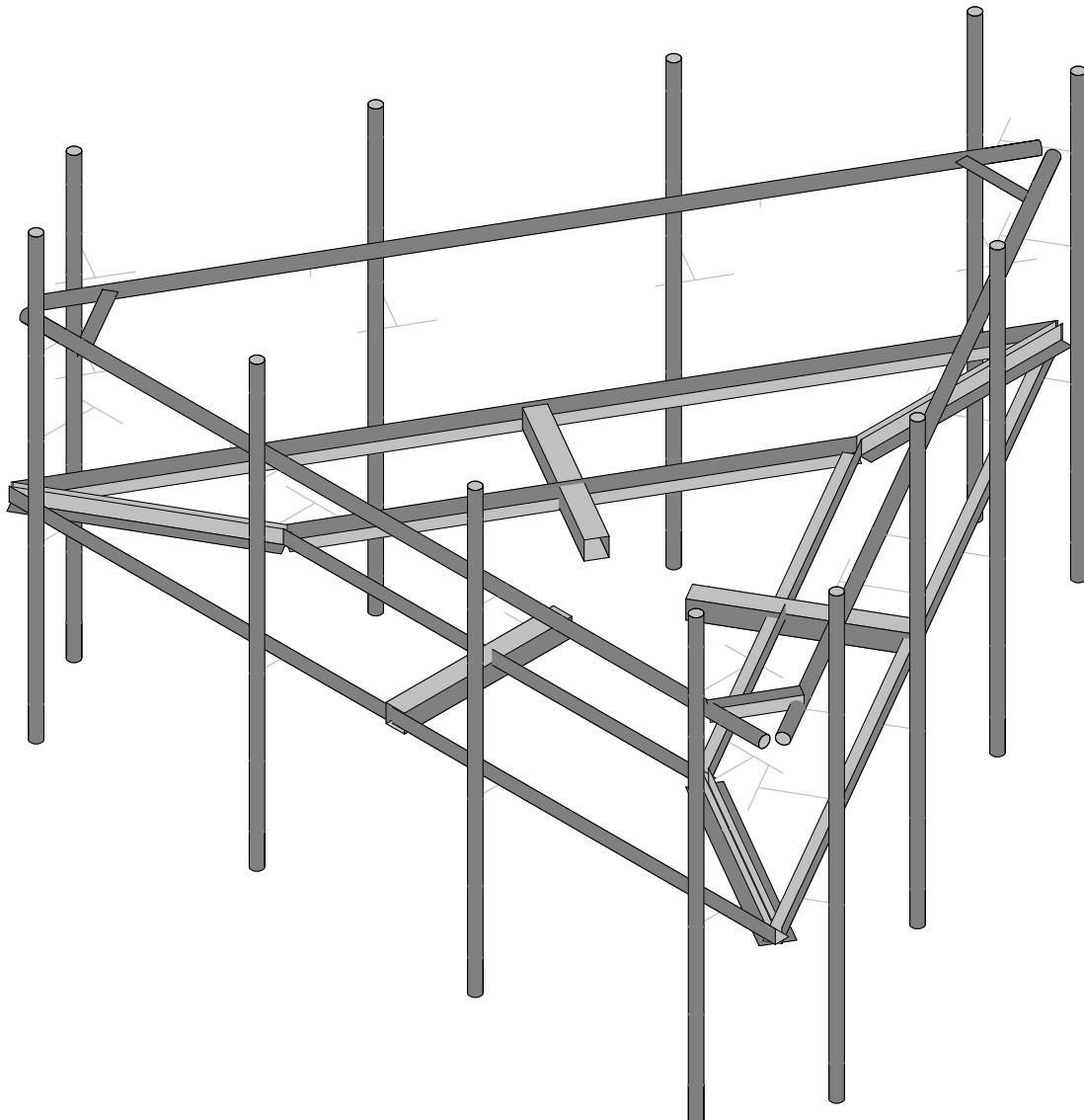
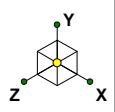
Don George, PE, SE, MLSE
208.602.6569
don.george@geostructural.com

6.0 Standard Conditions

- All data required to complete our structural analysis was furnished by our client and provided record data. GeoStructural has not conducted a site visit or independent study to verify existing conditions and the results of this analysis are based solely on the information provided. It has been assumed that the tower, antenna support structure and foundation have been constructed according to the provided existing drawings, previous structural analysis reports, mapping documents, etc.
- The default Structure Classification is Class II in accordance with ANSI/TIA-222-G §A.2.2 & §A.15.3 and has been assumed for this analysis. The owner shall verify this classification conforms with original or desired reliability criteria.
- This analysis assumes that the structure has been properly installed and maintained in accordance with ANSI/TIA-222-G §15.5 and that no physical deterioration has occurred in any of the components of the structure. Damaged, missing, or rusted members were not considered.
- This analysis verifies the adequacy of the main components of the structure. Not all connections, welds, bolts, plates, etc. were individually detailed and analyzed. Where not specifically analyzed, the existing connection plates, welds, bolts, etc. were assumed adequate to develop the full capacity of the main structural members.
- No consideration has been made for unusual or extreme wind events, rime/in-cloud ice loadings, harmonic or nodal vibration, vortex shedding or other similar conditions.
- It is the owner's responsibility to determine the appropriate design wind speed and amount of ice accumulation beyond code minimum values that should be considered in the analysis.
- This analysis report does not constitute a maintenance and condition assessment. No certifications regarding maintenance and condition are expressed or implied. If desired, GeoStructural can provide these services under a subsequent contract.
- This analysis only encompasses the antenna mount assembly. The tower, overall mount support structure, foundation, etc. are beyond the scope of this analysis. If desired, GeoStructural can provide these services under a subsequent contract.

7.0 Calculations & Software Output

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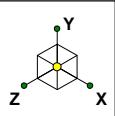
Jesse Drennen, PE

SK - 1

Mar 19, 2018 at 10:45 AM

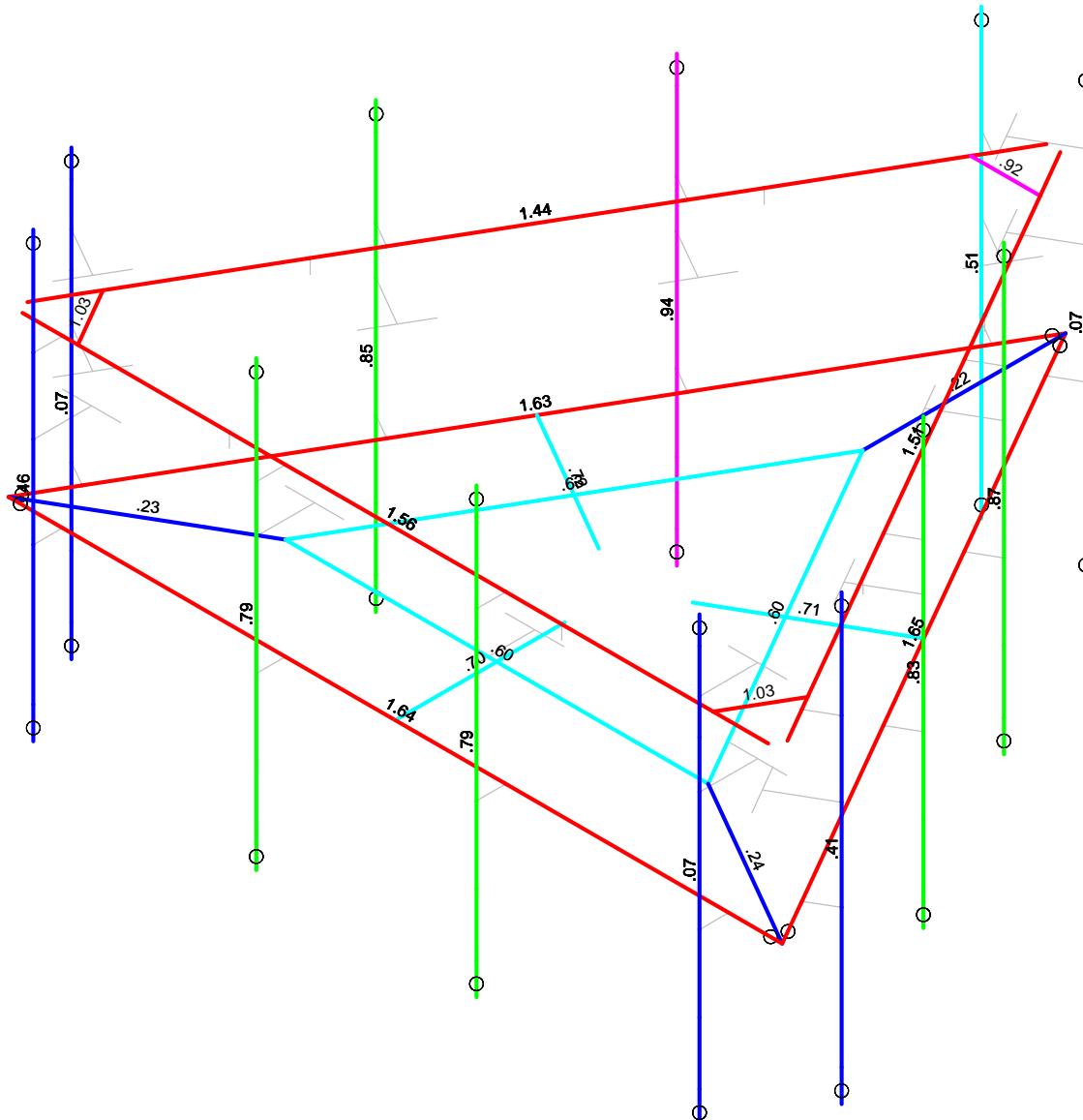
CT33XC566

CT33XC566_Mount Analysis_R0 1...



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(Env)

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| .50-.75 |
| 0.-.50 |



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

GeoStructural, LLC

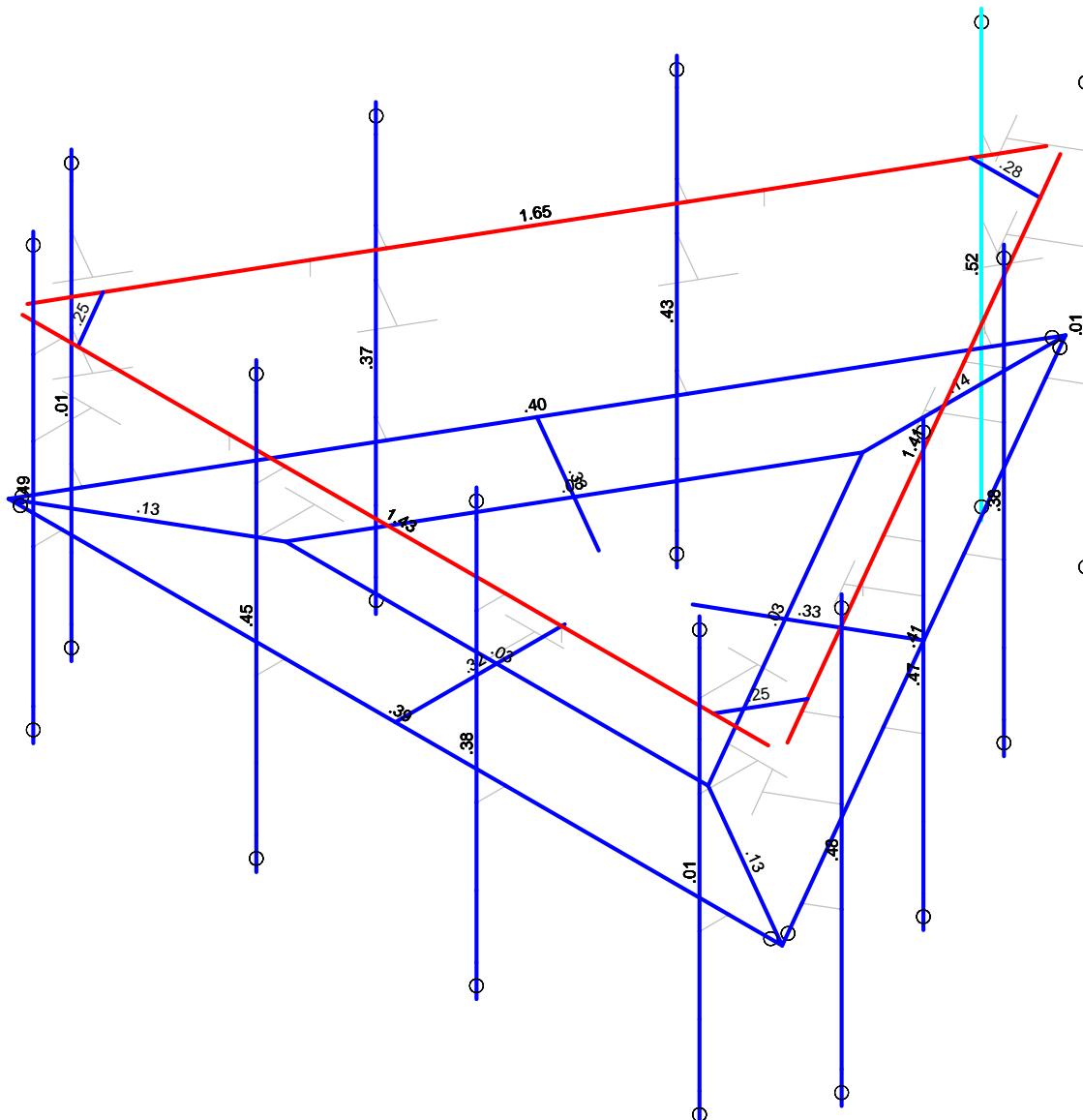
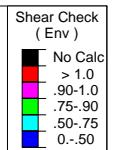
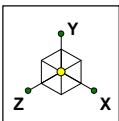
Jesse Drennen, PE

CT33XC566

SK - 1

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CT33XC566_Mount Analysis_R0 1...



Member Shear Checks Displayed (Enveloped)
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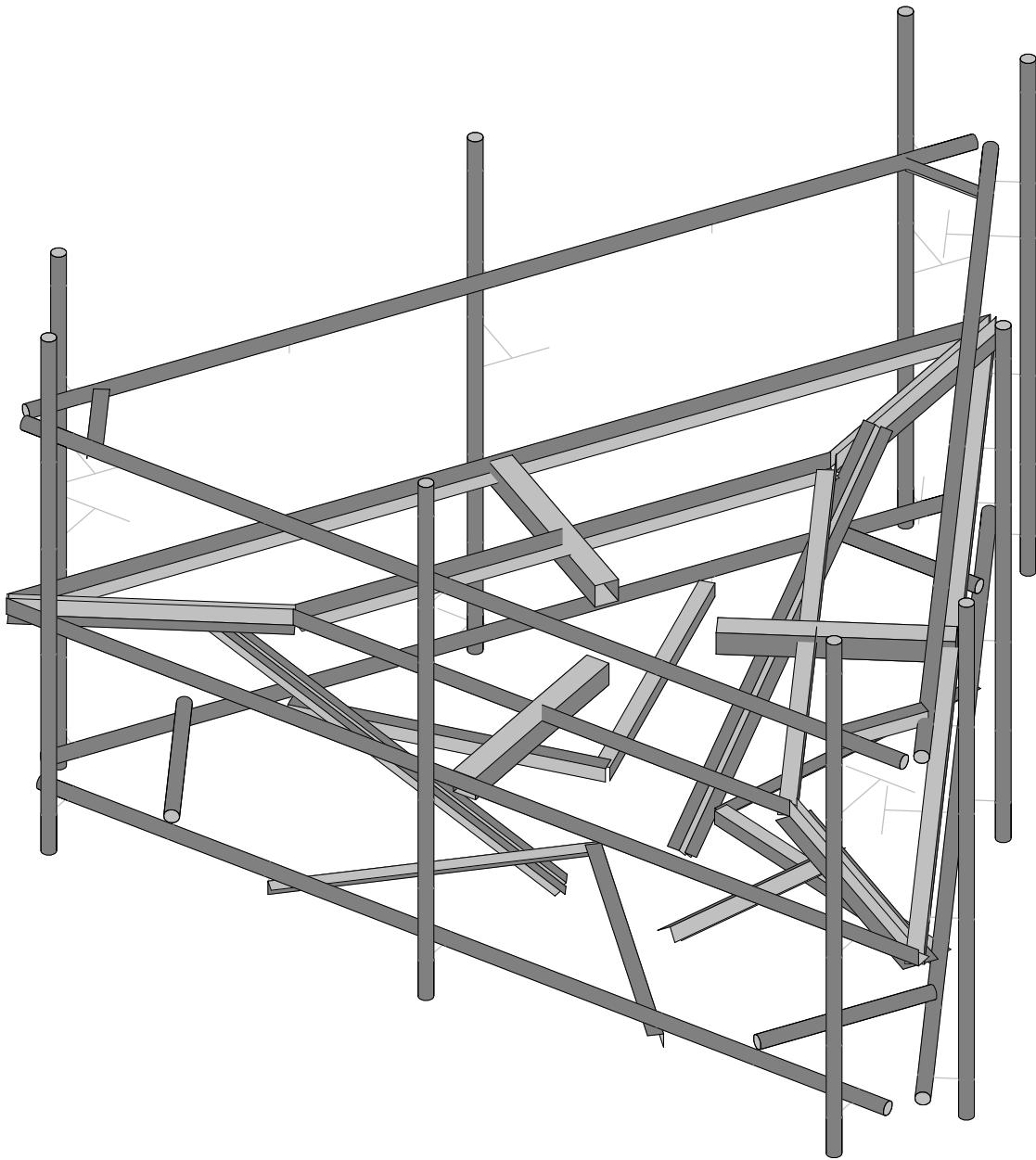
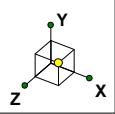
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CT33XC566

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Mar 19, 2018 at 10:49 AM

CT33XC566_Mount Analysis_R0 1...



Envelope Only Solution

GeoStructural, LLC

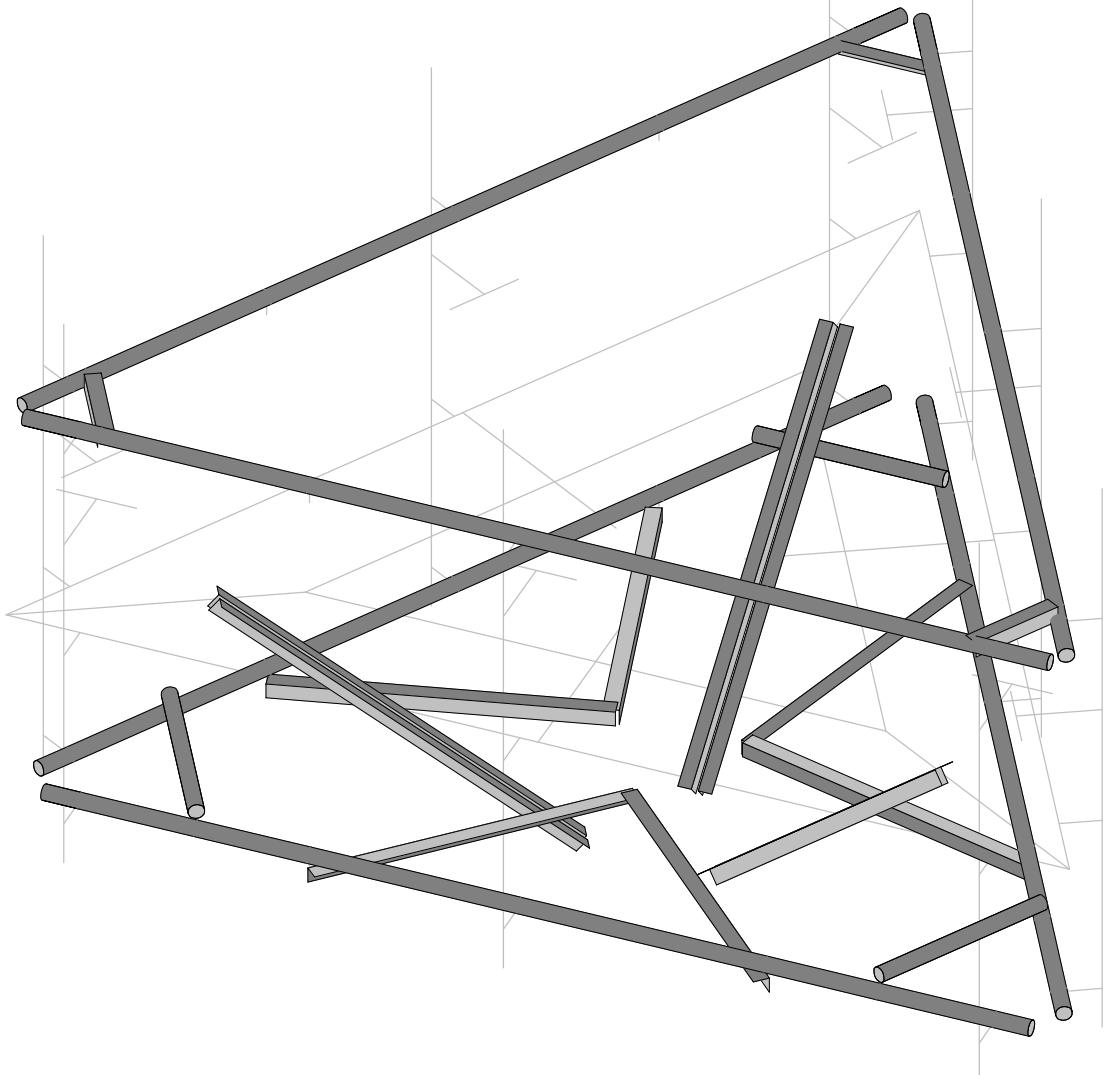
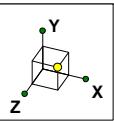
Jesse Drennen, PE

SK - 2

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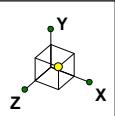
Mar 19, 2018 at 11:13 AM

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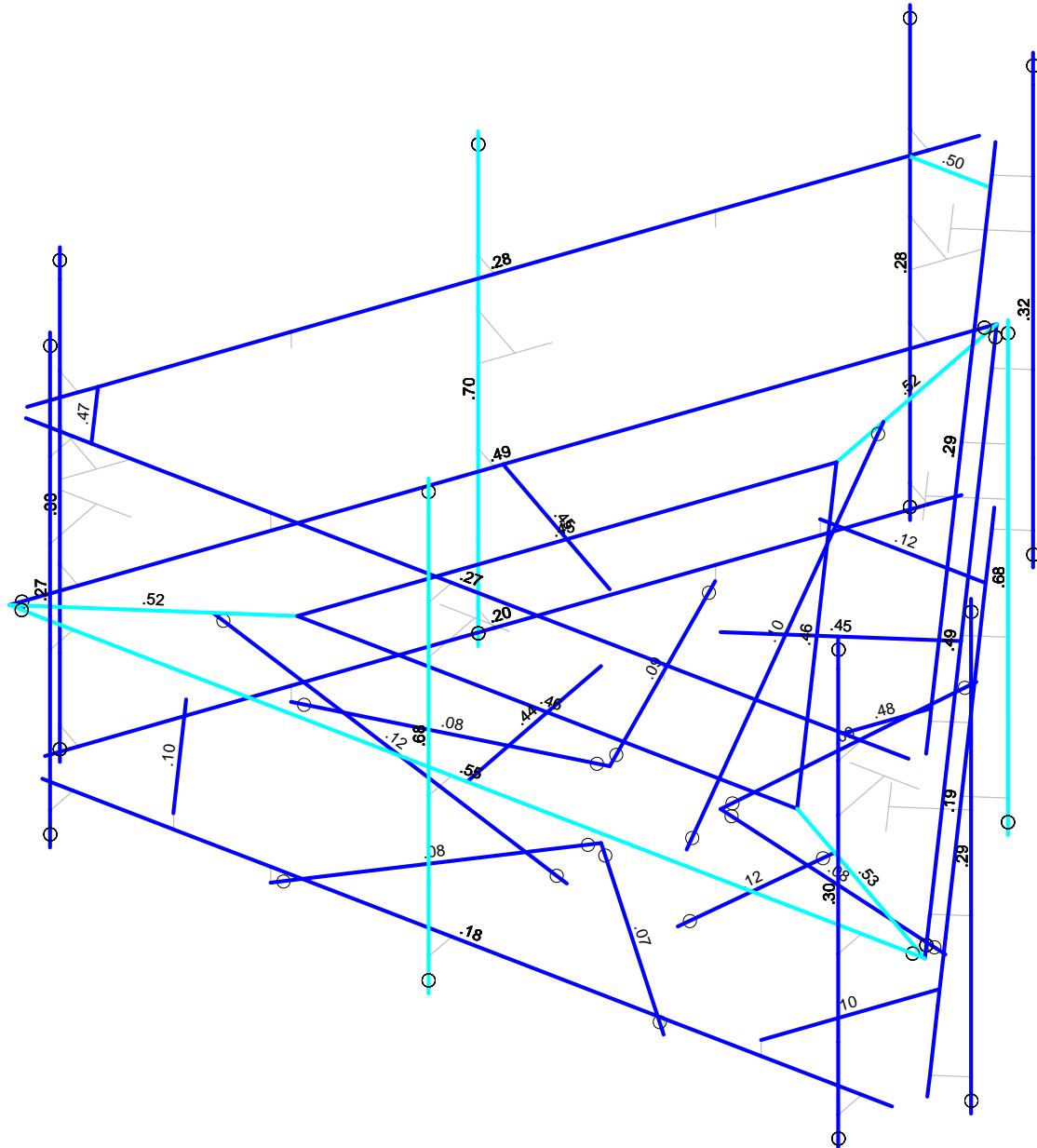
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| GeoStructural, LLC | CT33XC566 | SK - 8 |
| Jesse Drennen, PE | | Mar 19, 2018 at 11:14 AM |
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Envelope Only Solution

GeoStructural, LLC

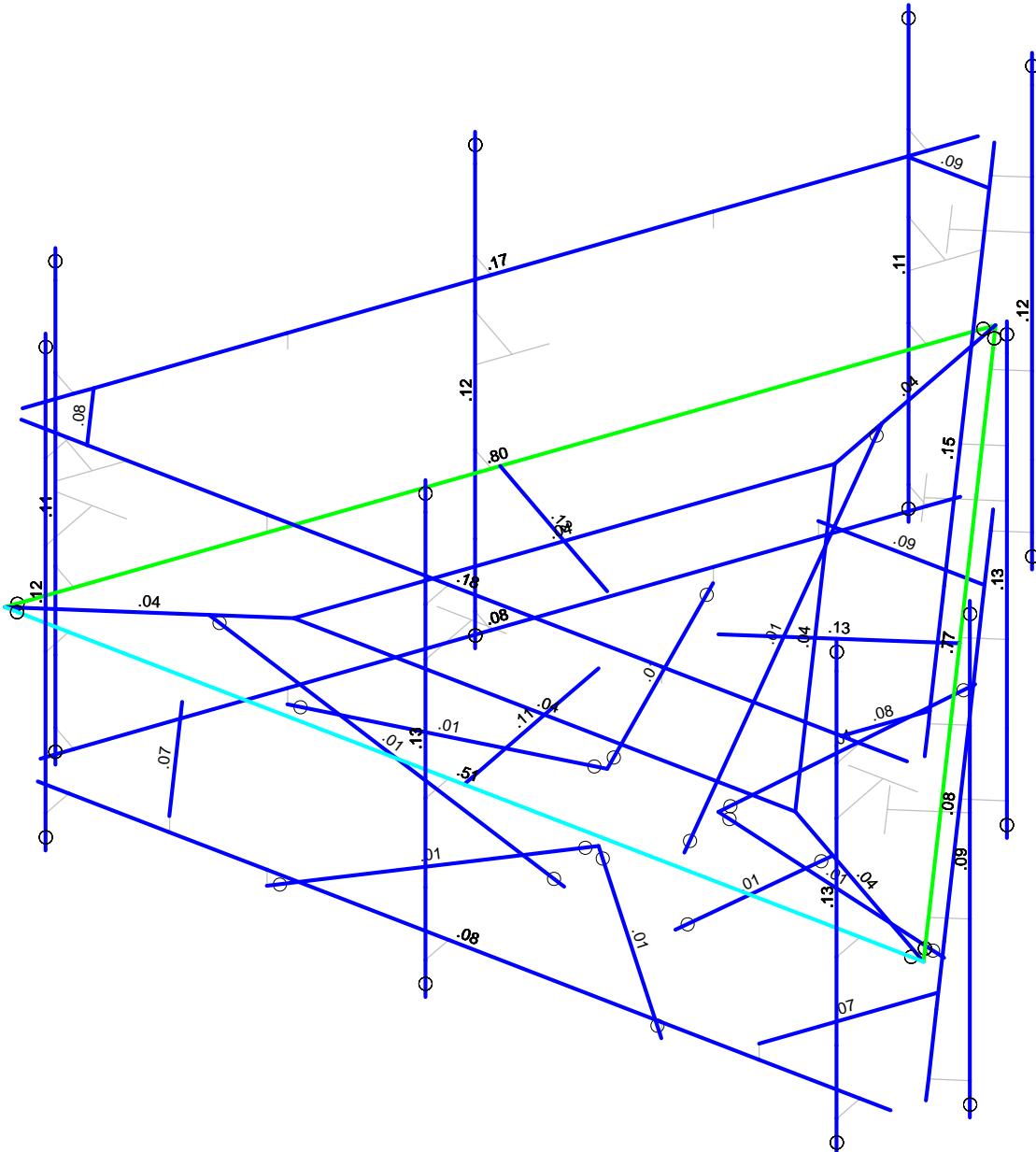
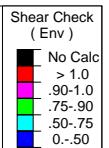
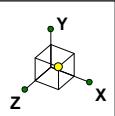
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SK - 3

CT33XC566

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CT33XC566_Mount Analysis_R0 1...



Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

GeoStructural, LLC

Jesse Drennen, PE

SK - 4

CT33XC566

Mar 19, 2018 at 11:13 AM

CT33XC566_Mount Analysis_R0 1...

Basic Load Cases

| BLC Description | | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distributed Area(Me...) | Surface(P... |
|-----------------|----------|----------|-----------|-----------|-----------|-------|-------|-------------------------|--------------|
| 1 | D | DL | | -1 | | 25 | | | |
| 2 | Di | SL | | | | 25 | | 54 | |
| 3 | Lm [500] | LL | | | | 1 | | | |
| 4 | Lv [250] | LL | | | | 2 | | | |
| 5 | Woz | WL | | | | 25 | | 48 | |
| 6 | Wox | WL | | | | 25 | | 48 | |
| 7 | Wiz | WL | | | | 25 | | 48 | |
| 8 | Wix | WL | | | | 25 | | 48 | |
| 9 | Ez | EL | | | | 25 | | | |
| 10 | Ex | EL | | | | 25 | | | |

Load Combination Design

| Description | ASIF | CD | ABIF | Service | Hot Rolled | Cold For... | Wood | Concrete | Masonry | Footings | Aluminum | Connecti... |
|-------------------|------|----|------|---------|------------|-------------|------|----------|---------|----------|----------|-------------|
| 1 1) 1.4D | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 2 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 3 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 4 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 5 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 6 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 7 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 8 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 9 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 10 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 11 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 12 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 13 2) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 14 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 15 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 16 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 17 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 18 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 19 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 20 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 21 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 22 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 23 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 24 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 25 3) 0.9D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 26 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 27 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 28 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 29 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 30 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 31 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 32 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 33 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 34 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 35 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 36 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 37 4) 1.2D+1.0... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 38 5) 1.2D+1.5... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 39 5) 1.2D+1.5... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 40 5) 1.2D+1.5... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |
| 41 5) 1.2D+1.5... | | | | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes |

Load Combination Design (Continued)

| Description | ASIF | CD | ABIF | Service | Hot Rolled | Cold For... | Wood | Concrete | Masonry | Footings | Aluminum | Connecti... |
|--------------------|------|----|------|---------|------------|-------------|------|----------|---------|----------|----------|-------------|
| 42 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 43 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 44 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 45 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 46 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 47 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 48 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 49 5) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 50 6) 1.2D+1.5... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 51 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 52 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 53 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 54 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 55 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 56 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 57 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 58 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 59 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 60 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 61 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 62 7) (1.2+0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 63 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 64 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 65 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 66 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 67 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 68 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 69 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 70 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 71 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 72 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 73 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 74 8) (0.9-0.2S... | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |

Envelope Joint Reactions

| Joint | | X [k] | LC | Y [k] | LC | Z [k] | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
|-------|------|-------|--------|-------|-------|-------|--------|-----------|--------|-----------|--------|-----------|-------|
| 1 | N25 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 2 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 3 | N30 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 4 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 5 | N35 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 6 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 7 | N42 | max | 2.425 | 16 | 1.312 | 34 | 3.168 | 3 | 2.572 | 36 | 3.296 | 21 | 4.372 |
| 8 | | min | -2.683 | 10 | .216 | 65 | -3.007 | 21 | .345 | 18 | -3.305 | 3 | .622 |
| 9 | N40 | max | 2.741 | 6 | 1.344 | 37 | 3.038 | 13 | 2.541 | 27 | 3.228 | 24 | -.636 |
| 10 | | min | -2.478 | 24 | .221 | 69 | -2.898 | 19 | .315 | 22 | -3.236 | 6 | -4.45 |
| 11 | N44 | max | 2.878 | 5 | 1.321 | 35 | 1.538 | 14 | -.75 | 63 | 1.92 | 5 | .098 |
| 12 | | min | -2.856 | 23 | .216 | 65 | -1.839 | 8 | -5.087 | 32 | -1.898 | 23 | -.125 |
| 13 | N128 | max | .057 | 17 | 2.232 | 26 | -.056 | 20 | 0 | 1 | 0 | 66 | 0 |
| 14 | | min | -.057 | 23 | -.002 | 20 | -2.36 | 26 | 0 | 1 | 0 | 60 | 0 |
| 15 | N130 | max | 0 | 24 | 2.232 | 30 | 1.179 | 29 | 0 | 4 | 0 | 22 | 0 |
| 16 | | min | -2.042 | 30 | -.067 | 24 | -.018 | 23 | 0 | 22 | 0 | 4 | 0 |
| 17 | N132 | max | 2.062 | 34 | 2.253 | 34 | 1.191 | 34 | 0 | 24 | 0 | 24 | 0 |
| 18 | | min | .031 | 16 | -.036 | 16 | .004 | 17 | 0 | 6 | 0 | 6 | 0 |
| 19 | N147 | max | .076 | 72 | .087 | 26 | .332 | 32 | 0 | 26 | 0 | 1 | 0 |

Envelope Joint Reactions (Continued)

| Joint | | X [k] | LC | Y [k] | LC | Z [k] | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
|-------|---------|-------|--------|-------|--------|-------|--------|-----------|----|-----------|----|-----------|----|
| 20 | | min | .136 | 42 | .009 | 69 | -.177 | 63 | 0 | 20 | 0 | 1 | 0 |
| 21 | N152 | max | .284 | 36 | .087 | 30 | .103 | 68 | 0 | 15 | 0 | 1 | 0 |
| 22 | | min | -.155 | 18 | .009 | 73 | -.191 | 36 | 0 | 9 | 0 | 1 | 0 |
| 23 | N157 | max | .145 | 71 | .087 | 34 | .107 | 70 | 0 | 25 | 0 | 1 | 0 |
| 24 | | min | -.312 | 28 | .009 | 65 | -.166 | 52 | 0 | 43 | 0 | 1 | 0 |
| 25 | Totals: | max | 6.755 | 17 | 10.632 | 31 | 6.384 | 14 | | | | | |
| 26 | | min | -6.755 | 11 | 1.756 | 74 | -6.384 | 8 | | | | | |

Envelope Member Section Deflections

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC | (n) L/y Ratio | LC | (n) L/z Ratio | LC |
|--------|------|--------|-----|--------|----|--------|----|-----------------|----|---------------|----|---------------|----|
| 1 | M28 | 1 | max | .023 | 14 | .045 | 23 | .047 | 14 | 1.145e-03 | 6 | NC | 1 |
| 2 | | | min | -.254 | 32 | -.049 | 5 | -.051 | 8 | -9.729e-04 | 24 | NC | 1 |
| 3 | | 2 | max | .023 | 14 | .019 | 23 | .052 | 14 | 1.097e-03 | 6 | NC | 1 |
| 4 | | | min | -.254 | 32 | -.024 | 5 | -.068 | 8 | -9.251e-04 | 24 | 3760.661 | 23 |
| 5 | | 3 | max | .023 | 14 | .05 | 5 | .17 | 8 | 1.091e-03 | 6 | NC | 1 |
| 6 | | | min | -.254 | 32 | -.047 | 23 | -.153 | 14 | -9.555e-04 | 24 | 966.562 | 5 |
| 7 | | 4 | max | .023 | 14 | .239 | 5 | .671 | 20 | 3.168e-04 | 38 | NC | 1 |
| 8 | | | min | -.254 | 32 | -.233 | 23 | -.688 | 2 | -2.622e-04 | 20 | 333.663 | 5 |
| 9 | | 5 | max | .022 | 14 | .376 | 5 | 1.234 | 20 | 3.922e-04 | 13 | NC | 1 |
| 10 | | | min | -.255 | 32 | -.372 | 23 | -1.306 | 2 | -3.334e-04 | 19 | 225.848 | 5 |
| 11 | M68A | 1 | max | .465 | 2 | .023 | 14 | .17 | 23 | 8.042e-03 | 23 | NC | 1 |
| 12 | | | min | -.469 | 8 | -.254 | 32 | -.175 | 5 | -8.112e-03 | 5 | NC | 1 |
| 13 | | 2 | max | .465 | 2 | -.038 | 63 | .173 | 23 | 8.042e-03 | 23 | NC | 1 |
| 14 | | | min | -.469 | 8 | -.25 | 31 | -.178 | 5 | -8.112e-03 | 5 | NC | 1 |
| 15 | | 3 | max | .465 | 2 | .01 | 20 | .176 | 23 | 8.042e-03 | 23 | NC | 1 |
| 16 | | | min | -.469 | 8 | -.272 | 26 | -.182 | 5 | -8.112e-03 | 5 | NC | 1 |
| 17 | | 4 | max | .465 | 2 | .078 | 20 | .18 | 23 | 8.042e-03 | 23 | NC | 1 |
| 18 | | | min | -.469 | 8 | -.296 | 26 | -.185 | 5 | -8.112e-03 | 5 | NC | 1 |
| 19 | | 5 | max | .465 | 2 | .146 | 20 | .183 | 23 | 8.042e-03 | 23 | NC | 1 |
| 20 | | | min | -.469 | 8 | -.32 | 26 | -.189 | 5 | -8.112e-03 | 5 | NC | 1 |
| 21 | M69A | 1 | max | .183 | 23 | .147 | 21 | .472 | 8 | 2.149e-02 | 20 | NC | 1 |
| 22 | | | min | -.189 | 5 | -.323 | 27 | -.466 | 2 | -2.382e-02 | 2 | NC | 1 |
| 23 | | 2 | max | .183 | 23 | .145 | 20 | .471 | 8 | 2.149e-02 | 20 | NC | 1 |
| 24 | | | min | -.189 | 5 | -.321 | 26 | -.466 | 2 | -2.382e-02 | 2 | NC | 1 |
| 25 | | 3 | max | .183 | 23 | .146 | 20 | .469 | 8 | 2.149e-02 | 20 | NC | 1 |
| 26 | | | min | -.189 | 5 | -.32 | 26 | -.465 | 2 | -2.382e-02 | 2 | NC | 1 |
| 27 | | 4 | max | .183 | 23 | .147 | 20 | .468 | 8 | 2.149e-02 | 20 | NC | 1 |
| 28 | | | min | -.189 | 5 | -.319 | 26 | -.464 | 2 | -2.382e-02 | 2 | NC | 1 |
| 29 | | 5 | max | .183 | 23 | .147 | 20 | .467 | 8 | 2.149e-02 | 20 | NC | 1 |
| 30 | | | min | -.189 | 5 | -.319 | 26 | -.463 | 2 | -2.382e-02 | 2 | NC | 1 |
| 31 | M40 | 1 | max | .69 | 20 | .009 | 20 | .242 | 5 | 4.667e-03 | 17 | NC | 1 |
| 32 | | | min | -.709 | 2 | -.274 | 26 | -.237 | 23 | -4.72e-03 | 11 | NC | 1 |
| 33 | | 2 | max | .69 | 20 | -.024 | 20 | .243 | 5 | 4.667e-03 | 17 | NC | 1 |
| 34 | | | min | -.709 | 2 | -.261 | 26 | -.237 | 23 | -4.72e-03 | 11 | NC | 1 |
| 35 | | 3 | max | .69 | 20 | -.036 | 63 | .243 | 5 | 4.667e-03 | 17 | NC | 1 |
| 36 | | | min | -.709 | 2 | -.251 | 31 | -.237 | 23 | -4.72e-03 | 11 | NC | 1 |
| 37 | | 4 | max | .69 | 20 | -.014 | 14 | .243 | 5 | 4.667e-03 | 17 | NC | 1 |
| 38 | | | min | -.709 | 2 | -.253 | 32 | -.238 | 23 | -4.72e-03 | 11 | NC | 1 |
| 39 | | 5 | max | .69 | 20 | .023 | 14 | .243 | 5 | 4.667e-03 | 17 | NC | 1 |
| 40 | | | min | -.709 | 2 | -.254 | 32 | -.238 | 23 | -4.72e-03 | 11 | NC | 1 |
| 41 | M41A | 1 | max | .237 | 23 | .262 | 2 | .081 | 24 | 6.129e-03 | 20 | NC | 1 |
| 42 | | | min | -.243 | 5 | -.259 | 20 | -.439 | 30 | -7.23e-03 | 2 | 4290.008 | 40 |
| 43 | | 2 | max | .237 | 23 | .538 | 2 | -.032 | 23 | 1.271e-02 | 20 | NC | 1 |
| 44 | | | min | -.243 | 5 | -.534 | 20 | -.346 | 29 | -1.431e-02 | 2 | 594.087 | 3 |
| 45 | | 3 | max | .237 | 23 | .709 | 2 | .009 | 20 | 2.075e-02 | 20 | NC | 1 |

