56 Prospect Street,
P.O. Box 270

Hartford, CT 06103

Kathleen M. Shanley Manager - Transmission Siting Tel: (860) 728-4527

March 3, 2022

Melanie A. Bachman<br>Executive Director<br>Connecticut Siting Council<br>10 Franklin Square<br>New Britain, CT 06051

## RE: Notice of Exempt Modification <br> Eversource Site \# 6581 <br> 790 Willis Street, Bristol, CT 06010 <br> Latitude: 41-38-56 N / Longitude: 72-56-50 W

Dear Ms. Bachman:

The Connecticut Light and Power Company doing business as Eversource Energy ("Eversource") currently maintains multiple antennas and microwave dishes at various mounting heights on an existing 130-foot self-support tower located at 790 Willis Street in Bristol. See Attachment A, Parcel Map and Property Card. The tower and property are owned by Eversource. Eversource is seeking the Connecticut Siting Council's authorization for the installation of one 20-foot dipole antenna to be mounted at 130 feet above ground level ("AGL") on a heavy-duty mounting kit, and the removal of one 24 -foot $31 / 2$-inch omni directional antenna and associated mount at 130 feet. There will be no changes to the area of the fenced compound, the tower or other existing antennas and equipment mounted on the tower. The tower and existing and proposed equipment on the tower are depicted on Attachment B, Construction Drawings, dated January 19, 2022 and Attachment C, Structural Analysis, dated January 13, 2022. The Connecticut Siting Council approved the self-support tower at this location in Petition No. 800 in January 2007.

The modification is required to eliminate transmitter induced noise issues from two antennas previously installed as part of Eversource's program to update its obsolete analog voice radio communications system to a modern digital voice communications system (refer to EM-EVER-017200423, dated May 11, 2020). The transmitter issue manifests as passive intermodulation, or PIM, noise located on the receive frequencies, which limits the system level coverage capability of the site.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies ("R.C.S.A.") §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this notice is being delivered to Jeffrey Caggiano, Mayor for the City of Bristol and Robert M. Flanagan, AICP, City Planner for the City of Bristol via the United States Postal Service or private carrier. Proof of delivery is attached. See Attachment D, Proof of Delivery of Notice.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2):

1. There will be no change to the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard as shown in the attached Radio Frequency Emissions Report, dated February 7, 2022 (Attachment E - Power Density Report) ${ }^{1}$.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Eversource respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § $16-50 j-72(b)(2)$. One original and two copies of this notice are enclosed.

Communications regarding this Notice of Exempt Modification should be directed to Kathleen Shanley at (860) 728-4527.

By :

cc: Honorable Jeffrey Caggiano, Mayor, City of Bristol
Robert M. Flanagan, AICP, City Planner, City of Bristol
Attachments
A. Parcel Map and Property Card
B. Construction Drawings
C. Structural Analysis
D. Proof of Delivery of Notice
E. Power Density Report

[^0]ATTACHMENT A - PARCEL MAP AND PROPERTY CARD


City of Bristol, Connecticut Assessment Parcel Map
Parcel: 0034800
Account \#: 0034800
Address: 790 WILLIS ST

## 790 WILLIS ST

| Location | 790 WILLIS ST | Mblu | $06 / / 8 \mathrm{~A} / /$ |
| ---: | :--- | ---: | :--- |
| Acct\# | 0034800 | Owner | CONN LIGHT + POWER CO |
| Assessment $\$ 449,190$ | Appraisal | $\$ 641,700$ |  |
| PID 5681 | Building Count | 1 |  |

## Current Value

| Appraisal |  |  |  |
| :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land | Total |
| 2017 | \$392,100 | \$249,600 | \$641,700 |
| Assessment |  |  |  |
| Valuation Year | Improvements | Land | Total |
| 2017 | \$274,470 | \$174,720 | \$449,190 |

## Owner of Record

Owner CONN LIGHT + POWER CO Sale Price \$0

## Co-Owner

Address 107 SELDEN ST
BERLIN, CT 06037

Sale Price $\quad \$ 0$
Certificate 1
Book \& Page 0277/0293
Sale Date 01/25/1952

## Ownership History

| Ownership History |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Owner | Sale Price | Certificate | Book \& Page | Sale Date |  |
| CONN LIGHT + POWER CO | $\$ 0$ | 1 | $0277 / 0293$ | $01 / 25 / 1952$ |  |

## Building Information

## Building 1 : Section 1

| Year Built: | 1950 |
| :--- | :--- |
| Living Area: | 900 |
| Replacement Cost: | $\$ 40,248$ |
| Building Percent 65 <br> Good:  <br> Replacement Cost     <br> Less Depreciation: $\$ 26,200$    <br> Building Attributes     <br> Field    Description  |  |


| STYLE | Warehouse |
| :---: | :---: |
| MODEL | Ind/Comm |
| Stories: | 1 |
| Occupancy | 1.00 |
| Exterior Wall 1 | Concr/Cinder |
| Exterior Wall 2 |  |
| Roof Structure | Gable |
| Roof Cover | Asphalt Shingl |
| Interior Wall 1 | Minim/Masonry |
| Interior Wall 2 |  |
| Interior Floor 1 | Concr-Finished |
| Interior Floor 2 |  |
| Heating Fuel | Electric |
| Heating Type | Hot Air-no Duc |
| AC Type | Unit/AC |
| Struct Class |  |
| Bldg Use | Public Utility |
| Bedrooms |  |
| Full Baths |  |
| Half Baths |  |
| Usrfid 218 |  |
| Usrfld 219 |  |
| 1st Floor Use: |  |
| Heat/AC | Heat/AC Pkgs |
| Frame Type | Masonry |
| Baths/Plumbing | Light |
| Ceiling/Wall | None |
| Rooms/Prtns | Light |
| Wall Height | 8.00 |
| \% Comn Wall |  |

Building Photo

(http://images.vgsi.com/photos2/BristolCTPhotos//\00\05\61\14
Building Layout

(http://images.vgsi.com/photos2/BristolCTPhotos//Sketches/568

| Building Sub-Areas (sq ft) |  |  | Legend |
| :--- | :--- | ---: | ---: |
| Code | Description | Gross <br> Area | Living <br> Area |
| BAS | First Floor | 900 | 900 |
| SLB | Slab | 900 | 0 |
|  |  | 1,800 | 900 |

## Extra Features

| Extra Features | Legend |  |
| :--- | :--- | :--- |
|  | No Data for Extra Features |  |

## Land

| Description | Public Utility | Frontage | 300 |
| :--- | :--- | :--- | :--- |
| Zone | R-25 | Depth |  |
| Neighborhood | 50 | Assessed Value | $\$ 174,720$ |
| Alt Land Appr | No | Appraised Value | $\$ 249,600$ |
| Category |  |  |  |

## Outbuildings

| Outbuildings |  |  |  |  |  | Legend |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code | Description | Sub Code | Sub Description | Size | Value | Bldg \# |
| CELL | Cell Tower/Site |  |  | 2.00 UNITS | \$210,000 | 1 |
| CB3 | PreCastConcCel |  |  | 300.00 S.F. | \$54,000 | 1 |
| CB3 | PreCastConcCel |  |  | 300.00 S.F. | \$54,000 | 1 |
| FCP | Carport |  |  | 900.00 S.F. | \$5,600 | 1 |
| GAR1 | Garage | FR | Frame | 420.00 S.F. | \$6,300 | 1 |
| CB3 | PreCastConcCel |  |  | 200.00 S.F. | \$36,000 | 1 |

## Valuation History

| Appraisal |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| Valuation Year | Improvements | Land |  |  |  |  |  |  |
| 19 |  | $\$ 392,100$ | $\$ 249,600$ |  |  |  |  |  |
| 2018 |  | $\$ 392,100$ | $\$ 249,600$ |  |  |  |  |  |
| 2017 |  | $\$ 392,100$ | $\$ 641,700$ |  |  |  |  |  |


| Assessment |  |  |  |  |  |
| :--- | :--- | ---: | ---: | ---: | :---: |
|  | Valuation Year | Improvements |  |  |  |
| 19 |  | $\$ 274,470$ | Land | Total |  |
| 2018 |  | $\$ 274,470$ | $\$ 174,720$ | $\$ 449,190$ |  |
| 2017 |  | $\$ 274,470$ | $\$ 174,720$ | $\$ 449,190$ |  |

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ATTACHMENT B - CONSTRUCTION DRAWINGS

## EVERS $=$ URCE <br> ENERGY







$\frac{\text { ANTENNA CABLE GROUNDING }}{\text { No SCALE }}$


NOTES
Do not install cabie ground kit at a bend and alwars otrect ground
wir doonn to crouno bar.

3. Meater proong shal be tre And part number as suppleo or

CONNECTION OF CABLE GROUND $\frac{\text { KIT TO ANTENNA CABLE }}{\text { No SCALE }}$


CABLE INSTALLATION WITH WALL $\frac{\text { FEED THRU ASSEMBLY }}{\text { No Scale }}$


F
BLACK \& VEATCH



SOUTH MTN RADIO 790 WILLIS ST
BRISTOL, CT 06010

SHEET TTLE
GROUNDING DETAILS -

## DESIGN BASIS

GOVEENNG CODE: 2018 CONNECTICUT STATE BuLIING CODE (2015 BBC BaSIS)
GENERAL CONDITIONS

2. THE ENINER IS NOT: A GURANTOR OF THE NSTALING CONTRACTOR'S WORK, RESPONSIBLE FOR

 IMNEDAAELY TO THE CONSTRUCTION MANAOCR
5. detalls Incluoed in this plan set are trical and aplly to smmar conomions.


8. THE Contractor sthal safeguro Agans dereang a fre hazaro, affecting tenant Egress
9. THE Contractor shall Remove All degri and contruction wate frou the sit each dar.
10. THE CONTRACTOR'S HOURS OF Work shall be in accordance wit local cooes and


THERMAL \& MOISTURE PROTECTION


 SHAL EE APPLED ON ACCOROANCE WTH MANUFACP
3. FRRETTOPRNG SHALL BE APPLED AS SOON AS PRACTCABLE ATER PENetrations ARE MADE AND

5. ANY BULING ROOF FENETRATION AND/OR RESTORATON SHALL BE PERFROMED SO THAT THE ROOF


6. ALLL Penetrations into ano/or through buliong exterior walls shall. be sealeo with

8. contractor to remove and re--Install all fire proofing as reaured during

SUBMITTALS
Contractor to submt shop dramngs to enginer for revew prior to fabrcation.
2. Contractor to notify enineer for inspection pror to closing penetrations.
3. Contractors shal verir all omension and conomions in the fill prior to farrcaton
 Prooucts.


## STEE




2. DAMAGED GAMVMIED SURFACES SHAL BE CIEANED WTH A WRE ERUSH AND PANTED WTH TWO
 SAME PANT IN SHOP OR FELD.
3. Desicn fabracaton and erecion of structural steel shall conform to the aisc "Manual

5. All steel elements shall be nstalleo plumb and level.
5. All ster maracterers desions sum prame ano level

## SITE GENERAL

CONTractor s.anl foliow conotions of all applicable permits and work in accoroance





 LIMTED TO. APPROPRATE A AAL PR

5. ALL ExSTMG NACTVE SEEER, WAIER, GAS, ELECRIC, FBER OPTC, OR OTHER UTLTIES, WHICH

6. Coniractor is fessonsile for repaling or replacing structures or utlumes damaged




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SOUTH MTN RADIO 790 WILLIS ST

NOTES
\& SPECIFICATIONS
N-1

## ELECTRICAL



AUHORTIES SHALL APPL.


4. ALL ELECTRRCAL Conouctors Shall be 100\% COPPER AND SHALL HAVE TPE THHN INSULATON

6. ALL BURIED ConDut SHALL BE MNMMM SCH 40 PVC UNLESS NOTED OTHERWSE, OR AS PER


9. Conout ano cable witin corrdors shall be concealed and exposed elisewhere, uniess


11. Wirng deyices shal be specificaion grade, ano wring device cover plates shall be


14. THE CONTRACTOR SHALL RE REOURED To USTT THE STE PROR To Subumting bio in order to

Contractor is responsible for all conirol wrng and alarm tie-

## GROUNDIN

\#. then shall be stranoed \#6 copper with green thwn insuation sutable for wet
2. \#2 thwn shall be strandeo \#t copper with thwn nsulaton sutable for wei
 BETS SERES 548




7. THE MNMUM gend ralus shall be 8 Inches for \#6 Wre Ano smaller and 12 INChes for


10. FERrous METAL cllps which completely surrouno the grounong conouctor shall be


NTENNA \& CABLE NOTES




3. antenna cables shall be color cooed at the followng locations:

AT THE ANEEGGDE ENTTY PPATE ON BOTH SIDES OF THE EQUPMENT SHELIER WALL.



5. MNMUM BENOING RADUS For COAXALL CABLES:
$7 / 8 \mathrm{INCH}, \mathrm{RMN}=15$ NCHES
$15 / 8 \mathrm{NCH}, \mathrm{M}$ NIN $=25$
 AlL CABLE CONNECTONS OUTSIDE SHALL BE COVERED WTH WATERPROOF SPLLING kII
. Contractor shall verry exact length and directon of travel in fiel prior to
Cige shall be furnished without spluces and with connectops at each eil

107 SELDEN STRET
BERLNCT 0 O637
PHONE: ( 800 ) $286-2000$

SOUTH MTN RADIO BRISTOL, CT 06010

SHEET TTILE
NOTES
\& SPECIFICATIONS

N-2


## REFERENCE CUTSHEETS

## BASE STATION ANTENNAS

870 SERIES DUAL EXPOSED DIPOLE

## 876F-70-2HSMP40DF1/ 2

The 876F-70-2HSMP40DF1/2 Dual Exposed Dipole is well suited for multicoupled RF system. It has an extremely rugged design for use in severe environmental conditions. It has internal cabling and a fix dipole-to-mast spacing. This antenna is a special version of the $876 \mathrm{~F}-70$ with increased spacing between the two antennas, giving an isolation of 40 dB . It's heavy duty and Low PIM deign. This antenna can be black anodized, please contact technical support for more information.

The $1 / 2$ wave pattern spacing version offer bidirectional pattern with more than 5 dBd Gain at 220 MHz .

| Electrical Specifications | 876 F-70-2HSMP40DF1/2 |
| :--- | :---: |
| Frequency Range, MHz | $215-225$ |
| Nominal Gain, dBd | $5.0(5.2$ @ 220MHz) |
| Isolation, dB | 40 |
| Bandwidth 1.5:1 VSWR, MHz | $1.5: 1$ (10) |
| Polarization | Vertical |
| Pattern | Bidirectional |
| Power Rating, Watts | 300 |
| PIM. (2x20W, 3rd ord.), dBc | 150 |
| Nominal Impedance, Ohms | 50 |
| Lightning Protection | DC Ground |
| Termination | Dual Feeds Terminating in 7/16 DIN F |
| Mechanical Speciffcations | 876 F-70-H1DWSM-40 |
| Length, in (mm) | $240(6096)$ |
| Width (1/2 Wave Spacing), in (mm) | 43 (1092) |
| Weight, Ibs. (kg) | $130(59)$ |
| Rated Wind Velocity, No Ice, mph (km/h) | $140(225)$ |
| Rated Wind Velocity, 1/2" ice, mph (km/h) | $105(169)$ |
| Lateral Thrust @ 100 mph, wind, lbs. (N) | $222(988)$ |
| Torsional Moment (N•M) | $471(638)$ |
| Projected Area, ft² (m²) | $8.5(0.78)$ |
| Mounting Information Mast O.D. (mm) | $2.9(74)$ |

[^1]876F-70-2HSMP40DF1/ 2


876F-70-2HSMP40DF1/2: Horizontal Radiation pattern


876F-70-2HSMP40DF1/2: Vertical Radiation pattern

## VHF Omni Antennas (160-222 MHz)

| Model Number |  | 160-174 MHz |  |  |  |  |  | 217-222 MHz |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 0 $\vdots$ $\vdots$ 0 0 0 0 0 0 0 |  | $\begin{aligned} & \text { Q } \\ & \text { !े } \\ & \text { M } \\ & \text { M } \\ & \text { O} \\ & \text { N } \\ & \text { N } \end{aligned}$ |  | $\begin{aligned} & \text { Q } \\ & \text { !े } \\ & \text { O} \\ & \text { H } \\ & 0 \\ & \text { U } \\ & \text { N } \end{aligned}$ | $z$ <br> 1 <br> 0 <br> 0 <br> 1 <br> 0 <br>  <br> 0 <br> 0 <br> 0 | $\begin{aligned} & \text { Q } \\ & \text { ì } \\ & \text { N} \\ & \text { O} \\ & \text { U } \\ & \text { N } \end{aligned}$ |  |  |
|  | Input Connector | N(F) | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | $\mathrm{N}(\mathrm{F})$ | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | N(F) | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | $N(F)$ | $\begin{array}{\|l\|l\|} \hline \text { 7/16 } \\ \text { DIN } \end{array}$ | $N(F)$ | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | $\mathrm{N}(\mathrm{F})$ | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | $\mathrm{N}(\mathrm{F})$ | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ | N(F) | $\begin{aligned} & 7 / 16 \\ & \text { DIN } \end{aligned}$ |
|  | Type | Single |  | Single |  | Dual |  | Single |  | Single |  | Single |  | Dual |  | Dual |  |
|  | Bandwidth, MHz | 14 |  | 14 |  | 14 |  | 5 |  | 5 |  | 5 |  | 5 |  | 5 |  |
|  | Power, Watts | 500 |  | 500 |  | 350 |  | 500 |  | 500 |  | 500 |  | 350 |  | 350 |  |
|  | Gain, dBd | 3 |  | 6 |  | 3 |  | 0 |  | 3 |  | 6 |  | 0 |  | 3 |  |
|  | Horizontal Beamwidth, degrees | 360 |  | 360 |  | 360 |  | 360 |  | 360 |  | 360 |  | 360 |  | 360 |  |
|  | Vertical Beamwidth, degrees | 30 |  | 16 |  | 30 |  | 60 |  | 30 |  | 16 |  | 60 |  | 30 |  |
|  | Beam Tilt, degrees | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
|  | Isolation (minimum) , dB | N/A |  | N/A |  | 30 |  | N/A |  | N/A |  | N/A |  | 30 |  | 30 |  |
| $\begin{aligned} & \frac{1}{\mathbf{d}} \\ & \frac{0}{2} \\ & \frac{1}{3} \\ & \frac{11}{2} \end{aligned}$ | Number of Connectors | 1 |  | 1 |  | 2 |  | 1 |  | 1 |  | 1 |  | 2 |  | 2 |  |
|  | Flat Plate Area, $\mathrm{ft}^{2}\left(\mathrm{~m}^{2}\right)$ | 2.53 (0.24) |  | 4.38 (0.41) |  | 4.5 (0.42) |  | 1.9 (0.18) |  | 1.9 (0.18) |  | 2.58 (0.24) |  | 2.4 (0.22) |  | 4.1 (0.38) |  |
|  | Lateral Windload Thrust, Ibf( N ) | 95 (423) |  | 164 (730) |  | 169 (752) |  | 53 (236) |  | 69 (307) |  | 108 (480) |  | 90 (400) |  | 169 (752) |  |
|  | Survival Wind Speed without ice, $\mathrm{mph}(\mathrm{kph})$ with $0.5^{\prime \prime}$ radial ice, $\mathrm{mph}(\mathrm{kph})$ | $\begin{aligned} & 110(177) \\ & 93(150) \\ & \hline \end{aligned}$ |  | $\begin{gathered} 75(121) \\ 60(97) \\ \hline \end{gathered}$ |  | $\begin{aligned} & 75(121) \\ & 65(105) \end{aligned}$ |  | $\begin{aligned} & 222(357) \\ & 193 \text { (311) } \end{aligned}$ |  | $\begin{aligned} & 172(277) \\ & 150(241) \end{aligned}$ |  | $\begin{aligned} & 110(177) \\ & 96 \text { (154) } \end{aligned}$ |  | $\begin{aligned} & 130(209) \\ & 115(185) \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 75(121) \\ & 65(105) \\ & \hline \end{aligned}$ |  |
|  | Mounting Hardware included | DSH3V3R |  | DSH3V3N |  | DSH3V3N |  | DSH2V3R |  | DSH2V3R |  | DSH3V3N |  | DSH3V3R |  | DSH3V3N |  |
|  | Length, ft(m) | 12.7 (3.9) |  | 21.9 (6.7) |  | 22.3 (6.8) |  | 7.7 (2.3) |  | 9.9 (3) |  | 18.1 (5.5) |  | 13.6 (4.1) |  | 24.3 (7.4) |  |
|  | Radome O.D., in(cm) | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  | 3 (7.6) |  |
|  | Mast O.D., in(cm) | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  | 2.5 (6.4) |  |
|  | Net Weight w/o bracket, lb(kg) | 37 (16.8) |  | 60 (27.2) |  | 63 (28.6) |  | 19 (8.6) |  | 26 (11.8) |  | 47 (21.3) |  | 40 (18.1) |  | 70 (31.8) |  |
|  | Shipping Weight, lb(kg) | 67 (30.4) |  | 90 (40.8) |  | 93 (42.2) |  | 39 (17.7) |  | 56 (25.4) |  | 77 (34.9) |  | 70 (31.8) |  | $100 \text { (45.4) }$ |  |



## Antenna Mounting Hardware



DSH1V3R


REGULAR MOUNTING
Mount aluminum base station antennas to round or angled tower legs. Center section of each clamp is welded to provide mechanical stability and all parts are hot-dipped galvanized steel.

| MODELS | DSH1V3R | DSH2V3R | DSH2H3R | DSH3V3R |
| :---: | :---: | :---: | :---: | :---: |
|  | DSH1V4R | DSH2V4R | DSH2H4R | DSH3V4R |
| Antenna Length, ft(m) | 0 (0) to 3.5 (1) | 3.5 (1) to 10 (3.1) | 3.5 (1) to 10 (3.1) | 10 (3.1) to 14 (4.3) |
| \# of Clamps | 1 | 2 | 2 | 3 |
| Mounting | Vertical | Vertical | Horizontal | Vertical |
| Pipe Mount, in (mm): 3R | 1.3 (32) to 3.5 (89) | 1.3 (32) to 3.5 (89) | 1.3 (32) to 3.5 (89) | 1.3 (32) to 3.5 (89) |
| Pipe Mount, in (mm): 4R | 1.3 (32) to 4 (102) | 1.3 (32) to 4 (102) | 1.3 (32) to 4 (102) | 1.3 (32) to 4 (102) |
| Weight, lb (kg) | 4 (1.8) | 7 (3.2) | 10 (4.5) | 9(4.1) |
| Shipping Weight, lb (kg) | 6 (2.7) | 8 (3.6) | 12(5.5) | 10(4.5) |

HEAVY-DUTY "NO-TORSION" MOUNTING
Utilizes three clamps on a galvanized steel tube to mount antennas to round tower members.

| MODEL | DSH3V3N | DSH3V4N |
| :--- | :---: | :---: |
| Antenna Length, $\mathrm{ft}(\mathrm{m})$ | $14(4.3)$ and greater | $14(4.3)$ and greater |
| \# of Clamps | 3 | 3 |
| Mounting | Vertical | Vertical |
| Pipe Mount, in $(\mathrm{mm})$ | $3(76.2)$ MAX. | $4(101.6)$ MAX. |
| Weight, lb $(\mathrm{kg})$ | $28(12.7)$ | $28(12.7)$ |
| Shipping Weight, Ib (kg) | $30(13.6)$ | $30(13.6)$ |
| Shipping Dimensions <br> $(W \times H ~ X ~ D), ~ i n(m m) ~$ | $11 \times 33 \times 4$ <br> $(279 \times 838 \times 102)$ | $11 \times 33 \times 4$ |

TOP SWAY BRACE - OUTRIGGER MOUNTING
Limit tip deflection on 3-inch diameter fiberglass antennas in high wind conditions. Attaches to the tower legs using supplied DSH2H3R hardware kit (above). Recommended on top-mounted antennas $>16$ feet long.

| MODEL | DSH2H3S |
| :--- | :---: |
| \# of Clamps | 2 |
| Mounting | Horizontal |
| Flange Inner Diameter, in (mm) | $3.38(85.7)$ |
| Tube Diameter, in (mm) | $2(50.8)$ |
| Length to Center of Flange ft (m) | 12 feet $(3.6)$ |
| Weight, lb $(\mathrm{kg})$ | $10(4.5)$ |
| Shipping Weight, lb $(\mathrm{kg})$ | $20(9.1)$ |
| Shipping Dimensions | $11 \times 33 \times 4$ |
| (W x H x D), in $(\mathrm{mm})$ | $(279 \times 838 \times 102)$ |

DIRECTIONAL ANTENNA MOUNTING HARDWARE Model DB380


| Antenna Length | $\mathrm{N} / \mathrm{A}$ |
| :--- | :---: |
| $\#$ of Clamps | 2 |
| Mounting | Antenna-to-Pipe |
| Pipe Mount, in(mm) | $3.5(76.2)$ |
| Weight, lb (kg) | $10(4.5)$ |
| Shipping Weight, lb $(\mathrm{kg})$ | $20(9.1)$ |

# TrunkLine Antenna, Standard (FCC 101, Cat A) , Single Polarized, 6 ft 

RFS Microwave Antennas are designed for microwave systems in all common frequency ranges from 4 GHz to 24 GHz . This allows the use of antennas in areas where extreme wind conditions are normal. The antennas utilise a conventional feed system and are available in three performance classes offering complete flexibility when designing a network. Standard Performance antennas are economical solutions for systems where side lobe suppression is of less importance. These antennas are required for use in networks where there is a low interference potential. Antennas are available in $2 \mathrm{ft}(0.6 \mathrm{~m})$ to $12 \mathrm{ft}(3.7 \mathrm{~m})$ diameters. Antennas from 4 ft up to 12 $\mathrm{ft}(3.7 \mathrm{~m})$ can be equipped with a moulded radome to reduce wind load and to protect the feed against the accumulation of ice and snow.

