Alex Murshteyn, Site Acquisition Consultant c/o Cellco Partnership d/b/a Verizon Wireless
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767
Mobile: (508) 821-0159
AMurshteyn@centerlinecommunications.com
February 16, 2018
Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051


RE: Notice of Exempt Modification // Site: Brookfield CT (ATC: 283426)
37 Carmen Hill Road, Brookfield, CT 06804
N 41.4929 // W 73.4273
Dear Ms. Bachman:


Cellco Partnership d/b/a Verizon Wireless currently maintains 12 antennas at the 79-foot and 71foot mounts on the existing 80 -foot self-supporting lattice tower, located at 37 Carmen Hill Road, Brookfield, CT. The tower and property are owned by American Tower. The Council approved Verizon Wireless use of this tower in 1995. Verizon Wireless now intends remove 6 of its antennas on the 71 -foot level plus all 3 of its antennas on the 79 -foot level to replace with 6 new ones on the 79 -foot level only, and install them on side-by-side mounts for its LTE ( $700 / 850 / 1900 / 2100 \mathrm{MHz}$ ) replacements as a part of its PCS/AWS/LTE upgrade. Additionally, Verizon Wireless will install 9 new remote radio head units (RRUs), including 3 replacements, to bring the total RRU count to 12, as well as 1 replacement over voltage protector (OVP) surge arrestor box, and 1 new hybrid fiber cable; altogether updating leased equipment rights, as reflected by the final configuration outlined in the structural analysis and proposed hereby.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16$50 \mathrm{j}-72(\mathrm{~b})(2)$. In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Stephen C. Dunn, First Selectman for the Town of Brookfield, its Land Use Director Alice Dew, including for the Planning and Zoning Commissions and to American Tower Corporation for American Towers LLC, which is the tower and ground owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Enclosed to accommodate this filing are construction drawings dated February 12, 2018 by ATC Tower Services, LLC, a structural analysis dated

February 8,2018 by A.T. Engineering Service, PLLC and radio frequency (RF) analysis table showing worst-case RF emission calculation by Verizon Wireless RF Design Engineering.

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading, as shown in the attached structural analysis by A.T. Engineering Service, PLLC, dated February 8, 2018.

For the foregoing reasons, Verizon Wireless respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,
 c/o Cellco Partnership d/b/a Verizon Wireless
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767
Mobile: (508) 821-0159
AMurshteyn@centerlinecommunications.com
Attachments
cc: Stephen C. Dunn, First Selectman - as elected official - 1Z9Y45030337370698
Alice Dew, Land Use Director - as P\&Z official - 1Z9Y45030339287301
American Tower Corporation - as tower \& property owner - 1Z9Y45030332796916

AMERICAN TOWER ${ }^{*}$
CORPORATION

## Structural Analysis Report

| Structure | $: 80$ ft Self Supported Tower |
| :--- | :--- |
| ATC Site Name | $:$ Brookfield CT, CT |
| ATC Site Number | $: 283426$ |
| Engineering Number | $:$ OAA722914_C3_01 |
| Proposed Carrier | $:$ Verizon |
| Carrier Site Name | $:$ Brookfield CT |
| Carrier Site Number | $:$ PSLC\# 468123 |
| Site Location | $: 37$ Carmen Hill Road |
|  | Brookfield, CT 06804-1004 |
| County | Fairfield |
| Date | February 8, 2018 |
| Max Usage | Pass |
| Result |  |

Feb 82018 5:31 PM

## AMERICANTOWER ${ }^{*}$

CORPORATION

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## Introduction

The purpose of this report is to summarize results of a structural analysis performed on the 80 ft self supported tower to reflect the change in loading by Verizon.

## Supporting Documents

| Tower Drawings | HTS Mapping Site \#KGI11464, dated February 21, 2008 |
| :--- | :--- |
| Foundation Drawing | ETS Mapping Job \#173310, dated November 30, 2017 |
| Geotechnical Report | FDH mapping Project \#17QQWL1600, dated November 30, 2017 |

## Analysis

The tower was analyzed using American Tower Corporation's tower analysis software. This program considers an elastic three-dimensional model and second-order effects per ANSI/TIA-222.

| Basic Wind Speed: | 93 mph (3-Second Gust, Vasd) / 115 mph (3-Second Gust, Vult) |
| :--- | :--- |
| Basic Wind Speed w/ Ice: | $50 \mathrm{mph}(3-$ Second Gust) w/3/4" radial ice concurrent |
| Code: | ANSI/TIA-222-G / 2012 IBC / 2016 Connecticut State Building Code |
| Structure Class: | II |
| Exposure Category: | B |
| Topographic Category: | 3 |
| Crest Height: | 116 ft |
| Spectral Response: | $\mathrm{Ss}=0.21, \mathrm{~S}_{1}=0.07$ |
| Site Class: | D - Stiff Soil |

## Conclusion

Based on the analysis results, the structure meets the requirements per the applicable codes listed above. The tower and foundation can support the equipment as described in this report.

If you have any questions or require additional information, please contact American Tower via email at Engineering@americantower.com. Please include the American Tower site name, site number, and engineering number in the subject line for any questions.

## Existing and Reserved Equipment

| Elevation ${ }^{1}(\mathrm{ft})$ |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 79.0 | 79.0 | 6 | Commscope JAHH-65B-R3B | Sector Frames | - | Verizon |
|  |  | 3 | Alcatel-Lucent B66A RRH4×45-4R w/o Solar Shield |  |  |  |
|  |  | 3 | Nokia Band 5 AHCA RRH4×40 |  |  |  |
| 71.0 | 71.0 | 2 | Antel BXA-80063-6CF-EDIN-X | Sector Frames | (12) $15 / 8$ " Coax |  |
|  |  | 1 | Antel BXA-80063-4CF-EDIN-X |  |  |  |

## Equipment to be Removed

| Elevation ${ }^{1}$ (ft) |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 70.0 | 70.0 | 1 | RFS DB-B1-6C-12AB-0Z | - | (1) $15 / 8$ " Hybriflex | Verizon |
|  |  | 3 | Alcatel-Lucent RRH2x60 700 |  |  |  |
|  |  | 1 | Antel BXA-70063/6CF |  |  |  |

## Proposed Equipment

| Elevation ${ }^{1}$ (ft) |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 79.0 | 79.0 | 1 | RFS DB-B1-6C-12AB-0Z | Sector Frames | (1) $15 / 8$ " Hybriflex | Verizon |
|  |  | 3 | Alcatel-Lucent RRH2×60 700 |  |  |  |
|  |  | 3 | Alcatel-Lucent B25 RRH4x30 |  |  |  |

${ }^{1}$ Mount elevation is defined as height above bottom of steel structure to the bottom of mount, RAD elevation is defined as center of antenna above ground level (AGL).

Install proposed coax alongside existing Verizon coax.

## Structure Usages

| Structural Component | Controlling Usage | Pass/Fail |
| :---: | :---: | :---: |
|  | $84 \%$ | Pass |
| Diagonals | $94 \%$ | Pass |
| Horizontals | $10 \%$ | Pass |
| Anchor Bolts | $82 \%$ | Pass |
| Leg Bolts | $55 \%$ | Pass |

## Foundations

| Reaction Component | Analysis Reactions |
| :---: | :---: |
| Uplift (Kips) | 55.7 |
| Axial (Kips) | 62.8 |
| Shear (Kips) | 6.5 |

The structure foundation piers are directly embedded into shallow rock and are assumed to be designed to withstand the analysis reactions.

## Deflection, Twist and Sway*

| Antenna Elevation (ft) | Antenna | Carrier | Deflection <br> (ft) | Twist ( ${ }^{\circ}$ ) | Sway (Rotation) ( ${ }^{\circ}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 79.0 | Alcatel-Lucent B25 RRH4x30 | Verizon | 0.122 | 0.002 | 0.172 |
|  | Alcatel-Lucent RRH2×60 700 |  |  |  |  |
|  | RFS DB-B1-6C-12AB-0Z |  |  |  |  |

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## Standard Conditions

All engineering services performed by A.T. Engineering Service, PLLC are prepared on the basis that the information used is current and correct. This information may consist of, but is not limited to the following:

- Information supplied by the client regarding antenna, mounts and feed line loading
- Information from drawings, design and analysis documents, and field notes in the possession of A.T. Engineering Service, PLLC

It is the responsibility of the client to ensure that the information provided to A.T. Engineering Service, PLLC and used in the performance of our engineering services is correct and complete.

All assets of American Tower Corporation, its affiliates and subsidiaries (collectively "American Tower") are inspected at regular intervals. Based upon these inspections and in the absence of information to the contrary, American Tower assumes that all structures were constructed in accordance with the drawings and specifications.

Unless explicitly agreed by both the client and A.T. Engineering Service, PLLC, all services will be performed in accordance with the current revision of ANSI/TIA-222.