Company : GeoStructural, LLC
 Designer : Jesse Drennen, PE
 Job Number :
 Model Name : CT33XC566

Mar 19, 2018
 11:12 AM
 Checked By: DWG

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | | |
|--------|------|--------|------|--------|------|--------|-------|-----------------|------------|------------|---------|-----------|---------|----------|----|
| 46 | | min | .242 | 5 | -.69 | 20 | -.275 | 26 | -2.294e-02 | 2 | 376.148 | 2 | 788.933 | 8 | |
| 47 | | 4 | max | .237 | .23 | .552 | 2 | -.055 | 64 | 1.3e-02 | 20 | NC | 1 | NC | 1 |
| 48 | | | min | .242 | 5 | -.548 | 20 | -.375 | 35 | -1.406e-02 | 2 | 614.849 | 2 | 1041.853 | 23 |
| 49 | | 5 | max | .237 | .23 | .298 | 2 | .07 | 16 | 7.52e-03 | 20 | NC | 1 | NC | 1 |
| 50 | | | min | .243 | 5 | -.295 | 20 | -.463 | 34 | -8.065e-03 | 2 | NC | 1 | 585.205 | 11 |
| 51 | M47 | 1 | max | .287 | 3 | .251 | 6 | .075 | 16 | 6.542e-03 | 24 | NC | 1 | NC | 1 |
| 52 | | | min | -.287 | 9 | -.244 | 24 | -.446 | 34 | -7.798e-03 | 6 | NC | 1 | 653.356 | 21 |
| 53 | | 2 | max | .287 | 3 | .503 | 6 | -.053 | 65 | 1.211e-02 | 24 | NC | 1 | NC | 8 |
| 54 | | | min | -.287 | 9 | -.502 | 24 | -.365 | 33 | -1.375e-02 | 6 | 712.267 | 12 | 1222.886 | 21 |
| 55 | | 3 | max | .287 | 3 | .669 | 6 | .009 | 24 | 1.995e-02 | 24 | NC | 1 | NC | 2 |
| 56 | | | min | -.287 | 9 | -.657 | 24 | -.285 | 30 | -2.215e-02 | 6 | 456.198 | 6 | 790.97 | 12 |
| 57 | | 4 | max | .287 | 3 | .585 | 6 | -.046 | 21 | 1.332e-02 | 24 | NC | 1 | NC | 4 |
| 58 | | | min | -.287 | 9 | -.584 | 12 | -.364 | 27 | -1.441e-02 | 6 | 641.717 | 11 | 1082.303 | 15 |
| 59 | | 5 | max | .287 | 3 | .378 | 6 | .061 | 20 | 8.267e-03 | 24 | NC | 1 | NC | 1 |
| 60 | | | min | -.287 | 9 | -.373 | 24 | -.457 | 26 | -8.802e-03 | 6 | 4117.184 | 40 | 632.418 | 3 |
| 61 | M48 | 1 | max | .279 | 7 | .368 | 10 | .061 | 20 | 7.085e-03 | 16 | NC | 1 | NC | 1 |
| 62 | | | min | -.279 | 13 | -.367 | 16 | -.439 | 26 | -8.181e-03 | 10 | 4066.584 | 42 | 651.789 | 25 |
| 63 | | 2 | max | .279 | 7 | .58 | 11 | -.04 | 20 | 1.251e-02 | 16 | NC | 1 | NC | 6 |
| 64 | | | min | -.279 | 13 | -.576 | 16 | -.354 | 26 | -1.402e-02 | 10 | 598.524 | 11 | 1037.22 | 25 |
| 65 | | 3 | max | .279 | 7 | .678 | 10 | 0 | 17 | 2.025e-02 | 16 | NC | 1 | NC | 2 |
| 66 | | | min | -.279 | 13 | -.659 | 16 | -.261 | 35 | -2.237e-02 | 10 | 431.245 | 11 | 819.816 | 4 |
| 67 | | 4 | max | .279 | 7 | .52 | 10 | -.048 | 73 | 1.312e-02 | 16 | NC | 1 | NC | 8 |
| 68 | | | min | -.279 | 13 | -.518 | 16 | -.35 | 30 | -1.409e-02 | 10 | 664.677 | 10 | 1302.908 | 19 |
| 69 | | 5 | max | .279 | 7 | .247 | 10 | .087 | 24 | 7.579e-03 | 16 | NC | 1 | NC | 1 |
| 70 | | | min | -.279 | 13 | -.248 | 4 | -.458 | 30 | -7.959e-03 | 10 | NC | 1 | 630.532 | 7 |
| 71 | M49A | 1 | max | .311 | 21 | .433 | 29 | .294 | 24 | 8.007e-03 | 5 | NC | 1 | NC | 1 |
| 72 | | | min | -.313 | 3 | -.015 | 23 | -.295 | 6 | -7.682e-03 | 23 | 118.047 | 4 | 380.791 | 17 |
| 73 | | 2 | max | .311 | 21 | .432 | 30 | .283 | 24 | 6.853e-03 | 6 | NC | 1 | NC | 12 |
| 74 | | | min | -.313 | 3 | -.009 | 24 | -.284 | 6 | -6.705e-03 | 24 | 157.742 | 4 | 495.991 | 17 |
| 75 | | 3 | max | .311 | 21 | .429 | 30 | .273 | 24 | 6.45e-03 | 6 | NC | 1 | NC | 4 |
| 76 | | | min | -.313 | 3 | -.011 | 24 | -.274 | 6 | -6.433e-03 | 24 | 237.028 | 4 | 812.545 | 15 |
| 77 | | 4 | max | .31 | 21 | .423 | 30 | .264 | 24 | 6.057e-03 | 18 | NC | 1 | NC | 1 |
| 78 | | | min | -.313 | 3 | -.013 | 24 | -.267 | 6 | -6.172e-03 | 12 | 158.018 | 21 | 489.699 | 15 |
| 79 | | 5 | max | .31 | 21 | .416 | 31 | .259 | 24 | 6.439e-03 | 19 | NC | 1 | NC | 1 |
| 80 | | | min | -.313 | 3 | -.016 | 24 | -.262 | 6 | -6.642e-03 | 13 | 118.004 | 21 | 382.894 | 15 |
| 81 | M50 | 1 | max | .331 | 25 | .445 | 33 | .276 | 4 | 7.172e-03 | 9 | NC | 1 | NC | 1 |
| 82 | | | min | -.333 | 7 | -.003 | 15 | -.271 | 22 | -7.133e-03 | 15 | 115.558 | 19 | 1270.598 | 21 |
| 83 | | 2 | max | .331 | 25 | .444 | 34 | .275 | 4 | 6.356e-03 | 22 | NC | 1 | NC | 4 |
| 84 | | | min | -.333 | 7 | 0 | 16 | -.269 | 22 | -6.489e-03 | 4 | 154.42 | 19 | 1758.183 | 21 |
| 85 | | 3 | max | .331 | 25 | .441 | 34 | .273 | 4 | 6.234e-03 | 22 | NC | 1 | NC | 2 |
| 86 | | | min | -.333 | 7 | 0 | 16 | -.268 | 22 | -6.491e-03 | 4 | 231.547 | 19 | 957.652 | 24 |
| 87 | | 4 | max | .331 | 25 | .435 | 34 | .273 | 4 | 6.113e-03 | 22 | NC | 1 | NC | 1 |
| 88 | | | min | -.333 | 7 | -.001 | 16 | -.269 | 22 | -6.493e-03 | 4 | 180.248 | 6 | 556.787 | 24 |
| 89 | | 5 | max | .331 | 25 | .428 | 35 | .276 | 4 | 6.758e-03 | 23 | NC | 1 | NC | 1 |
| 90 | | | min | -.333 | 7 | -.009 | 17 | -.273 | 22 | -7.216e-03 | 5 | 132.652 | 6 | 423.632 | 24 |
| 91 | M51A | 1 | max | .464 | 5 | .436 | 37 | .263 | 8 | 6.864e-03 | 13 | NC | 1 | NC | 1 |
| 92 | | | min | -.462 | 11 | -.002 | 19 | -.261 | 14 | -6.683e-03 | 19 | 123.647 | 24 | 853.175 | 13 |
| 93 | | 2 | max | .464 | 5 | .436 | 26 | .259 | 8 | 5.817e-03 | 13 | NC | 1 | NC | 3 |
| 94 | | | min | -.462 | 11 | .004 | 20 | -.257 | 14 | -5.775e-03 | 19 | 165.388 | 24 | 1035.744 | 13 |
| 95 | | 3 | max | .464 | 5 | .433 | 26 | .255 | 8 | 5.422e-03 | 14 | NC | 1 | NC | 3 |
| 96 | | | min | -.462 | 11 | .003 | 20 | -.253 | 14 | -5.541e-03 | 8 | 248.025 | 24 | 1472.283 | 12 |
| 97 | | 4 | max | .463 | 5 | .428 | 27 | .25 | 8 | 5.258e-03 | 15 | NC | 1 | NC | 1 |
| 98 | | | min | -.462 | 11 | 0 | 20 | -.249 | 2 | -5.469e-03 | 9 | 182.73 | 10 | 853.468 | 12 |
| 99 | | 5 | max | .463 | 5 | .423 | 27 | .246 | 20 | 5.903e-03 | 15 | NC | 1 | NC | 1 |
| 100 | | | min | -.462 | 11 | -.013 | 21 | -.246 | 2 | -6.222e-03 | 9 | 134.641 | 10 | 714.341 | 12 |
| 101 | M73 | 1 | max | .334 | 28 | .243 | 5 | .569 | 2 | 6.456e-03 | 20 | NC | 1 | NC | 1 |
| 102 | | | min | .025 | 22 | -.237 | 23 | -.563 | 20 | -6.982e-03 | 2 | NC | 1 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|-----|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 103 | | 2 | max | .334 | 28 | .242 | 5 | .558 | 2 | 6.456e-03 | 20 | NC | 1 |
| 104 | | | min | .025 | 22 | -.238 | 23 | -.553 | 20 | -6.982e-03 | 2 | NC | 1 |
| 105 | | 3 | max | .334 | 28 | .242 | 5 | .546 | 2 | 6.456e-03 | 20 | NC | 1 |
| 106 | | | min | .025 | 22 | -.239 | 23 | -.542 | 20 | -6.982e-03 | 2 | NC | 1 |
| 107 | | 4 | max | .334 | 28 | .242 | 5 | .535 | 2 | 6.456e-03 | 20 | NC | 1 |
| 108 | | | min | .025 | 22 | -.24 | 23 | -.532 | 20 | -6.982e-03 | 2 | NC | 1 |
| 109 | | 5 | max | .334 | 28 | .242 | 5 | .523 | 2 | 6.456e-03 | 20 | NC | 1 |
| 110 | | | min | .025 | 22 | -.241 | 23 | -.522 | 8 | -6.982e-03 | 2 | NC | 1 |
| 111 | M75 | 1 | max | .362 | 36 | .242 | 5 | .579 | 2 | 6.099e-03 | 2 | NC | 1 |
| 112 | | | min | .047 | 18 | -.237 | 23 | -.574 | 20 | -5.612e-03 | 20 | NC | 1 |
| 113 | | 2 | max | .362 | 36 | .244 | 5 | .568 | 2 | 6.099e-03 | 2 | NC | 1 |
| 114 | | | min | .047 | 18 | -.237 | 23 | -.563 | 20 | -5.612e-03 | 20 | NC | 1 |
| 115 | | 3 | max | .362 | 36 | .245 | 5 | .557 | 2 | 6.099e-03 | 2 | NC | 1 |
| 116 | | | min | .047 | 18 | -.237 | 23 | -.553 | 20 | -5.612e-03 | 20 | NC | 1 |
| 117 | | 4 | max | .362 | 36 | .246 | 5 | .546 | 2 | 6.099e-03 | 2 | NC | 1 |
| 118 | | | min | .047 | 18 | -.237 | 23 | -.542 | 20 | -5.612e-03 | 20 | NC | 1 |
| 119 | | 5 | max | .362 | 36 | .248 | 5 | .534 | 2 | 6.099e-03 | 2 | NC | 1 |
| 120 | | | min | .047 | 18 | -.238 | 23 | -.532 | 20 | -5.612e-03 | 20 | NC | 1 |
| 121 | M77 | 1 | max | .354 | 32 | .48 | 6 | .346 | 14 | 6.66e-03 | 23 | NC | 1 |
| 122 | | | min | .05 | 14 | -.478 | 24 | -.35 | 8 | -7.001e-03 | 5 | NC | 1 |
| 123 | | 2 | max | .354 | 32 | .47 | 6 | .346 | 2 | 6.66e-03 | 23 | NC | 1 |
| 124 | | | min | .05 | 14 | -.469 | 24 | -.348 | 8 | -7.001e-03 | 5 | NC | 1 |
| 125 | | 3 | max | .354 | 32 | .46 | 6 | .346 | 2 | 6.66e-03 | 23 | NC | 1 |
| 126 | | | min | .05 | 14 | -.459 | 12 | -.346 | 8 | -7.001e-03 | 5 | NC | 1 |
| 127 | | 4 | max | .354 | 32 | .449 | 6 | .345 | 2 | 6.66e-03 | 23 | NC | 1 |
| 128 | | | min | .05 | 14 | -.45 | 12 | -.344 | 20 | -7.001e-03 | 5 | NC | 1 |
| 129 | | 5 | max | .354 | 32 | .439 | 6 | .345 | 2 | 6.66e-03 | 23 | NC | 1 |
| 130 | | | min | .05 | 14 | -.44 | 12 | -.343 | 20 | -7.001e-03 | 5 | NC | 1 |
| 131 | M79 | 1 | max | .352 | 28 | .597 | 5 | .322 | 25 | 4.141e-03 | 6 | NC | 1 |
| 132 | | | min | .035 | 22 | -.592 | 23 | -.325 | 7 | -3.784e-03 | 24 | NC | 1 |
| 133 | | 2 | max | .352 | 28 | .588 | 5 | .316 | 25 | 4.141e-03 | 6 | NC | 1 |
| 134 | | | min | .035 | 22 | -.585 | 11 | -.319 | 7 | -3.784e-03 | 24 | NC | 1 |
| 135 | | 3 | max | .352 | 28 | .58 | 5 | .311 | 25 | 4.141e-03 | 6 | NC | 1 |
| 136 | | | min | .035 | 22 | -.578 | 11 | -.314 | 7 | -3.784e-03 | 24 | NC | 1 |
| 137 | | 4 | max | .352 | 28 | .571 | 5 | .305 | 25 | 4.141e-03 | 6 | NC | 1 |
| 138 | | | min | .035 | 22 | -.571 | 11 | -.309 | 7 | -3.784e-03 | 24 | NC | 1 |
| 139 | | 5 | max | .352 | 28 | .563 | 5 | .299 | 25 | 4.141e-03 | 6 | NC | 1 |
| 140 | | | min | .035 | 22 | -.564 | 11 | -.303 | 7 | -3.784e-03 | 24 | NC | 1 |
| 141 | M81 | 1 | max | .342 | 37 | .606 | 17 | .296 | 15 | 3.926e-03 | 16 | NC | 1 |
| 142 | | | min | .034 | 19 | -.613 | 11 | -.3 | 9 | -4.473e-03 | 10 | NC | 1 |
| 143 | | 2 | max | .342 | 37 | .6 | 17 | .29 | 15 | 3.926e-03 | 16 | NC | 1 |
| 144 | | | min | .034 | 19 | -.604 | 11 | -.295 | 9 | -4.473e-03 | 10 | NC | 1 |
| 145 | | 3 | max | .342 | 37 | .593 | 5 | .285 | 15 | 3.926e-03 | 16 | NC | 1 |
| 146 | | | min | .034 | 19 | -.596 | 11 | -.29 | 9 | -4.473e-03 | 10 | NC | 1 |
| 147 | | 4 | max | .342 | 37 | .586 | 5 | .28 | 15 | 3.926e-03 | 16 | NC | 1 |
| 148 | | | min | .034 | 19 | -.587 | 11 | -.285 | 9 | -4.473e-03 | 10 | NC | 1 |
| 149 | | 5 | max | .342 | 37 | .58 | 5 | .274 | 15 | 3.926e-03 | 16 | NC | 1 |
| 150 | | | min | .034 | 19 | -.579 | 11 | -.28 | 9 | -4.473e-03 | 10 | NC | 1 |
| 151 | M83 | 1 | max | .336 | 31 | .505 | 17 | .314 | 14 | 6.941e-03 | 11 | NC | 1 |
| 152 | | | min | .046 | 73 | -.51 | 11 | -.32 | 8 | -6.321e-03 | 17 | NC | 1 |
| 153 | | 2 | max | .336 | 31 | .495 | 17 | .314 | 14 | 6.941e-03 | 11 | NC | 1 |
| 154 | | | min | .046 | 73 | -.501 | 11 | -.318 | 8 | -6.321e-03 | 17 | NC | 1 |
| 155 | | 3 | max | .336 | 31 | .486 | 17 | .313 | 2 | 6.941e-03 | 11 | NC | 1 |
| 156 | | | min | .046 | 73 | -.491 | 11 | -.316 | 8 | -6.321e-03 | 17 | NC | 1 |
| 157 | | 4 | max | .336 | 31 | .477 | 17 | .313 | 2 | 6.941e-03 | 11 | NC | 1 |
| 158 | | | min | .046 | 73 | -.482 | 11 | -.314 | 8 | -6.321e-03 | 17 | NC | 1 |
| 159 | | 5 | max | .336 | 31 | .468 | 17 | .313 | 2 | 6.941e-03 | 11 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | | |
|--------|-----|--------|-------|--------|-------|--------|-------|-----------------|------------|------------|----------|-----------|----------|----------|----|
| 160 | | min | .046 | 73 | -.472 | 11 | -.312 | 20 | -6.321e-03 | 17 | NC | 1 | NC | | |
| 161 | M36 | 1 | max | .004 | 7 | -.03 | 63 | .009 | 54 | 2.065e-03 | 5 | NC | 1 | NC | |
| 162 | | min | -.003 | 25 | -.21 | 32 | -.009 | 72 | -1.604e-03 | 23 | NC | 1 | NC | | |
| 163 | | 2 | max | .004 | 7 | -.018 | 14 | .009 | 66 | 2.065e-03 | 5 | NC | 1 | NC | |
| 164 | | min | -.003 | 25 | -.221 | 32 | -.009 | 60 | -1.604e-03 | 23 | NC | 1 | NC | | |
| 165 | | 3 | max | .004 | 7 | -.004 | 14 | .009 | 66 | 2.065e-03 | 5 | NC | 1 | NC | |
| 166 | | | min | -.003 | 25 | -.232 | 32 | -.009 | 60 | -1.604e-03 | 23 | NC | 1 | NC | |
| 167 | | 4 | max | .004 | 7 | .009 | 14 | .008 | 66 | 2.065e-03 | 5 | NC | 1 | NC | |
| 168 | | min | -.003 | 25 | -.243 | 32 | -.009 | 60 | -1.604e-03 | 23 | NC | 1 | NC | | |
| 169 | | 5 | max | .004 | 7 | .023 | 14 | .008 | 66 | 2.065e-03 | 5 | NC | 1 | NC | |
| 170 | | min | -.003 | 25 | -.253 | 32 | -.009 | 60 | -1.604e-03 | 23 | NC | 1 | NC | | |
| 171 | M52 | 1 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | |
| 172 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | | |
| 173 | | 2 | max | 0 | 4 | .011 | 24 | .018 | 28 | 6.539e-05 | 15 | NC | 1 | NC | |
| 174 | | min | 0 | 22 | -.011 | 6 | .002 | 71 | -8.551e-05 | 9 | 4545.833 | 5 | 2077.957 | 28 | |
| 175 | | 3 | max | 0 | 4 | .025 | 24 | .064 | 28 | 2.256e-04 | 14 | NC | 1 | 4115.327 | 71 |
| 176 | | min | 0 | 22 | -.025 | 6 | .009 | 71 | -2.71e-04 | 8 | 1796.812 | 5 | 571.003 | 28 | |
| 177 | | 4 | max | 0 | 4 | .036 | 24 | .131 | 28 | 6.068e-04 | 25 | NC | 1 | 2107.981 | 22 |
| 178 | | min | 0 | 22 | -.036 | 6 | .017 | 22 | -6.798e-04 | 7 | 1154.904 | 5 | 279.145 | 28 | |
| 179 | | 5 | max | 0 | 4 | .047 | 24 | .208 | 28 | 1.007e-03 | 25 | NC | 1 | 1392.256 | 22 |
| 180 | | min | 0 | 22 | -.047 | 6 | .026 | 22 | -1.107e-03 | 7 | 853.959 | 23 | 175.856 | 28 | |
| 181 | M53 | 1 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | |
| 182 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | | |
| 183 | | 2 | max | 0 | 12 | .011 | 21 | .017 | 36 | 4.327e-05 | 19 | NC | 1 | NC | |
| 184 | | min | 0 | 18 | -.011 | 3 | .003 | 67 | -6.625e-05 | 13 | 4712.877 | 5 | 2098.957 | 36 | |
| 185 | | 3 | max | 0 | 12 | .026 | 22 | .064 | 36 | 2.033e-04 | 21 | NC | 1 | 4146.234 | 18 |
| 186 | | min | 0 | 18 | -.026 | 4 | .009 | 18 | -2.491e-04 | 3 | 1868.136 | 5 | 576.017 | 36 | |
| 187 | | 4 | max | 0 | 12 | .037 | 22 | .13 | 36 | 6.073e-04 | 21 | NC | 1 | 2115.407 | 18 |
| 188 | | min | 0 | 18 | -.037 | 4 | .017 | 18 | -6.799e-04 | 3 | 1193.346 | 5 | 281.3 | 36 | |
| 189 | | 5 | max | 0 | 12 | .049 | 22 | .207 | 36 | 1.011e-03 | 21 | NC | 1 | 1393.237 | 18 |
| 190 | | min | 0 | 18 | -.049 | 4 | .026 | 18 | -1.111e-03 | 3 | 861.12 | 5 | 177.048 | 36 | |
| 191 | M57 | 1 | max | .02 | 2 | -.002 | 14 | .032 | 5 | 5.747e-04 | 5 | NC | 1 | NC | |
| 192 | | min | -.019 | 20 | -.039 | 32 | -.032 | 23 | -5.455e-04 | 23 | NC | 1 | NC | | |
| 193 | | 2 | max | .02 | 2 | .02 | 14 | .045 | 5 | 9.11e-04 | 11 | NC | 6 | NC | |
| 194 | | min | -.019 | 20 | -.021 | 8 | -.045 | 23 | -8.402e-04 | 17 | 1121.104 | 26 | 3424.749 | 23 | |
| 195 | | 3 | max | .021 | 2 | .098 | 26 | .059 | 5 | 2.366e-03 | 11 | NC | 8 | NC | |
| 196 | | min | -.02 | 20 | -.029 | 20 | -.059 | 23 | -2.248e-03 | 17 | 324.755 | 26 | 1609.187 | 23 | |
| 197 | | 4 | max | .021 | 2 | .239 | 26 | .075 | 5 | 3.821e-03 | 11 | NC | 7 | NC | |
| 198 | | min | -.021 | 20 | -.039 | 20 | -.075 | 23 | -3.655e-03 | 17 | 159.467 | 26 | 1033.421 | 23 | |
| 199 | | 5 | max | .022 | 2 | .4 | 26 | .09 | 5 | 5.276e-03 | 11 | NC | 7 | NC | |
| 200 | | min | -.021 | 20 | -.05 | 20 | -.09 | 23 | -5.062e-03 | 17 | 100.545 | 26 | 757.779 | 23 | |
| 201 | M58 | 1 | max | .02 | 10 | -.003 | 22 | .017 | 15 | 7.392e-04 | 17 | NC | 1 | NC | |
| 202 | | min | -.02 | 16 | -.041 | 28 | -.017 | 9 | -7.371e-04 | 23 | NC | 1 | NC | | |
| 203 | | 2 | max | .021 | 10 | .021 | 22 | .024 | 15 | 1.496e-03 | 6 | NC | 2 | NC | |
| 204 | | min | -.02 | 16 | -.022 | 4 | -.024 | 9 | -1.429e-03 | 24 | 1089.018 | 34 | 5399.175 | 10 | |
| 205 | | 3 | max | .021 | 10 | .1 | 34 | .032 | 15 | 2.588e-03 | 7 | NC | 4 | NC | |
| 206 | | min | -.021 | 16 | -.032 | 16 | -.032 | 9 | -2.447e-03 | 25 | 317.436 | 34 | 2454.521 | 10 | |
| 207 | | 4 | max | .022 | 10 | .243 | 34 | .042 | 16 | 3.732e-03 | 7 | NC | 3 | NC | |
| 208 | | min | -.021 | 16 | -.045 | 16 | -.042 | 10 | -3.52e-03 | 25 | 156.235 | 34 | 1530.169 | 10 | |
| 209 | | 5 | max | .022 | 10 | .407 | 34 | .053 | 16 | 4.876e-03 | 7 | NC | 3 | NC | |
| 210 | | min | -.022 | 16 | -.059 | 16 | -.053 | 10 | -4.594e-03 | 25 | 98.609 | 34 | 1097.389 | 16 | |
| 211 | M59 | 1 | max | .021 | 6 | -.003 | 18 | .014 | 19 | 7.347e-04 | 17 | NC | 1 | NC | |
| 212 | | min | -.02 | 24 | -.038 | 36 | -.014 | 13 | -7.31e-04 | 23 | NC | 1 | NC | | |
| 213 | | 2 | max | .021 | 6 | .021 | 18 | .02 | 19 | 1.549e-03 | 4 | NC | 2 | NC | |
| 214 | | min | -.021 | 24 | -.022 | 12 | -.02 | 13 | -1.474e-03 | 22 | 1134.261 | 30 | 5936.106 | 24 | |
| 215 | | 3 | max | .022 | 6 | .098 | 30 | .028 | 18 | 2.576e-03 | 3 | NC | 11 | NC | |
| 216 | | min | -.021 | 24 | -.035 | 24 | -.028 | 12 | -2.432e-03 | 21 | 327.252 | 30 | 2699.244 | 12 | |

Company : GeoStructural, LLC
 Designer : Jesse Drennen, PE
 Job Number :
 Model Name : CT33XC566