## FEATURES / BENEFITS

$\rightarrow$ Field-proven reliability and long life
$\Theta$ Withstanding winds up to $200 \mathrm{~km} / \mathrm{h}(125 \mathrm{mph})$, an optional sway bar is available for added assurance in case mistakes are made during installation
$\rightarrow$ A single-piece configuration and compact packaging to reduce transportation costs
$\Theta \quad$ Frequencies ranging from 4 GHz to 15 GHz with support for two wideband frequency ranges (5.725-6.875 and $7.125-8.5 \mathrm{GHz}$ ) to reduce antenna requirements and simplify logistics

## GENERAL SPECIFICATIONS

| Product Type |  | Point to point antennas |
| :---: | :---: | :---: |
| Profile |  | TrunkLine |
| Performance |  | Improved Performance |
| Polarization |  | Single |
| Antenna Input |  | CPR137G |
| Reflector |  | 1-part |
| Radome |  | Optional |
| Antenna color |  | White RAL 9010 |
| Swaybar |  | 1: ( $2.0 \mathrm{~m} \times \varnothing 60 \mathrm{~mm}$ ) |
| ELECTRICAL SPECIFICATIONS |  |  |
| Frequency | GHz | 5.925-6.875 |
| 3dB beamwidth | degrees | 1.7 |
| Low Band Gain | dBi | 38.4 |
| Mid Band Gain | dBi | 39.1 |
| High Band Gain | dBi | 39.7 |
| F/B Ratio | dB | 55.0 |
| XPD | dB | 30.0 |
| Max VSWR / R L | VSWR / dB | 1.08 ( 28.3 ) |
| Regulatory Compliance |  | FCC Category A |
| MECHANICAL SPECIFICATIONS |  |  |
| Diameter | ft (m) | 6 (1.8) |
| Elevation Adjustment | degrees | $\pm 5$ |
| Azimuth Adjustment | degrees | $\pm 5$ |
| Polarization Adjustment | degrees | $\pm 5$ |
| Mounting Pipe Diameter minimum | mm (in) | 114 (4.5) |
| Mounting Pipe Diameter maximum | mm (in) | 114 (4.5) |
| Approximate Weight | kg (lb) | 65 (141) |
| Survival Windspeed | $\mathrm{km} / \mathrm{h}$ (mph) | 200 (125) |
| Operational Windspeed | km/h (mph) | 190 (118) |
| STRUCTURE |  |  |
| Radome Material |  | Fiberglass |
| FURTHER ACCESSORIES |  |  |
| optional Swaybar |  | 1: SMA-SK-60-2000A ( $2.0 \mathrm{~m} \times \varnothing 60 \mathrm{~mm}$ ) |
| Further Accessories |  | SMA-SKO-UNIVERSAL-L : Universal sway bar fixation kit |

## TrunkLine Antenna, Standard (FCC 101, Cat A) , Single Polarized, 6 ft

Mount Outline

| Dimension A | mm (in) | $2000(79)$ |
| :--- | :---: | :--- |
| Dimension C | $\mathrm{mm}(\mathrm{in})$ | $364(14.3)$ |
| Dimension D for 114mm (4.5in) Pipe | mm (in) | $175(6.9)$ |
| Dimension E | mm (in) | $283(11.1)$ |
| Dimension F | mm (in) | $590(23.2)$ |


| FST Side force max. @ survival wind speed | $\mathrm{N}(\mathrm{lb})$ | $2910(651)$ |
| :--- | :---: | :--- |
| FAT Axial force max. @ survival wind speed | $\mathrm{N}(\mathrm{lb})$ | $9900(2217)$ |
| MT Torque maximum @ survival wind speed | $\mathrm{Nm}(\mathrm{lb} \mathrm{ft})$ | $3055(2270)$ |



## External Document Links

Notes
Complete Antenna installation
Only available in North America
RPE (IQ-Link format)
RPE (PDF format)
RPE (Pathloss format)


| PARTS LIST |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITEM | QTY | PART NO. | PART DESCRIPTION | LENGTH | UNIT WT. | NET WT. |
| 1 | 4 | X-158320 | ANGLE CLAMP | $161 / 2$ in | 8.51 | 34.03 |
| 2 | 4 | x-126501 | BRACKET ANGLE LEG MOUNTING | $161 / 2 \mathrm{in}$ | 7.13 | 28.51 |
| 3 | 2 | x-154463 | UNIVERSAL PIPE MOUNTING PLATE (INNER) |  | 10.52 | 21.03 |
| 4 | 2 | x-155561 | UNIVERSAL PIPE MOUNTING PLATE (OUTER) |  | 13.16 | 26.31 |
| 5 | 2 | X-159999 | BACKING PLATE |  | 5.73 | 11.46 |
| 6 | 4 | X-UB1458 | 1/2" $\times 4$-5/8" $\times 7$ " $\times 3$ " GALV U-BOLT |  | 0.97 | 3.89 |
| 7 | 8 | G12R-20 | 1/2" $\times 20$ " GALV. THREADED ROD |  | 1.12 | 8.92 |
| 8 | 8 | G1203 | $1 / 2$ " $\times 3$ " HDG HEX BOLT GR5 FULL THREAD | 3 in | 0.22 | 1.74 |
| 9 | 8 | G1204 | $1 / 2^{\prime \prime} \times 4$ " HDG HEX BOLT GR5 FULL THREAD | 4 in | 0.27 | 2.16 |
| 9 | 8 | G12065 | $1 / 2$ " $\times 6-1 / 2$ " HDG HEX BOLT GR5 FULL THREAD | $61 / 2 \mathrm{in}$ | 0.41 | 3.28 |
| 10 | 32 | G12FW | 1/2" HDG USS FLATWASHER |  | 0.03 | 1.09 |
| 11 | 32 | G12LW | 1/2" HDG LOCKWASHER |  | 0.01 | 0.44 |
| 12 | 32 | G12NUT | 1/2" HDG HEAVY 2H HEX NUT |  | 0.07 | 2.29 |
| 13 | 4 | G5802 | 5/8" $\times 2$ " HDG HEX BOLT GR5 |  | 0.27 | 1.09 |
| 14 | 4 | G58FW | $5 / 8$ " HDG USS FLATWASHER |  | 0.07 | 0.28 |
| 15 | 4 | G58LW | 5/8" HDG LOCKWASHER |  | 0.03 | 0.10 |
| 16 | 4 | G58NUT | 5/8" HDG HEAVY 2H HEX NUT |  | 0.13 | 0.52 |
| 17 | 1 | P472 | 4-1/2" $\times$ 72" SCH. 40 GALVANIZED PIPE |  | 64.89 | 64.89 |
|  |  |  |  |  | TOTAL WT.\# | 148.00 |



DETAIL A
USED FOR 5" to 10-3/4" OD PIPE LEGS
\& 3" to 8" ANGLE LEGS

DETAIL B
USED FOR $1-1 / 2^{\prime \prime}$ to $4-1 / 2^{\prime \prime}$ OD PIPE LEGS



# Microwave Path Data Sheet <br> COMSEARCH 

19700 Janelia Farm Boulevard, Ashburn, VA, 20147
(703)636-5234 www.comsearch.com

PCN Date: 09/18/2019
New Path
Job Number: 190918COMSDS04
RCN Number: 19091852

| Administrative Information | SOUTH MTN CT | W HARTLAND CT |
| :---: | :---: | :---: |
| City/County | Bristol/Hartford | /Hartford |
| Status / License Basis | Engineering Proposal / PRIMARY OPERATION | Engineering Proposal / PRIMARY OPERATION |
| Call Sign | KVG93 |  |
| Licensee Code | S68716 | S68716 |
| Licensee Name | Eversource Energy Service Company | Eversource Energy Service Company |
| Radio Service / Station Class | MG -- Microwave Industrial/Business Pool | FXO -- Fixed |
| Site Information |  |  |
| Latitude (NAD 83) | $41^{\circ} 38{ }^{\prime} 56.00^{\prime \prime}$ | $41^{\circ} 58{ }^{\prime} 43.5{ }^{\prime \prime} \mathrm{N}$ |
| Longitude (NAD 83) | $72^{\circ} 56{ }^{\prime} 50.0{ }^{\prime \prime} \mathrm{W}$ | $72^{\circ} 58{ }^{\prime} 56.01{ }^{\prime \prime} \mathrm{W}$ |
| Ground Elevation (m/ft-AMSL) | 310.60 / 1019.0 | 371.71 / 1219.5 |
| Antenna Structure Registration \# |  |  |
| Path Azimuth ( ${ }^{\circ}$ ) | 355.473 | 175.450 |
| Path Length (km / miles) | $36.753 / 22.837$ |  |
| Transmit Antenna | 44008C | 44008C |
| Manufacturer | RFS | RFS |
| Model | PAD6-59B | PAD6-59B |
| Gain(dBi) / Beamwidth( ${ }^{\circ}$ ) / Tilt $\left({ }^{\circ}\right.$ ) | 38.7 / 1.80 / -0.01 | 38.7 / 1.80 / -0.24 |
| Centerline (m/ft - AGL) | 26.52 / 87.0 | 37.80 / 124.0 |

## Receive Antenna

Same As Transmit
Manufacturer
Model
Gain (dBi) / Beamwidth ( ${ }^{\circ}$ )
Centerline ( $\mathrm{m} / \mathrm{ft}$ - AGL)

## Diversity Receive Antenna

Manufacturer
Model
Gain (dBi) / Beamwidth ( ${ }^{\circ}$ )
Centerline ( $\mathrm{m} / \mathrm{ft}$ - AGL)

| Radio Information | TEEV61 |  |  | TEEV61 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Manufacturer | Aviat Networks, Inc. I600V4EHPL6-30M 256Q 179 |  |  | Aviat Networks, Inc I600V4EHPL6-30M 256Q 179 |  |  |
| Model |  |  |  |  |  |  |
| Model Description | ECLIPSE IRU 600 RAC $60-6 \mathrm{C}$ MAX TP |  |  | ECLIPSE IRU 600 RAC 60-6X MAX TP |  |  |
| Emission Designator / Modulation | 30M0D7W 256 QAM |  |  | $30 M 0 D 7 W$ 256 QAM |  |  |
| Loading | 1 CH DIG 179000.000 |  |  | 1 CH DIG 179000.000 |  |  |
| Stability (\%) | 0.0005 |  |  | 0.0005 |  |  |
|  | Nominal | Coordinated | Maximum | Nominal | Coordinated | Maximum |
| Power (dBm) |  | 37.0 |  |  | 37.0 |  |
| Received Level (dBm) |  | -31.9 |  |  | -31.9 |  |
| EIRP (dBm) |  | 72.6 |  |  | 72.1 |  |
| Fixed Loss: Tx / Common (dB) Free Space Loss (dB) | $0.0 / 3.1$ |  | 139.6 | $0.0 / 3.6$ |  |  |
| Transmit Frequencies (MHz) | 5945.200 | V(11T) |  | 6197.240 | V(21T) |  |

ATTACHMENT C - STRUCTURAL ANALYSIS REPORT

## Subject:

Eversource Designation:

Engineering Firm Designation:
Site Data:

## Structural Analysis Report

Number: ES-004
Site Name:

Black \& Veatch Corp Project Number:
790 Willis Street, Bristol, Hartford County, CT Latitude $41^{\circ} 38^{\prime} 56.0^{\prime \prime}$, Longitude $-72^{\circ} 56^{\prime} 50.0^{\prime}$ 130 Foot - Self Support Tower

SouthMtnsRS

405025

Black \& Veatch Corp is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above-mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC1: Proposed Equipment Configuration
Sufficient Capacity - 41.8\%
This analysis utilizes an ultimate 3-second gust wind of 130 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Structural analysis prepared by: Sanyukta R. Arvikar
Respectfully submitted by:

Joshua J Riley, P.E. Professional Engineer


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tnxTower Output

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Additional Calculations

## 1) INTRODUCTION

This tower is a 130 ft Self Support tower manufactured by Radian in December of 2006.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Seismic Ss:
Seismic S1:
Service Wind Speed:

Seismic loading does not control per engineering judgement.

Table 1 - Proposed Equipment Configuration

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{aligned} & \text { Number } \\ & \text { of } \\ & \text { Antennas } \end{aligned}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130.0 | 140.0 | 1 | comprod | 876F-70-2 | 2 | 7/8 | 1 |
| 87.0 | 87.0 | 1 | rfs | PAD6-W59BC | 1 | E65J | - |
|  |  | 1 | site pro 1 | R5-LL [PM 602-1] |  |  |  |

[^2]Table 2 - Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\lvert\, \begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}\right.$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 127.0 | 141.5 | 1 | unknown | 25' Omni | 10 | 7/8 | 1 |
|  | 141.0 | 1 | unknown | 24' Omni |  |  |  |
|  | 139.0 | 1 | unknown | 21' Omni |  |  |  |
|  | 138.0 | 1 | unknown | 18' Omni |  |  |  |
|  | 137.0 | 1 | unknown | 16' Omni |  |  |  |
|  | 136.0 | 1 | unknown | 16' Omni |  |  |  |
|  | 135.0 | 1 | unknown | 12' Omni |  |  |  |
|  | 134.0 | 1 | unknown | 10' Omni |  |  |  |
|  | 129.0 | 1 | unknown | 10"x8"x3" TMA |  |  |  |
|  | 127.0 | 1 | tower mounts | Sector Mount [SM 501-3] |  |  |  |
| 125.0 | 125.0 | 3 | rfs celwave | APXVAALL24_43 w/ Mount Pipe | 3 | $\begin{aligned} & 6 \times 24 \\ & \text { fiber } \end{aligned}$ | 1 |
|  |  | 3 | ericsson | AIR6449 w/ Mount Pipe |  |  |  |
|  |  | 3 | ericsson | AIR32 w/ Mount Pipe |  |  |  |
|  |  | 3 | ericsson | 4449 |  |  |  |
|  |  | 3 | ericsson | 4415 |  |  |  |
|  |  | 1 | tower mounts | Sector Mount [SM 502-3] |  |  |  |
| 117.0 | 117.0 | 1 | tower mounts | 6 ' x 3" Mount Pipe | 1 | E60 | 1 |
|  |  | 1 | unknown | PA6-59 |  |  |  |
| 113.0 | 120.0 | 1 | celwave | PD1142-1 | 11 | $\begin{aligned} & 1 / 2 \\ & 7 / 8 \end{aligned}$ | 1 |
|  | 113.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] |  |  |  |
| 107.0 | 107.0 | 1 | tower mounts | 6' x 3" Mount Pipe | 1 | E65 | 1 |
|  |  | 1 | unknown | 6 FT Dish |  |  |  |
| 104.0 | 111.0 | 1 | celwave | PD1142-1 | 1 | 7/8 | 1 |
|  | 104.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] |  |  |  |
| 98.0 | 98.0 | 1 | antennae | DB205-A | 1 | 7/8 | 1 |
|  |  | 1 | tower mounts | Side Arm Mount [SO 306-1] |  |  |  |
| 96.0 | 96.0 | 1 | tower mounts | 6' x 3" Mount Pipe | 1 | E60 | 1 |
|  |  | 1 | unknown | 8 FT Dish |  |  |  |
| 86.0 | 86.0 | 1 | tower mounts | 6' x 3" Mount Pipe | 1 | E60 | 1 |
|  |  | 1 | unknown | PAD8-59AW |  |  |  |
| 84.0 | 91.0 | 1 | celwave | PD1142-1 | 1 | 1/2 | 1 |
|  | 84.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] |  |  |  |
| 84.0 | 84.0 | 1 | antennae | 2' Yagi | 1 | 7/8 | 1 |
|  |  | 1 | tower mounts | 4'x2" Pipe Mount |  |  |  |
| 77.0 | 78.0 | 1 | andrew panel antennas | SBNH-1D6565A w/ Mount Pipe | $\begin{aligned} & 1 \\ & 4 \end{aligned}$ | $\begin{gathered} 1 / 2 \\ 15 / 8 \end{gathered}$ | 1 |
|  | 77.0 | 1 | tower mounts | Sector Mount [SM 402-1] |  |  |  |
|  |  | 1 | miscl | TMA |  |  |  |
|  | 67.0 | 2 | antennae | 3" Dia 20' Omni |  |  |  |
| 71.0 | 71.0 | 1 | tower mounts | 6' x 3" Mount Pipe | 1 | E65 | 1 |
|  |  | 1 | unknown | 4 FT Dish |  |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | $\text { \| } \begin{aligned} & \text { Number } \\ & \text { of } \\ & \text { Antennas } \end{aligned}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 63.0 | 73.0 | 1 | antennae | 3" Dia 20' Omni | $\begin{aligned} & 1 \\ & 1 \\ & 3 \end{aligned}$ | $\begin{gathered} 7 / 8 \\ 1 / 2 \\ 15 / 8 \end{gathered}$ | 1 |
|  |  | 1 | unknown | Diamond X-500A |  |  |  |
|  | 63.0 | 1 | tower mounts | Sector Mount [SM 402-1] |  |  |  |
|  |  | 1 | miscl | TMA |  |  |  |
|  | 53.0 | 2 | antennae | 3" Dia 20' Omni |  |  |  |
| 58.0 | 58.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] | 1 | 1/2 | 1 |
|  |  | 1 | decibel | DB212-1 |  |  |  |
| 54.0 | 54.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] | 1 | 1/2 | 1 |
|  |  | 1 | decibel | DB212-1 |  |  |  |
| 43.0 | 46.0 | 1 | antennae | 3" Dia. 6' Omni | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 3 / 8 \\ & 7 / 8 \end{aligned}$ | 1 |
|  | 43.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] |  |  |  |
|  | 40.0 | 1 | antennae | 3" Dia. 6' Omni |  |  |  |
| 43.0 | 43.0 | 1 | tower mounts | Side Arm Mount [SO 306-1] | 1 | 3/8 | 1 |
|  | 43.0 | 1 | decibel | DB230-2B |  |  |  |

Note:

1) Existing Equipment

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| TOWER STRUCTURAL ANALYSIS REPORTS | Centek Engineering, Inc., dated 09/16/2013 | Tower geometry and geotechnical data | Eversource |
| TOWER STRUCTURAL ANALYSIS REPORTS | Centek Engineering, Inc., dated 06/14/2019 | Tower geometry, tower loading and geotechnical data | Eversource |
| TOWER STRUCTURAL ANALYSIS REPORTS | Centek Engineering, Inc., dated 03/02/2021 | Tower loading | Connecticut Siting Council |

## 3.1) Analysis Method

tnxTower (version 8.1.1.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built and maintained in accordance with the manufacturer's specifications.
2) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
3) This analysis was performed under the assumption that all information provided to Black \& Veatch is current and correct. This is to include site data, appurtenance loading, tower/foundation details, and geotechnical data.
4) Tower loading is based on 2018 drone mapping photos and previous tower analyses.
5) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically and must be replaced if damaged or cracked