All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. A.T. Engineering Service, PLLC is not responsible for the conclusions, opinions and recommendations made by others based on the information supplied herein.


[^1]
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\section*{| Individual Base Foundation Design Loads |  |  |
| :--- | :--- | :---: |
| Vertical (kip) | Uplift (kip) | Horizontal (kip) |
| 62.75 | 55.71 | 6.51 | <br> 62.75 <br> $62.75 \quad 55.71$}



| Site Number: | 283426 | Code: | ANSI/TIA-222-G |
| :--- | :--- | :--- | :--- | © 2007-2018 by ATC IP LLC. All rights reserved.

## Analysis Parameters

| Location: | FAIRFIELD County, CT | Height $(\mathrm{ft}):$ | 80 |
| :--- | :--- | :--- | ---: |
| Code: | ANSI/TIA-222-G | Base Elevation $(\mathrm{ft}):$ | 0.00 |
| Shape: | Triangle | Bottom Face Width $(\mathrm{ft}):$ | 10.58 |
| Tower Manufacturer: |  | Top Face Width $(\mathrm{ft}):$ | 4.50 |
| Tower Type: | Self Support | Anchor Bolt Detail Type | c |

Kd:
Ke:

## Ice \& Wind Parameters

| Structure Class: | II | Design Windspeed Without Ice: | 93 mph |
| :--- | :--- | :--- | :--- |
| Exposure Category: | B | Design Windspeed With Ice: | 50 mph |
| Topographic Category: | 3 | Operational Windspeed: | 60 mph |
| Crest Height: | 116 ft | Design Ice Thickness: | 0.75 in |

## Seismic Parameters

| alysis Method: Equivalent Modal Analysis \& Equivalent Lateral Force Methods |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Class: |  | D - Stiff Soil |  |  |  |
| Period Based on Rayleigh Method (sec): |  | 0.54 |  |  |  |
| $\mathrm{T}_{\mathrm{L}}(\mathrm{sec})$ : | 6 | p: | 1.3 | $\mathrm{C}_{\text {S }}$ : | 0.065 |
| $\mathrm{S}_{\mathrm{s}}$ : | 0.208 | $\mathrm{S}_{1}$ : | 0.066 | Cs, Max: | 0.065 |
| $\mathrm{F}_{\mathrm{a}}$ : | 1.600 | $F_{v}$ : | 2.400 | $\mathrm{C}_{\mathrm{S}}$, Min: | 0.030 |
| $\mathrm{S}_{\mathrm{ds}}$ : | 0.222 | $\mathrm{S}_{\mathrm{d} 1}$ : | 0.106 |  |  |

## Load Cases

| 1.2D + 1.6W Normal | 93 mph Normal to Face with No lce |
| :---: | :---: |
| 1.2D + 1.6W 60 deg | 93 mph 60 degree with No Ice |
| 1.2D + 1.6W 90 deg | 93 mph 90 degree with No lce |
| 1.2D + 1.6W 120 deg | 93 mph 120 degree with No Ice |
| $1.2 \mathrm{D}+1.6 \mathrm{~W} 180 \mathrm{deg}$ | 93 mph 180 degree with No Ice |
| $1.2 \mathrm{D}+1.6 \mathrm{~W} 210 \mathrm{deg}$ | 93 mph 210 degree with No Ice |
| $1.2 \mathrm{D}+1.6 \mathrm{~W} 240 \mathrm{deg}$ | 93 mph 240 degree with No Ice |
| $1.2 \mathrm{D}+1.6 \mathrm{~W} 300 \mathrm{deg}$ | 93 mph 300 degree with No Ice |
| $1.2 \mathrm{D}+1.6 \mathrm{~W} 330 \mathrm{deg}$ | 93 mph 330 degree with No Ice |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ Normal | 93 mph Normal to Face with No Ice (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 60 \mathrm{deg}$ | 93 mph 60 deg with No lce (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 90 \mathrm{deg}$ | 93 mph 90 deg with No Ice (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 120 \mathrm{deg}$ | 93 mph 120 deg with No Ice (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 180 \mathrm{deg}$ | 93 mph 180 deg with No lce (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 210 \mathrm{deg}$ | 93 mph 210 deg with No lce (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 240 \mathrm{deg}$ | 93 mph 240 deg with No lce (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 300 \mathrm{deg}$ | 93 mph 300 deg with No Ice (Reduced DL) |
| $0.9 \mathrm{D}+1.6 \mathrm{~W} 330 \mathrm{deg}$ | 93 mph 330 deg with No Ice (Reduced DL) |
| 1.2D + 1.0Di + 1.0Wi Normal | 50 mph Normal with 0.75 in Radial Ice |

## Analysis Parameters

| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 60 \mathrm{deg}$ | 50 mph 60 deg with 0.75 in Radial Ice |
| :---: | :---: |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 90 \mathrm{deg}$ | 50 mph 90 deg with 0.75 in Radial Ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 120 \mathrm{deg}$ | 50 mph 120 deg with 0.75 in Radial Ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 180 \mathrm{deg}$ | 50 mph 180 deg with 0.75 in Radial Ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 210$ deg | 50 mph 210 deg with 0.75 in Radial ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 240 \mathrm{deg}$ | 50 mph 240 deg with 0.75 in Radial Ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 300 \mathrm{deg}$ | 50 mph 300 deg with 0.75 in Radial Ice |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi} 330 \mathrm{deg}$ | 50 mph 330 deg with 0.75 in Radial lce |
| $(1.2+0.2 S d s) *$ DL + E Normal | Seismic Normal |
| $(1.2+0.2 S d s) * D L+E 60 \mathrm{deg}$ | Seismic 60 deg |
| $(1.2+0.2 S d s) * D L+E 90$ deg | Seismic 90 deg |
| $(1.2+0.2 \mathrm{Sds})^{*} \mathrm{DL}+\mathrm{E} 120 \mathrm{deg}$ | Seismic 120 deg |
| $(1.2+0.2 \mathrm{Sds})^{*} \mathrm{DL}+\mathrm{E} 180 \mathrm{deg}$ | Seismic 180 deg |
| $(1.2+0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E} 210 \mathrm{deg}$ | Seismic 210 deg |
| $(1.2+0.2 S d s) * D L+E 240 \mathrm{deg}$ | Seismic 240 deg |
| $(1.2+0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E} 300 \mathrm{deg}$ | Seismic 300 deg |
| $(1.2+0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E} 330 \mathrm{deg}$ | Seismic 330 deg |
| (0.9-0.2Sds) * DL + E Normal | Seismic (Reduced DL) Normal |
| (0.9-0.2Sds) * DL + E 60 deg | Seismic (Reduced DL) 60 deg |
| (0.9-0.2Sds) * DL + E 90 deg | Seismic (Reduced DL) 90 deg |
| (0.9-0.2Sds) * DL + E 120 deg | Seismic (Reduced DL) 120 deg |
| (0.9-0.2Sds) * DL + E 180 deg | Seismic (Reduced DL) 180 deg |
| (0.9-0.2Sds) * DL + E 210 deg | Seismic (Reduced DL) 210 deg |
| (0.9-0.2Sds) * DL + E 240 deg | Seismic (Reduced DL) 240 deg |
| (0.9-0.2Sds) * DL + E 300 deg | Seismic (Reduced DL) 300 deg |
| (0.9-0.2Sds) * DL + E 330 deg | Seismic (Reduced DL) 330 deg |
| 1.0D + 1.0W Service Normal | Serviceability - 60 mph Wind Normal |
| 1.0D + 1.0W Service 60 deg | Serviceability - 60 mph Wind 60 deg |
| 1.0D + 1.0W Service 90 deg | Serviceability - 60 mph Wind 90 deg |
| 1.0D + 1.0W Service 120 deg | Serviceability - 60 mph Wind 120 deg |
| 1.0D + 1.0W Service 180 deg | Serviceability - 60 mph Wind 180 deg |
| 1.0D + 1.0W Service 210 deg | Serviceability - 60 mph Wind 210 deg |
| 1.0D + 1.0W Service 240 deg | Serviceability - 60 mph Wind 240 deg |
| 1.0D + 1.0W Service 300 deg | Serviceability - 60 mph Wind 300 deg |
| $1.0 \mathrm{D}+1.0 \mathrm{~W}$ Service 330 deg | Serviceability - 60 mph Wind 330 deg |