Mar 19, 2018
 11:12 AM
 Checked By: DWG

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|-----|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 217 | | 4 | max | .022 | 6 | .238 | 30 | .038 | 18 | 3.674e-03 | 3 | NC | 11 |
| 218 | | | min | -.022 | 24 | -.051 | 24 | -.038 | 12 | -3.457e-03 | 21 | 160.451 | 30 |
| 219 | | 5 | max | .023 | 6 | .398 | 30 | .048 | 18 | 4.772e-03 | 3 | NC | 11 |
| 220 | | | min | -.022 | 24 | -.069 | 24 | -.048 | 12 | -4.483e-03 | 21 | 101.097 | 30 |
| 221 | M60 | 1 | max | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | 1 |
| 222 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC | 1 |
| 223 | | 2 | max | 0 | 8 | .006 | 5 | .018 | 32 | 1.229e-04 | 5 | NC | 1 |
| 224 | | | min | 0 | 14 | -.006 | 23 | .003 | 63 | -9.689e-05 | 23 | 5389.315 | 5 |
| 225 | | 3 | max | 0 | 8 | .01 | 5 | .064 | 32 | 3.702e-04 | 5 | NC | 1 |
| 226 | | | min | 0 | 14 | -.01 | 23 | .009 | 63 | -3.171e-04 | 23 | 3308.443 | 5 |
| 227 | | 4 | max | 0 | 8 | .008 | 54 | .131 | 32 | 8.074e-04 | 5 | NC | 1 |
| 228 | | | min | 0 | 14 | -.008 | 72 | .019 | 63 | -7.253e-04 | 23 | 5315.203 | 5 |
| 229 | | 5 | max | .001 | 8 | .009 | 54 | .208 | 32 | 1.245e-03 | 5 | NC | 1 |
| 230 | | | min | 0 | 14 | -.009 | 72 | .029 | 63 | -1.134e-03 | 23 | NC | 1 |
| 231 | M61 | 1 | max | .012 | 23 | .021 | 25 | .038 | 36 | 8.699e-04 | 45 | NC | 1 |
| 232 | | | min | -.013 | 5 | -.021 | 7 | .003 | 18 | -2.025e-04 | 15 | 6194.713 | 41 |
| 233 | | 2 | max | .011 | 23 | .008 | 25 | .015 | 40 | 3.006e-03 | 32 | NC | 1 |
| 234 | | | min | -.011 | 5 | -.009 | 7 | -.003 | 22 | 3.175e-04 | 15 | 3602.741 | 32 |
| 235 | | 3 | max | .01 | 23 | 0 | 14 | -.006 | 63 | 5.253e-03 | 32 | NC | 2 |
| 236 | | | min | -.01 | 5 | 0 | 8 | -.042 | 32 | 7.547e-04 | 63 | 1541.347 | 32 |
| 237 | | 4 | max | .011 | 11 | .01 | 14 | .006 | 37 | 3.036e-03 | 32 | NC | 1 |
| 238 | | | min | -.011 | 17 | -.01 | 8 | -.002 | 42 | 3.651e-04 | 64 | 3790.482 | 32 |
| 239 | | 5 | max | .013 | 11 | .023 | 15 | .041 | 28 | 8.248e-04 | 31 | NC | 1 |
| 240 | | | min | -.012 | 17 | -.023 | 9 | .003 | 22 | -1.501e-04 | 24 | 7117.876 | 22 |
| 241 | M62 | 1 | max | .024 | 16 | .01 | 19 | .041 | 28 | 1.246e-03 | 11 | NC | 1 |
| 242 | | | min | -.024 | 10 | -.01 | 13 | .003 | 22 | -8.696e-04 | 17 | NC | 1 |
| 243 | | 2 | max | .022 | 16 | .008 | 20 | .006 | 30 | 3.085e-03 | 35 | NC | 1 |
| 244 | | | min | -.022 | 10 | -.008 | 2 | -.002 | 23 | -7.35e-05 | 17 | 3728.756 | 35 |
| 245 | | 3 | max | .021 | 4 | 0 | 18 | -.006 | 67 | 5.239e-03 | 36 | NC | 5 |
| 246 | | | min | -.021 | 22 | 0 | 12 | -.042 | 36 | 7.05e-04 | 18 | 1542.683 | 35 |
| 247 | | 4 | max | .022 | 3 | .016 | 17 | .004 | 30 | 3.021e-03 | 26 | NC | 1 |
| 248 | | | min | -.022 | 21 | -.017 | 11 | 0 | 70 | 3.456e-04 | 20 | 3643.546 | 37 |
| 249 | | 5 | max | .023 | 3 | .028 | 18 | .039 | 32 | 8.807e-04 | 27 | NC | 1 |
| 250 | | | min | -.023 | 21 | -.028 | 12 | .002 | 14 | -4.736e-04 | 22 | 4357.615 | 10 |
| 251 | M63 | 1 | max | .022 | 18 | .029 | 22 | .039 | 32 | 8.096e-04 | 12 | NC | 1 |
| 252 | | | min | -.022 | 12 | -.03 | 4 | .002 | 14 | -4.557e-04 | 18 | 4389.436 | 5 |
| 253 | | 2 | max | .021 | 18 | .016 | 23 | .005 | 33 | 3.01e-03 | 26 | NC | 1 |
| 254 | | | min | -.021 | 12 | -.017 | 5 | -.002 | 39 | 3.262e-04 | 20 | 3768.248 | 28 |
| 255 | | 3 | max | .02 | 6 | 0 | 22 | -.006 | 71 | 5.281e-03 | 28 | NC | 9 |
| 256 | | | min | -.02 | 24 | 0 | 4 | -.043 | 28 | 7.08e-04 | 22 | 1542.674 | 28 |
| 257 | | 4 | max | .022 | 6 | .006 | 20 | .016 | 46 | 3.077e-03 | 29 | NC | 1 |
| 258 | | | min | -.022 | 24 | -.007 | 2 | -.001 | 16 | -7.259e-05 | 23 | 3607.963 | 28 |
| 259 | | 5 | max | .024 | 6 | .007 | 21 | .038 | 36 | 1.268e-03 | 5 | NC | 1 |
| 260 | | | min | -.023 | 24 | -.007 | 3 | .003 | 18 | -9.166e-04 | 23 | 5610.349 | 47 |
| 261 | M64 | 1 | max | .008 | 72 | .053 | 24 | .069 | 24 | 7.403e-03 | 32 | NC | 1 |
| 262 | | | min | -.008 | 54 | -.053 | 6 | -.398 | 30 | -2.918e-03 | 14 | 1213.098 | 41 |
| 263 | | 2 | max | .008 | 72 | .076 | 14 | .015 | 25 | 8.051e-03 | 8 | NC | 7 |
| 264 | | | min | -.009 | 54 | -.093 | 8 | -.34 | 31 | -6.671e-03 | 14 | 2346.052 | 40 |
| 265 | | 3 | max | .009 | 72 | 0 | 14 | -.029 | 63 | 8.426e-03 | 32 | NC | 2 |
| 266 | | | min | -.009 | 54 | -.001 | 8 | -.208 | 32 | 1.157e-03 | 63 | 1393.743 | 31 |
| 267 | | 4 | max | .008 | 60 | .083 | 14 | .011 | 15 | 5.536e-03 | 32 | NC | 1 |
| 268 | | | min | -.008 | 66 | -.108 | 8 | -.363 | 33 | -2.377e-03 | 14 | 2360.015 | 24 |
| 269 | | 5 | max | .008 | 60 | .057 | 16 | .059 | 16 | 8.594e-03 | 32 | NC | 1 |
| 270 | | | min | -.008 | 66 | -.057 | 10 | -.407 | 34 | -2.912e-03 | 14 | 1476.978 | 23 |
| 271 | M65 | 1 | max | .045 | 16 | .035 | 22 | .059 | 16 | 7.65e-03 | 36 | NC | 1 |
| 272 | | | min | -.046 | 10 | -.035 | 4 | -.407 | 34 | -3.229e-03 | 18 | 778.68 | 22 |
| 273 | | 2 | max | .047 | 16 | .056 | 19 | .012 | 17 | 5.013e-03 | 12 | NC | 2 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | | |
|--------|------|--------|-------|--------|-------|--------|-------|-----------------|------------|------------|----------|-----------|----------|----------|----|
| 274 | | min | -.047 | 10 | -.073 | 13 | -.341 | 35 | -2.923e-03 | 18 | 1232.403 | 21 | 2169.095 | 14 | |
| 275 | | 3 | max | .049 | 4 | 0 | .18 | .026 | 18 | 8.406e-03 | 36 | NC | 6 | NC | 2 |
| 276 | | | min | -.049 | 22 | 0 | .12 | -.207 | 36 | 9.227e-04 | 18 | 1384.02 | 37 | 1276.672 | 36 |
| 277 | | 4 | max | .049 | 4 | .115 | .17 | .009 | 19 | 8.447e-03 | 12 | NC | 11 | NC | 1 |
| 278 | | | min | -.049 | 22 | -.138 | .11 | -.36 | 37 | -6.571e-03 | 18 | 999.819 | 16 | 1444.248 | 13 |
| 279 | | 5 | max | .05 | 4 | .078 | .17 | .05 | 20 | 8.408e-03 | 36 | NC | 1 | NC | 1 |
| 280 | | | min | -.049 | 22 | -.078 | .11 | -.4 | 26 | -3.245e-03 | 18 | 774.668 | 16 | 1321.266 | 14 |
| 281 | M66 | 1 | max | .047 | 18 | .078 | .23 | .05 | 20 | 7.691e-03 | 28 | NC | 1 | NC | 1 |
| 282 | | | min | -.047 | 12 | -.078 | .5 | -.4 | 26 | -3.422e-03 | 22 | 780.589 | 24 | 1195.866 | 14 |
| 283 | | 2 | max | .047 | 18 | .113 | .23 | .015 | 22 | 5.38e-03 | 4 | NC | 5 | NC | 1 |
| 284 | | | min | -.047 | 12 | -.13 | .5 | -.34 | 28 | -3.224e-03 | 22 | 1031.107 | 24 | 1502.058 | 15 |
| 285 | | 3 | max | .047 | 6 | 0 | .22 | -.026 | 22 | 8.441e-03 | 28 | NC | 4 | NC | 2 |
| 286 | | | min | -.047 | 24 | 0 | .4 | -.208 | 28 | 9.163e-04 | 22 | 1434.453 | 28 | 1321.687 | 29 |
| 287 | | 4 | max | .045 | 6 | .054 | .21 | .018 | 23 | 8.036e-03 | 4 | NC | 1 | NC | 1 |
| 288 | | | min | -.045 | 24 | -.077 | .3 | -.361 | 29 | -6.357e-03 | 22 | 1308.339 | 19 | 1690.932 | 43 |
| 289 | | 5 | max | .044 | 6 | .03 | .18 | .069 | 24 | 8.456e-03 | 28 | NC | 1 | NC | 1 |
| 290 | | | min | -.043 | 24 | -.031 | .12 | -.398 | 30 | -3.28e-03 | 22 | 796.732 | 18 | 1125.32 | 44 |
| 291 | M57C | 1 | max | .066 | 25 | .041 | .23 | .084 | 16 | 2.686e-03 | 15 | NC | 1 | NC | 1 |
| 292 | | | min | -.416 | 31 | -.046 | .5 | -.085 | 10 | -3.013e-03 | 9 | NC | 1 | 1565.322 | 23 |
| 293 | | 2 | max | .066 | 25 | .044 | .10 | .05 | 6 | 2.758e-03 | 15 | NC | 1 | NC | 1 |
| 294 | | | min | -.416 | 31 | -.04 | .16 | -.045 | 24 | -3.297e-03 | 9 | 3915.525 | 43 | 1416.96 | 9 |
| 295 | | 3 | max | .066 | 25 | .047 | .6 | .145 | 8 | 4.191e-03 | 15 | NC | 1 | NC | 5 |
| 296 | | | min | -.416 | 31 | -.043 | .24 | -.13 | 14 | -4.77e-03 | 9 | 1040.533 | 5 | 497.144 | 8 |
| 297 | | 4 | max | .066 | 25 | .21 | .5 | .307 | 8 | 7.174e-03 | 15 | NC | 1 | NC | 5 |
| 298 | | | min | -.416 | 31 | -.203 | .23 | -.305 | 2 | -7.494e-03 | 9 | 374.147 | 5 | 270.798 | 8 |
| 299 | | 5 | max | .066 | 25 | .342 | .6 | .456 | 20 | 7.286e-03 | 15 | NC | 1 | NC | 1 |
| 300 | | | min | -.416 | 31 | -.329 | .24 | -.481 | 2 | -7.597e-03 | 9 | 247.469 | 5 | 181.865 | 2 |
| 301 | M58B | 1 | max | .192 | 14 | .066 | .25 | .101 | 23 | 7.19e-03 | 23 | NC | 1 | NC | 1 |
| 302 | | | min | -.205 | 8 | -.416 | .31 | -.106 | 5 | -7.235e-03 | 5 | NC | 1 | NC | 1 |
| 303 | | 2 | max | .192 | 14 | .047 | .25 | .111 | 23 | 7.19e-03 | 23 | NC | 1 | NC | 1 |
| 304 | | | min | -.205 | 8 | -.415 | .31 | -.114 | 5 | -7.235e-03 | 5 | NC | 1 | NC | 1 |
| 305 | | 3 | max | .192 | 14 | .036 | .24 | .121 | 23 | 7.19e-03 | 23 | NC | 1 | NC | 1 |
| 306 | | | min | -.205 | 8 | -.416 | .30 | -.123 | 5 | -7.235e-03 | 5 | NC | 1 | NC | 1 |
| 307 | | 4 | max | .192 | 14 | .027 | .24 | .131 | 11 | 7.19e-03 | 23 | NC | 1 | NC | 1 |
| 308 | | | min | -.205 | 8 | -.417 | .30 | -.131 | 5 | -7.235e-03 | 5 | NC | 1 | NC | 1 |
| 309 | | 5 | max | .192 | 14 | .017 | .24 | .142 | 10 | 7.19e-03 | 23 | NC | 1 | NC | 1 |
| 310 | | | min | -.205 | 8 | -.419 | .30 | -.141 | 16 | -7.235e-03 | 5 | NC | 1 | NC | 1 |
| 311 | M59A | 1 | max | .141 | 16 | -.025 | .24 | .219 | 14 | 7.414e-03 | 2 | NC | 1 | NC | 1 |
| 312 | | | min | -.142 | 10 | -.408 | .30 | -.236 | 8 | -6.984e-03 | 20 | NC | 1 | NC | 1 |
| 313 | | 2 | max | .141 | 16 | -.004 | .24 | .205 | 14 | 7.414e-03 | 2 | NC | 1 | NC | 1 |
| 314 | | | min | -.142 | 10 | -.413 | .30 | -.22 | 8 | -6.984e-03 | 20 | NC | 1 | NC | 1 |
| 315 | | 3 | max | .141 | 16 | .017 | .24 | .192 | 14 | 7.414e-03 | 2 | NC | 1 | NC | 1 |
| 316 | | | min | -.142 | 10 | -.419 | .30 | -.205 | 8 | -6.984e-03 | 20 | NC | 1 | NC | 1 |
| 317 | | 4 | max | .141 | 16 | .038 | .24 | .178 | 14 | 7.414e-03 | 2 | NC | 1 | NC | 1 |
| 318 | | | min | -.142 | 10 | -.424 | .29 | -.189 | 8 | -6.984e-03 | 20 | NC | 1 | NC | 1 |
| 319 | | 5 | max | .141 | 16 | .06 | .23 | .164 | 14 | 7.414e-03 | 2 | NC | 1 | NC | 1 |
| 320 | | | min | -.142 | 10 | -.43 | .29 | -.174 | 8 | -6.984e-03 | 20 | NC | 1 | NC | 1 |
| 321 | M60A | 1 | max | .312 | 8 | .033 | .24 | .243 | 5 | 5.742e-03 | 6 | NC | 1 | NC | 1 |
| 322 | | | min | -.312 | 2 | -.422 | .30 | -.237 | 23 | -5.456e-03 | 24 | NC | 1 | NC | 1 |
| 323 | | 2 | max | .312 | 8 | .039 | .24 | .236 | 5 | 5.742e-03 | 6 | NC | 1 | NC | 1 |
| 324 | | | min | -.312 | 2 | -.42 | .31 | -.23 | 23 | -5.456e-03 | 24 | NC | 1 | NC | 1 |
| 325 | | 3 | max | .312 | 8 | .047 | .25 | .229 | 5 | 5.742e-03 | 6 | NC | 1 | NC | 1 |
| 326 | | | min | -.312 | 2 | -.419 | .31 | -.223 | 23 | -5.456e-03 | 24 | NC | 1 | NC | 1 |
| 327 | | 4 | max | .312 | 8 | .057 | .25 | .222 | 5 | 5.742e-03 | 6 | NC | 1 | NC | 1 |
| 328 | | | min | -.312 | 2 | -.417 | .31 | -.215 | 23 | -5.456e-03 | 24 | NC | 1 | NC | 1 |
| 329 | | 5 | max | .312 | 8 | .066 | .25 | .215 | 5 | 5.742e-03 | 6 | NC | 1 | NC | 1 |
| 330 | | | min | -.312 | 2 | -.416 | .31 | -.208 | 23 | -5.456e-03 | 24 | NC | 1 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 331 | M62A | 1 | max | .082 | 7 | .046 | 24 | .009 | 54 | 3.055e-03 | 16 | NC | 1 |
| 332 | | | min | -.071 | 25 | -.404 | 30 | -.008 | 72 | -3.07e-03 | 10 | NC | 1 |
| 333 | | 2 | max | .082 | 7 | .048 | 24 | .009 | 54 | 3.055e-03 | 16 | NC | 1 |
| 334 | | | min | -.071 | 25 | -.406 | 31 | -.007 | 72 | -3.07e-03 | 10 | NC | 1 |
| 335 | | 3 | max | .082 | 7 | .054 | 25 | .013 | 9 | 3.055e-03 | 16 | NC | 1 |
| 336 | | | min | -.071 | 25 | -.409 | 31 | -.011 | 15 | -3.07e-03 | 10 | NC | 1 |
| 337 | | 4 | max | .082 | 7 | .06 | 25 | .019 | 9 | 3.055e-03 | 16 | NC | 1 |
| 338 | | | min | -.071 | 25 | -.413 | 31 | -.015 | 15 | -3.07e-03 | 10 | NC | 1 |
| 339 | | 5 | max | .082 | 7 | .066 | 25 | .024 | 9 | 3.055e-03 | 16 | NC | 1 |
| 340 | | | min | -.071 | 25 | -.416 | 31 | -.019 | 15 | -3.07e-03 | 10 | NC | 1 |
| 341 | M75A | 1 | max | .065 | 17 | .061 | 24 | .08 | 24 | 2.822e-03 | 19 | NC | 1 |
| 342 | | | min | -.425 | 35 | -.061 | 6 | -.083 | 6 | -3.12e-03 | 13 | NC | 1 |
| 343 | | 2 | max | .065 | 17 | .011 | 21 | .061 | 11 | 2.745e-03 | 18 | NC | 1 |
| 344 | | | min | -.425 | 35 | -.018 | 3 | -.06 | 17 | -3.324e-03 | 12 | 1427.624 | 13 |
| 345 | | 3 | max | .065 | 17 | .108 | 18 | .108 | 21 | 3.707e-03 | 18 | NC | 9 |
| 346 | | | min | -.425 | 35 | -.123 | 12 | -.111 | 3 | -4.4e-03 | 12 | 523.23 | 12 |
| 347 | | 4 | max | .065 | 17 | .291 | 6 | .278 | 8 | 6.037e-03 | 19 | NC | 46 |
| 348 | | | min | -.425 | 35 | -.292 | 12 | -.273 | 14 | -6.493e-03 | 13 | 272.211 | 6 |
| 349 | | 5 | max | .065 | 17 | .483 | 6 | .415 | 8 | 6.127e-03 | 19 | NC | 1 |
| 350 | | | min | -.425 | 35 | -.458 | 24 | -.392 | 14 | -6.574e-03 | 13 | 176.405 | 6 |
| 351 | M76A | 1 | max | .179 | 19 | .065 | 17 | .16 | 16 | 7.648e-03 | 3 | NC | 1 |
| 352 | | | min | -.191 | 13 | -.425 | 35 | -.162 | 10 | -7.523e-03 | 21 | NC | 1 |
| 353 | | 2 | max | .179 | 19 | .045 | 17 | .162 | 15 | 7.648e-03 | 3 | NC | 1 |
| 354 | | | min | -.191 | 13 | -.425 | 35 | -.163 | 9 | -7.523e-03 | 21 | NC | 1 |
| 355 | | 3 | max | .179 | 19 | .027 | 16 | .167 | 3 | 7.648e-03 | 3 | NC | 1 |
| 356 | | | min | -.191 | 13 | -.425 | 34 | -.166 | 21 | -7.523e-03 | 21 | NC | 1 |
| 357 | | 4 | max | .179 | 19 | .017 | 16 | .172 | 3 | 7.648e-03 | 3 | NC | 1 |
| 358 | | | min | -.191 | 13 | -.428 | 34 | -.17 | 21 | -7.523e-03 | 21 | NC | 1 |
| 359 | | 5 | max | .179 | 19 | .008 | 16 | .178 | 3 | 7.648e-03 | 3 | NC | 1 |
| 360 | | | min | -.191 | 13 | -.43 | 34 | -.174 | 21 | -7.523e-03 | 21 | NC | 1 |
| 361 | M77A | 1 | max | .174 | 21 | -.038 | 16 | .208 | 19 | 8.099e-03 | 6 | NC | 1 |
| 362 | | | min | -.178 | 3 | -.421 | 34 | -.223 | 13 | -7.56e-03 | 24 | NC | 1 |
| 363 | | 2 | max | .174 | 21 | -.015 | 16 | .193 | 19 | 8.099e-03 | 6 | NC | 1 |
| 364 | | | min | -.178 | 3 | -.425 | 34 | -.207 | 13 | -7.56e-03 | 24 | NC | 1 |
| 365 | | 3 | max | .174 | 21 | .008 | 16 | .179 | 19 | 8.099e-03 | 6 | NC | 1 |
| 366 | | | min | -.178 | 3 | -.43 | 34 | -.191 | 13 | -7.56e-03 | 24 | NC | 1 |
| 367 | | 4 | max | .174 | 21 | .031 | 16 | .165 | 19 | 8.099e-03 | 6 | NC | 1 |
| 368 | | | min | -.178 | 3 | -.434 | 33 | -.175 | 13 | -7.56e-03 | 24 | NC | 1 |
| 369 | | 5 | max | .174 | 21 | .054 | 16 | .151 | 19 | 8.099e-03 | 6 | NC | 1 |
| 370 | | | min | -.178 | 3 | -.439 | 33 | -.159 | 13 | -7.56e-03 | 24 | NC | 1 |
| 371 | M78A | 1 | max | .298 | 25 | .025 | 17 | .287 | 9 | 6.086e-03 | 10 | NC | 1 |
| 372 | | | min | -.301 | 7 | -.433 | 35 | -.287 | 3 | -6.009e-03 | 16 | NC | 1 |
| 373 | | 2 | max | .298 | 25 | .035 | 17 | .283 | 9 | 6.086e-03 | 10 | NC | 1 |
| 374 | | | min | -.301 | 7 | -.431 | 35 | -.283 | 3 | -6.009e-03 | 16 | NC | 1 |
| 375 | | 3 | max | .298 | 25 | .045 | 17 | .28 | 9 | 6.086e-03 | 10 | NC | 1 |
| 376 | | | min | -.301 | 7 | -.429 | 35 | -.279 | 15 | -6.009e-03 | 16 | NC | 1 |
| 377 | | 4 | max | .298 | 25 | .055 | 17 | .277 | 9 | 6.086e-03 | 10 | NC | 1 |
| 378 | | | min | -.301 | 7 | -.427 | 35 | -.275 | 15 | -6.009e-03 | 16 | NC | 1 |
| 379 | | 5 | max | .298 | 25 | .065 | 17 | .276 | 10 | 6.086e-03 | 10 | NC | 1 |
| 380 | | | min | -.301 | 7 | -.425 | 35 | -.275 | 16 | -6.009e-03 | 16 | NC | 1 |
| 381 | M80A | 1 | max | .057 | 2 | .038 | 17 | .046 | 10 | 3.076e-03 | 20 | NC | 1 |
| 382 | | | min | -.045 | 20 | -.413 | 35 | -.046 | 16 | -3.084e-03 | 15 | NC | 1 |
| 383 | | 2 | max | .057 | 2 | .045 | 17 | .049 | 10 | 3.076e-03 | 20 | NC | 1 |
| 384 | | | min | -.045 | 20 | -.416 | 35 | -.048 | 16 | -3.084e-03 | 15 | NC | 1 |
| 385 | | 3 | max | .057 | 2 | .051 | 17 | .052 | 10 | 3.076e-03 | 20 | NC | 1 |
| 386 | | | min | -.045 | 20 | -.419 | 35 | -.049 | 16 | -3.084e-03 | 15 | NC | 1 |
| 387 | | 4 | max | .057 | 2 | .058 | 17 | .054 | 10 | 3.076e-03 | 20 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | |
|--------|-----|--------|------|--------|-------|--------|-------|-----------------|------------|------------|--------|-----------|----|----------|
| 388 | | min | .045 | 20 | -.422 | .35 | -.051 | 16 | -3.084e-03 | 15 | NC | 1 | NC | |
| 389 | | 5 | max | .057 | 2 | .065 | 17 | .058 | 11 | 3.076e-03 | 20 | NC | 1 | NC |
| 390 | | | min | -.045 | 20 | -.425 | 35 | -.053 | 17 | -3.084e-03 | 15 | NC | 1 | NC |
| 391 | M93 | 1 | max | .065 | 21 | .026 | 60 | .029 | 5 | 2.682e-03 | 23 | NC | 1 | NC |
| 392 | | | min | -.421 | 27 | -.026 | 66 | -.026 | 23 | -3.013e-03 | 5 | NC | 1 | NC |
| 393 | | 2 | max | .065 | 21 | .057 | 5 | .022 | 22 | 2.541e-03 | 23 | NC | 1 | NC |
| 394 | | | min | -.421 | 27 | -.055 | 23 | -.029 | 4 | -3.108e-03 | 5 | 1651.803 | 5 | 1715.528 |
| 395 | | 3 | max | .065 | 21 | .217 | 5 | .087 | 21 | 3.617e-03 | 23 | NC | 1 | NC |
| 396 | | | min | -.422 | 27 | -.205 | 23 | -.098 | 3 | -4.222e-03 | 5 | 440.183 | 5 | 824.087 |
| 397 | | 4 | max | .065 | 21 | .418 | 5 | .241 | 21 | 6.172e-03 | 23 | NC | 1 | NC |
| 398 | | | min | -.422 | 27 | -.417 | 11 | -.243 | 3 | -6.474e-03 | 5 | 228.923 | 5 | 367.7 |
| 399 | | 5 | max | .065 | 21 | .572 | 17 | .395 | 9 | 6.268e-03 | 23 | NC | 2 | NC |
| 400 | | | min | -.422 | 27 | -.597 | 11 | -.387 | 15 | -6.559e-03 | 5 | 160.468 | 11 | 234.014 |
| 401 | M94 | 1 | max | .27 | 22 | .065 | 21 | .147 | 19 | 7.336e-03 | 7 | NC | 1 | NC |
| 402 | | | min | -.285 | 4 | -.422 | 27 | -.149 | 13 | -7.179e-03 | 25 | NC | 1 | NC |
| 403 | | 2 | max | .27 | 22 | .044 | 21 | .156 | 18 | 7.336e-03 | 7 | NC | 1 | NC |
| 404 | | | min | -.285 | 4 | -.42 | 27 | -.157 | 12 | -7.179e-03 | 25 | NC | 1 | NC |
| 405 | | 3 | max | .27 | 22 | .022 | 21 | .17 | 6 | 7.336e-03 | 7 | NC | 1 | NC |
| 406 | | | min | -.285 | 4 | -.419 | 27 | -.17 | 24 | -7.179e-03 | 25 | NC | 1 | NC |
| 407 | | 4 | max | .27 | 22 | .01 | 20 | .184 | 6 | 7.336e-03 | 7 | NC | 1 | NC |
| 408 | | | min | -.285 | 4 | -.42 | 26 | -.182 | 24 | -7.179e-03 | 25 | NC | 1 | NC |
| 409 | | 5 | max | .27 | 22 | 0 | 20 | .198 | 6 | 7.336e-03 | 7 | NC | 1 | NC |
| 410 | | | min | -.285 | 4 | -.421 | 26 | -.195 | 24 | -7.179e-03 | 25 | NC | 1 | NC |
| 411 | M95 | 1 | max | .195 | 24 | -.038 | 20 | .297 | 23 | 8.875e-03 | 10 | NC | 1 | NC |
| 412 | | | min | -.198 | 6 | -.414 | 26 | -.315 | 5 | -8.474e-03 | 16 | NC | 1 | NC |
| 413 | | 2 | max | .195 | 24 | -.019 | 20 | .283 | 23 | 8.875e-03 | 10 | NC | 1 | NC |
| 414 | | | min | -.198 | 6 | -.418 | 26 | -.299 | 4 | -8.474e-03 | 16 | NC | 1 | NC |
| 415 | | 3 | max | .195 | 24 | 0 | 20 | .27 | 22 | 8.875e-03 | 10 | NC | 1 | NC |
| 416 | | | min | -.198 | 6 | -.421 | 26 | -.285 | 4 | -8.474e-03 | 16 | NC | 1 | NC |
| 417 | | 4 | max | .195 | 24 | .021 | 19 | .258 | 22 | 8.875e-03 | 10 | NC | 1 | NC |
| 418 | | | min | -.198 | 6 | -.426 | 37 | -.272 | 4 | -8.474e-03 | 16 | NC | 1 | NC |
| 419 | | 5 | max | .195 | 24 | .044 | 19 | .246 | 22 | 8.875e-03 | 10 | NC | 1 | NC |
| 420 | | | min | -.198 | 6 | -.43 | 37 | -.258 | 4 | -8.474e-03 | 16 | NC | 1 | NC |
| 421 | M96 | 1 | max | .414 | 4 | .024 | 21 | .279 | 13 | 5.052e-03 | 13 | NC | 1 | NC |
| 422 | | | min | -.411 | 10 | -.427 | 27 | -.279 | 7 | -4.919e-03 | 19 | NC | 1 | NC |
| 423 | | 2 | max | .414 | 4 | .035 | 21 | .273 | 13 | 5.052e-03 | 13 | NC | 1 | NC |
| 424 | | | min | -.411 | 10 | -.426 | 27 | -.273 | 7 | -4.919e-03 | 19 | NC | 1 | NC |
| 425 | | 3 | max | .414 | 4 | .045 | 21 | .267 | 13 | 5.052e-03 | 13 | NC | 1 | NC |
| 426 | | | min | -.411 | 10 | -.424 | 27 | -.266 | 7 | -4.919e-03 | 19 | NC | 1 | NC |
| 427 | | 4 | max | .414 | 4 | .055 | 21 | .261 | 13 | 5.052e-03 | 13 | NC | 1 | NC |
| 428 | | | min | -.411 | 10 | -.423 | 27 | -.26 | 19 | -4.919e-03 | 19 | NC | 1 | NC |
| 429 | | 5 | max | .414 | 4 | .065 | 21 | .255 | 13 | 5.052e-03 | 13 | NC | 1 | NC |
| 430 | | | min | -.411 | 10 | -.422 | 27 | -.254 | 19 | -4.919e-03 | 19 | NC | 1 | NC |
| 431 | M98 | 1 | max | .129 | 5 | .036 | 21 | .047 | 12 | 3.382e-03 | 24 | NC | 1 | NC |
| 432 | | | min | -.117 | 23 | -.408 | 27 | -.047 | 18 | -3.42e-03 | 6 | NC | 1 | NC |
| 433 | | 2 | max | .129 | 5 | .043 | 21 | .045 | 12 | 3.382e-03 | 24 | NC | 1 | NC |
| 434 | | | min | -.117 | 23 | -.411 | 27 | -.043 | 18 | -3.42e-03 | 6 | NC | 1 | NC |
| 435 | | 3 | max | .129 | 5 | .051 | 21 | .042 | 12 | 3.382e-03 | 24 | NC | 1 | NC |
| 436 | | | min | -.117 | 23 | -.414 | 27 | -.04 | 18 | -3.42e-03 | 6 | NC | 1 | NC |
| 437 | | 4 | max | .129 | 5 | .058 | 21 | .04 | 12 | 3.382e-03 | 24 | NC | 1 | NC |
| 438 | | | min | -.117 | 23 | -.418 | 27 | -.036 | 18 | -3.42e-03 | 6 | NC | 1 | NC |
| 439 | | 5 | max | .129 | 5 | .065 | 21 | .037 | 12 | 3.382e-03 | 24 | NC | 1 | NC |
| 440 | | | min | -.117 | 23 | -.421 | 27 | -.032 | 18 | -3.42e-03 | 6 | NC | 1 | NC |
| 441 | M54 | 1 | max | .061 | 15 | .039 | 23 | .068 | 24 | 2.573e-03 | 7 | NC | 1 | NC |
| 442 | | | min | -.452 | 33 | -.043 | 5 | -.082 | 6 | -1.966e-03 | 25 | NC | 1 | 2194.133 |
| 443 | | 2 | max | .061 | 15 | .034 | 24 | .057 | 10 | 3.261e-03 | 7 | NC | 1 | 4 |
| 444 | | | min | -.452 | 33 | -.044 | 6 | -.053 | 16 | -2.402e-03 | 25 | 4480.23 | 9 | 1243.391 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 445 | | 3 | max | .061 | 15 | .046 | 17 | .169 | 8 | 4.963e-03 | 7 | NC | 1 |
| 446 | | | min | -.452 | 33 | -.047 | 11 | -.144 | 14 | -4.136e-03 | 25 | 1083.342 | 5 |
| 447 | | 4 | max | .061 | 15 | .217 | 5 | .339 | 8 | 6.654e-03 | 7 | NC | 1 |
| 448 | | | min | -.453 | 33 | -.213 | 23 | -.339 | 2 | -6.324e-03 | 25 | 368.86 | 5 |
| 449 | | 5 | max | .061 | 15 | .369 | 5 | .547 | 20 | 6.667e-03 | 7 | NC | 1 |
| 450 | | | min | -.453 | 33 | -.369 | 11 | -.56 | 2 | -6.356e-03 | 25 | 232.824 | 5 |
| 451 | M55 | 1 | max | .261 | 14 | .061 | 15 | .152 | 23 | 7.157e-03 | 23 | NC | 1 |
| 452 | | | min | -.273 | 8 | -.453 | 33 | -.155 | 5 | -7.3e-03 | 5 | NC | 1 |
| 453 | | 2 | max | .261 | 14 | .038 | 15 | .162 | 23 | 7.157e-03 | 23 | NC | 1 |
| 454 | | | min | -.273 | 8 | -.456 | 33 | -.167 | 5 | -7.3e-03 | 5 | NC | 1 |
| 455 | | 3 | max | .261 | 14 | .018 | 16 | .173 | 23 | 7.157e-03 | 23 | NC | 1 |
| 456 | | | min | -.273 | 8 | -.46 | 34 | -.18 | 5 | -7.3e-03 | 5 | NC | 1 |
| 457 | | 4 | max | .261 | 14 | .004 | 16 | .184 | 23 | 7.157e-03 | 23 | NC | 1 |
| 458 | | | min | -.273 | 8 | -.466 | 34 | -.192 | 5 | -7.3e-03 | 5 | NC | 1 |
| 459 | | 5 | max | .261 | 14 | -.009 | 16 | .194 | 23 | 7.157e-03 | 23 | NC | 1 |
| 460 | | | min | -.273 | 8 | -.472 | 34 | -.204 | 5 | -7.3e-03 | 5 | NC | 1 |
| 461 | M56 | 1 | max | .194 | 23 | -.053 | 16 | .308 | 8 | 7.017e-03 | 20 | NC | 1 |
| 462 | | | min | -.204 | 5 | -.464 | 34 | -.292 | 14 | -8.74e-03 | 2 | NC | 1 |
| 463 | | 2 | max | .194 | 23 | -.031 | 16 | .291 | 8 | 7.017e-03 | 20 | NC | 1 |
| 464 | | | min | -.204 | 5 | -.468 | 34 | -.277 | 14 | -8.74e-03 | 2 | NC | 1 |
| 465 | | 3 | max | .194 | 23 | -.009 | 16 | .273 | 8 | 7.017e-03 | 20 | NC | 1 |
| 466 | | | min | -.204 | 5 | -.472 | 34 | -.261 | 14 | -8.74e-03 | 2 | NC | 1 |
| 467 | | 4 | max | .194 | 23 | .012 | 16 | .256 | 8 | 7.017e-03 | 20 | NC | 1 |
| 468 | | | min | -.204 | 5 | -.475 | 34 | -.246 | 14 | -8.74e-03 | 2 | NC | 1 |
| 469 | | 5 | max | .194 | 23 | .034 | 16 | .239 | 8 | 7.017e-03 | 20 | NC | 1 |
| 470 | | | min | -.204 | 5 | -.479 | 35 | -.231 | 14 | -8.74e-03 | 2 | NC | 1 |
| 471 | M57A | 1 | max | .101 | 9 | .036 | 15 | .008 | 66 | 3.463e-03 | 6 | NC | 1 |
| 472 | | | min | -.082 | 15 | -.432 | 33 | -.008 | 60 | -2.912e-03 | 24 | NC | 1 |
| 473 | | 2 | max | .101 | 9 | .042 | 15 | .007 | 66 | 3.463e-03 | 6 | NC | 1 |
| 474 | | | min | -.082 | 15 | -.437 | 33 | -.009 | 60 | -2.912e-03 | 24 | NC | 1 |
| 475 | | 3 | max | .101 | 9 | .049 | 15 | .007 | 24 | 3.463e-03 | 6 | NC | 1 |
| 476 | | | min | -.082 | 15 | -.442 | 33 | -.011 | 6 | -2.912e-03 | 24 | NC | 1 |
| 477 | | 4 | max | .101 | 9 | .055 | 15 | .01 | 25 | 3.463e-03 | 6 | NC | 1 |
| 478 | | | min | -.082 | 15 | -.447 | 33 | -.016 | 7 | -2.912e-03 | 24 | NC | 1 |
| 479 | | 5 | max | .101 | 9 | .061 | 15 | .015 | 25 | 3.463e-03 | 6 | NC | 1 |
| 480 | | | min | -.082 | 15 | -.452 | 33 | -.022 | 7 | -2.912e-03 | 24 | NC | 1 |
| 481 | M62B | 1 | max | .058 | 19 | .032 | 60 | .025 | 11 | 2.429e-03 | 11 | NC | 1 |
| 482 | | | min | -.444 | 37 | -.02 | 66 | -.02 | 17 | -1.82e-03 | 17 | 8900.045 | 20 |
| 483 | | 2 | max | .058 | 19 | .067 | 5 | .025 | 18 | 3.073e-03 | 12 | NC | 1 |
| 484 | | | min | -.444 | 37 | -.065 | 23 | -.037 | 12 | -2.206e-03 | 18 | 1617.278 | 11 |
| 485 | | 3 | max | .058 | 19 | .202 | 17 | .094 | 19 | 4.492e-03 | 11 | NC | 8 |
| 486 | | | min | -.444 | 37 | -.221 | 11 | -.108 | 13 | -3.657e-03 | 17 | 446.325 | 11 |
| 487 | | 4 | max | .058 | 19 | .423 | 5 | .262 | 7 | 5.889e-03 | 11 | NC | 1 |
| 488 | | | min | -.444 | 37 | -.42 | 23 | -.263 | 13 | -5.474e-03 | 17 | 232.066 | 11 |
| 489 | | 5 | max | .058 | 19 | .644 | 5 | .442 | 7 | 5.889e-03 | 11 | NC | 1 |
| 490 | | | min | -.445 | 37 | -.624 | 23 | -.443 | 13 | -5.491e-03 | 17 | 153.854 | 5 |
| 491 | M63A | 1 | max | .327 | 18 | .058 | 19 | .205 | 3 | 7.368e-03 | 3 | NC | 1 |
| 492 | | | min | -.338 | 12 | -.444 | 37 | -.205 | 21 | -7.302e-03 | 21 | NC | 1 |
| 493 | | 2 | max | .327 | 18 | .034 | 19 | .214 | 15 | 7.368e-03 | 3 | NC | 1 |
| 494 | | | min | -.338 | 12 | -.448 | 37 | -.215 | 9 | -7.302e-03 | 21 | NC | 1 |
| 495 | | 3 | max | .327 | 18 | .012 | 20 | .222 | 15 | 7.368e-03 | 3 | NC | 1 |
| 496 | | | min | -.338 | 12 | -.452 | 26 | -.225 | 9 | -7.302e-03 | 21 | NC | 1 |
| 497 | | 4 | max | .327 | 18 | 0 | 20 | .232 | 16 | 7.368e-03 | 3 | NC | 1 |
| 498 | | | min | -.338 | 12 | -.458 | 26 | -.236 | 10 | -7.302e-03 | 21 | NC | 1 |