This analysis may be affected if any assumptions are not valid or have been made in error. Black \& Veatch Corp should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

| Section No. | Elevation (ft) | Component Type | Size | Critical Element | P (K) | $\underset{(\mathrm{K})}{\text { SF }^{*} \text { P_allow }}$ | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 130-120 | Leg | ROHN 2.5 STD | 1 | -12.20 | 60.05 | 20.3 | Pass |
| T2 | 120-100 | Leg | ROHN 3 STD | 29 | -23.60 | 74.43 | 31.7 | Pass |
| T3 | 100-80 | Leg | ROHN 4 STD | 69 | -42.56 | 122.04 | 34.9 | Pass |
| T4 | 80-60 | Leg | ROHN 5 STD | 107 | -62.09 | 150.53 | 41.2 | Pass |
| T5 | 60-40 | Leg | ROHN 5 EH | 134 | -85.40 | 211.17 | 40.4 | Pass |
| T6 | 40-20 | Leg | ROHN 6 EHS | 161 | -107.07 | 256.16 | 41.8 | Pass |
| T7 | 20-0 | Leg | ROHN 6 EH | 189 | -128.00 | 318.80 | 40.2 | Pass |
| T1 | 130-120 | Diagonal | ROHN 2 STD | 9 | -3.39 | 25.36 | 13.4 | Pass |
| T2 | 120-100 | Diagonal | ROHN 2.5 STD | 36 | -4.71 | 35.92 | 13.1 | Pass |
| T3 | 100-80 | Diagonal | ROHN 2.5 STD | 74 | -6.27 | 31.52 | 19.9 | Pass |
| T4 | 80-60 | Diagonal | ROHN 2.5 X-STR | 113 | -8.46 | 21.63 | 39.1 | Pass |
| T5 | 60-40 | Diagonal | ROHN 3 STD | 140 | -7.88 | 29.61 | 26.6 | Pass |
| T6 | 40-20 | Diagonal | ROHN 3 STD | 165 | -8.05 | 26.21 | 30.7 | Pass |
| T7 | 20-0 | Diagonal | ROHN 3 STD | 192 | -8.22 | 22.99 | 35.7 | Pass |
| T1 | 130-120 | Horizontal | ROHN 1.5 STD | 7 | -2.43 | 23.71 | 10.2 | Pass |
| T2 | 120-100 | Horizontal | ROHN 2 STD | 34 | -2.87 | 34.21 | $\begin{gathered} 8.4 \\ 10.0(b) \\ \hline \end{gathered}$ | Pass |
| T3 | 100-80 | Horizontal | ROHN 2 STD | 73 | -4.24 | 28.55 | 14.9 | Pass |
| T4 | 80-60 | Horizontal | ROHN 2 STD | 112 | -4.95 | 23.75 | 20.8 | Pass |
| T5 | 60-40 | Horizontal | ROHN 2 STD | 139 | -5.04 | 17.60 | 28.6 | Pass |
| T6 | 40-20 | Horizontal | ROHN 2.5 STD | 163 | -5.46 | 30.30 | $\begin{gathered} 18.0 \\ 19.3(b) \\ \hline \end{gathered}$ | Pass |
| T7 | 20-0 | Horizontal | ROHN 2.5 STD | 190 | -5.85 | 23.43 | 25.0 | Pass |
| T1 | 130-120 | Top Girt | ROHN 1.5 STD | 4 | -0.48 | 23.77 | 2.0 | Pass |
| T1 | 130-120 | Inner Bracing | L2 $2 \times 2 \times 1 / 8$ | 16 | -0.00 | 8.80 | 0.8 | Pass |
| T2 | 120-100 | Inner Bracing | L2 $2 \times 2 \times 1 / 8$ | 42 | -0.01 | 6.48 | 0.9 | Pass |
| T3 | 100-80 | Inner Bracing | L2 $2 \times 2 \times 1 / 8$ | 79 | -0.01 | 4.43 | 1.1 | Pass |
| T4 | 80-60 | Inner Bracing | L2 $2 \times 2 \times 1 / 8$ | 120 | -0.01 | 3.34 | 1.2 | Pass |
| T5 | 60-40 | Inner Bracing | L2 1/2x2 1/2x3/16 | 147 | -0.02 | 6.99 | 0.9 | Pass |
| T6 | 40-20 | Inner Bracing | L 3x3x3/16 | 174 | -0.02 | 9.16 | 0.9 | Pass |
| T7 | 20-0 | Inner Bracing | L3 1/2x3 /12x1/4 | 201 | -0.02 | 14.24 | 0.8 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Leg (T6) | 41.8 | Pass |
|  |  |  |  |  |  | Diagonal (T4) | 39.1 | Pass |
|  |  |  |  |  |  | Horizontal (T5) | 28.6 | Pass |
|  |  |  |  |  |  | Top Girt (T1) | 2.0 | Pass |
|  |  |  |  |  |  | Inner Bracing (T4) | 1.2 | Pass |
|  |  |  |  |  |  | Bolt Checks | 26.7 | Pass |

tnxTower Report - version 8.1.1.0

| Section <br> No. | Elevation (ft) | Component Type | Size | Critical <br> Element | $\mathbf{P ( K )}$ | SF*P_allow <br> (K) | \% <br> Capacity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Pass / Fail |  |  |

Table 5 - Tower Component Stresses vs. Capacity - LC1

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 27.3 | Pass |
| 1 | Base Foundation | 0 | 27.8 | Pass |
| 1 | Base Foundation <br> Soil Interaction | 0 | 33.6 | Pass |


| Structure Rating (max from all components) $=$ | $41.8 \%$ |
| :---: | :---: |

Note:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity. Rating per TIA-222-H Section 15.5

## 4.1) Recommendation

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## Maximum Tower Deflections - Service Wind

| Section | Elevation | Horz. <br> Deflection | Gov. <br> Load <br> No. | Tilt | Twist | Check* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | in | Comb. | $\circ$ | $\circ$ |  |
| T1 | $130-120$ | 1.009 | 44 | 0.066 | 0.007 | OK |
| T2 | $120-100$ | 0.869 | 44 | 0.065 | 0.007 | OK |
| T3 | $100-80$ | 0.606 | 44 | 0.057 | 0.007 | OK |
| T4 | $80-60$ | 0.385 | 44 | 0.045 | 0.006 | OK |
| T5 | $60-40$ | 0.219 | 44 | 0.032 | 0.005 | OK |
| T6 | $40-20$ | 0.1 | 44 | 0.021 | 0.004 | OK |

*Limit State Deformation (TIA-222-H Section 2.8.2)

1) Maximum Rotation $=4$ Degrees
2) Maximum Deflection $=0.03 *$ Tower Height $=47$ in.

Critical Deflections of Tower at the MW Dish Elevations - Service Wind

| Elevation (ft) | MW Dish | Tilt ( $\left.{ }^{( }\right)$ | Twist ( ${ }^{\circ}$ ) | Diameter, $D$ <br> (ft) | Frequency, $\alpha$ (GHz) | Decibel <br> Points | Deformation <br> Limit ( $\theta$ )* | Deformation <br> Limit <br> Exceeded? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 117 | PA6-59 | 0.064 | 0.007 | 6 | 10 | 10 dB | 0.885 | Not Exceeded |
| 107 | 6 FT Dish | 0.06 | 0.007 | 6 | 10 | 10 dB | 0.885 | Not Exceeded |
| 96 | 8 FT Dish | 0.054 | 0.007 | 8 | 10 | 10 dB | 0.664 | Not Exceeded |
| 87 | PAD6W59BC | 0.049 | 0.006 | 6.58333 | 10 | 10 dB | 0.807 | Not Exceeded |
| 86 | PAD8-59AW | 0.048 | 0.006 | 8 | 10 | 10 dB | 0.664 | Not Exceeded |
| 71 | 4 FT Dish | 0.039 | 0.006 | 4 | 10 | 10 dB | 1.328 | Not Exceeded |

*Limit per TIA-222-H Annex D

Maximum Tower Deflections - Design Wind

| Section | Elevation | Horz. <br> Deflection | Gov. <br> Load <br> No. | Tilt | Twist | Combined <br> Max | Check $^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $130-120$ | 2.81 | 44 | 0.183 | 0.021 | 0.184 |
| T1 | $120-100$ | 2.418 | 44 | 0.18 | 0.021 | 0.181 | OK |
| T2 | $100-80$ | 1.685 | 44 | 0.157 | 0.019 | 0.158 | OK |
| T3 | $80-60$ | 1.069 | 44 | 0.123 | 0.018 | 0.124 | OK |
| T4 | $60-40$ | 0.609 | 44 | 0.088 | 0.015 | 0.089 | OK |
| T5 | $40-20$ | 0.28 | 44 | 0.057 | 0.01 | 0.058 | OK |
| T6 |  |  |  | OK |  |  |  |

*Up to 0.5 degree is considered acceptable per SUB090 Section 7

Critical Deflections of Tower at the MW Dish Elevations - Design Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Comb. | in | $\circ$ | $\circ$ | $f t$ |
| $f t$ |  | 44 | 2.303 | 0.178 | 0.021 | 59845.000 |
| 117 | PA6-59 | 44 | 1.932 | 0.167 | 0.02 | 47266.000 |
| 107 | 6 FT Dish | 44 | 1.551 | 0.151 | 0.019 | 36745.000 |
| 96 | 8FT Dish | 44 | 1.268 | 0.136 | 0.018 | 31007.000 |
| 87 | PAD6-W59BC | 44 | 1.238 | 0.134 | 0.018 | 30438.000 |
| 86 | PAD8-59AW | 44 | 0.844 | 0.107 | 0.017 | 32092.000 |
| 71 | 4 FT Dish |  |  |  |  |  |

## APPENDIX A

## TNXTOWER OUTPUT



## Tower Input Data

The main tower is a $3 x$ free standing tower with an overall height of 130.000 ft above the ground line.
The base of the tower is set at an elevation of 0.000 ft above the ground line.
The face width of the tower is 8.500 ft at the top and 22.540 ft at the base.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

- Tower is located in Hartford County, Connecticut.
- Tower base elevation above sea level: 1047.000 ft .
- Basic wind speed of 130 mph .
- Risk Category III.
- Exposure Category B.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- Topographic Category: 1.
- Crest Height: 0.000 ft .
- Nominal ice thickness of 2.000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56 pcf.
- A wind speed of 50 mph is used in combination with ice.
- Temperature drop of $50^{\circ} \mathrm{F}$.
- Deflections calculated using a wind speed of 60 mph .
- Pressures are calculated at each section.
- Stress ratio used in tower member design is 1.05 .
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.


## Options

[^3]Distribute Leg Loads As Uniform Assume Legs Pinned
$\checkmark$ Assume Rigid Index Plate
$\checkmark$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
Autocalc Torque Arm Areas
Add IBC .6D+W Combination
$\checkmark$ Sort Capacity Reports By Component
$\sqrt{ }$ Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
$\checkmark$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation
$\checkmark$ Consider Feed Line Torque
$\sqrt{ }$ Include Angle Block Shear Check
Use TIA-222-H Bracing Resist. Exemption
Use TIA-222-H Tension Splice
Exemption
Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No
Appurtenances
Outside and Inside Corner Radii Are
Known


Triangular Tower

Tower Section Geometry

| Tower <br> Section | Tower <br> Elevation | Assembly <br> Database | Description | Section <br> Width | Number <br> of <br> Sections |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ft |  | ft | Section <br> Length |  |  |
| T1 | $130000-000$ |  | 8.500 | 1 | ft |
| T2 | 120.000 | $120.000-$ | 8.540 | 1 |  |
| T3 | 100.000 |  |  |  | 20.000 |
| T4 | $80.000-80.000$ |  | 12.730 | 1 |  |
| T5 | $60.000-40.000$ |  | 14.960 | 1 | 1 |
| T6 | $40.000-20.000$ |  | 17.540 | 1 | 20.000 |
| T7 | $20.000-0.000$ |  | 20.040 | 1 | 20.000 |
|  |  |  |  | 20.000 |  |
|  |  |  |  |  |  |

Tower Section Geometry (cont'd)

| Tower <br> Section | Tower <br> Elevation | Diagonal <br> Spacing | Bracing <br> Type | Has <br> K Brace <br> End | Has <br> Horizontals | Top Girt <br> Offset | Bottom Girt <br> Offset |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| f1 | $130.000-$ | 5.000 | K Brace Down | No | Yes | 0.000 | in |

## Tower Section Geometry (cont'd)

| Tower Elevation ft | $\begin{aligned} & \text { Leg } \\ & \text { Type } \end{aligned}$ | $\begin{aligned} & \hline \text { Leg } \\ & \text { Size } \end{aligned}$ | Leg Grade | Diagonal Type | $\begin{aligned} & \hline \text { Diagonal } \\ & \text { Size } \end{aligned}$ | Diagonal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T1 130.000- } \\ 120.000 \end{gathered}$ | Pipe | ROHN 2.5 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T2 120.000- } \\ 100.000 \end{gathered}$ | Pipe | ROHN 3 STD | $\begin{aligned} & \text { A572-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Pipe | ROHN 2.5 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T3 100.000- } \\ 80.000 \end{gathered}$ | Pipe | ROHN 4 STD | A572-50 <br> (50 ksi) | Pipe | ROHN 2.5 STD | A572-50 (50 ksi) |
| $\begin{gathered} \text { T4 80.000- } \\ 60.000 \end{gathered}$ | Pipe | ROHN 5 STD | $\begin{aligned} & \text { A572-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Pipe | ROHN 2.5 X-STR | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T5 } 60.000- \\ 40.000 \end{gathered}$ | Pipe | ROHN 5 EH | $\begin{aligned} & \text { A572-50 } \\ & (50 \mathrm{ksi}) \end{aligned}$ | Pipe | ROHN 3 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T6 40.000- } \\ 20.000 \end{gathered}$ | Pipe | ROHN 6 EHS | A572-50 <br> (50 ksi) | Pipe | ROHN 3 STD | A572-50 (50 ksi) |
| $\begin{gathered} \text { T7 } 20.000- \\ 0.000 \end{gathered}$ | Pipe | ROHN 6 EH | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 3 STD | A572-50 <br> (50 ksi) |

Tower Section Geometry (cont'd)

| Tower Elevation <br> ft | No. of Mid Girts | $\begin{aligned} & \text { Mid Girt } \\ & \text { Type } \end{aligned}$ | $\begin{gathered} \text { Mid Girt } \\ \text { Size } \end{gathered}$ | Mid Girt Grade | Horizontal Type | Horizontal Size | Horizontal Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { T1 130.000- } \\ 120.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 1.5 STD | $\begin{aligned} & \hline \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ |
| $\begin{gathered} \text { T2 120.000- } \\ 100.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T3 100.000- } \\ 80.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T4 } 80.000- \\ 60.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T5 } 60.000- \\ 40.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T6 } 40.000- \\ 20.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2.5 STD | $\begin{gathered} \text { A572-50 } \\ (50 \mathrm{ksi}) \end{gathered}$ |
| $\begin{gathered} \text { T7 } 20.000- \\ 0.000 \end{gathered}$ | None | Flat Bar |  | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | Pipe | ROHN 2.5 STD | $\begin{aligned} & \text { A572-50 } \\ & \text { (50 ksi) } \end{aligned}$ |

Tower Section Geometry (cont'd)
$\left.\begin{array}{cccccc}\hline \begin{array}{c}\text { Tower } \\ \text { Elevation }\end{array} & \begin{array}{c}\text { Secondary } \\ \text { Horizontal Type }\end{array} & \begin{array}{c}\text { Secondary Horizontal } \\ \text { Size }\end{array} & \begin{array}{c}\text { Secondary } \\ \text { Horizontal } \\ \text { Grade }\end{array} & \begin{array}{c}\text { Inner Bracing } \\ \text { Type }\end{array} & \text { Inner Bracing Size }\end{array} \begin{array}{c}\text { Inner Bracing } \\ \text { Grade }\end{array}\right]$

Tower Section Geometry (cont'd)

| Tower Elevation <br> ft | $\begin{gathered} \text { Gusset } \\ \text { Area } \\ \text { (per face) } \\ f t^{2} \end{gathered}$ | Gusset Thickness <br> in | Gusset GradeAdjust. Factor $A_{f}$ |  | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Double Angle Double Angle |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Stitch Bolt Spacing Diagonals in |  | Stitch Bolt Spacing Horizontals in | Stitch Bolt Spacing Redundants in |
| $\begin{gathered} \text { T1 130.000- } \\ 120.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 |  | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T2 120.000- } \\ 100.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T3 100.000- } \\ 80.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T4 80.000- } \\ 60.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T5 60.000- } \\ 40.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T6 } 40.000- \\ 20.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ (36 \mathrm{ksi}) \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |
| $\begin{gathered} \text { T7 } 20.000- \\ 0.000 \end{gathered}$ | 0.000 | 0.375 | $\begin{gathered} \text { A36 } \\ \text { (36 ksi) } \\ \hline \end{gathered}$ | 1 | 1.05 | 1.05 | 36.000 | 36.000 | 36.000 |

## Tower Section Geometry (cont'd)

| Tower Elevation | Calc K Single Angles | Calc <br> K Solid Rounds | $K$ Factors ${ }^{1}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Legs | $X$ | K | $\begin{aligned} & \text { Single } \\ & \text { Diags } \end{aligned}$ | Girts | Horiz. | Sec. Horiz. | Inner <br> Brace |
|  |  |  |  | Brace | Brace |  |  |  |  |  |
|  |  |  |  | Diags | Diags |  |  |  |  |  |
|  |  |  |  | X | X | $X$ | $X$ | $X$ | $X$ | $X$ |
| $f t$ |  |  |  | Y | Y | Y | Y | Y | Y | Y |
| T1 130.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 120.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T2 120.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 100.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T3 100.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 80.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T4 80.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 60.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T5 60.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 40.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T6 40.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 20.000 |  |  |  | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| T7 20.000- | Yes | Yes | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 0.000 |  |  |  | 1 | 1 | 1 | 1 | , | 1 | 1 |

${ }^{1}$ Note: $K$ factors are applied to member segment lengths. K-braces without inner supporting members will have the $K$ factor in the out-ofplane direction applied to the overall length.

## Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | U | Net Width Deduct in | U | Net Width Deduct in | U |
| $\begin{gathered} \hline \text { T1 130.000- } \\ 120.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T2 120.000- } \\ 100.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T3 100.000- } \\ 80.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |

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| Tower Elevation ft | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in |  | Net <br> Width Deduct in | $U$ | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net <br> Width Deduct in | $U$ | Net Width Deduct in | $U$ |
| $\begin{gathered} \text { T4 80.000- } \\ 60.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T5 60.000- } \\ 40.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T6 40.000- } \\ 20.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T7 } 20.000- \\ 0.000 \end{gathered}$ | 0.000 | 1 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |


| Tower Elevation ft | Redundant Horizontal |  | Redundant Diagonal |  | Redundant SubDiagonal |  | Redundant SubHorizontal |  | Redundant Vertical |  | Redundant Hip |  | Redundant Hip Diagonal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in |  | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ | Net Width Deduct in | $U$ |
| $\begin{gathered} \hline \text { T1 130.000- } \\ 120.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T2 120.000- } \\ 100.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T3 100.000- } \\ 80.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T4 80.000- } \\ 60.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T5 60.000- } \\ 40.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T6 40.000- } \\ 20.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |
| $\begin{gathered} \text { T7 20.000- } \\ 0.000 \end{gathered}$ | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 | 0.000 | 0.75 |

Tower Section Geometry (cont'd)

| Tower Elevation ft | Leg Connection Type | Leg |  | Diagonal |  | Top Girt |  | Bottom Girt |  | Mid Girt |  | Long Horizontal |  | Short Horizontal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bolt Size in | No. | Bolt Size in | No. | Bolt Size in |  | Bolt Size in | No. | Bolt Size in |  | $\begin{gathered} \text { Bolt Size } \\ \text { in } \end{gathered}$ | No. | Bolt Size in | No. |
| T1 130.000- | Flange | 0.750 | 4 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 120.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T2 120.000- | Flange | 0.875 | 4 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 100.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T3 100.000- | Flange | 1.000 | 4 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 80.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T4 80.000- | Flange | 1.000 | 4 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 60.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T5 60.000- | Flange | 1.000 | 6 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 40.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T6 40.000- | Flange | 1.000 | 6 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 20.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |
| T7 20.000- | Flange | 1.000 | 0 | 0.625 | 3 | 0.625 | 0 | 0.625 | 0 | 0.625 | 0 | 0.625 | 2 | 0.625 | 0 |
| 0.000 |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  | A325N |  |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement <br> ft | Face Offset in | Lateral Offset (Frac FW) | \# |  | Clear Spacin $g$ in | Width or Diameter in | Perimete $r$ in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Climbing | C | No | No | Af (CaAa) | 130.000 - | - | 0.4 | 1 | 1 | 3.000 | 3.000 |  | 8.40 |
| Ladder (Af) |  |  |  |  | 0.000 | 10.000 |  |  |  |  |  |  |  |
| Safety Line 3/8 | C | No | No | Ar (CaAa) | $\begin{gathered} 130.000- \\ 0.000 \end{gathered}$ | $10.000$ | 0.4 | 1 | 1 | 0.375 | 0.375 |  | 0.22 |
| LDF5- | C | No | No | Ar (CaAa) | $130.000-$ | 0.000 | -0.44 | 10 | 10 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| Feedline | C | No | No | Af (CaAa) | 130.000 - | 0.000 | -0.4 | 1 | 1 | 3.000 | 3.000 |  | 8.40 |
| Ladder (Af) |  |  |  |  | 0.000 |  |  |  |  |  |  |  |  |
| E60 | C | No | No | Ar (CaAa) | $117.000-$ | 0.000 | -0.375 | 1 | 1 | 1.000 | 2.200 |  | 1.10 |
|  |  |  |  |  | 107.000 |  |  |  |  |  |  |  |  |
| E65+E60 | C | No | No | Ar (CaAa) | $107.000-$ | 0.000 | -0.375 | 2 | 2 | 1.000 | 2.200 |  | 1.10 |
|  |  |  |  |  | 96.000 |  |  |  |  |  |  |  |  |
| E60+E65+E6 | C | No | No | Ar (CaAa) | 96.000 - | 0.000 | -0.375 | 3 | 3 | 1.000 | 2.200 |  | 1.10 |
| 0 |  |  |  |  | 86.000 |  |  |  |  |  |  |  |  |
| E60+E60+E6 | C | No | No | Ar (CaAa) | 86.000 - | 0.000 | -0.375 | 4 | 4 | 1.000 | 2.200 |  | 1.10 |
| 5+E60 |  |  |  |  | 71.000 |  |  |  |  |  |  |  |  |
| E65+E60+E6 | C | No | No | Ar (CaAa) | 71.000 - | 0.000 | -0.375 | 5 | 5 | 1.000 | 2.200 |  | 1.10 |
| 0+E65+E60 |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| HYBRIFLEX | A | No | No | Ar (CaAa) | 125.000 - | 0.000 | -0.42 | 3 | 3 | 1.000 | 1.980 |  | 0.82 |
| 1-5/8" |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| Feedline | A | No | No | Af (CaAa) | 130.000 - | 0.000 | -0.42 | 1 | 1 | 3.000 | 3.000 |  | 8.40 |
| Ladder (Af) |  |  |  |  | 0.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 113.000 - | 3.000 | -0.47 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | Ar (CaAa) | 113.000 - | 2.000 | -0.454 | 1 | 1 | 0.500 | 0.630 |  | 0.16 |
| 75A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 104.000 - | 1.500 | -0.47 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 98.000 - | 4.500 | -0.47 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 84.000 - | 2.000 | -0.46 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | Ar (CaAa) | 84.000 - | 2.000 | -0.445 | 1 | 1 | 0.500 | 0.625 |  | 0.15 |
| 50A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| Feedline | C | No | No | Af (CaAa) | 80.000 - | 0.000 | 0.42 | 1 | 1 | 3.000 | 3.000 |  | 8.40 |
| Ladder (Af) |  |  |  |  | 0.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | Ar (CaAa) | 77.000 - | 0.000 | 0.405 | 1 | 1 | 0.500 | 0.625 |  | 0.15 |
| 50A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF7-50A(1- | C | No | No | Ar (CaAa) | 77.000 - | 0.000 | 0.37 | 4 | 4 | 1.000 | 1.980 |  | 0.82 |
| 5/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 63.000 - | 0.000 | 0.44 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | Ar (CaAa) | 63.000 - | 0.000 | 0.415 | 1 | 1 | 0.500 | 0.625 |  | 0.15 |
| 50A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF7-50A(1- | C | No | No | Ar (CaAa) | 63.000 - | 0.000 | 0.47 | 3 | 3 | 1.000 | 1.980 |  | 0.82 |
| 5/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | 58.000 - | 2.000 | -0.438 | 1 | 1 | 0.500 | 0.630 |  | 0.16 |
| 75A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF4- | C | No | No | Ar (CaAa) | 54.000 - | 2.000 | -0.43 | 1 | 1 | 0.500 | 0.630 |  | 0.16 |
| 75A(1/2) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 43.000 - | 0.000 | 0.43 | 1 | 1 | 1.000 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF2- | C | No | No | $\operatorname{Ar}(\mathrm{CaAa})$ | 43.000 - | 2.000 | -0.418 | 1 | 1 | 0.440 | 0.440 |  | 0.08 |
| 50A(3/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| LDF2- | C | No | No | Ar (CaAa) | 43.000 - | 2.000 | -0.424 | 1 | 1 | 0.440 | 0.440 |  | 0.08 |
| 50A(3/8) |  |  |  |  | 7.000 |  |  |  |  |  |  |  |  |
| ****Proposed |  |  |  |  |  |  |  |  |  |  |  |  |  |
| LDF5- | C | No | No | Ar (CaAa) | 127.000 - | 1.500 | -0.412 | 2 | 1 | 0.500 | 1.030 |  | 0.33 |
| 50A(7/8) |  |  |  |  | 0.000 |  |  |  |  |  |  |  |  |
| E65 | C | No | No | Ar (CaAa) | $\begin{gathered} 87.000- \\ 0.000 \end{gathered}$ | 4.500 | -0.412 | 1 | 1 | 0.500 | 2.200 |  | 1.10 |
| ** |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ** |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow <br> Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | $C_{A} A_{A}$ $f t^{2} / f t$ | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ** |  |  |  |  |  |  |  |  |

Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio n \& Tower Elevation ft \& Face \& $A_{R}$

$f t^{2}$ \& $A_{F}$

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{T1} \& \multirow[t]{3}{*}{130.000-120.000} \& A \& 0.000 \& 0.000 \& 7.970 \& 0.000 \& 0.10 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 22.117 \& 0.000 \& 0.21 <br>
\hline \multirow[t]{3}{*}{T2} \& \multirow[t]{3}{*}{120.000-100.000} \& A \& 0.000 \& 0.000 \& 21.880 \& 0.000 \& 0.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 53.320 \& 0.000 \& 0.45 <br>
\hline \multirow[t]{3}{*}{T3} \& \multirow[t]{3}{*}{100.000-80.000} \& A \& 0.000 \& 0.000 \& 21.880 \& 0.000 \& 0.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 68.546 \& 0.000 \& 0.52 <br>
\hline \multirow[t]{3}{*}{T4} \& \multirow[t]{3}{*}{80.000-60.000} \& A \& 0.000 \& 0.000 \& 21.880 \& 0.000 \& 0.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 107.445 \& 0.000 \& 0.81 <br>
\hline \multirow[t]{3}{*}{T5} \& \multirow[t]{3}{*}{60.000-40.000} \& A \& 0.000 \& 0.000 \& 21.880 \& 0.000 \& 0.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 127.489 \& 0.000 \& 0.89 <br>
\hline \multirow[t]{3}{*}{T6} \& \multirow[t]{3}{*}{40.000-20.000} \& A \& 0.000 \& 0.000 \& 21.880 \& 0.000 \& 0.22 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 131.240 \& 0.000 \& 0.90 <br>
\hline \multirow[t]{3}{*}{T7} \& \multirow[t]{3}{*}{20.000-0.000} \& A \& 0.000 \& 0.000 \& 17.722 \& 0.000 \& 0.20 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 99.051 \& 0.000 \& 0.77 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
Tower Sectio \\
n
\end{tabular} \& Tower Elevation ft \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Ice Thickness in \& AR

$f t^{2}$ \& AF

$f t^{2}$ \& \[
$$
\begin{gathered}
C_{A} A_{A} \\
\text { In Face } \\
{f t^{2}}^{2}
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
\text { ft }^{2}
\end{gathered}
$$
\] \& Weight

K <br>
\hline \multirow[t]{3}{*}{T1} \& \multirow[t]{3}{*}{130.000-120.000} \& A \& \multirow[t]{3}{*}{2.628} \& 0.000 \& 0.000 \& 19.661 \& 0.000 \& 0.47 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 66.600 \& 0.000 \& 1.45 <br>
\hline \multirow[t]{3}{*}{T2} \& \multirow[t]{3}{*}{120.000-100.000} \& A \& \multirow[t]{3}{*}{2.594} \& 0.000 \& 0.000 \& 57.773 \& 0.000 \& 1.23 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 175.603 \& 0.000 \& 3.68 <br>
\hline \multirow[t]{3}{*}{T3} \& \multirow[t]{3}{*}{100.000-80.000} \& A \& \multirow[t]{3}{*}{2.543} \& 0.000 \& 0.000 \& 57.217 \& 0.000 \& 1.21 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 234.878 \& 0.000 \& 4.67 <br>
\hline \multirow[t]{3}{*}{T4} \& \multirow[t]{3}{*}{80.000-60.000} \& A \& \multirow[t]{3}{*}{2.480} \& 0.000 \& 0.000 \& 56.537 \& 0.000 \& 1.17 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 346.446 \& 0.000 \& 6.85 <br>
\hline \multirow[t]{3}{*}{T5} \& \multirow[t]{3}{*}{60.000-40.000} \& A \& \multirow[t]{3}{*}{2.398} \& 0.000 \& 0.000 \& 55.653 \& 0.000 \& 1.13 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 423.737 \& 0.000 \& 7.97 <br>
\hline \multirow[t]{3}{*}{T6} \& \multirow[t]{3}{*}{40.000-20.000} \& A \& \multirow[t]{3}{*}{2.278} \& 0.000 \& 0.000 \& 54.369 \& 0.000 \& 1.07 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 442.797 \& 0.000 \& 7.97 <br>
\hline \multirow[t]{3}{*}{T7} \& \multirow[t]{3}{*}{20.000-0.000} \& A \& \multirow[t]{3}{*}{2.041} \& 0.000 \& 0.000 \& 40.044 \& 0.000 \& 0.80 <br>
\hline \& \& B \& \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& \& C \& \& 0.000 \& 0.000 \& 305.012 \& 0.000 \& 5.27 <br>
\hline
\end{tabular}

## Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{Z}$ | $C P_{X}$ <br> Ice <br> in | $C P_{Z}$ <br> Ice <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ft | in | in | 9.223 |  |  |
|  | T1 | $130.000-120.000$ | 3.384 | 8.185 | 3.532 |
| T2 | $120.000-100.000$ | 4.494 | 10.970 | 7.168 | 14.311 |
| T3 | $100.000-80.000$ | 9.740 | 13.955 | 14.807 | 19.312 |
| T4 | $80.000-60.000$ | 5.496 | 20.381 | 10.628 | 27.371 |
| T5 | $60.000-40.000$ | 1.358 | 24.024 | 6.546 | 33.538 |
| T6 | $40.000-20.000$ | 1.534 | 26.372 | 8.501 | 38.194 |
| T7 | $20.000-0.000$ | -0.374 | 24.870 | 5.731 | 36.017 |

Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} \hline K_{a} \\ \text { No Ice } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 1 | Climbing Ladder (Af) | $\begin{array}{r} 120.00- \\ 130.00 \end{array}$ | 0.6000 | 0.5472 |
| T1 | 2 | Safety Line 3/8 | $\begin{array}{r} 120.00- \\ 130.00 \end{array}$ | 0.6000 | 0.5472 |
| T1 | 3 | LDF5-50A(7/8) | $\begin{array}{r} 120.00- \\ 130.00 \end{array}$ | 0.6000 | 0.5472 |
| T1 | 4 | Feedline Ladder (Af) | $120.00-$ | 0.6000 | 0.5472 |
| T1 | 10 | HYBRIFLEX 1-5/8" | $120.00-$ | 0.6000 | 0.5472 |
| T1 | 13 | Feedline Ladder (Af) | 120.00- | 0.6000 | 0.5472 |
| T1 | 32 | LDF5-50A(7/8) | 120.00- | 0.6000 | 0.5472 |
|  |  |  | 127.00 |  |  |
| T2 | 1 | Climbing Ladder (Af) | $\begin{array}{r} 100.00- \\ 120.00 \end{array}$ | 0.6000 | 0.6000 |
| T2 | 2 | Safety Line 3/8 | 100.00- | 0.6000 | 0.6000 |
| T2 | 3 | LDF5-50A(7/8) | 120.00 | 0.6000 | 0.6000 |
|  |  |  | 120.00 |  |  |
| T2 | 4 | Feedline Ladder (Af) | 100.00- | 0.6000 | 0.6000 |
|  |  |  | $\begin{array}{r} 120.00 \\ 107.00-1 \end{array}$ |  |  |
| T2 | 5 | E60 | $\begin{array}{r} 107.00- \\ 117.00 \end{array}$ | 0.6000 | 0.6000 |
| T2 | 6 | E65+E60 | 100.00- | 0.6000 | 0.6000 |
|  |  |  | 107.00- |  |  |
| T2 | 10 | HYBRIFLEX 1-5/8" | $\begin{array}{r} 100.00- \\ 120.00 \end{array}$ | 0.6000 | 0.6000 |
| T2 | 13 | Feedline Ladder (Af) | 100.00- | 0.6000 | 0.6000 |
|  |  |  | 120.00 |  |  |
| T2 | 14 | LDF5-50A(7/8) | $\begin{array}{r} 100.00- \\ 113.00 \end{array}$ | 0.6000 | 0.6000 |
| T2 | 15 | LDF4-75A(1/2) | 100.00- | 0.6000 | 0.6000 |
|  |  |  | 113.00 |  |  |
| T2 | 16 | LDF5-50A(7/8) | $\begin{array}{r} 100.00- \\ 104.00 \end{array}$ | 0.6000 | 0.6000 |
| T2 | 32 | LDF5-50A(7/8) | 100.00- | 0.6000 | 0.6000 |
| T3 | 1 | Climbing Ladder (Af) | 120.00 | 0.6000 | 0.6000 |
|  |  | Cirning Ladder (A) | 100.00 |  |  |
| T3 | 2 | Safety Line 3/8 | $80.00-$ | 0.6000 | 0.6000 |
| T3 |  |  | 100.00 |  |  |
|  |  | LDF5-50A(7/8) | $\begin{aligned} & 80.00-0 \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T3 | 4 | Feedline Ladder (Af) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 6 | E65+E60 | $\begin{aligned} & 96.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 7 | $E 60+E 65+E 60$ | $86.00-$ 96.00 | 0.6000 | 0.6000 |
| T3 | 8 | $E 60+E 60+E 65+E 60$ | $\begin{array}{r} 80.00- \\ 86.00 \end{array}$ | 0.6000 | 0.6000 |
| T3 | 10 | HYBRIFLEX 1-5/8" | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 13 | Feedline Ladder (Af) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 14 | LDF5-50A(7/8) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 15 | LDF4-75A(1/2) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 16 | LDF5-50A(7/8) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 17 | LDF5-50A(7/8) | 80.00- | 0.6000 | 0.6000 |
| T3 | 18 | LDF5-50A(7/8) | $\begin{array}{r} 80.00- \\ 84.00 \end{array}$ | 0.6000 | 0.6000 |
| T3 | 19 | LDF4-50A(1/2) | $80.00-$ 84.00 | 0.6000 | 0.6000 |
| T3 | 32 | LDF5-50A(7/8) | $\begin{aligned} & 80.00- \\ & 100.00 \end{aligned}$ | 0.6000 | 0.6000 |
| T3 | 33 | E65 | $80.00-$ 87.00 | 0.6000 | 0.6000 |
| T4 | 1 | Climbing Ladder (Af) | $\begin{array}{r} 60.00- \\ 80.00 \end{array}$ | 0.6000 | 0.6000 |
| T4 | 2 | Safety Line 3/8 | $80.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 3 | LDF5-50A(7/8) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 4 | Feedline Ladder (Af) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 8 | $E 60+E 60+E 65+E 60$ | $\begin{array}{r} 71.00- \\ 80.00 \end{array}$ | 0.6000 | 0.6000 |
| T4 | 9 | E65+E60+E60+E65+E60 | $60.00-$ 71.00 | 0.6000 | 0.6000 |
| T4 | 10 | HYBRIFLEX 1-5/8" | $60.00-1$ | 0.6000 | 0.6000 |
| T4 | 13 | Feedline Ladder (Af) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 14 | LDF5-50A(7/8) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 15 | LDF4-75A(1/2) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 16 | LDF5-50A(7/8) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 17 | LDF5-50A(7/8) | $60.00-1$ | 0.6000 | 0.6000 |
| T4 | 18 | LDF5-50A(7/8) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 19 | LDF4-50A(1/2) | $60.00-$ 80.00 | 0.6000 | 0.6000 |
| T4 | 20 | Feedline Ladder (Af) | $60.00-1$ | 0.6000 | 0.6000 |
| T4 | 21 | LDF4-50A(1/2) | $60.00-$ 77.00 | 0.6000 | 0.6000 |
| T4 | 22 | LDF7-50A(1-5/8) | $\begin{array}{r} 60.00- \\ 77.00 \end{array}$ | 0.6000 | 0.6000 |
| T4 | 23 | LDF5-50A(7/8) | $60.00-1$ | 0.6000 | 0.6000 |
| T4 | 24 | LDF4-50A(1/2) | $60.00-$ 63.00 | 0.6000 | 0.6000 |
| T4 | 25 | LDF7-50A(1-5/8) | $60.00-$ 63.00 | 0.6000 | 0.6000 |
| T4 | 32 | LDF5-50A(7/8) | $60.00-$ | 0.6000 | 0.6000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ <br> No Ice | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T4 | 33 | E65 | $\begin{array}{r} 80.00 \\ 60.00- \\ 80.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 1 | Climbing Ladder (Af) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 2 | Safety Line 3/8 | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 3 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 4 | Feedline Ladder (Af) | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T5 | 9 | $E 65+E 60+E 60+E 65+E 60$ | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 10 | HYBRIFLEX 1-5/8" | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T5 | 13 | Feedline Ladder (Af) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 14 | LDF5-50A(7/8) | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T5 | 15 | LDF4-75A(1/2) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 16 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 17 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 18 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 19 | LDF4-50A(1/2) | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T5 | 20 | Feedline Ladder (Af) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 21 | LDF4-50A(1/2) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 22 | LDF7-50A(1-5/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 23 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 24 | LDF4-50A(1/2) | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T5 | 25 | LDF7-50A(1-5/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 26 | LDF4-75A(1/2) | $\begin{array}{r} 40.00- \\ 58.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 27 | LDF4-75A(1/2) | 40.00-1 54.00 | 0.6000 | 0.6000 |
| T5 | 28 | LDF5-50A(7/8) | $40.00-$ 43.00 | 0.6000 | 0.6000 |
| T5 | 29 | LDF2-50A(3/8) | $40.00-$ 43.00 | 0.6000 | 0.6000 |
| T5 | 30 | LDF2-50A(3/8) | $\begin{array}{r} 40.00- \\ 43.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 32 | LDF5-50A(7/8) | $\begin{array}{r} 40.00- \\ 60.00 \end{array}$ | 0.6000 | 0.6000 |
| T5 | 33 | E65 | $40.00-$ 60.00 | 0.6000 | 0.6000 |
| T6 | 1 | Climbing Ladder (Af) | $\begin{array}{r} 20.00- \\ 40.00 \end{array}$ | 0.6000 | 0.6000 |
| T6 | 2 | Safety Line 3/8 | $20.00-1$ | 0.6000 | 0.6000 |
| T6 | 3 | LDF5-50A(7/8) | $20.00-1$ | 0.6000 | 0.6000 |
| T6 | 4 | Feedline Ladder (Af) | 20.00- | 0.6000 | 0.6000 |
| T6 | 9 | $E 65+E 60+E 60+E 65+E 60$ | 20.00- | 0.6000 | 0.6000 |
| T6 | 10 | HYBRIFLEX 1-5/8" | $\begin{array}{r} 20.00- \\ 40.00 \end{array}$ | 0.6000 | 0.6000 |
| T6 | 13 | Feedline Ladder (Af) | $\begin{array}{r} 20.00- \\ 40.00 \end{array}$ | 0.6000 | 0.6000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T6 | 14 | LDF5-50A(7/8) | $\begin{array}{r} 20.00- \\ 40.00 \end{array}$ | 0.6000 | 0.6000 |
| T6 | 15 | LDF4-75A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 16 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 17 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 18 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 19 | LDF4-50A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 20 | Feedline Ladder (Af) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 21 | LDF4-50A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 22 | LDF7-50A(1-5/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 23 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 24 | LDF4-50A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 25 | LDF7-50A(1-5/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 26 | LDF4-75A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 27 | LDF4-75A(1/2) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 28 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 29 | LDF2-50A(3/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 30 | LDF2-50A(3/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 32 | LDF5-50A(7/8) | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T6 | 33 | E65 | $20.00-$ 40.00 | 0.6000 | 0.6000 |
| T7 | 1 | Climbing Ladder (Af) | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 2 | Safety Line 3/8 | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 3 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 4 | Feedline Ladder (Af) | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 9 | E65+E60+E60+E65+E60 | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 10 | HYBRIFLEX 1-5/8" | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 13 | Feedline Ladder (Af) | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 14 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 15 | LDF4-75A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 16 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 17 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 18 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 19 | LDF4-50A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 20 | Feedline Ladder (Af) | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 21 | LDF4-50A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 22 | LDF7-50A(1-5/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 23 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 24 | LDF4-50A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 25 | LDF7-50A(1-5/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 26 | LDF4-75A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 27 | LDF4-75A(1/2) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 28 | LDF5-50A(7/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 29 | LDF2-50A(3/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 30 | LDF2-50A(3/8) | 7.00-20.00 | 0.6000 | 0.6000 |
| T7 | 32 | LDF5-50A(7/8) | 0.00-20.00 | 0.6000 | 0.6000 |
| T7 | 33 | E65 | 0.00-20.00 | 0.6000 | 0.6000 |

# Discrete Tower Loads 

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: Horz \\
Lateral Vert ft ft ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustmen \(t\) \\
0
\end{tabular} \& Placement

ft \& \& \begin{tabular}{l}
$C_{A} A_{A}$ Front <br>
$f t^{2}$

 \& 

$C_{A} A_{A}$ Side <br>
$f t^{2}$
\end{tabular} \& Weight

K <br>
\hline \multirow[t]{4}{*}{Sector Mount [SM 501-3]} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 20.430 \& 20.430 \& 0.90 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 30.050 \& 30.050 \& 1.28 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 40.280 \& 40.280 \& 1.80 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 64.650 \& 64.650 \& 3.23 <br>

\hline \multirow[t]{4}{*}{(2) 14 'x2.5" Horizontal Pipe} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 4.169 \& 0.024 \& 0.08 <br>
\hline \& \& \& -4.000 \& \& \& 1/2" \& 5.651 \& 0.097 \& 0.11 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 7.150 \& 0.171 \& 0.15 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 10.198 \& 0.318 \& 0.26 <br>

\hline \multirow[t]{4}{*}{(2) 14'x2.5" Horizontal Pipe} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 4.169 \& 0.024 \& 0.08 <br>
\hline \& \& \& -4.000 \& \& \& 1/2" \& 5.651 \& 0.097 \& 0.11 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 7.150 \& 0.171 \& 0.15 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 10.198 \& 0.318 \& 0.26 <br>

\hline \multirow[t]{4}{*}{(2) 14'x2.5" Horizontal Pipe} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 4.169 \& 0.024 \& 0.08 <br>
\hline \& \& \& -4.000 \& \& \& 1/2" \& 5.651 \& 0.097 \& 0.11 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 7.150 \& 0.171 \& 0.15 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 10.198 \& 0.318 \& 0.26 <br>

\hline \multirow[t]{4}{*}{6'6"x3.5" Mount Pipe} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 2.161 \& 2.161 \& 0.02 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.554 \& 2.554 \& 0.03 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 2.957 \& 2.957 \& 0.06 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 3.790 \& 3.790 \& 0.11 <br>

\hline \multirow[t]{4}{*}{3' Dia 12' Omni} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 3.600 \& 3.600 \& 0.02 <br>
\hline \& \& \& -2.000 \& \& \& 1/2" \& 4.833 \& 4.833 \& 0.05 <br>
\hline \& \& \& \multirow[t]{2}{*}{8.000} \& \& \& Ice \& 6.083 \& 6.083 \& 0.08 <br>

\hline \& \& \& \& \& \& | 1" Ice |
| :--- |
| 2" Ice | \& 8.017 \& 8.017 \& 0.17 <br>

\hline \multirow[t]{4}{*}{2" Dia 10' Omni} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Leg} \& 3.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 2.000 \& 2.000 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 3.030 \& 3.030 \& 0.03 <br>
\hline \& \& \& \multirow[t]{2}{*}{7.000} \& \& \& Ice \& 4.060 \& 4.060 \& 0.04 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 6.120 \& 6.120 \& 0.07 <br>

\hline \multirow[t]{4}{*}{2.38" Dia 21' Omni} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 4.998 \& 4.998 \& 0.01 <br>
\hline \& \& \& 1.000 \& \& \& 1/2" \& 7.126 \& 7.126 \& 0.05 <br>
\hline \& \& \& \multirow[t]{2}{*}{12.000} \& \& \& Ice \& 9.271 \& 9.271 \& 0.10 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 13.611 \& 13.611 \& 0.24 <br>

\hline \multirow[t]{4}{*}{2.5" Dia 16' Omni} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 0.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{127.000} \& No Ice \& 4.000 \& 4.000 \& 0.03 <br>
\hline \& \& \& 1.000 \& \& \& 1/2" \& 5.629 \& 5.629 \& 0.06 <br>
\hline \& \& \& 9.000 \& \& \& Ice \& 7.275 \& 7.275 \& 0.10 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$ \& 10.617 \& 10.617 \& 0.21 <br>

\hline \multirow[t]{5}{*}{18' x 3' Dia Omni} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{127.000} \& No Ice \& 5.400 \& 5.400 \& 0.14 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 7.233 \& 7.233 \& 0.18 <br>
\hline \& \& \& 11.000 \& \& \& Ice \& 9.083 \& 9.083 \& 0.23 <br>
\hline \& \& \& \& \& \& 1" Ice \& 12.833 \& 12.833 \& 0.36 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{2.5' Dia 16' Omni} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 1.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{127.000} \& No Ice \& 4.000 \& 4.000 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 5.629 \& 5.629 \& 0.06 <br>
\hline \& \& \& 10.000 \& \& \& Ice \& 7.275 \& 7.275 \& 0.10 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 10.617 \& 10.617 \& 0.21 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{2" Dia 24' Omni} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{127.000} \& No Ice \& 4.800 \& 4.800 \& 0.05 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 7.225 \& 7.225 \& 0.08 <br>
\hline \& \& \& 14.000 \& \& \& Ice \& 9.667 \& 9.667 \& 0.13 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 14.600 \& 14.600 \& 0.28 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline 2" Dia 25' Omni \& C \& From Leg \& 0.000 \& 0.000 \& 127.000 \& No Ice \& 5.000 \& 5.000 \& 0.05 <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\hline \text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
\(f t\)
\(f t\)
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front $f t^{2}$ \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

K <br>
\hline \multirow{7}{*}{10"x8"x3" TMA} \& \multirow{7}{*}{C} \& \multirow{7}{*}{From Leg} \& 0.000 \& \multirow{7}{*}{0.000} \& \multirow{7}{*}{127.000} \& 1/2" \& 7.525 \& 7.525 \& 0.09 <br>
\hline \& \& \& 14.500 \& \& \& Ice \& 10.067 \& 10.067 \& 0.14 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 15.200 \& 15.200 \& 0.30 <br>

\hline \& \& \& 2.000 \& \& \& No Ice \& 1.000 \& 0.410 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 1.131 \& 0.510 \& 0.02 <br>
\hline \& \& \& \multirow[t]{2}{*}{2.000} \& \& \& Ice \& 1.270 \& 0.618 \& 0.03 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 1.570 \& 0.853 \& 0.05 <br>