## Tower Loading

## Discrete Appurtenance Properties $1.2 \mathrm{D}+1.6 \mathrm{~W}$

| Elevation Description (ft) | Qty | Wt. <br> (Ib) | EPA <br> (sf) | Length (ft) | Width (in) | Depth (in) | $\mathrm{K}_{\mathrm{a}}$ | Orient. Factor | Vert. <br> Ecc.(ft) | $\begin{gathered} M_{u} \\ (\mathrm{lb}-\mathrm{ft}) \end{gathered}$ | $\begin{gathered} \mathbf{Q}_{2} \\ (\mathbf{p s f}) \end{gathered}$ | $\begin{gathered} F_{a} \text { (WL) } \\ \text { (Ib) } \end{gathered}$ | $\begin{gathered} P_{a}(\mathrm{DL}) \\ (\mathrm{Ib}) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 79.00 Nokia Band 5 AHCA | 3 | 40 | 1.3 | 1.1 | 12.1 | 6.9 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 53 | 143 |
| 79.00 Alcatel-Lucent B25 | 3 | 53 | 2.1 | 1.8 | 12.0 | 7.2 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 85 | 191 |
| 79.00 Alcatel-Lucent | 3 | 57 | 2.2 | 1.8 | 12.0 | 9.0 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 86 | 204 |
| 79.00 Alcatel-Lucent B66A | 3 | 57 | 2.4 | 2.1 | 11.4 | 6.3 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 96 | 204 |
| 79.00 RFS DB-B1-6C-12AB- | 1 | 21 | 2.5 | 1.6 | 15.7 | 10.3 | 0.90 | 0.67 | 0.0 | 0.0 | 21.90 | 45 | 26 |
| 79.00 Commscope JAHH- | 6 | 61 | 9.1 | 6.0 | 13.8 | 8.2 | 0.90 | 0.77 | 0.0 | 0.0 | 21.90 | 1128 | 436 |
| 79.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 21.90 | 695 | 720 |
| 71.00 Amphenol Antel BXA- | , | 10 | 4.7 | 4.0 | 11.2 | 5.2 | 0.90 | 0.74 | 0.0 | 0.0 | 21.93 | 94 | 12 |
| 71.00 Amphenol Antel BXA- | 2 | 17 | 7.5 | 5.9 | 11.0 | 5.2 | 0.90 | 0.75 | 0.0 | 0.0 | 21.93 | 300 | 41 |
| 71.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 21.93 | 696 | 720 |
| Totals | 26 | 2247 | 158.3 |  |  |  |  |  |  |  |  | 3278 | 2697 |

Discrete Appurtenance Properties $0.9 \mathrm{D}+1.6 \mathrm{~W}$

| Elevation Description (ft) | Qty | Wt. <br> (lb) | EPA <br> (sf) | Length (ft) | Width (in) | Depth (in) | $\mathrm{K}_{\mathrm{a}}$ | Orient. Factor | Vert. <br> Ecc.(ft) | $\underset{(\mathrm{lb}-\mathrm{ft})}{M_{\mathrm{u}}}$ | $\begin{gathered} \mathbf{Q}_{2} \\ (\mathbf{p s f}) \end{gathered}$ | $\begin{gathered} F_{\mathrm{a}}(\mathrm{WL}) \\ (\mathrm{Ib}) \end{gathered}$ | $\begin{gathered} \mathrm{P}_{\mathrm{a}}(\mathrm{DL}) \\ (\mathrm{Ib}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 79.00 Nokia Band 5 AHCA | 3 | 40 | 1.3 | 1.1 | 12.1 | 6.9 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 53 | 107 |
| 79.00 Alcatel-Lucent B25 | 3 | 53 | 2.1 | 1.8 | 12.0 | 7.2 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 85 | 143 |
| 79.00 Alcatel-Lucent | 3 | 57 | 2.2 | 1.8 | 12.0 | 9.0 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 86 | 153 |
| 79.00 Alcatel-Lucent B66A | 3 | 57 | 2.4 | 2.1 | 11.4 | 6.3 | 0.90 | 0.50 | 0.0 | 0.0 | 21.90 | 96 | 153 |
| 79.00 RFS DB-B1-6C-12AB- | 1 | 21 | 2.5 | 1.6 | 15.7 | 10.3 | 0.90 | 0.67 | 0.0 | 0.0 | 21.90 | 45 | 19 |
| 79.00 Commscope JAHH- | 6 | 61 | 9.1 | 6.0 | 13.8 | 8.2 | 0.90 | 0.77 | 0.0 | 0.0 | 21.90 | 1128 | 327 |
| 79.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 21.90 | 695 | 540 |
| 71.00 Amphenol Antel BXA- | 1 | 10 | 4.7 | 4.0 | 11.2 | 5.2 | 0.90 | 0.74 | 0.0 | 0.0 | 21.93 | 94 | 9 |
| 71.00 Amphenol Antel BXA- | 2 | 17 | 7.5 | 5.9 | 11.0 | 5.2 | 0.90 | 0.75 | 0.0 | 0.0 | 21.93 | 300 | 31 |
| 71.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 21.93 | 696 | 540 |
| Totals | 26 | 2247 | 158.3 |  |  |  |  |  |  |  |  | 3278 | 2023 |

## Discrete Appurtenance Properties $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$

| ElevationDescription <br> (ft) | Qty | Ice Wt <br> (lb) | Ice EPA (sf) | Length (ft) | Width (in) | Depth (in) | $\mathrm{K}_{\mathrm{a}}$ | Orient. Factor | Vert. Ecc.(ft) | $\underset{(\mathrm{lb}-\mathrm{ft})}{\mathrm{M}_{\mathrm{u}}}$ | $\begin{gathered} \mathbf{Q}_{2} \\ \text { (psf) } \end{gathered}$ | $\begin{gathered} F_{\mathrm{a}} \text { (WL) } \\ \text { (Ib) } \end{gathered}$ | $\begin{aligned} & \mathrm{P}_{\mathrm{a}}(\mathrm{DL}) \\ & (\mathrm{Ib}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 79.00 Nokia Band 5 AHCA | 3 | 82 | 2.1 | 1.1 | 12.1 | 6.9 | 0.90 | 0.50 | 0.0 | 0.0 | 6.33 | 15 | 269 |
| 79.00 Alcatel-Lucent B25 | 3 | 115 | 3.1 | 1.8 | 12.0 | 7.2 | 0.90 | 0.50 | 0.0 | 0.0 | 6.33 | 23 | 376 |
| 79.00 Alcatel-Lucent | 3 | 126 | 3.2 | 1.8 | 12.0 | 9.0 | 0.90 | 0.50 | 0.0 | 0.0 | 6.33 | 23 | 412 |
| 79.00 Alcatel-Lucent B66A | 3 | 121 | 3.5 | 2.1 | 11.4 | 6.3 | 0.90 | 0.50 | 0.0 | 0.0 | 6.33 | 25 | 398 |
| 79.00 RFS DB-B1-6C-12AB- | . 1 | 103 | 3.6 | 1.6 | 15.7 | 10.3 | 0.90 | 0.67 | 0.0 | 0.0 | 6.33 | 12 | 107 |
| 79.00 Commscope JAHH- | 6 | 267 | 11.9 | 6.0 | 13.8 | 8.2 | 0.90 | 0.77 | 0.0 | 0.0 | 6.33 | 267 | 1673 |
| 79.00 Round Sector Frame | 2 | 675 | 31.3 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 6.33 | 273 | 1470 |
| 71.00 Amphenol Antel BXA- | - 1 | 114 | 6.6 | 4.0 | 11.2 | 5.2 | 0.90 | 0.74 | 0.0 | 0.0 | 6.34 | 24 | 116 |
| 71.00 Amphenol Antel BXA- | 2 | 168 | 10.2 | 5.9 | 11.0 | 5.2 | 0.90 | 0.75 | 0.0 | 0.0 | 6.34 | 74 | 343 |
| 71.00 Round Sector Frame | 2 | 675 | 31.3 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 6.34 | 273 | 1470 |
| Totals | 26 | 6184 | 263.0 |  |  |  |  |  |  |  |  | 1008 | 6633 |

Discrete Appurtenance Properties $1.0 \mathrm{D}+1.0 \mathrm{~W}$ Service

| Elevation Description (ft) | Qty | Wt. <br> (lb) | EPA <br> (sf) | Length (ft) | Width <br> (in) | Depth (in) | $\mathrm{K}_{\mathrm{a}}$ | Orient. <br> Factor | Vert. <br> Ecc.(ft) | $\begin{gathered} M_{u} \\ (\mathrm{lb}-\mathrm{ft}) \end{gathered}$ | $\begin{gathered} \mathbf{Q}_{2} \\ (\mathbf{p s f}) \end{gathered}$ | $\begin{gathered} F_{\mathrm{a}} \text { (WL) } \\ \text { (Ib) } \end{gathered}$ | $\begin{gathered} P_{\mathrm{a}}(\mathrm{DL}) \\ (\mathrm{Ib}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| Site Number: | 283426 |
| :--- | :--- |
| Site Name: | BROOKFIELD CT, CT |
| Customer: | VERIZON WIRELESS |


| Code: | ANSI/TIA-222-G |
| :--- | :--- |
| Engineering Number: | OAA722914_C3_01 |