| 499 | | 5 | max | .327 | 18 | -.011 | 21 | .247 | 16 | 7.368e-03 | 3 | NC | 1 |
| 500 | | | min | -.338 | 12 | -.464 | 27 | -.253 | 10 | -7.302e-03 | 21 | NC | 1 |
| 501 | M64 | 1 | max | .247 | 16 | -.054 | 20 | .37 | 11 | 8.062e-03 | 24 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | |
|--------|------|-----------|----------|--------|-------|--------|------|-----------------|-----------|-----------|--------|-----------|----|---|
| 502 | | min -.253 | 10 | -.454 | 26 | -.357 | 17 | -9.787e-03 | 6 | NC | 1 | NC | 1 | |
| 503 | 2 | max .247 | 16 | -.033 | 20 | .353 | 12 | 8.062e-03 | 24 | NC | 1 | NC | 1 | |
| 504 | | min -.253 | 10 | -.459 | 26 | -.341 | 18 | -9.787e-03 | 6 | NC | 1 | NC | 1 | |
| 505 | 3 | max .247 | 16 | -.011 | 21 | .338 | 12 | 8.062e-03 | 24 | NC | 1 | NC | 1 | |
| 506 | | min -.253 | 10 | -.464 | 27 | -.327 | 18 | -9.787e-03 | 6 | NC | 1 | NC | 1 | |
| 507 | 4 | max .247 | 16 | .012 | 21 | .322 | 12 | 8.062e-03 | 24 | NC | 1 | NC | 1 | |
| 508 | | min -.253 | 10 | -.469 | 27 | -.313 | 18 | -9.787e-03 | 6 | NC | 1 | NC | 1 | |
| 509 | 5 | max .247 | 16 | .035 | 21 | .306 | 12 | 8.062e-03 | 24 | NC | 1 | NC | 1 | |
| 510 | | min -.253 | 10 | -.474 | 27 | -.299 | 18 | -9.787e-03 | 6 | NC | 1 | NC | 1 | |
| 511 | M65A | 1 | max .136 | 11 | .031 | 19 | .049 | 22 | 3.527e-03 | 10 | NC | 1 | NC | 1 |
| 512 | | min -.119 | 17 | -.424 | 37 | -.05 | 4 | -3.009e-03 | 16 | NC | 1 | NC | 1 | |
| 513 | 2 | max .136 | 11 | .038 | 19 | .046 | 22 | 3.527e-03 | 10 | NC | 1 | NC | 1 | |
| 514 | | min -.119 | 17 | -.429 | 37 | -.048 | 4 | -3.009e-03 | 16 | NC | 1 | NC | 1 | |
| 515 | 3 | max .136 | 11 | .045 | 19 | .042 | 22 | 3.527e-03 | 10 | NC | 1 | NC | 1 | |
| 516 | | min -.119 | 17 | -.434 | 37 | -.045 | 4 | -3.009e-03 | 16 | NC | 1 | NC | 1 | |
| 517 | 4 | max .136 | 11 | .051 | 19 | .038 | 22 | 3.527e-03 | 10 | NC | 1 | NC | 1 | |
| 518 | | min -.119 | 17 | -.439 | 37 | -.043 | 4 | -3.009e-03 | 16 | NC | 1 | NC | 1 | |
| 519 | 5 | max .136 | 11 | .058 | 19 | .035 | 21 | 3.527e-03 | 10 | NC | 1 | NC | 1 | |
| 520 | | min -.119 | 17 | -.444 | 37 | -.042 | 3 | -3.009e-03 | 16 | NC | 1 | NC | 1 | |
| 521 | M70 | 1 | max .075 | 23 | .049 | 22 | .082 | 4 | 2.87e-03 | 4 | NC | 1 | NC | 1 |
| 522 | | min -.445 | 29 | -.063 | 4 | -.072 | 22 | -2.206e-03 | 22 | NC | 1 | NC | 1 | |
| 523 | 2 | max .075 | 23 | .019 | 3 | .065 | 5 | 3.674e-03 | 4 | NC | 7 | NC | 1 | |
| 524 | | min -.445 | 29 | -.011 | 21 | -.057 | 23 | -2.8e-03 | 22 | 1194.044 | 4 | 3881.975 | 3 | |
| 525 | 3 | max .076 | 23 | .134 | 4 | .092 | 19 | 5.079e-03 | 4 | NC | 13 | NC | 16 | |
| 526 | | min -.445 | 29 | -.111 | 22 | -.103 | 13 | -4.259e-03 | 22 | 486.642 | 4 | 729.815 | 3 | |
| 527 | 4 | max .076 | 23 | .313 | 5 | .254 | 7 | 6.706e-03 | 4 | NC | 1 | NC | 1 | |
| 528 | | min -.445 | 29 | -.309 | 23 | -.253 | 13 | -6.362e-03 | 22 | 258.713 | 4 | 338.567 | 2 | |
| 529 | 5 | max .076 | 23 | .546 | 5 | .402 | 8 | 6.761e-03 | 4 | NC | 1 | NC | 1 | |
| 530 | | min -.445 | 29 | -.546 | 11 | -.387 | 14 | -6.436e-03 | 22 | 159.329 | 5 | 227.36 | 8 | |
| 531 | M71 | 1 | max .219 | 22 | .076 | 23 | .21 | 6 | 7.64e-03 | 6 | NC | 1 | NC | 1 |
| 532 | | min -.233 | 4 | -.445 | 29 | -.211 | 12 | -7.584e-03 | 24 | NC | 1 | NC | 1 | |
| 533 | 2 | max .219 | 22 | .053 | 23 | .207 | 19 | 7.64e-03 | 6 | NC | 1 | NC | 1 | |
| 534 | | min -.233 | 4 | -.448 | 29 | -.209 | 13 | -7.584e-03 | 24 | NC | 1 | NC | 1 | |
| 535 | 3 | max .219 | 22 | .031 | 24 | .213 | 19 | 7.64e-03 | 6 | NC | 1 | NC | 1 | |
| 536 | | min -.233 | 4 | -.45 | 29 | -.216 | 13 | -7.584e-03 | 24 | NC | 1 | NC | 1 | |
| 537 | 4 | max .219 | 22 | .018 | 24 | .218 | 19 | 7.64e-03 | 6 | NC | 1 | NC | 1 | |
| 538 | | min -.233 | 4 | -.455 | 30 | -.223 | 13 | -7.584e-03 | 24 | NC | 1 | NC | 1 | |
| 539 | 5 | max .219 | 22 | .004 | 24 | .224 | 19 | 7.64e-03 | 6 | NC | 1 | NC | 1 | |
| 540 | | min -.233 | 4 | -.46 | 30 | -.23 | 13 | -7.584e-03 | 24 | NC | 1 | NC | 1 | |
| 541 | M72 | 1 | max .224 | 19 | -.043 | 24 | .272 | 4 | 7.12e-03 | 16 | NC | 1 | NC | 1 |
| 542 | | min -.23 | 13 | -.45 | 30 | -.254 | 22 | -8.691e-03 | 10 | NC | 1 | NC | 1 | |
| 543 | 2 | max .224 | 19 | -.02 | 24 | .253 | 4 | 7.12e-03 | 16 | NC | 1 | NC | 1 | |
| 544 | | min -.23 | 13 | -.455 | 30 | -.237 | 22 | -8.691e-03 | 10 | NC | 1 | NC | 1 | |
| 545 | 3 | max .224 | 19 | .004 | 24 | .233 | 4 | 7.12e-03 | 16 | NC | 1 | NC | 1 | |
| 546 | | min -.23 | 13 | -.46 | 30 | -.219 | 22 | -8.691e-03 | 10 | NC | 1 | NC | 1 | |
| 547 | 4 | max .224 | 19 | .028 | 24 | .214 | 4 | 7.12e-03 | 16 | NC | 1 | NC | 1 | |
| 548 | | min -.23 | 13 | -.465 | 30 | -.202 | 22 | -8.691e-03 | 10 | NC | 1 | NC | 1 | |
| 549 | 5 | max .224 | 19 | .052 | 24 | .195 | 4 | 7.12e-03 | 16 | NC | 1 | NC | 1 | |
| 550 | | min -.23 | 13 | -.47 | 30 | -.184 | 22 | -8.691e-03 | 10 | NC | 1 | NC | 1 | |
| 551 | M73A | 1 | max .056 | 3 | .05 | 23 | .044 | 24 | 3.148e-03 | 2 | NC | 1 | NC | 1 |
| 552 | | min -.038 | 21 | -.423 | 29 | -.044 | 6 | -2.592e-03 | 20 | NC | 1 | NC | 1 | |
| 553 | 2 | max .056 | 3 | .056 | 23 | .046 | 24 | 3.148e-03 | 2 | NC | 1 | NC | 1 | |
| 554 | | min -.038 | 21 | -.429 | 29 | -.048 | 6 | -2.592e-03 | 20 | NC | 1 | NC | 1 | |
| 555 | 3 | max .056 | 3 | .063 | 23 | .048 | 24 | 3.148e-03 | 2 | NC | 1 | NC | 1 | |
| 556 | | min -.038 | 21 | -.434 | 29 | -.052 | 5 | -2.592e-03 | 20 | NC | 1 | NC | 1 | |
| 557 | 4 | max .056 | 3 | .069 | 23 | .053 | 23 | 3.148e-03 | 2 | NC | 1 | NC | 1 | |
| 558 | | min -.038 | 21 | -.439 | 29 | -.058 | 5 | -2.592e-03 | 20 | NC | 1 | NC | 1 | |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 559 | | 5 | max | .056 | 3 | .075 | 23 | .057 | 23 | 3.148e-03 | 2 | NC | 1 |
| 560 | | | min | -.038 | 21 | -.444 | 29 | -.064 | 5 | -2.592e-03 | 20 | NC | 1 |
| 561 | M104 | 1 | max | .005 | 26 | .03 | 20 | .047 | 5 | 3.513e-04 | 66 | NC | 1 |
| 562 | | | min | 0 | 20 | -.034 | 2 | -.047 | 23 | -4.117e-04 | 60 | 7688.612 | 69 |
| 563 | | 2 | max | .004 | 26 | .033 | 20 | .043 | 5 | 2.635e-04 | 66 | NC | 1 |
| 564 | | | min | 0 | 20 | -.044 | 2 | -.043 | 23 | -3.088e-04 | 60 | 2542.945 | 26 |
| 565 | | 3 | max | .003 | 26 | .03 | 20 | .034 | 5 | 1.757e-04 | 66 | NC | 5 |
| 566 | | | min | 0 | 20 | -.047 | 26 | -.034 | 23 | -2.059e-04 | 60 | 1811.849 | 26 |
| 567 | | 4 | max | .001 | 26 | .018 | 20 | .019 | 5 | 8.783e-05 | 66 | NC | 1 |
| 568 | | | min | 0 | 20 | -.032 | 26 | -.019 | 23 | -1.029e-04 | 60 | 2542.945 | 26 |
| 569 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 570 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 571 | M105 | 1 | max | .005 | 30 | .031 | 24 | .021 | 19 | 1.573e-03 | 22 | NC | 1 |
| 572 | | | min | 0 | 24 | -.035 | 6 | -.021 | 13 | -1.638e-03 | 4 | 7640.56 | 73 |
| 573 | | 2 | max | .004 | 30 | .047 | 24 | .021 | 20 | 1.18e-03 | 22 | NC | 1 |
| 574 | | | min | 0 | 24 | -.058 | 6 | -.021 | 2 | -1.228e-03 | 4 | 2293.665 | 6 |
| 575 | | 3 | max | .003 | 30 | .048 | 24 | .021 | 21 | 7.864e-04 | 22 | NC | 2 |
| 576 | | | min | 0 | 24 | -.062 | 6 | -.022 | 3 | -8.188e-04 | 4 | 1634.236 | 6 |
| 577 | | 4 | max | .001 | 30 | .031 | 24 | .015 | 21 | 3.932e-04 | 22 | NC | 1 |
| 578 | | | min | 0 | 24 | -.04 | 6 | -.015 | 3 | -4.094e-04 | 4 | 2293.665 | 6 |
| 579 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 580 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 581 | M106 | 1 | max | .006 | 34 | .031 | 16 | .025 | 15 | 1.493e-03 | 24 | NC | 1 |
| 582 | | | min | 0 | 16 | -.035 | 10 | -.025 | 9 | -1.55e-03 | 6 | 7730.414 | 65 |
| 583 | | 2 | max | .004 | 34 | .047 | 16 | .025 | 14 | 1.12e-03 | 24 | NC | 1 |
| 584 | | | min | 0 | 16 | -.058 | 10 | -.025 | 8 | -1.162e-03 | 6 | 2293.665 | 10 |
| 585 | | 3 | max | .003 | 34 | .048 | 16 | .024 | 25 | 7.465e-04 | 24 | NC | 2 |
| 586 | | | min | 0 | 16 | -.062 | 10 | -.024 | 7 | -7.75e-04 | 6 | 1634.236 | 10 |
| 587 | | 4 | max | .001 | 34 | .031 | 16 | .016 | 25 | 3.732e-04 | 24 | NC | 1 |
| 588 | | | min | 0 | 16 | -.04 | 10 | -.016 | 7 | -3.875e-04 | 6 | 2293.665 | 10 |
| 589 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 590 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 591 | M57A | 1 | max | .034 | 5 | .085 | 10 | .06 | 25 | 2.71e-03 | 9 | NC | 1 |
| 592 | | | min | -.03 | 23 | -.083 | 16 | -.42 | 31 | -2.6e-03 | 15 | 4505.953 | 47 |
| 593 | | 2 | max | .033 | 5 | .032 | 23 | .033 | 25 | 1.058e-03 | 21 | NC | 1 |
| 594 | | | min | -.03 | 23 | -.037 | 5 | -.346 | 31 | -1.556e-03 | 3 | 3136.973 | 8 |
| 595 | | 3 | max | .033 | 5 | .06 | 8 | .025 | 14 | 2.255e-04 | 14 | NC | 1 |
| 596 | | | min | -.03 | 23 | -.05 | 14 | -.268 | 32 | -1.882e-03 | 32 | 2179.941 | 5 |
| 597 | | 4 | max | .034 | 5 | .034 | 17 | .032 | 15 | 1.591e-03 | 19 | NC | 1 |
| 598 | | | min | -.03 | 23 | -.034 | 11 | -.381 | 33 | -1.626e-03 | 13 | 1490.139 | 5 |
| 599 | | 5 | max | .034 | 5 | .077 | 6 | .055 | 15 | 3.243e-03 | 7 | NC | 1 |
| 600 | | | min | -.03 | 23 | -.064 | 24 | -.449 | 33 | -2.562e-03 | 25 | 1083.966 | 5 |
| 601 | M58A | 1 | max | .383 | 31 | .027 | 23 | .036 | 23 | 1.125e-03 | 9 | NC | 1 |
| 602 | | | min | -.041 | 25 | -.027 | 5 | -.04 | 5 | -9.608e-04 | 15 | NC | 1 |
| 603 | | 2 | max | .383 | 31 | .028 | 23 | .037 | 23 | 1.125e-03 | 9 | NC | 1 |
| 604 | | | min | -.041 | 25 | -.029 | 5 | -.041 | 5 | -9.608e-04 | 15 | NC | 1 |
| 605 | | 3 | max | .383 | 31 | .028 | 23 | .038 | 23 | 1.125e-03 | 9 | NC | 1 |
| 606 | | | min | -.041 | 25 | -.03 | 5 | -.042 | 5 | -9.608e-04 | 15 | NC | 1 |
| 607 | | 4 | max | .383 | 31 | .029 | 23 | .039 | 23 | 1.125e-03 | 9 | NC | 1 |
| 608 | | | min | -.041 | 25 | -.032 | 5 | -.043 | 5 | -9.608e-04 | 15 | NC | 1 |
| 609 | | 5 | max | .383 | 31 | .03 | 23 | .04 | 23 | 1.125e-03 | 9 | NC | 1 |
| 610 | | | min | -.041 | 25 | -.033 | 5 | -.044 | 5 | -9.608e-04 | 15 | NC | 1 |
| 611 | M59B | 1 | max | .417 | 33 | .025 | 23 | .042 | 4 | 6.162e-04 | 24 | NC | 1 |
| 612 | | | min | -.037 | 15 | -.032 | 5 | -.041 | 22 | -8.677e-04 | 6 | NC | 1 |
| 613 | | 2 | max | .417 | 33 | .026 | 23 | .042 | 4 | 6.162e-04 | 24 | NC | 1 |
| 614 | | | min | -.037 | 15 | -.032 | 5 | -.041 | 22 | -8.677e-04 | 6 | NC | 1 |
| 615 | | 3 | max | .417 | 33 | .028 | 23 | .042 | 4 | 6.162e-04 | 24 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | |
|--------|-------|--------|------|--------|-------|--------|-------|-----------------|------------|------------|--------|-----------|----|----------|
| 616 | | min | .037 | 15 | -.033 | 5 | -.041 | 22 | -8.677e-04 | 6 | NC | 1 | NC | |
| 617 | | 4 | max | .417 | 33 | .029 | 23 | .042 | 5 | 6.162e-04 | 24 | NC | 1 | NC |
| 618 | | | min | -.037 | 15 | -.033 | 5 | -.041 | 23 | -8.677e-04 | 6 | NC | 1 | NC |
| 619 | | 5 | max | .417 | 33 | .03 | 23 | .043 | 5 | 6.162e-04 | 24 | NC | 1 | NC |
| 620 | | | min | -.037 | 15 | -.034 | 5 | -.042 | 23 | -8.677e-04 | 6 | NC | 1 | NC |
| 621 | M63C | 1 | max | .402 | 35 | .012 | 22 | .049 | 5 | 1.321e-03 | 12 | NC | 1 | NC |
| 622 | | | min | -.045 | 17 | -.017 | 4 | -.047 | 23 | -1.271e-03 | 18 | NC | 1 | NC |
| 623 | | 2 | max | .402 | 35 | .012 | 22 | .049 | 5 | 1.321e-03 | 12 | NC | 1 | NC |
| 624 | | | min | -.045 | 17 | -.017 | 4 | -.047 | 23 | -1.271e-03 | 18 | NC | 1 | NC |
| 625 | | 3 | max | .402 | 35 | .013 | 23 | .05 | 5 | 1.321e-03 | 12 | NC | 1 | NC |
| 626 | | | min | -.045 | 17 | -.018 | 5 | -.047 | 23 | -1.271e-03 | 18 | NC | 1 | NC |
| 627 | | 4 | max | .402 | 35 | .015 | 23 | .05 | 5 | 1.321e-03 | 12 | NC | 1 | NC |
| 628 | | | min | -.045 | 17 | -.019 | 5 | -.047 | 23 | -1.271e-03 | 18 | NC | 1 | NC |
| 629 | | 5 | max | .402 | 35 | .016 | 23 | .051 | 5 | 1.321e-03 | 12 | NC | 1 | NC |
| 630 | | | min | -.045 | 17 | -.02 | 5 | -.047 | 23 | -1.271e-03 | 18 | NC | 1 | NC |
| 631 | M64 2 | 1 | max | .404 | 37 | .063 | 5 | .011 | 2 | 3.097e-04 | 67 | NC | 1 | NC |
| 632 | | | min | -.033 | 19 | -.061 | 23 | -.006 | 20 | -5.848e-04 | 61 | NC | 1 | NC |
| 633 | | 2 | max | .404 | 37 | .061 | 5 | .01 | 3 | 3.097e-04 | 67 | NC | 1 | NC |
| 634 | | | min | -.033 | 19 | -.06 | 23 | -.006 | 21 | -5.848e-04 | 61 | NC | 1 | NC |
| 635 | | 3 | max | .404 | 37 | .059 | 5 | .009 | 3 | 3.097e-04 | 67 | NC | 1 | NC |
| 636 | | | min | -.033 | 19 | -.058 | 23 | -.006 | 21 | -5.848e-04 | 61 | NC | 1 | NC |
| 637 | | 4 | max | .404 | 37 | .057 | 5 | .008 | 3 | 3.097e-04 | 67 | NC | 1 | NC |
| 638 | | | min | -.033 | 19 | -.056 | 23 | -.006 | 21 | -5.848e-04 | 61 | NC | 1 | NC |
| 639 | | 5 | max | .404 | 37 | .055 | 5 | .008 | 4 | 3.097e-04 | 67 | NC | 1 | NC |
| 640 | | | min | -.033 | 19 | -.054 | 23 | -.007 | 22 | -5.848e-04 | 61 | NC | 1 | NC |
| 641 | M68 1 | 1 | max | .393 | 27 | .063 | 5 | .008 | 13 | 6.632e-04 | 5 | NC | 1 | NC |
| 642 | | | min | -.037 | 21 | -.061 | 23 | -.006 | 19 | -5.299e-04 | 23 | NC | 1 | NC |
| 643 | | 2 | max | .393 | 27 | .062 | 5 | .008 | 13 | 6.632e-04 | 5 | NC | 1 | NC |
| 644 | | | min | -.037 | 21 | -.059 | 23 | -.006 | 19 | -5.299e-04 | 23 | NC | 1 | NC |
| 645 | | 3 | max | .393 | 27 | .06 | 5 | .008 | 12 | 6.632e-04 | 5 | NC | 1 | NC |
| 646 | | | min | -.037 | 21 | -.057 | 23 | -.006 | 18 | -5.299e-04 | 23 | NC | 1 | NC |
| 647 | | 4 | max | .393 | 27 | .058 | 5 | .008 | 12 | 6.632e-04 | 5 | NC | 1 | NC |
| 648 | | | min | -.037 | 21 | -.055 | 23 | -.007 | 18 | -5.299e-04 | 23 | NC | 1 | NC |
| 649 | | 5 | max | .393 | 27 | .056 | 5 | .008 | 12 | 6.632e-04 | 5 | NC | 1 | NC |
| 650 | | | min | -.037 | 21 | -.053 | 23 | -.008 | 18 | -5.299e-04 | 23 | NC | 1 | NC |
| 651 | M69 1 | 1 | max | .399 | 29 | .011 | 12 | .047 | 23 | 8.778e-04 | 22 | NC | 1 | NC |
| 652 | | | min | -.048 | 23 | -.009 | 18 | -.052 | 5 | -1.249e-03 | 4 | NC | 1 | NC |
| 653 | | 2 | max | .399 | 29 | .011 | 12 | .047 | 23 | 8.778e-04 | 22 | NC | 1 | NC |
| 654 | | | min | -.048 | 23 | -.01 | 18 | -.052 | 5 | -1.249e-03 | 4 | NC | 1 | NC |
| 655 | | 3 | max | .399 | 29 | .011 | 11 | .047 | 23 | 8.778e-04 | 22 | NC | 1 | NC |
| 656 | | | min | -.048 | 23 | -.011 | 17 | -.051 | 5 | -1.249e-03 | 4 | NC | 1 | NC |
| 657 | | 4 | max | .399 | 29 | .013 | 23 | .047 | 23 | 8.778e-04 | 22 | NC | 1 | NC |
| 658 | | | min | -.048 | 23 | -.013 | 5 | -.051 | 5 | -1.249e-03 | 4 | NC | 1 | NC |
| 659 | | 5 | max | .399 | 29 | .014 | 23 | .047 | 23 | 8.778e-04 | 22 | NC | 1 | NC |
| 660 | | | min | -.048 | 23 | -.015 | 5 | -.05 | 5 | -1.249e-03 | 4 | NC | 1 | NC |
| 661 | M70 1 | 1 | max | .049 | 5 | .048 | 23 | .02 | 5 | 2.805e-03 | 40 | NC | 1 | NC |
| 662 | | | min | -.045 | 23 | -.399 | 29 | -.016 | 23 | -1.365e-03 | 23 | 721.417 | 13 | 1245.9 |
| 663 | | 2 | max | .049 | 5 | .042 | 24 | .012 | 5 | 2.965e-03 | 41 | NC | 1 | NC |
| 664 | | | min | -.045 | 23 | -.4 | 30 | -.01 | 23 | -1.101e-03 | 23 | 953.646 | 13 | 1827.285 |
| 665 | | 3 | max | .049 | 5 | .042 | 24 | .006 | 5 | 3.13e-03 | 42 | NC | 1 | NC |
| 666 | | | min | -.045 | 23 | -.398 | 30 | -.005 | 23 | -9.002e-04 | 24 | 844.224 | 22 | 2723.782 |
| 667 | | 4 | max | .049 | 5 | .041 | 24 | .005 | 61 | 3.31e-03 | 42 | NC | 1 | NC |
| 668 | | | min | -.045 | 23 | -.392 | 30 | -.004 | 67 | -9.157e-04 | 24 | 547.389 | 22 | 4961.89 |
| 669 | | 5 | max | .049 | 5 | .041 | 25 | .008 | 9 | 3.51e-03 | 43 | NC | 1 | NC |
| 670 | | | min | -.045 | 23 | -.383 | 31 | -.006 | 15 | -1.193e-03 | 25 | 417.558 | 22 | 3551.095 |
| 671 | M71 1 | 1 | max | .05 | 5 | .037 | 15 | .014 | 7 | 2.147e-03 | 8 | NC | 1 | NC |
| 672 | | | min | -.046 | 23 | -.417 | 33 | -.008 | 25 | -1.068e-03 | 14 | 586.262 | 5 | 4165.838 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|-------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 673 | | 2 | max | .05 | 5 | .034 | 16 | .009 | 8 | 1.804e-03 | 33 | NC | 1 |
| 674 | | | min | -.046 | 23 | -.417 | 34 | -.005 | 14 | -7.618e-04 | 15 | 771.205 | 5 |
| 675 | | 3 | max | .05 | 5 | .035 | 16 | .008 | 9 | 1.593e-03 | 34 | NC | 1 |
| 676 | | | min | -.046 | 23 | -.414 | 34 | -.005 | 15 | -6.175e-04 | 16 | 801.893 | 14 |
| 677 | | 4 | max | .05 | 5 | .036 | 16 | .01 | 10 | 1.539e-03 | 11 | NC | 1 |
| 678 | | | min | -.046 | 23 | -.409 | 34 | -.007 | 16 | -7.759e-04 | 17 | 520.079 | 14 |
| 679 | | 5 | max | .05 | 5 | .045 | 17 | .015 | 11 | 1.864e-03 | 12 | NC | 1 |
| 680 | | | min | -.046 | 23 | -.402 | 35 | -.011 | 17 | -1.158e-03 | 18 | 397.14 | 14 |
| 681 | M72_1 | 1 | max | .063 | 5 | .033 | 19 | .011 | 2 | 2.345e-03 | 12 | NC | 1 |
| 682 | | | min | -.061 | 23 | -.404 | 37 | -.006 | 20 | -1.213e-03 | 19 | 1602.445 | 70 |
| 683 | | 2 | max | .063 | 5 | .025 | 20 | .009 | 2 | 1.994e-03 | 37 | NC | 1 |
| 684 | | | min | -.061 | 23 | -.405 | 26 | -.005 | 20 | -8.911e-04 | 19 | 2116.23 | 70 |
| 685 | | 3 | max | .063 | 5 | .026 | 20 | .008 | 13 | 1.838e-03 | 26 | NC | 1 |
| 686 | | | min | -.061 | 23 | -.404 | 26 | -.005 | 19 | -8.182e-04 | 20 | 1310.531 | 7 |
| 687 | | 4 | max | .063 | 5 | .026 | 20 | .008 | 13 | 1.986e-03 | 3 | NC | 1 |
| 688 | | | min | -.061 | 23 | -.399 | 26 | -.006 | 19 | -1.104e-03 | 21 | 850.652 | 7 |
| 689 | | 5 | max | .063 | 5 | .037 | 21 | .008 | 13 | 2.44e-03 | 4 | NC | 1 |
| 690 | | | min | -.061 | 23 | -.393 | 27 | -.006 | 19 | -1.597e-03 | 22 | 651.993 | 7 |
| 691 | M73_1 | 1 | max | .338 | 31 | .03 | 23 | .03 | 23 | 1.062e-03 | 25 | NC | 1 |
| 692 | | | min | -.032 | 25 | -.033 | 5 | -.036 | 5 | -1.284e-03 | 7 | NC | 1 |
| 693 | | 2 | max | .338 | 31 | .031 | 23 | .031 | 23 | 1.062e-03 | 25 | NC | 1 |
| 694 | | | min | -.032 | 25 | -.035 | 5 | -.037 | 5 | -1.284e-03 | 7 | NC | 1 |
| 695 | | 3 | max | .338 | 31 | .031 | 23 | .031 | 23 | 1.062e-03 | 25 | NC | 1 |
| 696 | | | min | -.032 | 25 | -.037 | 5 | -.037 | 5 | -1.284e-03 | 7 | NC | 1 |
| 697 | | 4 | max | .338 | 31 | .032 | 23 | .032 | 23 | 1.062e-03 | 25 | NC | 1 |
| 698 | | | min | -.032 | 25 | -.039 | 5 | -.038 | 5 | -1.284e-03 | 7 | NC | 1 |
| 699 | | 5 | max | .338 | 31 | .033 | 23 | .032 | 23 | 1.062e-03 | 25 | NC | 1 |
| 700 | | | min | -.032 | 25 | -.04 | 5 | -.039 | 5 | -1.284e-03 | 7 | NC | 1 |
| 701 | M74_1 | 1 | max | 0 | 7 | .056 | 5 | .338 | 31 | 1.204e-03 | 23 | NC | 1 |
| 702 | | | min | 0 | 25 | -.046 | 23 | -.032 | 25 | -3.147e-03 | 29 | 434.182 | 8 |
| 703 | | 2 | max | 0 | 7 | .035 | 6 | .268 | 31 | 9.031e-04 | 23 | NC | 1 |
| 704 | | | min | 0 | 25 | -.025 | 24 | -.024 | 25 | -2.36e-03 | 29 | 591.144 | 8 |
| 705 | | 3 | max | 0 | 7 | .025 | 30 | .189 | 31 | 6.021e-04 | 23 | NC | 1 |
| 706 | | | min | 0 | 25 | -.013 | 25 | -.016 | 25 | -1.574e-03 | 29 | 907.924 | 8 |
| 707 | | 4 | max | 0 | 7 | .015 | 31 | .099 | 31 | 3.01e-04 | 23 | NC | 1 |
| 708 | | | min | 0 | 25 | -.007 | 25 | -.008 | 25 | -7.868e-04 | 29 | 1851.702 | 8 |
| 709 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 710 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 711 | M75_1 | 1 | max | .372 | 33 | .03 | 23 | .032 | 17 | 1.458e-03 | 9 | NC | 1 |
| 712 | | | min | -.031 | 15 | -.034 | 5 | -.032 | 23 | -1.323e-03 | 15 | NC | 1 |
| 713 | | 2 | max | .372 | 33 | .031 | 23 | .032 | 17 | 1.458e-03 | 9 | NC | 1 |
| 714 | | | min | -.031 | 15 | -.034 | 5 | -.032 | 23 | -1.323e-03 | 15 | NC | 1 |
| 715 | | 3 | max | .372 | 33 | .033 | 23 | .033 | 17 | 1.458e-03 | 9 | NC | 1 |
| 716 | | | min | -.031 | 15 | -.034 | 5 | -.033 | 23 | -1.323e-03 | 15 | NC | 1 |
| 717 | | 4 | max | .372 | 33 | .034 | 23 | .034 | 17 | 1.458e-03 | 9 | NC | 1 |
| 718 | | | min | -.031 | 15 | -.034 | 5 | -.034 | 11 | -1.323e-03 | 15 | NC | 1 |
| 719 | | 5 | max | .372 | 33 | .036 | 11 | .034 | 17 | 1.458e-03 | 9 | NC | 1 |
| 720 | | | min | -.031 | 15 | -.035 | 17 | -.035 | 11 | -1.323e-03 | 15 | NC | 1 |
| 721 | M76_1 | 1 | max | 0 | 9 | .372 | 33 | .05 | 11 | 2.77e-03 | 36 | NC | 1 |
| 722 | | | min | 0 | 15 | -.031 | 15 | -.049 | 17 | -1.138e-03 | 18 | 388.378 | 8 |
| 723 | | 2 | max | 0 | 9 | .293 | 33 | .03 | 10 | 2.077e-03 | 36 | NC | 1 |
| 724 | | | min | 0 | 15 | -.023 | 15 | -.027 | 16 | -8.535e-04 | 18 | 527.606 | 8 |
| 725 | | 3 | max | 0 | 9 | .206 | 33 | .019 | 9 | 1.385e-03 | 36 | NC | 1 |
| 726 | | | min | 0 | 15 | -.016 | 15 | -.015 | 15 | -5.69e-04 | 18 | 808.26 | 8 |
| 727 | | 4 | max | 0 | 9 | .107 | 33 | .011 | 9 | 6.925e-04 | 36 | NC | 1 |
| 728 | | | min | 0 | 15 | -.008 | 15 | -.008 | 15 | -2.845e-04 | 18 | 1640.73 | 9 |
| 729 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|-------|--------|-------|--------|-------|--------|-------|-----------------|------------|-----------|----------|-----------|----------|
| 730 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC |
| 731 | M77 1 | 1 | max | .364 | 35 | .008 | 22 | .045 | 5 | 3.102e-04 | 19 | NC | 1 |
| 732 | | min | -.04 | 17 | -.01 | 4 | -.042 | 23 | -.9106e-04 | 37 | NC | 1 | NC |
| 733 | | 2 | max | .364 | 35 | .009 | 23 | .045 | 5 | 3.102e-04 | 19 | NC | 1 |
| 734 | | min | -.04 | 17 | -.011 | 5 | -.041 | 23 | -.9106e-04 | 37 | NC | 1 | NC |
| 735 | | 3 | max | .364 | 35 | .009 | 23 | .046 | 5 | 3.102e-04 | 19 | NC | 1 |
| 736 | | min | -.04 | 17 | -.011 | 5 | -.041 | 23 | -.9106e-04 | 37 | NC | 1 | NC |
| 737 | | 4 | max | .364 | 35 | .01 | 23 | .046 | 5 | 3.102e-04 | 19 | NC | 1 |
| 738 | | min | -.04 | 17 | -.012 | 5 | -.04 | 23 | -.9106e-04 | 37 | NC | 1 | NC |
| 739 | | 5 | max | .364 | 35 | .011 | 23 | .046 | 5 | 3.102e-04 | 19 | NC | 1 |
| 740 | | min | -.04 | 17 | -.012 | 5 | -.039 | 23 | -.9106e-04 | 37 | NC | 1 | NC |
| 741 | M78 1 | 1 | max | 0 | 11 | .048 | 5 | .364 | 35 | 1.031e-03 | 14 | NC | 1 |
| 742 | | min | 0 | 17 | -.041 | 23 | -.04 | 17 | -3.006e-03 | 32 | 323.703 | 12 | 463.512 |
| 743 | | 2 | max | 0 | 11 | .042 | 4 | .287 | 35 | 7.733e-04 | 14 | NC | 1 |
| 744 | | min | 0 | 17 | -.034 | 22 | -.029 | 17 | -2.255e-03 | 32 | 438.987 | 12 | 665.475 |
| 745 | | 3 | max | 0 | 11 | .037 | 3 | .202 | 35 | 5.155e-04 | 14 | NC | 1 |
| 746 | | min | 0 | 17 | -.029 | 21 | -.018 | 17 | -1.503e-03 | 32 | 671.169 | 12 | 1090.794 |
| 747 | | 4 | max | 0 | 11 | .023 | 3 | .105 | 36 | 2.578e-04 | 14 | NC | 1 |
| 748 | | min | 0 | 17 | -.019 | 21 | -.01 | 18 | -7.516e-04 | 32 | 1363.611 | 12 | 2251.626 |
| 749 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 750 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC |
| 751 | M79 1 | 1 | max | .357 | 37 | .045 | 17 | .013 | 4 | 1.731e-03 | 12 | NC | 1 |
| 752 | | min | -.026 | 19 | -.045 | 11 | -.011 | 22 | -1.522e-03 | 18 | NC | 1 | NC |
| 753 | | 2 | max | .357 | 37 | .044 | 17 | .012 | 5 | 1.731e-03 | 12 | NC | 1 |
| 754 | | min | -.026 | 19 | -.045 | 11 | -.011 | 23 | -1.522e-03 | 18 | NC | 1 | NC |
| 755 | | 3 | max | .357 | 37 | .042 | 17 | .012 | 5 | 1.731e-03 | 12 | NC | 1 |
| 756 | | min | -.026 | 19 | -.044 | 11 | -.011 | 23 | -1.522e-03 | 18 | NC | 1 | NC |
| 757 | | 4 | max | .357 | 37 | .041 | 17 | .012 | 17 | 1.731e-03 | 12 | NC | 1 |
| 758 | | min | -.026 | 19 | -.043 | 11 | -.012 | 11 | -1.522e-03 | 18 | NC | 1 | NC |
| 759 | | 5 | max | .357 | 37 | .039 | 17 | .011 | 17 | 1.731e-03 | 12 | NC | 1 |
| 760 | | min | -.026 | 19 | -.043 | 11 | -.012 | 11 | -1.522e-03 | 18 | NC | 1 | NC |
| 761 | M80 1 | 1 | max | 0 | 12 | .357 | 37 | .045 | 11 | 2.903e-03 | 28 | NC | 1 |
| 762 | | min | 0 | 18 | -.026 | 19 | -.041 | 17 | -1.117e-03 | 22 | 425.654 | 13 | 625.274 |
| 763 | | 2 | max | 0 | 12 | .283 | 37 | .052 | 11 | 2.177e-03 | 28 | NC | 1 |
| 764 | | min | 0 | 18 | -.022 | 19 | -.047 | 17 | -8.379e-04 | 22 | 576.312 | 13 | 963.496 |
| 765 | | 3 | max | 0 | 12 | .2 | 37 | .049 | 11 | 1.451e-03 | 28 | NC | 1 |
| 766 | | min | 0 | 18 | -.018 | 18 | -.043 | 17 | -5.586e-04 | 22 | 879.494 | 13 | 1617.922 |
| 767 | | 4 | max | 0 | 12 | .104 | 36 | .03 | 11 | 7.257e-04 | 28 | NC | 1 |
| 768 | | min | 0 | 18 | -.011 | 18 | -.026 | 17 | -2.793e-04 | 22 | 1784.091 | 13 | 2270.767 |
| 769 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 770 | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 | NC |
| 771 | M81 1 | 1 | max | .349 | 27 | .051 | 5 | .012 | 11 | 1.414e-03 | 22 | NC | 1 |
| 772 | | min | -.026 | 21 | -.047 | 23 | -.011 | 17 | -1.614e-03 | 4 | NC | 1 | NC |
| 773 | | 2 | max | .349 | 27 | .051 | 5 | .012 | 23 | 1.414e-03 | 22 | NC | 1 |
| 774 | | min | -.026 | 21 | -.045 | 23 | -.012 | 5 | -1.614e-03 | 4 | NC | 1 | NC |
| 775 | | 3 | max | .349 | 27 | .05 | 5 | .012 | 23 | 1.414e-03 | 22 | NC | 1 |
| 776 | | min | -.026 | 21 | -.044 | 23 | -.012 | 5 | -1.614e-03 | 4 | NC | 1 | NC |
| 777 | | 4 | max | .349 | 27 | .049 | 5 | .012 | 23 | 1.414e-03 | 22 | NC | 1 |
| 778 | | min | -.026 | 21 | -.043 | 23 | -.013 | 5 | -1.614e-03 | 4 | NC | 1 | NC |
| 779 | | 5 | max | .349 | 27 | .049 | 5 | .012 | 23 | 1.414e-03 | 22 | NC | 1 |
| 780 | | min | -.026 | 21 | -.041 | 23 | -.014 | 5 | -1.614e-03 | 4 | NC | 1 | NC |
| 781 | M82 1 | 1 | max | 0 | 4 | .051 | 5 | .349 | 27 | 1.006e-03 | 18 | NC | 1 |
| 782 | | min | 0 | 22 | -.043 | 23 | -.026 | 21 | -3.045e-03 | 36 | 467.758 | 3 | 599.952 |
| 783 | | 2 | max | 0 | 4 | .057 | 5 | .276 | 27 | 7.546e-04 | 18 | NC | 1 |
| 784 | | min | 0 | 22 | -.048 | 23 | -.022 | 21 | -2.284e-03 | 36 | 634.287 | 3 | 918.686 |
| 785 | | 3 | max | 0 | 4 | .052 | 5 | .195 | 27 | 5.031e-04 | 18 | NC | 1 |
| 786 | | min | 0 | 22 | -.044 | 23 | -.017 | 22 | -1.523e-03 | 36 | 969.664 | 3 | 1617.917 |