\hline \multicolumn{10}{|l|}{*** ${ }^{\text {a }}$} <br>
\hline \multirow[t]{5}{*}{Sector Mount [SM 502-3]} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 29.820 \& 29.820 \& 1.67 <br>
\hline \& \& \& \& \& \& 1/2" \& 42.210 \& 42.210 \& 2.27 <br>
\hline \& \& \& \& \& \& Ice \& 54.430 \& 54.430 \& 3.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 78.490 \& 78.490 \& 5.18 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAA4L24 43-UNA20_TIA w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 20.480 \& 10.869 \& 0.20 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 21.231 \& 12.393 \& 0.34 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 21.990 \& 13.942 \& 0.48 <br>
\hline \& \& \& \& \& \& $1{ }^{1 /}$ Ice \& 23.444 \& 16.291 \& 0.81 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAA4L24_43-UNA20_TIA w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 20.480 \& 10.869 \& 0.20 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 21.231 \& 12.393 \& 0.34 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 21.990 \& 13.942 \& 0.48 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 23.444 \& 16.291 \& 0.81 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{APXVAA4L24_43-UNA20_TIA w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 20.480 \& 10.869 \& 0.20 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 21.231 \& 12.393 \& 0.34 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 21.990 \& 13.942 \& 0.48 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 23.444 \& 16.291 \& 0.81 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR6449 B41 TMOBILE_TIA w/Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 5.870 \& 3.270 \& 0.13 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 6.233 \& 3.728 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 6.606 \& 4.203 \& 0.23 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 7.382 \& 5.200 \& 0.36 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR6449 B41_TMOBILE_TIA w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 5.870 \& 3.270 \& 0.13 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 6.233 \& 3.728 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 6.606 \& 4.203 \& 0.23 <br>
\hline \& \& \& \& \& \& $1{ }^{1 / \mathrm{Ice}}$ \& 7.382 \& 5.200 \& 0.36 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR6449 B41_TMOBILE_TIA w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 5.870 \& 3.270 \& 0.13 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 6.233 \& 3.728 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 6.606 \& 4.203 \& 0.23 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.382 \& 5.200 \& 0.36 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR 32 w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 3.760 \& 3.150 \& 0.12 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 4.120 \& 3.490 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 4.480 \& 3.840 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{1 /}$ Ice \& 5.240 \& 4.580 \& 0.41 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR 32 w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 3.760 \& 3.150 \& 0.12 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 4.120 \& 3.490 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 4.480 \& 3.840 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 5.240 \& 4.580 \& 0.41 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{AIR 32 w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 3.760 \& 3.150 \& 0.12 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 4.120 \& 3.490 \& 0.18 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 4.480 \& 3.840 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 5.240 \& 4.580 \& 0.41 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4415} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 1.856 \& 0.683 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.027 \& 0.801 \& 0.06 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 2.204 \& 0.925 \& 0.07 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.582 \& 1.196 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral Vert ft ft
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front $f t^{2}$ \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

K <br>
\hline \multirow[t]{4}{*}{4415} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Face} \& 3.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 1.856 \& 0.683 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.027 \& 0.801 \& 0.06 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 2.204 \& 0.925 \& 0.07 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 2.582 \& 1.196 \& 0.11 <br>

\hline \multirow[t]{4}{*}{4415} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 3.000 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{125.000} \& No Ice \& 1.856 \& 0.683 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.027 \& 0.801 \& 0.06 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 2.204 \& 0.925 \& 0.07 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 2.582 \& 1.196 \& 0.11 <br>

\hline \multirow[t]{5}{*}{4449} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 1.969 \& 1.402 \& 0.07 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.145 \& 1.558 \& 0.09 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.329 \& 1.720 \& 0.11 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 2.719 \& 2.068 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4449} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 1.969 \& 1.402 \& 0.07 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.145 \& 1.558 \& 0.09 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.329 \& 1.720 \& 0.11 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 2.719 \& 2.068 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4449} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{125.000} \& No Ice \& 1.969 \& 1.402 \& 0.07 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.145 \& 1.558 \& 0.09 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.329 \& 1.720 \& 0.11 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.719 \& 2.068 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{4}{*}{10' Hori. 5"x5" Tube} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Face} \& \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{117.000} \& No Ice \& 5.000 \& 0.208 \& 0.16 <br>

\hline \& \& \& $$
0.000
$$ \& \& \& 1/2" \& 5.712 \& 0.268 \& 0.20 <br>

\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 6.423 \& 0.334 \& 0.25 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 7.847 \& 0.490 \& 0.33 <br>

\hline \multirow[t]{5}{*}{4' x 2" Horizontal Face Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{117.000} \& No Ice \& 0.870 \& 0.010 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 1.110 \& 0.050 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.370 \& 0.100 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.900 \& 0.240 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6' x 3" Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{117.000} \& No Ice \& 1.767 \& 1.767 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.04 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.06 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 3.272 \& 3.272 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Side Arm Mount [SO 3061]} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{113.000} \& \& \& 2.260 \& <br>

\hline \& \& \& $$
0.000
$$ \& \& \& 1/2" \& 0.810 \& 3.830 \& 0.06 <br>

\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.230 \& 5.480 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 2.080 \& 9.370 \& 0.19 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>

\hline \multirow[t]{4}{*}{PD1142-1} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& $$
\begin{aligned}
& 4.000 \\
& 0.000
\end{aligned}
$$ \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{113.000} \& No Ice \& \[

$$
\begin{aligned}
& 1.316 \\
& 2
\end{aligned}
$$
\] \& 1.316

3.210 \& 0.01
0.02 <br>
\hline \& \& \& 7.000 \& \& \& Ice \& 5.121 \& 5.121 \& 0.05 <br>
\hline \& \& \& \& \& \& $1{ }^{1 / \mathrm{Ic}}$ \& 8.993 \& 8.993 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{10' Hori. 5"x5" Tube} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{107.000} \& No Ice \& 5.000 \& 0.208 \& 0.16 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 5.712 \& 0.268 \& 0.20 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 6.423 \& 0.334 \& 0.25 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.847 \& 0.490 \& 0.33 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{10' Hori. 5"x5" Tube} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{107.000} \& No Ice \& 5.000 \& 0.208 \& 0.16 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 5.712 \& 0.268 \& 0.20 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 6.423 \& 0.334 \& 0.25 <br>
\hline \& \& \& \& \& \& $1{ }^{1 / \mathrm{Ic}}$ \& 7.847 \& 0.490 \& 0.33 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6'x2" Horizontal Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Face} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{107.000} \& No Ice \& 1.425 \& 0.047 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 1.842 \& 0.077 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 2.266 \& 0.115 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.137 \& 0.212 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
\(f t\)
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& \begin{tabular}{l}
$C_{A} A_{A}$ Front <br>
$f t^{2}$

 \& 

$C_{A} A_{A}$ Side <br>
$f t^{2}$
\end{tabular} \& Weight

K <br>
\hline \multirow[t]{4}{*}{6' x 3" Mount Pipe} \& \multirow[t]{4}{*}{B} \& \multirow[t]{4}{*}{From Leg} \& 0.500 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{107.000} \& No Ice \& 1.767 \& 1.767 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.04 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.06 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 3.272 \& 3.272 \& 0.11 <br>

\hline \multirow[t]{5}{*}{Side Arm Mount [SO 3061]} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{104.000} \& No Ice \& 0.410 \& 2.260 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 0.810 \& 3.830 \& 0.06 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.230 \& 5.480 \& 0.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 2.080 \& 9.370 \& 0.19 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{PD1142-1} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{104.000} \& No Ice \& 1.316 \& 1.316 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 3.210 \& 3.210 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{7.000} \& \& \& Ice \& 5.121 \& 5.121 \& 0.05 <br>
\hline \& \& \& \& \& \& 1" Ice \& 8.993 \& 8.993 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>

\hline \multirow[t]{10}{*}{| Side Arm Mount [SO 3061] |
| :--- |
| 3' Yagi |} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{98.000} \& No Ice \& 0.410 \& 2.260 \& 0.04 <br>

\hline \& \& \& 0.000 \& \& \& 1/2" \& 0.810 \& 3.830 \& 0.06 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.230 \& 5.480 \& 0.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 2.080 \& 9.370 \& 0.19 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 4.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{98.000} \& No Ice \& 2.083 \& 2.083 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 3.787 \& 3.787 \& 0.05 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 5.517 \& 5.517 \& 0.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 9.055 \& 9.055 \& 0.18 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{12' Hori. 5"x5" Tube} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Face} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{96.000} \& No Ice \& 6.000 \& 0.208 \& 0.19 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 6.854 \& 0.268 \& 0.24 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 7.708 \& 0.334 \& 0.30 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 9.416 \& 0.490 \& 0.40 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{4' x 2" Horizontal Face Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{96.000} \& No Ice \& 0.870 \& 0.010 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 1.110 \& 0.050 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.370 \& 0.100 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.900 \& 0.240 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6' x 3" Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{96.000} \& No Ice \& 1.767 \& 1.767 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.04 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.272 \& 3.272 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{8' Horizontal x 2" Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Face} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{86.000} \& No Ice \& 1.900 \& 0.047 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.450 \& 0.077 \& 0.05 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 3.008 \& 0.115 \& 0.07 <br>
\hline \& \& \& \& \& \& 1" Ice \& 4.145 \& 0.212 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{6' x 3" Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{86.000} \& No Ice \& 1.767 \& 1.767 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.04 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.272 \& 3.272 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{PD1142-1} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 4.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{84.000} \& No Ice \& 1.316 \& 1.316 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 3.210 \& 3.210 \& 0.02 <br>
\hline \& \& \& 7.000 \& \& \& Ice \& 5.121 \& 5.121 \& 0.05 <br>
\hline \& \& \& \& \& \& $1{ }^{1 /}$ Ice \& 8.993 \& 8.993 \& 0.14 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Side Arm Mount [SO 3061]} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{84.000} \& No Ice \& 0.410 \& 2.260 \& 0.04 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 0.810 \& 3.830 \& 0.06 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 1.230 \& 5.480 \& 0.09 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 2.080 \& 9.370 \& 0.19 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3' Yagi} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{84.000} \& No Ice \& 2.083 \& 2.083 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 3.787 \& 3.787 \& 0.05 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 5.517 \& 5.517 \& 0.09 <br>
\hline \& \& \& \& \& \& 1" Ice \& 9.055 \& 9.055 \& 0.18 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Offset Type \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
ft \\
\(f t\)
\(f t\)
\end{tabular} \& Azimuth Adjustmen \(t\) \& Placement

ft \& \& $C_{A} A_{A}$ Front $f t^{2}$ \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

K <br>
\hline \multirow[t]{4}{*}{4' x 2" Pipe Mount} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 0.500 \& \multirow[t]{4}{*}{0.000} \& \multirow[t]{4}{*}{84.000} \& No Ice \& 0.785 \& 0.785 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 1.028 \& 1.028 \& 0.04 <br>
\hline \& \& \& \multirow[t]{2}{*}{0.000} \& \& \& Ice \& 1.281 \& 1.281 \& 0.04 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 1.814 \& 1.814 \& 0.07 <br>

\hline \multirow[t]{5}{*}{Sector Mount [SM 402-1]} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 9.720 \& 7.050 \& 0.28 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 13.660 \& 9.870 \& 0.40 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 17.550 \& 12.660 \& 0.57 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 25.280 \& 18.130 \& 1.01 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{SBNH-1D6565A w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 5.599 \& 4.774 \& 0.06 <br>
\hline \& \& \& -6.000 \& \& \& 1/2" \& 6.007 \& 5.446 \& 0.11 <br>
\hline \& \& \& 1.000 \& \& \& Ice \& 6.417 \& 6.095 \& 0.16 <br>
\hline \& \& \& \& \& \& 1" Ice \& 7.263 \& 7.443 \& 0.30 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia 20' Omni} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 4.000 \& 4.000 \& 0.06 <br>
\hline \& \& \& -6.000 \& \& \& 1/2" \& 6.000 \& 6.000 \& 0.10 <br>
\hline \& \& \& \multirow[t]{3}{*}{-10.000} \& \& \& Ice \& 8.000 \& 8.000 \& 0.14 <br>
\hline \& \& \& \& \& \& $1{ }^{1 /}$ Ice \& 12.000 \& 12.000 \& 0.23 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia. 6' Omni} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 1.767 \& 1.767 \& 0.05 <br>
\hline \& \& \& 6.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.06 <br>
\hline \& \& \& \multirow[t]{3}{*}{3.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.08 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 3.272 \& 3.272 \& 0.12 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia 20' Omni} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 4.000 \& 4.000 \& 0.06 <br>
\hline \& \& \& 6.000 \& \& \& 1/2" \& 6.000 \& 6.000 \& 0.10 <br>
\hline \& \& \& \multirow[t]{3}{*}{-10.000} \& \& \& Ice \& 8.000 \& 8.000 \& 0.14 <br>
\hline \& \& \& \& \& \& 1" Ice \& 12.000 \& 12.000 \& 0.23 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{TMA} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{77.000} \& No Ice \& 0.600 \& 0.407 \& 0.01 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 0.704 \& 0.497 \& 0.02 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 0.815 \& 0.593 \& 0.02 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.059 \& 0.815 \& 0.04 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{$6^{\prime} \times 3$ " Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 0.500 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{71.000} \& No Ice \& 1.767 \& 1.767 \& 0.03 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 2.129 \& 2.129 \& 0.04 <br>
\hline \& \& \& \multirow[t]{3}{*}{0.000} \& \& \& Ice \& 2.501 \& 2.501 \& 0.06 <br>
\hline \& \& \& \& \& \& 1" Ice \& 3.272 \& 3.272 \& 0.11 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Sector Mount [SM 402-1]} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 0.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{63.000} \& No Ice \& 9.720 \& 7.050 \& 0.28 <br>
\hline \& \& \& 0.000 \& \& \& 1/2" \& 13.660 \& 9.870 \& 0.40 <br>
\hline \& \& \& 0.000 \& \& \& Ice \& 17.550 \& 12.660 \& 0.57 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 25.280 \& 18.130 \& 1.01 <br>
\hline \& \& \& \& \& \& 2 " Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia 20' Omni} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{63.000} \& No Ice \& 4.000 \& 4.000 \& 0.06 <br>
\hline \& \& \& -6.000 \& \& \& 1/2" \& 6.000 \& 6.000 \& 0.10 <br>
\hline \& \& \& 10.000 \& \& \& Ice \& 8.000 \& 8.000 \& 0.14 <br>
\hline \& \& \& \& \& \& $1{ }^{1 / \mathrm{Ic}}$ \& 12.000 \& 12.000 \& 0.23 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia 20' Omni} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{63.000} \& No Ice \& 4.000 \& 4.000 \& 0.06 <br>
\hline \& \& \& -6.000 \& \& \& 1/2" \& 6.000 \& 6.000 \& 0.10 <br>
\hline \& \& \& -10.000 \& \& \& Ice \& 8.000 \& 8.000 \& 0.14 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 12.000 \& 12.000 \& 0.23 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{Diamond X-500A} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{63.000} \& No Ice \& 4.998 \& 4.998 \& 0.01 <br>
\hline \& \& \& 6.000 \& \& \& 1/2" \& 7.126 \& 7.126 \& 0.05 <br>
\hline \& \& \& 10.000 \& \& \& Ice \& 9.271 \& 9.271 \& 0.10 <br>
\hline \& \& \& \& \& \& $1{ }^{\text {" Ice }}$ \& 13.611 \& 13.611 \& 0.24 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \multirow[t]{5}{*}{3" Dia 20' Omni} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.000 \& \multirow[t]{5}{*}{0.000} \& \multirow[t]{5}{*}{63.000} \& No Ice \& 4.000 \& 4.000 \& 0.06 <br>
\hline \& \& \& 6.000 \& \& \& 1/2" \& 6.000 \& 6.000 \& 0.10 <br>
\hline \& \& \& \multirow[t]{3}{*}{-10.000} \& \& \& Ice \& 8.000 \& 8.000 \& 0.14 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 12.000 \& 12.000 \& 0.23 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline
\end{tabular}



| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ <br> 0 | Placement |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A} A_{A}$ Side $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.000 |  |  | Ice | 5.460 | 5.460 | 0.17 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" Ice } \\ & \text { 2" Ice } \end{aligned}$ | 8.820 | 8.820 | 0.23 |
| ****Proposed*** |  |  |  |  |  |  |  |  |  |
| 876F-70-2 4-Bay Dipole | C | From Face | 0.000 | 0.000 | 130.000 | No Ice | 10.680 | 10.680 | 0.13 |
|  |  |  | 0.000 |  |  | 1/2" | 17.160 | 17.160 | 0.17 |
|  |  |  | 10.000 |  |  | Ice | 23.640 | 23.640 | 0.21 |
|  |  |  |  |  |  | 1" Ice 2" Ice | 36.600 | 36.600 | 0.29 |
| R5-LL [PM 602-1] | A | From Leg | 0.500 | 0.000 | 87.000 | No Ice | 5.250 | 1.580 | 0.09 |
|  |  |  | 0.000 |  |  | 1/2" | 6.500 | 1.950 | 0.12 |
|  |  |  | 0.000 |  |  | Ice | 7.750 | 2.320 | 0.14 |
|  |  |  |  |  |  | 1" Ice | 10.250 | 3.060 | 0.19 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| *** |  |  |  |  |  |  |  |  |  |
| ** |  |  |  |  |  |  |  |  |  |


| Dishes |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | Face or Leg | Dish <br> Type | Offset Type | Offsets: <br> Horz <br> Lateral Vert ft | Azimuth Adjustment | 3 dB <br> Beam <br> Width <br> 。 | Elevation | Outside Diameter <br> ft |  | Aperture Area <br> $f t^{2}$ | Weight |
| PA6-59 | A | Paraboloid | From | 0.500 | 0.000 |  | 117.000 | 6.000 | No Ice | 28.300 | 0.19 |
|  |  | w/Radome | Leg | 0.000 |  |  |  |  | 1/2" Ice | 29.050 | 0.33 |
|  |  |  |  | 0.000 |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 29.801 | 0.48 |
|  |  |  |  |  |  |  |  |  | 2" Ice | 31.302 | 0.78 |
| 6 FT Dish | B | Paraboloid | From | 0.500 | 0.000 |  | 107.000 | 6.000 | No Ice | 28.300 | 0.19 |
|  |  | w/Radome | Leg | 0.000 |  |  |  |  | 1/2" Ice | 29.050 | 0.33 |
|  |  |  |  | 0.000 |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 29.801 | 0.48 |
|  |  |  |  |  |  |  |  |  | 2" Ice | 31.302 | 0.78 |
| 8 FT Dish | A | Paraboloid |  | 0.500 | 0.000 |  | 96.000 | 8.000 | No Ice | 50.300 | 0.04 |
|  |  | w/Radome | Leg | $0.000$ |  |  |  |  | 1/2" Ice | $51.292$ | $0.30$ |
|  |  |  |  | 0.000 |  |  |  |  | 1" Ice | 52.284 | 0.57 |
|  |  |  |  |  |  |  |  |  | 2" Ice | 54.268 | 1.09 |
| PAD8-59AW | C | Paraboloid | From | 0.500 | 0.000 |  | 86.000 | 8.000 | No Ice | 50.300 | 0.04 |
|  |  | w/Radome | Leg | 0.000 |  |  |  |  | 1/2" Ice | 51.292 | 0.30 |
|  |  |  |  | 0.000 |  |  |  |  | 1" Ice | 52.284 | 0.57 |
|  |  |  |  |  |  |  |  |  | 2" Ice | 54.268 | 1.09 |
| 4 FT Dish | A | Paraboloid | From | 0.500 | 0.000 |  | 71.000 | 4.000 | No Ice | 12.570 | 0.08 |
|  |  | w/Radome | Leg | 0.000 |  |  |  |  | 1/2" Ice | 13.100 | 0.15 |
|  |  |  |  | 0.000 |  |  |  |  | 1" Ice | $13.620$ | $0.21$ |
|  |  |  |  |  |  |  |  |  | 2" Ice | 14.680 | 0.35 |
| ***** |  |  |  |  |  |  |  |  |  |  |  |
| PAD6-W59BC | A | Paraboloid | From | 1.000 | -34.500 |  | 87.000 | 6.583 | No Ice | 34.040 | 0.14 |
|  |  | w/Radome | Leg | 0.000 |  |  |  |  | 1/2" Ice | 34.910 | 0.29 |
|  |  |  |  | 0.000 |  |  |  |  | 1" Ice | 35.770 | 0.47 |
|  |  |  |  |  |  |  |  |  | 2" Ice | 37.510 | 0.83 |

## Load Combinations

| Comb. | Description |  |
| :---: | :--- | :--- |
| No. | Dead Only |  |
| 2 | 1.2 Dead +1.0 Wind 0 deg - No Ice |  |

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| Comb. No. | Description |
| :---: | :---: |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 29 | 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind $240 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

## Maximum Member Forces

| Sectio <br> $n$ | Elevation <br> ft | Component <br> Type | Condition | Gov. <br> Load | Axial | Major Axis <br> Moment | Minor Axis <br> Moment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  |  |  | Comb. | K | kip-ft |  |




## Maximum Reactions

| Location | Condition | Gov. <br> Load <br> Comb. | Vertical K | $\begin{gathered} \text { Horizontal, X } \\ K \end{gathered}$ | $\underset{K}{\text { Horizontal, Z }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Leg C | Max. Vert | 18 | 135.68 | 16.32 | -8.62 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 18 | 135.68 | 16.32 | -8.62 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 5 | -95.84 | -11.97 | 8.13 |
|  | Min. Vert | 7 | -106.97 | -14.11 | 7.37 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 7 | -106.97 | -14.11 | 7.37 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 16 | 123.88 | 14.12 | -9.32 |
| Leg B | Max. Vert | 10 | 137.22 | -16.64 | -8.77 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 23 | -108.24 | 14.20 | 7.38 |
|  | Max. $\mathrm{Hz}_{\mathrm{z}}$ | 25 | -98.16 | 12.09 | 8.42 |
|  | Min. Vert | 23 | -108.24 | 14.20 | 7.38 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 10 | 137.22 | -16.64 | -8.77 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 12 | 125.37 | -14.34 | -9.68 |
| Leg A | Max. Vert | 2 | 137.76 | 0.06 | 19.28 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 21 | 6.51 | 2.16 | 0.64 |
|  | Max. $\mathrm{H}_{\mathrm{z}}$ | 2 | 137.76 | 0.06 | 19.28 |
|  | Min. Vert | 15 | -118.35 | -0.11 | -17.31 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 9.59 | -2.26 | 0.94 |
|  | Min. $\mathrm{Hz}_{\mathrm{z}}$ | 15 | -118.35 | -0.11 | -17.31 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $_{x}$ $K$ | Shear $_{z}$ $K$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 32.79 | 0.00 | 0.00 | 25.61 | 9.16 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg No Ice | 39.35 | 0.08 | -32.03 | -2433.00 | 4.75 | 2.81 |
| 0.9 Dead+1.0 Wind 0 deg No Ice | 29.51 | 0.08 | -32.03 | -2440.68 | 2.01 | 2.81 |
| 1.2 Dead+1.0 Wind 30 deg No Ice | 39.35 | 15.62 | -27.30 | -2064.53 | -1182.90 | 21.96 |
| 0.9 Dead+1.0 Wind 30 deg No Ice | 29.51 | 15.62 | -27.30 | -2072.22 | -1185.65 | 21.96 |
| 1.2 Dead+1.0 Wind 60 deg No Ice | 39.35 | 25.84 | -14.77 | -1109.99 | -1984.87 | 26.22 |
| 0.9 Dead+1.0 Wind 60 deg No Ice | 29.51 | 25.84 | -14.77 | -1117.67 | -1987.61 | 26.22 |
| 1.2 Dead+1.0 Wind 90 deg No Ice | 39.35 | 28.48 | 0.40 | 68.75 | -2232.56 | 22.94 |
| 0.9 Dead+1.0 Wind 90 deg No Ice | 29.51 | 28.48 | 0.40 | 61.07 | -2235.31 | 22.94 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice | 39.35 | 26.80 | 15.69 | 1256.37 | -2071.96 | 27.69 |
| $\begin{aligned} & 0.9 \text { Dead+1.0 Wind } 120 \mathrm{deg} \\ & \text { - No Ice } \end{aligned}$ | 29.51 | 26.80 | 15.69 | 1248.69 | -2074.71 | 27.69 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No Ice | 39.35 | 16.43 | 28.32 | 2211.97 | -1253.07 | 16.10 |
| 0.9 Dead+1.0 Wind 150 deg <br> - No Ice | 29.51 | 16.43 | 28.32 | 2204.29 | -1255.82 | 16.10 |
| 1.2 Dead+1.0 Wind 180 deg <br> - No Ice | 39.35 | 0.02 | 32.19 | 2509.85 | 11.85 | -3.76 |
| 0.9 Dead+1.0 Wind 180 deg <br> - No Ice | 29.51 | 0.02 | 32.19 | 2502.17 | 9.10 | -3.76 |
| 1.2 Dead+1.0 Wind 210 deg <br> - No Ice | 39.35 | -15.95 | 27.77 | 2172.86 | 1242.01 | -23.28 |
| 0.9 Dead+1.0 Wind 210 deg <br> - No Ice | 29.51 | -15.95 | 27.77 | 2165.18 | 1239.27 | -23.28 |
| 1.2 Dead+1.0 Wind 240 deg <br> - No Ice | 39.35 | -26.13 | 15.54 | 1246.90 | 2042.63 | -27.50 |
| 0.9 Dead+1.0 Wind 240 deg <br> - No Ice | 29.51 | -26.13 | 15.54 | 1239.21 | 2039.88 | -27.50 |
| 1.2 Dead+1.0 Wind 270 deg | 39.35 | -28.04 | 0.42 | 72.73 | 2221.16 | -24.37 |