Tower Loading

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 79.00 Nokia Band 5 AHCA | 3 | 40 | 1.3 | 1.1 | 12.1 | 6.9 | 0.90 | 0.50 | 0.0 | 0.0 | 9.11 | 14 |
| 79.00 Alcatel-Lucent B25 | 3 | 53 | 2.1 | 1.8 | 12.0 | 7.2 | 0.90 | 0.50 | 0.0 | 0.0 | 9.11 | 22 |
| 79.00 Alcatel-Lucent | 3 | 57 | 2.2 | 1.8 | 12.0 | 9.0 | 0.90 | 0.50 | 0.0 | 0.0 | 9.11 | 22 |
| 79.00 Alcatel-Lucent B66A | 3 | 57 | 2.4 | 2.1 | 11.4 | 6.3 | 0.90 | 0.50 | 0.0 | 0.0 | 9.11 | 25 |
| 79.00 RFS DB-B1-6C-12AB- | 1 | 21 | 2.5 | 1.6 | 15.7 | 10.3 | 0.90 | 0.67 | 0.0 | 0.0 | 9.11 | 12 |
| 79.00 Commscope JAHH- | 6 | 61 | 9.1 | 6.0 | 13.8 | 8.2 | 0.90 | 0.77 | 0.0 | 0.0 | 9.11 | 293 |
| 79.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 9.11 | 181 |
| 71.00 Amphenol Antel BXA- | 1 | 10 | 4.7 | 4.0 | 11.2 | 5.2 | 0.90 | 0.74 | 0.0 | 0.0 | 9.13 | 24 |
| 71.00 Amphenol Antel BXA- | 2 | 17 | 7.5 | 5.9 | 11.0 | 5.2 | 0.90 | 0.75 | 0.0 | 0.0 | 9.13 | 78 |
| 71.00 Round Sector Frame | 2 | 300 | 14.4 | 0.0 | 0.0 | 0.0 | 0.90 | 0.90 | 0.0 | 0.0 | 9.13 | 181 |
| Totals | 26 | 2247 | 158.3 |  |  |  |  |  |  |  | 600 |  |
|  |  |  |  |  |  |  |  |  |  | 85 | 2247 |  |


| Site Number: | 283426 | Code: | ANSI/TIA-222-G | © 2007-2018 by ATC IP LLC. All rights reserved. |
| :--- | :--- | :--- | :--- | :--- |
| Site Name: | BROOKFIELD CT, CT | Engineering Number: | OAA722914_C3_01 |  |
| Customer: | VERIZON WIRELESS |  |  |  |

## Tower Loading

## Linear Appurtenance Properties

| Elev From <br> (ft) | $\begin{aligned} & \text { Elev } \\ & \text { To } \\ & \text { (ft) } \\ & \hline \end{aligned}$ | Description | Qty | Width <br> (in) | Weigh ( $\mathrm{lb} / \mathrm{ft}$ ) | Pct In Block | Spread On Faces | Bundling Arrangement | Cluster <br> Dia (in) | Out Of Zone | Spacing (in) | Orientation Factor | Ka Override |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 79.00 | Waveguide | 1 | 2.00 | 6.00 | 0 | Lin App | Individual | 0.00 | N | 1.00 | 1.00 | 0.00 |
| 10.00 | 79.00 | $15 / 8$ " Hybriflex | 1 | 1.98 | 1.30 | 0 | Lin App | Individual | 0.00 | N | 1.00 | 1.00 | 0.00 |
| 10.00 | 71.00 | 15/8" Coax | 12 | 1.98 | 0.82 | 50 | Lin App | Block | 0.00 | N | 0.50 | 1.00 | 0.00 |


| Site Number: | 283426 | Code: | ANSI/TIA-222-G |
| :--- | :--- | :--- | :--- | © 2007-2018 by ATC IP LLC. All rights reserved.

## Equivalent Lateral Force Method

(Based on ASCE7-10 Chapters 11, 12 \& 15)

$\underline{\text { LoadCase }} \underline{(1.2+0.2 S d s) * D L+E} \quad$ Seismic

| - Section | Height <br> Above Base <br> (ft) | Weight <br> (ib) | $\begin{aligned} & W_{z} \\ & (\mathrm{lb}-\mathrm{ft}) \end{aligned}$ | $\mathrm{C}_{\mathrm{vx}}$ | Horizontal Force (lb) | Vertical Force (lb) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 70.00 | 773 | 58,937 | 0.170 | 92 | 962 |
| 3 | 50.00 | 956 | 51,709 | 0.149 | 80 | 1,189 |
| 2 | 30.00 | 1,021 | 32,813 | 0.095 | 51 | 1,271 |
| 1 | 10.00 | 1,357 | 14,213 | 0.041 | 22 | 1,688 |
| Nokia Band 5 AHCA RRH4x40 | 79.00 | 119 | 10,278 | 0.030 | 16 | 148 |
| Alcatel-Lucent B25 RRH4×30 | 79.00 | 159 | 13,721 | 0.040 | 21 | 198 |
| Alcatel-Lucent RRH2x60 700 | 79.00 | 170 | 14,678 | 0.042 | 23 | 212 |
| Alcatel-Lucent B66A RRH4x45-4R w/o | 79.00 | 170 | 14,704 | 0.043 | 23 | 212 |
| RFS DB-B1-6C-12AB-0Z | 79.00 | 21 | 1,847 | 0.005 | 3 | 27 |
| Commscope JAHH-65B-R3B | 79.00 | 364 | 31,376 | 0.091 | 49 | 452 |
| Round Sector Frame | 79.00 | 600 | 51,776 | 0.150 | 81 | 747 |
| Amphenol Antel BXA-80063-4CF-EDIN-X | 71.00 | 10 | 766 | 0.002 | 1 | 12 |
| Amphenol Antel BXA-80063-6CF-EDIN-X | 71.00 | 34 | 2,631 | 0.008 | 4 | 42 |
| Round Sector Frame | 71.00 | 600 | 46,433 | 0.134 | 72 | 747 |
|  |  | 6,354 | 345,882 | 1.000 | 538 | 7,906 |

$\underline{\text { LoadCase (0.9-0.2Sds) * DL + E }}$
Seismic (Reduced DL)

| Section | Height Above Base (ft) | Weight <br> (lb) | $\begin{gathered} \mathbf{W}_{\mathbf{z}} \\ (\mathrm{lb} \mathrm{ft}) \end{gathered}$ | $\mathrm{C}_{\mathrm{vx}}$ | Horizontal Force (lb) | Vertical Force (Ib) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 70.00 | 773 | 58,937 | 0.170 | 92 | 661 |
| 3 | 50.00 | 956 | 51,709 | 0.149 | 80 | 818 |

Site Number: 283426
Site Name: BROOKFIELD CT, CT
Customer: VERIZON WIRELESS

| Equivalent Lateral Force Method |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 30.00 | 1,021 | 32,813 | 0.095 | 51 | 874 |
| 1 | 10.00 | 1,357 | 14,213 | 0.041 | 22 | 1,161 |
| Nokia Band 5 AHCA RRH4x40 | 79.00 | 119 | 10,278 | 0.030 | 16 | 102 |
| Alcatel-Lucent B25 RRH4×30 | 79.00 | 159 | 13,721 | 0.040 | 21 | 136 |
| Alcatel-Lucent RRH2x60 700 | 79.00 | 170 | 14,678 | 0.042 | 23 | 146 |
| Alcatel-Lucent B66A RRH4x45-4R w/o | 79.00 | 170 | 14,704 | 0.043 | 23 | 146 |
| RFS DB-B1-6C-12AB-0Z | 79.00 | 21 | 1,847 | 0.005 | 3 | 18 |
| Commscope JAHH-65B-R3B | 79.00 | 364 | 31,376 | 0.091 | 49 | 311 |
| Round Sector Frame | 79.00 | 600 | 51,776 | 0.150 | 81 | 513 |
| Amphenol Antel BXA-80063-4CF-EDIN-X | 71.00 | 10 | 766 | 0.002 | 1 | 8 |
| Amphenol Antel BXA-80063-6CF-EDIN-X | 71.00 | 34 | 2,631 | 0.008 | 4 | 29 |
| Round Sector Frame | 71.00 | 600 | 46,433 | 0.134 | 72 | 513 |
|  |  | 6,354 | 345,882 | 1.000 | 538 | 5,436 |


| Site Name: | BROOKFIELD CT, CT |
| :--- | :--- |
| Customer: | VERIZON WIRELESS |

## Equivalent Modal Analysis Method

(Based on ASCE7-10 Chapters 11, 12 \& 15 and ANSI/TIA-G, section 2.7)

| Spectral Response Acceleration for Short Period (S $\mathbf{S}_{\mathbf{s}}$ ): | 0.21 |
| :---: | :---: |
| Spectral Response Acceleration at 1.0 Second Period ( $\mathrm{S}_{1}$ ): | 0.07 |
| Importance Factor ( $\mathrm{I}_{\mathrm{e}}$ ): | 1.00 |
| Site Coefficient F a: | 1.60 |
| Site Coefficient F ${ }_{\text {v }}$ : | 2.40 |
| Response Modification Coefficient (R): | 3.00 |
|  | 0.22 |
| Desing Spectral Response Acceleration at 1.0 Second Period (S | d1): 0.11 |
| Period Based on Rayleigh Method (sec): | 0.54 |
| Redundancy Factor (p): | 1.30 |