Company : GeoStructural, LLC
 Designer : Jesse Drennen, PE
 Job Number :
 Model Name : CT33XC566

Mar 19, 2018
 11:12 AM
 Checked By: DWG

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|--------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 787 | | 4 | max | 0 | 4 | .032 | 5 | .102 | 28 | 2.515e-04 | 18 | NC | 1 |
| 788 | | | min | 0 | 22 | -.027 | 23 | -.011 | 22 | -7.613e-04 | 36 | 1969.888 | 3 |
| 789 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 790 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 791 | M83 1 | 1 | max | .346 | 29 | .01 | 47 | .045 | 23 | 5.372e-04 | 3 | NC | 1 |
| 792 | | | min | -.036 | 23 | -.007 | 17 | -.045 | 5 | -5.294e-04 | 9 | NC | 1 |
| 793 | | 2 | max | .346 | 29 | .01 | 11 | .045 | 11 | 5.372e-04 | 3 | NC | 1 |
| 794 | | | min | -.036 | 23 | -.008 | 17 | -.044 | 17 | -5.294e-04 | 9 | NC | 1 |
| 795 | | 3 | max | .346 | 29 | .011 | 11 | .045 | 11 | 5.372e-04 | 3 | NC | 1 |
| 796 | | | min | -.036 | 23 | -.009 | 17 | -.043 | 17 | -5.294e-04 | 9 | NC | 1 |
| 797 | | 4 | max | .346 | 29 | .011 | 11 | .045 | 11 | 5.372e-04 | 3 | NC | 1 |
| 798 | | | min | -.036 | 23 | -.01 | 17 | -.042 | 17 | -5.294e-04 | 9 | NC | 1 |
| 799 | | 5 | max | .346 | 29 | .012 | 11 | .045 | 11 | 5.372e-04 | 3 | NC | 1 |
| 800 | | | min | -.036 | 23 | -.011 | 17 | -.041 | 17 | -5.294e-04 | 9 | NC | 1 |
| 801 | M84 1 | 1 | max | 0 | 29 | .346 | 29 | .046 | 11 | 2.95e-03 | 31 | NC | 1 |
| 802 | | | min | 0 | 23 | -.036 | 23 | -.042 | 17 | -9.353e-04 | 25 | 334.775 | 4 |
| 803 | | 2 | max | 0 | 29 | .274 | 29 | .038 | 12 | 2.213e-03 | 31 | NC | 1 |
| 804 | | | min | 0 | 23 | -.026 | 23 | -.033 | 18 | -7.015e-04 | 25 | 454.268 | 4 |
| 805 | | 3 | max | 0 | 29 | .193 | 29 | .033 | 13 | 1.475e-03 | 31 | NC | 1 |
| 806 | | | min | 0 | 23 | -.016 | 23 | -.027 | 19 | -4.677e-04 | 25 | 695 | 4 |
| 807 | | 4 | max | 0 | 29 | .101 | 29 | .021 | 13 | 7.375e-04 | 31 | NC | 1 |
| 808 | | | min | 0 | 23 | -.009 | 22 | -.018 | 19 | -2.338e-04 | 25 | 1412.823 | 4 |
| 809 | | 5 | max | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 810 | | | min | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | NC | 1 |
| 811 | M55A | 1 | max | .05 | 14 | .025 | 14 | .03 | 23 | 1.291e-03 | 17 | NC | 1 |
| 812 | | | min | -.059 | 8 | -.266 | 32 | -.033 | 5 | -1.359e-03 | 11 | NC | 1 |
| 813 | | 2 | max | .05 | 14 | .024 | 14 | .031 | 23 | 1.291e-03 | 17 | NC | 1 |
| 814 | | | min | -.059 | 8 | -.263 | 32 | -.035 | 5 | -1.359e-03 | 11 | NC | 1 |
| 815 | | 3 | max | .05 | 14 | .024 | 14 | .033 | 23 | 1.291e-03 | 17 | NC | 1 |
| 816 | | | min | -.059 | 8 | -.26 | 32 | -.037 | 5 | -1.359e-03 | 11 | NC | 1 |
| 817 | | 4 | max | .05 | 14 | .023 | 14 | .034 | 23 | 1.291e-03 | 17 | NC | 1 |
| 818 | | | min | -.059 | 8 | -.257 | 32 | -.039 | 5 | -1.359e-03 | 11 | NC | 1 |
| 819 | | 5 | max | .05 | 14 | .023 | 14 | .036 | 23 | 1.291e-03 | 17 | NC | 1 |
| 820 | | | min | -.059 | 8 | -.254 | 32 | -.04 | 5 | -1.359e-03 | 11 | NC | 1 |
| 821 | M61A 1 | 1 | max | .07 | 4 | .056 | 25 | .03 | 23 | 1.723e-03 | 43 | NC | 1 |
| 822 | | | min | -.07 | 22 | -.413 | 31 | -.034 | 5 | -6.917e-04 | 25 | NC | 1 |
| 823 | | 2 | max | .07 | 4 | .058 | 25 | .033 | 23 | 1.723e-03 | 43 | NC | 1 |
| 824 | | | min | -.07 | 22 | -.414 | 31 | -.036 | 5 | -6.917e-04 | 25 | NC | 1 |
| 825 | | 3 | max | .07 | 4 | .061 | 25 | .035 | 23 | 1.723e-03 | 43 | NC | 1 |
| 826 | | | min | -.07 | 22 | -.414 | 31 | -.038 | 5 | -6.917e-04 | 25 | NC | 1 |
| 827 | | 4 | max | .07 | 4 | .063 | 25 | .038 | 22 | 1.723e-03 | 43 | NC | 1 |
| 828 | | | min | -.07 | 22 | -.415 | 31 | -.041 | 4 | -6.917e-04 | 25 | NC | 1 |
| 829 | | 5 | max | .07 | 4 | .066 | 25 | .043 | 22 | 1.723e-03 | 43 | NC | 1 |
| 830 | | | min | -.07 | 22 | -.416 | 31 | -.044 | 4 | -6.917e-04 | 25 | NC | 1 |
| 831 | M61B | 1 | max | .034 | 5 | .09 | 24 | .055 | 17 | 2.884e-03 | 13 | NC | 1 |
| 832 | | | min | -.032 | 23 | -.091 | 6 | -.428 | 35 | -2.85e-03 | 7 | 1950.594 | 7 |
| 833 | | 2 | max | .034 | 5 | .028 | 23 | .041 | 17 | 1.444e-03 | 25 | NC | 1 |
| 834 | | | min | -.032 | 23 | -.032 | 5 | -.371 | 35 | -1.943e-03 | 7 | 2928.876 | 13 |
| 835 | | 3 | max | .034 | 5 | .06 | 12 | .03 | 18 | 1.299e-04 | 17 | NC | 2 |
| 836 | | | min | -.032 | 23 | -.045 | 18 | -.277 | 36 | -2.061e-03 | 36 | 4085.855 | 19 |
| 837 | | 4 | max | .033 | 5 | .037 | 17 | .027 | 19 | 1.489e-03 | 23 | NC | 6 |
| 838 | | | min | -.032 | 23 | -.039 | 11 | -.366 | 37 | -1.654e-03 | 5 | 2643.751 | 12 |
| 839 | | 5 | max | .033 | 5 | .03 | 61 | .051 | 19 | 3.353e-03 | 11 | NC | 1 |
| 840 | | | min | -.031 | 23 | -.018 | 67 | -.442 | 37 | -2.706e-03 | 17 | 6292.516 | 3 |
| 841 | M62B 1 | 1 | max | .035 | 5 | .027 | 53 | .057 | 21 | 3.18e-03 | 5 | NC | 1 |
| 842 | | | min | -.033 | 23 | -.025 | 71 | -.424 | 27 | -3.034e-03 | 23 | 9171.399 | 61 |
| 843 | | 2 | max | .035 | 5 | .038 | 23 | .028 | 21 | 1.578e-03 | 17 | NC | 3 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | | |
|--------|--------|--------|-------|--------|-------|--------|-------|-----------------|------------|-----------|----------|-----------|----------|----|---|
| 844 | | min | -.033 | 23 | -.043 | 5 | -.357 | .27 | -1.981e-03 | 11 | 2166.964 | 5 | 1255.829 | 24 | |
| 845 | 3 | max | .035 | 5 | .055 | 4 | .019 | .22 | 2.017e-04 | 22 | NC | 1 | NC | 2 | |
| 846 | | min | -.034 | 23 | -.046 | 22 | -.256 | .28 | -1.842e-03 | 28 | NC | 1 | 916.255 | 27 | |
| 847 | 4 | max | .036 | 5 | .028 | 17 | .038 | .23 | 1.462e-03 | 15 | NC | 1 | NC | 10 | |
| 848 | | min | -.034 | 23 | -.03 | 11 | -.356 | .29 | -1.536e-03 | 9 | 3351.024 | 4 | 1316.809 | 20 | |
| 849 | 5 | max | .036 | 5 | .089 | 4 | .067 | .23 | 3.32e-03 | 4 | NC | 1 | NC | 1 | |
| 850 | | min | -.034 | 23 | -.073 | 22 | -.441 | .29 | -2.545e-03 | 22 | NC | 1 | 779.899 | 43 | |
| 851 | M79A 1 | 1 | max | .076 | 6 | .053 | 17 | .032 | .23 | 8.487e-04 | 12 | NC | 1 | NC | 1 |
| 852 | | min | -.073 | 24 | -.424 | 35 | -.034 | 5 | -4.401e-04 | 18 | NC | 1 | NC | 1 | |
| 853 | 2 | max | .076 | 6 | .056 | 17 | .036 | .23 | 8.487e-04 | 12 | NC | 1 | NC | 1 | |
| 854 | | min | -.073 | 24 | -.424 | 35 | -.037 | 5 | -4.401e-04 | 18 | NC | 1 | NC | 1 | |
| 855 | 3 | max | .076 | 6 | .059 | 17 | .039 | .23 | 8.487e-04 | 12 | NC | 1 | NC | 1 | |
| 856 | | min | -.073 | 24 | -.424 | 35 | -.039 | 5 | -4.401e-04 | 18 | NC | 1 | NC | 1 | |
| 857 | 4 | max | .076 | 6 | .062 | 17 | .042 | .23 | 8.487e-04 | 12 | NC | 1 | NC | 1 | |
| 858 | | min | -.073 | 24 | -.425 | 35 | -.042 | 5 | -4.401e-04 | 18 | NC | 1 | NC | 1 | |
| 859 | 5 | max | .076 | 6 | .065 | 17 | .045 | .11 | 8.487e-04 | 12 | NC | 1 | NC | 1 | |
| 860 | | min | -.073 | 24 | -.425 | 35 | -.045 | 5 | -4.401e-04 | 18 | NC | 1 | NC | 1 | |
| 861 | M97 | 1 | max | .02 | 71 | .053 | 21 | .033 | .23 | 1.36e-03 | 4 | NC | 1 | NC | 1 |
| 862 | | min | -.02 | 53 | -.419 | 27 | -.035 | 5 | -9.134e-04 | 22 | NC | 1 | NC | 1 | |
| 863 | 2 | max | .02 | 71 | .056 | 21 | .029 | .23 | 1.36e-03 | 4 | NC | 1 | NC | 1 | |
| 864 | | min | -.02 | 53 | -.419 | 27 | -.03 | 5 | -9.134e-04 | 22 | NC | 1 | NC | 1 | |
| 865 | 3 | max | .02 | 71 | .059 | 21 | .025 | .23 | 1.36e-03 | 4 | NC | 1 | NC | 1 | |
| 866 | | min | -.02 | 53 | -.42 | 27 | -.025 | 5 | -9.134e-04 | 22 | NC | 1 | NC | 1 | |
| 867 | 4 | max | .02 | 71 | .062 | 21 | .021 | .23 | 1.36e-03 | 4 | NC | 1 | NC | 1 | |
| 868 | | min | -.02 | 53 | -.421 | 27 | -.021 | 5 | -9.134e-04 | 22 | NC | 1 | NC | 1 | |
| 869 | 5 | max | .02 | 71 | .065 | 21 | .016 | 11 | 1.36e-03 | 4 | NC | 1 | NC | 1 | |
| 870 | | min | -.02 | 53 | -.421 | 27 | -.016 | 17 | -9.134e-04 | 22 | NC | 1 | NC | 1 | |
| 871 | M110 | 1 | max | .055 | 23 | .051 | 15 | .03 | .23 | 7.34e-04 | 15 | NC | 1 | NC | 1 |
| 872 | | min | -.064 | 5 | -.443 | 33 | -.034 | 5 | -1.227e-03 | 9 | NC | 1 | NC | 1 | |
| 873 | 2 | max | .055 | 23 | .053 | 15 | .031 | .23 | 7.34e-04 | 15 | NC | 1 | NC | 1 | |
| 874 | | min | -.064 | 5 | -.445 | 33 | -.036 | 5 | -1.227e-03 | 9 | NC | 1 | NC | 1 | |
| 875 | 3 | max | .055 | 23 | .056 | 15 | .033 | .23 | 7.34e-04 | 15 | NC | 1 | NC | 1 | |
| 876 | | min | -.064 | 5 | -.448 | 33 | -.038 | 5 | -1.227e-03 | 9 | NC | 1 | NC | 1 | |
| 877 | 4 | max | .055 | 23 | .058 | 15 | .034 | .23 | 7.34e-04 | 15 | NC | 1 | NC | 1 | |
| 878 | | min | -.064 | 5 | -.45 | 33 | -.041 | 5 | -1.227e-03 | 9 | NC | 1 | NC | 1 | |
| 879 | 5 | max | .055 | 23 | .061 | 15 | .037 | .24 | 7.34e-04 | 15 | NC | 1 | NC | 1 | |
| 880 | | min | -.064 | 5 | -.452 | 33 | -.044 | 6 | -1.227e-03 | 9 | NC | 1 | NC | 1 | |
| 881 | M111 | 1 | max | .018 | 22 | .047 | 19 | .031 | .23 | 8.209e-04 | 18 | NC | 1 | NC | 1 |
| 882 | | min | -.026 | 4 | -.435 | 37 | -.033 | 5 | -1.437e-03 | 12 | NC | 1 | NC | 1 | |
| 883 | 2 | max | .018 | 22 | .05 | 19 | .028 | .23 | 8.209e-04 | 18 | NC | 1 | NC | 1 | |
| 884 | | min | -.026 | 4 | -.438 | 37 | -.031 | 5 | -1.437e-03 | 12 | NC | 1 | NC | 1 | |
| 885 | 3 | max | .018 | 22 | .053 | 19 | .024 | .23 | 8.209e-04 | 18 | NC | 1 | NC | 1 | |
| 886 | | min | -.026 | 4 | -.44 | 37 | -.028 | 5 | -1.437e-03 | 12 | NC | 1 | NC | 1 | |
| 887 | 4 | max | .018 | 22 | .055 | 19 | .021 | .22 | 8.209e-04 | 18 | NC | 1 | NC | 1 | |
| 888 | | min | -.026 | 4 | -.442 | 37 | -.026 | 4 | -1.437e-03 | 12 | NC | 1 | NC | 1 | |
| 889 | 5 | max | .018 | 22 | .058 | 19 | .018 | .22 | 8.209e-04 | 18 | NC | 1 | NC | 1 | |
| 890 | | min | -.026 | 4 | -.444 | 37 | -.024 | 4 | -1.437e-03 | 12 | NC | 1 | NC | 1 | |
| 891 | M112 | 1 | max | .061 | 22 | .063 | 23 | .034 | .23 | 7.2e-04 | 22 | NC | 1 | NC | 1 |
| 892 | | min | -.073 | 4 | -.434 | 29 | -.036 | 5 | -1.379e-03 | 4 | NC | 1 | NC | 1 | |
| 893 | 2 | max | .061 | 22 | .066 | 23 | .036 | .23 | 7.2e-04 | 22 | NC | 1 | NC | 1 | |
| 894 | | min | -.073 | 4 | -.437 | 29 | -.039 | 5 | -1.379e-03 | 4 | NC | 1 | NC | 1 | |
| 895 | 3 | max | .061 | 22 | .069 | 23 | .039 | .23 | 7.2e-04 | 22 | NC | 1 | NC | 1 | |
| 896 | | min | -.073 | 4 | -.439 | 29 | -.043 | 5 | -1.379e-03 | 4 | NC | 1 | NC | 1 | |
| 897 | 4 | max | .061 | 22 | .072 | 23 | .041 | .23 | 7.2e-04 | 22 | NC | 1 | NC | 1 | |
| 898 | | min | -.073 | 4 | -.442 | 29 | -.046 | 5 | -1.379e-03 | 4 | NC | 1 | NC | 1 | |
| 899 | 5 | max | .061 | 22 | .075 | 23 | .044 | .23 | 7.2e-04 | 22 | NC | 1 | NC | 1 | |
| 900 | | min | -.073 | 4 | -.445 | 29 | -.05 | 5 | -1.379e-03 | 4 | NC | 1 | NC | 1 | |

Envelope Member Section Deflections (Continued)

| | Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|-----|--------|-----|-----------|----|--------|----|--------|----|-----------------|--------|-----------|--------|-----------|----|
| 901 | M108 | 1 | max .028 | 18 | .029 | 13 | .054 | 11 | 1.194e-03 | 17 | NC | 1 | NC | 1 |
| 902 | | | min -.262 | 36 | -.021 | 19 | -.05 | 17 | -1.321e-03 | 11 | NC | 1 | NC | 1 |
| 903 | | 2 | max .028 | 18 | .043 | 13 | .075 | 11 | 1.414e-03 | 17 | NC | 1 | NC | 1 |
| 904 | | | min -.262 | 36 | -.027 | 19 | -.064 | 17 | -1.508e-03 | 11 | 1873.438 | 37 | 2248.515 | 37 |
| 905 | | 3 | max .028 | 18 | .155 | 17 | .087 | 20 | 9.995e-04 | 17 | NC | 39 | NC | 1 |
| 906 | | | min -.262 | 36 | -.172 | 11 | -.098 | 2 | -1.041e-03 | 11 | 496.319 | 11 | 781.163 | 13 |
| 907 | | 4 | max .028 | 18 | .616 | 5 | .354 | 7 | 1.413e-03 | 4 | NC | 1 | NC | 1 |
| 908 | | | min -.263 | 36 | -.605 | 23 | -.347 | 25 | -1.394e-03 | 10 | 152.755 | 5 | 247.297 | 7 |
| 909 | | 5 | max .028 | 18 | 1.138 | 5 | .638 | 7 | 1.543e-03 | 4 | NC | 26 | NC | 4 |
| 910 | | | min -.263 | 36 | -1.079 | 23 | -.603 | 25 | -1.521e-03 | 10 | 83.453 | 5 | 142.801 | 7 |
| 911 | M109 | 1 | max .437 | 18 | .028 | 18 | .227 | 3 | 8.109e-03 | 15 | NC | 1 | NC | 1 |
| 912 | | | min -.449 | 12 | -.262 | 36 | -.226 | 21 | -8.199e-03 | 9 | NC | 1 | NC | 1 |
| 913 | | 2 | max .437 | 18 | -.036 | 67 | .228 | 3 | 8.109e-03 | 15 | NC | 1 | NC | 1 |
| 914 | | | min -.449 | 12 | -.258 | 36 | -.227 | 21 | -8.199e-03 | 9 | NC | 1 | NC | 1 |
| 915 | | 3 | max .437 | 18 | -.004 | 24 | .228 | 3 | 8.109e-03 | 15 | NC | 1 | NC | 1 |
| 916 | | | min -.449 | 12 | -.275 | 30 | -.227 | 21 | -8.199e-03 | 9 | NC | 1 | NC | 1 |
| 917 | | 4 | max .437 | 18 | .06 | 24 | .229 | 3 | 8.109e-03 | 15 | NC | 1 | NC | 1 |
| 918 | | | min -.449 | 12 | -.298 | 30 | -.227 | 21 | -8.199e-03 | 9 | NC | 1 | NC | 1 |
| 919 | | 5 | max .437 | 18 | .125 | 24 | .229 | 3 | 8.109e-03 | 15 | NC | 1 | NC | 1 |
| 920 | | | min -.449 | 12 | -.322 | 30 | -.228 | 21 | -8.199e-03 | 9 | NC | 1 | NC | 1 |
| 921 | M110A | 1 | max .229 | 3 | .121 | 24 | .447 | 12 | 2.048e-02 | 24 | NC | 1 | NC | 1 |
| 922 | | | min -.228 | 21 | -.323 | 30 | -.435 | 18 | -2.27e-02 | 6 | NC | 1 | NC | 1 |
| 923 | | 2 | max .229 | 3 | .123 | 24 | .448 | 12 | 2.048e-02 | 24 | NC | 1 | NC | 1 |
| 924 | | | min -.228 | 21 | -.322 | 30 | -.436 | 18 | -2.27e-02 | 6 | NC | 1 | NC | 1 |
| 925 | | 3 | max .229 | 3 | .125 | 24 | .449 | 12 | 2.048e-02 | 24 | NC | 1 | NC | 1 |
| 926 | | | min -.228 | 21 | -.322 | 30 | -.437 | 18 | -2.27e-02 | 6 | NC | 1 | NC | 1 |
| 927 | | 4 | max .229 | 3 | .126 | 24 | .45 | 12 | 2.048e-02 | 24 | NC | 1 | NC | 1 |
| 928 | | | min -.228 | 21 | -.321 | 30 | -.438 | 18 | -2.27e-02 | 6 | NC | 1 | NC | 1 |
| 929 | | 5 | max .229 | 3 | .14 | 23 | .451 | 12 | 2.048e-02 | 24 | NC | 1 | NC | 1 |
| 930 | | | min -.228 | 21 | -.322 | 29 | -.439 | 18 | -2.27e-02 | 6 | NC | 1 | NC | 1 |
| 931 | M111A | 1 | max .658 | 24 | .01 | 24 | .287 | 9 | 4.789e-03 | 21 | NC | 1 | NC | 1 |
| 932 | | | min -.67 | 6 | -.284 | 30 | -.287 | 3 | -4.776e-03 | 15 | NC | 1 | NC | 1 |
| 933 | | 2 | max .658 | 24 | -.026 | 24 | .289 | 9 | 4.789e-03 | 21 | NC | 1 | NC | 1 |
| 934 | | | min -.67 | 6 | -.271 | 30 | -.289 | 3 | -4.776e-03 | 15 | NC | 1 | NC | 1 |
| 935 | | 3 | max .658 | 24 | -.038 | 67 | .291 | 9 | 4.789e-03 | 21 | NC | 1 | NC | 1 |
| 936 | | | min -.67 | 6 | -.259 | 36 | -.291 | 3 | -4.776e-03 | 15 | NC | 1 | NC | 1 |
| 937 | | 4 | max .658 | 24 | -.011 | 18 | .293 | 9 | 4.789e-03 | 21 | NC | 1 | NC | 1 |
| 938 | | | min -.67 | 6 | -.261 | 36 | -.294 | 3 | -4.776e-03 | 15 | NC | 1 | NC | 1 |
| 939 | | 5 | max .658 | 24 | .028 | 18 | .296 | 9 | 4.789e-03 | 21 | NC | 1 | NC | 1 |
| 940 | | | min -.67 | 6 | -.263 | 36 | -.296 | 3 | -4.776e-03 | 15 | NC | 1 | NC | 1 |
| 941 | M112A | 1 | max .003 | 11 | -.026 | 18 | .049 | 22 | 1.299e-03 | 21 | NC | 1 | NC | 1 |
| 942 | | | min -.003 | 17 | -.208 | 36 | -.049 | 4 | -1.577e-03 | 3 | NC | 1 | NC | 1 |
| 943 | | 2 | max .003 | 11 | -.013 | 18 | .052 | 10 | 1.299e-03 | 21 | NC | 1 | NC | 1 |
| 944 | | | min -.003 | 17 | -.221 | 36 | -.052 | 16 | -1.577e-03 | 3 | NC | 1 | NC | 1 |
| 945 | | 3 | max .003 | 11 | 0 | 18 | .054 | 10 | 1.299e-03 | 21 | NC | 1 | NC | 1 |
| 946 | | | min -.003 | 17 | -.235 | 36 | -.054 | 16 | -1.577e-03 | 3 | NC | 1 | NC | 1 |
| 947 | | 4 | max .003 | 11 | .015 | 18 | .057 | 10 | 1.299e-03 | 21 | NC | 1 | NC | 1 |
| 948 | | | min -.003 | 17 | -.248 | 36 | -.057 | 16 | -1.577e-03 | 3 | NC | 1 | NC | 1 |
| 949 | | 5 | max .003 | 11 | .028 | 18 | .06 | 10 | 1.299e-03 | 21 | NC | 1 | NC | 1 |
| 950 | | | min -.003 | 17 | -.261 | 36 | -.059 | 16 | -1.577e-03 | 3 | NC | 1 | NC | 1 |
| 951 | M118 | 1 | max .017 | 22 | .023 | 22 | .055 | 4 | 8.888e-04 | 17 | NC | 1 | NC | 1 |
| 952 | | | min -.245 | 28 | -.025 | 4 | -.052 | 22 | -9.758e-04 | 11 | NC | 1 | NC | 1 |
| 953 | | 2 | max .017 | 22 | .027 | 22 | .068 | 5 | 8.363e-04 | 17 | NC | 1 | NC | 1 |
| 954 | | | min -.245 | 28 | -.041 | 4 | -.062 | 23 | -9.218e-04 | 11 | 1877.974 | 30 | 2477.718 | 12 |
| 955 | | 3 | max .017 | 22 | .17 | 5 | .08 | 20 | 7.8e-04 | 17 | NC | 30 | NC | 1 |
| 956 | | | min -.245 | 28 | -.156 | 23 | -.086 | 2 | -8.459e-04 | 11 | 503.986 | 5 | 824.724 | 3 |
| 957 | | 4 | max .017 | 22 | .621 | 17 | .335 | 9 | 1.613e-03 | 6 | NC | 39 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC | | |
|--------|------|--------|------|--------|-------|--------|-------|-----------------|------------|------------|---------|-----------|---------|---------|---|
| 958 | | min | .245 | 28 | -.639 | 11 | -.324 | 15 | -1.651e-03 | 12 | 145.967 | 11 | 257.299 | 9 | |
| 959 | | 5 | max | .017 | 22 | 1.116 | 17 | .609 | 9 | 1.715e-03 | 6 | NC | 26 | NC | 6 |
| 960 | | | min | -.246 | 28 | -1.179 | 11 | -.572 | 15 | -1.752e-03 | 12 | 80.106 | 11 | 148.323 | 9 |
| 961 | M119 | 1 | max | .441 | 10 | .017 | 22 | .219 | 7 | 8.042e-03 | 19 | NC | 1 | NC | 1 |
| 962 | | | min | -.444 | 4 | -.245 | 28 | -.218 | 25 | -8.139e-03 | 13 | NC | 1 | NC | 1 |
| 963 | | 2 | max | .441 | 10 | -.039 | 71 | .218 | 7 | 8.042e-03 | 19 | NC | 1 | NC | 1 |
| 964 | | | min | -.444 | 4 | -.241 | 36 | -.217 | 25 | -8.139e-03 | 13 | NC | 1 | NC | 1 |
| 965 | | 3 | max | .441 | 10 | .014 | 16 | .217 | 7 | 8.042e-03 | 19 | NC | 1 | NC | 1 |
| 966 | | | min | -.444 | 4 | -.264 | 34 | -.216 | 25 | -8.139e-03 | 13 | NC | 1 | NC | 1 |
| 967 | | 4 | max | .441 | 10 | .079 | 16 | .217 | 7 | 8.042e-03 | 19 | NC | 1 | NC | 1 |
| 968 | | | min | -.444 | 4 | -.288 | 34 | -.216 | 25 | -8.139e-03 | 13 | NC | 1 | NC | 1 |
| 969 | | 5 | max | .441 | 10 | .144 | 16 | .216 | 7 | 8.042e-03 | 19 | NC | 1 | NC | 1 |
| 970 | | | min | -.444 | 4 | -.311 | 34 | -.215 | 25 | -8.139e-03 | 13 | NC | 1 | NC | 1 |
| 971 | M120 | 1 | max | .216 | 7 | .166 | 17 | .449 | 4 | 2.068e-02 | 16 | NC | 1 | NC | 1 |
| 972 | | | min | -.215 | 25 | -.317 | 35 | -.446 | 10 | -2.295e-02 | 10 | NC | 1 | NC | 1 |
| 973 | | 2 | max | .216 | 7 | .151 | 17 | .447 | 4 | 2.068e-02 | 16 | NC | 1 | NC | 1 |
| 974 | | | min | -.215 | 25 | -.313 | 35 | -.444 | 10 | -2.295e-02 | 10 | NC | 1 | NC | 1 |
| 975 | | 3 | max | .216 | 7 | .144 | 16 | .444 | 4 | 2.068e-02 | 16 | NC | 1 | NC | 1 |
| 976 | | | min | -.215 | 25 | -.311 | 34 | -.441 | 10 | -2.295e-02 | 10 | NC | 1 | NC | 1 |
| 977 | | 4 | max | .216 | 7 | .141 | 16 | .442 | 4 | 2.068e-02 | 16 | NC | 1 | NC | 1 |
| 978 | | | min | -.215 | 25 | -.31 | 34 | -.439 | 10 | -2.295e-02 | 10 | NC | 1 | NC | 1 |
| 979 | | 5 | max | .216 | 7 | .138 | 16 | .44 | 4 | 2.068e-02 | 16 | NC | 1 | NC | 1 |
| 980 | | | min | -.215 | 25 | -.308 | 34 | -.437 | 10 | -2.295e-02 | 10 | NC | 1 | NC | 1 |
| 981 | M121 | 1 | max | .657 | 16 | -.003 | 16 | .279 | 13 | 4.784e-03 | 25 | NC | 1 | NC | 1 |
| 982 | | | min | -.677 | 10 | -.26 | 34 | -.279 | 7 | -4.769e-03 | 19 | NC | 1 | NC | 1 |
| 983 | | 2 | max | .657 | 16 | -.031 | 17 | .281 | 13 | 4.784e-03 | 25 | NC | 1 | NC | 1 |
| 984 | | | min | -.677 | 10 | -.249 | 34 | -.281 | 7 | -4.769e-03 | 19 | NC | 1 | NC | 1 |
| 985 | | 3 | max | .657 | 16 | -.034 | 71 | .283 | 13 | 4.784e-03 | 25 | NC | 1 | NC | 1 |
| 986 | | | min | -.677 | 10 | -.242 | 28 | -.283 | 7 | -4.769e-03 | 19 | NC | 1 | NC | 1 |
| 987 | | 4 | max | .657 | 16 | -.014 | 22 | .285 | 13 | 4.784e-03 | 25 | NC | 1 | NC | 1 |
| 988 | | | min | -.677 | 10 | -.244 | 28 | -.285 | 7 | -4.769e-03 | 19 | NC | 1 | NC | 1 |
| 989 | | 5 | max | .657 | 16 | .017 | 22 | .287 | 13 | 4.784e-03 | 25 | NC | 1 | NC | 1 |
| 990 | | | min | -.677 | 10 | -.245 | 28 | -.287 | 7 | -4.769e-03 | 19 | NC | 1 | NC | 1 |
| 991 | M122 | 1 | max | .001 | 13 | -.026 | 22 | .047 | 24 | 1.35e-03 | 25 | NC | 1 | NC | 1 |
| 992 | | | min | 0 | 19 | -.209 | 28 | -.047 | 6 | -1.626e-03 | 7 | NC | 1 | NC | 1 |
| 993 | | 2 | max | .001 | 13 | -.016 | 22 | .048 | 12 | 1.35e-03 | 25 | NC | 1 | NC | 1 |
| 994 | | | min | 0 | 19 | -.218 | 28 | -.048 | 6 | -1.626e-03 | 7 | NC | 1 | NC | 1 |
| 995 | | 3 | max | .001 | 13 | -.005 | 22 | .049 | 12 | 1.35e-03 | 25 | NC | 1 | NC | 1 |
| 996 | | | min | 0 | 19 | -.227 | 28 | -.049 | 18 | -1.626e-03 | 7 | NC | 1 | NC | 1 |
| 997 | | 4 | max | .001 | 13 | .006 | 22 | .05 | 12 | 1.35e-03 | 25 | NC | 1 | NC | 1 |
| 998 | | | min | 0 | 19 | -.236 | 28 | -.05 | 18 | -1.626e-03 | 7 | NC | 1 | NC | 1 |
| 999 | | 5 | max | .001 | 13 | .017 | 22 | .052 | 12 | 1.35e-03 | 25 | NC | 1 | NC | 1 |
| 1000 | | | min | 0 | 19 | -.244 | 28 | -.051 | 18 | -1.626e-03 | 7 | NC | 1 | NC | 1 |
| 1001 | M128 | 1 | max | .346 | 8 | .02 | 16 | .243 | 5 | 5.885e-03 | 16 | NC | 1 | NC | 1 |
| 1002 | | | min | -.346 | 2 | -.45 | 33 | -.237 | 23 | -6.011e-03 | 10 | NC | 1 | NC | 1 |
| 1003 | | 2 | max | .346 | 8 | .028 | 15 | .238 | 5 | 5.885e-03 | 16 | NC | 1 | NC | 1 |
| 1004 | | | min | -.346 | 2 | -.45 | 33 | -.233 | 23 | -6.011e-03 | 10 | NC | 1 | NC | 1 |
| 1005 | | 3 | max | .346 | 8 | .039 | 15 | .232 | 5 | 5.885e-03 | 16 | NC | 1 | NC | 1 |
| 1006 | | | min | -.346 | 2 | -.451 | 33 | -.228 | 23 | -6.011e-03 | 10 | NC | 1 | NC | 1 |
| 1007 | | 4 | max | .346 | 8 | .05 | 15 | .227 | 5 | 5.885e-03 | 16 | NC | 1 | NC | 1 |
| 1008 | | | min | -.346 | 2 | -.452 | 33 | -.223 | 23 | -6.011e-03 | 10 | NC | 1 | NC | 1 |
| 1009 | | 5 | max | .346 | 8 | .061 | 15 | .222 | 5 | 5.885e-03 | 16 | NC | 1 | NC | 1 |
| 1010 | | | min | -.346 | 2 | -.453 | 33 | -.219 | 23 | -6.011e-03 | 10 | NC | 1 | NC | 1 |
| 1011 | M129 | 1 | max | .419 | 24 | .014 | 20 | .287 | 9 | 5.441e-03 | 21 | NC | 1 | NC | 1 |
| 1012 | | | min | -.421 | 6 | -.441 | 37 | -.287 | 3 | -5.748e-03 | 3 | NC | 1 | NC | 1 |
| 1013 | | 2 | max | .419 | 24 | .025 | 19 | .283 | 21 | 5.441e-03 | 21 | NC | 1 | NC | 1 |
| 1014 | | | min | -.421 | 6 | -.442 | 37 | -.283 | 3 | -5.748e-03 | 3 | NC | 1 | NC | 1 |

Envelope Member Section Deflections (Continued)

| Member | Sec | x [in] | LC | y [in] | LC | z [in] | LC | x Rotate [r...] | LC (n) | L/y Ratio | LC (n) | L/z Ratio | LC |
|--------|-------|--------|-----|--------|----|--------|----|-----------------|--------|------------|--------|-----------|----|
| 1015 | | 3 | max | .419 | 24 | .036 | 19 | .279 | 21 | 5.441e-03 | 21 | NC | 1 |
| 1016 | | | min | -.421 | 6 | -.443 | 37 | -.28 | 3 | -5.748e-03 | 3 | NC | 1 |
| 1017 | | 4 | max | .419 | 24 | .047 | 19 | .275 | 21 | 5.441e-03 | 21 | NC | 1 |
| 1018 | | | min | -.421 | 6 | -.444 | 37 | -.277 | 3 | -5.748e-03 | 3 | NC | 1 |
| 1019 | | 5 | max | .419 | 24 | .058 | 19 | .271 | 21 | 5.441e-03 | 21 | NC | 1 |
| 1020 | | | min | -.421 | 6 | -.444 | 37 | -.273 | 3 | -5.748e-03 | 3 | NC | 1 |
| 1021 | M130 | 1 | max | .307 | 4 | .032 | 23 | .279 | 13 | 6.503e-03 | 24 | NC | 1 |
| 1022 | | | min | -.302 | 22 | -.44 | 29 | -.279 | 7 | -6.864e-03 | 6 | NC | 1 |
| 1023 | | 2 | max | .307 | 4 | .043 | 23 | .277 | 25 | 6.503e-03 | 24 | NC | 1 |
| 1024 | | | min | -.302 | 22 | -.441 | 29 | -.278 | 7 | -6.864e-03 | 6 | NC | 1 |
| 1025 | | 3 | max | .307 | 4 | .054 | 23 | .277 | 24 | 6.503e-03 | 24 | NC | 1 |
| 1026 | | | min | -.302 | 22 | -.442 | 29 | -.277 | 6 | -6.864e-03 | 6 | NC | 1 |
| 1027 | | 4 | max | .307 | 4 | .065 | 23 | .28 | 24 | 6.503e-03 | 24 | NC | 1 |
| 1028 | | | min | -.302 | 22 | -.444 | 29 | -.281 | 6 | -6.864e-03 | 6 | NC | 1 |
| 1029 | | 5 | max | .307 | 4 | .076 | 23 | .284 | 24 | 6.503e-03 | 24 | NC | 1 |
| 1030 | | | min | -.302 | 22 | -.445 | 29 | -.285 | 6 | -6.864e-03 | 6 | NC | 1 |
| 1031 | M110B | 1 | max | .044 | 18 | .029 | 18 | .032 | 23 | 1.241e-03 | 9 | NC | 1 |
| 1032 | | | min | -.058 | 12 | -.277 | 36 | -.034 | 5 | -1.188e-03 | 15 | NC | 1 |
| 1033 | | 2 | max | .044 | 18 | .029 | 18 | .034 | 23 | 1.241e-03 | 9 | NC | 1 |
| 1034 | | | min | -.058 | 12 | -.273 | 36 | -.036 | 5 | -1.188e-03 | 15 | NC | 1 |
| 1035 | | 3 | max | .044 | 18 | .029 | 18 | .037 | 23 | 1.241e-03 | 9 | NC | 1 |
| 1036 | | | min | -.058 | 12 | -.269 | 36 | -.038 | 5 | -1.188e-03 | 15 | NC | 1 |
| 1037 | | 4 | max | .044 | 18 | .028 | 18 | .039 | 23 | 1.241e-03 | 9 | NC | 1 |
| 1038 | | | min | -.058 | 12 | -.266 | 36 | -.04 | 5 | -1.188e-03 | 15 | NC | 1 |
| 1039 | | 5 | max | .044 | 18 | .028 | 18 | .041 | 23 | 1.241e-03 | 9 | NC | 1 |
| 1040 | | | min | -.058 | 12 | -.262 | 36 | -.042 | 5 | -1.188e-03 | 15 | NC | 1 |
| 1041 | M111B | 1 | max | .048 | 22 | .019 | 22 | .034 | 23 | 1.195e-03 | 13 | NC | 1 |
| 1042 | | | min | -.056 | 4 | -.255 | 28 | -.035 | 5 | -1.139e-03 | 19 | NC | 1 |
| 1043 | | 2 | max | .048 | 22 | .018 | 22 | .035 | 23 | 1.195e-03 | 13 | NC | 1 |
| 1044 | | | min | -.056 | 4 | -.253 | 28 | -.037 | 5 | -1.139e-03 | 19 | NC | 1 |
| 1045 | | 3 | max | .048 | 22 | .018 | 22 | .036 | 23 | 1.195e-03 | 13 | NC | 1 |
| 1046 | | | min | -.056 | 4 | -.25 | 28 | -.038 | 5 | -1.139e-03 | 19 | NC | 1 |
| 1047 | | 4 | max | .048 | 22 | .018 | 22 | .038 | 23 | 1.195e-03 | 13 | NC | 1 |
| 1048 | | | min | -.056 | 4 | -.247 | 28 | -.039 | 5 | -1.139e-03 | 19 | NC | 1 |
| 1049 | | 5 | max | .048 | 22 | .017 | 22 | .039 | 23 | 1.195e-03 | 13 | NC | 1 |
| 1050 | | | min | -.056 | 4 | -.245 | 28 | -.04 | 5 | -1.139e-03 | 19 | NC | 1 |

Envelope AISC 14th(360-10): LRFD Steel Code Checks

| Member | Shape | Code Check | Loc[ft] | LC | Shear ...Loc[ft] | Dir | LC | phi*Pnc... | phi*Pnt... | phi*Mn... | phi*Mn... | Cb | Eqn |
|--------|-------|------------|---------|---------|------------------|------|---------|------------|------------|-----------|-----------|----------------|-----------------|
| 1 | M66 | L3x3x4 | .491 | 6.983 | 7 | .800 | 6.983 | y | 10 | 32.733 | 46.656 | 1.688 | 2.278 1 H2-1 |
| 2 | M65 | L3x3x4 | .489 | 6.983 | 3 | .773 | 6.983 | y | 6 | 32.733 | 46.656 | 1.688 | 2.278 1 H2-1 |
| 3 | M64 1 | L3x3x4 | .549 | 6.982 | 29 | .507 | 6.982 | y | 2 | 32.733 | 46.656 | 1.688 | 2.278 1 H2-1 |
| 4 | M41A | PIPE 2.0 | .267 | 1.122 | 11 | .185 | 1.122 | 2 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b | |
| 5 | M48 | PIPE 2.0 | .278 | 12.3... | 13 | .167 | 12.3... | 11 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b | |
| 6 | M47 | PIPE 2.0 | .289 | 1.122 | 3 | .155 | 1.122 | 5 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b | |
| 7 | M108 | PIPE 2.0 | .677 | 3.083 | 5 | .133 | 5.25 | 10 | 14.916 | 32.13 | 1.872 | 1.872 2..H1-1b | |
| 8 | M54 | PIPE 2.0 | .295 | 3.083 | 4 | .128 | 3.083 | 12 | 14.916 | 32.13 | 1.872 | 1.872 2..H1-1b | |
| 9 | M28 | PIPE 2.0 | .677 | 3.083 | 2 | .127 | 5.25 | 6 | 14.916 | 32.13 | 1.872 | 1.872 2..H1-1b | |
| 10 | M53 | HSS4x4x3 | .449 | 0 | 34 | .126 | 0 | y | 3 | 102.875 | 106.812 | 12.662 | 12.662 3..H1-1b |
| 11 | M52 | HSS4x4x3 | .455 | 0 | 30 | .123 | 0 | y | 7 | 102.875 | 106.812 | 12.662 | 12.662 3..H1-1b |
| 12 | M62B | PIPE 2.0 | .320 | 3.083 | 3 | .123 | 3.083 | 4 | 14.916 | 32.13 | 1.872 | 1.872 1..H1-1b | |
| 13 | M118 | PIPE 2.0 | .703 | 3.083 | 11 | .118 | 5.25 | 7 | 14.916 | 32.13 | 1.872 | 1.872 2..H1-1b | |
| 14 | M57C | PIPE 2.0 | .266 | 3.083 | 11 | .117 | 3.083 | 4 | 14.916 | 32.13 | 1.872 | 1.872 1..H1-1b | |
| 15 | M70 | PIPE 2.0 | .333 | 3.083 | 6 | .113 | 3.083 | 8 | 14.916 | 32.13 | 1.872 | 1.872 2..H1-1b | |
| 16 | M93 | PIPE 2.0 | .276 | 3.083 | 7 | .110 | 3.083 | 12 | 14.916 | 32.13 | 1.872 | 1.872 1..H1-1b | |

Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

| Member | Shape | Code Check | Loc[ft] | LC | Shear .. Loc[ft] | Dir | LC | phi*Pnc... | phi*Pnt ... | phi*Mn ... | phi*Mn ...Cb | Eqn |
|--------|--------|---------------|---------|-------|------------------|------|---------|------------|-------------|------------|--------------|------------------|
| 17 | M60 | HSS4x4x3 | .436 | 0 | 29 | .108 | 0 | y 5 | 102.875 | 106.812 | 12.662 | 12.662 2...H1-1b |
| 18 | M51A | L2.5x2.5x3 | .504 | 0 | 5 | .095 | 1.25 | y 5 | 27.293 | 29.192 | .873 | 1.972 2... H2-1 |
| 19 | M75A | PIPE 2.0 | .294 | 3.083 | 4 | .091 | 3.083 | 8 | 14.916 | 32.13 | 1.872 | 1.872 1...H1-1b |
| 20 | M72_1 | PIPE 2.0 | .122 | 2.5 | 5 | .087 | 2.5 | 11 | 29.81 | 32.13 | 1.872 | 1.872 2...H1-1b |
| 21 | M49A | L2.5x2.5x3 | .475 | 0 | 10 | .084 | 1.25 | y 9 | 27.293 | 29.192 | .873 | 1.972 1... H2-1 |
| 22 | M50 | L2.5x2.5x3 | .478 | 0 | 2 | .084 | 1.25 | y 13 | 27.293 | 29.192 | .873 | 1.972 1... H2-1 |
| 23 | M61B | PIPE 2.0 | .191 | 6.618 | 36 | .084 | 10.9... | 12 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b |
| 24 | M62B_1 | PIPE 2.0 | .197 | 6.618 | 28 | .080 | 10.9... | 4 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b |
| 25 | M57A_1 | PIPE 2.0 | .179 | 6.347 | 32 | .077 | 2.026 | 8 | 17.855 | 32.13 | 1.872 | 1.872 1 H1-1b |
| 26 | M71_1 | PIPE 2.0 | .096 | 2.5 | 13 | .073 | 2.5 | 7 | 29.81 | 32.13 | 1.872 | 1.872 2...H1-1b |
| 27 | M70_1 | PIPE 2.0 | .098 | 0 | 3 | .072 | 2.5 | 3 | 29.81 | 32.13 | 1.872 | 1.872 2...H1-1b |
| 28 | M61 | L3x3x4 | .458 | 7.627 | 34 | .042 | 0 | z 30 | 13.292 | 46.656 | 1.688 | 3.507 2... H2-1 |
| 29 | M62 | L3x3x4 | .455 | 0 | 34 | .042 | 0 | z 34 | 13.292 | 46.656 | 1.688 | 3.499 2... H2-1 |
| 30 | M63 | L3x3x4 | .448 | 0 | 26 | .042 | 0 | z 26 | 13.292 | 46.656 | 1.688 | 3.503 2... H2-1 |
| 31 | M58 | LL3x3x4x0 | .528 | 1.067 | 34 | .039 | 1.105 | y 32 | 79.399 | 93.312 | 6.48 | 4.911 1...H1-1b |
| 32 | M57 | LL3x3x4x0 | .518 | 1.067 | 26 | .038 | 1.105 | y 36 | 79.399 | 93.312 | 6.48 | 4.911 1...H1-1b |
| 33 | M59 | LL3x3x4x0 | .519 | 1.067 | 30 | .038 | 1.105 | y 28 | 79.399 | 93.312 | 6.48 | 4.911 1...H1-1b |
| 34 | M74_1 | L2.5x2.5x3 | .077 | 2.141 | 32 | .010 | 0 | z 29 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 35 | M82_1 | L2.5x2.5x3 | .088 | 2.141 | 5 | .010 | 4.282 | z 36 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 36 | M78_1 | L2.5x2.5x3 | .081 | 2.141 | 2 | .010 | 0 | z 32 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 37 | M84_1 | L2.5x2.5x3 | .081 | 2.141 | 2 | .010 | 0 | y 31 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 38 | M80_1 | L2.5x2.5x3 | .088 | 2.141 | 11 | .010 | 4.282 | y 28 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 39 | M76_1 | L2.5x2.5x3 | .072 | 2.141 | 32 | .010 | 0 | v 36 | 15.939 | 29.192 | .873 | 1.724 1... H2-1 |
| 40 | M105 | LL2.5x2.5x... | .116 | 3.01 | 5 | .008 | 6.021 | z 4 | 36.392 | 58.32 | 3.954 | 2.55 1...H1-1b |
| 41 | M106 | LL2.5x2.5x... | .116 | 3.01 | 11 | .008 | 0 | z 6 | 36.392 | 58.32 | 3.954 | 2.55 1...H1-1b |
| 42 | M104 | LL2.5x2.5x... | .104 | 3.01 | 27 | .006 | 0 | y 26 | 36.392 | 58.32 | 3.954 | 2.55 1...H1-1b |

SPECIAL CONSTRUCTION NOTE:
SPRINT WORK IS CONTINGENT ON THE FOLLOWING:
 * COMPLETION OF A GLOBAL STRUCTURAL STABILITY ANALYSIS.
 * COMPLETION OF AN ANTENNA/RRH MOUNT STRUCTURAL ASSESSMENT.
 * GC SHALL FURNISH, INSTALL AND COMPLETE ALL REQUIRED STRUCTURAL MODIFICATIONS AS INDICATED IN BEFORE-MENTIONED ANALYSIS AND ASSESSMENT.