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| Load Combination | Vertical <br> K | Shear $_{x}$ K | Shear $_{z}$ <br> K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 270 deg <br> - No Ice | 29.51 | -28.04 | 0.42 | 65.05 | 2218.41 | -24.37 |
| 1.2 Dead+1.0 Wind 300 deg | 39.35 | -25.88 | -14.94 | -1122.84 | 2011.58 | -28.42 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 300 deg | 29.51 | -25.88 | -14.94 | -1130.53 | 2008.83 | -28.42 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 330 deg | 39.35 | -15.75 | -27.92 | -2110.74 | 1213.99 | -16.77 |
| - No Ice |  |  |  |  |  |  |
| 0.9 Dead+1.0 Wind 330 deg | 29.51 | -15.75 | -27.92 | -2118.43 | 1211.24 | -16.77 |
| - No Ice |  |  |  |  |  |  |
| 1.2 Dead+1.0 Ice+1.0 Temp | 153.69 | 0.00 | 0.00 | 201.03 | -21.09 | -0.00 |
| 1.2 Dead+1.0 Wind 0 | 153.69 | 0.03 | -12.19 | -729.42 | -23.08 | 5.32 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 30 | 153.69 | 5.86 | -10.24 | -584.59 | -468.70 | 14.30 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 60 | 153.69 | 9.65 | -5.59 | -232.09 | -766.72 | 17.20 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 90 | 153.69 | 11.01 | 0.05 | 206.26 | -877.86 | 17.46 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 120 | 153.69 | 9.88 | 5.77 | 649.82 | -785.97 | 15.34 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 150 | 153.69 | 5.99 | 10.44 | 1002.60 | -480.06 | 7.03 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 180 | 153.69 | -0.01 | 12.22 | 1134.09 | -19.90 | -5.48 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 210 | 153.69 | -5.91 | 10.32 | 994.44 | 432.70 | -14.51 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 240 | 153.69 | -9.69 | 5.72 | 646.57 | 730.50 | -17.41 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 270 | 153.69 | -10.94 | 0.08 | 208.94 | 830.35 | -17.69 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 300 | 153.69 | -9.73 | -5.65 | -235.94 | 730.41 | -15.46 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| 1.2 Dead+1.0 Wind 330 | 153.69 | -5.88 | -10.37 | -593.99 | 427.97 | -7.14 |
| deg+1.0 Ice+1.0 Temp |  |  |  |  |  |  |
| Dead+Wind 0 deg - Service | 32.79 | 0.02 | -6.92 | -503.03 | 7.83 | 0.60 |
| Dead+Wind 30 deg - Service | 32.79 | 3.38 | -5.90 | -424.03 | -247.07 | 4.68 |
| Dead+Wind 60 deg - Service | 32.79 | 5.59 | -3.20 | -219.30 | -419.30 | 5.59 |
| Dead+Wind 90 deg - Service | 32.79 | 6.16 | 0.08 | 33.71 | -472.58 | 4.89 |
| Dead+Wind 120 deg - | 32.79 | 5.79 | 3.39 | 288.60 | -437.86 | 5.90 |
| Service |  |  |  |  |  |  |
| Dead+Wind 150 deg - | 32.79 | 3.55 | 6.12 | 493.56 | -262.02 | 3.43 |
| Service |  |  |  |  |  |  |
| Dead+Wind 180 deg - | 32.79 | 0.00 | 6.95 | 557.52 | 9.34 | -0.80 |
| Service |  |  |  |  |  |  |
| Dead+Wind 210 deg - | 32.79 | -3.44 | 6.00 | 485.23 | 273.30 | -4.96 |
| Service |  |  |  |  |  |  |
| Dead+Wind 240 deg - | 32.79 | -5.65 | 3.36 | 286.58 | 445.24 | -5.86 |
| Service |  |  |  |  |  |  |
| Dead+Wind 270 deg - | 32.79 | -6.07 | 0.09 | 34.56 | 483.78 | -5.19 |
| Service |  |  |  |  |  |  |
| Dead+Wind 300 deg - | 32.79 | -5.60 | -3.23 | -222.03 | 438.62 | -6.05 |
| Service |  |  |  |  |  |  |
| Dead+Wind 330 deg - | 32.79 | -3.40 | -6.03 | -433.87 | 267.33 | -3.57 |
| Service |  |  |  |  |  |  |

## Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.00 | -32.79 | 0.00 | 0.00 | 32.79 | 0.00 | $0.000 \%$ |
| 2 | 0.08 | -39.35 | -32.03 | -0.08 | 39.35 | 32.03 | $0.000 \%$ |
| 3 | 0.08 | -29.51 | -32.03 | -0.08 | 29.51 | 32.03 | $0.000 \%$ |
| 4 | 15.62 | -39.35 | -27.30 | -15.62 | 39.35 | 27.30 | $0.000 \%$ |

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|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ | PY | PZ |  |
| Comb. | K | K | K | K | K | K |  |
| 5 | 15.62 | -29.51 | -27.30 | -15.62 | 29.51 | 27.30 | 0.000\% |
| 6 | 25.84 | -39.35 | -14.77 | -25.84 | 39.35 | 14.77 | 0.000\% |
| 7 | 25.84 | -29.51 | -14.77 | -25.84 | 29.51 | 14.77 | 0.000\% |
| 8 | 28.48 | -39.35 | 0.40 | -28.48 | 39.35 | -0.40 | 0.000\% |
| 9 | 28.48 | -29.51 | 0.40 | -28.48 | 29.51 | -0.40 | 0.000\% |
| 10 | 26.80 | -39.35 | 15.69 | -26.80 | 39.35 | -15.69 | 0.000\% |
| 11 | 26.80 | -29.51 | 15.69 | -26.80 | 29.51 | -15.69 | 0.000\% |
| 12 | 16.43 | -39.35 | 28.32 | -16.43 | 39.35 | -28.32 | 0.000\% |
| 13 | 16.43 | -29.51 | 28.32 | -16.43 | 29.51 | -28.32 | 0.000\% |
| 14 | 0.02 | -39.35 | 32.19 | -0.02 | 39.35 | -32.19 | 0.000\% |
| 15 | 0.02 | -29.51 | 32.19 | -0.02 | 29.51 | -32.19 | 0.000\% |
| 16 | -15.95 | -39.35 | 27.77 | 15.95 | 39.35 | -27.77 | 0.000\% |
| 17 | -15.95 | -29.51 | 27.77 | 15.95 | 29.51 | -27.77 | 0.000\% |
| 18 | -26.13 | -39.35 | 15.54 | 26.13 | 39.35 | -15.54 | 0.000\% |
| 19 | -26.13 | -29.51 | 15.54 | 26.13 | 29.51 | -15.54 | 0.000\% |
| 20 | -28.04 | -39.35 | 0.42 | 28.04 | 39.35 | -0.42 | 0.000\% |
| 21 | -28.04 | -29.51 | 0.42 | 28.04 | 29.51 | -0.42 | 0.000\% |
| 22 | -25.88 | -39.35 | -14.94 | 25.88 | 39.35 | 14.94 | 0.000\% |
| 23 | -25.88 | -29.51 | -14.94 | 25.88 | 29.51 | 14.94 | 0.000\% |
| 24 | -15.75 | -39.35 | -27.92 | 15.75 | 39.35 | 27.92 | 0.000\% |
| 25 | -15.75 | -29.51 | -27.92 | 15.75 | 29.51 | 27.92 | 0.000\% |
| 26 | 0.00 | -153.69 | 0.00 | 0.00 | 153.69 | 0.00 | 0.000\% |
| 27 | 0.03 | -153.69 | -12.19 | -0.03 | 153.69 | 12.19 | 0.000\% |
| 28 | 5.86 | -153.69 | -10.24 | -5.86 | 153.69 | 10.24 | 0.000\% |
| 29 | 9.65 | -153.69 | -5.59 | -9.65 | 153.69 | 5.59 | 0.000\% |
| 30 | 11.01 | -153.69 | 0.05 | -11.01 | 153.69 | -0.05 | 0.000\% |
| 31 | 9.88 | -153.69 | 5.77 | -9.88 | 153.69 | -5.77 | 0.000\% |
| 32 | 5.99 | -153.69 | 10.44 | -5.99 | 153.69 | -10.44 | 0.000\% |
| 33 | -0.01 | -153.69 | 12.22 | 0.01 | 153.69 | -12.22 | 0.000\% |
| 34 | -5.91 | -153.69 | 10.32 | 5.91 | 153.69 | -10.32 | 0.000\% |
| 35 | -9.69 | -153.69 | 5.72 | 9.69 | 153.69 | -5.72 | 0.000\% |
| 36 | -10.94 | -153.69 | 0.08 | 10.94 | 153.69 | -0.08 | 0.000\% |
| 37 | -9.73 | -153.69 | -5.65 | 9.73 | 153.69 | 5.65 | 0.000\% |
| 38 | -5.88 | -153.69 | -10.37 | 5.88 | 153.69 | 10.37 | 0.000\% |
| 39 | 0.02 | -32.79 | -6.92 | -0.02 | 32.79 | 6.92 | 0.000\% |
| 40 | 3.38 | -32.79 | -5.90 | -3.38 | 32.79 | 5.90 | 0.000\% |
| 41 | 5.59 | -32.79 | -3.20 | -5.59 | 32.79 | 3.20 | 0.000\% |
| 42 | 6.16 | -32.79 | 0.08 | -6.16 | 32.79 | -0.08 | 0.000\% |
| 43 | 5.79 | -32.79 | 3.39 | -5.79 | 32.79 | -3.39 | 0.000\% |
| 44 | 3.55 | -32.79 | 6.12 | -3.55 | 32.79 | -6.12 | 0.000\% |
| 45 | 0.00 | -32.79 | 6.95 | -0.00 | 32.79 | -6.95 | 0.000\% |
| 46 | -3.44 | -32.79 | 6.00 | 3.44 | 32.79 | -6.00 | 0.000\% |
| 47 | -5.65 | -32.79 | 3.36 | 5.65 | 32.79 | -3.36 | 0.000\% |
| 48 | -6.07 | -32.79 | 0.09 | 6.07 | 32.79 | -0.09 | 0.000\% |
| 49 | -5.60 | -32.79 | -3.23 | 5.60 | 32.79 | 3.23 | 0.000\% |
| 50 | -3.40 | -32.79 | -6.03 | 3.40 | 32.79 | 6.03 | 0.000\% |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 。 |
| :---: | :---: | :---: | :---: | :---: | :---: | | Twist |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | ft | $130-120$ | 1.009 | 44 |
| T2 | $120-100$ | 0.869 | 44 | 0.066 |
| T3 | $100-80$ | 0.606 | 44 | 0.065 |
| T4 | $80-60$ | 0.385 | 44 | 0.057 |
| T5 | $60-40$ | 0.219 | 44 | 0.045 |
| T6 | $40-20$ | 0.100 | 44 | 0.032 |
| T7 | $20-0$ | 0.030 | 44 | 0.021 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130.000 | 876F-70-2 4-Bay Dipole | 44 | 1.009 | 0.066 | 0.007 | 315602 |
| 127.000 | Sector Mount [SM 501-3] | 44 | 0.967 | 0.066 | 0.007 | 315602 |
| 125.000 | Sector Mount [SM 502-3] | 44 | 0.939 | 0.066 | 0.008 | 315602 |
| 117.000 | PA6-59 | 44 | 0.828 | 0.064 | 0.007 | 150659 |
| 113.000 | Side Arm Mount [SO 306-1] | 44 | 0.774 | 0.063 | 0.007 | 140781 |
| 107.000 | 6 FT Dish | 44 | 0.695 | 0.060 | 0.007 | 128868 |
| 104.000 | Side Arm Mount [SO 306-1] | 44 | 0.656 | 0.059 | 0.007 | 121816 |
| 98.000 | Side Arm Mount [SO 306-1] | 44 | 0.582 | 0.055 | 0.007 | 106652 |
| 96.000 | 8 FT Dish | 44 | 0.558 | 0.054 | 0.007 | 102394 |
| 87.000 | PAD6-W59BC | 44 | 0.456 | 0.049 | 0.006 | 86955 |
| 86.000 | PAD8-59AW | 44 | 0.446 | 0.048 | 0.006 | 85388 |
| 84.000 | PD1142-1 | 44 | 0.425 | 0.047 | 0.006 | 82387 |
| 77.000 | Sector Mount [SM 402-1] | 44 | 0.356 | 0.043 | 0.006 | 80791 |
| 71.000 | 4 FT Dish | 44 | 0.303 | 0.039 | 0.006 | 89281 |
| 63.000 | Sector Mount [SM 402-1] | 44 | 0.240 | 0.034 | 0.005 | 103901 |
| 58.000 | (2) 4.5 ' $\times 2$ " horizontal mount pipe | 44 | 0.205 | 0.031 | 0.005 | 108626 |
| 54.000 | Side Arm Mount [SO 306-1] | 44 | 0.178 | 0.028 | 0.005 | 106270 |
| 43.000 | Side Arm Mount [SO 306-1] | 44 | 0.115 | 0.022 | 0.004 | 98935 |

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 。 |
| :---: | :---: | :---: | :---: | :---: | :---: | | Twist |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $f t$ | $130-120$ | 4.631 | 12 |
| T1 | $120-100$ | 3.984 | 12 | 0.302 |
| T2 | $100-80$ | 2.774 | 12 | 0.297 |
| T3 | $80-60$ | 1.759 | 12 | 0.259 |
| T5 | $60-40$ | 1.002 | 12 | 0.203 |
| T6 | $40-20$ | 0.460 | 12 | 0.145 |
| T7 | $20-0$ | 0.138 | 13 | 0.094 |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation ft | Appurtenance | Gov. <br> Load <br> Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130.000 | 876F-70-2 4-Bay Dipole | 12 | 4.631 | 0.302 | 0.035 | 80042 |
| 127.000 | Sector Mount [SM 501-3] | 12 | 4.436 | 0.301 | 0.035 | 80042 |
| 125.000 | Sector Mount [SM 502-3] | 12 | 4.306 | 0.300 | 0.035 | 80042 |
| 117.000 | PA6-59 | 12 | 3.794 | 0.294 | 0.035 | 36828 |
| 113.000 | Side Arm Mount [SO 306-1] | 12 | 3.545 | 0.288 | 0.034 | 33049 |
| 107.000 | 6 FT Dish | 12 | 3.181 | 0.276 | 0.033 | 28641 |
| 104.000 | Side Arm Mount [SO 306-1] | 12 | 3.004 | 0.269 | 0.033 | 26597 |
| 98.000 | Side Arm Mount [SO 306-1] | 12 | 2.663 | 0.254 | 0.032 | 23167 |
| 96.000 | 8 FT Dish | 12 | 2.553 | 0.249 | 0.032 | 22224 |
| 87.000 | PAD6-W59BC | 12 | 2.086 | 0.224 | 0.030 | 18734 |
| 86.000 | PAD8-59AW | 12 | 2.038 | 0.221 | 0.030 | 18390 |
| 84.000 | PD1142-1 | 12 | 1.942 | 0.215 | 0.030 | 17743 |
| 77.000 | Sector Mount [SM 402-1] | 12 | 1.629 | 0.194 | 0.029 | 17449 |
| 71.000 | 4 FT Dish | 12 | 1.388 | 0.176 | 0.028 | 19414 |
| 63.000 | Sector Mount [SM 402-1] | 12 | 1.101 | 0.153 | 0.025 | 22882 |
| 58.000 | (2) $4.5^{\prime} \times 2$ " horizontal mount pipe | 12 | 0.938 | 0.139 | 0.024 | 24079 |
| 54.000 | Side Arm Mount [SO 306-1] | 12 | 0.817 | 0.129 | 0.023 | 23511 |
| 43.000 | Side Arm Mount [SO 306-1] | 12 | 0.528 | 0.102 | 0.018 | 21780 |

## Bolt Design Data

| Section No. | Elevation <br> ft | Component Type | Bolt Grade | Bolt Size in | Number Of Bolts | Maximum Load per Bolt K | Allowable Load per Bolt K | Ratio <br> Load <br> Allowable | Allowable Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 130 | Leg | A325N | 0.750 | 4 | 1.02 | 30.10 | 0.034 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 1.13 | 13.81 | 0.082 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 1.24 | 13.81 | 0.090 | 1.05 | Bolt Shear |
| T2 | 120 | Leg | A325N | 0.875 | 4 | 3.97 | 41.56 | 0.096 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 1.57 | 13.81 | 0.114 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 1.45 | 13.81 | 0.105 | 1.05 | Bolt Shear |
| T3 | 100 | Leg | A325N | 1.000 | 4 | 8.50 | 54.52 | 0.156 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 2.09 | 13.81 | 0.151 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 2.13 | 13.81 | 0.154 | 1.05 | Bolt Shear |
| T4 | 80 | Leg | A325N | 1.000 | 4 | 12.94 | 54.52 | 0.237 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 2.82 | 13.81 | 0.204 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 2.50 | 13.81 | 0.181 | 1.05 | Bolt Shear |
| T5 | 60 | Leg | A325N | 1.000 | 6 | 12.08 | 54.52 | 0.222 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 2.63 | 13.81 | 0.190 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 2.56 | 13.81 | 0.185 | 1.05 | Bolt Shear |
| T6 | 40 | Leg | A325N | 1.000 | 6 | 15.29 | 54.52 | 0.281 | 1.05 | Bolt Tension |
|  |  | Diagonal | A325N | 0.625 | 3 | 2.68 | 13.81 | 0.194 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 2.80 | 13.81 | 0.203 | 1.05 | Bolt Shear |
| T7 | 20 | Diagonal | A325N | 0.625 | 3 | 2.74 | 13.81 | 0.198 | 1.05 | Bolt Shear |
|  |  | Horizontal | A325N | 0.625 | 2 | 3.02 | 13.81 | 0.219 | 1.05 | Bolt Shear |

## Compression Checks

## Leg Design Data (Compression)

| Section No. | Elevation <br> ft | Size | $L$ <br> ft | $L_{u}$ ft | Kl/r | $A$ $i n^{2}$ | $\begin{gathered} P_{u} \\ K \end{gathered}$ | $\begin{gathered} \phi P_{n} \\ K \end{gathered}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | 130-120 | ROHN 2.5 STD | 10.000 | 5.000 | $\begin{gathered} 63.3 \\ K=1.00 \end{gathered}$ | 1.704 | -12.20 | 57.19 | $0.213^{1}$ |
| T2 | 120-100 | ROHN 3 STD | 20.036 | 6.679 | $\begin{gathered} 68.9 \\ \mathrm{~K}=1.00 \end{gathered}$ | 2.228 | -23.60 | 70.89 | $0.333{ }^{1}$ |
| T3 | 100-80 | ROHN 4 STD | 20.036 | 6.679 | $\begin{gathered} 53.1 \\ \mathrm{~K}=1.00 \end{gathered}$ | 3.174 | -42.56 | 116.23 | $0.366{ }^{1}$ |
| T4 | 80-60 | ROHN 5 STD | 20.042 | 10.021 | $\begin{gathered} 64.0 \\ \mathrm{~K}=1.00 \end{gathered}$ | 4.300 | -62.09 | 143.37 | $0.433{ }^{1}$ |
| T5 | 60-40 | ROHN 5 EH | 20.055 | 10.028 | $\begin{gathered} 65.4 \\ \mathrm{~K}=1.00 \end{gathered}$ | 6.112 | -85.40 | 201.11 | $0.425^{1}$ |
| T6 | 40-20 | ROHN 6 EHS | 20.052 | 10.026 | $\begin{gathered} 54.1 \\ \mathrm{~K}=1.00 \end{gathered}$ | 6.713 | -107.07 | 243.97 | $0.439{ }^{1}$ |
| T7 | 20-0 | ROHN 6 EH | 20.052 | 10.026 | $\begin{gathered} 54.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 8.405 | -128.00 | 303.62 | $0.422^{1}$ |

[^4]
## Diagonal Design Data (Compression)

| Section <br> No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio | $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

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${ }^{1} P_{u} / \phi P_{n}$ controls

## Horizontal Design Data (Compression)

| Section No. | Elevation <br> ft | Size | $L$ $f t$ | $L_{u}$ ft | K//r | A $i n^{2}$ | $P_{u}$ $K$ | $\phi P_{n}$ $K$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 130-120 | ROHN 1.5 STD | 8.520 | 4.140 | $\begin{gathered} 79.8 \\ \mathrm{~K}=1.00 \end{gathered}$ | 0.799 | -2.43 | 22.58 | $0.107{ }^{1}$ |
| T2 | 120-100 | ROHN 2 STD | 9.933 | 4.821 | $\begin{gathered} 73.5 \\ \mathrm{~K}=1.00 \end{gathered}$ | 1.075 | -2.87 | 32.58 | $0.088{ }^{1}$ |
| T3 | 100-80 | ROHN 2 STD | 12.017 | 5.821 | $\begin{gathered} 88.7 \\ \mathrm{~K}=1.00 \end{gathered}$ | 1.075 | -4.24 | 27.19 | $0.156{ }^{1}$ |
| T4 | 80-60 | ROHN 2 STD | 13.835 | 6.686 | $\begin{array}{r} 101.9 \\ \mathrm{~K}=1.00 \end{array}$ | 1.075 | -4.95 | 22.62 | $0.219^{1}$ |
| T5 | 60-40 | ROHN 2 STD | 16.250 | 7.893 | $\begin{gathered} 120.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 1.075 | -5.04 | 16.76 | $0.301{ }^{1}$ |
| T6 | 40-20 | ROHN 2.5 STD | 18.790 | 9.119 | $\begin{array}{r} 115.5 \\ \mathrm{~K}=1.00 \end{array}$ | 1.704 | -5.46 | 28.86 | $0.189{ }^{1}$ |
| T7 | 20-0 | ROHN 2.5 STD | 21.290 | 10.369 | $\begin{gathered} 131.3 \\ \mathrm{~K}=1.00 \end{gathered}$ | 1.704 | -5.85 | 22.32 | $0.262{ }^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Top Girt Design Data (Compression) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | L | $L_{u}$ | K//r | $A$ | $P_{u}$ | $\phi P_{n}$ | $\begin{aligned} & \text { Ratio } \\ & P_{u} \end{aligned}$ |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 130-120 | ROHN 1.5 STD | 8.500 | 4.130 | $\begin{gathered} 79.6 \\ K=1.00 \end{gathered}$ | 0.799 | -0.48 | 22.63 | $0.021{ }^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Inner Bracing Design Data (Compression)

| Section No. | $f t$ | Size | L | $L_{u}$ | Kl/r |  | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 130-120 | L2x2x1/8 | 4.260 | 4.260 | $\begin{gathered} 128.6 \\ \mathrm{~K}=1.00 \end{gathered}$ | 0.484 | -0.00 | 8.38 | $0.000{ }^{1}$ |