LoadCase $\underline{(1.2+0.2 S d s) * D L+E} \quad$ Seismic


| Site Number: | 283426 | Code: | ANSI/TIA-222-G | © 2007-2018 by ATC IP LLC. All rights reserved. |
| :--- | :--- | :--- | :--- | ---: |
| Site Name: | BROOKFIELD CT, CT | Engineering Number: | OAA722914_C3_01 |  |
| Customer: | VERIZON WIRELESS |  |  |  |

Equivalent Modal Analysis Method
Site Number: 283426

Code:
Engineering Number: OAA722914_C3_01
Site Name: BROOKFIELD CT, CT
Customer: VERIZON WIRELESS
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ANSI/TIA-222-G
2/8/2018 10:30:39 AM

## Force/Stress Summary

| Section: 1 - | Bot Elev (ft): 0.00 |  |  |  |  | Height (ft): 20.000 |  |  |  |  | Shear Bear <br> Num phiRnvphiRn |  |  | Use |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Max Compression Member | Pu <br> (kip) | Load Case | Len <br> (ft) | Bracing \% |  |  |  | F'y <br> (ksi) | Phic Pn Num (kip) Bolts |  |  |  |  |  |  |
| LEG PXX - 2-1/2" DIA PIP HORIZ | $\begin{array}{r} -60.64 \\ 0.00 \end{array}$ | 1.2D + 1.6W | $\begin{array}{r} 6.68 \\ 0.000 \end{array}$ | 100 0 | $\begin{array}{r} 100 \\ 0 \end{array}$ | $\begin{array}{rr} 0 & 100 \\ 0 & 0 \end{array}$ | $\begin{array}{r} 94.9 \\ 0.0 \end{array}$ | $\begin{array}{r} 50.0 \\ 0.0 \end{array}$ | $\begin{array}{r} 93.81 \\ 0.00 \end{array}$ | 0 0 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.00 \end{aligned}$ | 64 0 | Member X |
| DIAG SAE-1.75X1.75X0.12 | -2.00 | 1.2D + 1.6W 90 | 12.22 | 50 | 50 | ) 50 | 211.4 | 36.0 | 2.12 | 1 | 1 | 7.95 | 6.96 | 94 | Member $Z$ |
| Max Tension Member | Pu <br> (kip) | Load Case | Fy (ksi) | $\underset{(k s i)}{F u}$ |  | hit Pn (kip) | Num Bolts | Num Holes |  |  | Bear phiRn (kip) |  | Shear trn <br> ip) | Use \% | Controls |
| LEG PXX-2-1/2" DIA PIP | 53.46 | 1.2D + 1.6W 60 | 50 | 65 |  | 181.35 | 0 | 0 |  | 0.00 | 0.00 |  |  | 29 | Member |
| HORIZ | 0.00 |  | 0 | 0 | 0 | 0.00 | 0 | 0 |  | 0.00 | 0.00 |  | 0.00 | 0 |  |
| DIAG SAE - 1.75X1.75X0.12 | 1.951 | $1.2 \mathrm{D}+1.6 \mathrm{~W} 90$ | 36 | 58 |  | 11.15 | 1 | 1 |  | 7.95 | 4.13 |  | 3.81 | 51 | Blk Shear |
| Max Splice Forces | $\begin{gathered} \mathrm{Pu} \\ (\mathrm{kip}) \end{gathered}$ | Load Case |  | phiR <br> (kip |  |  |  | Num <br> Bolts | Bolt Ty | pe |  |  |  |  |  |
| Top Tension | 44.50 | 0.9D + 1.6W 180 |  | 0.0 | 00 |  | 0 | 0 |  |  |  |  |  |  |  |
| Top Compression | 50.02 | $21.2 \mathrm{D}+1.6 \mathrm{~W}$ |  | 0.0 | 00 |  | 0 |  |  |  |  |  |  |  |  |
| Bot Tension | 56.06 | 0.9D + 1.6W 180 |  | 81.3 |  | 8 | 32 | 4 | 5/8 A3 |  |  |  |  |  |  |
| Bot Compression | 62.88 | $1.2 \mathrm{D}+1.6 \mathrm{~W} 120$ |  | 0.0 | 00 |  | 0 |  |  |  |  |  |  |  |  |

Section: 2 - Bot Elev (ft): 20.00
Height (ft): 20.000


| Max Splice Forces | Pu <br> (kip) | Load Case | phiRnt <br> (kip) | Use <br> $\%$ | Num <br> Bolts | Bolt Type |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |
| Top Tension | 32.15 | $0.9 \mathrm{D}+1.6 \mathrm{~W} 180$ | 0.00 | 0 | 0 |  |
| Top Compression | 36.15 | $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 0.00 | 0 |  |  |
| Bot Tension | 44.50 | $0.9 \mathrm{D}+1.6 \mathrm{~W} 180$ | 81.36 | 55 | 4 | $5 / 8$ A325 |
| Bot Compression | 50.02 | $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 0.00 | 0 |  |  |

## Force/Stress Summary

Section: 3
Bot Elev (ft): $\mathbf{4 0 . 0 0}$ Height (ft): 20.000

| Max Compression Member | Pu <br> (kip) | Load Case | Len <br> (ft) | Bracing \% |  |  |  | (ksi) | Phic Pn Num (kip) Bolts |  | Shear Bear <br> Num phiRnvphiRn <br> Holes (kip) (kip) |  |  | $\begin{gathered} \text { Use } \\ \% \end{gathered}$ | Controls |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LEG PX-2" DIA PIPE | -34.72 | 1.2D + 1.6W | 4.01 | 100 | 100 | 100 | 62.8 | 50.0 | 49.93 | 0 | 0 | 0.00 | 0.00 | 69 | Member X |
| HORIZ | 0.00 |  | 0.000 | 0 | 0 | 0 | 0.0 | 0.0 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0 |  |
| DIAG SAE - 1.5X1.5X0.1563 | -1.47 | 1.2D + 1.6W 90 | 7.485 | 50 | 50 | 50 | 152.2 | 36.0 | 4.29 | 1 | 1 | 7.95 | 8.70 | 34 | Member $Z$ |
| Max Tension Member | $\begin{aligned} & \text { Pu } \\ & \text { (kip) } \end{aligned}$ | Load Case | $\begin{aligned} & \text { Fy } \\ & \text { (ksi) } \end{aligned}$ | $\underset{(k s i)}{F u}$ |  | hit Pn (kip) | Num Bolts | Num <br> Holes |  |  | Bear phiRn (kip) | BIK ph | hear Pn <br> p) | Use \% | Controls |
| LEG PX-2" DIA PIPE | 30.65 | $1.2 \mathrm{D}+1.6 \mathrm{~W} 60$ | 50 | 65 |  | 66.60 | 0 | 0 |  | 0.00 | 0.00 |  |  | 46 | Member |
| HORIZ | 0.00 |  | 0 | 0 | 0 | 0.00 | 0 | 0 |  | 0.00 | 0.00 |  | 0.00 |  |  |
| DIAG SAE - 1.5X1.5X0.1563 | 1.43 | $1.2 \mathrm{D}+1.6 \mathrm{~W} 90$ | 36 | 58 |  | 11.17 | 1 | 1 |  | 7.95 | 5.17 |  | 3.91 |  | Blk Shear |
| Max Splice Forces | $\begin{gathered} \text { Pu } \\ \text { (kip) } \end{gathered}$ | Load Case |  | phiR <br> (kip |  |  | Jse $\%$ | Num Bolts | Bolt T | ype |  |  |  |  |  |
| Top Tension | 17.98 | 0.9D + 1.6W 18 |  | 0.0 | 00 |  | 0 | 0 |  |  |  |  |  |  |  |
| Top Compression | 20.63 | 1.2D + 1.6W |  | 0.0 | . 00 |  | 0 |  |  |  |  |  |  |  |  |
| Bot Tension | 32.15 | $50.9 \mathrm{D}+1.6 \mathrm{~W} 18$ |  | 81. |  |  | 40 | 4 | 5/8 A3 |  |  |  |  |  |  |
| Bot Compression | 36.15 | 1.2D + 1.6W |  | 0.0 | 00 |  | 0 |  |  |  |  |  |  |  |  |