SPECIAL CONSTRUCTION NOTE:
GENERAL CONTRACTOR SHALL FURNISH AND INSTALL ALL ANTENNA MOUNT STRUCTURAL AUGMENTS (STRUCTURAL MODIFICATIONS) AT SPRINT'S RAD/VERTICAL EQUIPMENT SPACE PER RECOMMENDATIONS FROM SBA-PROVIDED ANTENNA MOUNT STRUCTURAL ANALYSIS AND ANY SUPPLEMENTAL CONSTRUCTION DRAWINGS (PROVIDED BY OTHERS).



PROJECT:

DO MACRO UPGRADE
EQUIPMENT DEPLOYMENT

SITE NUMBER:

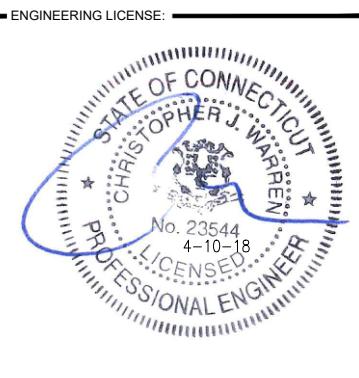
CT33XC566

SITE ADDRESS:

100 OLD TATNIC HILL ROAD
BROOKLYN, CT 06234

SITE TYPE:

MONPOLE



| SITE INFORMATION | | AREA MAP | PROJECT DESCRIPTION | DRAWING INDEX | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|---|---------------------|--|--|-----------|-------------|------|-------|----------------------------|------|------------------|------------------------|---|---------------|------------------------|---|--------------|------------------------|---|------------------|-----------|---|-------------|-----------------|---|--------------|-----------------------------------|---|-----|------------------------------|---|-----|---------|---|-----|--------------------------------|---|------|---------------|---|------|------------------|---|
| SITE INFORMATION: | | | SPRINT PROPOSES TO MODIFY AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY. • REMOVE (6) PANEL ANTENNAS • INSTALL (6) PANEL ANTENNAS • INSTALL (3) 2.5 GHz RRH'S ON PROPOSED PIPE MOUNT • RELOCATE (3) 1900 MHz RRH'S ON PROPOSED PIPE MOUNT • INSTALL (6) 800 MHz RRH'S ON EXISTING PIPE MOUNT • INSTALL (4) HYBRID CABLES • REMOVE EXISTING (5) 1-5/8" COAX • INSTALL RAN EQUIPMENT INSIDE EXISTING MMBTS CABINET • INSTALL STRUCTURAL AUGMENTS | <table border="1"> <thead> <tr> <th>SHEET NO.</th> <th>SHEET TITLE</th> <th>REV.</th> </tr> </thead> <tbody> <tr> <td>T-1</td> <td>TITLE SHEET & PROJECT DATA</td> <td>0</td> </tr> <tr> <td>SP-1</td> <td>OUTLINE SPECIFICATIONS</td> <td>0</td> </tr> <tr> <td>SP-2</td> <td>OUTLINE SPECIFICATIONS</td> <td>0</td> </tr> <tr> <td>SP-3</td> <td>OUTLINE SPECIFICATIONS</td> <td>0</td> </tr> <tr> <td>A-1</td> <td>SITE PLAN</td> <td>0</td> </tr> <tr> <td>A-2</td> <td>TOWER ELEVATION</td> <td>0</td> </tr> <tr> <td>A-3</td> <td>ANTENNA LAYOUT & MOUNTING DETAILS</td> <td>0</td> </tr> <tr> <td>A-4</td> <td>EQUIPMENT & MOUNTING DETAILS</td> <td>0</td> </tr> <tr> <td>A-5</td> <td>DETAILS</td> <td>0</td> </tr> <tr> <td>E-1</td> <td>ELECTRICAL & GROUNDING DETAILS</td> <td>0</td> </tr> <tr> <td>RF-1</td> <td>RF DATA SHEET</td> <td>0</td> </tr> <tr> <td>RF-2</td> <td>PLUMBING DIAGRAM</td> <td>0</td> </tr> </tbody> </table> | SHEET NO. | SHEET TITLE | REV. | T-1 | TITLE SHEET & PROJECT DATA | 0 | SP-1 | OUTLINE SPECIFICATIONS | 0 | SP-2 | OUTLINE SPECIFICATIONS | 0 | SP-3 | OUTLINE SPECIFICATIONS | 0 | A-1 | SITE PLAN | 0 | A-2 | TOWER ELEVATION | 0 | A-3 | ANTENNA LAYOUT & MOUNTING DETAILS | 0 | A-4 | EQUIPMENT & MOUNTING DETAILS | 0 | A-5 | DETAILS | 0 | E-1 | ELECTRICAL & GROUNDING DETAILS | 0 | RF-1 | RF DATA SHEET | 0 | RF-2 | PLUMBING DIAGRAM | 0 |
| SHEET NO. | SHEET TITLE | | REV. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T-1 | TITLE SHEET & PROJECT DATA | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SP-1 | OUTLINE SPECIFICATIONS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SP-2 | OUTLINE SPECIFICATIONS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SP-3 | OUTLINE SPECIFICATIONS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A-1 | SITE PLAN | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A-2 | TOWER ELEVATION | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A-3 | ANTENNA LAYOUT & MOUNTING DETAILS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A-4 | EQUIPMENT & MOUNTING DETAILS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| A-5 | DETAILS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| E-1 | ELECTRICAL & GROUNDING DETAILS | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF-1 | RF DATA SHEET | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF-2 | PLUMBING DIAGRAM | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| APPLICANT: | SPRINT 1 INTERNATIONAL BLVD, SUITE 800 MAHWAH, NJ 07495 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TOWER OWNER: | SBA TOWERS LLC, 8051 CONGRESS AVENUE BOCA RATON, FL 33487 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SBA SITE ID: | CT01915-S | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SBA SITE NAME: | SOUTH BROOKLYN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SBA CONTACT: | STEPHEN ROTH (860) 539-4920 sroth@sbsite.com | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | LOCATION MAP | APPLICABLE CODES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES. 1. INTERNATIONAL BUILDING CODE (2012 IBC) 2. TIA-222-G OR LATEST EDITION 3. NFPA 780 – LIGHTNING PROTECTION CODE 4. 2014 NATIONAL ELECTRIC CODE OR LATEST EDITION 5. ANY OTHER NATIONAL OR LOCAL APPLICABLE CODES, MOST RECENT EDITIONS 6. CT BUILDING CODE 7. LOCAL BUILDING CODE 8. CITY/COUNTY ORDINANCES | <table border="1"> <thead> <tr> <th colspan="3">APPROVALS</th> </tr> <tr> <th>TITLE</th> <th>SIGNATURE</th> <th>DATE</th> </tr> </thead> <tbody> <tr> <td>PROJECT MANAGER:</td> <td></td> <td></td> </tr> <tr> <td>CONSTRUCTION:</td> <td></td> <td></td> </tr> <tr> <td>RF ENGINEER:</td> <td></td> <td></td> </tr> <tr> <td>ZONING/SITE ACQ:</td> <td></td> <td></td> </tr> <tr> <td>OPERATIONS:</td> <td></td> <td></td> </tr> <tr> <td>TOWER OWNER:</td> <td></td> <td></td> </tr> </tbody> </table> | APPROVALS | | | TITLE | SIGNATURE | DATE | PROJECT MANAGER: | | | CONSTRUCTION: | | | RF ENGINEER: | | | ZONING/SITE ACQ: | | | OPERATIONS: | | | TOWER OWNER: | | | | | | | | | | | | | | | | | |
| APPROVALS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TITLE | SIGNATURE | DATE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PROJECT MANAGER: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CONSTRUCTION: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RF ENGINEER: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ZONING/SITE ACQ: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| OPERATIONS: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TOWER OWNER: | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CALL CONNECTICUT ONE CALL (800) 922-4455 CALL 3 WORKING DAYS BEFORE YOU DIG! | | | THE FOLLOWING PARTIES HEREBY APPROVE AND ACCEPT THESE DOCUMENTS AND AUTHORIZE THE CONTRACTOR TO PROCEED WITH THE CONSTRUCTION DESCRIBED HEREIN. ALL DOCUMENTS ARE SUBJECT TO REVIEW BY THE LOCAL BUILDING DEPARTMENT AND MAY IMPOSE CHANGES OR MODIFICATIONS. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Know what's below. Call before you dig. www.call811.com | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

T-1

THESE OUTLINE SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT STANDARD CONSTRUCTION SPECIFICATIONS, INCLUDING CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

SECTION 01 100 – SCOPE OF WORK

PART 1 – GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE SPRINT CONSTRUCTION STANDARDS FOR WIRELESS SITES, CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITHE.

1.3 PRECEDENCE: SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES INCLUDING THE STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF THIS OCCURS.

1.4 NATIONALLY RECOGNIZED CODES AND STANDARDS:

- A. THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
 - 1. GR-63-CORE NEBS REQUIREMENTS: PHYSICAL PROTECTION
 - 5. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.
 - 3. GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY –GENERIC CRITERIA FOR NETWORK TELECOMMUNICATIONS EQUIPMENT.
 - 4. NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70 (NATIONAL ELECTRICAL CODE – "NEC") AND NFPA 101 (LIFE SAFETY CODE).
 - 5. AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
 - 6. INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
 - 7. AMERICAN CONCRETE INSTITUTE (ACI)
 - 8. AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
 - 9. CONCRETE REINFORCING STEEL INSTITUTE (CRSI)
 - 10. AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
 - 11. PORTLAND CEMENT ASSOCIATION (PCA)
 - 12. NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
 - 13. BRICK INDUSTRY ASSOCIATION (BIA)
 - 14. AMERICAN WELDING SOCIETY (AWS)
 - 15. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
 - 16. SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
 - 17. DOOR AND HARDWARE INSTITUTE (DHI)
 - 18. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
 - 19. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE.

1.5 DEFINITIONS:

- A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT DOCUMENTS.
- B. COMPANY: SPRINT CORPORATION
- C. ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND "A&E". THE DESIGN PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT.
- D. CONTRACTOR: CONSTRUCTION CONTRACTOR; CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK.
- E. THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC TASKS RELATED TO BUT NOT INCLUDED IN THE WORK.
- F. OFCI: OWNER FURNISHED, CONTRACTOR INSTALLED EQUIPMENT.
- G. CONSTRUCTION MANAGER – ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT...

1.6 SITE FAMILIARITY: CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOWLEDGE OF FIELD CONDITIONS.

1.7 POINT OF CONTACT: COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.

1.8 ON-SITE SUPERVISION: THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK.

1.9 DRAWINGS, SPECIFICATIONS AND DETAILS REQUIRED AT JOBSITE: THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS, STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.

A. THE JOBSITE DRAWINGS, SPECIFICATIONS AND DETAILS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS. AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A&E VENDOR FOR PRODUCTION OF "AS-BUILT" DRAWINGS.

B. DETAILS ARE INTENDED TO SHOW DESIGN INTENT. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK. CONTRACTOR SHALL NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY VARIATIONS PRIOR TO PROCEEDING WITH THE WORK.

C. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO PROCEEDING WITH THE WORK.

1.10 USE OF JOB SITE: THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.

1.11 UTILITIES SERVICES: WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT ANDAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY COMPANY INVOLVED:

1.12 PERMITS / FEES: WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC UTILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.

1.13 CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.

1.14 METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION: CONTRACTOR SHALL PERFORM WORK AS DESCRIBED IN THE FOLLOWING INSTALLATION AND COMMISSIONING MOPS.

NOTE: IN SHORT-FORM SPECIFICATIONS ON THE DRAWINGS, A/E TO INSERT LIST OF APPLICABLE MOPS INCLUDING EN-2012-001, EN-2013-002, EL-0568, AND TS-0193

1.15 USE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS:

PART 2 – PRODUCTS (NOT USED)

PART 3 – EXECUTION

3.1 TEMPORARY UTILITIES AND FACILITIES: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS. TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE. USE OF THE LESSOR'S OR SITE OWNER'S UTILITIES OR FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.

3.2 ACCESS TO WORK: THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.

3.3 TESTING: REQUIREMENTS FOR TESTING BY THIS CONTRACTOR SHALL BE AS INDICATED HEREWITHE, ON THE CONSTRUCTION DRAWINGS, AND IN THE INDIVIDUAL SECTIONS OF THESE SPECIFICATIONS. SHOULD COMPANY CHOOSE TO ENGAGE ANY THIRD-PARTY TO CONDUCT ADDITIONAL TESTING, THE CONTRACTOR SHALL COOPERATE WITH AND PROVIDE A WORK AREA FOR COMPANY'S TEST AGENCY.

3.4 DIMENSIONS: VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS.

3.5 EXISTING CONDITIONS: NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERENT FROM THOSE INDICATED ON THE DRAWINGS. DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

SECTION 01 200 – COMPANY FURNISHED MATERIAL AND EQUIPMENT

PART 1 – GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITHE.

PART 2 – PRODUCTS (NOT USED)

PART 3 – EXECUTION

3.1 RECEIPT OF MATERIAL AND EQUIPMENT:

- A. A COMPANY FURNISHED MATERIAL AND EQUIPMENT IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.
- B. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON RECEIPT SHALL:
 - 1. ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.
 - 2. VERIFY COMPLETENESS AND CONDITION OF ALL DELIVERIES.
 - 3. TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT.
 - 4. RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY-FOUR HOURS AFTER RECEIPT, REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
 - 5. PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING.
 - 6. COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SITE.

3.2 DELIVERABLES:

- A. COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE.
- B. IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY.
- C. UPLOAD DOCUMENTATION INTO SPRINT SITE MANAGEMENT SYSTEM (SMS) AND/OR PROVIDE HARD COPY DOCUMENTATION AS REQUESTED.

SECTION 01 300 – CELL SITE CONSTRUCTION CO.

PART 1 – GENERAL

1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.

1.2 RELATED DOCUMENTS:

- A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
- B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITHE.

1.3 NOTICE TO PROCEED

- A. NO WORK SHALL COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE OF THE WORK ORDER.
- B. UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.

PART 2 – PRODUCTS (NOT USED)

PART 3 – EXECUTION

3.1 FUNCTIONAL REQUIREMENTS:

- A. THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. THE ACTIVITIES DESCRIBED ARE NOT EXHAUSTIVE, AND CONTRACTOR SHALL TAKE ANY AND ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH COMPANY PROCESSES.
- B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED.
- C. MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
- D. PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS, INCLUDING BUT NOT LIMITED TO THE FOLLOWING:

PLANS PREPARED FOR:



1 INTERNATIONAL BLVD, SUITE 800
MAHWAH, NJ 07495
TEL: (800) 357-7641

PROJECT MANAGER:



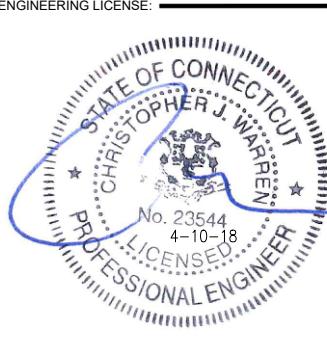
SBA COMMUNICATIONS CORP.
134 FLANDERS ROAD, SUITE 125
WESTBOROUGH, MA 01581
TEL: (508) 251-0720

PLANS PREPARED BY:



1033 Watervliet Shaker Rd | Albany, NY 12205
Phone: 518-690-0790 | Fax: 518-690-0793
www.infinigy.com
JOB NUMBER 526-104

ENGINEERING LICENSE:



CHECKED BY:

APPROVED BY:

| REVISIONS: | DESCRIPTION | DATE | BY | REV. |
|------------|-------------|------|----|------|
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ISSUED FOR CONSTRUCTION 04/10/18 RWF 0

SITE NUMBER:

CT33XC566

SITE ADDRESS:

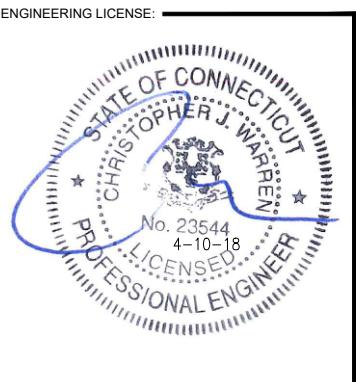
100 OLD TATNIC HILL ROAD
BROOKLYN, CT 06234

SHEET DESCRIPTION:

OUTLINE SPECIFICATIONS

SHEET NUMBER:

SP-1



CHECKED BY:

APPROVED BY:

| REVISIONS: | DESCRIPTION | DATE | BY REV. |
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| ISSUED FOR CONSTRUCTION | | 04/10/18 | RWF 0 |

SITE NUMBER:

CT33XC566

SITE ADDRESS:

100 OLD TATNIC HILL ROAD
 BROOKLYN, CT 06234

SHEET DESCRIPTION:

OUTLINE SPECIFICATIONS

SHEET NUMBER:

SP-2

CONTINUE FROM SP-1

1. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
2. PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS.
3. MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELCO BACKHAUL.
4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
5. INSTALL ABOVE GROUND GROUNDING SYSTEMS.
6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
7. INSTALL "H-FRAMES", CABINETS AND SHELTERS AS INDICATED.
8. INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
9. ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.
10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.
12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS.
13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
17. INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
18. PERFORM, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
19. PERFORM ANTENNA AND COAX SWEEP TESTING AND MAKE ANY AND ALL NECESSARY CORRECTIONS.
20. REMAIN ON SITE MOBILIZED THROUGHOUT HAND-OFF AND INTEGRATION TO ASSIST AS NEEDED UNTIL SITE IS DEEMED SUBSTANTIALLY COMPLETE AND PLACED "ON AIR."

3.2 GENERAL REQUIREMENTS FOR CIVIL CONSTRUCTION:

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.
 1. IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.
 2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD.
- D. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE Affected BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION
- E. CONDUCT TESTING AS REQUIRED HEREIN.

3.3 DELIVERABLES:

- A. CONTRACTOR SHALL REVIEW, APPROVE, AND SUBMIT TO SPRINT SHOP DRAWINGS, PRODUCT DATA, SAMPLES, AND SIMILAR SUBMITTALS AS REQUIRED HEREINAFTER
- B. PROVIDE DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
 1. ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
 2. PROJECT PROGRESS REPORTS.
 3. CIVIL CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
 4. ELECTRICAL SERVICE COMPLETION DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
5. LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
6. POWER INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
7. TELCO READY DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
8. PPC (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
9. TOWER CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
10. TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
11. BTS AND RADIO EQUIPMENT DELIVERED AT SITE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
12. NETWORK OPERATIONS HANDOFF CHECKLIST (HOC WALK) COMPLETE (UPLOAD FORM IN SMS)
13. CIVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
14. SITE CONSTRUCTION PROGRESS PHOTOS UNLOADED INTO SMS.

SECTION 01 400 – SUBMITTALS & TESTS

PART 1 – GENERAL

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
 - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
 - B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITHE.
- 1.3 SUBMITTALS:
 - A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.
 - B. SUBMIT THE FOLLOWING TO COMPANY REPRESENTATIVE FOR APPROVAL.
 1. CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING.
 2. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
 3. SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
 4. ALL EQUIPMENT AND MATERIALS SO IDENTIFIED ON THE CONSTRUCTION DRAWINGS.
 5. CHEMICAL GROUNDING DESIGN
 - D. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.
- 1.4 TESTS AND INSPECTIONS:
 - A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
 - B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS.
 2. AGL, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.
 3. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
 - C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING:
 1. AZIMUTH, DOWNTILT, AGL – UPLOAD REPORT FROM ANTENNA ALIGNMENT TOOL TO SITERRA TASK 465. INSTALLED AZIMUTH, DOWNTILT, AND AGL MUST CONFORM TO THE RF DATA SHEETS. SWEEP AND FIBER TESTS
 2. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
 3. ALL AVAILABLE JURISDICTIONAL INFORMATION
 4. PDF SCAN OF REDLINES PRODUCED IN FIELD

PART 2 – PRODUCTS (NOT USED)

PART 3 – EXECUTION

3.1 REQUIREMENTS FOR TESTING:

- A. THIRD PARTY TESTING AGENCY:
 1. WHEN THE USE OF A THIRD PARTY INDEPENDENT TESTING AGENCY IS REQUIRED, THE AGENCY THAT IS SELECTED MUST PERFORM SUCH WORK ON A REGULAR BASIS IN THE STATE WHERE THE PROJECT IS LOCATED AND HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
 2. THE THIRD PARTY TESTING AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
 3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASHTO, AND OTHER METHODS IS NEEDED.
 4. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASHTO, AND OTHER METHODS IS NEEDED.

3.2 REQUIRED TESTS:

- A. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR FOUNDATIONS AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
 2. ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED IN SECTION: HOT MIX ASPHALT PAVING.
 3. FIELD QUALITY CONTROL TESTING AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
 4. TESTING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS, PADS AND ANCHOR LOCATIONS
 5. STRUCTURAL BACKFILL COMPACTION TESTS FOR THE TOWER FOUNDATION.
 6. SITE RESISTANCE TO EARTH TESTING PER EXHIBIT: CELL SITE GROUNDING SYSTEM DESIGN.
 7. ANTENNA AND COAX SWEEP TESTS PER EXHIBIT: ANTENNA TRANSMISSION LINE ACCEPTANCE STANDARDS.
 8. GROUNDING AT ANTENNA MASTS FOR GPS AND ANTENNAS
 9. ALL OTHER TESTS REQUIRED BY COMPANY OR JURISDICTION.

3.3 REQUIRED INSPECTIONS

- A. SCHEDULE INSPECTIONS WITH COMPANY REPRESENTATIVE.
- B. CONDUCT INSPECTIONS INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. GROUNDING SYSTEM INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
 2. FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
 3. COMPACTION OF BACKFILL MATERIALS; AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS; ASPHALT PAVING; AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
 4. PRE- AND POST-CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES.
 5. TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
 6. ANTENNA AZIMUTH , DOWN TILT AND PER SUNLIGHT TOOL SUNSIGHT INSTRUMENTS – ANTENNALIGN ALIGNMENT TOOL (AAT)

CONTINUE FROM SP-2

7. VERIFICATION DOCUMENTED WITH THE ANTENNA CHECKLIST REPORT, BY A&E, SITE DEVELOPMENT REP, OR RF REP.
 8. FINAL INSPECTION CHECKLIST AND HANDOFF WALK (HOC.). SIGNED FORM SHOWING ACCEPTANCE BY FIELD OPS IS TO BE UPLOADED INTO SMS.
 9. COAX SWEEP AND FIBER TESTING DOCUMENTS SUBMITTED VIA SMS FOR RF APPROVAL.
 10. SCAN-ABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
 11. ALL AVAILABLE JURISDICTIONAL INFORMATION
 12. PDF SCAN OF REDLINES PRODUCED IN FIELD

C. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.

D. CONSTRUCTION INSPECTIONS AND CORRECTIVE MEASURES SHALL BE DOCUMENTED BY THE CONTRACTOR WITH WRITTEN REPORTS AND PHOTOGRAPHS. PHOTOGRAPHS MUST BE DIGITAL AND OF SUFFICIENT QUALITY TO CLEARLY SHOW THE SITE CONSTRUCTION. PHOTOGRAPHS MUST CLEARLY IDENTIFY THE PHOTOGRAPHED ITEM AND BE LABELED WITH THE SITE CASCADE NUMBER, SITE NAME, DESCRIPTION, AND DATE.

3.4 DELIVERABLES: TEST AND INSPECTION REPORTS AND CLOSEOUT DOCUMENTATION SHALL BE uploaded TO THE SMS AND/OR FORWARDED TO SPRINT FOR INCLUSION INTO THE PERMANENT SITE FILES.

A. THE FOLLOWING TEST AND INSPECTION REPORTS SHALL BE PROVIDED AS APPLICABLE.

 1. CONCRETE MIX AND CYLINDER BREAK REPORTS.
 2. STRUCTURAL BACKFILL COMPACTION REPORTS.
 3. SITE RESISTANCE TO EARTH TEST.
 4. ANTENNA AZIMUTH AND DOWN TILT VERIFICATION
 5. TOWER ERECTION INSPECTIONS AND MEASUREMENTS DOCUMENTING TOWER INSTALLED PER SUPPLIER'S REQUIREMENTS AND THE APPLICABLE SECTIONS HEREIN.
 6. COAX CABLE SWEEP TESTS PER COMPANY'S "ANTENNA LINE ACCEPTANCE STANDARDS".

B. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES THE FOLLOWING;

 1. TEST WELLS AND TRENCHES: PHOTOGRAPHS OF ALL TEST WELLS; PHOTOGRAPHS SHOWING ALL OPEN EXCAVATIONS AND TRENCHING PRIOR TO BACKFILLING SHOWING A TAPE MEASURE VISIBLE IN THE EXCAVATIONS INDICATING DEPTH.
 2. CONDUITS, CONDUCTORS AND GROUNDING: PHOTOGRAPHS SHOWING TYPICAL INSTALLATION OF CONDUCTORS AND CONNECTORS; PHOTOGRAPHS SHOWING TYPICAL BEND RADIUS OF INSTALLED GROUND WIRES AND GROUND ROD SPACING;
 3. CONCRETE FORMS AND REINFORCING: CONCRETE FORMING AT TOWER AND EQUIPMENT/SHELTER PAD/FOUNDATIONS – PHOTOGRAPHS SHOWING ALL REINFORCING STEEL, UTILITY AND CONDUIT STUB OUTS; PHOTOGRAPHS SHOWING CONCRETE POUR OF SHELTER SLAB/FOUNDATION, TOWER FOUNDATION AND GUY ANCHORS WITH VIBRATOR IN USE; PHOTOGRAPHS SHOWING EACH ANCHOR ON GUYED TOWERS, BEFORE CONCRETE POUR.
 4. TOWER, ANTENNAS AND MAINLINE: INSPECTION AND PHOTOGRAPHS OF SECTION STACKING; INSPECTION AND PHOTOGRAPHS OF PLATFORM COMPONENT ATTACHMENT POINTS; PHOTOGRAPHS OF TOWER TOP GROUNDING; PHOTOS OF TOWER COAX LINE COLOR CODING AT THE TOP AND AT GROUND LEVEL; INSPECTION AND PHOTOGRAPHS OF OPERATIONAL OF TOWER LIGHTING, AND PLACEMENT OF FAA REGISTRATION SIGN; PHOTOGRAPHS SHOWING ADDITIONAL GROUNDING POINTS FOR TOWERS GREATER THAN 200 FEET.; PHOTOS OF ANTENNA GROUND BAR, EQUIPMENT GROUND BAR, AND MASTER GROUND BAR; PHOTOS OF GPS ANTENNA(S); PHOTOS OF EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA; PHOTOS OF COAX WEATHERPROOFING – TOP AND BOTTOM; PHOTOS OF COAX GROUNDING—TOP AND BOTTOM; PHOTOS OF ANTENNA AND MAST GROUNDING; PHOTOS OF COAX CABLE ENTRY INTO SHELTER; PHOTOS OF PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
 5. ROOF TOPS: PRE-CONSTRUCTION AND POST-CONSTRUCTION VISUAL INSPECTION AND PHOTOGRAPHS OF THE ROOF AND INTERIOR TO DETERMINE AND DOCUMENT CONDITIONS; ROOF TOP CONSTRUCTION INSPECTIONS AS REQUIRED BY THE JURISDICTION; PHOTOGRAPHS OF CABLE TRAY AND/OR ICE BRIDGE; PHOTOGRAPHS OF DOGHOUSE/CABLE EXIT FROM ROOF;
 6. SITE LAYOUT – PHOTOGRAPHS OF THE OVERALL COMPOUND, INCLUDING EQUIPMENT PLATFORM FROM ALL FOUR CORNERS.
 7. FINISHED UTILITIES: CLOSE-UP PHOTOGRAPHS OF THE PPC BREAKER PANEL; CLOSE-UP PHOTOGRAPH OF THE INSIDE OF THE TELCO PANEL AND NIU; CLOSE-UP PHOTOGRAPH OF THE POWER METER AND DISCONNECT; PHOTOS OF POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE; PHOTOGRAPHS AT METER BOX AND/OR FACILITY DISTRIBUTION PANEL.
 8. REQUIRED MATERIALS CERTIFICATIONS: CONCRETE MIX DESIGNS; MILL CERTIFICATION FOR ALL REINFORCING AND STRUCTURAL STEEL; AND ASPHALT PAVING MIX DESIGN.
 9. ANY AND ALL SUBMITTALS BY THE JURISDICTION OR COMPANY.

SECTION 01 400 – SUBMITTALS & TESTS

PART 1 – GENERAL

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.**

1.2 RELATED DOCUMENTS:

 - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
 - B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HEREWITHE.

PART 2 – PRODUCTS (NOT USED)

PART 3 – EXECUTION

3.1 WEEKLY REPORTS:

 - A. CONTRACTOR SHALL PROVIDE SPRINT WITH WEEKLY REPORTS SHOWING PROJECT STATUS. THIS STATUS REPORT FORMAT WILL BE PROVIDED TO THE CONTRACTOR BY SPRINT. THE REPORT WILL CONTAIN SITE ID NUMBER, THE MILESTONES FOR EACH SITE, INCLUDING THE BASELINE DATE, ESTIMATED COMPLETION DATE AND ACTUAL COMPLETION DATE.
 - B. REPORT INFORMATION WILL BE TRANSMITTED TO SPRINT VIA ELECTRONIC MEANS AS REQUIRED. THIS INFORMATION WILL PROVIDE A BASIS FOR PROGRESS MONITORING AND PAYMENT.

3.2 PROJECT CONFERENCE CALLS:

 - A. SPRINT MAY HOLD WEEKLY PROJECT CONFERENCE CALLS. CONTRACTOR WILL BE REQUIRED TO COMMUNICATE SITE STATUS, MILESTONE COMPLETIONS AND UPCOMING MILESTONE PROJECTIONS, AND ANSWER ANY OTHER SITE STATUS QUESTIONS AS NECESSARY.

3.3 PROJECT TRACKING IN SMS:

 - A. CONTRACTOR SHALL PROVIDE SCHEDULE UPDATES AND PROJECTIONS IN THE SMS SYSTEM ON A WEEKLY BASIS.

3.4 ADDITIONAL REPORTING:

 - A. ADDITIONAL OR ALTERNATE REPORTING REQUIREMENTS MAY BE ADDED TO THE REPORT AS DETERMINED TO BE REASONABLY NECESSARY BY COMPANY.

3.5 PROJECT PHOTOGRAPHS:

 - A. FILE DIGITAL PHOTOGRAPHS OF COMPLETED SITE IN JPEG FORMAT IN THE SMS PHOTO LIBRARY FOR THE RESPECTIVE SITE. PHOTOGRAPHS SHALL BE CLEARLY LABELED WITH SITE NUMBER, NAME AND DESCRIPTION, AND SHALL INCLUDE AT A MINIMUM THE FOLLOWING AS APPLICABLE:
 1. 1SHELTER AND TOWER OVERVIEW.
 2. TOWER FOUNDATION(S) – FORMS AND STEEL BEFORE POUR (EACH ANCHOR ON GUYED TOWERS).
 3. TOWER FOUNDATION(S) POUR WITH VIBRATOR IN USE (EACH ANCHOR ON GUYED TOWERS).
 4. TOWER STEEL AS BEING INSTALLED INTO HOLE (SHOW ANCHOR STEEL ON GUYED TOWERS).
 5. PHOTOS OF TOWER SECTION STACKING.
 6. CONCRETE TESTING / SAMPLES.
 7. PLACING OF ANCHOR BOLTS IN TOWER FOUNDATION.
 8. BUILDING/WATER TANK FROM ROAD FOR TENANT IMPROVEMENTS OR COMMENTS.
 9. SHELTER FOUNDATION--FORMS AND STEEL BEFORE POURING.
 10. SHELTER FOUNDATION POUR WITH VIBRATOR IN USE.
 11. COAX CABLE ENTRY INTO SHELTER.
 12. PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
 13. ROOFTOP PRE AND POST CONSTRUCTION PHOTOS TO INCLUDE PENETRATIONS AND INTERIOR CEILING.
 14. PHOTOS OF TOWER TOP COAX LINE COLOR CODING AND COLOR CODING AT GROUND LEVEL.
 15. PHOTOS OF ALL APPROPRIATE COMPANY OR REGULATORY SIGNAGE.
 16. PHOTOS OF EQUIPMENT BOLT DOWN INSIDE SHELTER.
 17. POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE AND POWER AND TELCO SUPPLY LOCATIONS INCLUDING METER/DISCONNECT.
 18. ELECTRICAL TRENCH(S) WITH ELECTRICAL / CONDUIT BEFORE BACKFILL.
 19. ELECTRICAL TRENCH(S) WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL.
 20. TELCO TRENCH WITH TELEPHONE / CONDUIT BEFORE BACKFILL.
 21. TELCO TRENCH WITH FOIL-BACKED TAPE BEFORE FURTHER BACKFILL.
 22. SHELTER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
 23. TOWER GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).

- 24. FENCE GROUND-RING TRENCH WITH GROUND-WIRE BEFORE BACKFILL (SHOW ALL CAD WELDS AND BEND RADII).
 - 25. ALL BTS GROUND CONNECTIONS.
 - 26. ALL GROUND TEST WELLS.
 - 27. ANTENNA GROUND BAR AND EQUIPMENT GROUND BAR.
 - 28. ADDITIONAL GROUNDING POINTS ON TOWERS ABOVE 200'.
 - 29. HVAC UNITS INCLUDING CONDENSERS ON SPLIT SYSTEMS.
 - 30. GPS ANTENNAS.
 - 31. CABLE TRAY AND/OR WAVEGUIDE BRIDGE.
 - 32. DOGHOUSE/CABLE EXIT FROM ROOF.
 - 33. EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA.
 - 34. MASTER BUS BAR.
 - 35. TELCO BOARD AND NIU.
 - 36. ELECTRICAL DISTRIBUTION WALL.
 - 37. CABLE ENTRY WITH SURGE SUPPRESSION.
 - 38. ENTRANCE TO EQUIPMENT ROOM.
 - 39. COAX WEATHERPROOFING-TOP AND BOTTOM OF TOWER.
 - 40. COAX GROUNDING -TOP AND BOTTOM OF TOWER.
 - 41. ANTENNA AND MAST GROUNDING.
 - 42. LANDSCAPING – WHERE APPLICABLE.

FINAL PROJECT ACCEPTANCE: COMPLETE ALL REQUIRED REPORTING TASKS PER CONTRACT, CONTRACT DOCUMENTS OR THE SPRINT INTEGRATED CONSTRUCTION STANDARDS FOR WIRELESS SITES AND UPLOAD INTO SITERRA.