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| Section No. | Elevation | Size | $L$ | $L_{u}$ | KI/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T2 | 120-100 | L2x2x1/8 | 4.967 | 4.967 | $\begin{gathered} 149.9 \\ K=1.00 \end{gathered}$ | 0.484 | -0.01 | 6.17 | $0.001{ }^{1}$ |
| T3 | 100-80 | L2x2x1/8 | 6.008 | 6.008 | $\begin{gathered} 181.4 \\ K=1.00 \end{gathered}$ | 0.484 | -0.01 | 4.21 | $0.002{ }^{1}$ |
| T4 | 80-60 | L2x2x1/8 | 6.918 | 6.918 | $\begin{gathered} 208.8 \\ K=1.00 \end{gathered}$ | 0.484 | -0.01 | 3.18 | $0.004{ }^{1}$ |
| T5 | 60-40 | L2 1/2x2 1/2x3/16 | 8.125 | 8.125 | $\begin{gathered} 197.0 \\ K=1.00 \end{gathered}$ | 0.902 | -0.02 | 6.65 | $0.002{ }^{1}$ |
| T6 | 40-20 | L 3x3x3/16 | 9.395 | 9.395 | $\begin{gathered} 189.1 \\ K=1.00 \end{gathered}$ | 1.090 | -0.02 | 8.73 | $0.002{ }^{1}$ |
| T7 | 20-0 | L3 1/2x3 / $12 \times 1 / 4$ | 10.645 | 10.645 | $\begin{gathered} 184.2 \\ K=1.00 \end{gathered}$ | 1.688 | -0.02 | 14.24 | $0.001^{* 1}$ |

* DL controls
${ }^{1} P_{u} / \phi P_{n}$ controls


## Tension Checks

## Leg Design Data (Tension)

| Section <br> No. | Elevation | Size | $L$ | $L_{u}$ | $K l / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio <br> $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  |  |  |  |  |  |  |  |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Diagonal Design Data (Tension)

| Section <br> No. | Elevation | Size | $L$ | $L_{u}$ | $K I / r$ | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio <br> $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  |  |  |  |  |  |  |  |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Section No. | Elevation | Size | L | $L_{u}$ | KI/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{\mu} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | ${ }_{\phi} P_{n}$ |
| T1 | 130-120 | ROHN 1.5 STD | 8.520 | 4.140 | 79.8 | 0.799 | 2.48 | 35.98 | $0.069{ }^{1}$ |
| T2 | 120-100 | ROHN 2 STD | 9.933 | 4.821 | 73.5 | 1.075 | 2.89 | 48.35 | $0.060{ }^{1}$ |
| T3 | 100-80 | ROHN 2 STD | 12.017 | 5.821 | 88.7 | 1.075 | 4.26 | 48.35 | $0.088{ }^{1}$ |
| T4 | 80-60 | ROHN 2 STD | 13.835 | 6.686 | 101.9 | 1.075 | 5.00 | 48.35 | $0.103{ }^{1}$ |
| T5 | 60-40 | ROHN 2 STD | 16.250 | 7.893 | 120.3 | 1.075 | 5.11 | 48.35 | $0.106{ }^{1}$ |
| T6 | 40-20 | ROHN 2.5 STD | 18.790 | 9.119 | 115.5 | 1.704 | 5.61 | 76.68 | $0.073{ }^{1}$ |
| T7 | 20-0 | ROHN 2.5 STD | 21.290 | 10.369 | 131.3 | 1.704 | 6.04 | 76.68 | $0.079{ }^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Top Girt Design Data (Tension)

| Section No. | ft | Size | L | $L_{u}$ | Kl/r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | ${ }_{\phi} P_{n}$ |
| T1 | 130-120 | ROHN 1.5 STD | 8.500 | 4.130 | 79.6 | 0.799 | 0.48 | 35.98 | $0.013^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

| Inner Bracing Design Data (Tension) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | L | $L_{u}$ | K//r | A | $P_{u}$ | $\phi P_{n}$ | $\begin{aligned} & \text { Ratio } \\ & P_{u} \end{aligned}$ |
|  | $f t$ |  | $f t$ | $f t$ |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| T1 | 130-120 | L2x2x1/8 | 4.260 | 4.260 | 81.6 | 0.484 | 0.00 | 15.69 | $0.000{ }^{1}$ |
| T2 | 120-100 | L2x2x1/8 | 4.270 | 4.270 | 81.8 | 0.484 | 0.00 | 15.69 | $0.000{ }^{1}$ |
| T3 | 100-80 | L2x2x1/8 | 6.008 | 6.008 | 115.1 | 0.484 | 0.00 | 15.69 | $0.000{ }^{1}$ |
| T4 | 80-60 | L2x2x1/8 | 6.355 | 6.355 | 121.8 | 0.484 | 0.00 | 15.69 | $0.000{ }^{1}$ |

${ }^{1} P_{u} / \phi P_{n}$ controls

## Section Capacity Table

| Section <br> No. | Elevation <br> $f t$ | Component <br> Type | Size | Critical <br> Element | $P$ <br> $K$ | $\varnothing P_{\text {alow }}$ <br> $K$ | $\%$ <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T1 | $130-120$ | Leg | ROHN 2.5 STD | 1 | -12.20 | 60.05 | 20.3 | Pass |
| T2 | $120-100$ | Leg | ROHN 3 STD | 29 | -23.60 | 74.43 | 31.7 | Pass |
| T3 | $100-80$ | Leg | ROHN 4 STD | 69 | -42.56 | 122.04 | 34.9 | Pass |
| T4 | $80-60$ | Leg | ROHN 5 STD | 107 | -62.09 | 150.53 | 41.2 | Pass |
| T5 | $60-40$ | Leg | ROHN 5 EH | 134 | -85.40 | 211.17 | 40.4 | Pass |
| T6 | $40-20$ | Leg | ROHN 6 EHS | 161 | -107.07 | 256.16 | 41.8 | Pass |
| T7 | $20-0$ | Leg | ROHN 6 EH | 189 | -128.00 | 318.80 | 40.2 | Pass |
| T1 | $130-120$ | Diagonal | ROHN 2 STD | 9 | -3.39 | 25.36 | 13.4 | Pass |
| T2 | $120-100$ | Diagonal | ROHN 2.5 STD | 36 | -4.71 | 35.92 | 13.1 | Pass |
| T3 | $100-80$ | Diagonal | ROHN 2.5 STD | 74 | -6.27 | 31.52 | 19.9 | Pass |
| T4 | $80-60$ | Diagonal | ROHN 2.5 X-STR | 113 | -8.46 | 21.63 | 39.1 | Pass |
| T5 | $60-40$ | Diagonal | ROHN 3 STD | 140 | -7.88 | 29.61 | 26.6 | Pass |
| T6 | $40-20$ | Diagonal | ROHN 3 STD | 165 | -8.05 | 26.21 | 30.7 | Pass |
| T7 | $20-0$ | Diagonal | ROHN 3 STD | 192 | -8.22 | 22.99 | 35.7 | Pass |
| T1 | $130-120$ | Horizontal | ROHN 1.5 STD | 7 | -2.43 | 23.71 | 10.2 | Pass |
| T2 | $120-100$ | Horizontal | ROHN 2 STD | 34 | -2.87 | 34.21 | 8.4 | Pass |
| T3 | $100-80$ | Horizontal |  |  |  |  |  | 10.0 (b) |

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| Section No. | Elevation ft | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \emptyset P_{\text {allow }} \\ K \end{gathered}$ | \% <br> Capacity | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T6 | 40-20 | Horizontal | ROHN 2.5 STD | 163 | -5.46 | 30.30 | $\begin{gathered} 18.0 \\ 19.3(b) \end{gathered}$ | Pass |
| T7 | 20-0 | Horizontal | ROHN 2.5 STD | 190 | -5.85 | 23.43 | 25.0 | Pass |
| T1 | 130-120 | Top Girt | ROHN 1.5 STD | 4 | -0.48 | 23.77 | 2.0 | Pass |
| T1 | 130-120 | Inner Bracing | L2x2x1/8 | 16 | -0.00 | 8.80 | 0.8 | Pass |
| T2 | 120-100 | Inner Bracing | L2x2x1/8 | 42 | -0.01 | 6.48 | 0.9 | Pass |
| T3 | 100-80 | Inner Bracing | L2x2x1/8 | 79 | -0.01 | 4.43 | 1.1 | Pass |
| T4 | 80-60 | Inner Bracing | L2x2x1/8 | 120 | -0.01 | 3.34 | 1.2 | Pass |
| T5 | 60-40 | Inner Bracing | L2 1/2x2 1/2x3/16 | 147 | -0.02 | 6.99 | 0.9 | Pass |
| T6 | 40-20 | Inner Bracing | L 3x3x3/16 | 174 | -0.02 | 9.16 | 0.9 | Pass |
| T7 | 20-0 | Inner Bracing | L3 1/2x3 /12x1/4 | 201 | -0.02 | 14.24 | $0.8$ <br> Summary | Pass |
|  |  |  |  |  |  | Leg (T6) | 41.8 | Pass |
|  |  |  |  |  |  | Diagonal (T4) | 39.1 | Pass |
|  |  |  |  |  |  | Horizontal (T5) | 28.6 | Pass |
|  |  |  |  |  |  | Top Girt (T1) | 2.0 | Pass |
|  |  |  |  |  |  | Inner Bracing (T4) | 1.2 | Pass |
|  |  |  |  |  |  | Bolt Checks RATING = | 26.7 41.8 | Pass Pass |

## APPENDIX B

## BASE LEVEL DRAWING

$\qquad$ Flat $\qquad$


## ${ }^{\text {Dob: }}$ ES-004 SouthMtnRS

FAX: (913) 458-8136

Project: 405025

$|$| Project: $\mathbf{4 0 5 0 2 5}$ | Drawn by: Josh Riley | App'd: |
| :--- | :--- | :--- |
| Client: Eversource | Date: $01 / 13 / 22$ | Scale: NTS |
| Code: TIA-222-H |  | Dwg No. E-7 |
| Path: |  |  |

## APPENDIX C

## ADDITIONAL CALCULATIONS

BLACK \& VEATCH
Building a world of difference:


## Anchor Rod Data

Diameter ofAnchor Rod:

$$
\mathrm{D}:=1 \cdot \mathrm{in}
$$

Anchor Rod Grade:

Number of Anchor Rods:
Length from top of concrete to bottom of anchor rod leveling nut:

Threads in Shear Plane?:

$N:=8$
lar $:=2.5 \cdot \mathrm{in}$

Thread Series:

| Coarse |  |
| :--- | :--- |
|  | Fine <br> F-Thread |
|  |  |

Grout Factor $\eta$ :

| 0.90 |
| :--- |
| 0.70 |
| 0.55 |
| 0.50 |

(Thread selection invalid if $\mathrm{n}=0$ )

Rod Ultimate Strength: $\quad \mathrm{Fu}=125 \cdot \mathrm{ksi}$

Rod Yield Strength: $\quad$ Fy $=105 \cdot \mathrm{ksi}$
Anchor Rod Plastic
Section Modulus:
(based on tension root
diameter)
Radius of Gyration:
$\mathrm{r}:=\left(\frac{1}{4}\right) \cdot\left(\mathrm{D}-\frac{0.9743 \mathrm{in}}{\mathrm{n}}\right)=0.22 \cdot \mathrm{in}$
Net Area of Anchor Rod:

$$
\mathrm{Z}:=\frac{1}{6} \cdot\left(\mathrm{D}-\frac{0.9743 \mathrm{in}}{\mathrm{n}}\right)^{3}=0.113 \cdot \mathrm{in}^{3}
$$

$$
\mathrm{An}:=\frac{\pi}{4} \cdot\left(\mathrm{D}-\frac{0.9743 \mathrm{in}}{\mathrm{n}}\right)^{2}=0.606 \cdot \mathrm{in}^{2}
$$

Nominal Unthreaded
Area of Anchor Rod:
$\mathrm{Ab}:=\frac{\pi}{4} \cdot(\mathrm{D})^{2}=0.785 \cdot \mathrm{in}^{2}$

## Anchor Rod Design Capacities

Design Tension Strength:
TIA-222-G/H Section 4.9.6.1

$$
\begin{aligned}
& \mathrm{Rnt}:=\mathrm{Fu} \cdot \mathrm{An}=75.718 \cdot \mathrm{kip} \\
& \phi \mathrm{t}=0.75 \\
& \phi \mathrm{Rnt}:=\phi \mathrm{t} \cdot \mathrm{Rnt}=56.788 \cdot \mathrm{kip}
\end{aligned}
$$

Design Compression Strength:

$$
\begin{aligned}
& \mathrm{Rnc}:=\mathrm{Fy} \cdot \mathrm{An}=63.603 \cdot \mathrm{kip} \\
& \phi \mathrm{c}=1 \\
& \phi \mathrm{Rnc}:=\phi \mathrm{c} \cdot \mathrm{Rnc}=63.603 \cdot \mathrm{kip}
\end{aligned}
$$

Design Buckling Strength:

$$
\begin{aligned}
& \mathrm{K}_{0}:=1.2 \\
& \mathrm{Fcr}=102.033 \cdot \mathrm{ksi} \\
& \mathrm{Fe}=1.533 \times 10^{3} \cdot \mathrm{ksi} \\
& \mathrm{Rnb}:=\mathrm{Fcr} \cdot \mathrm{An}=61.806 \cdot \mathrm{kip} \\
& \phi \mathrm{c}=1 \\
& \phi \mathrm{Rnb}:=\phi \mathrm{c} \cdot \mathrm{Rnb}=61.806 \cdot \mathrm{kip}
\end{aligned}
$$

Design Shear Strength:
TIA-222-G/H Section 4.9.6.3

$$
\text { Rnv }:=\left\lvert\, \begin{aligned}
& 0.55 \cdot \mathrm{Fu} \cdot \mathrm{Ab} \text { if Thread_Type }=\text { "No" } \wedge \text { TIA }=\text { "Rev-G" } \\
& 0.45 \cdot \mathrm{Fu} \cdot \mathrm{Ab} \text { if Thread_Type }=\text { "Yes" } \wedge \text { TIA }=\text { "Rev-G" } \\
& 0.625 \cdot \mathrm{Fu} \cdot \mathrm{Ab} \text { if Thread_Type }=\text { "No" } \wedge \text { TIA }=\text { "Rev-H" } \\
& 0.5 \cdot \mathrm{Fu} \cdot \mathrm{Ab} \text { if Thread_Type }=\text { "Yes" } \wedge \text { TIA = "Rev-H" }
\end{aligned}\right.
$$

$R n v=49.087 \cdot \mathrm{kip}$

Rnvc $:=0.6 \cdot \mathrm{Fy} \cdot 0.5 \cdot \mathrm{An}=19.081 \cdot \mathrm{kip}$
TIA-222-H Section 4.9.9
$\phi \mathrm{v}=0.75 \quad \phi \mathrm{c}=1$
$\phi R n v:=\phi v \cdot R n v=36.816 \cdot \mathrm{kip} \quad \phi R n v c:=\phi c \cdot R n v c=19.081 \cdot \mathrm{kip}$

Design Flexural Strength:
TIA-222-G/H Section 4.7.1
$\mathrm{Rmn}:=\mathrm{Fy} \cdot \mathrm{Z}=11.853 \cdot \mathrm{kip} \cdot \mathrm{in}$
$\phi \mathrm{f}=0.9$
$\phi R m n:=\phi f \cdot \mathrm{Rmn}=10.668 \cdot \mathrm{kip} \cdot \mathrm{in}$

## Anchor Rod Loading Demands

Tension Demand:

$$
\text { Put }:=\frac{\text { Axial_U }}{\mathrm{N}}=2.25 \cdot \mathrm{kip}
$$

Compression Demand:

$$
\text { Puc }:=\frac{\text { Axial_C }}{\mathrm{N}}=17.25 \cdot \mathrm{kip}
$$

Shear Demand:

$$
\begin{aligned}
& \text { Vut }:=\frac{\text { Shear_U }}{\mathrm{N}}=2.125 \cdot \mathrm{kip} \\
& \text { Vuc }:=\frac{\text { Shear_C }}{\mathrm{N}}=2.375 \cdot \mathrm{kip}
\end{aligned}
$$

Moment Demand:

$$
\begin{aligned}
& \text { Mut }:=0.65 \cdot \mathrm{lar} \cdot \text { Vut }=3.453 \cdot \mathrm{kip} \cdot \mathrm{in} \\
& \text { Muc }:=0.65 \cdot \mathrm{lar} \cdot \text { Vuc }=3.859 \cdot \mathrm{kip} \cdot \mathrm{in}
\end{aligned}
$$

$$
\text { SR_g }:=\left\{\begin{array}{l}
\frac{\text { Put }+\frac{\text { Vut }}{\eta}}{\phi R n t} \text { if } \eta>0.50 \\
\frac{\text { Put }+\frac{\text { Vut }}{\eta}}{\phi R n t} \text { if } \eta=0.50 \wedge \text { lar } \leq \mathrm{D} \wedge \text { Put }>\text { Puc } \\
\frac{\text { Puc }+\frac{\text { Vuc }}{\eta}}{\phi R n t} \text { if } \eta=0.50 \wedge \text { lar } \leq \mathrm{D} \wedge \text { Put }<\text { Puc } \\
\left(\frac{\text { Vut }}{\phi R n v}\right)^{2}+\left(\frac{\text { Put }}{\phi R n t}+\frac{\text { Mut }}{\phi R m n}\right)^{2} \text { if } \eta=0.5 \wedge \text { lar }>\mathrm{D} \wedge \text { Put }>\text { Puc } \\
\left(\frac{\text { Vuc }}{\phi R n v}\right)^{2}+\left(\frac{\text { Puc }}{\phi R n t}+\frac{\mathrm{Muc}}{\phi R m n}\right)^{2} \text { if } \eta=0.5 \wedge \text { lar }>\mathrm{D} \wedge \text { Put }<\text { Puc }
\end{array}\right.
$$

$$
\text { SR_g }=0.108
$$

## Anchor Rod Interaction Check

$$
\text { SR_Pc }=0.287
$$

$$
\text { SR }:=\left\lvert\, \begin{aligned}
& \text { SR_g if TIA }=\text { "Rev-G" } \\
& \max (\text { SR_Pt, SR_Pc }) \text { if TIA }=\text { "Rev-H" } \wedge \mathrm{S} 15=\text { "No" } \\
& \frac{\max \left(\mathrm{SR} \_\mathrm{Pt}, \mathrm{SR} \_P c\right)}{1.05} \text { if TIA }=\text { "Rev-H" } \wedge \mathrm{S} 15=\text { "Yes" }
\end{aligned}=0.273\right.
$$

Check $_{\mathrm{SR}}:=|$| "Passing" if $\mathrm{SR} \leq 1.00 \wedge$ TIA $=$ "Rev-G" $\wedge \mathrm{S} 105=$ "Yes" |
| :--- |
| "Acceptable" if $1.00<\mathrm{SR} \leq 1.05 \wedge$ TIA $=$ "Rev-G" $\wedge \mathrm{S} 105=$ "Yes" |
| "Failing" if $\mathrm{SR}>1.05 \wedge$ TIA $=$ "Rev-G" $\wedge \mathrm{S} 105=$ "Yes" |
| "Passing" if $\mathrm{SR} \leq 1.00 \wedge$ TIA $=$ "Rev-G" $\wedge \mathrm{S} 105=$ "No" |
| "Failing" if $\mathrm{SR}>1.00 \wedge$ TIA $=$ "Rev-G" $\wedge \mathrm{S} 105=$ "No" |
| "Passing" if $\mathrm{SR} \leq 1.0 \wedge$ TIA $=$ "Rev-H" |
| "Failing" if $\mathrm{SR}>1.0 \wedge$ TIA $=$ "Rev-H" |

$$
\begin{aligned}
& \text { SR_Pt }:=\left\lvert\,\left(\frac{\text { Put }}{\phi R n t}\right)^{2}+\left(\frac{\text { Vut }}{\phi R n v}\right)^{2}\right. \text { if lar } \leq D \\
& \left(\frac{\text { Put }}{\phi \text { Rnt }}\right)^{2}+\left(\frac{\text { Vut }}{\phi \text { Rnv }}\right)^{2} \text { if } \mathrm{D}<\text { lar } \leq 3 \text {.in } \wedge \text { Grout }=\text { "Yes" } \\
& \left(\frac{\text { Put }}{\phi \text { Rnt }}+\frac{\text { Mut }}{\phi R m n}\right)^{2}+\left(\frac{\text { Vut }}{\phi R n v}\right)^{2} \text { if } 3 \cdot \text { in }<\text { lar } \wedge \text { Grout }=\text { "Yes" } \\
& \left(\frac{\text { Put }}{\phi \mathrm{Rnt}}+\frac{\text { Mut }}{\phi \mathrm{Rmn}}\right)^{2}+\left(\frac{\text { Vut }}{\phi \mathrm{Rnv}}\right)^{2} \text { if } \mathrm{D}<\operatorname{lar} \wedge \text { Grout }=\text { "No" } \\
& \text { SR_Pt }=4.901 \times 10^{-3} \\
& \text { SR_Pc := } \left\lvert\,\left(\frac{\text { Puc }}{\phi R n c}\right)+\left(\frac{\text { Vuc }}{\phi R n v c}\right)^{2}\right. \text { if lar } \leq D \\
& \left(\frac{\text { Puc }}{\phi \text { Rnc }}\right)+\left(\frac{\text { Vuc }}{\phi \text { Rnvc }}\right)^{2} \text { if } \mathrm{D}<\operatorname{lar} \leq 3 \cdot \text { in } \wedge \text { Grout }=\text { "Yes" } \\
& \left(\frac{\text { Puc }}{\phi \mathrm{Rnc}}+\frac{\mathrm{Muc}}{\phi \mathrm{Rmn}}\right)+\left(\frac{\mathrm{Vuc}}{\phi \mathrm{Rnvc}}\right)^{2} \text { if } 3 \cdot \text { in }<\operatorname{lar} \wedge \text { Grout }=\text { "Yes" } \\
& \left(\frac{\mathrm{Puc}}{\phi \mathrm{Rnc}}+\frac{\mathrm{Muc}}{\phi \mathrm{Rmn}}\right)+\left(\frac{\mathrm{Vuc}}{\phi \mathrm{Rnvc}}\right)^{2} \text { if } \mathrm{D}<\operatorname{lar} \leq 4 \cdot \mathrm{D} \wedge \text { Grout }=\text { "No" } \\
& \left(\frac{\text { Puc }}{\phi \operatorname{Rnb}}+\frac{\mathrm{Muc}}{\phi \mathrm{Rmn}}\right)+\left(\frac{\mathrm{Vuc}}{\phi \mathrm{Rnvc}}\right)^{2} \text { if lar }>4 \cdot \mathrm{D} \wedge \text { Grout }=" \mathrm{No} "
\end{aligned}
$$