Section: 4 - Bot Elev (ft): 60.00 Height (ft): 20.000
Shear Bear

| Max Compression Member | Pu (kip) | Load Case | Len <br> (ft) | Bracing \% |  |  |  | $\begin{aligned} & \text { F'y } \\ & \text { (ksi) } \end{aligned}$ | Phic Pn Num |  | Num | phiRnvphiRn |  | Use |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | X | Y | Z | KL/R |  |  |  | Holes | (kip) | (kip) | \% | Controls |
| LEG PST - 2" DIA PIPE | -17.87 | 1.2D + 1.6W | 4.00 | 100 | 100 | 100 | 61.0 | 50.0 | 36.68 | 0 | 0 | 0.00 | 0.00 | 48 | Member X |
| HORIZSAE - 1.5X1.5X0.25 | -0.46 | 1.2D + 1.6W 60 | 4.500 | 100 | 100 | 100 | 184.9 | 36.0 | 4.56 | 1 | 1 | 7.95 | 13.92 | 10 | Member $Z$ |
| DIAG SAE-1.5X1.5X0.1563 | -2.16 | 1.2D + 1.6W 90 | 6.021 | 50 | 50 | 50 | 122.5 | 36.0 | 6.47 | 1 | 1 | 7.95 | 8.70 | 33 | Member $Z$ |


| Max Tension Member | Pu <br> (kip) | Load Case | $\begin{gathered} \text { Fy } \\ \text { (ksi) } \end{gathered}$ | $\begin{gathered} \text { Fu } \\ (\mathbf{k s i}) \end{gathered}$ | Phit Pn <br> (kip) | Num Bolts | Num <br> Holes | Shear phiRnv (kip) | Bear phiRn (kip) | Blk Shear phit Pn (kip) | Use \% | Controls |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LEG PST-2" DIA PIPE | 15.52 | 0.9D + 1.6W 60 | 50 | 65 | 48.15 | 0 | 0 | 0.00 | 0.00 |  | 32 | Member |
| HORIZ SAE - 1.5X1.5X0.25 | 0.51 | 1.2D + 1.6W | 36 | 58 | 17.41 | 1 | 1 | 7.95 | 8.27 | 6.25 |  | Blk Shear |
| DIAG SAE - 1.5X1.5X0.1563 | 2.08 | $1.2 \mathrm{D}+1.6 \mathrm{~W} 90$ | 36 | 58 | 11.17 | 1 | 1 | 7.95 | 5.17 | 3.91 |  | Blk Shear |


| Max Splice Forces | Pu <br> (kip) | Load Case | phiRnt <br> (kip) | Use <br> $\%$ | Num <br> Bolts | Bolt Type |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |
| Top Tension | 0.00 |  | 0.00 | 0 | 0 |  |
| Top Compression | 1.80 | $1.2 \mathrm{D}+1.0 \mathrm{Di}+$ | 0.00 | 0 |  |  |
| Bot Tension | 17.98 | $0.9 \mathrm{D}+1.6 \mathrm{~W} 180$ | 81.36 | 22 | 4 | $5 / 8 \mathrm{~A} 325$ |
| Bot Compression | 20.63 | $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 0.00 | 0 |  |  |

Far Field Approximation
with downtilt variation

(
Enter Main Beam

| Distance from Antenna Structure Base in Horizontal plan | 0.1 | 8.4 | 20.8 | 27.5 | 34.7 | 42.5 | 51.3 | 61.3 | 73.0 | 87.1 | 104.8 | 128.0 | 160.3 | 209.4 | 294.7 | 484.1 | 554.1 | 1298.2 | \#NUM! |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Angle from Main Beam (reference to horizontal plane) | 90 | 80 | 70 | 65 | 60 | 55 | 50 | 45 | 40 | 35 | 30 | 25 | 20 | 15 | 10 | 5 | 4 | 0 | 0 |
| dB down from centerline (referenced to centerline) | 30.3 | 27.3 | 25.7 | 25.7 | 26 | 26 | 26.2 | 25.5 | 23.7 | 20.9 | 18.1 | 21.6 | 16.5 | 14.7 | 13.9 | 3.4 | 2.3 | 0.1 | 0 |
| Reflection Coefficient (1 to 4, 2.56 typical) | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 |
| Power Density ( $\mathrm{mW} / \mathrm{cm}^{\wedge}$ ) | 0.0001 | 0.000 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.000 | 0.0003 | 0.0005 | 0.0002 | 0.0003 | 0.0003 | 0.000 | 0.0009 | 0.0009 | 0.00 | \#NUM! |
| Percent of Occupational Standard | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | \#NUM! |
| Percent of General Population Standard | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 | 0.1 | 0.1 | 0.0 | 0.1 | 0.1 | 0.0 | \#NuM! |

Antenna Type BXA-80063/6CF - CDMA SERVICE
Dipole / Wire/ Yagi Antenna Types

| Location: | BROOKFIELD CT |
| :---: | :---: |
| Site \#: | 2-107 |
| Date: | 11/06/17 |
| Name: | Maria Montrose |
| File Name: | p:rl\|rif_safel2cel0107.x|s |


Instructions:
Instructions:

1) Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to ba saved as.
 4) From manufacturer's plots, or data sheet, input Angle from mainbeam and $d B$ below mainbeam centerline.
2) Enter Reflection coefficient ( 2.56 would be typical, 1 for free space)
3) Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
4) An odd distance may be entered in the rightmost column of the lower table.

Far Field Approximation
with downtilt variation
wnikcon wireless

Enter Main Beam
Distance in feet below：

| $\begin{gathered} \sum_{j}^{j} \\ \sum_{\#}^{\prime} \end{gathered}$ | 0 － | － | $\begin{array}{c\|c} \stackrel{\circ}{\circ} & \sum_{n}^{2} \\ \end{array}$ | $\sum_{\sum}^{\sum}$ <br> $\sum$ | $\left.\begin{aligned} & \sum_{\sum}^{2} \\ & \sum_{\#}^{2} \end{aligned} \right\rvert\,$ <br> $\sum$ | $\begin{aligned} & \sum_{i}^{i} \\ & \sum \\ & \sum \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \stackrel{\circ}{0} \\ \dot{\infty} \end{array}$ | $\bigcirc$－ | $\begin{gathered} \stackrel{\sim}{\omega} \\ \stackrel{+}{-} \end{gathered}$ | $\begin{gathered} \stackrel{\circ}{\circ} \\ \stackrel{\sim}{\mathrm{N}} \end{gathered}$ | $\begin{aligned} & \overline{0} \\ & 0 \\ & 0 \end{aligned}$ | $\bigcirc$ | $\bigcirc$ |
| $\begin{gathered} \stackrel{\rightharpoonup}{\mathbf{o}} \\ \underset{\sim}{\circ} \end{gathered}$ | $\checkmark$ | $\begin{gathered} \circ \\ 0 \\ \hline \end{gathered}$ | $\begin{array}{r} \circ \\ \stackrel{\leftrightarrow}{\sim} \\ \hline \end{array}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | ${ }_{-}^{\circ} \mathrm{O}$ | $\stackrel{\circ}{\circ}$ |
| $\begin{gathered} \stackrel{\sim}{j} \\ \stackrel{y}{j} \end{gathered}$ | n | 0 | $\begin{array}{\|} \stackrel{\leftrightarrow}{\circ} \\ \stackrel{N}{\mathrm{~N}} \end{array}$ | $\begin{aligned} & 0 \\ & 0 . \\ & 0 \\ & 0 \end{aligned}$ | No | － |
| $\begin{aligned} & \infty \\ & \underset{\sim}{0} \\ & \underset{\sim}{2} \end{aligned}$ | 안 | $\begin{array}{r} \stackrel{0}{0} \\ \dot{\sim} \\ \hline \end{array}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\mathrm{C}} \\ & \hline \end{aligned}$ | 0 <br>  <br> 0 | $\bigcirc$ | 응 |
| $\begin{gathered} 0 \\ \infty \\ \stackrel{1}{n} \end{gathered}$ | $\stackrel{\sim}{\sim}$ | $\begin{aligned} & \circ \\ & \vdots \\ & \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{n}{\mathrm{i}} \\ & \hline \end{aligned}$ | O <br> O <br> 1 | $\bigcirc{ }^{\circ} \mathrm{O}$ | $\bigcirc$ |
| $\begin{array}{r} - \\ \stackrel{6}{6} \\ \stackrel{r}{2} \\ \hline \end{array}$ | 은 | $\begin{gathered} 0 \\ \text { in } \\ \hline \end{gathered}$ | $\begin{gathered} \circ \\ \stackrel{\circ}{\mathrm{i}} \\ \hline \end{gathered}$ | $\begin{array}{r}0 \\ \hline 0 \\ 0 \\ 0 \\ \hline\end{array}$ | $\bigcirc$ | $\bigcirc$ |
| $\stackrel{\stackrel{\rightharpoonup}{\dot{m}}}{\stackrel{1}{2}}$ | N | $\begin{gathered} \stackrel{\rightharpoonup}{\mathrm{N}} \\ \stackrel{\rightharpoonup}{\mathrm{o}} \\ \hline \end{gathered}$ | $\begin{gathered} \stackrel{0}{0} \\ \stackrel{N}{\mathrm{~N}} \end{gathered}$ | 0 0 0 0 0 | $\bigcirc$ | $\stackrel{\square}{0}$ |
| $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | 앙 | $\begin{gathered} \stackrel{0}{2} \\ \underset{\sim}{N} \end{gathered}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\mathrm{~N}} \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 . \\ & 0 \\ & \hline \end{aligned}$ | $\bigcirc$ | $\bar{\square}$ |
| $\begin{array}{\|c} \circ \\ \stackrel{\circ}{8} \\ \hline \end{array}$ | $\stackrel{0}{0}$ | $\begin{gathered} \hat{ल} \\ \dot{\sim} \\ \hline \end{gathered}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\mathrm{H}} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{0}{8} \\ & 0 . \end{aligned}$ | $\bigcirc$ | $\bigcirc$ |
| $\stackrel{-}{\hat{\circ}}$ | 안 | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{\sim}{*} \\ & \hline \end{aligned}$ | $\begin{array}{r} \bullet \\ \stackrel{0}{\mathrm{~N}} \\ \hline \end{array}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 . \end{aligned}$ | 을 | $\bigcirc$ |
| $\begin{aligned} & \infty \\ & \\ & \hline \end{aligned}$ | 1 | $\stackrel{\stackrel{\circ}{\circ}}{\stackrel{+}{+}}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \\ & \hline \end{aligned}$ | ： | $\bar{\circ}$ | $\stackrel{\square}{\circ}$ |
| $\begin{gathered} \stackrel{\infty}{i} \\ \hline \end{gathered}$ | in | $\begin{gathered} \stackrel{\sim}{m} \\ \underset{\sim}{3} \\ \hline \end{gathered}$ | $\begin{array}{r} \circ \\ \stackrel{0}{\mathrm{i}} \\ \hline \end{array}$ | $\begin{aligned} & \hline 0 \\ & 0 \\ & 0 \\ & \hline 0 \\ & \hline \end{aligned}$ | 응 | $\stackrel{\square}{0}$ |
| $\begin{aligned} & \dot{9} \\ & \dot{子} \end{aligned}$ | 绍 | $\begin{aligned} & \stackrel{\rightharpoonup}{\overleftarrow{~}} \\ & \underset{N}{4} \\ & \hline \end{aligned}$ | $\begin{gathered} \circ \\ \\ \hline \end{gathered}$ | $\begin{aligned} & \text { O} \\ & 0 \\ & 0 \end{aligned}$ | $\bigcirc$ | $\bigcirc$ |
| $\begin{array}{r} \stackrel{n}{\omega} \\ \stackrel{\mu}{0} \\ \hline \end{array}$ | 8 | $\begin{gathered} \stackrel{\circ}{0} \\ \underset{\sim}{2} \\ \hline \end{gathered}$ | مٌ | $\begin{aligned} & 00 \\ & 0.6 \\ & 0 \\ & 0 \end{aligned}$ | 응 | $\bar{\circ}$ |
| $\hat{N}$ | $\stackrel{\square}{\circ}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\mathrm{N}} \\ \stackrel{N}{6} \\ \hline \end{gathered}$ | $\begin{aligned} & \stackrel{\circ}{\mathrm{j}} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 0 \\ & 0 \end{aligned}$ | 응 | $\bar{\circ}$ |
| $\stackrel{+}{\mathrm{i}}$ | － | $\begin{gathered} \stackrel{0}{0} \\ \stackrel{e}{6} \end{gathered}$ | $\begin{array}{r} 8 \\ \stackrel{\circ}{\mathrm{i}} \\ \hline \end{array}$ | $\begin{aligned} & \hline 8 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | 웅 | $\bigcirc$ |
| へ－ | $\infty$ | $\begin{gathered} \infty \\ \stackrel{\sim}{0} \\ \hline \end{gathered}$ | $$ | 0 <br> 0 <br> 0 <br> 0 | 응 | 응 |
| $\stackrel{\square}{0}$ | － 8 |  | $\begin{gathered} \circ \\ \stackrel{\circ}{\mathrm{c}} \\ \hline \end{gathered}$ | $\begin{array}{r} 8 \\ 0 \\ 0 \\ \hline \end{array}$ | $\bigcirc$ | 응 |
|  |  |  |  |  |  |  | JAHH－65B－R3B

Instructions：
1）Fill in Site Location，Site number，Date，Name of Person Responsible for Date，and enter File Name to ba saved as．
 3）Enter Antenna Height（in feet to bottom of antenna），Antenna Gain（expressed as dBi，add 2.17 to dBdeline．
4）From manufacturer＇s plots，or data sheet，input Angle from mainbea
5）Enter Reflection coefficient（ 2.56 would be typical， 1 for free space）
6）Spreadsheet calculates actual power density，then relates as Occupational or General Population percentage of FCC Standard．
7）An odd distance may be entered in the rightmost column of the lower table．
Estimated Radiated Emission

Dipole／Wire／Yagi Antenna Types

| Location： | BROOKFIELD CT |
| :--- | :--- |
| Site \＃： | $2-107$ |
| Date： | $11 / 06 / 17$ |
| Name： | Maria Montrose |
| File Name： | p：Irllif＿safel2cel0107．xls |



## Antenna Type

Far Field Approximation
Estimated Radiated Emission
Single Emitter Far Field Model Dipole / Wire/ Yagi Antenna Types

| Location: | BROOKFIELD CT |
| :--- | :--- |
| Site \#: | $2-107$ |
| Date: | $11 / 06 / 17$ |
| Name: | Maria Montrose |
| File Name: | p:lrnft satel2cel0107.xls |





4) From manufacturer's plots, or data sheet, input Angle from mainbeam and dB below mainbeam centerline.
6) Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
Estimated Radiated Emission
Dipole / Wire/ Yagi Antenna Types

| Location: | BROOKFIELD CT |
| :--- | :--- |
| Site \#: | $2-107$ |
| Date: | $11 / 06 / 17$ |
| Name: | Maria Montrose |
| File Name: | p:Irlirf_safel2cel0107.xls |
|  |  |
| Operating Freq. (MHz | $\mathbf{2 1 4 5 . 0}$ |
| Antenna Height (tt): | $\mathbf{7 9 . 0}$ |
| Antenna Gain (dBi): | $\mathbf{1 8 . 4}$ |
| Antenna Size (in.): | $\mathbf{7 2 . 0}$ |
| Downtilt (degrees): | $\mathbf{5 . 0}$ |
| Feedline Loss (dB): | $\mathbf{0 . 5}$ |
| Power @ J4 (w): | $\mathbf{1 8 0 . 0}$ |
|  |  |


| Distance from Antenna Structure Base in Horizontal plan |
| :--- |
| Angle from Main Beam (reference to horizontal plane) |
| dB down from centerline (referenced to centerline) |
| Reflection Coefficient (1 to 4, 2.56 typical) |
| Power Density ( $\mathrm{mW} / \mathrm{cm}^{\wedge} 2$ 2) |
| Percent of Occupational Standard |
| Percent of General Population Standard |

[^2]Instructions:

1) Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to ba saved as.
 3) Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dBi, add 2.17 to dBd to ob
2) From manufacturer's plots, or data sheet, input Angle from mainbeam and dB below mainbeam centerline.
3) Enter Reflection coefficient ( 2.56 would be typical, 1 for free space)
4) Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.

Estimated Radiated Emission Single Emitter Far Field Model

Dipole / Wire/ Yagi Antenna Types



Cumulative All Antennas
Instructions:
Instructions:

1) Fill in Site Location, Site number, Date, Name of Person Responsible for Date, and enter File Name to ba saved as.
2) References to J4 refer to a poim where the transmission line exits the equipment sheter and proceeds to the antenna(s).
3) Enter Antenna Height (in feet to bottom of antenna), Antenna Gain (expressed as dBi, add 2.17 to $d B d$ to ob
4) Enter Reflection coefficient (2.56 would be typical, 1 for free space)
5) Spreadsheet calculates actual power density, then relates as Occupal
6) Spreadsheet calculates actual power density, then relates as Occupational or General Population percentage of FCC Standard.
7) An odd distance may be emtered in the rightmost column of the lower table.