PLANS PREPARED FOR:



1 INTERNATIONAL BLVD, SUITE 800
MAHWAH, NJ 07495
TEL: (800) 357-7641

PROJECT MANAGER:



SBA COMMUNICATIONS CORP.
134 FLANDERS ROAD, SUITE 125
WESTBOROUGH, MA 01581
TEL: (508) 251-0720

• PLANS PREPARED BY: ■



Digitized by srujanika@gmail.com



CHECKED BY:

APPROVED BY

| REVISIONS: | | DATE | BY |
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| DESCRIPTION | | | |
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| ISSUED FOR CONSTRUCTION | 04/10/18 | RWF | C |

■ SITE NUMBER: _____

CT33XC566

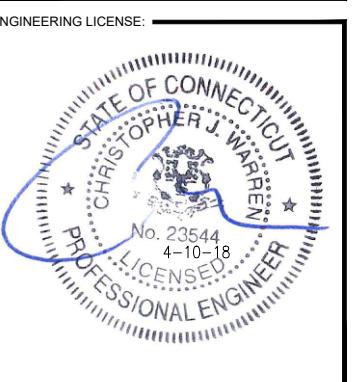
SITE ADDRESS: 100 OLD TATNIC HILL ROAD
BROOKLYN, CT 06234

■ SHEET DESCRIPTION: _____

OUTLINE SPECIFICATIONS

■ SHEET NUMBER: _____

SP-3



CHECKED BY:

APPROVED BY:

| REVISIONS: | DESCRIPTION | DATE | BY | REV. |
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ISSUED FOR CONSTRUCTION 04/10/18 RWF 0

SITE NUMBER:

CT33XC566

SITE ADDRESS:

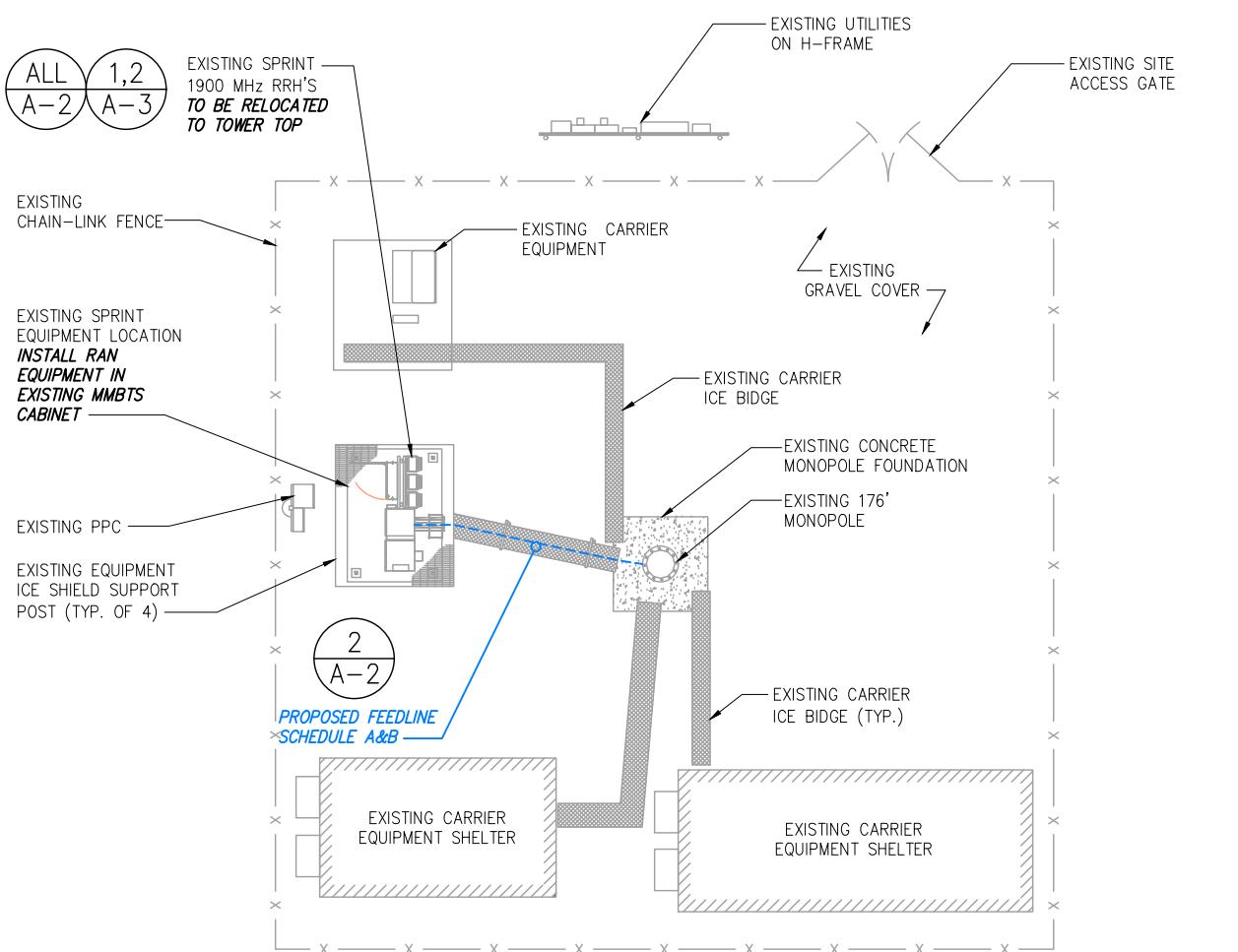
100 OLD TATNIC HILL ROAD
 BROOKLYN, CT 06234

SHEET DESCRIPTION:

SITE PLAN

SHEET NUMBER:

A-1



2
A-2

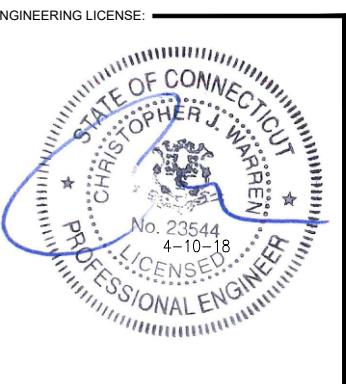
PROPOSED FEEDLINE
SCHEDULE A&B



SOURCE: WESTCHESTER SERVICES 11/16/17



SOURCE: WESTCHESTER SERVICES 11/16/17



CHECKED BY: _____

APPROVED BY: _____

| REVISIONS: | DESCRIPTION | DATE | BY | REV. |
|------------|-------------|------|----|------|
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ISSUED FOR CONSTRUCTION 04/10/18 RWF 0

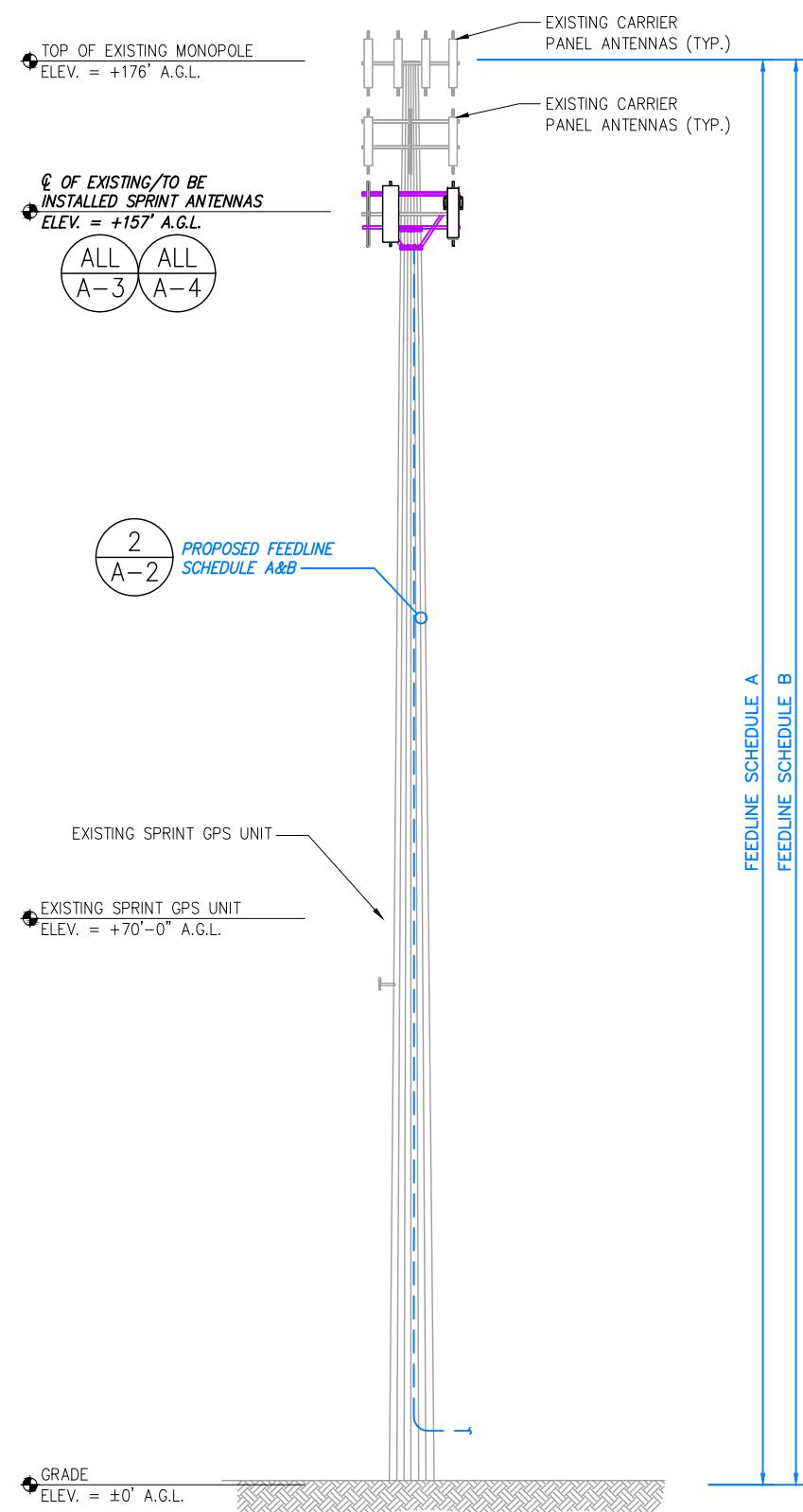
SITE NUMBER: CT33XC566

SITE ADDRESS: 100 OLD TATNIC HILL ROAD BROOKLYN, CT 06234

SHEET DESCRIPTION: TOWER ELEVATION

SHEET NUMBER: A-2

NOTE:
 THESE PLANS HAVE BEEN DEVELOPED FOR THE MODIFICATION OF AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY OWNED OR LEASED BY SPRINT IN ACCORDANCE WITH THE SCOPE OF WORK PROVIDED BY SPRINT. INFINIGY HAS INCORPORATED THIS SCOPE OF WORK IN THE PLANS. THESE PLANS ARE NOT FOR CONSTRUCTION UNLESS ACCCOMPANIED BY A PASSING STRUCTURAL STABILITY ANALYSIS PREPARED BY A LICENSED STRUCTURAL ENGINEER. STRUCTURAL ANALYSIS MUST INCLUDE BOTH TOWER AND MOUNT.



SPECIAL CONSTRUCTION NOTE:
 GENERAL CONTRACTOR SHALL FURNISH AND INSTALL ALL ANTENNA MOUNT STRUCTURAL AUGMENTS (STRUCTURAL MODIFICATIONS) AT SPRINT'S RAD/VERTICAL EQUIPMENT SPACE PER RECOMMENDATIONS FROM SBA-PROVIDED ANTENNA MOUNT STRUCTURAL ANALYSIS AND ANY SUPPLEMENTAL CONSTRUCTION DRAWINGS (PROVIDED BY OTHERS).

NOTE:
 FOR DETAILS OF MOUNT AUGMENT REFER TO MOUNT AUGMENT CD's DONE BY OTHERS

Q of EXISTING/TO BE INSTALLED SPRINT ANTENNAS
ELEV. = +157' A.G.L.

ALL
A-3 A-4

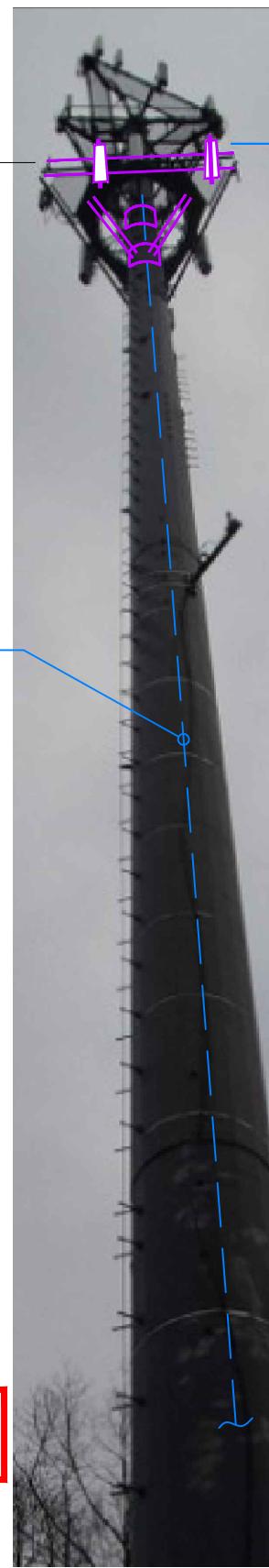
SPECIAL TOWER TOP EQUIPMENT INSTALLATION WORK
NOTE (SAFETY-CLIMB ALIGNMENT REQUIREMENTS):
 GENERAL CONTRACTOR SHALL ORIENT PROPOSED PLATFORM REINFORCEMENT KIT RING-MOUNTS SO THAT EXISTING SAFETY CLIMB CABLE IS NOT OBSTRUCTED/RE-ROUTED FROM VERTICAL ALIGNMENT AND IS NOT IN PHYSICAL CONTACT WITH EXISTING OR PROPOSED RING-MOUNT HARDWARE. GENERAL CONTRACTOR SHALL INSTALL NEW OR ADDITIONAL SAFETY-CLIMB CABLE GUIDES IF ADDITIONAL CLEARANCE IS REQUIRED. ADDITIONAL CABLE GUIDES SHALL BE ATTACHED SECURELY TO THE POLE USING MECHANICAL FASTENERS OR FIELD WELDED BY A CERTIFIED WELDING TECHNICIAN.

| FEEDLINE SCHEDULE | FEEDLINE DESCRIPTION | LOCATION |
|-------------------|--|--------------------------|
| A | EXISTING TO BE REMOVED: (5) 1 5/8" COAX | UP INSIDE MONPOLE TO RAD |
| B | PROPOSED: (4) 1 1/4" HYBRID TO 157' RAD | UP INSIDE MONPOLE TO RAD |

NOTE:
 EXISTING SPRINT EQUIPMENT FEEDLINE INVENTORY BASED ON COLOCATION APPLICATION AND SBA RECORD, NOT FIELD OBSERVATIONS. RFDS AND FEEDLINE LEASING ENTITLEMENTS MAY DIFFER.

SPECIAL INSTALLATION NOTE:
 JUMPERS FROM RRHs TO ANTENNA SHALL NOT EXCEED 15'. NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY DISCREPANCY

NOTE:
 VERIFY PROPOSED AZIMUTHS WITH RF ENGINEER PRIOR TO INSTALLATION

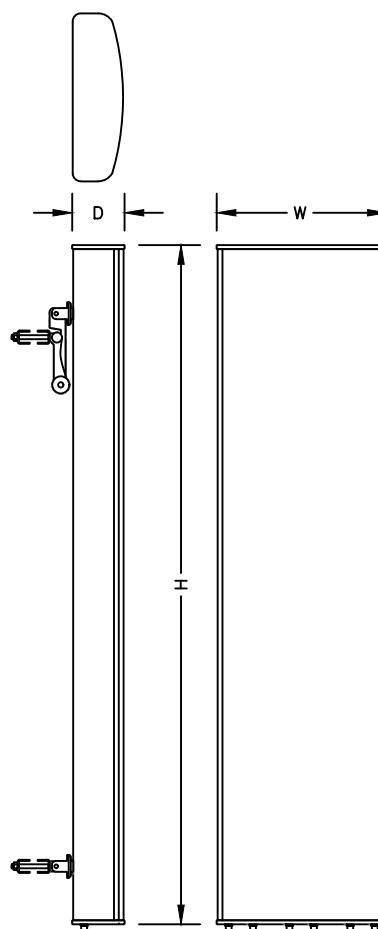
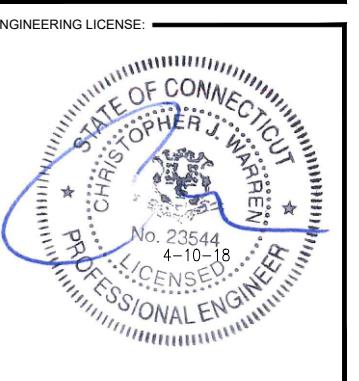


SOURCE: WESTCHESTER SERVICES 11/16/17

PLANS PREPARED FOR:
Sprint
 1 INTERNATIONAL BLVD, SUITE 800
 MAHWAH, NJ 07495
 TEL: (800) 357-7641

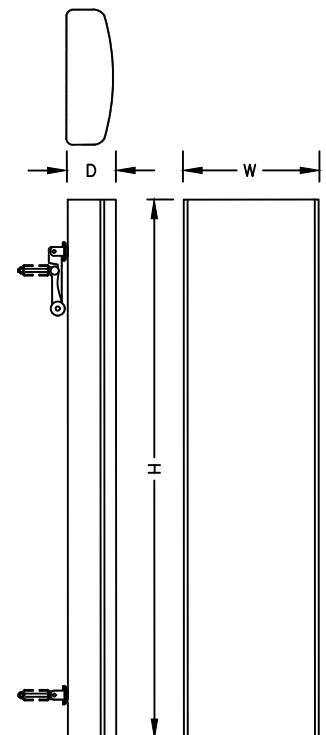
PROJECT MANAGER:
SBA 
 SBA COMMUNICATIONS CORP.
 134 FLANDERS ROAD, SUITE 125
 WESTBOROUGH, MA 01581
 TEL: (508) 251-0720

PLANS PREPARED BY:
INFINIGY®
 FROM ZERO TO INFINIGY
 the solutions are endless
 1033 Watervliet Shaker Rd | Albany, NY 12205
 Phone: 518-690-0790 | Fax: 518-690-0793
www.infinigy.com
 JOB NUMBER 526-104



ANTENNA SPECIFICATIONS

| | |
|---------|-------------|
| MANUF. | COMMSCOPE |
| MODEL # | NNVV-65B-R4 |
| HEIGHT | 72" |
| WIDTH | 19.6" |
| DEPTH | 7.8" |
| WEIGHT | 84.7± LBS. |



ANTENNA SPECIFICATIONS

| | |
|---------|------------------|
| MANUF. | RFS |
| MODEL # | APXVTM14-ALU-I20 |
| HEIGHT | 56.3" |
| WIDTH | 12.6" |
| DEPTH | 6.3" |
| WEIGHT | 56.2± LBS. |

ANTENNA DETAIL

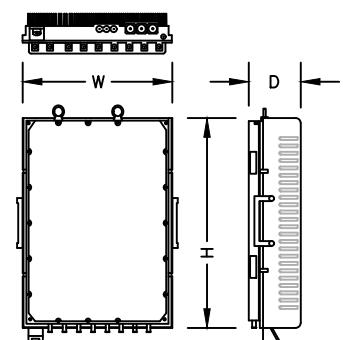
NO SCALE

1

ANTENNA DETAIL

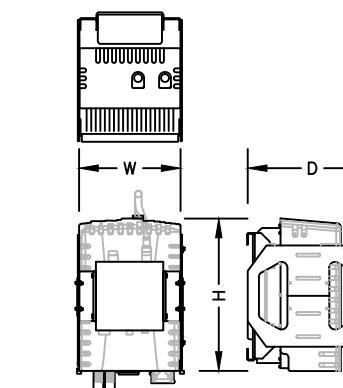
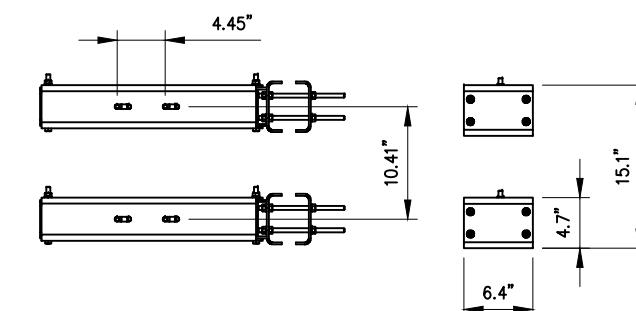
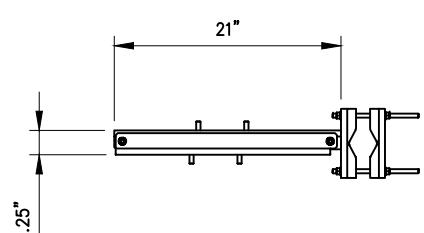
NO SCALE

2



2.5 GHZ RRH SPECIFICATIONS

| | |
|---------|---------------|
| MANUF. | NOKIA (ALU) |
| MODEL # | TD-RRH8X20-25 |
| HEIGHT | 26.1" |
| WIDTH | 18.6" |
| DEPTH | 6.7" |
| WEIGHT | 70± LBS |



800 MHZ RRH SPECIFICATIONS

| | |
|---------|--------------|
| MANUF. | NOKIA (ALU) |
| MODEL # | 800MHZ 2X50W |
| HEIGHT | 19.7" |
| WIDTH | 13" |
| DEPTH | 10.8" |
| WEIGHT | 53± LBS |

2.5 RRH

NO SCALE

3

DUAL RRH MOUNT DETAIL

NO SCALE

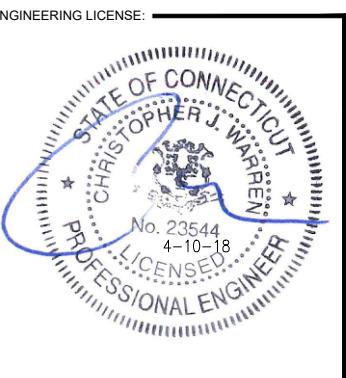
4

800 MHZ RRH

NO SCALE

5

A-4



RFS HYBRIFLEX RISER CABLE SCHEDULE

| Fiber Only (Existing DC Power) | Hybrid cable MN: HB058-M12-050F 12x multi-mode fiber pairs, Top: Outdoor protected connectors, Bottom: LC Connectors, 5/8 cable, 50 ft | 50 ft |
|-----------------------------------|--|--------|
| | MN: HB058-M12-075F | 75 ft |
| | MN: HB058-M12-100F | 100 ft |
| | MN: HB058-M12-125F | 125 ft |
| | MN: HB058-M12-150F | 150 ft |
| | MN: HB058-M12-175F | 175 ft |
| | MN: HB058-M12-200F | 200 ft |

| 8 AWG Power | Hybrid cable MN: HB114-08U3M12-050F 3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 50 ft | 50 ft |
|-------------|--|--------|
| | MN: HB114-08U3M12-075F | 75 ft |
| | MN: HB114-08U3M12-100F | 100 ft |
| | MN: HB114-08U3M12-125F | 125 ft |
| | MN: HB114-08U3M12-150F | 150 ft |
| | MN: HB114-08U3M12-175F | 175 ft |
| | MN: HB114-08U3M12-200F | 200 ft |

| 6 AWG Power | Hybrid cable MN: HB114-13U3M12-225F 3x 6 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 225 ft | 225 ft |
|-------------|--|--------|
| | MN: HB114-13U3M12-250F | 250 ft |
| | MN: HB114-13U3M12-275F | 275 ft |
| | MN: HB114-13U3M12-300F | 300 ft |

| 4 AWG Power | Hybrid cable MN: HB114-21U3M12-325F 3x 4 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 325 ft | 325 ft |
|-------------|--|--------|
| | MN: HB114-21U3M12-350F | 350 ft |
| | MN: HB114-21U3M12-375F | 375 ft |

RFS HYBRIFLEX JUMPER CABLE SCHEDULE

| Fiber Only | Hybrid Jumper cable MN: HBF012-M3-5F1 5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable | 5 ft |
|------------|---|-------|
| | MN: HBF012-M3-10F1 | 10 ft |
| | MN: HBF012-M3-15F1 | 15 ft |
| | MN: HBF012-M3-20F1 | 20 ft |
| | MN: HBF012-M3-25F1 | 25 ft |
| | MN: HBF012-M3-30F1 | 30 ft |

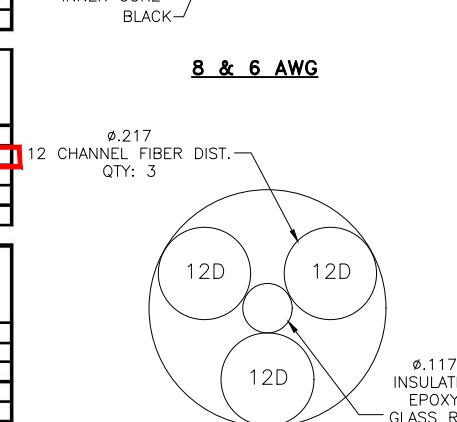
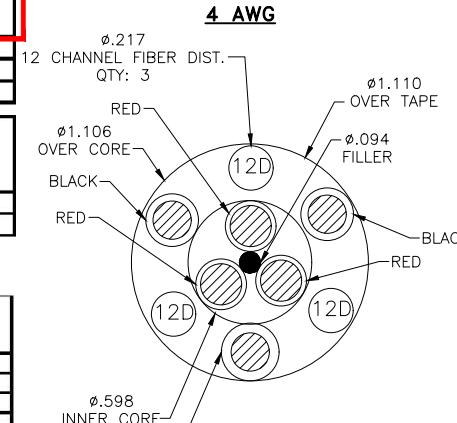
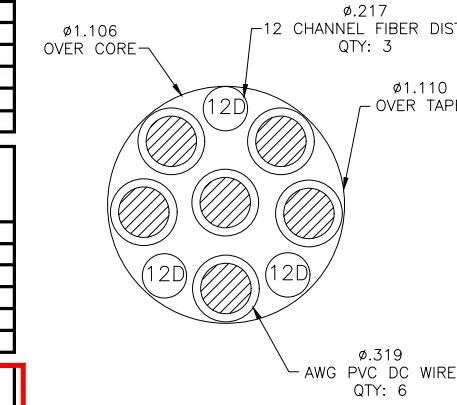
| 8 AWG Power | Hybrid Jumper cable MN: HBF058-08U1M3-5F1 5 ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable | 5 ft |
|-------------|--|-------|
| | MN: HBF058-08U1M3-10F1 | 10 ft |
| | MN: HBF058-08U1M3-15F1 | 15 ft |
| | MN: HBF058-08U1M3-20F1 | 20 ft |
| | MN: HBF058-08U1M3-25F1 | 25 ft |
| | MN: HBF058-08U1M3-30F1 | 30 ft |

| 6 AWG Power | Hybrid Jumper cable MN: HBF058-13U1M3-5F1 5 ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable | 5 ft |
|-------------|--|-------|
| | MN: HBF058-13U1M3-10F1 | 10 ft |
| | MN: HBF058-13U1M3-15F1 | 15 ft |
| | MN: HBF058-13U1M3-20F1 | 20 ft |
| | MN: HBF058-13U1M3-25F1 | 25 ft |
| | MN: HBF058-13U1M3-30F1 | 30 ft |

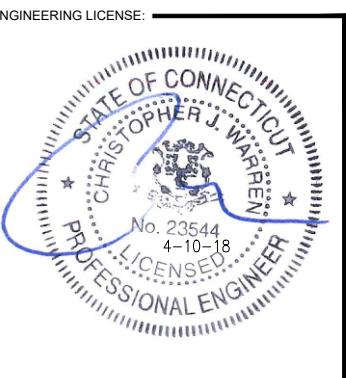
| 4 AWG Power | Hybrid Jumper cable MN: HBF078-21U1M3-5F1 5 ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 7/8 cable | 5 ft |
|-------------|--|-------|
| | MN: HBF078-21U1M3-10F1 | 10 ft |
| | MN: HBF078-21U1M3-15F1 | 15 ft |
| | MN: HBF078-21U1M3-20F1 | 20 ft |
| | MN: HBF078-21U1M3-25F1 | 25 ft |
| | MN: HBF078-21U1M3-30F1 | 30 ft |

NOTE:
 SPRINT CM TO CONFIRM HYBRID OR FIBER RISER CABLE
 AND HYBRID OR FIBER JUMPER CABLE MODEL NUMBERS IF
 HYBRID CABLES ARE REQUIRED BEFORE PREPARING BOM.

- * PROPOSED CABLE LENGTH WAS DETERMINED USING THE SUM OF THE RAD CENTER OF ANTENNAS, AND DISTANCE FROM EXISTING EQUIPMENT AREA TO TOWER BASE WITH AN ADDITIONAL 20' BUFFER. LENGTH TO BE VERIFIED IN FIELD PRIOR TO ORDERING MATERIALS.
- * SPRINT CM TO CONFIRM HYBRID RISER CABLE AND HYBRID JUMPER CABLE MODEL NUMBERS BEFORE PREPARING BOM.

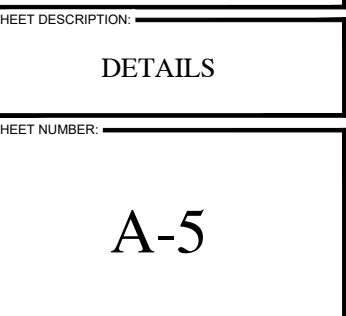


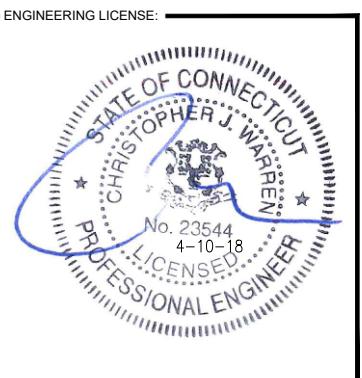
FIBER ONLY



| | |
|-------------------------|--------------------------|
| CHECKED BY: | |
| APPROVED BY: | |
| REVISIONS: | DESCRIPTION DATE BY REV. |
| ISSUED FOR CONSTRUCTION | 04/10/18 RWF 0 |
| SITE NUMBER: | CT33XC566 |

| | |
|--------------------|---|
| SITE ADDRESS: | 100 OLD TATNIC HILL ROAD BROOKLYN, CT 06234 |
| SHEET DESCRIPTION: | DETAILS |
| SHEET NUMBER: | A-5 |





CHECKED BY:

APPROVED BY:

| REVISIONS: | DESCRIPTION | DATE | BY | REV. |
|------------|-------------|------|----|------|
| | | | | |
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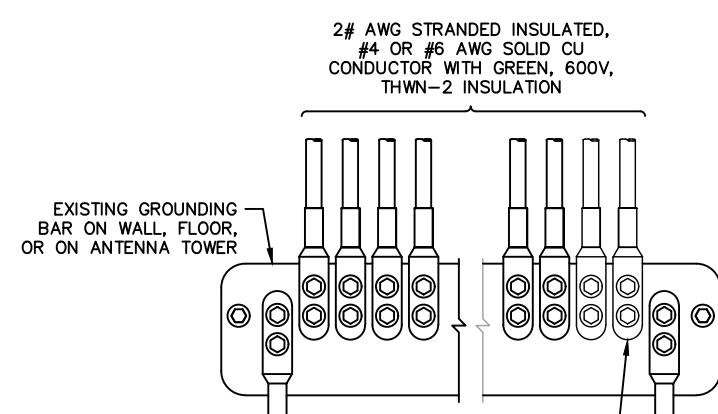
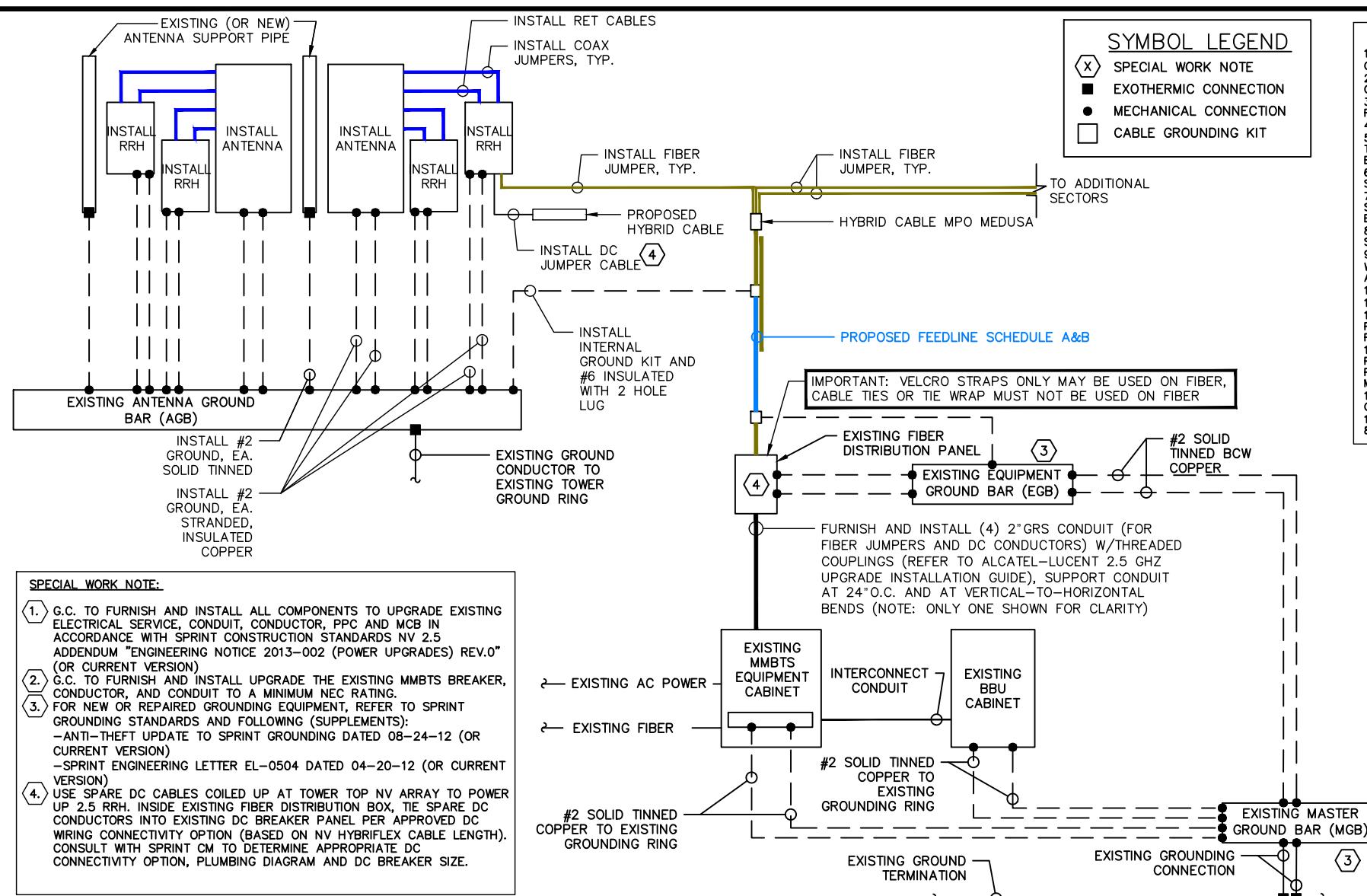
ISSUED FOR CONSTRUCTION 04/10/18 RWF 0

SITE NUMBER: CT33XC566

SITE ADDRESS: 100 OLD TATNIC HILL ROAD
BROOKLYN, CT 06234

SHEET DESCRIPTION: ELECTRICAL & GROUNDING DETAILS

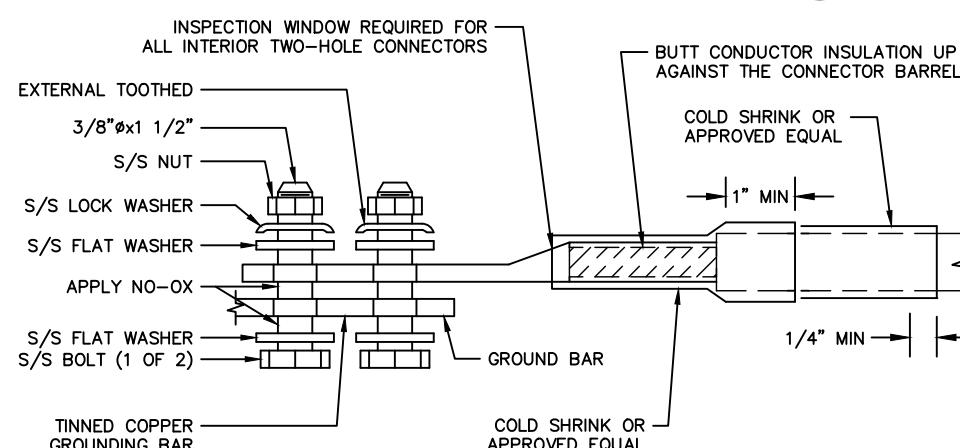
SHEET NUMBER: E-1



INSTALLATION OF GROUNDING CONDUCTOR TO GROUNDING BAR

SCALE: N.T.S.

2
E-1



TWO HOLE LUG

SCALE: N.T.S.