## Anchor Rod Results

| Axial Tension Demand: | Put $=2.25 \cdot \mathrm{kip}$ |
| :---: | :---: |
| Axial Tension Capacity: | $\phi \mathrm{Rnt}=56.788 \cdot \mathrm{kip}$ |
| Axial Compression Demand: | Puc $=17.25 \cdot \mathrm{kip}$ |
| Axial Compression Capacity: | $\phi \mathrm{Rnc}=63.603 \cdot \mathrm{kip}$ |
| Shear Tension Demand: | Vut $=2.125 \cdot \mathrm{kip}$ |
| Tension Shear Capacity: | $\phi \mathrm{Rnv}=36.816 \cdot \mathrm{kip}$ |
| Shear Compression Demand: | Vuc $=2.375 \cdot \mathrm{kip}$ |
| Compresison Shear Capacity: | $\phi \mathrm{R}_{\mathrm{nvc}}=19.081 \cdot \mathrm{kip}$ |
| Moment Tension Demand: | $\mathrm{M}_{\mathrm{ut}}=3.453 \cdot \mathrm{kip} \cdot \mathrm{in}$ |
| Moment Compression Demand: | $\mathrm{M}_{\mathrm{uc}}=3.859 \cdot \mathrm{kip} \cdot \mathrm{in}$ |
| Moment Capacity: | $\phi \mathrm{R}_{\mathrm{mn}}=10.668 \cdot \mathrm{kip} \cdot \mathrm{in}$ |
| Governing | SR = 27.305.\% |
| Stress Ratio | Check $_{\text {SR }}=$ "Passing" |

## SST Unit Base Foundation



| Top \& Bot. Pad Rein. Different?: | $\Gamma$ |
| ---: | :---: |
| Tower Centroid Offset?: | $\overline{ }$ |
| Block Foundation?: | $\bar{\square}$ |


| Superstructure Analysis Reactions |  |  |
| ---: | :---: | :--- |
| Global Moment, M: | 2542 | ft-kips |
| Global Axial, P: | 39 | kips |
| Global Shear, V: | 33 | kips |
| Leg Compression, $\mathbf{P}_{\text {comp }}:$ | 138 | kips |
| Leg Comp. Shear, $\mathbf{V}_{\text {u_comp }}:$ | 19 | kips |
| Leg Uplift, $\mathbf{P}_{\text {uplifit: }}:$ | 118 | kips |
| Leg Uplift. Shear, $\mathbf{V}_{\text {u__uplift: }}$ | 17 | kips |
| Tower Height, $\mathbf{H}:$ | 130 | ft |
| Base Face Width, BW: | 22.5417 | ft |
| BP Dist. Above Fdn, bp ${ }_{\text {dist }}:$ | 2 | in |
| Anchor Bolt Circle, BC: | 10 | in |


| Foundation Analysis Checks |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating* | Check |
| Lateral (Sliding) (kips) | 206.03 | 33.00 | 15.3\% | Pass |
| Bearing Pressure (ksf) | 9.00 | 1.14 | 12.1\% | Pass |
| Overturning (kip*ft) | 7965.51 | 2679.50 | 33.6\% | Pass |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| Pad Flexure (kip*ft) | 1877.46 | 547.49 | 27.8\% | Pass |
| Pad Shear - 1-way (kips) | 1541.78 | 75.55 | 4.7\% | Pass |
| Pad Shear - Comp 2-way (ksi) | 0.190 | 0.018 | 9.2\% | Pass |
| Flexural 2-way (Comp) (kip*ft) | 978.81 | 0.00 | 0.0\% | Pass |
| Pad Shear - Tension 2-way (ksi) | 0.190 | 0.016 | 7.9\% | Pass |
| Flexural 2-way (Tension) (kip*ft) | 978.81 | 0.00 | 0.0\% | Pass |
|  |  | *Rating per TIA-222-H Section 15.5 |  |  |
|  |  | Soil Rating*:Structural Rating*: |  | 33.6\% |
|  |  |  |  | 27.8\% |


| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 4.00 | ft |
| Pad Width, $\mathbf{W}:$ | 31.00 | ft |
| Pad Thickness, T: | 4.00 | ft |
| Pad Rebar Size (Bottom), Sp: | 7 |  |
| Pad Rebar Quantity (Bottom), mp: | 16 |  |
| Pad Clear Cover, $\mathbf{c c}_{\text {pad }}:$ | 3 | in |


| Material Properties |  |  |
| ---: | :---: | :--- |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 4 | ksi |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |


| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 100 | pcf |
| Ultimate Gross Bearing, Qult: | 12.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 34 | degrees |
| SPT Blow Count, $\mathbf{N}_{\text {blows: }}:$ | 10 |  |
| Base Friction, $\mu:$ | 0.45 |  |
| Neglected Depth, N: | 3.3 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | $\mathrm{N} / \mathrm{A}$ | ft |

## ATTACHMENT D - PROOF OF DELIVERY OF NOTICE



PO: S0424674



FedEx
E
THU $=03$ M MR 10:30 PRIORITY OVERNIGHT 00 BNHA
Part न 156948-434 RIT2 01/14.


PO: SO424674
ต:


THU = 03 MAR 10:30 PRIORITY OVERNIGH'通: $2 \times-1643739112005$ 00 BDLA



ATTACHMENT E - POWER DENSITY REPORT

# Calculated Radio Frequency Emissions Report EVERS=URCE ENERGY 

ES-004

790 Willis Street

Bristol, CT 06010

February 7, 2022

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## 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the Eversource installation on the existing self-support tower located at 790 Willis Street in Bristol, CT.

Eversource has recently installed one omnidirectional antenna (Comprod 876F-70-2HSMP40DF1/2) for both transmit and receive purposes as part of its 220 MHz communications system and one microwave dish for backhaul communications. The original proposal also consisted of one omnidirectional antenna and one microwave dish, however the model of the original omni-directional antenna (db Spectra DS20C03F36D-D) has changed. This report provides an updated analysis based on the current installation as reflected in the updated plans ${ }^{1}$.

This report considers the existing antenna configuration as detailed by Eversource along with power density information of the other existing antennas to calculate the cumulative \% MPE (Maximum Permissible Exposure) of the facility at ground level.

## 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include Maximum Permissible Exposure (MPE) limits for transmitters operating between 300 kHz and 100 GHz . The FCC MPE limits are based upon those recommended by the National Council on Radiation Protection and Measurements (NCRP), developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

The FCC general population/uncontrolled limits set the maximum exposure to which most people may be subjected. General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Public exposure to radio frequencies is regulated and enforced in units of milliwatts per square centimeter $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$. The general population exposure limits for the various frequency ranges are defined in the attached "FCC Limits for Maximum Permissible Exposure (MPE)" in Attachment B of this report.

Higher exposure limits are permitted under the occupational/controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure, and they must be able to exercise control over their exposure. General population/uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals. Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population/uncontrolled exposure and for occupational/controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

[^5]
## 3. Power Density Calculation Methods

The power density calculation results were generated using the following formula as outlined in FCC bulletin OET 65, and Connecticut Siting Council recommendations:

$$
\text { Power Density }=\left(\frac{1.6^{2} \times 1.64 \times \mathrm{ERP}}{4 \pi \times R^{2}}\right) X \text { Off Beam Loss }
$$

Where:
EIRP $=$ Effective Isotropic Radiated Power $=1.64 \times$ ERP
$\mathrm{R}=$ Radial Distance $=\sqrt{\left(H^{2}+V^{2}\right)}$
$\mathrm{H}=$ Horizontal Distance from antenna
$\mathrm{V}=$ Vertical Distance from radiation center of antenna
Ground reflection factor of 1.6
Off Beam Loss is determined by the selected antenna pattern

These calculations assume that the antennas are operating at 100 percent capacity and full power, and that all antenna channels are transmitting simultaneously. Obstructions (trees, buildings, etc.) that would normally attenuate the signal are not taken into account. The calculations assume even terrain in the area of study and do not consider actual terrain elevations which could attenuate the signal. As a result, the calculated power density and corresponding $\%$ MPE levels reported below are much higher than the actual levels will be from the final installation.

## 4. Calculated \% MPE Results

Table 1 below outlines the power density information for the site. The Eversource omnidirectional and microwave antennas have narrow vertical beamwidths of $40^{\circ}$ and $1.7^{\circ}$, respectively; therefore, the majority of the RF power is focused out towards the horizon. Please refer to Attachment C, for the vertical patterns of the recently installed Eversource antennas. Likewise, the other transmit antennas exhibit similar directionality of varying vertical beamwidths. As a result, there will be less RF power directed below the antennas relative to the horizon, and consequently lower power density levels around the base of the facility. The calculated results in Table 1 include a nominal 10 dB off-beam pattern loss for the omnidirectional and panel antennas, and 30 dB off-beam pattern loss for the highly directional microwave dish to account for the lower relative gain below the antennas. Any inactive or receive-only antennas are not listed in the table unless specified otherwise, as they are irrelevant in terms of the \% MPE calculations.

| Carrier | Antenna <br> Height (Feet) | Operating <br> Frequency <br> (MHz) | Number of Trans. | ERP Per Transmitter (Watts) | Power Density $\left(\mathrm{mw} / \mathrm{cm}^{2}\right)$ | Limit | \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Eversource | 141.5 | 154.46375 | 1 | 250 | 0.0005 | 0.2000 | 0.24\% |
| Eversource | 141 | 153.695 | 1 | 250 | 0.0005 | 0.2000 | 0.25\% |
| Eversource | 139 | 145.14 | 1 | 250 | 0.0005 | 0.2000 | 0.25\% |
| Eversource | 138 | 224.22 | 1 | 250 | 0.0005 | 0.2000 | 0.26\% |
| Eversource | 137 | 451.1 | 1 | 250 | 0.0005 | 0.3007 | 0.17\% |
| Eversource | 135 | 939.4375 | 1 | 250 | 0.0005 | 0.6263 | 0.09\% |
| Eversource | 134 | 939.95 | 1 | 250 | 0.0005 | 0.6266 | 0.09\% |
| Eversource | 117 | 6034.15 | 1 | 7000 | 0.0002 | 1.0000 | 0.02\% |
| Eversource | 120 | 47.76 | 1 | 250 | 0.0007 | 0.2000 | 0.35\% |
| Eversource | 107 | 6735 | 1 | 7000 | 0.0002 | 1.0000 | 0.02\% |
| Eversource | 111 | 37.76 | 1 | 250 | 0.0008 | 0.2000 | 0.41\% |
| Eversource | 98 | 174 | 1 | 250 | 0.0011 | 0.2000 | 0.53\% |
| Eversource | 96 | 6805 | 1 | 7000 | 0.0003 | 1.0000 | 0.03\% |
| Eversource | 86 | 6004.5 | 1 | 7000 | 0.0004 | 1.0000 | 0.04\% |
| Eversource | 91 | 37.46 | 1 | 250 | 0.0012 | 0.2000 | 0.62\% |
| Eversource | 84 | 900 | 1 | 250 | 0.0015 | 0.6000 | 0.25\% |
| Eversource | 71 | 6805 | 1 | 7000 | 0.0006 | 1.0000 | 0.06\% |
| Eversource | 73 | 146.52 | 1 | 250 | 0.0020 | 0.2000 | 1.00\% |
| Eversource | 73 | 448.375 | 1 | 250 | 0.0020 | 0.2989 | 0.67\% |
| Eversource | 58 | 48.34 | 1 | 250 | 0.0033 | 0.2000 | 1.66\% |
| Eversource | 54 | 48.4 | 1 | 250 | 0.0039 | 0.2000 | 1.95\% |
| Eversource | 46 | 173.25 | 1 | 250 | 0.0056 | 0.2000 | 2.81\% |
| Eversource | 43 | 37.6 | 1 | 250 | 0.0066 | 0.2000 | 3.28\% |
| CSP | 78 | 851 | 1 | 315 | 0.0022 | 0.5673 | 0.39\% |
| CSP | 67 | 775 | 1 | 250 | 0.0024 | 0.5167 | 0.47\% |
| CSP | 53 | 775 | 1 | 199 | 0.0032 | 0.5167 | 0.63\% |
| CSP | 40 | 851.0125 | 1 | 158 | 0.0049 | 0.5673 | 0.87\% |
| T-Mobile | 125 | 2500 | 1 | 3590 | 0.0091 | 1.0000 | 0.91\% |
| T-Mobile | 125 | 2500 | 1 | 3590 | 0.0091 | 1.0000 | 0.91\% |
| T-Mobile | 125 | 700 | 1 | 2256 | 0.0057 | 0.4667 | 1.23\% |
| T-Mobile | 125 | 600 | 1 | 1128 | 0.0029 | 0.4000 | 0.72\% |
| T-Mobile | 125 | 600 | 1 | 1128 | 0.0029 | 0.4000 | 0.72\% |
| T-Mobile | 125 | 1900 | 1 | 3166 | 0.0080 | 1.0000 | 0.80\% |
| T-Mobile | 125 | 2100 | 1 | 4308 | 0.0109 | 1.0000 | 1.09\% |
| T-Mobile | 125 | 1900 | 1 | 2034 | 0.0052 | 1.0000 | 0.52\% |
| T-Mobile | 125 | 1900 | 1 | 4034 | 0.0102 | 1.0000 | 1.02\% |
| Eversource | 87 | 5945.2 | 1 | 11147 | 0.0006 | 1.0000 | 0.06\% |
| Eversource | 135 | 217 | 4 | 124 | 0.0011 | 0.2000 | 0.54\% |
| - |  |  |  |  |  | Total | 25.92\% |

Table 1: Proposed Facility \% MPE ${ }^{2} 3$

[^6]
## 5. Conclusion

The above analysis concludes that RF exposure at ground level with the new Eversource 220 MHz and microwave antenna installation is below the maximum power density limits as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Using the conservative calculation methods discussed herein, the highest expected percent of Maximum Permissible Exposure at ground level with the proposed installation is $\mathbf{2 5 . 9 2 \%}$ of the FCC General Population/Uncontrolled limit.

As noted previously, the calculated \% MPE levels are more conservative (higher) than the actual levels will be from the finished installation.

## 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in FCC OET Bulletin 65 Edition 97-01, IEEE Std. C95.1, and IEEE Std. C95.3.

| Report Prepared By: | Sohail Usmani |
| :--- | :--- |
|  | Senior RF Engineer |
| C Squared Systems, LLC |  |

February 7, 2022
Date C Squared Systems, LLC

Keth wellante
Reviewed/Approved By: Keith Vellante
Director - RF Services
C Squared Systems, LLC

## Attachment A: References

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering \& Technology
IEEE C95.1-2005, IEEE Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz IEEE-SA Standards Board

IEEE C95.3-2002 (R2008), IEEE Recommended Practice for Measurements and Computations of Radio Frequency Electromagnetic Fields With Respect to Human Exposure to Such Fields, $100 \mathrm{kHz}-300 \mathrm{GHz}$ IEEE-SA Standards Board

## Attachment B: FCC Limits for Maximum Permissible Exposure (MPE)

(A) Limits for Occupational/Controlled Exposure ${ }^{4}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength $(\mathrm{E})$ <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength $(\mathrm{E})$ <br> $(\mathrm{A} / \mathrm{m})$ | Power Density $(\mathrm{S})$ <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-3.0$ | 614 | 1.63 | $(100)^{*}$ | 6 |
| $3.0-30$ | $1842 / \mathrm{f}$ | $4.89 / \mathrm{f}$ | $\left(900 / \mathrm{f}^{2}\right)^{*}$ | 6 |
| $30-300$ | 61.4 | 0.163 | 1.0 | 6 |
| $300-1500$ | - | - | $\mathrm{f} / 300$ | 6 |
| $1500-100,000$ | - | - | 5 | 6 |

(B) Limits for General Population/Uncontrolled Exposure ${ }^{5}$

| Frequency <br> Range <br> $(\mathrm{MHz})$ | Electric Field <br> Strength (E) <br> $(\mathrm{V} / \mathrm{m})$ | Magnetic Field <br> Strength (E) <br> $(\mathrm{A} / \mathrm{m})$ | Power Density $(\mathrm{S})$ <br> $\left(\mathrm{mW} / \mathrm{cm}^{2}\right)$ | Averaging Time <br> $\|\mathrm{E}\|^{2},\|\mathrm{H}\|^{2}$ or S (minutes) |
| :---: | :---: | :---: | :---: | :---: |
| $0.3-1.34$ | 614 | 1.63 | $(100)^{*}$ | 30 |
| $1.34-30$ | $824 / \mathrm{f}$ | $2.19 / \mathrm{f}$ | $\left(180 / \mathrm{f}^{2}\right)^{*}$ | 30 |
| $30-300$ | 27.5 | 0.073 | 0.2 | 30 |
| $300-1500$ | - | - | $\mathrm{f} / 1500$ | 1.0 |
| $1500-100,000$ | - | - |  | 30 |
|  |  |  |  |  |
| $\mathrm{f}=$ frequency in $\mathrm{MHz} *$ Plane-wave equivalent power density |  |  |  |  |

Table 2: FCC Limits for Maximum Permissible Exposure (MPE)

[^7]

Figure 1: Graph of FCC Limits for Maximum Permissible Exposure (MPE)

Attachment C: Eversource Antenna Data Sheets and Electrical Patterns
217 MHz


Attachment D: Current CSC Power Density Data for the Subject Facility (07/16/2021)

| Carrier | Antenna <br> Height (Feet) | Operating <br> Frequency (MHz) | Number of Trans. | ERP Per <br> Transmitt er (Watts) | $\begin{gathered} \text { Power } \\ \text { Density } \\ \left(\mathrm{mw} / \mathrm{cm}^{2}\right) \end{gathered}$ | Limit | \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Amateur Radio | 126 | 448.325 | 1 | 650 | 0.00162 | 0.2989 | 0.54\% |
| Amateur Radio | 126 | 224.22 | 1 | 100 | 0.00025 | 0.2000 | 0.12\% |
| CL\&P | 127 | 153.695 | 1 | 5 | 0.00001 | 0.2000 | 0.01\% |
| CL\&P | 127 | 451.1 | 1 | 189 | 0.00046 | 0.3007 | 0.15\% |
| CL\&P | 127 | 154.46375 | 1 | 990 | 0.00243 | 0.2000 | 1.22\% |
| CL\&P | 122 | 952.55625 | 1 | 71 | 0.00019 | 0.6350 | 0.03\% |
| CL\&P | 125 | 937 | 3 | 200 | 0.00152 | 0.6247 | 0.24\% |
| CL\&P | 115 | 48.34 | 1 | 100 | 0.00030 | 0.2000 | 0.15\% |
| CL\&P | 109 | 6765 | 1 | 5250 | 0.01780 | 1.0000 | 1.78\% |
| CL\&P | 102 | 6835 | 1 | 309 | 0.00121 | 1.0000 | 0.12\% |
| CL\&P | 102 | 6735 | 1 | 1738 | 0.00678 | 1.0000 | 0.68\% |
| CTSP | 108 | 800 | 5 | 100 | 0.00173 | 0.5333 | 0.32\% |
| CL\&P | 92 | 6805 | 1 | 1660 | 0.00807 | 1.0000 | 0.81\% |
| CL\&P | 81 | 6865 | 1 | 288 | 0.00184 | 1.0000 | 0.18\% |
| CL\&P | 81 | 37.76 | 1 | 100 | 0.00064 | 0.2000 | 0.32\% |
| CL\&P | 58 | 48.4 | 1 | 120 | 0.00160 | 0.2000 | 0.80\% |
| CL\&P | 53 | 53.05 | 1 | 100 | 0.00163 | 0.2000 | 0.81\% |
| CL\&P | 52 | 37.46 | 1 | 115 | 0.00195 | 0.2000 | 0.98\% |
| CL\&P | 38 | 37.6 | 1 | 446 | 0.01566 | 0.2000 | 7.83\% |
| CL\&P | 37 | 173.25 | 1 | 204 | 0.00763 | 0.2000 | 3.82\% |
| CL\&P | 37 | 928.55625 | 1 | 32 | 0.00120 | 0.6190 | 0.19\% |
| T-Mobile | 125 | 2500 | 1 | 3590 | 0.0091 | 1.0000 | 0.91\% |
| T-Mobile | 125 | 2500 | 1 | 3590 | 0.0091 | 1.0000 | 0.91\% |
| T-Mobile | 125 | 700 | 1 | 2256 | 0.0057 | 0.4667 | 1.23\% |
| T-Mobile | 125 | 600 | 1 | 1128 | 0.0029 | 0.4000 | 0.72\% |
| T-Mobile | 125 | 600 | 1 | 1128 | 0.0029 | 0.4000 | 0.72\% |
| T-Mobile | 125 | 1900 | 1 | 3166 | 0.0080 | 1.0000 | 0.80\% |
| T-Mobile | 125 | 2100 | 1 | 4308 | 0.0109 | 1.0000 | 1.09\% |
| T-Mobile | 125 | 1900 | 1 | 2034 | 0.0052 | 1.0000 | 0.52\% |
| T-Mobile | 125 | 1900 | 1 | 4034 | 0.0102 | 1.0000 | 1.02\% |
|  |  |  |  |  |  | Total | 29.04\% |



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[^0]:    ${ }^{1}$ It should be noted that the Power Density Report denotes each channel as a transmitter. The depiction of antennas in the Structural Analysis and Construction Drawings accurately reflects the number of antennas. Also, the "Antenna Height" column on Table 1 in the Power Density Report reflects the Transmit or "TX" antenna centerline.

[^1]:    

    876F-70-2HSMP40DF1/2

[^2]:    Note:

    1) Antenna to be installed on existing pipe mount
[^3]:    Consider Moments - Legs
    Consider Moments - Horizontals
    Consider Moments - Diagonals Use Moment Magnification
    Use Code Stress Ratios
    Use Code Safety Factors - Guys
    Escalate Ice
    Always Use Max Kz
    Use Special Wind Profile
    $\sqrt{ }$ Include Bolts In Member Capacity
    Leg Bolts Are At Top Of Section
    $\sqrt{ }$ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric

[^4]:    ${ }^{1} P_{u} / \phi P_{n}$ controls

[^5]:    ${ }^{1}$ Stamped Black \& Veatch site drawings dated 1/19/2022 (Rev. 1).

[^6]:    ${ }^{2}$ The operating parameters for the Eversource and CSP (CT State Police) were provided directly by each respective operator. The T-Mobile information was sourced from the CSC Power Density Database dated 07/16/2021. For reference, this data is included as Attachment D. Please note that $\%$ MPE values listed are rounded to two decimal points and the total $\%$ MPE listed is a summation of each unrounded contribution. Therefore, summing each rounded value may not identically match the total value reflected in the table.
    ${ }^{3}$ Antenna heights listed for Eversource are in reference to the antenna centerline and based upon information provided by Eversource with respect to the Black \& Veatch Structural Analysis Report dated 01/13/2022. The available data for the CSP antennas do not have a one-toone match with the structural analysis, so a worst-case antenna height was applied for those antennas.

[^7]:    ${ }^{4}$ Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure
    ${ }^{5}$ General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure