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BXA-80063/6CF (CDMA)
JAHH-65B-A3B-4DT(700)
JAHH-65B-R3B-4DT(550)
JAHH-65B-R3B-5DT(AWS)
JAHH-65B-R3B-50T(PCS)


## Property Information

| Property Location | 37 CARMEN HILL RD |
| :--- | :--- |
| Owner | AMERICAN TOWERS LLC |
| Co-Owner | C/O PROPERTY TAX DEPT |
| Mailing Address | PO BOX 723597 |
|  | ATLANTA $\quad$ GA 31139 |
| Land Use | $435 \quad$ Cell Site Vac Lnd |
| Land Class | I |
| Zoning Code | R100 |
| Census Tract | 205100010600 |


| Neighborhood |  |
| :--- | :--- |
| Acreage | 4 |
| Utilities |  |
| Lot Setting/Desc | Level |
| Town Clerk Map \# 1 |  |
| Town Clerk Map \# 2 |  |
|  |  |

Photo

## Sketch <br> Sketch



Valuation Summary (Assessed value $=70 \%$ of Appraised Value)

| Item | Appraised | Assessed |
| :--- | :--- | :--- |
| Buildings | 0 | 0 |
| Extras | 0 | 0 |
| Improvements | 16030 | 11220 |
| Outbuildings | 16030 | 11220 |
| Land | 490010 | 343010 |
| Total | 506040 | 354230 |

## Sub Areas

| Subarea Type | Gross Area (sq ft) | Living Area (sq ft) |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  | 0 |
| Total Area |  |  |

Outbuilding and Extra Items

| Type | Description |
| :--- | :--- |
| Comm Shed | 240.00 S.F. |
| Guyed Tower | 80.00 L.F. |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |

## Sales History

| Owner of Record | Book/ Page | Sale Date |  |
| :--- | :---: | :---: | :---: |
| CHARTER COMMUNICATIONS ENTERTAINMENT 1LP | $313 / 836$ | $11 / 1 / 1996$ |  |
| FLORIDA TOWER PARTNERS LLC | $683 / 643$ | $4 / 10 / 2014$ | 508 |
| AMERICAN TOWERS LLC | $692 / 597$ | $11 / 20 / 2014$ | 352340 |

Town of Brookfield, Connecticut - Assessment Parcel Map
Parcel: B05010
Address: 37 CARMEN HILL RD



GENERAL CONSTRUCTION NOTES

2. CONTRACTOR SHALL CONTACT LOCAL 811 FOR IDENTFICATION OF UNDERGROUND UTLITIES
PRIOR TO START OF CONSTRUCTION.
3. Contractor shall be responsille for coordinating all required inspections.
 IMPROVEMENTS SHALL BE EVER
REPORTED TO THE ENGINER.
5. DO Not Change size or spacing of structural elements.
6. Detalls shown are typical: simlar detalls Apply to similar conditons unless
otherwise noted.
7. THESE DRAWING DO NOT INCLUDE NECESSARY COMPONENTS FOR CONSTRUCTION SAFETY
 BoLTS, ETC.
9. CONTRACTOR SHALL DETERMNE EXACT LOCATION OF EXISTING UTLITTES, GROUNDS DRAINS,
DRAIN PPIPSS,
 MAMEDAL OR CORRECTINE ACTIIN. ANY SUCH REMEDALALACTION SHALL REQUIRE WRITTEN
APPROVAL BY THE VERIZON WRELESS REP PRIOR TO PROCEEDNG.
11. EACH CONTRACTOR SHALL COOPREATE WTH THE VERIZON WRRLESS REP, AND COORDINATE

13. ALL CABLEICONDUUT ENTRYYEXIT PORTS SHALL BE WEATHERPROOFED DURING INSTALLATION
USING A SLLIONE SEALANT.
14. WHEERE EXIITTING CONDITIONS DO NOT MATCH THOES SHOWN IN THIS PLAN SET, CONTRACTOR SHALL NOTIFY THE VERIZON WRELESS REP IMMEDIATELY.
15. CONTRACTOR SHALL ENSURE ALL SUBCONTRACTORS ARE PROVIDED WITH A COMPLETE AND
16. Contractor shall remove all rubbish and debris from the site at the end of each
17. CONTRACTOR SHALL COORDINATE WORK SCHEDULE WTH LANDLORD AND TAKE PRECAUTIONS
TO MINIIZ IMPACT AND DISRUPTION OF OTHER OCCUPANTS OF THE FACLITT.
18. CONTRACTOR SHALL UURNISH VERZZON WIRELESS WITH A PDF MARKED UP AS-BULLT SET OF
19. PRIO TO SUBMISIIN OA BID, CONTRACTRR SHALL LOORDINATE WTTH VERRZN MRELESS REP TO DETERM INE WHAT, IF ANY, ITEMS WILL BE PROVIDED. ALITEMS NOT TROVIDED SHALL
PROVDOE AD INSTALLED BY THE CONTRACTOR. CONTRACTOR WLL INSTAL ALL ITEMS
PROVIDED


21. CONTRACTOR SHALL INSTALL ALL SITE
SPECIFICATONS AND REQUIREMENTS.
22. CONTRACTOR SHALL SUBMIT ALL SHOP DRAWINGS TO VERZON MRLLESS FOR REVIEW AND
APPROVAL PRIOR TO FABRICATION.
 PLANS.
 CoNTRACOR SHAL BE SOLELY RESPONSIBLE F FR ALL THE CONSTRUCTION MEANS. METHODS,
TECHN OUESS SEUUECEE ANO PROCEDURES ANO FOR COORDNATING ALL PORTIONS OF THE
WORK UNOR THE CONTRACT.
25. CONTRACTOR SHAL NOTEY


26. COntracto

 AND FIRE REEVEN
BARRIERS, ETC.

THE CONTRACTOR SHALL PROTECT AT HIS OWN EXPENSE, ALL EXISTING FACIITIES AND SUCH


28. ALL WORK SHALL BE INTALLED INA AIRST CLASS, NEAA AND WORKMANLIE MANNER B


29. IN ORDER TO ESTABLISH STANDARDS OF QUALIT AND PERFORMANCE ALL TTPES OF MATERIALS LSTTED HEREINAF TER BY MANUFACTURER'S NAMES ANDOR MANUFACTURE
CATALOG NUMBER SHALL BE PROVIDED BY THESE MANUFACTURERS AS SPECIFIED.

STRUCTURAL STEEL NOTES:

1. STRUCTURAL STEEL SHALL CONFORM TO THE LATEST EDTION OF THE AISC "SPELIIICATION
2. STRUCTURAL STEEL ROLLED SHAPES, PLATES AND BARS SHALL CONFORM TO THE FOLLOWING
A. ASTM A.572, GRADE 50 - ALL W SHAPES, UNLESS NOTED OR A992 OTHERWISE
B. ASTM A-36 - all other rolled shapes, plates and bars unless noted otherwise.
C. ASTM A-500, GRADE B-HSS SECTION (SQUARE, RECTANGULAR, AND ROUND)
D. ASTM A.325, TYPE SC OR N- ALL BOLTS FOR CONNECTING STRUCTURAL MEMBERS
E. ASTM F-155407-ALL ANCHOR BOLTS, UNLESS NOTED OTHERWISE
3. ALL EXPOSED STRUCTURAL STEEL MEMBERS SHALL BE HOT-DIPPED GALVANIED AFTER FABRICATION PER ASTM A123. EXPOSED
GALIANIZD PER ASTM A153 OR B695.
4. ALL FIELD CUT SURFACES, FIELD DRILLED HOLES AND GROUND SURFACES WHERE EXISTING


5. CONNECTIONS:
A. ALL WELDING TO BE PERFORMED BY AWS CERTFIED WELDERS AND CONDUCTED IN
ACCORDANCE WTH THE LATEST EDTIN OF THE AWS WELDNG CODE D1.1.

C. INSPECTION SHALL BE PERFORMED BY AN AWS CERTIFIED WELD INSPECTOR.
D. IT IS THE CONTRACTORS RESPONSIBUITY TO PROVIDE BURNNGMELING PERMITS AS

E. ALL ELECTRODES TO BE LOW HYOROGEN, MATCHING FILLER METAL, PER AWS D1.1
F. MINIMUM WELD SIZE TO BE 0.1875 INCH FILLET WELDS, UNLESS NOTED OTHERWISE,
G. PRIOR TOO FILLD WELIING GALVANIING MATERIAL. CONTRACTOR SHALL GRIND OFF GALVANIING $1 /$ BEYOND ALL FIELD WELD SURFACES. AFTTR WELD AND WELD
INSPECTION IS COMPLETE, REPAR ALL GROUND AND WELDED SURFACES WTH ZR



Feb 132018 12:52 AM cosign


GENERAL NOTES

| Shlef Numere | Rensown |
| :---: | :---: |
| $\mathrm{G}-002$ | 0 |









[^0]:    *Deflection, Twist and Sway was evaluated considering a design wind speed of 60 mph (3-Second Gust) per ANSI/TIA-222-G

[^1]:    93 mph no ice
    50 mph w/ $/ 3 / 4^{\prime \prime}$ radial ice
    Loads: $\begin{aligned} & 93 \mathrm{mph} \text { no ice } \\ & 50 \mathrm{mph} \text { w/ } 3 / 4^{\prime \prime} \text { ra }\end{aligned}$

[^2]:    Antenna Type JAHH-65B-R3B