3
E-1



RF Design Sheet



| Site Identification | |
|---------------------|-----------------------|
| Cascade | CT33XC566 |
| SMS Schedule ID | 12323276 |
| SMS Schedule Name | DO Macro Upgrade |
| PID | |
| RRU OEM | ALU |
| Switch OEM | Alcatel Lucent |
| RFDS Issue Date | 2017-08-15 00:00:00.0 |
| RFDS Revision Date | 2017-10-20 10:07:46.0 |
| RFDS Revision | 3 |

| | |
|--------------------------|--|
| Filter Analysis Complete | YES |
| RFDS - Issue Date | 08/15/2017 |
| Design Status | Complete |
| Project Description | DO Macro Upgrade - Add 800MHz (3G + 4G) and 2600 MHz |

| Contact Information | |
|---------------------------|----------------------------|
| Engineer Email | Bill.M.Hastings@sprint.com |
| Sprint Badged RF Engineer | Bill Hastings |
| RF Engineer Email | Bill.M.Hastings@sprint.com |
| RF Engineer Phone | 978-590-9700 |
| RF Manager | Jonathan Hull |
| RF Manager Email | Jonathan.B.Hull@sprint.com |
| RF Manager Phone | 617-233-2020 |

| Carrier Count | |
|---------------|---|
| 2500 LTE | 3 |
| 1900 LTE | 1 |
| 1900 EVDO | |
| 1900 Voice | 1 |
| 800 LTE | 1 |
| 800 Voice | 1 |

| Location Details | |
|------------------|----------------------|
| Latitude | 41.76706 |
| Longitude | -71.97242 |
| Market | Northern Connecticut |
| Region | Northeast |
| City | Brooklyn |
| State | CT |
| Zip Code | 06234 |
| County | Windham |

| | |
|---------|---|
| 2500MHz | 3 |
| 1900MHz | 3 |
| 800MHz | 3 |

| Band: 2500 | Alpha | Beta | Gamma | Delta | Epsilon | Zeta |
|-----------------------|-----------------|-----------------|-----------------|-------|---------|------|
| Radio Model | | | | | | |
| Model Number | TD-RRH8x20-25 | TD-RRH8x20-25 | TD-RRH8x20-25 | N/A | N/A | N/A |
| Weight (lbs) | 76.2 | 76.2 | 76.2 | N/A | N/A | N/A |
| Dimensions | 26 x 18.6 x 6.7 | 26 x 18.6 x 6.7 | 26 x 18.6 x 6.7 | N/A | N/A | N/A |
| Manufacturer | ALU | ALU | ALU | N/A | N/A | N/A |
| Number of RRUs needed | 1 | 1 | 1 | 0 | 0 | 0 |

| Trunk Cable 1 | | | | | | |
|------------------|-----------|-----|-----|-----|-----|-----|
| Model Number | Hybriflex | N/A | N/A | N/A | N/A | N/A |
| Weight (lbs.) | 1 | N/A | N/A | N/A | N/A | N/A |
| Dimensions (In.) | 1.54 | N/A | N/A | N/A | N/A | N/A |
| Manufacturer | ALU | N/A | N/A | N/A | N/A | N/A |

| Band: 800 | Alpha | Beta | Gamma | Delta | Epsilon | Zeta |
|-----------------------|--------------|--------------|--------------|-------|---------|------|
| Radio Model | | | | | | |
| Model Number | RRH-2x50-800 | RRH-2x50-800 | RRH-2x50-800 | N/A | N/A | N/A |
| Weight (lbs) | 69.1 | 69.1 | 69.1 | N/A | N/A | N/A |
| Dimensions | 16 x 13 x 10 | 16 x 13 x 10 | 16 x 13 x 10 | N/A | N/A | N/A |
| Manufacturer | ALU | ALU | ALU | N/A | N/A | N/A |
| Number of RRUs needed | 2 | 2 | 2 | 0 | 0 | 0 |

| Band: 2500 | Alpha | Beta | Gamma | Delta | Epsilon | Zeta |
|--|-------------------|-------------------|-------------------|-------|---------|------|
| Antenna1 | | | | | | |
| Model Number | APXVTM14-ALU-I20 | APXVTM14-ALU-I20 | APXVTM14-ALU-I20 | N/A | N/A | N/A |
| Weight (lbs) | 56.2 | 56.2 | 56.2 | N/A | N/A | N/A |
| Dimensions | 56.3 x 12.6 x 6.3 | 56.3 x 12.6 x 6.3 | 56.3 x 12.6 x 6.3 | N/A | N/A | N/A |
| Manufacturer | RFS | RFS | RFS | N/A | N/A | N/A |
| Ant1 Top Jumper Make/Mode/Qty | 2.5 Jumper | 8 | 2.5 Jumper | 8 | N/A | 0 |
| Ant 1 RF requested Diameter | 1/2" | 1/2" | 1/2" | N/A | N/A | N/A |
| Ant 1 RF requested Top Jumper Length(ft) | 8 | 8 | 8 | N/A | N/A | N/A |
| Antenna 1 Azimuth | 50 | 150 | 300 | N/A | N/A | N/A |
| Antenna 1 Mechanical DT | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Center Line (ft) | 154.9540732 | 154.9540732 | 154.9540732 | N/A | N/A | N/A |
| Antenna 1 Electrical DT | 2 | 2 | 2 | N/A | N/A | N/A |
| Antenna 1 Electrical DT 2 | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Electrical DT 3 | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Twist | N/A | N/A | N/A | N/A | N/A | N/A |

| Band: 1900 | Alpha | Beta | Gamma | Delta | Epsilon | Zeta |
|--|-----------------|-----------------|-----------------|-------|---------|------|
| Antenna1 | | | | | | |
| Model Number | NNVV-65B-R4 | NNVV-65B-R4 | NNVV-65B-R4 | N/A | N/A | N/A |
| Weight (lbs) | 84.7 | 84.7 | 84.7 | N/A | N/A | N/A |
| Dimensions | 72 x 19.6 x 7.8 | 72 x 19.6 x 7.8 | 72 x 19.6 x 7.8 | N/A | N/A | N/A |
| Manufacturer | CommScope | CommScope | CommScope | N/A | N/A | N/A |
| Ant1 Top Jumper Make/Mode/Qty | 800/1900 Jumper | 4 | 800/1900 Jumper | 4 | N/A | 0 |
| Ant 1 RF requested Diameter | 1/2" | 1/2" | 1/2" | N/A | N/A | N/A |
| Ant 1 RF requested Top Jumper Length(ft) | 8 | 8 | 8 | N/A | N/A | N/A |
| Antenna 1 Azimuth | 50 | 150 | 300 | N/A | N/A | N/A |
| Antenna 1 Mechanical DT | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Center Line (ft) | 154.9540732 | 154.9540732 | 154.9540732 | N/A | N/A | N/A |
| Antenna 1 Electrical DT | 3 | 3 | 3 | N/A | N/A | N/A |
| Antenna 1 Electrical DT 2 | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Electrical DT 3 | N/A | N/A | N/A | N/A | N/A | N/A |
| Antenna 1 Twist | N/A | N/A | N/A | N/A | N/A | N/A |



CHECKED BY:

APPROVED BY:

REVISIONS: DESCRIPTION DATE BY REV.

ISSUED FOR CONSTRUCTION 04/10/18 RWF 0

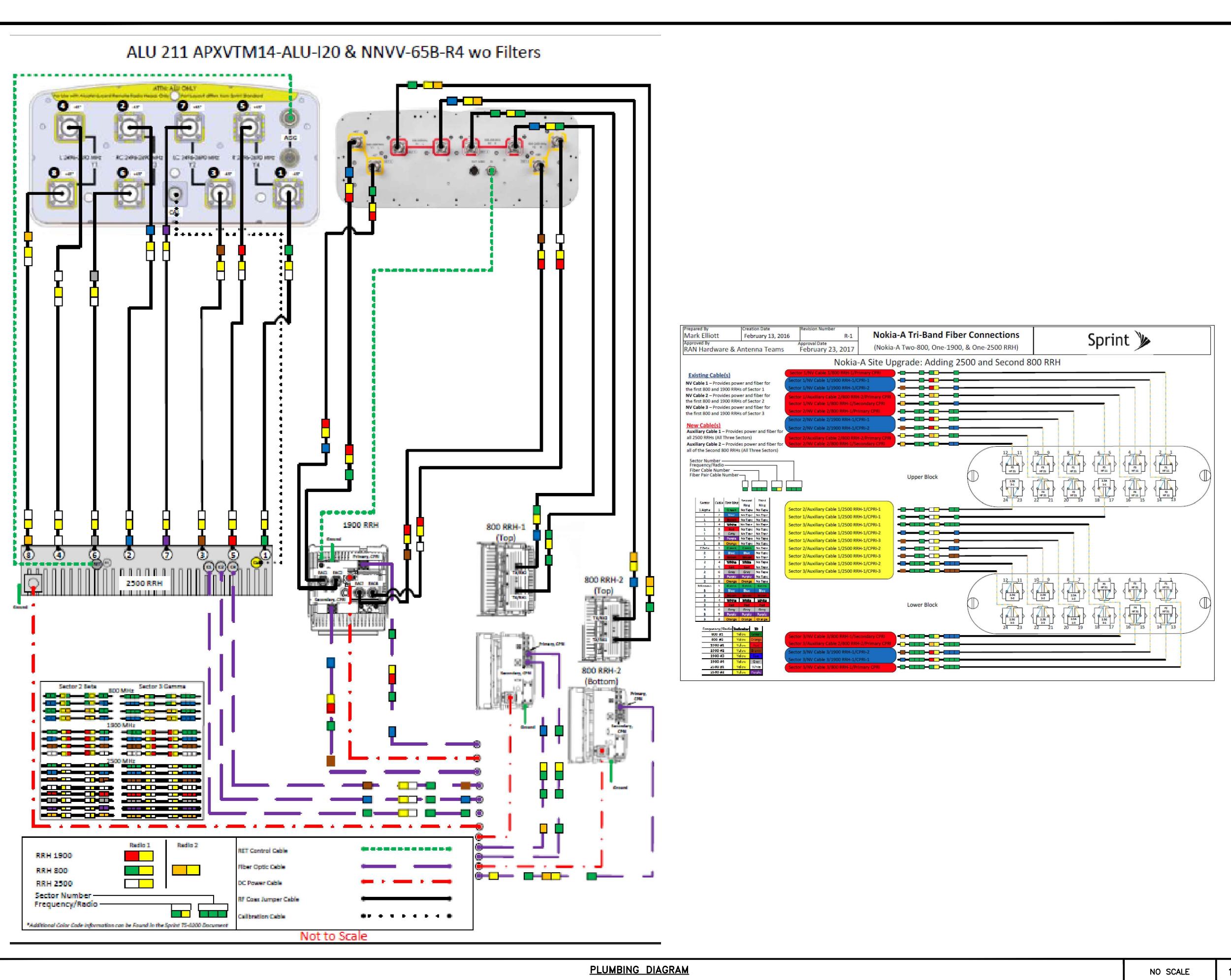
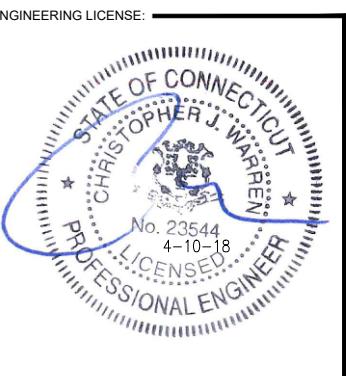
SITE NUMBER: CT33XC566

SITE ADDRESS: 100 OLD TATNIC HILL ROAD BROOKLYN, CT 06234

SHEET DESCRIPTION: RF DATA SHEET

SHEET NUMBER:

RF-1



RF-2



1 INTERNATIONAL BLVD., SUITE 800
MAHWAH, NJ 07495
P: 800.357.7641



134 FLANDERS RD., SUITE 125
WESTBOROUGH, MA 01581
P: 508.251.0720



GEOSTRUCTURAL
PO BOX 2421, BOISE, ID 83701
P: 503.539.4787
E: CONTACT@GEOSTRUCTURAL.COM
WWW.GEOSTRUCTURAL.COM

| REVISIONS: | | |
|------------|----------|------------------------|
| | | |
| | | |
| | | |
| | | |
| 0 | 04/16/18 | ISSUE FOR CONSTRUCTION |
| | | JAD |

CHECKED BY: DWG

THE INFORMATION CONTAINED IN THIS SET OF DOCUMENTS IS PROPRIETARY BY NATURE. ANY USE OR DISCLOSURE OTHER THAN THAT WHICH RELATES TO THE CLIENT NAMES IS STRICTLY PROHIBITED.



SITE INFORMATION:

MOUNT AUGMENTATION

CT33XC566

BROOKLYN, CT

LATITUDE: 41.76716
LONGITUDE: -71.97194

SHEET TITLE:

TITLE SHEET

SHEET NUMBER:

S1

CT33XC566

DO MACRO EQUIPMENT DEPLOYMENT

MOUNT AUGMENTATION @ 157'

MONOPOLE TOWER

BROOKLYN, CT
WINDHAM COUNTY

SITE INFORMATION

STRUCTURE TYPE: MONOPOLE

MOUNT TYPE: PLATFORM

LATITUDE: 41.76716 (NAD 83)

LONGITUDE: -71.97194 (NAD 83)

CITY, STATE: BROOKLYN, CT

COUNTY: WINDHAM

SBA SITE: CT01915-S South Brooklyn

COORDINATES ARE FOR NAVIGATIONAL PURPOSES ONLY, NOT TO 1A ACCURACY.

DO NOT SCALE DRAWINGS

CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, CONDITIONS ON THE JOB SITE & SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR THE LABOR & MATERIALS FOR THE DISCREPANCIES.

CODE COMPLIANCE

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES.

BUILDING CODE AND DESIGN STANDARD: 2012 IBC / TIA-222-G / 2016 CT

RIGGING PLAN REQUIRED

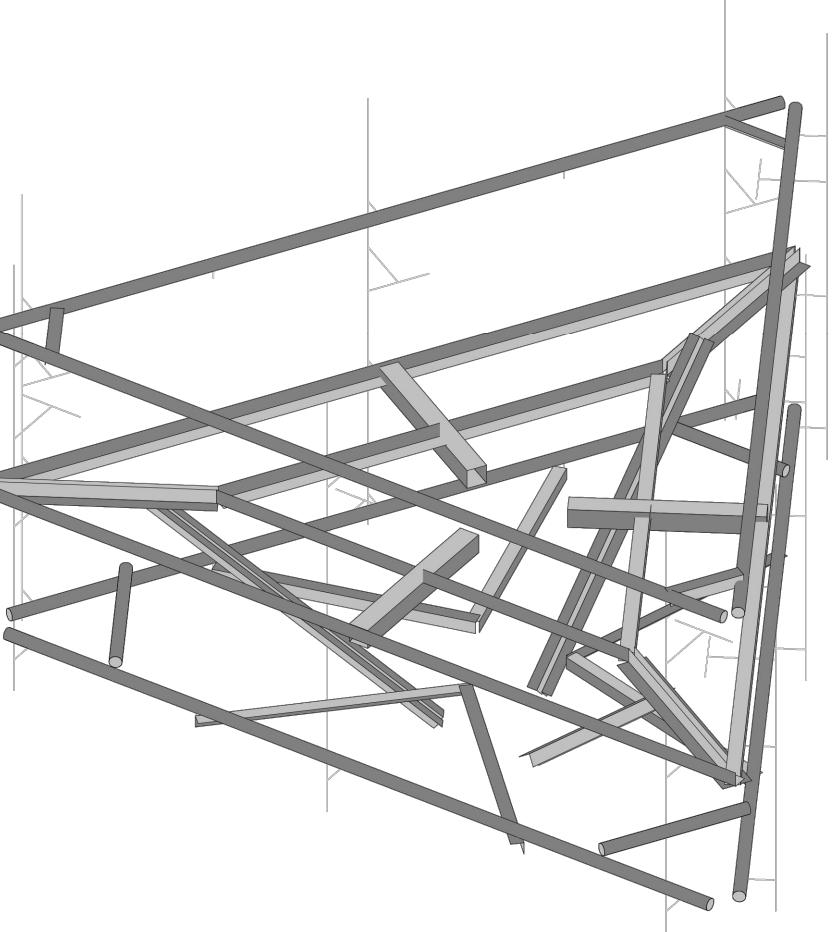
THIS SET OF PLANS DOES "NOT" CONSTITUTE A RIGGING PLAN.

A PROPER RIGGING PLAN SHALL BE PERFORMED BY A LICENSED PROFESSIONAL ENGINEER PRIOR TO PROCEEDING ON ANY AUGMENTATIONS SHOWN HEREIN.

GENERAL DESIGN NOTES

1. THIS PLAN HAS BEEN DESIGNED UTILIZING THE CORRESPONDING MOUNT STRUCTURAL ANALYSIS.
2. THESE PLANS HAVE BEEN DESIGNED IN ACCORDANCE WITH THE GOVERNING PROVISIONS OF TIA/EIA-222, ASCE 7, AWS, ACI, AND AISC. MATERIALS AND SERVICES PROVIDED BY THE CONTRACTOR SHALL CONFORM TO THE ABOVE-MENTIONED CODES AND THE CONTRACT SPECIFICATIONS.
3. ALL STRUCTURE INFORMATION OBTAINED IN THE FORM OF INFORMATION PROVIDED BY THE CLIENT. CONTRACTOR SHALL OBTAIN AND BECOME FAMILIAR WITH THE REFERENCED DOCUMENTS. CONTRACTOR SHALL ISSUE A REQUEST FOR INFORMATION (RFI) IN THE EVENT ANY DISCREPANCIES ARE DISCOVERED BETWEEN THESE DOCUMENTS AND THE AS-BUILT CONDITIONS IN THE FIELD IN A SITE VISIT THAT SHALL BE PERFORMED PRIOR TO STARTING FABRICATION OR CONSTRUCTION.
4. ALL MATERIALS UTILIZED FOR THIS PROJECT MUST BE NEW AND FREE OF ANY DEFECTS.
5. ALL PRODUCT OR MATERIAL SUBSTITUTIONS PROPOSED BY THE CONTRACTOR SHALL BE APPROVED IN WRITING BY THE ENGINEER. CONTRACTOR SHALL PROVIDE DOCUMENTATION TO ENGINEER SUITABLE TO DETERMINE IF SUBSTITUTE IS ACCEPTABLE FOR USE AND MEETS THE ORIGINAL DESIGN CRITERIA. DIFFERENCES FROM THE ORIGINAL DESIGN, INCLUDING MAINTENANCE, REPAIR AND REPLACEMENT, SHALL BE NOTED. ESTIMATES OF COSTS/CREDITS ASSOCIATED WITH THE SUBSTITUTION (INCLUDING RE-DESIGN COSTS AND COSTS TO SUB-CONTRACTORS) SHALL BE PROVIDED TO THE ENGINEER. CONTRACTOR SHALL PROVIDE ADDITIONAL DOCUMENTATION AND/OR SPECIFICATIONS TO THE ENGINEER AS REQUESTED.
6. PROVIDE STRUCTURAL STEEL SHOP DRAWING(S) TO THE ENGINEER OF RECORD FOR APPROVAL PRIOR TO FABRICATION (ONLY IF SPECIFICALLY REQUESTED BY ENGINEER).
7. UNLESS NOTED OTHERWISE, ALL NEW MEMBERS AND REINFORCING SHALL MAINTAIN THE EXISTING MEMBER WORK LINES AND NOT INTRODUCE ECCENTRICITIES INTO THE STRUCTURE.
8. ANY CONTRACTOR-CAUSED DAMAGE TO PROPERTY OF THE LAND OWNER, PROPERTY OF THE STRUCTURE OWNER, PROPERTY OF THE CUSTOMER, SITE FENCING OR GATES, ANY AND ALL UTILITY AND/OR SERVICE LINES, SHOWN OR NOT SHOWN ON THE PLANS, SHALL BE REPAIRED OR REPLACED AT THE SOLE COST OF THE CONTRACTOR AND SHALL BE ACCOMPLISHED BY THE CONTRACTOR OR SUBCONTRACTOR AS APPROVED BY THE ENGINEER OF RECORD AND LAND OWNER. DAMAGE TO EQUIPMENT OR PROPERTY OF ANY KIND BELONGING TO OTHER COMPANIES (BESIDES THE INDICATED CUSTOMER) SHALL BE ADDRESSED BY THE CONTRACTOR WITH THE COMPANIES THAT OWN THE DAMAGED ITEMS.

MOUNT AUGMENTATION CONFIGURATION



AUGMENTATION SCOPE

AUGMENT ALL SECTORS OF CARRIER'S EXISTING MOUNT INSTALLATION AS REQUIRED (UNLESS NOTED OTHERWISE)

CONTRACTOR NOTES

- PRIOR TO BEGINNING CONSTRUCTION, ALL CONTRACTORS AND SUBCONTRACTORS MUST ACKNOWLEDGE IN WRITING TO TOWER OWNER THAT THEY HAVE OBTAINED, UNDERSTAND, AND WILL FOLLOW STRUCTURE OWNER STANDARDS OF PRACTICE, CONSTRUCTION GUIDELINES, ALL SITE AND STRUCTURE/TOWER SAFETY PROCEDURES, ALL PRODUCT LIMITATIONS AND INSTALLATION PROCEDURES USED ON SITE, AND PROPOSED AUGMENTATIONS DESCRIBED. RECEIPT OF ACKNOWLEDGEMENT MUST OCCUR PRIOR TO BEGINNING CONSTRUCTION OR CLIMBING. IT IS THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO PROVIDE THIS DOCUMENTATION FOR STRUCTURE OWNER ON COMPANY LETTERHEAD AND THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO OBTAIN THIS DOCUMENTATION FROM ANY SUBCONTRACTORS (ON SUBCONTRACTOR LETTERHEAD) AND DELIVER IT TO THE STRUCTURE OWNER.
- IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT ARE NOT REPRESENTED ON THESE DRAWINGS, OR ANY CONDITIONS THAT WOULD INTERFERE WITH THE INSTALLATION OF THE AUGMENTATIONS, THE ENGINEER OF RECORD SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE SIGNIFICANCE OF THE DEVIATION.
- THE CONTRACTOR SHALL SOLICIT AND HIRE THE SERVICES OF A QUALIFIED AUGMENTATION INSPECTOR PRIOR TO BEGINNING CONSTRUCTION. THE AUGMENTATION INSPECTOR MAY BE AN EMPLOYEE OF THE CONTRACTOR'S FIRM, HOWEVER THE INSPECTOR'S ONLY DUTIES SHALL BE INSPECTION, TESTING, AND REPORT CREATION AS REQUIRED ON THE "AUGMENTATION INSPECTION NOTES" SHEET.
- THE CONTRACTOR SHALL NOTIFY THE TOWER OWNER OF THE PLANNED CONSTRUCTION & INSPECTION SCHEDULE, AS WELL AS ANY CHANGES TO THE SCHEDULE, WITHIN TWO BUSINESS DAYS OF THE COMPLETION OF THE SCHEDULE OR SCHEDULE REVISION BOTH PRIOR TO BEGINNING CONSTRUCTION AND DURING CONSTRUCTION AS THE SCHEDULE CHANGES. THE STRUCTURE OWNER WHEN THE WORK HAS BEEN COMPLETED WITHIN 2 BUSINESS DAYS OF THE COMPLETION OF THE WORK AND ASSOCIATED AUGMENTATION INSPECTIONS & TESTING (WHEN APPLICABLE).
- IT IS ASSUMED THAT ANY STRUCTURAL AUGMENTATION WORK SPECIFIED ON THESE PLANS WILL BE ACCOMPLISHED BY KNOWLEDGEABLE WORKMEN WITH TOWER CONSTRUCTION EXPERIENCE. THIS INCLUDES PROVIDING THE NECESSARY CERTIFICATIONS TO THE STRUCTURE OWNER AND ENGINEER INCLUDING BUT NOT LIMITED TO TOWER CLIMBER AND RESCUE CLIMBER CERTIFICATIONS, ET CETERA.
- THESE DRAWINGS DO NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION METHODS, MEANS, TECHNIQUES, SEQUENCES AND PROCEDURES.
- CONTRACTOR SHALL WORK WITHIN THE LIMITS OF THE STRUCTURE OWNER'S PROPERTY OR LEASE AREA AND APPROVED EASEMENTS. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY WORK IS WITHIN THESE BOUNDARIES. CONTRACTOR SHALL EMPLOY A SURVEYOR AS REQUIRED. ANY WORK OUTSIDE THESE BOUNDARIES SHALL BE APPROVED IN WRITING BY THE LAND OWNER PRIOR TO MOBILIZATION. CONSTRUCTION STAKING AND BOUNDARY MARKING IS THE RESPONSIBILITY OF THE CONTRACTOR.

STRUCTURAL ERECTION AND BRACING REQUIREMENTS

- THE STRUCTURAL DRAWINGS ILLUSTRATE THE COMPLETED STRUCTURE WITH ALL ELEMENTS IN THEIR FINAL POSITIONS, PROPERLY SUPPORTED AND BRACED.
- THE CONTRACTOR SHALL PROVIDE SHORING AND BRACING AS REQUIRED DURING CONSTRUCTION TO ENSURE STABILITY. DESIGN AND SEQUENCING OF CONSTRUCTION SHORING AND BRACING IS OUTSIDE THE SCOPE OF THIS WORK.
- THE CONTRACTOR IS RESPONSIBLE FOR THE DESIGN AND EXECUTION OF ALL MISCELLANEOUS SHORING, BRACING, TEMPORARY SUPPORTS, GUYING, ETC. NECESSARY TO PROVIDE A COMPLETE AND STABLE STRUCTURE AS SHOWN ON THESE DRAWINGS.

BOLTS

- ALL CONNECTIONS OF STRUCTURAL STEEL MEMBERS SHALL BE MADE USING SPECIFIED GALVANIZED HIGH STRENGTH ASTM A325 OR A490 BOLTS WITH THREADS EXCLUDED FROM SHEAR PLANE.
- FASTENERS SHALL BE INSTALLED IN PROPERLY ALIGNED HOLES, WITH BOLT HEADS FACING DOWN WHERE APPLICABLE.
- ALL BOLTS AT EVERY CONNECTION SHALL BE INSTALLED SNUG-TIGHT UNTIL THE SECTION IS FULLY COMPACTED AND ALL PLIES ARE JOINED, AND THEN TIGHTENED FURTHER BY AISC - 'TURN OF THE NUT' METHOD. TIGHTENING SHALL PROGRESS SYSTEMATICALLY.
- BOLT LENGTHS UP TO AND INCLUDING 4 DIAMETERS SHALL BE TENSIONED 1/3 TURN BEYOND SNUG-TIGHT. BOLT LENGTHS OVER 4 DIAMETERS SHALL BE 1/2 TURNS BEYOND SNUG-TIGHT.
- ALL BOLTED CONNECTIONS SHALL USE LOCK WASHERS.

STRUCTURAL STEEL

- STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED, AND ERECTED IN ACCORDANCE WITH THE CURRENT EDITION OF THE AISC STEEL CONSTRUCTION MANUAL AND SECTION 4 OF THE TIA CODE.
- PRE-QUALIFIED STRUCTURAL STEEL SHALL CONFORM TO THE FOLLOWING MINIMUM GRADES UNLESS OTHERWISE NOTED:
 - CHANNELS & ANGLES ASTM A36, (Fy = 36 KSI)
 - PLATES ASTM A36, (Fy = 36 KSI)
 - PIPES ASTM A53 GR.B, (Fy = 35 KSI)
 - HSS ROUND ASTM A500 GR.B, (Fy = 42 KSI)
 - HSS RECTANGULAR ASTM A500 GR.B, (Fy = 46 KSI)
 - STRUCTURAL BOLTS ASTM A325
 - U-BOLTS ASTM A307 GR.A
 - NUTS FOR BOLTS ASTM A563 (THREADING TO MATCH BOLT)
 - WASHERS FOR BOLTS ASTM F436
 - SEE TABLE 5-1 OF THE TIA CODE FOR ADDITIONAL SHAPES AND STANDARDS THAT ARE NOT LISTED ABOVE.
- NON PRE-QUALIFIED STRUCTURAL STEEL SHALL CONFORM TO THE FOLLOWING STANDARDS PER THE TIA CODE:
 - THE CARBON EQUIVALENT OF STEEL SHALL NOT EXCEED 0.65 PER SECTION 5.4.2 OF THE TIA CODE
 - ELONGATION OF STEEL SHALL NOT BE LESS THAN 18%
 - TEST REPORTS SHALL BE IN ACCORDANCE WITH ASTM A6 OR A568
 - TOLERANCES SHALL BE IN ACCORDANCE WITH ASTM A6
- FIELD CUT EDGES, EXCEPT DRILLED HOLES, SHALL BE GROUND SMOOTH AND COLD GALVANIZED.
- ALL WELDING WORK SHALL CONFORM TO THE AWS D1.1 STRUCTURAL WELDING CODE. ALL WELDING SHALL BE PERFORMED BY CERTIFIED WELDERS ONLY. WELDING ELECTRODES SHALL BE E70XX.
- ALL DETAILING, FABRICATION AND ERECTION OF STRUCTURAL STEEL SHALL CONFORM TO AISC SPECS AND CODES, LATEST EDITION.
- UPON REQUEST, THE CONTRACTOR SHALL SUBMIT DETAILED, ENGINEERED, COORDINATED AND CHECKED SHOP DRAWINGS FOR ALL STRUCTURAL STEEL TO THE ENGINEER OF RECORD TO REVIEW FOR COMPLIANCE WITH DESIGN INTENT PRIOR TO THE START OF FABRICATION AND/OR ERECTION.
- TORCH-CUTTING OF ANY KIND SHALL NOT BE PERMITTED.
- ALL BOLT HOLES SHALL BE STANDARD SIZE BOLT HOLES PER AISC 360, UNLESS OTHERWISE NOTED. ALL HOLES SHALL BE SHOP DRILLED OR SUB-PUNCHED AND REAMED. BURNING OF HOLES IS NOT PERMITTED. WHERE SLOTTED OR OVERSIZE HOLES ARE SPECIFIED ON THE DRAWINGS, EXTRA-THICK ASTM F436 PLATE WASHERS SHALL BE USED (3/16" MINIMUM THICKNESS) WITH A DIAMETER SUITABLE TO COVER THE EXTENTS OF THE SLOT OR HOLE. BOLTS SHALL BE HEAVY-HEX WHERE AVAILABLE IN THE SIZE AND GRADE SPECIFIED, OTHERWISE BOLTS SHALL BE HEX HEAD CAP SCREWS.
- ALL STEEL HARDWARE, INCLUDING ADHESIVE OR EMBEDDED ANCHOR BOLTS AND THEIR ACCESSORIES, SHALL BE HOT-DIP GALVANIZED IN ACCORDANCE WITH ASTM A153 (EXCEPT BOLTS SMALLER THAN 1/2" SHALL CONFORM TO FE/ZN 3 AT PER ASTM F1941 WHERE HOT-DIP GALVANIZED BOLTS ARE NOT AVAILABLE). ALL STEEL MEMBERS, INCLUDING WELDMENTS, SHALL BE HOT-DIP GALVANIZED IN ACCORDANCE WITH ASTM A123. REPAIR DAMAGE TO GALVANIZED COATINGS USING ASTM A780 PROCEDURES WITH A ZINC RICH PAINT (SUCH AS ZINC GALVILITE) FOR GALVANIZING DAMAGED BY HANDLING, TRANSPORTING, CUTTING, WELDING, OR BOLTING. DO NOT HEAT SURFACES TO WHICH REPAIR PAINT HAS BEEN APPLIED. CALL OUT HOLES REQUIRED FOR HOT-DIP GALVANIZING ON SHOP DRAWINGS.
- MEMBERS SHALL BE SHOP-FABRICATED AND WELDED TO THE EXTENT PRACTICABLE IN ORDER TO REDUCE FIELD INSTALLATION COSTS.

NOMINAL HOLE DIMENSIONS

| BOLT Ø | STANDARD HOLE Ø |
|--------|-----------------|
| 1/2"Ø | 9/16"Ø |
| 5/8"Ø | 11/16"Ø |
| 3/4"Ø | 13/16"Ø |
| 7/8"Ø | 15/16"Ø |
| 1"Ø | 1 1/16"Ø |



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SITE INFORMATION:

MOUNT AUGMENTATION

CT33XC566

BROOKLYN, CT

LATITUDE: 41.76716
LONGITUDE: -71.971949

SHEET TITLE:
NOTES AND SPECIFICATIONS

SHEET NUMBER:
S2



REVISIONS:

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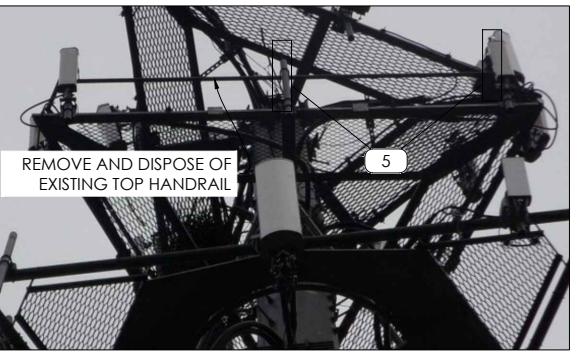
SHEET TITLE:
**AUGMENTATIONS,
SECTIONS &
DETAILS**

SHEET NUMBER:

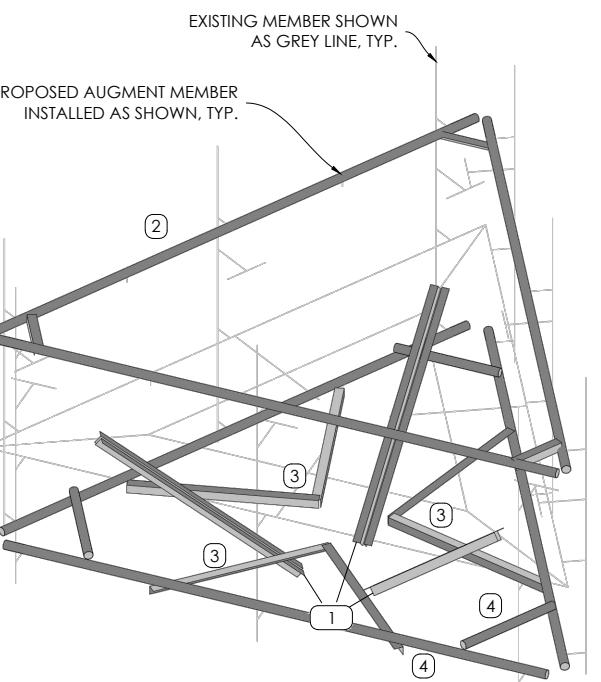
S3

NEW MOUNT AUGMENTATIONS

- 1 PLATFORM REINFORCEMENT KIT
SITPRO1 PART# PRK-1245L. ATTACH PRK COLLAR TO MONOPOLE SHAFT ~4.0' BELOW EXISTING STANOFF CENTERLINE AND DOUBLE ANGLE KICKER BRACKET TO BACK-TO-BACK ANGLES AT PLATFORM CORNERS AS SHOWN PER MANUF. SPECS. [(1) KIT TOTAL]
 - 2 HANDRAIL KIT COMPONENTS
SITPRO1 PART# HRK12-U OR HRK14-U. ATTACH TO MOUNT PIPES ~3.0' ABOVE EXISTING STANOFF CENTERLINE. VERIFY MOUNT FACE WIDTH IN FIELD PRIOR TO ORDERING. [(1) KIT TOTAL]
 - 3 HANDRAIL KIT COMPONENTS - V-BRACE KIT
SITPRO1 PART# PRK-SFS-H-L. ATTACH COLLAR MOUNT TO MONOPOLE SHAFT ~2.5' BELOW EXISTING STANOFF CENTERLINE. NOTE: IF THE PRK-SFS-H-L KIT IS NOT AVAILABLE, PROVIDE (6) TOTAL L $\frac{1}{2}$ x2 $\frac{1}{2}$ x $\frac{3}{8}$ x ~8' LONG REPLACEMENT ANGLES, FIELD-CUT AND DRILL TO SUIT. [(1) KIT TOTAL]
 - 4 HANDRAIL KIT COMPONENTS - BOTTOM FACE RAIL
 - PIPE2.0STD X 14.0' HORIZ. RAIL, [(3) TOTAL]. ATTACH SFS-H-L KIT ANGLES TO NEW HORIZ. RAIL.
 - PIPE2.0STD X ~4' LONG CORNER BRACE, [(3) TOTAL]. ATTACH TO NEW HORIZ. RAIL W/ (6) SITPRO1 PART# PUCK BRACKETS.
 - PIPE2.0STD X 8.0' MOUNT PIPES, [(9) TOTAL] W/ SITEPRO1 SCX x-K, [(9) TOTAL] CROSS-OVER PLATES. ATTACH ALL MOUNT PIPES TO EXISTING AND NEW HORIZ. RAILS.
 - 1/2"Ø OR 5/8"Ø U-BOLTS, (18) TOTAL. ATTACH ALL MOUNT PIPES TO EXISTING BOTTOM RAIL W/ (2) U-BOLTS.
 - 5 PANEL ANTENNAS TO BE INSTALLED IN POSITIONS 1 AND 3 (AS CLOSE TO THE CENTER OF FACE NEAR EXISTING STANOFF AS POSSIBLE. RRH UNITS TO BE INSTALLED ON DUAL SWIVEL BRACKETS BEHIND PANEL ANTENNAS IN POSITIONS 1 AND 3.
LOWER THE PANEL ANTENNA INSTALLATION CENTERLINE APPROXIMATELY 1.5'.
- AUGMENTATIONS SHALL BE COMPLETED PRIOR TO THE INSTALLATION OF ANY NEW EQUIPMENT.

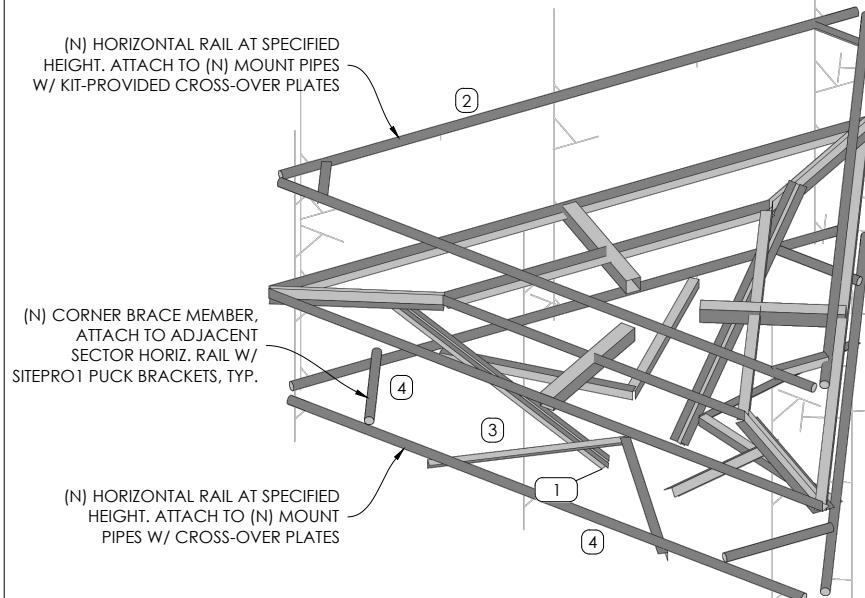


PLATFORM @ 157' AUGMENTATION



CONSTRUCTION NOTES

1. SCOPE OF WORK MUST BE COMPLETED AT WIND SPEEDS < 20 MPH.
2. ALL DIMENSIONS ARE APPROXIMATE. CONTRACTOR SHOULD FIELD-VERIFY ALL DIMENSIONS BEFORE FABRICATION OF STEEL AND COMMENCEMENT OF WORK. FIELD CUT MEMBERS AS REQUIRED.
3. CONTRACTOR TO COORDINATE THE TEMPORARY REMOVAL/RELOCATION/REPLACEMENT OF ELEMENTS (E.G. COAX, CLIPS, TMAs, ETC.) CONNECTED TO, OR IN THE DIRECT PATH, OF NEW AUGMENTATION MEMBERS.



INSTALLATION NOTES

1. AUGMENT MEMBER(S) MAY NEED TO BE FIELD-CUT TO LENGTH TO ACCOMMODATE THIS INSTALLATION. CONTRACTOR TO CUT AND DRILL TO SUIT AS REQUIRED AND APPLY (2) COATS OF COLD-GALV. COMPOUND TO CUT MEMBER ENDS.
2. CONTRACTOR TO CHECK ALL EXISTING MEMBER CONNECTION BOLTS, PARTICULARLY STANOFF TO TOWER BOLTS, FOR PROPER INSTALLATION AND TIGHTNESS.
3. COORDINATE PLACEMENT OF NEW AUGMENT MEMBERS WITH EXISTING TOWER AND CLIMBING FACILITY ELEMENTS (E.G. STEP PEGS, COAX PORTS, ETC.)
4. REFER TO CONSTRUCTION DRAWINGS (BY OTHERS) AND MOUNT STRUCTURAL ANALYSIS FOR APPROVED INSTALLATION LOCATIONS AND QUANTITIES OF APPURTENANCES.

